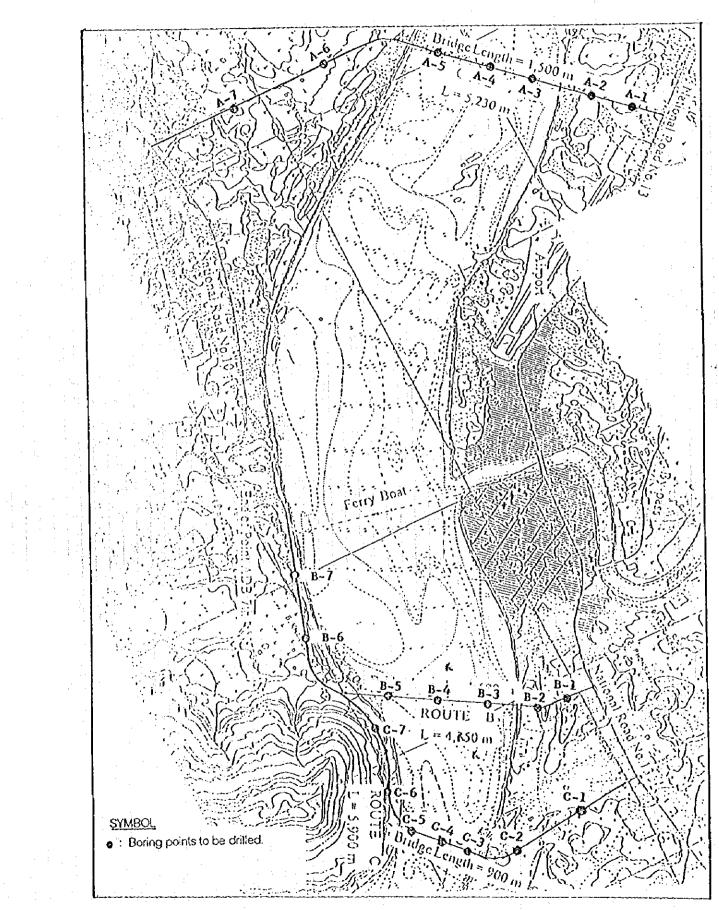
Note A.3-22 GEOLOGICAL INVESTIGATION

I. INTRODUCTION

This report presents the results of geotechnical investigation undertaken as part of the feasibility study on construction of the Mekong bridge at Pakse in Laos, which is to be carried out by The Japan International Agency. The work was consulted by Nippon Koei Co.,Ltd. and commenced by Geo-mining Enterprise. Field investigation was carried out between September to December 1995.

FIG. 1 POSITION OF BORING HOLES



2. SCOPE AND COMMENCEMENT OF THE WORK

2.1 GENERAL

The work was carried out under contract and under supervision of the Engineer. The contractor provided full technical and geological supervision to provide a drilling report containing drill logs and the results of tests.

The mobilization was began on 11/09/95 and completed preparation on 16/09/95. Inaccessible to vehicles, the work was commenced on 17/09/95 at right bank of proposed route - B and C while high water level (low river bank level) because of easier to winch up the rig to river bank and boring points. And then the work was commenced at left bank of proposed route - C and B, and proposed route - A at right bank and left bank respectively. Boring holes in the river were commenced latest. The drilling work was completed on 13/12/95.

2.2 INVESTIGATION SITES

The sites were studies on three proposed bridge route and position of boring holes as show in Fig. 1. The list of no's of boring holes are listed in the table below.

		N	umber of boring	(NOS.)	
Location	Site	Land-1	Land-2	In the river	
		(Left bank)	(Right Bank)		
A	Proposed Route-A	2	2	3	
B	Proposed Route-B	2	2	3	
С	Proposed Route-A	2	2	3	· · ·
· · · · · · · · · · · · · · · · · · ·		6	6	9	· · ·

Number of boring (Nos.)

2.3 DRILLING AND DOWN HOLE TESTING

The boring holes were carried out Standard Penetration Test in soil and fully cored in rock using double core barrel NWM with water flushing. A Tone THC-1 lightweight rig was used for the majority of holes as most locations were inaccessible to vehicles and in the river. a Russian truck-mounted rig was used for boring hole No. A-1, A-2, A-6, A-7 and B-1.

All core was logged on site and placed in wooden core boxs. All core was pliotographed in colour. Full engineering geological logs were prepared for each hole. Included on the logs are descriptions of rock type, physical characteristics, defects, strength, the result of standard penetration test, and information on ground water levels and core recovery. The HQ standard pipe was used as casing incase collapse of the bore hole.

Standard Penetration Test was carried out in accordance with test No. 19, BS 1377 : 197 using the split-barrel sampler and a self - tripping hammer. It was carried out at 1.0 m. interval at each bore hole. The holes were advanced by drag bit dia. 3" with water or bentonite slurry flushing. Samples were placed in sealed plastic bags.

Undisturbed samples were taken at bore hole No. A-2 and A-6 on the proposed route-A, proposed bore hole No. B-1 and B-2 on the proposed route-B and bore hole No. C-2 and C-6 on the propose route-C at the depth 2 metres above rock surface with thin-wall tube sampler 74 mm. dia driven by hammer. Samples were sealed by wax.

Included on the description of bore holes were summarized in Table. 1.

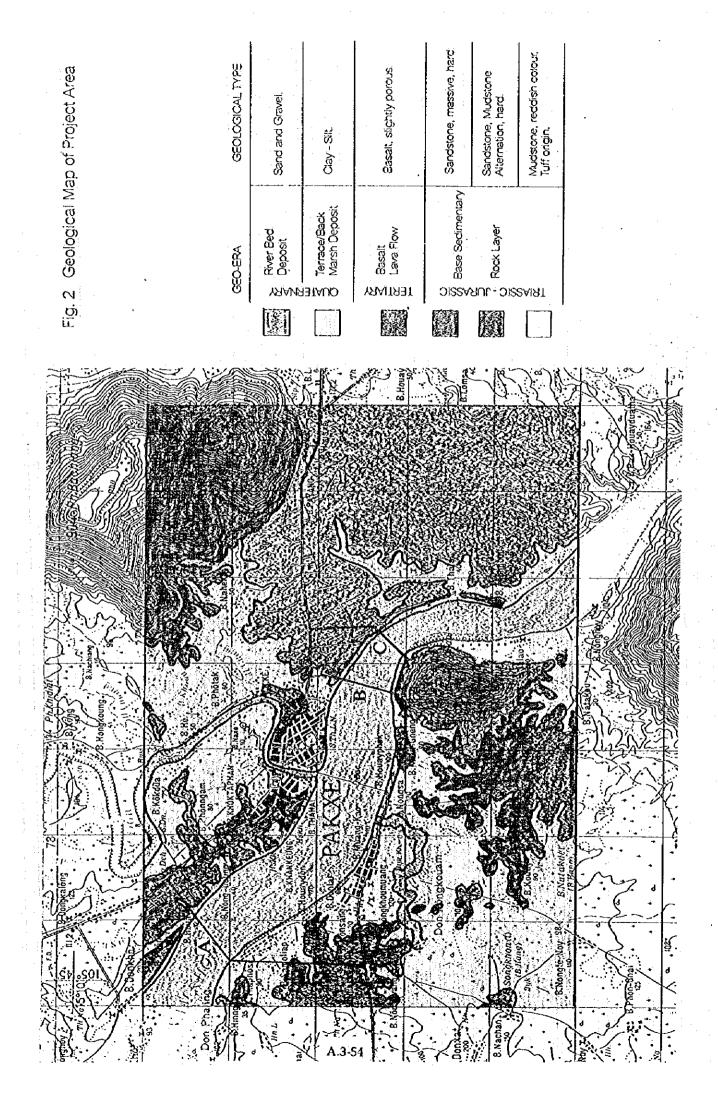
2.4 LABORATORY TESTS.

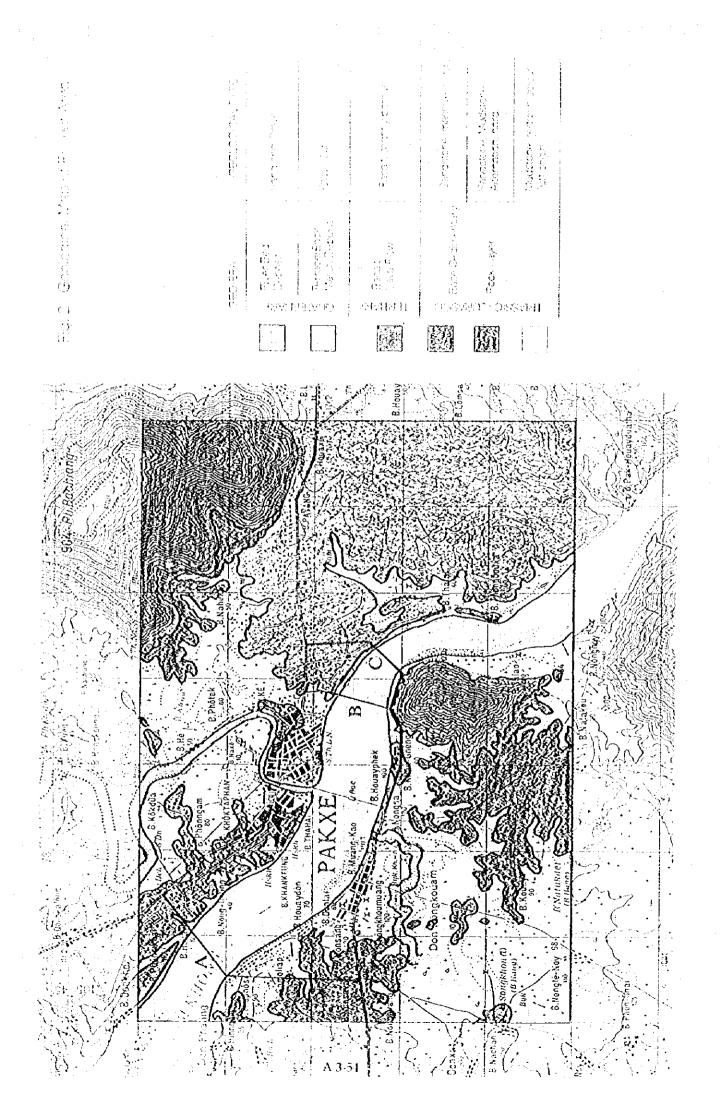
Samples from bore holes included disturbed samples from STP, undisturbed samples and core samples which selected by the Engineers were transported to Bangkok for testing at Asian Institute of Technology as soon as possible. The test types and number of laboratory tests are listed in Table 2.

						:					
				•							
Location	Hole No.	Coordinate	nate	Elevation	Drill	Drill Lenght (m)	С Эларан	Commen	Commenced Date	Water level	Remark
1		N	E	(m)	Soil	Rock	Total	Start	Complete	(m)	
	A-1	1.675.387.459	8,582,638.814	103.26	7.38	3.00	10.35	31-Oct-95	56-vov-10	3.00	On Land
	A-2	1.674,942.378	8,582,236.443	97.65	12.40	3.00	15.40	04-Nov-95	06-Nov-95	Not Record	On Land
	A-3	1.674.571.477	8,581,901.133	81.26	16.50	5.00	21.50	25-Nov-95	29-Nov-95		In The River
	A-4	1,674,274.756	8,581,632.886	83.25	3.10	5.00	8.10	24-Nov-95	24-Nov-95	-	In The River
	A-5	1.673,978.036	8,581,364.638	81.78	0.55	5.00	5.55	01-Dec-95	01-Dec-95	•	In The River
	9-A-6	1.672.884.432	8.581.050.000	96.3	4.20	3.00	7.20	28-Oct-95	29-Oct-95	Not Record	On Land
	A-7	1,671,884.432	8,581,050.000	-101.45	4.37	3.00	7.37	27-Oct-95	28-Oct-95	4.00	On Land
	B-1	1,672,020.000	8,587,700.000	56.79	2.35	3.65	6.00	- 25-Oct-95	26-Oct-95	Artificail	On Land
	B-2	1,671.621.468	8,587,683.497	110.45	15.80	3.00	18.80	20-Oct-95	24-Oct-95	00.6	On Land
	B-3	1,671,251.834	8,587,530.956	86.6	10.50	19.75	30.25	03-Nov-95	11-Nov-95	•	In The River
	B.4	1.670.883.645	8,587,374.637	81.16	10.80	5.00	15.80	13-Nov-95	15-Nov-95		In The River
	B-5	1,670,515.452	8,587,218.319	76:92	15.78	4.35	20.13	16-Nov-95	22-Nov-95	•	In The River
	B-6	1.670.030.073	8.586,895.438	105.16	00.00	3.16	3.16	30-Sep-95	30-Sep-95	1.60	On Land
	B-7	1,670,086.403	8,585,805.016	100.75	5.00	3.05	8.05	17-Sep-95	18-Sep-95	0.60	On Land
	C-1	1.671.662.178	8.588.806.619	111.34	3.00	3.05	6.05	03-Oct-95	03-Oct-95	1.60	On Land
	C-2	1,670,965.227	8.588.871.885	108.89	10.90	3.25	14.15	04-Oct-95	11-Oct-95	10.00	On Land
	C-3	1.670,440.116	8,588,663.729	16.27	7.10	5.00	12.10		-	•	In The River
	C.4	1,670,233.284	8.588,446.425	69.01	17.50	00.00	17.50			-	In The River
	C-5	1,670,032,445	8,588,224.034	78.86	1.20	5.00	6.20			•	In The River
	5 C	1.669,973.954	8,587,936.913	96.55	3.20	3.00	6.20	25-Sep-95	27-Sep-95	3.00	On Land
÷	C-7	1.670.167.390	8,587,477.964	104.32	2.00	3.00	5.00	21-Sep-95	23-Sep-95	1.20	On Lánd
1					() () ()						

Material	Test Type	Number of Test
	Atterberg Limits	9
	Specific Gravity	21
Soil	Unit Weight	2
	Water Content	21
	Grain Size Analysis	21
	Unconsolidated Undrained Triaxial Compression Test	0
Rock	One Dimensional Compression Test	10
	Elastic Modulus Analysis	2

Table 2 : Types and Number of Laboratory Tests



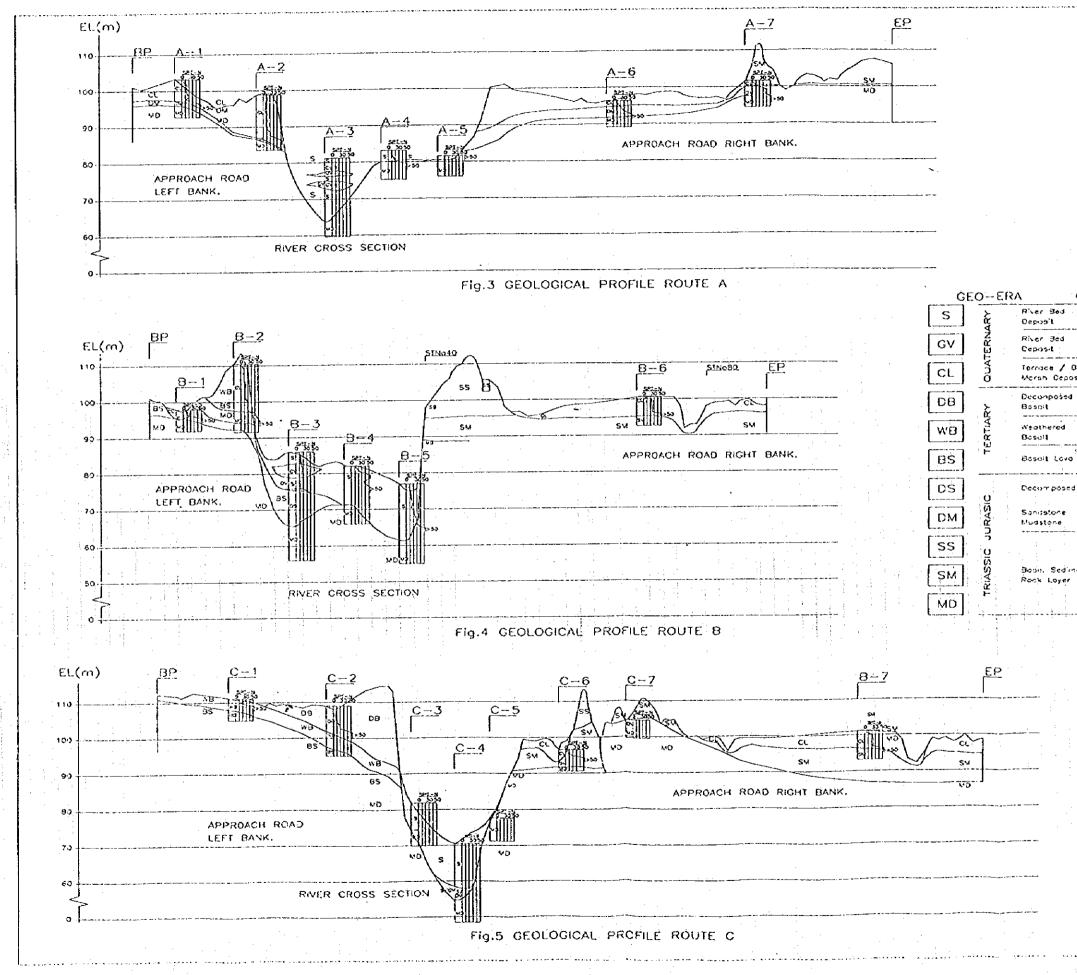


3. GEOLOGICAL SETTING

The project is located in an area dominated by terrigeneous continental and shallow marine sediment of Triassic - Jurassic Era that are mapped as Indosinias Group of Khorat Group in Thailand. The lower formations is reddish brown Mudstone with some Tuff origin widespread in low flat area that are capped by Alluvial deposit and at the river bedrock. The middle formations is Sandstone and Mudstone alternation spread in high terrain area at left and right bank of Mekong river on the north-west direction of project area. The upper formations is massive Sandstone, that characterized by high escarpments or flat- topped mountain is occurred at the small mountain which is local named "Phon Salao" on the right bank of proposed route - B and C.

The Basalt lava flow of Tertiary Era is spreaded along the left bank of proposed route - B and C with small hill or high terrain topographic feature.

Quaternary deposits are devided into two groups as : sand and gravel of river bed deposit of Mekong river and its distribution. and clay-silt of terrace and back marsh deposit spread on flat plain area in both side of Mekong River.



· ·

020	Sand, Fine to Modelium	
	Gravel. Well grain sized Large size 50-70 mm.	
Bock sit	Clay Clay-sil. Slightly solt.	a
	Origin Roca Changed Into Clay Laterite	
	Hard Clay with Iragments Rock Texture Pressarved.	а*
Floa	Basat, slighty paraus	
a j	Origin Rock Gnanged Into Elay (Laterita)	
	Vecentely firm in consistency.	
1éntáry	Sondstone massive hord Sonastate, Vudstana	
ience y	Atternétion, hard Mudstore readigh color Moderotely hard fulf Origin	
· · · · · · · · · · · · · · · · · · ·		
• •	(m) 10 5 0 100 500(m)	
		l l

4. PRESENTATION OF RESULT

4.1 GEOLOGICAL FEATURE OF STUDY SECTION

4.1.1 Proposed route - A

A cross-section along the proposed route - A and subsurface data is illustrated on Figure 3.

The subsoil on the left bank comprises of clay and silt of terrace and back marsh deposit with thickness ranging from 6 to 12 metres and underlied by Mudstone, that decomposed layer about 1 meter of thickness. On the river bed, river bed deposit consists of sand and gravel with thickness ranging from 16.50 metres at hole No. A-3 to 0.55 metre at hole No. A-5. The bed rock is Mudstone. The bed rock level is deepest at hole No. A-3 of elevation 64.76 metres and shallower at hole No. A-4 and A-5 of elevation about 80 metres. On the right bank, subsoil is clay and silt of terrace and back marsh deposit with thickness ranging from about 6 metres at the bank decrease to about 1 metres in further. The underlying bedrock is Mudstone, that decomposed layer about 3 metres of thickness. At the end of proposed route-A, 950 metres in length, is small hill and high terrain area of hard Sandstone.

4.1.2 Proposed route - B

A cross-section along the proposed route - B and subsurface data is illustrated on Figure 4.

Subsurface strata on the left bank comprises of Basalt lava flow on the river bank with rather thick decomposed layer about 13-15 metres of thickness at top hill. And weathered layer about 3 metres of thickness. The underlying layer is Mudstone, that occure on flat plain area at hole No. B-1 was capped by clay and silt of Alluvial deposit with thickness 2.35 metre. On the river bed, river bed deposit consists of sand and gravel with thickness ranging from 10 metres at hole No. A-3 and A-4 to 15 metres at hole No. A-5. On the left side of river underlied by Basalt lava flow of very high spacing fracture with thickness 10 metres. On the middle and right side of river underlied by Mudstone. Elevation of bed rock is deepest on the right side of river (hole No. B-5) 61.14 metres and shallower on the left side of river (hole No. B-3) 76.10 metres respectively. On the right bank consists of massive Sandstone at the part of Phou Saloa Mountain and clay & silt of terrace and back marsh deposit at flat plain area with thickness about 5 metres, was underlied by hard Sandstone.

4.1.3 Proposed route - C

A cross-section along the proposed route - C and subsurface data is illustrated on Figure 5.

Subsurface strata on the left bank is Basalt lava flow that rather thick decomposed layer about 18 metres on river bank and decreasing in further. On the river bed, river bed deposit consists of medium sand with gravel of thickness about 2-3 metres above bed rock. The river bed deposit is thicknest at hole No. C -4 of 17.5 metres and thiner at hole No. C-3 and C-5 respectively. On the right bank, sub-surface stratas composed of massive Sandstone at the part of Phou Salao and Sandstone-Mudstone alternation at foot of moutain. At the flat area is capped by clay-silt of terrace and back marsh deposit with thickness about 5 metres.

A.3-58

4.2 LABORATORY TEST RESULT

The laboratory testing result is summarized on Table 3.

TABLE 3 SUMMARY OF LABORATORY TEST

ft: unit weight saturated (g/cm3) PL: Plastic limit. DL: Liquid limit. 0 Trizxial Ø : Internal friction angle (°) Ö 1,034.48 1,538.16 ß Uniaxial 592.31 561.71 Ŋ 26.1 28.2 24.2 24.6 59.8 39.7 1 20 C : Coehesion (kg f/cm2). 15.8 17.8 21.1 23.2 6.0 6.5 님 59 1.87 1.98 ر 16.6 1.65 20.9 13.2 20.4 17.6 24.6 0.97 19.3 4 V ŴC 57 3 1% 2.63 2.66 2.69 2.57 2.75 2.68 2.75 2.70 2.69 2.67 SS GS: Specific Gravity. Wc: Natural water content ES : Elastic modulus (kg. f/cm2) 4,00 0.26 104 0.22 Sand & Clay D 50 ŧ (%) (%) Grain Size 8 2 F g \$ 0 88 ന 2 8 Sand (%)) ģ 8 83 8 1 5 88 4 5 Gravel 0 and the second 0 (%) 4 0 (n 0 0 o 0 : Uniaxial compressive strength (kg f/cm2). Sandy Silty Clay (CH) D 50 : Diameter (mm.) of quantity 50 %. Soil/Rock Type 2.00 - 3.50 |Silty Clay (CL) Silty-Clay-(CH) 9.00 - 10.00 Clayey Sand Sandy Clay 18.33 - 18.50 Sandstone 5.37 - 5.60 Sandstone 4.91-5.10 Mudstone Mudstone Mudstone Siltstone 14.15 - 14.30 Siltstone 5.00 - 8.00 Gravel Sand 9.00 - 13.00 Sand Clay 8.38 - 8.58 4.00 - 5.45 0.00 - 2.60 2.35 - 2.55 1.00 - 1.45 6 20 - 6 44 2.00 - 4.45 0.00 - 1.45 Depth Ê A-6 A-3 A-7 - A-2 A-6 A-3 A-3 A-4 Α7 Hole A-2 A-2 A-3 **A**4 A-5 Ā A-2 A-I őZ. Ŋ A-3-1 A-7-2 Sample A-6-1 A-6-2 A-2-2 -A-2-3 A:4-1-A-4-2 A-3-2 A-3-3 A-5-1 A-7-1 A-2-4 A-5-4 A-1-2 A-2-1 Note : A-1-1 °Z A 3-59

TABLE

3 SUMMARY OF LABORATORY TEST (Continue)

 χ t : unit weight saturated (g/cm3) PL : Plastic limit. LL : Liquid limit. Ø Triaxiai Ø : Internal friction angle (°) Ö 1.016.83 1.635.06 ВS Uniaxial 352.61 438.8 DO O 26.4 Ц 31.7 42.4 69 15.4 20.1 C: Cochesion (kg f/cm2). h 4 1% ŭ ŴC 18.6 42.6 42.8 22.2 10.0 22.4 27.7 1.22 17.4 16.0 2.21 % 2.65 2.74 2.77 2.64 2.64 2.68 2.64 2.61 2.68 \mathfrak{S} GS: Specific Gravity. Wc: Natural water content Sand & Clay D 50 ES : Elastic modulus (kg. f/cm2) 0.28 0.24 0.22 4 1 Grain Size (%) ŝ S 8 32 ---ó ----88 • -4 Sand (%) 5 2 66 S ŝ S 8 2 Ś Gravel 0-(%) 0 16 3 ò \$ ----0 ò Silty clay with sand (CL) : Uniaxial compressive strength (kg f/cm2). 11.00 - 12.00 Silty clay with gravel Soil/Rock D 50 : Diameter (mm.) of quantity 50 %. Type 1.00 - 3.45 Sandy silty clay 100 Silty Clay (CL) Silty clay (CL) Mudstone 2.10 - 2.50 Sandstone 12.24 - 12.36 Mudstone 19.25 - 19.40 Mudstone 3.00 - 7.00 - Gravel 17.31 - 17.45 Basalt Sand 1.00-3.00 Sand 1.00-4.00 Sand 3.00 - 3.30 0.50 - 1.50 1.00 - 3.00 3.00 - 3.45 1.00 - 1.45 Depth Ē Hole ы К К က်ရှိ Ч 8-2 8-2 8-2 2-2 с С 8 7 ц Ц а Х Š. Ä 4 Ч Н С 14 1-1 Ŋ Sample 1-1-1-20 B-2-2 B-1-2 B-2-1 B-3-1 B-3-2 B-3-3 B-4-2 B-5-1 B-5-2 4 B-6-1 B-7-2 °. Zo B-7-1 Note : A.3-60

TABLE

3 SUMMARY OF LABORATORY TEST (Continue)

Samile	Hoie	Denth	Soil/Rock			Grain Size							Uniaxial	a 1	Triaxial	cial
No.	o Z	(II)	Type	Gravel	Sand	Sand & Clay	D 50	GS	MC	Ĭt.	Ла		Ŋ	ES	υ	Q
				ر %)	8	(%)			P%		%	%				
E E	5	4.10 - 4.45	Baselt						0.08				497.76			
C-2-1	5 5	2.00 - 4.50	2.00 - 4.50 Silty clay with sand	15	25	60	•	2.77	40.10			i				
C-2-2	50	13.00 - 13.27 Basalt	Basalt						0.45			:	612.31			
							:		· · · · · · · · · · · · · · · · · · ·							
								-	- -							
15 0 A3	ပ်	1.00 - 2.00	Silty clay	0	10	06	*	2.63	25.6							
-61	ဗိ	4.45 - 4.63 Mudstone	Mudstone						1.87				251.23			
C-7-1	C3	3.77 - 4.00	Mudstone						1.64				583.64			
		;														
											· ·					L
											1					
					and the second se											-
													:		:	
					-						:					
Note :	D 50 :	Diameter (mm	D 50 : Diameter (mm.) of quantity 50 %. GS.	GS : Specific Gravity.	Gravity.	Wc : Natural water content	Water CO	ntent	It : unit weight saturated (g/cm3)	veight sat	urated (g	(cm3)	PL : Plastic limit.	ic limit.	LL : Lig	LL : Liquid limit.
:	: nd	Unizxial comp	Uniaxial compressive strength (kg f/cm2)	1 	ES : Ela	Elastic modulus (kg. t/cm2)	g. t/cm2)		C : Coehesion (kg t/cm2).	esion (kg	t/cm2).	Ø	Ø : Internal triction angle (7)	triction ;	angie (')	

	I. SITI				PROJE RDINATE		THE CC THE ME .675,387.459	····· - ··· ·	SRIDGE	TA : 	•••••••		L	et no.		1
]	DATE	FR	OM_31/10/9	<u>5 TO 0</u>	1/11/95			INATIO	<u>0</u> אכ אביים אכ	DRILL R DMSRI	KG	
/			e core Dvery:	1(00 %		PTH	10.380 103.260		ł	LOG			ESAK		
	DEPTH	ELEVATION	Rock Type Or Formation	CTIO			DESCRIPTIC	'n	·	BIT & DIAMETER	GROUNDWATER	& CORE & CORE		ALUE 30 40 5	SAMPLING	DEPTH
	 1	102.81 101.81	FINE SANDY CL	- //	COLOUR, CONTENI	SOFT IN , MEDIUI	T, ORANGISH Y I CONSISTENC' M PLASTICITY. T, REDDISH BR	(HIGH WATI	0.45 M. ER 1.45 M.	-						1
	2.						TIFF IN CONSIS , MEDIUM PLAS				3.00					2
06/01/15	4		CLAY				, ORANGISH BF TO VERY STIFF			DRAG BIT 3					A1-1	3
	5 _				MEDIUMW	AJER CO	NTENT, MEDIU	M PLASTICIT	Y.							- - 5
	6_ 7_	97.06	SILTY CLAY		INTO SOIL, STIFF IN CO	REDDISH DNS!STEI	DISTONE, ORIGI H BROWN IN CO NCY, MEDIUM V	LOUR, VER	r Ent,							- 6 - 7
	8_	95.88			SLIGHTLYV	ROVININ VEATHER	RED SURFACE WITH	- - -		76 MM				:	A12	8
	9_ - 10_		MUDSTONE		8.58, 8.64	AND 9.9 NBEDDIN	5° AT 7.43, 7.48, 19 M. 19 2 6 C M. AT		.74.	DIAWOND BIT 7	- - - - -			•		9 - 10
		92.45	· · · · · · · · · · · · · · · · · · ·		- 100 - 63	······································	END OF HOLE		10.38 M	·		× ***			•	- 11
	12							-						. e		12
Ì	13_ 14	-				:			· · · · · · · · · · · · · · · · · · ·							_13
	יד <u>י</u> הי					· .	· .									

