2-4. Ore reserve estimation

2-4-1. Drill data

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The gold and porphyry copper exploration has been performed mainly by drilling in preference to geophysical and geochemical surveys in the Samarsky survey area because the area is covered by new sediments and there are few outcrops of rocks and almost no outcrop of mineral showings.

Drilling has therefore been adopted both for geological mapping (shallow holes that penetrate the sediment cover) and for exploration of copper and gold deposits. 595 mapping drillholes have been completed with a total length of 18,708m. Of a total of 76 gold and copper exploration drillholes, 46 have been used to delineate the copper deposit (representing a total drilled length of 27,976m). Twelve drillholes have penetrated the copper ore deposit in the central part of the Samarsky area.

Although exploration drilling was originally planned in a 100m x 100m rectangular grid pattern, this spacing was only utilized in the central part of the ore body and the average hole spacing is, in fact, 200m to 400m.

The present category of the confirmed reserve in the Samarsky survey area is C2. Drill locations are shown in Plate III-2-4-1 together with the boundary of the ore block. The copper-bearing part of the core sample was determined by semi-qualitative analysis of all cores.

After that only samples with high copper contents were separated and analyzed in the Karagandageologiya laboratory for copper, molybdenum, silver, gold and zinc. The analyzed sample units are basically 2m long core section.

These analyzed data are put in the hand-written chemical master file with their drill numbers and sampling depths.

For the preparation of the database of ore reserves in Samarsky deposit, analytical results were entered by the Japanese survey team using personal computers with spread-sheet-type software.

Because of time limitation in this year's survey, only data inside the Samarsky porphyry copper ore body were considered. The total number of drillholes entered is 30 and the total number of analyzed data is 2,197 sets.

2-4-2. Result of ore reserve estimation

In the Samarsky survey area two types of ore deposit have been discovered as mentioned above. This year, the Japanese survey team checked the geological ore reserve estimation for the Samarsky porphyry copper deposit. The copper deposit block is delineated by the conditions listed below:

(1) The cut-off grade of copper deposit is 0.5% Cu on the basis of studies by the Karagandageologiya on the engineering and economical conditions for the Samarsky deposit. The rich ore is defined by the value of Cu equal to or higher than 1.0%.

(2) In the case where the ore is intersected in two distinct layers separated by a length of country rock, the country rock and both intersection are considered to be one ore intersection provided: a) the length of included country rock does not exceed 15m and b) the length weighted mean of grades exceeds 0.5% Cu. If either of these conditions is not met then the intersections are considered separately (i.e. two different ore bodies).

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(3) If the ore intersection continues to the bottom of a drillhole then the length of intersection was assumed to extend for an additional 100m. As all the exploration drill holes are 600m deep, the maximum depth of the calculated geological ore block is 700m (about 200m above sea level).

(4) The panel/section method was used by Karagandageologiya to delineate the block ore body in plan. Parallel panel sections were arranged at 100m intervals along an east-west axis. The section view of the ore body on each panel was determined by the distribution of ore intersections in drillholes located in the plane of the section. The shape of the ore body in plan was determined by interpolating between neighbouring section.

(5) In cases where the extent of the ore body was not defined in any panel to the north or south an additional intersection of 0m was assumed at a distance of 100m. In this manner the ore body was closed in the north and south directions by wedges.

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The delineated block of the Samarsky porphyry copper deposit is shown in Plate III-2-4-4 together with the drillhole locations.

An ore body defined in this manner was used by Karagandageologiya to evaluate the geological reserves by the following method. (1) Area of ore in panels

A planimeter was used to determine the area of intersection of the ore body in the panels described above. The planimeter calculation was checked by summing the area of triangles fitted to the area of intersection.

(2) Average grade of panels

Average ore grade of a drillholes is calculated by the length-weighted average of each analyzed sample.

The calculation equation is as below:

Average grade of a bore hole= Sum of ((ore grade) x (ore length))

Sum of (ore length)

The panel average grade is calculated by the length weighted average of the average grade of drillholes in each panel. The calculation equation is as bellow:

Average grade of panel = ______ Sum of ((drill Av.grade) x (drill ore length))

Sum of (drill ore length)

The block average grade is calculated by the area-weighted mean of the average grades of all panels in a block.

(3) Volume calculation of a block

For volume estimation of ore, each block was calculated by either prism-equation, truncated-pyramid-equation or wedge-equation. In cases where the difference of ore area in the neighbouring panels was less than 40%, the prism-volume calculation equation was adopted. If the difference was more than or equal to 40%, the truncated pyramid-volume calculation equation was adopted. And in the case that ore extends beyond the last panel section, the wedge-volume calculation equation was adopted.

(4) Weight of ore

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In order to calculate the weight of ore reserves, Karagandageologiya utilized the average measured copper ore density of 2.76 t/m³.

The weight calculations in a block are as below:

The weight of ore reserve = (volume of ore body) x 2.76

Amount of each metal component = (weight) x (each ore grade %)/100

By summing these values, they obtained the geological ore reserve of the Samarsky porphyry copper deposit in early 1994. The result is listed in the Table III-2-4-1 together with the result calculated by the Japanese survey team.

The Japanese survey team checked the accuracy of the Karagandageologiya estimate by repeating the calculation using the same procedure.

In this operation the Japanese team adopted the same value of each analyzed sample, ore block delineation, cut-off grade and delineation condition used by Karagandageologiya. The panel area, block volume, density and average ore grade were calculated, and using these values, the weight and amount of metal in each block were determined. The subsequent summation of blocks gave the final geological ore reserve estimation. Except for the measurement and the calculation of ore block areas in panel sections, all other calculations were by personal computer using spread-sheet type software.

Comparing the geological ore reserves of Samarsky calculated by Karagandageologiya

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2	TEAM/Calc.	Japanese Survey Tean	Karagandageologiya	
ITEM		(1995)	(1994)	Note
		Geological Ore Reserve	Geological Ore Reserve	
Category	of Estimation	(not Mining Reserve)	(not Mining Reserve)	(1,1,1,1,1,1,1,1,1,1,1,1,1,1,1,1,1,1,1,
Calculati	on Method	Panel/section Method	Panel/section Method	in de la grafi
No. of Us	ed Drills	14	14	المراجع والمراجع
No. penet	rate Ore	12	1 2	
				Ratio(A)/(B)
Outline o	f Estimation	(A)	(B)	(%)
Dimension	Leng. (ENE) (m)	800	800	
of Dep.	Width(WNW)(m)	400(max)- 300	400(max)- 300	
Depth	Min. (m)	89	89	9
of Dep.	Max. (m)	612	612	
Averagé T	hickness (m)			
Yolume	(ŋ)	41,447,469	40,729,933	101.8
Ore Densi	ty	2.76	2.76	100.0
Orè Weigh	t (t)	114,395,015	112,414,616	101.8
	Cu (%)	1.28	1.24	102.8
Ore Grade	Mo (%)	0.01	not calculated	
	A g (g/t)	2.46	not calculated	.
	Au (g/t)	0.48	not calculated	-
	Cu (t)	1,458,777	1,397,806	104.4
Metal	Mo (t)	10,576	not calculated	1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 -
Amount	Ag (kg)	281,709	not calculated	ан <u>а</u> г 1
	Au (kg)	54,716	not calculated in	a, Alexa le ye
ee Alexandria Alexandria	1) Ore body b	oundary delineated by	the Karagandageologiya	is adoped.
Condition	It is the	bisector of drills pen	etrated ore and not pe	netrated.
of	2) Block volu	me is calculated by ei	ther prism or truncate	d pyramid
Calculation	depending	on the defference of s	ection area on end pan	el.
	In the cas	e of ore-pinch out, ve	dge volume calculation	ls adopted.
1. N. N. F.	3) The cut-of	f grade is 0.5%Cu. Int	erlayer is less than 1	5 m.
Results	1) There is n	o significant differen	ce in the results.	to bate o teneto.
	2) The differ	ence of values depends	on area and grade dif	ferences.

Table III-2-4-1Summary Table of Ore Reserve Estimationon the Samarsky Copper-Molybdenum Deposit

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and the Japanese survey team, similar values are observed, and are shown in Table III-2-4-1.

The total area of Samarsky ore block panels calculated by the Japanese survey team is $378,838m^2$ (99.0% of $382,663m^2$ of Karagandageologiya). Then the volume of ore body is $41,447,469m^3$ (101.8% of $40,729,933m^3$). Multiplying the conventional value of density, 2.76 (same value) the total ore reserve is calculated as 114,395,015t (101.8% of 112,414,616t).

The average copper content is 1.28%Cu (102.8% of 1.24%Cu) and the copper metal amount is 1,458,777t (104.4% of 1,397,806t) as calculated by the Japanese survey team.

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In these calculations of geological ore reserves some problems were identified. The most important problem is that only 12 drillholes intersect the ore body. From such a small number of intersections it is impossible to precisely delineate the ore body. The continuity of the ore block is therefore very uncertain at present.

Another problem is the density used in the calculations. The pyrite content of ore samples should also be considered in order to obtain more appropriate density values.

Finally the accuracy of chemical analysis of each element is not known. In the Zhaman-Aibat samples, the discrepancy is extraordinarily large indicating that it would be prudent to also check the analysis of samples of the Samarsky area.

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Appendix

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Appendix 1. Microscopic Observation of Rocks in Thin Section

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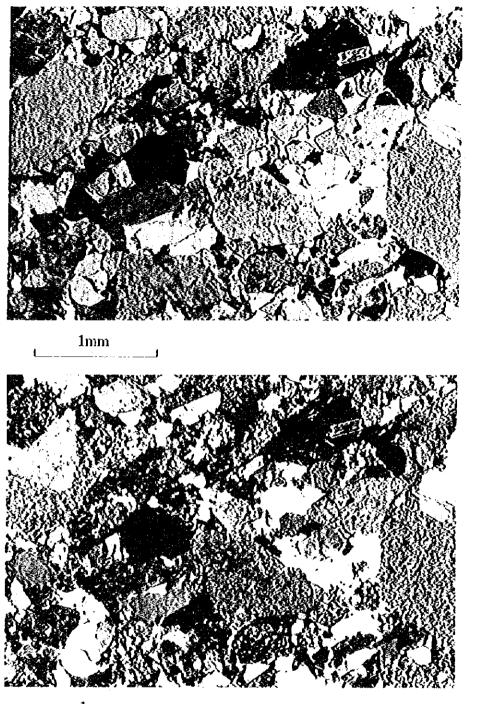
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	ture Identified Binerals			Feldspar: plagioclase. K-felkspar. 40%.	Muscovite, Opeque minerals, Goethite(?)				n Quartz:angular, 30%.	Feldspar:plagioclase. Opeque minerals.	Calcite (20v)	Dertz:angular, 40%.	Feldspartplagioclase.K-feldspar, 40%,	0therstchlorite, Coethite(?)				1 Quartz:angular. 30%.	Feldspar:plagioclase. K-feldspar, 40%.	Chlorite. Coethire. Biotic	Quartz:angular.20%	Feldspar:plagioclase. K-feldspar, 20%.	Nuscovite, Chlorite, Opcaue minerals	Calcito.Opeque minerals, etc.		Quartz:angular.20N	Feldspartplagioclase. K-feldspar, Perthire(?)	. 10%. Chlorite. Opeque minerals	Quartz:angular, 40%.	Feldspar:plagioclase. K-feldspor. Perthire(?)	.40%,	Rock fragment:10%. Others:10%.
	Nicroscopic Feature	Matriv-carbonitization			·	Natrix:carbonatization			Watrix:carbonitization			Matrix:carbonitization			Matrix:carbonitiaztion.ouatz.	plagioclase. K-feldspar.	chlorite, etc.	Matrix:carbonitization		•	Matrix:carbonitization			Micritic		Matrix: carbonitization			Matrix:carbonitizaton			
	Macroscopic Feature	Poor sorting.		AVELACE GLADE COLLO. DOBI O		Pebble size congls. : Max. dia 95mm d.	volcanic rocks. Limestone (micrites).	Chert	Average diameter:0.06mmx			Average diameter:0. Imm ø			Pebble size congls.: Nax. dia. 10mm × 6mm	Limestone (micritic). Chert. Sandstone		Average diameter:0.18mm ø	· · ·		Average diameter:0.05mm¢			Fossils:brachiopods, mollusca, etc.		Average diameter:0.05mm ø	Rocks fragment:limestone.chert.	volcanic rocks	Average diameter:0.5mm d	Rock fragment: limestone, chert.	volcanic rocks	
	Rock Name	Very fine-grained sandstone	(Red sandstone)			Carbonatized conglomerate	("Raimundo" conglomerate)		Lauinated very fine-grained	sandstone (Grey sandstone)		Yery fine-grained sands tone	(Grey sandstone)		Carbonatized conglomerate	<pre>("Interformational conglomerate")</pre>		Fine grained sandstone	(ked sandstone)		Coarse-grained siltstone	(Green aleurolite)		Fossiliferous limestone	(Blomicrite)	Coarse-grained siltstone	(Warl)		Coarse-grained sandstone	(Red-sands tone)		
	Formation	Cadz				Codz	•	1	Cadz			ZDC	•		Crts			Crts			វរ			Cis		uxiz	•		DZIJ			•
- H		314.0				673.2			381.2			2.020	,		132.0			912.0					• • •	\$11.5	Ē	· · ·			1.001			
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Sample No.: TS-2 DDH: 710 Depth: 673.2m Formation: Zhezkazgan Rock Name: Conglomerate

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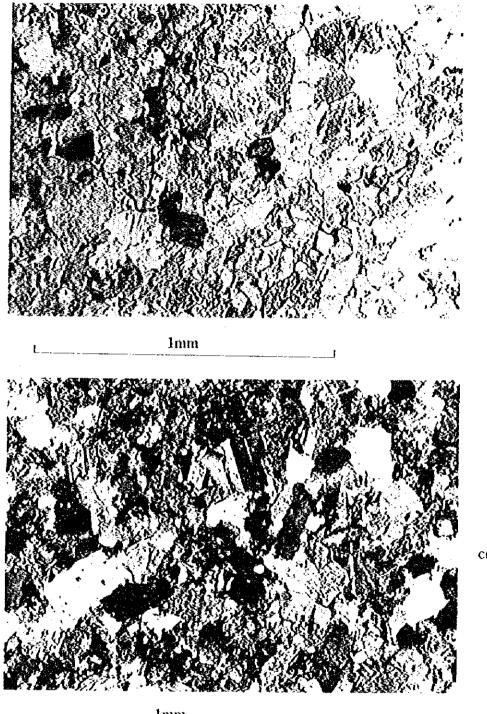
Photomicrographs of Rocks in Thin Section

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Sample No.: TS-3 DDH: 584 Depth: 381.2m Formation: Zhezkazgan Rock Name: Sandstone

Photomicrographs of Rocks in Thin Section

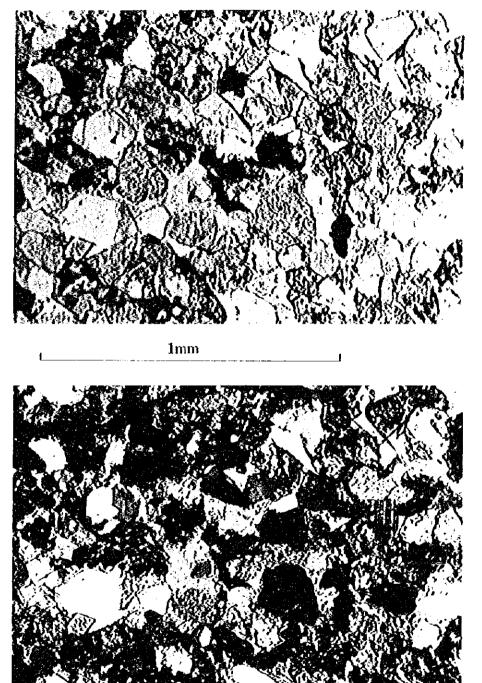
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Sample No.: TS--6 DDH: 577 Depth: 912.0m Formation: Taskuduk Rock name: Sandstone

Photomicrographs of Rocks in Thin Section

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010	from (m) to (m)	Orcbody /llorizon	Ore Type	Observation	Mineral composition (5) Mou MAK Co Ban Cc De Gui PV 65 So (5-15-
643.5 6	644. 05	Central/4-I	9 5 7	Wain constituent minerals are bornite chalcopyrite, sphalerite and galena, and small amounts of digenite, covellite and native silver are also identified under the microscope. These minerals, as an aggregate. fill parts of interstices of clastic particles.	2 2 2 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5
629. 45	630	Central/4-I	Gu ore	Chalcopyrite, pyrite and a small amount of goothite occur as interstices-filling minerals among clastic grains. Anhedral grains of pyrite are included in intersitial	35
635.3	635. 8	Eastern/3-Y	Cu ore	cuarropyrics Native copper and a small amount of digenite fill the lintersities of clastic marticles.	
575. 5	576	Eastern/4-1	Cu ore	Aggregates of chalcocite and digenite fill the interstices of clastic particles. Digenite occasionally occurs as lamella in chalcocite.	60 60 70 70 70 70 70 70 70 70 70 70 70 70 70
635.3	636.6	Eastern/3-V	oro ng	Round aggregates of chalcocite and a small amount of digeni te occur interstitially. Digenite is sometimes observed as llamella disenite in chalcoite aggregates.	35
624. 9	625. 7	Eastern/3-VI	Q. ore	Pyrite and small amounts of chairopyrite, covellite and goethite fill the interspaces of clastic particles. Chalcopyrite and covellite occur toghter as veinlets within interstitial pyrite.	× 1 80
	587.7 588.2	Eastern/4-I	Qu ore	Chalropyrite and small abounts of bornite and covellite fill parts of the intersaces of clastic particles. Bornite is often included in intperstitial chalcopyrite, and covellite occurs along fissures of some of rims of chalcopyrite.	3 2 2 2 2 2 2 3 3 3 3 3 3 3 3 3 3 3 3 3
	620.9 621.4	Contral/4-1	Cu-Ag ore	Chalcocite, bornite. digenite and small amounts of native silver, covellite and an unkroun mineral are constituent minerals. Chalcocite and bornite occur together, and are often found as graphic texture up to 12mo in max.size. Small grains of native silver (10-40 µm in size) are contained in digenite. An unknown mineral occurs as lamella in clalcocite. If's optical properties are: slightly darker than chalcocite distinctly birefectant (Greamy olive to bluish grey), and weakly anisotropic.	1 40 50 10 10 1
	681.5- 682.5	Central/4-I	Cu-Ag ore	Bornite. chalcopyrite. chalcocite.pyrite.mative silver. digenite and covellite fill the interspaces of clastic particles. Small grains of mative silver (40-50 µm in size) are found in the assemblage of bornite.chalcocite and digenite.	25 25
	636. 5 637. 4	637.4 Central/4-1	Cu-Pb orc	Galerra and small amounts of pyrite, bornite, chalcocite, digenite. germanite series mineral (probably colusite?) occur interstitially among clastic particles. Small grains of mative silver (20-40xm in size) are contained in galona grains. Germanite series minerals is brownish grey in color. slightly lighter than bornite, and isotropic. It is associated with bornite and galema.	

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Appendix 2. Microscopic Observation of Ore Minerals in Polished Section (2)

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No. Time (6) (6) (6) (6) (6) (6) (6) (6) (6) (7) (6) (7) (6) (7) (6) (7) (6) (7) (6) (7) (6) (7) (6) (7) (6) (7) (6) (7) (6) (7) (6) (7) (6) (7	Xo. 552(1Y)	from (m) ti					10Ae	Bn C	ľ	ĺ
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500 552.3 555.7 Bastrend's-11 Gue Poor examines of depicto.tete 50 30 10 582.5 565.4 Nerthernd's-1 Gue Poor Second of classic of control. Bastrend of control. 50 30 10 7.5 17.5 18.5 Takina Gue Poor Second of classic of classic of control. 10 5 56 4 10 7.6 17.5 18.5 Takina Gu or Second of classic of c	500 552(1V)	6 000								
355(11) 6£5.4 Werthermirkeri Charten and anome of calculation for theme. Anome of calculation for theme of calculation for theme of the of theme of theme of theme of theme of theme of the of theme of the of theme of theme of theme of the of theme of		7-070	628.7			amounts of digenite and galena. Bornite and chalcocite		8	01	
SSC(T) 685.4 Gerchenrefel Car-Th orion Intervention 1 0 1 1-5 17.5 18.5 Taskura Cu oro Controlity, and the matter of control of same strated. 1 0 1 1 1-5 17.5 18.5 Taskura Cu oro Controlity, and the matter of control of same strated. 1 0 1 1 1-5 18.5 Taskura Cu oro Controlity, and the matter of control of same strated. 1 0 5 5 1 1 1 1-5 18.5 Taskura Cu oro Controlity, and the matter of control of same strated. 1 1 1 1 1 1 1-5 18.5 Taskura Cu oro Controlity, and the matter of control of same strated. 1						occasionally occur as graphic texture. The second of a			<u> </u>	
15 11.5 18.3 Taskina Qu see Restruction of feature and small sector. As the interfact of the i		662.5	563. 4	Northern/4-1	Cu-Pb orc	interspaces of clastic particles. Large grains of				
75 17.5 13.5 Taskettar Qu uce Datatomic corrects and statil amounts of chalcopyrine statements. 10.0 Datatomic correct statements. Privatic corrects and born to secret statement. 10 5 26 20 10 10.0 External statements. Datatoment of constructions. 10 5 25 20 10 10 11.1 External statements. Datatoment of constructions. 10 5 25 20 10 10 11.1 External statements. Datatoment of constructions. 10 5 25 20 10 10 11.1 External statements. Datatoment of challocopies. Datatoment of challocopies. 25 26 <t< td=""><td></td><td></td><td>•</td><td></td><td></td><td>aggregates of galena(about.8mm × 5mm in size) include</td><td></td><td></td><td></td><td></td></t<>			•			aggregates of galena(about.8mm × 5mm in size) include				
7.5 17.5 18.5 Tatakura Qu orc convelition particle convelition particle 0 5 32 10 10 International convelition particle convelition particle convelition particle convelition 2 32 10 10 International convelition particle convelition convelition convelition 2 32 10 10 International convelition convelition convelition convelition convelition 2 32 2 20	-					prismatic crystais (0.2-1.200-10 lengun of sangue minerais. Chalcocite. digenite and small amounts of chalcopyrite.		· · · · ·		
chalcocite and contrace occur as related in the and contrace occur as related in the and contract and contrac		17.5				covellite.pyrite. sphalerite and bornite are constituent		5 35 20 10	÷	
2 3 0 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8				;		EXERCIALS. UNALCOPYLIC AND CONTICE OCCUPAS FULCES IN UNC assemblace of chalcocite. digenite and covelbile.				
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	•									
				•			_	auve copper		
	· · · ·		•		:			auve silver	<i>,</i>	•
	•							nalcopyrite Smite	•	
								unux jaleneite		
								venite		
			:		•			wellite		
	•		24					manite series mineral(?)(probab	ly colusite)	
60 7 ⁶⁹								rite		
7 09			•		ал А — — — — — — — — — — — — — — — — — — —			xethite		
					•			shalerite		
					•	7	•	alena		
			:					unknown mineral		
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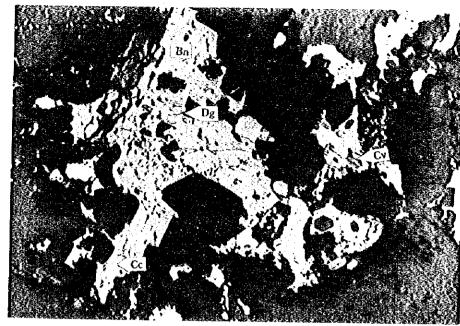
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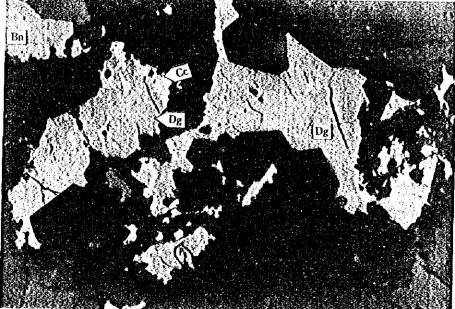
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Sample No.	:	P-1
DDH No.	:	179
Depth	:	643.50 ~ 644.05m
Orebody	:	Central
Ore horizon	:	4-I
Ore type	:	Cu Ore
Magnification		: × 100



Sample No.	:	P1
DDH No.	÷	719
Depth	:	$629.45 \sim 630.00 \mathrm{m}$
Orebody	:	Central
Ore horizon	:	4-I
Ore type	:	Cu Ore
Magnification		: × 200

Bn: bornite Cc: chalcocite Dg: digenite Cv: covellite

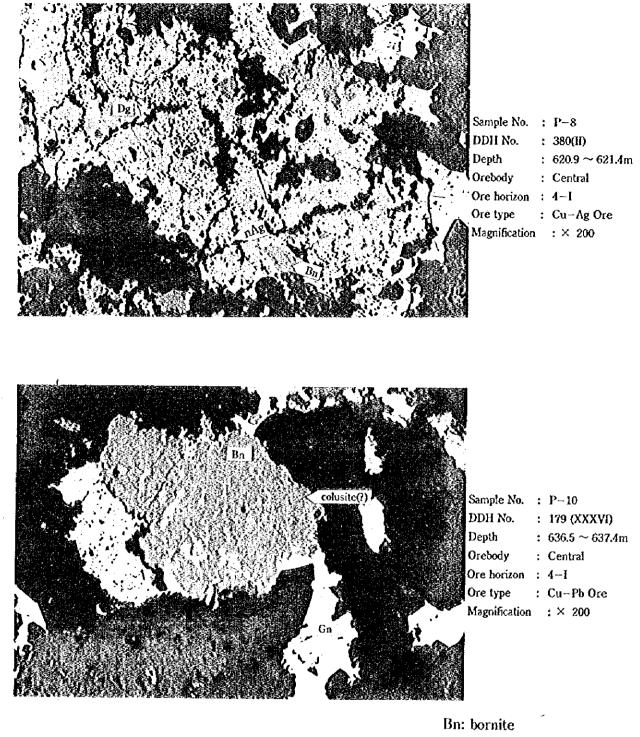
Photomicrographs of Ore Minerals in Polished Section

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Gn: galena Dg: digenite nAg: native silver



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Sample	HOO	Depth	Formation	S102	A1203	Ti02	Fe203	FeO	CaO	Mn0	Na20	Mgo	K20	P205	IOT	Total
No.	No.	E		(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	8	(%)	8	8	(%)
WRA- I	664	74.5	Pıka	21.2	4.01	0.2	0.76	1.53	32.5	0.11	1.45	6.98	0.97	0.1	29.7	99, 51
WRA- 2	577	130	Pizd	66.1	12	0.6	4.07	0.61	3.92	0.09	4.79	1.23	2.1	0.14	3.92	99.57
¥RA- 3	577	378	Csdz	68.8	12.7	0.57	2.68	1.1	60 60	0. 08	4.83	1.07	1.33	0.12	2.46	
¥RA- 4	584	404.6	Cadz	66.5	12.1	0.42	0.71	1.52	4.96	0.12	4.53	1.08	1.72	0.11	5, 01	
WRA- 5	389	601.8	Cadz	65.4	12.6	0.55	0.95	2.88	4.27	0.12	4	1.78	1.61	0.15	4.72	99, 02
WRA- 6	593	601.9	Csdz	60.2	16.7	0.64		4.43	1.63	0.13	1.63	2.65	3.95	0.16	4. 79	98, 79
WRA- 7	577	972	C2tS	49.2	11.4	0.39	2.14	0.87	12	0.08	5.05	1. 73	0.5	0.11	3.58	87.05
WRA- 8	753	330	C2ts	62.8	16.2	0.73	4.75	0.85	1,41	0.03	3.94	2.14	3.28	0.15	3.06	
WRA- 9	584	827.8	C ₂ ts	63.8	15.5	0.61	1.33	3.48	1.15	0.09		3. 37	2.29	0, 15	8	
FRA-10	373	1045	C1V3-5	27.9	5.39	0.22	0.65	1.47	34				· · · ·	2 C	2 2 2 2	

