Table 3.10Tank Model Simulation Results (7/11)Estimated Monthly Runoff at Song Luy Gauging Station

5.66 7.04 Dec 7.47 4.75 Niov 9.08 9.09 9.08 9.07 9.07 11.96 11.16 Oct 51.98 32.00 34.05 47.50 46.39 48.92 53.57 55.57 15.57 15.57 15.57 15.57 25.85 57.23 57.23 57.23 57.23 57.23 57.23 57.23 57.23 57.87 75.42 75.42 60.52 86.278 44.52 57.87 57.87 17.26 57.87 57.87 57.87 57.87 57.87 57.87 57.87 57.87 57.87 57.87 57.57 19.61 32.04 24.82 22.85 43.63 Sep 57.52 31.59 31.59 51.76 51.76 51.76 37.23 37.23 37.23 41.42 70.96 70.96 t0.34 29.57 15.67 34.11 Aug 21.80 33.50 33.50 33.50 36.15 36.15 36.15 36.15 24.05 24.05 24.05 24.05 24.05 24.05 24.05 25.15 25.15 25.11 11.96 44.42 25.40 25.50 25 4.41 4.41 28.05 17.39 6.10 23.53 **Jul** 2.92 15.65 2.42 50.85 17.14 11.45 11.45 13.31 6.85 6.85 6.85 6.85 4.98 4.98 4.98 4.98 4.98 4.98 4.98 4.93 5.91 10.73 36.91 19.61 1 7.22 19.30 20.68 17.58 7.22 
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Table 3.10Tank Model Simulation Results (8/11)Estimated Monthly Runoff at Ta Lai Gauging Station

Year	lan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec	Mean
1963	142.66	45.53	66.6	6.53	27.04	62.87	291.86	426.37	505.49	922.97	440.04	217.26	258.22
1964	98.78	29.74	8.03	6.21	20.06	104,10	349.69	782.75	697.72	851.50	444.15	263.39	304.68
1965	112.36	36.26	9.75	7.01	6.90	50.91	364.88	402.55	480.24	470.58	415.21	237.81	216.20
1966	95.92	28.82	9.39	10.52	25.62	78.53	103.85	488.95	600.87	462.83	- 17.79	373.38	231.37
1961	146.58	52.67	14.47	8.44	43.52	237.70	422.80	822.24	<b>S</b> 82.29	1,202.40	1.061.02	354.43	437.38
1968	133.30	37.60	12.55	9.29	9.10	127.15	476.20	469.71	671.92	546.99	465.80	301.52	271.76
1969	136.92	61.31	19.85	10:37	9.84	9.82	95.58	343.20	619.62	778.89	363.45	155.11	217.00
1970	56.25	16.61	10.65	10.31	37.11	145.83	439.18	261.67	481.86	600.97	594.07	255.61	242.51
1971	109.11	37.20	13.32	13.75	76.52	198.43	113.62	407.57	588.30	602.06	442.92	199.59	233.53
1972	78.15	22.79	12.16	11.59	11.65	11.54	56.98	330.64	658.89	633,12	436.44	213.26	206.44
1973.	89,04	28.69	13.32	12.07	12.60	140.77	147.83	191.68	662.08	489.85	296.91	143.13	185.66
1974	54.73	17.91	12.75	12.54	19.32	30.13	156.83	370,47	361.34	499.06	395.66	168.48	174.94
1975	78.08	27.46	14.05	14.22	16.77	86.39	199.27	527.40	467.72	452.79	348.02	194.61	202.23
1976	97.43	37.68	15.59	13.54	47.06	293.79	639.49	552.15	554.92	602.66	443.11	190.59	290.67
1977	81.14	27.32	14.97	14.14	14.44	75.57	467.61	823.06	402.82	480.27	352.71	142.84	241.41
1978	58.36	20.85	14.97	14.63	33.51	97.45	322.23	630.55	1,135.15	1,094.68	710.30	285.35	368.17
6261	114.97	38.36	17.25	15.47	40.22	167.93	259.47	394.52	440.24	518.20	465.04	254,49	227.18
0861	118.91	44.20	18.44	16.09	49.57	27.49	36.89	103.84	608.77	796.67	378.60	215.75	201.27
1981	111.50	45.13	19.23	16.57	103.39	472.98	340.80	422.78	593.73	776.62	465.29	218.71	298.90
1982	95.81	34.19	18.28	17.12	17.01	17.62	213.91	651.10	551.82	883.68	545.48	209.81	271.32
1983	79.20	26.96	18.12	21:32	18.18	122.66	412.22	414.26	1,114.31	972.25	433.42	200.55	319.45
1984	89.40	31.81	19.03	18.24	18.20	57.02	437.33	630.16	608.50	553.70	313.24	147.68	243.69
1985	60.43	24.15	18.95	18.65	18.60	18.62	188.58	413.34	494.62	463.32	197.44	97.36	167.84
1986	37.18	20.19	18.95	18.87	18.80	100.69	338.39	522.71	1,010.79	869.66	466.43	215.24	303.16
1987	88.47	31.53	20.19	21.24	160.26	384,74	931.42	1.012.47	573.35	790.81	542.07	237.50	399.50
1988	98.39	34.62	21.12	20.29	31.97	247.88	440.30	420.63	689.72	647.11	452.39	220.51	277.08
1989	93.32	35.50	22.27	20.92	20.89	296.07	497.58	655.44	554.53	624.40	388.27	178.34	282.29
1990	74.65	29.50	21.81	34.21	61.90	145.79	457.96	530.81	983.80	652.85	369.72	229.84	299.40
1991	98.68	38.10	23.07	25.89	22.29	56.31	254.29	530.72	470.34	931.82	609.15	279.28	278.33
1992	116.13	43.68	24.05	22.92	155.73	354.04	433.95	1.029.65	1.042.07	779.81	381.40	160.35	378.65
Mean	94.86	33.55	16.22	15:43	38.27	140.69	329.70	518.78	650.26	698.42	457.18	218.73	267.67

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Table 3.10Tank Model Simulation Results (9/11)Estimated Monthly Runoff at Ta Pao Gauging Station

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ž		War	Apr	VEIV		Jur	Aug	SCP	5	VOV	y S	Mean
0.4	Q	0.40	0.40	0.40	0.40	0.40	55.74	164.18	336.62	20.4 4	3.45	52.77
0.0	0	0.60	0.60	0.60	0.60	09.0	37.02	132.90	141 92	111.07	4.24	36.78
ö	ŝ	0.80	0.80	0.80	0.80	0.93	110.66	236.78	252.91	54.65	6.66	55.68
Ě	33	1.00	16.94	18.55	1.95	1.17	1.10	1.10	1.17	1.20	1.20	3.98
4	27	1.30	1.30	1.30	1.34	1.40	205.20	329.77	231.98	56.83	5.48	69.87
4	8	1.60	1.60	1.60	1.62	8.41	344.46	261.09	266.22	63.39	5.19	79.88
<b>.</b>	94	1.90	1.90	2.00	2.00	25.05	183.07	426.34	316.66	69.22	6:12	86.55
Ŕ	61	2.30	2.30	2.31	4.58	134.67	203.21	545.82	254.34	76.05	28.88	105.09
0	8	2.94	2.72	2.80	2.80	2.83	50.86	249.02	332.92	94.84	21.64	65.24
ব	61	3.24	3.20	3.27	. 3.30	3.32	3.40	3.41	3.50	3.50	3.57	4.10
ŝ	.67	3.70	3.75	3.80	3.82	3.90	3.94	5.11	83.69	12.58	5.13	11.39
ম	5	4.30	4.31	4.40	4.42	4.50	10.63	48.44	330.17	198.17	18:03	52.98
ŝ	80.	4.90	5.00	5.04	5.10	5.17	5.20	60.6	293.19	112.19	11.15	38.93
ŝ	73	5.63	5.70	5.76	5.80	130.55	278.21	255.89	61.67	29.54	18.71	67.52
~	53	6.42	6.44	6.50	6.60	59.77	175.32	240.74	137.56	26.56	16.05	58.49
9	.13	7.33	7.27	7.30	7.46	106.88	264.94	393.68	280.18	101.12	38.77	102.91
ς.	74	8.13	8.10	8.18	23.41	330.10	316.68	145.90	275.97	112.16	29.03	106.97
2	.62	9.03	9.00	9.08	19.81	158.74	197.09	251.73	162.97	67.34	24.59	78.04
13	.38	10.95	9:95	10.00	20.63	80.10	300.25	159.42	221.23	82.20	26.14	79.23
1	.67	10.82	10.88	10.94	16.91	157.16	181.08	383.37	163.70	117.15	59.41	95.01
	5.45	12.14	11.85	11.98	12.87	106.73	303.38	146.64	348.37	188.91	47.92	102.37
ž	16.5	13.08	12.82	12.90	57.55	174.42	456.48	308.28	190.30	47.48	24.18	111.41
	13.93	13.73	13.81	13.90	13.97	14:07	138.94	239.00	301.65	86.10	42.86	75.77
ដ	0.47	15.44	14.80	14.90	15.81	180.25	387.54	284.55	183.80	78.95	58.80	106.94
	8.06	15.86	15.80	15.88	15.94	16.02	108.78	171.87	135.67	100:51	48.39	57.34
2	3.64	16.78	16.78	16.85	16.92	17.00	17.09	17.17	154.63	163.12	42.06	43.57
7	8.14	17.70	17.72	17.80	20.95	206.80	288.96	283.24	122.52	37.76	26.86	90.13
2	3.65	18.60	18.66	18.75	18.82	18.90	95.27	218.84	185.19	147.61	42.41	68.53
Ř	12.0	19.55	19.60	19.66	19.74	23.11	193.51	274.11	125.71	37.50	28.06	67.29
ล	0.43	20.40	20.50	20.55	20.61	20.70	209.51	194.56	141.68	63.39	32.84	65.60
6	43	8.35	8.82	8.93	11.55	66.45	170.92	212.74	201.27	80.38	24.59	68.01

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Table 3.10Tank Model Simulation Results (10/11)Estimated Monthly Runoff at Thanh Binb Gauging Station

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							T. T.				Nor	200	Man
Year	Jan	L CO	Mar	Apr	VEAU	in,	Jul I	Aug.	369	13	1011		
1963	3.26	2.99	2.68	2.48	2.14	4.88	6.41	12.78	22.26	19.72	0.11-	4	1.43
1964	3.43	3.13	2.83	2.50	6.81	7.80	10.08	9.36	16.57	19.16	11.42	5.09	8.18
1965	3.97	3.63	3.35	3.62	5.38	3.11	7.29	13.02	18.55	15.28	61.1	4.78	7.48
1966	3.86	3.54	3.24	2.90	3.15	7.42	6.55	10.86	23.19	10.28	4.95	3.68	6.97
1967	3.25	2.98	2.69	2.86	5.63	5.04	8.77	12.61	9.58	19.05	6.56	3.81	6.90
1968	3.28	3.01	3.75	5.92	4.93	8.28	8.44	14.78	12.19	14.47	6.32	5.28	7.56
1969	3.95	3.57	3.28	5.14	8.89	14.59	19.58	14.60	10.74	15.99	7.53	4.77	9.39
1970	4.15	3.84	3.50	4.01	4.59	5.79	18.46	20.24	9.59	16.93	8.14	4.80	8.67
1261	4.18	3.83	3.50	3.14	3.16	5.17	3.60	14.61	25.77	21.51	6.04	3.99	8.21
1972	4.18	3.83	3.50	3.14	3.16	5.17	3.60	14.61	25 77	21.51	6.9	3.99	8.21
1973	4.65	3.58	3.25	3.05	5.64	2.89	3.72	5.23	18.75	13.69	6.27	4.82	6.29
1974	3.45	2.88	2.60	2.42	5.35	10.54	5.14	8.85	15.90	19.86	8.94	5.38	7.61
1975	3.76	9 9	3.10	2.76	3.45	3.68	10.75	12.86	20.01	20.36	8.05	4,19	8.03
1976	3.55	3.26	2.94	2.68	2.68	8.30	11.51	8.03	24.38	16.26	5.86	4,10	7.80
1677	3.65	3:37	3.05	2.71	2.41	5.91	S.01	4.96	23.68	12.50	4.82	3.34	6.53
1978	2.85	2.58	2.28	9.21	7.80	4,41	14.81	20.35	25.81	21.37	8.70	5.14	10.44
1979	4.05	3.65	4.85	12.40	11.78	15.12	32.40	28.59	16.67	25.68	11.33	6.58	14.42
1980	5.18	4.73	4.31	3.88	7.75	19.39	9.56	17.72	17.27	22.25	13.87	6.25	11.01
1981	5.01	6.33	4.74	4.65	4.87	19.93	11.28	22.74	14.94	18.75	10.52	5.58	10.78
1982	4.63	4.88	5.42	10.68	9.05	9,84	16.77	12.85	34.44	15.38	8.31	5.91	11.51
1983	4.97	4.58	4 17	5.41	3.58	11.50	8.92	21.34	16.71	36.00	10.86	5.54	11.13
1984	7.45	6.43	4.34	7.89	14.34	13.28	9.74	23.33	13.08	13.90	6.61	4.99	10.45
1985	4.51	4.15	3.76		8.15	5.92	9.08	7.11	13.69	23.62	<b>4</b> 4	4.28	8.09
1986	3.75	3.43	3.13	2.79	4.79	60.9	6.05	12.11	11.75	24.30	7.78	5.72	7.64
1987	3.71	3.30	3.01	2.68	2.38	6.22	12.31	12.86	11.97	11.30	<b>4</b> .8	5.63	6.99
1988	3.42	3.02	2.73	3.97	3.20	3.10	11.64	5.02	11.19	11.96	5.85	3.18	5.69
6861	2.60	2.35	2.09	1.96	7.54	8.39	17.76	8.32	7.03	10.70	4.07	3.10	6.33
0661	2.81	2.55	2.28	2.68	- 3.19	13.02	7.94	14.16	16.24	9.34	10.51	4.78	7.46
1661	3.39	3.08	2.77	4.64	2.70	2.25	8.75	7.15	14.94	17.00	5.11	3.25	6.25
1992	2.87	2.61	2.34	5.99	5.85	11.03	11.95	13.70	11.39	8.22	4 40	3.48	6.98
mean	3.93	3.62	3.32	4.48	5.48	8.27	10.69	13.49	17.14	17.54	7.59	4.65	8.35

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Table 3.10Tank Model Simulation Results (11/11)Estimated Monthly Runoff at Tri An Gauging Station
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Year	Jan	Fcb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov -	Dec	Mcan
1959	44.85	39.91	48.55	148.25	234.67	311.49	356.04	1,093.87	958.11	744.69	800.08	372.51	429.92
1960	68.25	44.52	39.91	38.26	-389.15	733.95	776.88	1,554,94	1,293.56	1,858.13	1.073.46	153.31	668.69
1961	67.48	79.78	87.73	86:34	11.11	663.96	851.36	1,008.74	1,132.63	676.63	744.97	312.10	481.95
1962	105.37	69.76	50.44	121.07	90.62	176.59	490.91	799.69	1,217.51	1.197.75	281.85	77.70	389.94
1963	51.11-	46.14	42.02	50.22	396.79	585.54	905.15	491.13	986.60	1,020.46	760.32	154.35	457.49
1964	71.74	50,46	45.71	229.71	505.69	450.05	342.71	1,022.05	1,053.20	1,015.23	566.78	114.45	455.65
1965	57.85	50.94	57.08	103.25	- 151.52	168.24	536.69	946.84	1.211.53	1,014.61	510.46	136.32	412.11
1966	58.95	55.06	47.68	63.72	191:38	611.80	531.36	523.06	1.217.01	797.83	343.97	\$8.91	377.56
1961	53.05	48.06	44.56	71.17	291.67	301.58	644.40	885.73	704.91	1.045.03	428.85	129.25	387.36
1968	63.22	51.32	107.12	237.25	208.38	476.19	486.29	1,175.84	745.33	756.02	473.61	213.92	416.21
1969	76.55	56.46	62.20	123.64	350.61	973.45	1,254.91	1,082.30	850.42	994.16	488.78	143.25	538.06
1970	79.70	62.37	57.47	95.92	225.56	582.44	1;213.38	1.278.75	537.92	878.37	299.26	104.23	451.28
1671	81.19	59.27	54.34	50.24	109.96	576.62	698.97	1.099.99	1.047.60	1,373.71	402.87	97.13	470.99
1972	64:83	59.54	55.56	51.59	332.00	435.70	627.94	881.32	855.87	851.15	647,00	247.40	425.82
1973	86.61	60.78	63.80	102.20	263.97	117.26	225.32	320.90	1,149.99	956.18	318,26	215.70	323.41
1974	93.38	57.71	53.00	51.10	148.13	592.02	892.45	1,474.86	1.379.36	1,021.19	355.43	109.77	519.03
1975	70.72	65.05	60.81	76.92	431.64	800.78	428.42	1,022.44	1,030.96	1,126.37	364.55	136.84	467.96
1976	72.46	65.50	61.25	57.10	59.18	236.16	862.88	990.74	1,200.60	1,296.39	408.74	96.34	450.61
1977	69.42	65.74	63.56	140.28	135.33	563.07	825.72	635.10	1,605.70	1,083.39	283.93	165.26	469.71
1978	15.87	68.49	64.28	320.90	238.47	470.65	730.14	1.088.56	1,756.62	1,223.36	397.69	130.97	547.37
6261	86.61	74.39	145.33	341.81	541.02	770.96	1,617.27	1,484.56	724.74	1,173.04	579.73	141.59	640.09
1980	87.47	80.06	75.02	70:26	417.00	1,017.82	936.13	876.15	1,164.89	915:53	518.70	136.10	524.59
1981	82.98	124.66	81.95	140.03	197.81	971.32	813.20	1,342.12	822.22	1,018.37	449.17	121.08	513.74
1982	83.09	77.37	104.63	371.21	358.20	554.17	998.63	951.25	1,667.13	810.53	569.79	251.58	566.46
1983	95.58	82.99	78.21	255.96	84.67	427.54	880.80	1.227.78	827.64	1,664.64	1.008.32	213.86	570.67
1984	114.03	89.67	81.41	16.96	371.50	1,067.69	823:78	1,832.53	1.320.80	944.87	243.23	104.86	591.19
1985	90.51	85.41	80.67	131.35	264.97	440.23	688.66	819.94	995.12	1,373.78	427.14	207.09	467.07
1986	98.76	83.35	78.95	74.87	315.54	535.11	934.64	1.537.27	1,126.58	1,195.46	454.87	221.73	554.76
1987	98.93	87.83	83.34	80.35	83.71	435.76	972.79	807.97	845.78	729.23	539.77	224.92	415.87
1988	92.93	82.15	78.16	74.53	74.23	449.90	714.52	- 481:91	450.30	1.061.33	620.25	145.39	360.47
Mean	78.20	67.49	68.49	128.65	251.17	549.93	768.74	1.024.61	1.062.69	1.060.58	512.26	165.60	478.20

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Table 3.11 Parameters for Discharge Estimate at Damsites

