TABLE A.5-4 FUTURE OD TABLE BY VEHICLE TYPE: ROUTE C (1/6) - YEAR 2000 -

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	D	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	Tota
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	2	66	0	6	1	4	0	0	• 0	0	3	0	0	24	0	1	0	0	10
	3	43	6	0	11	6	0	0	0	0	4	0	0	0	0	19	0	0	9
	4	8	2	9	0	4	0	0	Ð	0	2	0	2	29	0	1	0	0	
	5	323	5	4	1	173	8	4	1	0	3	0	0	1	0	110	0	0	63
	6	2	0	1	0	10	. 0	17	1	0	0	0	0	0	0	0	0	0	3
	7	. 2	0	્ 1	0	3	21	0	5	0	0	0	0	0	0	0	0	• 0	3
	8	1	0	0	0	0	0	8 '	0	0	0	0	0	0	0	0	0	0	1
	- 9	2	1	1	. 0	1	-0	0	0	0	7	0	0	0	0	0	0	0	1
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	2	59	0	4	2	3	0	0	0	0	4	0	° 0.	4	0	0	0	0	Ĩ
	3	25	4	0	6	2	0	0	0	0	2	0	0	4	; 0	5	0	0	: 4
	4	6	2	8	0	2	- Q	0	0	0	2	2	2	5	0	0	0	<u>`</u> 0.	
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	10	17	4	2	2	2	0	0	. 0	3	0.	. 1	0	2	0	· ·	0 0	0	1
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TABLE A.5-4 FUTURE OD TABLE BY VEHICLE TYPE: ROUTE C (2/6) - YEAR 2000 -

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A.5-16

TABLE A.5-4 FUTURE OD TABLE BY VEHICLE TYPE: ROUTE C (3/6) - YEAR 2010 -

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10(a) 55 21 16 8 60 / 11 3 5 11 6 12 24 0 66 0 0 660	.									· · · ·		-										
		1	otal	55	21	16	8	66	1	11	3	3			16	<u> </u>			•			

A.5-17

TABLE A.5-4	FUTURE OD TABLE BY	VEHICLE TYPE:	ROUTE C	(4/6) - YEAR 20)10 -

Truck	
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0	D	1	2	3	4	5	6	7	- 8	9	10	11	12	13	14	15	16	17	Tot
	1	0	15	6	2	98	0	0	0	0	5	0	0	3	0	57	0	0	18
	2	11	0	- 3	0	2	0	0	0	0	2	0	. 0	3	0	0	0	0	2
	3	6	0	0	2	0	0	0	0	0	0	0	0	3	0	5	0	0	1
	4	3	0	3	0	0	0	0	0	0	0	0	0	3	0	191	Q	0	20
	5	94	4	0	0	64	4	2	0	0	0	0	0	3	0	71	0	0	24
	6	0	0	0	0	2	0	5	0	· 0	0	0	0	0	0	0	0	0	
	7	0	0	0	0	4	3	0	0	0	0	0	0	Ó	0	Ó	Ō	0	
	8	0	0	Ó	· 0	0	0	0	0	0	0	0	0	0	Ō	0	ō	Ō	
	9	0	0	0	0	0	0	Ó	0	0	3	Ô	Ō	0	-0	0	ŏ	ō	
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	15	66	. 0	ŏ	191	72	ŏ	õ	ŏ	ŏ	ŏ	ŏ	ŏ	ŏ	ŏ	0	0	29	35
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	Total	188	22	15	200	245		7	0	3	12		0	0	0	29	0	0	
	Tutal	100	22	13	200	240					12	6	13	27	0	360	0	29	1,13
	ehicle																·		
0	D	1	2	3	4	5	8	7	8	9	10	11	12	13	14	15	16	17	Tot
	D 1	: 0	346	208	44	940	9	3	0	10	103	0	0	63	0	368	16 0	0	2,09
	D 1 2	0 331	346 0	208 26	44 7	940 16	9 1	3 1	0	10 0	103 19	0 0	0	63 55	0	368 2			2,09 45
	D 1 2 3	0 331 192	346 0 22	208 26 0	44 7 42	940 16 21	9 1 1	3 1 1	0	10 0 0	103 19 16	0 0 0	0 0 0	63 55 13	0 0 0	368 2 57	0	0 0 0	2,09
	D 1 2 3 4	0 331 192 41	346 0 22 8	208 26 0 39	44 7 42 0	940 16 21 12	9 1 1 1	3 1 1 1	0 0 0 0	10 0 0	103 19 16 8	0 0 0 3	0 0 0	63 55 13 72	0 0 0 0	368 2 57 192	0 0	0 0 0	2,09 45 36 36
	D 1 2 3 4 5	0 331 192 41 892	346 0 22 8 27	208 26 0 39 19	44 7 42 0 9	940 16 21 12 810	9 1 1 1 37	3 1 1 1 24	0 0 0 0 3	10 0 0 1	103 19 16 8 13	0 0 3 0	0 0 0 11 1	63 55 13 72 9	0 0 0 0 0	368 2 57 192 470	0 0 0	0 0 0	2,09 49 36 38 2,31
	D 1 2 3 4 5 6	0 331 192 41 892 13	346 0 22 8 27 1	208 26 0 39 19 1	44 7 42 0 9	940 16 21 12 810 33	9 1 1 1 37 0	3 1 1 1 24 77	0 0 0 3 8	10 0 0 1 0	103 19 16 8 13 1	0 0 3 0	0 0 11 1 0	63 55 13 72	0 0 0 0	368 2 57 192	0 0 0	0 0 0	2,09 45 36 38 2,31
	D 1 2 3 4 5 6 7	0 331 192 41 892 13 4	346 0 22 8 27 1 1	208 26 0 39 19 1 1	44 7 42 0 9 1	940 16 21 12 810 33 23	9 1 1 37 0 82	3 1 1 24 77 0	0 0 0 3 8 28	10 0 0 1 0	103 19 16 8 13 1 1	0 0 3 0 0	0 0 11 1 0 0	63 55 13 72 9 1 1	0 0 0 0 0 0 0	368 2 57 192 470	0 0 0 0 0	0 0 0 0	2,09 45 36 2,31 13
	D 1 2 3 4 5 6 7 8	0 331 192 41 892 13 4 2	346 0 22 8 27 1 1	208 26 0 39 19 1 1	44 7 42 0 9 1 1	940 16 21 12 810 33 23 0	9 1 1 37 0 82 4	3 1 1 24 77 0 34	0 0 0 3 8 28 0	10 0 0 1 0	103 19 16 8 13 1 1 1 0	0 0 3 0	0 0 11 1 0	63 55 13 72 9 1	0 0 0 0 0 0	368 2 57 192 470 0	0 0 0 0 0	0 0 0 0 0	2,09 45 36 2,31 13 14
	D 1 2 3 4 5 6 7 8 9	0 331 192 41 892 13 4 2 10	346 0 22 8 27 1 1 1 4	208 26 0 39 19 1 1 1 2	44 7 42 0 9 1 1 1 0 0	940 16 21 12 810 33 23 0 3	9 1 1 37 0 82	3 1 1 24 77 0	0 0 0 3 8 28 0 0	10 0 0 1 0	103 19 16 8 13 1 1	0 0 3 0 0	0 0 11 1 0 0	63 55 13 72 9 1 1	0 0 0 0 0 0 0	368 2 57 192 470 0 0	0 0 0 0 0 0	0 0 0 0 0 0 0	2,09 45 36 2,31 13 14 4
	D 1 2 3 4 5 6 7 8 9 10	0 331 192 41 892 13 4 2 10 100	346 0 22 8 27 1 1	208 26 0 39 19 1 1	44 7 42 0 9 1 1 0 0 9	940 16 21 12 810 33 23 0	9 1 1 37 0 82 4	3 1 1 24 77 0 34	0 0 0 3 8 28 0	10 0 0 1 0 0	103 19 16 8 13 1 1 1 0	0 0 3 0 0 0	0 0 11 1 0 0 0	63 55 13 72 9 1 1 0	0 0 0 0 0 0 0 0	368 2 57 192 470 0 0 0	0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0	2,09 45 36 38 2,31 13 14 4 4
	D 1 2 3 4 5 6 7 8 9	0 331 192 41 892 13 4 2 10	346 0 22 8 27 1 1 1 4	208 26 0 39 19 1 1 1 2	44 7 42 0 9 1 1 1 0 9 5 6	940 16 21 12 810 33 23 0 3	9 1 1 37 0 82 4 0	3 1 1 24 77 0 34 0	0 0 0 3 8 28 0 0	10 0 0 1 0 0 0 0 0	103 19 16 8 13 1 1 1 0 27	0 0 3 0 0 0 0 0	0 0 11 1 0 0 0	63 55 13 72 9 1 1 0 0	0 0 0 0 0 0 0 0 0	368 2 57 192 470 0 0 0 1	0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0	2,09 45 36 2,31 13 14 4 4 20
	D 1 2 3 4 5 6 7 8 9 10	0 331 192 41 892 13 4 2 10 100 2 0	346 0 22 8 27 1 1 1 1 4 16 0 0	208 26 0 39 19 1 1 1 2 17 2 2	44 7 42 0 9 1 1 1 0 0 9 6 10	940 16 21 12 810 33 23 0 3 23 0 3 12 2 3	9 1 1 37 0 82 4 0 1 0 0	3 1 1 24 77 0 34 0	0 0 0 3 8 28 0 0 0	10 0 0 1 0 0 0 0 28	103 19 16 8 13 1 1 0 27 0 5 0	0 0 3 0 0 0 0 0 0 0 3	0 0 11 1 0 0 0 0 0	63 55 13 72 9 1 1 0 0 3	0 0 0 0 0 0 0 0 0 0 0 0	368 2 57 192 470 0 0 0 1 16	0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0	2,09 45 36 38 2,31 13 14 4 4 20 5
	D 1 2 3 4 5 6 7 8 9 10 11	0 331 192 41 892 13 4 2 10 100 2	346 0 22 8 27 1 1 1 4 16 0	208 26 0 39 19 1 1 1 2 17 2	44 7 42 0 9 1 1 1 0 9 5 6	940 16 21 12 810 33 23 0 3 12 2 2	9 1 1 37 0 82 4 0 1 0	3 1 1 24 77 0 34 0 1 0	0 0 0 3 8 28 0 0 0 0 0	10 0 0 1 0 0 0 0 28 0	103 19 16 8 13 1 1 0 27 0 5 0 12	0 0 3 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 11 1 0 0 0 0 0 0 0 0 16	63 55 13 72 9 1 1 0 0 3 19	0 0 0 0 0 0 0 0 0 0 0 0 0	368 2 57 192 470 0 0 0 1 16 1 6	0 0 0 0 0 0 0 0 0 0 0 0		2,09 45 36 38 2,31 13 14 4 20 5 15
	D 1 2 3 4 5 6 7 8 9 10 11 12	0 331 192 41 892 13 4 2 10 100 2 0	346 0 22 8 27 1 1 1 1 4 16 0 0	208 26 0 39 19 1 1 1 2 17 2 2	44 7 42 0 9 1 1 1 0 0 9 6 10	940 16 21 12 810 33 23 0 3 23 0 3 12 2 3	9 1 1 37 0 82 4 0 1 0 0	3 1 1 24 77 0 34 0 1 0 0	0 0 0 3 8 28 0 0 0 0 0 0	10 0 0 1 0 0 0 0 28 0 0	103 19 16 8 13 1 1 0 27 0 5 0	0 0 3 0 0 0 0 0 0 0 3 0 16	0 0 11 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	63 55 13 72 9 1 1 1 0 0 3 19 111		368 2 57 192 470 0 0 0 1 16 1 12	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0	Tot 2,09 45 36 2,31 13 14 4 4 20 5 15 35
	D 1 2 3 4 5 6 7 8 9 10 11 12 13	0 331 192 41 892 13 4 2 10 100 2 0 34	346 0 22 8 27 1 1 1 4 16 0 33	208 26 0 39 19 1 1 1 2 17 2 45	44 7 42 0 9 1 1 0 0 9 6 10 57	940 16 21 12 810 33 23 0 33 12 2 3 12 2 3 17	9 1 1 37 0 82 4 0 1 0 3	3 1 1 24 77 0 34 0 1 0 1	0 0 0 3 8 28 0 0 0 0 0 0 1	10 0 0 1 0 0 0 0 0 28 0 0 5	103 19 16 8 13 1 1 0 27 0 5 0 12	0 0 3 0 0 0 0 0 0 0 3 0 16 25	0 0 11 1 0 0 0 0 0 0 0 0 0 0 0 16 0 118	63 55 13 72 9 1 1 0 3 19 111 0		368 2 57 192 470 0 0 0 1 16 1 12 3	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		2,09 45 36 38 2,31 13 14 4 4 20 5 15 35
	D 1 2 3 4 5 6 7 8 9 10 11 12 13 14	0 331 192 41 892 13 4 2 10 100 2 0 34 0	346 0 22 8 27 1 1 1 4 16 0 33 0	208 26 0 39 19 1 1 1 2 17 2 2 45 0	44 7 42 0 9 1 1 0 9 6 10 57 0	940 16 21 12 810 33 23 0 3 12 2 3 12 2 3 17 0	9 1 1 37 0 82 4 0 1 0 3 0	3 1 1 24 77 0 34 0 1 0 0 1 0	0 0 0 3 8 28 0 0 0 0 0 0 0 1 0	10 0 0 1 0 0 0 0 0 28 0 0 5 0	103 19 16 8 13 1 1 0 27 0 5 0 12 0	0 0 3 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 16 25 0	0 0 11 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	63 55 13 72 9 1 1 1 0 3 19 111 0 0		368 2 57 192 470 0 0 0 1 16 1 12 3 0			2,09 45 36 2,31 13 14 4 20 5 15 35
	D 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15	0 331 192 41 892 13 4 2 10 100 2 0 34 0 470	346 0 22 8 27 1 1 1 1 4 16 0 33 0 1	208 26 0 39 19 1 1 1 2 17 2 45 0 1	44 7 42 0 9 1 1 0 9 6 10 57 0 192	940 16 21 12 810 33 23 0 3 12 2 3 12 2 3 17 0 456	9 1 1 37 0 82 4 0 1 0 3 0 0 0	3 1 1 24 77 0 34 0 1 0 0 1 0 0	0 0 0 3 8 28 0 0 0 0 0 0 0 1 0 0	10 0 0 1 0 0 0 0 0 0 0 0 28 0 0 5 0 0	103 19 16 8 13 1 1 0 27 0 5 0 12 0 1	0 0 3 0 0 0 0 0 0 0 0 0 0 0 0 0 16 25 0 0	0 0 11 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	63 55 13 72 9 1 1 0 0 3 19 111 0 0 1		368 2 57 192 470 0 0 1 16 1 12 3 0 0 0 0		0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	2,09 45 36 2,31 13 14 4 4 20 5 15 35 1,15
	D 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16	0 331 192 41 892 13 4 2 10 100 2 0 34 0 470 0 0	346 0 22 8 27 1 1 1 4 16 0 33 0 1 0	208 26 0 39 19 1 1 1 2 17 2 2 45 0 1 0	44 7 42 0 9 1 1 0 9 6 10 57 0 192 0	940 16 21 12 810 33 23 0 3 12 2 3 12 2 3 17 0 456 0 0	9 1 1 37 0 82 4 0 1 0 3 0 0 0 0 0	3 1 1 24 77 0 34 0 1 0 0 1 0 0	0 0 0 3 8 28 0 0 0 0 0 0 0 0 0 0	10 0 0 1 0 0 0 0 0 28 0 0 28 0 0 5 0 0 0	103 19 16 8 13 1 1 0 27 0 5 0 12 0 1 0	0 0 3 0 0 0 0 0 0 0 0 0 0 0 16 25 0 0 0	0 0 11 1 0 0 0 0 0 0 0 0 0 0 0 16 0 0 118 0 0 0 0	63 55 13 72 9 1 1 0 0 3 19 111 0 0 1 1 0		368 2 57 192 470 0 0 0 1 16 1 12 3 0 0		0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 29	2,09 45 36 2,31 13 14 4 4 20 5 15 35 35

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A 5-18

TABLE A.5-4 FUTURE OD TABLE BY VEHICLE TYPE: ROUTE C (5/6) - YEAR 2020 -

<i>.</i>

M/C												·····							
0	Đ	1	2	3	4	5	6	7	8	9	10		12	13 85	<u>14</u> 0	<u>15</u> 309	16 0	17	Tolai 2 354
	1	0	316	218 23	44 1 6	,270 14	6 1	- 1	1 0	9	91 11	0	0	70	Õ	2	õ	ŏ	414
	2 3	286 201	0 20	23	42	25	1	1	ŏ	ŏ	19	ŏ	Ŏ	ō	ŏ	80	0	0	389
	4	34	8	38	õ	11	1	1	Ó	0	7	0	9	89	0	2	0	0	200
	5	1,302	18	18	5	560	29	13	5	1	12	0	1	3	0	389	0	0	2,356
	6	11	2	2	1	35	0	56	6	0	1	0	0	1	0	0	0	0	116 126
	7	6	2	2	1	15	72	0	25 0	0	1	0	0	1	0	0	0	0	44
	8	3 7	1 6	1 5	1	0 4	· 0	37 0	0	0	21	0	0	0	ŏ	1	ŏ	ŏ	45
	9 10	84	9	19	11	13	1	í	ō	24	0	0	0	0	0	15	0	0	177
	11	3	ŏ	3	2	3	0	0	0	0	2	0	5	17	0	1	0	0	36
	12	0	0	5	8	4	0	0	0	, 0 -	0	_ <u></u> 11	0	106	0	11	. 0	0	147
	13	35	33	55	65	- 11	3	- 3	1	6	12	21	125	0	0	2	0 0	0 0	372 0
	14	0	0	0	0	0 408	0	0 0	0	0	0 1	0	0 1	0 1	0	õ	0	. 0	815
	15	398 0	2	2 0	1	400 0	0	0	õ	ŏ	0	ŏ	ò	ò	ō	ŏ	ŏ	Õ	0
	16 17	0	: 0	0 0	ŏ	ŏ	Ö	õ	Ö	Ŏ	Ō	Ō	0	0	Ó	; Q	Ó	0	0
	Tolal		416	391	187 1	2,373	115	119	39	41	179	- 33	142	374	0	813	0	0	7,592
Light													<u>.</u>		-			47	Talat
0	D	1	2	3	4	5	6	7	8	9	<u>10</u> 75	<u>11</u> 0	12	13	<u>14</u> 0	15	. 16	<u>17</u> 0	Total 888
	1	0	236 0	137 13	28 6	121 9	1 0	0	Ő	0	12	ö	Ö	10	ŏ	0	ŏ	ŏ	292
	2	242 121	12	0	22	10	ŏ	0	ŏ	0	. 8	Ō	0	11	0	22	0	0	205
	4	27	7	22	0	8	0	0	0	¹ 0	· .7	4	.7	16	0	0	0	0	98
	5	35	17	- 11	9	525	22	- 14	0	0	9	0	0	6	0	325	0	0	970
	6	- 11	0	0	0	16	0	50	9	0	0	. 0	0	0	0	0	0	0	87 80
	7	0	0	0	0	- 8 -	52	0	19 0	0	0	0	0	0	0	ŏ	° ŏ	0	27
	8 - 9	0	0	0	0	0	.8	. 0	ö	Ö	14	ŏ	ŏ	÷ŏ	. ŏ	Ξŏ	Ö.	0	23
	10	72	12	8	. 7	8	ŏ	ŏ	Ō	12	0	5	0	6	÷ 0	5	0	• • •	136
	: 11	0	0	Ō	5	0	0	0	0	0	5	0	11	5	0	0	0	- 0	26
·	12	0	0	· 0	6	0	0	0	0	0	0	9	0	38	0	· 7	0	0	60 111
	13	11	10	13	14	4	0	0	0	4	5	6	. 40 0	0		3	0	0 0	0
	14	- 0 - 339	0	0	0	0 285	0	0	÷ŏ	0	÷ õ	Ō	÷ŏ	0	· · ř	Ö.	Õ	ō	625
	15 16	3,39	0	0	ŏ	0	ŏ	0	ŏ	ŏ	ŏ	0	0	0.0	÷ Ō	0	0	- Q -	.0
1.5	17		ŏ	Ō	Ō	0	0	0	Ó	0	0	0	0	: 0	<u> </u>	0	0	0	0
	Total	868	294	204	97	995	89	84	28	23	136	24	58	108	0	621	0	0	3,630
						:										:			
Bus									<u>.</u>									17	Total
0	D	1	2		4	5	<u>6</u> 0	7	8	9 0	: 10 · 7	<u>11</u> 0	12	13	14	<u>15</u> 44	<u>16</u> 0	17	Tolai 84
	1		17 0	9 6	3 0	0	0	0	· 0	. 0	5	0	0	6	0	0	ŏ	· ŏ	32
	3		- 4	ŏ	4	, Ö	ŏ	· ŏ	Ö	; Ö	i õ	0	0	- 5	0	6	0	· 0	25
	4				0	0	0	0	:: 0	0	0	. 0	0		0	0	0	0	11
	5	0	0	0	0	22	3	3	0	0	0	0	0	0	0	64	0	0	93
	6				· 0	4	. 0	7	0	0	0	0	0	0 0	0	0	0	0	11 16
	7				0	3	· 8 0	0 5	5	0	0	0	0	· · ŏ	0	0	0	Ö	5
	- 8				0	0	0	0	õ	0	4	ŏ	0	ŏ	. 0	Ŏ	· Õ	· 0	4
	10				ŏ	Õ	ō	Ō	ō	4	0	0	0	÷ • 0	0	0	0	0	16
	11				Ó	0	0	0	0	0		0	4	5	0	0	0	0	9
	12				0	0	0	0	0 A	0	0	4	0	: 14	0	0	0	0	18
	13				4	3	0	0	0	0	0	5 0	14 0	0	· 0 · 0	0	0	0	39 0
	14		0		0	0 61	0	0	0	0		0	Ö	ŏ	: ŏ	Ő	ŏ	· ŏ	115
	15 16				Ő	0	0	ŏ	Ŏ	ŏ			ŏ	ō	Ō	Ő	Ō	0	0
	17		-		Ō	Ŏ	0	0	0	0		0	0	. 0	0	0	0	0	0
	Tota			25	11	- 94	11	15	5	4	16	9	18	33	0	115	0	0	479

TABLE A.5-4 FUTURE OD TABLE BY VEHICLE TYPE: ROUTE C (6/6) - YEAR 2020 -

0	Ð	1	2	: 3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	Tot
	1	0	24	10	3	119	0	0	0	0	7	0	0	5	0	114	0	0	28
	2		0	4	0	4	0	0	0	0	3	0	0	6	0	0	0	0	3
	3		0	0	3	0	· 0	0	0	0	0	0	0	5	0	12	0	0	í
	4	-	0	5	0	0	0	0	0	0	0	0	0	5	0	230	0	0	24
	5		5	0	0	75	6	3	0	0	0	0	0	4	0	136	0	0	34
	6		0	0	; 0	4	0	7	0	0	0	0	0	0	0	0	0	0	1
	7		0	0	0	5	5	0	0	0	0	0	0	0	0	0	0	0	1
	8		. 0	0	0	0	0	0	0	0	0	: 0	0	0	0	0.	0	0	
	9	0	0	.0	0	• 0	0	0	0	0	· 4	0	0	0	0	0	0	0	
	10	9	0	. <u>(</u> 0	0	0	0	0	0	4	0	0	0	0	0	6	: O	:0	1
	11	0	0	0	0	0	- 0	0	0	0	÷ 0	0	4	5	0	0	0	0	· · ·
:	12		0	0	0	0	0	0	0	0	0	4	0	15	0	5	0	0	i
	13		4	5	7	4	0	0	0	0	- 4	4	18	0	0	0	0	0	5
	14	0	0	0	0	0	0	0	0	0	0	· 0	0	0	0	0	0	0	
	15	130	0	0	230	140	0	0	0	0	0	0	0	0	0	0	0	45	54
	16	0	0	. 0	0	0	0	0	· 0	0	0	0	0	0	· 0	O	0	0	
	17	0	0	0	0	0	0	0	0	0	0	0	<u> </u>	0	0	45	0	0	
	Total	287	33	24	243	352	11	10	0	. 4	18	8	22	45	0	549	0	45	1,65
_	/ehicle							<u>-</u>											
4 <u> \</u> 0	D	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	Tot
_	D 1	0	593	374	78	1,510	13	5	1	16	180	0	0	109	0	729	0	0	3,60
_	D 1 2	0 559	593 0	374 46	78 12	1,510	13 1	5 1	1 0	16 0	180 31	0 0	0	109 92	0	729 3	0	0	3,60 77
_	D 1	0 559 334	593 0 36	374 46 0	78 12 71	1,510 26 35	13 1 1	5 1 1	1 0 0	16 0 0	180 31 27	0 0 0	0 0 0	109 92 21	0 0 0	729 3 119	0 0 0	0	3,60 77 64
_	D 1 2 3 4	0 559 334 66	593 0 36 15	374 46 0 70	78 12 71 0	1,510 26 35 19	13 1 1	5 1 1 1	1 0 0	16 0 0	180 31 27 14	0 0 0 4	0 0 0 16	109 92 21 114	0 0 0 0	729 3 119 232	0 0 0	0 0 0 0	3,60 77 64 55
_	D 1 2 3	0 559 334 66	593 0 36	374 46 0 70 29	78 12 71 0	1,510 26 35 19 1,182	13 1 1 1 60	5 1 1 33	1 0 0 5	16 0 0 0	180 31 27 14 21	0 0 0 4 1	0 0 16 2	109 92 21 114 14	0 0 0 0	729 3 119 232 911	0 0 0 0 0	0 0 0 0 0	3,60 77 64 55 3,76
_	D 1 2 3 4 5	0 559 334 66 1,454	593 0 36 15 39	374 46 0 70	78 12 71 0 15	1,510 26 35 19	13 1 1	5 1 1 1	1 0 0 5 15	16 0 0	180 31 27 14	0 0 0 4	0 0 0 16	109 92 21 114	0 0 0 0	729 3 119 232 911 0	0 0 0 0 0	0 0 0 0 0	3,60 77 64 55 3,76 22
_	D 1 2 3 4 5 6	0 559 334 66 1,454 23	593 0 36 15 39 2	374 46 0 70 29 2	78 12 71 0 15 1	1,510 26 35 19 1,182 59	13 1 1 60 0	5 1 1 33 120	1 0 0 5	16 0 0 1	180 31 27 14 21 1	0 0 4 1 0 0	0 0 16 2 1 1	109 92 21 114 14 1	0 0 0 0 0 0	729 3 119 232 911 0 0	0 0 0 0 0 0	0 0 0 0 0 0	3,60 77 64 55 3,76 22 23
_	D 1 2 3 4 5 6 7	0 559 334 66 1,454 23 7 3	593 0 36 15 39 2 2 2	374 46 0 70 29 2 2 2	78 12 71 0 15 1	1,510 26 35 19 1,182 59 31	13 1 1 60 0 137	5 1 1 33 120 0	1 0 0 5 15 49	16 0 0 1 0	180 31 27 14 21 1 1	0 0 4 1 0	0 0 16 2 1 1 0	109 92 21 114 14 1 1	0 0 0 0 0 0 0	729 3 119 232 911 0 0 0	0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0	3,60 77 64 55 3,76 22 23 7
_	D 1 2 3 4 5 6 7 8	0 559 334 66 1,454 23 7 3 16	593 0 36 15 39 2 2 2 1	374 46 0 70 29 2 2 2 1	78 12 71 0 15 1	1,510 26 35 19 1,182 59 31 0	13 1 1 60 0 137 8	5 1 1 33 120 0 61	1 0 0 5 15 49 0	16 0 0 1 0 0	180 31 27 14 21 1 1	0 0 4 1 0 0 0	0 0 16 2 1 1	109 92 21 114 14 1 1 1 0	0 0 0 0 0 0 0 0 0	729 3 119 232 911 0 0 0 1	0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0	3,60 77 64 55 3,76 22 23 7 7
_	D 1 2 3 4 5 6 7 8 9	0 559 334 66 1,454 23 7 3	593 0 36 15 39 2 2 2 1 6	374 46 0 70 29 2 2 2 1 5	78 12 71 0 15 1 1 1 0	1,510 26 35 19 1,182 59 31 0 5	13 1 1 60 0 137 8 0	5 1 1 33 120 0 61	1 0 0 5 15 49 0	16 0 0 1 0 0 0 0	180 31 27 14 21 1 1 43	0 0 4 1 0 0 0 0	0 0 16 2 1 1 0 0	109 92 21 114 14 1 1 1 0 6	0 0 0 0 0 0 0 0 0 0 0 0	729 3 119 232 911 0 0 0 1 27	0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0	3,60 77 64 55 3,76 22 23 7 7 7 34
_	D 1 2 3 4 5 6 7 8 9 10	0 559 334 66 1,454 23 7 3 16 172	593 0 36 15 39 2 2 2 1 6 26	374 46 0 70 29 2 2 2 2 1 5 27	78 12 71 0 15 1 1 1 0 18	1,510 26 35 19 1,182 59 31 0 5 21	13 1 1 60 0 137 8 0 1	5 1 1 33 120 0 61 0 1	1 0 0 5 15 49 0 0 0	16 0 0 1 0 0 0 0 44	180 31 27 14 21 1 1 1 43 0	0 0 4 1 0 0 0 0 5	0 0 16 2 1 1 0 0 0 24	109 92 21 114 14 1 1 1 0 6 32	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	729 3 119 232 911 0 0 0 1 27 1	0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0	3,60 77 64 55 3,76 22 23 7 7 7 34 8
_	D 1 2 3 4 5 6 7 8 9 10 11	0 559 334 66 1,454 23 7 3 16 172 3	593 0 36 15 39 2 2 2 1 6 26 0	374 46 0 70 29 2 2 2 1 5 27 3	78 12 71 0 15 1 1 1 0 18 7	1,510 26 35 19 1,182 59 31 0 5 21 3	13 1 1 60 0 137 8 0 1 0	5 1 1 33 120 0 61 0 1 0	1 0 0 5 15 49 0 0 0 0	16 0 0 1 0 0 0 0 44 0	180 31 27 14 21 1 1 1 43 0 7	0 0 4 1 0 0 0 5 0	0 0 16 2 1 1 0 0	109 92 21 114 14 1 1 1 0 6	0 0 0 0 0 0 0 0 0 0 0 0	729 3 119 232 911 0 0 0 1 27	0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0	3,60 77 64 55 3,76 22 23 7 7 34 8 24
_	D 1 2 3 4 5 6 7 8 9 10 11 12	0 559 334 66 1,454 23 7 3 16 172 3 0	593 0 36 15 39 2 2 2 1 6 26 0 0	374 46 0 70 29 2 2 2 2 1 5 27 3 5	78 12 71 0 15 1 1 1 0 18 7 14	1,510 26 35 19 1,182 59 31 0 5 21 3 5	13 1 1 60 0 137 8 0 137 8 0 1 0 0	5 1 1 333 120 0 61 0 1 0	1 0 0 5 15 49 0 0 0 0 0	16 0 0 1 0 0 0 0 44 0 0	180 31 27 14 21 1 1 5 43 0 7 0	0 0 4 1 0 0 0 0 5 0 28	0 0 16 2 1 1 0 0 0 24 0	109 92 21 114 14 1 1 1 0 6 32 173	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	729 3 119 232 911 0 0 0 1 27 1 24 5			3,60 77 64 55 3,76 22 23 7 7 7 34 8 24 57
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_	D 1 2 3 4 5 6 7 8 9 10 11 12 13 14	0 559 334 66 1,454 23 7 3 16 172 3 0 53 0	593 0 36 15 39 2 2 2 1 6 26 0 0 52 0	374 46 0 70 29 2 2 2 1 5 27 3 5 78 0	78 12 71 0 15 1 1 1 0 18 7 14 90 0	1,510 26 35 19 1,182 59 31 0 5 21 3 5 23 0	13 1 1 60 0 137 8 0 137 8 0 1 0 0 3 0	5 1 1 33 120 0 61 0 1 0 3 0	1 0 0 5 15 49 0 0 0 0 0 0 1 0	16 0 0 1 0 0 0 0 44 0 0 10 0	180 31 27 14 21 1 1 1 43 0 7 0 21 0	0 0 4 1 0 0 0 5 0 28 36 0	0 0 16 2 1 1 0 0 0 24 0 197 0	109 92 21 114 14 1 1 1 0 6 32 173 0 0		729 3 119 232 911 0 0 0 1 27 1 24 5 0			Tot 3,60 77 64 55 3,76 22 23 7 7 7 34 8 24 57 2,10
_	D 1 2 3 4 5 6 7 7 8 9 10 11 12 13 14 15	0 559 334 66 1,454 23 7 3 16 172 3 0 53 0 922	593 0 36 15 39 2 2 2 1 6 26 0 0 52 0 2	374 46 0 70 29 2 2 2 2 1 5 27 3 5 78 0 3	78 12 71 0 15 1 1 1 0 18 7 14 90 0 231	1,510 26 35 19 1,182 59 31 0 5 21 3 5 23 0 894	13 1 1 60 0 137 8 0 137 8 0 137 137 0 0 3 0 0	5 1 1 33 120 0 61 0 61 0 1 0 3 0 0 0	1 0 0 5 15 49 0 0 0 0 0 0 1 0 0	16 0 0 1 0 0 0 0 44 0 0 10 0 0	180 31 27 14 21 1 1 1 43 0 7 0 21 0 1	0 0 4 1 0 0 0 5 0 28 36 0 0	0 0 16 2 1 1 0 0 24 0 197 0 1	109 92 21 114 14 1 1 1 0 6 32 173 0 0 1		729 3 119 232 911 0 0 0 1 27 1 24 5 0 0		0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 45	3,60 77 64 55 3,76 22 23 7 7 7 34 8 24 57 2,10