	D	RI	LLO	3	PROJE	CT:	THE C	EASIBILIT ONSTRU(EKONG E	CTION O	F		SE		EET N	· L	A-2	
- c	ITE		NE A	COOF	DINATE			78 E:8,582,2		118	ICHI	JATIO	ง ถ้	DRILL	RIG		
	111.		YL.,	<u>م</u>	ATE	FRO	OM 04/11	/95_TO <u>·0</u>	3/11/95			EO	• • • •	SOMSF			
A	-		CORE	10	0 0 %		PTH VATION	15.400 97.650			OGG	•	TA	WEESAI	<		
	DEPTH	ELEVATION	ROCK TYPE OR FORMATION	NLUM SLUM			DESCRIPT	ION		BIT & DIAMETER	GROUNDWATER LEVEL	& CORE		1-VALUE	;	SAMPLING	DEPTH
	 1 		CLAY		COLOUR, S	STIFF IN C		gish Brown Y, Medium Wa	TER		-			<u></u>	- 	A-3-1	
	2	93.65		_///					2.00 M.								-
26/ 1/32	3_								-		-						-
5	. : •					• • • •	· · · · · · · · · · · · · · · · · · ·								:		- ;
	4 - 5_		CLAY WITH FINE SANE	· / /	COLOUR, WATER CO	FIRM IN C	CONSISTENC	NGISH BROWN Y, HIGH TO SA CHTY, SILT INCU IT WITH DEPTH	TURATE UDED,					•	· · ·		
	6_					: •	:									A-3-2	-
00	7_	90.65							7.00 M.								1
	8						· · · · · · · · · · · · · · · · · · ·										
	9_ 10		CLAYEY FINE SAND		FINE TO I GRANULI SUB-ROL	MEDIUM I E GRAIN 4 IND IN PA	n grain siz Size at 12.00 RTICLE SHA	ROWN IN COL E WITH SOME - 12 20 M., PE, WELL GRA IM DENSITY, HI	N SIZE								1
20								ICITY OF CLAY								A-3-(ع م (
28/11/95	- 12_	85.4							12 20 M				·.		50	т Хбин	-
	13_	85.25 - 84.60	SANDSTON	ιE	CHANG	ed into R, very (SOIL, REDDI STIFF IN CON	DRIGIN ROCK SH BROWN IN ISISTENCY. R, MEDIUM IN	12.40 M].						-	
V			MUDSTON	E	GRAIN	SIZE, SLI	GHTLY HARD), MODERATEL	Y) BT 7			.00				-
20/11/05	14	83.9/	SILTSTON		REODI	SH BROV TLY WEAU RE WITH	n in Colou Thered, Slk Some Tuff	R, SLIGHTLY H SHTLY POROU ORIGIN	ARD, /	AMOND BT 76 MM					:		

DRI	LL LO	G s	PROJ	ECT:	THE	CONS	TRU	CTION	OF		KSE					•	
E L	INE A									INCL	INATI	ÓN	0 I	DŔILI	RIG		
]	DATE	FR	OM <u>04/1</u>	1/95]	ro <u>o</u> e	V 11/ 95				U.,				•	
		1	100 %										TAWE	ESA	<		
ELEVATION	OR	COLUMN SECTION		· · · ·	DESCRIP	TION			DIAMET	SROUNDWATER				·		SAMPLING	DEPTH
82 25	SILTSTONE				<u>^</u>			15.40 M	<u> </u>			.'	0 20	30 4() 50		
-			HARD,	slightly Rigin				Y - 2/2	-			<u>e.</u> .			-	•	- - 16
-			- RQD =		<u> </u>				ľ			н 1			•		·
					END OF HO	ίE									·		. 17
															•		- :
								•		-					. •		. 18
					÷.,												- 19
														•	•		- 19
															•		20
																	20
				• • •		•	:								. • •		21
			. ÷.			·											
							;		1	÷			a sa N				.22
							н н 1										;
																	23
				· . · ·					ľ				;		-	- · ·	``
															-		_24
						•				ľ.							_
													÷				.25
1								e to s							-		-
								•						•	-		26
															· ·		-
															•		.27
1															• •		-
												÷					_28
					· · · .									· .			
				-			14										_29
	1			: .								<u>-</u>					- 30
	E L RAG RECC NOLEVEL	E LINE A	RAGE CORE RECOVERY:	E LINE A COORDINATE DATE IND % ROCK TYPE OR FORMATION 82 25 SUISTONE PURPLI HARD, O - ROD	E LINE A COORDINATE DATE FRU RAGE CORE RECOVERY: 100 % ELE COR FORMATION C C CORDINATE DEF ELE C COVERY: 2 C C C C C C C C C C C C C C C C C C	PROJECT: THE OTHER E LINE_A COORDINATE DATE N1.674.942.1 FROM_04/1 RAGE CORE RECOVERY: 100 % DEPTH_ELEVATION_ Image: Second stress of the secon	PROJECT: THE CONS THE MEKC DATE PATE FROM_04/11/05_1 ROCK TYPE THE CONS ROCK TYPE THE CONSTRUCT DESCRIPTION THE CONSTRUCT ROCK TYPE THE CONS	PROJECT: THE CONSTRUCT THE MEKONG B DATE PROJECT: THE CONSTRUCT THE MEKONG B DATE PROJECT: THE CONSTRUCT THE MEKONG B DATE PROJECT: THE CONSTRUCT PURPLISH BROWN IN COLOUR, MODERATEL PURPLISH BROWN IN COLOUR, MODERATEL	DRILL.LOG PROJECT: THE CONSTRUCTION THE MEKONG BRIDGE E LINE_A COORDINATE DATE N:1.674.942.378 E:3.582.238.443 FRAGE CORE DATE FROM_04/11/05_TO_06/11/05_ M RAGE CORE 100 % DEPTH15.400M RECOVERY: 100 % DEPTH15.400M B225 SUISTONE SUISTONE PURPLISH BROWN IN COLOUR, MODERATELY 15.40 PURPLISH BROWN IN COLOUR, MODERATELY 15.40 PURPLISH BROWN IN COLOUR, MODERATELY 15.40 M B225 SUISTONE SUISTONE SUISTONE PURPLISH BROWN IN COLOUR, MODERATELY 15.40 PURPLISH BROWN IN COLOUR, MODERATELY 15.40 PURPLISH BROWN IN COLOUR, MODERATELY 15.40 M B226 SUISTONE PURPLISH BROWN IN COLOUR, MODERATELY 15.40 M PURPLISH BROWN IN COLOUR, MODERATELY 15.40 M PURPLISH BROWN IN COLOUR, MODERATELY 15.40 B226 SUISTONE PURPLISH BROWN IN COLOUR, MODERATELY 15.40 M B226 SUISTONE PURPLISH BROWN IN COLOUR, MODERATELY 15.40 M B226 SUISTONE PURPLISH BROWN IN COLOUR, MODERATELY 15.40 M B226 SUISTONE PURPLISH BROWN IN COLOUR, MODERATELY 15.40	PROJECT: THE CONSTRUCTION OF THE MEKONG BRIDGE AT THE MEKONG BRIDGE	E LINE_A COORDINATE DATE N1.674.942.378 E.8582.236.443 FROM_04/11/05_TO_00711/05_TO_00	DRILL LOG PROJECT: THE CONSTRUCTION OF THE MEKONG BRIDGE AT PAKSE E LINE_A COORDINATE DATE N.1.674,942.378 E-3.582.236.443 FROM G4/11/05_TO_081	DRILL.LOG PROJECT: THE CONSTRUCTION OF THE MERONG BRIDGE AT PAKSE E LINE_A COORDINATE DATE N1.674.942.378 E:8.582.236.443 FROM_04/11/35_TO_06/11/35 NOLINATION_ DRILED_ ERAGE CORE RECOVERY: 100 % DEPTH15.400M ELEVATION97.650M NOLINATION_ DRILED Image: Core of the state of t	DRILL LOG PROJECT: THE CONSTRUCTION OF THE MERONG BRIDGE AT PAKSE SHE SHE SHE SHE SHE SHE SHE SHE FROM_QUILINGS TO DEVIDES TO MATE INCLINATION_0 FROM_QUILINGS TO DEVIDES TO MATE INCLINATION_0 SHE SHE SHE SHE SHE SHE SHE SHE SHE SHE	DRILL: LOG PROJECT: THE CONSTRUCTION OF THE MEKONG BRIDGE AT PAKSE: MOLENCE SHEET N E UNE_A COORDINATE DATE N:1.674,942.376 E3.582,236.443 FROM_04/1105_TO_021/355. INCLINATION_0_D_DRILL DRILLED_SOMSF. RAGE CORE RECOVERY: 100 % DEPTH	DRILL LOG PROJECT: THE CONSTRUCTION OF THE MEKONG BRIDGE AT PAKSE Mole No. 2 SHEET NO. 2 E LINE_A COORDINATE DATE N.1.674.942.376 E.9.592.236.443 FROM_04/1105_TO_08/11255 INCLINATION_0 OF DRILLED NOLINATION_0 OF DRILLED NOLINATION_0 OF DRILLED NOLINATION_0 OF DRILLED SOMSRI LOGGED ERAGE CORE RECOVERY: 100 % DEPTH_15.400_M ELEVATION_07.550_M INCLINATION_0 OF DESCRIPTION NouLe Image: Statistic Net Image: Statistic Net DESCRIPTION Image: Statistic Net Image: Statistic Net Image: Statistic Net PUBRIENTBROWN BLOODUR, MODERATELY Information_RODE AT EXCHANGE ANTIP SOME Information_RODE AT EXCHANGE ANTIP SOME Information_RODE AT EXCHANGE ANTIP SOME Information_RODE AT EXCHANGE ANTIP SOME Information_RODE AT EXCHANGE ANTIP SOME Image: Statistic Net	DRILL LOG PROJECT: THE CONSTRUCTION OF THE MEKONG BRIDGE AT PAKSE: INCLINATION_0_2 OF SHEET NO_2_OF E LINE_A COORDINATE DATE N11674,942.378 E3.582.230.443 FROM_04/1105_TO_0671055 INCLINATION_0_0_R01055 BRAGE CORE DATE FROM_04/1105_TO_0671055 INCLINATION_0_0_R01055 COCKTYPE OR B 100 % DEFTH

SITE LINE_A COORDINATE DATE N1.074.971.477 EA.581.00.1.33 FROM_201106_TO_291106 NOLINATION_0_0_0RULERG_14CC AVERAGE CORE RECOVERY: 100 % DEPTH_21500_M ELEVATION_01250_M ORILLED SCMS0 VERAGE CORE RECOVERY: 100 % DESCRIPTION SCMS0 DOGGED TAVEESAK VERAGE CORE RECOVERY: 100 % DESCRIPTION SCMS0 DOGGED SCMS0 VERAGE CORE RECOVERY: 8 SCMS0 DESCRIPTION SCMS0 NVALUE SCMS0 SCMS0 RARE BED DEPOSIT, LIGHT BROWIN ROOKOUR, NORR BED DEPOSIT, LIGHT BROWIN ROOKOUR, NORR BED DEPOSIT, LIGHT GRWIN ROOKOUR, NORR BED DEPOSIT, LIGHT GRWIN ROOKOUR, NORR BED DEPOSIT, LIGHT GRWIN ROOKOUR, NEDWIN GRWINE? SCM0 SCM0 or SCM0 or NASSUE SCMS0 SCM0 or SCM0 or NASSUE SCMS0 9 9 SAND SCM or NASSUE SCM0 NR ROOKOU		DR	ILL LO	G	PROJE	CT:	THE FEAT THE CON THE MEK	ISTRUCT	ION O	F		SE	1	E NO.	L	4-3)F_2
AVERAGE CORE RECOVERY 100 % DEPTH21500M ELEVATION31259M LOGGEDIAVEESAK I I I INVELUEIAVEESAK INVELUEIAVEESAK I I I INVELUEIAVEESAK INVELUEIAVEESAK I I INVELUEIAVEESAK INVELUEIAVEESAK INVELUEIAVEESAK I I INVELUEIAVEESAK INVELUEIAVEESAK INVELUEIAVEESAK I I IIII IIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIII	SIT	re I	LINE A		·	<u></u>		i							¦G]	HC-
8 1 SWD MTH RIVER BED DEFOSIT, LIGHT BROWN IN COLOUR, MEDIUM TO VERY COARSE SANDWITH SOME GRAVEL 5000 dT 2 GRAVEL SWD MTH GRAVEL CAN SEE, SUB ROUND IN PAYTICLE SHAPE, WELL GRAN SEE, SUB ROUND IN PAYTICLE SHAPE, POOR GRAN SEE, SUB ROUND IN PAYTICLE SHAPE, WELL GRAN SEE, SUB ROUND IN VERY HOH DENSITY. SOUTH SEE SHAPE, WELL GRAN SEE SHAPE INTO COLORE, MEDIUM GRAN SEED DEFOSIT, LIGHT GRAVIN COLORE, NOT YEAR BED DEFOSIT, LIGHT GRAVIN COLORE, NEEDING GRAN SEED DEFOSIT, LIG			l l	10	0 %					1						
1 RIVER BED DEPOSIT, LIGHT BROWN IN COLOUR, MEDIUM TO YERY COARSE SANDWITH SOME GRAVEL 500 ch 2 SAND WITH GRAVEL SNEW COARSE SANDWITH SOME GRAVEL CRAIN SIZE DISTRIBUTION, VERY HIGH DENSITY 500 ch 3 78.255 SAND SNEW COARSE SANDWITH SOME GRAVEL CRAIN SIZE DISTRIBUTION, VERY HIGH DENSITY 500 M 4 77.255 GRAVEL NIVER BED DEPOSIT, LIGHT BROWN IN COLOUR, MOSTIV 28 MM, GRAVIN SIZE, SUB ROUND IN PARTICLE SIMPE, POOR GRAVIN SIZE OUS IRRUTION, VERY HIGH DENSITY SUM 5 76.255 SAND NIVER BED DEPOSIT, LIGHT GRAVIN COLOUR, MOSTIV 28 MM, GRAVIN SIZE DISTRIBUTION, VERY HIGH DENSITY SUM 6 GRAVEL SIMOP, WERT BROWN IN ROLOUR, MOSTIV 28 MM, GRAVIN SIZE DISTRIBUTION, VERY HIGH DENSITY SUM 8 33.255 SOM SUM SIZE DISTRIBUTION, VERY HIGH DENSITY SUM SIZE DISTRIBUTION, VERY HIGH DENSITY 9 10 SUMO RIVER BED DEPOSIT, LIGHT GRAVIN COLOUR, MEDIUM GRAVIN SIZE, ROUND IN PARTICLE SUMPE, WELL GRAVIN SIZE DOSTRIBUTION, VERY SUM SIG 11 SUMO RIVER BED DEPOSIT, LIGHT GRAVIN COLOUR, MEDIUM GRAVIN SIZE DISTRIBUTION, VERY SUM SIG 12 SUMO RIVER BED DEPOSIT, LIGHT GRAVIN COLOUR, MEDIUM GRAVIN SIZE DOSTRIBUTION, VERY SUM SIG 13 SUM SIG SUM SIG SUM	DATE DEPTH	ELEVATION	OR	COLUMN			DESCRIPTION			BIT & DIAMETER	GROUNDWATER LEVEL	& CORE B RECOVERY		0 30 40 5	1	SAMPLING
Sint of the second s	2		GRAVEL		MEDIUM T GRANULE SHAPE, W	O VERY GRAIN & ELL GRA	COARSE SAND V SIZE, SUB-ROUNI	MTH SOME	нқн					50/20 cm		-3-1
SAND SUSTRUCTOR SUSTRUCTOR SUSTRUCTOR Sustruction MEDIUM GRAIN SIZE, SUB ROUND IN PARTICLE 500M. Sustruction SUSTRUCTOR Sustruction G GRAVEL GRAVEL G GRAVEL Sustruction G GRAVEL GRAVEL G GRAVEL Sustruction G GRAVEL GRAVEL	26/11/95	-	GRAVEL	10.00000 10.00000 10.00000	MOSTLY 2 PARTICLE	-8 MM. G SHAPE,	RAIN SIZE, SUB- POOR GRAIN SIZ	ROUND IN ZE	1	-	· .					
6 GRAVEL Solid on Additional and the property of the product of t	Ę	576.2	1	0.0	RIVER BE	D DEPO	SIT, LIGHT GRAY ZE, SUB-ROUND	IN COLOUR, IN PARTICLE	5.00 M.							
9_ 10_ 10_ 10_ 10_ 10_ 10_ 10_ 10	7/1/95	7_		0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	HIGH DEA RIVER BED MOSTLY 2- SHAPE, WA	DEPOSI 8 MM. GI 5 LL GRAI	IT, LIGHT BROWN	IN COLOUR, D IN PARTICLE		CROWN FOR HO				SQVIG ON.		A-3-2
11_ SAND RIVER BED DEPOSIT, LIGHT GRAY IN COLOUR, MEDIUM GRAIN SIZED DOMINANT, SUB-ROUND IN PARTICLE SHAPE, POOR GRAIN SIZE DISTRIBUTION, VERY HIGH DENSITY. 50/19 cm. 12_ 12_ 13_ 50/11 cm. 80/14_ 50/10 cm.		-														1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
	28/11/95		SAND		MEDIUM	GRAIN SI SHAPE	ZED DOMINANT, POOR GRAIN SS	SUB-ROUND II ZE	N					50/19 cm.		A-3-3
	<u> </u> 	3_ 3_												50/11 cm.		
	29/11/95	14				: .		: . ·						•		-

Ľ	DR	ILL LO	G	PROJE	CT:	TH	E CON	STRU	TY STUI CTION BRIDGE	OF		KSE		Hole Shee	e no. Et no.	L	-3
site ave		INE <u>A</u> SE CORE	C	RDINATE PATE 00 %	FR DE	XOM_2 PTH	5/11/95	_TO2 21.500			DRIL	LED		Ó D SO TAWEI	MSRI	IG <u>T</u> ⊦	<u>IC-1</u>
٦ 	RECO	OVERY:	¥ ب		ELE	EVATIO	N	81.259	<u> </u>		LOG	GED					
DEPTH	ELEVATION	ROCK TYPE OR FORMATION	CTIO			DESCI	RIPTION			BIT & DIAMETER	GROUNDWATER LEVEL	& CORE	3 RECOVERY	N-VA	NLUE 30 40 50	SAMPLING	DEPTH
16	64.759	SAND		RIVER BED GRAIN SIZE SHAPE, PO DENSITY.	D DOMI	NANT, SU	B-ROUND	IN PARTI	CLE						(10 cm		16
17_ 18_ 19_	62 259	SAND STONE		REDDISH B SIZE, MODE CROSS-LAN - BEDDING - 2 JOINT 70 - RQD = 789	RATELY INATIO DIP 5 AND 8	Y HARD, S N INTEXT	SLIGHTLY FURE	WEATHER		BIT 76 MM						<u>A-3-4</u>	1-
20	59.759	MUDSTONE		REDDISH 6 SLIGHTLY V 19.50-20.35 - SUBVERT - 19.00-19.5 - 19.50-20.3 - 20.35-21.5	Veathe M. Caljo D.M. RC 5 M. RC	RED THO INT AT 21 ID = 30 4 ID = 100	CK BEDDII 1.10 M. %			DIAMOND 8			20				19 20 21
22_ 23_ 24						END OF	HOLE						•				22 23 24
25_ 26_					:												25
27_						:	· .	·		:				4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	· · ·		27
28_ 29_												· · · ·					28 29
30							· .										30

	D	RI	LL LO	G	PROJE	CT:	THE CON	SIBILITY S ISTRUCTI KONG BRI	ONO	F		(SE		.e no. Eet no	A-4	
S	ITE	L	NE <u>A</u>		RDINATE DATE		0,674,274.766 0M_24/11/95	E:8,581,632.	886	II		NATIC		_DRILL RI GKAEW	G TH	21
A			e core Very:	1	00 %		PTH	8.100 83.247	M. M.			GED	TAN	/EESAK		
DATE	DEPTH	ELEVATION	ROCK TYPE OR FORMATION	CTIO CTIO			DESCRIPTION			BIT & DIAMETER	GROUNDWATER 1 EVEL	% CORE		VALUE	SAMPLING	DEPTH
	 1 2		SAND		TO COARS	E GRAI	sit, brown in co n size, sub-roum ain size distribu	IO IN PARTICU	3	METAL CROWN FOR HO SIZE					A-41	- 1
24/11/05	467	80,147 75,147	MUDSTONE		SLIGHTLY	^r WEATH TEO WI NT WITH 6.90 M.	N IN COLOUR, MOL IEREQ WITH SOM TH SANOSTONE A I ROUGH SURFAC	É TUFF ORIGIN T 4.10-5.28 M.	:D.	DIAMOND BIT 76 MM.				50/10	A 42	3 4 5 6
	9_ 10_ 11_ 12_ 13_ 14_ 15_						ENDOFHOLE									

	SIT	E L	ILL LOC INE A SE CORE OVERY:	COOF	PROJE RDINATE DATE	N:1 FR	THE	295 TC 5.	RUCT G BRI 81,364 01/12 550	ION O IDGE .638		PA	INATIO	SHI	LE NO. EET NO _DRILL F GKAEW /EESAK	10		1
DATE	DEPTH	ELEVATION	ROCK TYPE OR FORMATION	CTIO			DESCRIPT	ION			BIT & DIAMETER		& CORE		VALUE 30 40 5		SAMPLING	DEPTH
	-	81.23	SAND		RIVER BE	D DEPO	SIT, LIGHT B	ROWN IN	JNDED	0.55 M.			:		50/22	cm-1		
	1_	80.73	SANDSTONE		\ IN PARTIC	LE SHA	PE, POOR G ERY HIGH DE	RAIN SIZE		1.05 M.	ļ				3422	un.		1
	2_ 3_		MUDSTONE		GRAYISH SIZE, HAS RQD = 100 REDDISH SLIGHTLY SANDSTOL - BEDDING	BROWN RD, SLIGE D % BROWN I WEATHE NE AT 1.8 DIP 7	IN COLOUR, TLY WEATH N COLOUR, RED, ALTER 33-2.21 M.	MEDIUM C ERED MODERATI NATED WI	ELY HAR		DIAMOND BIT 76 MM.		×**			-		2
24/11/25	5_	77.783	SILTSTONE		1.43 M. • RQD = 88 PURPLISH	8ROWN GHTLY W	IN COLOUR,	MODERAT	ELY E TUFF	4.00 M.	DIAM					•		4
	6 7 8 9 10							OLE									-	6 7 8 9 10
	12_ 13_ 14_ 15_							· · · · · · · · · · · · · · · · · · ·										12 13 14

A 3-68

DF	RILL LOO	G PROJE	THE MEKONG BRIDGE AT PAKSE SHEET NO. 1_0F
SITE	LINE A	COORDINATE DATE	FROM 28/10/95 TO 29/10/95
1	GE CORE	100 %	DEPTH7.200 M. DRILLEDSOMSRI ELEVATION96.300 M. LOGGEDTAWEESAK
DATE OEPTH CI EVATION	ROCK TYPE OR FORMATION	CTIO	DESCRIPTION DESCRI
1_95 \$9001/82 3_	clay	CONSIS ALLUVA COLOU CONTE DECOM CHANG COLOU	SOIL, GRAYISH IN COLOUR, SOFT IN 0.20 M. SISTENCY 1.00 M. MAL DEPOSIT, ORANGISH BROWN IN DUR, STIFF IN CONSISTENCY, HIGH WATER TENT, MEDIUM PLASTICITY. DMPOSED MUDSTONE, ORIGIN ROCK NGED INTO SOIL, REDDISH BROWN IN DUR, VERY STIFF IN CONSISTENCY, HIGH ER CONTENT, MEDIUM PLASTICITY. 420 M.
5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	MUDSTONE & SILTSTONE 9,10	MODER TEXTUR - VERY 48849 - 75 JOI 4.25 A	DISH BROWN IN COLOUR, SLIGHTLY HARD, ERATELY WEATHERED, SLIGHTLY POROUS IN IURE WITH SOME TUFF ORIGIN RY CLOSE SPACING FRACTURE 2-6 CM AT 4.40-4.58, 4.95, 5.60-5.67 AND 6.79-6.89 M. JOINTS ROUGH AND MN STAIN ON SURFACE AT 5 AND 4.86 M. D = 64% 7.20 M.
8_ 9_ 10_ 11_ 12_ 13_ 14_ 15			END OF HOLE

	r	ND		C	PROJE	CT	THE FEASIBILITY			NC			HÔLE NO.		A	-7
	60	лл	balia baW	U			THE MEKONG B			PAP	(SE		SHEET NO). 1	OF	1
	SITE	: 1	INE A	ĊOO	RDINATE	•	.671,884.432 E:8,581,0					aŭ				
				(DATE	FR	OM 27/10/95 TO 28/	10/95		NCLI DRILL		ΟŊ	<u>0</u> DRILL SOMSRI	RIG		
,	AVE	RAG	E CORE	11	00 %		PTH7.370	M.		JRILL	_		TAWEESAK			
-	· F	RECO	OVERY:		r	ELE	EVATION 101.450	M.	Ľ			 		•···	 1	·
DALE	HLd3C	ELEVATION	ROCK TYPE OR FORMATION	NU CTIO			DESCRIPTION		BIT & DIAMETER	GROUNDWATER LEVEL	CORE PICONE		N-VALUE	50	SAMPLING	DEPTH
	 1	101.00	FINE SANDY CL		COLOUR SHAPE, I LOW DEI	, FINE G POOR GI NSITY, M	SIT, ORANGISH YELLOWIN RAIN SIZE, ROUND IN PARTIC RAIN SIZE DISTRIBUTION, VEF EDIUM WATER CONTENT. HTE, ORANGISH BROWN AND	/ 1						-	A-71	
27/10/95	2 3		CLAY		DECOMP	ÉNCY, M OSED M	Y IN COLOUR, VERY STIFF IN IEDIUM WATER CONTENT UDSTONE, ORIGIN ROCK SOIL, REDDISH BROWN IN		DRAG BIT 3"					-		. 2 . 3
	- 4 	97.08			WATER C	ONTENT	TIFF IN CONSISTENCY, MEDIL (, MEDIUM PLASTICITY. SIN COLOUR, SLIGHTLY HARI	4.37 M.	: :	4.00						4
28/10/95	5_ 6_	96.03	MUDSTONE		FRACTUR ROD = 44	RE 2-6 CI	EATHERED VERY CLOSE SPA M. AT 4.81-5.21 M. IN COLOUR, MEDIUM GRAIN S	5.37 M.	ND BIT 76 MM.	an a		8	· · · · ·	-	<u>A7-2</u>	5
	7	94.63 94.08	SANDSTON		MODERAI - RQD = 1	ELY HAP	RD, SLIGHTLY WEATHERED	6.82 M.						•		7
	8	.)			T .	IGHTLY	WEATHERED, WITH SOME TU							•		_ 8
	9_					 	END OF FIOLE						•			9
	10												:	•		_ 10
	11_													•		11
	12_															_12
	13_													•		_13
	14_ 15								-					• . :		14

	D	RI	LL LOC	3	PROJE		THE THE	FEASIE CONST MEKON	RUCT IG BRI	on (Dge)F		SE		OLE		L	B- OF	
\$	ыте	L	NE <u>B</u>		RDINATE DATE).000 E:8, 10/95 T(NATIO	DN_		RILL MSRI			
,			e core Very	9	5 %		PTH Evation	97	6.000 7.950	M M.			ED	T.	AWE	ESAK			
DATE	DEPTH	ELEVATION	ROCK TYPE OR FORMATION				DESCR	IPTION			BIT & DIAMETER	GROUNDWATER LEVEL	% CORE	1.	N-VA		50	SAMPLING	Hiddu
	: - 1_ -	96.50	CLAY		STIFF IN C MEDIUM P	ONSIST LASTICI	ency, Hig Ty.	I YELLOW IN H WATER CC	ONTENT,	1.45 M.	G BIT 3"	-				,		B-1-1	-
0/95	- 2	95.60	LAITERITIC			F IN CC	NSISTENC	H BROWN IN Y, MEDIUM 1	WATER	2.35 M.	DRAG	UER		. .			· · ·		
26/10/95	34	93.30	MUDSTONE			WEATH		ur, slighte Th some te	JFF ORIGI	N. 4.65 M	DIAMOND BIT 76 MM	ARTIFICAL WATER		8		-	•	8-1-2	· · · · ·
26/10/95	5 6	91.95	SILTSTONE		HARD, ORIGIN	SLIGHTI DOMIN NT AT 5	Y WEATHE ANT AT 4.7 20 AND 5			F 6.00 M				- - -	• •				
	78						ENDOF	HOLE							· · · · · · · · · · · · · · · · · · ·				
	9_ 10_ 11_			-				•		· · ·									
	12																1		
	14	-				- .									•		;		

I	DR	ILL LO	G	PROJE	CT:	THE C	ASIBILITY ONSTRUC	TION	OF	-		F		IOLE N		B OF	
		ь - I	<u></u>	I RDINATE	N:1	l	8 E:8,587,68					·	-1				
SIT	E	LINE B		DATE	مد <u>ن</u> م		95 TO 24/		-	INCI	lina	πic	N_1	0_DR	ILL RIC	<u>THC</u>	2-1
A3 /8		GE CORE	· • · · · · · · · · · ·		<u> </u>		18.800			DRII	LEC)		SOM	SRI		
		OVERY:	6	3%	DEF FIF		110.450	M. M.		LOG	GE)	T,	AWÉES	AK		
- <u> </u>	T		1	 _					┯┸		1					7	<u> </u>
	Z	ROCK TYPE							E	GROUNDWATER	Ж	RECOVERY				1	
DEPTH	ELEVATION		NWN			DESCRIPTI	ON ¹		AME	Å	S S	С С Ш		N-VALU	JE	LIN	DEPTH
		FORMATION	COLUMN						BIT & DIAMETER	IS -	<u> </u>	р П				SAMPLING	Ш а
			1							ဗီ	%	cn	io	20 30	49 50		:
-	-									ŀ		1					
: 1 _	-			·					Ì								1
-				DECOMPO	SED BA		ROCK CHANGE										
2	_	SILTY CLAY		SOIL, REC	DISH BR	OWN IN COLC	UR, FIRM IN								:		2
	_			PLASTICH		DIUM WATER	CONTENT, LOM	ł		· .	:					631	
3										·	•				· .		3
-								1 	· .								
4	106.4	is						4.00 M									4
		÷	2.07					:			İ .		·				
5								÷							· .		5
		LATTERITIC				SALT, ORIGIN F DWN IN COLO	COCK CHANGER	DINTO		1			1				
6		SILTY CLAY		CONSISTE	NCY, HIG		ITENT, MEDIUM	۰ <i>،</i> 							. :-		م
			0.00	PLASTICIT	Υ.	· ·					1			1 .			ь. У
1001/17 7	103	15						7.00 M							•		
				DECOMPC	SED 849		ROCK CHANGE		in in								- 1
8	102.5	CLAY		SOIL, YELL	OWSH	BROWN IN CO	LOUR, STIFF IN	7 95 M	品し		:			r 1			
				CONSISTE	NGY, HIG	H WATER CO	ITENT, MEDIUM	· / ·	08AG				1	2	•••		- 8
9	1			\				Γ.		9.00				:			
–	- -																- 9
										× ±	·		- 1				- :
10_							OCK CHANGED			· ·	2			2			_ 10
-		SILTYCLAY					IR, STIFF TO VE WATER CONTE							\			- 1
, 11				LOWPLAS											-	8-2-2	_ 11
12				•													
*12_	- ·			:				:			. 						12
								•					·· ··		i pe		_
13_	97.4	5	40					13.00 M			2				: . . (_13
. :_		SILTY CLAY												. \			_
14_]	WITH	E.C.					ur.			Ĺ				$\sum_{i=1}^{n}$	ĺĺ	- 14
_	·	BASALT FRAGMENT		CONTENT, L		SISTENCY, ME STICITY,	DIUM WATER				1		•				-
15		T T CONTRACTOR	2.14 3.16.9/4 1.9/6				·							1 - ¹	•	. 1	- 15

DI	RILL LOO	G PRO	JECT:	THE FEASIBILITY THE CONSTRUC THE MEKONG BI	TION O	F		SE		e no. Et no. <u>2</u>	B-	
SITE	LINE_B	COORDINAT DATE		,671,621,468 E:8,587,68 OM_20/10/95_TO_24/				NATION		DRILL RIG OMSRI	THC	-1
	AGE CORE	63 %		PTH18.800 EVATION110.450	M	1	.OGC		TAW	EESAK		
DATE OGPTH	ROCK TYPE	CTIC N		DESCRIPTION		BIT & DIAMETER	GROUNDWATER LEVEL	KECOVERY	•	/ALUE 30 40 50	SAMPLING	UEDTH
16	SILTY CLAY WITH BASALT 4.65ERAGMENT_	COL	OUR, VERY	SALT, REDDISH BROWN IN STIFF IN CONSISTENCY, CONTENT, LOW PLASTICITY.	15.80 M.	76 MM.						-1
\$617 18e	BASALY 92 30	VVV MOD VVV FRAC VVV RQD VVV	TURE 2-6 C = 14 %		18.15 M.	DIAMOND BIT 76		2XX 130				1
119 	MUDSTONE		HARD, SLIG - 50 [°] JOINT	Rown in Colour, Slightly Shtly Weathered At 18:25 M. Dip 10° at 18:32 and 18:40 M %	18.60 M	·			· · ·			
20_				END OF HOLE								1.4
21 22 23										a and the second s		
24_ 25_ 26												
27												
29_ 30					· · · · ·						•	

	 	DR	RILL LO	G	PROJE	CT.	THEC	EASIBILITY CONSTRUCT IEKONG BRI	ION	OF			E		OLE I HEET		1	B- OF	
	SIT	E	LINE B		RDINATE DATE	-		34 E 8 587 530 /95 _CO10/1							b_or		ÎG_	THO	<u>21</u>
			ge core Overy:	4	9%		PTH EVATION	30 250 86.602	M M		drii Lõg				NEESO				
	DEPTH	ELEVATION	ROCK TYPE OR FORMATION				DESCRIPT	ION		BIT & DIAMETER	GROUNDWATER	core	RECOVERY		N-VAL		0	SAMPLING	DEDTU
	1_	85.6	SAND		MEDIUMO	RAINS		OWN IN COLOUR, IND IN PARTICLE FRIBUTION	1.00 M.				-	֠	<u></u>	- <u></u>		•••••	
CR/11/20	2	82.60	SAND		MEDIUM D RIVER BEI COARSE S ROUND IN	ENSITY D DEPO SAND SI PARTIC	/. XSIT, LIGHT BR OME VERY CO	IOWN IN COLOUR, DARSE GRAIN SIZE JELL GRAIN SIZE ITY.	, 3.00 м.		-							B-3-1	
	4 5 6	-	GRAVEL	, 4 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	2-8 MM. GF WELL GRA	vain siz In size D of fi	ZE, ROUND IN DIŠTRIBUTIO ELOSPAR ANČ	N COLOUR, MOSTL PARTICLE SHAPE, N, HIGHLY ROCK FRAGMENT		METAL CROWN FOR HO SIZE				· · · · · · · · · · · · · · · · · · ·				8-3-?	
	7	79.č	D2 SAND	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	MEDIUM TO PARTICLE	D COAR SHAPE,	ISE GRAIN SIZ POOR GRAIN	Y IN COLOUR E, SUB-ROUND IN SIZE DISTRIBUTIC ASALT FRAGMENT		~							and a second		
	10_	76.60 76.10	CONVEL	0.0.0 0.00 0.00 0.00 0.00			DSIT, GROWN	IN COLOUR 10	0.00 M. 0.50 M.							·			- 1(
	11 12		BASALT	VVV VVV VVV VVV VVV VVV VVV	PARTICLE	SHAPE TION, C	E, WELL GRAI	SUB-ROUND IN N SIZE F SOME BASALT		317 76 M2M.			1 130	•					
	13_ 14_			VVV VVV VVV VVV VVV		PAĊING	ARD, SLIGHTL FRACTURE 2	Y POROUS, VERY 6 CM.		DIAMOND BIT 76 MM			0	· · ··	• • •				_1:

A DESTRUCTION OF A DESTRUCTUCTION OF A DESTRUCTION OF A D

Ľ	RI	LLLO	G	PROJE	CT:	THEC	EASIBI CONSTR IEKON	RUCT	ON O	F		(SE			EET		E.	B-	
SITE	: 1	NE B	COORI		•	,671,251.8			• • • • • •		NCU	NAT	ION	Ιð	DR	at i	RIG	THC	>1
		· · · · · · · · · · · · · · · · · · ·	DA	TE	FR	OM 03/1	<u>1/95_</u> TO	10/1	/95	1.	DRILL								
		e core Very:	49	%		PTH VATION		250 602	_M. M.	1	.0G(WEE				
DEPTH	ELEVATION	ROCK TYPE OR FORMATION	CTION N			DESCRIP	rion			BIT & DIAMETER	GROUNDWATER LEVEL	se core	1 RECOVERY		1-VAL 20 30		50	SAMPLING	рертн
- 16_ 17_				:						-			230	- - -		<u>.</u>		8-3-3	16
18_		BASALT			PACING	ARD, SLIGHT FRACTURE 2		S, VERY							·				- 18 :
50 19 20				:	· .	: : : : : : : : : : : : : : : : : : :				MM 97 TIB CNOMAIC		XXXXX					•		19 _20
21 5811-0 22 23	55.85 2								20.75 M.										21 22 - 23
24_ 25_		POSSIBLE MUDSTONE O CONGLOMER		NO CORE	RECOVE	ERY.													24
26 Selivit 27 28		ε		• •					1										20
29	-	2						· · · · · · · · · · · · · · · · · · ·	30 25 M.									•	29

	D	RI	LL LO	3	PROJE	CT:	THE FEASIBILITY STU THE CONSTRUCTION THE MEKONG BRIDG	OF		KSE		HOLE NO. SHEET NO	B- 1_OF	
~~			INE B	coo	RDINATE	N:1	.670,883.643 E:8,587,374.637	·	·•			<u>و</u>		~ •
5	ITE				DATE	FR	OM 13/11/95 TO 15/11/95	-				N <u>0</u> DRILL RII MANEESORNI	3 <u>1H</u>	<u>1</u>
A)			e core Very:	1	00 %	DEF Ele	PTH15.800M EVATION81.162M			LED GEO		TAWEESAK		
		ELEVATION	ROCK TYPE OR FORMATION	COLUMN SECTION			DESCRIPTION	BIT & DIAMETER		% CORE	B RECOVERY	N-VALUE 10 30 30 40 50	SAMPLING	DEPTH
	1												A-4-1	. 1
	3 4		SAND		MEDIUM T PARTICLE	D COAR: SHAPE,	SIT, LIGHT BROWN IN COLOUR, ISE GRAIN SIZE, SUB-ROUND IN FOOR GRAIN SIZE DISTRIBUTION, UDED, MEDIUM TO HIGH DENSITY.	SHO SIZE					•	3
	5_ 6_							METAL CROWN FOR HO SIZE						5
1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.	* 	74.162 73.162	SÁND		VERY CO/ PARTICLE VERY HIG	RSE GR POOR (1 DENS)								7
	- 9_	72.162	SAND		MEDIUM (POOR GR	RAIN SL	SIT, LIGHT GRAY IN COLOUR, IZE, SUB-ROUND IN PARTICLE, E DISTRIBUTION, VERY HIGH 9.001	<u>A.</u>				50/25 cm.		 _ 9
1	0_	76.362	SAND		COARSE SUB-ROU	'o very ND in Pa	SIT, LIGHT BROWN IN COLOUR. Y COARSE GRAIN SIZE, ARTICLE SHAPE, POOR GRAIN W, VERY HIGH DENSITY. 10.80	M				an a		_10
1	1	69.862	SANDSTON	-	SILT RICH SLIGHTLY	IN GRAI	LIN COLOUR, FINE SAND WITH NN SIZE, MODERATELY HARD, IERED 11.30	ч.						11
1	2 3		MUDSTONE		SLIGHTLY	BROWN WEATH NE AT 1 PACING I DRILLING	R IN COLOUR, SLIGHTLY HARD, RERED, ATTERNATEO WITH 12 25-12 45 M. FRACTURE 6-20 CM BROKEN G	DIAMOND BIT 76 MM.			500		. 1.42	12 13
	45	67.012	SANDSTONE		GRAYISH SILTY RIC SUGHTLY	BROWN H IN GR WEATH MTH RC	I IN COLOUR, FINE SAND WITH WIN SIZE, MODERATELY HARD, 14 15 IERED WITH SOME TUFF ORIGIN OUGH SURFACE AT 15 31 M.		-					14