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<b>Basin</b> Name	Dai Ninh	Dong Nai 3	Dong Nai 4	Dong Nai 6	Ta Lai	Dong Nai 8
Rain(mm)	1,591.50	1.880.70	2,805.60	2,788.10	2,798.50	2.328.70
c.a.(km2)	1.158.00	2,428.00	169.00	2,521.00	2.574.00	197.00
Factor*		0.24	0.02	0.36	0.37	
-						
Basin Name	Ham Thuan	Ta Pao				
Rain(mm)	2,531.30	2,315.10				
c.a.(km2)		637.00				
Basin Name	Thac Mo	Can Dong	Fu Mieng	P. Hoa (dam)	P. Hoa (gauge)	
Rain(mm)	2,425.00	2,393.30	2,325.00	2,304.00		
c.a.(km2)		1,240.00	670.00	1,137.00		-
Factor**			0.19	0.31	0.14	

\* percentage of the total rainfall volume of each sub-basin

to the total rainfall volume of Ta Lai basin minus Dai Ninh basin

\*\* percentage of the total rainfall volume of each sub-basin

to the total rainfall volume of Phuoc Hoa basin minus Thac Mo basin

	Num			and Nor Read	C COURSE OF THE C	1 m 1 m	(Insurant)					Man Butter			10.00	Total Total	444									Une : a U
	/	Dar Ninh	Ort IN Jun	UNK Net 4. C	iong Nar G	1	Dong Nut X	Confl. with	Total .	ž	3			7	Eurostic -		1	huc Molt Can	· · _ ·		17			1.5	welh HamAn	
	(mm)v	S In 1	Ē	:   ;;	-	2.7'W.S	1	1		U VVV C	2.511.6		2.42.4		-		+-	i e	1	3	1				3	Ē
	(imi)	1.1%	2,454	£4)	2.21	2.574		4	541.4	373	(WE)	114	140.5	4,0001	1042	14.025	2								Ľ	
		××.	2.5	5	1	2		4.41	27.4.72	12 M	14 H	1111	25°UX	167.41	24.45	=10,W	10.4		41,701							11 ×00.35
	. 63	ž.	10.49	- <b>(2</b> 01	137.32	10.2	:	197	10.12	14°39	9.8	20.25	97.24	194.61	2	1. XXV	N.7X		\$5° \$2							
		2	98.74	5	¥ 12	75.49		5	8	N.	21.45	1	10.5		15.97	102.74	W.		202			÷				
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		( g	) =	012		1	÷	615		3	1175	1		2 X.	È.	8	13		ÿ							
		3	50	010	E	Ş	:	0.10	6.65	4.07	15,03	2 <b>~</b> ~4	21.36	42.81	2.74	32.00	90		2.61							
	*	3	141	10	4.34	4		uro .	20.44	10.01	11.12	Carol 1	12.42	10, 72	1.1	107.04	¥.		28.05		1					
		2	2.85	8	34	A I		5	1.101	10	76.20	52	10.2	217.05	11,81	2	F.		5		:					
			8 9	1.00	12.21	200	۰.	22.0		2 2		10.75	14.24	197 P.	1 1 1	DX-34C	CN C1		14.00							45.27 1.045.60 1.045.60
			20.45	No.	212.16	20.02	19		44 W W	105.00	- S6-71	44.24	160.51	221.74	54.29	104.71	14.10		6K.Al							
1         1		70.04	115.02	12761	214.76	291.103	18.81	3.95	X44.41	24.24	10. KN	JX.4 -	HT/H	255.96	63.52	1,200,304	15.37		1.12							
		4	E S	6X'1	140.62	AC.05		Č.	11.104	12.4)	¥455	06761	ents.	132.59	33.04	020.99	80'X		15736							
100         300 <td></td> <td>14.7%</td> <td>W/15</td> <td>6.02</td> <td>12.9%</td> <td>91.42</td> <td></td> <td>Ş</td> <td>277.57</td> <td>1.24</td> <td>¥.11</td> <td>5.11.</td> <td>14 CO</td> <td>10.11</td> <td>17.14</td> <td>724.77</td> <td>- 4,14</td> <td></td> <td>\$0'0¥</td> <td></td> <td>•</td> <td></td> <td></td> <td></td> <td></td> <td></td>		14.7%	W/15	6.02	12.9%	91.42		Ş	277.57	1.24	¥.11	5.11.	14 CO	10.11	17.14	724.77	- 4,14		\$0'0¥		•					
10         100	ş	14.05	21.15	2.40	X 43	X 7		ž	110.70	23	Ţ	3.47	11.55	21.11	1.74	147.60	48.1		14.76							
	_	4. 61	245	ş	SC #	2		9 <b>.</b> 9		1	1.5	\$	2	0, 11	52	2	<b>.</b>		3.14						. •	
		8	<u>.</u>	510	ផ្ត			4r0		8	Ş	54	9	17,66	81	24.35	5		1	÷						
(10         (10         (10)         (		2.19	1	100	6			5			11 Jun	j		0.00		000000	3		17.44							
Method         Method<		1961-11	4.4	5	14,78	14,74	3	0.65		02%	20.00	14.53	62° 44	0.4	1,	1.5%.02	5		60.611							
		ž	<b>10</b> '04	ž	17 23	ž		6.		17.10	SUNV.	11"12	105	16.181	ਸੂ	12.22	\$		2.69]							
		10.15	10.48	8.72	2	0.21		994		8 st :	9	R	115.67	231.47	1796	600. I K	424 1	•	29.30							
No.         Visto         V	:	1	1.15	20	2			i f		4	(m. 1)			1.02		11 IUX										
17.4         3.17         3.65         3.59         3.59         3.59         3.59         3.59         3.59         3.59         3.59         3.59         3.59         3.59         3.59         3.59         3.59         3.59         3.59         3.59         3.59         3.59         3.50 <th< td=""><td></td><td>24.74</td><td>11.54</td><td>15</td><td>140.94</td><td>1</td><td></td><td>0%.4</td><td></td><td>1011</td><td>1946.12</td><td>22.16</td><td>1912</td><td>147.67</td><td>122</td><td>611.17</td><td>0112</td><td></td><td>N.N</td><td></td><td></td><td>÷</td><td></td><td></td><td></td><td>:</td></th<>		24.74	11.54	15	140.94	1		0%.4		1011	1946.12	22.16	1912	147.67	122	611.17	0112		N.N			÷				:
		17.64	52.17	3.0	N0.29	N2.29		3,40		V. 4	24.73	10.57	35.14	70.446	17.04	305.12	4.23		17.62							
	8	Į	19.36	2.01	2.2	30.59	÷.	17		£	57.9 7	5.67	ł,	17.85	<b>J</b> .	¥.	1.S	÷	10.54	÷	÷					
	:	8	6	6	5	5.40		0.47		<b>ਵ</b> (	242	257	2	16.16	1	50 C	S i		3.16							
11.10         3.33         0.24         5.30         5.30         5.30         5.30         5.40         5.11         2.30         5.30         5.40         5.30         5.40         5.30         5.40         5.30 <t< td=""><td></td><td></td><td>5</td><td>016</td><td>i i i</td><td></td><td></td><td>210</td><td></td><td></td><td>60 S.</td><td>190</td><td></td><td></td><td></td><td>14.14</td><td></td><td></td><td>707</td><td></td><td></td><td></td><td>1</td><td></td><td></td><td></td></t<>			5	016	i i i			210			60 S.	190				14.14			707				1			
Z*29         [11]         [136         [139         [136         [140         [141         [136         [130         [131         [130         [131         [130         [131         [130         [131         [130         [131         [130         [131         [130         [131         [130         [131         [130         [131         [130         [131         [130         [131         [130         [131 <th< td=""><td></td><td>\$</td><td>200</td><td>AL.0</td><td>\$.10</td><td>ន្ត</td><td></td><td>0,42</td><td></td><td>2.41 X</td><td>N/N</td><td>5</td><td>24.A2</td><td>\$¥ \$\$</td><td>4.65</td><td>SULS.</td><td></td><td></td><td>56 11</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></th<>		\$	200	AL.0	\$.10	ន្ត		0,42		2.41 X	N/N	5	24.A2	\$¥ \$\$	4.65	SULS.			56 11							
Zulio         Hand         Hand <t< td=""><td></td><td>W.'W</td><td>214</td><td>Ŕ</td><td>N.XI</td><td>11.41</td><td></td><td><u>R</u></td><td></td><td>0.01</td><td>\$8.69</td><td>11-112</td><td>20,83</td><td>141.W</td><td>12.45</td><td>236,00</td><td>3.01</td><td></td><td>5.61</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></t<>		W.'W	214	Ŕ	N.XI	11.41		<u>R</u>		0.01	\$8.69	11-112	20,83	141.W	12.45	236,00	3.01		5.61							
44.00         11.04         10.01 <th< td=""><td></td><td>14142</td><td>IR.M.</td><td>8</td><td>5</td><td>N 62</td><td>÷</td><td>07.1</td><td></td><td>13.74</td><td>1.0</td><td>AV I.</td><td>w7.</td><td>74.22</td><td>14.05</td><td>206.19</td><td>05</td><td></td><td>57.41</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></th<>		14142	IR.M.	8	5	N 62	÷	07.1		13.74	1.0	AV I.	w7.	74.22	14.05	206.19	05		57.41							
77.90         10.00         15.40         10.00         7.40         10.00         7.40         10.10         11.10         1					0.01	11.201		0				00.82	07702	10.00	9 7 9		0.1		100	÷						
NUM         11.30         17.46         17.41         16.41         1		1.6.0	10001	10.45	3,7			1.5			125.99	28.85	20.84	190.47	11 M	704.57	100		21.17			۰.				
11.3*9         KG3         KG4         KG3         KG4         KG4 <thkg4< th=""> <thkg4< t<="" td=""><td></td><td>ž</td><td>113.511</td><td>11.79</td><td>174 KS</td><td>174.19</td><td></td><td>K15</td><td></td><td>17.93</td><td>WIN</td><td>R X</td><td>¢ ¥</td><td>130, 55</td><td>0. 64</td><td>744.7</td><td>15%</td><td></td><td>1. 98</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></thkg4<></thkg4<>		ž	113.511	11.79	174 KS	174.19		K15		17.93	WIN	R X	¢ ¥	130, 55	0. 64	744.7	15%		1. 98							
11.48         1.1.88         1.1.8         1.1.8         1.1.8         1.1.8         1.1.8         1.1.8         1.1.8         1.1.8         1.1.8         1.1.8         1.1.8         1.1.8         1.1.8         1.1.8         1.1.8         1.1.8         1.1.8         1.1.1         1.2.0         1.2.1         2.2.6         1.2.1         1.2.1         2.2.6         1.2.1         2.2.6 <t< td=""><td></td><td>19.51</td><td>×5.26</td><td>97X</td><td>12.161</td><td>134.47</td><td></td><td>6.12</td><td></td><td>X,48</td><td>21.30</td><td>3.3%</td><td>4</td><td>A9.16</td><td>26.57</td><td>NC LOS</td><td>6.43</td><td>÷</td><td>29.17</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></t<>		19.51	×5.26	97X	12.161	134.47		6.12		X,48	21.30	3.3%	4	A9.16	26.57	NC LOS	6.43	÷	29.17							
(6)%         9.%         (10)         (5.1)         (5.4)         7.11         0.66         (1.0)         7.01         7.13         2.06         7.01         7.14         <	ç.	\$	W. IC	:5	44.09	10.0		2.40		3,6	10.04	•35	11.21	30.30	10.17	142.71	5		10.11					-		
WM         LOM         D11         LOM         D13         D24         LAM         TAM         D23         D24         LAM         TAM         D24         LAM         TAM         D24         LAM         LAM         D24         LAM         LAM         D24         LAM         LAM         D24         LAM         LAM         LAM         D24         LAM         LAM <thlam< th="">         LAM         <thlam< th=""> <thlam< th=""> <thlam< th=""></thlam<></thlam<></thlam<></thlam<>		10.94	9,80	8	12.21	15.54	÷	0.166		ŝ	7.61	22.5	10,61	23.67	14	NO.64	8		214							
J.J.       L.D.       G.D.       L.D.       G.D.       L.D.       G.D.       L.D.		Ş	<u>s</u> i	2	8	2		924		8	09.6	91.4		2.73	1	44.74	0.57		5.41							
1.2.1         1.2.2         1.2.1         1.2.1         1.2.1         1.2.1         1.2.1         1.2.1         2.2.0         1.2.1         2.2.0         1.2.1         1.2.1         1.2.1         1.2.1         2.2.0         1.2.1         1.2.1         1.2.1         1.2.1         1.2.1         1.2.1         2.2.0         1.2.1         2.2.0         1.2.1         2.2.0         1.2.1         2.2.0         1.2.1         2.2.0         1.2.1         2.2.0         1.2.1         2.2.0         1.2.1         2.2.0         1.2.1         2.2.0         1.2.1         2.2.0         1.2.1         2.2.0         1.2.1         2.2.0         1.2.1         2.2.0         1.2.1         2.2.0         1.2.1         2.2.0         1.2.1 <th< td=""><td></td><td></td><td><u>q</u> '</td><td>3</td><td></td><td>5</td><td></td><td></td><td></td><td>5</td><td></td><td>2.6</td><td>1011</td><td>4179</td><td>5</td><td>19.47</td><td>8</td><td></td><td>ž</td><td></td><td></td><td></td><td></td><td></td><td>÷</td><td></td></th<>			<u>q</u> '	3		5				5		2.6	1011	4179	5	19.47	8		ž						÷	
72.04 72.27 0.01 142.29 145.00 VAI AND 479.14 42.01 14.40 01.00 12.44 45.54 44.15 11.60 72.79 177.01 177.01 12.04 55.11 175.96 74.57 175.01 127.04 55.11 175.96 74.57 175.01 127.04 55.11 175.96 75.56 75.10 127.04 12.11 125.06 125.44 15.17 125.01 127.12 1546.15 144.57 125.06 125.44 15.17 125.01 127.12 1546.15 144.57 125.06 125.44 15.17 125.01 127.12 1546.15 144.57 125.06 125.44 15.17 125.01 127.12 1546.15 144.57 125.06 125.44 15.17 125.01 125.75 44.55 144.50 125.76 125.76 125.75 144.57 125.75 144.57 125.75 144.57 125.75 144.57 125.75 144.57 125.75 144.57 125.75 144.57 125.75 144.57 125.76 125.47 125.10 177.01 127.12 1546.15 140.01 127.11 1346.15 140.01 134.11 1346.15 140.01 134.11 1346.15 140.01 134.		1 N N	5 9		2	3		ale c	ſ	101		5	1 2	DV PS1	5		197									
46.51 INC.RE 1906 20290 201420 INC.0 11.07 INC.0 11.07 INC.0 155.09 10.014 46.59 10.014 46.59 10.014 12.01 12.05 155.09 10.014 12.01 12.05 155.09 155.09 15.00 12.010 12.01 12		5	88	10.6	142.19	45,45	4	5		64 04	057441	05.65	12.44	1 22		ALA.			10.41							
33.35 200.69 20.84 106.85 106.85 104.84 14.84 24.72 101.15 26.54 25.65 105.05 102.05 1		15.5	141.02	19.08	242.50	249.42	97¥	11.47		20.56	109.14	, wo	155.09	310.69	OA.NU	N. W.S.	1.1.20		2							
70.2W 244.2 27.4W 41.247 25.1% 42.4% 124.7% 124.4% 27.1% 100.0% 42.7% 142.21 25.5% 15.44 15.19.27 20.6% 24.7% 15.4% 15.4% 15.7% 25.7% 25.2% 40.3% 22.4% 25.4% 25.4% 15.4% 25.5% 25.2\% 25.2		13.35	200.69	20.14	104.87	16.51	10.9	14.46		27.22 22	1.0	14.41	SC.151.	205.24	54.42	05,000,1	13.92		144.97	_				•••		
24.19 26.59 25.51 275.15 382.51 25.62 17.36 1.102.02 18.62 64.77 26.29 27.72 19.584 7.249 25.549 25.54 200 4.75 7.251 1.60 4.751 25.55		70,24	12 Mar	2	412,877	23,12	22	06'61		21.10	100.001	10.7261	I C CP 1	5.3	1.1.4.1	1. 6.161.201										
		1×147				10.000					Ĩ	-		20.2.12	2	15,10,1	10.02		143,440; 	-			÷		~	· · ·

