

9.3 Prediction and Assessment of Environmental Impacts

9.3.1 Air Pollution

To predict the degree of the impact of pollutants emitted from the Maritsa East No.1 Power Plant exerting upon the surrounding environment, atmospheric dispersion analysis of air pollutants has been carried out. With the prediction items comprised of the short and long term dispersion of air pollutants, this prediction has been carried out over a radius range of 30km.

The pollutants consisting of sulfur oxides (SO_x), nitrogen oxides (NO_x) and dust are predicted to be diffused where these pollutants are assumed to behave equally. The meteorological conditions used herein are those described in "Meteorological Conditions".

Although the short term dispersion conditions calculated herein are only those after completion of the reconstruction project, the long term diffusion conditions are calculated with regard to the following three cases: namely, the diffusion conditions during operation of Maritsa East No.1 Power Plant Units 1-6, present dispersion conditions and those after implementation of the reconstruction project.

The impact at pollutants from Maritsa East Nos.2 and 3 Power Plant exerting upon the surrounding environment is also considered very serious. An integrated assessment of environmental impacts including these power plants is, therefore, expected to be made separately. The following study is made in relation to Maritsa East No. 1 Power Plant only.

(1) Prediction of Short Term Dispersion

Calculation for prediction of short term dispersion is performed by using the Bosanquet Satten formula.

(a) Formula of The Effective Height of Stack (Bosanquet Formula- I)

$$H_e = H_o + \alpha (H_m + H_i)$$

$$H_m = \frac{4.77}{1+0.43U/V} \cdot \frac{\sqrt{Q \cdot V}}{U}$$

$$H_i = 6.37g \cdot \frac{Q(T-T_1)}{U^3 \cdot T_1} \left(\log_e J^2 + \frac{2}{J} \cdot 2 \right)$$

$$J = \frac{U^2}{\sqrt{Q \cdot V}} \left(0.43 \sqrt{\frac{T_1}{g \cdot G}} - 0.28 \cdot \frac{V}{g} \cdot \frac{T_1}{T - T_1} \right) + 1$$

where;

- H_e : Effective height of stack (m)
- H_o : Actual height of stack (m)
- α : Flue gas ascending coefficient (= 0.65)
- H_m : Rising height by momentum (m)
- H_t : Buoyant height by temperature (m)
- U : Wind velocity (m/s)
- V : Leaving velocity of flue gas (m/s)
- Q : Amount of flue gas at ambient temperature (m^3/s)
- T : Temperature of flue gas ($^{\circ}K$)
- T_1 : Ambient temperature ($^{\circ}K$)
- g : Acceleration of gravity (m/s^2) ($g = 9.8 m/s^2$)
- G : Temperature gradient of atmosphere ($^{\circ}C/m$)

(b) Formula for Dispersion Calculation (Sutton's Formula)

$$c(x) = \frac{2q \cdot \eta}{\pi \cdot C_y \cdot C_z \cdot U \cdot X^{2-n}} \cdot \exp\left(-\frac{1}{x^{2-n}} \cdot \frac{H_e^2}{C_z^2}\right)$$

$$C_{max} = 0.234 \cdot \frac{C_z}{C_y} \cdot \frac{q}{U \cdot H_e^2} \cdot \eta$$

$$X_{max} = \left(\frac{H_e}{C_z}\right)^{\frac{2}{2-n}}$$

where;

- $C(x)$: On-ground concentration at leeward distance X from pollutant emission source
- x : Leeward distance from pollutant emission source (m)
- α : Maximum density of on-ground concentration
- C_{max} : Maximum density of on-ground concentration
- X_{max} : Distance to maximum density of on-ground concentration from pollutant emission source (m)

- q : Amount of pollutant emission
- Cy : Dispersion variable (Vertical) (=0.07)
- Cz : Dispersion variable (Horizontal) (=0.07)
- V : Wind velocity (m/s)
- n : Atmospheric disorder coefficient (=0.25)
- He : Effective height of stack (m)
Time correction coefficient (1 hour: 0.15, 24 hour: 0.15 x 0.59)

(c) Calculation Conditions

The constant used for this calculation are as given Table 9-3-1-1. As the dimensions of the smoke sources are indicated in Table 9-3-1-2 are adopted herein.

(d) Calculated Results

Calculated maximum on-ground concentration and distance of maximum on-ground concentration are presented in Table 9-3-1-3. The on-ground concentration curve in Figure 9-3-1-1,2.

The maximum on-ground concentrations distances is 14.7km down the wind. The maximum on-ground concentrations of air pollutants all satisfy the environmental standards of Bulgaria.

(2) Prediction of Long Term Dispersion

CONCAWE Formula and Briggs' Formula are adopted for prediction of the effective height of stack. For calculation of dispersion, Plume and Puff Formulae are adopted.

(a) Formula of the effective height of stack

① Windy condition : CONCAWE Formula

$$H_e = H_o + \Delta H$$

$$\Delta H = 0.175 \cdot QH^{1/2} \cdot U^{-3/4}$$

② Windless condition : Briggs' Formula

$$H_e = H_o + \Delta H$$

$$\Delta H = 1.4 \cdot Q_H^{1/4} (dQ/dz)^{-3/8}$$

$$QH = \rho \cdot Q \cdot C_p \cdot (T - T_1)$$

where:

H_e : Effective height of stack (m)

H_o : Actual height of stack (m)

ΔH : Exhaust gas rising height (m)

Q_H : Exhaust calorie (cal/s)

ρ : Density of flue gas at 0°C (= 1,293 g/m³)

Q : Amount of flue gas (m³N/s)

C_p : Specific heat (= 0.24 cal/kg)

T : Flue gas temperature (°C)

T_1 : Ambient temperature (°C)

U : Wind velocity (m/s)

(b) Formula for dispersion calculation

① Windy condition : Plume Formula

$$C(X) = \frac{2Q}{\sqrt{2\pi} \cdot \frac{\pi}{8} \cdot X \cdot \sigma z \cdot U} \exp\left(-\frac{1}{2} \cdot \frac{He^2}{\alpha z^2}\right)$$

② Windless condition : Puff Formula

$$C(R) = \frac{2Q}{(2\pi)^{3/2} \cdot \alpha^2 \cdot \gamma} \cdot \frac{1}{\frac{R^2}{\alpha^2} + \frac{He^2}{\gamma}}$$

Where:

$C(X)$: On-ground concentration at leeward distance $X(m)$ from pollutant emission source (m^3/m^3)

$C(R)$: On-ground concentration at distance $R(m)$ from pollutant emission source (m^3/m^3)

Q : Amount of pollutant emission ($N m^3/s$)

U : Wind velocity (m/s)

X : Leeward distance from pollutant emission source (m)

R : Distance from pollutant emission source (m)

He : Effective height of stack (m)

σz : Dispersion width in vertical direction at leeward distance $X(m)$ (m)

α : Dispersion variable (Horizontal) (m/s)

γ : Dispersion variable (Vertical) (m/s)

Regarding dispersion variables, the following are adopted.

Windy condition: Approximate function of Pasquill - Gifford, Chart (Refer to Table 9-3-1-4.)

Windless condition: Dispersion variable at no wind condition using the Pasquill's stability (Refer to Table 9-3-1-5.)

(c) Conditions of Pollutant Sources

As the dimensions of the smoke sources are indicated Table 9-3-1-6.

(d) Results of Calculation and Assessment

The annual mean concentration values are based on the prediction Figures 9-3-1-3~9-3-1-11.
The Maximum on-ground concentrations are as follows.

① Case I (The Past)

(I) SO_x

The maximum on-ground concentration is 165 μ g/m³ (yealy mean).

(II) NO_x

The maximum on-ground concentration is 5 μ g/m³ (yealy mean).

(III) Dust

The maximum on-ground concentration is 48 μ g/m³ (yealy mean).

The maximum SO_x above-ground concentration substantially exceed the environmental standards of Bulgaria (50 μ g/m³). Therefore, the atmospheric air quality during operation of Units 5 and 6 of Maritsa East No.1 Power Plant is not deemed to have been so desirable.

② Case II (The Present)

(I) SO_x

The maximum on-ground concentration is 100 μ g/m³ (yealy mean).

(II) NO_x

The maximum on-ground concentration is 5 μ g/m³ (yealy mean).

(III) Dust

The maximum on-ground concentration is 31 μ g/m³ (yealy mean).

The maximum SO_x above-ground concentration exceed the environmental standards of Bulgaria. Consequently, the atmospheric air quality during operation of Units 5 and 6 of Maritsa East No.1 Power Plant is not deemed to have been so desirable.

③ Case III (The After Replacing)

(I) SO_x

The maximum on-ground concentration is 16 μ g/m³ (yealy mean).

(II) NO_x

The maximum on-ground concentration is 4 μ g/m³ (yealy mean).

(III) Dust

The maximum on-ground concentration is 0.6 μ g/m³ (yealy mean).

The concentration of sulfur oxides (SO_x), nitrogen oxides (NO_x) and dust all satisfy the environmental standards of Bulgaria.

Now, Since the existing Units 1~6 boilers and coal drying equipment (the units 7~10 boilers have already been demolished) in the Maritza East No.1 Power Plant will not be used and demolished upon completion of this replacement project. Consequently, the total amount of SO₂ emission will be reduced ultimately by as much as 50.9t/h (=54.4ton/hour - 5.3ton/hour), hence reduction ratio is about 90%. (Refer to Table 9-3-1-7).

In addition, the amount of dust emissions will also be reduced by as much as [8.28 ton/hour - 0.20ton/hour=8.08ton/hour.]or reduction ration of about 98%. (Refer to Table 9-3-1-8).

Consequently, the contribution degree of this reconstruction project for improving the environment can be regarded of vital significance.

Table 9-3-1-1 Calculation Constant

| Item | Unit | 1 Hour Value | 24 Hour Value |
|--|------|---------------|---------------|
| On-ground Concentration | — | | |
| Effective Height of Stack | — | | |
| Temperature | °C | 15 | 15 |
| Wind velocity | m/s | 6 | 6 |
| Dispersion Variable | — | Cy=Cz=0.07 | Cy=Cz=0.07 |
| Ambient Atmospheric Disorder Coefficient | — | n=0.25 | n=0.25 |
| Temperature Gradient | °C/m | G=0.0033 | G=0.0033 |
| Flue Gas Ascending Coefficient | — | $\alpha=0.65$ | $\alpha=0.65$ |
| Time Correction Coefficient | — | $\eta=0.224$ | $\eta=0.046$ |

Table 9-3-1-2 Data/Specification of Pollutant Emission Sources

| Plant Specification Unit NO. | Unit | Maritsa East # 1 (After Replacing) | R2 (230MW) |
|---------------------------------|-----------------------------------|------------------------------------|---------------|
| Stack Height | m | 180 | 180 |
| Stack Inner Diameter at the Top | m | 4.8 | 4.8 |
| Flue Gas Flow | 10 ³ m ³ /h | 1.297 | 1.297 |
| SOx Conc. | ppm | 940 | 940 |
| NOx Conc. | ppm | 292 | 292 |
| Dust Conc. | mg/ m ³ N | 100 | 100 |
| Stack outlet gas Temp. | °C | 170 | 170 |
| Velocity | m/s | 30 | 30 |

Table 9-3-1-3 Maximum On-ground Concentration and Distance of Maximum On-ground Concentration with reference Environmental Standards

| Item | Unit | Maximum On-ground Concentration | Bulgarian Standard |
|--|---------------|---------------------------------|--------------------|
| SOx | 1 hour value | 97 | 254 |
| | 24 hour value | 20 | 150 |
| NOx | 1 hour value | 21 | 102 |
| | 24 hour value | 4 | 60 |
| Dust | 1 hour value | 4 | 424 |
| | 24 hour value | 1 | 250 |
| Distance to Maximum On-ground Concentration Position | km | 17.6 | — |

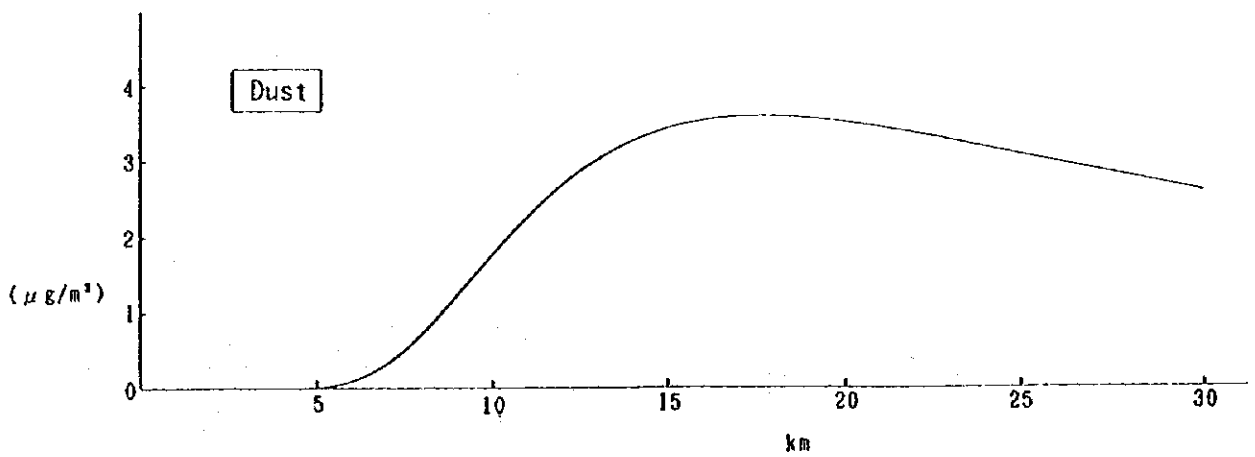
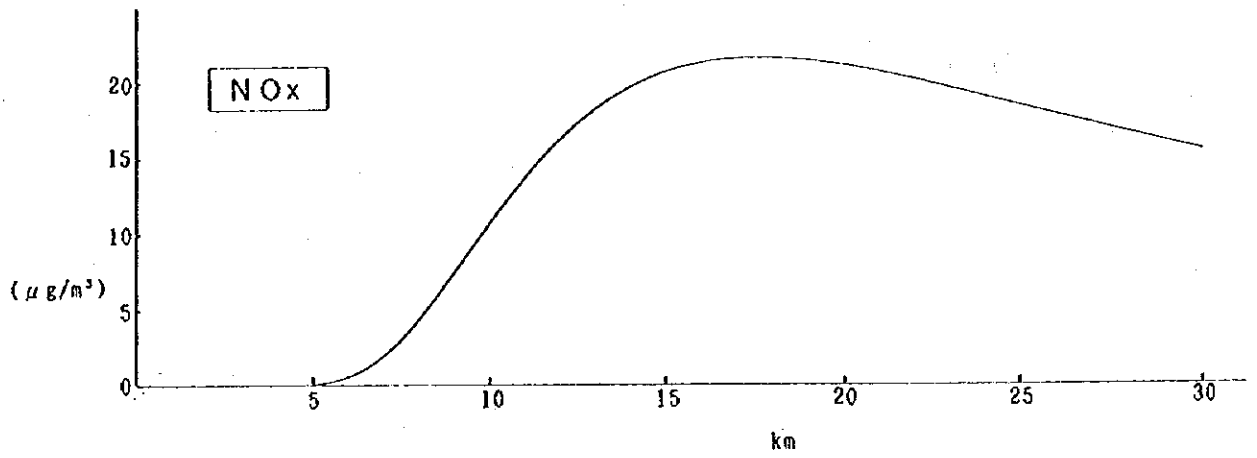
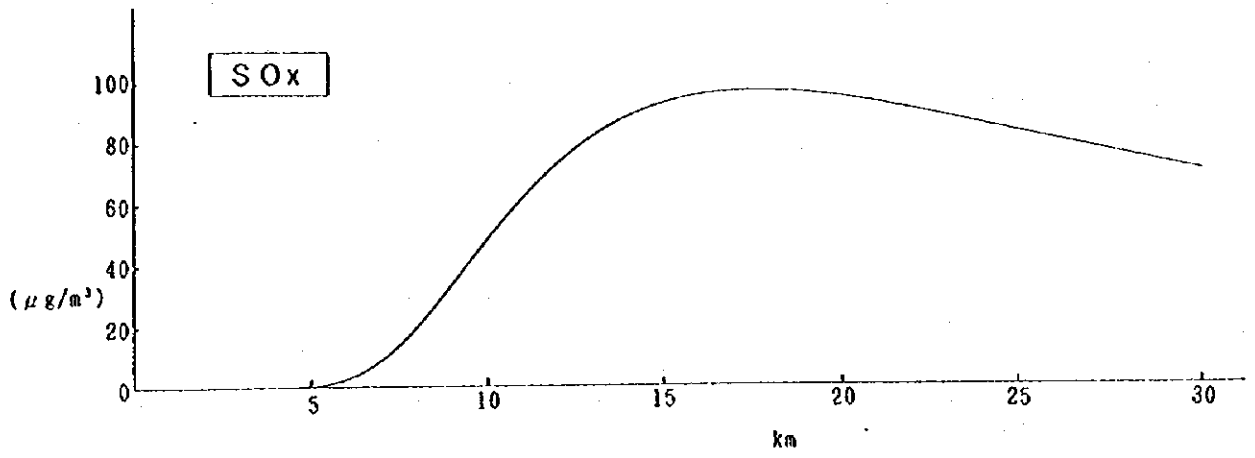


Figure 9-3-1-1 On-ground Concentration Curve for 1 Hour Value

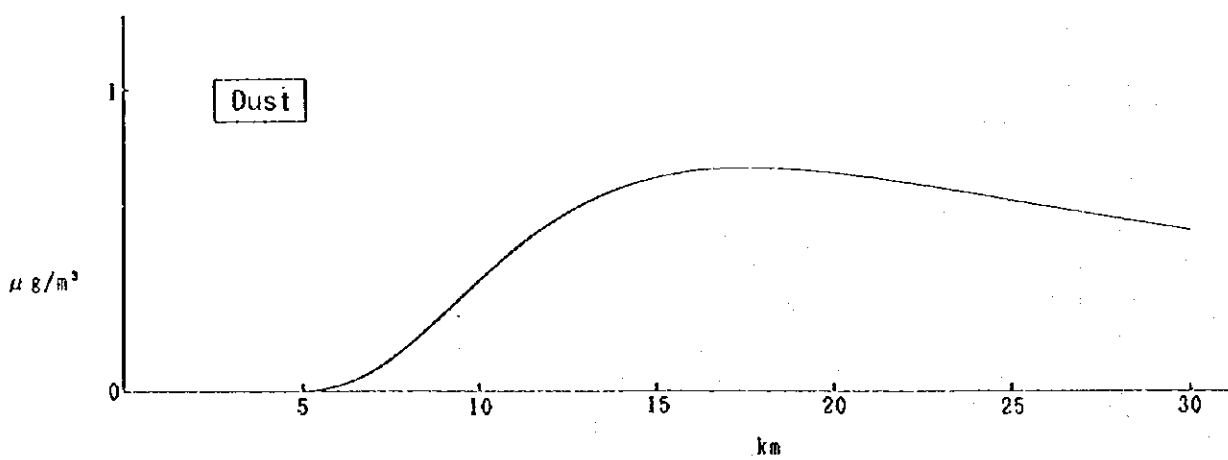
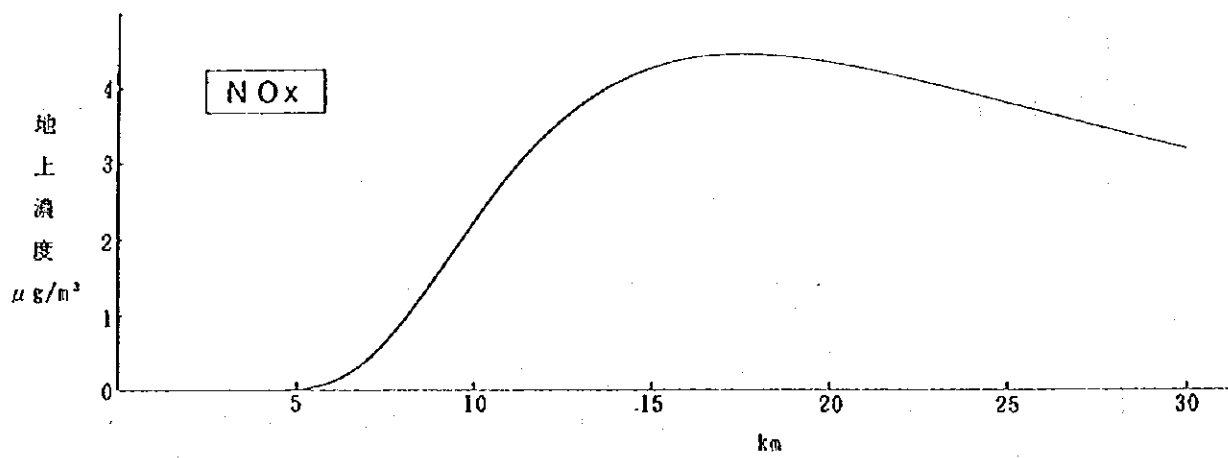
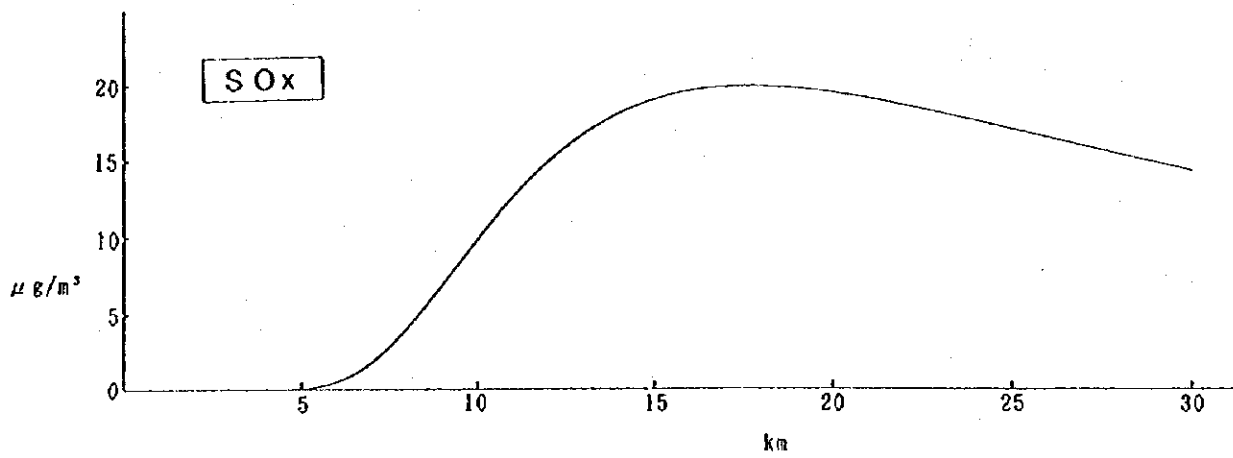


Figure 9-3-1-2 On-ground Concentration Curve for 24 Hour Value

Table 9-3-1-4 Dispersion Variable (Windy condition)
(Approximate function of Pasquile.Gyford Figure)

$$\sigma_z(x) = b \cdot x^a$$

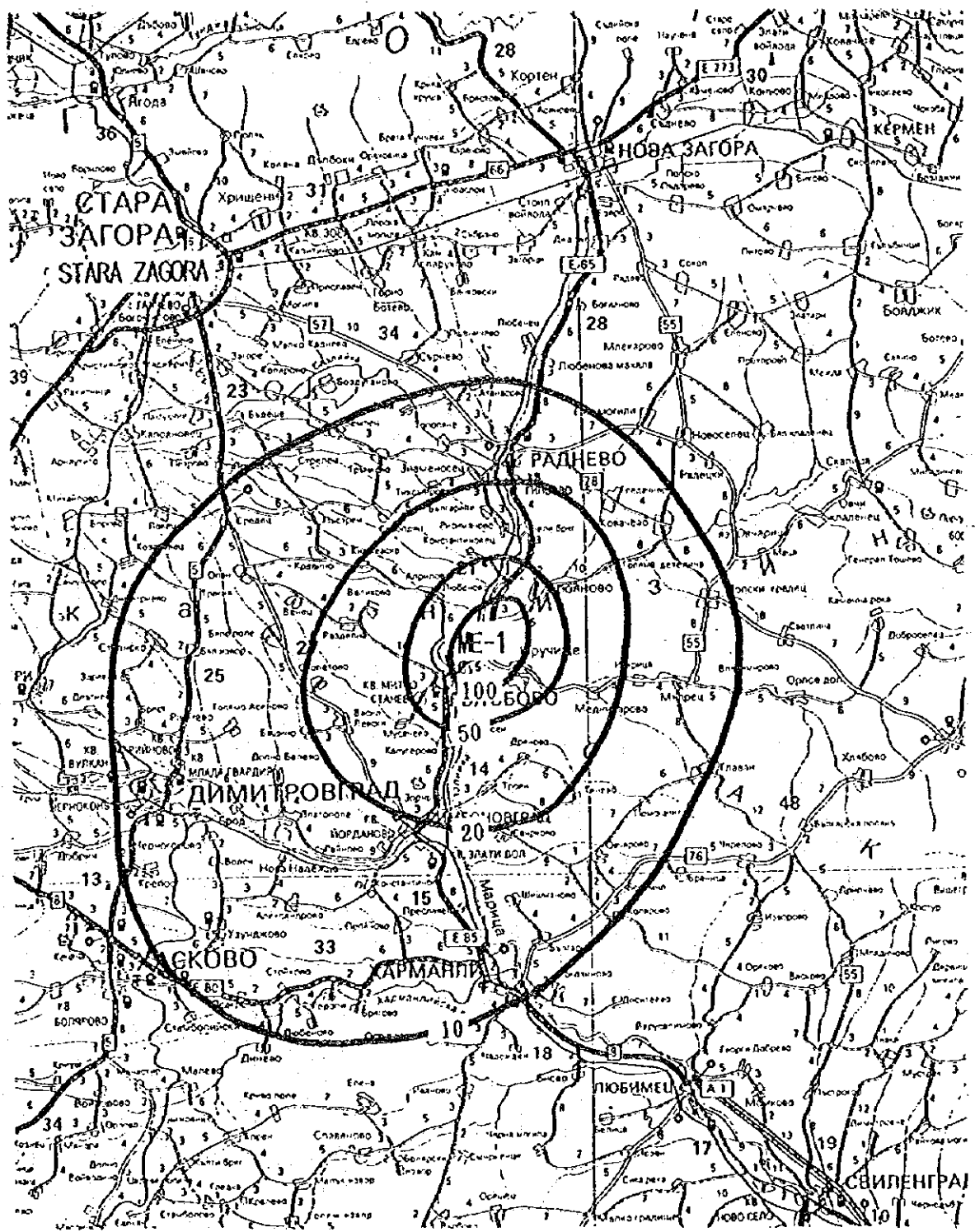
| Atmospheric Stability | a | b | Leeward distance X (m) |
|-----------------------|-------|--------|------------------------|
| B | 0.964 | 0.1272 | 0 - 500 |
| | 1.094 | 0.0570 | 500 - |
| C | 0.918 | 0.1068 | 0 - |
| | 0.872 | 0.1057 | 0 - 1,000 |
| | 0.775 | 0.2067 | 1,000 - 10,000 |
| CD | 0.737 | 0.2943 | 10,000 - |
| | 0.826 | 0.1046 | 0 - 1,000 |
| | 0.632 | 0.400 | 1,000 - 10,000 |
| D | 0.555 | 0.811 | 10,000 - |
| | 0.788 | 0.0928 | 0 - 1,000 |
| | 0.565 | 0.433 | 1,000 - 10,000 |
| E | 0.415 | 1.732 | 10,000 - |
| | 0.784 | 0.0621 | 0 - 1,000 |
| | 0.526 | 0.370 | 1,000 - 10,000 |
| F | 0.323 | 2.41 | 10,000 - |

Table 9-3-1-5 Dispersion Variable (Windless condition)

| Atmospheric Stability | α | γ |
|-----------------------|----------|----------|
| B | 0.781 | 0.474 |
| C | 0.635 | 0.208 |
| CD | 0.542 | 0.153 |
| D | 0.470 | 0.113 |
| E | 0.439 | 0.067 |
| F | 0.439 | 0.048 |

