9.5 Reservoir Sedimentation

The estimated amount of reservoir sedimentation is reported in Section 6.3.4 and tabulated below.

Because no more data were gathered in the course of Pre-feasibility Study Stage, the amount presented in Hydropower Potential Study Stage is applied to the Study.

Projects		C	atchment Area [km ²]	Specific Annual Yield [ton/km ² /y]	Sediment Volume after 100 years [10 ⁶ m ³]
Se Kong	No.4		5,400	419	226
Xe Kaman	No.1		3,800	420	160
Xe Namnoy	Mid		531	426	23
Xe Namnoy	Down		721	425	31

The above catchment area of the Xe Namnoy Midstream Project was changed from 537 km² by recheck of the catchment area.

The above catchment area of the Xe Namnoy Downstream project excludes the catchment area of the Midstream Project because the Downstream Project will be developed as a cascade project with the Midstream Project in terms of economic point.

Table 9.2 - 1Discharge Measurement Record
of Se Kong River at Sekong Town

· · .		•		1	
		Water			
· ·	ang	Level	Area	Velocity D	ischarge
No.	Date	[m]	[m2]	[m/s]	[m3/s]
1	93/11/06	2.35	567	0.30	167
2	93/11/11	1.23	489	0.23	111
3	93/11/11	1.22	484	2.08	100
4	93/11/19	1.15	502	1.43	68
. 5	93/11/26	2.88	566	3.67	197
6	93/12/01	2.82	535	3.61	180
7	94/01/10	1.54	569	1.19	60
8	94/01/15	1.48	518	0.92	46
9	94/01/20	1.42	588 :	1.04	- 58
10	94/01/29	1.36	545	0.88	50
11	94/02/05	1.42	483	0.93	49
12	94/02/11	1.30	412	0.80	- 41
13	94/02/18	1.31	380	0.62	29
14	94/02/24	1.20	404	0,65	31
15	94/03/12	1.20	419	0.79	
. 16	94/03/17	1.15	363	0.56	26
17	94/03/24	1.09	436	0.67	33
18	94/03/30	1.26	383	0.57	28
19	94/04/05	1.23	445	0.76	39
20	94/04/10	1.17	364	0.52	24
.21	94/04/21	1.50	491	1.00	53
22	94/04/26	1.42	447	1.00	50
23	94/05/08	1.13	465	0.76	38
- 24	94/05/15	1.52	471	0.94	49
25	94/05/20	2.32	508	1.17	64
26		1.99	463	1.09	58
27	94/06/01	2.02	472	1.08	-55
28	94/06/09	1.99	457	1.07	55
29	94/06/18	3.14	632	0.95	619
30	94/06/29	2.22	473	1.15	61
	Max	3.14			619
	Min	1.09		1.0	24

9 - 24

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			Converted			Discharge
		Water Level	Water Level			Measured
		at	at			at
		B. Hatsaykhao	B. Fangden	Area	Velocity	B. Hatsaykad
No.	Date	[m]	[m]	[m2]	[m/s]	[m3/s
1.	93/10/01	1.42	1,72	220	0.83	183
2	93/11/12	0.32		189	0,43	
3	93/11/16	0.30	0.60	186	0.39	72
4	93/11/26	0.40	0.70	198	0.43	84
5	93/12/07	0.61		223	0.60	.134
6	93/12/12	0.51	0.81	211	0.55	11(
	93/12/17	0.47	0.77	237	0.64	151
8	93/12/20	0.45		204	0.50	10
9	94/01/04	0.26		182	0.38	6
10	94/01/15	0.21	0.51	177	0.33	5
11	94/01/24	0.17		175	0.32	5
12	94/01/28	0.14	0.44	169	0.30	5
13	94/02/12	0.13	0.43	160	0.28	4
14	94/02/16	0.12	0.42	159	0.27	4:
15	94/02/18	0.11		158	0.27	4
16	94/02/24	0.09	0.39	157	0.25	4
17	94/03/03	0.08	0.38	155	0.24	3
18	94/03/08	0.07	0.37	154	0.23	
19	94/03/11	0.1	0.40	157	0.26	
20	94/03/28	0.06	0.36	154	0.22	
21	94/04/07	0.2	0.50	165	0.33	
22	94/04/24	0.22	0.52	166	0.35	
23	94/04/25	0.19	0.49	164	0.31	5
24	94/04/28	0.15	0.45	159	0.32	
25	94/05/14	0,28	0,58	172	0.39	
26	94/05/18	0.22	0.52	166	0.36	6
27	94/05/21	0.38	0.68	182	0.46	8
28	94/05/29	0.43		186	0.52	
	Max	1.42				18
·	Min	0.06	0.36			3

Table 9.2 - 2Discharge Measurement Recordof Xe Kaman River at B. Hatsaykhao

Table 9.2 - 3 Discharge Measurement Record of Xe Namnoy River at B. Latsasin

Date 91/05/17	Water Level [m]	Area		Sischarge	Index
91/05/17	[m]			levier de	
91/05/17		[m2]	(m/s)	[m3/s]	No.
	1.02	17.44	0.21	3.7	1
91/05/23	0,96	16.03	0.22	3.6	1
91/05/27	0.93	18.14	0.26	4.8	1
91/05/30	0.97	19.40	0.30	5.8	1
91/06/05	1.06	19.24	0.47	9.1	1
		-			· 1
					1
92/02/08					
92/02/11	0.74	14.02	0.17	2.4	1
92/02/14	0.74	14.05	0.18	2.5	1
	0,74	12.78			1
					1
1. 1. 1. 1.					· .]
and the second					1
			and the second		. ł
					1
92/03/23	0.58	8.48	0.08		1
92/03/23	0.56	8.52	0.08	0.7	1
92/03/26	0.53	5.11	0.09	0.5	1
92/04/03	0.52		0.09	0.4	1
					1
					1 1
	·				
93/10/22	1.74	90.20	0.36	32.5	er in d
93/10/27	1.68	85.10	0.22	19.1	
93/11/07			0.13	9.2	
					1. 1919 - 1919 -
93/12/20	0.99	62.50	0.20		
93/12/29	0.95	56.25	0.21	- 11.5	
	0.92	49.38	0.22		
94/02/08					
94/02/16	0.73	3.10	0.24		
94/02/25	0,78	3.65	0,28		
					1
94/04/30	1.12	3.85			
94/05/05	1.06	1.69	0.54	0.9	۱ (۱
94/05/10	1.28	2.34	0.53		
94/05/18					
94/06/30	2.37	114.75			
94/07/03	2.22	108.38	0.68		
94/07/07	2.33	105.50	0.95	100.1	
		267.00	2.16		
		a girth. A chuirtean			
	91/06/07 92/02/02 92/02/05 92/02/05 92/02/14 92/02/17 92/02/17 92/02/17 92/02/17 92/03/15 92/03/15 92/03/19 92/03/23 92/03/23 92/03/23 92/03/23 92/03/23 92/03/23 92/03/23 92/03/23 92/03/23 92/03/23 92/04/27 93/10/12 93/10/14 93/10/22 93/10/17 93/11/15 93/11/29 93/12/03 93/12/11 93/11/29 93/12/03 93/12/11 93/11/29 93/12/03 93/12/11 93/11/29 93/12/03 93/12/11 93/11/29 93/12/03 93/12/11 93/11/29 93/12/03 93/12/11 93/12/20 93/12/20 93/12/21 93/12/20 93/12/21 93/12/20 93/12/21 93/12/20 93/12/21 93/12/20 93/12/21 93/12/20 93/12/21 93/12/20 93/12/21 93/12/20 93/12/21 93/12/20 93/12/21 93/12/20 93/12/21 93/12/21 93/12/20 93/12/21 93/12/21 93/12/20 93/12/21 93/12/	91/06/07 1.03 92/02/02 0.77 92/02/05 0.76 92/02/08 0.74 92/02/11 0.74 92/02/12 0.74 92/02/14 0.74 92/02/17 0.74 92/02/16 0.67 92/02/26 0.67 92/03/01 0.65 92/03/15 0.62 92/03/23 0.56 92/03/23 0.56 92/03/23 0.56 92/03/23 0.58 92/03/23 0.58 92/04/23 0.50 92/04/27 0.47 92/04/27 0.47 92/04/29 0.48 93/10/18 1.87 93/10/12 1.74 93/10/27 1.68 93/11/29 1.24 93/11/29 1.24 93/11/29 1.24 93/12/29 0.95 94/01/26 0.76 94/01/26 0.76 94/01/26	91/06/07 1.03 21.68 92/02/02 0.77 14.42 92/02/05 0.76 14.22 92/02/11 0.74 14.05 92/02/14 0.74 14.05 92/02/17 0.74 14.05 92/02/17 0.74 12.78 92/02/26 0.67 12.21 92/03/01 0.65 12.41 92/03/15 0.62 10.34 92/03/15 0.62 10.34 92/03/23 0.56 8.48 92/03/23 0.56 8.52 92/03/26 0.53 5.11 92/04/23 0.50 4.71 92/04/23 0.50 4.71 92/04/29 0.48 4.43 93/10/16 1.87 95.90 93/10/22 1.74 90.20 93/10/27 1.68 85.10 93/10/27 1.68 85.10 93/11/27 1.21 61.25 93/11/27 1.61 8	91/06/07 1.03 21.68 0.40 92/02/02 0.77 14.42 0.18 92/02/05 0.76 14.22 0.17 92/02/06 0.74 14.05 0.20 92/02/11 0.74 14.02 0.17 92/02/12 0.74 12.78 0.20 92/02/23 0.69 12.36 0.16 92/02/26 0.67 12.21 0.15 92/03/15 0.62 10.34 0.09 92/03/15 0.62 10.34 0.09 92/03/23 0.58 8.48 0.08 92/04/03 0.52 4.94 0.09 92/04/03 0.52 4.94 0.09 92/04/23 0.50 4.71 0.08 92/04/23 0.50 4.71 0.08 93/10/14 1.69 77.10 0.13 93/10/12 1.74 90.20 0.36 93/10/12 1.74 0.20 0.36 93/10/12	91/06/07 1.03 21.68 0.40 8.6 92/02/02 0.77 14.42 0.18 2.6 92/02/05 0.76 14.22 0.17 2.4 92/02/06 0.74 14.05 0.20 2.8 92/02/14 0.74 14.05 0.18 2.5 92/02/12 0.69 12.36 0.16 2.0 92/02/23 0.69 12.36 0.16 2.0 92/02/26 0.67 12.21 0.15 1.8 92/03/04 0.65 12.44 0.14 1.7 92/03/15 0.62 10.34 0.09 1.9 92/03/23 0.56 8.48 0.08 0.7 92/03/23 0.56 8.52 0.08 0.7 92/03/23 0.56 8.52 0.08 0.7 92/04/23 0.52 4.94 0.09 0.4 92/04/23 0.50 4.71 0.08 0.3 92/04/23 0.48

