

however, was not be represented in the simulation and inundation in the lowest reaches was not well simulated in the study.

12.5.4 POTENTIAL INUNDATION STUDY IN PASIG RIVER BASIN

Potential flood inundation over flood prone areas in the Pasig river basin was simulated under the following condition for 2 cases of probable flood hydrographs in different return periods which were given by the study of USACE. The flood runoff was input at the outlet of the Timbu river.

Topographic data : DTM produced by the 1995 simulation study
 : Area of analysis 27 km x 10 km
 : Mesh size 100 m x 100 m

Hydrographs at Delta 5	
Return period	Peak discharge (m ³ /s)
20-year flood	430
100-year flood	490

Sediment concentration is given by Brown's equation for the initial discharge

The distribution of maximum water depth of every meshes is illustrated on topographic maps produced by GIS as shown in Figure 12.17 for 20 year flood and Figure 12.18 for 100 year flood.

The potential inundation areas estimated in this study are summarized as follows:

Inundation Area in Pasig river basin (unit: ha)		
Water Depth	20-Year Flood	100-Year Flood
0 < h < 0.2	3,596	2,434
0.2 < h < 1.0	2,246	3,922
1.0 < h	224	487
Total	6,066	6,843

Total area of analysis : 27000 ha

12.6 FUTURE PROSPECT OF DISASTER MITIGATION MEASURE

12.6.1 High Risk Areas (See Figure 12.19)

(1) Lahar Avulsion into the Taug River

In June and early July 1995, the riverbed near Delta 5 aggraded by 2 to 3 m, then lahar avulsion into the Taug River was anticipated to extend the damage to Angeles City. During the 1995 rainy season channel down-cutting and widening proceeded in the whole stretch of the Pasig-Potrero River. As the active channel incised deeper, the natural ridge between the Pasig and Taug rivers became wider. This means that the width to be eroded also became wider. Thus, these channel development processes make avulsion beyond this ridge or lateral erosion to break through it less unlikely.

(2) Lahar Avulsion into the Porac River

Lahar avulsion into the Porac River has been anticipated since the beginning of the 1991 eruption. The possibility of lahar overtopping in the right bank into the Porac River becomes smaller because of the progressing channel incision. Although there is still some possibility of lahar intrusion into the Porac River by progressive meandering to break through the deposits and the terrace, the distance from the active channel to the Porac

River is more than 2 km as of now. The necessary measure to be taken in the 1996 rainy season is close monitoring regarding this matter.

(3) Lahar Overtopping around the Angeles-Porac Road

Most of the big-scale mudflows that reached to the Angeles-Porac road overtopped the left bank due to change of riverbed gradient. At present the prevailing active channel is more than 100 m wide and 20 m deep, and the flow capacity could be evaluated as corresponding to more than a 500-year flood if the riverbank was stable against flood runoff. In accordance with the reduction of frequency of mudflow occurrence, lahar overtopping in the left bank becomes more unlikely. On the other hand, the incised meander is progressing in the whole stretch, and there is some possibility of breaking the dike and overbanking onto the area in Porac and Bacolor. The necessary measure to be taken in the 1996 rainy season is also close monitoring regarding this matter.

(4) Dike Breach and Overbanking Floods along the Gugu Tertiary Dike

The major issue along the downstream reach of the Gugu tertiary dike is also dike breaching and overbanking floods caused by progressive incised meandering. Once flood water completely scours the base of the dike and reaches the low ground, it starts to rush toward the lower areas with new channeling and widely spreading out transported sediment as created in Bacolor from August to October 1995. Several critical portions were found along the old channel formed in August 1995. In order to prevent this type of flooding, construction of a protective structure with firm foundation is required at the diversion point and proper monitoring is necessary from the Angeles-Porac road to the diversion point.

(5) Dike Breach along the Right Tertiary Dike

If the diversion channel shifts toward the catch basin of the right tertiary dike, a disaster similar to the August-October 1995 events will likely happen to Santa Rita and Guagua. In order to prevent dike breaching and flooding with severe sediment deposition in Santa Rita and Guagua, the possible countermeasures are (1) construction of river training structure from the diversion point to the downstream end of the tertiary dike along the active channel, (2) construction of protective open levee with slope protection outside of the existing tertiary dike, and (3) continuous dredging and excavation in the center channel from the diversion point to the downstream end of the tertiary dike.

Combination of the protective open levee and channel excavation is deemed to be the most applicable countermeasure among the alternatives taking necessary maintenance and reliability of structures against anticipated riverbed fluctuation and meandering into consideration. It is required to connect the open levee to the right primary dike upstream of the Santa Barbara bridge for discharging overtopped flood water back to the Pasig-Potrero River, so as to prevent extending floods to the downstream areas.

(6) Flooding and Sediment Deposition along the Active Channel

Flooding and sediment deposition along the active channel on the lower reaches is the most serious and urgent problem in the whole stretch of the Pasig-Potrero River. The lower reaches have to receive muddy water even in a small amount of rain, and then transported sediment gradually accumulates over the ponding areas. The possible countermeasures are (1) construction of new channel and embankment along the active channel, (2) closing the active channel, and channel excavation along the primary dike between the diversion point and the confluence with the Guagua River, (3) construction of the protective ring dike with slope protection along the left bank of Palawe Creek connecting to the right dike of the San Fernando River, and (4) construction of the protective open levee with slope protection traversing from Dolores to Santa Barbara across the affected area.

Combination of the protective open levee and channel excavation is also deemed to be the most applicable countermeasure taking necessary land acquisition and necessary maintenance into consideration. It is required to connect the open levee to the left primary dike near the Santa Barbara bridge for discharging flood water back to the Pasig-Potrero main channel.

12.6.2 Basic Concept on Required Activities

During the 1995 rainy season, the Pasig River incised deeply on the pre-eruption alluvial deposit as well as the lahar deposit after the 1991 eruption, and the frequent and sharp meandering progressed in the whole stretch like a river course on the alluvial plain. The progress of meandering was observed to be very rapid because bank material of lahar deposit has a non-cohesive nature due to lack of clay particles. If this type of meander, incised and free meander, is planned to be controlled, bank protection work with deep foundation has to be made over the whole stretch because of the rapid progress of meandering. This type of measure is extremely costly, so that meandering which is now progressing on the Pasig River could be regarded as uncontrollable. Thus, continuous monitoring activity will play an important role to prevent serious flooding and sediment deposition, in particular, along the upper and middle reaches.

After every moderate-scale lahars and heavy rain shower, monitoring along the active channel should be conducted from Watch Point 5 to the downstream end of the tertiary dike. The major purposes of monitoring is inspecting the location and situation of the active river channel, clarifying the critical portions and their levels, and selecting the appropriate remedial measures.

Table 12.1 Major Lahar Events in Pasig-Potrero River in 1995

Lahar Event	Daily Rainfall (mm)	Range of Deposition Depth (m)	Volume of Deposits (million m ³)	Remarks
June 1 to 7	40 (Jun. 01) 13 (Jun. 02) 62 (Jun. 03) 17 (Jun. 04) 20 (Jun. 06) 16 (Jun. 07)	1.0	1	Typhoon Auring
July 7 to 11	61 (Jul. 07) 24 (Jul. 09) 27 (Jul. 10) 7 (Jul. 11)	Inner Area : 0.5-3.0 Outer Area : 0.8	5	
July 18	65 (Jul. 18)	0.2-1.0	2	
July 27 to 30	6 (Jul. 27) 68 (Jul. 28) 36 (Jul. 29) 109 (Jul. 30)	Inner Area : 0.6-2.6 Outer Area : 0.2-3.0	15	Typhoon Karing
August 15 to 19	44 (Aug. 15) 13 (Aug. 17) 46 (Aug. 18) 38 (Aug. 19)	Inner Area : 0.5-4.0 Outer Area : 1.0-1.8	14	
August 28 to September 3	25 (Aug. 28) 80 (Aug. 29) 49 (Aug. 30) 12 (Sep. 02) 69 (Sep. 03)	Inner Area : 0.2-4.0 Outer Area : 1.0-2.8	27	Typhoon Gening and Helming
September 30 to October 1	32 (Sep. 30) 251 (Oct. 01)	1.4-4.2	22	Typhoon Maneng
Total			86	

Note : 1) Daily rainfall indicates the data of Upper Sacobia Gauge observed by PHIVOLCS.

2) Inner area means the area between the tertiary dike system, while outer area means the area outside this system.

3) Volume of deposits indicates the volume of sediment accumulated since the earlier event.

Table 12.2 Estimate of Channel Erosion in 1995

Channel Segment	Average Eroded Area (m ²)	Active Channel Length (km)	Volume of Channel Erosion (million m ³)
Mouth of Timbu Creek - Delta 5	1,800	3.0	5.4
- Dike-Breach Point	2,400	6.4	15.4
- Diversion Point	1,500	6.2	9.3
- Downstream End of Dike System	570	18.6	10.6
Total			40.7

Note : Channel segment between diversion point and downstream end of dike system includes both the previously active and diversion channels.

Table 12.3 Summary of Secondary Explosion and Lahar Events
in 1992

Month	Rainfall (mm)	Frequency of Secondary Explosion H: Column Height in km				Frequency of Lahar in Number of Days					
		H: Column Height in km				Sacobia River			Pasig River		
		H<1	1≤H<3	3≤H<5	5≤H	Small	Moderate	Big	Small	Moderate	Big
Jan	0										
Feb	0										
Mar	0										
Apr	2		1								
May	98		2								
Jun	321	1	1								
Jul	527		5	1							
Aug	925	12	10	1	9						
Sep	171	20	16		4						
Oct	135	4	2		2						
Nov	36	1	1								
Dec	0										
Total	2215	38	38	2	15	-	-	-	-	-	-

Note: Monthly rainfall is referred to data observed at P12

Lahar data is not compiled on the daily basis

in 1993

Month	Rainfall (mm)	Frequency of Secondary Explosion H: Column Height in km				Frequency of Lahar in Number of Days					
		H: Column Height in km				Sacobia River			Pasig River		
		H<1	1≤H<3	3≤H<5	5≤H	Small	Moderate	Big	Small	Moderate	Big
Jan	0										
Feb	0	1									
Mar	0										
Apr	0										
May	0										
Jun	463	8	4			3	1				1
Jul	349	10	9	1		2	3		2		1
Aug	689	3	9	2	6	7	4		8		1
Sep	449		5	6		14	2		6		
Oct	319	6	18	1		4	2	1	2		4
Nov	171	2	2	1					1		2
Dec	52		2								
Total	2492	30	49	11	6	30	12	1	19	9	0

Note: Monthly rainfall is referred to data observed at P12

in 1994

Month	Rainfall (mm)	Frequency of Secondary Explosion H: Column Height in km				Frequency of Lahar in Number of Days					
		H: Column Height in km				Sacobia River			Pasig River		
		H<1	1≤H<3	3≤H<5	5≤H	Small	Moderate	Big	Small	Moderate	Big
Jan	21				1						1
Feb	59	1	4								1
Mar	29	6	3								1
Apr	2	2	2		1				1		1
May	28	14	5						6		
Jun	120	3	4			5	1		3		2
Jul	1086	4	11	3		12	2		3		3
Aug	434	2	17	7	3	9	1		7		2
Sep	289	3	8	2	3	15	1		16		5
Oct	188	4	6	1	5	1	1		7		1
Nov	0	1							3		
Dec	13										
Total	2269	40	60	13	13	42	6	0	46	16	10