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TABLE A.6-1 ADT COUNTS AND PROJECTIONS FOR NORMAL AND INDUCED TRAFFIC FOR 2010 AND 2020

	EXISTING			ALTERNATIVE A	TIVE A				Ą	ALTERNATIVE B	TIVE B			87. 8 . 881. 883. 8	4	ALTERNATIVE C	TIVE C		
Total Length (km)	5.4			5.4						3.7		• • • • •				5.2			
Avg. Speed (kph)	45	-		72.4						67.8						67.9			
Traffic Type.	60% of NR-13 Normal Traffic	Normal	Traffic	Induced Traffic	Traffic	Total T	fotal Traffic	Normal Traffic		Induced Traffic	Traffic	Total Traffic	raffic	Normal Traffic	Traffic	Induced Traffic	Traffic	Total Traffic	raffic
Vehicle Types/Yr.	1995	2010 2020	· · · · ·	2010 2020		2010	2020	2010	2020	2010	2020	2010		2010	2020	2010	2020	2010	2020
2/3 wheelers	1,170	1,866	3,260	261	434	434 2,127	3,694	1,866	3,260	238	396	2,104	3,656	1,866	3,260	209 209	350	1	3,610
Cars/pickups	1,007	439	785	73	118	512	803	439	785	52	118	512	903	439	785	2	7	512	
Buses	\$	3	8	ŝ	6	8	107	ß	8	S	o	g	107	ន	86	S	6	8	
Trucks	357		200 1 062	47	2	777	1,071	730:	1,007	47:	8	117	1,071	730	1,007	47	2	11	1,071
TOTAL	2,577	3,088	5.150	386	625	3.474	5,775	3,088	5,150	363	587	3,451	5,737	3,088	5,150	334	541	3,422	5,691
Source : Traffic Study, JICA Study Team	IICA Study Team							:											

TABLE A.6-2 VEHICLE KILOMETERS PER DAY VEHICLE NUMBER PROJECTED

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Alternatives	EXISTING	Α.		8				A		ŝ		U I	
Traffic type	60% of NR-13	Total Traffic	affic	Total Tr	ratfic	Total Traffic	affic	Induced Traffic	raffic	Induced Traffic	affic	Induced Traffic	affic
Vehicle type/Year	1995	2010	2020	2010	2020	2010	2020	2010	2020	2010	2020	2010	2020
2/3 wheelers	6318	11485.8	19947.6	7784.8	13527.2	10790	18772	1409.4	2343.6	880.6	1465.2	1086.8	1820
cars, pick ups	5437.8	2764.8	4876.2	1894.4	3341.1	2662.4	4695.6	394.2	637.2	270.1	436.6	379.6	613.6
puses	232.2	313.2	577.8	214.6	395.9	301.6	556.4	27	48.6	18.5	33.3	26	46.8
trucks	1927.8	4195.8	5783.4	2874.9	3962.7	4040.4	5569.2	253.8	345.6	173.9	236.8	244.4	332.8
Total	13916	18759.6	31185	12768.7	21226.9	17794.4	29593.2	4094.4	5395	3353.1	4191.9	3746.8	4833.2

TABLE A.6-3AIR EMISSIONS DATA AND CALCULATIONS OF LOADINGS
FOR 5 POLLUT 1995, 2010 AND 2020

Distance (km)	5.4	5	.4	3	7	5	2
Scenario	EXISTING	Alterna	ative . A	Altern	ative B	Alterna	ative C
Traffic Type	60% of NR-13	Total	Traffic	Total	Traffic	Total	Traffic
Vehicle Types	1995	2010	2020	2010	2020	2010	2020
2/3 wheelers	26.29	47.79	83.00	32.39	55.29	44.90	78.11
Cars pickups	2.56	1.30	2.30	0.89	1.57	1.25	2.21
Buses	0.45	0.61	1.12	0.42	0.77	0.58	1.08
Trucks	1.83	3.98	5.49	2.73	3.76	3.83	5.29
Total THC	31.13	53 68	91.91	36.43	62.39	50.56	86.69

1) Estimated total hydrocarbon (THC) emission along new road/bridge section (tonnes/vr).

2)

Air Pollution parameters	Total hydrocarbons (THC)	Carbon monexide (CO)	Oxides of Nitrogen (NOx)	Sulphur dioxide (SO2)	Total suspended particles (TSP)
Vehicle types	, · · ·		<u>.</u>		L
2/3 wheelers	\$1.4	21.4	0.14	0.648	0.08
Cars pickups	1.29	10 24	1.31	1.74	0.07
Buses	5.3	6.6	16.5	6.6	1.4
Trucks	2.6	6	11.8	4.29	0.9

3) Estimated carbon monoxide (CO) emissions along new road/bridge section (tonnes/yr)

Distance (km)	5.4	5	.4	3	7	S	2
Scenario	EXISTING	Alterna	tive . A	Alterna	ative B	Altern	ative C
Traffic	60% of NR-13	Total	Traffic	Total	Traffic	Tola	Traffic
Vehicle Types	1995	2010	2020	2010	2020	2010	2020
2/3 wheelers	49.35	89.72	155.81	60.81	105 66	84 28	146.63
Cars pickups	20.32	10.33	18.23	7.08	12.49	9.95	17.55
Buses	0.56	0.75	1.39	0.52	0.95	0.73	1.34
Trucks	4.22	9.19	1267	6.30	8.68	8 85	12.20
Total CO	74.45	109.99	188.10	74.71	127.78	103.81	177.72

4) Estimated NOx emission (tonnes/yr) along new road/bridge section

Distance (km)	5.4	5.	4	3).7	5	2
Scenario	EXISTING	Alterna	NO.A	Allem	alive B	Altern	etive C
Traffic	60% of NR-13	Total I	raffic	Total	Traffic	Total	Traffic
Vehicle Types	1995	2010	2020	2010	2020	2010	2020
2/3 wheelers	0.32	0.59	1.02	0.40	0.69	0.55	0.96
Cars pickups	2.60	1.32	2 33	0.91	1.60	1.27	2.25
Buses .	1.40	1.89	3.48	1.29	2.39	1.82	3.35
Trucks	8.30	18.07	24.91	12.38	17.07	17.40	23.99
Tolal NOx	12.62	21.87	31.74	14 98	21.74	21.04	30.55

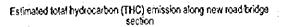
5) Estimated sulphur dioxide (SO2) emission along new road/bridge section (tohnes/yr)

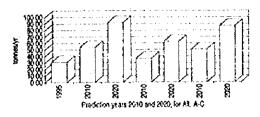
Distance (km)	5.4	5	5.4	3	7	5	52
Scenario	EXISTING	Altern	alive . A	Altern	ative 8	Altern	ative C
Traffic	60% of NR-13	Total	Traffic	Total	Traffic	Îda	Traffic
Vehicle Types	1995	2010	2020	2010	2020	2010	2020
2/3 wheelers	1.49	272	4.72	1.84	320	255	4 44
Cars'pickups	3.45	1.76	3.10	1.20	2.12	1.69	2 98
Buses	0.56	0.75	1.39	0.52	0.95	0.73	1.34
Trucks	3.02	6.57	9.06	4.50	620	6.33	8.72
Total SO2	8.52	11.80	18.27	8.06	12.47	11.30	17.48

6) Estimated total suspended particulate mater (TSP) along new road/bridge section (tonnes/yr)

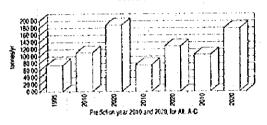
Distance (km)	5.4		5.4	3	17		2
Scenario	EXISTING	Altern	ative A	Алет	ative 8	Atem	ative C
Traffic	60% of NR-13	Total	Tratfic	Total	Traffic		Traffic
Vehicle Types	1995	2010	5050	2010	2020	2010	2020
2/3 wheelers	0.18	0.34	0.58	0.23	039	0.32	0.55
Cars pickups	0.14	0.07	0.12	0.05	0.09	0.07	0.12
Buses	0.12	0.16	0.30	0.11	020	0.15	0.28
Frucks	0.63	1.38	1.19	0.94	1.30	133	1.83
Total TSP	1.07	1.95	2.19	1.33	1.98	1.87	2.78

(Base data for 1995, is valid only for Pakse)

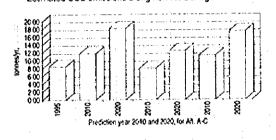


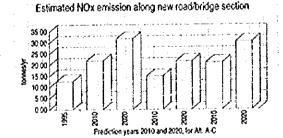


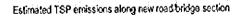
Estimated carbon monoxide (CO) emission along new road/bridge section



Estimated SO2 emissions along new road bridge section







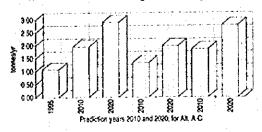


FIGURE A.6-1

ESTIMATED EMISSION LOADINGS ALONG THE PROPOSED ROUTES A, B AND C; 2010 AND 2020 (Base year: 1995, Pal)

SURFACE WATER QUALITY MEASUREMENTS, JAN. TO DEC. 1992 TABLE A.6-4

SEDON RIVER AT DAM SITE, PAKSE

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Date		Temp PH TSS	Ŧ		2000 Cond	J	X 8	9	×	4	0	ğ	. Total-Fer	スーパーのひんご	N-leiol N-rus	Total-N	Ìð	S-lens:		5	201-000
	(m3/MC)	0	-1 (e	(1/2 m)	(m,Sm)	(meau)) (č	men.l) ((mea.)	((10000)	(may.))			d'am,	(mm)		(mel)	_ Ľ	• -=	4.94
20-Jan-92		2.1	7.25	16.0	14.7	1-0354	0.233	316	2015	1.168	1	0.2761	1030	0.000	8		10101	1000			
14-Feb-92		26.6	7.371	380	13.21	0.958	0.211	1:10	1.200		Ľ	0714	1000	0,181	1946 0		000	1016	1]-
17-Mar-92		3.6	1.31	1011	13.0	0.988	1.16	16:00	1,0381	1970.3	1210	1110	14.51	ist of	6"		13	7	1.22		
17-Ap-92		<u>, 0.01</u>	į	0'1-	5.1	1111	1220	1110	2015	ก		lano -	10000	0.451	57		-8:0	1012	14.20	6-17	
12-W-21	:	1210	2	0 11	14,4	1.100	0.226	0.104	0.033	111		1277	0.000	0.017	1000		10.	10.0	14.00	181	$\left \right\rangle$
12-140-51		31.0]	8	ရ ရ	9.6	0.611	0.003	0.077	0.023	1.70	C.ONB	0.0071	a u o	0.061	1050.0	-	2.118	Ē	107 71	9	5
16-14-01				20.01	5.3	1052.0	0.111	150	0.034 (10; -10	1015	0.120	1.52.6	0.097	1001		19211	10 20	19.33	9.6-1	2
17-Aug-92		ที่	7.541 3	N-LO	6.3	0.367	5130	1013	u.031	0.4671	0.036	1170	0.200	0.0021	142011		115		- <u>8</u> -:	: .	
12-Sep-92		วิ	\$ 195.8	020	r. •	0.4161	0.137	0.046	0.018	1994-0	0.030	0.121	1000	0.101	102010	-	1720.0	L		10.621	5
10-00-51	* * * *	310	18.1	0.5	5.4	0.5891	3610	0.065	1.026	U.75	1 ITUO	0.1*11	10050	12.0	19:00		19NC	11102			
10-NOV-91		24.61	-36	13.0	:0.6	- Ser C	124	0.160	95.51	2:52	U.V.V	142.0		167010	110		: 52: 5	15:00	17.CO	9.6	. .
[6-Dec-92]		5.6	15.	0.2	11	05	0.311	0.195	202	19(1	0.019	1790	0.111	51.6	12_07	-	-1000	10.04	10,01	0.0	
																•					}

MEKONG RIVER AT PAKSE

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ŝ			к.	2	ŝ	3	Mc	e Z	×	ź	с	ğ	Total-Fei	-Neta+son interest	スーマエス	Tersi-N. POt-P	1-ros	Total-P	-	8	NIX-QOU
	(mJ.ec)	Ĉ		((aa)	(@S:@)	((((((((((((((((((((ເວັດສຸ)	(Upset)	(mea.l)	(boai	(meo l)	(@wwill)	1,120,1	(ham)	11221	i me h	(l'action	diam.	int and .	ine :	1.00
21-120-92		16.6	8.00	0.1	19.7	ing i	0.566	11.10	0.015	1.6681	5270	1035.0	110	10TO	1.00.0	-	1SDL	1200	Ģ		
15-Feb-92		10,021	3.00	16.01	111	1.23	0.507 [0.361	0.031	2	0.10	182.0	0.11	0.0521	0.028		1.51.	0.0161	9		
17-Mar-92		23.5	& I6	26.01	12.00	1.62	0.407	0.086	0.036	1.518	0.213	0.244	1170	0.0941	Ē		1000	0.0501	Ş	8111	2
17-Apr-92		32.2	8	1051	24.91	1.611	0.397	1101.0	0.016	1.395	0.226	0.558	0.651	0.062			1.160	L	0.9	3.39	
22-Wav-22		32	153	10:57	3.7	252	0.3781		0.030 {	15231	0.327)	0.520	3.101	0,074	0.639		0.018.1	L	Ā	13	S.H.
16-Jun-92		33.5	7.44	150.0	31.4	1005	0.3221	0224	0,024-1		0.485	0.2461	11:0	0.092			0.071 1	ŀ	010	19.7	
17-Jui-92		26.0	7.82	260	16.4	5.00	19220		1230.2		10.0	0.2461	0.69	0.2.0	ŀ		З с		io: v	i X	
17-Aug-92		- 26,4	1.80	39.0	14.3	0.622	1020		0.045	8	1110	125.0	0.51	0.236	·	-	0.000	128)6	ē		
16-Sep-92		ž	12	<u>a</u> S	1	0.981	0.245	1210	0.046	10001	12120	0.211	0.67	0.12	0.021		10101	0.031	Ŕ	- 10 10	
17-00-92		26.4	101	:760	14.9	1.012	0.253	0.125.1	0:0201	1.0.1	0.302	0.2361	1 89.53	2.169	1.050.1	-	0.053	1001	i and	1 5 5 1	;
16-Nov-92		10.02	7.851	0.505	16.8	1,2251	0.348.	0.1844		112211	9.161.0	0.2551	0.541	26.70	0.000	-	0.0361	1000	ę.	- 9 <u>-</u> 0	
17-Dec-92		1.1	2	60.01	21.7	1.331	0.451	0.332 /	1783	1-619	1920	0,235.0	t T	1. C2	12210		1919 V		ě	0.11	
																					4

Source: Lower Mekong Hydrological Yearbook, 1992. Mekong Commission, Vientiane. Lao PDR.

TABLE A.6-5RESULTS OF SURVEY ON THE RELATIONSHIP BETWEEN ANNUAL EARNINGS
OF LOCAL STORES AND THE CAR FERRY TRAFFIC IN PAKSE (1/2)

							·		r	AL	r	[
									% of	% 01	Imaged	
i			No.	Dist.	Annual	No.	Women	No.	earnings	earnings	Impact	· · ·
Survey		Bus.		from Ferry	Earnings (People	Owner	woment	Irom	from	of Ferry	Comment-on what sold
No.	Survey Date	Туре		Dock (m)	Kol	Employed	(1=yes,	working	Ferry	long-	closing	
	1	~	Dosness	DOCK (m)	יעיי	Cubiolog	2=no)	full-time	Traffic	boat	(1-4)	
: 1	1								i	Traffic		
	18/11/95	2	3	300	7,000,000	1	1	1	20	50	2	fertilizer, beer
	18/11/95	2	5	310	3,000,000	1	1	1	40	20	2	pharmaceutica!s
2 4	18/11/95	2		315	2,000,000	1	1	1	30	20	2	cakes, plastic bags
			3	300	16,000,000		1	1	10	10	1	gold/silver
5	18/11/95	2	15	280	3,000,000	2		2	20	25	1	ceremonial mat, candles
6	18/11/95	2		270	4,000,000	1			25	25	2	ceremonial mat., candles
7	18/11/95	2	10		200,000				10	10	1	bedding items/material
8	18/11/95	2	0.1	60				╞╌╤╌╬╌┈╧╵	1	2		gold/silver, jeweiry
9	18/11/95	6	0.5	265	250,000	· · · · · · · · · · · · · · · · · · ·			20	20		gold/silver, jeweiry
10	18/11/95	6	3	260	20,000,000]]			20	30		bedding, cooking ware
11	18/11/95	2	10	265	2,000,000	1	1	<u>}</u>	50			
12	18/11/95	3	10	260	3,000,000	2	1	<u> </u>	6	7	ļ	ceremonial mat, candles
13	18/11/95	2	0.4	255	400,000	1	1	1	8	10	1	ceremonial mat., candles
14	18/11/95	1	1	250	400,000	1	1	1	60	30	1	tobacco, cigs ,sugar
15	18/11/95		7	245	24,000,000	2	1	1.1	20	18	2	pharmaceutica!s
	18/11/95	22	25	240	2,000,000	2	1	2	10	15	1	general store
16		6	10	235	38,000,000		1	1	10	10	1	bicycles and parts
17	18/11/95				3,000,000			2	10	12	1	small gnd. store
18	18/11/95	2	5	230	20,000,000		<u> </u>	2	10	10	1-1	insecticide, fertil., sugar
19	18/11/95	2	10	225	20,000,000			2	12	10		salt, candle wax
20	18/11/95	2	16	220		2		<u></u>	10	12	2	pharmaceuticals
21	18/11/95	2	7	215	22,500,000		<u></u>			30	3	polatoes, soft drinks
22	18/11/95	2	8	210	300,000		<u> </u>	<u> </u>	30			
23	18/11/95	2	12	210	22,500,000	2	1 1	1	30	30	2	pharmaceuticals
24	18/11/95	2	6	205	10,950,000	2	1	1	20	20	2	pharmaceuticals
25	18/11/95	2	13	200	2,500,000	2	1	2	2	3	1	cookware
26	18/11/95	2	5	195	3,500,000		1 1	1	30	30	2	foodstuffs, produce
		2	0.4	190	100,000	1	101	1	35	30	2	foodstuffls
27	18/11/95		20	185	3,000,000		i	2	34	30	2	small gnrl. store
28	18/11/95	2			50,000		1	2	2		1	tailor, cloth, clothing
29	18/11/95	4	0.1	170	300,000	2		1	20	25	1.1	bread, sandwitches
- 30	18/11/95	<u> 1</u>	2	160					25	25		beer, soft drinks
31	18/11/95	1	5	140	5,000,000	2	1		20		· · · · · · · · · · · · · · · · · · ·	food, drinks
32	18/11/95	3	0.8	110	2,000,000	2	1	2	5	32		bananas (boiled)
33	18/11/95	3	5	115	3,000,000		11_	2	3	15	+ +	
34	18/11/95	3	1	120	3,600,000		1	3	10			noodles,bread
35	18/11/95	3	2	130	2,500,000		1	1	5	3	· · · · · · · · · · · · · · · · · · ·	noodies,bread
36	18/11/95	1	T T	140	3,000,000) 1	1	1	1	2	1	fruit, soft drinks
37	18/11/95	2	6	140		10	1	5 2 2 2	4	5	1	fuil meals (rest.)
38	18/11/95	2	5	150	15,000,000		1	2	0	0	1	Rice
	18/11/95	2	7	152	16,000,000		1	2	0	0	1	Rice
39				153	13,000,000	2	1	2	0	0	1	Rice, Papaya
40	18/11/95	2	2		1,000,000		+	• • • · · · · · · · · · · · · · · · · ·			1	tailor, clothing
41	18/11/95	4	2	153	1,00,00	$\frac{2}{3}$	+	2	2	1	1-1-1-	laylor, clothing
42	18/11/95	4	0.5	155	42,000			1	20	25		gort. store
43	18/11/95	2	2	160	5,822,220		1		10	15		detergent, soap
44	18/11/95	2		165	18,000,000) 2	1			5	- -	bike parts, constructin, mat.
45	18/11/95	6	11	170	32,000,000) 3	1	1	10 5			gnri. store, detergent, so
46	18/11/95	2	5	175	2,000,000	2	1	1	<u> </u>	5 5 2 25		grin, store, detergent, so
47		2	15	310	16,000,000		1	1	10	5	_	pharmaceuticals
48	18/11/95		7	300	18,000,00	3	1	3	5	5	<u> 1</u>	foodstuffs, soup
49	18/11/95		5	275	6,000,00	0 3	1 1	2	3	2	1	gori, store, rice sacks
			5	270	9,022,22	2 2	1	1	20	25	1	ceremonial items
50	18/11/95	- <u> </u> - <u>-</u>			3,000,00	0 3	+ i	3	20	15	1	ceremonial items
51	18/11/95		3	265	3,000,00				2	5	· • • • • •	clothing
52	18/11/95	4	1	260	6,000,00					2		fishing supplies
53	18/11/95	6	10	255	11,000,00		1	1				
54	18/11/95	2 2	10	250	14,000,00		1	1	10	5		foodstuffs
55	18/11/95	2	3	240	5,000,00	0 1	1.1	1 1	10			salt, buckels
1 33	18/11/95	2	15	235	7,000,00	0 3	1	2	20	10		cooking equip., bedding
22 - 22				-1	210,000,00	ñ	1	1 1	10	10	1 1	jeweiny (gold/silver)
56	19/11/05	- A	3	Z3U	1510,000,00	V				والاستنقار بمريدتها والرار	سيشيد مندر الم	
56	18/11/95	6	<u></u>	230	8,000.00	ŏ 2	1-1-	2	30	12	1	foodstuffs, soap
56	18/11/95 18/11/95	2	8	230	8,000,00	0 2		23	30 2 10	12 1		

TABLE A.6-5RESULTS OF SURVEY ON THE RELATIONSHIP BETWEEN ANNUAL EARNINGS
OF LOCAL STORES AND THE CAR FERRY TRAFFIC IN PAKSE (2/2)

61		Туре	Yrs. In Business		κοj	Employed	Owner (1=yes, 2=no)	No. woment working full-time	earnings from Ferny Traffic	long- boat Traffic	Impact of Ferry closing (1-4)	Comment-on what sold
	18/11/95	3	22	228	3,000,000	2 3	1	2	5	8	1	colfee, ovaitine
62	20/11/95	2	1	345	18,250,000	3	1	2	10	12	1	pharmaceuticals
63	20/11/95	4	17	285	25,500,000	1	. 1	1	10	10	1	clothing, buttons
64	20/11/95	2	15	350	10,950,000	2 2	1	1	3 7	3	1	pharmaceuticals
65	20/11/95	4	2	290	2,190,000		1	<u> </u>	7	5	1	clothing, buttons
66	20/11/95	4	10	295	7,300,000	2	1 .	<u><u></u><u></u></u>	8	8	1.	clothing
67	20/11/95	6	10	300	62,050,000	2	1	1	5	3		jewelry
68	20/11/95	6	17	305	127,700,000	2	1	2	7	5	2	jewelry
69	20/11/95	. 4	6	295	1,825,000	2	1	1	7	7		ciothing
70	20/11/95	6	4	280	109,500,000	3 5	1	1	10	10		constrctn. materials
71	20/11/95	3	2	270	25,550,000		1	3	0	0	1	complete meals
72	20/11/95	6	5	240	2,555,000	2	1	2	10	8	<u> </u>	shovels, hoes, picks, elect
73	20/11/95	2		230	10,000,000		1	1	12	15	1	gari. toodstutts
74	20/11/95	1	10	225	3,560,000	2		2	<u> </u>	8	1	coconut, chicken
75	20/11/95	1	3	220	2,190,000		1	1	5	28		noodies, soft drinks
76	20/11/95	1	1	215	91,550,000	1	1		5	10	1	chicken, duck
77	20/11/95	1	2	210	7,300,000	2	1	2	2	15	1	alcohol, water
78	20/11/95	1	6	205	9,125,000	1	1	1	5	20	2	soft drinks, chicken
79	20/11/95	1	0.8	200	2,550,000	1	1	1	2	30	1	soup, noodles
80	20/11/95	1	3	180	2,190,000	1	1		2	40		soft drinks, tea
81	20/11/95	1	3	175	2,190,000	1	1	1	1	50		soft drinks, coffee
82	20/11/95		1	170	1,900,000	1	1	1	1	40		
83	20/11/95	1	1	165	3,285,000		1	1	1	30		solt drinks, colfee
84	20/11/95	1	3	160	8,395,000	1			8	10	1	solt drinks, tea
85	20/11/95	1	4	150	1,825,000	1	1	·	2	50		solt drinks, collee
86	20/11/95	1	1	140	1,277,500		<u></u>	<u> </u>	1	40	1	soft drinks, coffee
87	20/11/95	1	0.3	130	2,190,000	2	1	2	2 1	40	1	soft drinks, alcohol
88	20/11/95	1	<u>`2</u>	125	2,555,000	1	<u> </u>			<u> </u>		bread, soft drinks
89	20/11/95	<u>]</u>	2	115	1,277,500		1		2	40		soft drinks
90	20/11/95	<u> </u>	- 1	110	1,825,000	<u>]</u>]	2	38	2	papaya, alcohol
91	20/11/95		0.6	100	1,095,000		<u>1</u>	···· } !	3	40	· · · · · · · · · · · · · · · · · · ·	soft drinks, alcohol
92	20/11/95		2	90	2,555,000		····	1	2	35		soft drink, tea
93	20/11/95		1	60	2,500,000				3	50		solt drinks, collee
94	20/11/95	1	0.1	40	1,460,000	2		2	20	20		solt drinks, collee
95	20/11/95		3	30	3,650,000		1	1	30	20		solt drinks, collea
96	20/11/95	6	3	2.5	4,015,000	·····			50 20	15	3	soft drinks, collee
97 98	20/11/95		1		59,568,000	<u>-</u>	1		<u>40</u>	20	2	auto fuel
	20/11/95	1		1.5	3,650,000	2		2		2	3	soft drinks, orange juice
99	20/11/95	3	4	10	7,300,000	3	1	2	60 100	5		potable water, cake
100	20/11/95 20/11/95	- <u>1</u> -	1	0	2,190,000 2,920,000				100	0		solt drinks, collee
101	20/11/95		2	0	3,650,000				100	0		soup, noodles
102	20/11/95	···· <u>1</u> ···	3	100	2,555,000	4				<u> </u>	4	solt drink, collee
103	20/11/95	3	15	100	2,000,000	2		÷	2			soft drinks, cake
104	20/11/95	6	13	30	3,050,000	2		2	10		2	papaya, cake constrct. mat., steel

