5 FEASIBILITY STUDY

5.1 **Priority Projects Sites**

Through the overall evaluation including economic and technical evaluation, priority projects consisting of the following works have been selected for the Feasibility Study (refer to Figure 5.1).

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- 1. Improvement of the Western Banjir Canal (Estuary Manggarai Barrage, I=17 km)
- 2. Improvement of the Cisadane River (Estuary Pasar Baru Barrage, l=21 km)
- 3. Construction of the Ciliwung Floodway (I=1 km)

Present conditions of the objective reaches of the WBC and the Cisadane river are described hereunder. The condition of the Ciliwung Floodway is described in ANNEX 8 (Design and Cost Estimate).

5.1.1 Western Banjir Canal

(1) General Situation

The Ciliwung river has a mountainous basin in the upstream of Bogor city. The middle stream basin of the Ciliwung river is already densely populated. The upstream and middle reaches of the river do not have flood embankment but have rather big carrying capacities, since the river flows through in deep valley. The Ciliwung river bifurcates to the WBC and the Ciliwung Drain at Manggarai Barrage in the midst of DKI Jakarta. The WBC flows through the western part of DKI Jakarta and flows into the Java Sea; the Cideng drain, the Krukut river and the Angke drain join the WBC.

The objective reaches of river improvement for the priority projects are the reaches of approximately 17 km from the estuary up to the Manggarai Barrage; the catchment areas at the Manggarai and Karet barrages are 337 km² and 421 km² respectively.

(2) River

(a) Estuary - Confluence of Angke Drain

(i) Short-cut Work at Kapuk Muara in 1995

The WBC near the estuary so-called Muara Angke has rather meandering river course, because the river course is the former Angke river course itself.

The recent biggest change of the WBC river course is the completion of short-cut work at extremely meandering part in Kelurahan Kapuk Muara (0.8 k - 1.1 k) as shown in Figure 5.2; the work was executed by Ciliwung-Cisadane River Basin Development Project Office (PPWSCC) by using local budget in 1995/1996 fiscal year.

The length of the short-cut is about 200 m and consequently the WBC river course was shortened by about 450 m. The former meandering river course still remains but the water surface is covered completely by vegetation now.

(ii) Nature Reserve Muara Angke

Nature Reserve Muara Angke with mangrove forest is located on the left bank of the WBC near the estuary. The area is now strictly preserved from the environmental aspects. Newly constructed gentle slope embankment, with sodding, planted trees and with the elevation of about PP 3.5 m (approximately TTG 2.9 m), forms clear boundary between the Nature Reserve and the residential area of Pantai Indah Kapuk as shown in Figure 5.2. The design of the embankment was conducted by PPWSCC and the construction work was executed by the developer.

The elevation of the embankment is higher than the design embankment elevation of the WBC (refer to Section 5.3). The embankment can practically function as a left side embankment of the WBC; Nature Reserve Muara Angke can greatly lower the flood water level of the WBC by its function as a natural retarding basin.

(iii) Squatters in River Area

Downstream of Mandara Permai bridge (1.9 k), squatters are located along the right bank of the WBC.

(iv) Angke Drain

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The Angke Drain (Lower Angke river), the biggest drain along the WBC joins the WBC with gravity drainage. The detailed design by the West Jakarta Flood Control System Project has once been conducted including the design of the WBC from the Estuary to the Teluk Gong siphon and the Angke Drain.

(b) Confluence of Angke Drain - Karet Barrage

(i) Parapet Wall

The water level of January and February 1996 floods reached up to the top of embankment of the WBC, besides overflow occurred at several places. In order to cope with the serious situation of the 1996 floods, construction of parapet walls on the embankment has been conducted immediately after the floods by using local budget.

The construction work extends from the bridge on Jl. Pangeran Tubagus Angke (5.6 k) southward to the Karet Barrage (12.4 k) as shown in Figure 5.3. The height of the parapet walls ranges from 50 cm to 80 cm.

(ii) Rehabilitation of Embankment near Cideng Pumping Station in 1996

In February 1996 flood, the right embankment downstream of Cideng pumping station (9.2 k) was damaged by overflowing flood water, fortunately the embankment did not collapse completely though. The damaged portion of the embankment was rehabilitated by revetment immediately after the flood.

(iii) Utilization of High Water Channel

The high water channel has been utilized mainly as sport grounds and cultivated land. The high water channel is generally protected by bamboo revetment. The WBC has relatively wide (around 60 m) and flat high water channel from Aipda K. S. Tubun bridge (11.3 k) up to the Karet Barrage (12.3 k).

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(iv) Squatters in River Area

From the confluence of the Angke Drain (2.9 k) up to near the Teluk Gong siphon (4.7 k), many squatters are located without break on both sides of high water channel and embankment: the practical flow area is only within the low water channel.

From the Teluk Gong siphon (4.7 k) up to Pangeran Tubagus Angke bridge (5.6 k), many squatters are also located on the right side high water channel and embankment.

(c) Karet Barrage - Manggarai Barrage

(i) Channel Condition

The WBC flows in this reaches crossing the boundary between the terrace and the low-lying plain; the WBC generally flows in parallel with a railway on the right bank and the roadway on the left bank. There is almost no embankment on the left bank throughout these reaches: the ground elevation on the left bank is generally higher than that of the right bank.

From the K. H. Mas Mansyur bridge (13.1 k) up to the M. H. Thamrin bridge (13.9 k), the crown of the right embankment is quite wide. As the elevation of the railway along the right bank is the same as that of the embankment, the railway becomes a part of the embankment; the embankment is practically almost like super-levee. High water channel exists only on the right bank in these reaches.

The right embankment is terminated at Madiun bridge (15.2 k). Upstream reaches of this point have no embankment with no high water channel up to the Manggarai Barrage.

Some reaches has rather steep sideslopes of approximately 1:1 (vertical to horizontal) with no revetment excluding near bridges; the sideslopes are covered by grass and there are trees in places.

The sideslope of this reaches seems to be rather stable without any revetment, some portion was eroded by the big floods in 1996 though. The reason why the sideslope seems to be stable is estimated that the reaches were excavated through the diluvial terrace and the

material of sideslope seems to be compacted silt or clay of diluvial origin.

(ii) Park on Right Embankment

From the M. H. Thamrin bridge (13.9 k) up to the Sukabumi bridge (16.0 k), DKI Jakarta has put the right bank of the WBC in beautiful condition as a riverside park with promenade, benches, trees and streetlights on the embankment crown. This right bank stretch functions as one of the valuable place of recreation and relaxation for the citizens.

(iii) Cideng Drain

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The Cideng Drain joins the WBC from the left bank at 14.5 k with gravity drainage. In January 1996 flood, the flood water of the WBC flowed backward to the Cideng Drain and flowed into the Setiabudi regulation ponds through the lower portion of the embankment.

(3) Related Structures

(a) Embankment

The of the WBC exists as follows:

Confluence of the Angke drain (2.9 k) - Aipda K. S. Tubun bridge (11.3 k) : on both banks

Aipda K. S. Tubun bridge (11.3 k) - Karet barrage (12.4 k) : on left bank only

K. H. Mas Mansyur bridge (13.1 k) - Halimun bridge (15.2 k) : on right bank only

The slope of the existing embankment is generally 1:1.5. The present minimum crown width is 3 m. The embankment from 2.9 k to 12.4 k is covered by wet masonry revetment and asphalt pavement.

(b) Barrage

(i) Karet Barrage

The Karet Barrage is located crossing the WBC just downstream of the confluence with the Krukut river (12.4 k); the barrage has four slide gates and is integrated with a railway bridge. The functions of the barrage are as follows:

to supply flushing water to the Krukut Drain from the gate located on the right bank near the barrage; and

to supply raw water for the PAM Jaya treatment plant at Pejompongan, the confluence of the Krukut river with the WBC.

The barrage usually dams up the stream by about 2 m in the height. According to PAM Jaya, the main source of raw water at the plant will be the Kali Malang after completion of pipe construction from Cawang to the Pejompongan site.

(ii) Manggarai Barrage

The Manggarai Barrage is located at the upstream end of the WBC (16.9 k); the barrage on the WBC has two slide gates (Manggarai I gate) and is integrated with a railway bridge and a roadway bridge.

The functions of the barrage are as follows:

- to supply flushing water to the Ciliwung Drain from the Manggarai II gate located on the right bank; and
- to regulate the flood discharge distribution from the Ciliwung river to the WBC and the Ciliwung Drain.

It is said that the barrage dammed up the flow by about 3 m in height in January 1996 flood, because the gate is quite narrow. The necessity of the improvement of the barrage is discussed in Section 5.3.

(c) Bridge

There are 18 roadway bridges and three railway bridges crossing the WBC. Some bridges such as Prof. Dr. Latumeten and Kyai Tapa bridges have extremely low girders hanging down from the river bank. The treatment of these bridges is discussed in Section 5.1.

(d) Siphon

Three siphons as follows go under the WBC.

- Teluk Gong siphon of the Grogol drain (4.7 k)
- Siphon of Cideng drain (14.5 k)
- Siphon of Kali Baru (16.6 k)

(4) Present Carrying Capacity

Present carrying capacity of the WBC is estimated by using non-uniform flow formula based on the river survey results of feasibility study level conducted by the Study Team in 1996. The conditions for the calculation are shown below.

Calculation method

The same method described in Section 3.9 is adopted.

Tide level

Spring tide of PP 1,15 m (approximately TTG 0.55 m) is adopted for the lower-end water level.

Manning's roughness coefficient

n=0.025 : low water channel n=0.040 : high water channel

The results are shown in Figure 5.4. The bankfull capacity and the freeboard (minimum 0.8 m) capacity are around 350 m³/s and 250 m³/s in average respectively.

In the middle reaches, the carrying capacity has increased by about 70 m³/s in average by the new parapet wall constructed in 1996.

5.1.2 Cisadane River

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(1) General Situation

The river basin has a mountainous area in the upstream reaches. In the middle stream reaches, Tangerang city, now developing as a satellite city of Jakarta, is located. The present land use along the embanked reaches downstream of Tangerang city is agricultural land and Soekarno-Hatta International airport.

The objective reaches of the river improvement for the priority projects are the reaches from the estuary to the Pasar Baru barrage (22.3 k); the catchment area at the Pasar Baru barrage is $1,411 \text{ km}^2$. The high water channel is generally covered with rich riverside forest or has been utilized as cultivated land.

(2) River

(a) Condition near the Estuary

According to the topographic map with a scale of 1:25,000 issued in 1989 that was the only available map in the previous stage, no shoal exists at the estuary. However, the actual situation is quite different from that on the map: there exists a big shoal almost like small island of about 9 ha on the left side of the estuary. The detailed topographic maps along the Cisadane river including the estuary with a scale of 1:5,000 were prepared in this feasibility study stage.

In downstream reaches from Desa Cirumpakabeting which is located about 2.5 km from the estuary, the natural levee and the embankment of the Cisadane river almost disappear and the ground becomes almost flat. The small villages near the estuary are generally located on the concave bank of the meandering portion, since sheer cliffs at the portion are convenient for the water-borne traffic. Many fish ponds are scattered around the estuary. The river bed material still consists of sand even at the estuary.

(b) Natural Levee and Former River Course

(i) Teluknaga on the right bank

A remarkably developed natural levee, extending from 8.8 k on the right bank, exists along the former Cisadane river course. The city area of Teluknaga and other villages are located on the natural levee, since the ground elevation of the levee is higher than that of surrounding area and accordingly the area on the natural levee is precious safe place against the flood.

The former river course exists along the center of the natural levce; the former river course itself has been almost filled up and is utilized as a part of irrigation canal originated from the Pasar Baru Barrage. The width of the irrigation canal is about 7 m and the canal flows through the densely populated area of Teluknaga.

(ii) Left Bank between 9.2 k and 9.9 k

There exists a big oxbow lake of the former Cisadane river course with vast water area of around 9 ha on the left bank between 9.2 k and 9.9 k: there is no description of this lake on the topographic map with a scale of 1:25,000 issued in 1989. The lake is surrounded by relatively high former embankment of the Cisadane river. The relative height of the embankment from the water surface is estimated around 3 m, there is no survey result of this dike though.

(iii) Right bank at 13.1 k

There exists a distinct former river course with a circle shape on the right bank at 13.1 k near the north west edge of Cengkareng airport. The former river course forms deep sunken place. Some houses are located surrounded by this former river course.

(c) Bed Rock around 17.4 k

Tufaceous bed rock with gravel is exposed on the river bed from 17.4 k to 18.0 k. The bed slope forms stepwise shape in the reaches.

(d) Riverside Park in Tangerang

The right bank of the Cisadane river in the city area of Tangerang had been densely built-up area with no roadway. In April 1996, the area of about 1.3 km on the right bank was redeveloped as a riverside park with new roadway; the number of evacuated houses was 474 according to the local newspaper.

(3) Related Structures

(a) Embankment

The embanked reaches of the Cisadane river are located from 2.9 k up to around 17 k from the estuary. The reaches from 17 k up to Pasar Baru barrage form deeply dissected valley and has no embankment.

The artificial embankment is located on slightly high natural levee and accordingly the height of the artificial embankment is not so high.

(b) Bridge and Barrage

Pasar Baru barrage is located at the upper end of the objective reaches of the Master Plan (21.3 k). Kali Baru bridge at 6.4 k is the only bridge crossing the Cisadane river.

(4) Present Carrying Capacity

Present carrying capacity of the Cisadane river is estimated by using non-uniform flow formula based on the river survey results of feasibility study level conducted by the Study Team in 1996. The conditions for the calculation are shown below.

Calculation method

The same method described in Section 3.9 is adopted.

Tide level

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Spring tide of PP 1.15 m (approximately TTG 0.55 m) is adopted for the lower-end water level.

Manning's roughness coefficient

| 0.0 k - 12.7 k | 12.7 k - 21.3 k | |
|------------------------------|------------------|---------------|
| n=0.030 : low water channel | n=0.035 : low w | ater channel |
| n=0.050 : high water channel | n=0.050 : high w | vater channel |

The results are roughly summarized as follows (refer to Figure 5.5).

| Reaches | Bankfull (m ³ /s) 1.0 m freeboar | d (m³/s) |
|----------------|---|----------|
| 0.0 k - 3.5 k | 600 | 200 |
| 3.5 k - 12.7 k | 1,500 | 1,200 |
| 12.7 k - | 1,800 - 1,100 - 1,100 - 1,100 - 1,100 - 1,100 - 1,100 - 1,100 - 1,100 - 1,100 - 1,100 - 1,100 - 1,100 - 1,100 - | 1,500 |

5.1.3 On-going Flood Control Plan

In order to cope with the serious damage caused by the big floods in January and February 1996, the Government of Indonesia has promoted the program to execute urgent and short-term flood control works. These flood control programs will be executed in line with this present Study.

The work items related to the present Study are listed as follows:

1. Channel excavation including disposal of excavated material of the Western Banjir Canal : 8 km

- 2. Embankment improvement of the Western Banjir Canal : 18 km
- 3. Drainage improvement of the Ciliwung Drain (Manggarai Barrage Kapitol) : 8.4 km
- 4. Rehabilitation of slide gates of the Pasar Barn Barrage on the Cisadane river: 7 units

As already mentioned in Section 3.6, seven slide gates of the Pasar Baru Barrage on the Cisadane river do not function properly due to the deterioration. Accordingly, rehabilitation work of the gates will be implemented by this project.

5.2 Optimum Scale for Urgent Flood Control Project (1st Stage Project)

5.2.1 General

The flood control of the Western Banjir Canal and the Cisadane systems have been selected as priority projects.

But implementation of the priority projects on the Master Plan level at once needs huge project costs. Accordingly, effective stepwise implementation of the priority projects is required.

On the other hand, in January and February 1996, DKI Jakarta was hit by the worst floods of the Ciliwung river and the Western Banjir Canal (WBC) since World War II. Accordingly prompt action of flood control in DKI Jakarta is absolutely needed.

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In consideration of these above, urgent flood control project to be implemented immediately as 1st stage project should be formulated. The optimum scale of the urgent flood control project is discussed hereunder. In the discussion, cost and benefit are those in the master plan level in 1995. The subsequent feasibility study is conducted for the formulated optimum scale.

5.2.2 Alternative Schemes

(1) Basic Considerations

First of all, it is considered that the urgent flood control project (1st stage project) of the WBC should be a project which can cope with the flood of the same scale as that of big floods in 1996 in consideration of social aspects; it is said that the floods in 1996 were the biggest for the past 25 - 50 years.

The following four design scale alternative schemes have been examined for optimum scale of the urgent flood control project. The alternative schemes are shown in Table 5.1 and Figure 5.6.

| Alternatives | WBC | Ciliwung Floodway | Cisadane |
|--------------|-------------------|--|--------------------------------|
| Alt. 1 | M/P scale (1/100) | 2 tunnels (300 m ³ /s x 2 units), discharge volume: 600 m ³ /s | 1/50 (1,900 m ³ /s) |
| Alt, 2 | M/P scale (1/100) | 1 tunnel (300 m ³ /s x 1 unit), discharge volume: 300 m ³ /s | 1/25 (1,500 m ³ /s) |
| Alt. 2' | M/P scale (1/100) | 2 tunnels (300 $m^3/s \ge 2$ units), | 1/25 (1,500 m ³ /s) |
| Alt. 3 | 1/50 | discharge volume: 300 m ³ /s 1 tunnel (300 m ³ /s x 1 unit), discharge volume: 300 m ³ /s | 1/10 (1,200 m³/s) |

In Alt.2', only 300 m³/s is planned to be discharged to the floodway as the 1st stage; full scale discharge of 600 m³/s should be discharged after the completion of the river improvement of the Cisadane river, in the reaches downstream of the Pasar Baru Barrage, with the Master Plan level.

Concerning the WBC, the objective discharges for the river improvement of the Alt.2 and Alt.3 are also the same as that of the Alt.1 of which the safety level is once in 100 years. But the safety level of the Alt.2 and Alt.3 will be less than once in 50 years because only half of design discharge of the Ciliwung Floodway will be diverted to the Cisadane river.

(2) Alternatives of Cisadane River

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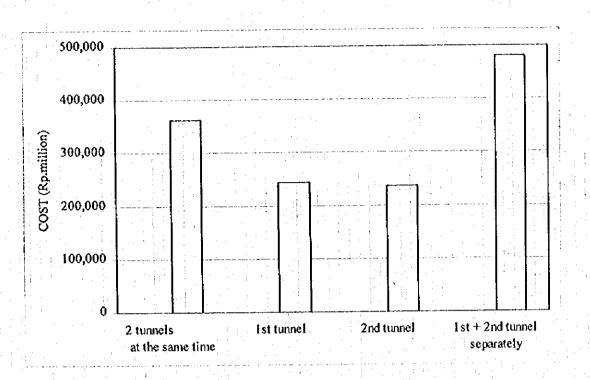
Each alternative has its own design scale of the Cisadane river from 10-year to 50-year. Here it is necessary to estimate work quantity of the Cisadane river improvement for the following economic evaluation. Preliminary design of the Cisadane river is roughly conducted based on the following considerations:

river improvement work of each alternative forms a part of the master plan;

- river improvement reaches of each alternative will be different according to each design discharge and present carrying capacity; and
- land aquisition in the 1st stage should be carried out according to the right of way of the master plan stage;

5.2.3 Comparison of Construction Cost of Ciliwung Floodway

The comparison of construction cost of the Ciliwung Floodway is studied as shown in the figure below. To construct two tunnels at the same time is cheaper than to construct 1st tunnel in the urgent flood control project and construct 2nd tunnel later in the master plan stage separately.



5.2.4 Evaluation and Conclusion

(1) Economic Evaluation

Economic evaluation is conducted for the alternatives as one aspect of project evaluation. Flood damage reduction benefits and financial project costs are estimated based on the method described in the Main Report for the Master Plan. The estimated EIRR and B/C are as follows: 0

| Alternatives | Flood reduction | Economic project cost | EIRR | B/C |
|--------------|-------------------------|-----------------------|--------|----------------------|
| : | benefit (Million Rp) | (Million Rp) | (%) (4 | discount rate : 12%) |
| Alt. 1 | 85,815 | 456,332 | 16.1 | 1.37 |
| Alt. 2 | 79,196 | 365,553 | 18.0 | 1.57 |
| Alt. 2' | 79,196 | 405,686 | 16.4 | 1.41 |
| Alt. 3 | 68,800 | 323,684 | 17.8 | 1.54 |

(2) Overall Evaluation

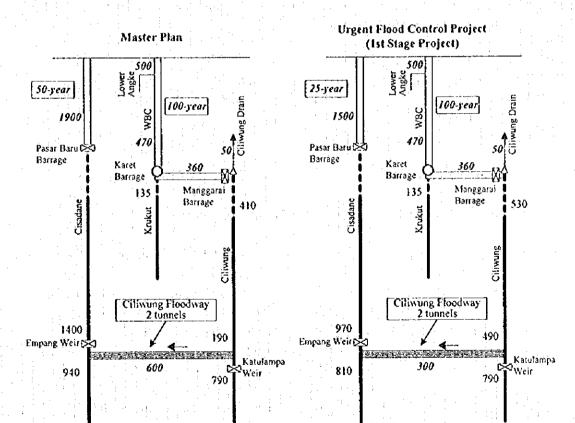
The Alt.2 has the highest EIRR and B/C. However, judging from technical viewpoint on construction of the tunnel, the Alt.2' has higher advantage than the Alt.2. The Alt.2' has

still higher EIRR and B/C than that of the Alt.1 i.e. the Master Plan stage and has same design discharge distribution with Alt.2.

As for the construction of the Ciliwung floodway, the two tunnels proposed in the master plan are to be constructed in advance during the stage of the urgent flood control project. The design discharge to the two tunnels is proposed temporarily to be 300 m³/s in accordance with the river improvement of the Cisadane river in downstream reaches with 25-year design scale.

The construction of 2 tunnels in advance is proposed with the consideration to the demerits such as various procedures, increase of the cost, negative impact of giving inconvenience to the surrounding residents and the others to be accompanied by future additional works.

Accordingly, the Alt.2' is selected as the optimum scale for the priority project to be implemented as an urgent flood control project (1st stage project).



The design discharge distribution thus proposed is as follows:

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5.3 Preliminary Design of Western Banjir Canal for Urgent Flood Control Project

Preliminary design of the Western Banjir Canal is conducted for the urgent flood control project (1st stage project).

5.3.1 Design Criteria

In principle, the design is conducted in accordance with the criteria in "Flood Control Manual in Indonesia" (hereinafter referred to as the Manual), which was prepared by DGWRD in collaboration with Canadian International Development Agency in 1993. The criteria in the Manual concerning the river improvement such as embankment, bridge clearance and others are shown in Table 5.2.

The following criteria in Japan are also referred to:

- Manual for River Works in Japan
- Cabinet Order concerning Structural Standards for River Management Facilities
- Latest Guideline for River Improvement in Japan published in 1996

According to the latest river improvement criteria in Japan (Guideline for River Improvement in Japan, 1996), it is desired to decrease construction and maintenance costs and to preserve environment as much as possible. However the latest guideline is applied for the WBC limitedly because of the following reasons:

- the WBC is an artificial floodway;
- it is necessary to increase the carrying capacity within the present right of way to avoid land acquisition in the densely populated area; and

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it is necessary no to raise the design high water level as much as possible to decrease the number of bridges to be reconstructed.

5.3.2 Treatment of Existing Flood Control Plans

(1) Master Plan for Drainage and Flood Control of Jakarta (1973)

The design of the WBC for 100-year flood was once prepared along the proposed extension of the WBC in "Master Plan for Drainage and Flood Control of Jakarta" formulated by NEDECO in 1973. However, the proposed extension was abandoned mainly because of the land acquisition problem. Accordingly, the existing WBC had no consistent design high water level until the following project determined the partial high water level in lower reaches in 1987. As the adopted elevation datum was PP, it is necessary to pay attention to use the data by PP datum with the data based on TTG datum in this Study.

The proposed alignment and longitudinal profile at that time are shown in Figures 5.7 and 5.8 respectively.

(2) West Jakarta Flood Control System Project III (1987)

The detailed design for the improvement of the WBC from the estuary up to the Teluk Gong siphon and the Angke Drain (Lower Angke river) was prepared in "West Jakarta Flood Control System Project III" (hereinafter referred to as the Detailed Design) in 1987. The

Angke Drain was planned to join the WBC with gravity drainage. As the adopted elevation datum was PP, it is necessary to pay attention to use the data by PP datum with the data based on TTG datum in this Study.

The outline of the Detailed Design of the WBC is as follows:

estuary - confluence of Angke drain : channel excavation and embankment works confluence of Angke drain - Teluk Gong siphon : embankment works

In principle, it is desired that the existing plan be introduced into this feasibility study as much as possible. However, it is necessary to modify the Detail Design near the estuary especially the embankment alignment because of the following changes of the situation since 1987:

short-cut works of the WBC near the estuary were completed in 1995, which was executed by using local budget and was not included in the Detailed Design;

a big scale residential development project is now already going on within the proposed embankment alignment by the Detailed Design near the Permai bridge; and

the condition at the estuary will be changed by reclamation project in future.

The proposed alignment, longitudinal profile and standard cross section are shown in Figures 5.9, 5.10 and 5.11 respectively.

5.3.3 River Improvement

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(1) Basic Improvement Items

The basic improvement items are summarized as follows (refer to Figure 5.12):

Estuary (0.0 k) - Confluence of Angke Drain (2.9 k)

- new embankment or raising of present embankment with sodding
- no parapet wall is included
- widening and excavation of low water channel
- no revenuent for standard slope of 1:2.0
- low water channel revetment for some water colliding fronts

Confluence of Angke Drain (2.9 k) - Karet Barrage (12.4 k)

- raising of present embankment as occasion demands
- no parapet wall is included
- widening and excavation of low water channel as occasion demands
- revetment works and asphalt pavement for embankment
- (both banks; 2.9 k 11.3 k, only left bank; 11.3 k 12.4)
- no low water channel revetment for standard slope of 1:1.5
- low water channel revetment for some steep slope portions of 1:1.0

Karet Barrage (12.4 k) - Halimum Bridge (15.2 k)

- no raising of present embankment
- no embankment on left bank
- sodding on right embankment as occasion demands
- widening and excavation of low water channel as occasion demands
- no low water channel revetment for standard slope of 1:1.5
- low water channel revetment for some steep slope portions of 1:1.0

Halimun Bridge (15.2 k) - Manggarai Barrage (16.9 k)

- no embankment
- channel excavation as occasion demands*
- *

The WBC has no banquette in this reaches and the relative height from the ground to the design river bed is around 10 m in places. According to the information from PPWSCC, it is possible to excavate up to 12 m by the backhoe shovel equipped with attachment; the total arm length is 15 m.

(2) Design Discharge

As already discussed in Section 5.2, the design discharge distribution for the urgent flood control project (1st stage project) is the same with the master plan scale of 100-year.

| - | Estuary (0.0 k) - Angke Drain (2.9 k) | : 500 m³/s |
|---|--|-------------------------|
| - | Angke Drain (2.9 k) - Krukut River (12.4 k) | : 470 m³/s |
| - | Krukut River (12.4 k) - Manggarai Barrage (16.9 k) | : 360 m ³ /s |

These are revised value in the feasibility study stage as already discussed in section 4.6.

(3) Objective Reaches

The objective reaches of the river improvement for the urgent flood control project (1st stage project) are approximately 17 km from the estuary up to the Manggarai Barrage.

(4) Right of Way

According to the present legislation, the authorities should acquire and control overall land to a distance of 5 meters beyond the outside toe of embankments as a right of way of river. However, this right of way of 5 m is not included as an objective area for land acquisition in consideration of present densely urbanized land use situation and difficulties of land acquisition along the WBC.

(5) Alignment

In principle, proposed alignment of the WBC is on the existing one except near the estuary to avoid any land acquisition.

Near the estuary, newly constructed embankment of PP. 3.5 m between the forest reservation area and the new residential development of Pantai Indah Kapuk is utilized as the left embankment of the WBC. The area between the WBC and the new embankment can function as a natural retarding basin effectively and can make the flood water level lower.

The proposed design alignment is shown in Figure 5.13.

(6) Water Level at Estuary

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The water level of TTG 0.85 m (approximately PP 1.45 m) is adopted at the present estuary. This is the same figure adopted in the present Detailed Design. The channel to be prepared in the future reclaimed area by PANTURA as the continuation of the WBC should be designed not to give any raise of design high water level proposed by this WBC improvement plan. The condition required is already discussed in Section 4.7.

(7) Longitudinal Profile

In general, it is desirable to consider the followings to determine the design longitudinal profile:

the high water level should be designed to be slightly lower than (at least approximately equal to) the both side's ground elevations; and

the design river bed should be designed to have similar gradient of the present average river bed.

However, as the WBC flows through in densely populated area and has many related structures such as drainage facilities, pumping stations, bridges, siphons, barrages and so on, the following considerations are also introduced in the plan:

It is absolutely necessary to cope with the new increased design discharge within the present right of way to avoid the serious social impact concerning the land acquisition: the design high water level will become higher than that of the ground elevation in the reaches downstream of the Karet Barrage;

On the other hand, from the viewpoint of the clearance of the bridges on the WBC; it is desirable to make the design high water level lower to avoid reconstruction of the bridges as much as possible;

It is necessary not to change the high water level drastically from that in existing WBC improvement plan especially at the confluence of the Augke Drain; and

It is necessary to pay attention to the elevation of three siphons which go under the WBC to determine the design river bed elevation.

The design longitudinal profile is shown in Table 5.3 and Figure 5.14.

The sand bar at the estuary is estimated to be flushed in flooding time, detail study might be needed in the detail design stage though.

The design high water level is proved to be appropriate by non-uniform flow calculation as shown in Figure 5.15 based on the actual design cross sections of Figure 5.18. The backwater effect by the bridge piers is evaluated by using the D'Aubuisson's formula in this non-uniform flow calculation.

(8) Cross Sectional Profile

The proposed criteria for minimum condition of embankment of the WBC is shown in Table 5.4.

The design river width and low water channel width are determined based on that of the present as shown in Figure 5.16.

In the Master Plan stage, the sideslopes of the standard cross sections from the confluence of the Angke Drain up to the Manggarai Barrage were determined in accordance with the minimum embankment sideslopes of 1:2 in the Manual.

However, it is necessary to decrease land aquisition as much as possible to avoid the serious social impact. Accordingly, it is necessary to adopt steeper sideslopes of 1:1.5 to cope with the increased design discharge within the present right of way. Sideslopes of 1:1.0 is adopted in some critical portions with narrow channel width.

If the present river width is wider than that of the standard cross section, the present river width is preserved as it is. If the present river bed is deeper than that of the design river bed, the present river bed is preserved as it is, too.

The standard cross sections are prepared as shown in Table 5.5 and Figure 5.17. The actual design cross sections are shown in Figure 5.18.

(9) Manning's Roughness Coefficient

The following Manning's roughness coefficients (n) are adopted:

- 0.025 : low-water channel

- 0.040 : high-water channel

These are the same figures as that of the plan in the proposed Eastern Banjir Canal.

(10) Freeboard

According to the Manual, the minimum required freeboard corresponding to the design discharge is 0.8 m. However, the freeboard of 1.0 m is adopted taking into account the importance of the to-be protected area and the margin for future envisaged land subsidence.

This freeboard of 1.0 m was also adopted in detailed design of lower reaches of the WBC by "West Jakarta Flood Control System Project III (1987)". The freeboard of 1.5 m had been

adopted in NEDECO's mater plan in 1973.

Freeboard of 0.6 m is adopted where the design high water level is lower than the ground elevation.

(11) Inspection Road

Inspection road with minimum 3 m width is provided on both embankments where there is no road available along the WBC at present.

Special attention will be needed to the riverside park on the right bank from the M. II. Thamrin bridge up to the Sukabumi bridge to harmonize the function of flood control and promenade.

(12) Revetment

Embankment

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Revetment of wet masonry on the side slopes of the embankment and asphalt pavement on the crown are provided in the following reaches in the same way as the present.