Note: Monthly rainfall is referred to data observed at UPPER-SACOBIA

in 1995

Month	Rainfall (mm)	Frequency of Secondary Explosion H: Column Height in km				Frequency of Lahar in Number of Days					
		H: Column Height in km				Sacobia River			Pasig River		
		H<1	1≤H<3	3≤H<5	5≤H	Small	Moderate	Big	Small	Moderate	Big
Jan	0										
Feb	0										
Mar	19								1		1
Apr	0										
May	258		1			2			4		2
Jun	211	2				2			2		3
Jul	508		2	1	2	4	1		5		3
Aug	501	3	2	2	1	1	2		4		1
Sep	484	3	5			2			4		4
Oct	374	3	5	2			1		1		1
Nov											
Dec											
Total	2355	11	15	5	3	11	6	0	21	21	5

Note: Monthly rainfall is referred to data observed at UPPER-SACOBIA

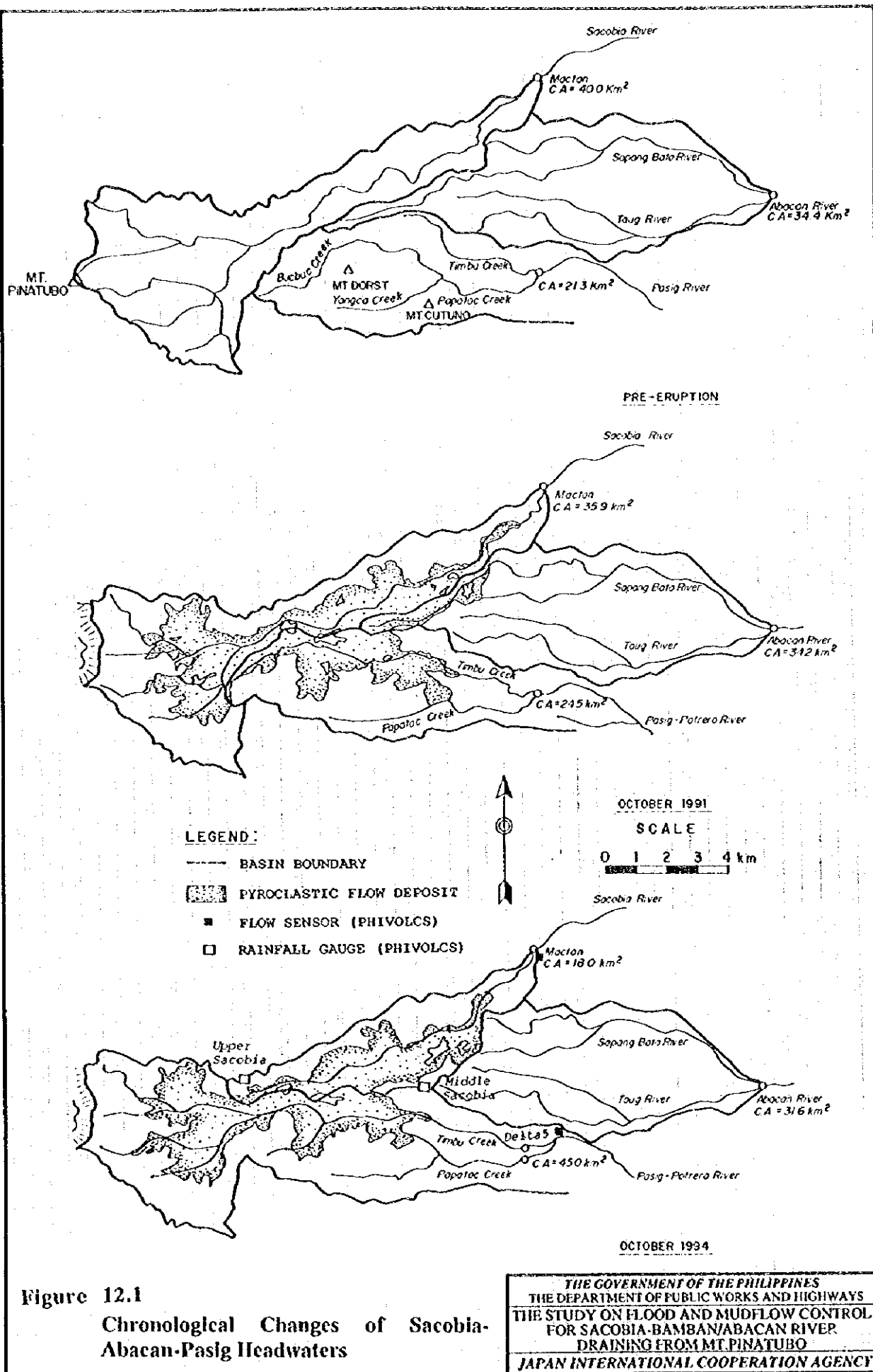
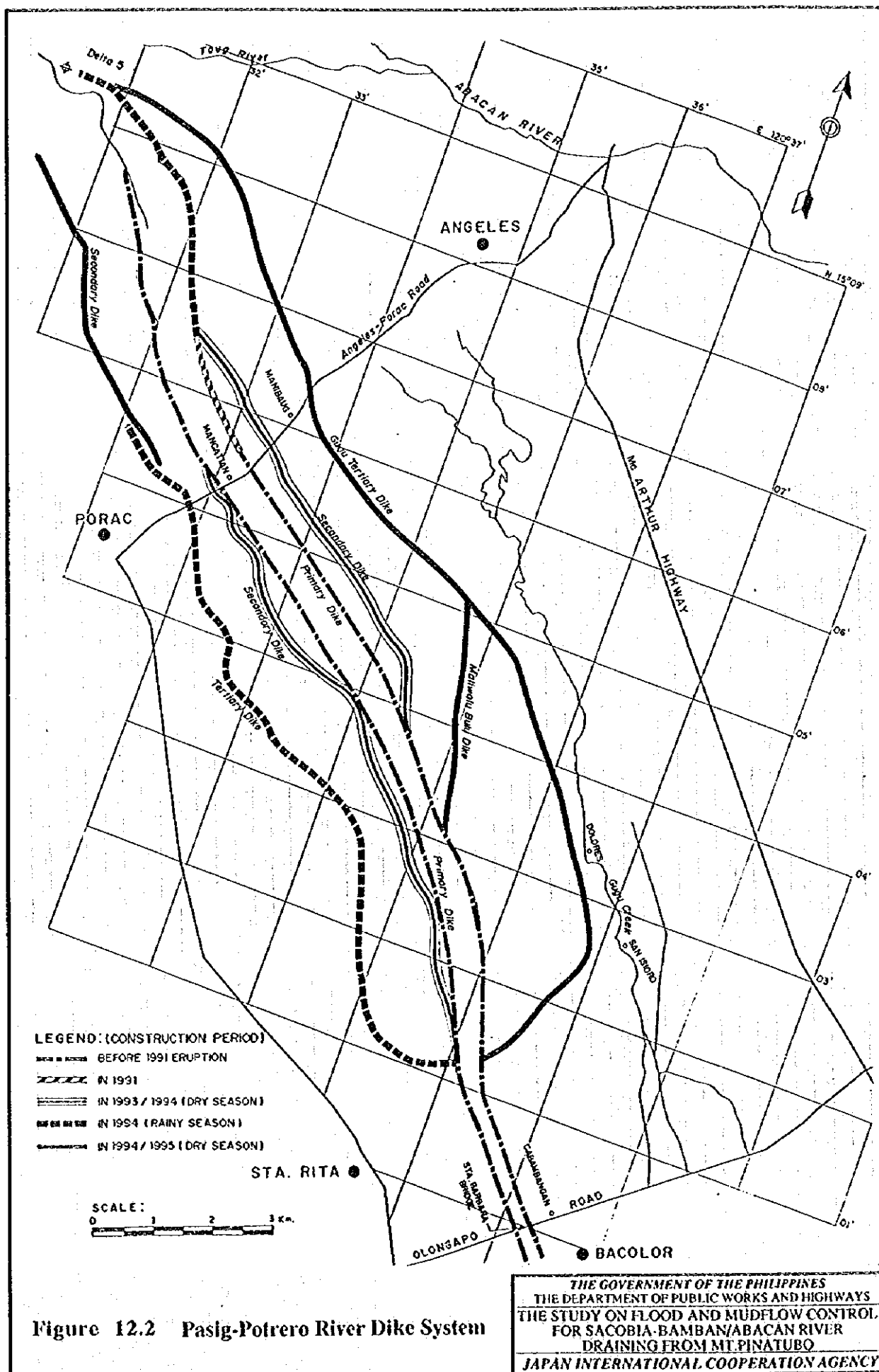
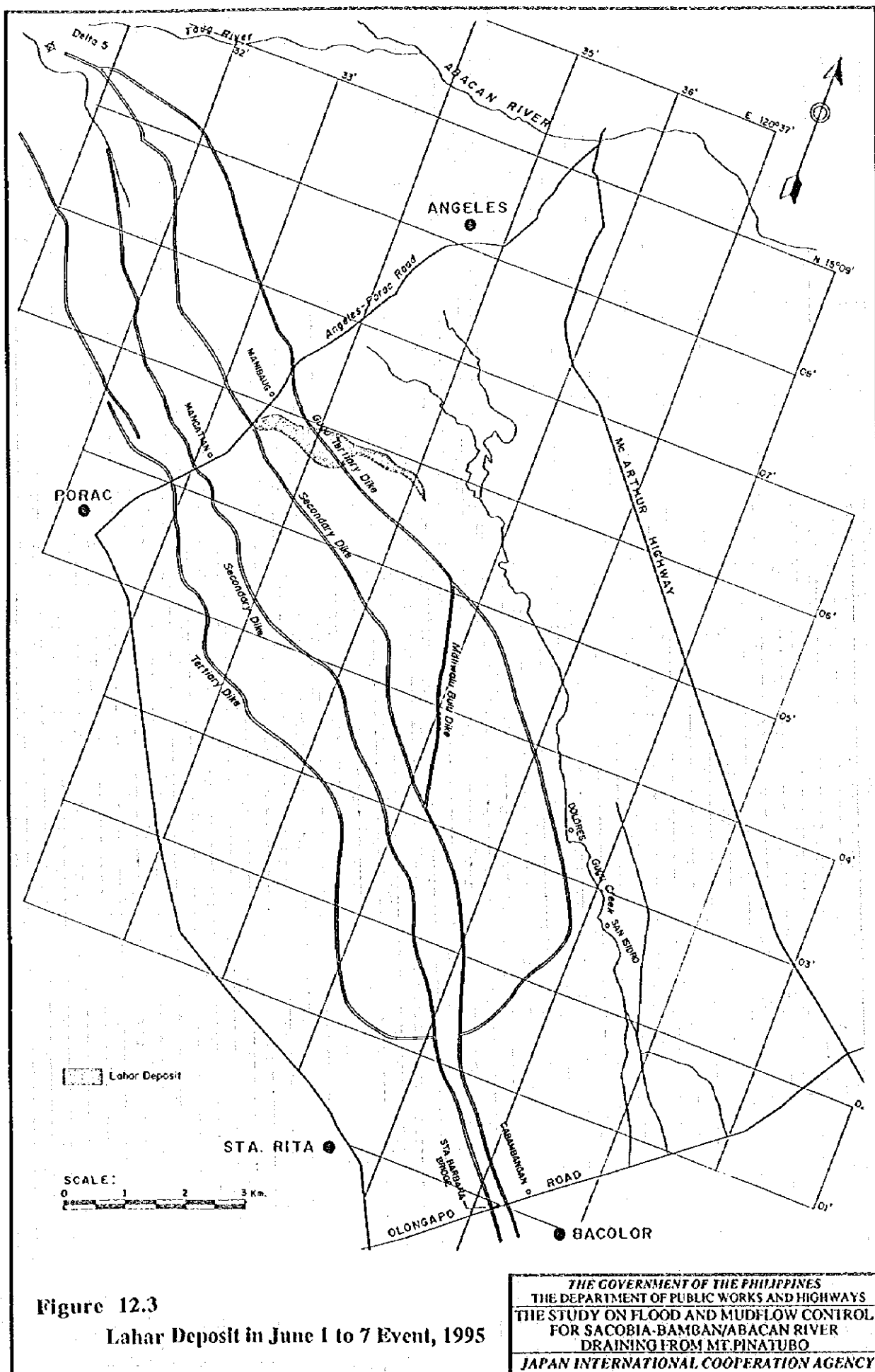
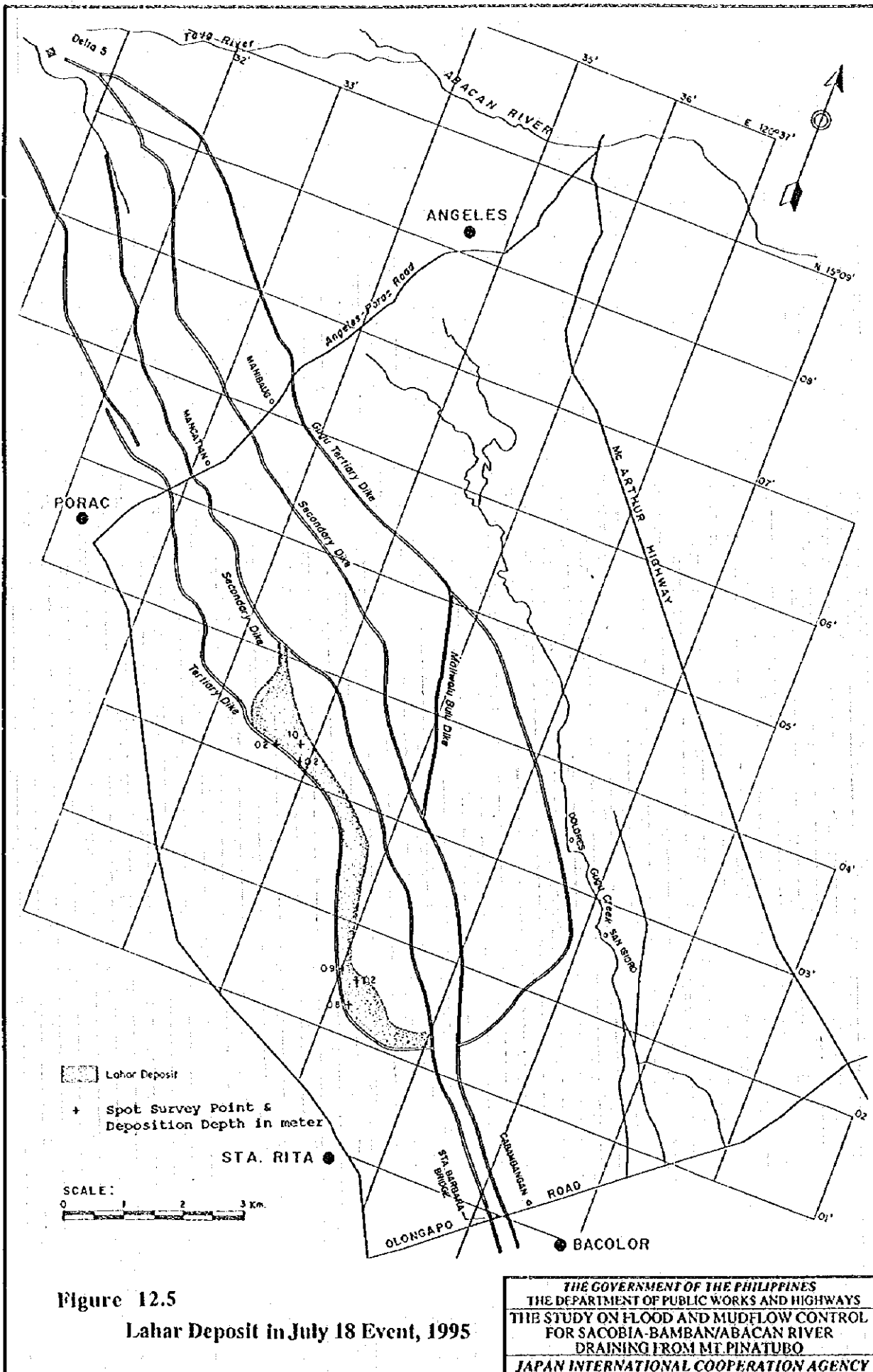