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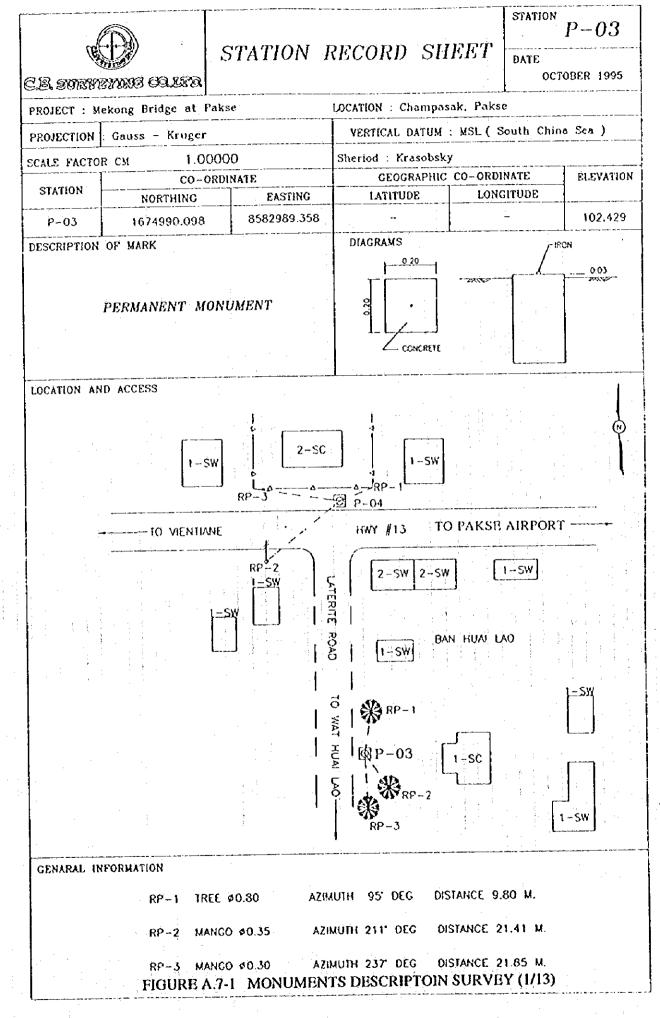
TABLE A.6-6 COMPARISON MATRIX FOR ALIGNMENTS OF ALTERNATIVES A, B AND C FROM ASSESMENT OF EXISTING CONDITIONS AT PASE, YEAR: 1995

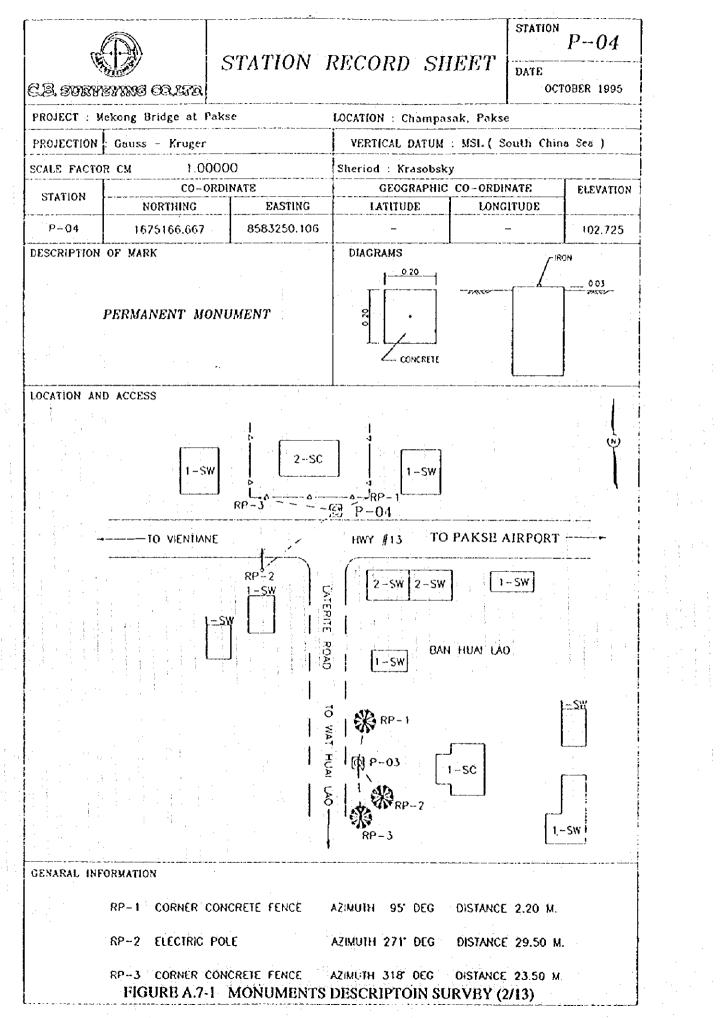
Evwonnentel Conponent	Sensitivity Weighting (1-10)	Indicator	Indicator description	Units data collected	Scale conversion retriionship (1-10)	Atomative A	¥ .	Attemative B	20 8	Attemative C	v.	Weigh	Weighted Value		Scalar Averages	16. 16.
					1=minimat (least) 10—extreme(wors)	Actual Actual	Weighted Scalar Value	Actual	Weighted Scaler Value	K Actual V	Vloighted Scalar Value	¥.16	010 018 018	¥ 114	8.11	n c
BOPHYSICAL EW.				TOMMENYI		-					-					
7	s	•	Emission basengs for 5 politizaria in tomoscyr	THC	Ct=1 - 1001=10	91.9	9	62.4	624	86.7	8.5			ິ	8.90 5.	5.96 8.31
		2	erro.	00	0t=1 - 200t=10	188.1	8.4	8°121	6.4 [177.7	8.9	•				
		E I		NOK	01=1 - 501=10	31.7	7.4	21.7	- 4.3	30.5	6.1			-		
		4		S02	01=1 - 201=10	18.25	9.1	12.5	625	17.5	8.75	-				
		5		150	01=1 - 31=10	2.9	3.6	2	66	. 2.8	6.9	44.50	29.79 4	155	 .	
	• • •	ي م	eensine features (temples, schools and homes) within 200m wide zone endoed to noise environment which is at least 20 GBA above the background invel(considenty, ventaley, end.)	No. temples, achoold, thospitalis, houses	đa1, >200 a 10.	8	87	22	80	5	25	10.8 9	4 8 .6		87 67	8.1
Water Resources	2	2	brasence of a sensitive water resources feature	Scale	1=none to 10=extreme	-	1	55	2	Ŧ	¥				2.5	6.5
		6			1-none to 10-extreme	*			•	4	Ī	115	45.5	R		-
C. Lotter Dataset		•		herd	AV	4	42	24		151	ľ	ŀ		ŀ	5	74
		», S				<u></u>		52		1 - 1 -						
		2				2	3	5	,	²		Ĭ	-	-	+-	
Terrethel Resources	3	۴	number of economicately important treephant species (mature) removed in 40-m wide ROW (6 species to consider)	No. of trees	0 trees=1 - 20 trees =10	0	1 t	15	7.5	<u>,</u>	8	:			- -	27
		12	encroachment on whittle habitat	Scale	On none to 10-extreme		2	8	3	4	4	e	15.73	ġ.		
Mergation / Compensation	\$	ت	cost of biophysical environmental impact mitigation	Ouncone to 10-extremety high	O-none to 10-extremely high	3	4					4	26	2	R	
HUMANBUET ENV.						•								-	_	
Settloment	5	*	no. Overlarge to be taken within 40-m wide ROW	No units	0 stret, #1 = 60stret.e10	4	23	36	63	51	8.5	17.93	60.7	87.67	1.79 6.	6.07 8.77
		15	e ROW	â	0 Set - 6000Se10	35000	1.5	235000	3.9	529000	3.8				_	
		16		No.Unis	0-stret.=1-200strut.=10	8	9 7	160		180	8		-			
	19 19 1	41		m2	0 m2#1 - 150K m2#10	101000	6.7	000/		146000	9.7	3	37.72	202	6.75	4.72 8.78
		8		Ŷ	0 m2#1 + 280K m2=10	214000	2.6	215000	1	21300	7.6			-		
		5 5	X	Ŷ	05=1-75045=10	000,05	6.7	10000	4	20002	8	:				
	. N	8	extent of access restriction (lost road knks)	scale	O-none-10-extreme	8	Ş .		2	3	\$			_		-
Socioeconomic	6.		extent of interference with peoplets invelthood	scale	Omone to 10-extreme		5	8	8	0	5	49.5	<u>ଷ</u> ,ମ୍ବ	ह्य	5.5	7.75 4.25
		8	change in existing landscape	Scale	O-none to 10-extreme	1 7	7	8	5	4						
		8	Extent of visual intrusion of approach roads	Scale	Ownore to 10wextreme	<u>۲</u>	7	4	7	n	3				··	
		8	restriction to blanned orderity urban growth and development	Scale	Ownone to 10-extreme	8	. 63		80	-4	*					
CHITICAL DEVELOPMENT RESTRICTIONS	j j o	8	iõese kocal Planning actions (e.g., anport ruimejns) which serkously innoede skonneiti alternative	Scala	On no impedence, 10n critical impedence	6	6)		4	2	2	ŝ				
Of IDI IN PARCE H TATION	:. c			Scale	most fav.=1 keast destrokkew10	a	0	9	9				3	3		
NOTION CONSULT ALLON	,	ę								5	ř	5	5			, -

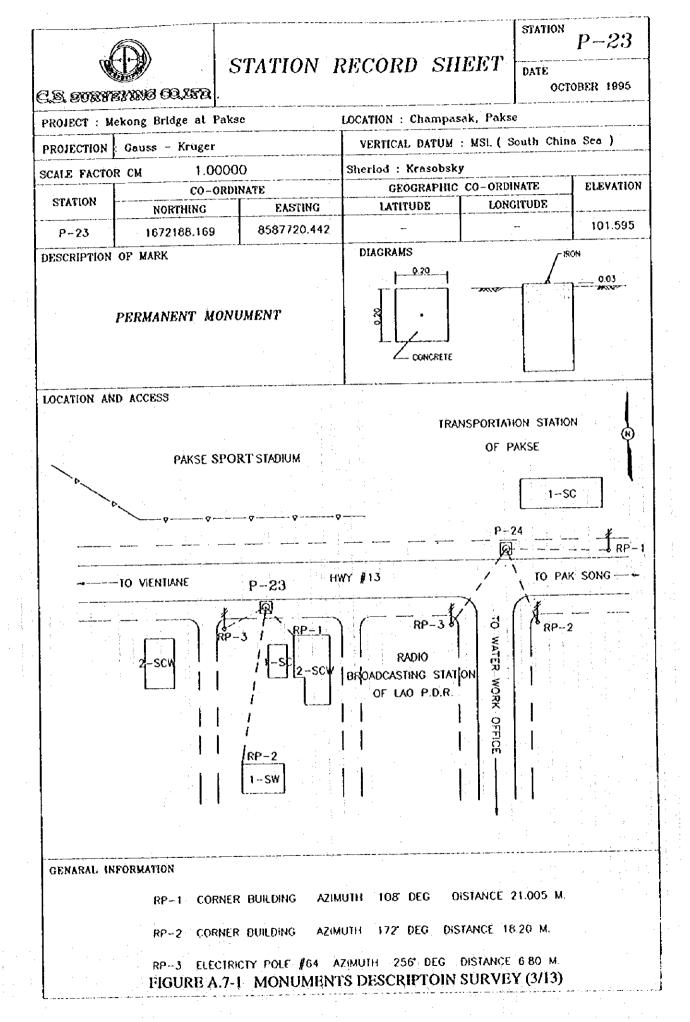
TABLE A.6-7

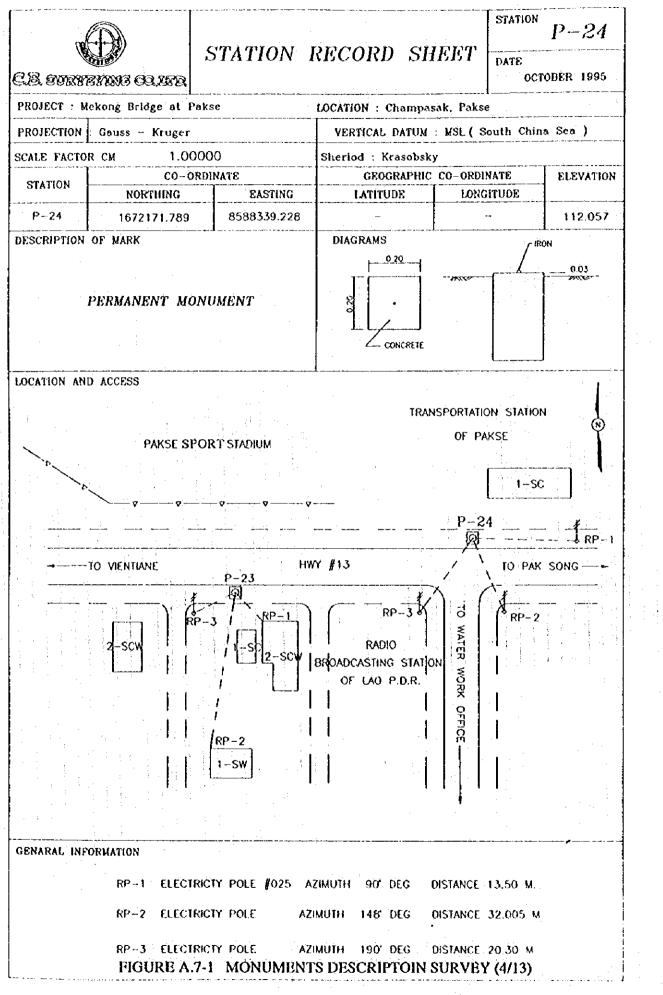
SUMMARY OF PROPERTY AFFECTED BY THE APPROACH ROADS OF THE PROPOSED BRIDGES ROUTES

		BRI	BRIDGE ALTER	RNATIVE A	S A	BRI	IDGE ALT	BRIDGE ALTERNATIVE B	E B	BRII	BRIDGE ALTERNATIVE C	TRNATIV	ы С
Iter	Item Description	E-40A	E-200A	W-40A	W-200A	E-40B	E-200B	W-40B	W-200B	E-40C	E-200C	W40C	W-200C
Bldgs.	1-SW	2	2	10	30	18	58	18	97	26	58	12	17
	1-SWC	0 1	0	0 : :	0			0	o	Ô	m		
	2-SW	0	0	2	3	0	2	13	\$	ō			4
	2-SWC	0	1	0	0		2	2	12	I	6		
	1-SC	0	0	0	0	0	2	2	S				
	2-SC	0	0	0	0	0	1	Ó	0	4	6	°	
	3-SC	0	0	0	0	0	0	Ċ	0			0	
	Other Bldgs.	0	0	ō	ō		80	0	2	ō	L J	0	
	Relig Sites : Wats	none	none	none	DODE	none	Wat Pan	none	Wat Kang	none	none	none	Wat Kang
							Sawan		Yang				Yang
Water	Deep Wells	0	0	0	0	0	0	0	0	4	4	0	-
Roads	Intersections	0	0	9		2	2	0	1	9	8	0	
Agricult	Rice Fields (m2)	21000	94000	80000	120200	16000	80000	54000	135000	92000	138000	54000	135000
Trees	Tamarind (No.)	0	0	0	0		2	Ō	3	6	9		
	Teak	J	0	0	0	10	25	0	0	0	0	0	
	Mango	0	0	0	0	0	0	ŝ	20	9	12	сл	20
	Palm	0 1	0	0	0	0	0	-					
Special	Features	high antenna	high antenna	none	none	none	none	none	Kang Yang School	Saman Sai School	none	поле	Kang Yang
and the second second										! -		:	School
					•••••								
													- 1



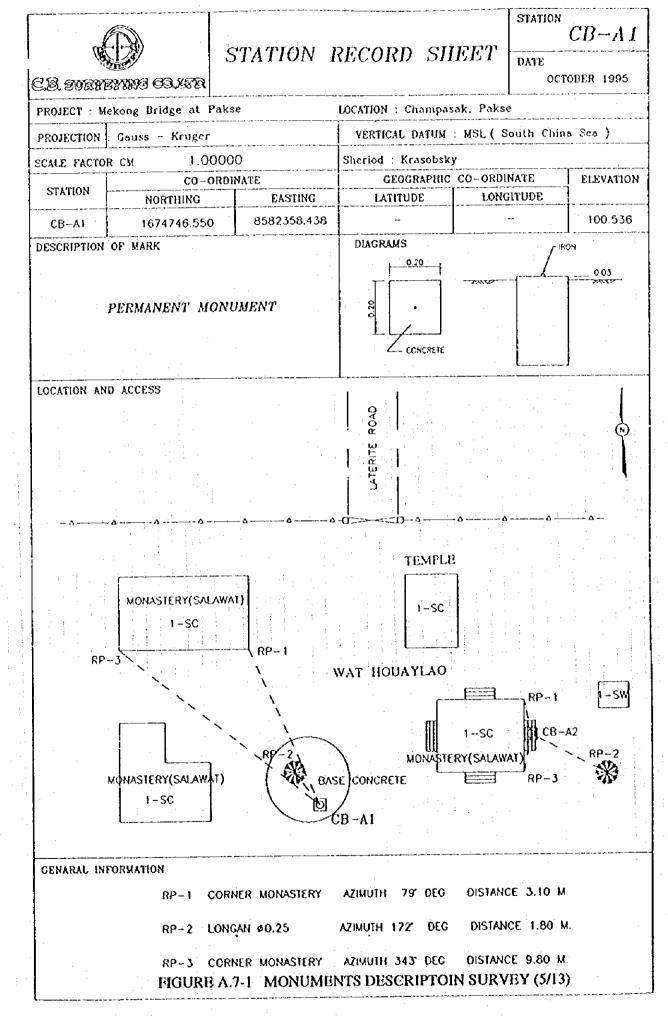




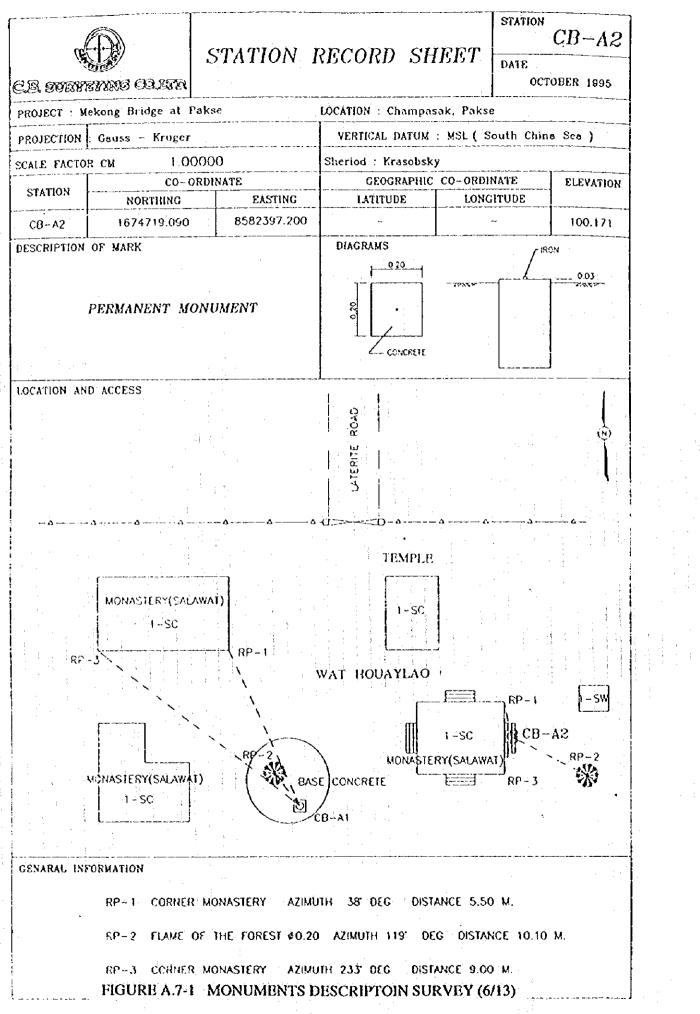


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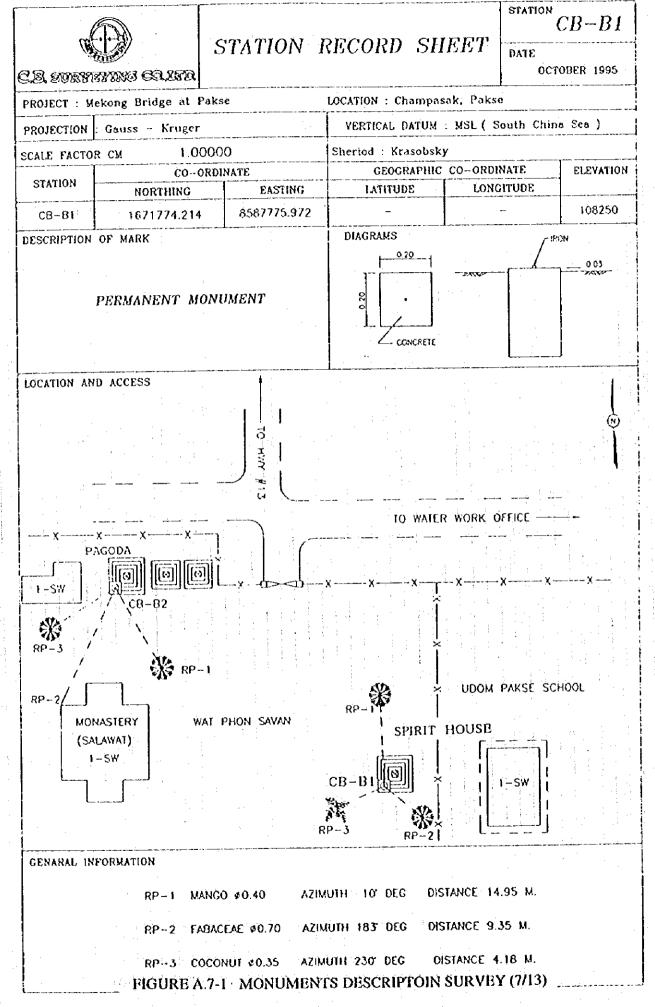
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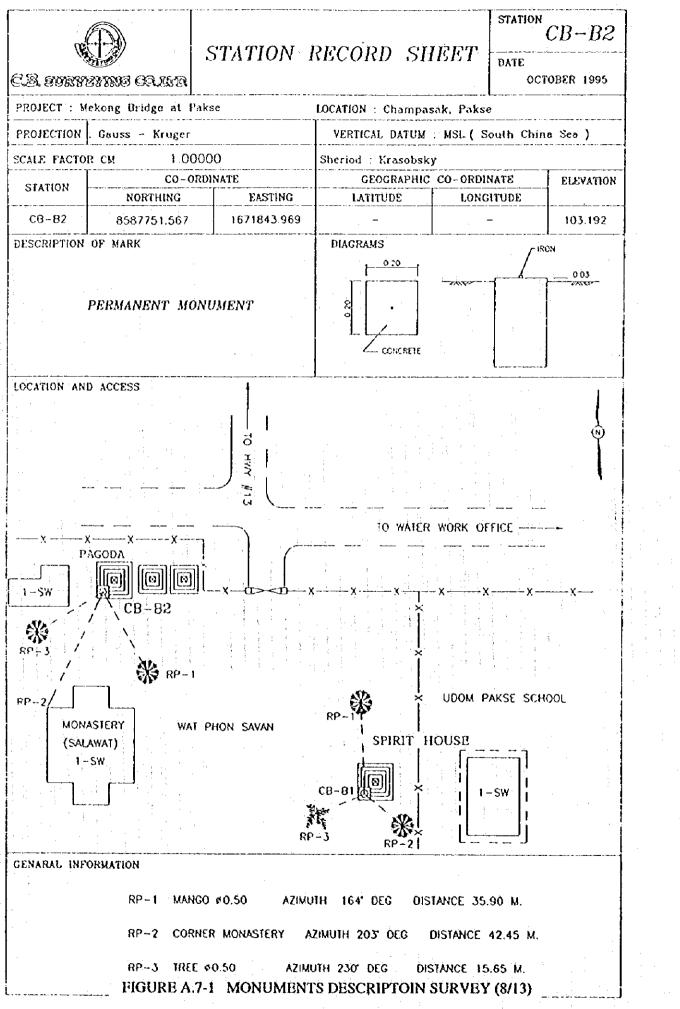


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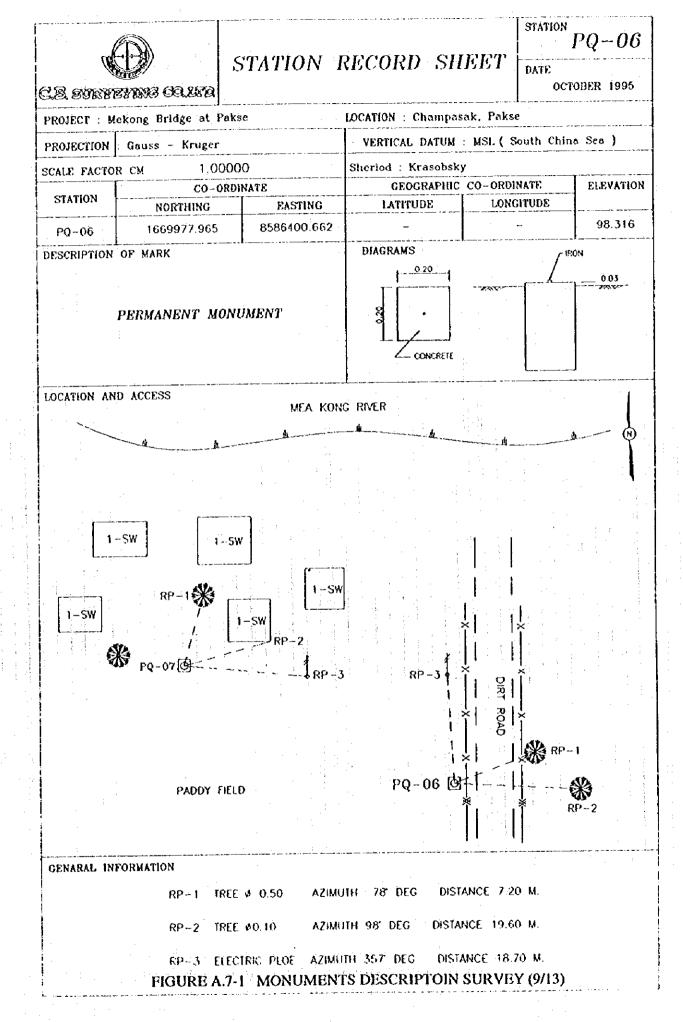
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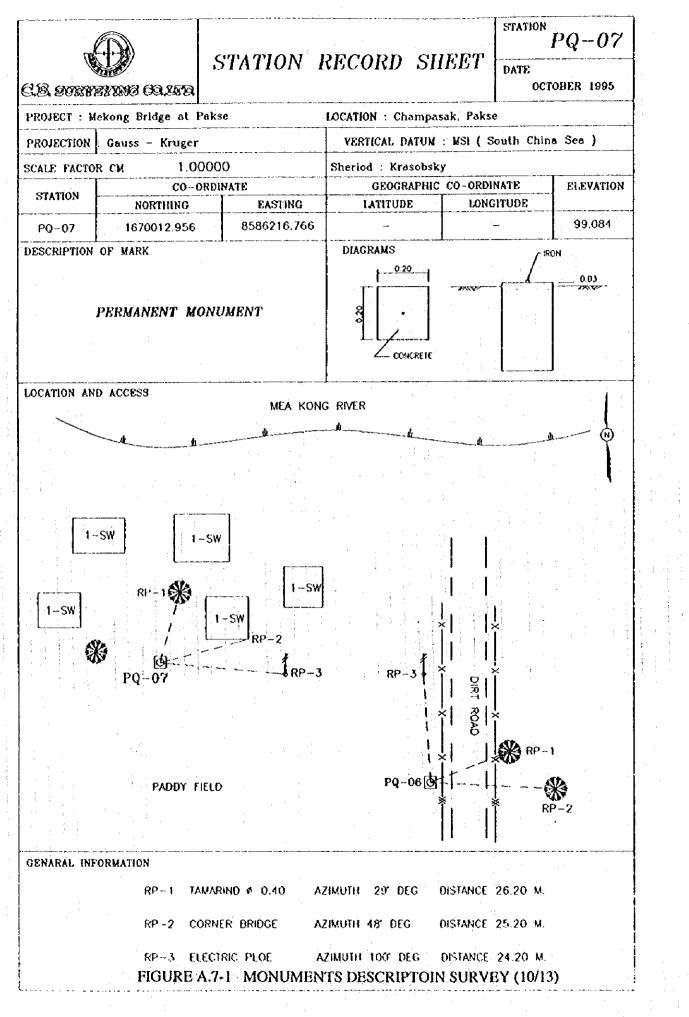


