# APPENDICES FOR CHAPTER 9

# APPENDIX 9.1-1

# RESULTS OF CULVERT CAPACITY ANALYSIS

# PROXIDE OF A

ERRICA PROMEO BERRETA ORIGINARIA

## NOTES FOR THE TABLE

AREA - Discharge Area No.

No. - Culvert No. - Culvert Location
Pipe - Pipe size (designed)
Box - Box size (designed)

LT ELEV. - Left side invert elevation

FLOW - Flow direction

RT ELEV. - Right side invert elevation

LENGTH - Culvert length

SLOPE - Culvert slope gradient
V - Water flow velocity

Q - Discharge capacity of each culvertRD & SLOPE - Discharge from roadway and slopes

TD - Total discharge from catchment area and roadway/slopes

AD - Total discharge capacity of culverts in the catchment area REMARKS - Add'l; Additional new culvert.

When the existing culvert needs to be replaced with bigger size culvert, existing culvert size is shown in the remarks.

Designed size is shown in "PIPE" or "BOX".

NOTE - Where no (or blank) TD, catchment area cannot be identified from 1/50,000 map or culverts are located in the same catchment area of a bridge.

REA	NO.	STATION	PIPE	80X	LT ELEV.	FLOW	RT ELEV.	LENGTH (m)	SLOPE (%)	V (m/s)	Q (m³/s)	RD & SLOPE (m3/s)	TD (m³/s)	AD (m½)	REMARK
		1113+420.00	0.61		1.32	-	1.50	12.00	-1.500	5.81	18.819	(11/0/3)			<del> </del> -
i	1	1113+574.40		1.80X1.80	-0.30	<b>◄</b> ····	0.26	18.05	-3.102	8.35	27.063	200			
		1113+602.30		2.40 X 2.40	0.45	- <b></b>	2.08	19.14	-8.517	16.77	96.573	0.159		11.1	
	3	1113+805.50	0.91		9.97	<b>-18</b> √	11 56	23.61	-6.736	6.448	4.192	0.100			,
	4	1113+903.40	0.61		16.50	≪1	18 77	21.62	-10.497	6.165	1.801	1 7	i		'
	_	1114+123.85	0.91		26 57	<b>≪</b> - · · ·	27.46	21.34	-4.170	5.074	3.298	0.111	ļ	i	
ļ		1114+507.84	0.91		47.28	<b>4</b>	48.71	24.82	-5.761	5.963	3.876		}		: .
ļ		1114+892 20	0.61		54.92	<b>◄</b>	56.04	21.10	-5.308	4.384	1.281				· '
ļ		1115+218.30	0.91		39.58	<┫ - ~-	40 59	23.82	-3.820	4,856	3.157	11 1			4
ļ		1115+737.50	2-0.91		23.93	<b>4</b>	24.78	30.67	-2.771	4.136	5.377	0.295		1.33	4.54
ļ	11	1115+741 50	0.91		22 72	- <b>4</b>	24.38	30.70	-5.408	5.777	3.756	0.390		{	l · ·
- 1	12	1116+005.95	0.91		25.36	<b>-4</b>	27.22	26.45	-7.031	6,588	4.283	7		420	
	13	1116+142.25	0.91	0004000	24.44	~■	25.49	21.22	-4.947	5.526	3.592			14.5	
1	14	1116+315.70		3.00 X 3.00	12.34		12.98	17.50	-3.657	12.75	114.738	0.246			
1	15	1116+451.28	0.91		7.71	<b>-≪I</b> — —	8.95	28.42	-4.363	5.190	3.374	0.205			
	16	1116+668.80	0.61		2.66		4.32	23.68	-6.165	4.725	1.380	0.345			
	17	1116+736.05	0.61		3.21		4.22	18.54	-5.447	4.441	1.297				
	18	1116+893.90	0.91		2.24		3.02	21.72	-3.591	4.708	3.061	0.218	i i	1	l
	20	1117+008.15	0.61		2.51	⋖4	3.17	23.72	-2.783	3.174	0.927				1.1
1	21	1117+114.30 1117+161.25	0.61 0.61	—— <u>—</u>	2.40	<b>⋖</b> 1	2.99	21.83	-2.703	3.129	0.914	0.098	{	i	l
	22	1117+195.65	0.61	·	2.17	<b>41</b> ·····	3.07	20.86	-4.315	3.953	1,155				l
	23	1117+359.25	2-0.91		1.97	<b>4</b>	3.05	20.01	-5.396	4.421	1.291	0.213			
	25	1117+359.25	0.61	·····	2.30 1.38	◀	2.75	20.71	-2.173	3.663	4.762		,		l
ŀ	26	1117+532 20	0.91		0.58		2.35	15.58	-6.228	4.749	1.387	0.069			l
. }	27	1117+560	0.61			<b>4</b>	0.82	21.32	-1.126	2.636	1.714	0.063			
- 1	28	1117+696.55	0.61		0.65 2.22	-4	3.41	18.50	-4.108	3.857	1.127	* * * * *			l
1	29	1117+697.35	2-0.91		2.10	<b>4</b>	2.91	24.41	-2.826	3.199	0.934	0.075		ł	
	31	1117+829.40	0.91		1.46	< <b>4</b>	2.70	24.75	-2.424	3.868	5,029	0.058			l
	32	1117+979.67	0.61		0.56	₩	1.71 0.96	21.78	-1.148	2.662	1.730	0.053	!	ĺ	l
	33	1118+023.35	0.61		0.37		0.54	20.82 18.18	-1.921 -0.935	2.637	0.770	0.147			l
	34	1118+278.00	0.61		1.29	₩	1.99			1.840	0.538				l
	35	1118+443.90	0.91		1.00		1.75	31.43 24.67	-2 227 -3 041	2.840	0.829	A440			1.0
	36	1118+731.70	0.61		2.36	₩	3.02	19.73	-3.346	4.332	2.816	0.112			l
	37	1118+810,45	0.61		2.07	4	2.49	23.28	-1.804	3.481 2.556	1.017 0.747	0.304 0.088			l
	38	1118+912.36	0.61		1.10	4	2.15	22.22	4.725	4.136		0.068		i	
	39	1118 993 90	0.61		1.20	4	1.31	20.55	-0.535	1.392	1.208 0.407				l
		1119+120 66	0.91		0.53	4	-1.31	20.55	-0.555	0.000	0.000			ŀ	
	41	1119+156.90	0.61		0.69	<b>4</b>	0.85	22 58	-0.708	1,602	0.468				<b>l</b> .
	42	1119+245.80	0.91		0.96	-4	0.99	20.17	0.149	0.958	0.623				l
	43	1119+345.55	2-0.91		0.40	4	1.75	22.23	6.073	6.122	7.960				l
	45	1119+553.30	0.91		1.15	4	1.22	21.16	0.331	1,429	0.929			l	l
	46	1119+657.90	0.91			-43	2.30	21.10	-0.331	0.000	0.000				l
	47	1119+762.50		2.90 X 2.10	0.05	4	0.48	15.94	-2.698	12.32	75.054				[
	48	1119+794.30	0.91		1.82	<b>▼</b>	1.84	19.93	-0.100	0.787	0.512			·	
	49	1119+806.50	0.91			⋖4	1.87			0.000	0.000				COVER
	50	1119+819.25	0.91			-4	2.18			0.000	0.000				COVER
	51	1119+878 85	0.91		1.88	<b>4</b>	2.29	21.50	-1.907	3.431	2 230				0012,0
	52	119+917.60	0.91		2.20	-4	2.26	20.12	-0.298	1.357	0.882				
	53	1120+191.80	0.91		2.09		2.37	18.19	-1.539	3.082	2.004				i
	54	1120+296.00	0.91		1.76		2.09	21.92	-1.505	3.048	1.982				
į		1120+391.00	0.91		1.00	4	1.15	23.36	-0.642	1 99 1	1.294				
	56	1120+392 00	0.61		1.48		1.66	23.65	-0.761	1 660	0.485				
		1120+447.05			1.86	4	2.15	20.88	-1.390	2 930	1.904				ļ
		1120+531.90	0.91		1.85	4	2 23	20.79	-1.828	3,359	2.184				
		1120+588.60	0.91		1.75	***	2.19	20.79	-2.117	3 615	2 350				
		1120+628.00	0.91		1.81	-4	1,99	22 21	0.810	2 237	1.454				
	61	1120+722.90	0.91		1.93		2 36	20.97	-2.051	3.558	2.313				· .
		1120+846.50	0.91		2.14	4	2 22	21.97	-0.364	1.499	0.974				