Table 9-3-1-6 Data/Specification of Pollutant Emission Sources

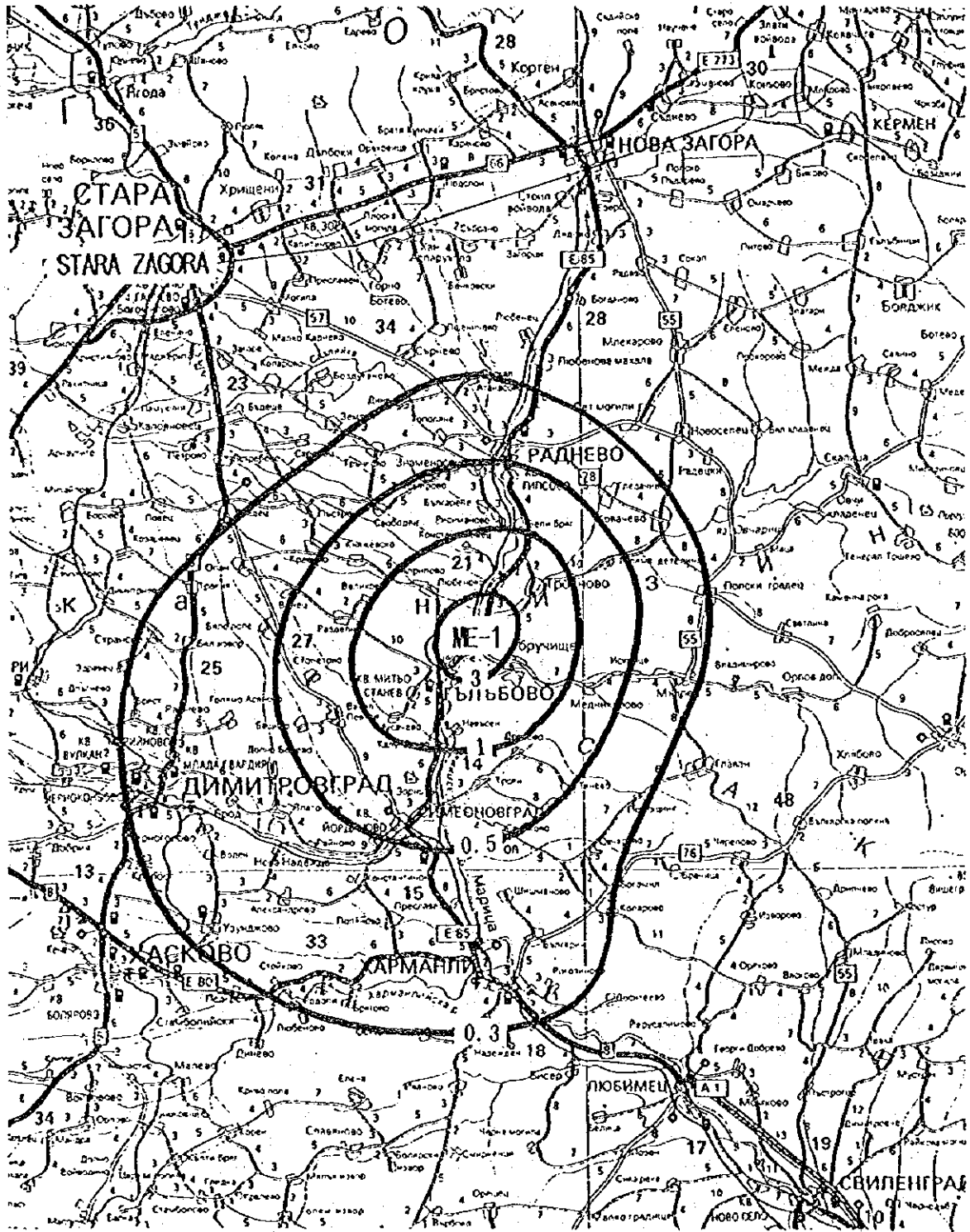
| | Unit | Maritsa East #1 | | |
|------------------------------------|-----------------------------------|----------------------|--------------------------|-------------------------------|
| | | Case I (The Past) | Case II (The Present) | Case III (After Replacing) |
| Plant Specification | | | | |
| Boiler No. | | 1~6 (210t/h×6) | Dryer 1~14 | Dryer 1~7 |
| Stack Height | m | 150 | 120 | 120 |
| Stack Inner Diameter at the Top | m | 6 | 5 | 5 |
| Flue Gas Flow | 10 ³ m ³ /h | 2,316 | 806 | 403 |
| SO _x Conc. | ppm | 5,000 | 5,000 | 5,000 |
| NO _x Conc. | ppm | 240 | 97 | 97 |
| Dust Conc. | mg/m ³ N | 200 | 15,000 | 15,000 |
| Stack Outlet Gas Temp. | °C | 190 | 92 | 92 |
| Velocity | m/s | 12.0 | 11.0 | 11.0 |
| | | | | 180 |
| | | | | 4.8 |
| | | | | 2,594 |
| | | | | 940 |
| | | | | 292 |
| | | | | 100 |
| | | | | 170 |
| | | | | 30 |



Unit : $\mu\text{g}/\text{m}^3$

0 10 20 30km

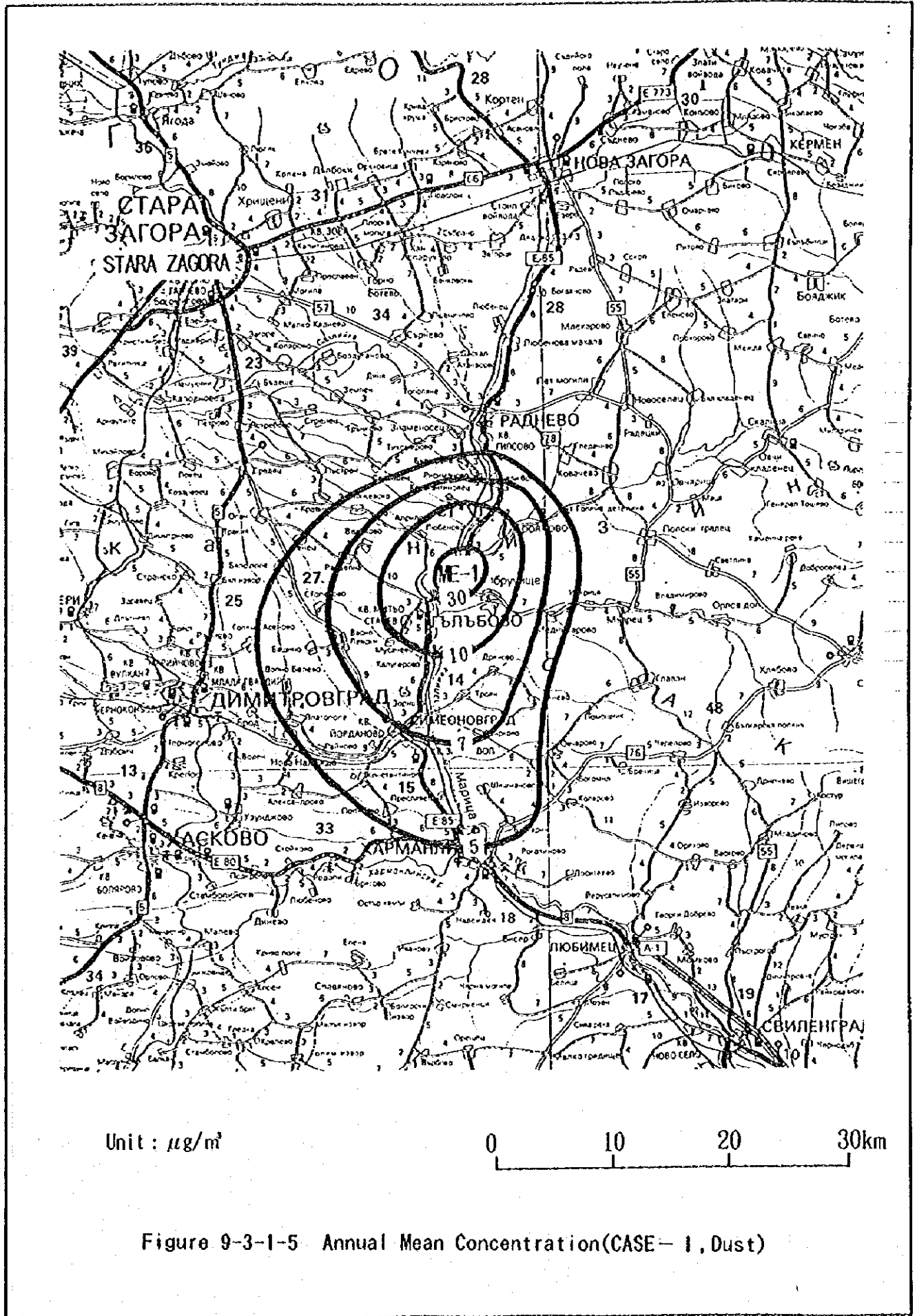
Figure 9-3-1-3 Annual Mean Concentration(CASE-1, SOx)

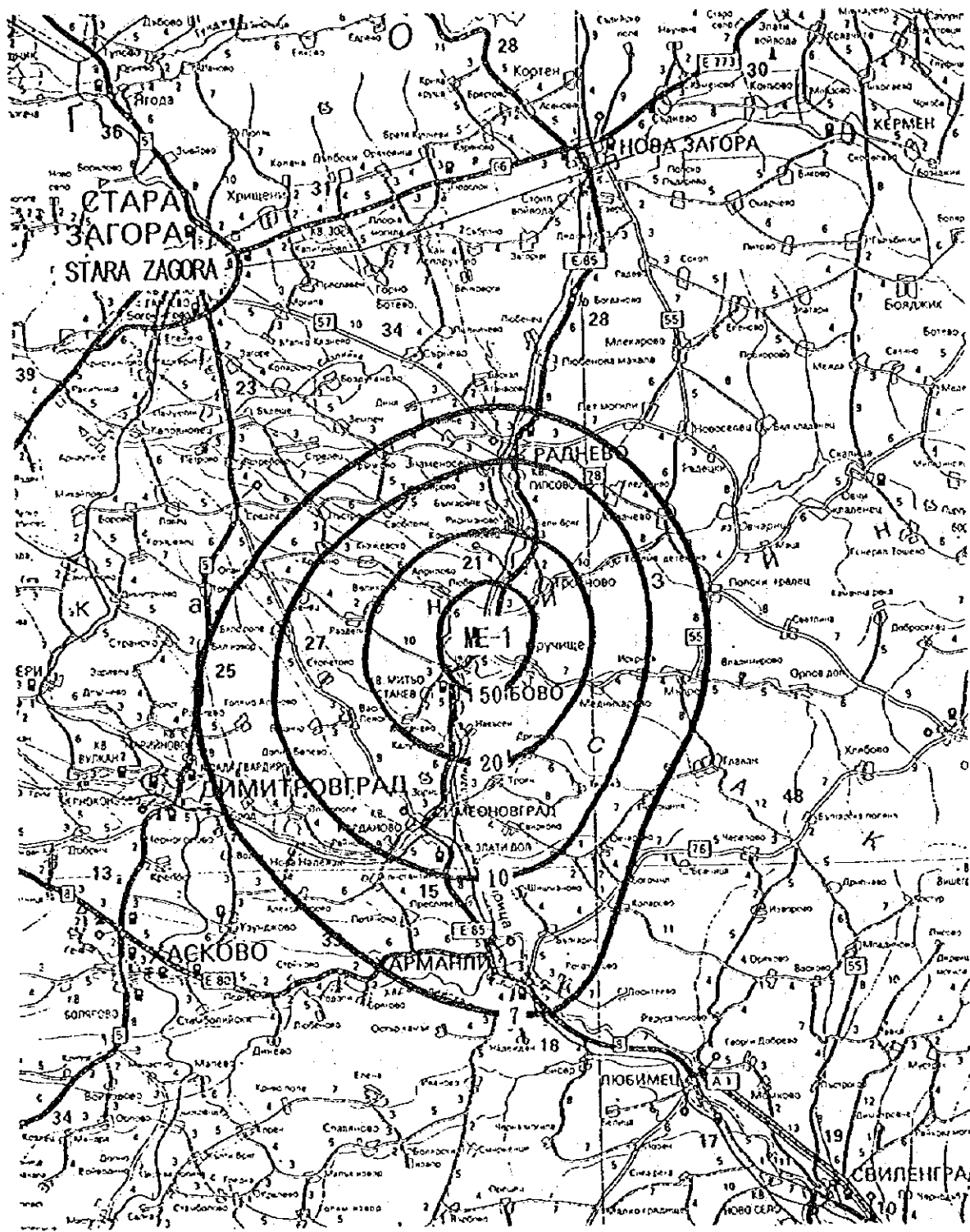


Unit: $\mu\text{g}/\text{m}^3$



Figure 9-3-1-4 Annual Mean Concentration(CASE-1, NOx)

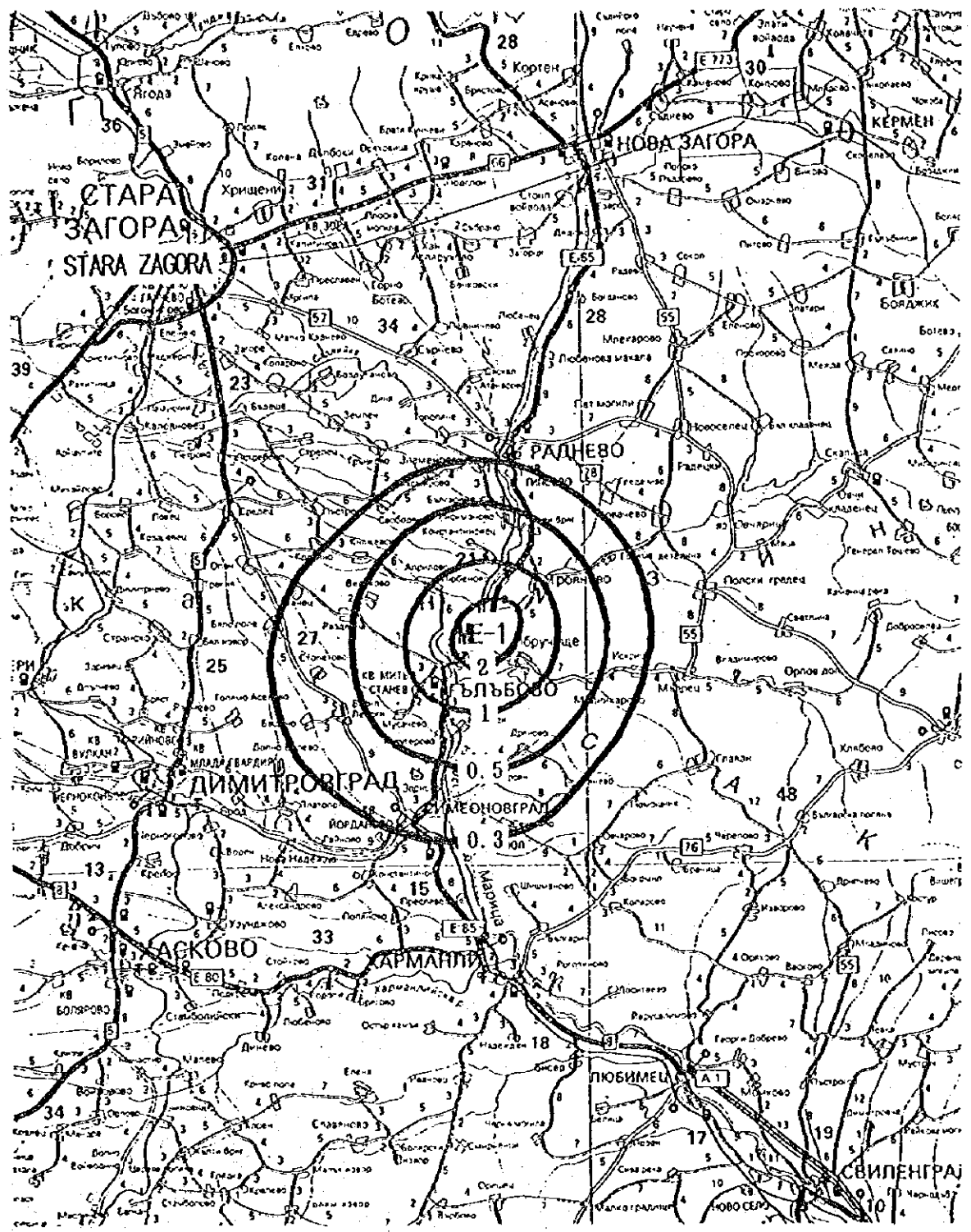




Unit : $\mu\text{g}/\text{m}^3$

0 10 20 30km

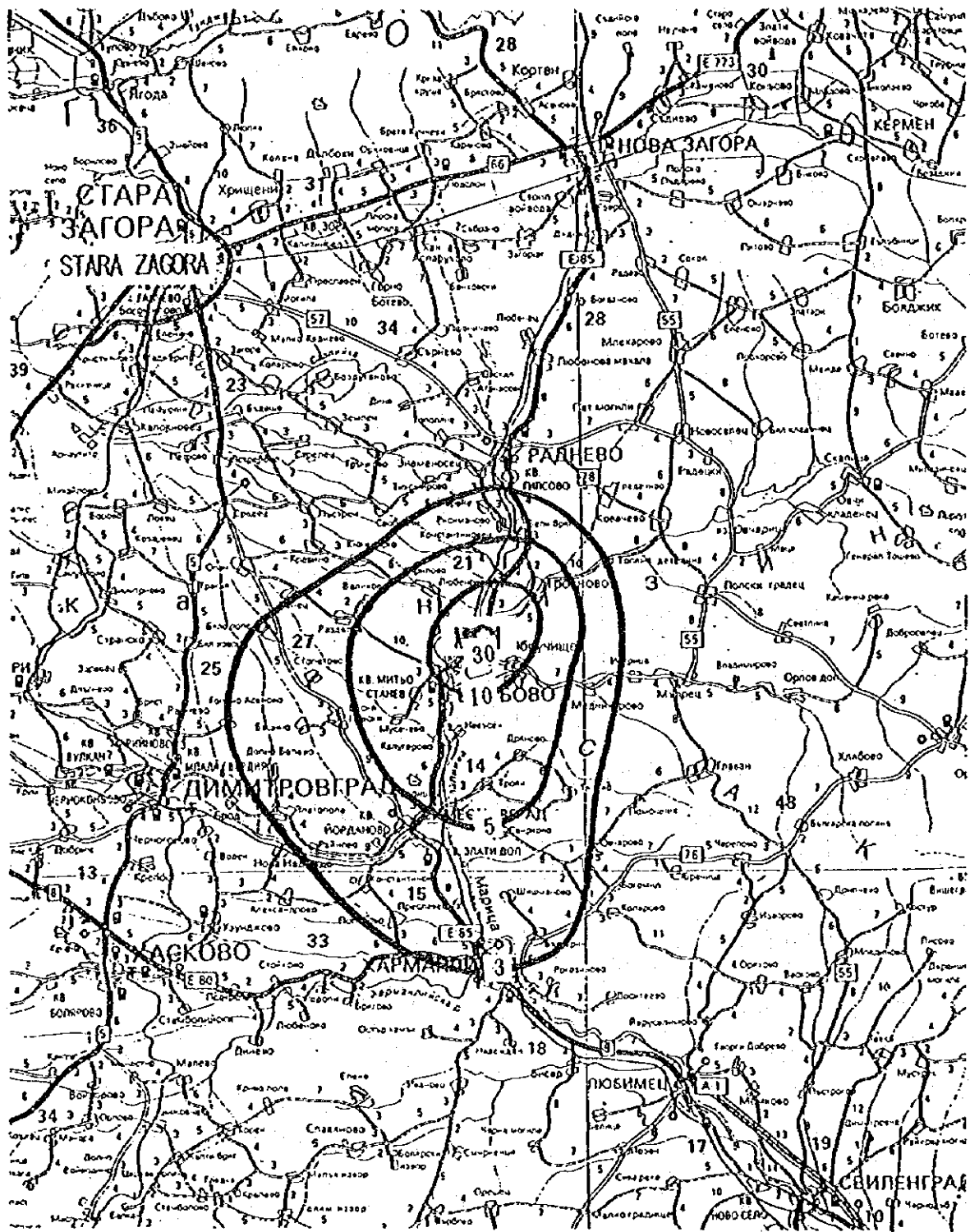
Figure 9-3-1-6 Annual Mean Concentration(CASE-II, SOx)



Unit : $\mu\text{g}/\text{m}^3$



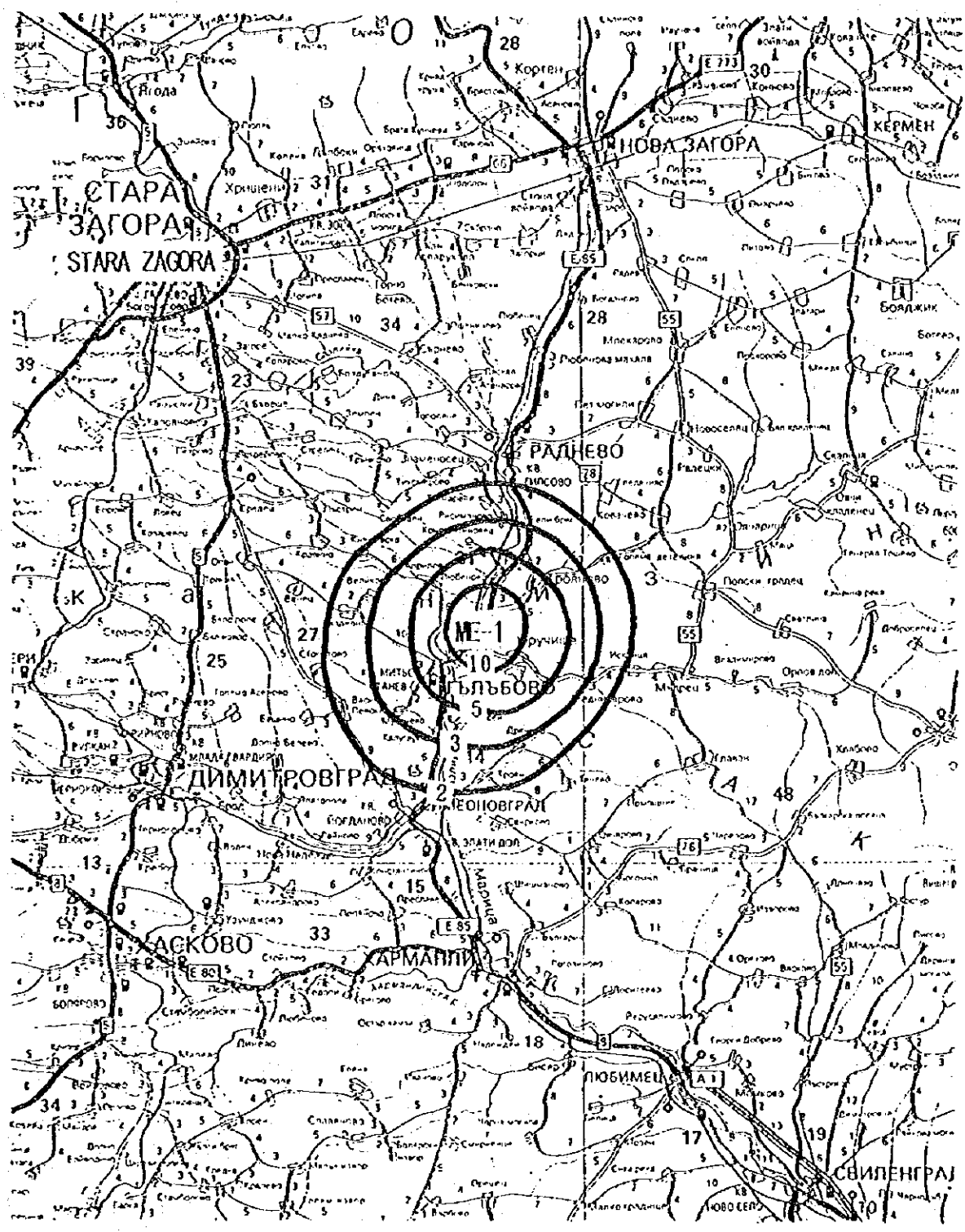
Figure 9-3-1-7 Annual Mean Concentration(CASE - II, NOx)



Unit : $\mu\text{g}/\text{m}^3$

0 10 20 30km

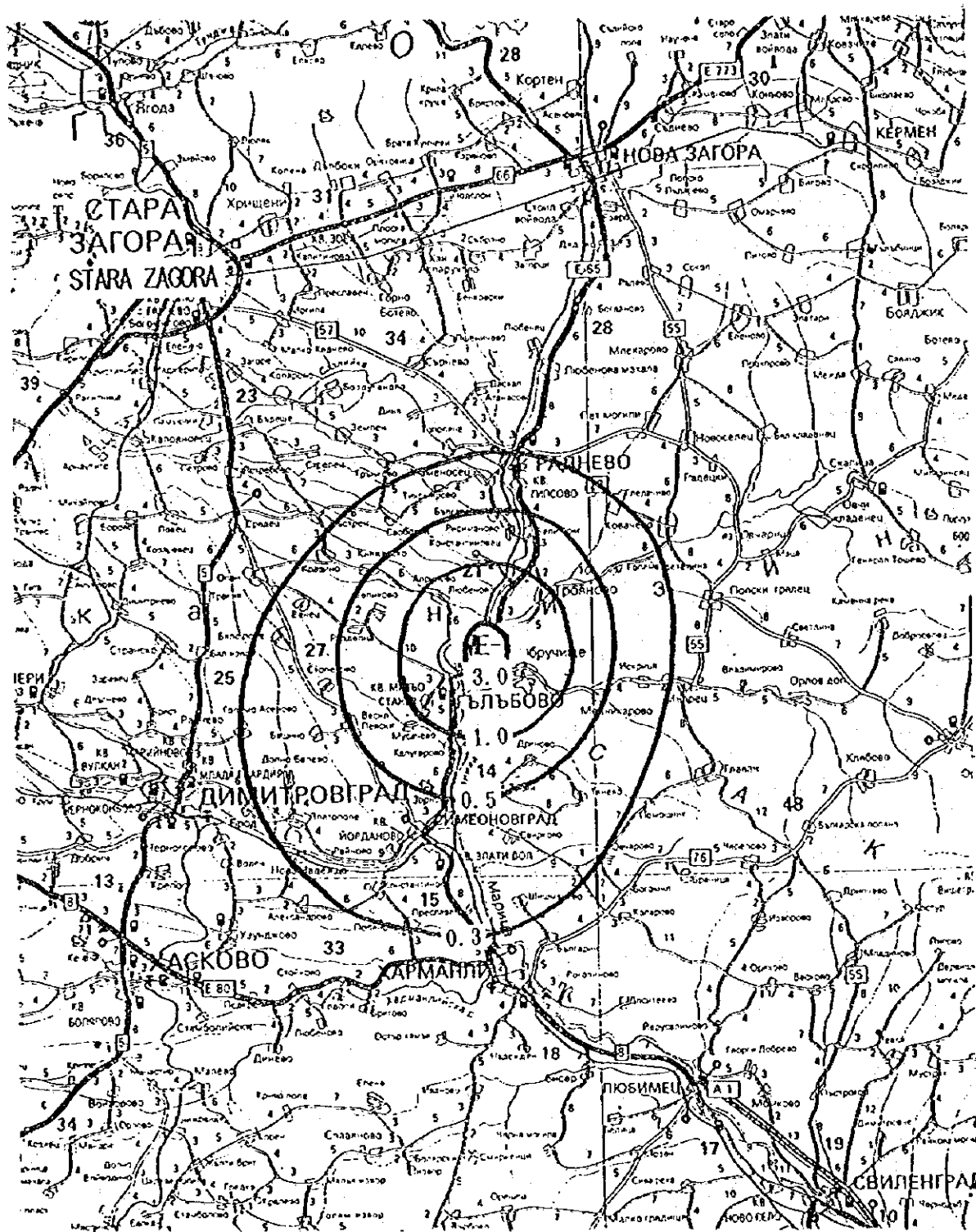
Figure 9-3-1-8 Annual Mean Concentration(CASE- II, Dust)



