ANNEX B

Canal Lining Plan

THE STUDY ON THE LINING OF DISTRIBUTARIES AND MINORS IN PUNJAB IN THE ISLAMIC REPUBLIC OF PAKISTAN

VOLUME II

ANNEX B CANAL LINING PLAN

Table of Contents

B.1 Design Discharge	•••••	B -	1
B.1.1 Authorized Discharge			
B.1.2 Design Discharge	••••	В -	1
B.2 Design Criteria	••••	В -	2
B.2.1 General		В -	2
B.2.2 Basic Design Concept		В -	4
B.2.3 Design Criteria		В -	6
B.3 Cost Comparison		В	8
B.3.1 Comparison by Material		B -	8
B.3.2 Comparison on Canal Section		В-	9
B.4 Lining Plan		В-	9

LIST OF TABLES

Table B - 1(1/3)	Breakdown of Authorized and Designed Discharge
	Calculation for LJC AreaBT - 1
Table B - 1(2/3)	Breakdown of Authorized and Designed Discharge
-	Calculation for LCC Area BT - 12
Table B - 1(3/3)	Breakdown of Authorized and Designed Discharge
	Calculation for CBDC Area
Table B - 2	Material for Canal Lining BT - 32
Table B - 3	Summary Table of Canal Route Survey for LJC AreaBT - 33
Table B - 4	Summary Table of Canal Route Survey for LCC Area BT - 34
Table B - 5	Summary Table of Canal Route Survey for CBDC Area BT - 35
Table B - 6	Sedimentation Data for Lower Jhelum Canal
Table B - 7	Sedimentation Data for Lower Chenab Canal System BT - 37
Table B - 8	Summary of Survey Data of Soil Mechanics
Table B - 9	Cost Comparison of Lining on Distributaries
	and Minors by Different B/D Ratio
	LIST OF FIGURES
.	
Figure B - 1	Actual Progress of Canal Route Survey BF - 1
Figure B - 2	Proportionality Comparison of Outlet (AOSM)BF-2
Figure B - 3	Design B/D Ratio for Discharge
Figure B - 4	Design Flow-Chart for Lining of Distributaries and Minors BF - 4
Figure B - 5	Alternative Lined Canal Section
Figure B - 6	Typical Cross Section of Lined Canal

Annex B Canal Lining Plan

B.1 Authorized Discharge and Design Discharge

B.1.1 Authorized Discharge

The authorized discharge in the Study area is based on the so-called Irrigation Branch Method which was derived from the experience gained by the Department during the last hundred years. The Full Supply Factor which should be derived from the statistical records for other projects in operation, is the duty, i.e. the area successfully irrigated during a base period, per cusees of mean supply at channel head, was determined without considering crop water requirements, since the canal system in the Study area was designed with the objective of extensive irrigation to bring more areas under irrigation in order to settle more people.

After determining the full supply factor, the Intensity of Irrigation, which is the percentage of the cultivable area irrigated annually, was determined to be 75% in the area. By studying different factors such as the type of soil, cultivation, habits of the people, marketability, climate, etc. the quantity of area to be irrigated in Kharif as well as Rabi was fixed. The ratio of area to be irrigated in Kharif and Rabi is known as Kharif-Rabi Ratio, which was originally determined to be 35% -40% per annum. After taking all the above factors into consideration, the number of cusees required at the outlet to irrigate one thousand acres of area fit for irrigation, known as Water Allowance, was fixed to be 2.84 cusees/1.000 acres.

The authorized discharge of each outlet has been updated from time to time in the Outlet Register of the respective branch offices on the basis of area to be supplied with irrigation water inclusive of the other allowances such as gardens or paddocks which are entitled to an extra supply. The latest authorized discharge at each outlet which was provided by the respective branch offices was adopted as the basis of the design discharge for preliminary design as will be discussed in the subsequent paragraphs.

B.1.2 Design Discharge

A series of discussions was made between the Chief Engineers/Superintending Engineers/Executive Engineers of the respective Irrigation Zones and the IICA Study Team for the determination of the design discharge. It is a common practice to adopt Consumptive Use Method to estimate irrigation water requirement. The study made in the Inception Report indicates that the water requirement thus estimated is as high as four times of the

actual surface water supply during the peak demand period with increase of crop intensity almost to 150% under the pressure of growing population in the recent years. According to the request of PID, adjustment of design discharge was made based on the above water requirement on the original condition that the crop intensity is 75% consisting of 35% in Kharif and 40% in Rabi. As a result, it is understood that the design discharge in the peak month is also as high as two times of the present surface water supply.

As discussed in the preceding paragraphs, design discharge estimated rationally based on the consumptive use cannot be justified in view of the limited amount of total water resources for Punjab. It is also noted that there is no master plan for the increase of application of water despite the fact that the area is suffering from shortage of water. Nonetheless it is proposed that the design discharge be increased by 10% of present authorized discharge at outlet considering the future development of water resources including diversion of water from the Indus and creation of reservoirs by constructing dams in the near future. The procedure for the calculation of the proposed design discharge for the priority canals for lining is as follows and calculation sheets are attached as Table B-1. It is understood that after lining of the channel, saved water will be the advantage for the beneficiaries in terms of quantity and equity.

- (1) The last updated authorized discharge at each outlet and CCA stated in the Outlet Register in the respective branch offices has been adopted as the basic figure.
- (2) The authorized discharge stated above has been increased by 10% and accumulated from the tail to the head of the distributaries and the minors.
- (3) The channel discharge has been designed by adding the standard absorption loss (Oab) stated in the guidelines¹ for unlined channels;

 $Qab = 0.0133 \times L \times Q^{0.5625}$, where L: length of section (1,000 feet) and Q: discharge of the section in cusec.

B. 2 Design Criteria

B.2.1 General

The design criteria was prepared based on the design concept to attain 1) silt transportation throughout the canals from the head to the tail with constant velocity by way

¹Source: Design Guidelines for Irrigation Channels, Design Directorate Publication No.

of steeper gradient and narrower/deeper section, 2) maximum depth limited up to 5 feet and 3) proportional distribution of water and silt through each outlet against discharge fluctuation in the parent canal. Most of the specifications stated below are described on water depth basis according to the suggestions made by Design Directorate. 3 inch thick in-situ concrete lining is generally proposed as lining method with proper earthwork by way of by-pass(diversion) construction. Precast concrete method and/or membrane are also recommended for further study to be applied where discharge is small or construction work is limited within the canal closure period.

Discussion meeting on the design criteria was held on 19th November, 1996. The following items are discussed for subject of design criteria for fined channels. Design Directorate sent comments and requested its review and confirmation among engineers concerned. Summary of the comments and conclusion by the study team are the followings.

- Design Directorate suggested 1:1.5 side slope where canal depth is deeper than 4 feet. The study team concluded that 1:1.25 slope can make slope stable enough.
- Freeboard of 1 to 1.5 feet were claimed by the Design Directorate and it was concluded that 1 foot freeboard can convey increased discharge in future up to 50 % (10% is already counted into designed full supply level) and large enough. 0.5 feet freeboard was proposed by the study team for water depth is not more than 2 feet.
- Transition to and from the existing lining portions is to be taken part into design.
- Smoothening of corners in the canal prism is to be taken into consideration in the design.
- Proportionality of water and silt distribution were proved as stated below.

Contract agreement concluded on 26th day of October, 1996 between the JICA Study Team and the Khyber Consulting Engineers. Field works were completed on 20th of December, 1996 and survey results were checked and approved by the Study Team. The final report on the survey will be prepared in December. Actual work progress are given in Figure B-1 and Table B-2~4 show the summary of canal route survey. The total length of distributaries and minors to be surveyed was 553.2 km. Survey interval along center or control line is to be 600m (approx. 2 RD) and all points where any discontinuities are observed in the cross area, shape, slope, section lined/un-lined, drop, regulator or so. Elevations of canal bottom center and both banks are surveyed. Beginning and end points of existing lining portion, all points where any discontinuities such as the above were observed, and canals section by above stated interval covering the right-of-way of each canal. Vegetation, water-logging and surface condition within the right-of-way are observed. Kind,

condition and location of each and every structure are observed and checked. Bottom elevations of watercourses at the head connecting to each outlet are listed.

The table given below shown the comparison of length of canals of the contract of quantities and actual survey quantities.

No.	Name of Canal System	Contract	Surveyed	(Unit : Km) Balance
110.				
l.	Lower Jhelum Canal	198.48	185.48	-13.00
2.	Lower Chenab Canal	303.69	289.14	-14.55
3.	Central Bari Doab Canal	51.06	66.65	+15.59
	Total	553.23	541.27	-11.96

According to the data² by ISRIP and their analysis, diameters of soil particles of suspended load at 90% pass and 50% pass are 0.066 mm and 0.027 mm for LJC area and 0.185 mm and 0.112 mm in LCC area. Concentrations of suspended load above 0.062 mm are 7.7 PPM only in LJC and 245.0 PPM in LCC area. The data above show that water flowing in LJC area are of less silt suspension and most of the suspended load can be washed throughout to farm land by normal flow velocity (1-1.5 ft/sec). Condition in LCC on the other hand requests special treatment since most suspended load precipitates within distributaries and minors canal reaches and concentrations are high. Table B-5&6 show the data from ISRIP.

B.2.2 Basic Design Concept

- (1) Soil mechanics survey was conducted on 10 points within the study area and its results show dominance of sandy silt in LCC area and more clayer silt in the other areas. Permeability are relatively low in all area. Inside friction angles and cohesion show that earth material acquired near by canals are suitable for embankment and that canal inside slope could be designed as sharp as 1: 1. Table B-7 shows the summary data of the survey.
- (2) Water tightness of concrete is a important property as lining material. Methods to increase the water tightness are 1) application of admixtures AE or so, 2) improvement of water cement ration and size of aggregate and 3) careful construction supervision. According to evaluation of the methods above, approaches recommended to be applied to the project are 1) application of AE admixture to decrease entrapped air and water cement ratio, 2) application of rich mixed concrete (1:2:4) to decrease permeability of concrete, 3) application of steel slip form and rather small aggregate size to reduce required volume of water and 4)

² Siltation Data taken by ISRIP for 1982-1984 for branches and distributaries in LCC and main canal in LJC.

execution of careful supervision on even and less air content concrete as well as careful eurling to avoid surface crack.

Comparative study result on proportionality of outlet performances by types of outlets is shown in Figure B-2, where Type A (Hs = $0.3 \times D$, Y = Hs), Type B (Hs = $0.46 \times D$, Y = $0.23 \times D$), Type C (Hs = $0.375 \times D$, Y = Hs) and Type D (Hs = $0.5 \times D$, Y = $0.3 \times D$). Considering discharge fluctuation of current condition as well as future increase of discharge, Hs and Y are proposed to be $0.375 \times D$ for AOSM(Type C). Proportionality of outlet discharge by location of outlet for different designed water depth of parent canal are also studied and ensured for the Type C outlet selected above. According to the working paper 37 of SWABI SCARP, AOSM outlet shows higher capacity of silt absorption through the outlet than the conventional APM outlet. Outlet discharges(Q_{out}) are calculated;

$$Q_{out}(AOSM) = k \times Bt \times Y \times Hs^{0.5}$$
 and $Q_{out}(Open Flume) = k \times Bt \times G^{1.5}$

(4) Depth & Velocity Oriented Design

The Manning's formula is to be employed for hydraulic design. Designed full supply level at each outlet is to be set not lower than the last design full supply level to ensure the better condition. Section is to be changed at the points of outlets where discharge changes more than 10% of the head discharge or at drops only. No design modification will be given for the existing lined portion. Proper transition or some countermeasures will be given in case that hydraulic regime in the new-lined section is extremely different from that in the existing lined portion.

Head reaches where discharge is relatively large are to be designed with the design B/D given to the specific discharge and with slope which is same as or milder than the existing design not to exceed maximum depth and maximum velocity and subsequently same procedure is to be applied to keep the standard velocity by changing gradient for relevant discharge for the upstream portion. Downstream portions are to be designed with steeper slope so as to keep the standard velocity. B/D ratio proposed is shown in Figure B-3. Velocity and depth of water at the tail is to be carefully designed so as to clear at least the minimum allowable velocity and depth. Design flow chart are shown in Figure B-4.

(5) Canal related Structure

1) AOSM or open flume outlets are proposed. AOSM is suitable for upstream of the channel where operation head is enough, 2) New VR(village road) bridge is proposed at

such points to minimize crossing of canal by heavy machinery or cattle/buffalo. Footpath rank bridges are proposed to be replaced with VR bridge, 3) New steps are proposed to be installed at one side of channel in turn. Buffalo wallow is proposed to be located at the head of the watercourses nearest to each bridges both from upstream and downstream and 4) Discharge control gates are proposed at the diversion facilities where no gates are installed presently. Meter Flume is to be replaced with a couple of stuff gauges.

B.2.3 Design Criteria

(1) Lining Material and its Characteristics

As practical lining material, concrete lining of 3 inch thick over 1 inch mortar plaster on the smoothen/trimmed surface in trapezoidal section are proposed. Smoothening at slope toe corner is proposed to avoid silt precipitation. Roughness coefficient is assumed to be 0.016. Side slope = 1: 1 for the sections where the water depth is less than 3 feet(0.91 m) and 1:1.25 for the case of deeper water depth than 3 feet are proposed.

(2) B/D Ratio, Depth of Water, Velocity and Freeboard

The designing discharge range is approximately from 4 cusec(0.12m3/s) to 500 cusec(11m3/s) and proposed B/D ration are from 0.8(identical for 1:1 section) to 4.5 respectively as shown in Figure B-3. Minimum bottom width (B min) is set at 1.5 feet (0.46m) to keep workability. Velocity is proposed to be kept higher than 2 ft/s(0.61 m/s), design standard velocity, throughout but minimum allowable velocity of 1.5 ft/s(0.46 m/s) is also given for the case where the relevant gradient could not allow the standard velocity inevitably. Maximum velocity is allowed up to 4 ft/s (1.22 m/s) considering allowable velocity of 3 inch lining and safety of children and baby cattle.

Maximum depth is proposed to be no deeper than 5 feet (1.52 m) considering up-lift pressure at the canal bottom and sides during small discharge/empty periods and easiness of construction. Standard depth range for design are from 4 to 2 feet and minimum depth is no shallower than 1.5 feet (0.46m) according to a standard depth of 1 foot over crest at tail cluster. Freeboard within lining is proposed as 1.0 foot (0.30 m) where water depth is deeper than 2 feet (0.61 m) and as 0.5 feet (0.15 m) where water depth is equal to or shallower than 2 feet (0.61 m). In accordance with USBR criteria 0.5 feet (0.15 m) earthen freeboard is also proposed throughout for all the channels.

(3) Earthwork and Dimension of Canal Section

Specifications of earthwork and dimension of improved canal cross section are proposed as follows. Stripping thickness of 0.2 m or 0.3 m are proposed respectively for outside and inside of canal prism. Bank cutting thickness within canal prism of 1.0 m or 2.0 m and over-embankment exceeding designed lining surface is proposed by 0.5 m or 1.0 m respectively for the cases that water depth is shallower than or equal to/deeper than 3.5 feet. Compaction is to be done up to designed lining height and earthen freeboard is formed by spoil banking.

Width and minimum embankment from field level for operation and maintenance road are 4.0 m and 0.3 m(1 foot) respectively. Bank width for filling section are proposed to be 1.0 m (Q < 50 cusec), 1.5 m (50 < Q < 150 cusec), 2.0 m (150 < Q < 300 cusec) and 2.5 m (Q > 300 cusec). Half width are respectively proposed for cutting section.

(4) Outlet

All outlets are to be renewed at the construction of lining. Pipe cum APM/AOSM with a outlet chamber is proposed generally. Operation head (Hm) = $0.82 \times Hs - 0.5 \times Bt$ are to be retained for the purpose of proportional operation of outlets as a semi-modular against discharge fluctuation. Open flume outlet remains as tail cluster at the tail or where Hm could not be ensured. Steel guide block for the adjusting part and covering (not air-tight) over the chamber are proposed. Outlet discharge measuring gauge is proposed to be installed at the outlet mouth. Hs and Y are proposed to be $0.375 \times D$ for AOSM. Open flume is proposed to set at $0.9 \times D$ depth. Width of orifice (Bt) are proposed to employ standard sizes such as 0.2, 0.25, 0.32, 0.4, 0.5 & 0.63 feet.

(5) Other Related Structures

Bridge; New VR(village road) bridge (PC slab with effective width of 3.7m by standard of highway department) is proposed at such points to minimize crossing of canal by heavy machinery or cattle/buffalo where cattle are obviously crossing canals, bank are damaged by buffalo watering or where congested houses and shops nearby. Installation interval is to be not shorter than 5 RD considering that all the existing bridges are to be used with necessary repair work or replaced by same rank bridge and footpath rank bridges are to be replaced with VR bridge.

<u>Drops</u>; Drops are proposed to be re-designed according to the new canal design or removed. Vertical drop (water cushion type) are proposed for all.

Steps & Buffalo Wallow; All the existing steps are to be removed at construction and new steps are proposed at one side of channel in turn so as to keep habitats and cattle from cross-passing there. To minimize bank damage by cattle and buffalo, buffalo wallow is proposed at the head of the watercourses nearest to each bridge both from upstream and downstream.

Diversion Facilities from Branch Canals & Meter Flume; Discharge control gates are proposed at the diversion facilities where no gates are installed presently. Cost incurred for earthworks and civil works required for gate installation shall be borne by PID. Meter Flume is to be removed at construction and replaced with a couple of stuff gauges installed within head reaches of each channels since existing meter flumes are observed out of use/function. For monitoring purpose, H/Q (water depth - discharge) curve shall be prepared by PID using the stuff gauges right after construction.

B.3 Cost Comparison

B.3.1 Comparison by Material

Unit construction cost and major repair cost for 10 years are estimated roughly for cost-benefit comparison study below for average canal assumed (30 cusec). Total cost for concrete and brick lining are close each other but periodical major repair would be required for brick lining to keep long-term water tightness and hence repair cost is higher and much conditional. Accordingly, concrete and brick lining could be economically viable. Application of membrane as a whole is denied but partial application for the particular area are to be left as alternative method considering its high water tightness and durability against alkali/salt. In accordance with all study results of literature review, field inspection, technical discussions, pre-qualification study and rough cost-benefit evaluation above, concrete lining is basically proposed for the project. Sections compared are shown in Figure B-5.

Lining Method	(relative cost	Repair Cost (% of initial const. cost)	Long- term water- Tightness	Availability of Const. Material
A: Concrete Lining	1.0	3-5	Δ	0
B: Brick Lining	0.8	8-12		0
C: Membrane Lining	2.0	1-3	0	Δ

B.3.2 Comparison on Canal Section

Cost comparison of concrete lining sections by different B/D ratio were done using present canal prism situation and design B/D ration according to relevant discharges. Results of the comparison state that 1) work volumes for concrete and mortar as well as lining surface preparation increase relatively to B/D ration and hence narrowest section shows the smallest cost, 2) earthwork volumes show fluctuation and more corresponding to current canal prism than B/D ratio, and therefore 3) since unit price of concrete work is quite higher than that of earthwork, the comparison is concluded that the narrowest section come to be the most economical section in general. On the other hand side, canal depth of the narrowest section (B/D = 0.8) comes very deep. It is accordingly decided that the narrowest section will be applied to the project in general with a depth regulation of about 1.5 m (5 feet) considering easiness of construction work and safeties of habitats and households. Results of cost comparison by sections are shown in Table B-8.

B.4 Lining Plan

According to the references, study results of similar projects and field investigation results, construction methods applicable for distributaries and minors are a)temporary diversion method, b)construction of new canal by the original canal trace and c)construction on original trace while canal closure period. Compaction and trimming of canal slope are difficult and critical path for the construction within the canal closure period.

Proper supervision on earthwork quality control is one of the most important factor to affect life expectancy of canal lining. According to the advantage of temporary diversion method which would make continuous construction through an year round and easy quality control possible, temporary diversion method is proposed to be applied for the project in general and meteorological data stands for negligible breaks of continuous construction. Quality control strictly on water contents of earth material for embankment, cement mix as well as curing stage are recommended to ensure long term durability of canal bank and lining. Steel slip form, severe control on cement mix and long enough curing under wet condition are also proposed to be emphasized to make seepage minimum through canal prism. Lining sections at construction and at completion are shown in Figure B-6.

TABLES

Table B - 1 (1/3) Breakdown of Authorized and Design Discharge Calculation for LJC Area

N. State of St.			Control		Village	Chack No	Outlet Discharge	charge	Section	8	Design	E	Outlet CCA	1	Section Im	Improved under	Remarks
Watercourse	(feet)	(8)	Distance				Authorized	Design		arge	Discharge	١.	(acre)	<u>a</u>			
			(feet)	(w)		:	(cusec) (m3/s)	اءا	(casec)	(m,7/s)	(casec)	(m3/s)	:		(ha)		
Pindi Distributary											٠.				٠		
•						*.				0.46		·			2.285		
390/L	390	-119	390	611		85/NB	1.34 0.038	38 1.47	16.34	0.46	19.12	0.541	451	183	2,285		
246 4302/L	4302	1311	3912	1192		85/NB				0.42	17.62	0.45 7	/Q ;	9	20102	•	
10200/L	10200	3109	2898	1798		91/NB				0.36	14.7]	0.417	9	ì	 \$		
11300/L	11300	3444	1188	335		91/VB				0.31	12.42	0.352	791	320	1,527		
14700/R	14700	248	250	1036 R Depot	Sepor					0.24	98.6	0.279	431	174	1.206		
715031 0361	1603	7557	1221	\$ \frac{4}{5}		84/NR				0.21	8.36	0.237	390	158	1.032		
1	3000	3 6	1	} :		QIV Y	114 0022			810	7 08	0000	383	155	874		
7/00001	0000	200	1	, i		04470				3	63.4	371	¥15	300	710		
ZZ500/11L	2500	0858	3	1/6		1/NB				3	9	3	9 6	3 2) i		
22500/TF	22500	6858	0	0		8IVI8				2 :	ç ;	211.0	5 ;	Š	710		
22500/TR	22500	8289	0	0 R.Depot	Sepor	R.Depot		_		0.0	1.68	0.048	340	219	219		
							6.34 0.463	53					2.646 2.285	2285		,	
Hujjan Distributary							1.	; ;; }						•	4		
•			. ′		:	:				5.16					25.236		
5698/R	5698	1737	8698	1737 Hujan	uat		1.39 0.039			5.16	228.02	6.458	489		25,236		
8250/R	8250	2515	2552	778 Hujan	<u> </u>		2.54 0.072	٠.	_	5.12	224.89	6369	833		25,039		
356 9000/L	0006	2743	750	229 Hujian	iiaa				3 178.30	5.05	221.39	6.270	427	٠.	24,677		
9400/R	9400	2865	8	122 Obc	Chowal				-	5.02	219.85	6.226	823	٠.	2502		
101507	10150	3005	750	229 Huilan	or ii		700 67 :			4.95	217.16	6.150	524	• -	24,171		
15648/	15648	4770	\$	1676 Rawana	wana		0.89 0.025		3 173.26	4.91	215.32	860.9	312		23,959		
16508/R	16508	5032	98	263 Ch	Chowal					4.88	212.84	6.028	791		23,833		
16730/1	16730	8	72	68 Rawana	Wana		-			4.82	210.15	5.951	532		23,513		
7774/1	17774	8.45	5	318 Tloni	·č			2		4.78	208.43	5.903	579		23,298		
0/7/0/1	7007	2	35	(C) 104	ιē					4.73	206.33	5.843	294		23,063		
1,000	0008	28.8	š	20 1100	Ē					4.70	205.37	5.816	786		22,944		
23500/R	23500	7163	\$500	1676 K.Raia	Saia.		0.98 0.028	28 1.08		2	202.90	5.746	345	041	22,626		
25577//	25577	7796	2077	633						9.5	200.37	5.674	\$65		22,487		
25593/R	25593	7801	16		K.Raja	:			1 161.32	4.57	198.07	5.609	868		22,258 OFWIN	W.W.	
28966/L	28966	8829	3373	1028						4.50	195.26	5.530	3439		21,894		Arian Minor(11.62)
29088/L	29088	8866	122	37 Uppi	Ē	19/SB		٠.		4.22	182.77	5.176	\$		20,503 OFWM	××	
29089/R	29089	8866		0 CB	0 Uppi/K.Raja					•	180.79	5.120	294		20,242 OFWM	٧×	
34634/1.		10556	5545	1690 K.Momir	Momin					4	179.88	5.8 4	823		20,123 OFWM		
36461/R		111113	1827	557			19.06 0.540		5 143.80	4.07	175.77	4.978	5748	-	19,767	3	Kot Momin Minor
36863/1		11236	402	123 K.Raja	Raia	:					152.97	4.332	357.5		17,441 OFWN	_	(22.35)
30380/8	39280	1072	7217	737 K	K Raja					3.50	151.76	4.298	320	142	17.296 OFWIN	ww	•
0,000	×15.60	0676					607 0 170			87 2	150.13	4.252	2140		17.155	\$	Kor Raia Minor(6.99)
4,000	0000	> (143	:	0.00				2 20	£2 ¢3	4 030	659	7,7	16 289 OFWA		
42020/K	02024	71101	70-1	;		000	5.0 e.				20.051	200	\$ 01. 2		16.025 OFWY	W.W.	
43203/L	43.203	13108	3	SO A.Raja	refe v				- •	•	170 80	2	2.5			To:	-
43210/R	43210	13170	. 7	, ,	K.Raja		_			7.7	138,38	3 6		X 9	0000	ř	100 / 100 /
43310/R	43310.	13201	8	<u>유</u>			13.85 0.392		7. 112.61	3.19	13/.82	5.50	60		70,01	ឆ្នាំ	British Milnorf 19.27)
49050/R	49050	14950	5740	1750		 	_	_		2.80	121.53	3,442	> .	2	13,873		
									. :	:			:				

Table B - 1 (1/3) Breakdown of Authorized and Design Discharge Calculation for LJC Area

Š	No. Number of	άχ	Section	on Village	Chack No.	Ourlet Dischargo	ngc	Section	ų	Design	e	Ourier CCA		Section Improved under	Remarks
૭	(onginal) Watercourse	(fect) (m)	Distance			Authorized	Design	Discharge	Ec	Discharge	•	(acre)	(ha)	25	
			(feet)	(E)		(cusec) (m3/s)	(cnsec)	(casec) ((m3/s) (cusec)	'm3/s}			(ha)	
Ä	375 49157/L	49157 14983	101	33 K.Raja		1.50 0.042	1.65	98.76	2.80	120,40	3,410	530		13,873	
		49178 14989	či	•		11.11 0.315	13.11	97.26	2.75	118.73	3.362	3728		(3,659	Sabowal Minor(13.11)
ક્ષ	376 49910/R	-	732	223	65/SB		0.95	86.15	7.4	19:501	2.931	305	122	12,150 OFWM	
92	378 54700/L		4790	1460	91/SB	1.10 0.031	1.21	85.29	2.42	83	2,860	386	157	12,028	
73		- 1	8	27	65/53	0.83 0.024	0.91	84.19	2.38	87.49	2.905	284	611	11.870 OFWM	
83			S482	1291	65/SB	1.68 0.048	1.85	83.36	2.36	01.53	2.875	265	239	11.751 OFWM	
83	381 61361/R		1089	332	91/SB	0.55 0.016	0.61	81.68	2.31	98.70	2.795	194	_	11.512 OFWM	
ည	61700/L	61700 18806	339	103		1.95 0.055	2.15	81.13	2.30	16.76	2.773	689	279	11,434	
31	62472/L	62472 19041	77	235			ς; δ	81.62	2.24	95.70	2,710	786	•	11,155	
33	62573/R	62573 19072	101	31		2.03 0.057	2.23	76.95	2.18	93.11	2.637	716		10,837	
33	382 71738/L	71738 21866	9165	2793 Laliani	•	1.90 0.054	5.03	74.9	2.12	98.06	2.573	899	270	10,547	
Ą	383 71852/R	71852 21900	114	35 Laliani		1.60 0.045	1.76	73,01	2.07	87.24	2.471	563		10,277 OFWM	
33	384 73000/R	73000 22250	1148	350 Laliani		2.10 0.059	2.31	71.41	2.02	85.46	2.420	740		10,049 OFWM	
9			8	122 Laliani				69.31	96.	82.96	2.350	358		9,749 OFWM	
3	386 75000/L		009			0.99 0.028	89	68.29	.93	81.78	2.316	349	141	9,604 OFWM	
38	387 76485/R	76485 23313	1485	453 Laliani		2.15 0.061	2.37	67.30	6.	80.44	2.278	757	308	9,463 OFWM	
33	388 78516/L	78516 23932	2031	619 Laliani		0.98 0.028	1.08	65.15	1.85	77.84	2.204	<u>4</u>	139	9,157	
4		78516, 23932	0			0.91 0.026	3.5	4.17	1.82	76.45	2.165	319	129	9,018 OFWM	
7	390 79968/R	79968 24374	1452	443 12/SB		2.69 0.076	2.96	63.26	1.79	75.45	2.137	947	383	8,888 OFWM	
45	391 80994/L	80994 24687	1026	313 12/58		1.68, 0.048	1.85	60.57	1.72	72.27	2.047	283	236	8,505 OFWM	
	83285/L	83285 25385	2291	869			10.91	58.89	1.67	70.27	86:	3239	1311	8,269	M. Wala Minor(10.91)
43		83350 25405	65	20 M.wala		1.12 0.032	1.23	49.66 89.66	1.4.1	59.03	1.672	394	159	6,958	•
র		87430 26649	4080	1244 M.wala	: -	0.23 0.007	0.25	48.54	1.37	57.79	1.637	72	న	6,799	
ž,	394 88477/L	88477 26968	1047	319 M.wala		1.75 0.050	1.93	48.31	1.37	57.01	1.614	611	247	6,770 OFWM	
ð,	395 89500/R	89500 27280	1023	312 M.WALA	65-SB	1.22 0.035	1.34	46.56	1.32	54.95	1.556	417	691	6,523 OFWM	
47	396 91868/L		2368	722 M.WALA	65-SB	1.25 0.035	1.38	45.34	1.28	53,47	1.514	23	171	6,354	
			252	77			12.13	8.8	:: 2:	51.80	1,467	3633	1470	6,183	Tangu Minor(12,13)
8 7			155	47	:S/SB	2.23 0.063	2,45	33.70	0.95	39.64	1.123	787	318	4,712 WAPDAIOFWM	
•		-	SE SE	983 Jaspal			22.36	31.47	68.0	37.17	1.053	6551	2651	4,394	Jaspal Minor(22.36)
\$			8	335	15/SB		8	12.51	0.35	14.49	0.410	320	230		
ଦ୍ଧ	_		2 <u>8</u> 2	295	15/88	0.80 0.023	0 88 88 9	8.1	0.33	13.42	0.380	280	113	1,613 OFWM	
51			1555	474		0.78 0.022	0.86	10.80	0.31	12.44	0.352	274	111	1.500	
22			ဇ္တ	9 Lalyani		'	1.17	10.02	0.28	11.49	0.325	342	138	1,389 OFWM	
ß			8	6 Lalyani		1.91 0.054	2.10	8.96	0.25	10.33	0.292	675	273	1,251 WAPDA/OFWM	
¥			7450	2271 Lalyani			1.08	7.05	0.20	8.22	0.233	ğ	5	977 OFWM	
55		•	0	0 Lalyani			0.15	6.07	0.17	6.83	0.193	51	77	837	
፠			3973	1211	13/SB	1.78 0.050	38.	5.93	0.17	6.67	0.189	286	238	816 OFWM	
53	415 111473/TCR		0	0	13/SB	1.73 0.049	8	4.15	0.12	4.57	0.129	277	234	578	
80			0	Õ,	13/SB	1.36 0.039	1.50	2,42	0.07	5.66	0.075	478	193	344 OFWM	
85	417 111473/TLL	111473 33977	0	0	13/SB	1.06 0.030	1.17	1.06	0.03	1.17		373	151	151	
						182.23 5.16	<u> </u>	:				62,359 23	236		

Table B - 1 (1/3) Breakdown of Authorized and Design Discharge Calculation for LJC Area

### 1700 Clear Clear Counce Cou	3	Coine Watercourse	((,,,)	Ê	Distance	e [*]	: :		γ	Authorized	Design	Discharge	28	Discharge	.	(acre)	(pa)	CCY	
Secondary 19/SB 1.36 0.039 1.50 9.87 0.28 11.62 0.33 481 1.40 0.040 1.54 8.51 0.24 9.89 0.280 496 2.80 Norman 1.42 0.040 1.54 8.51 0.24 9.89 0.280 496 2.80 Norman 1.42 0.040 1.54 8.51 0.24 9.89 0.280 496 2.80 Norman 1.42 0.040 1.54 8.51 0.24 9.89 0.280 496 2.80 Norman 1.04 0.029 1.14 5.69 0.16 5.50 0.186 3.67 3.77 3.75	5			Į.		(E)		- 1	(cusec.	(m3/s)		1 1	(5)	i i	m.3/s)			(ha)	
oman 1978	riar	1 Minor(RD 2890	%/L, Hu	jan D	istribut	ary)	1				34	9.87	0.28					1.392	
oman 1:40 0.040 1:54 8:51 0.24 9:89 0.280 496 2 oman 1:42 0.040 1:55 7:11 0.20 8:14 0.230 458 oman 1:42 0.040 1:55 7:11 0.20 8:14 0.230 458 oman 2:40 0.068 2.44 4.65 0.13 5.26 0.149 946 2.25 0.066 2.48 0.070 791 2.25 0.066 2.48 0.070 791 2.25 0.066 2.48 0.070 791 2.25 0.066 2.48 0.070 791 2.25 0.066 2.48 0.070 791 2.25 0.066 2.48 0.070 791 2.25 0.066 2.48 0.070 791 2.25 0.099 1:91 19:06 0.54 22.35 0.633 559.5 2.25 0.003 2.25 0.099 2.012 0.570 4.33 2.25 0.003 2.25 0.099 2.012 0.570 4.33 2.25 0.003 2.25 0.099 2.012 0.570 4.33 2.25 0.003 2.25 0.099 2.012 0.570 4.33 2.25 0.099 2.25 0.099 2.20 2.20 0.090 2.20 2.20 0.090 2.20 2.2	1	27.5 4.4.5.4.4	0.36.0	370	7,40%	1270	أ	9/CB	-	4 0.039	Ç	9.87	0.28	1	0.33	481	195	1,392 OFWM	
oman 1,20 0,040 1,56 7,11 0,20 8,14 0,230 458 oman 2,40 0,029 1,14 5,69 0,16 6,55 0,186 367 oman 2,40 0,028 2,64 4,65 0,13 5,26 0,149 846 oman 2,20 0,068 2,64 4,65 0,13 5,26 0,149 846 367 oman 2,20 0,064 2,48 2,23 0,06 2,48 0,070 791 omin 1,23 0,035 1,39 1,30 1,30 0,34 1,31 1,30 0,34 1,31 1,30 0,34 1,31 1,30 0,34 1,31 1,30 0,34 1,31 1,30 0,34 1,31 1,30 0,34 1,31 1,30 0,34 1,31 1,30 0,34 1,31 1,30 0,34 1,31 1,45 0,32 1,24 0,366 550 1,33 1,33 1,33 1,33 1,33 1,33 1,33 1,3	~ a (1/1/4/1/201	1 5	2 (27.0	:						70		0320	707	201	1 197 OFWN	
oman 1.42 0.040 1.56 7.11 0.20 8.14 0.250 4.55 oman 2.40 0.068 2.48 2.25 0.06 2.48 0.070 791 2.25 0.064 2.48 2.25 0.06 2.48 0.070 791 2.25 0.064 2.48 2.25 0.06 2.48 0.070 791 2.25 0.064 2.48 2.25 0.06 2.48 0.070 791 2.25 0.064 2.48 2.25 0.06 2.48 0.070 791 2.25 0.064 2.48 2.25 0.06 2.48 0.070 791 2.25 0.065 2.48 0.070 791 2.25 0.065 2.48 0.070 791 2.25 0.065 2.48 0.070 791 2.25 0.065 2.48 0.070 791 2.25 0.065 2.48 0.070 791 2.25 0.065 2.48 0.070 791 2.25 0.085 2.25 0.0	c i	463 9000/R	8	2/43	8	13/3 KOT M(пещо		t. :	3		7	7.0				2 0	300	
oman 1.04 0.029 1.14 5.69 0.16 6.55 0.186 367 oman 2.25 0.064 2.48 2.25 0.06 2.48 0.070 791 2.40 0.068 2.64 4.65 0.13 5.26 0.149 846 3.791 2.25 0.064 2.48 0.070 791 3.439 1.1 2.25 0.064 2.48 0.070 791 2.25 0.064 2.48 0.070 791 2.25 0.064 2.48 0.070 791 2.25 0.064 2.48 0.070 791 2.25 0.064 2.48 0.070 791 2.25 0.084 2.23 0.053 559.5 0.085 2.23 0.053 559.5 0.085 2.23 0.063 559.5 0.085 2.23 0.065 0.24 17.37 0.040 1.27 0.029 1.12 15.02 0.43 17.37 0.402 2.23 0.049 2.23 0.040 1.21 15.0 0.040 15.97 0.452 2.03 0.040 1.21 0.020 1.12 15.0 0.040 15.97 0.452 2.03 0.041 1.15 0.061 2.37 2.15 0.067 7.24 0.205 8.11 0.067 7.24 0.205 8.11 0.060 2.32 0.067 7.24 0.205 8.13 1.10 0.054 2.15 0.061 2.37 2.15 0.067 7.24 0.205 8.13 1.20 0.034 1.32 4.83 0.14 5.54 0.157 4.25 0.19 1.20 0.034 1.32 4.83 0.14 5.54 0.157 4.25 0.10 0.09 0.031 1.20 0.034 1.32 4.83 0.14 5.54 0.157 4.25 0.10 0.09 0.031 1.20 0.224 0.06 2.24 0.070 2.24 0.06 2.24 0.070 2.24 0.06 2.24 0.070 2.24 0.06 2.24 0.070 2.24 0.06 2.24 0.070 2.24 0.06 2.24 0.070 2.24 0.09 0.116 4.88 0.09 0.031 1.20 0.034 1.27 1.15 0.03 1.27 0.036 2.40 0.070 2.10 0.034 0.038 1.27 0.036 2.24 0.007 0.15 0.036 0.038 0.039 1.27 1.15 0.03 1.27 0.036 2.40 0.070 2.24 0.06 2.24 0.070 2.24 0.06 2.24 0.070 2.24 0.06 2.24 0.070 2.24 0.06 2.24 0.070 2.24 0.06 2.24 0.070 2.24 0.09 0.116 0.09 0.116 0.09 0.010 0.09 0.00 0.00 0.00 0.00 0.0	m	464 9450/1	9450	288	450	137 Kot M.	oman		7.	0.040	9	7.	0.40		0.430	9	3	220	
oman 2.40 0.068 2.64 4.65 0.13 5.26 0.149 846 3 oman 2.25 0.064 2.48 2.25 0.06 2.48 0.070 791 3 igos 0.54 1.74 0.049 1.91 19.06 0.54 22.35 0.633 559.5 17.32 0.49 20.12 0.570 433 17.32 0.49 20.12 0.570 433 17.32 0.49 20.12 0.570 433 17.32 0.49 20.12 0.570 433 17.32 0.49 20.12 0.570 433 17.32 0.49 20.12 0.570 433 17.32 0.49 20.12 0.570 433 17.32 0.49 20.12 0.570 433 17.32 0.49 20.12 0.570 433 17.32 0.49 20.12 0.570 433 17.32 0.49 20.12 0.570 425 20.00 1.18 16.09 0.46 18.55 0.525 20.00 1.12 15.00 0.45 17.37 0.492 20.00 1.12 0.000 1.13 17.37 0.492 20.00 1.14 0.050 1.15 0.044 1.71 11.45 0.32 12.54 0.366 5.00 1.15 0.051 1.15 0.051 1.15 0.051 1.15 0.051 1.15 0.051 1.15 0.051 1.15 0.051 1.15 0.031 1.15 0.031 1.15 0.031 1.15 0.031 1.15 0.031 1.15 0.031 1.17 0.036 1.13 0.031 1.15 0.031 1.17 0.036 2.46 0.070 2.44 0.000 2.4	٠,	465 134100.		4087	3960	1207 Kot Mc	Sman		1.0	4 0.029	1.14	5,69	0.16		0.186	367	149	811	
19.06 0.54 0.070 791 19.06 0.54 0.070 791 19.06 0.54 0.070 791 19.06 0.54 0.070 19.06 0.54 0.0633 559.5 1.74 0.049 1.91 19.06 0.54 22.35 0.633 559.5 1.73 0.035 1.32 0.035 1.32 0.035 1.32 0.035 1.32 0.040 0.46 18.55 0.525 376 14.3 0.040 1.12 0.029 0.46 18.55 0.525 376 14.3 0.040 1.57 14.00 0.40 15.97 0.452 355 10.058 1.12 0.032 1.12 1.25 0.041 1.57 0.492 355 1.25 0.041 1.57 0.040 1.57 14.00 0.40 15.97 0.452 355 10.058 1.12 0.041 1.71 11.45 0.32 12.94 0.366 5.50 1.32 0.057 1.32 0.057 1.32 0.057 0.314 5.32 0.057 0.314 5.32 0.057 0.314 1.058 0.133 1.13 0.056 2.37 0.067 2.067 0.133 1.13 0.034 1.32 4.83 0.14 5.54 0.157 4.25 0.157 4.25 0.157 4.25 0.157 4.25 0.157 4.25 0.157 4.25 0.157 4.25 0.157 4.25 0.157 4.25 0.157 4.25 0.157 4.25 0.157 4.25 0.157 4.25 0.157 4.25 0.157 4.25 0.157 4.25 0.157 0.057 1.20 0.034 1.32 4.83 0.14 5.54 0.157 4.25 0.057 0.057 1.20 0.034 1.32 2.48 0.10 4.09 0.116 4.88 0.10 4.09 0.116 4.88 0.10 4.09 0.116 4.00 0.116 0.0034		CE (000 CE) 227		200	900	1278 KA VE			2.0	89000	43,0	4.65	0.13		0.149	846	33	662 OFWM	
19,006 0.54 1,90 0.46 1,90 0.46 1,	n' v	10001 CO	20071		2	37.007.000			i c	2000	.2.48	30.0	Š		0.070	79.	320	320 OFWM	
ly 0.6 0.54 19.06 0.54 19.06 0.54 19.06 0.54 19.06 0.54 1.74 0.049 1.91 19.06 0.54 22.35 0.633 559.5 comin 1.72 0.035 1.35 17.32 0.49 20.12 0.570 433 comin 1.02 0.029 1.12 15.02 0.43 17.37 0.492 355 comin 1.43 0.040 1.57 14.00 0.46 18.55 0.525 376 comin 1.43 0.040 1.57 14.00 0.45 14.38 0.407 398 1.12 0.023 1.27 0.040 15.79 0.492 355 comin 10/SB 1.51 0.043 1.66 9.90 0.28 11.10 0.314 532 10/SB 1.81 0.051 1.99 8.39 0.24 9.43 0.267 621 10/SB 2.32 0.066 2.35 6.58 0.19 7.24 0.205 804 11/SB 2.32 0.066 2.35 6.58 0.19 7.24 0.205 804 11/SB 2.15 0.061 2.37 2.15 0.06 2.37 0.067 7.49 11/SB 2.19 0.034 1.32 4.83 0.14 5.54 0.157 4.25 apa 1.20 0.034 1.32 4.83 0.14 5.54 0.157 4.25 apa 1.39 0.039 1.53 3.63 0.10 4.09 0.116 488 8AASB 1.15 0.033 1.27 1.15 0.03 1.27 0.036 406	ا،	40/ 1/000/11	300/-						8.6	7 0.28						3.439	1.392		
19,06 0.54 19,06 0.54 1,74 0.049 1.91 19,06 0.54 22.35 0.633 559.5 comin 1.23 0.035 1.35 17.32 0.49 26.12 0.570 433 comin 1.07 0.030 1.18 16.09 0.46 18.55 0.525 376 aja 1.02 0.029 1.12 15.02 0.43 17.37 0.492 355 comin 9SB 1.12 0.032 1.23 12.57 0.36 14.38 0.407 398 comin 10/SB 1.13 0.043 1.56 9.90 0.28 11.10 0.314 532 10/SB 1.81 0.051 1.99 8.90 0.28 11.10 0.314 532 11/SB 2.13 0.066 2.35 6.58 0.19 7.24 0.267 621 11/SB 2.15 0.066 2.35 6.58 0.19 7.24 0.267 621 11/SB 2.15 0.061 2.37 2.15 0.067 7.49 2.668 aja 1.24 0.035 1.36 6.07 0.17 6.99 0.198 437 aja 1.20 0.034 1.32 4.83 0.14 5.54 0.157 4.25 aja 1.39 0.039 1.53 3.63 0.10 4.09 0.116 488 8.ASB 1.15 0.033 1.27 1.15 0.03 1.27 0.036 4.06							:	:											
ly 0.6 0.54 19.06 0.54																			
ly 0.6 0.54 19,06 0.54	5	Momin Minor(R)	736461/	R. Hu	ian Dis	tributary)												,	
(Raja 1.74 0.049 1.91 19.06 0.54 22.35 0.633 559.5 (Momin 1.23 0.035 1.32 17.32 0.49 20.12 0.570 433 (Raja 1.07 0.039 1.18 16.09 0.46 18.55 0.525 376 (Raja 1.02 0.029 1.12 15.02 0.43 17.37 0.492 355 (Momin 9SB 1.12 0.032 1.12 15.02 0.43 17.37 0.492 355 (Momin 9SB 1.12 0.032 1.12 15.02 0.43 17.37 0.492 355 (Momin 1.05B 1.12 0.032 1.12 15.02 0.43 17.37 0.492 355 (Momin 10/SB 1.21 0.043 1.45 0.32 12.94 0.36 407 398 (Momin 10/SB 1.31 0.064 1.35 0.024 1.32 0.24 0.32 12.94 0.36 50 530 (Moss 2.13 0.066 2.35 0.066 2.35 0.024 2.32 0.066 2.35 0.066 2.37 0.067 2.49 (Kaja 1.1/SB 2.37 0.066 2.37 0.	})" !								19.06	0.54					2.668	
t Momin 1.23 0.035 1.35 17.32 0.49 20.12 0.570 433 t Momin 1.07 0.030 1.18 16.09 0.46 18.55 0.525 376 1.02 0.029 1.12 15.02 0.43 17.37 0.492 355 t Momin 9SB 1.12 0.032 1.27 14.00 0.40 15.97 0.452 503 t Momin 10/SB 1.12 0.032 1.25 12.57 0.36 14.38 0.407 398 t Momin 10/SB 1.31 0.043 1.66 9.90 0.28 11.10 0.314 532 1.10 0.051 1.99 8.99 0.24 9.43 0.267 621 11/SB 2.13 0.066 2.35 6.58 0.19 2.44 0.267 621 11/SB 2.15 0.066 2.37 2.16 0.06 2.37 0.067 749 11/SB 2.15 0.061 2.37 2.15 0.06 2.37 0.067 749 t Momin 10/SB 1.20 0.034 1.32 4.89 0.17 6.99 0.198 4.37 t Raja 1.20 0.034 1.32 4.83 0.14 5.54 0.157 4.25 t Raja 1.39 0.039 1.53 3.63 0.10 4.09 0.116 488 1.15 0.033 1.27 1.15 0.03 1.27 0.036 4.06	_	423 4214/R	4214	1284		1284 Kot Ra	r)a		1.7	•	16.1	19.06	0.54	22.35	0.633	5.655	226	2,668 OFWM	
t Momin 1.07 0.030 1.18 16.09 0.46 18.55 0.525 376 18.39 1.02 0.029 1.12 15.02 0.43 17.37 0.492 355 1.02 0.029 1.12 15.02 0.43 17.37 0.492 355 1.000 1.000 1.57 14.00 0.40 15.97 0.452 503 1.12 0.032 1.25 0.040 1.71 11.45 0.32 12.94 0.366 550 10.0SB 1.51 0.043 1.66 9.90 0.28 11.10 0.314 532 1.051 1.005 2.35 0.066 2.55 6.58 0.19 7.24 0.205 804 1.00SB 2.13 0.061 2.37 0.067 749 1.00SB 2.13 0.060 2.32 4.26 0.12 7.46 0.133 713 1.00S 0.54 1.20 0.03 1.35 0.05 1.35 0.067 7.49 1.00SB 2.13 0.005 1.35 0.05 0.05 0.05 0.05 0.05 0.05 0.05 0	•	424 7215/1	7215	2199		915 Kot Me	omino		1.2		1.35	17.32	0.49	20.12	0.570	433	175	2,442 OFWM	
t Raja 1.02 0.029 1.12 15.02 0.43 17.37 0.492 355 1.02 0.040 1.57 14.00 0.40 15.97 0.452 503 1.000 1.57 14.00 0.40 15.97 0.452 503 1.000 1.57 14.00 0.40 15.97 0.452 503 1.000 1.55 0.044 1.71 11.45 0.32 12.94 0.366 550 1.00SB 1.51 0.043 1.66 9.90 0.28 11.10 0.314 532 1.00SB 1.31 0.005 1.99 8.39 0.24 9.43 0.267 621 1.00SB 2.13 0.066 2.55 6.58 0.19 7.24 0.205 804 1.00SB 2.15 0.066 2.32 4.26 0.12 4.69 0.133 713 713 1.00S 0.54 1.00S 0.24 4.69 0.133 713 713 1.00S 0.54 1.32 0.067 7.49 0.15 0.057 7.49 0.15 0.057 1.20 0.034 1.32 4.83 0.14 5.54 0.157 4.25 1.00S 0.039 1.53 3.63 0.10 4.09 0.116 488 1.00 0.039 1.15 0.033 1.27 1.15 0.03 1.27 0.036 4.06 1.00 0.13 1.15 0.033 1.27 1.15 0.03 1.27 0.036 4.00	l M	425 7225/L	7225	2202		3 Kot Me	omin		0.1		1.18	16.09	0.46	18.55	0.525	376	152	2,267 OPWM	
t Momin 9SB 1.12 0.030 1.57 14.00 0.40 15.97 0.452 503 1.12 0.032 1.23 12.57 0.36 14.38 0.407 398 1.12 0.032 1.23 12.57 0.36 14.38 0.407 398 1.10 0.05B 1.51 0.044 1.71 11.45 0.32 12.94 0.366 550 1.05B 1.10 0.314 532 1.294 0.365 550 1.10 0.314 532 1.10 0.314 532 1.10 0.314 532 1.10 0.314 532 1.10 0.314 532 0.366 2.35 6.58 0.19 7.24 0.205 804 1.05B 2.15 0.066 2.35 6.58 0.19 7.24 0.205 804 1.15B 2.15 0.061 2.37 2.15 0.06 2.37 0.067 749 1.15B 2.15 0.061 2.37 2.15 0.06 2.37 0.067 749 0.198 437 48aja 1.20 0.034 1.32 4.83 0.14 5.54 0.157 4.25 1.86 0.039 1.53 3.63 0.10 4.09 0.116 488 1.15 0.033 1.27 1.15 0.03 1.27 0.036 4.06 2.16 0.036 1.15 0.033 1.27 1.15 0.03 1.27 0.036 4.06	. 4	C27 11566/P	11566	3424		1323 Kot Ra	ii.		0.1		1.12	15.02	0.43	17.37	0.492	355	7	2,115 OFWM	
F. S. B.	· vn		11785	3592		67 Kot Ma	omin		1.4		1.57	6.4	0.40	15.97	0.452	503	20 40 40	1,971 OFWM	
t Momin 1.55 0.044 1.71 11.45 0.32 12.94 0.366 550 10/SB 1.51 0.043 1.66 9.90 0.28 11.10 0.314 532 10/SB 1.81 0.051 1.99 8.39 0.24 9.43 0.267 621 10/SB 2.32 0.066 2.55 6.58 0.19 7.24 0.205 804 10/SB 2.11 0.060 2.32 4.26 0.12 4.69 0.133 713 713 713 713 72.15 0.06 2.37 0.067 749 7.24 0.054 2.15 0.061 2.37 2.15 0.06 2.37 0.067 749 749 749 749 749 749 749 749 749 74	v		15394	1692		1100	_	SB	1.1		1.23	12.57	0.36	14.38	0.407	368	161	1,767 OFWM	
10/SB 1.51 0.043 1.66 9.90 0.28 11.10 0.314 532 10/SB 1.81 0.051 1.99 8.39 0.24 9.43 0.267 621 11/SB 2.32 0.066 2.55 6.58 0.19 7.24 0.205 804 10/SB 2.11 0.060 2.32 4.26 0.12 4.69 0.133 713 713 11/SB 2.15 0.061 2.37 2.15 0.06 2.37 0.067 749 2.068 10.06 0.54 10.060 0.54 2.068 10.06 0.054 10.060 0.067 10.060 10.060 0.067 10.060 10.060 0.060 10.06	~		17695	5393	3301	701 Kot M			1.5		1.71	11,45	0,32	12.94	0.366	250	553	1.606	
10/SB 1.81 0.051 1.99 8.39 0.24 9.43 0.267 621 11/SB 2.32 0.066 2.55 6.58 0.19 7.24 0.205 804 10/SB 2.11 0.060 2.32 4.26 0.12 4.69 0.133 713 713 11/SB 2.15 0.061 2.37 2.15 0.06 2.37 0.067 749 6.59 11/SB 1.24 0.034 2.15 0.06 0.17 6.99 0.198 437 180ja 1.20 0.034 1.32 4.83 0.14 5.54 0.157 4.25 1.80 0.031 1.20 0.034 1.32 4.83 0.10 4.09 0.116 488 1.09 0.031 1.20 2.24 0.06 2.46 0.070 384 8.458 1.15 0.033 1.27 1.15 0.03 1.27 0.036 4.06	20		17887	\$452	192	\$		O/SB	2.1		9.1	8.8	32.0	11.10	0.314	232	215	1.384	
11/SB 2.32 0.066 2.55 6.58 0.19 7.24 0.205 804 10/SB 2.11 0.060 2.32 4.26 0.12 4.69 0.133 713 713 11/SB 2.15 0.061 2.37 2.15 0.06 2.37 0.067 7.34 0.594 2.7 0.067 0.134 0.135 113 0.054 0.134 0.135 0.054 0.137 0.067 0.17 0.057 0.198 4.37 0.058 0.198 4.37 0.034 0.135 0.034 0.132 4.83 0.14 5.54 0.157 4.25 0.159 0.198 1.15 0.034 1.15 0.053 1.17 0.056 2.46 0.070 384 0.155 0.035 0.157 0.116 488 0.115 0.033 1.127 0.115 0.034 0.056 0.115 0.035 0.137 0.036	٥		22250	6782	4363	1330	7	O/SB	1.8		\$	8.39	0.24	9.43	0.267	621	22	1,168 OFWM	
10/SB 2.11 0.060 2.32 4.26 0.12 4.69 0.133 713 713 715 715 716 717 717 717 717 717 717 717 717 718 719 719 719 719 719 719 719 719 719 719	0		22250	6782	0	0	7	I/SB	23		2:55	6.58	0.19	7.24	0.205	8	325	917 OFWM	
(Raja 1.24 0.034 1.37 2.15 0.06 2.37 0.067 749 2.668 1.36 0.034 1.32 0.034 1.32 0.034 1.32 0.034 1.32 0.034 1.32 0.03 1.32 0.03 1.32 0.03 1.32 0.03 1.32 0.03 1.32 0.03 1.33 0.03 0.0			22250	6782	0	0	-	O/SB	2.1		2.32	4.26	0.12	4.69	0.133	713	582	592	
(Kaja 1.24 0.035 1.36 6.07 0.17 6.59 0.198 4.37 (Kaja 1.20 0.034 1.32 4.83 0.14 5.54 0.157 4.25 (Kaja 1.39 0.034 1.32 4.83 0.14 5.54 0.157 4.25 (Kaja 1.39 0.034 1.32 3.63 0.10 4.09 0.116 4.88 1.09 0.031 1.20 2.24 0.06 2.46 0.070 384 8.45 8.45 8.45 8.45 8.45 8.45 8.45 8.	c		22250	6782	•	0		1/SB	2		2.37	2.15	8	2.37	0.067	749	303	303 OFWM	
6.07 0.17 (Raja 1.24 0.035 1.36 6.07 0.17 6.99 0.198 437 (Raja 1.20 0.034 1.32 4.83 0.14 5.54 0.157 4.25 (Raja 1.39 0.039 1.53 3.63 0.10 4.09 0.116 488 1.09 0.031 1.20 2.24 0.06 2.46 0.070 384 8/ASB 1.15 0.033 1.27 1.15 0.03 1.27 0.036 406								P	<u>.</u> 61	ŀ						6,594	2,668		
(Raja 1.24 0.035 1.36 6.07 0.17 6.99 0.198 4.37 (Raja 1.20 0.034 1.32 4.83 0.14 5.54 0.157 4.25 (Raja 1.39 0.039 1.53 3.63 0.10 4.09 0.116 488 1.09 0.031 1.20 2.24 0.06 2.46 0.070 384 8.48 8.48 8.48 8.48 8.48 8.48 8.48		7	W07311																
418 2200/L 2200 671 Z200 671 Kot Raja 1.24 0.035 1.36 6.07 0.17 6.99 0.198 437 419 5800/R 5800 1768 3600 1097 Kot Raja 1.20 0.034 1.32 4.83 0.14 5.54 0.157 425 420 9215/TR 9215 2809 3415 1041 Kot Raja 1.39 0.039 1.53 3.63 0.10 4.09 0.116 488 421 9215/TC 9215 2809 0 0 8/ASB 1.15 0.033 1.27 1.15 0.03 1.20 0.34 0.03 4.06 4.06 422 9215/TL 9215 2809 0 0 8/ASB 1.15 0.033 1.27 1.15 0.03 1.20	Š	Kaja Minor(K.)	*1200CT*	r Cort		(Sural y)						6.07	0.17					998	:
419 5800/R 5800 1768 3600 1097 Kot Raja 1.20 0.034 1.32 4.83 0.14 5.54 0.157 425 420 9215/TR 9215 2809 3415 1041 Kot Raja 1.39 0.039 1.53 3.63 0.10 4.09 0.116 488 421 9215/TC 9215 2809 0 0 0 8/422 9215/TL 9215 2809 0 0 0 8/422 9215/TL 9215 2809 0 0 0 8/422 9215/TL 9215 2809 0 0		418 2200/1.	2200	671	3200	671 Kot R.	55		1	¥ 0.035	1.36	6.07	0.17	85.9	0.198	437	177	866 OFWM	
420 9215/TR 9215 2809 3415 1041 Kot Raja 1.39 0.039 1.53 3.63 0.10 4.09 0.116 488 421 9215/TC 9215 2809 0 0 0 1.09 0.031 1.20 2.24 0.06 2.46 0.070 384 422 9215/TL 9215 2809 0 0 8/ASB 1.15 0.033 1.27 1.15 0.03 1.27 0.036 406	• •	419 5800/R	880	1768	3606	1097 Kot R:	er c				1.32	4.83	0.14	5.54	0.157	\$3	172	689 OFWM	
421 9215/TC 9215 2809 0 0 8/ASB 1.15 0.033 1.27 1.15 0.036 406 246 0.070 384	'n	420 9215/TR	9215	2809	3415	1041 Kot R:	a,c		1.5		1.53	3.63	0.10	. 4.09	0.116	488	197	\$17	
422 9215/TL 9215 2809 0 0 8/ASB 1.15 0.033 1.27 1.15 0.03 1.27 0.036 406	4	421 9215/TC	9215	2808	0	0	. :		7.1		1.20	2.24	0.0	2.46	0.070	38	155	320	:
0016	v	422 9215/TL	9215	2809	0	. 0		VASB			1.27	1.15	0.03	1.27	0.036	\$	ž	164	
748 748					200		2		9(1. ·	1.					2,140	998		