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Appendix 3. Whole Rock Analysis of Samples from the Zhaman-Aibat Deposit Area

			· · · ·			-
Serial	Sample	Au	Ag	Cu	Pd	Zn
No.	No.	(g/t).	(g/t)	(\$)	(%)	(\$)
1	2		6	2.09	0.01	0.01
2	3		13	4.82	<0.01	<0.01
3	4		8	3.2	0.01	<0.01
4	5		7	2.62	<0.01	<0.01
5	6	<0.1	au 19 - a	5.16	0.01	<0.01
6	10	· .	5	1.56	<0.01	0.01
7	13		22	4.28	0.02	0.01
8	14	in the second se	60	8.99	0.03	<0.01
9	17		24	6.24	<0.01	<0.01
10	19		11	2.43	0.05	<0.01
- 11 - • •	21	<0.1	26	5.49	0.1	<0.01
12	22		25	5.28	<0.01	<0.01
13	23		15	3. 72	0.16	<0.01
14	24		8	1.62	1.4	<0.01
15	28		- 14	7.04	0.01	<0.01
16	30	· · · ·	4	1.56	<0.01	<0.01
17	33	i	47	0.96	<0.01	<0.01
18	34		44	0. 92	<0.01	0.01
19	35		8	4.42	<0.01	<0.01
20	36	<0.1	<1,	0. 78	<0.01	<0.01
21	41	<0.1	 <1 ⊂ _	2.88	0.01	<0.01
22	42		3	1.43	<0.01	<0.01
23	43	н — — — — — — — — — — — — — — — — — — —	10	2.49	0.26	<0.01
24	44		10	2.24	0.81	<0.01
25	45		67	12.1	0. 03	<0.01
26	46	<0.1	26	6.24	<0.01	<0.01
27	47		24	6.32	<0.01	0.01
28	48		5	1.43	0.13	<0.01
29	49		13	3. 81	0. 04	<0.01
30	50	an a	17	4.02	<0.01	0.01

Appendix 4. Chemical Analysis of Ore Samples and Rock Samples (1) - Ore Samples -

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Serial	Sample	Au	Ag	Cu	Pd	Zn
No.	No.	(g/t)	(g/t)	· (X)	(%)	(5)
1	1	<0.1	2	0.25	0.38	0.01
2	7		<1	0.23	< 0. 01	0.01
3	. 8		2	0.5	<0.01	0.01
4	9		2	0.63	0.06	0. 02
5	11	<0.1	1	<0.01	<0.01	0.01
6	12		4	0.56	<0.01	0.01
7	- 15		1	0.35	<0.01	<0.01
8	16	<0.1	2	0.37	0.5	0. 07
9	18		2	0.43	<0.01	<0.01
10	20		<1	0.39	0. 09	0.01
11	25		<1	0.19	0.02	<0.01
12	26	<0.1	4	0.34	0.8	<0.01
13	27		<1	0.24	0.04	<0.01
14	29		. <1 -	0.46	<0.01	<0.01
15	31	<0.1	2	0.59	<0.01	<0.01
16	32		298	0.09	<0.01	<0.01
17	37			0. 07	0.01	0.16
18	38			0.64	0.01	0.3
19	39			0.07	0.06	0.39
20	40			0.15	0.17	0.07

Appendix 4. Chemical Analysis of Ore Samples and Rock Samples (2) - Rock Samples -

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Appendix 5.

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Data List of Analyzed Samples

in

the Zhaman-Aibat Copper Deposit

(Block-A)

ine	//ell .	Spi.	Sp1	Interval	Spl.	Spl.	Cu	% Cu	Pb	V DL	7. 4	17-	1	T
No.	No.	No.	From		Leng	feigh				· ·	Zn X		ng g/t	
213		11103	3 549.		0.6				- X	ade na X	grad	с п Х	grade	-
		3							*****				16.00	9.(
····				And Apple on Annual	0.5		0.5						0.90	0.1
		4(ter 🖌 🖌 🖌 🖌 🖌	The second second second	1.0		0.9						1.70	1.1
· · · · · ·		41			1.1	21.0	1.8	7 1. 9	<u>6</u>				5.60	5.8
		4/			0.8	17.0	0.0	6 0.0	5				0.00	
	· • • • • • • • • • • •	43	553.	5 554.2	07	13.0	0.0							
<u> </u>		44	554.		0.9	18.0	0.6						0.00	
		45		556.0	0.9	18.0	12.30						2.30	2.0
• • •	•••••	46	and the spectrum is a set								.			117.0
	· · · · · · · · · · · · · · · · · · ·	47			0.8	17.0	0.1						412.00	350.2
·····				· · · · · · · · · · · · · · · · · · ·	0.6	12.0	1.0					1	58.00	34.8
<u>.</u>	····.	48	11 Non-1993		0.7	13.0	0.98	0.6	{ [1.1			46.00	29.9
		111045			0.9	90.0	2. 30	11.0	7					117.0
		111046		556.8	0.8	90.0	0.12		***		···[·····	······		350.2
		111049	558.0	558.6	0.6	22.0	0.03				•••			930. Z
		50	558.6		0.8	34.0		(•		·····	0.00	
		51	559.5		0.6	22.0	·			····	··]·····	·····	·	
		52	560.0				••••••••							
•••••		11064			1.0	40.0			-				.	
·····	·····		568.8		0.4	12.0	0.65			2 0.17	0.97	0.39	2.40	0.9
		65	569.2		0.4	12.0	0.55	0. 22					3.30	1, 3
		66	569.6	570.0	0.4	12.0	4.29	1.72	0. 65	0.26	1		16.80	6.7
		67	570.0	571.0	1.0	30.0	0.09		er an		•••••••	•••••••	1.60	1.6
		68	571.0	571.6	0.6	18.0	0.22			0.36				
	. d. 1	69	571.6	572.0	0.5	13.5	4.18			· · · · · · · · · · · · · · · · · · ·		0.00	2.40	1.4
		70	572.0	572.9	0, 8	34.0	0.13					0.08	19.50	8.71
		•••••••••				V4. V	U. 13	0.11	0.88	0.75			0.90	0.71
		11066	569.6	570 0		<u> </u>			· .					
·····		11069		570.0	0.4	90.0	4.29	1.72		0.25			16.80	6.72
	····	11003	571.6	572.0	0.5	90.0	4.18	1.88	7.20	3.24	0.18	0.08	19.50	8.78
••••••				ينبيه بيبينية										
	.,	11083	581.5	582.0	0.5	20.0	0.47						2.30	1.04
			<u></u>					1				•••••		x+ V9
	1	11088	584.3	585.2	0.9	45.0	0.85	0.77	0. 59	0.53		••••••	5.90	E 04
	• . !	89	585.2	586.2	1.0		0.04	0.04		0.00	•••••••			5. 31
		90	586.2	587.2	1.0		0.03	0.03			· · · · · · · · · · · · · · · · · · ·		0.00	
		91	587.2	587.8									0.00	
	••••••	92	587.8	588.5			0.56	0.36	<u>.</u>		· · · · · · · · · · · · · ·		2.30	1.50
	· · · · · · · · · · · · · · · · · · ·	93	588.5				1. 22	0.79					3.40	2.21
·			300. 3	589.3			1. 21	0.97					2.00	1.60
		94	589.3	590.2		18.0	0.96	0.86	1.1				3.80	3.42
		95	590.2	590.8	0.6	12.0	3.45	2.07						15.84
. <u></u>]		96	590.8	591.5	0.7	13.0	2.15	1.40					14.20	
		97	591.5	592.4			0.06	0.05	•••••		•••••••••••••••••••••••••••••••••••••••		1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1	9.23
		98	592.4	593.1			0.87	0.66			••••	··-··· [·	0.00	
T		99	593.1	594.0			1.44		 		[]	·····].	1.00	0.75
		100	594.0	595.0				1.30		[·····	·		1.00	0.90
••••	·····	101	595.0	595.7			1. 91	1. 91			[1.80	1.80
· · · •				A REPORT OF A R			1.95	1.27		[ľ	1.40	0.91
····		102	595.7	596.4	0.8	15.0). 76	0.57					1.00	0.75
				·····								1	······	
		1095	590.2	590.8	0.6	90.0	3. 45	2.07					26.40	15.84
	11	1103	596.4). 27	0.16	• • • • • • • • • • • • • • • • • • • •	•••••••		······		10.04
		104	597.0				. 05	0.04		· · · · · · · · · · · · ·	· · · · · · · · · · · · · · · · · · ·		0.00	
	j l		597.8				. 49	0.27		·····			0.90	0.72
I			598.4								·····	· · · · · · · · · ·	7.20	3.96
	•••••		·····	000.0	<u>v. ə 4</u>	1.5	48	0.46					3.00	2.85
		1100				.				[1		
····	····[#.#.	1109	601.3	602.4	0.9 12	0.0 0	. 05	0.05	0.28	0.27		·····	0.60	0. 57
		.		I	<u> </u>	ľ					····	•••••••••••	····	<u></u>
	11		602.2	603.0	0.8 4	8.0 0	. 16	0.13	1.42	1.14			2 10	
		111	603.0					0.20	1.80		[2.00
	1									0.81				1.13
•••	····[····	· • • • • • • • • • • • • • • • • • • •	· · · · · · · · · · · · · · · · · · ·	VV3. V	<u>v. v. 4</u>	<u>v. v 0</u>	. 09	0.07	0.01	0.01			0.50	0.38

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						. 1		•							
	Line No.	Vell No.	Spl. No.	Spl.In From	terval To	Spl.	Spl.	Cu X	Cu	Pb X grade	Pb	Zn X grade	Zn n•X	Ag g/t grade	Ag m·g/t
	<u>av.</u>	<u>av.</u>	<u>ao.</u> 113	604.3	605.0	Leng. 0.8	Weight 30.0	grade 0.90	0.68	RISOO	B A	SIGUE	IL A	1.00	0.75
	· • • • • • • • • • • • • • • • • • • •		114	605.0	605.8	0.8	30.0	1.27	0.95					9.50	7.13
			115	605.8 606.4	606.4 607.0	0.7	26.0	1.73	1.12 1.12					8.40 8.60	5.46 5.16
			117	607.0	607.5	0.5	18.0	0.61	0. 27					3.50	1. 58
	·····.		111126	624.0	624.7	0.7	21.0	0.69	0.48			······		4.00	2.80
-	· · · · · · · · · · · · · · · · · · ·	·····	127	624.7	625.2	0.5	15.0	2. 58	1.29	·····			1	16.00	8.00
1			128 129	625.2 626.0	626.0 626.7	0.8	25.5	0.93 7.60	0.79	0.05	0.03			4.40	3.74 25.35
2	213	553	111130	626.7	627.3	0,6	18.0	3.55	2.13					14.00	8.40
		·	- 131	627.3	628.3	1.0	30.0	2.62	2.62					11.00	11.00
	•••••		111129	626.0	626.7	0.7	65.0	7.60	4. 94	0.05	0.03			39.00	25. 35
	213	553	111130	626.7	627.3	0.6	60.0	3. 55	2.13				- 175 	14.00	8.40
:	221	554	111178	536.4	537.0	0. 6	55.0	0. 41	0. 23					0.50	0.28
;			179 180	537.0 537.4	537.4	0.5 0.8	50.0	0.10 1.42	0.05	0.19	0. 14			1.50	0.75 3.75
2	انه م ا		IOV	331.4	330.2	V. 0	10.0	1:46	1.07	V. 13	U. 14			3.00	9. IJ
			111194 195	546.9 547.5	547.5	0.6	18.0 15.0	0.47	0.28	····				3.00	1.80
			195	548.0	548.8	0.8	24.0	0.09 0.46	0.05	·		· · · · · · · · · · · · · · · · · · ·	·····	2.30	1.84
		 	197	548.8	549.3	0.5	13.5	1.61	0.72					3.50	1.58
	·····		198 199	549.3 550.2	550.2 550.9	0.9	27.0	0. 12 0. 25	0.11 0.19			······		1.20	1.08
	221		111200	550,9	551.4	0.5	15.0	0.82	0. 41				1944. 	1.60	0.80
	187	500	107593	637.1	638.1	1.0	2.4	0.08	0.08					1.60	1.60
1. and 1.		·····	107594	638.1	639.1	1.0	2.5	0.10	0.10					0.60	0.60
	207	535	107595 109522	639.1 570.9	639.8 571.5	0.7	1.4	0.07 0.17	0.05	0.04	0.02	· · · ·		0.60	0.42
													·····		
	193		109120 109121	623.0 623.5	623.5 624.5	0.5	1.2	0.42	0.21			. :		4.30 2.60	2.15 1.30
•															
-	193	377	17122	595.6 596.7	596.7 597.5	1.1		0.08	0.09						
÷	.	initian. Initian	17124	597.5	598.1	0.6		0.11	0.07					2.30	1. 38
-	.		17125	598.1 599.0	599.0 599.8	0.9	1000 - 1000 	0.16 0.38	0.14	3.				3.40 3.50	3.08 2.80
1.4.4.4.4.4.4.4.4.4.4.4.4.4.4.4.4.4.4.4		المانية. المحديقة									· • • • • • • • • • • • • • • • • • • •	<u> </u>			
4	211	255	30042	600.6	601.5	0.9	2.2	3.16	2.84		- <u></u>			7, 30	6.57
	195	261	30163	628.8	629.7	0.9	2.0	0.00	0.00					0,00	
1.1	213	298	30167 31136	870.4	871.4 522.5	1.0	1 2	A.11	0.06				· · · · · · · · ·	3.30	1.65
1	213	610	31130	522.0	J66. J	0.5	1.2	0.11	0.00					3. 30	1.65
			31203	531.3	531.8	0.5	1.4	0.14	0.07	0.00		0.18	0.09	9.50	4.75
			31204	531.8	532.3	0.5	1, 1	0.00		0.32	0.16	0.34	0.17	2, 30	1.15
1			ł					·····	, 						
	:		31205	532.3	532.8	0.5	1.0					0.38	0.19	1.70	0.85
•		1	31206	532.8	533.3	0.5	1.0	0.23	0.12				· · · · · · · · · · · · · · · · · · ·	8.60	4.30
1	193	377	17119	593.5	594.6	1.1				•••••••••••••••••••••••••••••••••••••••				7.40	8.14
							1			.					

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	line	fell	Spl.	I Spl D	nterval	Spl.	Spl.	Cu X			DL	17. N		: • · · · /•	·····
	No.	No	No.	From	To		veight		Cu m•X	Pb % gradě	Pb	Zn X grade		lg g∕t	Ag
1			17123	596.7	597.5	0.8	i es sire	Scout		Reade		RISO		grade	<u>m·g/t</u>
	207	400	18994	628.2	629.3	4.1	3.0	1.61	1.77		· · · · · · · · · · · · · · · · · · ·			53.00	58.30
1	209	415	18895	541.5	542.3	0.8	5.0					·····		5.40	4.08
×			18920	560.8	561.7	0.9	7.0							4.70	4.23
ŝ	213	423	103659	568.3	569.3	1.0	2.4	0.12	0.12	0.20	0.20	41.00	0.41	6.00	6.00
			103726	597.9	598.4	0.5	1.2	0.05	0.03					4.90	2.45
			103727	598.4	598.9	0.5	0.9	0.00						5.80	2.90
2			728	598.9	599.7	0.8	2.2	0.03	0.02	0.15	0.12	1.1		7.10	5.68
	213	670	118458	557.9	558.4	0,5	1.1	0.37	0.19			:		9.20	4.60
1		·	469	558.4	559.2	0.8	2.0	0.03	0.02					1.00	0.80
÷	· ·	<u></u>	470	559.2	559.7	0.5	1.5	0.56	0. 28	0.11	0.06	0.40	0.20	6.30	3.15
	· · · · · · · · · · ·		471	<u>\$59.7</u>	560.7	1.0	2.6	0.08	0.08			0.05	0.05	3.10	3.10
			473	561.7	562.7	1.0	2.3	0. 22	0.22			0.06	0.05	1.90	1.90
5			474	562.7	563.5	0.8	1.5	0.31	0.25		·····	0.18	0.14	3.90	3.12
	213	670	475	563.5 564.5	564.5	1.0	2.3	0.39	0.39	· · · · · · · · · · · · · · · · · · ·				4.30	4.30
÷.	235		116082	476.4	565.0 477.3	0.5	1.0	0.94	0.47		A		· · · ·	8.80	4.40
	633	V16	83	477.3	477.8	0.9	2.0	0.05	0.05	0.08	0.07	· · · · · · · · · · · ·	ري. 1997 - محمد ماري	1. 20	1.08
	····#··· ·		84	478.8	479.3	0.5	1.1	0.52 0.23	0.26	·····		· · · · · · · · · · ·		2.40	1.20
		 2	116093	484.4	484.9	0.5	1.1 1.1	3.16	0.12 1.58	· • • • • • • • •	· • · · · · · · · · · · · · ·			1.20	0.60
:			116103	477.8	478.8	1.0	2.6		10.80	•••••				34.60	17.30
	231		115543	515.9	516.8	0.8	2.0	0.78	0.66	0.03	0.03	••••••	·	67.00	67.00
:			544	516.8	517.6	0.8	2.0	0.25	0.21	<u>v. v.</u>	0.00	······		1.40	1.19 0.51
:			545	\$17.6	518.2	0.6	1.1	0.19	0.11	:		•••••	•••••	0.00	V. 01
			546	518.2	518.8	0.6	1.0	0.05	0.03			•••••	••••••	0.00	·····
:			547	518.8	519.2	0.5	0.7	0.04	0.02			······	••••••	0.00	
1		· .	548	519.2	519.6	0.9	0.8	1.44	0.58		••••••••			8.20	3.28
	231		115549	519.6	520.1	0.5	1.2	1.90	0.95	·				11.60	5.80
÷	225	619	116054	524.4	524.9	0.5	1.0	0.29	0.13					1.00	0.45
		ş.i	55	524.9	525.8	0.9	2.2	0.10	0.09			2.5		0.00	
	· · · · / · · • ·		56	525.8	526.4	0.7	1.5	0.04	0.03					0.00	
		·····	57	526.4	526.9	0.5	1.3	0.22	0.11					0.50	0.25
s N			58	526.9	527.5	0.7	11	0.11	0.07					0.00	
	••••••		59	527.5	528.1	0.6	1.6	0.51	0.28				·····	1.00	0. 55
$\frac{1}{2} = \frac{1}{2}$			60 61	528.1 528.7	528. 7 529. 5	0.7	1.6	0.41	0.27	. <u>.</u>	· · · · · · · · · · · · · · · · · · ·			1.60	1.04
·			62	529.5	530.4	0.8	2.1	0.05	0.04	•••••	·····	····		0.00	
		·····	83	530.4	531.3	0.9	2.3	0.03	0.03	0.15				0.00	
. :		·····		531.3	531.8	0.5	1.2	0.11	0.05	0.15	0.14	•••••	•••••	0.50	0.45
			64 65	531.8	532.4	0.6	1.4		0.03	· · · · · · · · · · · · · · · · · · ·	· · · · · · · · · · ·			0.50	0.25
			66	532.4	533.3	0.8	2.1	0.54	0.46				·····	3.40	0.48 2.89
	225	619	116067	533.3	534.1	0.8	2.0	0.33	0. 28	• • • • • • • •	· · · · · · · · · · · · · · · · · · ·		· · · · · · · · · · · · · · · · · · ·	3.10	2.63
	231		117650	504.1	504.9	0.8		0.28	0. 21	·····			· · · · · ·	3.00	2. 25
			651	504.9	505.4	0.5	1.1	0.02	0.01					0.00	D. 20
		: 	652	505.4	505.9	0.5	1.1							0.00	
			117659	505.9	505.4	0.5	1.2	0.04	0.02	5.80	2.90		· · · · ·	6.60	3. 30
	231		17661	511.0	\$11.5	0.5	1.2							2.50	1.25
	233	649	17611	485.3	485.9	0.5	1.4	0.41	0.25					2.80	1.68
	6.0.0	·	612	485.9	486.4	0.5	1.1	0.37	0.19					1.80	0.90
	233		17613	486.4	487.1	0.7	1.7 1.3	0.71		0.15	0.11			2.50	1.75
	199	103	19682	596.1	596.6	0.5	1.3	0.28	0.14		· · ·	0.11	0.06	1.40	0.70
		·····	683	596.6	597.1	0.5			0.02					0.50	0. 25
- 2			684	597.1	597.7	0.6				0.10		0. 91	0.50	0.70	0.39
	•••••		685 686	597.7 598.2	598.2	0.6							0.06	0.70	0.39
			687	598.8	598.8 599.2	0.6							0.22	0.60	0, 36
			688	599.2	599.9	0.5							0.08	3.90	1.75
	•••••••			599.2	600.9	0.9							0.16	1.90	1.33
		I.					<i></i>	V. IV	<u> </u>	V. 10	0.15	0.46	0,44	1.10	1.05

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Line	¥ell	Spl.	Spl. In	ferral	Spl.	Spl.	Cu X	Cu	Pb X	Pb	Zn X	Zn	Ag g/1	A a
No.	No.	No.	From	To		Weight			grade		grade		grade	Ag m•g∕t
		690	600.9	602.0	1.1	2.6	1.16	1.22	0.13	0.14	A1 440		1.70	1. 79
		691	602.0	602.7	0.8	1.8	3.11	2.33	0.03	0.02			12.70	9. 53
	·······	692	602.7	603.2	0.5	1.2	0.73	0.37					3.60	1.80
		119714	620.5	621.1	0.6	1.4	2.08	1.25					61.50	39.60
		715	621.1	621.9	0.8	1.5	0.01	0.01	·····			<u>،</u>	0.50	0.38
· · · · · · · · · · · · · · · · · · ·		716	621.9	622.4	0.5	1.2	0.01	0.01	· · ·		· · · · · · · · · · · · · · · · · · ·			
		717	522.4	622.9	0.5	1.2	0.01	0.01						
		718	\$22.9	623.5	0.7	1.5	0.84	0.59					2.30	1.61
		719	623.5	624.2	0.7	1.8	0.02	0.01					0.00	
		720	624.2	625.0	0.8	1.8	0.02	0.02					0.00	
		721	625.0	626.1	1.1	2.2	1.35	1.43			- 1 -		24.50	25.73
199	709	119722	626.1	626.6	0.\$	1.2	1.41	0.71					32.20	16.10
197	720	120008	616.6	617.1	0.6	1.4	0.24	0.13					1.00	5. 50
		120010	617.9	618.6	0.7	2	D. 001		0.39	0.27			0.5	0.35
		120013	620	620.7	0.7	2	1.88	1. 32	0.48	0.34			7.3	5.11
e e e e e e e e e e e e e e e e e e e		14		621.35	0.65	2.3	0.23	0.15	0.01	0.01		- 11 A	1.4	0.91
				622.05	0.7	2	0. 21		0.001				0.9	0.63
			622.05	622.6	0.55	1.3	2.58	1.42					7.3	4.02
		17	622.6	623.4	0.8	2.5	1.78	1.42					1.8	<u>1.44</u>
		18	623.4	624.4	1	2.8	3. 77	3.77				2.111 	3.7	3.7
	·	19	624.4	625.1	0.7	2	1.97	1.38			· · · · · ·	يەر 	2.4	1.68
102	200	20	625.1	625.8	0.7	1.8	1.92	1.34	····			1 9 1 1 1 1 1 2 1 1 1	4	2.8
197		120023	626.9	627.4	0.5	1.5	0.29	0.15	A 10	A 16	0.10	A 45	0.9	0.45
201	122	120365	612.5 615.2	613.5 616.2	1	2.5	0.26	0.26	0.18	0.18	0.15	0.15	1.3	1.3
		369 370		617.1	0.9	2.6	0.02	0.02	0.23	0.23			0.001	
		371	616.2 617.1	617.8	0.9	2 1.9	0.1	0.09	0.15	0.14	······		0.001	
		120373		619.05	0.85	2.2	0. 52	0.36	V. VI	V. VI	·····	•••••	0.001	
				619.05 519.75	0.03	1.5	0.95	0. 67			••••••		0.001	· • • • • • • • •
			619.75	620.4	0. 65	1.6	1.71	1.11		· · · · · · · · · · · · · · · · · · ·			0.001	
		376	620.4	620.9	0.5	1.2	0.99	0.5	······				0.001	·····
		317	620.9	621.4	0.5	1.1	0.24	0.12		·····			0.001	
		120379	621.9	622.4	0.5	1.1	1.33	0.67		·····	••.•		0.00	
		380	622.4	623.0	0.7	1.5	1.29	0.84	••••••				0.00	••••••••••••••••••••••••••••••••••••••
		381	623.0	623.7	0.7	1.5	2.11	1.37		• • •	· · · · · · · · · · · · · · · · · · ·		0.00	
201	122	120382	623.7	624.7	1.1	2.5	0.60	0.63					0.00	
201		120372	617.8	618.2	0.4	1.0	3.96	1.58					0.00	
207		120439	\$68.0	568.7	0.7	1.6	0.24	0.17	0.08	0.06			0.60	0.42
		440	568.7	569.4	0.7	1.7	0.14	0.10			0.03	0.02	0.00	
		441	569.4	570.5	1.1	2.6	0.26	0.27	2. 				1.30	1.37
		442	570.5	571.2	0.7	2.0	0.14	0.10					0.70	0.49
		443	571.2	571.8	0.7	1.5	0.30	0.20					0.70	0.46
		444	571.8	572.4	0.6	1.4	0.44	0.26					2.20	1.32
) 		445	572.4	572.9	0.5	1.1	1.88	0.85				· · · · · · · · · · · ·	12.40	5. 58
s		446	572.9	573.5	0.6	1.4	0.09	0.05				· · · · ·	0.50	0.30
<u>, , , , , , , , , , , , , , , , , , , </u>	مندروا	447	573.5	574.0	0.6	1.5	0.06	0.04						مىلىيىتىيىلەت
i India		448	574.0	574.6	0.5	1.2	3.05	1.53	·····			· · · · · ·	16.00	8.00
1		449	574.6	575.0	0.5	1.2	6.25	3.13			•••••		21.70	10.85
		120450	575.0	575.6	0.5	1.4	0.42	0.21			·····		1.00	0.50
1.1.1.1.1.1.1	مار <u>ب</u>	451	575.6	576.0	0.5	1.2	0.16	0.08			••••••			
		452	576.0	576.5	0.5	1.2	0. 98	0.49	····		· · · · · · · · · · · · · · · · · · ·		2.00	1.00
207	726	120453	576.5	577.6	1.1	2.5	2.61	2.87		·····	· · · · · · · · · · · · · · · · · · ·	<u>n - 1</u>	4.40	4.84
225	715	120231	618.2	619.2	1.0	2.6	0.20	0.20	·····		· · · · · · ·		0.90	0, 90
···		232	619.2	619,9	0.7	2.0	0.45	0.32				[2.90	2.03
		120238	623.1	623.6	0.5	· 1.4	0.46	0.23					1:40	0.70
		120244	628.1	628.6	0.5	1:3	0.85	0.43					0.70	0.35
4 	· · · · · · · · · ·	245	628.6	629.1	0.5	1.4	0.37	0.19	·····	······	· · · · · · · ·		1.10	0.55
۰ ۱	I	246	629.1	630.2	1.1	2.8	0.12	0.14	l	I	ľ	b	0.75	0.85

