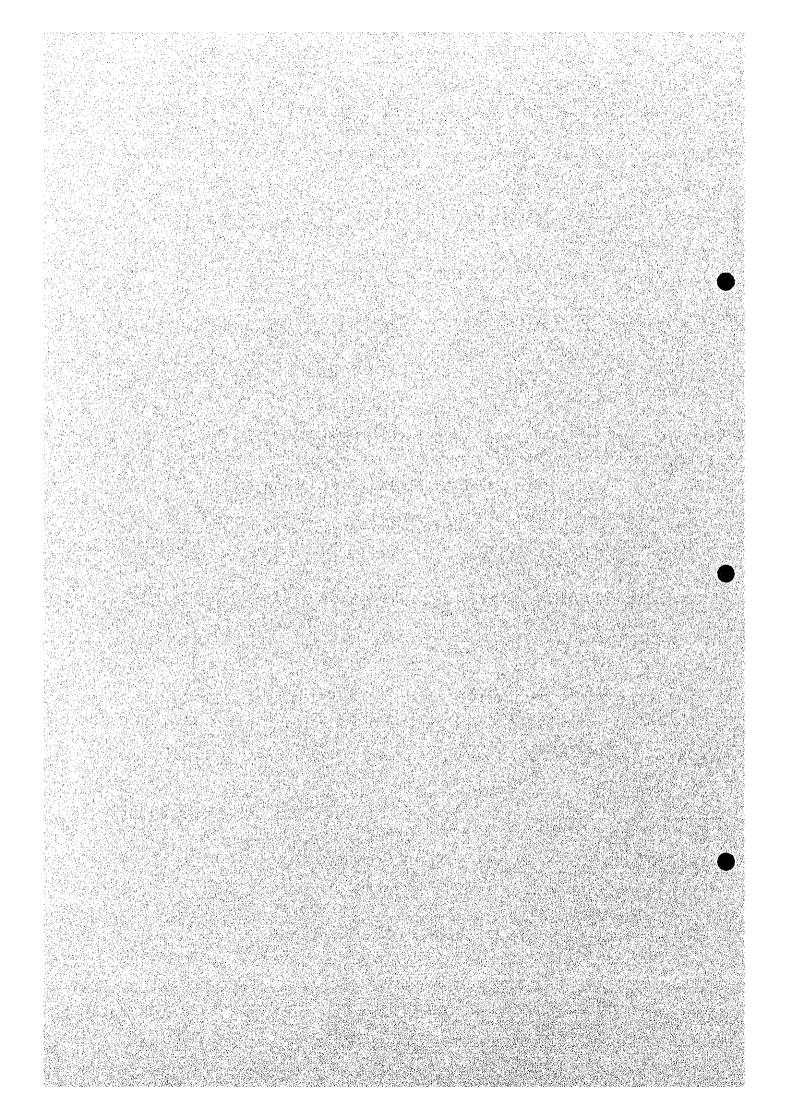
CHAPTER 9

FEASIBILITY DESIGN



CHAPTER 9 FEASIBILITY DESIGN

9.1 General

The feasibility design is to be carried out for the purpose of efficiently realizing formation of the power supply facilities to the densely populated areas in accordance with the short and long term distribution system improvement and expansion plan described in CHAPTER 6. In other words, this feasibility design shall be carried out according to the following standards and criteria of MEA primarily for selecting the overhead and underground transmission line routes as well as the substation sites so as to match the local situations while reflecting the results of the first and second site survey, and those of detailed survey of the model districts carried out simultaneously. Meanwhile, any advanced equipment shall designed according to the relevant international standards (ISO):

er de geleg en de en la en de la de la la en la en

- Basic Criteria for Power System Planning
- Overhead Subtransmission Construction Standards

han moved electric and salt the fergine of a field

- Underground (Transmission Line/Cable) Construction Standards

Before discussing on the feasibility design of the respective equipment and facilities, let us first of all describe herein on the results of studying the transformer capacity of distribution substations, voltage of related transmission and distribution systems and size of distribution line conductor in the model zones and surrounding areas.

t a mai the seas and the acceptance with a season of the season of the season of the season of the season of t The season of the

rdigadis dans propries revinces anno esta di transcriptorio populari di sistema del propio di sistema del sist Indistrutorio della consistema di constituta propio del constituto di sistema della constituta di sistema del Baltandonio della sistema di sistema di sistema della constituta di sistema di sistema di sistema di sistema d

AND MARKET THE REPORT OF THE ARCHITECTURE AT THE RESIDENCE

9.2 Selection of Model Districts

The model districts of which detailed feasibility studies are to be carried out have been selected through the discussions between MEA and the Study Team, bearing in mind the large-scale demand areas in the center of cities and taking into account the industrial and geographical elements as follows:

- Sathorn Area (high load density area)
- Phahol Yothin Area (commercial area)
- Jomthong Area (industrial area)

(1) Feature of the model districts

(a) Sathorn Area: The straightful repeated last matter the engine of feater grant and or

This area is located in the southeastern part of the city center near by Silom street, one of the most busy streets, as is shown in Fig. 9.2-1(a). There are many high-rise buildings in the district and also buildings under construction on both sides of the Sathorn street. The load demand tends to increase rapidly.

Note that the second of the

(b) Phahol Yothin Area while the restriction of an interpretation of the control of the control

This area is located in the northern part of the Victory Monument, as is shown in Fig. 9.2-1(b). There are many commercial and business high-rise buildings adjacent to commercial and residential areas and some buildings under construction on both sides of the Phahol Yothin street. This street is also expected to install the outgoing subtransmission lines from new Sanampao T/S

(c) Jomthong Area

This area is located in the western part of the Chao Phraya River and along with Klong Daokhanong River, as is shown in Fig. 9.2-1(c). This area has been prospering as a small industry area. There are many small industry shops on both sides of the street and narrow area. Electric power for this area has been supplied from Klongwatsing and Taksin distribution substations. As MEA plan to install new distribution substation in this area, they are now seeking the land for the substation.

(2) Load forecast of each district Load densities of each district are listed below, based on the results of load forecast by MEA.

	FY 1993	FY		FY	2006
Area	MVA/km²	MVA/km²	aa i (%)	MVA/km²	aa 1 (%)
(a) Sathorn	25.11	44.86	7.5	55.39	4.3
(b) Phahol Yoth	in 7.36	16.03	10.2	21.30	5.8
(c) Jomthong	6.42	15.11	11.3	20.73	6.5

(3) Load demand for buildings

The load demand for each high-rise building located in Sathorn and Phahol Yothin Area are as shown in the table below:

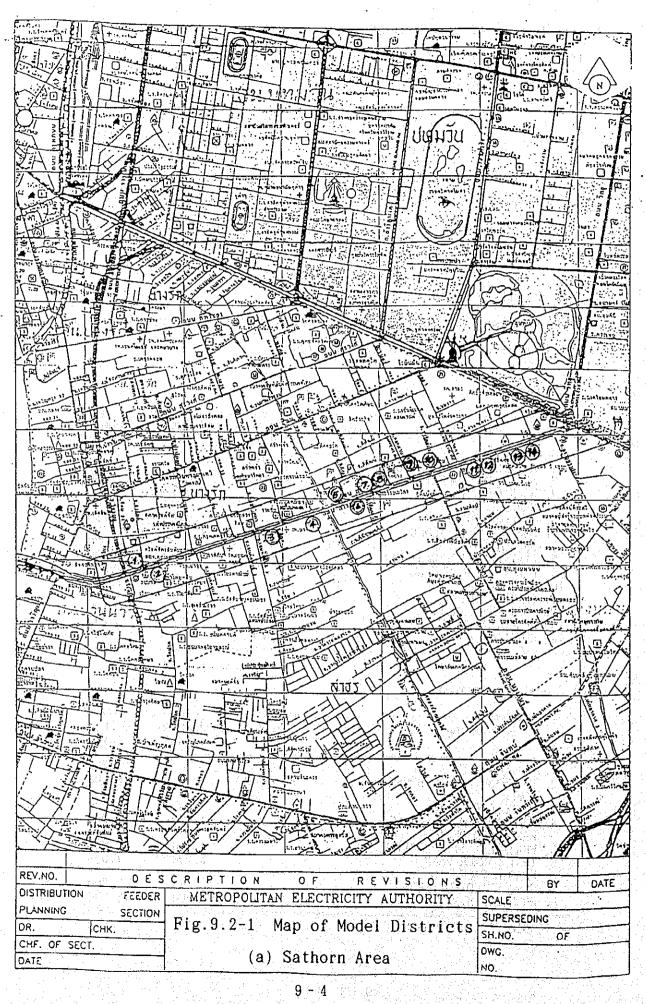
(a) Sathorn Area

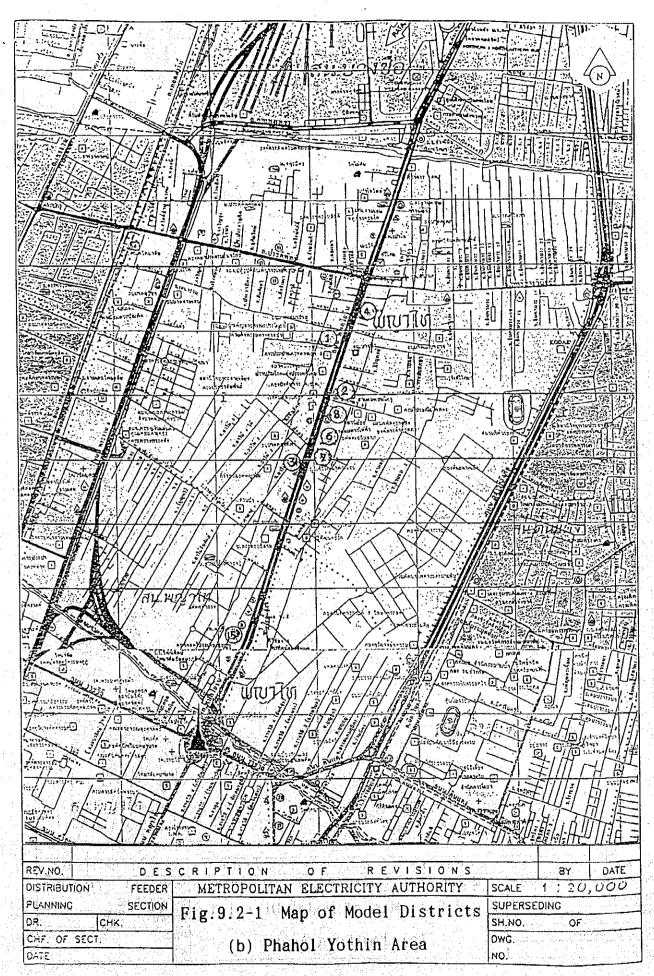
Building	Storey	Area (m²)	Load Demand (kVA)	Connect (kVA)
1. ATM INTERNATION		40,749	900	7,250
2. SRI-SIAM PROPER 3. BANK OF ASIA	ТҮ 33	73, 169	862 2,000	8,900
4. RAJANAKARN	32		1,847	9,600 4,050
5. SATHORN THANI 6. SATHORN CITY TO	WER 31	50,000	2,382	10,400
7. SAENGTHONG THAN 8. EVERGREEN INTER			899	8,000 3,000
9. BNH MEDICAL CEN	TRE 12	27, 215	2,632	4,000 7,200
10. HARINTHORN 11. CENTRAL INTER	20 _		440	4,000
12. THAIVA TOWER II 13. SUKHOTHAI HOTEL	1 A 1 A 1 A 1 A 1 A 1 A 1 A 1 A 1 A 1 A		1,467	10,500 3,200
14. ROYAL SATHORN	19	20,000		4,200

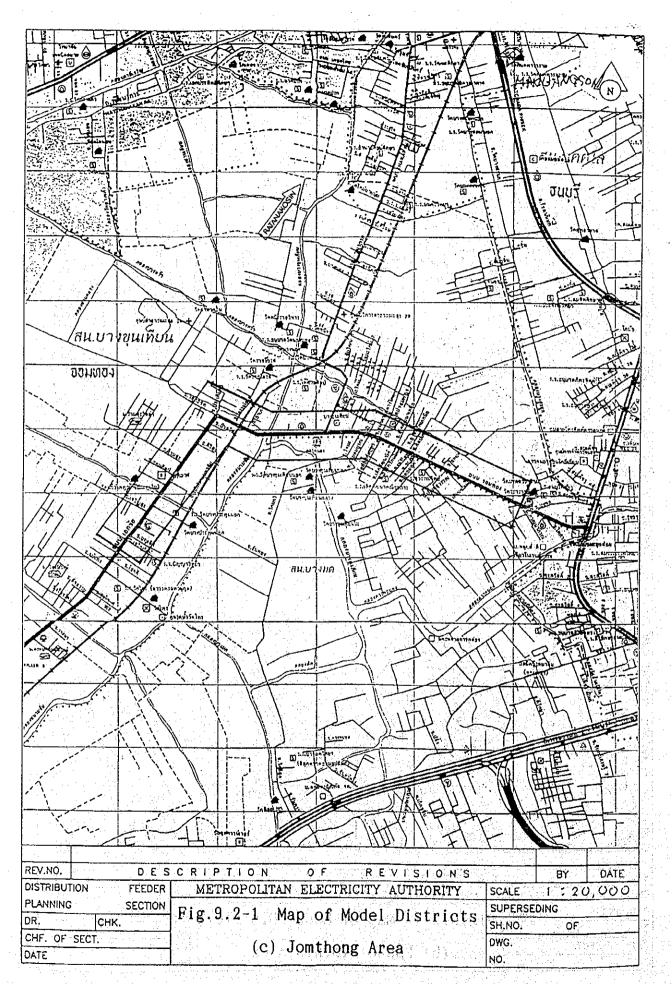
(b) Phahol Yothin Area

	Building	Storey Area	Load Demand (kVA)	Connect (kVA)
1. 2.	MAISON MANEEYA BANCHANG LAND & HOUSE	_ - 1¹/₄ Rai		2,500 6,000
3. 4.	TOWER BONPONG BUILDING THE GOVERNMENT SAVING		2,000 1,400	3,200 2,000
5. 6.	BANK HEAD OFFICE PHAYATHAI II, HOSPITAL THAI FARMER BANK,		1,600 5,600	4,000 7,500
7. 8.	HEAD OFFICE S.P. BUILDING (IBM) PHAHOLYATHIN		900	7,200 13,200

Note: * 400Rai=650ha







9.3 Study of Model Districts

9.3.1 Study of Distribution System and Capacity of Distribution Substation in the Model Districts

For executing detailed feasibility design, the following model districts have been selected as described in Section 9.2.

- · Sathorn zone (High density commercial area)
- · Paphol Yothin zone (Commercial area)
- · Jomthong zone (Industrial area)

With regard to these model districts, subtransmission lines and distribution substations in the surrounding areas, optimum systems of distribution system and distribution substation are studied on the basis of the following items as parameters:

Substation capacity

• Case 1 : 3×40 MVA

• Case 2 : 4×40 MVA

• Case 3 : 3×60 MVA

• Case 4 : 3×80 MVA

(1) Prerequisite conditions of distribution substation

The respective cases of expansion plans are formulated by optimum system study, based on the following prerequisite conditions:

and an office manager of the Alexandria

- (a) The power demand in the model districts and surrounding areas are studied based on the power demand obtained in Section 6.3.
- (b) The distribution voltage, size of distribution conductor and number of distribution lines per one bank are all based on the same conditions as those described below in the respective cases because of the following reasons:

Namely, when the portions of feeders downstream of substation transformer are studied based on individual parameters, then the parameters become too many and complex to promote further study.

The distribution voltage, size of distribution conductor and number of distribution lines per one bank subsequent to feeders are studied in Clause 9.3.3.

· Distribution voltage : 24 kV

· Conductor size

: 185 mm²

• Maximum number of distribution conductors per one bank : seven feeders(c) The capacity of substations will be so planned as to become roughly equal in the respective cases.

(d) The extension plan of the substations in the respective cases is formulated based on the planning policy described in Section 6.3.

Meanwhile, the 3×80 MVA configuration is studied for the model districts, an additional bank configuration.

For this purpose, the planning policy for this configuration should also be set in advance similarly as described in Section 6.3.

* At the time of 2-bank configuration of the action persons and a

Normal: 75%,

Emergency: 125%

Switching-over by distribution line: 20 MVA in maximum

Although the load to be switched over by distribution line is 15 MVA in maximum in the case of 60 MVA bank, the load is 20 MVA in the case of 80 MVA.

· At the time of 3-bank configuration

Normal: 80%,

Emergency: 120%

Switching-over by distribution line: None

The level at the time of dissimilar capacity bank configuration at the execution stage of the substation expansion project is studied below.

• At the time of 1 x 80 MVA + 1 x 40 MVA configuration

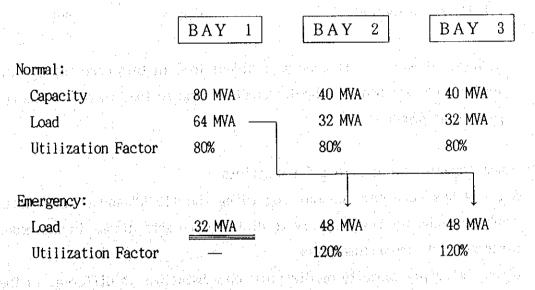
	BAY 1	BAY 2	Makaba Shekabar
	i Karangan belangan belangan dari		
Capacity	80 MVA	40 MVA	
Load A A A A A A	60 MVA	30 MVA	Brog Ha
Utilization Facto	or 75%	75%	
Emergency:		December on A	
Load	40 MVA	50 MVA	aligini.
Utilization Facto	or —	125%	
			Tarrier and the same

In this case, 40 MVA is left over as a residual load. Out of this much load, 20 MVA can be switched over by distribution line, but 20 MVA is left over without being switched over.

Therefore, the substation should be operated by lowering the normal load by 10 MVA.

The normal load and availability factor of the substation at this time, are 70 MVA and 58.3%, respectively.

• At the time of 1 x 80 MVA + 2 x 40 MVA configuration



In this case, 32 MVA is left over as a residual load. Out of this much load, 20 MVA can be switched over by distribution line, but 12 MVA is left over without being switched over.

In this case, therefore, the substation should be operated by lowering the normal load by 12 MVA.

At this time, the normal load and availability factor of the substation are 116 MVA and 72.5%, respectively.

es di all'archi finz vonastrat Tobos e da la confect federal sono

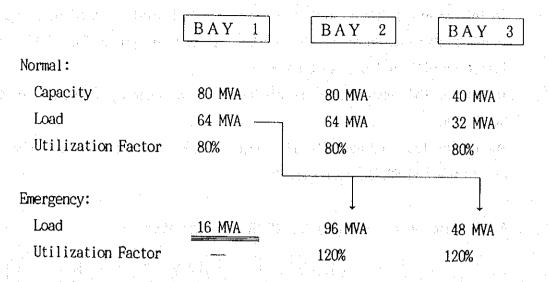
and any military many make the template well and inclinations and it

lighted by by had been ward to distinct of a first could be

a latify class are been trained by the back of the

(digital) to produce the calculation of the control of the calculation of the calculation

• At the time of $2 \times 80 \text{ MVA} + 1 \times 40 \text{ MVA}$



Although 16 MVA is left over as residual load in this case, all of the load can be switched over by distribution line so that there will be no particular problem.

(2) Power distribution plan to model districts

A study has been carried out regarding the 115 kV and 69 kV system configurations for power supply to distribution substations in the model districts and surrounding areas.