Figure 12.1
Chronological Changes of Sacobia-
Abacan-Pasig Headwaters







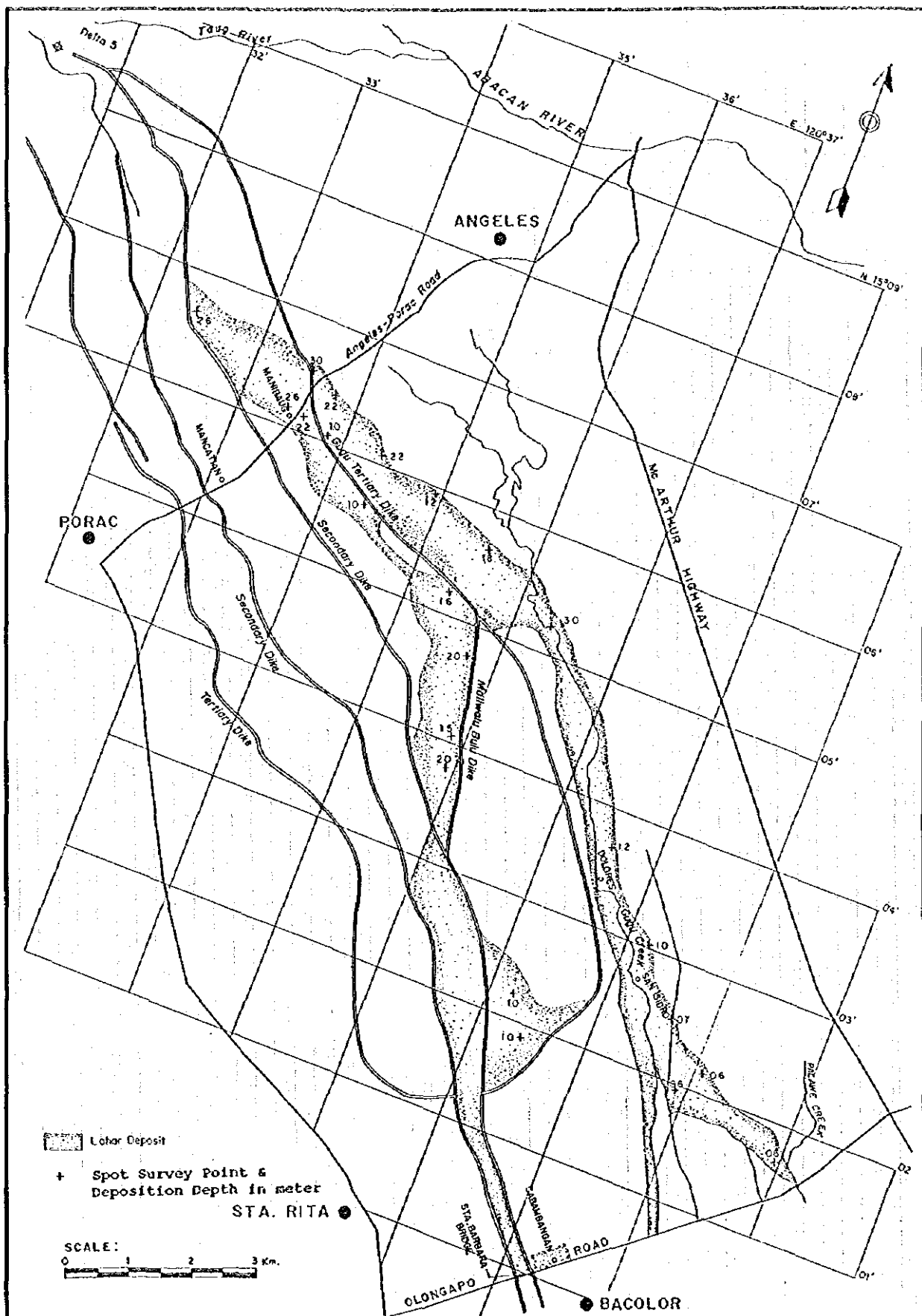
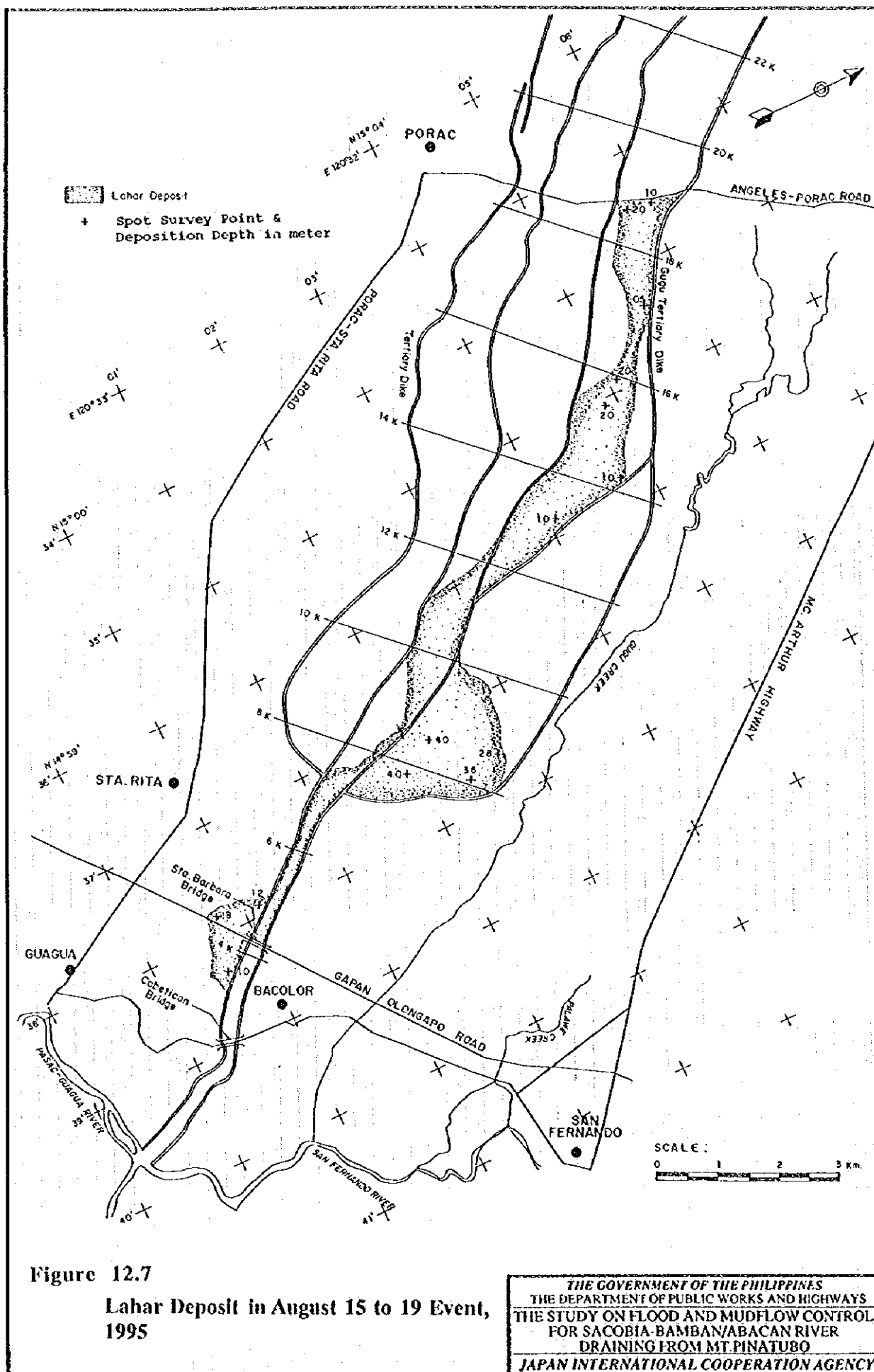


