Chapter 4 Ore Reserve Calculation

4-1 Objective

The objective of the ore reserve calculation is to assess the mineral potential of the survey area.

4-2 Method

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The calculation was carried out by ZCCM using LYNX computer of Canadian LYNX GEOSYSTEM INC.

Kriging method, Inverse Distance Squared method and manual calculation on orebody sections were studied for the ore reserve calculation. In the Kriging, borehole data points may not be enough for constructing a reliable semi-variogram, while the manual calculation overestimated the tonnage and the grade in the part of low density of borehole. Consequently Inverse Distance Squared method was adopted to the ore reserve calculation of the area.

In the Inverse Distance Squared method the grade of a block is calculated that:

$$X = \sum_{i=1}^{N} (xi/di^2) / \sum_{i=1}^{N} (1/di^2)$$

X : block grade

xi: grade composite value of neighbouring sample point (intersection grade of drill hole etc.)

di: distance between centre of block and sample point

i : neighbouring sample point

N : number of samples used for the estimation

Inverse Distance Squared method was used under the following conditions.

3D GRID MODEL DIMENSIONS: 150 x 150 x 1300 (m)

SEARCH ELLIPSOID DIMENSIONS: 800 x 800 x 800 (m) CUT-OFF GRADE: 1% T-Cu

ORE DENSITY: 2.67

Assay results of gold and silver for the intersections of drill holes are listed in the appendices. These results are generally low (in the order of ppb). However, there are several relatively high grade ores in some part of the Southern Area Shoot, Northern Area Shoot and in the western part of the survey area. The matter how to treat these gold and silver assays in the calculation of ore reserves are now being discussed by ZCCM.

4-3 Results

68 boreholes were found to have intersections of 1% Cu mineralization.

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The orebody being mostly gentle slope lying, each 3D Grid cell created one orebody intersection as seen in the plan.

Figures and tables of various kinds on the results of the calculation are shown in appendices.

ZCCM has made a policy not to use the word ore unless an economic evaluation has been made, and concluded that the tonnage and grade of the results be expressed under two headings:

(A) Potentially Economic Mineralization: This will be summation of blocks which have a minimum true thickness of 3m and a minimum block grade of 2% t-Cu. The blocks should also be connected with each other making a minable body. This criterion was used to quantify the Northern Area Shoot and the Southern Area Shoot.

(B) Subeconomic mineralization: The grade and tonnage of the remaining blocks of the 1% Cut-Off mineralization.

The areas around NN-75, MJZC-9(NN-84) and RCB-2 were purposely left out from the Potentially Economic Mineralization as those are separated from the Northern Area Shoot and require further drilling to firm up the block grades and tonnages. However those areas are regarded as of considerable promise for location of economic mineralization.

The tonnages and grades of the survey area are as follows.

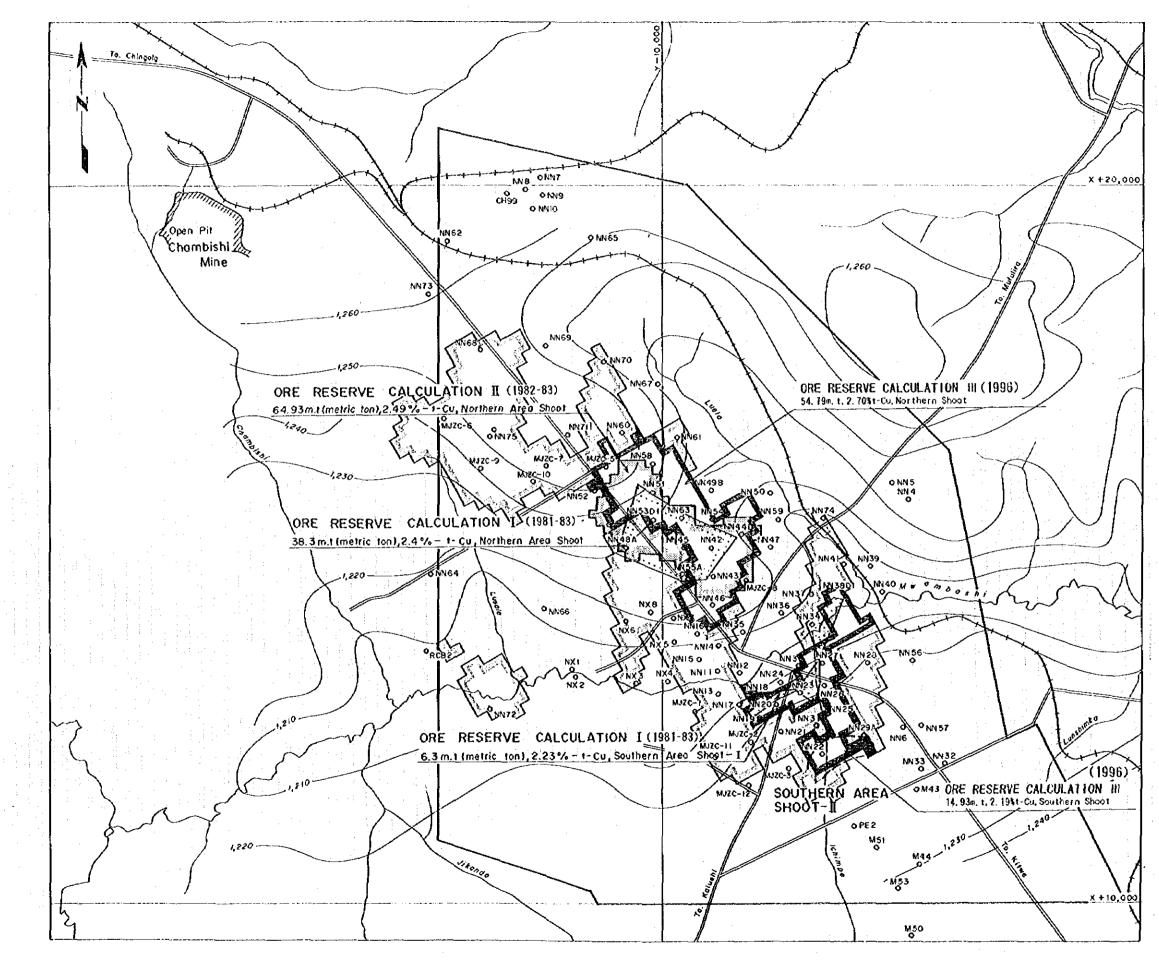
POTENTIALLY ECONOMIC MINERALIZATION;

NORTHERN AREA SHOOT: 54,793,000 tons, 2.70% T-Cu, 0.13% T-Co SOUTHERN AREA SHOOT: 14,934,000 tons, 2.19% T-Cu, 0.13% T-Co SUBECONOMIC MINERALIZATION (includes isolated patches of 2% Cu and 3m true thickness blocks): 107,909,000 tons, 1.83% T-Cu, 0.03% T-Co

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LEGEND

Dritting Holes



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Topographic Elevation Contour in Metre

Survey Area

ORE RESERVE CALCULATION III (1996)

Subeconomic Blocks, 10, 91m. t. 1. 83%t-Cu

Northern Area Shoot

	True Thickness	Total Cu¥	Total CoX
NN58	22.92	2.21	0.09
51	14.21	2.68	0.06
48-8	4.67	2.07	0.02
53-D1	4. 92	2. 15	0.05
63	18.41	2.11	0.21
45	10.39	2. 32	0.06
42	16. 27	2.29	0.10
44-D1	15.90	2.86	0. 18
55-A	3. 02	2.04	0.04
43	12.02	2.93	0.09

Southern Area Shoot-I

	True Thickness (m)	Total CuX	Total CoX
NN11	5.49	1.88	0.04
NN18	4.48	2.81	0.07
20	5.06	1.92	0.13
23	4.75	2.62	0.27
26	4.63	1.87	0. 12
27	5. 12	2.31	0.28
38-D1	3, 90	2.98	0.01
40	9.78	2.17	0.04

Southern Area Shoot-II

	True Thickness	Total CuX	Total CoX
NN22 -	5.61	2. 37	0. 13
29	9.08	1.75	0. 17

Nothwestern Area

	Truə Thiknəss (•)	Total Cu%	Total Co%
NN75	10. 72	2. 11	0.09
MJZC-9	5, 79	3, 12	0.08

Fig. 2-4-1 Ore Reserve Calculation

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Table 2-5-1 Results of Chemical Analysis of Ore Samples (1)

MJZC-1

MJZC-2

Semple	9ış tı	1-04	t-co	13-C
58591 10	9990 (1)	ŵ	8	a l
LC14323	499.53 ~ 500.03	<0.01	<0.01	(Q.Q1
LC14324	500.03 ~ 500.53	(0.01	<0.01	<0.01
LC14325	500.53 ~ 501.03	<0.01	<0.01	<u><0 01</u>
LC14326	501.03 ~ 501.53	<u><0.01</u>	<u><0.01</u>	<u>(0.01</u>
LC14327	501.53 ~ 502.03	(0.01	(0.0)	(0.01
LC14328 LC14329	<u>502.03</u> ~ 502.53 502.53 ~ 502.90	<u><0.01</u> <0.01	<u><0.01</u> <0.01	<u><0.01</u> <0.01
LC14330	502.90 ~ 503.40	<0.01	<0.01	<0.01
LC14331	503 40 ~ 503 90	<0 01	(0.01	<0 01
LC14332	503 90 ~ 504 40	<0.01	<0 01	<0 01
LC14333	504 40 ~ 504 90	<0.01	<0.01	<0.01
LC14334	504.90 ~ 505.53	<0.01	<0.01	<0.01
LC14335	505.53 ~ 506.03	<0.01	0.02	<0.01
LC14336	505.03 ~ 505.53	<0.01	0.02	<0.01
LC14337	505.53 ~ 507.03	(0.01	0.03	<0.01
LC14338	507.03 ~ 507.53	<0.01	0.06	<0.01
LC14339 LC14340	507.53 ~ 508.03 508.03 ~ 508.20	0.02	0.02	<0.01 <0.01
LC14340	508.20 ~ 508.70	(0.01	0.05	<0.01
LC14342	508.70 ~ 509.20	<0.01	0.03	(0 01
LC14343	509.20 ~ 509.70	<0.01	0.03	<0.01
LC14344	509.70 ~ 510.20	0.01	0.03	<0.01
LC14345	510.20 ~ 510.70	<0.01	0.03	<0.01
LC14346	510.70 ~ 511.20	0.02	0.04	(0 01
LC14347	<u>511.20 ~ 511.53</u>	0.02	0.04	<0.01
LC14348	511.53 ~ 512.03	0.07	0.05	<0.01
LC14349 LC14350	512.03 ~ 512.53 512.53 ~ 513.03	0.05	0.02	<0.01 <0.01
LC14350	$512 \ 53 \ \sim \ 513 \ 03$ $513 \ 03 \ \sim \ 513 \ 53$	0.32	0.02	<0.01
LC14352	513.53 ~ 514.03	0.11	<0.01	<0.01
LC14353	514 03 ~ 514 53	0 11	(0.01	<0.01
LC14354	514 53 ~ 515 03	0.13	0.01	<0.01
LC14355	515.03 ~ 515.28	0 07	<0.01	<0.01
LC14356	<u>515.26 ~ 515.76</u>	0.25	0.02	(0.01
LC14357	515.76 ~ 516.26	0 10	0.01	<0.01
LC14358	516.26 ~ 516.76	0 19	0.01	<0.01 (0.01
LC14359 LC14360	$\frac{516.76}{516.99} \sim \frac{516.99}{517.53}$	0.21	0.02	<u><0.01</u> <0.01
LC14361	517.53 ~ 518.03	0 19	0.02	<0 01
LC14362	518.03 ~ 518.53	0.12	0.05	<0.01
LC14363	518.53 ~ 519.03	0.31	0.06	<0.01
LC14364	519.03 ~ 519.53	0.23	0.11	<0.01
1014365	519.53 ~ 520.03	0.07	0.07	(0.01
LC14366	<u>520.03 ~ 520.53</u>	0.05	0.04	<u><0.01</u>
LC14367	520.53 ~ 520.93	0.02	0.02	<u><0.01</u> <0.01
LC14368 LC14369	<u>520.93 ~ 521.18</u> 521.18 ~ 521.68	0.02	0.04	<u><0.01</u>
LC14309	521.68 ~ 522.18	0.43	0.01	<0.01
LC14371	522.18 ~ 522.68	0.59	0.01	<0.01
LC14372	522.68 ~ 523.18	0.61	(0.01	<0.01
LC14373	523.18 ~ 523.53	0.41	<0.01	<0.01
LC14374	523.53 ~ 524.03	0.88	<0.01	<0.01
LC14375	<u>524.03 ~ 524.23</u>	0.72	<u><0.01</u>	<u><0.01</u>
LC14376	524 23 ~ 524 53	0.59	0.01	<0.01
LC14377	524.53 ~ 525.03	0.55	0.02	(0.01
LC14378 LC14379	<u>525 03 ~ 525 53</u> 525 53 ~ 526 03	0.40	<0.01 <0.01	<u><0 01</u> <0 01
LC14380	526.03 ~ 526.53	0 24	<0.01	(0.01
LC14381	526.53 ~ 527.03	0 24	(0 01	<0.01
LC14382	527.03 ~ 527.53	0 31	0.01	<0.01
LC14383	527.53 ~ 528.03	0 23	0 01	<0.01
LC14384	528.03 ~ 528.53	0.06	(0.01	<0.01
LC14385	528.53 ~ 529.03	0.09	<0.01	<0.01
LC14386	529 03 ~ 529 53	0 03	<u><0.01</u>	<0.01
LC14387	529.53 ~ 530.03	0.09	<0.01	<u>(0 01</u>
LC14388 LC14389	530.03 ~ 530.53 530.53 ~ 530.83	0.07	<0.01 <0.01	<0 01 <0 01
2014003		1 9.92		
riden	Depth	1-Cu	AS-CU	I-Co
		1		
(0)	(0)	0 62	<u> </u>	02