Index No. = 1 : The data used in determination of the rating curve

	en de la composition de la composition de la composition de la	Water Level	Area	Velocity Di	schame
No.	Date	[m]	[m2]	[m/s]	[m3/s]
<u>1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 </u>	91/05/03	0.34	7.030	0.185	1.30
2	91/05/08	0.34	6.830	0.212	1.45
3	91/05/13	0.33	6.575	0.183	1.21
4	91/05/16	0.45	9,315	0.255	2.38
5	91/05/18	0.49	10,460	0.271	2.84
6	91/05/22	0.49	9.985	0.265	2.65
7	91/05/27	0.43	7.450	0.240	1.79
8	91/05/30	0.42	8.100	0.222	1.81
9	91/06/05	0.41	7.588	0.197	1.50
10	91/06/13	0.55	11.490	0.333	3.83
11	91/06/18	0.48	11.135	0.222	2.47
12	91/06/26	0.68	11.950	0.440	6.13
13	91/07/04	0.77	16.225	0.622	10.09
14	91/07/07	0.69	14.023	0.630	6.30
15	91/07/17	0.81	16.822	0.584	9.83
16	91/07/24	1.14	28.050	1.178	33.03
17	91/07/31	0.96	22.350	0.865	19.32
18	91/08/07	0.94	21.575	0.843	18.19
19	91/08/16	1.05	21.755	0.985	23.68
20	91/08/17	1.24	31.450	1.275	40.08
21	91/08/20	1.28	32,700	1.465	47.89
22	91/08/27	1.15	27.875	1.189	33.16
-23	91/08/29	1.16	27.850	1.270	35.36
24	91/09/03	0.96	20.150	0.934	18.82
25	91/09/15	0.93	19.850	0.869	17.26
26	91/09/18	0.84	17.666	0.796	14.07
27	91/09/25	0.94	21.194	0.923	19.56
28	91/10/04	1.13	27.413	1.294	35.49
29	91/10/09	1.02	22.655	1.032	23.37
30	91/10/16	0.90	18.280	0.893	16.34
31	91/10/23	0.76	15.635	0.629	9.85
32	91/10/30	0.67	14.027	0.455	6.39
33	1. I I I I I I I I I I I I I I I I I I I	0.60	12.102	0.421	5.10
34	91/11/27	0.50	9,899	0.304	3.01
35	91/12/04	0.46	9.366	0.270	2.54
36	91/12/11	0.44	9.946	0.270	2.69
37	91/12/18	0.43	8.302	0.220	1.83
38	91/12/25	0.40	8.172	0.226	1.85
	Max	1.28		÷ .	47.894
<u></u>	Min	0.33		· · · · · · · · · · · · · · · · · · ·	1.200

Table 9.2 - 4Discharge Measurement Recordof Xe Katam River at B. Nonghin (1/3)

<u></u>	······	Water				. —			Water			
		Level	Area	Velocity Di	ischarge				Level	Area		Discharge
No.	Date	[m]	(m2)	[m/s]	[m3/s]	. N		Date	[m]	[m2]	[m/s]	[m3/s]
39	92/01/02	0.38	8,603	0.206	1.78	. 8	6	92/07/01	1.04	22.642	0.986	22.32
40	92/01/08	0.38	8.848	0.227	2.01	8 - 18		92/07/04	0.86	17.218	0.738	12.71
41	92/01/15	0.36	8.495	0.192	1,63	8		92/07/07	0.79	16.014	0.648	10.38
42	92/01/21	0.36	8.573	0.203	1.74	8		92/07/10	0.78	16.009	0,622	9,96
43	92/01/29	0.34	7.894	0.192	1.51			92/09/01	1.18	33,55	0.352	11.82
44	92/02/03	0.33	7.495	0.187	1.40		91 :	92/09/04	1.07	24.31	0.454	11.049
45	92/02/08	0.33	7.523	0.190	1.43	-		92/09/08	0.93	21.821	0.82	17.889
46	92/02/12	0.32	7.419	0.177	1.13			92/09/08	0.93	21.821	0.820	17.89
47	92/02/15	0.32	7.389	0.171	1.27		14	92/09/15	0.83	17.900	0.699	12.52
48	92/02/19	0.31	7.361	0.154	1.13			92/09/18	0.80	15.817	0.707	
49	92/02/22	0.30	7.277	0.145	1.05		Ж	92/09/21	0.86	18.99	0.155	2.952
50	92/02/26	0.30	7.302	0.148	1.09		97	92/09/24	1.12	25.25	0.25	
51	92/02/29	0.30	7.410	0.141	1.05		8	92/09/27	0,96		0.208	4.577
52	92/03/04	0.30	7.540	0.148	1.12		99	92/09/30	0.86	21,595	0.191	41.143
53	92/03/07	0.28	7.044	0.116	0.82			92/10/05	0.79	15.974	0.746	11.93
54	92/03/11	0.28	7.054	0.113	0.80	10	D1	92/10/08	0.74	14.699	0.626	9.21
55	92/03/14	0.28	7.128	0.117	0.83	10	22	92/10/12	0.68	13,145	0.548	7.21
56	92/03/18	0.33	7 770	0.190	1.47		23	92/10/15	0.65	12,468	0.509	6.35
57	92/03/21	0.31	7.520	0.156	1.18	10	04	92/10/18	0.63	11.875	0.478	5.68
58	92/03/25	0.33	7.950	0.160	1.28	10	D5	92/10/22	0.59	11.172	0.447	5.00
59	92/04/01	0.32	7.770	0.149	1.16	. 10	96	92/10/25	0.60	11.550	0.443	5.12
60	92/04/08	0.30	7.460	0.141	1.05		07	92/10/28	0.58	10.991	0.421	4.63
61	92/04/11	0.29	7.288	0.119	0.87	- 11	80	92/10/31	0.61	12.024	0.452	5.44
62	92/04/18	0.46	9.482	0.253	2.40	. 1	09	92/11/02	0.58	11.001	0.423	4.66
63	92/04/22	0.39	8.621	0.223	1.92	1	10	92/11/05	0.55	10.682	0.426	4.56
64	92/04/25	0.38	8,607	0.207	1.78	1	11	92/11/08	0.53	9.762	0.361	3.53
65	92/04/29	0.34	7.776	0.192	1.49	1	12	92/11/11	0.52	9.750	0.360	3.52
66	92/05/02	0.40	8.420	0.214		1	13	92/11/14	0.50	9,440	0.369	3.49
67	92/05/05	0.42	8.710	0.218	1.90	1	14	92/11/17	0.49	9.300	0.337	
68	92/05/08	0.48	9.704	0.254	2.46		15	92/11/20	0.48	8.798	0.322	2.84
89	92/05/11	0.45	9.624	0.260	2.50			92/11/23	0.47	8.332	0.326	
70	92/05/14	0.48	9.812	0.292	2.87	. 1	17	92/11/26	0.46	7.823	0.308	2.41
71	92/05/17	0.50	10.221	0,306	3.13		18	92/11/30	0.44	7,362	0.275	
72	92/05/20	0.61	12.240	0.418	5,12		19	92/12/02	0.42	7.402	0.255	
73	92/05/23	0,50	10.520	0.317	3.33			92/12/05	0.42	7.402	0.263	
74	92/05/26	0.82	16.508	0.678	11.19		21		0.42	7.412	0.262	
75	92/05/29	0.70	14.288	0.518	7.40		22	92/12/12	0.40	6.885	0.237	
76	92/06/01	0.62	12.335	0.408	5.03		23	92/12/15	0.39	6.520	0.236	
77	92/06/04	0.76	15.384	0.583	8.97	1		92/12/18	0.39	6.520	0.239	
78	92/06/07	0.71	14.224	0.548	7.79		25	92/12/21	0.38	6.389	0.244	
79	92/06/10	0.73	15.040	0.551	8.29			92/12/24	0.38	6.389	0.253	
80	92/06/13	0.94	20.082	0.852	17.11		27	92/12/28	0.38	6.439		
81	92/06/16	0.92	19.086	0.818	15.61	1	28		0.41	7.101	0.260	
82	92/06/19	0.95	19.512	0.868	16.94			Max	1.48		1.00	86.40
83	92/06/22	1.04 :	22.038	1.018	22.43	· · · ·		Min	0.28			0.80
84	92/06/25	1.00	21.683	0.923		1.1		ي مروحه الم	1	1411		· .
85	92/06/28	1.48	39.562	2.184	86.40	· ·	12		an e ta		t (· · · ·

Table 9.2 - 4Discharge Measurement Recordof Xe Katam River at B. Nonghin (2/3)