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ine	Well	Spl.	Spl. I	iterval	Sp1.	Spl.	Cu X	Cu	Pb %	Pb	Zn X	Zn	Ag g/t	A
No.	No.	No.	Fron	To	Leng.	Weight			grade		grade		grade	m•;
		120248	630.9	631.4	0.5	1.2	2.98	1.49	<u> </u>		9.00		12.90	6
		249	631.4	632.0	0.6	1.5	0.14	0.08				· · · · · · · · · ·	1.00	Ŏ
••••••••• :		250	632.0	632.6	0.6	1.5	0.32	0.19			· · · · · · · · · · ·	·····	2.00	
		251	632.6	633.0	0.4	1.3	1.95	0.78		·····;·				1
•••••	· · · · · · · · ·	252	633.0	633.8						·····	•••••••••		16.30	6
••••••					0.8	1.8	5.54	4.43	i-	<u></u>			36.30	29
·····	····	253	633.8	634.3	0.5	1.2	1.95	0.98	·			<u>.</u>	16.80	8
<u></u>	⁵	254	634.3	635.2	0.9	2.4	1.63	1.55			18 J	·····	13.30	12
· · · · • • • • •		255	635.2	635.9	0.6	1.6	9.80	4.90		· · · · · · · · · · · · · · · · · · ·	.		55.80	27.
		256	635.9	636.3	0.5	1.3	0.30	0.15					3.20	1.
		120256	636.3	636.9	0.5	-1.1	0.86	0.43					5.40	2.
		120257	636.9	637.3	0.5	1.0	0.04	0.02		1	÷.,		0.00	
		258	637.3	638.4	1.1	2.9	0.35	0.39					3.20	3
	• •	120265	657.9	658.5	0.6	1.4	0.25	0.15					1.10	0.
		119968	489.6	490.1	0.6	1.3	••••••		0.18	0.10	0.29	0.16	5.40	2
••••••		119969	490.1	490.9	0.8	1.8		• • • • • • • • • • • • • •	0.02	0.02	0.13	0.10	0.00	
······		119970	490.9	491.6	0.1	1.3	· • • • • • • • • • •	•••••	0.05	0.04	0.09	0.06	0.00	
¥ :>	· · · · · · · · · · · · · · · · · · ·	971	491.6	492.1	0.6	1.1	•••••••••••••••••••••••••••••••••••••••	·····	0.05	0.03	0.11	0.06	0.00	•••••
	·••••••••	972	492.1	492.7	0.6			•••••	0.25					ļ
225	715	119973	492.7	493.3	0.6	1.3	·····			0.14	0.23	0.13	1.80	1.
231		130152	497.9	493. 3		1.2		0 00	0.10	0.05	0. 23	0.13	1.20	Ó.
491	[9]				0.6	1.1	0.48	0.29	·····	·····	•••••	·····	10.00	6.
		153	498.5	499.6	1.1	2.3	1.21	1.33	····	•••••••••		· · · · · · · · · · · · · · · · · · ·	17.10	18.
		154	499.6	500.0	0.4	0.9	1.12	0.45		· · · · · · · · · · · · · · · · · · ·			16.90	6.
		155	500.0	500.8	0.8	1.8	2.26	1.81			•••••		43.00	34.
		155	500.8	501.7	0.9	1.2	3.45	3.11					48.00	43.
		157	501.7	502.8	0.9	1.2	3.45	3.11					34.00	30.
		158	502.8	503.8	1.1	2.4	1.15	1.21					18.00	18.
		159	503.8	504.5	0.7	1.5	1.09	0.71					16.00	10.
		160	504.5	505.0	0.6	1.3	1.63	0.98					18.40	11.
		161	505.0	506.0	0.9	1.8	0.76	0.72		•••••••			9.30	8.
		162	506.0	507.1	1.1	2.3	1, 17	1.29					16.40	18.
1.		163	507.1	508.1	1.1	2.4	0.65	0.68		••••••	••••••	•••••••	13.80	14.
<u>е</u>		164	508.1	509.0	0.8	2.0	0.43	0.34	••••••••••	••••••	·		7.00	5.
		165	509.0	509.5	0.6	1.3	0.36	0.20			·····	· · · · · · · · · · · · · · · · · · ·	16.90	9.
		166	509.5	510.2	0.8	1.7	0.60	0.45	•••••			• • • • • • • • • • • • •		
		167	510.2	511.3	1.1	2.5	0.23		• • • • • • • • • • • • • • • • • • • •	<i>i</i>		<u>.</u>	12.00	9,
231	751	130168	511.3	511.7	0.5			0.24	·····		····		1.40	1.
211	255	3042	600.6	601.5	0.9		0.44	0.20		•••••			4.50	2.
193							3.16	2.84	·····	· · · · · · · · · · · · · · · · · · ·				
	261	30163	628.8	629.7	0.9		0.00						0.00	
213	298	31186	522.0	522.5	0.5		0.11	0.06					3.30	1.
	· · · · · · · · ·	31203	531.3	531.8	0.5		0.14	0.07		· · · · · · · · · · · · · · · · · · ·	0.18	0.09	9.50	4.
		204	531.8	532.3	0.5	1.1			0.32	0.16	0.34	0.17	2.30	1.
		205	532.3	532.8	0, 5	1.0				:	0.38	0.19	1.70	0.
213	298	31206	532.8	533.3	0.5	1.0	0.23	0.12	ľ				6.60	3.
93	377	17123	596.7	597.5	0.8									
		17119	593.5	594.6	1.1							· · · · · ·	7.40	8.
207	400	18994	628.2	629.3	1.1	3.0	1.61	1.77					53.00	58.
209	415	18895	541.5	542.3	0.8	5.0						· · · · · · ·]	5.40	4.
	415	18920	560.8	561.7	0.9	7.0	·····	·····			••••••	[4.70	4.
213		03659	568.3	569.3	1.0		0.12	0.12	••••••	· · · · · · · · · · ·		•••••		
		03726	597.9	598.4	0.5	1 9	V. 16	v. 16	· • · · · · • • • • • • • • • • • •	•••••	••••••		6.00	6.
· · · · · · · ·	····· ł	727	598.4			1.3	0.00	A AA					4.90	2.
	100			598.9	0.5				0.20	0.10	0.41	0. 21	5.80	2.
13		03728	598.9	599.7	0.8	2.3			0.15	0.12	·		7.10	5.
		07311	580.8	581.4	0.6			0.04					1.60	0. 1
		07904	694.0	694.5	0.5		0.22	0.11				1	0.00	
03	513	13726	\$60.6	561.6	1.0	2.2	Ì	<u> </u>	. I				6.40	6, 4
	 	727	561.6	562.6	1.0	2.2			·····[·				2.80	2.8
03	513 1	13728	562.6	563.2	0.6	1.5				• • • • • • • • • • •		••••	4.40	2. €
			\$74.8	575.3	0.5		0.05	0, 03	0. 58	0.34			0.50	0.2

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	fell-	Spl. 🔄	Spl. In		Spl.	Spl.	Cu 🕅	Cu	Pb X	Pb	Zn 🖇		lg g∕t	Ag
No.	No.	No.	From	То		#eight			grade		grade	m·X	grade	n•g/1
		507	575.3	576.1	0.8	1.8	0.65	0.52	0.11	0.09			1.60	1.28
••••••••••••••••••••••••••••••••••••••		508	576.1	576.7	0.6	1.2	2.89	1.73					12.90	1.14
		509	576.7	577.2	0.5	1.3	1.67	0.84					7.00	3. 50
		510	577.2	578.0	0.8	1.8	0. 21	0.17	••••••		•••••••	· · · · · · · · ·	0.80	0.64
····	uy duyu T									·····		÷,		
		511	578.0	578.7	07	1.6	0.25	0.18	·····		•••••		1.60	1.12
		512	578.7	579.2	0.5	1.1	0.69	0.35					1.60	0.80
<u></u>		513	579.2	580.0	0.8	2.0	0. 73	0.58					1.60	1, 28
		514	580.0	580.6	0.7	1.6	0.24	0.16				1.1	0.50	0. 33
		515	580.6	581.5	0.8	2.0	3.39	2.71					7.20	5.76
205	576	112516	581.5	582.2	0.8	2.0	4.47	3.35					17.00	12.75
201	527	113740	410.5	411.3	0.8	2.0	Ò. 36	0.29			÷ 1,			1
4		110568	553.8	554.3	0.5	5.1.80.						eter e		
201		110570	554.8	555.3	0.5		0	•••••						
219		110738	541.6	542.2	0.6	1.4	0.17	0.09	0.23	0.13			0.80	0.44
010		739	542.2	542.9	0.8	1.9	0.69	0. 52	<u> <u>va</u> 6.9</u>	V. IV		•••••	0.50	0.38
	<u></u>		542.9	543.4	0.5		0. 09		ۇرىيىلىدۇ. م				0.50	
••••••••	····	740				1.1		0.06		0.00				0.25
	a da di	741	543.4	544.0	0.6	1.6	0.40	0.24	0.13	0.08		· · · · · · · · · · · · · · · · · · ·	0.80	0.48
	anti a	742	544.0	544.7	0.7	1.7	0.32	0.22	0.05	0.04			0.80	0.50
	a an Marianta	743	544.7	545.3	0.7	1.5	0.78	0.55				<u> 1</u>	2.60	1. 50
		744	545.3	546.0	0.7	1.5	1.82	1.18	· · · ·	1 - 1 - 1 - 1 			7.40	4.8
		745	\$46.0	546.5	0.5	1.5	2.08	1.25	í				10.40	6.2
	199	746	546.5	547.0	0.5	1.3	1.81	0.91					8.20	4.10
219	\$50	110747	547.0	547.6	0.6	1.3	0.69	0.38				1,5 E	2.70	1.49
209		112093	575.9	576.4	0.5	1.2	0.04	0.02	0.30	0.15			0.50	0.25
		94	576.4	577.0	0.7	1.7	0.09	0.08	0.33	0.23			0.00	
		95	577.0	577.6	0.6	1.5	1.60	0.96	0.10	0.06		••••	3.00	1.80
		96	577.6	578.2	0.6	1.5	1.30	0.78	0.11	0.07		·····	3.00	1.8
			578.2						<u>v. 11</u>	0.01				
		97		578.9	0.7	1.6	2.50	1.63	<u>.</u>	0.00			6.00	3.90
	· · · ·	98	578.9	579.7	0.8	21	1.50	1.28	0.31	0.26	1 1 1 1 1 	·····	2.00	1.7(
	÷	99	579.7	580.7	1.0	2.4	0.17	0.17	·····				0.50	0.50
		100	580.7	581.3	0.5	1.3	1.00	0.50			•••••		1.00	0. 50
		101	581.3	582.0	0.8	2.1	1.45	1.16					1.50	1. 20
		111	582.0	582.7	0.7	1.7	1.60	1.12					1.60	1.12
		102	582.7	583.7	0.9	2.2	2.10	1.89				1	2.10	1.89
		103	583.7	584.2	0.6	1.4	1.70	0.94					2.50	1. 38
209	570	112104	584.2	584.7	0.5	1.2	0.43	0.22				- (:	2.00	1.00
239		111230	465.4	465.9	0.5	1.2			0.05	0.03	0.31	0.16	2.90	1.4
		231	465.9	466.5	0.5	1.3			V. VV	v. vv	0.12	0.07		0.6
	n sin a							•••••			V. 14		1.00	
		232	466.5	467.2	0.6	1.5		<u>.</u>					0.50	0.30
		233	467.2	468.0	0.8	2.4		<u>, 14</u>					1.60	1.30
		234	468.0	469.0	1.0	2.4				100 N = 1 112112		L. L	6.10	6.10
		235	469.0	470.0	1.0	2.5			0.08	0.08	0.24	0.24	6.50	6. 50
		236	470.0	470.8	0.8	2.2			0.31	0.25	0.86	0.69	5.80	4.6
		237	470.8	471.7	0.9	2.2					0.15	0.14	2.10	1.8
		238	471.7	472.5	0.8	1.8					0.18	0.14	1.60	1.28
		239	472.5	473.2	0.7	1.6							1.60	1. 12
		240	473.2	474.2	1.0	2.9	•••••••			 *			1.10	1.1(
		241	474.2	474.7	0.5	1.2	· · • • • • • • • • • • • •				•••••		1.30	0.6
···•						1.6	· · • • • • • • • • • •	· · · · · · · · · · · · · · · · · · ·	0.00	0 05	A 19	0 02		
	ļ	242	474.7	475.2	0.5	1.2	·····	h.`	0.09	0.05	0.13	0.07	1.60	0.80
		243	475.2	475.8	0.6	1.4	·····		0.09	0.05	0.21	0.12	3.00	1.6
		244	475.8	476.3	0.5	1.2							1.90	0.9
	<u> </u>	245	476.3	476.8	0.5	1.2			 		0.20	0.10	1.30	0.6
		246	476.8	477.3	0.5	1.2					0.29	0.15	1.90	0.9
		247	477.3	478.0	08	1.8			0.13	0.10	0.28	0.21	3.00	2. 2
239	571	112248	478.0	478.7	0.7	1.2	··· <i>·</i> ····		0.05	0.04	0.24	0.17	2.60	1.82
							·!····							
				hi					· · · · · · · · · · · · · · · · · · ·		••••			· · · · · · · · · · · ·
	I	.	E					L					F	

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-	line	Well	Spl.	Sp1. In	térval	Spl.	Spl.	Cu X	Cu	Pb X	Pb ::	Zn X	Zn	Ag g/1	Ag
	No.	No.	No.	From	To	. <u>eng.</u>	Weight	grade	n•%	grad		grade		grade	n·g/t
	213	670	118468 469	557.9 558.4	558.4 559.2	0.5	11	0.37	0.19				¹	1 66	0.00
1			470	559.2	559.7	0.5	2.0 1.2	0.56	0.02	0.11	0.06	0.40	0.20	1.00 6.30	0.80 3.15
2			471	559.7	560.7	1.0	2.6	0.08	0.08					3.10	3.10
		· · · · · · · · · · · ·	473	561.7 562.7	562.7	1.0	2.3	0.22	0.22	t <u>.</u>		0.06	0.05	3.50	3.50
			474	563.5	563.5 564.5	0.8 1.0	1.5 2.3	0.31 0.39	0.25			0.18	0.14	3.90 4.30	3.12 4.30
			476	564.5	565.0	0.5	1.0	0.94	0.47	- 		······	· · · · · · · · · · · · · · · · · · ·	8.80	4.40
Ż	233		116705	470.5	471.5	1.0	1.9			0.30	0.24	0.32	0.26	2.80	2.24
21 M 1	231		117718 112507	608.6 575.3	609.1 576.1	0.5 0.8	1.2	0.65	Λς	0.05	0.03	0.18	0.09	0.00	1:00
		<u>Y IY</u>	508	576.1	576.7	0.6	2.9	0.03	0.52	0.11	0.09	•••••	·····	1.60 12.90	1.28 7.74
			509	576.7	\$77.2	0.5	1.3	1.67	0.84					7.00	3.50
	239	440	118259 260	501.4 502.0	502.0	0.6	1.4	0.45	0.25				· · · · · · · · · · · · · · · · · · ·	8.00	4.40
			261	502.6	502.6 503.3	0. 1 0. 1	1.6	1.02 0.18	0.66 0.13			· · · · · · · · · · · · · · · · · · ·		13.20 3.10	8.58 2.17
			262	503.3	504.0	0.7	1.6	0.05	0.03		·····	••••••		1.00	0.65
			263	504.0	504.8	0.8	2.1	0.07	0.06	0.44	0.37	0.15	0.13	4.60	3. 91
-	• • • • • • • • • • • • • • • • • • • •		264 265	504.8 505.4	505.4 505.9	0.6 0.5	1.1 1.0	0.07	0.04	0.57	0.34	0.35	0. 21	4.70	2.82
· .	233	638	116700	467.3	467.7	0.5	1.0	V. UV	0.03	0.22	0.02 0.10	0.18	0.08	0.50 2.10	0.23 0.95
			701	467.7	468.6	0.8	2.0			0.10	0.09			1.30	1.11
	· · · · · ·	·····	702 703	468.6	469.1	0.5	1.4	· · · · · · · · ·		0.23	0.12	0.14	0.07	2.10	1.05
			704	409.1	470.1	1.0 0.6	2.2 1.5	• • • • • • • • • • • • • • • • • • • •	·····	0.11	0.11	· · · · · · · · · · · · · · · · · · ·	·····	1.70 1.00	1.70 0.60
÷		· · · · · · · · · · · · · · · · · · ·	705	470.7	471.5	0.8	1.9	••••••••	::	0.30	0.24	0.32	0.26	2.80	2.24
	· ·····		705	471.5	472.4	0.9	2.2	·····		0.06	0.05			1.50	1.35
	·····		707 708	472.4 473.1	473.1 474.1	0.7	1.8 2.6	ini di secondo di	••••••	0.12 0.29	0.08	0.15 0.47	0.11 0.47	2.70 7.40	1.89
-:			116728	487.2	487.7	0.5	1.3	0. 52	0.26	V. 27	V. 63	V. 41	V. 41	6.85	7.40 3.43
•	······	· · · · · · · · · · · · · · · · · · ·	729	487.7	488.2	0.6	1.3	0.05	0.03	0.58	0.32	0.86	0.47	3.70	2.04
		·····	730 731	488. 2 488. 9	488. 9 489. 9	0.7 1.0	1.7 2.5	0.04	0.03	0.09	0.06	0, 48	0.34	1.70	1.19
			732	489.9	490.5	0.7	1.6	2.01	0.08	·	·····	<u>.</u>	··· ·· ·······························	1.25 70.30	1.25 45.70
. 1	233		116733	490.5	491.2	0.5	1.5	0.79	0.47					18.40	11.04
	231		116792	483. 2 543. 3	483.8 544.1	0.6 0.8	1.5	0.15	0.09		 	· · · · · · · · · · · · · · · · · · ·	·····	8.20	4.92
	239		16829	486.6	487.4	0.8	1.3 1.5	0. 41 0. 25	0.33			· • · · · · · · · · · · · · · · · · · ·		13.80 1.60	11.04 1.28
			830	487.4	487.9	0.5	1.2	0.71	0.32	••••••			•••••••	4.00	1.80
	237	641	117018 19	479.9 480.7	480.7	0.8	1.9	0.72	0.58		4			6.40	5.12
	· · · ·		20	400.1	481.4 481.9	0.7 0.5	1.7 1.2	2.99 1.94	2.09 0.97		· · · · ·	4 · ·		24.40 39.60	17.08 19.80
		·i	21	481.9	482.9	1.0	2.3	0.57	0.57	·····	••••••			5. 50	5.50
1			22	482.9	483, 9	1.0	2.3	0.35	0.35	•••••				2.70	2.70
			23 24	483.9 484.9	484.9 485.9	1.0 1.0	2.4 2.3	0. 20 0. 27	0.20 0.27	· · · · · · · · ·				1.40	1.40
į		·····	25	485.9	486.9	1.0	2.3	0.37	0.37	· · · · · · · · · · · · · · · · · · ·		· · · · · · · · ·	· · · · · · · · · ·	2.00 4.40	2.00
ļ			26	486.9	487.9	1.0	2.4	0.31	0.31					2.50	2.50
	233	642	17072 73	489.2 489.9	489. 9	0.8	1.9	0.21	0.16	0.26	0.20	0.56	0.42	4.60	3. 45
			13 74		490.6 491.0	0.7	1.7 1.0	0.16 2.14	0.11 0.85	••••••	• • • • • • • • • • • • • • • • • • • •		,	2.50 15.60	1.75 6.24
			75	491.0	491.8	0.8	2.0	0.17	0.13					0.00	v. 24
			76	491.8	492.4	0.6	1.4	0.08	0.05					0.60	0.36
			17 78		493.0 493.6	0.6		0.40	0.24	0.66	0.40	····;•-••	· · · · · · · · · · · · · · · · · · ·	0.80	0.48
			79	493.6	493.0	0.6		0.74	0.30	·····	••••••	·····		1.05	0.68
	•••••••		80	494.2	494.7	0.5	1.3	2.01	1.01					11.90	5.75
			81	494.7	495.3	0.6	1.4	1.87	1.12					15.90	9.54