Confluence of the Angke drain (2.9 k) - Aipda K. S. Tubun bridge (11.3 k) : both banks Aipda K. S. Tubun bridge (11.3 k) - Karet barrage (12.4 k) : left bank only

The reasons why the embankment revetment is requited are as follows:

the proposed embankment dimension is required minimum;

- flood continuation time is quite long as already proved by 1996 big floods; and

the revetment is useful as a measure for excess flood.

River channel

Low and high water channel revetments are provided in the following portions:

confluence of tributaries (Angke drain, Krukut river, Cideng drain)

near structures such as bridges, barrages and pumping stations

Low water channel revenment is provided in the following portions:

water colliding front along the meandering teaches of Muara Angke steeper stope portions than 1:1.0

In upstream reaches from K. H. Mas Mansyur bridge (13.1 k), it is desirable to pay attention in revetment works not to spoil the view along the WBC as a riverside park.

5.3.4 Bridge

(1) Freeboard

(a) Design Criteria

Here, there are following design criteria for bridges freeboard:

1) Bina Marga

According to the Manual, Bina Marga requires minimum freeboard of 1.5 m above bankfull flood.

However, if this criteria is adopted, more than half of present bridges crossing the WBC do not satisfy the criteria. It is practically impossible to adopt this criteria judging from the serious social impact caused by the interruption of heavy traffic of those bridges.

2) Cabinet Order concerning Structural Standards for River Management Facilities, etc. in Japan

"Cabinet Order concerning Structural Standards for River Management Facilities, etc. in Japan" requires the same freeboard as the embankment freeboard; the minimum freeboard of 0.8 m is required in the WBC from the design discharge of under 500 m³/s excluding no embankment reaches of 0.6 m freeboard in the upstream end. The soffit elevation of bridge girder and required freeboard line are shown in Figure 5.19.

(b) Considerations

Bridges lower than proposed HWL

The following two bridges have extremely low girders and the girder soffit elevations become lower than that of the proposed HWL. Those bridges are required to be reconstructed.

- Prof. Dr. Latumeten bridge (6.9 k)
- Kyai Tapa bridge (8.4 k)

Bridges lower than freeboard line

According to the above criteria 2), the girder soffit elevation of following five bridges are higher than HWL but still lower than minimum freeboard line. Those bridges are fundamentally necessarily to be reconstructed.

- Teluk Gong Raya bridge (5.0 k)
- Railway bridge (future) (7.9 k)
- Railway bridge on Karet barrage (12.4 k)
- K. H. Mas Mansyur bridge (13.1 k)

Roadway bridge on Manggarai barrage (16.9 k)

The reconstruction of those five bridges will be an obstacle and seems to be practically difficult judging from the present extremely heavy traffic situation in the central DKI Jakarta. However, the project cost is estimated by the reconstruction of seven bridges including above five bridges in accordance with the criteria in this feasibility study stage. Further consideration concerning the treatment of those five bridges will be needed in the succeeding detailed design stage.

(2) Protection of Pier

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Some protection works for the following eight bridge piers will be needed resulting from the channel widening and excavation works.

- Mandara Permai bridge (1.9 k)
- Tol Airport Cengkareng bridge (2.7 k)
- Access bridge to Tol Airport Cengkareng (2.9 k)
- Tol Road bridge (4.7 k)
- Pangeran Tubagus Angke bridge (5.6 k)
- Tomang flyover (9.4 k)
- New flyover near TN. Abang Station (10.7 k)
- Aipda K. S. Tubun bridge (11.3 k)

5.3.5 Barrages

(1) Karet Barrage

The Karet Barrage will remain for flushing of the Krukut Drain in future. The flood water levels at the barrage are roughly estimated by using non-uniform flow calculation in order to know the carrying capacity and backwater as shown in Figure 5.20. The backwater caused by the barrage is estimated within 50 cm even by the new design discharge of 470 m³/s. It is concluded that the barrage has enough carrying capacity and the improvement of the barrage is basically not necessary.

(2) Manggarai Barrage

It is said that the Manggarai barrage dammed up the flow by about 3 m in height in January 1996 flood, because the flow width was quite narrow. The estimated flood water levels at the barrage by non-uniform flow calculation in Figure 5.20 coincide well with the actual situation.

Improvement of the barrage is necessary because the carrying capacity of the barrage is not enough for the design discharge of 360 m³/s and the improvement can also make lower the flood water level of upper side of the barrage.

In view of the present condition, installation of a new opening on the right bank is proposed.

The effects of a new opening with several width are roughly estimated by non-uniform flow calculation as shown in Figure 5.21. The opening width is enough if the width of 5.5 m (same as the present gate width) is adopted. The facility aspects is discussed in ANNEX 8.

5.3.6 Treatment of Tributaries

(1) Krukut River

The Krukut river is treated as flood plain zoning area in the Master Plan to preserve flood retarding function; the Krukut river is not objective reaches for river improvement.

(2) Drainage Channels

The following two urban drainage channels which join the WBC with gravity drainage are now treated as an urban drainage channel under the control of DKI Jakarta.

Angke Drain

The HWL and design river bed of the WBC is determined TTG 1.68 m and -3.92 m (approximately PP 2.28 m and -3.32 m) respectively at the confluence of the Angke Drain (2.9 k). On the other hand, according to the detailed design of "West Jakarta Flood Control System Project III (1987)", the HWL and design river bed of the lower end of the Angke Drain have been PP 2.30 m and -3.00 m respectively. Therefore, there is little influence for the present detailed design of the Angke Drain.

Cideng Drain

In January 1996 flood, the flood water of the WBC flowed backward to the Cideng Drain and flowed into the Setiabudi regulation ponds through the lower portion of the embankment of the drain. The embankment of the drain in the reaches near the WBC was already heightened after the floods.

The flood water of the Cideng drain is also drained to the WBC through the Cideng pumping station. The HWL of the WBC is determined TTG 3.98 m (approximately PP 4.58 m) at the pumping station (9.5 k). On the other hand, according to the detailed design of "West Jakarta Flood Control System Project (1986)", the HWL of the WBC have been partly assumed to be PP 5.00 m. Therefore, there is no bad influence for the present pumping station.

5.3.7 Proposed Project Works

The major required project works in the urgent flood control project (1st stage project) for the priority projects are as follows (in detail refer to ANNEX 8):

| · | Work Item | Unit | Quantity |
|---------------------------------------|--|-----------------|------------|
| 1 1. | Land Aquisition and Compensation | | - <u> </u> |
| | Land aquisition House | ha nos. | 0.0 C |
| 2. | Channel Improvement (L=16.9 km) | | |
| | Preparatory Excavation and dredging | ls m³ | 1,354,000 |
| | Embankment | in ³ | 1,334,000 |
| | Low and high water channel revetments (around tributaries and related structures) | m² | 17,100 |
| · · · · · · · · · · · · · · · · · · · | Low water channel revetment (water colliding front, steep slope) | m² | 24,700 |
| | Embankment protection | | |
| | -Wet masonry | m² | 72,300 |
| | -Sod facing | - m² - | 42,900 |
| | Asphalt pavement of embankment crown | m^2 | 25,100 |
| | Drop structure | nos. | 0 |
| · · · · · | Construction of new drainage structure | nos. | 4 |
| • | Improvement of existing drainage structure | nos. | 3 |
| | Reconstruction of existing bridges | nos. | 7 |
| | Construction of New Opening at Manggarai Barrage | nos. | · 1 |

5.4 Preliminary Design of Cisadane River for Urgent Flood Control Project

Preliminary design of the Cisadane river is conducted for the urgent flood control project (1st stage project) here.

5.4.1 Design Criteria

In principle, the design of the Cisadane river is conducted in accordance with the same criteria as adopted in the design of the WBC.

The following considerations based on the latest river improvement criteria in Japan (Guideline for River Improvement in Japan, 1996) are also introduced positively to determine the design:

same design high water level is adopted in the urgent flood control project (1500 m³/s) and Master Plan stage (1900 m³/s);

- widening and excavation of low water channel should be limited as much as possible in order to maintain the natural stability of present channel, to decrease the construction and maintenance costs, and to preserve the present environment;
- if the present embankment is located extremely close to the water colliding front, setting back of embankment is adopted to avoid failure of embankment due to scoring;

revetment works should be limited as much as possible;

former river course and oxbow lake should be treated as a part of river and included within the embankment alignment to preserve it's natural retarding effect and environment: no need to maintain uniform river width; and 0

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ground clearing of high water channel should be limited as much as possible to preserve riverside forest and environment, since the flood discharge on high water channel is limited and river side forest can decrease the hydraulic energy force against embankment.

5.4.2 River Improvement

(1) Basic Improvement Items

The basic improvement items for the urgent flood control project (1st stage project) are summarized as follows (refer to Figure 5.22):

0.0 k = 1.8 k

- no river improvement

1.8 k - 3.5 k

new embankment

3.5 k - 7.7 k

- raising of present embankment as occasion demands
- setting back of embankment as occasion demands
- low water channel revetment for some water colliding fronts

7.7 k - 11.8 k

- raising of present embankment as occasion demands
- setting back of embankment as occasion demands
- widening and excavation of low water channel as occasion demands
- low water channel revetment for some water colliding fronts

11.8 k - 16.8 k

- raising of present embankment as occasion demands .
- setting back of embankment as occasion demands

16.8 k - 21.3 k (Pasar Baru Barrage)

no river improvement

(2) Design Discharge

As already discussed in Section 5.2, the design discharge for the urgent flood control project (1st stage project) is 1,500 m³/s; the design scale is 25-year.

(3) Objective Reaches

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The objective reaches of the improvement are determined from 1.8 k up to 16.8 k of the upper end of embanked reaches based on the present carrying capacity (refer to Section 5.1). There is no need of river improvement from the estuary to 1.8 k because of the following reasons:

It is necessary to keep the water of fish pond brackish;

There will be not so many property to be protected even in future; and

The geological condition near the estuary will not be suitable for the embankment.

The upstream reaches from 16.8 k to the Pasar Baru barrage are not objective reaches for the urgent flood control project (1st stage project), present roadways along the both river banks should be preserved as inspection road though.

(4) Right of Way

In principle, overall lands to a distance of 5 meters beyond the outside toe of embankments is treated as right of way of river in accordance with the Manual.

(5) Alignment

The proposed embankment alignment is shown in Figure 5.23.

(6) Water Level at Estuary

The proposed high water level of the Cisadane river is rather high and the mangrove forest around the estuary will be kept as it is by the reclamation plan by KAPUKNAGA.

However, the channel to be prepared in the future reclaimed area by KAPUKNAGA as the continuation of the Cisadane river should be designed not to give any raise of design high water level proposed by this Cisadane improvement plan. The condition required is already discussed in Section 4.7.

(7) Longitudinal Profile

The design longitudinal profile is shown in Table 5.6 and Figure 5.24.

According to the sounding survey result around the estuary conducted by the Study Team in 1996, the sea-bed is relatively shallow. However, the sand bar at the estuary is estimated to be flushed in flooding time and the proposed design high water level is high enough, no matter how the sand bar will be flushed. Detail study might be needed in the detail design stage about this matter.

The slope of the river bed and ground clearly change around 12.7 k. It should be avoided to determine the design river bed elevation too low: bed rock is exposed on some river bed especially around 17.5 k as already mentioned in Section 5.1.

The design high water level is proved to be appropriate by non-uniform flow calculation as shown in Figure 5.25 based on the actual design cross sections of Figure 5.27. The spring tide of TTG 0.55 m (approximately PP 1.15 m) is adopted at the present estuary for the non-uniform flow calculation.

(8) Cross Sectional Profile

The design river width and low water channel width are determined based on that of the present as shown in Figure 5.26.

If the present river width is wider than that of the standard cross section, the present river width is preserved as it is. If the present river bed is deeper than that of the design river bed, the present river bed is preserved as it is, too.

The standard cross sections are prepared as shown in Table 5.7 and Figure 5.27. The actual design cross sections are shown in Figure 5.28.

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(9) Manning's Roughness Coefficient

The following Manning's roughness coefficients (n) are adopted:

| 1.8 k - 12.7 k | 12.7 k - 16.8 k |
|------------------------------|------------------------------|
| n=0.030 : low water channel | n=0.035 : low water channel |
| n=0.050 : high water channel | n=0.050 : high water channel |

(10) Freeboard

The freeboard of 1.0 m corresponding to the design discharge of $1,500 \text{ m}^3/\text{s}$ is adopted in accordance with the Manual.

(11) Inspection Road

Inspection road of 5 m width is provided on both embankments.

(12) Revetment

Some low water channel revetment works are required in water colliding fronts.

5.4.3 Related Structures

(1) Bridge

8. 8 Kali Baru bridge (6.4 k) is the only bridge along the objective reaches. The girder elevation of TTG 7.0 m has enough clearance against the design high water level. There is no need to reconstruct this bridge.

It is not necessary to consider the protection of the bridge piers, since there is no excavation works there.

(2) Pasar Baru Barrage

As already mentioned in Section 5.1, the rehabilitation work of the Pasar Baru barrage will be implemented by the Project Type Sector Loan of OECF as a part of short-term flood control program. Accordingly the rehabilitation works of the barrage is not included in the objective of the Study.

5.4.4 Proposed Project Works

The major required project works in the urgent flood control project (1st stage project) for the priority projects are as follows (in detail refer to ANNEX 8):

| | Work Item | Unit | Quantity |
|-----|--|----------------|----------|
| 1 | Land Aquisition and Compensation | | |
| 1. | Land Addisition and Compensation | | |
| | Land aquisition | ha | 45.3 |
| | House | nós. | 460 |
| 2. | Channel Improvement (L=15.0 km) | | |
| | Preparatory | ls | 1 |
| | Excavation and dredging | m³ | 825,000 |
| | Embankment | m ³ | 913,000 |
| | Low water channel revetment | m ² | 8,400 |
| . • | Drop structure | nos. | 0 |
| · . | Construction of new drainage structure | nos. | 3 |
| 4. | Improvement of existing drainage structure | nos. | 2 |
| | Reconstruction of bridge | nos. | C |

The number of houses to be expropriated were counted by using the topographic maps with a

scale of 1:5,000 prepared by the Study Team in 1996. The number might include not only human habitation but also warehouse, livestock house and so on, since it is impossible to distinguish the type of house by the maps. Accordingly, it is necessary to investigate and classify those houses in the proceeding detailed design stage.

5.5 Preliminary Study on Ciliwung Floodway Route

5.5.1 Introduction

The location of Ciliwung Floodway was once proposed in the master plan based on the topographic map with the scale of 1:25,000 that was the only available map in that stage. The map was the one issued in 1989 based on the aerial photographs taken in 1981/1982.

Since the information of the map was rather old, and the information on the map was not much detailed, alternative study on the location of Ciliwung Floodway in this feasibility study stage has been conducted based on the above-mentioned topographic map and aerial photographs with a scale of 1:5,000 taken in May, 1996.

The alternative study has been conducted with two stages: an alternative study on the general location of Ciliwung Floodway and a study on the rather detailed location of the inlet and outlet facilities.

Detailed route study is conducted in succeeding section 4.4 based on the results of the topographic survey of the floodway area that has been conducted in this feasibility study stage.

5.5.2 Alternative Study on General Location

(1) Conceivable Route

As a general rule, it is desirable that the Ciliwung Floodway be an open channel floodway which connects the Ciliwung and the Cisadane rivers with the shortest route. However, it is inevitable that the Ciliwung floodway becomes a tunnel floodway to avoid the serious land acquisition problem in the densely populated area of Bogor city. The southern part of the Bogor city is the only area to satisfy the conditions for construction of floodway tunnel such as:

- enough overburden depth; and

- short distance between the Ciliwung and the Cisadane rivers.

Conceivable alternative routes of the proposed Ciliwung Floodway are shown in Figure 5.29. Alt.1 is the shortest route from the Ciliwung to the Cisadane rivers. Alt.2 connects the Ciliwung and Cisadane rivers through the Cipaku river, small right tributary of the Cisadane river.

In downstream reaches of the Alt.1, the floodway must be constructed by open channel

because of shortage of relative height between the elevation of the Ciliwung river bed and the terrace on which the city area of Bogor is located. Construction of the floodway with open channel may cause not only serious land aquisition problem but also interruption problem of north-south traffic and canals in the center of city area. Accordingly construction of the floodway with open channel in this stretch is considered practically impossible.

Towards the upstream reaches of the Alt.2, the distance between the Ciliwung and Cisadane tivers increases. Besides the improvement length of the Cipaku river increases. Accordingly the upstream area of the Alt.2 is not considered for the conceivable route of the floodway.

(2) Comparative Study

(a) Land Use

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According to the aerial photographs with a scale of 1:5,000 taken in May 1996, the area along alternative routes has already been urbanized mainly as residential area with one and/or two stories houses. The extent of urbanization is almost the same between the areas along two alternative floodway routes.

The land use condition in the topographic map with a scale of 1:25,000 is quite different from that of the present, since the map was prepared based on the aerial photographs taken in 1981/1982. The land use condition in some Bogor city map on the market is also different from that of present,

(b) General Longitudinal Profile

General longitudinal profiles along the two alternative routes are prepared as shown in Figure 5.30, by using 12.5 m pitch contour line on the topographic map with a scale of 1:25,000.

The overburden depth along the Alt.1 is around 30 m, even though relatively low elevation portion near a small river exists in the middle of the route. On the other hand, the overburden depth along the Alt.2 is around 20 m. The average gradient of both alternatives from the Ciliwung to Cisadane rivers is approximately i=1/100.

(c) Selection of Optimum Route

In consideration of the following aspects, the Alt.1 is adopted as the optimum floodway route:

Alt.1

- total floodway length is short (approximately 1 km);
- no serious land acquisition problem may be caused because of its short open channel stretch; and
- this route has smooth bifurcation alignment from the Ciliwung river and has smooth confluence alignment with the Cisadane river.

Alt.2

- total floodway length is long (approximately 1.5 km);
- the Cipaku river which forms downstream reaches of the floodway is a very small river, with the basin area of only about 6 km², and accordingly overall widening and straightening of the river are required;
- the river-bed of the Cipaku river consists of rock at location and accordingly there will be difficulties in excavation work even for open channel; and

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land aquisition problem may be caused because many houses are existing along the Cipaku river.

5.5.3 Study on Location of Inlet and Outlet Facilities

Here the discussion on the locations of inlet and outlet facilities are presented hereunder. The details are discussed in ANNEX 8 (Design and Cost Estimate).

(1) Location of Inlet Facilities

For selection of inlet facilities location, the following criteria have been considered:

- 1. the location of fixed weir to keep the water-level of the Ciliwung river at certain level before diversion of flood should be considered,
- 2. accordingly the longitudinal sloe of the river-bed of the Ciliwung river should be rather gentle one. Too much steep slope causes much more height of fixed weir,
- 3. location of temporary diversion channel of the Ciliwung river during the construction work, should be taken into consideration to avoid human resettlement as much as possible,
- 4. the land on the left side of the Ciliwung river should be as high as possible to have enough overburden depth above the tunnel, and to avoid human resettlement as much as possible,
- 5. the location of access road for tunnel construction works should be taken into consideration to avoid human resettlement as much as possible,
- 6. the alignment of the Ciliwung river to the tunnel should be a smooth one to lead much part of flood discharge of the Ciliwung river to the Cisadane river,
- 7. the river width should be as uniform as possible around the inlet.

The river-bed of the Ciliwing river has a rather sharp natural drop just downstream of the proposed site. Accordingly the intet facilities should be located upstream of the drop.

In the reaches upstream of the bridge over the Ciliwung river, the left side land has rather gentle side slope to the low water channel and may houses are located on the slope close to the low water channel. Accordingly the inlet facilities should be located downstream of the bridge site.

Temporary diversion channel of the Ciliwung river should be constructed on the right side of the river in due consideration of the present situation. Accordingly the location of the inlet

facilities should be the place where the houses are not many on the right side of the river. The presently proposed site is the better place than other sites to satisfy the condition.

The presently proposed site is better than the other locations to satisfy the conditions for an access road for construction works.

(2) Location of Outlet Facilities

For selection of outlet facilities location, the following criteria have been considered:

1, the Ciliwung Floodway should join the Cisadane river with a smooth alignment,

2. human resettlement for the construction of floodway should be as less as possible,

- 3. the location of access road for floodway construction works should be taken into consideration to avoid human resettlement as much as possible,
- the river width of the Cisadane river should be as uniform as possible for smooth flow of sediment in.

The presently proposed site is the only place for the Ciliwung Floodway to join the Cisadane river with a smooth alignment.

Some houses are located rather close to the low water channel in the reaches downstream of presently proposed site.

Grave yard and military facilities are located on the right side of the river in further downstream reaches, and Ciliwung Floodway should avoid to pass underneath these facilities.

The river width of the Ciliwung river has rather uniform river width near the presently proposed site for the outlet.

5.6 Non-structural Measures

5.6.1 General

(1) Flood Risk Map

Low-lying area of DKI Jakarta has been suffering from habitual inundation for many decades. In order to cope with this, the Ministry of Public Works has been implementing various flood control and drainage projects in the area.

But the implementation of the flood control and drainage master plan in the area still needs much fund and time to be completed. And since the area is fundamentally located in the flood plain, even after completion of those flood control and drainage projects in line with the master plan, the area will be still subject to flooding. The causes may be failure of facilities, failure of operation of facilities, limitation of design scale, human activities against flood control and drainage facilities such as garbage dumping to river area or illegal structure construction in river area and others, abnormal high tide, other abnormal natural phenomena,

Due to these reasons, non-structural measures for flood damage mitigation is inevitable in addition to structural measures. Flood risk map in low-lying area of DKI Jakarta is thus prepared as one of such non-structural measures.

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(2) Flood Warning System

etc.

Since the flood of the Ciliwung river is to be diverted to the Cisadane river, it is necessary to improve the Cisadane river in its downstream reaches where the carrying capacity is not enough for the design discharge. But in addition to the river improvement of the Cisadane river, establishment of flood warning system for the Cisadane river is also required. As observed in the flood in January 1996, the river flow of the Cisadane river in Bogor city was just in a normal situation on the day when the big flood of the Ciliwung river attacked Bogor city and DKI Jakarta. Accordingly a flood warning system for the Cisadane river is indispensable for the projects.

5.6.2 Flood Risk Map

(1) General

Flood risk map is prepared to the condition that inundation would occur when failure of dike happens and the failure of dike may occur at any place in the objective reaches of the river during a flood of design discharge hydrograph

(2) Objective Area

The objective area of flood risk map covers the area of downstream basin of the Cengkareng Floodway, the Ciliwing, the Western Banjir Canal, the Cipinang, the Sunter, the Jatikramat, the Buaran, and the Cakung rivers. The area is about 500 km² wide.

(3) Flood Risk Map

The prepared flood risk map is shown in the MAIN REPORT (Feasibility Study).

5.6.3 Flood Warning System

(1) Present Situation of River Use

The present situation of river use of the Cisadane river in the reaches downstream of the outlet site of the Ciliwung floodway is as follows:

(a) Just downstream site

The area is in the city of Bogor and the river is used for washing, playing and fishing. In the reaches just upstream of Empang barrage, river is used for inland fishery, sand mining, and

water intake by Empang barrage.

(b) In the middle reaches

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The area is outside of Bogor city and the Cisadane river forms a very deep valley. The river is used for sand mining at places and partly for upland cropping.

In the reaches just upstream of Pasar Baru Barrage, the area is located in Tangerang city. The river water level is kept high by the Pasar Baru Barrage and the urban area is just close to the river water surface.

(c) In the downstream reaches (to the river-mouth)

In the reaches just downstream of Pasar Baru barrage, river water in dry season is very little since the river water is taken for irrigation purpose by the barrage. Since there exists only one bridge in the reaches, many ferry facilities are found. In the reaches near the estuary, water transportation and sand mining are found.

(2) Flood Propagation

From the outlet site of the Ciliwing floodway to the site of Pasar Baru barrage, the river length is about 85 km. Accordingly the propagation time of flood from the outlet of the Ciliwing floodway to the Pasar Baru barrage site is estimated to be about 8 hours. The Cisadane river in the reaches forms a very deep valley and the flood peak in the upstream reaches decreases so much.

Accordingly, by the diversion of flood of the Ciliwung river to the Cisadane river, the river water level of the Cisadane river will rise rapidly in the reaches just downstream of the outlet site, but it will not rise so rapidly in the middle and downstream reaches of the Cisadane river.

In the middle reaches of the Cisadane river, many tributaries join the Cisadane river. Accordingly for the proper operation of the Pasar Baru barrage, the information on flood not only about the flood from the Ciliwung floodway, but also about floods from the many tributaries are needed.

(3) Basic Concept of Flood Warning System

Basic concept of flood warning system for the Cisadane river is that information on flood diversion from the Ciliwung river to the Cisadane river should be conveyed to the society of the riverine area along the Cisadane river before the flood reaches the objective area. And the monitoring system for flood of the Ciliwung and Cisadane rivers should be established for that purpose.

(4) Flood Warning System

(a) Monitoring Site

The following should be the monitoring sites for flood warning:

1) inlet site of the Ciliwung floodway (Katulampa barrage as supplementary site)

- 2) outlet site of the Ciliwung floodway
- 3) Empang barrage
- 4) Serpong water-level gauging station
- 5) Pasar Baru barrage
- 6) Depok
- 7) Manggarai

(b) Facilities and Functions

| 1) Inlet site | : radio communication for downstream sites | |
|----------------------|---|--|
| 2) Outlet site | : radio communication for upstream and dov | viistream sites |
| | warning to the riverine area by sirens | e de la constante de la constan La constante de la constante de |
| 3) Empang barrage | : radio communication for upstream and dov | vnstream sites |
| | warning to the riverine area by sirens | |
| 4) Serpong site | : telemetering for downstream sites | |
| 5) Pasar Baru barrag | e : radio communication with upstream sites | |
| | warning to the riverine area by siren car | |

(c) Network System

The proposed network system for flood warning and reporting is shown in Figure 5.31.

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5.7 Preliminary Design of Cisadane River for 2nd Stage Project

(1) General

The preliminary design of the Cisadane river for the urgent flood control project (as 1st stage project) is already presented with a design scale of 25-year ($Q=1,500 \text{ m}^3/\text{s}$) as shown in section 5.4.

Here, the preliminary design of the Cisadane river is presented for the succeeding works for the Master Plan with a design scale of 50-year ($Q=1,900 \text{ m}^3/\text{s}$) (as 2nd stage project). The objective reaches are from 1.8 km to 20.1 km. Judging from the present carrying capacity, river improvement works is not required in the reaches from 20.1 km to Pasar Baru Barrage (21.3 km).

(2) River Improvement

The design criteria to be applied is basically the same with that for the urgent flood control (1st stage project). Accordingly, there is no change of the design river width and the design high water level in the objective reaches of the urgent flood control project (1.8 km - 16.8

km). The major additional work items for upgrading from 25-year to 50-year are as follows:

widening of low water channel in the reaches from 4.3 km to 10.8 km; and new embankment along new objective reaches from 16.8 km to 20.1 km

The proposed alignment, the design longitudinal profile, the design cross sections and the related tables are compiled in VOLUME VI (SUPPLEMENTAL STUDY).

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(3) Proposed Project Works

The major required project works for the Master Plan are as follows:

Additional Works from 25-year to 50-year Design Scale Unit Quantity Work Item Land Aquisition and Compensation ۱. 3.4 Land aquisition ha 60 nos. House Channel Improvement (L=18.3 km) 2. Is Preparatory 1,271,000 m^3 Excavation and dredging 98,000 m³ Embankment Low water channel revetment m² nos. Drop structure Construction of new drainage structure nos: Improvement of existing drainage structure nos. Reconstruction of bridge nos.

| Work Item | Unit | Quantity |
|--|----------------|-----------|
| 1. Land Aquisition and Compensation | **** | |
| Land aquisition | ha | 48.7 |
| House | nos. | 520 |
| 2. Channel Improvement | | |
| Preparatory | ls | 1 1 |
| Excavation and dredging | mi | 2,096,000 |
| Embankment | m ³ | 1,011,000 |
| Low water channel revetment | m² | 8,400 |
| Drop structure | nos. | 0 |
| Construction of new drainage structure | nos. | 3 |
| Improvement of existing drainage structure | nos. | 2 |
| Reconstruction of bridge | nos. | 0 |

Project Works from Present Condition to 50-year Design Scale

6 RECOMMENDATIONS

In view of the serious direct and indirect damages and confusion due to the big flooding in January and February 1996 in DKI Jakarta, it is proposed that the urgent flood control project be implemented very soon as an urgent scheme.

The following recommendations on the flood control master plan and the feasibility study are also proposed.

6.1 Master Plan

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(1) Eastern Banjir Canal

In the present study on the flood control master plan in JABOTABEK area, construction of the Eastern Banjir Canal is proposed as the flood control measure for the eastern part of DKI Jakarta. But the plan needs huge amount of land acquisition cost even though the plan claims the least cost among other alternatives plans. Accordingly it seems that the preparation of such huge amount of land acquisition cost would be very difficult.

But according to the information on PANTURA DKI Jakarta (reclamation plan along the north coast of Jakarta), they are planning to utilize the Eastern Banjir Canal as the waterway and Roro harbor for the Marunda industrial area with the minimum width of 200m of the Eastern Banjir Canal for the downstream reaches.

If a joint planning and implementation with PANTURA DKI Jakarta is realized for construction of the Eastern Banjir Canal, land acquisition and implementation costs for its downstream reaches will be greatly decreased for the government. In this case, the construction of the Eastern Banjir Canal would be much more realistic.

Regarding the upstream reaches of the Eastern Banjir Canal, in order to reduce the land acquisition cost, it is conceivable to make a plan to utilize the space over the Eastern Banjir Canal as housing area or an objective area for city redevelopment project. This can be conducted by joint project with private sector.

Accordingly it is recommended that joint planning with PANTURA DKI Jakarta or other private sectors be conducted in early stage for construction of the Eastern Banjir Canal, since the flood control in the eastern part of DKI Jakarta is socially and urgently needed together with the flood control of the eastern part of DKI Jakarta.

(2) Operation Rule of Barrage

Pasar Baru barrage across the Cisadane river has 10 gates. This barrage was constructed for irrigation purpose but due to its deterioration, some gates does not function properly. It is estimated that one reason of the deterioration is the rusting caused by biased usage of specific gates.

Accordingly, it is recommended that the operation rule be reconsidered so as to operate all the gate evenly. This recommendation might be applied to Bekasi and Cikarang barrages.

(3) Present River Area

The middle reaches of the rivers in Jabotabek area are basically located in the deep valley. And accordingly the area is not included in the area to be protected from flooding in due consideration of the retarding effect to the downstream reaches and small beneficiary area due to its topographical situation.

But in some rivers, many people are already living in the river area even though the area is not delineated as the river area officially.

Technically, the people in those area should be relocated after official delineation of the river area is announced to the public. But for the time being, it does not seem to be possible to relocate the people so soon. Accordingly the delineation of the river area should be implemented first. And then the public announcement should be made that the area is the river area. And then the possibility of flooding to certain elevation to certain amount of discharge of the river with the occurrence possibility should be announced to the public.

At the same time, the effective flood forecasting and warning system should be established so that people can evacuate safely with their properties in the houses. Flood warning should be made by using plural measures including TV.

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(4) Future River Area

After the finalization of flood control master plan in Jabotabek area by the authorized agencies, the area to be the river area in future in accordance with the master plan flood control, should be delineated and certain land use regulation should be conducted so that land acquisition in future should not hinder the implementation of the project.

(5) Bridge

Past flooding on January 6 to 8 in 1996 revealed that some bridges form a bottle neck to flood flow and some bridge do not seem to have enough freeboard. The girder level of bridge or that of aqueduct do no seem to have enough high elevation. This situation should be examined soon and proper action should be taken.

(6) Garbage Issue

Garbage issue of rivers in Jabotabek area especially in DKI Jakarta has already reached to the level not to be overlooked anymore. Garbage dumped to the river flow causes so bad smell and deteriorates the amenity of rivers so much.

Garbage dumped to the river is, not only the problem of environment, but also the problem of flood control, as already clearly shown in the recent flood on January 6 to 8, 1996, being

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serious obstacle to flood flow. But construction of garbage screen in the midst of rivers at certain place to protect the downstream reaches may become a serious problem to the upstream reaches.