Since the supply capacity of distribution substations is different in the respective cases, a policy of system configuration to be applied in all of the respective cases has been studied, and an expansion plan has been formulated based on the policy. The policy of system configuration studied herein is presented in Table 9.3-1.

The expansion plan in the respective cases mentioned above has been formulated on the basis of the subtransmission line expansion plan described in Section 6.4 taking into account effective utilization of the existing systems around the respective model districts and surrounding areas as well as the transmission line expansion plan constituting the basis of this study. Case 3 is almost the same as the base plan in Section 6.4.

The system configurations used in this study are outlined in Fig. 9.3-1.

(3) Advantage and disadvantage of system configurations to be applied

The results of formulating the expansion plans of distribution systems and distribution substations in the respective cases based on the prerequisite conditions mentioned previously are presented in Table 9.3-2(a),(b),(c) and Fig. 9.3-2, and the construction cost therefore in Table 9.3-3(a), (b), (c).

(a) Evaluation of the respective cases

The construction cost in the respective cases is as completed in the tables below. However, the second of the least of the second of the least of the le

The number of substations to be constructed in Case 1 is largest among the respective cases followed by Case 2. Since the modification cost of GIS for adding to four banks is high, the construction cost in the respective model districts is apparently higher in both of the cases than the other cases. He will be the design and the rest of the cases and the second of the cases are the cases and the cases.

The 3 x 60 MVA and 3 x 80 MVA plans with the smallest number of substations to be constructed are advantageous, since the substation construction cost dominates over the other cost when the construction is economically evaluated.

Total Cost and again the property of the control of

1000				
Name of Area	Case 1	Case 2	Case 3	Case 4
Sathorn	1,915.8	1,518.1	1,244.7	1,341.6
Phahol Yothin	1,355.2	1,140.0	1,036.2	923.2
Jomthong	799.4	624.8	473.2	457.1
alassa Total grassassa	4,070.4	3,282.9	2,754.1	2,721.9

ng mang like nga anggang pilipang sikelikali penggan tenggan tenggan pilipang kanalakan penggan penggan pengga

Present Value

(Unit: Million Baht)

Name of Area	Case 1	Case 2	Case 3	Case 4
Sathorn	1,338.7	1,107.0	970.8	978.1
Phahol Yothin	874.7	768.7	743.6	692.9
Jomthong	629.5	505.0	401.6	363.2
Total	2,842.9	2,380.7	2,116.0	2,034.2

(b) Economic comparison of Cases 3 and 4

In Cases 3 and 4, the substation capacity to be expanded in the

respective model districts is roughly equal. However, while the number of substations to be constructed in Case 4 is slightly lower than in Case 3 so that the substation expansion cost of Case 4 is advantageous over Case 3 on one hand, the capacity of transmission lines to be expanded along with expansion of substations in Case 4 is greater than that in Case 3 and therefore disadvantageous over Case 3. The results of study are individually outlined below:

- i) Although the substation expansion cost in the Sathorn area is lower in Case 4 than that in Case 3, the total construction cost is higher in Case 4 than that in Case 3 since the transmission expansion cost is higher in Case 4.
- ii) In the Paphol Yothin area, the substation expansion cost is lower in Case 4, and although the expansion cost of transmission line is slightly increased, the total construction cost is advantageous in Case 4 over Case 3.
- iii) In the Jomthong area, the substation expansion cost in Case 4 is lowered by half that in Case 3, and although the transmission line expansion cost in Case4 is roughly twice that in Case 3, the total construction cost in Case 4 is advantageous over that in Case 3.

As mentioned above, the difference in the total construction cost results from the relationship between the scales of substation and transmission line expansion work in the respective model areas. In other words, the difference in the total construction cost is caused by the extent of the possibility of reusing the existing distribution systems in individual areas.

From this study, it is impossible to indiscriminately evaluate the advantages and disadvantages of the cases of 3 \times 60 MVA and 3 \times 80 MVA because of actual situations inherent to the respective model districts. However, the above two cases are substantially advantageous economically over the other cases of 3 \times 40 MVA and 4 \times 40 MVA, and the extent of this advantage over these cases is roughly equal as conceptionally presented below:

torus experied of the testino half tradebre see Ji Task & Saskitani

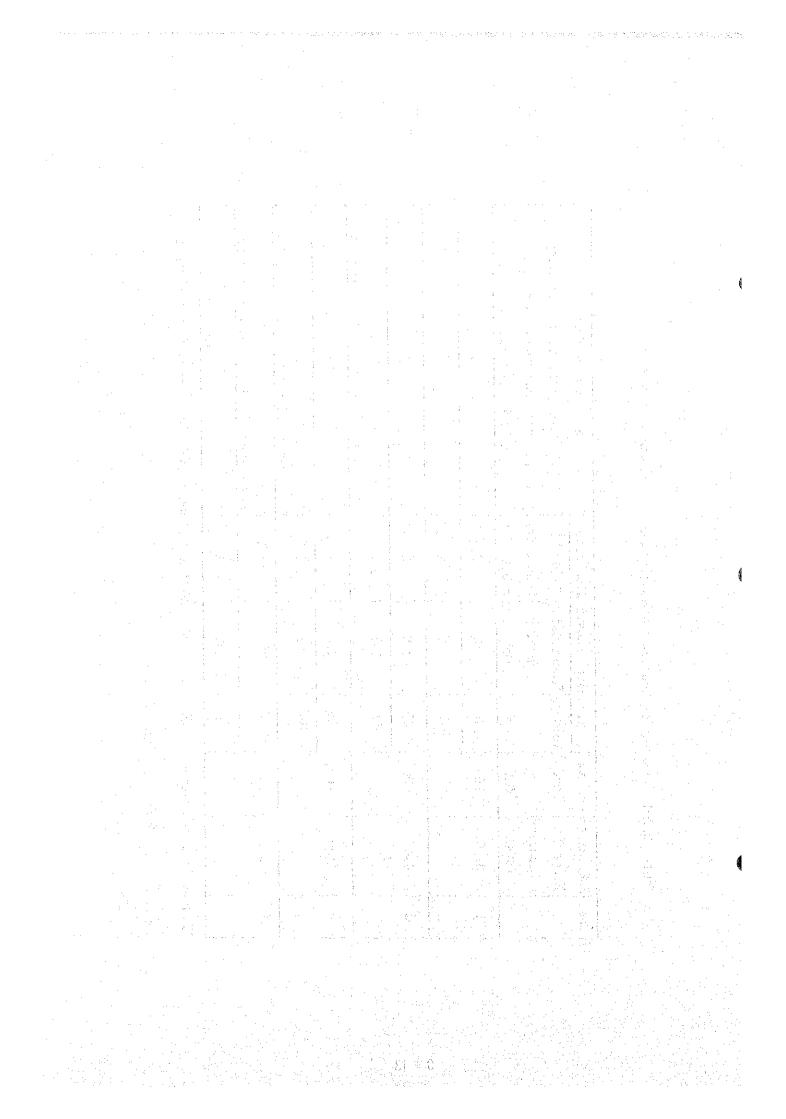
3 imes 40 MVA > 4 imes 40 MVA \gg 3 imes 60 MVA and 3 imes 80 MVA

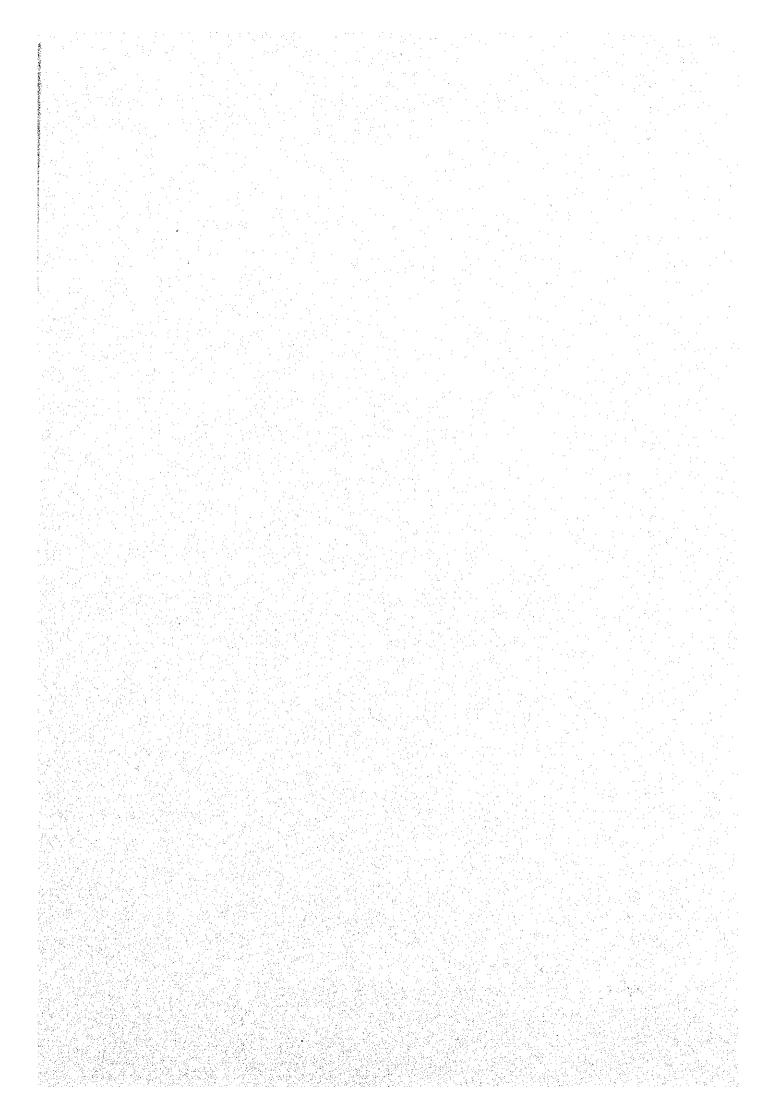
Table 9.3-1 Relation of Substation Capacity and System Configuration

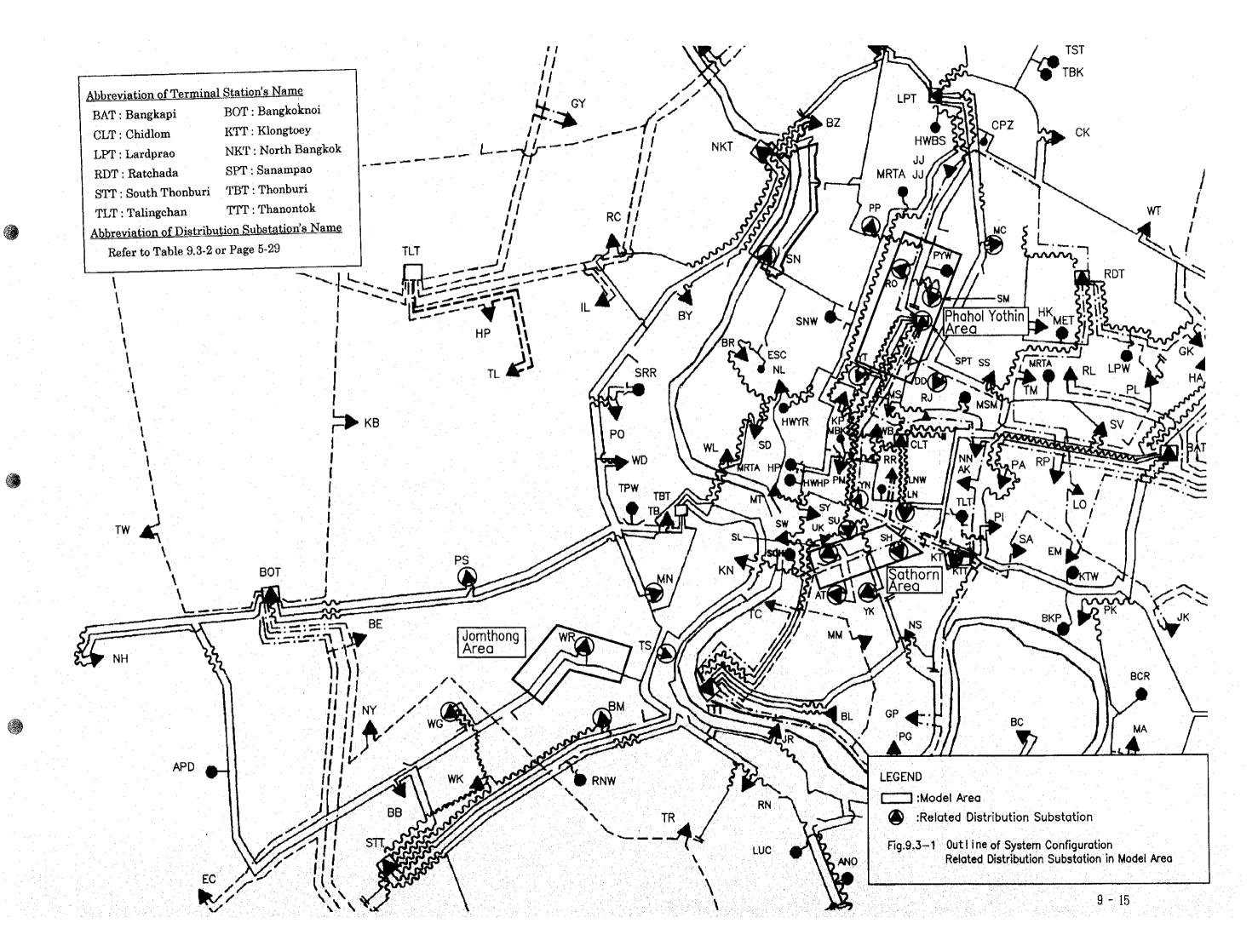
Case	Case Substation Maximum	Maximum	Stand	Standard Transmission Line	sion Line	System configuration
	No. of Tr.	Load	Voltage	Voltage Transmission Allowable	Allowable	: Number of connecting substations
	x Capacity			Capacity	Connecting	in single subtransmission line
	(MVA)	(MVA)	(kV)	(MVA)	substation	with both end terminal station
1	3x40	96	115	288	3	3
			69	192	2	2
2	4x40	144	115	288	2	2
			69	192	1+1/3	2 but spare line for 2bank is required
ε	3x60	144	115	288	2	2
			69	192	1+1/3	2 but spare line for 2bank is required
4	3x80	192	115	288	1+1/2	2 but spare line for 2bank is required
			69	192	1	•

Maximum load is assumed at 80% loading or 120% load on sound bank when 1 transformer shuts down

Refer to Fig. 9.3-3 and Fig. 9.3-4







ozie bindir (1997) National de distributo de la defensa de la figura

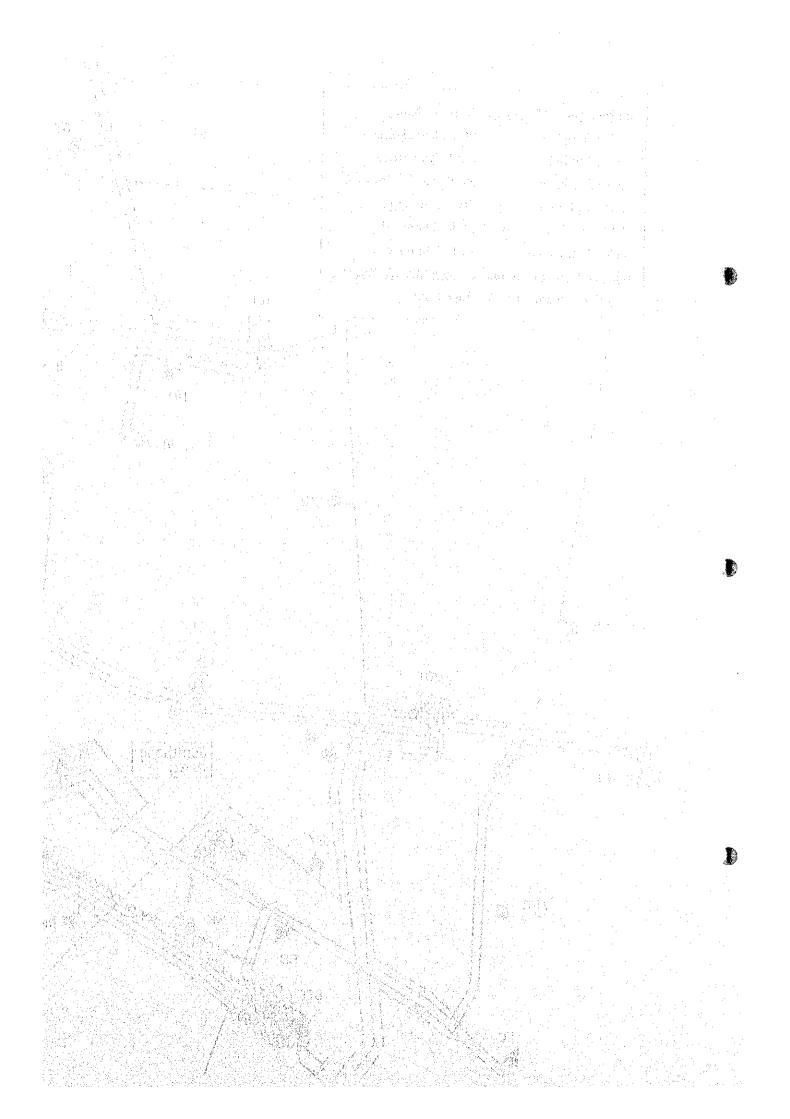
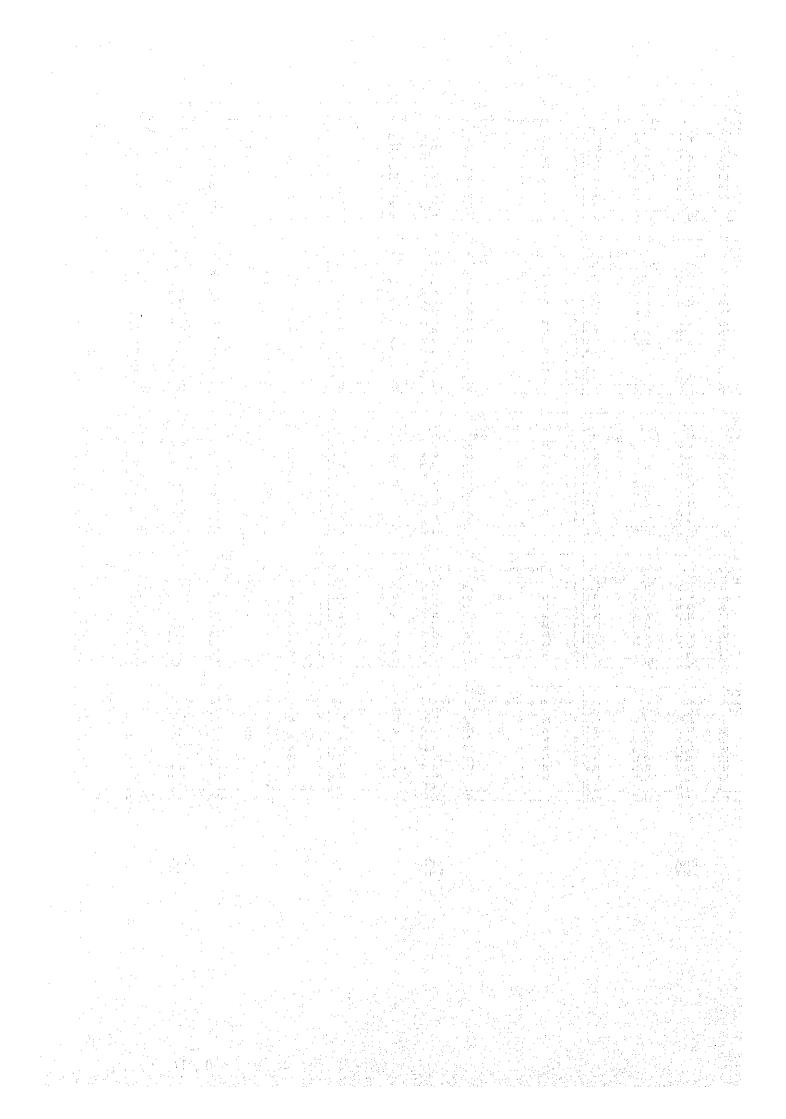