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No. No. From To engr. foight grade ar.36 ar.adg m.3 ar.adg	•		4.13	(Ca)	<u>e-1 7-</u>		5-1	Spl.	Cu X	Cu	Pb %	Pb	Zn 🕺	Zn	ha a/1	Ag
223 642 11783 495.5 0.6 1.5 2.25 1.1 0.78 0.35 1.7 1.7 1.7 10 7.70 229 644 117213 481.2 481.7 0.5 1.2 3.15 1.86 0.04 0.02 0.20 0.16 0.80 0.40 229 644 117213 481.2 481.7 0.9 2.4 0.04 0.02 0.20 0.08 0.80 0.00 299 698.8 495.7 0.9 2.4 0.07 0.9 0.08 0.05 0.08 0.09 0.05 0.03 0.6 0.05 0.03 0.05 0.03 0.05 0.03 0.05 0.03 0.05 0.03 0.05 0.03 0.05 0.03 0.05 0.03 0.05 0.03 0.05 0.03 0.05 0.03 0.05 0.03 0.05 0.03 0.05 0.03 0.05 0.03 0.05 0.03 0.05 <	i.															
233 642 11133 195. 9 495. 3 0.5 1.1 0.76 0.85	2	<u> aq</u>	<u>no.</u>				the second second	and the second second	the second second		61 040	N 74	Brado	<u> </u>		the second s
229 644 117273 481. 2 65 1.2 5. 15 1.58 94. 00 17. 00 299 (48. 8 493. 7 0. 3 2.4 0. 09 0.08 0.02 0.01 0.60 0.05 0.03 1.00 0.05 0.03 1.00 0.05 0.03 1.00 0.05 0.03 1.00 0.05 0.03 1.00 0.05 0.03 1.00 0.05 0.03 1.00 0.05 0.03 1.00 0.05 0.03 1.00 0.05 0.03 1.00 0.05 1.11 0.30 0.5 1.11 0.17 0.03 0.05 1.33 0.5 5.99 0.40 0.18 0.24 0.11 1.3.99 1.5 4.5 0.40 0.40 0.18 0.42 0.11 1.27 1.27 1.27 1.27 1.27 1.22 1.28 1.16 0.17 1.12 1.12 1.20 1.00 1.00 1.00 1.00 1.14 <t< td=""><td></td><td>233</td><td>642</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>· · · · ·</td><td></td><td>····.</td><td></td><td></td><td></td></t<>		233	642								· · · · ·		····.			
117298 468.3 468.4 9.5 1.2 0.44 0.02 0.20 0.10 0.60 0.00 2394 495.8 493.7 0.9 2.4 0.99 0.08 0.03 0.04 0.04 0.04 0.04 0.04 0.04 0.04 0.04 0.04 0.04 0.04 0.04 0.03 0.04 0.04	1				144.4									· · · · · · · · · · · · · · · · · · ·		
117298 468.3 468.4 9.5 1.2 0.44 0.02 0.20 0.10 0.60 0.00 2394 495.8 493.7 0.9 2.4 0.99 0.08 0.03 0.04 0.04 0.04 0.04 0.04 0.04 0.04 0.04 0.04 0.04 0.04 0.04 0.03 0.04 0.04	÷	229	644	117273	481.2	481.7	0.5	1.2	3.15	1.58					34.00	17.00
299 198. 8 499. 7 0.9 2.4 0.9 0.03 0.03 0.03 1.00 9.00 300 499. 7 500. 3 0.6 1.4 2.42 1.09 0.40 0.15 0.23 0.03 13.30 5.93 302 500.6 501.6 0.8 2.20 9.76 0.18 0.24 0.11 3.30 15.4 237 645 117169 495.9 476.6 0.7 1.5 0.20 0.13	-										0.04	0.02	0.20	0.10		
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		Line No. 233 197 197 197	Well No. 652 706 706 709	Sp1. No. 827 119526 527 528 529 530 531 532 533 534 535 536 119682 683 684 685	Sp1. 1r From 511. 7 589. 8 590. 7 591. 5 591. 9 592. 7 593. 3 594. 0 594. 6 595. 1 595. 9 595. 9 596. 4 596. 1 596. 6 597. 1	terval To 512.2 590.7 591.5 591.9 592.7 593.3 594.0 594.6 595.1 595.9 596.4 597.3 596.6	Sp1, eng. 0, 5 0, 8 0, 8 0, 8 0, 8 0, 8 0, 6 0, 7 0, 7 0, 6 0, 8 0, 5 0, 8	Spl. feight 1.2 2.1 2.0 1.0 2.3 1.4 1.4 1.4 1.4 1.7 1.4	Cu X grade 2.70 0.42 1.17 0.95 4.12 0.03 0.09 0.15 4.32 0.73 0.05	Cu m·% 1.35 0.36 0.88 0.43 3.30 0.02 0.06 0.10 2.38 0.55	Pb % grade 0, 09 0, 17 0, 88 0, 08	Pb m·% 0.08 0.13 0.40 0.06	Zn X grade 0. 27	Ó. 23	Ag g/t grade 72.50 2.70 3.00 3.00 16.70 0.50 0.50 0.50 6.00 13.80	36. 2. 1. 13. 0. 0. 3.
		233 197	652 706	No. 827 119526 527 528 529 530 531 532 533 534 535 535 536 119682 683 684 685	From 511.7 589.8 590.7 591.5 591.9 592.7 593.3 594.0 594.6 595.1 595.9 595.4 596.4 596.6	To 512.2 590.7 591.5 591.9 592.7 593.3 594.0 594.6 595.1 595.9 595.4 597.3 596.6	Leng. 0.5 0.8 0.8 0.5 0.8 0.5 0.8 0.7 0.7 0.7 0.6 0.8 0.5	Veight 1.2 2.1 2.0 1.0 2.3 1.4 1.4 1.4 1.7	grade 2.70 0.42 1.17 0.95 4.12 0.03 0.09 0.15 4.32 0.73	m·X 1. 35 0. 36 0. 43 3. 30 0. 02 0. 06 0. 10 2. 38	grade 0. 09 0. 17 0. 88	m·X 0.08 0.13 0.40	8rade 0. 27	0.23	grade 72, 50 2, 70 3, 00 16, 70 0, 50 0, 50 0, 50 6, 00 13, 80	m•g 36. 2. 1. 13. 0. 0. 3.
		197	706	119526 527 528 529 530 531 532 533 534 535 534 535 536 119682 683 684 685	589.8 590.7 591.5 591.9 592.7 593.3 594.0 594.6 595.1 595.9 596.4 596.1 596.6	590. 7 591. 5 591. 9 592. 7 593. 3 594. 0 594. 6 595. 1 595. 9 595. 4 597. 3 596. 6	0.8 0.8 0.5 0.8 0.6 0.7 0.7 0.6 0.8 0.8 0.5	2.1 2.0 1.0 2.3 1.4 1.4 1.4 1.4 1.4	0.42 1.17 0.95 4.12 0.03 0.09 0.15 4.32 0.73	0.36 0.88 0.43 3.30 0.02 0.06 0.10 2.38	0.17 0.88	0.13 0.40			2.70 3.00 3.00 16.70 0.50 0.50 0.50 6.00 13.80	36. 2. 1. 13. 0. 0. 3. 10.
		197	706	527 528 529 530 531 532 533 534 535 536 119682 683 684 685	\$90. 7 \$91. 5 \$91. 9 \$92. 7 \$93. 3 \$94. 0 \$94. 6 \$95. 1 \$95. 9 \$96. 4 \$96. 1 \$96. 6	591.5 591.9 592.7 593.3 594.0 594.6 595.1 595.9 596.4 597.3 596.6	0.8 0.5 0.8 0.6 0.7 0.7 0.6 0.8 0.5	1.0 2.3 1.4 1.4 1.4 1.4 1.4	1.17 0.95 4.12 0.03 0.09 0.15 4.32 0.73	0.88 0.43 3.30 0.02 0.06 0.10 2.38	0.17 0.88	0.13 0.40			3.00 3.00 16.70 0.50 0.50 0.50 6.00 13.80	2. 1. 13. 0. 0. 3.
			706	528 529 530 531 532 533 534 535 536 119682 683 683 684 685	591.5 591.9 592.7 593.3 594.0 594.6 595.1 595.9 595.9 595.4 595.4 596.4 596.1	591.9 592.7 593.3 594.0 594.6 595.1 595.9 595.4 595.4 597.3 596.6	0.6 0.7 0.7 0.6 0.8 0.5	1.0 2.3 1.4 1.4 1.4 1.4 1.4	0.95 4.12 0.03 0.09 0.15 4.32 0.73	0.43 3.30 0.02 0.06 0.10 2.38	0.88	0.40			3.00 16.70 0.50 0.50 0.50 6.00 13.80	1. 13. 0. 0. 3.
			706 709	529 530 531 532 533 534 535 536 119682 683 684 685	591. 9 592. 7 593. 3 594. 0 594. 6 595. 1 595. 9 596. 4 596. 1 596. 6	592.7 593.3 594.0 594.6 595.1 595.9 596.4 597.3 596.6	0.6 0.7 0.7 0.6 0.8 0.5	2.3 1.4 1.4 1.4 1.4 1.4 1.7	4.12 0.03 0.09 0.15 4.32 0.73	3.30 0.02 0.06 0.10 2.38					16.70 0.50 0.50 0.50 6.00 13.80	13. 0. 0. 3.
			706 709	531 532 533 534 535 536 119682 683 683 684 685	593.3 594.0 594.6 595.1 595.9 596.4 596.1 596.6	594.0 594.6 595.1 595.9 596.4 597.3 596.6	0.6 0.7 0.7 0.6 0.8 0.5	1.4 1.4 1.4 1.7	0.09 0.15 4.32 0.73	0.06 0.10 2.38					0.50 0.50 6.00 13.80	0. 0. 0. 3.
			706 709	532 533 534 535 536 119682 683 684 685	594.0 594.6 595.1 595.9 596.4 596.1 596.6	594.6 595.1 595.9 596.4 597.3 596.6	0.7 0.6 0.8 0.5	1.4 1.4 1.7	0.15 4.32 0.73	0.10 2.38	••	· · · · · · · · · · · · · · · · · · ·		······	0.50 6.00 13.80	0. 3
			706 709	533 534 535 536 119682 683 684 685	594.6 595.1 595.9 596.4 596.1 596.6	595.1 595.9 596.4 597.3 598.6	0.6 0.8 0.5	1.4 1.7	4.32 0.73	2.38	i 		· · · · · · · · · · · · · · · · · · ·	······································	6.00 13.80	3
			706 709	534 535 536 119682 683 684 685	595.1 595.9 596.4 596.1 596.6	595.9 596.4 597.3 595.6	0.8	1.7	0.73	0.55	••••••		•••••		13.80	
			706 709	536 119682 683 684 685	596.4 596.1 596.6	597.3 595.6	0.5							the second s		
			706 709	119682 683 684 685	596.1 596.6	595.6	0.8			0.03	0.06	0.03	0.34	0.17	1.50	0.
			103	683 684 685	596.6			2.1	0.86	0.73					9.00	7.
				684 685		1 1 1 1	0.5	1.3	0.28 0.03	0.14 0.02	·		0.11	0.06	1.40	0.
				685		597.1 597.7	0.5	1.4	0.08	0.04	0.10	0.06	0.91	0.50	0.50	0. 0.
					597.7	598.2	0.6	1.4	0.10	0.05	0.03	0.02	0.11	0.06	0.70	0.
				686	598.2	598.8	0.6	1.6	0.03	0.02	0, 13	0.08	0.36	0.22	0.60	0.
				687	598.8	599.2	0.5	1.3	1.26	0. 57	0.08	0.04	0.17	0.08	3.90	1.
				688 689	599, 2 599, 9	599.9 600.9	0.7 0.9	1. 8 2. 5	0. 13 0. 16	0.09 0.15	0.05 0.16	0.04	0.23 0.46	0.16	1.90	1.
			l :	690	600.9	602.0	1.1	2.6	1.16	1. 22	0.10	0.15	U. 40	0.44	1.10 1.70	1. 1.
				691	602.0	602.7	0.8	1.8	3.11	2.33	0.03	0.02		······································	12.70	9.
				692	602.7	603.2	0.5	1.2	0. 73	0.37					3.60	1.
	$(1,1,2,\dots,2^{n-1})$			119714	620.5	621.1	0.6	1.5 1.8	2.08	1.25					61.50	36.
		· • · • • • • •	·····	715 716	621.1 621.9	621.9 622.4	0.8 0.5	1.0	0.01 0.01	0.01 0.01			•••••	••••	0.50 0.00	0.
	:	· · · · · · · · · · · · · · · · · · ·		717	622.4	622.9	0.5	1.2	0.01	0.01	• • • • • • • • • • • • •	·····i			0.00	
1				718	622. 9	623.5	0.7	1.7	0.84	0.59					2.30	1.
J				719	623.5	624.2	0.7	1.7	0.02	0.01	·				0.00	
				720 721	624.2 625.0	625.0 626.1	0.8	-2.0 2.6	1.36	1.09 1.48					0.00	
		199	709	119723	626.1	626. 6	0.5	1.2	0.01	0.01					24.50 32.20	25. 16.
	1	199	494	107308	579.0	579.8	0.8	1.5	0.08	0.06		· • • • • • • • • • • • • • • • • • • •			1.60	1.
				107311	580.8	581.4	0.6	1.2	0.07	0.04					1.60	0.
		203	513	113726	560.6	561.6	1.0	2.2			•••••••••••••••••••••••••••••••••••••••		.	,	6.40	6.
				727 728	561.6 562.6	562.6 563.2	1.0 0.6	2.2 1.5	·····		· · · · · · · · · · · · · · · · · · ·		•••••		2.00	2.
		205	576	112504	573.6	574.3	0.7	1.4	0.10	0.07	0.46	0.32	•••••	·····	4.00	2. 0.
				505	574.3	574.8	0.5	1.1	0.03			0.18		•••••	0.50	0.
	ł.	. <u>.</u>		506	574.8	575.3	0.5					0.34			0.50	0.
	·	· · · · · · ·	· · · · ·	507 508	575.3 576.1	576.1 576.7	0.8	1.8	0.65	0. 52	<u>0. 11</u>	0.09			1.60	1.
				509	576.7	577.2	0.5	1.2 1.3	2.89 1.67	1.73	·····				12.90 7.00	7. 3.
				510	577.2	578.0	0.8	1.8	0.21	0.17	· - · · · · · · · · · · · · ·		· · · · · · · · ·		0.80	0.
				511	578.0	578.7	0.7	1.6	0.25	0.18					1.60	1.
•				512	578.7	579.2	0.5	1.1	0.69	0.35			· · · · · · · · · · · ·	······	1.60	0.
)				513 514	579.2 580.0	580.0 580.6	0.8	2.0 1.6	0.73 0.24	0.58		·····			1.60	1.
·				515	580.6	581.5	0.8	2.0	3. 39	2. 71					0.50 7.20	0. 3 5. 1
•				516	581.5	582.2	0.6	1.5	4. 47	2.68					17.00	12.7
				112509	576.7	577.2	0.5	1.3	1.67	0.84					7.00	3. 5
		205	576	112515	580.6	581.5	0.8	2.0	3.39	2.71					7.20	5. 7
		205		112516 116015	581.5 484.9	582.2 495.8	0.6	1.5 2.1	4.47	2.68 0.14	0.30	0. 26	0 12		17.00	10.2
				16016	495.8	496.5	0.7	1.8	8.85	0. 20	V. 90	v. 20	0.12	0.10	3.00 28.60	2. 5
•	;		1	16017	495.5	497.1	0.6	1.4	1.48		0.07	0.04			12.00	7.2
		231		15788 789	505.8 506.4	506.4 506.9	0.6 0.5		0.44			0.08			4.50	2.7

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1 		Vel 1	Spl.	Spl. In		Spl.	Spl.	Cu X	Cu	Pb X	Pb	Zn X		lg g/t	Ag
	<u>No.</u>	No.	No.	From	To		Weight			grade	л Х	grade	<u>n•%</u>	grade	m·g/t
1			790	506.9	507.4	0.5	1.2	0.24	0.12					1.50	0.75
			791	507.4	508.3	0.9	2.2	0, 31	0.28				· · · ·	1.00	0.90
:	· · ·		792	508.3	509.3	1.0	2.7	0.16	0.16	0.14	0.14			1.00	1.00
			793	509.3	510.3	1.0	2.5	0.07	0.07		· · · · · · · · · · · · · · · · · · ·			0.00	
2		<u>.</u>	794	510.3	511.3	1.0	2.5	0.63						2.20	2.20
1	231		115795	511.3	512.3	1.0	2.3	0.32	0.32				2	3.20	3.20
<	237		116350	448.1	448.9	0.8	1.7	1.05	0.85					15.40	12. 32
1	· ·		116357	454.1	455.0	0.9	1.7			0.22	0.20	0.23	0.21	1.60	1.44
2	219	550	110738	541.6	542.2	0.6	1.4	0.17	0.09	0.23	0.13			0.80	0.44
			739	542.2	542.9	0.8	1.9	0.69	0.52					0.50	0.38
9 2			740	542.9	543.4	0.5	1.1	0.12	Ö. Ö6				1.25	0.00	
•			741	543.4	544.0	0.6	1.5	0.40	0.24	0.13	0.08			0.80	0.48
	Ţ.	10	742	544.0	544.7	0.7	1.7	0.32	0.22	0.05	0.04		1	0.80	0.56
	i.		743	544.7	545.3	0.6	1.5	0.78	0.47		~			2.60	1.55
-			744	\$45.3	546.0	0.7	1.5	1.82	1.18					7.40	4.81
÷.			745	546.0	546.5	0.6	1.5	2.08	1.25					10.40	6.24
	2		746	\$46.5	547.0	0.5	1.3	1.81	0.91					8.20	4.10
	219	550	110747	547.0	547.5	0.6	1.3	0.69	0.38					2.70	1.49
5 1	209	\$70	112093	\$75.9	576.4	0.5	1.2	0.04	0.02	0.30	0.15			0.50	0.50
			94	576.4	577.0	0.7	1.7	0.09	0.06	0.38	0.27			0.00	
÷			112095	\$77.0	577.6	0.6	1.5	1.60	0.96	0.10	0.05			3.00	1.80
			96	\$77.6	578.2	0.6	1.5	1.30	0.78	0.11	0.07			3.00	1.80
-			97	578.2	578.9	0.7	1.6	2.50	1.63					6.00	3.90
			98	578.9	579.7	0.8	2.1	1.50	1.28	0.31	0.26			2.00	1.70
			99	579.7	580.7	1.0	2.4	0.17	0.17					0.50	0.50
			100	580.7	581.3	0.5	1.3	1.00	0.50					1.00	0.50
1			101	581.3	582.0	0.8	2.1	1.45	1.16		N			1.50	1.20
			111	582.0	582.7	0.7	1.7	1.60	1.12					1.60	1.12
			102	582.7	583.7	0.9	2.2	2.10	1.89					2.10	1.89
			103	583.7	584.2	0.6	1.4	1.70	0.94	1.1	н ¹ н			2.50	1.38
1	209		112104	584.2	584.7	0.5	1.2	0.43	0.22					2.00	1.00
	239	571	112230	465.4	465.9	0.5	1.2			0.06	0.03	0.31	0.16	2.90	1.45
			112231	465.9	466.5	0.6	1.3					0.05	0.03	1.00	0.60
•			232	466.5	467.2	0.6	1.5					0.12	0.07	0.50	0.30
			233	467.2	468.0	0.8	2.4							1.60	0.85
4 1			234	468.0	469.0	1.0	2.4		:					6.10	6.10
			235	469.0	470.0	1.0	2.5			Ô. Ô8	0.08	0.24	0.24	6.50	6.50
			236	470.0	470.8	0.8	2.2			0.31	0.25	0.86	0.69	5.80	4.64
			-237	470.8	471.7	0.9	2.2					0.15	0.14	2.10	1.89
			238	471.7	472.5	0.8	1.8					0.18	0.14	1.60	1.28
1		1. 1. 1	239	472.5	413.2	0.7	1.6							1.60	1.12
			240	473.2	474.2	1.0	2.9							1.10	1.10
			241	474.2	414.7	0.5	1.2							1.30	0.65
ł		10 A.S.	242	474.7	475.2	0.5	1.2	1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.		0.09	0.05	0.13	0.07	1.60	0.80
1			243	475.2	475.8	0.6	1.4			0.09	0.05	0.21	0.12	3.00	1.65
			244	475.8	476.3	0.5	1.1					1 × 1		1.90	0.95
ł			245	476.3	476.8	0.5	1.2					0.20	0.10	1.30	0.65
1	239		112246	476.8	417.3	0.5	1. 2					0.29	0.15	1.90	0.95
	199		107904	694.0	694.5	0.5	Ô. 8	0.22	0.11					0.00	
	1.11		107308	579.0	579.8	0.8	1.5	0.08	0.06					1.60	1.28
2.1	199		107314	580.8	581.4	0.5	1.2	0.07	0.04					1.60	0.80
1.11	237		116358	455.0	455.9	Ŏ. 9	1.7			0.05	0.05	0.06	0.05	0.50	0.45
1			116359	455.9	458.4	0.5	1.0			0.15	0.08	0.30	0.15	2.20	1.10
			116360	456.4	457.2	0.8	2.0			0.12	0.10	0.34	0.27	1.70	1.36
			116379	473.4	474.3	0.9	2.2	0.11	0.10	,				1.60	1.44
			380	474.3	475.1	0.8	2.0	0.11	Ó. 09	0.10	0.08	0.48	0.38	2.40	1.92
			381	475.1	475.6	0.5	1.2	0.12	0.06	0.19	0.10	0.30	0.15	10.30	5.15
		I	382	475.6	476.6	1.0	2.7	0.05	0.05	0.25	0.25	0.20	0.20	8.40	8.40
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	fell	Spl.	Spl. Ir	iterval	Šp1.	Spl.	Cu %	Cu	РБ Х	Pb ::	Zn X	Zn	Ag g/t	Ag
No.	No.	No.	From	То	leng.	Weight	grad		grad		grad		grade	n.8/
	1.18 	383	476.6	477.6	1.0	2.7	0.03	0.03	0.11		0.11	0.11	2.00	2.0
		384	477.6	478.5	0.9	2.2	0.02	0.02	0.19	••] ••••••••			1.40	1.2
		385 386	478.5 479.2	479.2 479.8	0.7	1.7	0.73	0.51	0.09	0.06			5.00	4.2
	· · · · · ·	387	479.8	419.0	0.6	1.5	2.31	1.39	· · · · · · · · ·				24.00	14.4
		388	480.4	480.9	0.6	1.6	3.89	0.18					3.00	1.6
		116584	520.3	520.9	0.6	1.5	0.28	0.17	• • • • • • • • •	· · [· , · · · · · · ·			34.00	20.4
		116590	525.5	526.0	0.5	1.2	2.72	1.36					5.10	2.5
		591	526.0	526.8	0.8	2.1	0.73	0.58					2.10	1.6
	مدينية	592	526.8	527.4	0.6	1.5	0.01	0.01					0.00	
237		116593	527.4	527.9	0.5	1.3 1.2	0.38	0.19	1				15.10	· · · · · · ·
229	625	116562	514.9	515.4	0.5	1.2	0.26	0.13					2.10	1.0
		563	515.4	515.9	0.5	1.2	0.02	0.01					0.00	
· · · · · · · · ·		564	515.9 516.5	516.5	0.6	1.6	1.36	0.82		. <u></u>	:[4.30	2.5
· • • • • • • • • • • • • • • • • • • •		565 566	510.5	517.0 517.4	0.5	1.2	2.54	1.27					3.00	1. \$
· • • • • • • • • • • • • • • • • • • •	·····	567	\$17.4	517.9	0.5	1.1	1.03 0.23	0.40				••••••	1.40	0.6
********		568	517.9	518.4	0.5	1.1	0.06	0.03	······		·	•••••	0.50	0.2
······		569	518.4	518.9	0.5	1.3	0.09	0.05		•			0.00	·• ·· ·
		570	518.9	519.3	0.5	1.1	1.62	0.73					3.10	5.9
		571	519.3	519.8	0.5	1.2	0.28	0.13				· - <i>•</i> • • • • • • • • •	0.80	0.7
- <u></u>		572	519.8	520.3	0.5	1.2	0.48	0.24			.		2.10	1.0
229		116573	520. 3	520.8	0.5	1.2	0.22	0.11					1.70	0.8
235	629	16287	509.8	510.2	0.6	1.1	0.36	0.20					3.00	1. 3
233	141	288 16487	510.2 499.6	510.7	0.5	1.2	0.66	0.33	·····.	· · · ·			8.50	4.2
200	0.91	488	499. 0 500. 2	500.2 500.8	0.6 0.6	1.5	0.20	0.12	·····		·	· · · · · · · · · · · · · · · · · · ·	1.60	0.90
aline i		489	500.8	501.3	0.5	1.1	0.10	0.05 0.76			·····	· • · · · · · • • • • • •	0.50	0.30
		490	501.3	502.3	1.0	2.4	0.17	0.17	E			•••••	13.40 0.50	6.7(0.5(
		491	502.3	502.8	0.5	1.0	0.77	0.39			·····		5.00	2. 50
		492	502.8	503.3	0.5	1.0	1.38	0.69	·····		1	·······	16.00	8.00
		493	503.3	503.9	0.6	1.8	1.43	0.86					19.20	11. 52
		494	503.9	504.4	0.5	1.3	1.31	0.66					17.20	8.60
		495	504.4	504.9	0.5	1.3	0.88	0.44			<u></u>	· · · · ·	13.80	9.10
		496 497	504.9 505.6	505.6	0.7	1.7	0.98	0.69	· • • • • • • • • • • • • • • • • • • •	i		• · ·	13.00	9.10
	••••••	498	506.6	506.6 507.6	1.0	2.4 2.1	0.48	0.48			•••••	: 	6.80	3.00
233	631 1	16500	508.2	508.9	0.7	<i>t</i> . 1 1. 7	0.01	0.58			•		3.00	3.00
		16517	523.2	523.7	0.5	1.3	0.21	0.11	· · · · · · · · · · · · · · · · · · ·		·····		12.00 0.70	8.40 0.35
	1	16516	522.6	523.2	0.6	1.5	0.42	2.52	 		·,		3.00	1.80
		16705	470.7	471.5	0.8	1.9			0.30	0.24	0.32	0.26	2.80	2. 24
239	440 1	18259	501.4	502.0	0.6	1.4	0.45	0.25					8.00	4.40
	·····	260	502.0	502.6	0.7	1.4 1.6 1.7	1.02	0.66					13.20	8.58
·····	·····		502.6	503.3	0.7	1.1	0.18	0.13		:	· · ·		3.10	2.17
•••••	••••••		503.3	504.0 504.8	0.7	1.6 2.1	0.05	0.03					1.00	0.65
			504.0	505.4	0.8	2. 1 1. 1	0.07	0.06	0.44	0.37	0.15	0.13	4.60	3.91
	·····		505.4	505.8	0.5		0.06	0.04	0.57	0.34 0.02	0.35	0. 21	4.70	2.82
233	638 1		467.3	467.7	0.5	1.1		0.00	0. 22	0.02	0.18	0.08	0.50 2.10	0.23
		701	467.7	468.6	0.8	0.2		••••••••••••••••••••••••••••••••••••••	0.10	0.09	.X	0.00	1. 30	1.11
		702	468.6	469.1	0.5	1.4			0.23	0.12	0.14	0.07	2.10	1.05
				470.1	1.0	2.2			0.11	0.11		-	1.70	1.70
				470.7	0.6	1.5			0.10	0.05		× • • • • •	1.00	0.60
				471.5	0.8	1.9			0.30	0.24	0.32	0.26	2.80	2. 24
	·····			472.4	0.9	2.2			0.06	0.05			1.50	1.35
				473.1 474.1	0.7	1.8 2.6			0.12	0.08		0.11	2.70	1.89
					1 0 1	7 6 1	1		1 20 1	0.29	0.47	0.47	7.40	7.40

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	fell	Spl.	Spl.In		Spl.	Spl.	Cu X	Cu	Pb %	Pb	Zn X		Ag g/1	Ag
<u>\o.</u>	No.	<u>No.</u> 723	From	To		Weight			grade	<u>m·X</u>	grade	m·X	grade	m·g/
		724	484, 1 484, 6	484.6 485.2	0.5	1.3	2.55	1.28	·····		·		50.20 11.35	25.1 6.8
3	.1:	725	485.2	485.6	0.5	1.0	1.27	0.57	·····	·	·····		26.30	11.8
		726	485.6	486.2	0.6	1.6	2.06	1.24			an", ••••••		35.80	21.4
999	629	727 116728	486.2	487.2	0.9	2.2	2.26 0.52	2.03	·	4 2.1 		·····	45.80	41.2
233 231		117718	401.2	487.7 609.1	0.5	13	V. 96	0.25	Ó. 05	0.03	0.18	0.09	3.70 0.00	2.0
		719	609.1	609.6	0.5	1.3			0.05	0.03	0. 23	0.12	0.00	
97	706	118526	589.8	590.7	0.8	2.1	0.42	0.36	0.09	0.08	0. 27	0. 23	2.70	2.3
		527 528	<u>590.7</u> 591.5	591.5 591.9	0.8	2.0	1.17 0.95	0.88	0.17 0.88	0.13			3.00 3.00	2.2
·····		529	591.9	592.7	0.8	2.3	4.12	3.30	0.08	0.08			16.70	13.3
		530	592.7	593.3	0.6	-1.4	0.03	0.02	· · · · · · · · · · · · · · · · · · ·			1997 - 1997 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 -	0.50	0.3
		531	593.3	594.0	0.7	14	0.09	0.06	·····				0.50	0.3
÷		532 533	594.0 594.6	594.6 595.1	0.7	1.4	0.15 4.32	0.10 2.38	·				0.50	0.3 3.3
		534	595.1	595.9	0.8	1.7	0.73	0.55			·····		13.80	10.3
	DAA	535	595.9	596.4	0.5	1.4	0.05	0.03	0.06	0.03	0.34	0.17	1.50	0.7
197 233	706 638	118536 116729	596.4 487.0	597.3 488.2	0.8	2.1	0.86	0.73	0.58	0.32	0.86	0. 47	9.00 3.10	7.6 2.0
		730	488.2	488.9	0.7	1.7	0.04	0.03	0.09	0.06	0.48	0.34	1.70	1.1
		731	488. S	489.9	1.0	2.5	0.08	0.08					1.25	1.2
		732 733	489.9	490.5 491.2	0.7	1.6	2.01	1.31					70.30	45.7
231	639	116792	490.5	483.8	0.0	1.5	0.15	0.47			<u>.</u>		8.20	11.0 4.9
		116854	543.3	\$44.1	0.8	1.3	0.41	0.33			**************************************		13.80	11.0
239	640	116829	486.6	487.4	0.8	1.5	0.25	0.20					1.60	1.2
237	641	116830 117018	487.4	487.9 480.7	0.5	1.2	0. 71 0. 72	0.32					4.00 6.40	1.8
		19	480.7	481.4	0.7	1.7	2.99	2.09					24.40	17.0
	1	20	481.4	481.9	0.5	1.2	1.94	0.97		. 81 			39.60	19.8
		21 22	481.9 482.9	482.9 483.9	1.0 1.0	2.3	0. 57 0. 35	0.57		a sa			5.50 2.70	5. 5 2. 7
·•···		23	483.9	484.9	1.0	2.4	0.20	0.20		······	· · · · · · · · · · · · · · · · · · ·	•••••••	1.40	1.4
		- 24	484.9	485.9	1.0	2.3	0. 27	0.27					2.00	2. 0
447		25 117026	485.9 486.9	486.9 487.9	1.0	2.3	0.37	0.37			·····		4.40	4.4
237 233	642	117072	400. 9	489.9	1.0 0.8	2.4	0. 31 0. 21	0.31	0.26	0.20	0.55	0.42	2.50	2.5 3.4
		73	489.9	490.6	0.7	1.7	0.16	0.11					2.50	1.1
÷		74	490.6	491.0	0.4	1.0	2.14	0.86					15.60	6.2
<u>.</u>	· [· · · · · · · · · ·	75 76	491.0 491.8	491.8 492.4	0.8	2.0	0.17 0.08	0.13					0.00	0.3
•••••• • ••		71	492.4	493.0	0.6	1.4	0.40	0.24	0.66	0.40			0.80	0.4
		- 78	493.0	493.6	0.7	1.5	0.46	0.30					1.05	0.6
•••••		79 80	493.6 494.2	494. 2 494. 7	0.6	1.4	0.74 2.01	0.41			100 se 111 g		1.90 11.50	1.0 5.7
		81	494.7	494.1	0.5	1.3	2.01 1.87	1.01	1		[15.90	9.5
		82	495.3	495.9	0.6	1.5	2.45	1.47					25.70	15.4
		83	495.9	496.3	0.5	1.1	0.78	0.35				[17.10	1.1
		117074 117080	490.6 494.2	491.0 494.7	0.4	1.0 1.3	2.14 2.01	0.86	[· · · · · · · · · · · · · · · · · · ·	3	15.60 11.50	6. 2 5. 7
		117081	494.7	495.3	0.6	1.4	1.87	1. 12					15.90	9.5
		117082	495.3	495.9	0. 6	1.5	2.45	1.47					25.70	15.4
233	642	117083	495.9	496.3	0.5	1.1	0. 78	0.35	[17.10	1.1