PK-1					•	1 14	1510	FCU	LYEK	15					
												RD &	70		
AREA	NO.	STATION	PIPE	вох	LT	FLOW	RT	LENGTH		/ V	Q	SLOPE	TO	AD	REMARKS
L				l	ELEV.	<u> </u>	ELEV.	(m)	(%)	(m/s)	(m³/s)	(m3/s)_	(m³/s)	(m³/s)	l : :
	63	1121+364.68	0.91		2.60	- 🌬	2.32	21.82	1.283	2.814	1.829				l
	64	1121+378		3.00 X 2.00	2.29	<b>P</b>	2 28	13.01	0.077	1.67	10.005				<b></b>
1-1	65	1122+507.30 1125+000		2-1.50X1.90	1.18		0.66	20.69	2.514	6.99	39.840		42.00	100	]
1-1	66	1125+134.60		2-1.80x1.80 2-1.80x1.80	7.25 6.20		7.10 6.02	14.00 18.00	1.071	4.70 4.54	30.471 29.437	0.042	43.09	59.9	1-061
~~~	67	1125+251.35	0.91	2-1.0021.00	6.70		6.06	16.00	4.000	4.969	3.230	0.213			1-0.61
j i	68	1125+265.40	0.61	<del> </del> -	7.50		7.32	17.54	1,026	1,927	0.563	0.210			}
1.2	69	1125+570.50	1.22		5.70	>	5.54	16.00	1.000	3.021	3.529	0.352	16.47	27.8	1-0.61
	70	1125+726.20	0.91		6.90		6 26	16.00	4.000	4.969	3.230	0.159		ì	1-0.61
	.71	1125+824.90	1.22		7.20		6.24	16.00	6.000	7.399	8.645	0.176			1-0-61
	72	1125+886.65	1.22		7.50		6.30	20.00	6.000	7.399	8.645	0.245		·	1-0.61
1.3	73	1125+988.60	1.22		7.50	>>-	621	18.00	7.167	8.087	9.448	0.406			1 0 61
1.3	75	1126+162.00 1126+305.13	1.22		8.10 9,40		6.65 8.68	18.00 18.00	8.056 4.000	8.573 6.041	10.017 7.059	0.257 0.172	11.48	26.5	1-0-91
1.4	76	1126+560.80	1.22	12	9.00		7.85	23.00	5.000	6.755	15.784	0.168	14.29	32.3	1-0.61 1-0.61
	77	1126+748.20	1.22	72	7.30		6.20	20.00	5.500	7.084	16.554	0.100	14.23	32.3	1-0.61
	78	1126+817.20	1.22		6.30		5.54	20.00	3,800	5.888	6.880	V.211	<b></b> -		1 0 61
1-5	79	1127+000.55	0.91		7.60		6.81	18.00	4,389	5.205	3,383	0.068	10.81	14.3	1-0-61
	80	1127+117.25	0.91		7.84		7.04	15.00	5,000	5.555	3.611				1-0.61
	81	1127+223.55	0.61		8.49		8.39	14.93	0.667	1.555	0.454		} .		
1-6	82	1127+457.10		2-2.40x2.40	5.30	<b>J</b> e-	5.19	22.00	0.500	4.06	46.799		29.70	46.8	1-1.52
1-7	84	1127+673 20	1.52	x2	7.10	- 10-	6.70	16.00	2.500	5.530	20.060		18.03	27.5	1-0.61
	85	1127+849.30	1.22	<u> </u>	8.70		7.89	18.00	4.500	6.408	7.487		· · · · · · · · · · · · · · · · · · ·		1 0.61
1-8	86	1128+017	1.22		9.10		8.40	16.00	4.375	6.318	7.382		9.71	12.4	1-0.91
1-9	87 88	1128+118.05 1128+268.60	1.22	2-1.50x1.50	8.70		8.36	17.00	2.000	4.272	4.991		l	l	1-0.91
1-10	00	1128+920	1.22	x3	9.20 9.95	<b>&gt;</b>	8.93 8.75	18.00 27.00	1,500 4,444	5.45 6.368	24.529 22.322		13.04	24.5	1-0 91
1-10	89	1129+013.25	0.61	^3	9.57		9.91	15.21	-2.235	2.845	0.831		16.81	22.3	Addi
1-11	90	1129+482.53	0.00	2-1,50x1.50	10.40		9.48	18.00	5.111	9.49	42.726	* .	54.79	43.6	1-0.6x0.6
	91	1129+659.00	-	1.50 X 2.00	8.30		8.12	19.71	0.913	4.25	12.759			1-3.0	1-0.000
1-13	92	1129+884.30		1.00 X 1.00	8.98	<b>&gt;</b>	8.75	21,06	1.092	3.35	3.349		37.14	46.6	<del></del>
. :	93	1130+131.35		2-1.50x1.50	10.23	<b> </b>	9.76	18.00	2.611	6.79	30.538				1-0.61
1-14	94	1130+406.20	1.52	x2	12.00	<b>p</b>	11.60	16.00	2.500	5.530	20.060		12.55	20.1	1-0.61
	95	1130+990.10	1.22		11.20	<b> &gt;</b> -	10.98	22.00	1.000	3.021	3.529	-			1-0.61
1-15	96	1131+426.30	1.22		14.30	<b>&gt;</b>	13.49	18.00	4.500	6.408	7.487	0.111	21.40	30.0	1-0.61
	97	1131+527.05	0.61	* 7.	12.60		11.50	29.38	4.425	4.003	1.169	0.036			
	98	1131+531.70 1131+904.70	1.52		14.30		12.66	20.82	7.878	9.817	17.805				
	99	1131+960	0.61 1.22		11.51 12.80	· · · · <b>&gt;</b>	10.50	24.58	4.110	3.858	1.127	0.513			l
1-16	100	1132+018.85	1.22	<b>]</b>	12.00		11.60	18.00 18.00	5.000	7.799 6.755	9.113 7.892	0.122 0.086	21.95	25.0	Addi
, ,,	101	1132+245.68	122	1.75 X 1.20	13.71	<b>&gt;</b> _	13.61	13.16	0.760	3,69	7.750	0.085	21.95	25.9	1-0.91
	102	1132+372.35		2-1.50x1.50	10.00		9.61	26.00	1.500	5.14	23.146	0.100	<del></del>	<del> </del>	1-0.91
1-17	103	1132+534.70	0.61		13.63		14.01	22.81	-1.666	2.456	0.717		15.04	23.1	\
I İ	104	1132+720.45	0.91	1.5	13.51	- <b>4</b>	13.76	23.05	-1.085	2.587	1.682				
	105	1132+951.60		3-1.50x1.00	15.80	···	15.46	17.00	2.000	5.36	24.117		<del></del>	<del></del>	1-0.61
1-18		1133+038.25		3-1.50x1.00			15.63	17.00	1.000	3.79	17.053		68.37	80.9	2-0.61
		1133+071.20		3-1.50x1.00		<b></b>	15.74	16.00	1.000	3.79	17.053	i			1-0.61
L		1133+178.8		3-1.50x1.25	15.90		15.74	18.00	1.000	4.02	22.629			L	1-0.61
1-19		1133+568.50		2-1,80x1.80	14.30	<b>b</b> >	13.86	20.00	2.200	7.03	45.582		44.74	58.9	1-0.61, 0.91
		1133+722.55 1133+950.60	1.52	x2	14.60		14.42	18.00	1.000	3.498	12.687				1-0.61
1-20		1134+533.44	0.91	<b> </b>	14.22	<b>&gt;</b>	14.18	24.06 39.76	0.168 4.351	1.013	0.658	0.470	052	1/ *	
' 20		1134+712.80	1.22	x2	19.10	. · · • •	18.45	26.00	2.500	5.183 4.776	3,359 11,161	0.179	9.53	14.5	1.0.01
1-21		1134+877.65	1,22	×2	19.10		15.43	28.00	13.107	10.936	25.555		14.48	30.0	1-0.91 1-0.91
		1134+934.40		<b></b>	17.68		15.17	33.62	7.466	6.788	4.413				
		1135+123 20		x2	27.10		26.30	16.00	5.000	5.555	7.223				1-0.61
		11356187.19					2.10	17.30		39.583		ANA	A 24	Sign	DELETE
1-22	120	1135+279.40	0.75		19.16	<b></b>	18.92	37.10	0.647	1.757	0.776	n seeps (東京縣 西海河)。	8.85	22.5	
		1135+402.15	1.22		21.50	<b> </b>	20.82	17.00	4.000	6.041	7.059				1-0.61
		1135+613.60	0.91		23.07	<b>b</b> >	22.98	26.37	0.341	1,451	0.943		1		1-0.75
	123	1135+743.20	0.91		26.10		20.99	31.17	16.394	10.060	6.539			L i	1-0.61
													-		CONTRACTOR OF STREET

PK-1				·											
ADCA		CTATION	OVOE	504	LT	FLOIC	RT	LENGTH	SLOPE	ν	Q	RD &	TD	AD	
AREA	NO.	STATION	PIPE	вох	ELEV.	FLOW	ELEV.	(m)	(%)	(m/s)	(m³/s)	SLOPE (m3/s)	(m²/s)	(m³/s)	REMARKS
	124	1136+348.60	0.61		23.06		21.15	23.36	8.175	5.441	1,589	(III-O)	-	<b></b>	
1-23	125	1136+579.50	0.75		25.41		24.88	23.82	2 225	3.258	1.439		6.79	14.0	
	126	1136+726 00	1.52		22.45		21.67	26.25	2.972	6,030	10.935		}	}	
1.23	127	1137+082 10		3.00 X 3.00	21.52		21.03	18.84	2.600	10.75	96.756	0.188	19.89	97.4	
	128	1137+099.65	0.61		22.37	-	22 12	18.61	1.343	2 206	0.644	0.100	''	''''	
	129	1137+730.10		2-2.40 X 1.80	22.83		22.52	18.34	1.691	6.96	60.166	0.054			
1-23"	130	1137+884.50	0.91		24.37		23.92	20.14	2 234	3.713	2.414	0.00	12.42	64.4	
	131	1137+911.20	0.91		24.18	<b>b</b> -	23.92	19.86	1.309	2.843	1.848			• • • • • • • • • • • • • • • • • • • •	
1-24	132	1139+079.30	0.91	x2	31.80		31.57	15.00	1.533	3.076	4,000		7.39	11.2	2-0.61
	134	1139+581.75	0.91	x2	39.80		38.80	20.00	5.000	5.555	7 223		l		1-0.61
1-25	135	1139+708.10	0.91		38.57	<b>&gt;</b>	37.87	21.00	3.333	4.536	2.949	0.106	12.88	132.7	
	136	1139+859 26	1 1	3.00 X 3.40	36.28		35.63	18.83	3.452	12.72	129.750	0.464	1		IN:2-2.4X3.1
	137	1140+149.40	1.22		49.29		48.37	24.45	3.763	5.860	6.847			f	
1-26	138	1140+246.70	0.91		47.97	<b>b</b> >-	46.87	32.63	3.371	4,562	2 955		10.65	27.9	
,	139	1140+332.30		1.50 X 1.80	47.91		47.38	22.43	2.357	6.70	18.084	0.123			****
	140	1140+570.30	1.22	x2	57.20	· >	56.84	25.00	1.440	3.625	8.471	0.048			1-0.61
	141	1140+679 20	0.61		57.08	· · · · · •	54.76	32.10	7.227	5.116	1.494				
1-27	142	1140+816.40	1.52	x2	56.80	· <b>D</b> o	56.30	27.00	1.852	4.760	17.265		32.12	42.7	1-0.61
	143	1140+856.60	0.91		53.07	<b>B</b>	52.65	27.83	1.509	3.052	1.984	0.513		ì .	
	144	1141+165.80	1.22	x2	61.60		60.65	26.00	3.654	5.774	13.493	,			1-0.91
1-28	145	1141+283.80	1.22	x2	59.70		58.50	20.00	6.000	7.399	17.290		26.22	35.4	1-0.61
	146	3141+454.15	1.52	x2	59.39		58.92	23.00	2.043	5.000	18.136			1.5	1-1.52 Add1
	147	1141+533.05	0.91		59.37		59.10	26 29	1.027	2.518	1.637			* * * * * * * * * * * * * * * * * * * *	7
1-29	148	1142+944.79		1-2.40x1.80	75.20	₩	76.34	31.00	-3.677	10.27	44.366		32.47	53.1	1-0.91
	149	1143+016.90	1.22	x2	74.62	-c# · · · ·	75.10	31.00	-1.548	3.759	8.784	0.040		1 1	1-0.91
11	150	1143+233.50	0.91	x2	76.91	<b></b>	77.30	16.00	-2.438	3.879	5.043	0.095			1-0.61
1-30	151	1143+360.00	0.91	×2	77.70	-c#	77.87	18.00	-0.944	2.414	3.139		32.39	38.2	1-0.61
	152	1143+611.75		2.50X2.50	75.42	<b>¤</b>	75.55	19.62	-0.663	4.61	30.035				17 1
	153	1143+993.75	1.22	x2	74.80	∢ —	75.65	31.00	-2.742	5.002	11.688				1-0.61
	154	1144+104.50	0,91		71.83		72.08	25.96	-0.963	2.438	1.585		4 1		
1-31	155	1144+773.70		1.00X1.00	79.89	<b>◄</b>	80.10	29.42	-0.714	2.71	2.708		54.55	82.0	1.0
	156	1144+898.25		1-2.40x2.40	81.46		82.90	40.30	-3.573	10.86	62.554				2-0.91
	158	1145+203.95	0.91		83.31	~e¶	84.21	19.13	-4.704	5.388	3.503		<u> </u>		
	159 160	1145+419.40	0.91	<b> </b>	87.10	<b></b>	87.30	14.75	-1.356	2.893	1.881	1	7.44		
	161	1145+599.20 1147+425.75	0.61 0.61		86.74		86.82	16.45	-0.466	1.327	0.388				1.1.1
	162	1147+845.87	0.01	1-1.80x1.80	98.30		98.50	28.56	:-0.700	1.592	0.465		13. 1		
	163	1148+019	1.22	x2	103.61		104.30	20.00	-3.450	8.81	28.541				1-0.61
1-32	164	1148+260.60	1.22	x2	94.23	-4	101.16	20.00	-4.300	6 264	14.637				1-0.61
	165	1148+367.80	0.61	<u> </u>	95.60		95.36 98.21	30.00 21.52	-3.767	5.863	13.700		62.57	95.5	1-0.61
	166	1148+437.85	0.01	1-2.40x2.40	94.83		95.05	17.00	-2.835 -1.294	3.204	0.936		415	3.44	
1-33	167	1148+986.65		1-2.40×2.40	76.75	4	77.18	22.00	-1.955	6.54 8.03	37.645				1-0.91
1.34	168	1149+968		1-2.40x1.80	72.61	7	72.89	18.50	-1.514	6.59	46.264		23.43	46.3	1-1.52
1-35	169	1150+372 25		1-2.40x1.80	69.43	7	69.92	25.50	1.922	7.42	28.463 32.071	<u></u>	17.67 20.80	28.5	1-1.52
	170	1150+572.15	0.91	x2	73.40	-21	73.85	16.00	-2.812	4.167	5.417		20.60	32.1	1-1.52
1-36	171	1150+664.55	0.61		73.87	4	74.29	14.59	-2.879	3.229	0.943	100	15.96	19.4	1-0.61
	172	1150+861.50	0.91		71.88	-4	72.09	17.44	-1.204	2.726	1.772		10.50	13.4	
		1150+861.51	0.91		71.88		72.09	17.44	1.204	2.726	1.772			100	
	174	1150+942.50	1.22	x2	73.36		73.63	15.00	-1.800	4.053	9.470		Υ.		1-0.61
		1151+174,30			74.57		75.85		₹-5 2 <b>(</b> \$	1 2 707		443.00	24.40	Y. C. P. C.	W Brode
	176	11511844.25	122		88.01	-	59 40	20.00	1.950	4 218	3700	0 273			3 (4) 6
		1152+593.00			60.38	-4	61.01	20.94	-3.009	4.310	2.802		100 1 TO 10 10 10 10 10 10 10 10 10 10 10 10 10	eges esti	1-0.61
1-40	178	1152+801.80		1-1.80x1.80	54.90		55.25	16.00	2.188	7.01	22.726	1.0	27.33	67.2	1-0.91
	180	1152+885 20	0.91	]	51.42	-4	52.30	23.00	3.826	9.28	30.056	1.19			1-0.51
L	181	1153+274.70		x2	48.60	-	49.15	24.00	2.292	4.573	10,686	5 E			2-0.91
Ι	183	1153+452 60	090		50.35		51.15		3.838	4.738		S 2 2 19		082805	\$ 10.61
	184	1153+690.65	0.61	J.	50.07	-4	50.85	26.40	-2 954	3.271	0.955	0.059	THE RESERVED TO SERVED TO	CHES CARBOACH	A 13.7.12
				And in case of the Control of the Co	<del></del>	-					لي مر سرحيا				

PK-1							LIGI	Ģi Oi	)						
	(				17	[	RT	LENGTH	SLOPE	v	Q	RD&	τo	1 45	i .
AREA	NO.	STATION	PIPE	BOX	LT ELEV.	FLOW	ELEV.			(m/s)	(m³/s)	SLOPE	(m³/s)	AD (m³/s)	REMARKS
	L	-:			CLEV.			(m)	(%)	(1182)	(11175)	(m3/s)	(111.12)	(11178)	<u> </u>
	185	1153+871.30	0.61	x2	46.58		47.32	29.18	-2.538	3.032	1.771	0.132	}		
	187	1153+957.96	1.22		47.19	≪(	47.63	39.00	-1.128	3.209		j	•		1-0.61
	188	1154+133.05		2-1,40 X 2.00	45.51	⋖	45.51	15.76	0.000	0.00		I	ĺ	Î	
1.42	189	1154+316.90		2-1.50 X 2.00	47,07	⋖	47.17	12.08	-0.828	4.05			59.30	35.3	
:	190	1154+362,40	0.30	40.00	48,48		48.68	18 04	0.998	. 1,184		養養養	5.880.0m.48.	ALCONO.	. NIA .
	191	1154+435 20	0.91		46.21	- <b>4</b>	46.40	17.00	-1.118	2.627	1.707	j	j		1-0.61
	192	1154+700.30	1.22		46.87	◀	47.10	21.00	-1.095	3.161	3.694				1-0.91
	193	1154+937.50		3.00 X 1.80	49.05	⋖	49.05	12.63	0.000	0.00			Farmen 2 of Street	Several Server Control of	<b></b>
	184.	1[55f000]	0.45	530	50.28	425	50.51	15,85	31,451	251,871		是汉章		20.37	. NA
1-43	195	1155+310.65	122	x2	45.40	4	45.82	19.00	-2 211	4.491	10.495	Į	49.30	19.8	1-0.91
	196	1155+338.40	1.22	x2	45.07	⋖	45.30	21.00	1.095	3.161	7.387				1-0.61
	197	1155+435 20	0.91	TO THE SECTION ASSESSMENT	46.23		46.41	17.12	-1.052	2.548	1,656	22,000,000	A \$ 100 E \$ 100	र स्टब्स्ट १५ कर	
- : ;	198	1155(926.10	0.45	4 70 000	45.07	<b>2</b> 3 5	35413	318.88	-1.801	2.085	0.331	32.E	433.0	No.	AIN SE
	199	1156+083.60	1 12 TH 12 TH	2-1.50 X 2.00		<b>-4</b>	42.82	12 36	0.486	3.10		and the same	W8945	2107.29Tt28U	 
1-44	300	11,61163,40	0.61	2-1.50 X 2 00	43.70		44.01	20.91	11.483	2317		<b>建筑新</b>	20.00		Bridge (
1-44	201 202	1156+319.50 1156+521.35	0.61	2-1.50 A 2.00	42.14	4	42.39 44.56	12.30 20.17	-2.032	6.34 2.282	38,069	ł	75.68	60.1	<b>{</b>
	203	1156+589.13	0.91		43.21	4	43.80	20.17	-1.438 -2.814	4.168	0.666 2.709	•			i
<del></del>	204	1156+702.40	20.61	STATE OF STREET	43.40	4	43.00 585555	20.97	2.014 	0.000		<del></del>	18-22-W-00-00	ED ARVE	1-0.51
	205	1157/013/43	ठेल इ		40.60	41.5	40.93	18 00	2 062	3 538				0.0	NAW Bridge
1	206	1157+578.50	0.91	## 123 M	38.50	<b>4</b>	38 93	16.00	-2 688	4.073	2648		12.52.5	5.0	3.1061
	207	1158+094.95	0.61	<del> </del>	38.76		38.64	24.00	0.500	1.345	0 393	<del> </del>	<del> </del> -		1 0.61 THE HSE
:	209	1158+103.35	1.07		36.95		36.84	23.69	0.464	1.886	1,695	1			IIIE nac
	210	1158+294.60	0.91		38.42		37.65	25.80	2 984	4 292	2.790				<b>}</b>
2	211	1158+304.40	0.91		38.05		37.54	25.66	1.988	3.503		1			
	212	1158+314.10	0.91		38.08	- 1>	37.57	25.79	1.977	3.494	2 271	<b>!</b>			<del>}</del>
1	213	1158+324.70	0.91	1.0	38.09		37.30	25.47	3.102	4.376		1			<del></del>
1-47	214	1159+264.55		2-2.40x2.40	38.00		37.70	17.00	1.765	7.63	87,921	<del> </del>	77.92	87.9	1-0.61
	215	1159+803 20	0.61		45.54	<b>b</b> e-	45.10	45.65	0.964	1.868	0.546	ļ			
1	216	1160+059.02	0.61	ļ	39.99		38.62	38.13	3.593	3.607	1.054	0.190		, i	}
1-48	217	1160+221.49		1-1.80x1.80	37.55		35.37	18.00	6.556	12.14	39 342	0.170	30.57	63 1	1-0.91
	218	1150+368.80		1-1.80x1.80	39.70		39.33	20.00	1,850	6.45	20,900				1-0.91
	219	1160+489.65	0.61		40.75	Br	39.64	21.00	5.286	4.375	1.278	4			7.
	220	1160+696.70	1.22		39.63	<b>b</b> e-	39.60	20.00	0.150	1.170	1.367			·	1 0 61
:	221	1160+752 35	1.52	x2	39.78		39.48	18.00	1.667	4.515	16.379	1			2.1.07
1-49	223	1160+861.45	0.91	- ;	38.45	<b>&gt;</b>	38.05	15.96	2.506	3.933	2.557	<b>j</b>	38.77	57.7	· · · · · · · · · · · · · · · · · · ·
	224	1160+943.15	0.61		38.10		37.64	23.00	2.000	2 691	0.786	]	ļ	J	<u> </u>
	225	1161+090.70		4.00 X 1.60	36.54	—- <b>Þ</b> ~	36.35	22.00	0.864	5.73	36.657	l			
	226	1161+108.47	1 52	x2	36.50		35.66	22.00	3.818	6.834	24.790				1-0.91
1-50	227	1161+231.55	0.61	, y	37.97	<b>&gt;</b> -	37.64	18.88	1.748	2.516	0.735		18.90	29.0	
	228	1161+320.09	0.91	ļ	38.30		37.49	18.00	4.500	5.270					L
4	229	1161+480.30	0.61		37.81	<b>J&gt;</b> -	37.69	19.28	0.622	1.501	0.439	}			
	230	1161+576.80	ļ	2-1.80x1.80	35.80	··· Ben	36,59	19.00	-4.158	12.89	83.511	Į	:		1-0.61
1-51	231	1161+682,10		1.50 X 1.90	36.38	<b>&gt;</b>	38.35	19,00	0.158	1.75	4.992		42.97	101.2	<u> </u>
	232	1161+774.65	0.91	<u> </u>	37.70		37.48	18.00	1.222	2.747	1.785	1	1 - 1		1-0.61
*	233		<del> </del>	120 X 1.50	38.65		38 56	14.50	0.621	3.47					
· ·		1162+032.90	0.61		40.00		39.81	20.80	0.913	1.819	0.531				
		((62+(41.60	200	300 X 160	40.33	是新產	40.32	3.11.84	180.0			antas	144 ] 2	7.8	, Bridga √
;	-			1.70 X 1.70	38.87		38.73	17.63	0.794	4.07	11.756	,			
1.	237			ļ	45.06		45.57	19.79	2.475	2.994		,	1		
	238	1163+440	0.61		49.15		48.50	18.00	4.062	3.835	1.120	Į .	•		
	544	1163+568,35	0.61	2240242	48.53	KA-	47.68	23.01	3.694	3.657	1.068	J			ļ
4 64	2/0	1163+720	<del></del>	2-2.40x2.40 2-3.00x2.40			45.25	15.00	1.000	6.32	72.809	1960	50	40.0	Addi
	240	1163+872.10			43.33	<b> </b>	43.18	14.00	1.071	6.54	94.206	<b></b> -	56.71	167.0	1-0.61
1-54	241	1164+053.70 1164+130	<del> </del> -	1.40 X 1.40		-	41.97	19.52	1.230	7.01	13.737		17.20	39.5	····
	880	1165/421.70	20.00	1-1.80x1.80	48.30	- <b>&gt;</b>	42.43	17.00	1.588 2.531	7.97	25.807	5385-367-807	ভূ ভূমানা কৰে। ভূমানা কৰিছে		Addi
				114 A 34	49.44	植色文	47.77	20.94	-Charge and delivers	3,027	0.884		24.00	\$47.4	NAW! Bridge
		1165198076		SHIMELY		an =	49.20	17.37	1.389	2243		1000	. 21/10	\$ 0.741	. NIAVN/ Bridge
1	244	1166+341.60	0.61	l	49.46		49.20	14.92	1.743	2.512	0.734	ı			l

K-2 (1	/2)														
					LŦ		RT	LENGTH	SLOPE	٧	Q	RD &	TO	AD	
REA	NO.	STATION	PIPE	вох	ELEV.	FLOW						SLOPE			REMARKS
				4.5	ELEV.		ELEV.	(m)	(%)	(m/s)	(m³/s)	(m3/s)	(m³/s)	(m³/s)	l . I
	1	1167+504.06		1-2.40x2.10	43.20		42.40	18.50	4.324	11.582	58.374				1-0.91
	2	1167+508.75	0.91		44.25	— <b>b</b> -	43.57	18.63	3,650	4 747	3.086				
	3	1167+515 97	0.91	x2	44.32		43.46	20.48	4.199	5.091	6.619				
		1168+528.5		2-6.5x3.0	42.57		42.42	15.60	0.962	8.793	342.931				(toA
	5	1168+906.76		2.40X1.40	57.84		49.18	55.06	15.448	19.584	65.802	0.191			<del> </del>
	6	1169+347.55	1.52	x2	82.41		82.91	26.11	-1.915	4.840	17.556	0.131		. :	
	8	1169+644.40	0.61	<del></del>	108.63		107.73	60.00	1.500	2.331	0.681	0.143			<b></b>
	9	1169+782.81	0.61		102.53		99.06	60.64	5.722		1.330	0.143			<b> </b>
	3	1169+965.34	0.61	<b> </b>	121.64			I		4.552		0.053			
	10					<b>4</b>	123.64	40.00	-5.000	4.255	1.243				
0.4		1170+016.66	0.91		117.94		126.44	39.29	-21.634	11.558	7.512	0.343			
2-1	11	1170+462.70	· · · · · · · · · · · · · · · · · · ·	1-1.50x1.80	139.00		137.62	32.00	4.312	9.060	24.462	0.433	18.93	24.46	1-1.52
2-2	12	1170+984.33	1.22	x2	145.15		143.73	20.00	7,100	8.049	18.809	0 223	13.12	18.81	1-0.91
	13	1171+045.15	0.91		140.74		139.81	17.77	5 234	5.684	3.695	0.048		}	
	14	1171+344.30	0.91		116.61	<b>b</b> -	114.53	40.47	5.140	5.632	3.661	0.250			
2-3	15	1171+443	0.91		108.24		105.13	33.56	9.267	7.563	4.916	0.049	24.97	46.16	1.64
	16	1171+607.64	0.61	x2	100.84		98.85	37.00	5.351	4,402	2.572	0.113			
	18	1171+731.88	1.52		93.05		84.94	39.75	20.403	15.798	28,653	0.057	, .		
	19	1171+800.00	0.61		90.75	Pas-	83.68	30.76	22.984	9.123	2.665	0.057			
2-4	20	1172+010.68	1.22	X2	79.95	· · · · Do-	78.45	22.00	6.818	7.838	18.432	0.167	9.37	18.43	1-1.07
2-5	21	1172+230.67	1.22	x2	63.08		60.47	34.60	7.543	8.296	19.387	0.193	11.19	64.97	
	22	1172+292.60	1.52	x2	56.84	<b>B</b> >-	48.76	62 60	12.907	12.566	45.580			J .	
	24	1172+482.14	0.91		51.27	<b>b</b>	47.77	40.45	8.653	7.308	4.751				
	25	1172+645.90	0.61		46.94		46.71	23.25	1.011	1.913	0.559	0.124		l i	
2-6	26	1172+842 25	- :	2-3.00X3.00	38.89		38.52	15.33	2.414	10.357	186.428	0.120			
	27	1173+171.28	0.91		35.85		35.52	16.53	1.996	3.510	2.282		62.64	194.45	-
	28	1173+209.10	0.61		35.38		35.27	18.11	0.607	1.483	0.433	0.094			2.3 4.4
2-7	29	1173+405.15		2-2.40x1.80	35.70	·- · <b>p</b> -	35.57	16.00	0.813	4.827	41.708	0.315	24.02	45.71	1-0.91
	\$0°	1173193870	1.4.4.2	.1-1.40X1.50	35.[2]		34.6	30 May 18	<b>支热税</b> (4	3.0.00	. 8,0,000	16084	4 PAX	200	#ANA BA
2-8	31	1173+942.85		2-2.40x1.80	35.65	— <b>J</b>	35.53	15.00	0.800	4.790	41.386		34.30	42.43	1-1 22
	32	1174+097.70	0.91		36.71		36.64	16.92	0.414	1.598	1.039				
	33	1174131289	273.4-7	1-0.6000.60	\$7,80		37,46	30 R.O.	1109/556	20,000	<b>64 0,000</b>	1000	ALCONO.	ASS.564.	4 KANA SA
	3	31741359.44	45.5	1-0.60X0.60	38,02		37.74	1.574		€ 0.000	31,0,000			4.37	ANA
1	35	1174+605.51	0.91		37.68		37.63	19.89	0.246	1.233	0.802	- AT AN AT SHEET WAS	CON NO CARREST	- PAGESTAN NE	
2-9	36	1174+663.47	1.07		39.03		38.64	20.32	1.934	3.849	3.459		10.50	16.08	
i		1174+720	- 1	1-1.10X0.90	40.50	- Ba-	40.23	18.00	1.500	3.988	3.948			70.00	
	37	1174+724.67	0.91		40.44		39.71	17.23	4.237	5.114	3.324				
ì	38	1174+994.78	1.22		40.04		39.77	16.08	1.660	3.892	4.548				
	39	1175+484.72	0.91		40.55		40.00	16.00	3.437	4.606	2.994		7/ 1		1-0.61
	40	1175+570.55	0.91	i	39.50	<b>]</b> >-	39.15	15.74	2 224	3.705	2.408		10.0		
2-10	41	1175+783.95	0.91	t	38.01	· <b>k</b> -	37.79	16.05	1.364	2.902	1.887		16.93	21.25	
	42	1175+815.20	0.91	<del></del>	37.77		37.43	17.00	2.000	3.514	2.284				1-0.61
	43	1175+992.59		1-1.50X1.50	35.78		35.68	16.37	0.544	3.099	6.972		i i	5 (3)	1-0.01
	44	1176+215.00	1.22		36.28		35.96	18.00	1.778	4.028	4.706	0.328			1-0.91
	45	1176+649.90	0.91		36.45		36.10	15.83	2 211	3.694	2.401	0.178			170.31
	46	1176+745.27	0.61		38.15	·	35.91	16.00	1.500	2.331	0.681	0.042		* * *	
	47	1176+797.08	2-0.91	<b> </b>	36.05		35.47	17.17	3.378	4.566	5.937	0.042			<b></b>
2-11	49	1176+902 40	0.91	j	36.15		36.00	15.00	1.000	2.484	1.515		20.22	46.31	}
	50	1177+148.61	0.91		36.21	- b	35.72	14.37	3.410	4.588	2.982		20.22	-0.01	
	52	1177+173.85	3.1.22	l	35 92		35 35	13.17	4.328	6.284	22.027			'	
	54	1177+319 20	1.52	ł	38.02		37.57	15.92	2.827	5.880	10.665				
2-12	55	1177+402.85	2 1 22	i	39.42		39.07	16.99	2.060	4.335	10.083		38.30	53.05	
- ·-	57	1177+488.60	<del></del>	2-1.80x1.80	39.70		39.31	20.00	1.950	6.623	42.914		30.30	00.00	1091
2-12	58	1177+580	<del></del>	2-2.40×2.40	40.51		40.28	26.00	0.885	5.404	62.249	0.281	47.78	62.25	2-1.52
-	لسندينا					-		5	L	V.704	UZ £13	V.401	71.10	UZ.ZJ	271.04

PK-2 (	2/2}
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2-13 2-14 2-15	80 61 62 63 64 65 66 67 68 69 70	STATION  1178+041.18 1178+375.10 1178+463.24 1178+560.33 1178+749.75 1178+949.55 1179+094.10 1179+183.43 1179+516.58 1179+784.88	PIPE  1.52 0.61 0.61 1.22 1.52 0.61 1.22	BOX 2-1.50x1.50	£1 ELEV. 49.22 65.58 68.34 63.42 58.00 45.57	FLOW	RT ELEV. 44.84 64.09 63.25 60.03 56.08	LENGTH (m) 41.68 20.77 28.04 31.42	SLOPE (%) 10.509 7.174 18.153	(m/s) 11.338 5.097	Q (m³/s) 20.563 1.489	RD & SLOPE. (m3/s) 0.328 0.041	TO (m³/s)	AD (m'/s) 36.01	REMARKS
2-13 2-14 2-15 2-16	60 61 62 63 64 65 66 67 68 69 70 71	1178+041.18 1178+375.10 1178+463.24 1178+760.33 1178+749.75 1178+949.55 1179+094.10 1179+183.43 1179+516.58 1179+784.88	1.52 0.61 0.61 1.22 1.52 0.61 1.22		ELEV. 49.22 65.58 68.34 63.42 58.00 45.57	A A A	64 09 63 25 60 03	(m) 41.68 20.77 28.04	(%) 10.509 7.174	11.338 5.097	(m³/s) 20.563 1.489	(m3/s) 0.328	(m³/s)	(m'/s)	REMARKS
2-13 2-14 2-15 2-16	61 62 63 64 65 66 67 68 69 70	1178+375.10 1178+463 24 1178+560.33 1178+749.75 1178+949.55 1179+094.10 1179+183.43 1179+516.58 1179+784.88	0.61 0.61 1.22 1.52 0.61 1.22	2-1.50x1.50	49.22 65.58 68.34 63.42 58.00 45.57	- &	44.84 64.09 63.25 60.03	41.68 20.77 28.04	10.509 7.174	11.338 5.097	20.563 1.489	0.328			
2-13 2-14 2-15 2-16	61 62 63 64 65 66 67 68 69 70	1178+375.10 1178+463 24 1178+560.33 1178+749.75 1178+949.55 1179+094.10 1179+183.43 1179+516.58 1179+784.88	0.61 0.61 1.22 1.52 0.61 1.22	2-1.50x1.50	65.58 68.34 63.42 58.00 45.57	- &	64.09 63.25 60.03	20.77 28.04	7.174	5.097	1.489		13.62	36 01	
2-13 2-14 2-15 2-16	62 63 64 65 66 67 68 69 70	1178+463 24 1178+560.33 1178+749.75 1178+949.55 1179+094.10 1179+183.43 1179+516.58 1179+784.88	0.61 1.22 1.52 0.61 1.22	2-1.50x1.50	68.34 63.42 58.00 45.57	A	63 25 60.03	28.04	7.174	5.097		0.041	13.62	36.01	
2-14	63 64 65 66 67 68 69 70	1178+463 24 1178+560.33 1178+749.75 1178+949.55 1179+094.10 1179+183.43 1179+516.58 1179+784.88	0.61 1.22 1.52 0.61 1.22	2-1.50x1.50	68.34 63.42 58.00 45.57	<b>A</b>	63 25 60.03	28.04					13.62	38.01	
2-14	63 64 65 66 67 68 69 70	1178+560.33 1178+749.75 1178+949.55 1179+094.10 1179+183.43 1179+518.58 1179+784.88	1.22 1.52 0.61 1.22	2-1.50x1.50	63.42 58.00 45.57	<b>A</b>	60.03			8.108	2 368				
2-15	64 65 66 67 68 69 70 71	1178+749.75 1178+949.55 1179+094.10 1179+183.43 1179+516.58 1179+784.88	1.52 0.61 1.22	2-1.50x1.50	58.00 45.57	🌬			10.789	9.922	11.593	0.049			
2-15	65 66 67 68 69 70 71	1178+949.55 1179+094.10 1179+183.43 1179+516.58 1179+784.88	0.61		45.57			32.00	6.000	10 287	46 292	0.187	30.39	46.29	1-1.52
2-16	66 67 68 69 70 71	1179+094.10 1179+183.43 1179+516.58 1179+784.88	0.61				42.84	39.26	6.954	9.223	16.727	0.558	30.33	10.23	1 32
2-16	67 68 69 70 71	1179+183.43 1179+516.58 1179+784.88	1.22		55.50		52.30	23.00	13 913	7.098	2.073	0.050	14.00	26.64	
2-16	68 69 70 71	1179+516.58 1179+784.86											11.08	25.51	<b> </b>
2-16	69 70 71	1179+784.88			58.81		58.12	19.10	3.613	5.741	6.708	0.204			ļ
2-16	70 71		0.61		58.97	- · - · · • •	47.54	51.13	22.355	8.997	2.628	0.059			<b></b>
	71		1.22		53.22	>>	47.24	31.37	19.063	13.189	15.410				
2-17		1179+836.97	0.91		53.12	-	51.73	20.35	6.830	6.493	4.221	· ·	11.19	25,52	
2-17		1179+894.50	0.61		54.38		52.68	17.82	9.540	5.877	1.717	0.127			
2.17	72	1180+045.96	0.61		59.87	📂	58.43	18.62	7.734	5.292	1.545				
	73	1180+208.72	1.52	x2	63.00		58.75	25.00	17.000	14.421	52.309	0.153	36.05	52.31	2-0.91
1 1	75	1180+351.27	0.91		68.86		67.64	20.43	5.937	6.054	3.935				
i [	76	1180+380.94	0.61		69.48		67.68	23.31	7.713	5.285	1.544	0.050	1		
2-18	77	1180+453.67	0.91		68.99		66.40	34.63	7.502	6.805	4.424	0.104	1.95	11,20	<del></del>
1 7	78	1180+603.31	0.61		77.32		76.12	22.03	5.456	4.445	1.298	0.199	""	20	<del></del>
1 h	79	1180+920.35	0.61		77.27	-4	80.44	38.76	-8.179	5.442	1.590	0.33			
2-19	80	1181+167.85	1.22	x2	69.49	4	70.70	22.00	-5.500	7.084	16.554	0.199	19.75	25.89	4004
] ~ ' ' } -	81	1181+387.96	122	XZ									19./5	25,89	1-0.61