Table 9.3-2 (a) Case Study of Substation (Sathorn Area)

Table 9, 9 2 (a) case study of substitution (said				2010
No ABB Substation Bank configuration Capacity Load-1 Load (NYA) (NT) (NY		Load-1 Load-2 Utilization Bank configuration Capacity Load-1 (NT) (NYA) factor (X) (NYA) (NYA)	Load-2 Utilization Bank configuration Capacity Load-1 (NYA) factor (N) (NYA) (NY)	Load-2 Utilization Sank configuration Capacity Load-1 Load-2 Utilization (NYA) factor (%) (NYA)
32	12 12 13 12 13 13 14 15 15 14 15 15 14 15 15	38.00 49.16 61.5 2 × 40 × 80 39.96 94.07 121.71 67.6 3 × 40 1 × 60 180 97.01 37.10 48.00 60.0 2 × 40 × 80 80 43.26 69.71 90.19 56.4 3 × 60 × 180 61.58 44.81 57.98 48.3 3 × 60 × 180 86.47 42.50 54.99 68.7 2 × 60 × 120 61.47 53.35 69.02 57.5 2 × 60 × 120 61.32 0.00 0.0 × × 0 0.00 379.54 491.05 59.9 940 451.07	51.51 64.4 3 × 60 × 180 92.15 125.05 69.5 3 × 40 1 × 60 180 103.19 55.78 69.7 2 × 40 × 80 44.46 79.38 44.1 3 × 60 × 180 71.64 111.46 61.9 3 × 60 × 180 96.42 79.23 66.0 3 × 60 × 180 96.42 79.04 65.9 3 × 60 × 180 95.22 0.0 3 × 60 × 180 77.51 581.43 61.9 3 60 × 180 77.51	118.50 65.8 3 × 60 × 180 85.89 109.63 66.9 132.70 73.73 3 × 40 1 × 60 180 106.56 136.34 75.7 57.17 71.5 1 × 40 1 × 60 100 47.77 61.12 61.1 92.13 51.2 3 × 60 × 180 76.97 98.48 54.7 123.99 68.9 3 × 60 × 180 81.65 104.45 58.0 129.97 72.2 3 × 60 × 180 90.96 116.38 64.7 122.45 68.0 3 × 60 × 180 102.31 130.90 72.7 93.68 55.4 3 × 60 × 180 33.28 106.55 59.2 876.59 65.4 1360 675.19 863.66 63.5
Case-1 (3 × 40MYA)		DAAC	2011	2016
No ABB Substation Bank configuration Capacity Load-1 Load	ud-2 Utilization Bank configuration Capacity VA) factor (%) (MVA)	Load-1 Load-2 Utilization Bank configuration Capacity Load-1 (NY) (NYA) factor (%) (NVA) (NY)	Load-2 Utilization Bank configuration Capacity Load-1 (NYA) factor (%) (NYA) (NYA)	Load-2 Utilization Bank configuration Capacity Load-1 Load-2 Utilization (NYA) factor (X) (NYA)
32	51. 14 63.9 2 × 40 × 80 111. 14 69.5 5 × 40 × 160 55. 24 69.1 2 × 40 × 160 79. 06 65.9 3 × 40 × 120 59. 35 74. 2 2 × 40 × 80 0. 0 2 × 40 × 80 0. 0 3 × 40 × 120 0. 0 3 × 40 × 120 0. 0 0 0 × × 0 0. 0 0 × × 0 0. 0 0 × × 0 0. 0 0 × × 0 0. 0 0 × × 0 0. 0 0 × × 0 0. 0 0 × × 0 0. 0 0 × × 0 0. 0 0 × × 0 0. 0 0 × × 0 0. 0 0 × × 0 0. 0	38.00 49.16 61.5 2 × 40 × 160 39.96 94.07 121.71 78.1 4 × 40 × 160 97.01 37.10 48.00 60.0 2 × 40 × 120 61.58 59.71 90.19 75.2 3 × 40 × 120 61.58 44.81 57.98 72.5 3 × 40 × 120 68.82 42.50 54.99 68.7 3 × 40 × 120 61.47 53.35 69.02 57.5 3 × 40 × 120 61.47 53.35 69.02 57.5 3 × 40 × 120 80 29.11 0.00 0.0 2 × 40 × 80 29.11 0.00	51.51 64.4 3 × 40 × 120 59.82 125.05 78.2 4 × 40 × 160 90.80 27.82 34.8 2 × 40 × 80 44.46 79.38 66.2 3 × 40 × 120 71.64 88.71 73.9 3 × 40 × 120 68.86 79.23 65.0 3 × 40 × 120 67.21 92.21 76.8 3 × 40 × 120 71.41 37.52 46.9 3 × 40 × 120 75.25 0.0 2 × 40 × 80 34.73 0.0 2 × 40 × 80 32.57 0.0 2 × 40 × 80 35.76 0.0 2 × 40 × 80 38.76 581.43 66.1 40 × 80 38.76	116. 76 73. 0 4 × 40 × 160 93. 25 119. 90 74. 6 57. 17 71. 5 2 × 40 × 80 23. 89 30. 55 38. 2 92. 13 76. 8 3 × 40 × 120 51. 13 65. 42 54. 5 88. 55 73. 8 3 × 40 × 120 65. 31 83. 56 69. 6 86. 43 72. 0 3 × 40 × 120 72. 77 93. 10 77. 6 91. 83 76. 5 3 × 40 × 120 63. 95 81. 82 68. 2 58. 70 48. 9 3 × 40 × 120 65. 52 83. 83 69. 9 57. 52 71. 9 2 × 40 × 80 34. 73 44. 44 55. 6 41. 89 52. 4 2 × 40 × 80 41. 91 53. 62 67. 0 58. 85 73. 6 3 × 40 × 120 55. 82 72. 70 60. 6 49. 84 62. 3 2 × 40 × 80 41. 64 53. 28 66. 6
Case-2 (4 × 40 NVA)		8000	2011	2016
No ABB Substation Bank configuration Capacity Load-1 (MYA) (MT) (M	Add-2	Load-1	Load-2	Load-2
Next-sub I X X 0 0.00	0.0 × × 0 355.93 68.4 720	0.00 0.0 × × 0 0.00 379.54 491.05 68.2 849 451.07	9.0 3 × 40 × 120 60.02 581.43 69.2 1280 681.67	
Case-3 (3 × 60 NVA)	VV V			
1996	2001 pad-2 Utilization Bank configuration Capacity		toad-2 Utilization Bank configuration Capacity Load-1	2016 2016 CMVA) factor (X) CMVA) factor (X) CMVA) factor (X) CMVA) (MVA) (MVA) (MVA) factor (X)
(NYA) (NT) (NT) (NT	MYA Factor (X) (MYA St. 14 63.9 2 × 40 × 80	(NT) (NYA) factor (K) (NYA) (NYA)	MYA factor (\$)	5 118.50 65.8 3 × 60 × 180 85.69 109.63 60.4 3 132.70 73.7 3 × 40 1 × 60 180 166.56 136.34 75.6 6 57.17 71.5 1 × 40 1 × 60 100 47.77 61.12 61.12 4 92.13 76.8 2 × 40 1 × 60 140 76.97 98.48 70. 2 123.99 68.9 3 × 60 × 180 81.65 104.46 58.7 7 129.97 72.2 3 × 60 × 180 90.96 116.38 64. 2 122.45 68.0 3 × 60 × 180 102.31 130.90 72. 1 99.68 55.4 3 × 60 × 180 83.28 106.55 59.
Casc-4 (3 × 89NYA) 1996	2001	2006	2011	2016
No ABB Substation Bank configuration Capacity Load-1 L	coad-2 Utilization factor (%) Bank configuration Capacity (MYA) 51.14 63.9 2 × 40 × 80 80 111.14 69.5 4 × 40 × 160 55.24 69.1 2 × 40 × 80 79.06 65.9 3 × 40 × 120 59.35 74.2 2 × 40 × 80 80 59.35 74.2 2 × 40 × 80 80 160 0.0 2 × 80 × 160 160 160	Load-1	Load-2	9 132.70 66.4 3 × 40 1 × 80 200 106.56 136.34 68. 6 57.17 71.5 1 × 40 1 × 80 120 47.77 61.12 50. 44 92.13 76.8 3 × 40 × 120 38.49 49.24 41. 7 173.83 72.4 3 × 80 × 240 123.28 157.73 65. 7 129.97 54.2 3 × 80 × 240 123.28 157.73 65.
142 St Satom × × 0 0.00 189 AT Satomtai × × 0 0.00	0.0 × × 0 0.0 × × 0	0.00 0.0 2 × 80 × 160 61.32 0.00 0.0 × × 0 0.00	79.04 49.4 3 × 80 × 240 133.9 0.0 × × 0 0.0	0 0.0 × × 0 0.00 0.
	355.93 68.4 680		581. 43 63. 2 1280 681. 6	6 876.59 68.5 1320 675.20 863.86 65.
Indoor type substation : Klongtocy(KT), Silom(SL), Surawong(SU)				
Load-1 : Coincident load Load-2 : Non-coincident load				
Diversity factor 1. 1805		1. 1825	1. 18)	18 1. 1818 0. 9237



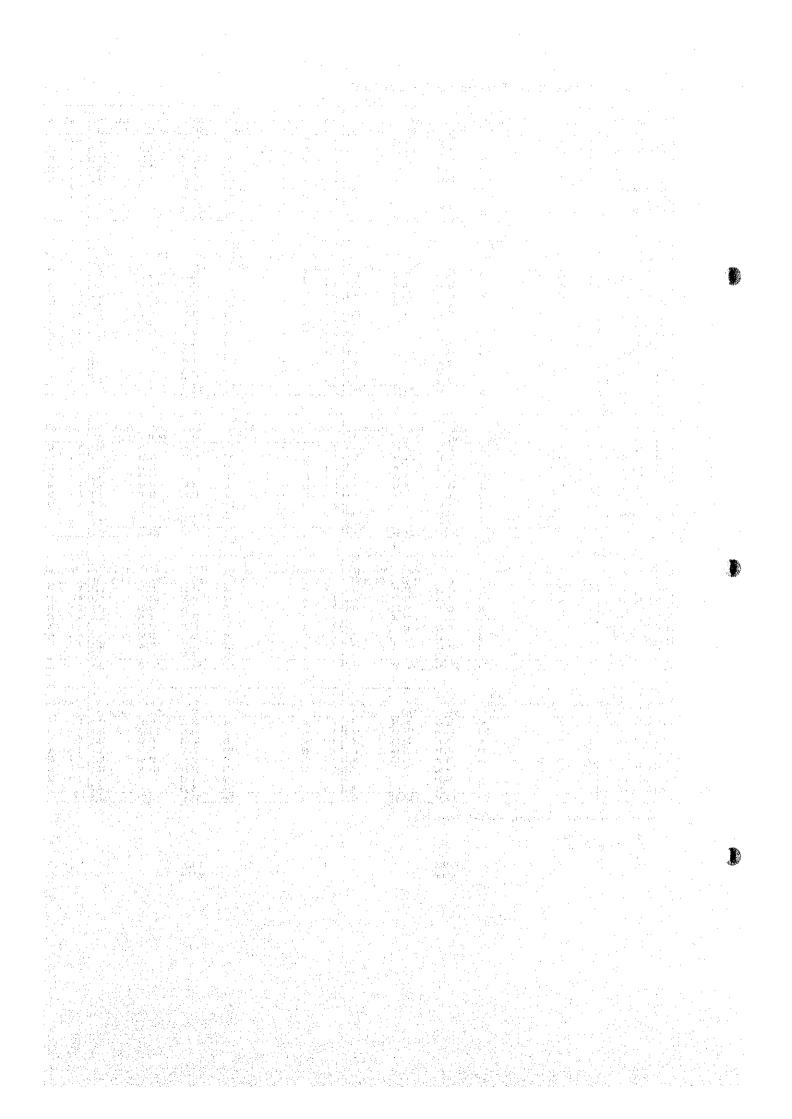
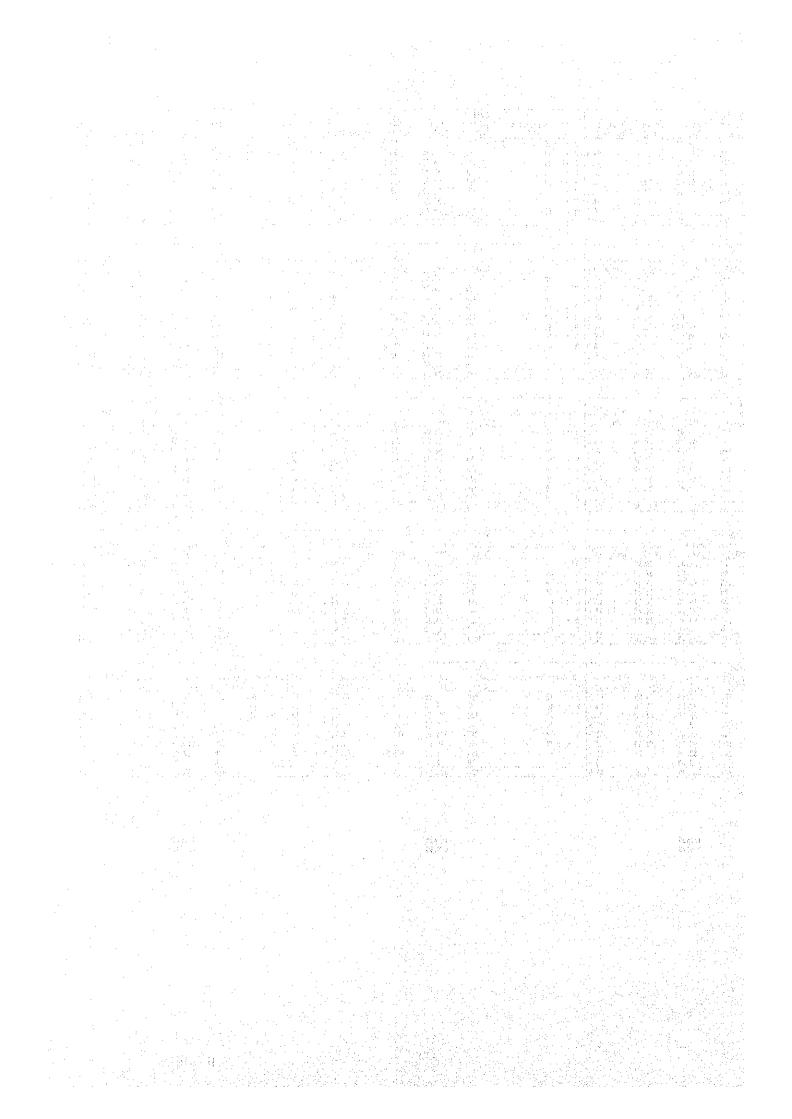


Table 9.3-2 (b) Case Study of Substation (Phahol Yothin Area)