		Water		Mataatt	Disaharra
		Level	Area	Velocity	Discharge
No.	Date	[m]	[m2]	[m/s]	[m3/s]
129	93/01/01	0.38	6.789	0.228	1.55
130	93/01/04	0.37	6.744	0.258	1.74
131	93/01/07	0.37	6.715	0.644	4.33
132	93/01/10	0.36	6.542	0.213	1.40
133	93/01/14	0.35	6.444	0.198	1.28
134	93/01/17	0.34	6,303	0.197	1.25
135	93/01/20	0.34	6.272	0.186	1.17
136	93/01/24	0.33	6.030	0.191	1.15
137	93/01/27	0.32	6.160	0.192	1.19
138	93/01/31	0.32	6.100	0.177	1.08
139	93/02/03	0.32	6.500	0.205	1.34
140	93/02/06	0.31	6.480	0.184	1.20
141	93/02/09	0.31	6.420	0.169	1.09
142	93/02/13	0.30	6.305	0.186	1.17
143	93/02/17	0.30	6.295	0.170	1.08
144	93/02/21	0.35	6,835	0.224	1.53
145	93/02/25	0.28	5.710	0.165	0.95
146	93/02/28	0.28	5.720	0.172	0.99
147	93/03/02	0.28	5.720	0.168	0.97
148	93/03/05	0.28	5.630	0,165	0.93
149	93/03/10	0.26	5.530	0.162	0.90
150	93/03/16	0.26	6.880	0.173	1.20
151	93/03/21	0.26	6.735	0.216	1.46
	Max	0.38			4.33
	Min	0.26			0.90
	a serie de l'étaire				

Table 9.2 - 4Discharge Measurement Recordof Xe Katam River at B. Nonghin (3/3)

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	Dra	Drainage Area :	vea :	5,400 km2	km2				•	· .	J	[m3/s]						
																	Annual	Annual
			•									1		Standard		L	NOV TIONNY	Ÿ
,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	-	4 C C	Mar	Δnr	May	lin i	10	Aud	Sep	500	Nov	Dec	Average	Deviation	Max	Min [x	r10^6m3]	
1001			INIO:					389	613	166	91		264	234.1	613	59	3,470	
	10	28	35	33	6	111	133	344	789	116	106	80	157	216.7	789	23	4,956	
1006		3	2 6		118	164	764	665	312	163	126	120	217	246.0	764	33	3 6,897	1,277
1000	3 6	4 (* F 4	5	8 8	65	146	642	612	316	153	194	116	207	211.2	642	38	6,570	
1098	1 8	3 5	5	8	110	123	134	224	121	329	134	95	124	82.2	329	38	3,928	
	y y	48	3	4	127	223	367	444	461	279	147	81	194	158.3	461	4	6,147	
	3 42			47	80	149	248	303	699	427	250	187	211	188.3	699	47	6,662	
1001	3 8	i ii	2	20	: 23	115	159	548	001	391	149	116	185	171.5	548	20	5,854	
1991		34	3 6	34	3 ▼	133	223	527	358	510	252	87	196	180.5	527	\$	6,212	:
1001	3 4	2 9	3	i.	24	67	135	473	248	199	142	202	144	125.4	473	49	4,579	
1001	2 a 2 a	S.	34	3 4	92	116	370	· · ·					105	120.0	370	41	1,936	Ì
Averano	3 3			42	86	135	318	453	432	273	159	114	181		•		5,201	6 63
St Dav	5 4	- 00	0	.	58	4	224	140	206	135	8	45		178				
2.00	2 0	2	5	8	127	223	764	665	789	510	252	202			789	-	6,897	1,277
X .S	34	58	52	ន	47	67	133	224	121	116	9	59				53	1,936	358
			11									· · ·		•			:	
Note -	Monthly Discharges based on regression analysis	ICTIALOGIE	baaed on I	regression	arnalyais :			1984 - July 1986		from E	3.Nanay in	Xe Done	B.Nanay in Xe Done River basin					
		•		•				987 - May 1988			3.Nanay in	Xe Done	B.Nanay in Xe Done River basin				•	
					 - -			1986 - Dec. 1986	9		Savannakhi	li in Xe D	Savannakhili in Xe Done River basin	nain Main			l • •	
			•	· .		•		1968 - May 1969	Ō		Attapu in Se Kong River basin	e Kong R	iver basin				1	•
					·	, 	Dec. 1989				Attapu in Se Kong River basin	e Kong R	iver basin				40 Z 2010	
- - 		• • • • • • •	,	-		. •	- 6	Nov. 1990		* .	Attapu in Se Kong River besin	e Kong R	iver besin					
		•						•••		. •	Attapu in Se Kong River basin	e Kong R	wer basin				· · · ·	•

Tale 9.2-5 Monthly Discharge of Se Kong No.4

9 - 30

Year Jan 1985 90.6 1986 62.8 1988 62.3 1988 37.6 1989 25.9 1990 20.7 1991 36.1 1992 52.5	Feb 58.9 36.3 36.3 36.3 252.7 111.7 111.7 111.7 27.6 27.6	Mar								•					Ó	Dumoff Vol	Disco and
		Mar											Standard		Ē.		Honur
		Mar		Marrie	1	1.1	Aun	Car	10 0	Nov	Dec	Dec Average	Deviation	Max	Min [x1	Min [x10^6m3]	E E E
90.6 90.6 37.6 25.9 20.7 20.7 20.7 20.7 20.7			Į	ABW			No.	316.7	293.0	320.8	164.6	285	68.8	330	165	3,763	066
90.6 90.6 37.6 25.9 20.7 20.7 20.7 20.7 20.7 20.7 20.7 20.7			(;	1	0 101	114 G	213.0	226.5	196.9	137.5	109.7	116	67.1	226	39	3,683	696
62.8 86.3 25.9 26.1 26.1 52.5 52.5		30.0	4 9 4 4 7	÷.	C 7 4		204 0	283.2	1000	170.2	245.3	145	114.6	322	16	4,600	1,211
86.3 37.6 25.9 26.1 36.1		18.4	16.0	2	2.10		0.034		30	172 8	82.3	84	60.5	195	13	2,661	200
37.6 25.9 20.7 36.1 52.5		32.0	14.0	· .			100.4	5 5	2.02	78.7	48.5	62	77 0	279	12	2,504	629
25.9 20.7 36.1 52.5	e generale e	15.2	12.4		2.0.7	0.00	1.73.1	2005	1.0.1	243	37.9	110	111.5	325		3,490	918
20.7 36.1 52.5		71	0 I 0 I		9.75	4 477	1.020	47.5	276.7	168.0	643	127	149.9	447	13	4,024	1,059
36.1 52.5	Ġ.	12.8	13.7			0 0 0	0.023	15.7	244.6	85.5	10	166	201.5	620	20	5,269	1,387
52.5		23.7	20.9		5.20		7.070	3440		145.1	57.9	150	126.8	402	4	4,744	1,249
	1 13	51.4	9.04	÷.,	0.011	210.0		1410				191	265.0	848	30	6.069	1,597
50.9		42.0	37.3	30.4	60.4	3/0.9	04/ A	200.2	5	5		200	103.5	321	ਲ	1,643	432
		34.4	39.7		83.6	320.0	CHC .	340	244		6	135				3,859	1,016
Average 51	g	58	24	0 4	ខ្ល	1/3	200				5 6	3	143			•	
	16	4	- - 	÷	5	8	RI7	2	5		3			010		E DEG	1 597
	59	5	14	130	138	377	848	205	377	321	240			0	t t		
	12	· ~	0	13	42	74	151	2	26	54	38				_	1.045	
								:		•							·
Note; Monthly Discharges based on regression analysis	charges ba	and on re	gression a	naiysis :		Aug. 1984 June 1998	1984 - May 1988 1988 - Oct. 1991	8 F	from	from Konturn in Dak Bla River basin Attapu in Se Kong River basin	Dak Bla F e Kong Ri	liver basin Iver basin					
							•			Attapu in Se Kong River basin	ie Kong R	iver basin					
			· . · ·	.:		Apr. 1993				Attapu in Se Kong River basin	ie Kong R	iver basin					
							& July 1994			Attapu in Se Kong River	ж Kong к	IVEL Dasin					

 Table 9.2 - 6
 Monthly Discharge [m3/s] of Xe Kaman No.1

 Drainage Area : 3,800 km2

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																	Annuai	Annual
	н.Э. 1			•			•			•	•	·		Standard			Runoff Vo.	Runoff
~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	<u>_</u>	, Li	Mar	Anr	Mav	uil.	hul.	Aug	Sen	ช 0	Nov	Dec	Average	Deviation	Max	Min	x10^6m3]	
		- 20						45.1	43.3	40.2	43.8	16.1	88	12	45	16	497	
1 200	7.7	a c	C C C	45	14.8	61.6	51.1	55.6	53.6	33.2	16.5	8.9	50	23	8	ີ. ເ	828	÷
200	1 8	200	) ( 	) () ()	15.6	19.5	23.8	66.5	60.4	41.0	30.1	11.3	23	8	67	` <b>+</b> ~	740	
280	r or	4.0	) r	4	12.5	20.2	94.3	89.9	45.6	21.2	16.5	6.2	56	ŝ	<b>94</b>	<del>.</del>	837	
280		i c	<u>ار</u>	4	14.8	29.8	22.6	45.4	17.2	28.3	14.8	47	16	4	45	•	495	
080		n ∧ i. <del>s</del>	40	en en	20.4	42.9	55.3	78.5	91.4	414	14.1	5.3	90	32	9	0	953	
	1 T r c		- 'C 		40	118	26.7	37.5	54.4	75.4	38.4	24.1	24	24	75	Ö	753	
200	, a , c	9.6		0.6	2	29.9	76.8	108.8	88.3	48.9	14.7	6.6	32	<b>6</b> 2	109	<b></b>	1,026	
500	o o i e	) r	1	0.6	6	15.9	415	72.9	55.1	32.3	11.2	5.7	20	24	73	•	646	
100		۲ I T		ŝ.	45	12.0	33.3	79.2	57.0	28.2	13.4	77	20	25	62	2	645	
	2	- C	) <del>-</del> -		86	12.6	43.8				- 		10	15	4	-	192	. 1
Averane	Ľ,			~	1-	56	47	68	57	68	21	9	24				692	1,303
St Dev	-	-	•	<del>.</del>	G	16	24	8	5	<u>φ</u>	5	Q	- 1 .	26				
,	~	4	m	4	5	8	2	109	9	75	44	24			109		1,026	1,931
	6	0	0	· .	2	5	23	38	17	21	- 11	5				0	192	36
] .									-									
Note :	Monthly Discharges based on regression analysis	charoes t	n no beset	egression a	anahosis :		Aug. 1984	Dec 15	from	B.Fangden in Xe Katam River basin	In Xe Katar	'n River b	asin				· . · .	
						-	May 1994 - Jul. 1994	Jul. 1994	LUI	B.Fangden in Xe Katam River basin	in Xe Katar	m River b	asin	•			÷	
	•																	