	82				52.98	-ed	54.80	26.00	-7.000	7.992	9.338	0.255	<u> </u>		1-0.61
		1181+757.75	0.61		37.28	🌬	37.18	19.26	0.519	1.371	0.401				
	85	1182+422.02	<b>980</b>	1-0.70X0.70	38 28	母子	38.05	多色型	17.6%	18 0,000	< 0.000	4.50	的杂色	100	OF NIA 1
3	26	1182+537.09	4000	1-0.80X0.40	\$37.55	*** <b>&gt;</b>	37.5)	数を対する	A STATE	<b>14 0 000</b>	<b>*** 0.000</b>	學校的	40多次	基础等的	NA I
2-20	87	1182+769.40		2-1.50x1.25	37.10		36.96	14.00	1.000	4.023	15.086		40.46	70.94	1-0.61
L	68	1183+001.20		2-1.50x1.25	40.20	<b>&gt;</b>	39.57	14.00	4.500	8.534	32.002	0.061			1-0.61
1	89	1183+095.60		2-1.50x1.25	40.70	255	40.35	14.00	2.500	6.351	23.853			:	1-0.61
2-22	90	1183+185.50		2-1.50X1.20	39.74	b	39.22	19.38	2.683	6.522	23,479		25.70	33,46	
i i		1183+460.00	1.22	x2	41.70		41.38	16.00	2.000	4.272	9,983		-5	5	Addi
i i	91	:11831480.50	.0.61	Salvassa	42.40		42.09	STATE OF STATE	1000	3,0,000	A .0 000	4.17 (MA)	AMASS	Sec. 25.	585 867 85.
2 23	.92	11841014.88	5 1.7	1-0.40X0.40	38.58	[]	38,42	2 4 3 14		0.000				27 34 49	NA.
1 · · · · ·	93	1184+221.25	**(*.04.3 H.B	2-1.50×1.50	35.20		34.70	20.00	2 500	6.640		1875-07	10.60	學發著	
	94	1184+454.50		2-1.50x1.50	37.10		36.06				29.882		19.10	29.88	1-0.61
2 24	95	1184+629.80	0.91	x2	37.80	<u> </u>		16.00	6.500	10.707	48.183				1-0.61
1 429						<b>&gt;</b>	37.64	16.00	1.000	2.484	3.230		46.90	61.33	1-0.61
1 -	96	1184+711	0.91	x2	38.10	•	37.94	16.00	1.000	2.484	3.230			:	1-0.61
<b>  </b>	97	1184+828.80	0.91	x2	38.40		37.80	14.00	4.286	5.143	6.687		ļ		1-0.61
1 1	98	1185+037.60	1.22		38.00	··· Þ	37.73	18.00	1.500	3.700	4.323	0.047			1-0.61
1 1		1185+180	1.22		38.60		38.36	16.00	1.500	3.700	4.323		"		Addi
	100	1185+497.28	1.22	x2	41.50	🗫	41.23	18.00	1.500	3.700	8.645	0.306	21,15	30.50	1-0.91
	101	1185+803.50	1.22	x2	44.70		43.93	22.00	3 500	5.651	13.206	0.095	1		1-0.61
2-26	102	1186+130.05	-	1-2.50X1.50	40.65		40.45	14.49	1.380	6.067	22,753	0.422	30.62	32.74	
		1186+160	1.22	1/2	43.00		42.64	18.00	2.000	4.272	9.983				Add I
	105	1186+849.05	1.52		42.24		42.09	27.78	0.540	2.570	4.661				
	108	1187+983.31		3-2.40x1.80	39.60		39.42	18.00	1.000	5.355	69.407		33.30	69.41	1-0.91
	110	1188+405.65		2-3.00X2.40	44.25		44.23	13.28	0.151	2.453	35.319	<del></del>		07.41	1-0.31
	111	1188+882.20		1-1.60x1.25	38.00	Þ	37.60	16.00	2.500	6.845			50.00	64.04	2064
1 -	113	1189+098.50	1.22	12	36.40	<del></del>					15.401		52.30	61.34	2-0.61
				**			38.16	16.00	1.500	3.700	8.645			1.7	1-0.61
}	114	1189+225.50	0.91		36.50		36.26	16.00	.1.500	3.043	1.978		<u>-</u>		1-0.91
	115	1189+606.83		2-1.80x1.50	35.20		34.88	16.00	2,000	6.424	34.692		24.10	34.69	1-0.61
	116	1189+807.71		3-1.80x1.50	35.10	<b>&gt;</b>	34.92	18.00	1.000	4.543	35.797		42.50	€6.02	1-1.22
	117	1189+928.62		3-1.80x1.25	35.10		34.94	16.00	1.000	4.329	29.221				1-0.61

AREA NO STATION PIPE BOX LEV ROW AT CHORN SOPE V Q Q REA TO MAN REMARKS    1	PX-3															
	ADEA	RΩ	MOLTATO	DIOC	BUA	LT	ELOW	RT	LENGTH	SLOPE	٧	a		ΤD	AD	DELLIPEO
2   1191693   0   0   1	V), L		SIATION	FIFE	60^	ELEV.	FLOW	ELEV.	(m)	(%)	(m/s)	(m³/s)		(m³/s)	(mYs)	REMARKS
1	PK-2						• •								<del></del>	
1								L					0.138		<u> </u>	
Fig.	3-1												0.089	36.23		<del></del>
1						_					1			0.23	43.51	
12   1911   1917   192   2   38.46   P   54.62   24.66   27.75   48.69   5.051							in 🗨	16.4	1300	3.4 2	100	1.82	907372	S 34.54	Sep. 2017	
10   1011/17/30   94   3464   3479   1641   2005   1371   0641   17   17   17   17   17   17   17	. }						1									
11   11111111   112   122   12   134.6	3-2				XZ								0.045	22.55	29.08	1-0.91
1921-19200	1				x2			<del></del>	<del></del>				l	]	1	1.091
3.	3-2	•							<del></del>					33.41	35.57	
329   18   192141160   10   11   11   11   12   12   13   14   15   16   15   15   16   16   16   17   17   16   16   17   17				0.91		38.60	· · · >	38.50			1.936					
15   11221-125-50   091				سيبينا		وتربدت	THE REAL PROPERTY.		25	913 35 AC	3 G-12	\$18.55	90000	<b>全线</b>	Nit Will	the second second second
1992/600   1922   2	3.3			0.01	2502012000		The same of the same of	40.70	1762	4.694	MAP 14	2006	3.44			DELETE
16					x2								ł	17.45	24.95	Addi
1991-1997-40   2-180-180   680		16	1192+682	1.22										. '	<u> </u>	7,331
1991/48000   91				1.22			<del></del>						<u></u>			Addi
1981   1981   1981   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982   1982	3-3	1/		0.01	2-1.80x1.80								<b> </b>	27.04	35,14	
119316200 0 041   58.80   1 66.57   15.00   15.30   30.06   2000   2000   2000   Addit   Addit   Addit   30.00   11931600   122   22   61.40   1 60.19   30.00   1615   38.35   87/2   2008   38.60   57.04   10.91   30.00   1615   38.35   87/2   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00   30.00		18	~~~~		510 S.A.	TAX PROPERTY.		I			3.062		REGERE	SECTION.	10 TO	
20					**************************************		A. C.				3 076	A	S1467 828.00	S422741		
14	3-3"				8		<b>-</b>	58.33					0.032	16.22	19.62	
1195-700	2.4			1.22			<del></del>				~~~~~					
11591620	3-4	21						<del></del>			Pro reference			38.60	52.04	
1199/080	3-5	$\vdash$		·			<del></del>						1	30.74	4204	
36 22 1196-346.70							ł ———						1		42.04	
11991600	3-6	22				31.70	<b>&gt;</b>	31.47	15.00	1.533	4.981	18.680		40.46	46.11	
38 22 1197/04965 152				1.22											1.14	
24 1197/967 85 091 33.52	3-8	23		152	2-1.50x1.25								* -		<u> </u>	
39							<del></del>							5.10		
28   1198-8458   122   3020	3-9	25		0.91			···						·	3.34		
3-10 28 1199169728				1.22												
29 1198-1985,85 122	2.50						<del></del>									
30   199-6935   122   21.55   P 21.50   16.36   15.28   3734   4.863   3734   4.863   31   199-12465   091   22.92   P 21.50   15.71   8.402   7.202   4.881   34   1209-1264   091   22.402.40   21.01   P 20.76   16.00   15.83   7.181   82.730   36.32   37.34   3.835   3.427   36.32   37.34   3.835   3.427   36.32   37.34   3.835   3.427   36.32   37.34   3.345   3.427   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42   3.42	15.0			122			·			<u></u>			1 x 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	64.15	68.03	
31 1199194656 0.91	l						•									1-0.61
34   1200-1006-47   2-2-40x-240   21.01   ⇒ 20.76   16.00   1.583   7.181   82.735   30   1200-178.35   2-2-40x-180   21.62   ⇒ 21.24   16.50   2.303   8.127   70.200   2.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.000   3.		_		0.91		22.82	>									
36   1200+178,35   2-240+150   2162	3-10			0.61	A 2 44 A 44			<del></del>					)	160.22	162.63	
38 1200-78876	:			<del> </del>			ļ						l		1	
3-12 39 1201+0502 85 0.61				<b> </b> -										<u> </u>	<b></b>	
40 1201124075	3-12	39		0.61			·							62 35	65 61	M001
42 1201+970 92 0.61	<u></u>	_						24.87		2 000	6.424		j			1-0.61
3-14 43 1202+12050	3-13			061	1-1.80x1.80		<b>├</b> ──							19.67	26.72	
3-14 44 1202+255.80 0.91	<b> </b> -			001	1-1-50v1-50		ļ ————	<b>.</b>								L
46 1202+565-67	3-14			0.91			<del> </del>							1		1-061
48 1203+286.52		46											\$ 75 - 5	2	V	1-0.61
49 1203+401.30 0.61 18.35							<b>B</b>								4,500	11, 1 F 11
\$\begin{array}{c c c c c c c c c c c c c c c c c c c				061	2-2.40x1.80		4	!					A STATE OF			
51 1203+429.60 0.91 18.03 ► 17.29 16.67 4.439 5.25 3.403  52 1203+528.64 0.61 17.73 ► 17.55 14.34 1.255 2.132 0.623  53 1203+588.16 0.61 17.42 ► 16.55 14.99 5.804 4.584 1.339  55 1203+614.85 0.61 17.69 ► 18.99 14.34 4.881 4.204 1.228  56 1203+58.761 1.52 ×2 14.36 ► 16.13 14.69 7.624 5.254 1.535  57 1203+587.61 1.52 ×2 14.36 ► 14.26 16.19 0.618 2.749 9.971  59 1204+122.38 0.91 12.60 ► 12.55 17.93 0.279 1.312 0.853  60 1204+299.57 0.91 12.64 ► 12.61 16.71 0.180 1.053 0.684  61 1205+343.15 1.52 7.23 ► 7.09 17.91 0.782 3.092 5.608  62 1205+418.65 1.52 6.58 ► 6.51 17.84 0.392 2.191 3.973  63 1205+592.35 1.52 6.83 ► 6.68 16.37 0.918 3.348 6.072  64 1206+225.16 1.52 ×2 4.53 ► 4.19 2.332 1.458 4.223 15.319  65 1206+27.60 0.61 7.77 ► 7.55 15.07 1.460 2.299 0.672  67 1206+283.5 0.61 7.32 ► 7.13 17.87 1.063 1.992 0.573  68 1207+871.20 0.61 8.51 ► 8.02 1.906 2.571 3.051 0.891  70 1208+000.00 0.61 9.00 ► 8.86 15.22 0.920 1.825 0.533  71 1209+022.20 1.52 5.20 ► 4.65 21.75 2.943 6.000 10.881	•				<del> </del>		<del> </del>									1
52 (203) 528 64 (961) 53 (203) 558 56 (061) 17.73		51					<del>                                     </del>								* * * *	
53   1203+588.16   0.61   17.42   16.55   14.99   5.804   4.584   1.339     55   1203+614.85   0.61   17.69   16.99   14.34   4.881   4.204   1.228     56   1203+656.47   0.61   17.25   16.13   14.69   7.624   5.254   1.535     57   1203+867.61   1.52   ×2   14.36   14.26   16.19   0.618   2.749   9.971     59   1204+122.38   0.91   12.60   12.55   17.93   0.279   1.312   0.853     60   1204+293.57   0.91   12.64   12.61   16.71   0.180   1.053   0.684     61   1205+343.15   1.52   7.23   7.09   17.91   0.782   3.092   5.608     62   1205+418.65   1.52   6.83   6.68   6.51   17.84   0.392   2.191   3.973     63   1205+592.35   1.52   6.83   6.68   6.83   6.37   0.916   3.348   6.072     64   1206+225.16   1.52   ×2   4.53   4.19   23.32   1.453   4.223   15.319     65   1206+767.04   0.61   7.77   7.55   15.07   1.460   2.299   0.672     67   1206+928.35   0.61   7.32   7.33   7.33   7.35   1.063   1.962   0.573     68   1207+871.20   0.61   8.51   8.02   19.06   2.571   3.051   0.891     70   1208+00.00   0.61   9.00   8.86   15.22   0.920   1.825   0.533     71   1209+022.20   1.52   5.20   4.56   21.75   2.943   6.000   10.881		-			為抵抗制		33.00	A rel	17.53	1457.14	1.00		1180	SYLO	223315	DELETE
55 1203+614.85 0.61					<b>}</b>		· · · · · · · · · · · · · · · · · · ·									
56 12031656.47 0.61 17.25 → 16.13 14.69 7.624 5.254 1.535  57 1203+887.61 1.52 ×2 14.36 → 14.26 16.19 0.618 2.749 9.971  59 1204+122.38 0.91 12.60 → 12.55 17.93 0.279 1.312 0.853  60 1204+299.57 0.91 12.64 → 12.61 16.71 0.180 1.053 0.684  61 1205+343.15 1.52 7.23 → 7.09 17.91 0.782 3.092 5.608  62 1205+418.65 1.52 6.58 → 6.51 17.84 0.392 2.191 3.973  63 1205+592.35 1.52 6.83 → 6.68 16.37 0.916 3.348 6.072  64 1206+225.16 1.52 ×2 4.53 → 4.19 23.32 1.458 4.223 15.319  65 1206+877.60 0.61 7.77 → 7.55 15.07 1.460 2.299 0.672  66 1206+877.60 0.61 7.77 → 7.55 15.07 1.460 2.299 0.672  67 1206+928.35 0.61 7.32 → 7.13 17.87 1.063 1.962 0.573  68 1207+418.32 → 7.13 17.87 1.063 1.962 0.573  68 1207+671.20 0.61 8.51 → 8.02 19.06 2.571 3.051 0.891  70 1208+000.00 0.61 9.00 → 8.86 15.22 0.920 1.825 0.533  71 1209+022.20 1.52 5.20 → 4.56 21.75 2.943 6.000 10.881							<del></del>							l .		
57       1203+867.61       1.52       x2       14.36       → 14.26       16.19       0.618       2.749       9.971         59       1204+122.38       0.91       12.60       → 12.55       17.93       0.279       1.312       0.853         60       1204+299.57       0.91       12.64       → 12.61       16.71       0.180       1.053       0.684         61       1205+343.15       1.52       7.23       → 7.09       17.91       0.782       3.092       5608         62       1205+418.65       1.52       6.58       → 6.51       17.84       0.392       2.191       3.973         63       1205+592.35       1.52       6.83       → 6.68       16.37       0.916       3.348       6072         64       1206+225.16       1.52       x2       4.53       → 4.19       23.32       1.453       4.223       15.319         65       1206+877.60       0.61       7.77       → 7.55       15.07       1.460       2.299       0.672         67       1206+928.35       0.61       7.32       → 7.13       17.87       1.063       1.902       0.573         69       1207+871.20       0.61       8.51 <t< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td><del></del></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></t<>							<del></del>									
60 1204+299.57 0.91 12.64 ► 12.61 16.71 0.180 1.053 0.684 61 1205+343.15 1.52 7.23 ► 7.09 17.91 0.782 3.092 5.608 62 1205+418.65 1.52 8.58 ► 6.51 17.84 0.392 2.191 3.973 63 1205+592.35 1.52 6.83 ► 6.68 16.37 0.918 3.348 6.072 64 1206+225.16 1.52 ×2 4.53 ► 4.19 23.32 1.458 4.223 15.319 65 1306+787.04 0.61 7.77 ► 7.55 15.07 1.460 2.299 0.672 66 1206+827.60 0.61 7.32 ► 7.13 17.87 1.063 1.962 0.573 68 1207+418.32		57	1203+867.61	1.52	x2		·						:			<del></del>
61 1205+343.15 1.52 7.23 ► 7.09 17.91 0.782 3.092 5.608 62 1205+418.65 1.52 6.58 ► 6.51 17.84 0.392 2.191 3.973 63 1205+592.35 1.52 6.83 ► 6.68 16.37 0.918 3.348 6.072 64 1206+225.16 1.52 ×2 4.53 ► 4.19 23.32 1.458 4.223 15.319 65 1306+787.04 0.61 7.77 ► 7.55 15.07 1.460 2.299 0.672 66 1206+827.60 0.61 7.32 ► 7.13 17.87 1.063 1.962 0.573 68 1207+418.32					ļ							0.853				
62 1205+418.65 1.52 6.58 ► 6.51 17.84 0.392 2.191 3.973 63 1205+592.35 1.52 6.83 ► 6.68 16.37 0.918 3.348 6.072 64 1206+225.16 1.52 ×2 4.53 ► 4.19 23.32 1.458 4.223 15.319 65 1206+77.60 0.61 7.77 ► 7.55 15.07 1.460 2.299 0.672 67 1206+928.35 0.61 7.32 ► 7.13 17.87 1.063 1.962 0.573 68 1207+871.20 0.61 8.51 ► 8.02 19.06 2.571 3.051 0.891 70 1208+000.00 0.61 9.00 ► 8.86 15.22 0.920 1.825 0.533 71 1209+022.20 1.52 5.20 ► 4.56 21.75 2.943 6.000 10.881							f						٠.			
63 1205+59235 1.52 6.83	·				ļ											<b></b>
64 1206+225.16 1.52 x2 4.53 → 4.19 23.32 1.458 4.223 15.319 65 1306+797.04 0.61					<b> </b>											<b> </b>
65 1206+767.04   0.61   7.77   ▶ 7.55   15.07   1.460   2.299   0.672   66 1206+877.60   0.61   7.32   ▶ 7.13   17.87   1.063   1.962   0.573   68 1207+418.32   ▶ 8.02   19.06   2.571   3.051   0.891   69 1207+871.20   0.61   8.51   ▶ 8.02   19.06   2.571   3.051   0.891   70 1208+000.00   0.61   9.00   ▶ 8.86   15.22   0.920   1.825   0.533   71 1209+022.20   1.62   5.20   ▶ 4.56   21.75   2.943   6.000   10.881			1206+225.16	1.52		4.53		4.19			4.223					<del>                                     </del>
66 1206+877.60 0.61 7.77 → 7.55 15.07 1.460 2.299 0.672 67 1206+928.35 0.61 7.32 → 7.13 17.87 1.063 1.962 0.573 68 12074871.20 0.61 8.51 → 8.02 19.06 2.571 3.051 0.891 70 1208+000.00 0.61 9.00 → 8.66 15.22 0.920 1.825 0.533 71 1209+022.20 1.52 5.20 → 4.56 21.75 2.943 6.000 10.881					14 (4.16.)			-	7.0			<b>第一个中央</b>	<b>多数46%</b>	<b>金花雄</b>	Va Air	DELETE
68   1207(4)832									·		·					
69     1207+871.20     0.61     8.51     ►     8.02     19.06     2.571     3.051     0.891       70     1208+000.00     0.61     9.00     ►     8.86     15.22     0.920     1.825     0.533       71     1209+022.20     1.62     5.20     ►     4.56     21.75     2.943     6.000     10.881				-	20022333			-	17.87				STEP SEC.	RELECTED IN	THE PARTIES OF	
70     1208+000 00     0.61     9.00     ▶     8.86     15.22     0.920     1.825     0.533       71     1209+022 20     1.62     5.20     ▶     4.56     21.75     2.943     6.000     10.881	1				A-1-27-48-18-19				19.06				201201	55 65 55 E	SALAK	ALEXED BY
71 1209+022.20 1.52 5.20 <b>►</b> 4.56 21.75 2.943 6.000 10.881		70	1208+000.00													
172 17203+450.00 0.91 [x2   8.50  > 5.94   20.73   2.701   4.683   5.303							- · · •		21.75	2.943	6.000	10.881				
		72	1203+450.00	0.91	[x2	8.50	<b> &gt;</b>	5.94	20.73	2.701	4.683	5.309				

PK-4 (	1/2)					LIC	) I U	FCUL	VERI	5					
	٦				1.7	7	D.T	LCNOT!	CLODE	.,		RD 8	70		
AREA	NO.	STATION	PIPE	BOX	LT ELEV.	FLOW	RT ELEV.	LENGTH (m)	SLOPE (%)	(m/s)	Q (m³/s)	SLOPE	TO (m3/s)	AD (m³/s)	REMARKS
				<u> </u>								(m3/s)	(11,513)	(1175)	
	1	1211+627.08	1.52		0.66	<b>&gt;</b>	0.50	23.43	0.683	2.890	5.242				
	3	1212+327.05 1212+600.00	1.52		2.46		2.41	22.68	0 220	1 642	2.978	STANSON SECTION	SAMPLE SA	YACOSSO SE	25 <b>521 675</b> 77
	4	12124583.51	0.61		\$ 12.0		24.6	7.70	134	0.000	0.000			લ્ફ્રેલ્ડિયા	DECETE
	5	1213+086.75	0.61	x2	5 80	<b>4</b>	5.87	24.00	-0.300	1.042	0.609	543X#X1	R # 82	NEW COLUMN	- Charles
	6	1213+501.31	0.61		6.95		6.99	20.53	-0.195	0.840	0.245			i	
1	7	1213+966.85	0.61		7.90	⋖	8.04	20.30	-0.690	1.580	0.462				
]	8	1214+866.43	0.61		9.47	<b>b</b>	9.43	18.95	0 211	0.874	0.255	,		ļ	
	9	1215+015.50			9.01		8.98	21.35	0.140	0.931	0.605				
	10	1215+170.50		x2	9.89	<b> </b>	9.51	21.81	1.742	2 512	1.467		:		
	12	1215+416.60	0.61	<del></del>	9.12 9.15		8.86 8.76	23.11	1.125	2.018 3.244	0.590 2.109	<b>{</b>			<u> </u>
'	14	1215+995.90	1.52	<del></del>	6.12		6.07	26 24	0.191	1.527	2.769	ł		l	
	15	1216+300.90	1.22		5.74		5.52	21.93	1.003	3.025	3.535		٠,		
<b>'</b>	16	12161949.35		0.80x0.80	₹7.72 ·		6.94	72.90:	3,408	6 097		2 5 19 5 4	100000	<b>发现</b> 自	YA NA SS
1	17	1217+045.06	0.61		6.93		6.86	17.53	0.399	1.202	0.351	ACA MEN	JOSEC MILESCO	31.86-71.8-12.66 DK	
	18	1217+964.42	0.91		4.58		4.46	18.00	0.667	2.029	1,319	] '			
<b>[</b>	19	1218+105.40	0.61		5.32	· D>-	5.25	16.37	0.423	1.244	0.363	ĺ			
1	20	1218+446.13	1.22		4.09		4.04	19.29	0.259	1.538	1.797				
	21	1218+519.08 1218+712.20	0.61		4.90 4.95	<b>&gt;</b>	4.72	18.05 13.50	0.997	1.900	0.555				
i '	23	1218+820.02	0.61		4.72	- <b>&gt;</b>	4.79	15.62	1.185 0.320	2.071 1.077	0.605 0.314	1			}
1 1	24	1218+929.25	0.01	1-1.80x1.60	3.82		3.80	13.30	0.180	1.960	5.646	}	ľ		
1	25	1219+157.50	1.22	11.00%11.00	3.98	- 32-	3.89	14.21	0.634	2.404	2.809				
	26	1216+453.50		0.80x0.60	4.67		4.41	21.25	1,224	3.055	1,955	1000元	3000	OF TAX	AL NIA WA
	27	1219+773.10	0.91		4.88		4.58	16.38	1.831	3.362	2.186			To \$5 65 \$500 CH 2	
1 .	28	1219+783.45	0.91		4.35		4.19	16.45	0.973	2.450	1.593	}			
	29	1219+821.13		2-3.00x2.80	2.87		2.87	13.00	0.000	0.000	0.000				1-3.0x2.8 Add"
	30 31	1219+881.32 1200+023.32		2-2.40x1.80	3.77		3.70	13.00	0.538	3.930	33.953				1-2.4x1.8 Add
<b>1</b> '	33.	12201084.20	0.81	2-2.40x1.80	3.10 3.08 a	1345	3.04	16.00	0.375	3.280 0.000	28.335	323-2-1	MAR		2-1.52 2 DELETE
1.	34	1220+158.20		3VA7437502	4.34		4.31	15.97	0.188	1.077	0.700	<b>公司的</b>	<b>高数数据</b> 6	公室景点是在影	S Seroib
1	33	1220+223,43	486	0.80x0.80	6.00	No. of Par	4.05	841.45	2.291	A.181		erand.		53.67.5	SEE NIA SEE
	36	1220+679.40	1.22		4.10		3.89	15.80	1.330	3.483	4.070	TO SERVICE THE PARTY OF THE	4.2 W. T. S.	200003.23	768 36 658 553 118
	37	1220+943 85	0.61		5.12		4.89	13.88	1.659	2 451	0.716	1		·	
]	38	1220+969.10			5.23		5.14	15.36	0.586	1.457	0.426	La companya da companya da co	an and or harde		
	38.1	1221+024.08	7.1	0.60x0.60	_4.80.	7.6 E	4,54	20,85	0.288	1,482				NA SAN	MA E
1	40	1221+140.12 1221+261.78	1,52	x3	5.02 4.58	<b>A</b>	4.77	14.62 18.40	0.924	2.489 3.362	0.727 18.291				
1	44	1221+378.10	0.91	<del> </del>	4.60		4.49	15.20	0.724	2.114	1.374	}		*	
1	45	1221+750.22	0.91		4.96		4.82	13.13	1.066	2 565	1.668	1		1.5	
1	38	1222+01970		1-0.80x0.00	, 5.03 £		A.81	18.43	1,194	3018				NAME OF	SALANA SA
	47	1222+240.20	0.61		5.88		5.67	14.89	1.411	2.260	0.660	100 M 200 DB 300 M	WORKSON DELIN	and the second of	
1	48	1222+467.20	0.51		6.74	<b>A</b>	6.59	15.02	0.939	1.902	0.558				
	49	1222+599.60		x2	6.94		6.83	14.44	0.762	1.661	0.970	[			
<b>1</b>	51	1222+755.70	0.91	1 A 5A A 64	6.02	**************************************	5.94	18.07		1.653	1.075	\$ \$1 \$1 \$1500 per	94 T 478 F 579	graphic section	Common and a restriction
		1223+027,03 1223+075,76		1-5.6010.00	6.79	A V	9.36 6.70	319 37 15 77	0.878	, 2.588 1.438	x 1.656 0.420	-110-00-01-0	# ak dis	NE BOX	NA 🤝
1		1223+399.90			7.04		6.81	15.81	1.454	2 295	0.670			· '	
1		1223+717.50			7.49		7.34	16.33	0.916	1.821	0.532	l	,		
1	57	1223+914.28	1.52		6.98	<b> &gt;</b> -	6.67	17.34	1.788	4.676	8.481		i		
1		12241727,50	9342		8,38		8.31	17.74	0.395	1.693	0.914	WWW		43.55	SE NA SE
1	59	1224+291.50		1-5.00x2.50		- ≱⊳	8.29	12.31	0.731	6.614	82.678		1		
1		1224+337.80		1-5.00:2.50			6.16	12.31	0.569	5.834	72.929				
1		1224+654.20 1224) 840.00		2-1.80x1.50	6.98	2515	6.96	7.77 34.00 60/	0.257	2 305	12.448	Sagaran a	ESSEPTEMENT	A PERSONAL SEC.	(KARIEVE):
	68 68	12241840.00		400	6.68	<b>&gt;</b>	8 16 6.62	19.75	0.304	1.928	3.496	Malente.	KANADA	<b>《新教》</b>	* DELETE
1	67	1224+919.60			6.81		6.67	22.84	0.504	2 738	4.966				<b></b>
ĺ	68	1224+939.70			6.87		6.75	22.80	0.526	2 537	4.602				
1	69	1225+019.69			6.92		6.68	23.16	1.038	3.560	6.457	i			
1	70	1225+039.28			6.85		6.65	22.94	0.872	3.266	5.923				
Mary and State of the last	لحصمه			Control of the last of the las	Commercial			THE PERSON NAMED IN				Tarana Tarana			Mrs

PK-4 (2/2)

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109 1233+868.27 0.61 111 1234+615.10 0.61

111 \$ 1234+615.10 | 0.61 112 | 1234+773.40 | 0.61 113 | 1234+967.70 | 0.61 114 | 1235+231.62 | 0.61 115 | 1235+664 | 1.22 116 | 1236+289.40 | 1.22 117 | 1236+289.40 | 1.22 118 | 1236+624 | 20 119 | 1236+766 | 95 | 0.44

119 1236+766 95

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AREA		STATION	PIPE	вох	LT ELEV.	FLOW	RT ELEV.	LENGTH (m)	SLOPE (%)	V (m/s)	Q (m³/s)	RD & SLOPE (m3/s)	TD (m3/s)	AD (m³/s)	REMARKS
	71	1225+059.77	1.52		6.66	···· 📂	6.64	22.94	0.087	1.033	1.873				
	72	1225+139.59	1.52		7.07		6.77	16.24	1.847	4.753	8.620	ļ			
	73	1225+179.14	1.52		7.07		6.49	15.55	3.730	6.755	12 251		1	•	
	74	1225+219.00		1-3.00x2.10	6.51		6.51	11.69	9.000	0.000	0.000		l .		
	75	1225+259.25	1.52		6.65	<b>&gt;</b>	6.32	17.02	1.939	4.870	8.832				
	76	1225+298.94	1.52		6.54		6.47	15.35	0.456	2.362	4.284				
	77	1225+339.64		3-3.00x2.10	6.47		6.45	11.73	0.171	2.519	47.601		1		
	78	1225+388.95	1.52	·	6.49		6 35	15.24	0.918	3.352	6.079		!		
	79	1225+439,19	1.52		6.47		6 33	15.35	0.912	3.341	6.059				
	80	1225+478.55		3-3.00x2.00	6.47	· · · ·	6.47	11.17	0.000	0.000	0.000				
	81	1225+518.83	1.52		6.37	<b>}&gt;</b>	6.27	15.69	0.637	2.792	5.065				
	82	1225+559.07	1.52		5.49	<b>д</b> ъ-	6.41	15.46	0.517	2.516	4.563				
	83	1225+598 99	1.52		6.54		6.45	15.32	0.587	2 680	4.861				
	84	1225+639.52	1.52		6.54	·· •	6.48	15.42	0.389	2.182	3.957	j			
	85	1225+679.66	1.52		6.61		6.47	15.43	0.907	3.331	6.042				
	86	1225+719.42	1.22		7.06	· <b>b</b> >	6.97	15.02	0.599	2.338	2.732		1		
	87	1225+783.77	1.22		6 25	<b>-4</b>	7.60	14.74	-9.160	9.142	10.682		·		
	88	1226+074 20	0.61	x2	7.71		7.68	20.93	0.143	0.720	0.421				
	90	1226+143.40	0.61		8.04		7.82	17,82	1.234	2.114	0.618		l		
	91	12281371 50	14.3	1-0.80x0.80	7 69		7.58	*19.52	0.664	2.074	1 327	91.6KW	100 M. A.	Markey	ZE NAVY
	₹2	1227+171.98	1000	1-1-00x 1-00	10.26	42.1	10.24	19.88	0.102	1,022	1.022	33.34	<b>*</b> ₹ ₹ *	4.00	S NA S
	93	1227+239.75	0.61		9.06		8.95	20.61	0.534	1.390	0.406	1,247184742844	HARLEN TO THE	THE STREET	A STANCE OF
	94	1227+295.02	0.61		8.80		8.74	23.86	0.251	0.954	0.279	1	100		
	95	1227+454.65	1.22	x2	10.00		9.66	18,14	1.874	4.135	9.683			1.1	
	97	1229+247.30	1.52		16 24		16.21	18.14	0.165	1.422	2.580				<b></b>
!	98	1229+376.85	1.22	x2	16.70	30-	16.67	17.17	0.175	1.263	2.951				<b> </b>
	100	1229+581.40	1.22		17.70		17.13	15.93	3.367	5.543	6.477			i i	<del></del>
	102	1231+619.56	0.61		14.50	· <b>P</b>	13.93	18.20	3,132	3.368	0.984				
	103	1232+540.60			12.69		12.64	17.96	0.278	1.846	3.347				<b></b>
	104	1232+834.40		x2	13.20		13.04	17.00	0.241	2.931	6.848	l			<b></b>
		6007245 84					70.04	17.00	V.641	6.001	0.040		·	I	

PACKAGE-5 (1/2)

PAU	MO	E-5 (1/2)	and the state of t				- Annanan au								
AREA	NO.	STATION	PIPE	вох	LT ELEV.	FLOW	RT ELEV.	LENGTH (m)	GRADE (%)	V (m/s)	Q (m³/s)	RD & SLOPE _(m3/s)	TD (m³/s)	AD (m³/s)	REMARKS
4-1	121	1237+075.00 1237+347.65	1.22	x2	26.28 24.90	₩	26.60 25.50	16.00	-2.000 -3.000	4.272 5.232	9.983 12.226	701/04:21	14.50	24.74	1-0.61 1-1.22 Addī
4-2	•	1237+380		2-1.25x1.0	27.70	◄	27.90	13.00	-1.538	4.373	10.933		11.70	19.58	Addi
4-3		1237+840 1237+935	1.22	x2 1-2.40x1.80	30.17 36.11		30.50 36.40	22.00 19.00	-1.500 -1.526	3.700 6.616	8.645 28.583		14.60	28.58	Add1 1-1.22
4-4	123	1238+337.20		1-2.40x2.40	47.60		47.51	18.00	0.500	4.062	23.400	<u>·</u>	19.20	23.40	1-1.22
4-5	124	1238+572 20		1-2.40x2.40	41.70		41.61	18.00	0.500	4.062	23.400	0.298	34.17	64.81	1-0.61
	125	1238+923.50		1-1.80x2.10	45.50	<b>&gt;</b> -	44.60	18.00	5.000	10.955	41.411	0.072			1-0.91
4-6	126	1239+021.20 1239+258.3	1.52	x2	47.00 45.55	<b>b</b> >	46.55	18.00	2.500	5.530	10.030	0.099		مد مف	1-0.61
4-0	127 129	1239+230.3	1.52	x2	56.16	· · · <b>þ</b> >-	45.23 54.02	19.95 34.57	1.604 6.190	4.430 8.702	16.068 31.565	0.648	24.95	26.10	ļ
4-7	131	1239+896.24	1.22	~=	67.69	>	63.54	38.70	10.724	9.892	11.558	0.048	27.06	96.70	
	132	1240+008.86	1.52		71.09	· · · Þ>-	68.59	25.96	9.631	10.854	19.686				
	133	1240+010.76 1240+460	1.52	x2	71.72 96.70		70.17 96.00	21.72	7.135 3.043	9.343 5.270	33.889 6.157	0.492			Add?
		1240)718	1225	34.35.5	1		#3 JA	30.00	98.35078	3.210	6.131		hassa	is No.	EDELETE:
	20.107	1240+720	1.22	334,312,43,7	110.20		109.10	17.00	6.471	7.684	8.978	CONTRACT	e except to 2012.	The Section of the Contracts	Addil
5-1	3	1240+911.50	1.22		126.96		125.09	31.00	6.033	7.420	8.669	0.029	13,75	33.90	
ļ	3	1240+972.60 1241+173.80	1.22		130.20	<del></del>	128.40 135.88	22.00	8.182	8.640	10.095	0.219			1-0.91
ľ	4	1241+257.50	1.22		141.38		139.43	37.51 38.96	18.208 5.005	12.890 6.758	15.060 7.896	0.065 0.061			
5-2	5	1241+354.00	0.91		144.51	>	140.96	43.13	8.230	7.128	4.633	0.153	29.27	38.70	
	6	1241+528.90	0.91		148.86		145.36	46.75	7.487	6.798	4.419				
	- <del>7</del>	1241+766.80 1242+096.30	0.91		163.37 185.21	— <b>&gt;</b>	159,94 180,16	44.96 31.44	7.630 16.063	6.863 7.627	4.461 2.228	0.391		,	
5-3	9	1242+458 00	0.91		185.62	4	187.35	33.86	-5.109	5.615	3.650	0.477	17.60	31.47	
	10	1242+678.50		1-1.80x1.80	176.00		177.00	30.50	-3.279	8.59	27.82	0.098	******		1-0.91
	11	1242+923.00	0.91		162.64	◀—	163.48	40.81	-2.058	3.564	2.317	0.132			
5-4	12	1243+006.50 1243+298.60	1.22	1-1.80x1.80	163.90 155.44	<b>⋖</b>	167.85 155.76	31.00 38.00	-12.742	10.783 4.35	12.598	0.028	20.02	FE 40	1-0.61
	14	1243+552.70		1-1-80X1-50	145.26	4	145.18	40.17	-0.842 -2.290	6.83	14.10 18.56	0.264 0.182	38.93	55.19	1-1-22
	15	1243+746.80	1.22		148.65	<b>4</b>	151.23	55.46	-4.652	6.515	7.612	0.219		1	<b></b>
	16	1244+032.40	0.91		174.37	-4	174.98	27.64	-2.207	3.691	2.399	0.017			
5-4A	17	1244+149.60 1244+401.70	0.61	,	180.98 169.53		180.20	18.97	4.112	3.859	1.127	2 252	3.13	7.13	
	19	1244+486.50	0.01	l	170.46		167.79 167.67	35.28 32.01	4.932 8.717	4.226 7.335	1.234 4.768	0.256 0.053			
	20	1244+710.70	0.61		161.64	-4	165.76	42.17	-9.769	5.948	1.737	0.000			
5-5	21	1244+877.50	1.22		163.47		164.11	21.00	-3.048	5,273	6.161	0.140	13,33	22.92	1-0.91
	22	1245+012.30 1245+050	1.22	·	149.95 156.08	-4	152.88	35.29	-8.075	8.584	10.029	0.090			
		1245+200	1 22		148.40	-	156.62 148.80	27.00 20.00	-2.000 -2.000	4.272 4.272	4.931 4.991	0.185			Add'i
	23	1245+285.80		1.80x1.80	140.93	⋖ –	141.37	36.03	-1.055	4.87	15.78	<b>3.103</b>			74001
5-6	24	1245+535.80	1 22		131.63	◀	132.87	52.84	-2.347	4.627	5.407	0.037	29.19	36.65	
5-7	25 26	1245+838.70	1.22 0.61	x2	127.06 106.63	₩	127.50 107.95	20.00	-2.200 -5.066	4.480 4.283	10.470 1.251	0.264			1-0.91
٠.	27	1245+543.00	0.91		98.22	4	100.42	29.71	-7.385	6.752	4.389	0.396 0.418			AFGA BR.
5-8	28	1245+928.60	0.91		97.79	<b>⋖</b>	103.01		-13.801	9.230		0.208	7.99	18.35	
	29	1247+121.00			107.32	4	112.24	40.20	-12 239	10.568	12.347				
5-9 5-10	30	1247+219.50 1247+609.00	1.22	X2 2-3.00X3.00	113.46	≪1	118.48 112.42	31.00	-16.194	12.156	28.405	0.198	15.30	28.41	1-0.91
ا ` ` `	32	1247+721.00	0.61	2-7-0-7-3-00	119.55	-44	120.28	49.41 23.14	-7.327 -3.155	18.05 3.380	324.82 0.987	0.190	16.59	325.81	
	33	1247+829.00	0.91		106.23		112.52	42.19	-14.908	9.593	6.236	0.048			
5-11	34 35	1247+905.00 1248+294.20		<b> </b>	104.95	-15	110.13	44.92	-11.532	8.437	5.484	0.024	,		
3-11	36	1248+294.20	0.61		99.88 112.48		105.82 113.53	48.40 18.40	-12.313 -5.706	10.600 4.546	12.384 1.328	0.240 0.050	11.44	27.03	
<u></u>	37	1248+503.50	0.61		109.63	4	111.51	22.71	-8 278	5.475	1.599	0.077			
	38	1248+697.80			93.92	₩	97.69	35.75	-10.544	8.067	5.244	0.148	· ···		
5-12	39	1248+807.40		<b></b>	92.12		93.65	27.00	-5. <b>C</b> 67	7.191	8.402	0.083	19,63	27.87	1-0.61
	40	1248+939.40 1248+982.40	1.52 0.91	.1	83.19 85.78	-≪	84.64 86.10	40.90 18.00	-3.545 -2.000	6.588 3.514	11.944 2.284			.	1-0.61
5-13	42	1249+305.00		2-3.00X3.00		4	76.62	45.09	-1.818	8.99	161.82	0.193	80.29	161.82	1-0.01
		1249+500	1.22	x2	92.00	-d	92.80	18.00	-5.000	6.755	15.784	0.533			Addi
5-14		1249+940	1.22		118.10	₹	118.70	17.00	-3.529	5.875	6.631	0.475	17.61	28,43	Addil
<u> </u>	43	1250+398.40 1250+867.50	0.91		119.57 88.71	₩	126.13 94.81	47.32 54.18	-13.664 -11.259	9.251 8.336	6.013 5.419	0.440		· · · · · · · · · · · · · · · · · · ·	· ·
	45	1250+956.30	0.61	J	95.79		97.19	21.94	-6.380	4 807	1.404	0.418 0.036			<b>  </b>
5-15	46	1251+099.00	1.52		80.15	a	83.28	45.21	-8.923	9 202	16.690	0.075	30.76	44.54	
	47	1251+248.60	0.61		87.05		87.33	16.40	-1.707	2.486	0.726	0.300			
5-16	48	1251+417.00 1251+760	1.52	x2	87.07 80.50	-di	90.17 81.50	20.00	-10.239 -5.000	11.192	20.298	0.127	10 44	30.60	A de de la constantina della c
V	49	1251+914.00	0.61		65.54	-4	71.36	33.35	-3.000 -17.451	7.821 7.949	28.358 2.322	0.299 0.108	19.11	30.69	Addi
5-17	50	1252+061.50		1-2.40X1.70	57.66	-41	58.50	35.88	-2.342	8.07	32.93	0.066	18.04	36.97	
	51	1252+360.00	0.91		58.42	<b>-4</b> · ·	59.76	21.35	-6.276	6.224	4.046	0.676		******	

### PACKAGE-5 (2/2)

						namedii dale-Marki	Constitution of the last							ACID STREET, SHOWS	
AREA	NO.	STATION	PIPE	вох	LT ELEV.	<b>£</b> LOW	RT ELEV,	LENGTH (m)	GRADE (%)	V (m/s)	Q (m³/s)	RD & SLOPE (m3/s)	TD (m³/s)	AD (m³/s)	REMARKS
		1252+510	1.22		61.80	<b>43</b> ···-	63.30	30.00	-5.000	6.755	7.892	V155.34		1,	Addii
5-18	52	1252+804.80	0.91	i	63.50	<b>4</b>	65.94	33.79	-7.222	6 677	4.340	i l	22.40	30.97	
	53	1252+913.30	1	1-1.80X1.40	57.08	<b>~4</b>	58.13	37.84	-2.775	7.43	18.74				
	54	1253+154.70	1.22		58.11	<b>~₹</b>	58.56	18.86	-2.386	4.666	5.451	0.417			
5-19	55	1253+411.40	1.22		61.14	<b></b>	62.80	23.00	-7.217	8.115	9.482		12.52	25.20	1-0.61
	56	1253+499.00	1.22		61,64		63.50	22.00	-8.455	8.763	10.262				1-0.61
5-20	57	1253+559.40	0.91		61.07	<b>~■</b>	61.76	34.65	-1.992	3.506	2.279			19.64	
	58	1253+836.50	1.22	x2	52.91	<b>~~</b>	53 20	19.00	-1.526	3.732	8.721	0.112	12.81		1-0.61
	<u> </u>	1253+900	1.22	x2	50.51	~ <b>4</b>	50.90	26.00	-1.500	3.700	8.645		• •	<u> </u>	Addii

## PACKAGE-6

					-	الشائد وملامي			-						
ARE	NO.	STATION	PIPE	вох	LT. ELEV.	FLOW	RT. ELEV.	LENGTH (m)	GRADE (%)	V (m/s)	Q (m³/s)	RD &	TD (m <sup>3</sup> /s)	AD (m³/s)	REMARKS
6-1	1	1254+181.70		1-1.80×1.40	48.45	4	48.57	22.93	-0.522	3.225	8.126	(m3/s)	26.53	28 62	
ļ.,	2	1254+289.10		1-2.40x2.00	48.55	4	48.68	21.59	-0.602	4.270	20.496		<del> </del>		<u></u>
6-2	ļ	1254+840 1255±600		2-1.50x1.00 2-1.50x1.00	47.98 47.02	4	49.30	16.00	-8 250 -2 000	10.885 5.359	32.654 16.078		11.90 9.69	32.65 16.08	l'bbA
6-4		1255+820		2-1.80x1.25	47.52	4	47.80	14.00	-2.000	6.122	27.549		21.02	27.55	i tooA
	3	1256+049.00		1-3.00x3.00	47.93	<b>4</b>	48.43	27.25	-1.835	9.031	81 279				7.001
6-5	4	1256+251.85	0.91		53.90	4	54.60	25.00	-3.600	4.714	3.064		19.18	85.09	1-0,61
L	5	1256+422 50	0.61		53.14	■	53.64	27.95	-1.789	2.545	0.743			Į.	
	X-		0.61	3.35.2			51,89	<b>美國教</b>				14.17.3813	91513	<b>32.5</b>	DELETE
6-6	ļ <u>.</u> .	1256+680		2-2.40x2.10	48.80		49.15	14.00	2.500	8.806	88.769	l	32.70	88.77	Addit
6-7	7 8	1256+795.00	0.61	1-1.20x1.20	45.98		45.55	27.93	1.540	4.491	6.467		1 12 12	14.00	
) °-'	<b> -</b> °	1257+163.00 1257+200	0.01	1-1.80x1.25	40.72	▶	40.51	21.73 14.00	0.966 -1.500	1.870 5.302	0.546 11.929		11.16	11.93	Addi
	<del> </del>	1257+840	0.91	1-1.00×1.23	49.90		49.40	15.00	3.333	4.536	2 949		ł		Addi
•	9	1258+149.10	1.22	x2	52.60		51.91	23.00	3.000	5.232	12 226		l		1-0.61
6-8	10	1258+348 20	1.22	x2	60.00		59.40	24.00	2.500	4.776	11.161		18.51	29.39	1-0.91
L	11	1258+714.40	0.91		50.51		48.65	51.88	3.585	4.704	3.058	0.150			
1 -	12	1259+063.30	0.61		55.68		55.45	33.64	0.684	1.574	0.450	0.158			
ļ	13	1259+216.50	0.61	700 F	50.65	<b>&gt;</b> -	50.22	32.53	1.322	2.188	0.639		2000		
1	14	1253+595,10	0.61	7.807.6	18.32	- P		1000	261		19102		Wind	的被心	DELETE
6-9	15	1259+777.50 1259+950.30	0.61 1.22	x2	40.42 36.05	Þ	39.23 35.09	25.40 18.00	4.685 5.383	7.009	1.203	0.114	17.57	22.01	105
1	17	1260+075.00	1.22	×2	33.60	<b>P</b>	33.39	21.00	1.000	3.021	3.529		17.37	23.81	1-0-61
1 1	18	1260+139.85	1.22		34.40	8>-	34.26	24.00	0.583	2.307	2.695		l	<b>l</b>	1-0.61
6-10	19	1260+312.00		1-2.40x2.40	34.80		34.44	18.00	2.000	8.125	48.799		28.85	46.80	1-0.61
	20	1260+454.90	061	`	34.90	<b>b</b>	33.99	26.41	3.446	3.532	1.032	· ·		7.7	
6-11	21	1260+728.20		1-2.40x1.50	33.80	>	33.55	19.61	1.275	5.744	20.679	0.066	18.12	30.01	
	22	1260+857.60	0.61		38.95	<b>&gt;</b>	35.90	24.64	12.377	6.695	1.955	0.036			<b></b>
<b>}</b>	23	1260+983.60 1261+218.30	0.91		45.09 47.66		41.08	25.97 29.35	15.442	9.763	6.346 2.616	0.074	<u> </u>		
6-12	25	1261+557.40	1.22	<b></b>	32.88		46.89 32.83	21.00	2.624 0.238	4.024 1.474	1.722	·	29,44	50.46	1-0.91
	26	1261+734.94		1-1.80×1.50	28.96		28.95	21.30	0.047	0.984	2.657		20.77	50.40	
	27	1261+888.15		2-1.80x1.80	29.30	— <b>⊳</b> -	28.94	18.00	2.000	6.707	43.461				1-0.91
1	28	1262+109.60	0.61		30.53		30.38	18.30	0.836	1.740	0.508				
لـــا	29	1262+263.25	0.61	2-8-8-9-8-8	30.23	<b>D</b>	29.49	22.56	3.281	3.447	1.007		sa darac	THE THE PERSON ST	
6-13	\$Q 31	1262+771.00	432-18	1-0.60x1.00 2-2.40x2.40	30,28 28,40	美色	30.26 27.86	16.00	3 375	10 555	121.588	12000	<b>1919</b>		5) NIA
* "	32	1262+932.08	1 22	2-2.40,2.40	28.75		28.55	17.00	1.176	3.276	3.828		88.90	125.42	1-0.91 1-0.61
	33	12631378.30	25133	1-0,60x0.60	39.63	184.84	30.54	415.38	0.585	1744	81/2/2	1100	NU S	<b>47.8</b> 174	ANA S
6-14	34	1263+478.15	0.61		29 28		28.96	20.98	1.525	2.350	0.686	(30) \$100,440	25.79	47.18	
	35	1263+542		2-1.50x1.25	28.80		27.30	20.00	7.500	11.017	41.314	1.			1-0.91
<b>}</b>	36	1263+850.41	1.22	6 4 05 4 05	28.11		27.56	25.58	2,150	4.429	5.175				
1	37	1264+888.60 1265+029.50		1-1.25x1.25 1-1.25x1.00	25.20 25.20	>>-	24.96 24.99	15.00 14.00	1.600	4.704	7.350 5.398				1-0.61
8-15	39	1265+161.05	0.91	1-1.2021.00	24.30		24 22	16.00	0.500	1.757	1.142	٠.;	18.25	30.29	1-0.61 1-0.61
	40	1265+186.24	0.91		24.20	50-	24.04	16.00	1.000	2.484	1.615		10.20	00.20	1-0.61
	41	1265+204.12	1.22	x2	23,40	>-	22.70	20.00	3.500	5.651	13.206			*.	1-0.61
	42		1.22	-	23.70		23.67	15.00	0.200	1.351	1.578				1-0.61
1 3	43	1265+669.70	0.91		22.11	·	22.07	23.00	0.191	1.087	0.706	1			* *
1	44	1267+521.80 1267+563.40	1.22	1-1.40x1.80	20.64		20.50	25.99 22.22	0.539 0.315	2 217	2.591 5.972	:			
	45	1267+668.80	0.61	2006.00	23.83	A	23.64	319.67 S	0.966	1,870	0.646	71.55.74	Made	28 2 3 3 S	O NASA
	47	1268+055.10	0.61	54 55 0.011	21.61		21.58	24.35	0.123	0.668	0.195	23246.83	47.8-72-57.402	\$1250.1665.	SEY 150 3 Sep.
	48	1268+198.15	061		21.90	<b>-</b>	21.20	18.42	3.800	3.710	1.084				
	49	1268+268.00	1.22		21,53		20.82	38.88	1.826	4.082	4.769				
	50	1268+804.50	1.22		24.41	<b>b</b> -	24.18	20.23	1.137	3 221	3.763	\$2,5 #10EP	SSERVE SON	Section Assets	200000
	<u>\$1</u> 52	1270+111,70 1270+225.00	733	40.00	34.13		43034	.27.83	100	1.10		有种物。	NO PE	1.40	DELETE
	53	1270+356.30	THE PERSON	1-1.20x1.10	35.27		33.72	21.67	7.153	9.489	12 526	edsila.	Caracina	7.655E	DELGTE
4	.84	1270+264.41	0.91	4.000	212.33	B.O.	13252	3. O. O.		3 30 2	4.4	Salata.		MAG	OELEJE
	55	1270+458.10	1.22		33.67		33.50	24.00	0.725	2 572	3.005	CONTRACTOR STATE	n was minerally	* 38.00 p.264	1-0.91
	56	1270+605.40	0.91		32.08		30.70	40.75	3.387	4.572	2.972				
6-16	57	1270+626.8	061	0460 153	32.00		31.73	35.53	0.760	1.659	0.485	المما	13.40	20.52	
L	58	1270+973.00	-	2-1,50x1.50	32.06		31.84	27.00	0.815	3.791	17.059	0.061			1-0.91

PACK	AGE-1	7				LI	SIUF	CULV	ERTS						10.430.
		-			ıT		DT	LENGTH	COADC	T		RD &	TD	AD	
area	NO.	STATION	PIPE	BOX	LT. ELEV.	FLOW	RT. ELEV.	(m)	GRADE (%)	V (m/s)	Q (m³/s)	SLOPE	(m½)	(m½s)	REMARKS
		4074.400.40										(m3/s)			<b>!</b>
7-1	1	1271+103.10 1271+103.10		1-1 20x1 20 2-2 00x2 25	31.03 31.03	<b> </b>	30.95 30.95	26.6	0.301	1.985	5.716 25.751		40.64		l bbA
	2	1271+930.50	0.61	E-E.WALLES	44.46	<b>4</b>	44.90	26.60 36.00	0.301 -1.222	2.851 2.104	0.615	0.012	18.61	31.47	A001
	3	1272+034.00	0.61		46.00	- <b>-</b>	44.20	33.94	5.304	4.382	1.280	0.109			
	4	1272+321.00	0.91		39.52	>	38.17	27.22	4.960	5.533	3.597	0.027		1	·
7-2	5	1272+439.00	1.22		39.36	— <b>b</b> o-	38.03	29.00	4.586	6.469	7.558	]	13.66	18.59	1-0.91
	L	1272+550 1272+840.00	1.22		44.82		43.80	23.00	4.435	6.361	7.432	0.043			
7-3	6	1272+965.00	0.61 1.22		39.62 40.20		38.92 39.74	47.30 25.00	1.480	2.315 4.097	0.676 4.787	0.030	45.77	47.6	1001
1-0	8	1273+098.00	1.22	<del></del>	41.70		39.70	23.00	8.696	8.908	10.408	0.085	13.77	17.95	1-0.61
	9	1273+355.00	0.91		50.71		49.96	45.13	1.662	3.203	2.082	0.000			1 0.01
7-4	10	1273+700.00	0.91		45.21	🕪	45.07	28.50	0.491	1.741	1.132	0.115	25.94	35.91	<del></del>
	11	1273+788.00		1-1.80x1.80	44.30	▶	43.26	20.30	5.123	10.734	34.779	1	<u></u>	<b>\</b>	1-0.61
	12	1274+552.00	0.91		48.84		48.11	24.94	2.927	4.250	2.763				
7-5	13 14	1275+347.90 1275+884.30	1.22 0.91		83.87		80.83	55.73	5.455	7.055	8.243	0.195		l	
1-3	15	1276+136.00	1.22		87.96 78.48	<b>A</b>	84.92 76.03	30.72 25.09	9.895 9.763	7.815 9.438	5.080 11.028	0.517 0.239	21.73	44.84	<b> </b>
	16	1276+179.00	1.22		73.35	>-	64.63	34.56	25.233	15.174	17.729	0.239		1	<b> </b>
	17	1276+454.30		2-3.00X3.0	60.45		60.15	17.14	1.750	8.820	158,760	0.258		<b></b>	<del></del>
l i	18	1276+713.10	1.22		63.56		63.05	31.26	1.631	3.858	4.508	0.051			
l i	19	1276+844.00	0.91		72.30	<b>&gt;</b>	72.07	16.00	1.438	2.979	1.936	0.036			1-0.61
	20	1277+076.50	0.61		72.27		71.32	21.65	4.396	3.990	1.165	0.094			
	21	1277+275.15	0.61	1-2.90x1.90	73.09 72.99		72.34 72.50	20.72	3.620	3.620	1.058	·			
7-6	23	1277+531.00	0.61	1-2.90x1.90	81.34		82.52	23.44 28.59	2.090 -4.127	8.461 3.866	46.619 1.129	}	40.02		
. •	24	1277+571.15	0.61		80.35	4	80.42	25.63	-0.273	0.994	0.290	0.222	18.83	50.84	<u> </u>
	25	1278+008.40	1.22		102.20		102.00	14.00	1.429	3.610	4.218	0.014		Ī	1-0.61
	26	12781658.15	0.61	36.00 Km	115.53	3	116.60	€39,19	-2.731	3.143	0.918		\$160 M	30.00	
7-7		1278+821	0.91		127.20		127.50	14.00	-2.143	3.637	2.364	BE-060	***********	WHITE SERVE	1-0.61
	27	1279+004.00	1.22	<u> </u>	127.60	- <b>4</b>	128.20	25.00	-2.400	4.680	5.468				1-0.61
7-8	28 29	1279+212.00 1279+476.70	1.22	ļ	117.30		116.70 104.75	14.00	4.286	6.253	7.307	0.128	1	l	1-0.61
	30	1279+605.00	0.61		103.29		102.99	19.00 19.02	1.316	3.465 2.390	4.048 0.698	0.139 0.072	8.89	12.05	1-0.61
	31	1279+924	0.61		98.37		98.68	16.16	-1.918	2.636	0.770	0.161			
	32	1280+365.50	0.91		76.18	∢	76.86	29.02	-2.343	3.803	2.472	<i>3.</i> 10.	4		}
	33	1280+704.00		1-2.30x2.60	63.98	· <b>b</b> >-	63.96	21.80	0.092	1.736	10.384				· · · · · · · · · · · · · · · · · · ·
	34	1280+999.20	1.22	L	67.10		66.85	25.00	1.000	3.021	3.529				1-0.61
	35	1281+480 1281+765.50	1.22		81.85		82.00	13.00	-1.154	3.245	3.791				Addl
	36	1282+395.00	0.61		93.24 106.65		92.46 106.73	14.81 15.95	5.267	4.367	1.276				
	37	1282+615.00	0.91		111.09	4	111.16	16.02	-0.502 -0.437	1.760 1.642	1.144 1.068				
	38	1283+442.00		1-2.40×1.40		<b>—</b>	83.79	29.97	1.101	5.228	17.568	0.289			
	39	1283+780.00			93.48		97.11	35.59	3.850	4.875	3.169	0.100			<del></del>
	40	1284+045.00		1-3.00X1.5			82.21	39.47	0.152	2.146	9.656	0.203			
	41	1284+236.60 1284+317.50		4 4 00024 7	89.38	- Þ	86.37	29.87	10.010	6.021	1.759				
	42	1284+317.50	0.61	1-1.80X1.8	86.65 118.94		86.45 117.69	34.68	0.577	3.602	11.669	0.198			
	44	1284+836.00		ļ	125.41		122.39	20.81 30.01	6.007 10.063	4.664 6.037	1.362 1.763	0.069 0.130			
<b>.</b> '	45	1284+959.00			131.33		127.40	39.43	9.967	6.008	1.755	0.130			
	46	1285+287.50	1.22		133.08		132.94	27.80	0.504	2.144	2.505	V.11.0			
1	47	1285+414.50	0.61		134.21		133.07	26.16	4.357	3.972	1.160	1			
1	48	1285+643.20	0.91		133.30		133.10	17.00	1.176	2.695	1.752				1-0.61
	49	1286+072 50		ļ	126.41	🔛	126.02	21.35	1.827	3.358	2.183				
	50 51	1286+244.75 1286+353.35			123.82 122.61		123.20 122.02	21.28	2.914	4.245	2.757		1. 7.		
-	52	1286+711.30			116.78		116.62	17.04 16.00	3.462 1.000	3.541 3.021	1.034 3.529			ļ	1-0.91
	53	1287+211.00		<del></del>	110.55	80-	110.05	18.00	2.778	5.035	5.882				1-0.91
	54	1287+601.00			103.44		103.46	16.92	-0 118	0.654	0.191				
7-9	55		1.22		100.41		100.09	27.63	1.158	3.251	3.798		13.17	19.48	
	56	1288+021.75			96.07		96.06	18.03	0.055	0.711	0.831		1		
	57	1288+340.20	1.22		95.40		95.10	18.00	1.667	3.900	4.556	]	11.14		1-0.61
7-10	58	1288+993.40 1290+300	0.61 1.22		90.27 81.00	4	90.73	18.43	-2.496	3.007	0.878				
ا ۱۰۰۰	59	1290+667.00	1.44	1-1.80x2.10		4	81.50 93.00	17.00 23.00	-2.941 -1.739	5.180 6.461	6.053 24.423	0.044	1.61	30.48	Add'i
	60	1290+827.00		1-2.30x1.20		4	87.81	28.94	-2.038	6.675	18.422	0.055			1-0.91
	وسيسا			and the second second second		L			5.000	7.010	17.74 6	AND DESCRIPTIONS			

	c						وسائده موسور جيوانك		GRAD		_	RD&		i	<del></del>
AREA	NO.	STATION	PIPE	вох	LT	FLOW	RT	LENGTH	E (	(m/s)	(m3/s)	SLOPE	TD (m <sup>1</sup> /s)	AD (m³/s)	REMARK
8-1	1	1291+106.64	1.22		96.58		96.86	(m) 23.48	%) -1.193	3.299	3.854	(m3/s) 0.09	4.36	8.73	ļ
0-1		1291+940	1.22		99.90		99.50	21.00	1.905	4.169	4.871	0.09	4.30	0.73	Addi
8-2		1292+080	1.22	x2	101.90	- <b>b</b> -	101.60	14.00	2.143	4.422	10.333		6.68	10.33	Addil
	2	1292+326.00	0.91		106.25	-≪	106.72	22.71	-2.069	3.574	2.323				
	3	1292+584.30	0.61		102.83	· ⊳	102.14	20.45	3.374	3.495	1.021	0.113	_		
8-3	4 5	1292+755.00	0.61		97.24	🌬	96.47	23.96	3.214	3.411	0.996	0.236	1.26	10.01	<u> </u>
	6	1292+910.00 1293+386.60	0.91 1.22	<b></b>	85.80 73.51	·-· <b>b</b> >	84.55 73.07	34.70 22.56	3,602 1,951	4.715 4.219	3.065 4.929	0.012 0.266			
8-4	7	1293+547.00	7.22	1-1.50x1.20	68.67		68.55	15.08	0.796	3.551	6.392	0.153	2.48	8.51	<del>]</del> -
	8	1293+769.20	0.61		57.97		54.58	23.28	14.560	7.261	2.121	0.123	2.10	0.01	
	9	1294+350.61	0.61		45.89	- <b>b</b> >	44.59	21.83	5.955	4.644	1.356				
	10	1294+661.00	0.61		37.96	<b>&gt;</b>	37.50	18.74	2.449	2.978	0.870	0.219		· ·	
	11	1294+793.00	0.91		37.00	· · •	36.35	16.73	3.885	4.897	3.183	0.206	-		
	12 13	1295+008.00 1295+521.00	1.22 0.61		36.45 51.73		35.99 51.22	17.29 21.62	2.661 2.359	4.928 2.923	5.758 0.854	0.18			ļ
8-5	14	1295+926.00	0.61		54.93		54.64	19.97	1,452	2.293	0.670	:	0.81	2.42	<u> </u>
•	15	1295+995.50	0.61		53.39	\$5>	52.63	29.37	2.588	3.061	0.894		0.07	2.42	<del></del>
	16	1296+529.00	0.61		57.46		56.46	23.85	4.193	3.896	1.138				
	17	1296+841.20	0.61		40.95	-≪1	43.48	28.64	-8.835	5.656	1.652	0.194			
	18	1296+947.00	0.61		37.50	<b></b>	37.56	22.87	-0.262	0.975	0.285	0.058		1	
	19 20	1297+043.50 1297+234.15	0.61	2-3.00x2.70	36.52 34.16	-4 -	36.70	18.47 22.38	-0.975	1.879 8.700	0.549 140.938	0.037			ļ
	21	1297+328.50	——	1-2.50x2.70	33.93		33.76 33.69	13.66	1.788 1.757	7.958	53,716				<u> </u>
	22	1297+558.00	0.91	3.	35.67	≪1	36.34	28.70	-2.335	3.796	2.468	0.315			
8-6	23	1297+938.50	1.22		50.30	····  }>>	49.41	43.00	2.070	4.346	5.078	0.018	2.24	5.08	1-0.61
۸.	24	1298+181.80	0.91		44.00	-≪6	45.60	46.67	-3.428	4.600	2.990	0.051			
	25	1298+343.40	0.91		41.85	⋖	42.53	38.49	-1.767	3.302	2.147	0.072	1.3	ł	
	26 27	1298+440 1298+590.90	0.61	·	46.25		45.65	28.63	2.099	2.757	0.805	0.06			<b></b>
	28	1298+674.50	0.61		45.20 44.28	<b>⋖</b>	46.32 45.04	30.77 24.19	-3.640 -3.141	4.740 3.373	3.081 0.985	0.056 0.05	٠.		<u> </u>
	29	1298+733.00	0.61		43.53	-di	44.88	29.59	-4.568	4.067	1.188	0.031			<del></del>
	30	1298+928.00	0.61	y .	39.27	<b>b</b> o-	38.72	38.27	1.437	2.281	0.666	0.054			
	31	1299+104.10	0.61	14,759	44.61		44.35	36.44	0.719	1.614	0.471	0.063		:	
	32	1299+240	0.91		49.80	<b>D</b> =-	49.00	22.00	3.636	4.738	3.080				
	33	1299+508.20 1299+709.50	0.61 1.22		39.35	>>	37.47	47.88	3.926	3.771	1.101	0.213		1	
	35	1300+064.37	1.22	2-3.00x1.85	34.40 32.71	₩	34.90 32.62	21.00 12.43	-2.381 0.724	4.661 5.003	5.446 55.534	0.114			1-0.61
8-7	36	1300+361.10		1-2.50x2.10	32.04		31.24	12.56	6.369	14,300	75.073	2 1	0.38	75.07	-
	37	1300+900.00	0.61		31.72		31.21	19.82	2.573	3.053	0.892	. :		, , , , , ,	f
	38	1300+924.10	0.91		32.02		31.71	15.54	1.995	3.509	2.281		: .	. *	
	39	1301+087.60	0.61		31.52	· }>-	31.29	19.45	1.183	2.069	0.604				
8-8	40	1301+169.23			31.27	<b>j</b> es-	30.76	22.92	2.207	2.827	0.826		0.40		1 000
0.0	41	1301+792.50	0.61		32.12		31.78 32.45	17.00 19.72	2.018 0.406	4.291 1.212	5.013 0.354		3.42	5.37	1-0.61
	43	1302+298.00	0.91		34.02	_ <b>&gt;</b>	33.91	25.42	0.413	1.597	1.038				
	44	1302+381.00	0.91		34.74	<b>B</b>	34.60	20.75	0.665	2.026	1.317				
.	45	1302+487.00	0.61		34.25	<b> &gt;</b> -	33.85	26.05	1.536	2.358	0.689				
	46	1302+640	0.61		35.17	🌬	34.72	41.25	1.091	1.987	0.581				
8-9	47	1302+955.00 1303+074.50	0.61	<b> </b>	32.81		32.60	30.19	0.682	1.572	0.459	0000	0.16	0.46	
:	40	1303+074.50	1.22	<b> </b>	32.55 34.19	₩	32.41 33.90	26.41 23.00	0.534 1.261	1.390 3.392	0.406 3.963	0.057			Addl
	49	1303+368.00	0.61		33.56	<b> </b> >-	32.35	28.35	4.268	3.931	1.148	0.095			7001
3-10A	50	1303+711.5		1-1.50x1.50	31.75		31.56	18.00	1.072	4.349	9.785	0.056	8.63	28.30	1-1.22
	51	1303+848.20			31.70	- 🌬	31.20	22.00	2 273	4.554	5.321	0.117			1-0.61
	52	1304+077-00	1.22		33.80		32.90	19.00	4.737	6.574	7.681	0.093			1-0.61
0 000	53	1304+292.30	0.61	4 2 60-2 65	35.01	<b>-4</b>	36.43	16.99	-8.359	5.502	1.607	0.138	A= 53 -	1	
3-10B 8-11	54 55	1305+312.60 1305+424.15		1-3.00x3.00 1-2.60x2.50	26.10 24.76		25.97 24.58	13.00 15.05	1.000	6.667 6.366	60.000		35.39	60.00	1-0.61
<b>9</b> 41	56	1305+706.65	122	1-E 00XE.00	26.60		26.46	16.00	1.163 0.875	2.826	39.786 3.301		0.95	43.09	1-0.61
	57	1305+804.90			26.40	>	26.26	15.00	0.933	2.918	3.410				1-0.61
	58	1305+912.80	1.22		26.50	- <b>J</b>	26.36	16.00	0.875	2.826	3.301				1-0.61
	59	1305+973.50	1.22		26.40	<b>]</b> s>-	26.26	15.00	0.933	2.918	3.410	}			1-0.61
8-12	60	1306+099.10	1.22		27.30	-·· <b> </b>	27.17	15.00	0.867	2.812	3.266	0.055	1.37	21.49	1-0.61
	61	1306+256.30			27.80	· · · <b>k</b> >-	27.66	16.00	0.875	2.826	3.301				1-0.61
. 1	62 63	1306+449.00 1306+501.50	1.22 0.61		27.90 30.30	<b>&gt;</b>	27.76 29.11	16.00 16.87	0.875 7.053	2.826 5.054	3.301 1.476			'	1.0.61
	64	1306+702.00	0.61		29.91		29.11	26.57	1.694	2.477	0.723				
						_	~~								

	(AGE	E-9													
RE	NO.	STATION	PIPE	вох	ELEV.	FLOW	ELEV.	LENGTH (m)	GRADE (%)	V (m/s)	Q (m³/s)	RD & SLOPE (m3/s)	TĐ (m³/s)	AD (m³/s)	REMARK
	1	1307+050.50	1.22		28.10	···· >-	26.96	19.00	6.000	7.399	8,645	(IROS)			1-0.61
Į	2	1307+078.00	1.22		28.00	<b>&gt;</b>	27.32	17.00	4.000	6.041	7.059	] '			1-0.61
ļ	_3	1307+133.00	1.22	·	27.90		27.63	18.00	1.500	3.700	4.323				1-0.61
ŀ	4	1307+234.30 1307+278.50	1.22		27.08 27.59		26.83 27.28	20.00 22.00	1.250 1.409	3.377	3.945 4.190				1-0.91
ł	-6	1307+672 85		2-1.80x2.10	28.87	•	27.30	20.84	7.534	13.447	101.662	ł .			1-1.8x2.1 A
ì	Ť	1307+900		1-1.50x1.50	28.90		28.75	15.00	1.000	4.200	9.449	{ · · · · · · · · · · · · · · · · · · ·	,		Addi
Ì	7	1307+946.60	1.22		27.82	<b>j</b> es-	27.51	22.33	1.388	3.559	4.158	i l			<u> </u>
- [		1308+010		1-1.50x1.50	29.00	· Þ	28 86	14.00	1.000	4.200	9,449	i l			Addil
	8	1308+090.10		2-1.50x1.50	27.97	À	27.72	49.00	0.510	3.000	13.499	]			1-1.22
	_9_	1308+254.00		2-3.00x3.00	28.01	<b>)</b>	27.88	9.45	1.375	7.818	140.723				
	10	1308+303	1.22	5 4 65 4 65	29.42		29.15	28.00	0.964	2.966	3.466			ļ	Addit
ŀ	-10	1308+449.35	1 22	2-1.50x1.50	29.70 29.70		28.98 29.54	16.00 16.00	4.500 1.000	8.909 3.021	40.090 3.529			!	2-0.91 Addii
ŀ	12	1308+797.00	1 22		30.10		29.96	14.00	1.000	3.021	3.529				1-0.91
1	13	1308+880.00	122	:	30.30	<b>Þ</b>	30.06	16.00	1.500	3.700	4.323		57.77	215.47	1-0.61
		1308+900	1.22	1.2	30.00		29.84	16.00	1.000	3.021	3.529	,			Addi
- [		1308+990	1.22		30.80	<b>J</b> D	30.64	16.00	1.000	3.021	3.529			1	Addil
- 1	14	1309+026.90	1.22		31.20		30.96	16.00	1.500	3.700	4.323				1-0.61
1	15	1309+143.00	1.22	0.000.000	32.57	🌬	31 66	17.54	5.188	6.880	8.039		-	1	
-	16	1309+180.00 1309+300.00		2-3.00x2.20 2-1.50x1.20	31.86 32.22		31.40 31.62	14.63 15.50	3.144 3.871	10.953	144.582				l
2	18	1309+563.60		1-1.50x1.50	34.29		33.96	14.28	2311	7.834 6.384	28.201 14.365		39.62	47,80	1-0.91
٠,	19	1309+760.80	1.22	1-1302130	34.6		34 27	15.00	2 200	4.480	5,235		39.02	41.00	1-0.61
3	20	1309+898 25	1.22	1 1	35.20		35.04	16.00	1.000	3.021	3.529		28.79	74.37	1-0.61
	21	1310+108.00		2-2.50x1.50	36.82	— <b>b</b>	36.34	14.35	3.345	9.445	70.840	1.			
4	22	1310+263.60		2-2.50x1.80	36.60	·- ·- Þ-	36.32	14.00	2.000	7.697	69.277		48.76	77.92	1-0.61
		1310+360	1.22	x2	37.05		36.81	16.00	1.500	3.700	8.645		4.1		Addi
5	23 24	1310+421.90	1.22	x2 x2	36.30	<b> &gt;</b> -	35.64	22.00	3.000	5.232	12.226	l	19.31	26.34	1-0.91
-	25	1310+513.00 1310+914.50	0.91	XZ	39.60 54.66	— <b>Þ</b> -	38.72 53.17	22.00 27.81	4.000 5.358	6.041	14.118	0.115		3000	1-0.61
6	26	1311+055.00	1.22	x2	56.01		54.05	26.00	7.538	5.751 8.294	3.738 19.381	0.056	38.82	59.21	1-0.61
1	27	1311+151.00	1.22	x2	54.48		52 32	28.00	7.714	8 390	19.605	0.026	30.02	39.21	1-0.61
ı	28	1311+253.50	1.22	x2	53.30	· · · · <b>k</b>	52.10	22.00	5.455	7.055	16.486				1-0.61