D	RII	L LO	G	PROJE		THE FE The CC The Mi)NSTR EKONC	UCT	ION O)F		SE	HOLE SHEE		B- 05	
SITE		VE B		RDINATE	•	,670,883.64 OM_13/11/					INCLI	VATIO	N <u>0</u> DF	RILLRIC	<u>тн</u>	<u>-1</u>
AVEI	RAGE	CORE	. <u>.</u>		DEI	νтн	15.8	300	M.		DRILL		MANEÉS TAWE			
		/ERY:		100 %	ELE	VATION	81.	162	M.	ŗĽ		······	······································			
DEPTH	ELEVATION	ROCK TYPE OR FORMATIO				DESCRIPTI	N			BIT & DIAMETER	GROUNDWATER LEVEL	& CORE 5 RECOVERY	N-VA	LUE 0 43 50	SAMPLING	HLABO
16_	65.362	SANDSTON	E	SILTY RK	CH IN GR Y WEATH WITH RO	IN COLOUR, F AIN SIZE, MOD ERED WITH SO DUGH SURFAC	ERATELY DME TUFF	HARD, ORIGI	15.80 M			8				16
17_					. I	END OF HOLE			· · ·							
18_		· ·			1 - 41 41										•	18
- 19_																1
-					• •											20
20_									· .						-	
21_			11 11. AB													2
22_								: : : :: :								2
	-							· ·								2
23_														•		-
24_	-						-									2
25																2
	-			i i	!				·.					1 . 1		2
26															4 	-
27														- 		
28															-	
	_															-
29							:						1	н (т. 1		.
30	<u>)</u>	· · · · ·					~									

	·	[. İ .	 ·	PROJE			EMEK	ISTRU (ONG E:8,587	BRI	DGE	AT			L	HEET NO.	<u>.</u>		
	SITÉ		INE	B		DATE	FR	OM_16	11/95	_TO_	22/11	/95						RG	<u>r HĊ</u>	
,		RAG ECC		ore RY:	1	00 %		PTH Evation	۷	20.13 76.91		_M. M.		DRILL			NEESORNI AWEESAK			
UALE	DEPTH	ELEVATION		OCK T OR DRMA	COLUMN			DESCR	RPTION				BIT & DIAMETER	GROUNDWATER LEVEL	CORE CORE		N-VALUE	- E - E	SAMPLING	DEPTH
	1_ 2 3_ 3_		· · ·				· .												-5-1	- - 1 - 2 - 3
	4 5 6 7 8 9			SAND		RIVER BE MEDIUM I SHAPE, P MUSCOVI DENSITY	N GRAIN DOR GR TY INCL	I SIZE, SU AIN SIZE UDED, MI	IB-ROUN DISTRIB	d in Par Ution D Very F	TICLE		METAL CROWN FOR HID SIZE							4
							:		- - 	· ·			ΒM							9 10
	11_ 12_							· · ·									50 cm			11 12
	- 13_ 14_ 15	· · ·					•	·				· · ·					50/24 cm 50/23 cm 50/21 cm			13

Ď	RI	LL LO	G	PROJE	CT:	THE	FEASIE CONST MEKON	RUC	TION C)F		SE		HOLE SHEE). <u>2</u>	B-	
SITE	LI	NE <u>B</u>		RDINATE	معميدهم	0M_16									-	RIG_	THC	2
		e core Very:	1	00 %		PTH		20.130	M. M.		.060			TAW				
DATE DEPTH	ELEVATION	ROCK TYP OR FORMATIO	NUC NUC	-		DESCRI	PTION			BIT & DIAMETER	GROUNDWATER LEVEL	% CORE	-	N-V/	30 40	50	SAMPLING	
ຣູ້ 16_ 	61.136	SAND		MEDIUM SHAPE, F MUSCOV	IN GRÀIN IOOR GR ITY INCL	SIT, LIGHT (I SIZE, SUB AIN SIZE D UDED, MEC SING WITH	-ROUND IN ISTRIBUTK IUM TO VE	i partici DN,									-	
- 17 		MUDSTON	E	SLIGHTI ALTERN 18.21-18 BEDDIN	Y WEATI ATED W .47 M. G DIP 5	N IN COLOL HERED, WI TH SANDST FRACTUR	TH SOME T	UFF OR! 14-16-59	gin 9 And	DIAMOND BIT 76 MM.	1		435					
22/11/96	56.786			- 15.78-1 - 18.78-1	8,78 M. 9,78 M.	RQD = 20 % RQD = 100 RQD = 0 %	%		20.13 M		-					•	B 5 2	Σ
21_						ENDOF	łOłe							-				
22_																		
24_ 25	-					· ·									· .	· ·		
26					14 	• • • •	-									i		
27														•				
29	-				· .		14										•	:

	ſ	DR	ILL LO	G	PROJE	CT:	TH	E FEA E CO E ME	NST	RŲC	TIC	ON C	ÓF		KS	E	1	ole Hee			B _OF	····
	SITE	Ξ	INE B		RDINATE DATE		.670,03 OM_3(80.073	E:8,5	586,8	95.4	38		·			ц N <u>(</u>				TH	<u>C-1</u>
			SE CORE OVERY:	1	100 %	DEF ELE	PTH VATIO	N	3 105	.160 .160		М. М.		dril Log			T/	APIO		•		
DATE	DEPTH	ELEVATION	ROCK TYPE OR FORMATION				DESCF	RIPTIO	1		• • • • • • • • • • • •		BIT & DIAMETER	GROUNDWATER	& CORE	3 RECOVERY		N-VA 20 3		۰. ۲.	SAMPLING	DEPTH
CEIEDIDE	12	162.00	SANDSTONE		GRAYISH E Size, Hare Included, In Bedding - 80 Joint, Of Clay / - Bedding - RQD = 90	D, SLIGHI GENTLY 3 ROUGH 8 NT 0,15 M DIP 3-10	LÝ WEAT INCLINÉ SURFACE	FHERED D CROS	I, MICA IS-LAM LING W	PART IINATH MTH F	icle On Ilm	16 M.	DLAMOND BIT 76 MM.	1.60		316 316	Ľ			· · · · · · · · · · · · · · · · · · ·	B-5-1	1
	4					E	ND OF H	OLE					-							. •		
	- 5_					- - - - -				-												_ 4 _ 5
	6 7 8													a man and a set of the								6 - 7 - 8
	9_ 0_					•		• . •														9 10
	- 11_ 12_					-			•										•			- 11 - 12
	13_								·									•. •				13
	14_ _ 15								•						-		· · ·		• • •			_14

 $\mathbf{a}_{1} = \left\{ \mathbf{a}_{1} \in \mathbf{A}_{1} : \mathbf{a}_{2} \in \mathbf{A}_{2} : \mathbf{a}_{2} \in \mathbf{A}_{2} : \mathbf{a}_{2} \in \mathbf{A}_{$

	DR		LO	G	PROJE	CT:	THE FEASIBILITY STUDY THE CONSTRUCTION OF THE MEKONG BRIDGE A				-				HOLE NO. SHEET NO			B-7		
SIT	SITE LINE B COO						1,670,086.403 E:8,585,805.016 COM_17/08/95_TO_18/08/95_							N <u>0</u> DRILL RIG APICHAT			THC	-1		
	AVERAGE CORE RECOVERY:			1	100 %		PTH8.050M. EVATION100.750M.			DRILLED				TAWEESAK				·		
DEPTH	ELEVATION	RO	CK TYPE OR RMATION				DESCRIP	пом			BIT & DIAMETER	GROUNDWATER LEVEL	CORE DECOVERY	-		30 43	50 	SAMPUING		
			YEY SILTI IE SAND		COLOUR,	UVIAL DEPOSIT, YELLOWISH BROWN IN LOUR, FINE IN GRAIN SIZE, VERY LOW DENSITY, 1,00 M SH WATER CONTENT, LOW PLASTICITY OF CLAY.				0.60										
96/60/21			TTERITIC CLAY		VERY STIFF IN CONSISTENCY, MEDIUM WATER				DRAG BIT 3			1				8-7-1 8-7-2				
		CLAY			ALLUVIAL DEPOSIT, YELLOWISH BROWN IN COLOUR, VERY STIFF IN CONSISTENCY, MEDIUM WATER CONTENT, HIGH PLASTICITY. 5.00 M.										•					
18/09/95	- - - -	S/ 2.76	NDSTON	Ē	Size, H/ Partici Lamina - Beddi	RD, SLIG E INCLU TON IN E IG DIP 5 IG DIP 7	SHTLY WEAT	, MEDIUM IN C HERED, MICA Y INCLINED OF	-2205	8.05 M.	DIAMOND BIT 76 M.M.			350						
	9_					·	END OF HO	XE								•	. د. • •			
	9 0								1 . 1 1											
	1 2									: 					:					
1	3_		· .										· · ·			:				
	4_		· . ·			• .	:		:							··· · : - ·		•		

	Ľ	DR	ILL LO	G	PROJE	ECT:	THE F The C The N	ONST	RUCI		DF		⟨SE		le no. Eet no	ι	C-	·
(SITE	=	LINE_C		RDINATE		,671,662.1	78 E:8,	588,89	3.619	-r	······		 >N0	DRIH	RÌG	ТНС	
~	•••••				DATE	- FR	OM_03/10			0/95		ORILI		•	PICHAT	-		
1			ge core overy:	1	00 %		PTH Evation		6.050 1.340	M. M.			GED	TAV	VEESÄK	<u> </u>		
UATE 1 1	DEPTH	ELEVATION	ROCK TYP OR FORMATIO	CTION			DESCRIPT	(ION			BIT & DIAMETER	GROUNDWATER LEVEL	& CORE 3 RECOVERY		VALUE	50	SAMPLING	
CG/0	1_ 2_ 3_	108.3	LATTERITIC SILTY CLAY WITH BASA FRAGMENT		VERY STIF	FINCO	lt, reddish Nsistency, n I plasticity	AEDIUM V		JR, 3.00 M.	DRAG BIT 3	1.60 1.60			50410			
03/10/9	4 5	105.2	BASALT		- 40 JOINT - 20 JOINT 3.65 AND	WITH IRO WITH IRO 4.45 M. TICAL JC NO 5.87 N	IC AND PORG ON STAIN SU ON STAIN SU HNTS WITH IF M	RFACE AT RFACÉ AT	13.19 M. 13.25,	CE 6.05 M	DIAMOND BIT 76 MM.						C-1-1	
		•					END OF HO	E			•						Ť	
	7 8																	
	9_						•											-
	10									- - 1 -					Хс 			- 1
	• •									- - 								
The second second	11_														* *			1
	-														· ·			
	12_														•			1
	13_	:																1
	- 14																- 54	-
	-			:					:			· · ·						
	15																	

Ľ	RI	LL LOC	3	PROJE	CT:	THE FEASIBILITY STU THE CONSTRUCTION THE MEKONG BRIDGE	OF			HOLE NO. SHEET NO1	C- _OF	
SITE	: 1	INE C		RDINATE DATE		1,670,965.227 E:8,588,871.885 COM_04/10/95 TO_11710/95				DN_0_DRILL RIC	; THO	-1
••		E CORE	1(00 %		PTH14.150M. EVATION108.890M.	1		lled Geed	TAWEESAK		
F		VERY:						T			1	[.
DEPTH	ELEVATION	ROCK TYPE OR FORMATION	SECTION COLUMN			DESCRIPTION	BIT & DIAMETER		<pre>LEVEL % CORE % RECOVERY</pre>		SAMPLING	DEPTH
1-		LATTERITIC SILTY CLAY		SOIL, BRO	XVN IN C	ASALT, ORIGIN ROCK CHANGED INTO COLOUR, STIFF IN CONSISTENCY, CONTENT, MEDIUM PLASTICITY. 2.001						_ 1
3_											- C21	
4_ 5_	-	SILTY CLAY		SOIL, RE FIRM TO	DDISH B VERY SI PTH, ME	BASALT, ORIGIN ROCK CHANGED INTO BROWN TO DARK BROWN IN COLOUR, ITIFF IN CONSISTENCY INCREASING EDIUM WATER CONTENT, MEDIUM	Į	0 10 0				
6 7					· · ·							- 6
8	-					7.50	<u>M.</u>					
9	-	SILTY CLAY WITH BASAL FRAGMENT		VERY ST CONTEN BASALT	IFF IN CA	SALT, DARK BROWN IN COLOUR, CONSISTENCY, MEDIUM WATER UM PLASTICITY, HARD AND FRESH IN ENT.		10	.00			1
11 12 05/01/11		BASALT		HARD, F CLOSE SUBH AT13.00 + 45JOIN 13.57 M - 10.90	SPACING ORIZON 13.29, 1 175 WIT 13.00 M.	10.90 RITIC AND POROUS IN TEXTURE 3 FRACTURE 6-20 CM. AT 10.90-13:00 M ITAL JOINTS WITH IRON STAIN SURFAC 13:40, 13:43, 14:00 AND 14:15 M. I'H IRON STAIN SURFACE AT 13:50 AND RQD = 21 % RQD = 21 %	 - -	DIAWOND BIT 76 MM.			01	-
14	-	4			- 9, 2 9* (VE	14.15 END OF HOLE	M.				• • • • • •	1 1 1

]	DRI	LL LO	G	PROJE	CT:	THE FEA THE COI THE MEI	NSTRU	CTION	OF			E	HOLE NO. SHEET NO	ļ	-3 F_1
	SITI	: L			rdinate Date		.670,440.116 OM_11/12/95		و سرموند مرغوم						RIG_T	IC-1
			e core overy:	1	00 %		PTH EVATION	12.100 108.890			DRIL LOG			KONGKAEW TAWEESAK		
DATE	DEPTH	ELEVATION	ROCK TYPE OR FORMATION	CTION			DESCRIPTION	ł		BIT & DIAMETER	GROUNDWATER		3 RECOVERY	N-VALUE	SAMPLING	DEDTH
11/125/95	- 1_															
÷	2		- - - -						- - 	SIZE.						
	3_ 		SILTY CLAY		BELOW 6	5 METRE	IN GRAIN SIZE, M ES GRÀNUTES AN			CROWN FOR HCI SIZE	· · ·					
12/10/95	4_ 5_				INCLUDE).				METAL CF					•	
• • •	6				;											
	- 7	101,39							7.10 M	<u>.</u>		×			•	17- 1 1
	8_					:										
13/10/95	9_ - 10		MUDSTONE SANDSTONE ALTERNATION		ALTERNA	EDAT	DUR, MUDSTONE , NTERVALS OF 3 M ED, MODERATELY	IM. TO 5 MA		DIAMOND BIT 76 MIN			800			-
	11_									DIAM						1
•	12	97.99				-+		· .	12.10 M							
	13_						END OF HOLE								C-2-	1:
	- 14						· · · ·		· · ·							

	D	RI	LL LO	G	PROJE	CT:	T	IE CO	ASIB DNST EKON	RUC	TIO	NO	F		SE			E N	0. NO	C· I_OF	
: <	SITE	L	NE_C_	3	RDINATE DATE		1,670,2 ROM_(ICLI	:			DRII GKAE	LL RIC	<u>3 TH</u>	<u>C-1</u>
ł			e core Very:		00 %		evatio			.500 .890		И. М.		OGG				EES			
DATE	DEPTH	ELEVATION	ROCK TYP OR FORMATIO				DESC	CRIPTI	ON				BIT & DIAMETER	GROUNDWATER LEVEL	% CORE	-		VALU	E 40 50	SAMPLING	DEPTH
	- 1_ 2_					<u> </u>															- 1
07/12/95	3 4_		SAND		FINE TO I DISTRIBL QUARTZ DENSITY	TION, S AND SA	SAND GF	IAIN CO	NSIST C	F IRO!	41,										- 4
08/12/05	5 6 7 8						and the second second second second second second second second second second second second second second second	a a construction of the second s					METAL CROWN FOR HO SIZE.								
	" - 10_ - 11_																				
SOCMON -	14_	97.9	9								14	1.95 N					•	· · · · · · · · · · · · · · · · · · ·			- 1

A 3-85

	ſ	R	LL LO		PROJE		TH TH	IE CO IE MI	DNS EKC	TRU NG I	ICT BR	STUE ION (IDGE	DF		KSE		1	ole Iee			OF	
;	SITE	: L	INE C		RDINATE DATE		,670,2 OM_0							NCL	NA	rio	N_0	D	ŔIL	L RIG	THO	2-1
							PTH							DRIL	LED		KO	NGK	AE	<u>N</u>		
1			e core Very:	1	00 %		EVATIC					M. M.	ļ	LOG	GED)	ΤA	WE	ESA	K		
UALE	DEPTH	ELEVATION	ROCK TYPE OR FORMATION	MU OITO		L	DESC	RIPTIC	- MC				BIT & DIAMETER	GROUNDWATER LEVEL	CORE	RECOVERY	1	\- VA	LÜE		SAMPLING	DEPTH
-					·····								<u>1</u>	G	%	cn	10	20 3 1 -	0 '4 L	50		
09/12/20	16		SAND AND GRAVEL		WELL GR 10 CM. IN	4.		BUTION	r, Mad	UMUM	SIZE				-					- - - - -		
	17_	97.99		0 0 0								17.50 M									ľ	
•	18				·		END	OF HOL	E	<u> </u>							÷					•
	_									-								:	•	÷		_
ĺ	19			:					÷	;							çes.				- 1	- '
	-									-	•		1				·	:	:			
	20						·	24 1										:				-
	21		· ·				· • • ·		· .			· · ·			К		····•					
		11 II II II II II II II II II II II II I				1							•				: :			:		-
	22_	4								: . *									: : :			-
	23			1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 -														. *				
	23							. :				• 	4	•			·					- 1
	24_				· ·		:										·		•••			- (
	-						•					• • •						- - 				
	25						: ;			•												_ 1(
	26							.j														- 1
									-					•								
	27_		:																			12
									·								7 1-1 2			••••••••		
	28																÷	•		•		1 ;
	29	:															۰	• •		•		 -14
										:	•							: :-	:			
	30							_ <u>`</u> ,,							L			-				1

e de la construction de la const

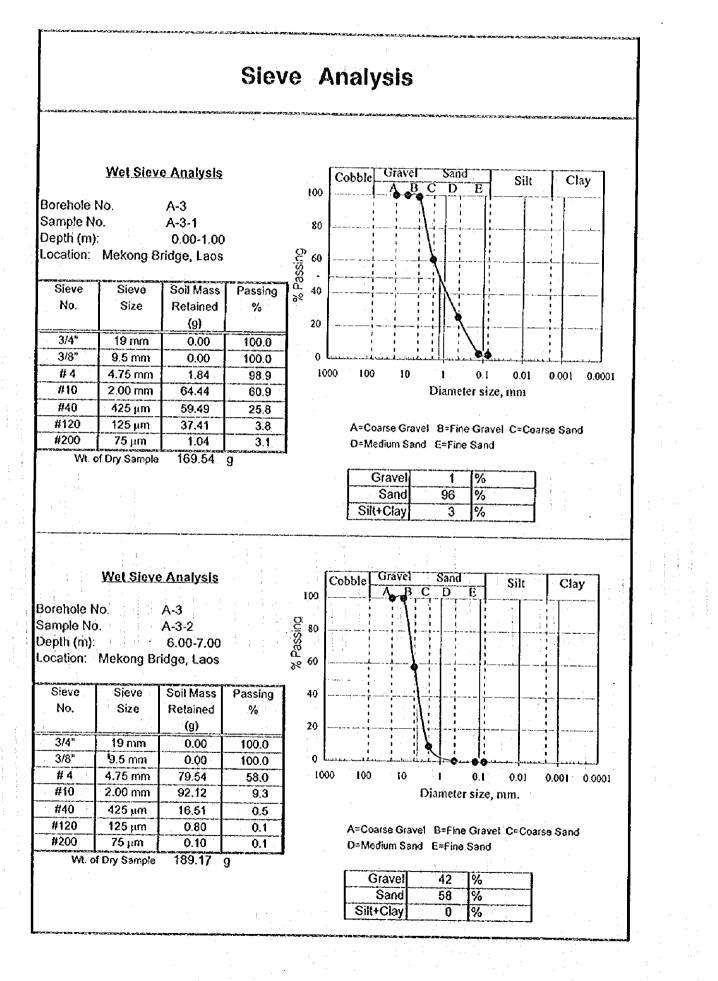
	D	RI	LL LO	3	PROJE	CT:	THE (EASIBI	RUCTI	ONO	F		SE		e no. Et no		C- OF_	{
ç	SITE		NE <u>C</u>		RDINATE DATE		,670,032. OM_10/1	· · · · · · · · · · · · · · · · · · ·			1			N <u>0</u> KONG			THC	-1
,			e core Very:	1(00 %		PTH	12. 108.		_M. M.		060	•		EESAK			
DATE	DEPTH	ELEVATION	ROCK TYPE OR FORMATION	NLUM			DESCRIP	NOITION			BIT & DIAMETER	GROUNDWATER LEVEL	& CORE <u>\$</u> RECOVERY		/ALUE 30 40	50	. SAMPLING	DEPTH
		101.39	SAND		FINE TO M	EDIUMIN	GRAIN SIZ	e, medium		1.20 M.	NEW CONN							 _ 1
	2_					······												2
10/12/95	3. - 4_		MUDSTONE, SANDSTONE ALTERNATIO		STRIPE T ALTERNA	EXTURE	UR, TUFF C MUDSTON NTERVALS (20 - 2.00 M.	E AND SANU OF 2-5 MM, 1	STONE		DIAMOND BIT 76 MM.		***					- 3 - 3 - 4
	5_	97.99					• •			5.20 M.	ð						-	5 6
	78						END OF H											- 7
12/10/05	9_ 10_ 11_																	9 10
	12_ 13_																62-2	12
	14 15	-				:						:			:			14

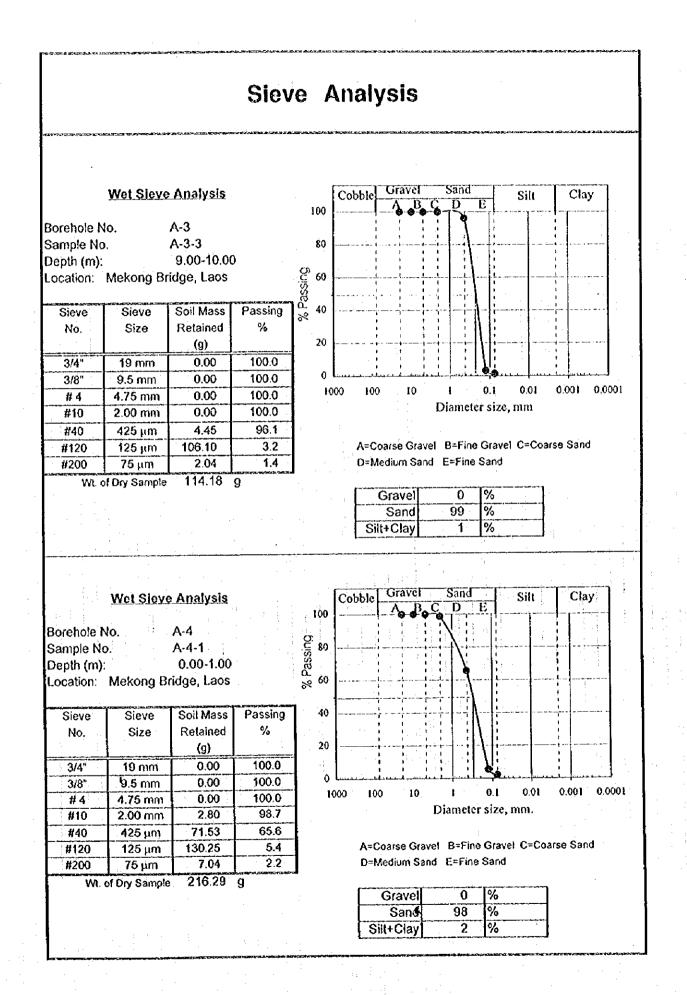
	D	RI	ll LO	G	PROJE	CT:	THE C	EASIBII ONSTR IEKON(UCTIO	ON C)F		(SE		1.1	e no et n	I	C- OF	
SI	ſΕ	LI	INE_C		RDINATE DATE		,669,973.9 OM_25/09					NĊLI	NAT	ION	Ô	DRILL	RIG	THO	2-1
A١				1	00 %		PTH		:00 :50	_M. M.		DRILI LOGO				EESA			
	RE		VERY:	<u> </u>	· · · · · · · · · · · · · · · · · · ·					_1×1.									
Depth		ELEVATION	ROCK TYPE OR FORMATIO				DESCRIPT	ION			BIT & DIAMETER	GROUNDWATER LEVEL	% CORE	N N N N N N N N N N N N N N N N N N N	N-V 10 20	40 40	.50	SAMPLING	DEPTH
1	- 95	55	CLAYEY SIL	т	CONSIST	ENCY, ME	BROWN IN CO EDIUM WATER HIGH ROOTS	R CONTENT	FIN LOW	00 M.						╧━┺┲┨╌┽╖			
2		3,35	SILTY CLAY		FIRM TO S	STIFF IN C , MEDIUN ED WEAT	, YELLOWISH COSISTENCY M PLASTICITY THERED GRA	, MEDIUM V (WITH FRA	vater Gment (VN	•	DRAG BIT 3*	3.00				•		C-5-1	_ 2 _ 3
4	-	2 20	SANDSTONE		SIZE, MOI WEATHER	ERATEL) ED, MICA	IN COLOUR, 1 Y HARD, MOE A PARTICLE II LAMINATION	ERATELY	GRAIN K GENTLY	33 M	76 MM.		*	••••		•			4
5			MUDSTONE		- 35 JOINT - BEDDING - RQD = 8	AT 3.45 / DIP 5 AT	М.	IN BEUUIN	/		DIAMOND BIT 7			8 N	. 1	*		<u>C-62</u>	_ 5
6	90).35			SLIGHTLY	WEATH	N COLOUR, S ERED, SLIGH ME TUFF OR	TLY POROL	· · ·	20 M.			*	· 					6
7 8 8					- CLOSE : 5 00-5 20 - BEDDIN	SPACING M. G DIP 10 5, 4,85, 5.	WTH MN ST	>20 CM. AT AIN SURFA	CE AT										7
. g			· · · · ·			E	END OF HOLE												- 9
10						·													10
11												- 		.,	· · ·	•			11
12			:														•	1	12
13															-				13
14	-						 								· · · ·	:		- 	- 14

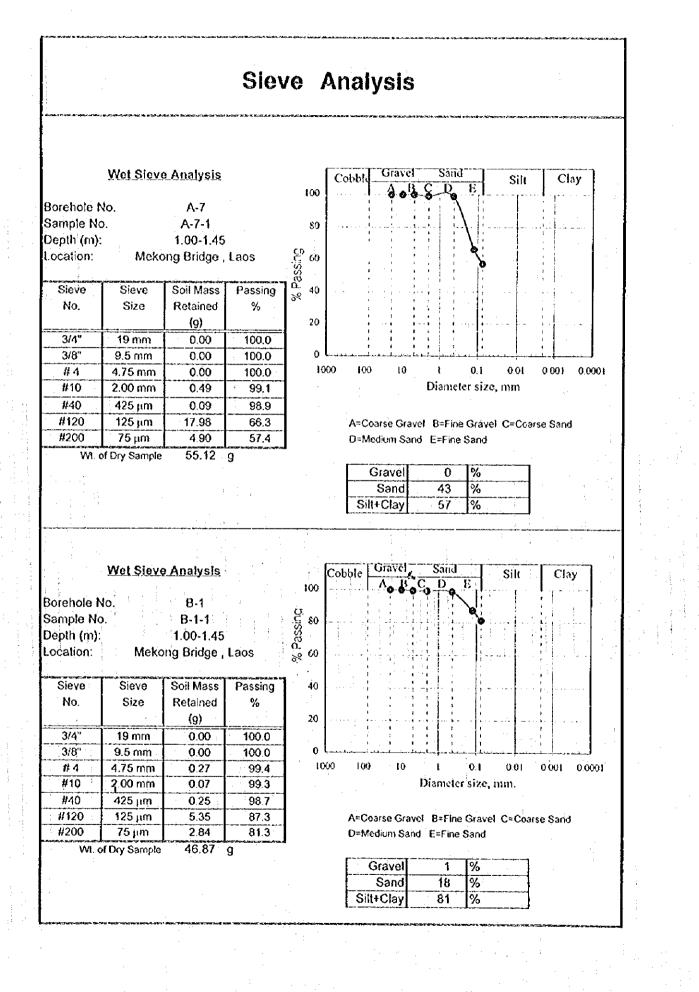
SITE	E	NE_C_		RDINATE DATE				3,587,477 [O23/0			NCLI		DN_1	j_df Apic	RILL RIG	; TH(>-1
		e core Very:		100 %		PTH		5.000 04.320	M. M.		.0GC		T	AWEE			
DEPTH	ELEVATION	ROCK TYPE OR FORMATION	MOLO			DESCRI	PTION		:	BIT & DIAMETER	GROUNDWATER LEVEL	CORE FECOVERY	-	N-VAI	LUE 0 40 50	SAMPLING	HLGHC
	03.32	SANO WITH SANOSTONE BOULDER	_	TOMED	JM IN GI	osit, brov Rain Size, Iedium de	GAP GRA		1.00 M.		1.20				- - - - -		-
- 53109/95		CLAY		DECOMP	ONTEN OSED M	T. IUDSTONE, ISH BROW	ORIGINR	OCK CHAN DUR, VERY	GED 2 00 M	DRAG BIT 3"						• · · · · · · · · · · · · · · · · · · ·	
4	102.32 99.32	MUDSTONE		SLIGHTU SOME TU - CLOSE	(WEATH FF ORK SPACING TICAL, 1	51N AT 2.00 5 FRACTU 60 - 70 ANG	CA PARTIC -3.77 M RE 6-20 CM	LE INCLUD	:	DIAMOND BIT 76 MM			300		•	<u>C7</u>	
6_					g dip 7 75 and	WITHIROP	I STAIN SU	IRFACE AT									
78						ENDOF	HOLE										
9_			1						:				•			-	-
· 10_	-							•	-		:						
11_														•	· . ·		
12_																	
13_ 14_																	
-							•										

	•		Sle	ve	A	nalysis	3		
	- - -	: Protection of Apple	м_марала	97. 27. 47. 447. 1979		an an an an an an an an an an an an an a	<u>1,</u>	37378 372789 <i>0</i> 948 <i>4</i> 947 6 94	5
	Wet Sleve	<u>e Analysis</u>		100		obble Gravel		E Silt	Claÿ
Borehole N	lo,	A-1							
Sample No	Ι,	A-1-1		80		·	╏─╁┤╌┼	·	
Depth (m):		2.00-4.45		C D			111		
Location:	Meko	ong Bridge,	Laos	% Passing			N, I I		·····
Sieve	Sieve	Soil Mass	Passing] 🖧 🕯			· · · · · · · ·		
No.	Size	Retained	%	° .					
		(g)		20					
3/4"	19 mm	0.00	100.0	- -					
3/8"	9.5 mm	0.00	100.0	0		ادەرى تە يەرەكەت. مە مە	u-l-frus	•	
#4	4.75 mm	0.00	100.0	1	.000	100 10	1	0.1 0.01	0.001 0.0001
#10	2.00 mm	0.66	99.1]			Diame	er size, mm	
#40 #120	425 µm	2.39	96.0	1				N.	a j
#120	<u>125 µm</u> 75 µm	7.79	<u> </u>	1				e Gravel C=Co	arse Sand
The Cold Street of Cold Street	f Dry Sample	76.31		J		D≟Mèdium Sar	nd EFFING	Sand	
	i biy bunpic	10.01	9			Gravel	0	1%	
i						Sand	14	%	
			1 - F			Silt+Clay	86	%	
	·					•		-td	
1			··· .	÷					
	Wat Slove	Analysis		i		LLL Gravel	Sand		
	TICL DIEVE	Allalysis		100	Co	bble Gravel	C D	E Silt	Clay
Borehole N	0.	A-6						8	
Sample No	•	A-6-1	1 (% Passing 09 08		1 8 8 1 8 1 8			
Depth (m):	1,14	2.00-3.50		ass					
Location:	Meko	ng Bridge,	Laos	₩ 60					
		-		· :					
Sieve No.	Sieve	Soil Mass	Passing	40		4	·· -· • • · • • • • • • • • • • • • • •	÷	
(10,	Size	Retained (g)	%	20	1				3
3/4"	19 mm	0.00	100.0			للا، بديرة المانية (1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1	1		
3/8"	9.5 mm	0.00	100.0		ليب ا	1			
#4	4.75 mm	0.00	100.0		000	100 10	1	0.1 0.01	0.001 0.0001
#10	2.00 mm	0.16	99.8	ł		· · · ·		size, mm.	
#40	425 µm	0.40	99.4						
#120	125 µm	2.49	96.9			A=Coarse Grav	rel B=Fine	Gravel C=Coa	arse Sand
#200	75 µm -	4.91	91.8			D=Medium San			
Wt. of	Dry Sample	97.26	9	-		·		<u>.</u>	
		;				Gravei	0	%	
						Sand	8	%	
						Silt+Clay	92	%	