Figure 12.6
Lahar Deposit in July 27 to 30 Event, 1995

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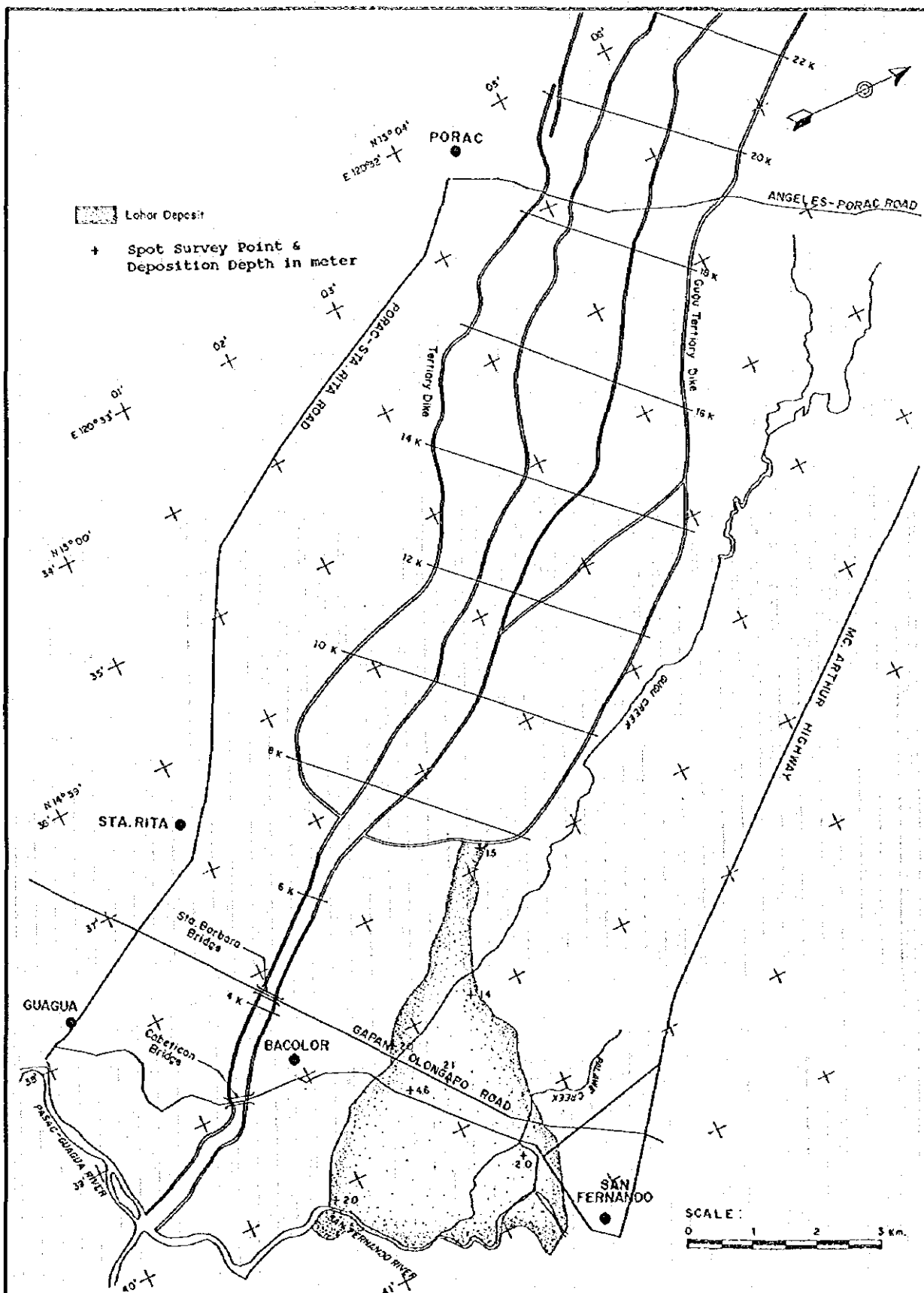







Figure 12.9
Lahar Deposit in September 30 to
October 1 Event, 1995

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LEGEND:

-  AREA COVERED BY LAHAR DEPOSITS IN 1991
-  ADDITIONAL AREAS COVERED BY LAHAR DEPOSITS IN 1992
-  ADDITIONAL AREAS COVERED BY LAHAR DEPOSITS IN 1993
-  ADDITIONAL AREAS COVERED BY LAHAR DEPOSITS IN 1994
-  ADDITIONAL AREAS COVERED BY LAHAR DEPOSITS IN 1995

SCALE:
0 1 2 3 km

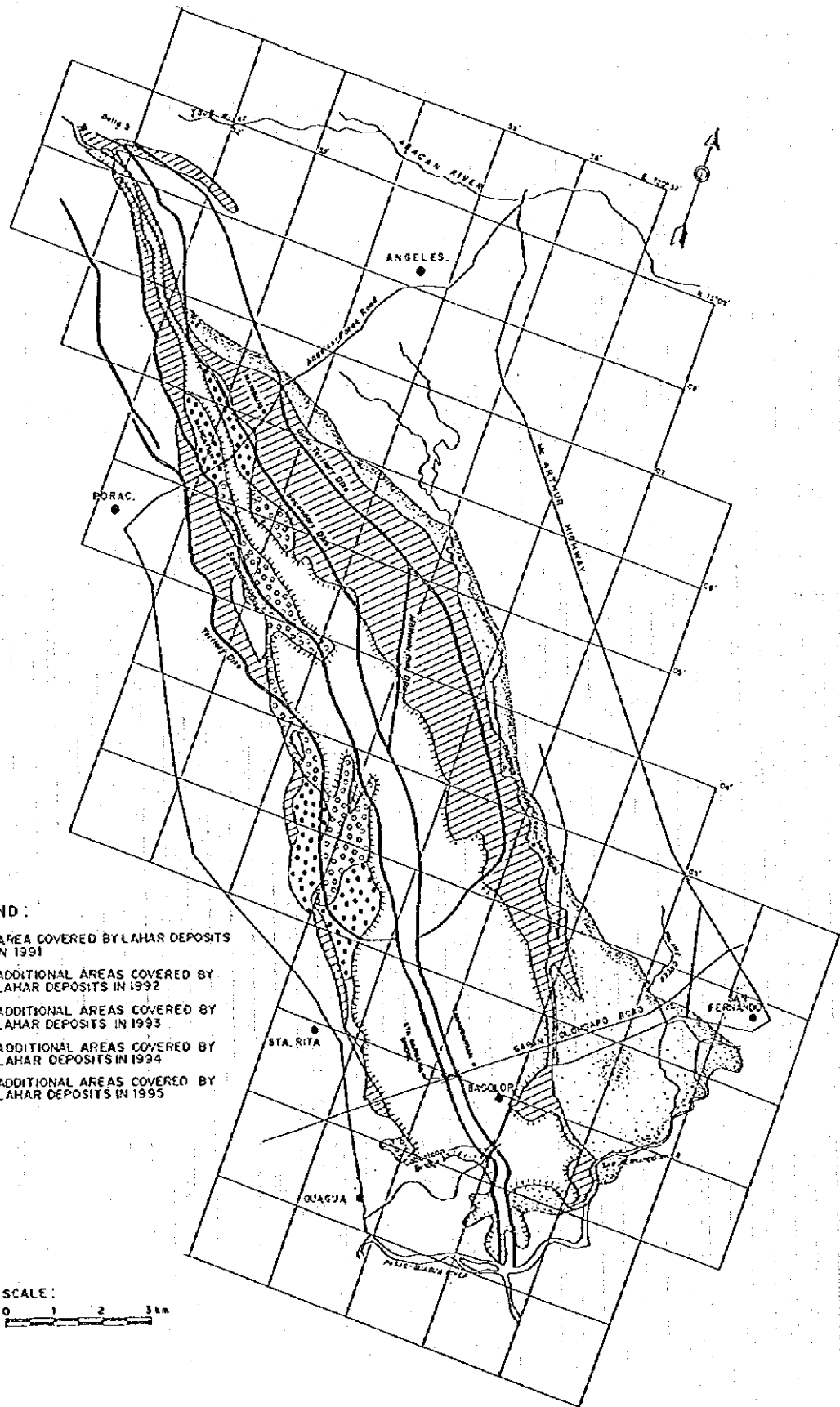


Figure 12.10
Lahar Deposits after 1991 Mt. Pinatubo Eruption

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Sediment Concentration
by Volume (%)

Observed Sediment Concentration

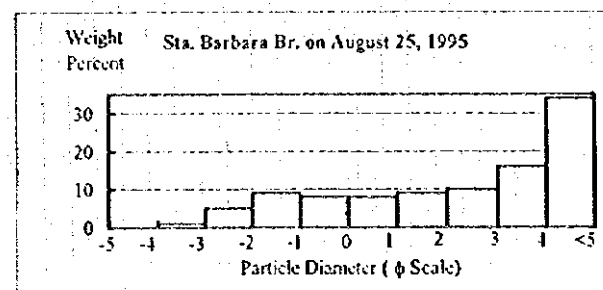
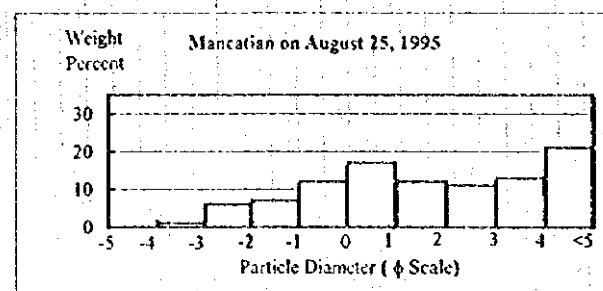
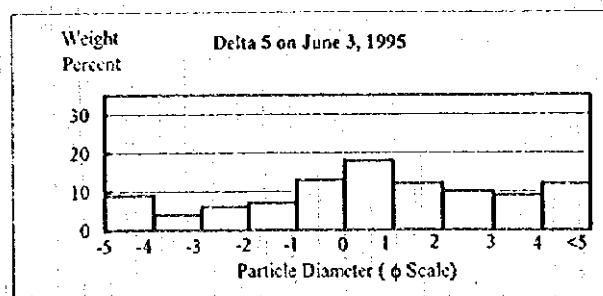
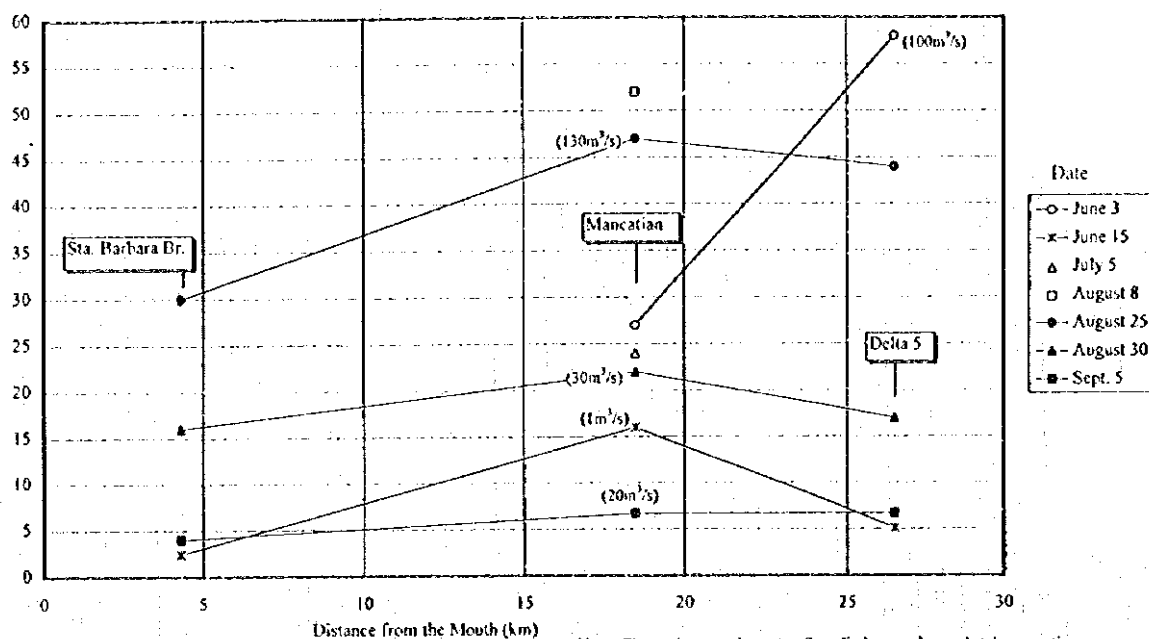