Table 9.3-2 (b) Case Study of Sub	station (Phahol Yothin Area)		The second second			
No ABB Substation Bank configuration Capacity (NYA)	(NT) (NYA) factor (%)	2001 onfiguration Capacity Load-1 Load-2 (NYA) (NY) (NY)	Utilization Bank configuration Capacity factor (%) 70.8 2 × 40 1 × 60 140	Load-1 Load-2 Utilization Bank configuration (NT) (NYA) factor (X) 58.64 75.59 54.0 2 × 40 1 × 60	2011 Capacity Load-1 Load-2 Utilization Bank con	2016 Infiguration Capacity Load-1 Load-2 Utilization (MYA) (MY) (MYA) factor (%) 10 1 × 60 140 80.14 102.53 73.2
43 MC Nochit 2 × 40 1 × (40) 120	45.29 58.95 73.7 2 × 59.22 77.08 64.2 3 ×	0) × 80 45.40 58.7 × 0 0.00	4 74.2 2 × 40 × 80 2 69.6 3 × 40 × 120 5 71.3 2 × 40 × 80 9 69.0 2 × 60 × 120 4 73.4 2 × 60 × 120 0.0 2 × 60 × 120	40.54 52.26 65.3 2 × 40 × 63.79 82.22 68.5 3 × 40 × 64.06 82.57 68.8 3 × 60 × 62.44 80.48 67.1 3 × 60 × 63.80 82.24 68.5 2 × 60 ×	80 41. 28 53. 09 66. 4 1 × 4 120 68. 45 88. 02 73. 4 2 × 4 80 43. 27 55. 64 69. 6 2 × 4 180 87. 95 113. 10 62. 8 3 × 6 180 70. 75 90. 98 50. 5 3 × 6 120 54. 13 69. 61 58. 0 2 × 6	10 1 × 60 100 50.76 64.94 64.9 10 1 × 60 140 84.16 107.68 76.9 10 × 80 46.49 59.48 74.4 10 × 180 108.13 138.35 76.9 10 × 180 81.85 104.72 58.2 10 × 120 66.55 85.15 71.0
187 RO Rajchatru X X Q Total 480	0.00 0.0 × 221.42 288.20 69.0	× 0 0.00 580 318.89 412, §	9.0 × × 0 5 71.1 780	0.00 0.0 2 × 60 × 395.43 509.70 65.3	120 55.48 71.35 59.5 2 × 6 1020 494.37 635.74 62.3	69 × 120 68.22 87.28 72.7 1060 586.30 750.13 70.8
Case-1 (3 × 40MYA) 1996	Load-1 Load-2 Utilization Bank	2001 configuration Capacity Load-1 Load-2	2006 Utilization Back configuration Capacity	Load-1 Load-2 Utilization Bank configuration	2011 Capacity Load-1 Load-2 Utilization Bank co	2016 nfiguration Capacity Load-1 Load-2 Utilization
No ABB Substation Bank configuration (NYA) 43 MC Mochit 3 × 40 × 120	(NY) (NYA) factor (%) 44.52 57.95 48.3 3 ×	(NYA) (NY) (NYA) 40 × 120 65.63 84.9	factor (%) (NYA) 11 70.8 3 × 40 × 120	(NT) (NYA) factor (%) 58.64 75.59 63.0 3 × 40 ×	(NYA) (NT) (NYA) factor (X) 120 73.06 93.95 78.3 3 × 4	(NYA) (NT) (NYA) factor (N) 40 × 120 68.11 87.14 72.6
67 SM Sailom 2 × 40 × 30 69 SM Sassen 3 × 40 × 120 89 VT Yothee 2 × 40 × 30 104 PP Pradipat 2 × 40 × 30 122 DD Dindaeng 168 MP Sananpao × × 0 187 KO Rajchakru × × 0 New-sub 1 × × 0	34.63 45.07 56.3 2 × 37.76 49.15 61.4 3 × 0.00 0.0 2 × 0.00 0.0 × 0.00 0.0 × 0.00 0.0 × 0.00 0.0 × 0.00 0.0 × 0.00 0.0 × 0.00 0.0 × 0.00 0.0 × 0.00 0.0 × 0.00 0.0 × 0.00 0.0 × 0.00 0.0 × 0.00 0.0 × 0.00 0.0 × 0.00 0.0 × 0.00 0.0 × 0.00 0.0 × 0.00 0.0 × 0.00 0.00 × 0.00 0.00 × 0.00 0.00 × 0.00 0.00 × 0.00 0.00 0.00 × 0.00 0.00 0.00 × 0.00 0.00 0.00 0.00 × 0.00	40 × 80 45.87 59.3 40 × 120 64.56 83.5 40 × 80 44.10 57.0 40 × 120 53.33 68.9 40 × 80 45.40 58.7 × 0 0.00 × 0 0.00 × 0 0.00 × 0 0.00 10 0.	122	42.16 54.34 67.9 2 × 40 × 64.06 82.57 68.8 3 × 40 × 62.44 80.48 67.1 3 × 40 ×	120 58.68 75.46 62.9 3 × 4 80 43.27 55.64 69.6 2 × 4 120 72.24 92.90 77.4 3 × 4 120 70.75 90.98 75.8 3 × 4 120 54.13 69.61 58.0 3 × 4 120 55.48 71.35 59.5 3 × 4	10 × 80 45.11 57.72 72.2 140 × 120 72.13 92.28 76.9 10 × 80 46.49 59.48 74.4 140 × 120 73.38 93.89 78.2 140 × 120 58.46 74.80 62.3 140 × 120 68.55 85.15 71.0 140 × 120 68.52 87.28 72.7 140 × 120 68.72 87.28 72.7 140 × 120 46.79 59.86 49.9 140 × 80 41.06 52.53 65.7 1080 586.30 750.13 69.5
Total 480 Case-2 (4 × 40MYA)	221. 42 288. 20 60. 01			VII. V		2016
Ho ABB Substation Bank configuration Capacity (NYA)	Load-1 Load-2 Utilization Bank (NN) (NYA) factor (X)	2001 configuration Capacity Load-1 Load-2 (NYA) (NY) (NYA)	Utilization Bank configuration Capacity factor (X) (NYA)	(NW) (NYA) factor (%)	(NYA) (NYA) factor (N)	onfiguration Capacity Load-) Load-2 Utilization (NYA) (NYA) (NYA) factor (X)
43 MC Nochit 3 × 40 × 120 67 SM Sailoa 2 × 40 × 80 69 SM Sansen 3 × 40 × 122 89 YT Yothee 2 × 40 × 86 104 PP Pradipat 2 × 40 × 86 1122 DD Dindaeng × × 6 168 MP Sanaspao × × 6	44.52 57.95 48.3 3 × 45.29 58.95 73.7 2 × 59.22 77.08 64.2 3 × 34.63 45.07 56.3 2 × 37.76 49.15 51.4 3 × 0.00 0.00 2 ×	40 × 120 65.63 84.5 40 × 80 45.87 59.3 40 × 120 64.56 83.5 40 × 80 44.10 57.0 40 × 120 53.33 68.5 40 × 80 45.40 58.5 × 0 0.00	91 70.8 3 × 40 × 120 84 74.2 2 × 40 × 80 852 69.6 3 × 40 × 120 95 71.3 2 × 40 × 80 99 57.5 3 × 40 × 120 74 73.4 3 × 40 × 120 0.0 3 × 40 × 120	40.54 52.26 65.3 2 × 40 × 63.79 82.22 68.5 3 × 40 × 64.06 82.57 68.8 4 × 40 × 62.44 80.48 67.1 3 × 40 × 63.80 82.24 68.5 3 × 40 ×	80 41.28 53.09 66.4 2 × 120 68.45 88.02 73.4 4 × 80 43.27 55.64 69.6 2 × 160 87.95 113.10 70.7 4 × 120 70.75 90.98 75.8 4 × 120 54.13 69.61 58.0 3 ×	40 × 160 80.14 102.53 64.1 40 × 80 45.11 57.72 72.2 40 × 160 84.16 107.68 67.3 40 × 80 46.49 59.48 74.4 40 × 160 96.55 123.53 77.2 40 × 160 81.85 104.72 65.5 40 × 120 66.55 85.15 71.0 40 × 160 85.44 109.32 68.3 1080 586.29 750.13 69.5
187 RO Rajchakru X	0.00 0.00 × 221.42 288.20 60.0	× 0 0.00 600 318.89 412.5	0.01 × × 9 55 68.81 760	0.00 0.0 3 × 40 × 395.43 509.70 67.1	120 55.48 71.35 59.5 4 × 920 494.37 635.74 69.1	1080 586.29 750.13 69.5
Case 3 (3 × 60 NYA) 1996 No ABB Substation Bank configuration Capacity	load-1 Load-2 Utilization Bank	2001 configuration Capacity Load-1 Load-2	Utilization Bank configuration Capacity	Load-1 Load-2 Utilization Bank configuration	2011 Capacity Load-1 Load-2 Utilization Bank or	2016 onfiguration Capacity Load-1 Load-2 Utilization
(NYA) 43 NC Nochit 3 × 40 × 120	(NT) (NYA) factor (X)) 44.52 57.95 48.3 3 ×	(NYA) (NY) (NYA) 40 × 120 65.63 84.	factor (X) (NYA) 91 70.8 3 × 40 × 120	(NW) (NYA) factor (X) 58.64 75.59 63.0 3 × 40 ×	(NYA) (NV) (NYA) factor (X) 120 73.06 93.95 78.3 2 ×	(NYA) (NT) (NYA) factor (X) 40 1 × 60 140 80.14 102.53 73.2 40 1 × 60 100 50.76 64.94 64.9
67 SM Sailon 2 × 40 × 86 69 SM Sansen 3 × 40 × 126 89 YT Yothee 2 × 40 × 86		40 × 80 45.87 59.3 40 × 129 64.56 83.3 40 × 80 44.10 57.3	52 69.6 3 × 40 × 120 05 71.3 2 × 40 × 80	63.79 82.22 68.5 3 × 40 × 42.16 54.34 67.9 2 × 40 ×	120 68.45 88.02 73.4 2 × 80 43.27 55.64 69.6 2 ×	40 1 × 60 140 84.16 107.68 76.9
104 PP Fradipat 2 × 40 × 8 122 DD Dindaeng × × 168 RP Sanampao × ×	1 37.76 49.15 61.4 2 × 0 0.00 0.0 2 × 0 0.00 0.0 ×	60 × 120 53.33 68. 60 × 120 45.40 58. × 0 0.00	74	62.44 80.48 67.1 3 × 60 × 63.80 82.24 68.5 2 × 60 ×	180 70.75 90.98 50.5 3 ×	40 × 80 46.49 59.48 74.4 60 × 180 108.13 138.35 76.9 60 × 180 81.85 104.72 58.2 60 × 120 66.55 85.15 71.0 60 × 120 68.22 87.28 72.7
187 RO Rajchakru X X	0 0.60 0.0 × 0 221.42 288.20 60.0	× 0 0.00 640 318.89 412.	0.01 × × 0 55 64.51 760	0.00 0.0 2 × 60 × 395.43 509.70 67.1	1000 494.37 635.74 63.6	60 × 120 68.22 87.28 72.7 1060 586.30 750.13 70.8
Case-4 (3 × 80NYA) 1996 No ABB Substation Bank configuration Capacity	y Load-1 Load-2 Utilization Bank	2001 configuration Capacity Load-1 Load-2	2006 Utilization Bank configuration Capacity	Load-1 Load-2 Utilization Bank configuration	2011 Capacity Load-1 Load-2 Utilization Bank o	2016 onfiguration Capacity Load-1 Load-2 Utilization
43 MC Nochit 3 × 40 × 12	(NV) (NVA) factor (X) 0 44.52 57.95 48.3 3 ×	(NYA) (NYA) (NYA) 40 × 120 65.63 84.	factor (%) (NYA) 91 70.8 3 × 40 × 120	(NT) (NYA) factor (N)	(NYA) (NF) (NYA) factor (%) 120 73.06 93.95 78.3 2 ×	(NYA) (NW) (NYA) factor (%)
67 SM Sailou 2 × 40 × 8 69 SM Samsen 3 × 40 × 12 89 YT Yothee 2 × 40 × 8	0 59.22 77.08 64.2 3 × 0 34.63 45.07 56.3 2 ×	40 × 80 41.21 53. 40 × 120 64.56 83. 40 × 80 44.10 57. 40 × 80 41.92 54.	52 69.6 3 × 40 × 120	1 63.79 82.22 68.5 3 × 40 × 1 42.16 54.34 67.9 2 × 40 ×	120 68.45 88.02 73.4 2 × 80 43.27 55.64 69.6 2 ×	40 1 × 80 120 50.76 64.94 54.1 40 1 × 80 160 84.16 107.68 67.3 40 × 80 46.49 59.48 74.4 80 × 240 142.24 181.99 75.8
104 PP Pradipat 2 × 40 × 8 122 DD Dindaeng × ×	0 37.76 49.15 61.4 2 × 0 0.00 0.0 2 × 0 0.00 0.0 ×	80 × 160 61.47 79. × 0 0.00	23 67.8 2 × 80 × 160 53 49.7 2 × 80 × 160 0.0 2 × 80 × 160	0 62.44 80.48 50.3 2 × 80 × 1	160 70.75 90.98 56.9 2 ×	40 1 × 80 160 80.14 102.53 64.1 40 1 × 80 120 50.76 64.94 54.1 40 1 × 80 160 84.16 107.68 67.3 40 × 80 46.49 59.48 74.4 80 × 240 142.24 181.99 75.8 80 × 160 89.24 114.18 71.4 80 × 160 93.27 119.33 74.6 × 0 0.00 0.00
187 180 Rajchakru X X	0 0.00 0.0 × 0 221.42 288.20 60.0	× 0 0.00 640 318.89 412.	0.0 × × 6 55 64.5 880		960 494.38 635.74 66.2	1080 586.30 750.13 69.5
indoor type substation : Sailon(SN), Yothee(Y	()					
Load-1 : Coincident load Load-2 : Non-coincident load				gander van de kalender en gebeure. Bereitste		1 1010
Diversity factor Power factor	1. 1805 0. 9070	1. 1825 0. 9140		1. 1820 0. 9170	1. 1818 0. 9190	1. 1818 0. 9 237



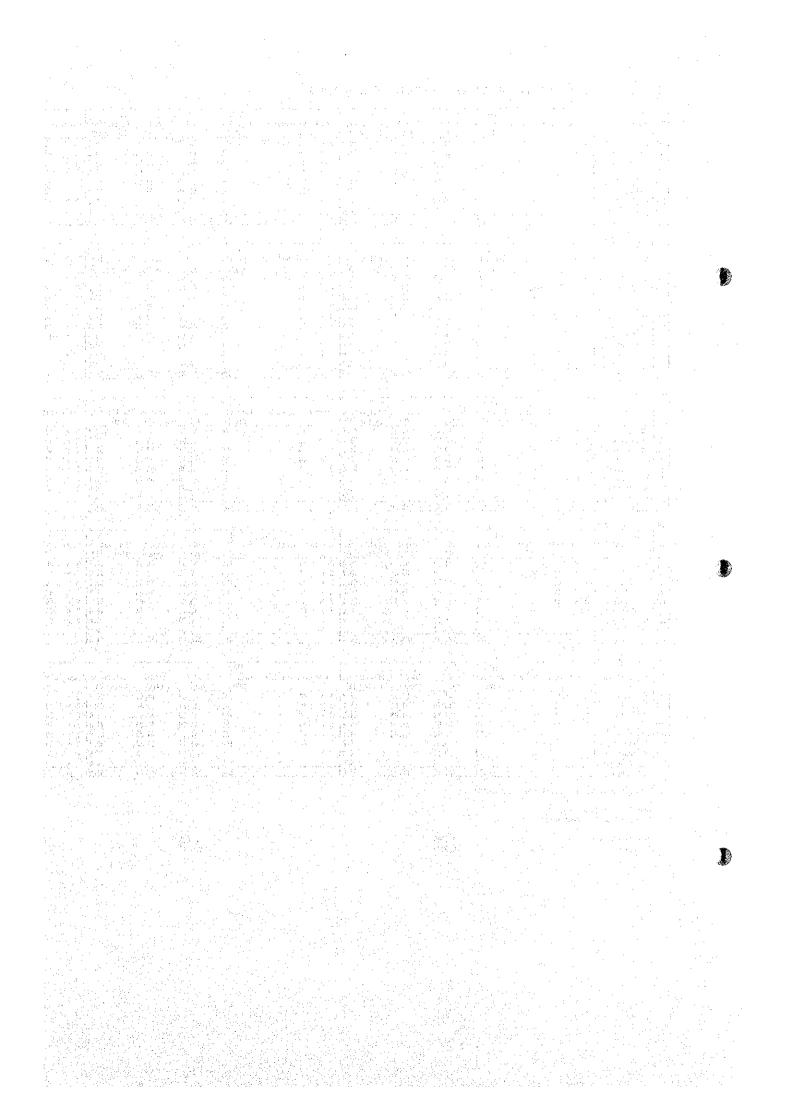
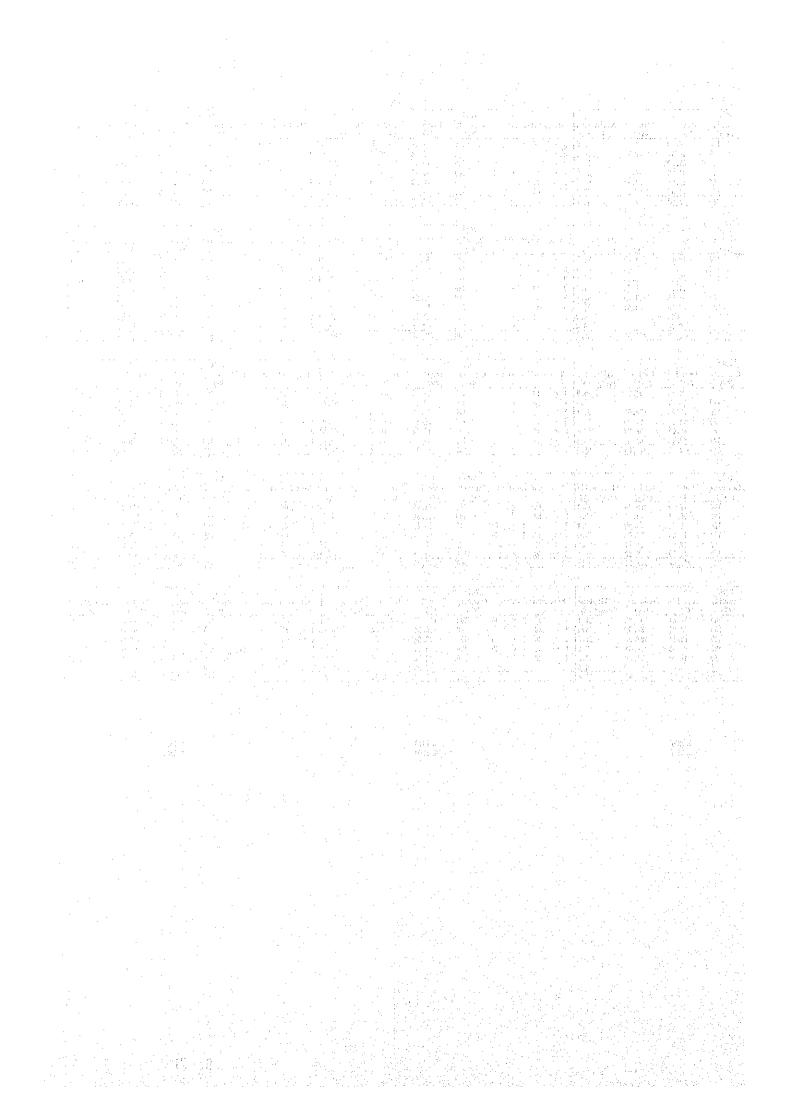
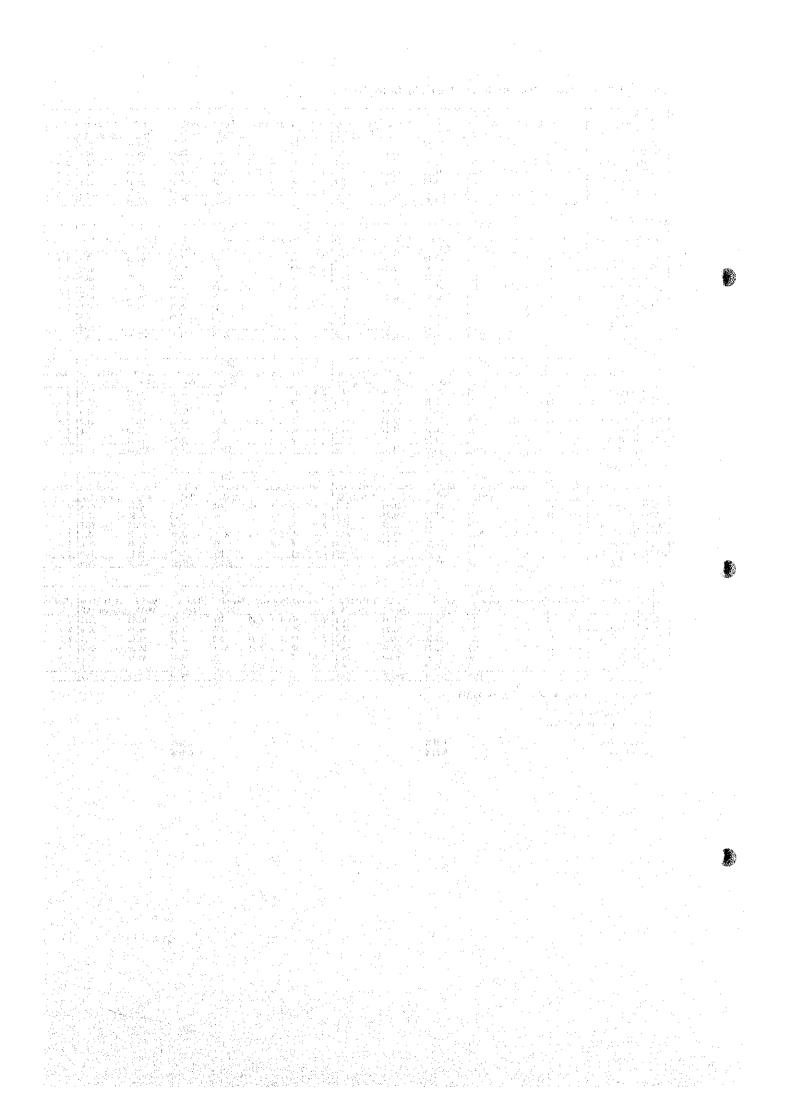
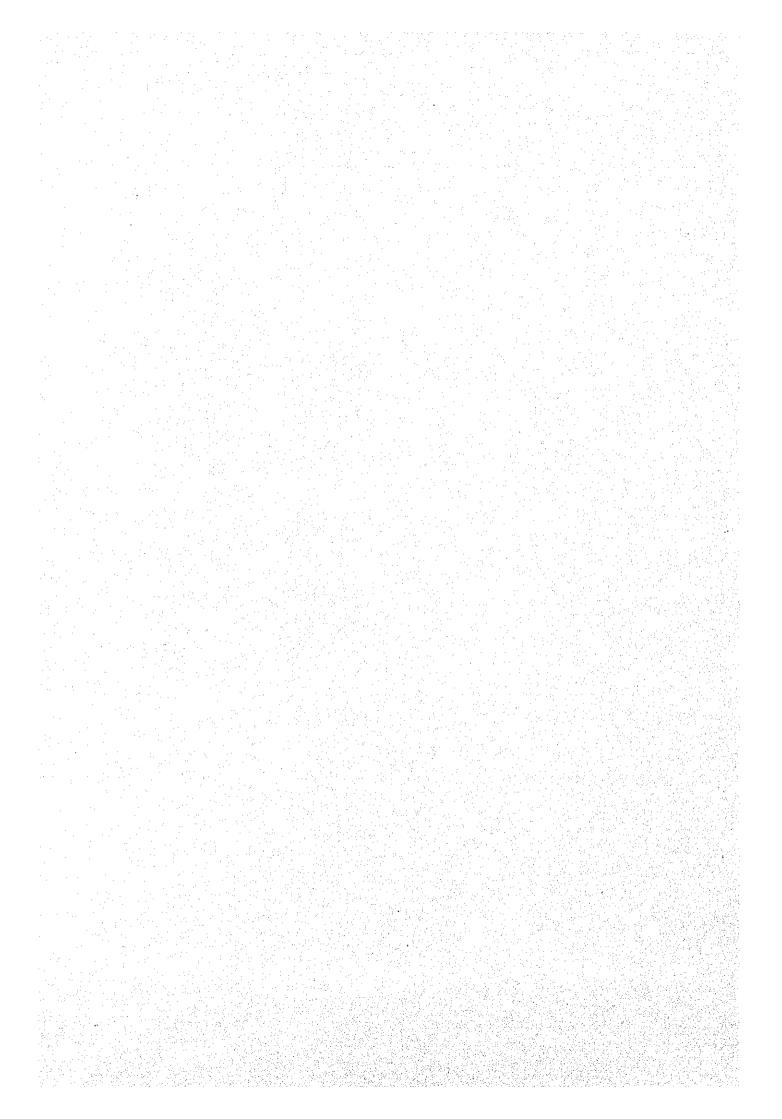