Marker (section)         Table (se	Nurth		Cher Nu Ri	WALLAND) -	V (hr Th An	(Re-War)		-1	· 1	- 31	Ngu Rimit	1		Tn An	Yound Co	Corfl. with		' F	ě	Be River			1		
		Cong Nu 3 domento	Dong Nui 4: dumuto :	Cong Nut-61 durrente	Tu Los	Demy: Nas N. C	Conf. with	1	ð		9 0 8 8			T.		•	Max Mur Ca umaker Ca		Michie Phi	Ac Har 71					ž
	1212	1	Í.		45.24	2.975	51K	134,45	3.065	14.63	Ţ	20.7%	41.66	tates	140.15	÷	Jon NG	7.73	4.00%	7.¥2	TTC	16.20	72.82	04.040	11,112
	50.11			÷	04.6	0.74	0.62	w.ce	12.2	1.17	3,49	29.11	ă E	3.47	65,81	0.944	H W	1.21	0.0	÷	65.0	÷.		105.04	4.64
	<b>5</b> }		_		a a	9	7	10.01	\$	472	1	<b>9</b> 01	14 OZ	<b>A</b>	35.89	0.45 0	\$	3.03		7.67	8	7.4%		£∵€	
					1	120					5	21.22		1.1	10.00	2	¥ :		9		<u>A</u>	1		S .	5
					Ş	100	ð	1.72.07	9.19	20 KU	10.20	100.71	00102		12.54	9	( ) ( ) ( ) ( )	25,69	1997	27 64	0.1	1	_	LOUI La sed	1
	1.1	-			60°.4	0 VO	7.80	10.001	15.26	1420	89.65	18, 02	170, 47	16.91	W.C. 6	*	30.80	64,76	NO.	0.69	27.45	<b>V5.15</b>		10.54	0.15
	2.00				155.17	10.45.	7,76	AK, DKA		135.73	58.02	192.87	10,040	1.71	VILLA	11.78	144,95	07.77	44	14.45	43.26	2 12		511.13	12.00
	4,1			•	THE P	14.14	10"11	647.749	1.00	21,15	Ę,	10.61	60.35	16.54	201.55	10.23	10, 10	244, 44X	12.14		2112	10.15		1000	N.
	3.3.0				144.49	12.16	\$	VI W	14.90	35.01	15"112	71.16	1,56,65	40.37	205.1K	12.4	373.47	189,62	1978	102.305	24.26	21.22		11. SH	HA.A.
	11-12	•			NC-SV1	10.01	140	OX CAN	2.00	50 H		94.45	0 11	31.40	545.10	00	104,23	12,121	16769	117,60	53.5%	1. W. K		221,50	1
	44'61			_	102,44	21	- <b>- - - - - - - - - -</b>	11.17	4.76,	17.59	1.52	25.00	E g	20.24	183.32	AX 7	9	32.70	41.73	2K.#7	13.15	34,446		¥2.44	10.65
	2.4				45.72	10	Ţ,	17.71	101	1.13	4.70	1.4.4	î F	WY:6	- HC-CXI	ž A	A. 16	N 01	14	10°	4.14	17.80		265.49	11.42
	171				3.2	5	8	2.5	2	1500	Į	1	EV.NI	4.00	×7.21	1.1	24.60	4 1	Q. I	2.1V	8	9.10		- <b>3</b> . X	5.74
	171				3	0.44	100	29.02	8		577	() <b>*</b> 'X	16.43	3.(3)	19.75	9.°0	21.91	A.61	<u>8</u>	3.14		7.57		73,200	ġ
	2					12	0.17	10,77	14F.		5.50	7.46	13.00	\$ 1	15.12	30.0	97.4	6.10;	3,20	÷.	2,45	1.47		11.10	1.7
	2 				9	រុរ ខ្មែរ រ	0.16	10.11	11.82	13.65	£.	62.00	ŝ	1.50	1-2.05	X.	18.4	1		8.2	3	1.42	_	50'E	7.83
No.         No. <td>*</td> <td></td> <td></td> <td></td> <td>Å,</td> <td>Į.</td> <td>0,16</td> <td>10.26</td> <td>16.21</td> <td>1.2</td> <td>1.1</td> <td>8 *</td> <td>10.45</td> <td>90'01</td> <td>1.0.1</td> <td>4</td> <td>2.11</td> <td>а Н</td> <td><b>6.</b> I</td> <td>10.01</td> <td>120</td> <td>14.02</td> <td></td> <td>244.76</td> <td>870</td>	*				Å,	Į.	0,16	10.26	16.21	1.2	1.1	8 *	10.45	90'01	1.0.1	4	2.11	а Н	<b>6.</b> I	10.01	120	14.02		244.76	870
No.         No. <td>1</td> <td></td> <td></td> <td></td> <td></td> <td>213</td> <td>4.1</td> <td>5</td> <td>a H H H H</td> <td>113, 931</td> <td>10.04</td> <td>164,02</td> <td>16.307</td> <td>24.41</td> <td>142.44</td> <td>06</td> <td>215,445</td> <td>6.15</td> <td>1.2.1</td> <td>5</td> <td>42</td> <td>A7.09</td> <td></td> <td>115.2077</td> <td>12.41</td>	1					213	4.1	5	a H H H H	113, 931	10.04	164,02	16.307	24.41	142.44	06	215,445	6.15	1.2.1	5	42	A7.09		115.2077	12.41
11.1         11.1 <th< td=""><td>3</td><td></td><td></td><td></td><td></td><td>7.64</td><td>5.62</td><td>136.46</td><td>22</td><td>148.1.1</td><td>41.72</td><td>210.49</td><td>51.5</td><td>43.36</td><td>¥21.75</td><td>10.49</td><td>272.99</td><td>57.15</td><td>1.1</td><td>5.5</td><td>20.77</td><td>10,401</td><td></td><td>W.VIC.</td><td>4.74</td></th<>	3					7.64	5.62	136.46	22	148.1.1	41.72	210.49	51.5	43.36	¥21.75	10.49	272.99	57.15	1.1	5.5	20.77	10,401		W.VIC.	4.74
10.1         30.1 <th< td=""><td>10.</td><td></td><td></td><td></td><td></td><td>24</td><td>10.15</td><td>15 CW</td><td>2116</td><td>142.51</td><td>(C</td><td>S. 17</td><td>Y 17</td><td>A- 99</td><td>25,122,1</td><td>1406</td><td>10.57</td><td>51.14</td><td>27.89</td><td>44, 91</td><td>21.37</td><td>NS</td><td></td><td>NAS. NO</td><td>11.04</td></th<>	10.					24	10.15	15 CW	2116	142.51	(C	S. 17	Y 17	A- 99	25,122,1	1406	10.57	51.14	27.89	44, 91	21.37	NS		NAS. NO	11.04
77.8         7.8         7.9 <td>.9.6</td> <td></td> <td></td> <td></td> <td></td> <td>1.1</td> <td>12.76</td> <td>is tox</td> <td>20.45</td> <td>67.62</td> <td>×0.35</td> <td>267.11</td> <td>202-22</td> <td>74. 111</td> <td>1.419,20</td> <td>11.11</td> <td>244.12</td> <td>20.12</td> <td>20,42</td> <td>11-11-</td> <td>20.44</td> <td>117,63</td> <td></td> <td>10104</td> <td>M. 1X</td>	.9.6					1.1	12.76	is tox	20.45	67.62	×0.35	267.11	202-22	74. 111	1.419,20	11.11	244.12	20.12	20,42	11-11-	20.44	117,63		10104	M. 1X
No.         No. <td>212</td> <td></td> <td></td> <td></td> <td></td> <td>Đ,</td> <td>8</td> <td>371.30</td> <td>SY '92</td> <td>00.70</td> <td>A.</td> <td>150.40</td> <td>102.49</td> <td>37.86</td> <td>717.x7</td> <td>4.16</td> <td>131.74</td> <td>61,70</td> <td>× 1</td> <td>Ş. Y</td> <td>EN-PC</td> <td>×7.94</td> <td></td> <td>1,20,04</td> <td>CN.94</td>	212					Đ,	8	371.30	SY '92	00.70	A.	150.40	102.49	37.86	717.x7	4.16	131.74	61,70	× 1	Ş. Y	EN-PC	×7.94		1,20,04	CN.94
No.         No. <td></td> <td></td> <td></td> <td></td> <td></td> <td><u> </u></td> <td></td> <td></td> <td></td> <td>29.72</td> <td></td> <td></td> <td>202</td> <td>97.1</td> <td>1.62</td> <td>5 - 1 </td> <td>N 1</td> <td>2 - N</td> <td>8</td> <td>5ň</td> <td>ð</td> <td>31.14</td> <td></td> <td>01.65</td> <td>4.1</td>						<u> </u>				29.72			202	97.1	1.62	5 - 1 	N 1	2 - N	8	5ň	ð	31.14		01.65	4.1
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MAAD         MAAD         MAD         MAD <thmad< t<="" td=""><td>N.N.</td><td></td><td></td><td></td><td>138,600</td><td></td><td>87</td><td>151.151</td><td>18.74</td><td>62.64</td><td>2.5</td><td>94.74</td><td>14.12</td><td>96.96</td><td>CANY, CA</td><td>8.80</td><td>18 <b>4</b></td><td>115.79</td><td>A0.7X</td><td>102.21</td><td>65 ST</td><td>150.41</td><td></td><td>Taki</td><td>61 G2</td></thmad<>	N.N.				138,600		87	151.151	18.74	62.64	2.5	94.74	14.12	96.96	CANY, CA	8.80	18 <b>4</b>	115.79	A0.7X	102.21	65 ST	150.41		Taki	61 G2
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Wyse         1354         1554         1554         1554         1555         9426         9426 <th< td=""><td>žž.</td><td></td><td></td><td></td><td>97-261</td><td></td><td>AK.9</td><td>425.33</td><td>W.W.</td><td>- 132.0%</td><td>14°</td><td>140,041</td><td>124.23</td><td>55.79</td><td>1,022.1</td><td>11.49</td><td>14 402</td><td>166.45</td><td>X AK</td><td>147.11</td><td>01.00</td><td>201.42</td><td></td><td>100.07</td><td>1.5</td></th<>	žž.				97-261		AK.9	425.33	W.W.	- 132.0%	14°	140,041	124.23	55.79	1,022.1	11.49	14 402	166.45	X AK	147.11	01.00	201.42		100.07	1.5
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		5	19.41	-01'02			<u> </u>			20,40	95. <del>1</del>	14.14	61.121	24.1	10,21	10							
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		24	W. 16	10001						116.87	12.1.2	<b>M</b> 11	600.AS	7,67	14243	51.74							
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		5	N AL	188.66				:		245.44	66-164	8	10,110,1	15:22	307,02	132.00							
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		Ş	¢1.15	\$						88	54.19	14,64	00740	4.7.4	40.45	24.26			. <u>.</u>				i ¥
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		10.42	() + ()	154.26		•				201,314	404,70	52.52	105.44	12.70	2ML.7K	101.26					_		
		10-11	2	INCIN						45-111	14122	91 M	244.02	25.4	1076	45.87					-		
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			102	20102			i.	•		194.16	20.412	1	1.168.05	1.124		14 AC				-	• •		
		ž	19.41	2 1	-		÷		<u></u>	22	10.00	02.00	CX IX	7.4	1001	5							
8 71	4	4.74	70.27	10.57	9	2	2140	5.05	<b>R</b> .78	24,20	54.5	15.74	36.36	1.81	01.138	30.26	13.446	24.72	1217	NJ - 24,772	164, 154 471, 35	14 MAR	
~		ĥ	1.9.1				t	÷.		17,62	25.35	2 × 2	55.961	204	10.21	11,40							
		0.54	54.1	1		10	5		1	27.42	23.24	2	16761	1.6	12.24	2.17						1	

Table 3.12 Estimated Flow at Damsites (4/7)