Figure 12.11
Observed Sediment Concentration and
Transported Material in Pasig-Potrero River

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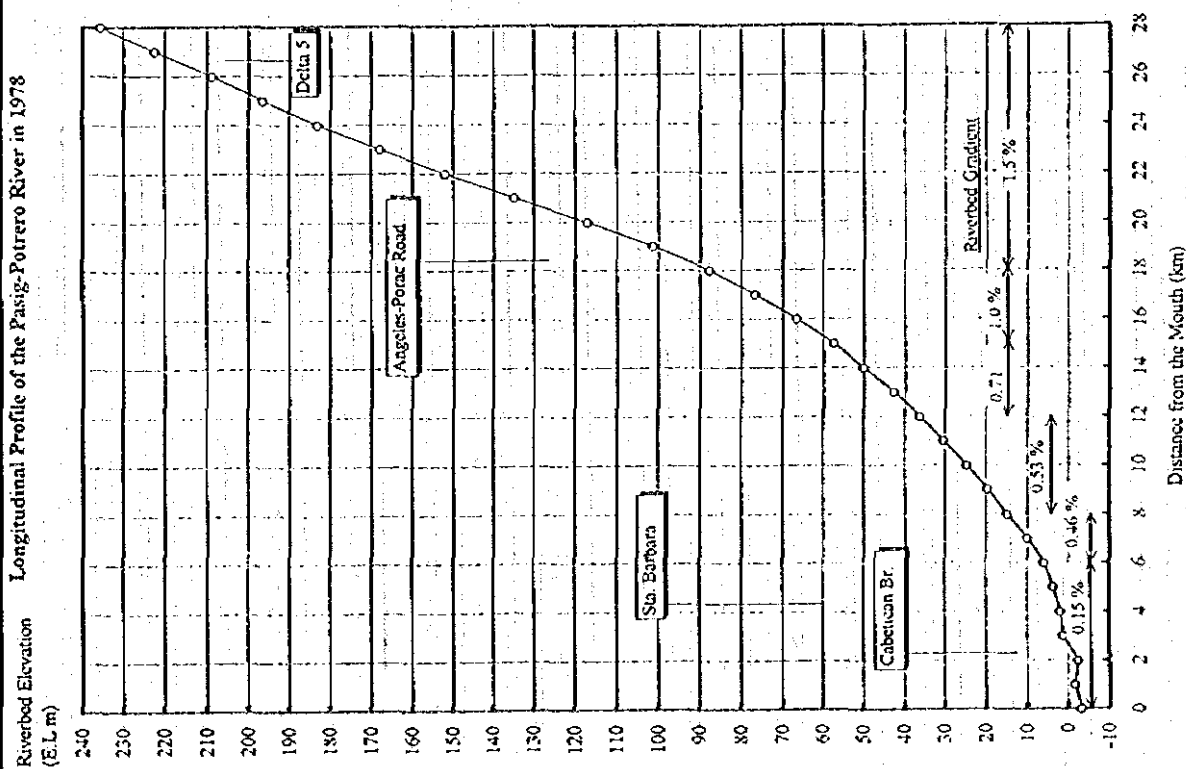
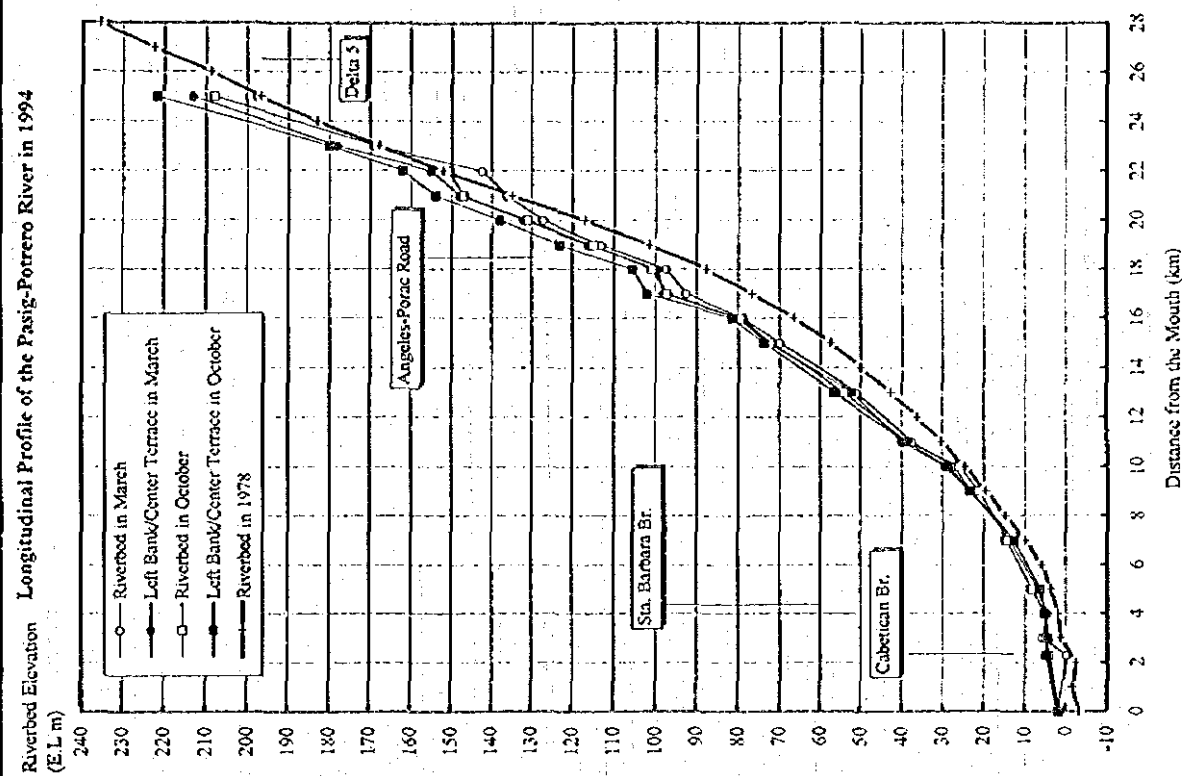
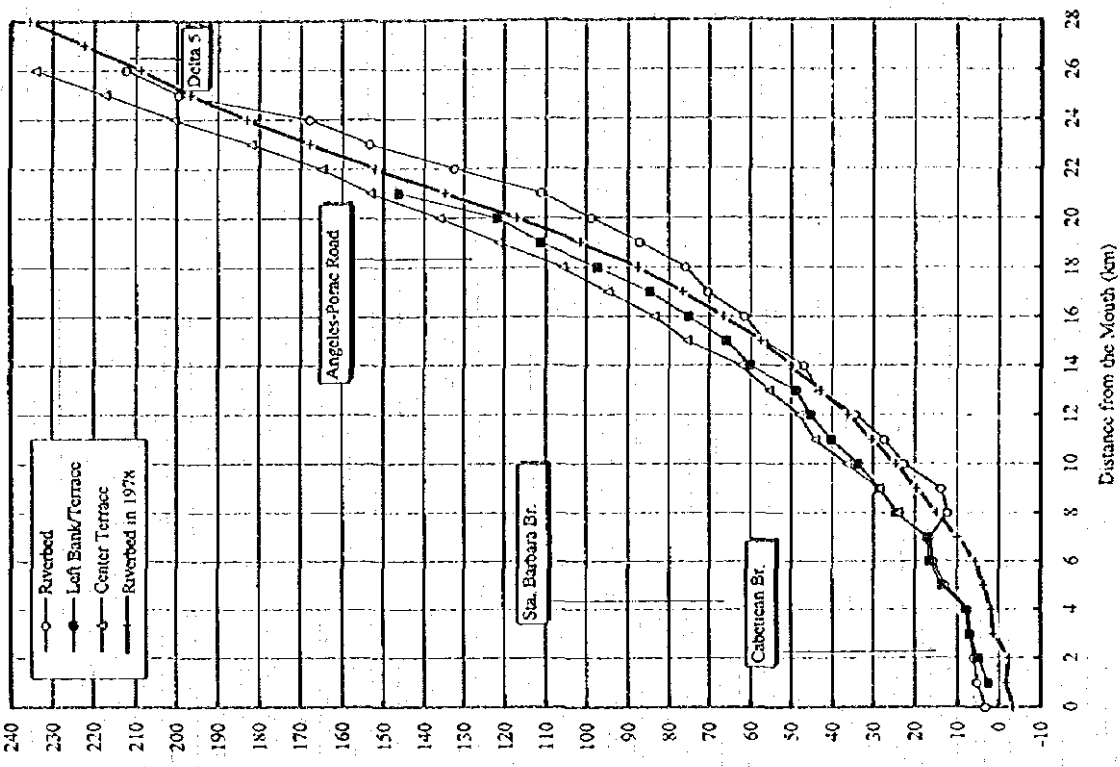


Figure 12.12 (1/2)

Changes of Longitudinal Profile of
Pasig-Potrero River

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Riverbed Elevation Longitudinal Profile of the Pasig-Potrero River in October 1995
(E.L.m)



Riverbed Elevation Longitudinal Profile of the Pasig-Potrero River in July 1995
(E.L.m)