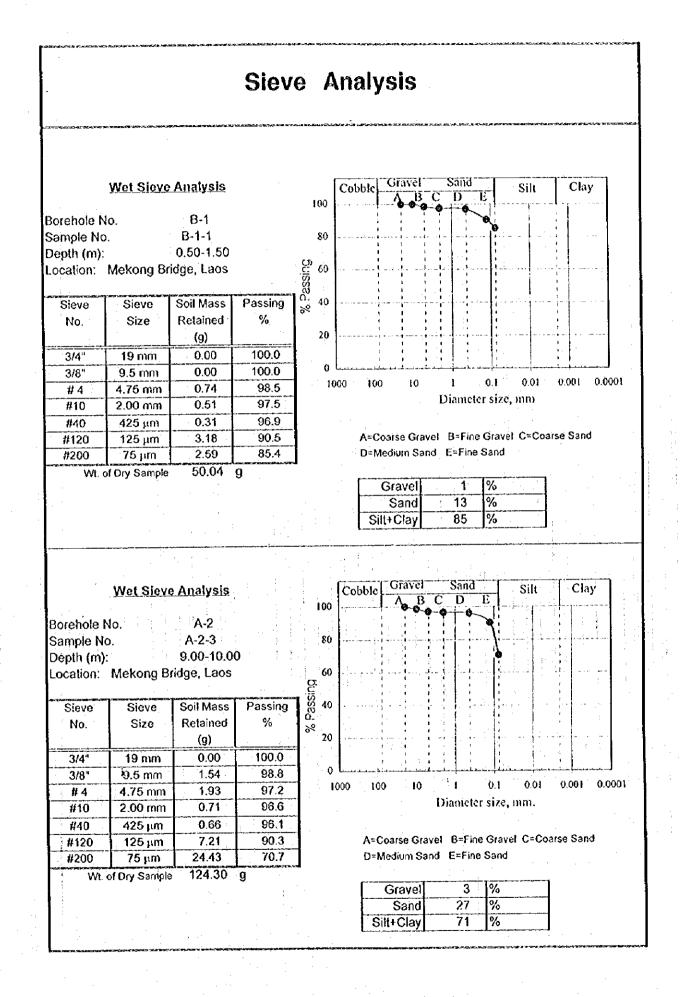
1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 -	aran prastatestates	nter star jacob in sin an	Siev	ve /	Analysis
	Wet Sieve	Analysis			Cobble Gravel Sand Silt Clay
	1101 01010	majoo		100	
3orehole N		A-2			
Sample No		A-2-1		80	
Depth (m):		1.00-1.45		· m ·	$\begin{bmatrix} 1 & 1 & 1 & 1 & 1 & 1 \\ 2 & 1 & 1 & 1 & 1 & 1 & 1 \\ 2 & 1 & 1 & 1 & 1 & 1 & 1 & 1 \end{bmatrix} = \begin{bmatrix} 1 & 1 & 1 & 1 \\ 1 & 1 & 1 & 1 & 1 \end{bmatrix}$
location:	Mekong Br	idge, Laos	· .	60 Bossed %	
Sieve	Sieve	Soil Mass	Passing	C2 40	
	Sieve	Retained	**************************************	~ ~	
No.	OIZC	(9)	10	20	
3/4"	19 mm	0.00	100.0		
3/4	9.5 mm	0.00	100.0	0	Laurente marifinder fanne fansk fanse
#4	4.75 mm	0.00	100.0	10	000 100 10 1 0.1 0.01 0.001 0.0001
#10	2.00 mm	0.00	100.0		Diameter size, mm
#40	425 µm	0.10	99.9		
#120	125 µm	1.44	99.1		A=Coarse Gravel B=Fine Gravel C=Coarse Sand
#200	75 μm	10.42	92.9		D=Medium Sand E=Fine Sand
Nan management	f Dry Sample	168.83	0	•	
			•		Gravel 0 %
					Sand 7 %
		1997 - 19			Silt+Clay 93 %
	<u></u>				
	Wet Sieve	Analysis			Cobble Gravel Sand Silt Clay
Darabata N	· · · ·			100	Cobble Gravel Sand Silt Clay
	\o.	A-2		1 E	Cobble Gravel Sand Silt Clay
Borehole N Sample No	√o. ⊃.	A-2 A-2-2		1 E	Cobble Gravel Sand Silt Clay
Sample No Depth (m):	√o. ⊃.	A-2 A-2-2 4.00-4.45		1 E	Cobble Gravel Sand Silt Clay
Sample No Depth (m):	√o. ⊃.	A-2 A-2-2 4.00-4.45		% Passing 09 00	Cobble Gravel Sand Silt Clay
Sample No Depth (m): Location:	No. D. Mekong B	A-2 A-2-2 4.00-4.45 ridge, Laos	Passion	% Passing 80	Cobble Gravel Sand Silt Clay
Sample No Depth (m): Location: Sieve	Vo. D. Mekong Bi Sieve	A-2 A-2-2 4.00-4.45 ridge, Laos Soit Mass	Passing %	1 E	Cobble Gravel Sand Silt Clay
Sample No Depth (m): Location:	No. D. Mekong B	A-2 A-2-2 4.00-4.45 ridge, Laos Soil Mass Retained	Passing %	50 80 50 80 60 40	Cobble Gravel Sand Silt Clay
Sample No Depth (m): Location: Sieve No.	No. D. Mekong B Sieve Size	A-2 A-2-2 4.00-4.45 ridge, Laos Soit Mass Retained (9)	%	50 80 50 80 60 40	Cobble Gravel Sand Silt Clay
Sample No Depth (m): Location: Sieve No. 3/4"	No. D. Mekong Br Sieve Size 19 mm	A-2 A-2-2 4.00-4.45 ridge, Laos Soit Mass Retained (9) 0.00	% 100.0	50 80 50 80 60 40	Cobble Gravel Sand Silt Clay
Sample No Depth (m): Location: Sieve No. 3/4" 3/8"	Vo. D. Sieve Size 19 mm 9.5 mm	A-2 A-2-2 4.00-4.45 ridge, Laos Soit Mass Retained (9) 0.00 0.00	% 100.0 100.0	500580 40 20 0	Cobble Gravel Sand Silt Clay
Sample No Depth (m): Location: Sieve No. <u>3/4"</u> <u>3/8"</u> # 4	Vo. D. Mekong Bi Sieve Size 19 mm 9.5 mm 4.75 mm	A-2 A-2-2 4.00-4.45 ridge, Laos Soil Mass Retained (9) 0.00 0.00 0.00	% 100.0 100.0 100.0	500580 40 20 0	Cobble Gravel Sand Silt Clay
Sample No Depth (m): Location: Sieve No. 3/4" 3/8" # 4 #10	No. D. Mekong Bi Sieve Size 19 mm 9.5 mm 4.75 mm 2.00 mm	A-2 A-2-2 4.00-4.45 ridge, Laos Soit Mass Retained (g) 0.00 0.00 0.00 0.13	% 100.0 100.0 100.0 99.9	500580 40 20 0	Cobble Gravel Sand Silt Clay A B C D E Silt Clay Image: Silt Image: Silt Image: Silt Clay Image: Silt Clay Image: Silt Image: Silt Image: Silt Image: Silt Clay Image: Silt Image: Silt Clay Image: Silt Image: Silt Image: Silt Image: Silt Clay Image: Silt Image: Silt Clay Image: Silt Image: S
Sample No Depth (m): Location: Sieve No. 3/4" 3/8" # 4 # 10 #40	No. Mekong Bi Sieve Size 19 mm 9.5 mm 4.75 mm 2.00 mm 425 µm	A-2 A-2-2 4.00-4.45 ridge, Laos Soil Mass Retained (9) 0.00 0.00 0.00 0.13 0.39	% 100.0 100.0 99.9 99.7	500580 40 20 0	Cobble Gravel Sand Silt Clay A B C D E Silt Clay Image: Silt Image: Silt Image: Silt Clay Image: Silt Clay Image: Silt Image: Silt Image: Silt Image: Silt Clay Image: Silt Image: Silt Clay Image: Silt Image: Silt Image: Silt Image: Silt Clay Image: Silt Image: Silt Clay Image: Silt Image: S
Sample No Depth (m): Location: Sieve No. 3/4" 3/8" # 4 #10 #40 #120	No. Mekong Bi Sieve Size 19 mm 9.5 mm 4.75 mm 2.00 mm 425 µm 125 µm	A-2 A-2-2 4.00-4.45 ridge, Laos Soit Mass Retained (9) 0.00 0.00 0.00 0.13 0.39 17.12	% 100.0 100.0 100.0 99.9 99.7 89.6	500580 40 20 0	Cobble Gravel Sand Silt Clay A B C D E Silt Clay A B C D E Silt Clay 000 100 10 1 0.1 0.001 0.0001 Diameter size, mm.
Sample No Depth (m): Location: Sieve No. 3/4" 3/8" # 4 #10 #40 #120 #200	No. Mekong Bi Sieve Size 19 mm 9.5 mm 4.75 mm 4.25 μm 125 μm 75 μm	A-2 A-2-2 4.00-4.45 ridge, Laos Soil Mass Retained (9) 0.00 0.00 0.00 0.00 0.13 0.39 17.12 59.74	% 100.0 100.0 99.9 99.7 89.6 54.4	500580 40 20 0	Cobble Gravel Sand Silt Clay A B C D E Silt Clay Cobble I O E Silt Clay I O I O I O I O I O I O I O I O I O I O
Sample No Depth (m): Location: Sieve No. 3/4" 3/8" # 4 # 10 # 40 # 120 # 200	No. Mekong Bi Sieve Size 19 mm 9.5 mm 4.75 mm 2.00 mm 425 µm 125 µm	A-2 A-2-2 4.00-4.45 ridge, Laos Soil Mass Retained (9) 0.00 0.00 0.00 0.00 0.13 0.39 17.12 59.74	% 100.0 100.0 100.0 99.9 99.7 89.6	500580 40 20 0	Cobble Gravel Sand Silt Clay A B C D E Silt Clay
Sample No Depth (m): Location: Sieve No. 3/4" 3/8" # 4 #10 #40 #120 #200	No. Mekong Bi Sieve Size 19 mm 9.5 mm 4.75 mm 4.25 μm 125 μm 75 μm	A-2 A-2-2 4.00-4.45 ridge, Laos Soil Mass Retained (9) 0.00 0.00 0.00 0.00 0.13 0.39 17.12 59.74	% 100.0 100.0 99.9 99.7 89.6 54.4	500580 40 20 0	Cobble Gravel Sand Silt Clay A B C D B Silt Clay A B C D Silt C

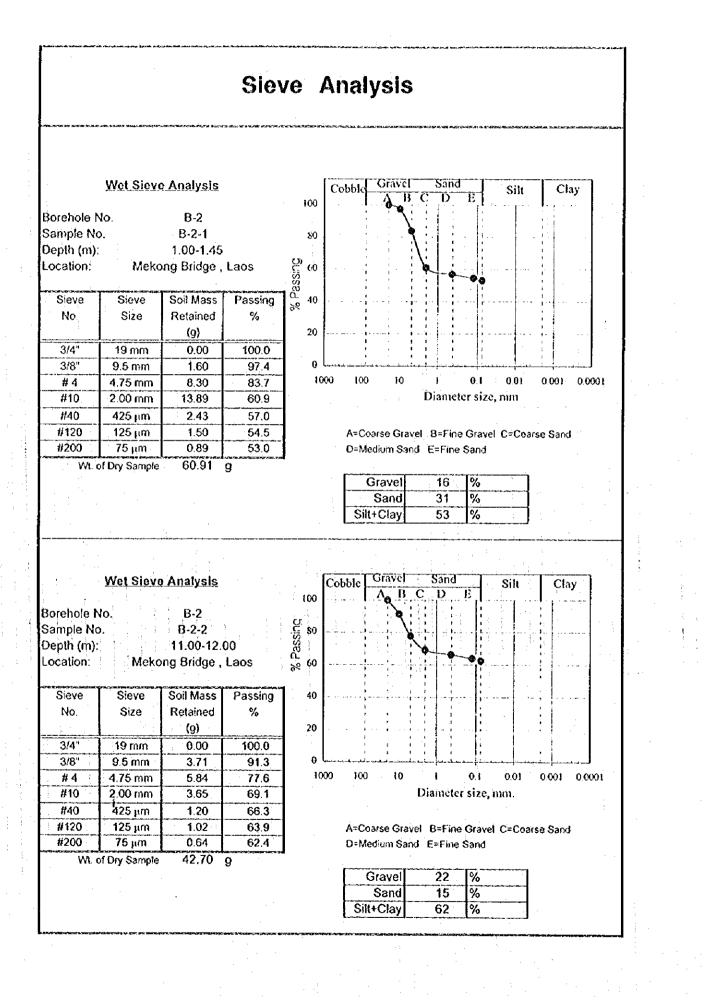




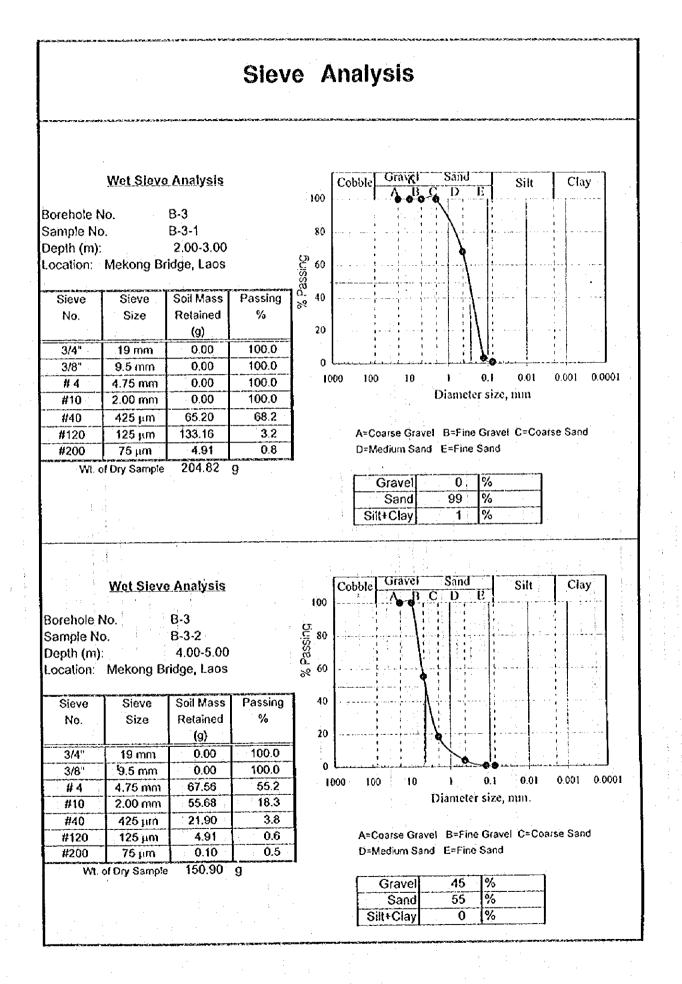


.



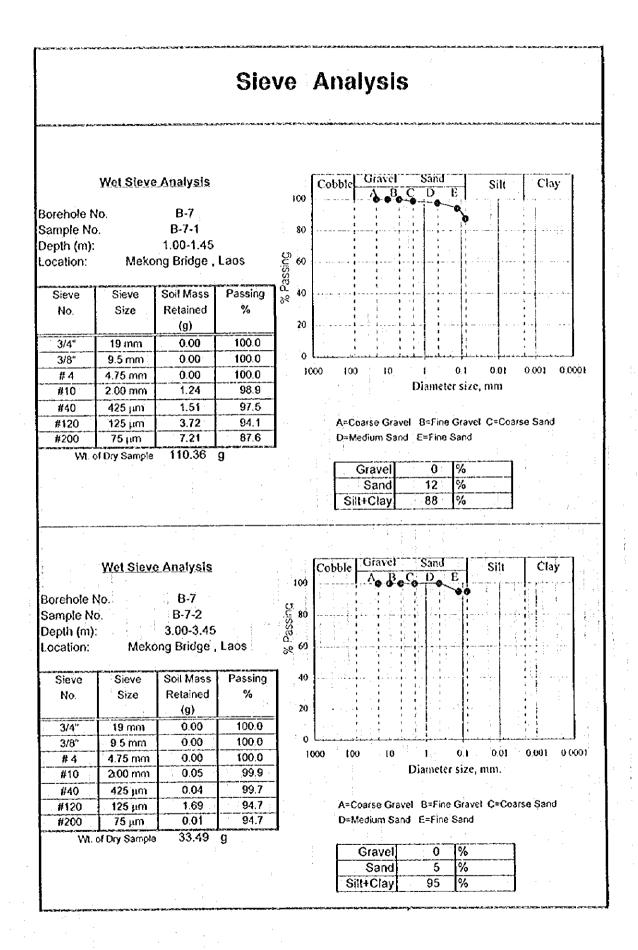


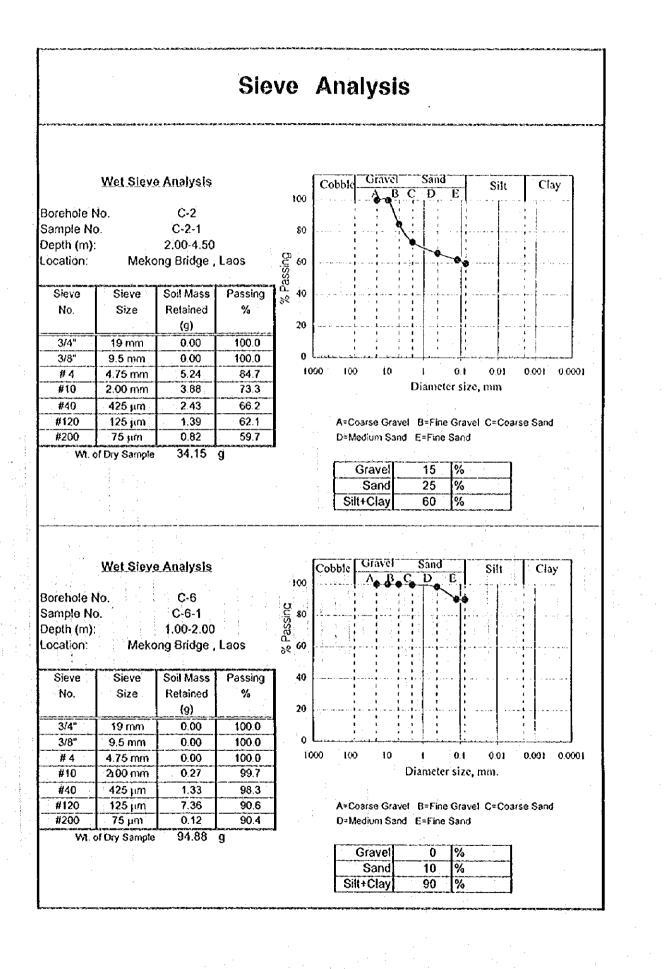
A 3-96



anananananan karanan ka	Slev	ve Analysis
Wet Sieve Analysis	5	Cobble Gravel Sand Silt Clay
Borehole No. B-4		
Sample No. B-4-1		80
Depth (m): 1.00-2.0	0	
Location: Mekong Bridge, Laos	5	0
Sieve Sieve Soil Mass	Passing	4 0
No. Size Relained	%	
(9)	<u> </u>	20
3/4" 19 mm 0.00	100.0	
3/8" 9.5 mm 0.00 #4 4.75 mm 0.00	100.0	
#4 4.75 mm 0.00 #10 2.00 mm 0.00	100.0	1000 100 10 1 0.1 0.01 0.001 0.0001 Diameter size, mm
#40 425 µm 24.02	88.9	
#120 125 μm 188.59	2.2	A=Coarse Gravel 8=Fine Gravel C=Coarse Sand
#200 75 µm 2.65	0.9	D=Medium Sand E=Fine Sand
Wt. of Dry Sample 217.32	g	
		Gravel 0 %
		Sand 99 %
		Silt+Clay 1 %
 A second sec second second sec	이 같은 것이 많이 있어?	
	1	
Wet Sieve Analysis		Cobble Gravel Sand Silt Clay
		Cobble Gravel Sand Silt Clay
Borehole No. B-5		100 A B C D E Shit Ciay
Borehole No. 8-5 Sample No. 8-5-1		100 A B C D E Shit Ciay
Borehole No. B-5		Coolic A D C D E Sht Clay
Borehole No. B-5 Sample No. B-5-1 Depth (m) 2.00-3.00 Jocation: Mekong Bridge, Laos		$\begin{array}{c} C \\ C \\ C \\ C \\ C \\ S \\ S \\ C \\ S \\ S \\$
Borehole No. 8-5 Sample No. 8-5-1 Depth (m) 2.00-3.00	Passing	100 A B C D E Shit Ciay
Borehole No. 8-5 Sample No. 8-5-1 Depth (m): 2.00-3.00 ocation: Mekong Bridge, Laos Sieve Sieve Soil Mass		$\begin{array}{c} C \\ C \\ C \\ C \\ C \\ S \\ S \\ C \\ S \\ S \\$
Borehole No. B-5 Sample No. B-5-1 Depth (m): 2.00-3.00 ocation: Mekong Bridge, Laos Sieve Sieve Soil Mass No. Size Retained (g) 3/4" 19 mm 0.00	Passing % 100.0	$\begin{array}{c} C \\ 100 \\ C \\ \hline \\ \hline \\ \hline \\ \hline \\ \hline \\ \hline \\ \hline \\ \hline \\ \hline$
Borehole No.B-5Sample No.B-5-1Depth (m):2.00-3.00.ocation:Mekong Bridge, LaosSieveSieveNo.SizeRetained(g)3/4"19 mm0.003/8"'9.5 mm0.00	Passing % 100.0 100.0	$\begin{array}{c} C \\ C \\ C \\ C \\ C \\ S \\ S \\ C \\ S \\ S \\$
Borehole No. B-5 Sample No. B-5-1 Depth (m) 2.00-3.00 .ocation: Mekong Bridge, Laos Sieve Sieve Soil Mass No. Size Retained .3/4" 19 mm 0.00 3/8" 9.5 mm 0.00 # 4 4.75 mm 0.00	Passing % 100.0 100.0 100.0	$\begin{array}{c} C \\ C \\ C \\ C \\ C \\ C \\ C \\ C \\ C \\ C $
Borehole No. B-5 Sample No. B-5-1 Depth (m) 2.00-3.00 .ocation: Mekong Bridge, Laos Sieve Sieve Soil Mass No. Size Relained 3/4" 19 mm 0.00 3/8" 9.5 mm 0.00 # 4 4.75 mm 0.00 #10 2.00 mm 0.00	Passing % 100.0 100.0 100.0 100.0	$\begin{array}{c} C \\ C \\ C \\ C \\ C \\ S \\ S \\ C \\ S \\ S \\$
Borehole No. B-5 Sample No. B-5-1 Depth (m) 2.00-3.00 .ocation: Mekong Bridge, Laos Sieve Sieve Soil Mass No. Size Relained 3/4" 19 mm 0.00 3/8" 9.5 mm 0.00 # 4 4.75 mm 0.00 # 40 425 µm 0.73	Passing % 100.0 100.0 100.0 100.0 99.6	$ \begin{array}{c} $
Borehole No. B-5 Sample No. B-5-1 Depth (m) 2.00-3.00 .ocation: Mekong Bridge, Laos Sieve Sieve Soil Mass No. Size Relained 3/4" 19 mm 0.00 3/8" 9.5 mm 0.00 # 4 4.75 mm 0.00 #10 2.00 mm 0.00	Passing % 100.0 100.0 100.0 100.0	$\begin{array}{c} c \\ c \\ c \\ c \\ c \\ c \\ c \\ c \\ c \\ c$
Borehole No. B-5 Sample No. B-5-1 Depth (m) 2.00-3.00 .ocation: Mekong Bridge, Laos Sieve Sieve Soil Mass No. Size Relained (g) 3/4" 19 mm 0.00 3/8" 9.5 mm 0.00 #4 4.75 mm 0.00 #10 2.00 mm 0.00 #40 425 µm 0.73 #120 125 µm 193.04	Passing % 100.0 100.0 100.0 100.0 99.6 1.7 0.6	$ \begin{array}{c} $
Borehole No. B-5 Sample No. B-5-1 Depth (m) 2.00-3.00 .ocation: Mekong Bridge, Laos Sieve Sieve Soil Mass No. Size Relained (g) 3/4" 19 mm 0.00 3/8" 9.5 mm 0.00 #4 4.75 mm 0.00 #10 2.00 mm 0.00 #40 425 µm 0.73 #120 125 µm 193.04 #200 75 µm 2.22	Passing % 100.0 100.0 100.0 100.0 99.6 1.7 0.6	$\begin{array}{c} Could \\ \hline \\ \hline \\ \hline \\ \hline \\ \hline \\ \hline \\ \hline \\ \hline \\ \hline \\ $
Borehole No. B-5 Sample No. B-5-1 Depth (m) 2.00-3.00 .ocation: Mekong Bridge, Laos Sieve Sieve Soil Mass No. Size Relained (g) 3/4" 19 mm 0.00 3/8" 9.5 mm 0.00 #4 4.75 mm 0.00 #10 2.00 mm 0.00 #40 425 µm 0.73 #120 125 µm 193.04 #200 75 µm 2.22	Passing % 100.0 100.0 100.0 100.0 99.6 1.7 0.6	$ \begin{array}{c} $
Borehole No. B-5 Sample No. B-5-1 Depth (m) 2.00-3.00 .ocation: Mekong Bridge, Laos Sieve Sieve Soil Mass No. Size Relained (g) 3/4" 19 mm 0.00 3/8" 9.5 mm 0.00 #4 4.75 mm 0.00 #10 2.00 mm 0.00 #40 425 µm 0.73 #120 125 µm 193.04 #200 75 µm 2.22	Passing % 100.0 100.0 100.0 100.0 99.6 1.7 0.6	$\begin{array}{c} Could \\ \hline \\ \hline \\ \hline \\ \hline \\ \hline \\ \hline \\ \hline \\ \hline \\ \hline \\ $
Borehole No. B-5 Sample No. B-5-1 Depth (m) 2.00-3.00 .ocation: Mekong Bridge, Laos Sieve Sieve Soil Mass No. Size Relained (g) 3/4" 19 mm 0.00 3/8" 9.5 mm 0.00 #4 4.75 mm 0.00 #10 2.00 mm 0.00 #40 425 µm 0.73 #120 125 µm 193.04 #200 75 µm 2.22	Passing % 100.0 100.0 100.0 100.0 99.6 1.7 0.6	$ \begin{array}{c} $

and which have not been a second of the seco





Specific Gravity

Depth (m) From Image: state of the stat	요. 슈. 프, 카드/드니/Ya 등 , 사실하는 요. 드, 특성가입니(우), 유가 유리 등 주 등 등 등 등 등 등 등 등 등 등 등 등 등 등 등 등 등		ente control de la control de						,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	eren an da state an da state	
Dublement Art Cold B71 A74 B21 C221 B111 A641 B22 B71 To To<				6 77	A '7			011	<u> </u>	82	B. 7
Sample Ro Ref R											8-7-2
To D37 D29 D53 D63 D19 D56 D6 D39 D17 D7 Wt of Container 18.16 15.9 15.85 16.55 16.09 17.27 14.58 16.95 14.86 24.3 Wt of Container 18.16 15.9 15.85 16.55 16.09 17.27 14.58 16.95 14.86 24.4 Wt of Container 18.16 15.9 101 76.11 131 18.97 90.26 93.28 90.52 87.74 71. Wt of Dry Soil 74.91 85.05 60.32 114.4 73.88 72.99 73.7 73.57 72.88 46.2 Flask No. A B C D E A B C 10.1 87.74 71.3 16.95 161.05 194.7 101.3 585 Flask + Soil 582.9 572.2 554.4 585.3 561 596.9 610.5 594.7 601.3 582 <t< td=""><td></td><td>A-1-1</td><td>0-6-1</td><td>8-7-1</td><td>A-7-1</td><td>D-2-1</td><td>0-2-1</td><td>D-1-1</td><td>7.0.1</td><td>0-2-2</td><td></td></t<>		A-1-1	0-6-1	8-7-1	A-7-1	D-2-1	0-2-1	D-1-1	7.0.1	0-2-2	
Container No. D57 D29 D63 D63 D19 D56 D6 D39 D17 D7 Wt of Container 18:16 15.9 15.85 16.55 16.09 17.27 14.58 16.95 14.86 24.3 Wt of Container 18:16 15.9 15.85 16.55 16.09 17.27 14.58 16.95 18.95 18.95 18.95 18.95 14.41 73.88 72.99 78.57 73.57 74.26 26.5 26.5 27.42 2.770 2.676 2.699 2.774 2.6 <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>											
Wit of Container 18.16 15.9 15.85 16.05 17.27 14.58 16.95 14.86 24.1 Wit of Container 18.16 15.9 15.85 16.05 16.09 17.27 14.58 16.95 17.27 14.58 16.95 17.27 14.58 16.95 17.27 14.58 16.95 17.27 14.58 16.95 17.27 14.58 16.95 17.27 17.27 17.37 77.357 72.88 46.1 Wit of Dry Soil 74.91 85.05 60.32 114.4 73.88 72.99 78.7 73.57 72.88 46.1 15.9 15.9 16.95 26.5 26.5 26.5 26.5 26.5 26.5 26.5 26.5 26.5 26.5 26.5 26.5 26.5 26.5 26.5 26.5 26.5 26.5 27.7 27 27.75 27 27.6 2.676 2.689 2.774 2.6 26.5 2.774 2.6 2.5 2.605 2.742 2.770 2.676 2.689 2.774 2.6 2.676 2.676 2.689	<u>_</u>						0.00		- 000	047	D70
Wit of Contrainer 90.7 101 76.17 131 89.97 90.26 93.28 90.52 87.74 71 Wit of Controlly Soil 74.91 85.05 60.32 114.4 73.88 72.99 78.7 73.57 72.88 46. Flask No. A B C D E A B C D E Temporature, C 25 27 27 27.5 27 26.5 26.6 27.74 2.6 Specific Gravity, Gs 2.748 2.625 2.608 2.565 2.742 2.770 2.676 2.689 2.774 2.6 Sample No.		· · · · · · · · · · · · · · · · · · ·									
Wt. of Control by Soli 76.7 73.67 72.88 46. Wt. of Dry Soli 74.91 85.05 60.32 114.4 73.88 72.99 78.7 73.67 72.88 46. Flask No. A B C D E A B C ·D. E Temperature, C 25 27 27 27.5 27 26 26.5 26.5 26.5 26.5 27.87 601.3 59.7 Wt. of Water + 121.4 135.1 140.3 135.9 137.5 107.2 93.5 109.1 96.78 95. Flask + Soil 563.9 572.2 554.4 585.3 561 596.9 610.5 594.7 601.3 58 Flask + water											
With of Dy Soli Original Solid Differentiation A B C · D. E Flask No. A B C D E A B · C · D. E Temperature, C 25 27 27 27.5 27 26 26.5 26.5 26.5 26.5 27.8 95. Flask + Soil 583.9 572.2 554.4 585.3 561 596.9 610.5 594.7 601.3 582 Flask + water -									and a second second		
Temperature, C 25 27 27 26 28.5 26.5 27.6 27.5 27 26 28.5 26.5 27.6 29.5 107.2 93.5 109.1 96.78 95.7 Flask + Soil 583.9 572.2 554.4 585.3 561 596.9 610.5 594.7 601.3 585.7 Flask + water								an in some some or to state			
Temperature, C 20 21 <td>· · · · · · · · · · · · · · · · · · ·</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1</td> <td></td> <td></td>	· · · · · · · · · · · · · · · · · · ·								1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		
Wit of Water + 12.14 135.1 145.5 156.5											
Flask + Soli 50.5 512.2 50.74 50.55 50.74	Wt. of Water +				and the second second second second second second second second second second second second second second second						
Specific Gravity, Gs 2.748 2.625 2.608 2.565 2.742 2.770 2.676 2.689 2.774 2.6 Borehole No.	Flask + Soil	583.9	572.2	554.4	585.3	561	596.9	610.5	594.7	601.3	585.8
Borehole No. Sample No. Sample No. Sample No. Depth (m) From Sample No. To Sample No. Wt of Container Sample No. Wt of Container Sample No. Temperature, C Sample No. Flask + Soil Sample No. Specific Gravity, Gs Sample No.	Flask+water										·
Borehole No. 2.746 2.020 2.000 <td></td> <td></td> <td></td> <td>· · · · · · · · · · · · · · · · · · ·</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>0.017</td>				· · · · · · · · · · · · · · · · · · ·							0.017
Sample No. Depth (m) From To Container No. Wt of Container Wt of Container Wt of Continer Wt of Dry Soil Flask No. Temperature, C Wt. of Water + Flask + Soil Flask + Soil Flask + Soil Specific Gravity, Gs	Specific Gravity, Gs	2.748	2.625	2.608	2.565	2.742	2.770	2.676	2.689	2.774	2.677
Sample No.	anna hAraparan an		A AND REAL PROPERTY OF A DESCRIPTION OF A DESCRIPTION OF A DESCRIPTION OF A DESCRIPTION OF A DESCRIPTION OF A D	an share a shere a she							
Depth (m) From	Borehole No.	CALCELON								<u>;</u>	
Depth (m) From To Image: Container No. Wt of Container Image: Container No. Wt of Cont+Dry Soil Image: Container No. Wt of Dry Soil Image: Container No. Flask No. Image: Container No. Temperature, C Image: Container No. Wt of Water + Image: Container No. Flask + Soil Image: Container No. Flask + Soil Image: Container No. Specific Gravity, Gs Image: Container No. Image: Container No. Image: Container No. Image: Container No	Sample No.			<u> </u>							
Container No. Wt of Container Wt of Cont+Dry Soil	Depth (m) From	·							· · · ·		
Wt of Container	То			I			L				
Wt. of Cont+Dry Soil	Container No.										
Wt. of Dry Soil	Wt of Container										
Wt. of Dry Soil					· · ·			·			· · · · · · · · · · · · · · · · · · ·
Flask No.				1							
Wt. of Water +			1								
Flask + Soil Flask + water Specific Gravity, Gs Borehole No. Sample No. Depth (m)	Temperature, C									. <u></u>	
Flask+water Specific Gravity, Gs Borehole No. Sample No. Depth (m)	Wt. of Water +		4		:		·				
Specific Gravity, Gs Borehole No. Sample No. Depth (m)	Flask + Soil						i			·	·
Specific Gravity, Gs Borehole No. Sample No. Depth (m)	Flask+water			· · · · ·			·				
Specific Gravity, Gs Borehole No. Sample No. Depth (m)					· · · ·					·	
Borehole No. Sample No. Depth (m) From				1							
Sample No	Specific Gravity, Gs										
Sample No	and a second second and a second second second second second second second second second second second second s						and the state of the state of the state of the state of the state of the state of the state of the state of the			and the second second second second second second second second second second second second second second secon	
Sample No	Borehole No.	and a state of the					1		ļ	ļ	
Depth (m) From		1									1
						1	· · · · · · · · ·	ļ			·
				1		<u> </u>	<u> </u>	<u> </u>		<u> </u>	<u> </u>
Container No.	Container No.		1					<u> </u>	 	ļ	
Wt of Container		1	1					_			<u> </u>
Wt. of Cont+Dry Soil		1					1	_	<u> </u>	· · ·	
Wt. of Dry Soil											
Flask No.		1								_	
Temperature, C		· · ·							_	ļ	.
Wt. of Water +		1						<u></u>			
Flask + Soil		1						<u> </u>		 	
Flask+water							: 			.	
					<u> </u>						
Specific Gravity, Gs	Specific Gravity, Gs								1	<u> </u>	L