Unit : $\mu\text{g}/\text{m}^3$

0 10 20 30km

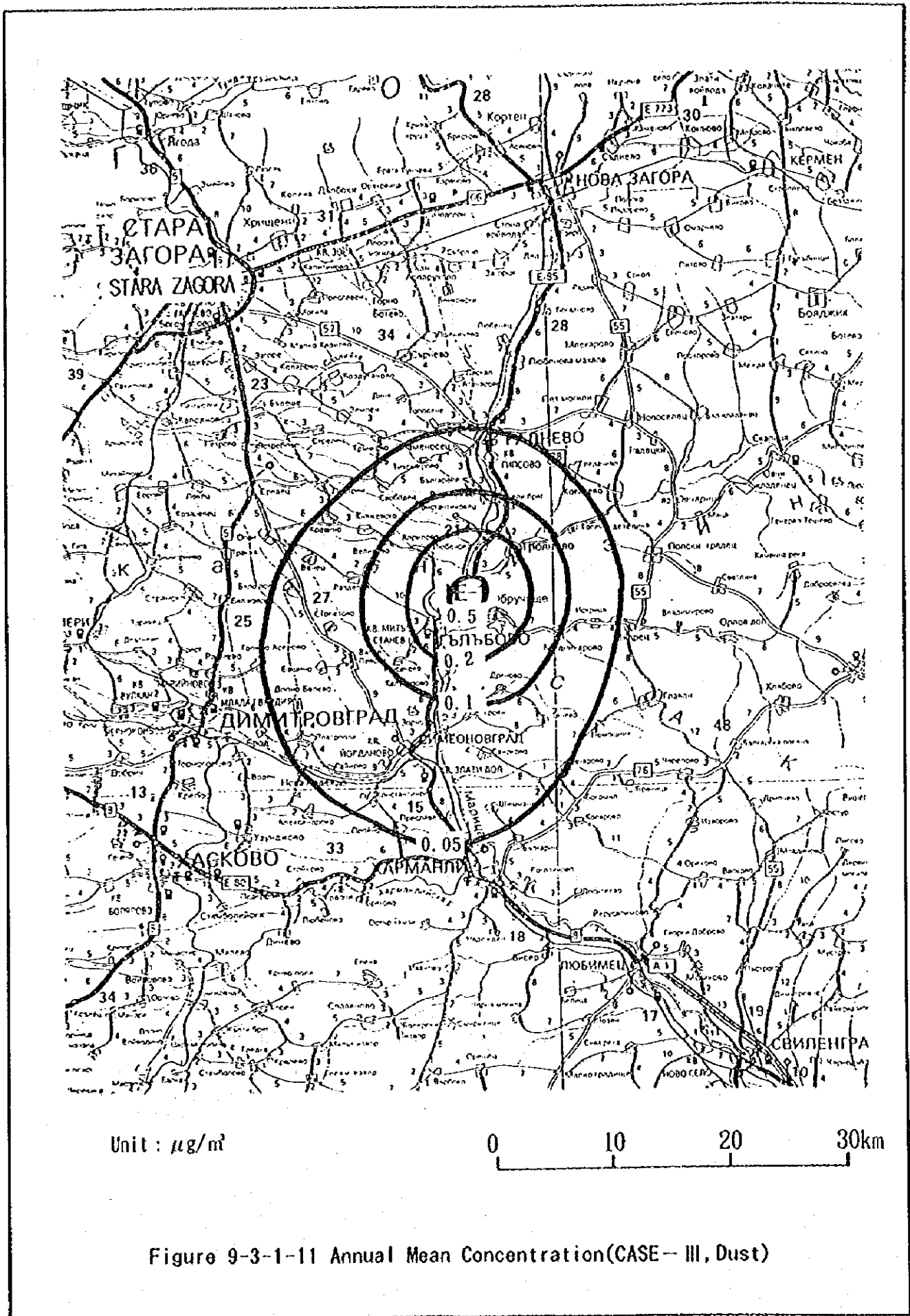
Figure 9-3-1-9 Annual Mean Concentration(CASE - III, SOx)

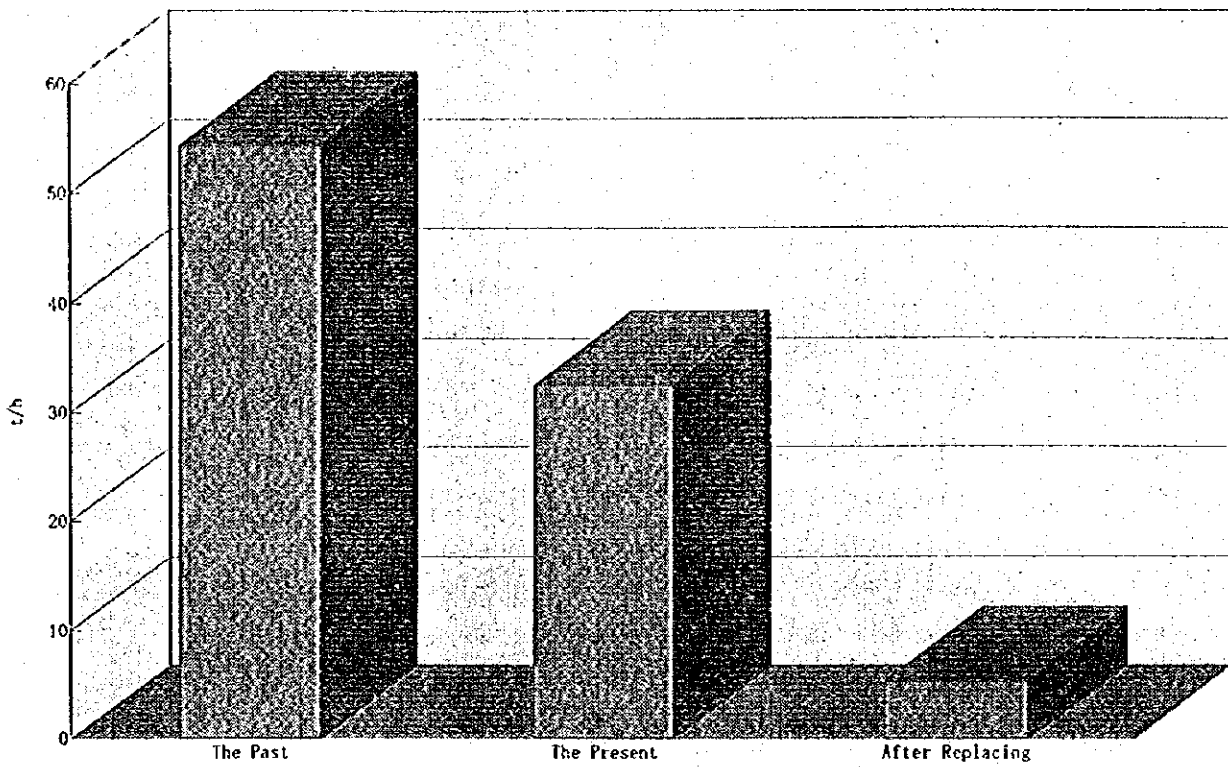


Unit : $\mu\text{g}/\text{m}^3$



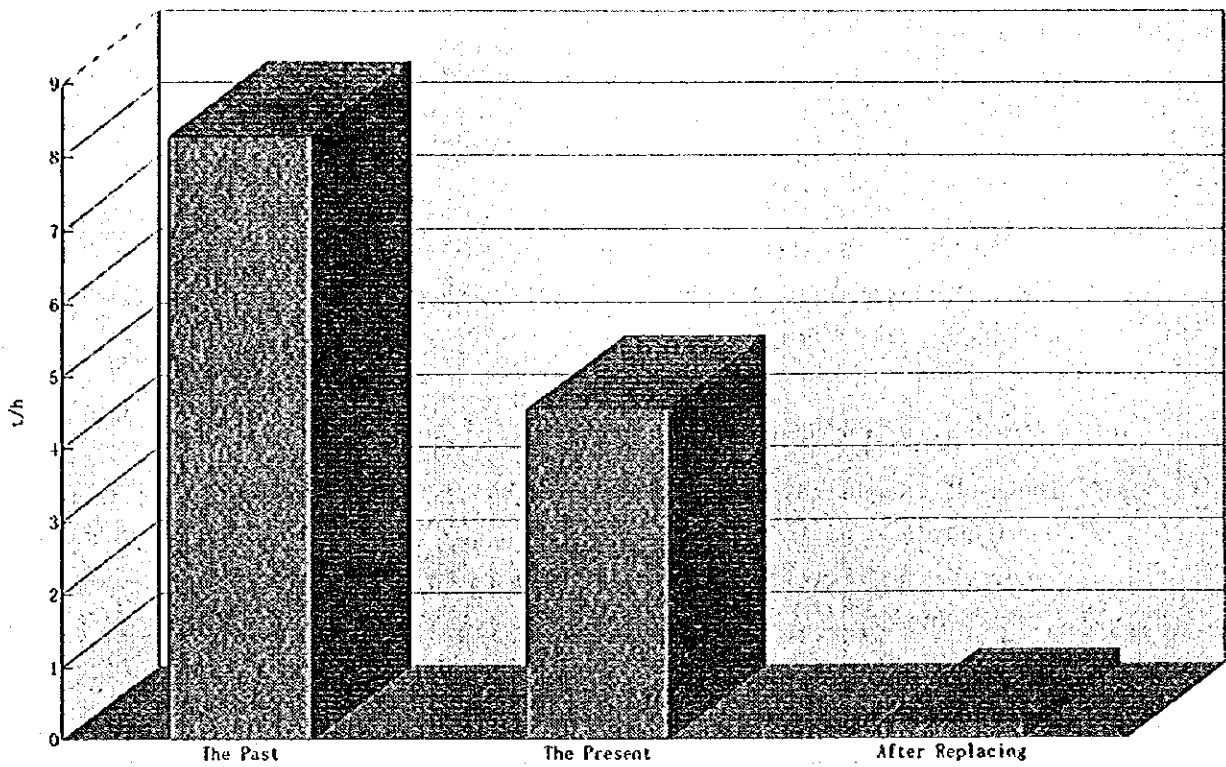
Figure 9-3-1-10 Annual Mean Concentration(CASE - III, NOx)





| | The Past | The Present | After Replacing |
|-------------------------------|-------------------------------------|----------------------|-----------------|
| Operating Condition | No.1~4 unit No.5~6 unit Dryer | No.1~4 unit Dryer | No.R1~R2 unit |
| Total SOx Amount of Discharge | About 54.4t/h | About 32.5t/h | About 5.3t/h |
| Reduction Ratio | Base | About 40 % | About 90 % |
| | About 167 % | Base | About 84 % |

**Table9-3-1-7 Total SOx Amount of Discharge and Reduction Ratio
at Maritsa East No.1**



| | The Past | The Present | After Replacing |
|--------------------------------|-------------------------------------|----------------------|-----------------|
| Operating Condition | No.1~4 unit No.5~6 unit Dryer | No.1~4 unit Dryer | No.R1~R2 unit |
| Total Dust Amount of Discharge | About 8.28t/h | About 4.54t/h | About 0.20t/h |
| Reduction Ratio | Base | About 45 % | About 98 % |
| | About 182 % | Base | About 96 % |

**Table9-3-1-8 Total Dust Amount of Discharge and Reduction Ratio
at Maritsa East No.1**

9.3.2 Noise

(1) Prediction and Evaluation of Noise

(a) Sound Source Power Level

The sound source power level of the machinery which will be newly built upon reconstruction are shown in Table 9-3-2-1. The machinery installed indoors is included in the building sound sources.

(b) Prediction and Evaluation of Noise

The result of the forecast noise level at the site boundary based on the above data (a) is as shown in Table 9-3-2-2 and contour maps based on replaced equipment are shown in Figure 9-3-2-1a,b. These show a slightly increase from the current levels.

As there is not the noise standard at the site boundary in Bulgaria, evaluation is done by comparing forecast noise levels at the site boundary with the highest admissible noise levels in industrial district - 70 dB(A) in the daytime, 60 dB(A) at night (Hygienic Norms No. 0-64) - as reference.

Though two forecast noise levels in Table 9-3-2-2 (boundary No.2,3 at night) are over the reference admissible one in addition to current excess boundary points (boundary No.16 in the daytime, boundary No. 13,16,17,18 at night), it is judged that noise levels at residential areas are lower than those of reference admissible owing to reduction effect of distance. It is not considered a problematic level.

(2) Recommendation

In the regulations on the noise in Bulgaria, more importance is attached to the noise from the viewpoint of the work environment rather than the noise at the site boundary. However, when the life of the power plant is taken into consideration, it is expected that the noise regulation is strengthened during the period of the plant's life. It will result in a larger amount of expenses and harder works if prevention measures are taken after the actual troubles have occurred.

Therefore, it is desirable to install those machinery which may become the generating source of indoor noise, adopt low-noise machinery for those installed outdoors, and take a countermeasures such as building shield walls and installing mufflers when necessary.

Table 9-3-2-1 Sound Power Level List

| No | Facility | Time | SPL (dBA) | No | Facility | Time | SPL (dBA) |
|----|--------------------------|----------|--------------|----|------------------------|----------|--------------|
| 1 | A Bucket Wheel Reclaimer | day-time | 89 | 29 | LJT-1 (LBC-2→3) | day-time | 70 |
| 2 | B Bucket Wheel Reclaimer | day-time | 89 | 30 | LJT-2 (LBC-3→4) | day-time | 70 |
| 3 | B Tripper | day-time | 85 | 31 | LJT-3 (LBC-5→6) | all day | 70 |
| 4 | B Portal Reclaimer | all day | 95 | 32 | Vacuum Fan | all day | 102 |
| 5 | BC-1A Conveyer | day-time | 78 | 33 | Filter Separator | all day | 95 |
| 6 | BC-1B Conveyer | day-time | 78 | 34 | Air-Intake Valve | all day | 80 |
| 7 | BC-2 Conveyer | day-time | 80 | 35 | Vacuum Transfer Tube | all day | 96 |
| 8 | BC-3 Conveyer | day-time | 80 | 36 | No.1 Ash Transfer Fan | all day | 103 |
| 9 | BC-5 Conveyer | day-time | 80 | 37 | No.1 Ash Transfer Tube | all day | 75 |
| 10 | BC-6C Conveyer | day-time | 80 | 38 | Ventilator for Silo | all day | 85 |
| 11 | BC-7B Conveyer | all day | 75 | 39 | No.2 Ash Transfer Fan | day-time | 103 |
| 12 | BC-8B Conveyer | all day | 77 | 40 | No.2 Ash Transfer Tube | day-time | 75 |
| 13 | BC-9B Conveyer | all day | 77 | 41 | Boiler House (upper) | all day | 58 |
| 14 | BC-1A Conveyer Drive | day-time | 90 | 42 | Boiler House (middle) | all day | 60 |
| 15 | BC-1B Conveyer Drive | day-time | 90 | 43 | Boiler House (lower) | all day | 59 |
| 16 | BC-7B Conveyer Drive | all day | 92 | 44 | Boiler Conveyer House | all day | 67 |
| 17 | BC-2 Sampler House | day-time | 70 | 45 | Boiler House (roof) | all day | 57 |
| 18 | JT-1 (BC-3→5) | day-time | 70 | 46 | ESP | all day | 67 |
| 19 | JT-4 (BC-5→6C) | day-time | 70 | 47 | IDF | all day | 80 |
| 20 | Screen Crusher House | all day | 80 | 48 | Flue Gas Duct | all day | 70 |
| 21 | BC-9B Sampler House | all day | 80 | 49 | Turbine House (upper) | all day | 58 |
| 22 | Tripper | day-time | 85 | 50 | Turbine House (middle) | all day | 60 |
| 23 | Portal Reclaimer | all day | 94 | 51 | Turbine House (lower) | all day | 55 |
| 24 | LBC-2 Conveyer | day-time | 70 | 52 | Turbine House (roof) | all day | 53 |
| 25 | LBC-3 Conveyer | day-time | 70 | 53 | Main Trans | all day | 70 |
| 26 | LBC-4 Conveyer | day-time | 70 | 54 | House Trans | all day | 70 |
| 27 | LBC-5A Conveyer | all day | 69 | 55 | Starting Trans | day-time | 70 |
| 28 | LBC-6A Conveyer | all day | 69 | 56 | Waste water pump group | all day | 75 |

Table 9-3-2-2 Noise Forecast at Boundary

| dB(A) | | | | | |
|-------|---------|-------|------|---------|-------|
| No. | Daytime | Night | No. | Daytime | Night |
| (1) | 56.9 | 56.7 | (14) | 57.0 | 60.0 |
| (2) | 61.3 | 61.2 | (15) | 61.0 | 58.6 |
| (3) | 65.4 | 65.3 | (16) | 71.0 | 68.1 |
| (4) | 58.7 | 56.2 | (17) | 61.0 | 64.7 |
| (5) | 54.6 | 52.3 | (18) | 60.0 | 61.4 |
| (6) | 50.8 | 46.2 | (19) | 57.6 | 60.0 |
| (7) | 51.4 | 56.2 | (20) | 56.8 | 58.9 |
| (8) | 59.7 | 56.2 | (21) | 53.1 | 55.6 |
| (9) | 59.3 | 54.5 | (22) | 53.8 | 54.9 |
| (10) | 63.2 | 55.6 | (23) | 51.8 | 51.6 |
| (11) | 60.6 | 56.4 | (24) | 49.5 | 45.4 |
| (12) | 56.5 | 56.6 | (25) | 49.0 | 46.4 |
| (13) | 59.3 | 61.5 | (26) | 50.4 | 46.1 |

- Notes: 1) Measured date: Daytime 1995.6.28 15:00, Night 1995.6.29 21:00
 2) During taking night data at (7) - (23), there was influence of traffic.

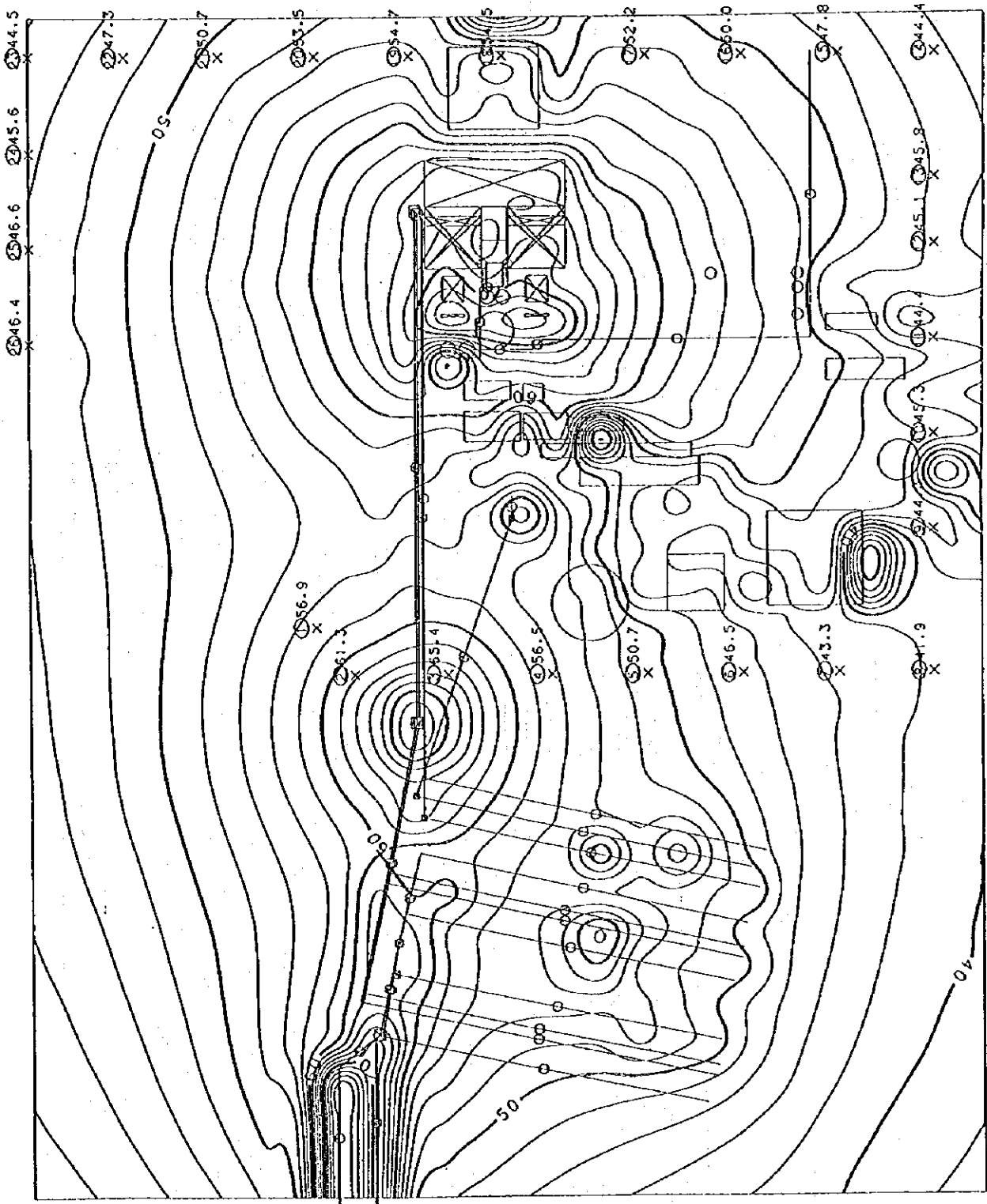


Figure 9-3-2-1a Contour Map based on replaced equipment (Daytime)

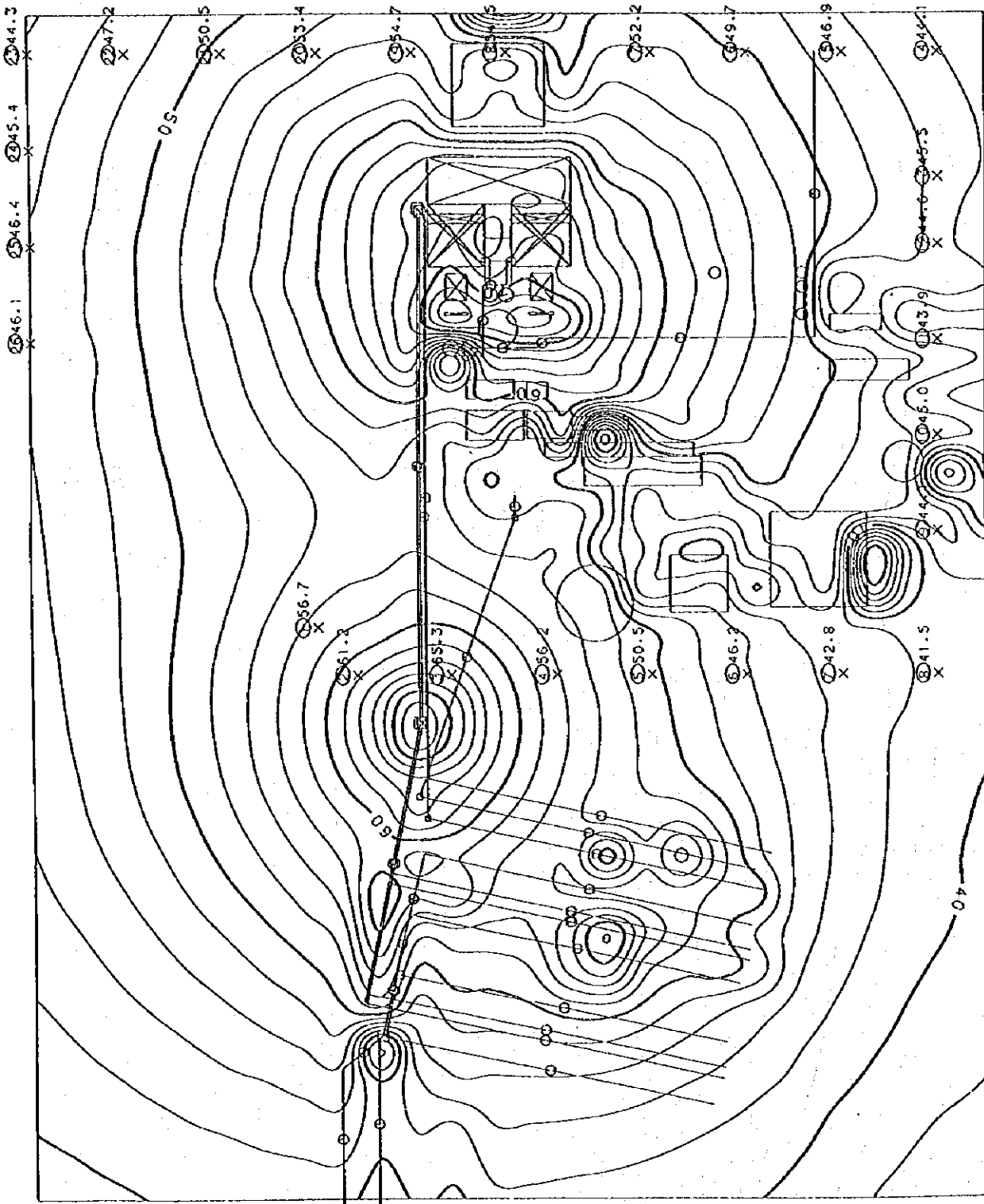


Figure 9-3-2-1b Contour Map based on replaced equipment (Night)

9.4 Study of the Lake Water Temperature

Rozovkladenetz lake is located near the Maritsa East No.1 Thermal Power Plant. As it supplies the water for the power generation and receives the discharge water from the power plant, its water temperature is expected to rise. Therefore, the study of lake water temperature was carried out. Consequently, the applicability of the Rozovkladenetz lake water as a condenser cooling water source has been evaluated based on the results of actually measuring the lake water temperature, and executing the diffusion analysis of warm waste water and so forth. At the same time, the impact of warm waste water upon the aqueous environment has also been assessed.

9.4.1 Measurement of Lake Water Temperature

(1) Measurement Period

Summer : 27 Jul., 1995 ~ 29 Jul., 1995

Winter : 5 Dec., 1995

(2) Measurement Points

Nine Points (Refer to Figure 9-4-1-1)

(3) Measurement Profile

The measurement profile at Rozovkladenetz lake is shown in Figure 9-4-1-2. The maximum depth is about 7 m.

(4) Measurement Result

(a) Summer (See Table 9-4-1-1)

The water temperature is within a range from 21.7 ~ 32.0 °C. Among the interlayer water temperatures, the water temperature in the surface layer is observed higher than that in other layers. The water temperature at the condenser cooling water discharge outlet also was higher than at other measurement points.

(b) Winter (See Table 9-4-1-2)

In winter, the water temperature is within a range from 8.2°C to 15.8°C and distributed roughly equally between the respective water layers. The temperature is observed higher at the condenser cooling water discharge outlet than that at the other measurement points.

According to the results of investigations, the water temperature tends to be higher at the condenser cooling water discharge outlet than other points as mentioned above. However, the distribution range of warm waste water is limited to the water area adjacent to the discharge outlet. Therefore, the Rozovkladenetz lake is evaluated to satisfy the requirements of a condenser cooling water source for cooling the existing power plant equipment.

The subsequent extent of the impact of this replacement project will be predicted through analysis of warm waste diffusion and so forth.

9.4.2 Prediction of Warm Water Distribution

The simulation and analyses of waste water diffusion have been carried out to predict the range of mixing and diffusion of warm waste water from the equipment under this replacement project.

(1) Simulated Condition

(a) Flow amount of discharged water

20.7 m³/s

(b) Discharged water velocity

2.02 m³/s

(c) Rising temperature

7°C

(d) Water temperature and Ambient temperature

| | <u>Water temperature</u> | <u>Ambient temperature</u> |
|-------------------|--------------------------|----------------------------|
| CASE - I (Summer) | 23°C | 26°C |
| CASE - I (Winter) | 0°C | 5°C |

(2) Calculation results

According to the results of calculation presented in Figure 9-4-1-2,3, there has been observed to be no impact of warm waste water upon the cooling water intake.