Sec. 1

Table 9.2-7 Monthly Discharge [m3/s] of Xe Namnoy Midstream Project

$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	Jan         Feb         Mar         Apr         May         Jun         Jul         Aug         Sep         Oct         Nov         Dec         Average         Deviation         Max           Jan         Feb         Mar         Apr         May         Jun         Jul         Aug         Sep         Oct         Nov         Dec         Average         Deviation         Max           25         1.8         1.4         5.8         21.2         17.8         19.2         18.6         11.9         6.4         3.9         9.5         7.1         21.2         22.9         23.0         14.4         10.9         4.6         8.6         7.4         22.9         23.0         14.4         10.9         4.6         14.8         14.8         12.1         4.9         14.8         22.9         23.0         14.4         10.9         4.6         13.9         14.8         23.0         30.6         16.0         7.4         22.9         23.0         30.5         14.4         3.0         95.6         10.4         6.4         33.9         10.9         8.6         10.9         8.6         10.4         10.9         35.0         30.0         10.1         10.1         10.1	Jan         Feb         Mar         Apr         May         Jun         Jul         Aug         Sep         Oct           3.3         2.2         1.9         2.4         5.8         21.2         17.8         19.2         18.6         11.9           2.5         1.8         1.4         5.8         21.2         17.8         19.2         18.6         11.9           2.5         1.8         1.4         5.0         6.1         7.4         8.8         22.9         20.8         14.4           2.1         1.7         1.5         1.4         5.0         7.6         32.0         30.6         16.0         7.9           2.1         1.7         1.5         1.4         5.8         10.8         8.4         15.9         6.6         10.3           2.2         1.8         1.4         5.8         10.8         8.4         15.9         6.6         10.3           2.1         1.1         1.1         2.0         7.6         13.1         18.2         25.8         25.8           2.0         0.9         1.4         5.1         2.1         3.1         18.2         25.6         6.9           1.2         <		Devis		Runoff Vol	₹₫
Jain         Feb         Main         Au         Main         Au         Main         Au         Main         Main<	Jain         Teo         Main         Main <th< th=""><th>Jain     Teu     Main     Ann     Main     Ann       3.3     2.2     1.9     2.4     5.8     21.2     17.8     19.2     18.6     11.9       2.5     1.8     1.4     2.0     6.1     7.4     8.8     22.9     20.8     14.4       2.1     1.7     1.5     1.4     5.0     7.6     32.0     30.6     16.0     7.9       2.1     1.7     1.5     1.4     5.8     10.8     8.4     15.9     6.6     10.3       2.2     1.8     1.4     5.8     10.8     8.4     15.9     6.6     10.3       2.2     1.8     1.4     5.8     10.8     8.4     15.9     6.6     10.3       2.3     1.5     1.1     2.0     7.6     32.0     30.6     16.0     7.9       2.3     1.5     1.1     2.0     7.6     19.2     26.8     31.0     14.6       2.0     0.9     1.4     1.7     4.0     20.1     18.6     25.6     6.9       1.2     1.1     1.1     2.1     2.1     3.1     18.2     28.0     24.6     19.4       1.4     1.1     1.2     1.3     3.6     5.4     14.4<th>11 -</th><th>-</th><th></th><th>Min [x10^6m3]</th><th></th></th></th<>	Jain     Teu     Main     Ann     Main     Ann       3.3     2.2     1.9     2.4     5.8     21.2     17.8     19.2     18.6     11.9       2.5     1.8     1.4     2.0     6.1     7.4     8.8     22.9     20.8     14.4       2.1     1.7     1.5     1.4     5.0     7.6     32.0     30.6     16.0     7.9       2.1     1.7     1.5     1.4     5.8     10.8     8.4     15.9     6.6     10.3       2.2     1.8     1.4     5.8     10.8     8.4     15.9     6.6     10.3       2.2     1.8     1.4     5.8     10.8     8.4     15.9     6.6     10.3       2.3     1.5     1.1     2.0     7.6     32.0     30.6     16.0     7.9       2.3     1.5     1.1     2.0     7.6     19.2     26.8     31.0     14.6       2.0     0.9     1.4     1.7     4.0     20.1     18.6     25.6     6.9       1.2     1.1     1.1     2.1     2.1     3.1     18.2     28.0     24.6     19.4       1.4     1.1     1.2     1.3     3.6     5.4     14.4 <th>11 -</th> <th>-</th> <th></th> <th>Min [x10^6m3]</th> <th></th>	11 -	-		Min [x10^6m3]	
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	33 $22$ $19$ $24$ $58$ $212$ $178$ $192$ $186$ $11.9$ $55$ $7.7$ $212$ $19$ $302$ $25$ $18$ $14$ $50$ $76$ $50$ $144$ $109$ $46$ $86$ $7.4$ $229$ $114$ $273$ $221$ $15$ $16$ $76$ $320$ $306$ $160$ $79$ $66$ $30$ $95$ $114$ $273$ $305$ $221$ $11$ $11$ $11$ $20$ $306$ $160$ $79$ $56$ $33$ $108$ $10.4$ $310$ $114$ $112$ $114$ $112$ $112$ $111$ $112$ $112$ $112$ $112$ $112$ $112$ $112$ $112$ $112$ $112$ $112$ $112$ $112$ $112$ $112$ $112$ $112$ $112$ $112$ $112$ $112$ $112$ $112$ $112$ $112$ $112$ $112$ $112$ $112$ $112$ $112$ $112$ $114$	3.3       2.2       1.9       2.4       5.8       21.2       17.8       19.2       18.6       11.9         2.5       1.8       1.4       2.0       6.1       7.4       8.8       22.9       20.8       14.4         2.1       1.7       1.5       1.4       5.0       7.6       32.0       30.6       16.0       7.9         2.1       1.7       1.5       1.4       5.8       10.8       8.4       15.9       6.6       10.3         2.2       1.8       1.4       5.8       10.8       8.4       15.9       6.6       10.3         2.2       1.1       1.1       1.1       2.0       7.6       32.0       30.6       16.0       7.9         2.2       1.8       1.4       5.8       10.8       8.4       15.9       6.6       10.3         2.3       1.5       1.1       2.0       7.6       4.0       2.8       9.7       13.3       18.9       25.8         2.0       1.4       1.2       4.0       20.1       18.6       37.7       25.6       6.9         1.4       1.1       1.2       1.3       3.6       5.4       14.4       20.0 <td>თ. დ. ო. ა</td> <td></td> <td></td> <td>3.4 159</td> <td></td>	თ. დ. ო. ა			3.4 159	
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	3.3     2.4     1.4     2.6     7.4     8.8     2.9     20.8     14.4       2.1     1.7     1.5     1.4     5.0     7.6     32.0     30.6     16.0     7.9       2.1     1.7     1.5     1.4     5.8     10.8     8.4     15.9     5.6     10.3       2.2     1.8     1.4     1.4     5.8     10.8     8.4     15.9     5.6     10.3       2.2     1.8     1.4     1.6     7.6     15.1     19.2     26.8     31.0     14.6       2.3     1.5     1.1     2.0     7.6     15.1     19.2     26.8     31.0     14.6       2.3     1.5     1.1     2.0     7.6     15.1     19.2     26.8     31.0     14.6       2.0     0.9     1.4     1.7     4.0     20.1     18.6     37.7     25.6     6.9       1.4     1.1     1.2     1.3     3.6     6.5     19.7     14.6     20.0     9.9       1.4     1.1     1.2     1.3     3.6     6.5     19.7     14.6     20.0     9.9       1.4     1.1     1.2     1.3     3.6     5.4     14.4     20.0     9.9 <tr< td=""><td></td><td></td><td></td><td>1.9 302</td><td></td></tr<>				1.9 302	
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	22     1.8     1.4     5.0     7.5     32.0     30.6     16.0     7.9       22     1.8     1.4     1.4     5.8     10.8     8.4     15.9     6.6     10.3       22     1.8     1.4     1.4     5.8     10.8     8.4     15.9     6.6     10.3       23     1.5     1.1     2.0     7.6     15.1     19.2     26.8     31.0     14.6       20     0.9     1.4     1.5     4.0     4.8     9.7     13.3     18.9     25.8       20     0.9     1.4     1.5     4.0     4.8     9.7     13.3     18.9     25.8       12     1.1     1.1     1.1     2.1     3.1     18.2     28.0     24.6     19.4       15     1.1     1.2     1.7     4.0     20.1     18.6     37.7     25.6     6.9       14     1.1     1.2     1.3     3.6     5.4     14.4     20.0     9.9       14     1.2     1.3     3.6     5.4     14.4     20.0     9.9       14     1.2     1.3     2.8     3.9     5.4     14.4     19.6     13.4				1.4 273	
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	21     1.1     1.5     1.4     5.8     10.8     8.4     15.9     6.6     10.3       23     1.5     1.1     2.0     7.6     15.1     19.2     26.8     31.0     14.6       20     0.9     1.4     1.5     4.0     4.8     9.7     13.3     18.9     25.8       20     0.9     1.4     1.5     4.0     4.8     9.7     13.3     18.9     25.8       12     1.1     1.1     2.1     3.1     18.2     28.0     24.6     19.4       15     1.1     1.1     2.1     3.1     18.2     28.0     24.6     19.4       14     1.1     1.2     1.7     4.0     20.1     18.6     37.7     25.6     6.9       14     1.1     1.2     1.3     3.6     6.5     19.7     14.6     20.0     9.9       14     1.2     1.3     2.8     3.9     5.4     14.4     10.6     13.4				1.4 305	