Table B - 1 (1/3) Breakdown of Authorized and Design Discharge Calculation for LJC Area

1"	No. Num	Number of	CX CX		Section	on Villago	331	Chack No.	[₹ 	Outlet Discharge	orge	Section		Design		Outlet CCA		Section Improved under	Kemarks
94	÷	Watercourse	(feet)	Ê	Distance				Auc	Authorized	Design	Discharge	. &	Discharge		(acre)	<u>ا</u> ڇ		
			:	:	(fect)	(m)			(cusec)	(m3/s)	(casec)	(casec) ((m3/s) ((casec) (u	(m3/s)			(ha)	
	Bhiki Minor(RD 43310/R, Hujjan Distributary)	D 4331(1/R. Hu	ijan D	istribut	ary)													
												13.85	0.39					1,974	
	436 4147/1	۲.	4147	42,5	4147	1264		8/SB	0.80	0.023	0.88	13.85	0.39		197	182	114	1,974 OFWM	
	437 9775/L	بر	5775	2979	8295	1715 B.KHURD	ð	. :	1,14		1.25	13.05	0.37		.428	6	163	1,860	
	438 10496/R	Š	128	3199	13.	220 Deowal	:		1.35		1.49	16.11	0.34		.383	474	192	1,697	
	439 13242/R	Š	13242	4036	2746	837 Deowal	:		2.47		2.72	10.56	0.30		340	898	351	505,1	
	441 13531/L	3	13531	412	583	88 Decomal		:	1.68		1.85	8.8 8.08	0.23		.259	265	239	1,154	
	440 13581/R	<u> </u>	13581	4139	8	15 Deowal			0.89	0.025	0.98	6.41	0.18		3.206	315	127	915 OFWM	
	442 13861/R	€	13861	4225	280	85 Decwal			1.45		8	5.52	0.16		.178	511	207	788	
	20785/IF	X.F	20785	6335	6924	2110			2.47		2.72	4.07	0.12		.133	870	352	581	
	443 2078S/TR	YTR	20785	6335	0	0 Deowal			1.68	0.045	1.76	3.6	0.05	1.76	0.050	565	223	229 OFWM	
									13.85	0.39				1		4,878	1974		
		! !	:	:			. •	1			:	:		-	· · · · · · · · · · · · · · · · · · ·	1.974			
	,	1		;	;												-		
	Sahowal Minor(KD49178/K, Kujjan Distributary)	(KD49.	178/K, 1	tujjan		outary)						11						363 1	
	445 6334/!		6334	1931	25.59	1031		65/SB	000	0.003	010		300	1	177	3.1	1	1.575	
	446 7330/L	1	7330	27.34	8	304 Laliani			1 61		1.77	11.02	0.31		329	% 84		1.563 OFWM	
	447 7800/R	ρc	7800	23.77	07.4	143 Lafrani			. 43		1.62	6	0.27		307	518		1.342 OFWM	
	448 14850/L	7	14850	4526	7050	2149 Laliani			28		230	7.94	0.22		260	736		1,132 OFWM	
	449 15236/R	8	15236	4	88	118 Laliani	1		0.89		0.98	5.85	0.17		7,186	3,4		834 OFWM	
	450 18904/TL	Ę	18904	5762	3668	1118 Laliani			2.10		231	8,4	0.14		.158	739		707 OFWM	
	450 18904/TR	£38	18904	2925	0	0 Laliani	:		2.86	0.081	3.15	2.86	80.0	3.15 (0.089	8	408	408 OFWM	
			1.						11.11	0.31						3,893 1,575	1575		
	∫elewaei	Vinor	3D 832	35/1-1	Tuijan	Marulianwala Minor(RD 83265/L. Hujian Distributary	3												
			 - -		3				i	*		9.23	0.26				:	1.311	
	452 4042/R	*	4042	1232	4042	1232			1.77	0.050	1.95	9.23	0.26	10.01	0.309	625	ı	1,311 WAPDA	
	453 7644/7	_ل م	\$	2330	3602	1098 M.Wala	es		1.56		1.72	7.46	0.21		248	538		1.058 WAPDA	
	454 12488/R	K	12488	3806	484	1476			200		2.27	5.8	0.17		.195	427		840 WAPDAOFWM	
	455 19250/TR	Æ	19250	2867	6762	2061			\$		1.80	3.84	0.11		5.125	<i>S</i> 77		547	
	19250/11	Ĕ	19250	5867	0	0			2.20		2.42	2.20	90.0		690.	775	314	314	
									9.23							3,239 1,311	1311		

Table B - 1 (1/3) Breakdown of Authorized and Design Discharge Calculation for LJC Arca

No. Norther of RD Section	Minor(RD 921) Minor(RD 921) Minor(RD 921) 453 6242/L 458 9990/R 459 10022/L 461 15873/TR 461 15873/TR 461 469 196/L 470 8900/R 471 9755/L	(feet) (feet) 200, Hu 200, Hu 62,2 9990 19022 14873 15873 7916	(m)	Section Section Distance (feet) (n	o Voltage (m) (tary)	Chack No.	Authorized D (cusec) (mWs) (c	esign usec)	5 8 5 E	9	Oischarge usec) (m.Vs)	(acre) (b	2	(ha)	
(ongoal) angu Minc 1 457 6 2 458 9 3 459 10 4 460 11 3 3 461 11 1 468 4 2 469 7 3 470 9	######################################	(ice:) 20/L, Hu 62/2 9990 19022 14873 15873 7916 7916	(m) jjan D 1903 3045 3055 4533 4838	Distance (feet) Stribut 6242 3748 32	(m) tary)		(m.Vs)		m) () Jacob	9	51.1		(MA)	(ha)	
angu Mino 1 457 6 2 458 19 3 459 19 5 461 11 5 461 11 aspal Mino 1 468 4 2 469 7 3 470 9	r(RD 921. 2421. 2421. 390.R 3873/TL 3873/TL 3873/TR 3873/TR 3873/TR 5916/L 593/R	6242 9990 19022 14873 15873 15873 7916 7916	ijan D 1903 3045 3055 4533 4838 ijan I	(feet))istribut 6242 3748 32	(m) (tary)		(m.vs)		usec) (m	1	_			(ng)	
angu Mino 1 457 65 2 458 99 3 459 10 4 460 11 aspal Mink 2 469 471 9	r(RD 921; 227, 3027, 3873/TL 3873/TL 3873/TL 5873/TL 5873/TL 5916/L 500/R	90/L, Hu 9262 9260 10022 14873 15873 15873 70/L, Hu	ijan D 1903 3045 3055 4538 4838 1ijan I	istribut 6242 3748 33	tary)				- 1						
2 457 67 2 458 99 3 459 10 4 460 11 3 470 8 4 471 9	227. 2027. 2022. 2873.71. 2873.71. 2873.71. 295. 295. 295.	6242 9890 10022 14873 15873 15873 700/L, Hu	1903 3045 3055 4533 4838 1jian E	6242 3748 33								:		***	
2 458 99 3 459 10 4 4 460 11 5 461 11 aspal Minc 1 468 4 2 469 7 3 470 9	227. 2027. 2873/TL 2873/TR 2873/TR r(RD 955 r(RD 955	6242 9990 10022 14873 15873 15873 700/L, Ht	1903 3045 3055 4533 4838 1jjan F	9242 3748 32					- 1	-	- 1			1.470	
2 458 99 3 459 16 4 460 11 5 461 11 aspal Minc 1 468 4 2 469 7 3 470 8	990R 9022L 8873/TL 8873/TR 77(RD 955 195/R 996/L	9990 19022 14873 15873 15873 790 /L. Ht	3045 3055 4533 4838 Lijan I	3748	1903 M.Wala			2.24					53	1,470	
3 459 16 4 460 13 5 461 13 aspal Minc 1 468 4 2 469 7 3 470 9	%22/L %73/TL \$873/TR nr(RD 955 49%/R 99/6/L	10022 14873 15873 15873 100£, Hu	3055 4533 4838 1ijan D	32	1142 M.Wala	•		1,75			55 0.271		223	1,180	
2 460 11 3 461 11 3 468 4 1 468 4 2 468 7 3 470 9	873/TR 873/TR nr(RD 955 498/R 916/L 916/L	15873 15873 100£, Hv 4498 7916	4533 4838 1jan E		cleW.W 01			2.05					99 799 799	957	
2 461 1: aspal Mine 1 468 4 2 469 7 3 470 8	1873/TR 11 (RD 955) 196/L 916/L 900/R	15873 7916 7916	4838 jjan D	4851	1479 M.Wala	:	1:94 0.055	2.13					277	691 WAPDA/OFWM	*
aspal Mink 1 468 4 2 469 7 3 470 8	r(RD 955) 498/R 916/L 900/R	7916	jan D	000	305	17/SB		3.26	2.96	0.08	3.28 0.093		414	414 WAPDA/OFWM	И
aspal Mine 1 468 4 2 469 7 3 470 8 4 471 9	17(RD 955) 498/R 916/L 900/R	30/L. Hu 4498 7916	——————————————————————————————————————				10,39 0.29					3,633	1470		
aspal Mine 1 468 4 2 469 7 3 470 8	7(RD 955) 498/R 916/L 900/R	7916	 ijan D									1,470			
aspal Minc 1 468 4 2 469 7 3 470 8 4 471 9	17 (RD 955) 498/R 916/L 900/R	7916	ijan D												
2 469 7 469 7 470 8 471 9 471 9	1 (AC 525) 498/R 916/L 900/R	4498	i	Sico miles	(1000)				•						
	498/R 916/L 900/R	4498 7916		יוארו זיינו). 1				70 01	75 0				2 641	
	998/R 900/R 755/1.	7916 7916					- 1			ı	ı	l	000	1370	
	2167 300/R 7657	7916	1371	\$2	1371 Laliani		1.61 0.046	1.7	2.70			200	97	C.D. OFWM	
	900/R		2413	3418	182	16/SB		2.78			20.25 0.573		277	2,423 OFWM	
	7887	888	2713	984	300	14/SB	1.15 0.033	1.27					\$	2,101 OFWM	
		9755	2973	855	261	16/SB	1.34 0.038	1.47		0.39 15	15.89 0.450		185	1.937 OFWM	
A 473 Q	80000	0000	3033	501	20	14/SB		0.87		0.35 14	4.36 0.407		113	1,752 OFWM	
1	91100	1000	0636	1363	3091	14/60		00				240	141	1 639	
	7/1/K	1771	6000	1970	CNOT	90.		· ·					***	1 400	
	17413/L	17413	5307	218	699	16/88		1.43		200	2.10 0.343		COT :	MWTO OCT	
8 475 1	18542/R	18542	5652	1129	ž	14/28		1.07	-				38	1.313 OFWM	
9 4762	20833/L	20833	63.50	2291	869	17/SB	1.64 0.046	8.	878	0.23	9.42 0.267		234	1,175	
	21253/R	21253	6478	420	128	14/ASB	1.04 0.029	1.14			7.51 0.213		143	\$1	
778	240837	24083	7740	2830		17/58		1.21			6.35 0.180	0. 385	156	797	
7007	470 24082A	22020	73.40	C		14/ASR	- 2	1.42					183	\$	
V 00	VIII 0000	21200		21.7	.00	03/41		Ý					163	458	
	7 1 30C	3000	7 6	7176	707	4774 CD	2000 1000	200	4.4				Š	205	
	2/300/1L	2007	3	$\left \cdot \right $		ace.ii	- 1	4:40	ı				197 4	À.	
							450 05.81		•			1000	7.00.7		
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		:				•			:	\$ '					
Kirana Distributary	ributary		:						'					26.30	
									1		- 1	١	×		
~ (300/L	88	ჳ გ	88	91 Ghullapur		0.74 0.021		371.58 10	10.52 45	453.92 12.855	200	5 5 5 8 6		
	X/000/X	2950	ŝ	0007	sos Countapur			10.1			432.30 14.04		000		
w	8900/R	8900	2713	5950	1814	66/20/21/SB					_	3	597		
φ.	9200/R	9200	2804	8	16		108.19 3.064		Ξ.	5.6	-	¥		35,728	Chokera Dismbutary
4	93000	9300	2835	8	30 G.Pur Med	tla Ta	1.74 0.049		259.18		337.30 9.552				
	5 930078	0300	283	C	C	66/SE		3				:	212		
	C TOTEOR	10160	6623	. (200	2607 34612					_					
91	4 MC10	20101		200	177 C								Ī		
7 7:	18150/L	18150	2555	?	diam o						66.6 06.624				
8 8 3	8 19235/L	19235	5863	1085	331 Mula										
0	26220/R	26220	7992	6985	2129 Mtila		1.51 0.043								
` <u>`</u>	10.000	26220	7007	C	o Mrila	•		1.72	250:50	7.09 32		5 551	223		
	260096	26000	0010	889	207 Meila		1 23 0 040								
11	488	2007	272	3											

Table B - 1 (1/3) Breakdown of Authorized and Design Discharge Calculation for LJC Area