Table 9.3-2 (c) Case Study of Substation (Jor	mthong Area)				
	oad-2 Utilization Bank configuration Capacity Los (NYA) factor (X) (NYA) ()	2006 1-1 Load-2 Utilization Bank configuration Capaci (NYA) factor (X) (NYA)		ty toad-1 Load-2 Utilization Bank configuration Capacity	Load-1 Load-2 Utilization (NY) (NYA) factor (%)
9 BM Bangmod 2 × (40) × 80 39.40 33 WG Klongwatsing 2 × (40) × 80 29.39 38 MH Bahaisawan 2 × 40 1 × 60 140 36.14 52 PS Petchkasem 1 × 40 2 × 22.4 84.8 44.76 B1 TS Taksin 2 × 40 × 80 34.68 151 WR Wuttakart × 0 0.00	51,28 64,1 2 × (40) 1 × 60 140 38,25 47,8 2 × 60 × 120 47,04 33,6 2 × 40 1 × 60 140 58,26 68,7 1 × 40 2 × 22,4 84,8 45,14 56,4 2 × 40 × 80 0,0 2 × 60 × 120	11.30 92.24 65.9 3 × 60 × 14 13.20 55.89 46.6 2 × 60 × 15 12.58 55.09 65.0 1 × 40 1 × 60 15 12.58 55.09 65.0 1 × 40 1 × 60 15 13.32 43.11 35.9 2 × 60 × 15	20 56.41 72.71 60.6 3 × 60 × 11 10 59.00 76.05 54.3 2 × 40 1 × 60 10 00 44.25 57.04 57.0 1 × 40 1 × 60 11 10 42.08 54.24 67.8 2 × 40 × 11 10 42.08 54.24 67.8 2 × 60 × 11	80 84.49 108.65 60.4 3 × 60 × 180 80 76.38 98.22 54.6 3 × 60 × 180 40 73.36 94.34 67.4 2 × 40 1 × 60 140 90 50.41 64.82 64.8 2 × 60 × 120 80 42.58 54.76 68.5 2 × 40 × 80 20 50.74 55.25 54.4 2 × 60 × 120 90 377.96 486.04 60.8 820	86.78 111.03 61.7 97.36 124.56 69.2 75.35 96.40 68.9 62.00 79.33 66.1 43.73 55.95 69.9 53.78 68.81 57.3 419.00 536.08 65.4
Case-I (3×40NYA)					
	.oad-2 Utilization Bank configuration Capacity Los			ty Load-1 Load-2 Utilization Bank configuration Capacity	Load-1 Load-2 Utilization
9 BM Banganod 2 × 40 × 80 39.40 33 WG Klongwatsing 2 × 40 × 80 29.39 38 MK Asharisawan 3 × 40 × 120 36.14 52 PS Petchkasea 1 × 40 2 × 22.4 84.8 44.76 81 TS Taksin 2 × 40 × 80 34.68 151 WR Futtakart × × 0 0.00 0.00 Neg-sub 2 × × 0 0.00 0.00	51.28 64.1 3 × 40 × 120 38.25 47.8 2 × 40 × 80 47.04 39.2 3 × 40 × 120 58.26 68.7 1 × 40 2 × 22.4 84.8 45.14 56.4 2 × 40 × 80 0.0 2 × 40 × 80 0.0 0 × × 0 0.0 0 × × 0	13.20 55.89 69.9 3 × 40 × 1 1 1 1 1 1 1 1 1 1	20 70.78 91.23 76.0 3 × 40 × 12 20 56.41 72.71 60.6 3 × 40 × 12 20 59.00 76.05 63.4 3 × 40 × 12 80 44.25 57.04 71.3 3 × 40 × 12 80 42.08 54.24 67.8 2 × 40 × 12 80 50.10 64.58 53.8 3 × 40 × 12 0 0.00 0.00 0.0 2 × 40 × 12	20 63.37 81.49 67.9 3 × 40 × 120 20 63.33 89.16 74.3 3 × 40 × 120 20 73.36 94.34 78.8 3 × 40 × 120 20 50.41 64.82 54.0 3 × 40 × 120 80 42.58 54.76 68.5 2 × 40 × 80 20 50.74 65.25 54.4 3 × 40 × 120 80 28.17 36.22 45.3 2 × 40 × 80 0 0.00 0.0 2 × 40 × 80	(NT) (NYA) factor (\$) 65.06 83.24 89.4 73.03 93.44 77.9 46.02 58.88 49.1 62.00 79.33 66.1 43.73 55.95 68.9 53.78 68.81 57.3 46.04 58.91 73.6 29.33 37.52 46.9 418.99 535.08 55.8
	239.97 54.01 564.8	89.91 375.98 66.4 6	40 322.62 415.85 55.01 7	60 377.95 486.04 61.01 840	110. 39 000. 00 00. 01
Case-2 (4 × 40NYA) No ABB Substation Bank configuration Capacity Load-1 L	2001 Load-2 Utilization Bank configuration Capacity Lo	2006 d-1 Load-2 Utilization Bank configuration Capaci		ty toad-1 Load-2 Utilization Bank configuration Capacity	Load-1 Load-2 Utilization
SM Bangand 2 × 40 × 80 39.40 33 WG Klongwatsing 2 × 40 × 80 29.39 38 WN Kahaisawan 3 × 40 × 120 36.14 52 PS Potchkasca 1 × 40 2 × 22.4 84.8 44.76 81 TS Taksin 2 × 40 × 80 34.68 15] FR Tuttakart × × 0 0.00 Total 444.8 184.37	51.28 64.1 3 × 40 × 120 38.25 47.8 2 × 40 × 80 47.04 39.2 3 × 40 × 120 58.26 68.7 1 × 40 2 × 22.4 84.8 45.14 55.4 2 × 40 × 80 0.0 2 × 40 × 80	43.20 55.89 69.9 3 × 40 × 162.04 80.27 66.9 3 × 40 × 142.58 55.09 65.0 2 × 40 × 37.47 48.48 60.6 2 × 40 × 33.32 43.11 53.9 3 × 40 × 1	20 70.78 91.23 76.0 4 × 40 × 1 20 56.41 72.71 60.6 4 × 40 × 1 20 59.00 76.05 63.4 3 × 40 × 1 80 42.08 57.04 71.3 3 × 40 × 1 80 42.08 54.24 67.8 2 × 40 × 20 50.10 64.58 53.8 3 × 40 × 1	NT NT Factor (\$) NYA Sactor (\$) Sactor (\$) NYA NYA	(NT) (NYA) factor (N) 86. 78 111. 03 69. 4 85. 19 109. 00 68. 1 46. 02 58. 88 49. 1 74. 17 94. 89 59. 3 43. 73 55. 95 69. 9 83. 11 106. 33 66. 5 419. 00 536. 08 63. 8
Case-3 (3 × 60NYA)			200	0.00	
Second S	51.28 64.1 2 × 40 1 × 60 140 38.25 47.8 2 × 40 × 80 47.04 39.2 3 × 40 × 120 58.26 68.7 1 × 40 2 × 22.4 84.8 45.14 56.4 2 × 40 × 80 0.0 2 × 60 × 120	(NYA) factor (%) (NYA) (NYA)	ty Load-1	ty Load-1 Load-2 Utilization Bank configuration Capacity	Load-1
Case-4 (3 × 80 MVA) 1996	2001	2006			
(NYA) (NT)	(NYA) factor (X) (NYA) (d-1 Load-2 Utilization Bank configuration Capaci) (NYA) factor (%) (NYA)) (NT) (NVA) factor (X) (NVA)	Load-1 Load-2 Utilization (NT) (NYA) factor (N)
9 M Bangaod 2 × 40 × 80 39.40 33 TC Klongwatsing 2 × 40 × 80 29.39 38 IN Mahaisawan 3 × 40 × 120 36.14 52 PS Potchkasea 1 × 40 2 × 22.4 84.8 44.76 81 TS Taksin 2 × 40 × 80 34.68 151 FR Futtakart × × 0 0.09 Total 444.8 184.37	51.28 64.1 2 × 40 1 × 80 160 38.25 47.8 2 × 80 × 160 47.04 39.2 2 × 40 1 × 80 160 58.26 68.7 1 × 40 2 × 22.4 84.8 45.14 56.4 2 × 40 × 80 0.0 × 0 239.97 54.0 644.8	71.26 92.19 57.6 2 × 80 × 167.31 87.08 54.4 2 × 40 1 × 80	60 68.01 87.66 54.8 3 × 80 × 2 60 63.64 82.03 51.3 2 × 40 1 × 80 1 20 44.25 57.04 47.5 1 × 40 1 × 80 1 80 42.08 54.24 67.8 2 × 40 × 9 0 0.00 0.0 × ×	111.05 142.80	114. 12 146. 01 60. 8 132. 01 168. 89 70. 4 78. 63 100. 60 62. 9 50. 52 64. 63 53. 9 43. 73 55. 95 69. 9 0. 00 0. 0. 0 119. 01 536. 08 63. 8
Indoor type substation : Mahaisaman(MN), Taksin(TS)	277. VII. VII. VIII. O	VIV. 40 44.53	V V20. V2 11V-V4 V1-V1	VI. V.	202, 20 40.0
Load-1 : Coincident load Load-2 : Kon-coincident load					

1. 1818 0. 9237 1. 1805 0. 9070 1. 1825 0. 9140 1.1820 0.9170 1. 1818 0. 9190 Diversity factor Power factor

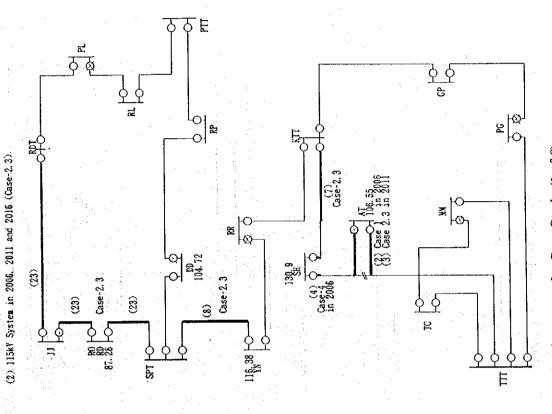






Figures indicated in parentheses are correspond to the expansion work numbers in Table 9.3-3.

Figures underneath symbol of substation mean the maximum load in MVA



(1), 115kV System in 2001

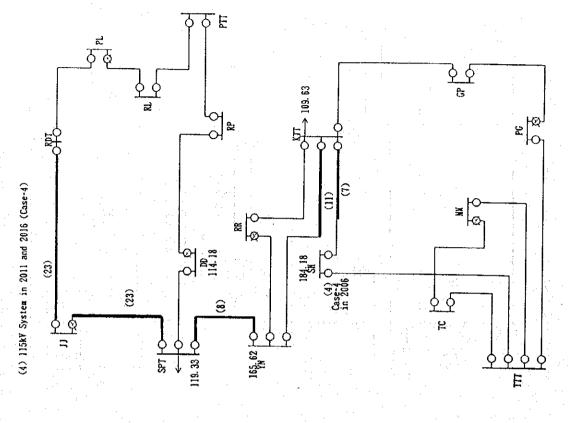
Series (2)

Series (2)

Series (3)

Ser

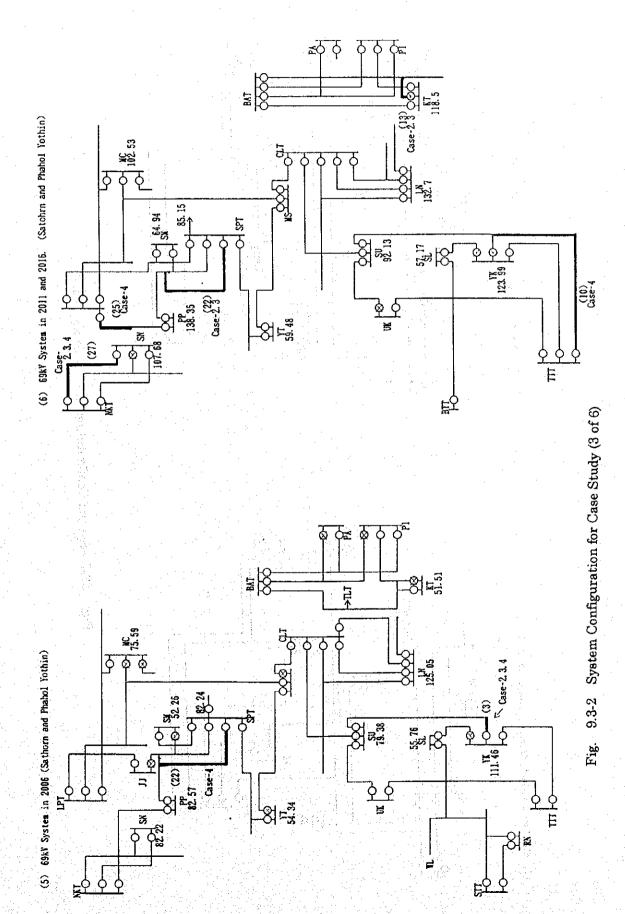
Fig. 9.3-2 System Configuration for Case Study (1 of 6)



8.1. 2

Fig. 9.3-2 System Configuration for Case Study (2 of 6)

(3) 115kV System in 2011 and 2016 (Case-1)



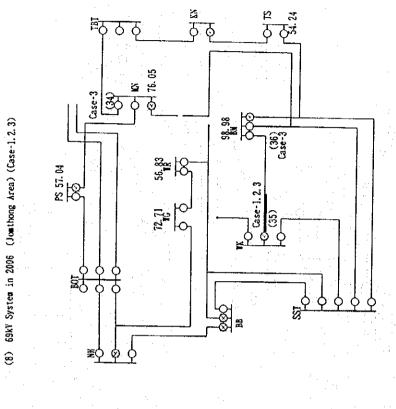
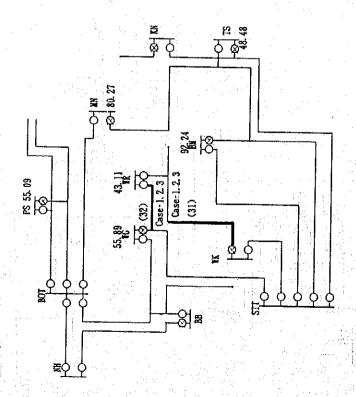
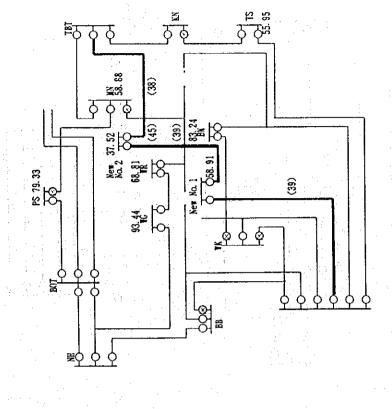


Fig. 9.3-2 System Configuration for Case Study (4 of 6)



(7) 69kY System in 2001 (Jonthong Area) (Case-1, 2, 3)



(10) 69kV System in 2011 and 2016 (Jomthong Area) (Case-1)

(9) 69kV System in 2001 and 2006 (Jomthwng Area) (Case-4)

FS 55. 09

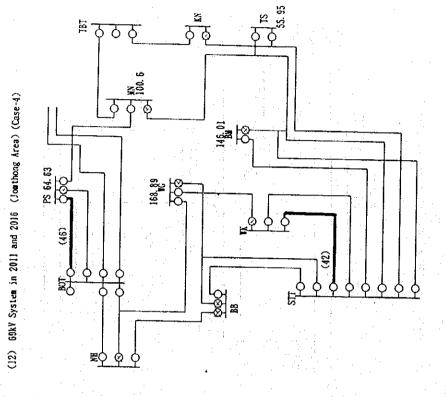
(34) in 2001

(34) in 2001

(34) in 2001

(35) in 2006

Fig. 9.3-2 System Configuration for Case Study (5 of 6)



| Section | Property |

Fig. 9.3-2 System Configuration for Case Study (6 of 6)

(11) 69kV System in 2011 and 2016 (Jouthong Area) (Case-2.3)