2.2 $1.4$ $1.4$ $1.4$ $1.4$ $1.4$ $1.4$ $1.4$ $1.4$ $1.4$ $1.4$ $1.4$ $1.4$ $1.4$ $1.4$ $1.6$ $1.1$ $2.1$ $31.0$ $14.6$ $5.6$ $3.3$ $10.8$ $10.4$ $31.0$ $1.1$ $343$ $220$ $0.9$ $1.4$ $1.5$ $4.0$ $4.8$ $9.7$ $13.3$ $18.9$ $25.8$ $13.6$ $8.9$ $8.7$ $7.9$ $25.8$ $0.9$ $277$ $216$ $1.1$ $1.1$ $1.1$ $2.1$ $3.8$ $2.5.8$ $13.6$ $8.9$ $3.1$ $1.8$ $2.1$ $8.8$ $10.5$ $280$ $1.1$ $222$ $280$ $21.7$ $11.7$ $280$ $21.7$ $11.7$ $28$ $21.7$ $11.7$ $28$ $21.7$ $11.7$ $28$ $3.9$ $5.4$ $14.4$ $12.2$ $20.0$ $11.1$ $220.0$ $11.1$ $220.0$ $11.1$ $220.0$ $11.1$ $220.0$ $11.1$ $220.0$ $11.1$ $220.0$ $21.1$ $22$	22       1.8       1.4       1.5       1.1       2.0       7.6       15.1       1.0       1.1       343         23       1.5       1.1       2.0       7.6       15.1       1.2       7.9       25.8       0.9       277         1       1.2       1.1       2.1       2.1       2.1       2.1       2.2       28.0       1.4       5.5       3.3       10.8       10.4       31.0       1.1       343         1       1.1       1.1       2.1       3.1       18.2       25.8       13.6       5.5       3.7       1.1       2.80       277       290       277       1.1       280       277       280       277       1.1       280       1.1       27       280       271       280       277       1.1       280       1.1       272       280       1.1       280       1.1       280       1.1       272       280       1.1       236       1.1       272       200       1.1       236       1.1       230       1.1       230       1.1       230       277       230       277       230       277       230       277       230       277       230       276	22     1.8     1.4     1.4     2.0     0.0     0.7       23     1.5     1.1     2.0     7.6     15.1     19.2     26.8     31.0     14.6       20     0.9     1.4     1.5     4.0     4.8     9.7     13.3     18.9     25.8       12     1.1     1.1     1.1     2.1     3.1     18.2     28.0     24.6     19.4       15     1.1     1.1     1.1     2.1     3.1     18.2     28.0     24.6     19.4       15     1.1     1.1     1.1     2.1     3.1     18.2     28.0     24.6     19.4       15     1.1     1.2     1.7     4.0     20.1     18.6     37.7     25.6     6.9       14     1.1     1.2     1.3     3.6     6.5     19.7     14.6     20.0     9.9       14     1.2     1.3     2.8     3.9     5.4     14.4     10.6     13.4	. :	÷		1.4 192	
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	23     1.5     1.0     1.0     1.0     1.0     1.0     1.0       20     0.9     1.4     1.5     4.0     4.8     9.7     13.3     18.9     25.8       12     1.1     1.1     1.1     2.1     3.1     18.2     28.0     24.6     19.4       15     1.1     1.2     1.7     4.0     20.1     18.6     37.7     25.6     6.9       14     1.1     1.2     1.3     3.6     6.5     19.7     14.6     20.0     9.9       14     1.2     1.3     2.8     3.9     5.4     14.4     20.0     9.9       14     1.2     1.3     2.8     3.9     5.4     14.4     20.0     9.9		:		1.1 343	
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	20       0.9       1.4       1.3       1.3       1.8       2.8       1.6       1.8       2.1       8.8       10.5       28.0       1.1       280         1       1.1       1.1       2.1       3.1       18.2       28.0       24.6       19.4       3.8       2.1       8.8       10.5       28.0       1.1       280         3       1.4       1.1       1.2       1.7       4.0       20.1       18.6       37.7       25.6       6.9       3.1       1.8       10.3       12.2       37.7       1.1       326         1       1.1       1.2       1.3       3.6       6.5       19.7       14.6       20.0       9.9       5.7       2.1       7.2       7.2       20.0       1.1       230         4       1.2       1.3       1.7       4.8       10.2       16.7       2.24       196       13.4       7.6       3.6       8.8       6.5       277         e       2.0       0.4       0.3       0.5       1.6       6.5       7.0       8.1       7.6       3.6       8.8       8.6       3.7       3.7       3.1       2.30       3.7       3.6       3.4 <td>20     0.9     1.9     1.3     1.0     2.0     2.4.6     19.4       1.2     1.1     1.1     2.1     3.1     18.2     28.0     24.6     19.4       1.5     1.1     1.2     1.7     4.0     20.1     18.6     37.7     25.6     6.9       1.4     1.1     1.2     1.3     3.6     6.5     19.7     14.6     20.0     9.9       1.4     1.2     1.3     2.8     3.9     5.4     14.4     20.0     9.9       1.4     1.2     1.3     2.8     3.9     5.4     14.4     20.0     9.9       1.4     1.2     1.3     2.8     3.9     5.4     14.4     20.0     9.9</td> <td></td> <td></td> <td></td> <td>0.9 277</td> <td></td>	20     0.9     1.9     1.3     1.0     2.0     2.4.6     19.4       1.2     1.1     1.1     2.1     3.1     18.2     28.0     24.6     19.4       1.5     1.1     1.2     1.7     4.0     20.1     18.6     37.7     25.6     6.9       1.4     1.1     1.2     1.3     3.6     6.5     19.7     14.6     20.0     9.9       1.4     1.2     1.3     2.8     3.9     5.4     14.4     20.0     9.9       1.4     1.2     1.3     2.8     3.9     5.4     14.4     20.0     9.9       1.4     1.2     1.3     2.8     3.9     5.4     14.4     20.0     9.9				0.9 277	
1       1.2       1.1       1.1       1.1       1.1       1.1       1.1       326         3       1.5       1.1       1.2       1.7       4.0       20.1       18.6       37.7       25.6       6.9       3.1       1.8       10.3       12.2       37.7       1.1       326         3       1.4       1.1       1.2       1.3       3.6       6.5       19.7       14.6       20.0       9.9       5.7       2.1       7.2       20.0       1.1       230         4       1.4       1.2       1.3       3.6       6.5       19.7       14.6       20.0       9.9       5.7       2.1       7.2       20.0       1.1       230         4       1.2       1.3       1.7       4.8       10.2       16.7       22.4       19.6       13.4       7.6       3.6       8.8       8.6       8.6       3.7       377       30         6       0.6       0.4       0.3       0.5       1.6       6.5       7.0       8.4       7.6       8.6       8.6       37.7       30       277       373         6.0       0.4       0.3       0.4       1.3       0.6	1       12       11       11       11       11       11       11       12       11       11       11       12       37.7       1.1       326         3       1.4       1.1       1.2       1.7       4.0       20.1       18.6       37.7       25.6       6.9       3.1       1.8       10.3       12.2       37.7       1.1       230         4       1.4       1.2       1.3       3.6       6.5       19.7       14.6       20.0       9.9       5.7       2.1       7.2       7.2       20.0       1.1       230         4       1.2       1.3       1.7       4.8       10.2       16.7       22.4       19.6       13.4       7.6       3.6       8.8       8.6       2.77       8.0       2.77       8.0       2.77       8.0       2.77       8.0       2.77       8.0       2.77       8.0       0.6       0.4       0.3       0.5       1.6.7       2.24       19.6       13.4       7.6       3.6       8.8       8.6       3.77       3.0       3.77       3.0       3.73       3.2       3.7       3.0       3.73       3.0       3.1       1.8       1.0.3       3.77 </td <td>12         11         11         11         11         21         21         22         23         25         63           15         11         12         1.7         4.0         20.1         18.6         37.7         25.6         6.9           14         1.1         1.2         1.3         3.6         6.5         19.7         14.6         20.0         9.9           14         1.2         1.3         2.8         3.9         5.4         14.4         10.7         15.7         13.4</td> <td></td> <td>). ·</td> <td></td> <td>1.1 280</td> <td></td>	12         11         11         11         11         21         21         22         23         25         63           15         11         12         1.7         4.0         20.1         18.6         37.7         25.6         6.9           14         1.1         1.2         1.3         3.6         6.5         19.7         14.6         20.0         9.9           14         1.2         1.3         2.8         3.9         5.4         14.4         10.7         15.7         13.4		). ·		1.1 280	
2       1.5       1.1       1.2       1.3       3.6       6.5       19.7       14.6       20.0       9.9       5.7       2.1       7.2       7.2       20.0       1.1       230         4       1.4       1.2       1.3       3.6       6.5       19.7       14.6       20.0       9.9       5.7       2.1       7.2       7.2       20.0       1.1       230         4       1.4       1.2       1.3       3.6       6.5       19.6       13.4       7.6       3.6       8.8       4.7       14.4       1.2       80         6       2.0       1.4       1.2       1.3       1.7       4.8       10.2       16.7       22.4       19.6       13.4       7.6       3.6       8.8       8.6       2.77       80         6.0       0.4       0.3       0.5       1.6       6.5       7.0       8.2       6.7       5.7       4.0       2.1       8.6       37.7       31.0       27.7       343         3.3       2.2       1.9       2.8       7.4       1.8       4.0       2.1       8.6       37.7       1.4       8.9       37.7       0.9       31.1       1.8 <td>2     1.5     1.1     1.2     1.3     3.6     6.5     19.7     14.6     20.0     9.9     5.7     2.1     7.2     7.2     20.0     1.1     230       4     1.4     1.2     1.3     2.8     3.9     5.4     14.4     5.7     2.1     7.2     7.2     20.0     1.1     230       4     1.4     1.2     1.3     2.8     3.9     5.4     14.4     1.2     1.3     4.7     14.4     1.2     80       6     0.6     0.4     0.3     0.5     1.6     