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ine		Spl.	Spl. In		Spl.	Spl.	Cu %		РЬ 🗙	Pb	Zn %	Zn	hg g/t	Ag
No.	No.	No.	From	τo		Veight	grade		grade	m•%	grade		grade	n g/
233	642	117073	489.9	490.6	0.7	1.7	0.15	Q. 11					2.50	1.7
- :		117072	489.2	489.9	0.8	1.9	0.21	0.16	0.26	0.20	0.56	0.42	4.60	3.4
229		117273	481.2	481.7	0.5	1.2	3.15	1.58					0.00	
		117298	498.3	498.8	0.5	1.2	·····		0.04	0.02	0.02	0.10	0.80	0.4
		299	498.8	499.7	0.9	2.4	•••••••		0.09	0.08	0.03	0.03	1.00	0.9
		300	499.7	500.3	0.6	1.6	0 11	0.07			0.05			
•••••	·····		500.3				0.11	0.07	0.15	0.09		0.03	1.80	1.0
		301		500.8	0.5	1.4	2.42	1.09	0.04	0.18	0.24	0.11	13.30	5.9
		302	500.8	501.6	0.8		12.20	9.76	· · · · · · · · · · · · · · · · · · ·				143.30	114.6
		303	501.6	502.0	0.5	1. 2	3.71	1.67			<u> </u>		34.30	15.4
229		117304	502.0	502.4	0.5	1.1	0. 21	0.09	•				2.70	1.2
237	645	117169	475.9	476.6	0.7	1.5	0.20	0.13					0.00	. I
		170	476.6	477.1	0.5	1.1	0.60	0.30					5.40	2.7
		171	477.1	477.7	0.6	1.5	0.37	0.22					2.80	1.6
		172	477.7	478.2	0.5	1.1	0.14	0.07					1.60	0.8
	i.,	173	478.2	478.7	0.5	1.1	0.05	0.02	·····	···•···	••••••	·····	0.90	0.4
یئی بینی . ایک	······································	174	478.7	479.2	0.6	1.2	0.07	0.04	••••••••••				0.80	0.4
		175	479.2	479.8	0.6	1.8	4.13	2.48			••••	·····		
· · · · ·												· · · · · · · · · · · ·	45.50	27.3
····		176	479.8	480.3	0.7	1.5	0.71	0.46	0.40				15.20	9.8
		177	480.4	481.5	1.1	2.7	0.51	0.54	0.10	0.11			2.70	2.8
		178	481.5	482.5	1.0	2.3	0.28	0.28	0.02	0.02			2.40	2.4
		179	482.5	483.5	0.5	1.2	0.48	0. 22					14.60	6.5
		180	483.5	483.9	0.5	1.2	0.38	0.17					2.20	0.9
·	12	181	483.9	485.0	1.1	2.6	0.16	0.17		:			2.60	2.7
237	645	182	485.0	485.6	0.6	1.3	3.05	1.68					43.00	23.6
239	646	117331	467.7	468.7	1.0								3.00	3.0
		117522	615.2	615.7	0.5	• • • • • • • • • • • • • • • • • • • •	0.66	0. 33					5.00	2.5
	-	523	615.7	616.4	0.7	• • • • • • • • • • • • • • • • • • • •	0.77	0.54	••••••	·····		····	3.00	2.1
· · · · ·	••••	11531	622.2	622.7	0.5		0.18	0.09	0.28	0.14	0.09	0.05	3.00	1.5
231	648	117715	607.0	607.5	0.5	1.3	<u>v. 10</u>		0.08	0.04	0.03	0.03	0.80	
201	040	716	607.5	608.0	0.5									0.4
						1.2	······	••••••••••••	0.05	0.03	0.18	0.09	0.00	· - · · · - - · · ·
	·····	717	608.0	608.6	0.6	1.5	4 00		0.04	0.02	0. 21	0.13	0.00	·
		117783	761.7	762.3	0.6	1.1	1.39	0.76	0. 02	0.01			21.00	11.5
· · · · · · · · · · · · · · · · · · ·		784	762.3	763.0	0.7	1.6	0.75	0.53					14.80	10.3
,		785	763.0	763.5	0.5	1.0	0.53	0.27					12.40	6.2
		786	763.5	764.0	0.5	0. 9	1.35	0.68				4.1	34.00	17.0
233	δ49	117611	485.3	485.9	0.6	1.4	0.41	0.25					2.80	1.6
		612	485.9	486.4	0.5	1.1	0.37	0.19				· · ·	1.80	0.9
		613	486.4	487.1	0.7	1.7	0.71	0.50	0.15	0.11			2.50	1.7
		614	487.1	487.6	0.5	1.1	0.17	0.09	0.12	0.06		•••••	1.00	0.5
		615	487.6	488.1	0.5	1.3	0.06	0.03			·····	······	0.00	<u> </u>
		616	488.1	488.6	0.5	1 2	0.05	0.03	••••••	••••		·····		••••
		617	488.6	489.6	1.0	1.2 2.5			••••		· · · · · · · · · · · · · · · · · · ·	·····	0.00	
			489.6				0.44	0.44		·····	·····		8.40	8.4
· · · · · ·		618		490.2	0.6	1.4	0.12	0.07			····		1.00	0.6
		619	490.2	491.0	0.8	2.0	1.19	1.01					2.25	19.1
		117620	491.0	491.6	0.6	1.4	0.30	0.17					4.60	2.5
233		117804	496.2	498.7	0.5	1.2	0.37	0.19					1.80	0.9
		117812	501.7	502.7	1.0	2.5	0.22	0.22					0.50	0.5
		813	502.7	503.2	0.5	1.3	0.12	0.06					0.50	0.2
		815	503.7	504.3	0.6	1.4	0.77	0.46					2.20	1.3
		816	504.3	505.0	0.7	1.7	0.68	0.48					2.60	1.8
7		817	505.0	505.5	0.5	1.7 1.1	0.80	0.40	••••••	••••••		· · · · · · · · · · · · · · ·	5.20	2.6
	·	818	505.5	506.1	0.6	1.4	0.58	0.35				····;-··••		
	· • · • • • • • • • •		506.1	\$06.8		1 · 9						• • • • • • • • • • • •	3.30	1. 9
		819			0.7	1.5	0.01	0.01	• / /			. 	0.00	
		820	505.8	507.3	0.5	1.2							0.00	
		821	507.3	507.8	0.5	1.2							0.00	
		822	507.8	508.6	0.5	1.8	0.12	0.06					1.10	0.5
		823	508.6	509.6	1.0	2.0	0.19	0.19					5.60	5. 6
		824	509.6	510.5	0.9	2.0	0.13	0.12					4.20	3.7

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Line	Well	Spl.	Spl. In	terval	Spl.	Spl.	Cu X	Cu	Pb X	Pb	Za X	Zn	Ag g/t	Ag
No.	No.	No	From	To	eng.	Weight			grade		grade		grade	n·g/t
		825	\$10. \$	\$11.1	0.6	1.4	0.15	0.09					4.80	2.88
		826	\$11.1	\$11.7	0.6	1.5	0.12	0.07	19 ³				1.60	0.96
233	652	117827	\$11.7	\$12.2	0.5	1.2	2. 70	1.35					72.50	36.25
227		121405	350.3	351.0	0.7	1.4	0.26	0.18				• 11 v	1.00	0.70
		407	351.0	351.5	0.5	1.2	0.21	0.11		····•			2.00	1.00
		121421	493.6	494.1	0.5	1.2			0.11	0.06	0.25	0.13	2.00	1.00
		121426	495.6	497.2	0.6	1.4			0.08	0.04	0.49	0.27	2.00	1.10
191		120333	640.7	641.2	0.5	1.1	0.01	0.01	0.23	0.12	0.21	0.11	1.90	0.95
		334	641.2	641.8	0.5	1.1	0.04	0.02	0.41	0.21	0.52	0.26	2.60	1.30
		335	641.8	642.5	0.8	1.7	0.10	0.08	0.73	0.55	0.46	0.35	2.60	1.95
		335	642.5	643.0	0.5	1.3	0.13	0.06	0.64	0.29	0.38	0.17	2.00	0.90
		120339	644.2	644.9	0.7	1.4	1.17	0.76	0.04	0.03			30.00	19.50
187	780	132527	631.8	632.3	0.6	1.4	0.31	0.17	0.01	0.01			0.50	0.28
		\$28	632.3	632.7	0.4	0.9	0.53	0.21					0.50	0.20
		529	632.7	633.3	0.6	1.5	0.38	0.23	0.03	0.02			1.40	0.84
		530	633.3	633.9	0.6	1.4	Ò. 23	0.13	0.05	0.03	0.14	0.08	2.50	1.38
		531	633.9	634.4	0.5	1.0	0.05	0.03	0.31	0.16	0.07	0.04	4.00	2.00
		532	634.4	635.1	0.7	1.7	0.36	0.25	0.16	0.11	0.02	0.01	1.00	0, 70
		533	635.1	635.8	0.7	1.5	0.09	0.06	0.17	0.12			0.50	0.35
	-	534	635.8	636.5	0.7	1.5	0.05	0.04	0.08	0.06			1.20	0.84
		535	636.5	637.0	0.5	1.2	0.36	0.18				_	2.50	1.25
187	780	132536	637.0	637.7	0.7	1.7	0, 75	0.53		4		- 12 - 12 - 12 - 12 - 12 - 12 - 12 - 12	5.80	4.05
235	774	132300	459.5	460.2	0.7	2.4		. N	0.31	0.22		19.24	2.40	1.68
		304	469.0	470.0	1.0	2.4				۰.	0.30	0.30	1.50	1.50
		133313	452.4	452.9	0.4	0.8			0.51	0.20		5 - 5 - 2 5	9.00	3.60
		319	452.9	453. 2	0.3	1.0		·	0.43	0.15			4.80	1.68
		314	453.2	453.9	0.7	1.7			0.86	0.60			15.70	10.99
235	774	315	453.9	454.9	1.0	2.3			0.56	0.56			2.40	2.40
207	782	132944	601.5	602.0	0.4	1.0	0.69	0.28			1		0.50	0.20
	· · ·	945	602.0	602.5	0.6	1.3	1.95	1.07		1			11.80	6.49
		946	602.5	603.0	0.6	1.5	0.46	0.25		· ·			2.20	1.21
		947	603.0	603.6	0.6	1.3	0.14	0.08		·			0,50	0.28
207		132948	603.6	604.1	0.6	1.3	0.23	0.13					0.50	0.28
187		132736	634.8	635.3	0.5	1.3	0.02	0.01		· '.	0. 22	0.11	0.00	
		132742	638.8	639.4	0.6	2.4	1.74	1.04	· · · · · · · ·	· ·		1.2. N.	10.80	6.48
187		132743	639.4	639.9	0.5	1.2	1.00	0.50					10.40	5.20
203	776	133014	578.3	579.0	0.7	1.7			0.07	0.05	0.41	0.29	4.00	2.80
	ني : 	15	579.0	579.5	0.5	1.1			0.10	0.05	0.40	0.20	2.00	1.00
24 21		133020	582.0	582.7	0.7	1.7			0.04	0.03	0.31	0. 22	1.40	0. 98
		21	582.7	583.2	0.5	1.3			0.13	0.07	0.15	0.08	1.40	0.70
203		133022	583.2	584.0	0.8	2.0			0.04	0.03	0.69	0.55	1.00	0.80
189	795	133347	634.4	635.1	0.8	1.6	2.23	1.67					16.70	12.53
		348	635.1	635.5	0.4	1.0	0.05	0.02		· · · · · · · · · · · · · · · · · · ·	·····		1.10	0.44
		349	635.5	636.3	0.8	2.0	0.04	0.03			····		0.50	0.38
· · · · · · · · · · · ·		350	636.3	636.7	0.4	1.0	0.00		· · · · · ·				0.50	0.20
. : 		351	636.7	637.3	0.7	2.0	0.02	0.01			···· ····		0.70	0.46
s		352	637.3	637.8	0.5	1.2	0,23	0.10			····;	· · · · · · · · · · · · · · · · · · ·	1.30	0.59
·		353	637.8	638.5	0.7	1.5	0.85	0.60		••••••		le e e e e e e e e e e e e e e e e e e	3.20	2.24
		354	638.5	639.5	1.0	2.6	2.78	2.18		·•···•			4.70	4. 70
189		133355	639.5	639.9	0.4	1.0	0.46	0.18				·····	4.40	1.76
209	793	133306	601.3	602.3	1.0	2.6			0.30		.		0.50	0.50
		307	602.3	603.2	0.9	2.2	0.12	0.11	0.36	0.32		· · · · · · · · · · · · · · · · · · ·	0.70	0.63
· · · · · · · · ·	а ^{. с}	308	603.2	603.7	0.5	1.2	0.38	0.17		· · · · · · · · · · · · · · · · · · ·	···· ;•·· ;	•	2.00	0.90
		309	603.7	604.3	0.7	1.8	1.48	1.04				· • · · · · · · · · · · · · · · · · · ·	8.00	5.60
209		133310	604.3	604.9	0.8	1.5	0.24	0.14					1.00	0.60
190	801	133674	664.5	665.3	0.8	1.3	0, 49	0.25	·	·····			22.70	11.35
215	815	135634	589.5	590.4	0.9	2.2	0.31	0.28						
	F	635	590.4	591.4	1.0	2.1	0.40	0.40					l ·	1

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	<u></u>	<u></u>	F						T				****		
а 1.		Well	Spl.		terval	Spl.	Spl.	Cu X	Cu	Pb X	Pb	Zn X	Zn	Ag g/t	Ag
-	No.	No.	No.	From	To	Leng.	Weight			grade	<u>m•%</u>	grade	R•%	grade	<u>m·g/1</u>
			135639	593.7	594.4	0. 7	1.7	0.54	0.38						
1	 		640	594.4	595.1	0.7	1.7	0.54	0.38						
	1		641	595.1	595.8	0.7	>1.7	0.56	0.39	· · · · · · · · · · · ·		··· ··· ····			
		ng ing terri	642	595.8	595.7	0.9	2.2	0.85	0.77						
÷	215		135643	596.7	597.6	0.9	2.2	0.65	0.59	· · · · · · · · · · · · · · · · · · ·					
	207	811	135369	618.3	618.8	0.5	1.2	0.23	0.12						
			370	618.8	619.2	0.4	1.2	0.11	0.04			3 3			
	·····		371	619.2	619.7	0.5	1.1	0.20	0.10	·					
•			372	619.7	620. 2	0.5	1.1	0.64	0.32						
	209	814	135539	613.1	613.9	0.8	2.0	0.45	0.36		· .	:			
:			540	613.9	614.7	0.8	2.3	1.12	0.90						
1			541	614.7	615.4	0.7	2.0	1.47	1.03	. '				•	
	5. ja.	·	542	615.4	616.4	1.0	2.6	1.11	1.11	· · · ·				1	
			543	616.4	617.4	1.0	2.4	1.56	1.56						2
	209	803	133897	605.1	607.1	1.0	2.5	0.68	0.68	•••••					
8	209	803	133944	607.1	607.6	0.5	1.1	0.67	0.34				: : -		
											••••••		:		·····
	219	555	111290	617.0	617.5	0.5	40.0	0.03	0.01	0.07	0.04	0.00	•••••	•••••	
	2		291	617.5	618.0	0.6	44.0	0.03	0.02	0.00		0.00			
			292	618.0	618.7	0.7	52.0	0.04	0.03	0.00	·····	0.00			•••••
1			293	618.7	619.3	0.6	48.0	0.21	0.13				·······	0.00	
			294	619.3	620.3	1.1	84.0	0.24	0.25				· · · · · · · · · · · · · · ·	0.50	0.52
			111299	644.7	645.8		120.0	0.25	0.28	·····			· · · · · · · · · · · · · · · · · · ·	0.00	
			111295	641.5	642.5		120.0			0.26	0.29		••••••••	0.00	••••
			111300	645.8	646.3	0.5	40.0	0.10	0.05				· · · · · · · · · · · · · · · · · · ·	0.00	
			301	646.3	647.2	0, 9	76.0	0.04	0.04	0.17	0.20			0.80	0.76
:			302	647.2	647.8		120.0	0.05	0.03	0.70	0.39			0.00	·····
		••••••	303	647.8	648.3		120.0	0.04	0.02	1. 20	0.60	·····		0.50	0.25
			304	648.3	649.0		120.0			1.38	0.97	····2··		3.00	2.10
			111313	655.1	656.0	0.9	76.0	0.06	0.06			•••••••		0.00	6.10
		·····	314	656.0	656.9	0.8	68.0	0.14	0.12		·····		······	0.80	0.68
			315	656.9	657.8	0.9	72.0	0.54	0.49	••••••••••			·····	2.80	2.52
- 1		.1.1	316	657.8	658.2	0.4	32.0	0.91	0.36			•••••	·····	5. 50	2.20
	219	555	317	658.2	658.7	0.5	40.0	0.31	0.16	•••••			······	0.80	0.40
	201	504	10945	586.8	587.3	0.5	45.0	0.20				••••••	••••	0.00	0. 10
1.1			946	587.3	587.7	0.5	40.5	0.34						0.00	· · · · · · · · · · ·
			947	587.7	588.3	0.6	49.5	0.07	·····	0.20	•••••			0.00	
1		· · · · ·	948	588.3	588.9		120.0	0.20		0.20	•••••		· • • • • • • • • • • • • • • • • • • •	1.60	
			949	588.9	589.5		120.0	0.09			· • · · · · · · · · · · · · · · · · · ·	•••••	•••••	1. VV	•••
	201	504	10950	589.5	590.2		120.0	2.84		···	·····	•	·	17 60	10 90
1.1	201	505	10991	597.0	597.6		120.0	0.54	·····	·····;····	••••••			17.60 4.60	12.32 2.53
			994	599.2	599.8		120.0	0.35	·····	· • • • • • • • • • • • • •	•••••		· · · · · · · · · · · · · · · · · · ·		
- 1			995	599.8	600.8		120.0	2.90		·····		••••••••••	••••••	1.00	0.50
÷.,	201	505	10999	603.0	603.0		120.0	0.50		0. 11		•····•	· · · · · · · · ·	18.40	19.32
-	205		109543	568.3	568.7	0.5	60.0	0.07	0.04	<u>v. 11</u>	······	0.96	0 12	2.40	A 60
1			544	568.7	569.3	0.5	60.0	0. 20	0.10			0.26	0.13	1.00	0.50
·			109087	663.7	664.2	0.5	40.0	0. 22	0.10	••••••	••••••	V. 21	v. 14	1.20	0.60
			89	664.7	665.2	0.5	40.0	0. 50	0. 25	· · · · · · · · · · · · · · ·				0.60	0.30
		·····	09104	676.3	677.1					····	····			0.00	····
	·····	····· ľ	105	677.1	677.6	0.8		0.27	0.23		···· ···		····	0.00	······
	·····	·····	105	677.6	678, 1	0.5		0.27	0.14		<u>.</u>	·····		0.00	
	·····[107	678.1	678.6	0.5		0.04		· · · · · · · · · · · · · · · · · · ·		•••••••	·····		
· · ·	····		107			0.5		0.12			····.		·····		,[
	·····			678.6 679.1	679.1	0.5		0.00		•••••				····	
· · ·	•••••		109		679.6	0.5	20.0	• • • • • • • • •	····	••••••					
, i			110	679.6	680.1	0.5	20.0								
	· · · ·	·····	111	680. 1	680.6	0.5	20.0		A 44	·····					
	·····		112	680.6	681.3	0.7			0, 69					1.40	0.91
· 1.			113	681.3	681.7	0.5	40.0	V. 32	0.16					1.00	0.50

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Ē	ine	Yell	Spl.	Spl In	terval	Spl.	Sp1,	Cu %	Cu	Pb %	Pb	Zn %	Zn	Ag g/t	Ag
	No.	No.	No.	From	To		Veight			gráde		grade		grade	n∘g/t
	205	532	114	681.7	682.3	0.5	40.0	1.13	0.57	BIAUG	10 70	RIAUC	U1 70	1.40	0.70
	209		110295	610.8	611.2	0.5	50.0	2.91	1.45	·····				4.40	2.20
	4V J		296	611.2	611.8	0.5	50.0	4.47	2.24					23.40	11.70
			297	611.8	612.3	0.6	55.0	1. 52	0.84		· · · · , · • • • •			64.00	35.20
	•••••		298	612.3	613.2	0.9	18.0	0.06	0.05			••••••		1.20	1.08
			299	613.2	613.7	0.5	10.0	0.02	0.01		· · · · · · · · · · · · · · · · · · ·	·····	·····	0.50	0.25
	• • • • • •		-300	613.7	614.7	1.0	20.0	0.28	0.28		·	•••••		0.50	0.50
· •			301	614.7	615.4	0.7	14.0	0.52	0.36					1.10	0.17
			302	615.4	615.9	0.5	10.0	0.46	0.23	i				0.90	0.45
			303	615.9	616.9	1.0	20.0	0.14	Ö. 14	0.09		••••••		1.70	1.70
			304	616.9	617.9	1.0	20.0	0.25	0.25	0.04				2.10	2.10
			305	617.9	618.4	0.5	9.0	0.25	0.11	0.00				1.50	0.07
	217	539	110197	536.3	\$36.6	0.4	28.0	0.67	0.27				1947	2.10	0.84
					537.35	0.7	49	0.05	0.04					0.001	یں۔ دیکھیتیں
:				537.35	538	0.65	45.5	0. <u>9</u> 9	0.64		يتشتذ			5.4	3. 51
		· · · · · ·	110211		545.35	0.55	33			0.2	0.11			0.001	
		<u>.</u>			545.85	0.5	30	0.08	0.04	0.54	0.27	····;		0.6	0.3
		.			546.25	0.4	24	0.05			0.001			20.5	
	÷	·			546.75	0.5	30	0.16	0.08	0.5	0.25			0.8	0.4
	217	539	215 216	546.75	547.7 548.2	0.95	95	0.62	0.87	·····		·		4.2	3.99
	217		111341	541	541.7	0.5 0.7	50 120	0.13	0.31			·····		3.6	1.8 0.98
	211	000	111352		553.85	0.5	60	0.22	0.11			·-,		0.6	0.3
1		in de la composición de la composición Composición de la composición de la comp		553.85	554.3	0.45	60	0.26	0.12			•••••	·····	0.5	0.23
. •			113355		555.55	0.45	27	0.03	V. 16	0.44	0.2	······································	····	0.7	0.32
÷				555.55	356	0.45	27	0.05		0.05	0.02	······		0.6	0.27
		1	357	556	556.5	0, 5		D. 001		0.28	0.14	••••••		1.1	0.55
			358	556.5	557	0.5	30	0:001		0.27	0.14			1	0.5
	229	602	115142	504.4	504.9	0.5	120	•••••	•••••••	0.26	10 N.			1.1	0.55
			143	504.9	505.4	0.5	20	0.56	0.28					2.3	1.15
·].	· · · · · · · · · · · · · · · · · · ·		144	505.4	505, 8	0.4	- 16	2.64	1.06					11.1	4.44
			145	505.8	506.5	0.7	28.0	3.34	2.34				1.1	49.90	34.93
		· · · ·	146	506.5	507.0	0.5	20.0	5.01	2.51					34.00	17.00
÷ .			147	507.0	507.5	0.5	20.0	1.62	0.81	0.13				11.60	5.80
	229	602	115148	507.5	508.0	0.5	20.0	1.51	0.76					12.50	6.25
	217	556	111368	563.0	563.8	0.8	16.0	0.70	0.56					2.80	2.24
		·····	369	563.8	564.3		10.0	2.20	1.10		· • · · • • • • • • •			3.60	1.80
			370 371	564.3 564.8	564.8 565.5	0.5	10.0 14.0	1.20 1.95	0.60 1.37		· • • • • • • • • • • • • • • • • • • •			4.70 7.10	2.35 4.97
1	••••		372	565.5	566.5	1.0	20.0	0.03	0.03					0.00	4.34
ŀ	•••••		373	566.5	567.0	0.6	11.0	0.02	0.01				4	0.00	
			374	567.0	567.7	0.7	13.0	0.60	0.39					1.80	1.17
	. .	· · · · · ·	375	567.7	568.5	0.8	16.0	0.09	0.07					0.00	
	•••••		376	568.5	569.4	0.9	18.0	0.04	0.04		1. 2			0.00	
2			377	569.4	570.0	0.6	12.0	0.78	0.47		1 × .			3.60	2.16
			378	570.0	570.9	0.9	18.0	2.08	1.87	·				9.60	8.64
			379	570.9	\$71.8	0.9	18.0	3.85	3.47		2.			21.70	19.53
			380	571.8	\$72.5	0.7	14.0	3.28	2.30		5 (1) 			13.20	9.24
- E			111378	570.0	570.9	0.9		2.08	1.87				[9.60	8.64
1			111379	570.9	571.8	0.9		3.85	3.47					21. 70	19.53
			111380	571.8	572.5	0.7		3.28	2.30	· · · · · ·		.		13.20	9.24
	217	558	111426	530.1	530.6	0.5	120.0	0.51	0.26			[2.30	1.15
			435	537.7	538.3		120.0	1.33	0.80		· • · • • • • • • • • • • • • • • • • •			7.60	4.56
	· · · · · · · ·		469	615.4	616.0	0.6	120.0	1.35	0.81	·		·····		4.30	2.58
	41A		11114	C07 4	LOD A			5 AA	0.10					17 24	
	219	561	111495	527.4	527.9	0.5		5.00	2.48	•				7.70	3.85
		•••••	496	527.9 528.6	528.6 529.1	0.7		0.87	0.61	••••••	·	[· · · · · · · · ·	1.10 5.20	0.77
÷ J.	••••••	I	1 421	320.0	1 969. 1	0.5	l	3.72	1.86	Ii.	ŀ	J	I	į 0.2V	2.60