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		N N			Dony Net	RINCE (BURNER)	mutite To	An Revenue					a Nga Kawar			To An	Toul Toul	1			Ē	c-River			-1						
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		1											3	2.17	55.71	84	74.94	<b>857</b> 0 -	552 X	47.4	2.30	1.87	1.76	6.02	1	104°3V	201	٤			
			17.04					. 4					10.92	16.46	¥7.27	10.01	190.20	2.45	17.41	9. H	10.0	10.15	4.62	15.7%		CITAN	5.0	ř.			
						-						-	*6.77	155,47	MI.M	473	X47.62	10,82	214.45	40'M4	4	W.03	16.42	ž		21.442	A.4.	Į.,			
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										1		-	1	164.04	0. 12	12.64	1.1404,76	9	120.00	2.24	10.86	22.49	2.27	CL 1%		102.04	72.70	70			
										2	:		HE	90.00	145.61	17,04	201, V2	\$	10.76	24.73	12.44	21.X3	\$6.6	01.01		×44,07	1.74	×.			
			5	-	-								57	20.02	20.15	15.45	272.75	.74	27.13	NXX.	4.4	24	15	15.02		OVENE	2				
						:							1017	16.56	81	7.44	140.95	1.80	611	1	1.12	2	0.86	7.32		175.44	7.81	×.			
						•		•		:		2	4,76	15.82	31.70	3,74	70.54	0.91	12.19	YIIY	4	576	8	ŝ		44,44	¥	¥			
												1	6.7	รีม	45.12	3.57	67.AN	0.754	ç	\$05	2.45	4.4	ш.	5.05		95.15	4	5			
			44								1	1	21.13	1.8	155.45	100	1 N2.NK	5	2	ą	22	2	252	0		W.112	24.2	Ы			
No.         No. <td></td> <td></td> <td>4</td> <td></td> <td><b>.</b></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>12.01</td> <td>71 14</td> <td>140.71</td> <td>01.9</td> <td>173.55</td> <td>2.21</td> <td>3.61</td> <td>5.92</td> <td>111</td> <td>8</td> <td>2.14</td> <td>5.43</td> <td></td> <td>201.42</td> <td>×.</td> <td>â</td>			4		<b>.</b>								12.01	71 14	140.71	01.9	173.55	2.21	3.61	5.92	111	8	2.14	5.43		201.42	×.	â			
0.000         1.000 <th< td=""><td></td><td></td><td>SAN .</td><td></td><td>-</td><td>:</td><td></td><td>:</td><td></td><td></td><td></td><td></td><td>26.45</td><td>K7,Y7</td><td>124.15</td><td>10.Nut</td><td>205.49</td><td>597</td><td>15.00</td><td>×</td><td>\$7¥</td><td>2.17</td><td>2</td><td></td><td></td><td>257,422</td><td>¥7(1</td><td>Ā.</td></th<>			SAN .		-	:		:					26.45	K7,Y7	124.15	10.Nut	205.49	597	15.00	×	\$7¥	2.17	2			257,422	¥7(1	Ā.			
mode         mode <th< td=""><td></td><td></td><td>51.455</td><td></td><td></td><td></td><td></td><td>.:</td><td>. •</td><td></td><td>i</td><td>Ē</td><td>Ŧ</td><td>140.67</td><td>267.92</td><td>24.75</td><td>544,85</td><td>56.0</td><td>120.07</td><td></td><td>12.74</td><td>21.45</td><td>ř.</td><td>67 Y2</td><td></td><td>15°W.*</td><td>4 1</td><td>¥</td></th<>			51.455					.:	. •		i	Ē	Ŧ	140.67	267.92	24.75	544,85	56.0	120.07		12.74	21.45	ř.	67 Y2		15°W.*	4 1	¥			
77.00         1000 <t< td=""><td>0000         <th< td=""><td></td><td>47.42</td><td></td><td></td><td></td><td></td><td></td><td>-</td><td>•</td><td></td><td>5</td><td>SV., N</td><td>127.50</td><td>255.56</td><td>16716</td><td>12774</td><td>12.55</td><td>201102</td><td>96'X¥</td><td>40.64</td><td>78,47</td><td>6797 1</td><td>14.50</td><td></td><td></td><td>74.11</td><td>e,</td></th<></td></t<>	0000         0000 <th< td=""><td></td><td>47.42</td><td></td><td></td><td></td><td></td><td></td><td>-</td><td>•</td><td></td><td>5</td><td>SV., N</td><td>127.50</td><td>255.56</td><td>16716</td><td>12774</td><td>12.55</td><td>201102</td><td>96'X¥</td><td>40.64</td><td>78,47</td><td>6797 1</td><td>14.50</td><td></td><td></td><td>74.11</td><td>e,</td></th<>		47.42						-	•		5	SV., N	127.50	255.56	16716	12774	12.55	201102	96'X¥	40.64	78,47	6797 1	14.50			74.11	e,			
No.         No. <td></td> <td></td> <td>2.0</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>76.55</td> <td>124.50</td> <td>\$1015</td> <td>out.tel</td> <td>1,143,64</td> <td>14,60</td> <td>1935</td> <td>126.1</td> <td>\$¥10</td> <td>14.52</td> <td>52.17</td> <td>174,78</td> <td></td> <td>×17.7%</td> <td>1.1.3</td> <td>ล้</td>			2.0										76.55	124.50	\$1015	out.tel	1,143,64	14,60	1935	126.1	\$¥10	14.52	52.17	174,78		×17.7%	1.1.3	ล้			
Num         Title         T			12 V. 74										41.68	134.57	11 II	W.M	1,262.20	14.11	162.68	10.08	42.11	70.82	12.26	61.11.		1.1	117				
10.1         10.1 <th< td=""><td></td><td></td><td>200</td><td></td><td></td><td>:</td><td></td><td></td><td></td><td></td><td></td><td></td><td>07.AK</td><td>112.13</td><td>24.80</td><td>No.</td><td>X15,44</td><td>10.66</td><td>71.21</td><td>45.60</td><td>CA.52</td><td>40,25</td><td>14.14</td><td>57.42</td><td></td><td>102.90</td><td>49.10</td><td>2</td></th<>			200			:							07.AK	112.13	24.80	No.	X15,44	10.66	71.21	45.60	CA.52	40,25	14.14	57.42		102.90	49.10	2			
100         100 <td></td> <td></td> <td>Ę F</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>:</td> <td></td> <td>16.04</td> <td>55.33</td> <td>110.011</td> <td>14.12</td> <td>147.14</td> <td></td> <td>10.01</td> <td>1</td> <td>12.04</td> <td>20.25</td> <td>5</td> <td>2H.AK</td> <td></td> <td>47.274</td> <td>21.34</td> <td>₽.</td>			Ę F								:		16.04	55.33	110.011	14.12	147.14		10.01	1	12.04	20.25	5	2H.AK		47.274	21.34	₽.			
100         100 <td></td> <td>~</td> <td>AT AL</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>507</td> <td>20.02</td> <td>40.14</td> <td>6.82</td> <td>12.021</td> <td>54.1</td> <td>25.44</td> <td>7.80</td> <td>4,10</td> <td>61.25</td> <td>41.5</td> <td>13.65</td> <td></td> <td>141.34</td> <td>×</td> <td>•</td>		~	AT AL										507	20.02	40.14	6.82	12.021	54.1	25.44	7.80	4,10	61.25	41.5	13.65		141.34	×	•			
(1)         (1) <td></td> <td>2</td> <td>14.44</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>-</td> <td>17.76</td> <td>35.01</td> <td>2</td> <td>67.15</td> <td>0.166</td> <td>18,35</td> <td>21.16</td> <td>54.0</td> <td>\$</td> <td>0.71</td> <td>5.75</td> <td></td> <td>10.10</td> <td>4.36</td> <td>-</td>		2	14.44										-	17.76	35.01	2	67.15	0.166	18,35	21.16	54.0	\$	0.71	5.75		10.10	4.36	-			
100         101 <td></td> <td></td> <td>M. V.I</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>1.14</td> <td>57,91</td> <td>9. E</td> <td>127</td> <td>41 .CK</td> <td>6.7</td> <td>11.12</td> <td>50.1</td> <td>1,600</td> <td>2.04</td> <td>2</td> <td>ŝ</td> <td></td> <td>NK.06</td> <td>25.2</td> <td></td>			M. V.I										1.14	57,91	9. E	127	41 .CK	6.7	11.12	50.1	1,600	2.04	2	ŝ		NK.06	25.2				
NI         NI<	Image:         Image:<		10.97									÷	1911	72.M.S.	157.49	10,01	189'AN	ă	89. C	4.9%	85	1.37	8	2.00		217.27	4.67	5.1			
			2										20	20,00	A. 14	100	1.5.15	0.RI	N L	4.07	1	3.60	3	2		. L' 64	3.94	7			
	True         True <th< td=""><td></td><td>G</td><td>,</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>х<b>.</b>П</td><td>14.42</td><td>154.29</td><td>15,91</td><td>301.60</td><td>9VV</td><td>9.21</td><td>Ļ</td><td>4</td><td>4.17</td><td>8</td><td>6.45</td><td></td><td>114.11</td><td>14.55</td><td>2</td></th<>		G	,									х <b>.</b> П	14.42	154.29	15,91	301.60	9VV	9.21	Ļ	4	4.17	8	6.45		114.11	14.55	2			
77.1         77.1         77.1         77.2         77.1         77.2         77.1         77.2         77.1         77.2         77.1         77.2         77.1         77.2         77.1         77.2         77.1 <th< td=""><td>Number         Number         Numbr         Numbr         Numbr</td></th<> <td></td> <td>12.02</td> <td></td> <td>:</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>41.30</td> <td>147.29</td> <td>200.24</td> <td>60°.04</td> <td>110.64</td> <td>27.4</td> <td>147,53</td> <td>1.5</td> <td>0.47</td> <td>2.00</td> <td>20.8</td> <td>X. 65</td> <td></td> <td>101-101</td> <td>*</td> <td>5</td>	Number         Numbr         Numbr         Numbr		12.02		:								41.30	147.29	200.24	60°.04	110.64	27.4	147,53	1.5	0.47	2.00	20.8	X. 65		101-101	*	5			
(11)         2000         2000         7001         2000         7001         2000         7001         2000         7001         2000         7001         2000         7001         2000         7001         2000         7001         2000         7001         2000         7001 <th< td=""><td>0.144         3000         3004         1030         1030         7030         7030         <t< td=""><td></td><td>74.74</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>10'11</td><td>189.72</td><td>05,0%5</td><td>45.15</td><td>N55,72</td><td>10.92</td><td>11, 20</td><td>1</td><td>21.24</td><td>39.16</td><td>AN. 71</td><td>61.15</td><td></td><td>wy521**</td><td>1</td><td>Ņ</td></t<></td></th<>	0.144         3000         3004         1030         1030         7030         7030 <t< td=""><td></td><td>74.74</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>10'11</td><td>189.72</td><td>05,0%5</td><td>45.15</td><td>N55,72</td><td>10.92</td><td>11, 20</td><td>1</td><td>21.24</td><td>39.16</td><td>AN. 71</td><td>61.15</td><td></td><td>wy521**</td><td>1</td><td>Ņ</td></t<>		74.74										10'11	189.72	05,0%5	45.15	N55,72	10.92	11, 20	1	21.24	39.16	AN. 71	61.15		wy521**	1	Ņ			
			91.46				1	. :					75.82	10.01	2 M WH	17.76	1.473.82	14'41	10.012	14 12	41.15	12.49	5	124.07		2,047,04,	1.13	ų.			
memory         value         value <t< td=""><td>Matrix         Matrix         Matrix&lt;</td><td></td><td>132.81</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>P1 (60</td><td>230.45</td><td>62.75</td><td>\$2.03</td><td>1.554.60</td><td>19.54</td><td>217.53</td><td>101.19</td><td>WW N</td><td>14.32</td><td>1970</td><td>11.05</td><td></td><td>502</td><td>575</td><td></td></t<>	Matrix         Matrix<		132.81										P1 (60	230.45	62.75	\$2.03	1.554.60	19.54	217.53	101.19	WW N	14.32	1970	11.05		502	575				
	Desi         Corr         Corr <th< td=""><td></td><td>40.07</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>42.XN</td><td>\$. 1</td><td>145.77</td><td>40.99</td><td>1.6.91</td><td>- 26°6</td><td>2 4</td><td>70.52</td><td>17.27</td><td>62.60</td><td>R A</td><td>19.10</td><td></td><td>263.09</td><td>1</td><td><b>7</b>1 -</td></th<>		40.07										42.XN	\$. 1	145.77	40.99	1.6.91	- 26°6	2 4	70.52	17.27	62.60	R A	19.10		263.09	1	<b>7</b> 1 -			
	Z1         1         1         2         2         2         2         1         1         2         1         2         1         2         1         2         1         2         1         2         1         2         1         2         1         2         1         2         1         2         1         1         2         1         2         1		102				1						55-11	17.70	÷.	15.82	ž		26.4	¥ 9		8	99	8		0	12.04	ñ i			
Z271         112         0.01	2011         113         0.00         120         100 </td <td>•</td> <td>21,42</td> <td></td> <td></td> <td></td> <td>:</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>1</td> <td>2</td> <td></td> <td>4</td> <td>1.01</td> <td>ř.</td> <td>6.6</td> <td>1074</td> <td></td> <td>N.</td> <td></td> <td></td> <td></td> <td></td> <td>00</td> <td>- i -</td>	•	21,42				:						1	2		4	1.01	ř.	6.6	1074		N.					00	- i -			
	1000         200         103 <td></td> <td>23.71</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>S.</td> <td>8</td> <td>10.00</td> <td></td> <td>1612</td> <td></td> <td>5</td> <td></td> <td></td> <td>5</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>-</td>		23.71										S.	8	10.00		1612		5			5						-			
MAND         2700         OCM         413         423         OLM         700 </td <td>Model         2.70         0.23         4.13         6.23         0.04         <th0.04< th="">         0.04         0.04         <th< td=""><td></td><td>16.00</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>÷</td><td></td><td></td><td>AN 11</td><td>5</td><td></td><td></td><td>7071</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></th<></th0.04<></td>	Model         2.70         0.23         4.13         6.23         0.04 <th0.04< th="">         0.04         0.04         <th< td=""><td></td><td>16.00</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>÷</td><td></td><td></td><td>AN 11</td><td>5</td><td></td><td></td><td>7071</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></th<></th0.04<>		16.00									÷			AN 11	5			7071												
0.00         1.00         0.00         1.00         0.00         1.00         0.00         1.00         0.00         1.00         0.00         1.00         0.00         1.00         0.00         1.00         0.00         1.00         0.00         1.00         0.00         1.00         0.00         1.00         0.00         1.00         0.00         1.00         0.00         1.00         0.00         1.00         0.00         1.00         0.00 <th< td=""><td>Mode         Mode         <th< td=""><td></td><td>3</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>497</td><td>41.04</td><td>10 m</td><td>2</td><td>and it.</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></th<></td></th<>	Mode         Mode <th< td=""><td></td><td>3</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>497</td><td>41.04</td><td>10 m</td><td>2</td><td>and it.</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></th<>		3										497	41.04	10 m	2	and it.														
Matrix         Like         Matrix         Like         Matrix         Like         Matrix         Like         Matrix         Like         Matrix         Like         Like <thlike< th=""> <thlike< th=""> <thlike< th=""></thlike<></thlike<></thlike<>	Matrix         Matrix <th matrix<="" th=""> <th matrix<="" th=""> <th matrix<<="" td=""><td>÷</td><td>2</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>27.701</td><td>A 017</td><td>1</td><td>TT LT</td><td></td><td>14.47</td><td>10.00</td><td></td><td>6.0</td><td>4.24 C</td><td>10</td><td></td><td>50 105</td><td>2</td><td></td></th></th></th>	<th matrix<="" th=""> <th matrix<<="" td=""><td>÷</td><td>2</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>27.701</td><td>A 017</td><td>1</td><td>TT LT</td><td></td><td>14.47</td><td>10.00</td><td></td><td>6.0</td><td>4.24 C</td><td>10</td><td></td><td>50 105</td><td>2</td><td></td></th></th>	<th matrix<<="" td=""><td>÷</td><td>2</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>27.701</td><td>A 017</td><td>1</td><td>TT LT</td><td></td><td>14.47</td><td>10.00</td><td></td><td>6.0</td><td>4.24 C</td><td>10</td><td></td><td>50 105</td><td>2</td><td></td></th>	<td>÷</td> <td>2</td> <td></td> <td>27.701</td> <td>A 017</td> <td>1</td> <td>TT LT</td> <td></td> <td>14.47</td> <td>10.00</td> <td></td> <td>6.0</td> <td>4.24 C</td> <td>10</td> <td></td> <td>50 105</td> <td>2</td> <td></td>	÷	2											27.701	A 017	1	TT LT		14.47	10.00		6.0	4.24 C	10		50 105	2	
Mode         Total         Mode         Total         Mode         Total         Mode         Total         Mode         Total         Mode         Total         Total <thtotal< th=""> <thtotal< th=""> <thtotal< t<="" td=""><td>MAN         WAN         MAN         MAN<td>÷.,</td><td>00.64</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>199 PL</td><td>9 11</td><td></td><td>10.01</td><td>7.12</td><td>503</td><td>20.00</td><td>- G - G - G</td><td>14</td><td>el ec</td><td>8</td><td>3</td><td></td><td>14</td><td>4</td><td>1</td></td></thtotal<></thtotal<></thtotal<>	MAN         WAN         MAN         MAN <td>÷.,</td> <td>00.64</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>199 PL</td> <td>9 11</td> <td></td> <td>10.01</td> <td>7.12</td> <td>503</td> <td>20.00</td> <td>- G - G - G</td> <td>14</td> <td>el ec</td> <td>8</td> <td>3</td> <td></td> <td>14</td> <td>4</td> <td>1</td>	÷.,	00.64										199 PL	9 11		10.01	7.12	503	20.00	- G - G - G	14	el ec	8	3		14	4	1			
4.27         12.75         13.74         20.41         7.43         7.44         11.60.77         14.81         22.26         7.43         7.44         7.43         7.44         7.43         7.44 <th7.44< th="">         7.44         7.44</th7.44<>	Matrix         Matrix<						. •		-			. •	10.10	24,48	10 J.M.	14 (H	1.1.6.97	ixvi .	249.57	01.19	17,82	K0.42	10.01	145 74		1.145.05	NA.37	ă			
31.27       11000       12.30       1021       17.34       25.31       17.34       25.41       10.00       12.34       25.41       10.00       12.34       25.41       10.00       15.34       11.34       25.41       11.34       25.31       17.14       10.00       15.34       11.34       25.41       11.34       25.41       11.34       25.41       11.34       25.41       11.34       25.41       11.34       25.41       11.34       25.41       11.34       25.41       11.34       25.41       11.34       25.41       11.34       25.41       11.34       25.41       11.34       11.34       25.41       11.34       15.41       15.44       25.41       15.44       25.41       11.44       25.41       11.44       25.41       11.44       25.41       11.44       25.41       15.44       25.41       15.44       25.41       15.44       25.41       15.44       25.41       15.44       25.41       15.44       25.41       15.44       25.41       15.44       25.41       15.44       25.41       15.44       25.41       15.44       25.41       15.44       25.41       15.44       25.41       15.44       25.41       15.44       25.41       15.44       25.41	31.27       11.060       7.2.6       10.20       12.0       70.20       12.0       70.20       12.0       70.00       72.00       70.00 <th70.00< th=""> <th70.00< th=""> <th70.< td=""><td>•</td><td></td><td></td><td></td><td></td><td></td><td></td><td>-</td><td></td><td></td><td>•</td><td>P F</td><td>2016</td><td>11 4.97</td><td>÷. 14</td><td>1.160.17</td><td>14.61</td><td>232.66</td><td>74.72</td><td>34.01</td><td>09.60</td><td>20,89</td><td>127.27</td><td></td><td>243.43</td><td>TYC.</td><td>1</td></th70.<></th70.00<></th70.00<>	•							-			•	P F	2016	11 4.97	÷. 14	1.160.17	14.61	232.66	74.72	34.01	09.60	20,89	127.27		243.43	TYC.	1			
Quark         Count         Till         None         None         None         <	CON       TATE       WAT       TATE       WAT       TATE       WAT       WAT <t< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>÷</td><td>12.27</td><td>171.64</td><td>10 XIV</td><td>51.42</td><td>21.5</td><td>12.44</td><td>257,191</td><td>0.11</td><td>15.45</td><td>100.07</td><td>45.54</td><td>10.5%</td><td></td><td>1.738.73</td><td>20.00</td><td>- 3</td></t<>											÷	12.27	171.64	10 XIV	51.42	21.5	12.44	257,191	0.11	15.45	100.07	45.54	10.5%		1.738.73	20.00	- 3			
Itell         Ook         318         47.14         Mode         11.97         44.04         11.07         24.64         34.25         14.19         53.91         73.9	Itell         Ook         318         47.14         47.04         11.07         26.06         34.35         14.06         15.30         15.40         15.		, ALAS	_									OVE	44.84	V2.00	ล	NC.0A4	5.62	\$	42.15	- 	37.19	10.01	\$1.99		674.52	0.21				
16.65         10.35         1.48         1.57         0.50         1.57         0.50         1.50         0.51         1.50         0.50         1.50         0.50         1.50         0.50         1.50         0.50         1.50         0.50         1.50         0.50 <th0.50< th="">         0.50         0.50         <t< td=""><td>16.05     10.34     1.84     1.95     3.46     1.95     3.45     1.95     3.45     1.95     3.46     1.97.2     1.27     3.46     1.97.2     1.27     3.46     1.97.2     1.27     3.46     1.97.2     1.27     3.46     1.97.2     1.27     3.46     1.97.2     1.47     1.27     3.46     1.97.2     1.47     1.27     3.46     1.97.2     1.47     1.27     3.46     1.97.2     1.44     3.47     1.41     1.47     1.49     1.46     1.46     1.46     1.47     1.41     1.41     1.41     1.41     1.41     1.41     1.41     1.44     1.41</td><td></td><td>1</td><td></td><td></td><td></td><td>•</td><td></td><td></td><td></td><td></td><td></td><td>UVV.</td><td>21.47</td><td>44,04</td><td>00'11</td><td>20%,43</td><td>2.46</td><td>14.25</td><td>SURE</td><td>10+16</td><td>15.21</td><td>13</td><td>24.49</td><td></td><td>32,027</td><td>12.21</td><td>۰,</td></t<></th0.50<>	16.05     10.34     1.84     1.95     3.46     1.95     3.45     1.95     3.45     1.95     3.46     1.97.2     1.27     3.46     1.97.2     1.27     3.46     1.97.2     1.27     3.46     1.97.2     1.27     3.46     1.97.2     1.27     3.46     1.97.2     1.47     1.27     3.46     1.97.2     1.47     1.27     3.46     1.97.2     1.47     1.27     3.46     1.97.2     1.44     3.47     1.41     1.47     1.49     1.46     1.46     1.46     1.47     1.41     1.41     1.41     1.41     1.41     1.41     1.41     1.44     1.41		1				•						UVV.	21.47	44,04	00'11	20%,43	2.46	14.25	SURE	10+16	15.21	13	24.49		32,027	12.21	۰,			
[3,1]     2.09     0.22     3.40     0.44     0.46     2.46     1.44     5.44     1.45     1.46     0.46     0.46     0.44     0.45       (1,3)     1.20     0.12     1.20     0.42     0.42     0.46     1.34     1.46     1.46     1.46     1.46     0.46     0.46     0.44     0.44       (1,3)     1.20     0.12     1.20     0.42     0.42     1.34     1.34     2.07     0.44       (1,3)     1.20     0.42     0.42     1.34     1.34     1.34     1.34     2.07     0.44       (1,4)     1.20     0.42     0.44     1.34     1.34     1.34     1.34     2.07     0.44       (1,4)     0.42     0.42     0.44     1.34     1.34     1.34     2.07     0.44       (1,4)     1.20     0.42     0.44     1.34     1.34     1.34     1.34     2.07     0.44       (1,4)     1.20     0.42     0.44     1.34     1.34     1.34     3.07     1.24     2.07     0.44       (1,4)     1.20     0.42     0.44     1.34     1.34     1.34     1.34     3.04     1.34     3.04       (1,4)     1.34     1.34	[1,1]       2.0       0.22       1.22       1.20       0.21       1.21       2.00       0.41       0.40       0.20       5.92       2.44       9.277       4.11         1.3.1       1.20       0.12       1.46       1.40       0.40       1.41       1.44       3.00       5.21       0.40       0.50       0.40       5.99       2.41       2.40       3.40       3.50       3.40	×	16.63										1005	14,14	38.85	3.06	107.27	1.10	21.52	3	30	3.5	. vo	10, NK		157.25	200,7				
(1.3.w)     1.20     0.12     1.46     1.40     1.24     1.24     1.24     2.07     0.04       7.01     2.76     0.29     4.29     1.34     1.34     1.34     1.34     1.34     2.72     0.27     1.24     2.07     0.04       7.01     2.76     0.29     4.29     0.34     0.37     1.344     1.344     1.00     1.354     1.24     2.07     0.04       7.01     2.76     0.29     4.24     0.30     1.354     1.344     1.344     1.344     1.344     1.344     2.17     3.06     1.04       7.00     2.79     0.29     4.24     0.30     1.354     1.344     1.346     1.344     1.344     1.344     2.17     3.06     0.34       7.00     2.79     0.29     4.24     0.31     1.344     1.344     1.347     1.34     1.34     1.34     1.354     1.464       7.00     2.79     0.29     2.70     1.444     2.17     1.44     2.17     3.04     1.64       7.00     2.74     1.70     1.354     1.70     1.354     1.70     1.344     2.17     3.04     1.64       7.00     4.244     2.17     1.444     1.170     1.171 </td <td>(130)       (12)</td> <td></td> <td>3</td> <td></td> <td>14.24</td> <td>15 22</td> <td>1.45</td> <td>61.65</td> <td>0.43</td> <td>14.16</td> <td>0.49</td> <td>0.26</td> <td>0.43</td> <td>6.30</td> <td>. 42</td> <td></td> <td>2.27</td> <td>7</td> <td></td>	(130)       (12)		3											14.24	15 22	1.45	61.65	0.43	14.16	0.49	0.26	0.43	6.30	. 42		2.27	7				
7.01         2.76         0.29         4.24         4.24         0.47         0.49         1.944         2.17         1.944         2.144 </td <td>7.00         27.0         <th< td=""><td></td><td>13.84</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>ALK.</td><td>17.21</td><td>15.44</td><td>3,02</td><td>12.12</td><td>0.73</td><td>121</td><td>2.35</td><td>1</td><td>2.07</td><td>1</td><td>5.19</td><td></td><td>\$2.04</td><td>SANS .</td><td></td></th<></td>	7.00         27.0 <th< td=""><td></td><td>13.84</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>ALK.</td><td>17.21</td><td>15.44</td><td>3,02</td><td>12.12</td><td>0.73</td><td>121</td><td>2.35</td><td>1</td><td>2.07</td><td>1</td><td>5.19</td><td></td><td>\$2.04</td><td>SANS .</td><td></td></th<>		13.84										ALK.	17.21	15.44	3,02	12.12	0.73	121	2.35	1	2.07	1	5.19		\$2.04	SANS .				
AVV         2.75         0.30 <sup>1</sup> 4.20 <sup>1</sup> 0.40 <sup>1</sup> 1.44 <sup>1</sup> 1.44 <sup>1</sup> 1.40 <sup></sup>	AUX         273         0.20         4.21         0.40         0.21         0.40         17.10         10.24         10.34         1.40         17.10 <td></td> <td>10.7</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>14.5</td> <td>19,89</td> <td>10,46</td> <td>0.1</td> <td>62.50</td> <td>0.40</td> <td>107</td> <td>17</td> <td>512</td> <td>1,45</td> <td>8</td> <td>5,64</td> <td></td> <td>KK, 70</td> <td>562</td> <td></td>		10.7										14.5	19,89	10,46	0.1	62.50	0.40	107	17	512	1,45	8	5,64		KK, 70	562				
7.00 229 0.20 4.20 4.21 1.51.1 12.15 0.20 4.20 2.61.2 0.21 11.71 12.00 2.67.25 0.267 1.12 10.00 4.24 2.02 2.02 2.02 2.02 2.02 2.02	7.00° 2.279 0.29 4.26 4.26 0.41 0.31 14.26 25.56 66.001 14.26 25.76 14.36 24.776 14.36 24.26 11.29 15.69 15.49 75.62 24.45 11.24 15.64 11.24 15.64 11.24 15.64 11.25 12.51 11.25 12.55 12.51 11.25 12.55 12.51 12.55 12.		\$				. :	. i.				•	14	5,467	107.59	7.07	19460	1.7	11.15	52.9	3.54	2.00	- 127	¥7.		17.05	7,4%				
M.W. M.TS M.W. STUT 4.20 3.00 (15.57) 17.10 20.00 (16.66) 30.00 166.66 30.35 20.66 166.66 30.35 20.56 20.57 11.19 18.85 4.57	MuNI MAS AND SALE SALE SALE SALE SALE SALE SALE SALE		200,2								ŝ	÷	ML.71	121.40	247.76	14.445	241.54	3.66	CA-14	21.51	A.	2	K.65	15'NZ		417,46	2	•			
	- ME UID UN HIN HAN ON AN AN AND NOT HUN TOH AND AN AND TON HAN TOH TOH AND HAN HAN HAN HAN WAN AND AND AND AND AND AND		51712									2	50.00	01-141	111.55	4.2	16,865	<b>9</b> 2	129.46	5	161711	14,82	4.57	2		10,20	N.W.	•			
· 36.75 비행하는 9.55 (41.18) (44.66) 9.35 (5.23.25) 32.45 119.15 51.18 170.14 34.65) 42.94 815.72 10.34 195.07 25.82 25.82 25.82			8		:					•			SI'IX.	11011	10.10	17.64	X13,277	10.04	147.07	14.14	124.62	19	54 C	101 34		1.276.75	1	1			

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Tahle 3.12 Estimated Flow at Damsites (5/)