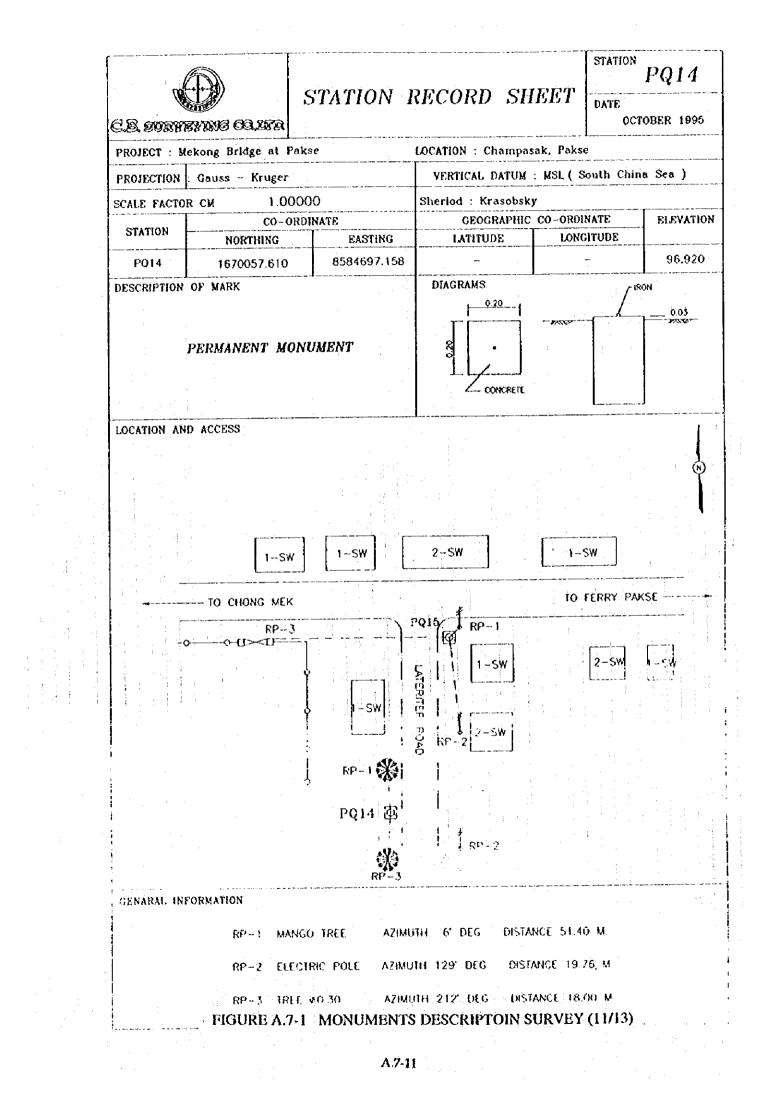


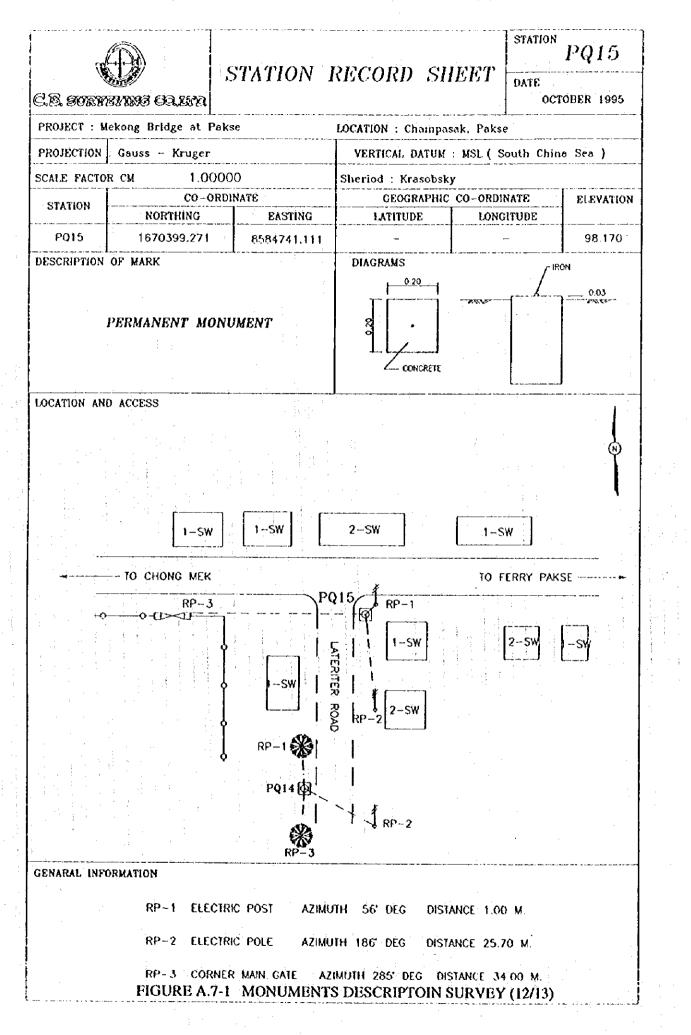
A.7.8

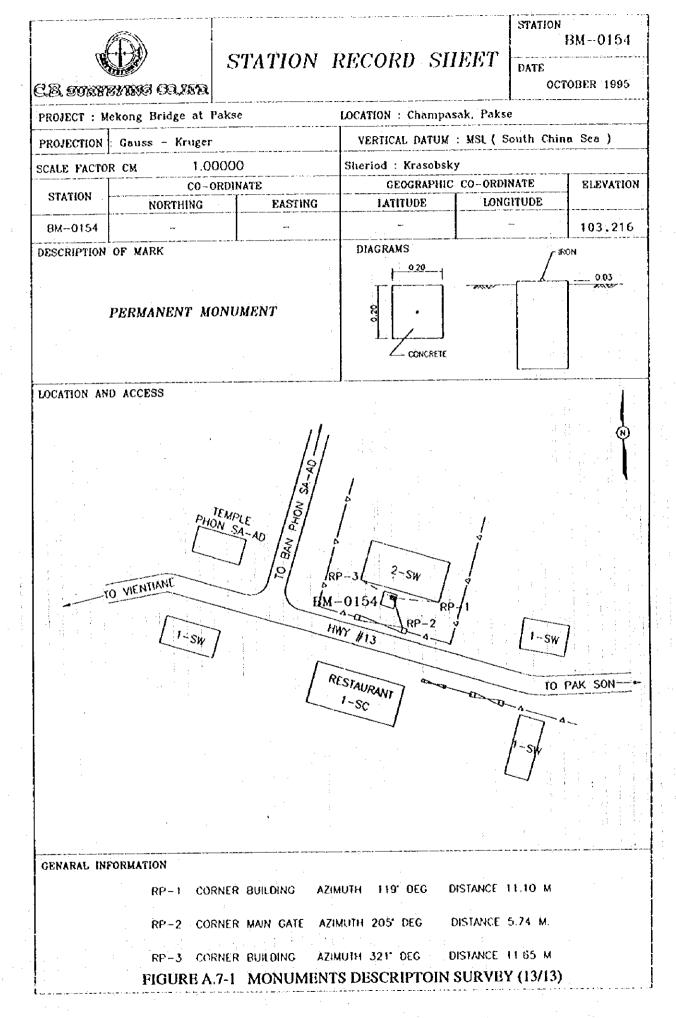
. .

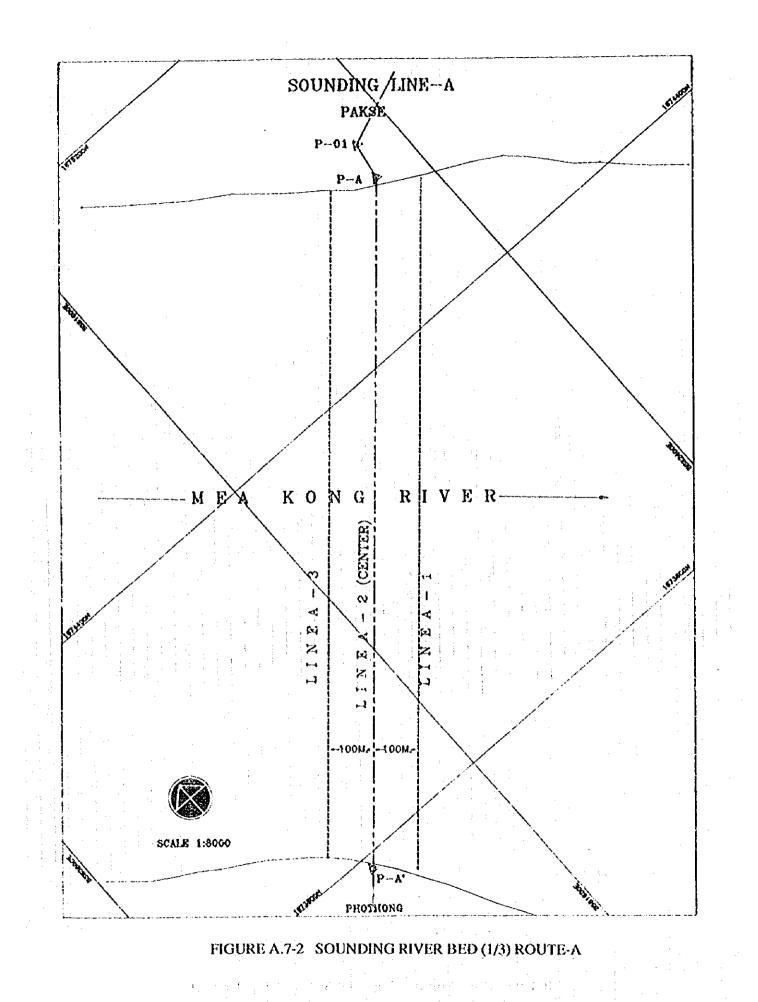












A 7-14

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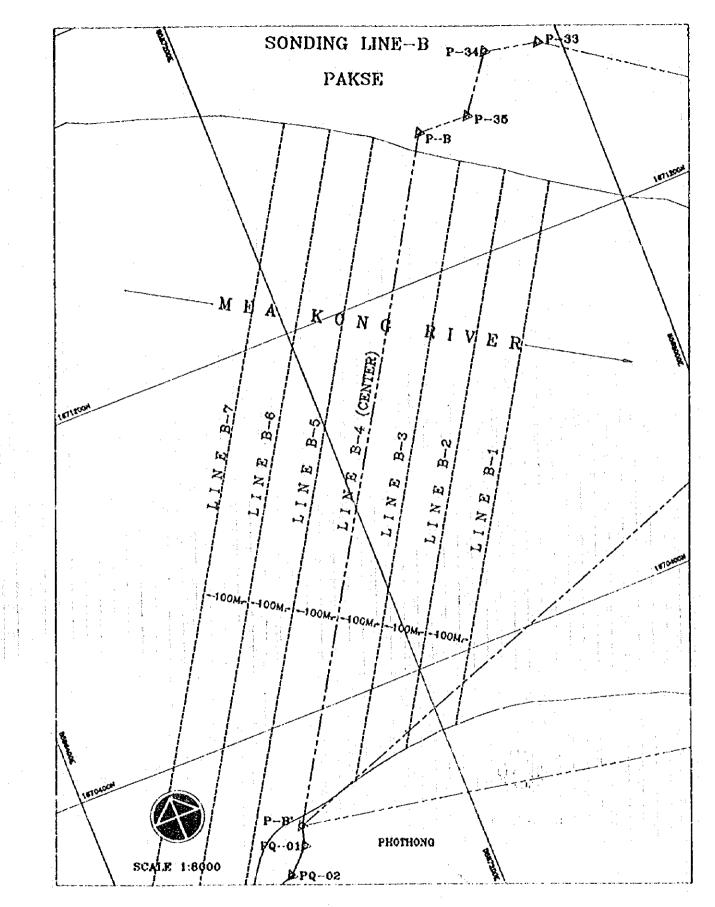
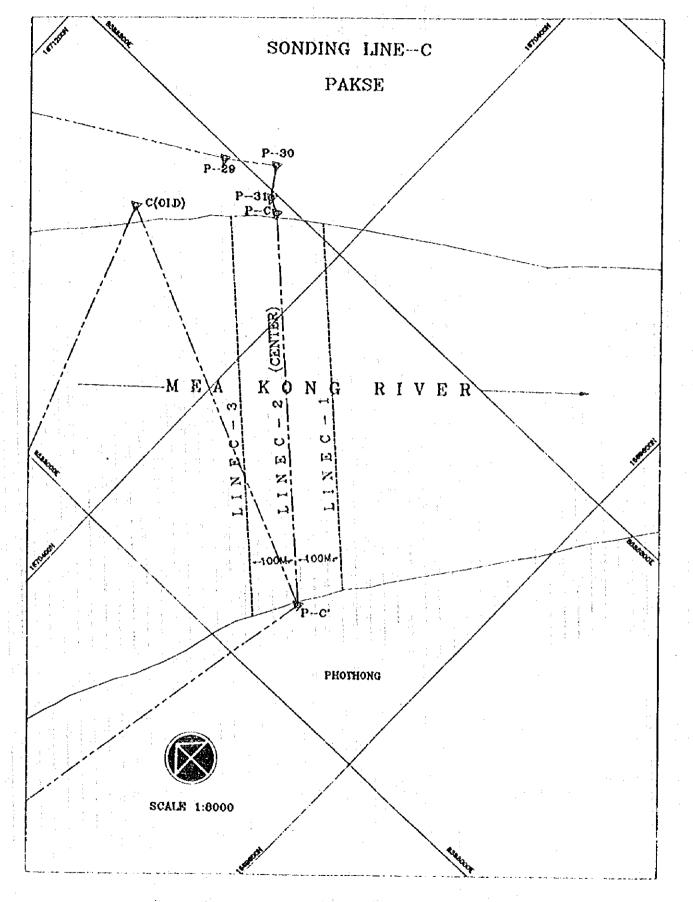
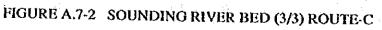
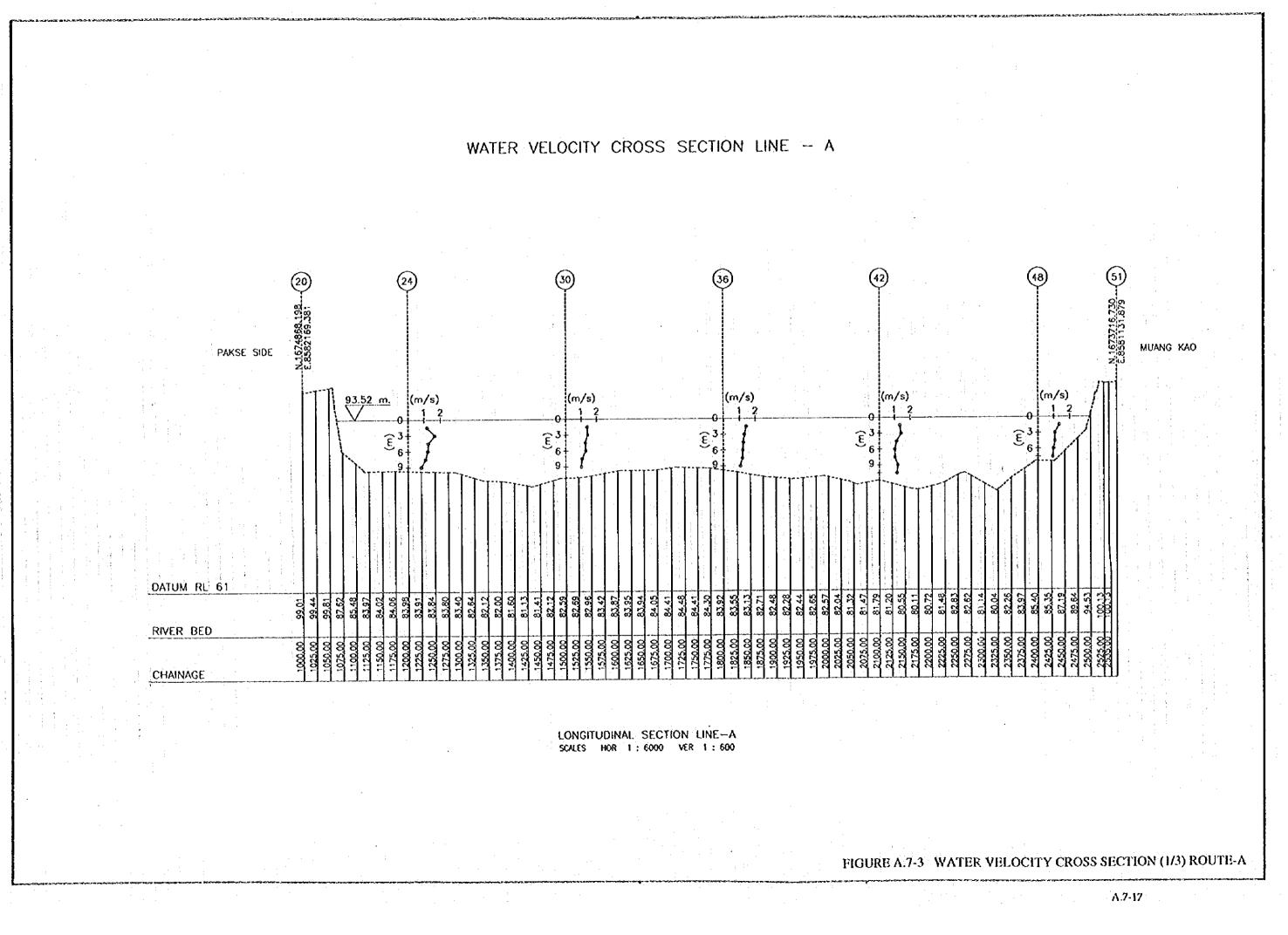


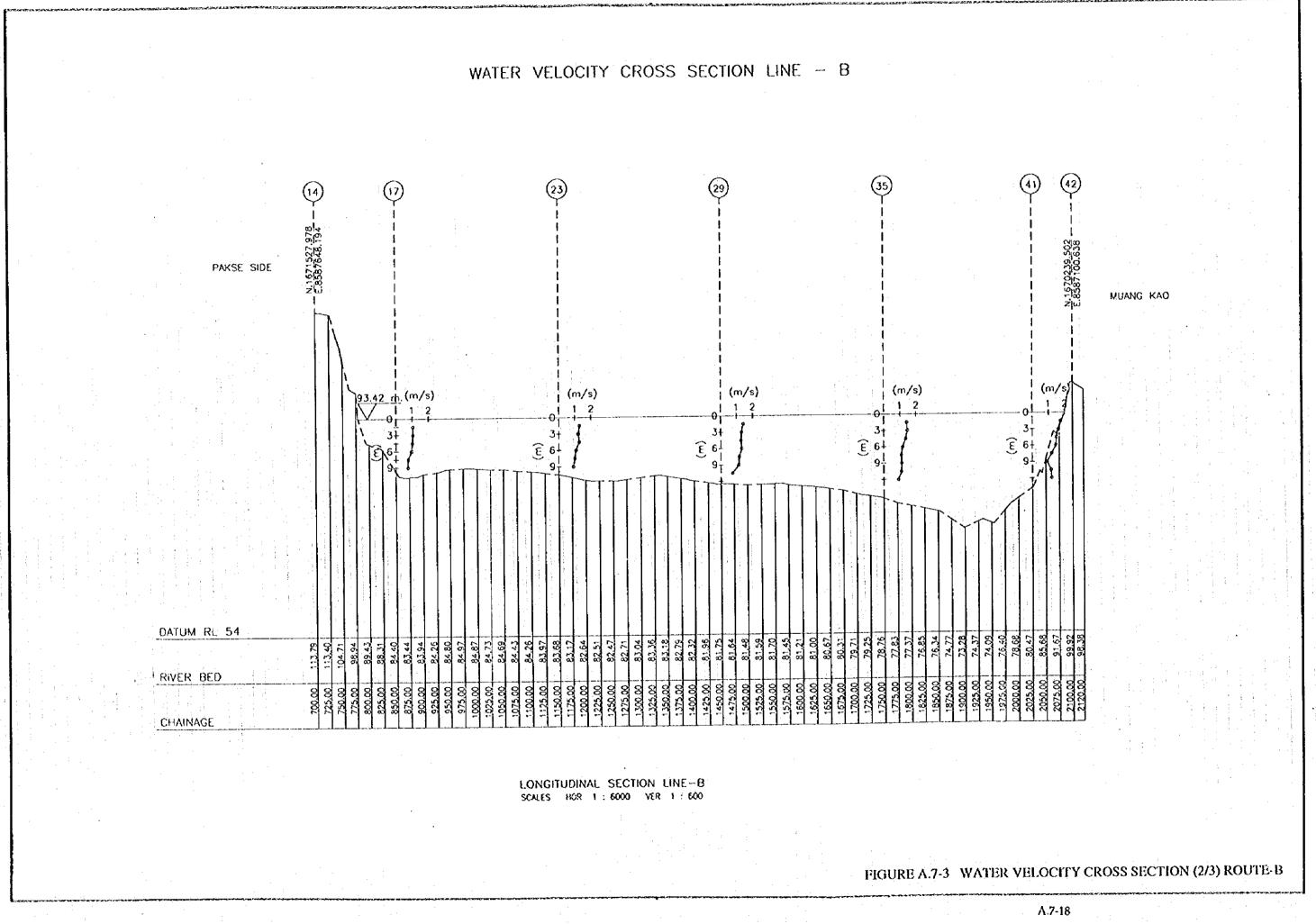
FIGURE A.7-2 SOUNDING RIVER BED (2/3) ROUTE-B