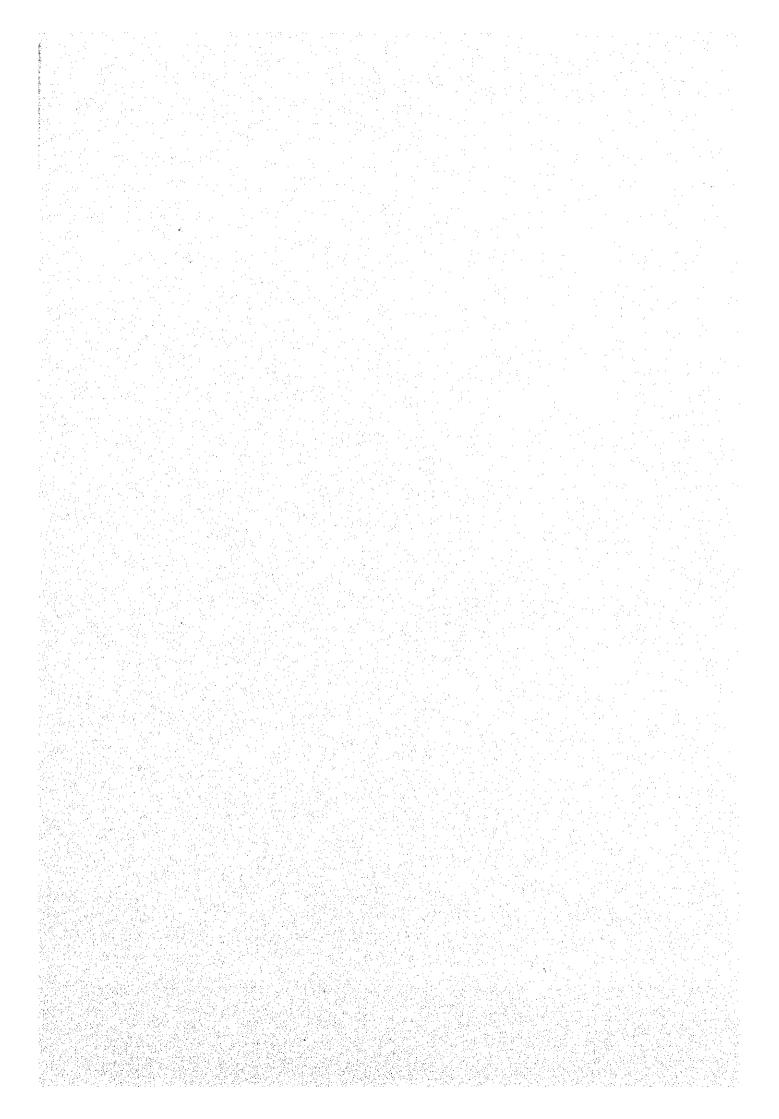
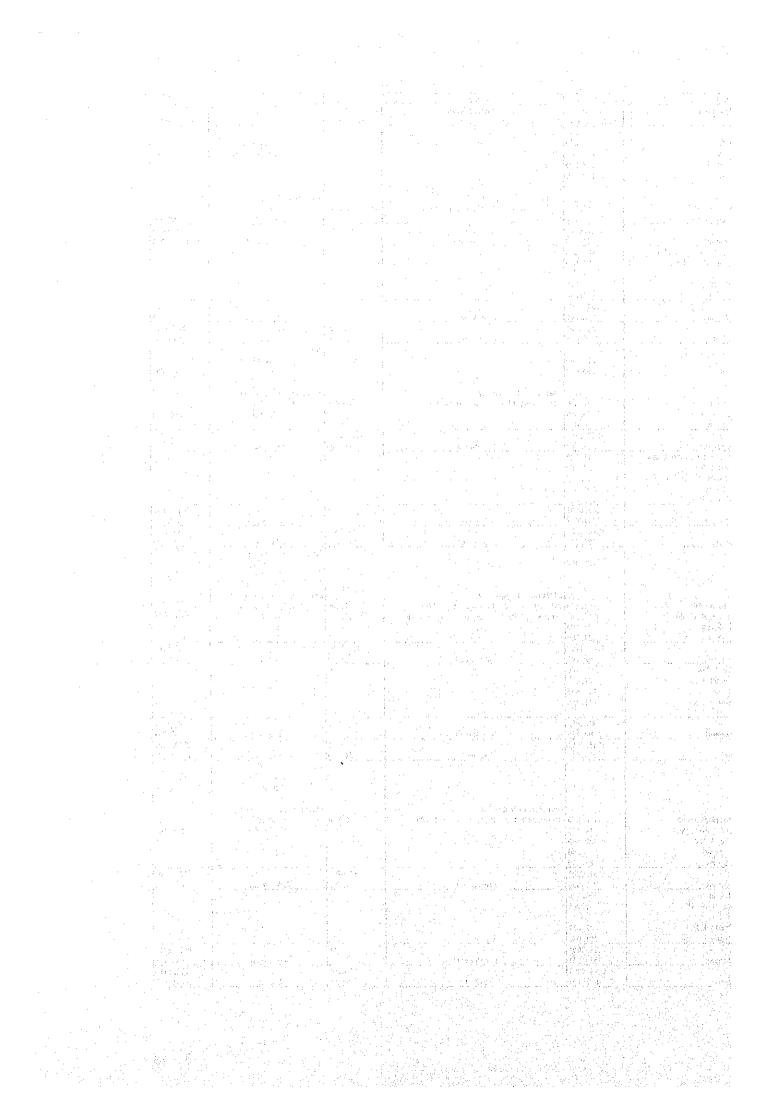


Table 9.3-3 (a) Cost of Case Study (Sathorn Area)

	2001		2006		2011		2016		Total Construction	Cost
	Construction	(1000 Baht)	Construction	Cost (1000 Baht)	Construction	(1000 Baht)	Construction	(1000 Baht)	Construction	(1000 Baht)
-1 Substation	New Samyarn(YN) : 2×40 (115kY) Satorn(SH) : 3×40 (115kY)		New Satorntai (AT) : 2×40 (115kV)		New New-substation 1: 2×40 New-substation 2: 2×40 New-substation 2: 2×40 New-substation 3: 2×40 New-substation 4: 2×40	152, 200 152, 200 152, 200 152, 200		**************************************	New 7 substations 600 MVA	1, 083, 80
			Addition of capacity Yenarkart(YK): 2×40 to 3×40 Samyarn(YN): 2×40 to 3×40	18, 400	4	17, 300 18, 400	Addition of capacity New-substation 3 : 2×40 to 3×40	18, 400	Addition of capacity 5 substations 200 MVA	89, 80 (791, 070
	Sub-Amount	(322, 800) 322, 800		(133, 970) 187, 900		(327, 630) 644, 500	Sub-Amount	(6, 670) 18, 400	Sub-Amount	1, 173. 6
Line	(1) Thanontok-YN-SH-Thanontok 2*400 14. 7km, 2*800 12. 5km	284, 500 52, 553	(2) Link Satorntai 2*800 1.0km		(5) New-ss 1, 2 Klongtoey loop 2*800 7km (6) New-ss 3, 4 Branch near YN and SH 2*800 4km (7) Klongtoey-Sat. Rd. 2*800 1.2km	159, 320 91, 040 27, 312				
		(337, 053)		(16, 230)	(8) Sanampao-YN 2*800 4.6km	104, 696 (194, 380)		0		(547, 66
	Sub-Amount	337, 053		22, 760	Sub-Amount	382, 368	Sub-Amount	(5.053)	Sub-Amount	742, 1
		(659, 853) 659, 853		(150, 200) 210, 660		(522, 010) 1, 026, 868	Amount	(6, 670) 18, 400	Amount	(1, 338, 73 1, 915, 1
≥-2 Substatio	Amount New Samyarn (YN) : 2×40 (115kY) Satorn (SH) : 3×40 (115kY)	152, 200 170, 600)	210,000	New Satorntai (AT): 4×40 New substation 1: 3×40	211, 200 170, 600			New 4 substations 480 MVA	701, 6
			Addition of capacity Yenarkart(YK) : 2×40 to 4×40(69kV) Samyarn(YN) : 2×40 to 3×40		Addition of capacity Klongtoey(KT): 2×40 to 4×40 Samyarn(YN): 3×40 to 4×40	61, 300 40, 600 40, 600)	40, 600	Addition of expacity 6 substations 320 MVA	262, 8
		(322, 800))	(56, 820)	Satorn(SH) : 3×40 to 4×40	(266, 530)		(14, 720)		(660, 8
	Sub-Amount	322, 800	Sub-Amount O(3) Link Yenarkart 2*800 0.1km	79,700	Sub-Amount (9) Klontoey-New-ssl Branch SH 2*800 2.0km	524, 300 45, 520		40,600	Sub-Amount	967.
Line	(1) Thanontok-YN-SII-Thanontok 2*400 14.7km, 2*800 12.5km	52, 653		2,00	(10) Link Satorntai 2*800 1.0km (11) Klongtoey-Sat. Rd. 2*800 1.2km (12) Sanampao-YN 2*800 4.6km (13) Link Klongtoey 2*800 0.5km	22, 760 27, 312 104, 696 11, 380				
		(337, 053)		(1, 430)		(107, 600)		0		(446, (
	Sub-Amount	337, 053		2, 000 (58, 250)		(374, 130)		(14, 720)	Sub-Amount	550, (1, 106, 9
	Amount	(659, 853) 659, 853		81,70		735, 968		40, 600	Amount	1,518,
e-3 Substatio		167, 000 167, 000	0		New Satorntai (AT) : 3×60	188, 300			New 3 substations 420 MVA.	522,
			Addition of capacity Yenarkart(YK) : 2×40 to 3×60	61,80	Addition of capacity Klongtoey(KT): 2×40 to 3×50 Lumpini(LN): 4×40 to 3×40+1×60 Samyarn(YN): 2×60 to 3×60 Satorn(SH): 2×60 to 3×60	61, 80 17, 00 21, 30 21, 30	Surawong(SU) : 3×40 to 2×40 + 1×60	17, 000 17, 000	Addition of capacity 7 substations 380 MVA	217.
		(334,000		(44, 060)	(157, 440		(12, 320) 34, 000	Sub-Amount	(547, 8 739,
Line	Sub-Amount (1) Thanontok-YN-SH-Thanontok 2*400 14.7km, 2*800 12.5km	334, 00 284, 50 52, 55	0 (3) Link Yenarkart 2*800 0.1km	61, 80	0 Sub-Amount 3 (2) Link Satorntai 2*800 1.0km (7) Klongtoey-Sat.Rd. 2*800 1.2km (8) Sanampao-YN 2*800 4.6km (13) Link Klongtoey 2*800 0.5km	309, 70 22, 76 27, 31 104, 69 11, 38	0 2 6	34,000	300 Asiount	100,
								-		(422, 9
	Sub-Amount	(337, 053 337, 05		(1, 430 2, 00		(84, 460 166, 14		0	Sub-Amount	505,
		(671, 053	0)	(45, 490)	(241, 900)	(12, 320) 34, 000	Amount	(970.
se-4 Substati	On New Samyarn(YN) : 2×80 (115kY)	671, 05 181, 00		181,00		475, 84	8 Amount		New 2 substations 320 MVA	362,
			Addition of capacity Yenarkart(YK) : 2×40 to 2×80	39, 00	Addition of capacity Klongtoey(KT): 2×40to115kV 2×80 Lumpini(LN): 4×40 to 3×40+1×80 Yenarkart(YK): 2×80 to 3×80	146, 00 19, 50 22, 80		19, 500	Addition of capacity 7 substations 480 MVA	316
					Samyarn (YN) : 2×80 to 3×80 Satorn (SH) : 2×80 to 3×80	34, 80 34, 80	ol			
		(181,000		(156, 860	0)	(131, 100)	(7, 070) 19, 500		(476, 678
Lîne	Sub-Amount (1) Thanontok-YN-Thanontok 2*400 14. 7km, 2*800 12. 3km		00 Sub-Amount 48 (4) Link Satorn 2*800 0.2km 53 (3) Link Yenarkart 2*800 0.1km		00 Sub-Amount 52 (10) Thanontok-YK 2*800 7.5km 03 (11) Klongtoey-Satorn Rd. link YN 115kY 2*800 1.8km	257, 90 150, 22 40, 96	8	19,000	Jun Vahari	010
					(7) Klongtoey-Sat.Rd. 2*800 l.2km (8) Sanampao-YN 2*800 d.6km	27, 31 104, 69			<u> </u>	
	Sub-Amount	(332, 60 332, 50		(5, 320 7, 4	0)	(164, 300 323, 20))	0	Sub-Amount	(502, 1 663,
	Voc Medit	(513, 50	1)	(162, 170	0)	(295, 400))	(7, 070)		(978, 1
	Amount	513, 5	01 Amount	227, 4	55 Amount	581, 10)1 Amount	19, 500) Amount	1,34

^{():} Present value of cost at 200

Interest: 7%



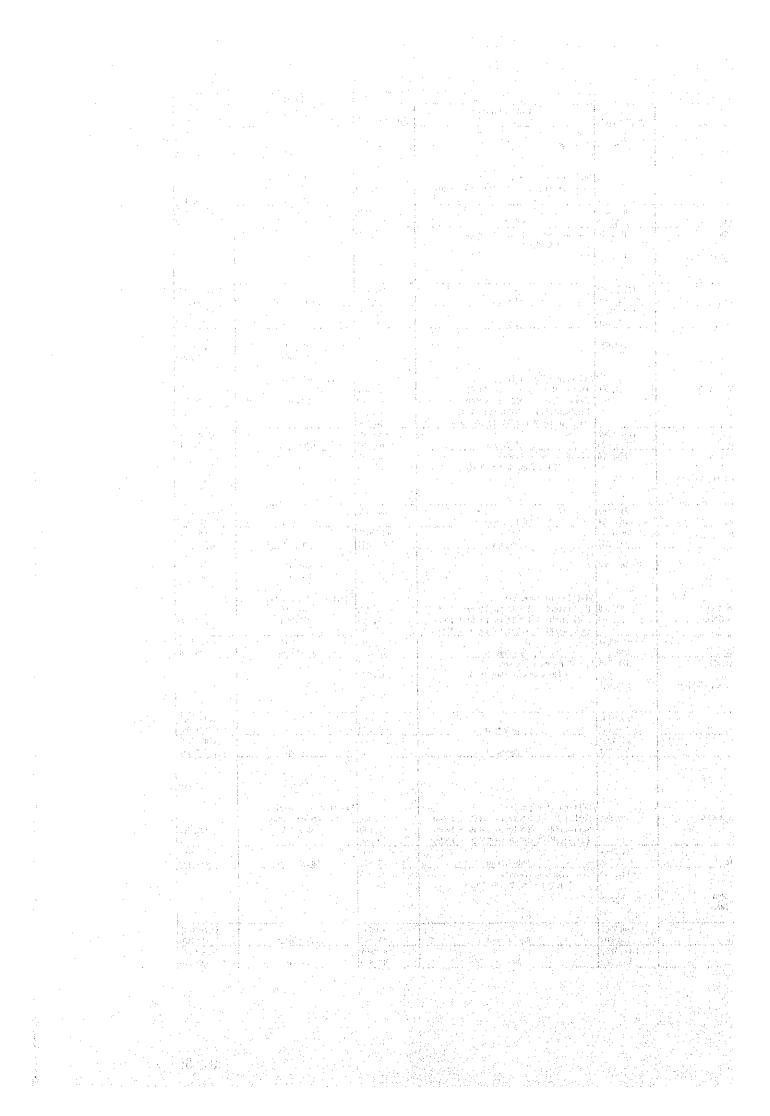
Skarn Aller Carrier Contract The Contract

Table 9, 3-3 (b) Cost of Case Study (Phahol Yothin Area)

	Į	2001		20		2011	C	2016	Park	Total	Post
		Construction	Cost (1000 Baht)	Construction	Cost (1000 Baht)	Construction	Cost (1000 Baht)	Construction	Cost (1000 Baht)	Construction	Cost (1000 Baht
9-1	Substation	New Dindaeng(DD) : 2×40		New Sanampao(NP) : 3×40		New Rajchakru(RO) : 3×40 New-substation 1 : 2×40		New- New-substation 2 : 2×40		New 5 substations 480 MVA	797, 8
:		Addition of capacity Pradipat(PP) : 2×40 to 3×40	17, 300	Addition of capacity Dindaeng(DD): 2×40 to 3×40	18, 400			Addition of capacity New-substation 1 : 2×40 to 3×40	18, 400	Addition of capacity 3 substations 120 MVA	54,
			(169, 500)		(134, 750)		(164, 100)		(61, 830)		(530, 1
	Line	Sub-Amount 115kV loop for Dindaeng	169, 500	Sub-Amount	189,000	Sub-Amount (23) Sanampao-RO-JJ-Ratchada	322, 800 150, 216	Sub-Amount (26) New-ss 2 Branch near DD	170,600 45,520	Sub-Amount	851,
	Line	(21) Ratchada-DD-Sanampao 2*400 2.0km, 2*800 8.2km	186, 632 7, 150			115kV 2*800 6.6km (24) New-ss 1 Branch near RO 2*800 5km	113, 800	2*800 2km			
			(193, 782)		0		(134, 210)		(16, 500)	Sub-Amount	(344, 4
		Sub-Amount	193, 782 (363, 282)		(134, 750)	Sub-Amount	264, 016 (298, 310)	Sub-Amount	45, 520 (78, 330)	SUD-AMOUNT	(874, 0
	<u> </u>	Amount	363, 282	Amount	189,000	Amount	586, 816	Amount	216, 120	Amount New	1, 355,
e-2	Substation	New Dindaeng (DD) : 2×40	152, 200	New Sanampao(NP): 3×40	170, 600	New Rajchakru(RO) : 3×40	170, 600			3 substations 320 MVA	493,
		Addition of capacity Pradipat(PP): 2×40 to 3×40	17, 300	Addition of capacity Dindaeng(DD) : 2×40 to 3×40	18, 400	Addition of capacity Pradipat(PP) : 3×40 to 4×40	44, 000	Addition of capacity Mochit(MC): 3×40 to 4×40 Samsen(SN): 3×40 to 4×40 Dindaeng(DD): 3×40 to 4×40	40, 600 44, 000 40, 600	280 MYA	245.
			(169, 500)		(134, 750)		(109, 090)	Rajachakru(RO): 3×40 to 4×40	40,600 (60,090)		(473,
		Sub-Amount	169, 500		189, 000	Sub-Amount	214, 600	Sub-Amount	165, 800		738.
	Line	115kV loop for Dindaeng (21) Ratchada-DD-Sanampao	186, 632			(23) Sanampao-RO-JJ-Ratchada 115kV 2*800 6.6km	150, 216	(27) N. Bangkok-Samsen 2*400 4. 5km, 2*800 0. 6km	12, 018 15, 025		
		2*400 2. 0km, 2*800 8. 2km	7, 150			(22) Sanampao-PP branch near Sailom 2*800 1.5km	30, 048				
			(193, 782)		, C		(91, 640)		(9, 800) 27, 043	Sub-Amount	(295, 40
	-	Sub-Amount	193, 782 (363, 282)		(134, 750)	Sub-Amount	180, 261 (200, 730)		(69, 900)		(768,
		Amount	363, 282	2 Amount	189,000) Amount	394, 86	Amount	192,843	Amount New	1, 139
e-3	Substation	New Dindaeng(DD): 2×60	167,000	New Sanampao(NP) : 2×60	167, 00	Kajchakru(RO) : 2×60	167, 006			3 substations 360 MVA	501
		Addition of capacity Pradipat(PP) : 2×40 to 2×60	34,000			Addition of capacity Pradipat(PP): 2×60 to 3×60 Dindaeng(DD): 2×60 to 3×60	27, 800 21, 300	l · · ·	17, 000 17, 000 17, 000	220 MVA	134
			(201, 000)		(119, 070		(109, 850)		(18, 480) 51, 000		(448, 63
-	Line	Sub-Amount 115kV loop for Dindaeng	201,00	0 Sub-Amount	167,00	0 Sub-Amount (23) Sanampao-RO-JJ-Ratchada	216, 10 150, 21	5 (27) N. Bangkok-Samsen	12,018	3	000
		(21) Ratchada-DD-Sanampao 2*400 2.0km, 2*800 8.2km	186, 63 7, 15			115kV 2*800 6.6km (22) Sanampao-PP branch near Sailom 2*800 1.5km	30, 04	2*400 4.5km, 2*800 0.6km	15, 025		
			(193, 782				(91, 640		(9, 800)		(295,
	 	Sub-Amount	193, 78 (394, 782	2 Sub-Amount	(119, 070	Sub-Amount	180, 26 (201, 490		(28, 290)		40 (743
		Amount	394, 78	2 Amount	167, 00	0 Amount	396, 36		78, 043	Amount	1,03
se-4	Substation	New Dindaeng (DD) : 2×80	181,00	New 0 Sanampao(NP) : 2×80	181,00	0				New 2 substations 320 MVA	36
				Addition of capacity Pradipat(PP) : 2×40 to 2×80	41,00	Addition of capacity Pradipat(PP) : 2×80 to 3×80	22, 80	Addition of capacity Mochit(MC): 3×40 to 2×40 + 1×80 Sailom(SM): 2×40 to 1×40 + 1×80 Samsen(SN): 3×40 to 2×40 + 1×80	19, 500 19, 500 19, 500	280 MVA	12
			(181,000		(158, 280		(11, 590		(21, 200))	(372
	Line	Sub-Amount 115kV loop for Dindaeng	181,00	0 Sub-Amount (12) Sanampao-PP branch near Sailor	222, 00 30, 04	0 Sub-Amount 5 (23) Sanampao-JJ-Ratchada	22, 80 147, 94	0 Sub-Amount 0 (27) N. Bangkok-Samsen	58, 500 10, 015		48
• .	Billo	(21) Ratchada-DD-Sanampao 2*400 2.0km, 2*800 8.2km	186, 63 7, 15	2 2*800 1.5km		115kV 2*800 6.5km (25) Lardprao-PP branch near Prachacuen 2*800 2.1km	42,06	2*400 4.5km, 2*800 0.6km	15, 02!		
			(193, 782	2)	(21, 420)	(96, 590)	(9, 080)		(320
		Sub-Amount	193, 78	32 Sub-Amount	30,04	5 Sub-Amount	190, 00	3 Sub-Amount	25, 040	0 Sub-Amount	43
	1 .		(374, 782	3) [(179, 700	N1	(108, 180	18 B	(30, 280)	J 1	(692

(): Present value of cost at 2001 Interest: 7%

.......