Periodical removal of garbage in rivers during low flow season should be conducted. This activity would contribute to elimination of garbage problem during flood.

(7) Preservation of Situ-Situ

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Lakes and ponds in the Jabotabek area so called Situ-situ in the local dialect, as discussed in the sub-section 4.4.2, play an important role for flood retention. Situ-situ have, not only the function of flood retention, but also the function of water resources conservation as infiltration place in the basin. Besides the Situ-situ also plays an role of giving amenity to the society as recreation place and an role to preserve the fauna and flora in the basin. This has an important significance from the viewpoint of environment.

(8) Regulation of Land Development

So many and wide areas in Jabotabek area are recently intensively developed as industrial, commercial, resort, and residential area, without appropriate facilities to prevent the increase of flood flow due to the development. The development, not only increases the flood peak flow, but also reduces the basin storage of water resources causing deficit of water resources in the basin or salt water intrusion in groundwater.

To avoid these situation, certain legislation should be enacted so that land development should accompany the construction of appropriate flood retention facilities such as flood retention pond, and the rainfall infiltration facilities such as infiltration pavement and the like.

(9) Small Scale Improvement of I.K.P.N. Complex Along Pesanggrahan River

Floods have been caused by river water flown into the area over the existing concrete wall along the left bank of the Pesanggrahan river as well as local rainwater on the area. It can be suggested that the following measures be taken for improvement of the present situation:

Improvement and extension of the existing concrete wall (left bank only),

Improvement of local drainage channel in the area and replacement of the existing drainage pump.

The location of the area is indicated as in Figure 3.6.

(10) Rehabilitation of the Cidurian and the Cimanceuri Rivers

The river improvement of the Cidurian and the Cimanceuri rivers are situated in rather low priority since the economic internal rate of returns are small. But the present situation of the rivers are that flooding in downstream areas occurs almost every year because some portion

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of the present flood embankment of the rivers in the downstream reaches are breached and flood water easily overtops there and inundates in the hinterland.

6.2 Feasibility Study

(1) Restriction of Development along the Western Banjir Canal

River improvement of the Western Banjir Canal has been proved to be indispensable for flood control of DKI Jakarta through the floods in 1996. And it has been also proved that the downstream reaches improvement has an important role for the river improvement of the whole reaches. (1)

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However, as can be seen along the downstream reaches of the WBC, it is practically impossible to implement the present Detailed Design of the WBC conducted in 1987 by "West Jakarta Flood Control System Project (III)" as it is because of the on-going big scale residential development projects within the proposed alignment.

Accordingly, it is absolutely necessary to regulate the development strictly within the proposed alignment of present feasibility study not to repeat this kind of situation again.

(2) Coordination with KAPUKNAGA

Reclamation of the north coast of the JABOTABEK area including the area near the estuary of the Cisadane river is planned by KAPUKNAGA project. Even though the estuary area is not included for reclamation by the project, downstream reaches of the Cisadane river has a close relationship with the project, since the development of the coastal area is included in the project.

As urgent flood control project, the project includes a plan to construct the embankment along the downstream reaches of the Cisadane river. But the downstream end of the embankment is planned not in consideration of the reclamation plan since the detailed design of the development is not available yet. Accordingly the coordination with KAPUKNAGA project for this aspect will be needed for further step of the project.

(3) Construction of Embankment

For construction of embankment of the Western Banjir Canal, even though the embankment is planned to be provided with revenment works or pavement on the crown in order that the embankment would not collapse totally even overtopping occurs for floods over the design scale, it is still important to pay attention so that no foreign body would not be included in the embankment during the construction stage.

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| 75 | Evaluation for Flood Control Project (West Jakarta Flood Control System Project) | 1993 | 3 | Ministry of Construction and International Engineering Consultants Association (IECA) |
| 76 | Pekerjaan Konsolidasi Design Ciliwung- Cisadane, Laporan Akhir, Volume-II, Laporan Utama | 1993 | | PT Trikarsa Sarana Teknindo, DGWRD |
| 11 | Pekerjaan Konsolidasi Design Ciliwung- Cisadane, Laporan Akhir, "Volume-II Laporan Penunjang | 1993 | 3 | PT Trikarsa Sarana Teknindo, DGWRD |
| | Guidelines and Criteria for Planning and Design of River Flood Control, Volume I | 1993 | | Canadian International • Development Agency, DGWRD |
| 79 | Guidelines and Criteria for Planning and Design of River Flood Control, Volume II | 1993 | | Canadian International Development Agency, DGWRD |
| 80 | Guidelines and Criteria for Planning and Design of River Flood Control, Volume III | 1993 | 6 | Canadian International Development Agency, DGWRD |

Table 2.1 PREVIOUS STUDIES CONCERNING FLOOD CONTROL (6/7)

| \0 . | Data Name | Date of Iss | suc | Publishing Body |
|-----------------|---|-------------|------------|---------------------------------|
| 81 | East Jakarta Flood Control Project Stage 1, | 1993 | 12 | Nikken Consultants, INC. and |
| | The Rehabilitation of Irrigation Schemes and | | | others, DGWRD |
| | Flood Alleviation Works Project, Review | | | |
| | Report Volume I, Review Study | | | |
| 82 | Perencanaan Detail Rehabilitasi dan | 1994 | 1 | CV. Imaya Consulting |
| | Pengembangan Situ-Situ di Wilayah | · · · . | | Engineers, DGWRD |
| | Jabotabek, Final Report (Vol.1) | | | |
| 83 | Jabotabek Water Resources Management | 1994 | 2 | DGWRD |
| | Study, Final Report, Executive Summary | · · · · · | | |
| 84 | Pengukuran dan Perencanaan Perbaikan | 1994 | 2 | P.T. Adhikara Mitra Cipta, |
| | Sungai Kali Pesanggrahan di Hulu Jalan Toll | | | DGWRD |
| 85 | Jabotabek Water Resources Management | 1994 | 2 | Iwaco, DHV Consultants, |
| | Study, Final Report Volume I, Main Report | | · " | Deteft Hydrulics, DGWRD |
| 86 | Project Aid Proposal for Conservation Works | 1994 | 8 | DGWRD |
| | of Situ-situ in the Jabotabek Area | | 0 | |
| 87 | Data Pendukung Kesepakatan Bersama | 1994 | 10 | DGWRD |
| 01 | antara Direktorat Jenderal Pengairan | 1994 | 10 | DOWKD |
| | | | · · | |
| | Departen Pekerjaan Umum dan Pemerintah DKI Jakarta | | Ľ | |
| 0.0 | | 1004 | | |
| 88 | Kesepakatan Bersama antara Direktorat | 1994 | | DGWRD, DKI Jakarta |
| | Jenderal Pengairan Departemen Pekerjaan | | [| |
| | Umum dan Pemerintah Daerah Khusus | | er Ag e | |
| · . | Ibukota Jakarta tentang Pengendalian Banjir | | ļ | |
| : | dan Drainase di Wilayah Daerah Khusus | | | |
| ÷ | Ibukota Jakarta | | | |
| 89 | Prosedur Operasi Lapangan Musim Hujan | 1994 | | DGWRD |
| | 1994-1995 | | | |
| 90 | Studi Penataan Lingkungan Kali | 1995 | 1 | PT Agusta Primakarsa, |
| | Mookervaart, Final Report | | | DGWRD |
| 91 | Pengembangan Pantai Utara Jakarta | 1995 | 2 | PT Puncak Wawasan Indah, |
| | | | | PT Puri Fadjar Mandiri, DKl |
| | | | : | Jakarta |
| 92 | Perencanaan Rehabilitasi Situ Cipondoh | 1995 | 2 | CV Teguh Utania Consultant, |
| | | | | DGWRD |
| 93 | The Study on Cinjung-Cidurian Integrated | 1995 | 2 | Japan International Cooperation |
| - | Water Resources, Volume I, Executive | | | Agency (JICA), DGWRD |
| | Summary | | , , , | |
| 91 | The Study on Ciujung-Cidurian Integrated | 1995 | 1.7 | Japan International Cooperation |
| | Water Resources, Volume II, Main Report | | í | Agency (JICA), DGWRD |
| : | reactive excounters, relative is, train report | | | ngeny (nen), buttle |
| 05 | The Study on Ciujung-Cidurian Integrated | 1995 | - 1 | Japan International Cooperation |
| و <i>ر</i> ا | Water Resources, Volume III, Supporting | 1993 | | |
| | | | | Agency (JICA), DGWRD |
| : 04 | Report The Study on Civilian Cidurian Internated | 1001 | | |
| 70 | The Study on Ciujung-Cidurian Integrated | 1995 | 2 | Japan International Cooperation |
| 1 | Water Resources, Volume IV, Data Book | | | Agency (IICA), DGWRD |

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Table 2.1 PREVIOUS STUDIES CONCERNING FLOOD CONTROL (7/7)

| No. | Data Name | Date of Iss | ue | Publishing Body |
|-----------|--|-------------|----|-------------------------------|
| 97 | Inventory of Watershed in Ciliwung- | 1995 | 3 | DGWRD |
| | Cisadane River Basin Development Project Indonesia | : | | |
| 98 | Interim Report bagi Persiapan Studi Makro | 1995 | 7 | PT. Puri Fadjar Mandiri, DKI |
| 1 | Aspek-aspek Reklamasi dan Hidrolik Proyek | | | Jakarta |
| | Pengembangan Wilayah Pantai Utara Jakarta | | | |
| 99 | Outline of West Jakarta Flood Control | 1995 | 11 | Nikken Consultants, INC. |
| | Project and East Jakarta Flood Control Project | | | |
| 100 | Ring Kanal untuk Mengatasi Masalah Banjir di DKI Jakarta | 1995 | | DGWRD |
| 101 | Debiet : Pencana & Maximum Tahunan | 1995 | | Divisi Pengairan Barat, Perum |
| | Bendung Beet-Cikarang-Bekasi dari Th. 1977 S/D Th. 1994 | | | Otorita Jatiluhur |
| 102 | Buku Pedoman Pelaksanaan Pengendalian Banjir (P3B) Priode 1995/1996 | 1995 | | DKI Jakarta |
| 103 | Prosedur Operasi Lapangan Musim Hujan 1995-1996 | 1995 | - | DGWRD |
| 104 | Penjelasan Singkat Proyek Pengendalian | | | Proyek Pengendalian Banjir |
| | Banjir Jakarta Raya | | | Jakarta Raya |
| 105 | Penjelasan Masalah Banjir DI DKI Jakarta | | : | Proyek Pengendalian Banjir |
| · · · · · | | | | Jakarta Raya |
| 106 | Program Eksploitasi & Pemeliharaan Saluran | | • | Perum Otorita Jatiluhur |
| ···· | Induk Tarum-Barat | | | |
| 107 | Pola Induk Tata Pengairan Daerah Chusus Ibukota Djakarta Raya | | | DKI Jakarta |

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| lo. | River Systems | Principal Point on Main Rivers/Related Rivers | Area (km2) |
|-----------|------------------------|---|---------------------|
| | 011 | Cidentian (address) | 803 |
| 1 | Cidurian | Cidurian (cstuary) | A.A |
| | (803 km²) | Cidurian (Parigi) | 596 |
| . • | | Cidurian (before confluence with Cibeureum) | 378 |
| | | Cibeureum | 218 |
| 2 | Cimanceuri | Cimanceuri (estuary) | 570 |
| | (570 km²) | Cimanceuri (confluence with Cipaseun <balaraja>)</balaraja> | 415 |
| | | Cimanceuri (confluence with Cimatuk) | 233 |
| | | Cipaseun | 116 |
| | | Cimanceuri (confluence with Cimatuk) | 102 |
| | | Cimatuk | 131 |
| 3 | Cirarab (161 km2) | Cirarab (estuary) | 161 |
| 4 | Cisadane | Cisadane (estuary) | 1,411 |
| | (1,411 km²) | Cisadane (Pasar Baru weir) | 1,248 |
| | in the start of | Cisadane (after confluence with Cianten) | 846 |
| | | Cisadane (before confluence with Cianten) | 433 |
| | | Cianten | 413 |
| 5 | Cengkareng Floodway | Cengkareng Floodway (Cengkareng weir) | 459 |
| | (459 km ²) | Cengkareng Floodway (confluence with Angke) | 392 |
| | | Mookervaart canal | 67 |
| | | Angke <including sepak=""></including> | 255 |
| | | Angke (proposed Angke floodway site) | 107 |
| : | | Pesanggrahan <including grogol=""></including> | 137 |
| : | | Pesanggrahan (confluence with Sodetan) | 94 |
| • | | Pesanggrahan river (Proposed Cinere Dam site) | 72 |
| | | Grogol river (upstream of Sodetan) | 30 |
| 6 | Western Banjir Canal | Western Banjir Canal (Karet weir) | 421 |
| Υ. | (421 km^2) | Krukut | 84 |
| | (421 Km) | | 337 |
| | | Ciliwung (Manggarai) Ciliwung (Proposed Depok Dam site) | 251 |
| | | | 152 |
| | 1 | Ciliwung (Proposed Ciliwung Floodway site) | متحاصيت المستند الم |
| | | Ciliwung (Proposed Ciawi Dam site) | 88 |
| 7 | Proposed Eastern | Proposed Eastern Banjir Canal (Estuary) | 207.0 |
| | Banjir Canal | Cipinang (upstream of EBC) | 50.5 |
| | (207 km²) | Sunter (upstream of EBC) | 73.1 |
| | | Buaran (upstream of EBC) | 13.0 |
| | | Jatikramat (upstream of EBC) | 16.5 |
| | | Cakung (upstream of EBC) | 34. |
| . <u></u> | | Residual basins | 19.4 |
| -8 | CBL Floodway | CBL Floodway (Estuary) | 91: |
| · | (1,135 km²) | Bekasi (upstream of CBL Floodway) | 40 |
| | | Bekasi (Bekasi weir) | 38 |
| | : | Bekasi river (confluence of Cikeas and Cileungsi) | 37 |
| | | Cikeas | 110 |
| | | Cileungsi | 26 |
| | | Cisadang (upstream of CBL Floodway) | 13: |
| | | Cikarang (upstream of CBL Floodway) | 23 |
| | | Cilemahabang (Estuary) | 22 |
| 2 | | Residual basins | 14 |
| 9 | Other residual ba | sins including urban drainage area in DKI Jakarta | 90 |
| | | Total JABOTABEK area | 6,07 |

Table 3.1 CATCHMENT AREA OF RIVERS



Table 3.2 DIMENSIONS OF RIVERS

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| o Z | River systems | No. | Related rivers | | Dime | Dimensions of basins | basins. | - | Character | Characteristics of basins |
|---------|--------------------------|--------|--|--------|---------------|----------------------|---------|-------------|--------------------------------|---------------------------|
| | | | | Length | Elevation (m) | n (m). | Average | - Area | Topography | Present land use |
| | | | | (km) | max. | min. | slope | (km2) | | in flood plain |
| | Cidurian | - | Cidurian | 129.3 | 17:00.0 | 0.0 | 1/80 | 803 | 803 Mountainous | Rural |
| 2 | Cimanceuri | 2 | Cimanceuri | 101.3 | 600.0 | 0.0 | 1/170 | 570 | 570 Mountainous | Rural |
| m | Cirarab | С. | 3 Cirarab | 49.0 | 62.5 | 0.0 | 1/780 | 161 | 161 Hilly | Rural |
| 4 | Cisadane | 4 | 4 Cisadane | 137.8 | 2100.0 | 0.0 | 0//1 | 1411 | 1411 Mountainous Urban + Rural | Urban + Rural |
| Ś | Cengkareng Floodway | ŝ | 5 Cengkareng Floodway | 5.7 | 3.0 | 0.0 | 1/2630 | | 459 Plain | Urban |
|) / | (459 km ²) | 6 | 6 Mookervaart Canal | 13.0 | 14.0 | 3.0 | 1/1180 | | 67 Plain | Urban |
| | | - | 7 Angke <including sepak=""></including> | 81.8 | 225.0 | 2.0 | 1/370 | | 255 Hilly | Urban |
| • | | 8 | 8 Pesanggrahan <including grogol=""></including> | 65.5 | 175.0 | 3.0 | 1/380 | | 137 Hilly | Uròan |
| : : | | 6 | 9 Grogol (upstream of Sodetan) | 21.0 | 100.0 | 21.0 | | | 30 Hilly | Urban |
| 9 | Western Banjir Canal | 10 | 10 Western Banjir Canal | 17.3 | 6.3 | 0.0 | 1/2750 | 421 | 421 Plain | Urban |
| | (421 km^2) | 17 | 11 Krukut | 33.5 | 100.0 | 3.0 | 1/350 | | 84 Hilly | Urban |
| | | 12 | 12 Ciliwung (upstream of Manggarai) | 109.0 | 1500.0 | 6.3 | 1/70 | 337 | 337 Mountainous Urban | Urban |
| - | Proposed Eastern | 13 | 13 Proposed Eastern Banjir Canal | 23.7 | - 12.5 | 0.0 | 1/1900 | 207.0 Plain | - 1 1 2 - 1 - 1 | Urban |
| | Banjir Canal | 14 | 14 Cipinang (upstream of EBC) | 36.0 | 115.0 | 12.5 | 1/350 | | so.siHilly | Urban |
| - | (207 km^2) | 15 | 15 Sunter (upstream of EBC) | 37.0 | 120.0 | - 11.5 | 1/340 | | 73.1 Hilly | Urban |
| | - - - - - | 16 | 16 Buaran (upstream of EBC) | 9.0 | 32.0 | 10.0 | 1/410 | | 13.0 Hilly | Urban |
| | : | 17 | 17 Jatikramat (upstream of EBC) | 13.5 | 41.0 | . 9.5 | 1/430 | | 16.5 Hilly | Urban |
| - - | | 18 | 18 Cakung (upstream of EBC) | 30.5 | 103.0 | 6.5 | 1/320 | 1 | 34.5 Hilly | Urban |
| ∞ | 8 CBL Floodway | 12 | 19 CBL Floodway | 28.8 | 10.0 | 0.0 | 1/2880 | • | 915 Plain | Rural |
| | $(1,135 \mathrm{km}^2)$ | 20 | 20 Bekasi (upstream of CBL) | 115.1 | 1500.0 | 4.3 | 1/80 | | 403 Mountainous | Urban + Rural |
| | : | 21 | 21 Cisadang (upstream of CBL) | 36.5 | 87.5 | 8-0 | 1/460 | | 135 Hilly | Rural |
| | | 8 | 22 Cikarang (upstream of CBL) | 65.3 | 300.0 | 10.0 | 1/230 | | 230 Hilly | Rural |
| : | - | ਲ | 23 Cilemahabang | 62.8 | 52.0 | 3.0 | 1/1280 | | 220 Plain | Rural |

| Table 3.3 | PRESENT CARRYE | NG CAPACITIES OF CHANNELS |
|-----------|----------------|---------------------------|
| | | |

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| | | unit : m³/s |
|---|--|---------------------------------------|
| River Systems and Rivers | Bankful F | reeboard |
| Cidurian River System | | |
| - Cidurian | 200 - 850 | 100 - 650 |
| | $\frac{1}{2} \left(\frac{1}{2} \right)^{-1} = \frac{1}{2} \left(1$ | : |
| 2 Cimanceuri River System - Cimanceuri | 175 - 750 | 100 - 625 |
| - Cinfanceuri | 175 - 750 | 100 - 025 |
| 3 Cirarab River System | | |
| - Cirarab | 25 - 175 | 20 - 100 |
| | | |
| 4 Cisadane River System | | |
| - Cisadane | 300 - 3200 | 200 - 2800 |
| | | |
| 5 Cengkareng Floodway System | | |
| | 76 600 | CO 200 |
| - Cengkareng Floodway | 75 - 500 30 - 470 | 50 - 300 25 - 380 |
| - Mookervaart Canal | 30 - 470 30 - 300 | 25 - 225 |
| - Angke - Pesanggrahan | 30 - 250 | 20 - 180 |
| - Grogol | 150 - 400 | 100 - 300 |
| - 010g01 | | |
| 6 Western Banjir Canal System | | · · · · · · · · · · · · · · · · · · · |
| | | |
| - Western Banjir Canal | 100 - 800 | 75 - 625 |
| - Krukut | 25 - 120 | 20 - 175 |
| - Ciliwung | 200 - 1700 | 175 - 1450 |
| | | |
| 7 Proposed Eastern Banjir Cunal System | | |
| - Eastern Banjir Canal | | |
| - Cipinang | 13 - 23 | 7 - 12 |
| - Sunter | 11 • 28 | 5 - 20 |
| - Buaran | 7 - 29 | 1 - 14 |
| - Jatikramat | 2 - 8 | 0 - 0 |
| - Cakung | 4 - 112 | 1 - 6 |
| | | |
| 8 CBL Floodway System | | |
| | | |
| - CBL Floodway | 200 - 1000 | 100 - 950 |
| - Bekasi | 100 - 2000 | 80 - 1600 |
| - Cisadang | 30 - 200 | 20 - 150 |
| - Cikarang | 350 - 950 | 250 - 750 |
| - Cileinahabang | 100 - 275 | 75 - 200 |

Table 4.1

CRITERIA ON FLOOD CONTROL DESIGN SCALE IN INDONESIA

| Conveyance | Project Type (for River Flood Control Project) and | Initial | Final |
|--------------------|--|---------|-------|
| System | Total Population (for Drainage System) | Phase | Phase |
| River | Emergency Project | 5 | 10 |
| | New Project | 5 co 10 | 25 |
| | Updating Project | | |
| | - for rural and/or urban with P < 2.000,000 | 25 | 50 |
| | - for urban with P > 2,000,000 | 25 | 100 |
| Primary Drainage | Rural | 2 | . 5 |
| System (Catchment | Urban P < 500,000 | 5 | 10 |
| area > 500 ha) | Urban 500,000 < P < 2,000,000 | 5 | 15 |
| | Urban P > 2,000,000 | 10 | 25 |
| Secondary Drainage | Rural | 1 | 2 |
| System (Catchment | Urban P < 500,000 | 2 | 5 |
| area < 500 ha) | Urban 500,000 < P < 2,000,000 | 2 | 5 |
| | Urban P > 2,000,000 | 5 | 10 |
| Secondary Drainage | Rural and Urban | 1 | 2 |
| System (Catchment | | | |
| area < 500 ha) | | · [· | |

Notes:

1) Higher design flood standard should be applied if an economic analysis indicates that it is desirable, or if flooding is a significant risk to human life.

2) P = Total Urban Population

- Emergency Project : Emergency Projects are developed without preliminary engineering and economic feasibility studies at sites where flooding is excessive and flooding problems present a significant risk to human life.
- 4) New Project : New Projects include flood control projects where no previous flood control projects have been developed or where Emergency Projects have been developed.
- Updating Project : Updating Projects include rehabilitation projects and improvements to existing projects. Most River Basin Development Projects are considered to be updating projects.

Source : "Recommended Minimum Return Period of Design Flood" in Flood Control Manual, Volume II, Guidelines for Planning and Survey (DGWRD, Jun. 1993)

Table 4.2 OBJECTIVE RIVERS AND DESIGN SCALES FOR FLOOD CONTROL MASTER PLAN

| · | | | - | | | | | | | and a second of the second | | Target Year = 2025 | |
|---|---------------------------------------|----------|---|--------|---------|----------------------|----------|-------------|------------------------------|--|------------------|---------------------|------------------|
| Z | No. River systems | No. | Related rivers | | Ĕ | Dimensions of basins | f basins | | Ü | Characteristics of basins | asins | Design scale (year) | e (year) |
| | | | | Length | Elevati | Elevation (m) | Average | Arca | Topography | Topography Condition of flood plain in 2025 | od plain in 2025 | Existing overal! | This study |
| | | | | (km) | max. | -mm. | stope | (km2) | | Population(P) | Land use | flood control plan | project type |
| | I Cidurian | 1 | 1 Cidurian | 129.3 | 1700.0 | 0.0 | 1/80 | 803 | 803 Mountainous P<2,000,000 | P<2,000,000 | Urban + Rural | Not available | 25 New |
| | 2 Cimaneeuri | 2 | 2 Cimanceuri | 101.3 | 600.0 | 0.0 | 1/170 | 570 | 570 Mountainous P<2.000.000 | P<2.000.000 | Urban + Rural | Not available | 25 New |
| | 3 Citarab | 3 | 3 Citarab | 49,0 | 62.5 | 0.0 | 1/780 | 161 | 161 Hilly | P<2,000,000 | Urban + Rural | Not available | 25 New |
| 4 | 4 Cisadane | 4 | 4 Cisadane | 137.8 | 2100.0 | 0.0 | 01/1 | 1411 | 1411 Mountainous P<2,000,000 | P<2,000,000 | Urban + Rural | Not available | SO New |
| L | 5 Cengkareng Floodway | · . | 5 Cengkareng Floodway | 7.9 | 3.0 | 0.0 | 1/2630 | 459 | 459 Plain | P<2,000,000 | Urban | 100 | 100 100 Updating |
| ÷ | (459 km ²) | | 6 Mookervaart Canal | 13.0 | 14.0 | 3.0 | 1/1180 | 67 | 67 Plain | P<2,000,000 | Urban | 25 | 25 New |
| | | 7 | 7 Angke-cincluding Sepak> | 81.8 | 225.0 | 2:0 | 1/370 | 255 | 255 Hilly | P<2,000,000 | Urban | 100 | 100 100 Updating |
| | · · · · · · · · · · · · · · · · · · · | 8 | 8 Pesanggrahan-including Grogol> | 65.5 | 175.0 | 3.0 | 1/380 | 137 | 137 Hilly | P<2,000,000 | Urban | 001 | 100 100 Updating |
| | | 6 | 9 Grogol (upstream of Sodetan) | - 21.0 | 100.0 | 21.0 | 1/270 | 30 | 30 Hilly | P<2.000.000 | Urban | 23 | 25 New |
| | 6 Western Banjir Canal | ÷ | 10 Western Banjir Canal | 17.3 | . 6.3 | 0.0 | 1/2750 | 121 | 421 Plain | P>2,000,000 | Urban | 1001 | 100 100 Updating |
| | (421 km ²) | | 11 Krukut | 33.5 | 100.0 | 3.0 | 1/350 | 84 | 84 Hilly | P~2,000,000 | Urban | 25 | 25 25 Updating |
| ÷ | | 12 | 12 Ciliwung (upstream of Manggatai) | 109.0 | 1500.0 | 6.3 | 1/70 | 337 | 337 Mountainous P<2,000,000 | | Urban | 1 001 | 100 100 Updating |
| | 7 Proposed Eastern | 131 | 13 Proposed Eastern Banjir Canal | 23.7 | 12.5 | 0.0 | 1/1900 | 207.0 Plain | | P>2.000,000 | Urban | 1001 | 100 100 Updating |
| | Banjir Canal | 14 (| 14 Cipinang (upstream of EBC) | 36.0 | 115.0 | 12.5 | 1/350 | SO.5 Hilly | | P<2,000,000 | Urban | 25 | 25 Updating |
| | (207 km²) | 51 | 15 Sunter (upstream of EBC) | 37.0 | 120.0 | 2.11 | 1/340 | 73.1 Hilly | 2 | P<2,000,000 | Urban | 25 | 25 Updating |
| | | 161 | 16 Buaran (upstream of EBC) | 0'6. | 32.0 | 0.01 | 1/410 | 13.0 Hilly | | P<2.000,000 | Urban | 25 | 25 Updating |
| | : : : | 17.1 | 17 Jatikramat (upstream of EBC) | 13.5 | 41.0 | 9.5 | 1/430 | 16.5 Hilly | | P<2,000,000 | Urban | 25 | 25 Updating |
| | | 181 | 18 Cakung (upstream of EBC) | 30.5 | 103.0 | 6.5 | 1/320 | 34.5 Hilly | | P~2,000,000 | Urban | 25 | 25 Updating |
| | 8 CBL Floodway | ž | 19 CBL Floodway | 28.8 | 10.0 | 0.0 | 1/2880 | 915 | 915 Plain | P<2,000,000 | Urban + Rural | so | 50 Updating |
| | (1,135 km ²) | 20 | 20 Bekasi (upstream of CBL) | 115.1 | 1500.0 | 4.3 | 1/80 | 403 | 403 Mountainous P<2,000,000 | | Urban + Rural | Not available | SO New |
| | | ភ | 21 Cisadang (upstream of CBL) | 36.5 | - 87.5 | 8.0 | 1/460 | 135 | 135 Hilly | P<2,000,000 | Urban + Rural | Not available | 25 New |
| | | สั | 22 Cikarang (upstream of CBL) | 65.3 | 300.0 | 10.0 | 1/230 | 230 | 230 Hilly | P<2.000.000 | Urban + Rural | Not available | 25 New |
| | | ñ | 23 Cilemahabang | 62.8 | 52.0 | 3.0 | 1/1280 | 220 Plain | Plain | P<2,000,000 | Urban + Rural | Not available | 25 New |
| | Note ; Design scale of each river | each riv | Note ; Design scale of each river is proposed according to the criteria | ĥà | | | | • • • | Project | Discharge | Design | Improvement | |

Note , Design scale of each nyer is proposed according to the enteria. in "Flood Control Manual Volume II (Jun. 1993, DGWRD)"

Additional judgment is proposed by the Study Team as follows; 1 Updating project (P-C2,000,000) ; A>1 00km2 ; 50-year, A<100km2 ; 25-year

2 Design scale of 50-year is proposed for the new projects of Cisadane and Bekasi rivers

taking into account the existence of Tangerang and Bekasi city areas in the flood plains respectively.

3 Design scale should be equal or greater than that of existing plan (Angke, Pesanggrahan rivers and Cengkareng floodway).