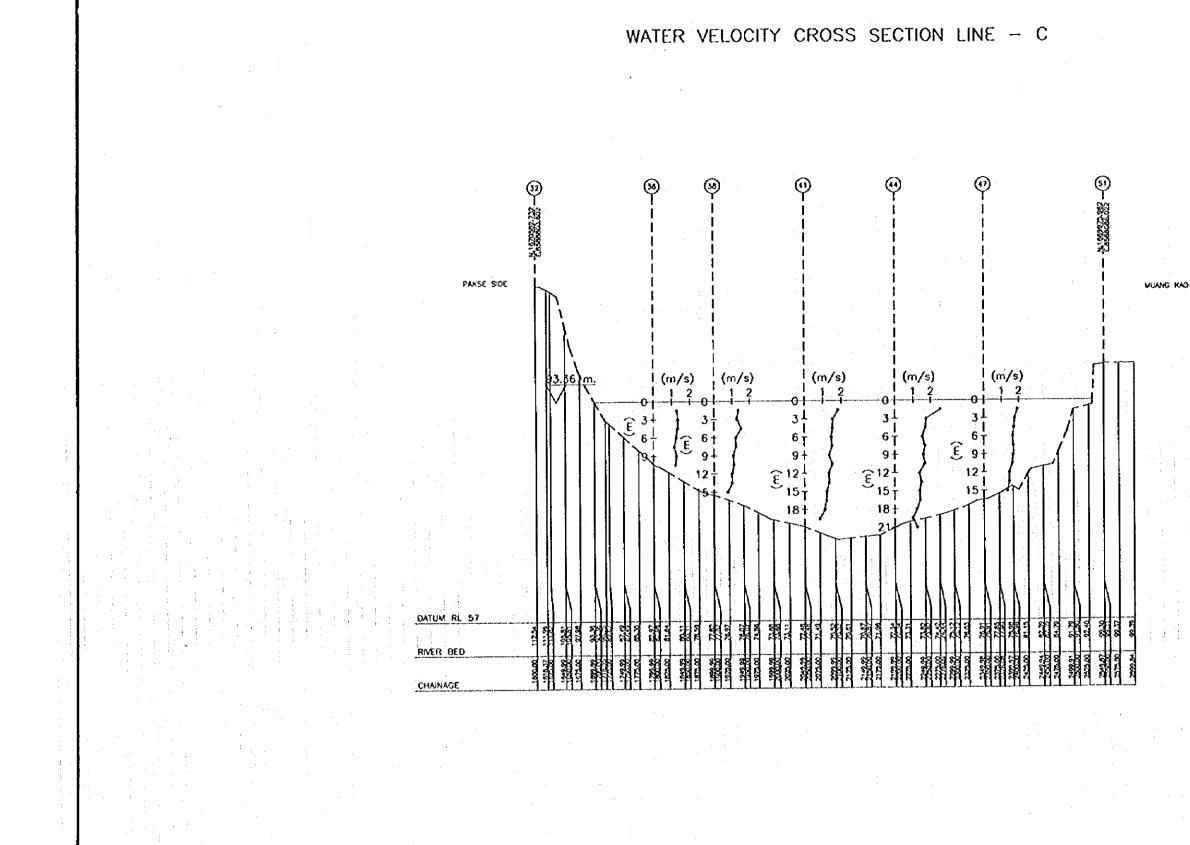




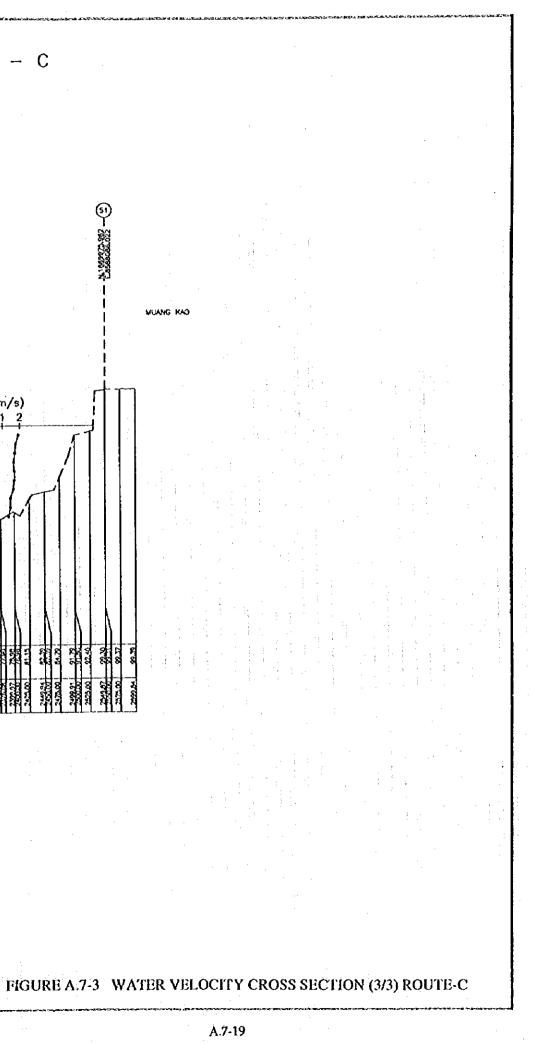
A.7

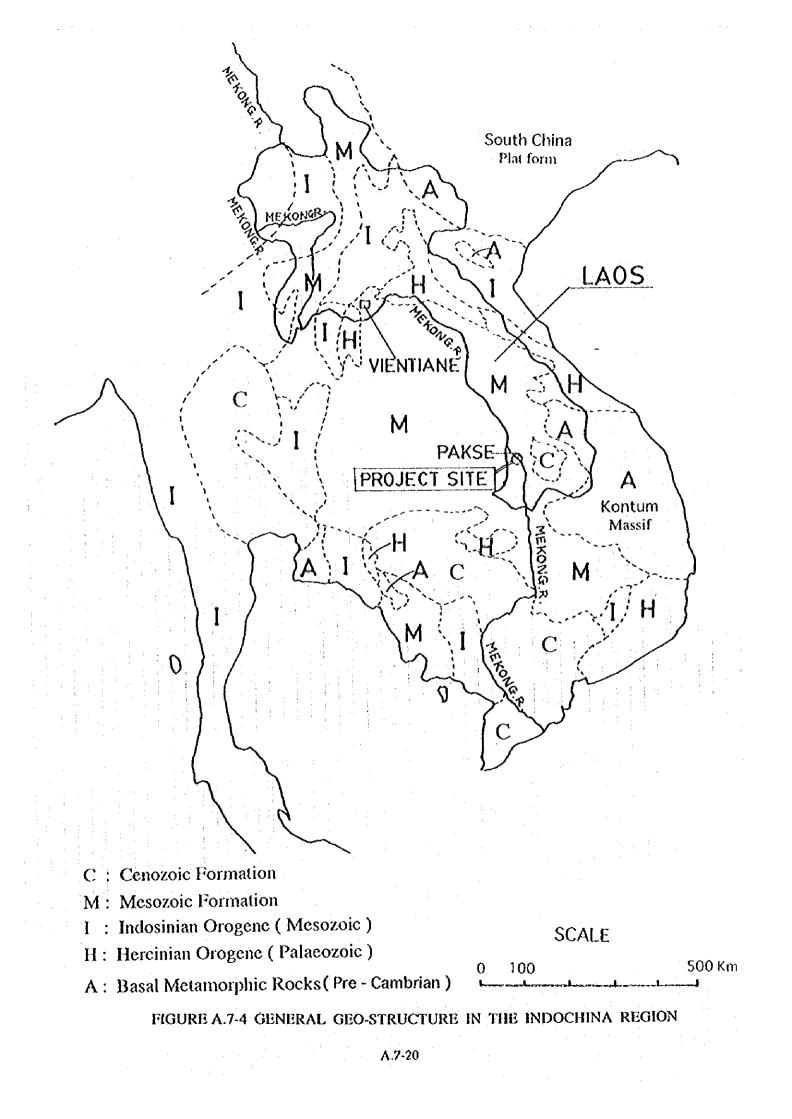


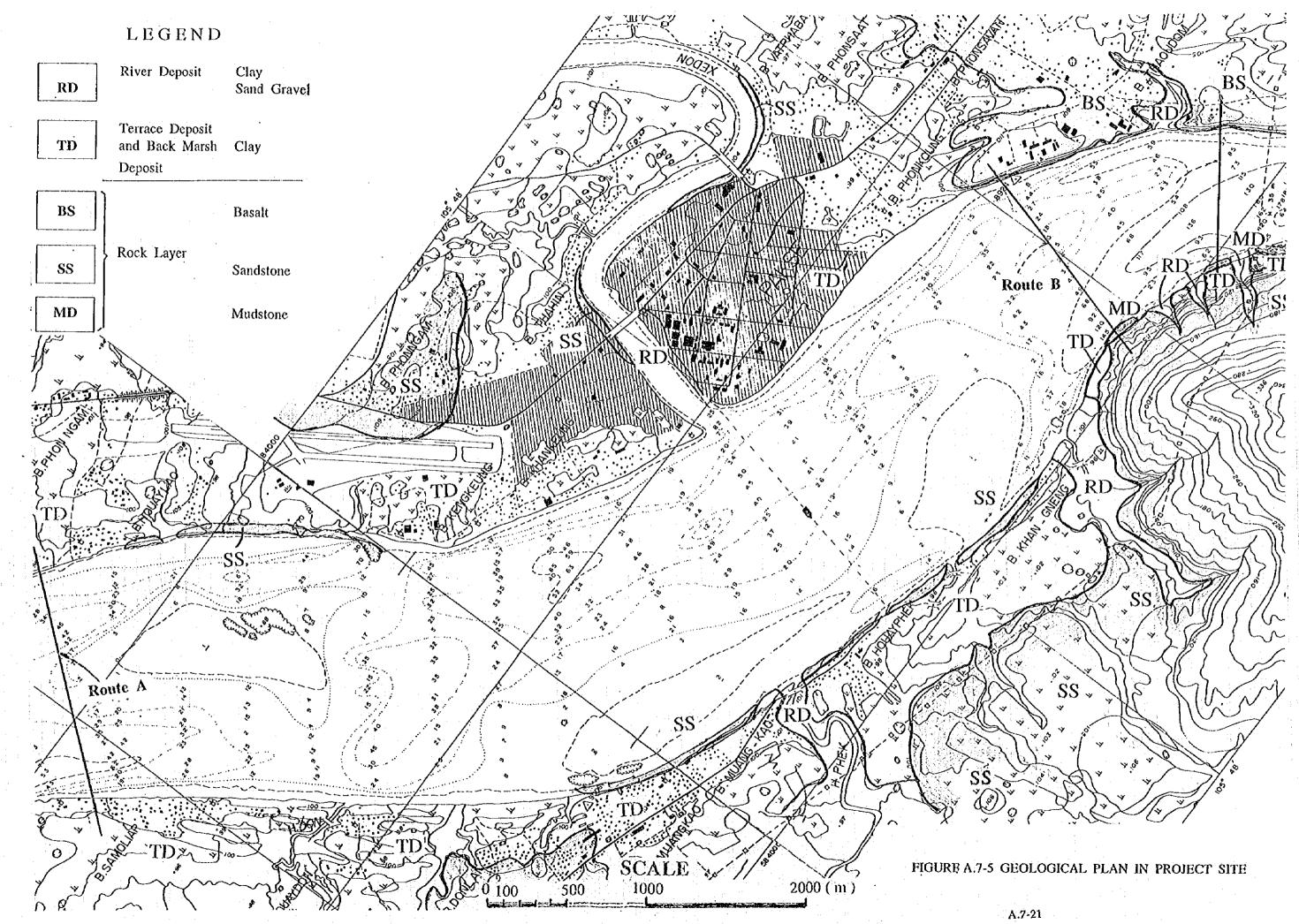




LONGITUDINAL SECTION LINE--C SCALES HOR 1 : 6000 VER 1 : 600







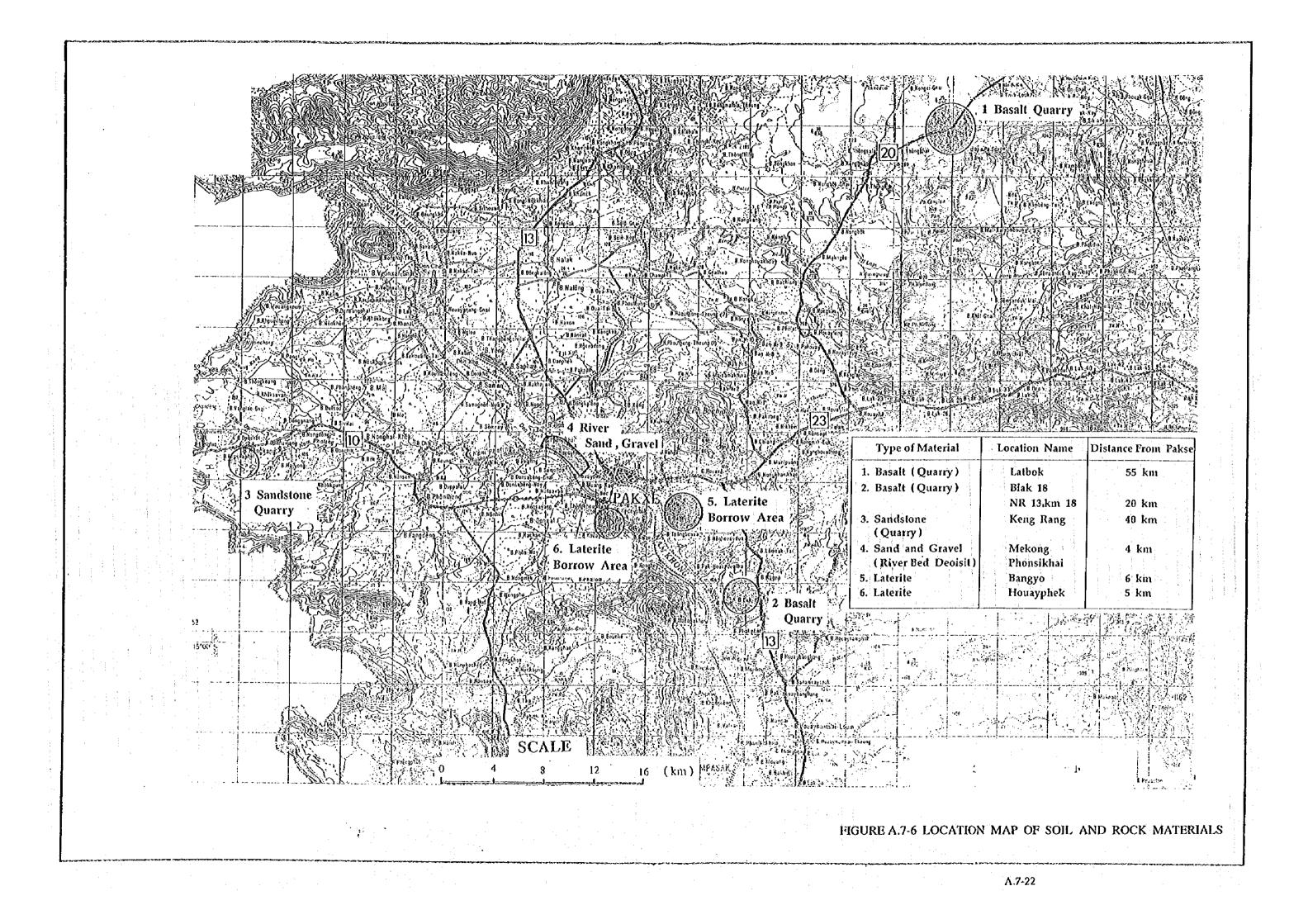


TABLE A.9-1	COST COMPARISON FOR FOUNDATION STRUCTURES (ROUTE-A)

· .

A TYP	e of Foundation				Cast-in-situ	Pile		Direct Found	lation				
B Dire	ct Construction Cost	Uoit: USS				270,70	<u>9</u>		365,157				-
NO.	DESCRIPTION	SPEC	UNIT	UNIT COST	QUANTIN	AMOUNT	REMARKS	QUANTITY	AMOUNT	REMARKS	QUANTITY	AMOUNT	REMAR
<u> </u>						T							ļ
a)	Works					185,60			141,160	.		· · · · ·	
	1) Steel sheet piling	ប-នា, L=7៣	_ P			1						جائبت المستنا	
	2) Steel sheet piling	U-111, L=8m	<u>.</u> P	37				ļ					
	3) Steel pine-sheet oiling	J=800 L=12m	pc	1150			D	60	69,000	.			
	4) Support erection	H beam	ŧŧ.	·			01 · · · ·	40	2,400				
	 Weight for caisson 	H-beam		5 (2 · ·					· · · · · · · · · · · · · · · · · · ·	
	 Sheet pile removal 	បញ	N	25			°		48,300				
	 Steel pipe-sheet removal 	d=\$00,L=12m	1_2	805				6			•••••		
	 Support removal 	H-beam	!	54				4	1,800	~			
	9) Weight removal	El-beam	·	4.			· · · · · · · · · · · · · · · · · · ·	· · · · · · · · · · · · · · · · · · ·		· · · · · ·			
	10) Embakment of islet	Sand & gravel	<u></u> m3				Y					····· · ···	
	11) Removal of ister	Sand & gravel					· · · · · · · · · · · · · · · · · · ·				· · · · · · · · ·		
	12) Drilling, S&G & rock (A)	1500d*5+5m	<u>n</u> J	23200]	8 185,60	<u> </u>	<u>.</u> i					
	13) Drilling, S&G & rock (B)		no	<u>1390</u> 0	1	·	ງ		· ··				
	14) Drilling, S&G & rock (B)	1000d*10.5+2	no	1110	1	· · · · · · · ·	<u>/</u>	· · · · · · · · · · · · · · · · · · ·] - · · - · · - ·			
	15) Drifling, S&G & rock (C)	2000d*4+7m	<u>no</u>	41500			·	· · · · · · · · · · · · · · ·					
	16) Drilling, SAG & rock (C)		no	27000	I		<u></u>	· · · · · · · · · · · · · · · · · · ·					
	17) Drilling, SAG & tock (C)	1000d*4+5m	no	1650	· · · · · · · · · · · · · · · · · · ·		×	1,00	10.050				
· · · ·	18) Excevation manual	Sand & gravel					· · · · · · ·	10	the second second second				
.	19) Excavation, manual	Rock	m.		1	- -	<u></u>	71		· · · · · · · · · · · · · · ·			
11	20) Backfill	Sand & gravel	. <u>m</u> 3		1	• · · · • — —	-		1	· · ···- · -			1
			·	·····		81,38		- [223.99	,			
<u>. b</u>	Materials		· · · · ·						(k			
1	 Concrete caisin 		<u>h0</u>	· · · · · · · · · · · · · · · · · · ·			<u></u>))			
	2) Steel sheet pile	U-III, L=7 m	<u></u>			· · · · · · · · · · · · · · · · · · ·	<u></u>		· · · · · · · · · · · · · · · · · · ·				
11	3) Steet sheet pile	14-111, L=8 m	. <u> </u>		<u>]</u>		N		· · · · · · · · · · · · · · · · · · ·)			
	4) Steel pipe sheet pile	d=800,L=12m	- <u></u>	· • · · · · · · · · · · · · · · · · · ·	() · · ·		0	7,20	50,43				
	5) Steel pipe-sheet pile	d=800,L=7.56			<u>'</u>		0	6)			
	6) Steel pipe-sheel pile	1=800,1,=4.5m											
·	7) Steel pipe-sheet pile	d=1000,L=19m d=1000,L=22m					6						
	8) Steel pipe-sheet pile	H-beam		· · · · · · · · · · · · · ·				3,60	10,80	0			
	9) Supporting beams	2000d*19m	<u></u>				J	-		0			
· · · · ·	(0) Casing pipe	1500d+13m	- ^k			8 40,8				0		سفير في ال	
	11) Casing pipe	1500d*18.5m					0			D		<u>.</u>	- 1
	12) Casing pipe	1000 4*19 m				1	0			D	·		
	13) Casing pipe [4] Concrete form	Metal	- 1 m			2,6	м	9	5 1,14	D.			2
· · · ·	15) Concrete form	Weeden					0			0			
	16) Sliding form	Metal	m			-	0	23	\$ 4,70	0			
	17) Form support	B-beam, etc.			\$ 51	4,07	26			0			
	18) Scaffolding	Chil type	- m		4		0	30					
	19) Lean concrete	180kg/cm2	- ភា	a la servició de servició	0		0	1	x 90				
	20) Concrete	240kg/cm2	In In			16 I.R.O	18	49	2 30,36	6			
	21) Concrete	400kg/cm2					0		1	0			
+	22) Reinforcement hat	Deformed		65	0	13 15,8	70	3	9 26,91	<u>of</u>			
			1		Materials i	in pites		-			·		
	· · · · · · · · · · · · · · · · · · ·					3,7	15			0			. .
1	13) Concrete	240kg/cm2	m3		3	28 1,7	83			9			
1.4	24) Reinforcement bar	Detormed	1	6	Ø	1 19	32			9		· - · · · · · · · · ·	
	25) Concrete form		m2		2					0			
	26) Sweitedge	For caison	1	300	X1		9	<u></u>		Ч			
L			÷.,	· · · ·						•	2 ° -		
												:	
								- 1 - 1		· · · · ·		1.1	
							••		÷		-		
						÷					:		
	·					· .						e de les Maria de la	2.1
												· · · · ·	
												- 1 - E - E	; ·
													1.1

А.9-1

}	pe of Foundation				Cast-in-situ	Pile		Open Caisse	hat		Interlocking	Steel Pipe Pil	e Well
Di	rect Construction Cost	Unit: US\$				245,10	2		412,138			432,45	3
<u>.</u> 0.	DESCRIPTION	SPEC	0MI	UNIT COST	QUANTIT	AMOUNT	REMARKS	QUANTITY	AMOUNT	REMARKS	QUANTIES	AMOUNT	REMARK
					l								
્મ્	Works		1.27			E11,200			196,576			214,54	2
	1) Steel sheet piling	U-131, L=7m	PS	35		1 9	1		0				0
·	2) Steel sheet piling	U-B1, L=8m	R5	37				· · · · · · · · · · · · ·	0				DI
	3) Steel pipe-sheet pilong	J≈ 800,1.≖12m		1,150	°	!	······································	76	\$7,400				D
	 Support crection 	H-beam		60				25	1,500		24	1,4-1	D
	5) Weight for caisson	H-beam	· *	50	[· · · · ·	×	100	5,000				P
	6) Sheet pile removal	U-31		25	1	<u>، د</u>	·	83	2,075	· · · ·	- . . .		P
	 Steel pipe-sheet removal 	δ=\$00,L=12m	N	805					61,180				2
	8) Support removal	H-beam	· •	5.5		0			0			1,29	5
	9) Weight removal	H-beam	-	45				···· • ···	0				7
	10) Embakment of islet	Sand & gravel	3	`		· · · · · · · · · · · · · · · ·	.	1,805	9.025			(2
	11) Removal of islet		<u></u>	· · · · · · · · · · · · · · · · · · ·		<u>، ، م</u>	[1,805	9,025			(۱
	12) Dolling, S&G & rock (A)	1500d+5+6m	nó.	23,200		<u> </u>	····		0	· · · · · · · · · · ·		(1
	13) Drilling, 5&O & reck (8)	15004*10 5+2	_D0.	13,900		111,200			0			(
	14) Drilling, S&O & rock (B)	10000+10.5+2	no	11,100		0			0		19	210,900	
	 Drilling, \$&O & rock (C) 	2000d*4+7m	no.	41,500		0		<u> </u>	0			(
	16) Drilling, S&O & rock (C)	1500d*4+7m	BO.	27,000		: 0			0			(
:	17) Drilling, S&G & rock (C)	1000d*4+5m	_ло.	16,500		0			0			(
<u>`</u>	18) Excevation, manual	Sand & gravel	- m3	10		0		1,706	17,000		· · · · · · ·	(
	19) Excavation, manual	Rock	- m3	60		0		40	2,400			(
	20) Backfitt	Sand & gravel	m3	3	· · · · · · · · · · · · · · · · · · ·	0		657	1,971		302	906	
													· · · · · · · · ·
b)	Materials					100,236			137,735		· • ••• • • • • • • • •	198,192	
	1) Concrete caisson		90.			: 0				See below			
	2) Steel sheet pile	U 111, L=7 m	t.d	3		0		· ···- • -··· •	·	~~~~~	-1		
	3) Steel sheet pile	U-111, L=8 m	. Ld				1.16-15-1	· · · · · · · · ·	ä			····· · · · · · · · · · · · · · · · ·	
	4) Steel pipe-sheet pile	J=800,L=12m	- t d		• • • • • •	·····		14,610	102,270 3	monthe			
1.11	 Steel pipe-sheet pile 	d=800,L=7.5m					· · · · · · · · · · · ·			11110116			
÷	6) Steel pipe-sheet pile	d=800,L=4 5m	}` ĭ	1.625									
	7) Sicel pipe-sheet pile	d=1000,L=19m	i - J	8,784			· · · · · · · · · ·					U	
·	 Steel pipe sheet pile 	d=1000.1.=22m	$= \frac{100}{100}$	10,240		· · · ·		** _ ** - ** -				166,896	
2	 Supposing beams 	H beam	1	10,2-6		×							1 -
-1	10) Casing pipe	2000.0*19m		16 500					· · · · · · ·		720	2,160	
	10) Casing pipe	1500d*13m		5,100		·		· · · · · · · · · · · · · · · · · · ·	<u>9</u>			•	
	12) Casing pipe	1500d*18.5m	- P.	7,200			· · · · · · · · · · · · · · · ·	· · · · · · · · · · · · · · · · · · ·	9	• •····		0	
		1000J*19m	_ <u>P</u>			57,600	i ÷÷÷	· · · ·					
· . · · · ·	13) Casing pipe		. PC	6,200	·····		، سېلېدې م. اد	· · · · , /	9			0	
- <u>+</u>	14) Concrete form	Metal Wooden	<u>m2</u>	12	217	2,604	·				86	1,032	
1.00	15) Concrete form		m 2	13		6	·			.		0	
444	16) Shding form	Metal	<u>m2</u>		<u></u> .	9		227	4,540		·	0	
÷	17) Form support	H beam, cic.	<u>. m3</u>	· *		6,144		25	200			0	
	18) Scaffolding	Unit type	_ <u>m2</u>			0		294	1.06			0	
	19) Lean concrete	150kg/cm2	3	50			· · · · · · · · · · · · · · · · · · ·		0			0	
	20) Concrete	240kg/cm2	_m3	63	286	11,018		250	15,750		238	(4,994	
	21) Concrete	400kg/cm2	_m3			0		T	0			D	
	22) Reinforcement har	Deformed		690	23	15,870		20	13,800		19	13,110	
					Materials in			Materials for	Caissop .	f:	Materials in E	rile i	
						33,666			77,826		T	19,719	
	13) Concrete	240kg/cm2	m3	63	254	16,002		410	25,830		313	19,719	
71	24) Reinforcement bar	Deformed	a 🗍 🗌	690	26	17,664	·······	49	33,948			A	
	25) Concreté form	Metal	m 2	12		0	· · · · · · · · ·	4.9	5,148				···
	26) Steel edge	For caison		3 000					12,900				

TABLE A.9-2 COST COMPARISON FOR FOUNDATION STRUCTURES (ROUTE-B)

A.9-2

T.	pe of Foundation				Cust in situ	Prie, d=1500	<u>mm</u>	Cast in situ	Pile, d=2(X00)	ាតា	Interlocking Steel Pipe Pile Well		
	rect Construction Cost	Unit: US\$:		781,611	•		\$16,655			1,240,632	
ō.	DESCRIPTION	SFEC	UNIT	UNIT COST	QUANTITY	AMOUNT	REMARKS	QUANTID	AMOUNT	REMARKS	QUANTITY	AMOUNT	REMAR
<u>v</u> .									415,000		·	703,260	··· • • • • • • • • •
D	Works					455,000			413,000				
	1) Steel sheet piling	U-111, L=7/10	E	35								· · · · · · · · · · · · · · · · · · ·	
	2) Steel sheet piling	U-111, L=8m	<u>. e</u>	37					· · · · · · · · · · · · · · · · · · ·			· · · · · · · · · · · · · · · · · · ·	
÷	3) Steel pipe-sheet piling	d=800.L=12m	£c	1150		· · · · · · · · · · · · · · · · · · ·		1 . .		· · · · · · · ·			
-	4) Support creation	H-beam	_:.*	60		· · · · · · · · · · · · · · · · · · ·							
	5) Weight for caisson	H-bcam		\$ 0			.		· · · · · · · · · · · · · · · · · · ·				
• •	6) Sheet pile removal	V- (1)	PC	25			1		· · · · · · · · · ·	· - · ;- ·			
	7) Steel pipe-sheet removal	d=800,L=12m	1. 1.	805		····	 		`		11.01		1
	8) Support removal	H-bcam	1	54		<u>-</u>	}						
	9) Weight temoval	H-beam	1	45		',	3						
	10) Embakment of islet	Sand & gravel	_m]	5			<u>4</u>	·	2	,			8
	(1) Removal of islet	Sand & gravel	_ <u>m3</u>				<u> '</u>]						
• •	12) Drilling, S&G & rock (A)	1500d*5+6m	ng	23200	1		1		······)	3	• · · · · · ·		1
	13) Drilling, S&G & rock (B)	15001*10.5+2	no	13200					– – ?	3			1
	14) Drilling, S&G & cock (8)	10004+10.5+2	no.	11100			· · · · · · · · · · · · · · · · · · ·		415,000	í			
	15) Drilling, S&G & rock (C)	2000d*4+7m	n -0	4150			D			1			÷
	16) Drilling, S&G & rock (C)	1500d*4+7m	no	2700		4\$6,00	D I			1	47	693,00	
	17) Drilling, S&G & rock (C)	1000d 4+5m	60.	1650			P		1				í - ···
	(8) Excavation manual	Sand & gravel	m3	1			0		····				<u> </u>
-	19) Excavation, manual	Reck	B	6		1	0			2		10.36	· · · · ·
	20) Backfill	Sand & gravel	m?	1	2		0			DI	3,420	10,26	<u> </u>
. •	20) BJCCHR		- [<u> </u>		· · · · · · · · · · · ·				· · · · · · ·
) Materials		-	1		195,37	B		298,15	5		491,57	<u></u>
_b							0			P			· · · · ·
	 Concrete caison 	U-113, L=7 m		· · · · · · · · · · · · · · · · · · ·	3		0			0		· · · · · · · · · · · · · · · · · · ·	
	2) Steel sheet pile	U-III, L=8 m		· · · · · · · · · · · · · · · · · · ·			0	:		0			ol
	3) Steel sheet pile	d=800 L=12m	· • •		7		0			0			0
	4) Steel pipe-sheet pile	d=800,L=7.5m					0			0			0
	5) Steel pipe-sheet pile				· ···· ··· ·		0			0	<u></u> .		9
	6) Steel pipe sheet pile	d= 800 L= 4.5m				1			1 1	0	1 <u>1</u>		9
	7) Steel pipe sheet pile	d=1000,L=19n		· · · · · · · · · · · · · · · · · · ·		· · · · · ·			1	0	4	430,05	9
	8) Steel pipe sheet file	d=1000,L=22n			· · · · · · · · · · · · · · · · · · ·		<u> </u>	•	· · · · · · · · · · · · · · · ·	0			0
	9) Supporting beams	H-beam			2 · · · - · · · · · · · · · · · · · · ·		ă	1	65,00	0			0
	10) Casing pipe	20003*19m		1			<u>.</u>			0			ol
	(1) Casing pipe	1500J*33m	£		a supreme server and the server	R 129.60	J	- {		ol			0
	(12) Casing pipe	1500d*18.5m				N 123'00	ງ			0	- -		0
	13) Casing pipe	10004-1911	P			7 4,10	a	93	11,24	iul	120	5 1,5	2
	14) Concrete form	Metal	<u>m</u>			459	A	··		6		1	0
	15) Concrete form	Woodca	. <u> </u> <u>n</u>		3		2	- • •		0		1	0
	16) Sliding form	Metal	m		1	· · · · · · · · · · · · · · · · · · ·	y	-	· [+	ol	1		0
	17) Form support	H-beam, elc.			<u></u>				• • • • • • • · · · · · · · · · · · · ·	0	· } · · · · · · · · · · · · · · · · · ·		0
• • •	18) Scaffolding	Cait type	m			· · · · · · · · · · · ·	<u></u>	· · · · · · · · · · · · · · · · · · · · ·			- 1	1	0
	19) Lean concrete	1BOkg/cm2	m		io 		×	1,03	7 65,3	ăl	50	3 31,6	39
	20) Concrete	240% g/cm2	m		<u>s</u> <u>s</u>	8 32,6	24		·	а о	1	1	0
	21) Concrete	400kg/cm2	m		15	1	. <u></u>		2 56,5		-	28,2	x
	22) Reinforcement bar	Deformed		0 6		2 28.9	st.	Materials i			Materials in		-1
	····			1	Materials			Materials I	n pales 103,50	· · · · · · · ·		45,8	51
. <u></u> .		1	_	1		100,2					72		
	23) Concrete	240kg/cm2	6.0		<u>n</u>			2			·· [• · · · · · · · · · · · · · · · · ·	` · [™] "	0
	24) Reinforcement bar	Deformed	-k	6	×	6 52,5	64		5 51,7	<u>~</u>]			
	25) Concrete form	Metal	- m2		<u>i</u> 2		9		. 	.y			1
	26) Steel edge	For calson	- 1:	30		1	0		1	9			<u> </u>

TABLE A.9-3 COST COMPARISON FOR FOUNDATION STRUCTURES (ROUTE-C)

A.9-3

TABLE A.9-4 COST DATA FOR BRIDGE TYPES AND SPAN LENGTH RANGE

:

and all the second second second		-			***		n a synthesis aligned for the state	(16060)
		RSTRUCTURE			TRUCTURE C		TOTAL	C0\$1
SPAN	AREA	UNIT COST		NUMBERS	UNIT COST			
	<u> </u>	US \$ / M2	U\$ \$	<u>N</u>	US \$ /N	US \$	<u>US</u> \$	US & - M2
	(ROUTE-A)		· · · · · · · · · · · · · · · · · · ·					
58	17160	2.858	35315.28	33	524	17292	52607.28	
70	17160	2.529	43397.64	25	579	14475	57872.64	
100	1716B	3,325	57074.16	18	661	11898	68972.16	4.019356
· -• ·				······				
								L
	(ROUTE-B)							- è
58	15180	2.058	31240.44	29	557	16153	47393.44	
78	15188	2.529	38398.22	23	615	14145	52535.22	
168	15188	3.326	58488.68	17	781	11917	62485,68	4.111046
	·	· · · · · · · · · · · · · · · · · · ·						
			·					
	(ROUTE-C)		·			· · · · · · · · · · · · · · · · · · ·		
78	18450	2,529	26428,85	15	1874	16118		
DE SPAN			5536			586	45330.05	3.746285
100	10450	3.326	34756.7	13	1185	15145		
IDE SPAN			2286		· ·	596	52693.7	4.354851
	•••••							
	·							
								l
]		L

BRIDGES TYPES AND SPAN LENGTH RANGE (CONTINUOUS STEEL BOX GIRDER WITH RC SLAB)

BRIDGES TYPES AND SPAN LENGTH RANGE (Continuous steel box girder with steel deck)

		<u> </u>	<u> </u>		1.1			10000 S
	SUPE	RSTRUCTURE	COST	SU8S	TRUCTURE C	OST	TOTAL	
SPAN	AREA	UNIT COST	COST	NUMBERS	UNIT COST	COST		
	M2	US \$ /M2	US \$	N	US \$ -N	US \$	USS	US \$ / N2
	(ROUTE-A)				· · · · · · · · · · · · · · · ·	·		
]			·	T
85	17168	3.843	52328.84	25	579	14475	66795.84	3.8925315
186	17168	3.521	68428.36	18	661	11898	72318.35	4.2143566
130	11160	4.865	69755.4	13	723	9399	79154.4	4.6127273
160	17168	4.591	77237.16	11	785	8635	a second seco	5.0842851
								1
	(ROUTE-B)	•			Per manua sera 1 .	B	K	£
		1		1	I	·	1	T
78	15188	3.049	46283.82	23	615	14145	60428.82	3.9888182
160	15180	3.521	53448.76	17	701	11917		4.3262461
138	15188	4 865	61726.7	12	758	9216		4.6721146
160	15188	4.581	68325.18	10	832	8328		5.9490896
· · · ·								0.0400000
	(ROUTE-C)	• • •	L _	L	•	K	L	L
78 }	18458	2.795	29207.75	15	1874	16118	1	1
SIDE SPAN			5586			588	48109.75	3.9788124
188	10450	3.521	36734.45	13	1165	15145		P
SIDE SPAN			2286	an an an the state		506	54731.45	4.5232683
158	18458	4.501	47835.45	9	1316	11844	3-131.43	4.0002000
SIDE SPAN			2286	1 - N - N		586	61671.45	5.096814
268	18458	5.299	55374.55	8	1837	14696		1
SIDE SPAN		1.00 37 777	2286	Ĭ	1001	566	72862.55	6.0216983
				┟				0.0010303
and the surgery strategies of the second strategies of	Contraction of the Contraction of the Contraction	the second se		<u>}</u>		1		•

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BRIDGES TYPES AND SPAN LENGTH RANGE (THROUGH TYPE STEEL ARCH)