Specific Gravity

ana amanga ang na sa	e estatuto e adarte doma	. United international states of the			entropy and the second second second second	n managan sa stanan singa	reract desider similari	alle filter destrict alle Site	-	-
The state of the s	ana ana amin'ny soratra dia ma	Internation College	-	-1.20 Mar. 1. 10 Mar. 1.			-		-	
Borehole No.	B-3	8-3 ·	8-4	B-5	A-2	A-2	A-3	A-3	A-3	A-4
Sample No.	B-3-1	B-3-2	B-4-1	B-5-1	A-2-1	A-2-2	A-3-1	A-3-2	A-3-3	A-4-1
Depth (m) From	1.00	3.00	2.00	3.00	0.00	4.00	1.00	5.00	10.00	1.00
То	2.00	4.00	3.00	4.00	1.00	4.45	2.00	6.00	11.00	2.00
Container No.	D-73	D-123	D-140	D30	D-70	D72	D-71	D-82	D 115	D-62
Wt of Container	27.71	22.58	23.16	14.58	24.17	20.69	27.82	21.78	22.59	15.68
Wt. of Cont+Dry Soil	74.17	192.49	155.24	247.57	176.11	229.75	187.97	146.88	112.79	167.87
Wt. of Dry Soil	46.46	169.91	132.08	232.99	151.94	209.06	160.15	125.1	90.2	152.19
Flask No.	A	B	С	C	D	E	E	A	8	С
Temperature, C	26	26	26	27.5	26.5	28	26	27	27	27
Wt. of Water +	65.37	167.7	153.5	240.15	148.81	184.04	152.84	142.86	140.61	143.39
Flask + Soil	620.88	592.82	587.11	562.31	598.37	598.72	600.96	591.97	570.51	609.23
: .										
Specific Gravity, Gs	2.635	2.641	2.684	2.642	2.697	2.685	2.754	2.627	2.675	2.662
na population de la compacta de la compacta de la compacta de la compacta de la compacta de la compacta de la c	and the second second	A RADING A DESCRIPTION	lan makanan sarat	korenne se enveri	anneria esta association de la companya de la companya de la companya de la companya de la companya de la comp	Lacot whith restricts at	angangan sing di kanan di kanan di kanan di kanan di kanan di kanan di kanan di kanan di kanan di kanan di kana			and the second full have
Borehole No.	8-1	A-2				a ayaa sagagaa caaayaa	and a subscription of the		o ve colline b êlt é	
Sample No.	B-1-1	A-2-3								
Depth (m) From	0.5	9								
To	1.5	10								
Container No.	D-2	D-4								
Wt of Container	14.99	19.1								
Wt. of Cont+Dry Soil	53.25	117.3							. 	
Wt. of Dry Soil	38.26	98.2					;			
Flask No.	A	В		·····						
Temperature, C	27	27		· · ·	·					÷ .
Wt. of Water +	213.08	220,47			1					<u> </u>
Flask + Soil	468.00	495.62						•	· · · · · ·	
	100.00	100.02			i					
						······································			·	
Specific Gravity, Gs	2.654				· · · ·					

Project:	Mekong River Br	idge, Laos		— — A.— A.—.B.1	Tested by: Date:	THS Dec-95	Sheet No:
Location:	<u></u>	· · · · · · · · · · · · · · · · · · ·			Date.	Dec-35	
Test No:	CARLE BUILDING FROM STATES			In the second second second second second			
Borehole No	:	A-1	A-1	A-1	A-1	A-6	A-6
Sample No:		A-1-1	A-1-1	A-1-1	A-1-1	A-6-1	A-6-1
Depth (m.)	From	2.00	2.00	2.00	2.00	2.00	2.00
	То	4.45	4.45	4.45	4.45	3.50	3.50
Tin No:		8-57	B-38	B-10	B-47	B-46	8-3
Wt. of Tin	gm.	21.89	20.88	21.07	21.09	21.03	22.24
Wt. of Tin +	Wet Soil gm.	83.40	72.31	162.23	156.27	96.90	131.60
Wt. of Tin +	Dry Soil gm.	73.02	63.55	138.24	133.64	87.68	119.44
Wt. of Water	gm.	10.38	8.76	23.99	22.63	9.22	12.16
Wt. of Dry S	oil gm	51.13	42.67	117.17	112.55	66.65	97.20
Water Cont	ent %	20.3	20.5	20.5	20.1	13.8	12.5
Sample Heig	uht cm.	an an an an an an an an an an an an an a	CALCELE SCOTTER STREET	7.15	7.15		
Sample Diar				3.53	3.53		
Wt. of Wet S			•••••	141.16	135.18		
Volume of S	and the second se			69.98	69.98		
	Neight ton/m ³			2.02	1.93		
Dry Unit W				1.67	1.61		
and a state of the second second second second second second second second second second second second second s	ĸĸĸŧŢĸĸġĸġĸġĸġĸĸĸĸĸĸĸĸĸġĸĸĸŢġ'nĸŊĸĸĸĸĸĸĸĸŀ	an an an an an an an an an an an an an a	anant, a bayan yang dan generatan kanang sang sang				
Test No:			er an an an an an Anton Calific with a provide a matrix is an	L DA LA MARINA			
Borehole No	D:	A-7	A-7	A-7	A-7	B-1	B-1
Sample No:		A-7-1	A-7-1	A-7-1	A-7-1	B-1-1	B-1-1
Depth (m.)	From	1.00	1.00	1.00	1.00	1.00	1.00
	То	1.45	1.45	1.45	1.45	1.45	1.45
Tin No:		B-30	8-1	B-58	B-16	B-4	8-8
Wt. of Tin	gm.	21.16	20.96	21.91	20.75	22.11	22.17
Wt. of Tin +		151.31	152.33	59.04	86.73	71.10	75.31
Wt. of Tin +		132.01	134.46	53.90	77.20	63.90	66.48
Wt. of Wate	er gm.	19.30	17.87	5.14	9.53	7.20	8.83
Wt. of Dry S	a dag shi a shi na ƙwalar ƙasar ƙasar	110.85	113.50	31.99	56.45	41.79	44.31
Water Con		17.4	15.7	16.1	16.9	17.2	19.9
Sample Hei	ight cm.	7.15	7.15				
Sample Dia		3.53	3.53				
Wt. of Wet		130.15	131.37				
Volume of \$	a a an inclusion and a second firm that the	69.98	69.98				
	Weight ton/m ³	1.86	1.88				
Dry Unit W		1.58	1.62		T		

Designation Mar	lena Diver	7 - ² - 4					
	ekong River I	snage			Tested by:	THS	Sheet No:
Location. Pa	kse, Laos				Date:	Dec-95	2
Test No:	CEN ALCON DE LE MARCHE	A	B	A	B	A	B
Borehole No:		A-2	A-2	A-3	A-3	A3	
Sample No:		A-2-3	A-2-3	A-3-1	A-3-1	A3 A-3-2	A3
Depth (m.)	From	9.00	9.00	0.00	1.00	5.00	A-3-2 6.00
	To	10.00	10.00	1.00	2.00	6.00	7.00
Tin No:		D4	D5	D-75	D 71	D-82	D-68
Wt. of Tin	ġm.	19.10	15.94	25.43	24.82	21.78	23.73
Wt. of Tin + Wet		142.43	167.58	225.13	216.30	151.81	222.01
Wt. of Tin + Dry		117.37	139.75	194.97	187.97	146.88	212.31
Wt. of Water	gm.	25.06	27.83	30.16	28.33	4.93	9.70
Wt. of Dry Soil	gm.	98.27	123.81	169.54	163.15	125.10	188.58
Water Content	%	25.5	22.5	17.8	17.4	3.9	5.1
Sample Height	CN).					V.V Winderstammen	4,1
Sample Diamete			•				· · · · · · · · · · · · · · · · · · ·
Wt. of Wet Soil	gm.						· · · · · · · · · · · · · · · · · · ·
Volume of Samp		· · ··· ···· ····		· · · · · · · · · · ·			
Total Unit Weig							
Dry Unit Weigh							
Dry Onit Weight		and Andra Market Strategy and a strategy and					
Test No:		A	B	A	B	A	8 1
Borehole No:	· ·	A-3	A-3	A-4	A-4	B-1	B-1
Sample No:		A-3-3	A-3-3	A-4-1	A-4-1	B-1-1	8-1-1
Depth (m.)	From	9.00	10.00	0.00	1.00	0.50	0.50
	То	10.00	11.00	1.00	2.00	1.50	1.50
Tin No:		D-81	D-115	D-44 .	D-62	D-1	D-2
Wt. of Tin	gnı.	21.41	22.59	15.94	15.68	13.67	14.99
Wt. of Tin + Wet	Soil gm.	163.50	135.14	279.51	198.03	71.86	60.07
Wt. of Tin + Dry	Soil gm.	135.59	112.79	232.23	167.87	63.35	53.32
Wt. of Water	gm.	27.91	22.35	47.28	30.16	8.51	6.75
Wt. of Dry Soil	gn).	114.18	90.20	216.29	152.19	49.68	38.33
Water Content	%	24.4	24.8	21.9	19.8	17.1	17.6
Sample Height	CM.			a an an an an an an an an an an an an an		and a subsect of the second second second second second second second second second second second second second	
Sample Diamete	r cm.						
Wt. of Wet Soil	gm.						
Volume of Samp							
Total Unit Welg	ht ton/m³						
Dry Unit Weigh							
and and a state of the state of	and a subserve of the subsection of the subsection of the subsection of the subsection of the subsection of the	\$-0.000 AND AND -0.000 AND -0.000		And the second state of th	Law and the second second second second second second second second second second second second second second s		

Project:	Mekong Bridge,	Laos			Tested by:	THS .	Sheet No:
Location:					Date:	Dec-95	2
				a service and the service of the ser	Land Barbook Provide State State State		and a construction of the second second second second second second second second second second second second s
Test No:	an an an an Anna an Anna an Anna an Anna an Anna an Anna an Anna an Anna an Anna an Anna an Anna an Anna an Ann			· · · · · · · · · · · · · · · · · · ·			
Borehole No:		B-2	B-2	B-2	B-2	8-7	B-7
Sample No:		B-2-1	B-2-1	B-2-2	8-2-2	8-7-1	B-7-1
Depth (m.)	From	1.00	1.00	11.00	11.00	1.00	1.00
	To	1.45	1,45	12.00	12.00	1.45	1.45
Tin No:		B-2	B-5	B-50	B-43	8-61	B-59
Wt. of Tin	gm.	25.60	21.53	21.15	21.05	22.02	20.98
Wt. of Tin + W		76.16	67.21	68.22	76.93	79.43	80.35
Wt. of Tin + D	and a second sec	61.19	53.45	54.62	59.59	70.82	71.69
Wt. of Water	gm.	14.97	13.76	13.60	17.34	8.61	8.66
Wt. of Dry Soi	and the second second second second second second second second second second second second second second second	35.59	31.92	33.47	38.54	48.80	50.71
Water Conter		42.1	43.1	40.6	45.0	17.6	17.1
Sample Heigh			Carlos and a second state of the	THE COLOR OF THE REAL PROPERTY OF		COMPACE SINCE STREET, STRE	
Sample Diam	a second of the second of the second	*** · ····		······			
Wt. of Wet So					and a second second second second second second second second second second second second second second second		
Volume of Sal		· · · · · · · · · · · · · · · · · · ·	1				
		l			1		
and the second	eight ton/m ³		· · · · · · · · · · · · · · · · · · ·				
Dry Unit Wei	ght ton/m ³		A THE REAL PROPERTY OF	a germanica se estado po to accurato		<u>****</u> >#################################	The second second second second second second second second second second second second second second second s
Track May	المتعادي المحادث المعادي والمحادث والمحادث والمحادث والمحادث والمحادث والمحادث والمحادث والمحادث والمحادث والم		and the second second second second second second second second second second second second second second second		2	[
Test No:		B-7	8.7	C-2	C-2	C-6	<u></u>
Borehole No:		B-7-2	B-7-2	C-2-1	C-2-1	C-6-1	
Sample No:		3.00	3.00	2.00	2.00	1.00	
Depth (m.)	From To	3.45	3.45	4.50	4.50	2.00	· · · · · · · · · · · · · · · · · · ·
	10	L	B-77	8-7	B-18	8101	
Tin No:		B-28	21.40	21.21	20.84	17.94	
Wt. of Tin	gm.	21.05	70.78	86.67	77.94	122.08	
Wt. of Tin + V	the same of the second se	75.48	64.03	68.16	61.40	100.85	
Wt. of Tin + D	وجسعه وآورهم دراهاريا فأرز	67.91	6.75	18.51	16.54	21.23	
Wt. of Water	gm.	7.57	1	46.95	40.56	82.91	1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 -
Wt. of Dry So		46.86	42.63	<u></u>	40.33	25.6	1
Water Conte		16.2	15.8	39.4	40.0	23.0	
Sample Heigl					·		
Sample Diam					-		
Wt. of Wet Sc							
Volume of Sa		<u> </u>	<u> </u>	<u> </u>	<u> </u>	<u> </u>	+
Total Unit W	eight ton/m ³			<u> </u>			
Dry Unit Wei			T			l	
	And the second s				an in the state of	and a state of the second second second second second second second second second second second second second s	

a A Galant BON: Burker in spirywyny o	N: & STAR SECT CALL-A. & A. ()	England, direction and statements and statements	3.58 8.46 75 12 1945 37.5 % C		gan mangagangan na minang man	and the second second second second second second second second second second second second second second second	
Project:	Mekong River I	Bridge			Tested by:	THS	Sheet No:
Location:	Pakse, Laos				Date:	Dec-95	1
Test No:	78.2727 - 744 - 745 - 746 - 747 - 748 - 747 - 747 - 747 - 747 - 747 - 747 - 747 - 747 - 747 - 747 - 747 - 747 - -	A state and a second seco	В	A	B	A	8
Borehole No:	· · · · · · · · · · · · · · · · · · ·	B-3	B-3	8-3	B-3	B-4	B-4
Sample No:	·····	B-3-1	B-3-1	B-3-2	8-3-2	B-4-1	B-4-1
Depth (m.)	From	1.00	2.00	3.00	4.00	1.00	2.00
	То	2.00	3.00	4.00	5.00	2.00	3 00
Tín No:		D-73	D-76	D-123	D-64	D-77	D-140
Wt. of Tin	gm.	27.71	28.72	22.58	23.36	21.25	23.16
Wt. of Tin + V	Net Soil gm.	84.26	279.22	217.63	182.02	289.05	183.66
Wt. of Tin + I		74.07	233.54	192.49	174.26	238.57	155.24
Wt. of Water	gm.	10.19	45.68	25.14	7.76	50.48	28.42
Wt. of Dry Sc	oil gm.	46.36	204.82	169.91	150.90	217.32	132.08
Water Conte	ent %	22.0	22.3	14.8	5.1	23.2	21.5
Sample Heig	ht cm.			an an talain an	and a state of the	andre and a second second second second second second second second second second second second second second s	a an an an an an an an an an an an an an
Sample Dian	neter cm.						
Wt. of Wet S	oil gm.			· · · · · · · · · · · · · · · · · · ·			
Volume of Sa	ample cc.				· · · · · · · · · · · · · · · · · · ·		Second States
Total Unit W	leight ton/m³						
Dry Unit We	ight ton/m ³	-			ar allenia (1) anna 20, 21, 22, 22, 22, 22, 22, 22, 22, 22, 22		
			-		an an an an an an an an an an an an an a	an an an an an an an an an an an an an a	
Test No:		A	B	A	B	<u> </u>	В
Borehole No:	· · · · · · · · · · · · · · · · · · ·	B-5	B-5	A-2	A-2	A-2	A-2
Sample No:		8-5-1	B-5-1	A-2-1	A-2-1	A-2-2	A-2-2
Depth (m.)	From	2.00	3.00	0.00	1.00	4.00	4.00
	То	3.00	4.00	1.00	1.45	4.45	5.45
Tin No:	· · · · · · · · · · · · · · · · · · ·	D-86	D-30	D-70	D-65	D-79	D-72
Wt. of Tin	gm.	21.80	14.58	24.17	22.42	21.44	20.69
Wt of Tin + V	-	270.77	315.70	206.08	222.92	291.34	280.48
WL of Tin + E	Dry Soil gm.	219.02	247.60	176,11	191.25	241.54	231.20
Wt. of Water	gm.	51.75	68.10	29.97	31.67	49.80	49.28
Wt. of Dry Sc	o <mark>il gm</mark> .	197.22	233.02	151.94	168.83	220.10	210.51
Water Conte	ent %	26.2	29.2	19.7	18.8	22.6	23.4
Sample Heig	en en en la marca de la composición de la composición de la composición de la composición de la composición de						and and an an an array of the second
Sample Diam	neter cm.			- · · · · · · · ·		······································	· · · · · · · · · · · · · · · · · · ·
Wt. of Wet Sc	oil gm.				· · · · · · · · · · · · · · · · · · ·		
Volume of Sa	emple cc.						···· •• · · · · · · · · · · ·
Total Unit W	eight ton/m ³				•		
Ory Unit Wei	ight ton/m ³						

Atterberg Limits

a martin dunin araightiga an an an an an an an an an an an an an	a provinsi and and an and a sub-	andra a the state of the state	indensi arabiyak wasirini ma	1 Ing 1997 Ang 1997 A	an ang bergan ang ang ang ang ang ang ang ang ang	and a spinor house of the same	an tha an an tain an Arabahan a
Borehole No.	A-1	<u></u>		darita ș ficator cultur	n andre andre de crystanse		
Sample No.	A-1-1	ω	»		ω		
Test No./Blows		Test 1	Test 2	33	28	22	15
A set of the set of	3m.	20.71	21.08	20.78	20.65	25.74	20.88
Wet soil + cont., g	and a second second second second second second second second second second second second second second second	30.82	31.29	28.92	29.75	34.69	30.59
Dry soil + cont., g	— — — — — — — — — — — — — — — — — — —	28.89	29.39	25.91	26.35	31.39	26.8
ຍ. ຍ	%	23.59	22.86	58.67	59.65	58.41	64.02
	verage	23.			59	.8	
Borehole No.	A-6		n men mennen in schwaler af stiefelt die CoteCote	and the second second second second second second second second second second second second second second secon	ar allen ander af soler fall andere fall an	, and a start desired and a start of the	
Sample No.	A-6-1	ω	• · · · · · · · · · · · · · · · · · · ·	[ω		
Test No /Blows		Test 1	Test 2	34	26	18	10
	gm.	20.78	20.81	20.94	21.04	21.75	25.58
Wet soil + cont.,		34.27	33.8	34.02	32.16	32	38.25
Dry soil + cont., g	2	32.19	31.87	31.25	29.68	29.69	35.27
00 00 00 00 00 00 00 00 00 00 00 00 00	%	18.23	17.45	26.87	28.70	29.09	30.75
a ser se transfer anna a ser se de l'he fier de la ser se transfer de la ser se de la ser de la ser de la ser s	verage	17		<u></u>	28	.2	<u> </u>
Borehole No.	A-7	render ber hernen stemmer in Albeit statet	TAN ADDA WANTON DATA		de 305 para suis 6.1000 international seus	99699 2020 2020 2020 2020 2020 2020 2020	
Sample No.	Λ-7-1	ω	р Р	[(0	۰ <u>۲</u>	
Test No./Blows		Test 1	Test 2	34	28	21	15
· · · · · · · · · · · · · · · · · · ·	gm.	22.17	20.98	20.82	21.66	21.42	21.62
Wet soil + cont.,		31.99	33.2	28.09	30.66	30.14	30.45
Dry soil + cont.	2 al run 'nors'e i	30.3	31.04	25.54	27.47	26.97	27.13
(U _n	%	20.79	21.47	54.03	54.91	57.12	60.25
A	verage	21	.1	La-m	56.1	<u></u>	
Borehole No.	B-1	Constant of the second se		an an an an an an an an an an an an an a	an an an an an an an an an an an an an a		
Sample No.	B-1-1	ω	P		6)L	
Test No./Blows		Test 1	Test 2	36	26	20	14
the second second second second second second second second second second second second second second second se	gm.	20.61	21.86	20.93	20.8	20.92	20.69
Wet soil + cont.,	-The second end of the	29.92	31.87	31.96	31.14	31.85	32.5
Dry soil + cont.	The second secon	28.78	30.63	29.69	29	29.53	29.95
0 _p	%	13.95	14.14	25.91	26.10	26.95	27.54
and the second second second second second second second second second second second second second second secon	Verage	14	.0		26	5.4	
Borehole No.	B-7						and a second second second second second second second second second second second second second second second
Sample No.	B-7-1	ω	P		6) _ເ	
Test No /Blows		Test 1	Test 2	30	23	14	: 14
a fair and a second second second second second second second second second second second second second second	gm.	20.71	21.97	20.82	21.13	20.77	20.77
Wet soil + cont.	Carl and a second second second	30.81	29.56	29.54	29.89	31.41	31.41
Dry soil + cont.	Carlor and a second second	29.51	28.51	27.5	27.75	28.65	28.65
	%	1 <u></u>	16.06	30.54	32.33	35.03	35.03
	The state of the s	40	.4		31.7		
- WHERE BE ALL CONTRACTOR OF THE REAL PROPERTY OF T	\verage i i	R 13	2T	and an address of the state of		and the second state of th	
- WHERE AN ADDRESS OF THE OWNER AND ADDRESS OF THE OWNER.	Average B-7	31	n				
1	the second second second second second second second second second second second second second second second se	CI ()		<u> </u>	0	01.7	
8orehole No. Sample No.	B-7			18	0 26	⁰ 1./ 18	12
Borehole No. Sample No. Test No./Blows	B-7 B-7-2)p	18 20.82		<u> </u>	20.83
Borehole No. Sample No. Test No./Blows Container,	B-7 B-7-2 gm	(c) Test 1	Test 2		26	18	20.83 30.69
Borehole No. Sample No. Test No./Blows Container, Wet soil + cont.,	B-7 B-7-2 gm. gm.	C Test 1 22.42	Pr Test 2 23.25	20.82	26 22.11	18 20.82	20.83
Borehole No. Sample No. Test No./Blows Container,	B-7 B-7-2 gm. gm.	Test 1 22.42 35.13 33.03	Test 2 23.25 34.77	20.82 29.16	26 22.11 30.53	18 20.82 29.16	20.83 30.69

Atterberg Limits

• -

Borchole No.	٨-2		Samp	le No.	A-2-1			
	() _p		(*	([,])[.			
Fest No. /Blows	Test 1	Test 2	36	27	20 '	12		
Container, gan.	20.89	20.7	21.07	20.83	20.69	20.89		
Wet soil + cont., gan.	31.01	30.2	31.2	31.09	33.98	31.78		
Dry soil + cont., gm.	29.05	28.38	28.38	28.18	30,19	28.52		
Water Content, 6, (%)	24.02	23.70	38.58	39.59	39.89	12.73		
ω _ρ	23.9	в.		(v ₁	39.7	° _G		
and a state of the state of t				·				
Borehole No.	۸-2		Stamp	le No.	٨-2-2	9999-9929-9949-994-994-994-994-9		
	(:)p		(?)				
Test No. /Blows	Test 1	Test 2	32	26	20	12		
Container, gm.	22.08	20.76	20.66	20.61	20.98	20.68		
Wet soit + cont., gm	33.61	34.56	31.95	31.73	32.75	33.98		
Dry soil + cont., gm.	31.8	32.39	29.76	29.55	30.38	31.19		
Water Content, io. (%)	18.62	18.66	24.07	24.38	25.21	26.55		
(i)p	18.6	96		ω	24.6	° ć		
Borchole No.	Λ-2		Samp	le No.	Λ-2-3			
ana an an an an an an an an an an an an	t			والمراجع المراجع المراجع والمحافظ المحافظ المحافظ المحافظ المحافظ والمحافظ والمحافظ المحافظ المحافظ والمحافظ المحافظ والمحافظ والمح	. San , Mari, winan she wat she yer ying a she a she he was may say ay.			
	(((0)				
Test No./Blows	Test I	Test 2	32	24	18	12		
Container, gm.	20.75	21.01	21.63	20.92	21.04	21.79		
Wet soil + cont., gm.	31.03	33.87	31.65	34.89	31.83	37.62		
Dry soil + cont., gm.	29.48	31.95	29.71	32.19	29.69	34.36		
Water Content, we (%)	17.75	17.55	24.01	23.96	21.71	25.93		
(Up	17.7	: %		σ	24.2	• • •		

ASIAN INSTITUTE OF TECHNOLOGY GEOTECHNICAL ENGINEERING LABORATORY

Unioxial Compressive Strength

Geotechnical Investigation of Mekong Bridge at Pakse in Laos Date : 17 Nove 1995 Bamp's Type **Sandslone** Sample No. A-2 Diameter, cm 5.42 Langth/Diaineter 2 101.42 Uniaxial Compressive Birongth, MPa Axial Stain at 50% of Fallure Stress, % 0.35 Radial Strain at 60% of Failure Strass, % Q.CB Tangent Modulus at 50% of Failure Stress, GPa 19.79 Secant Modulus at 50% of Failure Stress, OPa 15.08 Poisson's Ratio at 50% of Failure Stress 0.28 Water Content at Test Condition, % 0.91 100 οQ 80 And al 70 Axial 80-SPOS STA 50 40 30 20 10 oţ 0.1 02 93 04 0.5 0.0 0.7 0.0 81:a'n, % Testad and Forwarded By Approved ilidan Indra Jworchan Ur. Noppadol Phionwej Laboratory Coordinator Laboratory Supervisor

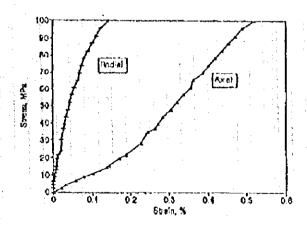
ASIAN INSTITUTE OF TECHNOLOGY GEOTECHNICAL ENGINEERING LABORATORY

Unlaxial Compressive Strength

Geotechnical Investigation of Mekong Bridge at Pakse in Laos

Osts: 17 Nov 1995

Sample Type	Sandstone
9amp'a No.	8.8
Olamatér, cm	5.42
Length/Diameter	2 13
Uniaxial Compressive Strength, MPa	\$9.69
Axial Stain at 50% of Falluro Bleas, 15	0.31
Rediel Strain at 50% of Fallure Stress, N	0.04
Tangent Modulus at 60% of Failure Stress, GPa	25.85
Secant Modulus at 50% of Failure Stress, GPs	16.03
Paisson's Ratio at 50% of Failura Strass	0.13
Water Content at Test Condition, %	0.77



Testad and Forwarded By

Indra Jworchán Laboratory Supervisor

Appro Dr. Noppzool/Phienwej

Laboratory Coordinator

SCHOOL OF CIVIL ENGINEERING GEOTECHNICAL ENGINEERING LABORATORY

UNIAXIAL COMPRESSIVE STRENGTH

Geotechnical Investigation of Mekong Bridge at Pakse in Laos

Date : 20 Dec 199

Sample No.	A-3-4	8-4-2	B-5-2
Sample Type	Sandstone	Mudstone	Mudstone
Dlameter, cm	5,44	5.44	5.36
Length/Diameter	2.14	2.02	2.17
Total Unit Weight, kN/m3	25.72	25.78	28.24
Uniaxial Compressive Strength, MPa	55.07	43.02	34,57
Water Content at Test Condition, %	0,97	1,22	2.21

Tested By : Sangwan Y.

Forwarded By

Indra Jworchan Laboratory Supervisor

Approved By, DrDannia Belgado Laboratory Coordinator

SCHOOL OF CIVIL ENGINEERING GEOTECHNICAL ENGINEERING LABORATORY

UNIAXIAL COMPRESSIVE STRENGTH

Geotechnical Investigation of Mekong Bridge at Pakse in Laos

Date : 20 Dec 1995 Sample No. A.7-2 C-1-1 C-2-2 C-6-2 C-7-1 Sample Type Sandston Sandston Sandston Slitetone Mudelone Diameter, cm 5.38 5,43 5.41 5.38 5.42 Length/Dlameter 2.27 2.23 2.17 2.26 2.17 Total Unit Weight, kN/m3 24.54 25.67 25.01 24.54 25.37 Uniaxial Compressive Strength, MP 58.07 48.80 80.03 24.63 57.22 Water Content at Test Condition, % 1.85 0.08 0.45 1 87 1.64

Tested By : Sangwan Y.

Forwarded By

Monteni-

Iridra Jworchan Laboratory Supervisor

Approved By Dr Dennis Belgado Laboratory Coordinator

A 3-112

TABLE A.5-1 PRESENT OD TABLE BY VEHICLE TYPE (1/2)

VC																				
)	D		1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	Tot
	1		0	44	31	6	148	1	1	0	1	14	0	0	1	0 0	56 0	0	0	30
	2		4	0	4 0	-1	2	0	0 0	0	0 0	2	0	ő	0	õ	5	ŏ	0	1
	3		7 3	1 1	5	ő	0	õ	ō.	ŏ	ŏ	1	ŏ	Ť	1	ŏ	Ő	ŏ	ŏ	1
	. 4	14		3	3	ĩ	85	7	4	1	ŏ	2	ŏ	Ó	- 0	ŏ	86	ō	ō	3
	6		1	ŏ	Ŭ.	, 0	3	0	12	1	Ö	ō	0	Ō	0	0	0	Ó	Ó	
	7		ò	Ō	0	ō	1	7	0	3	0	0	0	0	÷ 0	0	0	0	0	
	8		ō.	0	0	0	0	0	2	0	0	0	0	• •	0	0	0	· 0	0	
	. 9		1	1	1	Q -	0	0	0	0	0	4	0	0	- 0	0	0	0	0	
	.10	•.	6	11	2	1	1	0	0	0	2	0	0	- O	0	0	2	. 0	0	
	11		1	0	1	1	0	0	0	0	0	1	Ó	3	E 1	0	0	0	0	
	12		0	0	1	2	0	0	0	0	0	0	1	. 0	2	0	3	0	0	
	13		2	16	27	30	5	2	2	1	2	6	5	49	0	0	1	0	0	1
	14		0	0	0	0	0	0	. 0	0	0	0	0	0	0	0	0	0	0	1
	15		54	0	0	0	73	0	0	0	0	0	0	0	0 0	0	0	0 · 0	0	1
	16		0	0	0	0	0	0	0	0	0	. 0	0	. 0 0	0	0	Ö	ŏ	ŏ	
	17		0	0 67	0 75	<u>0</u> 44	0	0	0 21	<u></u>	<u>0</u> 5	<u>0</u> 31	6	53		<u> </u>	153	ŏ		1,0
	Tola	25	24	01	/0	44	019		41		- J				<u> </u>			`	.	.,.
ight	t ·																-			
)	D		1	2	3	4	5	6	7	8	9	10	11	12	13	. 14	15	16	17	To
	1		0	30	13	3	9	1	• 0	0	1	8	0	0	2	0	42	0	0	1
	. 2		30	0	2	1	1	0	0	0	0	2	0.	0	2	0	0	0	0	
	3		12	2	0	3	1.	0	0	0	. 0	1	0	0	2	0	4	0	0	· .
	4		3	- 1	3	0	1	0.	0	0	0	1	::: 1 ∷::0	1	3	0	0 64	0 · 0	0	. (
	5		2	2	1	1	63	: 5	2	- 0, 1	0 0	- 1	0	- 0	0	Ő	· 0	· 0	0	· · · '
	6		1	0	0	0	2	0 8	8	2	0	õ	0	0	. 0	Ö	ŏ	÷ ŏ	' 0	
	7		0	0	0	0	. 0	· 1	- 2	ó	ŏ	, Õ	ō	- 0 .	ŏ	ŏ	ŏ	ō	ŏ	
	8		0	ō	ŏ	ŏ	ŏ	Ö	ō	· ŏ	÷Õ	2	ō	ō	ō	Ō	. 0	0	0	÷
	10		8	2	· 1	៍រំ	1	ŏ	Ŏ	ŏ	2	ō	ĩ	. 0	1	0	÷ 1	0	Ō	
•	់ាំ		õ	Ō	. ò	1	0	i Õ	ō	Ō	0	1	0	2	- 1	0	0	· 0	. 0	.*
	12		õ	0	0	1	0	0	0	0	.:0	: 0	: 2	0	8	0	2	· 0	· 0	
	13		2	3	3	4	1	0	0	: O.	1	11	2	10	0	0	1	. 0	÷ Ø	
-	14		0	0	0	. 0	0	0	0	0	0	0	0	0	0	0	<u> 0</u>	÷ 0	· . 0	÷ ÷
) i 1ŝ		40	0	0	: 0	55	0	Ō	0.1	0	0	0	0	0	0	• 0	, Ó	<u></u> 0	
	³ 16	; .	0	Ó	· 0	0	0	0	0	01	0	0	0	0	0	0	0	0	• 0	14
•	17		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
	Tota		99	40	23	15	135	15	12	3	4	17	6	13	20	0	114	0	0	5
					·				1	: 7									· .	
lus								· ·	7	8	9	10	11	12	13	14	15	16	17	T
)	D		1	2	3	<u> </u>	5	6	- 0	0	0	2	0	0	Ť	0	8	0	0	
	. 1		0 5	5 0	- 1	0	Ö	Ö.	, Õ	ŏ	ŏ	1	ŏ	õ	i 1	Ö Ö	Ō	0	0	
		: }	э 2	1	. 0	ť	Ö	ŏ	ŏ	ŏ	· Õ	0	ŏ	ō	· i	Ō	1	0	Û	14
			1	ò	- ĭ	·	ŏ	ŏ	ŏ	Ö	0	0	Ō	Ó	1	0	0	0	0	÷
	į		ò	Ő.	:0	ŏ	12	1	1	0	Ō	ŏ	: <u>0</u>	0	0	0	12	. Ö	0	
	ė		ŏ	0	ō	0	1	0	2	0	0	0	: Ò	Ó (0	.: 0	0	. 0	· 0	÷
			0	0	Ö	0	- 1 -	2	0	1	0	0	0	0	· 0	0	6 0	÷ 0	0	
		3	0	0	0	- 0	0	0	1	0	0) O	0	0	0	0	0	0	0	
	()	0	- O	0	0	0	0	0	0	0	1	· 0	ି 0	0	0	<u></u> 0	0	0	
	-1()	2	- E 1 -	0	0	0	0	0	0	1	0	0	0	0	. 0	0	0	0	
	. 11		0	0	0	0	0	0	0	0	0	0	. 0	1	. 1	0	0	• 0	0	
	1		0	0	0	0	0	0	0	0	0	. 0	1	0	3	0	0	0	0	
	1:		1	1	1	1	. 1	0	0	0	0	0	1	3	0	0	0	0	0	
	14		0	0	0	0	0	0	0	0	0	. 0	0	0	0	0	0 0	0 0	0	
	1!		8	0	0	0	10	0	0	0	0	0	0	0	0	0	0	0	ŏ	
	10		0	0	0	0	0	0	0	0	0	· 0	0	0	-	0	0	0	Ő	
	17	f	0	0	0	0	0	0 -	0	<u> </u>	-			· ·						
	Tola	1	19	8	- 5	3	25	3	- 4	1	1	4	2	4	8	0	21	0	· 0	

A.5-1

TABLE A.5-1 PRESENT OD TABLE BY VEHICLE TYPE (2/2)