9.4.3 Estimating the Range of Warm Waste Water

The lake area to be required in case condenser cooling water under this reconstruction project is to be cooled only around the lake surface has been estimated based on the respective method presented in Table 9-4-1-3. According to the results of calculation, the lake area estimated to be required based on either of the respective methods is smaller than the Rozovkladenetz lake area. Since the calculated area is the effective area, therefore, it cannot necessarily be said that there is a sufficient allowance in the calculated lake area.

9.4.4 Assessment

The Rozovkladenetz Lake is an artificial lake built to acquire condenser cooling water for Maritsa East No.1 Power Plant. To study whether this lake has been functioning satisfactorily or not as a cooling water supply source, warm waste diffusion analysis and so forth have been carried out. As a result, there is concluded to be no problem regarding the function of the lake.

At the existing discharge outlet, a stone embankment has been provided presumably in anticipation of the increase in the amount of evaporation due to rise of water temperature and attaining uniform diffusion of warm waste water throughout the lake. Since the extend of the effect of this embankment has been unknown, such an effect is disregarded in this study. However, this embankment is considered to act further favorably.

Therefore, According to the results of study adopted the existing data, the implementation of this reconstruction project is evaluated to cause no lake water temperature rise. However, it is recommended to execute the following items;

- Since the precipitation is small around the proposed project site, the amount of lake water lost by evaporation should be made up with water from the rivers adjacent thereto.
- The discharge channel branched from the main discharge channel for fish culturing should not be used for discharging warm waste water in order to secure a sufficient separation between both of the discharge channels (Fish culturing should be carried out on the main discharge channel side.)
- The basic data (surface area of lake, bathymetric, meteorological data etc) should be reconfirm.

Where further extension project is to be planned after implementation of this reconstruction project, it will be necessary to carry out detailed studies regarding the cooling capacity of the lake after executing particularly accurate meteorological observation. In this case, it is recommended to install cooling towers as far as practicable, as seen in the case of the Maritsa East Nos.2 and 3.

Although a certain extent of impact of warm waste water upon the surrounding environment is predicted, the range of such an impact is limited to the area around the discharge outlet. Rather, fish raising has already been practiced by making effective use of warm waste water.

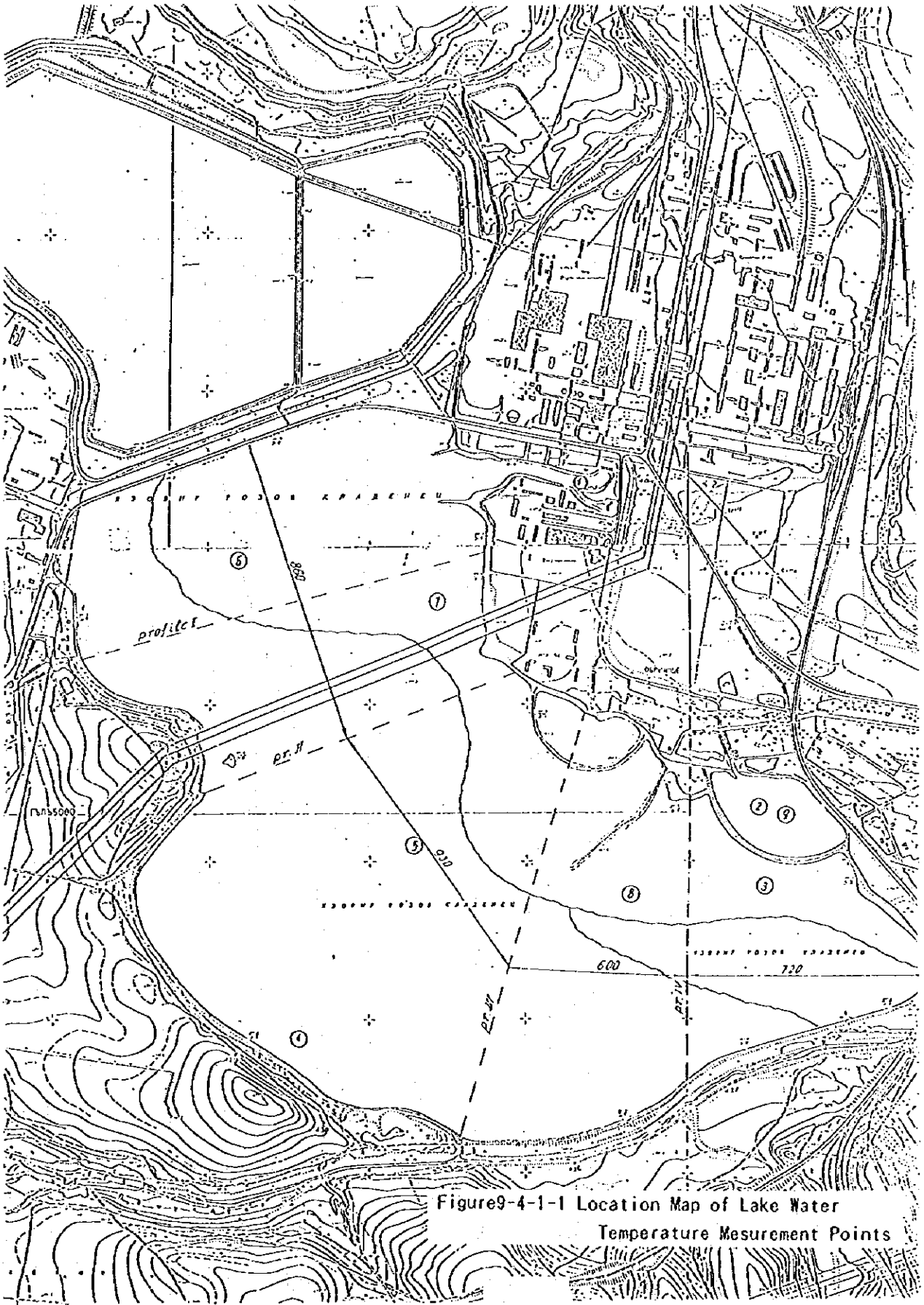


Figure 9-4-1-1 Location Map of Lake Water Temperature Measurement Points

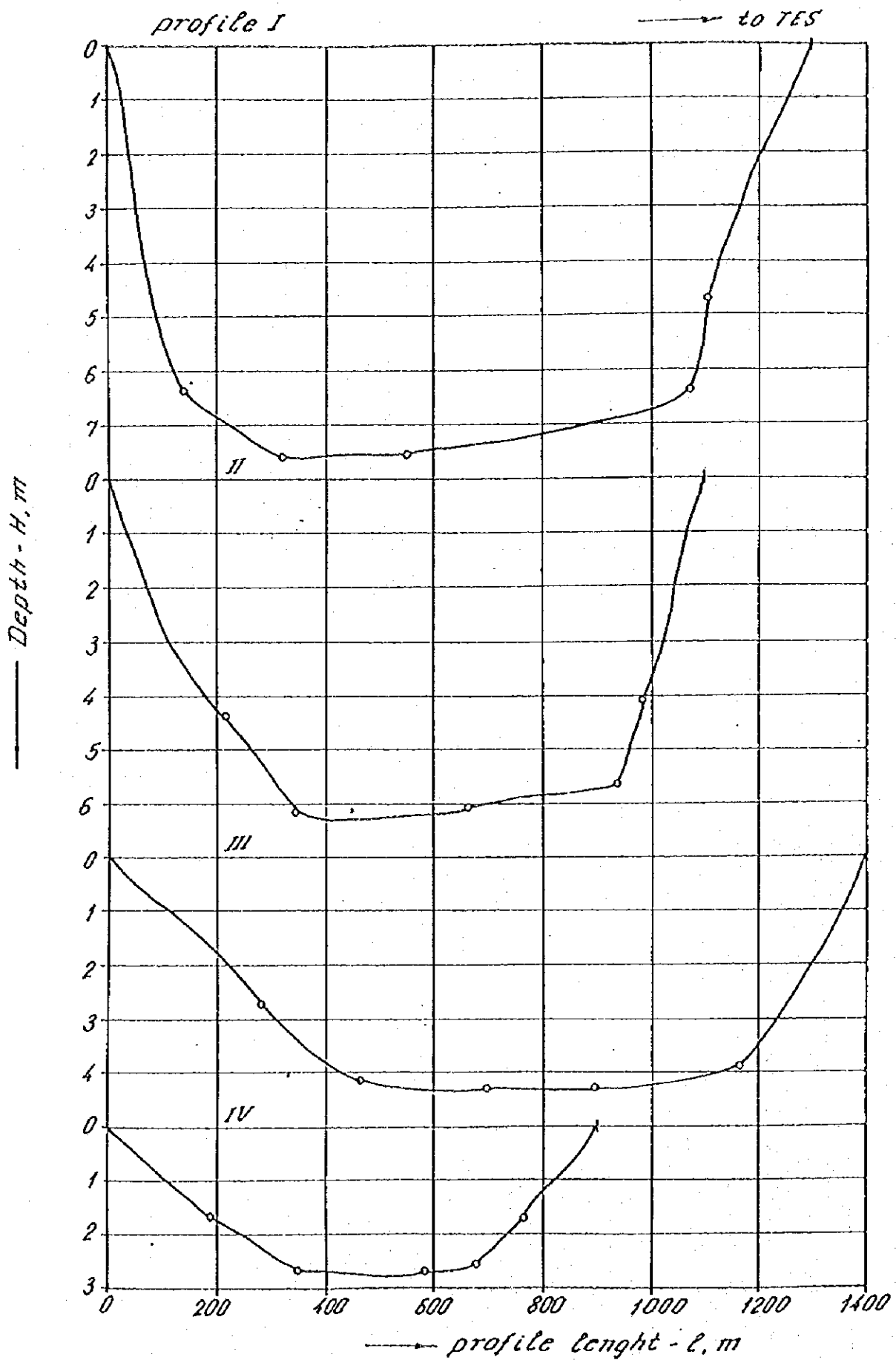


Figure 9-4-1-2 Measurement Profile at Rozovkladenetz Lake

**Table 9-4-1-1 Measurement Result of Lake Water Temperature
at Rozovkladenetz Lake**

| No. | Sampling Point | Temperature °C | Date of Measurement | Note |
|-----|--|--|------------------------|--------------------------------|
| 1 | 2 | 3 | 4 | 5 |
| 1. | Depth 0.1 m 1 m 2 m 3 m 4 m 5 m 6 m 7 m 7.5 m | 31.1 26.4 25.9 25.8 25.6 25.5 22.8 22.4 21.7 | 27.07.95 | Sunny 15-18 ³⁰ h |
| 2. | Depth 0.1 m 1 m 2 m 2.3 m | 32.0 31.8 31.7 31.7 | 29.07.95 | Cloudy 18-21 h |
| 3. | Depth 0.1 m 1 m 2 m 2.5 m | 30.0 29.2 27.3 27.1 | 29.07.95 | Cloudy 18-21 h |
| 4. | Depth 0.1 m 1 m 2 m 3 m 4 m 5 m 5.3 m | 28.7 28.0 27.2 26.8 26.0 25.6 25.4 | 29.07.95 | Cloudy 18-21 h |

| | | | | | |
|----|-------|---|--|----------|--------------------------------|
| 5. | Depth | 0.1 m 1 m 2 m 3 m 4 m 5 m 5.7 m | 29.3 28.8 26.8 26.3 25.4 24.7 24.0 | 29.07.95 | Cloudy 18-21 h |
| 6. | Depth | 0.1 m 1 m 2 m 3 m 4 m 5 m 6 m 7 m 7.5 m | 31.1 26.4 25.9 25.8 25.6 25.5 22.8 22.4 21.7 | 27.07.95 | Sunny 15-18 ³⁰ h |
| 7. | Depth | 0.1 m 1 m 2 m 3 m 4 m 5 m 6 m 7 m | 31.1 28.5 26.7 26.3 25.7 25.5 24.4 23.6 | 27.07.95 | Sunny 15-18 ³⁰ h |
| 8. | Depth | 0.1 m 1 m 2 m 2.2 m | 29.3 28.1 27.0 26.8 | 29.07.95 | Cloudy 18-21 h |
| 9. | Depth | 0.1 m 1 m 2 m 3 m 3.7 m | 32.5 32.2 32.2 32.2 32.1 | 29.07.95 | Cloudy 18-21 h |

**Table 9-4-1-2 Measurement Result of Lake Water Temperature
at Rozovkladenetz Lake**

| No. | Sampling Point | Temperature °C | Date of Measurement | Note |
|-----|---|--|---------------------|---|
| 1 | 2 | 3 | 4 | 5 |
| 1. | Depth 0.1 m 1 m 2 m 3 m 4 m 5 m 6 m 6.5 m | 9.3 9.2 9.0 9.0 9.0 9.1 9.2 9.2 | 05.12.95 | Cloudy 13-18 h Tair=2.6°C 5 boilers and 4 turbines work |
| 2. | Depth 0.1 m 1 m 1.5 m | 15.8 15.5 15.4 | 05.12.95 | Cloudy 18-21 h |
| 3. | Depth 0.1 m 1 m 1.5 m | 15.3 9.8 8.4 | 05.12.95 | Cloudy 18-21 h |
| 4. | Depth 0.1 m 1 m 2 m 3 m 4 m 4.5 m | 9.6 9.0 8.9 8.5 8.2 8.2 | 05.12.95 | Cloudy 18-21 h |

| | | | | | |
|----|-------|--|---|----------|--------------------------------|
| 5. | Depth | 0.1 m 1 m 2 m 3 m 4 m 4.5 m | 9.5 9.0 8.9 8.5 8.2 8.2 | 05.12.95 | Cloudy 18-21 h |
| 6. | Depth | 0.1 m 1 m 2 m 3 m 4 m 5 m 6 m 6.5 m | 9.9 10.4 10.5 10.5 10.5 10.4 9.9 9.8 | 05.12.95 | Sunny 15-18 ³⁰ h |
| 7. | Depth | 0.1 m 1 m 2 m 3 m 4 m 5 m 6 m | 10.3 9.3 9.0 8.9 9.1 9.2 9.2 | 05.12.95 | Sunny 15-18 ³⁰ h |
| 8. | Depth | 0.1 m 1 m 1.3 m | 14.9 8.5 8.3 | 05.12.95 | Cloudy 18-21 h |
| 9. | Depth | 0.1 m 1 m 2 m 2.8 m | 16.0 15.8 15.6 15.6 | 05.12.95 | Cloudy 18-21 h |

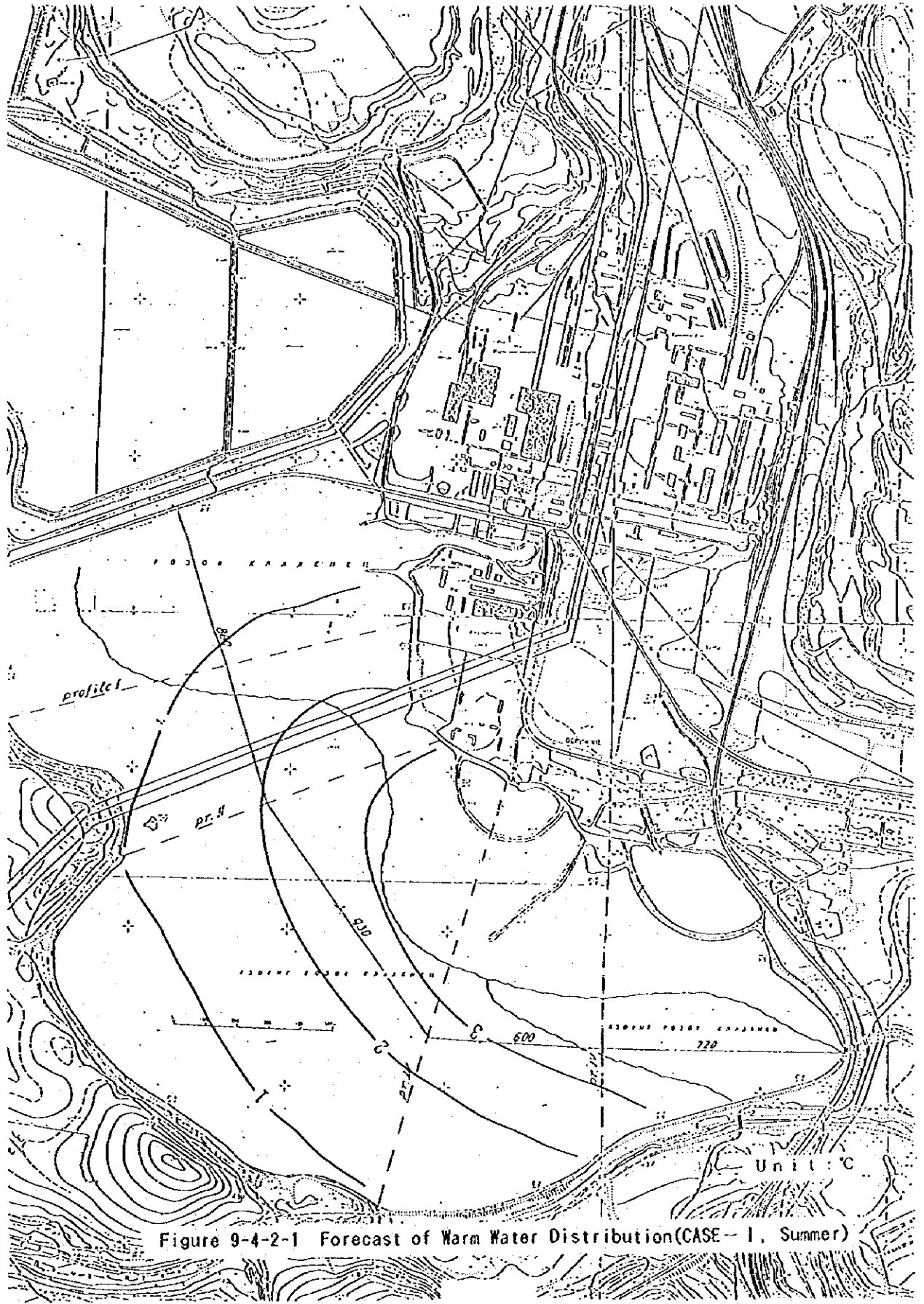


Figure 9-4-2-1 Forecast of Warm Water Distribution(CASE - I, Summer)

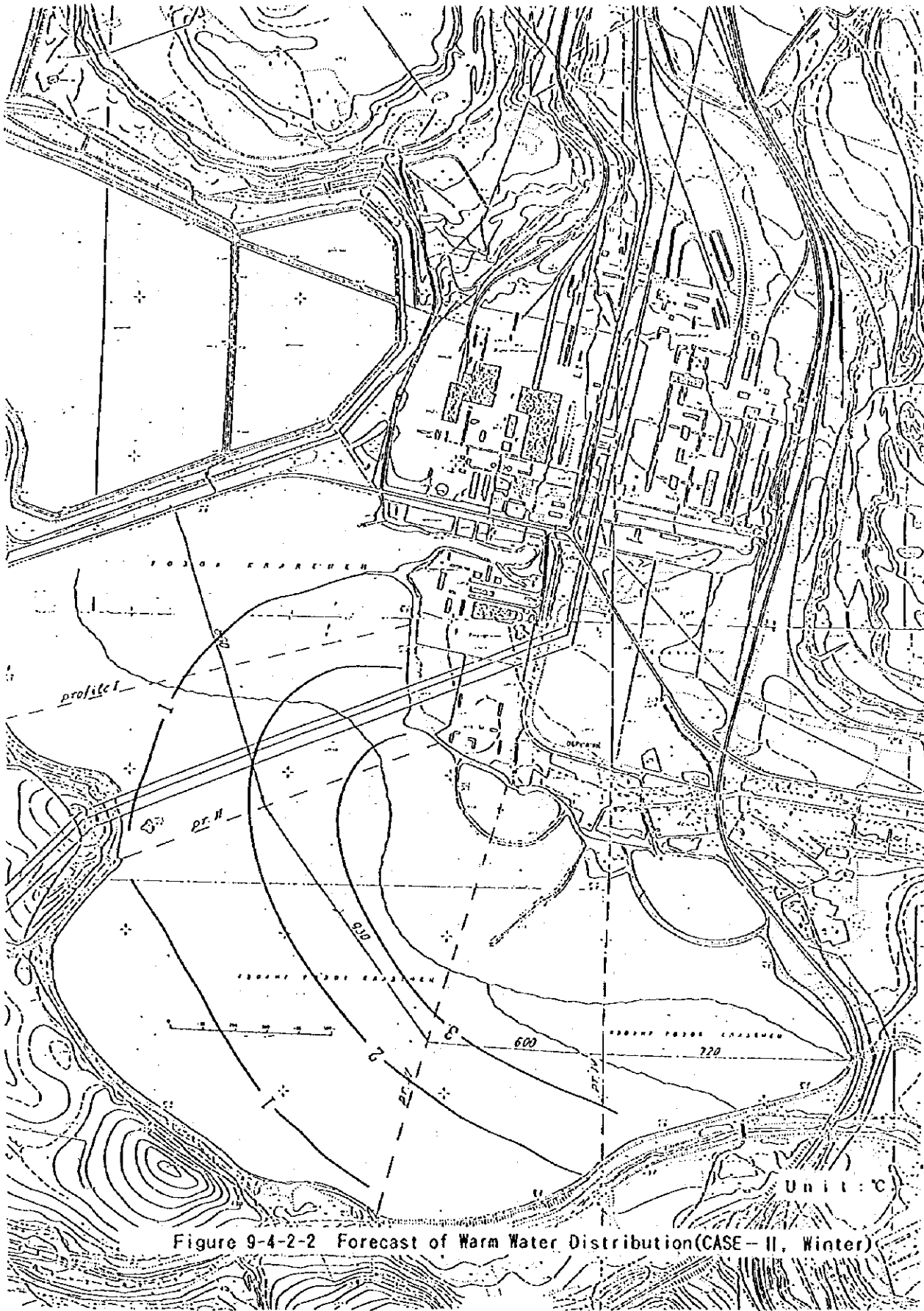


Figure 9-4-2-2 Forecast of Warm Water Distribution(CASE - II, Winter)

Table 9-4-1-3 Methods of Estimating The Range of Warm Waste Water

| Method | Description | Results | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
|---|---|---|---|---------------------|------------------------|---------------------|--------|------------|-----|--|-----|-----------------|------------|--------|------|------|------------|-------|-------|------------|------|--|--|-----------------|------------|--------|------|------|--------|-------|-------|------------|------|------|
| 1. Method based on actual measurement values, etc (The Japan Society of Civil Engineers) | <ul style="list-style-type: none"> Values estimated based on the results of predicting the distribution of warm waste water diffusion, and those estimated based on the results of prediction from experiment of numerical values. Estimation based on the discharge rate of 20m³/sec. Estimation based on the intake and discharge water temperature difference of 7°C. | Warm waste water diffusion : 130ha (<360ha) Equivalent radius : 0.91km (<1km) ※The surface area of the Rozovkladnetz = 360ha The distance between intake and discharge channels = 1 km | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 2. Method based on empirical formula (Formula of Nitta) | <ul style="list-style-type: none"> The range of impact is estimated by replacing the difference of warm waste water density with a water temperature difference according to an empirical formula induced based on the results of study regarding the diffusion of fresh water. | 216ha (<360ha) ※Flow amount of discharged water = 20.7m ³ /s | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 3. Method based on energy balance (Electricity Authority of The United Kingdom) | <ul style="list-style-type: none"> The range of impact is estimated of exhaust heat from a power plant per unit time is equal to the value obtained by integrating the amount of heat lost per unit area with respect to an overall water temperature rise area. | 290ha (<360ha) ※Flow amount of discharged water = 20.7m ³ /s | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 4. Method based on evaporation heat (Thermal and Nuclear Power Engineering Society) | <ul style="list-style-type: none"> The range of impact is estimated on the assumption that warm waste water is cooled by the evaporation heat based on the amount of water evaporated from the surface of a pond. <table border="1" style="margin-left: auto; margin-right: auto;"> <thead> <tr> <th></th> <th>Ambient Temperature (°C)</th> <th>Humidity (%)</th> <th>Water Temperature (°C)</th> <th>Wind Velocity (m/s)</th> </tr> </thead> <tbody> <tr> <td>Summer</td> <td>23</td> <td>65</td> <td>26</td> <td>2.5</td> </tr> <tr> <td>Winter</td> <td>0</td> <td>83</td> <td>5</td> <td>3.5</td> </tr> <tr> <td>Yealy mean</td> <td>12</td> <td>73</td> <td>18</td> <td>2.5</td> </tr> </tbody> </table> | | Ambient Temperature (°C) | Humidity (%) | Water Temperature (°C) | Wind Velocity (m/s) | Summer | 23 | 65 | 26 | 2.5 | Winter | 0 | 83 | 5 | 3.5 | Yealy mean | 12 | 73 | 18 | 2.5 | <table border="1" style="margin-left: auto; margin-right: auto;"> <thead> <tr> <th></th> <th>At wind blowing</th> <th>At no wind</th> </tr> </thead> <tbody> <tr> <td>Summer</td> <td>21ha</td> <td>49ha</td> </tr> <tr> <td>Winter</td> <td>132ha</td> <td>309ha</td> </tr> <tr> <td>Yealy mean</td> <td>35ha</td> <td>83ha</td> </tr> </tbody> </table> (<360ha) ※Flow amount of discharged water = 20.7m ³ /s | | At wind blowing | At no wind | Summer | 21ha | 49ha | Winter | 132ha | 309ha | Yealy mean | 35ha | 83ha |
| | Ambient Temperature (°C) | Humidity (%) | Water Temperature (°C) | Wind Velocity (m/s) | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Summer | 23 | 65 | 26 | 2.5 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Winter | 0 | 83 | 5 | 3.5 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Yealy mean | 12 | 73 | 18 | 2.5 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | At wind blowing | At no wind | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Summer | 21ha | 49ha | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Winter | 132ha | 309ha | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Yealy mean | 35ha | 83ha | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 5. Method based on heat exchange between the water surface and atmosphere (Power Plant Sytem Design) | <ul style="list-style-type: none"> The diffusion range is predicted based on heat exchange between the water surface and atmosphere. The calculation conditions are assumed to be the same as those mentioned above. <table border="1" style="margin-left: auto; margin-right: auto;"> <thead> <tr> <th></th> <th>Amount of daily solar radiation (cal/cm² · day)</th> </tr> </thead> <tbody> <tr> <td>Summer</td> <td>552</td> </tr> <tr> <td>Winter</td> <td>126</td> </tr> <tr> <td>Yealy mean</td> <td>339</td> </tr> </tbody> </table> | | Amount of daily solar radiation (cal/cm ² · day) | Summer | 552 | Winter | 126 | Yealy mean | 339 | <table border="1" style="margin-left: auto; margin-right: auto;"> <thead> <tr> <th></th> <th>At wind blowing</th> <th>At no wind</th> </tr> </thead> <tbody> <tr> <td>Summer</td> <td>21ha</td> <td>49ha</td> </tr> <tr> <td>Winter</td> <td>132ha</td> <td>309ha</td> </tr> <tr> <td>Yealy mean</td> <td>35ha</td> <td>83ha</td> </tr> </tbody> </table> (<360ha) ※Flow amount of discharged water = 20.7m ³ /s | | At wind blowing | At no wind | Summer | 21ha | 49ha | Winter | 132ha | 309ha | Yealy mean | 35ha | 83ha | | | | | | | | | | | | |
| | Amount of daily solar radiation (cal/cm ² · day) | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Summer | 552 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Winter | 126 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Yealy mean | 339 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | At wind blowing | At no wind | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Summer | 21ha | 49ha | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Winter | 132ha | 309ha | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Yealy mean | 35ha | 83ha | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |

9.5 Environmental Preservation Plan

9.5.1 Basic Items of Requirements

To prevent or mitigate the environmental impact resulting from implementation of this project, countermeasures should be taken to preserve the environment.

9.5.2 Countermeasures for Preventing Air Pollution

The basic concept of the countermeasures for preventing air pollution caused by flue gas discharged from thermal power plant is to reduce the amount of emissions by taking various countermeasures ; reduction of the amount of sulfur oxides by desulfurizing characteristic in a circulating type fluidized bed combustion boiler, nitrogen oxides by low temperature the combustion in the same boiler, dust by adoption of electrostatic precipitator and other means.

9.5.3 Countermeasures for Prevention of Water Pollution

To reduce the amount of the water pollution load to lakes and rivers as much as practicable, countermeasures should be taken as appropriate to treat general waste water from power plant.