7	29	1311+635.00	3	2-1.80x1.80	44.98		44.28	17.95	3.900	9.365	60.688		35.37	101.46	
	30	1311+780.00		2-1.80x1.80	43.54	···· <b>}</b> >-	43.22	18.18	1.760	6.292	40.772				
8	31	1312+074.00	1.22	x2	53,40		52.28	32.00	3.500	5.651	13.206	0.081	15.50	23.19	1-0.91
9	32	1312+221.30	1.22	3 3 00-0 40	62.70		61.02	21.00	8.000	8.544	9.983	0.115		1 1 1	1-0.91
٠,	34	1312+741.50	0.61	3-3.00x2.40	68.79 88.99	<b>&gt;</b>	66.20 88.06	38.00 39.18	6.816 2.374	16.500 2.932	356.407 0.856	0.081	33.93	357.26	<u> </u>
	35	1313+010.10	1.22		76.43		75.21	35.37	3.449	5.610	6.555	0.153	<del></del>		
10	36	1313+169.50	0.61	<del></del>	80.74	- 30-	79.87	23.32	3.731	3.676	1.074	0.133	32.14	343.96	
	37	1313+405.60		3-3.00x3.00	66.07	<b>b</b>	64.59	42.39	3.491	12.457	338.335	0.110			
	38	1313+740.00	0.61	4 .	72.61	⋖	72.98	29.14	-1.201	2.086	0.609	0.033		:	
11	39	1313+931.80		1-1.30x1.20	67.85		66.92	28.90	3.218	6.724	10.490		29.69	42.57	
	40	1314+028.20		1-1.80x2.10			66.93	29.00	3.000	8.486	32.077	0.029			1-0.6x0
	41	1314+452.80 1315+404.80	<u></u>	1-1.80x1.20 1-1.50x1.20	38.22 24.60		37.67 24.27	31.68 18.91	1.736 1.745	5.639	12.179	0.060	- : :		
13	43	1315+601.50	1.22	x2	25.11	-	24.74	17.00	2.178	5.260 4.456	9.467 10.414	0.065	20.49	29.47	1-0.61
	44	1315+774.50		1-1.80x1.50	25.39	<b>b</b> -	25.31	19.41	0.412	2.916	7.874		20.49	25.47	1-0.01
	45	1315+973.90	0.91		27.00	>	26.58	37.25	1.128	2.638	1.715	0.036			}
14	46	1316+182.00	1.22	x2	32.84	<b> </b> >-	32.34	28.00	1.788	4.037	9.433		7.59	10.10	1-0.91
	47	1316+290.20	0.61		33.93		33.44	34.14	1.435	2 260	0.668			<u> </u>	
ļ	48	1315+663.20	1.22		30.84	· Þ	30.77	44.89	0.158	1.429	2.058				
ļ	49 50	1316+671.00	0.91	<b> </b>	33.83 30.58	<b>&gt;</b>	33.08 29.68	32.95 28.69	2.276 3.137	3.748 4.400	2.437			N 5-	
1	51	1317+061.20	0.61		33.56	<b>D</b>	33 22	17.58	1.934	2.646	2.860 0.773	0.071	1.	· · · · · · ·	
	52	1317+851.10		2-3.00x3.00	33.03		32.84	19.54	0.972	6.574	118,330				}
. 1	53	1318+091.50	0.61		34.50	<b>-4</b>	34.19	17.14	1.809	2.559	0.748			÷ .	<b></b>
		4044 000			32.91	🌬	32.58	18.77	1.758	2.523	0.737				
	54	1318+258.30					30.70	20.00	1.200	3.309	7.732		6.93	14.79	1-0.91
15	55	1318+447.50	1.22	x2	30.94					0.004	- 0.70		F 75.7		
_	55 58	1318+447.50 1318+777.00		x2	29.34	-··- <b>b</b> >-	29.14	20.00	1.000	3.021	7.059				<u></u>
_	55 56 57	1318+447.50 1318+777.00 1319+013.80		x2 1-1.80x2.10	29.34 29.26	<b> &gt;</b>	29.10	20.00	0.800	4.382	16.564		13.98	16.56	<u></u>
16	55 56 57 58	1318+447.50 1318+777.00 1319+013.80 1319+217.80	1 22	x2 1-1.80x2.10 2-2.40x2.10	29.34 29.26 27.97	- <b>-</b>	29.10 28.04	20.00 22.41	0.800 -0.312	4.382 3.113	16.564 31.378		13.98	- 4	1-1.22
16	55 56 57 58 59	1318+447.50 1318+777.00 1319+013.80 1319+217.80 1319+993.20		x2 1-1.80x2.10 2-2.40x2.10 x2	29.34 29.26 27.97 27.08		29.10 28.04 26.80	20.00 22.41 18.00	0.800 -0.312 1.556	4.382 3.113 3.767	16.564 31.378 8.804			16.56 27.01	1-1 22 1-0 91
16	55 56 57 58	1318+447.50 1318+777.00 1319+013.80 1319+217.80 1319+993.20 1320+179.00	1 22	x2 1-1.80x2.10 2-2.40x2.10 x2 1-1.80x2.00	29.34 29.26 27.97 27.08 25.25	- <b>-</b>	29.10 28.04 26.80 25.00	20 00 22 41 18 00 23 00	0.800 -0.312 1.556 1.087	4.382 3.113 3.767 5.057	16.564 31.378 8.804 18.207		13.98	- 4	1-1.22 1-0.91 1-0.61
16	55 56 57 58 59 60	1318+447.50 1318+777.00 1319+013.80 1319+217.80 1319+993.20	1 22	x2 1-1.80x2.10 2-2.40x2.10 x2	29.34 29.26 27.97 27.08		29.10 28.04 26.80	20.00 22.41 18.00	0.800 -0.312 1.556	4.382 3.113 3.767 5.057 3.645	16.564 31.378 8.804 18.207 61.238		13.98	- 4	1-1 22 1-0.91 1-0.61
16	55 56 57 58 59 60 61	1318+447.50 1318+777.00 1319+013.80 1319+217.80 1319+993.20 1320+179.00 1320+467.63	1 22	x2 1-1.80x2.10 2-2.40x2.10 x2 1-1.80x2.00	29 34 29 26 27 97 27 03 25 25 22 84		29.10 28.04 26.80 25.00 22.68	20.00 22.41 18.00 23.00 51.87	0.800 -0.312 1.556 1.087 0.308	4.382 3.113 3.767 5.057	16.564 31.378 8.804 18.207		13.98 23.69	27.01	1-0.91 1-0.61 1-0.61
16	55 56 57 58 59 60 61 62	1318+447.50 1318+777.00 1319+013.60 1319+217.80 1319+993.20 1320+179.00 1320+467.63 1320+696.50	1 22	x2 1-1.80x2 10 2-2.40x2.10 x2 1-1.80x2 00 2-3.00x2 80	29 34 29 26 27 97 27 08 25 25 22 84 24 70	- A	29 10 28 04 26 80 25 00 22 68 24 50	20 00 22 41 18 00 23 00 51 87 24 00	0.800 -0.312 1.556 1.087 0.308 0.833	4.382 3.113 3.767 5.057 3.645 2.758	16.564 31.378 8.804 18.207 61.238 3.222		13.98	27.01	1-1-22 1-0-91 1-0-61 1-0-61
16	55 56 57 58 59 60 61 62	1318+447.50 1318+777.00 1319+013.80 1319+217.80 1319+993.20 1320+179.00 1320+467.63 1320+696.50 1320+966.00 1321+100	1 22	x2 1-1.80x2.10 2-2.40x2.10 x2 1-1.80x2.00 2-3.00x2.80 2-2.60x2.00 1-1.25X1.00	29 34 29 26 27 97 27 08 25 25 22 84 24 70 21 02 23 95 22 70	- A	29 10 28 04 26 80 25 00 22 68 24 50 20 22 23 90 22 15	20 00 22.41 18.00 23.00 51.87 24.00 23.36 19.00 22.00	0.800 -0.312 1.556 1.087 0.308 0.833 3.425 0.263 2.500	4.382 3.113 3.767 5.057 3.645 2.758 10.524	16.564 31.378 8.804 18.207 61.238 3.222 109.452		13.98 23.69	27.01	1-1-22 1-0-91 1-0-61 1-0-61
16	55 56 57 58 59 60 61 62 63	1318+447.50 1318+777.00 1319+013.80 1319+217.80 1319+993.20 1320+179.00 1320+696.50 1320+696.50 1321+100 1321+375.50	122	x2 1-1.80x2 10 2-2.40x2 10 x2 1-1.80x2 00 2-3.00x2 80 2-2.60x2 00	29 34 29 26 27 97 27 08 25 25 22 84 24 70 21 02 23 95 22 70 27 70		29.10 28.04 26.80 25.00 22.68 24.50 20.22 23.90 22.15 27.13	20 00 22 41 18 00 23 00 51 87 24 00 23 36 19 00 22 00 19 00	0.800 -0.312 1.556 1.087 0.308 0.833 3.425 0.263 2.500 3.000	4 382 3 113 3 767 5 057 3 645 2 758 10 524 1 809 4 776 5 232	16.564 31.378 8.804 18.207 61.238 3.222 109.452 4.522 5.580 12.228		13.98	27.01	1-0-91 1-0-61 1-0-61 1-0-61 Addit
17	55 56 57 58 59 60 61 62 63	1318+447.50 1318+777.00 1319+013.80 1319+217.80 1319+993.20 1320+467.63 1320+696.50 1320+966.00 1321+100 1321+780 1322+222.80	1.22 1.22 1.22 1.22 1.22 0.91	x2 1-1.80x2.10 2-2.40x2.10 x2 1-1.80x2.00 2-3.00x2.80 2-2.60x2.00 1-1.25X1.00 x2	29.34 29.26 27.97 27.03 25.25 22.84 24.70 21.02 23.95 22.70 27.70 25.52		29.10 28.04 26.80 25.00 22.68 24.50 20.22 23.90 22.15 27.13 25.64	20 00 22 41 18 00 23 00 51 87 24 00 23 36 19 00 22 00 19 00 32 41	0.800 -0.312 1.556 1.087 0.308 0.833 3.425 0.263 2.500 3.000 -0.370	4 382 3.113 3.767 5.057 3.645 2.758 10.524 1.809 4.776 5.232 1.512	16.564 31.378 8.804 18.207 61.238 3.222 109.452 4.522 5.580 12.228		13.98 23.69 10.60	27.01	1-1-22 1-0-91 1-0-61 1-0-61 1-0-61 Add1 1-0-61 Add1
16	55 56 57 58 59 60 61 62 63 64	1318+447.50 1318+777.00 1319+013.80 1319+217.80 1319+993.20 1320+179.00 1320+467.63 1320+696.00 1321+100 1321+78.0 1322+222.80 1322+400	122	x2 1-1.80x2.10 2-2.40x2.10 x2 1-1.80x2.00 2-3.00x2.80 2-2.60x2.00 1-1.25X1.00 x2	29.34 29.26 27.97 27.08 25.25 22.84 24.70 21.02 23.95 22.70 27.70 25.52 26.32	- A - A - A - A - A - A - A - A - A - A	29 10 28 04 26 80 25 00 22 68 24 50 20 22 23 90 22 15 27 13 25 64 26 02	20 00 22 41 18 00 23 00 51 87 24 00 23 36 19 00 22 00 19 00 32 41 15 00	0.800 -0.312 1.556 1.087 0.308 0.833 3.425 0.263 2.500 3.000 -0.370 2.000	4.382 3.113 3.767 5.057 3.645 2.758 10.524 1.809 4.776 5.232 1.512 4.272	16.564 31.378 8.804 18.207 61.238 3.222 109.452 4.522 5.580 12.228 0.983 9.983		13.98 23.69 10.60	27.01	1-1 22 1-0 91 1-0 61 1-0 61 Add1 Add1 Add1
16	55 56 57 58 59 60 61 62 63	1318+447.50 1318+777.00 1319+013.80 1319+217.80 1319+993.20 1320+467.63 1320+696.50 1320+966.00 1321+100 1321+780 1322+222.80	1.22 1.22 1.22 1.22 1.22 0.91	x2 1-1.80x2.10 2-2.40x2.10 x2 1-1.80x2.00 2-3.00x2.80 2-2.60x2.00 1-1.25X1.00 x2	29.34 29.26 27.97 27.03 25.25 22.84 24.70 21.02 23.95 22.70 27.70 25.52		29.10 28.04 26.80 25.00 22.68 24.50 20.22 23.90 22.15 27.13 25.64	20 00 22 41 18 00 23 00 51 87 24 00 23 36 19 00 22 00 19 00 32 41	0.800 -0.312 1.556 1.087 0.308 0.833 3.425 0.263 2.500 3.000 -0.370	4 382 3.113 3.767 5.057 3.645 2.758 10.524 1.809 4.776 5.232 1.512	16.564 31.378 8.804 18.207 61.238 3.222 109.452 4.522 5.580 12.228		13.98 23.69 10.60	27.01	

App. 9.1-16

PK-10 (	(1/2)					LISI	OFG	ULVE	KIS						
	1,72		1			,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	T	LEWSTI	CLOPE			RD&	10	1	T
AREA	NO.	STATION	PIPE	BOX	ELEV.	FLOW	RT ELEV.	LENGTH (m)	SLOPE (%)	(m/s)	Q (m³/s)	SLOPE	(m <sup>3</sup> /s)	AD (m³/s)	REMARKS
									L			(m3/s)	(/////	furial	ļ
10-1	1	1324+120.11 1324+735	1.22		22.07 24.90		22.05	27.43	0.073	0.816	0.953		7.70	44.64	A
10-1	2	1325+016.00	1.22	x2 1.00X2.00	22.06		24.04 21.71	20.00 18.94	4.300 1.848	6.264 4.920	14.637 9.839	ł—	7.70	14.64	Popy
	3	1325+321.00	<b></b> -	1.50X1.80	20.95	- P2>	20.95	21.71	0.000	0.000	0.000	ì			
	4	1325+614.70		2.00X1.40	21.73		21.55	20.11	0.895	4.404	12 331		<del> </del>	-	
10-2	5	1325+738.87	1.22		21.90	)>-	21.60	20.00	1.500	3.700	4.323	ł	29.60	43.52	1-0.61
	- 6	1325+960.00		2-1.80X1.80	22.45		22.32	17.01	0.764	4.147	26.870				
10-3	7	1326+055.00	1.52	x2	23.60	<b>&gt;</b>	23.40	20.00	1.000	3.498	12.687	0.054	15.55	21.33	2-0.61
10-4	8	1326+179.70 1326+419.30	1.22	x2 2-1-25X1.60	24.40 24.57		24.10 23.56	20.00	1.500 3.676	3.700 7.660	8.645 34.472	0.054	27.45	34.47	1-0.61
	10	1326+618.55	1 22	x2	27.00		26.24	20.00	3.800	5.888	13.760	0.043	27.43	34,47	1-0.61
	11	1326+698.70	1.22	<u></u>	27.70	••••	26.50	20.00	6.000	7.399	8.645	i .			1-0.61
	12	1326+804.87	<b> </b>	1.50X1.00	27.01		26.96	28.90	0.173	1.576	2.364	j	1	ļ	
10-5	13	1326+893.00		1.50X1.40	26.33		26.10	20.40	1.127	4.390	9.219	1	33.80	50.17	Ì
	14	1327+022 50	1.22		30.70		29.93	16.00	4.813	6.627	7.743	0.057			1-0.61
j j	15	1327+137.50	1.22		32.30		32.00	20.00	1.500	3.700	4.323	0.038	]		1-0.61
10-6	16 17	1327+225.00 1327+405.50	0.91	2242242	35.20		34.03	18.00	6.500	6.334	4.118	0.000			1-0.61
10-5	18	1327+582.50	<b></b>	2-2.40x2.40 1.80X1.20	29.13 27.62	<b> &gt;</b>	28.85 27.22	16.00	1.750 2.069	7.600 6.155	87.554 13.295	0.092 0.116	53.99	87.55	1-1.3x1.0
[` <u>`</u>	19	1327+789.30	<b> </b>	2-1.50x1.25	26.01		25.50	16.00	3 206	7.203	27.013	0.116	20.11	40.31	1 0 61
	20	1327+853.00	1.22		24.50		23.70	19.00	4.200	6.191	7.233	0.123	f		1-0.61
10-8	21	1328+056.67	1.22		25.08	<b>p</b> -	24.17	22.38	4.068	6.091	7.117	1	19.18	33.00	
	22	1328+116.70	1.22		24.59		23.74	23.63	3.588	5.722	6.686	0.134			10
l	23	1328+315.23	1.22	ļ	29.80	- 🍋	27.04	24 00	11.500	10.244	11.969	0.021	<u> </u>		1-0.61
	24	1328+364.50	1.22		29.80		28.92	22.00	4.000	6.041	14.118				1-0.91
10-9	25	1328+627.10	1.22		24.17	· 🌬	22 80	22.59	6.065	7.439	8.692	0.211			
10-9		1328+740	1.22		23.50 23.50		23.05 23.08	15.00 14.00	3.000	5.232	6.113	0.036	29.05	37.69	Addi
	26	1328+791.17	1.22		22.46		22.30	28.19	3.000 0.568	5.232 2.276	6.113 2.659			1.00	Add'l
	27	1329+209.97	1.22	x2	26 60		24.60	25.00	8.000	8.544	19.965	0.091	<del> </del>		1-0.91
10-10	28	1329+270 27	1.22	x2	23.80	- · - Bo-	23.40	22 00	1.818	4.073	9.518	}	105.39	140.95	1-0.61
	29	1329+352.47		2-3.00x2.40	21.90	<b>b-</b> -	21.66	16.00	1.500	7.741	111.456	1			1-0.61
	30	1329+607.56	1.22		22.30	4	21.73	19.00	3.000	5.232	6.113				1-0.61
10-11	31	1329+753.68		2-2.40x1.80	21.70	<b>b</b>	21.43	15.00	1.800	7.185	62.079	]	58.60	75.14	1-0.91
10-12	32	1330+092.6 1330+352.70	1 22	1-1.20X1.20	23.90		23.55	19.71	1.776	4.823	6.945				
10-12	34	1330+669.50	1.22	x2	25.68		25.86 25.30	16.00 16.00	2.400	3.058 4.680	7.146 5.468	4	9.40	1261	1-0.61
		1331+125	0.61	]	27.01		26.92	16.40	0.549	1,410	0.412	<del> </del>	<b> </b> -	ļ	1-0.61
	35	1331+370.60	1.22		27.53		27.34	21.55	1.160	3.254	3.802		[		<b>!</b>
Ę	36	1331+776.70	0.61		29.94		29.34	17.63	3,403	3.510	1.025		1	·	<del></del>
1.0	37	1331+956.80	0.91		29.35	>	29.30	21.92	0.228	1.186	0.771	0.035			
[ : ]	38	1332+074.11	1.22		28.77	—- <b>b</b> -	28.10	19.94	3.360	5.537	6.469	0.050	[	ĺ	
	39	1332+210.00	L	1.50X1.80	21.60		21.25	23.04	1.519	5.377	14.518				
10-13	40	1332+353.80	1.22		21.95	<b>b</b> -	21.45	21.57	2.318	3.782	2.459	0.110	40.79	59.36	
	43	1332+746.80	122	2.00X2.00	19.61	<b>3</b> to-	20.15 19.45	17.00 18.53	0.882 0.864	2.837 4.728	3.315 18.912	0.090	<b>.</b>		1-0.61
	44	1332+927.50		1.80X1.20	19.55		19.45	17.88	0.559	3.200	6.913			-	
,	45	1333+139.04	<u> </u>	1.80X1.20	20.62	<b>R</b>	20.55	16.60	0.422	2.779	6.002				
	46	1333+422.94	0.91		24.27		24.15	21.73	0.552	1.846	1.200			7	
	476	±13331719.00	0.81	134467634	24.84	1	24.44	A VANCAS	抽機	0.000	4 0 COO /	14.25	13/4°4	Box (1)	DELETE
10-14	48	1334+126.75		1-3.00X1.80	22.89		22 73	37 26	0.429	3.822	41.275		40.40	41.28	
}	<u> </u>	1334+800	1.22	1-2.40X1.80								<u> </u>	<b> </b> -		
10-15	49	1335+014.00		x2 x2	19.60 19.10	<b>B</b> >-	19.04 17.10	16.00 20.00	3.500 10.000	5.651 9.552	13.206	0.238	27.24	49.72	Add')
13	73	1335+140	·	x2	18.90		18.34	16.00	3.500	5.651	22.322 13.206	0.239	27.64	48.73	1-0.61 Add1
10-16	50	1335+422.40		1/2	19.00		18.46	18.00	3.000	5.232	12 226	0.056	16.81	24.45	1-0.61
		1335+580.00		72	19.60		19.12	16.00	3.000	5.232	12.226	0.253	'''	14.40	Addil
	51	1335+737.00	1.22	x2	20.70	<b>p</b>	19.89	18.00	4.500	6.408	14.974	0.053	t		1-0.91
10-17	52	1335+815.60		2.50X1.50	19.91	- · · - <b>b</b> :-	19.58	20.79	1.588	6.507	24.402		39.15	50.54	J
	53	1336+168.90	1.22	x2	19.00	· <b>D</b>	18.55	18.00	2.500	4.776	11.161		L		1-0.91
10-18	54	1336+388.40		2-1.80X1.20	17.95		17.54	21.09	1.944	5.967	25.775		33.60	44.59	
<b> </b>		1336+420	<u> </u>	1-1.80x1.80	19.10	<b>k</b> >	18.89	14.00	1.500	5.808	18.819		<u>                                     </u>		AddT
	55	1336+831.50	1.22		20.11		19.60	18.58	2.748	5.007	5.851		<b>i</b> 1		1-0.91
	_56 57	1336+921.20 1337+088.60	1.22		19.80 19.80	<u> </u>	19.58	20.00 18.00	1.100 3.500	3.168 5.651	3.702 6.603		'		1-0.61 1-0.91
10-19	58	1337+291.00	1.22		19.30	- 1	18.58	17.71	4.092	6.103	7.131	0.308	31.74	42.21	1-0.91
J'' ''	59	1337+491.60	0.91		23.29		22.45	20.56	4.037	4.992	3.245	<b>9.500</b>	37.14	74.61	1-0.91
1	60	1337+530.50	1.22		22.00	}>>-	20.90	17.00	6,500	7.701	8.998	0.030			1-0.61
i	61	1337+599.50	1.22		20.59	<b>)</b>	20.02	16.00	3.588	5.721	6.685				1-0.61
American American		and the second second		A CONTRACTOR OF THE PROPERTY O	A THE RESERVE		**************************************							Name and Address of the Owner, where the Owner, which is	

PK-10 (	(2/2)					LIŞI	OFC	ULVE	RTS						
					LT	-	RT	LENGTH	SLOPE	v	Q	RD &	τD	AD	
AREA	NO.	STATION	PIPE	BOX	ELEV.	FLOW	ELEV.	(m)	(%)	(m/s)	(m³/s)	SLOPE	(m³/s)	(m³/s)	REMARKS
												(m3/s)	(11.70)	(1117)	
40.00	62	1337+730.25	4.00	2-2.40x2.40	17.90		17.42	16.00	3.000	9.951	114.634	0.118			1-0.91
10-20	63	1337+809.40	1.22	0.0.4070.00	17.90	🌬	17.70	19.73	1.014	3.041	3.554		112.83	150.68	·
	64 65	1337+851.05 1338+021.85	1.22	2-2 40X2 00	17.59	·· <b>j</b> s	17.53	15.86	0.378	3.385	32.492	0.109			
10-21	66	1338+178.85	0.91		18.62 19.20		17.81 18.35	19.00	4.263 3.438	6 237 4 606	7.287 2.994	0.096 0.339	24.94	37.07	1-0.61
	67	1338+566.94		1.80X1.80	20.70		20.03	24.73 22.04	3.040	8.268	26.789	0.333	24.94	37.07	
	68	1338+769.55	1.22		20.86		20.73	27.58	0.471	2.074	2.423	0.317	·		
10-22	69	1338+978.94		×2	20.80		19.96	21.00	4.000	6.041	14.118	0.094	19.94	25.32	1-0.61
	70	1339+065.30	1.22	x2	19.24		18.90	22.00	1.545	3.755	8.775	0.031			1-1.22
	71	1339+307.50		1.20X1.00	18.31		17.91	20.63	1.939	4.827	5.793	0.188			
10-23	72	1339+555.50	1.22	x2	17.30	·· 📂-	16.49	18.00	4.500	6.408	14.974	0.330	23.08	28.97	1-0.91
	73	1339+797.00	1.22	x2	17.69		17.42	20.00	1.350	3.510	8 202	0.163			1-1.22
10-24	74	1340+069.50	1.22		16.10	🌬	15.74	24.00	1.500	3.700	4.323	0.124	11.22	16.55	1-0.91
10-25	75 278	1340+209.05	1.22	x2	15.90	<b>b</b> >	15.18	24.00	3.000	5.232	12 226	www.	Construction of	Participants (E)	1-0.91
10-23	77	1340+608.85 1340+723.00	1.22	0.000	20.25		<b>N</b>	3,6,65	42.402	0000	0 000	0.018	27.85	<b>3.127</b>	DELETE
10-26	78	1340+916.00	1.22	1-1.80x1.80	20.25 16.71		17.36 16.20	22.00 27.00	13.123	10.943	12.785	0.060	7.34	12.79	1-0.91
10-27	79	1341+325.40		2-2 50X2 20	15.84		15.70	27.69	0.506	6.505 4.075	21.077 44.829	0.141	14.94 69.10	21.08 107.87	1-1-22
		1341+360		2-2 50X2 20	18.80		18.64	16.00	1.000	5.731	63.044		09.10	107.07	Addil
	80	1341+756.50	0.61		19.01	<b>44</b>	19.46	28.00	-1.607	2.413	0.705		<b></b>		7001
10-28	81	1342+025.20	0.91		23.60		23.15	38.63	1.165	2.632	1.743	0.061	5.90	6.35	- <del></del>
	82	1342+135.10	0.61		29.60		27.23	23.99	9.878	5.981	1.747	0.050			
	83	1342+233.05	0.91		30.13		29.60	29.38	1.804	3.337	2.169				
	84	1342+461.10	0.91		30.78	— <b>&gt;</b>	29.66	37.25	2.953	4 270	2.775				
10-29	85	1342+563.15	0.61		29.09		27.92	25.73	4.548	4.058	1.185		15.30	26.07	
	86 87	1343+018.15 1343+242.80		2.40X1.80	16.85		16.68	18.62	0.913	5.118	22.109	·			
٠.	88	1343+751.05	0.61	1.80X1.90	17.28 18.72	· · · · >	17.18 18.59	17.65	0.567	3.612	12.354		+		
	89	1343+962.35	0.91		18.06		17.82	20.84	0.524 1.193	1.503 2.714	0.439 1.764				
	90	1344+013.50	0.91		18.67		18.45	17.57	1.252	2.780	1.807	14			<b></b>
	91	1344+115.20	0.91	<del> </del>	18.72	4	18.88	18.51	-0.864	2.310	1.502				1.5
10-30	92	1344+508.75	0.61		21.10	<b>-4</b>	21.71	30.13	-2.024	2.707	0.791		21.90	28.75	
	93	1344+670.70		1-1.80x1.80	19.90	🗫	19.20	20.00	3.500	8.872	28.747	1 1			1-0.91
		1344+720	1.22	1	20.10		19.86	16.00	1.500	3.700	4.323				Addi
40.54	94	1344+796.10		1.80X2.00	18.80	>	18.55	23.25	1.075	5.031	18.110	_	1.5		
10-31	95 98	1345+017.35	0.61	ertar erenem	32.16		33.36	22.12	-5.425	4.432	1 295	THE THE ENGINEERS	17.40	22,43	
	97	1345+168,75 1345+864,30	30.91 0.61	100.00	24.45	4	3333	1000	X (4)	0.000	0.000	2048 R		2000	DELETE
10-32	98	1345+987.50	1.22	x2	21.38	<b> &gt;-</b>	23.72	23.33 18.00	3.129 2.272	3.366 4.553	0.983				4001
17,17	100	1346+068.00	1.22	x2	21.45		20.75	16.00	4.375	6.318	10.640 14.764		14.80	26.39	1-0.61
	101	1346+323.40		2-3.00X3.00	20.33		19.80	17.14	3.092	11.723	211.021			<b> </b>	1-0.61
	102	1346+372.20	0.91		20.57		20.30	22.14	1.220	2.744	1.784	1.3		159	
	103	1346+661.30		2.40X2.40	20.05		19.90	17.27	0.868	5.354	30.838			5.4	
	<u> </u>	1346170876	0.61	200 2012	. 20.85		20.79	373.57	3.54	0.000	0 000	3 (31)	40 B	MAK	SCHAMA
		1346+955	0.61		22.75		22.50	19.00	1.318	2.183	0.638	AS A PART AND A CO.	S. P. S.	WENT SHEET IN	
-	105	1347+227.80		3.00X3.00	20.88	⊳	20.45		1.663	8.596	77.367	4.5			-
10-33	105	1347+522.10 1347+938.50	1.22	ļ <u>.</u>	21.62		21.50	24.66	0.487	2.107	2.462				
10-33	107 109	1347+938.50	1.52	x2 x2	22.80 21.80	-	22.00	23.00	3.478	6.523	23.661		17.40	23,66	1-0.61
	111	1348+453.00	0.91	- <del>-</del>	22.00	J>-	21.70	17.00 20.00	0.588 1.500	2317	5.414				2-0.61
10-34	112	1348+592.40		3.00X2.40	20.93	-	20.91	19.94	0.100	3.043 2.002	1.978 14.413	·	24.00	38.00	1-0.61
	113	1348+676.15	0.91		21.40		20.40	20.00	5.000	5.555	3.611		24.00	36.00	1-0.61
	114	1348+771.50	1.22	f	20.70		20.54	16.00	1.000	3.021	3.529				1-0.61
		1348+860.00	1.22	x2	21.00		20.84	16.00	1.000	3.021	7.059				Addil
	113	3348+884.00	1.22	12		***		31.2	14 A		0.000	1034	12027		Kiðis
				A STATE OF THE REAL PROPERTY.			Particular dise			te of morning					

AREA	NO.	STATION	PiPE	вох	LT	FLOW	RT ELEV.	LENGTH (m)	GRADE (%)	V (m/s)	Q (m³/s)	RD & SLOPE	TD (m³/s)	AD (m³/s)	REMA
	<b>41</b>	1349+183.20	1.22	enduckter	ELEV.	6- P	STUMBER ST		§1.000	3.021	3.629	(m3/s)		12 12 A	SOEL
11-1	2	1349+360.50		x5	21.90	<b>-</b> -	21.50	23.00	1.739	3.984	9.309	emi.	16.80		
''''	3	1349+623.80		x2	21.00	\$30	20.20	20.00	4.000	6.041	14.118		10.00	20.45	1-0.
11-2	4	1349+939.00		1-2.40x1.80			18.25	18.00	1.389	6.311	27.266	<del> </del> -	24.96	28.96	
````}	5	1349+944.00	0.91		18.56		18.29	24.48	1.103	2.609	1.696	0.164		-	}
}	6	1350+309.50			22.63		22.10	17.57	3.017	3.305	0.965	0.092			<u> </u>
Ì	7	1350+497.50			22.01		21.71	21.21	1.414	2.263	0.661		1		
11-3	8	1350+534.50		3.00X3.00	19.89		19.69	20.24	0.988	6.627	59.643	i .	16.16	68.08	
į	9	1350+623.80	0.61		21.28	🗠	20.94	26.71	1.273	2.147	0.627	i			
ľ	10	1350+727.00	0.91		22.60		22.05	19.00	2.895	4.227	2.748	0.064		[	1-0.
1	11	1350+878.00	1.22		22.04	··· 🗫	21.80	25.38	0.946	2.937	3.432		'		
11-4	12	1350+947.00		2-2.40x2.40	22.58		22.42	17.50	0.914	5.493	63.284		28.90	63.28	1.0.
$\neg \neg$	13	1351+183.50	0.91		21.57		21.41	26.10	0.613	1.945	1.265	0.137		1	
11-5	14	1351+207.00	0.91		21.30	- 10>	21.67	19.98	-1.852	3.381	2.198	1	22.90	31.32	
[	15	1351+239.00			22.00		21.30	23.00	3.043	5.270	12.314	0.03			1-0.
(	16	1351+386.00		x2	20.30		20.15	21.00	0.714	2.553	5.966	0.03	1		1-0.
[	17	1351+430.30		x2	21.18	<b>j</b> s.	20.72	25.00	1.840	4.097	9.575	<u> </u>	<u>L_</u> .		1-0.
1	18	1351+637,10	0.91		19.80	Dec	19.75	24.59	0.203	1.120	0.728				
11-6	19	1352+132.50			20.36		19.82	25.62	2.108	2.763	0.807	]	10.40	15.91	
[	20	1352+461.00		x2	23.70	~ <b>t</b> s=-	22.95	21.00	3.571	5.709	13.340	0.195			1-0
ſ		1352+730.50			25.73	·	24.73	28.66	3.489	3.555	1.038		L	L ;	
11-7	22	1352+920.00		x2	25.71	··· <b>P</b>	25.40	24.00	1.292	3.975	14.419	]	13.18	21.48	1-0.
	23	1353+075.00	1.22	X2	25.60	···	25.41	19.00	1.000	3.021	7.059	0.08	L	<u>L</u>	1-0.
		1353+220		2-1.25X1.0	24.75		24.50	15.00	1.667	4.552	11.380				Ado
11-8 [		1353+390	•	2-1.80x1.5	24.20		23.90	13.50	2.222	7.913	42.732	1	59,50	59.61	Ado
	24	1353+391.00		x2	24.58		24.03	19.00	2.895	4.227	5.496	<b>l</b> '			1-0.
11-9	25	1353+451.70		x2	23.80		23.55	18.00	1.389	3.560	8.319		15.50	16.37	1-0.
	26	1353+604.30		x2	23.64	🗫	23.38	20.00	1.300	3.444	8.048	]		100	1-1.22
	27	1353+988.40	1.22	x2	22.82		22.65	17.00	1.000	3.021	7.059				1-0.
[		1354+020	0.91	x2	23.20		23.60	15.00	1.333	2.869	3.730	1	100		Add
11-10	28	1354+174.00	0.61		23.37		23.35	17.65	0.113	0.641	0.374	]	42.30	49.83	
Į	29	1354+181.50		1-1.20X1.2	23.19		22.81	20.20	1.881	4.964	7.148	}			
1	<u> </u>	1354+340		2-1.80x1.25	22.90	🌭	22.60	16.50	1.818	5.837	31.521	1			Add
1	30	1354+413.60		x2	22.71		22.47	16.00	1.500	3.700	8.645				1-0.
11-11	31	1354+520,40	0.61		学(学家)	84	1.4	23,61	0.000	0,000	0,000	343	26 F. Y.		F DEL
[	32	1354+573.90		x2	19.50	🕪	18.40	28.00	3.929	5.987	13.991		13.20	25.92	
	33	1354+729.30			22.39		22.20	21.92	0.867	2.812	3 286	<b>]</b>		,	
- 1	34	1355+212.00		2.40x2.40	21.17		21.03	32.10	0.436	3.794	21.854			4	
. 1	35	1355+259.00			21.43	<b>j</b> te-	20.61	29.62	2.768	5.026	5.872	]	i '		
· l	36	1355+535.50		1. 1.	22.58		22.19	20.42	1.910	3.433	2.232	}	ł	1	
ļ	37	1355+655.00			22.70	· 🌬	22.58	19.00	0.632	2.401	2.805	]	l '		1-0.
ļ	38	1356+254.00			23.1	🕦	22.90	21.09	0.948	1.853	0.541	]	* +		
İ	39	1356+368.00		2.40x2.40	20.88	-4 -	21.02	23.48		4.743	27.317				
J		1356+574.40			22.00	<b>J</b> B	21.79	34.87	0.602	1.928	1.253	]	J '	]	
ļ		1356+624.00		2. S. S.	21.69		21.89	26.06	-0.767	1.667	0.487	] .			
ļ		1356+792.60			21.59		21.21	25.27	1.504	3.704	4.328				
- 1	43	1357+302.40			22.73		22,44	22.58	1.284	2.816	1.830	]		l	
		13577694.00		3.20x1.00	23.15	+4.	22,80	20,03		4,583		41.75%	WANT.	特級亞	\$ X NI
ļ		1357+858.40		4 1 1	24.75	<b>B</b>	24.59	19.63	0.815	1.718	0.502	[	[		
. [		1358+002.80			24.25	<b>-∞</b>	24.27	21.01	-0.095	0.587	0.171				
· [		1358+159.00			24.42	· · ·   <b>b</b> b>-	24.43	18.08	-0.055	0.448	0.131				
, 1		13581652,80		30 PM	25.25	N E	2.00 62	<b>17.21</b>	2000	(0,000)	0.000	多数對	到资金	2377	<b>OEL</b>
1		1358+851.70		ļ	23.21		24.17	23.73		3.827	1.118	<b>!</b>		[	<u> </u>
		1359+068.90			23.10		24.28		-4.646	6.511	7.607	[		·	
-		1359+546.00			24.45		24.40	26.00	0.192	1.325	1.548	[	· ·	l	<u></u>
	52	1359+610.00		2-2.60X2.4	23.89	-	23.91	18.32		1.966	24.536	Į į		l	ļ
. ,	1000	1359+660.00		Single Street in	24.90		25.10	17.00		عدم د جنوبي		940 mercan	www.arma.arma.arma.arma.arma.arma.arma.a	green transcomment	Add
}		1359+709.20			14.			16.78	0.000	0.000		<b>300</b>	A Section	ARY.	OEL
}	54	1359+953.00		0.0	25.82	<b>▼</b>	26.28	16.25	-2.831	3.202	0.935				
١	55	1360+495.70		2-2.40X2.4	20.23	◀	20.29	19.57	-0.307	3.181	36.647				
1		1360+754.70			23,59		23.64	21.90	-0.228	1.443	1.686	<u> </u>	,	]	
· · · [		1360+804.52			23.27		23.32	25.34		1.342	1.568	<b>?</b>		ľ	
ļ		1361+090.90		2.40x2.40	23.04		23.15	20.71	-0.531	4.187	24.117	Į I		ł	L
, Į		1361+156.50		2.40x2.40	23.27	- <b>}</b> ~	23.14	22.45		4.372	25.182				
ļ		1362+036.30			27.09		27.24	18.81	-0.797	1.699	0.496		LONG MOXING	Mar was her are	
l		13621976.30	0.61	1918/1919	26.87	4	-26.89		080.0	0.638	0.157		多形形	数则是	S NU
. [		1363+278.00		3.00x3.00	24.94	-≪1 -	25.44	18.10	-2.762		99.723				
. [		1363+424.90		3.00x2.40	25.92	<b>D</b> >	25.90	19.01	0.105	2.050	14.760				
. [		1363+602.30		3.00x3.00	24.57	-4	24.62	19.43		3.382	30.437	Į ļ		١ '	
ſ	65	1363+703.00		3.00x3.00	24.87	-4	24.91	19.81	-0.202	2.996	26.961	<u> </u>			
-								9.1-							