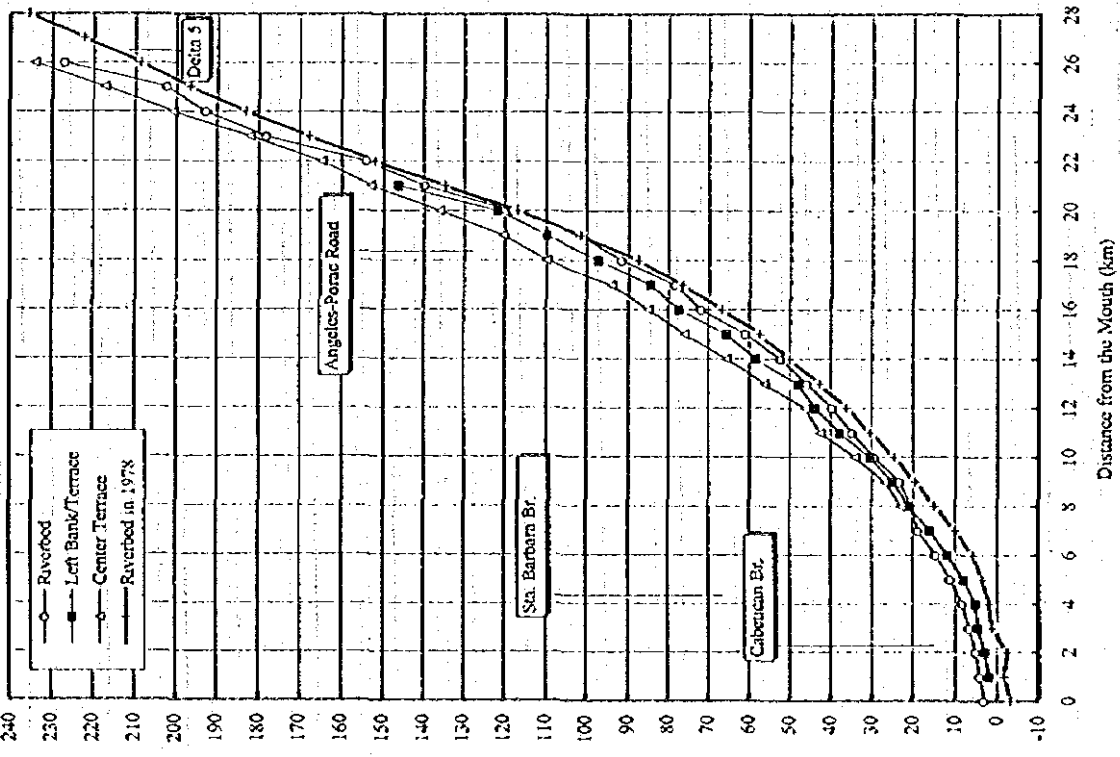


Figure 12.12 (2/2)

Changes of Longitudinal Profile of
Pasig-Potrero River

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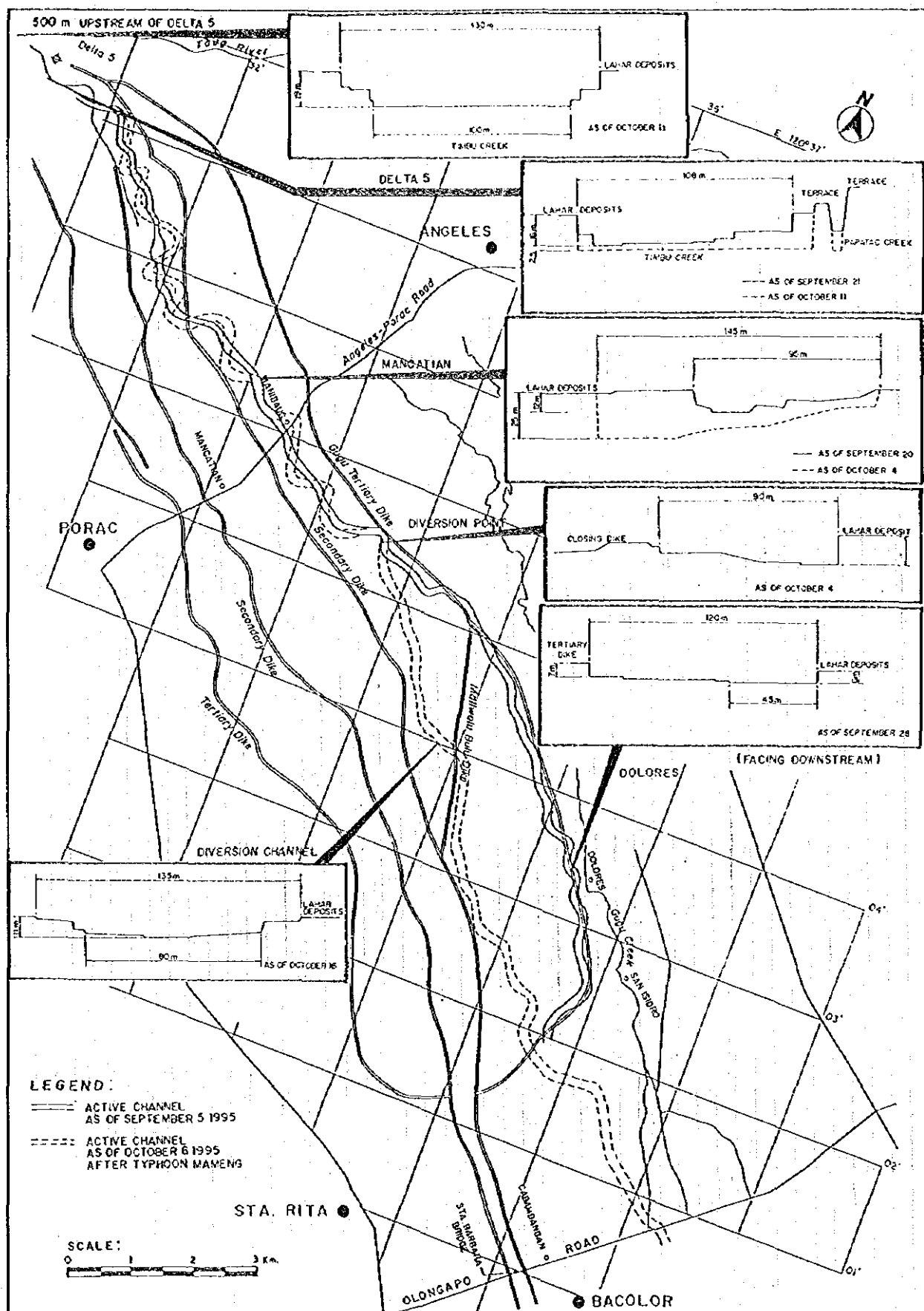
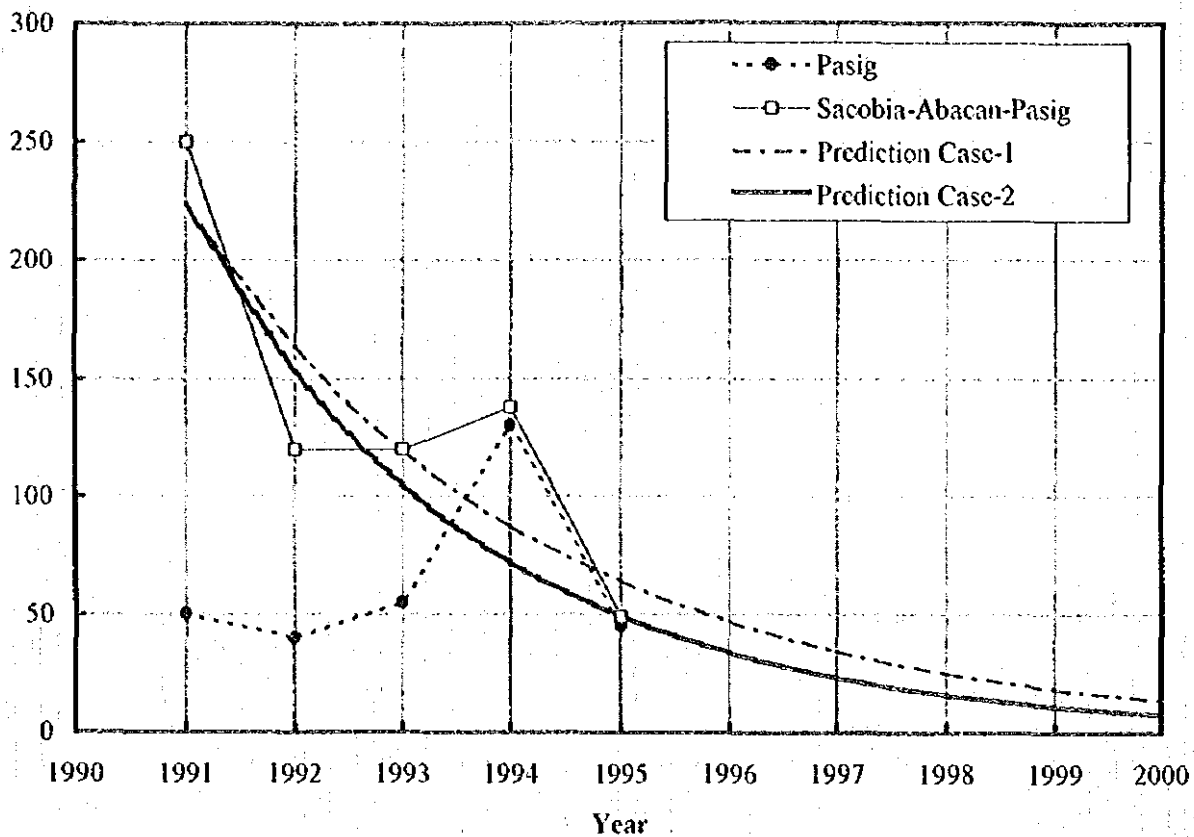


Figure 12.13
River Course Meandering and Cross-Sectional Changes
along Pasig-Potrero River in 1995

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Annual Sediment
Delivery (million m3)

Sediment Delivery Prediction



Annual Sediment Delivery

Year	Actual		Prediction	
	Pasig	Sacobia- Abacan- Pasig	Case-1	Case-2
1991	50	250	223	223
1992	40	120	163	153
1993	55	120	119	105
1994	130	138	87	72
1995	45	49	64	49
1996			47	34
1997			34	23
1998			25	16
1999			18	11
2000			13	7