		(THROUGH	TYPE STEE	L ARCH)				
							a an	(10000\$
	SUPE	RSTRUCTURE	COST	SUBS	TRUCTURE CO		TOTAL	COST
SPAN	AREA	UNIT COST		NUMBERS	UNIT COST	COST		
- VI 80	M2	US \$ /M2	US \$	N	US\$/N	US \$	USS	105 \$ /12
	(ROUTE-A)							
								05 45 215
78	17168	2.211	37948.76	25	578	14475	52415.76	3.0343313
188	17160	2.874	49317.84	18	661	11898	61215.84	1.0013000
130	17160	3.722	63869.52	13	723	9399	73268.52	4.2091213
168	1716B	3.832	65757.12	11	785	8635	74392.12	4,3352021
							L	
	(ROUTE-B)				, ·			·····
							47787.98	3 1420102
78	15180	2.211	33562.96	23	615	14145		3.6598461
188	15188	2.874	43627.32	17	701	11917		4.3275336
138	15180	3.722	56499.96	12	766	9192	and the second second second second	4.3802890
160	15180	3.832	58169.76	18	832	8320	00483.10	4.3006030
				L			<u></u>	L
	(ROUTE-C)				1001	10113	T	• • • • • • • • • • • • • • • • • • •
78	18458	2.826	21171.7	15	1874	16110	40073.7	3,311876
SIDE SPAN			2296			586	40013.1	0.01101
188	18458	2.874	30033.3	13	1165	15145 586	47978.3	3.964487
SIDE SPAN		L	2286			11844	41310.3	5.304.01
150	18458	3.685	38588.25	9	1316	526	\$3144.25	1.392886
SIDE SPAN		I	5586			14696	1	1.7.7.4.6.7.4.4
288	10450	4,495	46983.2	8	1837	526	1 64411 2	5,328198
SIDE SPAN	<		2286			200	1	f
		1	A DESCRIPTION OF THE OWNER OWNER OF THE OWNER OWNER OF THE OWNER	A DESCRIPTION OF THE OWNER WALL	A DESCRIPTION OF THE OWNER OWNER	and a second second	-	lare an array of the

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BRIDGES TYPES AND SPAN LENGTH RANGE (THROUGH TYPE CONTINUOUS STEEL TRUSS)

		CTRROUGH	TYPE CONT	INUOUS STE	EL TRUSS)		14 14 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	
1								100205
i	SUPF	RSTRUCTURE	COST	SU8S	TRUCTURE CO	ST	TOTAL	COST
SPAN	AREA	UNIT COST	COST	NUMBERS	UNIT COST	COST		······
- 1	M2	US\$ /82	US \$	N	US\$/N	US \$	US \$	(US\$/M2
· · · · · · · · · · · · · · · · · · ·	(ROUIE-A)							
58	17168	1.916	32878.56	33	524	17292	50170.56	
70	17168	2,175	37323	25	579	14475		3.8185315
100	17160	2.726	46778.16	18	661	1898		3.4193566
138	17160	3.54	60746.4	13	723	9399		4.0617273
160	17160	4.275	73359	11	785	8635	81994	4.778205
								J
	(ROUTE-B)		-					1
58	15188	1.918	29284.88	29	557	16153		2.9888975
78	15180	2.175	33016.5	23	615	14145		3.186818
108	15188	2.726	41388.68	17	781	11917		3.511046
130	15180	3.54	53737.2	15	168	9216		4.147114
160	15180	4.275	64894.5	18	832	8320	73214.5	4.823089
	• • • • • • • • • • • • • • • • •						L	L
	(ROUTE-C)	l					· · · · · · · · · · · · · · · · · · ·	· · · · · · · · · · · · · · · · · · ·
78	18458	2.175	22728.75	15	1874	16118	1	Letter Barrie
SIDE SPAN			2285	•	I	506	41630.75	3.448557
188	18450	2.727	28497.15	13	1165	15145	· · · · · · · · · · · · · · · · · · ·	In the second
SIDE SPAN			2286		J	586	46434.15	3.837533
150	18458	4.831	42750.95	9	1316	11844	S. Contractory	les serve
SIDE SPAN			2286	l	1	586	57386.95	4.742723
288	10450	5.012	52375.4	8	1837	14696	the strain.	de Canada a
SIDE SPAN			228C		1	586	69663.4	5.773834
				1			1	

		CONTINU	OUS PC BOX	GIRDER				
	والمراجع وال					-		<u>() 6990 (\$)</u>
Ļ		RSTRUCTURE			TRUCTURE C		TOTAL	COST
SPAN (AREA	UNIT COST		NUMBERS	UNIT COST		[
	112	US \$ / N2	US \$	N	US \$ /N	US \$	<u>US\$</u>	US \$ / H2)
	(ROUTE-A)							
50	17160	1.671	28674.36	33	617	20361	49835.36	2.8575385
70	17160	1.749	38812.84	25	632	17050	47862.84	2.7425897
188	17168	1.866	32020.56	18	778	14884	46824.56	2.6820839
130	17160	2.203	37883.48	13	851	11063	48866.48	2.847697
								· · · · · · · · · · · · · · · · · · ·
-	(ROUTE-8)	•					L	· · · · · · · · · · · · · · · · · · ·
58	15180	1.671	25365.78	29	655	18995	44368 78	2.9223175
78	15180	1.749	26549.82	23	723	16529	43178.82	2.8444545
100	15180	1.866	28325.88	17	825	14025	42350.88	2.169913
138	15188	2.203	33441.54	12	983	10836	44277.54	2.916834
			39441.54			10030	44211,04	2.310034
		······································						
 _	(ROUTE-C)		ا م الم الم الم الم الم	L		•		
	1.0012-07	·····	· · · · · ·	<u> </u>		·	r	· · · · · ·
			an a	• · • • • · · • • · · · ·	a server	alan a alan a		
	10450	1.014	10000			12610		
100	10450	1,844	19269.8	13	1370	17810		112122222
SIDE SPAN	1650		2756			595	48432.8	3.3415537
158	10450	2.208	23073.6		1548	13932		
SIDE SPAN	1650	· · · · · · · · · · · · · · · · · · ·	2758			595	40358.6	3.3354215
500	18450	2.513	26269.85	8	2161	17288		
SIDE SPAN	1659		2758			595	46981.85	3.876186

BRIDGES TYPES AND SPAN LENGTH RANGE (CONTINUOUS PC BOX GIRDER)

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BRIDGES TYPES AND SPAN LENGTH RANGE (CONTINUOUS RIGID FRAME PC BOX GIRDER)

r		CIDE	RSTRUCTURE	1900	cuee	TANCTURE C	0.0.Y		(19880 \$
	\$PAN	AREA	UNIT COST		NUMBERS	TRUCTURE C		TOTAL	COST
ł	vrna -	M2	US \$ /N2	USS	N	US\$/N	US \$	USS	US \$ / N2
F		(ROUTE-A)	03 4 112		A	03.971	03.0	03	1 105 \$702
	58	17160	1.61	27627.6	33	617	28361	47989.6	2.7965385
1	70	17168	1.693	29051.88	25	682	17050		2.6865897
	188	17160	1.818	31195.88	18	178	14894		2.6340839
1-	130	17168	2.178	37374.48	13	851	11063	48437.48	2.822697
17	168	17168	2.415	41441.4	11	923	10153		3.0866667
1									1.000000
1-		(ROUTE-8)	· · · · · · · · · · · · · · · · · · ·		• • • • • • • • • • • • • • • • • • •	••••••	••••••••••••••••••••••••••••••••••••••	•	
E	58	15180	1.61	24439.8	29	655	18995	43434.8	2.8613175
E	78	15188	1,693	25699.74	23	723	16629		2.7884545
1	198	16188	1.818	27597.24	17	825	14826	41622.24	2.741913
E	138	16180	2,178	33662.84	12	903	10836	43898.24	2.891834
	168	15180	2.415	36659.7	18	979	9798	46449.7	3.8599275
1									1
1		(ROUTE-C)						1	•••••••
	70	10450	1.681	17566,45	15	1263	18945		1
	SIDE SPAN			2758			595	39864.45	3.2945826
1-	188	18459	1.795	18757,75	13	1370	17818		
14	SIDE SPAN			2758			595	39928.75	3.2992355
	<u>150</u>	18450	2 351	24561.95	9.	1548	13932		
11	SIDE SPAN	***********		2758			595	41852.95	3.4589215
L	200	18458	2 676	27964.2	6.	2161	17298		
13	SIDE SPAN			2758	l		695	48605.2	4.8169587
L		States of the second							I

A 9-6

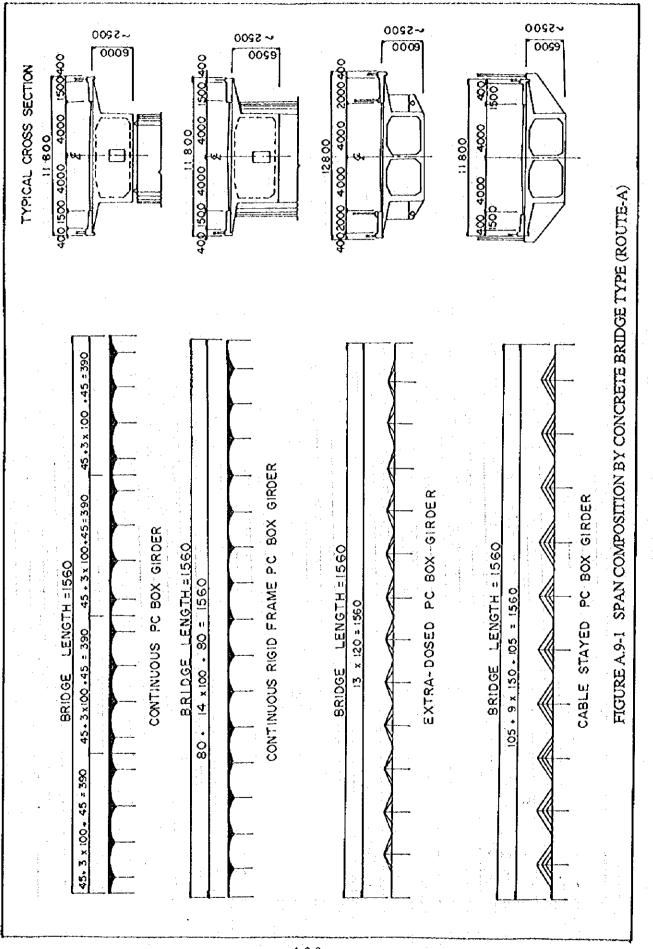
		(EXTRA-D	OSED PC 80	X GIRDER)				
			and and the state of the second s	personante de la compañía			TOTAL	(19034 \$
	SUPE	RSTRUCTURE	COST		TRUCTURE CO		IDIHL	<u>CUSI</u>
SPAN	AREA	UNIT COST	COST	NUMBERS	UNIT COST	COST		
	h2	US \$ /M2	US \$	N N	USSIN	US \$	US \$	(US \$ 2H2
	(ROUTE-A)						r	<u></u>
								0700000
1881	17168	2.056	35288.96	18	778	14084		2.872083
138	17160	2.428	41654.48	13	851	11863	52727.48	3.07269
160	17160	2.641	45319.56	11	923	10153	55472,56	3.2326661
					` `		l	I
	(ROUTE-8)	f					r	
1		<u> </u>				<u> </u>		
100	15180	2.856	31210.08	17	825	14025	45235.86	2.97991
130	15180	2,428	36857.84	12	903	10836	47693.04	3.14163
160	15189	2.641	49099.38	10	979	9798	49860.36	3.285927
								L
	(ROUTE-C)	L	·	· · · · · · · · · · · · · · · · · · ·				
	10010 01	1						
، - مع نب ه	• • • • • • • • • •							<u> </u>
188	18450	2.834	21255.3	13	1378	17818		
IDE SPAN			2758	1		595	42418.3	3.505644
158	18450	2.576	26919.2	8	1548	12384		
IDE SPAN			2758	l		595	42656.2	3.525305
200	18458	3.456	35115.2	6	2161	12966		La se sere
IDE SPAN			2758	1		\$95	52434.2	4.33340
THE SPHR	·	{		+			[
		1	And the second sec	As experiences to here and server	Contraction with the second second	C. Cranter Street & Lot Lot L		, -

BRIDGES TYPES AND SPAN LENGTH RANGE (EXTRA-BOSED PC BOX GIRDER)

BRIDGES TYPES AND SPAN LENGTH RANGE (Cable Stayed PC 60x Girder)

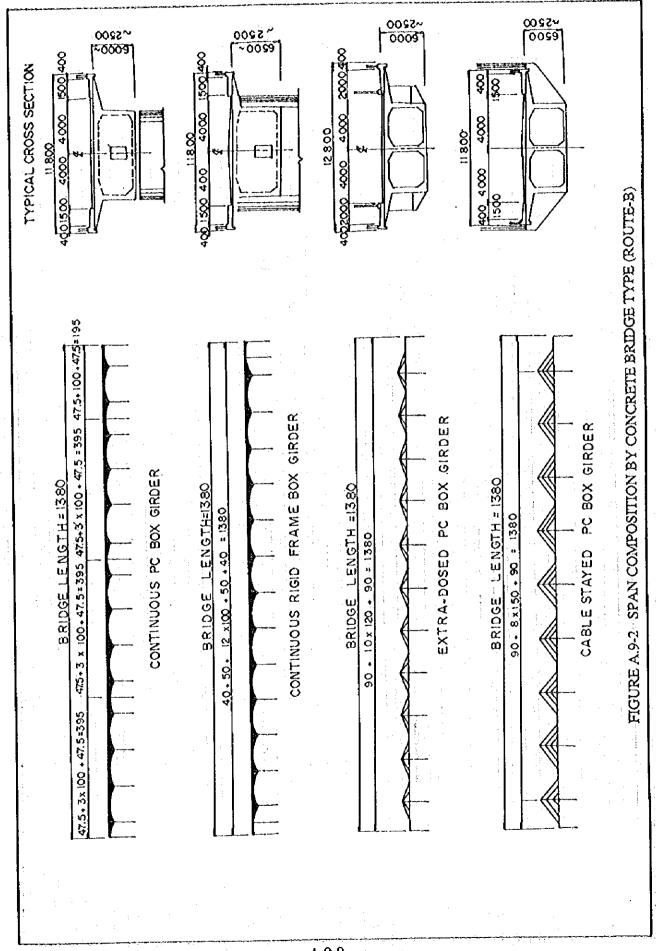
		(CABLE \$	TAYED PC B	OX GIRDERI	· ·			(19830 \$
	SUPF	RSTRUCTURE	COST	\$U8S	TRUCTURE C	0\$T	TOTAL	
SPAN	ARER	UNIT COST		NUMBERS	UNIT COST		· · ·	
	M2	US \$ /H2	US \$	N	US \$ /N	US \$	US \$	US \$ / M2
	(ROUTE-R)							y
								<u> </u>
						14004	57916.44	3.3758839
100	17160	2.559	43912.44	18	778		62234.12	3.626697
138	17168	2.982	51171.12	13	851	11063		3.786666
168	17168	3.195	54826.2	31	923	10153	04313.6	<u>p. 100000</u>
				I			l	المستحد والمستحد
	(ROUTE-B)	· · · · · · · · · · · · · · · · · · ·					·	1
			· · · · · · · · · · · · · · · · · · ·	<u></u>		<u>_</u>		
							52878.62	3.48291
182	15188	2.559	36845.62	17	825	14025		3.69589
138	15188	2.982	45286.76	12	903	10835	\$6102.76	3.839927
168	15180	3.195	48588.1	19	979	9798	58298.1	13.033321
			· · · · · · · · · · · · · · · · · · ·			L	L	1
	(ROUTE-C)						r	1
				•••••				
100	18458	2.538	26522.1	13	1370	17810		1.
SIDE SPAN			2758			595	47685,1	3.948917
150	18458	3,131	32716.95	9	1548	13932	.	1
SIDE SPAN		· · · · · · · · · · · · · · · · · · ·	2758			595	58003.95	4.132557
200	18458	3.456	36115.2	8	2169	17288		1. States
STDE SPAN		} · · · · · · · · · · · · · · · · · · ·	2758	l		595	56748.2	4.689933
		t		1	I	L		L

A.9-7

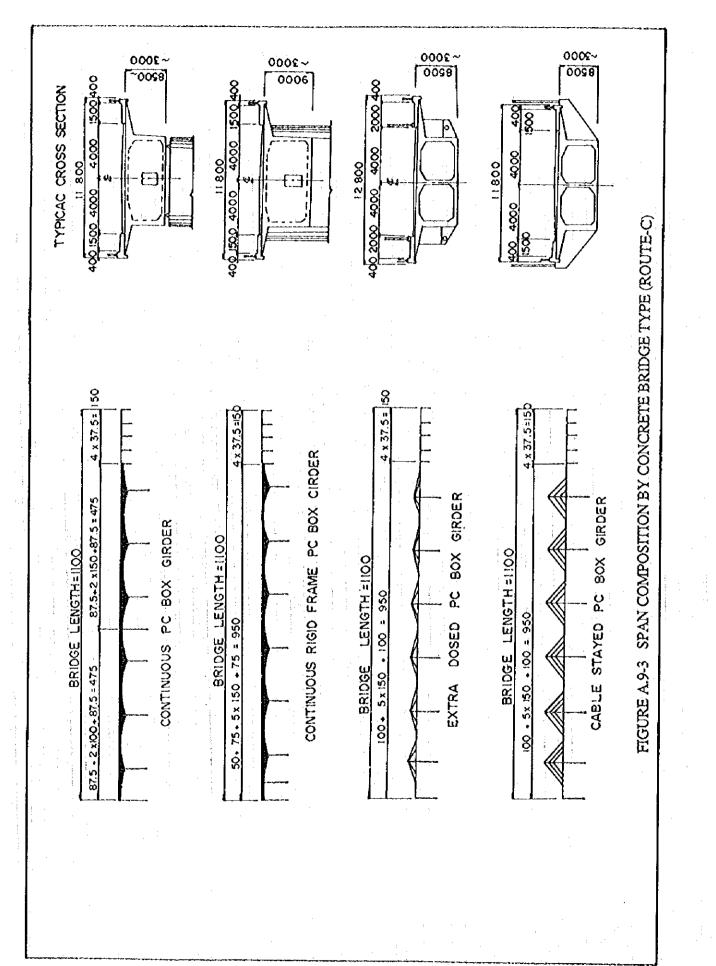


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A.9-10

TABLE A.9-5 CONSTRUCTION COSTS OF ALTERNATIVE ROUTES

1+ome of Works			ROUTE-A			ROUTE-B			ROUTE-C	
	:	Quantity	Unit	Amount	Quantity	Unit	Amount	Quantity	Unit	Amount
1 Superstructure										
1) DC hox concrete		16.810		9,750	14,700		8,526	12,240		6,889
	m3		0.580	9.750	14,700	0.580	8,526		0.590	6,608
Nail Spail	m3				0		0	1,040	0.270	281
2) Deformed har		2.520	1.650	4,158	2,210	1.650	3,647	 	1.650	3,036
	ب ه ا	1.220			1	12.800	13,696		12.800	14,336
	m2	17.160	0.220	3,775	15,180	0.220	3,340	12,10	0.220	2,662
	each	~	98.000		9	98.000	588	-	98.000	294
1	each	4	30.000	120	8	12.000	96	F	000.6	144
		LSI LSI		2,465	LS L		2,388	SJ		1,949
				36,570			32,280		·	29,31
								-		
2 Substructure										
	£	1,860	5.340	0		3.880	-			r~•
2) Pier/Abut concrete	m3	10,440	0.190	1,984	11,0	0.190	2	ດົ	0.1	
3) Deformed bar	ب	1.045	1.650		1,105	1.650	-	92	1.650	1,526
		LS LS		220			327	א גו		·
				13,860			11,870		ни и на села и на се 	14,370
· •		(3800m)			(3030m)			(4690m)		
3 Approact Nodus	e e	411300	0.027	, 11.105	_	0.022	5,81	2 239,800		5,51
	2	41,800		(()		0.009	31.0	0 51,590	600.0	
2) Pood ataintie		S		- C			1,587	Z] [2		1,455
3) AUGU SU ULUIUS				326			8	1 IS		0
4) MISCENATEOUS		3		12.510				0		8,480
Sub-rorai.										
Tatal-				62,940			52,670	0		52,160
									_	

		aladadaan a cur maana a dadaa 3				a Talence contra une serence mente	***	(US\$1,000)
			COSTS			BENEFITS		B - C
1		(1)	(2)	(3)	(4)	(5)	(6)	(7)
No.	Year	Investment	Maintenance &	Total	User cost	Savings in	Total	Net
		Cost	Operation	Cost	Savings	Ferry Operation	Benefit	Cash Flow
	1996	1386		1386	0		0	-1380
	1997	24413		24413	0		0	-2441.
	1998	23078		23078	0		0	-2307
	1999	20621		20621	0	:	0	-2062
-	2000	5190	7.6	5198	362	996	1358	-384
1	2001		15.2	15.2	854	1705	2559	254
2	2002		15.2	15.2	985	1861	2846	283
3	2003		15.2	15.2	1116	2246	3362	334
.4	2004		15.2	15.2	1247	2217	3464	344
5	2005		15.2	15.2	1379		3798	378
6	2006		15.2	15.2	1510		4366	435
7	2007		15.2	15.2	1641	2883	4523	450
8	2008	i	15.2	15.2	1772	3362	5134	511
- 9	2009		15.2	15.2	1903	3650	5553	553
10	2010		15.2	15.2	2034	3750	5784	576
n	2011		15.2	15.2	2246	4131	6377	636
12	2012		15.2	15.2	2457	4090	6547	653
13	2013		15.2	15.2	2669	4487	7156	714
14	2014	а.	15.2	15.2	2880	4463	7343	732
15	2015		15.2	15.2	3092	5	7755	774
16	2015		15.2	15.2	3303	(4) (1) (1) (1) (1) (1) (1) (1) (1) (1) (1	8392	837
17	2017		15.2	15.2	3515		8609	859
18	2018		15.2	15.2	3726		9267	925
19	2019		15.2	15.2	3938	1	9506	949
20	2020		15.2	15.2	4149		10187	1017
21	2021	1	15.2	15.2	4361		10665	1065
22	2022	1. a. 1	15.2	15.2	4572		10942	1092
23	2023		15.2	15.2	4784		11663	1164
24	2023		15.2	15.2	4995		11968	1195
25	2025		15.2	15.2	5206		12719	1270
26	2026		15.2	15.2	5418		13271	1325
27	2027		15.2	15.2	5629		13840	1382
28	2028		15.2	15.2	5841		14427	1441
29	2029		15.2	15.2	6052	-	14819	1480
30	2030	-25228		-25220	3132		7830	3305
, <u> </u>	TOTAL	49460	456	49916	96765	149264	246029	19611

TABLE A.10-1 COST BENEFIT CASH FLOWS (ROUTE-A)

-			r Calendral annin Restricted at the do-	th C Andraw Managiran pakin S. Inc. and				(US\$1,000
			COSTS			BENEFITS		B • C
		(1)	(2)	(3)	(4)	(5)	(6)	(7)
No.	Ýcar	Investment	Maintenance &	i Total	User cost	Savings in	Total	Net
:		Cost	Operation	Cost	Savings	Ferry Operation	Benefit	Cash Flow
	1996	1160		1160	0		0	-1160
	1997	20618		20618	0		0_0	-2061
	1998	20369		20369	0		0	-20369
. 1	1999	17257		17257	. 0		0	-1725
	2000	3286	6.1	3292	391	996	1387	-190
1	2001		12.1	12.1	926	1705	2631	261
2	2002		12.1	12.1	1069	1861	2930	291
3	2003		12.1	12.1	1213	2246	3459	344
4	2001		12.1	12.1	1357	2217	3573	356
5	2005		12.1	12.1	1501	2419	3920	390
6	2006		12.1	12.1	1644	2856	4500	448
7	2007		12.1	12.1	1788	2883	4671	465
8	2008		12,1	12.1	1932	3362	5293	528
9	2009		12,1	12.1	2075	3650	5725	571
10	2010	:	12.1	12.1	2219	3750	5969	595
11	2011		12.1	12.1	2448	4131	6579	656
12	2012		12.1	12,1	2677	4090	6767	675
13	2013		12.1	12.1	2906	4487	7393	738
14	2014		12.1	12.1	3135	4463	7598	758
15	2015		12.1	12.1	3364	4664	8028	801
16	2016		12.1	12.1	3593	5089	8682	867
17	2017		12.1	12.1	3822	5094	8916	890
18	2018		12.1	12.1	4051	5541	9592	957
19	2019		12.1	12.1	4280	5568	9848	983
20	2020		12.1	12.1	4509	6038	10547	1053
21	2021		12.1	12.1	4738	6305	11043	1103
22	2022		12.1	12.1	4967	6370	11337	1132
23	2023		12.1	12.1	5196	6879	12075	12063
24	2024		12.1	12.1	5425	6973	12398	12380
25	2025		12.1	12.1	5654	7512	13166	1315
26			12.1	12.1	5883	7853	13736	13724
27	2027		12.1	12.1	6112	8211	14323	1431
28	2028		12.1	12.1	6341	8586	14927	1491
29	2029		12.1	12.1	6570	8766	15336	15324
30	2030	-21205	6.1	-21199	3399	4698	8028	29290
	TOTAL	41485	364	41849	105185	149264	254449	212600

TABLE A.10-2 COST BENEFIT CASH FLOWS (ROUTE-B)

A.10 - 2

	The second se		00000	an a		BENEFITS		B-C
			COSTS				(6)	(7)
	·	(1)	(2)	(3)	(4)	(5) Savings in	Total	Net
NO.	Year	Investment	Maintenance &	Total	User cost		Benefit	Cash Flow
		Cost	Operation	Cost	Savings	Ferry Operation	<u> </u>	-114
	1996	1148	1	1148	0 0		0	-2079
	1997	20793		20793			0	-2017
	1998	20172		20172 17089	0		0	-1708
	1999	17089		1	349	996	1345	-191
	2000	3254	9.4	3263			2534	251
- 1	2001		18.8	18.8	829 962		2823	280
2	2002		18.8	18.8			3340	332
3	2003		18.8	18.8	1094 1227	2240	3443	342
4	2004		18.8	18.8	1227		3778	376
-5	2005		18.8	18.8			4347	432
6	2006		18.8	18.8	1491	2856 2883	4507	448
- 7	2007	8 d	18.8	18.8	1624 1756		5118	509
8	2008		18.8	18.8			5539	552
- 9	2009		18.8	18.8	1889	1	5771	575
10	2010		18.8	18.8	2021		6339	634
-11	2011		18.8	18.8	2228		6526	650
12	2012	· · · · ·	18.8	18.8	2436	the second se	7130	711
13	2013		18.8	18.8	2643	the second se	7314	729
14	2014		18.8	18.8	2851	1	7722	770
15	2015		18.8	18.8	3058		8354	833
16	2016		18,8	18.8	3265		8567	854
17	2017		18.8	18.8	3473		9221	920
18	2018		18.8	18.8	3680		9221	943
19	2019		18.8	18.8	3888		10133	1011
20	2020		18.8	18.8	4095		10155	105
21	2021		18.8	18.8	4302		10880	1036
22	2022		18.8	18.8	4510		11596	115
23	2023		18.8	18.8	4717	10 A A A A A A A A A A A A A A A A A A A	11398	1187
24	2024		18.8	18.8	492		12644	1262
25	2025		18.8	18.8	5132		12044	1317
26	2026		18.8	18.8	5339		13192	137
27	2027		18.8	18.8	5547		14341	1432
28	2028		18.8	18.8	5754		14341	1470
29	2029		18.8	18.8	5962	1	7783	289
30	2030	-21185	5 9.4	-21176	3085	• 4098	1785	207
	TOTAL	4127	563	41834	95490) 149264	244753.539	2029

TABLE A.10-3 COST BENEFIT CASH FLOWS (ROUTE-C)

A.10 - 3

Note A.11.1 PRELIMINARY DESIGN OF SUPER STRUCTURE

A11.1.1 GENERAL

In this preliminary design, structural analysis was done based on the following layouts;

- Structural frame of one box concrete box girder with sliding bearings on both ends, sliding hinges on each other spans and three span continuous Extradosed portion. (See the Figure of main frame and adopted model for analysis.)
- Piers and Pile caps are considered as parts of main frame.
- Pile foundations are considered as a part of main frame and they are converted to elastic resistance for vertical and horizontal movement, and rotating.
- Stay cables for Extradosed structure are covered by elastic protection materials for anti-corrosion.

A11.1.2 STRUCTURAL ANALYSIS

(1) STRUCTURAL TYPE AND SPAN ARRANGEMENT

Structural layout, structural type and span arrangement, of the Pakse Bridge is as follows;

- Thirteen span continuous prestressed concrete box girder bridge with central sliding hinges and extradosed box girder portion.
 - Between A1 and P10, nine(9) span continuous PC box girder with rigidly connected
 - piers and central sliding hinges on each other span.
 - Span arrangement : 70 + 9@ 102 = 988 m.
- Between P10 and P13(and A2), three(3) span continuous Extradosed PC box girder
- with rigidly connected piers and supporting towers for stay cables on P11 and P12.