	Scapla	Depth	I-Cu	Aš-Cu	1-Co	As-Co	XI	2
	No.		a	(1)	(1)	(1)	ppe	000
	KC15160	638.29 ~ 638.62	<0.01	<0.01	0.01	<0.01	50	21
11	KC15161	638.62 ~ 639.12	(0.01	(0.01	0.02	<0.01	42	17
.	KC15152	639.12 ~ 639.62	<0.01	<0.01	0.09	(0.01	44	8
1	KC15163	639.62 ~ 640.12	(0.01	<0.01	0.04	(0.01	48	18
	KC15164	640.12 ~ 640.62	(0.01		0.03	<0.01	47	3
. [KC15165	640.62 ~ 641.12	<0.01	(0.01	0.02	<0.01	59	12
÷	KC15156	641.12 ~ 641.62	(0.01	<0.01	0.03	(0.01	52	11
	KC15167	641.62 ~ 642.12	0.01	(0.01	0.03	(0.01	44	5
	KC15168	642.12 ~ 642.62	<0.01	<0.01	0.02	(0.01	45	9
	KC15169	642.62 ~ 643.12	<0.01		0.03	(0.01	48	10
.	KC15170	643. 12 ~ 643. 62	(0 01	(0.01	0 02	(0.01	42	10
	KC15171	643.62 ~ 644.12	(0.01	(0 01	0.02	(0.01	n	13
Ì	KC15172	644 12 ~ 644 62	(0.01	(0.01	0.04	<0.01	45	12
	KC15173	644.62 ~ 645.12	(0.01	(0 01	0.03	(0.01	45	12
	XC15174	645.12 ~ 645.62	(0.01	(0.01	0.04	<0.01	45	13
	KC15175	645. 62 ~ 646. 12	0.05	(0.01	0.06	(0.0)	39	ī
	KC15176	645.12 ~ 646.62	0.02	(0.01	0.05	<0.01	48	8
	KC15177	645 62 ~ 647.12	0.05	(0.01	0.06	(0.01	41	9
	KC15178	647.12 ~ 647.62	0.07	(0.01	0.05	<0.01	39	10
	KC15179	647.62 ~ 648.12	0.29	<0.01	0.02	(0.01	42	10
	KC15180	648.12 ~ 648.62	0.47	<0.01	0.05	(0.01	41	18
	KC15181	648.62 ~ 649.12	0.14	<0.01	0.01	(0.01	32	18
	KC15182	649. 12 ~ 649. 62	0.46	<0.01	0.02	<u><0.01</u>	43	33
÷	KC15183	649. 62 ~ 650. 07	0.49	(0.01	0.03	(0.0)	47	27
	KC15184	650 07 ~ 650 57	0.28	(0.01	0.02	(0.01	38	22
1	KC15185	650.57 ~ 651.07	0.36	<0.01		(0.01	38	23
· ·	KC15186	651.07 ~ 651.57	0.64	0.01	0.02	<0.01	37	31
	KC15187	\$51.57 ~ 652.07	0.66	<0.01	0.03	(0.01	38	97
	KC15188	652.07 ~ 652.66	0.58	<0.01	0.05	<0.01	52	115
÷	KC15189	652.65 ~ 652.83	1.62	<0.01	0 07	(0.01	45	139
÷	KC15190	652.83 ~ 653.33	0.83	(0.01	0.05	<0.01	45	139
	KC15191	653.33 ~ 653.83	0.49	<0.01	0.02	(0.01	28	115
	KC15192	653.83 ~ 654.33	6,85	0.02	0 12	(0.01	70	335
	KC15193	654.33 ~ 654.83	0.73	<0.01	0.04	<0.01	37	45
1	KC15194	654.83 ~ 655.33	1.02	(0 01	0.05	(0.01	33	56
	KC15195	655 33 ~ 655 83	3 13	<0 01	0 21	(0.01	40	149
	KC15196	655.83 ~ 655.97	1.00	(0 01	0.09	(0.01	37	51
1	KC15197	555.97 ~ 656.41	0.83	<0 01	0 10	<0.01	35	55
1	KC15198	656.47 ~ 656.97	1.03	<0.01	0.21	<0.01	60	51
	XC15199	656 97 ~ 657.25	0.77	<0.01	0.09	<0.01	33	39
	KC15200	657.25 ~ 657.75	9.37	<0.01	0.03	<0.01	32	30
-	KC19784	657.75 ~ 658.25	0.07	<0.01	0.04	<0.01	22	24
	KC19785	658.25 ~ 658.43	0.46	(0.01	0.03	<0.01	29	28
	KC19786	658.43 ~ 658.51	0.21	<0.01	0.12	<0.01	30	21
×.	KC19787	658.51 ~ 659.01	<0.01	<0.01	<0.01	<0.01	21	12
	KC19788	659.01 ~ 659.51	<0.01	<0.01	<0.01	<0.01	28	13
1	KC19789	659.51 ~ 660.01		<0.01				13
	KC19790	660 01 ~ 650 51		<0.01				11
	KC19791	660.51 ~ 661.01		<0.01				22
	KC19792	661.01 ~ 661.51		(0.01			30	20
	KC19793	661.51 ~ 661.97	<0.01	<0.01	<0.01	<0.01	18	18
1	Sidth	Depth	1-0+	As-Cu	I-Co	1		
		4-3						

	Depth	1-00			
()	(a) (a)	(1)	$\langle \mathbf{a} \rangle$	(1)	
3.14	653 83 ~ 656 97	2.21	<0.01	0.12	ł

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Table 2-5-1 Results of Chemical Analysis of Ore Samples (2)

MJZC-3

MJZC-4

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:	Seaple	Dapth	T-Cu	AS-Cu	T-Co	AS-Co		Sample	Depth	1-04	ÁS-Ču	1-Co	A3-Co
Ĺ	No.	(3)	(1)	(1) 1745 A. S.	(1)	(1)		No.	(1)	(1)	(1)	(1)	(1)
· [KC19701	632 47 ~ 632 66	<0.01	<0.01	<0.01	<0.01	1	KC15105	913.94 ~ 914.44	<0.01	<0.01	<0.01	(0.01
	KC19702	632 65 ~ 633 13	<0.01	<0.01	<0.01	<0.01		KC15106	914,44 ~ 914,94	<0.01	<0.01	<0.01	<0.01
[KC19703	633 13 ~ 633 63	<0.01	<0.01	<0.01	<0.01		KC15107	914.94 ~ 915.44	<0.01	<0.01	<0.01	<0.01
	KC19704	633 63 ~ 634 13	<0.01	<0.01	<0 01	<0.01		KC15108	915 44 ~ 915 94	<0.01	<0.01	<0.01	<0.01
	KC19705	634 13 ~ 634.63	<0.01	<0.01	<0.01	(0.01		KC15109	915 94 ~ 916 44	<0.01	<0.01	<0 01	<0.01
	KC19705	634.63 ~ 634.84	<0.01	<0.01	<0.01	<0.01		KC15110	916 44 ~ 916 94	<0.01	(0.01	<0.01	<0.01
	KC19707	634.84 ~ 635.03	<0.01	<0.01	<0.01	<0.01		KC15111	916 94 ~ 917.44	<0.01	<0.01	<0.01	<0.01
	KC19708	635.03 ~ 635.32	<0.01	<0.01	0.02	<0.01		KC15112	917.44 ~ 917.94	<0.01	<0.01	<0.01	<0.01
	KC19709	635.32 ~ 635.61	(0.01	<0.01	0.02	<0.01		KC15113	917.94 ~ 918.44	<0.01	(0.01	<0.01	<0.01
	KC19710	635 61 ~ 635.94	(0.01	<0.01	0.03	<0.01	1	KC15114	918 44 ~ 918 94	<0.01	<0.01	<0.01	<0.01
	KC19711	635.94 ~ 636.31	0.80	<0.01	0.02	<0.01		KC15115	918 94 ~ 919 44	(0.01	<0.01	<0.01	<0.01
	XC19712	635.31 ~ 636.81	1.16	<0.01	(0.01	<0.01		KC15116	\$19.44 ~ \$19.94	(0.01	<0.01	<0.01	<0.01
	KC19713	635.81 ~ 637.31	0.34	<0.01	0.02	<0.01	V.	KC15117	919.94 ~ 920.44	<0.01	<0.01	0.01	<0.01
	KC19714	637 31 ~ 637.81	0.05	<0.01	0.01	<0.01		KC15118	920.44 ~ 920.94	<0.01	<0.01	<0.01	<0.01
ł	KC19715	637.81 ~ 638.31	0.06	<0.01	0.01	<0.01		KG15119	920.94 ~ 921.44	(0.01	<0.01	<0.01	(0.0)
	KC19716	638.31 ~ 638.81	0.02	<0.01	0.01	<0.01		KC15120	921 44 ~ 921 94	<0.01	(0.01	<0.01	(0.01
	KC19717	638.81 ~ 639.31	<0.01	<0.01	<0.01	<0 01		K¢15121	921 94 ~ 922 44	<0.01	<0.01	<0.01	<0.01
	KC19718	639.31 ~ 639.81	0.01	<0.01	<0.01	<0.01		KC15122	922.44 ~ 922.94	<0.01	(0.01	<0.01	<0.01
	KC19719	639.81 ~ 640.31	0.02	<0.01	0.01	<0.01		KC15123	922.94 ~ 923.44	<0.01	<0.01	<0.01	<0.01
	KC19720	640.31 ~ 640.66	<0.01	<0.01	0.01	(0.01		KC15124	923.44 ~ 923.94	<0.01	<0.01	<0.01	<0.01
	KC19721	640 66 ~ 640 84	0.02	<0.01	0.02	<0.01		KC15125	923 94 ~ 924 44	(0.01	<0.01	<0.01	<0.01
. 1	KC19722	ببعجيب وتعياب ربيك بينك	0.02	(0.01	0.03	<0.01		KC15126	924 44 ~ 924 94	1 <0.01	(0.01	<0.01	<0.01
	KC19723	641.34 ~ 641.84	0.03	<0.01	0.03	<0.01		KC15127	924 94 ~ 925 19	<0.01	<0.01	<0.01	<0.01
ł	KC19724	641.84 ~ 642.26	0.06	<0.01	0.03	(0.01		KC15128	925.19 ~ 925.69	<0.01	<0.01	<0.01	<0.01
	KC19725	642 26 ~ 642 79	0.30	<0.01	0.03	<0.01		KC15129	925.69 ~ 926.19	(0.01	<0.01	<0.01	<0.01
	KC19726	642.79 ~ 643.29	0.01	<0.01	0.03	<0.01		KC15130	926 19 ~ 926 69	<0.01	<0.01	<0.01	<0.01
ľ	KC19727	643.29 ~ 643.8	0.01	<0.01	0.03	<0.01		XC15131	926 69 ~ 927.19	(0.01	<0.01	<0.01	<0.01
ľ	KC19728	643 80 ~ 644 31	0.11	<0.01	0.08	<0.01		KC15132	927. 19 ~ 927. 69	(0.01	<0.01	<0.01	(0.01
	KC19729	644 31 ~ 644 74	0.80	0.01	0.09	<0.01		KC15133	927.69 ~ 928.19	(0.01	<0.01	<0.01	(0.01
	KC19730	644 74 ~ 645 24	1 09	0.01	0.06	(0.01		KC15134	928 19 ~ 928 69	0.02	<0.01	<0.01	<0.01
	KC19731	645 24 ~ 645 72	0.22	(0 01	0.05	<0.01	:	XC15135	928.69 ~ 929.19	(0.01	(0.0)	<0.01	<0.01
	KC19732	645. 72 ~ 645. 23	0.42	<0.01	0.05	<0.01		KC15136	929.19 ~ 929.69	0.02	<0.01	<0.01	(0.01
	KC19733	646.23 ~ 646.73	0.78	(0.01	0.04	<0.01		KC15137	929.69 ~ 930.14	0.03	<0.01	<0.01	<0.01
:	KC19734	646.73 ~ 647.23	0.55	<0.01	0.07	<0.01	-	KC15138	930.14 ~ 930.64	0.07	(0.01	<0.01	<0.01
·	KC19735	647 23 ~ 647.73	0.45	<0.01	0.05	<0.01		KC15139	930 64 ~ 931.14	0.21	(0.01	0.02	<0.01
	XC19735	647. 73 ~ 648. 23	2.51	0.04	0 27	(0.01		KC15140	931.14 ~ 931.64	0.45	<0.01	<0.01	(0.01
Ì	XC19737	648.23 ~ 648.73	1.38	0.01	0 12	<0.01		X¢15141	931.64 ~ 932.14	0.13	<0.01	<0.01	<0.01
:	KC19738	648.73 ~ 649.23	0.92	(0.01	0.20	<0.01		XC15142	932.14 ~ 932.64	0.12	<0.01	<0.01	<0.01
<u>.</u>	KC19739	649.23 ~ 649.73	1.32	0.01	0.11	<0.01		KC15143	932.64 ~ 933.14	0.12	<0.01	<0.01	<0.01
	KC19740	649. 73 ~ 649. 84	1.62	0.02	0.31	<0.01		KC15144	933. 14 ~ 933. 64	0.06	<0.01	<0.01	<0.01
	KC19741	649.84 ~ 650.13	0.02	0.01	0 23	<0.01		KC15145		0.11	<0.01	<0.01	<0.01
·	KG19742	650 13 ~ 650 42	<0.01	<0.01	0.01	<0.01		KC15145	934 14 ~ 934 64	0.12	<0.01	<0.01	<0.01
	KC19743	650. 42 ~ 650. 71	(0.01	(0.01	0.02	<0.01		K015147		0.04	<0.01	<0.01	<0.01
	KC19744	650.71 ~ 651.19	<0.01	(0.0)	<0.01	<0.01		KC15148	934.94 ~ 935.44	0.12	<0.01	<0.01	<0.01
1	XC19745		0.03	<0.01	<0.01	<0.01		KC15149	935.44 ~ 935.99	0.50	<0.01	<0.01	<0.01
	XC19746	651.67 ~ 652.15	<0.01	<0.01	<0.01	<0.01		KC15150	935.99 ~ 938.49	0.13	<0.01	0.02	<0.01
	KC19747	• • ^	<0.01	(0 01	<0.01	<0.01	1	KC15151	936 49 ~ 936 99	0.15	<0.01	0 01	< 0.01
1	KC19748		<0.01	(0.01	<0.01	<0.01		KC15152	935 99 ~ 937.49	0.41	<0.01	0 02	<0.01
l			**************************************	ba mare	*****	<u>.</u>	•	KC15153	937.49 ~ 937.99	0.15	<0.01	0.05	<0.01
. 1	Width	Depth	T-C.	AS-CU	T-C0			KC15154	937.89 ~ 938.49	0.02	<0.01	0.02	<0.01
	(1)	(•)	ao	(1)	ω			KC15155		0.01	<0.01	0.02	<0.01
	2 11	COLOR DO NO. OF COLOR DO NO.		<0.02	0.00	l		KC15156	938 99 ~ 939 49	0.02	<0.01	0 02	<0.01
L				*		•		KC15157	939 49 ~ 939 99	<0.01	<0.01	0.01	<0.01
								KC15158	939 99 ~ 940.49	<0.01	(0.01	0.01	<0.01
							1	KC15159	940.49 ~ 940.94	(0.01	(0.01	0.01	(0.01
							1						

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Table 2-5-1 Results of Chemical Analysis of Ore Samples (3)