 ... not available X : available

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Updating Updating

| No. | Name of River | Province | Catchment Area (km ²) | Design Flood (m ³ /s) | Specific Discharge (m ³ /s/km ²) | Return Period (year) | Remarks |
|-----|-------------------|-------------------|---|--|---|----------------------------|---------------------------------------|
| | Cimanuk | West Java | 3,006 | 1,440 | 0.48 | 25 | |
| 2 | Scrang | Central Java | 937 | 900 | 0.96 | 25 | |
| 3 | - | West Java | 3,680 | 1,900 | 0.52 | 25 | |
| 4 | Ular | North Sumatra | 1,080 | 800 | 0.74 | 25 | |
| 5 | Pemali | Central Java | 1,228 | 1,300 | 1.06 | 25 | |
| 6 | Cipanas | West Java | 220 | 385 | 1.75 | 25 | |
| 7 | Solo | Central/East Java | 3,400 | 1,500 | 0.44 | 10 | *1 |
| | -do- | -do- | 3,400 | 2,000 | 0.59 | 40 | *2 |
| 8 | Madiun | East Java | 2,400 | 1,100 | 0.46 | 10 | *1 |
| - | -do- | -do- | 2,400 | 2,300 | 0.96 | 40 | *2 |
| 9 | Wanipu | North Sumatra | 3,840 | 1,320 | 0.34 | 20 | |
| 10 | Arakundo | Ache | 5,495 | 1,800 | 0.33 | 20 | |
| 11 | Kring Ache | + | 1,775 | 1,300 | 0.73 | 20 | |
| 12 | Brantas | East Java | 10,000 | 1,350 | 0.14 | - 10 | i i i i i i i i i i i i i i i i i i i |
| | -do- | -do- | 10,000 | 1,500 | 0.15 | 50 | *2 |
| 13 | Bah Bolon | North Sumatra | 2,776 | 1,220 | 0.44 | 20 | |
| 14 | Walanae | South Sulawesi | 3,190 | 2,900 | 0.91 | 20 | · |
| 15 | Biba | South Sulawesi | 1,368 | 1,900 | 1.39 | 20 | |
| -16 | Jenebarang | South Sulawesi | 729 | 3,700 | 5.08 | 50 | |
| 17 | Ciujung | North Banten | 1,850 | 1,100 | 0.59 | 10 | *1 |
| | -do- | -do- | 1,850 | 1,600 | 0.86 | 50 | *2 |
| 18 | Kuranji | West Sumatra | 213 | 870 | 4.08 | 25 | *1 |
| | -do- | -do- | 213 | 1,000 | 4.69 | 50 | *2 |
| 19 | Air Dingin | West Sumatra | 131 | 600 | 4.58 | 25 | *] |
| | -do- | -do- | 131 | 700 | 5.34 | 50 | *2 |
| 20 | | East Java | 290 | 230 | 0.79 | 20 | |
| 21 | Surabaya | East Java | 631 | 370 | 0.59 | 50 | |

Table 4.3 DESIGN SCALE AND DISCHARGE OF RIVERS IN INDONESIA

*1 : 1st stage and/or urgent plan *2 : 2nd stage and/or overall plan

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Bridge on CMR-49 (Cimanceuri) Bridge near CPS-15 (Cipaseun) June. with Cikeas and Cileungsi Stretches of Flood Plain Zoning (Non-structural measures) Outlet of Angles Floodway Inlet of Angke Floodway Outer Ringroad Upper End Bridge near CDR-50 Target Year = 2025 13.8 Irrigation canal (CRR-18) 71. Scrang Raya Outer Ringroad JI. Kemang 16.3 Jl. Toli Jakarta - Merak Lower End 42.0 Jl. Scrang Raya 14.6 Pasar Baru weir 16.0 Jl. Scrang Raya 21.3 Manggarai weir 8.8 June, with WBC 11.2 Bekasi woir 11.7 Polor weir OBJECTIVE STRETCHES OF FLOOD CONTROL MASTER PLAN 000 0.0 0.00 000 155.7 0.0 000 0.0 0.00 0.0 Total E Boundary of DKI and Tangerang (Present carrying capacity > Design discharge) Stretches of River Improvement (Structural measures) (Present carrying capacity > Design discharge) (Present carrying capacity > Design discharge) II. Toll Jakarta - Cikampek Toll Jakarra - Cikampek Irrigation canal (CRR-18) Junc. with Cisadang river June, with Pesanggrahan Upper End 3.2 June. with Cengkareng Jl, Toll Jakarta - Merak Jl. Raya Pondok Gede Jl. Raya Pondok Gede II. Raya Pondok Gede JI. Jakarta - Cikarung Jl. Scrang Raya Pasar Baru weir JI. Scrang Raya Manggarai weir Cipinang inlet Bekasi weir 5.0 June. with Cengkareng Polor weir 6.0 June. with Cengkareng Lower End 20.0 June, with CBL 3.2 June, with EBC 7.6 June, with CBL 11.5 June, with EBC 8.5 Cipinang inlet 7.2 Sunter inlet. 3.4 Buaran inlet 31.9 Estuary 22.2 Estuary 16.8 Estuary 21.0 Estuary 17.4 Estuary 23.6 Estuary 8.1 Estuary 22.1 Estuary 0.0 0.0 238.7 (ju) 0.0 Total Design Scales (year) 3 ង 8 Total 33 8 8 X ខ្លួនអន្តរ ននុងអង Table 4.4 Junc. with Cengkareng Junc. with Cengkareng June, with Cengkareng irrigation canal from Pondok Pinang weir Bridge near CLA-27 Cisadane (CRR-9) func. with Bekasi Karet weir (Karet weir) Junc. with WBC Design Control Points Jl. Serang Raya June with EBC June with EBC Scrang Raya Pasar Baru weir June, with CBL Cipinang inlet Cikarang weir Bekasi weir Sunter inlet **Buaran inlet** (Balaraja) (Parigi) Estuary Estuary 7 Proposed Eastern Banjir Canal System **Objective Rivers** 5 - Cengkareng Floodway System River Systems Western Banjir Canal System Cengkareng Floodway ğ 2 Clmanceuri River System Western Banjir Canal Eastern Banjir Canal 4 Cisadane River System 1 Cidurian River System Mookervaart Canal 8 CBL Floodway System 3 - Cinarab River System CBL Floodway Pcsanggrahan Cilemahabang Ciliwing Jatikramat Cisadang Cipinang Cikarang Calung - Grogol Angke · Krekur Sunter. Buaran Bekasi Ż 0

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Table 4.5 EVALUATION OF FLOOD CONTROL ALTERNATIVES

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| No. | | | ↓ •- | | | | | | | |
|--------------------------------|---|---------------------|---|--------------|---|----------------------|----------------------|--------------|----------------------|---------------|
| River System | | Cengkareng Floodway | Floodway | | | Western Banjir Canal | anal | | Eastern Banjir | |
| Alternative | | CKR-1 | CKR-2 | CKR-3 | CKR-3 | WBC-1+CSD-1 | WBC-3+CSD-1 | EBC-1-1 | EBC-1-2 | EBC-1-3 |
| utline of Plan | | River Imp. | River Imp. | River Imp. | River Imp. | River Imp. | River Imp. | Box culvert | PC-sheet Pile | Double- |
| | | | & Limo Dan | ઝ | & Angke Fidw. | | 8 | | | cross-section |
| | | | | Angke Fldw. | & Limo Dam | | Ciliwung Fldw | | | |
| Financial Project Cost | | 585 | 1317 | 858 | 1647 | 757 | 167 | 3416 | 1561 | 1666 |
| (Rp.billion) | | | | | | | | | | |
| | Point | 2 | 1 | 2 | 0 | 2 | 2 | 0 | 0 | 0 |
| Land acquisition/house | | 406 | 621 | 295 | 571 | 466 | 305 | 828 | 649 | 1088 |
| compensation cost (Rp.billion) | 1911 | | | | | | | | | |
| | Point | 9 | 4 | 00 | 6 | 9 | 8 | 2 | 2 | 0 2 2 2 |
| EIRR (%) | | 42.9 | 11.4 | 13.7 | 7.4 | 22.5 | 15.4 | 6.7 | 18.6 | 27.4 |
| | Point | 6 | 4 | 6 | 2 | 6 | | 2 | 6 | 6 |
| Technical Evaluation | | Ordinary | Complicated | Complicated | Complicated | Ordinary | Complicated | Ordinary | Ordinary | Ordinary |
| | Point | 2 | 1 | 1 | 1 | 2 | | 2 | 2 | 2 |
| Environmental Impact | | might affect | might affect | might affect | might affect | not affect | not affect | might affect | might affect | might affect |
| | Point | 0 | 0 | 0 | 0 | 2 | 2 | 0 | 0 | 0 |
| Overall Point | | 16 | 10 | 17 - | 6 | 81 | 19 | -9 | 1 01 | 8 |
| Selection for Optimum | | | | * | | - | * | | * | - |
| | | | | | | | | | | |
| | Financial Cost | | Land Acquisition ct | etc. | EIRR | | Technical Evaluation | | Environmental Impact | |
| Crucria | 0:1500 <x< td=""><td></td><td>0 : 1000<x< td=""><td></td><td>0 X<5</td><td></td><td>I * comolícated</td><td></td><td>0 : not affect</td><td></td></x<></td></x<> | | 0 : 1000 <x< td=""><td></td><td>0 X<5</td><td></td><td>I * comolícated</td><td></td><td>0 : not affect</td><td></td></x<> | | 0 X<5 | | I * comolícated | | 0 : not affect | |
| | 1:1000 <x<< td=""><td>1500</td><td>2: 800<x<1000< td=""><td></td><td>2 5<x<10< td=""><td></td><td>2 : Ordinary</td><td></td><td>2: might affect</td><td></td></x<10<></td></x<1000<></td></x<<> | 1500 | 2: 800 <x<1000< td=""><td></td><td>2 5<x<10< td=""><td></td><td>2 : Ordinary</td><td></td><td>2: might affect</td><td></td></x<10<></td></x<1000<> | | 2 5 <x<10< td=""><td></td><td>2 : Ordinary</td><td></td><td>2: might affect</td><td></td></x<10<> | | 2 : Ordinary | | 2: might affect | |
| | 2:500 <x<1000 3: X<500</x<1000 | 000 | 4: 000 <x< 800<br="">6: 400<x< 600<="" td=""><td></td><td>4 : 10<x<12 6 : 12<x< td=""><td></td><td>· ·</td><td></td><td></td><td></td></x<></x<12 </td></x<></x<> | | 4 : 10 <x<12 6 : 12<x< td=""><td></td><td>· ·</td><td></td><td></td><td></td></x<></x<12 | | · · | | | |

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1) River Imp. : River Improvement
2) EIRR : Economic Internal Rate of Return

6 : 400<X< 600 8 : 200<X< 400 10 : X< 200

| No River Systems and Objective Rivers | Optimum Alternative Schemes | Design Control Points | Design Scales (year) | Catchment Area (km²) | Design Discharges (m ³ /s) | | | ncipa) Incesi | utes | Object stretches | | |
|--|---|--|----------------------------|----------------------------|---|--------------------------------|-------------------------------|--------------------|----------------------|---------------------------------------|---|-------|
| | · · · · | | | | | River improvement | Floodway Flood control dam | Flood plain zoning | Other non-structural | River Improvement (structural) | r 1000 r 1am 20ning (non-structural) | |
| | | | | <u> </u> | | <u>i</u> | | | | · · · · · · · · · · · · · · · · · · · | | 1. |
| Cidurian River System | CDR-I | II. Serang Raya | 25 | \$96 | 650 | _ X ; | 7 | X | X | 31.9 | 16 0 | |
| المقصودة أسرا | Chief. | (Parigi) | : | 415 | 290 | x | 1 | | x x | 22.2 | 42 0 | ÷ |
| 2 Cimanceurl River System | CMC-1 | JI. Serang Raya (Balaraja) | 25 | 512 | . 290 | | | | | | 42.0 | |
| 3 Ciearab River System | CRB-I | Irrigation canal from | 25 | 147 | 75 | × x | | Ч х | : x | 16.8 | 13.8 | 1.1 |
| | | Cisadane (CRR-9) | · | | | 1.1 | 5 | í - | | | | |
| 4 Cisadane River System | CSD-1+WBC-3 | Pasar Baru barrage | 50 | 1248 | 1900 | X | -: | · · x | x | 210 | 14.6 | 1.1 |
| | | 4 C C C C C | | | - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 | | | i . | | | | |
| 5 Cenghareng Hoodway System | CKR-3 | Real Provide States | , | | | - X | x | - X | x | : | | |
| | | | | | 1.1.1 | 1 | | , ÷., | | | | · · · |
| Cengkareng Floodway | | Estvary | 100 | 459 | | : X | • | • | x | 83 | 00 | |
| - Mockers and Canal | | June, with Cengkareng | 25 | 67 | | X | • | · · | | 60 | 00 | |
| - Angke | | June, with Cengkareng | 100 | 224 | | X | x | ч X С X | | 5.0 3.2 | 117 | |
| - Pesanggrahan | | June, with Cengkareng Pondek Pinang barrage | 25 | 30 | | | • | ÷ A | · · · | 32 | . 163 | |
| Gregol* | | ronoca rinang banage | - 25 | . 30 | 62 62 | | - | · · · | | | | · |
| 6 Western Banjir Canal System | WBC-3 | | 1 A 1 | | 1. A. 1. | : X | x | $: \mathbf{x}$ | í x | | | |
| | 1 | | 1.1 | | | | | | | | · | |
| Western Banjir Canaf | and the second | Karet barrage | 100 | 421 | 450 | Ń. | • | • • | x | 17.4 | 00. | |
| Chiwung | | (Manggaral bairage) | 100 | 337 | 410 | . • | x | · X | × | 0.0 | 213 | |
| - Krokut | | June, with WBC | 25 | 84 | 135 | ÷ | • | • N | X . | 0.0 | 88 | |
| | | | | | $0 \leq 1 \leq n \leq n$ | | 1 | | | | | 1.1 |
| 7 Proposed Eastern Banjir Canal Sys | tem EBC-1-2 | | 8 - 11 A | | | х | X | ••• | X | | | |
| | | | | | | | ÷ | | 1.1 | | | |
| - Eastern Banjir Canal | | Estuary | 100 | - 207 | | | X | • • | X | 23.6 | 0.0 | |
| - Cipinang | | Cipinang inlet | . 25 | - 50.5 | | X | - | • | x | 8.5 | 0.0 | · · |
| - Sünter - Buasan | | Sunter inlet Buaran inlet | 25 25 | -73,1 | | × X X | | | | 7.2 | 00. | |
| - Jatikramat | 1.1 | June, with EBC | 25 | 16.5 | | $\cdot \cdot \hat{\mathbf{x}}$ | ۰ ۴ . – | ••• | ×Â | 3.4 | 0.0 | |
| Calung | | June, with EBC | 25 | 34.5 | | x | | | | 115 | 0,0 | |
| - CENNING | | Just Millinge | | | | ~ | • | | | 11.2 | 0.0 | |
| 8 CBI Floodway System | CBL-I | · · | · | | | х | • | - X | x | | • | |
| | | | 1 | | · . | | | | | | | |
| - CBL Floodway | 1. Sec. | June, with Bekasi | 50 | 877 | | Х | • | • | : X | 22.1 | 0.0 | |
| - Bekasi | | Bekasi barrage | 50 | 389 | | X | • | - X | | 20.0 | 112 | |
| - Cisadaog | | June, with CBL | 25 | 135 | | х | | | X | 7.6 | 0.0 | |
| Cikarang* Cilemahabang* | | Cikarang barrage Bridge near CLA-27 | 25 | 236 124 | | • | • | • • | • | · · · · | | |
| បារជាធរធរខ្មរខ្ល | | DEROSE REAL A.11 | 25 | 124 | 55 | • | | | | • | • | |
| | | | Total | | 1 | | | 1.1 | - | 239 | 156 | |
| | | | • • • • | | | | | | . ÷ | | | |

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Table 4.6 OUTLINE OF PROPOSED FLOOD CONTROL MASTER PLAN

• Present carrying capacity > Design discharge

| CIDURIAN RIVER | | | | | • | | 1 | | | | |
|----------------|------------|------------------|-----------------------|---------------------|-------------------|--------------------|-------------------|-----------------------|---------------------|--------------------|------------------|
| Section | Distance / | Accumulative | Existing | Existing Ground | round | Existing Dike | Dike | | Desis | ų, | |
| No | (km) | Distance (km) | River Bed (m. TTG) | Left (m, TTG) (i | Right (m, TTG) | Left (m, TTG) (| Right (m, TTG) | River Bed (m, TTG) | н. w.C. (в. ТТС) | H.W.L. (m. TTG) | Dike (m, TTG) |
| CDR01 | 0:00 | 0.000 | -1.70 | 0.03 | -0.61 | 0.00 | 126 | 4.50 | | | |
| CDR02 | 0:950 | 0:950 | -3.03 | -0.76 | -0.67 | 1.12 | 2.29 | 4.20 | | • | |
| CDR03 | 1.000 | 1.950 | -3.05 | -0.57 | 0.05 | 2.71 | 4.27 | -3.83 | | • | |
| CDR04 | 1.000 | 2.950 | -2.44 | 1:96 | 2.10 | 4.77 | 5.64 | -3.57 | 0.93 | 3.23 | 4.23 |
| CDR05 | 0.950 | 3.900 | -2.71 | 1.96 | 1.1 | 5.24 | 3.84 | -3.27 | | | : |
| CDR06 | 1.050 | 4.950 | -2.22 | 1.92 | 2.13 | 5.01 | 5.97 | -2.93 | | | |
| CDR07 | 0.950 | 5.900 | -3.57 | 2.65 | 1.76 | 4.42 | 2.09 | -2.63 | • | | |
| CDR08 | 1.000 | 6.900 | -2.26 | 2.10 | 2.82 | 5.53 | 6.63 | -2.32 | | - | |
| CDR09 | 1,000 | 1.900 | -2.59 | 2.19 | 2.77 | 5.27 | 5.98 | -2.00 | • | · . | |
| CDR10 | 1.000 | 8.900 | 3.04 | 3.89 | 3.23 | 6.60 | 5.48 | -1.68 | : | | |
| CDR11 | 1.000 | 9,900 | -3.20 | 3.27 | 3.39 | 6.67 | 6.37 | -1.37 | | | |
| CDR12 | 1.000 | 10.900 | -2.19 | 3.02 | 4.12 | 6.92 | 8.29 | -1.05 | | | |
| CDR13 | 0.950 | 11.850 | -0.08 | 6.45 | 6.13 | 7.47 | 8.30 | -0.75 | : | | |
| CDR14 | 1.000 | 12.850 | -1.42 | 6.01 | 4.60 | - 16-2 | 8.85 | -0.43 | : | | |
| CDR15 | 1.050 | 13.900 | 44.0- | 7.24 | . 6.05 | 8.83 | 8.26 | -0.10 | | | ••• |
| CDR16 | 1.000 | 14:900 | 0.01 | 4.74 | 5.08 | 7.85 | 9.10 | 22.0 | - | - | |
| CDR17 | 000 | 15.900 | 0.10 | 6.17 | 5.74 | 9.08 | 8.96 | 0.53 | | | |
| CDR18 | 0:950 | 16.850 | -0.05 | 6.34 | 6.07 | 9.25 | 8.89 | 0.83 | | ī | |
| CDR19 | 1.000 | 17.850 | -0.25 | 8.10 | 7.47 | 10.24 | 9.65 | 1.15 | | | |
| CDR20 | 1.050 | 18.900 | 1.08 | 7.73 | 7 76 | 10.55 | 10.77 | . 1.48 | | | |
| CDR21 | 1.100 | 20.000 | 1.29 | 8.11 | 7.62 | 9.33 | 10.03 | 1.83 | : | | |
| CDR22 | 1.050 | 21.050 | 1.79 | 8.50 | 7.55 | • | : | 2.16 | | • | |
| CDR23 | 1.000 | 22.050 | 2.84 | 9.30 | 8.43 | - 1 | | 2.48 | : | | |
| CDR24 | 1.050 | 23.100 | 1.87 | 9.89 | 9.96 | | • | 2.81 | | | |
| CDR25 | 1.000 | 24.100 | 2.86 | 7.21 | 8.31 | 8.51 | | 3.13 | • • | : | |
| CDR26 | 1.050 | 25.150 | 66.1 | 10.39 | 12.30 | 12.75 | : | 3.46 | | | |
| CDR27 | 1.050 | 26.200 | 2.58 | 10.29 | 9.25 | | | 3.79 | | | |
| CDR28 | 1.000 | 27,200 | 3.80 | 11.14 | 11.48 | | • | 11.4.11 | • | ļ | |
| CDR29 | 1.000 | 28,200 | 427 | 11 95 | 10.76 | | 1 | 4.42 | | | |
| CDR30 | 0.750 | 28.950 | 3.26 | 13.24 | 12.60 | | • • • | 4.66 | • | | |
| CDR31 | 1.000 | 29:950 | 4,42 | 12.05 | 11.92 | . : | • | 4,98 | | | |
| CDR32 | 1.000 | 30.950 | 4.48 | 11.75 | 14.05 | | | 5.29 | | | - |
| | | | | | | | | | | | |

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Table 4.7 DIMENSION OF LONGITUDINAL PROFILES (2110)

(m, TTG) (m, TTG) (m, TTG) Dike H.W.L. Design -0.50 0.20 0.48 0.99 H.W.C. River Bcd (m, TTG) -0.57-0.57-0.22-0.2Existing Dike Lett Right (m. TTG) (m. TTG) 3.37 4.33 3.87 4.02 5.88 5.23 2.11 2.65 4.66 6.09 5.86 6.10 7.32 7.12 7.43 9.47 Existing Ground Left Right (m, TTG) (m, TTG) 8.51 9.35 9.35 13.08 Existing River Bed (m. 110) Distance Accumulative Distance (m) 0.000 0 Ē CMR25(II. Raya Serang) CIMANCEURI RIVER CMR01 CMR02 CMR03 CMR04 CMR04 CMR10 CMR10 CMR11 CMR11 CMR12 CMR13 CMR03 CMR23 MR22 CNR24 CNR21 Section No.

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|---------------|-------------|---|---------------------------------------|-----------------------------------|----------------------------|-------|----------------|-------|-------|-------|-----------------|-------|-------------------------|-------|-------|------------|----------|--------|---------------|--------|------------------------|---|---|-----|-----|---|---|-----|------------|-----|--------|-----|-----|--------|---------------------------------------|-------|-----|
| | | • | | | · | • | | | | | | | | | : | | • | | | | : | | | | | | | | | • | | • | | • • | | · · · | |
| | · · | | ·· : · : | | • • | | | | • | | | | | | : | | · . : | | | . • | • | | | | | | | | : · · · | : | | | • | | | | |
| | : : : | | | Dike | a, 11G) | 0.60 | 60.1 | 1.57 | 2.06 | 2.49 | 3.42 | 4.00 | 4.53 | 4,82 | 5.41 | t 7 | 98.9 | 7.34 | 7.85 | 8.26 | 8.74 | | | | | | | . : | | | - | | | | | | |
| () | | | | en H.W.L | (m. TTG) (m. TTG) (m. TTG) | | 0.49 | 0.97 | 1.46 | 1.89 | 2.82 | 3.40 | 3.93 | 4.22 | 4.81 | | C/ C | 674 | 7.25 | 7.66 | 8.14 | | : | : | | | | • | : | | - - | · · | | · † . | | | |
| · · · · | | | | H.W.C. H | (m, TTG) | ş | -0.51 | -0.03 | 0.46 | 68.0 | 1 82 | 2.40 | 2.93 | 32 | 3.81 | 47.4 75 | 4 YC Y | 5 74 | 6.25 | 6.66 | 7.14 | | | | · · | | | | | | | | | | · · · · · · · · · · · · · · · · · · · | | 7 |
| | · · · · · | | · · · · · · · · · · · · · · · · · · · | River Bed | | , ş | -2.51 | -2.03 | -1.54 | | 7 81 9 19 | 070 | 0.93 | 12 | 1.81 | 47.7 | 962 | 3.74 | 4.25 | 4 66 | 5.14 | | | | | | | | | · . | • | | . * | | • | • | |
| | | S (3/10) | | g Dike Richt | (m, 11G) | | 1.68 | 3.03 | 2.83 | 3.60 | 5.00 | 4,83 | | 6.02 | 5.91 | 20.0 | | 6.54 | 6.98 | | | | | | | | | | | • | • | | | : | | : | |
| | | DIMENSION OF LONGITUDINAL PROFILES (3/10) | | Existing Dike | (m. TTG) (m. TTG) | | 2.04 | 2.72 | 2.89 | 3.75 | 2.6U | 5.06 | | 5.97 | 4.97 | 0./0 | + 1 v | 7.27 | | | | | | | | | ÷ | • . | | | | | | | | | |
| | | NGITUDIN | | Existing Ground Left Rivht | (m. TTG) | | 80 | 1.15 | 1.46 | 2.91 | 2.83 | 2.96 | 5.88 | 4.63 | 4.71 | 4.48 | | 5.56 | 6.88 | 7.78 | 7.90 | | | | | | | | | | | ÷ | | | | | |
| , 1 2. | · · · | SION OF LO | | Existing | (m, TTC) (m, TTG) | | 1 61 | 1.71 | 1.88 | 2.53 | 2.14 3.11 | 3,21 | 5.88 | 4.36 | 3.57 | 21.9 | 00.0 | 7.26 | 5.78 | 6.32 | 9.86 | | : | | | | | | | | | | | | | | |
| | | | | Existing. River Red | (m, 17G) | 6 | -2.86 | -2.87 | -2.12 | -2.42 | 95 - 96 - 0- | -0.97 | 0.88 | 0.01 | 0.05 | 0.85 | 25.2 | 2.98 | 3.99 | 4 | 4.89 | | | | | | | | | | | | | | | | |
| | | Table 4.7 | | Distance Accumulative Distance | · · | 000 0 | 1 000 | 2.000 | 3.000 | 3.900 | 4,700 5,800 | 7.000 | 8.100 | 8.700 | 006-6 | 10.800 | 12 000 | 13.875 | 14.925 | 15.775 | 16.775. | | | | | | | | | | | | | | | | |
| | | | | Distance A | (m.) | | 0001 | 1.000 | 1.000 | 0.900 | 0.800 | 1.200 | 1.100 | 0.600 | 1,200 | 0.900 | 050.1 | 050-1 | 1.050 | 0.850 | 1.000 | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | • | | canal) | | | | | | | • | (Iene) | | | | | | | | | | | | | | | | |
| A. | | | CIRARAB RIVER | | | | | | | - | | | CRR09(Irrigation canal) | ~ | | ~1 ~ | | • | ~ | - | CRR18(Imigation canal) | | | | | | | | | | | | | | | | |
| · · · · · | | | CIRV | Section | 2 | | COXAC CREAC | CRR03 | CRRO | CRR05 | CKR07 | CRR08 | CRR05 | CRR10 | CKRII | CKKIZ | | CRRIS | CRR16 | CRR17 | CRRI | | • | | • | - | • | | | | | | • | | | | |
| | . " | | | • . | | | а 12 | | | | • | | • | | | | | | • • * : | | : | • | | | : | | | | | . : | | • | | | | | |

Table 4.7 DIMENSION OF LONGITUDINAL PROFILES (4/10)

CISADANE RIVER

River Bed H.W.C. H.W.L. Dike (m, TTG) (m, TTG) (m, TTG) 3.50 3.50 4.13 Design Left Right (m. TTG) (m. TTG) 2.332 5.17 5.17 5.17 5.17 5.17 5.17 5.56 5.68 8.55 5.627 7.56 6.68 8.55 7.56 6.68 8.55 7.56 9.10 9.13 9.13 9.13 9.13 9.13 10.041 11.022 1.73 Existing Dike Left Right (m. TTG) **Existing Ground** Existing River Bed (m. 11G) Distance Accumulative 0.000 0.973 1.898 2.798 2.798 4.835 6.023 7.173 8.123 8.123 9.023 9.023 9.023 9.023 11.1123 11 Distance (km) 0.000 0.973 0.925 0.926 0.996 0.996 0.996 0.996 0.996 0.996 0.1105 0.1105 0.1105 0.1115 0.115 <u>(j</u> SD22(Pasar Baru weir) CSD01 CSD02 CSD03 CSD04 CSD05 CSD06 CSD05 CSD06 CSD05 CSD06 CSD05 CSD06 Section No.

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| | 2.20 2.31 2.45 | 2.57 2.71 3.07 3.20 3.46 3.33 3.46 | 3.56 3.95 4.14 4.15 4.13 4.13 4.13 4.13 4.13 4.13 5.65 4.13 5.65 4.13 5.65 4.13 5.65 5.65 5.65 5.65 5.65 5.65 5.65 5.6 | 1 4 4 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 | |
|--|-------------------------------------|---|---|---|---|
| € H.w.L. | 1.20 2.20 1.31 2.31 1.45 2.45 | 151 198 200 200 200 200 200 200 200 200 200 20 | 258 233 233 233 235 258 258 258 258 258 258 258 258 258 25 | 332 | |
| Design | -0.55 -0.44 -0.30 | -0.18 -0.04 0.20 0.32 0.58 0.58 0.71 | 0.81 0.91 1.40 1.78 2.82 2.82 0.02 | 500 750 750 750 | |
| | | 4,18 4,18 3,3,2,3,2,3,2,4,18 3,3,5,8 3,2,5,5,8 3,3,5,5,8 3,3,5,5,8 3,3,5,5,8 3,3,5,5,8 4,4,5,5,5,8 4,4,5,5,5,8 4,4,5,5,5,8 4,4,5,5,5,8 4,4,5,5,5,5,5,5,5,5,5,5,5,5,5,5,5,5,5,5 | | | |
| (S/10) Dike Right | 0.46 1.32 1.54 | 1.8 1.6 2.3 2.3 2.3 2.5 2.5 2.5 2.5 2.5 2.5 2.5 2.5 2.5 2.5 | 2.11 2.29 3.18 3.18 3.18 3.18 | | |
| DIMENSION OF LONGTTUDINAL PROFILES (\$/10) (isting Existing Ground Existing Dike ter Bed Left Right Left Right | 0.27 | 2.01 2.64 2.10 2.10 2.11 2.21 2.21 2.22 2.22 2.22 | 2,38 2,76 2,79 3,16 3,16 3,16 3,16 | | |
| SCTUDIN. | 0.01 0.25 0.48 | 0.96 0.66 0.13 0.13 1.07 1.59 0.58 0.58 | 0.78 0.55 0.55 0.93 0.93 0.93 | 5.126 | |
| SION OF LONGTTUDIA Existing Ground Left Right | -0.41 -0.06 -1.22 | 0.16 0.37 0.37 0.37 0.37 1.29 1.29 1.33 1.33 1.34 1.34 1.34 1.34 1.34 1.34 | 1.22 0.86 0.75 0.63 1.19 1.19 | 4.85 | |
| / DIMENS Existing River Bed | 4.57 4.21 -3.87 -3.87 | 6.14 4.14 4.15 4.18 4.18 5.18 5.18 5.18 5.18 5.18 5.18 5.18 5 | 4 5 5 4 6 6 4 2 7 1 2 8 4 7 1 6 6 6 7 8 7 1 1 6 6 7 7 8 7 1 1 6 7 8 7 1 7 8 7 1 7 8 7 1 7 8 7 1 7 8 7 8 7 8 7 8 7 8 7 8 7 8 7 8 7 8 7 8 | 1 4 6 8 9. | |
| Table 4.7 Distance Accumulative R | 0.000 0.0000 0.989 0.989 | 1.483 2.028 2.520 3.001 3.498 4.512 4.512 5.034 | 5.440 5.820 5.820 5.995 6.490 7.017 7.017 7.017 | 8.146 | |
| Distance | 0.000 0.444 0.544 | 0.495 0.544 0.492 0.487 0.487 0.507 0.507 | 0.406 0.380 0.175 0.495 0.495 0.276 0.000 | 0.693 | |
| CENCKARENG FLOODWAY Section | | | CEN12 CEN13 Cengkareng Barrage Conf. with Mookervaart Canal CEN14 Drop Strucutre Drop Strucutre | | |
| CENCK Section No. | CEN01 CEN02 CEN03 | CENQ CENQ CENQ CENQ CENQ CENQ CENQ CENQ | CEN12 CEN13 Cengkareng Barra Conf. with Mooke CEN14 Drop Strucutre | D3 CEN15 | : |

| | Distance / | Accumulative | Existing | цл, | puno | u u | | W . | c | |
|-----------------------|------------|------------------|-----------------------|---------------------------------|------------------|---------------------------------|-----------------------|------------------------------------|--------------------|------------------|
| No. | (km) | Distance (km) | River Bed (m. TTC) | Lett Right (m. TTG) (m. TTG) | Right m, TTC) | Left Right (m. TTG) (m. TTG) | River Bed (m. TTG) | H.W.C. H.W.L. (m, TTG) (m, TTG) | н. w (m. TTG) (| Uike (m, TTG) |
| Conf. with Cengkareng | 0.00 | 0.000 | | 1 | | | -2.60 | | 3.01 | 3 61 |
| MKV13 | 0.570 | 0.570 | | 2.74 | 2.07 | • | -2.35 | | 301 | 3.61 |
| MKV12 | 0.900 | 1.470 | | 3.47 | 5.54 | | - 62 | | 10 10 | 19 1 |
| MKVII | 1.000 | 2.470 | | 3.95 | 4.10 | - | -1.51 | | 3.01 10.5 | 19:5 |
| MKV10 | 0.975 | 3,445 | | 3.97 | 3.02 | | -1.08 | | 10.5 | 10.7 |
| MKV09 | 0.815 | 4.260 | -3.07 | 5.07 | 3.47 | | 0.72 | . ; | 3.28 | 3.85 |
| WKV08 | 0.800 | 5.060 | | 5.51 | 4.84 | | 05.0- | | 8 | 4 |
| MKV07 | 0.975 | 6.035 | -0.33 | 5.79 | 5.62 | | 0.07 | | 4.07 | 4.0/ |
| ANGKE RIVER | | | | | | | | | | |
| Camion | Dictance | A crimination | Evicting | Evicting Gr | or mo | Existing Dike | | Design | | • |
| Section No. | | Distance | River Bed | Left Right | Right | Left Right | River Bed | H.W.C. | HWL | Dike |
| | (ken) | (uzy) | (m. TTG) | (m, 17G) (m | 0110 | (m, TTG) (m, TTG) | (m. TTG) | (m. 11G) (m. 11G) (m. 11G) | m, TTG) (| m, TTG |
| QA | 000.0 | 000.0 | -2.88 | 2.10 | 1.80 | | -1.70 | 2.63 | 3.43 | 4.23 |
| A11 | 1.020 | 1.020 | | 2.70 | 2.40 | · · · | -1.19. | | 3.43 | 4.23 |
| A25 | 0.970 | 1.990 | | 3.00 | 130 | | | | 3:60 | 4.40 |
| Ĩ | 1.085 | 3.075 | -0.76 | 4.60 | 3.80 | | 0.16 | | 4.14 | 4.94 |
| A37 | 0.945 | 4.020 | | 4.80 | 4.20 | | 0.31 | | 4.61 | 5.41 |
| A44 | 0.635 | 4.655 | • | 6.00 | 5.40 | | 0.63 | : | - 70 v | 5.73 |
| Polor Weir | 0.315 | 4.970 | . • | 5.90 | 7.52 | | 6/.0 | 4 | 50.0 | 2.07 |
| PESANGGRAHAN RIVER | | | | | | | | | | |
| | a contract | | Eutorian | Cuinting Co | - | Evicting Dite | | Decion | | ÷ it: |
| Section | DISTRICT | Distance | Exisung River Bed | Left Right | Right | Left Right | River Bed | HWC | HWL | Dike |
| | (cm) |) By | (m, 110) | 6 | (m, TTC) | (m, TTG) (m, TTG) | (m, TTG) | | (C) (| (m. TTC) |
| PLC/LLC | | 000 0 | | | | | -0.75 | 3.05 | 4 50 | 02.5 |
| D6 | 0.080 | 0.080 | -1.59 | 2.18 | 222 | 3.60 | -0.69 | | 4.56 | 5.36 |
| P35 | 0.852 | 0.932 | | 3.34 | 4.65 | 4.90 | 0.0 | | 5.25 | 6.05 |
| P44 | 1.006 | 1.938 | : | 17'7 | 4.40 | | 0.80 | : | 6.05 | 6.85 |
| PSG01 | 0.854 | 2.792 | | 5.14 | 5.31 | • | 1.48 | | 6.73 | 7.53 |
| Toll Road | 0.310 | 3.102 | | 5.01 | 5.04 | | 1.73 | 5.53 | 6.98 | 7.78 |
| | | | | | | | | | | |
| | | ŗ | | | • | | | | • | |
| - | | : | | | • | | | | | ÷ |
| | | | | | | | | | ę | |