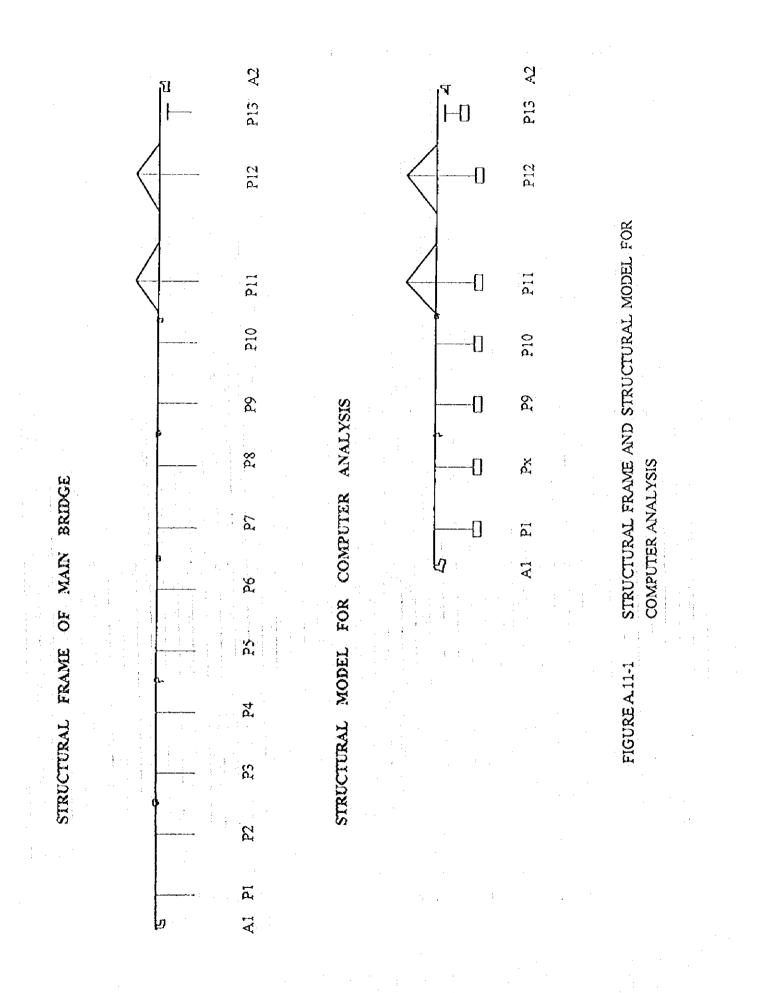
Span arrangement : 102 + 150 + 100 + (40) = 392 m. Main frame is shown in Figure A11-1.

(2) STRUCTURAL MODEL FOR COMPUTER ANALYSIS

The structural model for computer analysis was established based on the following conceptions;

- Full size model is necessary for Extradosed PC box girder portion including end side span of 40 m., P13 to A1.
- Four(4) span model of PC box girder box portion could represent the full size structure of ninc(9) span continuous PC box girder.

The frame model for computer analysis is also shown in Figure A.11-1.



(3) DESIGN CRITERIA

The design criteria were established based on the preliminary survey and study on traffic conditions in the project area and design criteria for relevant projects in Laos and other countries.

- Loading Conditions (i)
- -

	Dead Loads		
	Reinforced Concrete	e : 2,50 t/m	3
	Plain concrete	: 2.30 t/m	3
	(for pavement)		
	Live Loads		
•	Lane Load	25 ton / vehicle	
	Uniform Load(1)	1.00t/m2	in 5.50 m. width,for Bending M.
		0.50 t/m2	in 2.50 m, width.
		1.20 t/m2	in 5.50 m. width, for Sharing F.
		0.35 t/m2	on Sidewalk for Bending and Sharing.
	Uniform Load(2)	0.35 t/m2	in 5.50 m. width,
		0.175 t/m2	in 2.50 m. width.
	Impact	i = 10 / (25 + L)	
	Other Loads		
	The following loads	s are considered in	the design;
	1) Effect due to t	lemperature changi	ng (Thermal Effect),
	2) Effects due to	creep and shrinkay	ge of concrete,
	3) Seismic Load	(Effect due to Ear	thquakc),
	4) Wind load.		
	In actual design, effe	cts of 1) and 2) are	e estimated together with Dead Load as a part
	of it.		

kg/ cm2

kg/cm2

350

240

(ii) Materials

Concrete

-

- 1) Prestressed Concrete
- 2) Reinforced Concrete

Reinforcing Steel

<u>.</u>		Ultimate Strength / Force	Yield Strength / Force
Stay Cab	ole	kg/mm2 ton/cab.	kg/mm2_ton/cab.
Multi Strands	27-T15.2	190/718.2	160/610.2
Main Cal	ble		
Multi Strands	12-T12.7	190/22.4	160 / 190.8
Transversal	Cable		
Multi Cable	12-Φ8	160/96.6	140/84.6
Share B	ar		
PC Bar	φ26	120/63.7	95 / 50.4

(iii) MAJOR DIMENSIONS OF BOX GIRDER

SECTION	GIRDER	WIDTH	WIDTH	DEPTH	DEPTH
	DEPTH	of Box	of Web	of Btm. Slab	of Up. Slab
A1	3.00	6.50	0.60	0.50	0.30
Span Center	3.00	6.50	0.40	0.25	0.30
P1 to P10	6.50	6.50	0.60	1.00	0.30
Span Center	3.00	6.50	0.40	0.25	0.30
P11&P12	6.50	6.50	0.60	1.00	0.30
Span Center	3.00	6.50	0.40	0.25	0.30
P13	3.00	6.50	0.60	1.00	0.30
Span Center	3.00	6.50	0.40	0.25	0.30
A2	3.00	6.50	0.60	0.50	0.30
1					

Towers for Extradosed spans:

a b h

Dimension of Tower: 1.00 x 3.00 x 13.00 m. (P11 & P12)

(4) RESULTS OF ANALYSIS

(i) Moment and Deflection Diagram

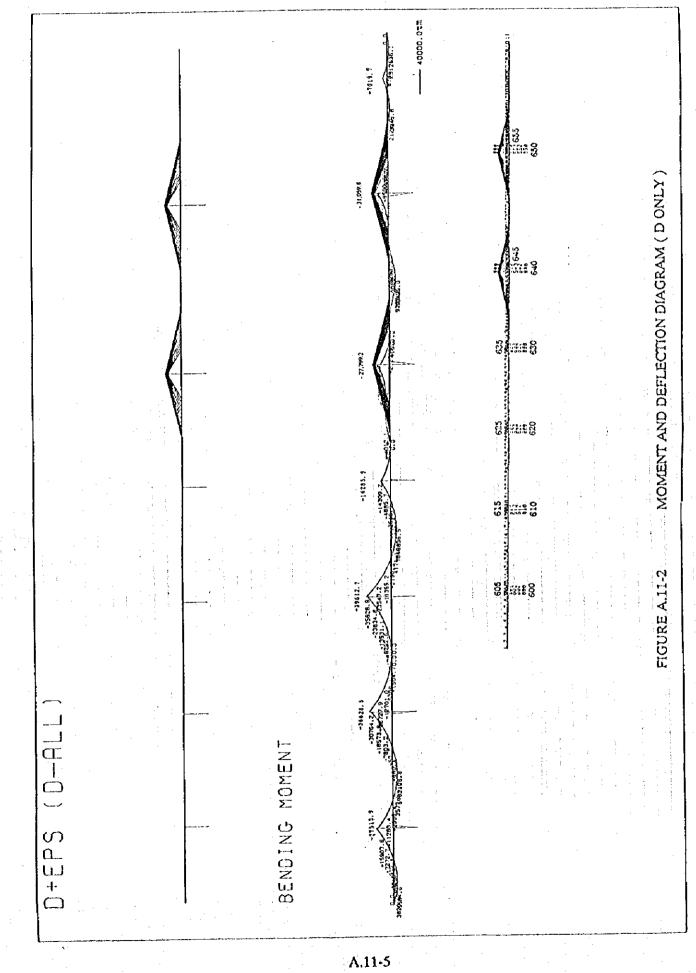
The results of structural analysis are summarized in the Figure A11-2, A11-3 and A11-4, as Moment Diagrams and Deflection Diagrams for three(3) loading conditions;

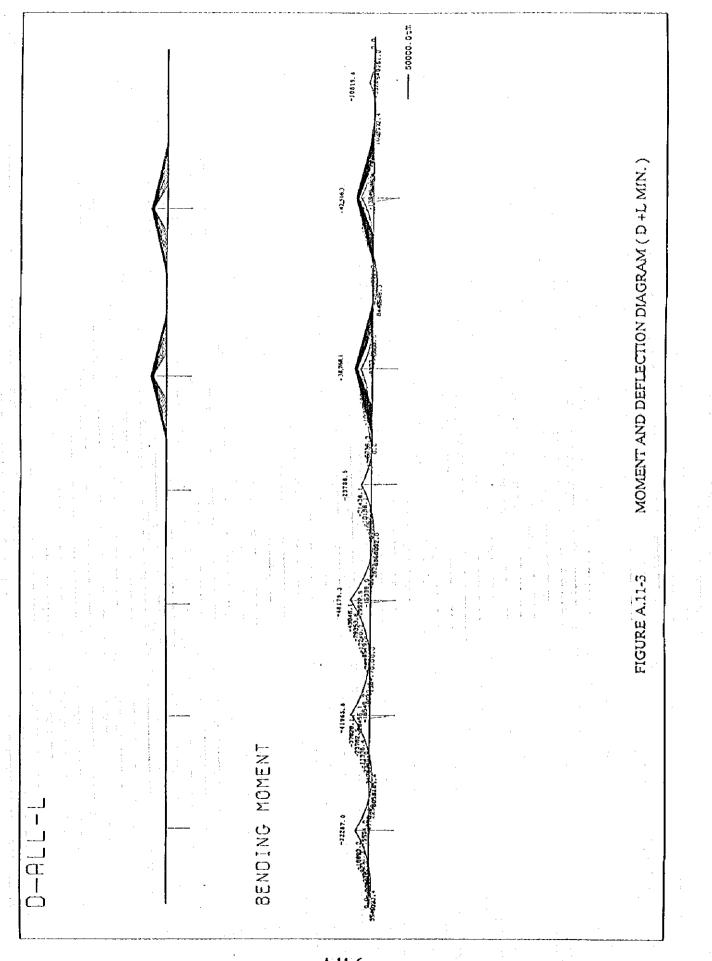
Dead Load only,

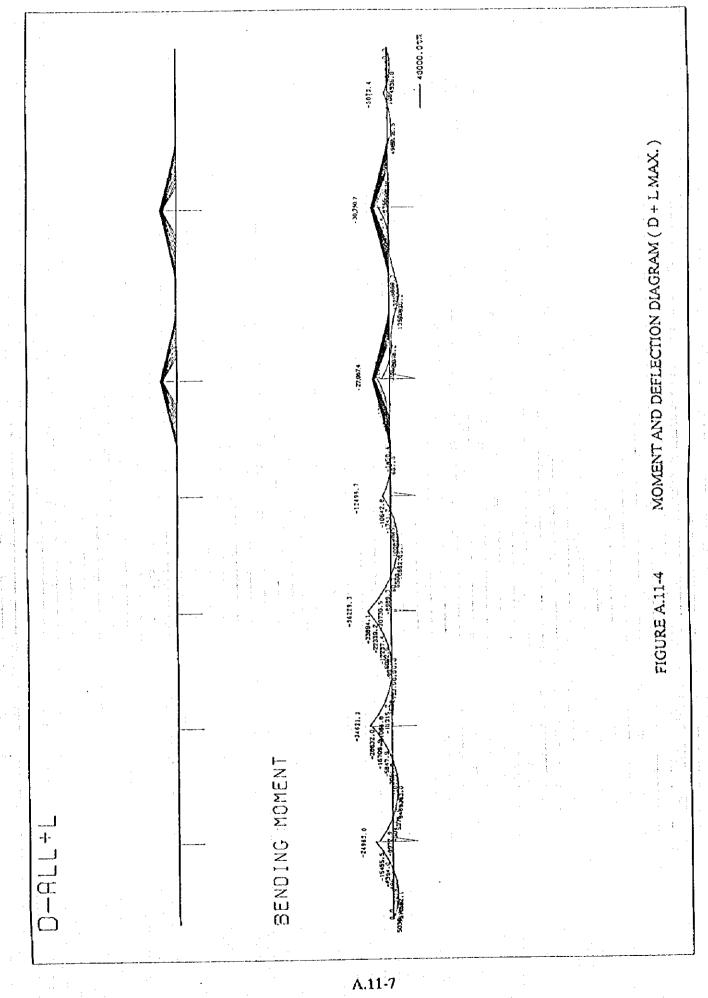
Dead Load and Live Load(only for negative moment portion)

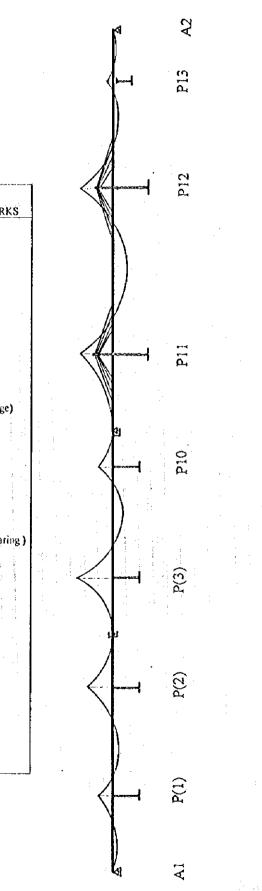
- Dead Load and Live Load (only for positive moment portion)

The summarized figures of estimated Bending Moments on pier top and span center are in Table A11-1.









	BE	NDING MOM	ENTS (ton.m.)	
	D (only)	D+L(M-)	D+L(M+)	REMARK
AL	•••••	·		
mid	5,385	5,023	7,562	
P(1)	- 27,513	- 32,287	- 24,963	
mid	7,129	6,185	9,353	
P(2)	- 36,629	- 41,966	- 34,621	
mið.		 	•	(slid hinge)
P(3)	- 39,613	- 48,179	- 36,229	
miđ.	8,836	7,092	11,716	
P10	- 16,286	- 23,789	- 12,499	
mid				(sld bearin
PH	- 27,799	- 38,768	- 27,067	
mid.	10,425	9,549	14,820	
P1 2	- 31.060	- 42,516	- 30,751	
mid.	3,246	2,772	5,179	
> P13	- 7,020	- 10,820	- 5,073	
mid		·		
A2			•	

(iii) Arrangement of PC Steels

[PC Box Girder]

Main Cables

Pier Top98 strands of 12-T12.7Span Center24 strands of 12-T12.7

[Extradosed PC Box Girder]

Stay Cables

Nine(9) strands of 27-T15.2 on each side of Box Girder, 18 strands in total.

Maximum working force : 354 tons / stay cable Allowable tensile force : 430 tons / stay cable

** Maximum working force on stay cables are shown in Table A.11-2.

Main Cables

Pier Top Span Center 86 strands of 12-T12.7 32 strands of 12-T12.7

Arrangement of Main Cables at Pier Top and Span Center on PC Box and Extradosed PC Box Girder are shown in Figure A11-5 & A11-6.

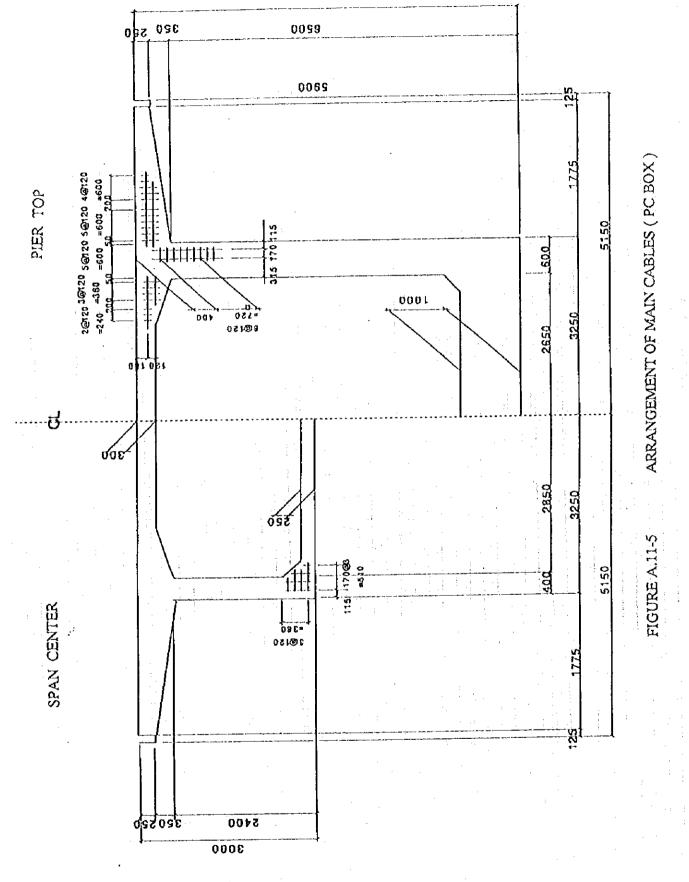
TABLE A.11-2 MAXIMUM WORKING FORCE ON STAY CABLES

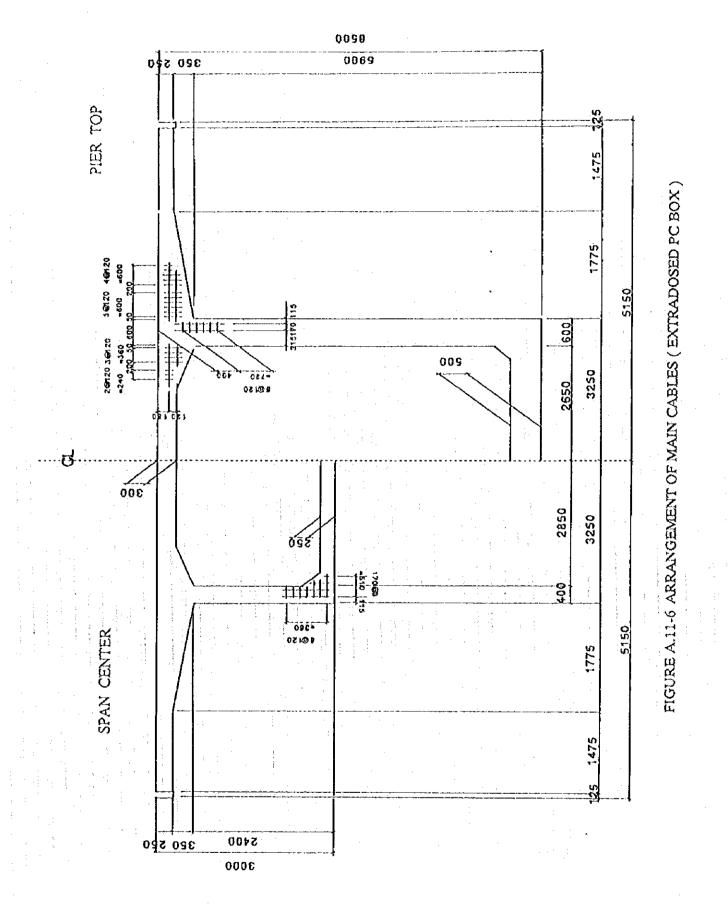
	D+EPS	L-MAX	L-MIN	D+EPS+LMAX	D+EPS+LMIN
Cl	670	38	-13	708	657
<u>C2</u>	670	36	-11	706	659
<u>C3</u>	670	34	-9	704	661
C4	670	32	-7	702	663
C5	670	31	-6	701	664
<u>C6</u>	670	30	-6	700	664
C7	670	28	-5	698	665
<u>C8</u>	670	27	-5	697	665
<u>C9</u>	670	26	-5	696	665
<u>C10</u>	670	35	-5	705	658
C11	670	35	-11	705	659
C12	670	- 35	-10	705	660
C13	670	35	-9	705	661
<u>C14</u>	670	34	-8	704	662
<u>C15</u>	670	33	-7	703	663
C16	670	32	-6	702	664
C17	670	31	-6	701	664
<u>C18</u>	670	30	-5	700	665
<u>C19</u>	670	36	-9	706	661
C20	670	35	-8	705	662
C21	670	35	-7	705	663
C22	670	35	-7	705	663
C23	670	34	-6	704	664
C24	670	33	-5	703	665
C25	670	32	-4	702	666
C26	670	31	-4	701	666
C27	670	30	-3	700	667
C28	670	34	-9	704	661
<u>C29</u>	670	33	-7	703	663
<u>C30</u>	670	32	-5	702	665
C31	670	31	-4	701	666
<u>C32</u>	670	30	-4	700	666
C33	670	-29	-3	699	667
<u>C34</u>	670	29	-3	699	667
C35	670	28	-3	698	667
<u>C36</u>	670	27	-3	697	667

(tons per two stay cables --- 27 - T15.2)

Allowable Tensile Force per two Stay Cables 0.6 Pu = 0.6 x 718.2 x 2 = 861.84 0.75 Py = 0.75 x 610.2 x 2 = 915.3

Pa = 0.6 Pu = 861.84 tf





Note A.11.2 PRELIMINARY DESIGN OF SUB-STRUCTURE

A11.2.1 SELECTED MODELS FOR PRELIMINARY DESIGN

The models for Preliminary Design of Sub-structure were selected based on similarity of pier heights, pile length, soil conditions and loading conditions due to upper structure (main frame).

The selected models and the represented groups are as follows;

Selected	Al	P2	P9	P10	P11	P12
Model Represented	Al	P1 - P5	P6 - P9	P10	P11	P12
Group						

P13 and A2 are minor structures and are not difficult to decide dimensions and estimate quantities for cost estimation, therefore they are out of the structural analysis in this stage.

A11.2.2 LOADING DUE TO SUPER STRUCTURE(MAIN FRAME)

Sub-structures, piers, pile caps and pile foundations were designed for the specified loading conditions based on the specified Design Standards.

The considered loading conditions are as follows;

- Déad loads
- Live loads
- Effects of Earthquake(Seismic loads)

Effects of Temperature changing

- Effects of Shrinkage and Creep of concrete members
- Pressure due to river current

Structural analysis of main frame were conducted using computer and summarized in the specified combinations of loading, as follows;

(Case - 1)	Due to Dead Loads, Shrinkage and Creep,(D)
(Case - 2)	Due to Dead Loads and Live Loads,(D+L)
(Case - 3)	Due to $(D + L)$ and Temperature Changing, $(D + L + T)$
(Case - 4)	Due to (D) and Effects of Earthquake,(D+E)
(Case - 5)	Due to $(D + L)$ and Pressure due to River Current, $(D+L+R)$

The results are shown in Table A11-3.

TABLE A11-3 LOADING FOR PRELIMINARY DESIGN

Loa	idings	Δ1	ľ²2	P9	P10	P11	P12	Remarks
	Vertical Load (N)	1699	4580	4678	4236	9950	10247	:
Ð	Horizontal	· ·						••••••••••••••••••••••••••••••••••••••
only,	Load (H) Bending	162.3	287.0	153.0	233.0	312.0	214.8	· · · ·
	Moment(M)	350.8	0.0	3.0	10.0	15.0	12.0	
	Vertical							
D+L	Load (N) Horizontal	1918	5151	5217	5037	10907	11203	
	Load (H)	162.6	20.0	233.0	153.0	25.0	312.0	: :
	Bending			:				
: . 	Moment(M)	350.8	3.0	0.0	1.0	6.0	3,0	·
	Vertical							· · ·
	Load (N)	1652	4644	4676	4448	10051	10327	
D + E	Horizontal		-					1
	Load (H)	257.2	165.0	78.0	92.7	214.8	214.8	
	Bending							
· · ·	Moment(M)	798.7	47.2	47.2	69.6	91.0	87.9	

CALCULATION OF BEARING CAPACITIES PILE FOUNDATION A11.2.3

Bearing capacities of the pile foundations of the proposed bridge were estimated based on the "SPECIFICATIONS FOR HIGHWAY BRIDGES, Part VI : Specifications for Substructures " issued by the Japan Road Association.

(1) Soil Conditions

The surveyed soil conditions are as follows;

- Bearing layer is rock layers of sand stone or mud stone.
- They are covered by common soil of sand and/ or silty sand in 3 to 8 meter depth.
- The planned piling method is rock drilling oiling method for cast-in-situ reinforced concrete pile foundation.
- The planned location of pile tip is at fresh rock layer, 3 meter drilled in rock layer from top of rock layer.

The results of Geotechnical Survey, conducted by the JICA Study Team for the Pakse Bridge Project, show the followings;

- Three(3) core borings were conducted with 15 to 30 meter length in total, in river.
- Depth of the surveyed soil and rock layers are as follows;

	(Soil)	(Rock)	(Totaĺ)	: 1:
(B-3)	10.50	19.75	30.25	m.
(B-4)	10.80	5.00	15,80	m.
(B-5)	15.78	4.35	20.13	m.

Uniaxial Compressive Strength

		a second a second s
(B-3)	Sandstone	55.07 M.Pa
· · ·	Mudstone	43.02 M.Pa.
· · ·	Mudstone	34.57 M.Pa.

- (2) Design Criteria and Formula used
- Design Criteria (i)
 - Ultimate bearing capacity

qd = 3 qu

(where)

qu: Uniaxial Compressive Strength in Laboratory Test Considering the data of the Laboratory Tests, 34.57 to 55.07 M.Pa., and applicable capacity of Rock Drilling Machine, 272 kg/cm2

adopted qu for deign :

(ii) Formula used

Ra = r/n + (Ru - Ws) + Ws - W(where) r : Revision Factor 1.00 n : Safety Ratio

Ru : Ultimate Bearing Capacity

1

f

Ru = qd x A + U lx f

qd : Ultimate Bearing Strength of Bearing Layer, assumed as

equivalent to very hard Stiff Clay,

qd = 3 x qu = 3 x 272.0 = -816.0 (Vm2)

A : Sectional Area of Pile Tip $O 1.50 = 1.767 \text{ m}^2$

U : Perimeter of Pile

: Length of embedment of pile on each soil layer

: Coefficient of friction due to soil

Sandy soil f = 0.5 N (N < 20)

Silty soil f = C or N (N < 15)

Ws : Effective Weight of soil to be converted by RC Pile

W : Effective Weight of RC Pile

(3) Estimated Pile Bearing Capacities

The whole pile foundations in river portion were categorized into 5 categories, P2 group of P1 to P5, P9 group of P6 to P9, P10, P11 and P12, due to it's length and soil conditions.

And pile bearing capacities were estimated for these 5 model piers and A1, 6 models in total.

The results of estimations are summarized in the Table, shown below.