	Ð	1	2	3	4	5	6	7	8	9	10	11	: 12	13	.14	15	16	17 -]
	1	0	5	2	1	31	0	0	0	0	2	0	0	1	0	19	0	0	
	2	5	0	1	0	1	0	0	0	0	1	0	0	1	0	0	Ó	0	
	3	2	0	0	1	0	0	0	0	0	0	· 0	0	1	0	2	0	0	
	4	1	0	1	0	0	0	0	0	0	0	0	0	1	0	0	0	0	
	5	30	1	0	0	28	2	1	0	· 0	0	× 0	0	1	0	28	0	0	
	6	. 0	0	0	0	1	0	2	. 0	0	÷ 0	0	0	0	0	0	0	0	
	7	0	0	0	0	1	1	0	. 0	0	0	· 0	0	0	0	0	0	0	
	8	0	0	0	0	0	0	0	0	. 0	0	0	0	0	0	0	0	0	
	9	0	0	0	0	0	0	0	· 0	0	: 1	0	0	0	0	0	0	0	
	10	2	0	0	0	0	0	0	0	1	0	• 0	0	0	0	1	0	0	
	11	0	0	0	0	0	0	0	0	0	0	0	1	1	0	0	0	0	
	12	. 0	0	0	0	0	0	0	0	0	0	1	0	3	0	1	0	0	
	13	1	1	. 1	2	1	0	0	0	0	1	1	4	0	0	0	0	0	
	14	0	0	0	0	. 0	0	0	0	0	0	0	0	0	0	0	0	0	
	15	18	0	0	: 0	24	0	0	0	0	0	0	0	0	0	0	0	0	
	16	. 0	0	0	0	. 0	0	0	0	0	0	0	0	0	0	0	0	0	
	17	. 0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
.	Tolai	59	7	5	4	87	3	3	0	1	. 5	2	5	9	0	51	0	0	
0	D 1	0	2 84	<u>3</u> 48	4	5 188	6	7	8	9	10 26	<u>11</u> 0	12	13	14	15 125	16 0	17	
	2	74	0	8	2	4	0	. 0	Ō	- 0	6	. Ŭ	ŏ.		-		· •		
·														5	Û	0	· 0	· 0	
	3	23	- 4	0	7	2	0	0	0	õ				5 4	0	0	0 0	0	
		23 8	4	0	7 0	2 1	0		0		2	0	0	4	0	12	0	Ó	
1	3		· · · ·					0		0					-			0	
	3 4	8	2	10	0	1	0	0	0	0 0	2 2	0 1	0 2	4	0	12 0	0	Ó	
	3 4 5	8 172	2 6	10 4	0 2	1 188	0 15	0 0 8	0 1	0 0 0	2 2 3	0 1 0	0 2 0	4 6 2	0 0 0	12 0 150	0 0 0	0 0 0	-
	3 4 5 6	8 172 2	2 6 0	10 4 0	0 2 0	1 188 7	0 15 0	0 0 8 24	0 1 2	0 0 0 0	2 2 3 0	0 1 0 0	0 2 0 0	4 6 2 0	0 0 0	12 0 190 0	0 0 0	0 0 0	
	3 4 5 6 7	8 172 2 0	2 6 0	10 4 0 0	0 2 0 0	1 188 7 4 0	0 15 0 18	0 0 8 24 0	0 1 2 6	0 0 0 0	2 2 3 0	0 1 0 0	0 2 0 0	4 6 2 0 0	0 0 0 0	12 0 190 0 0	0 0 0 0	0 0 0 0 0	
	3 4 5 6 7 8	8 172 2 0 0	2 6 0 0	10 4 0 0	0 2 0 0	1 188 7 4 0	0 15 0 18 1	0 0 8 24 0 5	0 1 2 6 0	0 0 0 0 0	2 2 3 0 0	0 1 0 0 0	0 2 0 0 0	4 6 2 0 0 0	0 0 0 0 0	12 0 190 0 0	0 0 0 0 0	0 0 0 0 0 0	
	3 4 5 6 7 8 9 10	8 172 2 0 0 2 18 1	2 6 0 0 1 4 0	10 4 0 0 0 1	0 2 0 0 0 2 2	1 188 7 4 0 0 2 0	0 15 0 18 1 0 0 0	0 8 24 0 5 0	0 1 2 6 0 0	0 0 0 0 0	2 2 3 0 0 8	0 1 0 0 0 0	0 2 0 0 0 0	4 2 0 0 0 0	0 0 0 0 0 0	12 0 190 0 0 0	0 0 0 0 0	0 0 0 0 0 0 0	
	3 4 5 6 7 8 9 10 11 12	8 172 2 0 0 2 18 1 0	2 6 0 1 4 0	10 4 0 0 1 3 1 1	0 2 0 0 0 2 2 3	1 188 7 4 0 0 2	0 15 0 18 1 0 0	0 8 24 0 5 0 0	0 1 2 6 0 0 0 0 0 0 0	0 0 0 0 0 0 6 0 0	2 3 0 0 0 8 0	0 1 0 0 0 0 0 1	0 2 0 0 0 0 0	4 6 2 0 0 0 0	0 0 0 0 0 0 0	12 0 190 0 0 0 4	0 0 0 0 0 0 0	0 0 0 0 0 0 0	
	3 4 5 6 7 8 9 10 11 12 13	8 172 2 0 0 2 18 1 0 16	2 6 0 1 4 0 21	10 4 0 0 1 3 1 1 32	0 2 0 0 2 2 3 37	1 188 7 4 0 2 0 0 8	0 15 0 18 1 0 0 0 0 2	0 0 8 24 0 5 0 0 0 0 0 2	0 1 2 6 0 0 0 0 0 0 1	0 0 0 0 0 0 6 0 0 3	2 2 3 0 0 0 8 0 2 0 8 0 2 0 8	0 1 0 0 0 0 1 0 5 9	0 2 0 0 0 0 0 7 0 66	4 6 2 0 0 0 0 1 4 16 0	0 0 0 0 0 0 0 0 0	12 0 150 0 0 0 4 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0	
	3 4 5 6 7 8 9 9 10 11 12 13 14	8 172 2 0 0 2 18 1 0 16 0	2 6 0 0 1 4 0 21 0	10 4 0 0 1 3 1 1 32 0	0 2 0 0 2 2 3 37 0	1 188 7 4 0 2 0 0 0 8 0	0 15 0 18 1 0 0 0 2 0	0 0 8 24 0 5 0 0 0 0 0 2 0	0 1 2 6 0 0 0 0 0 1 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	2 3 0 0 8 0 2 0 8 0 8 0 2 0 8 0	0 1 0 0 0 0 1 0 5 9 0	0 2 0 0 0 0 0 7 0 66 0	4 6 2 0 0 0 1 4 16	0 0 0 0 0 0 0 0 0 0	12 0 190 0 0 0 4 0 6	0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0	
	3 4 5 6 7 8 9 10 11 12 13 14 15	8 172 2 0 0 2 18 1 0 16 0 120	2 6 0 0 1 4 0 0 21 0 0	10 4 0 0 1 3 1 1 32 0 0	0 2 0 0 2 2 3 37 0 0	1 188 7 4 0 2 0 0 8 0 162	0 15 0 18 1 0 0 0 2 0 0	0 8 24 0 5 0 0 0 0 2 0 0	0 1 2 6 0 0 0 0 0 1 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	2 2 3 0 0 8 0 2 0 8 0 8 0 0	0 1 0 0 0 0 1 0 5 9 0 0	0 2 0 0 0 0 0 7 0 66 0 0	4 6 2 0 0 0 1 4 16 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0	12 0 150 0 0 0 4 0 6 2	0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0	
	3 4 5 6 7 8 9 10 11 12 13 14 15 16	8 172 2 0 2 18 1 0 16 0 120 0	2 6 0 1 4 0 21 0 0 0 0	10 4 0 0 1 3 1 1 32 0 0 0	0 2 0 0 2 2 3 37 0 0	1 188 7 4 0 2 0 0 8 0 162 0	0 15 0 18 1 0 0 0 2 0 0 0	0 8 24 0 5 0 0 0 2 0 0 0 0	0 1 2 6 0 0 0 0 0 1 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	2 3 0 0 8 0 2 0 8 0 8 0 2 0 8 0	0 1 0 0 0 0 1 0 5 9 0 0 0 0	0 2 0 0 0 0 0 7 0 66 0 0 0	4 6 2 0 0 0 0 1 4 16 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0	12 0 150 0 0 0 4 0 6 2 0	0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0	
	3 4 5 6 7 8 9 10 11 12 13 14 15	8 172 2 0 2 18 1 0 16 0 120 0 0	2 6 0 0 1 4 0 0 21 0 0	10 4 0 0 1 3 1 1 32 0 0	0 2 0 0 2 2 3 37 0 0	1 188 7 4 0 2 0 0 8 0 162	0 15 0 18 1 0 0 0 2 0 0	0 8 24 0 5 0 0 0 0 2 0 0	0 1 2 6 0 0 0 0 0 1 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	2 2 3 0 0 8 0 2 0 8 0 8 0 0	0 1 0 0 0 0 1 0 5 9 0 0	0 2 0 0 0 0 0 7 0 66 0 0	4 6 2 0 0 0 1 4 16 0 0 0		12 0 150 0 0 0 4 0 6 2 0	0 0 0 0 0 0 0 0 0 0 0 0		

A.5-2

TABLE A.5-2 FUTURE OD TABLE BY VEHICLE TYPE: ROUTE A (1/6) - YEAR 2000 -

M/C

) 1	5 1 -	2	•															
1			3	4.	5	6	7	8	- 9	10 20	<u>11</u> 0	12	13	14	15	<u>16</u> 0	17	Total 576
~	0	77	46	10	321 4	2	0	0.	0	3	ŏ	ŏ	24	õ	1	· ŏ	õ	107
2 3	66 43	0 6	6 0	1	6	Ö	ŏ	õ	ŏ	4	ŏ	ŏ	0	õ	19	ō	Ō	91
4	40 8	2	9	0	š	ŏ	ŏ	ō	ō	2	Ō	2	29	0	1	0	0	56
		5	4	1	173	8	4	. 1	0	3	0	0	. 1	0	110	0	0	644
6	2	1	1	• 0	10	0	17	i	0	0	0	0	0	0	0	0	0	33
. 7	2	- 1	· 0	0	3	21	0	5	0	-				-				34
8	1	0	; 0	0	0									+				10
9	2	1	1.			-		-	-					-				45
										-			-	· · ·				12
					A									-			Ō	49
		-								4	9	41	0	0	- 1	0	0	123
		1.1			ŏ	ō	Ó	0	0	Ó	0	0	0	0	0	0	0	0
		-	1	0	117	0	0	0	0	0	Ó	0	0	0	0	0	0	211
16	0	0	0	0	0	0	0	0	0	· 0	0	0	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0	0	0	0	0					0
Total	581	107	91	52	648	35	33	9	12	45	11	46	122	: 0	211	<u>, 0</u>	0	2,003
											· .			•				
D	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	Tola
	0			6	29	2	0	0	2	17	0	0	4	0	67	0	0	213
	59	0	4	2	3	0	Ŭ.	0	0	4	0	J 0	-1 4	0	· 0	0		76
3	25	4	0	6	2	0	0	0	Q	2	0			0				49
<u> </u>	6	2	6	0	2	0	0	0			1.1.1							27
5	6	5	2	2									1.1					24
6			-			-				-								21
					· · · ·									•				6
									· · · ·					0	0	0	0	7
		: T						÷ŏ		0	- 1	- 10	2	0	ⁱ . 1	0	0	35
					ō	Ō	0	· 0 ·	0	2	: 0	4	2	.0	· 0	0	0	i 10
	-	Ō	Ó	2	. 0	• 0	Ó	0	0	0	3	0		.0	3	0		20
13	: 3	: 4	5	. 5	1	0	0	0	- 1	1	2				1.1.1			37
14	0	0	0	0	0	0	0							-	1	-		162
15	85	0	0	0		1	-			11 1 2	- i -				. K.			102
			-					;			1.1			- 7.	- E.	1		· · · č
		<u> </u>	<u>``</u>	5 1 C									35	Ō	162	0	0	948
10(3)	201	10	49	13	201						:							
									•	· · ·		· .			12.			
D	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	Tola
1	0	8	3	2	0													30 12
2	7	0	1.1								· ·							Ş
	~								1									3
															. 0	0	0	
											0	0	0	0	Ó	0	0	. ³ (
					1			0	0	0	• 0	÷ 0	0	0	0	0	0	11
		ŏ	- Ō	Ō	• 0	0	0	0	0	2	• , 0	, Ó	0	0	0	0	0	1
	3	1	0	0	0	0	0	0	2	0	0	0		. 0	0		· ·	
11	0	0	0	0	0	Ő	0	0	0	: 0	0	1				-		
12	0	0	· 0	0	0	0	0	0	0	0	1	0	5	0	0	0	0	
40	1	1	2	2	1	0	0	0	0	0	2	5	0	0	0	0	0	.'
13		~	0	- 0	0	0	0	0	0	• 0	0	0	-	-			v	
14	0	0			4.0	~	. A	~	•	^		•	- A	- 0	A	- ` 0	0	
14 15	14	0	0	0	16	0	0	0	0 0	0	0	0 0	0	0) 0 0	0	
14					16 0- 0	0 0 0	0 -0 0	0	0 0 0	0 0 0	0	0 0 0	0	0	• 0			3 (
	5 6 7 8 9 10 11 12 13 14 15 16 17 Total D 1 2 3 4 5 6 7 8 9 10 11 12 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 Total D 1 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 Total D 1 1 12 13 14 15 16 17 Total D 1 1 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 7 Total D 1 1 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 7 Total D 11 12 12 13 14 15 16 17 7 Total D 11 12 12 17 7 7 8 9 10 11 12 13 14 15 16 17 7 7 8 9 10 11 12 12 13 14 15 16 17 7 7 8 9 10 11 12 12 13 14 15 16 17 7 7 8 9 10 11 12 2 3 4 5 6 7 8 9 10 11 12 2 3 4 5 11 12 12 13 14 15 16 17 7 7 8 9 10 11 12 2 3 4 5 6 7 8 9 10 11 12 2 3 4 5 6 7 8 9 10 11 12 2 3 4 5 6 7 8 9 10 11 1 2 2 3 4 5 16 7 7 8 9 10 11 1 2 2 3 4 5 16 7 7 8 9 10 11 1 2 2 3 4 5 16 7 7 8 9 10 11 1 2 2 3 4 5 5 6 7 8 9 10 11 1 2 2 3 4 5 5 6 7 8 9 10 11 1 2 2 3 14 5 5 6 7 7 8 9 10 11 1 2 2 3 14 5 7 7 7 8 9 10 11 1 12 7 7 7 8 9 10 11 1 12 7 7 8 9 10 11 1 12 7 7 7 7 8 9 10 17 7 8 1 10 11 1 1 1 1 1 1 11 11 11 11 11 11 1	5 333 6 2 7 2 8 1 9 2 10 22 11 1 12 0 13 10 14 0 15 91 16 0 17 0 Tolal 581 D 1 1 0 2 59 3 25 4 6 5 6 6 2 7 0 8 0 9 3 10 17 11 0 12 3 14 0 15 85 16 0 17 0 Total 207 D 1 0 2 10 1 1 0 2 7 3	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	5 333 5 4 1 6 2 1 1 0 7 2 i 0 0 8 1 0 0 0 9 2 1 1 0 10 22 3 4 2 11 1 0 1 3 13 10 10 17 22 14 0 0 0 0 15 91 1 1 0 16 0 0 0 0 7 0 0 0 0 7 0 0 0 0 7 0 0 0 0 7 0 0 0 0 7 0 0 0 0 7 0 0 0 0 7 0 0 0 0 7 0 0 0 0 9 3 <td>5 3333 5 4 1 173 6 2 1 1 0 10 7 2 1 0 0 3 8 1 0 0 0 1 10 22 3 4 2 3 11 1 0 1 1 1 12 0 1 3 1 1 12 0 0 1 3 1 13 10 10 17 22 3 14 0 0 0 0 0 15 91 1 1 0 117 16 0 0 0 0 0 17 0 0 0 0 0 16 2 6 0 2 2 3 25 4 0 6 2 4 6 2 6 0 2 3 3 0 <t< td=""><td>5 333 5 4 1 173 8 6 2 1 1 0 10 0 7 2 1 0 0 3 21 8 1 0 0 0 0 0 9 2 1 1 0 1 0 10 22 3 4 2 3 0 11 1 0 1 1 0 1 0 12 0 1 3 1 0 117 0 13 10 10 17 22 3 2 14 0 0 0 0 0 16 0 0 0 0 0 0 0 0 13 107 91 52 648 35 35 0 1 2 3 4 5 6 1 0 57 29 6 29 2 2 59</td><td>5 333 5 4 1 173 8 4 6 2 1 1 0 10 0 17 7 2 i 0 0 3 21 0 8 1 0 0 0 0 8 9 2 1 1 0 1 0 0 0 10 22 3 4 2 3 0 0 11 1 0 1 1 1 0 0 1 12 0 0 1 3 1 0 0 1 13 10 10 17 22 3 2 1 14 0 0 0 0 0 0 0 0 16 0 0 0 0 0 0 0 0 17 1 0 57 29 6 29 2 0 0 2 59</td><td>5 333 5 4 1 173 8 4 1 6 2 1 1 0 10 0 17 1 7 2 1 0 0 3 21 0 5 8 1 0 0 0 0 1 0 0 0 9 2 1 1 0 1 0 0 0 0 10 22 3 4 2 3 0</td><td>5 333 5 4 1 173 8 4 1 0 6 2 1 1 0 10 0 17 1 0 7 2 1 0 0 3 21 0 5 0 8 1 0 0 0 0 0 0 0 0 9 2 1 1 0 1 0 0 0 0 10 2 3 4 2 3 0 0 0 0 11 1 1 1 1 0 0 0 0 0 0 13 10 10 17 22 3 2 1 1 2 14 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0</td><td>5 333 5 4 1 173 8 4 1 0 3 6 2 1 1 0 10 0 17 1 0 0 7 2 1 0 0 3 21 0 5 0 0 8 1 0</td><td>5 33 5 4 1 173 8 4 1 0 3 0 6 2 1 1 0 10 0 177 1 0<</td><td>1 3 5 4 1 173 8 4 1 0 3 0 0 6 2 1 1 0 10 0 17 1 0</td></t<><td>a b b c 1 1 0 3 0 0 1 6 2 1 1 0 1 0 3 0 0 1 6 2 1 1 0 1 0</td><td>a b b c <</td><td>5 33 5 4 1 173 8 4 1 0 3 0 0 1 0 110 6 2 1 0 0 0 1 0 <th< td=""><td>s s s s i</td><td>5 333 5 4 1 173 8 4 1 0 3 0 0 1 0 10 0<!--</td--></td></th<></td></td>	5 3333 5 4 1 173 6 2 1 1 0 10 7 2 1 0 0 3 8 1 0 0 0 1 10 22 3 4 2 3 11 1 0 1 1 1 12 0 1 3 1 1 12 0 0 1 3 1 13 10 10 17 22 3 14 0 0 0 0 0 15 91 1 1 0 117 16 0 0 0 0 0 17 0 0 0 0 0 16 2 6 0 2 2 3 25 4 0 6 2 4 6 2 6 0 2 3 3 0 <t< td=""><td>5 333 5 4 1 173 8 6 2 1 1 0 10 0 7 2 1 0 0 3 21 8 1 0 0 0 0 0 9 2 1 1 0 1 0 10 22 3 4 2 3 0 11 1 0 1 1 0 1 0 12 0 1 3 1 0 117 0 13 10 10 17 22 3 2 14 0 0 0 0 0 16 0 0 0 0 0 0 0 0 13 107 91 52 648 35 35 0 1 2 3 4 5 6 1 0 57 29 6 29 2 2 59</td><td>5 333 5 4 1 173 8 4 6 2 1 1 0 10 0 17 7 2 i 0 0 3 21 0 8 1 0 0 0 0 8 9 2 1 1 0 1 0 0 0 10 22 3 4 2 3 0 0 11 1 0 1 1 1 0 0 1 12 0 0 1 3 1 0 0 1 13 10 10 17 22 3 2 1 14 0 0 0 0 0 0 0 0 16 0 0 0 0 0 0 0 0 17 1 0 57 29 6 29 2 0 0 2 59</td><td>5 333 5 4 1 173 8 4 1 6 2 1 1 0 10 0 17 1 7 2 1 0 0 3 21 0 5 8 1 0 0 0 0 1 0 0 0 9 2 1 1 0 1 0 0 0 0 10 22 3 4 2 3 0</td><td>5 333 5 4 1 173 8 4 1 0 6 2 1 1 0 10 0 17 1 0 7 2 1 0 0 3 21 0 5 0 8 1 0 0 0 0 0 0 0 0 9 2 1 1 0 1 0 0 0 0 10 2 3 4 2 3 0 0 0 0 11 1 1 1 1 0 0 0 0 0 0 13 10 10 17 22 3 2 1 1 2 14 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0</td><td>5 333 5 4 1 173 8 4 1 0 3 6 2 1 1 0 10 0 17 1 0 0 7 2 1 0 0 3 21 0 5 0 0 8 1 0</td><td>5 33 5 4 1 173 8 4 1 0 3 0 6 2 1 1 0 10 0 177 1 0<</td><td>1 3 5 4 1 173 8 4 1 0 3 0 0 6 2 1 1 0 10 0 17 1 0</td></t<> <td>a b b c 1 1 0 3 0 0 1 6 2 1 1 0 1 0 3 0 0 1 6 2 1 1 0 1 0</td> <td>a b b c <</td> <td>5 33 5 4 1 173 8 4 1 0 3 0 0 1 0 110 6 2 1 0 0 0 1 0 <th< td=""><td>s s s s i</td><td>5 333 5 4 1 173 8 4 1 0 3 0 0 1 0 10 0<!--</td--></td></th<></td>	5 333 5 4 1 173 8 6 2 1 1 0 10 0 7 2 1 0 0 3 21 8 1 0 0 0 0 0 9 2 1 1 0 1 0 10 22 3 4 2 3 0 11 1 0 1 1 0 1 0 12 0 1 3 1 0 117 0 13 10 10 17 22 3 2 14 0 0 0 0 0 16 0 0 0 0 0 0 0 0 13 107 91 52 648 35 35 0 1 2 3 4 5 6 1 0 57 29 6 29 2 2 59	5 333 5 4 1 173 8 4 6 2 1 1 0 10 0 17 7 2 i 0 0 3 21 0 8 1 0 0 0 0 8 9 2 1 1 0 1 0 0 0 10 22 3 4 2 3 0 0 11 1 0 1 1 1 0 0 1 12 0 0 1 3 1 0 0 1 13 10 10 17 22 3 2 1 14 0 0 0 0 0 0 0 0 16 0 0 0 0 0 0 0 0 17 1 0 57 29 6 29 2 0 0 2 59	5 333 5 4 1 173 8 4 1 6 2 1 1 0 10 0 17 1 7 2 1 0 0 3 21 0 5 8 1 0 0 0 0 1 0 0 0 9 2 1 1 0 1 0 0 0 0 10 22 3 4 2 3 0	5 333 5 4 1 173 8 4 1 0 6 2 1 1 0 10 0 17 1 0 7 2 1 0 0 3 21 0 5 0 8 1 0 0 0 0 0 0 0 0 9 2 1 1 0 1 0 0 0 0 10 2 3 4 2 3 0 0 0 0 11 1 1 1 1 0 0 0 0 0 0 13 10 10 17 22 3 2 1 1 2 14 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	5 333 5 4 1 173 8 4 1 0 3 6 2 1 1 0 10 0 17 1 0 0 7 2 1 0 0 3 21 0 5 0 0 8 1 0	5 33 5 4 1 173 8 4 1 0 3 0 6 2 1 1 0 10 0 177 1 0<	1 3 5 4 1 173 8 4 1 0 3 0 0 6 2 1 1 0 10 0 17 1 0	a b b c 1 1 0 3 0 0 1 6 2 1 1 0 1 0 3 0 0 1 6 2 1 1 0 1 0	a b b c <	5 33 5 4 1 173 8 4 1 0 3 0 0 1 0 110 6 2 1 0 0 0 1 0 <th< td=""><td>s s s s i</td><td>5 333 5 4 1 173 8 4 1 0 3 0 0 1 0 10 0<!--</td--></td></th<>	s s s s i	5 333 5 4 1 173 8 4 1 0 3 0 0 1 0 10 0 </td

A.5-3

۰.

TABLE A.5-2 FUTURE OD TABLE BY VEHICLE TYPE: ROUTE A (2/6) - YEAR 2000 -

0	D	1	. 2	3	4	5	6	7	8	9	10	- 11	12	13	14	15	16	- 17	Tota
	1	0	8	4	1	55	0	0	0	0	3	0	0	2	0	28	0	0	10
	2	6	0	2	0	់រ	0	0	0	0	1	0	0	2	0	0	0	0	1
	3	3	0	0	1	0	0	0	0	0	0	0	0	2	0	3	0	0	
	4	2	0	2	0	0	0	0	0	0	0	0	0	2	0	54	Ó	0	6
	5	54	2	0	0	39	3	1	0	0	0	0	0	2	0	37	0	0	13
	6	0	0	0	0	2	Ö	3	0	0	0	0	0	0	: 0	0	0	0	
	7	0	0	0	0	2	2	0	0	0	0	0	0	¹ 0	0	0	0	0	
	8	0	0	0	0	0	0	0	0	· 0	0	0	0	0.	; 0	0	0	0	
1	9	0	· 0	0	0	0	0	0	0	0	2	· 0	0	0	0	0	0	0	
	10	3	0	0	0	0	0	0	÷ 0	2	0	• 0	0	0	0	2	0	0	
	11	0	0	0	0	0	0	0	0	0	0	0	2	1	0	0	0	0	
	12	0	0	0	0	0	0	- 0	0	0	0	2	0	5	.0	1	0	0	
	13	1	2	2	3	1	0	0	0	- 0	1	1	6	0	0	0	0	0	1
	14	0	0	0	0	0	0	0	0	° 0	0	0	0	ĺ0	0	0	0	Ò	
	15	32	0	0	54	39	0	0	0	0	0	0	0	0	0	0	0	14	13
	16	0	Q	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
	17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	- 14	Û.	0	i 1
	Total	101	12	10	59	140	5	4	0	2	7	3	8	16	0	139	Ö	14	52
	/ehicle																		
All \ O	D	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	
	D1	0	150	82	19	406	4	1	0	.4	43	0	0	33	0	177	Ó	0	92
	D 1 2	.0 .138	150 0	82 14	19 3	406 8	4	1	0	4 0	43 9	0	0	33 32	0 0	177 1	0	0	92 20
	D 1 2 3	0 138 74	150 0 11	82 14 0	19 3 20	406 8 9	4 1 0	1 1 0	0 0 0	4 0 0	43 9 6	0 0 0	0 0 0	33 32 8	0 0 0	177 1 29	0 0 0	0 0 0	92 20 15
	D 1 2 3 4	0 138 74 18	150 0 11 4	82 14 0 19	19 3 20 0	406 8 9 6	4 1 0	1 1 0 0	0 0 0 0	4 0 0 0	43 9 6 4	0 0 0 2	0 0 0 4	33 32 8 37	0 0 0	177 1 29 55	0 0 0	0 0 0 0	92 20 15 14
	D 1 2 3 4 5	0 138 74 18 393	150 0 11 4 13	82 14 0 19 7	19 3 20 0 3	406 8 9 6 374	4 1 0 20	1 1 0 0 10	0 0 0 0 1	4 0 0 0 0	43 9 6 4 6	0 0 2 0	0 0 4 1	33 32 8 37 5	0 0 0 0	177 1 29 55 248	0 0 0 0	0 0 0 0	92 20 15 14 1,08
	D 1 2 3 4 5 6	0 138 74 18 393 4	150 0 11 4 13 1	82 14 0 19 7 1	19 3 20 0 3 0	406 8 9 6 374 18	4 1 0 20 0	1 1 0 0 10 39	0 0 0 1 3	4 0 0 0 0 0	43 9 6 4 6 0	0 0 2 0 0	0 0 4 1 0	33 32 8 37 5 0	0 0 0 0 0 0	177 1 29 55 248 0	0 0 0 0 0	0 0 0 0 0	92 20 15 14 1,08 6
	D 1 2 3 4 5 6 7	0 138 74 18 393 4 2	150 0 11 4 13 1 1	82 14 0 19 7 1	19 3 20 0 3 0 0	406 8 9 6 374 18 8	4 1 0 20 0 41	1 0 0 10 39 0	0 0 0 1 3 11	4 0 0 0 0 0 0	43 9 6 4 6 0	0 0 2 0 0 0	0 0 4 1 0 0	33 32 8 37 5 0 0	0 0 0 0 0 0 0	177 1 29 55 248 0 0	0 0 0 0 0 0	0 0 0 0 0 0	92 20 15 14 1,08 6 6
	D 1 2 3 4 5 6 7 8	0 138 74 18 393 4 2 1	150 0 11 4 13 1 1 1 0	82 14 0 19 7 1 1	19 3 20 0 3 0 0 0 0	406 8 9 6 374 18 8 0	4 1 0 20 0 41 2	1 0 0 10 39 0 14	0 0 0 1 3 11 0	4 0 0 0 0 0 0 0 0	43 9 6 4 6 0 0 0	0 0 2 0 0 0 0	0 0 4 1 0 0 0	33 32 8 37 5 0 0 0	0 0 0 0 0 0 0 0 0	177 1 29 55 248 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0	92 20 15 14 1,08 6 6 11
	D 1 2 3 4 5 6 7 8 9	0 138 74 18 393 4 2 1 5	150 0 11 4 13 1 1 1 0 1	82 14 0 19 7 1 1 1 0	19 3 20 0 3 0 0 0 0 0	406 8 9 6 374 18 8 0 1	4 1 0 20 0 41 2 0	1 0 0 10 39 0 14 0	0 0 0 1 3 11 0	4 0 0 0 0 0 0 0 0 0	43 9 6 4 6 0 0 0 15	0 0 2 0 0 0 0 0 0	0 0 4 1 0 0 0 0	33 32 8 37 5 0 0 0 0	0 0 0 0 0 0 0 0 0	177 1 29 55 248 0 0 0 0	0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0	92 20 15 14 1,08 6 6 11 11 2
	D 1 2 3 4 5 6 7 7 8 9 10	0 138 74 18 393 4 2 1 5 45	150 0 11 4 13 1 1 1 0 1 8	82 14 0 19 7 1 1 1 0 1 6	19 3 20 0 3 0 0 0 0 0 4	406 8 9 6 374 18 8 0 1 1 6	4 1 0 20 0 41 2 0 0	1 0 0 10 39 0 14 0 0	0 0 0 1 3 11 0 0	4 0 0 0 0 0 0 0 0 0 0 14	43 9 6 4 6 0 0 0 15 0	0 0 2 0 0 0 0 0 0 0	0 0 4 1 0 0 0 0 0	33 32 8 37 5 0 0 0 0 0 2	0 0 0 0 0 0 0 0 0 0 0 0	177 1 29 55 248 0 0 0 0 0 6	0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0	92 20 15 14 1,08 6 6 11 2 2 9
	D 1 2 3 4 5 6 7 8 9 10 11	0 138 74 18 393 4 2 1 5 45 1	150 0 11 4 13 1 1 1 0 1 8 0	82 14 0 19 7 1 1 0 1 6 1	19 3 20 0 3 0 0 0 0 4 3	406 8 9 6 374 18 8 0 1 6 1	4 1 0 20 0 41 2 0 0 0 0	1 0 0 10 39 0 14 0 0	0 0 0 1 3 11 0 0 0	4 0 0 0 0 0 0 0 0 0 0 14 0	43 9 6 4 6 0 0 0 15 0 3	0 0 2 0 0 0 0 0 0 0 1 0	0 0 4 1 0 0 0 0 0 9	33 32 8 37 5 0 0 0 0 2 10	0 0 0 0 0 0 0 0 0 0 0 0 0	177 1 29 55 248 0 0 0 0 6 0	0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0	92 20 15 14 1,08 6 6 6 11 2 2 2 2
	D 1 2 3 4 5 6 7 8 9 10 11 12	0 138 74 18 393 4 2 1 5 45 1 0	150 0 11 4 13 1 1 1 0 1 8 0 0	82 14 0 19 7 1 1 0 1 6 1	19 3 20 0 3 0 0 0 0 4 3 5	406 8 9 6 374 18 8 0 1 6 1 6 1	4 1 0 20 0 41 2 0 0 0 0 0 0	1 1 0 10 39 0 14 0 0 0 0	0 0 0 1 3 11 0 0 0 0	4 0 0 0 0 0 0 0 0 0 0 0 14 0 0	43 9 6 4 6 0 0 0 15 0 3 0	0 0 2 0 0 0 0 0 0 1 0 8	0 0 4 1 0 0 0 0 9 0	33 32 8 37 5 0 0 0 0 2 10 59	0 0 0 0 0 0 0 0 0 0 0 0 0 0	177 1 29 55 248 0 0 0 0 0 6 0 8	0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0	92 20 15 14 1,08 6 11 24 24 24 24 24 24 24 24 24 24 24 24 24
	D 1 2 3 4 5 6 7 7 8 9 10 11 12 13	0 138 74 18 393 4 2 1 5 45 1 5 45 1 0 15	150 0 11 4 13 1 1 1 0 1 8 0 1 7	82 14 0 19 7 1 1 1 0 1 6 1 1 26	19 3 20 0 3 0 0 0 0 0 4 3 5 32	406 8 9 6 374 18 8 0 1 6 1 1 6	4 1 0 20 0 41 2 0 0 0 0 0 0 0 2	1 1 0 10 39 0 14 0 0 0 1	0 0 0 1 3 11 0 0 0 0 0	4 0 0 0 0 0 0 0 0 0 0 14 0 3	43 9 6 4 6 0 0 0 15 0 3 0 6	0 0 2 0 0 0 0 0 0 0 1 0 8 14	0 0 4 1 0 0 0 0 0 0 0 0 0 0 0 0 56	33 32 8 37 5 0 0 0 0 2 10 59 0		177 1 29 55 248 0 0 0 0 0 6 0 8 2	0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0	92 20 15 14 1,08 6 6 6 6 11 2 9 21 24 24 24 24 24 24 24 24 24 24 24 24 24
	D 1 2 3 4 5 6 7 8 9 10 11 12 13 14	0 138 74 18 393 4 2 1 5 45 1 0 15 0	150 0 11 4 13 1 1 1 0 1 8 0 1 7 0	82 14 0 19 7 1 1 1 0 1 6 1 1 26 0	19 3 20 0 3 0 0 0 0 4 3 5 32 0	406 8 9 6 374 18 8 0 1 6 1 1 6 0	4 1 0 20 0 41 2 0 0 0 0 0 0 0 2 0	1 0 0 10 39 0 14 0 0 0 1 0	0 0 0 1 3 11 0 0 0 0 0 1 0	4 0 0 0 0 0 0 0 0 0 0 0 0 14 0 0 3 0	43 9 6 4 6 0 0 0 15 0 3 0 6 0	0 0 2 0 0 0 0 0 0 0 1 0 8 14 0	0 0 4 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	33 32 8 37 5 0 0 0 0 2 10 59 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	177 1 29 55 248 0 0 0 0 6 0 8 2 0			92 20 15 14 1,08 6 1 2 9 2 2 2 8 2 19
	D 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15	0 138 74 18 393 4 2 1 5 45 1 5 45 1 0 15	150 0 11 4 13 1 1 0 1 8 0 1 7 0 1	82 14 0 19 7 1 1 0 1 6 1 1 26 0 1	19 3 20 0 3 0 0 0 0 0 4 3 5 32 0 54	406 8 9 6 374 18 8 0 1 6 1 1 6 0 248	4 1 0 20 0 41 2 0 0 0 0 0 0 0 0 0 0 0	1 0 0 10 39 0 14 0 0 0 0 1 0 0	0 0 0 1 3 11 0 0 0 0 0 0	4 0 0 0 0 0 0 0 0 0 0 0 14 0 3 0 0 0	43 9 6 4 6 0 0 0 15 0 3 0 6 0 0	0 0 2 0 0 0 0 0 0 0 0 1 0 8 14 0 0	0 0 4 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	33 32 8 37 5 0 0 0 0 2 10 59 0 0 0 0		177 1 29 55 248 0 0 0 0 6 0 8 2 0 0 0		0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 14	Tota 92 20 15 14 1,08 6 6 6 6 19 19 29 29 29 20 19 20 19 20 19 20 19 20 19 20 15 5 14 4 1,08 6 6 6 20 20 20 20 20 20 20 20 20 20 20 20 20
	D 1 2 3 4 5 6 7 8 9 10 11 12 13 14	0 138 74 18 393 4 2 1 5 45 1 0 15 0 223	150 0 11 4 13 1 1 1 0 1 8 0 1 7 0	82 14 0 19 7 1 1 1 0 1 6 1 1 26 0	19 3 20 0 3 0 0 0 0 4 3 5 32 0	406 8 9 6 374 18 8 0 1 6 1 1 6 0	4 1 0 20 0 41 2 0 0 0 0 0 0 0 2 0	1 0 0 10 39 0 14 0 0 0 1 0	0 0 0 1 3 11 0 0 0 0 0 1 0	4 0 0 0 0 0 0 0 0 0 0 0 0 14 0 0 3 0	43 9 6 4 6 0 0 0 15 0 3 0 6 0	0 0 2 0 0 0 0 0 0 0 1 0 8 14 0	0 0 4 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	33 32 8 37 5 0 0 0 0 2 10 59 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	177 1 29 55 248 0 0 0 0 6 0 8 2 0			92 20 15 14 1,08 6 6 6 11 2 2 2 2 1 2 1 2 1 2 1 2 1 2 1