Course) Cour	Number of		-RD		Section	Villag	 မွ	Chack No.	Outlet Discharge	rge	Section	5	Design	 	Outlet CCA	 -	ا ۔	Improved under	Remarks
Control Cont	(original) Watercourse (feet) (m) D	(u) (u)			Distance		:		Authorized	Design	Disch	vec	Discha		(acre)	(ha)	ð		
22/58 0.05 0.07 0.07 42/51 7.01 3183.34 9.016 2.27 92 44-065 Maulia. 22/58 0.054 0.054 2.07 0.024/51 7.01 9.037 0.00 312.00 35.00 4.00 312.00 4.00 312.00 4.00 31.	9	£	E	ĝ	_	(w)			(cusec) : (m3/s)-	(casec)	(casec)	(m3/s)		(m3/s)			(ha)		
Maila 2258 Haga 625 165 245 3 165 3 165 3 165 4 55 6 182 3 3 9 13 3 1 1 1 1 1 1 1 1 1 1 1 1 1 1	30205/L 30205	9506		3305		1001	•	8S/C	0.64 0.018	0.70	247.51		318.34	9.016	77		34,065		
25/58 189 0054 2.054 5.054 5.151 2.057 6.90 312.65 8.854 461 187 33.572 1.0573	30210/R 30210 9208	9208		v,		- 1'				1.41	246.87		316.52	8.96%	420	182	33,973		
255B 122 0054 112 240,47 639 15400 8782 671 124 3335 0PWM 255B 152 0054 112 240,47 681 3475 8721 671 243,335 0PWM 255B 152 0054 121 240,47 681 3475 8721 677 274 3335 0PWM 255B 152 0055 121 240,47 681 3475 8.721 677 274 3335 0PWM 255B 152 0055 122 288 570 311,58 8,452 347 140 32,312 66,978 125 0055 124 224,14 662 26,98 462 337 489 32,172 24,98 32,172 24,98 32,172 24,98 32,172 24,98 32,172 24,99 32,172 24,9	31328/L 31328 9549 1	65.86	_ `	1118		34)		27SB		2.08	245.59	8 8	315.11	8.924	\$6	69 i	33,791		
2578 122 0.054 2.11 20,247 6.81 30793 8.721 676 274 33.020 66/88 20,057 2.22 238.55 6.70 301.58 8.565 713 289 2.778 66/88 20,058 20,059 1.13 251.17 666 20,648 8.452 3.47 140 32.172 6.758 1.12 0.055 1.13 224.14 6.65 20,84.8 8.452 3.47 140 32.172 6.758 1.12 0.055 1.13 224.14 6.65 20,84.8 8.452 3.47 140 32.172 6.758 1.12 0.055 1.13 224.14 6.65 20,84.8 8.452 3.47 140 32.172 6.758 1.12 0.055 1.13 224.14 6.65 20,84.8 8.452 3.47 140 32.172 6.758 1.13 0.057 1.14 22.16 6.65 20,84.8 8.452 3.47 140 32.172 6.758 1.13 0.057 1.14 22.16 6.65 20,84.8 8.452 3.147 6.65 31.816 7.45 1.10 0.057 1.14 22.16 6.65 20,84.8 8.452 3.14 7.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10	15 347.27.1 34.23 10364 5397 16 34.23 10564 5597 17 17 17 17 17 17 17 17 17 17 17 17 17	70501	, ye.	·		oso Madia		23/62		‡ :	243.70	2 %	217.00	406.8	Ş Ę	3 6	23,226 O	Ž/nG	
66/58 120 0.057 122 238.55 676 303.85 8.665 711 299 32,788 26/58 120 0.059 113 253,176 666 298,48 8,540 470 100 0.029 113 253,176 666 298,48 8,540 470 100 0.029 113 253,176 666 298,48 8,540 470 100 0.029 113 253,176 666 298,48 8,540 470 100 100 0.029 113 253,176 666 298,48 8,540 470 100 100 100 100 10 113 253,176 10 0.029 113 253,176 10 0.029 113 253,176 10 0.029 113 253,176 10 0.029 114 20,000 114 20,000 114 10 0.029	40785/L 40735 12416 5935	12416 5935	5935		-	6081		25/SB		7 7 7	240.47		307.93	8.721	929	27.4	33.062		
69/58 136 0.039 150 2.65.5 6.70 301.56 8.540 463 187 32.499 67/58 120 0.035 11.3 235.17 6.65 296.46 453 187 32.499 67/58 120 0.035 11.3 235.17 6.65 296.78 4.05 31.21 67/58 120 0.035 11.3 232.9 6.60 296.78 4.05 31.21 67/58 120 0.035 11.2 23.29 6.60 295.18 4.06 21.81 67/58 120 0.035 11.2 23.29 6.60 295.18 4.09 6.60 11.816 67/58 10.005 11.6 22.29 6.60 295.18 4.09 6.60 11.816 67/58 10.005 11.6 2.20.29 6.20 20.20 11.814 67/58 10.005 11.6 2.20.4 6.31 28.19 4.09 6.60 11.816 67/58 10.005 11.6 2.20.4 6.31 28.19 4.98 20.19 67/58 10.005 11.6 2.20.4 6.31 28.19 4.09 6.20 11.816 67/58 10.005 11.6 2.20.4 6.31 28.19 4.09 6.20 199 9.0.89 67/58 10.005 11.0 20.005 11.0 20.005 11.0 20.005 11.0 20.005 67/58 10.005 11.0 20.005 11.0 20.005 11.0 20.005 11.0 20.005 67/58 10.005 11.0 20.005 11.0 20.005 11.0 20.005 11.0 20.005 67/58 10.005 11.005 11.0 20.005 11.0 20.005 11.0 20.005 67/58 10.005 11.0 20.005 11.0 20.005 11.0 20.005 67/58 10.005 11.0 20.005 11.0 20.005 11.0 20.005 67/58 10.005 11.0 0.005 11.0 20.005 11.0 20.005 67/58 11.0 0.000 11.0 21.0 21.0 21.0 21.0 21.	40930 12475 195	12475 195	195			59	Ť	59/SB	٠	2.22	238.55		303.85	3.605	713	586	32,788		
25/58 1120 0025 113 253.17 666 298.46 8.452 347 140 32312 25/58 1120 0026 213.2 224.14 662 296.78 8.405 390 183 32.172 25/58 1120 0026 124.2 224.14 662 296.78 8.405 390 183 32.172 25/58 123 0026 124.2 224.14 632 286.14 8.104 434 176 31.025 25/58 123 0027 1.44 226.8 6-2 287.6 2 8.145 437 666 518.16 25/58 123 0027 1.44 226.8 6-2 287.6 2 8.145 437 666 518.16 25/58 124 0020 154 224.14 632 284.4 8.058 492 199 30.849 25/58 1120 0020 1154 224.14 632 284.5 8.058 492 199 30.849 25/58 1120 0020 1154 224.14 632 284.2 8.058 492 199 30.849 25/58 1120 0020 1154 224.14 632 284.2 8.058 492 199 30.849 25/58 1120 0020 1154 224.14 632 284.2 8.058 492 199 30.849 25/58 1120 0020 1154 224.14 632 284.2 8.058 492 199 30.849 25/58 1120 0020 1154 224.14 632 284.2 8.058 492 199 30.849 25/58 1120 0020 1154 217.87 61.2 87.2 7944 415 168 30.511 0.9404 25/58 1120 0020 1154 217.87 61.2 87.2 7944 415 168 30.511 0.9404 25/58 1120 0020 1154 217.87 61.2 87.2 7947 415 168 30.511 0.9404 25/58 1120 0020 1154 192.15 651 284.9 7.020 4051 1659 29.354 25/58 1120 0020 1154 192.15 651 284.9 7.020 4051 1659 29.354 25/58 1120 0020 1154 192.0 564 24.2 7.020 565.7 0.9404 25/58 1120 0020 1154 192.0 564 24.2 7.020 565.7 0.9404 25/58 1120 0020 1154 192.0 564 224.7 069 370 27.507 0.9404 25/58 1120 0020 1154 192.0 564 224.7 069 370 27.507 0.9404 25/58 1120 0020 1154 192.0 564 224.7 069 370 27.507 0.9404 25/58 1120 0020 1154 193.1 183.4 5.2 22.2 25.2 25.0 26.0 26.0 26.0 26.0 26.0 26.0 26.0 26	. 45800 13960 4870	13960 4870	4870		~	484	Ĭ	85/SB		1.50	236.53	_	301.56	8.540	463	187	32,499		
67/5B 1,22 0,0035 1,34 224,14 6.62 295,13 8.457 89 183 32,172 23/5B 1,99 0,005 2,19 222,94 6.62 295,10 8.234 197 660 11816 23/5B 1,29 0,005 1,19 225,68 6.42 2022 8.234 197 660 11816 23/5B 1,21 0,003 1,44 20,03 6.82 2022 8.234 197 660 11816 23/5B 1,23 0,003 1,42 224,14 6.35 284,54 8.088 492 199 30,849 73/5B 1,40 0,004 1,54 224,14 6.35 284,54 8.088 492 199 30,849 73/5B 1,18 0,003 1,08 20,74 6.31 281,94 785 343 10,80 73/5B 1,18 0,003 1,09 20,003 1,09 20,88 2,18 20,95 6.24 30,203 80/5B 1,12 0,003 1,19 20,003 1,10 20,004 1,10 20,004 1,10 20,004 80/5B 1,10 0,004 1,10 1,10 20,004 1,10 1,10 20,004 1,10 1,10 20,004 1,10 1,10 20,004 1,10 1,10 20,004 1,10 1,10 20,004 1,10 1,10 20,004 1,10 1,10 20,004 1,10 1,10 20,004 1,10 1,10 20,0	47470/L 47470 14469 1670	14:69 1670	1670		Δ	8		3/SB		1.13	235.17	8	298.46	8.452	347	140	32,312		
25/58 1.99 0.036 2.19 222.92 6.60 295.10 8.357 4.89 1989 120.14 4.25 0.120 4.49 220.29 6.54 292.28 2.284 497 60.1816 73/58 1.13 0.037 1.42 226.93 6.54 292.62 8.284 497 60.1816 73/58 1.00 0.037 1.42 226.93 6.54 292.62 8.145 497 60.11816 73/58 1.00 0.037 1.42 226.93 6.54 292.62 8.145 497 60.11816 73/58 1.00 0.037 1.42 226.93 6.54 292.62 8.145 417 67 10.05 73/58 1.00 0.031 1.03 221.74 6.53 294.4 415 168 10.05.11 0.040 73/58 1.00 0.031 1.03 221.74 6.52 296.2 7.944 415 168 10.03.43 0.444 80/58 1.00 0.031 1.00 221.74 6.22 277.09 78-4 415 168 10.03.43 0.444 80/58 1.12 0.032 1.03 221.75 6.22 277.09 78-7 440 0.03-43 0.444 80/58 1.12 0.032 1.03 221.76 6.22 277.09 78-7 440 0.03-43 0.444 81/58 1.00 0.00 1.03 1.03 221.66 6.14 27.27 6.95 40.21 175 28/35 0.444 81/58 1.00 0.00 1.05 1.05 1.05 26/4 7.05 40.11 1.05 28/35 0.444 81/58 1.00 0.00 1.05 1.05 1.05 26/4 7.05 40.11 1.05 28/35 0.444 81/58 1.00 0.00 1.54 1.98 77 56/2 26/4 70.15 1.05 29/35 0.444 81/58 1.10 0.00 1.15 1.96 7.5 56 22/4 7.05 40.1 1.05 29/35 0.444 81/58 1.10 0.00 1.10 1.10 1.10 1.10 1.10 1.1	48515 14787 1045	14787 1045	1045		~	م	Č	37/SB		1.34	234,14	6.63	296.78	8.405	380	158	32,172		
7.5/SB 1.23 0.037 1.44 220.65 6.54 292.25 8.234 1497 666 31.816 23/SB 1.23 0.037 1.44 226.66 6.42 826.4 8.058 492 139 30.650 23/SB 1.23 0.037 1.44 226.66 6.42 826.4 8.058 492 199 30.839 11.30 0.037 1.35 224.14 6.35 234.54 8.058 492 199 30.839 11.30 0.038 0.028 1.08 222.14 6.31 2319.4 7.984 415 168 30.511 0.99 0.028 1.09 210.68 6.25 278.20 7.879 44 15 168 30.511 0.99 0.028 1.09 210.68 6.25 278.20 7.879 44 15 168 30.511 0.99 0.028 1.09 210.66 6.14 272.81 7.700 499 141 29.786 80.788 1.21 0.006 2.22 215.65 6.11 271.77 7.004 7.15 1.006 2.22 215.65 6.11 271.77 7.004 7.15 1.006 2.22 215.65 6.11 271.77 7.004 7.15 1.006 2.22 215.65 6.11 271.77 7.004 7.15 1.006 2.22 215.65 6.11 271.77 7.004 7.15 1.006 2.22 215.65 6.11 271.77 7.004 7.15 1.006 2.22 215.65 6.11 271.77 7.004 7.15 1.006 2.22 215.65 6.11 271.77 7.004 7.15 1.006 2.24 7.004 7.004 7.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10	49700/L 49700 15149 1185	15149 1185	1185		쏬			23/SB	1	2.19	232.92	8.80	295.10	8.357	489	861	32,014		
73/58 131 0.037 1.44 226.68 6.42 287.62 8.145 458 185 31,220 23/58 123 0.035 135 222.44 6.38 286.14 8.104 434 176 31,025 73/58 140 0.035 135 222.44 6.38 286.54 8.086 492 199 30.896 73/58 140 0.033 130 221.74 6.31 281.94 7.985 343 139 30.656 73/58 118 0.033 130 221.74 6.32 286.52 7.995 343 139 30.656 73/58 118 0.033 130 221.74 6.32 286.52 7.995 343 139 30.656 73/58 118 0.033 130 221.74 6.32 286.52 7.895 343 139 30.656 73/58 112 0.035 132 21.736 6.32 277.09 7.877 347 140 30.343 0°°°°°° 80/58 1172 0.049 138 21.748 71.726 349 141 29.778 80/58 123 0.035 135 21.748 71.726 349 141 29.778 80/58 125 0.046 127 15.65 6.11 271.72 7.695 715 289 29.643 0°°°°°° 81/58 125 0.056 126 121.54 6.0 26.4 7.095 715 289 29.643 0°°°°°° 81/58 116 0.046 177 195.26 5.42 7.095 370 150 27.457 0°°°°° 86/58 1140 0.046 177 195.26 5.32 24.37 6.921 66.7 229 26.90 86/58 119 0.034 173 192.26 5.42 26.93 6.96 201 27.108 0°°°°° 86/58 119 0.034 173 192.26 5.42 26.93 6.96 201 27.108 0°°°°° 86/58 119 0.034 173 192.85 5.42 22.91 68.5 200 26.473 0°°°°°° 86/58 119 0.034 173 192.85 5.42 22.91 68.5 200 26.473 0°°°°° 86/58 119 0.034 173 192.85 5.42 22.91 68.5 200 26.473 0°°°°° 86/58 119 0.034 173 192.85 5.42 22.91 68.5 200 26.473 0°°°°° 86/58 119 0.034 173 192.85 5.42 22.91 68.7 220 26.478 0°°°° 86/58 119 0.034 173 192.85 5.42 22.91 68.7 220 26.478 0°°°° 86/58 119 0.034 173 192.85 5.42 22.91 68.7 220 26.478 0°°°° 86/58 119 0.034 173 192.85 5.42 22.91 68.7 21 172 25.25 26.90 86/58 119 0.034 173 183.85 5.10 22.5 6.5 6.3 172 25.2 26.70 0°°°° 86/58 119 0.034 173 183.85 5.10 22.5 6.5 6.3 172 25.2 26.70 0°°°° 86/58 119 0.034 131 183.85 5.10 22.5 6.5 6.3 172 25.2 26.70 0°°°° 86/58 119 0.034 131 183.85 5.10 22.5 6.5 6.3 172 25.2 26.70 0°°°° 86/58 119 0.034 131 183.85 5.10 22.5 6.5 6.3 172 25.2 26.70 0°°°° 86/58 119 0.034 131 183.85 5.10 22.5 6.5 6.3 172 25.2 26.70 0°°°° 86/58 119 0.039 153 183.87 5.8 23.1 5.9 29.0 6.2 20.3 172 24.7 6°°°° 86/58 119 0.039 153 183.83 5.9 23.0 0°°°° 86/58 119 0.039 153 183.83 5.9 23.0 0°°° 86/58 119 0.050	49885 15205	15205		185 5	'n	9				4.84	230.93	6.54	292.52	8.284	1497	Š	31,816	•	saruli Minor(4.84)
23/58 1.23 0.035 1.35 225.37 6.38 236.14 8.104 454 176 31.025 73/58 1.00 0.004 1.25 226.14 6.51 281.94 7.885 343 139 30.656 73/58 1.18 0.033 1.30 221.76 6.28 280.25 7.944 415 188 30.511 0°°°°°°°°°°°°°°°°°°°°°°°°°°°°°°°°°°°	50000/R 50000 15240 115	15240 115	115		ěi,			73/SB		4	226.68	6.42	287.62	8.145	458	185	31,210		
73XB 1.40 0.040 1.54 224.14 6.35 284.54 8.053 492 199 30,849 73XB 1.00 0.020 1.08 222.74 6.31 281.94 7.983 343 139 30,603 73XB 1.00 0.028 1.00 220.58 6.25 278.20 7.879 347 140 30,349 9.008 80XB 1.02 0.028 1.00 220.58 6.25 278.20 7.879 347 140 30,343 9.008 80XB 1.03 0.028 1.09 210.58 6.22 277.09 7.847 602 244 30,203 9.004M 80XB 1.03 0.028 1.09 210.58 6.12 277.09 7.847 602 244 30,203 9.004M 80XB 1.04 0.040 1.89 210.56 6.14 272.81 7.26 349 141 22/784 9.008 81XB 1.05 0.030 1.06 1.99.12 5.64 250.34 7.625 4051 1639 29,543 9.004M 81XB 1.05 0.030 1.16 199.12 5.64 250.34 7.055 715 289 29,643 9.004M 81XB 1.05 0.030 1.16 199.12 5.64 250.34 7.055 70 150 27,457 9.004M 81XB 1.05 0.030 1.16 199.12 5.64 250.34 7.055 70 150 27,457 9.004M 81XB 1.05 0.040 1.35 196.67 5.92 6.99 7.05 70 150 27,457 9.004M 81XB 1.04 0.040 1.35 196.67 5.92 6.99 7.05 7.00 7.7307 80XB 1.05 0.045 1.77 192.05 5.44 22.31 6.86 29 20 25,473 9.004M 80XB 1.19 0.044 1.73 192.05 5.44 22.31 6.86 499 178 25,835 9.004M 80XB 1.15 0.045 1.15 188.34 5.34 22.31 6.86 439 178 25,835 9.004M 80XB 1.15 0.045 1.15 188.34 5.34 22.31 6.86 439 172 25,288 9.004M 80XB 1.15 0.045 1.15 188.34 5.34 22.31 6.86 439 172 25,288 9.004B 80XB 1.15 0.045 1.15 188.34 5.34 22.72 6.437 422 172 25,388 9.004B 80XB 1.15 0.045 1.15 188.34 5.34 22.72 6.437 422 172 25,388 9.004B 80XB 1.15 0.045 1.17 188.34 5.34 22.72 6.437 422 172 25,388 9.004B 80XB 1.15 0.045 1.17 188.34 5.34 22.72 6.437 422 172 25,388 9.004B 80XB 1.15 0.045 1.17 188.34 5.34 22.72 6.437 422 172 25,388 9.004B 80XB 1.15 0.045 1.17 188.24 5.12 22.72 6.437 422 172 25,388 9.004B 80XB 1.15 0.045 1.17 18.02 4.04 5.10 22.25 6.30 477 193 24,573 0.004B 80XB 1.15 0.045 1.17 18.02 4.08 11.71 5.00 502 21.80 9.00 502 25,314 6.00 502 21.80 9.00 502 25,314 6.00 502 21.31 6.00 6.00 1.20 1.20 6.20 5.00 502 21.31 6.00 6.00 6.00 1.20 1.20 6.20 5.20 5.20 5.20 5.20 5.20 5.20 5.20 5	50790/L 50790 15481 790	18481 790	28	_	$\bar{\mathbf{x}}$			3/SB		1.35	25.37	6.38	286.14	8.18 8.18	484	176	31,025		
73/58 0.088 0.022 1.08 222/74 6.31 281.94 7.988 343 139 30,650 73/58 118 0.033 1.20 221.76 6.32 280,52 7.944 415 168 30,511 0evum 80/58 11.20 0.049 1.089 219.59 6.22 277.09 7.847 602 244 30,203 0evum 81/58 0.099 0.028 1.09 210,55 6.12 277.09 7.847 602 244 30,203 0evum 81/58 0.099 0.028 1.09 216.66 6.14 272.81 7770 432 1.15 29,539 0evum 81/58 0.099 0.028 1.09 216.66 6.14 272.81 7770 432 1.15 29,539 0evum 81/58 0.099 0.028 1.09 216.66 6.14 272.81 7770 432 1.15 29,539 0evum 81/58 1.25 0.356 1.446 213.54 6.05 26.40 7.559 4051 1.05 29,534 86/58 1.25 0.356 1.16 190.12 564 226.47 7.055 715 289 29,534 86/58 1.40 0.040 1.54 198.07 5.61 249.39 7.063 493 200 27,307 86/58 1.41 0.040 1.55 196.67 5.57 246.23 6.993 496 201 27,108 0evum 86/58 1.61 0.046 1.77 195.26 5.57 24.93 7.063 493 200 27,307 86/58 1.61 0.046 1.77 195.26 5.42 22.31 6.802 493 200 26,478 0evum 86/58 1.61 0.044 1.77 195.26 5.42 22.31 6.802 493 200 26,478 0evum 86/58 1.90 0.034 1.31 192.48 5.34 23.47 6.81 499 202 26,478 0evum 86/58 1.90 0.034 1.31 192.48 5.34 23.47 6.81 499 202 26,478 0evum 86/58 1.90 0.034 1.31 192.48 5.34 23.47 6.81 499 202 26,478 0evum 86/58 1.90 0.034 1.31 192.48 5.34 23.47 6.81 189 24,951 1.30 0.039 1.31 192.48 5.34 23.47 6.81 189 24,951 1.30 0.039 1.31 192.48 5.34 23.47 6.81 189 24,951 1.30 0.039 1.31 192.84 5.34 23.47 6.81 189 24,951 1.30 0.039 1.31 192.84 5.34 23.47 6.81 189 24,951 1.30 0.039 1.31 192.84 5.30 22.95 6.90 495 1.30 24,751 0evum 95/58 1.30 0.039 1.31 192.85 5.30 22.95 6.90 439 1.35 24,352 0evum 95/58 1.30 0.039 1.31 192.85 6.30 5.90 5.90 5.90 2.91 180 24,354 0evum 95/58 1.30 0.039 1.31 192.85 6.30 2.90 5.90 5.90 2.33 1.35 1.34 0evum 95/58 1.30 0.039 1.31 192.85 6.30 5.90 5.90 2.32 24,70 0evum 95/58 1.30 0.039 1.31 192.85 6.30 2.90 5.00 2.33 1.40 2.54 2.40 6.80 6.80 6.80 6.80 6.80 6.80 6.80 6.8	54100/R 54100_16490 3310 1	16490 3310	3310	_	8			73/SB	_	1.54	224,14	6.35	284.54	8:058	492	8	30,849		
73/58 1130 0.033 1.30 221.76 6.28 280.52 79.44 415 168 30.511 OPWM 80/58 1.70 0.099 0.023 1.90 220.58 6.22 578.27 0.75 787 140 30.43.6 0.99 0.003 1.90 210.58 6.22 578.27 0.77 78 1.40 30.43.6 0.099 0.003 1.90 210.58 6.22 578.27 7.77 4.22 1.40 30.43.6 0.09 0.003 1.90 210.58 6.22 578.27 7.70 4.32 1.75 29,959 0PWM 80/58 1.23 0.035 1.35 217.87 6.17 274.37 7.77 4.32 1.75 29,959 0PWM 80/58 1.23 0.035 1.35 217.87 6.17 274.37 7.77 4.32 1.75 29,959 0PWM 80/58 1.85 0.052 2.15 6.64 6.14 272.81 7.75 4.95 7.15 29,959 0PWM 80/58 1.85 0.052 2.04 200.97 5.69 254.94 7.22 6.35 4051 16.99 2.04 200.97 5.69 254.94 7.22 6.35 4051 16.99 2.04 200.97 5.69 254.94 7.22 6.35 4051 16.99 2.04 200.97 5.69 254.94 7.22 6.35 4051 16.90 27.47 0PWM 80/58 1.40 0.040 1.54 198.07 5.61 249.37 1.03 49.6 27.77 14.0 0PWM 80/58 1.40 0.046 1.77 195.26 5.32 244.37 6.92 49.5 20.0 27.70 0PWM 80/58 1.19 0.034 1.13 192.05 5.42 23.70 6.47 418 169 26.024 0PWM 80/58 1.19 0.034 1.13 192.05 5.42 23.70 6.47 418 169 26.024 0PWM 80/58 1.13 0.035 1.13 19.24 5.13 2.33 6.68 4.39 4.30 5.32 25.30 9WWM 80/58 1.13 0.039 1.13 183.54 5.25 2.35 4.30 6.35 6.33 4.08 1.72 52.28 9W/58 1.13 0.039 1.13 183.54 5.10 222.54 6.50 5.31 6.32 24.37 6.32 6.32 24.37 6.32 6.32 6.32 24.37 6.32 6.32 6.32 6.32 6.32 6.32 6.32 6.32	55200 16825 1100	16825 1100	2 1100		335			.3/SB		1.08	222.74	6.31	281.94	7.985	ğ	139	30,650		
80/SB 1.09 0.028 1.09 220.58 6.25 278.20 7.879 347 140 30.343 OFWM 80/SB 1.12 0.049 1.89 219.59 6.22 277.09 7.847 602 244 30.203 OFWM 80/SB 1.12 0.049 1.89 219.59 6.22 277.09 7.847 602 244 30.203 OFWM 81/SB 1.22 0.028 1.09 216.64 6.14 272.81 7.706 349 141 29.784 80/SB 1.21 0.060 2.32 216.65 6.11 271.72 7.695 715 289 29.643 OFWM 81/SB 1.25 0.052 2.04 210.57 5.64 25.44 7.055 715 289 29.643 OFWM 81/SB 1.05 0.040 1.54 198.07 5.61 249.39 7.063 370 1.50 27.27 714 OFWM 81/SB 1.05 0.040 1.54 198.07 5.61 249.39 7.063 493 10.5 27.27 714 OFWM 86/SB 1.40 0.040 1.54 198.07 5.61 249.39 7.063 493 200 27.307 80/SB 1.40 0.040 1.55 196.67 5.72 244.37 6.921 549 20.25 6.907 80/SB 1.61 0.046 1.77 192.56 5.72 24.37 6.921 549 20.25 6.907 80/SB 1.50 0.044 1.77 192.56 5.32 244.37 6.921 549 20.2 26.47 0FWM 86/SB 1.50 0.044 1.77 192.56 5.32 244.37 6.921 6.02 26.77 0FWM 86/SB 1.19 0.044 1.77 192.56 5.32 244.37 6.921 6.02 26.77 0FWM 86/SB 1.19 0.034 1.31 188.54 5.34 224.37 6.921 6.02 26.77 0FWM 86/SB 1.19 0.034 1.31 188.54 5.34 224.37 6.03 26.37 0FWM 86/SB 1.19 0.034 1.31 188.54 5.34 224.72 6.647 4.18 169 26.02 0FWM 90/SB 1.19 0.034 1.31 188.54 5.34 224.72 6.647 4.18 169 26.02 0FWM 90/SB 1.30 0.039 1.51 188.54 5.34 224.72 6.648 4.39 1.78 25.83 0FWM 90/SB 1.37 0.039 1.51 188.54 5.34 224.72 6.501 531 215 25.503 90/SB 1.37 0.039 1.51 188.54 5.34 224.72 6.304 4.39 1.35 24.54 5.004 5.004 1.77 177.50 5.03 215.40 5.004 5.00 5.004 5.00	58410/R 58410 17803	17803 3210	3210		978			73/SB		1.30	221.76	6.28	280.52	7.944	415	168	30,511.0	FWM	
77/5B 172 0.049 1.89 219.59 6.22 277.09 7.847 602 244 30.203 0pwm 80/SB 1.23 0.035 1.35 217.87 6.17 272.81 7.770 432 1.15 29.989 0pwm 81/SB 0.99 0.028 1.09 216.64 6.14 272.81 7.726 349 1.41 29.784 7.726 349 1.41 29.784 7.726 349 1.41 29.784 7.726 349 1.41 29.784 7.726 349 1.41 29.784 7.726 349 1.41 29.784 7.726 349 1.41 29.784 7.726 349 1.41 29.784 7.726 349 1.41 29.784 7.726 349 1.41 29.784 7.726 349 1.41 29.784 7.726 349 1.41 29.784 7.726 349 1.41 29.784 7.726 349 1.42 20.737 7.726 349 2.737 9.727	\$8500/L \$8500 17831 90	17831 90	&		73		ω.	30/SB		8	220.58	8.23	278.20	7.879	3,7	5	30,343 0	FWM	
80/SB 1,23 0,035 1,35 2,17,87 6,17 274,37 7,770 432 1,75 29,959 OFWM 81/SB 0,99 0,0028 1,09 2,664 6,14 272,81 7,726 349 141 29,778 7,15 28,959 0,0028 1,09 2,664 6,14 272,81 7,726 349 141 29,778 86/SB 12,57 0,356 144 2,13.54 6,19 2,1717 7,75 349 141 29,778 9,959 0,003 1,25 1,35 6,61 2,717 2,20 6,36 254,94 7,220 6,36 257 27,714 OFWM 81/SB 1,05 0,030 1,16 199,12 5,64 250,54 7,095 370 150 27,457 OFWM 81/SB 1,41 0,040 1,55 196,67 5,57 24,93 7,063 496 201 27,108 OFWM 89/SB 1,41 0,040 1,55 196,67 5,57 24,37 6,921 567 200 27,377 6,971 1,61 0,046 1,77 192,05 5,43 24,37 6,921 567 200 26,478 OFWM 89/SB 1,57 0,044 1,73 192,05 5,44 24,37 6,921 6,93 200 26,478 OFWM 89/SB 1,94 0,055 2,13 190,48 5,39 22,70 6,47 418 169 26,024 OFWM 89/SB 1,19 0,034 1,31 183,45 5,19 227,2 6,47 418 169 26,024 OFWM 89/SB 1,50 0,049 1,31 183,45 5,19 227,5 6,43 178 25,835 OFWM 89/SB 1,50 0,049 1,51 180,48 5,29 27,2 6,47 117 25,677 OFWM 89/SB 1,57 0,049 1,51 180,48 5,29 27,26 6,301 1,72 25,673 OFWM 89/SB 1,37 0,039 1,51 180,48 5,29 27,20 6,437 4,25 17 193 24,571 99,038 1,37 0,039 1,51 178,87 5,07 221,04 6,260 459 186 24,758 OFWM 96/SB 1,37 0,039 1,51 178,87 5,07 221,04 6,260 459 186 24,758 OFWM 96/SB 1,37 0,039 1,51 178,87 5,07 221,04 6,260 459 186 24,757 OFWM 96/SB 1,37 0,039 1,51 178,87 5,07 221,04 6,260 459 186 24,757 OFWM 96/SB 1,37 0,039 1,51 178,87 5,07 221,04 6,260 459 186 24,757 OFWM 96/SB 1,37 0,039 1,51 178,87 5,07 221,04 6,260 459 186 24,757 OFWM 96/SB 1,37 0,039 1,51 178,87 5,07 221,04 6,260 459 186 24,757 OFWM 96/SB 1,37 0,039 1,51 178,87 5,07 221,04 6,260 459 178 24,572 OFWM 96/SB 1,34 0,055 1,34 174 174 14,014	61135/R 61135 18634 2635	18634 2635	2635		803			77/SB		88.	219.59	6.22	277.09	7.847	8	%	30,203 0	FWM	
81/SB 0.99 0.028 1.09 216.64 6.14 272.81 7.726 349 141 29,784 80/SB 2.31 0.060 2.32 215.65 6.11 271.72 7695 715 289 29,633 0FWM 12,710 0.060 2.32 215.65 6.11 271.72 7695 715 289 29,534 86/SB 1.85 0.052 2.04 200.77 5.69 254.94 7.220 636 2.77.74 0FWM 81/SB 1.05 0.030 1.16 199.12 5.64 220.54 7.095 370 150 27,771 0FWM 140 0.040 1.54 198.07 5.61 249.39 7.063 493 200 27,307 0FWM 86/SB 1.41 0.040 1.55 196.67 5.57 246.92 6.993 496 201 27,108 0FWM 86/SB 1.61 0.046 1.73 192.05 5.53 244.37 6.921 5.67 229 26,907 0FWM 89/SB 1.94 0.055 2.13 1904.8 5.39 2.70 6.712 6.22 26,207 0FWM 89/SB 1.19 0.034 1.31 188.54 5.34 234.72 6.47 418 169 26,024 0FWM 89/SB 1.19 0.034 1.31 188.54 5.34 234.72 6.47 418 169 26,024 0FWM 89/SB 1.30 0.039 1.31 188.54 5.34 234.72 6.47 418 169 26,024 0FWM 94/SB 1.30 0.039 1.51 188.54 5.14 225.55 6.303 477 193 24,951 90/SB 1.37 0.039 1.51 180.24 5.10 222.56 6.303 477 193 24,951 90/SB 1.37 0.039 1.51 180.24 5.10 222.56 6.303 477 193 24,951 90/SB 1.31 0.045 1.71 177.50 5.03 213.81 5.31 233.85 6.38 408 165 24,135 0FWM 94/SB 1.37 0.039 1.51 180.24 5.10 222.56 6.303 477 193 24,951 90/SB 1.31 0.045 1.51 178.87 5.07 21.04 6.260 453 1.32 24,951 90/SB 1.31 0.045 1.51 178.87 5.07 21.04 6.260 453 1.32 24,951 90/SB 1.31 0.045 1.31 18.34 6.35 21.34 6.35 24,951 90/SB 1.34 0.055 0.018 0.72 174.64 4.95 215.49 50/SB 24,758 0.049 1.37 0.040 1.57 174.01 4.93 21,38 6.566 648 262 24,076 WAPDA 100/SB 1.40 0.052 1.24 172 1.55 5.990 503 23,814 WAPDA	1 61800 18837	18837 665	\$8		g		•	SO/SB		1.35	217.87	6.17	274.37	7.770	432	175	29,959 0	FWM	
86/SB 211 0.060 2.32 215.65 6.11 271.72 7.695 715 289 29,643 orwww 86/SB 1.85 0.035 1.446 213.54 6.05 269.40 7.629 4.051 1.659 29,334 86/SB 1.85 0.035 2.04 200.97 5.69 254.94 7.220 6.36 2.77.74 orwww 81/SB 1.05 0.040 1.54 1.807 7.512 249.97 7.053 496 27 27.774 orwww 81/SB 1.41 0.040 1.55 1.866 7.5 24.37 6.921 567 229 26,907 86/SB 1.41 0.040 1.77 1.95.26 5.53 244.37 6.921 567 229 26,907 88/SB 1.60 0.045 1.77 1.95.26 5.32 244.37 6.921 567 229 26,907 88/SB 1.50 0.045 1.77 1.95.26 5.42 24.37 6.921 567 229 26,907 88/SB 1.57 0.044 1.73 192.05 5.44 239.44 6.781 499 202 26,473 orwww 89/SB 1.19 0.034 1.13 188.54 5.34 224.37 6.647 418 169 26,270 orwww 89/SB 1.40 0.041 1.73 182.55 5.31 233.35 6.647 418 169 26,224 orwww 89/SB 1.50 0.034 1.58 187.35 5.31 233.35 6.647 418 169 26,224 orwww 89/SB 1.51 0.043 1.66 184.66 5.23 229,54 6.501 531 1.74 25,677 orwww 89/SB 1.51 0.043 1.51 180.24 5.10 222.56 6.303 477 193 24,951 90/SB 1.37 0.039 1.51 180.24 5.10 222.56 6.303 477 193 24,951 90/SB 1.37 0.039 1.51 180.24 5.10 222.56 6.303 477 193 24,951 90/SB 1.37 0.039 1.51 178.87 5.07 221.04 6.560 433 1.35 24,954 90/SB 1.37 0.039 1.51 178.87 5.07 221.04 6.560 433 1.35 24,954 90/SB 1.37 0.039 1.51 178.87 5.07 221.04 6.560 433 1.35 24,954 90/SB 1.34 0.035 1.35 1.74 6.50 433 1.75 24,944 98/SB 1.34 0.055 0.018 0.72 174.66 4.93 213.83 6.056 648 262 24,076 wAPDA 100/SB 1.42 0.040 1.56 172.17 4.88 211.52 5.909 502 23.314 wAPDA	61800/R1 61800		837. 0 0	0	0		•	11/SB	1.	8	216.64	6.14	272.81	7.726	349	141	29,784		
86/SB 12.57 0.356 14.46 213.54 6.05 269.40 7.629 4051 1639 29.354 86/SB 1.85 0.052 2.04 200.97 5.69 24.94 7.220 6.36 257 27.714 oPwW 81/SB 1.05 0.030 1.54 198.07 5.61 249.39 7.053 493 20 27.377 86/SB 1.41 0.040 1.54 198.07 5.61 249.39 7.053 496 201 27.108 oPwW 86/SB 1.41 0.040 1.55 196.65 5.43 24.37 6.921 6.92 26.907 89/SB 1.60 0.045 1.77 195.26 5.32 244.37 6.921 6.92 26.907 89/SB 1.60 0.045 1.77 195.05 5.44 229.44 6.781 499 202 26.478 oPwW 89/SB 1.94 0.055 2.13 190.48 5.39 237.02 6.712 6.22 26.27 0PwW 89/SB 1.94 0.055 2.13 190.48 5.39 237.02 6.712 6.22 26.27 0PwW 89/SB 1.51 0.044 1.73 188.54 5.34 23.47 6.647 418 169 26.024 0PwW 89/SB 1.50 0.034 1.31 188.54 5.34 23.47 6.647 418 169 26.024 0PwW 89/SB 1.50 0.039 1.51 188.54 6.501 5.11 25.567 0PwW 89/SB 1.51 0.043 1.67 183.15 5.19 277.29 6.437 425 172 25.285 90/SB 1.51 0.043 1.67 183.15 5.19 277.29 6.437 425 172 25.285 90/SB 1.51 0.045 1.77 17.56 5.10 222.56 6.303 477 193 24.951 90/SB 1.51 0.046 1.77 17.56 5.03 21.70 6.204 5.89 185 24.758 0PwW 94/SB 1.51 0.046 1.77 17.56 5.03 21.70 6.204 5.89 185 24.758 0PwW 94/SB 1.51 0.046 1.77 17.56 5.03 21.70 6.204 5.80 165 25.116 94/SB 1.51 0.046 1.77 17.75 5.02 25.65 6.303 477 193 24.951 98/SB 1.51 0.046 1.77 17.75 5.02 26.03 477 193 24.951 98/SB 1.51 0.046 1.77 17.75 5.004 5.00 22.4.77 6.804 98/SB 1.52 0.055 2.02 174.01 4.93 213.83 6.056 648 262 24.776 wAPDA 100/SB 1.42 0.040 1.56 172.17 4.88 211.52 5.990 502 203 23.814 wAPDA	00819		837 0 0	0	0		~	SO/SB		2.32	215.65	6.11	271.72	7.695	71.5	583	29,643 0	FWM	-
86/SB 1.85 0.052 2.04 200.77 5.69 254.94 7.220 636 257 81/SB 1.05 0.030 1.16 199.12 5.64 250.54 7.063 493 200 86/SB 1.44 0.040 1.55 196.07 5.51 246.92 6.993 496 201 1.61 0.046 1.77 195.26 5.53 244.37 6.921 567 229 89/SB 1.60 0.045 1.77 195.26 5.53 244.37 6.921 567 229 89/SB 1.50 0.045 1.73 192.05 5.44 239.44 6.781 499 202 89/SB 1.94 0.055 2.13 190.48 5.39 237.02 6.712 6.22 522 89/SB 1.19 0.034 1.31 188.54 5.34 23.47 6.647 418 169 90/SB 1.25 0.035 1.31 188.54 5.34 23.47 6.647 418 169 90/SB 1.25 0.035 1.38 185.91 5.26 231.69 6.562 431 174 90/SB 1.51 0.043 1.51 188.54 5.32 229.54 6.501 531 215 90/SB 1.37 0.039 1.51 180.24 5.10 222.56 6.303 477 193 90/SB 1.37 0.039 1.51 177.55 5.04 221.04 6.260 439 175 90/SB 1.37 0.039 1.51 177.56 6.303 477 193 90/SB 1.37 0.039 1.51 177.56 6.303 6.303 477 193 98/SB 1.37 0.039 1.51 177.66 4.95 215.49 6.103 6.260 488 262 100/SB 1.42 0.052 2.02 174.04 4.93 213.83 6.056 6.48 262 100/SB 1.42 0.054 1.57 177.56 4.95 215.49 6.103 5.20 203 100/SB 1.42 0.052 2.02 174.01 4.93 213.83 6.056 6.48 262 203 100/SB 1.42 0.050 1.56 172.17 4.88 211.52 5.990 502 203 203 203 203 203 203 203 203 203 2	2 61800 18837 0	18837 0	0		0				_	14.46	213.54	6.05	269.40	7.629	4051	1639	29,354		Radda Minor(14.46)
81/SB 1.05 0.030 1.16 199.12 5.64 250.54 7.095 370 150 150 150 150 150 150 150 150 150 15	69700	21245 7900	7900	_	2408		~	S6/SB		5.8	200.97	\$.69	254.94	7.220	636	257	27,714 0	FWM	
8658 1.40 0.040 1.54 198.07 5.61 249.39 7.063 493 200 1.61 0.040 1.55 196.67 5.57 246.92 6.993 496 201 1.61 0.046 1.77 195.26 5.53 244.37 6.921 567 229 89/SB 1.60 0.045 1.76 193.65 5.48 242.31 6.862 493 200 86/SB 1.57 0.044 1.75 192.05 5.44 239.44 6.781 499 202 89/SB 1.94 0.055 2.13 190.48 5.39 2370.2 6.712 622 522 89/SB 1.19 0.034 1.31 188.54 5.34 234.72 6.647 418 169 90/SB 1.25 0.035 1.31 188.54 5.34 234.72 6.647 418 169 90/SB 1.25 0.035 1.38 185.91 5.26 231.69 6.562 431 174 90/SB 1.52 0.043 1.66 184.66 5.23 229.54 6.501 531 215 90/SB 1.39 0.039 1.51 180.24 5.10 222.56 6.303 477 193 90/SB 1.37 0.039 1.51 177.50 5.04 5.04 5.04 5.05 5.08 5.04 5.04 5.04 5.04 5.05 5.08 5.04 5.04 5.04 5.04 5.04 5.05 5.08 5.08 5.08 5.08 5.08 5.08 5.08	21245 0	21245 0	o		0		Ψ,	11/SB		1.16	199.12	8.0 3	250.54	7.095	370	150		FWM	
86/SB 1.41 0.040 1.55 196.67 5.57 246.92 6.993 496 201 Hadda 89/SB 1.61 0.046 1.77 195.26 5.53 244.37 6.921 567 229 86/SB 1.57 0.044 1.73 192.05 5.48 239.44 6.781 499 202 89/SB 1.94 0.055 2.13 190.48 5.39 237.02 6.712 6.22 252 89/SB 1.94 0.054 1.73 192.05 5.44 239.44 6.781 499 202 89/SB 1.94 0.054 1.73 188.45 5.44 239.44 6.781 169 202 89/SB 1.64 0.041 1.58 187.35 5.31 233.35 6.608 439 178 89/SB 1.25 0.035 1.38 185.91 5.26 231.69 6.562 431 174 94/SB 1.51 0.043 1.66 184.66 5.23 229.54 6.501 531 215 90/SB 1.37 0.039 1.51 180.24 5.10 222.56 6.303 477 193 90/SB 1.37 0.039 1.51 180.24 5.10 222.56 6.303 477 193 90/SB 1.37 0.039 1.51 178.87 5.07 221.04 6.260 459 186 94/SB 1.37 0.039 1.51 178.87 5.07 221.04 6.260 459 186 95/SB 1.37 0.039 1.51 178.87 5.07 221.04 6.260 459 186 98/SB 1.37 0.039 1.51 178.87 5.07 221.04 6.260 459 185 98/SB 1.38 0.055 1.35 175.89 4.98 217.15 6.150 459 175 98/SB 1.38 0.055 1.37 174.01 4.93 213.83 6.056 648 262 100/SB 1.44 0.052 2.02 174.01 4.93 213.83 6.056 648 262 203 203	72827 22198 3127	22198 3127	3127		953	Hadda			_	Z,	198.07	5.61	249.39	7.063	493	8	27,307		
Hadda 89/SB 1.61 0.046 1.77 195.26 5.53 244.37 6.921 567 229 86/SB 1.60 0.045 1.76 193.65 5.48 242.31 6.862 493 200 89/SB 1.94 0.055 1.13 190.48 5.39 237.02 6.712 6.627 418 1.90 0.034 1.31 188.54 5.34 234.72 6.647 418 169 90/SB 1.25 0.035 1.38 185.91 5.26 231.69 6.562 431 174 90/SB 1.51 0.043 1.65 184.66 5.23 229.54 6.501 5.31 215 90/SB 1.52 0.043 1.67 183.15 5.19 227.29 6.437 425 175 90/SB 1.37 0.039 1.51 188.24 5.19 227.29 6.437 425 175 90/SB 1.37 0.039 1.51 188.24 5.19 227.29 6.437 425 175 90/SB 1.30 0.036 1.51 178.87 5.10 222.56 6.303 477 193 98/SB 1.23 0.036 1.31 178.87 5.10 222.56 6.303 477 193 98/SB 1.44 0.052 2.02 174.01 4.93 213.83 6.056 6.48 262 2.03 100/SB 1.44 0.052 2.02 174.01 4.93 213.83 6.056 6.48 262 2.03 100/SB 1.44 0.052 2.02 174.01 4.88 211.52 5.990 2.03	36 762251 76225 23233 3398 1036	23233 3398 1	3398	_	1036		•	KVSB		1.55	196.67	5.57	246.92	6.993	496	23	27,108 0	FWM	
89/SB 1.60 0.045 1.76 193.65 5.48 242.31 6.862 493 200 86/SB 1.57 0.044 1.73 192.05 5.44 239.44 6.781 499 202 89/SB 1.94 0.055 2.13 190.48 5.39 237.02 6.712 6.22 252 89/SB 1.19 0.034 1.31 188.54 5.34 234.72 6.647 418 169 90/SB 1.25 0.035 1.38 185.91 5.26 231.69 6.562 431 174 90/SB 1.51 0.043 1.66 184.66 5.23 229.54 6.501 5.31 215 90/SB 1.52 0.045 1.67 183.15 5.19 222.55 6.388 408 165 90/SB 1.37 0.039 1.51 180.24 5.10 222.56 6.303 477 193 90/SB 1.37 0.039 1.51 180.24 5.10 222.56 6.303 478 165 90/SB 1.37 0.039 1.51 180.24 5.10 222.56 6.303 478 195 90/SB 1.51 0.046 1.77 177.50 5.03 219.07 6.204 563 228 94/SB 1.61 0.046 1.77 177.6 5.03 219.07 6.204 563 228 98/SB 0.65 0.018 0.72 174.66 4.95 217.15 6.103 230 93 98/SB 1.84 0.052 2.02 174.01 4.93 213.83 6.056 648 262 203 100/SB 1.42 0.040 1.56 172.17 4.88 211.52 5.990 502 203	77215 23535. 990	23535 990	8		Ö					1.77	195.26	5.53	244.37	6.921	8	83	26.907	-	
86/SB 1.57 0.044 1.73 192.05 5.44 239.44 6.781 499 202 89/SB 1.94 0.055 2.13 190.48 5.39 237.02 6.712 622 252 89/SB 1.19 0.034 1.31 188.54 5.34 234.72 6.647 418 169 90/SB 1.19 0.034 1.31 188.54 5.34 234.72 6.647 418 169 90/SB 1.25 0.035 1.38 185.91 5.26 231.69 6.562 431 174 94/SB 1.51 0.043 1.66 184.66 5.23 229.54 6.501 531 215 90/SB 1.39 0.039 1.53 181.63 5.19 225.56 6.303 408 165 94/SB 1.37 0.039 1.51 180.24 5.10 222.56 6.303 408 165 95/SB 1.51 0.046 1.77 177.50 5.03 219.04 6.260 459 186 95/SB 1.61 0.046 1.77 177.65 5.03 219.07 6.204 563 228 94/SB 1.63 0.035 1.35 175.89 4.98 217.15 6.150 433 175 98/SB 1.84 0.052 2.02 174.04 4.93 213.83 6.056 648 262 100/SB 1.84 0.052 2.02 174.01 4.93 213.83 6.056 648 262 203 100/SB 1.42 0.040 1.56 172.17 4.88 211.52 5.990 502 203	81020/R 81020 24695 3805	24695 3805	3805		116	•	~	83/SB	_	1.76	193.65	5.48	242.31	6.862	493	8	26,677 0	FWM	
89/SB 1.94 0.055 2.13 190.48 5.39 237.02 6.712 622 252 89/SB 1.19 0.034 1.31 188.54 5.34 234.72 6.647 418 169 90/SB 1.19 0.034 1.31 188.54 5.34 234.72 6.647 418 169 90/SB 1.25 0.035 1.38 185.91 5.26 231.69 6.562 431 174 94/SB 1.51 0.043 1.66 184.66 5.23 229.54 6.501 531 215 90/SB 1.39 0.039 1.53 181.63 5.19 227.29 6.437 4.25 172 90/SB 1.37 0.039 1.51 180.24 5.10 222.56 6.303 4.08 165 95/SB 1.37 0.039 1.51 180.24 5.10 222.56 6.303 4.08 165 95/SB 1.61 0.046 1.77 177.87 5.07 221.04 6.260 4.59 186 95/SB 1.23 0.035 1.35 175.89 4.98 217.15 6.150 4.33 175 98/SB 0.65 0.018 0.72 174.66 4.95 215.49 6.103 230 93 98/SB 1.84 0.052 2.02 174.01 4.93 213.83 6.056 648 262 100/SB 1.42 0.040 1.56 172.17 4.88 211.52 5.990 502 203	83423/L 83423 25427 2403	25427 2403	2403		73	63	ω	86/SB	_	1.73	192.05	4	239.44	6.781	49	50 50 50 50 50 50 50 50 50 50 50 50 50 5	26,478 0	FWM	
89/SB 1.19 0.034 1.31 188.54 5.34 234.72 6.647 418 169 90/SB 1.44 0.041 1.58 187.35 5.31 233.35 6.608 439 178 89/SB 1.25 0.035 1.38 185.91 5.26 231.69 6.562 431 174 90/SB 1.52 0.043 1.66 184.66 5.23 229.54 6.501 531 215 90/SB 1.39 0.039 1.53 181.63 5.19 227.29 6.437 4.25 172 90/SB 1.37 0.039 1.51 180.24 5.10 222.56 6.303 4.77 193 90/SB 1.37 0.039 1.51 178.75 5.07 221.04 6.260 4.59 186 95/SB 1.61 0.046 1.77 1.77 1.75 0.721.04 6.260 4.59 186 94/SB 1.23 0.035 1.35 175.89 4.98 217.15 6.150 433 175 98/SB 1.84 0.052 2.02 174.06 4.93 213.83 6.056 648 262 100/SB 1.42 0.040 1.56 172.17 4.88 211.52 5.990 502 203	84000/R 84000 25603 577	25603 577	577		11	9	•	88/8B	_	2.13	190.48	5.39	237.02	6.712	622	22	26,276 0	FWM	
90/SB 1,44 0,041 1,58 187,35 5,31 233,35 6,608 439 178 89/SB 1,25 0,035 1,38 185,91 5,26 231,69 6,562 431 174 9,05B 1,51 0,043 1,66 184,66 5,23 229,54 6,501 531 215 9,0/SB 1,39 0,039 1,53 181,63 5,14 225,55 6,388 408 165 9,0/SB 1,37 0,039 1,51 180,24 5,10 222,56 6,303 4,77 193 9,0/SB 1,37 0,039 1,51 180,24 5,10 222,56 6,303 4,77 193 9,0/SB 1,61 0,046 1,77 178,9 4,98 217,15 6,150 4,33 175 9,87 8 1,84 0,052 2,02 174,06 4,99 215,49 6,103 230 93 1,50 1,50 1,50 6,103 230 93 1,50 1,50 1,50 6,103 230 93 1,50 1,50 1,50 6,103 2,30 1,50 1,50 1,50 6,103 2,30 1,50 1,50 1,50 1,50 6,103 2,30 1,50 1,50 1,50 1,50 1,50 1,50 1,50 1,5	84205/R 84205 25666 205	25666 205	205		O	c)	~	:8/SB		1.31	188.54	35	234.72	6.647	418	69	26,024 0	FWM	
89/SB 1.25 0.035 1.38 185.91 5.26 231.69 6.562 431 174 24/SB 1.51 0.043 1.66 184.66 5.23 229.54 6.501 5.31 215 90/SB 1.52 0.043 1.67 183.15 5.19 227.29 6.437 4.25 172 90/SB 1.39 0.039 1.53 181.63 5.14 225.55 6.388 408 165 94/SB 1.37 0.039 1.51 180.24 5.10 222.56 6.303 4.77 193 90/SB 1.61 0.046 1.77 173.87 5.07 221.04 6.260 4.59 186 95/SB 1.23 0.035 1.35 175.89 4.98 217.15 6.150 4.33 175 98/SB 0.65 0.018 0.72 174.66 4.95 215.49 6.103 230 93 98/SB 1.84 0.052 2.02 174.01 4.93 213.83 6.056 648 262 100/SB 1.42 0.040 1.56 172.17 4.88 211.52 5.990 502 203	84465/L 84465 25745 250	25745 260	8	_	ř	•	0.	%/SB		58	187.35	5.31	233.35	6.608	439	178	25,855	FWM	
94/SB 1.51 0.043 1.66 184.66 5.23 229.54 6.501 531 215 90/SB 1.52 0.043 1.67 183.15 5.19 227.29 6.437 4.25 172 90/SB 1.52 0.043 1.67 183.15 5.19 227.29 6.437 4.25 172 90/SB 1.39 0.039 1.51 180.24 5.10 222.56 6.303 4.77 193 90/SB 1.61 0.046 1.77 178.87 5.07 221.04 6.260 4.59 186 94/SB 1.23 0.035 1.35 175.9 4.98 217.15 6.150 4.33 175 98/SB 0.65 0.018 0.72 174.61 4.93 213.83 6.056 648 262 100/SB 1.42 0.040 1.56 172.17 4.88 211.52 5.990 502 203	87200 26579 2735	26579 2735	2735		8		<i>ح</i>	:9/SB		1.38	185.91	5.26	231.69	6.562	431	174		FWM	
90/SB 1.52 0.043 1.67 183.15 5.19 227.29 6.437 425 172 90/SB 1.39 0.039 1.53 181.63 5.14 225.55 6.388 408 165 94/SB 1.37 0.039 1.51 180.24 5.10 222.56 6.303 477 193 90/SB 1.37 0.039 1.51 178.87 5.07 221.04 6.260 459 186 95/SB 1.61 0.046 1.77 177.50 5.03 219.07 6.204 563 228 94/SB 1.23 0.035 1.35 175.89 4.98 217.15 6.150 4.33 175 98/SB 0.65 0.018 0.72 174.66 4.95 215.49 6.103 230 93 98/SB 1.84 0.052 2.02 174.01 4.93 213.83 6.056 648 262 100/SB 1.42 0.040 1.56 172.17 4.88 211.52 5.990 502 203	89285/R 89285 27214 2085	27214 2085	2085		Š	<u>ن</u> م	<u>.</u>	4/SB		38.	84.88	5.23	229.54	6.501	531	215	25,503		
90/SB 1.39 0.039 1.53 181.63 5.14 225.55 6.388 408 165 94/SB 1.37 0.039 1.51 180.24 5.10 222.56 6.303 477 193 90/SB 1.37 0.039 1.51 180.24 5.10 222.56 6.303 477 193 90/SB 1.61 0.046 1.77 177.50 5.03 219.07 6.204 563 228 94/SB 1.23 0.035 1.35 175.89 4.98 217.15 6.150 433 175 98/SB 0.65 0.018 0.72 174.66 4.95 215.49 6.103 230 93 98/SB 1.84 0.052 2.02 174.01 4.93 213.83 6.056 648 262 100/SB 1.42 0.040 1.56 172.17 4.88 211.52 5.990 502 203	242	27288 242	242		,		•	%/SB		1.67	183.15	5.19	227 29	6.437	425	172	25,288		
94/SB 1.37 0.039 1.51 180.24 5.10 222.56 6.303 477 193 90/SB 1.37 0.039 1.51 178.87 5.07 221.04 6.260 459 186 95/SB 1.61 0.046 1.77 177.50 5.03 219.07 6.204 563 228 94/SB 1.23 0.035 1.35 175.89 4.98 217.15 6.150 433 175 98/SB 0.65 0.018 0.72 174.66 4.95 215.49 6.103 230 93 98/SB 1.84 0.052 2.02 174.01 4.93 213.83 6.056 648 262 100/SB 1.42 0.040 1.56 172.17 4.88 211.52 5.990 502 203		28887 5245	5245:		1595	_	01	W/SB		1.53	181.63	5 14	225.55	6.388	408	165	25,116		
90/SB 1.37 0.039 1.51 178.87 5.07 221.04 6.260 459 186 595/SB 1.61 0.046 1.77 177.50 5.03 219.07 6.204 563 228 54/SB 1.23 0.035 1.35 175.89 4.98 217.15 6.150 433 175 598/SB 0.65 0.018 0.72 174.66 4.95 215.49 6.103 230 93 598/SB 1.84 0.052 2.02 174.01 4.93 213.83 6.056 648 262 100/SB 1.42 0.040 1.56 172.17 4.88 211.52 5.990 502 203	28	28895 28	83			σ.	5	4/SB		1.51	180.24		222.56	6.303	477	193	24,951		
95/SB 1.61 0.046 1.77 177.50 5.03 219.07 6.204 563 228 24/SB 1.23 0.035 1.35 175.89 4.98 217.15 6.150 433 175 98/SB 0.65 0.018 0.72 174.66 4.95 215.49 6.103 230 93 98/SB 1.84 0.052 2.02 174.01 4.93 213.83 6.056 648 262 100/SB 1.42 0.040 1.56 172.17 4.88 211.52 5.990 502 203		29409 1685	1685		V	4		W/SB		1.51	178.87		221.04	6.260	459	186	24,758 0	FWM	
94/SB 1.23 0.035 1.35 175.89 4.98 217.15 6.150 433 175 5 98/SB 0.65 0.018 0.72 174.66 4.95 215.49 6.103 230 93 98/SB 1.84 0.052 2.02 174.01 4.93 213.83 6.056 648 262 100/SB 1.42 0.040 1.56 172.17 4.88 211.52 5.990 502 203	_	29570 530	530	_	-	. 62	Ů.	5/SB		1.7	177.50	5.03	219.07	6.204	563	228	24,572 0	PWM	
98/SB 0.65 0.018 0.72 174.66 4.95 215.49 6.103 230 93 3 98/SB 1.84 0.052 2.02 174.01 4.93 213.83 6.056 648 262 100/SB 1.42 0.040 1.56 172.17 4.88 211.52 5.990 502 203 3	98145 29915 1130	29915 1130	1130		۴,	4	Ů,	4/SB	-	1.35	175.89	4 98	217.15	6.150	433	175	24 344		
98/SB 1.84 0.052 2.02 174.01 4.93 213.83 6.056 648 262 2 100/SB 1.42 0.040 1.56 172.17 4.88 211.52 5.990 502 203 3	101620/L 101620 30974 3475 1	30974 3475 1	3475		ò	ŝ	•	8/SB		0.72	174.66	4.95	215.49	6.103	230	93	24,169		
: 100/SB 1.42 0.040 1.56 172.17 4.88 211.52 5.990 502 203 3	102646/L 102646 31287 1026	31287 1026	1026		~	13	Ů,	8/SB		2.02	174.01	4 93	213.83	6.056	2 8	262	24,076 W	/APDA	
	103840/R 103840 31650 1194	31650 1194	1194		~	8	_	00/SB	1,42 0.040	1.56	172.17	4.88	211.52	5.990	205	203	23.814 W	/APDA	

Table B - 1 (1/3) Breakdown of Authorized and Design Discharge Calculation for LJC Area

1														100		The state of the s	Dammer
0	ģ	Number of		Section	g :	Village	Chack No.	Cutter Discharge	large Trivial		: 6	Pichama Pichama	1	Cutter CC.	1		
5	(semigrap)	w atercourse	(10)	A CANADA				(A) (A)		١	(×,E)	(3)(2)(3)	٤			æ	
3	3	avovovo.	100000 21074	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	222		98/SR		-	17075	1	L	5 937	373	151 2	23.611	
: 5	1 12	104900T.		3	90		98/SB		1.27			208.19	5.896	\$		23,460	
} ·		104900/R		0	0				20.77	_	4.77	206.92	5.860	8928	•	23,296	Malkana Minor(30,77)
×		107157/L		2257	889		98/SB		200	• • •	4. 8.	176.15	4.989	416		19,748 WAPDA/OFWM	
8	57.1	110250/L	110250 33604	3093	943		102/SB	1.23 0.035	1.35	Ξ.	8.	174.31	4.936	432		19,579 WAPDA	
88	288	111500/R	111500 33985	1250	381		100/SB	1.46 0.041	1.61	Ξ.	3.97	172.21	4.877	515		19,405	
\$	59 1	113775/L	113775 34679	2275	693		102/SB	1.27 0.036	1.40	_	3.93	170.30	4.823	433	_	19,196 WAPDA/OFWM	
8	8	114928/R	114928 35030	1153	351		105/SB		8	_	3.89	168.36	4.768	33	_	19,021	
\$		116055/L	• •	1127	344		102/SB		1.30		3.87	167.08	4.732	415		18,891 WAPDA	
8	ŝ	118000/R	118000 35966	1945	593		105/SB		1.38	-	3.83	165.52	4.687	410	-	18,723 OFWM	
ŝ	83	119327/L	119327 36371	1327	404		106/SB		1.20	_	3.80	163.69	4.636	% %	155	18,558 WAPDA	
Ŗ	8	119347/L		ឧ	9		106/SB		2.21	-	3.77	162.18	4.593	8	279	18,402 WAPDAVOFWM	
\$3	8	120100/L	120100 36606	753	230		106/SB		1.95		3.71	159.96	4.530	Ş	24	18,123 WAPDA/OFWM	-
8	8	121714/L	121714 37098	1614	492		106/SB		2.1.	129.24	3.8	157.84	4.470	677	274	17,878 WAPDA/OFWM	
6	-	121850/L	121850 37140	136	4		110/SB	1			3,61	155.36	4,400	403	183	17,604 WAPDA	
38	88	121864/R	121864 37144	4	4		105/SB	1.27 0.036			3.57	154.06	4.363	428	173	17,441	
9	69	123475/L	123475 37635	1611	491		110/SB			-	3.54	152.66	4.323	817	331	17,268 WAPDAOFWM	•
5	5	126331/L	126331 38506	2856	871		114/SB			122.55	3.47	149.72	4.240	88	283	16,938 WAPDA	
7.	71	126500/R		69	22		107/SB				3.41	146.89	4.160	945	382	16,655 WAPDA	
17	2	126620/L		120	37		111/SB	1.60 0.045		5 117.67	3.33	143.68	4.069	2 62		16,272	
l	•	126620AL			0			12.15 0.344			3.29	141.89	4.018	4277		16,045	Wasuana Mibor(14.34)
1,	73	131150/R		4530	1381	:	107/SB	2.05 0.058		5 103.92	2.94	127.55	3.612	722	292	14,314 OFWM	
7,		137100/L		2950	1814		113/SB		1.43		2.88	124.38	3.522	432	175	14,022	
75	75	140615/L	140615 42859		1071		113/SB	0.70 0.020		-	2.85	121.76	3.448	247	8	13,847	
92		142000L	142000 43282		422		113/SB				2.83	120.30	3.407	335	136	13,747	
		142200/L	142200 43343	8	19	-			•		2.80	118.98	3.370	3234	388	13,611	Tandalian Minor(11.32
5	1	142360/R	•	8	46		112/SB			_	2.53	107.62	3.048	827	335	12,302 WAPDA/OFWN	•
32		144900/R	•	2540	774		112/SB	1			4.6	105.01	2.974	337		11,968 OFWM	
79	67	145048/L	•	148	\$\$		116/SB		0.78		2.43	103.49	2.931	23.5	25	11,831	
Ş	8	147325/R	٠.	2277	694		115/SB				2.41	102.68	2.908	305		11,730	
81	81	149485/R	•	516	658	•					233	101.33	2.870	8 5	× 6	11,608	
8	23	150600/L	7	11115	950		116/SB				200	3 5	000.7	3 8		11,209	
83	8 8	150660/R	150660 45921	88	3 <u>5</u>		85/251	1.65 0.047	× 5	83.44	2.50	25.60	7727	080 787		11.400 OFWM	
d b	8 8	100/00K	•		3 5		03/67	1	-		16	8	27.0	453		11 012 OFWIN	
8 %	8 %	150510/R	• •	3 8	149 M Area	Α.σ.	00741	_			2.23	94.62	2.680	B.S.		10.829	Bulk Supply
3	3	1,5000	_	2	۶		•		•		2.20	93.43	2646	2866	2374	10,829	Rodian Minor(20,24)
		155300/R	_	3800	1158			12.95 0.367	15.01		1.71	73.18	2.072	4394		8,455	Munde Minor(15.01)
%	55	156800/L	-	1500	457		116/SB			3 47.42	1.34	57.60	1.631	8	8	9,676	
88	88	159767/R	159767 48697	2967	Š		123/SB	1.12 0.032			1.33	56.78	1.608	38	8	6,595 OFWM	
8	8	164272/L	٠.	Ť	1373		126/SB		_		1.30	55.17	1.562	8	8	6,435	
8	8		4,	2072	632		127/SB	_			1.28	\$3.8	1.528	259	528	6,353	
6		'		8	33		128/SB	0.35, 0.010	200	43.56	3 2	35.15	1/4/1	124	3 5	0,120	100
		100450/1	46/00 004001	> .	> '			6.10 0.431	ř	_	77.7	3.1.	3	6007	1477	2/2/5	Alira Minor(9.45)

Table B - 1 (1/3) Breakdown of Authorized and Design Discharge Calculation for LJC Area