	Al	P2	P9	P10	P11	P12
Depth of Soil Layer (m)				1		· · · · · · · · · · · · · · · · · · ·
Sandy Soil	2.50	5.00	6.00	1.50	0.50	•••
Silty Soil	10.50	` i		8.50	12.00	',
Rock (weathered)	2.00	3.00	3.00	2.00	2.00	13.00
Ru (ton / pile)	2,454	2,088	2,290	2,502	2,785	2,667
Ra (Design Loading)	796	684	750	815	907	870
Ra (Scismic Loading)	1,200	1,030	1,129	1,228	1,367	1,311

Note A.11.3 PRELIMINARY DESIGN OF APPROACH ROAD

TABLE A.11-4

HORIZONTAL ALIGNMENT OF PROPOSED ROUTE

BP		0+ 0.000	0	579.259	1,672,198.000	8,587,630.000
IA.1						
		Station	Cumulative	Intermed.	Northing	Easting
KA		0+579.259	579.259	100.000	1,671,618.741	8,587,630.000
BC	1	0+679.259	679.259	35.857	1,671,518.897	8,587,625.838
EC	1	0+715.115	715.115	100.000	1,671,483,569	8,587,619.780
KE	1	0+815.115	815.115	1,138.527	1,671,388.042	8,587,590.441
		A=200.000	tau= 7.0943	IP=	1,671,552.020	8,587,630.000
		R=400.000	IA= 5.0810	IP=	1,671,501.097	8,587,623.601
<u> </u>		A=200.000	tau = 7.0943	IP=	1,671,450.952	8,587,612.670
IA.2					Northing	Easting
		Station	Cumulative	Intermed.	1,670,314.554	8,587,211.142
KA 👘	2	1+953.642	1953.642	100.000		8,587,173.955
BC		2+ 53.642	2053.642	392.462	1,670,221.800	8,586,866.232
EC	2	2+446.104	2446.104	100.000	the second se	8,586,766.388
KE	2	2+546.104	2546.104	863.339	1,670,000.000	0,000,700.000
		A=200.000	tau= 7.0943	IP=	1,670,251.644	8,587,188.914
		R=400.000	IA=56.1258	1P=	1,670,030.799	8,587,078.21
		A=200.000	tau= 7.0943	IP=	1,670,000.000	8,586,833.11
		·				
ĨÀ.3		Station	Cumulative	Intermed.	Northing	Easting
KA	3	3+409.443	3409.443	100.000		8,585,903.05
BC	3	3+509.443	3509.443	81.821		8,585,803.20
EC	3	3+591.264	3591.264	100.000	1,670,022.566	8,585,723.62
KE	3	3+691.264	3691.264	719.717	1,670,062.664	8,585,632.09
	<u> </u>					
		A=200.000	tau= 7.0943	IP=	1,670,000.000	8,585,836.32
		R=400.000	IA=11.4312	IP=	1,670,009.280	8,585,762.47
		A=200.000	tau= 7.0943	IP=	1,670,033.370	8,585,692.04
	<u> </u>					
EP		4+410.981	4410.981		1,670,378.664	8,584,985.46

VERTICAL ALIGNMENT OF PROPOSED ROUTE (1/3)

TABLE A.11-5

Station	IP.Elev.	VCL	Inter.	Grade %
0.000	101.75	0.000	400.000	0.300
400.000	102.95	200.000	300.000	3.000
700.000	111.95	400.000	650.000	0.346
1350.000	114.20	400.000	1350.000	-0.900
2700.000	102.05	200.000	550.000	0.300
3250.000	103.70	200.000	600.000	-0.300
3850.000	101.90	200.000	300.000	0.300
4150.000	102.80	200.000	260.980	-0.307
4410.980	102.00	0.000		

Super Elevation

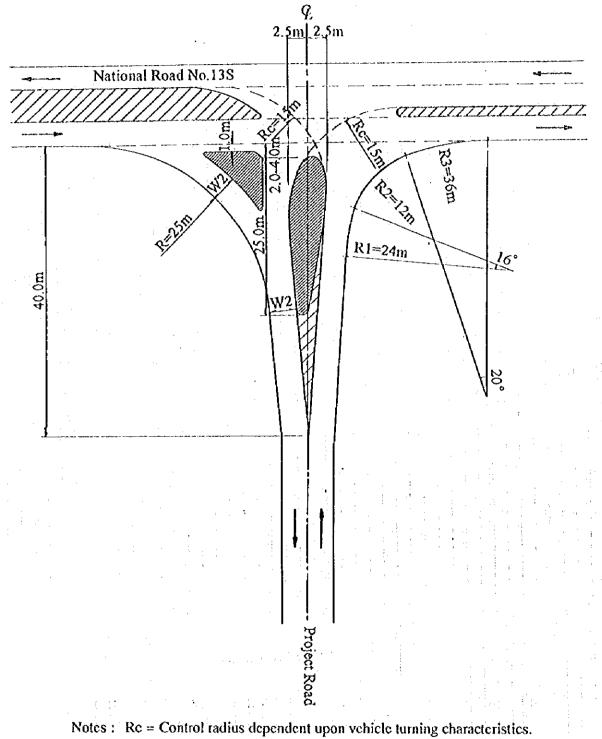
Station	P.H.	Left	Right	G.H.
0.000	101.75	3.000	-3.000	101.01
50.000	101.90	3.000	-3.000	100.27
100.000	102.05	3.000	-3.000	100.04
150.000	102.20	3.000	-3.000	98.56
200.000	102.35	3.000	-3.000	97.95
250.000	102.50	3.000	-3.000	97.61
300.000	102.65	3.000	-3.000	98.62
350.000	102.97	3.000	-3.000	100.00
400.000	103.63	3.000	-3.000	101.29
450.000	104.62	3.000	-3.000	101.66
500.000	105.95	3.000	-3.000	104.38
550.000	107.37	3.000	-3.000	108.89
579,260	108.12	3.000	-3.000	110.82
600.000	108.62	1.405	-3.000	111.64
650.000	109.70	-2.442	-3.000	110.39
679.260	110.26	-7.000	-7.000	112.58
700.000	110.62	-7.000	-7.000	108.71
715.120	110.87	-7.000	-7.000	103.43
750.000	111.38	-1.593	-2.000	91.72
800.000	111.96	1.166	-2.000	86.54
815.120	112.11	2.000	-2.000	84.16
850.000	112.39	2.000	-2.000	83.43
900.000	112.64	2.000	-2.000	84.57
950.000	112.82	2.000	-2.000	85.00
1000.000	112.99	2.000	-2.000	84.72
1050.000	113.16	2.000	-2.000	84.40
1100.000	113.34	2.000	-2.000	83.95
1150.000	113.51	2.000	-2.000	83.13
1200.000	113.64	2.000	-2.000	82.63
1250,000	113.70	2.000	-2.000	82.75
1300.000	113.68	2.000	-2.000	83.41
1350.000	113.58	2.000	-2.000	83.02
1400.000	113.40	2.000	-2.000	81.91
1450.000	113.14	2.000	-2.000	81.87

VERTICAL ALIGNMENT OF PROPOSED ROUTE (2/3)

		Super E	levation	
Station	P.H.	Left	Right	G.H.
1500.000	112.81	2.000	-2.000	81.88
1550.000	112.40	2.000	-2.000	81.52
1600.000	111.95	2.000	-2.000	80.70
1650.000	111.50	2.000	-2.000	79.97
1700.000	111.05	2.000	-2.000	78.74
1750.000	110.60	2.000	-2.000	76.49
1800.000	110.15	2.000	-2.000	75.45
1850.000	109.70	2.000	-2.000	72.56
1900.000	109.25	2.000	-2.000	73.57
1950.000	108.80	2.000	-2.000	80.25
1953.640	108.77	2.000	-2.000	80.81
2000.000	108.35	-0.558	-2.000	98.03
2050.000	107.90	-6.338	-6.338	101.88
2053.640	107.87	-7.000	-7.000	101.82
	107.45	-7.000	-7.000	104.50
2100.000	107.00	-7.000	-7.000	105.15
2150.000	106.55	-7.000	-7.000	109.22
2200.000	106.35	-7.000	-7.000	110.11
2250.000	105.65	-7.000	-7.000	111.66
2300.000	the second s	-7.000	-7.000	109.78
2350.000	105.20	-7.000	-7.000	107.25
2400.000	104.75		-7.000	105.63
2446.100	104.34	-7.000 -6.291	-6.291	105.43
2450.000	104.30		-3.000	102.24
2500.000	103.85	-0.546	-3.000	98.32
2546.100	103.44	3.000	-3.000	97.96
2550.000	103.40	3.000		96.53
2600.000	102.95	3.000	-3.000	96.94
2650.000	102.58	3.000	-3.000	90.94
2700.000	102.35	3.000	-3,000	96.13
2750.000	102.28	3.000	-3.000	
2800.000	102.35	3.000	-3.000	97.06
2850.000	102.50	3.000	-3.000	97.69
2900.000	102.65	3.000	-3.000	98.14
2950.000	102.80	3.000	-3.000	98.41
3000.000	102.95	3.000	-3.000	98.65
3050.000	103.10	3.000	-3.000	98.64
3100.000	103.25	3.000	-3.000	98.88
3150.000	103.40	3,000	-3.000	98.89
3200.000	103.51	3.000	-3.000	98.98
3250.000	103.55	3.000	-3.000	99.24
3300.000	103.51	3.000	-3.000	99.61
3350.000	103.40	3.000	-3.000	99.75
3400.000	103.25	3.000	-3,000	100.02
3409.440	103.22	3.000	-3.000	100.10
3450.000	103.10	-0.120	-3.000	100.48
3500.000	102.95	-5.284	-5.284	100.65

VERTICAL ALIGNMENT OF PROPOSED ROUTE (3/3)

		Super Elevation						
Station	P.H.	Left	Right	G.H.				
3509.440	102.92	-7.000	-7.000	100.68				
3550.000	102.80	-7.000	-7.000	100.92				
3591.260	102.68	-7.000	-7.000	100.75				
3600.000	102.65	-5.411	-5.411	100.74				
3650.000	102.50	-0.174	-3.000	100.49				
3691.260	102.38	3.000	-3.000	100.22				
3700.000	102.35	3.000	-3.000	100.18				
3750.000	102.20	3.000	-3.000	100.17				
3800.000	102.09	3.000	-3.000	98.78				
3850.000	102.05	3.000	-3.000	92.01				
3900.000	102.09	3.000	-3.000	93.40				
3950.000	102.20	3.000	-3.000	94.03				
4000.000	102.35	3.000	-3.000	97.78				
4050.000	102.50	3.000	-3.000	98.64				
4100.000	102.61	3.000	-3.000	98.84				
4150.000	102.65	3.000	-3.000	99.00				
4200.000	102.61	3.000	-3.000	97.50				
4250.000	102.49	3.000	-3.000	99.27				
4300.000	102.34	3.000	-3.000	99.61				
4350.000	102.19	3.000	-3.000	98.12				
4400.000	102.03	3.000	-3.000	97.91				
4410.980	102.00	3.000	-3.000	98.38				



Recommended value = 15 m.
The ratio R1 : R2 : R3 to be 2 : 1 :3. R2 = 12 m is recommended.
W1 = The Approach Road lane width, 3.5 m.

W2 = 5.5 m (exclude offset to raised kerbs)

FIGURE A.11-7

INTERSECTION WITH NR 13S

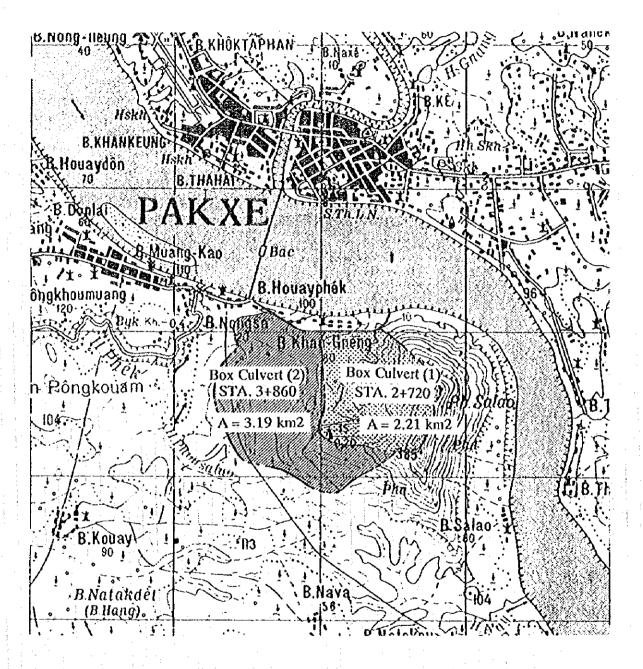


FIGURE A.11-8

CATCHMENT AREA OF BOX CULVERTS

Box Culvert (1): STA. 2+720

Discharge

$Qd = 0.278 \times C \times I \times A$

Rational Formula

where

Qd: Discharge (m3/sec)			
C: Runoff Coefficient :	c1 = 0.80 (69%)	÷	
	c2 = 0.70(31%)	Total	C = 0.769
I: Return Period of Rainfall	Intensity :		I = 12.00 cm/hr
(25 years, 30 min. durati		· .	
A : Catchment Area :	a1 = 1.53 km2		
	a2 = 0.68 km2	Total	A = 2.21 km2

Qd = 56.7 m3/sec

Runoff Capacity of Box Culvert

 $Qc = K \times A \times R^{2/3} \times S^{1/2}$

Manning's Formula

OK

where

Qc: Capacity (m3/sec)			2.1
K : Roughness Coefficient		K = 60	
A: Cross-sectional area of water	(m2)	A = 25 n	12
R : Hydraulic Radius		R = 0.60	
S: Longitudinal slope (%)		S = 0.30	0 %

then

 $Qc = 58.4 \text{ m}^{3/\text{sec}} > Qd = 56.7 \text{ m}^{3/\text{sec}}$

Box Culvert (2): STA. 3+860

Discharge

$Qd = 0.278 \times C \times I \times A$

Rational Formula

Formula

Manning's

K = 60A = 25 m2

R = 0.60S = 0.300 %

where

Qd: Discharge (m3/sec)			
C: Runoff Coefficient :	c1 = 0.80 (11%)		
: :	c2 = 0.70 (89%)	Total	C = 0.711
I: Return Period of Rainfall	Intensity :		I = 7.38 cm/hr
(25 years, 60 min. durat	ion)	÷ .	
A: Catchment Area:	a1 = 0.36 km2		÷* .
	a2 = 2.83 km2	Total	A = 3.19 km2

Qd = 46.5 m3/scc

Runoff Capacity of Box Culvert

 $Qc = K \times A \times R^{2/3} \times S^{1/2}$

where

Qc: Capacity (m3/scc) K : Roughness Coefficient A : Cross-sectional area of water (m2) R : Hydraulic Radius S : Longitudinal slope (%)

o . iongnuumaraioj

then

Qc = 58.4 m3/sec >	Qd= 46.5 m3/sec	OK

DISCHARGE OF ROAD SURFACE DRAINAGE (1/2)

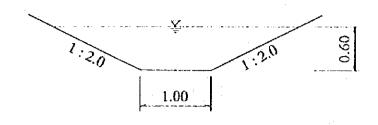
Station	Distance	Left	Area	Qf	Right	Area	Qſ	
0.000	0.00	11.0	· .		11.0			
50.000	50,00	15.2	655	0.020	19.0	750	0.02	
100.000	50.00	18.7	848	0.026	20.0	975	0.03	
150.000	50.00	17.5	905	0.027	18.5	963	0.03	
200.000	50.00	18.4	898	0.027	18.3	920	0.03	
250.000	50.00	19.0	935	0.028	18.4	918	0.03	
300.000	50.00	17.3	908	0.028	16,3	868	0.03	
350.000	50.00	16.8	853	0.026	16,0	808	0.02	
400,000	50.00	17.9	868	0,026	16.0	800	0.02	
450.000	50.00	15.5	835	0.025	14.3	758	0.02	
500.000	50.00	14.3	745	0.023	15.0	733	0.02	
550,000	50.00	16.2	763	0.023	16.6	790	0.02	
579.260	29.26	16.7	481	0.015	16.3	481	0,01	
600.000	20.74	15.8	337	0,010	15,4	329	0.01	
650.000	50.00	10.6	660	0.020	20.0	885	0.03	
679.260	29.26	13.4	351	0.011	18.6	565	0.02	
700.000	20.74			· ·	·-			
715.120	15.12	-			•			
750.000	34,88	-			-		ана стала Стала стала стала Стала стала ста	
800.000	50.00	-		÷.,				
815,120	15.12	-			19 - 1		: · .	
850.000	34.88	-			: - .			
900,000	50.00	• •			-	· · · ·		
950.000	50.00	-						1
1,000.000	50.00	-						
1,050.000	50,00	· · ·			-			
1,100.000	50.00				· -			· · · ·
1,150.000	50.00	-	1		• .	· · · ·		
1,200.000	50.00							
1,250.000	50.00	1						т. — — — — — — — — — — — — — — — — — — —
1,300.000	50.00	- 1			-			+
1,350.000	50.00				•			
1,400.000	50,00	- 1	1997 - 1 997 - 1997 -		1 · · · · · · · · · · · · · · · · · · ·			
1,450.000	50.00	-	÷ .		· · · ·	•		
1,500.000	50.00				-		х. Х	
1,550.000	50.00	-	4 T		-			
1,600.000	50.00	-						
1,650.000	50.00	· -			· -			
1,700.000	50,00	-	.*		-			
1,750.000	50.00	• •			· · ·			
1,800.000	50.00	-	· · ·		· -			•
1,850.000	50.00	-			-			÷
1,900.000	50.00		Ľ.		-			•
1,950.000	50.00	•	- 1	1	-	1		
1,953.610		-			•		· ·	
2,000.000		-			•	1 t		
2,050.000	50.00	-			• •			•
2,053.640					• • •			
2,100.000	46.36	8.0			17.5			
2,150.000		6.0	350	0.011	19.1	915	0.028	
2,200.000		4.1	253	0.008	14,3	835	0.025	н ^с

Λ.11-25

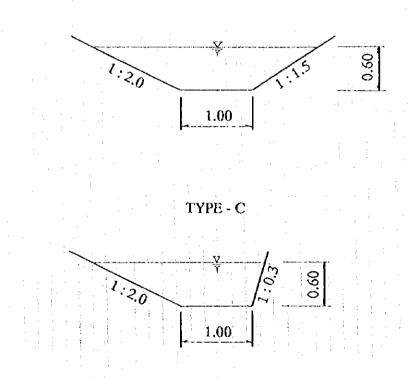
DISCHARGE OF ROAD SURFACE DRAINAGE (2/2)

Station	Distance	Left	Area	Qſ	Right	Årea	Qf
2,250.000	50.00	4.5	215	0.007	14.7	725	0.022
2,300.000	50.00	5.1	240	0.007	15.2	748	0.023
2,350.000	50.00	5,5	265	0.008	14,5	743	0.023
2,400.000	50.00	10.7	405	0.012	16.7	780	0.024
2,446.100	46.10	8.2	436	0.013	16.3	761	0.023
2,450.000	3.90	7.8	31	0.001	16.7	64	0.002
2,500.000	50,00	8.7	413	0.013	18.4	878	0.027
2,546.100	46.10	18.6	629	0.019	18.7	855	0.026
2,550.000	3.90	20.0	75	0.002	20,3	76	0.002
2,600.000	50.00	20.6	1015	0.031	19.8	1003	0.030
2,650.000	50.00	22.0	1065	0.032	18.3	953	0.029
2,700.000	50.00	21.5	1088	0.033	23.8	1053	0.032
2,750.000	50.00	21.0	1063	0.032	20.5	1108	0.034
2,800.000	50.00	22.5	1088	0.033	22.9	1085	0.033
2,850.000	50.00	18.9	1035	0.031	17.7	1015	0.031
2,900.000	50.00	19.0	948	0.029	16.7	860	0.026
2,950.000	50.00	19.0	950	0.029	17.6	858	0.026
3,000.000	50.00	19,3	958	0.029	17.2	870	0.026
3,050.000	50.00	19.0	958	0.029	16.7	848	0.026
3,100.000	50.00	19.0	950	0.029	17.6	858	0.026
3,150.000	50.00	19.3	958	0.029	17.2	870	0.026
3,200.000	50.00	19.0	958	0.029	16,5	843	0.026
3,250.000	50.00	19.6	965	0.029	16.5	825	0.025
3,300.000	50.00	19.6	980	0.030	16.8	833	0.025
3,350.000	50.00	18.6	955	0.029	15.9	818	0.025
3,400.000	50.00	17.6	905	0.027	15.1	775	0.024
3,409.440	9.44	17.8	167	0.005	15.2	143	0.004
3,450,000	40.56	12.1	606	0.018	20.7	728	0.022
3,500.000	50.00	11.3	585	0.018	20.2	1023	0.031
3,509.440	9.44	11.1	106	0.003	19.9	189	0.006
3,550.000	40.56	10.1	430	0.013	19.4	797	0.024
3,591.260	41.26	9.0	394	0.012	18.5	782	0.024
3,600.000	8.74	8.1	75	0.002	18.2	160	0.005
3,650.000	50.00	7.9	400	0.012	18.7	923	0.028
3,691.260	41.26	13.1	433	0.013	13.4	662	0.020
3,700.000	8.74	13.0	114	0.003	13.5	118	0.004
3,750.000	50.00	13.8	670	0.020	14.0	688	0.021
3,800.000	50.00	18.8	815	0.025	17.4	785	0.024
3,850.000	50.00	16.0	870	0.026	20.6	950	0.029
3,900.000	50.00	21.4	935	0.028	19.6	1005	0.030
3,950.000	50.00	21.2	1065	0.032	19.0	965	0.029
4,000.000	50.00	19.3	1013	0.031	15.3	858	0.026
4,050.000	50.00	18.4	943	0.029	16.2	788	0.024
4,100.000	50.00	17.2	890	0.027	17.9	853	0.026
4,350.000	50.00	16.2	835	0.025	18.8	918	0.028
4,200.000	50.00	21.0	930	0.028	18.1	923	0.028
4,250.000	50.00	22.0	1075	0.033	22.0	1003	0.030
4,300.000	50.00	24.0	1150	0.035	14.0	900	0.027
4,350.000	50.00	21.0	1125	0.034	12.4	660	0.020
4,400.000	50.00	17.3	958	0.029	15.2	690	0.021
4,410.980	10.98	17.3	190	0.006	14.3	162	0.005









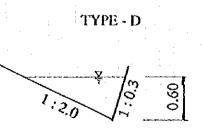


FIGURE A.11-9

TYPE OF SIDE DITCH

TABLE A.11-7SIDE DITCH RUN-OFF (1/2)

Station	Distance		Турс	Grade	Qc	Qſ	Right	Туре	Grade	Q¢	Qſ	
	** **	98.25	A	-0.005	0.792		98.25	Α	-0,005	0.792		
50,000	50.00		A	-0.005	0.792	0.020	98.00	Α	-0.005	0.792	0.023	
100.000	50.00		A	-0.005	0,792	0.026	97.75	Α	-0.005	0.792	0,030	
150,000	50.00		A	-0.005	0.792	0.027	97.50	Α	-0.005	0.792	0.029	
200.000	50.00		A	-0.005	0.792	0.027	97.25	A	-0.005	0.792	0.028	
250.000	50.00		A	0.020	0.792	0.028	97.00	A	0.000	0.792	0.028	
350.000	50.00		A	0.020	0,792	0.028	98.00	A	0.020	0.792	0.026	
400.000	50.00		A	0.020	0.792	0.026	99,00	A .	0.020	0.792	0.024	
450.000		100.00	A	0.020	0,792	0.026		A	0.020	0.792	0.024	
500.000		101.00	A A	0.040	0.792	0.025	101.00	A	0.040	0.792	0.023	
550.000		105.00	B	0.040 0.040	0.792 0.738	0.023 0.023	103.00	A	0.040	0.792	0.022	
579.260		105.00	B	0.040	0.738		105.00	B	0.040	0,738	0.024	
600.000		107.00	B	0.040	0.738		100.17	B	0.040	0,738	0.015	
650.000		109.00	B	0.040	0.738		107.00	B B	0.040	0.738	0.010	
679.260	-	108.85	B	-0.005	0.738		109.00	B	-0.005	0.738	0.027	
700.000		108.75	B	0.005	0.738	0.011	108.75	B	-0.005	0.738	0.017	
715.120	15.12	100.10	D		0.750		100.75	D		0.736		
750.000		-					_					
800,000	50.00	-					_					
815.120	15.12						_			· ·	1	
850.000		-	:			:	.		:	:		
900.000	50.00	-		•			-					
950.000	50.00	· •				đ i	· · · ·	. :			· .	
1,000.000	50.00	-					· ·	:				
1,050.000	50.00	-		· ;			-					
1,100.000	50.00	-			·	i.				·		
1,150.000	50.00	• •	i s	:	÷ .		-				•	:
1,200.000	50,00	-			¹	:		-				
1,250.000	50.00	÷. +		÷		1.1.1						
1,300.000	50.00			с. С								
1,350.000	50.00				: : : :							
1,400.000	50.00	-				, ·	-	1.1.1		:		
1,450.000	50.00	-		4		:					•	+
1,500.000	50.00	•					· -					
1,550.000	50.00					· .	-					
1,600.000	50.00 50.00	-				· .	-					
1,030.000	50,00	• •					· · · ·					•
1,750.000	50,00		· · · ·			· ·						
1,800.000	50.00					•						
1,850.000	50.00						•					
1,900.000	50.00						•					
1,950.000	50.00	_					-	. :		-		
1,953.640	3.64	-										
2,000.000	46.36	-					•				•	
2,050.000	50.00	-	,				-					
2,053.640	3.64	-					-					
2,100.000	46.36	104.80	A		2.100		• •			_		
2,150.000	50.00	105.40	A	0.012	2.100	0.011	· .				0.028	
2,200.000	50.00	106.00	С		2.028		105.00	D		0.828	0.025	:

SIDE DITCH RUN-OFF (2/2)

		1.6	Turna	Grade	Qc	Qſ	Right	Туро	Grade	Qc	Qſ
	Distance	Left	Туре С	-0.010	2.028	0.007	104.60	D	-0.008	0.828	0.022
2,250.000		105.50	c	-0.010	2.028	0.007	104.20	D	-0.008	0.828	0.023
2,300.000		105.00	C C	-0.010	2.028		103.80	D	-0.008	0.828	0.023
2,350.000		104.50 104.00	B	-0.010 -0.010	2.459	0.012	103.40	В	-0.008	0.738	0.024
2,400.000			B	-0.010	2.459		103.03	B	-0.008	0.738	0.023
2,446.100		103.54	Б В	-0.010	2.459	0.001	103.00	B	-0.008	0.738	0.002
2,450.000		103.50	A	-0.060	0.792	0.013	101.00	Ă	-0.040	0.792	0.027
2,500.000	50.00	100.50	• A	-0.060	0.792	0.019	98.00	A	-0.065	0.792	0.026
2,546.100	46.10	97.73		-0.060	0.792	0.002	97.50	A	-0.128	0.792	0.002
2,550.000	3.90	97.50	A	-0.000	0.792	0.031	97.00	A	-0.010	0.792	0.030
2,600.000	50.00	96.30	A	-0.024	0.792	0.032	-			•	0.029
2,650.000	50.00	95.80		-0.010	0.792	0.032	-			-	0.032
2,700.000	50.00	95.30	A A	0.020	0.792	0.032	95.00	Α	;	0.792	0.034
2,750.000	50.00	94.30		0.020	0.792	0.033	96.00	A	0.020	0.792	0.033
2,800.000	50.00	95.30	A	0.020	0.792	0.031	97.00	Ă	0.020	0.792	0.031
2,850.000	50.00	96.30	A	0.020	0.792	0.029	98.00	Ā		0.792	0.026
2,900.000	50.00	97.30	Å	0.003	0.792	0.029	98.14	Å	0.003	0.792	0.026
2,950.000	50.00	97.45	A	0.003	0.792	0.029	98.29	A	0.003	0.792	0.026
3,000.000	50.00	97.61	= A A	0.003	0.792	0.029	98.43	Á	0.003	0.792	0.026
3,050.000	50.00	97.76	A	0.003	0.792	0.029	98.57	A	0.003	0.792	0.026
3,100.000	50.00	97.92	A	0.003	0.792	0.029	98.71	A	0.003	0.792	0.026
3,150.000	50,00	98,07		0.003	0.792	0.029	98.86	A	0.003	0.792	0.026
3,200.000	50.00	98.23 98.38	A	0.003	0.792	0.029	99.00	A	0.003	0.792	0.025
3,250.000	50.00	98,54	· A	0.003	0.792	0.030	99.14	A	0.003	0.792	0.025
3,300.000	50.00	98.69	A	0.003	0.792	0.029	99.29	A	0.003	0.792	0.025
3,350.000	50.00	98.85	Ā	0.003	0.792	0.027	99.43	A	0.003	0 792	0.024
3,400.000	9,44	98.87	Ā	0.003	0.792	0.005	99.46	A	0.003	0.792	0.004
3,409.440	40.56	99.00	A.	0.005	0.792	0.018	99.57	· A	0.003	0.792	0.022
3,450.000 3,500.000	50.00	1		0.007	0.792	0.018	99.71	A	0.003	0.792	0.031
3,509.440	9.44	99.40	A	0.007	0.792	0.003	99.74	Α	0.003	0.792	0.006
3,550.000	40.56		A	0.007	0.792	0.013	99.86	A	0.003	0.792	0.024
3,591.260	41.26	(1) (2) (2)	. A	0,007	0.792	0.012	99.98		0.003	0.792	0.024
3,600.000	8 74	100.00	A		0.792	0.002	100.00	Α		0.792	0.005
3,650.000	50.00		A	-0.005	0.792	0.012	99.75		-0.005	0.792	0.028
3,691.260	41.26		A	-0.005	0.792	0.013	99.54	A	0.005	0.792	0.020
3,700.000	8.74			-0.005	0.792	0,003	99.50	Α	-0.005	0.792	0.004
3,750.000	50.00				0,792	0.020	99.25	A	-0.005	0.792	0.021
3,800.000	50.00				•	0.025	99.00	Α	:	0.792	0.024
3,850.000	50.00				-	0.026		н 1	1	· •	0.029
3,900.000	50.00	1			· · •	0.028	-			· -	0.030
3,950.000	50.00			-		0.032	-			•	0.029
4,000.000	50.00		Α	;	0.792	0.031	98,50	A	:	0.792	0.026
4,050.000	50.00			0.013	0.792	0.029	98.25	Α	-0.005	0.792	0.024
4,100.000	50,00			0.013	0.792	0.027	98,00	A	-0.005	0.792	0.026
4,150.000	50.00				0.792	0.025	97.75	` A'	-0.005	0.792	0.028
4,200.000	50.00			-0.006	0.792	0.028	97.50	A	-0.005	0.792	0.028
4,250.000	50.00			-0.006	0.792	0.033	97.25	A	-0.005	0.792	0.030
4,300.000	50.00				0.792	0.035	97.00	A		0.792	0.027
4,350.000				0.010	0.792	0.034	•			•	0.020
4,400.000	1 A A A A A A A A A A A A A A A A A A A			0,010	0.792	0.029) -			-	0.021
4,410.980					0.792	0.000				-	0.005
.,					5 N.				1. A.		

Safety Factor Calculation of Circular Slip Analysis

[Condition]Method :Circular Slip AnalysisStress :Total Stress AnalysisEarthquake :CommonBlock Width :2.00m

[Calculation]

Fs= s $/ \tau = \Sigma (Cu \times L + W' \times \cos \theta \times \tan \phi \times u) / \Sigma (W' \times \sin \theta)$

when;

s : Shear Resistance on Slip Surface (tf)

 τ : Shear Stress on Slip Surface (tf)

W : Total Weight of Block (tf / m)

W': Efficient Weight of Block (tf / m)

 θ : Gradient of Slip (degree)

L : Length of Slip (m)

u : Pore Water Pressure (tf / m2)

Cu : Coefficient of Total Stress (tf / m2)

 ϕ u: Angle of Internal Friction of Total Stress (degree)

[Input Data]

Total	Coordinatio	on Point :	13			:
Numb	er of Block	c:	- 3			
Coord	lination				. i	
No.	X - co	ordination	Y - co	ordination		
1		-35.000		5.500		
2		-20.400		5.800		
2 3		-18.000		6.000		•
4		-5.500		12.120)	
5		0.00		12.280)	
6		5.500)	12.120)	
. 7		16.600		6.600		
8		13.800		6.300		
9		21.000		6.800		
10)	21.000		4.500		
11		21.000		0.000		
12	1	-35.000	I	0.000		
13		-35.000		4,500		
Block	Componer	nt				
A	3	4	5	6	7	
B	1	2	3	8	9	
С	13	10	11	12		

13

8 10

Soil Constant

Block	Unit Weight	Submerged Unit Weight	Coefficient	Angle of Internal Friction
	(t/m3)	(t/m3)	(tf/m2)	(degree)
Λ	2.00		0.00	25
B	1.60		15.00	0
C	1.80		0.00	20

Coordination of Circular Center

x	-20.000 to	-11.000 m	3 division
Y	15.000 to	24.000 m	3 division

Range of Circular Radius	
Coordination Y of Maximum Radius	: 4.500 m
Coordination Y of Minimum Radius	: 4.500 m
Increase of Radius	: 0.000 m

The result of calculation (Fs = 5.273) is greater than general safety factor (Fs = 1.25).