A.5-4

TABLE A.5-2 FUTURE OD TABLE BY VEHICLE TYPE: ROUTE A (3/6) - YEAR 2010 -

M∕C

N∕C																			
0	D	1	2	3	4	5	6	1	.8	9	10	11	12	13	14	15	16	17	Tot
	1	0	180	119	24	784	4	3	0	5	51	0	• •	48	0	149 2	0	0	1,36 24
	2	166	0	13 0	3 24	9 15	1	1	0	0 0	7 11	0	0	43 0	: 0 0	40	ŏ	ŏ	21
	3 4	114 19	12 5	21	24 0	6	0	0	ŏ	ŏ	4	õ	7	55	· 0	- 1	Ő	ō	12
	5	800	12	13	4	371	17	10	3	Ō	7	0	1	2	0	206	0	0	1,44
	6	6	2	1	-1	20	0	36	3	0	1	0	· 0	1	0	0	0	0	7
	7	5	. 2	1 t	1	10	43	0	14	0	- 1	0	0	1	0	0	0	0	i
	8	2	1	1	0	0	0	20	0	0	0	0	0	0	0	0	0	0	í
	9	5	4	2	0	2	0	0	0	0	12	0	0	0	. 0	1	0	0	. : 11
	10	47	6	12	5	7	1	· 1	0	15	' 0 2	0	0	· 0 10	0	9 0	0	0	1
	11	- 2	0	2	2 6	23	0 0	0	0	0	- 0-	5	- 0 0	69	Ö	· 5	Ū	ŏ	
	12 13	0 22	22	31	41	9	3	· 1	1	3	ž	15	÷75	Õ	ŏ	1	0	0	2
	14	0	· 0	0	0	ŏ	ŏ	; ò	· o	ŏ	ò	0	0	Ō	0	0	Ó	0	:
	15	192	ž	ĩ	1	218	ō	Ō	Ō	Ō	1	0	0	1	0	0	· 0	0	4
	16	0	ō	Ó	0	0	Ó	0	0	0	0	° 0	0	0	0	0	0	0	÷.,
	17	. 0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
	Total	1,380	247	219	111	1,456	70	73	22	24	104	21	87	229	0	414	0	0	4,4
<u>_ight</u> o	D	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	To
<u> </u>	1		138	76	15	81	5	0	0	5	42	0	0	9	0	138	0	0	5
	2	142	0	7	4	5	Ō	. 0	ō	Ō	7	0	0	6	0	0	0	0	1
	3	68	7	ò	13	6	. o	0	0	. 0	5	· 0	. 0	7	0	9	0	0	; 1
	4	17	3	12	0	5	0	0	0	0	4	3	4	11 -	• •0	0	0	0	
•	5	22	i2	6	- 5	348	14	- 9	0	0	6	0	0	- 4 -	0	161	0	0	5
	6	7	0	0	0	· 9	0	. 31	5	0	0	0	. 0	0	0	: 0	0	0	
. '	7	0	0	0	0	6	31	0	11	0	0	0	0	0	0	0	0	0 0	
	8	0	0	0	0	0	4	11	0	0	0	· 0 · 0	0	0	0	· 0 · 0	: 0 ∶`0	0	
	9	5	0	· . 0	0	0	0	្ល	0	0	9	3	, ŏ	3	ŏ	: 3	ŏ	0	
:	10	42	· 7 0	5 0	4	5	0.	0	ŏ	0	3	0	7	3	Ō	· · ŏ	Ö	0	· :
	11	0	· 0	. 0	4	· 0	÷ŏ	ŏ	ŏ	ŏ	ŏ	5	0	24	÷ Ó	4	0	0	:
	13	7	- 6	8	9	3	· · ō	Ŏ	· 0	2	3	4	24	0	0	2	Ö	0	. 1
1	14	ò	. ŏ	Ō	. 0	Ō	0	0	0	0	0	0	0	0	0	. 0	: 0	0	
	15	184	0	. 0	0	135	0	0	0	0	0	0	0	0	0	. 0	0	0	3
· ·	16	0	Ó	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
·	17	Ó	0	0	0	0	0	0	0	0	0	0	0	0	0	0		. 0	
	Total	494	173	114	58	603	54	51	16	14	79	15	35	67	: 0	317	0	0	2,0
_ :	•											: :	•						
BUS	D	1	2	3	4	5	6	7	8	9	10	11	12	13	- 14	15	16	17	To
<u> </u>	1		13	7	3	0	<u> </u>	0	0	0	5	0	0	3	0	- 24	0	0	
	2	12	0	3	0	Ō	0	0	0	0	. З	0	0	3	0	0	0	0	
	3	4	3	0	3	0	0	0	0	0	· `0	0	0	3	<u></u> 0	3	<u>)</u>	: 0	i.
	4	2	0	- 3	0	0	0	0	0	0) 0	0	0	3	0	: 0	0	0	-1
	5	0	0	0	0	27	2	3	0	0	0	0	0	0	0	32	0	0	(
	6	0		0	0	2	0	5	0	0	: 0	0	0	0	0	0	0	0	
	7	0		0	0	3	5	0	3	0	0	0	0	0	0	ŏ	÷ŏ	ŏ	
	8	0		0	0	· 0 0	0 0	3	0	ŏ	ંડે	ŏ	ō	: 0	÷ŏ	Ξŏ	÷ŏ	Ö	
	9 10	0		0	0	Ő	ŏ	ŏ	ŏ	š	ŏ	ŏ	ŏ	0	- <u>,</u>	Ō	0	0	7
	10	5 0			ŏ	.0	. 0	Ō	ŏ	Ō	ō	ō	3	3	·: 0	0	0	0	
	12	0			ŏ	0	0	ŏ	ō	Ō	Ō	3	0	9	0	0	0	0	
	13	3			2	2	0	Ō	Ō	Ō	0	3	9	0	0	0	0	0	
	-14	ŏ			ō	Ō	Ő	0	0	0	0	0	0	0	0		0	0	
	15	29			. 0	31	0	0	0	Ó	0	0	0	0	0		0	0	
	16	0		• 0	0	0	0	0	0	0	0	0	0	0	0		0	0	
		0	0	0	0	0	0	0	0	. 0	0	0	0	. 0	0	0	0	0	
	17	55	<u> </u>	16		66	7	-11	3	3	11	6	12	24	Ō		0		

TABLE A.5-2 FUTURE OD TABLE BY VEHICLE TYPE: ROUTE A (4/6) - YEAR	
THE ATTEND & TOTORDOD THE ADDITION AND A THE ACTION AND A THE ATTENDED AND ATTENDED AND A THE ATTENDED AND ATTENDED AND ATTENDED AND ATTENDED AND ATTENDED AND ATTENDED AND ATTENDED AND ATTENDED AND ATTENDED AND ATTENDED AND ATTENDED AND ATTENDED AND ATTENDED A	211111-

Т	riick.
	I Q Q I I

		Total 186 21 16 200	17 0 0 0	16 0 0 0	15 57 0 5 191	14 0 0 0 0	13 3 3 3 3	12 0 0 0 0	11 0 0 0 0	10 5 2 0 0	9 0 0 0 0	-	7 0 0 0 0	0 0 0	98 2 0	4 2 0 2 0	3 6 3 0 3	2 15 0 0 0	1 0 11 6 3	D 1 2 3 4	0			
		242 7 7 0 3 12	0 0 0 0	000000000000000000000000000000000000000	71 0 0 0 0 3	0 0 0 0 0	3 0 0 0 0	0 0 0 0	000000000000000000000000000000000000000	0 0 0 3 0	0 0 0 0 3	0 0 0 0 0	2 5 0 0 0	3	2 4 0	0 0 0 0 0	0 0 0 0 0	4 0 0 0	94 0 0 0 0 6	5 6 7 8 9 10				
		6 15 30 0 358 0	0 0 0 29 0	0 0 0 0 0	0 3 0 0 0	0 0 0 0	3 9 0 0 0 0	3 0 10 0 0	0 3 3 0 0	0 2 0 0 0 0 0	000000000000000000000000000000000000000	0 0 0 0	0 0 0 0	0 0 0 0 0	0 2 0 72 0	0 0 5 0 191 0	0 0 3 0 0 0	0 0 3 0 0 0	0 0 2 0 66 0	11 12 13 14 15 16				
·		29 1,134	0 29	0	29 360	0	0 27	0 13	- 0 - 6	0 12	0 3	0	0 7	7	0 245	0 200	0 15	0 22	0 188	17 Totat thicle	All Ve			
		Total 2,118 459 365	17 0 0	16 0 0	15 368 2 57	14 0 0	13 63 55 13	12 0 0 0	11 0 0	10 103 19 16	9 10 0 0	8 0 0 0	7 3 1 1 1	6 9 1 1	5 963 16 21	4 44 7 42	3 208 26 0	2 345 0 22 8	1 0 331 192 41	D 1 2 3 4	0	·		
- 	•	387 2,339 136 143 43	0 0 0 0	0 0 0	192 470 0 0	0 0 0 0	72 9 1 1 0	11 1 0 0	3 0 0 0	8 13 1 1 0	0 1 0 0 0	0 3 8 28 0	1 24 77 0 34	1 37 0 82 4	11 810 33 23 0	0 9 1 1 0	39 19 1 1 1	27 2 2 1	918 13 5 2	4 5 6 7 8		•		
· · ·		47 205 53 155 354	0 0 0	0 0 0 0	1 16 0 12 3	0 0 0	0 3 19 111 0	0 0 16 0	0 3 0 16 25	27 0 5 0 12	0 28 0 0 5	0 0 0 1	0 1 0 0	0 1 0 0 3	3 12 2 3	0 9 6 10 57	2 17 2 2 45	4 16 0 33	10 100 2 0 34	9 10 11 12 13		•		
		0 1,153 0 29 7,986	0 0 29 0 0 29 29	0 0 0 0	0 0 29 ,151	0 0 0	0 1 0 0 347	118 0 0 0 147	0 0 0 0 48	0 1 0 206	0 0 0 44	0	0 0 0 0	0 0 0 139	0	0 192 0 0	0 1 0 0	0 2 0 0	0 470 0 0	14			-	
						-						·		•								• •		
							•						-						.*					
						-							-	•								•		

TABLE A.5-2 FUTURE OD TABLE BY VEHICLE TYPE: ROUTE A (5/6) - YEAR 2020 -

.

2

/C					.									40	10		- 4 E	16	17	Tota
) 	Ð		1	2	3	4	5	6	- <u>7</u> -5	8	9	10 91	<u>11</u> 0	12 0	- <u>13</u> - 85	<u>14</u> 0	15 310	<u>16</u> 0		2,39
	1			316	218		,308 14	6 ' 1	ວ 1	0	ů 0	51 11	ŏ	ŏ	70	õ	4	ŏ	ō.	41
	2		86	0	23	6 42	24	1	1	0	õ	19	ŏ	ŏ	, 0	ŏ	80	Ō	ō	38
	3		201	20	0	42	10	1	1	ŏ	õ	7	ŏ	9	89	ō	2	Ó	0	19
	4		34	8	38	5	560	29	13	5	1	12	õ	1	3	Ō	389	0	0	2,39
	5	•	341	19	18	ว 1	35	20	56	6	ò	1	ŏ	Ó	1	0	0	Ō	Ō	11
	6		11	3	2 2	1	30 15	72	õ	25	õ	i	0	Ō	1	Ö	0	0	0	12
	7		8	3	1	0	0	0	37	ĨÕ -	ŏ	Ö.	ō	Ö	1	0	0	0	· 0	4
	8		·4 ·7:	6	5	0	-4	õ	0	0	Õ	21	Ō	0	0	0	11 f	0	0	1
	.9			9	19	ท้	13	1	1	0	24	0	0	0	0	0	15	0	0	12
	10		84 : 3	9 0	3	2	2	o i	0	0	0	2	0	5	17	0	<u>1</u>	0	0	:
	11		0	õ	5	.8	4	ŏ	Ō	Ō	Ó	0	11	0	106	0	11	0	0	1
	13		35	33 :	55	65	11	3	3	1	6	12	21	125	0	0	2 -	0	- 0	3
	14		0	0	0	õ	0	ō	Ō	0	0	0	• •	0	0	0	0	0	0	
	1		400	3	2	1	408	Ō	Ō	0	0	1	0	1	1	0	0	0	0	8
	16		.0	ŏ	Ō	ò	0	Ō	Ō	Ó	0	0	0	0	0	0	0.	0	0	
	1		0	ŏ	õ	ŏ	Ö	Ō	Ō	0	0	Ò	0	0	0	0	0	0	0	
	Tota		-	420	390		2,409	115	119	39	41	178	33	142	373	0	815	0	0	7,6
	100	<u>π</u> ε,	414	460	0.00															
ight																				
				2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	To
0 	D		<u> </u>	236	137	28	121		- <u>;</u>	0	7	75	0	0	15	0	262	0	0	8
		1	242	230	137	6	9	0	ō	ō	Ō	12	Ō	0	10	0	0	0	0	2
			242 121	12	0	22	10	ŏ	. õ	. Õ	Ō	8	0	0	11	0	22	. 0	· · 0 ·	2
			27	7	22	0	. 8	, ŏ	0	Ö	- 0	7	4	: 7	16	0	0	0	0	
		4 c	35	17	11	ŷ	525	22	· 14	Ō	0	9	0	· 0	6	:0	322	0	0	9
		5		0	0	0	16	- 0	50	9	0	0	0	0	0	0	0	: O	· 0	v
		6	11	0	ŏ	ŏ	. 8	52	0	19	Ō	· 0	0	0	0	0	0	0	0	.1
		7	0	0	ö	ŏ	Ō	8	- 19	0	0	0	0	0 :	0	0	0	0	0	
Ξ.		8 9 -	0	Ö	ŏ	0	· 0	Ū	- 0	ŏ	ō	14	0	0	0	:0	0	· • 0	0	
		-		12	8	27	. 8	Ō	Ō	ō	12	0	5	0	6	0	5	0	· 0	1
		0	72		Ő	5	: 0	Ō	· ŏ	ō	0	5	0	11	5	0	0	. 0	· 0.	
		1	0	0	0	6	Ö	ŏ	ŏ	÷ŏ	Ŏ.	0	- 9	0	38	0	. 7	0	: 0	1.1
		2	0		13	14	·· 4	ŏ	· õ	. 0	4	5	6	40	0	0	3	<u> </u>	0	- 1
:		i3	11	10 0	· 0	0	0	ŏ	Ö	0	:0	0	0	. 0	0	. 0	0	0	0	
2.5		4	0		. 0	÷ ŏ	285	ŏ	0	0	0	0	0	0	0	0	0	0	· 0	6
	-	5	339	0	- O	ŏ	0	ŏ	ō	Ō	្រត់	0	0	0	0	0	0	<u>`</u> 0	' 0	
11		6	÷ 0			ŏ	Ö	ŏ	Ő.	Ō	Ō.		0	0	0	0	0	; 0	0	
	حد غم م	17	0	0 294	204	97	995	89	84	28	23		24	58	108	0	621	0	0	3,6
	Tot	ar	868	294	204	. 31	335										1			
												• •			1		· .			4
Bus					··							10		12	13	14	15	16	17	T
0	D		1	2	3			6	7		9	10	11	12	4	0				
		1	Q	17	9			0	0	0			-	ŏ	6	ŏ	0	-		
		2	15	0	6	0		0	0	0	0	5	0	ŏ	5	ŏ				۰.
	1	3	5	- 4	0	. 4		0	0	0	0	. O	. 0	ŏ	. 4	÷ ŏ		•		
		4	2	: 0	5	0		0	0	. 0	0	0	0	0	0	ŏ			0	
		5	0	0	0	0		3	3	0		ŏ	0	- 0	ŏ	÷ŏ			· · _	
		6	0	0	0			0	7	0	0	ŏ	· o	ŏ	ŏ	ŏ				
		7	. 0	0	0			8	0	5	0	. 0	° Ö	ŏ	ŏ	0	-	· .		
				- 0	0			0	5	0	0	4	0	0	ŏ	Ő			· · ·	1
		8	0		· ·			0	0	0	0 4	ō	ŏ	ŏ	ŏ	÷ŏ				
		8 9	0	0	0						- 4	v	v							1
		8 9 10	0 7	0 5	0	0	0	0	0		· ^	6	•		- K	· •	<u>م</u>) 0		
		8 9 10 11	0 7 0	0 5 0	0	0	0	0	0	0	0	0	0	4	5 14	0 0				
		8 9 10 11 12	0 7 0 0	0 5 0 0	0 0 0	0 0 0	0	0 0 0	0	0	0	0	· 4	0	14	0	i j C) 0	0	
	•	8 9 10 11 12 13	0 7 0 0 3	0 5 0 0 5	0 0 0 5	0 0 4	0	0 0 0 0	0 - 0 0	0 0 0	0	0	· 4 · 5	0 14	14 0	0	i i C) 0	0	
		8 9 10 11 12 13 14	0 7 0 0 3 0	0 5 0 5 0 5 0	0 0 0 5 0	0 0 4 0	0 0 0 3	0 0 0 0 0	0 0 0 0	0 0 0	0 0 0	0 0 0	4 5 0	0 14 0	14 0 0	0) 0) 0) 0	0 0 0	
		8 9 10 11 12 13 14 15	0 7 0 0 3	0 5 0 0 5 0 0	0 0 5 0 0	000000000000000000000000000000000000000	0 0 3 0 61	0 0 0 0 0	0 0 0 0	0 0 0 0	0 0 0	0 0 0 0	4 5 0	0 14 0 0	14 0 0	0) 0) 0) 0	0 0 0	
		8 9 10 11 12 13 14 15 16	0 7 0 0 3 0	0 5 0 5 0 5 0	0 0 5 0 0	000000000000000000000000000000000000000	0 0 3 0 61	000000000000000000000000000000000000000	000000000000000000000000000000000000000	0 0 0 0 0	0 0 0 0	0 0 0 0	4 5 0 0	0 14 0 0	14 0 0 0) 0) 0) 0) 0	000000000000000000000000000000000000000	
, 		8 9 10 11 12 13 14 15	0 7 0 3 0 54	0 5 0 0 5 0 0	0 0 5 0 0 0 0		0 0 3 0 61 0 0	0 0 0 0 0 0 0	0 0 0 0	0 0 0 0	0 0 0	0 0 0 0	4 5 0	0 14 0 0	14 0 0 0 0	0) 0) 0) 0) 0	0 0 0 0 0 0 0 0	

TABLE A.5-2 FUTURE OD TABLE BY VEHICLE TYPE: ROUTE A (6/6) - YEAR 2020 -

T	ruck	÷
---	------	---

.

	(-		_														5 N.S.		· · · · · ·
0	D	1	2	3	4	-	6	7	8	9	10	11.	12	-13	14	15	16	17	Total
	1	0	24	10	3	119	0	0	0	0	7	0	0	5	0	114	0	0	283
	2	16	0	4	0	4	0	0	0	0	3	0	0	6	0	0	0	0	- 33
	- 3	7	0	0	3	0	0	÷ 0	0	0	0	0	0	5	0	12	0	0	27
	4	3	0	5	0	0	-0	0	0	0	0	0	0	5	0	230	0	0	243
	5	118	5	0	0	75	6	3	0	0	0	0	0	4	0	136	0	0	347
	6	0	0	0	0	4	0	7	0	0	0	0	0	0	0	0	0	0	11
	7	0	0	0	· 0	5	5	0	0	0	0	0	0	0	Ö	0	0	0	10
	8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	· 0	0
	9	0	0	0	0	0	· 0	· 0	0	. 0	- 4	0	0	0	0	0	0	0	4
	10	9	0	0	: 0	0	0	0	0	4	0	• •	. 0	0	0	6	0	0	20
	11	Ö	. 0	Ó	• 0	` O	0	0	0	0	0	- 0	4	5	0	Ó	Ó	Ö	9
	12	. 0	÷ 0	÷ 0	0	0	0	0	0	0	Ó	4	0	15	់ខ	5	0	Ō	24
	13	4	⁻¹ 4	5	7	4	· 0	0	Ó	0	4	4	18	0	Ö	Ó	Ō	0	50
	14	0	Ó	0	0	0	Ō	0	0	0	Ó	Ó	0	. Ŏ	Ō	ŏ	Ō	0	0
	15	130	0	0	230	140	Ō	-0	· 0	Ō	Ö	Ō	ι ό	ŏ	· Õ	Ō	ŏ	. 45	546
	16	0	Ö	Ō	0	0	Ō	Ō	0	Ō	Ő	Ō	Õ	ŏ	Ō	ŏ	õ	0	0
	17	0	0	Ō	Ō	Ō	Ö	Ō	ŏ	0	Ō	Õ	Ō	ŏ	Ő	45	· ŏ	0	45
i	Total	287	33	24	243	352	11	10	0	4	18	8	22	45	0	549	0	45	1,653
	ehicle D	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	Total
	• 1	0	593	374	78		13	6	1	16	180	0	0	109	0	730	0	0	3,649
11.1	2	559	0	46	12	27	2	. 2	1	• 0	31	0	0	92	0	4	Ó	0	775
	3	334	36	÷ 0	71	34	1	1	0	0	27	0	• 0	21	0	119	0	0	645
	4	66	15	70	0	18	1	1	0	0	14	4	16	114	0	232	0	0	551
	5	1,494	40	29	15	1,182	60	33	5	÷ 1	21	. 1	- 1	13	0	911	0	Ó	3,806
	6	23	3.	2	1	59	0	120	15	. 0	1	0	0	1	0	0	0	0	225
	7	. 8 -	3	2	<u> </u>	31	137	· 0	: 49	0	5 1	0	0	1	0	0	0	0	233
,	8	4	1	1.	1	0	8	61	0	0	1	0	0	1	0	0	0	0	77
	9	16	6	5	0	4	0	0	·: 0	0	43	0	0	0	· 0	1	0	0	76
	< % 10	172	26	27	18	21	i 1	i	0	. 44	0	5	. 0	6	0	27	0	0	348
È j	1.011	3	0	3	7	3	0	· 0	0	0	- 7	0	24	32	0	1	0	0	80
	12	0	0	5	14	4	0	0	0	0	0	28	0	173	Ō	24	Ō	ō	249
	- 13	53	52	78	90	23	3	3	1	10	21	36	197	0	Ō	5	ō	Ō	573
	14	0	0	0	0	0	0	0	0	0	0	0	0	0	- 0	Ō	Ō	Ō	0
	- 15	923	3.	2	231	894	ō	ō	Ō	. 0	Ť	Õ	៍ រំ	ĩ	õ	Ö	ŏ	45	2,103
÷ :	13				0	0	Ő	ŏ	° õ	ŏ	ō	ŏ	0	ò	õ	ŏ	ŏ	ō	0
• : • • •		0	0	. 0	U														
	· 16	0	0	0 0		õ	Ō	· · · · ·	-		· · · ·	<u>`</u> <u>`</u>	0	. <u>^</u>		-			
	16	0	0 0 778	0 0 644	0		-	0	0	0	0	74	0 240	0 564	0	45 2,100	0	0 45	45 13,436

A.5-8

TABLE A.5-3 FUTURE OD TABLE BY VEHICLE TYPE: ROUTE B (1/6) - YEAR 2000 -

M/C

VC							. .												
) ()	1	2	3	4	5	6	7	8	9	10		12	13	14	15	16	17	Total
	1	0	77	46	10	317	2	1	0	2	20	. 0	0	25	0	71	0	0	571 106
	2	66	0	6	1	4	0	0	0	0	3	• 0	0	24	0	1 19	0	0	91
	3	43	6	0	11	6	0	0	0	0	4	0	0	0 29	0	19	Ö	ŏ	57
	4	8	2	9	0	4	0	0	0	0	2 3	0	0	- 29	ŏ	110	õ	ŏ	640
	5	328	5	4	1	.173	8	4 17	1	0	0	0	0	ò	ŏ	0	ŏ	ō	32
	6	2	1	1	0	10	0 21	0	5	0	· 0	ŏ	õ	0	ō	Ō	- ŏ '	ŏ	33
	7	2	1	í A	0	3	0	8	0	ŏ	ŏ	0	Õ	0	ŏ	ŏ	0	ŏ	10
	8	1	0	0	0	0 1	1 1	0	õ	. 0	ž	. 0	0	ŏ	õ	ŏ	Ō	· · õ	13
	9	2	1	1	0	3	0	0	0	7	. 0	- 0	0	ŏ	ŏ	3	Ö	ŏ	45
	10	22	3	4	2	່ 1	0	0	ŏ	0	ં ર્ય	÷Ŏ	ž	5	· ŏ	0	ŏ	Ō	12
	11	1	0	1 1	3	1	ŏ	õ	ŏ	ŏ	0	2	õ	37	0	4	ò	0	49
	12	0	10	17	22	3	2	1	ĭ	- 2	4	9	41	0	0	1	0	0	123
	13	10	10	0	0	0	0	, O	0	0	0	0	0	0	0	0	0	0	0
	14	0	1	1	õ	117	ŏ	õ	õ	Ő	0	ō	0	Ō	0	0	0	0	211
	15 16	91	0	ò	ŏ	0	ŏ	ŏ	ŏ	0	:0	0	0	Ó	0	0	0	0	Ò
	10	0	ŏ	ŏ	ŏ	Ö	ŏ	ŏ	ŏ	· Õ	0	ō	Ō	Ö.	Ó	0	0	0	0
•	Total	0 576	106	91	52	644	35	33	9	12	45	11	46	122	0	210	0	0	1,994
	10(a)	510													`				
laht	1																		
ight	<u> </u>		~	-		5	6	7	8	. 9	10	11	12	13	14	15	16	17	Total
0	D		2	3	4	29	2	0	0	2	17	0	0	4	0	67	0	0	213
	1	0	57	29	2	23	- Ū	ŏ	Ö	0	4	ŏ	Ō	4	0	0	0	0	76
	2	59	· 0	4 0	6	2	0	· 0		· ŏ:	2	ŏ	Ō	4	0	5	0	: 0	49
	3	25	4	6	0	2	° õ	ŏ	õ	ŏ	2	2	2	5	0	0	0	0	27
	4	6	2 5	2	2	145	7	4	÷.	0	2	0	0	2	0	84	0	0	260
	5	6		2	0	4	ò	16	2	ŏ	Ō	Ō	0	0	0	0	0	0	24
	6	2	0 0	ŏ	ŏ	2	15	0	4	ŏ	· 0	Ő	0	0	0	0	0	0	- 21
	7	0	0	· 0	ŏ	õ	2	4	0	0	0	ō	0	0	: 0	0	· 0	4 O	6
	9 9	3	0	0	ŏ	ŏ	ō	0	Ō	ō.	4	0	0	0	· 0	. Ó	÷ o -	- O	1
	-10	17	4	2	2	2	÷ŏ÷	- Õ	0	3	0	1	0	2	0	1	0	0	35
	11	0	0	ō	2	0	0	Ō	0	0	2	0	4	2	0	0	·· 0	0	10
	12	ŏ	ŏ	. Ŏ.	2	0	. 0 :	0	0	0	0	3	· 0	12	0	: 3	0	· 0	20
	13	ંડું	4	5	5	1	0	0	ò	- 1	· 1	2	14	0	Ó	1	0	0	37
	14	Ŏ	0	ō	Ĩ	0	0	0	ō	· 0	0	0	° 0	. 0	0	0	0	0	0
	15	85	ŏ	ŏ	Ŏ	76	0	0	0	0	0	0	Ó	0	÷ 0	0	0	0	162
	16	Ő	ŏ	0	÷.	0	0	0	0	0	² 0	0	. Q	0	0	0	0	0	. 0
·	17	Ő	ŏ	0	· 0	0	0	0	0	0	0	0	0	0	0	0	0	. 0	0
·	Total	207	76	49	27	267	26	24	6	6	34	8	20	35	0	162	0	0 0	948
	10101									; ;	÷ ;	:					-		
									;			-			-				
Bus								<u>_</u>				44	10	12	14	15	16	17	Tola
0	D	1	2	3	4	5	6		8.	9	<u>10</u> 3	<u>11</u> 0	<u>12</u> 0	<u>13</u> 2	0	12	0	0	30
	1	0	8	3	2	0	0	0	0	0			ŏ	2	0	0	ŏ	ŏ	12
	- 2	7	0	2	0	0	0	0	0	Ō	1	0	· ŏ	2	0	ĭ	ŏ	ŏ	
	3		1	0	2	0	0	0	0	0		i õ	. 0	1	. ŏ	i	Ō	ŏ	
	- 4	2	0	2		0	0	0	0.	0	0	- 0	0	. 0	i õ	17	0	ŏ	3
	5		0	0	0	17	2	<u>.</u> 1		0 0	0	Ö	Ō	Ŏ	ŏ	0	ťŏ	· Õ	Ĩ
	6		0	0	0	2	0	3	0	Ö	0	0	0	ŏ	ŏ	Ő	Ō		:
	7	-	0	0	0	1	3	0	2	0	ŏ	. 0	- ŏ	ŏ	ŏ	0	0	0	
	8			. 0	0	0	0	2	0	ŏ	2	. 0	ŏ	ŏ	Ŏ	0	0	0	1.1
	9		0	0	0	0	0	0		2	0	ő	ŏ	ŏ	ŏ	Ö	ŏ	Ō	
	10		1	0	0	0	. 0	0	· 0	0	0	· o	1	2	0			ŏ	÷.,
	11		0	0	0	0	0			0	0	1	0	5	ŏ	•			
	12		0	0	. 0	0	0	0	0	0	0	. 2	5	0	Ö			Ő	
		: 1	1	2	2	1	0	0	0	0	0	0	0	0	ŏ			ŏ	
	13							0	v	v	0	V	v			-			
	14	0	0	0	. 0			Â	•	່ ຄ	•	^	•	•	n	0	0	. 0	
	14 15	0 14	.0	0	0	16	0	0	0	: 0 0	0	0 0	0	0	0	-			
	14	0 14 0				16 0		0	0 0 0	0 0 0	0	0 0	0 0	0 0 0	0 0 0	-	0	0	3

Α.5-9

TABLE A.5-3	FUTURE OD TABLE BY	VEHICLE TYPE:	ROUTE B	(2/6) - YEAR 2000 -
-------------	--------------------	---------------	---------	---------------------

Т	ruci	k.

	cķ	-													_					
0	Ð	1	2	3	4	5	6	7	8	9	\$0	11	12	13	14	15			Total	
	1	0	8	4	1	55	0	0	0	0	3	0	Ō	2	0	28		-		
	2	6	0	2	0	1	0	0	0	0	1	0	0	2	0	0				
	3	3	0	0 2	1	0	0	0	0	0	0 0	0 0	0 0	2	0	3 54	-		9 60	
	5	54	- 2	0	ŏ	39	3	1	ŏ	ŏ	0	0	0	2	0	34	0	-	139	
	ě	- 0	0	ŏ	õ	2	ŏ	3	ŏ	ŏ	ŏ	ŏ	ŏ	0	ŏ	0	0 0	ŏ	133	
	÷ 7	Ō	ō	ē	0	2	ž	ō	ŏ	ŏ	ŏ	ŏ	ŏ	ŏ	ŏ	ŏ	ŏ	ŏ	4	
	8	0	0	0	0	0	0	0	Ő	Ö	Ō	. 0	Ō	ō	Ŏ	0	Ō	õ	o O	
	9	0	0	0	0	0	0	0	0	0	2	0	0	ō	- 0	Ő	Ō	Ō	2	
	10	3	. 0	0	0	• • •	0	0	0	2	0	0	0	· 0	0	- 2	0	0	7	
	11	0		- 0	0	0	0	0	0	0	· 0	0	2	1	0	· 0	- 0	0	3	
	12	0	0	0	0	0	0	0	0	0	0	2	0	- 5	. 0	- 1	0	· 0	8	
	13	1	2	2	. 3	1	0	0	0	0	1	1	6	0	0	0	0	0	17	
	14	0	0	0	0 54	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
	15	32 0	0	0	୍ୟ 0	39 0	0	0	0	· 0 0	0	0	0	0	0	0	0	14	139	
	10	ŏ	Ö	0	Ö	Ö	ŏ	0	0	Ŭ Ŭ	0	0	0.	0	0	0 14	.0	0	0	
	Total	101	12	10	59	140	5	4	<u> </u>	2	7	3		16	0	139		<u>0</u> 14	<u>14</u> 521	
0	Vehicle D	1	2 150	3 82	4	5 401	6 4	7	8	9	10 43	11 0	12 0	13 33	14 0	15 177	16 0	- <u>17</u> 0	Total 915	·
	2	138	. 0	14	3	8	0	0	0	0	9	0	0	32	0	1	0	0		
	3	- 74	: _11 4	• 0	20	9	0	0	0	0	6	0	0	. 8	0	29	0	0	158	•
	. 4	18 388	13	19 7	0 3	6 374	0 20	0 10	0	0	4	2	4	37	0	55	0	0	149	1.
			10	1	0	18	20	39	3	0	6 0	0	1	5 0	0	248	0	0	1,076	
		2	- 1	1	· 0	8	41	0	- 1 1	0	0	Ö	ě	0	0	0	· 0 0	0	- 67 - 65	
	. 7		0	. 0	ŏ	ŏ	2	14	0	ŏ	Ö	Ő	ŏ	ĕ	ŏ	. 0	ŏ	ŏ	18	· · ·
	8	. 1		-	-	-	õ	0	Ŭ.	Ŏ	15	ŏ	ŏ.	ŏ	ŏ	ŏ	ŏ	÷ŏ	24	
	· ·	. I . 5	1	1	0	· 1	v .			· • · ·		1	0	2	Ō	6	· ŏ	° õ	93	
	8			1 6	0 : 4	: 1 6	õ	0	0	14	0					-	-			
	8 9	5	1				•		0	14 0	0 3	0	9	10	Ó (Ģ	0	·- 0	28	
	8 9 10 11 12	5 45 1 0	1 8 0 0	6	4 3 5	6	0 0 0	0	-		-			10 59	0 2 0	0 8	0	0 0	28 83	
	8 9 10 11 12 13	5 45 1 0 15	1 8 0 0 17	6 1 1 26	4 3 5 32	6 1 2 6	0 0 0 2	0 0 0 1	0 0 1	0 0 3	3 0 6	0 8 14	9 0 66	-	-		1.1		-	1
	8 9 10 11 12 13 14	5 45 1 0 15 0	1 8 0 0 17 0	6 1 1 26 0	4 3 5 32 0	6 1 2 6 0	0 0 0 2 0	0 0 0 1 0	0 0 1 0	0 0 3 0	3 0 6 0	0 8 14 0	9 0 66 0	59 0 0	0 0 0	8 2 0	0 0 0	0	83 192 0	
	8 9 10 11 12 13 14 15	5 45 1 0 15 0 223	1 8 0 17 0 1	6 1 1 26 0 1	4 3 5 32 0 54	6 1 2 6 0 248	0 0 2 0 0	0 0 1 0 0	0 0 1 0 0	0 0 3 0 0	3 0 6 0 0	D 8 14 0	9 66 0	59 0 0 0	0 0 0	8 2 0 0	0 0 0 0	0 0 0 14	83 192 0 542	
	8 9 10 11 12 13 14	5 45 1 0 15 0	1 8 0 0 17 0	6 1 1 26 0	4 3 5 32 0	6 1 2 6 0 248	0 0 0 2 0	0 0 0 1 0	0 0 1 0	0 0 3 0	3 0 6 0	0 8 14 0	9 0 66 0	59 0 0	0 0 0	8 2 0	0 0 0	0	83 192 0	

A.5-10

TABLE A.5-3 FUTURE OD TABLE BY VEHICLE TYPE: ROUTE B (3/6) - YEAR 2010 -

6.8	5
M	

.