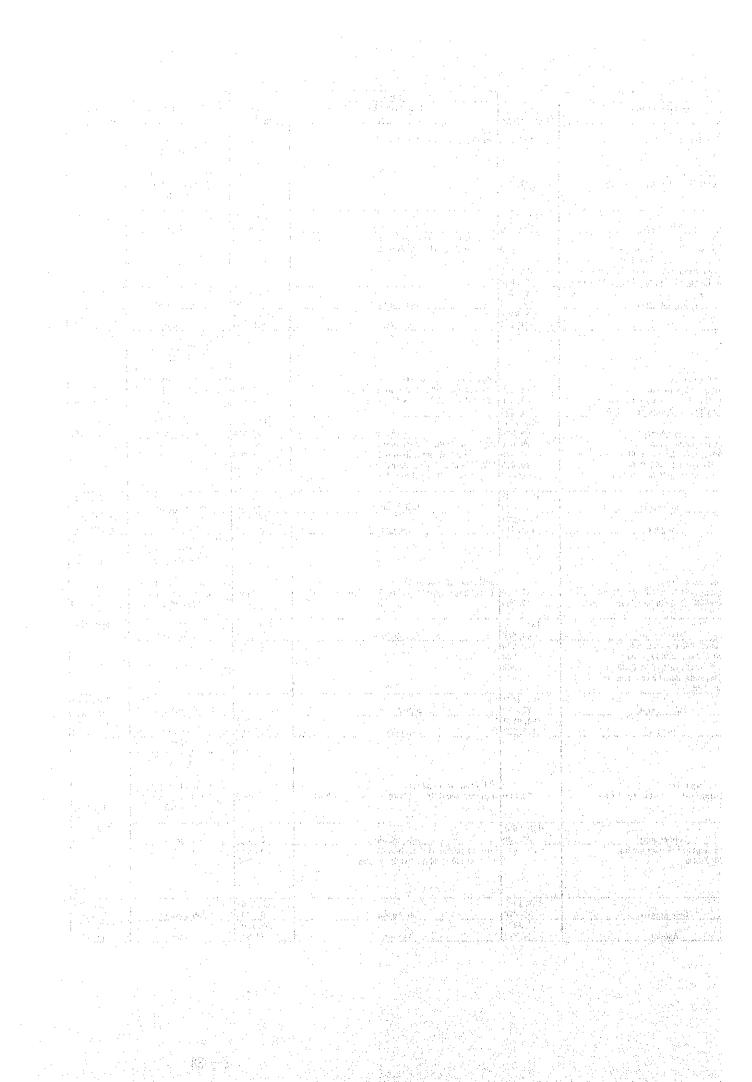


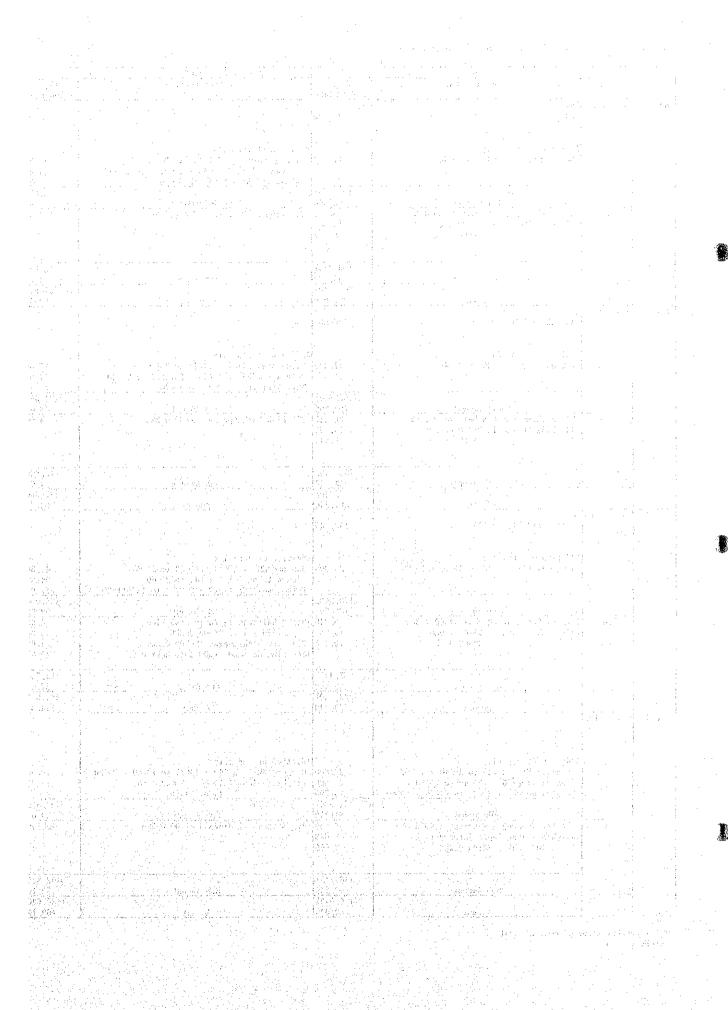
			en de la companya de La companya de la co		
The state of the s		e at le la			:
		· .			
			rangan di kacamatan di Kabupatèn di Kabupatèn di Kabupatèn di Kabupatèn di Kabupatèn di Kabupatèn di Kabupatèn Kabupatèn di Kabupatèn di Kabupat Kabupatèn di Kabupatèn di Kabupa		
		1.	and the second of the second of		
	•	:	· · · · · · · · · · · · · · · · · · ·		
		ling som en Segular i som en			
					:
and the second	The second secon	: 14/1			
Appendig Might Common to the Common of the C	and the first of the second of	filia Tanana			
Professional Control			reserve to the second of the s	1 1 1	
Leady to					
		ing. Kabupatèn			
		Artenia. Maiotoria		i	
					•
			Allen and the second of the se		e e
	in the control of the state of				:
				- :	
				· <u>:</u>	
			ing the state of t		

Table 9.3-3 (c) Cost of Case Study (Jomthong Area)

	т	2001		2006		2011		2016		Total	
	Ţ	Construction	Cost	Construction	Cost	Construction	Cost	Construction	Cost	Construction	Cost
	<u> </u>		(1000 Baht)		(1000 Baht)		(1000 Baht)	N	(1000 Baht)	M	(1000 Baht)
Case-1 S	ubstation	New Wuttakart(WR) : 2×40	136, 500			New Substation 1: 2×40	136, 500	New-substation 2 : 2×40	136, 500	New 3 substations 240 MVA	409, 500
		Addition of capacity Bangmod(BM) : 2×40 to 3×40	17, 300	Addition of capacity Kiongwatsing(WG): 2×40 to 3×40 Petchkasem(PS): 1×40 + 2×22.4 to 2×40 Wuttakart(WR): 2×40 to 3×40	17, 300 14, 000 17, 300	Addition of capacity Petchkasem(PS) : 2×40 to 3×40	17, 300			Addition of capacity 5 substations 155 MVA	83, 200
		Sub-Amount	(153, 800) 153, 800	Sub-Amount	(34, 650) 48, 600	Sub-Amount	(109, 660) 153, 800	Sub-Amount	(97, 320) 136, 500	Sub-Amount	(395, 430) 492, 700
<u> </u>	Line	(31) Watkampaeng-Ekachai 2*800 1.5km	30, 045	(35) Link Watkampaeng 2*800 0.2km		Thonburi-New-ss 1	100,000	(45) Interconnect New-ss 1 and ss 2	81, 984		
		(32) Link Wuttakalt 2*400 4.0km 2*800 0.5km	13, 380 10, 015			(38) Thonburi-Mahaisawan Rd. 2*400 2.1km, 2*800 1.0km (39) Mahaisawan RdNew-ss(Ekachai) -S.Thonburi 2*400 6km, 2*800 6km	20, 030 7, 025 120, 180 20, 070	Brabch line 2*800 2ckt 2km			
		Sub-Amount	(53, 440) 53, 440	Sub-Amount	(2, 860) 4, 096	Sub-Amount	(119, 290) 167, 305	Sub-Amount	(58, 450) 81, 984	Sub-Amount	(234, 040) 306, 735
-		Suo-Amount	(207, 240)	SQD-AROUTE	(37, 510)		(228, 940)		(155, 780)		(629, 470)
2 0 6		Amount	207, 240	Amount	52, 606	Amount	321, 105	Amount	218, 484	Amount New	799, 435
Case-2 S	Substation	New Wuttakart(WR) : 2×40	136, 500							1 substations 80 MVA	136, 500
-		Addition of capacity Bangmod(BM): 2×40 to 3×40	17, 300	Addition of capacity Klongwatsing(WG): 2×40 to 3×40 Petchkasem(PS): 1×40 + 2×22, 4 to 2×40 Wuttakart(WR): 2×40 to 3×40	17, 300 14, 000 17, 300	Klongwatsing(WG) : 3×40 to 4×40		Addition of capacity Petchkasem(PS): 3×40 to 4×40 Wuttakart(WR): 3×40 to 4×40	44, 000 44, 000		259, 200
			(153, 800)		(34, 650)		(75, 080)	Sub-Amount	(62, 740) 88, 000	Sub-Amount	(326, 270) 395, 700
	Line	Sub-Amount (31) Watkampaeng-Ekachai 2*800 1.5km	153, 800 30, 045	Sub-Amount (35) Link Watkampaeng 2*800 0.2km	48,600	Sub-Amount (38) Thomburi-Mahaisawan Rd.	105, 300 20, 030	(46) Bangkoknoi-Petchkasem	50, 075		390, 100
	Ditte	(32) Link Wuttakalt 2*400 4.0km 2*800 0.5km	13, 380 10, 015			2*400 2.1km, 2*800 1.0km (36) Link Bangmod 2*800 0.5km (40) Link K. watsing 2*800 0.3km	7, 025	2*400 2.5Km, 2*800 2.5km (47) Thonburi-Wuttakart	8, 363 60, 090 10, 035		
			(53, 440)		(2, 860)		(30, 710)	7.J. 4	(91, 660) 128, 563	Sub-Amount	(178, 670) 229, 088
	·	Sub-Amount	(207, 240)	Sub-Amount	4,006 (37,510)		43, 079 (105, 790)	Sub-Amount	(154, 410)		(504, 950)
		Amount	207, 240	Amount	52,606		148, 379	Amount	216, 563		624, 788
Case~3	Substation	New Wuttakart(WR) : 2×60	150,000							New 1 substations 120 NVA	150, 000
		Addition of capacity Bangmod(BM): 2×40 to 2×40 + 1×60	20, 300	Addition of capacity Bangmod (BM) : 2×40 + 1×60 to 3×60 Klongwatsing (WG) : 2×40 to 2×60 Petchkasem (PS) :1x40 + 2x22.4 to 1x40+1x60		Addition of capacity Klongwatsing(MG): 2×60 to 3×60 Mahaisawan(MN): 3x40 to 2x40 + 1x60	27, 800 17, 000	Addition of capacity Petchkasem(PS) : 1×40 + 1×60 to 2×60	17, 000	255 NYA	174, 600
i		C.I. I.	(170, 300) 170, 300		(65, 950) 92, 500		(31, 940) 44, 800		(12, 120) 17, 000		(280, 310) 324, 600
	Line	Sub-Amount (31) Watkampaeng-Ekachai 2*800 1.5km (32) Link Wuttakalt 2*400 4.0km 2*800 0.5km	30, 045 13, 380	(34) Mahaisawan-Tapra intersection	4, 006 3, 345 4, 685	(38) Thomburi-Mahaisawan Rd.	20, 030 7, 025 6, 009 40, 060				
			(53, 440)		(15, 720)		(52, 140)		()	1	(121, 300)
		Sub-Amount	(223, 740)		22, 049 (81, 670)		73, 124 (84, 080)		(12, 120)	Sub-Amount	148, 613 (401, 610)
		Amount	223, 740	Amount	114, 549		117, 924		17, 00	Amount	473, 213
Case-4	Substation									New O substations O MYA	
		Addition of capacity Bangmod (BM) : 2×40 to 2×40 + 1×80 Klongwatsing (WG) : 2×40 to 2×80 Mahaisawan (MN) : 3×40 to 2×40 + 1×80	39,000 19,500	1x40 + 1x80	19, 50 19, 50		22, 800	Addition of capacity Petchkasem(PS) : 1×40 + 2×80 to 3×80	19, 500	395 NVA	162, 600
			(81, 300		(27, 810		(16, 260)		(13, 900		(139, 270) 162, 600
	Line	Sub-Amount (33) Watkampaeng-K. watsing 2*800 2.0km (34) Mahaisawan-Tapra intersection 2*400 1.4km, 2*800 0.2kM	81, 30 40, 06 4, 68 4, 00	0 (37) S. thonburi-Bangmod 2*800 6.5km	39, 00 130, 19	0 Sub-Amount 5 (42) Souththonburi-Watkanpeang 2*800 2.6km	22, 800 52, 078	Sub-Amount (46) Bangkoknoi-Petchkasem 2*400 2.5km, 2*800 2.5km	19, 506 55, 076 8, 36		102,000
							(0=		(45, 550		(909, 000)
		Sub-Amount	(48, 749 48, 74	9 Sub-Amount	(92, 830 130, 19	Sub-Amount	(37, 130) 52, 07	Sub-Amount	(45, 230 63, 43	Sub-Amount	(223, 939) 294, 460
		A	(130, 049		(120, 630		(53, 390)		(59, 130 82, 93		(363, 199) 457, 060
L	<u> </u>	Amount	130, 04	9 Amount	169, 19	6 Amount	74, 87	3 Amount	82, 93	8 Amount	45

^{():} Present value of cost at 2001 Interest: 7%





	of early and a second of
	State in the state of
어느 그는 어느 아는 그는 그들이 가는 분들을 모양하는 이 그는 것이다. 그는 그렇게 뭐 그렇게 뭐 없었다.	
그 것이다. 그는 사람이 하는 것이 이렇게 되었다면 하는 것이 살을 사고 없는데 하는 것이 되었다.	
가는 이 그러는 그리고 그들도 있는데 이 문제에 가는 그는 말을 다고 한 날씨를 하는데 없다.	
하늘 그 말 시간이 다른 아내는 아내가 그런 그는 아이다. 그리다 살으면 함께	
그는 면서 이 물로 가게 되었다. 그들일 이 맛이 되고 하면 되지 않는 나는 바람이었다.	
할 때 보고 하는 사람들이 가게 들어보고 살았다. 하셨다면 하고 하는 것은 것 같아 없었다.	
그 그들은 많은 이번 이번 이번 사람이 사람이 살아 가는데 그런 모르는데 되었다.	
네 이 마이 이 이 그 모든 사람이 없는 방안 되었다면 하는 사람들은 모든 것 같은 전혀들할 수	
병원에 얼마나 그 아이들의 이렇는 회사회의 장면 방향 전, 이번 너를 다음한 경향 작용 작업	
입사 하다 하는 이 사람들이 그는 하는데, 그는 이 때문 그리는 그리는 그를 모양하는데,	
네 네가 그는 나는 이 이 전을 하는 사람이 하는 것들은 사람이 가장 모든 것이다.	
그는 이 그 이 그 집에 나는 한 때문 하루 보고 나라는 학생들은 나는 이 하는데 없는 것만	
어느 나는 이 이 사람이 나는 사람들이 되었다. 그렇게 하는 것이 하는 것이 때문에 가지 않는 것이다.	
그는 네트 그리다 하는데 교사가 되었다. 그런 교육들은 그렇게 한다고 되었다고 나를 모르겠다. 다	
는 사람들은 사람들이 되었다. 그 사람들은 사람들이 되었다. 그런 사람들은 사람들이 되었다. 그는 사람들이 되었다. 그는 사람들이 되었다. 그는 사람들이 되었다. 	
함께 보는 그는 어느 하고 하는 것 하는 것 하나 있다. 그는 하는 것 같은 사람들은 하는 것 같은 것이다. 그는 것이다는 것이다는 것이다. 그는 것이다는 것이다는 것이다는 것이다는 것이다는 것이다.	
Books -	
그리트 그는 그는 그 그 중에는 이 등만 한다고 하는 하는 것이 있는 것이 되는 것이 되었다. 그는 그 없는 그 없는 것이 되었다.	
그는 그는 이 사람들을 살았다. 그는 사람이 하는 사람이 동안 보고 함께 된 사람들은 사람들은 사람들은 사람들은 다음이 되었다.	
이 이 이 나는 이 그는 말을 데 그는 후 사람은 사람이 모두 모두 없다면 보고 하면 하셨다면 되었다.	
가는 사람들이 되었다. 하는 사람들이 많은 사람들이 많은 사람들이 되었다. 그 사람들이 사람들이 사람들이 바람들이 바람들이 되었다. 그 사람들이 바람들이 바람들이 되었다. 사람들이 바람들이 바람들이 바람들이 되었다. 사람들이 사람들이 사람들이 되었다.	
그 아이에 가는 모든 이 시설 하이면 아이지는 사람들에 밝힌 중요한 회사로 하는 경우를 통해 있다.	
되는 뭐 하는 그렇게 다른 바람이 많아 많아 나는 이 이번 이 아니라 나를 수 있는 것을 하는 것 같아.	
하는 것이 있는 것도 하면 되었다. 그는 사람이 되었다는 것이 되었다는 것이 되었다는 것이 되었다. 그는 것이 되었다는 것이 되었다는 것이 되었다. 	
그는 이 그는 그는 이 그는 아이들은 아이들은 그들은 이 아이들은 사람들은 사람들이 살아왔다. 그는 아이들은 사람들은 사람들이 되었다.	
마이트 등 사람이 되었다. 그는 사람들은 사람들은 사람들은 사람들은 사람들은 사람들은 사람들은 사람들은	
요요. 그는 그 그는 그들이 그렇게 되는 그는 그들이 되는 것들은 사람들 전에 가를 받는 경기를 받는 것을 하는 것을 하는 것을 하는 것을 하는 것을 하는 것을 하는 것을 했다. 하는 것으로 보는 것으로 보고 있는 것으로 살아 있는 것을 보는 보고 보고 있는 것을 보고 있는 것을 하는 것을 보고 있는 것을 보고 있는 것을 보고 있다면 것을 하는 것을 하는 것을 하는 것을 하는	

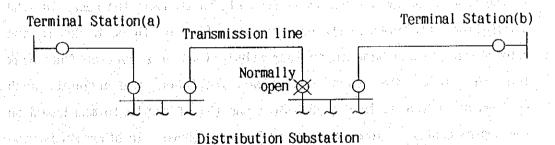
9.3.2 Economical Comparison of System Voltages using 115 kV and 69 kV System

The power is transmitted at 69 kV around the city center area and at 115 kV in the surrounding areas according to the patterns of the MEA's power system, but the 115 kV system tends to be further increased.