PACKAGE-12

AREA NO STATION PIPE BOX ELV FLOW RT LENGTH GRADE V Q Q ROS SLOPE (170) A (170) SLOPE (170) A (170) SLOPE (170) A (170) SLOPE (170) A (170) SLOPE (170) A (170) SLOPE (170) A (170) SLOPE (170) A (170) SLOPE (170) A (170) SLOPE (170) A (170) SLOPE (170) A (170) SLOPE (170) A (170) SLOPE (170) A (170) SLOPE (170) A (170) SLOPE (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A (170) A		· · ·		-							-					
AFEA NO	1					ŧΤ	i	ŔĨ	LENGTH	GRADE	l v i	n		TO	Δn	1
1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.061   1.06	AREA	NO.	STATION	PIPE	вох		FLOW									REMARKS
2   1364-163 80								LLL.	(13)	- •	fire?}	finis)	(m3/s)		furist	1 1
2   1364-163 80		3.13	1364+086 20	3.00 A.	1-2008240	28.76		26.69	13 H.E	10 ST	0.000	\$ 0.000 P		3 6 6	V.Yeer	SENASS.
3   1884-482 00   122   25.55   22.29   0.124   1.063   1.242     4   1864-893 00   61   28.64   27.29   23.30   25.69   31.00   0.000     5   1864-893 00   61   28.64   28.05   23.50   0.511   22.55   0.951     6   1836-1985 0   61   28.64   28.05   23.50   0.511   22.55   0.951     7   1355-1965 0   61   28.64   28.52   20.44   1.566   2.381   0.695     8   1885-191 30   1.300-130   27.74   27.70   27.70   1.40   1.056   6.940   6.55     9   1386-1172 50   172   27.00   27.30   20.72   1.400   35.44   4.175     10   1386-1965 0   172   27.00   27.30   20.72   1.400   35.44   4.175     11   1866-1961 0   172   1.1251(1.0) 34.4   30.65   19.00   1.105   3.007   4.533     12   1877-1970   1.1251(1.0) 34.4   30.65   19.00   1.105   3.007   3.566     13   1837-18070   1.72   32.32   4.524   3.085   19.00   1.105   3.007   3.566     14   1836-1965 0   61   35.27   4.533   3.607   3.566     15   1836-1965 0   61   35.27   4.533   3.607   3.566     16   1836-1965 0   61   3.527   4.533   3.607   3.566     16   1836-1965 0   6.81   3.527   4.533   3.607   3.566     17   1839-195 0   6.81   3.528   3.528   3.528   3.528   3.529   3.600     18   1836-195 0   6.91   3.728   4.335   3.565   3.291   3.600   3.600   3.600   3.600   3.600   3.600   3.600   3.600   3.600   3.600   3.600   3.600   3.600   3.600   3.600   3.600   3.600   3.600   3.600   3.600   3.600   3.600   3.600   3.600   3.600   3.600   3.600   3.600   3.600   3.600   3.600   3.600   3.600   3.600   3.600   3.600   3.600   3.600   3.600   3.600   3.600   3.600   3.600   3.600   3.600   3.600   3.600   3.600   3.600   3.600   3.600   3.600   3.600   3.600   3.600   3.600   3.600   3.600   3.600   3.600   3.600   3.600   3.600   3.600   3.600   3.600   3.600   3.600   3.600   3.600   3.600   3.600   3.600   3.600   3.600   3.600   3.600   3.600   3.600   3.600   3.600   3.600   3.600   3.600   3.600   3.600   3.600   3.600   3.600   3.600   3.600   3.600   3.600   3.600   3.600   3.600   3.600   3.600   3.600   3.600   3.600   3.600   3.600   3.600   3.600	l .	_	1364+183 80		1-3.00X3.00			24.74	1931			85,269			.52 35,042	
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6   1965/1965/0   061   29.00     29.00     28.00   29.64   29.55   32/12   0.055       8   1985/1965/0   101   2010   27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.07     27.0				<u> </u>	1-0-6010-60	· · · · — · · · · · · · · · · · · · · ·									·	
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15   1585165280   061		13	1367+680.70	1.22		32.32	<b>-</b>	32.64	30.83	-1.038	3.077	3.596				
16   15691/25650   061		14	1368+080.50	0.61	100	35.27	<b>~≪</b> · · · — ·	35.45	23.68	3.463	3.541	1.034				
16   15991/265/50   061		15	1368+682.80		1-1.40x1.20	31.63		31.78	26.39	-0.558	2.917	4.900				
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17   1389+507-80   091   37.78   38.73   46.83   -1.452   2294   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968   1968	1	18A	19691430.00	6.6.0	10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO	23.5		0.00	63 353	33.4	0.000	₹0,000 3	1.3	6.2.3	X37.44	<b>CAPITES</b>
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29   1371+788 60   091		27	1371+352.90	0.61		58.32	· Þ	58.10	28.39	0.778	1.679	0.490				
30   1371+883.50   0.61   63.77		28	1371+495.00		1-1.60X1.30	56.72	<b>&gt;</b>	56.13	39.99	1.475	5.069	10.543		500	1.0	
30   1371+833.50   0.61   63.77		29	1371+788.60	0.91		64.20		63.35	41.19	2.064	3.569	2.320				
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38   1373+715.40   0.91   38.85   39.44   32.11   -1.837   3.358   2.169     39   1373+813.00   1.22   ×2   37.66													1.1	4.4	+ 7	
39   1373+813.00   1.22   x2   37.66   → ▶ 37.28   26.76   2.167   4.447   5.196     12-1   41   1373+995.60   0.91   38.03   → ▶ 37.46   27.15   2.099   3.600   2.340     42   1374+016.20   0.91   38.20   → ▶ 37.63   27.14   2.100   3.600   2.341   0.21     43   1374+244.20   1.22   44.80   →   44.00   22.00   3.636   5.760   6.730     44   1374+325.00   1.22   x2   44.75   →   43.88   38.00   2.289   4.571   10.681     45   1374+537.00   1.22   41.70   →   41.38   28.00   1.500   3.700   4.323     12-2   46   1374+796.50   0.61   47.44	<u> </u>				ļ											
12-1 41 1373+996.60 0.91 38.03 → 37.46 27.15 2.099 3.600 2.340 42 1374+016.20 0.91 38.03 → 37.63 27.14 2.100 3.600 2.341 0.21 374+24.20 1.22 44.80 → 44.00 22.00 3.636 5.760 6.730 1.0.61 44 1374+325.00 1.22 x2 44.75 → 43.88 38.00 2.289 4.571 10.681 45 1374+537.00 1.22 41.70 → 41.38 28.00 1.500 3.700 4.323 1.0.91 1.0.61 4.56 4.7 1374+99.60 0.61 47.44 ← 48.37 20.85 4.460 4.019 1.174 0.054 16.7 23.5 48 1375+189.00 1.22 x2 56.80 → 52.49 33.04 -1.967 4.237 4.950 4.9 1375+265.50 1.22 x2 56.80 → 53.00 26.00 6.769 7.256 8.477 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0.61 1.0						<del></del>										
42       1374+016 20       0.91       38 20       →       37.63       27.14       2.100       3.600       2.341       0.21         43       1374+244 20       1.22       44.80       →       44.00       22.00       3.636       5.760       6.730       1.061         44       1374+325.00       1.22       x2       44.75       →       43.88       38.00       2.289       4.571       10.681       1.061         45       1374+537.00       1.22       41.70       →       41.38       28.00       1.500       3.700       4.323       10.61         47       1374+899.60       0.61       47.44       →       48.37       20.85       -4.450       4.019       1.174       0.054       16.7       23.5         47       1374+899.60       0.61       44.56       →       -41.58       34.67       -0.057       0.456       0.133       0.202         48       1375+189.00       1.22       51.84       →       -52.49       30.04       -1.967       42.37       4.950         49       1375+265.50       1.22       x2       56.80       →       55.30       50.00       5.769       7.256       8.477       1.061	l :				)/2	<del></del>			·					- 1		10.1
43 1374+244.20 1.22 44.80 -▶ 44.00 22.00 3.636 5.760 6.730 1.0.61  44 1374+325.00 1.22 x2 44.75 -▶ 43.88 38.00 2.289 4.571 10.681  45 1374+537.00 1.22 41.70 -▶ 41.38 28.00 1.500 3.700 4.323  12-2 46 1374+796.50 0.61 47.44 - 48.37 20.85 4.450 4.019 1.174 0.054 16.7 23.5  47 1374+899.60 0.61 44.56 - 41.58 34.67 -0.057 0.456 0.133 0.202  48 1375+189.00 1.22 51.84 - 52.49 33.04 -1.967 4.237 4.950  49 1375+265.50 1.22 x2 56.80 -▶ 55.30 26.00 5.769 7.256 8.477  12-3 50 1375+734.30 0.91 67.67 - 68.94 22.23 5.713 5.938 3.860 28.1 103.1  12-4 54 1376+203.70 1.22 x2 69.00 - 69.35 28.00 -1.346 3.505 8.190 1.0.61  12-6 54 1376+203.70 1.22 x2 56.00 - 69.35 28.00 -1.346 3.505 8.190 1.0.61  12-8 54 1376+456.60 1.22 x2 56.00 - 69.35 28.00 -1.346 3.505 8.190 1.0.61	12-1						📂				3.600	2.340		15.2	16.6	
44   1374+325.00   1.22   x2   44.75	]				<u> </u>	38 20		37.63	27.14	2.100	3.600	2 341	. 0.21			
44       1374+325.00       1.22       x2       44.75       → 43.88       38.00       2.289       4.571       10.681       10.681       10.61       10.61       10.61       10.61       10.61       10.61       10.61       10.61       10.61       10.61       10.61       10.61       10.61       10.61       10.61       10.61       10.61       10.61       10.61       10.61       10.61       10.61       10.61       10.61       10.61       10.61       10.61       10.61       10.61       10.61       10.61       10.61       10.61       10.61       10.61       10.61       10.61       10.61       10.61       10.61       10.61       10.61       10.61       10.61       10.61       10.61       10.61       10.61       10.61       10.61       10.61       10.61       10.61       10.61       10.61       10.61       10.61       10.61       10.61       10.61       10.61       10.61       10.61       10.61       10.61       10.61       10.61       10.61       10.61       10.61       10.61       10.61       10.61       10.61       10.61       10.61       10.61       10.61       10.61       10.61       10.61       10.61       10.61       10.61       10.61	L	43		1.22		44.80		44.00	22.00	3.636	5.760	6.730		:		1-0.61
45   1374+537.00   1.22   41.70		44	1374+325.00	1.22	x2	44.75	· <b>B&gt;</b>	43.88	38.00	2 289	4.571	10.681				
12-2 46 1374+796.50 061 47.44 4 48.37 20.85 4.450 4.019 1.174 0.054 16.7 23.5 47 1374+899.60 061 44.56 4 52.49 33.04 -1.967 4.237 4.950 2.02 48 1375+189.00 1.22 51.84 4 52.49 33.04 -1.967 4.237 4.950 2.02 2.02 2.02 2.02 2.02 2.02 2.02 2.	]	45	1374+537.00	1.22		41.70		41.38	28.00					1		
47       1374+899 60       0.61       44.56       -       44.58       34.67       -0.057       0.456       0.133       0.202         48       1375+189.00       1.22       51.84       -       52.49       33.04       -1.967       4.237       4.950         49       1375+265.50       1.22       x2       56.80       -       -       55.30       26.00       6.769       7.256       8.477       1.0.61         12-3       50       1375+734.30       0.91       67.67       -       -       68.94       22.23       -5.713       5.938       3.860       28.1       103.1         51       1376+036.60       2.240x2.40       77.15       -       -       77.60       20.00       -2.250       8.618       99.276       1.0.61         53       1376+203.70       1.22       x2       69.00       -       69.35       28.00       -1.346       3.505       8.190       1.0.61         12-4       54       1376+456.60       1.22       x2       61.00       -       62.00       32.00       -2.300       4.581       10.705       0.121       19.6       19.8       1.0.91	12-2	46	1374+796.50		<b> </b>								0.054	16.7	23.5	
48 1375+189.00 1 22 51.84 ← 52.49 33.04 -1.967 4.237 4.950 49 1375+265.50 1.22 x2 56.80 ← 55.30 26.00 6.769 7.256 8.477 10.61  12-3 50 1375+734.30 0.91 67.67 ← 68.94 22.23 -5.713 5.938 3.860 28.1 103.1  51 1376+036.60 2-2.40x2.40 77.15 ← 77.60 20.00 -2.250 8.618 99.276 10.61  53 1376+203.70 1.22 x2 69.00 ← 69.35 28.00 -1.346 3.505 8.190 10.61  12-4 54 1376+456.60 1.22 x2 61.00 ← 62.00 32.00 -2.300 4.581 10.705 0.121 19.6 19.8 10.91					<u> </u>				<u></u>						20,0	
49       1375+265.50       1.22       x2       56.80       → 55.30       26.00       6.769       7.256       8.477       1.061         12-3       50       1375+734.30       0.91       67.67       -4       68.94       22.23       -5.713       5.938       3.860       28.1       103.1         51       1376+036.60       2-2.40×2.40       77.15       -4       -77.60       20.00       -2.250       8.618       99.276       1.061         53       1376+203.70       1.22       ×2       69.00       -4       -69.35       28.00       -1.346       3.505       8.190       1.0.61         12-4       54       1376+456.60       1.22       ×2       61.00       -4       -62.00       32.00       -2.300       4.581       10.705       0.121       19.6       19.8       1.0.91					h		£						V 202	)		
12-3 50 1375+734.30 0.91 67.67 4 - 68.94 22.23 5.713 5.938 3.860 28.1 103.1 51 1376+036.60 2-2.40x2.40 77.15 4 - 77.60 20.00 -2.250 8.618 99.276 1.0.61 53 1376+203.70 1.22 x2 69.00 4 - 69.35 28.00 1.346 3.505 8.190 12-4 54 1376+456.60 1.22 x2 61.00 4 - 62.00 32.00 -2.300 4.581 10.705 0.121 19.6 19.8 10.91	1				12		<del></del> -	<del></del> -	·							
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V. V. V. V. V. V. V. V. V. V. V. V. V. V																
[ 195   15107519.10   U91     150.45     60.53   25.09   -0.319   1.403   0.912   0.039	12-4				1×4									19.6	19.8	1.0.91
	L	25	13/6+3/9.70	0.91	]	60.45	14	60.53	25.09	-0.319	1.403	0.912	0.039			

March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   Marc	PX-13					-										
Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Section   Sect						LEFT		RIGHT	LENGTH	GRADE	v	٥	RD &	OT	άA	
15	AREA	NO.	STATION	PIPE	80X		FLOW				1		_	(m3/s)	(m³/s)	REMARKS
13			40		<u> </u>							l			1	ļ
13	13-1	1											0,120	9.58	13.79	4.220
1   13   13   13   14   15   15   15   15   15   15   15	133	-											0.002	216	1 - 2 4 · · ·	Augi
1.   1.   1.   1.   1.   1.   1.   1.	13-3				ļ								0.093	2.10	2.41	}i
134   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5   1.5	<b> </b>				<b></b> -								<del> </del>	<b> </b> -	<del>}</del>	<del> </del>
1	13.4												0.127	20.05	38.82	<b> </b>
1391-000   172													4			
15   18   18   18   18   18   18   18					·								1		l	Addii
133   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139   139	l i	7											0,388	:	1	
1986   10   1394-11585   3300310   10   2260   2311   1001   6735   3955   3020   1717   1850	13-5	8	1379+238.00		2-1.50x1.80	82 50		81.45	17.50	6.000	10 687	57.709	0.211	45.70	60.21	1-0.91
1   1800-08723   951		9	1379+334.00	0.61		84.20	-	79.56	22.92	20.244	8.562	2.501	0.768		Į.	
13   13   13   13   13   13   13   13	13-6	10	1379+815.55		3-3.00X3.0	53.09	· >>	52.65	43.11	1.021	6.735	181.851	0.029	17.17	186.06	1
13											6.478					
1, 1351-596-60	l.:				<u></u>								4	۱		
6   13019150   001	13-7			0.91			<del>}</del>							13.42	44.30	
1				0.04	1-1.50X1.2		·								1	ļ
1	lI													<b> </b> -	<del> </del>	<b>!</b>
19   134175400 091	1 1				<u> </u>								3		1	
13   3317/500   0.91	1												0.145	] :	1	
20   1381-19500   0.61	1 1												1		1	<b> </b>
2	ĺĺ				f								0.515	i	1	<b></b>
22   1920-19200   091	l ì												4		l	<b></b>
19.61   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.62   19.6													<del></del>	<del></del>	<del> </del>	
13													1	1	1	1-0.61
13-5   3831-116   25   3831-116   25   23   23   24   25   26   27   26   27   27   28   28   27   28   28   28		24	1383+148.50										0.248	ĺ	ĺ	
27   3331-6386 0   91   42   62   14   45   15   15   15   15   15   15	13-8	25	1383+414.35	0.91		41.28		40.48	29.62			<del></del>	ł	72.79	93.93	
\$\begin{array}{c c c c c c c c c c c c c c c c c c c		26	1383+470.80		2-3.00X3.0	40.58		40.47	31.44	0.350	3.944	70.983	0.077		1	
Page   9331459900   064	1 1	27	1383+638.80	0.91		42.62		42.17	36.93	1.219	2.742	3.566	1	<u> </u>	İ	
20   0384-02488   061	í (			0.91		42.60		42.14	36.90	1.247	2.774	1.803	0.040	Ţ	ĺ	
13					<u> </u>		~=-						L		l	
139   32   138444300   991   4799							<b>p</b>					· — — —	4			
33   1984+48300							·						4		1	
34   1334/5590   1-150X/15   12-99   1-1-50X/15   12-99   1-1-50X/15   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-99   12-9	13-9			0.91	3 4 6 3 6 4 5								4	45.04	85.03	
13-10   35   1384497510   0.61													2			1 0.61
\$\frac{35}{1985763190}	12 10			0.64	1-1.50X1.5									00.74		
1386-1000   122   6430   ⇒ 6356   1700   2000   4272   4991   0.322   0.323   0.333   1385113700   122   5.567   ⇒ 5301   27182   2317   4653   5.463   5.463   0.342   0.333   1385138500   122   2   5.569   ⇒ 6318   2400   17.08   3948   9.26   0.333   1385138500   0.91   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80   1.80	ا ۱۰۰ د ا			0.61	2 2 40 7 2 4								2	20,04	212.45	
37   1358-137.00   122   2   55.67   ⇒ 53.01   27.82   23.77   46.53   5.436   0.079   17.88   23.87   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.61   10.6		<del>"</del>		1 22	2-2.40X2.4									l	<b> </b>	A 447
13-11   33   1381/28500   122   22   53.59   1		37											4	17.88	23.87	- Nout
39   1386148500   122	13-11				x2								0.073	11.00	20.07	1.061
13   14   138814961 00   61   118012   15   52   52   52   52   14   2024   4115   2714     13   13   13   138814961 00   118012   15   525   58   58   58   1700   2411   7701   23719   000   0008   16   51   29.11   14611     13   13   13871470   00   24   0024   59   00   50   50   50   16   0007   10   10   10     14   13871470   00   118021   5   56   00   50   50   10   10   10   10     15   13   13   13   13   13   13   13	```				^~								}	ļ	J	
13-12   41   1385+961-20		40											<del></del>		<del> </del>	1
13-13   43   1387/19020	13-12	41	1386+961.20		1-1.80x2.10	59.25	-	58.83	17.00				0.008	18.51	29.11	1-0.61
44 1387+578:00 0-51 55:07		42	1387+072.00		2-2.40X2.4	58.08	Br-	58.03	18.04	0.277	3.025	34.845	0.058		i	
45   1391-742-0   0.61	13-13 [			0.51		56.60	<b>p</b>	56.18	22.05	1.904	2.626	0.767	0 207	12 26	50.03	
13-14   46   1397-967-60   061   1-30000   51.50	{				1-1.80X1.5		<b>-</b>						0.325			
47 1388-02150						ļ	<b>)&gt;-</b>						0.281			
48   1388/24400   0.61   66.58	13-14			0.61									Į	4.61	70.72	
13-15   59				2.4	1-3.00X3.0									L	<b> </b>	l
SO   13881592																
13-16   51   1389+027.70   1-2.40X16   81.52	13-15			0.91	1 4 6074 8								ę .	7.43	20.63	
S2   1389+150.50   0.61	12.16								<u> </u>							
S3   1389+683 50   0.61	13-10			0.61	1-2.4071.0								0.087	10,41	39,64	<del> </del>
54   1359166450   0.01   66.79	1 1															} <b>-</b>
1390+000	[ . }												0.217			<b>├──</b> ┤
SS   13501+120-10   0.9.1   55.56	l Ì				1/2						~		•	l	1	Addi
13-17   58   1390+488.80   2.180X18   50.12	լ հ	55											1	ì	i	
57   1591+15950   0.75   48.39	13-17	_			2-1.80X1.8								0.073	25,42	35.02	; <u>-</u>
13-18   59   1391+377.000   122   42   48.70   → 49.10   18.00   3.333   5.515   12.837   60   1391+655.30   1-1.80X1.5   53.65   → 53.55   19.45   0.514   3.257   8.795							- >>						L		L	
60 1391+656 30	L. 1														l	
61 1391+918.70 0.61 61.63	13 18			1.22										17.94	21.95	1061
627   1391+920   7061   731   6224   74   6458   75   74   74   74   74   74   74   74	<b> </b>				1-1.80X1.5									ļ	ļ	I
13-19   63   1392+005.70   0.61   63.59   -3   66.22   39.97   -6.580   4.881   1.426   0.015   17.34   25.95   64   1392+243.00   0.75   64.32   -4   66.42   33.17   6.332   5.495   2.427	j			~	\$250 elem				34.52 \$339843	-6.345	4.793		0.019	CAPTER A	A CONTRACT SOF	Ner 2223
S   1392+03.00   O   O   O   O   O   O   O   O   O	امدوا				<b>经外外</b> 证				1 3 X X X	1998 SE		بالم سنتسيب بالمرا	2 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	****		PETELED
1392+440	[·~·» }				<del> </del> -								0.013	17.34	29.95	<del> </del>
65 1392+465 50	}	<u>~'-</u>			0										I	AATI
66 1392+739.45	}	65											0.064		1	
13-20	<u> </u>			<del> </del>									0.004	<del> </del>	<del> </del>	<del>                                     </del>
13-21 67 1393+305 20 0.61 50.30	13-20			1.22									<del></del>	500	12.89	Addi
68 1393+497.00 1.22 x2 49.50	13-21	67			<u> </u>											<del> </del>
69 1393+629.8 0.91	'				x2									2.,,	1	1-0.61
70 1393+631.3 0.91 48.02 ► 47.65 21.70 1.705 3.244 2.109  71 1393+872.30 0.61 51.08 ► 50.32 17.06 4.455 4.016 1.173  72 1394+035.50 0.91 50.12 ► 49.97 20.50 0.732 2.125 1.381  73 1394+037.10 0.91 50.11 ► 49.91 20.35 0.983 2.463 1.601  74 1394+033.60 0.91 50.18 ► 49.95 19.34 1.190 2.710 1.761  75 1394+110.00 2.3.00×3.0 49.48 ► 49.95 19.34 1.190 2.710 1.761  76 1394+269.00 0.61 50.77 ► 50.73 22.60 0.178 0.802 0.234  77 1394+64.60 1.3.00×3.0 43.74 ◄ 44.55 28.35 -2.893 11.339 102.050  13-22 78 1394+885.00 1-3.00×3.0 44.55 ◄ 45.31 18.66 4.562 14.239 128.147 9.40 128.15															<del>                                     </del>	
71 1393+872-30 0.61 51.08	l i	~~~-6														
72 1394+035 50 0.91 50.12 49.97 20.50 0.732 2.125 1.381 73 1394+037.10 0.91 50.11 49.91 20.35 0.983 2.463 1.601 74 1394+033.60 0.91 50.18 49.95 19.34 1.190 27.10 1.761 75 1394+10.00 2.3.00×3.0 49.48 49.95 19.34 1.190 27.10 1.761 76 1394+269.00 0.61 50.77 49.99 12.19 0.738 5.727 103.091 76 1394+269.00 0.61 50.77 50.73 22.60 0.178 0.802 0.234 77 1394+64.60 1.3.00×3.0 43.74 44.55 28.35 -2.893 11.339 102.050 13-22 78 1394+886.00 1-3.00×3.0 44.55 45.31 18.66 4.562 14.239 128.147 9.40 128.15																
74     1394+033.60     0.91     50.18		:					···- <b>D</b> o-		20.50							
75 1394+110 00 23.00X3.0 49.48 - ► 49.39 12.19 0.738 5.727 103.091 76 1394+269.00 0.61 50.77 ► 50.73 22.60 0.178 0.802 0.234 77 1394+464.60 1-3.00X3.0 43.74 ◄ 44.55 28.35 -2.893 11.339 102.050 13-22 78 1394+836.00 1-3.00X3.0 44.55 ◄ 45.31 18.66 -4.562 14.239 128.147 9.40 128.15	, i						- <b>- b</b>								J	[]
76 1394±269 00 0.61 50.77 ► 50.73 22.60 0.178 0.802 0.234  77 1394±464 60 1-3.00×3.0 43.74 ◄ 44.56 28.35 -2.893 11.339 102.050  13-22 78 1394±886.00 1-3.00×3.0 44.55 ◄ 45.31 18.66 -4.562 14.239 128.147 9.40 128.15	[			0.91												
77 1334+6460 1-3.00X3.0 43.74 -4 44.55 28.35 -2.893 11.339 102.050 13-22 78 1394+886.00 1-3.00X3.0 44.55 -4 45.31 18.66 4.562 14.239 128.147 9.40 128.15	[				2-3.00X3.0											
13-22 78 1394+886.00 1-3.00×3.0 44.55 -4 - 45.31 16.66 -4.562 14.239 128.147 9.40 128.15	[			0.61												
															<u></u>	<b> </b> ]
Ann 9 1.21	13-22	78	1394+836.00		1-3.00X3.0	44.55	- <b>46</b> - ··	WIND SIZE AND ADDRESS.			14.239	128.147		9.40	128.15	<u> </u>

App. 9.1-21

### PACKAGE-14

ARE	NO.	STATION	PiPE	вох	LT	FLOW	RT	LENGTH	GRADE	V	Q	TD	AD	REMARKS
, u (L		U VIANOR	1 11 4.	DOX	ELEV.	] rcon	ELEV.	(m)	(%)	(m/s)	(m³/s)	(m³/s)	(m³/s)	REWARA
		0000+010 1	0.91		51.00	₩	52.10	19.00	-5.789	5.978	3.866			
		1393+521	1.22		49.70		50.20	19.00	-2.632	4.900	5.725			1
		1393+800	1.22		51.10		51.30	18.00	-1.111	3.184	3.720	1		
		1394+080	1.22		51.20		51.40	21.00	-0.952	2.948	3.444		1 . 1	
		1394+400	1.22		51.20		52.65	19.00	-7.632	8.345	9.750			1
		1395+127.5	1.22		50.85	-≪	51.50	18.00	-3.611	5.740	6.707			
	L	1395+460		1-3.0x3.0	49.00	-≪4	49.20	21.42	-0.934	6.442	57.977			1
		1395+520		1-5.0x4.5	47.40		47.76	20.00	-1.600	12 272	276.120			İ
		1395+926	1.22		52.20	<b>⋖</b>	52.40	14.00	-1.429	3.610	4.218			
		1396+026.5	1.22		50.00		51.50	33.00	-4.545	6.440	7.525			

PACI	KAGE	-15 (1/2)													
					LŦ		RT	LENGTH	GRADE	٧	Q	RUL	TD	AD	
AREA	NO.	STATION	PIPE	BOX	ELEV.	FLOW	ELEV.	(m)	(%)	(m/s)	(m3/s)	SLOPE	(m³/s)	(m³/s)	REMARKS
		*******							L1			(m3/s)	(111,2)	V::131	
1	}— <u>:</u>	1396+183 1396+243.90	1.22	x2 x2	52 09 50 73		53.00	26.00	-3.500	5.651	13.206	0.170			1-0.61
15-1	╂─╬╂	1396+371.50	1.24	124x24	47.85		51.50 47.95	22.00 38.33	-3 500 -0 261	5.651 2.934	13.206 16.903	0.078	40.72	56.85	1-0.61
'	1- 1	1396+803.00	1.22	x2	55.31	₹	56.00	23.00	3.000	5.232	12 226	0.101	40.72	20.03	1061
1	- 3	1396+965	0.61	<del></del>	53.87	-4	54.73	48.44	-1,775	2.536	0.741	0.097			1.00,
1	6	1397+086.50	0.61	·	58.43	<b>-</b>	58.80	35.09	-1.054	1.954	0.571	0.001			
15-2	7	1397+594.60		×2	52.60		53.20	22 00	-2727	4.989	11.657		7.82	11.66	1-0.91
15-3		1398+200	1.22	x2	48.63	<b>4</b>	19.50	29.00	-3.000	5.232	12 226				Add1
L	[8]	1398+413.00	0.91		50.19	-	50.56	24.85	-1.501	3.044	1.979	0.064	10.54	14.20	
15-4	9	1398+670.00		2-3.0x3.0	49.57	<b>-4</b>	50 26	50 89	-3.303	12.116	218.090	0.117	8.99	218.09	
15-5	10	1398+920.70	·	1-2.472.4	49.50		50.30	16.00	-5.000	12.847	73.996	0.234	69.74	74.00	
15-6	11	1399+149.50		2-3.0x3.0	46.33		46.33	26 21	0.000	0.000	0.000	0.687	112.01	0.00	1.0.61
15-7	12	1399+488.00	0.61	3 6 6 6 6	50.73		52.54	24.52	-7.392	5.170	1.510		31.54	67.33	
	13	1399+605.15 1399+879.00	0.04	2-3.0x3.0	44.76		44.87	36.56	-0.301	3.657	65.823	0.172			
15-8	15	1399+941.00	0.91	ł	58.56 53.63		59.11	22.11	2.489	3.918	2.547	0.030			
1,2-8	16	1400+071.50	0.61	<del> </del>	58.73		59.47 60.21	32.08 24.90	-18.204 -5.944	10.600	6.891	0.038	19.96	43.11	
	17	1400+192 00	0.01	1-1.9x1.9	50.38		51.58	36.19	-3.316	8.953	1.355	0.474			
15.9	1	1400+340		1-1.8x2.1	51.88		52.70	19.00	-4.300	10.159	32.320 38.403	0.174	22.75	40.94	Addi
1	19	1400+351.00	0.91	7.002.1	49.74	4	50.45	28.74	2.470	3.905	2 538		24.63	; 7V.9 <del>4</del>	- AUG I
15-10	20	1400+629.00		1-2.4x1.8	52.60	-4	52 67	19.45	-0.360	3 212	13.876	0.219	9.03	17.19	
1	21	1400+763.50	0.91	T	52.00	-4	52.81	19 22	4214	5.100	3.315	0.588			<b> </b>
		1400+840	1.22		52.00	-	52.60	17.00	-3.529	5.675	6.631				rock
15-11		1401+040	1.22	x2	55.66		57.20	18 00	-3.000	5.232	12 226		8.11	12.23	AddT
15-12	22	1401+531.3		1-3.0x3.0	47.64	<b>49</b>	49.17	45.32	-3.299	12.108	108.975	0.119	10.04	111.12	
L	23	1401+682.50	0.91	L	50.84	<b>***</b>	51.45	34.75	-1.755	3.292	2.140	0.025			
15-13A		1401+833.40	0.61	ļ	51.68		52.94	24.85	-5.070	4.285	1.252	0.073	8.90	13.48	
	25	1402/025.00	1.22	X2	51.81	€	52.50	23.00	-3.000	5.232	12.226	0.151	'		1-061
N 1	26	1402+346	0.61	<u> </u>	53.53		53.60	22.17	-1.218	2.100	0.613				
	27	1402+618.00	0.61		53.20	~₫	53.38	16.94	-0.945	1.849	0.540				
1	28	1402+845.27		1-1.5X1.5	54.26	-≪1	54.44	19.65	-0.915	4.020	9.044				
15-138		1402+911	224	2-3 0x3.0	50.10		50.24	25.07	-0.558	4.982	89.674	0.138	31.79	99.53	
15-14	30 31	1403+162 50 1403+773.50	0.61 1.22	-	61.76 56.69	<b></b>	62.25	18.03	-2.718	3.137	0.916	0.314			
15-15	32	1403+872.35	1.22	x2 x2	55.74	<b>*</b>	57.50 56.48	18.00	-4.500	6.408	14.974	0.282	11.47	14.97	1-0,91
15-18	33	1404+109.53	1.22	1-1-5X1.5	53.46	<b>*</b>	54.58	19.73	-3.789 -5.677	5.880	13.741		8.28	13.74	1-0.91
15-17	34	1404+486.10	0.61	1-, 54. 5	53.54		53.72	21.67	0831	1.734	0.507	0.191	7.70	22.51	<b>}</b>
,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	35	1404+659.00	V.V.	2-3.0x3.0	50.87		51.00	21.97	-0.592	5.128	92.308	0.151	21.04	92.81	<b></b>
15-18	36	1405+071.50	0.61	- C. GAG. C	54.53	-4	55.03	19.13	-2.614	3.076	0.899	0.062	28.93	92.76	
	37	1405+174.30		1-2.4x2.4	52.73	-	54.00	16.48	-7.706	15,949	91.865	0.074	20.00	32.10	
		1405+320	1.22	1	53.04		53.32	14.00	2 000	4 272	4.991	- 0,0,0			Addi
15-19A	38	1405+535.60	0.91		53.89	-≪	54.07	23.16	-0.777	2.190	1.424	0.086	5.13	6,42	
L	39	1405+715.30		1-2.4X1.8	52.97	<b></b>	52.97	17.80	0.000	0.000	0.000	0.111			
15-198		1406+025.85	0.91		55.80		56.48	19.15	-3.551	4.682	3.043	0.233			1-0.61
	41	1406+343.00		2-3.0x3.0	53.19	···	53.68	17.49	-2802	11.159	200.856	0.045	77.44	203.90	
15-20	42	1406+699.50	1.22	×2	53.54		54.00	23.00	-2 000	4.272	9.983	0.128	14.73	19.97	1-0.91
L	43	1406+955.00	1.22	x2	55.34	<b>-4</b>	55.80	23.00	2 000	4.272	9.983	0.100			1-0.91
į.	44	1407+101.00	0.91	<u> </u>	54.37	·	55.53	27 22	-4.262	5.129	3.334				
1	45	1407+408.50	1.22	x2	55.10	◀	56.00	20.00	4.500	6.408	14.974	0.070			1091
15-21	46 47	1407+626.00 1407+796.50	4 32	1-1-2×2.4	53.49	<b>4</b>	54.00	18.92	-2.696	6.710	19.325	0.106			
1321	48	1407+979-50	1.22 0.91		56.82 55.86	<b></b>	57.90	18.00	-6.000	1.399	8.645	[	52.87	65.11	1-0.91
	50	1408+092.00	0.91	ł	56 21	4	58.74	29.74	2.959	4 274	2.778	*			
1	51	1408+302.00	0.91	<del> </del>	56.17	<b>4</b>	57.25 56.31	31.37 25.08	-3.315 -0.582	4.524	2.941 1.232				ļl
1	<del>⊢∸</del> 1	1408+380	1.22	л2	56.49		57.00	18.00	-2.833	1.896 5.085	11.882	0.134			0.00
	52	1409+099.50		x2	58.57	•	59.20	21.00	-2 655 -3 000	5 232	12.226	0.047			Add1 1-0.61
15-23	53			x2	51.72	-45	57.90	18.00	1,000	3.021	7.059	: 0.04/	9.11	20.33	1-0.61
L	54	1409+263.40	0.91	1	57.79		57.87	18.98	-0.421	1,613	1.049	1		10.00	
15-24	55	1409+392 50	1.22	×2	56.51	-a	57.50	18.00	-5.500	7.084	18.554		13.06	18.55	
	56	1409+998.00	0.61		61.92	<b>4</b>	62.55	22.31	-2.824	3.198	0.934	0.063		,	
15-25	57	1410+195.20	1.22	<b>1/2</b>	61.34		61.50	16.00	-1.000	3.021	7.059		14.46	22.37	1-0.91
1 :		1410+320		x2	59.40	-4	59.80	20 00	2.000	4.272	9 983	J			Addil
	58	1410+530 50	0.91		61.13	-4	61.67	20.67	-3.599	4.714	3.064	0.014		.	
<u></u>	59	1410+531.40	0.91	<u> </u>	61.16	◀	61.30	20.54	-0.682	2.051	1.333				
1	60	1410+951.80	1.22		57.60	.≪4	57.79	18 00	-1.056	3.103	7.252				1-0.91
1	61	1410+967.90	1.22	x2	57.20		57.40	19.00	-1.053	3.039	7.242	J		١ ,	1-0.91
15-28	62	1411+131,55	0.91		58.67	4	58.69	17.19	-0.118	0.847	0.551	ŀ	21.61	24.57	
1	63	1411+224.00	0.91	<u></u>	58.77		59.24	20.08	-2.326	3.789	2.463	I			
L	64	1411+279.00	1 22	122	58.83	<u>-∢</u>	59.00	17.00	-1.000	3.021	7.059				1-0.91
	100								-						