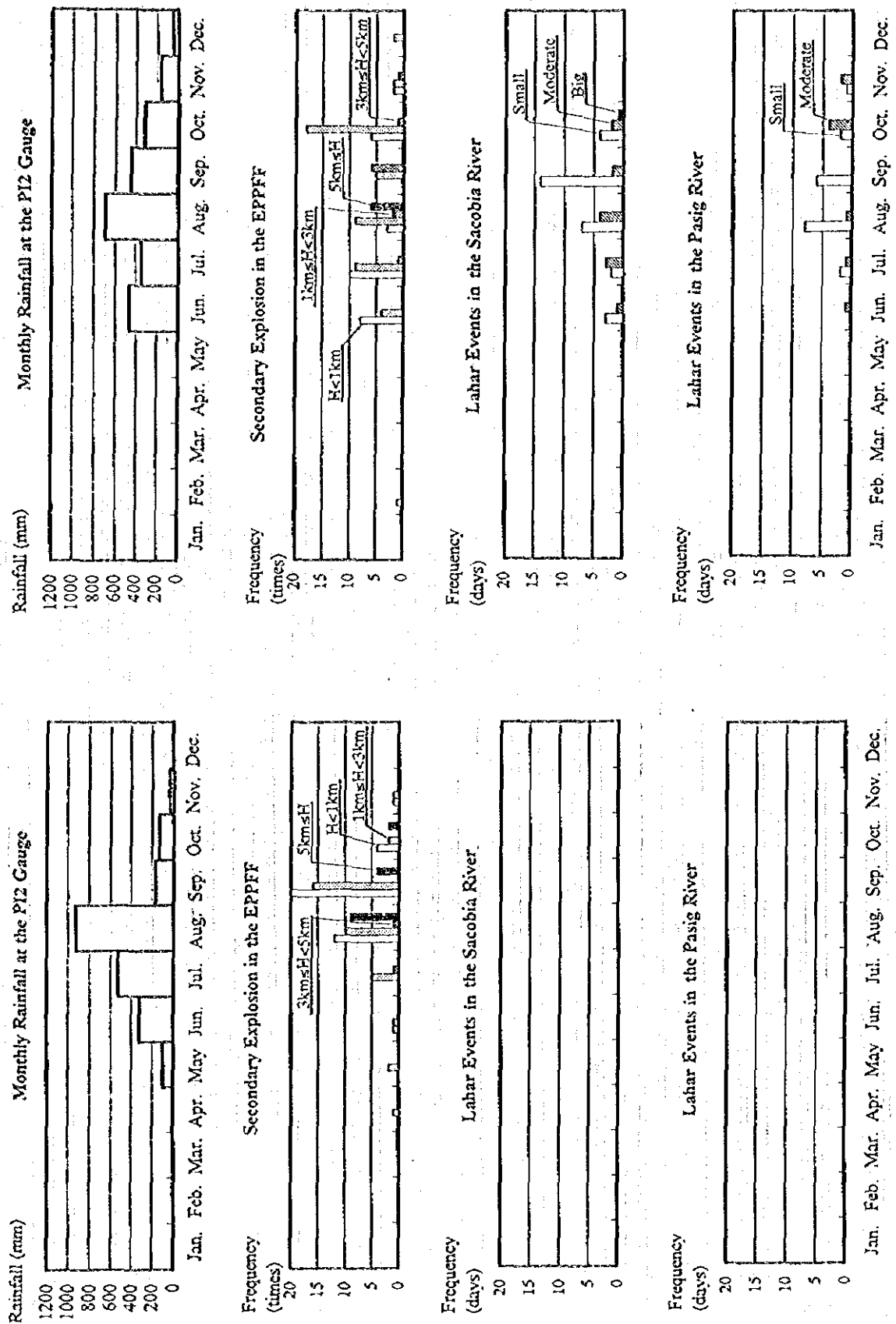
- Note: 1) Case-1 is predicted using all actual data of Sacobia-Abacan-Pasig from 1991 to 1995.
 2) Case-2 is predicted excluding the 1994 data as a extraordinary value.
 3) Regression lines are as follows;
 Case-1: $Y=304.6\text{Exp}(-0.312T)$ Correlation Coefficient = 0.846
 Case-2: $Y=325.1\text{Exp}(-0.377T)$ Correlation Coefficient = 0.966

Figure 12.14 Sediment Delivery Prediction

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Figure 12.15 (1/2)

Summary of Lahar Events, 1992-1995



Lahar Events in 1993

Lahar Events in 1992

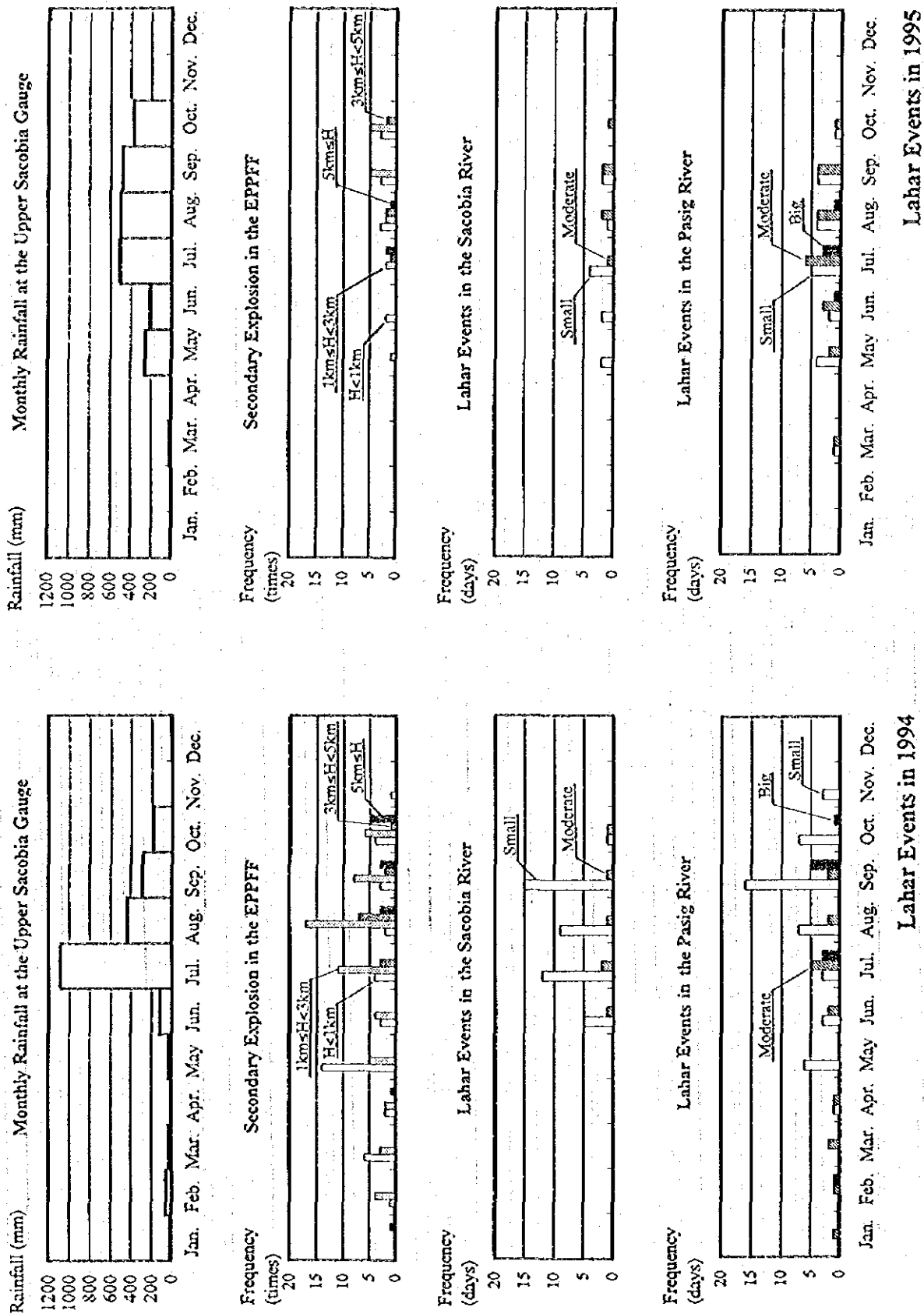


Figure 12.15 (2/2)

Summary of Lahar Events, 1992-1995

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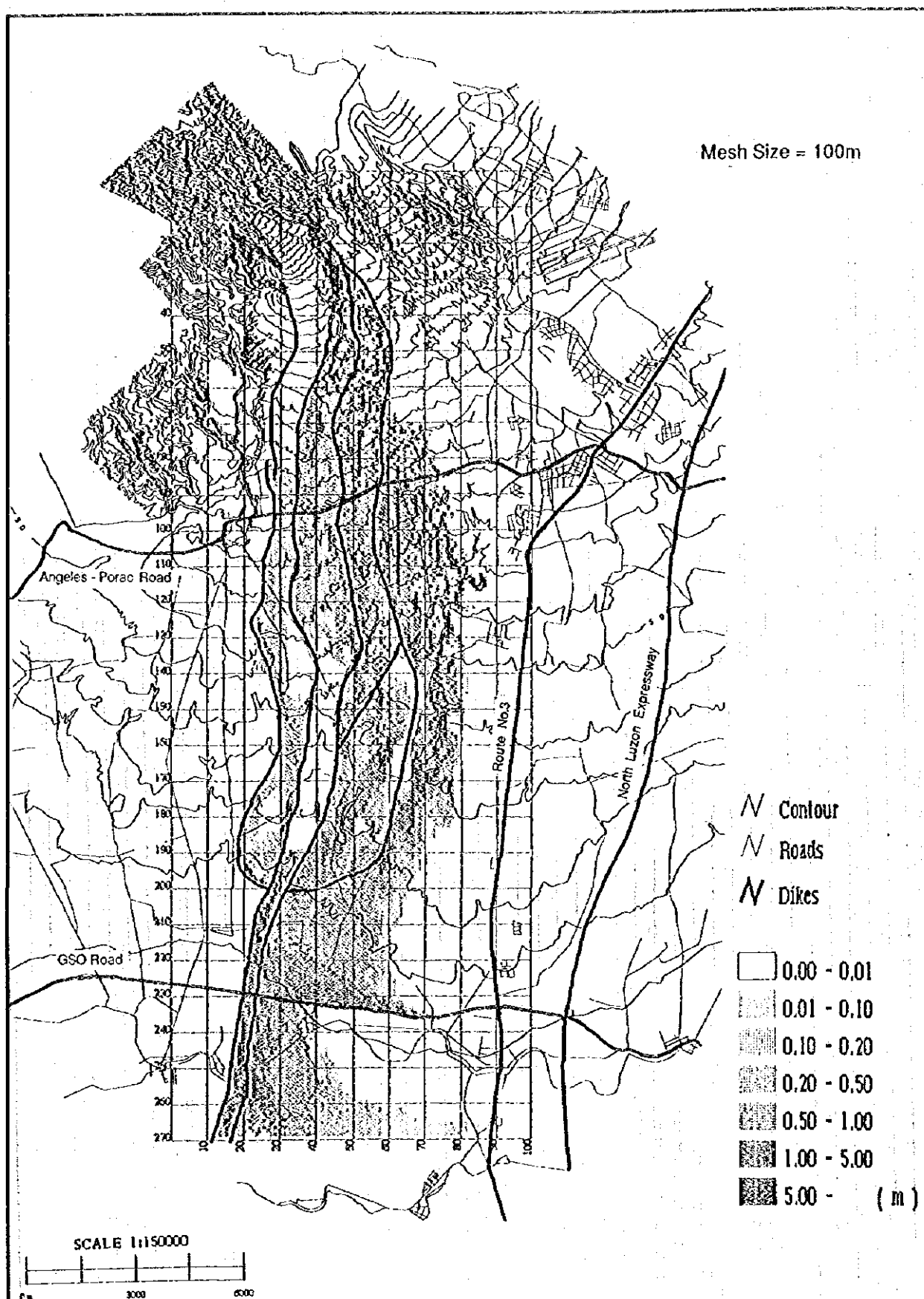
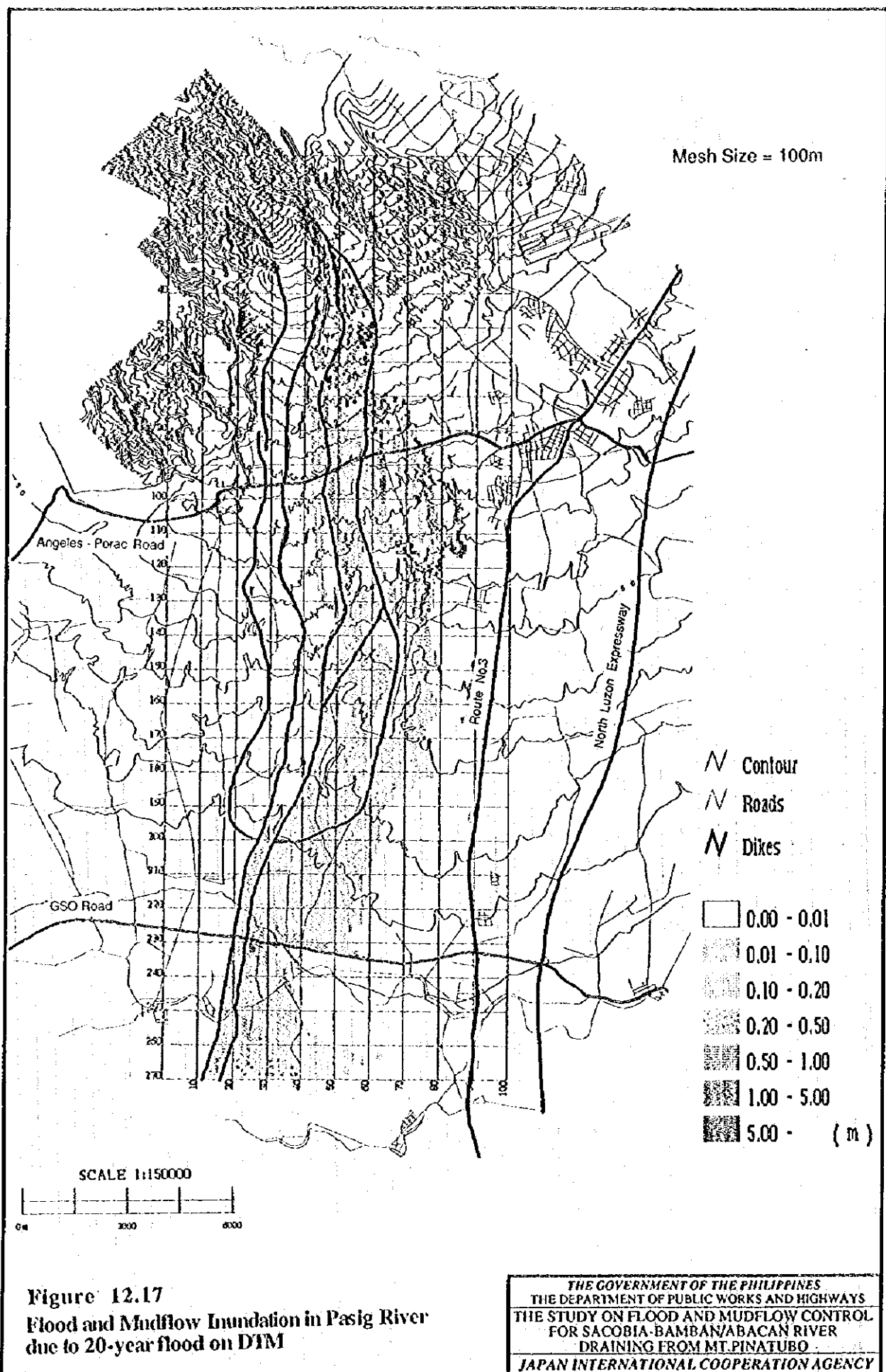