Table 4.7 DIMENSION OF LONGITUDINAL PROFILES (6/10)

| WESTERN BANJIR CANA | L | | | | | | | | | | |
|---------------------|----------|------------------|-----------------------|---------------------------------|------------------|---------------------------------|------------------|--|-------------|-----------------------|---|
| Section | Distance | Accumulative | Existing | Existing Ground | puno | Existing Dike | Dike | a a martina da compañía de la compañía de | Sis | | |
| Ň | (km) | Distance (km) | River Bod (m, 17G) | Left Right (m. TTG) (m. TTG) | Right m. TTG) | Left Right (m. TTG) (m. TTG) | Right n, TTG) | River Bed H.W.C. (m. TTG) (m. TTG) | | H.W.L. (m, TTG) (1 | Dike (m. TTG) |
| WBC01 | 0000 | 0000 | 2.56 | -0.18 | -0.15 | | | 4.95 | -0.95 | 0.85 | 1.85 |
| WBC02 | 0.625 | 0.625 | 4.36 | -0.97 | -0.41 | -0.50 | 0.05 | 4.74 | -0.74 | % | 2.8 |
| WBC03 | 0.485 | 1.110 | -5.38 | 0.09 | -0.42 | 0.47 | 0.29 | 4,58 | -0.58 | 13 | 222 |
| WBC04 | 0.525 | 1.635 | -6.89 | 1.90 | 0.05 | | 0.73 | 44 | -0.41 | 1 40 | 2.40 |
| WBC05 | 0.638 | 2,273 | -3.68 | -0.23 | 0.12 | 0.97 | 0.81 | -4,19 - 55 | -0.19 | 191 | 197 |
| WBC06 | 0.437 | 2.710 | | -0.23 | 60.0 | | • | 4 5 8 | 6 6 6 | 0.5 | 0.7 |
| WBC07 | 0.038 | 2.543 | 6 - 1 - 1 | -0.05 | 10.0 | 1 00 | | 3,65 | 1.0 | 16.1 7 14 | 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 |
| WEC00 | 2120 | 4 348 | | 0.14 | 1 | 2.34 | | -3.50 | 0.50 | 230 | 3.30 |
| WBCIO | 0.537 | 4.885 | | 0.48 | 0.48 | 3.12 | 2.66 | -3.32 | 0.68 | 2.48 | 3.48 |
| WBCII | 0.500 | 5:385 | | 2.60 | 2.47 | 3.54 | 3.40 | -3.16 | 0.85 | 2.65 | 3.65 |
| WBC12 | 0.512 | 5:897 | : | 0.30 | 0.30 | 2.54 | 2.85 | -2.98 | 8 | 2.82 | 3.82 |
| WBC13 | 0.476 | 6.373 | | 15.1 | 1.31 | 3.42 | 2.99. | | 1.17 | 2.97 | 3.97 |
| WBC14 | 0.512 | 6.885 | | 0.32 | 0.95 | 3.54 | 3.55 | -2.66 | 1.35 | 3.15 | 4.15 |
| WBCIS | 0.475 | 7.360 | , | 2.09 | 1.55 | 3.88 | 3.62 | -2.50 | 1.50 | 3.30 | 4.30 |
| WBC16 | 0.463 | 7.823 | | 3.86 | 0.94 | 3.93 | 4.02 | -2.34 | 1,66 | 3.46 | 4 46 |
| WBC17 | 0.400 | 8.223 | | 2.93 | 1.97 | 3 39 | 3.48 | -191- | 1.79 | 3.59 | 4.59 |
| WBC18 | 0.537 | 8.760 | -3.81 | 1.70 | 1.78 | 3.76 | 4.09 | -2.03 | 1.97 | 3.7 | 4.1 |
| WBC19 | 0.513 | 9.273 | | 1.87 | 3.12 | 4.07 | 6,12 | -1:86 | 2.14 | 3.94 | 4.94 |
| WBC20 | 0.425 | 9.698 | | 3.25 | 5.08 | 4.50 | 5.16 | -1.72 | 2.28 | 4.08 | 5.08 |
| WBC21 | 0.462 | 10.160 | | 3.02 | 232 | 4.25 | 47: | -1.56 | 4 | 424 | 524 |
| WBC22 | 0.425 | 10.585 | 2.53 | 2.55 | 3.6 | 4.65 | 4.63 | -1.42 | 2.58 | 4.38 | 5.38 |
| WBC3 | 0,463 | 11.048 | | 4,68 | 3.19 | 4.69 | 4.17 | -1.27 | 2.73 | 4.53 | 5.53 |
| WBC24 | 0.475 | 11.523 | 4 1. | 4.55 | 2.83 | 5.18 | 3.26 | 11.1- | 2.89 | 69' 4 | 5.69 |
| WBC25 | 0.475 | 11.998 | -0.58 | CI m | 5.00 | 4.38 | | -0.95 | 3.05 | 4.85 | 5.85 |
| Karet Barrage | 0.381 | 12.379 | | | | | | -0.82 | 3.18 | 4,98 | 5.98 |
| | 0.00 | 12.379 | | | | - | - | -0.30 | 3.70 | 5.50 | 6.50 |
| WBC26 | 0,100 | 12.479 | -2.26 | 4.80 | 5.52 | 6.65 | 6.59 | -0.27 | 3.73 | 5.53 | 6.53 |
| WBC27 | 0.544 | 13.023 | 66 O | 6.47 | 6.71 | 7.17 | 7.48 | -0.09 | 3.91 | . 5.71 | 6.71 |
| WBC28 | 0.456 | 13.479 | 0.37 | 7.42 | 7.42 | 8.02 | . 7.73 | 0.07 | 4,07 | 5.87 | 6.87 |
| WBC29 | 0.388 | 13,867 | 0.90 | 9.40 | 9.17 | 9.76 | | 0.20 | 4.20 | 6.00 | 7.00 |
| WBC30 | 0.512 | 14.379 | 6.0 | 4.25 | 3.30 | 2.10 | 7.09 | . 0.37 | 4.37 | 6.17 | 7.17 |
| WBC31 | 0.463 | 14,842 | 0.68 | . 5,60 | 6.40 | 7 49 | 7.95 | 0.52 | 4.52 | 6.32 | 7.32 |
| WBC32 | 0.468 | 15.310 | 0.59 | 11.03 | 10.80 | | : | 0.68 | 4.68 | 6.48 | 7 48 |
| WBC33 | 0.525 | 15,835 | 21.5 | 8.35 | 7.32 | | | 0.85 | 4.85 | 6.65 | 7.65 |
| WBC34 | 0.475 | 16.310 | 121 | 8.33 | 8.59 | | | 10.1 | 5.01 | 6.81 | 7.81 |
| WBC35 | 243 0 | 14 873 | | 0.40 | 12 55 | | | 000 | C C Y | S | S |
| | | 10.00 | 11.77 | | | | | , T. | N7.6 | 22.2 | |

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le. 4.7 DIMENSION OF LONGITUDINAL PROFILE \$ (8/10-1)

| Section | | | E | xisting Groun | | | Design | |
|---------|-------|--|--|---|---|--|---|------------|
| No. | | Distance | (Centre) | (Lefl) | (Right) | River Bed | HWL | Dike |
| | ÷ . | (km) | | (m.PP) | (m.PP) | (m.PP) | (m.PP) | (m.PP) |
| VEBC | 0.00 | 0 | 1.43 | 1.43 | 1.43 | -2.00 | 3.20 | 4.2 |
| VEBC | 1.00 | 1,000 | 1.73 | 1.73 | | -1.78 | 3.42 | 4.4 |
| VEBC | 2.00 | 2,000 | 2.23 | 2 23 | 2.23 | -1.56 | 3.64 | 4.6 |
| VEBC | 2.50 | 2,500 | 2.43 | 2.43 | 2.43 | -1.44 | 3.76 | 4.7 |
| NEBC | 3.00 | 3,000 | 2.23 | 2 23 | 2.23 | -1.33 | 3.87 | 4.8 |
| VEBC | 3.50 | 3,500 | 2.23 | 2.23 | 2.23 | -1.22 | 3.98 | 4.9 |
| VEBC | 4.00 | 4,000 | 2.33 | 2.33 | 2.33 | -1.11 | 4.09 | 5.0 |
| VEBC | 4.50 | 4,500 | 2.63 | 2.63 | 2.63 | -1.00 | 4.20 | 5.2 |
| NEBC | 5.00 | 5,000 | 2.63 | 2.63 | 2.63 | -0.89 | 4.31 | 5.3 |
| NEBC | 5.50 | 5,500 | 2.53 | 2.53 | 2.53 | -0.78 | 4.42 | 5.4 |
| NEBC | 6.00 | 6,000 | 2.53 | 2.53 | 2.53 | -0.67 | 4.53 | 5.5 |
| NEBC | 6.50 | 6,500 | 2.53 | 2 53 | 2.53 | -0.56 | 4.61 | 5.6 |
| NEBC | 6.60 | 6,600 | 2.83 | 2.83 | 2.83 | -0.53 | 4.67 | 5.6 |
| NEBC | 6.70 | - And the second se | 2.93 | 2.93 | 2.93 | -0.51 | 4.69 | 5.6 |
| NEBC | 7.00 | | 3.53 | 3.53 | 3.53 | -0.44 | 4.76 | 5.7 |
| NEBC | 7.50 | | 3.53 | 3.53 | 3.53 | -0.33 | 4.87 | 5.8 |
| NEBC | 8.00 | | 3.53 | 3.53 | 3.53 | -0.22 | 4.98 | 5.9 |
| NEBC | 8.50 | | 4.03 | 4.03 | 4.03 | -0.11 | 5.09 | 6.0 |
| NEBC | 9.00 | | 3.53 | 3.53 | 3.53 | 0.00 | 5.20 | 6.2 |
| NEBC | 9.50 | And and a second se | 6.53 | 6.53 | 6.53 | 0.11 | 5.31 | 6 |
| | 10.00 | and the second | 6.53 | 6.53 | 6.53 | 0.28 | 5.28 | 6 |
| NEBC | 10.00 | | 5.53 | 5.53 | 5.53 | 0.44 | 5.44 | 6 |
| NEBC | | a second s | 6.53 | 6.53 | 6.53 | 0.61 | 5,61 | 6.0 |
| NEBC | 11.00 | | 4.03 | 4.03 | 4.03 | 0.73 | 5.73 | 6 |
| NEBC | 11.3 | | 4.03 | 4.53 | 4.53 | 0.78 | 5.78 | 6. |
| NEBC | 11.50 | and the second s | and the second sec | 4.53 | 4.53 | | 5.91 | 6 |
| NEBC | 12,00 | | 4.53 | 3.23 | 3 23 | 1.11 | 6.11 | |
| NEBC | 12.50 | | 3.23 | 3.53 | 3.53 | 1.28 | 6.28 | 7. |
| NEBC | 13.00 | | 3.53 | 3.53 | 3.53 | 1.20 | 6.44 | 7. |
| NEBC | 13.50 | | 5.55 | 6.03 | 6.03 | 1.61 | 6.61 | <u>7</u> . |
| NEBC | 14.00 | | | | 4.13 | | 6.78 | 7 |
| NEBC | 14.50 | | 4.13 | 4.13 | 4.13 | i contra a | 6.94 | 7. |
| NEBC | 15.00 | - Andrew Street St | 4.23 | 4.23 | | the second s | and the second se | 8. |
| NEBC | 15.50 | | 5.53 | 5.53 | 5.53 | 2.11 2.28 | 7.11 | 0. 8. |
| NEBC | 16.00 | | 4.83 | 4.83 | 4.83 | | 7.44 | 0. 8. |
| NEBC | 16.5 | | 5.03 | 5.03 | 5.03 | | | |
| NEBC | 17.00 | | 9.53 | 9.53 | 9.53 | | 7.61 | 8. |
| NEBC | 17.0 | a de a companya de la | 9.53 | 9.53 | 9.53 | | 8.27 | |
| NEBC | 17.9 | | 12.59 | 13.68 | 10.15 | l | 8.59 | 9 |
| BKT | 25 | | 8.50 | 8.35 | 8.66 | | 9.63 | 10 |
| BKT | 25 | | 12.23 | 8.50 | 15.00 | | 9.68 | 10 |
| BKT | 25 | | | 8.51 | 8.80 | | 9.71 | 10 |
| BKT | 25 | | and the second s | 8.36 | 8.76 | and the second sec | 9.73 | 10. |
| BKT | 25 | | | 8.63 | 9.36 | | 9.75 | 10 |
| BKT | 25 | | | 8.22 | 8.2 | | 9.82 | 10 |
| BKT | 26 | | 10.34 | 13.70 | 8.40 | | 9.86 | 10 |
| BKT | 26 | | 13.60 | 14.99 | 10.50 | | | - 10 |
| BKT | 26 | | 15.54 | 15.18 | | | | 10. |
| BKT | 26 | | 15.18 | 15.10 | | | | 10. |
| BKT | . 26 | | 15.23 | 10.51 | 15.62 | | | 11 |
| BKT | 27 | | | Contraction of the second s | 13.4 | | | |
| ВКТ | 27 | 2 19,282 | | | | | | |
| BKT | 27 | | | | the second se | | | |
| BKT | 27 | | | 16.26 | 16.0 | 5.18 | | |
| BKT | 27 | | | | 17.6 | 3 5.22 | 10.22 | 11 |



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| Section | | | E | Existing Grou | | | Design | |
|---------|-----|--|----------|---------------|---------|---|---------------|--------|
| No. | 1.1 | Distance | (Centre) | (Left) | (Right) | River Bed | HWL | Dike |
| | | (km) | | (m.PP) | (m PP) | (m.PP) | <u>(m.PP)</u> | (m.PP) |
| BKT | 280 | 19,680 | 16.87 | 18.36 | 15.30 | 5.26 | 10.26 | 11.20 |
| BKT | 282 | 19,773 | 14.50 | 13.21 | 14.43 | 5.30 | 10.30 | 11,30 |
| BKT | 283 | 19,823 | 11.45 | 12.71 | 11.18 | 5.32 | 10.32 | 11.32 |
| BKT | 284 | 19,872 | 11.83 | 12.80 | 11.07 | 5.34 | 10.34 | 11.34 |
| BKT | 286 | 19,957 | 10.27 | 11.12 | 11.90 | 5.37 | 10.37 | 11.3 |
| BKT | 288 | 20,073 | 10.07 | 10.24 | 10.44 | 5.42 | 10.42 | 11.4 |
| BKT | 290 | 20,174 | 9.56 | 10.88 | 10.62 | 5.46 | 10.46 | 11.4 |
| BKT | 292 | | 10.06 | 10.79 | 9.98 | 5.50 | 10.50 | 11.5 |
| BKT | 294 | | 10.64 | 11.00 | 12.60 | 5.53 | 10.53 | 11.5 |
| ВКГ | 296 | | 12.59 | 11.58 | 14.32 | 5.56 | 10.56 | 11.5 |
| BKT | 298 | | 15.12 | 13.81 | 15.97 | 5.61 | 10.61 | 11.6 |
| BKT | 300 | | 17.24 | 15.26 | 16.82 | 5,65 | 10.65 | 11.6 |
| BKT | 302 | | 14.95 | 13.94 | 14.60 | 5.69 | 10.69 | 11.6 |
| BKT | 304 | | 13.04 | 13.70 | 12.51 | 5.75 | 10.75 | 11.7 |
| BKT | 306 | the second s | 11.45 | 12.50 | 11.30 | 5.79 | 10.79 | 11.7 |
| BKT | 308 | | 12.56 | 11.93 | 12.21 | 5.83 | 10.83 | 11.8 |
| BKT | 310 | | 12.48 | 13.50 | 12.67 | 5.88 | 10.88 | 11.8 |
| BKT | 312 | | 15.12 | 14.56 | 15.10 | 5.91 | 10.91 | 11.9 |
| BKT | 314 | and the second s | 16.90 | 15.39 | 16.46 | 5.95 | 10.95 | 11.9 |
| ВКТ | 316 | | 16.12 | 12.87 | 16.12 | 5.99 | 10.99 | 11.9 |
| BKT | 318 | | 15.07 | 14.01 | 16.12 | 6.03 | 11.03 | 12.0 |
| вкт | 320 | | 15.80 | 14.98 | 16.15 | 6.08 | 11.08 | 12.0 |
| ВКТ | 322 | | 9.92 | 10.14 | 10.48 | 6.13 | 11.13 | 12.1 |
| вкт | 324 | a second second | 10.20 | 10.58 | 10.76 | 6.17 | 11.17 | 12.1 |
| BKT | 326 | | 9.67 | 9.72 | 9.80 | 6.22 | 11.22 | 12.2 |
| BKT | 328 | | 9.10 | 9.41 | 9.10 | 7.25 | 11.25 | 12.2 |
| BKT | 330 | | 15.42 | 16.85 | 15.20 | 7.29 | 11.29 | 12.2 |
| BKT | 332 | | 18.88 | 19.46 | 16.82 | 7.33 | 11.33 | 12.3 |
| BKT | 334 | | 15.26 | 17.56 | 15.40 | | 11.38 | 12.3 |
| BKT | 336 | | 17.74 | 15.66 | 17.85 | 7.43 | 11.43 | 12.4 |
| вкт | 338 | | 14.69 | 13.97 | 16.18 | | 11.48 | 12.4 |
| BKT | 34(| | 15.88 | 15.22 | 15.87 | 7.52 | 11.52 | 12 5 |
| BKT | 34/ | | 12.03 | 12.76 | 12.51 | 7.57 | 11.57 | 12 |
| вкт | 34 | | 12.94 | 12.25 | 11.19 | | 11.63 | 12.0 |
| BKT | 340 | | 11.62 | 12.23 | 12.06 | | 11.68 | 12.0 |
| BKT | 34 | | 17.51 | 16.96 | | | 11.73 | 12.3 |
| BKT | 34 | | 17.75 | 17,72 | | | 12.95 | 13.9 |
| BKT | 35 | | 17.86 | 16.92 | 17.00 | A DESCRIPTION OF TAXABLE PROPERTY. | 12.98 | 13 9 |
| BKT | 35 | | 18.26 | 18.12 | 18.53 | | 13.03 | 14.(|
| BKT | 35 | | 14.26 | 16.63 | 16.04 | the second se | 13.08 | 14.0 |
| CP. | | 1 23,610 | 10.30 | 14.30 | 14.53 | 9.21 | 13.21 | 14.2 |

Table. 4.7 DIMENSION OF LONGITUDINAL PROFILE S (8/10-2)

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Table 4.7 DIMENSION OF LONGITUDINAL PROFILES (9/10)

| Section | Distance | Distance Accumulative | Existing | Existing Ground | punor | Existing Dike | ikc | - 1 | | 5 | |
|-------------------------|----------|-----------------------|------------------|-----------------|----------|------------------|------------|----------|--------|----------|----------|
| No. | | Distance | River Bed | Left | Right | Left | Rught | r Bod | H.W.C. | | Dike |
| | (cm) | (km) | (m, 17G) | (m, TTG) (| (m, 11G) | (m, TTG) (m | () 11() | (m, 11G) | | (m, 17G) | (m, TTG) |
| "B' OI | 0000 | 0.000 | | | 0.57 | • | - | -5.40 | | -0.20 | 0.80 |
| | 1 038 | 1 078 | | | 0.85 | · · | | -5.23 | | 9 | 0.97 |
| CPLV2 CPLV3 | 1.087 | 2.125 | -2.38 | 0.37 | 1 49 | 0.71 | ÷. | -5.05 | -2.05 | 0.15 | 1.15 |
| BLO4 | 1.088 | 3.213 | : | | 0.95 | | 1.30 | 4.86 | • • | 0.34 | 134 |
| CB1.05 | 0.925 | 4,138 | • | • | 2.13 | 760 | 2.54 | 4.71 | | 0.49 | 1.49 |
| CB1.06 | 1.037 | 5.175 | | | 13 | 1.30 | 2.51 | 4.54 | | 0.66 | 1.66 |
| CBI 07 | 0.950 | 6,125 | | | 0.86 | | 2.33 | 4.38 | • | 0.32 | 1.82 |
| CBL 08 | 1.025 | 7.150 | | · | 0.55 | 1.68 | 3.36 | 4.21 | ÷ | 6.0 | 8 |
| CB1.09 | 1.100 | 8.250 | : | | 1.35 | 2.10 | 4.52 | 4.3 | | 1.18 | 2.18 |
| CBL10 | 0.975 | 9.225 | | | 1.18 | 2.35 | 5.07 | -3.86 | | 1.4 | 2.34 |
| CBLII | 1.000 | 10.225 | | | 1.38 | 1.82 | 3.98 | -3.70 | | 1.50 | 2:50 |
| Conf. with Bekasi River | 0.525 | | : | • | 2:55 | 2.46 | 4.09 | -3.61 | | 1.59 | 2.59 |
| CBL12 | 0.525 | 11.275 | - | | 371 | 3.09 | 4.20 | -3.35 | | 1.85 | 2.65 |
| CBL 13 | 006.0 | 12.175 | | | 4 | 3.01 | 3.38 | -2.90 | | 2.30 | 3.10 |
| CBL14 | 0.983 | 13.163 | | . ' | 2.21 | 2.74 | 4.40 | 2.40 | | 2.80 | 3.60 |
| CBL15 | 1.037 | 14.200 | | : | 3.87 | 2.41 | S.49 | -1.88 | | 3.32 | 4.12 |
| CBL16 | 1.025 | 15.225 | | | 3.08 | 4.08 | 5.52 | -1.37 | | 3.83 | 4.63 |
| CBL17 | 1.050 | 16.275 | | | 334 | | 4.52 | -0.85 | • | 4.35 | 5.15 |
| CBL18 | 1.025 | 17300 | | | 4.25 | * • • • | 5.11 | -0.33 | | 4.87 | 5.67 |
| CBL19 | 1.000 | 18.300 | | | 4,99 | | 6.26 | 0.17 | | 5.37 | 6.17 |
| CBL20 | 1.013 | 19.313 | : | | 5.56 | | 6.36 | 0.67 | | 5.87 | 6.67 |
| CB1.21 | 000"1 | 20.313 | ; | | 7.31 | | 7.36 | 1.17 | | 6.37 | 7.17 |
| CB1.22 | 0.925 | 21.238 | | | 8.00 | | : 9.31 | 1.64 | | 6.84 | 7.64 |
| | 000 0 | 201.00 | | | 100 | : | 0.94 | 202 | | 204 | 2.02 |