Table 3.12 Estimated Flow at Damsites (6/7)

Name				1				1	Du Nea Ha	Hum Thum.	Ta Pure	All with	₽	Munth	<u>م</u> ٦	me Nat	They Mo	Cun Dring 1 Fe	A Mining Phr	WAY HAVE PAR	AN HALL CON	Confi. with T	<u>ී</u>	nî, weh - H	547	¥
	On NAN ID	Dur Nich Dang Nu 3, Dang Nu 4, Ding Nu 6	1 D W	1	3	CAN LESS CAL & RUN	Cuter, Marin	-	÷	:					-		-			•						
/unut	durmite	shrring durants	3			Cherrit	ng Nal		Lawor .	- mn	ginujec i D	ony Nu		F	n Andam	A Be	mmure e	- Alland	umaine i d	umsuc 1	Tauk Du		٥	N & Be		¥ ₹
1-	0.0	105.241 10	Ē	141 141	30. W	10,11	51X	51.72	W.W.	120.24:	162.12	170,00	- 64-242	47.64	10.004	オニ	10,012	77.02	10-01	(V) (V)	10.4		15-151	1,502.97	(W.VI	HX 445.1
	141 A.				01041	10.01	7.90	400,22	11.04	1,99,41	CK. LA	226.57	454.05	57.10	N. 2 M	12.60	11.112	114,10	10.110	100.72	45,944		20.5 Ltv	1,763.17		
	21.12	115	127	11.13	14.14	6. 7	1.2	2015.001	11.76	01 W	2.5	12.14	189.99	22.01	417.06	21.12	120.82	4X.61	12	42.91)	19,55		331.60	75.14		ç
	15.24		107	24.75	.01.01	2.17	09.1	101,12	12.34	15.54	27.61	14.72	123.74	12,44A	240,73	2	NL'N.	20,05	12.25	25.45	-11,111		140.95	427.77		ŧ
9	13.84			Ş	K. 72	L'A C	LAD LAD	CA.XC	- 20	17.35	2.42	24,000	19.6P	8	ŝ	1.1	32.12	1.1.JX,	7.02.	11.41	5,345		1516	¥ 01		ŝ
	12.05		0.19	. 75	24	0.45	0.33	20.02	ş	13.31	(w);	147 K I	37.40	ě.	N2.15	609	14°0	121	1.19	2.00	0.91		14.14	нали		ŝ
	3		0.145	2,20	2.77	9	5	10,01	×	12.47	2.01	27.72	33.32	3.00	M K	0,7d	14.27	1,142	0,40	191	9 <b>4</b> 0		5 G	K4.11		ç
	E.		0.21	2.12	121	0.45	10°0	01/11	51	13.01	9 Y	18,44	17.0M	5.16	19.44	6,74	10.47:	2.76	1.450	244	1111		24.00	X4. XK		ğ
	2		00	241	5	6	0.31	17.6	M 1	51.15	1	25.82	01.121	1.5.6	14.041	2.10	¥.03	4.14	2.17	3.05.	1.46		2.1	7134.11		17
				\$	1.			N, 19	1	12.24	1.55	14.24	277.11	21.24	102.05	11.	:0×11	6.57	0.45	5,80	ł		40.25	448.35		ŧ
		,					3	44 11	5	-101	5	- LLL	10.00	4	X. 11. X	110	143.70	2.76	17.52	12.74	0.14		27N. 44	1.000.11		<b>*</b>
	2													5			11 11	1 2 2	10.001	3	13		124, 264	00.000		1975
	141	- 	-		17. 67	Į	\$	1.1.1.1	74.44	£.												•				
	41.6				76157	9	5	1,049,05	19762	6.	DIVE	02.381	01210	UXTE	1.437.41				0					10 14		
	9V'AX				291.52	14.16	14.25	11.27	2.5	10.10	- 1 - 1 - 1 - 1	19 <u>5</u>	16'0m'	8	1,271.26		62.016	9 7	0	in the second	0					
-	2 2		10.77		143.59	N. 01	7.04	1	S	e I	27.46	5.5	2.12	17.24	50.05	10'6	5177	7	11 12	AL.14	1			10000		
	21,10	44,00	*.7x	70,405	12.56	Ē.	1.51	5	11.17	11.26	17.1	1.1.1	117.55	00.51	NO.0%	14	ET IX	25.42	11.14	ដ	0.22		1	3 5		ž
Jan - K7	13.70			5.5	5	1.51	1.44	- mc 16	2	17.14	1.05	24.42	* 7	7.85	141.000	3	45.82	10.11	5.31	× 6, ×	4.07		12.54	12.77		Ş
	0			101	11	010	5.0	1.174	.70	1,144	SAS:	14.41	14.45	7.99	23.00	0.97	N.22	14()	0'31	9.0	0.16		45.99	200.011		ē
	2		100	112	04	0.45	0.00	20.47	÷.	10.01	2	19.36	34,41	101	63.11	CUNI	127	17	7.25	3,751	1/2/1		10.4	Ch'fix		×
			Ĩ			0.0	21.0	200	2	14.01	3	20.7	(n n)	3.45	65.41	0.43	11.57	¥.	0,66	1111	0.51		2A.6I	90.XS		3
			_							1	2014	910	12.84	11.45	204.51	CX C	2.2	3	8	3.12	1.60		24.45	30.00		۶
							1								ç								273 MD	847 44		ž
								10040	1		190		00.446		N 101	5	201 2 201	104.40	ÿ	5	0.01		741.03	2.187.71		2.1%
	(† -					2								04.64									1001	5		3
	4			1971-00	1000		2									5 3		1000		AT 14	Ş					
	Ĭ			192.9%	N. 78	0.11	6			14.14			1012	10.14					Ģ	10.00	1		3	12000		
	1	25'11'			5.7.4	8							(											100		-
	(C1716)				110.14	17.07	ž	-0°5%	010				10-117				07 m 1			_				107 102		
	10.1		Ŕ	10.17	ŝ	<u>,</u>	64.6	100						Ì		1										1
ž	17-00 10 10 10		17	R.	8	i i	i i	10219	e l		2			2				8	1	5						1
	N 11	÷	5	Ś	×.7%	0,171	5	*		5	6 6		24.4			Ş		<u>s</u> i								
-	10.01		627 2	4.03	Ē.	6.0		N.15		140		0		2				•								
	14 64		0.14:	2.04	511	<b>9</b>	0.10	21.00	5.8	26 01	6	12.51	3110	2	55.0%	0	992 2	ň,	ö		14.		2	10 K		2
	2	E,	620	9.72	×.	9.71	0.12	IC N	1.1	12.001		17.10	E A	e.		16.0	Ţ	7	i.	2	£.		4	4.14		2 :
•••	11.43	2000	242	12.44	177		4,05	257.44	Ś	01.1	ň,	24-0x	0%"141	23.03	1977	\$45	0 ¥	23,65	12.42	N.Y.	1.1		145.(5)	11.15		2
	1.4	<u>e</u> 7		19441	144.51	98.6	12.7	457.11	20,62	10712	2.5	07601	219.5	01.17	714.56	<u>4</u> ,12	120,74	7	£.4		5		144.97	Ś		3
	19-10	12.24	<b>1</b> ***	24	20.2	ι, γ	68.9	A.M.R.	1	\$ <b>1</b> ,	102	21.27	170.64	1	24	4. X	1014	20,60	59°%	14,67	202		200	9.00		5
•	00717		÷	2'6.47	242.74	501	1	116.37	1.2	8 ¥	th. 52	¥-14		41.7X	0, 100	5	102.11	11.14	21.14	8	11.71		2	14.161		
	0.4		14.X.1	214,40	2	14.40	0.00	117.0	0. IV	117.52	\$0.23	A	3.14.74	¥0.4	1,062,93	13.57	277.45	1001	10.01	0.10	5		765.31	1X. 14X. 1		
	21.52	10.001	10.60	1 <b>57.</b> 110,	101.02	IN CUT	7.41	7N.9NA	242	A. 16	10.00	94.621	260.32	40,67	770,46	24.2	14,00	15.54	22.00	55.24	4.X		275.44	10,021,1		5
	12	72.64		76,14	71.03	16.4	W.C	107622	NSA V	5.65	10.14	52	10.20	19.67	W.CH	4.01	WY THE	32.07	10.44	F.A	12.90		2272VI	*1.D*		2
ŝ	W. 1	19,844	50	30.5	A R	1.0%	2	54.54	3,422	12.65	÷	17.92	15.01	(#*1	140H	2	24,449	201	58.0	11	a A		Ă,¥	202		ñ.
•	X.67	6.16	0,MS	9,716	10,01	0.7%	0.56	(X'Y)		11.62	54	14.41	11.00	81	33.06	10	17,61	97	R.	2.94	F.		99°	W HOL		=
	10	3.45	0.0	5	5,44	0.00	0,0	23,13,	6	<b>CLU</b>	4.76	102	w ()	8	57.67	0,74	14,81	¥,	10.07	Z	0.75		ş Xi	X4.41		×
, MA	R.	2	0.14	57	5.12	0.47	0.14	21.73	1.61	1.42	5.73	19,0%	34,21	2	2.5	140	7.5%	ş	124	97.1	1,71		14.1%	N.X		*
	7.85	1010	0.35	4.7	10.4	0,46	0.74	21.00	0.40	47.25	0.0	67.14	134.59	N.71	16.151	71	10.97	EV.	8	144	2.26		14.52	ZV1172		7
in l	15.00	62.82	2		10°76	05.0	57.7	15.00.	2	00714	AL .55	1.00	125	32.55	610 K2	CX.1	122.80	ALM.	67	2.40	1.24		02.W	61-762		¥
	61.52	102.34	10,03	-15-151	161,445	11.06	¥.15	18.012	LS"QE	135.04	21.12	6K 161	304465	50.21	194 ISA	12.15	211.91	11.14	13.51	2.5	25.67		2010	QV 144		ŝ,
Auk	10.01	148,04	19.11	207.X4	233.50	÷ 1	10.74	CK.0%V	17.73	ICHCI .	59.55	\$ 15	14.4	en.02	1,137,62	2°4	10.012	20.07	41.50	E.E	A. II		117265	20H.25		ž
<u>.</u>	2.5	12. W	13,00	142.2%	12.121	12.34	40%	\$75.8	12.0	137.52	7 3 3	194.42	201.72	27.20	1001	13.04	257.64	96.011	57.93	C) (A	E.H		66 I I I.	10 <b>~</b> W2		1
	V.49	LNK 00	A.41	213.34	21K.61	9.61	10.21	CALINES	6.0	1 1	31,52	5	210.07	47,82	VC 10	5	10.01	1111	10.68	97-011	9		744, 16	WWW I		-
	12.01	44 44	9,14	1.121	05.461	1	Ş	51.64	14,30	CV 12	F.	75.05	1.00.44	10.34	\$74.16	04 f	01,121	A.72	29.7%	£0'05	2		402.37	3.75		ĉ
	11.45	55.64	Ę	N.N.N.		\$	~ ~																			
-				1.		4	5	2	- <b></b>	<b>1</b> 11		E.4	42.24	5	8	2		3	5	21.13	1.V.X	112	143.641		Å.	: :

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Maaa Maraa M	Nin			Crimy Na	Demy Nur River (uppercurred) the Tin Am Reversion	ream of the	Tr An Kree	(LIUN)				N al	Le Ngu River		¥ ۳	- Tou	-	with .			Rc Rum				-		Tenul	
	77	Du Ninh damare	Dony Nu J	T Dong Nu	N June N		- N -	Nar K, Confi wishing the l		÷	Nya. Hum US										eng i Phone te dama	Him Photo:				ž		
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		17 43						21°S		274.72	44	W V2																1.05
	Jun - 91	11.00						2.20	24.4	100.50	M.	14.73																9.15
		66"11						6.45	24.0	25762	¥,	17.57						1										F. Fi
		10.01						150	24	96"12	a.	12,46																2.4
		21.5						0.11	8	SX H	99	Å.																F) B
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		9 ×						121	_	11.40		21.72																07.04
		72.2%					•	100		24412	_	12,02																2
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(10)         (50) <th< td=""><td></td><td>SR.N.</td><td></td><td></td><td>:</td><td></td><td></td><td>1</td><td></td><td>692(6)</td><td></td><td>20.65</td><td></td><td></td><td></td><td>-</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></th<>		SR.N.			:			1		692(6)		20.65				-												
1000         2001         2006         1000         2010         2001 <th< td=""><td></td><td>(M. 11</td><td></td><td></td><td>_</td><td></td><td>•</td><td>Ę</td><td></td><td>290.04</td><td></td><td>14.04</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>÷</td><td></td><td></td><td></td><td></td><td>7</td></th<>		(M. 11			_		•	Ę		290.04		14.04											÷					7
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0.26         0.26 <th< td=""><td>• • •</td><td>ž</td><td></td><td></td><td></td><td></td><td></td><td>0. M</td><td>0.34</td><td>10.10</td><td>Ĥ</td><td>11.449</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>1</td><td></td><td></td><td></td><td></td><td>W</td></th<>	• • •	ž						0. M	0.34	10.10	Ĥ	11.449											1					W
1179         3.00         46601         1.00         5.00         1.00         6601         1.00         6601         1.00         6601         1.00         6601         1.00         6601         1.00         6001         1.000         6001         1.000         6001         1.000         6001         1.000         6001         1.000         6001         1.000         6001         1.000         6001         1.000         6001         1.000         6001         1.000         6001         1.000         6001         1.000         6001         1.000         6001         1.000         6001         1.001         6001         1.001         6001         1.001         6001         1.001         6001         1.001         6001         1.001         6001         1.001		12.04						0.31	0.34	23.61		1771										_						Ę
Nath         T/1         14.27         11.41         17.11         27.06         11.42         11.71         27.06         11.42         11.71         27.06         11.42         11.71         27.06         11.42         11.71         27.06         11.42         11.71         27.06         11.42         11.20         20.06         11.42         11.20         20.06         11.20         20.06         11.20         20.06         11.20         20.06         11.20         20.06         11.20         20.06         11.20         20.06         11.20         20.06         11.20         20.06         20		2157	671F			;		1		161.74	i.	24.44																55.AK
YZ-W         V-W         142.18         142.71         V-W         12.11         470.71         72.24         W-M         72.12         W-M         72.11         11.55         72.11         11.55         92.11         11.55         11.55         92.11         11.55         11.55         92.11         11.55         11.55         92.11         11.55         11.55		i u	Į,			_		7.256		367.72	ī	13												•.			-	N.E.
During         Control         Control <thcontrol< th=""> <thcontrol< th=""> <thco< td=""><td></td><td>10 H</td><td>5</td><td>ء . س</td><td></td><td></td><td></td><td></td><td></td><td>12.037</td><td></td><td>KI 12</td><td></td><td></td><td></td><td></td><td>:</td><td></td><td></td><td></td><td></td><td></td><td></td><td>•</td><td></td><td></td><td></td><td>5</td></thco<></thcontrol<></thcontrol<>		10 H	5	ء . س						12.037		KI 12					:							•				5
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	/Vurk	JUL	αnζ	May	Apr	Mar	م م	FC	Jan Feb
	50.21	36.80	21.22	5.57	.13	l v		6.03	14.40 6.03
	103.04	98.53	17.70	10.27	8	7		6.18	13.27 6.18
	97.40	32.98	11.14	10.58		8.7(		8.24	19.47 8.24
	74.39	80.02	11.83	6.84		6.79		7.39	14.88 7.39
	131.95	68.08	8.32	7.31		7.31		7.98	15.78 7.98
	107.57	57.50	10.86	7.56		7.61		8.56	16.74 8.56
	50.06	10.01	24.99	9.84		8.30		10.49	23.55 10.49
	145.20	86.07	53.67	8.99		8.55		11.50	25.47 11.50
	139.34	114.01	16.43	S. 38		8.88		9.57	15.01 9.57
	40.32	25.85	15.25	9.72		9.40		10.27	17.99 10.27
	51.82	73.97	121.62	60.20	÷ .	10.01		11.25	21.26 11.25
	128.51	87.26	25.69	10.53		10.70		10.96	18.03 10.96
	125.02	121.55	30.77	28.55		10.55		12.85	23.98 12.85
	103.89	44 77	12.62	- 11.10		10.96		11.27	15.81 11.27
	69.54	23.31	11.83	11.49	÷	11.49		12.33	20.53 12.33
	118.34	112.64	38.45	11.49		11.49		11.82	16.32 11.82
	123.44	111.14	45.83	14.11		12.20		16.71	33.73 16.71
	35,55	31,95	15.73	12.38		12.39		14.16	25.06 14.16
	41.67	17.04	12.83	12.53	,	12.67		15.63	30.32 15.63
•	96.49	63.68	67.09	34.61	÷.	12.60		13.64	20.98 13.64
	108.84	68.70	13.59	13.05		13.05		14.60	25.16 14.60
	60.77	23.06	14.78	13.05	÷	13.05		13.07	14.42 13.07
	64.36	42.95	13.05	13.05		13.05		13.56	16.67 13.56
	96.31	59.00	30.81	23.55		13.58		14.40	22.36. 14.40
	106.98	94.35	30.13	14.18		13.58		14.38	20.46 14.38
	149.43	156.00	69.37	16.42		13,89		14.18	17.73 14.18
	101.12	54.91	27.19	16.89		14.27		15.92	26.76 15.92
	80.37	48.24	24.33	14.62	. 1	14.62	-	15.53	23.38 15.53
	109.04	54.20	15.28	14.62	- 1	14.62		15.39	22.90 15.39
	07.70	20 62	24.05	Ser 1		10.02		12.00	MC1 5000 1
146.83 2272.19 2272.19 2272.19 2272.19 2230.49 150.12 150.12 150.23 150.		87.00 155.99 156.99 156.98 151.07 151	50.21     \$7.00       103.04     125.73       97.40     156.99       7.4.39     169.62       131.95     156.90       107.57     92.03       50.06     38.38       145.20     208.19       139.34     112.57       40.32     81.49       51.82     38.38       139.34     112.57       40.32     81.49       51.82     82.13       139.34     112.57       40.32     81.49       51.82     82.13       139.34     112.57       135.55     104.25       125.02     151.07       135.55     104.25       135.55     151.07       135.55     102.72       96.49     102.72       96.49     167.98       64.36     133.19       96.43     167.98       64.36     167.26       199.45     167.98       106.98     107.26       109.04     107.26       109.05     139.77       109.06     139.77       109.06     139.77       109.06     139.77       109.06     139.77       109.06     139.77       109.06     <	36.80       50.21       87.00         36.80       50.21       87.00         98.53       103.04       125.73         32.98       97.40       156.99         80.02       74.39       169.62         68.08       131.95       156.90         57.50       107.57       92.03         79.01       50.06       38.38         86.07       145.20       208.19         114.01       139.34       112.57         25.85       40.32       81.49         73.97       51.82       208.19         114.01       139.34       112.57         25.85       40.32       81.49         73.97       51.82       82.13         87.26       128.51       104.25         121.55       125.02       151.07         23.31       69.54       108.58         17.04       118.34       92.00         111.14       123.44       146.37         31.95       35.55       151.07         65.68       66.54       108.58         17.04       118.34       90.64         54.00       168.84       190.64         54.01	21.22       36.80       50.21       87.00         17.70       98.53       103.04       125.73         111.14       32.98       97.40       156.99         111.83       80.02       74.39       169.62         8.32       68.08       131.95       156.90         11.83       80.02       74.39       169.62         8.32       68.08       131.95       156.90         10.86       57.50       107.57       92.03         24.99       79.01       50.05       38.38         53.67       86.07       145.20       208.19         15.25       25.85       40.32       81.49         15.25       25.69       87.26       104.25         25.69       87.26       128.51       104.25         25.69       87.26       18.34       104.25         25.69       87.26       133.44       146.37         15.73       31.95       35.55       71.64         11.83       23.34       112.57       104.25         25.69       87.26       18.34       106.26         15.73       31.95       35.55       71.64         15.73       31.95	5.57         21.22         36.80         50.21         87.00           10.27         17.70         98.53         103.04         125.73           10.28         11.14         32.98         97.40         155.69           6.84         11.183         80.02         74.39         169.62           7.31         8.32         68.08         131.95         156.69           7.56         10.86         57.50         107.57         92.03           9.89         53.67         86.07         145.20         208.19           9.72         15.25         25.85         40.32         81.49           6.020         121.62         73.97         51.82         82.13           9.72         15.25         25.85         87.26         13.93         112.57           9.72         15.25         25.85         87.26         112.57         97.03           11.49         12.162         73.97         51.82         82.13         97.07           11.49         12.155         12.502         151.07         112.57         92.03           11.49         12.156         17.04         112.57         12.05         12.07           11.401         <	5.13         5.57         21.22         36.80         50.21         87.00           7.66         10.27         17.70         98.53         103.04         125.73           8.70         10.38         11.14         32.98         97.40         156.59           6.79         6.84         11.83         80.02         74.39         169.62           7.61         7.56         10.86         57.50         107.57         92.03           8.30         9.84         24.99         79.01         50.06         38.38           8.30         9.84         24.99         79.01         50.06         38.38           8.30         9.84         24.99         79.01         50.06         38.38           8.38         8.38         16.43         114.01         139.34         112.57           9.40         9.75         15.22         25.85         90.35         11.49           10.01         60.20         121.62         73.97         51.49         104.25           10.75         15.22         25.85         71.64         112.57         10.425           10.76         11.49         11.85         25.34         106.54         164.23 <tr< td=""><td>6.03         5.13         5.57         21.22         36.80         50.21         87.00           6.18         7.66         10.27         17.70         98.53         103.04         125.73           8.24         8.70         10.58         11.14         32.98         97.40         156.69           7.39         6.79         6.84         11.83         80.02         74.39         169.62           7.38         7.31         8.33         103.04         125.73         97.40         156.69           8.56         7.61         7.56         10.86         77.61         73.33         80.02         74.39         169.62           9.57         0.58         8.38         16.43         114.01         139.34         125.73           9.57         9.607         10.52         25.46         87.26         139.24         112.57           9.56         11.25         10.01         10.53         25.56         87.26         139.34         112.57           10.27         9.02         11.23         11.40         12.44         146.7         104.25           11.25         10.06         10.53         25.55         40.33         81.45         104.25</td><td>14.40 <math>6.03</math> <math>5.13</math> <math>5.57</math> <math>21.22</math> <math>56.80</math> <math>50.21</math> <math>87.40</math> <math>156.99</math> <math>19.47</math> <math>8.24</math> <math>8.76</math> <math>10.27</math> <math>17.70</math> <math>98.53</math> <math>103.04</math> <math>125.73</math> <math>15.78</math> <math>7.39</math> <math>6.77</math> <math>6.18</math> <math>7.66</math> <math>125.73</math> <math>19.67</math> <math>156.90</math> <math>15.78</math> <math>7.39</math> <math>6.77</math> <math>0.28</math> <math>8.740</math> <math>156.90</math> <math>19.67</math> <math>125.73</math> <math>15.78</math> <math>8.56</math> <math>7.56</math> <math>10.36</math> <math>77.50</math> <math>130.56</math> <math>125.73</math> <math>15.77</math> <math>11.50</math> <math>8.58</math> <math>16.43</math> <math>11.40</math> <math>125.73</math> <math>125.69</math> <math>100.57</math> <math>17.99</math> <math>10.27</math> <math>9.40</math> <math>8.007</math> <math>155.30</math> <math>103.54</math> <math>112.57</math> <math>17.99</math> <math>10.27</math> <math>9.40</math> <math>11.40</math> <math>11.40</math> <math>112.57</math> <math>17.99</math> <math>10.27</math> <math>9.40</math> <math>16.71</math> <math>102.79</math> <math>108.56</math> <math>17.99</math> <math>11.25</math> <math>15.25</math> <math>15.26</math> <math>12.85</math> <math>10.425</math> <math>17.99</math></td></tr<>	6.03         5.13         5.57         21.22         36.80         50.21         87.00           6.18         7.66         10.27         17.70         98.53         103.04         125.73           8.24         8.70         10.58         11.14         32.98         97.40         156.69           7.39         6.79         6.84         11.83         80.02         74.39         169.62           7.38         7.31         8.33         103.04         125.73         97.40         156.69           8.56         7.61         7.56         10.86         77.61         73.33         80.02         74.39         169.62           9.57         0.58         8.38         16.43         114.01         139.34         125.73           9.57         9.607         10.52         25.46         87.26         139.24         112.57           9.56         11.25         10.01         10.53         25.56         87.26         139.34         112.57           10.27         9.02         11.23         11.40         12.44         146.7         104.25           11.25         10.06         10.53         25.55         40.33         81.45         104.25	14.40 $6.03$ $5.13$ $5.57$ $21.22$ $56.80$ $50.21$ $87.40$ $156.99$ $19.47$ $8.24$ $8.76$ $10.27$ $17.70$ $98.53$ $103.04$ $125.73$ $15.78$ $7.39$ $6.77$ $6.18$ $7.66$ $125.73$ $19.67$ $156.90$ $15.78$ $7.39$ $6.77$ $0.28$ $8.740$ $156.90$ $19.67$ $125.73$ $15.78$ $8.56$ $7.56$ $10.36$ $77.50$ $130.56$ $125.73$ $15.77$ $11.50$ $8.58$ $16.43$ $11.40$ $125.73$ $125.69$ $100.57$ $17.99$ $10.27$ $9.40$ $8.007$ $155.30$ $103.54$ $112.57$ $17.99$ $10.27$ $9.40$ $11.40$ $11.40$ $112.57$ $17.99$ $10.27$ $9.40$ $16.71$ $102.79$ $108.56$ $17.99$ $11.25$ $15.25$ $15.26$ $12.85$ $10.425$ $17.99$