Figure 12.16
Flood and Mudflow Inundation in
Pasig River in 1995 on DTM

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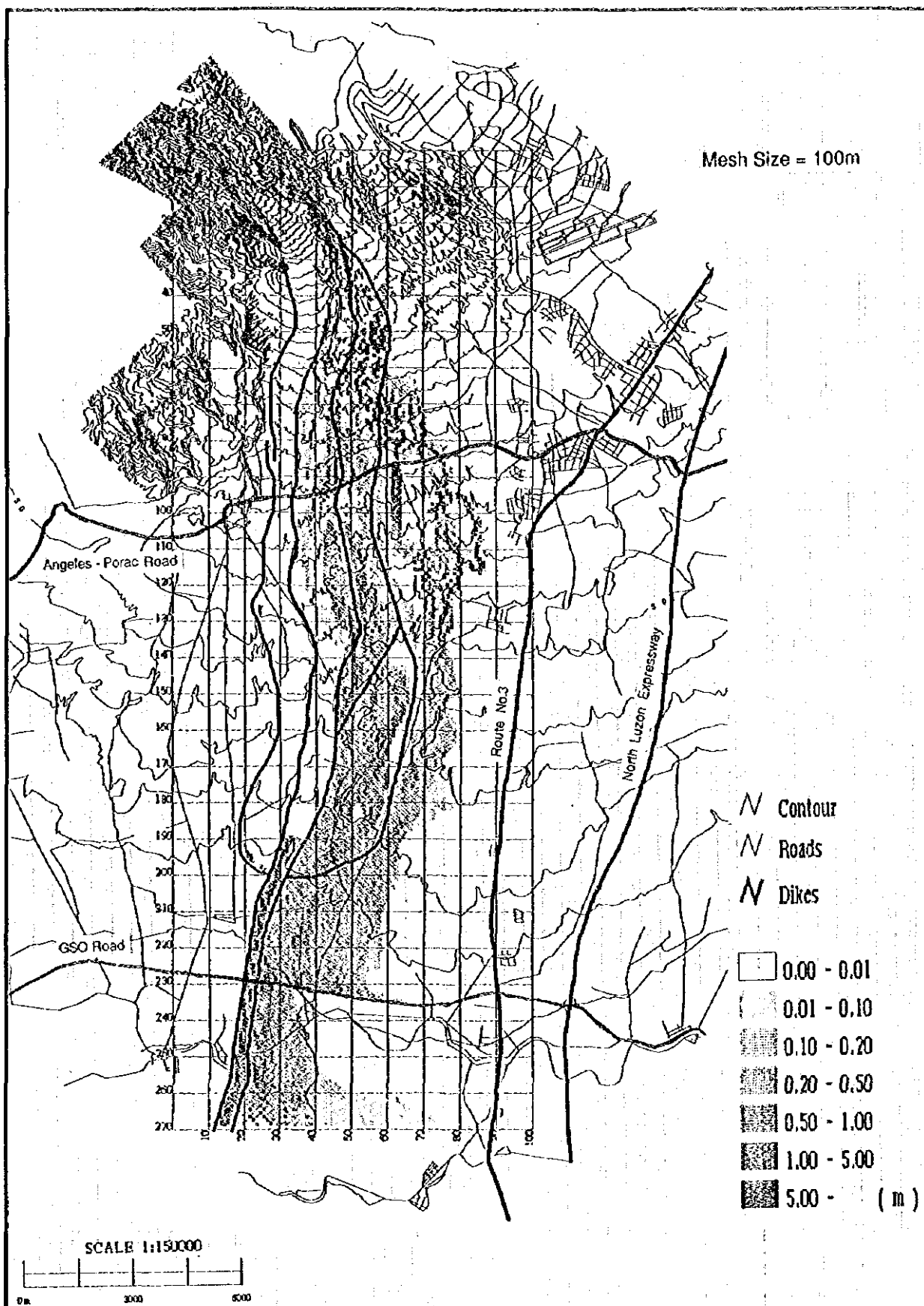


Figure 12.18

**Flood and Mudflow Inundation in Pasig River
due to 100-year flood on DIM**

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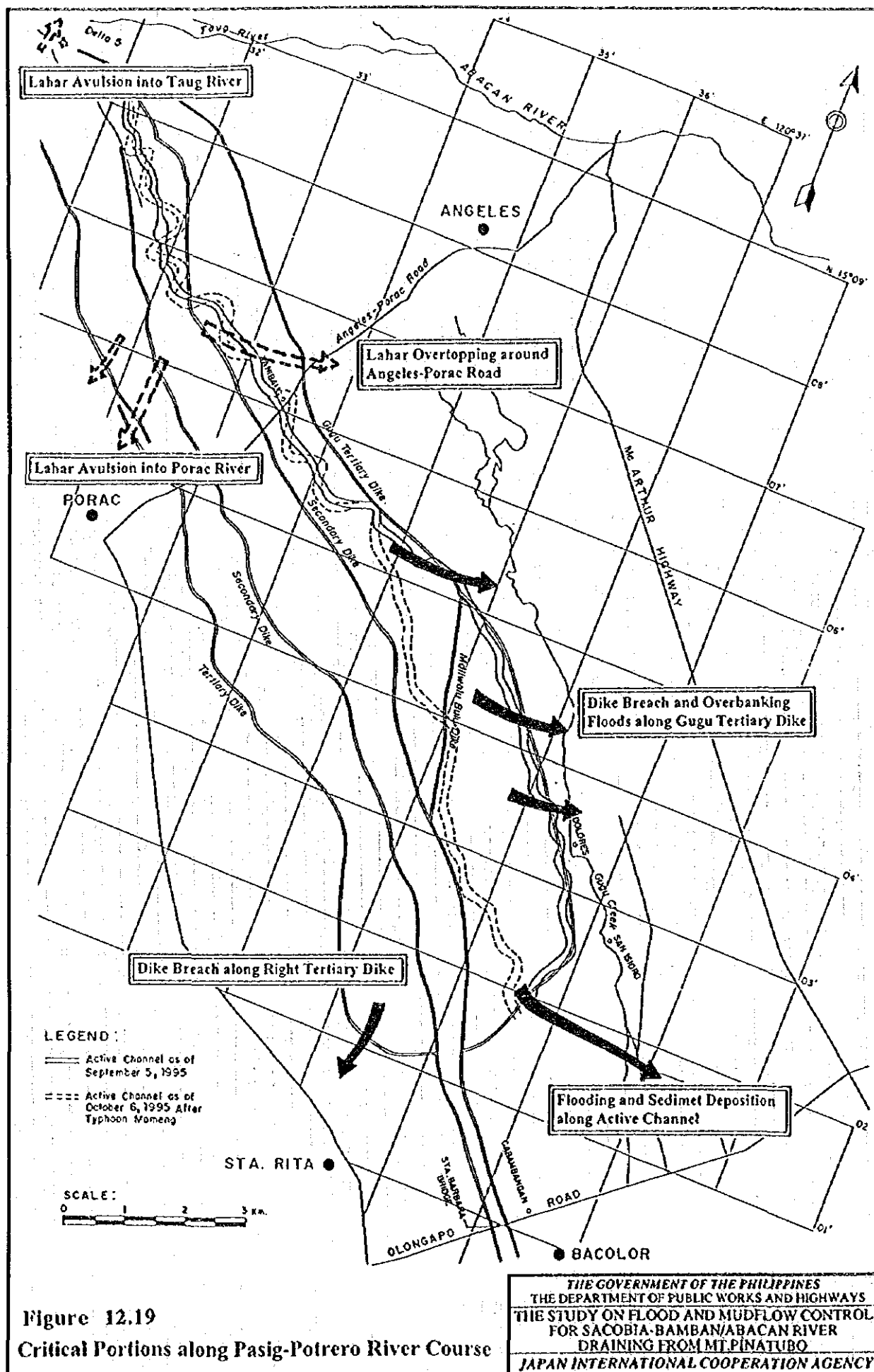


Figure 12.19
Critical Portions along Pasig-Potrero River Course

REFERENCES



REFERENCES

CHAPTER 1 SCOPE OF STUDY

- Ref.1.1 JICA, "Inception Report, the Study on Flood and Mudflow Control for Sacobia-Bamban/Abacan River draining from Mt.Pinatubo", November 1993
- Ref.1.2 JICA, "Progress Report (No.1), the Study on Flood and Mudflow Control for Sacobia-Bamban/Abacan River draining from Mt.Pinatubo", March 1994
- Ref.1.3 JICA, "Interim Report (No.1), the Study on Flood and Mudflow Control for Sacobia-Bamban/Abacan River draining from Mt.Pinatubo", June 1994
- Ref.1.4 JICA, "Progress Report (No.2), the Study on Flood and Mudflow Control for Sacobia-Bamban/Abacan River draining from Mt.Pinatubo", December 1994
- Ref.1.5 JICA, "Interim Report (No.2), the Study on Flood and Mudflow Control for Sacobia-Bamban/Abacan River draining from Mt.Pinatubo", March 1995
- Ref.1.6 JICA, "Progress Report (No.3), the Study on Flood and Mudflow Control for Sacobia-Bamban/Abacan River draining from Mt.Pinatubo", October 1995
- Ref.1.7 JICA, "Draft Final Report, the Study on Flood and Mudflow Control for Sacobia-Bamban/Abacan River draining from Mt.Pinatubo", March 1996

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