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| Distance Existing (arr) Existing Distance Distance Existing Existing Distance (arr) Existing Distance (arr) Distance (arr) Existing Distance (arr) Distance (arr) Distance (arr) Existing Distance (arr) Distance (arr) Distance (arr) Distance (arr) Existing Distance (arr) Distance (arr) Distance (arr) Existing Distance (arr) Distance (arr) Distance (arr) Existing Distance (arr) Distance (| BEKASI RIVER | | | | | | | | - | | |
|--|----------------------------|----------|-------------------|-----------------------|---------------------|--------------------|---------------------------------|---------------------------------------|----------|--------------------|------------------|
| Distance Actimulative Existing Existing Distance NoverBod | | | | | · · · | | | • | | | |
| Distance Rayer Left Rayer | sction | | Accumulative | Existing | Existing G | round | Existing Dike | | Å | 5 | |
| Conf. with CELJ 0.000 | No. | (km) | | River Bed (m, TTG) | Left (m, TTG) (t | Right m, TTG) | Left Right (m, TTG) (m, TTG) | River Bed (m. TTG) | | H.W.L. (m, TTG) | Dike (m. TTG) |
| 1100 1.000 5.04 1.00 2.81 3.81 3.81 2.94 4.25 2.94 4.35 3.30 1.000 3.000 3.56 3.55 3.75 5.37 5.36 3.75 5.37 5.39 4.35 5.36 3.55 5.34 4.35 5.35 5.34 4.35 5.36 3.55 5.36 3.55 5.36 3.55 5.36 3.55 5.36 3.55 5.36 3.55 5.36 3.56 <td< td=""><td>BKS01(Conf. with CBL)</td><td>0.000</td><td>0.000</td><td></td><td>5.15</td><td>0.34</td><td>1.38</td><td>-3.61</td><td></td><td>2.39</td><td>3.39</td></td<> | BKS01(Conf. with CBL) | 0.000 | 0.000 | | 5.15 | 0.34 | 1.38 | -3.61 | | 2.39 | 3.39 |
| 1000 2000 -538 294 294 426 420 420 170 337 1000 2000 300 -406 335 456 511 521 431 554 1000 5000 -205 535 456 511 541 431 554 1000 5900 -205 501 456 511 541 511 541 531 546 513 546 513 554 531 546 513 541 511 541 511 511 541 511 511 541 511 511 541 511 511 541 511 511 541 511 511 541 521 541 521 541 521 542 521 541 521 541 521 541 521 541 521 541 551 521 521 521 521 521 551 521 551 5 | BKS02 | 1.050 | 1.050 | • | 1.00 | 2.81 | | -2.94 | | 3.06 | 4.06 |
| 1000 3000 -4.69 3.55 3.75 5.20 5.46 -1.67 2.33 4.53 12000 5.900 -2.05 5.34 4.70 5.86 -1.06 2.33 5.93 5.45 5.91 5.45 5.91 | CSO3 | 1.000 | 2:050 | | 2.94 | 2.94 | | -2.30 | ; | 3.70 | 4.70 |
| 0000 3500 2.05 5.35 4.56 5.91 5.63 5.91 5.63 5.91 5.61 6.71 5.91 5.61 6.71 5.91 5.61 6.71 5.91 5.61 6.71 5.91 5.61 6.71 5.91 5.61 6.71 5.91 5.61 6.71 5.91 5.61 6.71 5.91 5.61 6.71 5.91 5.61 6.81 6.83 5.86 0.46 3.93 5.72 9.91 7.21 9.91 7.21 9.91 7.21 9.91 7.21 9.91 7.21 9.91 7.21 9.91 7.21 9.91 7.21 9.91 7.21 9.91 7.21 9.91 7.21 9.91 7.21 9.91 7.21 9.91 7.21 9.92 7.21 9.93 7.21 9.93 7.21 9.93 7.21 9.93 7.21 9.93 7.21 9.93 7.21 9.93 7.21 9.93 7.21 9.93 7.21 <th< td=""><td>SQ</td><td>1.000</td><td>3.050</td><td></td><td>3.65</td><td>3.75</td><td></td><td>-1.67</td><td></td><td>433</td><td>5.33</td></th<> | SQ | 1.000 | 3.050 | | 3.65 | 3.75 | | -1.67 | | 433 | 5.33 |
| 1.000 5.950 -2.85 6.41 4.70 5.86 -0.46 3.34 6.13 1.300 5.300 -0.30 5.30 6.57 7.39 1.34 5.49 7.39 1.300 5.300 -0.36 8.39 7.59 1.30 5.34 5.49 7.39 1.300 5.300 -0.46 8.39 7.39 2.37 7.39 5.34 7.39 1.300 1.300 1.323 8.39 1.03 1.31 5.41 1.01 5.11 5.41 7.29 5.37 7.39 5.36 5.37 7.39 5.36 5.37 7.39 5.36 5.31 5.35 | SOS | 0.900 | 3.950 | -2.05 | 3.93 | 4 56 | | -1.09 | : | 4.91 | 16.2 |
| 1.000 5.90 -3.80 6.1 6.34 0.18 4.18 6.18 0.750 8.000 -0.27 6.92 7.01 1.01 5.01 7.01 0.750 8.000 -0.27 6.92 7.01 1.01 5.01 7.01 0.750 8.000 0.03 8.66 10.33 2.70 6.12 8.17 0.750 8.000 1.125 11.125 11.025 0.73 8.73 8.40 7.01 8.71 0.800 11.225 0.57 14.07 <t< td=""><td>S06</td><td>1.000</td><td>4.950</td><td>-2.83</td><td>6.34</td><td>4,70</td><td>5.86</td><td>-0.46</td><td></td><td>5.54</td><td>6.54</td></t<> | S06 | 1.000 | 4.950 | -2.83 | 6.34 | 4,70 | 5.86 | -0.46 | | 5.54 | 6.54 |
| 1.300 7.200 -0.27 6.32 7.01 1.01 5.01 7.01 0.750 8.000 -0.46 8.39 7.49 5.49 7.49 5.49 7.49 5.49 7.49 5.49 7.49 5.49 7.49 5.49 7.49 5.49 7.49 5.49 7.49 5.49 7.49 5.49 7.49 5.49 7.49 5.49 7.49 5.49 7.49 5.49 7.49 5.49 7.49 5.49 7.49 5.49 1.13 1.21 3.44 9.47 9.13 9.13 9.14 9.14 9.14 9.14 9.15 9.14 9.14 9.15 1.13 1.22 5.44 1.13 1.22 5.45 1.13 1.23 5.45 1.13 1.23 5.45 1.13 1.23 5.45 1.13 1.23 5.45 1.13 1.23 5.45 1.13 1.23 5.45 1.13 1.24 5.45 1.14 5.45 1.149 5.46 | S07 | 1.000 | 5.950 | | 6.51 | 6.34 | | 0.18 | | 6.18 | 7.18 |
| 0750 8.000 -0.46 8.99 7.49 1.49 5.49 7.49 0.000 9.000 0.03 8.39 9.35 10.44 5.49 7.27 9.27 8.29 9.29 0.000 10.800 11.922 0.57 9.74 8.01 3.37 7.27 9.27 9.29 0.1025 11.722 11.722 11.722 13.19 15.22 6.13 11.18 9.11 11.18 9.21 11.18 9.21 11.18 9.21 11.18 9.21 11.18 9.21 11.18 9.21 11.18 9.21 11.18 9.21 11.18 9.21 11.18 9.21 11.18 9.21 11.18 | SOS | 1.300 | 7.250 | | 6.92 | 10.7 | | 1.01 | | | 8.01 |
| 1000 9000 0.05 8.99 9.35 5.11 6.12 8.13 0.9000 1.125 1.1325 1.13 8.66 10.33 3.277 5.39 9.39 0.9000 1.1325 1.1325 1.231 8.66 10.33 3.277 7.279 9.39 0.9000 1.1325 1.139 8.66 10.33 3.277 7.29 9.99 0.8000 1.2752 1.45 1.213 8.64 10.041 1.241 0.8000 1.6525 3.56 1.437 15.33 1.319 15.33 1.319 15.33 1.318 1.31 | S09 | 0.750 | 8.000 | | 8.99 | 67.7 | | 1.49 | | . i | 8.49 |
| 0900 9900 0.23 7.38 10.14 2.70 6.70 8.70 1137 1273 1.45 12.31 8.64 10.33 3.27 7.27 9.27 1075 1.350 1.45 13.19 13.28 5.93 7.99 9.99 1075 1.350 1.45 13.19 13.28 5.91 11.18 1075 1.5735 1.45 13.19 13.28 5.93 11.18 1075 1.5735 1.47 1.573 1.43 9.15 11.18 0.800 1.5735 6.71 13.73 15.73 5.91 10.92 12.24 6.51 10.13 12.41 0.800 1.5735 6.72 13.73 13.15 12.14 12.91 12.15 13.15 13.15 13.15 15.15 13.15 15.15 15.15 15.15 15.15 15.15 15.15 15.15 15.15 15.15 15.15 15.15 15.15 15.15 15.15 | SIO | 1.000 | 000.6 | -0.68 | 8.99 | 9.35 | | 2.12 | | | 9.12 |
| 0900 10.800 1.19 8.66 10.33 3.27 7.27 9.27 1.125 11.925 0.57 9.74 8.07 9.13 1.39 9.38 1.18 1.125 11.925 0.57 9.74 8.07 9.13 1.33 8.45 5.95 7.99 9.99 1.0750 18.450 3.97 14.07< | SII | 0.900 | 006.6 | : | 7.58 | 10.14 | | 2.70 | | : | 9.70 |
| 1.125 1.125 0.57 9.74 8.07 3.99 7.99 8.99 3.90 0.56 3.50 0.56 3.50 0.56 3.50 0.56 3.50 0.56 3.56 0.56 3.56 0.57 3.53 9.51 11.118 3.53 9.51 11.118 3.53 9.51 11.118 3.53 9.51 11.118 3.53 9.53 11.118 3.53 9.53 11.118 3.53 9.53 11.118 3.53 9.53 11.118 3.53 9.53 11.124 3.53 9.53 11.124 3.53 9.53 11.125 3.53 9.53 13.53 | S12 | 0.900 | 10.800 | | 8.66 | 10.33 | | 3.27 | | : | 10.27 |
| 0300 12.725 1.45 12.31 8.45 13.32 8.15 9.15 11.18 9.18 11.18 9.18 11.18 9.18 11.18 9.18 11.18 9.18 11.18 9.18 11.18 9.18 11.18 9.18 11.18 9.18 11.18 9.18 11.18 9.18 11.18 9.18 11.18 9.18 11.18 9.18 11.15 13.24 6.52 10.04 13.55 | S13 | 1.125 | 11.925 | | 9.74 | 8.07 | | 3.99 | | | 10.95 |
| I 075 I 3800 I 65 I 313 I 3.2.8 S 38 9.38 I 118 0.875 1.487 15.37 14.07 14.07 14.06 15.37 5.35 9.38 11.35 5.35 11.35 5.35 11.53 5.35 11.53 5.35 11.53 5.35 11.53 5.35 11.53 11.55 5.35 11.53 12.43 6.52 13.53 5.35 11.53 13.53 5.35 11.53 13.53 5.35 11.55 13.53 5.35 13.53 5.35 13.53 5.35 13.53 13.53 13.53 13.53 13.53 13.55 | 214 2 | 0.800 | 202 01 | | 12.31 | 8 64 | | 4 50 | ı | | 11 \$(|
| 1.050 1.4300 1.400 1.400 1.400 1.537 1.537 1.537 1.537 1.537 1.537 1.537 1.537 1.537 1.537 1.537 1.537 1.537 1.537 1.537 1.535 1.535 1.537 1.537 1.537 1.537 1.537 1.537 1.537 1.537 1.537 1.537 1.535 1.135 1.235 1.135 1.235 1.135 1.245 1.235 <t< td=""><td></td><td>1 075</td><td>13 800</td><td></td><td>13 10</td><td>12.72</td><td></td><td>81 ¥</td><td></td><td></td><td>51 61</td></t<> | | 1 075 | 13 800 | | 13 10 | 12.72 | | 81 ¥ | | | 51 61 |
| 0.875 15.775 5.37 15.35 13.55 <th< td=""><td></td><td>000</td><td>000171</td><td></td><td>101</td><td></td><td></td><td>20.2</td><td></td><td></td><td></td></th<> | | 000 | 000171 | | 101 | | | 20.2 | | | |
| Own 15.75 5.40 15.37 1.400 15.37 1.400 1.202 1.202 1.203 1.213 1. | | 2001 | | 14.0 | | 3 | ç | | | | 10.41 |
| 0.800 0.8.25 5.36 15.37 5.37 15.37 5.32 10.32 15.35 1 | | C/0'0 | C7/-C1 | 4.38 | 7.7 | 71.5 | CH.Z1 | | | : | |
| 1.000 17.525 6.72 17.07 15.73 7.55 11.55 12.55 11.55 12.55 11.55 12.55 11.55 12.15 14.19 15.15 17.05 17.46 17.46 17.46 | S18 | 0.800 | 10.525 | 8 | 14.87 | 15.37 | • | 6.92 | | | 13.92 |
| Betasis weir) 1.000 18.525 6.91 18.42 17.83 8.19 12.19 14.19 ANG RAVER 1.500 20.025 7.43 19.38 18.96 9.15 13.15 15.15 17.05 17.15 17.05 17.15 17.05 17.40 17.40 17.40 17.40 17.40 17.40 17.40 17.40 | S19 | 1.00 | 17.525 | 6.72 | 17.07 | 15.73 | · . | 7.55 | | - | 14.55 |
| Bekassi weir) 1.500 20.025 7.43 19.38 18.96 9.15 13.15 15.15 | S20 | 1.000 | 18.525 | 6.91 | 18.42 | 17.83 | | 8.19 | | | 15.19 |
| ANG RIVER Distance Accumulative Existing Ground Existing Dise Design Distance Accumulative Evisting Ground Existing Dise Design Design Distance Accumulative Evisting Ground Existing Dise Design Design Distance Nam) (an) (n, TTG) (n, TTG) (n, TTG) (n, TTG) Cont. with CBL) 0.000 3.66 6.72 8.97 3.90 7.40 Cont. with CBL) 0.000 0.000 3.66 6.72 8.97 3.90 7.40 Cont. with CBL) 0.000 0.000 3.56 6.72 8.97 3.90 7.40 Cont. with CBL) 0.000 0.000 3.56 6.72 8.97 9.36 Cont. with CBL) 0.000 0.000 3.56 6.72 8.93 9.36 Cont. with CBL) 0.875 0.825 8.21 10.94 12.34 9.36 9.36 0.825 3.488 7.325 11.57 | S21(Bekasi weir) | 1.500 | 20:025 | 7.43 | 19.38 | 18.96 | | 9.15 | | | 16.15 |
| ANG RAVER Distance Accumulative Existing Cround Existing Office Existing Dist Design Design Distance Accumulative Existing Existing Office Distance Accumulative Existing Cround Existing Dist Existing Dist Design Distance River Bed H.W.C. H.W.L. Di Distance Distance Exist 100 (m, TTG) (m, TTG) (m, TTG) Distance Exist 100 (m, TTG) M.L.TG) Distance Distance Exist 10 Distance Exist 110 Exist 110 </td <td></td> | | | | | | | | | | | |
| ANG RIVER Distance Accumulative Existing Ground Existing Ground Existing Dite Design Design Distance Accumulative Existing Cound Existing Ground Existing Dite Existing Dite Design Design Distance River Bed Left Right Left Right Left Right River Bed H.W.L. D (am) (am) (m, TTG) (m, TTG) (m, TTG) (m, TTG) (m, TTG) (m, TG) Conf. with CBL 0.000 3.66 6.72 8.97 3.90 7.40 Conf. with CBL 0.000 3.66 6.72 8.97 4.84 8.34 Conf. with CBL 0.000 3.66 6.72 8.97 4.84 8.34 Conf. with CBL 0.000 3.65 10.39 10.39 5.86 9.36 Conf. with CBL 0.875 0.875 10.39 10.39 5.86 9.36 0.825 3.488 7.38 11.157 7.65 11.157 7.65 11.155 | | | | | | | - | | | | |
| Distance Accumulative Existing Ground Existing Dike Design Design Distance River Bed Left Right Left Right River Bed H.W.C. H.W.L. D (nm) (nm) (nn, TTG) < | SADANG RIVER | | | | | | | 11 11 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 | • | | |
| Ubstance Existing Unice Existing Unic | | | | - | (, , | | i i | | F | | |
| Distance Kiver Bed Left Right Left Right Left Right Kiver Bed H.W.L. H.W.L. </td <td></td> <td>TISIGNOC</td> <td></td> <td>cusung.</td> <td>P</td> <td>Lound</td> <td>ĥ</td> <td></td> <td></td> <td></td> <td></td> | | TISIGNOC | | cusung. | P | Lound | ĥ | | | | |
| Conf. with CBL) 0.000 0.000 3.66 6.72 8.97 3.90 7.40 0.375 0.375 0.375 4.20 9.53 9.29 4.84 8.34 0.375 0.375 0.375 4.20 9.53 9.29 4.84 8.34 0.375 0.375 0.375 10.09 10.39 5.86 9.36 0.383 2.665 8.21 10.09 10.39 5.86 10.26 0.825 3.488 7.85 11.08 11.14 7.65 11.15 0.800 4.238 8.32 11.08 11.15 8.51 12.36 0.800 6.275 10.37 13.25 13.47 9.68 13.18 0.9000 6.275 10.37 13.25 13.16 10.65 14.15 1.1.355 7.600 12.06 16.41 17.10 15.57 15.57 | | (rm) | UNITARIO (MAI) | Kiver Bed (m. TTG) | (m. 77G) (1 | n, TTG) n, TTG) | Lett Kught (m. TTG) (m. TTG) | Kiver Bcd (m, TTC) | | | (п. TTG) |
| Conf. with CBL) 0.000 0.000 3.66 6.72 8.97 3.90 7.40 0.875 0.875 4.20 9.53 9.29 3.96 7.40 0.875 0.875 0.875 4.20 9.53 9.29 3.96 7.40 0.875 0.875 0.875 4.20 9.53 9.29 5.36 9.36 0.875 0.875 0.825 8.21 10.09 10.39 5.86 9.36 0.825 3.488 7.85 11.08 11.14 7.65 11.15 0.825 3.488 7.35 13.47 10.37 13.25 13.18 0.800 6.275 10.37 13.25 13.15 9.68 13.18 0.900 6.275 10.37 13.25 13.15 9.68 13.18 1. Jakara-Cikarang 1.325 7.600 12.06 16.41 17.10 15.57 | | | | | : | | | | - | | · . |
| 0.875 0.875 0.875 4.20 9.53 9.29 4.84 8.34 0.950 1.825 6.54 10.09 10.39 5.86 9.36 0.838 2.665 8.21 10.94 12.34 6.76 10.26 0.825 3.488 7.85 11.14 7.65 11.15 0.825 3.488 7.85 11.08 11.14 7.65 11.15 0.825 3.488 7.85 11.08 11.14 7.65 11.15 0.826 3.488 7.85 11.75 11.57 8.51 12.01 0.800 4.238 8.32 11.75 11.57 9.68 13.18 0.900 6.275 10.37 13.25 13.16 16.65 14.15 0.900 6.275 10.37 13.25 13.16 15.07 15.57 | G01(Conf. with CBL) | 0.000 | 0.000 | 3.66 | 6.72 | 8.97 | | 3.90 | | 7.40 | . 8.00 |
| 0.950 0.25 0.54 0.09 0.55 0.35 0.338 2.665 8.21 10.94 12.34 6.76 10.26 0.825 3.488 7.85 11.08 11.14 7.65 11.15 0.825 3.488 7.35 11.75 11.57 8.51 12.01 0.800 4.238 8.32 11.75 11.57 8.51 12.01 1.087 5.375 9.87 13.95 13.47 9.68 13.18 0.900 6.275 10.37 13.25 13.15 10.65 14.15 1.1.325 7.600 12.06 16.41 17.10 12.07 15.57 | | 0.875 | 0 275 | | 0.51 | 000 | | V 8 V | | 0.24 | 000 |
| 0.838 2.665 8.21 10.94 12.34 6.76 10.26 0.825 3.488 7.85 11.08 11.14 7.65 111.15 0.800 4.288 8.32 11.75 11.57 8.51 11.15 0.800 4.288 8.32 11.75 11.57 8.51 12.05 1.087 5.375 9.87 13.95 13.47 9.68 13.18 0.900 6.275 10.37 13.25 13.15 10.65 14.15 1. Jakara-Cikarang 1.325 7.600 12.06 16.41 17.10 15.57 | i con | 0.050 | 508 1 | | | 6776 | · · · | 40°4 | | 9.7C | |
| 0.000 2.000 0.01 10.26 10.21 12.01 10.26 12.01 12.01 12.01 12.01 12.02 13.18 12.02 13.18 13.16 13.16 13.16 13.207 13.207 13.57 13.207 13.57 13.57 15.57 15.57 15.57 15.57 15.57 15.57 15.57 15.57 15.57 15.57 15.57 15.57 15.57 15.57 15.57 15.57 < | | | 170'I | | | 10.07 | | | | | 70 41 |
| 0.825 3.488 7.85 11.08 11.14 7.65 11.15 0.800 4.288 8.32 11.75 11.57 8.51 12.01 1.087 5.375 9.87 13.95 13.47 9.68 13.18 0.900 6.275 10.37 13.25 13.15 10.65 14.15 0.1.1.26 15.16 15.16 15.16 15.16 15.57 | | 0.000 | 400.4 1 | 17.0 | 10.94 | 4C-71 | | 0.0 | | 10.20 | 00''' |
| 0.800 4.288 8.32 11.75 11.57 8.51 12.01 1.087 5.375 9.87 13.95 13.47 9.68 13.18 0.900 6.275 10.37 13.25 13.15 10.65 1.4.15 11. Jakara-Cikarang) 1.325 7.600 12.06 16.41 17.10 12.07 12.07 | 5C05 | 0.825 | 3,488 | 7.85 | 11.08 | 11.14 | | 7.65 | | - H - 12 | 47.H |
| 1.087 5.375 9.87 13.93 13.47 9.68 13.18 0.900 6.275 10.37 13.25 13.15 10.65 10.65 14.15 11. Jakara-Cikarang) 1.325 7.600 12.06 16.41 17.10 15.57 | 9000 | 0.800 | 4.288 | | 11.75 | 11.57 | | 8.51 | | 12.01 | 12.61 |
| 0.900 6.275 10.37 13.25 13.15 10.65 14.15 14.15 14.15 15.57 15.15 15.57 15.57 15.57 15.57 | SG07 | 1.087 | 5.375 | | 13.93 | 13.47 | | 9.68 | | 13,18 | 13.78 |
| 1.325 7.600 12.06 16.41 17.10 12.07 11 12.07 11 12.07 | SG08 | 0.900 | 6.275 | | 13:25 | 13.15 | | 10.65 | | . 14,15 | 14.75 |
| | SG09(J1, Jakarta-Cikarang) | 1.325 | 7.600 | | 16.41 | 17.10 | | 12.07 | | 15.57 | - 16.17 |

Table 4.8 DIMENSION OF STANDARD CROSS SECTIONS (1/5)

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| CIDURIAN RIVER | (Estuary - JI Serang Ray | (a <parig≥)< th=""><th>Q=650m3's (25-year)</th></parig≥)<> | Q=650m3's (25-year) |
|----------------|--------------------------|--|---------------------|
| | | | |

| | · · · · · | . 1 | Gradient | ាភាស | | a and against the |
|------------|------------------|-------|----------------------|--------|-----------|-------------------|
| | | | Water level | 6 60 | | Q(a+2ah m 7s) |
| Low Water | Width(top,m) | 51.0 | Fotal water depth(m) | 6 60 | | 656.9 |
| Channel | Width(bottoen.m) | 33.0 | Water depth(m) | 4 50 | | Free board(m) |
| | Depúi | 4 50 | Width(m) | 510 | | 10 |
| | 1 | 20 | A(m ⁴) | 306 3 | | Crown width(m) |
| | л | 0.030 | S(m) | 53 12 | | 50 |
| | Bed height(m) | 0.0 | R(m) | \$ 166 | V(m/s) | 1.91 |
| | ł., | | g(m7s) | 584.0 | | |
| High Water | Width(one side) | 250 | Water depth | 2 30 | S(m) | 30.1 |
| Channel | Skoe gradient | - 20 | Width(m) | 29.6 | R(m) | 2 083 |
| | η | | A(m [*]) | | qh(m'/s) | 36 4 |
| | | | V(m/s) | 0.58 | 201(m /s) | 12 9 |

CIMANCEURI RIVER (Estuary - J. Serang Raya <Bataraja>) Q=290n3/s(25-year)

| 1,1 | • | er n | Gradient | 1/2860 | h | · · · · · · · · · · · · · · · · |
|---------------------------------------|-----------------|-------|----------------------|--------|-----------|---------------------------------|
| | | | Water kvel | · 5 BO | | Q(q1+2qh,m /s) |
| Low Water | Wich (10p.m) | 28.0 | Total water depth(m) | 5.80 | | 292 3 |
| Channel | Width(bottom,m) | 14.0 | Water depth(m) | 3 50 | | Free board(m) |
| 1.10 | Depth | 3.50 | Width(m) | 28 O | | Ō B |
| 11 - 11 - 11 - 11 - 11 - 11 - 11 - 11 | Ĩ. | 20 | A(m) | 137.9 | | Crown width(m) |
| | n . | 0.030 | S(#) | 29 65 | | 50 |
| 1. T | Bed height(m) | 00 | R(m) | 4.651 | V(m's) | 1.74 |
| | | 1.1 | q(m /s) : | 239.5 | 1 | |
| High Water | Width(one side) | 17.0 | Water depth | 2 30 | S(m) | 22 |
| Channel - | Slope gradient | 20 | Width(m) | 21.6 | R(m) | 2 005 |
| 1 | 3 | 0.050 | A(m') | . 44.4 | qt/(m*/s) | 26.4 |
| | | | V(m/s) | 0 59 | 2qh(m'/s) | 52 B |

| CIRARA8 | RIVER (Estuary | inga | tion canal(CRR-9)) | | Q=75m3's | i(25-year) |
|------------|-----------------|-------|----------------------|--------|-----------|----------------|
| | | | Gradient | 1/2060 | | 1. :. <u>-</u> |
| | | Í. | Water kvel | 3.00 | | Q(q+2qh,m'/s) |
| Low Water | Width(top.m) | 19.0 | Total water depth(m) | 3.00 | | 76.3 |
| Channel | Width(bottom,m) | 110 | Water depth(m) | 2.00 | | Free board(m) |
| | Depth | 2.00 | Wintth(m) | 19.0 | | 0.6 |
| | [| 20 | Ā(m') | 49.0 | | Crewn with(m) |
| | 0 | 0.030 | S(m) | 19.94 | | 5.0 |
| | Sed height (m) | 0.0 | R(m) | 2.457 | V(m's) | 1 34 |
| | | | q(m/s) | 65.3 | | |
| High Water | Width(one side) | 32.0 | Water depth | 1 00 | \$(m) | 14 2 |
| Channel | Skipe gradient | 2.0 | With(m) | 14,0 | R(m) | 0.913 |
| | a | 0.050 | A(m') | 13,0 | qh(m'/s) | 5.4 |
| - | | | V(m's) | 0.41 | lah(m'/s) | 10.8 |

canal (RR-9) - Irrigation canal (CRR-18)1 CIRARAB RIVER

| | CIT BALLAL CALLA | | I BIGALOG CARAGE AN | -10/1 | 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 | |
|------------|------------------|-------|----------------------|--------|---------------------------------------|--|
| | 1 | · . | Gradient | 1/2060 | | |
| | | · · · | Water kvel | 3 00 | | Q(q1+2qh,m /s) |
| low Water | Width(top,m) | 15.0 | Total water depth(m) | 3 00 | | 55.8 |
| Channel | Width(bottom,m) | 7.0 | Water depth(m) | 2 00 | | Free board(m) |
| | Depth | 2 00 | Width(m) | 150 | · · · · · | 06 |
| | 1 | | A(m ²) | 37.0 | | Crown wighh(m) |
| | n | 0.030 | S(m) | 15.94 | | 5.0 |
| | Bed height(m) | | F.(m) | 2 321 | V (m/s) | 1 29 |
| | | | q(m'/s) | 47.6 | | ···· · · · · · · · · · · · · · · · · · |
| High Water | Width(one side) | | Water depth | 001 | 5(m) | 11 2 |
| Channel | Skipe gradient | 20 | Width(m) | 110 | Ř(m) | 0 890 |
| | A | 0.050 | A(m ²) | | qh(m'/s) | 4.1 |
| | | | Y(m's) | 0.41 | 2q1(m/s) | B 2 |

CISADANE RIVER (Estuary - Pasar Baru wer)

| CISADANI | RIVER (Estuary | - Pasa | r Baru wer | | Q=1600m | 3.'s(SO-year) |
|------------|-----------------|--------|-----------------------|------------------|-----------|---------------------------------------|
| | | | | Barrana An An | | <csd-1></csd-1> |
| | | | Gradient | 1/3030 | | • • • • • • • • • • • • • • • • • • • |
| | | | Water level | 9.50 | | Q(q+2qh, o 4) |
| Low Water | Width(top.m) | 76.0 | Total water depth(m) | 9.50 | | 1505 2 |
| Channel | Walth bottom m} | 48 0 | Water depth(m) | 7.00 | | Free board(m) |
| | Depth | 7.00 | Width(m) | 76.0 | 1.1.1.1 | 10 |
| | 1 | 20 | A(m²) | 624.0 | | Crown width(m) |
| | 0 | 0.030 | \$(m) | 79.30 | | 5.0 |
| | Bed height(m) | 00 | R.(m) | 7.568 | V(m/s) | 2.4 |
| | | | q¥(m ¹ /s) | 1502.3 | | |
| figh Water | Walth(one side) | 30.0 | Water depth | 2 50 | \$(m) | 35 (|
| Channel | Slope gradient | 20 | Width(m) | 35 0 | R(m) | 2 28 |
| | n | 0 050 | A(m ¹) | 813 | qh(m /s) | 51.4 |
| 1.5 | | | V(m/s) | 0 63 | 2qh(m /s) | 102 1 |

Table 4.8 DIMENSION OF STANDARD CROSS SECTIONS (2/5)

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6 2

Estuary - J(. Oradient Varier level 57 O Totat water depd(m) 33 O Water depd(m) 4 CO Width(m) 3 O A (m²) 0 025 S(m) 1) O O R(m) cont 3 O Width(m) 0 040 A (m²) 0 040 A (m²) 5 O Water depdn Ment 3 O Width(m) 0 040 A (m²) 5 O Water depdn Ment 3 O Width(m) 0 040 A (m²) 5 O Water depdn Ment 3 O Width(m) 0 040 A (m²) 5 O Water depdn Ment 3 O Width(m) 0 040 A (m²) 5 O Width(m) 0 040 A (m²) 0 0 Q=\$10m3/x(100-year) <CKR-3> CENGKARENG FLOODWAY (Estuary - JCF-9) 1/4000 5 75 5 75 Q(qF2qh,m/s) Width(top;m) Width(bottom;m) Depth Low Water Free board(m) 4 00 Channel 57.0 279 B 58 30 Crown w 4.799 Bed height(m) V(m's) 1.75 S(m) 10.3 R(m) 13.3 Qh(m³/s) 0.46 Qh(m³/s) With(one side) High Water Channe! Slope gradient

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| | | | Q=510m3's(100-year) | |
|---------------|--|--|---------------------|--|
| CENGKARENG FL | | | | |
| | | | | |
| | | | | |

| | | | ŧ | | | <ckr-j></ckr-j> |
|---------------------------------------|-----------------|---------|----------------------|--------|------------------------|-----------------|
| 1 · · · · · · · | | | Gradient | 1/4000 | | |
| <u> </u> | | 1 ····· | Water level | 5.75 | N 197 P | Q(al+2ah.m /s) |
| Low Water | Width(top,m) | 53.0 | Total water depth(m) | 5.75 | ÷ | 5136 |
| Channel | Width(bottom,m) | 37 0 | Water depth(m) | 4 00 | | Free board(m) |
| | Depth | 4.00 | Width(m) | 53 0 | : | 10 |
| 1 | 1 | 20 | A(m') | 272 8 | | Crown width(m) |
| | n | 0.025 | S(m) | \$4 89 | : | S .0 |
| | Bed beight(m) | 0.0 | R(m) | 4.969 | V(m/s) | 1 84 |
| | | | q(m/s) | 502.3 | · · · · · · | |
| High Water | Width(one side) | 5.0 | Water depth | 175 | \$(m) | 89 |
| Channel | Sloce gradient | 2.0 | Width(m) | 85 | R(m) | 1 325 |
| 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 | n | 0.040 | A(m²) | 118 | qh(m'/s) | 5.6 |
| | | · | V(m/s) | 0.48 | 2qn(m [*] /s) | 113 |

| CENGKAR | ENG FLOODWA | Y | f The Third Control of the first fir | | Q=510m3 | (100-year) |
|------------|-----------------|-------|--|-------------------------|------------|----------------|
| | (Cengkareng we | - M. | okervaart cenal) | · · · · · · · · · · · · | 1 | (CKR-)> |
| | | | Gradient | 73125 | | |
| | | | Water level | 5.55 | | Q(qH2qh,m/s) |
| Low Water | Width(top.m) | \$1.0 | Total water depth(m) | 5 55 | | 517 |
| Channel | Width(bottom.m) | 35 0 | Water depth(m) | 4.00 | | Free board(m) |
| | Depth | 4.00 | Width(m) | 510 | · | |
| ,i ,i | 1 | 20 | A(m ²) | 251.1 | | Crown width(m) |
| | n | 0 025 | S(m) | 52.89 | | 5.0 |
| - | Bed height(m) | 0.0 | R(m) | 4.747 | V(m/s) | 2.03 |
| ÷ . | | | o(m /s) | 507,4 | | |
| High Waler | Width(one side) | 5.0 | Water depth | 1 55 | S(m) | 8 : |
| Channel | Slope gradieni | 20 | Wilth(m) | 81 | R(m) | 1,195 |
| | n | 0.040 | A(m ²) | 10 2 | qh(m'/s) | 5. |
| | | | V(m/s) | 0.50 | 20h (m /s) | 103 |

CENGKARENG FLOODWAY (Mookervaart canal - Angle river) Q-420m3/s(100-year)

| | 2 | Gradient | 1/3125 | | |
|-------------|--|---|---|---|--|
| i | | Water level | 5 55 | | Q(al+2ah,m/s) |
| h(top.m) | 44.0 | Total water depth(m) | 5 55 | | 431 7 |
| h(bottom m) | 28 0 | Water depth(m) | 4.00 | | Free board(m) |
| h | 4.00 | Width(m) | 44.0 | | 1.0 |
| | 20 | A(m [*]) | 212 2 | | Crown with(m) |
| | 0.025 | S(m) | 45.89 | | 5.0 |
| hcight(m) | 00 | R(m) | 4 624 | V(m's) | 1.99 |
| | · · · · | q(m /s) | 421.4 | | |
| h(one side) | 50 | Water depth | 1 55 | S(m) | 85 |
| gradient | 20 | Դ'idth(m) | | | 1 199 |
| | 0.040 | | | | 5.1 |
| | | V(m/s) | 0.50 | 2qh(11 /3) | 10 2 |
| | h(top.m) h(bostom.m) h hoight(m) h(one side) gradient | h(top.m) 44 0 5(bottom.m) 28 0 h 4 00 2 0 0.025 height(m) 0 0 h(one side) 5 0 gradient 2 0 | Water kvel h(top,m) 44.0 Total water depth(m) h(top,m) 28.0 Water depth(m) h 4.00 Width(m) 2.0 A (m ⁴) 0.025 S(m) height(m) 0.025 S(m) height(m) 5.0 K(m) 0.025 S(m) 6.0 K(m) | Water kvel 5.55 h(top,m) 44.0 Total water depth(m) 5.35 h(top,m) 28.0 Water depth(m) 4.00 h 4.00 Width(m) 44.00 2.0 A(m') 217.2 0.025 S(m) 0.025 S(m) 45.89 height(m) 0.0 R(m) 4.624 Q(m'/s) 421.4 h(one side) 5.0 Water depth 1.55 i gradieni 2.0 Width(m) 8.1 0.002 A(m'/s) 421.4 | Water level 5.55 h(np,m) 44.0 Total water depth(m) \$35 h(np,m) 28.0 Water depth(m) 4.00 h 4.00 Water depth(m) 4.00 h 4.00 Water depth(m) 4.00 2.0 A(m ²) 212.2 0.025 S(m) 45.89 height(m) 0.0 R(m) 4.624 V(m/s) q(m ² /s) 421.4 h(one side) 5.0 igradient 2.0 Water depth 1.55 g(m ² /s) 41.7 1.55 S(m) |

Q=290m3's(100-year) CENGKARENG FLOODWAY (Angke river - upper end)

| | 1 | 1. | | | | <ckr-1&3></ckr-1&3> |
|------------|-----------------|-------|-----------------------|-------|----------|---------------------|
| | | | Gradient | /2380 | | |
| | t | | Water level | 4,50 | | Q(q+2qh,m*/s) |
| Low Water | Width(top.m) | | Tetal water depth(rn) | 4 50 | | 292 9 |
| Channel | Width(bottom,m) | 25.0 | Water depth(m) | 4.00 | | Free board(m) |
| | Depta | 4 00 | Width(m) | 41 0 | | 1.0 |
| - FL 197 | 1 | 20 | A(n*) | 152 5 | | Crown with(m) |
| | л : | 0 025 | S(m) | 42 89 | | 5.0 |
| | Bed height(m) | | R(m) | | V(m's) | 19 |
| | | | c(m/s) | 2013 | | |
| High Water | Width(one side) | 50 | Water depth | 0.50 | 5(m) | 6 |
| Channel | Slope gradient | 20 | Width(m) | | R(m) | 0.445 |
| | n | 0.040 | A(m') | | (e\'mydp | 0.8 |
| | | 1 | V(m 3) | 0 10 | 2ah(m7s) | 1.7 |
| | | | | | | |