MJZC-7

Samp1e	Gepth	1 T-Ca	A3-C0	1-Co
<u>()</u>	(0)	(1)		<u>(1)</u>
LC14390	992.91 ~ 963.41	0.02	0.02	(0.0)
LC14391	963.41 ~ 953.91 963.91 ~ 964.41	(0.01 (0.01	<0.01 <0.01	<0.01 <0.01
1014393	964.41 ~ 964.91	0.01	40.01	<0.01
104391	964.01 ~ 965.41	40.01	0.01	<0.01
LC14395	965.41 ~ 965.91 965.91 ~ 968.41	(0.0) (0.01	<0.01 <0.01	<0.01 <0.01
LC14397	968.41 ~ 968 11	-(0.01	<0.01	<0.01
1611398	966.91 ~ 967.21	(0.01	<0.0t	<0.01
LC11100	967.21 ~ 967.77 967.77 ~ 968.15	(0.01 (0.01	- <u>(0.01</u> - (0.01	<0.01 <0.01
LC19001	968.15 ~ 968.65	(0.01	(0.01	<0.01
LC18002	968.65 ~ 969.15	<0.01	<0.01	0.01
LC18003	969.15 ~ 969.65 969.65 ~ 979.15	10.0>	<9.01 <9.01	<u><0_01</u> <u><0_01</u>
1018005	970.15 - 970.85	(0.01	(0.01	<0.01
LC18006	970.65 ~ 971.15	<0.01	<0.01	<0.01
LC18002	971.15 ~ 971.65 971.65 ~ 972.15	0.02	<0.01 <0.01	<0.01 . <0.01
1018009	972.15 ~ 972.65	0.14	(0.Q)	<0.0F
10:0010	. 873.05 (77 873.15	<u></u>	20.01	1 0 01
LC18011	973.15 ~ 974.15 974.15 ~ 974.69	0.71	<0.01 <0.01	0.03
LCIBOIS	974.80 ~ 975.23	0.07	(0,01	9.02
1016014	975.23 ~ 975.11	0.02	<0.01	0.02
LC19015	975.77 ~ 976.31 976.31 ~ 976.85	0.12	<0.01 <0.01	0.01
LC19017	976.85 ~ 977.39	0.06	(0 .01	0.02
LC13018	977,39 ~ 977.93	0.21	(0.01	0.01
LC18019 LC18020	977.93 ~ 979.47 978.47 ~ 979.01	0.07	<0.0(<0.01	0.02
1016021	979.01 ~ 979.55	0.04	<0.01	0.04
1019022 -	979.66 ~ \$80.09	2.28	2 0.92	0.03
LC18023	995.09 ~ 990.15 7990.15 ~ 980.65	0.37	<0.01 (1.25)	0.10
LC18025	990,85 ,~ 991.15	1.62	0.01	1 0 03
LC13028 2	981.15 \$91.65	2,39	# 0.02	0.04
1618020	2 901,65 ~ 992.15 (892.15 ~ 962.65	2.51	0.02	0.03
LC18020	962.65 ~ 983.15	0.67	<0.01	6.03
LC18030	983.65 ~ 984.15	0.12	0.61	6.03
1013032	984.15 ~ 994.65	0.02	<0.01	0.03
1019033	964.65 ~ 985.15	0.03	<0.01	0.03
LE 18034	965.15 ~ 985.21 1655.31 ~ 635.84	0.65	<0.01 7 9.01	0.03 0.04
1019030	G 895,84 × 958.87	1.22	0.01	0.02
2 LC18937	1 8:35.31 ~ 835.50	1,84 5	0.01	0,92
1018036	985.90 ~ 987.42 597.43 ~ 907.96	0.73	<u>- 0.01</u> - 20.01	0.01
1018040	687.95 ~ 688.43	0.30	10.01	<0.01
101804)	\$98.49 ~ 988.02	0.14	(Q.QE	0.01
LC18042	969.02 ~ 989.55 929.55 ~ 990.08	0.09	<0.01 <0.01	<0.01 0.01
EC19044	950.58 ~ 990.81	{ 0.10	(D, C)	<0.03
1018045 1018045	990.81 ~ 991.14 991.14 ~ 991.31	0.08	(0,0) (0,0)	<0.01 <0.01
LC18047	991.31 ~ 991.81	0.09	<0.01	(0.01
LC19C49	991.81 ~ 992.31	0.64	<0.01	<0.01
LC18049 \ LC18050	992.31 ~ 992.81 992.81 ~ 993.31	0.07	<0.01	<0.01
1018051	993.21 ~ 993.81	0.06	(0.6)	0.01
1018052	193.61 ~ 196.21	0.05	(0.0)	<0.01
LC19053	994.31 ~ 994.81 994.81 ~ 995.31	0.06	<u><0.01</u> <9.01	< <u>0.01</u> <0.01
LC19065	995.31 ~ 995.81	0.06	<9.01	0.01
LC18058	995.81 ~ 998.31 996.31 ~ 995.81	0.04	<0.01 <0.01	<0.91
LC18057 LC18058	995.81 ~ 997.31	0.06	(0.01	<0.01 <0.01
LE18059	997.31 ~ 997.91	0.05	(0.01	<0.01 <0.01
LC18660	997.61 ~ 998.31 998.31 ~ 998.81	0.03	<0.01 <0.01	0.01
LC18062	998.81 ~ 999.17	0.09	(0.01	<0.01
LC18063	999.17 ~ 999.47	11.0	<0.01	0.01
LC18064	999.47 ~ 999.97 939.97 ~ 1000.47	0.23 0.56	<0.01 <0.01	0.01 <0.01
1018066	1000.47 ~ 1000.82	0.90	(0.01	<0.01
LC18/27	1000.82 ~ 1001.12	0.90	0.01	0.02
1019068	1001.12 ~ 1001.47	2.19	<0.01	0.02
LC19070 ?	1001, 97 1 - 1002.47	1.99	(40.01 -	0.01 -
1010071	1002,47 ; ~ 1003.48	. 2.66	7 (0.01) (0.01	0.061
1010072	1003.45 ~ 1003.95 1003.96 ~ 1004.23	0.42	(0.01	0.02
1010074	1004.22 . 1004.73	2.00	0,81	0,14
LC18075	1004.73 ~ 1005.03	0.42	<0.01 <0.01	0.32
LC18078 LC18077	1005.03 ~ 1005.13 1005.13 ~ 1005.68	0.06	(0.01	0.02
LC18078	1005.68 .~ . 1006.23	0.06	(9.01	<0.01
LC18079	1006.23 ~ 1006.78 1006.78 ~ 1007.33	10.98	(0.01 (0.01	<u></u>
LC18080 LC18081	1007.33 ~ 1007.68	0.06	<0.01	<0.01 <0.01
(019082	1007.68 ~ 1008.43	0.07	<0.01	<0.0L
LC18083	1008.43 ~ 1008.95 1008.98 ~ 1009.13	0.13	<0.01 <0.01	10.0> 10.0>
LC18084	1009.98 ~ 1009.13			
Tidth	Depth	T Cu		T-Co
(0)	(*) \$79.55 ~ 582.65	(8)	(3)	(1)
3 18	979.55 ~ \$27.43	1.13	0.01	0.
		2 C 1 C 1 C 1 C 1 C 1 C 1 C 1 C 1 C 1 C		C
2 64	1000.62 ~ 1003.45 1000.62 ~ 1004.73	2.32 1.63	<0.01 <0.01	0.0 0.0

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*0- E(15919) E(15919) E(15919) E(15919) E(15921) E(15922) E	$\begin{array}{c c c c c c c c c c c c c c c c c c c $		(2) (3) (4) (5) (5) (5) (5) (5) (5) (5) (5	(1) 0,000 0,00
(C) 5919 (C) 5919 (C) 5919 (C) 5912 (C)	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	0 01 (0	10.03 10.05 10	60 00 00 00 00 00 00 00 00 00 00 00 00 0
10:5920 10:5920 10:5921 10:5922 10:5922 10:5922 10:5927 10:5929 10:592	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C0 01 (0 01 (0 01 (0 01 (0 01 (0 01 (0 01 (0 01 (0 01 (0 01) (0 01)	10.0) 10	60 00 00 00 00 00 00 00 00 00 00 00 00 0
LE15912 LE15922 LE15922 LE15925 LE15925 LE15925 LE15925 LE15925 LE15927 LE15927 LE15929 LE159344 LE15934 LE159	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	(0,0) (0,0)	(0.01 (0.01 (0.01 (0.01 (0.01 (0.01 (0.01 (0.01 (0.01 (0.01	00 00 00 00 00 00 00 00 00
C15924 C015925 C015925 C015926 C015926 C015929 C015929 C015929 C015929 C015929 C015929 C015939 C015939 C015939 C015949 C015949 C015949 C015949	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	0.12 0.19 0.19 0.24 0.23 0.23 0.10 0.05 0.04	<0.04 <0.01 <0.01 <8.01 <0.03 <0.03 <0.01 <0.01	<0.0 <0.0 <0.0 <0.0 0.0
CC15925 CC15927 CC15927 CC15927 CC15926 CC15927 CC15929 CC15934 CC15934 CC15934 CC15934 CC15934 CC15934 CC15934 CC15940 CC15940 CC15940 CC15940	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	0.19 6.40 0.24 0.23 0.10 - 0.05 0.04	<0.01 <0.01 <8.01 <0.01 <0.01 <0.01	<0.01 <0.01 0.01 <0.01
1015927 1015929 1015929 1015929 1015929 1015929 1015929 1015939 1015939 1015939 1015939 1015939 1015939 1015939 1015939 1015939 1015939 1015939 1015939 1015939	$\begin{array}{c} 423,455 \\ -823,450 \\ -823,650 \\ -824,610 \\ -824,610 \\ -824,610 \\ -824,600 \\ -824,600 \\ -824,600 \\ -925,450 \\ -925,460 \\ -925,460 \\ -925,460 \\ -925,460 \\ -925,460 \\ -925,460 \\ -925,460 \\ -925,460 \\ -925,460 \\ -922,450 \\ -922,$	0.17 0.24 0.23 0.10 0.05 0.04	<0.01 <0.01 <0.01 <0.01	0.0i (0.0i
LC15929 LC15929 LC15939 LC15931 LC15932 LC15933 LC15933 LC15935 LC15938 LC15938 LC15939 LC15939 LC15939 LC15939 LC15939 LC15940 LC15942 LC15943	974 19 974 69 974 69 9724 69 924 69 9725 46 925 45 9725 46 975 56 9726 48 976 45 9726 48 976 45 9726 48	0.24 0.23 0.10 0.05 0.04	<0.01 (0.01 (0.01	(0.0)
LC15930 LC15930 LC15931 LC15932 LC15933 LC15934 LC15936 LC15936 LC15939 LC15939 LC15939 LC15939 LC15939 LC15949 LC15941 LC15943	924.96 ~ 925.46 925.45 ~ 925.96 925.96 ~ 926.46 925.45 ~ 926.46 926.45 ~ 928.94 926.45 ~ 928.94 928.95 ~ 927.45	0.10 0.05 0.04	(0.91	<0.0
LC 15931 LC 15932 LC 15933 LC 15933 LC 15935 LC 15935 LC 15935 LC 15935 LC 15939 LC 15939 LC 15939 LC 15949 LC 15942 LC 15943	925.45 ~ 925.95 925.96 ~ 926.48 928.45 ~ 928.94 928.45 ~ 928.94	0.05		<0.0
LC15933 LC15934 LC15936 LC15936 LC15937 LC15939 LC15939 LC15940 LC15940 LC15941 LC15943	976.45 ~ 928.95 975.95 ~ 927.45	0.04	(0.6)	(0.0)
LC15934 LC15935 LC15935 LC15937 LC15937 LC15938 LC15938 LC15939 LC15940 LC15940 LC15941 LC15941 LC15941 LC15943	925 95 - 927 45		<0.01 (0.61	<0.01 <0.0
1C15936 1C15937 1C15938 1C15939 1C15939 1C15940 1C15941 1C15941 1C15942 1C15943	1 927.45 ~ 977 98	0.13	(0.01	<0.0×
LC15937 LC15938 LC15939 LC15940 LC15941 LC15941 LC15942 LC15943	927.96 ~ 928.45	0.09	<0.01 <0.01	+0.03 +0.01
LC15939 LC15940 LC15941 LC15941 LC15942 LC15943	928 45 - 928 96	0.13	<0.01	<0.0
1015941 L015942 L015943	929 96 ~ 929 45 929 46 ~ 929 95	0.08	<0.01 <0.01	<u> </u>
LE15942 LE15943	029.96 ~ 930.45 930.46 ~ 930.58	0.04	(0.01 (0.01	(0.01
	930.58 ~ 931.08	0.06	(0.01	<0.01 (0.01
	931.08 ~ 931.58 931.58 ~ 932.09	0.07	(0,01 (0,01	<0.01 <0.01
LC15945	932.08 ~ 932.58	61.G	<0.01	(0.0)
LC15945	937 58 ~ 933.08 933 98 ~ 933.58	0.07	<0.01	<u>. (0.01</u>
LC15948	933 58 ~ 933 88	0.12	<0.01	(Q.Č)
LC15949 LC15950	933.88 ~ 934.18 934.18 ~ 934.49	0.02	(0.0) (0.0)	(0.0 (0.0
1015051	931.49 - 931.98	0.09	10.01	0.0
LC15952 LC15953	934.99 ~ 935.49 935.49 ~ 935.98	0.12 <0.01	<0.01 <0.01	<u><0.0</u> <0.0
LC15954	935,98 ~ 936 (S 936,48 ~ 938,64	<0.01 <0.01	<0.01 <0.0)	<0.6 (0.0)
£C(5958	838 64 ~ 837.14	<0.01	<0 C1	<3.0
1015957 1015958	937,14 ~ 937,54 937,64 ~ 937,54	(0.01 (0.61	<0.61 <0.61	<0.01 <0.02
LC 15959	937.94 ~ 938.44	(0.01	<0.01	< 3.0
LC15960 LC15961	938.44 ~ 938.94 938.94 ~ 938.94	(0.0) (0.6)	<0.01 <3.87	<0.01 <0.01
LC15982	939 14 ~ 939 94	(0.01	10.01	<0.61
LC15963 LC15964	939.04 ~ 940.44 949.44 ~ \$49.94	<0.01 (0.01	<0.01 <0.01	<u>(0.01</u> (0.04
LC15065	543 94 ~ 541 44 Sel 48 ~ 981 98	0.01 0.02	(0.61 (0.61	<0.01
1018387	911.94 ~ 912.14	<0.01 <0.01	(0.01	(0.0)
LC15968	942.14 ~ 942.73 942.73 ~ 943.23	(0.0) (0.0)	<0.01 <0.01	<0.01 <0.01
LE15970	\$43.23 ~ \$13.73	0.02	(0.01	<0.0
LC1597) LC15972	543 73 - 944 73 544 73 - 944 73	0.03	<0.01 <0.01	(0.0) (0.0)
LC15973	914.73 ~ 945.23 915.23 ~ 945.73	0.07	<0.01	(0.0)
1C15974 1C15975	845 73 ~ 643 23	(0.0)	(0,01 (0,01	(0.01 (0.01
1015978 L015977	948 23 - 948.73 948.73 - 947.23	<0.01 <0.01	<0.01 <0.01	<0.01 <0.01
LC15979	\$47.23 - \$47.73	<0.01	(0.6>	(0.0)
LC15979	047.73 ~ 048.45 949.45 ~ 849.78	0.11	<0.01 <0.01	0.0
1015081	\$i8.78 ~ \$49.58	1.81	: <0.61	0.87
LC15983	949.58 ~ 949.75	0.61	<0.01 <0.01	8.04 8.01
LC+SQG4	11 949.75 ~ 950.06	1.45	(0.01	
LC15995 LC15996	050.05 ~ 050.55	2.42	-07.01 -07.01	
LC15987	651.05 ~ 951.13 961.13 ~ 051.43	0.55	19.0) 19.0>	<0.01 0.02
1615989	951.43 ~ 951.93	0.57	<0.01	<0.0
LC15990 LC15991	951.93 ~ 952.43 952.43 ~ 952.93	0.48	(0.01 (0.01	<0.01 <0.01
1015092	. 952.93 ~ 953.33	1.20	(0.01	0.01
(C15993 (C15994	953.33 ~ 953.63 953.63 ~ 951.15	0.70	(0.01 . (0.01	<0 01 (0.01
1015955	\$1.15 ~ 21.07	1.32	(Q. ()	- 0.01
LC 15998 LC 15997	954 67 ~ 954 96 954 98 ~ 955 48	0.47	(0,0) (0,0)	(0.0) (0.0)
LC15938 LC15959	955.49 ~ 954.00	0.56	<0.01	(0.01
LC15000	958.00 ~ 958.52 958.52 ~ 957.01	0.28	<0.01 (0.01	0.01
LC14301	957.04 ~ 957.56 957.58 ~ 958.08	0.41	(0.0) (0.0)	(0.0) (0.0)
LC14303	958 09 ~ 958 80	0.50	(Ð. Öl	(Ö. C)
1014304	958.60 ~ 959.12 959.12 ~ 958.64	0.14	<0.01 <0.01	<0.03 <0.03
1011328	959 64 ~ 960 18	ō. i ģ	(0.01	(0.0
LC14307 LC14308	960.18 ~ 950.58 960.58 ~ 961.11	0.17	(0,0) (0,0)	<u>(0,0)</u> (0,0)
1011301	\$61.11 ~ \$61.56	(0.01	<0.01	<0.0
(CIU)	962.06 ~ 962.39	0.25	<0_61 <0.01	(0.0) (0.0)
10115	967.39 ~ 967.64 967.84 ~ 963.39	0.06 0.20	<9.01 <9.01	(0.0) (0.0)
iću)ji	963.39 ~ 963.64	0.02	<0.01	(0.01
10(43)5	963 84 ~ 964 39 964 39 ~ 965 09	(0.01 (0.01	<0.01 <0.01	(0,0) 10.01
1011317	965.09 ~ 965.39	(0, ŌI	<0.01	<0.0
	965.39 ~ 965.64 965.64 ~ 968.39	(0.0) (0.01	<0.01 <0.01	(0,0) (0,0)
111320	958 39 ~ 958 56	(0.01	(0.01	(0.0
Fidth (+)	Ocptis (a)	(1)	A\$-Cu (\$)	1-Go (1)
2 09	\$43 45 ~ \$51 13	1.76	(0.01 (0.01	0.0