Table 3.13 Estimated Monthly Runoff

Dam Site: Dau Tieng Dam Catchment Area: 2700 km2

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3	Thanh	Thanh Binh	e'l'a	T'a Lai	Dai	Nga	Ta	Pao	Phu	Phu Dien	1ri	Tri An
Year	Date	Q(m3/s)	Date -	]	Date	te Q(m3/s)	Date	Q(m3/s)	Date	Q(m3/s)	Date	O(m3/s)
1973	:				:							
974							•		•			
1 976												
7			•				9.7	412				
1978					· .	:	8.29	528				
2					7 07	128.0	7.07	642				
2	10.06	63.4	•		10.7	83.0	8.30	416			9.11	2.080
	10.15	67.4			8.2	109.0	8.17	473			8.05	4,420
2	9.07	70.9			9.3	130.0	0.6	808			9.11	391
3	10.09	83.9				:	10.18	474			10.18	2,310
2	8.20	55.9	•		8.20	144.0	8.20	728			8.21	2,840
8	10.24	57.7			6.2 .:	75.7	6.23	314			10.04	1.650
Ś	8:02	55.8			8.7	96.9	8.11	:568			8.21	2,900
1987	8.14	56.3	8.22	2.920	8.7	96.9	8.22	672	8.26	532	8.23	3,170
22	9.27	57.0	10.09	1.427	10. ?	49.5	10.09	498	10.15	389	9.29	1,362
2	7.16	48.0	8.06	6.500	7.2	66.9	9.08	532	10. 7	389		
8	6.17	52.2	9.04	1.620	8.7	129.0	9.04	524	9.06	790.		
					1.	-						
F	Phuoc	1 ong	Phuo	ke Hoa	2	An Vien	loc	Loc Ninh	Dau	Dau Tien	S	Can Dang
Ycar	Date	ate Q(m3/s)	Date	Q(m3/s)	Dat	O(m3/s)	Date	Q(m3/s)	Date	Q(m3/s)	Date	O(m3/s
1973			10.14	0.14 1.370	-						•	
2			· .									
2			10.24	605	• •		10. ?	46.8				
1976			9.25	\$36			9.23	39.1	8, 7	167	9.22	63.1
5	9,11	385	9.12	208	•		7.21	26.4	8.30	159	10.01	41.0
20	8.28	061,1	9.01	1,520	10.05	68.2	10.25	36.3	9.2	177	7.14	41.9
\$	8.05	755	8.09	1,050	10.06	56.5	10.05	33.4			10.07	37.9
õ	9.11	586	9.14	1.030	9.11	79.2	8.19	42.2			10.29	68.5
5	8.10	789	8.20	1,180	8.05	73.2	72.6	38.8			9.25	48.8
ġ	9.08	634	9.12	1.380	9.08	135.0	9.28	. 33.6			9.12	58.4
 22	8.16	515	8 19	1,865	8.11	127.0	11,14	54.3	•		10.13	78.3
55	8.20	542	8.22	806	10.14	55.9				•	10.11	93.6
ŝ	01.6	457	9.12	698	9.13	62.4					10.22	54.4
8	8.16	920	8.21	1,590	9.27	68.1	• •				10.03	55.6
5	8.22	976	8.25	1,080	10.31	51.6					10.11	38.7
2	10.09	502	10.11	1.030	10.04	87.3					10.03	39.2
1989	9.08	516	60.6	1.017	9.27	60.7					10.21	863
<u>д</u>	9.05	841	9.06	1.310	8.17	124.0		·			0 2 2	148.0

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			÷		Availab	e Rainfa	ll Data					
No.	Station	8/78	9/78	9/82	8/83	10/83	8/84	8/86	8/87	9/89	8.90	9/90
1	Bac Loc	Ā	A	A	Α	A	Α	A	Α	A	A	A
2	Bien Hoa	Α	Α	Α	Α	Α	-	Α	Λ	Α	٨	Α
3 1	Binh Ba	A	Α	Α	Α	Α	Α	Α	Α	٨	+	-
4	Binh Long	- A -	A	Α	Α	Α	A	A	Α	Α	Α	Α
5	Da Lat	A =	Α	A	A	Α	Α	Α	Λ	A ···	Λ	Α
6	Da Te	A	A	A	Α	Α	Å	Α	Λ	Α	A	A
7	Dau Tieng	A I	A	A	Α	Α	Α	- A -	Α	Α	Α	Α
8	Di Linh	A	A	Α	٨	Α	Α	Λ	Α	Α	Α	Α
9	Don Duong	A	Α	Α	A	Α	$\mathbf{A}^{-1}$	A	Α	`_ <b>A</b>	A	A
10	Dong Phu	-	-	-	-	-	Å	Α	Α	Α	Α	Α
11	Go Dau Ha	-	· -	-	•	-	Α	Α	: <b>A</b>	Α	Α	Α
12	Ham Tan	A	Α	Α	Α	Α	A	A	A	Ά	Λ	Α
13	La Buong	A	Α	Α	Α	Α	Α	Α	Α	Α	-	-
14	Lien Khuong	A	A	Α	Α	Α	۸	Α	A	Α	Α	Α
15	Loc Ninh	A	۸	Α	Α	Α	•••	· .•	-	-	-	-
16	Long Thanh	•	-	-		-	-	Á	Α	Α	Α	Α
17	Moc Hoa	A	Α	Α	Α.	A	` <b>A</b> -	; A	Α	Α	A	A
18	Phan Rang	-	-	- '	A	Α	A	: A -	• <b>A</b> .	Α	٨	A
19	Phuoc Hoa	A	A	A	Α	Λ	• <b>A</b> •	Α	Α	Α	A	Α
20	Phuoc Long	Á :	· A	Δ	Α	A	A	A	A	A	Ά	Α
21	Phan Thiet	A (	Α	Α	Α	Α	Α.	A	A	A	Α	Δ.
22	Phuoc Le	A	A	Α	Α	Α	<b>A</b> .	Δ	$\mathbf{A} = \mathbf{A}$	A	-	Α
23	Song Luy	ΪA.	A	A	<b>. A</b>	A	A	÷A	A	A	Α	Α
24	So Sau	A	Α	A	Α	A		-	-	-	-	•
25	Tan An	A	Α	A	Α	Α :	Λ	Λ.	A	A	A	Α
26	Tan My	• A –	Λ ,	. A	Α	Α	A	A	Å	Α	Λ	$[ \Lambda ]$
27	Ta Pao	Α	A	A	Α.	Α	Α	• A •	. <b>A</b> .	Α	• A •	A
28	Tay Ninh	A I	Â	Α	A	Α	A	Α	A	Α	A	Δ.]
29	Thac Can	Α	$\mathbf{A} \in \mathbf{A}$	ΞĂ	Α	-	Α	Α	A	± Å }	Α	Α.
30	Thong Nhat	A	A	Α	Ā	Λ	Λ	Α	A	Α	Α	Α
31	T.S.Nhat	A	Α	A	Α	۸	Α	Α	<b>A</b> -	Α	Α	<b>A</b> .
32	Tue Trung	$\mathbf{A}$	. <b>A</b>	A	A.	Α	·		Α	ΓA	A	A
33	Vung Tau	A	Α	Â	A	Α	A	A	: <b>A</b>	• <b>A</b> :	A	Α
34	Xuan Loc	A	<u> </u>		<u>A</u>	Α	<u>A</u>	<u>A</u>	A	Λ	_ <u>A</u>	<u>` A</u>

# Table 3.15Availability of Daily Rainfall and Discharge Datafor Flood Analysis

	Available Discl	harge Data		:				· · ·				
No.	Station	8/78	9/78	9/82	8/83	10/83	8/84	8/86	8/87	9/89	8/90	9/90
1	Ta Lai	-	-	-	-	-			A	Α	1 A	A
2	Ta Pao	Α	Α	· A	А	Α	A	Α	A	Α	Å	$\mathbf{A}_{1}$ :
3	Phu Dien	- ( - · ·		-	-	-	· _	-	Λ	٨	A	A
4	Trì An	A	<b>A</b>	Υ A		-		. <b>-</b> -	-	- '	-	-
- 5	Phuoc Hoa	A	A	Α	Α	Α	A	Α	Α	Α.	Á	A
6	Dau Tieng	A	Α	-	-	-	-	•		-	· •	-
7	Can Dang	Α	A	A	A	A	A	Α	Λ	Α	_Λ	A

(Remarks) A: -: data available

data not available

	Slope		- (1/)	24	95	57	29	54	83	65	44	37	25	286	333	200	1240	B2		(u)	1,500				1.000					<b>.</b>		
	13		0	63	2		~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	C1	-		<u>6</u>	6	(7)	<u> </u>	4	ž	1	B		(m)	100	125	175	60	80	001	70	75	100	200	300	500
	ΗР		(m)	1,115	475	865	260	581	684	1,000	6	780	907	140	45	125	125	 Slope		. (1/1)	632	6,375	2,154	236	8,125	1,900	1,207	8,846	32,000	11,625	19,500	3,267
	Lower	elev.	(m.MSL)	485	125	105	40	519	116	100	50	180	33	20	15	25	25	Hp		(m)	360	20	65	403	16	50	147	13	Ś	ø	6	00
:	Upper	clev.	(m.MSL)	1,600	600	970	300	1,100	800	1,100	140	960	940	160	60	150	150	 Lower	elev.	(m.MSL)	125	105	64	116	100	50	33	20	15	ы	0	0
	River	length	(km)	250	140	170	138	148	125	165	85	185	295	180	195	200	155	Upper	elev.	(m.MSL)	- 485	125	105	519	116	100	180	ຕິ	20	10	61	30
	Basin	arca	(km2)	3,586	2.690	2,574	1.079	1,363	637	1,060	1.036	2,200	1,910	1.655	1,662	1,750	950	Channel	lenght	(km)	228	128	140	95	130	95	178	115	160	93	ð G	- 98
		Basin		Dong Nai No.3	Dong Nai No.6	TaLai	Tri An and the second	Ham Thuan/Dami	Ta Pao	Phu Dien	conf. DN/LN	Thac Mo	Fu Mieng	Phuoc Hoz	conf. Be/DN	Dau Tieng L	Dau Tieng R		River Channel		D.N.3-D.N.6	D.N.6-Ta Lai	Ta Lai-Tri An	Ham Thuan-Ta Pao	Ta Pao-Phu Dien	Phu Dien-conf.	Thac Mo-Fu Mieng	Fu Mieng-Phuoc Hoa	Phuoc Hoa-conf.	D.Tieng-Rach Tra	Rach Tra-D.N.conf.	Tri An-Saigon conf.
		River		Dong Nai	Dong Nai	Dong Nai	Dong Nai	La Nga	La Nga	La Nga	La Nga	Be	ы М	Ъс	Be	Saigon	Saigon				Dong Nai	Dong Nai	Dong Nai	La Nga	La Nga	La Nga	Вс	ň	е Д	Saigon	Saigon	Dong Nai
	Basin	°.		1	(1	(1)	4	11	12	13	4	51	2	33	23	31	32	Chan.	°Z		7	Ś	~	2	4	16	ដ	ß	27	33	ŝ	9

Table 3.16 Parameters for Flood Analysis

# Table 3.17 Basin and Channel Constants for Storage Function

Basin	k	þ	TI	Er	A
No.			(hr)		(km2)
1	60.45	0.50	22.56	0.5	4,361
2	60.45	0.50	12.00	0.5	2,690
3	60.45	0.50	14.88	0.5	2,574
4	60.45	0.50	12.00	0.5	1,082
5	60.45	0.50	3.00	0.5	2,213
. 11 -	60,45	0.50	12.96	0.5	1,363
12	60.45	0.50	10.56	0.5	637
. 13	60.45	0.50	14.40	0.5	1,060
- 14	60.45	0.50	6.72	0.5	1,033
21	60.45	0.50	24.48	0.5	2,200
22	60.45	0.50	39.60	0.5	1,910
23	60.45	0.50	23.76	0.5	1,655
24	60.45	0.50	25.92	0.5	1,662
31	60.45	0.50	26.64	0.5	1,750
32	60.45	0.50	20.16	0.5	950
33	60.45	0.50	3.30	0.5	1,603
34	60.45	0.50	1.30	0.5	414

# **Basin Constant**

# **River Channel Constant**

÷.,						a tha tha in t
	hannel	k	р	TI I	Fi	
	No.			(hr)		(km)
·	2	720	0.60	4.21	1.0	228
	5	883	0.60	7.49	1.0	128
	7	801	0.60	4.78	1.0	140
	12	183	0.60	1.07	1.0	95
	14	2,496	0.60	8.62	1.0	130
	16	419	0.60	3.05	1.0	95
}	22	592	0.60	4.54	1.0	178
	25	716	0.60	7.96	1.0	115
	27	1,644	0.60	21.07	1.0	160
	33	783	0.60	4.12	1.0	98
1	35	451	0.60	7.38	1.0	93
	61	814	0.60	4.01	1.0	39