9.5.4 Noise Preventive Countermeasures

Although the regulations pertaining to the noise control standards in Bulgaria have not been clarified, a priority is given for reducing the noise level in the working environment of workers rather than the noise level at the border of power plant. When the service life of power plant is taken into account, however, the noise control regulation is predicted to be strengthened certainly during the service life, where any noise preventive countermeasure is to be taken after occurrence of trouble, the modification cost and work for noise reduction will become extraordinarily extensive.

Therefore, appropriate noise preventive countermeasures should preferably be taken by indoor installation of equipment causing noise, adoption of low noise type for equipment installed outdoors, and installation of noise insulation wall and silencer as required.

9.5.5 Countermeasures for Prevention of Vibration

To reduce the vibration level at the border of the power plant according to the relevant environmental standards, any equipment constituting a vibration source should be separated sufficiently from the border of the site, and sufficiently firm foundation be adopted for any

such equipment. In addition, other appropriate vibration preventive countermeasures should be taken as required.

9.5.6 Countermeasures for Preventing Settlement of Ground

Any ground water should not be pumped up to prevent differential settlement of ground.

9.5.7 Countermeasures for Preventing Offensive Odor

Any such chemical as causing offensive odor should not be used.

9.5.8 Countermeasures for Warm Water Discharge

Rising temperature, which is the water temperature difference between intake water and discharge water, will be of 7 °C less. The countermeasures pertaining to intake and discharge of cooling water have been considered to minimize its impact upon aquatic life in lake water area.

9.5.9 Countermeasures for Disposal of Industrial Wastes (Coal ash)

Any coal ash and other industrial wastes should be disposed of by land reclamation at the existing coal disposal yard or other specified ash disposal site. Moreover, the portion of the fully reclaimed yard should be covered with soil to prevent dispersion of coal ash.

9.5.10 Countermeasures to be Taken during the Reconstruction Work

During the reconstruction work, sufficient countermeasures should be taken to prevent air and water pollution in the surrounding area. In addition, noise and vibration preventive countermeasures should be taken as required to reduce the noise and vibration levels by using sound insulation cover, selection of appropriate low noise or low vibration equipment and so forth.

9.5.11 Others

- (1) For preservation of the historical remains existing within the compound of the power plant, appropriate countermeasures should be taken under instructions of the relevant authority. In addition, equipment arrangement and reconstruction work should be carried out so carefully as to eliminate any adverse effect upon the historical remains.

- (2) To ensure harmony with the surrounding environment, planting should be carried out within the compound of the power plant.

9.6 Environmental Monitoring Plan

9.6.1 Basic Environment Monitoring Plan

To reinforce the monitoring system for preservation of environment, installation of monitoring equipment has been promoted in Bulgaria.

In consideration of such situations, an appropriate environment monitoring plan will be formulated regarding air pollution, water pollution and so forth.

9.6.2 Smoke and Dust

On the basis of a basic policy for smoke and dust emission monitoring, the concentrations of SO_x, NO_x dust and CO should be measured periodically after installing measurement seats in the boiler flue (Refer to Figure 9-6-1).

In the future, it is desirable to perform regular monitoring in the central control room by installing continuous measuring instruments, and constantly monitor the flue gas conditions at the chimney outlet by installing industrial TV sets at the same time.

9.6.3 General Waste Water

As a means of monitoring the quality of general waste water causing water pollution, pH value and turbidity should be measured periodically to check the water quality at the outlet of waste water treatment equipment to be installed in the power plant. In the future, it is desirable to continuously measure the quality of waste water by using automatic measuring instruments.

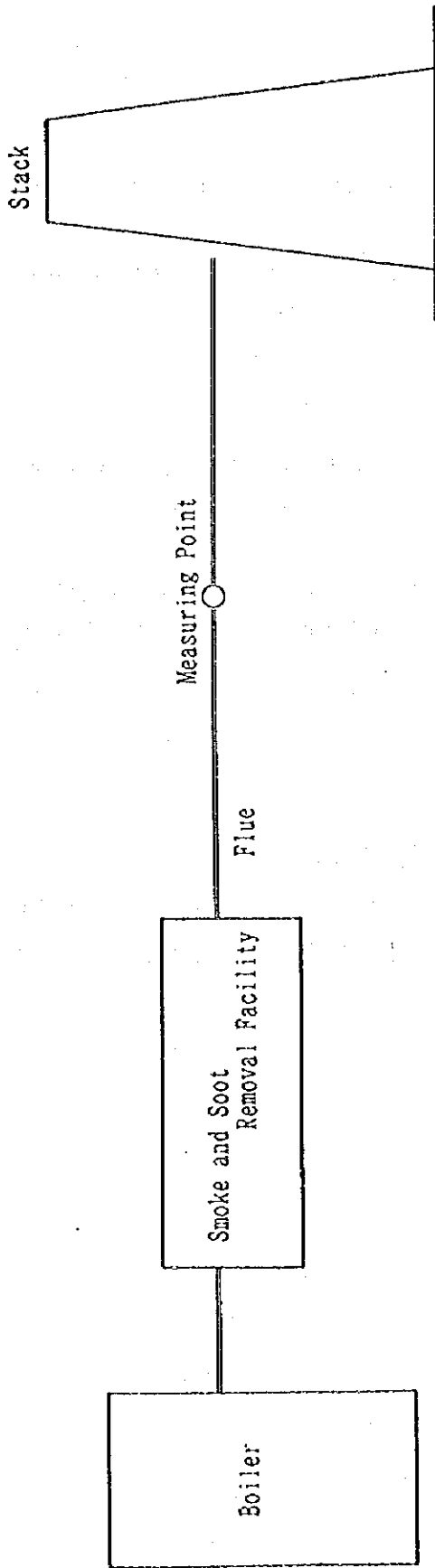


Figure 9-6-1 SO_x, NO_x, Dust and CO Monitoring System

9.7 Overall Evaluation

The Maritsa East No. 1 Thermal Power Plant Reconstruction Project is intended to bear a part of the burdens of future electric power supply in Bulgaria and make effective utilization of lignite, only a domestic energy source available in the country.

The reconstruction project should be implemented to ensure thorough preservation of the natural and social environment in the surrounding area.

In other words, the amount of smoke and dust emitted from the power plant should be reduced to a minimum possible extent by installing the flue gas desulfurization equipment, electrostatic precipitators and other equipment. To prevent water pollution caused by discharge of waste water, moreover, general waste water should be treated appropriately by adopting waste water treatment and other equipment. The countermeasures for reducing the noise and vibration levels from any equipment constituting such noise and vibration sources should be taken by indoor installation of equipment, adoption of low noise equipment, adoption of firm equipment foundations and so forth.

In addition to the above, such miscellaneous countermeasures as described herein should be taken. Thereby, it is considered possible to reduce the impact of the Maritsa East No. 1 Thermal Power Plant Reconstruction Project upon the surrounding environment.

After completion of the reconstruction project, the total amount of dust and sulfur oxide emissions will be reduced to much smaller than the present levels. In parallel with promotion of home electrification and regional heat supply, it is predicted possible to reduce environmental pollution resulting from burning of coal (Briquette) used as a domestic heat source.

Therefore, this reconstruction project is concluded to contribute highly significantly for improving the environmental quality in the surrounding area.

CHAPTER 10. ECONOMIC EVALUATION AND FINANCIAL EVALUATION

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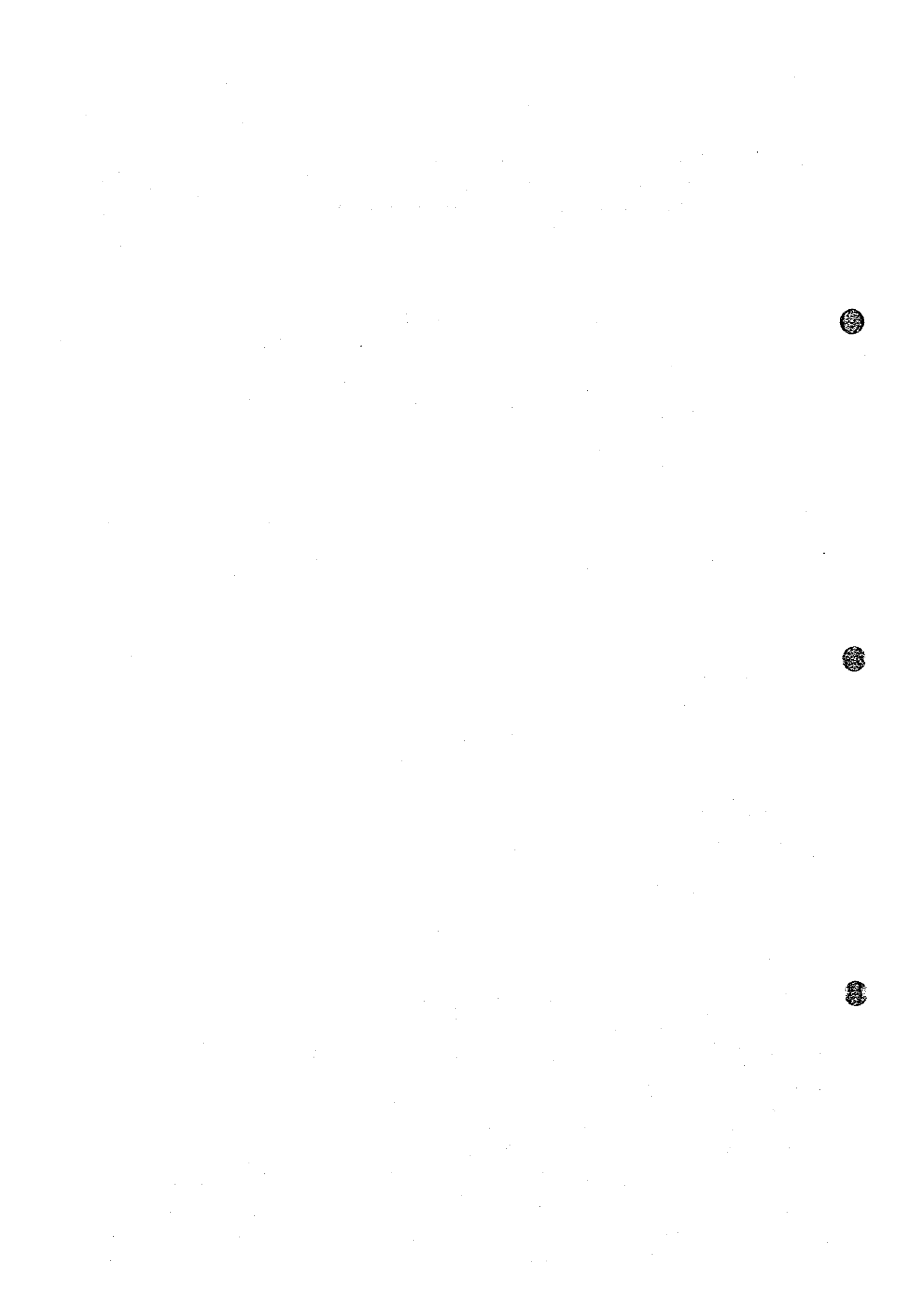
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10-1-1-1 Flow Chart of Economic and Financial Evaluation



CHAPTER 10 ECONOMIC EVALUATION AND FINANCIAL EVALUATION

10.1 Economic Evaluation

10.1.1 Methodology

(1) Basic approach

The economic evaluation of the project is made on the bases of indexes such as (1) net present value, (2) benefit/cost ratio and (3) economic internal rate of return (EIRR) of the project. These indexes are derived from the economic benefit and economic cost of the project. These indexes themselves are determined using so-called "Discounted Cash Flow."

When the market prices of the goods and services are determined directly and totally based on their actual economic values, such market prices can directly be applied to the calculations of the costs and benefits for the purpose of the economic evaluation of the project. However, in most instances, the market prices deviate from their actual economic values due to the effect of imperfect market mechanism.

The estimations of cost and benefit are primarily designed to serve the purpose of the optimum allocation of the limited resources. Thus, in order to attain this purpose, the given market prices of goods and services should be converted to their actual costs and benefits which reflect their actual economic values. For this reason, the World Bank and other international financing organizations estimate the project prices and market prices on the bases of international market prices.

On the other hand, economic evaluation for a development project is carried out measuring "its socio-economic impact on the country" by comparing two cases; the project is developed and the project is not developed. As a rule, development project may result in waking an alternative project not realized due to consumption of limited economic resources for this awarded project. Therefore, a selected project gives an impact on the country not only in producing its product but also in consuming limited resources.

In this regard, an alternative equipment approach is applied to this project. If a project is incorporated in a long term electric power development policy to satisfy future power demand (i.e., if the project is not to be implemented, another means of supply is to be substituted for it), an alternative equipment approach will be employed to measure and evaluate economic costs of the proposed project and the alternative project.

(2) Method of economic evaluation

In general, the method of economic evaluation adopted by the international financing organizations including the World Bank consists of the following phases:

Phase-1: Excluding the (items transferred to) domestic income

Phase-2: Converting a market price into a calculated price by the category such as foreign trade goods, Non-foreign trade goods, skilled labor and skilled labor

Phase-3: Determining an economic internal rate of return based on calculated price, and comparing it with an opportunity cost of the capital in the country concerned

Phase-4: Making socio-economic evaluation of the project, taking into account the national saving and distribution of income, based on the above result

The economic evaluation of the present project is made by the processes including phase 4. (See Fig. 10-1-1-1)

In general, when the calculation of the benefit is possible, the economic evaluation of a electric power development project is made primarily by measuring for comparison the benefit and cost attributed to this project itself, based on the Long-Range Marginal Cost (LRMC) method or the tariff system.

The cost-benefit is calculated for comparison as follows :

a) Cost

All the costs accruing during the term of the project should be added except the following transfer items.

- Taxes and Public Rates

The expenditures falling under this category will not reduce the resources available for the development of national economy at all. Since the economic calculation of the project aims at optimum allocation of the economic resources, the expenditure such as tax payment, which is a transfer of the economic resources and not the expense for consumption, should be excluded from the calculation of the cost.

1) Interest

The economic benefit can be considered to be an opportunity cost of the invested capital. The opportunity cost of the capital is a result of economic calculation and this cost itself includes the interest on the borrowing. Thus, the interest paid or payable should be excluded from the calculation in order to prevent the duplication of the calculation.

2) Depreciation cost

In the economic calculation, the costs are calculated on accrual basis. The depreciation cost accrues from the equipment investment and will not be calculated during the term of construction work but after the completion of the construction work in terms of accounting. Furthermore, the depreciation cost is calculated as the cost not requiring the expenditure of the fund.

Moreover, the capital cost is included in the category of the cost, and so reckoning the depreciation cost will result in duplicate entry of the cost. For this reason, the depreciation cost should be excluded.

3) Repayment of borrowing

Borrowing, like a tax, is a transfer cost and not a consumption cost, and so the borrowing should be excluded from the calculation.

b) Benefit

The cost of an alternative power plant is regarded as a benefit of the proposed project. For instance, executing a proposed project will give an impact on national economy by consuming the resources which would be consumed for the alternative project, accordingly the cost or resources which would be consumed for the alternative project can be considered to be a benefit of the proposed project.

In calculating the cost-benefit as described above, the following concepts of (c) present value and (d) economic costs should be taken into account. Figure 10-1-1-1 shows the calculation flowchart for this cost-benefit.

c) Present value

In making economic calculations, all the costs-benefits are estimated only at their present values. Therefore, they must be converted into present values using a discount rate.

d) Economic cost (Shadow price)

In general, project cost is estimated based on the actual or current price prevailing in the market of a country (market price). Market prices are usually distorted and to exclude this distortion, the market price is converted into a shadow price. The shadow price system is applied to all the costs of the project.

Costs of the project are divided into two categories: tradable goods and non tradable goods. As for tradable goods, importable goods are taken at their CIF price, and exportable goods are taken at their FOB price. Non tradable goods are taken at opportunity cost which is equivalent to the international market price.

In order to simplify the process, the standard conversion factor (SCF), determined from the total value of major exports (FOB) and imports (CIF), is used as a general indicator to avoid distorting domestic prices and to convert these prices of non-tradable goods into international market prices.

In making these economic evaluations, the most recent economic data are well used to calculate a standard conversion factor (SCF) and to convert the prices of non-tradable goods into international market prices. The SCF is obtained by the following calculation formula:

$$SCF = \frac{CIF + FOB}{CIF + TAX(import) + FOB - Tax(export) + Subsidies}$$

As shown above, economic evaluations are made by the following indexes after having converted the cost-benefit into shadow prices :

The details are as follows.

e) Economic evaluation

- Net Present Value (Benefit-Cost)

$$\sum \frac{B_n}{(1+i)^n} - \sum \frac{C_n}{(1+i)^n} = \text{Net present value}$$

where,

B: benefit, C: cost, i = Opportunity cost of capital, n = period (years)

[Note] A higher present value indicates better conditions of a project.

- Ratio of benefit to cost (benefit/cost)

$$\frac{\sum \frac{B_n}{(1+i)^n}}{\sum \frac{C_n}{(1+i)^n}} = \text{Cost/Benefit Ratio}$$

(Remarks)

The bigger the Cost/Benefit Ratio is, the better the Project is.

- Economic Internal Rate of Return (EIRR)

$$\sum \frac{B_n}{(1+i)^n} = \sum \frac{C_n}{(1+i)^n}$$

- i: Internal Rate of Return is the rate which offers that the accumulated Present Value benefit and accumulated cost are the same.

(Remarks)

- If EIRR is higher than opportunity cost; the better the Project is.
- If FIRR is higher than interest rate, the better the Project is. (FIRR is described in the next chapter 10.2 in detail.)

(3) Selection of alternative power plant

The recent energy development plan of Bulgaria is considered to stress priority on the following points:

- A high priority is given to the measures for saving the consumption of energy for both the industrial and civil uses under the current pressing condition of supply-demand of electric power.
- Extension of service lives of existing and currently operating cogeneration plants of heat supply and corresponding improvement of measures for the conservation of environment.
- Construction of new lignite-fired thermal power plants with environmental facilities by increasing the output of the lignite as domestically available energy resource or extension of the service lives of existing ones measures in view of national security with respect to the stable supply of energy and national defense.

- d) Necessity of constructing coal-fired thermal power plants to introduce and operate imported coal thermal power plants or combined cycle gas turbine power plants to a certain extent in parallel with the construction of lignite-fired thermal power plants using the domestically available lignite, as part of the country's electric power development plan.
- e) Considering the feasibility of constructing other atomic power plants for stable supply of electric power in the future, though it should be preceded by the repairing and restoration of existing Kozloduy nuclear power plant.

As the power supply for the base load, this project is proposed to construct alternative coal-fired thermal power plants which can offer equivalent services in view of these economic evaluations.

After consultations with NEK, it is decided from the viewpoint of economic evaluations of the Maritsa East R1 and R2 units that imported coal-fired thermal power plants will be constructed as alternative project to them.

10.1.2 Economic Cost of Project

The economic cost of the proposed project can be obtained by applying the conversion factor given above on the basis of the financial cost obtained in "Chapter 8.2, Construction Cost", excluding the interest which may be yielded during the construction works.

On the basis of the "Chapter 5, Optimum Development Plan", this project is designed to supply electricity for power plant and centralized regional heating. The heat are supplied only in winter, so that their cost is included in the power plant cost and not itemized in this project.

According to the construction schedule, there are 6 months time lag between R1 and R2 unit. However, in economic calculation, it is assumed that R1 and R2 units are to be commercial operation from January 2002.

(1) Investment cost

In the economic cost required for the construction works are included the direct construction cost, physical contingency, and engineering cost without taking into account possible inflations during the construction works.

In general, the economic cost due to the expropriation of a land used as the power plant site is compensated by the product given at the sacrifice of such a land. In the present project, this

product can be considered to be very small in comparison with the total economic cost of the construction works, judging from the use of the planned replacement land. Therefore, it is not included in the investment cost.

The foreign currency portion in the construction cost of the present project is given in CIF price. In calculating the domestic currency portion, it is usual to take into account controls on raw material prices, governmental subsidies or regulations. This rule is also applied to Bulgaria to calculate the economic cost of the domestic currency portion after consulting with NEK. As a result, standard conversion factor (SCF) of 0.97 was determined.

Tables 10-1-2-1 and 10-1-2-2 give the market and economic costs incurred by the present project.

(2) Operation and maintenance cost (O&M Cost)

The O&M cost is obtained by multiplying the economic cost of the construction works by a certain maintenance cost rate (4%).

(3) Fuel cost

The lignite coal used as the fuel for the present project is procured from the north lot of Troyanovo coal mine in Maritsa East Complex.

The fuel cost is calculated by multiplying the lignite-coal price (on the basis of coal price at 6.0 US\$/ton as in January, 1996) by the annual consumption of coal.

This method is used to calculate the initial investment cost as the cost flow to estimate the project from economical point of view and the total economic cost incurred throughout its whole life of the project.

10.1.3 Parameters and Economic Cost of Alternative Thermal Power Plant

As mentioned before, an imported coal fired thermal power plant was assumed as the alternative facility with which the economic benefit of this project is calculated.

The economic cost of the alternative thermal power plant is regarded as one of the benefits to be offered by the present project and is compared with the economic cost of the project.

The alternative thermal power plant as the basis of the economic evaluation is supposed to be constructed at the location inland from Black Sea and nearest to the Maritsa East project site.

The basis conditions and factors adopted to economically estimate this thermal power plant are given in Tables 10-1-3-3 and 10-1-3-4. Table 10-1-3-4 also gives the conditions applied to calculate the economic cost for the Maritsa East No.1 Power Plant project.

(1) Initial investment cost for the alternative thermal power plant

The economic cost for the alternative thermal power plant is divided into foreign currency and domestic currency portions. The latter portion is calculated using the standard conversion factor. Tables 10-1-3-1 and 10-1-3-2 give the initial investment of the project and the total cost throughout its whole life in relation with its market and economic costs.

(2) Operation and maintenance cost (O&M Cost)

The O&M cost is calculated by multiplying the total economic cost of the project by a factor of 4%.

(3) Fuel cost

The imported fuel coal is supposed to be procured from international market at its most economic price on the following conditions:

Fuel cost was calculated by multiplying annual energy consumption by the cost of imported coal and cost of heavy oil (Coal: 60.00US\$/ton).

In this method, the initial investment of the project and the total economic cost throughout the whole life of the project is calculated as the benefit flow to evaluate the alternative thermal power plant.

10.1.4 Economic Evaluation

On the basis of the flows of the benefits and costs calculated on the above-mentioned suppositions, the surplus of benefit (B - C), benefit/cost ratio (B/C) and equivalent discount rate (so called economic internal rate of return : EIRR) of the present project are calculated as given in Tables 10-1-4-1 and 10-1-4-2.

(1) Net present value and benefit/cost ratio

As indicated by the deux indexes of net present value (benefit - cost) and benefit/cost ratio (B/C), the construction, maintenance costs and fuel cost of the present project prove to be economically more advantageous than the alternative project.

(2) Economic internal rate of return

As shown by Table 10-1-4-2, the discount rate (namely, EIRR) is set to be 25.3% when the present value of the investment to the present project throughout its whole life becomes equal to that of the alternative thermal power plant in the first year of the project. This rate exceeds evidently the opportunity cost of capital set to 10%.

As described in Item (1) and (2), this project proves to be more advantageous than the alternative imported coal thermal power plant from economical point of view and can be said to be feasible enough judging from all index.

10.1.5 Sensitivity Analysis

The sensitivity of the proposed project is analyzed under the following conditions:

| | |
|--------|--------------------------------------|
| Case 1 | Increase by 20% in construction cost |
| Case 2 | Discount rate changed to 8%, 12% |
| Case 3 | Increase by 5% in fuel cost |

As a result, the EIRR, B-C and B/C resulting from these flows are shown in Table 10-1-5 and indicate the advantageous merits inherent in the present project.

10.2 Financial Evaluation

10.2.1 Methodology

In making the financial evaluation of the proposed project, a cash flow at market prices was developed for all costs of the project; direct construction cost, maintenance cost and fuel cost of the project.

This cash flow of these costs was compared with the cash flow of the benefit calculated based on the estimate of revenue deriving from the sales of electricity and heat for district heating, generated from this project, and then financial internal rate of return (FIRR) was calculated by the discount cash flow method (DCF method).

The discount rate was determined to be 10% through discussion with NEK. Table 10-2-2-1 shows basic conditions used for financial evaluation of this project.

10.2.2 Financial Cost of Project

Total amount of initial investment of this project was obtained on the bases described in "Chapter 8.2 Construction Cost". The operation and maintenance cost was determined to be 4% of construction cost.

From the above, total financial cost of initial investment and all life of project which is a cost flow for making financial evaluation of the project, was calculated. Table 10-2-2-1 shows the calculated costs.

10.2.3 Financial Revenue of the Project

The financial revenue of the project derives from the sales of electricity and heat for district heating. This revenue was calculated based on electricity tariff (4.5 cent/kWh) to be applied in 2001 to major cities and industrial areas such as Sofia and Ruse, which are considered to be MW class electricity consumption area located in the neighborhood of the project site. Likewise, the revenue of heat for district heating was calculated based on heat tariff (\$31.4/Gcal) to be applied to residences and factories in Maritsa East in 2001. Throughout the life of the project, (a) the average of annual generation of electric power is considered to be electric power which can be sold to consumers and (b) the amount of heat supplied for district heating was considered to be the amount of heat which can be sold. Table 10-2-3-1 shows the annual financial revenue calculated based on the above mentioned tariff.

10.2.4 Financial Evaluation

Table 10-2-4-1 shows the result of the financial evaluation. As shown in this table, the financial internal rate of return (FIRR) was calculated to be 8.8 %.

This FIRR is higher than the interest rate of 8% in terms of borrowing foreign currency. On the other hand, this rate is lower than the average interest rate of 10% in terms of borrowing foreign currency for both foreign and local portion from international financial organization (this interest can be considered to be opportunity cost of the capital). Thus, it is concluded that NEK should examine average unit electricity tariff so that the project can be more attractive under the same discount rate. NEK should also examine the condition of borrowing from international financial organization for decreasing necessary amount of fund.

10.3 Repayment Schedule of Borrowing

10.3.1 Basic Consideration and Condition

In general, construction of a power plant requires a huge amount of initial investment during the term of construction work. Furthermore, the return from that investment starts only after the construction work is completed. The period required for the recovery of the investment is much longer than those required for the investments in the manufacturing facilities of durable goods. Thus, it is natural for the investor to seek the borrowings available at lowest possible interest rate, with longest possible period of deferment of repayment and longest possible repayment term.

In Bulgaria, the interest rate itself reflects inflation and the domestic central base interest rate is extremely high. Thus, as a result of discussion with NEK about borrowing condition of the project, the conditions of other projects are taken into account and a repayment schedule was created on the premise that all necessary funds including foreign and domestic moneys were procured from international financial organizations.

Interest rate: Interest rate of international funds is 8% for foreign money and 10% for domestic money. In any cases, no commitment charge is included.

Repayment condition: Repayment during the term of construction work for the project is to be deferred.

The sum of the principal and interest is to be paid by equal installment in 20 years for foreign fund and 15 years for domestic fund.

10.3.2 Necessary Amount of Fund

The proposed project is scheduled to be incorporated into the existing electric power supply network in 2001. The amount of necessary fund including fund borrowed from international financial organization was estimated based on the prices as of January 1996.

At this time, inflation during the term of construction was not taken into account.

A rise of current inflation in Bulgaria is abnormally high and this brings to 32.9% for 1995. Estimating changes of exchange rate to dollar and other currencies, of Bulgarian currency, future prices were set on dollar basis for both foreign funds and domestic funds and a prospect of fund repayment flow was established.

Table 10-3-2-1 shows the schedule of borrowing and schedule of repayment.

10.3.3 Revenue and Cost

The revenue was calculated based on electricity tariff and heat tariff and the amount of electricity and heat which can be sold, obtained from estimation of its demand. The expenditure includes depreciation cost, fuel cost and operation/maintenance cost. Then, the balance of income and expenditure was considered.

(1) Revenue by sale

The investment is recovered by revenue derived from (1) sale of electricity and (2) sale of heat for district heating, which is supplied to Maritsa East area in winter.