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MJZC-6

Scispile (•)	Dopth (1)	1-0.5 (1)	15-CU (\$)	1-Co (1)
LC19754	873,77 ~ 874,38	0.51	0.01	<0,0
LC19795	874.38 ~ 874.73	0.47	0.02	0,0
LC19796	874.73 ~ 875.23	0.18	0,03	0.01
C19797	875.23 ~ 875.73	0.01	0.01	
L C19798	875.73 ~ 875.23	0.01	(0.01	0_01
LC19759	876.73 ~ 876.73	0.03	0.01	0.01
LC19500	876,73 ~ 877,23	0.01	0.01	<0,0
L¢14201	877.23 ~ 877.60	0.19	0.03	0,03
LC14202	877.60 ~ 878.05	0.07	0.04	<0.01
LC14203	<u>\$55.15 ~ 955.65</u>	<0.01	<0.01	(0,01
LC14204 LC14205	\$55,65 ~ \$56,15	0.01	<0.01	(Q.Q)
LC14205	955.15 ~ 956.65	0.02	0.01	0.01
LC14207	956,65 ~ 957,15 957,15 ~ 957,65	<0.01 0.04	<0.01	(0,01
LC14208	957,65 ~ 958,15	0.05	0.02	<0.01 <0,01
LC14209	958,15 ~ 958,65	0.01	0.01	<0.01
LC14210	958.65 ~ 959.15	0.12	0.01	<0.01
14211	959,15 ~ 559,35	0.10	0.01	<0.0
LC14212	359,35 ~ 559.73	1.84	0.04	40,01
	953.73 ~ 961.15	0.02	<0.01	(0.0)
C14214	961.15 ~ 961.65	<9.01	(0.0)	0.0
LC14215	961.65 ~ 962.15	<0.01	<9.01	<0.01
LC14216	962.15 ~ 962.65	<0.01	<0.03	(0.0)
LC14217	962,65 ~ 963,15	<0.01	<0.01	(0.0)
LÇİ4218	963.15 ~ 963.65	<0,01	<0.01	<0.0)
LC14219	963.65 ~ 964.15	<0.01	<0.05	<0.01
LC14220	964,15 ~ 964,65	<9.01	<0.01	<0.01
LC14221	964,65 ~ 965,15	0,13	<0.01	<0.01
C14222	965.15 ~ 965.65	0,38	40.01	<0.0)
LC14229	965,65 ~ 966.15	<0.01	<0.01;	<0,01
LC14221	966,15 ~ 966,65	0.01	<0.01;	<0.01
LC14225	956.65 ~ 966.95	0.01	<0.01	<0.0)
C14226	956.55 ~ 967.45	<0.01	<0.01	<0.01
LC14227	967,45 ~ 967,55	<0.01	<0.01	<0.01
LC14228	967,95 ~ 968,45	<0.01	<0.01	(0,0)
C14229	968,45 ~ 968,55	0.04	<0.01	(0,0)
C14230	968.95 ~ 969.45	<0.01	<0.01	<0.01
LC14231	969,45 ~ 969,56	<0.01	<0.01	0.01
LC14232	963.56 ~ 970.06	ļļ	<0.01	(0.0)
LC14233	970,66 ~ 970,56	0.01	<0.01	(0,0)
LC14234	970.56 ~ 971.06	<0.01	<0.01	<0.01
C14235 C14236	971.06 ~ 971.56	i	<u>(0,01]</u>	<0.0
LC14237	971.56 ~ 972.06		<0.01	(0,01
LC14238	972.06 ~ 972.56 972.56 ~ 972.96	0.04	<0.01 0.01	<0.01
C14239	972,96 ~ 973,45	0.07	0.01	<0.01 0.01
C14240	973.45 ~ 973.76	0.08	0.01	<0,0
C14241	973,76 ~ 974,06	0.08	<0.01	<0.01
LC14242	914.06 ~ 974.35	0.26	<0.01	<0,01
C14243	914.36 ~ 974.85	0.29	0.01	<0,0
C14244	974.85 ~ 975.36	0.21	(9.01	<0.01
C14245	\$75.36 ~ \$75.85	0.27	(9,01	<0,01
C14246	975.85 ~ 978.36	0.41	<9.01	<0.01
C14247	976.35 ~ 976.85	0.22	<0.01	<0.01
C14248	976,85 ~ 977,36	0.62	<0.01	<0.01
£14249	977,36 ~ 977,85	0.63	<0.01	<0.01
C14250	977,85 ~ 978,16	0.52	<0.01	<0.01
C14251	978,15 ~ 978,45	0.14	<0.01	<0.01
C14252	<u> 978,45 ~ 978,55</u>	0,12	<0.01	<0.01
C14253	978,95 ~ 979,45	0.43	<0.01	0.0
C14254	979,45 ~ 979,55	0.15	<u><9.0</u> 1]	0,01
C14255	979.55 ~ 980.45	0.22	<u><0.01</u>]	<0,01
C14256	\$80,45 ~ \$30,95	0.47	<0,01	0,01
C14257	980.95 ~ 931.10	0.31	<0.01	<0.01
C11251	\$81.10 ~ \$31.40	0.54	0.02	<0.01
C14259	941,40 ~ 941,90	1.22	0.01	<u>a</u> , 01
C14260	981.90 ~ 982.45	1.13	0.02	<u>- 0,01</u>
C14261	<u>\$82.40 ~ \$82.90 ;</u>	46	<u></u>	<0.0
CI 1262	932,90 ~ 383,43	1.57	0.01	0.02
C1 (263	\$83,40 ~ \$83,55	1.02	-0.01	<u>. 0.0</u>
C14264	983.95 ~ 984.45	0,84	0.01	0.01
C14265	<u>924,45</u> ~ <u>924,95</u>	0.44	<u>(0,01</u>	<u><0.0</u> }
C14266	<u>984.96</u> ~ 985.46	0.29	0.01	<u>(0,0)</u>
<u>C14267</u>	\$85.46 ~ \$85.85	0.67	(0.01	0.01
C14268	985.85 ~ 985.35	0.16	<0.01	<u>_<0,0</u>]
C14269	986.85 ~ 986.85 956.85 ~ 967.35	0.05	<0,01	<0.01 <0.01
	- 200.00 ~ 351.53	0.06	<0.01	<v.9< td=""></v.9<>
C14270 C14271	\$37.35 ~ \$87.85	0,21	<0.01	<0,01

	A	1.7.4		7
Science	Depth	1-0	A5-00	T-Co
<u>()</u>	<u>()</u>	$\lfloor 0 \rfloor$	<u>_())</u>	<u>_(i)</u>
LC14273	0.00 ~ 0.50	0.52	<0,01	<0.0
LC14274	953.85 ~ 589.53	0,10	<0.01	<0.0
LC14275	989.53 ~ 990.03	0.25	<0.01	Q.Q
L¢14276	990.03 ~ 990.53	0.16	<0.01	Ø.0
LC14277	990.53 ~ 990.96	0.11	<0.03	0.0
LC14276	990.95 ~ 991.46	0.42	<0.01	<0.0
LC14279	991.45 ~ 991.96	0,29	<0.0)	<0.0
LC14280	991,96 ~ 992.46	0.32	10.0>	<0.0
LC14281	992.45 ~ 992.79	0.32	<0.01	<0.0
LC14282	992,79 ~ 993,29	0,38	<0.01	<0.0
LC14283	993.29 ~ 993.79	0,17	<0.01	Q.0
LC14284	993,79 ~ 994,29	0.41	<0.01	<0,0
LC14285	994,29 ~ 994,79	0.50	<0.01	Q.0
LC14285	994,79 ~ 935,00	0.58	0,01	0.0
1014287	995,00 ~ 995,6		6 01	0 0
LC14288	995.68 ~ 996.1		<0.01	<0.0
LC14289	996.18 ~ 996.6		<0.01	<0.0
LC14290	996.68 ~ 996.9		0.01	<0.0
LC14291	996.96 ~ 997.4			
			0,01	(0,0
LC14292	<u>997.45</u> ~ <u>997.9</u>		<u><0.01</u>	<0,0
LC14293	997,96 ~ 938,44	······································	<u>(0,01</u>	<0.0
LC14294	998.46 ~ 998.96		<0.01	- 40.0
LC14295	998.96 ~ 999.4		<0.01	<3.0
LC14296	999,46 ~ 999.9		<0.01	<0.0
LC14297	999.96 ~ 1000.40		<0.01	<0.0
LC14258	1000.46 ~ 1001.0		<0.01	<0.0
LC14299	1001.05 ~ 1001.5		<0.01	0.0
LC14300	1001.55 ~ 1002.05		<0.01	0.0
LC15901	1002.05 ~ 1002.5		<0.01	8 .0
LC15902	1002.55 ~ 1002.96		<0.01	0.0
LC15903	1002.96 ~ 1003.10		<0.01	0.0
1015904	1003.10 ~ 1003.60		<0.01	<0,0
LC15905	1003.60 ~ 1004.10		<0.01	0.0
LC15306	1004.10 ~ 1004.60		<9.01	<0,0
LC15907	1004.60 ~ 1005.10		<9.01	<0.0
LC15908	1005.10 ~ 1005.60	+	<0.01	0,0
LC15909	1005.50 ~ 1006.10		<9.01	<0.0
LC15910	1006.10 ~ 1006.43		<0.01	<0,0
LC15911	1006.43 ~ 1006.9		<0_01	0.0
LC15912	1006,93 ~ 1007.3		<0.01	0.0
LC15913	1007.35 ~ 1007.85		0_0I	Q.Q
LC15914	1007.85 ~ 1008.35		<0.01	<0,0
LC15915	1008,35 ~ 1008.96	<0.01	<0.01	(0.0
<u>.</u>		:	<u>`</u>	
: Vidth	Depth	I-Cu	AS-Cu	1-Co
<u>_()</u>	(•)	<u>(0)</u>	<u>(</u>)	<u></u>
3,35	981.10 ~ \$84.45	1.14	<0.01	(0,0
1,39	994.29 ~ 955.68	0,89	<u>(0,01</u>	0.0
÷ .	1			
			÷	

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	Table 2-5-1	Results of	Chemical	Analysis	of	Ore	Samples	(5)
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MJZC-9