6.5     7.0     8.2     6.7     5.7     4.0     2.1     8.6     8.6       3.3     2.2     1.9     2.8     7.6     3.6     6.7     5.7     4.0     2.1     8.6       3.3     2.2     1.9     2.8     7.6     3.6     6.9     3.1     1.8     8.6       3.3     2.2     1.9     2.1     3.1     3.1     8.4     8.9     8.6       3.3     2.2     1.9     2.1     8.4     13.3     6.6     6.9     3.1     1.8       1.2     0.9     1.1     2.1     3.1     3.6     6.9     3.1     1.8       1.2<td>1.0         1.1         1.2         1.4         1.1         1.2         1.3         3.6         6.5         19.7         14.6         20.0         9.9           1.4         1.1         1.2         1.3         3.6         6.5         19.7         14.6         20.0         9.9           1.4         1.2         1.3         2.8         3.9         5.4         14.4         19.6         13.4           2.4         1.7         4.7         4.8         10.7         16.7         77.4         19.6         13.4</td><td></td><td></td><td></td><td>1.1 326</td><td></td></td>	2     1.5     1.1     1.2     1.3     3.6     6.5     19.7     14.6     20.0     9.9     5.7     2.1     7.2     7.2     20.0     1.1     230       4     1.4     1.2     1.3     2.8     3.9     5.4     14.4     5.7     2.1     7.2     7.2     20.0     1.1     230       4     1.4     1.2     1.3     2.8     3.9     5.4     14.4     1.2     1.3     4.7     14.4     1.2     80       6     0.6     0.4     0.3     0.5     1.6     6.5     7.0     8.2     6.7     5.7     4.0     2.1     8.6     8.6       3.3     2.2     1.9     2.8     7.6     3.6     6.7     5.7     4.0     2.1     8.6       3.3     2.2     1.9     2.8     7.6     3.6     6.9     3.1     1.8     8.6       3.3     2.2     1.9     2.1     3.1     3.1     8.4     8.9     8.6       3.3     2.2     1.9     2.1     8.4     13.3     6.6     6.9     3.1     1.8       1.2     0.9     1.1     2.1     3.1     3.6     6.9     3.1     1.8       1.2 <td>1.0         1.1         1.2         1.4         1.1         1.2         1.3         3.6         6.5         19.7         14.6         20.0         9.9           1.4         1.1         1.2         1.3         3.6         6.5         19.7         14.6         20.0         9.9           1.4         1.2         1.3         2.8         3.9         5.4         14.4         19.6         13.4           2.4         1.7         4.7         4.8         10.7         16.7         77.4         19.6         13.4</td> <td></td> <td></td> <td></td> <td>1.1 326</td> <td></td>	1.0         1.1         1.2         1.4         1.1         1.2         1.3         3.6         6.5         19.7         14.6         20.0         9.9           1.4         1.1         1.2         1.3         3.6         6.5         19.7         14.6         20.0         9.9           1.4         1.2         1.3         2.8         3.9         5.4         14.4         19.6         13.4           2.4         1.7         4.7         4.8         10.7         16.7         77.4         19.6         13.4				1.1 326	
3     1.4     1.1     1.2     1.3     5.0     0.3     0.5     1.4     1.2     1.3     2.7     8.0       4     1.4     1.2     1.3     2.8     3.9     5.4     14.4     1.2     1.2     8.6       4     1.4     1.2     1.3     2.8     3.6     13.4     7.6     3.6     8.8     8.6       2.0     1.4     1.3     1.7     4.8     10.2     16.7     22.4     19.6     13.4     7.6     3.6     8.8     8.6       0.6     0.4     0.3     0.5     1.6     6.5     7.0     8.2     6.7     5.7     4.0     2.1     8.6       3.3     2.2     1.9     2.8     7.6     5.8     14.4     8.9     3.7     0.9     8.6       3.3     2.2     1.9     2.8     7.6     5.8     14.4     8.9     37.7     0.9     8.0       1.2     0.9     1.1     1.1     2.1     3.1     3.4     1.8     4.13.3     6.6     6.9     3.1     1.8     0.9     80	3     1.4     1.1     1.2     1.3     5.0     0.3     1.4     1.2     1.3     2.7     4.0     1.2     1.3     1.7     4.8     10.2     16.7     22.4     19.6     13.4     7.6     3.6     8.8     8.6       2.0     1.4     1.3     1.7     4.8     10.2     16.7     22.4     19.6     13.4     7.6     3.6     8.8     8.6       0.6     0.4     0.3     0.5     1.6     6.5     7.0     8.2     6.7     5.7     4.0     2.1     8.6       3.3     2.2     1.9     2.8     7.6     25.8     14.4     8.9     8.6       3.3     2.2     1.9     2.8     7.6     25.8     14.4     8.9     3.77     0.9     80       3.3     2.2     1.9     2.8     7.6     5.1     31.0     25.8     14.4     8.9       3.3     2.2     1.9     2.8     7.6     6.6     6.9     3.1     1.8     0.9     80       3.3     2.2     1.9     2.1     3.1     8.4     13.3     6.6     6.9     3.1     1.8       1.2     0.9     1.1     1.1     2.1     3.3     6.6     6.9 <td>1.4 1.1 1.2 1.3 3.0 0.3 19.1 17.0 20.0 0.3 1.4 1.2 1.3 2.8 3.9 5.4 14.4 2.6 1.7 1.8 10.7 16.7 27.4 196 13.4</td> <td></td> <td></td> <td></td> <td>1.1 230</td> <td></td>	1.4 1.1 1.2 1.3 3.0 0.3 19.1 17.0 20.0 0.3 1.4 1.2 1.3 2.8 3.9 5.4 14.4 2.6 1.7 1.8 10.7 16.7 27.4 196 13.4				1.1 230	
4         1.4         1.2         1.3         2.8         5.9         0.5         1.4         1.3         1.7         4.8         10.2         16.7         22.4         19.6         13.4         7.6         3.6         8.8         277         277         6         3.6         8.8         8.6         277         277         6.0         0.6         0.4         0.3         0.5         1.6         6.5         7.0         8.2         6.7         5.7         4.0         2.1         8.6         37.7         343         343         343         343         37.7         31.0         25.8         14.4         8.9         37.7         0.9         80         37.7         0.9         80         37.7         0.9         80         37.7         0.9         80         37.7         0.9         80         37.7         0.9         80         37.7         0.9         80         37.7         0.9         1.1         1.1         2.1         3.1         8.4         13.3         6.6         6.9         3.1         1.8         1.1         1.8         1.3         6.6         6.9         3.1         1.8         0.9         80           1.20.91.11.1	4         1.4         1.2         1.3         2.8         5.9         0.5         1.4         1.3         1.7         4.8         10.2         16.7         22.4         19.6         13.4         7.6         3.6         8.8         277         277         277         277         277         276         8.2         6.7         5.7         4.0         2.1         8.6         3.43         3.43         3.3         2.2         1.9         2.8         7.6         3.6         8.6         3.7.7         3.05         1.4         8.9         3.7.7         3.43         3.43         3.3         2.2         1.9         2.8         7.6         3.43         3.43         3.3.3         2.2         1.9         2.8         7.6         3.43         3.43         3.43         3.43         3.43         3.77         3.10         2.5.8         1.4.4         8.9         3.7.7         3.05         6.6         6.9         3.1         1.8         3.7.7         0.9         3.05         3.05         3.7.7         3.1         3.43         3.7.7         3.10         2.5.8         1.4.4         8.9         3.7.7         3.1         1.8         3.7.7         3.0.9         3.0.9         3.0.9	14 12 1.3 2.8 3.9 3.4 14.4 55 4.4 4.5 4.7 4.8 407 467 224 196 13.4				1.2 80	
e 2.0 1.4 1.3 1.7 4.8 10.2 16.7 22.4 19.6 13.4 7.0 3.0 8.6 37.7 4.8 37.7 3.43 3.3 2.2 1.9 2.8 7.6 21.2 32.0 37.7 31.0 25.8 14.4 8.9 3.1 1.8 37.7 0.9 80 1.2 1.1 2.1 3.1 8.4 13.3 6.6 6.9 3.1 1.8	e 2.0 1.4 1.3 1.7 4.8 10.2 16.7 22.4 19.6 13.4 7.0 3.0 60 8.6 0.6 0.4 0.3 0.5 1.6 6.5 7.0 8.2 6.7 5.7 4.0 2.1 8.6 3.3 2.2 1.9 2.8 7.6 21.2 32.0 37.7 31.0 25.8 14.4 8.9 1.2 0.9 1.1 1.1 2.1 3.1 8.4 13.3 6.6 6.9 3.1 1.8 1.2 0.9 1.1 1.1 2.1 3.1 8.4 13.3 6.6 6.9 3.1 1.8					776	
0.6 0.4 0.3 0.5 1.6 6.5 7.0 8.2 5.7 3.0 2.3 4.0 2.1 3.7 3.7 3.43 3.3 2.2 1.9 2.8 7.6 21.2 32.0 37.7 31.0 25.8 14.4 8.9 3.1 1.8 7.6 21.2 32.0 37.7 31.0 25.8 14.4 8.9 3.1 1.8 7.6 3.7 7 3.0 80	0.6 0.4 0.3 0.5 1.6 6.5 7.0 8.2 b.7 3.7 4.0 2.1 4.0 2.1 3.3 3.7 3.3 3.3 2.2 1.9 2.8 7.6 21.2 32.0 37.7 31.0 25.8 14.4 8.9 3.3 2.2 1.9 2.8 7.6 21.2 32.0 37.7 31.0 25.8 14.4 8.9 8.0 1.1 1.1 2.1 3.1 8.4 13.3 6.6 6.9 3.1 1.8 0.9 80 80 1.2 0.9 1.1 1.1 2.1 3.1 8.4 13.3 6.6 6.9 3.1 1.8 1.4 1.8 1.4 1.8 1.4 1.8 1.4 1.8 1.4 1.8 1.4 1.8 1.4 1.8 1.4 1.8 1.4 1.8 1.4 1.8 1.4 1.8 1.4 1.8 1.4 1.8 1.4 1.8 1.4 1.8 1.4 1.8 1.4 1.8 1.4 1.8 1.4 1.8 1.4 1.8 1.4 1.8 1.4 1.8 1.4 1.8 1.4 1.8 1.4 1.4 1.8 1.4 1.4 1.4 1.4 1.4 1.4 1.4 1.4 1.4 1.4		·		•	i	•
3.3     2.2     1.9     2.8     7.6     21.2     32.0     37.7     31.0     25.8     14.4     8.9     37.7     0.9     0.9       1     1     1     1     2.1     3.1     8.4     13.3     6.6     6.9     3.1     1.8	3.3     2.2     1.9     2.8     7.6     21.2     32.0     37.7     31.0     25.8     14.4     8.9     31.1     0.9     80       1.2     0.9     1.1     1.1     2.1     3.1     8.4     13.3     6.6     6.9     3.1     1.8       1.2     0.9     1.1     1.1     2.1     3.1     8.4     13.3     6.6     6.9     3.1     1.8			00	ľ		
12 0.9 1.1 1.1 2.1 3.1 8.4 13.3 6.6 6.9 3.1 1.8 0.9 80	12 0.9 1.1 1.1 2.1 3.1 8.4 13.3 6.6 6.9 3.1 1.8 0.9 80	<b>3</b> 3 2 2 1 9 2 8 7 6 2 1 2 3 2 0 3 7 7 3 1 0 2 5 8			31.1	•	2.0
	1001 Part 1	12 09 11 11 21 31 84 133 66 69		-			<b>2</b>