Table 4.8 DIMENSION OF STANDARD CROSS SECTIONS (3/5)

| MOOXERV | AARTCANAL | | | | Q=125m3 | s(22-)ear) |
|--|----------------------|-------|-------------------------|-----------|---------------------|----------------|
| | {Cengkareng Floe | dw Iy | · Boundary of DKI and I | Fangerang | 2 | |
| | /* 1 11178 11.1 } | | Gradient | \$72260 | | |
| | | | Water level | 100 | treated line drawns | Q(q+?qh,m?s) |
| Low Water | Wichh(top,m) | 300 | Total water depth(m) | 4 00 | | 121.4 |
| Channe1 | Width(bottom,m) | 14.0 | Water depth(m) | 4.00 | | Free board(m) |
| | Öeçin 👘 | 4.00 | Width(m) | 30.0 | | 0.6 |
| | 1 | 20 | Ā(m') | 88 0 | | Crown width(m) |
| | ¢. | 0 030 | S(m) | 31 89 | | 5 (|
| de la composición de | Bed height(m) | 0.0 | R(m) | 2 760 | V(m's) | 1 38 |
| 1.1.1 | | | գ((m'/s) | 121.4 | | |
| High Water | Width(one side) | 00 | Water depth | 0 00 | S(m) | 00 |
| Channel | Skipe gradient | 20 | Width(m) | 00 | R(m) | 0.000 |
| | a | 0 050 | A(m ²) | | gh(m/s) | 00 |
| 1 - C | 1 | | Y(m's) | 0.00 | 201(m /s) | 0.0 |

| ANGKE RIVER (Co | oul with Ce | ngkare | ng Floodwa; | y - Polor weir) | 2 | Q-160m3/s(|
|-----------------|-------------|--------|-------------|-----------------|---|------------|
| | | | | | | |

| | | | | | | << KR-3&4> |
|------------|-----------------|-------|--------------------------------|--------|-----------|----------------|
| | | | Gradient | 1/2000 | | <pre>.</pre> |
| | | | Water level | 4.30 | | Q(q+2qh,m /s) |
| Low Water | Width(top.m) | 265 | Total water depth(ni) | 4 30 | | 161 |
| | Width(bottom,m) | 160 | Water depth(m) | 3.50 | ÷. | Free board(m) |
| | Depth | 350 | Width(m) | 26 S | | 01 |
| | 1 | 15 | A(m ²) | 95.6 | | Crown width(m) |
| | n | 0.030 | S(m) | 28.62 | | 50 |
| | Bed height(m) | 00 | Ř(m) | 3 340 | V(m/s) | 3.61 |
| · · · · · | | 1 | q l (m [*] /s) | 159 2 | | |
| Righ Water | Width(one side) | 3.0 | Water depth | 0 80 | S(m) | |
| Channel | Slope gradient | 15 | Wicth(m) | . 4.2 | R(m) | 0.64 |
| | n | 0 050 | A(m') | 29 | q (m /s) | 1 (|
| | | 1 | V(m's) | 0.33 | 20h(m³/s) | 113 |

| PESANGOR | AHAN RIVER | | | | Q=290m3 | s(100-year) |
|------------|---------------------------------------|--------|-----------------------|----------|-----------|---------------------|
| | (Conf with Ceng | kareng | Floodway - Toll Jakar | a-Merak) | | <ckr+1&3></ckr+1&3> |
| | | | Gradient | 1/1250 | | |
| | · · · · · · · · · · · · · · · · · · · | | Water level | 5 25 | | Q(q+2qh,m7s) |
| Low Water | With(top,m) | 26.4 | Fotal water depth(m) | 5 25 | | 292 3 |
| Charmel | Width(bottom,m) | 150 | Water depth(m) | 3.80 | | Free board(m) |
| | Depth | 3 80 | Witth(m) | 26 4 | | 0.8 |
| | 1 | 15 | A(m ²) | 116.9 | | Crown width(m) |
| | n | 0 030 | S(m) | 28.70 | | \$.0 |
| | Bed height(m) | 00 | R(m) | 4 074 | V(m/s) | 24 |
| 5 | | | q(m'/s) | 281 3 | 1.5 | <u>.</u> |
| High Water | Width(one side) | 50 | Water de pih | 1.45 | \$(m) | 1.6 |
| Channel : | Skipe gradient | 15 | Wath(m) | | R(m) | 1 155 |
| | a | 0.650 | A(m²) | . 88 | qn(m/s) | 5 5 |
| | | | V (m/s) | 0.62 | 2q6(m'/s) | 110 |

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Table 4.8 DIMENSION OF STANDARD CROSS SECTIONS (4/5)

| | | | | | | <\BC-3> |
|------------|-----------------|-------|----------------------|--------|-----------|---------------|
| | | | Gradient | 1/3000 | | |
| | | | Water kvel | 5 B() | | Q(3F 2of m'A) |
| Low Water | Width(top,m) | 45.0 | Total water depth(m) | 5.80 | | 485. |
| Channel | Width(bottom,m) | 24.0 | Water depth(m) | 4.00 | | Free board(m) |
| | Depth | 4 00 | Width(m) | 45 0 | | 1 |
| | 1 | 3.0 | A(m') | 230 4 | | Crewn widih(m |
| · · | a · | 0 025 | S(m) | 49 30 | | 5 |
| 1. A. | Bed height(m) | 00 | R(m) | 4.674 | V (n/s) | 20 |
| | | | q(m'/s) | 470 3 | | |
| High Water | Width(one side) | 5.0 | Water depth | 1 80 | S(a) | 10 |
| Chansel | Slope gradient | 30 | Width(m) | 10.4 | R(m) | 1 29 |
| | n | 0 040 | A(n1) | | oh(m³/s) | 7 |
| 14.77 | | | V(m/s) | 0 54 | 2qh(m'/s) | 13 |

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| | | · · · | | | | <wbc-3></wbc-3> |
|----------------|-----------------|-------|----------------------|--------|------------------------|-----------------|
| | | | Gradient | 1/3000 | 1.1 | |
| | | | Water kyel | 5.80 | | Q(q+2qh,m'/s) |
| Low Water | Width(top,m) | 42.0 | Total water depth(m) | 5 80 | | 452 |
| Channel | Width(bottom,m) | 26 0 | Water depth(m) | 4 00 | | Free board(m |
| 4 ¹ | Depth | 4 00 | Width(m) | 42 0 | | |
| . E. | T | 20 | A(m') | 2116 | | Crown width(r |
| | n | 0.025 | S(m) | 43.89 | | |
| | Bed height(m) | 00 | R(m) | 4.821 | V(m/s) | 2 |
| | | | q(m'/s) | 441.0 | | |
| High Water | Width(one side) | 4.0 | Water depth | 1 80 | S(m) : | 8 |
| Channel | Skipe gradient | . 20 | Width(m) | 7.6 | R(m) | |
| | G. | 0.640 | A(m') | | qh(m'/s) | 1 1 |
| 1.1.1.1 | | | ((m/s) | 0 \$4 | 2qh(m ³ /s) | 11 |

Q=340in3/s(100-year) WESTERN BANJIR CANAL (Karet weir - Manggarai weir) · -Gradient 1/3000
 Gradient

 Water Evel

 34 0 Fotal water depth(m)

 18 0 Water depth(m)

 4 00 Width(m)

 2 0 A(m²)

 0 0 0 Vidth(m)

 0 0 Vidth(m)
 3.60 Q(al+2ah,m7s) Width(top.m) Width(bottom.m) 5 80 4 00 34 0 165 2 Low Water 345 Free board(m) Channel Depth 1 Crown with(m 35 89 4.603 V (m/s) 333 8 50 Bed height(m) 1 80 S(m) 7.6 R(m) 10 4 gh(m²/s) 0 54 2qb(m²/s) Width(one side) High Water 8.0 1 301 Slope gradient Channel

5.3 11.4

Table 4.8 DIMENSION OF STANDARD CROSS SECTIONS (5/5)

| CBL FLOO | DWAY (Estuary - | Beka | siriver) | | Q=780m3 | s(50-year) |
|------------|---------------------------------------|-------|-----------------------|--------|------------------------------|---------------|
| | 5 | | | | Q=780m3/s(50-year) CBL-1> | |
| | 5 | | Gradient | | | |
| | 1 | | Water level | 5 Z(| | Q(q+2qh m 7s) |
| Low Water | Width(top,m) | 1120 | Total water depth(m) | 5 20 | | 782 6 |
| Channel | Width(bottom,m) | 110 0 | Water depth(m) | 3.00 | | Free board(m) |
| | Depth | 100 | Width(m) | 1220 | | 1.0 |
| | 1 | 20 | A(m ²) | 616.4 | | Crown with(m) |
| | a . | 0 030 | S(m) | 123.42 | | 50 |
| | Bed height(m) | 00 | Ř(m) | 4 994 | V(m/s) | 1 26 |
| | · · · · · · · · · · · · · · · · · · · | | ql(m ¹ /s) | 775.0 | | |
| High Water | Width(one side) | 3.0 | Water depth | 2 20 | S(m) | 7.9 |
| Channel | Slope gradient | 20 | Width(m) | 7,4 | R(m) | 1.445 |
| 4.11.11 | 9 | 0.050 | A(m ²) | 11.4 | ch(m /s) | 3.8 |
| | | [| V(m/s) | | 2q3(m1/s) | 75 |
| | 1 | • | | | | |

| CBLHOO | DWAY (Bekasir | NCF - C | jamoe) | | <u><u><u>v</u>-330.0.0</u></u> | 's(50-year) ≪CBL-1> |
|-------------|-----------------|---------|----------------------|--------|--------------------------------|------------------------|
| | | | Gradient | 172000 | | |
| | | · | Water level | 5 20 | | (Qat+20h m 7s) |
| Low Water | Width(top,m) | 320 | Total water depth(m) | 5 20 | | |
| Channel | Width(tottom,m) | 20 0 | Water depth(m) | 3.00 | | Free board(m) |
| | Depth | 3.00 | Width(m) | 32 0 | | 08 |
| | 1 | 20 | A(m') | 48.4 | ; | Crown withh(m) |
| | n | 0.030 | \$(m) | 33.42 | | 50 |
| 1. 1. T. T. | Bed height(m) | 00 | R(m) | 4.441 | V(m/s) | 2 01 |
| 1.12 | | I | q(m/s) | 298.6 | | |
| High Water | Width(one side) | 5.0 | Water depth | 2 20 | S(m) | 13.9 |
| Channel | Slope gradient | 20 | Wich(an) | 13.4 | R(m) | 1.770 |
| | n | 0 050 | A(m ²) | 24.6 | q h(m³/s) | 16 |
| | | | V(m/s) | 0.65 | 20h(m'/s) | 32 3 |

| CBL FLOO | DWAY (Cijambe | Cost | fang) | Q=300m3/s(50-year) | | | |
|--------------------------------------|---|----------|----------------------|--------------------|-----------|---------------|--|
| | | | | | CBLP | | |
| | • · · · · · · · · · · · · · · · · · · · | (| Gradient | 7/2000 | | | |
| بغضت سيست | | · · · · | Water level | 5.20 | | (Xa#2ah m 75) | |
| low Water | With(top.m) | 260 | Total water depth(m) | 5 20 | | 301 | |
| Channel | Width bottom m) | 140 | Water depth(m) | 3.00 | | Free board(m) | |
| $\left\ x_{i}^{N} \right\ _{L^{2}}$ | Depth | 3 00 | Width(m) | 26 0 | (| 0 | |
| | I. | 20 | A(m ²) | 117 2 | | Crown with(m | |
| | n | 0.039 | S(m) | 27.42 | | | |
| · · · · · | Bed height(m) | 00 | R(m) | 4 275 | V(m/s) | 19 | |
| | · | | q(m /s) | 230.1 | | | |
| High Water | With(one side) | 21.0 | Water de pih | 2 20 | S(m) | 25 | |
| Channel | Slope gradient | 20 | Wishta(m) | 25.4 | R(m) | 1.90 | |
| | Π. | 0 050 | A(m ²) | 51.0 | oh(m/s) | 35 | |
| | · · · · · · · · · · · · · · · · · · · | <u> </u> | V (m 's) | 0.70 | 2qh(m'/s) | 71 | |

| BÉKÁSI RI | VER (Conf with | CBL - | Bekasi wes) | | Q=590m3/ | s(SO-year) |
|---|-----------------|-------|----------------------|--------|-----------|-----------------|
| | | | 1 | | | C8L-1> |
| | | 1 | Gradient | | | |
| • ···• | · | | Waler level | | | Q(all-Zah,m /s) |
| ow Water | Width(top.m) | 410 | Total water depth(m) | 600 | | 593 3 |
| | Width(bottom m) | 280 | Water ocpih(m) | 4.00 | | Free board(m) |
| | Depth | 4 00 | Width(m) | 44.0 | | 10 |
| | 1 | 20 | A(m ²) | 232 0 | | Crown with(m) |
| | n | 0 030 | S(m) | 45.89 | | 5.0 |
| | Bed height(m) | 00 | R(m) | \$ 056 | V(m's) | 2 43 |
| | | - | q(m /s) | 574.9 | | |
| High Water | Wall (one side) | 5.0 | Water depth | 2 00 | S(m) | 9.5 |
| Channel | Skice gradient | 20 | Wikht(m) | 9.0 | R(m) | 1 478 |
| | a | 0.050 | A(m ²) | 14.0 | qh(m/a) | 9.2 |
| | · | | V(m/s) | 0.65 | 201(m /s) | 18 5 |
| 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - | 1 · | | | | | |

| | | with CBL | | |
|--|--|----------|--|--|
| | | | | |

| ÷., | | | |
|-----|-------|------------|------|
| | | | |
| | (1-)) | Qm3 s(25-y | rari |
| ÷. | × | | |
| | | | |
| | | - C 01 | |

| | | !!! | | | | Y 100-12 |
|--------------|-----------------|----------|----------------------|-------|-----------|----------------|
| | | 1.1.1 | Gradient | 1/930 | | |
| - | | | Water level | 130 | | Q(q1+2qh,m/h) |
| Low Water | Width(top.m) | 26.0 | Total water depth(m) | 3 50 | | 130.5 |
| Channel | Width(bottom m) | 120 | Water depth(m) | 3 50 | | Free board(m) |
| 1 | Depth | 3 50 | Width(m) | 26.0 | | 0.6 |
| · · · . |] | 20 | Ā(m') | 56 5 | i | Crown width(m) |
| 1.1.1 | n | 0 030 | S(m) | 27 65 | | 5.0 |
| 1 I I | Bed height(m) | 00 | R(m) | 2 405 | V(m's) | 1 % |
| | | | q (m %) | 130.5 | | |
| Ish Water | Width(one side) | 00 | Water depth | 0.00 | S(m) | 0.0 |
| Channel | Skipe gradient | 20 | Width(m) | | R(m) | 0.000 |
| | л | 0 050 | A(m') | | qh(m /s) | 00 |
| <i>t</i> | | † | V(m's) | 0.00 | 201(m'7s) | 00 |



Table 4.9 OVERALL EVALUATION OF MASTER PLAN

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| | - | | | | | | | |
|---|---------------------|------------------------|-------------------|------------------------|---|------------------------|---|--|
| | | £.1 | | 4 | 2 | 6 | | × |
| Kuver System | Cidunan | Cunanceuri | Cuwab | Congcareng Floodway | Western Barnjir Canal + Cisudane | Eastern Banju Canal | CbL Floodway | Non-structural Measures |
| Outline of Plan | Kiver Improvement | Kiver improvement | River improvenent | prie 10 | River Improvement and I Ciliwung Doodway | ent and | kuver Improvement | Flood forecasturg and warning system, |
| (Immovement Length) | 3Clon | 1000 | 1 2 Jon | | | s?tam | Solem | |
| Implementation Program (vear) | 2014-2023 | 2022-2025 | 2013-2016 | 2013-2025 | 1102-3002/3002-2661 | 2005-2017 | 2014-2019 | flood rek map, |
| Eeneficial Population | | | | | | | | • |
| m 2025 (1000 nos) | 495 | 805 | 144 | 2505 | 1 ×65 | 4,119 | s, 1,607 | institutions, |
| The second se | | 076 | | 021 | 012 | 210 | 025 | Lood fighting system. |
| Land Use In 2025 | | Agriculture | Agneulture | Area | Gov. nd. & Comm. | Kes. & Industrial | Agn. & Residential | mithic education |
| point | | | | | | | | home-home-home-home- |
| Return Period of Design | 7 | <u>بر</u> | ĩ | 100 | 100 and 40 | 100 | 50 | |
| Financial Project Cost | | | | | | | | school education. |
| (Rp. billion) | [] | XO | Fi | X X X X | | 104. | 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 | etc. |
| hunod | | | | - | | | | |
| Financial Land/House Cost (Rp. billion) | £ | <u>65</u> | (a | šči | 305 | 643 | ž | |
| point 10 | 010 | 10 | 10 | × | × | e | 16 | |
| ERR (%) | 3.8 | | 121 | 14.6 K | 16.1 | 20.6 6 | 6. | • |
| "echnical Evaluation | Ordinary | Ordinary | - Ordunary- | Complicated | Complicated | Ordmary- | Ordunary | |
| hunod | | 5 | | | | 4 | c 4 | |
| Social Beneficial Impact points | 11am2 | धावगाः 1 | struell | bug. | very bug | | muddle 3 | |
| Envronmental Impact | not affect | might affect | not effect | not attect 2 | not attect 2 | not affect 2 | mucht affect 0 | |
| Protect Nature | F/S not available | F/S. not available | F/S not available | D/D: partly available | D/D: party available | Partly implemented | F/S: not available | |
| Overnell Pount | 20 | 20 | 26 | 34 | 40 | 31 | | |
| Priority Projects for F/S | | | - | | Ø | | | |
| | Evaluation Criteria | | | | | | | |
| | Land Use | Financial Protect Cost | Cand & house cost | EDRR | Reneficial Population | Technical Evaluation | Technical Evaluation Social Peneficial Impact | Environmental Impact |
| • | 1: Agriculture | 0-1,500-X | °. | 0: X< 5 | 1: X<500 | 1: Complicated | 1: small | 0: might affect |

*1) 25. Inplainentation Program, Ger. : Goverrmental Office Area, Commercial Area, Ind.: Industrial Area, Agn.: Agn: Agneutonal Area, Landitouse Cost: Land acquisition/house compensation cost 1; X.4500 3; 500-4742 000 5; 1000-4445 000 7: 3000-4445 000 6:12<X ----4: 600-X-000 6: 400-X-600 8: 200-X-400 10 X<00 3: X<500 7 Resid & Industrial 9: Gov.,Ind.& Comm.

2: not affect

3: medium 1: small

1: Complicated 2: Ordinary 7: very bug

S: lug

4:10<X<12

2:5<X<10 0: Y< 5

0: 1,000-3X

1.1,000<X<1,500 2: 500<%<1,000

3: Agn. & readential

5. Residential

*2) The project costs here are all those estimated on the master plan level.

Table 4.10 CONCEPT OF DESIGN DISCHARGE DISTRIBUTION AT MANGGARAI

NEW MASTER PLAN (by JICA Study Team)

| | | | · | ****** | un | it : m3/s |
|------------------------------|----------------|-----|-------|--------|-------------------------------|-----------|
| Return Period (year) | <mark>.</mark> | | · · · | - | . ¹ - . | 100 |
| Ciliwung River | Q<360 | 370 | 380 | 390 | 400 | 410 |
| Western Banjir Canal | Q<360 | 360 | 360 | 360 | 360 | 360 |
| Ciliwung-Gunung Sahari Drain | 0 | 10 | 20 | 30 | 40 | 50 |
| PRESENT MASTER PLAN (6 | y NEDECO) | | | | uni | t : m3/s |
| Return Period (year) | 2 | 5 | 10 | 25 | 50 | 100 |
| Ciliwung River | 100 | 170 | 218 | 280 | 325 | 370 |
| Western Banjir Canal | 100 | 170 | 180 | 205 | 250 | 295 |
| Ciliwung-Gunung Sahari Drain | 0 | 0 | 38 | 75 | 75 | 75 |

3

Source :

Explanatory note on the design of the rehabilitation works for the Ciliwung Drain and Gunung Sahari Drain (Nov. 1975, NEDECO)

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ALTERNATIVE SCHEMES FOR OPTIMUM SCALE OF PROJECTS Table 5.1

| | | • | | | |
|---|--|---|----------------------------------|--|----------------------------------|
| | | Alt. I | Alt. 2 | Alt 2' | Alt. 3 |
| | | WBC: 100-year, | WBC: 100-year, | | WBC: 50-year, |
| | Design Scale | Cisadane: 50-year | Cisadane: 25-year | Cisadane: 25-vear | Cisadane: 10-vear |
| | Floodway tunnel (unit | 2 | 1 | 2 | |
| | Financial Project Cost | 191 - 191 - 191 - 191 - 191 - 191 - 191 - 191 - 191 - 191 - 191 - 191 - 191 - 191 - 191 - 191 - 191 - 191 - 191 | 672 | 714 | 595 |
| | (Rp. billion) | 1 | 2 | 2 | 3 |
| | ERR | 16.1% | 18.0% | 16.4% | 17.8% |
| | | 1 | 3 | 2 | 3 |
| | Technical Evaluation | Technical Evaluation (1) Investigation of ground | (1) Investigation of ground | (1) Investigation of ground | (1) Investigation of ground |
| | | water once, (2) no restriction | water twice, (2) restriction to | water once, (2) no restriction | water once, (2) no restriction |
| | · · | to existing tunnel and channel, | existing tunnel and channel, | to existing tunnel and channel, | to existing tunnel and channel, |
| | · · · | (3) access casy by existing | (3) access difficult after | (3) access carsy by existing | (3) access easy by existing |
| | | road, (4) inlet weir | sel, (4) | | road, (4) inlet weir |
| - | | construction once, (5) | inlet weir reconstruction | construction once, (5) | construction once, (5) |
| | | temporary works once | needed, (5) temporary works | | temporary works once |
| | | 3 | | | |
| | Environmental Impact (1) T | (1) Temporary land use once, | (1) Temporary land use twice, | (1) Temporary land use once, | (1) Temporary land use twice, |
| | | (2) affect to ground water | (2) affect to ground water | (2) affect to ground water | (2) affect to ground water |
| | | once, (3) river water | twice, (3) river water | once, (3) nver water | twice, (3) nver water |
| | | disturbance once, (4) possible | disturbance twice, (4) possible | disturbance once, (4) possible disturbance twice, (4) possible | disturbance twice, (4) possible |
| | | impact to historical assets once impact to historical assets | | | impact to historical assets |
| • | and the second | | | 3 | |
| | Social Impact | (1) Land acquisition once, (2) | (1) Land acquisition later more | (1) Land acquisition later more (1) Land acquisition once, (2) (1) Land acquisition later more | (1) Land acquisition later more |
| | | transportation of heavy | difficult, (2) transportation of | transportation of heavy | difficult, (2) transportation of |
| ÷ | | equipment once, (3) affect to | heavy equipment twice, (3) | equipment once, (3) affect to | heavy equipment twice, (3) |
| • | | groundwater once, (4) noise, | affect to groundwater twice, | groundwater once, (4) noise, | affect to groundwater twice, |
| ÷ | • | vibration, resettlement once, | (4) noise, vibration, | wbration, resettlement once, | (4) noise, vibration, |
| | | (5) benefit big | resettlement twice, (5) benefit | (5) benefit middle | resettlement twice, (5) benefit |
| | | | middle | | middle |
| | | | | | |
| • | Overall Score | 11 | 8 | 13 | 6 |
| | | | | Optimum | |
| | | | | | |

Note: Estimated financial project cost is on the Master Plan level.

Design Criteria for Dykes and Floodwalls

| ττρέ | CRITERIA |
|---|---|
| Design flood | The dyke height should be selected to convey the discharge of the Design Flood Standard without over-topping. |
| | Sideslope erosion protection should accompdate the 50 year flood without damage. |
| Right-of-Vay and Land Use | In accordance with existing law the government acquires and has control over all lands to a distance of 5 metres beyond the outside toe of dykes. |
| | Permanent residential or industrial type structures should not be allowed within the regulatory floodplain. |
| | Righ crops (e.g. banana plantations) and crops which leave soil exposed to potential erosion (e.g. vegetable crops) should not be permitted. |
| | Certain types of agriculture are allowable within the regulatory floodplain. Livestock pasture or low height crops which provide erosion protection for underlying soils are recommended. |
| | Land-use within the regularotry floodplain should have a negligible impact on flood water levels. |
| Construction Haterials and Geotechnical | Utilize locally available construction materials including silts, sands and clays where workable. Dykes built of silts and sands should be capped with a 0.3 metre thickness of clay for protection against rapid failure in the event of overtopping. |
| | Dykes should be compacted to a minimum 90 percent of Standard Procter Density, or greater depending on specific site requirements. |
| Cross Section Details | Winimum Top of Dyke Width $0_3500 \text{ m}^3/\text{s}$ use 3 metres $500 \text{ m}^3/\text{s}$ $40 \le 2000 \text{ m}^3/\text{s}$ use 4 metres $1 \ge 2000 \text{ m}^3/\text{s}$ use 5 metres Greater width may be required for local traffic, inspection vehicles or maintenance equipment |
| ۰۰ بر ۱ ۱ | <pre>Hinimum Dyke/Floodwall Freeboard Q<200 m³/s use 0.5 metres 200 m³/s (q<500 m³/s use 0.8 metres 500 m³/s (q< 2000 m³/s use 1.0 metres Q ≥ 2000 m³/s use 1.2 metres In all cases freeboard should be greater than wave setup and runup resulting from the 1:10 year wind event.</pre> |
| | Ninimum Dyke Sideslopes should be 1:2 (vertical to horizontal). Flatter slopes or berms may be required based on the results of stability calculations. |
| | Dyke slopes should be protected against erosion by vegetation, planting of shrubs or use of armor (e.g. rock riprap) depending on site and soil conditions. |
| Special Considerations | Additional safeguards should be provided where dykes and floodwalls are located in critical areas where the risk to life or property in the event of dyke failure is high (see Figure 4.2), or where dykes are of significant height (e.g. > 3.5 metres). These safeguards should include: |
| • | • an additional 0.3 metres freeboard along such such critical reaches |
| ÷., | armouring of the inside sideslopes where dykes are built from relatively erosive materials (e.g. silts and sands) |
| | • an impervious core and downstream filter where dyke embankment or foundation seepage is a concern |
| and a second second Second second | • minimum embankment compaction of 95 percent of Standard Procter Density. |

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source : Flood Control Manual (CIDA, 1993)

Table5.2DESIGN CRITERIA IN INDONESIA (2/2)

Design Criteria for Bridges and River Crossings

| TYPE | CRITERIA |
|-------------------|--|
| Design Floods | At least equal to project flood standard. Any backwater effect during the design flood should not exceed 0.3 m. Higher standards for specific sites may be required by the Departemen Perhubungan or Bina Harga. |
| Freeboard | Bina Marga requires minimum freeboard of 1.5 m above bankfull flood. |
| | Department of Public Works "Guideline for Bridge & Highway Loading" requires at least 1.0 metre freeboard between the 50 year flood level and bottom of bridge girder. |
| | Bina Marga requires that for navigable waterways freeboard should be at least 12 metres above the 50 year flood level. The top of road crossing should be at least 0.5 metres above top of dyke/floodwall level. |
| River Engineering | Bridge crossing location and design layout should be selected to suit the river engineering and geomorphological characteristics of the stream. |
| Bridge Spans | Total bridge span should not be less then the natural width of the river channel and should be designed to safely pass the design flood. |
| Bridge Piers | Bridge piers should be located and spaced to insure passage of debris during the flood. |
| | Bridge piers should be designed to accommodate potential scour and channel degradation. |
| | Sand mining should be prohibited in the vicinity of bridge piers. |

Design Criteria for Weirs

| Түре | CRITERIA |
|------------------------|---|
| Design Floods | At least equal to project Design Flood Standard. |
| | Ministry of Public Works Standard SNI 03-2415-1991 requires that weirs be designed for a flood return period between 50 and 100 years. |
| 4 <u>-</u> | Weics which are located upstream of major population densities should be designed such that catastrophic consequences do not occur in the event of overtopping or operator error. |
| River Engineering | Structure should be able to safely pass the design floods without interception of sediment and debris loads. |
| | River works should be designed to withstand river bed scour and degradation during design flood event and lateral erosion during project life. |
| foundation & Abutments | The foundation and abutments must be stable and should not undergo excessive deformation under any loading condition. |
| | Seepage through the foundation and abutments must be controlled to prevent uplift, piping, instability, sloughing, erosion, etc. |
| freedoard | Top of structure and wingwalls should be at least 0.5 metres higher than adjacent dykes. |

source : Flood Control Manual (CIDA, 1993)

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| · · · · | | | | | • | : | | | : | | | | - | | | | | • . | | | | | | | | | | | | | | | | | | | | | | - | | | |
|-------------------------|-----------------------------------|-------|---------|-------|---------|--------|--------|----------------|-------------|-----------------------|--------------|------------|-------|--------|-----------|------|-------|-----------------|------------|------------------------|----------|-------|--------|-------------------|---|---------------------|-------|------------------|--|-------|-----------|-------|----------------|---------------------------------------|-------|-------|---|---|-------|-------|---|-----|-------|
| | · · | | - | | | | | | | • | | | | : | | • | | • | | | ; | • | : | | | | | • | | | • | | | | | | • | • | | • | | | |
| | ыке ц 11G) | 1.85 | 1.94 | 661 | 2.08 | 2.16 | ม | 5.5 | 64 E 7 | 2.61 | 2.68 | 2.78 | 2.86 | ч 8 | 3.07 | 1 | 335 | 3.40 | 3,45 | | 3.67 | 3.71 | 3.79 | 3.84 | 100 | 4,10 | 4.17 | 2 | 4,35 4,4 | 451 | 4.62 | 4.69 | 4.78 | 20 A | 5.09 | \$.17 | l | | | | | | |
| Design Li vi - | - 11C) (I | 0.85 | 80 | 0.99 | 1.08 | \$1.1¢ | 2 | 1.39 | <u> </u> | 3 | 1.68 | 1.78 | .1.86 | 8 | 2.07 | 2.27 | 125 | 2.40 | 2.45 | | 8 6 7 | 2.7 | 2.79 | 1 | 8 | 3.10 | 3.17 | 5 2 2 1 | | 151 | 3,62 | 3.69 | 87.7 | 200 E | 8.8 | 4.17 | | | | ÷ | | | |
| | | 4 75 | \$ 1 | 4 ¢] | () 1 | ¥ 1 | 1 1 | ក្ | 1 | 5 8 1 7 | 3.92 | -3.82 | 3.74 | 3 | 5 F | | 1 2 | -3.20 | 51.5 | 8 5 | 7.93 | -2.89 | 18 7 | 2.4 | 87. | 2.5 | 2.43 | -2.33 | | 8 | -1 98 | 16 1- | 1 83 | 191 | 151- | -1.43 | | • | | : | | . (| 10000 |
| | | | | | • | | | | | cartenie | | | | | • | | | | • | Andre . | - VIRVE | | | | | . 5 | | • | | | | | : | · · · · · · · · · · · · · · · · · · · | | 1 | | 2 | | | | | |
| Bottom of Bridge Girder | Name | | | • | ÷ | : . | | Mandara Permai | | Tol Aimort Censkarens | | • | | | | ; | | Teluk Gong Raya | • | Panashat Tubadus Anake | | | • | | 1 · · · · · · · · · · · · · · · · · · · | Prof. Dr. Latumeten | | 1 | Pailway (Funite) | | Kyai Tapa | | : | Tomane | 9.000 | | | | - | • | • | | • |
| Bottom of | Bridge (russ (m. TTG) (m. TTG) | | | | | · . | | 1.64 | | 3 53 | | · . | • | • | • | . · | | 2.63 | | 57 | 8 | | | | | 2,14 | | | 1.47 | | 2.51 | | | 9.05 | | | | : | | | • | | |
| Existing Parapet | ~ | | | | | | | | | | | · . · · | | | 1.1 | • | | | | | 3.80 | 3.75 | | | | | | | | Ì | 4.30 4.60 | | | | | | | | | • | • | | 6 |
| Exi | | | | | | | | | _ | | | | | | | | | | | | | | | | | | | | • | : | | | | | | • • • | | | | | | | |
| Existing Dike | kught (m, TTG) | | | : | | 1.40 | | | | | 96'0 96'0 | | | | | | | | | | | 3.25 | 3.29 | 8.4 | 8 × × | 4,19 | (F.(| ក្នុ | 4.90 10 10 10 10 10 10 10 10 10 10 10 10 10 | 3 | 4.17 | 4.10 | 4.77 4.04 | 16.4 | 5.16 | 4.68 | | | | | | | |
| Existin | ил. 170) | | 2.90 | 5.9 | 2.90 | 2.8 | 5.90 | 81 | 272 272 | 3 F | 8 | 1,45 | 2.00 | 3.81 | 185 19 | 105 | 3.21 | 3.24 | 55 | 3 5 | | 4.01 | 3.37 | 3.30 | (# C | 426 | 3,87 | 61.4 10 | 4.4 | 3.85 | 3,78 | 3.86 | 4.39 6.03 | 434 | 4.36 | 4.84 | | | | | | | |
| puno | KIRTIC) | 28.0 | 0.79 | 0.71 | 0.63 | 16'0 - | 0,87 | 621 | (9°) | | 0,63 | 0.37 | เร | 1,70 | 1.02 | 0.21 | 121 | 0.70 | <u>ل</u> ت | | 5 | 1.01 | 1,29 | - 86° | | 5 | 111 | 1.70 | (R. 1 | 1.17 | 2.03 | 5 | <u>8</u> 8 | 12 | 3.52 | 1872 | | | | | | ÷ | |
| Existing Ground | Lett (m. TTG) (n | 0.9% | 8 | 6,0 | . E. O | 0.80 | 0,41 | 67 I | 9 1 2 | 800 | 26.0 | 0.49 | 0.37 | 2.01 | 6 2 | 0.50 | 3 | 0.84 | ន្ម | 2 2 2 2 2 | 215 | 2.68 | 3.43 | 22 | 9.5 6 | 1.85 | 3.68 | 80 | 8 9 9 9 | 59 | 2.53 | 1.28 | 8 | 5 | 151 | 3.05 | | | | | | | |
| Existing | KUVET LAG | -237 | -3.37 | -5.27 | 4 21 | 4.54 | 4 X | 5.16 | 10 Y | 46 | 10.5 | 8 | 4.65 | 8 | 51 F | 2 2 | 22 | -3.67 | 50 C | 88 | 3 57 | 22.5 | 3.64 | ក្ត | 28 | 18.5 | -2.19 | | 2.02 | -5.37 | 0.70 | 8 | 1.81 | 9 | 8.7 | 4.55 | | | | | • | | |
| mulative E | Ustance Ku (km) (n | 0000 | 0.120 | 0.510 | 0.815 | 1,105 | 1.455 | 1,935 | 2.295 | | 2,975 | 3,265 | 3.485 | 3.783 | 4.088 | 4678 | 4,853 | 4.998 | 5.133 | 5 F F C | 5.750 | 5.860 | 6,100 | រៀ | 5053 | 6.975 | 7,150 | 7,445 | 7.875 | 8.115 | 8.420 | 2.62 | 8.878 9.172 | 9.436 | 9,746 | 9,961 | | | | • | : | | |
| Distance Accumulative | 510 (mg) | 000 0 | 071.0 | 0:190 | 205.0 | 06770 | 0.350 | 0.480 | 0.360 | 0.150 | 1250 | 0.290 | 0.220 | 0.298 | 0.305 | 282 | 0.215 | 2.145 | 0.135 | 0.220 | 0110 | 0.110 | 240 | រ រ | | 1,280 | 113 | S I | 202.0 | 0.240 | 305 | 0.205 | 0.755 | 0.258 | 1310 | 0.215 | | | | 5 | | | SAL S |
| E | <u>ب</u> | 1. | | 0.5 | | | 1 | 6 | 22 | | 12 | | | | | | | | 5 | 44 | . 1 | 5,8 | 6.1. 0 | 0 4 6 4 9 4 | | Ś | | : | 10 | • | ÷ | | 5 C C | | | 10.0 | | | | | | | |