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inę	Well-	Spl.	Spl.In	terval	Spl.	Spl.	Cu X	Cu	Pb X	РЪ	Zn %	Zn	Ag g/t	Ag
No.	No.	No,	From	To	leng.	Veight		m•%	grade		grade		grade	m·8/
		498	529.1	529.9	0.8		0.56	0.45		· · ·		÷.,	0.50	0.4
		499	529.9	530.6	0.8	15.0	0.08	0.05			0.44	0.33	0.00	
·····		500	530.6	531.3	0.7	14.0	0.17	0.12	0.15	0.11			0.00	
		501 502	531.3 531.9	531.9	0.5	10.0	2.99	1.50				·····	5.60	2.8
•••••		503	532.5	532.5	0.8	13.0 16.0	1.46 2.64	0.95 2.11	0. 27	0. 22		·····	2.80	1.8
·····		504	533.3	534.2	0.8	17.0	2.09	1. 78	0. 21	0. 22		····•	11.60	9.2 8.6
		505	534.2	535.0	0.8		13.00	8.32	0.03	0.02			55.00	44.0
··· · ···		506	535.0	535.9	0.9	18.0	6.73	6.06			·····		28.60	25.7
		507	535.9	536.3	0.5	10.0	6.85	3. 42	:	••••••••		· · · · · · · · · · ·	24.00	12.0
		508	536.3	536.9	0.5	10.0	1.52	0.76					4.90	2.4
·		509	536.9	537.3	0.5	10.0	3.91	1.98	0.04	0.02		. Г.	13.90	6.9
		510	537.3	537.8	0.5	10.0	4.11	2.05		منيورو مورد د			18.50	9.2
223	562	111676	523.8	524.8		120.0	0.47	0.47	0.10	0.10		:	1.00	1.0
		677 678	524.8 525.8	525.8 526.4	1.0		0.82 0.32	0.82	0.07	0.07 0.05		· · · · · · · · · · · · · · · · · · ·	0.90	0.9
		679	526.4	527.1	0.6 0.7		0.32	0.13	0.08 0.18	0.05		<u>.</u>	0.80	0.4
		680	527.1	527.9	0.8		0.60	0.45	0. 10	0.13			1.80	0.1 1.3
••••		681	527.9	528.5	0.6	· · · · · · · · · · · ·	0.11	0.07	0.00	¥• 31		1. A	1.80	1.0
		682	528.5	529.3	0.9	•••••	0.84	0.76					3.00	2.7
		683	529.3	530.0	0.7	·····	1.28	0.90					6.90	4.8
221	564	111573	531.0	531.5	0.5	: 	0.28	0.14					3.00	1.5
		574	531.5	532.0	0.5	·····	2.95	1.48		· <u></u>	· · ·		21. 20	10.6
		\$75	532.0	532.8	0.8		0.11	0.09	0.06	0.05	· · · · · · · · · ·	·-···	1.40	1.1
		576 577	532.8 533.4	533.4 534.0	0.7 0.6		0.80 2.05	0.52	0.71 0.05	0.46			2.00	1.3
		578	534.0	534.5	0.5	• : •	2.03 5.25	2.63	0.00	<u>v. və</u>			8.00 27.00	4.4 13.5
		579	534.5	\$35.0	0.5	••••••	4.10	2.05	V. VU	••••••••		•••••	20.00	10.0
••••••••		580	535.0	\$35.7	0.7		0.19	0.13				·····	1.00	0.7
221	564	581	535.7	536.4	0.7	:	1.50	1.05					8.00	5. 6
221	566	566854	522.1	522.6	0.5		0.04	0.02			0.41	0.21	0.80	0.4
••••••		855	522.6	523.2	0.6	· · · · · · · · · · · · · · ·	0.17	0.10			0. 24	0.14		
	· · · · · · ·	856	523.2	524.0	0.8						<u>.</u>	•••••		· · · · · · · · · · · · · · · ·
•••••	<u>.</u>	857 858	524.0 524.9	524.9 525.6	0.9		0.00	A 06		· · · · · · · · · · · · · · · · · · ·	A 22	A 19	1.10	1.0
••••		859	525. 6	526.4	0.8 0.7		0.08	0.05	••••••		0.23 0.33	0.17	1.40 3.70	1.0 2.5
• • • • • • • •		860	526.4	527.0	0.7	•••••••	0.70	0.46		· • • • •	0.15	0. 23	9.40	6.1
		566865	529.6	\$30.5	0.9	••••	0.08	0.07	1.00	0.90	0.28	0.25	2.00	1.8
		866	530.5	531.1	0.6		4.30	2.58					96.30	57.7
•••••••		867	531.1	531.6	0.6		3.35	1.84	0.11	0.06			10.00	5.5
•••••		868	531.6	532.3	0.7		4.75	3.09	0.46	0.30		۰۰ د . ۱۰۰۰ منب	19.80	11.8
		112035	592.5	593.5	1.0		0.25	0.25		·····	· · · · · · · · · · · · · · · · · · ·	· · · · · · · · · · · · · · · · · · ·	0.50	0.5
••••••••••••••••••••••••••••••••••••••		36 112041	593.5 596.7	594.2 597.2	0.7 0.5	·····	1.25 0.42	0.88		·····		••••••	2.00	1.4
		111924	619.4	620.0	0.6		0.42	0. 21				······································	0.70 1.00	0.3 0.5
		933	625.6	626.0	0.5		0.90	0.41	· · · · · · · · · · · · · · · · · · ·				0.00	v. ə
•••••		937	628.2	628.7	0.5		0.49	0.25	·····		··••••••••••••••••••••••••••••••••••••	•••••••••••••••••••••••••••••••••••••••	1.20	0.6
• •		948	636.9	637.2	0.4		0.03	0.01	0.23	0.09	0.93	0.36	1.40	0.5
: :		949	637.2	637.8	0.6		0.13	0.07			0.46	0.25	0, 00	
· • · • • • • • • •		952	639.2	639.7	0.5		0.03	0.01	0.10	0.05	0.23	0.10	0.00	
		953	639.7	640.2	0.5		0.25	0.13	0.02	0.01	0.37	0.19	0.80	0.4
		954	640.2	640, 7	0.5	 	5.15	2.58	0.04	0.02	0.82	0.41	9.80	4.9
	••••••	955 956	640.7 641 1	641.1	0.5	·····	0.12	0.05	0.10	0.05	0.78	0.35	0.80	0.3
· · • · • • • • · · ·	· • • • • • • • •	955	641.1 649.1	641.6 649.6	0.5	······	0.23	0.10	·····		0.50	0. 23	0.00	1 A
221	566	566969	649. f	650 <i>.</i> 1	0.5	••••••	1.10 0.75	0.55	•••••			· · · · · · · · · · · · · · ·	2.70	1.3
223		111883	523, 5	524. 1	0.5	•••••	1.50	0. 38	·····	••••••••••	·••••;•••••		0.80	0.4
		884	524.1	524.8	0.7		5.05	3. 54		•••••	·····		<u>4. 40</u> 19. 80	13.8

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line	Yell	Spl.	Spl. In	terval	Spl.	Spl.	Cu X	Cu	Pb X	Pb	Zn X	Zn	Ng g/t	Ag
No.	No.	No.	From	То	Leng.	Weight	grade	n•%	grade	m•%	grade	n•%	grade	m·g/t
		885	524.8	525.6	0.8		12.20	9.76				сf.	57.20	45.76
		886	525.6	\$26.2	0.7		3.65	2. 37					0.80	0.52
		887	526.2	526.8	0.6		0.43	0.24					3.00	1.65
· · · · · · · · · · · · · · · · · · ·		915	549.1	549.5	0.4		1.75	0.70	2.40	0.09			8.00	3.20
· · · · · ·		916	549.5	\$50.3	0.8		0.11	0.09	0.10	0.08			1.40	1.12
	·····	917	550.3	550.8	0.5		0.32	0.02					2.40	1.20
229	611	115242	518.2	518.9	0.7		0.32	0.22			••••••	<u></u>	0.50	0.35
		243	518.9	519.4	0.5		0.64	0.32	·····	·····	·····	-1	0.60	0.30
·····	· · • • • • • • • • •	244	519.4	519.9	0.5		0.12	0.05	·····				0.00	···· •• ••
•		245	519.9	520.4	0.5	•••••	0.17	0.09					1.00	0.50
		246	520.4	\$21.1	0.7		0. 57	0.40			• • • • • • • • • • • • •		3. 20	2.24
101	170		614.7	615.7			0.42	0.42	·····		•••••		24.50	24. 50
191	173	9488			1.0	1.3			<u></u>		·····			
		9489	615.7	616.7	1.0	1.3	0.43	0.43						180.00
203	205	12372	560.9	561.3	0.9	1.2	1.76	1.58		····· <u>·</u> ···		· · · · · · · · · · · · · · · · · · ·	12.60	11.34
235	216	13221	491.2	492.2	1.0	2.4	0.28	0.28				·····	1.00	1.00
		13226	494.4	495.2	0.8	1.0	0.83	0.66	· · · · · ·	· · ·			3.00	2.40
		13227	495.2	495.0	0.8	0.8	1.17	0.94			ai e.		5, 50	4.40
235	216	13228	496.0	498.7	0.7	0.8	0.00	:		<u>.</u>				
199	218	14579	584.3	584.9	0.6	2.0	0.00		1997 - 1997 		· ·		0.90	0.54
		14580	584.9	585.5	0.6	0.8	0.00					1	0.60	0.36
199	218	14581	585.5	586.0	0.5	1.2	0,00						0, 90	0.45
197	293	31276	547.1	547.6	0.5	2.5	0.13	0.07					4.60	2.30
203	307	15923	631.5	632.0	0.5	2.4	0.32	0.15					8.15	4.08
203	321	16097	630.2	630.9	0.7	4.0	0.69	0.48					14.30	10.01
193	377	17122	595.6	596.7	1.1		0.08	0.09						
		17123	596.7	597.5	0.8		0.00		[
	········	17124	597.5	598.5	0.6		0.11	0.07					2.30	1.38
····		17125	598.1	599.0	0.9	-	0.16	0.14					3, 40	3.05
	·····	17126	599.0	599.8	0.8	1	0.38	0.30			•••••		3.50	2.80
217	100	104931	542.1	543.1	1.0	2.3	0.14	0.14			••••••		2.30	2.30
617	400	104932	543.1	544.1	1.0		0.04	0.04					4.00	4.00
			544.1	544.6	0.5	2.1		0.04		· · · · · · · · · · · · · · · · · · ·			0.50	0.25
·····	· · · · · · · · · · · ·	933	544.6			1.1	0.00	0.05		•••••••••				
		934		545.1	0.5	1.4	0.09	0.05					1.80	0.90
····		935	545.1	545.6	0.5	0.8	0.16	0.08		•••••	·····		2.80	1.40
		104936	545.6	546.3	0.7	1.6	0.09	0.05			•····•		2.20	1.54
203	466	105167	\$65.0	565.5	0.5	1.7	0.00						3.80	1.90
Ì		168	565, 5	566.0	0.5	1.0	0.00	· · · · · · · · · · · · · ·						اليت بينية
		169	566.0	566.6	0.6	1.7	0.00			.	<u>.</u>	.		
187	500	107593	637.1	638.1	1.0	2.4	0.08	0.08	.	ļ	[1.60	1.60
	[107594	638.1	639.1	1.0	2.5	0.10	0.10			Į	.	0.60	0.60
		107595	639.1	639.8	0.7	14	0.07	0.05			[]]]		0.60	0.42
207		109522	570.9	\$71.5	0.6	1.4	0.17	0.10	0.04	0.02			3.50	2.10
193	525	109120	632.0	632.5	0.5	1.2	0.42	0.21					4.30	2.15
		109121	623.5	624.0	0.5	1.0	0.36	0.18					2.60	1.30
213	553	111035	547.9	548.7	0.8	2.0	0.03	0.02	0.01	0.06	0.06	0.05	4.30	3.44
219		111315	656.9	657.8	0.9	2.4	0.54	0.49		- 12			2.80	2, 52
		111316	657.8	658.2	0.4	1.0	0.91	0.36		L			5.50	2.20
· · · · · · · · · · · · · · · · · · ·		111317	658.2	658.7	0.5	1.2	0.31	0.16		1		 	0.80	0,40
211	255		600.6	601.5	0.9	2.2	3.16	2.84			:		7.30	6.57
					1			1						1
		1			and at			. <u>1</u>	····· 、			1		
239	617	112015	104 4	105 0	۸.	21	0 17	0.14	0 20	0.26	0.12	0.10	3.00	2.55
234	DI	116015	496.0	495.8	0.8	2.1	0.17	0.14	0.30	0.20	V. 12	0.10		
· · · · ·		16	495.8	496.5	0.7	1.8	8.85	6.20	0.02			. .	128.60	90.02
		17	496.5	497.1	0.6	1.4	1.48	0.89	0.07	0.04			12.00	7.70
239		116018	497.1	497.7	0.6	1.4	2.35	1.41	1			.[43.40	26.04
231	622	115788	505.8	506.4	0.6	1.5	0.44	0.26	0.13	0.08	[4.50	2.70
l		789	506.4	506.9	0.5			0.94	[18.00	9.00
	1	790	506.9	507.4	0.5	1.2	0.24	0.12	1	1.	1	1	1.50	0.75

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	Line	Well	Spl.	Sol In	terval	Spl.	Spl.	Cu X	Cu	РЬХ	Pb	Zn X	Zn	Ag g/t	Ag
÷	No.	No.	No.	From	To		Weight			grade		grade		grade	m·g/t
			791	507.4	508.3	0.9	2.2	0.31	0.28					1.00	0.90
			792	508.3	509.3	1.0	2.7	0.16	0.16	0.14	0.14			1.00	1.00
		· · · · ·	793	509.3	510.3	1.0	2.5	0.07	0.07				1. 1. 1 ^{. 1} .	0.00	
1		· · · ·	794	510.3	511.3	1.0	2.3	0. 63	0.63			· · ·		2.20	2.20
÷	231		115795	511.3	512.3	1.0	2.3	0.32	0.32	·····	 			3, 20	3.20
	237		116350	448.1	448.9	0.8	1.7	1.06	0.85	<u> </u>	A 65	Δο	A 64	15.40	12.32
			116357	454.1	455.0 455.9	0.9	1.7			0.22	0.20	0.23	0.21	1.60	1.44
		. .	358 359	455.0 455.9	455. 4	0.5	0.7 1.0		· • • • • • • • • • • • •	0.05 0.15	0.03	0.30	0.05	0.50 2.20	0.45 1.10
			360	456.4	457.2	0.8	2.0	· • · · · · · · · · · · · · ·		0.12	0.10	0.34	0. 27	1.70	1.36
		····	116379	473.4	474.3	0.9	2.2	0.10	0.10					1.60	1.44
			116380	474.3	475.1	0.8	2.0	0.11	0.09	0.10	0.08	0.48	0.38	2.40	1. 92
e.			381	475.1	475.6	0.5	1.2	0.12	0.06	0.19	0.10	0.30	0.15	10.30	5.15
			382	475.6	476.6	1.0	2.7	0.05	0.06	0.25	0.25	0.20	0.20	8.40	8.40
		<u></u>	383	476.6	477.6	1.0	2.7	0.03	0.03	0.11	0.11	0.11	0.11	2.00	2.00
		100 	384	477.6	478.5	0.9	2.2	0.02	0.02	0.19	0.17			1.40	1.26
			385	478.5	479.2	0.7	1.7	0.79	0.51	0.09	0.06	• · · · · · · · · ·	<u>.</u>	6.00	4.20
			386 387	479.2 479.8	479.8 480.4	0.6	1.5 1.2	2.31	1.39 0.18	•••••	·····	••••••	- 	24.00 3.00	14.40 1.65
1		· · · · · · · · ·	388	479.0	480.9	0.6	1.6	3.89	2.33					34.00	20.40
		·····	116584	520.3	520.9	0.6	1.5	0.28	0.17		· · · · · · · · · · · · · · ·	·····		1.40	1.26
	·····		116590	\$25. \$	526.0	0.5	1.2	2.72	1.36		······		· • · · · · · ·	5.10	2.55
			591	526.0	526.8	0.8	1.2 2.1	0.73	0.58					2.10	1.68
•			592	526.8	527.4	0.6	1.5	0.01	0.01					0.00	
	237		116593	527.4	527.9	0.5	1.3	0.38	0.19					15.10	7.55
:	229	625	116562	514.9	515.4	0.5	1.2	0.26	0.13		·····		. .	2.10	1.05
		· · · ·	563	515.4	515.9	0.5	1.2	0.02	0.01	.	· • • • • • • • • • • • • •		•••••	0.00	
÷		·····	564	515.9	516.5	0.5	1.6	1.32	0.82	•····	.		· • · · · · · · · · · · · · ·	4.30	2.58
:	·····		565 566	516.5 517.0	517.0 517.4	0.5	1.2	2.50 1.03	1.25		·····	·······	·•····	<u>3.00</u> 1.40	1.50 0.63
	<u>.</u>	· • · · • · • · • · ·	567	517.4	517.9	0.5	1.1	0.23	0.10				· • · · · · · · · · · · · · · ·	0.50	0.27
	···· 、	· • · · • · • · • · • ·	568	517.9	518.4	0.5	1.1	0.06	0.03		·••••••			0.00	
			569	518.4	518.9	0.5	1.3	0.09	0.05	•••••				0.00	
			570	518.9	519.3	0.5	1.1	1.62	0.73					13.10	5.90
÷			571	519.3	519.8	0. 5	1. 2	0.28	0.13					0.80	0.76
			512	519.8	520.3	0.5	1.2	0.48	0.24		· · · · · · · · · · · · · · ·		· • • • • • • • • • • • • • • • • • • •	2.10	1.05
1	229		116573	520.3	520.8	0.5	1.2	0.22	0.11	•••••	·····		. .	1.70	0.85
÷.,	235	οZA	116287 288	509.8 510.2	510.2 510.7	0.6 0.5	1.1 1.2	0.36	0.20	•••••			· · · · · · · · · ·	3.00 8.50	1.35
	233	631	116487	499.3	500.2	0.6	1.6	0.20	0.33	· · · · · · · · · · ·	·····			16.00	9.25
			488	500.2	500.8	0.6	1.5	0.10	0.06				i , '	0.50	0.30
			489	500.8	501.3	0.5	1.1	1.51	0.76		··· · ····		· · · · · · · · · · · · · · · · · · ·	13.40	6.70
			490	501.3	502.3	1.0	2.4	0.17	0.17			• • • • • • • • • • •		0.50	0.50
			491	502.3	502.8	0.5	1.0	0.77	0.39				· · · · · · · · · · · · · · · · · · ·	5.00	2.50
	,×.		492	502.8	503.3	0.5	1.0	1.38	0.69				. . .	16.00	8.00
			493	503.3	503.9	0.6	1.0 1.8 1.3	1.43	0.86		. 		····	19.20	11.52
			494	503.9	504.4	0.5	1.3	1.31	0.66					17.20	8.60
			495 496	504.4 504.9	504.9 505.6	0.5	1.3	0.88 0.98	0.44	:-				13.80	6.90
		·····	490	504.9	505.6	0.7	1.7 2.4	0. 98	0. 69 0. 48			••••••	····	13.00 6.80	9.10 6.80
		· • • • • • • • •	498	506.6	507.6	1.0	2.4	0. 40	0. 58	•••••••••••••••••••••••••••••••••••••••	••••••	·····	•••••••	3.00	3.00
		· · · · · · · · ·	499	507.6	508.2	0.6	1.5	0.01	0.01	******	·····		••••••	0.00	
	233	631	116500	508.2	508.9	0.7	1.7	0.01	0.01				•••••••	12.00	8.40
					1		••••••••••							-1.2	
:	239	633	116516	522.6	523. 2	0.6	1.5	0.42	0.25					3.00	1.80
			517	523.2	523.7	0.5	1.3	0.21	0.11					0.70	0.35
	235	612	116081	475.9	476.4	0.5	1.2	0.22	0.11	0.10	0.05	0.27	0.14	1.40	0.70
	I	l	82	476.4	477.3	0.9	2.0	0.05	0.05	0.08	0.07			1. 20	1.08

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line	Well	Sp1.	Spl In	terval	Spl.	Sel	Cu %	6	Pb X	Pb	7n ¥	7.	ha alt	1 10	1
No.	No.	No.	From	То	Leng.	Spl. Weight		Cu m·X	grade	1 A A	Zn X grade	2n מיא	Ag g/t grade	Ag m·g/t	
		83	477.3	477.8	0.5 0.5	1.1	0.52	0.26					2.40	1.20	
·		84	478.8	479.3	0.5	1.1	0.23	0.12				۰ ۲۰. در ۲۰۰	1.20	0.60	
235	612	116093 116103	484.4	484.9 478.8	0.5	1.1	3.16 10.80	1.58	· · · · · · · · · · · ·				34.60	17.30	
231	614	115543	515.9	516.8	1.0 0.8	2.0	0.78	10.80 0.65	0.03	0.03			67.00 1.40	67.00	
		544	516.8	517.6	0.8	2.0	0.25	0.21	V. UU	v. vv	·····ii···		0.60	0.51	
		545	517.6	518.2	0.6	1.1	0.19	0.10					0.00		
		546	518.2	518.8	0.6	1.0	0.06	0.03			••••••		0.00		
[547	518.8	519.2	0.5	0.7	0.04	0.02	· :'	· · · · · · · ·	· · · · · · · · ·		0.00		
231	614	548 115549	519.2 519.6	519.6 520.1	0.4	0.8	1.44	0.58		·····		•••••	8.20 11.60	3.28 5.80	
225		116054	524.4	524.9	0.5	1.0	0.29	0.13	••••••				1.00	0.45	
		55	524.9	525.8	0.9	2.2	0.10	0.09			2	¢.	0.00		
		56	525.8	526.4	0.7	1.5	0.04	0.03	· · · ·				0.00		
		57 58	526.4 526.9	526.9 527.5	0.5	1.3	0.22	0.11					0.50	0.23	
		59	527.5	528.1	0.7	1.1 1.6	0.11 0.51	0.07 0.28			· · · · · · · · · · · · · · · · · · ·	· · · · · · · · · · · · · · · · · · ·	0.00	0.55	
		60	528.1	528.7	0.7	1.6	0.41	0.27	•••••				1.60	0.88	
		61	528.7	529.5	0.8	2.1	Ő. OŠ	0.04					0.00		
	. <u>.</u>	62 63	529.5	530.4	0.8	2.1	0.03	0.03					0.00		
		63	530.4	531.3	0.9	2.3	0.06	0.05	0.15	0.14	2 		0.50	0.45	
		64 65	531.3 531.9	531.8 532.4	0.5	1.2 1.4	0.11 0.05	0.06				<u>.</u>	0.50	0.25	
·		66	532.4	533.3	0.8	2.1	0.54	0.46	·,· ··· ··		······		0.80 3.40	2.89	
225	619	116067	533.3	534.1	0.8	2.0	0.33	0.28		•••••			3.10	2.64	
231	648	117650	504.1	504.9	0.8	1.7	Ŏ. 28	0.21					3.00	5.10	
		651	504.9	505.4	0.5	1.1	0.02	0.01					0.00		•
		652 653	505.4 505.9	505.9	0.5	1.1	0.00	0 00	с. с. оо	à ÀA			0.00	0.00	
231	648	117661	511.0	506.4 511.5	0.5	1.2	0.04	0.02	5.80	2. 90		••••••	6.60 2.50	3.30 1.25	
					· • • • •		0.00			 			<u> </u>	3.20	
205	532	109088	664.2	664. 7	0.5	40.0	0. 17	0.09					0.60	0.30	
219	555	111216	537.3	538.4	1.1	63.0	0.28		0.05	0.05	0.25	0.26	2.60	2.73	·
		217	538.4	539.4	1.1	63.0	0.12	0.13				0.05	2.30	2.42	
	· · · · · · · · · · · · · · · · · · ·	218	539.4	540.0	0.6	36.0	0.48	0.29				: 	2.00	1. 20	
		111222 111227	568.4 572.1	569.1 572.8		120.0 120.0	0.25	0.19		······			1.00	0.75	
		111239	589.3	589.7	0.5	54.0	0.39 0.73	0.27 0.33	0.01	0.01	••••••••••		1.00 5.00	0.70 2.25	
		240	589.7	590.4	0.6	12.0	0.27	0.16	0.93	0.56			2.30	1.38	
		241	590.4	591.2	0.8	17.0	1.19	1.01	0.07	0.06			6.50	5.53	
		242	591.2	591.7	0.5	10.0	0.18	0.09					2.00	1.00	
· · · · · · · · · · · ·		243 244	591.7 592.5	592.5 593.3	0.8 0.8	15.0 16.0	0.37	0.28		<u>A A</u>		ų darijas Videntas	2.10	1.58	
••••••		244 245	593.3	593.8	0.8	10.0	0.67 0.91	0.54	0.05 0.69	0.04	•••••••		4.20 12.00	3.36	
		246	593.8	594.3	0.5	10.0	0.33	0.17	0.25	0.13	·····a	· • · • · • · •	4.00	2.00	
		247	594.3	595.1	0.8	16.0	1.03	0.82	0.08	0.06	ан ₁₁ н		10.00	8.00	•
		248	595.1	595.7	0.6	12.0	3.65	2.19					37.00	22.20	
		249 250	595.7 596.3	596.3	0.6		56.19 0 50	3.71	•••••				53.00	31.80	
· • • • • • • •		230	595.1	596, 7 595, 7	0.4	8.0 12.0	0.59 3.65	0.24 2.19	·····	····· •	·····		5.20 37.00	2.08 22.20	
		111249	595.7	596.3	0.6	12.0	6.19	2. 1 3. 71				······	53.00	31.80	
	1	111250	596.3	596.7	0.4	8.0	0.59	0.24				1	5.20	2.08	
		111251	596.7	597.5	0.8	32.0	0.17	0.14							
		252	597.5	598.0	0.6		0.15	0.08	е. 1			····			
·····•;		253 254	598.0 598.8	598.8 599.5	0.8		0.08	0.06	•••••		·····		· · · · · · · · · · ·	· · · · · · · · · · · · · · · · · · ·	
	i	255			0.9		0.05	0.03							