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B CQ2 CQ3 CQ3 CQ3 CQ3 CQ3 CC12702 1377, 85 13777, 85 13777, 85 1377, 85 <th>1</th> <th>Seepte</th> <th>Depth</th> <th>[-Cu</th> <th>AS-Cu</th> <th>I-Co</th>	1	Seepte	Depth	[-Cu	AS-Cu	I-Co
IC 12704 1377, 85 <t< th=""><th></th><th></th><th>(•)</th><th>(1)</th><th>(3)</th><th>(1)</th></t<>			(•)	(1)	(3)	(1)
IC 17700 1578.45 1379.55 0.01 0.01 0.01 IC 12705 1979.50 1979.57 0.05 0.01 0.01 0.01 IC 12705 1979.50 1979.50 1979.50 0.05 0.01 0.01 0.01 IC 12705 1979.57 1080.57 1080.57 0.05 0.01	1		1377.45 ~ 1377.95	the second s	manufactor and the second	
C (2720) 1073, 50 100, 10 0, 01 0, 01 0, 01 C (2725) 1073, 57 1080, 17 0, 05 0, 01 0, 05 0, 01 0, 05 0, 01 0, 05 0, 01 0, 05 0, 01 0, 05 0, 01 0, 0						
IC1226 1373 67 \sim 1360, 17 0.05 0.01 0.01 0.01 0.01 IC12705 1380, 17 0.06 0.01 0.01 0.01 0.01 IC12705 1381, 17 0.061, 17 0.06 0.01 0.01 0.01 IC12705 1381, 17 0.014, 07 0.11 0.05 0.01 0.01 0.01 IC12715 1382, 17 0.124 0.024, 17 0.13 0.01 0.01 0.01 IC12716 1383, 17 0.183, 16 0.11 0.01<	ļ					· •
SC12727 1980, 17 \sim 1981, 17 \circ 0.01	ļ	·				
C:12726 130007 130007 0.0607 0.06 0.01 0.01 C:12703 130117 1302.17 1.17 0.01 0.01 0.01 C:12711 1302.17 1.182.17 1.12 0.01 0.01 0.01 C:12711 1302.17 1303.17 0.135.07 0.135 0.01 0.01 C:12715 1303.17 1033.67 0.15 0.01 0.01 0.01 C:12716 1303.17 1035.68 0.52 0.01 0.01 0.01 C:12716 1304.68 1305.68 0.52 0.01 0.01 0.01 C:12716 1304.68 1305.68 0.52 0.01 0.01 0.01 C:12716 1306.88 1305.86 0.52 0.01 0.01 0.01 C:12721 1306.87 1308.78 1.18 0.01 0.01 0.01 C:12721 1306.87 1308.78 0.18 0.01 0.01 0.01 C:12727						
EC:12703 1081.17 \sim 1082.17 0.36 $(0,0)$ $(0,0)$ $(0,0)$ $(0,0)$ EC:12711 1082.17 \sim 1082.17 $(0,0)$ $(0,0)$ $(0,0)$ EC:12712 1082.17 \sim 1082.17 $(0,0)$ $(0,0)$ $(0,0)$ EC:12712 1082.17 \sim 1083.67 $(0,0)$ $(0,0)$ $(0,0)$ EC:12716 1083.67 $(0,0)$ $(0,0)$ $(0,0)$ $(0,0)$ EC:12716 1084.68 $(0,2)$ $(0,0)$ $(0,0)$ $(0,0)$ EC:12716 1084.76 $(0,0)$			a company and the second			
EC12/11 1082.17 \sim 103.27 0.17 0.51 0.01 EC12/12 1083.17 \sim 1083.67 0.15 0.01 0.01 EC12/13 1083.17 \sim 1084.68 0.22 (3.01) 0.01 EC12/15 1084.63 \sim 1084.64 0.52 (3.01) (0.01) EC12/15 1084.63 \sim 1085.66 0.52 (3.01) (0.01) EC12/16 1085.67 0.52 (3.01) (0.01) (0.12) (0.01) (0.12) EC12/11 1086.16 (1087.16) (2.55) (0.01) (0.12) (0.01) (0.12) EC12/14 1086.76 1087.75 (2.56) (0.01) (0.12) (0.01) (0.12) EC12/24 1088.76 (183.5) (0.11) (0.11) (0.11) (0.1) (0.21) EC12/24 1088.76 (193.5) (0.13) (0.01) (0.21) (0.10)			and the second sec			
SC1272 1032, 57 (0.3, 17 <th(0.3, 17<="" th=""> (0.3, 17 <</th(0.3,>						
EC12713 1083.17 \sim 1084.27 0.15 $(3,01)$ $(0,01)$ EC12715 1084.27 \sim 1084.68 0.22 $(3,01)$ 0.01 EC12715 1084.68 0.22 $(3,01)$ 0.01 EC12715 1084.68 0.22 $(3,01)$ 0.01 EC12715 1084.68 2.244 $(3,01)$ $(0,01)$ EC12715 1086.68 2.244 $(3,01)$ $(0,01)$ EC12715 1086.78 (2.95) $(0,01)$ $(0,01)$ EC12723 1084.76 (1087.78) (2.59) $(0,01)$ $(0,01)$ EC12723 1084.76 (1087.78) (2.57) (2.01) $(0,01)$ EC12723 1084.76 (1087.78) (2.57) (2.01) (0.01) EC12724 1084.76 (1087.78) (2.57) (2.01) (0.01) EC12725 1084.76 (1087.78) (2.57) (2.01) $(2.017.78)$ EC12726 1094.78 (1087.78)						
4C12716 1083, E7 1084, 22 0.22 (4,01) 0,01 6C12715 1084, 63 1085, 18 (4,01) 0,01 6C12717 1085, 18 1085, 18 (4,01) (0,01) 6C12717 1085, 18 1085, 18 (4,01) (0,01) 6C12718 1085, 18 1085, 18 (4,01), 16 (2,01) (0,01) 6C12721 1084, 65 1087, 18 (2,55) (0,01) (0,01) (0,01) 6C12721 1084, 75 (2,56) (0,01) <td< td=""><td></td><td></td><td>· · · · · · · · · · · · · · · · · · ·</td><td></td><td></td><td></td></td<>			· · · · · · · · · · · · · · · · · · ·			
EC12715 1024, 55 \sim 1035, 56 \circ , 52 \circ , 0, 01 \circ , 0, 01 EC12717 1035, 18 \sim 1035, 56 \circ , 52 \circ , 0, 01 \circ , 0, 01 EC12718 1036, 56 \sim 1045, 18 \circ 1045, 18 \circ , 145 \circ , 0, 01 \circ , 0, 01 EC12718 1036, 18 \sim 1047, 18 $<$ 2, 56 \circ , 0, 01 \circ , 0, 01 EC12712 1348, 25 1084, 25 $<$ 2, 55 \circ , 0, 01 \circ , 0, 01 EC12724 1388, 25 1084, 25 $<$, 75 $<$, 0, 01 \circ , 01 $<$, 0, 01 EC12725 1394, 26 1393, 05 0, 02 $<$, 0, 01 $<$, 0, 01 $<$, 0, 01 EC12727 1394, 26 1035, 05 0, 03 0, 01 0, 02 $<$, 01 0, 02 EC12726 1394, 26 1035, 05 0, 03 0, 01 0, 02 $<$, 01 0, 02 EC12726 1395, 05 1393, 05 0, 03 0, 01 0, 02 C12731 1395, 05 033 0, 01 0, 02		and the second sec				
KC12117 1985.18 \sim 1985.68 6.52 $(3,01)$ $(3,01)$ KC12118 1986.85 (1667.16) $(7,45)$ $(3,01)$ $(3,01)$ GC12129 1986.85 (1667.16) $(2,58)$ $(0,01)$ $(0,01)$ GC12121 1986.85 (1687.75) $(2,58)$ $(0,01)$ $(0,01)$ GC12121 1987.85 (1687.75) $(2,58)$ $(0,01)$ $(0,01)$ KC12121 1987.86 (1987.75) $(2,59)$ $(0,01)$ $(0,01)$ $(0,01)$ KC12121 1987.86 (1987.75) $(2,59)$ $(0,01)$ $(0,01)$ $(0,01)$ KC12124 1988.76 (1987.75) $(2,59)$ $(0,01)$ $(0,01)$ $(0,01)$ KC12124 1988.76 (1987.75) $(2,59)$ $(0,01)$ $(0,01)$ $(0,01)$ KC12124 1989.75 (1987.75) (1987.75) $(2,01)$ $(0,01)$ $(0,01)$ KC12125 1999.75 (1987.75) (1987.75) (1987.75)		· · · · · · · · · · · · · · · · · · ·				
C1218 1985,63 $21,645,19$ 1.46 $-0,01$ $-0,01$ C02719 1986,65 $22,441$ $(3,0,01)$ $0,01$ C02729 1986,75 $21,007,18$ $22,56$ $0,01$ $0,01$ C02727 1987,75 $21,007,18$ $22,56$ $0,01$ $0,01$ C02727 1987,75 $21,007,75$ $22,59$ $0,01$ $0,01$ C02727 1987,75 $1088,76$ 118 $0,01$ $0,01$ C02727 1987,75 $1088,75$ $1088,75$ $108,75$ $0,10$ $0,01$ C02727 1987,75 $1081,25$ $0,19$ $0,01$ $0,02$ C12725 1984,95 $198,25$ $0,19$ $0,01$ $0,02$ C12729 1991,00 $1991,25$ $0,13$ $0,01$ $0,02$ C12729 1991,00 $1992,55$ $0,03$ $0,01$ $0,02$ C12729 1992,50 $1993,55$ $0,02$ $0,01$ $0,02$ C12728 1992,55 $1992,55$ $0,02$ $0,01$ $0,02$	1	i in constanta a		· · · · · · · · · · · · · · · · · · ·		
SC12713 1006, 18 $2, 106, 18$ $2, 44$ $(0, 0, 1)$ $(0, 2, 18)$ $(0, 0, 1)$ SC1272 1007, 18 $2, 1007, 78$ $2, 55$ $(0, 0)$ $(0, 0)$ SC1272 1007, 18 $2, 1007, 78$ $2, 55$ $(0, 0)$ $(0, 0)$ SC1272 1007, 76 $(1007, 78)$ $2, 35$ $(0, 0)$ $(0, 0)$ SC1272 1007, 76 $(1007, 78)$ $(2, 30, 0)$ $(0, 0)$ $(0, 0)$ SC1272 1007, 76 $(1007, 78)$ $(2, 30, 0)$ $(0, 0)$ $(0, 0)$ $(0, 0)$ $(0, 0)$ SC1272 1007, 76 $(1007, 78)$ $(2, 0)$ $(0, 0)$ <					h	
Sci 2211 [007.18 2 , 1087, 75 2 , 59 0 , 61 2 , 61 Sci 1272 [1387, 75] 2 , 1088, 75 0 , 18 0 , 01 0 , 01 0 , 01 Sci 12723 [1388, 26] $1058, 76$ 0 , 18 0 , 01 0 , 01 0 , 01 Sci 12725 [1388, 26] $1059, 25$ 0 , 18 0 , 01 0 , 01 0 , 01 Sci 12725 [1393, 50] $1059, 25$ 0 , 18 0 , 01 0 , 02 Sci 12725 [1393, 50] $1091, 50$ $1092, 55$ 0 , 33 0 , 01 0 , 02 Sci 12725 [1932, 50] $1092, 50$ $1092, 50$ 0 , 03 0 , 01 0 , 02 CC 12723 [1932, 50] $1092, 50$ $1092, 50$ 0 , 02 0 , 01 0 , 02 CC 12723 [1933, 50] $1092, 50$ 0.02 0.01 0 , 02 CC 12733 [1934, 50] $1095, 50$ 0.02 0.01 0 , 02 CC 12733 [1934, 50] $1095, 50$ $1095, 50$		KC15113	1086.18 - 1086.68	2.41	<0.01	0.01
Image: state interval Image: state interval						
KC12723 1988.25 \sim 1989.75 0.18 (0.0) 0.02 KC12724 1988.76 \sim 1989.75 (1.53) (3.0) 0.01 KC12725 1984.76 \sim 1999.05 0.02 (3.0) 0.61 KC12725 1984.06 \sim 1999.05 0.02 (3.0) 0.62 KC12727 1980.06 \sim 1981.06 0.33 (0.01) 0.62 KC12728 1991.06 \sim 1992.05 0.33 (0.01) 0.62 KC12723 1992.06 \sim 1992.55 0.02 (0.61) 0.62 KC12723 1993.05 0.02 (0.61) 0.62 (0.61) 0.62 KC12733 1994.05 0.92 0.02 (0.61) 0.62 (0.01) 0.62 KC12733 1994.05 0.92 0.02 (0.01) 0.62 (0.01) 0.62 KC12733 1994.55 0.95	: 1					
\$C12724 1065.76 1059.25 0.72 $C0.01$ 0.01 $$C17725$ 1954.26 1059.50 0.22 (3.0) 0.52 $$C17725$ 1954.50 1095.50 0.19 0.01 5.62 $$C17726$ 1955.50 0.21 0.61 5.62 $$C17726$ 1951.50 0.33 0.01 5.62 $$C17723$ 1091.50 1092.50 0.33 0.01 0.02 $$C17733$ 1092.50 0.03 0.01 0.02 0.01 0.02 $$C17733$ 1093.50 1092.50 0.02 0.01 0.02 0.01 0.02 0.01 0.02 0.01					the second second	
KC12725 1089, 50 1099, 60 0,02 C3,01 0,02 KC12727 1390, 50 1091, 50 0,19 0,01 0,02 KC12728 1390, 50 1091, 50 0,01 0,02 0,01 0,02 KC12730 1091, 50 1092, 50 0,03 0,01 0,02 0,03 0,01 0,02 KC12731 1092, 50 1092, 50 0,03 0,01 0,02 0,02 0,02 0,02 0,02 0,02 0,02 0,02 0,02 0,02 0,02 0,02 0,02 0,02 0,01 0,02 0,02 0,01 0,02 0,01 0,02 0,01 0,02 0,01 0,02 0,01 0,02 0,01 0,02 0,01 0,02 0,01 0,02 0,01 0,02 0,01 0,02 0,01 0,02 0,01 0,02 0,01 0,02 0,01 0,02 0,01 0,02 0,01 0,02 0,01 0,02 0,01 0,02 <t< td=""><td></td><td></td><td>a see an an and the second /td><td></td><td></td><td></td></t<>			a see an an and the second			
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KC12728 1335.50 1291.00 0.79 0.01 5.03 KC12730 1091.00 1091.50 1092.00 0.33 0.01 0.02 KC12731 1092.00 1092.50 0.03 0.01 0.02 KC12731 1093.00 1092.50 0.03 0.01 0.02 KC12731 1093.50 1093.53 0.01 0.02 (0.01 0.02 KC12733 1093.50 1094.53 0.02 (0.01 0.02 (0.01 0.02 KC12735 1094.03 1095.35 0.02 (0.01 0.02 (0.01 0.02 KC12734 1095.35 1095.55 0.23 (0.01 0.02 (0.01 0.02 KC12740 1095.35 1095.85 0.23 (0.01 0.02 (0.01 0.02 KC12740 1095.35 1097.85 0.23 (0.01 0.02 (0.01 0.02 KC12741 1098.85 1097.85 0.23 (0.01 0.02 (0					· · · · · · · · · · · · · · · · · · ·	
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kC12745 1939.35 \sim 1939.85 0.05 0.01 0.03 kC12747 17399.85 \sim 1400.35 0.33 $c2.01$ 0.02 kC12747 17039.85 \sim 1100.35 0.42 0.01 0.02 kC12748 1100.35 \sim 1101.35 0.41 $c0.01$ 0.02 kC12755 1101.35 \sim 1101.35 0.01 $c0.01$ 0.02 kC12755 1101.35 \sim 1101.35 0.01 $c0.01$ 0.02 kC12755 1103.85 \sim 1102.35 0.01 $c0.01$ 0.02 kC12755 1103.85 \sim 1103.35 0.01 $c0.01$ 0.03 kC12755 1103.85 \sim 1103.35 0.01 $c0.01$ 0.05 kC12755 1103.85 \sim 1103.85 0.01 $c0.01$ 0.05 kC12755 1104.35 \sim 1105.35 0.06 $c3.01$ 0.65 kC12756 1104.85 \sim 1105.76 0.05 $c3.01$ 0.65						
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$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	ļ		1103.85 ~ 1104.95	0.01	<0.61	0,95
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$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		#C+2759	1105.76 - 1106.28	0.07	(0,61	(0.01
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4C12779 1115.25 ~ 1115.75 0.75 0.01 0.01	ļ	(Ciam)	1114.25 ~ 1114.78	0.77	<0.01	0.01
10.01 0.01 0.01 10.12783 1115.78 ~ 1115.26 0.79 <0.61 0.01						
		·		0,70		

Sampte	Depth	f-Cu	AS-CU	1-Co
No	(b)	0	0	(1)
KC12781	1115.25 - 1115.76	0.38	<0.01	0.01
KC12782	1115,76 ~ 1117,00	0.13	(0.01	<3.01
KC12783	1117.00 ~ 1117.50	1.56	(0.01	@ 01
KC12784	1117.50 ~ 1118.00	10	<0.01	<0.01
KC12785	1118.00 ~ 1118.50	0,62	<0.01	0.01
XC12785	1118.50 ~ 1119.00	0.33	<d.01< td=""><td>0.01</td></d.01<>	0.01
KC12787	1119.00 ~ 1119.50	0.11	<0.0)	<0.01
XC12783	1119.50 ~ 1120.00	1,03,-	<0.01	0,06
KC12783	1120.00 ~ 1120.50	D, 73	<9.01	0.03
KC12790	1129,55 ~ 1120,75	0.32	<0.01	0.01
KC12731	1123.78 ~ 1121.25	0,41	<0.01	0.01
CC12792	1121.25 ~ 1121.75	0,15	<0.01	<0.01
KC12793	1121.75 ~ 1122.25	0.04	0.01	<3,01
KC12794	1)22.25 ~ 1)22.75	0.04	(9.01	0,01
KE12795	1122.76 - 1123.25	9_02	<0.01	<0.01
KC12795	1123 25 ~ 1123 75	9.07	<0.01	(0,61
KC12797	1123,76 ~ 1124,25	0.03	(0.01	B.01
KC12798	1124.25 ~ 1124.75	0.01	<0.01	D.01
KC+2739	1124,75 ~ 1125,25	0.01	(O.01	D.01
KC42839	1125.25 ~ 1125.75	0.03	<9.01	D.01
KC1510E	1125,75 ~ 1)25,25	0.01	<0.01	0.01
KC15102	1125,28 ~ 1125,75	0,02	<0.01	0.01

fidth	Depth	1-Cu	AS-Cu	1-Co
(0)	(+)	(0)	(D)	(1)
2.58	2085.58 ~ 1088.26	7.29	<3.01	(9.01
5.93	1108.35 ~ 1114.25	3.12	<9.01	9.08
8.24	1114.25 ~ 1120.50	0,78	<0.01	<0.02