B.Latsasin in Xe Namnoy River basin Xe Set P/S in Xe Set River basin

Jan. 1965 - Dec. 1990 Jun & July 1994

Table 9.2-8 Monthly Discharge [m3/s] of Xe Katam River at B.Nonghin

			  			÷.				4. .*	•••		•	:			Annual	Annual
							• .		. *					Standard			Runoff Vol.	Runoff
Year	Jan	це р	Mar	Apr	Мау	nn	μĻ	Aug	Sep	ð	Nov	Dec	Average	Average Deviation	Max	Min	[x10^6m3]	[ພພ]
1984		.,.						61.7	59.4	55.3	60.1	18.8	51.0	18.2	61.7	18.8	673	69
1985	14	0.9	56	7.7	21.9	86.0	71.6	7.77	75.0	47.0	24.2	13.8	37.4	1 1 1	86.0	5.6	1,184	1,642
1986	8.2	5.2	3.3	6.1	22.9	28.3	34.2	92.8	84.4	57.7	42.9	17.0	33.6	30.6	92.8	3.3	1,064	1 47
1987	6.4	4.8	3.9	3.5	18.7	29.2	130.9	124.8	64.1	30.7	24.2	10.1	37.6		130.9	3.5	1,197	1,66(
1988	7 0	с Г	36	3.5	21.8	42.5	32.5	63.8	25.1	40.4	21.8	8.0	22.9		63.8	3.5	728	1,01
1989	7.3	ි හ ි හ	21	5.8	29.5	60.4	4 11	109.2	126.8	58.3	20.9	11.6	42.8		126.8	2.1	1,355	1 88
1990	6.2	1.6	3.7	6.6	14.4	17.8	38.2	53.0	76.1	104.9	54.2	34.6	34.1		104.9	1.6	1,081	1,500
1991	5.2	3.9	3.0	2.3	77	29.5	93.2	135.8	113.3	72.5	18.4	8.8	41.1		135.8	2.3	1,307	1.81
1992	5.7	3.6	3.0	3.3	8.3	47.0	65.3	123.2	88.1	38.0	14.2	7.7	33.9		123.2	3.0	1,077	1 49
1993	5.0	Э.Э	3.3	3.5	9.9	20.7	60.4	89.0	80.2	39.7	20.5	9.8	28.8	31.2	89.0	3.3	913	1,26
1994	5.1	2.8	3.0	6.1	13.6	19.4	60.0						15.7	20.5	60.0	2.8	292	40
Average	6.8	4.1	3.5	4.6	16.9	38.1	66.4	93.1	79.3	54.4	30.1	14.0	34.5		- 		1,087	1,508
St.Dev.	1.9	1.5	0.9	1.7	7.2	21.6	30.0	29.2	28.1	21.6	16.1	8.1		35.1				•
Max	11.4	6.9	5.6	7.7	29.5	86.0	130.9	135.8	126.8	104.9	60.1	34.6			135.8		1,355	1,880
Min	5.0	16	2.1	2.3	77	17.8	32.5	53.0	25.1	30.7	14.2	7.7				1.6	292	405

100

in propotion to the catchment area.

Table 9.2-9 Monthly Discharge [m3/s] between Xe Namnoy Mid and Downstream Projects

		•	•				-						Ctopdard		Ő	Dunoff Vo.	<b>3</b> 0000
	in the second second			•				•		-			orginala		2		
Veor lan	ц Ц	Mar	Anr	Мач	hul	Jub	Aug	Sep	0 0	Nov	Dec	Average	Deviation	Max	Min [x	[x10^6m3]	[mm]
							19.3	18.7	17.5	18.9	4.4	15.8	6.4	19.3	4.4	208	932
	σ	50	3	7.6	27.7	23.2	25.1	24.3	15.5	8.3	5.0	12.5	10.0	27.7	2.5	394	1,769
t iq		α i τ	2 C	6	96	11.5	29.9	27.2	18.9	14.2	6.1	11 3	96	29.9	1.8	357	1,600
, c		- <del>-</del>	) (C i -	999	0 0 0	41.8	39.9	20.9	10.3	8.3	3.9	12.5	14.3	41.8	1.8	399	1,787
	1 C 1 C	, α Γ	, a		14 1	10.9	20.7	8.6	13.4	2.6	3.2	7.9	6.0	20.7	1.8	251	1,127
i	ο 1 <del>-</del>	7	5	10.01	19.7	25.0	35.0	40.6	19.0	7.3	4.4	14.2	13.6	40.6	4.1	448	2,011
: 		σ. • •	5 1 1	2	63		17.4	24.6	33.7	17.8	11.6	11.4	10.3	33.7	1.2	362	1,624
1001 1 A	<b> </b>	, 4 , 4	4	10	4	23.8	36.6	32.1	25.3	5.0	2.7	11.5	13.7	36.6	4	366	1,641
. 0	- IC	2	22	2.2	26.3	24.3	49.3	33.4	9	4.0	2.4	13.4	16.0	49.3	1.5	426	1,909
1003 1.0	, r	, <u>.</u>		4	84	25.7	19.0	26.1	13.0	7.4	2.7	9.5	9.4	26.1	1.5	300	1,346
	- <del>-</del>	) 	90	) - -	71	18.9						5.7	6.2	18.9	1.5	105	470
	6	17	2.3	6.3	13.3	21.8	29.2	25.6	17.6	6.6 6	4.6	11.5				362	1,622
	20	е О	0 7	5	8	- 0,	10.7	8.8	7.4	5.2	2.7		11.2				
4	6	2.5	3.6	10.01	27.7	41.8	49.3	40.6	33.7	18.9	11.6			49.3		448	2,011
- <del>-</del>	12	4	4	2.7	4	10.9	17.4	8.6	9.1	4.0	2.4				1.2	105	470

Table 9.2-10 Monthly Discharge [m3/s] of Xe Pian Diversion Scheme

Drainage Area 223 km2

T

Table 9.4 - 1 Design Monthly Evaporation

Monthly Evaporation [%]

Annual [%]	101.0	101.2	100.7		
Dec	10.1	11.9	10.01		
Nov	7.9	10.9	6.3		
ъ С	6.6	0.7	73		•
Seo	4.9	4	5.4		· .
AIN	4.2	5.0	5.9		
	4.9	5.5	6.5		
	5.0	4 4	6.6		
May	8.2	9.1°	7.3		
Apr	12.1	81	8.2		
Mor	14.6	12.9	10.7	5 	
	11.7	12.5	12.8		
	11.0	9.5	10.7		
	-		-	2	· · ·
	[%]		14 [%]		
	Pakse	Attapu	Nikhon		