Colored Colo	Watercourse 171590/L 1		Oistan	*			A fair V	pozu	Design	Dischary	2	Discharge	(acte)	(Pa	₹	
128/58 144 0042 154 336 094 307 1132 497 201 4390 1128/58 144 0042 154 336 095 3997 1132 458 231 4739 0944 1132 353 094 3310 1079 377 24 4519 0944 1132 2557 034 3310 1079 377 24 4519 0944 1132 2557 034 3310 1079 377 24 4519 0944 1132 2557 034 3379 0392 393 159 4133 155 044 037 112 032 125 2557 034 3379 0392 339 159 4133 155 044 037 112 032 2557 034 3379 0392 0383 159 4133 159 044 037 122 2557 034 3379 0392 0383 159 4133 1378 137 0392 0383 0392 0383 159 4133 1378 137 0392 0383 043 043 043 139 139 149 4133 137 0392 0383 044 138 044 045 149 1884 035 034 0392 0383 0383 034	II~			ĺ			MINN						1		;	
127/88	~		(feet)	(m)			(casec)	(m,3/s)		cusec) (r	n3/s) (ca	(m3/	0		(ha)	
127/58			5140	1567		128/SB	1.41	0.040	1.55	35.05		2.07	25 49			
131/58			2210	674		127/SB	1 49	0.042	<u></u>	33.64		9.97 1.1.	32 23	•	4.729	
133/58			2180	\$		127/SB	2	9700	1.80	32.15			_		4,516	
135.68	_		120	37		131/SB	0.94	0.027	1.03	30.51						
131/SB 165 0.047 1.82 28.45 0.81 33.79 0.857 582 224 5.594 132/SB 127 0.010 0.037 26.80 0.75 30.90 0.878 2022 822 3.711 132/SB 127 0.036 1.40 18.4 0.15 22.10 0.658 642 262 2.82 3.711 133/SB 2.12 0.036 1.40 18.4 0.15 22.10 0.658 642 282 3.711 135/SB 2.12 0.036 1.40 18.4 0.15 22.10 0.658 642 282 23.71 136/SB 2.12 0.036 1.40 18.4 0.15 2.03 0.437 8.8 642 2.62 0.898 133/SB 2.12 0.036 1.40 18.4 0.15 1.043 1.84 135/SB 1.37 0.039 1.51 1.316 0.37 15.21 0.437 8.8 136/SB 1.37 0.039 1.51 1.316 0.37 15.21 0.437 8.8 136/SB 1.38 0.045 1.74 1.17 0.33 1.36 0.335 490 1.98 1.641 136/SB 1.38 0.039 1.51 1.16 0.37 15.21 0.437 8.8 136/SB 1.38 0.039 1.54 1.02 1.02 1.16 0.32 422 136/SB 1.37 0.039 1.46 8.61 0.24 9.8 0.274 4.8 189 1.216 0.899 139/SB 1.46 0.054 1.79 1.23 1.80 0.335 490 1.98 1.641 139/SB 1.46 0.054 1.39 4.00 0.11 4.46 0.126 4.44 1.80 5.60 0.999 139/SB 1.47 0.030 1.18 1.07 0.03 1.18 0.037 56. 222 1.53 0.9999 139/SB 1.47 0.047 1.84 2.74 0.08 3.06 0.087 56. 222 1.53 0.9999 14/SB 1.48 0.054 1.79 1.257 0.35 4.46 0.137 52.4 2.22 1.659 0.9999 158/SB 1.48 0.054 1.79 1.257 0.35 4.46 0.137 52.2 2.23 1.639 0.9999 158/SB 1.40 0.044 1.79 1.257 0.35 4.46 0.410 5.32 2.23 1.639 0.9999 158/SB 1.40 0.044 1.79 1.257 0.35 4.46 0.410 5.32 2.23 1.639 0.9999 158/SB 1.40 0.044 1.79 1.257 0.35 4.46 0.410 5.32 2.23 1.644 0.9999 158/SB 1.40 0.044 1.34 1.25 0.24 5.32 0.4099 158/SB 1.40 0.044 1.79 1.257 0.35 5.27 2.1 0.44 5.8 61.0999 158/SB 1.40 0.044 1.37 1.25 0.35 5.27 2.1 0.44 5.8 61.0999 158/SB 1.40 0.044 1.57 0.122 5.20 1.25 5.0 2.21 1.044 0.999 158/SB 1.40 0.044 1.54 2.38 0.44 0.137 5.77 2.13 0.9999 158/SB 1.40 0.044 1.54 2.38 0.44 0.137 5.77 2.13 0.9999 158/SB 1.40 0.044 1.54 2.38 0.44 0.137 5.77 2.13 0.9999 158/SB 1.40 0.044 1.54 2.38 0.44 0.137 5.77 2.13 0.9999 158/SB 1.40 0.044 1.54 2.38 0.44 0.137 5.77 2.13 0.9999 158/SB 1.40 0.04			0	0		128/SB	1.12	0.032	1.33	29.57						
133/58 1.34 0.010 0.37 26.80 0.76 31.47 0.891 119 48 37.59 133/58 1.24 0.055 1.40 18.54 0.55 24.30 0.688 20.2 20.11 133/58 2.12 0.055 1.40 18.54 0.55 24.30 0.688 46.2 260 2.888 133/58 2.14 0.061 2.35 15.35 0.43 17.53 0.505 4.45 18.0 2.45 0.999 133/58 2.14 0.061 2.35 15.35 0.43 17.53 0.508 754 305 2.143 133/58 2.14 0.061 2.35 15.35 0.43 17.53 0.508 754 305 2.143 133/58 1.37 0.039 1.37 13.10 0.37 15.21 0.431 4.81 15.135 136/58 1.38 0.045 1.74 11.79 0.33 13.60 0.385 4.90 198 1.641 136/58 1.38 0.035 1.72 10.50 1.25 1.65 0.22 4.68 189 1.016 0.999 139/58 1.30 0.035 1.32 1.20 0.23 1.32 4.68 1.32 1.35 0.999 139/58 1.30 0.035 1.32 1.03 1.33 1.30 0.33 3.64 0.12 4.68 1.35 0.999 139/58 1.30 0.035 1.32 1.30 0.03 1.18 1.07 0.03 1.18 0.037 3.64 2.23 3.63 0.999 139/58 1.37 0.035 1.38 1.07 0.03 1.18 0.037 3.64 2.23 3.63 0.999 139/58 1.37 0.035 1.38 1.07 0.03 1.18 0.037 3.64 3.23 3.63 0.999 139/58 1.37 0.035 1.38 1.07 0.03 1.18 0.037 3.64 3.23 3.63 0.999 139/58 1.30 0.035 1.30 0.30 1.38 0.30			5252	160]		131/SB	1 65	0.047	1.82	28,45				•		
1325B 137 0.056 26.46 0.75 30.99 0.878 2032 822 3711 1335B 127 0.055 2.02 2.068 0.59 2.43 0.688 642 260 2.888 1335B 127 0.055 2.44 1757 0.50 20.45 0.579 758 307 2.443 0.9wM 1335B 2.14 0.061 2.35 1.53 0.43 1.549 0.578 754 307 2.443 0.9wM 1355B 137 0.055 131 0.37 1.54 0.47 8.5 754 30.7 2.443 0.9wM 1365B 138 0.045 1.74 11.79 0.23 1.540 0.335 462 227 1.443 1365B 138 0.045 1.74 11.79 0.23 1.540 0.335 462 227 1.443 1365B 138 0.055 1.52 1.75 1.52 0.43 1.54 4.55 1.89 1.05 0.9wM 1367SB 138 0.053 1.54 1.02 0.31 1.540 0.325 4.62 227 1.443 1367SB 138 0.053 1.54 1.02 1.25 1.02 1.16 0.329 6.72 2.77 1.443 1367SB 138 0.053 1.54 1.02 1.17 0.03 1.18 0.033 3.76 1.25 1.05 0.9wM 1397SB 139 0.054 1.02 1.00 1.18 1.07 0.03 1.18 0.033 3.76 1.52 1.52 1397SB 1.07 0.030 1.18 1.07 0.03 1.18 0.033 3.76 1.52 1.52 1397SB 1.44 0.054 1.18 1.07 0.03 1.18 0.033 3.76 1.52 1.52 1397SB 1.45 0.042 1.45 0.042 1.44 0.058 1.44 0.058 1.04 0.048 1397SB 1.45 0.042 1.45 0.043 1.18 0.033 3.76 1.52 1.52 1387SB 1.50 0.054 0.073 3.04 2.76 0.08 3.04 0.087 6.087 6.097 1397SB 1.50 0.054 0.073 3.04 2.76 0.08 3.04 0.086 6.097 6.097 6.008 1397SB 1.50 0.054 0.073 3.04 2.76 0.08 3.04 0.086 6.097 6.098 1388 0.090 0.023 0.08 1.094 0.03 1.18 0.03 2.23 1.639 0.wm 1388 0.090 0.023 0.08 1.094 0.03 1.022 2.33 1.44 0.008 1497 0.054 1.19 0.051 1.19 0.051 1.25 0.056 6.059	-		1208	398			0.34	0.010	0.37	26.80						
1375B 134 0.052 202 2.056 0.55 24.30 0.658 642 260 2.898	_		8	302			5.78	20.16	9.60	26.46			•			Dhabian Minor(6.60)
133/5B 127 0306	-		2212	674		132/SB	1.84	0.052	2.02	20.68						
132/SB	-		3280	8		133/SB	1.27	0.036	1 40	18.84					-	
134/SB		-2.	1120	4		132/SB	2.22	0.063	77.7	17.57						
13658			2190	88		133/SB	2.14	0.061	2.35							
136/5B 137 0.039 1.51 13.16 0.37 15.21 0.431 481 195 1.836 136/5B 1.58 0.045 1.74 11.79 0.33 15.00 0.385 490 198 1.641 136/5B 1.35 0.038 1.46 8.61 0.24 9.68 0.274 468 189 1.216 0ewwh 139/5B 1.30 0.034 1.45 1.25 7.28 0.21 8.20 0.232 432 195 1.026 0ewwh 139/5B 1.30 0.034 1.39 1.52 7.28 0.21 8.20 0.232 432 195 1.026 0ewwh 139/5B 1.30 0.034 1.39 2.74 0.08 3.06 0.087 864 228 380 139/5B 1.07 0.030 1.18 1.07 0.03 1.18 0.033 376 15.2 15.2 139/5B 1.07 0.030 1.18 1.07 0.03 1.18 0.033 376 15.2 15.2 14/5B 1.49 0.062 1.64 4.25 0.12 4.84 0.137 854 8.056 14/5B 1.60 0.049 1.79 12.57 0.36 1.497 606 17/5B 1.60 0.049 1.79 12.57 0.36 1.447 606 17/5B 1.50 0.040 1.79 12.57 0.36 1.447 606 18/5B 1.79 0.051 1.97 8.0 0.24 9.72 2.23 1.69 0ewwh 18/5B 1.50 0.040 1.79 12.57 0.36 1.44 0.275 359 218 1.306 18/5B 1.79 0.051 1.97 8.0 0.24 8.0 0.24 6.0 0.24 8.0 0.24 18/5B 1.50 0.040 1.54 2.98 0.08 2.88 0.24 6.0 0.24 3.08 0.24 8.0	_		2668	813			0.05	0.001	9.0				B.S.		1,836	
113/58 1.58 0.045	~4		1650	503		136/SB	1.37	0.039	1.51							
136/SB 1.60 0.045 1.76 10.21 0.29 11.61 0.329 562 227 1,443 136/SB 1.30 0.038 1.46 8.61 0.24 9.68 0.274 482 195 10.26 0 PWM 136/SB 1.30 0.039 1.25 2.28 2.27 2.30 2.21 4.42 195 10.26 0 PWM 139/SB 1.26 0.036 1.39 4.00 0.11 4.46 0.126 4.44 180 560 0 PWM 139/SB 1.26 0.036 1.39 4.00 0.11 4.46 0.126 4.44 180 560 0 PWM 139/SB 1.26 0.036 1.39 4.00 0.11 4.46 0.126 4.44 180 560 0 PWM 139/SB 1.67 0.047 1.84 2.74 0.08 3.06 0.087 564 2.28 3.80 139/SB 1.67 0.047 1.84 2.74 0.08 3.06 0.087 564 2.28 3.80 139/SB 1.49 0.042 1.44 4.25 0.12 4.34 0.137 5.24 2.12 6.06 74/SB 1.49 0.042 1.44 4.25 0.12 4.34 0.137 5.24 3.44 77/SB 1.65 0.046 1.79 12.57 0.36 2.44 0.137 5.22 1.659 0 PWM 81/SB 1.53 0.043 1.68 1.04 0.29 1.25 0.35 2.23 1.659 0 PWM 84/SB 1.39 0.045 1.59 0.051 1.97 8.61 0.24 9.72 0.275 5.22 1.084 0 PWM 84/SB 1.39 0.045 1.58 0.04 1.74 0.049 5.27 2.13 2.13 0.70 WM 84/SB 1.48 0.046 1.74 1.58 0.04 1.74 0.049 5.27 2.13 2.13 0.70 WM 84/SB 1.58 0.045 1.74 1.58 0.04 1.74 0.049 5.27 2.13 2.13 0.70 WM 84/SB 1.58 0.045 1.74 1.58 0.04 1.74 0.049 5.27 2.13 2.13 0.70 WM 84/SB 1.58 0.045 1.74 1.58 0.04 1.74 0.049 5.27 2.13 2.13 0	-		4505	1373		113/SB	1.58	0.045	1.74		_				: .	
137/SB	63		3165	965		136/SB	8	0.045	1.76		_					
136/SB 1.38 0.039 1.52 7.28 0.21 8.20 0.232 482 195 1,026 opwm 139/SB 1.90 0.054 2.09 5.90 0.17 6.58 0.186 670 271 831 opwm 139/SB 1.56 0.036 1.39 4.00 0.11 4.46 0.087 544 180 560 opwm 139/SB 1.07 0.030 1.18 1.07 0.03 1.18 0.033 376 152 152 139/SB 1.07 0.030 1.18 1.07 0.03 1.18 0.033 376 152 152 139/SB 1.07 0.030 1.18 1.07 0.03 1.18 0.03 376 152 152 139/SB 1.07 0.030 1.18 1.07 0.03 1.18 0.03 376 2023 144/SB 1.49 0.042 1.64 4.25 0.12 4.84 0.137 524 212 506 144/SB 1.49 0.042 1.64 4.25 0.12 4.84 0.137 524 212 506 144/SB 1.60 0.046 1.79 12.57 0.36 4.46 0.410 552 223 1.639 opwm 1257 0.80 0.023 0.38 10.94 0.31 12.22 235 239 218 1.30 1258 0.80 0.023 0.38 10.94 0.31 12.22 235 239 218 1.30 1259 0.80 0.023 0.38 10.94 0.31 2.25 235 0.94 0.94 147 0.80 0.80 0.80 0.80 0.24 2.25 0.84 0.94 148 0.80 0.80 0.80 0.80 0.34 2.8 0.14 0.25 2.35 0.94 0.94 147 0.80 0.80 0.80 0.80 0.34 2.8 0.89 2.8 0.94 0.94 148 0.80 0.80 0.80 0.80 0.34 2.8 0.80 2.35 0.12 0.94 148 0.80 0.80 0.80 0.80 0.34 2.90 0.94 0.35 0.35 0.35 0.35 0.95 0.94 0.94 0.35	(1		250	76		137/SE		0.038	1.46			_				
139/SB	64		2368	722		136/SB		0.039	1.52			_	-	_		
137/SB 1.26 0.036 1.39	C		307	246		139/SB	8	0.054	508	8	0.17	_		_		
139/SB 1.67 0.047 1.84 2.74 0.08 3.06 0.087 564 228 380 139/SB 1.07 0.030 1.18 1.07 0.03 1.18 0.033 376 152 152 371.58 10.52	C		475	145		137/SB	1.26	0.036	1.39	8	0.11					
139/SB 1.07 0.030 1.18 1.07 0.03 1.18 0.033 376 152	~		1870	570		139/SB	1.67	0.047	28.	2.74	0.08					
371.58 10.52 4.25 0.13 4.25 0.13 4.25 0.13 4.25 0.13 4.25 0.13 4.25 0.13 4.25 0.14 4.25 0.14 4.25 0.14 4.25 0.25 4.25 0.25 4.29 0.25 4.20	e i		8	6		139/SB	1.07	0.030	1.18	1.07	0.03					
371.5\$ 10.52 36.322 74/SB 1.49 0.042 1.64 4.25 0.12 74/SB 2.76 0.078 3.04 2.76 0.086 973 394 4.25 0.12 74/SB 4.25 0.12 74/SB 1.63 0.046 1.79 12.57 0.36 77/SB 0.80 0.023 0.88 10.94 0.31 12.52 0.355 223 77/SB 1.63 0.046 1.79 12.64 0.31 12.52 0.355 2.23 77/SB 1.63 0.046 1.79 12.67 0.36 14.46 0.410 552 223 77/SB 1.63 0.046 1.79 12.67 0.36 14.46 0.410 552 223 82/SB 1.79 0.051 1.97 8.61 0.24 9.72 0.275 552 223 82/SB 1.79 0.051 1.97 8.61 0.24 9.72 0.275 552 223 82/SB 1.81 0.051 1.99 4.79 0.14 5.37 0.152 580 235 84/SB 1.40 0.040 1.54 2.98 0.08 3.28 0.093 406 164 84/SB 1.58 0.045 1.74 1.58 0.04 1.77 0.049 527 213	7		8	18												Proposed Tail
4,25 0,12 74/SB 1,49 0,042 1,64 4,25 0,12 4,84 0,137 524 212 74/SB 2,76 0,078 3,04 2,76 0,08 3,04 0,086 973 394 4,25 0,12	:						371.58	10.52					89,754 36,322			
74/SB 1,49 0,042 1,64 4,25 0,12 4,84 0,137 524 212 74/SB 2,76 0,078 3,04 2,76 0,08 3,04 0,086 973 394 1,497 6,06 1,75 0,12 1,497 6,06 1,75 0,12 1,257 0,36 1,446 0,410 552 223 77/SB 0,80 0,023 0,88 10,94 0,31 12,52 0,355 223 1,14 8,158 1,79 0,051 1,97 8,61 0,24 9,72 0,275 552 223 8,258 1,79 0,051 1,97 8,61 0,24 9,72 0,275 552 223 8,258 1,99 0,051 1,97 8,61 0,24 9,72 0,275 552 223 8,258 1,90 0,051 1,97 8,61 0,24 9,72 0,275 552 223 8,258 1,90 0,051 1,97 8,61 0,24 9,72 0,275 552 223 8,258 1,90 0,051 1,97 8,61 0,24 9,72 0,275 552 223 8,458 1,90 0,040 1,54 2,98 0,08 3,28 0,093 4,06 1,64 8,458 1,58 0,045 1,74 0,049 527 2,13	8	/R,Kirana	Distribu	tary)	:											
74/SB 1.49 0.042 1.64 4.25 0.12 4.84 0.137 524 212 74/SB 2.76 0.078 3.04 2.76 0.08 3.04 0.086 973 394 6.25 0.12 12.57 0.36 1.497 606 77/SB 0.80 0.023 0.084 10.94 0.31 12.57 0.35 223 77/SB 1.63 0.045 1.79 12.57 0.36 14.46 0.410 552 223 77/SB 1.53 0.045 1.79 12.57 0.36 14.46 0.410 552 223 82/SB 1.79 0.051 1.97 8.61 0.24 9.72 0.275 552 223 82/SB 2.03 0.057 2.23 6.82 0.19 7.75 0.200 614 248 84/SB 1.81 0.051 1.99 4.79 0.14 537 0.152 580 235 84/SB 1.40 0.040 1.54 2.98 0.08 3.28 0.093 406 164 84/SB 1.58 0.045 1.74 1.58 0.04 1.74 0.049 527 213		- 1								- 1		- 1	1	-		
71/58 1.63 0.046 1.79 12.57 0.36 606 77/58 1.63 0.046 1.79 12.57 0.36 77/58 0.002 0.88 10.94 0.31 12.52 0.355 281 114 81/58 1.79 0.051 1.99 4.79 0.14 5.37 0.35 5.39 2.18 82/58 2.03 0.057 2.23 6.24 9.72 0.255 5.52 82/58 1.81 0.051 1.99 4.79 0.14 5.37 0.152 580 2.35 84/58 1.40 0.040 1.54 2.98 0.08 3.28 0.093 4.06 1.64 84/58 1.58 0.045 1.74 1.58 0.04 1.77 0.049 5.27 2.13		- 1	2500 2000	0 0	:	74/SB 74/SB		0.042	~ ~ \$ \$							
77/58 1.63 0.046 1.79 12.57 0.36 77/58 0.023 0.88 10.94 0.31 12.52 0.355 281 114 81/5B 1.53 0.043 1.68 10.14 0.29 11.47 0.325 281 114 82/5B 1.79 0.051 1.97 8.61 0.24 9.72 0.255 539 2.18 82/5B 2.03 0.057 2.23 8.61 0.24 9.72 0.255 552 82/5B 1.81 0.051 1.99 4.79 0.14 5.37 0.152 580 2.35 84/5B 1.40 0.040 1.54 2.98 0.08 3.28 0.093 406 164 84/5B 1.58 0.045 1.74 1.58 0.04 1.74 0.049 527 2.13							4.25	0.12							ļ	
77/58 1.63 0.046 1.79 12.57 0.36 4.46 0.410 552 223 77/58 0.80 0.023 0.88 10.94 0.31 12.52 0.355 281 114 81/58 1.53 0.043 1.68 10.14 0.29 11.47 0.355 281 114 82/58 1.79 0.051 1.97 8.61 0.24 9.72 0.255 539 218 82/58 2.03 0.057 2.23 6.82 0.19 775 0.250 614 248 84/58 1.81 0.051 1.99 4.79 0.14 537 0.152 580 235 84/58 1.40 0.040 1.54 2.98 0.08 3.28 0.093 406 164 84/58 1.58 0.045 1.74 1.58 0.04 1.77 0.049 527 213	ı		:		: . }				ž.,	:			Š	٥		
77/SB 1.63 0.046 1.79 12.57 0.36 14.46 0.410 552 223 77/SB 0.80 0.023 0.88 10.94 0.31 12.52 0.355 281 114 81/SB 1.53 0.043 1.68 10.14 0.29 11.47 0.325 281 114 82/SB 1.79 0.051 1.97 8.61 0.24 9.72 0.275 552 223 82/SB 2.03 0.057 2.23 6.82 0.19 7.75 0.205 614 248 84/SB 1.81 0.051 1.99 4.79 0.14 5.37 0.152 580 235 84/SB 1.40 0.040 1.54 2.98 0.08 3.28 0.093 406 164 84/SB 1.58 0.045 1.74 1.58 0.04 1.77 0.049 527 213	180	0/R .Kirana	Distrib	stary)										٠		
771 2530 771 77/SB 1.63 0.046 1.79 12.57 0.36 14.46 0.410 552 223 1705 3065 934 77/SB 0.80 0.023 0.88 10.94 0.31 12.52 0.355 281 114 2097 1285 392 81/SB 1.53 0.043 1.68 10.14 0.29 11.47 0.325 281 114 2120 75 23 82 1.79 0.051 1.97 8.61 0.24 9.72 0.275 552 223 3200 3545 1081 82/SB 1.79 0.057 2.23 6.82 0.19 7.75 0.226 614 248 4112 2990 911 84/SB 1.81 0.051 1.59 4.79 0.14 5.37 0.152 580 235 4112 0 0 84/SB 1.40 0.049 1.74 0.049 5.77 <t< td=""><td></td><td></td><td></td><td>•</td><td></td><td></td><td></td><td>1 -1 -1</td><td></td><td></td><td></td><td></td><td>-</td><td></td><td>1.639</td><td></td></t<>				•				1 -1 -1					-		1.639	
1705 3065 934 77/SB 0.80 0.023 0.88 10.94 0.31 12.52 0.355 281 114 2097 1285 392 81/SB 1.53 0.043 1.68 10.14 0.29 11.47 0.325 539 218 2120 75 23 82/SB 1.79 0.051 1.97 8.61 0.24 9.72 0.275 552 223 3200 3545 1081 82/SB 2.03 0.057 2.23 6.82 0.19 7.75 0.220 614 248 4112 2990 911 84/SB 1.81 0.051 1.99 4.79 0.14 5.37 0.152 580 235 4112 0 0 84/SB 1.40 0.040 1.54 2.98 0.08 3.28 0.093 406 164 4112 0 0 84/SB 1.58 0.045 1.74 0.049 527 21			2530	17		77/58	1.63	0.046	25.7	l		ı		1		
2097 1285 392 81/SB 1.53 0.043 1.68 10.14 0.29 11.47 0.325 539 218 2120 75 23 82/SB 1.79 0.051 1.97 8.61 0.24 9.72 0.275 552 223 3200 3545 1081 82/SB 2.03 0.057 2.23 6.82 0.19 7.75 0.220 614 248 4112 2990 911 84/SB 1.81 0.051 1.99 4.79 0.14 5.37 0.152 580 2.35 4112 0 0 84/SB 1.40 0.040 1.54 2.98 0.08 3.28 0.093 4.06 1.64 4112 0 0 84/SB 1.58 0.045 1.74 1.58 0.04 1.74 0.049 527 213			3065	33		8S/LL	0.80	0.023	0.88							
2120 75 23 82/SB 1.79 0.051 1.97 8.61 0.24 9.72 0.275 552 223 3200 3545 1081 82/SB 2.03 0.057 2.23 6.82 0.19 7.75 0.20 614 248 4112 2990 911 84/SB 1.81 0.051 1.99 4.79 0.14 5.37 0.152 580 235 4112 0 0 84/SB 1.40 0.040 1.54 2.98 0.08 3.28 0.093 406 164 4112 0 0 84/SB 1.58 0.045 1.74 1.58 0.04 1.74 0.049 527 213			1285	392		81/SB		0.043	38.							
3200 3545 1081 82/SB 2.03 0.057 2.23 6.82 0.19 7.75 0.220 614 248 861 4112 2990 911 84/SB 1.81 0.051 1.99 4,79 0.14 5.37 0.152 580 235 612 4112 0 0 84/SB 1.40 0.040 1.54 2.98 0.08 3.28 0.093 406 164 378 4112 0 0 84/SB 1.58 0.045 1.74 1.58 0.04 1.74 0.049 527 213 213			75	ន		82/SB		0.051	1.97							
4112 2990 911 84/SB 1.81 0.051 1.99 4.79 0.14 5.37 0.152 580 235 612 4112 0 0 84/SB 1.40 0.040 1.54 2.98 0.08 3.28 0.093 406 164 378 4112 0 0 84/SB 1.58 0.045 1.74 1.58 0.04 1.74 0.049 527 213 213			3545	1081		82/SB		0.057	2.23							
4112 0 0 84/SB 1.40 0.040 1.54 2.98 0.08 3.28 0.093 406 164 378 4112 0 0 84/SB 1.58 0.045 1.74 1.58 0.04 1.74 0.049 527 213 213			2883	911		84/SB		0.051	8:						612	
4112 0 0 84/58 1.58 0.045 1.74 1.58 0.04 1.74 0.049 527 213			0	0		84/SB		0.040	1.54						378	
			0	0		84/SB	1.58	0.045	1.74							

Table B - 1 (1/3) Breakdown of Authorized and Design Discharge Calculation for LJC Area

ž	3	(teet)	(m)	Distance	, 8			Authorized			Discharge	Ď	Discharge	(acte)	æ	CCA		
,			•	(feet)	(w)	:		(cusec) (m3/s)	(cusec)	ŀ	(cnsec) (m3/s)	(cosec)	(m3/s)			(ha)		Ì
														1.639				
] - -											
7.27	Walkana Minor(RD 104900/R .Kirana Distributary)	1049007	R. Kir.	ana Dist	ributary)			:										
						'			:	23						3.548		
	214 [610/L	1610	167	1610	167	2	101/SB		l.	1.98 25	ı		178.0 7	625	253	3,548 WAPDA		
	213 44050	4405	1343	2075	852	ő	100/SE						_	528	214	3,295 WAPDA		
1 1	215 7645/18	7645	2330	3240	886	દ	/SB			0.83 22.			_	566	108	3,082		
١ <	71C-04 51C	883	2686	17	358	10	1/20						_	417	169	2,974 WAPDA		
tv	717 102037	1000	3110	1383	422	2 2	101/SB	1 17 0.0	0.033	_	20.63 0.58	8 24.16	_	405	164	2,805 WAPDA		
, v	218 12126/9	13134	4003	2	893 Assignmen		}							867	351	2,641 WAPDA		
1 (13405	4113	196	110 Assignmela	- 				٠. ـ			3 0.562	21:1	88	2,291		
- 00	•	16290	200	2705	852		3/SB							88	239	2,205 WAPDA		
0		17460	5322	1170	357	Ö	103/SB							555	22	1,966 WAPDA		
٠ 9	•	20782	3	3322	1013	0	103/SB							823	333	1,744 WAPDA		
-		22990	7007	2208	673	8	99/ASB						_	516	88	1,411		
: 3		24000	7315	1010	308 P.A.F		:			0.08				22	2	1,202		
ነ ተኅ	225 33130/L	33130	36001	9130	2783 P.A.F									L.S.		1,192		
•		33330		200	19	0	%/SB							8	349	~¯		
•		33330			0	0	8S/6		. T.	4.65 5				1519				
9		33330		0	0	01	104/SB							\$	-	228 WAPDA		
								l	0.73					8768	3548			
														3.548	-			
}	10 / 10 A	000000		Dist.														
-	Washana Minor (A.) A20400/ E, Minana Distributary	3007	17'7'	ST PINE	ti iodidai y/					12		Ţ				1,731	•	. !
-	205 7650/R	7650	2332	7650	2332	Ξ	11/58	1.57 0.0			12.15 0.34		1	551		1.731		
~	206 10300/R	10300	3139	2650	808	11.	3/SB					-				1,508 WAPDA		
~	207 10320/R	10320		8	9	11	114/SB	1.61 0.0	0.046			25 10.17	17 0.288		229	1,268 WAPDA		
4	208 116SO/R	11680		1360	415	11	114/SB									1,039		
Ŋ	209 16000/L	90091		4320	1317	11	114/SB		0.050	93 5						797		
φ	210 16000/TF	16000	4877	0	0	Π	S/SB		_							547 OFWM		
<u>-</u>	211 ZZ600/TR	22600		000	2012	7	115/SB		7							384	:	
90	212 22600/TL	22600		0	0	Ξ	S/SB			34 1	22 0.0	:		:	٠.	174		
								12.15 0	0.34					4,277	1.731			

Table B - 1 (1/3) Breakdown of Authorized and Design Discharge Calculation for LJC Area

Company Nationary Company Nationary Company Nationary Company Nationary Nationary Company Company Nationary Company									\(\frac{1}{2}\)		ľ		١			į	ļ	l
133/8			,	. I	53 Z		Village	Chack No.	Outlet	SI.	; 3	cction	5 2	5.00		5	Section improved under	ker Kemans
1135/8	೨				J. Star				*	1	3	٦ŀ.	Ş	3	(aric)	(III)	\ \{\text{2}	
1355B 0,40 0,011 0,44 9,75 0,28 11,32 0,321 140 57 1165B 1,15 0,031 1,24 9,75 0,28 11,32 0,371 140 57 1165B 1,15 0,032 1,27 0,23 0,23 0,23 0,24 0,24 2,77 0,22 8,64 0,245 2,78 0,22 8,81 15 10,032 1,23 1,20 0,23 1,20 0,23 0,23 0,24 1,3 0,34					(ict)	(m)						. 1	1	1			(400)	
113/5 0.40 0.00 0.44 975 0.28 1132 0.331 140 57 116/5 1.15 0.033 1.27 9.35 0.28 1132 0.337 114 127 116/5 1.15 0.033 1.27 9.35 0.28 10.20 0.202 0.28 124 127 116/5 1.15 0.033 1.27 9.35 0.22 0.220 0.28 124 127 116/5 1.10 0.021 1.21 6.93 0.07 7/8 0.220 0.28 127 116/5 1.00 0.021 1.21 6.93 0.07 7/8 0.220 0.28 125 116/5 1.00 0.021 1.21 6.93 0.07 7/8 0.220 0.28 125 120/5 1.20 0.037 1.21 6.93 0.04 4.53 0.157 18.5 120/5 1.20 0.037 1.43 1.20 0.04 1.43 0.119 885 3.58 120/5 1.20 0.037 1.43 1.20 0.04 1.43 0.040 4.63 187 118/5 1.03 0.029 1.13 1.740 0.49 1.23 0.505 5.77 224 118/5 1.03 0.029 1.13 1.740 0.49 1.23 0.505 5.77 224 118/5 1.20 0.037 1.21 7.88 0.22 0.237 1.24 121/6 1.24 0.038 1.27 0.06 1.27 0.06 1.25 0.33 1.27 121/6 1.24 0.038 1.27 0.06 2.21 0.06 2.31 0.06 2.31 121/6 1.24 0.039 1.23 0.20 0.37 1.24 121/6 1.29 0.039 0.035 1.41 0.17 0.06 2.31 0.065 2.31 121/6 1.29 0.039 0.035 1.41 0.117 0.33 0.44 315 0.24 121/6 1.29 0.039 0.039 0.037 0.04 0.05 0.04 315 0.04 121/6 1.29 0.039 0.030 0.07 0.02 0.01 0.05 0.03 0.04 315 0.04 121/6 1.29 0.039 0.035 0.08 0.03 0.04 0.05 0.04 315 0.04 121/6 1.29 0.039 0.035 0.08 0.03 0.04 0.00 0.07 0.05 0.08 0.04 121/6 1.29 0.039 0.035 0.08 0.03 0.08 0.03 0.04 121/6 1.29 0.039 0.035 0.08 0.03 0.09 0.09 0.09 0.09 0.09 0.09 0.09	Tanc	fallian Minor(R	D 14220	N. L.	irana D	istributa	র	-								\$:
113/SB			.						ŀ				١	- 1			1.304	
1165B 1.15 0.033 1.27 9.35 0.26 10.83 0.307 314 177 1167SB		229 975/R	975	33	\$78	297		113/SB							- - - -	S	1,38 28	
istrerabad 0.070 0.014 0.55 8.20 0.22 9.26 0.262 R.F. 106/SB 1.07 0.022 0.85 7.70 0.22 8.64 0.245 270 109 119/SB 0.86 0.024 0.95 5.83 0.17 6.52 0.185 288 157 119/SB 0.86 0.024 0.95 5.83 0.17 6.52 0.185 288 157 119/SB 0.08 0.002 0.09 4.97 0.14 5.53 0.157 B.S. 115 120/SB 1.180 0.031 1.19 4.89 0.14 5.53 0.157 B.S. 115 120/SB 1.19 0.037 1.43 1.30 0.04 1.43 0.040 4.63 187 130 0.04 1.43 0.040 4.63 187 130 0.04 1.43 0.040 4.63 187 130 0.04 1.43 0.040 4.63 187 130 0.04 1.43 0.040 4.63 187 130 0.09 0.028 0.09 0.028 0.09 1.13 17.40 0.49 0.04 1.43 0.040 6.49 118/SB 1.00 0.029 1.13 17.40 0.49 0.021 1.18 0.029 1.13 17.40 0.49 0.037 1.20 0.037	64	230 7020/L	7020	2140	8045	1843		116/SB							314	121	1,248	
116/SB	4,0		8512	2594	1492	455		P.R				_			R.F.		1.13	Rest House Supply
119/SB	4	232 8950/R	8950	2728	438	134		116/SB							270	8	1,121	•
1995B 0.86 0.024 0.95 5.83 0.17 6.52 0.185 2.85 115	V 1		10.06	3080	156	352		119/SB							388	157	1.011	
internibad 120/SB 1.08 0.0024 0.99 5.03 0.117 0.159 1.150 120/SB 1.08 0.0031 1.19 4.89 0.14 5.43 0.157 B.S. 1.150 120/SB 1.08 0.0031 1.19 4.89 0.14 5.43 0.157 B.S. 1.150 120/SB 1.08 0.0037 1.43 1.30 0.04 1.43 0.040 4.83 358 358 1.150 118/SB 1.09 0.0037 1.43 1.30 0.04 1.43 0.040 6.57 1.304 118/SB 1.03 0.039 1.13 17.40 0.49 0.271 330 1.24 118/SB 1.03 0.039 1.13 17.40 0.49 0.271 330 1.24 117/SB 1.04 0.020 1.13 1.74 0.29 11.28 0.24 0.573 363 1.47 0.24 1.25/SB 1.78 0.036 2.17 7.68 0.22 0.27 0.67 0.302 6.26 2.33 1.24 121/SB 1.34 0.038 1.37 0.65 2.17 1.68 0.23 0.180 4.71 1.191 1.12/SB 1.34 0.038 1.24 0.39 1.35 0.180 4.71 1.191 1.12/SB 1.24 0.038 1.24 0.39 0.37 1.29 0.37 1.29 0.37 1.29 0.37 1.29 0.37 1.29 0.37 1.29 0.37 1.29 0.39 0.37 1.29 0.39 0.37 1.29 0.39 0.37 1.29 0.39 0.37 1.29 0.39 0.37 1.29 0.39 0.37 1.29 0.39 0.37 1.29 0.39 0.37 1.29 0.39 0.37 1.29 0.39 0.37 1.29 0.39 0.37 1.29 0.39 0.37 1.29 0.39 0.37 1.29 0.39 0.37 1.29 0.39 0.37 1.29 0.39 0.39 0.37 1.29 0.39 0.37 1.29 0.39 0.37 1.29 0.39 0.39 0.37 1.29 0.39 0.39 0.39 0.39 0.39 0.39 0.39 0.3) N		070	2006		246		03/01					_		You		730	
120/SB	D +		7771	0740	t.	0	-:	119/08							3	3	t 3	
120/SB 1.08 0.031 1.19 4.89 0.14 5.43 0.154 478 193 120/SB 2.51 0.077 1.43 1.30 0.04 1.43 0.040 4.63 187 120/SB 2.51 0.077 1.43 1.30 0.04 1.43 0.040 4.63 187 1304 1.304 1	-	_	11390	3,22	150	46 Nis	nterabad	:							B.S.		739	Bulk Supply
120/SB	99		13000	3962	1610	164		120/SB							478	193	739 OFWM	
120/SB	0	-	13000	36,	•	C		120/02							588	358	446	
13/15 1.25	٠,		2000	2062	> <	o c		03/061			. :				3 5	9 6	200	
118/SB	2		2000	7000		,		77.77		ı		П		ı	1000		101	
118/SB				:						Q.					200	<u> </u>	٠	
118/SB															£00.			
118/SB	3		D/002131	Virginia	2	Shartomy		,										
118/SB	į		W/MCTCT	40.11		iones y)	•					١.						
113/SB											17.					- 1	2,374	
118/SB 0.99 0.022 1.09 16.37 0.46 19.09 0.541 333 135 117/SB 1.64 0.046	~	239 220/L	220	67	220	67		118/SB							363		2,374	
117/SB	લ	240 2651AL	2651	808	2431	741		118/SB				_			333		2,227	
18/SB	۴٠,	241 S000/R	2000	1524	2349	716		117/SB		ì		Ī.			577		2.092 WAPDA	
17/8B 0.74 0.021 0.81 10.20 0.29 11.58 0.328 259 105 12.58 1.78 0.050 1.96 9.46 0.27 10.67 0.302 259 105 12.58 1.78 0.056 2.17 7.68 0.22 8.71 0.247 679 275 12.158 1.34 0.038 1.47 5.71 0.16 6.35 0.180 4.71 191 12.158 1.34 0.038 1.47 5.71 0.16 6.35 0.180 4.71 191 12.158 1.24 0.038 1.47 5.71 0.16 6.35 0.180 4.71 191 12.158 1.24 0.059 2.31 2.10 0.06 2.31 0.065 2.374 2.374 2.374 2.374 2.378 0.39 0.025 0.39 1.25 0.37 1.295 0.37 1.295 0.37 1.295 0.37 1.295 0.37 1.295 0.37 1.295 0.37 1.297 0.31 1.40 0.37 1.297 0.31 1.40 0.32 0.30 0.30 0.35 1.41 0.32 0.30 0.30 0.35 1.24 0.30 0.30 0.37 0.39 0.30 0.30 0.35 0.35 0.30 0.30 0.35 0.35 0.30 0.30 0.37 0.35 0.	4	242, 7660/L	7660	2335	2660	811		118/SB							638		1.859	
177SB 0.74 0.021 0.81 10.20 0.29 11.58 0.228 259 105 122/SB 1.78 0.056 2.17 7.68 0.22 8.71 0.247 679 275 121/SB 1.34 0.038 1.47 5.71 0.16 6.35 0.180 471 191 121/SB 2.27 0.064 2.50 4.37 0.12 4.81 0.136 800 324 121/SB 2.27 0.064 2.50 4.37 0.12 4.81 0.136 800 324 121/SB 2.10 0.059 2.31 2.10 0.06 2.31 0.065 740 299 121/SB 2.10 0.059 2.31 2.10 0.06 2.31 0.065 740 299 124/SB 0.34 0.010 0.37 12.95 0.37 15.01 0.425 119 48 124/SB 0.39 0.025 0.98 12.61 0.36 14.62 0.414 315 127 124/SB 0.30 0.008 0.33 10.44 0.30 11.92 0.338 L.S. 124/SB 1.49 0.051 1.97 8.71 0.25 9.82 0.278 652 256 124/SB 1.34 0.052 2.02 6.22 0.18 7.03 0.199 649 263 125/SB 2.31 0.065 2.28 2.07 0.06 2.28 0.064 772 259	v		11800	3507	4140	1262									380		100	New Charles
122/SB 1.78 0.050 1.96 9.46 0.27 10.57 0.302 626 253 122/SB 1.37 0.056 2.17 7.68 0.22 8.71 0.247 679 275 121/SB 2.27 0.064 2.50 4.37 0.12 4.81 0.136 800 324 121/SB 2.10 0.059 2.31 2.10 0.06 2.31 0.065 740 299 121/SB 2.10 0.059 2.31 2.10 0.06 2.31 0.065 740 299 121/SB 2.10 0.059 2.31 2.10 0.06 2.31 0.065 740 299 123/SB 0.39 0.025 0.37 12.95 0.37 15.01 0.425 119 48 124/SB 0.39 0.025 0.98 12.61 0.36 14.62 0.414 315 127 124/SB 0.39 0.008 0.33 10.44 0.30 11.92 0.338 1.5. 124/SB 0.30 0.008 0.33 10.44 0.30 11.92 0.338 1.5. 124/SB 0.70 0.000 0.77 6.92 0.20 7.82 0.278 653 256 124/SB 1.34 0.055 2.25 6.22 0.18 7.03 0.199 649 263 125/SB 2.31 0.065 2.28 0.064 7.24 2.39 1.25/SB 2.31 0.065 2.28 0.064 7.24 2.39 1.25/SB 2.07 0.059 2.28 2.07 0.06 2.28 0.064 7.24 2.39 1.25/SB 2.07 0.059 2.28 2.07 0.06 2.28 0.064 7.24 2.39	, v		17495	4110	789	514		117/CB		. :	:				250		1.447	****
122/SB 1.97 0.056 2.17 7.58 0.22 8.71 0.247 679 275 121/SB 1.34 0.038 1.47 5.71 0.16 6.35 0.180 471 191 121/SB 2.70 0.064 2.50 4.37 0.12 4.81 0.136 800 324 121/SB 2.10 0.059 2.31 2.10 0.06 2.31 0.065 740 299 121/SB 2.10 0.059 2.31 2.10 0.06 2.31 0.065 740 299 123/SB 0.39 0.025 0.37 12.95 0.37 15.01 0.425 119 48 124/SB 0.39 0.025 0.98 12.61 0.36 14.62 0.414 315 127 124/SB 0.39 0.008 0.33 10.44 0.30 11.92 0.338 1.25 119 4.9 182 124/SB 0.70 0.008 0.33 10.44 0.30 11.92 0.338 1.50 124/SB 0.70 0.000 0.77 6.92 0.20 7.82 0.278 6.32 256 124/SB 1.34 0.055 2.02 6.22 0.18 7.03 0.199 649 263 125/SB 2.07 0.059 2.28 2.07 0.06 2.28 0.044 774 293 125/SB 2.07 0.059 2.28 2.07 0.06 2.28 0.044 774 293	, [•	13485	4110	?	c		#2/ccl							ŝ		1 342 WAPPAMEN	ž
121/SB	- 00	-	17865	2775	4380	1225	•	43/661		:					200		1 080 one	Ē
121/SB	0	246 10800/TT	00801	200	1024	9		23/1¢1			:				ì	<u> </u>	214 OE304	
121/SB	٠ ٢	11/00/00 Day	19000	700	1755	2		00/17							1 6	7 (NATO TO	
121/58 2.10 0.039 2.31 2.10 0.06 2.31 0.065 740 299 2.374 2.374 2.374 2.374 2.374 2.374 2.374 2.374 2.374 2.374 2.374 2.374 2.374 2.375 0.34 0.010 0.37 12.95 0.37 15.01 0.425 119 48 124/58 0.39 0.025 0.98 12.61 0.36 14.62 0.414 315 127 124/58 1.28 0.036 1.41 11.72 0.33 13.40 0.380 452 183 118/58 0.30 0.008 0.33 10.44 0.30 11.92 0.338 L.S. 124/58 1.43 0.040 1.57 10.14 0.29 11.41 0.323 449 182 129/58 1.39 0.00 0.077 6.92 0.20 782 0.278 632 2.56 125/58 1.84 0.052 2.02 6.22 0.18 7.03 0.199 649 263 125/58 2.07 0.059 2.28 2.07 0.06 2.28 0.064 774 2.33	₹:	71/00001 /#Z	9881	250	> <	> 6		121/38							3 3	470	623 OFWM	
17.40 0.49 5,866 2,374 2,374 2,374 12,95 0.37 12,95 0.38 1.25 0.38 1.25 0.38 1.25 0.38 1.25 0.38 1.25 0.38 1.35 0.30 0.008 0.33 10.44 0.30 11,92 0.338 1.25 12,978 1.79 0.051 1.97 8.71 0.25 9.82 0.278 632 256 12,978 0.37 6.92 0.37 6.92 0.37 6.92 0.37 6.92 0.37 6.92 0.37 6.92 0.38 1.35 0.39 649 263 12,978 2.31 0.065 2.28 0.064 724 293 12,578 2.07 0.059 2.28 2.07 0.06 2.28 0.064 724 293	=		00861	669	٥	5		121/SB			Ì		- 1	- 1	740	25 26 26 26 26 26 26 26 26 26 26 26 26 26	299 OFWM	
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251 SSZOVL 5520 1682 1255 383 124/SB 1.28 0.036 1.41 11.72 0.33 13.40 0.380 452 183 183 253 9000/R 9000 2743 3480 1061 1061 118/SB 0.30 0.008 0.33 10.44 0.30 11.92 0.338 L.S. 252 9230/L 9230 2813 230 70 124/SB 1.43 0.040 1.57 10.14 0.29 11.41 0.323 449 182 254 9860/L 9860 3005 630 192 129/SB 1.79 0.051 1.97 8.71 0.25 9.82 0.278 6.32 2.41 98 255 10500/L 10500 3200 640 195 124/SB 0.70 0.020 0.77 6.92 0.20 7.82 0.227 241 98 255 11000/R 11000 3353 500 152 126S 125/SB 1.34 0.055 2.02 6.22 0.18 7.03 0.199 649 2.63 257 16135/TR 16135 4918 5135 1.66S 129/SB 2.07 0.059 2.28 2.07 0.06 2.28 0.064 774 2.93	. 14	250 4265/L	4265	1300	3968	1203		124/SB							315	122	1 730	
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254 9860/L 9860 3005 630 192 123/SB 1.79 0.051 1.97 8.71 0.25 9.82 0.278 652 256 255 10500 3200 640 195 125/SB 0.70 0.020 0.77 6.92 0.20 7.82 0.222 241 98 255 10500/K 11000 3353 500 152 125/SB 1.84 0.052 2.02 6.22 0.18 7.03 0.199 649 263 257 16135/TL 16135 4918 5135 1565 125/SB 2.07 0.059 2.28 2.07 0.06 2.28 0.064 724 293 253 16135/TR 16135 4918 0 0 125/SB 2.07 0.059 2.28 2.07 0.06 2.28 0.064 724 293	٠,		9226	3 2	3 5	? ?	: 1	90.471					•		,	70.	1.420 OF WM	
255 10500/L 10500 3200 640 195 124/SB 0.70 0.020 0.77 6.92 0.20 7.82 0.222 241 98 256 11000/R 11000 3353 500 152 125/SB 1.84 0.052 2.02 6.22 0.18 7.03 0.199 649 263 257 16135/TL 16135 4918 5135 1565 129/SB 2.07 0.065 2.54 4.38 0.12 4.98 0.141 813 329 258 16135/TR 16135 4918 0 0 125/SB 2.07 0.059 2.28 2.07 0.06 2.28 0.064 724 2.93	0 1	7/0086 DC7	88	3	3	192		28/82						:	052	2	1,238 WAPDA	
256 11000/R 11000 3353 500 152 125/SB 1.84 0.052 2.02 6.22 0.18 7.03 0.199 649 263 257 16135/TL 16135 4918 5135 1565 125/SB 2.31 0.065 2.24 4.38 0.12 4.98 0.141 813 329 258 16135/TR 16135 4918 0 0 125/SB 2.07 0.059 2.28 2.07 0.06 2.28 0.064 724 293	7	255 10500/L	10500	3500	કુ	195		124/SB							73	88	982 OFWM	
257 16135/TL 16135 4918 5135 1565 129/SB 2.31 0.065 2.54 4.38 0.12 4.98 0.141 813 329 258 16135/TR 16135 4918 0 0 125/SB 2.07 0.059 2.28 2.07 0.06 2.28 0.064 724 293	œ	256 11000/R	11000	3353	Š	152	٠	125/SB							£	263	885 WAPDA	
258 16135/TR 16135 4918 0 0 125/SB 2.07 0.059 2.28 2.07 0.06 2.28 0.064 724 293	٥		16135	4918	5135	1565		129/SB							813	329	622 OFWM	
500	2		16135	4918	0	0		125/SB		į	Ċ	- :			724	203	293 OFWM	
707.7											l	ĺ	١	ı	4 204	1770		

Table B - I (1/3) Breakdown of Authorized and Design Discharge Calculation for LJC Area

Kemarks																			od tasi	
	-																		Proposed tail	
Improved under					¥			W.W.	Ī.	WM						WW	WM		WM	٠.
c	ర్త (శై			1.147	1.017 OFWM	847	628	S41 OF	364	187 OFWIN					822	822 OFWM	656 OF	486	237 OFWM	
1	(tra)		٠	651	171	218	€	17	171	187	1,147		· ·			166	170	543	237	822
Cutiet CCA	(ace)	1.778		319	425	239	215	438	438	462	2,833	1.146			-	411	420	615	586	2,032
ا چ	arge (m3/s)			0.269	0.237	0.197	0.146	0.124	0.083	0.043			•			0.187	0.150	0.10	0.052	
5	Discharge (cused) (m.		·	9.48	8.38	6.96	5.17	4.39	2.93	1.51						9.60	5.30	3.86	1.83	
Section	Discharge usec) (m3/s)				0.21											0.16		-		
ξ	Disc (cusec)			% ∞ ×	7.25	-									5.78	5.78	_			
ırye	Design (cused)			8	1.32	.68	0.67	1.38	1.42	1.51						1.29	1.33	1.91	1.83	
Correct Lossenarge	Authorized (cusec) (m3/s)			970 0 16	1.20 0.034	53 0.043	51. 0.017	25 0.035	29 0.037	1.37 0.039						1.17 0.033	1.21 0.034	74 0.049	1.66 0.047	
	A Cuso			c			Ö		4		»					-1		1		5.
Chack No.				124/KB	126/SB	126/SB	126/SB	130/SB	130/SB	130/SB		. :				133/SB	131/SB	134/SB	135/SB	
Village	٠.										:	•							:	
>	ء ا		र्दे	\$89	976	. 258	166	881	0	0		-		outary)	•	65	1032	1279	35	
Coppos	Distance (feet) (m)		stributa	7745		2835	. •		0	0		:		a Distri		195	3385 1(115	
ļ	(m)		ana Di	yxy						4097				Kiran	:	65		2370	2405	
S	(jæg)		Killa Minor(RD 166450/L,Kirana Distributary)	Abec		•			13440	1			:	Dhabian Minor(RD 183550/R.Kirana Distributary)		195	3580			
Number of	J		D 1664	0	دز ه	,	×	Ę	Ę	Ę		٠		11 Q	 -		æ	æ	_1	
	(onginal) Watercourse		nor(R	744 P	261 4465/L	52 7300/	263 10550/R	264 13440/TI	265 13440/TF	266 13440/TR				Winor.		267 195/L	268 3580/R	12777 69	270 7890/L	
So.	ന്മനം)		illa Mi	Š	រដ	3	4		77	. K				habiar		1 2	2	3	7	