(Remarks) k; p: Constants for storage function Er : Effective rainfall coefficient Fi : Inflow rate of channel

T1 : Lag time (hr)A : Basin area (km2)L : Channel length (km)

Table 3.18 Rainfall Hyctograph for Design Discharge Calculation

								and a second sec														
No	No. Station	Year	lst	2nd	3rd	4th	5th	· 6th	7th	8th -	9th	10th	11th	12th	13th	14th	15th	16th	17th	18th	19th	4 2 2 2 2
1	Bao Loc	20-yr	30.3	48.3 217.3	217.3	28.7	28.7	28.7	28.7	28.7	28.7	28.7	18.9	18.9	18.9	18.9	18.9	15.7	15.7	15.7	15.7	15.7
		100-yr	100-yr 30.6	55.0	55.0 280.2	35.5	35.5	35.5	35.5	35.5	35.5	35.5	23.4	23.4	23,4	23.4	23.4	19.4	19.4	19.4	19.4	19.4
7	Bien Hoa	20-yr	31.2	35.2	35.2 146.7	20.7	20.7	20.7.	20.7	20.7	20.7	- 20.7	13.6	13.6	13.6	13.6	13.6	11.3	11,3	11.3	11.3	11.3
		100-11		40.8 42.1 181.3	181.3	25.6	25.6	25.6	25.6	25.6	25.6	25.6	16.9	16.9	16.9	16.9	16.9	14.0	14.0	14.0	14.0 -	40
S	Da Lat	20-yr	22.4	61.8	61.8 235.2	31.0	31.0	31.0	31.0	31.0	31.0	31.0	20.4	20.4	20.4	20.4	20.4	16.9	16.9	16.9	16.9	16.9
		100-VT	25.6		77.0 325.3	415	41.5	41.5	41.5	41.5	41.5	41.5	27.4	27.4	27.4	27.4	27.4	22.7	22.7	22.7	22.7	22.7
~	7 Dau Tieng	20-yr	22.3	40.7	40.7 190.3	24,6	24.6	24.6	24.6	24.6	24.6	24.6	16.2	16.2	16.2	16.2	16.2	13.4	13.4	13.4	13.4	13.4
:	-	100-11	,	25.8 48.4 245.9	245.9	31.0	31.0	31.0	31.0	31.0	31.0	31.0	20.5	20.5	20.5	20.5	20.5	17.0	17.0	17.0	17.0	17.0
2	16 Long Thanh	20-yr	32.6	42.0	42.0 203.6	27.0	27.0	27.0	27.0	27.0	27.0	27.0	17.8	17.8	17.8	17.8	17.8	14.7	14.7	14.7	14.7	14.7
	:	100-11	40.0		52.6 268.9	35.1	35.1	35.1	35.1	35.1	35.1	35.1	23.1	23.1	23.1	23.1	23.1	19.2	19.2	19.2	19.2	19.2
20	20 Phuoc Long	20-yr	23.9		30.3 195.1	24.2	24.2	24.2	24.2	24.2	24.2	24.2	16.0	16.0	16.0	16.0	16.0	13.2	13.2	13.2	13.2	13.2
		100-yr	24.6	24.6 28.5 247.3	247.3	29.1	29.1	29.1	29.1	29.1	29.1	29.1	19.2	19.2	19.2	19.2	19.2	15.9	15.9	15.9	15.9	15.9
28	Tay Ninh	20-yr	1.91	58.7	58.7 130.4	20.2	20.2	20.2	20.2	20.2	20.2	20.2	13.3	13.3	13.3	13.3	13.3	11.0	11.0	11.0	11.0	11.0
	· · · · · · · · · · · · · · · · · · ·	100-yr	21.5	77.4	77.4 159.8	25.1	25.1	25.1	25.1	25.1	25.1	25.1	16.6	16.6	16.6	16.6	16.6	13.7	13.7	13.7	13.7	13.7
31	Tan Son Nhat 20-vr	20-vr	19.3		44.9 148.4	20.6	20.6	20.6	20.6	20.6	20.6	20.6	13.6	13.6	13.6	13.6	13.6	11.3	11.3	11.3	11.3	11.3
		100-yr	19.8		57.1 184.4	25.3	- 25.3	25.3	25.3	25.3	25.3	25.3	16.7	16.7	16.7	16.7.	16.7	13.8	13.8	13.8	13.8 -	13.8
33	33 Vung Tau	20-yr	22.9	27.7	27.7 159.7	20.4	20.4	20.4	20.4	20.4	20.4	20.4	13.5	13.5	13.5	13.5	13.5	11.1	11	11.1	11.1	11.1
		100-yr	28.7	30.6	30.6 206.8	25.8	25.8	25.8	25.8	25.8	25.8	25.8	17:0	17.0	17.0	17.0	17.0	14.1	14.1	14.1	14.1	14 1
34	34 Xuan Loc	20-yr	24.7		39.4 207.0	26.3	26.3	26.3	26.3	26.3	26.3	26.3	17.4	17,4	17.4	17.4	17.4	14.4	14,4	14.4	14.4	14.4
		100-vr	100-vr 25.9 47.2 273.7	47.2	273.7	33.6	33.6	33.6	33.6	33.6	33.6	33.6	22.2	22.2	22.2	22.2	22.2	18.4	18.4	18.4	18.4	18.4

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# Table 3.19 Daily Suspended Sediment Concentration at Ta Pao (1/2)

#### Ta Pao Gauging Station: Year 1990

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								<u> </u>			(	in gʻm3)
Date	Jan	Feb	Mar	Арг	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec
1	19.7	39.8	132.0	64.0	17.5	52.2	40.6	116.0	89.1	74.2	27.1	122.0
2	26.1	45.6	37.5	57.8	57.6	80.2	36.2	53.0	113.0	137.0	24.4	35.5
3	29.2	29.5	63.7	84.9	61.2	127.0	32.0	54.8	297.0	57,7	73.0	39.1
4	23.5	32.5	107.0	70.9	60.3	49.4	59.9	93.8	287.0	61.6	137.0	29.1
5	26.9	38.8	102.0	54.1	11.7	70.1	23.6	38.1	534.0	35.4	27.9	49.3
6	24.3	33.5	35.8	64.5	76.5	59.5	25.1	98.7	183.0	25.5	27.4	38.5
7	41.6	82.4	29.2	55.7	81.3	490.0	92.2	107.0	112.0	37.7	27.6	37.9
8	58.7	78.3	74.8	59.7	108.0	133.0	46.6	41.5	122.0	34.9	22.9	40.0
9	52.0	66.0	83.3	47.5	59.5	92.4	180.0	107.0	164.0	105.0	129.0	39.2
10	45.3	60.3	26.9	62.8	64.0	77.0	50.6	79.2	152.0	103.0	238.0	58.5
1	74.8	67.0	70.0	69.7	43.2	178.0	87.3	79.5	202.0	26.6	90.4	40.2
12	77.0	63.7	74.8	<b>59.9</b>	57.4	155.0	47.2	130.0	176.0	104.0	65.6	35.5
13	66.1	66.1	64.3	75.9	58.3	243.0	29.3	67.0	167.0	162.0	31.6	44.3
14 -	65.7	61.6	76.7	79.5	49.1	74.9	31.8	45.5	132.0	56.0	155.0	48.4
15	68.9	43.3	46.9	80.0	56.2	60.0		82.5	136.0	45.2	62.8	64.6
16	69.6	34.5	53.3	80.8	53.0	112.0	27.6	93.0	101.0	30.6	50.2	50 <b>.6</b>
17	59.8	36.7	49.2	60.3	71.2	159.0	91.5	178.0	84.7	52.6	24.4	62.8
18	73,3	62.0	122.0	70.5	66.0	130.0	23.6	154.0	74.6	55.0	28.5	31.4
19	71.3	31.3	47.2	63.2	57.8	59.5	29.4	161.0	93.6	70.4	52.5	33.4
20	63.7	27.0	54.5	51.0	57.8	73.4	26.9	120.0	73.4	78.2	38.9	42.0
21	82.5	22.8	65.2	53.0	53.1	207.0	38.6	101.0	75.4	27.7	50.6	32.1
$\overline{n}$	51.5	71.3	53.4	51.0	101.0	73.4	38.1	57.1	116.0	76.5	32.1	44.5
23	55.8	36.2	48.3	54.6	54.2	93.8	69.0	93.6	137.0	187.0	32.0	27.2
24	47.7	38.7	54.1	59.1	104.0	100.0	63.3	89.8	57.4	40.4	27.4	35.7
25	68.4	53.8	23.6	67.0	69.2	430.0	89.6	129.0	137.0	30.2	24.4	28.0
26	27.7	62.0	128.0	50.8	88.0	110.0	220.0	137.0	155.0	44.2	25.5	42.2
27	25.2	51.9	114.0	72.9	80.8	68.2	55.8	148.0	124.0	25,6	22.7	32.6
28	28.2	61.2	48.6	56.2	45.6	70.1	58.6	90.2	182.0	44.4	31.8	33.8
29	30.8	· .	45.8	52.6	\$0.0	69.3	66.3	78.1	190.0	36.7	29.0	37.2
30	33.3		52.2	78.3	108.0	72.9	50.5	129.0	74.0	24.5	31.3	61.2
-31	25.4		50.0		104.0		69.9	85.4		71.5		26.9
Total	1,514.0	1,397.8	2,034.3	1,908.2	2,055.5	3,770.3	1,838.5	3,037.8	4,541.2	1,961.3	1,641.0	1,343.7

Annual Total =

27,043.6

## Table 3.19 Daily Suspended Sediment Concentration at Ta Pao (2/2)

#### Ta Pao Gauging Station: Year 1990

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											(Unit:ton'da	y)
Date	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dee
1	30. <b>6</b>	35.4	111.5	43.5	8.1	59.5	332.9	F105.2	2,802.2	1,474.5	187.8	610.3
2	39.7	38.5	31.7	37.1	25.4	92.9	274.6	432.7	4,100.5	2,367.4	162.5	172.1
3	43,4	24.9	54.1	510	26.2	122.9	229.5	385.4	11,136.8	1,251.3	490.1	181.4
4	34.1	27.5	91.2	42.0	25.1	44.0	397.5	594.9	12,993.5	1,208.1	1,103.2	132.2
5	38.3	- 31.1	88.1	30.9	5.4	60.6	159.5	239.3	20,715.8	587.2	218.6	218.9
: 6	33.8	26.9	26.9	35.2	49.1	69.9	170.9	625.9	4,664.3	363.5	198.6	165.3
. 7	56.8	62.4	-19.3	30.4	49.5	1,837.4	559.2	678.6	2,341.8	530.9	201.0	159.1
8	76.6	59.3	48.0	30.5	62.2	355.1	248.8	263.2	2,803.9	542.8	203.8	162.4
9	67.8	48.6	58.9	27.4	30.8	168.4	1,121.3	891.2	4,279.2	1,551.3	3,811.8	155.5
10	61.8	43.2	18.1	38.3	34.9	143.7	334.4	539.9	3,401.4	1,388.3	4,133.2	226.4
- 11	106.6	48.0	56.1	42.0	24.2	373.7	543.1	465.7	3,525.5	372.3	968.5	151.8
12	111.8	48.3	61.6	31.8	32.1	380.3	283.0	809.8	2,721.9	1,491.6	674.5	131.0
:13	86.2	47.4	61.7	39.3	39.6	1,049.8	153.7	396.0	2,294.2	2,435.4	346.7	159.2
14	82.3	42.8	77.5	40.0	35.2	271.8	164.9	237.1	1,733.5	643.5	2,035.6	167.3
15	82.2	29.4	39.6	78.8	38.2	318.8	186.8	450.5	1,809.6	472.5	629.4	220.5
16	79.4	23.5	40.4	90.1	37.0	2,254.7	121.6	948.2	1,317.7	304.0	442.4	168.3
17	68.2	23.6	32.5	56.8	52.4	4,959.3	426.9	2,014.7	1,097.7	<b>5</b> 36.3	198.8	197.5
18	81.7	39.8	74.3	56.5	43.6	2,617.1	102.0	2,741.0	902.4	622.5	219.9	96.0
19	77.6	20.1	27.2	43.0	39.3	668.3	116.3	4,270.5	841.1	936,7	418.7	99.3
20	69.3	18.4	30.5	32.7	39.3	684.9	124.8	3,048.2	1.059.1	905.4	288.4	124.8
21	87.7	15.5	37.6	30.5	32.3	2,468.1	234.5	1,919.8	905.5	296.8	361.6	96.8
22	53.4	48.5	38.3	27.8	64.8	983.0	269.9	828.8	1,473.3	1,084.0	225.8	132.3
23	57.9	24.6	30.2	28.3	33.0	1,385.8	507.3	1,706.4	1,669.0	2,698.2	213.2	76.1
24	47.0	24.8	33.8	30,6	99.7	2,013.1	441.9	2,475.0	674.5	432.8	175.2	93.8
25	67.4	34.5	21.0	34.7	70.0	8,173.4	596.9	4,514.0	1,964.9	310.5	150.7	71.4
26	26.6	42.2	122.8	25.5	114.8	1.663.2	2,090.9	5.350.2	2,370.4	416.3	152.0	105.4
27	23.7	39.3	121.2	40.0	163.4	754.2	398.7	4,590.6	2,785.5	269.8	131.8	84.2
28	27.8	54.5	42.0	29.1	74.1	678.3	494.2	2,797.8	5,126.3	425.8	177.8	85.9
29	29.0		32.8	25.7	124.4	610.7	552.2	3,137.7	4,465.2	307.6	155.8	88.1
30	30.5		33.5	38.3	171.7	605.3	355.2	5,773.4	1,655.9	188.2	163.3	142.2
31	22.6		31.3		135.7	<u> </u>	551.4	3,792.6		518.3	·	59.0
Total	1,801.8	1,023.1	1,593.8	1,187.9	1,781.8	35,868.3	12,544.6	58,021.4	109,632.4	26,933.9	18,840.7	4,734.3

Annual Sediment Load	=	273,964.0 ton/year
Specific Weight	=	1.2 ton/m3
Annual Sediment Load	-	228,303.3 m3/year
catchment	-	2,000 km2
denundation rate	<b>#</b>	0.114152 mm/year

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## Table 3.20 Daily Suspended Sediment Concentration at Phu Dien (1/4)

#### Phu Dien Gauging Station: Year 1987

Date	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	ing/m3 Dec
1	20.3	7.9	11.2	10.2	11.4	39.8	66.8	49.4	14.4	31.0	19.2	72.3
2	20.3	7.9	11.2	10.2	11.4	39.8	66.8	49.4	31.0	31.0	19.2	72.
3	20.3	7.9	11.2	10.2	11.4	36.4	71.6	74.2	30.4	47.9	18.4	67.
4	20.3	6.9	10.4	9.4	29.9	36.4	71.6	74.2	30.4	47.9	18.4	67.
4 5	20.3	14.1	10.4	9.4	14.3	37.8	78.5	74.0	17.6	44.2	20.8	25.
	20.3	6.9	10.4	9.4	14.3	37.8	78.5	74.0	30.0	412	20.8	25.
6		10.3	12.2	8.6	:14.3	41.9	66.6	59.6	29.7	40.4	22.1	25.
7	20.3	10.3	12.2	8.6	17.3	41.9	66.6	59.6	29.7	40.4	22.1	25.
8	20.3 16.1	10.3	12.2	8.6	17.3	41.5	53.1	60.0	29.4	17.9	20.0	25.
9			9.7	8.9	17.3	33.8	53.1	60.0	29.4	17.9	8.3	28.
10	16.1	9.1		8.9	12.8	57.0	72.0	55.3	29.2	18.6	17.2	28.
11 I	16.1	9.1	9.7		12.8	57.0	53.1	55.3	29.2	12.6	17.2	28
12	20.3	9.1	14.1	8.9			65.0	53.3 74.6	33.1	12.6	27.8	37.
13	20.3	9.6	8.3	8.2	12.8	104.0		143.0	33.1	12.0	27.8	37
14	20.3	9.6	8.3	8.2	14.6	104.0	65.0			22.6	69.6	25
15	24.3	5.6	8.3	8.2	14.6	69.7	165.0	152.0	53.2		112.0	21
16	24.3	9.4	21.8	8.1	14.6	89.9	177.0	121.0	39.2	30. <b>5</b> 28.4	101.0	21
17	24.3	9.4	9.7	8.1	12.6	143.0	147.0	99.0	41.6			21
- 18	16.1	9.4	17.4	8.1	12.6	126.0	112.0	99.0	41.6	28.4	42.0	29
19	26.1	- <b>0.1</b> -	11.0	8.4	12.6	158.0	138.0	90.5	22.3	66.8	36.5	
20	16.1	11.1	11.0	8.4	19.6	55.2	128.0	90.5	8.3	66.8	39.0	29
21	17.2		11.0	8.4	19.6	55.2	78.5	85.0	23.7	28.0	39.0	29
22	17.2	6.8	11.2	8.4	32.6	49.4	78.5	91.5	12.8	28.0	61.4	41
23	17.2	6.8	11.2	8,4	38.9	49.2	78.5	95.4	25.2	65.2	61.4	41
- 24	20.8	6.8	11.2	8.4	38.9	45.6	47.4	90.0	25.2		61.3	41
25	20.8	6.8	9.7	6.4	38.9	39.8	47.4	85.5	26.6	31.9	61.3	52
26	20.8	6.8	9.9	6.4	25.6	39.8	47.5	69.4	26.8	31.9	45.0	52
27	16.3	6.8	9.9	6.5	25.6	47.0	45.7	65.2	14.8	56.5	45.0	52
28	16.3	6.8	10.0	6.7	22.4	44.2	51.2	48.3	28.1	56.5	45.0	20
29	16.3	9.0	10.0	6.7	22.4	63.0	51.2	40.3	29.5	40.1	31.2	20
30	16.3		10.0	6.7	22.4	63.0	50.3	64.6	29.5	40.1	31.2	20
31	16.3	i	10.0		22.4	: : :	50.3	61.4		16.1		20
Total	598.3	252.7	344.6	249.7	608.2	1,847.1	2,421.8	2,416.2	845.0	1,121.9	1,161.2	i 1,105