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PROPOSED LONGITUDINAL PROFILE OF WBC (2/2) Table 5.3

| | | | | | | | | | | | | | | | | : | | • | | | : | | | | | | : | | , | | | | | į | , | | | • | - | | | | |
|------------------------------|-------------|----------------------------|---|--------|--------|--------|--------|--------|----------|----------------|-----------|------------|---------------|--------|--------------|--------|--------------|--------|--------|--------------|--------|-------------------|--------|--------|-----------|------------|--------|------------|----------|--------|---------|----------------------|----------|------------------|--------------|----------|--------|--------|--------|-------------------|--------|--------|--------|
| : | Dike | n, TTG) | | 5.30 | 5.39 | 5.43 | 5,48 | 2,2 | 5.59 | 293 2 | 12.9 | 5/.C | 82 | 1.5 | 3.5 | | 200 | 9 9 9 | A1.9 | | 170 | | 2 i | 6.42 | \$. \$ | 6.71 | 6.88 | 6 <u>7</u> | <u>1</u> | 9.72 | 41.7 | - 1 | | 20 20 | 08.2 | 197 | 8.07 | 8.15 | 8.18 | 8.19 | | | |
| Design | HWL | ттс) (i | • | 4.30 | 4.39 | 4.43 | 4,48 | X. | 4.59 | 4 6 | 1.4 | | | 1 | 3 2 | 3 | | 3 5 | 2 | | | | 2 | 5.42 | 5 | 5.71 | 5.88 | 0.0 1 | 6.25 | 6.36 | × 5 | 0.0 8 | | 10.1 | | 7.37 | 7.47 | 7.55 | 7.58 | 7.59 | | | |
| G | River Bed H | (m. TTG) (m. TTG) (m. TTG) | • | -1 30 | -1.21 | -1.17 | 1.12 | 8 | 10,1- | 0.95 | 68) Q | 4 I 9 I | 2.0 | 8 5 | 3 | | | | | | | 11 S | 010 | 0.02 | 0.10 | 0.31 | 0.48 | 0.00 | 0.85 | 80 | 1.14 | - 00 - 10 - 10 | <u>.</u> | 1.62 | 1.80 | .0 | 2.07 | 2.15 | 2,18 | 617 | | | |
| Bottom of Bridge Girder | | Name | - | | | | | • | | Aipda KS Tubun | · · · | | | | | V D | Auct Darrage | | | | | K.H. Mas. Mansyur | | | | MH Thamrin | | - | | | Halumun | | | 8,17 Latuharhari | • • • • | - | | | | Manggarai Barrage | | | |
| Bottom of | | (m. TTG) (m. TTG) | | | | | | | | 8.13 | | | | • | • | č | 0710 | | | | | 227 | | : | • | 9.4 | | | | | 7,16 | | | 11.20 8.11 | • | | | | | | | | |
| | Bridge | (n 11 | | | | | | | | | • | • • | | | | | | • | | | | | | · . | | • | | | | : | | | - | | | | | : | | | | | |
| Existing Paranet | Kıght | (m, TTG) (m, TTG) | | | 0 | • | | | | 0 | • | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | ÷ | |
| P.vistru | Ę | (m, TTG | | 5.20 | 5.2 | 8.5 | 5.00 | 5.3 | <u>s</u> | 52 | 5 | 5.10 | 7 | 9. | 5.0 | | | | | | | | | | | | | | | | | | | | | | | | | | | | · |
| Dite: | Kight | п, 176) | | 5.49 | 5,97 | 6.04 | 4.63 | 5.0 | 5.00 | 4,40 | 5.84 | 5.14 | <u>8</u> | F. 1 | 6.21 | | | 8.11 | 8 | 8 | 5 2 | | 7.38 | 6.89 | 7.10 | 7.18 | 112 | 7.47 | 10.7 | 8.26 | | | | • . | 8.26 | | | | | | | | |
| Friendo Dike | Left | (m. TTG) (m. TTG) | | 4.78 | 4.51 | 4.62 | 4.95 | 4,91 | 4,90 | | 5.34 | 4.91 | 5.08 | 5.30 | 4.22 | | | 8.20 | | | 8.18 | | 1.57 | 8,46 | | | 6.70 | | | 7.85 | | | | | | | | | | | | | |
| , here | Kight | ر ۲۲ () | | 3.31 | 3.33 | 3.89 | 3.20 | 2.73 | 2.90 | 3,95 | 5.37 | 4.39 | 8,5 | 4.75 | 4 .13 | 6.60 | 6.71 | 6,16 | 23 | 5.15 | ų. | 7,98 | 5,95 | 5.4 | ŝ | 5.25 | 4.74 | 5.37 | 7.57 | × 8 | 9.70 | 12.51 | 11.57 | 11.62 | 9 | 6. 8 | 11.06 | 10,11 | 9.03 | 8.73 | 6.1 | 9 45 | 81.6 |
| Evisting Cround | Left | (m, TTG) (m, TTG) | | 3,29 | 3.68 | 1.52 | 44.0 | 3.34 | 3.56 | 5.16 | 4.7.1 | 431 | 3.71 | -8°.4 | 2 2 | 6.39 | 6.6¢ | 7.02 | 1.92 | 7.93 | 7.18 | 7.73 | 5.49 | 7,82 | 32.7 | 7.35 | 4,67 | 7.41. | 6,60 | 7.40 | 9.15 | 10,40 | 11.89 | 11,06 | 9.21 | 5,73 | 9.75 | 10.58 | 8.39 | 8.73 | 8.85 | 12.25 | 10.08 |
| Turkes. | River Bed | (m. 170) | | -1.48 | 1 | 78°C | 1.89 | -0.54 | -0:78 | -0.8 | -0.50 | -0.74 | - 0.49 | 2 2 | ମ୍ ବ : | -6,76 | -1.39 | وی | 0.59 | 0.50 | 1.38 | -135 | -0.53 | 0.68 | 0.68 | ŝ | 1.45 | 1.62 | 0. 11 | 0.89 | 5. | 99. | 155 | 3 | 4 272 | <u>8</u> | 55 | 0.02 | 1,0% | 1.48 | 1.36 | 1.90 | 50 |
| Disease Associations Evideon | Distance | (ms) | | 126,01 | 10.561 | 10.696 | 10.816 | 10.001 | 11.131 | 11.289 | 11,459 | 11.679 | 11.949 | 12.124 | 12.294 | 12.416 | 12,431 | 12,451 | 12.561 | 12:661 | 12.871 | 13.071 | 13.251 | 13.441 | 13,661 | 13.903 | 14,168 | 14.436 | 14.761 | 14,946 | 15.226 | 15.481 | 15.721 | 100'91 | 16.276 | 16.551 - | 16.721 | 16,841 | 16.886 | 16.901 | 16.911 | 16.93; | 16.963 |
| | - animatin | (wy | | 0360 | 0.240 | 0,135 | 0,120 | 0.175 | 0,140 | 0.158 | 0.170 | 0.220 | 0.270 | 0.175 | 0.170 | ដ | 0,015 | 0.020 | 0.110 | 0.100 | 0,210 | 0,200 | 0.180 | 0.190 | 0.220 | 0.242 | 0.265 | 0.268 | 0.325 | 0.185 | 0.280 | <u>67</u> 8 | 0140 | 0.280 | 0.275 | 0.275 | 0:120 | 0.120 | 0.045 | \$10.0 | 0.010 | 0.022 | 0.050 |
| | | ••• | | 10.3 | 10.6 | 10.7 | 10.8 | 11.0 | 11.1 | 511 | 11.5 | 11.7 | 11 S | 121 | <u>1</u> | 12.4 | 12,41 | 12.42 | | Kuukut River | 12.9 | 13.1 | 13.2 | 13.4 | 13.7 | 6.61 | 14.2 | 14,4 | 14.8 | 14.9 | . 15.2 | 15.4 | . 15.7 | | | 16.6 | 16.8 | 16.91 | 16,91 | 26.91 | 16.95 | 16.91 | 17.0 |
| . * | | | • | • | | | ÷ | | | • | | | | | | : | i | | • | | | | | - | j. | | | | • | | | | | | : | | | | | | | | |

Table 5.4 DESIGN CRITERIA FOR CROSS SECTIONS OF WBC

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Estuary - Angke Drain

| Project Name | Design Discharge (m3/s) | Crown Width (m) | Free- board (m) | Slope Gradient I | Roughness Coefficient W. C. H. W. C. |
|--|-----------------------------------|-----------------------|-------------------------|------------------------|--|
| New Master Plan (JICA) | 500 | | 4 1.0 |) 1.2.0 | 0.025 0.040 |
| Flood Control Manual (1993) Master Plan by NEDECO West Jakarta Flood Control Project | Q>500 *525 400 | | 4 1.0 4 1.5 4 1.0 | 5 1:2.0 | 0.030 0.030 |

*; This value includes the discharge of the Upper Angke river

Angke Drain - Krukut River

| Project Name | • | Crown Widtb (m) | Free- board (m) | Slope Gradient | | hness ficient 11. W. C. |
|---------------------------------------|-------|-----------------------|-----------------------|-------------------|---------|-------------------------------|
| New Master Plan (JICA) | 470 | 3 | 1.0 | 1:1.5 | 0.025 | 0.040 |
| Flood Control Manual (1993) | Q<500 | . 3 | 0.8 | 1:2.0 | - | - |
| Master Plan by NEDECO *1 | 370 | - | - | • | : · · - | · · · · · • |
| West Jakarta Flood Control Project *2 | 370 | 3 | 1.0 | 1:2.0 | 0.030 | 0.030 |

*1; proposed extention was alternated by the Cengkareng Floodway

*2 ; raising of levee up to Teluk Gong Syphon

Krukut River - Manggarai Barrage

| Project Name | Design Discharge (m3/s) | Crown Width (m) | Free- board (m) | Slope Gradient | Roughness Coefficient L. W. C. H. W. C. |
|--|-------------------------------|---|-----------------------|----------------------|---|
| New Master Plan (JICA) | 360 | | 3 1 | .0 1:1.5 | 5 0.025 0.040 |
| Flood Control Manual (1993) Master Plan by NEDECO | Q<500 290 | 1. A. | 3 0 4 1 | .8 1:2.0 .5 1:1.5 | |
| West Jakarta Flood Control Project | - | | • | • | |

Table 5.5 PROPOSED STANDARD CROSS SECTION OF WBC

0.0 k (Estuary) - 2.9 k (Angke Drain)

3

100-year, 500 m3/s

| | | | Gradient | 1/3600 | | |
|------------|--|-------|----------------------|--------|------------------------|-----------------------------|
| | and a subscription of the second distribution of | | Water level | 5.60 | | Q(q1+2qh,m ³ /s) |
| Low Water | Width(top,m) | 53.0 | Total water depth(m) | 5.60 | | 501.1 |
| Channel | Width(bottom,m) | -36.2 | Water depth(m) | 4.20 | | Free board(m) |
| 1 | Depth | 4.20 | Width(m) | 53.0 | | 1.0 |
| | Slope gradient | - 2.0 | $\Lambda(m^2)$ | 261.5 | | Crown width(m) |
| | n | 0.025 | S(m) | 54.98 | | 4.0 |
| 1. | Bed height(m) | 0.0 | R(m) | 4 756 | V(m's) | 1.89 |
| | | | ql(m³/s) | 493.1 | | |
| High Water | Width(one side) | 5.0 | Water depth | 1.40 | S(m) | 8.1 |
| Channel | Slope gradient | 2.0 | Width(m) | 7.8 | R(m) | 1.102 |
| | n | 0.040 | $\Lambda(m^2)$ | 9.0 | qh(m³/s) | 4.0 |
| 1.1 | · · · · · · · · · · · · · · · · · · · | | V(m/s) | 0.44 | 2qb(m ¹ /s) | 8.0 |

2.9 k (Angke Drain) - 12.7 k (Krukut River)

100-year, 470m3/s

| | 1997 - A. | | Gradient | 1/2800 | | |
|---|-----------------|-------|-----------------------|--------|-----------|-----------------------------|
| a and the state of the second | | | Water level | 5.60 | | Q(ql+2qh,m ¹ /s) |
| Low Water | Width(top,m) | 44.0 | Total water depth(m) | 5.60 | ÷ | 173.6 |
| Channel | Width(bottom,m) | 31.4 | Water depth(m) | 4.20 | | Free board(m) |
| | Depth | 4.20 | Width(m) | 44.0 | | . 1.0 |
| | Slope gradient | 1.5 | A(m ²) | 219.9 | | Crown width(m) |
| | n | 0.025 | | 46.54 | 1.1.1.1 | 3.0 |
| | Bed height(m) | 0.0 | R(m) | 4.725 | V(ni/s) | 2 13 |
| | | | ol(m ³ /s) | 468.2 | | |
| High Water | Width(one side) | 3.0 | Water depth | 1.40 | S(m) | 5.5 |
| Channel | Slope gradient | 1.5 | Width(m) | 5,1 | R(m) | 1.026 |
| | a | 0.040 | A(m ²) | 5.7 | qh(m³/s) | 2.7 |
| | | † | V(m/s) | 0.48 | 2qh(m'/s) | 5.5 |

12.7 & (Krukut River) - 15.2 & (Halimun Bridge)

100-year, 360m3/s

| | · · · · | | Gradient | 1/1600 | | |
|--|-----------------|-------|----------------------|--------|---------------|-----------------------------|
| and an | | | Water level | 5.40 | | Q(q1+200,m ¹ /s) |
| Low Water | Width(tep,m) | 31.0 | Total water depth(m) | 5.40 | | 374.1 |
| Channel | Width(bottom,m) | 18.4 | Water depth(m) | 4.20 | | Free board(m) |
| | Depth | 4.20 | Width(m) | 31.0 | | 1.0 |
| | Slope gradient | 1.5 | $\Lambda(m^2)$ | 140.9 | | Crown width(m) |
| • | ก | 0.025 | S(m) | 33.54 | | 3.0 |
| | Bed height(m) | 0.0 | R(m) | 4.202 | V(m/s) | 2.60 |
| | | | ql(m³/s) | 367.0 | | |
| High Water | Width(one side) | 4.0 | Water depth | 1.20 | S(n1) | 62 |
| Channel | Slope gradient | 1.5 | Width(m) | 5.8 | R(m) | 0.954 |
| | n | 0.040 | $\Lambda(m^2)$ | 5.9 | qh(m³/s) | 3.6 |
| | | | V(m/s) | 0.61 | 2qn(m'/s) | 7.1 |

15.2 k (Halimun Bridge) - 16.9 k (Manggaral Barrage)

100-year, 360m3/s

| | 1997 - 1 1 | | | Gradient | 1/1600 | | |
|-----|---------------|------------------|-----------------|--|---|------------------------|-----------------------------|
| - 1 | | | Γ | Water level | 5.40 | | Q(ql+2qh,m ³ /s) |
| | Low Water | Width(top,m) | 36.0 | Total water depth(m) | 5.40 | | 369.2 |
| | Channel | Width(botton),m) | 19.8 | Water depth(m) | 5,40 | | Free board(m) |
| | | Depth | 5.40 | Width(m) | 36.0 | | 0.6 |
| | | Slope gradient | 1.5 | A(m ²) | 150.7 | | Crown width(m) |
| | 1. | <u>ส</u> | 0.025 | the second s | 39.27 | | 3.0 |
| | | Bed height(m) | .0.0 | R(m) | 3.837 | V(m/s) | 2.45 |
| - | | | | gl(m'/s) | 369.2 | | |
| | Righ Water | Width(one side) | A second second | Water depth | 0.00 | S(m) | 0.0 |
| • • | Channel | Slope gradient | 1.5 | Width(m) | 0.0 | R(m) | 6.000 |
| | | n <u>'</u> | 0.040 | $\Lambda(m^2)$ | 0.0 | gh(m'/s) | 0.0 |
| | | ····· | | V(m/s) | and the second se | 2qb(m ³ /s) | 0.0 |

Table 5.6 PROPOSED LONGITUDINAL PROFILE OF CISADANE RIVER

| Šec No | | | Accumulation Distance | R | liver Bed | Left | g Groand Right | Left | g Dike Right | Observed Water Level in Dry Season (m. TTO) | Bottom of Bridge Girder | River Bed | | Dike (m. LEG) |
|--------------|-------------------|-------------------------|--------------------------|------|-------------------------|--------------------------|-------------------|----------------------|-----------------------|--|--|---|----------------------|----------------------|
| | 00 | (km) 0.000 0.400 | (km) 0 0 | 00 | m, TFG) | (m, 11G) 0 67 0 74 | | (m, 111G) | (m, TIG) | (m, TTG) 0 40 0 42 | (m, TÍG) | (m, 1TG) | {m, TTG} | (m, TIG) |
| | - 0 9 1 4 | 0.465 0,545 | 0.8 | 65 . | -4 10 -7 22 | 1 23 | 1.70 | | | 0 10 0 50 | | | | |
| • | 18 | 0.417 0.400 | 18 | ż7 | -4 48 | 2 00 | 1 87 | | | 0 50 0 50 | 1 | 493 480 | 4 04 | 4 71 5 04 |
| | 29 35 39 | 0.650 | 2 8 3 4 3 8 | \$7 | -3 97 -5 50 -4 39 | 1.67 2.15 1.78 | 311 | 4 94 | 3 30 4 10 | 0 20 0 30 0 60 | | -4 60 -4 41 -4 28 | 4 58 5 09 5 22 | 5 58 6 09 6 22 |
| | 43 | 0357 | 4 Z 4 6 | 56 | -5 59 | 2 12 | 4 05 | 4 37 | 4 70 | 0.00 | | -417 | 5 33 | 6 33 6 45 |
| | 53 59 | 0 598 0 605 | 5 2 5 8 | 51 - | -5 50 -3 84 | 3 26 3 41 | 2 92 | 3.62 4.42 | 4 71 | 0.40 0.42 | | -3 86 -3 67 | 5 64 5 83 | 6 64 6 \$3 |
| | 64 68 | 0 505 0 415 | 63 | 76 | -5 87 -4 34 | 4 65 3 70 | 3 20 | 5 64 6 77 | 6 50 6 53 | 0.41 €.40 | 7 (0) | -3 51 -3 38 | 5 99 6 12 | 6 99 7 12 |
| | 71 | 0 350 | 71 | 66 . | -8 10 -3 51 | 3 70 | 3 53 | 6 50 | 5 10 5 94 | 0.60 0.50 | | -3 27 -3 10 | 6 23 6 40 | 7 23 |
| | 82 88 92 | 0 498 0 650 0 364 | 81 88 91 | 14 | -3 53 -5 95 -3 45 | 4 96 4 89 5 32 | 4 2 2 | 6 65 7 20 7 70 | 5 45 7 60 7 90 | 0 50 0 50 0 80 | 1 | -2 95 -2 75 -2 63 | 6 55 6 75 6 87 | 7 55 7 75 7 87 |
| . • | 99 103- | 0 726 0 423 | 99 103 | 64 | -3 61 -3 33 | 5.69 5.65 | 4 27 | 5 70 8 20 | 6 05 7.95 | 0.40 | , , , , , , | 241 | 710 | 8 10 8 23 |
| | 108 113 | 0 510 0 492 | 10 B 11 3 | 37 | -5 C4 -6 16 | 4.13 | 5 89 | 8 30 | 8 99 7 80 | 0 80 0 90 | | -2 11 -1 96 | 739 754 | 8 39 8 54 |
| | 118 | 0 475 0 505 | 1)8 | 09 . | -7 42 -5 74 | 5.57 6.33 | 5 68 | 8 60 7.82 | 9.30 6.96 | 0.90 0.90 | en de La el Catrie | -181 -165 | 785 | 8 85 9 19 |
| | 127 131 135 | 0 440 | 127 | 09 | -1 51 -3 51 -1.08 | 8 14 8 34 8 19 | 9 2 3 | 8 84 9 60 9 57 | 9.07 | 1 00 | | -1 52 | 8 48 8 73 | 9 48 9 73 9 95 |
| | 13.9 14.4 | 0 438 | 138 | 97 | -1 37 -2 20 | 9 20 | 8 3 1 | 10 23 | 9 90 9 96 11 55 | 080 170 170 | | -1 04 -0 75 -0 41 | | 10 25 |
| | 4 B 15 I | 0.446 - 0.255 | 14 B | 38 . | -0 09 -2 20 | 9 08 8 37 | 8 05 | 9.75 10.35 | 9 25 10 30 | 2 70 2 90 | | 011 | 989 1006 | 10 89 |
| | 15 6 16 2 | 0 520 0 561 | 15 6 16 1 | 74 | -2 90 -1 45 | 7 82 9 55 | 9.45 | 10 51 10 62 | 11 10 11 49 | 2 90 2 90 | | 0 41 0 78 | 10 78 | 1141 1178 |
| | 16.8 | 0.668 | 168 | 12 | -0 74 | 10 79 | 13 75 | 11 08 11 64 | 12 49 14 70 | 3.00 4.49 | | 123 | 11.23 | 12.23 |
| | 180 185 191 | 0 610 0 465 0 582 | 18 C 18 4 19 C | 87 | 2 05 -0 77 1 36 | 11 59 11 52 12 30 | 11 89 | 11 87 | 12 50 12 95 | 5.10 5.20 5.30 | : : : | | | |
| | 19.5 30-1 | 0 435 0 570 | 195 | 04 | -013 362 | 12 46 | 11 44 | | 12 04 | 6.90 7.70 | | 1.1 | | |
| | 20-7 21-3 | 0 662 0 550 | 207 | 86 | 5 59 5 92 | 14.49 17 30 | 16 34 | | | 7.40 8.30 | | | | |
| | 2132 2135 | 0.030 | 213 | 46 | 7 30 | 17 39 | 16 13 | - | ÷., | 13 20 13 20 | | e de la composición d En el composición de la composición de l | | |
| | 215 218 223 | 0 200 0 255 0 329 | 21 5 | | 797 949 806 | 15 11 15 93 15 31 | | · . | | 13 20 13 20 13 50 | | | | |
| - , - | | | | | | | | | | | | | | |
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| | - | | | | | | 1.1.1 | | | | | | | |
| | | | | | - | | | | | | | | | |

PROPOSED STANDARD CROSS SECTION OF CISADANE RIVER Table 5.7

Optimum Scale Project (25-year, 1500m3/s)

1.8 k - 12.7 k

| | | Gradient | 1/3200 | | |
|-----------------|--|---|---|--|---|
| | | Water level | 9.50 | | Q(q1+2qh,m'/s) |
| Width(top,m) | 77.0 | Total water depth(m) | 9 50 | | 1501.2 |
| Width(bottom,m) | 47.0 | Water depth(m) | 7.50 | | Free board(m) |
| Depth | 7.50 | Width(m) | 77.0 | | 1.0 |
| 1 | 20 | A(m ²) | 619.0 | | Crown width(m) |
| n | 0.030 | S(m) | 80.54 | | 5.0 |
| Bed height(m) | 0.0 | R(m) | 7.686 | V(n¥s) | 2 29 |
| | | q!(m ¹ /s) | 1420.5 | | |
| Width(one side) | 35.5 | Water depth | 2.00 | S(m) | 40.0 |
| Slope gradient | 2.0 | Width(m) | 39,5 | R(m) | 1.876 |
| n | 0.050 | A(m ¹) | 75.0 | qh(m /s) | 40.3 |
| | 5 | V(m's) | 0.54 | 2qh(m'/s) | 80.7 |
| | Width(Cottom,m) Depth 1 n Bed height(m) Width(one side) | Width(top,m) 77.0 Width(tettom,m) 47.0 Depth 7.50 1 2.0 n 0.030 Bcd height(m) 0.0 Width(one side) 35.5 Slope gradient 2.0 | Water level Width(top,m) 77.0 Total water depth(m) Width(bettom,m) 47.0 Depth 7.50 Width(bettom,m) 47.0 Depth 7.50 Width(m) 1 1 2.0 A(m²) n 0.030 S(m) Bed height(m) 0.0 R(m) qt(m²/s) Width(one side) 35.5 Slope gradient 2.0 Notific(m) 0.050 | Water level 9.50 Width(top,m) 77.0 Total water depth(m) 9.50 Width(tottom,m) 47.0 Water depth(m) 7.50 Depth 7.50 Width(m) 77.0 1 2.0 A(m ³) 619.0 n 0.030 S(m) 80.54 Bed height(m) 0.0 R(m) 7.636 qt(m ³ /s) 1420.5 Width(one side) 35.5 Slope gradient 2.0 Width(m) 39.5 n 0.050 A(m ²) 75.0 | Water level 9.50 Width(top,m) 77.0 Total water depth(m) 9.50 Width(top,m) 77.0 Total water depth(m) 7.50 Depth 7.50 Width(m) 77.0 1 2.0 A(m ³) 619.0 n 0.030 S(m) 80.54 Bed height(m) 0.0 R(m) 7.636 V(ni's) 1420.5 Width(one side) 35.5 Width(m) 39.5 R(m) 39.5 Slope gradient 2.0 Width(m) 39.5 n 0.050 A(m ²) 75.0 gh(m ³ /s) |

<u>12.7 k - 16.8 k</u>

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| | | 1 | Gradient | 1/1490 | | |
|--|-----------------|-------|----------------------|--------|------------------------|-----------------------------|
| | | | Water level | 10.00 | | Q(q1+2qh,m ¹ /s) |
| Low Water | Width(top,m) | 63.0 | Total water depth(m) | 10.00 | | 1508.1 |
| Channel | Width(bottom,m) | 31.0 | Water depth(m) | 8.00 | | Free board(m) |
| 1.1 | Depth | 8.00 | Width(m) | 63.0 | | 1.0 |
| | 1 | 2.0 | A(m ²) | 502.0 | | Crown width(m) |
| | 8 | 0.035 | S(m) | 66.78 | | 5.0 |
| an a | Bed height(m) | 0.0 | R(m) | 7.518 | V(m/s) | 2.84 |
| | | 1 | q](m³/s) | 1425.9 | 11 | 1. A 1. |
| High Water | Width(one side) | 24.5 | Water depth | 2.00 | S(m) | : 29.0 |
| Channel | Slope gradient | . 2.0 | Width(m) | 28.5 | R(m) | 1.829 |
| | n | 0.050 | A(m²) | 53.0 | oh(m /s) | 41.1 |
| 1.1. ¹ . | [| 1 | V(m's) | 0.77 | 2qb(m ⁷ /s) | 82.1 |

Master Plan (50-year, 1900m3/s)

1.8 k - 12.7 k

| | | | Gradient | 1/3200 | | : |
|---|-----------------|---------|-----------------------|--------|------------------------|--|
| 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - | | | Water level | 9.50 | | Q(qt+2qh,m ³ /s) |
| Low Water | Width(top.m) | 91.0 | Total water depth(m) | 9.50 | · | 1901.6 |
| Channe! | WiJth(bottom,m) | 64.0 | Water depth(m) | 7.50 | | Free board(m) |
| | Depth | 7.50 | Width(m) | 94.0 | | 1.0 |
| | 1 | 2.0 | $A(m^2)$ | 780.5 | · | Crown width(m) |
| | π | 0.030 | | 97.54 | | 5,0 |
| | Bed height(m) | 0.0 | R(m) | 8.002 | V(m's) | 2.30 |
| | · | | ql(m ³ /s) | 1839.9 | | 1 |
| High Water | Width(one side) | 27.0 | Water depth | 2.00 | S(m) | , 31.5 |
| Channel | Slope gradient | 2.0 | Width(m) | 31.0 | R(m) | 1.84 |
| | n | 0.050 | $A(m^2)$ | 58.0 | oh(m'/s) | 30.1 |
| | | | V(m/s) | 0.53 | 20h(m ³ /s) | 61.6 |
| <u>12.7 k - 20.1</u> | <u>k</u> | <u></u> | . | | | a an |

| | | с. | Gradient | 1/1490 | | · · · · · · · · · · · · · · · · · · · |
|------------|-----------------|---------|-----------------------|--------|-----------------------|---------------------------------------|
| | | r | Water level | 10.00 | | Q(ql+2qh,m ² /s) |
| Low Water | Width(top,m) | 76.0 | Total water depth(m) | 10.00 | | 1919.9 |
| Channel | Width(bottom m) | 44.0 | Water depth(m) | 8.00 | 3 | Free board(m) |
| | Derah | 8,00 | Width(m) | 76.0 | | 1.0 |
| | 1 | 2.0 | A(m ²) | 632.0 | | Crown width(m) |
| 1 | n | 1 | S(m) | 79.78 | - | 5.0 |
| | Bed height(m) | 0.0 | 8(0) | 7.922 | V(m/s) | 2.94 |
| | | 1 · · · | ql(m ³ /s) | 1859.0 | | |
| High Water | Width(one side) | 18.0 | Water depth | 2.00 | S(m) : | 22.5 |
| Channel | Slope gradient | 2.0 | Width(m) | 22.0 | R(m) | 1.780 |
| | l | 0.050 | A(m ²) | 40.0 | qh(m ³ /s) | 30.4 |
| | | | V(m's) | 0.76 | 2gh(m3/s) | 60.9 |