Therefore, the conditions of system configuration and operation, construction cost, economic and other conditions are compared in the cases of adopting 69 kV and 115 kV system configurations.

(1) Configuration of system models

Adopted in this comparison according to the planning criteria of MEA are the distribution substation consisting of three 60 MVA transformer banks and a so-called "tapped-tie normally open" as is shown Fig. 5.2-1(a) wherein the subtransmission line is connected from a terminal station to another terminal station through two distribution substations.



(2) Capacity of subtransmission line

Comment in the first the second and

The subtransmission line with a capacity satisfying the MEA's planning criteria is assumed to be constructed.

Capacity of subtransmission line (MVA) (using double conductor)

69 kV	115 kV
Normal Emergency	Normal Emergency
Overhead 192 212	288 308
Underground 192 212	288 308

(3) Load conditions

The normal allowable loads in the respective substations are assumed as follows where the utilization factor is 80%:

Distribution substation: $3 \times 60 \text{ MVA} \times 0.8 = 144 \text{ MVA}$

Terminal station : $4 \times 300 \text{ MVA} \times 0.8 = 960 \text{ MVA}$

Since the allowable load in two terminal stations is 1,920 MVA, it is possible to transmit the power to about 14 distribution substations.

(4) Overall system configuration

2 substations are installed directly to the respective terminal stations out of the 14 distribution substations, and the remaining 12 substations are received the power through subtransmission lines.

Judging from the capacity of subtransmission line, it is possible to transmit the power to two distribution substations through one circuit in the case of 115 kV system.

In the case of 69 kV system, it is possible to transmit the power in 1.33 substations (192/144 MVA), namely, a portion of three banks in one substation and one bank in another substation, or a portion four bank load in total. When these conditions are taken into account, such systems as indicated in Fig. 9.3-3(a) and (b) of can be formed based on the system configuration presented in Item (1) above. In other words, the outgoing line from terminal station shall be of double conductor, and line between distribution substations can be connected through single conductor in the case of 115 kV system. In the case of 69 kV system, however, a standby line is required in either one of the substations when shutdown of single side subtransmission line is taken into account. The capacity of the standby line should be sufficient to transmit a portion of two banks as indicated in Fig. 9.3-4. As a result, such a system as indicated in Fig. 9.3-3(b) of has been formed.

Although the standby line consisting of single conductor will be sufficient, the double conductor standby line should be adopted for coping with future changes of system conditions with flexibility.

(5) Unit construction cost

Based on the data obtained during the First Field Investigation, the following unit construction costs are used:

garage to the control of the control of the	69 kV	115 kV
Distribution substation 60 MVA 2 banks 1 bank addition	150,000 20,300	167,000 21,300
Subtransmission line (overhead) 1 ckt/km double conductor (underground) 1 ckt/km double conductor	3,344	3,575 22,757
Subtransmission line outlet CB	9,100	11,400

(6) Distance of subtransmission line

Although the actual system may undergo progress along with lapse of time, the construction cost of the entire model systems is compared herein. In other words, how the construction cost would vary between the 69 kV and 115 kV systems is examined by using the distance between the terminal station and distribution substation and that between mutual distribution substations as parameters. The shorter the transmission distance, the more advantageous in case the substation equipment cost is lower for the 69 kV system. However, the longer the transmission distance, the more advantageous in the case of 115 kV system requiring no standby line. In addition, the 115 kV system is further advantageous in view of the transmission loss as well.

Meanwhile, the construction cost and transmission loss are calculated on the assumption that the respective substations are arranged at an equal distance.

રેફ્રેન્ટ્રુક્સ ફ્રાફ્સ્ટન કરવામાં તે તેના લોકો સ્વારન હતું હોં ઉપતાર ફ્રોફન ઉપયોગ કર્યો હાથે છે. એ એ પાસન હતા હો જેવી સ

(7) Comparison between construction cost and annual expenses including transmission loss

As shown in Table 9.3-4(a), in case of underground cable line, the longer the distance between any two distribution substations is than $2.7~\rm km$, as a border in terms of construction cost, the more advantageous is the 115 kV system, but the shorter this distance is than this border, the more

advantageous is the 69 kV system.

If compared in terms of annual expenses including transmission loss, the border of advantage in distance is roughly 2.0 km. As a sensitivity test, the cost of substation outlet circuit breakers is calculated where the cost on the 115 kV system is assumed to be raised further by 10% (from 11. 4 million Baht to 12.54 million Baht). As a result of comparing the construction cost based on this calculation, the border of construction cost is about 3 km, and about 2.3 km when the transmission loss is included, as is presented in Table 9.3-4(b).

In the case of overhead line, the border of line distance becomes longer since the construction cost of subtransmission line becomes relatively lower. As a result of comparing the annual expenses including transmission loss, about 2.1 km is a border distance, as is presented in Table 9.3-4(c). Detail comparison is presented in Table 9.3-5(a) and (b).

(8) Results of study really a state of a result and the state of a real state of the state of th

The reinforcement of the 115 kV system is deemed to be the most advantageous in attaining simplification of the system, reduction of the number of subtransmission line circuits, saving of transmission loss and so forth, taking into account the various economic effects incurred from the unit construction costs and the choice between overhead and underground conductors. However, the 69 kV system can not necessarily be disregarded altogether, as the 69 kV network has already been widely equipped in the central area of Bangkok, and the road conditions are so diverse that in some places only 69 kV overhead line is possible instead of 115 kV overhead line.

tro de la calega, alguno como calitada e individade en la percepta a que calega que en la procesa de falla de

(9) Comparison between 230 kV and 115 kV distribution substations Comparisons have been made in constructing distribution substations of 80 MVA x 3 for several sites with 230 kV and with 115 kV systems respectively in the similar method as above-mentioned. When constructing 230 kV distribution substations, it will be possible to decrease the transformer capacity of terminal substation, but the unit cost of individual distribution substations will become higher than in the case of 115 kV substation.

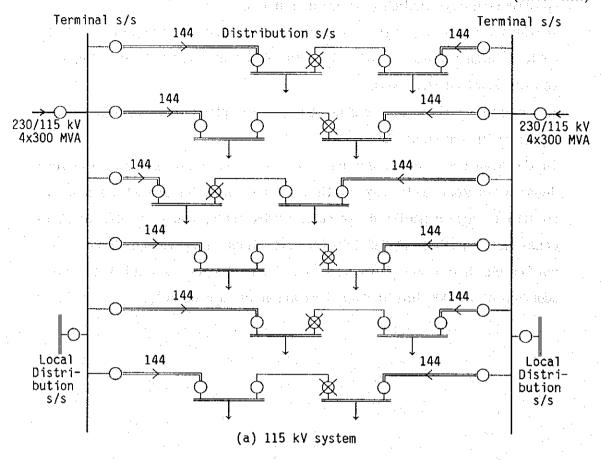
Therefore, the 115 kV plan will be advantageous in view of the construction cost including transmission line.

In the underground cable supply area, the construction cost of 230 kV cable is higher than that of 115 kV cable so that the 230 kV cable plan is apparently disadvantageous.

In the overhead line supply area, both of the plans indicate nearly equal values as indicated in Table 9.3-6.

In the area where construction of overhead line is possible, the load density is generally low so that there would be almost no need to construct large capacity distribution substation, and it is difficult to construct a number of 230 kV overhead lines along roads. When there conditions are taken into account, it is judged essential to avoid adoption of 230 kV distribution substation in such an area.

(Unit: MVA)



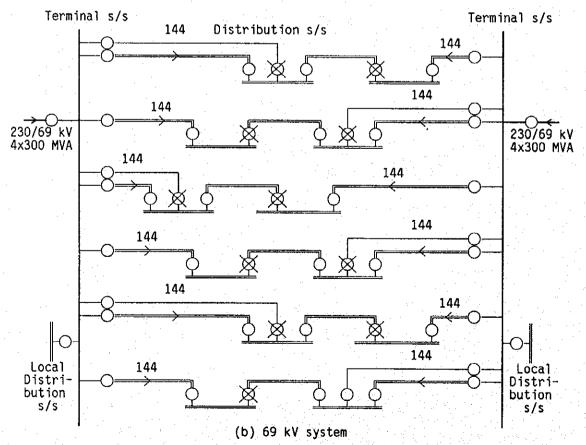
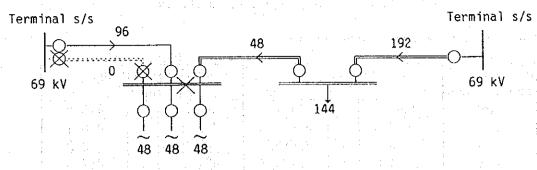
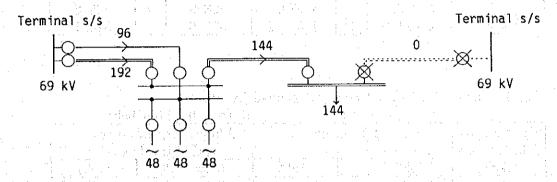


Fig. 9.3-3 Model System Configuration 9-40

(Unit: MVA)



(a) At the time of one of single line shut down of two lines



(b) At the time of single line shut down

Fig. 9.3-4 Load Flow at the time of single line shut down in Model System

Table 9.3-4 Cost Comparison Analysis

(a) In case of Underground Cable Line

Unit : Million Baht

Distance of	Construc	tion	cost	Annual Ex	pend	liture				
Substations				with Line Loss						
(km)	69kV	69kV 115kV		69kV		115kV				
1.9	3, 588. 5	<	3, 642. 5	475. 2	<	476. 7				
2.0	3, 636. 6	(3, 683. 5	<u>481. 9</u>	<	<u>482. 2</u>				
2.1	3, 684. 6			488. 7	>	487. 6				
2. 2	3, 732. 7	<	3, 765. 4	495. 4	. >	493. 1				
2.6	3, 924. 9	<	3, 929. 2	522. 2	>	515. 1				
2. 7	3,972.0	3,972.0 > 3,970.2		528. 9	>	520.6				
2.8	4, 021. 0	<u> </u>	4, 011. 2	535. 6	>	526. 1				

(b) In case of 115kV CB cost increased by 10%

Unit : Million Baht

		OHIC C MITITOH Danc								
Distance of	Construc	tion	cost	Annual Ex	pend	liture				
Substations		·	1	with Line Loss						
(km)	69kV		115kV	69kV		115kV				
2. 2	3, 732. 7	<	3, 788. 2	495. 4	<	496. 1				
2. 3	3, 780. 7	< ° ′	3, 829. 1	<u>502. 1</u>	-> -	<u>501. 6</u>				
2.4	3, 828. 8	3, 828. 8		508.8	>	507. 1				
2. 5	3, 876. 8	4	3, 911. 1	515.5	>	512.6				
2. 9	4, 069. 1	<-	4, 074. 9	542. 3	·>	534. 5				
3.0	<u>4, 117. 1</u>	>	<u>4, 115. 9</u>	549. 0	>.	540. 0				
3. 1	4, 165. 2	4, 165. 2 >		555. 7	>	545. 5				
3. 2	4, 213. 2	>	4, 197. 8	562. 4	>	551.0				

(c) In case of Overhead Line

Unit : Million Rab

		onic · Militon Danc							
Distance of	Construc	tion	cost	Annual Expenditure					
Substations				with Line Loss					
(km)	69kV		115kV	69kV		115kV			
2.0	2, 835. 9	<	2, 992. 9	398. 5	<	399.8			
2.1	2, 843. 9	<	2, 999. 3	<u>401. 0</u>	<	<u>401</u> . 2			
2.2	2,852.0	<	3, 005. 8	403.6	>	402.6			
2.3	2, 860. 0	<	3, 012. 2	406. 1	>	403. 9			
11.0	3, 558. 2	<	3, 572. 1	626.6	>	523. 4			
12.0	3, 638. 5	>	3, 636, 4	651.9	>	537. 1			
13.0	3, 718. 7	>	3, 700. 8	677. 3	>	550. 9			
14.0	3, 799. 0	>	3, 765. 1	702.6	>	564.6			

Table 9.3-5 Detailed Cost Data

(a) In case of Underground Cable Line on the assumption that distance between each substation is 2 km

each substat	1011-15	- 4		C 115 111							
		In Case	of <u>69kV</u>				of 115				
	No. of	Unit	Length	Cost	No. of	Unit	Length				
3	Unit	Cost	km	1000 BT	<u>Unit]</u>	Cost	km	1000 BT			
Terminal SS	2				2						
Main Tr 2ry CB	8	9, 100		72, 800		11, 400	i 1	91, 200			
Out going CB	12	9, 100		109, 200		11, 400	·	136, 800			
Spare Line CB	12	9, 100	5	109, 200	1 1			2 202 202			
Distribution SS	: 14	170, 300		2, 384, 200		188, 300		2, 636, 200			
Subtotal	 			2,675,400				2, 864, 200			
Transmission Line	18	,		720, 864				546, 168			
Transmission Line	6	20, 024	2	240, 288		,		273, 084			
Subtotal				961, 152	F	45, 514		819, 252			
Total cost			· · · ·	3, 636, 552				3, 683, 452			
Annual Expenditure	Maria .							070 040			
13% to Cost of SS	2150		1 1 1 1 1	347, 802				372, 346			
of Cable	1		14 E. S.	124, 950				106, 503			
Total Line Loss	k₩h/km		1 3 4 5 4	3, 011, 608	i '			1, 084, 179			
1.526 BT/kWh	1.526		2	9, 191			<u>2</u>	3, 309			
Total Expenditure				481, 943	<u> </u>			482, 158			

Loss Calculation

r at 20 °C =0.0224 ohm : r at 60 °C =0.02631 ohm for 800 sq.mm cable / km

Loss factor=0.5

1000	In	Case	of 69	kV		In	case	\mathbf{of}	115	kV	: · .		1
Base Loss/double conductor	<u> </u>	4.	1.11		57.30						<i>(</i>)	20.6	3
Total line Loss kW/km		1,			687.58		1		:	1.1		247.5	
Total Line Loss kWh/km				- 3.	011,608			1 - 1	4.13		1	, 084, 179	9

(b) In case of Overhead Line on the assumption that distance between each substation is 2.1 km

each substat	In Case of 69kV			In case of 115 kV				
					No. of		Length	
1	No. of		Length		, ,		km	1000 BT
	Unit	Cost	km	1000 BT	Unit	Cost	KIII	1000 D1
Terminal SS	2	in all part in		للمصد وي الروايا	2	1	1	
Main Tr 2ry CB	8	9, 100		72, 800	8	11, 400		91, 200
Out going CB	12	9, 100		109, 200	12	11, 400		136, 800
Spare Line CB	12	9, 100		109, 200	ļ. :			
Distribution SS	14	170, 300		2, 384, 200	14	188, 300		2, 636, 200
Subtotal		54.78.73.7	10 mg - 10 mg	2, 675, 400			J 	2, 864, 200
Transmission Line	18	3, 344	$\frac{1}{2.1}$	126, 403		3, 575	2.1	135, 135
Transmission Line	6		•	42, 134	1.6.5%		2.1	0
ましょれ あった 他でも ものつか。	y	1. 45-11		168, 538	1			135, 135
Subtotal				2, 843, 938			<u>-</u> -	2, 999, 335
Total	_			2,010,000	 	1		
Annual Expenditure			\$ 1.1.2	0.47 000			1	372, 346
13% to Cost of SS				347, 802				17, 568
of Cable			100	21, 910				
Total Line Loss	kWh/km	t dan v		9, 770, 843				3, 517, 504
1.526BT/kWh	1.526		2. 1	31, 312	L		2.1	11,272
Total Expenditure	1			401, 024				401, 186

Loss Calculation

r at 20 °C =0.0726 ohm : r at 60°C =0.08536 ohm for 400 sq.mm AAC conductor / km

LOSS TACTOR-0. 5		
	In Case of 69 kV	In case of 115 kV
Base Loss	185. 90	66.92
Total line Loss kW/km	2, 230, 79	
TOTAL TIME LOSS KW/Kiii	9,770,843	
Total Line Loss kWh/km	9,110,040	

Table 9.3-6 Cost Comparison between 230 and 115kV System

Installation capacity: 230/24kV 3*80MVA and 115/24kV 3*80 MVA In case of Overhead Line on the assumption that distance between each substation is 3.7~km

Equivalent capacity of 10 distribution SS 3*80MVA *10=2400MVA is added to 115kV side transformer capacity for Terminal stations

117	In Case of 230kV		In case of 115 kV					
	No. of	Unit	Length	Cost	No. of	Unit	Length	Cost
	Unit	Cost	km	1000 BT	Unit	Cost	km	1000 BT
	7.5							
Terminal SS	2				2			
Main trans 1*300MVA	0		2 3 45		8	47, 500	16.	380, 000
Main Tr. 1ry CB	0		A1	111	8	32,900		263, 200
Main Tr. 2ry CB	0			i i 0	8	11,400		91, 200
Out going CB	8	32, 900		263, 200	8	11, 400		91, 200
Spare Line CB	0	32, 900		0	8	11,400		91, 200
Distribution SS	10	269,000		2,690,000	10	188, 300		1, 883, 000
Subtotal	1 1		Market 1	2, 953, 200				2, 799, 800
Transmission Line	12	4, 422	3. 7	196, 337	12	3, 575	3. 7	158, 730
Transmission Line	0	4, 422	3.7	0	4	3, 575		
Subtotal				196, 337		7, 150		211, 640
Total	1 -			3, 149, 537	4 1 6 1		1.41	3, 011, 440
Annual Expenditure								
13% to Cost of SS				383, 916				363, 974
of Cable				25, 524			E. 145	27, 513
	kWh/km			1, 042, 223		1 s		4, 168, 893
1.526 BT/kWh	1.526		3. 7	5, 885			3.7	23, 538
		ar gr		ora diservice si		in Garage		
Total Expenditure				415, 324	A			415, 026

Loss Calculation

r at 20 °C =0.0726 ohm : r at 60 °C =0.08536 ohm for 400 sq.mm AAC conductor / km Loss factor=0.5

			4 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
	In Case of 230 kV	In case of 115 kV	And the latest
Base Loss/double conductor	29. 74		118.98
Total line Loss kW/km	237. 95	San to the	951.80
Total Line Loss kWh/km	1, 042, 223		4, 168, 893
			v Kaya Soci

Cost Comparison by Substation Distance

Distance of	Constru	uction Cost	Annual Expenditure with Loss			
Substations (km)	230kV	Comp. 115KV	230kV	Comp. 115kV		
4.0	3, 165. 5	3,028.6	417.8	419.2		
3.9	3, 160. 2	> 3,022.9	417.0	417. 8		
3.8	3, 154. 8	3,017.2	416. 2	416.4		
3.7	3, 149. 5	> 3,011.4	415.3	> 415.0		
3, 6	3, 144. 2	3,005.7	414.5	413.6		