PACE	AGE	- 15 (2/2)													
				[	ĹΤ		RT	LENGTH	GRADE	V	o l	ਲਹਣ	70	AD	
AREA	NO.	STATION	PIPE	BOX	ELEV.	FLOW	ELEV.		-	-	_	SLOPE		(m³/s)	REMARKS
				L				(m)	(%)	(m/s)	(m3/s)	(m3/s)	(m³/s)	(m/s)	
15-27	65]	1411+475.50		3-1.5x1.0	61 20		61.40	20.00	1.000	3.790	17.053		10.62	17.05	1-0.61
15-28	66]	1411+800.80		3-2.0x1.25	63.07		63.25	18 00	1.000	4.505	33.790		23.33	33.79	1-0.91
15-29	67	1412+237.00		x2	61.90	-4 ·	82.42	17.00	-3.059	5 283	12.345		14.28	14.59	1-0.61
1		1412+300		x2	63.80	-≪	64.00	15.00	1 333	2.197	1 284		196		Add'i
I	68	1412+472.10	0.61	x2	64.65	-≪	64.76	15.00	-0.753	1.652	0.965				1-0-61 Add'i
1	69	1412+980 00	0.91	L	63.93		63.99	14.97	-0.401	1.573	1.022				
	70	1413+275.90		x2	61.56		61.70	15.00	-0.933	2.913	6.819				1-0.91
i 1	71	1413+438.00		x2	61.43	- <b>4</b>	61.60	17.00	-1.000	3.021	7.059				1-0.91
15-30	72	1413+596.85	0.75		59 99	<b>4</b>	60 20	14.85	1.421	2.603	1.150		18.92	19.76	
	73	1413+598.00	0.75		60.01		60.31	14.85	-2.040	3.120	1.378				
	74	1413+689.80	0.91		59.12	-di - ·	59.22	19.19	0.521	1.793	1.166				
	75	1413+690.90	0 91		59.12		59 22	19.19	-0.521	1.793	1.166				
15-31	76	1414+247.50	1.22	x2	65.40		65.70	17.00	1.765	4.013	9.377				1-0.61
		1414+280	1.52	x2	65.30		65.60	20.00	1.500	4 284	15.538		31.11	35.23	Ado'i
L	77	1414+337.70	1.22	x2	66.00	<b>4</b>	66.32	15.00	-2.133	4.412	10.310				1-0.61
15-32	78	1414+553.05	1 22		67.28	4	67.46	19.75	-0.911	2 884	3 369		92.46	101.53	1-0-61
	79	1414+661.08		3-2.4x1.8	67.23	-al	67.55	16.00	-2.000	7.574	93.156				1-0.91
	80	1414+889.55		1-2.4X2.4	66.86		66 99	17.11	-0.760	5.008	28.845				
	81	1415+290.00	0.91		64.97		65 31	18.64	-1.824	3 355	2.181				
15-33A	82	1415+417.00	1.22	x2	64.58	-≪1	64.75	17.00	-1 000	3.021	7.059		33.17	48.03	1-0.91
	83	14151462.00	0.91		64.62		64.77	17.69	-0 845	2 288	1.487			,	
1 1	84	1415+504.00	1.22	x2	64.12		64.30	18.00	-1.000	3.021	7.059				1-0.91
	85	1415+543.50	0.91		65 23		<b>65</b> .35	16.01	-0.750	2.151	1.398	ĺ	:		
	86	1416+365.50		1-2.4X2.4	67.75	-d ·	67.98	16.92	-1.359	6.698	38 582				
15-338	87	1416+438.20	0.91		67.88		68.03	18.62	-0.806	2 230	1.450		72.78	86.83	
	89	1416+652.20		1-2.4x2.4	66.35	◄	66.65	15.00	-2.000	8.125	46.799	48.5		7,7477	1-0.91
15-34	90	1416+760	0.91	x2	67.00	-4	67.30	16.00	1.875	3.402	4.423		26.02	26.85	Add'i
	91	1416+798.00	1.52	×2	68 00		66.50	16.00	-3.125	6.183	22,427		-7:		1-0.61,1-0.91
15-35	92	1416+937.00	1.22	x2	67.50	-	67.80	15.00	-2.000	4.272	9.983		13.97	18.61	1-0.91
	93	1417+090.10	1.22	x2	67.65	<b>4</b>	67.90	16.00	1.563	3,776	8.823		,,	,	1-0.91,1-0.61
15-36	95	1417+328.00	1.22	x2	68.30	4	68.60	19.00	1579	3.796	8.870		8.61	8.87	1-0.61
15-37	96	1417+742.20		2-2.4x1.8	68.05	-4	68.16	16 50	0.667	4 373	37.780		30.39	37.78	1091
	1	1418+320	1 22	x2	69.40	4	69.80	16.00	-2 500	4.776	11.161	<del></del>			Addi
15-38	97	1418+370.50	1.22		68 23	-4	68.73	18 27	-2.463	4.741	5.539		22.80	27.14	7001
l	98	1418+372 50	1.22	<b> </b>	68.28		68.73	17.72	-2.540	4.814	5.624			27.14	<del></del>
Į į		1418+640	0.91	x2	70.40	<b></b>	70 80	18 00	2 2 2 2 3	3.704	4.815				Addi
i	99	1418+708.10	0.51	<del> </del>	69.64	4	70.40	22.40	3 393	3 505	1.024				7201
i	100	1418+938.00		1-2.4X2.4	69.60	-4	69.79	21.73	-0.874	5.372	30.944		1.15	1	
15-39	101	1419+167.40	1.22	x2	66.29	-01	67.00	23.00	-3.087	5.307	12.402		53.89	66.57	1-0.61
l	102	1419+452.00		12	64.25	4	64.80	16.00	-3.437	5.601	13.037	. 0.298	33.69	00.57	1-0.61
l	103	1419+492.10		x2	64 50	4	64.80	18.00	1.667	3.900	9.113	0.043			1-0.91
15-40	104	1419+700.80		1-2.4x20	62.99	4	63.35	17.50	2 057	7.893	37.687	0.043	22.68	37.89	1-0.51
1	105	1419+954.00	1.22	-	62 82		63 32	20.00	-2500	4.776	5.580		22.00	37.69	
i	106	1420+088	1 22	x2	63.00	-	64.00	18.00	5.556	7.120	16.638				1091
15-41	107	1420+380.60	0.61		64.80	4	65.53	19.79	-3.689	3.655	1.068		36.22	46.31	10.91
	108	1420+381.70	0.61	<del> </del>	64.77	-1	65.57	19.65	4.071	3.840	1.122	14.00	30.22	40.31	
Į	109	1420+686.40	1 22	x2	63.67	4	63.95	23.00	1217	3 3 3 3	7.788		\$1.4		
1	110	1420+855.00		<u>72</u>	64.04	4	64.84	20.00	4000	6.041	14.118		1		1 0.61
15-42	111	1421+120 00		x2	68.10	4	66.50	24.00	-1.667	3.900	9.113	0.095	18.41	40.80	1-0.61
	11 a	1421+134		x2	67.68		65 20	29.00	8.545	8.830	20.634	0.035	10.41	40.80	1-0.91
	112	1421+300.15	1.22	×2	69.29	4	69.78	20.00	2.450	4.728	11.049	0.530		* 3	Addi
	113	1421+525	122	x2	71.49	4	72 50	20.00	5.050	6.788	15.863	0.179			1-0.61
15-43	114	1421+609 2	1.22	t	7197		73 20	17.00	7 235	8.125	9.493	0.00		***	1-0.61
[ " "	115	14214976.00	****	1-2.4X2.5	77.91	4	78 25	19.96	1,703	7.498	43,190	0.697	53.59	68.55	1-0.61
<b>—</b>		1422+580	l	1-2.4x2.4	69.04		69.50	15.00		10.115		ļ	<u> </u>		li
15-44	116	1422+594.30	1.52	1-2.474.4	68.91		69.40	19.79	-3.100		58.265				Addi
'''''	119	1422+864.00	1.32	x2	71.55				-2.476	5.504	9.982		49.74	81.13	1-1.22
l i	120	1423+061.00	0.91	<u> </u> ^	76 88		71 94	19.00	2.053	4.328	10.113	'			1-0.61
15.45	121	1423+231.50		ł		<b>-9</b>	77.43	19.40	2 938	4 259	2.768	ļl			
1,2,42	''	1423+231.50	1 22	x2 x2	77.16		77.60	17.00	2 600	4.871	11.382		46.94	58.45	1-0.61
1	122	1423+519.5	1 22		73.65	4	73.95	19.00	-1.579	3 796	8.870		# * * *	2.75	AGGI
15 46	123			1-2.4X2.4	72 55		72.83	21.01	1.333	6.632	38.202			8 6.4	
11343	143	1424+603.50	L	3-1.8x1.5	82.65	-<1	83 25	26.00	1.538	5.635	45.641		39.42	45.64	1-0.91

PACKAGE - (	6 (	(1/2)	
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		10 /112/	DIOC	F-885	TISTES ET	COLAC	(187E) E	CENATO	35155		-	r 25 * 1			
			PIPE	BOX		FIOW	INV.ELE.			l v l	Q	RD&	TO	AD	!
AREA	NO.	STATION			NORTH		SOUTH	(m)	(%)	(m/s)	(m³/s)	SLOPE	(m³/s)	(m³/s)	REMARKS
1 1	ĺ	1		i i	(m)		(m)	ĺ		(ms)	(11/75)	(m3/s)	į i	1	i !
	1	14254017.6	0.91		82.05	4	82.56	26.35	-1.935	3.456	2 247				
16-2	3	1425+147		1.5x1.5	81.10	-4	81.60	19.80	-2.525	6.674	15,016	i !	i '		3-0.91
16-3	•	1425+500	1.22	x2	95.19		95.70	17.00	-3.000	5.232	12 226	1	10.41	13.17	Addi
~ ~	5	1425+972.5	2.74	(2-0.91)	91.18		91.22	46.81	-0.085	0.726	0.944			13.17	7.001
			2.74												<del> </del>
16-4	6	1426+213		1-2.0x2.0	99.75	<b>-41</b> -	100.10	17.50	-2.000	7.195	28.780		20.27	28.78	1-0.91
16-5	_	1426+441.2	1.52	L	93.26	<b>⊲</b> 4 -	94.50	31.00	-4.000	6.995	12.687		4.73	12.69	1-0.91
	8	1426+941.6	0.91		90.53	<b>⊲4</b> ··	91.72	39.10	-3.043	4.334	2.818				
16-6	9	1426+943	0.91		90.34	-⊲4	91.56	38.56	-3.164	4.419	2.873	0.458	12.82	14,66	
l i	4	1427+020	1.52		96.38	4	96.80	21.00	-2.000	4.946	8.971	•	1		Addi
16-8		1427+360	122	-2	102.31	4	103.00	23.00	-3.000	5.232	12.226		j		Addi
1.00	10	1427+407.5	0.91	<u> </u>	102.07		102 28	23.31				0.217	44.00	43.70	7424
<b>)</b> ——				}		4			-0.901	2.358	1.533	0.317	11.22	13.76	<b></b>
	37	1427+640.7	0.61		102.16	4	102.57	40.29	-1.018	1.920	0.561	0.319	, ,	i	
16-9		1427+955	1.52		119.30	<b>-44</b>	120.70	25.00	-5.600	8.277	15.011	]	10.06	17.51	Add'i
1	12	1427+958	0.91		117.79	<b>- I</b>	118.29	31.31	-1.597	3.140	2.041	)	i '		
	13	1429+081.6	0.61	<del></del>	83.01		82.70	15.13	2.049	2.724	0.796	0.490			h
16-10	14	1429+256	0.91		82.17		81.37	15.99	5.003	5.557	3.612	0.254	6.88	9.28	
		1429+360	0.91		83.30	.	83.00	15.00	2.000	3.514	2.284		, 5.40	. 0.20	Addii
1	15	1429+639.3	0.91		79.50		78.80	22.00	3.182	4.432	2.589	0.188	,	1	7001
10.00						-									
16-11	16	1429+924	1.22	XZ	78.94	·- ]=>	78.00	18.00	5.222	6.903	16.131	0.431	15.58	22.97	1-0.91
	17	1430+205.5	1.22		78.60	- 🌬	78.00	16.00	3.750	5.850	6.835	0.060	'	L	1-0.91
1	18	1430+541	0.91		74.87	-4-	75.28	24.48	-1.687	3.227	2.098				
16-12	19	1430+874	0.91	x2	72.16		72.45	20.00	-1.450	2.992	3.890	0.233	16.23	24.85	1-0.61
I i	20	1431+308	1,52	x2	72.03	~d ~	72.49	25.00	-1.840	4.744	17.209	0.258			1-0.61
1 1	21	1431+589	0.91		70.74	4-	70.98	23.02	1.043	2.537	1.649	0.200	. '		
<b>}</b>	22	1432+244.5	1.22	ļ	69.30										<del> </del>
1						<b>~4</b> ·-	69.50	17.00	-1.176	3.276	3.828		'	1 2 3	1-0.91
16-13	23	1432+246.5	1.22		69.30	- <b>44</b>	69.50	17.00	-1.176	3.276	3.828		6.62	13.33	1-0.91
	24	143244829	0.91	x2	67.88	<b>41</b>	68.13	21.32	-1.173	2.690	3.498	0.076	į	i .	1-0.91 Add'i
	25	1432+596.8	0.91		68.18	₹	68.66	26.42	-1.817	3.349	2.177	1			
16-14	26	1432+959.2	0.91		65.04	⋖4	65.60	27.11	-2.066	3.571	2.321	0.186	10.99	11 32	
1 1	27	1433+183.8	1.22	C .	62 70		63.09	24.00	-1.625	3.851	8.998	0.175	1	1	1-0.91
	28	1433+433.2	0.91		61.93	-	62.29	19.07	1,883	3.414	2.219	L		<b></b>	1-0.31
16-15	-	1433+471.9	0.91		62.52										
10-10			0.91				62.57	18.86	-0.265	1.279	0.832	l :	39.65	41.40	
<u></u>	31	1433+799.5	نـــــــا	2-1.6X1.5	60.90	<b>41</b> –	61.23	13.50	-2.444	7.103	38.354	5			1-0.91
1 .	32	1433+959	0.91		61.16	<b>⊲</b> 4 ⋅	61.55	20.05	-1.945	3.465	2.252				
	33	1434+060	0.91		60.99	◀	61.90	21.88	-4.159	5.067	3.294			Ĺ	
1	34	1434+294.7	1.22		62.50	-≪	62.70	15.00	-1.333	3.488	4.075		1 '	ł	1-0.61
16-16	35	1434+459.7	0.91		62 70	44 -	63.17	15.15	-3.102	4.376	2.845		43.17	55.20	
"	36	1434+531	1.22	10	62.58		62.80	15.40	-1.429	3.610	8.437	}	79.II	33.20	1000
J .	37			<u> </u>		≪4 .							- "	i	1-0.61
1 1		1434+648	0.61	<u> </u>	62.93	di	63.12	16.27	-1.180	2.067	0.604			i	<u></u>
<b> </b>	38	1434+763.9	5.00	ļ	61.24	-44	62.14	13.79	-6.526	10.729	33.689	<u> </u> _		l	<u> </u>
	39	14341945	2.74		64.38	-≪-	64.61	11.58	-1.986	7.301	43.028			1	
L I	40	1435+078.2	2.74		64.90	<b>I</b>	65.29	11.48	-3.397	9.548	56.273	0.065	<i>.</i>	1	
16-17	41	1435+305	1.22		67.87	4	68.16	14.00	-2.071	4.348	5.080		10.89	13.52	1-0.61
	42	1435+497.8	1.22	x2	64.70		64.90	14.00	-1.429	3.610	8.437				1-0.61
16-18	43	1435+787.8	2.74		61.15	4	61.70	12.86	-4.277	10.713	63.139	<u>-</u>	54.04	6244	1-2.01
100,10	44	1435+914.3		3									54.84	63.14	<b>├</b> ─ <del>,</del> - <u>-</u>
1			1.22	۸٤	60.50	<b>4</b>	60.95	13.00	-3.462	5.620	13.133	]			1-0.75
16-19	45	1436+352	1.22		58.00	₩.	58.30	16.00	-1.875	4.136	4.833		19.81	30.44	1-0.91
<b>L</b>	46	1430+489	1.22		57.80	⋖	58.30	16.00	-3.125	5.340	12.478			1	1-0.61
16-20	47	1436+810.5	1.52	x2	58.70		59.30	15.00	-4.000	6.995	25.374		23.35	25.37	2-0.91
	48	437+004.2	1.22	x2	58.05		58.26	14.00	-1.500	3.700	8.645			r <del></del> -	1-0.61
	49	1437+139.5	1.22		55.00	4	55.50	21.00	-2.381	4.661	10.692	0.072	4		1-0.61
16-21	50	1437+332.7	1.22		54.60							0.072	43.63	40 70	
10-21				X2		⋖-	55.20	24.00	-2.500	4.776	11.161		42.57	46.78	1-0.61
1	51	1437+699.3	1.22	x2	65.65	◄~~	56,00	19.00	-1.842	4.100	9.580	l		1	1-0.61
1 .														1 .	
l .	52 53	1437+836 1438+082	0.91		54.61 55.85	<b>*</b>	55.05 57.90	22.00 30.00	-2.000 -6.833	3.514 6.495	2 284 4.222		'		

PACK	AGE -	16 (2/2)												100	4.56
		The last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the last of the la	PIPE	BOX	INV.ELE.	FIOW	INV.ELE	LENGTH	GRADE	V		RO &	70	AD	
AREA	NO.	STATION			NORTH		SOUTH	(m)	(%)	•	Q (	SLOPE	(m³/s)	(m³/s)	REMARKS
					(m)		(m)	3.7		(m/s)	(m³/s)	(m3/s)	, ,	l ` .	
	54	1438+266.6	0.91		57.43	-91	57.13	27.93	1.074	2.575	1.674				
i I	55	1438+371.4	0.91		54.57	-41	54.93	26.95	-1.336	2.871	1.867				ļ
16-22	56	1438+487.3	1.22	:	58.80		59.00	15.00	-1.333	3.488	4.075		13.47	25.81	1-0.61
i I	57	1438+543.2	0.91		56.23		57.45	26.00	-4.692	5.382	3.498	0.059		1	
i I	58	1438+756.7	1.22		59.00		59.80	16.00	-5.000	6.755	7.892	0.250		<u> </u>	1-0.61
	59	1438+999.8	1.22	i	60.70		61.50	21.50	-3.721	5.827	6.808	0.135			1-0.61
	60	1439+213.5	0.91	i	57.34		59.11	32.36	-5.470	5.810	3.777	0.096	* .		
16-23	61	1439+324.6	0.91		61.52	-46 -	61.98	18.82	-2.444	3.896	2.555	0.182	7		
	62	1439+440	1.22		62.94	<b>-45</b> –	63.50	19.00	-2 947	5.186	6.059	0.063	18.38	18.54	1-0.61
	63	1439+509.5	1.22		65.30	-45 <b>6</b>	65.60	13.00	-2.308	4.589	5.362	0.340			1-0.91
		1440+150	0.61		68.00	-026	68.30	15.00	-2.000	2.691	0.786			ŀ	ltbA
	64	1440+419.0	0.61		52.03	- 120-	51.68	28.96	1.209	2.092	0.611			<del></del>	
16-24		1440+500	1.52	x2	53.04	- jb-	52.70	17.00	2.000	4.946	17.942	0.086			Addil
!	65	1440+580.0	0.91		47.40	🌬	48.32	39.63	-2.321	3.785	2.461		22.19	24.94	
	66	1440+797.8	0.91		49.07	- >	48.58	33.85	1.448	2 989	1.943		i		
	67	1440+799.3	0.91		49.07	<b> </b>	48.56	33.85	1.507	3.050	1.982				<b></b>
	68	1441+747.3	1.22	x2	92.70	-45	93.51	19.00	-4.263	6.237	14.574	0.128		4.5	1-0.61
16-26	69	1442+011	0.91		101.05	-4	103.19	38.09	-5.618	5.889	3.828	0.025	0.26	33.85	
	70	1442+173 2	1.22	;	102.71	TE	104.06	29.00	-4.655	6.517	7.615	0.108			1-0.61
	71	1442+173.6	1.22		102.63	-4	104.06	29.00	-4.931	6.708	7.637			l	1-0.61
	72	1442+231	0.61	<b></b>	101.80		104.11	22.00	-10.500	6.166	1.801	0.552			
	٠.	1442+362	0.91		108.10		108.30	17.00	-1.176	2.695	1.752	,,,,,,,			Addi
	73	1442+569.2	0.91		114.00	-≪1 -	117.54	29.00	-12 207	8.680	5.643	0.054			
16-27	74	1442+599.5	0.91		124.65		125.93	20.24	-6.324	6.243	4.061	0.368	27.14	33.06	
	75	1442+914.3	1.22		135.60		136.25	15.00	-4.333	6.288	7.347	0.632	277.17	00.00	1-0.61
	76	1443+265	1 22		143.30		144.70	26.00	-5.385	7.009	8.190	0.272		1	1-0.61
	77	1443+468.3	0.91		146.65		148.37	24.66	-6.975	6.561	4.265	0.244	+ *		1
	78	1443+728.4	0.61		145.71	-41	148.93	34.34	-9.377	5.827	1.702	0.143	·	<del> </del> -	
16-28	79	1443+857.7	0.91		159.04	-24 -	160.45	19.61	-7.190	6.662	4.331	0.128	11.28	17.79	<del></del>
l i	80	1444+226	0.91		144.98		149.19	26.18	-16.081	9.963	6.476	0.386		'''	
li	81	1444+296.8	0.91		134.32	~ <b>4</b> –	140.52	58.02	-10.686	8.122	5.279	0.044			
	82	1444+621.3	1.22	<del>-</del>	138.16		138.37	16.00	-1.313	3.461	4.043	0.440			1-0.61
16-29	83	1444+693.2	1.22		133.90	-4-	136.87	20.00	-14.850	11.641	13,601	0.135	13.48	19 93	1-0.61
l		1444+980	0.91		137.82		138.10	14.00	-2.000	3.514	2 284	00	10.40	'**	Addi
16-30		1446+020	1.22	x2	126.15		127.50	27.00	-5.000	6.755	15.734		12.59	17.07	Addi
i		1445+460	0.61		119.60		118.80	15.00	5.333	4.395	1.284		12.00	17.07	Addi
16-31	84	1446+738	0.61		113.76	-4 -	118 24	37.60	-11.915	6.569	1.919	0.165	19.26	30.11	_~~!
E.	85	1446+940		x2	116.50		123.60	44.50	-15.955	12.066	28.195	0.100	10.20	00.11	1-0.61
	86	1448+080	0.61		87.88		91.74	23.28	-16.581	7.749	2.263	0.122			1-0.01
16-32		1448+140	0.91		91.02	-4	91.50	16.00	-3.000	4.303	2.797	0.306	7.06	10.79	Add'I
1	87	1448+406	0.91		83.99	-	87.45	27.60	-12.572	8.809	5.727	0.076		10.13	7001
	88	1448+537.5	1.22		84.80	- <b>4</b>	85.44	18.00	-3.587	5.705	6.665	0.435	7.7		1-0.61
1	89	1448+719	0,91	<b> </b>	85.50		85.90	20.00	-7.000	6.573	4.273	0.038			}
16-33	90	1448+945.4	0.61	<u> </u>	80.55		82.60	21.65	9.469	5.856	1.710	<b>4.400</b>	9.27	21.84	<b> </b>
	91	1449+108.4	1.22	l	79.22	4	79.70	16.00	3.000	5.232	6.113	0.359	4.21	21.04	1-0.61
		1449+220	0.91	- <del></del> -	78.70		79.00	15.00	2 000	3.514	2 284				Addi
	92	1449+354	0.91		77.01		77.64		3 623	4.729	3.074	0.047		1 3	1-0.61
16-34	93	1449+740	1.22	·	56.50		57.00		2 632	4.900	5.725	V.V*1	5.60	5.73	1-0.61
	94	1449+963.8	1 22		46.84		47.79		5.588	7.141	8.343	0.529	3.00	3.13	1-0.61
16-35	95	1450+243.6	0.91		41.52		41.92		1.968	3.485	2.265	0.329	9.21	10.72	1-0.81
		1450+520	1 22		32.46		33.00		3 000	5.232	6.113	0.176	0.21	16.72	1-0.91
	96	1450+793	0.91	t	30.38	-4	30.93		2 570	3.983	2.589	0.199		ļ	1-0.91
16-36		1450+947.5	0.91		25.50		28.06	30.00	1.867	3.394	2.207	V. 199	12 28	42.04	<b></b>
	98	1450+948.5	0.91	<del></del>	27.02		31.59	30.00	15 233	9.697	6.303	3 7 7	12 20	13.91	
	99	1450+949.6	0.91	<b> </b>	25.42		26.33	30.00	3 033	4.327	2.813			915.15	}————
	100		1.22		25.65		25.80			3 021				<b></b>	I
16-37	101		1.22	<sub>v2</sub>	24.84		25.00	16.00	-1.000 -1.000	3.021	3.529	1,	48.45	40.00	1-0.91
	102	1453+267	1.22	<u> ^-</u>	25.01		25.35	23.00			7.059		15.15	18.52	1-0.91
		1453+850	0.91	\ <del>-</del>	24.00		23.80		-1.500 1.250	3.700 2.778	4.323 3.511				1-0.91
	103	1455+209		1-2.40X1.1	20.34		20.33	18.88	0.053	1.060	2.797			2.80	Addi

PACKAGE-17
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ARE	NO.	STATION	PIPE	вох	LT.	FLOW	RT	LENGTH	GRADE	٧	Q	TD	AD	REMARKS
AVE	NO.	SIATION	FIFE:	200	ELEV.	FLOW	ELEV.	(m)	(%)	(nv/s)	(m³/s)	(m³/s)	(m³/s)	LEWALL
	1	1457+987	0.61		10.26	À	10.18	13.69	0.570	1.436	0.420			I
	[ 2	1458+530	0.91		8.37	∢	9.06	12.79	-5.343	5.745	3.735			
	3	1459+213	0.91		7.49	¥	7.64	13.20	-1.114	2.622	1.704	}		
Į.	4	1459+460	0.91		7.18	≪1 -	7.20	13.44	-0.186	1.072	0.697	} .		
	5	1459+693	0.91		6.77	- ₹9	6.90	12.43	-1.046	2.541	1.652		ļ	
J	6	1459+892	0.91		6.27	Ť	6.31	12.65	-0.316	1.397	0.908	]	]	j
	7	1460+069.3	0.91		5.90		6.00	13.66	0.754	2.158	1.403			<b>,</b>
	8	1460+315	0.91		5.22	*	5.63	12.65	-3.273	4.495	2.922	1		
1	9	1462+065.6	0.91		3.14	-	3.09	10.38	0.405	1.580	1.027	<b>1</b>		
	10	1462+355.6	0.91		2.86	▶	2.84	10.81	0.240	1.218	0.792	1		
J	11	1462+954.5	0.91		2.12	-≪4	2.24	10.90	-1.045	2.540	1.651	] .	<b>j</b>	J .
	12	1463+134.7	0.91		1.62	4	1.86	12.52	-1.917	3.439	2.236			
1	13	1463+233.7	0.91		1.43	₩	1.53	11.67	-0.857	2.299	1.495	1		1
1	14	1463+359	0.91		1.27		1.25	11.56	0.208	1.132	0.736	1	•	
1	15	1463-649.5	0.91		0.85	•	0.15	11.94	5.854	6.011	3.908	ĺ		
,	16	1463+774.5	0.91		0.40	~4	0.53	11.58	-1.105	2.612	1.698	] .		,
	[17]	1464+110		3-3.1X2.0	-0.35		0.17	8.91	-5.839	14.72	273.74	<u> </u>	1	
	[18]	1464+298		3-3.1X2.0	0.07	₩	0.18	8.96	-1.227	6.75	125.51	1		
1	19	1464+362	0.91	:	0.65	4	0.70	11.00	-0.491	1.741	1.132	ĺ		ĺ
1	20	1464+437.8		3-3.1X2.0	-0.04	Ā	-0.11	11.48	0.610	4.76	88.47	1		
,	21	1464+637.8		3-3.1X2.0	0.38	- B>-	-0.40	12.24	0.131	2.20	40.96	]	<b>}</b>	
	22	1464+736.5	0.91		-0.13	· · · · À	-0.35	11.00	1.936	3.457	2.247			
	23	1464+828.8	0.91	<del> </del>	0.38	-4	0.67	12.18	-2.381	3.834	2.492			1
1	24	1464+927		3-3.1X2.74	0.03		-0.18	11.36	1.822	8.94	75.93	1		
1	25	1464.538.8		3-3.1X2.0	-0.11		0.23	11.11	-3.043	10.62	197.61	1	1	
j	26	1465+577.7	0.91	÷	0.56	- ■	0.81	11.05	2 262	3.737	2.429	1	]	<b>}</b>
	27	1465+962.7	0.91		1.22	4	1.32	11.62	-0.895	2.350	1.528	i .		
	28	1466+173.6	0.91		1.32	◀	1.60	11 28	-2.482	3.914	2.544	1		
	29	1466+635.5	0.91		2.24		2.64	12.36	3.236	4.469	2.905	1		
1	30	1467+238.7	0.91		1.78	4	2.11	15.74	-2.096	3.597	2.338	1		
}	31	1467+826	0.91		0.98	<b>44</b>	1.28	15.00	2.007	3.519	2.288	1		

	PACK	AGE - 18	(1/2)
	AREA	NO.	STA
1		A 183	1468+0
1		3	1468+0
1		5	1458+1
1		6	1468+2
		7	1468+2
		8	1468+5
		9	1468+6
		10	1469+1
		11	1469+2