Because it is difficult to estimate average electricity tariff and heat tariff for district heating in 2001, the electricity tariff to be applied to ordinary regions of Bulgaria, based on an estimation of the demand in this country is utilized.

The electricity tariff and heat tariff in 2001 was determined to be 4.5 cent/kWh and \$31.4/Gcal respectively as a result of discussion with NEK.

(2) Sales cost

The sales cost comprises operation/maintenance fuel cost and depreciation cost of the project. The annual O/M cost was estimated to be 4% of the construction cost.

Straight-line method was employed assuming that residual value was zero and the durable service life left was estimated to be 30 years.

10.3.4 Repayment Schedule of Borrowing

The source of fund to be appropriated for repayment of borrowing is supposed to be derived from the operating income [Sales of electricity and heat for district heating - Operation/Maintenance cost - (depreciation cost + interest paid)]. (Besides, the cash reserved by depreciation cost should be taken into account too.)

Tables 10-3-4-1 and 10-3-4-2 show cash flow statement and statement of profit and loss based on fund procurement, repayment condition and sales income/expenditure balance. As shown in Table 10-3-4-2, the investment cost will be recovered in the sixth year from the beginning of the operation. After that, income will exceed the investment cost, thereby producing profit.

10.4 Calculation Under the New Electric Tariff System

10.4.1 Present Situations of Electric Tariff and Their System

(1) Electric tariff

In Bulgaria there are two electric tariff systems, the systems to cover electricity for industrial use and the system to cover electricity for private use. Conventionally, electric tariff (end-user prices) and local heating tariff are approved by the government via Energy Committee.

Table 10-4-1-1 shows the current level of electric tariff.

Under the influence of domestic inflation and exchange rates resulting from the shift to the market economy which started in 1989, during the two years of 1994 and 1995 electric tariff was raised by 30% to 50% for home use, and 30% to 40% for industrial use.

Therefore, in November, 1994 the government decided to review the system intended to have the progress of inflation and the increase in costs reflected in the electric tariff as much as possible. Taking into account the variation in exchange rates, the progress of inflation, and changes in national incomes as the factors subject to adjustment, the cause of the repeated raise in electric tariff has been investigated.

In 1995 the average electric tariff per consumer type was 3.01 cent/kWh (approx. ¥3/kWh) for industrial use and 2.33 cent/kWh (approx. ¥2.3/kWh) for private use.

End-user prices are established and controlled through accumulation of the costs of individual power plants belonging to each local branch (Maritsa East No. 1 Power Plant Branch, etc.). However, since governmental subsidies are granted in various phases of establishing end-user prices so that the burdens on enterprisers and consumers may be eased, the electric tariff system as a whole is not considered as being based on the market price which reflects the costs involved (See Table 10-4-1-2).

In the current tariff system of the country, the tariffs to the end users are determined with political consideration and there is a big departure from the cost-based tariff systems.

The No.1 Maritsa East Power Plant is subjected to the cost control systems applicable to the regional branch of the company. The actual cost is reported to each regional office every 3 months, which are used as the basic data for the Government review of the electricity tariff. The total revenue in 1994 was 543,946,000 Lev (¥1,006 million) and the total cost of 1,081,849,000 Lev (¥2,001 million) was accrued, meaning that the region is not in a position to recover the cost.

The largest point of issue in the attempt of revising the current tariff system for 1994 onward is lack of a mechanism to collect long-term investment. From a static point of view there is no structure of well-balanced revenue and expenditure. In order to make a large-scale investment with a long-term capital to be loaned, a stable income base of a proper tariff system is needed. Therefore, an institutional problem at present is how to continuously reflect in the future electric tariff the capital expenses (interest and depreciation expenses) required for the intended proper investment.

We have not obtained the information regarding the new tariff systems which is said to be under review. If, for instance, the cost based pricing of each plant is adopted as is a standard for the Euro-American countries, special measures will have to be considered such as tax exemption for installation of environmental protection equipment or encouragement of foreign investment.

(2) Power generation costs

In NEK's statement of profit and loss, power generation costs and heat supply costs are not separately indicated.

For the details of cost items, refer to Table 10-4-1-2.

(a) Fuel costs

According to NEK, because of a sharp rise in coal prices the ratio of fuel costs to the total costs was raised by approx. 90% compared with that of 1992 although the amount of fuel consumption was slightly increased.

In view of the price liberalization expected to take place in the future, fuel costs may further rise.

(b) Repair and related costs

According to NEK, the costs of repairs both ordered to outside workshops and conducted within the organization were increased compared with those of 1992 owing to the rise in the prices of various machinery and materials. Although this is partly attributable to its decrepit equipment, this may have something to do with its insufficient capital to be invested in the renewal of the equipment as well as with the coefficient of utilization still being small.

Since regular inspections largely depend on the orders placed on outside workshops and, consequently, the expenses involved may be comparatively high.

(c) Personnel expenses

The manpower allocation at the No.1 Maritsa East Power Plant is shown in the chapter 2.1.2. The manpower related cost based on the price level in the year 2001 is estimated as follows.

Although the manpower plans for the R5 and R6 projects of the No.1 Maritsa East Power Plant is yet to be determined, NEK assumes 100 people including those for operations and maintenance of the existing No.5 and No.6 plants. By having more sophisticated replacing thermal plants, we believe that the manpower cost can be squeezed.

(d) Depreciation costs

The standards for depreciation are legally provided by the Ministry of Finance of the republic. Residual value is specified as zero, and depreciation ratios are separately specified for individual units and equipment.

Table 10-4-1-3 shows the outline of these standards.

As referred to in the previous chapter, in order to collect capital expenses for proper investment in the future, it would be necessary to consider a tariff system with depreciation costs reflected in tariff costs.

10.4.2 Consideration on the New Electric Tariff System and Its Effect

(1) Evaluation technique

This project is roughly divided into two parts, i.e. a) thermal power plant using lignite coal in accordance with the reconstruction plan and b) steam supply for heating. Profits will be obtainable in case electric tariff is established so that sales of electricity and steam for heating may cover the costs of investment, maintenance, and operation.

Based on the financial evaluation of chapter 10.2 and assuming the year 2001 standard electricity sales price for the cash balance calculation, a new tariff system will be reviewed as follows.

The electric tariff salable in the future will be the unit price sufficient to avoid a deficit in the net income, not the price with which to discuss the essence of the salable electric tariff. Accordingly, we have analyzed the cash flow in view of the financial evaluation and the profitability of the project. The basic assumptions used are two different unit prices which are

calculated from the current tariff as extended to the 5 years from 1996 through 2001 by two annual increasing rate of 5% and 11% respectively.

The tariffs for the years beyond year 2001 are assumed as follows. The same capital financing conditions as in the chapter 10.3.4 debts repayment schedule are used.

Case 1: Annual Rate 5% : Unit price for 2001 - 3.8 cent/kWh

Case 2: Annual Rate 11%: Unit price for 2001 - 5.0 cent/kWh

(2) The result of review

The cash flow analysis for each case of assumptions is demonstrated below.

1) In case the unit sale price is 3.8 cent/kWh:

The total annual amount of cash balance would mark a deficit for the period of 18 years but would turn out a surplus afterwards. In the final year of repayment to the financial institution the total surplus would be US\$35,208,000.

2) In case the unit sale price is 5.0 cent/kWh:

The cash balance for a single fiscal year would mark a deficit up to the 2nd year from the beginning but would turn out a surplus the next year onward.

In the case of electricity sales price of 3.8 cents/kWh, it is not advisable to balance the revenue and the cost and to repay the debt with the standard tariffs of electricity and steam fixed at the 2001 level without any change in future. This recommendation is based on the financial evaluation and the cash flow statement as well as the assumptions of 20- year repayment of foreign currency debts with 8.0% annual interest rate, and 15-year repayment of local currency debts carrying 10 % interest.

Thus, with the same financing conditions as above, the 5.0 cents /kWh case appears to be the most feasible level. Also, more favorable terms of borrowing must be negotiated with the international financial institutions in order to reduce the overall cost of procurement funds required.

10.5 Socio-Economic Influence

10.5.1 Outline

So far any certain method has not been established to evaluate socio-economic influence on macro basis by introduction of environmental equipment. It shall be pursued in the future.

Therefore, this chapter described some estimations made so far after it stated history of introduction of environmental technology in Japan and then estimated socio-economic influence by reconstruction of Maritsa East first thermal power plant in Bulgaria.

We have learned from our experience that there are the following possibilities for benefits and losses generated from introduction of environmental equipment.

(Benefits)

- Reduction of disease of the people
- Improvement of living, social and natural environment
- Economic growth and expansion of employment by investment for environmental equipment
- Decrease of the sum paid for the indemnity for healthy damage

(Losses)

- Rise of consumer price by addition of environmental cost and decrease of purchasing ability of the people

10.5.2 History of Introduction of Environmental Equipment in Japan

Since Japan promoted economic recovery and expansion of the production after World War II, GNP recovered in 1955 (10 years after 1945) to the same as the highest level before World War II. Average annual increase of GNP recorded 8.8% in the latter half of 1950's, 9.3% in the former half of 1960's and 12.4% in the latter half of 1960's. Economic growth had been triggered by export of industrial products and investment for production equipment. Since heavy chemical industry in which more environmental pollutant was discharged per unit production, environmental condition was getting worse in this period. However the portion of the investment for environmental protection in total capital investment of private sector was still low; around 3% in 1965.

Although some environmental laws were enacted after the latter half of 1950's, governmental position for environmental protection was still unclear at that period as seen in the example

that such clause as "the harmony between environmental protection and sound economic growth" was stipulated in the laws. No governmental authorities existed for integrate administration in the field of environmental protection.

Environmental pollution expanded in around 1970 all over the country, and it became the most serious social problem. A total of 14 new environmental laws were enacted and the clause of "to protect the environment in harmony with economic growth" was deleted from Environmental Organic Law. The Environmental Agency was established for the integration of the environmental administration in 1971. Since that period the movement for environmental protection promoted rapidly. In electric sector, its regulation system was arranged neatly. As a result, introduction of discharge substance suppression technology was accelerated, so that currently, flue gas desulfurizers have been introduced for mainly coal thermal power and high sulfuric heavy oil thermal power plants.

10.5.3 Examples of Estimate for Socio-Economic Influence by Introduction of Environmental Countermeasure

Although no concrete method for macro economical estimation on socio-economic influence by execution of environmental countermeasures has not been established yet as described in 10.5.1, some examples have been conducted. Thus, this section will describe two of them.

- (1) Comparison between the sum of damages from environmental pollution and the cost incurred from countermeasure for environmental protection

In a paper presented at the 1982 Tokyo conference of the Club of Rome, Professor Yoichi Kaya of the University of Tokyo offered a comparison between the amount of anti-pollution funds spent in one year to deal with sulfur oxides at their sources, such as plants, and the amount of damage estimated to result from pollution where there was a total lack of pollution countermeasures. This comparison was based on notably bold assumptions. As indicated by the tentatively calculated costs shown in Table 10-5-3-1, the total damage arising from the absence of anti-pollution measures (about ¥6 trillion, or \$45 billion, annually in 1976 prices) far exceeded the estimated actual costs of anti-pollution measures (about ¥80 billion, or \$3.7 billion, at 1976 prices).

- (2) Tentative statistics relating to the economic impact of anti-pollution investments

The impact on the economy of anti-pollution investments must be considered in terms of two major factors: namely, (1) the impact on prices, brought about by increased costs related to investments; and (2) the impact on income, induced by the increased demand for the anti-pollution products and services.

The first factor, the impact on prices, would vary according to the supply-demand relationship of the specific products. Nonetheless, cost increases due to investments in pollution control will have an effect on the prices of the particular products concerned. This, in turn, will affect the prices of the products consumed by the industries that manufacture goods using the particular products or parts in question as raw materials. This, furthermore, will affect the prices of the end consumer goods. When these prices rise, the demand for the various consumer goods will decline according to their price elasticities (rates of changes in demand according to price changes). This will result in a decrease in investment in plant and equipment in each industry, which in turn will lower its supply capacity.

The second factor, the significant impact on income will be that anti-pollution investments will become part of the cost of the industries making the investments, and at the same time will increase the demand for the products and services of the industries that receive the investments. Furthermore, the increased demand in the anti-pollution industries will expand the demand for materials and parts needed in investments relating to those industries, and will constitute a factor promoting investments in related industries and their capacity for supply.

As we have seen above, the effect of the first factor is to reduce the real GNP (i.e. price effect) and the second factor is to expand the real GNP (i.e. income effect).

The *Environment White Book* published in 1977 by Japanese Government focuses on these two effects and offers tentative statistics relating to the macroeconomics impact produced by the environmental measures taken during the decade between 1965 and 1975.

According to this document, the total private-sector investment in anti-pollution measures during this period was \$40 billion (about ¥5.3 trillion at 1970 prices). The following estimates for some economic indices were shown as the effect of the investment for the environmental equipment compared with the case where such investment had not been carried out.

10.5.4 Estimation of Socio-Economic Influence in Bulgaria

On the background of the above stated analysis, macro economic influences induced by introduction of environmental protection equipment for the reconstruction plant in coal thermal power plants in Bulgaria, are considered, regarding (1) changes of people's consciousness, (2) harm on people's health and other social cost, (3) impact on national economy, and (4) influence on surrounding countries by suppression of pollution diffusion, as follows.

(1) Review of electricity tariff system

Although cost relating to investment must be recovered by electricity tariff, the ratio occupied by electricity tariff is not so large. If appropriate cost recovery system is adopted, an effect of tariff reduction with a passage of time can be expected. Currently, Bulgaria is reviewing its electricity tariff system so as to include its money exchange rate to US dollar, inflational rate, and changes of fuel price in international market into its power generation cost.

Thus, it is possible to include environmental equipment cost in this review process accurately.

(2) Economic diffused influence and expansion of employment capacity can be expected due to increase of investment.

Although procurement of as many material as possible in the country is intended in achievement plan of this project as well, quite large economic diffusion effect and expansion of employment force such as expansion of GNP can be expected by domestic private and public organizations' achieving this production and distribution plan.

(3) Economic diffusion effect to export can also be expected.

From the viewpoints of technological standard of Bulgaria, it will not take so long time to absorb production and operation technologies of flue gas desulfurizer. Because Bulgaria applied for participation in EU in 1995, it is expected that installation and spreading of flue gas desulfurizers for new coal thermal power development and in existing power plant will be still greatly demanded. Thus, it is possible to position export of flue gas desulfurizers to other countries as a prominent goal for industrial growth, by making the best use of advantage of relative production cost of environmental protection equipment in the domestic country.

**Table 10-1-2-1 Initial Investment Cost of ME-1 Replacing Thermal Power Plant
(Market Price Basis)**

(Unit: 10³ US\$)

| Year | | 1 | 2 | 3 | 4 | Total |
|--------------------------------|----|---------------|----------------|----------------|----------------|----------------|
| Civil/Erection Island | FC | 18,600 | 13,000 | 15,500 | 14,900 | 62,000 |
| | LC | 24,700 | 17,300 | 20,500 | 19,700 | 82,200 |
| Boiler Island | FC | 0 | 76,800 | 96,100 | 19,200 | 192,100 |
| | LC | 0 | 13,600 | 17,000 | 3,300 | 33,900 |
| Turbine Island | FC | 0 | 36,000 | 45,100 | 9,000 | 90,100 |
| | LC | 0 | 6,400 | 7,900 | 1,600 | 15,900 |
| Coal/Limestone Handling Island | FC | 0 | 18,900 | 41,700 | 15,100 | 75,700 |
| | LC | 0 | 3,300 | 7,400 | 2,700 | 13,400 |
| General Expenses | FC | 2,000 | 6,000 | 6,000 | 23,000 | 37,000 |
| | LC | 0 | 0 | 0 | 3,000 | 3,000 |
| Total | FC | 20,600 | 150,700 | 204,400 | 81,200 | 456,900 |
| | LC | 24,700 | 40,600 | 52,800 | 30,300 | 148,400 |
| Total (FC + LC) | | 45,300 | 191,300 | 257,200 | 111,500 | 605,300 |

- (Note) 1. Interest on borrowing accrued during the term of construction work is not included in the above amounts.
2. General expenses include the indirect cost of contingency and engineering fee.

**Table 10-1-2-2 Initial Investment Cost of ME-1 Replacing Thermal Power Plant
(Economic Price Basis)**

(Unit: 10³ US\$)

| Year | | 1 | 2 | 3 | 4 | Total |
|--------------------------------|----|---------------|----------------|----------------|----------------|----------------|
| Civil/Erection Island | FC | 18,600 | 13,000 | 15,500 | 14,900 | 62,000 |
| | LC | 23,959 | 16,781 | 19,885 | 19,109 | 79,734 |
| Boiler Island | FC | 0 | 76,800 | 96,100 | 19,200 | 192,100 |
| | LC | 0 | 13,192 | 16,490 | 3,201 | 32,883 |
| Turbine Island | FC | 0 | 36,000 | 45,100 | 9,000 | 90,100 |
| | LC | 0 | 6,208 | 7,663 | 1,552 | 15,423 |
| Coal/Limestone Handling Island | FC | 0 | 18,900 | 41,700 | 15,100 | 75,700 |
| | LC | 0 | 3,201 | 7,178 | 2,619 | 12,998 |
| General Expenses | FC | 2,000 | 6,000 | 6,000 | 23,000 | 37,000 |
| | LC | 0 | 0 | 0 | 2,910 | 2,910 |
| Total | FC | 20,600 | 150,700 | 204,400 | 81,200 | 456,900 |
| | LC | 23,959 | 39,382 | 51,216 | 29,391 | 143,948 |
| Total (FC + LC) | | 44,559 | 190,082 | 255,616 | 110,591 | 600,848 |

- (Note)
1. Interest on borrowing accrued during the term of construction work is not included in the above amounts.
 2. General expenses include the indirect cost of contingency and engineering fee.

**Table 10-1-3-1 Initial Investment Cost of Alternative Thermal Power Plant
(Market Price Basis)**

(Unit: 10³ US\$)

| Year | | 1 | 2 | 3 | 4 | Total |
|--------------------------------|----|---------------|----------------|----------------|----------------|----------------|
| Civil/Erection Island | FC | 16,800 | 11,800 | 14,000 | 13,500 | 56,100 |
| | LC | 22,300 | 15,600 | 18,600 | 17,900 | 74,400 |
| Boiler Island | FC | 0 | 59,100 | 73,900 | 14,800 | 147,800 |
| | LC | 0 | 10,500 | 13,000 | 2,600 | 26,100 |
| Turbine Island | FC | 0 | 30,000 | 37,600 | 7,500 | 75,100 |
| | LC | 0 | 12,900 | 16,100 | 3,200 | 32,200 |
| Coal/Limestone Handling Island | FC | 0 | 13,700 | 30,100 | 10,900 | 54,700 |
| | LC | 0 | 5,800 | 12,900 | 4,700 | 23,400 |
| General Expenses | FC | 2,000 | 6,000 | 6,000 | 23,000 | 37,000 |
| | LC | 0 | 0 | 0 | 3,000 | 3,000 |
| Total | FC | 18,800 | 120,600 | 161,600 | 69,700 | 370,700 |
| | LC | 22,300 | 44,800 | 60,600 | 31,400 | 159,100 |
| Total (FC + LC) | | 41,100 | 165,400 | 222,200 | 101,100 | 529,800 |

- (Note) 1. Interest on borrowing accrued during the term of construction work is not included in the above amounts.
2. General expenses include the indirect cost of contingency and engineering fee.

**Table 10-1-3-2 Initial Investment Cost of Alternative Thermal Power Plant
(Economic Price Basis)**

(Unit: 10³ US\$)

| Year | | 1 | 2 | 3 | 4 | Total |
|--------------------------------|----|---------------|----------------|----------------|----------------|----------------|
| Civil/Erection Island | FC | 16,800 | 11,800 | 14,000 | 13,500 | 56,100 |
| | LC | 21,631 | 15,132 | 18,042 | 17,363 | 72,168 |
| Boiler Island | FC | 0 | 59,100 | 73,900 | 14,800 | 147,800 |
| | LC | 0 | 10,185 | 12,610 | 2,522 | 25,317 |
| Turbine Island | FC | 0 | 30,000 | 37,600 | 7,500 | 75,100 |
| | LC | 0 | 12,513 | 15,617 | 3,104 | 31,234 |
| Coal/Limestone Handling Island | FC | 0 | 13,700 | 30,100 | 10,900 | 54,700 |
| | LC | 0 | 5,626 | 12,513 | 4,559 | 22,698 |
| General Expenses | FC | 2,000 | 6,000 | 6,000 | 23,000 | 37,000 |
| | LC | 0 | 0 | 0 | 2,910 | 2,910 |
| Total | FC | 18,800 | 120,600 | 161,600 | 69,700 | 370,700 |
| | LC | 21,631 | 43,456 | 58,782 | 30,458 | 154,327 |
| Total (FC + LC) | | 40,431 | 164,056 | 220,382 | 100,158 | 525,027 |

(Note) 1. Interest on borrowing accrued during the term of construction work is not included in the above amounts.

2. General expenses include the indirect cost of contingency and engineering fee.

Table 10-1-3-3 Basic Condition for Economic Evaluation

1. The 1 US\$ = 67Lv is the exchange rate of average 1995, which is adopted in the economic and financial evaluation to convert into the unit price.
2. Basic price point for evaluation is assumed to be the prices as of January, 1996.
3. Other Parameter and Data

| Item | Assumed Data and Conditions |
|-------------------------------------|--|
| 1) Method of Analysis | Alternative Plant Approach (Imported coal-fired plant) |
| 2) Study Period | 30 year plus construction period |
| 3) Discount Rate | 10% |
| 4) Opportunity Cost of Capital | 10% |
| 5) Selection of Benefit | Cost of Imported coal-fired TPP |
| 6) Standard Conversion Factor (SCF) | 0.97 |

Table 10-1-3-4 Basic Factors for Economic Evaluation

| Item | Maritsa East No.1 Replacing Plant | Alternative Plant |
|---|-----------------------------------|-------------------------------|
| 1. Capacity | 230 MW x 2 Units | 230 MW x 2 Units |
| Heat supply | 25 Gcal/H | 25 Gcal/H |
| 2. Site | Maritsa East-1 site | Maritsa East 1 site |
| 3. Annual Utilization | 70 % | 70 % |
| 4. Plant efficiency | 28.5 % | 38.3 % |
| Boiler | 68.3 % | 93.8 % |
| Turbine | 45.0 % | 45.0 % |
| In-house ratio | 7.0 % | 9.0 % |
| Plant loss | 0.3 % | 0.3 % |
| 5. Annual production (GWh) | 2,821 | 2,821 |
| 6. Net annual production [at sending end] (GWh) | 2,623 | 2,567 |
| 7. Fuel calorific value [LHV] | 1,686 kcal/kg 7,058 kJ/kg | 5,898 kcal/kg 24,689 kJ/kg |
| 8. Fuel consumption (t/year) | $5,052 \times 10^3$ | 994×10^3 |
| 9. Fuel cost (unit cost) | | |
| - Economic cost | 6.6 \$/T | 60.0 \$/T |
| - Financial cost | 6.0 \$/T | 60.0 \$/T |
| 10. Annual O'M cost (US\$/year) | $22,030 \times 10^3$ | $18,960 \times 10^3$ |
| 11. Plant life | 30 years | 30 years |

Table 10-1-4-1 Net Present Values and Benefit-Cost Ratio

(Unit: 10³ US\$)

| | ME-1 Thermal Power Plant | | Alternative Thermal | | Difference | | |
|--|--------------------------|-------------------|---------------------|-------------------|------------|---------|-------|
| | Total Cost | Present Value (C) | Total Cost | Present Value (B) | Total | (B-C) | (B/C) |
| | 2,183,334 | 804,823 | 2,896,367 | 915,270 | 713,034 | 110,447 | 1.14 |

Table 10-1-4-2 Economic Evaluation of ME-1 Thermal Power Plant

(1,000 US \$)

| No. | YEAR | Maritsa East No.1 Replacing PROJECT | | | Alternative Thermal Power PROJECT (Imported Coal-fired) | | | (B) - (C) | |
|--------------------------|------|-------------------------------------|------------|-----------|---|-------------------------|-----------|-----------|----------------|
| | | Construct. Cost | O & M Cost | Fuel Cost | (C) TOTAL COST | IMPORTED TPP O & M Cost | Fuel Cost | | (B) TOTAL COST |
| 1 | 1998 | 44,559 | | | 44,559 | 40,431 | | 40,431 | -4,128 |
| 2 | 1999 | 190,082 | | | 190,082 | 164,056 | | 164,056 | -26,026 |
| 3 | 2000 | 255,616 | | | 255,616 | 220,382 | | 220,382 | -35,234 |
| 4 | 2001 | 110,591 | | | 110,591 | 100,158 | | 100,158 | -10,433 |
| 5 | 1 | | 22,438 | 30,312 | 52,750 | | 19,405 | 79,045 | 26,295 |
| 6 | 2 | | 22,438 | 30,312 | 52,750 | | 19,405 | 79,045 | 26,295 |
| 7 | 3 | | 22,438 | 30,312 | 52,750 | | 19,405 | 79,045 | 26,295 |
| 8 | 4 | | 22,438 | 30,312 | 52,750 | | 19,405 | 79,045 | 26,295 |
| 9 | 5 | | 22,438 | 30,312 | 52,750 | | 19,405 | 79,045 | 26,295 |
| 10 | 6 | | 22,438 | 30,312 | 52,750 | | 19,405 | 79,045 | 26,295 |
| 11 | 7 | | 22,438 | 30,312 | 52,750 | | 19,405 | 79,045 | 26,295 |
| 12 | 8 | | 22,438 | 30,312 | 52,750 | | 19,405 | 79,045 | 26,295 |
| 13 | 9 | | 22,438 | 30,312 | 52,750 | | 19,405 | 79,045 | 26,295 |
| 14 | 10 | | 22,438 | 30,312 | 52,750 | | 19,405 | 79,045 | 26,295 |
| 15 | 11 | | 22,438 | 30,312 | 52,750 | | 19,405 | 79,045 | 26,295 |
| 16 | 12 | | 22,438 | 30,312 | 52,750 | | 19,405 | 79,045 | 26,295 |
| 17 | 13 | | 22,438 | 30,312 | 52,750 | | 19,405 | 79,045 | 26,295 |
| 18 | 14 | | 22,438 | 30,312 | 52,750 | | 19,405 | 79,045 | 26,295 |
| 19 | 15 | | 22,438 | 30,312 | 52,750 | | 19,405 | 79,045 | 26,295 |
| 20 | 16 | | 22,438 | 30,312 | 52,750 | | 19,405 | 79,045 | 26,295 |
| 21 | 17 | | 22,438 | 30,312 | 52,750 | | 19,405 | 79,045 | 26,295 |
| 22 | 18 | | 22,438 | 30,312 | 52,750 | | 19,405 | 79,045 | 26,295 |
| 23 | 19 | | 22,438 | 30,312 | 52,750 | | 19,405 | 79,045 | 26,295 |
| 24 | 20 | | 22,438 | 30,312 | 52,750 | | 19,405 | 79,045 | 26,295 |
| 25 | 21 | | 22,438 | 30,312 | 52,750 | | 19,405 | 79,045 | 26,295 |
| 26 | 22 | | 22,438 | 30,312 | 52,750 | | 19,405 | 79,045 | 26,295 |
| 27 | 23 | | 22,438 | 30,312 | 52,750 | | 19,405 | 79,045 | 26,295 |
| 28 | 24 | | 22,438 | 30,312 | 52,750 | | 19,405 | 79,045 | 26,295 |
| 29 | 25 | | 22,438 | 30,312 | 52,750 | | 19,405 | 79,045 | 26,295 |
| 30 | 26 | | 22,438 | 30,312 | 52,750 | | 19,405 | 79,045 | 26,295 |
| 31 | 27 | | 22,438 | 30,312 | 52,750 | | 19,405 | 79,045 | 26,295 |
| 32 | 28 | | 22,438 | 30,312 | 52,750 | | 19,405 | 79,045 | 26,295 |
| 33 | 29 | | 22,438 | 30,312 | 52,750 | | 19,405 | 79,045 | 26,295 |
| 34 | 30 | | 22,438 | 30,312 | 52,750 | | 19,405 | 79,045 | 26,295 |
| TOTAL | | 600,848 | 673,126 | 909,360 | 2,183,334 | 525,027 | 582,140 | 2,896,367 | 713,034 |
| Present Value I = 10% | | | | | 804,823 | | | 915,270 | 110,447 |
| | | | | | | | | | 25.3% |
| | | | | | | | | | 1.14 |