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Table 2-5-1 Results of Chemical Analysis of Ore Samples (6)

MJZC-11

MJZC-10

Saaple No	Depth (=)	1-01 (1)	As-Cu (1)	1-Co (1)
KC12222	953.70 ~ 954.70	0.01	0.01	0.01
KC12223	954.70 ~ 955.70	<0.01	4.01	<9.01
KC12224 KC12225	955.70 ~ 958.70 955.70 ~ 957.70	0.0) (9.01	<0.01 <3.01	<0.01 <0.01
KC12225	9557.79 ~ 958.79	<0.01	<2.41	(3,0)
KC12227	958,70 ~ 959.70	<0.01	<2,01	<0.01
KC12228 KC12229	559.70 ~ 950.70 550.70 ~ 551.33	<0.01 <0.01	<3.01	(0.51
KC 12230	\$50,70 ~ \$51,33 \$51,33 ~ \$51,83	<9.01	<0.01 <0.01	<0.03 <0.03
4C12231	951.63 ~ 952.33	<0.01	0.01	<0.01
4C12232 4C12233	952.33 ~ 952.70 952.70 ~ 953.20	<0.01 <0.01	<3.01 (3.01	<0.01
1012234	962.70 ~ 953.20 \$53.20 ~ \$53.70	3.01	<u>ଏ</u> .01 ଏ.01	<0.01 (0.01
£E12235	963.70 - 954.20	<0.01	C).01	<3.01
#C12236 KC12237	\$54.20 ~ \$54.70 \$54.70 ~ \$55.20	0.01	<0.01 <0.01	<3.01 0.01
RC12238	954.70 ~ 955.29 955.20 ~ 955.79	<0.01	<0.01	0.02
KC12239	965.70 ~ 958.20	<0.01	<0.01	0.01
KC12240 KE12241	956.20 ~ 956.70	<0.01	<0.01	0.01
KC12242	556.70 ~ 957.20 557.20 ~ 957.70	<3.01 <0.01	(0,01 (0,01	0.01
KC12243	957.73 ~ 958.23	0.01	<3,01	0.01
KC 12244	958.22 ~ 958.70	<0.01	<9.01	<0.01
K£12245 K£12245	958.73 ~ 959.23 959.23 ~ 959.73	0.01	<0.01 <0.01	0.01 <0.01
1(1)2247	\$59.70 ~ \$70.20	<0.01	(0,01	(0.01
KC 12248	979.25 ~ 970.72	0.97	<0.01	<0.01
KC12243 KC12253	973.72 ~ 971.23 971.20 ~ 971.72	0.01 <0.01	(0,01 (0,01	<0.01 0.01
KC12751	971.70 ~ 972.20	0.01	0.01	0.01
KC 12252	972.20 ~ 972.70	<0.01	<0.01	0.01
KC12253 KC12254	972.79 ~ 973.20 973.20 ~ 973.62	0.01	<0.01 <0.01	0,01 0,01
KC12255	973.62 ~ 974.12	0.03	<0.01	0.03
KC 12255	\$74.12 ~ 974.62	0.03	<3.01	0.03
KC12257 KC12258	976.62 ~ 975.12 975.12 ~ 975.62	0.18	<0.01 <0.01	0.03
KC12259	975.62 ~ 976.15	0.08	<2.01	50.0
KC +2260	975.15 ~ 576.65	0,11	<0.01	0.02
KC12251 KC12252	975.65 ~ 977.18 977.15 ~ 977.65	0,32	<0.01 <0.01	9,02 <0,01
IC12253	977.65 ~ 978.15	0,12	<3.01	D.01
KC12254	978.15 ~ 978.55	0.10	<0.01	0.01
KC12255 KC12256	973.65 ~ 979.15 979.15 ~ 979.65	0.12	<0,01 <0,01	0.01
KC12257	979.65 ~ 983.16	0.05	<0.01	0,03
KC12256 KC12259	583.15 ~ 583.70 580.73 ~ 581.23	0.05	0.01	0.01
KC12270	980.70 ~ 981.20 981.20 ~ 985.70	0.06	<0.01 <0.01	0.01
KC12271	951,70 ~ 992.20	0.11	<0.01	0.02
4C12272 KC12273	582,23 ~ 542,70 582,20 ~ 583,20	1.77	(0.01	0.04
*C12274	582.20 ~ 583.20 983.20 ~ 583.70	8.80	<u>्र</u> ्.01 (0.01	0.03
#C12275	583.70 ~ 584.20	0.23	(0.01	0.04
4C12275 4C12277	584.20 ~ 984.70 584.70 ~ 985.20	<3.01 0.16	(0.0)	0.03
4012278	984.70 ~ 985.20 985.20 ~ 985.70	0.15	- (0,03 - (0,01	<0.01 0.04
¥C12279	985,73 ~ 985.20	0.05	<0.01	0.07
4012280 #012281	985.20 ~ 985.70 985.70 ~ 987.20	0,79	<0.01 <0.01	0.03
4012292	885.70 ~ 987.23 887.20 ~ 987.55	0.34	<0.01	0.02
KC12283	\$87.55 ~ 988.05	0.29	0,01	(0,01
KC12285	988.06 ~ \$39.55 988.55 ~ \$39.06	9,54 0,47	0.01	<0.01 <0.01
EC12285	988.55 ~ 589.08 989.06 ~ 989.70	0.24		<0.01
(155132	\$\$9,70 ~ \$90.20	0.21	<0.01	<0.01
KC12285 KC12289	990.20 ~ 990.70 990.70 ~ 991.20	0,39	<0.01 0.01	<0.01 <0.01
KC12290	991,23 ~ 991,88	0.05	<0.01	<0.01
RCH2291	991.88 ~ 992.98	9.25	<3.01	<9,01
C12292 C12293	992.38 ~ 992.68 992.88 ~ 993.58	0.22	0.01	<0.91 <0.91
KC12294	992.88 ~ 993.56 993.56 ~ 934.06	0,34	0.03	<0 01 <0 01
4012295	894.06 ~ 994.56	0.32	<0.01	<0.01
KC12295	994.56 ~ 995.06	0.35	<0,01	<0.01
KC12297 KC12298	995.06 ~ 995.56 995.56 ~ 995.05	0,13	0.01 0.08	<0.01 <0.01
RC12299	\$36.05 ~ \$95.56	0,10	0.01	<0.01
KC12300	995,56 ~ 997,06	0.09	0.02	(0.01
KC18932	\$97.06 ~ 997.56	0.09	<0.01	<0.01
Width	Depth	As-Cu	5-Co	
(1)	(•)	(1)	(1)	

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Sasp1# Depth I-Cu AS-Cu Co NS (2) (3) (3) (3) (3) 4C (513) 635, 65 635, 55 60, 61 (0, 01 (0, 01 1C (513) 635, 55 637, 05 60, 61 (0, 01 0, 01 (0, 01 0, 01 1C (1513) 636, 65 637, 05 60, 01 (0, 01 0, 01 0, 01 (0, 01 0, 01 1C (1513) 637, 05 638, 05 6, 01 (0, 01 0, 02 (1, 0, 01) 0, 02 1C (1511) 638, 05 638, 05 638, 05 (0, 01) (0, 01) 0, 02 1C (1511) 638, 05 639, 05 (0, 01) (0, 01) 0, 02 1C (1511) 640, 05 641, 05 0, 01 (0, 01) 0, 02 1C (1511) 641, 05 641, 05 0, 01 (0, 01) 0, 02 1C (1511) 641, 05 641, 25 0, 01 0, 01 0, 03 1C (1511) 641, 05 <td< th=""><th></th><th></th><th></th><th>· · · · · · · · · · · · · · · · · · ·</th><th></th></td<>				· · · · · · · · · · · · · · · · · · ·	
$\begin{array}{c} 4C15133 & 635, 65 &\sim 635, 55 &< 60, 61 &< 0, 61 &< 0, 61 &< 0, 61 &\\ c(5134) & 635, 55 &\sim 635, 55 &< 0, 61 &< 0, 61 &< 0, 61 &\\ c(5134) & 635, 55 &\sim 637, 65 &< 0, 61 &< 0, 61 &< 0, 61 &\\ c(5134) & 637, 65 &\sim 637, 65 &< 0, 61 &< 0, 61 &< 0, 61 &\\ c(5134) & 637, 65 &\sim 637, 65 &< 0, 61 &< 0, 61 &< 0, 61 &\\ c(5132) & 637, 65 &\sim 638, 55 &< 0, 61 &< 0, 61 &< 0, 61 &\\ c(5133) & 637, 65 &\sim 638, 65 &< 0, 61 &< 0, 61 &\\ c(5134) & 637, 65 &\sim 638, 65 &< 0, 61 &< 0, 61 &\\ c(5134) & 638, 55 &\sim 638, 65 &< 0, 61 &< 0, 61 &\\ c(5134) & 638, 55 &\sim 638, 65 &< 0, 61 &< 0, 61 &\\ c(5134) & 638, 55 &\sim 638, 65 &< 0, 61 &< 0, 61 &\\ c(5131) & 638, 55 &\sim 643, 95 &< 0, 61 &< 0, 61 &\\ c(5131) & 638, 55 &\sim 643, 95 &< 0, 61 &< 0, 61 &\\ c(5111) & 638, 55 &\sim 644, 05 &\\ c(5111) & 642, 55 &\sim 644, 05 &\\ c(5111) & 641, 65 &\sim 641, 55 &\\ c(5111) & 641, 65 &\sim 641, 55 &\\ c(5111) & 642, 55 &\sim 642, 25 &\\ c(5111) & 642, 55 &\sim 642, 25 &\\ c(5111) & 642, 55 &\sim 642, 25 &\\ c(5111) & 642, 55 &\sim 644, 25 &\\ c(5112) & 643, 25 &\sim 644, 25 &\\ c(5112) & 643, 25 &\sim 644, 25 &\\ c(5112) & 644, 75 &\sim 645, 25 &\\ c(5112) & 645, 55 &\sim 645, 55 &\\ c(5112) & 645, 55 &\sim 655, 55 &\\ c(5112) & 645, 55 &\sim 655, 55 &\\ c(5112) & 645, 55 &\sim 655, 55 &\\ c(5113) & 655, 53 &\sim 655, 50 &\\ c(5113) & 655$	Saspla	Depth	1-Cu	AS-Eu	
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4C15135 636.05 \sim 633.55 0.01 0.01 0.01 4C16136 638.55 \sim 637.35 0.01 0.01 0.01 4C16137 637.05 \sim 637.35 0.01 0.01 0.01 4C16137 637.05 \sim 638.05 0.01 0.01 0.01 4C16137 637.05 \sim 638.05 0.01 0.01 0.02 4C16117 638.05 \sim 638.05 0.01 0.01 0.02 4C16111 639.05 \sim 639.05 0.01 0.02 0.02 4C16111 640.05 \sim 647.55 0.01 0.02 0.02 4C16111 640.55 \sim 641.05 0.01 0.02 0.02 4C16116 640.55 \sim 641.25 0.01 0.02 0.01 0.02 4C16115 641.05 \sim 642.35 0.01 0.01 0.02 0.01 0.02 4C16116 642.75 \sim 642.35 0.02 0.01 0.02 0.01 0.02 0.01 0.02 0.01 <					
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$\begin{array}{cccccccccccccccccccccccccccccccccccc$			0.08	<0.01	50,0
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#CI5151 658,20 ~ 658,70 <3.01 <3.01 <0.01					
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Fidth	Depth	1-Cu	AS-Cu	T-Ca
(1)	(1)	(3)	(1)	(1)
1955.82	654.35 ~ 655.30	1.71	<0.01	0,05
1.45	555,30 ~ 658,70	0.43	<0.01	9,97

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<u>MJZC-12</u>

Sample	Depth	T-Cu	AS-Cu	T-Co
No.	(n)	(1)	(5)	(1)
KC16153	652.37 ~ 652.87	<0.01	(0.01	<0.01
KC16154	652.87 ~ 653.37	<0.01	<0.01	<0.01
KC16155	653.37 ~ 653.87	<0.01	<0.01	<0.01
KC16156	653.87 🚄 654.37	(0.01	<0.01	<0.01
KC16157	654.37 🔔 654.87	0.09	<0.01	<0.01
KC16158	654.87 🔔 655.17	<0.01	<0.01	<0.01
KC15159	655.17 ~ 655.67	<0.01	<0.01	<0.01
KC16160	655.67 🔔 656.17	<0.01	<0.01	<0.01
KC16161	656.17 _ 656.67	<0.01	<0.01	<0.01
KC16162	656.67 ~ 657.17	<0.01	(0.01	<0.01
XC16163	657.17 ~ 657.67	<0.01	<0.0J ·	(0.01
KC16164	657.67 ~ 658.37	<0.01	<0.01	0.04
KC16165	658.37 _ 658.87	<0.01	<0.01	0.03
KC16166	658.81 ~ 659.37	<0.01	<0.01	0.02
KC16167	659.37 ~ 659.87	<0.01	(0.01	0.01
XC16168	659.87 🔔 660.37	<0.01	(0.01	0.01
KC16169	660.37 ~ 660.87	<0.01	<0.01	0.01
KC16170	660.87 🚙 661.46	<0.01	<0.01	0.04
KC16171	651.45 661.96	1.49	(0.01	0.11
KC16172	661.96 🔔 662.46	0.01	<0.01	0.02
KC16173	662.46 🔔 662.96	0.33	(0.01	0.02
KC16374	662.96 🔔 663.46	0.29	(0.0)	0.01
KC16175	663.46 👡 663.96	0.18	<0.01	0.01
KC16176	663.96 🔔 664.37	0.29	<0.01	0.02
KC18177	654.37 ~ 664.87	0.07	<0.01	0.01
KC16178	664.87 ~ 665.37	0.12	<0.01	0.02
KC16179	665.37 ~ 665.87	0.18	<0.01	0.02
KC15180	665. 87 ~ 666. 37	0.12	<0.01	0.01
KC16181	666.37 💪 666.87	0.14	<0.01	0.01
KC16182	666 87 🔔 667.37	0.13	<0.01	0.01
KC16183	667. 37. ~ 667. 87	0.29	<0.01	0.01
XC16184	667.87 _ 668.37	0.03	<0.01	0.02
KC16185	658.37 ~ 658.87	0.28	<0.01	0.01
KC16186	668 87 👡 669 14	0.34	(0.01	0.02
KC16187	669.14 🚙 669,64	1,19	<0.01	0.03
KC16188	669-64 ~ 670.14	0.54	<0.01	0.01
KC16189	670.14 👡 670.45	0.50	<0.01	0.02
KC16190	670.45 ~ 670.95	0.65	<0.01	0.03
KC36191	670.95 ~ 671.45	0.65	<0.01	0.01
XC16192	671.45 ~ 671.95	0.85	<0.01	0.01
KC16193	671.95 ~ 672.24	0.98	(0.01	0.02
KC16194	672.24 ~ 672.74	2.85	(0.01	0.02
KC16195	672.74 ~ 673.24	1.30	(0.01	0.02
KC16198	613.24 , ~ , 613.74	2.68	(0.01	0.10
KC16197	673.74 🚄 674.14	0.45	(0.01	0.02
XC16198	674.14 ~ 674.64	0 01	(0.01	<0.01
KC16199	674.64 ~ 675.14	<0.01	<0.01	<0.01

Sample	Depth	T-Cu	AS-Cu	T-Co
No.	(a)	(5)	(5)	(8)
KC16200	675.14 _ 675.64	<0.01	<0.01	<0.01
KC+2201	675.64 🔔 676.14	<0.01	<0.01	(0.01
KC12202	676.14 ~ 676.46	<0.01	<0.01	<0.01
KC12203	676.45 ~ 676.95	<0.01	<0.01	<0.01
KG12204	676.95 ~ 677.46	<0.01	<0 01	<0.01
K612205	677.45 ~ 677.96	<0.01	<0.01	(0.01
KC12208	617.96 ~ 678.16	(0.01	<0.01	<0.01

Width	Pepth	1-Cu	AS-CU	1-00
(a)	(1)	(3)	(\$)	(1)
3.10	669.14 ~ 672.24	0.77	<0.01	0.05
1.50	672.24 ~ 673.74	2.28	<0.01	0.05

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Chapter 5 Comprehensive Analysis of the Survey Result

5-1 Geologic Structure, Characteristics of Mineralization and Mineralization Control

5-1-1 Zambian Copperbelt

The mineral deposits of the Zambian Copperbelt occur along two NW-SE trending linear zones, namely one along the western limb of the Kafue Anticline and the other along the Mufulira Syncline, as shown in Figure 1-2. The deposits occur in this belt which continues for several hundred kilometers and extend The mineralized zone of the Chambishi Southeast into Zaire. area occurs in the zone along the western flank of the Kafue In the Zambian side, most of the copper Anticline. deposits in the Ore Formation of the Lower Roan Group, occur and arė clearly bounded stratigraphically. The above alignment of the deposits parallel to the Kafue Anticlinal axis is the direction of the strike of the country rock formations which is parallel to the palaeo-coastline at the time of mineralization. The continuation of the individual deposits is several to over ten kilometers in the direction of the above coastline, while that the direction normal to the coast (toward the central in 🕤 part the basin) is shorter, in the order of of several hundred meters to several kilometers.