		· · · · · · · · · · · · · · · · · · ·	-					1				RO &	-			ı
اء.	NO	CTATION	0.00	564	LT		RT	LENGTH	GRADE	V	Q		10	AD		l
AREA	NO.	STATION	PIPE	BOX	ELEV.	FLOW	ELEV.	(m)	(%)	(m/s)	(m³/s)	SLOPE	(m³/s)	(m³/s)	REMARKS	ĺ
							·	<u> </u>				(m3/s)			L I	ĺ
	118%	1468+023.50	70.91	12 (2.77)	0.77	4	1 35	17,43	-3.385	4.57	5.943		神经马	NEW YEAR	STILL ST	ĺ
ĺ	3	1468+047.50	0.91	x2	1.150	4	1.220	16.76	0.418	1.606	2.087	1.7E 27.E & C	TIRELINES.	END EXPES	3033333	1
l	5	1458+170.00		3-3.0×2.4	0.300		0.100	13.60	-2.943	10.842	234.184				<del></del>	İ.
ŀ	6	1468+223.80	0.91	V 0.V AL. 1	1.50					4.152				* +		ĺ
ļ							200	17.90	-2.793		2.699				ļ	l
ļ	7	1468+247.43	0.91		1.07		1.51	17.17	-2.563	3.977	2.585					ĺ
Ų	8	1468+559.40	0.61		1.74		1.89	15.75	-0.952	1.857	0.000					ĺ
ſ	9	1468+657.35	0.61		1.66		2.00	15.66	-0.894	1.799	0.526		:	l i		ĺ
ì	10	1469+136.75	0.61		1.23	<b>4</b>	1.53	15.34	1.956	2.661	0.777					ĺ
ì	11	1469+271.06	0.61		1,16		1.50	17.24	-1.972	2.672	0.781					ŀ
}						<del></del>										ĺ
, ,	12	1469+303.00	0.61		0.57	<b>b</b> >	0.50	17.56	0.393	1.201	0.351		2.4			l
	13	1469+355.00	0.61		0.97	· <b>j</b> >-	-0.01	20.61	4.755	4.150	1 212					ĺ
- 1	14	1469+482.00	0.61		0.61	<b>⊲</b> 4 - · · -	0.93	17.71	-1.807	2.558	0.747					ĺ
ſ	15	1470+560.00	0.61		1.49	⋖	1.52	16.12	-0.186	0.821	0.240					ı
ì	16	1470+770.95	0.61		2.31		2.24	19.31	0.363	1.146	0.335					i
1	17	1470+971.10	0.61		1.89		2.16	18.51	-1.459	2 298	0.671					!
1															<b></b>	l
1	17A	1471+260.00	0.75		1.25	<b>4</b>	1.36	19.50	-0.564	1.640	0.724				L	l
1	18	1471+655.70	0.91		1.32		1.49	. 16.94	-1.004	2.489	1.618		7		i 1	ĺ
į	18B	1471+850.00	0.75		1.6		1.85	23.00	-1.087	2.277	1.005					į
•	19	1471+944.60	0.75	x2	1.49	-	1.54	21.02	-0 238	1.065	0.941					
}	20	1472+097.50	0.51		1.21		1.71	22.84	-2.189	2.816	0.822		l ·		<del>-</del>	
}	21	1472+472.30	0.75	x2	1.20		1.32	15.92	-0.754						<b></b> i	
1										1.896	0.837					
Í	22	1472+566.00	0.75	x2	0.84		1.00	15.23	-1.051	2 238	1.977		[ · .			į
1	24	1472+726.80	0.75	x2	1.60	⋖	1.62	16.30	-0.123	0.765	0.676		] :		3.9	į
1	26	1472+851.80	0.75		0.00	<b>4</b>	0.30	19.25	-1.558	2.726	1.204		} - [			
	27	1472+995.50	2.74		-0.69		-0.65	12.16	-0.329	2.971	17.511		]		<u>  </u>	
	28	1473+044.82		3-2.40X2.40		-	0.69	29.79	-1.981	8.085	139.713				<u> </u>	
	29		0.64	3-2.40A2.40										1.0		
		1473+153.00	0.61		1.75	◀ · · ·	1.93	15.89	-1.133	2.025	0.592		-:	1.41		
	30	1473+227.43	0.61		2.43		2.44	16.51	-0.061	0.468	0.137					
	31	1473+751.90	0.61		2.01	<b>∞4</b> —	2.43	16.60	-2.530	3.027	0.884					
- 1	32	1473+935.05	0.91		2.19		2.27	18.25	-0.438	1.645	1.069	i				
	33	1474+135.95	0.91	x2	2.07		2.11	13.05	-0.307	1.375	1.788	1			<b></b>	
	35	1474+336.12	0.91	)(2	2.49		2.41	13.07	0.612	1.944	2.527	1				
	37	1474+407.20	0.75	~~		<u> </u>										
					2.36		3.00	14.13	-4.529	4.648	2.052					
	38	1474+866.60	0.91		3.13		3.10	15.66	0.192	1.087	0.707				i	
	39	1475+198.60	0.61		3.38		3.38	15.96	0.000	0.000	0.000					
	40	1475+579.00	0.91		3.64		3.00	16.84	3.800	4.843	3.148					
	41	1475+710.75	0.61		4.69		4.83	12.90	-1.085	1.982	0.579	1			·	
	42	1475+845.15	0.61									!				
					4.68	- <b>4</b> ······	5.18	12.87	-3.885	3.751	1.096	1				
	43	1476+241.13	0.61		5.11		5.27	13,37	1.197	2.082	0.608	j				
	44	1477+010.70	0.91	x2	3.53	<b>~</b> 4	4.28	17.07	-4.394	5 208	6.771					
	46	1477+264.70	0.61		4.10	<b>-</b>	4.08	12.41	0.161	0.764	0.223					
	47	1477+431.20	0.75		3.94	<b>4</b>	4.05	16.14	-0.682	1.803	0.796				r	
- 1	0.48 %	14761007.00	0.91	1201213	्रक्रम <sup>्</sup>	1		NATURE.	50.00 <u>2</u> 50.002			5-63-86990673	PERSON.	\$5.500A.149A	E 222	
1				224 89 SE 1829			1.94		22 22 Age	0.000	0.000	SALL	10.00.24	200	DELETE-	
	49	1478+129.30	1.22		1.07		1.16	29.38	-0.306	1.672	1.953				1	
	50	1478+131.30	0.91	x2	1.11		1.26	29.33	-0.511	1.777	2.310					
	52	1478+258.95		2-1,30X1.80	0.53		0.65	22 98	-0.522	2.943	13.775					
	53	1478+386 80		1-2.40X1.80	-0.03		0.52	23.06	-2.385	8.271	35.730					
j	54	1478+650.75		1-3.00X2.20		4	2 52	23.27	-6.016	15.151						
	55	1479+177.95	0.61													
				x2	2.89	<b>-</b>	3.11	21.80	1.009	1.912	1.117					
	57	1479+407.45		x2	2.97	-4 -	3.39	14.56	2.885	3 232	1.888					
	59	1479+831.75	0.61		3.47		3.61	15.28	-0.916	1.821	0.532					
	60	1480+309.00	0.91		3.16	~ <b>4</b>	3.65	15.06	-3.254	4.481	2.913					
	608	1482+430.00	0.91		3.58	4	3.81	18.25	-1.260	2.789	1.813					
	61	1482+639.80		x2	2.85	<u> </u>	3.04	16.28	-1.167	2.684	3.489					
1	63	1482+700.92		x2	2.89		3 23	15.45	-2.201		4 792		•			
	65			x2		<b></b>				3.686						
		1482+817.95		**	2.84	<b>-</b> 4 ⋅ ⋅	2.99	17.49	-0.858	2.301	2.991					
	67	1483+200.01	1.22		3.65	⋖	3.94	16.13	1.798	4.050	4.732				1-0.61	
	68	1483+229.50	1.22		2.75		3.68	17.63	-5.275	6.938	8.106					
	69	1483+259.50	1.22		3.01	-ad	3.04	16.37	-0.183	1.293	1.511					
	70	1483+308.00	1.22		2.87	-4	3.10	16.76	-1.372	3.539	4.135					
]	71	1483+358.00	1.22	- <del></del> -	2.73		3.14	16.71					· .			
				<b> </b>	-	<u> </u>	<del></del>	1	-2.454	4.732	5.528					
	72	1483+398.40	1.22	- <u>-</u>	2.23	-41	2.41	16.64	-1.082	3.142	3.671					
1	73	1483+421.10		x2	1.63	4	2.36	15.85	-4.606	5.332	6 932					
1	75	1483+459.00	1.22		2.28	-44	2 36	16.92	-0.473	2.077	2 427					
1	76	1483+490.80	0.91	·	1.88		2.15	15.42	-1.751	3.288	2.137					
1	77	1483+560.50	0.61		2.10	-4	231	14.56	1.442	2 285	0.668				<b>-</b>	
				<del></del>		ļ									ļ	
ļ	78	1483+803.00	0.91	x2	2.36	4	2.72	13.96	-2.579	2.495	0.793				2-0.45	
	80	1484+634.80	0.91	x2	2.09	-44	2.16	14.29	-0.490	1.739	2 261					
	82	1484+828.00	1.22	L	2.39	- <b>∞</b> 4	2.62	16.53	-1.391	3.563	4.163					
	83	1485+046.42	0.91		3.40	-4	3.47	13.37	-0.524	1.798	1.169				· · · · · · · · · · · · · · · · · · ·	
	84	1485+908.98	0.61	] <del></del> -	4.20	- 10-	3.50	15.72	4.485	4.030	1.177				<del> </del>	
	85	1486+588.66	0.61	l	2.60	-01	290	13.55	-2 214	2.831	0.827	' 1			<del></del>	
		17007000.00	V.01	L	2.00		6 80	1 13.33	-2 219	2.031	V.021		ML The Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of the Later of th	-VIDEO CONTRACTOR		

DICK!	CE 4	1919)				LISI	Or v	OLVE	KIS						
PACKA	WE - 16	(212)					<del></del>					raca.			
	,, <u>,</u>		D. De	604	LT		RT	LENGTH	GRADE	v	Q	RD &	TD	AD	AF44.505
AREA	NO.	STATION	PIPE	80X	ELEV.	FLOW	EŁEV.	(m)	(%)	(m/s)	(m³/s)	SLOPE	(m³/s)	(m³/s)	REMARKS
<b></b>						ļ						(m3/s)			ļ
ļ	86	1486+632.60	0.61	<u> </u>	2.36		2.63	14.47	-1.866	2.599	0.759				ļ
	87	1486+654.20	0.61	x2	2.39		2.94	14.37	-3.827	3.723	2.175	Į I			ļ
	89	1486+685.00	0.61	x2	2.00	⋖-	2.38	14.47	-2 626	3.084	1.802				
l , l	91 92	1486+729.30	0.61	ļ	1.99	4	2.36	13.84	-2.652	3.099	0.905	Į į			
[ }		1486+895.00	1.22		1.35	⋖	1.37	15.67	-0.128	1.079	1.261		ĺ		[
	93	1486+897.00	0.61		1.42	⋖4	1.60	15.21	-1.183	2 070	0.605	Į .	1	1	·
}	95 98	1487+075.00	0.61		1.41	4	1.80	14 61	-2 642	3.093	0.903	Į l			
		1487+192 60	0.61	0 4 508 5	1.17	4	1.75	14.63	-3.958	3.786	1.106	<b> </b> -			
المما	97	1458+211.60		2-1.50X1.50	1.21		1.35	16.00	-0.875	3.928	17.678	[	-4.		1-0.91
18-1	98	1488+755.00	2.04	2-1.80X1.50	3.43	<b></b>	4.00	16.00	-3 594	8.612	46.504		51.0	65.0	1-0.91
	99	1488+943.60	0.61		4.41	<b>-⊲1</b> ·	4.78	16.73	-2 212	2.830	0.827				
	100	1489+450.00	0.91	<b></b>	5.00		5.50	19.50	-2.564	3.978	2.588			l	1-0.61
			0.61	2 4 90 7 4 50	5.26		5.32	19.44	-0.309	1.057	0.309				
18-2	102	1489+480.00		3-1 80X1.50	4.14	-di	4.65	16.00	-3.200	8.126	65.824		61.1	77.2	2-0.91
	104	1489+633 50	0.61	<u> </u>	4.00	<b>-46</b> · · · ·	4.80	15.57	-5.138	4.313	1.260				
<b>}</b> -}	105	1489+695.00	0.91	x2 x2	3.65		4.55	17.96	-5.011	5.562	7.231	<b></b>			1-0.91 Add'i
	108	1490+106.20 1490+259.20	1.22	x2	2.69	<u>-4 — </u>	3.09	18.53	-2.180	3.668	4.769				
18-3	109	1490+273.20	1.22	x2 x2	1.06	<b>-4</b>	1.44	19.74	-1.925	4.191	9.794				1-1.22 Addi
10-3	110		1.22		1.78	<b></b>	2.45	17.00	-3.941	5.997	14.013	<b>}</b>	51.4	55.1	l
	112	1490+546.60		x2	2.84		3.25	18.98	-2.415	4.694	10.969	Į			1-0.61
[ }	114	1490+720.00	1.22	x2	1.73	≪	1.95	16.00	-1.375	3.542	8.277	[			<u> </u>
107	116	1490+964.00 1491+158.60	1.22	x2 1-3.00X3.00	2.93 3.67	<	3.11	16.72	-1.077	3.134	7.324				2-0.91
18-4 18-5	118		4.60				3.96	13.95	-2.079	9.612	88.509	<b></b>	61.6	86.5	0.400
18-5	120	1491+566.50	0.91	x2	1.85		2.00	16.00	-0.937	3.386	24.568	]	15.6	27.9	2-1.22
18-6	121				2.40	-4	3.10	18.69	-4.194	5.088	3.308	<u> </u>			
15-0	122	1492+127.60	0.61	0 0 40 4 00	2.63	~	2.76	16.17	-0.804	1.706	0.498		37.9	46.8	
}i	123	1492+277.70	2-0.61	2-2.40x1.80	1.53		1.68	15.00	-1.000	5.355	46.271			ļ	1-0.61
18-7	125	1492+401.60	1.22	<b>]</b>	2.41		2.65	17.25	-1.391	2 245	1.311	]			J
10-7	126	1492+515.00	1.22	1 2 00 V 2 00	1.90		2.19	17.82	-1.627	3.853	4.502		31.8	75.1	
	127A	1492+980.00	1.22	1-3.00X3.00	1.70		1.99	17.25 17.00	-1.333	7.698	69.282	0004			
	1283	1493+285.30		12 32 6 8	4030	<b></b>	1000		0.000	0.000	0.000	0.021	E-1015-7875-	s Sacra de Cara.	A211 # A'6#
<b>,</b>	1403	1493+500	0.91	x2	1.76	<b>**</b>		13/12/5	600084	0.000	0.000	1800	b Man	<b>455</b>	OEL 1-0-61
18-8	129	1493+549.75	0.91	1X2 1X2	1.50		2.00 1.98	16.00	-1.500	3.043	3,956		00.0		Addi
'0-0	129	1493+700	0.91	X2	1.75			17.00	-2.824	4.175	5.428	l ' '	26.6	33.8	1-0.61
	130	1493+859.60	0.91	x2	1.07	4	1.52	17.00 17.00	-1.471 -2.647	3.013	3.917				Addi
	131	14934926.60	0.31	2-1.25x1.00	1.00		1.50			4.042	5.255				1-0.61
	132	1494+615.40	0.91	2-1.25(1.00				16.80	-2.976	6.083	15.207	ļ		ļ	1-0.61
	133	1494+821.00	0.91	<b> </b>	1.85		1.94	17.50	-0.514	1.782	1.158	ł ·			<u> </u>
	134	1494+821.00	0.91	ł	****			24.00	-0.875	2.324	1.511				<u> </u>
18.9	134	1495+414.70	0.31	2-2 00X2 25	1.21	<b>4</b>	2.00	18.65	4.252	5.123	3.330	J • ]	دمة	,,,	<b></b>
10.9	135		2-0.91	Z-2.00A2.25		<b></b>	1.60	16.78	-0.596	4.028	36.248		29.1	52.1	Addil
	137	1495+693.50 1495+893.60	0.61	ll	2.06	<b>~</b> € - · · - · ·	2.57	19.91	-2.562	3.976	5.170	Į į			
}	137	1495+893.60	0.91	<b> </b>	2.12	<b>4</b>	2.45	18.00	-1.839	2.580	0.754			'	
1 1	138	1498+426.60	061	25 AC	1.46		1.70	16.00	-1.500	3.043	1.978		and to facility to	\$25550000000000000000000000000000000000	Addi
1	* 17.3 E	1496+680.00	0.91	(*) S. 11. 12. 12. 12. 12. 12. 12. 12. 12. 12	APPLICATION OF	<b>€</b> 15%	\$ 38.95		3.000	0.000	0,000		LANGE	经税务	DELETE
		14907000.00	0.31	L	1.46	<b>4</b>	1.70	16.00	-1.500	3.043	1.978				Addil

PACKAGE-19

12 1501+997.50 0.91 15.27	1.0		(OE-1)													
1   191-6550   061	AREA	NO.	STATION	PiPE	вох	•	FLOW				_					REMARKS
Part		-	14974845 00	0.61									(m3/s)	(411.12)	(1175)	
No.   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State   State	1				l											1
A	ĺ			·	<del></del>				<del></del>							}
Fig.   1991/83170   061																<u> </u>
Part					<del></del>								0.136			<b></b>
Part	1 1				<b></b>								0.100			<u> </u>
8													0 333	1		
9				I ——	· i											<u> </u>
19-1   11   1501+80000   20-91   13-44		9					<b>D</b> ~									
12   1501-997.50   0.01   15.27     15.06   28.37   2.432   39.75   2.519	19-1	11		3			4							4.1	6.7	
March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   March   Marc	, ,	12	1501+997.50	0.91		15.27	⋖4	15.96			3.875	2.519		i		
192   15   1503/1962   0   13.03.00   10.55		13	1502+119.00	0.91		23.77	<b> </b>	22.77	25.36	3.943	4.933	3.207				
16   1504-1940   0   61   25   50   41   25   50   42   25   52   21   44   31   35   30   276   30   377   30   30   30   30   30   3		14	1503+097.40	0.61		18.32		15.88	19.18	2 294	2.882	0.842				
17   150412160 0 061	19-2	15	1503+392 20		1-3.0X3.0	10.58	-≪	11.03	15.13	-2.974	11.497	103.476		80.0	103.5	
18		16	1504+104.00	0.61		25.50	<b>⊲</b> 4	25.92	21.44	-1.959	2.663	0.778				<u>-</u>
19. 1   19. 19. 19. 19. 19. 19. 22   13.49		17	1504+219.60	0.61	1	27.56		29 24	19.67	-8.541	5.561	1.624				
155:1000   122		18	1504+378.40	0.61		29.11	P	29.70	22.66	-2.604	3.071	0.897				
20   1593123510   122	19-3	19	1504+947.50	1.22		13.49	<b>4</b>	13.96	52.55	-0.894	2.857	3.338		7.3	12.3	
21   150514100   0.91				1.22		2.15	4	2.62	19.00	-2.474	4.751	5.551			•	('bbA
22   15051884 20   122   27   25								16.99	38.00	-0.921	2.699	3.387				
23   1566+691 60   122	<b>i</b> 1				L		· 🌬		54.17	2.732		2.670	}			
24   \$5074035 50   0.91							<b>B</b> >-			10.118		11.227				
19.4   26   1507+319 60   1.22   12   12   20.55   14   21.75   30.80   2.273   4.554   10.641   0.344   13.3   16.9   11.122 Add1   19.5   27   1503+291.00   1.20   12.00   1.30   19.8   10.90   19.05   0.530   5.291   47.621   30.9   52.3   19.8   19.8   19.8   1503+291.50   0.91   2.20   21.60   19.05   0.530   5.291   47.621   30.9   52.3   19.8   19.8   19.8   1503+291.50   0.91   2.20   21.60   19.05   0.530   5.291   47.621   30.9   52.3   19.8   19.8   1503+291.50   0.91   2.20   21.60   1.20   21.60   17.00   1.765   4.013   4.669   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645   3.645				·												
26																<u> </u>
19-5   27	19-4				x2								0.344	13.3	16.9	1-1.22 Addi
28				1.22	ļ. <u></u>											<u> </u>
1508+50000   091   22   20.09   =   21.45   24.00   5.667   5.914   3.845   36.4   49.3   36.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   30.5   3	19-5				1-3.0X3.0	<u> </u>							į	30.9	52 3	<u> </u>
19-6   29		28			<b> </b>											
30	امدا			0.91	1 2 2 2 2 2											Addi
19.7   31   1509+1000   122   30.40   4   31.10   24.00   -2.917   5.159   6.028   7.6   18.1   31.1   1509+151.60   122   31.00   4   -2.752   29.50   11.797   10.375   12.122   7.6   18.1   31.1   1509+151.60   122   52.97   4   53.96   22.76   -4.350   6.300   7.361   30.2   118.8   32   1509+522.30   1.22   62.18   4   68.60   34.29   -18.723   13.071   15.222   0.026   34   1509+899.00   1.22   62.18   4   68.60   34.29   -18.723   13.071   15.222   0.026   34   1509+899.00   1.22   91.20   4   -91.28   14.89   -0.537   2.214   2.587   0.474   19.5   34.3   35   1510+043.40   1.22   91.20   4   -91.28   14.89   -0.537   2.214   2.587   0.474   19.5   34.3   35   1510+043.40   1.22   111.07   4   -113.52   17.62   -13.905   11.264   13.161   0.217   19.5   34.3   34   1510+051.50   1.22   128.38   4   -13.54   1.62   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.091   1.0	19-6			4 80	1-2.432.4									36.4	49.3	<u></u>
19.7   31   1509+151.60   1.22   31.00   ■   27.52   29.50   11.797   10.375   12.122   7.6   18.1		30														<del>   </del>
31A   1509+445.00   1.21   1.30x3 0   40.00   4   40.50   25.00   -2.000   9.426   84.653   32   1509+52230   1.22   52.97   4   53.96   22.76   -4.350   8.300   7.361   33   1509+270.00   122   62.18   4   68.60   34.23   -18.723   13.071   15.272   0.026   34.3   1509+899.00   122   80.31   4   82.53   21.44   -10.354   9.720   11.357   0.193   35   1510+340.00   1.22   91.20   4   91.28   14.89   -0.537   22.14   2.587   0.474   35   1510+340.00   1.22   111.07   4   113.52   17.62   -13.905   11.264   13.161   0.217   19.5   34.3   38   1510+601.50   1.22   128.38   4   -13.22   21.06   -13.485   11.033   12.961   0.280   38   1511+857.20   0.91   83.91		21			<del></del>		1									Addi
19-8 32 1509+522 30 1.22 52.97 ■ 53.96 22.76 -4.350 6.300 7.361 0.28 30.2 118.8 33 1509+620 00 1.22 62.18 ■ 68.60 34.29 18.723 13.071 15.272 0.026 34 15.09+899 00 1.22 80.31 ■ 82.53 1.44 -10.354 9.720 11.357 0.193 35 1510+043.40 1.22 9.120 ■ 91.20 ■ 91.28 14.89 -0.537 2.214 2.587 0.474 19-9 36 1510+340 00 1.22 111.107 ■ 113.52 17.62 -13.905 11.264 13.161 0.217 19-5 34.3 1510+601.50 1.22 128.38 ■ 126.91 28.34 -11.927 8.580 5.579 37 1210+571.20 0.91 128.38 ■ 131.22 1.06 -13.485 11.093 12.961 0.280 19-10 39 1511+857.20 0.91 8.991 ▶ 84.42 33.81 16.233 10.011 6.508 0.520 9.6 15.2 1511+365.72 0.091 122 68.90 ▶ 85.50 25.00 6.000 7.399 8.645 10.003 0.347 19-11 42 1512+585.52 1.22 68.90 ▶ 86.69 14.00 1.500 3.700 4.323 10.011 12.861 1512+585.52 1.22 60.82 № 48.30 31.00 8.129 8.612 10.063 0.347 11.091 14.10 ▶ 39.96 45.90 3.137 4.401 2.861 1512+585.50 0.91 41.40 ▶ 39.96 45.90 3.137 4.401 2.861 10.063 0.347 11.091 19-12 45 1512+589.50 0.91 36.74 ▶ 35.83 32.19 2.827 4.177 2.715 0.065 12.091 19-12 45 1512+589.50 0.91 36.74 ▶ 35.83 32.19 2.827 4.177 2.715 0.065 10.091 19-12 45 1513+585.40 1.22 ×2 9.73 ■ 9.10 16.00 3.938 5.994 14.007 5.6 14.00 1.0.91 19-13 47 1514+031.50 1.22 ×2 9.73 ■ 9.10 16.00 3.938 5.994 14.007 5.6 14.00 1.0.91 19-13 47 1514+031.50 0.91 10.50 ▶ 12.49 8.80 0.41 1.31 2.642 1.777 1.75 1.75 1.0.61 19-13 47 1514+031.50 0.91 10.50 ▶ 12.49 8.80 0.41 1.31 2.642 1.777 1.75 1.0.61 19-13 47 1514+031.50 0.91 10.50 ▶ 12.49 8.80 0.41 1.31 2.642 1.777 1.75 1.75 1.75 1.75 1.75 1.75 1.7	19-7			1.22	4 2 0 7 2 0									7.6	18.1	ļ <u>.</u>
33   1509+720 00   1.22   62.18   62.68   68.60   34.29   -18.723   13.071   15.272   0.026   34   1509+899 00   1.22   80.31   4   82.53   21.44   -10.354   97.20   11.357   0.193       35   1510+043.40   1.22   91.20   4   91.28   11.67   4   11.952   176.24   13.905   11.264   13.161   0.217   19.5   34.3       19-9   36   1510+340.00   1.22   111.07   4   11.952   176.24   -13.905   11.264   13.161   0.217   19.5   34.3       37   1210+571.20   0.91   123.53   4   126.91   28.34   -11.927   8.580   5.578       38   1510+601.50   1.22   128.38   4   131.22   21.06   -13.465   11.093   12.961   0.280       19-10   39   1511+857.20   0.91   8.9.91	10.0			122	1-3.0X3.0		1									L
34 15091899 00 122 80.31	13-0				ļ								0.000	30.2	118.8	ļt
35   1510+043.40   122   31 20   4   91 28   14.89   -0.537   2 214   2 587   0.474   19-9   36   1510+37.120   0.91   123.53   4   -126.91   28.34   -11.927   8.580   5.578   38   1510+601.50   122   128.38   4   -13.122   21.06   -13.485   11.093   12.961   0.280   19-10   39   1511+857.20   0.91   8.991							1						, ,			
19-9 36 1510·340·00 1 22 111.07					<del></del>											<del> </del>
37   1210+571 20   0.91   123 53   126 91   28 34   -11.927   8.580   5.578   38   1510+601.50   1.22   128 38   1-31.22   21.06   -13.485   11.093   12.961   0.280       19-10   39   1511+857 20   0.91   89.91	19-9						····							10.6	24.2	ļ[
38					1								0.211	19.0	U4.3	
19-10 39 1511+857 20 0.91 89.91 ► 84.42 33.81 16.238 10.011 6.508 0.520 9.6 15.2  40 1511+936 50 1.22 87.00 ► 85.50 25.00 6.000 7.399 8.645  1512+260 00 1.22 68.90 ► 68.69 14.00 1.500 3.700 4.323  41 1512+545.52 1.22 50.82 ► 48.30 31.00 8.129 8.612 10.063 0.347  19-11 42 1512+589 50 0.91 41.40 ► 39.98 45.90 3.137 4.401 2.861 4.171 2.715 0.065  44 1512+828.80 1.22 35.42 ► 33.13 29.00 7.897 8.488 9.918  19-12 45 1513+654.40 1.22 ×2 9.73 ◄ 9.10 16.00 3.938 5.994 14.007 5.6 14.0 1-0.91  48 1514+031.50 1.22 ×2 6.11 ➡ 6.39 26.00 -1.077 3.135 7.325 19-13 47 1514+130.40 2.1.50x1.5 5.31 ➡ 5.97 21.21 -3.112 7.408 33.338 37.5 43.1 2-1.22  49 1514+533.60 0.91 10.50 ► 12.49 26.90 -7.398 6.757 4.393 50 1514+63.30 0.91 9.16 ➡ 9.88 30.47 2.363 3.819 2.483 51 1514+763.30 0.91 9.16 ➡ 9.88 30.47 2.363 3.819 2.483 51 1514+763.30 0.91 9.10 10.00 ➡ 11.00 18.00 -5.556 7.120 8.319 19-14 53 1515+001.00 1.22 10.00 ➡ 11.00 18.00 -5.556 7.120 8.319 19-14 53 1515+001.00 1.22 10.00 ➡ 11.00 18.00 -5.556 7.120 8.319 19-18 53 1515+001.00 1.22 10.00 ➡ 11.00 18.00 -5.556 7.120 8.319 19-18 53 1515+001.00 1.22 10.00 ➡ 11.00 18.00 -5.556 7.120 8.319 19-18 53 1515+001.00 1.22 10.00 ➡ 11.00 18.00 -5.556 7.120 8.319 19-18 50 1.00 1.00 18.00 -5.556 7.120 8.319 19-18 50 1.00 1.00 1.00 18.00 -5.556 7.120 8.319 19-18 50 1.00 1.00 1.00 18.00 -5.556 7.120 8.319 19-18 50 1.00 1.00 18.00 -5.556 7.120 8.319 19-18 50 1.00 1.00 18.00 -5.556 7.120 8.319 19-18 50 1.00 1.00 18.00 1.00 18.00 1.00 18.00 1.00 1		38		<del></del>									0.280			
40	19-10	39			<b></b> -		· · · · · · · · · · · · · · · · · · ·	1						9.6	15.2	<del> </del>
1512+260.00   1.22   68.90		40	1511+936.50		1								0.020	0.0		1001
41			1512+260.00	1.22	l		<b>I</b>									
19-11 42 1512+589 50 0.91 41.40 ► 39.96 45.90 3.137 4.401 2.861 43 1512+725.00 0.91 36.74 ► 35.83 32.19 2.827 4.177 2.715 0.065 15.6 29.9 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.091 10.	1 1	41	1512+545.52	1.22	i	50.82	- b						0.347	1.		
43	19-11	42	1512+589.50	0.91	l	41.40		<del></del>						15.6	29.9	
44 1512+828.80 1.22 35.42 ► 33.13 29.00 7.897 8.488 9.918 1-0.91 19-12 45 1513+654.40 1.22 x2 9.73 ◄ 9.10 16.00 3.938 5.994 14.007 5.6 14.0 1-0.91 46 1514+031.50 1.22 x2 6.11 ◄ 6.39 26.00 -1.077 3.135 7.325 19-13 47 1514+130.40 2-1.50x1.5 5.31 ➡ 5.97 21.21 -3.112 7.408 33.338 37.5 43.1 2-1.22 49 1514+533.60 0.91 10.50 ► 12.49 26.90 -7.398 6.757 4.393 50 1514+643.30 0.91 9.16 ➡ 9.88 30.47 -2.363 3.819 2.483 51 1514+763.30 0.91 9.21 ➡ 9.53 28.30 -1.131 2.642 1.717 52 1514+903.00 1.22 10.00 ➡ 11.00 18.00 5.556 7.120 8.319 19-14 53 1515+001.20 1.22 10.00 ➡ 11.00 18.00 5.556 7.120 8.319 54 1515+096.00 1.22 10.97 ➡ 16.82 19.93 -4.354 6.303 7.365 0.082 55 1515+383.00 2.0.91 10.96 ➡ 11.89 52.27 -1.779 3.314 4.309 0.096	l i	43	1512+725.00	0.91	1	36.74	📂	35.83					0.065			
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46	19-12	45	1513+654.40	1.22	x2	9.73	4	9.10	16.00	3.938				5.6	14.0	
19-13 47 1514+130.40 2-1.50x1.5 5.31				1.22	x2	6.11	<b>⊲4</b> · ·	6.39	26.00							<del></del>
49 1514+533.60 0.91 10.50 → 12.49 26.90 -7.398 6.757 4.393 50 1514+643.30 0.91 9.16 ≪ 9.88 30.47 -2.363 3.819 2.483 51 1514+763.30 0.91 9.21 ≪ 9.53 28.30 -1.131 2.642 1.717 52 1514+903.00 1.22 10.00 ≪ 11.00 18.00 -5.556 7.120 8.319 19-14 53 1515+001.20 1.22 10.37 ≪ 11.18 26.89 -3.012 5.243 6.126 54 1515+096.00 1.22 15.95 ≪ 16.82 19.98 -4.354 6.303 7.365 0.082 55 1515+383.00 2-0.91 10.96 ≪ 11.89 52.27 -1.779 3.314 4.309 0.096	19-13				2-1.50x1.5	5.31		5.97	21.21	-3.112	7.408	33.338		37.5	43.1	L
51 1514+763 30 0.91 9.21 4 953 28 30 -1.131 2.642 1.717 52 1514+903 00 1.22 10.00 4 11.00 18.00 -5.556 7.120 8.319 19-14 53 1515+001 20 1.22 10.37 4 11.18 26.89 -3.012 5.243 6.126 54 1515+096 00 1.22 15.95 4 16.82 19.93 -4.354 6.303 7.365 0.082 55 1515+383 00 2-0.91 10.96 4 11.89 52 27 -1.779 3.314 4.309 0.096							···- • 🌬	12.49	26.90	-7.398	6.757	4.393				
52 1514+903 00 1.22 10.00 ◀ 11.00 18.00 -5.556 7.120 8.319 19.61 19.14 53 1515+001 20 1.22 10.37 ◀ 11.18 26.89 -3.012 5243 6.126 19.6 30.5 1515+096.00 1.22 15.95 ◀ 16.82 19.93 -4.354 6.303 7.365 0.082 19.6 19.6 19.6 19.6 19.6 19.6 19.6 19.6					<u> </u>		+		30.47	-2.363	3.819	2.483				
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54     1515+096 00     1.22     15.95     ■     16.82     19.98     -4.354     6.303     7.365     0.082     1-0.61       55     1515+383 00     2-0.91     10.96     ■     11.89     52.27     -1.778     3.314     4.309     0.096				<del></del>	<u> </u>	<del></del>	4		18.00	-5.556	7.120	8.319				1-0.61
55 1515+383.00 2-0.91 10.96 4 11.89 52.27 -1.779 3.314 4.309 0.096	19-14									-3.012		6.126	l i	19.6	30.5	
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5/ 1515+62/.50 0.91   10.09   4   10.90   29.66   -2.731   4.106   2.669								+					0.096			
	L	_57	1515+627.50	0 91	<u></u>	10.09	≪	10.90	29.66	-2.731	4.106	2.669				