Table B - 1 (23) Breakdown of Authorized and Design Discharge Calculation for LCC Area

Control of the Particulary Control of the	No. No. Watercourse No.	- [- 1	ž,	Section	>	Village	Chak No.		Authorite A	[Section	•	Design	1	1	1	2000	Project	Kemarks
700 238 780 238 1000 1000 100 100 100 100 100 100 100	(Original)	(38)	Ê) (1981)	(a)						13	٦ē	~!	ુ	Š	§ .				, facement)	:
1, 2, 2, 2, 3, 4, 4, 4, 4, 4, 4, 4, 4, 4, 4, 4, 4, 4,	Vest Circle										1	ι	1					l			
March Marc		: :			٠.	.:							:								
885 8027, 735 254 789 258 780 258 780 250 050 050 050 050 050 050 050 050 05	sarang Wala Distrib	utary			:		:					٠.	•	. :			. :		1		
88 95427, 322 98 618 125 355 1010/38 102.03 1.03 66.8 1,05 85.8 2.48 85.8 2.48 15.0 16.6 559 was seen seen seen seen seen seen seen se	1 885 780/L	780	238	780	238			102/18		١			[~.		C1	Š	115	l		ank	
889 95427, 9545 9011 6705 902 1010 102/10 10	2 886 2602/R	2602	793	1822	555			103/JB				, j	-			55	187		5,580		
889 94247, 9945 3331 105 3418 105 104/18 1070 104 105 101 104 104 104 104 104 104 104 104 104	3 887 3225/L	3225	983	623	8			102/18		_			_			00 00	8	_	5,504 ¥ £	sank	
899 1970/L 10970 344 1025 1 10 0 0 100/HB 0.01 01 01 01 01 01 01 01 01 01 01 01 01 0	\$ 888 9945/L	9945	3031	6720	2048			102/JB		_		•	_			ຜ	S S		6,358		-
991 11090/N 11090 3344 1023 312 1010/18 011 010 114 07	5 889 9945/R	9945	3031	0	0			103/1B.								Ċ,	8		5257		
99 (14574), 1751 (1451) 4742 (_	10970	3344	1025	312			102/18						٠.		m	364		6,213		
987 1737.5 1547, 1547, 1549, 1042, 1043, 1		11096	3382	126	200			103/JB					_			ω,	307		900'9		
889 18771/R 1721 5 274 2889 8 222 1100/18 0.55 002 0.55 674 187 712 2121 22 11 256 105 684 187 187 187 187 187 187 187 187 187 187		14515	47.4	3419	10.5		:	100/38					_			5	8		5,942		
885 288924. 28892 658 1395 317 100318 175 058 138 1712 2118 238 55 554 MBah-4-Dry 2009 200934. 2199 658 1395 1189 1189 1189 1189 1189 1189 1189 11		17213	5247	2698	822			110/18	:							N	262	•	5.861 US	Aid	
895 1989/TK 1985		18614	5674	071	427			106/3B								7	238	• •	5,743		
1950/L 21959/L 2199 684 126 377 106/18 6.91 0.01 107 728 200 106 125 17.0 106/18 6.91 0.01 107 108		1885	1665	Š	318			110/18								1	539		5,646 W.	4	
1879 1990 1991 1992 1992 1993 1994 1995		20893	6368	1236	377			106/JB					-		`	œ	321		5,420	,	
889 249776 2457 7558 7558 7559 7559 7559 7559 7559 75	21930/L	21930			٠					_		_	_		``				5,290	3	dhran Minor
889 25497R 24497 7467 2558 770 110/18 0.55 0.02 0.03 0.03 0.03 0.03 0.04 0.03 0.04 <td>• •</td> <td>21939</td> <td>6887</td> <td>1016</td> <td>319</td> <td></td> <td></td> <td>109/JB</td> <td>:</td> <td></td> <td></td> <td>•</td> <td></td> <td></td> <td></td> <td></td> <td>519</td> <td></td> <td>5.290 W.B</td> <td></td> <td></td>	• •	21939	6887	1016	319			109/JB	:			•					519		5.290 W.B		
552 25751/K 25751 7575 4724 1527 100/18 0.93 0.03 1.02 1.02 0.93 0.03 1.02 1.02 0.93 0.03 1.02 1.02 0.93 0.03 1.03 1.94 2.45 1.25 1.75 0.94 1.05 1.97 0.03 1.03 1.94 0.94 1.05 1.97 0.94 1.05 1.97 0.95 1.44 0.95 1.44 0.95 1.44 0.95 1.44 0.95 1.44 0.95 1.44 0.95 1.44 0.95 1.44 0.95 1.44 0.95 1.44 0.95 1.44 0.95 1.44 0.95 1.44 1.05 0.95 1.44 1.05 0.95 1.44 0.95 1.44 1.05 0.95 1.44 1.05 0.95 1.44 1.05 0.95 1.44 0.05 1.05 1.14 1.05 0.95 1.44 0.95 1.44 0.05 1.05 1.05 1.14		24497	7467	2558	780			110/18									8 8		5.080		
543 2589-27L 258-42 358-42 358-42 358-42 358-42 358-42 358-42 358-42 358-42 358-42 358-43 3		28751	8763	4254	1297			110/18									326		5,004 US	Aid	
544 33200L 332200L 33220C		28942	8822	161	28			108/1B				-	_				8		4.872		
545 33894R 33894 10331 674 205 100 JB 309 JB 144 30 JB 350 JB 110 JB 350 JB	6.	33220	10125	4278	8			108/1B.					-				341		4.836		
546 38830L 358830L 35883L	4.	33894	10331	674	205			110/38		-					_		378		4,698		
547 39194/R 39194 11946 3364 1025 115/18 1.45 0.04 1.57 49.26 14.0 58.5 1.659 494 200 548 3905/L 3906R 1306 11946 3364 1025 4126 11573 414 126 1357 11679 414 126 1357 11679 414 126 1357 11679 414 126 1357 11679 4126 11573 4126 11573 414 126 1357 11679 4126 11579 4126 11579 4126 11579 4126 11579 4126 11579 4126 11579 4126 11579 4126 11579 4127 11579	6.7	35830	10921	9161	88			108/JB					_				233		4,545		
S48 9050KL 3360K1 12073 414 126 108JB 196 0.06 216 47.83 1.35 55.71 1602 690 279 549 4126/LL 4126/LL 4126/LL 4126/LL 4126/LL 4126 126 160 133 45.81 1.30 54.36 1.40 102 44 554 4126/LL 4126/LL 4126 1226 12 116/HB 103 4581 1.30 53.84 1.52 44 554 4126/LL 4126/LL 1226 12 116/HB 103 10.34 45.81 1.37 53.84 1.26 14 15 535 4250/RL 42250 1.20 12.0 24 116/HB 100 102 44.31 1.24 55.84 12 44.31 16 55.84 12 44.31 16 55.84 12 44.31 16 57.84 12 44.31 16 57.84 12 44.37 56 22 56 22 57.84 57.84 57.84 57.84 57.84 57.84 57.84 57.84 57.84 57.84 57.84 57.84	٠.	39194	11946	3364	1025			115/38					_				464		4,451		
5569 412366L. 412366 12587. 1658 499 107/18 0.29 0.01 0.32 458 1739 54.45 1540 107 41236 45246. 1540 16718 0.29 0.01 0.32 45.81 129 45.81		39608	12073	4.4	126			108/18		-							8		4,251		
550 41296/L 41296 12587 50 15 116/18 1.26 0.04 1.39 4558 125 53.84 1525 1.42 179 551 47707 41270 12716 424 129 116/18 1.27 0.00 1.29 447 125 52.42 176 371 179 552 42510R 42510 12977 790 241 116/18 1.17 0.05 1.29 447 1.25 52.42 176 371 179 552 42510R 42550 12962 2.0 70 116/18 1.17 0.05 1.29 447 1.25 52.22 184 555 42556L 42550 12962 2.0 70 1116/18 1.00 0.0 1.11 4608 1.36 371 1.45 562 229 555 46964R 46964 14315 1014 309 119/18 1.00 0.0 1.0 4.0 1.13 381 1.25 3.5 1.9 555 46964R 46964 14315 1014 309 119/18 1.0 0.0 1.0 3.0 1.1 4.0 1.1 4.0 1.1 4.0 1.1 4.0 1.1 4.0 1.1 4.0 1.1	22 S49 41246/L	41246	12572	1638	664			107/JB					_		-		52		3,972		
551 41720/L 41720 12716 424 129 1167B 0.25 0.01 0.28 44.32 1.25 1.448 71.1 1.50 1.50 1.25 0.25 0.01 1.25 2.45 1.44 371 1.50 553 42350/L 42510 12957 790 241 1167B 1.70 0.03 1.20 4.07 1.25 2.40 1.25 2.25 1.84 371 1.50 524 4.835 1.40 1.31 4.61 1.37 566 225 1.50 4.00 1.25 4.20 1.25 4.24 1.37 566 225 525 4.62 1.34 4.61 1.34 4.64 1.34 3.64 1.34 3.74 1.35 3.65 1.35 3.00 1.31 4.61 1.34 3.74 1.35 3.00 1.30 3.74 1.34 3.64 3.74 1.34 3.64 3.74 1.34 3.64 3.74 1.34 3.74 3.74 3.74 3.7	23 550 41296/L	41296	12587	လွ	<u>~</u>			116/18									42		3,930		
552 42510R 42510 12957 790 241 115/1B 1.17 0.03 129 4407 125 52.12 1475 571 150 552 42510R 42510 1295 16 5 116/1B 1.17 0.05 120 4407 125 52.12 1475 566 229 555 42520R 42526 12962 1.16 5 116/1B 1.00 0.03 1.00 41.01 1.14 47.41 1.43 366 229 555 45950R 45950 14006 1115 340 119/1B 1.00 0.03 1.00 4.113 1.16 4.741 1.343 385 156 555 45950R 45950 14006 1115 340 119/1B 1.00 0.03 1.00 4.01 1.27 2.0 555 45950R 550 570 4.01 1.17 4.00 1.03 3.0 1.05 3.7 1.35 3.7 1.35 555 45050R 550 570 4.01 1.10 4.11 4.01 1.27 1.2 550 5505R <t< td=""><td>24. SSI 41720/L</td><td>41720</td><td>12716</td><td>424</td><td>23</td><td></td><td></td><td>116/38</td><td></td><td></td><td>-</td><td>•</td><td></td><td></td><td>_</td><td></td><td>Ä.</td><td></td><td>3,752</td><td></td><td></td></t<>	24. SSI 41720/L	41720	12716	424	23			116/38			-	•			_		Ä.		3,752		
553 42304L 42250 12962 16 48 116/18 177 0.05 155 429 0.121 50.73 1.447 566 229 554 4235L 4235L 4235L 136 136 136 138 435 138 435 138 36 435 138 138	25 552 42510/R	42510	12957	790	241			115/JB				•	_			:	371	8	3,752		
555 448357L 4509 1115 340 116/18 100 0.03 110 41.13 116 47.41 13.43 385 156 555 4699GAR 45990L 1400 1115 340 119/18 10.9 0.03 11.0 47.41 13.43 385 136 555 4699CAR 45990L 1315 104 309 1177 11.0 47.41 13.42 136 37 136 37 136 37 136 37 136 37 136 37 136 37 136 37 136 37 136 37 136 37 136 37 136 37 136 37 136 38 117 38 36 38 136 117 38 36 38 136 <td< td=""><td>26 553 42526/L</td><td>42526</td><td>12962</td><td>91</td><td>S</td><td></td><td></td><td>116/18</td><td>٠</td><td></td><td></td><td></td><td></td><td></td><td>7</td><td>_</td><td>88</td><td>228</td><td>3,601</td><td></td><td></td></td<>	26 553 42526/L	42526	12962	91	S			116/18	٠						7	_	88	228	3,601		
555 45950R 45950 14006 1115 340 119/18 1.09 0.03 1.20 40.13 1.14 47.41 1.343 385 156 556 45950R 45950R 45950R 119/18 1.09 0.03 1.20 40.13 1.14 47.41 1.343 385 156 556 45950R 4596G 14315 1014 309 117/18 5.00 1.01 385 1.30 44.91 1.272 1.27 1.55 245 255 255 255 250 1.10 385 1.30 337 1.35 337 1.35 1.35 337 1.35 337 1.35 1.35 337 1.35	27 554 44835/L	44835	3666	2309	ğ			116/18					-	-			4 <u>5</u> 4	3	3,372		
556 46964R 46964 14315 1014 309 119/18 0.96 0.03 1,06 39.04 1,11 46.08 1,305 337 136 557 50500L 5375 5050L 673 117/18 1,85 0.05 1,08 44.91 1,272 L.S. 558 52050L 5570 61655 2206 677 117/18 1,85 0.05 1,08 44.91 1,272 L.S. 558 52050L 5590 61055 10 117/18 1,18 0.04 34.28 0.98 1,69 117 560 54905L 54905 1670 117/18 1,15 0.05 1,27 31.57 0.89 36.98 1,17 560 54005L 1707 1099 335 117/18 1,15 0.05 1,27 31.57 0.89 36.98 1,07 1,17 561 56005R 56201 1998 335 117/18 1,15 0.05 1,26 36.42 0.86 35.53 1,17 1,17 1	28 555.45950/R	45950	14006	115	340			119/18					~	_	_	_	385	•	3,189		
557 20000L 50500 15392 3536 1073 117/18 3.50 0.10 3.85 3.80 1.00 44.91 1.272 L.S. 558 20000L 52706 16065 2206 672 117/18 1.85 0.05 2.04 34.58 0.98 40.66 1.152 605 2.45 558 52006L 54906 16735 219 117/18 1.15 0.03 1.27 31.27 0.98 40.66 1.152 605 2.55 560 54906L 54906 16735 119/18 1.15 0.03 1.27 31.27 0.89 342 1.75 561 56005R 56005 17070 1999 335 119/18 1.15 0.03 1.27 27.34 0.77 31.52 200 177 562 56210R 56200 1908 189 58 119/18 1.15 0.04 1.53 28.73 0.83 4.32 1.75 562 5630R 5640R 5650 100 58 58 <td>29 556 46964/R</td> <td>46964</td> <td>14315</td> <td>1014</td> <td>8</td> <td></td> <td></td> <td>119/18</td> <td></td> <td></td> <td></td> <td>•</td> <td></td> <td>•</td> <td></td> <td></td> <td>337</td> <td>•</td> <td>3,033</td> <td></td> <td></td>	29 556 46964/R	46964	14315	1014	8			119/18				•		•			337	•	3,033		
558 52706/L 52706 16665 220 672 117/18 1.85 0.05 2.04 34.58 0.98 40.66 1.152 0.05 2.45 0.05		20200	15392	3536	1078		٠.	17/0B									S.		2.896		
559 54905/K 55900 10735 2199 670 119JJB 1.16 0.03 1.28 32.73 0.93 38.39 1.087 392 159 560 54906/L 560 54906/L 560 54906/L 100 100 100 1.00 1.00 1.00 1.00 1.00 1.	31 558 52706/L	52706	16065	220	672			117/18			•		-	-	_		\$65		2,896		
S65 55900KL 54500 104.50 1 11/10 1 1 11/10 1 1 1 1	X/CO650 650 75	683	167.55	2.5	0/9			36/61					-				395		2,652		
562 62421, 62421 19026 6416 1966 117718 1.09 0.00 1.60 2042 0.80 35.03 1.00 375 4.20 1.75 56.2 62421, 62421 19026 6416 1966 117718 1.09 0.00 1.60 20.40 1.53 28.73 0.81 35.66 0.953 4.32 1.75 56.2 62421, 62501 19024 189 58 119718 1.15 0.03 1.28 24.69 0.70 28.40 0.804 189 76 56.5 65.940, 62601 19024 1.50 1.00 1.20 1.20 1.20 1.20 1.20 1.20 1.2		0000	2.00	- 2 €	2000			90//11				•					3 3	•	7,47		
564 GASSIAR 625401 FORM STATE STA	7/C0000 100 47	2000	2/2/2	X Y	2			00/6/1									Ċ.	•	0/07		
564 64539/R 64639 19702 109 19702 109 19702 109 19702 100 19702 100 19702 100 19702 100 19702 100 19702 100 19702 100 19702 100 19702 100 19702 100 1970 1970 1970 1970 1970 1970 1970	25 202-0242012 26 626-024000	12420	07061	2 5	8			11//18									754	•	555		
565 65940/R 65940 20099 1301 397 11991B 1150 0.03 1.28 24.69 0.70 28.40 0.804 189 76 556 65940/R 65950/R 65950		64620	10701	000	8 3	7. 7. 12.	·	97.61									င် နောင်		200		
566 67950/K 67950 27011 2010 613 1200/B 0.50 0.11 0.55 25.55 0.57 25.50 0.75	3/ 30* O*	64040 64040	3000	1301	207). (non'	110/12	•			• `					. o		10,0		
567 68872/R 68872/R 68872/R 68872/R 68872/R 68872/R 68872/R 69872 2092 231 120/B 0.34 0.03 1.03 23.03 6.65 26.2 0.745 259 105 568 69147/R 69147 21076 275 84 121/7B 0.57 0.02 0.63 22.09 0.63 25.9 0.713 183 74 183 74 183 74 183 74 183 74 183 74 183 1	} }	0.5959	2021	2010	7 7			12003					_						100		
69147/R 69147 21076 275 84 121/18 0,57 002 0.63 22.99 0.63 25.18 0.713 183 74 70850/L 70850/L 70850 1595 170 0.05 1.87 21.52 0.61 24.53 0.695 516 209 71706/R 71706 21856 856 261 120/18 0.87 0.02 0.96 19.82 0.56 22.53 0.638 299 121 1 73526/L 73526 22411 1820 555 121/18 1.09 0.03 1.20 18.95 0.54 21.50 0.669 317 128 1 75036/R 75036 22871 1510 460 120/18 1.72 0.05 1.39 17.86 0.51 20,17 0.571 79 32 1	\$	68872	20002	922	25			120/18					_				200	501	707		
70850L 70850 21595 1703 519 121/18 1.70 0.05 1.87 21.52 0.61 24.53 0.695 516 209 17106/R 71706 21856 856 261 120/18 0.87 0.02 0.96 19.82 0.56 22.53 0.638 299 121 17505/L 73526 22411 1820 555 120/18 1.09 0.03 1.20 18.95 0.54 21.50 0.609 317 128 175036/R 75036 22871 1510 460 120/18 172 0.05 1.89 17.86 0.51 20.17 0.571 79 32 1		69147	21076	275	ž			121/78			_	•	_) S	34	6		
71706/R 71706 21836 856 261 120/JB 0.87 0.02 0.96 19.82 0.56 22.53 0.638 299 121 17506/L 73526 22411 1820 555 120/JB 1.09 0.03 1.20 18.95 0.54 21.50 0.609 317 128 175036/R 75036 22871 1510 460 120/JB 1.72 0.05 1.89 17.86 0.51 20.17 0.571 79 32 1		70850	21595	1703	519			121/18				•	_				5.5	8	528		
73526/L 73526 22411 1820 555 121/18 1.09 0.03 1.20 18.95 0.54 21.50 0.609 317 128 1 75036/R 75036 22871 1510 460 120/18 1.72 0.05 1.89 17.86 0.51 20,17 0.571 79 32 1		71706	21856	886	261			120/18				٠.	_				28.	25	310		
75036/R 75036 22871 1510 460 120/18 1.72 0.05 1.89 17.86 0.51 20,17 0.571 79 32 1	44 571 73526/L	73526	22411	1820	555			121/18					_				317	128	861		
	45 572 75036/R	75036	22871	1510	8			120/38									5	E	1.070		

Table B - 1 (2/3) Breakdown of Authorized and Design Discharge Calculation for LCC Area

Remarks																					Saduana Minor(4.75)																							Khilliana Minor(10.65)			
Project	(Improvement)														US. Aud		US. Aid	US. Aid	JS. Aid	JS, Aid							W Bank			JS, Aid	•		W Bank	M.P.A.		W Bank	W Bank	W Bnnk	M.P.A.+W Bank				W Bank		M.P.A.+W Bank		
Section	CCA	(ha)	1,038	881	753	\$;	§ %	3 8	207	 				34.677	34,677	34,472	34,319 (34,162,1	33,956 1	33,861	33,679	32,958	32,635	32,382	32,145	32,035	51,839	31.05.3	Q.;	31.243	31,028	20.00	30.4% W Bank	30,209 M.P.A	30,115	29,924 w Bank	29,847 W Banl	29,650 W Bnnk	29,265	29,374	29.188		28,871	28.24	27,251 M.P.	26.883	-
			17	28 2	87		CCC	187	127	50		:			۱.	153						324											747	Z	161	77				186	174	144	327	1,293	19 8	9 6	; ì
Outlet	(acre) (ha)		B.S.	317	215	S S S	S (462	313	861	9	6,626			308	378	388	507	236	450	1,780	8	623	286	270	2	2	438	3 5	3	1 %	\$ \	919	232	472	81	487	210	472	459	429	355	8	3.198	397	758))
c	ě	(m3s)	0.515	0.501	0.437	0,414	0.357	0.245	0.20	0.176	27.7				8.873	8.817	8.762	8.718	8.662	8,615	8.551	8.414	8.333	8.270	8.194	8.147	8.05	8.045	\$ 5 \$ 5 \$ 5	55.5	/00/	170.7	7.724	7.645	7.621	7.580	7.563	7,519	7.480	7.437	7.386	7.334	7.289	7.217	6.915	6.845	5
Design	Discharge	(cosec)	18.17	16.48	15.42	14.62	258	8.66	7.22	6.23	OC.C				313,30	311.35	309.38	307.84	305.87	38.21	301.96	297.11	294.25	292.02	289.35	287.66	285.80	284.08	282.62	280.13	61.77	70077	27.77	269.95	269.12	267.64	267.04	265.52	264.14	262.59	260.80	258.97	257.39	\$ 5 5 5 5 7 7	244.18	239.68	
۶	rge	(m3s)	0.46	0 0 0 0 0 0	0.39	0.37	25.0	220	0.19	0.16	. I	1		7.02	7.02	86.9	6.95	6.92	6.88	98.9	6.82	6.71	8.0	6.59	6.55	6.52	6.49	\$ \$	9.4	6.35	() (9 4	31.	6.12	6.10	6.0 8.00	6.05	6.01	86.	5.95	5.92	5.88	5.85	5.79	5.53	0, 4, 0, 4,	;
Nection	Discharge	(cosec)	16.14	15.83	13,83	13.11	6	, 6 , 6 , 6 , 6	6.56	5.66	3			247.90	247.90	246.46	245.41	244.31	242.87	242.20	240.92	236.85	234.58	232.80	231.12	230.10	228.72	227.34	226.09	224.21	71.777	86.95	217.00	216.06	215.40	214.08	213.52	212.14	211.57	210.23	208.93	207.63	206.62	204.33	195.24	192.63	1
9.6	Design	(casec)	0.34	687	0.79	1.98	3.5	3 4	8	0.73	Ž.				1.58	1 16	1.21	1.58	0.74	4.	4.75	2.50	1.96	1.85	1.12	1.52	1.52	.38	2.07	2.30		36	38	0.73	1.47	0.59	1.52	0.63	1 47	1.43	1.43	1.1	2.52	10.65	1.24	2.32	ł .
Outlet Dicharse	pax.	(m3s)	0.01	0.03	0.02	0.05	3 S			0.02					300	0.03	0.03	8	0.05	9.	0.12	9.0	0.05	0.05	0.03	8	o S	9	0.05	8	3 8	33	3 6	000	800	0.05	8	0.02	8	8	900	0.03	8	0.26	0.03	\$ 8 5 6	;
Ö	Authorized	(casec)	0.31	2.0	0.72	1.80	왕 <u>3</u>	<u> </u>	8	88	3.00	70.21		1	4	1.05	1.10	4	0.67	1.28	4.07	2.27	1.78	7.68	1.82	1.38	1.38	3	1.88	503	1.26	8	11.	9	1.34	45.0	38	0.57	7,	1.30	130	1.01	2.29	8	<u> </u>	8 4 . 5	i
	•							•		:												:												:							- 1						
Sag.	*.		20/18	22/JB	122/JB	122/18	07/20	23/38	124/JB	123/18					16/18	49/1B	16/JB	#6/JB	50/JB	17/JE	1 : 1 7. 2 :	47/JE		50/JB	50/JB	SO/3B	53/JB	S1//1B	51/38	51/JB.	53/18	9770	GIVES	9		51/JB	S2/JE	54/JP	52/JE		:	52/JB	57/1B		58/JB	S7/JB	
											-							 				•		•			•	•									÷.									-	
Village							58 P.M.College	٠			Α.	•					:																													435 920 Agri Maiy	
		5	3	, j	48	213	85 8 57	. O	0	_	0 F.D				337	736	ž	345	847	783	87	336	257	111	% 4	328	189	တ္တ	67	4	20 C	9 5	717	§ <u>S</u>	0	7	4	747	27	356	8	477	ွှ	<u>:</u>	1267	435 25 26	2
Section	Distance	(teet) (m)	1973	<u>ئ</u> م			S 8	600	0	0.0	0	:		4 4	105	2414	666	1132	780	6957	283	8	8 75	550	752	077	620	25	335		g;	132	0 0	, o	0	35	14	155	242	. 8911	313	. 56.	8	r Lari		1428 3084	13
	(w)	J)		3818			24137		810	25018	×10	:			337				_					•							5 5 5 5 7				9,00			•		8833		9710	740			1456 J	
Ga			[4]	77016 23 28144 23				82079 25 25 25			\$7.67.078				501	_		5650		_		~~				_	_		20828		. i		0 36636							28979 8		:				37586 11 40670 17	•
Ş	(3		77	<u>r</u> ×	200	79								۶.	Ī	10%	4	*	·	2	11	27	53	S.	17	18	61	6	ឧ	ឧ	5 5	គី (3 6	; X	1 53	X	13	53	73	8	ጽ	31	31	8	æ 8	F. 4	ř.
Watercourse			S73 77009/R	574 77016/L 575 78144/L	576 78300/L	77 79000/R	578 791907L	580 82079/TR-1	581 82079/TR-3		78.4 8.20/9/11-2	-		Nasrana Distributary	275 1105/1.		277.4518/L				11284/R	1281 12388/L	_		7					•		•	201 21392/K		• • •	• • •			297 27811/L		30292/R		300 31956/R		301 36158/L	302 37586/R 303 40670/I	
37	3			7 4 7 4		_				\$;	Nasran			:I E	: <u>-</u> 1	S	9		7 L		∷ ∞	6	01		ဌ	91	<u></u>	.: :S	<u>.</u>	. 2	2 <u>2</u>	:		23	-	_			ਸ ਸ			'	## F	-

Table B • 1 (23) Breakdown of Authorized and Design Discharge Calculation for LCC Area

Pamarka	***************************************																:	Narwala Mibor(17,1)																Satiana Minor(8,23)											Natheri Minor(15.4)	
Section Property		(ha)		26,342 W Bank 26,200	25.870	25.768 M.P.A	25,536	25,481 W Bank	22,22 25,112 M P 4	24.959	24,959 M.P.A.+W Bank	24,673	24.24 3	24.363 W Bank	24,099 M.P.A	23,983	23,049 W Bank	23,441	21 676	20.831	20,400	20,190 W Bank	20,029 M.P.A.+W Bank	19,814 W Bank	19,621	19,439 W Bank	9,733	8.763	18,542 W Bank		18,021 W Bank	17,795 US Aid	17,621		6.230 US Aid	16,037	16,031	16,031	15,833	15,648 US Aid	15,492	15,278 US Aid	15,045	14.823 US AND	14,460	
Outlet CCA	a		577 234	352 142	252	573 232 3			377 153		708 287	321 130	445 180	651 263	286 116	_	8 8 8		342	431	210	8	215	<u>8</u>	.	200			. ~	321	22	77		282	88	•		198	<u>≋</u>	35	214	333	777	3 3	1.800 1.800	
Detion		c) (m3s)	46 6.697	41 6.638	99 6.485	_		. .	38 0.332 18 6.292			40 6.157	•					26/30					_		-	787.4				23 4.481	·								. ,	91 3.821		_			33 3507	
Section	y.	(m34) (cur	190.52 5.40 236	88.93 5.35 234	185.09 5.24 228.9	\$ 5.21	5.17	07.7	179.51 5.08 222 18	505	30.0	00.1	4.95		25.50	4	3.5	100.50 4.75 £0#.02 150.40 4.30 187.35	4.27	49.09 4.22 183	4.14	4.10	8	4.02	3.08	39.30 3.94 169.	3.82	88	3.76	3.72	366	3.61	200	17.85 3.34 141	3.30	3.26	3.26	3.26	3.22	3.18	3.15	1700	108.15 3.06 129.	70.57 5.04 127. 36.41 5.00 156	4.03 2.95 123.83	
er Disharge	od Dengh	(cosec) (50:1	20.05	8:	1.85	0.42	3.6	ند ر	0.55	5 2.21	0.04 1.38 1.	04.	25.5	S ((22)	ē \$	5.5	6	3,32	1.62	1.24	8	8	1.43	3.65	54	12	1.55	2.48	1.7	7	4.0	4	55	8	80	15.	1.43	1.20	69	S F	7):1		0.38 15.40 10	
Onc	Authorize	(casec)	1.59	28.6	96.0	1.68	0.38	1.73	0.03	9	2.01	1.25	127	1.85	0.81	2,34		1 50		3,02	1.47	1.13	1.51	136	1.30	23.5	200															8.7		1.10	13.29	
Chak No.			58/18	57/JB 50/JB	59/18	58/1B	59/1B	39/JB	61/1B		80/JB	217/218/RB	61/JB	60/IB	61/18	61/38	6778	62/TR	64/18	37//18	63/18	64/1B	64/JB	63/JB	68/JB	86/69	87/69	70/JB	87/69	70/JB	71/18	74/JB	9717	73/IB	74/JB			73/JB	73/JB	80/4/	76/38	76/18	27/77 27/77	41.VL		
Village										Rest House											:										-					Police St.	Buti R.H.				٠					
Nection	Distance	(feet) (m)	325	320 268	8	159 48	0	442 135	800 244	2	8	1098 335		_		22.50 05.22	2502	055 195		2297 700		-				4089	040			•	: . :		13:50 407	_		218	22		773 236			780 657	2414 736		819 250	
CX CX	(feet) (m)	0	12721	45001 15290				46582 14198		15038	•	16035	0400	200	7,422	\$ 60		5 19832	05661	20650	1 -	22018	22341		24013	\$1872 24955 \$2706 26280	263.15	26534	26663	88229 26892		27274	33500 0000	28903	28964	29182	29264			7,000	4.55	•	3001		32552	
Watercourse No.	1			45930/R 45				40384/K 46									023007K									818/2/K 81							900104K 90									10.094/L 10.0566				
No. No.	(buginal)		30 1304 4	30,5	1307		8	2 5	1312	1313	1314	1315	1316		1318 7		0 0751 O+	47 [32] 6		1323	1324	-	٠,	327	3.5	8 6751 CS	331	1332	1333	334	338	62 1336 89		58 538 9	1339	35	<u> </u>	•	7.	1 to 1	1	3	73 1347 10	25		

Table B - I (2/3) Breakdown of Authorized and Design Discharge Calculation for LCC Area

Remarks														Domra Minor(21.36)																														
Section Project	9		2,660 W Bank	12,433	1.950	1,811 W Bank	1,632 W Bank	11.425 W Bank	11,118	789.	10,384 W Sank	0,155 0,015 w Bank+110 A.Z	9,693	2,464	6,848 W Bank	5.544	6,280	COSE WESTER	5,740 US AIG	5.415	5,275	5,200	_	5,061 US Aid	, (o)	4,380	4,360 W Bank	4,353	2100 w bank	2/98	.667 W Bank	199	.452 W Bank	5,297 W Bank	2,132 m same	734 W Bank	411 W Bank	2,273 W Bank	1,081	.983 W Bank	726 W Rank	.542 W Bank	477 W Bank	
l	L		227 12	727	130	_	207					-		•	300	-) \ \ \ \ \ \ \ \	_			•	• • •	•		•	252	1 (*	1 (*)	•	215 3	m (2 2	•	<u> </u>	38
C triping	(acre) (ha)		262	<u> </u>	3 5	3	512	759	1.076	737	33	1 5			_	653	8	88	3 3	3	88	Š.	343	577	200	8	∞	623	3 5	LS.	ST	531	<u>%</u>	\$ £	2 4 2 4	8	7	474	25.	ģ.	505	3	\$	\$
	•	ا چ	3.066	3.016	868 808 808	2.868	2.812	2.766	2.692	28	272	2 4 6 2 4 6 3 6 4 6	2,347	2.293	1.688	1.620	1.554	3 3	307	1338	308	1.281 B	1.276	1.232	707.7	1,070	1.056	1.050	0 o c	0.910	0.893	0.887	0.839	0.80	2.5	0.663	0.585	0.551	0.503	0.476	0.419	0.356	0.338	0.302
Parison C	Discharge	(cusec)	108.27	8 8 8 8 8 8	5.50	101.28	85.28	97.65	95.05	91.68	86.6	8/ TX	82.89	80.98	59.59	57.21	8.8 8.8	3 3 3	20.10	4, C4	46.17	45.24	45.06	43.51	17:14	37.78	37.28	37.8	20.02	32.12	31.55	31.32	25.62	28.5	7 2	23.41	20.65	19.46	17.75	16.79	14.81	12.56	11.92	10.65
Section	Discharge	(cusec) (m3s)	-	89.13 2.52	85.75 2.43	84.77 2.40	`.	81.98 2.32			۱,	75.05 2.07	69.79 1.98	:_	_	٠		77.	45.2/	•		_		36.66 1.04	24.74	٠		31.61 0.90	29.53 0.84	27.21 0.77	٠	26.83 0.76	<u>.</u>	24.23. 0.69.			17.48 0.50		~	14.43 0.41	12.79 0.36			-4
	See See	1	1.77	75	<u> </u>	47	8	3.5	3.37	2.34	6	8 7	7	21.36	2.38	5.08	69. 69.	 	2.18	2 2	0.61	0.19	1.07	2,11	3 5	5.15	90:0	1.96) (c	0.28	9.14	8	2	7 8	2 5	2.65	1.07	1.53	0.76	8 6) (C) (C)	0.50	1.27	0.29
Outlet Dishama	Authorized	اچ		÷	000 860		1.45 0.04					500 65	1.61 0.05	_	2.16 0.06				86.7	٠				1.92 0.05		0.14 0.00	~	1.78 0.05	20.0 27.0	· •		_	٥.	1.13 0.03	100	2.41 0.07	_	•	_		1 43 0.04		1.15 0.03	
3	ا	~		1								j.	·	:					: :				:								17		: .						:	:				
2	3		\$0/JB	80/18	8/18	81/18	80/JB	81/1B	82/JB	82/JB	84/JB	83/18	83/1B		89/18	89/1B	83/JB	900	91/18 01/18	77.7	91/IB	2	90/JB	91/JB	200	97/78 90/18	93/JB	91/JB	97718		93/IB		92/18	94/18	30/96	96/JB	95/1B	96/18	95/1B	97/JB	95/18	95/JB	97/JB	95/JB
Vellege	ASSETT								,																						:					:				•				
	- 3	Ê	4	# {	2 t	116	es S	249	ረሳ -	2 :	0 5	3 3 3 3	388	X	v	266	478	88	<u> </u>	> .	856)	1308	513		g S S	476	4	202	000	8	21	=======================================	7	ç, v	423	483	262	803	84S	8 8	£ 1.50		1428
20000	Distance	(Ject)	13	9	725	8	175	817	77	1453	<u>7</u>	<u>8</u> 5	625		77	1858	1569	3807	25	>	2800	`	4285	1682	3	3302	1562	150	806	3211	952	167	9	0110) (S)	1300	1585	2622	2963	2773	050	25.45 84.75	8	4685
4	Ē	•	32556	32590	.,	34168	•	٠.	•		• • •		37018		٠,	` '	£1.		39353		40209		41515		•	2,002 2,002 4,002 4,002	•	•	44422							4713			- T.		50399			
	٤		106812	106922	5555	11218	112275	113092	113103	114556	1598	117864	121450	121531	121552	123410	124979	128786	129111	12001	131920	133900	136205	137887	016/51	143154	144718	144868	145/3/	148048	149900	: 50067	150103	150213	20120	54557	156142	158764	161727	164500	165350	7,587	16891	173599
	- 43			1350 106922A	1351 1083/5/R		_		1356 113103/R		1358 115900L		1361 121450/R		-	-		· ·	1366 129111/L		1360 131920L	•	1370 136205/R				1375 144718/L			1489487	1378 149900/L			,		1383 1545577			-			1200 16878/8		1392 173599/L
		į	ξ,	ا ۲	F 2	<u>ځ</u>	8	50	22	Ş	3 :	3 3	£ \$;	80 80	8	8	5 5	2, 2	*	ŏ	?	8	58	3 2 8	\$ 8	<u>5</u>	20.5	Š		ğ		20	8	6	3 2	9	Ξ	21	**	<u> </u>	3 5	1.	<u>**</u>

Table B - 1 (2/3) Breakdown of Authorized and Design Discharge Calculation for LCC Area