5-1-2 Ore deposit and country rock

In the Chambishi Southeast area, the orebodies occur in argillites and dolomites, and locally the mineralization also occurs in the Footwall Quartzite. It is inferred from the above that the orebodies were deposited under the shallow marine or laenvironment near the coast during the early stage qoonal of This is the stage which began with marine transgression. the deposition of the conglomerates of the Footwall Formation. The argillites' contain large amount of organic carbon which indicates stagnant reducing environment during mineralization.

Also the sulfide minerals are distributed zonally from the coast outwards as follows; bornite \rightarrow chalcopyrite \rightarrow chalcopyrite-pyrrhotite-pyrite \rightarrow pyrite-pyrrhotite. This indicates that the sea bottom environment, namely the environment for mineralization, gradually became reducing toward the offshore

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(Fleischer et al., 1976).

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5-1-3 Basement and ore deposit

The Northern Area Shoot, the most important ore deposit of area, occurs in the depression of the basement. And the the ore grade is low to barren where basement is inferred to have been high at the time of ore deposition. This inference ig made from distribution of the bloherm and thickness of the Formation. This is considered to be the result Footwall of water. retention of mineralizing fluid, biogenic stagnant formation of reduced sulfur, formation of heavy metal sulfides, and thus favorable environment for the preservation of metallic sulfide in the local depressions of the basement.

It is inferred from the contour map of the upper surface of the basement that: the rise of the basement on the southwestern side of the NW-SE trending depression occur clearly. The Northern Area Shoot occurs in this depression, and it is shown that this depression is closed; the extensive palaeo-basement highs at the time of ore deposition occur in the NW-SE extending basement high on the northwest side of the Northern Area Shoot; almost NE-SW extending local depression occur in the west survey area; the basement high between Northern Area Shoot and Southern Area Shoot extends further southward, and local depression occur in the NE-SW direction between MJZC-11 and MJZC-12.

It should be noted, however, that the present morphology of the upper surface of the basement does not necessarily reflect the conditions at the time of ore deposition. There are two types of basement rise; one which coincides with the palaeobasement highs at the time of ore deposition and the other risen by folding after the deposition of the Ore Shale. Parts of the palaeo-basement highs corresponds to the present depresand the limbs of the depressions. In some parts of sions the ore horizon, dolomite overlaps with the ore-bearing argillites, and thus it is inferred that the depth of the sea changed by vertical movement of the basement after the start of ore the deposition.

5-1-4 Diagenesis, metamorphism and mineralization

The mode of occurrence of the ore shoots suggests that dia-

genesis and metamorphism played important roles in their formation. Although of a different type, the importance of diagenesis for the formation of Kuroko deposits which deposited on the floor in Neogene Tertiary has been reported (Sugawara et sea al., 1982). Water escape structure (Lowe et al., 1974) similar to those in the sulfides of the Kuroko ores is observed in the ores of the present area, and it is certain that the proto-ore consisting of minute sulfide grains migrated during the dehydration caused by compaction after deposition. Also the geometamorphosed, logic units of this area have been regionally and the primary rocks and minerals have all been recrystallized.

5-1-5 Gravity anomalies, ore deposit and gabbro (amphibolite)

The gravity high and low zones extracted from the gravity contour maps, and the gabbro distribution and fold axes extracted from geological map are shown in Figure 1-12.

The gravity highs near the Chambishi mine coincide well with the distribution of gabbro, and those in the western and southparts of the survey area coincide with the anticlinal western There are small-scale gravity highs corresponding to the axes. basement high in the central part of the survey area, but gabbro also occur in this part. The gravity high on the northern side of the Northern Area Shoot occurs in the basement depression. Ore shoot does not occur in the gravity high, and the northern boundary of the Northern Area Shoot coincides very well with the southern boundary of the gravity high to the north. From the above, it is inferred that: Parts of the gravihighs indicate the occurrence of gabbro in the shallow tv Parts of the gravity highs indicate the subsurface zones. basement highs either formed by folding or palaeo-basement highs which existed before ore deposition. Some kind of relationship possibly exists between the distribution of gravity highs and ore shoots.

An isopach map of subsurface gabbroic bodies (accumulative thickness when there are some bodies) prepared from drilling data and the spatial relation of the gravity highs and the ore shoots are shown in Figure 1-13. It is seen from this map that: the gravity high on the northern side of the Northern Area Shoot coincides very well with the thick part of the gabbroic body; the small-scale gravity highs lying between the Northern Area Shoot and the Southern Area Shoot do not correspond to thick gabbro, but to the basement high; the ore shoots are developed where the gabbroic bodies are thin with the exception of the eastern part of the Southern Area Shoot. The genetic relation between gabbro and ore shoots is not necessarily clear, but the following is a possibility.

The most probable reason for the lack of association of ore shoots and thick gabbroic bodies is that the heavy load of the abbroic bodies caused the ore material to migrate to parts This migration is inferred to have with lower load. been greater in zones where the hard compact basement rocks were shallow. The eastern part of the Southern Area Shoot-I remains below gabbro, and this is probably because the basement was at this point. The Southern Area Shoot-I deep may indicate ore shoots can be formed where the gabbroic bodies that are relatively thin by the above mechanism.

There are two theories regarding the genesis of the gabbroic bodies of this area; namely magmatic intrusion and metamorphic The former genesis is widely believed, but the latter origin. cannot be totally discarded (Mendelsohn, 1961). The basis for the metamorphic origin is that; the chemical composition of the mixture of dolomite and argillite is similar to that of gabbro, the gain-size and texture of the gabbro changes irregularly and the gabbro gradually changes to dolomite, typical abruptly, skarn minerals do not occur in the vicinity of gabbroic bodies, amphibolite formed from pelitic dolomite is similar to that formed by alteration of mafic rocks. Also if gabbroic bodies are of intruded magma origin, the following hydrothermal activities and metamorphism are considered to have took part in the migration of ore materials. However, the orebodies would have solidified by then, and so the mechanism of migration been is difficult to envisage. If the gabbroic bodies are of metamorphic origin, as the distance between the dolomitic rocks and the orebodies is in the order of 500 m, it is considered that the orebodies were still in the stage of diagenesis, and horizontal movement could have been caused by the load of the dolomitic units. The age of the rocks of this area is very old, and it is difficult to clarify the relation between diagenetic, metamorphic, and igneous activities from the recrystallized units.

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5-2 Mineral Potential

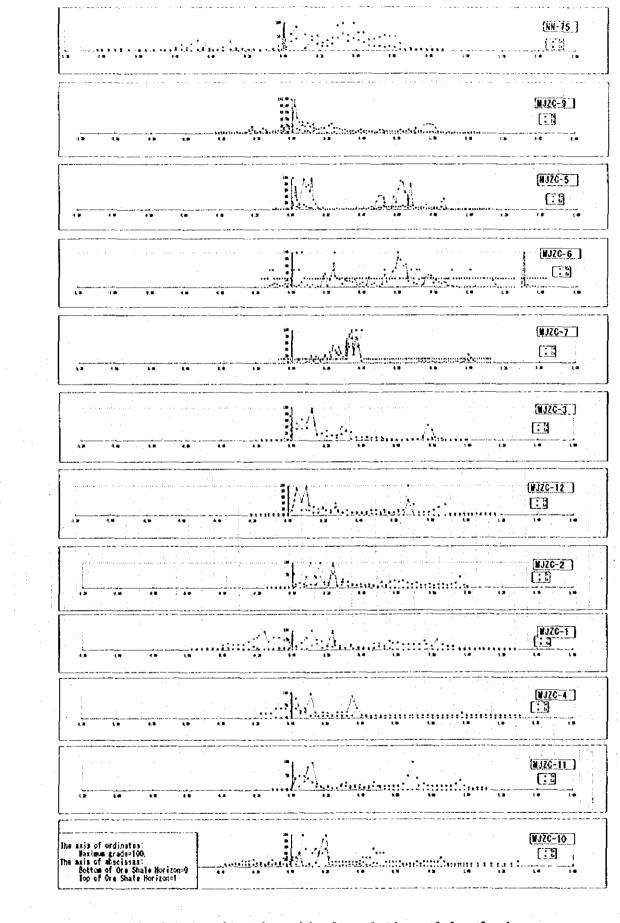
Zones of high potential for shale-type copper mineralization are in the limbs of palaeo-basement highs at the time of ore deposition, particularly in the local depressions parallel to the palaeo-coast lines. Also ore shoots were not formed where thick gabbroic bodies occur and in gravity highs in this area.

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It is seen from the results of the surveys carried out that the palaeo-basement highs at the time of ore deposition were distributed to the southeast, north, and northwest of the Northern Area Shoot. Of the above zones, based on the confirmation of ores in boreholes MJZC-9 and NN-75, the occurrence of ore shoots of significant scale was anticipated in the limbs of northwestern basement high. However, zones to the norththe west, north, and east of this ore shoot are considered to be in the vicinity of a palaeo-basement high at the time of the ore deposition, and also the deposits to the southeast of this ore is inferred to consist of low-grade pyrrhotite-pyrite shoot is difficult to envisage the development of large it ores, scale high-grade ore deposits in these parts of the survey On the other hand, the zones to the south and west of area. are not yet explored and do not contain high gravity MJZC-9 anomalies and are in the general direction of the extension of this ore shoot, therefore it is inferred that these zones would have high mineral potential.

The five boreholes drilled in the southern limb of the basement high to the southeast of the Northern Area Shoot are located at a relative basement high and most of the mineralization in the area belong to the pyrrhotite-pyrite-chalcopyrite zone and have low copper grade. Although of small scale, bornite zone was located in the lowest part of however, "Ore and chalcopyrite zone in the footwall guartzite. Shale" The occurrence of shoots are confined to the lowest part of the "Ore Shale" and its vicinity in this area and thus it is inferred that the period of copper precipitation was probably relatively short and thus it is possible that the ore deposits could not grow very large. If there were, however, deep local depressions of the sea floor at the time of ore deposition, it also would be possible to have formed relatively large ore shoots regardless of the length of precipitating time. From the above, the local basement depression inferred to exist to the south-southwest of MJZC-2 which confirmed relatively high-grade



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Fig. 2-5-1 Stratigraphic Correlation of Ore Grade - 147 -

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Table 2-5-2 Stratigraphic Correlation of Mineralization

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Drill Hole No.	MJZC-1	MJZC-4	MJZC-2	MJZC-4 MJZC-2 MJZC-3 MJZC-5 MJZC-6 MJZC-7	MJZC-5	MJZC-6	MJZC-7	MJZC-9	MJZC-9 MJZC-10 MJZC-11 MJZC-12	NJZC-11	NJZC-12	NN-75	
LOS Depth-Top (m)	504.1	919.4	638.2	632.4	967	969.5	923.8	1079.5	961.3	637.2	655.4	953.9	
LOS Depth-Bottom (m)	520.9	937.4	658.6		1005.1	1002.9	963.5	1112.2	987.4	656.6	674.1	971.35	
(m) bW SOL	16.8	18	20.4	17.3	38.1	33.4	39.7	32.7	26.1	19.4	18.7	17.45	17.45 0.13377
() Y-I SOT	85	86	2	85	45	58	45	60	82	8	8	70	
LOS True-Wd (m)	16.7	17.9	19.4	17.2	26.9	28.3	28.1	28.31	26.0	19.31	18.4	16.4	
Top-Cu Min(t-Cu>0.1%) *	0.567	0.403	0.562	0.795.	0.864	0.896	1.033	1.000	0.489	0.559	0.675	0.755	0.755 0.42017
Bottom-Cu Min *	-0.573	-0.032	0.004	-0.008	6 .18	-0.133	0.002	-0.292	-0.389	0.005	-0.002	-0.891	-0.6761
Cu Min. Range *	1.130	0.4351	0.558	0.803	0.960	1.029	1.031	1.292	0.878	0.554	0.677	1.646	1.646 0.80685
Cu m% of Cu Min *	5.124	1.462	10.658	6.751	21.051	11.950	12.172	34,517	6.421	4.562	8.029	31.651	31.651 0.98297
Co m% of Cu Min *	0.365	0.0861	0.667	0.768	0.759	0.223	0.293	1.201		0.280	0.294	1.216	1.216 0.90129
Top-Co.Min(t-Co>0.01%) -	0.914	0.078	0,995	0.847	0.838	0.717	0.397	1.031	0.869	1 085	0.878	0.870	0.870 0.19937
Bottom-Co Min *	-0.424	-0.196	0.00	-0.058	0.015	-0.133	0.304	-0.445	90.09	0.005	-0.002	-1.077	-0.7843
Co Min. Range -	1.338	0.274	0.991	0.905	0.853	0.850	0.093	1.476	0.875	1.080	0.880	1.947	1.947 0.70006
Top Depth-Cu Shoot (m)			653.83	647.73	32-626	981.40	948.45	1085.68		654.35	672.24	960.66	960.66 0.56189
LOS Upper Than Top Cu-Shoot (m) -			15.63	15.33	12.55	11.90	24.65	6.18	20.90	17,15	16.84	6.76	6.76 -0.7886
Top-Cu Shoot(t-Cu>1%) *			0.233	0.113	0.670	0.643	0.379	0.811	0.199	0.115	0.099	0.641	0.641 0.78499
Bottom-Cu Shoot *	····		0.079	-0.008	0.009	0.567	0.304	-0.177	0.160	0.0671	0.019	-0.593	-0.746
Total Cu m%-Cu Shoot *	0000	0.00	6.940	3.243	16.312	3.251	5.314	25.600	1.645	1.622	3.420	26.659	
Total Com%-Cu Shoot	0.00	0.00	0.377	0.384	0.345		0.071	0.509	0.035	0.047	0.070	1.070	1.070 0.84154
Max Cu-Peak *	0.232	0.108	0.233	0.113	0.112	0.598	0.363	0.013	0.199	0.115	0.099	0.000	-0.5345
(Shoot/Min: Cu-m%)*100 (%) *	õ	ō	8	8 1	4	27	44	74	26	36	\$	84	0.88137
(Co/Cu: Cu Min-m%)~100 (%) -	7	Ģ	9		4	5	8	3	5	ę	4	4	-0.2918
(Co/Cu: Cu Shoot-m%)*100 (%) *			5	12	2	1	1 1	-2	2	e	7	4	-0.1072
ABS/Top Co-Top Cu) •	0.357	0.325	0.433	0.052	0.026	0.179	0.636	80	0.38	0.526	0.203	0.115	-0.5491

LOS: Ore Shale Horizon 1-A: Intersection angle Min: Mineralized zone ABS: Absolute value

m%. Metai content r. a correlation coefficient with Cu content of Cu ore shoot

* : Number shows stratigraphic position in the case where bottom of LOS is 0 and top of LOS is 1.

copper is noteworthy. Presence of bornite was confirmed at MJZC-12 and the occurrence of palaeo-basement high near this borehole became a possibility. The occurrence of an anticlinal axis extending in approximately north-south direction is anticipated to the south of MJZC-12, and the basement high of this area is inferred to extend further southward. Therefore, the palaeo-basement highs are distributed in relatively shallow seas to the south of MJZC-12 and the occurrence of ore shoots of the chalcopyrite zone is a possibility.