N.P.V.
E.I.R.R.
B/C

Table 10-1-5-1 Sensitivity Analysis

| | | B-C (10 ³ US\$) | B/C | EIRR (%) |
|----------|----------------------------|----------------------------|------|----------|
| Case - 1 | Construction cost (20% up) | 17,411 | 1.02 | 11.2 |
| Case - 2 | Discount rate (8%) | 142,607 | 1.15 | 22.6 |
| | Discount rate (12%) | 78,468 | 1.11 | 25.3 |
| Case - 3 | Fuel cost (5% up) | 100,867 | 1.12 | 24.2 |

Table 10-2-1-1 : Basic Conditions for Financial Evaluation

| Item | Assumed Data and Conditions |
|-------------------------------------|--|
| 1) Revenue for Financial Evaluation | 4.5 cent/kWh (Electricity) 31.4 US\$/Gcal (Heat) These are estimated average tariff as of 2001 for NEK |
| 2) Study Period | 30 years plus construction period |
| 3) Method of Repayment | Principal & Interest in equal installment |
| 5) Escalation | Not considered |
| 6) Depreciation | Straight line method/zero residual value |

Table 10-2-3-1 Revenue from Sales of Electricity and Heat

| | Electricity | Heat |
|---|----------------|-------------------|
| Annual net energy | 2,624 GWh/year | 100,000 Gcal/year |
| Electricity price (cent / kWh) | 4.5 | - |
| Annual electricity revenue (10 ³ US\$) | 118,059 | - |
| Heat price (US\$ / Gcal) | - | 31.4 |
| Annual heat revenue (10 ³ US\$) | - | 3,140 |

(1) Basic assumption for Salable Annual Electricity and Heat Supply

1) Electricity

R₁ unit: [230MW x 12 months]

$$230\text{MW} \times 24 \text{ h} \times 365 \text{ day} \times 0.7 \times (1 - 0.07)$$

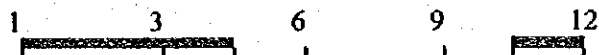
R₂ unit: [230MW x 6 months; 200MW x 6 months (During Heat Supply)]

$$230\text{MW} \times 24 \text{ h} \times (365 \text{ day}/2) \times 0.7 \times (1 - 0.07)$$

$$200\text{MW} \times 24 \text{ h} \times (365 \text{ day}/2) \times 0.7 \times (1 - 0.07)$$

2) Heat

a) The period of supply: 6 (months)



b) Average annual operating period: 4,000 (hours)

c) Total supply heat: 100,000 (Gcal/year)

Table 10-2-4-1 FINANCIAL EVALUATION OF ME-1 Thermal Power Plant

(Unit : 1,000 US \$)

| No. | YEAR | Marista East No.1 PROJECT | | | | (B) REVENUE | | (B) - (C) |
|-------|---------|---------------------------|------------|---------|----------------|-------------|------------|-----------|
| | | Construct. Cost | O & M Cost | FUEL | (C) TOTAL COST | POWER SALES | HEAT SALES | |
| 1 | 1998 | 45,300 | | | 45,300 | | | -45,300 |
| 2 | 1999 | 191,300 | | | 191,300 | | | -191,300 |
| 3 | 2000 | 257,200 | | | 257,200 | | | -257,200 |
| 4 | 2001 | 111,500 | | | 111,500 | | | -111,500 |
| 5 | 1 2002 | | 22,612 | 30,312 | 52,924 | 114,198 | 3,135 | 64,409 |
| 6 | 2 2003 | | 22,612 | 30,312 | 52,924 | 114,198 | 3,135 | 64,409 |
| 7 | 3 2004 | | 22,612 | 30,312 | 52,924 | 114,198 | 3,135 | 64,409 |
| 8 | 4 2005 | | 22,612 | 30,312 | 52,924 | 114,198 | 3,135 | 64,409 |
| 9 | 5 2006 | | 22,612 | 30,312 | 52,924 | 114,198 | 3,135 | 64,409 |
| 10 | 6 2007 | | 22,612 | 30,312 | 52,924 | 114,198 | 3,135 | 64,409 |
| 11 | 7 2008 | | 22,612 | 30,312 | 52,924 | 114,198 | 3,135 | 64,409 |
| 12 | 8 2009 | | 22,612 | 30,312 | 52,924 | 114,198 | 3,135 | 64,409 |
| 13 | 9 2010 | | 22,612 | 30,312 | 52,924 | 114,198 | 3,135 | 64,409 |
| 14 | 10 2011 | | 22,612 | 30,312 | 52,924 | 114,198 | 3,135 | 64,409 |
| 15 | 11 2012 | | 22,612 | 30,312 | 52,924 | 114,198 | 3,135 | 64,409 |
| 16 | 12 2013 | | 22,612 | 30,312 | 52,924 | 114,198 | 3,135 | 64,409 |
| 17 | 13 2014 | | 22,612 | 30,312 | 52,924 | 114,198 | 3,135 | 64,409 |
| 18 | 14 2015 | | 22,612 | 30,312 | 52,924 | 114,198 | 3,135 | 64,409 |
| 19 | 15 2016 | | 22,612 | 30,312 | 52,924 | 114,198 | 3,135 | 64,409 |
| 20 | 16 2017 | | 22,612 | 30,312 | 52,924 | 114,198 | 3,135 | 64,409 |
| 21 | 17 2018 | | 22,612 | 30,312 | 52,924 | 114,198 | 3,135 | 64,409 |
| 22 | 18 2019 | | 22,612 | 30,312 | 52,924 | 114,198 | 3,135 | 64,409 |
| 23 | 19 2020 | | 22,612 | 30,312 | 52,924 | 114,198 | 3,135 | 64,409 |
| 24 | 20 2021 | | 22,612 | 30,312 | 52,924 | 114,198 | 3,135 | 64,409 |
| 25 | 21 2022 | | 22,612 | 30,312 | 52,924 | 114,198 | 3,135 | 64,409 |
| 26 | 22 2023 | | 22,612 | 30,312 | 52,924 | 114,198 | 3,135 | 64,409 |
| 27 | 23 2024 | | 22,612 | 30,312 | 52,924 | 114,198 | 3,135 | 64,409 |
| 28 | 24 2025 | | 22,612 | 30,312 | 52,924 | 114,198 | 3,135 | 64,409 |
| 29 | 25 2026 | | 22,612 | 30,312 | 52,924 | 114,198 | 3,135 | 64,409 |
| 30 | 26 2027 | | 22,612 | 30,312 | 52,924 | 114,198 | 3,135 | 64,409 |
| 31 | 27 2028 | | 22,612 | 30,312 | 52,924 | 114,198 | 3,135 | 64,409 |
| 32 | 28 2029 | | 22,612 | 30,312 | 52,924 | 114,198 | 3,135 | 64,409 |
| 33 | 29 2030 | | 22,612 | 30,312 | 52,924 | 114,198 | 3,135 | 64,409 |
| 34 | 30 2031 | | 22,612 | 30,312 | 52,924 | 114,198 | 3,135 | 64,409 |
| TOTAL | | 605,300 | 678,360 | 909,360 | 2,193,020 | 3,425,933 | 94,050 | 1,326,963 |

Base case: 4.5 cent/kWh

F.I.R.R.

8.8%

Table 10-3-2-1 Fund Requirement and Repayment

(Unit : 1,000 US \$)

| No. | FUND REQUIREMENT | | | REPAYMENT SCHEDULE | | | | | | | | | | | | | | | | | |
|-------|------------------|---------|---------|----------------------------------|-----------|-----------|-------------------|-----------|-----------|-------|---------|--|--|---------|--|--|--|--|--|--|---------|
| | Foreign | Local | Total | FOREIGN FOR FOREIGN CONSTRUCTION | | | FOREIGN FOR LOCAL | | | | | | | | | | | | | | |
| | | | | Interest | Principal | Total | Balance | Interest | Principal | Total | Balance | | | | | | | | | | |
| 1 | 20,600 | 24,700 | 45,300 | () | | | | (0) | | | | | | | | | | | | | |
| 2 | 150,700 | 40,600 | 191,300 | (824) | | | | (1,235) | | | | | | | | | | | | | |
| 3 | 204,400 | 52,800 | 257,200 | (7,676) | | | | (4,500) | | | | | | | | | | | | | |
| 4 | 81,200 | 30,300 | 111,500 | (21,880) | | | | (9,170) | | | | | | | | | | | | | |
| 5 | | | | (33,304) | | | | 522,752 | | | | | | | | | | | | | 178,990 |
| 6 | | | | 41,820 | 11,423 | 53,243 | | 511,329 | 17,899 | | | | | 5,633 | | | | | | | 23,532 |
| 7 | | | | 40,906 | 12,337 | 53,243 | | 498,992 | 17,336 | | | | | 6,197 | | | | | | | 23,532 |
| 8 | | | | 39,919 | 13,324 | 53,243 | | 485,667 | 16,716 | | | | | 7,498 | | | | | | | 23,532 |
| 9 | | | | 38,853 | 14,390 | 53,243 | | 471,277 | 16,034 | | | | | 8,248 | | | | | | | 23,532 |
| 10 | | | | 37,702 | 15,541 | 53,243 | | 455,736 | 15,284 | | | | | 9,073 | | | | | | | 23,532 |
| 11 | | | | 36,459 | 16,785 | 53,243 | | 438,952 | 14,460 | | | | | 9,980 | | | | | | | 23,532 |
| 12 | | | | 35,116 | 18,127 | 53,243 | | 420,824 | 13,552 | | | | | 10,978 | | | | | | | 23,532 |
| 13 | | | | 33,666 | 19,578 | 53,243 | | 401,247 | 12,554 | | | | | 12,076 | | | | | | | 23,532 |
| 14 | | | | 32,100 | 21,144 | 53,243 | | 380,103 | 11,457 | | | | | 13,283 | | | | | | | 23,532 |
| 15 | | | | 30,408 | 22,835 | 53,243 | | 357,268 | 10,249 | | | | | 14,612 | | | | | | | 23,532 |
| 16 | | | | 28,581 | 24,662 | 53,243 | | 332,606 | 8,921 | | | | | 16,073 | | | | | | | 23,532 |
| 17 | | | | 26,608 | 26,635 | 53,243 | | 305,971 | 7,459 | | | | | 17,680 | | | | | | | 23,532 |
| 18 | | | | 24,478 | 28,766 | 53,243 | | 277,205 | 5,852 | | | | | 19,448 | | | | | | | 23,532 |
| 19 | | | | 22,176 | 31,067 | 53,243 | | 246,138 | 4,084 | | | | | 21,393 | | | | | | | 23,532 |
| 20 | | | | 19,691 | 33,552 | 53,243 | | 212,586 | 2,139 | | | | | | | | | | | | 23,532 |
| 21 | | | | 17,007 | 36,237 | 53,243 | | 176,349 | | | | | | | | | | | | | 0 |
| 22 | | | | 14,108 | 39,136 | 53,243 | | 137,214 | | | | | | | | | | | | | |
| 23 | | | | 10,977 | 42,266 | 53,243 | | 94,947 | | | | | | | | | | | | | |
| 24 | | | | 7,596 | 45,648 | 53,243 | | 49,299 | | | | | | | | | | | | | |
| 20 | | | | 3,944 | 49,299 | 53,243 | | 0 | | | | | | | | | | | | | |
| Total | 456,900 | 148,400 | 605,300 | 542,117 | 522,752 | 1,064,869 | | | 173,997 | | | | | 178,990 | | | | | | | 352,987 |

Note: Figures in parentheses are I.D.C.

Funds to be required do not include the amount of interest

Remarks: Repayment condition

Foreign currency : 8.00% (20 Year)
 Local currency : 10.00% (15 Year)
 Grace Period : 4 years (construction period including preparation)

Table 10-3-4-1 Profit and Loss Statement

| No. | Operating Revenue (A) | | Operating Expenses | | Total (B) | Operating Income (C)=A-B | Financial Expenses* | | Total* (D) | Net Income (E)=C-D |
|-------|-----------------------|---------|--------------------|---------|-----------|--------------------------|---------------------|------------|------------|--------------------|
| | O & M | | Depreciation | | | | F.C. | L.C. | | |
| | | | | | | | | | | |
| 1 | | | | | | | (0) | (0) | (0) | |
| 2 | | | | | | | (824) | (1,235) | (2,059) | |
| 3 | | | | | | | (7,676) | (4,500) | (12,176) | |
| 4 | | | | | | | (21,880) | (9,170) | (31,050) | |
| 5 | | | | | | | (33,304) | (13,325) | (46,629) | |
| 6 | 117,338 | 22,612 | | 16,921 | 39,533 | 77,805 | 41,820 | 17,899 | 59,719 | 18,086 |
| 7 | 117,338 | 22,612 | | 16,921 | 39,533 | 77,805 | 40,906 | 17,336 | 58,242 | 19,563 |
| 8 | 117,338 | 22,612 | | 16,921 | 39,533 | 77,805 | 39,919 | 16,716 | 56,635 | 21,170 |
| 9 | 117,338 | 22,612 | | 16,921 | 39,533 | 77,805 | 38,853 | 16,034 | 54,888 | 22,917 |
| 10 | 117,338 | 22,612 | | 16,921 | 39,533 | 77,805 | 37,702 | 15,284 | 52,987 | 24,818 |
| 11 | 117,338 | 22,612 | | 16,921 | 39,533 | 77,805 | 36,459 | 14,460 | 50,919 | 26,887 |
| 12 | 117,338 | 22,612 | | 16,921 | 39,533 | 77,805 | 35,116 | 13,552 | 48,669 | 29,137 |
| 13 | 117,338 | 22,612 | | 16,921 | 39,533 | 77,805 | 33,666 | 12,554 | 46,220 | 31,585 |
| 14 | 117,338 | 22,612 | | 16,921 | 39,533 | 77,805 | 32,100 | 11,457 | 43,556 | 34,249 |
| 15 | 117,338 | 22,612 | | 16,921 | 39,533 | 77,805 | 30,408 | 10,249 | 40,657 | 37,148 |
| 16 | 117,338 | 22,612 | | 16,921 | 39,533 | 77,805 | 28,581 | 8,921 | 37,502 | 40,303 |
| 17 | 117,338 | 22,612 | | 16,921 | 39,533 | 77,805 | 26,608 | 7,459 | 34,068 | 43,737 |
| 18 | 117,338 | 22,612 | | 16,921 | 39,533 | 77,805 | 24,478 | 5,852 | 30,330 | 47,475 |
| 19 | 117,338 | 22,612 | | 16,921 | 39,533 | 77,805 | 22,176 | 4,084 | 26,261 | 51,545 |
| 20 | 117,338 | 22,612 | | 16,921 | 39,533 | 77,805 | 19,691 | 2,139 | 21,830 | 55,975 |
| 21 | 117,338 | 22,612 | | 16,921 | 39,533 | 77,805 | 17,007 | 0 | 17,007 | 60,798 |
| 22 | 117,338 | 22,612 | | 16,921 | 39,533 | 77,805 | 14,108 | 0 | 14,108 | 63,697 |
| 23 | 117,338 | 22,612 | | 16,921 | 39,533 | 77,805 | 10,977 | 0 | 10,977 | 66,828 |
| 24 | 117,338 | 22,612 | | 16,921 | 39,533 | 77,805 | 7,596 | 0 | 7,596 | 70,209 |
| 25 | 117,338 | 22,612 | | 16,921 | 39,533 | 77,805 | 3,944 | 0 | 3,944 | 73,861 |
| Total | 2,346,755 | 452,240 | | 338,413 | 790,653 | 1,556,102 | 542,117 | 173,997 | 716,114 | 839,988 |

*Note: Figures in parentheses are I.D.C.

Remarks: Operating revenue:

Electricity : 2,537.73 GWh/Year x 0.045 US\$/kWh= 114,198 Thousand US\$/year

Heat : 100,000 Gcal/Year x 31.40 US\$/Gcal= 3,140.0 Thousand US\$/year

117,338 Thousand US\$/year

Table 10-3-4-2 Cash Flow Sheet

| No. | CASH INFLOW | | | | | CASH OUTFLOW | | | | | BALANCE | |
|-------|-------------------|------------|---------------|-----------|--------------------|--------------|---------|----------|--------|-----------|----------------|--------------|
| | Fund Re-quirement | Net Income | Depreci-ation | Total (A) | Construc-tion Cost | F.C. | L.C. | Subtotal | I.D.C. | Total (B) | Yearly (A)-(B) | Accumulation |
| | | | | | | | | | | | | |
| 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2 | 45,300 | 0 | 0 | 45,300 | 45,300 | 0 | 0 | 0 | 2,059 | 47,359 | -2,059 | -2,059 |
| 3 | 191,300 | 0 | 0 | 191,300 | 191,300 | 0 | 0 | 0 | 12,176 | 203,476 | -12,176 | -14,235 |
| 4 | 257,200 | 0 | 0 | 257,200 | 257,200 | 0 | 0 | 0 | 31,050 | 288,250 | -31,050 | -45,285 |
| 5 | 111,500 | 0 | 0 | 111,500 | 111,500 | 0 | 0 | 0 | 46,629 | 158,129 | -46,629 | -91,914 |
| 6 | 0 | 18,086 | 16,921 | 35,007 | 0 | 11,423 | 5,633 | 17,057 | 0 | 17,057 | 17,950 | -73,964 |
| 7 | 0 | 19,563 | 16,921 | 36,484 | 0 | 12,337 | 6,197 | 18,534 | 0 | 18,534 | 17,950 | -56,014 |
| 8 | 0 | 21,170 | 16,921 | 38,090 | 0 | 13,324 | 6,817 | 20,141 | 0 | 20,141 | 17,950 | -38,065 |
| 9 | 0 | 22,917 | 16,921 | 39,838 | 0 | 14,390 | 7,498 | 21,888 | 0 | 21,888 | 17,950 | -20,115 |
| 10 | 0 | 24,818 | 16,921 | 41,739 | 0 | 15,541 | 8,248 | 23,789 | 0 | 23,789 | 17,950 | -2,165 |
| 11 | 0 | 26,887 | 16,921 | 43,807 | 0 | 16,785 | 9,073 | 25,857 | 0 | 25,857 | 17,950 | 15,785 |
| 12 | 0 | 29,137 | 16,921 | 46,057 | 0 | 18,127 | 9,980 | 28,107 | 0 | 28,107 | 17,950 | 33,755 |
| 13 | 0 | 31,585 | 16,921 | 48,505 | 0 | 19,578 | 10,978 | 30,556 | 0 | 30,556 | 17,950 | 51,685 |
| 14 | 0 | 34,249 | 16,921 | 51,169 | 0 | 21,144 | 12,076 | 33,220 | 0 | 33,220 | 17,950 | 69,634 |
| 15 | 0 | 37,148 | 16,921 | 54,069 | 0 | 22,835 | 13,285 | 36,119 | 0 | 36,119 | 17,950 | 87,584 |
| 16 | 0 | 40,303 | 16,921 | 57,224 | 0 | 24,662 | 14,612 | 39,274 | 0 | 39,274 | 17,950 | 105,534 |
| 17 | 0 | 43,737 | 16,921 | 60,658 | 0 | 26,635 | 16,073 | 42,708 | 0 | 42,708 | 17,950 | 123,484 |
| 18 | 0 | 47,475 | 16,921 | 64,396 | 0 | 28,766 | 17,680 | 46,446 | 0 | 46,446 | 17,950 | 141,434 |
| 19 | 0 | 51,545 | 16,921 | 68,465 | 0 | 31,067 | 19,448 | 50,515 | 0 | 50,515 | 17,950 | 159,384 |
| 20 | 0 | 55,975 | 16,921 | 72,895 | 0 | 33,552 | 21,393 | 54,946 | 0 | 54,946 | 17,950 | 177,333 |
| 21 | 0 | 60,798 | 16,921 | 77,719 | 0 | 36,237 | 0 | 36,237 | 0 | 36,237 | 41,482 | 218,816 |
| 22 | 0 | 63,697 | 16,921 | 80,618 | 0 | 39,136 | 0 | 39,136 | 0 | 39,136 | 41,482 | 260,298 |
| 23 | 0 | 66,828 | 16,921 | 83,749 | 0 | 42,266 | 0 | 42,266 | 0 | 42,266 | 41,482 | 301,780 |
| 24 | 0 | 70,209 | 16,921 | 87,130 | 0 | 45,648 | 0 | 45,648 | 0 | 45,648 | 41,482 | 343,263 |
| 24 | 0 | 73,861 | 16,921 | 90,782 | 0 | 49,299 | 0 | 49,299 | 0 | 49,299 | 41,482 | 384,745 |
| Total | 605,300 | 839,988 | 338,413 | 1,783,701 | 605,300 | 522,752 | 178,990 | 701,742 | 91,914 | 1,398,956 | 384,745 | |

Table 10-4-1-1 Trend of Electricity and Heat Price

| Year (Month) | | Electricity (Lv/kWh) | | | Heating (Lv/GCal) | |
|--------------|------|----------------------|------------|----------|-------------------|-----------|
| | | Households | | Industry | | |
| | | Day time | Night time | | Households | Buildings |
| February | 1991 | 0.167 | 0.088 | 0.314 | 50 | 202 |
| June | 1991 | 0.284 | 0.150 | 0.534 | 85 | 343 |
| April | 1992 | 0.383 | 0.202 | 0.721 | 115 | 463 |
| December | 1992 | 0.440 | 0.233 | 0.793 | 149 | 509 |
| May | 1993 | 0.660 | 0.350 | 0.837 | 238 | 610 |
| April | 1994 | 0.850 | 0.450 | 1.138 | 450 | 705 |
| March | 1995 | 1.250 | 0.660 | 1.461 | 810 | n.a. |
| September | 1995 | 1.560 | 0.830 | 2.016 | 810 | n.a. |

Source: NEK

Table 10-4-1-2 Breakdown of Generating Cost Expenditures of ME-1

[Electric Power]

(Unit: 10³Ly)

| | Items | 1992 | 1993 | 1994 | |
|---------|---|--|-----------|-----------|-----------|
| | 1. Power Production (10 ³ Wh) | 1,103,096 | 1,117,711 | 979,873 | |
| | 2. Internal Energy Consumption (10 ³ Wh) | 240,906 | 238,165 | 199,040 | |
| | 3. Supply of Electricity (10 ³ Wh) | 862,190 | 879,546 | 780,833 | |
| | 4. Heat for Sale (GCal) | 1,558,904 | 1,555,046 | 1,102,194 | |
| Revenue | 5. Revenue of Electricity Sales | 155,908 | 96,430 | 543,946 | |
| Cost | 6. Fuel for Power Generation | 596,975 | 667,077 | 653,834 | |
| | 7. Energy | 980 | 2,550 | 2,564 | |
| | 8. Overhauls | 90,627 | 119,528 | 137,788 | |
| | 9. Materials and Contractor Services | 36,405 | 71,721 | 80,362 | |
| | 10. Insurance | NEK + 999 | NEK + 84 | NEK + 128 | |
| | 11. Depreciation | NEK | NEK | NEK | |
| | 12. Salaries | 54,850 | 83,871 | 120,682 | |
| | 13. Social ' employee benefits, unemployment fundds | 25,913 | 43,859 | 65,931 | |
| | 14. Financial Costs | 17,281 | 271 | 461 | |
| | 15. Special Costs | 9,475 | 6,972 | 20,099 | |
| | 16. TOTAL COSTS | 833,505 | 995,933 | 1,081,849 | |
| | | 17. Net Electricity Generation, Min. kWh | 862.190 | 879.546 | 780.833 |
| | | 18. Heat for Sale - thousands of Gcal | 1,558.904 | 1,555.046 | 1,102.194 |
| | 19. Costs per 1 kWh, Levs/kWh | 0.57 | 0.67 | 0.85 | |
| | 20. Costs per 1 Gcal, Levs/Gcal | 216 | 256 | 376 | |

Source: NEK

Table 10-4-1-3 Standard of Depreciation

| | Depreciation Rate | Depreciation Year* |
|---------------------|-------------------|---------------------|
| Building | 4% | years (30 years) 25 |
| Turbine | 20% | years (15 years) 5 |
| Machines | 20% | years (15 years) 3 |
| De-Sox Installation | - % | years (7 years) |

Note : The standard of DeSOx Installations is the case of ME-2.
The standard above is about the case of coal thermal power plant.

* : Figures indicated in () is a Japanese case

Source : NEK

Table 10-4-2(1) Financial Evaluation of ME-1 Thermal Power Plant (Case I)

(Unit : 1,000 US \$)

| No. | YEAR | Marista East No.1 PROJECT | | | | (B) REVENUE | | (B) - (C) |
|-------|---------|---------------------------|------------|---------|----------------|-------------|------------|-----------|
| | | Construct. Cost | O & M Cost | FUEL | (C) TOTAL COST | POWER SALES | HEAT SALES | |
| 1 | 1998 | 45,300 | | | 45,300 | | | -45,300 |
| 2 | 1999 | 191,300 | | | 191,300 | | | -191,300 |
| 3 | 2000 | 257,200 | | | 257,200 | | | -257,200 |
| 4 | 2001 | 111,500 | | | 111,500 | | | -111,500 |
| 5 | 1 2002 | | 22,612 | 30,312 | 52,924 | 96,434 | 3,135 | 46,645 |
| 6 | 2 2003 | | 22,612 | 30,312 | 52,924 | 96,434 | 3,135 | 46,645 |
| 7 | 3 2004 | | 22,612 | 30,312 | 52,924 | 96,434 | 3,135 | 46,645 |
| 8 | 4 2005 | | 22,612 | 30,312 | 52,924 | 96,434 | 3,135 | 46,645 |
| 9 | 5 2006 | | 22,612 | 30,312 | 52,924 | 96,434 | 3,135 | 46,645 |
| 10 | 6 2007 | | 22,612 | 30,312 | 52,924 | 96,434 | 3,135 | 46,645 |
| 11 | 7 2008 | | 22,612 | 30,312 | 52,924 | 96,434 | 3,135 | 46,645 |
| 12 | 8 2009 | | 22,612 | 30,312 | 52,924 | 96,434 | 3,135 | 46,645 |
| 13 | 9 2010 | | 22,612 | 30,312 | 52,924 | 96,434 | 3,135 | 46,645 |
| 14 | 10 2011 | | 22,612 | 30,312 | 52,924 | 96,434 | 3,135 | 46,645 |
| 15 | 11 2012 | | 22,612 | 30,312 | 52,924 | 96,434 | 3,135 | 46,645 |
| 16 | 12 2013 | | 22,612 | 30,312 | 52,924 | 96,434 | 3,135 | 46,645 |
| 17 | 13 2014 | | 22,612 | 30,312 | 52,924 | 96,434 | 3,135 | 46,645 |
| 18 | 14 2015 | | 22,612 | 30,312 | 52,924 | 96,434 | 3,135 | 46,645 |
| 19 | 15 2016 | | 22,612 | 30,312 | 52,924 | 96,434 | 3,135 | 46,645 |
| 20 | 16 2017 | | 22,612 | 30,312 | 52,924 | 96,434 | 3,135 | 46,645 |
| 21 | 17 2018 | | 22,612 | 30,312 | 52,924 | 96,434 | 3,135 | 46,645 |
| 22 | 18 2019 | | 22,612 | 30,312 | 52,924 | 96,434 | 3,135 | 46,645 |
| 23 | 19 2020 | | 22,612 | 30,312 | 52,924 | 96,434 | 3,135 | 46,645 |
| 24 | 20 2021 | | 22,612 | 30,312 | 52,924 | 96,434 | 3,135 | 46,645 |
| 25 | 21 2022 | | 22,612 | 30,312 | 52,924 | 96,434 | 3,135 | 46,645 |
| 26 | 22 2023 | | 22,612 | 30,312 | 52,924 | 96,434 | 3,135 | 46,645 |
| 27 | 23 2024 | | 22,612 | 30,312 | 52,924 | 96,434 | 3,135 | 46,645 |
| 28 | 24 2025 | | 22,612 | 30,312 | 52,924 | 96,434 | 3,135 | 46,645 |
| 29 | 25 2026 | | 22,612 | 30,312 | 52,924 | 96,434 | 3,135 | 46,645 |
| 30 | 26 2027 | | 22,612 | 30,312 | 52,924 | 96,434 | 3,135 | 46,645 |
| 31 | 27 2028 | | 22,612 | 30,312 | 52,924 | 96,434 | 3,135 | 46,645 |
| 32 | 28 2029 | | 22,612 | 30,312 | 52,924 | 96,434 | 3,135 | 46,645 |
| 33 | 29 2030 | | 22,612 | 30,312 | 52,924 | 96,434 | 3,135 | 46,645 |
| 34 | 30 2031 | | 22,612 | 30,312 | 52,924 | 96,434 | 3,135 | 46,645 |
| TOTAL | | 605,300 | 678,360 | 909,360 | 2,193,020 | 2,893,010 | 94,050 | 794,040 |

Case 1: 3.8 cent/kWh

F.I.R.R.