95/18	93/18	Watercourse No. (feet)	RD (m)	N D	Section Distance	Village	Chak No		Outlet Disharge Authorized D	Design	Section Discharge	Design Discharg	ign arze	Outlet CCA (acre) (h	٦	Section Project CCA (Improvement)	Kemarks
99018 0947 002 1039 888 025 1014 0.287 233 102 99018 094018 0940 003 103 103 103 103 103 103 103 103 10	9978			(feet))			(cox		1		(casec)	(m3s)			. [. '
99/18	99/18 197 0.05 217 7.22 0.21 8.11 0.250 666 278 99/18 2.54 0.07 2.90 2.64 0.07 2.90 0.052 951 377 255 915 915 385 94.07 2.00 2.04 0.07 2.90 0.052 951 377 255 915 915 915 915 375 915 915 915 915 915 915 915 915 915 91	205621	303				95/JB	00		0.79	•	10.14	0.287	253 378	<u> </u>	1,275 W Bank 1 172 W Bank	
99/18	99/18		1 5		-		98/18	<u>-</u> ز		2.17		8.11	0.230	989	278	1,039 W Bank	
99/18 24739 702 240 124 0.01 2.04 0.02 25.04 0.07 2.07 2.07 2.04 0.01 2.04 0.02 2.04 0.07 2.04 0.01 2.04 0.01 2.04 0.01 2.04 0.01 2.04 0.01 2.04 0.01 2.04 0.01 2.04 0.01 2.04 0.01 2.04 0.01 2.05 0.01 2.05 0.01 2.05 0.01 2.05 0.01 2.05 0.02 2.05 0.02 2.05 0.02 2.05 0.03 2.05 0	997B 247.99 7.02 2.64 0.07 2.70 0.024 2.65 34.577 (1.15) 2.64 0.07 2.70 0.024 2.65 34.577 (1.15) 2.65 0.07 2.86 0.031 2.85 2.65 34.577 (1.15) 2.65 0.07 1.10 0.031 2.65 34.577 (1.15) 2.65 0.07 1.10 0.031 2.65 34.577 (1.15) 2.65 0.07 1.10 0.031 2.65 34.577 (1.15) 2.65 0.07 1.10 0.031 2.65 3.65 34.577 (1.15) 2.65 0.07 1.10 0.031 2.65 3.65 34.577 (1.15) 2.65 0.07 1.10 0.031 2.65 3.65 3.65 3.65 3.65 3.65 3.65 3.65 3		\$63				98/JB	ત		2.98	-	5.89	0.167	951	385	762 W Bank	
\$\begin{array}{c} \text{3.675} \\ \text{5.675} \\ \text{5.677} \\ \text{5.6778} \\ \text{5.67798} \\ \text{5.6778} \\ \text	97) 534675 (407) 0.12 54078 1.09 0.03 1.10 1.00 0.03 1.10 1.00 0.03 1.10 1.00 0.03 1.10 1.00 0.03 1.10 1.00 0.03 1.10 0.03 1.10 1.00 0.03 1.10	128/1	Š				99/JB	247	- 1	3.	١.	X:7	7000	85.686	34,677	S// W Bank	
4.07 012 55/18 1,49 0.04 1,54 4.07 012 4,75 0135 659 257 55/18 1,49 0.04 1,54 2.80 0.07 2.86 0.081 552 228 55/18 1,40 0.04 1,74 2.80 0.07 1,10 0.031 563 228 55/18 1,58 0.04 1,74 9.09 0.26 10.06 0.302 5/8 228 55/18 1,70 0.05 1,77 7,10 0.20 0.03 1,20 0.	\$\begin{array}{c} \text{5.67} & \text{4.07} & 0.12 & 4.75 & 0.135 & 6.59 & 267 & 287													34.675			
55/18 1.59 0.04 1.64 4.07 0.12 4.73 0.135 5.8 226 57/18 1.00 0.03 1.10 1.00 0.03 1.10 0.031 5.8 226 57/18 1.00 0.03 1.10 1.00 0.03 1.10 0.031 5.8 226 57/18 1.00 0.03 1.10 1.00 0.03 1.10 0.031 5.8 228 55/18 1.00 0.03 1.10 1.00 0.03 1.10 0.031 5.8 228 55/18 1.00 0.03 1.76 7.51 0.21 8.4 0.240 5.6 228 55/18 2.19 0.06 2.21 2.00 0.06 2.22 0.005 0.131 770 214 55/18 2.00 0.06 2.22 2.00 0.06 2.22 0.005 0.131 770 214 55/18 2.00 0.06 2.22 2.00 0.06 2.22 0.005 0.131 770 214 65/18 1.22 0.03 1.24 14.57 0.41 17.10 0.444 4.28 173 65/18 1.12 0.05 1.24 14.57 0.41 17.10 0.444 4.28 173 65/18 1.12 0.05 1.23 9.19 0.26 10.33 0.29 6.6 2.61 65/18 1.12 0.05 1.23 9.19 0.26 10.33 0.29 6.7 2.46 65/18 1.13 0.05 1.20 1.21 8.05 0.24 1.26 0.33 1.25 65/18 1.13 0.05 1.20 1.20 0.05 2.09 0.056 6.7 2.46 67/18 1.13 0.05 1.20 1.20 0.05 2.09 0.056 6.7 2.46 67/18 1.14 0.05 2.09 1.20 0.05 2.09 0.056 6.7 2.46 67/18 1.15 0.05 1.20 1.20 0.05 2.09 0.056 6.7 2.46 67/18 1.15 0.05 1.20 1.20 0.05 2.09 0.056 6.7 2.46 67/18 1.15 0.05 1.20 1.20 0.05 2.09 0.056 6.7 2.46 67/18 1.15 0.05 1.20 0.09 7.10 0.20 2.09 0.056 6.7 2.46 72/18 1.16 0.03 1.20 0.09 7.10 0.20 2.09 0.056 6.7 2.47 72/18 1.18 0.05 1.20 0.09 7.10 0.20 2.20 0.056 6.7 2.47 72/18 1.18 0.05 1.20 0.09 7.10 0.20 2.20 0.056 6.7 2.47 72/18 1.18 0.05 1.20 0.09 7.10 0.20 2.20 0.056 6.7 2.47 72/18 1.20 0.05 2.00 0.09 7.10 0.20 2.20 0.056 6.7 2.47 72/18 1.20 0.05 2.00 0.09 7.10 0.20 2.20 0.056 6.7 2.47 72/18 1.20 0.05 2.00 0.09 7.10 0.20 2.20 0.056 6.7 2.47 72/18 1.20 0.05 2.00 0.09 7.10 0.20 2.20 0.056 6.7 2.47 72/18 1.20 0.05 2.00 0.09 7.10 0.00 7.20	\$5/18	11284/L	Nası	ana Di	stributary)											720	
555718 1.00 0.03 1.10 1.00 0.03 1.10 0.031 563 228 228 238 238 239 0.05 1.00 0.03 1.00 0.031 563 228 228 238 239 0.05 1.00 0.05 1.05 0.05 0.05 0.05 0.05	\$557/18 1,00 0.03 1,10 1.00 0.03 1,10 0.031 563 228	292	1				48/JB	7		2 5	l	2.75 2.85	0.135	689 558	267 226	720 W Bank+4 Drg 454	
97) 9 00 0.26 5557/18	55/57/18	Š			1		57/78 81/78	-ii		10		1.10	0.031	563	228	228 W Bank	
9.09 0.26 5.55/57/18 1.58 0.04 1.74 9.09 0.25 5.57/18 1.50 0.05 1.76 7.51 0.12 5.57/18 1.00 0.05 1.76 7.51 0.12 5.57/18 2.19 0.06 2.41 4.21 0.12 4.63 0.131 770 31.2 5.57/18 2.19 0.06 2.22 2.02 0.06 2.22 0.063 770 2.84 5.57/18 1.22 0.03 1.24 14.27 0.41 14.57 0.41 5.57 0.42 5.57 0.43 5.57 0.44 5.57 0.4	909 0.26 1.58 0.04 1.74 9.09 0.26 10.05 0.302 558 226 226 55/18 1.58 0.04 1.74 9.09 0.15 1.67 0.21 8.47 0.240 553 228 228 55/18 1.70 0.05 1.75 1.01 8.71 0.19 604 244 243 0.13 70 0.30 312 56/18 2.19 0.06 2.21 2.02 0.06 2.22 0.063 701 284 5.196 1.23 1.23 56/18 1.22 0.03 1.24 4.21 0.12 4.63 0.131 706 3.12 1.23 66/18 1.27 0.04 1.45 0.44 1710 0.484 4.28 173 1.75 66/18 1.27 0.04 1.44 0.13.55 0.34 15.13 0.428 646 261 267 66/18 1.27 0.04 1.45 1.208 0.34 13.66 0.387 474 192 192 657 184 646 246 267 266 267 268 <td< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td>₹</td><td></td><td></td><td></td><td></td><td>;</td><td>1,780</td><td>720</td><td></td><td></td></td<>							₹					;	1,780	720		
SSSISTIUB 1.58 0.004 1.74 9.09 0.26 1.005 0.302 558 226 228 238 239 239 238 239 238 239 238 239 238 239 238 238 239 238 239 238 239 238 239 238 239 238 239 238 239 238 239 238 239 239 238 239 238 239 238 239 238 239 238 239 239 239 239 239	SSISTIVE 1.58 0.04	32000/	R. Nas	rana D	istributary)										. :	1.503	
55JB 1.60 0.05 1.76 7.51 0.21 8.47 0.240 563 228 56JB 2.02 0.06 2.24 4.51 0.12 671 0.190 664 2.44 5.91 0.17 671 0.190 664 2.44 5.91 0.17 671 0.190 664 2.44 5.91 0.17 671 0.190 664 2.44 5.91 0.17 671 0.190 664 2.44 5.91 0.17 671 0.190 664 2.44 5.91 0.17 664 2.44 5.91 0.17 664 2.44 5.91 0.17 664 2.44 5.91 0.17 664 2.44 5.91 0.17 664 2.44 5.91 0.17 664 2.44 5.91 0.17 664 2.44 5.91 0.17 664 2.44 5.91 0.17 664 2.44 5.91 0.17 664 2.44 5.91 0.17 664 2.44 5.91 0.17 664 2.44 5.91 0.17 664 2.44 5.91 0.17 664 2.44 664 2	55/18 1.56 0.05 1.76 7.51 0.21 8.47 0.240 563 224 56/18 2.19 0.06 2.24 2.02 0.06 2.21 0.07 312 56/18 2.19 0.06 2.22 2.02 0.06 2.22 0.06 3.19 1.70 284 56/18 1.22 0.06 1.24 14.57 0.41 1.710 0.484 4.23 1.73 1.23 66/18 1.22 0.03 1.24 14.57 0.41 1.710 0.484 4.23 1.73 66/18 1.22 0.03 1.24 14.57 0.41 1.710 0.484 4.23 1.73 66/18 1.22 0.03 1.24 14.57 0.41 1.710 0.484 4.23 1.73 66/18 1.12 0.04 1.45 0.04 1.45 0.28 0.58 0.28 2.24 2.04 1.74 1.74 1.74 1.7	8	1		1		55/57/18			1.74	1	10.65	0.302	\$58	226	1.293 W Bank	
55/18 1.70 0.05 1.87 5.91 0.17 6.71 0.190 604 224 56/18 2.19 0.06 2.41 4.21 0.12 4.63 0.131 770 312 56/18 2.19 0.06 2.22 2.02 0.06 2.22 0.063 701 284 56/18 1.22 0.05 0.06 2.22 2.02 0.06 2.22 0.063 701 284 56/18 1.22 0.03 1.34 14.57 0.41 17.10 0.484 4.28 173 0.04 1.32 0.04 1.45 1.07 0.04 1.33 0.38 15.13 0.428 646 261 0.05 0.04 1.36 0.03 0.23 14.7 0.04 1.37 0.04 1.36 0.03 0.23 14.7 0.04 1.37 0.04 1.36 0.03 0.23 363 14.7 0.04 1.30 0.03 0.20 0.38 0.02 0.03 0.02 0.03 0.02 0.03 0.02 0.03 0.02 0.03 0.02 0.03 0.03	55/18 170 0.05 1.87 591 0.17 671 0.190 664 244 56/18 2.19 0.06 2.22 2.02 0.06 2.22 0.06 2.22 0.06 2.22 0.06 2.22 0.06 2.22 0.06 2.22 0.06 2.22 0.06 2.22 0.06 2.22 0.06 2.23 0.06 2.23 0.06 2.23 0.06 2.23 0.06 2.23 0.06 2.23 0.06 2.23 0.06 1.23 0.06 1.23 0.06 1.23 0.07 1.23 0.04 4.28 173 0.28 1.73 0.48 4.28 173 0.06 2.24 1.29 0.06 2.24 1.29 0.06 2.24 1.29 0.06 2.24 1.29 0.06 2.23 0.06 2.23 0.06 2.23 0.06 2.23 0.06 2.23 0.06 2.23 0.07 0.06 2.06 1.29 0.06 2.06 1.29 0.06 2.06 <t< td=""><td>8 8</td><td></td><td></td><td></td><td>:</td><td></td><td>• ==•</td><td></td><td>1.76</td><td></td><td>8.47</td><td>0.240</td><td>563</td><td>228</td><td>1.068</td><td></td></t<>	8 8				:		• ==•		1.76		8.47	0.240	563	228	1.068	
S6/18 2.17 0.05 2.22 2.02 0.06 2.22 0.065 7.01 2.44 1.09 0.20 0.20 0.22 2.02 0.06 2.22 0.065 701 224 1.09 0.20 0.20 0.22 0.065 7.01 2.44 1.29 1.2	5601B 2.07 0.06 2.21 0.06 2.22 0.06 2.22 0.06 2.23 0.05 3.196 1.293 5601B 2.09 0.26 2.22 0.06 2.22 0.06 2.22 0.06 2.23 0.05 1.293 5601B 1.22 0.03 1.34 14.57 0.41 17.10 0.484 4.28 173 173 6601B 1.22 0.03 1.34 14.57 0.41 17.10 0.484 4.28 173 264 261 6601B 1.27 0.04 1.40 13.35 0.43 15.13 0.428 6.42 261 263 264 261 6601B 1.37 0.04 1.73 10.76 0.34 13.65 0.387 474 192 660 1.37 0.02 1.21 0.25 0.25 0.25 0.25 267 267 267 267 267 267 267 267 267 268 267 268 2	145					55/JB	## (1.87		6.71	0.190	\$ 5	4 5	840 W Bank 505 to Bank	
14.57 0.41	14.57 0.41	14. 14. 14.					56/JB	4,0		222		2.22	0.063	? ? ?	3,3	284 Salah	•
55//8 1.22 0.03 1.34 14.57 0.41 17.10 0.484 4.28 173 66//8 1.27 0.04 1.40 13.35 0.38 15.13 0.428 646 261 261 66//8 1.27 0.04 1.40 13.35 0.38 15.13 0.428 646 261 261 66//8 1.52 0.04 1.45 12.08 0.34 13.66 0.387 474 192 66//8 1.57 0.04 1.73 10.76 0.30 12.18 0.345 553 224 66//8 1.12 0.05 1.23 9.19 0.26 10.33 0.293 363 147 66//8 1.12 0.05 1.23 9.19 0.26 10.33 0.293 363 147 66//8 1.10 0.03 1.21 6.27 0.18 7.02 0.199 607 67//8 1.70 0.03 1.20 6.77 0.18 7.02 0.199 607 67//8 1.54 0.04 1.90 0.05 2.09 0.059 670 271 67//8 1.50 0.05 2.09 1.90 0.05 2.09 0.059 670 271 67//8 1.50 0.05 2.09 1.90 0.05 2.09 0.079 670 271 71//18 0.72 0.02 0.79 7.10 0.20 8.23 0.23 255 103 72//8 1.76 0.05 1.94 6.38 0.18 7.43 0.210 619 251 72//8 1.35 0.04 1.41 3.79 0.11 4.35 0.123 454 119 72//8 1.35 0.04 1.41 3.79 0.11 4.35 0.123 454 184 72//8 1.56 0.03 1.28 0.04 1.28 0.076 4.09 1.09	655/18 1.22 0.03 1.34 14.57 0.41 17.10 0.484 428 173 66/18 1.27 0.04 1.40 13.35 0.34 15.13 0.428 646 261 66/18 1.27 0.04 1.40 13.35 0.34 15.13 0.428 646 261 66/18 1.27 0.04 1.45 12.08 0.34 13.66 0.387 474 192 66/18 1.12 0.04 1.73 10.76 0.36 138 0.345 553 224 66/18 1.12 0.05 1.23 9.19 0.26 10.33 0.25 655 657 677 246 675 677 246 677 246 677 246 677 246 219 671 247 219 671 247 219 671 247 219 273 249 119 271 247 219 273 273	:						6						3,196 1,293	1,293		
66/18	9750 2972 65/1/8 122 0.03 1.34 14.57 0.41 17.10 0.494 428 173 1127 344 66/1/8 1.22 0.04 1.40 13.35 0.38 15.13 0.428 646 261 127 344 66/1/8 1.27 0.04 1.40 13.35 0.38 15.13 0.428 646 261 2213 675 66/1/8 1.57 0.04 1.73 10.76 0.30 12.18 0.345 553 224 1083 338 66/1/8 1.15 0.05 1.23 9.19 0.26 10.33 0.293 363 147 1108 338 66/1/8 1.10 0.03 1.21 6.27 0.18 7.02 0.199 371 1.50 2203 671 67/1/8 1.73 0.05 1.90 0.05 1.08 0.209 371 1.50 0 0 6/1/1/8 1.54 0.04 1.69 3.44 0.10 3.78 0.107 542 219 0 0 6/1/1/8 1.50 0.05 2.09 1.90 0.05 2.09 0.059 670 271 0 0 0 6/1/1/8 1.50 0.05 2.09 1.90 0.05 2.09 0.059 670 271 0 0 0 6/1/1/8 0.05 2.09 1.90 0.05 2.09 0.059 670 271 0 0 0 6/1/1/8 0.05 2.09 1.90 0.05 2.09 0.059 670 271 0 0 0 7/1/1/8 0.05 1.94 6.38 0.18 743 0.210 619 294 119 0 0 0 7/1/1/8 0.05 0.91 4.9 2.51 0.07 2.76 0.078 476 193 0 0 0 7/1/1/8 0.05 0.91 4.9 2.51 0.07 2.76 0.078 476 193 0 0 0 7/1/8 1.35 0.04 1.49 2.51 0.07 2.76 0.078 476 193 0 0 0 7/1/8 1.35 0.04 1.49 2.51 0.07 2.76 0.078 476 193 0 0 0 7/1/8 1.35 0.04 1.49 2.51 0.07 2.76 0.078 476 193	62933	A. Nasr	ana Di	stributary)												
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66/JB 1.57 0.04 1.73 10.76 0.30 12.18 0.345 553 224 65/JB 1.12 0.05 1.23 9.19 0.26 10.33 0.293 363 147 65/JB 1.10 0.05 1.28 8.07 0.23 9.05 0.256 653 256 65/JB 1.10 0.03 1.21 6.27 0.18 7.02 0.199 371 150 67/JB 1.54 0.04 1.59 0.105 3.76 0.105 577 67/JB 1.54 0.04 1.59 0.05 2.09 0.059 670 271 67/JB 1.54 0.04 1.457 0.41 2.09 0.05 2.09 0.059 670 271 71/JB 0.72 0.02 0.79 7.10 0.20 8.23 0.233 255 103 71/JB 0.72 0.02 0.79 7.10 0.20 8.23 0.233 255 103 72/JB 1.28 0.04 1.44 3.79 0.11 4.35 0.120 619 251 72/JB 1.35 0.04 1.44 3.79 0.11 4.35 0.123 4.44 119 72/JB 1.35 0.04 1.44 3.79 0.11 4.35 0.123 4.46 119 72/JB 1.35 0.04 1.44 3.79 0.11 4.35 0.123 4.46 119	66/JB 1.57 0.04 1.73 10.76 0.30 12.18 0.345 553 224 65/JB 1.12 0.05 1.23 9.19 0.26 10.33 0.293 363 147 66/JB 1.80 0.05 1.98 8.07 0.23 9.05 0.256 652 256 65/JB 1.10 0.03 1.21 6.27 0.18 7.02 0.199 371 150 67/JB 1.54 0.04 1.69 3.44 0.10 3.78 0.107 542 219 67/JB 1.54 0.04 1.69 3.44 0.10 3.78 0.107 542 219 67/JB 1.54 0.04 1.69 3.44 0.10 3.78 0.107 542 219 71/JB 0.72 0.02 0.79 7.10 0.20 2.09 0.039 670 271 71/JB 0.83 0.02 0.79 7.10 0.20 8.23 0.233 255 103 71/JB 0.83 0.02 0.79 7.10 0.20 8.23 0.233 255 103 71/JB 0.83 0.02 0.79 4.62 0.13 5.26 0.149 294 119 72/JB 1.28 0.04 1.41 3.79 0.11 4.35 0.123 454 184 72/JB 1.35 0.04 1.49 2.51 0.07 2.76 0.078 4.76 193 72/JB 1.16 0.03 1.28 1.16 0.03 1.28 0.036 4.09 166	13		-4.			86/JB			\$ \$			0.387	4 4 5	132		
65/18	65/JB 1.12 0.05 1.23 9.19 0.26 10.33 0.223 363 147 65/JB 1.80 0.05 1.98 8.07 0.23 9.05 0.256 652 256 65/JB 1.10 0.03 1.21 6.27 0.18 7.02 0.199 371 150 67/JB 1.54 0.04 1.69 3.44 0.10 3.78 0.107 542 219 67/JB 1.54 0.04 1.69 3.44 0.10 3.78 0.107 542 219 67/JB 1.54 0.04 1.69 3.44 0.10 0.20 8.23 0.233 253 103 71/JB 0.72 0.02 0.79 7.10 0.20 8.23 0.233 253 103 71/JB 0.83 0.02 0.91 4.62 0.13 5.26 0.149 294 119 72/JB 1.28 0.04 1.41 3.79 0.11 4.35 0.123 454 184 72/JB 1.35 0.04 1.49 2.51 0.07 2.76 0.078 476 193 72/JB 1.16 0.03 1.28 1.16 0.03 1.28 0.036 409 166	136		CA.			66/JB	-		1.73			0.345	553	777		
65/18 1.00 0.03 1.78 6.37 7.25 7.02 0.150 0.151 150 0.151 150 0.151 150 0.151 150 0.151 150 0.151 150 0.151 150 0.151 150 0.151 150 0.151 150 0.152 0.152 0.153 0.151 150 0.152 0.152 0.153 0.151 150 0.152 0.153 0.153 0.153 0.153 0.153 0.153 0.153 0.153 0.153 0.154 0.151 150 0.152 0.153 0.153 0.153 0.153 0.153 0.153 0.151 150	65/18	246					65/JB	- -		<u> </u>			0.293	363	147		
67/18 1.73 0.05 1.90 5.17 0.15 5.76 0.163 607 246 67/18 1.54 0.04 1.69 3.44 0.10 3.78 0.107 542 219 67/18 1.54 0.04 1.69 3.44 0.10 3.78 0.107 542 219 67/18 1.90 0.05 2.09 1.90 0.05 2.09 0.059 670 271 5.286 2.139 2.139 2.139 2.139 2.139 2.139 2.139 2.139 2.139 2.139 2.139 2.139 2.139 2.139 2.139 2.139 2.139 2.139 2.138 0.04 1.41 3.79 0.11 4.35 0.123 4.54 1.19 7.278 1.35 0.04 1.41 3.79 0.11 4.35 0.123 4.54 1.19 7.278 1.35 0.04 1.28 0.21 6.03 2.21 6.039 2.22 6.039 2.23 6.	67/18 1.73 0.05 1.90 5.17 0.15 5.76 0.163 607 246 67/18 1.54 0.04 1.69 3.44 0.10 3.78 0.107 542 219 67/18 1.54 0.04 1.69 3.44 0.10 3.78 0.107 542 219 57/18 1.50 0.05 2.09 1.90 0.05 2.09 670 271 5.286 2.139 5.13	5.5					65/1B			1.38			0.19	371	3	-	
67/1/8	67/18 1.54 0.04 1.69 3.44 0.10 3.78 0.107 542 219 67/18 1.90 0.055 2.09 1.90 0.05 2.09 0.059 670 271 14.57 0.41 7.10 0.20 7.10 0.20 8.23 0.233 255 103 71/18 0.82 0.02 0.79 7.10 0.20 8.23 0.233 255 103 71/18 0.83 0.02 0.79 7.10 0.20 8.23 0.233 255 103 71/18 0.83 0.02 0.79 7.10 0.20 8.23 0.20 619 251 71/18 0.83 0.02 0.79 7.10 0.20 8.23 0.20 619 251 71/18 0.83 0.02 0.79 7.10 0.20 8.23 0.20 619 251 72/18 1.28 0.04 1.41 3.79 0.11 4.35 0.123 454 184 72/18 1.35 0.04 1.49 2.51 0.07 2.76 0.078 4.76 193 72/18 1.16 0.03 1.28 1.16 0.03 1.28 0.056 409 166 72/18 1.10 0.20 1.20 1.28 1.16 0.03 1.28 0.056 409 166	161					67/JB			8.			0.163	607	246		
67718 1.90 0.05 2.09 1.90 0.05 2.09 0.059 5.70 2.71 5.286 2.139 5.286 2.139 5.286 2.139 5.286 2.139 5.286 5.139 5.139 5.139 5.286 5.139 5.	67/18 1.90 0.05 2.09 1.90 0.05 2.09 0.059 0.07 2.11 14.57 0.41 7.10 0.20 2.03 2.28 2.139	161					67/18			1.69			0.107	¥.	219		
7.10 0.20 7.10 0.20 7.10 0.20 7.10 0.20 7.10 0.20 7.10 0.20 7.20 0.33 0.35 103 7.20 0.30 1.94 6.38 0.18 7.43 0.210 6.19 251 7.20 0.83 0.02 0.91 4.62 0.13 5.26 0.149 294 119 7.20 1.28 0.04 1.41 3.79 0.11 4.35 0.123 454 184 7.20 1.35 0.04 1.49 3.79 0.11 2.76 0.078 4.76 193 7.21 0.07 2.76 0.078 4.76 193	7.10 0.20 7.10 0.20 7.10 0.20 7.10 0.20 7.10 0.20 7.10 0.20 7.20 0.02 0.72 0.02 0.79 7.10 0.20 8.23 0.233 255 103 7.10 0.83 0.02 0.91 4.62 0.13 5.26 0.149 294 119 7.20 0.03 0.04 1.41 3.79 0.11 4.35 0.123 454 184 7.20 0.04 1.49 2.51 0.07 2.76 0.078 4.76 193 7.20 0.20 1.16 0.03 1.28 1.16 0.03 1.28 0.036 4.09 166 7.20 0.20 1.20 1.20 1.20 1.20 1.20 1.015	161	1			1 1, 1,	6//18	14		5	. 1		6000	5.286 2.139	2,139		
91 300 91 71/18 0.72 0.02 0.79 7.10 0.20 8.23 0.23 2.55 103 1832 5709 1740 72/18 1.76 0.05 1.94 6.38 0.18 7.43 0.210 619 251 1832 0 0 71/18 0.83 0.02 0.91 4.62 0.13 5.26 0.149 294 119 3658 5993 1827 72/18 1.28 0.04 1.49 3.79 0.11 4.35 0.123 4.54 184 3658 0 0 72/18 1.15 0.03 1.28 0.078 4.79 166 3658 0 0 72/18 1.16 0.03 1.28 0.07 2.76 0.03 1.58 1.66 0.03 1.58 0.03 1.69 169 169 169 169 169 169 169 169 169 169 169 1	91 300 91 71/18 0,72 0,02 0,79 7,10 0,20 8,23 0,233 255 103 1832 5709 1740 772/18 1,76 0,05 1,94 6,38 0,18 7,43 0,210 6,19 251 1832 0 0 771/18 0,83 0,02 0,91 4,62 0,13 5,26 0,149 294 119 3658 5993 1827 772/18 1,28 0,04 1,41 3,79 0,11 4,35 0,123 4,54 184 3658 0 0 772/18 1,35 0,04 1,49 2,51 0,07 2,76 0,078 4,76 193 3658 0 0 772/18 1,16 0,03 1,28 1,16 0,03 1,28 0,036 4,09 166 1,015 1,015	3792/R	Nasra	ına Dis	tributary)											1.015	÷
1832 5709 1740 72/18 1.76 0.05 1.94 6.38 0.18 7.43 0.210 619 251 1832 0 0 71/18 0.83 0.02 0.91 4.62 0.13 5.26 0.149 294 119 3658 5993 1827 72/18 1.28 0.04 1.49 3.79 0.11 4.35 0.123 454 184 3658 0 0 72/18 1.16 0.03 2.76 0.078 4.76 193 3658 0 0 72/18 1.16 0.03 1.28 0.036 4.09 166	1832 5709 1740 72/18 1.76 0.05 1.94 6.38 0.18 7.43 0.210 619 251 1832 0 0 71/15 0.83 0.02 0.91 4.62 0.13 5.26 0.149 294 119 3658 5993 1827 72/18 1.28 0.04 1.41 3.79 0.11 4.35 0.123 454 184 3658 0 0 72/18 1.35 0.04 1.49 2.51 0.07 2.76 0.078 476 193 3658 0 0 72/18 1.16 0.03 1.28 0.076 4.99 166 3658 0 0 72/18 1.16 0.03 1.28 0.036 4.99 166 7.10 0.20 1.20 1.20 1.01 2.00 1.01 2.00 1.01 2.00 1.01 1.01 1.01 1.01 1.01 1.01						71/118	C		0.70			0.233	255	103	1.015 W Bank	
1832 0 71/JB 0.83 0.02 0.91 4.62 0.13 5.26 0.149 294 119 3658 5993 1827 72/JB 1.28 0.04 1.41 3.79 0.11 4.35 0.123 454 184 3658 0 0 72/JB 1.35 0.04 1.49 2.51 0.07 2.76 0.078 4.76 193 3658 0 0 72/JB 1.16 0.03 1.28 0.036 4.09 166	1832 0 71/JB 0.83 0.02 0.91 4.62 0.13 5.26 0.149 294 119 3658 5993 1827 72/JB 1.28 0.04 1.41 3.79 0.11 4.35 0.123 454 184 3658 0 0 72/JB 1.35 0.04 1.49 2.51 0.07 2.76 0.078 476 193 3658 0 0 72/JB 1.16 0.03 1.16 0.03 1.28 0.036 409 166 7.10 0.20 1.28 0.20 1.015 1.015 1.015	,8					72/JB) ===i		8			0.210	619	251	9il w Bank	
3628 5993 1827 72218 128 0.04 141 3.79 0.11 4.35 0.125 454 184 3.58 0 0 72218 0.04 1.49 2.51 0.07 2.76 0.078 476 193 3658 0 0 77218 116 0.03 1.28 1.16 0.03 1.28 0.036 4.09 166	3638 5993 1827 72238 1.28 0.04 141 3.79 0.11 4.35 0.123 4.34 184 3.68 0 0 72238 7.21 0.07 2.76 0.078 4.76 193 3658 0 0 72238 1.16 0.03 1.28 0.036 4.09 166 7.20 0.20 1.16 0.03 1.28 0.036 4.09 166 7.10 0.20 1.16 0.03 1.28 0.036 4.09 1.015 1.015	8					71/38	ο.		16.0			0.149	\$ 5	611	661 W Bank	
3658 0 0 727/18 116 003 128 1000 409 166	3658 0 0 72JB 1.16 0.03 1.28 1.16 0.03 1.28 0.036 409 166 7.10 0.20 7.10 0.20 1.28 1.16 0.03 1.28 0.036 1.015	3 8		Ŕ	8		72/38			1.43			0.078	\$ 54	\$ 8	358 US Aid+MPA+W.I	
CO. CO. CO. C.	7.10 0.20	120		:			72/18			28			0.036	\$	<u>%</u>	166 US Aid+W Bank	

Table B • 1 (2/3) Breakdown of Authorized and Design Discharge Calculation for LCC Area

ON estudosesto.	Not No	â		Section	ç	Village	Chak No.	Outlet Disharge	sharge	Section	Design	ا	Outlet CCA	۱	Section Project	Remarks
(monor)	1	(feer)	Œ	Distance	ខ	•		Authorized	Design	Discharge	Discharge	֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֡֓֓֓֓֓֡֓֓֡֓֡	(acte) (t	(gg)	CCA (Improvement)	
		:)	(leet)	æ			(casec) (m3s)	s) (cusec)	(cusec) (m3s)	(cosec)	(m3s)			(ha)	
Natheri Minor (RD 106799/L, Nasrana Distributary)	W 10679	M.	Vasran	a Distr	ibutary)		:							-	300	
								- 1			07.31	ACAN	ı	1	NO 715 A.M	
1424 7850/1		850	2393	7850	239.3		2011			15.69 0.50	5 C	2000			407 115 Aid	
2 1425 8826/R		8826	2000	976	167		47/4/				3	0 30			380 US Aid	
		7557	7087	, ;	767		1770				950	0.27			.175 W Bank	
7/2/001 /2*1 #		4/00	2 6	71/	25		07/0				7 20	0.203			871	
		3	76/5	8	77/		35005			5.48 0.16	6.12	0.173			749	
		7 6	7/01	3	- - - - - - - - - - - - - - - - - - -		drienor.		. :		100	0.137			625 US Aid+W Bank	
7 1430 1509//TK		755	365	70,) c		78/78/1B	23.00%	2.45	2.23 0.06	2.4.2	000		318	318 W Bank	
		3	3				2000		١	ı			ľ	8		
							:		9	:			008.1			
Domra Minor (RD 121531/L, Nasrana Distributary)	D 12153	いい	vasran	a Distr	butary)						2			•		
															2,610	
1422 49501		0507	\$00	4950	1509 Ratlway St	way St.		l			21.36	0.605			5.616	
7 1723 50508		Ş	\$30	Ę	ç		84/IB		-		20.94	0.593			2,610	
AUDOUC 6.541 . 2		2 8	. 5	3 6	, ,		a1/88				18.53	0.525			239	
3 1434 0300/K		966	35	000	000		07/00	2			15.98	0.453			1,980	
4 1435 /992K		7	0,1	2			9000				14.50	0.413			820 M P A .W Bank	
S 1436-9561/L		9261	2914	200	478		87/78				\ \(\frac{1}{2}\)	2000			1 656	
6 1437 9794/L		9794	2985	233	71		85/JB				3.5	0,000		5 6	4000	
7 1438 11150/L	-	1150	338	1356	413		85/JB				٠,٠.٠ د د د د د د د د د د د د د د د د د د د	0.558		8	CAN W DANK	
8 1439 12645,		2645	3854	1495	456		88/18		٠.		40.0	0.770		177	OTC W Bank	
9 1440 I3230/L	_	3230	4033	585	178		86/18				7.7	7 (3 8	700 w bank	
10 1441 18069/11		6908	5507	4839	1475		86/18	29 0			0 7	50.0		ì	MEG W+'W'W 77/	
		69081	5507	0	0		87/18	1.70 0.05	35	3.49 0.10	\$ 5 5	900		ž Š	250 W Bank	
12 1443 18069/TF		8089	5507	٥	0		8///8				1.2	20.0	1	1 4	Allen a Torra	
		1	: :					.0 05.81	70				2,616	010		
Gojra Distributary	Y.Y.			:										•		
			•				A TO STANLEY	1		7		0.70	700	ľ	/ 1.July 1	
1 2957 155/1		155	47	155	43		361/JB			8. 6.70	8.50	555.	9.	3:	7.240	
2 2958 160/L		8	\$	Ý	cł.		361/JB			~ .	9 5	28. 28.	Ç:		/ CO W Bank	
3 2959 i80/L		8	55	న	v o		361/18				20.00	600	9 8		7.1 IO W ISANK	
		517	158	337	103		362/JB				3 5 8 5	70.7	e e		O,Y.V. W Dank	
\$ 2961 4360/L	ں	898	323	3843	171		362/JB			2000	2000	867	şç		0,000 w bank	
6 2962 5495/L	ر	2,49	675	1135	5,5		362/JB			-	00.80	26.5	250	110	0,4/J	
7 2963 7634/1		7634	2327	2139	652		363/18		:	46.57	8. 5	, oo	666	17.	O, 2007 W DARRAGO ONE A OAS	-
8 2964 13254/L		3254	9	2620	1713		304/18		<u> </u>	7.		100.1	275	5	5.050 W Book+115 AM	
9 2965 I33Z6/L	•	3326	662	7/	77.		303/18					107	5 6	Ē	5.7.17 W Pank+115 Aid	
10 2966 16923	- •	52691	2128	1666	983	:	204/25			50 50		007	1 %		5.546 W Rank	
11 2967 18961/L		18961	5779	20:48	3	•	364/18		200		:	300	ŝ		5.438 ·· Cars	
12 Z968 1930Z/R		70561	200	7 000	₹ 8	÷	366770					344	3.5		\$ 232	
5863		22191	45	5887	8 8	:	307000			30.56		5	286		10%	
		00000	6060	200	3 4		365/18					275	388	145	2,992	
7116027 1167 CI		70807	6070	; C	c		363/JB						575		4,847 W Bank	
2073		28915	8813	6018	1834		370/18	5. 2.	0.04 1.38	35.96 1.02	42.06	1.191	198		4,615	
2974		29090	8867	175	S. G	FDR COJRA			_	_			ξ, Τ.		4,535	
			1.													

Table B - 1 (2/3) Breakdown of Authorized and Design Discharge Calculation for LCC Area

<u>ا</u>	-												3.93)																																
Remarks													Zeera Minor(8.93)						İ			i																							
Section Project	5		4,535	4,555 4,484 W Bank	4,259	4,259	4,157 W Bank+US Aud	,992 W Bank	3,714 W Bank	3.578 W Bank	3,414 W Bank	3,220 W Bank		,678 W Bank+US Aid	1,383	.186 W Bank	924	727 W Bank	408 W Bank+US Aid			193	1,193 W Bank	984 W Bank+US Aid	776 W Bank+US Aid 580					610.	610.	20,882	4777	20,268	40,512 w Bank	10 043 W Rook	1707 TO 1800	19,782 4 Drg	19,050 W Bank 10,404	19,494 10,702 ms x 3, 11/ 0, 11	19,233 US A30+W DAM.	18.881	008,81	18,551 W Bank	.378
	چا	:		2,4 2,4 4,4		502	•	Ü	135 3	• •						762	6	318	ş	Š		-			8 8 8					53		157. 20				•	•	1			3.4			173 18	
Outlet CCA	(acre)		4 5	18	W.S.	253	2 08	83	33	6	479		-	729	487	Z		787	1	18,632 7 7,540					483		`				340	88	8	38	26.5	800	950	200	600	30.1	765	88	615	428	541
	!	m3s)	1.116	3 2	1.033	0.979	0.956	0.917	0.839	0.810	0.767	0.716	0.636	0.382	0.316	0.269	0.209	0.159	0.089				0.253	0.221	0.169						6.957	6.918	0.873	6.814	6,755	9699		270	6.0238	704.0	8 9	6313	6.283	6.202	6.129
Design	Discharge	(casec)	39.41	\$ 00 00 00 00 00 00 00 00 00 00 00 00 00	36.49	34.56	33.77	32.37	3.65	28.59	27.07	55 55	25.44	3.49	11.15	9.48	7.38	5.62	3.16			:	8.93	7.79	5.98 4.48						245.65	244.27	7.70	190.01	22.74	33.5	2000	37.7	220.83	27.77	25.05 20.05	222.93	221.82	218.99	216.41
Section	Discharge	(cusec) (m3s) (-		31.70 0.90		29.23 0.83		25.69 0.73		23.55 0.67				9.82 0.28				2.87 0.08			7.77 0.22	7.77 0.22		5.44 0.15 4.07 0.15	1				5.66	Į.			9071 77061						187.72 6.25			1	81.68 5.15	180.46 5.11
20	Design) (casec)	0.55	24.7	8	0.79	1.28	2.62	9.	131	ମ	2.73	8.93	233	3	2.10	7	3.5	9	٠.			0.96	é.	1 4 1 5 1 8 4 8 8 4 8						· ·		•											45.	1.73
Outlet Dishare	Authorized	(cusec) (m3s)	0.50 0.01	58 0.01			1.16 0.03	2.38 0.07			1.36 0.02							2.24 0.06	- 1	57.79 1.64			1		1.37 0.04					•	1.15 0.03			1.78 0.05		113 003		50.0						1.22 0.03	
Chak No.	•	•		3/0/18	370/3B	371/38	366/18	366/18	371/JB	371/18	371/18	367/JB		370/18	369/1B	367/JB	369/JB	369/1B	368/13				371/18	372/JB	372/JB 373/JB						437/GB	438/CB	438/CB	45//17/CB	43//05	437/68	00000	10000 10000 10000	45%CD	447/CB	440/GB	439/GB	440/GB	439/CB	441/GB
Village			conce						*											:																				i					
Section	Distance	(w)	39 70 Factories	578		8 2		377		: :-	_	4			1 774		6 1678	0	0 0			utary)		147	00	Ì						97.				. 65. 26.		0.75			_			7 1371	
	l	E		007		-		12.36		9 2479		_	•		3 254	: '	5506	-	<u>.</u>			Crstrib	1	2 4839	C] C						980							8 2 2						4 4497	
RD	(E)			9514	-				7, 10274				-					1508				Corra	Į.		2712	l					Į.	292				28.0	•	355		:		_		77 8494	
, io	(feet)		29319	21158	31230	312	32471	33707	33707	36186	39482	40990	41305	41367	43908	43908	49414	49414	49414		18	305/K,	Q	88	8897 8807				Ž	ì	380	∞ }	£ 5	ô		250	į	93	<u> </u>	3 3 3 3 3 3 3 3 3 3	19629	2000	2337	27867	2878
No. Watercourse No.	ન્ન		2975 29319/R	2976 30559/K		2979 31238/R						2984 40990/L	+1305/R			2987 43908/L	2988 49414/TF	2989 49414/TR	2990 49414/11		1000	Zeera Minor (RD 41305/K, Gojra Distributary)	2992 4058/L	2993 8897/TL	2994 8897/TR 2005 8897/TF		İ	ircle	Kilianwala Definibatary		582 380/L		384 3843/K	7/1669 585											597 28780AL
o,	_		<u>5</u>	38	វភ	ន	4		8		22							æ.	7			CCCT307	l		ሎ ዛ		ļ	East Circle	Kilian		-	с ч с	٠, .	-1 v	n 4) r-	۰ ٥	00	> <u>c</u>	2 =	: 23	!	8	7	\$

Table B - 1 (2/3) Breakdown of Authorized and Design Discharge Calculation for LCC Area

5.01 212.38 4.98 210.56 4.90 207.57 4.85 205.47 4.78 201.63 4.77 200.09
178.89 5.07 214.43 6.073 621 177.06 5.01 212.38 6.015 429 175.70 4.93 210.56 5.963 564 172.90 4.90 207.57 5.878 562 171.37 4.85 205.47 5.819 340 170.33 4.82 203.76 5.770 462 168.94 4.78 201.63 5.710 317 168.94 4.78 201.63 5.710 317
177.06 5.01 212.38 6.015 175.70 4.98 210.56 5.963 175.70 4.98 200.57 5.878 172.29 4.90 207.57 5.878 171.37 4.85 205.47 5.819 171.37 4.85 205.47 5.819 170.33 4.82 203.76 5.770 168.94 4.78 201.63 5.710 168.94 4.78 201.63 5.710
175.70 4.98 174.10 4.98 171.29 4.90 171.37 4.85 170.33 4.82 168.94 4.78
1.04 0.03 1.39 0.04 1.11 0.03 0.91 0.03
44/GB 1.11 444/GB 0.91
3 4 3
315
1233

Table B - 1 (2/3) Breakdown of Authorized and Design Discharge Calculation for LCC Area

cetion
(feer) (m)
640 93094/L 93094 28375 2194 669 455/541/456/GE
97670 29770 4556 1389 T/Wala Sugar Mill
642 98170R 98170 29922 500 152 542/CB
101535/R 101535 30948 3008 917
101825 31036 290
1024301. 102430 3124 003 104 1064801. 106480 32455 4050 1234
107000/R 107000 32614 520 158
108265/L 108265 32999 1265 386
630 111396/L 111396 33954 3131 954 550 545056 651 11386878 113868 27873 5163 660
113558/L 11358 34612 0 0
114654 34947 1096 334
116840/L 116840 35613 23
116865/R 116865 35620 25 8
35622 6
11000/1 117000 35662 64 20
119142/R 119142 36314 2142 653
121000/L 121000 36881 1858 566
123506/L 123506 37645 2506 764
125000/R 125000 38100 1
002 123800/L (23800 38304 800 204 333/UB 550/UB 663 1268661 126866 38666 990 302
126856/L 126856 38666 0 0
130570/R 130570 39798 3714 1132
131793/L 131793 40171 1223 373
135300/L 135300 41239 3507 1069
136506/L 136506 41607 1
140556/R 140556 42841 1805 550
140677/1 140677 42878 121 37
142239/R 142239 43384 1562 476
143377/R 143377 43701 1.138
146770/R 146770 44735 3393 1034
148324/L 148324 45209 1554 474
151086/TR 151086 46051 2762 842
677 151086/TC 151086 46051 0 0 557/GB
131080/12 131080 40031 0 0
Minor #7 (RD 116865/R, Kilianwala Distributary)
1230 5738
1747 8047

Table B • 1 (2/3) Breakdown of Authorized and Design Discharge Calculation for LCC Area

Remarks																													
Project	(improvement)	ا د کند د				1,567 US Aid+W Bank	.299.4 Drg	.154 US Aid	996 W Sank+4 Drg 780	- 30 H			**	704 w Bank 500	S US Aid				18,984 W Bank	W Sank	T COURT	vi è	> w	17,582 W Bank	S + Dank	17,256 W Bank	3 W Bank	16,629 W Bank 16,389 W Bank	
Section	§ ê							_		2							19 161	ı.											
Outlet CCA	(eu)	888					25.25							\$ \$	ļ									148				25 25 27 27 28	
Out	(acre)	500 759 759 759	4346	1.75							:	4,303		\$ \$	88	: 73 5		439					:					593 439	
52	(m3s)				0.387	0338	0.315	0.252	0.213	0.121	0.022							5.033	4.987	36.4	4.811	4.730	4.618	4.591	4.	4.46	4,339	4.29 4.23 8.23 8.23	
Design	Cusec) (m.				13.65	22	9.53	8.8	7.53 5.81	4 28	0.78		-					177.71	176.10	1,4,45	169.88	167.01	163.07	162.13	158.20	157.56	153.21	151.51	
Section	Cusec) (m3s)		1.38 0.04				9.65 0.27 8.31 0.24						4.93 0.14	4.93 0.14 3.50 0.10			42 99 4 05	142.99 4.05		140.23 5.97			132.37 3.75				125.53 3.56	124.40 3.52	
9	Design (cusec)	282	1.52		0.63	0.68	1.47	77		<u> </u>	0.78			25 S	1.82					£ 5	ງ ຄູ	3;	0.88	21	0.28	1.61	124	¥ 5	:
Shar	Authorized (cusec) (m3s)	م سد سد حد	- 1				0.52 0.04			1.14 0.03	0.71 0.02			1.43 0.04 1.85 0.05		4.93 0.14	:	1.25 0.04				2.18 0.06	·	1,11 0.03				1.76 0.05	
Chak No.		1.			GB	38	88	8	88	85	38			CB CB	CB			78/GB	8	200	98	CB CB	3	86	9	242/GB	8 g	244/GB 243/GB	}
Village					444/GB	44/GB	446/GB 445/GB	447/GB	447/GB 446/GB	447/GB	448/GB			551/GB 552/GB	552/CB			178	223/C8	247	266/GB	241/GB	24.7.58 3.5.4.7.58	242/GB	747/08	242	25.	24.5 24.5 24.5 24.5 24.5 24.5 24.5 24.5	i 1 ·
Ϋ́		S Coort														:													
uoi	E)	22000	3 0	tary)	1421	85	368 888	80	\$ <u>=</u>	555	.0		utary)	1917 705	0			293	23	925 42 i	177	129	411	07.5	\$ 4 \$ 57	745	8 8	85	
Section	Distance (feet)	0500	00	vistribu	4662	2202	2323 2323 2323	3308	ž 8	1820	, O		Distrib	6290 2310	0	,		096			2376	424	250	22.22	1558	25.5	2035	3537	i 1
	Ê	0814 0814 0818		wala D	1421		3463 3828						ınwala		2621			292.6	8.			3353			8 8 2 4			7496	
ΩX	()	13715 13715 13715	13715	, Kiliar	4662	823	11361	15867	17210	19420	21859		I, Kiii	06298 0898	8600	100		3	001	4030	10576	1000	12500	15125	19500	21945	24526	24592	
No. Watercourse No.	(onginal)	719 13715/R 720 13715/TC 721 13715/TCR	13715/1L 13715/LCL	Minor #3 (RD 41830/L, Kilianwala Distributary)	700 4662/R	701 6837/R 702 9038/R	703 11361/L 704 12559/R	707 15867/R	708 17210/R 709 18682/I	710 19420/R	712 21859/TF		Minor #8 (RD 126856/L, Kilianwala Distributary)	714 6290/R 715 8600/TF	716 8600/TL		Mungi Distrubutary	1929 960/R	1930 1000/L	1931 4030/L	1932 8200/L 1933 10576/L	1934 11000/L	1935 12350/L 1937 12600/R		1939 17942/L 19500/L	_	1942 24526/L	1943 24592/R	
Š	9	₩ 4 A)	۰۰	Minor	-	M W	4 v	∞ •	٥ ۾	: ::::::::::::::::::::::::::::::::::::	4 E		Minor	- ~	60		Mung		. 7	٠٠.	4 A	יניטי	ر د ۳	4	, 4. 7	. so (2 5	= 1	į

Table B - 1 (2/3) Breakdown of Authorized and Design Discharge Calculation for LCC Area

Name	885 259 169 2-4-0-0-0-0-0-0-0-0-0-0-0-0-0-0-0-0-0-0-	Watercourse No.	(foct)	(w)	Section	o Village	age.	Chak No.	Outlet I Authorized	E P	Užeso	X 41				Outlet CCA (acre) (ha		E _	Project (Improvement)	Remarks
8885 2031 619 244/GB 112 0004 113 11013 344 1450 4718 426 4718 6718 6718 6718 6718 6718 6718 6718 6	888.8. 2031 1919 244/GB 112.0.010 123.101.33.44 145.00 143.17.34.44 145.00 145.77 144.00 45.00 143.17.34.44 145.00 145.77 144.00 145.00 145.17.34.44 145.00 145.00 145.77 144.00 145.77 144.00 145.77 144.00 145.77 144.00 145.77 144.00 145.77 144.00 145.77 144.00 145.77 144.00 145.77 144.00 145.77 144.00 145.77 144.00 145.77 144.00 145.77 144.00 145.77 144.00 145.77 144.00 145.77 144.00 145.77 1			ı	(Sec)	(w)			(cosec)	(щ33)	(conec)		Ĭ		m3s)			(ha)		
959 350 350 350 350 350 350 350 350 350 350	9593 350 <td></td> <td>l</td> <td>8885</td> <td>2031</td> <td>619</td> <td></td> <td>244/GB</td> <td>71</td> <td>0.04</td> <td>38.1</td> <td>121.37</td> <td></td> <td>8:</td> <td>4.180</td> <td>426</td> <td>Ι.</td> <td>16,212 US Aid</td> <td></td> <td></td>		l	8885	2031	619		244/GB	71	0.04	38.1	121.37		8:	4.180	426	Ι.	16,212 US Aid		
8691 375 25.4 245GB 175 055 191 1179 373 147 4,441 642 187 25.4 642 625 191 1179 378 25.4 642 625 <	96.91 87.5 25.45G/2 17.5 0.05 14.11 (1.6.9.3.1) 14.5 15.5 25.45G/2 17.5 0.05 11.11 (1.6.9.3.1) 14.5 15.5 25.45G/2 17.5 0.05 12.1 14.1 3.2 18.5 18.6 18.5 18.6 18.5 18.6 18.5 18.6 18.5 18.6 18.5 18.6 18.6 18.5 18.6<			8 53 53 53	250	385		244/CB 243/CB	1.15	666	9 3	18.88		5 4 5 8	4.128 4.089	412		15,039		
9775 276 174 0.05 191 191 3.5 3.5 2.5 </td <td>9775 276 RK 235GGB 1174 0.05 1189 138 188 55 25 25 10007 239 73 24 11419 323 188,62 390 55 22 10007 239 75 24,60 124 0.04 168 11619 318 188,62 390 58 22 1120 250 250 250 124 0.04 188 108,93 310 378 386 186 22 22 112 0.04 188 108,93 310 378 386 186 310 388 186 386 186 386 186 386 186 386 187 386 186 386 187 388 186 188 386 186 386 186 386 186 386 186 386 186 386 186 386 186 386 186 386 186</td> <td></td> <td></td> <td>8</td> <td>833</td> <td>Ä</td> <td>. •</td> <td>245/GB</td> <td>1.76</td> <td>50.05</td> <td>2,</td> <td>,</td> <td>-</td> <td>2.71</td> <td>8 1</td> <td>618</td> <td>ន្ត</td> <td>15,710 w Ban</td> <td>34</td> <td></td>	9775 276 RK 235GGB 1174 0.05 1189 138 188 55 25 25 10007 239 73 24 11419 323 188,62 390 55 22 10007 239 75 24,60 124 0.04 168 11619 318 188,62 390 58 22 1120 250 250 250 124 0.04 188 108,93 310 378 386 186 22 22 112 0.04 188 108,93 310 378 386 186 310 388 186 386 186 386 186 386 186 386 187 386 186 386 187 388 186 188 386 186 386 186 386 186 386 186 386 186 386 186 386 186 386 186 386 186			8	833	Ä	. •	245/GB	1.76	50.05	2,	,	-	2.71	8 1	618	ន្ត	15,710 w Ban	34	
9877 334 102 223/GB 120 0.00 221 11419 233 1882 2856 634 215 10607 236 124 0.00 123 11419 233 188 183 184 185	9977 334 102 23/3GB 100 22/3 III,14 223 138 552 592 5			5775	276	*		245/GB	1,74	_	1.91		_	65.01	3.982	553		15.460 W Ban	يد	
100077 205	1,000,13, 20, 3, 6, 2, 2, 2, 2, 2, 2, 2, 2, 2, 2, 2, 2, 2,			2877	334	102	- 1 "	243/GB	2.03	7	533			29.8	3.926	\$		15,236		
1,500, 15,00,	1,000, 1, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0,			200	2395	7.30	٠.	245/GB	3 c	8 6	90.			9 5	3.860	<u> </u>	210	14.984 W Ban	. .	
1,00,000,000,000,000,000,000,000,000,00	1,00,00,00,00,00,00,00,00,00,00,00,00,00		-	: 8 20 20 20 20 20 20 20 20 20 20 20 20 20	នុទ	٥		25/25/26	4 6	5 6	0 0 0 0			4 ¢	37.5	85		14,708 W Ban	× .	
12.27 21.81 22.84 22.8	12.201 83.4 25.4 <		-	9 5	3 5	17	•	90/77	1 7 1	3 8	00.7	•		200	3 5	700	•	14,011 w 5am	¥ .3	
120 124	1201 334 234 <td></td> <td></td> <td>35</td> <td>3 6</td> <td>70/</td> <td></td> <td>40/047</td> <td></td> <td>5 S</td> <td>3 6</td> <td>• •</td> <td></td> <td>900</td> <td>37.6</td> <td>š Ę</td> <td>2</td> <td>14.00+ W BBIN</td> <td>د بد</td> <td></td>			35	3 6	70/		40/047		5 S	3 6	• •		900	37.6	š Ę	2	14.00+ W BBIN	د بد	
1352. 121. 122. 123. 124. 124. 125.	1373. 1376. 2376. 137. 237. 137.			1000	77.X	250		246/GB	- 1	200	8		•	. 88	, y	1 6		14.036 W.Ban	د ۲	
135.25 156.5 151	135.0.2 137.		-	26.2	1014	32.	. •	248/CB	,00		, , ,	•	•	9	Š	1 6	280	12 861 W Par	• 3	
1,502.2 790 241 248/GB	15623 790 241 248/GB 1196 0.05 216 99.15 281 11965 3389 674 271 27			3383	1676	511	1	247/GB	1.19		131			29	3.435	385	28	13.573		
1415 131	13751 418 127 247/G8 119 003 131 9719 275 117.34 3323 385 156 14452 1318 602 247/G8 146 900 173 9719 273 132 373 385 156 14452 1318 602 247/G8 136 004 178 9231 253 1373 385 179 15545 244 108 249/G8 136 004 158 9231 253 138 237 138 136 249/G8 136 005 158 875 248 105 231 360 248 136 136 005 158 875 248 137 136 136 136 136 136 136 136 136 136 136 136 136 136 136 136 137 136 137 136 137 136 137 136 137		_	3673	8	241	- "	248/GB	8	- 1	2.16		-	9.65	3.389	674	273	13.417 W Ban	<u> </u>	
14152 1318 402 237/GB 147 0.04 165 960 27.2 115.9 3.28 442 179 14861 231 688 248/GB 136 0.04 178 94.53 2.8 114.8 3.28	1415Z 1318 402 247/GB 147 004 162 560 272 115.9 3.254 442 179 14881 239 68 248/GB 136 005 178 94.25 28 136 3.25 111.85 3.25 3.15 3.25 120 150 150 140 3.25 111.85 3.25 3.15 3.25 3.15 3.25 3.15 3.25 3.25 3.15 3.25			3751	418	127	-•	247/GB	1.15		1.31	`		7.34	3.323	385	156	3.144 W Ban	4	
(488) 298 288/GB 1,62 0.06 1,78 94,93 2.68 114,08 3.231 568 29 15545 234 36 246/GB 1,54 0.04 1,50 0.04	14851 2991 688 288/GB 162 0.05 178 94.52 2.68 11.86 3.21 5.88 29.0 15564 224 1.6 0.04 1.5 0.04 1.5 1.0 3.21 5.8 20.0 15564 224 1.0 224/GB 1.5 0.04 1.5 2.9 1.6 1.0 2.9 1.0 1.0 2.9 1.0 1.0 2.9 1.0 1.0 2.9 1.0 1.0 2.9 1.0 1.0 2.9 1.0 1.0 2.9 1.0 1.0 2.9 1.0 </td <td></td> <td>></td> <td>4152</td> <td>1318</td> <td>402</td> <td>. •</td> <td>247/GB</td> <td>1.47</td> <td>٠.</td> <td>1.62</td> <td>_</td> <td></td> <td>5.95</td> <td>3.284</td> <td>42</td> <td></td> <td>12,988</td> <td></td> <td></td>		>	4152	1318	402	. •	247/GB	1.47	٠.	1.62	_		5.95	3.284	42		12,988		
15555 11	1,555.5 3.1 9 228/GB			4851	2291	869		248/GB	1.62	-	1.78		_	4.08	3.231	268		12,809 W Ban	ب د	
15545 2246 663 249/CB	15545 2246 663 249,CB 164 0.05 1.80 91.55 2.59 10.65 3.125 5.25 2.19 2.15 2.1			4860	31	6		248/GB	1.36	800	1.50	•		1,86	3.168	320		12,580		
15555 34 10 247/0B 124 245 2	15555 34 10 2477GB 2.35 0.07 2.60 89.91 2.55 108.14 3.062 5.42 219 12.238 15.64 2.49/GB 1.18 0.05 1.99 2.49/GB 1.18 0.05 1.99 2.4			5545	2246	589		249/CB	Z.	000	08:1			0.36	3.125	525		12,450		
15766 681 208 249/GB 181 0.05 159 87.55 2.48 105.55 2.989 664 244 12.018 1658 2.219 165	15766 181 208 249/GB 181 10.05 1.99 15.55 248 105.55 2.989 664 244 12.018			5555	34	01		247/GB	2.36		5.8	•		8.14	3.062	\$		12,238		
1576 19 6 249/GB	1576 19 6 259/GB 1.78 0.05 136 55.74 2.45 105.42 2.873 360 227 11.74 1578 19 6 259/GB 1.78 0.05 134 55.05 2.8 101.46 2.873 344 155 11.57 1750 1751 182 251/GB 1.18 0.05 134 55.05 2.8 274 2.4 351 1.29 1751 1752			5763	8	208	. •	249/GB	1.81		8			5.53	2.989	Š	4	12,018		
10008 2721 823	1500 272 229 220			5769	6]	\$	'	249/GB	32.1	0.00	8:			3,42	2.929	88	727	11,774		
17200 1775 602 231/GB	17200 1975 602 251/GB 2.11° 0.00 1.29 82.74 2.34 99.63 2.82 75 297 11.392 17975 189 53 21/GB 1.10° 0.00 1.99 82.74 2.34 250			8	2721	873	- '	220/08	7	0.03	4	•	-	8	7.873	584	155	747		
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24875 1373 418 228/GB 0.95 0.03 1.05 51.71 1.46 61.36 1.738 3.25 132 7.255 2.22 677 258/GB 0.95 0.03 1.05 50.71 1.46 61.36 1.738 3.25 132 7.255 2.2552 272 677 258/GB 0.95 0.03 1.05 50.76 1.44 60.13 1.703 3.35 136 7.123 2.556/GB 1.53 0.04 1.68 49.81 1.41 58.79 1.665 487 1.97 6.987 5.596 1022 312 256/GB 1.81 0.05 1.99 48.28 1.37 57.09 1.617 621 251 6.790 2.568 8.173 5.3 257/GB 2.40 6.40 1.35 5.45 1.557 767 310 6.539 2.558 8.173 5.3 2.567/GB 2.40 6.40 1.35 5.45 1.557 767 310 6.539	24875 1373 418 228/GB 0.95 0.03 1.05 5171 146 61.36 1.738 325 132 7.255 25552 2222 677 228/GB 0.95 0.05 1.05 50.76 1.44 60.13 1.703 335 136 7.125 25594 138 42 226/GB 1.53 0.04 1.68 49.81 141 58.79 1.665 487 197 6.987 25966 1022 312 256/GB 1.81 0.05 1.99 48.28 137 57.09 1.617 621 251 6.790 25958 173 53 257/GB 2.18 0.06 2.40 46.47 1.32 54.97 1.557 767 310 6.539 274-86 5011 1527 257/GB 1.92 0.05 2.11 44.29 1.25 5.255 1.488 665 259 6.229			8	9/7!	389		256/CB	2.17		2.39	53.88		3,92	1.810	45	5	7,556 US Aid		
2552 2222 677 258/G8 0.95 0.05 1.05 50.61 1.44 60.13 1.703 335 136 7.123 25594 138 42 256/G8 1.53 0.04 1.68 49.81 1.41 58.79 1.665 487 197 6,987 25906 102 312 256/GB 1.81 0.05 1.99 48.28 1.37 57.09 1.617 621 251 67.90 256/GB 1.83 0.05 2.40 48.28 1.37 57.09 1.617 621 251 67.90 256/GB 1.83 0.05 2.40 48.28 1.37 767 310 6.539 256/GB 1.61 6.21 48.28 1.35 54.97 767 310 6.539 256/GB 1.62 7.62 48.47 1.35 767 310 6.539 256/GB 1.62 7.62 48.47 1.35 48.47 <	2552 2222 677 258G8 0.95 0.05 0.05 1.05 50.76 1.44 60.13 1.703 335 136 7.123 25594 138 42 256G8 1.53 0.04 1.68 49.81 141 58.79 1.665 487 197 6.987 25966 1022 312 256GB 1.81 0.05 1.99 48.28 137 57.09 1.617 621 251 6.790 25958 173 53 257/GB 2.18 0.06 2.40 46.47 132 54.97 1.557 767 310 6.539 277486 5011 1527 257/GB 1.92 0.05 2.11 44.29 1.25 52.55 1.488 665 259 6.229			573	1373	418	•	258/GB	0		80.	51.71		36	1.738	35	32	7.255 W Ban	.	
25594 138 42 258/GB 1.55 0.94 1.68 49.38 1.41 58.79 1.665 487 197 25906 1022 312 256/GB 1.81 0.05 1.99 48.28 1.37 57.09 1.617 621 251 25958 1.73 53 257/GB 2.18 0.06 2.00 6.47 1.32 54,7 1.557 767 310 77.88 711 723 54,7 1.557 767 310	25594 138 42 258GB 1.55 0.05 1.68 49.38 1.41 58.79 1.660 48.7 197 25906 1022 312 256GB 1.81 0.05 1.99 48.28 1.37 57.09 1.617 621 251 25958 173 53 257GB 2.18 0.06 2.40 46.47 1.32 54.97 1.557 767 310 27486 5011 1527 257/GB 1.92 0.05 2.11 44.29 1.25 52.55 1.488 665 269		11	2222		779		2868	0.93		83	20.76		0,13	1.703	333	8		.	
25958 1022 512 259CB 1.83 0.05 1.99 48.28 1.57 57.09 1.617 621 251 251 25558 173 53 257CB 1.218 0.06 2.0 46.47 1.32 5497 1.557 767 310 27.88 (311 1527 767 10.0 0.06 2.0 46.47 1.32 5497 1.557 767 310	25968 173 53 257/CB 1.81 0.05 1.99 48.28 1.37 57,09 1.617 621 251 251 251 251 251 251 251 251 251 2		4,	300	82.	74.		2000			86.	8.69		2 (3	587	161	786,0		
255 1/5 25 22/108 218 0.00 2.40 46.47 1.52 54.77 1.557 310 27.08 2.40 46.47 1.52 54.77 1.557 310	25958 175 25 25/1/OB 2.18 0.00 2.40 40.97 1.52 54.97 1.557 767 310 277486 5011 1527 257/CB 1.92 0.05 2.11 44.29 1.25 52.55 1.488 665 269		* •	83	25	512	•	256/GB	8 6		85	48.28		8 8	1.617	25 }	รร	6,790		
	4,450 5011 1541 (2)/106 1.52 0.03 2.11 44,29 1.25 52,53 1,488 003 209		41	37.00	· ;	503.	. •	22//58	7.7		9:	750.47		7,4	755	0	310	6,539		