Annual Total = 12,972.6

# Table 3.20 Daily Suspended Sediment Concentration at Phu Dien (2/4)

#### Phu Dien Gauging Station: Year 1987

											(Unit: to:	ns'day)
Date	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec
1	67.4	15.8	15.4	8.8	7.7	46.4	588.7	623.2	436.7	790.1	262.1	748.6
2	65.9	15.8	166.6	8.3	7.1	46.4	594.5	563.4	865.1	768.7	257.1	723.6
3	65.9	15.3	17.9	8.3	6.7	48.7	686.7	814.2	782.7	1,167.1	228.9	560.5
4	65.9	13.1	16.6	9.0	23.0	41.5	760.9	794.9	722.3	1,179.5	213.0	476.2
5	64.5	26.9	15.5	14.0	13.0	36.3	997.0	805.6	392.3	1,088.4	222.8	161.1
6	64.5	13.1	15.5	11.0	16.7	36.3	1,193.7	754,4	642.8	1,034.6	201.3	151.2
7	63.3	18.2	16.8	8.2	17.4	44.5	1,001.2	493.3	615.9	970.4	202.4	143.4
8	63.3	18.2	15.5	8.7	22.0	48.9	880.4	469.1	595.3	956.4	190.9	137.6
9	51.2	18.2	15.5	12.8	20.2	52.7	564.3	414.7	561.4	414.5	171.1	127.9
10	50.2	15.6	11.3	13.2	18.4	39.4	495.5	426.1	541.1	408.3	72.7	135.0
11	46.3	15.6	11.3	10.8	12.3	97.5	634.5	395.1	529.8	411.4	160.5	139.4
12	57.2	15.1	15.7	9.5	12.3	117.2	430.3	386.1	542.4	267.8	160.5	156.8
13	54.9	15.3	9.3	7.8	15.6	286.6	506.0	545.3	623.4	252.6	240.2	211.0
14	53.1	15.8	8.9	7.1	43.2	299.2	730.1	1,483.3	634.9	229.5	261.8	208.0
15	62.8	8.9	9.7	7.1	15.5	251.1	2,594.6	2,101.2	1,084.8	390.5	769.7	124,4
16	62.8	15.1	44.8	8.6	14.0	399.2	3,180.9	2,205.9	897.5	500.7	1,451.5	94.5
17	59.8	14.5	27.3	7.3	9.7	876.0	2,845.0	1,924.6	1,024.4	463.8	1,247.9	91.5
18	39.6	14.5	47.1	10.8	8.5	980.9	2,293.4	2,018.6	1,085.5	446.6	504.4	90.0
19 -	64.3	16.5	23.9	8.9	9.7	1,911.2	3,123.9	1,884.4	614.6	1,038.9	410.0	117.
20	38.8	15.8	17.6	8.9	16.9	896.6	3,218.2	1,900.1	255.8	1,010.0	377.4	113.6
21	40.4	15.8	13.4	11.5	24.9	1,006.3	2,129.7	2,012.3	798.6	408.8	299.6	108.9
22	41.5	9.7	12.5	11.5	52.1	883.5	2,190.7	2,577.2	440.2	382.2	440.3	144.3
23	41.5	9.7	13.9	11.5	80.0	731.2	2,190.7	3,189.9	844.8	878.8	411.7	141.
. 24	50.1	9.7	14.2	8.1	73.3	488.5	1,277.8	3,359.2	812.1	890.1	395.1	138.
25	47.6	9.3	10.3	5.5	59.8	301.6	1,204.0	3,627.1	820.5	424.4	422.1	173.2
26	46.4	9.3	9.5	5.2	32.5	240.7	1,112.2	3,190.0	787.3	432.7	293.5	190.
27	35.3	9.7	9.5	5.0	32.5	255.0	995.0	2,844.8	427.1	795.7	297.4	220.
28	34.5	9.4	9.0	5.2	34.4	218.1	1,030.7	1,973.9	791.5	810.3	305.6	77.5
29	33.5		9.6	4.5	33.3	371.2	920.1	1,525.1	800.3	557.8	220.8	69.
30	33.5		9.6	4.5	31.9	524.7	808.3	2,282.8	774.8	533.6	269.6	65.2
31	33.5		8.5	:	28.4		717.1	2,015.9		215.6		63.9
Total	1,599.9	400.1	641.9	261.6	892.9	11,577.6	41,896.2	49,601.7	20,745.8	20,169.8	10,962.0	6,101.1

Annual Sediment Load Specific Weight Annual Sediment Load catchment denundation rate = 164,853.5 ton'year = 1.2 ton'm3 = 137,377.9 m3'year = 3,060 km2 = 0.04489 mm/year 0

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# Table 3.20 Daily Suspended Sediment Concentration at Phu Dien (34)

	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec
Date	19.5	2.8	7.7	10.6	3.3	34.0	33.3	57.9	34.7	31.7	25.0	13.7
2	24.6	3.6	7.7	10.6	3.3	31.4	33.3	77.9	34.7	31.7	25.0	13.7
2	24.6	3.6	7.7	10.6	3.3	34.0	33.3	64.0	347	31.7	25.0	13.7
•	28.6	3.8	8.8	14.0	2.8	31.0	48.0	65.2	42.0	29.3	20.7	10.3
4	28.6	3.8 3.8	8.8	14.0	2.8	31.0	48.0	60.3	42.0	29.3	20.7	13,6
5 6	28.6	3.8	8.8	14.0	2.8	31.0	48.0	60.3	42.0	29.3	20.7	13.0
7	14.7	2.7	7.1	23.3	1.8	67.0	44.7	32.7	35.3	46.0	49.7	10.3
8	14.7	2.7	7.1	23.3	2.0	80.0	44.7	32.7	35.3	46.0	49.7	10.3
8 9	14.7	2.7	7.1	23.3	2.0	80.0	447	32.7	35.3	46.0	40.7	15.4
	9.3	3.2	11.2	18.3	1.7	43.3	51.3	31.3	37.7	64.0	33.3	10.0
10	9.3 9.3	3.2	11.2	18.3	1.7	43.3	51.3	31.3	37.7	64.0	33.3	10.
11	9.5 8.7	32	11.2	18.3	1.7	43.3	51.3	32.3	37.7	64.0	33.3	10.
12		3.2	7.5	19.3	2.0	47.0	75.0	44.6	40.7	32.3	13.7	6,
13	7.6	3.2	7.5	10.7	2.0	47.0	80.2	44.6	40.7	32.3	13.7	6.
14	7.6 7.6	3.2 3.2	7.5	19.3	2.0	47.0	75.0	44.6	40.7	32.3	11.6	6
15		3.2	7.5	8.7	4.0	44.0	52.7	32.3	55.9	22.6	19.0	5.
16	7.3 7.3	3.2	7.5	8.7	6.0	46.3	52.7	32.3	63.3	22.6	19.0	5.
17	7.3	3.2	7.5	8.7	6.0	46.3	52.7	32.3	63.3	22.6	19.0	5.
18		5.8	7.6	3.7 7.0	10.3	42.7	57.6	21.7	59.3	13.0	16.3	3
19	3.5 8.9	5.8 	7.6	4.8	10.3	42.7	64.0	21.7	59.3	13.0	16.3	3
20	8.9	5.8	7.6	4.9 7.0	10.3	42.7	57.6	21.7	59.3	13.0	16.3	3 3
21. · ·	6.6	5.8 6.2	7.6	9.0	19.9	26.3	57.6	29.0	86.7	18.2	26.7	5
22 23	0.0 6.6	5.9	6.9	9.0	19.9	31.3	57.6	29.0	86.7	18.2	26.7	5
23 24	6.6	6.2	6.9	9.0	19.9	26.3	57.6	29.0	129.0	18.2	26.7	5
	4.4	6.0	6.9	7.7	28.6	23.7	64.0	27.0	79.3	23.3	23.3	9
25 26	4.4 4.4	6.0	6.3	7,7	28.6	23.7	64.0	27.0	54.8	23.3	23.3	.: <b>` 9</b>
26	4.4	6.0	6.3	7.7	28.6	23.7	64.0	21.6		23.3	23.3	9
27	4.4	6.7	6.3	6.7	24.5	16.0	70.3	28.5	43.3	19.8	11.0	3
28		6.7	7.3	6.7	1	16.0	70.3	28.5	43.3	19.8	11.0	3
29	4.0 4.0	0.7	7.3	6.7	24.5	16.0	70.3	35.0	50.0	19.8	11.0	4
30			7.3	0.7	24.5	10.0	61.0	35.0		19.8		4
31	4.0 340.8	125.4	241.1	362.7	325.8	1,158.0	1,736.1	1,164.0	1,584.0	920.4	705.0	251
Total	540.8	12.1.4	271.1					·				

#### Phu Dien Gauging Station: Year 1988

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#### Table 3.20 Daily Suspended Sediment Concentration at Phu Dien (4/4)

# Phu Dien Gauging Station: Year 1988

<u> </u>							v			<del></del>	(Unit: to	ns/day)
Date	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	<u> 0:1</u>	Nov	Dec
<b>)</b>	72.4	5.5	12.4	11.4	4.0	132.2	257.8	923.5	349.9	748.3	310.8	87.8
2	87.1	6.7	10.3	13.4	4.4	183.7	248.0	1,610.6	313.9	753.2	337.8	85.2
3	85.0	6.5	10.3	12.6	4.4	192.7	225.9	1,394.0	286.0	784.1	331.8	82.7
4	103.8	6.9	11.7	15.1	3.4	169.8	316.8	1.506.9	350.5	729.6	255.0	59.3
5	116.1	6.9	11.7	15.1	3.1	175.7	303.2	1,423.4	388.3	705.8	230.7	74.5
6	121.1	6.7	11.7	13.8	2.8	201.7	289.9	1,374.4	379.9	677.2	208.7	71.9
1	64.8	4.8	9.4	22.9	1.6	619.4	270.0	680.3	280.6	1,027.4	701.7	54.6
8	57.2	4.8	9.9	24.0	1.8	994.6	286.6	589.4	273.3	1,015.9	995.8	52.7
9	52.1	4.6	10.4	25.2	1.8	938.6	355.3	497.2	252.5	1,070.7	909.0	74.5
10	30.6	5.4	18.0	26.9	1.5	400.3	479.6	426.7	291.9	1,541.7	813.1	47.5
11	29.8	5.4	18.0	28.1	1.5	370.0	459.2	400.2	318.6	1,614.6	840.1	49.2
12	27.0	5.1	16.5	26.9	1.6	392.4	428.2	367.5	295.8	1,737.4	850.8	42.3
13	23.1	5.1	9.9	25.7	2.3	43.0	663.6	517.9	343.9	987.4	363.5	27.1
14	21.8	5.1	9.4	14.2	2.7	411.0	846.8	635.0	360.1	1,075.5	365.5	26.5
15	20.7	4.9	9.4	32.3	3.3	579.1	888.4	773.0	368.2	1,085.6	296.4	25.9
- 16	19.2	4.7	9.0	13.9	7.0	610.5	636.5	568.7	483.5	735.4	445.4	21.6
17	18.7	4.7	8.1	13.9	12,2	664.9	686.6	524.1	553.5	704.5	400.1	20.6
18	18.2	5.1	7.7	13.9	13.9	715.3	756.8	483.4	683.1	662.7	339.8	20.1
. 19	8.7	9.3	7.8	9.8	21.5	654.5	926.7	303.7	702.4	352.9	222.5	11.8
20	21.7	10.9	7.4	5.7	18.7	577.0	1,126.9	277.5	695.8	330.0	187.3	11.5
21	21.1	10.9	7.4	7.6	16.7	480.7	1,093.9	264.7	660.9	311.0	172.1	11.5
22	15.7	12.6	7.1	9.7	26.5	240.6	1,124.7	316.2	935.6	417.7	263.0	18.0
23	15.3	14.5	6.5	12.0	26.5	239.3	1,062.0	279.9	945.3	404.1	249.6	17.5
24	15.3	14.7	6.2	12.6	26.5	178.4	889.8	247.3	1,977.2	392.5	236.2	17.0
25	10.3	15.0	5.9	10.7	61.8	174.1	833.9	209.0	1,429.2	484.8	196.9	29.8
26	10.0	13.0	5.4	10.2	86.5	174.9	728.2	214.6	1,083.8	472.7	189.8	28.2
27	9.7	12.5	5.4	10.2	81.5	193.1	713.3	162.9	1,690.3	455.0	180.4	28.2
28	8.6	13.4	5.1	7.5	93.1	120.7	717.3	209.3	928.5	373.3	80.8	9.5
29	8.6	11.6	5.8	.7.2	82.6	119.2	614.7	234.9	939.4	354.1	76.7	9.3
30	8,3	18 a. S. 18	6.1	7.2	74.1	122.3	558.8	361.1	1,246.3	310.7	73.6	10.9
31	8.0		7.2		78.3		478.6	390.1		258.0		10.9
Total	1,130.1	237.3	287.0	459.9	767.5	11,069.7	19,267.8	18,167.6	19,808.2	22,573.5	11,124.8	1,138.2

Annual Sediment Load Specific Weight Annual Sediment Load catchment depundation rate = 106,031.6 ton/year
 = 1.2 ton/m3
 = 88,359.6 m3/year
 = 3,060 km2
 = 0.02888 mm/year

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## Table 3.21 Sedimentation Rates of Selected Reservoirs in the United States (1/2)

	Net	Year	Period	0-1-1-1	annual	Loss	
Name and location	drainage area,	storage began	of record,	Original capacity,	sediment- production	storag	e, 70
	sq mi	U gan	years	acre-ft	rate, tons/sq mi	Annüa]	Total
Northeast							
Barcroft, Alexandria, Va.	14.30	1915	42.6	2,092	618	0.38	12.1
Schoharie, Prattsville, N.Y.	312	1926	23.8	63,812	217	0.07	1.7
Byllesby, Byllesby, Va. Southeast	. <b>1,310</b>	1912	23.7	8,892	238	2.54	60.2
Franklinton, Franklinton, N.C.	1.12	1925	13.3	34.7	743	1.60	21.2
Concord, Kannapolis, N.C.	4.54	1925	10.2	1,201	2,235	0.65	6.5
Roxboro, Roxboro, N.C.	7.52	1924	22.6	531		0.69	15.6
ssaqueena, Clemson, N.C.	13.90	1938	11.4	1,836	1 .	1.01	11.5
larris, Tuscaloosa, Ala.	29.80	1929	24.5	2,241		0.16	3.8
High Point, High Point, N.C.	62.30	1928	10.3	4,354		0.71	7.2
Spartanburg, Spartanburg, S.C.	90.80	1926	20.9	3,506		0.84	17.5
Volichucky, Greenville, Tenn.	1,182	1913	39.8	21,750		1.40	55.0
Norris, Norris, Tenn.	2,823	1936	10.3	2,045,300		0.05	0.5
ay, Clanton, Ala.	9,077	1913	22.3	156,525		0.52	- 11.
Midwest	,						••••
Caldwell, Waberly, Ohio	1.00	1949	12.0	88	331	0.29	3.4
Decker, Piqua, Ohio	2.30	1940	10.0	115		1,83	18.3
hepard Mountain, Ironton, Mo.	3.96	1929	10.0	171	471	0.78	7.8
Vestville, Alliance, Ohio	8.22	- 1913	37.0	994	287	0.16	6.1
Jpper Pine, Eldora, Iowa	13.80	1934	13.3	660		2.38	31.5
Carlinville, Carlinville, 18.	25.80	1939	10.4	1,725		1,40	14.5
Bloomington, Bloomington, Ill.	60.30	1929	22.7	6,678		0.50	11.4
Crab Orchard, Carbondale, Ill.	160	1940	11.2	67,320		0.45	5.0
Springfield, Springfield, Ill.	258	1934	14.6	61,039		0.30	4.3
Faneycomo, Branson, Mo.	4,606	1913	22.4	43,980		2.06	46.1
Lake of the Ozarks, Eldon, Mo. South Central	13,900	1931	17.8	2,037,223	598	0.31	5.5
Loring, Zwolle, La.	0.95	1928	26.0	663	3,002	0,23	6.0
Grand Saline, Grad Saline, Tex.	2.02	1925	13.2	531		0.31	4,1
Ardmore Club, Ardmore, Okla.	3.91	1922	15.5	1,797		0.55	8.5
Boomer, Stillwater, Okla.	8.67	1925	10.3	2,812		0.59	6.0
Scarborough, Coleman, Tex.	10.60	1923	17.0	2,153		0.40	6.7
Clinton, Canute, Okla.	23.10	1930	19.8	4,415		1.23	24.2
Eddleman, Graham, Tex.	41.40	1929	25.3	6,538	687	0.40	10.1
Abilene, Abilene, Tex.	97.50	1921	27.0	10,325	274	0.19	5.2
Spavinaw, Spavinaw, Okła.	397	1924	11.0	31,686	1 1	0.34	3.1
Eagle Mountain, Ft. Worth, Tex.	809	1934	18.0	211,000		0.69	13.7
Dallas, Denton, Tex.	1,1,57	1928	10.5	180,759	1,304	0.72	7.5
Altus, Altus, Okla. Northern Great Plains	2,116	1948	12.6	156,668	778	0.70	8.8
Bennington, Rago, Kans.	1.40	1929	11.2	- 75		5.00	56.0
Kirk, Iola, Kans.	2.36	1897	42.0	111	450	0.91	38.3
Baker, Baker, Mont.	5.01	1908	29.1	756		1.15	33.0
Mission, Horton, Kans.	7.76	1924	13.0	1,852		1.20	15.0
Ericson, Ericson, Nebr.	41.00	1915	32.9	1,056		1.08	35.4
Sheridan, Quinter, Kans.	463	1948	10.8	436	123	4.06	43.9
Buffalo Bill, Cody, Wyo. Suernsey, Guernsey, Wyo.	1,460 5,400	1910 1927	31.0 26.4	455,838 73,810	461	0.11	3.9 39.
Seminoe, Leo, Wyo.	7,317	1927	11.5	1,020,000		0.08	0.9



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Sedimentation Rates of Sel	

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	Net	Year	Period		annual	Loss	of
	drainage	storage	of	Original	sediment-	storag	e, %
Name and location	area,	began	record,	capacity,	production	T	
	sq mi		years	acre-ft	rate,	Annual	Total
					tons/sq mi		
Southwestern(Continued)		1	:	· · ·			
Camp Marston, Julian, Calif.	1.59	1918	33.0	44	183	0.50	16.30
St. Marys, Walnut Creek, Calif.	2.97	1928	23.0	134		1.47	33.90
Gilmore, Bellota, Calif.	4.92	1917	28.0	579	144	0.11	3.10
Upper Crystal Springs,	,.,,	1	20.0	577			
San Francisco, Calif.	12.00	1878	57.8	29,138	1,843	0.06	3.4
Morena, San diego, Calif.	109.00	1910	38.3	66,767		0.31	11.70
Muddy Creek, Caddoa, Colo.	152	1919	20.0	16,918		0.48	9.64
Hodges, Escondido, Calif.	301	1919	29.5	36,601	531	0.29	8.50
Cucharas, Walsenburg, Colo.	608	1912	27.0	38,274		1,47	39.80
Sevier Bridge, Nephi, Utah	1,089	1908	24.0	250,000		0.26	6.20
Piute, Marysville, Utah	2,436	1910	28.0	81,200		0.32	8.90
Roosevelt, Globe, Ariz.	5,760	1909	36.8	1,522,200		0.25	9.20
McMillan, Carlsbad, N.M.	12,600	1894	46.1	91,000	147	1.25	\$7.50
John Martin, Cuddoa, Colo.	17,080	1942	9.5	701,775	396	0.60	5.54
Elephant Butte, Truth or							
Consequences, N.M.	25,866	- 1915	32.3	2,634,800	798	0.51	16.60
Mead, boulder City, Nev.	167,600	1935	13.7	31,250,000	877	0.33	4.60
Northwestern	ана алана Алана						
Mud Springs, Mountain Home,							
Idaho	1.06	1939	12.0	12	46	0.25	3.00
High Villey Ranch, Yakima,							
Wash.	4.10	1939	12.0	9	30	0.93	11.20
Emigrant Gap, Ashland, Ore.	61.20	1924	27.0	8,300	280	0.16	4.30
Cold Springs, Cold Springs, Ore.	186	1908	43.0	49,709	1,070	0.24	10.10
Arrowrock, Boise, Idaho	2,170	1915	2.80	279,250	173	0.09	2.80
Black Canyon, Emmett, Idaho	2,540	1924	12.0	37,659	173	0.89	10.70

Source: Handbook of applied Hydrology: Chow, 1964