The stratigraphic positions of geologic characteristics relevant to mineralization were extracted from the cores drilled during the present survey and NN-75. The thickness of the "Ore Shale Horizon" (LOS) of each hole were used as standard with minimum LOS as 0 and Maximum LOS as 1 (Fig. 2-5-1, Table 2-5-2).

The geologic characteristics relevant to mineralization are interpreted from the above drill cores and shown in Table 2-5-2. Of these, those common to the cores with high-grade ore shoots (NN-75, MJZC-9) are as follows.

- 1) Copper and cobalt mineralization started early.
- 2) Stratigraphic range of Copper and cobalt mineralization is wide.
- 3) Copper and cobalt contents (m x %) of the whole copper mineralized zones are relatively high.
- 4) The top of the ore shoots (T-Cu>1%) is stratigraphically high.
- 5) The bottom of the ore shoots (T-Cu>1%) is stratigraphically low.
- 6) Cobalt content (m x %) of the copper ore shoots is relatively high.
- 7) Highest copper grade occurs near the minimum LOS.
- 8) The metal content (m x %) of the ore shoots occupies a relatively large part of the total metal content (m x %) of the whole copper mineralized zone.
- 9) The upper limits of Cu and Co mineralizations are relatively close.

We believe that when many of the above characteristics are strongly observed, the vicinity of such boreholes would be worth exploring even when the site itself is low grade. Based on the above line of thinking, the vicinity of MJZC-3 and -6 would be most promising followed by MJZC-1, -2, -7, and -12. R

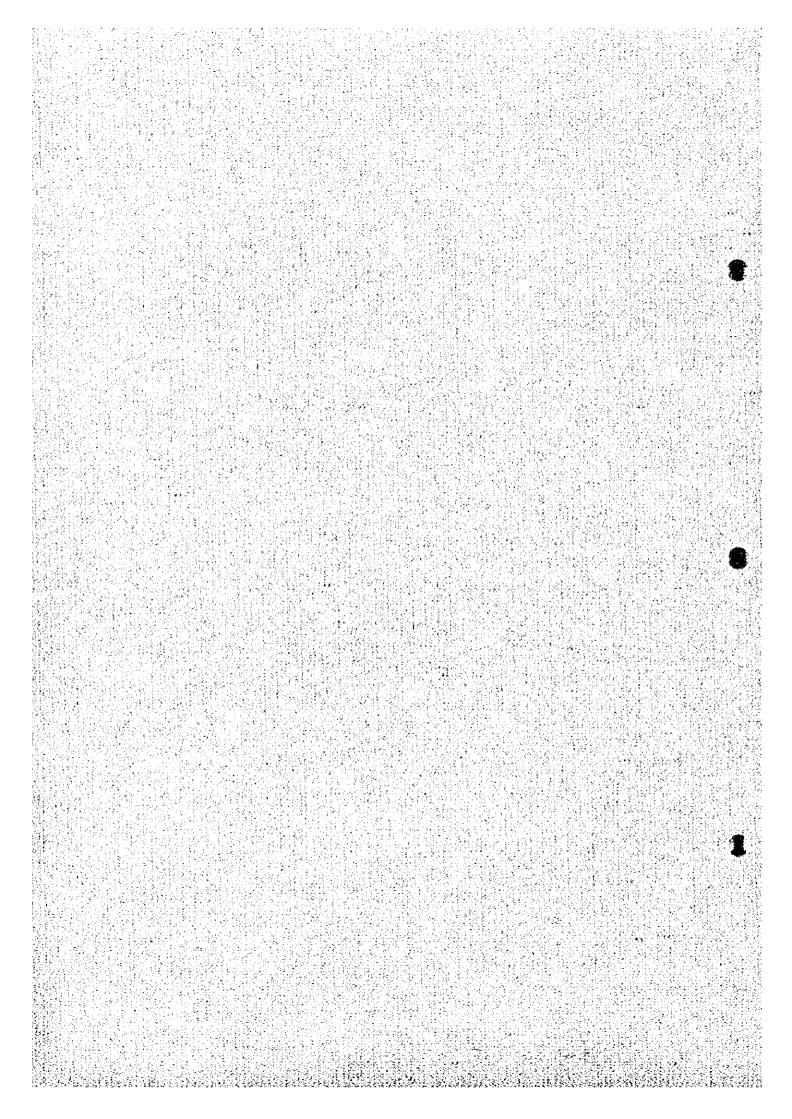
These drill site have considerable significance, and in particular MJZC-2, -3, -7 and -12 confirmed the local existence of high-grade ore (T-Cu>2) and they could have penetrated the edge of ore shoots although the mineralized zones are thin.

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PART III CONCLUSIONS AND RECOMMENDATIONS



PART III Conclusions and Recommendations

CHAPTER 1 Conclusions

During the course of the three year period of Fiscal 1993 to 1995 of the Chambishi Southeast area mineral exploration, drilling, and compilation and interpretation of existing data were carried out with the following conclusions.

1. All twelve boreholes drilled during this survey attained their objectives by penetrating the ore horizon. The nine boreholes reached the basement. The geology and mineralization of the survey area were thus clarified.

2. MJZC-9 drilled in the western part of the area confirmed the existence of high-grade ores (i. width 5.90m, grade T-Cu 3.12%, T-Co 0.08%; 11. width 2.58m, grade T-Cu 2.29%, T-Co <0.01%). These ores are considered to be continuous to the shoot confirmed to the north of this hole (NN-75). Thus it is now clear that ore shoot of considerable scale exists in this area. It inferred that this ore shoot is emplaced over a basement 18 depression which is elongated in the NE-SW direction and it is deemed possible that this shoot is developed further southward or westward.

3. The known areal extent of the Northern Area Shoot, which is the most important ore deposit of this area, expanded northwestward by the confirmation of ores by MJZC-5 (i. width 3.10m, grade T-Cu 1.93%, T-Co 0.03%; ii. width 2.64m, grade T-Cu 2.32%, T-Co 0.03%), while it shrank in the western and southeastern parts by the confirmation of low-grade ores of MJZC-4 and barren zone of MJZC-8.

4. The five boreholes drilled in the southern part of this area (MJZC-2, -3, -11, -12) were located in relatively raised basement areas, and they showed that many of the mineralized zones consisted of low-grade copper ores belonging to the pyrrhotitepyrite-chalcopyrite zone. But in some parts, small bornite lowermost part of the "Ore Shale" (MJZC-12), zone in the chalcopyrite zone in the footwall quartzite (MJZC-1), and local high-grade copper of pyrrhotite-pyrite-chalcopyrite zone (MJZC-2, -3, -12) were confirmed. In this area, the occurrence of ore shoots is limited only to the lowermost part of the "Ore Shale", and thus it is inferred that ore deposition occurred in relatively short period of time, thereby limiting the size of the ore deposits. If, however, deep local depression existed on the seafloor at the time of copper deposition, relatively large ore shoots could have been formed.

It is inferred from distribution of the bioherm and thick-5. Formation that there was a palaeo-baseness of the Footwall ment high at the ore-forming time in this area. The Northern Area Shoot which is the most important deposit of the area in the depressions of the basement. And the grade of occurs the horizon above the palaeo-basement high is low or barren. This is inferred to be the result of the formation of environment favorable for deposition and preservation of sulfides in these submarine depressions by accumulation of heavy-metalbearing dense solutions and formation of reduced biogenic sulfur in the stagnant sea water in these local troughs.

6. In almost all of the boreholes, stratigraphic zonal arrangement of the sulfide minerals is observed in the mineralized zones. The depth of the sea probably increased after the deposition of the "Ore Shale", because the Fe/Cu ratio generally increases upward from near the lowermost part of the "Ore Shale Most of the ore shoots in this zone belong to the Horizon". chalcopyrite zone, but the high cobalt zones exist not only in the chalcopyrite, but also in the pyrrhotite and pyrite zones. It is inferred that the chalcopyrite zone was formed within a sea depth zone. Therefore, we believe that the condinarrow for the formation of copper ore shoots would be; the tions and the continuation of the optimum depth range of the sea, existence of depressions suitable for the deposition and preservation of copper minerals.

7. The mode of occurrence of the rich orebodies indicate that diagenesis and metamorphism played important roles in the formation of ore shoots. Structures similar to water-escape structures of Kuroko (sulfide) deposits occur in these orebodies and the minute grain-sized sulfide proto-ore definitely migrated in conjunction with dehydration during the compaction after deposition.

8. There are two types of present basement highs, namely those which coincide with the palaeo-basement highs and those which were formed by the apparent rise of the basement by folding after the deposition of the ores. Rich ore could occur higher than the top of the latter type highs.

following is inferred from the gravity contour maps, 9. The drilling data. Parts of the high gravigeological maps, and ty anomalies reflect the gabbroic bodies in shallow subsurface Parts of the gravity high anomalies reflect the basezones. ment highs such as the relative rise by folding and palaeobasement highs. High-grade ores most probably do not exist at gravity highs which coincide with thick gabbroic bodies. The relatively thin and low-grade orebodies deposited over the tops and limbs of the palaeo-basement highs may turn out to be rich orebodies under relatively thin gabbroic bodies.

10. Ore reserve estimation was carried out to asses the mineral potential of the survey area with the following results.

POTENTIALLY ECONOMIC MINERALIZATION;

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NORTHERN AREA SHOOT: 54,793,000 tons, 2.70% T-Cu, 0.13% T-Co SOUTHERN AREA SHOOT: 14,934,000 tons, 2.19% T-Cu, 0.13% T-Co SUBECONOMIC MINERALIZATION :

107,909,000 tons, 1.83% T-Cu, 0.03% T-Co

CHAPTER 2 Recommendations for Future Exploration

Significant amounts of ore were confirmed in this survey area by drilling during this year. The ore deposits of this area, however, occur in relatively deep zones, the major deposits probably occurs at 550 to 1,050m below the surface. Therefore, in order to develop this deposit, it is necessary to further increase the ore reserves. The western and southern parts of the survey area have not been explored and the potential is considered to be promising.

It is now clear, from the results of the present survey, that a deposit which was hitherto unknown occurs in the western part of the area. Also borehole RCB-2 which previously confirmed ores is located far south of MJZC-9 which also confirmed ores. From the above it is strongly recommended that efforts be concentrated as follows to confirming new ore reserves and to exploring the vicinity.

First drill at sites where the depth of the ore deposits can be estimated at shallow depths, namely near the two boreholes which encountered ores (MJZC-9, NN-75), then drill at sites where the depth of the ore is considered to become deeper, namely south and west of MJZC-9.

The possibility of ore shoots still remain in the southern part of the area and thus it is recommended that drilling be carried out in the area to the south of MJZC-12.

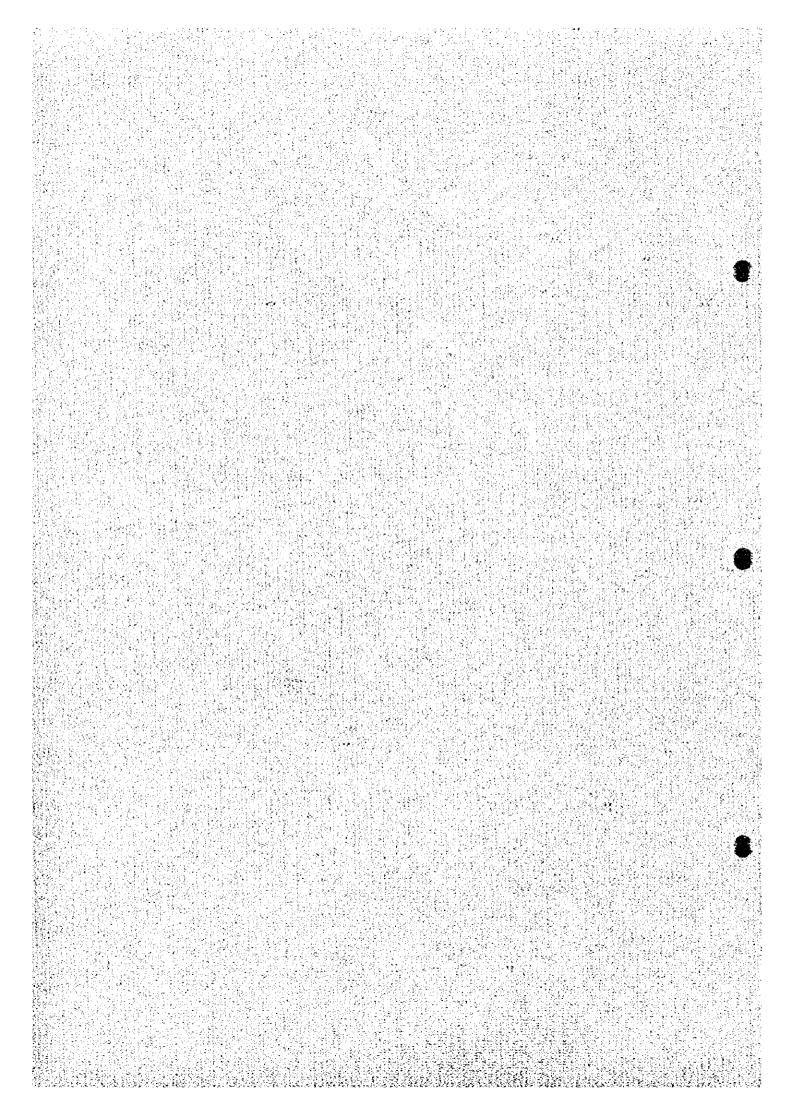
Also in order to accurately determine the ore reserves of the Northern Area Shoot, the main deposit, drilling should be carried out near the peripheries of the deposit.

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