Table B - 1 (2/3) Breakdown of Authorized and Design Discharge Calculation for LCC Area

592 240 5,846 w Bank 880 356 5,607 384 155 5,250 w Bank 501 3,095 490 198 4,892 430 4,520 408 165 4,240 233 94 4,075 Us Aid 332 123 3,881 Us Aid 305 123 3,846 469 190 2,219 577 234 2,029 421 170 1,796 425 170 1,796 436 229 949 566 229 949 566 229 949
240 5,846 w Bank 256 5,807 w Bank 256 5,807 w Bank 256 6,807 w Bank 256 6,807 w Bank 256 6,807 w Bank 256 6,809 w Bank 256 6,809 w Bank 256 6,809 w Bank 256 6,809 w Bank 256 6,809 w Bank 256 6,809 w Bank 256 6,809 w Bank 256 6,809 w Bank 256 6,809 w Bank 256 6,809 w Bank 256 6,809 w Bank 256 6,809 w Bank 256 6,809 w Bank 256 6,809 w Bank 256 6,809 w Bank 256 6,800 w Bank 256 6,
284 155 5.250 W Bank 490 198 5.095 W Bank 430 174 4,694 408 165 4,520 408 165 4,520 332 134 3,981 US Aid 357 15,504 3,723 469 190 2,219 577 234 2,029 421 170 1,766 425 172 1,625 439 178 1,453 560 227 1,176 566 229 949 385 156 720
430 174 4,694 692 280 4,520 408 165 4,520 233 94 4,075 US And 332 134 3,981 US And 332 134 3,981 US And 3716 1,504 3,723 469 190 2,219 577 234 2,029 421 170 1,796 429 172 1,625 246 100 1,796 439 178 1,354 560 227 1,176 566 229 949 385 156 720
408 165 4,240 233 94 4,075 US AND 352 134 3,881 US AND 367 123 8,846 577 234 2,029 421 170 1,796 425 172 1,625 439 178 1,453 560 227 1,176 566 229 949 385 156 720
332 134 3,881 US Aid 3,716 1,504 3,723 469 190 2,219 577 234 2,029 425 170 1,796 425 170 1,455 560 227 1,176 566 229 949 385 156 720
3.716 1,504 3,723 469 190 2,219 577 234 2,029 421 170 1,796 245 172 1,625 439 178 1,354 560 227 1,176 566 229 949 385 156 720
556 556 556 556 556 556 556 556 556 556
246 170 246 170 246 170 566 227 356 227 358 229
256 227 258 227 258
560 560 560 560 560 572 573 573 573 573 573 573 573 573 573 573
385 229 385 229 385 156
385 156

Table B - 1 (2/3) Breakdown of Authorized and Design Discharge Calculation for LCC Area

Name Color	No. Watercourse No.			************	c	Village	Chak No.		Owlet Disharge	- Pgc	Section	Design	'	ŭ		۱,	Project	Remarks
194GB	onal)	(læt)	Ē	Distan	g (£			Auc			23.4	Discha	13				overnent)	
154/GB	904 15561/R	15561	4743	4151	1265		194/CB	1.	1	Ι.	1_	3.13	0.089	365	1	386		
1924 0.54 2379 0.679 331	905 18989/R	68681	5788	3428	1045		154/GB	11		1.72	1.56 0.04	1.78	0.050	538	218	218 W Ban	-4	
154/GB		:						27.						9438 3,819				
154/03	a Distributary																	
154/08 1.60 0.05 176 1924 0.54 25.97 0.679 477 201 160/08 1.19 0.05 1.31 16.44 0.47 18.95 0.679 477 201 160/08 1.19 0.05 1.31 16.44 0.47 18.95 0.444 393 11.95 15.00 150/08 1.19 0.05 1.31 16.44 0.47 18.95 0.444 393 11.95 15.00 150/08 1.14 0.05 1.25 12.93 0.37 14.45 0.442 393 11.95 0.47 14.65 0.444 393 11.95 150/08 1.12 0.05 1.23 12.93 0.37 14.65 0.444 393 11.95 150/08 1.12 0.05 1.24 0.47 14.05 0.444 393 11.95 150/08 1.12 0.05 1.24 0.43 10.12 4.74 0.134 1.540 150/08 1.10 0.05 1.24 0.47 4.31 0.12 4.74 0.134 1.540 150/08 1.40 0.04 1.54 1.540 1.24 0.47 0.134 1.540 150/08 1.40 0.04 1.54 1.540 1.24 0.47 0.134 1.540 150/08 1.40 0.04 1.54 1.540 1.24 4.74 0.134 1.540 150/08 1.40 0.04 1.54 1.540 1.24 4.74 0.134 1.540 150/08 1.40 0.04 1.54 1.540 1.24 4.74 0.134 1.540 150/08 1.40 0.04 1.54 1.540 1.24 4.74 0.134 1.540 150/08 1.40 0.04 1.54 1.540 1.240 4.47 0.134 1.540 150/08 1.25 0.04 1.58 1.53 0.34 1.44 0.409 4.42 1.79 150/08 1.25 0.04 1.58 1.53 0.34 1.44 0.409 1.44 1.540 150/08 1.25 0.04 1.54 1.540 1.107 0.313 1.540 1.44 1.540 150/08 1.20 0.04 1.24 1.540 1.32 1.243 1.44 1.540	•	7 m								:						2,693		£
160/GB	1906 23665/R	23665	7213.	23665	7213		154/GB	ĭ	١.	1.76	l -	23.97	6.679			2,693 W Ban	**	
600GB 119 0.03 131 1644 047 1855 0537 411 156		25567	7793	205	580		160/GB	2		1 32	_	20.41	0.578			2,492 W Ban	.	
159/GB		29049	\$854	3482	18		160/GB	Ξ.		131	-	18.95	0.537			2,321 W Ban	-3	
159/GB		31100	9479	205	625		160/GB			3		17.41	0.493			2,155 W Ban	-33	
159/QB		32443	6886	1343	603		159/GB	⊒		1.25		15.97	0.452			986.		
162/GB			9828	-700	Įφ	٠	159/GB	7		. 1.23		14.63	0.414			1,833 W Ban	4	
182/GB			10608	2561	781		162/GB	-		1.49		13.41	0.380			1,674		
163/CB		. :	10992	1258	383		162/GB	1		7		11.78	0.334			1,485 W Ban	*	
163/GB	1914 36970/R		11268	Š	277		163/GB	8		0.77		10.37	0.294			1,311 W Ban	-31	
162/GB	1915 38266/R		11663	1296	395		163/GB	~		1.14		926	0.271			1.211 w Ban	*	
162/GB	1916 40643/TL		12388	2377	725		162/GB	=		1.97		8.35	0.237			1.062		
155/08	1917 40643/TR		12388	0	0		162/GB	71		3.		6.28	0.178			808		
1510 043 1510 044 1510 045 1510 055	1918 40048/17		88621	٥	O		162/GB	*	- 1	4.74		4.74	0.134			710		
1510 0.45 17.90 0.507 4.95 200 155/08 1.41 0.04 1.55 15.10 0.43 17.90 0.507 4.95 200 155/08 1.30 0.04 1.43 13.69 0.39 15.95 0.452 457 185 155/08 1.25 0.04 1.38 12.39 0.35 14.44 0.409 4.42 179 1.55/08 1.05 0.09 1.12 0.04 1.27 0.31 0.361 2.77 1.07 0.31 0.36 1.45 0.05 1.76 8.62 0.24 9.83 0.278 8.62 227 1.57/08 1.75 0.05 1.75 8.62 0.24 9.83 0.278 8.62 227 1.57/08 2.52 0.07 2.77 2.52 0.07 2.77 0.079 8.90 360 1.58/08 2.52 0.07 2.77 2.52 0.07 2.77 0.079 8.90 360 3.65/08 1.51/0 0.43 2.52 0.07 2.77 2.52 0.07 2.77 0.079 8.90 360 3.65/08 1.50 0.08 2.27 136.97 3.88 184.97 2.23 2.153								16.		** **		:			. 693			
155/G8	vala Minor (RD	11235/R	Yaniw	ala Dig	(ributary)						2.8				:			
5980 1823 5980 1823 5980 1823 1557GB 141 0.04 1.55 15.10 0.43 17.90 0.507 495 200 7270 2216 1290 393 1557GB 1.30 0.04 1.31 1.59 0.59 1.59 6.59 4.42 1.79 1.59 4.42 1.79 0.50 4.42 1.79 1.59 4.42 1.79 0.59 1.59 4.59 1.59 4.42 1.79 0.59 4.42 1.79 1.59 4.42 1.79 0.59 1.59 1.59 0.59 1.59 0.59 1.59 1.59 1.59 0.59 1.59 1.59 0.42 3.59 1.59 0.42 3.59 1.59 0.42 3.59 1.59 0.42 3.59 1.59 0.42 3.59 1.59 0.42 3.59 1.59 0.42 3.79 1.59 1.59 0.42 1.79 0.42 1.79 1.59 1.59 <td< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>1</td><td></td><td></td><td>i .</td><td></td><td></td><td></td><td>2,153</td><td></td><td></td></td<>									1			i .				2,153		
7270 2216 1350 393 155/GB 130 0.04 1.43 13.69 0.39 15.95 0.452 457 187 12560 3550 1734 157/GB 1.25 0.04 1.38 1.39 0.39 15.95 0.452 447 187 1366 4013 4013 229 701 157/GB 1.05 0.04 1.58 11.14 0.409 442 179 147 150	1919 5980/L	0869	1823	9869 9869	1823		155/GB	-		1.55		17.8 8.71	0.507	495	ı	2,153 W Ban	×	
12960 3950 5660 1734 157/CB 125 0.04 1.38 12.39 0.35 14.44 0.409 442 179 13167 4013 207 65 155/CB 1.50 0.05 1.65 11.14 0.32 12.73 0.361 527 213 156/CB 1.50 0.05 1.75 8.62 0.24 9.83 0.278 562 227 128 156/CB 1.50 0.05 1.76 8.62 0.24 9.83 0.278 6.15 249 157/CB 1.50 0.05 1.76 8.62 0.24 9.83 0.278 6.15 249 157/CB 1.50 0.05 1.75 0.05 1.93 702 0.20 8.05 0.228 6.16 249 156/CB 1.56/CB 0.54 0.02 0.70 5.27 0.15 6.05 0.171 2.26 9.1	• /	7270	2216	28	393		155/GB			1.43		15.95	0.452	457		1.952 w Ban	¥	
13167 4013 207 653 155/GB 150 0.04 1.65 11.14 0.32 12.73 0.361 527 213 155/GB 1.50 0.03 1.12 9.64 0.02 11.07 0.313 3.60 146 1.229 701 1.57/GB 1.02 0.03 1.12 9.64 0.02 1.03 3.23 0.278 616 2.22 1.00 2.32 1.00 2.22 1.00 2.22 2.23 2.2		12960	3950	2690	32		157/CB	7		1.38		14,44	0.409	4		1,767 US Aid	73	
15466 4714 2299 701 1577GB 1.02 0.03 1.12 9.64 0.27 11.07 0.313 360 146 15900 4846 474 132 156/GB 1.60 0.05 1.76 8.62 0.24 9.83 0.278 562 227 275 256 0.24 258 277 258 278 258 278 258 278 258 258 278 258		13167	5013	201	જ		155/CB	<u> </u>		8		12.73	0.361	22,		1,589		
15900		25.5	4714	223	5		157/GB	ĭ		112		1.07	0.313	8		1,375 US Aid	5+W Bank	
17004 5360 1704 170		15900	98	4	132		1SevGB	~ ;		2.5		9.83	0.278	262		222	. !	
25087 6153 2585 787 185 78		17604	5368	3	519		157/GB			1.93		8.05	0.228	919		1,002 US Aid	3+W Bank	
25000 7620 4813 1467 158/GB 2.11 0.06 2.32 4.63 0.13 5.25 0.149 744 301 661 25000 7620 0 0 158/GB 2.52 0.07 2.77 0.079 890 360 <td></td> <td>20187</td> <td>6153</td> <td>2583</td> <td>181</td> <td></td> <td>156/GB</td> <td>ö</td> <td></td> <td>0.70</td> <td></td> <td>6.05</td> <td>0.171</td> <td>22</td> <td></td> <td>753 W Ban</td> <td>.</td> <td></td>		20187	6153	2583	181		156/GB	ö		0.70		6.05	0.171	22		753 W Ban	.	
500 152.4 500 15.10 0.43 136.97 3.88 2.153 2.153 500 152.4 500 15.2 10.0 136.97 3.88 184.97 5.238 725 293 13850 4221 13350 4669 360/GB 1.90 0.05 2.09 134.91 3.88 184.97 5.238 725 293 18164 552.8 4.221 1350 3.0 136.97 3.88 184.97 5.238 725 293 18164 552.8 4.287 1307 13.004 1.44 130.01 3.67 177.20 5.018 2.50 101 18300 573 13 4.1 1.30 1.44 130.01 3.64 177 5.0 101 18300 579 4.1 1.30 1.44 130.01 3.64 1771 4.35 121 121 121 121 121 121 121 121 121 12		2,000	7620	. C	794		158/GB	616		232		, 1	0.149	<u>\$</u> \$	<u> </u>	ool w Ban	**	
500 152.4 500 152.4 500 152.4 500 152.8 725 293 13850 4221 13350 4669 360/GB 150 0.05 2.07 136.97 3.88 184.97 5.238 725 293 18157 5528 4221 13350 4669 360/GB 1.90 0.05 2.09 134.91 3.88 184.97 5.238 725 293 18164 5528 4221 1370 137 177.20 5.018 250 101 18300 5578 13 41 130.01 1.44 130.01 3.64 177.20 5.018 250 101 18300 5578 13 41 1.30.01 1.44 130.01 3.64 1771 4.854 200 81 19000 579 13 1.00 1.00 2.64 128.03 3.54 1779 53 21 19000 579 13		2000	200				00000	15.	١	7,77	J	1,1	200		2153	35		
500 152.4 500 152.4 500 152.4 500 152.3 725.238 725.238 725.293 13850 4221 13350 4669 360/GB 190 0.05 2.09 134.91 3.88 184.97 5.238 725.293 18137 5528 4221 13350 4669 3.60 13.00 3.01 134.91 3.88 184.97 5.238 725 293 18164 5528 4287 1307 8 1300 3.01 3.44 130.01 3.68 172.86 4.895 239 97 18300 5574 41 2.40 0.07 2.64 138.01 3.64 171.41 4.854 239 97 19000 579 700 213 2.41 0.07 2.64 128.03 3.56 1774 4.379 4.779 53 21 19000 579 8300 213 256.0GB 0.60 0.02 0.06																		
500 152.4 500 152.4 500 152.7 3.88 184.97 5.238 725 293 13850 4221 13350 4669 360,005 2.07 136.97 3.88 184.97 5.238 725 293 18137 5528 4287 1307 669 3.30 134.91 3.82 1371 663 268 18137 5528 4287 1307 8 130 134.91 3.82 1371 663 268 18164 5556 27 136.97 3.40 134.91 3.64 1372 5.018 250 101 18000 5536 41 240 0.07 2.64 1714 4.854 200 81 19000 500 571 560 1.26 12.66 17.66 17.67 4.779 53 21 1000 513 350 536 1.26 12.56 13.56 16.50 4.674	hal Distributar	>																
560/L 500 152.4 500 152.4 500 152.4 500 152.4 500 227 136.97 3.88 184.97 5.238 725 293 138.50/L 13850 4221 13550 4669 360/GB 1.90 0.05 2.09 134.91 382.88 5.171 663 268 1813.7R 1813.7 552.8 4287 1307 1307 130 137 177.20 5.018 268 101 1816.4R 1813.7 553.8 428 130 2.00 134.91 3.82.88 5.171 663 268 1816.4R 1813.7 553.8 43 137 177.20 5.018 20 101 1816.4R 1813.6 43 43 43 43 43 44 43 44 43 44 44 44 44 44 44 44 44 44 44 44 44 44 44 44 </td <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>٠.</td> <td>=</td> <td>3.242</td> <td></td> <td></td>														٠.	=	3.242		
1385QL 1385Q 4221 1335Q 4669 360/GB 1,50 0.05 2.09 134.91 3.82 187.11 663 268 18147/R 18137 5528 4287 1307 360/GB 3.0 134.01 3.77 177.20 5.018 250 101 18164/R 18154 41 24 0.04 1.44 130.01 3.68 4.895 239 97 18164/R 18164 1.36 41 2.40 0.07 2.64 128.70 3.64 1895 239 97 1830AL 1836 2.71 4.1 2.40 0.07 2.64 128.70 3.64 187 4.854 230 81 1970OR 500 213 5.64 0.07 2.64 128.70 3.66 175.4 4.79 3.7 1.75 4.39 1.7 1870OR 5.03 5.03 5.84 1.07 2.64 1.28.70 3.49 165.05		88	152.4	8	152			5	١.	1	1	184.97	5.238	725	ı	3,242		
18137/R 18137 5528 4287 1307 300 0.08 3.30 133.01 3.77 17720 5.018 250 101 18164/R 18164 5536 27 8 1.31 0.04 1.44 130.01 3.68 172.86 4.895 239 97 18300L 1836 27 8 41 2.40 0.07 2.64 128.70 3.64 171.41 4.854 200 81 19000R 1900 213 2.40 0.07 2.64 128.70 3.64 171.41 4.854 200 81 19000R 1900 213 2.40 0.07 2.64 128.70 3.64 4.779 53 21 18700R 1900 213 236/GB 0.64 0.07 2.64 126.83 3.67 4.779 53 21 28000R 213 8300 914 236/GB 0.67 0.07 126.63 3.47 162.4		13850	4221	13350	4069		360/GB	\$1				182.58	5.171	8		7,948		
18164R 18164 S55 27 8 1.31 0.04 1.44 130.01 3.68 172.86 4.895 239 97 18300L 18300L 18300 5578 136 41 2.40 0.07 2.64 128.70 3.64 171.41 4.854 200 81 19000R 19000 5791 700 213 0.64 0.02 0.70 126.30 3.58 168.74 4.779 53 21 19700R 19700 6005 700 126.30 3.58 168.74 4.779 53 21 28000R 213 236/GB 0.60 0.02 0.66 125.35 3.6 167.87 4.779 53 178 28000R 213 236/GB 0.60 0.02 0.66 122.25 3.47 162.45 4.601 237 96 31000 9449 3000 914 252/CB 1.11 0.03 1.22 121.98 3.45	18137/R	18137	5528	4287	1307);;	1			177.20	5.018	প্ল		089'		
18300L 18300 \$578 136 41 2.40 0.07 2.64 128.70 3.64 171.41 4.854 200 81 19000R 1900 5791 700 213 2.40 0.07 2.64 0.02 0.70 126.30 3.58 168.74 4.779 53 21 19700R 19700 6005 700 213 2.41 0.07 2.65 125.66 3.56 167.87 4.779 53 21 28000R 2530 2530 2530 2536/GB 0.67 0.02 0.07 125.65 3.49 165.05 4.674 2.11 85 31000R 31000 9449 3000 914 536/GB 0.67 0.02 0.74 122.65 3.47 162.45 4.601 237 96 36992R 36992 1127 359 161.02 2.502/GB 1.11 0.03 1.22 121.98 3.45 161.02 4.560 366	18164/R	18162	5536	27	00		٠					172.86	4.895	239		579		
19000/R 19000 5791 700 213 0.64 0.02 0.70 126.30 3.58 168.74 4.779 53 21 19700/R 19700 6005 700 213 2.41 0.07 2.65 125.66 3.56 167.87 4.779 53 21 28000/R 2300 8534 8300 2530 836 836 83 84 165.05 4.674 211 85 31000/R 31000 9449 3000 914 836/CB 0.67 0.02 0.74 122.65 347 162.45 4.601 237 96 36992R 36992 1127 5992 1826 262/CB 1.11 0.03 1.22 121.98 3.45 161.02 4.560 366 148	18300/L	18300	5578	136	4		-					171.41	48.84	Š		7.482		
19700/R 19700 6005 700 213 254 607 2.65 125.65 3.56 135.65 3.56 178 4.754 4.39 178 28000/R 2800 8534 8300 2530 536/GB 0.60 0.02 0.66 123.25 3.49 165.05 4.674 211 85 31000/R 31000 9449 3000 914 536/GB 0.67 0.02 0.74 122.65 3.47 162.45 4.601 237 96 36992/R 36992 1127 5992 1826 262/GB 1.11 0.03 1.22 121.298 3.45 161.02 4.560 366 148	19000/R	0006	5791	Ş	213			ič				168.74	4.770	Ç		1.401		
28000/R 28000 8534 8300 2530 536/GB 0.60 0.02 0.66 123.25 3.49 165.05 4.674 211 85 31000/R 31000 9449 3000 914 536/GB 0.67 0.02 0.74 122.65 3.47 162.45 4.601 237 96 36992/R 36992 11275 5992 1826 262/GB 1.11 0.03 1.22 121.98 3.45 161.02 4.560 366 148	19700/8		Š	8	213					-		1,50	4754	430		7.380		
31000/R 31000 9449 3000 914 536/GB 0.67 0.02 0.74 122.65 3.47 162.45 4.601 237 96 36992/R 36992 11275 5992 1826 262/GB 1.11 0.03 1.22 121.98 3.45 161.02 4.560 366 148			8834	Š	0.50		S36/CB	i è				30.54	A 6.74	} :		202		
36992R 36992 11275 5992 1826 262/GB 1.11 0.03 1.22 121.98 3.45 161.02 4.560 366 148			0440	Ş	710		90/90	Šè				16.05	1 5	334		7 1 15		
041 050 DOC+ 40101 Care octivity and the control of		•	776	600	763		00000	š -			- :	1,51	3 5	38	-	100		
	44100		7.41	1111	0701		2000	3			-	101.01	3	3		170.		

Table B - 1 (2/3) Breakdown of Authorized and Design Discharge Calculation for LCC Area

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ė,	No. Watercourse No.	2	3	Section		ViHage	Chak No	i	Authorized	TEN ST	و ا	Discharge		Discharge	١	(acre)	[-	5	
	(mugum)] }	9] [! :	(cusxc)	ا انوا	l _e	(cusec) (m3s)	(casec)	() ()	<u> </u>				
=	1224 42122/R	42122 13	2839	٥	3		263/GB		80	50.0		ł		Ĺ	4,486	297		16,872	
2	1226 45749/R	_	384	3627	138		263/GB		1,43	S.				56.21	.424	355	<u> </u>	6,752	
	45800/R	_	3960	ŝ	91		263/GB		-	20.0	11 69			53.81	1356	528		609'9	
ŭ	1229 49600/R	9800	5118	88	1158		264/GB		3.26	800		10.98 5.51			835	062	\$ 8	5,933	
: 3	471.50 CC I	-	07770	02321	3 5		20/59¢							8	7604	410		5.542 W Bank	
1 1			2002	388	719		85/099				191					869	7		
		• • •	30446	8	354					_			_	37.88		2,501	1,012	5,093	Thera Minor(8.02)
	68455/R	•	50802	1375	419				_	_	5.80 10					4,491	~~	14,081	MagneJa Minor(15.8)
	68560/R	٠,	0897	105	33						_	_	_	13.53		8	19	2,263	
<u>%</u>	-	•	\$1012	398	121		664/GB		_			~		112.27	3.179	Ł	261	12,102 W Bank	
6	•		(359	1118	ž		85/099							10.18	20	63		[tx]	
ឧ	٠.	ď	2043	2245	884		660/GB			200	_	83.93 2.38		08.53	3.074	457		11,633	
5		78584 2	3952	6263	8	÷	771/CB			0.03	۸1		_	89.0	3.021	33	3		
8		•	2821	6132	1869		661/GB		1.70	0.05	8.		2,31 10	18.52	98	573	232		
X	1238 88890/R	` •	7094	4174	1272		661/GB			3	<u>ب</u>	_		45.	2.876	4	5/	11,106 W Bank	
8		٠.	27203	38	011		67%/CB		 					99.33		574	232	10,927	
	89320/R		27225	2	7			-			_			7.47		1,620	£,703	0.695	Junegwala Ninor(41.74
Ė	1242 91240/R	• •	27810	1920	282		85/699	.*	_			_		55.72	578	224	212	5,992	
83			28512	2303	702		678/GB			0.05	_		_	53.84	1.525	230	217	5,780	
દ્ધ		•	29895	4537	1383		678/GB		3.		_	_	1.15 5	1.78	394.1	276	33		
ይ	1243 99192/R	``	30234	1112	339		679/GB		1.72	0.05	_		_	49.42	8	85 8	3	5,330 W Bank	
æ.	1244 102584/R	•	31268	3392	1034		679/GB		1.3	0.05				4 .	55	623	252	2,090	
32	1245 107058/R		1292	4474	1364		85/089		1.41	40.0		35.37 1.	_	45.06	1.276	\$	8		
33	1246 111631/R	6-1	34025	4573	1394		680/GB		1.45	\$	_		_	8	1.218	210	8	4,637 W Bank	
	112614/R	£47,	4325	983	8				5,47	5.7				40.91	1.159	1.994	3	4,431	Jandwala Minor(6.36)
¥.	•	,	4722	1303	397	:	681/GB		1.69		•		0.77 3		3.975	86	55	3,624	
35	1248 115000/L	•-•	35052	1083	0		719/CB		0.86						0.919	36	2		-
9.	1249 119000/L	•	8627.	8	1219		719/GB		0.72	j					6887	252	8	3,261 W Bank	
33		٠.,	718	2930	863	:	720/GB		4			23.77	0.67		0.857	24.5	219	3,159	
<u>8</u>	1250 121985/R	•	7181	\$	17		681/GB		1.85	.03					2.801	617	3	340	
	-		38225	3	<u>\$</u>		720/GB-	1	100						5,743	5 8	ξ	007.6	
<u>.</u>	··· ·	• • •	2875	65.5	2 6		807780			\$ 8 5 6		90.00			1 V C V C	ŝ	35	7.480	
₹ ₹	125 126250K	2 07.2021	2834	5740	1750		687/CB		3 5		3.5			20.52	0.581	551	223	2,249	
3			0835	7	-		688/GB		2.16	,		. 1			0.521	758	307	2,026	
4			13631	9175	2797		684/GB		 69:		1.63				0.454	220	210	61,719	
. 4	'	-4	5	635	498		684/GB			500					.1650	551		1,509	
4	1258 144854/L		4151	Ę	H		686/GB			0.05				12.01	0.340	572	231		
\$	_	- 1	45702	88 90 88	1551		685/CB	-		500	69			0.22	0.289	ž	22	1.277 W Bank	
47	-		5709	21	9		685/GB	: ·	1.12	0.03	123		77	8.28	0.235	36	8	1,049	
3		- T	460%4	1232	376		685/GB		8	0.03	90		∞ :	7.05	0.700	414	89	589 W Bank	
44			46086	S	Ċŧ		688/GB		1.72	0.05	68		4 5	5.70	1910	§ :	245	121	
8	1263 156082/TR	1	47574	4882	1488		688/GB		127	3 8	- - - - - -	% c	88	3.81	0.108 0.108	4 t	8 §	9/5 500	
; 	1204 15008/2/11:	1200021	4/0/				0000		70.7	330	07.7		3	07.7	. I	3 3	C77.0	27.0	
							:		70.051	00.0				:	-	18.695	# L		
				I															

Table B - 1 (2/3) Breakdown of Authorized and Design Discharge Calculation for LCC Area

	Remarks																											•													
	Project (Improvement)										V Bank																			- 10 / C	- Count	W Bank								V Bank	W Baok
	Feit SCC Section	(ha)	1.012	010	8	2 2	ž ž			1,818	1,818.1	3 %	31	385	1,22,1	8	82	ŝ	7 ç	32			4,703	4,703	4,479	4,522	3.818	3,532	3,249					2,397	2,268	3,5	770	1.633	1,473		
	٦			187	88	ò	3 4	1.012			115	} ⊽	2 4	145	236	8	<u> </u>	ŝ	38	5 22	818.			224	157	8 8	82	282	8	9 6	115	119	185	23	138	\$ \$	53	191	159	221	224
	Outlet CCA (acre) (hi			46.3	323	÷ (88	2,501			82 X	2 }	36.	358	583	492	313	ç ç	\$ \$	38	1,817			553	888	6 8 8	38	869	252	617	3,2	292	457	350	¥ ;	8 8 8	3 8	397	38	246	553
	ı	34)	٠.		0.185						0.447						Ė							182	929	1.073	8	871	38	707	8	28	8	565	532	9 9	413	377	337	0301	222
	Discharge	(m34)	, .	Ĺ	6.55						0 08.51																														
		Ü	. 0	l											_											35.91									_	_					
	Section Discharge	(cusec) (m3s)		80 0 0	5.51		666 75				12.98 0.37									0.51 0.0			44 098	2	32.87 0.93			26.05 0.7	.07 0.68		20.73 0.5		_							9.31 0.26	
					. 20					12	0.94									:			35			. 62 . 58:1		٠.													
		(cusec)	٠	l				6													7			٠																	
	Outlet Disharge uthorized D	(cusec) (m3s)			08 0.03			6.82 0.1			0.85 0.02															1.68 0.05			0.00					0.98 0.0							
	₹	ŝ	i				-	9			3 0	> C		0			D -	4 -	-	0	12	. :		1			~) C	1	-	1	ο,		→	4 -4		-		
	Chak No.			8	en en	٠,	စ္ ထု				20.6	o o	1 00	ø	α (: :0 (n ja	ο α	2 00	В				മും	. α	9 po	82	pa i	α α	ı œ	iα	, eq	M		aj p	oρ	ρ	24	œ.	മ്മ	20
ľ				662/CB	662/GB		20/58 88/88				864/GB	664/GB	64/GB	666/GB	665/GB	8000	25/28 25/28 25/28	00/899	668/GB	667/GB		1 1	1	85/68 85/68	20/08	67/CB	670/GB	670/C	95/1/6	0,029	671/GB	871/G	672/G	673/GB	26.6		673/6	674/GB	674/G	674/GB	500
	Village																		٠	:	-																				
,	Ħ.		<u> </u>						ary)													iary)																			
`	g 8	(E)	butary	×	1349		0		tribut		2284	335	12	77	Ş	0.6	<u>څ</u>	2030	0	0	* .	stribu		782	55	8	2374	50	? <u>}</u>	335	8	73	8	8.3	3 5	. 2	722	<u>Z</u>	8	88	<u>Ş</u>
	Destance	(feet)	Distri	\$63	4425	7	30		hal Dis		\$ £ \$ £	8	K K K	2	1820	0[#]	0000 0000	8	}	O	1.2	abal Di		85	×271	8	138	345	7408	8	3490	8	1:48	1214	366	1130	2370	2758	%	88 5	ر 7 07
	(w)		Mabai	180.7	1529	1041	4851		Pir Ma		22 5 24 5 24 5	4077	948	4868	5331	10/0	7855	5886	9885	9885	:	Pir M		762	2488	2978	5352	552	5089 6805	7230	8294	8318	2998	9037	0,70	10796	1518	12359	2568	2777	0/00
5	(jeet)		K V	£.	5018	2010	5915	: -!	55/R, 1		484 484 414	3375	28	15970	828	3363	2572	2470	32430	2430		320/R.		85	8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	27.2	_		22,620					29650						41918	-
	. 1		/080/						JD 684		•	• 1				(80 SS						,	-1 (C)	1 (1	71	~	64	(,)	o cr	. (*	. (*)	4	4	4 4	}
1,0	watercourse No.		r (RD	7/E6	5018/L 9775//	F 4 10	1269 15915/TL		inor (7		1,224,7	13375/L	15900/L	S970/L	17490/1	SYCKE I	81275	32430/TR	32430/TF	32430/TF		finor (20007	16.47	9770/R	17560L	17905/1	2520R	23720/L	27210/R	27290/R	28436/L	29650/R	4700/2	35420/L	37790/R	40548/L	300 41234/1	41918/1	1775
3	≘		Thera Minor (RD 67080/R, Pir Mabal Distributary)	1265 593/L	1266 5	2,46	1269		MagneJa Minor (RD 68455/R, Pir Mahal Distributary)			1272				0/7:						Junejwala Minor (RD 89320/R, Pir Mahal Distributary)		1281 2	325	1285 9	288		1288 2				232	1202				1298 4	300	9 5	
3			Ther		C1 17	• •	, v		Mag		¢-	۰.	tr	vo '	1 0	~ 0	00	0	1	13		June	ļ	r4 e	· 4	w	v > 1	٠.	00	9	=	<u>~</u> 1	13	2	<u> </u>	9		<u>-</u>	<u></u> :	<u>5</u> 8	}

Table B - 1 (2/3) Breakdown of Authorized and Design Discharge Calculation for LCC Area

No. Watercourse No.	óZ.	RD CD	S	Section	Village	Chak No.	Outlet Disharpe	rge Tee	Section	D035	1	Carrier	۳	Section Project	Kemarks
9	1	(m) (190J)	1	Distance	,		Authorized	Design	Discharge	Discharge		(acte)	(pa)	CCA (Improvement)	
			٦	(ω)			(cusec) (m3s)	(cusec)	(casec) (m3s)	(casec)	(m3s)		1	(p.)	
1303 46035/	l	925 143	2394	730		675/GB	50.0 19.1	1	6.13 0.17		0.198	553		868	
20 1304 40730/R		730				265/GB	2.73 0.08	8	4.52 0.13	5,12	0.145	962	389	645 -	
130X 52260T		57740 16075	75 3010	0 917		275/GB	1.79 0.05		1.79 0.05		0.057	631	. 1	255	
	l		1	ŀ								11,620	4,703		
												4,702			
Landand Minne (DD Dir Makel Dietributery)	ا بر	Mahaii) ice mily	(Auto)											
אין זענענעני אנפיאטנין	; ; }				ž.					٠.	:		į	807	
1075/PC		\$75	1	5 907		680/GB		1.98	5.47 0.15	6.36	0.1%	632	256	807	
1208 A6757	, «	2		_		681/GB		1.43		4.26	0,121	489	98.	551	
1300 67867	· •	200		7.7		681/GB		0.35		2.72	0.077	181	52	365	
13:00 12776/T	2	12276 3742	42 5491	•		682/GB	2.05 0.06	2.26		2.37	0.067	727	262	292	
X 2017771 20171												1,994	807		

Table B - 1 (3/3) Breakdown of Authorized and Design Discharge Calculation for CBDC Area

Remarks																				Kala Minor(33.95)																								
Section		(ha)		6.390	6,390 Un Improved	6,343. Improved Or w.M. Phase-il 6,241. Un Improved			14,890 Improved OFWM Phase-II		14,670 On Improved	14,377 Un Improved				5,7,7 On timpleyed				•		8,451 Improved Or W.M. Phase-1 8,309 11n Improved			7,852 Un Improved	7.665 Un Improved 7.527 Illa Improved	7.434 Improved OFWM Phase-II			6.597 Un Improved 6.472 Improved OFW/M Phase II			5,925 Improved OPWM Phase-II	5.755 On improved 5.671 Improved 4th drainage				5,045 Un Improved	4.036 Improved OFWM Phase-II	3,906 Un Improved		3.697 Un Improved		
	2			-	<u> </u>	107							-		S ?			•	158 1			2 : 2 :			_	85	٠.			11 %			25					5. 5.					35	
Outlet CCA	(acre) (ha)				115	1.139	126	1,222	203	;;	25 25 25 26 26 27 26 26 26 26 26 26 26 26 26 26 26 26 26	808	8	105	197	2	3	337	88	9,207 3	533	200	152	\$	462	2 % 2 %	357	1259	454	307	331	405	2.5 5.5	386	303	\$\$	ž	1.970 1.970	373	8	ද ද	55 Y	36	375
٠	۱	(m3/s)			4.327	25.4 25.7	4.135	2. 2.	3.924	3.895	3.830	3.733	3.658	3.618	3.6 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5	1 (V	3.328	3.261	3.218	3.172	2.210	27.75	2.101	2.076	2.8 4	1.957	1.895	1.837	1.719	796.	1.581	549	1.502	6 25	<u>\$</u>	1.369	1.359	278	1022	0.991	0.973	0.933	0.819	0.755
Design	Discharge	(caxec)			152.80	150.32	146.00	142.71	138.57	137.54	135.23	131.82	129.17	127.74	127.26	9.0	117.53	115.15	113.62	112.01	78.03	\$ % %	74.17	73.29	70.77	69.11 67.84	6.69	78,20	60.71	58.85 57.55	55.83	54.69	53.05	\$0.91 \$0.91	49.47	48.34	\$2.7	45.13	38	8,	38.38	5 5 7 5	28.91	26.66
	9	m:3/s)		3.60	9; 9;	5 6 6 6 7 6	3.46	3.38	328	350	35	3.5	3.07	8	600	56	2.87	2.76	2.73	2.69	80	ž. 2	6,2	r	1.71	6. 3	6	8	1.47		<u> 8</u>	133	81	3 %	1.21	1.18	1.17	9.5	80	0.85	35 35 36 37	0 0 0 0 7	0.70	0.65
Section	Discharge	(cusec) (m3/s)		127.28	127.28	126.08	122.32	119.33	115.73	115.12	23.55	110,86	108.46	107.30	106.99	25.5	8 20	97.53	96.39	86.38	65.82	88	63.10	62.37	60.30	% 52.52 82.93	57.12	55.77	\$2.02	50.67 40.74	47.93	46.94	5.7	£3.83	42.61	41.61	5.14	38.99	31.55	29.97	29.57	28.29 26.29	24.85	22.83
:	Design	- 1	- 1-		0.50	2 4 2 4	3.29	38	0.67	ខ្ល	8	8	1.23	2,	9.76		2.13	1.25	1.55	33.95	\$60	100	080	2.28	1.52	- 0 21 %	4	4.13	1.49	35	8	<u> </u>	55.5	3 2	1.10	0.28	2.61	74.0	17.	3	4.5	S 8	222	1.17
Outlet Discharge					10.0	3	80.0	0.10	0.02	0.03	200	0.07	0.03	10.0	200	<u> </u>	900	0.03	9 00	0.83	20.02	200	200	90.	9.0	000 000	8	=	8	() () () () ()	38	5.03	\$ 6 6 6	8	0.03	0.0	.07	0.17	ş	Ş	<u> </u>	3.5	90.0	0.03
Outlet	Authorized	(cusec) (m3/s)			÷	. 72 . 75				S ?						3.50				29.16		200		1		888			1	5; £			# S				٠.							8.
Chak No.	1 1	15)					:																•	Chak 2		•								:										
ľ					:	:								,		50,00		:	han		٠	G		O								ផ្ទ												
Village	;				Zucu	Surge Pans	Man S	Buch	Aulakh Auttar	hang Sucu	Sime	Bhamba Kalan				Vor Mahrah Khan			89 Kot Mehtab Khan		•	Abdul Am	Rakh Khadian		ន	d de	g	Jhagin	글 :	a Cita		Rakh Umer Utta	10 / 10 / 10 / 10 / 10 / 10 / 10 / 10 /	H and	hina	hina		7 F	1	뎙	bmar 1	ਜ਼ੁ	Jed.	च्यू ट्रि
						Raja Jhang		Rafa Jhang		Rala Jhang		-	Marta	Marta	514 Matta				Kot M		er.	Abdel Am	Rakh	506	Murc!	Cher Wala	Auhdkaba			Cheena Utta			Rakh Dhal	Rakh China		Rakh China		EdC date	Rakh Dha			Kakh Und		. Rakh Dha
Section	Distance	(œ	: !			222		7		270								1.			•	90				319	_		846						67	213	ż	313	7	612	i in	3 5		
8	å	(toet)			657	\$ %	2	8	8	288 288 288 288 288 288 288 288 288 288	2145	8	757	674	0964 0 0	8 8			292	<u>8</u>	9 5	0/91		1660		8 2	3950	257	2775	» <u>×</u>	38	2397	6 9	\$	22	8	818	200	2	2010	ដូខ្ល	252	8	1267
	Œ		: ,		85	32.5	1828	272	258	888	665	8	4335	4540	35	200	333	1757	368	7119	7810	6 6	8	101	Š	10721	12081	12168	888	13008	3136	3866	2000	14259	14326	14539	15182	3,5	15802	8 2	25.5	72.5	7398	X
S,	(Jeet)				759	\$ 50 \$ 50 \$ 50 \$ 50 \$ 50 \$ 50 \$ 50 \$ 50	8	880	2500	9385	13430	13469	14226	14900	19869	22307	250	24848	25 140	25333	25632	31020	31520	33180	3.5	35187	39650	39907	42682	42718	43110	45507	45040 45804	46797	47018	47717	49820	50853	\$1860	53870	53993	56490	2709	28365
Water Course	•		Chinna Distributary		657/L	5990/R	. √000√	7/0089	8500/R	9385/L 11785/D	3430/L	3469/R	14226/L	14900/R	19869/K	307/0	23400AL	24848/L	25140/R	25333/L	256327L	31020/R	31520/L	33180/R	X1418	35187/L 35700/R	39650/L	39907/R	42682/L	42090/K	43110A	45507/R	45040/L	46797/R	47018/R	47717/R	7/07265	5085.44	51860/R	53870/L	53993/R 56306/r	56499/L	\$7098/L	28362/L
No.	(original)		Dietri		1351 65					1356 93					1362 19 05	35			1367 25							373 38 38 38 38 38 38 38 38 38 38 38 38 38			1376 42			1379 45	281 48		1383 47			284					1392 57	
ů.	(0)		Chinna		,	i m	-1	v : \	ÞΙ	~ >	s ex	0	Ξ	ဌ	<u>.</u> 7	ĭ	2.	7.	81	1	<u>5</u> , §	37	ខ	ដ	4, 5	១ឧ	13	21	ස	2 2	51	82	1 , %	8	ξ.	<u> </u>	ž) S	3 :1	Ç	53	4 £	3 3		Ş.