5.9%

Table 10-4-2(2) Financial Analysis of ME-1 Thermal Power Plant (Case 1)

| No. | CASH INFLOW | | | | | CASH OUTFLOW | | | | | BALANCE | |
|-------|-----------------------|---------------|-------------------|--------------|------------------------|--------------|---------------------|----------|--------|--------------|-------------------|--------------|
| | Fund Re- quirement | Net Income | Depreci- ation | Total (A) | Construc- tion Cost | F.C. | Principal Repayment | | I.D.C. | Total (B) | Yearly (A)-(B) | Accumulation |
| | | | | | | | L.C. | Subtotal | | | | |
| 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2 | 45,300 | 0 | 0 | 45,300 | 45,300 | 0 | 0 | 0 | 2,059 | 47,359 | -2,059 | -2,059 |
| 3 | 191,300 | 0 | 0 | 191,300 | 191,300 | 0 | 0 | 0 | 12,176 | 203,476 | -12,176 | -14,235 |
| 4 | 257,200 | 0 | 0 | 257,200 | 257,200 | 0 | 0 | 0 | 51,050 | 288,250 | -31,050 | -45,285 |
| 5 | 111,500 | 0 | 0 | 111,500 | 111,500 | 0 | 0 | 0 | 46,629 | 158,129 | -46,629 | -91,914 |
| 6 | 0 | 322 | 16,921 | 17,243 | 0 | 11,423 | 5,633 | 17,057 | 0 | 17,057 | 186 | -91,728 |
| 7 | 0 | 1,799 | 16,921 | 18,720 | 0 | 12,337 | 6,197 | 18,534 | 0 | 18,534 | 186 | -91,543 |
| 8 | 0 | 3,406 | 16,921 | 20,326 | 0 | 13,324 | 6,817 | 20,141 | 0 | 20,141 | 186 | -91,357 |
| 9 | 0 | 5,153 | 16,921 | 22,074 | 0 | 14,390 | 7,498 | 21,888 | 0 | 21,888 | 186 | -91,171 |
| 10 | 0 | 7,054 | 16,921 | 23,975 | 0 | 15,541 | 8,248 | 23,789 | 0 | 23,789 | 186 | -90,985 |
| 11 | 0 | 9,122 | 16,921 | 26,043 | 0 | 16,785 | 9,073 | 25,857 | 0 | 25,857 | 186 | -90,800 |
| 12 | 0 | 11,372 | 16,921 | 28,293 | 0 | 18,127 | 9,980 | 28,107 | 0 | 28,107 | 186 | -90,614 |
| 13 | 0 | 13,821 | 16,921 | 30,741 | 0 | 19,578 | 10,978 | 30,556 | 0 | 30,556 | 186 | -90,428 |
| 14 | 0 | 16,485 | 16,921 | 33,405 | 0 | 21,144 | 12,076 | 33,220 | 0 | 33,220 | 186 | -90,242 |
| 15 | 0 | 19,384 | 16,921 | 36,304 | 0 | 22,835 | 13,283 | 36,119 | 0 | 36,119 | 186 | -90,057 |
| 16 | 0 | 22,539 | 16,921 | 39,460 | 0 | 24,662 | 14,612 | 39,274 | 0 | 39,274 | 186 | -89,871 |
| 17 | 0 | 25,973 | 16,921 | 42,894 | 0 | 26,635 | 16,073 | 42,708 | 0 | 42,708 | 186 | -89,685 |
| 18 | 0 | 29,711 | 16,921 | 46,632 | 0 | 28,766 | 17,680 | 46,446 | 0 | 46,446 | 186 | -89,499 |
| 19 | 0 | 33,780 | 16,921 | 50,701 | 0 | 31,067 | 19,448 | 50,515 | 0 | 50,515 | 186 | -89,314 |
| 20 | 0 | 38,211 | 16,921 | 55,131 | 0 | 33,552 | 21,393 | 54,946 | 0 | 54,946 | 186 | -89,128 |
| 21 | 0 | 43,034 | 16,921 | 59,955 | 0 | 36,237 | 0 | 36,237 | 0 | 36,237 | 23,718 | -65,410 |
| 22 | 0 | 45,933 | 16,921 | 62,854 | 0 | 39,136 | 0 | 39,136 | 0 | 39,136 | 23,718 | -41,692 |
| 23 | 0 | 49,064 | 16,921 | 65,985 | 0 | 42,266 | 0 | 42,266 | 0 | 42,266 | 23,718 | -17,973 |
| 24 | 0 | 52,445 | 16,921 | 69,366 | 0 | 45,648 | 0 | 45,648 | 0 | 45,648 | 23,718 | 5,745 |
| 24 | 0 | 56,097 | 16,921 | 73,018 | 0 | 49,299 | 0 | 49,299 | 0 | 49,299 | 23,718 | 29,463 |
| Total | 605,300 | 484,706 | 338,413 | 1,428,419 | 605,300 | 522,752 | 178,990 | 701,742 | 91,914 | 1,398,956 | 29,463 | |

Table 10-4-3(1) Financial Evaluation of ME-1 Thermal Power Plant (Case 2)

(Unit : 1,000 US \$)

| No. | YEAR | Marista East No.1 PROJECT | | | | (B) REVENUE | | (B) - (C) |
|-------|---------|---------------------------|------------|---------|----------------|-------------|------------|-----------|
| | | Construct. Cost | O & M Cost | FUEL | (C) TOTAL COST | POWER SALES | HEAT SALES | |
| 1 | 1998 | 45,300 | | | 45,300 | | | -45,300 |
| 2 | 1999 | 191,300 | | | 191,300 | | | -191,300 |
| 3 | 2000 | 257,200 | | | 257,200 | | | -257,200 |
| 4 | 2001 | 111,500 | | | 111,500 | | | -111,500 |
| 5 | 1 2002 | | 22,612 | 30,312 | 52,924 | 126,886 | 3,135 | 77,097 |
| 6 | 2 2003 | | 22,612 | 30,312 | 52,924 | 126,886 | 3,135 | 77,097 |
| 7 | 3 2004 | | 22,612 | 30,312 | 52,924 | 126,886 | 3,135 | 77,097 |
| 8 | 4 2005 | | 22,612 | 30,312 | 52,924 | 126,886 | 3,135 | 77,097 |
| 9 | 5 2006 | | 22,612 | 30,312 | 52,924 | 126,886 | 3,135 | 77,097 |
| 10 | 6 2007 | | 22,612 | 30,312 | 52,924 | 126,886 | 3,135 | 77,097 |
| 11 | 7 2008 | | 22,612 | 30,312 | 52,924 | 126,886 | 3,135 | 77,097 |
| 12 | 8 2009 | | 22,612 | 30,312 | 52,924 | 126,886 | 3,135 | 77,097 |
| 13 | 9 2010 | | 22,612 | 30,312 | 52,924 | 126,886 | 3,135 | 77,097 |
| 14 | 10 2011 | | 22,612 | 30,312 | 52,924 | 126,886 | 3,135 | 77,097 |
| 15 | 11 2012 | | 22,612 | 30,312 | 52,924 | 126,886 | 3,135 | 77,097 |
| 16 | 12 2013 | | 22,612 | 30,312 | 52,924 | 126,886 | 3,135 | 77,097 |
| 17 | 13 2014 | | 22,612 | 30,312 | 52,924 | 126,886 | 3,135 | 77,097 |
| 18 | 14 2015 | | 22,612 | 30,312 | 52,924 | 126,886 | 3,135 | 77,097 |
| 19 | 15 2016 | | 22,612 | 30,312 | 52,924 | 126,886 | 3,135 | 77,097 |
| 20 | 16 2017 | | 22,612 | 30,312 | 52,924 | 126,886 | 3,135 | 77,097 |
| 21 | 17 2018 | | 22,612 | 30,312 | 52,924 | 126,886 | 3,135 | 77,097 |
| 22 | 18 2019 | | 22,612 | 30,312 | 52,924 | 126,886 | 3,135 | 77,097 |
| 23 | 19 2020 | | 22,612 | 30,312 | 52,924 | 126,886 | 3,135 | 77,097 |
| 24 | 20 2021 | | 22,612 | 30,312 | 52,924 | 126,886 | 3,135 | 77,097 |
| 25 | 21 2022 | | 22,612 | 30,312 | 52,924 | 126,886 | 3,135 | 77,097 |
| 26 | 22 2023 | | 22,612 | 30,312 | 52,924 | 126,886 | 3,135 | 77,097 |
| 27 | 23 2024 | | 22,612 | 30,312 | 52,924 | 126,886 | 3,135 | 77,097 |
| 28 | 24 2025 | | 22,612 | 30,312 | 52,924 | 126,886 | 3,135 | 77,097 |
| 29 | 25 2026 | | 22,612 | 30,312 | 52,924 | 126,886 | 3,135 | 77,097 |
| 30 | 26 2027 | | 22,612 | 30,312 | 52,924 | 126,886 | 3,135 | 77,097 |
| 31 | 27 2028 | | 22,612 | 30,312 | 52,924 | 126,886 | 3,135 | 77,097 |
| 32 | 28 2029 | | 22,612 | 30,312 | 52,924 | 126,886 | 3,135 | 77,097 |
| 33 | 29 2030 | | 22,612 | 30,312 | 52,924 | 126,886 | 3,135 | 77,097 |
| 34 | 30 2031 | | 22,612 | 30,312 | 52,924 | 126,886 | 3,135 | 77,097 |
| TOTAL | | 605,300 | 678,360 | 909,360 | 2,193,020 | 3,806,592 | 94,050 | 1,707,622 |

Case 2: 5.0 cent / kWh

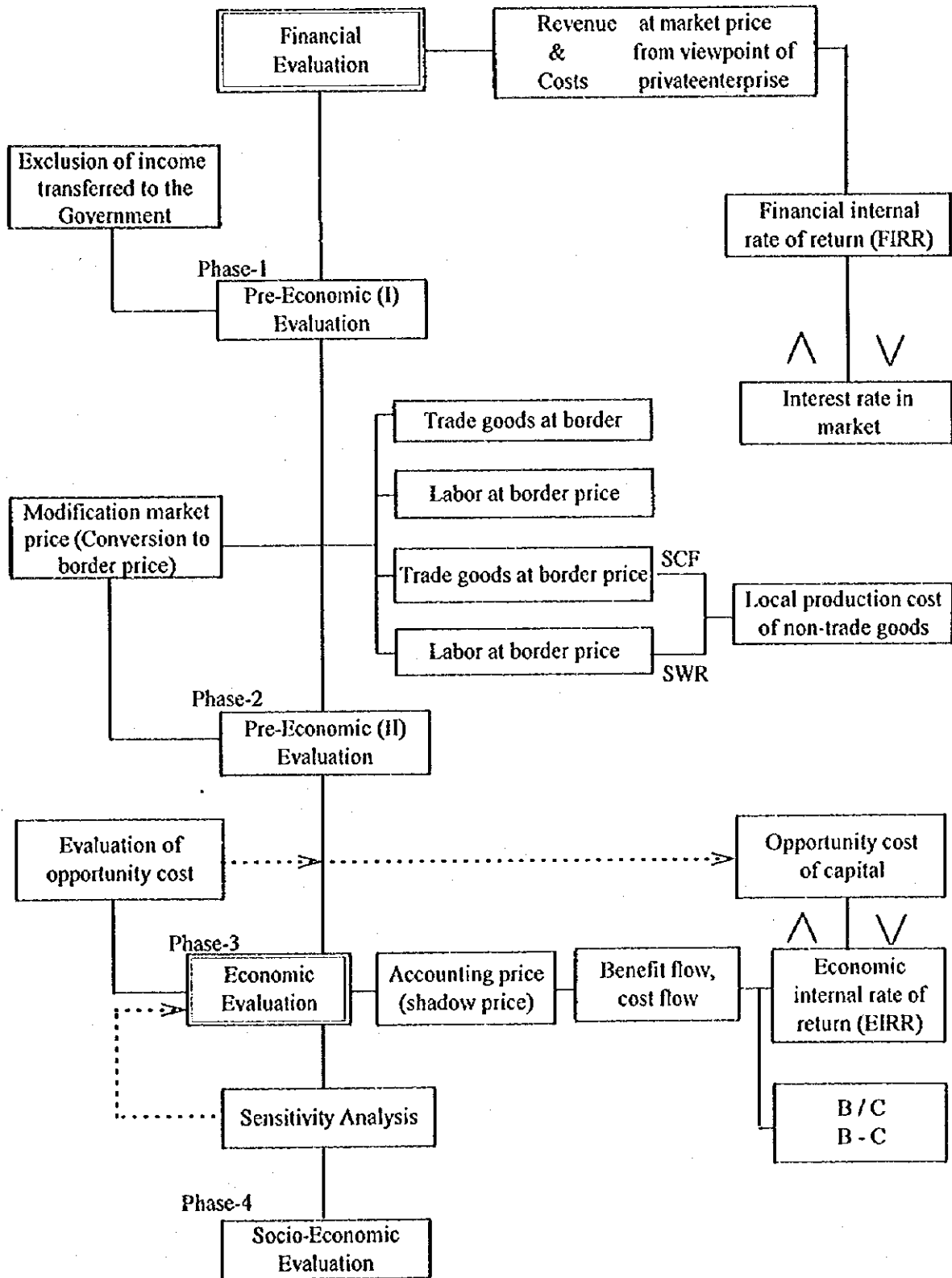
F.I.R.R.

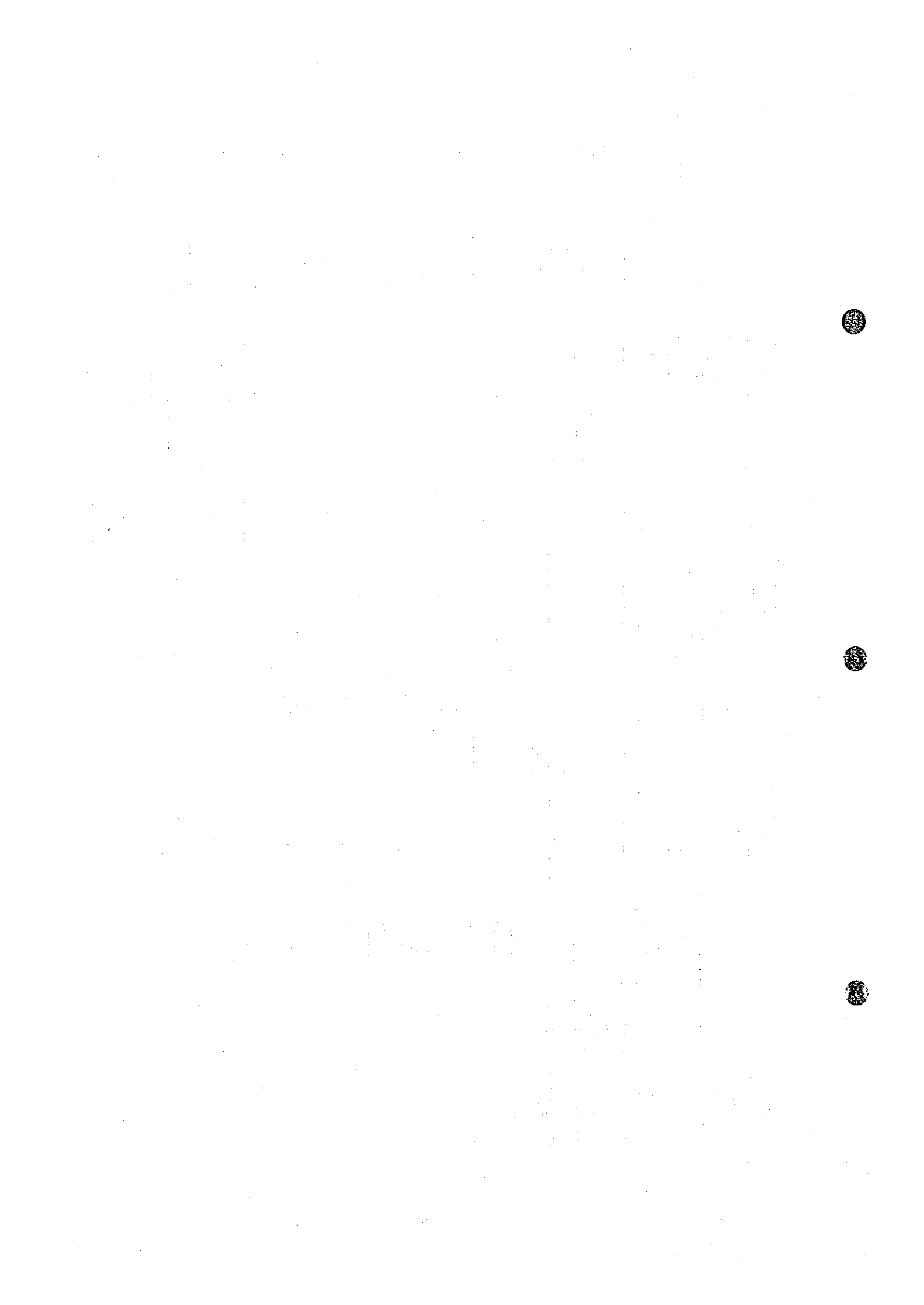
10.6%

Table 10-4-3(2) Financial Analysis of ME-1 Thermal Power Plant (Case 2)

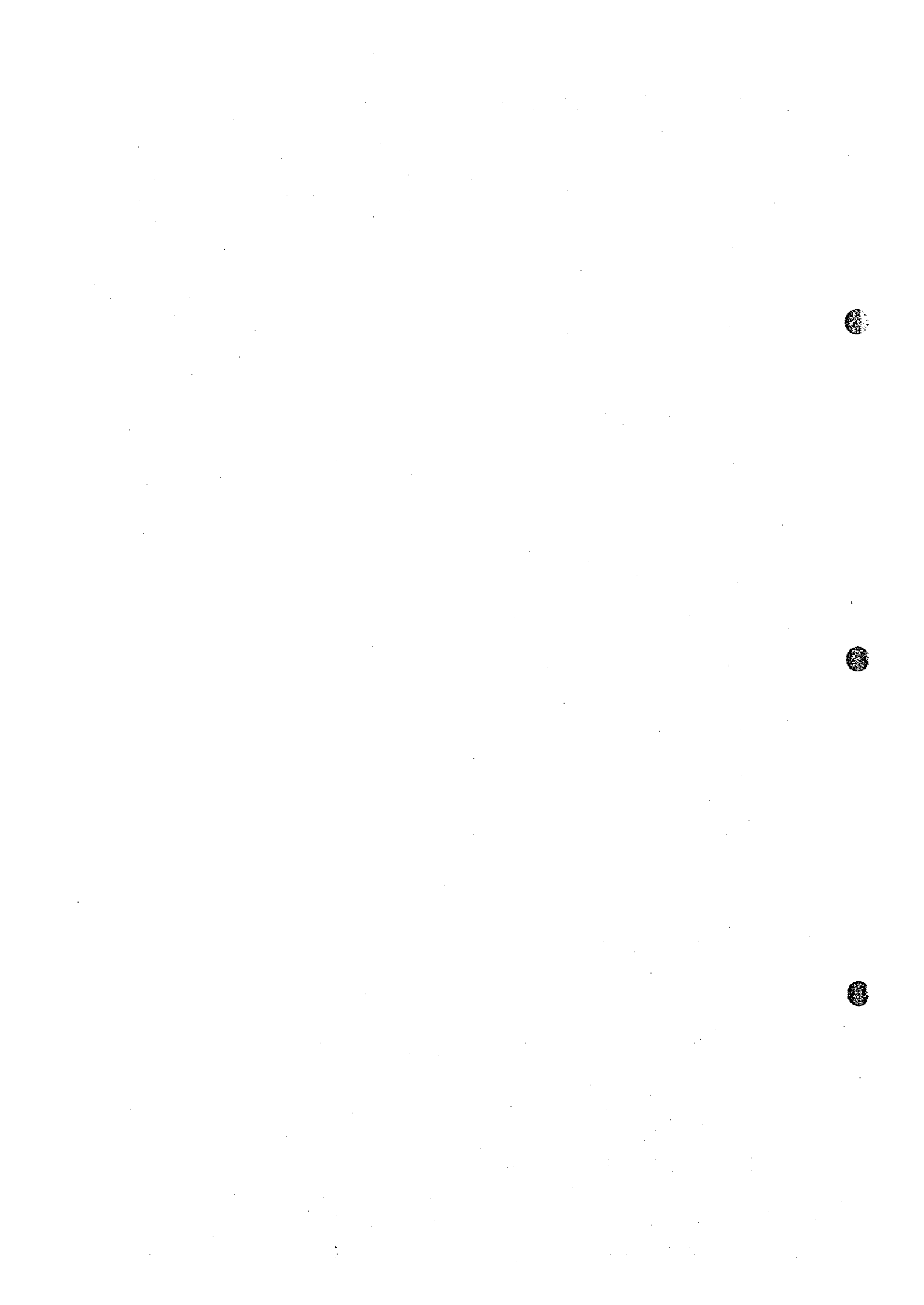
| No. | CASH INFLOW | | | | | | | | | | CASH OUTFLOW | | | | | BALANCE | |
|--------|-----------------------|---------------|-------------------|--------------|------------------------|---------------------|---------|----------|--------|--------------|-------------------|--------------|--------------|-------------------|---------|---------|------|
| | Fund Re- quirement | Net Income | Depreci- ation | Total (A) | Construc- tion Cost | Principal Repayment | | | I.D.C. | Total (B) | Yearly (A)-(B) | Accumulation | 1000 US\$ | | | | |
| | | | | | | F.C. | L.C. | Subtotal | | | | | Total (B) | Yearly (A)-(B) | BALANCE | | |
| | | | | | | | | | | | | | | | | F.C. | L.C. |
| (Unit) | (Unit) | (Unit) | (Unit) | (Unit) | (Unit) | (Unit) | (Unit) | (Unit) | (Unit) | (Unit) | (Unit) | (Unit) | (Unit) | (Unit) | | | |
| 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | | |
| 2 | 45,300 | 0 | 0 | 45,300 | 45,300 | 0 | 0 | 0 | 2,059 | 47,359 | -2,059 | -2,059 | 1000 | US\$ | | | |
| 3 | 191,300 | 0 | 0 | 191,300 | 191,300 | 0 | 0 | 0 | 12,176 | 203,476 | -12,176 | -14,235 | 1000 | US\$ | | | |
| 4 | 257,200 | 0 | 0 | 257,200 | 257,200 | 0 | 0 | 0 | 31,050 | 288,250 | -31,050 | -45,285 | 1000 | US\$ | | | |
| 5 | 111,500 | 0 | 0 | 111,500 | 111,500 | 0 | 0 | 0 | 46,629 | 158,129 | -46,629 | -91,914 | 1000 | US\$ | | | |
| 6 | 0 | 31,184 | 16,921 | 48,105 | 0 | 11,376 | 5,559 | 16,935 | 0 | 16,935 | 31,170 | -60,744 | 1000 | US\$ | | | |
| 7 | 0 | 32,650 | 16,921 | 49,571 | 0 | 12,286 | 6,115 | 18,401 | 0 | 18,401 | 31,170 | -29,575 | 1000 | US\$ | | | |
| 8 | 0 | 34,244 | 16,921 | 51,165 | 0 | 13,269 | 6,727 | 19,996 | 0 | 19,996 | 31,170 | 1,595 | 1000 | US\$ | | | |
| 9 | 0 | 35,979 | 16,921 | 52,899 | 0 | 14,330 | 7,399 | 21,730 | 0 | 21,730 | 31,170 | 32,764 | 1000 | US\$ | | | |
| 10 | 0 | 37,865 | 16,921 | 54,786 | 0 | 15,477 | 8,139 | 23,616 | 0 | 23,616 | 31,170 | 63,934 | 1000 | US\$ | | | |
| 11 | 0 | 39,917 | 16,921 | 56,838 | 0 | 16,715 | 8,953 | 25,668 | 0 | 25,668 | 31,170 | 95,103 | 1000 | US\$ | | | |
| 12 | 0 | 42,150 | 16,921 | 59,070 | 0 | 18,052 | 9,848 | 27,901 | 0 | 27,901 | 31,170 | 126,273 | 1000 | US\$ | | | |
| 13 | 0 | 44,579 | 16,921 | 61,499 | 0 | 19,496 | 10,833 | 30,330 | 0 | 30,330 | 31,170 | 157,443 | 1000 | US\$ | | | |
| 14 | 0 | 47,222 | 16,921 | 64,142 | 0 | 21,056 | 11,917 | 32,973 | 0 | 32,973 | 31,170 | 188,612 | 1000 | US\$ | | | |
| 15 | 0 | 50,098 | 16,921 | 67,018 | 0 | 22,740 | 13,108 | 35,849 | 0 | 35,849 | 31,170 | 219,782 | 1000 | US\$ | | | |
| 16 | 0 | 53,228 | 16,921 | 70,148 | 0 | 24,560 | 14,419 | 38,979 | 0 | 38,979 | 31,170 | 250,951 | 1000 | US\$ | | | |
| 17 | 0 | 56,634 | 16,921 | 73,555 | 0 | 26,525 | 15,861 | 42,386 | 0 | 42,386 | 31,170 | 282,121 | 1000 | US\$ | | | |
| 18 | 0 | 60,343 | 16,921 | 77,263 | 0 | 28,646 | 17,447 | 46,094 | 0 | 46,094 | 31,170 | 313,290 | 1000 | US\$ | | | |
| 19 | 0 | 64,379 | 16,921 | 81,300 | 0 | 30,938 | 19,192 | 50,130 | 0 | 50,130 | 31,170 | 344,460 | 1000 | US\$ | | | |
| 20 | 0 | 68,773 | 16,921 | 85,694 | 0 | 33,413 | 21,111 | 54,524 | 0 | 54,524 | 31,170 | 375,629 | 1000 | US\$ | | | |
| 21 | 0 | 73,557 | 16,921 | 90,478 | 0 | 36,086 | 0 | 36,086 | 0 | 36,086 | 54,392 | 430,021 | 1000 | US\$ | | | |
| 22 | 0 | 76,444 | 16,921 | 93,365 | 0 | 38,973 | 0 | 38,973 | 0 | 38,973 | 54,392 | 484,413 | 1000 | US\$ | | | |
| 23 | 0 | 79,562 | 16,921 | 96,483 | 0 | 42,091 | 0 | 42,091 | 0 | 42,091 | 54,392 | 538,805 | 1000 | US\$ | | | |
| 24 | 0 | 82,929 | 16,921 | 99,850 | 0 | 45,458 | 0 | 45,458 | 0 | 45,458 | 54,392 | 593,197 | 1000 | US\$ | | | |
| 24 | 0 | 86,566 | 16,921 | 103,487 | 0 | 49,095 | 0 | 49,095 | 0 | 49,095 | 54,392 | 647,588 | 1000 | US\$ | | | |
| Total | 605,300 | 1,098,303 | 338,413 | 2,042,016 | 605,300 | 520,584 | 176,630 | 697,214 | 91,914 | 1,394,428 | 647,588 | | | | | | |

Figure 10-1-1-1 Flow Chart of Economic and Financial Evaluation









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