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Line	fell	Spl.	Spl. In	terval	Špl.	Spl.	Cu %	Cu	Pb X	Pb	Zn X	Zn	Ag g/1	Ag
No.	No.	No.	From	То	leng.	Weight	grade	п•Х	grade	m•%	grado		grade	n•g∕t
		256	600.4	601.0	0.7	52.0	0.23	0.15				· · · · · · · · · · · · · · · · · · ·	1.00	0.65
		257	601.0	601.8	0.7	56.0	0.34	0.24					1.40	0.98
		258	601.8	602.2	0.5	36.0	0.73	0.33		- 1 ₁			2.60	1.17
		111262	608.5	609.5	1.0	60.0	0.45	0.45					1.00	1.00
		263	609.5	610.4	0.9	54.0	0.06	0.05		:			0.80	0.72
		264	610.4	610.9	0.5	27.0	0.38	0.17	1.53	0.69			1.40	0.63
		111305	649.0	650.5	1.5	30.0		· .	0.48	0.72			0.00	0.00
		306	650.5	651. Z	0.7	13.0			0.20	0.13			0.00	0.00
		307	651.2	652.0	0.8	16.0			0.58	0.46			0.00	0.00
		308	652.0	652.9	0.9	19.0			0.38	0.36			0.00	0.00
		309	652.9	653.4	0.5	10.0			0. 25	0.13			0.00	0.00
:		310	653.4	654.0	0.6	12.0			0.20	0.12			0.00	0.00
		311	654.0	654.5	0.5	10.0	0.03	0.01	0.18	0.09			0.00	0.00
		312	654.5	655.1	0.6	12.0	0.03	0.02	0.35	0.21			0.00	0.00
		111287	615.7	616.1	0.4	40.0	0.27	0.11			· ·	;	0.00	0.00
		288	616.1	616.5	0.4	40.0	0.03	0.01					0.00	0.00
219	555	111289	616.5	617.0	0.5	50.0	0.28	0.14					0.00	0.50
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line	Well	Spl.	Spl. In	terval	Spl.	Spl.	Cu X	Cu	Pb X	РЬ	Zn X	Zn	As s/t	Ag
No.	No.	No.	From	To		Weight		m - X	grade		grade		grade	m g/t
203		108436	537.9	538.4		120.0	0.390							10.00
		108439	570.4	571.1		120.0	0.030		0.160		D. 930			2.60
		494	571.1	571.8		120.0			0.050				· · · · · ·	0.00
		495	571.8	572.3		120.0	0.480	1 2 1			1111	· · · ·	· · · ·	1.00
1		496	572.3	573.0		120.0	5.300		0. 180	-				28.80
		497	\$73.0	573.5		120.0	0.760		1.980				/	4.00
: .		498	573.5	574.2		120.0	2.030		8.350		· · · · · · · · · · · · · · · · · · ·			10.40
		499	574.2	575.0		120.0	5.700		0.030	·····			••••	27.00
		500	\$75.0	575.5		120.0	3.150		D. 200					14.40
		501	\$75.5	576.0		120.0	4.550		1.160					15.20
		506	\$79.0	580.0	1.0	120.0	0.320			1				0.00
		533	602.9	603.7	0.8	120.0	0.430		t					0.00
		543	610.8	611.3	0.5	30.0	0. 500		0. 270	0.140	D. 060	0.030	0.800	0.40
		544	611.3	612.0	0.7	42.0	0.700		D. 390	0.270	0.060	0.040	0.800	0.56
		545	612.0	612.9	0.9	54.0	0.900		D. 490	0.440			0.001	
213	513	108571	637.5	638.2	0.7	120.0			D. 260			21	0.001	the state of the s
		576	630.6	631.1	0.5	60.0	0.510	0.260				-	1.400	0.70
		577	631.1	631.6	0.5	60.0	0.230		.		 		0.001	
		621	690.8	691.5		120.0	1.310	0. 920		0. 160				
		615	692.7	693.2		120.0	0.230	·	þ. 180					
		616	<u>693, 2</u>	694.0		120.0	0.020							
213	513	617	694.0	694.5	0.5	120.0	0.250		· · · · · · · · · · · · · · · · · · ·		· · · · · · · · · · · · · · · · · · ·			
		· · · · · · · · · · · · · · · · · · ·												
			[
157		108754				120.0	0.000		D. 300			0.300		
157		108755			0.50	30.0	0.120				0.000		0.000	0.000
157			644.15		0.50	30.0	0.090				0.000		0.000	0.000
157			644.65		1.05	63.0	0.100			0.000		0.000	0.000	0.000
157				646.60	0.90	90.0	0.320				D. 000	0.000	0.000	0.000
157 157	1			647.20	0.60 0.50	60.0 120.0	0.310 0.370	0.000	D. 640			0.000	0.000	0.000
205			570.50	647.70		120.0						0.000	0.000	0.000
203			571.20			120.0	0.280							0.000
205			571.70			120.0	0.200				p. 000 p. 000	0.000	0.000	0.000
205				572.70		120.0						0.000	0.000	0.000
205			672.70			120.0	0.860				b. 000		0.000	0.000
205		108830	573 20	573 70	0.50	120.0	0.650						0.000	0.000
205		108831			0.60	48.0	2.020	1.210	0 140	0 080	0 000	0.000	0.000	0.000
205		108832			0.90		2.990						0.000	0.000
201		108975			0.50		0.400						0.000	0.000
201		108976			0.50	60.0	0.060						0.000	0.000
201		108978			0.55	22.0	2.270						0.000	0.000
201		108978			0.55	22.0	1.600						0.000	0.000
201			581.20		0.50	20.0	4.350				D. 000		0.000	0.000
201		108980			0.50	20.0	2.800						0.000	0.000
201	521	108981	582.20	582.70	0.50	20.0	3.950						0.000	0.000
201	521	108982	582.70	583.25	0.55	22.0	1.480	0.810	D. 000	0.000	D. 000	0.000	0.000	0.000
193		109051			0.70	70.0	0.930						0.000	0.000
193		109052			0.80	80.0	0.900						0.000	0.000
193		109053			0.80	40.0	0.950						Ò. 000	0.000
193	525	109054	604.60	605.20	0.60	30.0	4.500						0.000	0.000
193		109055			0.70	35.0	0.990		D. 000			0.000	0.000	0.000
193		109056			0.50	25.0	0.770		D. 000			0.000	0.000	0.000
193	525	109057	506.40	606.90	0.50	20.0	1.250	0.630	D. 400	0. 200	D. 770	0. 390	0.000	0.000
193		109058			0.50	20.0	1.270	0.640	D, 310	0.160	D. 950	0. 480	0.000	0.000
193		109059			0.60	24.0	0.100	0.060	D. 890	0. 530	p. 110	0.070	0.000	0.000
193				608.70			3.350						0.000	0.000
193		300001	100 7A	200 20	01 61	1 31 0	0.400	h 240	h 200	h 120	h 000	0 000	0.000	0.000

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- 1-	Well	Spl.	Spl. In	1	Spl.	Spl.	Cu X	Cu		Pb	Zn X	Zn	Ag g/1	Ag
<u>No.</u>	No.	No.	Fron	To		Veight	grade	n•%	grade		grade	m•X	grade	a-g/
193		109062		609.90	0.60	60.0	3.050	1.830	0.000	0,000	D. 000	0.000	0.000	0.00
193	11111111111		609.90		0.60	60.0		2.050	D. 000	0.000	D. 000	0.000	0.000	0.00
193			610.50		0.60	120.0	0.250	0.000	b. 000	0.000	b. 000	0.000	0.000	0.00
193			513.30		0.50	120.0	0. 270	0.000	D. 000	0.000	D. 000	0.000	0.000	0.00
193			613.80	614.80	1.00	120.0	0.060	D. 000	D. 000	0.000	D. 000	0.000	0.000	0.00
193	525	109108	614.80	615, 50	0.70	120.0	0. 200	D. 000	b. 000		D. 000		0.000	0.00
193	525	109109	515.50	616.50	1.00	50.0	0.080	0.080	D. 000		D. 000		0.000	0.00
193	525	109110	616.50	617.40	0.90	45.0				0.000		0.000	0.000	0.00
193	525	109111	517.40	617.90	0.50	25.0		0.030		0.000		0.000	0.000	0.00
193	525	109112	617.90	618.40	0.50	25.0				•••••		0.000	0.000	0.00
193	525	109113	518.40	619.05	0.65	120.0		0.000				0.000	0.000	0.00
193	525	109114	519.05	619.60	0.55	16.5			*********			0.000	0.000	0.00
193			619.60		0.90	27.0	0.030					0.000	0.000	0.00
193		109116		621. 50	1.00	30.0	0.001					0.000	0.000	0.00
193				622.00	0.50	15.0	0.110		b. 000		D. 000		0.000	0.00
193				622. 55	0.55	16.5		D. 060				0.000	0.000	
193		109119	1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.	623.05	0.50	15.0						D. 000		0.00
193		109120		623. 55	0.50	60.0				0.000		0.000 0.000	0.000	0.00
193				624.05	0.50	60.0						0.000		0.00
201		109154		586.70		120.0				0.000			0.000	0.00
201		109155		587.30	0.60	48.0	1. 580					0.000	0.000	0.00
201				587.80	0.50	40.0	1. 430					D. 000	0.000	0.00
201				588.40	0.60	48.0						0.000	0.000	0.00
201		109250		737.70	********	120.0					*********	0.000	0.000	0.00
201				738.50	0.80	48.0	***********). 000). 430				0.000	0.000	0.00
201				39.20	0.70	40.0). 000	0.000	0.000
201			739.20		0.75). 740 570		0.000	r). 000	0.000	0.00
205			614. SÓ (0.50	45.0). 570). 000	0.000	0.000
205				515.50	0.50	15.0						000	0.000	0.006
205			18 million - Carlos Parto - Carlos - C	516.40	0.90	15.0). 000	0.000	0.000
205				517. 20	0.80	27.0). 000	0.000	0.000
205				11. 20		24.0). 000	0.000	0.000
205				18.60	0.50	15.0		0.660			000		0.000	0.000
					0.95	28.5	2. 920	2. 170		0.000	000 0		0.000	0.00(
0				73.60		20.0		000		D. 000		000	0.700	0.000
0			573.60		0.50	60.0		020		<u>), 010</u>		000	0.000	0.000
0			574.10 5		0.50	60.0	0.020			0.040			0.000	0.000
0	000	00922	574.60 5	10.10	0.50	10.0	0.400						1.100	0.550
			575.10 5			14.0	1.020						3.600	2. 52(
0			575.80 5				0.880). 000			4.300	3.010
			576.50 5		0.50		0.410 0) 000 p), 000	0.000 0	. 000	1.900	0.950
	522 1	00000	77.00 5	17.70			0.290 0). 000			1.000	Ò. 70(
			577.70 \$				0.050 0						0.001	0.000
			78.40 \$				0.750 0				000 b		3.200	2.880
			79.30 5				0.190 0						0.700	0.630
			80. 20 5			10.0	0.320 0				.000 0	.000	1.400	0.700
			80.70 5				0. 270 0		000 0		. 000 b	.000	0.800	0.400
			81.20 5				0. 530 0		. 000 0		. 000 p	.000	1.400	0.700
			33.60 5				0.220 0				. 000 0		1.000	0.000
			57. 55 5				1. 120 p	. 000 þ	. 000 0	. 000 p	. 000 0		1.309	0.000
			71. 50 5				0. 540 0	. 540 þ	. 000 0	. 000 b		. 000	1.200	1.200
			72.50 5		0.50		0. 120 0					000	0.001	0.000
09	533 h	09590 5	70.00 5	73.70			0. 220 p					000	0.700	0.490
			73.70 5				4. 420 4			.000 b		********		4. 500
			74. 70 5				0.090 D						0. 900	0.450
			75.20 5				0.060 0						0.001	0.450
09	533 1	09594	75.70 \$.000 0			
			76.20 5				1.450 0						0.001	0.000
		09596 5			0.50	15.0	V	• • • • •		.000 p	. vvv p.		3.900	1.950

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Line	Vell	Spl.	Spl. Interv	at Spl.	Spl.	Cu X	Cu 🗄	Pb X	Pb	Zn X	Zn	Ag g/t	Ag
No.	No.	No.	From To		Weight	and the second se	n·X	grade	· · · ·	grade	I	grade	n g
209		109597	677. 20 577.		19.5	4.400	2.860	0.000	0.000		0.000	4. 300	2.8
209	533	109598	677.85 578.	65 0.80	120.0	0.390	0.000	D. 000	0,000	Þ. 000	0.000	0.001	0.0
209		109605	<u>582.30 582.</u>		120. 0	0.530	0.000		0.000	þ. 6 00	0.000	1.100	0.5
209	533	109606	682.80 583.		120.0	0.260	p. 000	D. 000	0.000	D. 000	0.000	0.800	0.3
209	533		730.10 730.		120.0	0.330	p. 000		0.000		0.000	0.000	0.0
209	533	0		00 0.00	0.0	**********			0.000		0.000	0.000	0.0
209		109649 109650	726. 90 727. 727. 40 727.		20.0	0.170 0.190	0.400		D. 000 D. 000		0.000 0.000	0.800	0.4
209		109651	727.90 728.	and the second sec	20.0	0. 520	0.260		0.000		0.000	0.700	0.3
209		109652	728.40 729.		24.0	1.720	1.030		0.000		0.000	2.300	1.3
209			729.00 729.		24.0	1.700	1.020		0.000		b. 000	1.800	1.0
209			729.60 730.		20.0		0.610		p. 000		0.000	1.200	0.6
Ô	353		586.60 587.		120.0	0.250	0.000	þ. 200	0.000	þ. 000	0.000	1.200	1.2
0	353		589.70 590.		120.0		0.000		0.000	þ. 210	0.000	1.000	0.50
0	353		590. 20 590.		21.0						0. 460	4.600	3.2
0	353		590, 90 591.		15.0	1.850			0.040		0.000	7.000	3.50
0	553		591.40 <u>591</u> .		15.0				0.180		0.200	0.800	0.4
0	553 553		591.90 592. 592.40 593.		15.0 18.0	0.070	0.040 1.030		0,000 0,130	D. 001 D. 580	0.000 0.340	0.600	0.3
0	553		593.00 593.	·····	15.0		0.410	b. 400	0. 200		0.160	5.300	3.1
Ŏ	553		593.50 594.		30.0				0.630		0.000	5. 600	5. 6
0	553		594. 50 595.		15.0		0.120		0.880		0.000	1.000	0.5
0	553		595.00 595.		15,0				0. 220		0.000	1.000	0.50
0	553	16707	595.50 596.	50 1.00	120. 0	5.850	0.000	1.300	0.000	0.000	0.000	21. 200	21.20
0	553		596. 50 597.		25.0	1.990	1.000		0.040		0.000	9.400	4.70
0	553		597.00 597.		25.0	1.110	0.560		0.020		0.000	6.800	3.40
0	553		597.50 <u>5</u> 98.		35.0	0.200	0.140				0.090	1.200	0.8
0	553 553		598, 20 599. 599, 20 599.	******	50.0 100.0	0.780 0.340	0.780 0.170				0. 110 D. 000	3.200	3.2
225	454		520.90 521.		15.6						D. 000	1.200 4.100	0.6
225	454		521.50 522.		13.0				0.000		0.000	1.400	0.70
225	454		522.00 522.		13.0		0. 370		0.000		0.000	16.000	8.00
191	509		606.05 607.		55.0						D. 000	6.300	6.9
191			607.15 607.		35.0	0.300						3.700	2.5
191			607.85 808.		50.0	0.240						0.250	0.2
191			611.20 611.		120.0	0.360						2.200	1.6
191			620.60 621.		120.0	0.540						8.700	6.90
191			548.75 649.		120.0	0.520						0.900	0.4
<u>191</u> 191			569.70 670. 508.85 609.		120.0 33.0		0.000 0.110				0.000 0.000	17.000 2.200	7.6
191			509,40 609.		24.0						0.000	2.200	0.88
191			609,80 610.		36.0		0.000				0.000	4. 300	2.58
191			610.40 611.		48,0	0.030					0.000	1.800	1.4
207			585.20 586.		60,0	0.800		D. 000			0.000	4. 600	2. 3(
207	518		586.70 587.	20 0.50	60.0	1.340	0.670		0.000	D. 000	0.000	4.600	2. 30
207			587.20 587		20.0	0.290					0.000	1.500	0.75
207			587.70 588.		20.0	0.340					0.000	0. 500	0. 2
207			588.20 589.		32.0	0.230					0.000	0.001	0.00
207			589.00 589.		20.0	0.650		b. 000			0.000	1.200	0.60
207 207			589,50 590. 590,00 590.		20.0 36.0	0.030		D.000			0.000	0.001	0.00
207			590, 90 590. 590, 90 591.		30.0			p. 000 p. 000			0.000 0.000	0.001 0.700	0.00
207			591, 70 592.		28.0				0.000		0.000	0. 700	0.00
207			592.40 593.		20.0	0.260						0.001	0.00
207			459. 30 594.		40.0						0.000	0.001	0.00
207			454.00 594.		20.0			D. 000			0.000	0.001	0.30
207			594. 50 595.		24.0		0.160				0.000	0.500	0.30

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	No. 205 205 209 209 209 209 209 209 209 209 209 209	529 525 535 535 535 535 535 535 535 535 535	109473 109474 109475 109476 109477 109478 109479 109480 109509 109510 109511	From 511. 70 512. 50 513. 60 558. 80 559. 20 559. 90 561. 00 561. 60 561. 60 562. 20 562. 70 563. 20	terval To 612, 50 613, 60 614, 50 559, 20 559, 20 560, 50 561, 60 561, 60 562, 20 662, 70 563, 20	19 	Sp1. Weight 120, 0 88, 0 72, 0 35, 0 35, 0 35, 0 30, 0 25, 0 30, 0	0.080 0.020 0.100 0.250 0.390 0.580 0.110	Cu m·% 0.020 0.090 0.180 0.270 0.350	Pb % grade 0. 250 0. 000 0. 000 0. 090 0. 050	Pb m•% 0.060 0.040		Zn m•X 0. 110 0. 040	Ag g/t grade 0.001 0.000 0.000 0.500 0.800	Ag m·g/ 0.00 0.00 0.35 0.55
	205 209 209 209 209 209 209 209 209 209 209	529 535 535 535 535 535 535 535 535 535 53	109449 109450 109473 109475 109475 109476 109476 109478 109478 109480 109509 109510	b12.50 b13.60 b58.80 b59.20 b59.90 b61.00 b61.60 b62.20 b62.30 b63.20	613.60 614.50 559.20 559.90 560.50 561.00 561.60 562.20 662.70 563.20	0.80 1.10 0.90 0.70 0.60 0.50 0.60 0.60	120.0 88.0 72.0 35.0 35.0 30.0 25.0 30.0	0.080 0.020 0.100 0.250 0.390 0.580 0.110	0.090 0.180 0.270	0. 250 0. 000 0. 000 0. 090 0. 050	0. 060	D. 150	0. 110	0.001 0.000 0.000 0.500	0.00 0.00 0.35
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	205 209 209 209 209 209 209 209 209 209 209	529 535 535 535 535 535 535 535 535 535 53	109450 109473 109474 109475 109476 109476 109478 109478 109479 109480 109509 109510	b13.60 b58.80 b59.20 b59.90 b60.50 b61.00 b61.60 b62.20 b62.70 b63.20	614.50 559.20 559.90 560.50 561.00 561.60 562.20 662.70 563.20	0.90 0.70 0.70 0.60 0.50 0.60 0.60	72.0 35.0 35.0 30.0 25.0 30.0	0.100 0.250 0.390 0.580 0.110	0.090 0.180 0.270	D. 000 D. 090 D. 050				0,000 0,500	0.00
	209 209 209 209 209 209 209 209 209 209	535 535 535 535 535 535 535 535 535 535	109473 109474 109475 109476 109477 109478 109479 109480 109509 109510 109511	558.80 559.20 559.90 560.50 561.00 561.60 562.20 562.70 563.20	559,20 559,90 560,50 561,60 561,60 562,20 662,70 563,20	0.70 0.70 0.60 0.50 0.60 0.60	35.0 35.0 30.0 25.0 30.0	0.250 0.390 0.580 0.110	0.180 0.270	D. 090 D. 050				0.500	0.35
	209 209 209 209 209 209 209 209 209 209	\$35 535 535 535 535 535 535 535 535 535	109475 109476 109477 109478 109479 109480 109509 109510 109511	559.20 559.90 560.50 561.00 561.60 562.20 562.70 563.20	559.90 560.50 561.00 561.60 562.20 662.70 563.20	0.70 0.60 0.50 0.60 0.60	35.0 30.0 25.0 30.0	0, 390 0, 580 0, 110	0. 270	0.050					
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	209 209 209 209 209 209 209 209 209 209	535 535 535 535 535 535 535 535	109478 109479 109480 109509 109510 109511	561.60 562.20 562.70 563.20	562, 20 662, 70 563, 20	0.60			0.060		0.000	D. 000	0.000	2.100	1.05
	209 209 209 209 209 209 209 209 209 209	535 535 535 535 535 535 535	109479 109480 109509 109510 109511	562.20 562.70 563.20	662.70 563.20			2.550	1. 530	D. 000	0.000	D. 000	0.000	1.000	0.60
	209 209 209 209 209 209 209 209 209 209	535 535 535 535 535 535 535	109480 109509 109510 109511	562. 70 563. 20	563.20		30.0	0.390	0.230		0.000	D. 000	0.000	0.001	0.00
	209 209 209 209 209 209 209 209 209 209	535 535 535 535 535 535	109509 109510 109511	563. 20		0.50	25.0 25.0	0.130	0.070		0.000		0.000	0.001	0.00
	209 209 209 209 209 209 209 209 209	535 535 535 535	109510 109511		563.75		120.0	6.700	0.200 3.690	D. 620 D. 000	D. 310 D. 000		0.000 0.000	2.200 26.000	1.10 14.30
	209 209 209 209 209 209	535 535		F * * * * * * *	564.45	0.70	21.0	0.460	0. 320	D. 000	5.000		0.000	1. 100	0.77
	209 209 209 209 209	535	100510		564.95	0.50	15.0	2.480	1.240	D. 050 (). 030		0.000	10.000	5.00
	209 209 209			564.95		0.55	16.5	1.270	0. 700). 010		0.000	4.800	2.64
	209 209	999 B		65.50	**********	0.50	15.0	0.420	0.210		0.050	p. 000 k	000	0.500	0.25
	209				566.80	0.80	24.0		0.060). 190	D. 000 (D. 000	0.500	0.40
		12171711			567.45 567.95	0.65	19.5 15.0		0.060 0.060). 400). 000	0.500	0.32
	0.44				568.80	0.85	68.0		4.820). 070). 110). 000). 000	0.800 24.300	0.40
	209	535 1			69.40	0.60	48.0		3. 230). 010	0.010	0.000). 000		20.660
					69. 90	0.50	40. 0	3.910	1.960). 190	. 100	0.000 0	000	6. 200	3. 100
					70.40		120.0		D. 880	. 660	. 830	0.000	000	15.200	7.600
					70.90	0.50	30.0		D. 019	. 850	930). 000 0	000.	2.000	1.000
					71.50	0.60	36.0		0.100). 040 (. 020).000 (0		3. 500	2.100
					72.60	0.60	36.0 30.0). <u>130</u>	0.030 0	. 020). 000 0		0.500	0.300
					73.10	0.50	30.0	0. 270), 190), 140	.020 0 .050 0	. 510). 000 0). 000 0	. 000	0.500	0.250
1.				573.10 5		0.90	54.0). 750	. 000 0			. 000	0.500 2.800	0.250 2.520
			09617	598.80 5	99.30	0.50	60.0). 130		. 230	. 000 b	. 000	0.500	0. 250
ā.				599.30 5			60.0	0.240). 120	. 070 0	. 040		. 000	0.001	0.000
				594.40 6		0.50 1	20.0	0.410). 210	. 140 0	. 070	000 D	. 000	3.500	1.750
	209	537 1	10153	554.90 5 555.50 5			12.0	9.760	5.860 p	. 230 0				37.000	
		537 1	10155 5	56. 30 5				0.020		.001 0		.000 0			0.000
	209	537 1	10156	56.90 5	57.50			0.020 0.960					.000		0.000
	209	537 1	10157	57. 50 5				3. 980	390				.000 .000		78.600 20.880
	209	537 1	10158 5	58.10 5	59.00			0.130					.000		0.810
-1 -	209	537 1	10159 6	5 9.0 0 5	59.90			0.010	. 010 p				.000		0.000
· · ·	209	031 U 597 K	10160 6	59.90 5				0.010				.000 0			0.000
		537 1	10101 p	60.40 S	61 60			1.790						51.000 2	
		537 1	10153 6	54.90 5						. 000 0				73.000	
		537 1	10156 5	56.90 5	57.50			0.960 6			140 D 130 D			37.000 31.200 7	
	209	537 1	10157 5	57.50 5	58.10				. 390 D		560 b				0. 880
	209	537 1	10170 5	66. 50 5	67.00				. 920 D		000 0			40.000 7	
	209	37 1	<u>10171 5</u>	67.00 5				1.910 1	.530 D		000 þ				3.840
·	209	37 1	10172 6	67.80 5				0.070 0					000		1.120
н. 	209 5 209 5	37 11	10177 P	68.50 50 69.00 50					. 090 þ.				000		0.950
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		37 1	0176	70.40 5				2.090 1 0.750 0							1.060
	209 5	37 1	0170 5	56.50 5:				5.840 0					000		7.560
	209 5	37 11	0174 5	69.00 50	59.70 (4.230 1	. 590 b	000 h	000 h				0.000
	209 5	37 11	0177 5	71.30 57	72.10 (0.80	40.0	0. 140 þ	. 110 þ.	080 0.	080 0.	000 0.			1.680
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217 541 109808 541.10 541.80 0.70 70.0 0.510 0.360 0.000 0.	00 1. 120 00 1. 320 00 0. 960 00 0. 450 00 0. 250 00 0. 300 00 0. 300 00 6. 750 00 1. 920 00 1. 250
217 541 109822 550. 90 551. 50 0. 60 120. 0 0. 280 0. 170 0.000	00 1,320 00 0,960 00 0,450 00 0,250 00 0,300 00 4,450 00 6,750 00 1,920 00 1,250
217 541 109832 557.60 558.20 0.60 120.0 0.420 0.250 0.000 0.000 0.000 0.000 1.6 215 542 110470 537.50 538.00 0.50 25.0 0.670 0.340 0.060 0.030 0.000 0.000 0.000 0.000 0.000 0.50 25.0 0.670 0.340 0.050 0.030 0.000 0.000 0.000 0.55 215 542 110471 538.00 538.50 0.50 25.0 0.090 0.050 0.030 0.020 0.000 0.050 0.55 215 542 110472 538.50 539.00 0.50 25.0 0.130 0.070 0.050 0.030 0.110 0.660 0.6 215 542 110472 538.50 539.50 0.50 25.0 0.800 0.400 0.270 0.140 0.180 0.090 8.9 215 542 110474 539.50 540.40 0.450 1.260 1.130 0.000 0.000 0.000 7.5	00 0.960 00 0.450 00 0.250 00 0.300 00 4.450 00 6.750 00 1.920 00 1.250
215 542 110470 537.50 538.00 0.50 25.0 0.670 0.340 0.060 0.030 0.000 0.000 0.9 215 542 110471 538.00 538.50 0.50 25.0 0.090 0.050 0.030 0.020 0.000 0.000 0.5 215 542 110472 538.50 539.00 0.50 25.0 0.130 0.070 0.050 0.030 0.140 0.180 0.660 0.6 215 542 110472 538.50 539.50 0.50 25.0 0.130 0.070 0.050 0.140 0.180 0.090 8.9 215 542 110474 539.50 540.40 0.90 45.0 1.260 1.130 0.000 0.000 0.000 7.5 215 542 110474 539.50 540.40 0.60 66.0 0.770 0.460 0.000 0.000 0.000 7.5 215 542 110485 549.40 549.90 0.50 55.0 0.460 0.000 0.	00 0.450 00 0.250 00 0.300 00 4.450 00 6.750 00 1.920 00 1.250
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147 545 110988 559.70 660.55 0.85 60.0 0.350 p.300 p.020 p.570 p.000 p.000 6.4	i i i i i i i i i i i i i i i i i i i
147 545 110989 660. 55 661. 10 0. 55 120. 0 0. 480 p. 260 p. 760 1. 520 p. 000 p. 000 12. 0	the second s
147 545 110990 661. 10 661. 60 0. 50 30. 0 0. 440 p. 220 p. 070 p. 040 p. 000 p. 000 3. 6	
147 545 110992 562. 65 663. 30 0. 65 39. 0 0. 110 p. 070 p. 000 p. 000 p. 000 d. 6	
147 545 110991 561. 60 662. 65 1. 05 63. 0 0. 150 p. 160 p. 000 p. 000 p. 000 1. 0	
147 545 110993 663. 30 663. 75 0. 45 120. 0 6. 750 3. 040 p. 000 p. 000 p. 000 p. 000 28. 0	
215 548 110784 558 50 559 40 0. 30 27. 0 0. 000 p. 000 p. 000 p. 240 p. 220 0. 9	a migra a la sua da di di denda da da di
215 548 110785 559. 40 560. 35 0. 95 28. 5 0. 000 p. 000 p. 150 p. 140 p. 540 p. 510 2. 5	00 2.380
215 548 110786 660. 35 561. 00 0. 65 19. 5 0. 000 p. 000 p. 000 p. 000 p. 000 0. 9	00 0.590
215 548 110787 561.00 561.50 0.50 15.0 0.000 p.000 p.000 p.000 p.000 1.2	
215 548 110788 561. 50 562. 00 0. 50 15. 0 0. 000 0. 000 0. 030 0. 020 0. 130 0. 070 2. 6	
215 548 110789 562.00 562.80 0.80 24.0 0.150 0.120 0.470 0.380 0.330 1.060 6.5	
215 548 110790 562. 80 563. 60 0. 80 24. 0 0. 000 0. 000 0. 200 0. 160 0. 300 0. 240 2. 8	00 2.240
215 548 110795 566. 10 566. 60 0. 50 120. 0 0. 390 p. 200 p. 000 p. 000 p. 000 p. 000 2. 4	
215 548 110796 566. 60 567. 10 0. 50 120. 0 0. 040 0. 020 0. 000 0. 000 0. 000 0. 000 0. 0	
215 548 110797 667. 10 567. 60 0. 50 120. 0 0. 200 p. 100 p. 000 p. 000 p. 000 7. 2	
215 548 110836 505. 50 606. 25 0. 75 37. 5 0. 040 0. 030 0. 200 0. 150 1. 060 0. 800 1. 0	
215 548 110837 506. 25 506. 85 0. 60 30. 0 0. 000 0. 000 0. 090 0. 050 0. 220 0. 130 0. 6	
215 548 110838 606. 85 607. 50 0. 65 32. 5 0. 070 0. 050 0. 070 0. 050 0. 600 0. 390 0. 7	
215 548 110839 507. 50 608. 20 0. 70 35. 0 0. 060 0. 040 0. 000 0. 000 0. 300 0. 210 0. 5	
215 548 110847 513 80 614 30 0.50 20.0 0.560 0.280 0.000 0.000 0.000 1.6	
215 548 110848 514. 30 514. 80 0. 50 20. 0 0. 470 0. 240 0. 070 0. 040 0. 100 0. 050 4. 2	
215 548 110849 514.80 515.60 0.80 32.0 0.410 0.330 0.000 0.000 0.000 0.9	
215 548 110850 515. 60 616. 50 0. 90 36. 0 0. 050 0. 050 0. 000 0. 000 0. 000 0. 000 0. 0	
215 548 110851 516. 50 617. 15 0. 65 26. 0 2. 190 1. 420 0. 260 0. 170 0. 550 0. 360 0. 0	
213 553 111037 648. 70 549. 50 0. 80 120. 0 0. 380 p. 300 p. 250 p. 200 p. 120 p. 100 0. 7	
209 537 110152 554. 20 554. 90 0. 70 120. 0 0. 320 0. 000 0. 000 0. 000 0. 000 0. 000 2. 8	00 0.000
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Line	fell	Spl.	Spl. Interval	Sp1.	Spl.	Ci X	Cu	Pb X	Pb. :	Zn 🕺	Zn	18 8/1	A
No.	No.	No.	Fron To	Leng.	Weight	grade	n X	grade		grade		grade	1
211	223	13473	547. 10 548. 10	1.00	120.0	0.420	0.420	D. 000	0.000	Contraction of the local division of the loc	0.000	1.000	1.0
221	223	13489	558. 40 559. 40	1.00	120.0	0.300	0.300		0.000		0.000	1.700	1.7
211	223	13490	559. 40 560. 40	1.00	120.0	0.400	0.400		0.000		0.000	1.000	1.0
211	223		560. 40 561. 10		120.0	1.490	0.000		0.000		0.000	9.300	6. 5
211	223		561. 10 561. 50		24.0	0.030	0.010		0.000				
211	223	**********	561. 50 562. 00		30.0	0.010	0.010		0.000		0.000	0.001	0.0
211	223		562.00 562.50		30.0	0.001	0.000				0.000	0.001	0.0
211	223		562.50 563.00						0.000	<u>p. 000</u>		0.001	0.0
211	223		Address for the second second second second		30.0	0.001	0.000		0.000		0.000	0.001	0.0
		12100	0.00 0.00		0.0	0.000	0.000		0.000		0.000	0.000	0.0
211	223		563.00 564.00		120.0	0. 570	0. 570		0.000		0.000	0.110	0.1
211	223		564.00 564.90		120.0	0.240	0. 220	p. 000	0.000	Þ. 000 i	0.000	0.000	0.1
211	223		637.30 638.70		28.0	0.240	0.340	þ. 000	0.000	þ. 000 í	0.000	0.000	0.0
211	223	13512	638.70 639.80	1.10	22.0	0.350	0.390	D. 000	0.000		0.000	0.000	0.
211	223	13513	539.80 640.90	1.10	22.0	0.070	0.080				0.000	0.000	0.0
211	223	13514	640. 90 642. 00		22.0	0.280		0.000			0.000	1.000	1.
211	223		642.00 643.10		22.0	0.170	0.190	b. 000	D. 000		0.000	0.700	0.
211	223		543.10 644.00		18.0	0.310	0.280		0.000		0.000	0.850	
211	223	0	0.00 0.00		0.0	0.000	0.000		0.000		**********		0.
235	225		175. 10 476. 10		120.0	0. 470	0.470				D. 000	0.000	0.(
235	225		176. 10 176. 60		120.0	1.190	0.600		0. 430		000	0.800	0.1
235	225								D. 150		0.000	7.000	0.0
235					30.0	2.940	2.940		D. 000), 000	13.500	13.
	225		177.60 478.20	0.60	18.0	0.060	0.040				0.000	1.000	0.6
235	225		178.20 478.70	0.50	15.0	0.060	0.030). 000	1.500	0.1
235	225		178. 70 179. 20	0.50	15.0	1.830	0.920		000 0.000). 000	21.000	10. 5
235	225		179. 20 179. 70	0.50	15.0	0.001	0.000	p.000 (0.000	b. 000 k). 000	0.000	0.0
235	225	14247	179. 70 180. 30	0.60	18.0	2.290	1.370	þ. 000 i	000	b. 000 k). 000	24.000	14.4
235	225	0	0.00 0.00	0.00	0.0	0.000	0.000	þ. 000 í	0.000		000	0.000	0.0
235	225	14282	572.00 573.00	1.00	120.0	0.310	0.310	b. 000 k	000	D. 000 C	000	2. 500	0.0
223	226	14341	528.60 529.60	1.00	120.0	1.070		þ. 000 (000.		.000	4.000	0.0
223	226	14342	529. 60 530. 60	1.00	60.0	0.610					. 000	2.000	2.0
223	226	14343	530. 60 531. 60	1.00	60.0	0.940	0.940				. 000	3.000	3.0
223	226	0	0.00 0.00	0.00	0.0	0.000			000		000	0.000	0.0
223	226	14344	531. 60 532. 60	1.00	50.0	0.001			000		. 000	0.000	
223	226		532. 60 534. 00	1.40	70.0	0. 760	1.060). 000				0.0
223	226	0		0.00	0.0	0.000					. 000	4.500	2.3
203	227	14308	573. 30 574. 30	1.00	50.0	0.260		<u>0.000 k</u>		000 p		0.000	0.0
203	221		574. 30 575. 00				0.260					1.500	1.5
				0.70	35.0	0.050	0.040					0.000	0.0
203	227		575.00 575.60	0.60	30.0	0.140	0.080			D. 000 D		0.000	0.0
203	227	0	0.00 0.00	0.00	0.0	0.000). 000 p	. 000	0.000	0.0
203	227		575.00 576.30	0.70	0.0	4.680			070). 000 ()	. 000	60.000	42.0
203	227		76. 30 576. 80	0.50	25.0	7.400	3.700	D. 001 (. 000). 000 þ	. 000	70.000	35.0
203	227		76. 80 577. 30	0.50	25.0	3.920	1.960	þ. 001 þ	. 000). 000 þ	. 000	15.000	22.5
203	227	14404	77. 30 577. 80	0.50	25.0	5.080	2.540			0.000 0			20.0
203	227	0	0.00 0.00	0.00	0.0	0.000		D. 000 D	000) 000 b	000	0.000	0.0
203	227	14405	77. 80 578. 40	0.60	60.0	0.940		D. 001 0	000			11.000	6.6
203	227		78. 40 578. 90	0.50	50.0	1.120		D. 230 D				13.500	6.7
203	227	0	0.00 0.00	0.00	0.0	0.000	0.000			000 0		*************	
203			78.90 579.40	0.50		0.240						0.000	0.0
203			79. 40 579. 90	0.50		0. 180				000 0		4.000	2.0
203	227	14400	79. 90 580. 40								. 000	4.000	2.0
203				0.50		0.230). 000 0			. 000	4.500	2.2
			80. 40 581. 20	0.80		0.230	0.180		. 000		. 000	4.500	3.6
203			81. 20 582. 20	1.00		0.060	0.060				. 000	5.000	5.0
203			82. 20 583. 30	1.10		0.700	0.770				. 000	5.000	5.5
203	227	0	0.00 0.00	0.00	0.0	0.000	0.000				. 000	0.000	0.0
203		14413 5	83. 30 584. 30	1.00		0.140	0.140					1.000	1.0
203			84.30 585.30	1.00		0.001	0.000). 070 h	070 h	. 000 b.		1.000	1.0
203			85. 30 586. 30	1.00			0.060), 100 h	100 h	. 000 h	000	1.000	1.0
	227	0	0.00 0.00	0.00	0.0					No	000		1.0