Table B - 1 (3/3) Breakdown of Authorized and Design Discharge Calculation for CBDC Area

Kemarks																																							:		rest house
Section Improved	CCA	(ha)	2,833 Un Improved 2,643 Un Improved				1,849 Un improved		1 320 Immoved OFWM Phase-II	1.157 Improved OFWM Phase-1	927 Un Improved			455 Un Improved		3 TT 6	3.726 ile improved	3.677	3.232 Improved OFWM Phase-I	3,008 2,004 Tanasas October 17,000	2.843 Un Improved	2,798	2,709 Improved OFWM Phase-III	2,624 Improved OFWM Phase-II	2,220 improved Orwin rubes		2,274 Improved OFWM Phase-II	2,176 Improved OFWM Phase-II	1.888 Un Improved	1.724 Un Improved		1,391	I.145- Un Improved	652 13a Improved			234 Improved OPW-M Phase-111				9,816 9,816 Improved OFWM Phase-III
l	(eq.)		8 5	89	174	<u> </u>	6 5 7	ţ	3 5	230	151	15	130	224	16,390		707	3		38	9 2	\$	x	88	\$ 8	7.	8	8 5	3 2	8	24	245	238	ĝ.	13	146	234	3,726			17
Oudet CCA	(acre)		470 787	416	429	330	300	9 9	84	98	32	37.	421	554	40.49%		161	18	554	<u> </u>	112	22	211	44.5	į	82	242	69 5	£ &	219	Ş	8	8	25.0	3	\ <u>&</u>	577	9,207 3,726			KH 424
Design	Discharge	(m3/s)	0.719	0.581	0.535	0.488	0.453	36	0.374	0.280	នុ	0.184	0.146	0.104	CENIO		(300)	986				_						0.515		94.0		0.356		0.155			0.051			- 1	8.291 RH 8.269
2	Disch	(cosec)	25.39 23.18	20,50	18.88	7.24	16.01) ·	11.63	0.87	7.77	87.0	5.17	3.69	/ C. T		32.05	33.41	29.51	4.75 54.75	24.39	23.74	23.8	22.28	20.43			18.20				12.57			17.4		7			- 1	292.75 291.99
Section	Discharge	(m3/s)	<u>.</u>	049			0.39		_					000		200	ı			790		6 0.59						5000 8000				9 0.32				1	3 0.05			-	8 727 8 726
X		٦	Ĺ.		141 16.20		1.94 13.9	51.44 14.15 (1)		873				3.35		71 00	1 00 . 07	36.2	_	2.11 23.76	52 2123	0.73 20.76		59.65		0.59 17.39		0.33 16.13		0.76 12.6			26 60		1.79 4.3	~ ~	6.				0.55 226.68 1.96 256.18
charge	Design	(cosec)			:	٠				:			_			. :		, c		0.05						0.02	- 2	٠.					0.05			٠	0.05	£3			0.05
Outlet Discharge	Authorized	(casec) (m3/s)	2.01 0.06		1.28 0.04		1.76 0.05	;	36.0			1.11 0.03		1.65 0.05	1		77 72 0		1.73 0.05					22.0				030				1.89					0		* L	ı	0.50 1.78 0.00
Chak No.	П	n)		פונ	ម								Chak 16	Chak 16	Cnak 18				:									:				:						2			ri H
Village		(E)	3 Raxh Shah Annayer			707 Halloke	0 Halloke	984	239 Halloke		512 Pamir Hittar	745 Pamir Hittar	877	0			427 Doth Author		567 Rakh Aulke	6	537 Rakh Aulke		9 Rakh Aulke		225 Pathoke Ottar 225 Path Author			298 Rakh Uttar	9 Noti Tittar			582	307 Kali	278 Kali	74 Jive	0 Aufake	O Jhingir				198
Section	Distance) (1001)	٦	42.16	9639	2320	0	2775 2775			1680			4) 	butary)	25.7	2705	1860	8	1725	ă	_		3 5	975	105	979	700	524	475	1161	8	5 K	252	0	٥		1	- 1	650 4372
ß	(u) (beg)		58375 17787	•					7,5000 2,200		78232 23837	• • •			6350 52460	., Chinna Distri	-CV 3581	-		6029 1837				14590 4446	14770 4500			18057 5502			_	21961 6692			25632 7810	25632 7810	- 1				650 198 5022 1530
No. Water Course	नि		1394 58375/L	306 635937	1397 66732/R		1399 69052/R		1400 /3003/X		1403 78232/R				1407 83330/L1	Kala Minor (RD 25333/L, Chinna Distributary)	1950 1954	41404	1410 6000AL	6029/R	1412 9300/K	11245/1	_		1416 14770/K			1419 18057/R	19119/R 1420 19150/R	• • •			1423 22967/L	2403//L			1427 25632/TR		Theman Distributary	-	6507L 5022/L
Š			3 5	₹ 5	S	5	- K		38		2	_	_		ě	Kala M	-	- c	m	4 (r. «	-1 0	æ	on (2:	: 13	<u></u>	- ·	ت <u>ح</u>		<u>×</u>			3 8	•	18	۲,		Thema		()

Table B - 1 (3/3) Breakdown of Authorized and Design Discharge Calculation for CBDC Area

1991	ACTIBLES						Keent Minor	Days and the same	Athiput Minor		-																										Saharan Minor(28.99)						
- Inches				9,387 Un Improved	9.275 Un Improved	9,064 Improved OFWM Phase-II	On marches	Un Improved		~~	51. Un improved	8,518 Un Improved	6,5/% Improved Or wish rease-iii	8.085 Un Improved		,887 Un Improved	,695	525 Un Improved	.384 Improved 4th drainage	7,145. Un improved 6,082,175 Improved	∞	6,650 Un Improved	6.588 Un Improved	6,239 Un Improved	6,150 Improved OFWM Phase-III	6,100 On Improved				5,697 Un Improved	5.554 Un Improved	5,448 Un Improved	5,255 Un Improved	5.142 5.142 Tennovod OEWA Phase-II	4.896 Un Improved			.403 Un Improved	167	24 Un Improved	749 Un Improved	537 Un Improved	206 Un Improved
S. S. S. S. S. S. S. S. S. S. S. S. S. S	\ ,					99		185 8.8		87.			900			-	_		•	1., 201				_		97	200	231 6,007	_	102 5.697	_		113 5,2	246			4		781	-5		331 5	
100		(2)	747	277	520	\$ £	Ì	456	:	216	;;	345	2 4	3 8	429	476	419	S	<u> </u>	35	Š	152	862	S	អ្ន	88	: œ	571	197	35	25	475	280	A S	321	330	7,949	263	3 6	282	23	818	173
Parime	ı	ŝ	8.174	8.078	8.037	7.986		· v 0	v.	2.287	2.238	17 t	7.107	2115	2.089	2.050	1.998	1.937	1.880	2,87	246	1.678	1.658	1.581	1.554	466	525	1151	1.460	5 5	1374	1.350	336		2	1.159	1.126	0.305	0.280	0.00	0.172	0.124	0.0 \$4
	Dishar	(casec)	288.62	285.24	283.78	281.30	55.87.7 5.87.7 5.87.7 5.87.7 5.87.7	188.20	184.75	80.76	79,03	78.43	77 32	74.67	73.76	72.39	70.55	68.39	3	3 8 3 2	1 V	59.28	58.53	55.82	¥ ?	4 7 5 5 5 5	47.5	85.58	51.54	2000 2000 2000 2000 2000 2000 2000 200	48.52	47.66	46.10	3.7 3.5 3.5	42.53	40.91	39.76	10.77	9.89	799	6.08	4.40	<u>z</u>
3	Jischaria.	(w).(w)	Ĭ `	7.15		\$8						8 %	9 6	3.5		_		65	ያ ፡	1.52	• -	• ••	1				~	8	77.	2 2		1.16		2 8	~		0.97			7.0		-	<u>3</u>
3		5	1.				248 57		_					6024			2 57.45	_		335		50.07	- :			2.04		_		63.16			-	38.74					5.5.5 5.5.5 5.5.5		5.33		2.1.45
	22 00		!	280		0,47	` <i>`</i>		2	69:0				2000			1.32					_				7.0		,		0.19				2 5 5 -		1.03				3 85		2.63	Š
Orther Discharge	Authorized	٤	0.71 0.02	79 0.02	100 67.1	0.43 0.01		: -				1.10 0.03	- :	200	23 0.03	36 0.04	20 0.03	8	20.0	50.0	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	43.00	46 0.07	63 0.02	35 0.01		000	63 0.05	1	1.08 0.03	0.75	38 0.0	0.80 0.02	0.00	18 18 18 18 18 18 18 18 18 18 18 18 18 1				200	0.53			0.49 0.01
Nak No	ľ	(casec)	o-	ď	∵	oʻ-	88.88	:	00.86	O	0.2			ပ်င	S					-i c	·	ં	2	o	00	o c	o c	; ₋ ;	Ö	ï	Ö		0.	oʻ~	-	o	24.93	σ·	-i -	÷ 0	:	7	o ·
Village		۽	112 Chath Wala	562 Lil	807 Vegal	129 Vegai	C IOCUITATION	2440 Grenn Kot	139					1408 PED Latione	37 Mustafabad					1633 Dafa 191 Pafe	101	593 Sathoke	6 Arora Sathoke			20. Sukha Wala				310 Kukhan Wala			229 Mir Muhammad	390 Raia Lang	681 Rukha Wala		0	356 Raja Jang	1001 20 June	20 Julik	410 Rain Jang		411 Kala Khara
	Detano	(just)	308	18.5	2650	\$25	3	800	455	8	2226	4 5	3	46.2	123	2337	2768	600	228	5359 966	225	9,6	61	1955	8	28	2 2	74	1335	8 6	ä	250	8,	1380	2238	1015	0	1170	8 5 8 5	38	1345	4320	1350
O.A.	(a)		5390 1642	11185 3408		14260 4345		•				-	2017 2017	41017 17498			49245 15005		-	61794 18829	•					2007 71938				75968 25147	• • •	G	,,,,	80780 24524					27017		(4		95950 29236
No.	2		2 5390/R	5 93401L 5 11185/R		7 14260/L	73000	9 25309/L	2576-7	10 32407/L	11 34633/L			4.5939.21 4.1017/R	18 41 140/L	19 43477/L				74 61 / F.C.		27 68026/R	_	32 70000/R		2/0002/ 20	28 736130.			30 73908/R			42 79500/R	1/000/6/ 43 80780/R				47 85200/L	88650/K	52 88935/R		53 94600/L	54 95950/R
3		3	ς,	* ~	ø	t ~ o	c	۵		2	= '	<u>: 2</u> <u>5</u> 2	1:	1 V	9	13	20	<u>9</u>)	9	٦£	1 F	አ	አነ	29	5 13	9 8	3 8		88	3,3	8	æ	5 3	2,8	9	4	,	Çį (S S	. 3	ş	47	87

Table B - 1 (3/3) Breakdown of Authorized and Design Discharge Calculation for CBDC Area

No. No. Water Course	ð	×	Section	Village	Chak No.	Outlet Discharge	ischarge	Ŝ	Section	Design	5.	Ouder CCA	۱	Section Improved	Remarks
(legizno)	(feet) (m)	ı	Distance			Authorized	Design		Discharge	Discharge	1	(acre) (ha)		CCA	
1		(36)	Ê			(cusec) (m.Ws)	3)	Ş	(m.l/s)	(casec)	(m.Ws)		ŀ	(ha)	
49 56 96607/L	96607 29436	36 657		200 Rena.	;÷.,	0.67 0.02	0.02 0.74	96.0 20	0.03	1.07	0.030	235	S 4	136 Un Improved 41 Un Improved	
30 3/ 4/900/R		ļ	ı	Nata Anara		2 62 22 2	1	1	ı		,,,,	Ĺ	7180		
				•			·					.]	010		
1	7. T.		1												
Sanaran ivinor (KD 54050/L, Inchian Distributary)	own in them	TISTO UST	TO COLLEGE Y	_				24.9		-				3,217	
1 2213/R	2213 6	674 221	3 674	674 Rukhawala		0.38	0.01 0.42	24.93	ľ	28.82	0.821	117	l	217 Un Improved	
2995/1.				238 Kot arup Svigh	٠	22.0	100	1.38 24.5	0.70	28.38	0.804	356	3	3.170	
3 3640/L	-	109		Shahalpur Rukh.			0.02 0.65		0.65	26.92	0.763	183	`	3,026 Improved OFWM Phase-I	
4 4370/L	_				d.			` '		26.23	0.743	653	•	2,951	
5 6015/L	_			Theh Saharan	:	_,		•		23.41	0.663	137	\$	2,687 Improved OFWM Phase-II	
10500T		99 4485						_		22.85	2,00	295	: '	2,632 Un Improved	
7/5551: 2	-		5 291	Malloke Rakh		236				21.59	0.611	787	318	2,512	
8 11633/L	_	45 178		Ravi Thaman				_	0.47	18.92	0.536	ጀ	5	2,194 Improved OFWM Phase-III	
9 13050/R	_	-	4	Ravi Thaman		•		,		18.48	0.523	412	167	2,152 Improved OFWM Phase-II	
10 15050/L	•		_	Rakh Maluki						17.08	0.484	505	5	.985 Improved OFWM Phase-I	
11 15685/L	•	4779 635						57 13.31	0.38	15.05	0.426	\$0\$, 85	1,781 Un Improved	
12 15720/R	Ī	_						-		13.34	0.378	463	187	.576 Un Improved	
13 18300/L	_		786				0.09			11.88	0.337	941	381	.389 Improved OFWM Phase-II	
14 18830/L		5738 530	_	Theh Rosa			Ī		3. 0.21	8.35	0.236	145	Ŝ	.008 Improved OFWM Phase-II	-
15 23683/R	•		-	Shero Kahva	: .	0.93		1.02 6.94		7.84	0.222	261	8	949	
16 23763/TL	•	241 80		24 Kotli Rai Abu Bakar	·			-	0.17	9.6	0.187	635	257	844 Un Improved	
17 23763/TF	·	7241	0			2.40		2.64 4.21		4.63	0.131	839	3	587 Un Improved	
18 23763/TR	23763 7	724;	0					18.1	0.05	8:1	0.056	611	247	247 Improved OFWM Phase-III	
						24.93	17.						3,217		
							. :					3,217			

Table B-2 Meterial for Canal Lining

No. Meterial	Sample Specification	Cost*1	Water-2		5	Endurability #3	*3		Available	Roughness	Remarks
		(Brick =!)		enetratio	n Abbrac	on Degr	adation	Tightness Penetration Abbration Degradation Anti-Alkali in Market	in Marke		
Al Earth	Bentonite Lining (5% max 4 inch thick)	0.7-1.5	56	7	-1	-	Σ	×	•	0.02	
54	Soil Cement (10% mix of cement 8 inch thick)	0.5-1.0	70(vary)	×	Σ	<u>.</u>	Σ	H-W	•	0.02	
ঽ	Compacted Clay (4 inch thick)	0.4-0.7	2	ר	3	_	ני	Σ	•	0.02	
۸4	Stone Lining (4 inch thick stone masonry)	2040	88	ı	Ξ		Σ	x	-	0.018-0.02	0.018-0.02 Price high and supply short in Punjab
Bi Asphalt	Pre-mixed Asphalt Concrete (2 inch thick)	1.5-3.0	85(vary)	×	.		Σ	×	,	0.018-0.02	
B2	Prefabricated AsphaluBuumen mix or buried into soil	1.5-2.0	80(vary)	۱.	X			x		0.018-0.02	
C; Tile	Brick Tile Lining (4.5 inch brick on edge pitched by mortar)	(0.1)	88	Σ	x		7	Z Z		0.017-0.02	
ប	Ceramic Tile (0.5 inch thick tile pitched by mortar)	3.0-4.0	85	×	H	-	×	M-H	•	0.016-0.018	0.016-0.018 Price is very high
D1 Concrete		2.0-3.5	95	x	X		I	×		0.015	
ដ	Cement Concrete Lining (1:2:4 mix 3 inch thick)	1.0-1.2	86	Ή	H		Ξ	Н	٠	0.015	
ឧ	Mortar (Shot-crete) Lining (1:3 mix)	0.75-1.25	8	Ξ	Ι.		Σ	M-H	•	0.015-0.016	0.015-0.016 to be combined with geotextile/eq.
콥	Precast Concrete Slab/Block	15.20	95	I	×		×	π	•	0.016-0.018	
ជ	Reinforced Concrete Lining	-0.9	86	Ŧ	τ		Ξ	Н	$ \cdot $	0.015	
El Textile	Grouted Fablic Mat (Synthetic Fablic Sheet filled by mortar)	5.0	8	x	H		Σ	Ή			
ជ	Geo-textile (for subgrade or support of other materials)	0.8-2.0	vary	X	*	1	×	×		1	to be combined with other material
F1 Rubber	Vulcanized Synthetic Rubber Sheet (0,75mm thick.)	3.0-5.0	100	x	X	2	M-H	H		0.015-0.018	0.015-0.018 under experiment in Pakistan
	Same above reinforced by fiver(1.0mm)	5.0-7.0	8	æ	x	 	x	×		0.015-0.018	0.015-0.018 under experiment in Pakistan
C.	Non-valcanized (1.0 mm thick)	2.5-4.5	8	I	x	N	X-X	×		0.015-0.018	
GI Resin	Polyvinyl(PVC) Sheet (0.1-0.2 mm thick)	0.3-0,4	801	1	Ι		7. M.7	×	"(import)	0.013-0.015	*(import)! 0.013-0.015 [local product are low quality
ខ	Plyethylene Sheet (0.1-0.2 mm thick)	0.25-0.35	8	u	Ξ.	_	ר	×	•	0.013-0.015	0.013-0.015 local product are low quality
8	EVA(Vinyl Acetate) Sheet (0.1-0.2 mm thick)	0305	80	-1	Ξ	7	L'N	Σ		0.013-0.015	
ż	Plyethylene Sheet (HDPE,etc 0.8-1.2 mm thick)	30-50	901	×	=	2	Η·X	- H		0.013-0.015	0.013-0.015 Planned for PESS Project
H1 Scalants	Natural or artificial scalant material	•	vary	1	•			×		•	temporary treatment material
H3 Mix	Combination of above		vacy		•		:	•		•	

*1: costs include material, fabrication and finishing and exclude appurtenant earthworks required particularly per unit area. Total cost may vary wider. *2: initial water lightness on % saving of seepage against unlined case provided that joint are perfect. *3: H(high resistance), M(medium) and L(low). NINES:

Table B-3 Summary Table of Canal Route Survey for LJC Area

	Remarks	* is ommited for design)			ر بر																	only										
	8	(* is ommi			Left side only			•		_*												Right side only						~				
		Kınd	0,00 0.10 Bricks	0.14 Bricks	0.21 Bricks	Bricks	0.09 Bricks	0.10 Bricks	O TO Bricks	0.10 Bricks	0.14 Bricks	0.23 Bricks	C.76 Bricks							0.12 Bricks	0.12 Bricks	0.32 Bricks	9.46 Concrete	Bricks	80				_		 	
	:km)	Distance (km)	85	0.14	200	0.22	800	0.0	2 5	0.10	0.14	0.23	8.0	3 8	88	8	8.0	8	88	0.12	0.12	0.32	84.9 84.0	1.12	8	80	800	88	88	0.0	13.69	
Data	Lining (unit :km)	To (RD)	3.22	2,845	8,078	8.036	16,794	18,671	100,00	41 748	43,431	74,135	111,468							64.145	86,940	95,580	206,300	13.515		•••			-	•		
Surveyed Data		from (RD)	a	2 392	5,377	7.319	16.500	18.341	787.57	41.432	42,960	73,386	108,990							63.743	86.544	94,520	175,272	9.855					-			
	Outlet	(SON)	5.4	}			·						•	<u>.</u>	<u> </u>	0	7	S.	v ž	3 5				1 00	82	90	<u> </u>		-1 <u>c</u>	0	317.00	
	Lengin	(km)	33.98	-	:							•	•	4 7 7	2.70	6.21	2.68	5.87	8. 9 2. 9	62.88			9	4.12	96.6	7.01	3.91	0.1	4 4 8 8	7.89	 199.17	
		Kind	μ Y							200										9.19 Concrete	вттте в											
	r:km)	Distance (km)	-	•					_:-						:					1	urgent pro	·.							: ,		 3,	
Data	Lining (unit :km	(%) (%)	114 473					-		• .									: : : :	206.542	00 are within									:		Эераттепt. Кт
Original Data		from (RD)	000 001		:	•	:.	 		-										176,100	(160350-176100 are within urgent programme by PID)				:							and Power Dep. 184.18 km
	Outlet	(NOS)	0.0	3						- 				o ç	1 60	0	7	· ·	প বু	127			,	1 00	91	90	0:	- 5	<u> </u>	7	 320.00	b Imganon Area are ≃
	Length	Gran)	6.86				•				•		,	24.7	7.87	6.34	5.76	5.87	4. 0	62.95			1 50	1.7	10,16	689	3.96	3 6	4 4	2.41	194.12	in from Puny
	Name of	Minor					-							Kor Momin	Kot Raja	Bhikhi	Sahowal	Marulianwala	i angu				Sec.	Hadda	Malkana	Wasuana	untepur I	Kodian	Killa	Dhabian		Orginal Duta obtain from Punjab Irrigation and Power Department. Total Origenal Length for LJC Area are = 184.18 km
	Name of	tributry														<u> </u>	<u>.</u>	-		!				, 154	:) h-d	 Grand Total	
	Ž.		Pindi Huran										E. i.i.						or in				Kiman			_		S S		Kirana	 	
L			ģ r	1									ر.	•	· v.	\$	۲.	∞ « —–	~ °	==			2	. ≏	7		9 [- 2	9 2	ន	 	

Table B-4 Summary Table of Canal Route Survey for LCC Area

l															
	,				Omennai Data	i Cata	- Inches	T	1 1 1 1 1		Surveyed Data	Cara			
	10 ample of	vame of	13131	E I			,km)	Ī	130	1 1 1		Lining (unit, Kin)	.km)	7	Kemans
	Distributry	Minor	 (Gran)	(SON)	(RD)	(RD)	Oistance (km)	Kind	(Jcm)	(SON)	trom (RD)	(RD)	Distance (km)	Kind	(* is ommied for design)
ģ -	Sarangwala		25.04	56	10,000	11,000	0.20 Side		25.01	98	10,000	11,000	0.30	Bricks	
											78,150	82,070	1.20	1.20 Bricks	-
			19.7	<u> </u>			88	.:	54.67	စ္က			8 .		
ণ ব ~—	Nasrada	Khilliana	0.4	-1 W			3 6		4 4	1 10	>	3,010,	3 6		
· v		Narwala	.82	9	16,900	19.103	0.67 Brick	35	5.83	2	0	130	900	Bricks	
	: :					-			- - ·		1,000	19,103	2.47	2.47 Bncks	
ن	Nasrana	Sationa	8	v	0	.300	0.40 Side	સુ	3.88	<u> </u>	0 0	86	0.23	Bricks	
											100	8000	000	Succes	
											, : 5 8	2.0	0.05	0.03 Bricks	•
7	Nasrana	Natheri	4.60	30	0	13,000	3.97 Side	ge	19'4	0	0	860	0.26	Bricks	
				<u></u> -				= -			3,300	4.000	0.21	Bricks	
						1			Ŧ.		14,000	15,123	0.34	Bricks	
∞	Nasrana	Domra	5.51	Ħ	15.000	18,069	0.94 Side	ge	5.49	Ξ	0	770	0.23	Bricks	
						-	<u></u>		:	:	4.000	5.030	0.31	Bricks	
_					<u>*.</u>	i		=		-	6,928	7,108	0.05	Bricks	*
				-							17.000	18,000	0.30	0.30 Bricks	
<u>م</u>	Sojra		15.06	8	28.500	49,414	1.08 Bnck	Suck Suck	15.07	9	0	319	0.0	0.10 Bricks	Left side only *
											21,880	23,179	0.40	Bricks	
				_				==		-	28,547	29,731	0.36	8ncks	
					. <u>_</u> _	-			<u></u>		31.84	35,980	1.2.1	Bricks	-
		:			•	1					49,000	49,446	0.14	0.14 Bricks	
2		Zeera	2.71	4	8,397	8,897	0.10 Brick	Snck	2.71	4	%.400	966.88	0.15	Bricks	
=			36.97	88	108,300	121.278	3.96 Brick	Suck Suck	36.98	8	108,262	121,325	3.98	Bricks	
<u> </u>		Mungi	4,32	٥	0	0003	1.83 Brick	rick Fick	4.35	Φ	•				
∷	Janiwala/Hamuza		10.96	7					S.80	<u>,</u>	-				
4		Amirwala	7.62	101					7.70			-			
2	_			-					4.75	2	25,053	25.271	0.07	Concrete	•
2			47.57	51			8		47.57	45			8.0		
		Thera	4.85	'n			0.00		88.4	v,			0.00	-	
82		Magneja	68.6	22			8.0	<u> </u>	9.83	Ξ		_	8.0		
2		Junejwala	16.08	73		-	000		15.99	23			0.00	00.00	-
ន	Pir Mahal	Jandwala	3.74	4		:	8.0		3.76	e,			000		
77	Kilianwala		46.05	103	100,000	151,586	15.73 Brick	inck	46.33	63	100,533	152,033	15.70	Bricks	
23	: Kilianwala	Minor #3	99.9	=			00.0		6.68	4			89		
<u>ន</u>		Minor#7							4.19				•		-chevi
7,	Kalianwala	Minor #8	:				- :	<u></u> ,	2.62			-,-			
	Canad Total		24607	VV 0V7			30.04		226 23	ě			90.00		
	VIAID VOLA		240.74	0000			/ ChOn	œ.	Secure :	3/3.00			35.35		
	Kemarks:	Original Data obtain from Punjab Irrigation and Power Department.	an from Punja	to impation	and Power	coartment.									

BT-34

Table B-5 Summary Table of Canal Route Survey for CBDC Area

۱					Original Data						Surveyed Data	Data			
	Name of	Name of	Length	Ourdet		Lining (unit :km)	r :km)		rength	Outlet		Lining (unit :km)			Remarks
	Distributry	Minor		(SON)	irom (RD)	To (RD)	Distance (km)	Kind	(km)	(NOS)	from (RD)	To (RD)	Distance (km)	Kınd	Kind (* is ommited for design)
<u> </u>	Theman		29.85	20	\$6,000	000'99	3.02	3.02 Brick	29.50	35	0 0 17	388	0.12 Bricks 0.08 Bricks	nicks	
~	Theman China	Saharan	7.24 25.45	81.8					7.32	21.80	56.391	216	3.06 0.00 0.06 Bricks	nicks	
	China	Kala	7.81	ង					7.82	77	155.00	65,167	0.00	UCKS	
	Grand Total	ë	70.36	70.36 156.00			3.02		70.16	163.00			3.51		
	Remarks:	Remarks: Original Data obtain from Punjab Imgation and Power Department. Total Origenal Length for CBCD Area are = 67.3	an from Puny ngth for CBC	ab Imgatioi D Area are	n and Power I	Separtment. 67.34 km	E,						·		

	alle landere et en en en en en en en en en en en en en	Tab	le B-6 Sedi	mentation D	ate for Lowe	r Jelen	n Canal	
No.	Bed	Materia	1			spended		
	Distribution (mic	rons)			ation (unit: PPI		Distribution (microns)	
	50% Pass		t. Deviation	< 62 microns	> 62 microns	Total	50% Pass	90% Pas:
		285	1.39	23	5	28	70	120
1		263 258	1.39	33		35	20	5:
2			1.47	38		46	20	7
3		250				45	25	7
4		263	1.38	39			20	6
5		299	1.4	69		72	15	5
5		309	1.39	99		103	15	3
7		310	1.41	165		169	25	7
8	•	339	1.39	14		17		
9	1 .	311	1.34	25		27	20	6
10		345	1.39	34		37	30	. 6
l 1		311	1.31	20		30	25	9
12	•	275	1.47	24		27	20	6
13		285	1.39	23		28	30	
4		286	1.43	47		123	75	15
15		282	1.39	26		29	25	6
16		290	1.39	21		23	25	
7		312	1.37	122		123	20	
8		273	1.5	29		31	20	
9		262	1.53	47		48	20	
:0 .		252	1.33	175		187		
11		325	1.37	12		17	25	
22		302	1.61	29	and the second s	32	40	
23		277	1.42	24		31	25	7
24		274	1.47	26		37	25	
25		277	1.36	96		128	25	
26	The second secon	260	1.31	105		. 111	20	
27		300	1.27	112		113	20	3
8		265	1.33	73		· •77	35	
9		269	1.3	56		64	20	
0		282	1.41	33	4	37	25	
1		270	1.26	36		41	20	
32		249	1.29	58		85		
3		255	1.33	36		40		
4		250	1.27	31	7	38	25	
15		240	1.29	113	3	- 116		
36		300	1.37	123	6	129		
37		350	1.63	77	2	79		
8		280	1.4	96	5 7	103		
19	•	297	1.37	42		43		
Ю		. 311	1.37	220		224	20	
11		272	1.29	29		32	25	
12		288	1.27	38		43		
13		269	1.29	39		50		
14		288	1.36	50				
45		265	1.29	54				
		0451	1 20	£0.50	3 70	67.27	27.00	66.1
ave	2	84.71	1.38	59.58	7.69	01.21	27.00	00.

			· · · · · · · · · · · · · · · · · · ·		· · · · · · · · · · · · · · · · · · ·		
No.	Bed M		Concent	Susperation (unit: PPM)	nded Load	Distribution (microns)
		n (microns) St. Deviation		> 62 microns	Total	50% Pass	90% Pass
·							
UG 1	326	1.4	150	178	328	129 128	215 216
2	122	1.4	117 163	283 202	400 363	128	214
3 4	193 254	1.7 1.5	189	250	439	123	225
5	313	1.7	535	125	660	104	167
6	357	1.4	583	124	707	82	120
7	274	1,4	161	190	351	113	192
8	172	1.5	121	115	236	117	213
9	274	1.5	427	328	755	156 109	288 167
10	200	1.6 1.4	183 158	222 93	405 251	135	244
11 12	304 217	1.4	585	170	755	91	167
13	94	1.5	91	87	178	120	22:
14	167	1.7	680	310	990	157	34
15	138	1.3	275	125	400	118	17.
16	151	1.9	695	381	1076	106	259 239
17	246	1.5	119	206 91	325 234	12I 125	17.
18	244 235	1.4 1.5	143 620	91	711	80	14
19 EG 1	253 258	1.4	137	217	354	133	- 21
2	242	1.4	30	188	218	133	15
3	229	1.3	93	399	492	151	22
4	268	; 1.3	123 .	364	487	140	21
5	236	1.3	125 116	359 439	484 555	140 155	22 24
6 7	223 226	1.3 1.3	178	541	719	182	24
8	241	1.2	147	455	602	128	21
9	203	1.3	121	539	660	128	21
LS I	93	1.4	290	168	458	100	15
2	103	1.7	2182	231	2413	103	16 24
3	120	1.3	166	43 223	209 2145	109 96	: 18
4	116	1.2 1.3	1922 1635	158	1793	83	12
S ML 1	97	1.3	42	55	97	151	27
2	166	1.3	292	44	336	90	19
3	162	1.3	1041	. 193	1234	98	16
4	163	1.2	62	50	112	116	24 23
5	169	1.2	204	328 196	532 1331	154 114	16
6.	154 158	1.2 1.2	1135 404	84	488	130	16
- 8	176	1.3	191	378	572	148	2
ှိ	184	1.3	95	175	270	124	17
10	179	1.3	137	150	287	126	16
11	168	1.3	1089	245	1334	129	17
12	175	1.3	67	175	242 549	85 141	t <i>e</i> 19
13	179	1.3	320 1290	229 264	1554	141	IX
15	159 170	1.2	93	153	246	126	20
- 16	154	1.3	150	212	362	131	17
17	187	1.4	233	44	277	82	I
18	- 147	1.3	. 163	80	243	102	19
USI	141	1.3	1719	125	1844	82 8	17 15
KR I	145	1.2	38 I 442	88 155	469 597	82	i
AJ I	91 94	1.2	2309	524	2833	81	į.
3	105	1.3	686	496	1182	80	i
4	105	1.2	1754	516	2270	95	1
- 5	96	1.2	366	145	511	100	l.
6	96	1.2	346	135	481		1
7	96	1.3	2770	542	3312	87	1. 1
. 8	96	1.2	2541	256	2797 560	101 101	
9	101	1.2 1.3	407 406	153 220	626	85	i
10 11	89 93	1.3	676	487	1163	101	į
NS I	157	1.3	620	398	1018	81	1
2	159	1.2	2239	495	2734	83	1.
3	94	1.3	1693	571	2264	86	1
SEL	98	1.2	2585	484	3069	81 90	1: 1:
2	102	1.2	877	164	1041	99	(4
					869.42	111.87	185.

Table B-8 Summary of Survey Data of Soil Mechanics

							1		-					AT	Anteres Limi			Proctor compaction test	paction test	Specific	Natural	Natura	Natural Co-efficient of
9	_]			G PASS USS	USS			Propertie an	tte analysis		Per cent			pròre	plastic	planticity	Shrinkage	Optimum Maximum	Maximum	Gravity	mousture	ફે	permeability
Sample		26		97	8	8	8			pures	Nik	clay	Classification	Ĕ	Ĕ	index	ĮĘ,	mousture	}		Content	density	cms/sec. at
ġ.) 						0.	\$00.					۳,	FE	£.	8	content	density		8	Da/ch	natural dry
	-	_	-		-						:	-						ž	ib/cft				density (Lah)
227	-		_	_		L										-							
9869		8	0 0	90.4	38.	· 	8		8.0	9.0	26.0	O.X	8.0 Sandy suft		Non plastic			12.7	107.1	2.71	13.89	91.25	91.25/9.11-10%
1669	64	8		9,6	2 99.0		9	78.5	23.2	213	\$	8	28.2 Clay silt	30.4	12.7	7.7	21.5	12.5	112.4	2.67	12.73	95.00	95.00 4.13-101.7
X6469	۴,		8 8	98.1	5 97.9	0.80			28.5	30.0	\$15	2X S	2X.5 Clay silt	23	12.2	10.1	16.9	13.3	111.6	2.69	19.37	93.13	93.13 3.54*105.7
66669	4	100		×4 9x3	3 98.3	4.79	8	4	20.7	.23.×	53.5	20.7	20 7 Clay salt	19.4	X []	7.7	17.6	011	114.0	2.70	11.11	92.50	92.50 7.59*10%
2000	٧.	100	001	90 0 00 X	7 00 X	7 00.0	8	ç	14.2	×.7.×	Š		14.2 Sandvent	22.4	×	901	4	11.6	3 001	2.69	19.18	8	92.50!1 X4=10\cs
25		_	:		-		Ŀ					-									-		
7007		8		5.9 95.X	.X. 95.7				33.0	×	58.2	33.0	33.0 Silty clay.	24.4	14.7	9.5	19.5	120	111.4	2.39	21.65	86.25	96.25 7.08*10^-7
7007	64	<u>8</u>	6.79	96.9 96.7	7.96.4	0.96		X0.2	23.2	X.61	57.0	ri Fi	23.2 Clay silt	ä	15.5	6.5	14.4	4	117.1	5.69	22.54	\$6.38	99.38 7.08 10~7
7003	۳.	8.			1.7	.i. x5.1				3	.90	0.6	9.0 Sandy saft	-	Non plastic			11.4	102.X	2.72	10.37	\$0.00	90.00 5.95*10\4
3004	. 4	100	3	X 00 0 00	800	× 3	5		7.47	¥.	X 67		M 7 Silve clay	ac .	13.7	3. 3.	×	13.5	11.2	2 5×	7 X	\$228	96.25(8.85e10A.7
CBDC		60	0.440	3	. 70		ō		9		3		4177	;	9	,		2		į	Ę	2	
		•					ŀ	J	ł	ı	H	ı	SAFETY ALL	4.7.4				10.50	ı	7	21.1	43.03	6

8	IRURI DISTY: R.D. 4-L. Distance from left bank of disty: = 125 ft.(LCC-1)	7001 KIR
6997	KARKAN MINOR RD 5200-L. Distastice from left bank of minor = 60 ft.(LCC-2)	7002. KIR
¥669	MADUANA DISTY, RD 35-R Distance from right bank of disty, = 9% ft,(LCC-3)	7003 BAI
6 6669	Ş	70 YO
200	SEWAL MINOR RD-XXSQ-L. Distance from left bank of minor = X5 f(LCC-5)	7005 HA

7001 KIRANA DISTY: R.D. 62800-L. Distance from left bank of minor; = 400 ft.(LJC-1)
7002 KIRANA DISTY: R.D. 105700-R. Distance from right bank of disty; = 350 ft.(LJC-2)
7003 BALOCHRA DISTY: R.D. 350ft-L. Distance from left bank of disty; = 110 ft.(LJC-3)
7004 NAURANG DISTY: Distance from nght bank of disty; = 250 ft.(LJC-4)
7005 HADAL DISTY: R.D. 28-L. Distance from left bank of disty; = 335 ft.(CBD-1)

	l				
Lab. Sample No.		BoreHole	Sample	с (ит^2)	, (deg.)
9869 DDT	- <u>-</u>	PIT 1	10574	0000	31
}		.	10574/QTXL	0,000	3
6997	14	2	5750	8 8	<u> </u>
X669	*	PTT 3	10576/QTXL	7.140	H
			10576/A	0.40%	. 17
6669		4 PTT 4	TX0/L/201	8	ę,
	_		10577/CU	0. \$0.	×
7000	S S	25 25	1057W0TXL	2.550	29
	_		10.47K	1.020	×
2				,	
100		PT LC:	UD/BLOCK	4.1.4	73
			UD/BLOCK	3.672	4
7007		2 PIT LICE	VD/8LOCK	1.14	क्ष
			UD/BLOCK	2040	4
2007	_	3 PTT LIC-3	UD/BLOCK	0000	\$
			UD/BLOCK	0000	£;
7004	¥	PTUCA		1.836	31
				2.44X	14
CBDC 7005					
	_				

Table B-9 Cost Comparison of Lining on Distributaries and Minors by Different B/D Ratio

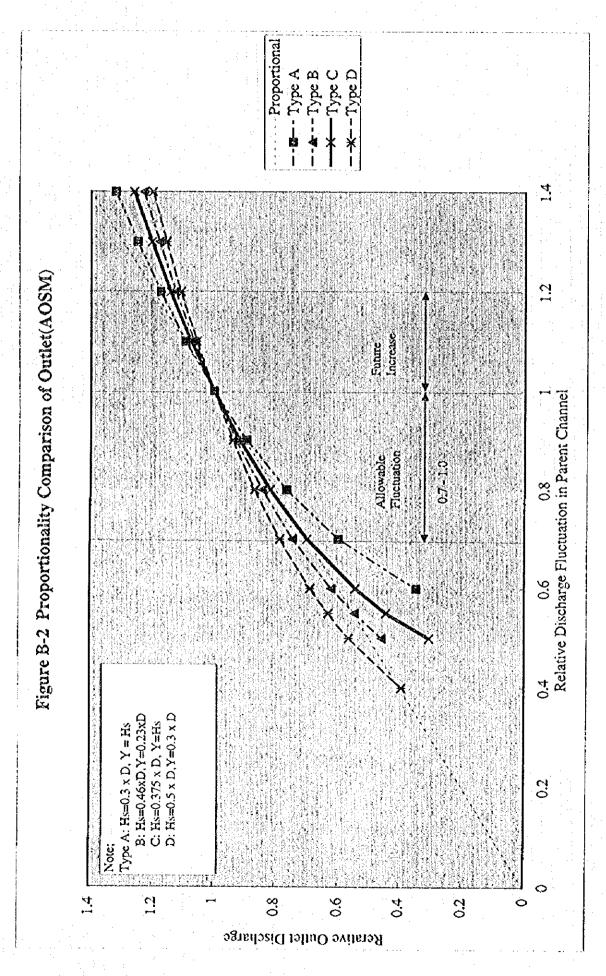
Work Item	Specification Unit Unit	7	ě						*	Work Vo	Volume												•	Linear-Meter Cost	1	96						
	-	J	Š	:	٠				i, ta	1	near Meter		;					۵	Charge	Discharge=100 Cusec	الإلال		۵	Discharges 200 Cases	C 000	¥		,	Discharge VM Cure	0	¥,	
		,	1	å	12	Discharge=100 Cure	ķ		Decher	i.	re-200 Cuser	ķ	ľ	Section	N.	Deschange=300 Cused	 			_		ر ا	_	~		4	¢	-	n	~	4	
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1																- :																
1. Parthwork											:	:																;		;		,
.1 Excavation	by muchine	Ę	ş	39 4.31 4.46 4.72 4.53 5.16 9.29 9.48	46.4	7. 4.	\$3.5	9	50 OF	04.0 04.0	0.923		=	0.70	9,46 11.22 10.70 10.22 10.22		50.	165.9	171.7	181.7	74.4	19K.7	357.57	38	361.9	356.1	¥,	4	412	63	? €	6
for Canal Pham	&manual .																															
1.2 Embankment and by machine,	ву тасыне,	É	×	58 6.13 · 6.99 6.84 6.8 6.7 13.5 13	3	ž 0	e e	<u>~</u>	7	3 13.7	7 13,7	7 14.X	14.7	14.7	14.7	15.1	16.7	354.9 4	404.7	%	393.7	387.9 7	781.07	355	792.1	~ §	2002	8553	×25	33	7	- *
Compaction of Bani normal	ni normal) -	٠.						•								 													
3 Berrow & Haul	within 75 m	m3	\$3	3.9×	76 4	4 X	4	£ 61	8,8	X6 X	8 9.06	5 10.1	1.6	9.33	19.6	86.6		23	259.9	24.6	247.6	i i	482.94	453.2. 4	490.3	4.3.4			511.6	524.7	3	627.4
1.4 Trimming &	Manual	Ë	0	9 6.56 6.56 6.98 7.29 8.19 7.95 X.07	\$	7.	% 9:	27.	5x X6	4× 7	4 X,X6	5 10.7	20.4	Š	9.75	102	12.7 5	59.67 59	59.67 6.	63,49 6	66,31 7	74.53	72.32	73.41 7	76.7K 2	X0.60	. 57.79	X2.33	X4.X7	88.70	93.16	115.39
Surface Finishing				5											٠.					•												
1.5 Excavation	by machine	Ę	2								:							0	0	0	0	0	0	0	0	0	٥	0	0	0	0	0
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2. Lining Work			٠	: .										: :				· · · · · · · · · · · · · · · · · · ·														
2,1 Mortur Phusics	1" mortar	뒽	ĸ	m2 52 6.56 6.56 6.98 7.29 8.19 7.95 8.07	Ş	× 2	×		35	x. x.	8.86	5 10.7	9.05	9.33	9.75	10.2	12.7	339.6 3	339.6	361,4 . 3	377.5 4	4242 4	411.65 4	417.9	437	45X.X	556.3	46X,6	483.1	\$04.9	5303	6.56.X
2.2 Concrete Insidu	3" that	Ę	š	0.50	8	53 0.	6.0.6	ŏ	51 0.6	10.04	4 0.67	7.0.K2	0.69	0.71	0,74	0.78	0.97	1497	1497	1593	1864	1 07%1	1814.4		936	202	2452	800	83	ij	2337	2895
23 Procast Panel	? thick	E C	8												٠.			¢	0	0	0	0	0	¢		,Φ	0	0	Ó	0	٥	0
2.4 Joint	Rubber Joint		n	25 2.19 2.19 2.33 2.43 2.73 2.65 2.69	61	33 2	63 2.7	22	65 2.6	1875 6	2.95	3.58	3.02	3.1	8	3.41	433 \$	X 2 X	X X	58.14 6	60.72 6	\$ \$3	£138	67.22 7	70.31	73.81	S 55	75.39	1.1	X1.22	85.3 1	105.67
2.5 Geomembrane	1 mm	Ç	3	•			÷		٠									0	0	0	0	0	0	٥	0	•	0	٥	٥	0	0	0
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:				٠,	•					:			:															,				
Construction Cost	ost	1	į	÷													**	2689	187	2898	2374	3248	3986	STATE	4155	4278	4971	474	4551	£8	858 828	Ę
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Note; Categories 1 to 7 in Work Volume stand for B/D rate of 0.x, 1.5, 3, 4.5, 6, 7.5 and %.5

FIGURES

Remarks 23 Completed ရ å TAXE COLUMN Annonnamentamentament de la company de la co TOTAL DESCRIPTION OF THE PERSON inistration and a second Š 25 ន *adamammaninininininina* Nov. 2 B **4** 26/0ct 8 2 3228 3 5 5 g ရှိ မှု မှု Levelling along the Canal / Distributerie Distributeries and Minors Client and Collection of Existing Date. Establishment of Field Camps and Mobilization to Sire, Reconnaissance and Liasion with Identification of Distributeries and Signing of Contract Agreement Cross Section / Profile Survey Activity Details Suctures Condition Survey Office Data Processing Compile Final Report Minors on Ground ۴, 4 -1 ż Ś ç

Figure B-1 Actual Progress of Canal Route Survey



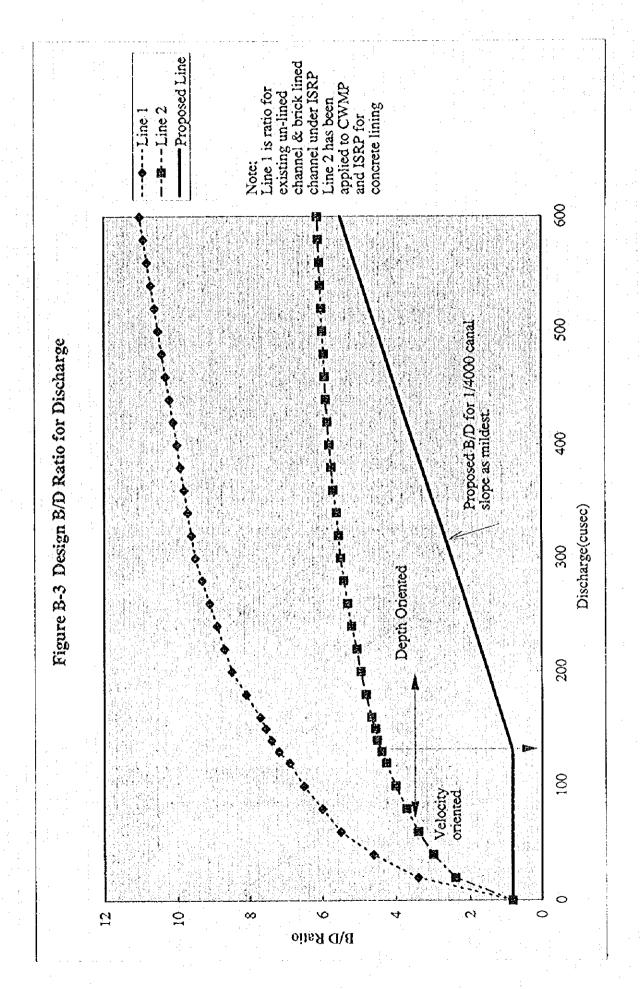


Table B-4 Design Flow-Chart for Lining of Distributaries and Minors