M/C																	-+			
0	D		1	2	3	4	5 773	6	7	8	.9	10 51	11	<u>12</u> 0	13 48	<u>14</u>	15 -149	16	17	Total 1,357
		1 2	0 166	180 0	119 13	24 3	8	4	1	ŏ	0	7	0	ŏ	43	Ō	2	ŏ	ŏ	244
		3	114	12	0	24	15	1	1	0	ō	11	ò	Ō	0	0	40	0	0	218
		4	19	5	21	0	7	1	1	0	0	4	0	7	55	0	1	0	0	121
		5	789	12	13	4	371	17	10	3	0	7	0	1	- 2	0	206	0	0	1,436
		6	6	1	- 1	1	20	0	36	3	0	1	0	0	1	0	0	0	0	70 76
		7	4	1	1 1	1 0	10 0	43 0	0 20	14 0	0.	1 0	0	0	0	0	õ	· Õ	0	24
	•	8 9	2 5	4	2	0	:3	0	20	õ	ŏ	12	ŏ	ŏ	ŏ	ŏ	- 1	÷ 0	. 0	27
		10	47	6	12	5	. 7	1	1	0	15	0	0	0	0	0	9	0	0	103
	. :	11	- 2	· 0	2	2	2	0	0	0	0	2	0	3	10	0	0	0	0	24
		12	0	· 0	2	6	3	0	0	0	0	0	5	0	69	0	5	0	0	91
		13	22	22	31	41	9	3 0	1 (0	1	3	7	15 0	75	0 0	0	- 1 - 0	· 0	0	231 0
		14 15	0 192	0	0	0	218	0	õ	0	0	ĭ	ŏ	ŏ	ĩ	ŏ	- ŭ	ŏ	ŏ	415
		16	172	· o	0	0	0	ŏ	Ő	ŏ	ō	Ó	Ō	0	Ó	Ō	0	0	0	0
		17	Ō	ō	÷ 0.	0	0	0	0	0	Ō	0	0	0	0	0	0	0	0	0
	T		1,368	245	219	111	1,447	70	73	22	24	104	21	87	229	0	414	0	0	4,435
Linh																				
Ligh .0	D		· 1	2	3	4	5	6	7	8	9	10	11	12	.13	14	15	16	17	Total
		1	0	138	76	15	81	5	0	0	5	42	0	0	9	0	138	0	0	509
•		2	142	0	_ 7	4	5	0	0	0	0	. 1	. 0	0	6	0	0	0	0	171
		3	68	7	0	13	6	0	0	0	0	5 4	0 	0 4	7 11	· 0 0	9	0	0	59
		· 4 · 5	17 22	3 12	12 6	0 5	5 348	0 14	9	0	8.0	6	. 0	õ	4	ŏ	161	ŏ	ŏ	586
		6	7	0	0	0	9	0	31	5	0	. 0	Ō	Ō	Ó	0	0	0	0	52
		7	. 0	ŏ	0	Ō	6	31	Ó	: 11	0	0	< 0	0	0	0	0) Q	• 0	48
	1.	8	0	0	0	0	0	4	ា	0	: 0	0	0	0	0	0	0	0	0	15
	- ⁻	9	5	0	0	0	0	0	0	: 0	· 0	9	0	0	0	0.	0	. 0 0	0	14 79
		10	42	7	5	. 4	5	0	0	0	7	0	3	0	3	· 0 0	3	i õ	. 0	17
		11	0	0	0 0	4	0	0	- 0	0	0	0	5	0	24	ŏ	4	ŏ	ŏ	37
• •	Ņ	13	. 7	6	8	9	3	· 0	° Õ	0	ે <u>ટ</u> ે	3	4	24	0	0	2	: 0	0	68
		14	0	: · .	0	0	0	0	E 0	0	5.0	·- 0	0	0	0	. 0	. 0	0	0	0
		15	184	0	0	Ö	135	0	0	0	0	0	0	0.	0	्	0	0	0	319
;	ł	16	0	0	0	0	<u>'</u> 0	0	0	0	0.	0	0	0	0	0	0	0	0	0
		17 fotal	494	0 173	0 • 114	0 58	0 603	<u>0</u> 54	<u>0</u> 51	0 16	· 0 14	0 79	-15	35	67	0	317	Ō	0	2,091
<u></u>		Ulai	4,34												. :				× :	
Bus	. ¹											· ·	· ·				<u> </u>			
0	Ð		<u> </u>	2	3	4	5	6	7	: 8	9	10	. 11	12	<u>13</u> 3	<u>14</u>	- 15 24	16	17	Total 56
		1	0	13	7	3	0	0	· 0 · 0	· 0 0	0	5 3	0 0	0	3	· Ö	0	0	ŏ	21
		2 3	12	0	3 0	03	0	÷ŏ	ŏ	·: 0	õ	ŏ	Ö	ŏ	. 3	Ő	3	0	. 0	16
		4	2	ŏ	3	ŏ	ō	ŏ	i õ	. 0	- 0	0	0	0	3	· 0	. 0	0	0	: 8
•		5	: 0	0	0	0	27	2	3	·. 0	0	0	0	0	0	0	32	0	0	64
		6	0	0	0	0	2	0	5	0	0	0	0	0	0	0	0	0	0	7
		7	0	0	0	0	3	5	0	- 3	0	· 0	· 0	0	. 0 . 0	· 0	0	0	0	11
		8	0	0	0	0	0	0	3	0	0	03	0	ŏ	0	.0	ŏ	0	ŏ	: 3
		9 10	· 0 5	0 3	0	0	ŏ	0	- 0	õ	3	õ	ŏ	ŏ	ō	ŏ		Ō	0	11
		11	0	0	ŏ	ŏ	ŏ	Ň	õ	0	0	÷ 0	Ő	3	3	Ó		· 0	ं 0	· 6
		12	. 0	Ō	0	0	0	0	0	0	0	• 0	3	0	9	0			0	12
		13	3	2	3	2	2	0	0	0	0	0	3	9	0	0		0	0	24
		- 14	0	0	0	0	0	0	0	0	0 0	0	0	0	0 · Ò	0			0	0 60
		15	29	0	0	0 0	31 0	0.	0	0	. U	0	. 0	0	0	0			ŏ	0
		16 17	0	0	0	0		0	Õ	ŏ.	ŏ	ŏ	ŏ	ŏ	. 0	Ő		-	Ő	0
•	i	Total	- 55	21	16	8		7	11	3	3	11	6	12	24	0	60	0	0	303
																				
							н н. С		:	. •	· .		•							
	·																		-	
									A	.5-11	. •	-								÷
			1											11.1						

į

•

TABLE A.5-3 FUTURE OD TABLE BY VEHICLE TYPE: ROUTE B	74761 VEAD 4010
- TADLE A.3-3 FUTURE OD TADLE DE VEHICLE ETER, ROUTE B	(4/0) · IEAK 2010 -

Tru								· · · · ·												
	D 1		2 15	<u>3</u> 6	4		<u>6</u> 0	7	8	<u>9</u> 0	<u>10</u> 5		12	13		15		17		
	1	. u 11	15	3	0	90 2	0	0	0	0		0	0	3	0	57	0	0		
	3	6	ŏ	0	2	Ó	ŏ	ŏ	ŏ	0	2 0	. 0 0	0	3	0	0 5	0	0		
	4	3	0	3	0	ŏ	- ŏ	Ő	Ō	ŏ	ŏ	0	ŏ	3	0	191	0 0	ŏ		
	5	94	4	ŏ	ŏ	64	4	2	ō	ŏ	ŏ	ŏ	ŏ	3	0	71	0	0		
	6	0	0	ŏ	ŏ	2	0	5	ŏ	ŏ	ŏ	ŏ	ő	0	Ő	0	0	ŏ	7	
	7	- Õ	ŏ	ŏ	ŏ	4	3	ŏ	ŏ	ŏ	ŏ	ŏ	ŏ	ŏ	Ő	õ	ŏ	ŏ	7	
	8	Ő	ŏ	Ö	õ	ō	ŏ	ŏ	ŏ	ŏ	õ	ŏ	ŏ	0	ŏ	Õ	. 0	ŏ	ó	
	- 9	ŏ	ŏ	Ŏ	ŏ	ŏ	ŏ	ŏ	ŏ	ŏ	3	ŏ	ŏ	ŏ	- ŏ	ŏ	ŏ	ŏ	3	
	- 10	6	Ŏ	. ŏ	ŏ		ŏ	ŏ	õ	3	ō	ŏ	· ŏ	ŏ	ŏ	. 3	ě	÷ŏ	12	
	÷11	- Õ	ŏ	ō	÷0	-	· ŏ	ŏ	ŏ	ŏ	. ŏ	÷ŏ	ં ૩	š	ŏ	ŏ	Ő	ŏ	6	
	12	õ	ō	ō	ŏ	Ō	ō	· ŏ	ő	ō	ŏ	3	ŏ	· 9	÷ ŏ	ંડે	ŏ	ŏ	15	
	13	2	3	3	5	2	ō	ŏ	ŏ	ŏ	ž	3	10	ŏ	. Õ	÷ŏ	ŏ	ŏ	30	
	14	0	0	. 0	0	· 0	0	Ō	÷ 0	Ó	i Ö	0	0	0	0	· 0	0	ō	0	
	15	66	· 0	- 0	191	72	Ó	Ó Ó	Ó	0	0	0	0	Ó	Ó	Ō	0	29	358	
	16	0	0	0	0	0	ò	0	Ō	0	0	Ó	Ó	- 0	Ō	0	Õ	0	0	
	17	0	0	0	0	0	0	0	0	0	0	0	Ó	0	Ó	29	Ō	0	29	
	Total	188	22	15	200	245	7	1	0	. 3	12	6	13	27	0	360	0	29	1,134	
	Vehicle D																;			
~			2		4	5	6	7	8	9	10		12	13	14	15		17	Total	
	. 1.	0	346	208	44	952	9	3	0	10	103	0	0	63	0	368	0	0	2,107	
	2	331	0	26	7	16	1	1	0	0	19	0	0	55	0	. 2	0	0	458	
	÷ 3 4	192	22	0	42 0	21 : 12	1	1	0	0	16	.0	0	13	0	57	0	0	365	
	4	905	8 27	39	9	810	1 27		0		8	3	11	72	0	192	0	0	388	
	э 6	905 13	- 27	19	- 9 - 1	33	37 0	24 77	· 8	1 0	13 1	0	1 0	9	0	470 ò	0	0	2,328	
	. 0	; ¹³	1	1	5 F	23	82	0	28	0	1		0	1	0.	0	0	0	136	
	8	2	1	1	· 0	20	4	34	20	ŏ	0	0	0	1	0	0	0	. U 0	143 43	
	9	: 10	4	2	·· ŏ	3	0	0	Ő	0	27	0	0	0	0	1	Ö	0	43	
1	10	100	16	17	- 9	12	1	៍រ	ŏ	28	0	3	ō	3	0	16	0	0	205	
	11	2	ō	: 2	÷ 6	2	0	0	ŏ	0	Š	ŏ	16	19	õ	1	· ŏ	ŏ	53	
	12	ō	ŏ	2	÷ 10	- 3	Ő	. 0	õ	ŏ	ŏ	16	ŏ	m	ŏ	12	ŏ	ŏ	155	
	13	34	33	45	57	17	ં રૂં	1	1	5	12	25	118	0	0	3	Ö	ŏ	354	
•	14	0	- 0	0	0	0	Ő	0	0	Ō	0	õ	0	ŏ	ŏ	0	ŏ	ŏ	0	1.1
- 	15	470	1	1	192	456	- 0 -	0	0	0	: • • •	Ō	° Õ	· 1	ō	ō	÷ŏ	29	1,152	
- 1 - L	16	÷ 0	÷ 0	0	0	0	0		0	0	0	0	Ó	0	0	÷ŏ	° Õ	0	0	

TABLE A.5-3 FUTURE OD TABLE BY VEHICLE TYPE: ROUTE B (5/6) - YEAR 2020 -

WC

MC					<u> </u>														
0	D	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	Tota
	1	0	316	218	44	1,290	6	5	1	9	91	0	0	85	: 0	310	0	0	2,375
	2	286	0	23	6	14	1	1	0	: 0	. 11	0	0	70 0	0	3 80	0	0	415
	3	201 34	20 8	0	42 0	25 11	1	1	0	0	19 7	0	0 9	89	0	5	0 0	0	389 200
	4	39 1,323	18	38 18	5	560	29	13	5	1	12	Ő		3	ŏ	389	. O	ŏ	2,377
	6	1,525	: 2	2	1	35	0	56	6	0	1	ŏ	o	ĩ	ŏ	õ	Ő	ŏ	118
	7	7	2	2	1	15	72	õ	25	. 0	1	Ō	· 0	1	i õ	ō.	-0-	Ō	127
	8	3	1	1	1	0	0	37	0	0	1	Ō	- 0	1	0	Ō	Ő	Ō	44
	9	7	6	5	0	4	Ō	0	0	0	21	· 0	0	0	0	1	0	0	45
	10	84	9	19	11	13	1	1	0	24	0	0	0	0	0	15	0	0	177
	11	3	0	3	2	3	0	· 0	⊂ O	0	2	0	5	17	0	1	0	0	36
	12	0	0	5	8	5	Q	0	÷ 0	· 0	0	11	· • •	106	0	11	0	0	147
	: 13	35	33	55	65	11	3	3	1	6	12	21	125	0	0	2	0	0	372
	14	0	0	0	0	0	0	0	0	0	0	0	0	· 0	0	. 0	0	0	(
	15	399	2	2	1	408	0	0	0	0	1	0	1	1	. 0	. 0	0	0	816
	16	0	0	0	- 0	0	0	0	0	0	0	0	0	0	0	. 0	0	0	
	· 17	0		0	0	0	0 115	0 119	0 39	<u>0</u> 41	0 179	<u>0</u> 33	0 142	0 374	0	0 814	0	0	7,638
	10(3)	2,394	416	391	187	2,393	115	119	39	41	179	33	142	014		015	0	<u> </u>	7,000
Ligh	t		•	•															
0	D	1	2	3	4	5	6	7.	. 8	9	10	11	12	13	14	15	16	17	Tota
	1	0	236	137	28	121	. 7	0	0	7	75	0	. 0	15	0	262	0	0	888
	2	242	0	13	6	. 9	0	0	0	0	12	0	0	10	0	· 0	0	0	292
	3	121	12	0	22	10	Q	0	0	0	8	, . 0	0	11	0	- 22	0	0	205
	4	. 27	- 7	22	0	8	0	0	0	0	7	- 4	7	16	0	0	0	0	. 98
	5	35	17	.11	9	525	22	. 14	0	0	9	<mark>.</mark> 0 .	0	6	0	322	0	• 0	97(
	6	11	- <u>0</u>	0	0	16	0	50	9	0	0	0	0	0	0	0	0	0	87
	7	0	0	0	0	6	52	-0	19	0	0	0	0	0	0	<u></u>	0	0	8(
	8	0	0	. 0	0	0	8	19	0	0	0	0	0	0	0	0	0	0	27
	9 10	9 72	0	0	0	0	0	0	0	0 12	: 14 0	· 0 5	0	6	0	0	· 0	0	136
	-11	0	0	.0	5	0	0	0	0	0	· 5	0	ា	·	0	0	õ	Ö	26
	12	0	Ő	.0	6	0	0	0	- 0	ŏ	0	. 9	Ó	38	.: ŏ	7	0	Ö	60
	13	ា	10	13	-14	4	0	ŏ	ŏ	4	5	6	40	0	÷ŏ	3	÷ŏ	Ō	111
	14	0	0	0	0	0	ŏ	0	ŏ	0	Ő	÷ 0	0	- 0	Ō	÷ō	0	Ō	0
	15	339	0	ŏ	ŏ	· ·	Ō	ō	0	0	0	0	Ō	0	o	÷ õ	0	0	625
	16	0	Ó	0	0	0	0	0	0	0	0	0	0	0	0	0	0	·: 0 ·	0
	17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
	Total	868	294	204	97	995	89	84	28	23	136	24	58	108	0	621		0	3,630
										:			7	- 					
Bus								· .				· · · ·							
0	D	1	2	3	4	5	6	<u>. 7</u> 0	<u>8</u> 0	9	10	<u>11</u> 0	12	13	<u>14</u>	15 44	16	17	Total 84
	1		17	9.	3	0	0	0	0	Ö	5	0	0	6	0	0	ŏ	ŏ	32
	2	15 5	0 :4	6	0	0	0	0	· 0	Ö	- 0	. ŭ	Ö	Š	÷ŏ	6	ŏ	ŏ	25
	4	2	0	-5	0	Ö	ŏ	ŏ	ŏ	ŏ	÷ŏ	ŏ	Ő	4	. ŏ	ŏ	ŏ	ō	11
	5	- 0	ŏ	ŏ	ŏ	22	3	3	ŏ	ŏ	ð	ŏ	. Õ	0	ŏ	64	0	Ŏ.	93
	6	ŏ	ŏ	ŏ	ŏ	4	ŏ	ĩ	ŏ	ŏ	Ö	: ŏ	0	ō	Ō	0	Ó	Ö.	11
	7	ō	· ŏ	ŏ	Ő	3	8	0	5	· 0	0	0	5 0 1	0	0	0	. 0	0	16
	8	Õ	ŏ	ō	ō	Ō	Ō	5	0	0	0	0	0	0	0	¹ 0	0.1	0	· 5
	9	0	Ō	Ō	Ō	0	Ō	0	0	0	- 4	0	[:] 0	0	0	0	0	0	4
	10	7	5	ō	Ő	Ó	Ō	0	0	4	0	0	0	0	0	Ō	0	Ò	16
	11	Ó	Ō	Ó	0	0	0	0	. 0	0	0	0	14	5	0	0	0	Ò	9
	12	0	0	0	0	0	0	0	0	0	0	4	0	14	0	. 0	0	0	18
	13	3	5	5	4	3	0	0	0	0	0	5	14	0	0	0	0	Ó	39
	14	0	0	0	0	0	0	0	0	0	0	0	0	· 0	0	0	Ò	0	j (
	15	54	0	0	0	61	0	0	0	0	0	0	0	0	0	0	0	0	115
	16	0	0	· 0	0	0	0	÷ 0	0	0	0	0	0	0	0	0	0	0	0
	. 10																		
	17 Total	0	0 31	0 25	0	0 94	0	0.	0	<u>0</u> 4	0 16	0	0 18	<u>0</u> 38	0	115	<u>0</u>	0	0 479

	D	1	2	<u> </u>	- 4		6	7	· 8	9	10	- 11	12	13	14	15	16	17	To
	1	- 0	24	10	3	119	0	0	0	0	7	0	0	5	0	114	0	0	2
	2	16	0	4	0	4	0	0	0	0	3	0	0	6	0	0	0	0	
	3	7	0	0	3	0	0	0	0	0	0	0	0	5	0	12	0	0	
	4	3	0	5	0	0	0	0	0	0	0	0	0	5	0	230	0	0	2
	5	118	5	0	0	75	6	3	0	0	0	0	0	4	0	136	0	÷ 0	3
	6	0	; 0	0	0		· 0	_ 7	0	0	0	0	· 0	0	0	0	0	0	
	7	0	0	0	0	5	5	0	0	- 0	0	0	0	÷ 0	Ó	0	0	÷ 0	
	8	0	0	0	0	0	. 0	0	0	0	0	0	0	0	0	0	0	0	
	9	. 0	0	0	• 0	•	0	0	0	0	4	0	· 0	0	0	0	. 0	· 0	
	10	· 9	. 0	. 0	0	0	0	0	0	4	0	0	0	< 0	· 0	6	÷ 0	. 0	1
	- 11	0	0	0	0	0	0	0	0	0	0	0	- 4	5	0	· 0	0	0	
	12	. 0	0.	0	· 0	0 I	0	0	0	Ó	· 0	4	0	15	0	5	0	0	
	13	4	4	5	7	4	0	0	0	0	- 4	: 4	18	0	0	0	0	- 0	
	14	0	· 0	0	0	0	0	0	0	0	: 0	: 0	0	0	· 0	0	0	0	
	15	130	0	0	230	140	0	0	0	0	: 0	0	0	0	Ó	0.	· 0	45	5
	16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
	17	0	0	. 0	0	.0	0	0	0	0	0	0	0	0	0	45	0	0	4
	Total	287	33	24	243	352	11	10	0	4	18	8	22	45	0	549	0	45	1,6
	/ehicle	· ·	· .				<u> </u>												
4!! \ 0	D	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	Tot
	D 1	0	593	374	78	1,531	13	6	1	16	180	0	0	109	14	15 730	16 0	17 0	
	D 1 2	0 559	593 0	374 46	78 12	1,531 26	13 1	6 1	1 0	16 0	180 31	0	0	109 92		730 3	·		3,63
	D 1 2 3	0 559 334	593 0 36	374 46 0	78 12 71	1,531 26 35	13 1 1	6 1 1	1 0 0	16 0 0	180 31 27	0 0 0	0 0 0	109 92 21	0 0 0	730 3 119	0 0 0	0 0 0	3,60 77 64
	D 1 2 3 4	0 559 334 66	593 0 36 15	374 46 0 70	78 12 71 0	1,531 26 35 19	13 1 1 1	6 1 1	1 0 0 0	16 0 0 0	180 31 27 14	0 0 0 4	0 0 0 16	109 92 21 114	0 0 0 0	730 3 119 232	0 0 0 0	0	3,63 77 64 55
	D 1 2 3 4 5	0 559 334 66 1,475	593 0 36 15 39	374 46 0 70 29	78 12 71 0 15	1,531 26 35 19 1,182	13 1 1 1 60	6 1 1 33	1 0 0 0 5	16 0 0 0	180 31 27 14 21	0 0 0 4 1	0 0 0 16 2	109 92 21 114 14	0 0 0 0 0	730 3 119 232 911	0 0 0 0	0 0 0	Tot 3,60 77 64 55 3,78
	D 1 2 3 4 5 6	0 559 334 66 1,475 23	593 0 36 15 39 2	374 46 0 70 29 2	78 12 71 0 15	1,531 26 35 19 1,182 59	13 1 1 1 60 0	6 1 1 33 120	1 0 0 5 15	16 0 0 1	180 31 27 14 21 1	0 0 4 1 0	0 0 16 2 1	109 92 21 114 14 14	0 0 0 0 0 0	730 3 119 232 911 0	0 0 0 0 0 0	0 0 0 0 0	3,60 77 64 55 3,78 22
	D 1 2 3 4 5 6 7	0 559 334 66 1,475 23 7	593 0 36 15 39 2 2	374 46 0 70 29 2 2 2	78 12 71 0 15 1	1,531 26 35 19 1,182 59 31	13 1 1 60 0 137	6 1 1 33 120 0	1 0 0 5 15 49	16 0 0 1 0	180 31 27 14 21 1	0 0 4 1 0 0	0 0 16 2 1 1	109 92 21 114 14 1 1	0 0 0 0 0 0 0	730 3 119 232 911 0 0	0 0 0 0 0 0	0 0 0 0 0 0	3,63 77 64 55 3,78 22 23
	D 1 2 3 4 5 6 7 8	0 559 334 66 1,475 23 7 3	593 0 36 15 39 2 2 1	374 46 0 70 29 2 2 2 1	78 12 71 0 15 1 1	1,531 26 35 19 1,182 59 31 0	13 1 1 60 0 137 8	6 1 1 33 120 0 61	1 0 0 5 15 49 0	16 0 0 1 0 0 0	180 31 27 14 21 1 1	0 0 4 1 0 0	0 0 16 2 1 1 0	109 92 21 114 14 1 1 1	0 0 0 0 0 0 0 0	730 3 119 232 911 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0 0	3,66 77 64 55 3,78 22 23 7
	D 1 2 3 4 5 6 7 8 9	0 559 334 66 1,475 23 7 3 16	593 0 36 15 39 2 2 1 6	374 46 0 70 29 2 2 2 1 5	78 12 71 0 15 1 1 1 0	1,531 26 35 19 1,182 59 31 0 5	13 1 1 60 0 137 8 0	6 1 1 33 120 0 61 0	1 0 0 5 15 49 0	16 0 0 1 0 0 0 0	180 31 27 14 21 1 1 1 43	0 0 4 1 0 0 0 0	0 0 16 2 1 1 0 0	109 92 21 114 14 1 1 1 0	0 0 0 0 0 0 0 0 0 0	730 3 119 232 911 0 0 0 0	0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0	3,60 77 64 55 3,78 22 23 7 7 7
	D 1 2 3 4 5 6 7 8 9 10	0 559 334 66 1,475 23 7 3 16 172	593 0 36 15 39 2 2 2 1 6 26	374 46 0 70 29 2 2 2 1 5 27	78 12 71 0 15 1 1 1 0 18	1,531 26 35 19 1,182 59 31 0 5 21	13 1 1 60 0 137 8 0 1	6 1 1 33 120 0 61 0 1	1 0 0 5 15 49 0 0	16 0 0 1 0 0 0 0 0 44	180 31 27 14 21 1 1 1 43 0	0 0 4 1 0 0 0 0 5	0 0 16 2 1 1 0 0	109 92 21 114 14 1 1 1 0 6	0 0 0 0 0 0 0 0 0 0	730 3 119 232 911 0 0 0 0 1 27	0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0	3,60 77 64 55 3,78 22 23 7 7 7 34
	D 1 2 3 4 5 6 7 8 9 10 11	0 559 334 66 1,475 23 7 3 16 172 3	593 0 36 15 39 2 2 1 6 26 0	374 46 0 70 29 2 2 2 1 5 27 3	78 12 71 0 15 1 1 1 0 18 7	1,531 26 35 19 1,182 59 31 0 5 21 3	13 1 1 60 0 137 8 0 1 0	6 1 1 33 120 0 61 0 1 0	1 0 0 5 15 49 0 0 0 0	16 0 0 1 0 0 0 0 0 44 0	180 31 27 14 21 1 1 1 43 0 7	0 0 4 1 0 0 0 5 0	0 0 16 2 1 1 0 0 24	109 92 21 114 14 1 1 1 0 6 32	0 0 0 0 0 0 0 0 0 0 0	730 3 119 232 911 0 0 0 1 27 1	0 0 0 0 0 0 0 0 0 0 0		3,60 77 64 55 3,78 22 23 7 7 7 34 8
	D 1 2 3 4 5 6 7 8 9 10 11 12	0 559 334 66 1,475 23 7 3 16 172 3 0	593 0 36 15 39 2 2 1 6 26 0 0	374 46 0 70 29 2 2 2 1 5 27 3 5	78 12 71 0 15 1 1 1 0 18 7 14	1,531 26 35 19 1,182 59 31 0 5 21 3 5	13 1 1 60 0 137 8 0 1 37 8 0 1 0 0	6 1 1 33 120 0 61 0 1 0 0	1 0 0 5 15 49 0 0 0 0 0	16 0 0 1 0 0 0 0 44 0 0	180 31 27 14 21 1 1 1 43 0 7 0	0 0 4 1 0 0 0 0 5 0 28	0 0 16 2 1 1 0 0 24 0	109 92 21 114 14 1 1 1 0 6 32 173	0 0 0 0 0 0 0 0 0 0 0	730 3 119 232 911 0 0 0 0 1 27 1 24	0 0 0 0 0 0 0 0 0 0 0		3,60 77 64 55 3,78 22 23 7 7 34 8 24
	D 1 2 3 4 5 6 6 7 8 9 10 11 12 13	0 559 334 66 1,475 23 7 3 16 172 3 0 53	593 0 36 15 39 2 2 1 6 26 0 0 52	374 46 0 70 29 2 2 1 5 27 3 5 78	78 12 71 0 15 1 1 1 1 0 18 7 14 90	1,531 26 35 19 1,182 59 31 0 5 21 3 5 21 3 5 23	13 1 1 60 0 137 8 0 1 37 8 0 1 0 0 3	6 1 1 33 120 0 61 0 1 0 3	1 0 0 5 15 49 0 0 0 0 0 0	16 0 0 1 1 0 0 0 0 0 44 0 0 10	180 31 27 14 21 1 1 1 43 0 7 0 21	0 0 4 1 0 0 0 0 5 0 28 36	0 0 16 2 1 1 0 0 24 0 197	109 92 21 114 14 1 1 1 0 6 32 173 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0	730 3 119 232 911 0 0 0 0 1 27 1 24 5	0 0 0 0 0 0 0 0 0 0 0 0 0 0		3,60 77 64 55 3,78 22 23 7 7 7 34 8 24 57
	D 1 2 3 4 5 6 7 8 9 10 11 12 13 14	0 559 334 66 1,475 23 7 3 16 172 3 0 53 0	593 0 36 15 39 2 2 2 1 6 26 0 52 0	374 46 0 70 29 2 2 2 2 1 5 27 3 5 78 0	78 12 71 0 15 1 1 1 1 0 18 7 14 90 0	1,531 26 35 19 1,182 59 31 0 5 21 3 5 21 3 5 23 0	13 1 1 60 0 137 8 0 1 37 8 0 1 0 0 3 0	6 1 1 33 120 0 61 0 1 0 3 0 3	1 0 0 5 15 49 0 0 0 0 0 0 1 0	16 0 0 1 0 0 0 0 0 44 0 0 0	180 31 27 14 21 1 1 1 43 0 7 0 21 0	0 0 4 1 0 0 0 0 5 0 28 36 0	0 0 16 2 1 1 0 0 24 0 197 0	109 92 21 114 14 1 1 1 0 6 32 173 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	730 3 119 232 911 0 0 0 1 27 1 24 5 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		3,60 77 64 55 3,78 22 23 7 7 34 8 24 57
	D 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15	0 559 334 66 1,475 23 7 3 16 172 3 0 53 0 923	593 0 36 15 39 2 2 1 6 26 0 52 0 52 0 2	374 46 0 70 29 2 2 2 2 1 5 27 3 5 78 0 3	78 12 71 0 15 1 1 1 1 0 18 7 14 90 0 231	1,531 26 35 19 1,182 59 31 0 5 21 3 5 23 0 894	13 1 1 60 0 137 8 0 137 8 0 137 8 0 137 8 0 137 0 0 0	6 1 1 33 120 0 61 0 1 0 3 0 0 0	1 0 0 5 15 49 0 0 0 0 0 0 0 0 1 0	16 0 0 1 0 0 0 0 0 44 0 0 0 10 0 0	180 31 27 14 21 1 1 1 43 0 7 0 21 0 1	0 0 4 1 0 0 0 5 0 28 36 0 0	0 0 16 2 1 1 0 0 0 24 0 197 0 1	109 92 21 114 14 1 1 1 0 6 32 173 0 0 1		730 3 119 232 911 0 0 0 1 27 1 24 5 0 0 0		0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 45	3,6 77 64 55 3,78 22 23 7 7 34 8 24 57 2,10
	D 1 2 3 4 5 6 7 8 9 10 11 12 13 14	0 559 334 66 1,475 23 7 3 16 172 3 0 53 0	593 0 36 15 39 2 2 2 1 6 26 0 52 0	374 46 0 70 29 2 2 2 2 1 5 27 3 5 78 0	78 12 71 0 15 1 1 1 1 0 18 7 14 90 0	1,531 26 35 19 1,182 59 31 0 5 21 3 5 21 3 5 23 0	13 1 1 60 0 137 8 0 1 37 8 0 1 0 0 3 0	6 1 1 33 120 0 61 0 1 0 3 0 3	1 0 0 5 15 49 0 0 0 0 0 0 1 0	16 0 0 1 0 0 0 0 0 44 0 0 0	180 31 27 14 21 1 1 1 43 0 7 0 21 0	0 0 4 1 0 0 0 0 5 0 28 36 0	0 0 16 2 1 1 0 0 24 0 197 0	109 92 21 114 14 1 1 1 0 6 32 173 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	730 3 119 232 911 0 0 0 1 27 1 24 5 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		3,63 77 64 55

TABLE A.5-3 FUTURE OD TABLE BY VEHICLE TYPE: ROUTE B (6/6) - YEAR 2020 -

A.5-14