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No. No. From To To<	: [Line	lell	Spl.	Spl. Interval	Spl.	Spl.	Cu X	Cu	Pb X Pb	Zn % Zn	Ag g/t	Ag
221 2411 2427 34417 388.30 1.00 20.0 1.860 1.860 1.000 2.000 3.000 0.000 3.000 0.000 201 221 14437 566.50 507.00 0.501 20.00 1.660 0.000 0.000 0.000 3.000 1.600 0.000					2								
221 14438 506. 50 5.50 20.0 0.310 0.160 0.000 0		203	227	14416	586. 30 587. 30	1.00	120.0	0. 480	0.480		All and a second second second	00 3.000	0.000
223 227 14437 b6. 30 b7.00 0.300 0.300 0.000 0.	•						120. 0			The second second second second		******	
					2 · · · · · · · · · · · · · · · · · · ·								
191 237 1544 179.67 070.0 0.000 0.0	8											·	
	10.12				analysis and a second								
	2												
191 237 30831 503.60 504 20.40 0.40													
191 237 30835 505 10 120 120 0.000	1				a provide the second				***********			******	
191 237 30834 504.50 60.90 0.030 0.030 0.030 0.030 0.030 0.030 0.030 0.040 0.030 0.030 0.040 0.030 0.040 0.030 0.040 0.030 0.040 0.										Construction of the second s second second s second second sec			
191 237 30835 502.00 0.050 0.000 0.	ż			30834	606.50 607.40	0.90	120.0	0.030	0.030	D. 080 D. 070	D. 620 D. 5	60 3.500	0.000
191 237 30835 609. 60 6. 60 200 0.001 0.000 0.000 0.800 0.700 7.500 0.000 191 237 30835 60.40 61.40 0.801 20.0 0.100 220 0.180 0.800 0.710 7.500 0.000 0.000 191 237 30845 61.40 61.41 51.2 0.001 0.000 0.200 0.100 0.400	4	191					120.0		0.030	0.030 0.020	0. 540 0. 4	30 3.500	
191 237 30838 509. 60 610. 40 0.30 120. 0 0.100 0.200 180 0.800 0.710 7.500 0.000 191 237 30839 510. 40 511.45 1.05 120. 0 0.800 0.200 120 1.510 9.000 0.000 0.000 191 237 30841 512. 20 1.350 0.660 0.300 0.200 1.000 0.600 0.000 1.000 0.000	•												
191 237 30839 \$10.0 10.1 130.0 0.000 0.200 0.000 0.200 0.000 0.200 0.00													
191 237 30840 511.4 612.30 0.85 120.0 0.000 0.200 0.3													
191 237 30841 312. 30 612. 30 1.350 0.680 0.930 0.630 0.310 0.160 42. 500 21. 250 203 239 15302 31. 30 581. 30 0.50 0.000 <td< td=""><td>2</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></td<>	2												
203 233 15302 81.30 85.0 92.0 0.050 0.050 0.000												ببتينية والمتعادية والمستوادية والمستواد	
203 233 15302 581.30 581.80 60.50 60.0 0.000 0.	1				the state of the s								
203 239 15303 81.80 52.30 0 50 6.00 0.000 1.400 0.700 203 239 15305 83.30 0.50 25.0 0.210 0.400 0.000 <t< td=""><td></td><td></td><td></td><td>* * - * * * * *</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>*********************</td><td>- TALE</td></t<>				* * - * * * * *								*********************	- TALE
203 233 15304 82.30 552.80 0.50 120.0 1.310 0.660 0.000 0.000 0.000 1.400 0.700 203 239 15305 83.30 68.30 0.50 25.0 0.200 0.000	•			15303	581.80 582.30	0.50	60.0	0.100	0.050	0.000 0.000		00 0.001	0.000
203 239 15305 532.80 533.30 0.50 25.0 0.280 0.140 0.000 0.0		203					0.0		0.000			00 0.000	0.000
203 239 15306 533.30 583.40 0.60 30.0 0.340 0.200 0.0													
203 239 15307 583.90 584.40 0.50 25.0 0.110 0.050 0.000 0.0												e de la seconda de la secon	
203 239 15308 584.40 584.90 0.50 25.0 0.270 0.140 0.000 0.0												• • • • • • • • • • • • • • • • • • •	
203 239 0 0.00 0.00 0.000 <td></td> <td></td> <td></td> <td></td> <td>• • • • • • • • • • • • • • • • • • •</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>					• • • • • • • • • • • • • • • • • • •								
203 239 15310 585.40 586.00 0.60 18.0 0.890 0.530 0.000 0.0													
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$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$				15312	586.50 587.00			0.310				00 1.000	0.500
203 239 315 588 00 588 50 15 0 0.160 0.080 0.000 <th< td=""><td>÷</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>, an against a start and a start and a start a</td><td></td><td>534251 C. 5444444</td><td></td></th<>	÷									, an against a start and a start and a start a		534251 C. 5444444	
203 239 316 588. 50 589. 00 0.50 15. 0 0.420 0.210 0.000 0.000 0.000 0.000 1.400 0.700 203 239 317 589. 00 589. 50 0.50 15. 0 0.350 0.180 0.000 <td></td> <td>a de la companya de l</td> <td></td>												a de la companya de l	
203 239 317 \$89.00 \$89.50 0.50 15.0 0.350 0.180 0.000	1									وحميمهما متقلته ومتا		بتعتقر كتعا	
203 239 0 0.00 0.00 0.00 0.000	-										an 🛛 🖬 🗤 🗤 🗤 🖓 🖓 🖓 🖓 🖓		
203 241 15264 \$86.90 \$87.40 0.50 120.0 0.580 0.290 0.900 0.500 0.000 1.500 0.000 203 241 265 \$87.40 \$87.90 0.50 60.0 0.001 0.000	:												
203 241 265 537.40 587.90 0.50 60.0 0.001 0.000													
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203 241 15267 588.40 588.90 0.50 120.0 0.340 0.170 0.001 0.000 0.000 1.000 0.500 203 241 268 588.90 589.60 0.70 120.0 2.030 1.420 0.000 0.000 0.000 0.000 2.000 4.900 203 241 269 589.60 590.40 0.80 120.0 0.740 0.000 0.000 0.000 0.000 2.000	÷												
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Line No.	No.	Spl.	Spl. Interv		Spl.	Cu X	Cu	РБ 🕺	РЪ	Zn X	Zn	Ag g/1	A
197	254	No. 30015	From To 599. 70 600.	Leng. 25 0.55	Veight		and the second division of the second divisio	grade	successively realized and	grade		grade	<u><u>n</u>•8</u>
197	254	0	0.00 0.			6.360	3,500		0.000		0.000	10.500	5.7
205	255	30059	594. 30 594.			0.000	0.000		0.000	D. 000	0.000	0.000	0.0
205	258		594. 80 595.			1.170	0.590		0.000	D. 000	0.000	6.500	0.0
205	256					0.001	0.000		0.000	<u>0.000</u>	0.000	0.000	0.0
205	256	0	595.30 595. 0.00 0.			0.490	0.250	D. 000	0.000	D. 000	0.000	5.000	2.5
203	256		595.80 596.			0.000	0.000		0.000	D. 000	0.000	0.000	0.0
205	256		596. 30 596.			0.001	0.000		0.000	D. 000	0.000	0.000	0.0
205	256		596, 80 597.			0.080	0.040		0.000	<u>0.000</u>	D. 000	0.000	0.0
205	256	30065	597.80 598.			0.001	0.000		0.000		0.000	0.000	0.0
205	256		598. 40 598.			0.100	0.050	b. 000	0.000		0.000	0.000	0.0
205	256	0	0.00 0.4			0.080	0.040	D. 000	0.000	D. 000	0.000	0.000	0.0
205	256		598.90 599.		0.0	0.000	0.000	D. 000	D. 000	D. 000	0.000	0.000	0.0
205	256		599. 40 599.		25.0	0.560	0.280	D. 000	0.000	E	0.000	1.800	0.
205	256		599.90 600.		25.0	0.910	0.460	D. 000	0.000		0.000	2.100	1.0
205	256		500.40 600.		25.0	0.530 0.640	0.270		0.000	C	0.000	1.500	0.1
205	256		500. 90 601. (25.0		0.320		0.000		0.000	2.400	1.
205	256	0.011	0.00 0.0		35.0	0.550	0.390		0.000		0.000	1.300	0.
195	258		522.60 623.2		52.0	0.360	0.000	D. 000 D. 000	0.000		0.000	0.000	0.0
195	258		623. 25 623. 8		44.0	0.260	0. 230		0.000 0.000	D. 000	0.000	1.000	0.6
195	258		623.80 624.4		48.0	0.310	0.190		0.000 0.000	0.000	0.000	0.001	0.0
195	258	0	0.00 0.0		0.0	0.000	0.000		0.000		0.000	0.001	0.0
195	258		524. 40 624. 9		120.0	1.000	0.500). 080		000.0	0.000	0.0
195	258		624. 90 625.		120.0	0. 420	0.250). 130			2.000	0.0
195	258		625. 50 625. 9		120.0	2. 420	0. 970). 050), 170), 000	2.500	0.0
195	258		625. 90 626. 9		120.0	0. 130	0.080). 000). 000	10.000	0.0
195	258	************	526. 50 627. 3		120.0	0. 160	0.130	D. 540). 430	D. 000		3.300	0.0
195	258		527. 30 628. 0		120.0	1. 210	0.850	b. 000 k	000	D. 000). 000). 000	2.500 10.500	0.0
195	266		512.00 612.6		120.0	0.370	0.220	D. 320). 190	D. 210). 130	2.000	0.0
195	265		612.60 613.2		120.0	0.660	0.400	p. 100	0.060). 000	1. 500	0.0
195	266		613.20 613.8		30.0	2.040	1.220	0.000	000	5. 000 g		6.000	3.6
195	266		613.80 614.3		25.0	0.300	0.150	0.000 k	0.000		000	0.001	0.0
195	266		514. 30 614. 8		25.0	1.140	0.570	0.000 b	. 000		000	2.000	1.0
195	265	228	514.80 615.3		25.0	1.630		0.000			0.000	3.000	1.5
195	266	229	515.30 615.9	0 0.60	30.0	1.870	1.120	D. 000 (000). 000 h		5.000	3.0
195	266	0	0.00 0.0		0.0	0.000	0.000			000		0.000	0.0
195	266	30230	515.90 616.6	0 0.70	35.0	4.560	3.190). 000 k			12.6
195	266		516.60 617.1	0 0.50	25.0	0.500). 000 (4.000	2.0
195	266	30232	517.10 617.8	0 0.70	35.0	2.210	1.550). 000 (10.8
195	266	30233	517.80 618.8		50.0	5.280	5. 280	0.000					23.5
195	266	0	0.00 0.0		0.0	0.000	0.000				. 000	0.000	0.0
195	266		18.80 619.6			0.001	0.000). 000 jo	. 000		.000	0.000	0.0
195	266		5 19. 60 620, 6		50.0	0.000	0.000). 000 jo	. 000	0.000	.000	0.000	0.0
195	266		20. 60 621. 3			0.001	0.000	000 0	. 000). 000 b	.000	0.000	0.0
195	266	0	0.00 0.0			0.000			.000	. 000 0	. 000	0.000	0.0
195	266		21. 35 621. 8			0. 730			.000). 000 ja	. 000	2.500	0.0
195	266		21. 85 622. 6			0.310). 000 D	. 000	2.500	0.0
193	268	30261	04. 45 605. 7			0.880				000 jo	. 000	5.800	0.0
193	268	30262				0.160			. 250	. 000 p	. 000	1.500	0.0
193		30263) 1.00		1.250			. 460	. 000 p	. 000	4.500	0.0
			07.30 607.9			2.340	1.400			. 000 þ		7.000	4.2
			07.90 608.9			5.160					000	3.500 1	13. 5
			08.90 610.0			3.440					. 000		9.0
			10.00 610.7			2.780						9.000	6.7
	268	30268 5	10, 75 611, 7			5.460	5.190		. 000 þ				7.51
	268	30269 6	11.70 612.20	0.50		1.450	0.730 0	. 000 p	.000 þ	.000 b	000		0.0
	268	30270 6	12.20 612.7		30.0	0. 320	0.160 b	. 000 0	. 000 b	. 000 b	.000		1.0
193	268	30271 6	12. 70 613. 40	E 0.70	42.0	o soo l	0 350 h	000 0	000 h	000 0	000		2.1

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4	line	iell	Spl.	Spl. Interval	Spl.	Spl.	Cu %	Cu	Pb % I	Pb	Zn %	Zn	lg g/t	Ag
t the second	No.	No.	No.	Fron To	leng.	Weight	grade	n•%	grade r	n•%	gråde	<u>n•%</u>	grade	m·g/t
14.4	193	268	30272	613.40 614.30	0.90	54.0	1.010				F	0.000	7.000	6.300
•	193	268	0	0.00 0.00	0.00	0.0	0.000			000	F	0.000	0.000	0.000
•	209	269		585.80 586.30	0.50	60.0	0.760					0.000	0.800	0.400
1	209 209	269 269	30246 0	586.30 586.80 0.00 0.00	0.50	60.0 0.0	0.340			000		0.000 0.000	0.500 0.000	0.250
	209	269	0	0.00 0.00	0.00	0.0	0.000					0.000	0.000	0.000
er S	209	269		586. 80 587. 30	0.50	120.0	1,410					0.000	0.000	0.000
	195	271		591. 70 592. 70	1.00	120.0	0.350					0.000	2.000	2.000
1.12 million	195	271	30361	592. 70 593. 60	0.90	120.0	0.880					0.000	0.000	0.000
4	195	271		593. 60 594. 20	0.60	36.0	0.070			000	0.000	0.000	0.000	0.000
	195	271		594.20 594.70	0.50	30.0	0.060					0.000	0.000	0.000
e S	195	271		594. 70 595. 20	0.50	30.0	0.070	***********				0.000	0.000	0.000
s" N	195	271		595.20 595.70	0.50	30.0	0.090					0.070	2.000	1.000
	195 195	271 271	0 30366	0.00 0.00 595.70 596.30	0.00	0.0 120.0	0.000		a service and the service of the ser	000		D. 000 D. 230	0.000 1.500	0.000
	195	271		596. 30 596. 70		120.0	0.090					0.060	2.500	0.000
*	195	271		596. 70 597. 30		120.0	0. 280					0. 370	2.500	0.000
	195	271		597. 30 597. 80		120.0	0.440			1.21.91.81.81.61		0.160	3.000	0.000
•	195	271	30370	597.80 598.70	0.90	120.0	0.140					0.440	2.000	0.000
-	195	271		598. 70 599, 20	0.50	120.0	0.180	0.090	D. 000 D.	000	0. 430	0. 220	2.000	0.000
	195	271		599.20 599.70	0.50	60.0	0.640	0.320				0.000	3.000	1.500
1	195	271		599.70 600.20	0.50	60.0	0.570					0.000	2.000	1.000
	195 195	271 271	0 30374	0.00 0.00 500.20 600.70	0.00	0.0	0.000			********		0.000	0.000 1.500	0.000
	195	271		609.40 609.90		120.0 120.0	0.300			*********		D. 000 D. 000	1.000	0.000
е. 1	195	271		609.90 610.40		120.0	0.800			000	D. 000	0.000	1.000	0.000
:	195	271		646.30 647.20		120.0	1.730	0.000		000	D. 000	0.000	11.000	0.000
	195	271		647.20 647.70		120.0	3.740	1.870			0.000	**********	22,000	0.000
	197	280		592, 80 593, 30		120.0	0.340	0.000				0.000	0.660	0.000
	197	280		593.30 593.80		120.0	0.890					0.000	4. 100	0.000
1	197	280		593.80 594.30		120.0	0.420					0.000	3.400	0.000
2	197 197	280 280		594.30 594.80 594.80 595.40		120.0 120.0	0.070	0.000		*******		D. 000 D. 000	1.600 2.550	0.000
	197	280		595. 40 596.00		120.0	0.310	0.000		******	1.350	0.000	6.000	0.000
i i	197	280	30502			120.0	0.090	0.000			D. 530	0.000	2.650	0.000
-	197	280		596. 40 596. 80		120.0	0.160				11112111231	0.000	2.650	0.000
3 	206	281		594.20 594.90		120.0	0.000					0.000	0.510	0.000
2 1	206	281		594. 90 595. 40			0. 420		D. 250 D.				0.500	0.000
	206	281		595.40 595.95	0.55		0.320		p. 000 p.				0.500	0.280
	206 205	281 281		595.95 596.50 596.50 597.10	0.55	27.5	0.480		<u>). 000 ().</u>				0.900	0.490
i.	206	281		597. 10 597. 10	0.60	30.0 30.0	0.130		D. 000 D. D. 000 D.			0.000 0.000	0.001	0.001
	206	281	0	0.00 0.00	0.00	0.0	0.000	0.000	p. 000 p.		D. 000		0.000	0.000
	206	281		597. 70 598. 20	0.50	120.0	2.960		b. 000 b.			0.000	9.800	0.000
4 2 -	206	281		598.20 598.70	0.50	10.0	0.250		D. 000 D.		0.000		1.200	0.600
r F	206	281		598.70 599.70	1.00	20.0	0.430		0.000 0.		0.000		1.000	1.000
	206	281		599.70 600,70	1,00	20.0	0.050		D. 000 D.				0.001	0.001
1	206	281		600.70 601.70	1.00	20.0	0, 140		0.000 0.		000		0.001	0.001
1.41.44	206 206	281	30015	601.70 602.25	0.55	11.0	0.400		000 D.		000	0.000	1.300	0.700
	206	281 281		502.25 603.20 503.20 604.00	0.95	19.0 16.0	0.180 0.380	0.110	000 C.	000		0.000	0.001 0.800	0.001
	206	281	0	0.00 0.00	0.00	0.0	0.000	0.000	0.000 0. 0.000 0.	000		0.000 0.000	0.000	0.000
s.	192	284		613.40 614.10	0.70	35.0	0.060		D. 001 D.		D. 000		0. 500	0.350
1.1	192	284		614.10 615.15	1.05	52.5	0.001		0.001 0.				0.001	0. 520
	192	284		615, 15 615, 90	0.75	37.5	0,090		D. 420 D.				0.700	0.520
	192	284	0	0.00 0.00	0.00	0.0	0.000	0.000	D. 000 D.	000	D. 000	0.000	0.000	0.000
	192	284		615.90 616.45	0. \$5		0.560		0. 430 0.				3.000	0.000
	192	284	30301	616.45 617.10	0.65	120.0	1.810	0.000	1.330 D.	000	0.000	0.000	5. 200	0.000

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