Monthly Evaporation [mm]

9 - 36

	lan	Feb	Mar	Apr	May	- un	InC	Aug	Sep	ođ	Nov	Dec	Annual
Se Kond No 4	109	116	144	120	82	49	48	41	48	. 65	78	100	1,000
Ye Kaman No 1	103	136	140	88	86	48	29	5	205	76	118	130	•
Ve Maman	50	114	Ч.	73	gg	23	58	53	48	66	83	89	:
AE NAITINY	3		2	2	3	2							

Note : Annual evaporation is quoted from "Interim Report, Nov,1993"

Fig.9.2-1 River Cross Section of Se Kong River at Sekong Town Gauging Station

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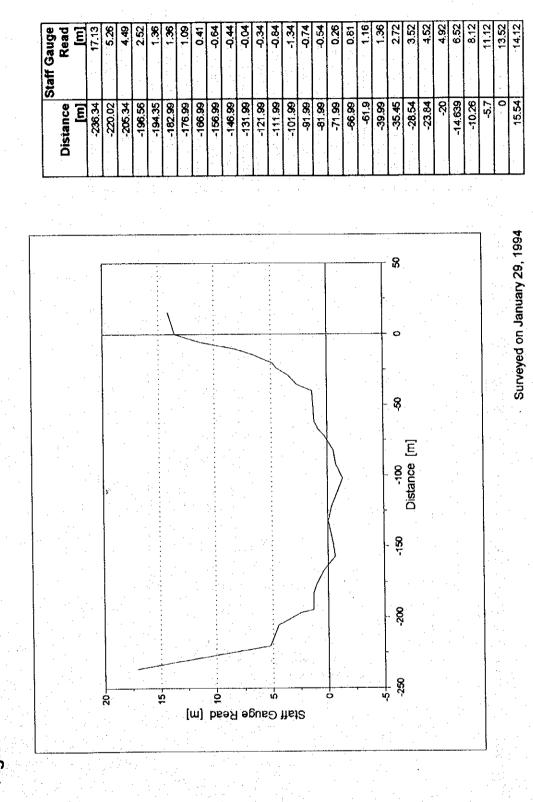
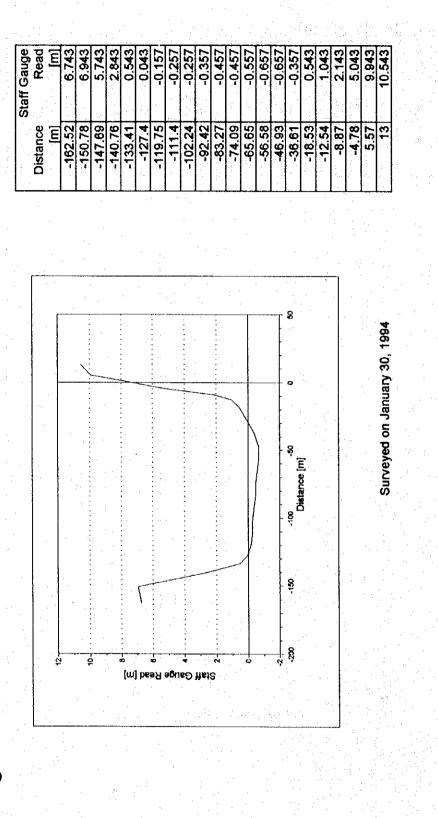
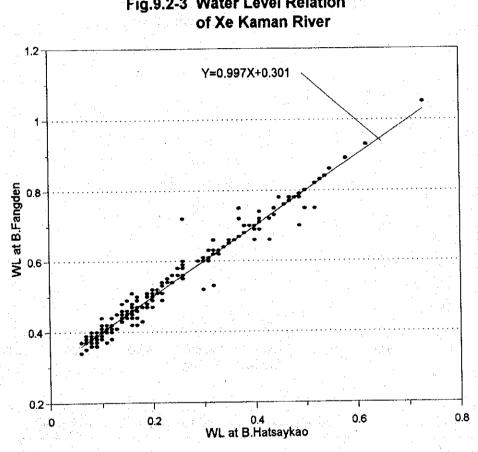


Fig.9.2 - 2 River Cross Section of Xe Kaman River at B.Fangden Gauging Station



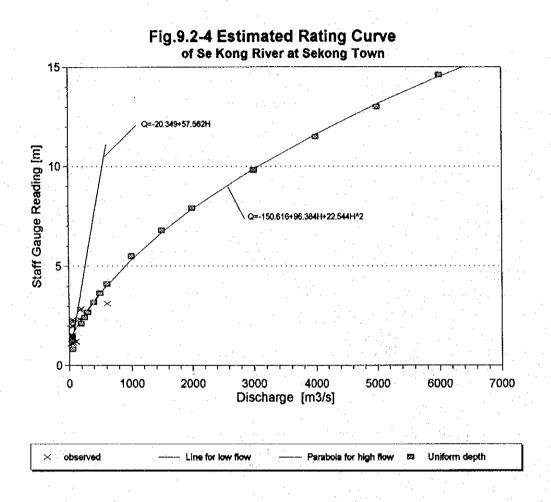
9 - 38

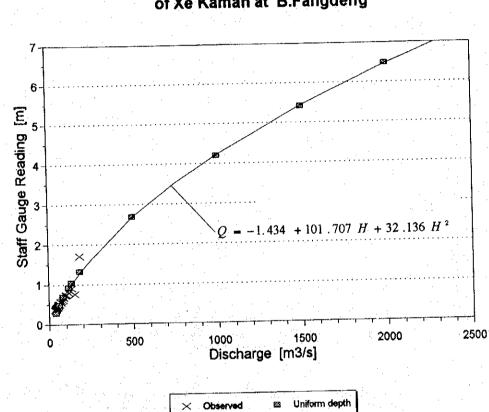
(c).



## Fig.9.2-3 Water Level Relation of Xe Kaman River

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#### Fig.9.2 - 5 Estimated Rating Curve of Xe Kaman at B.Fangdeng

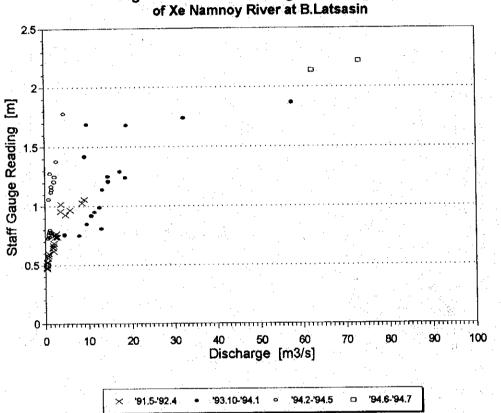
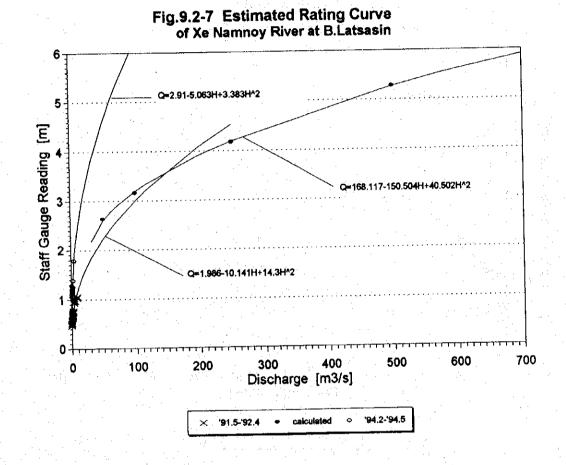


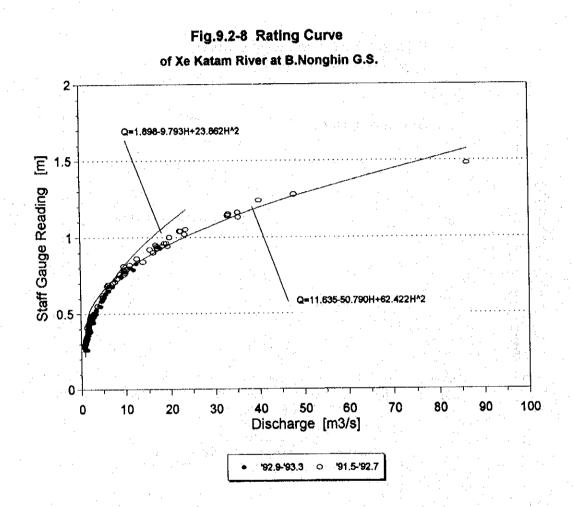
Fig.9.2-6 Observed Stage Discharge of Xe Namnoy River at B.Latsasin

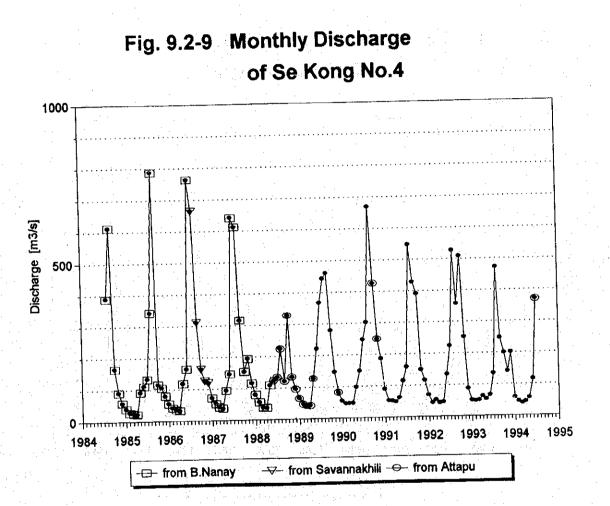
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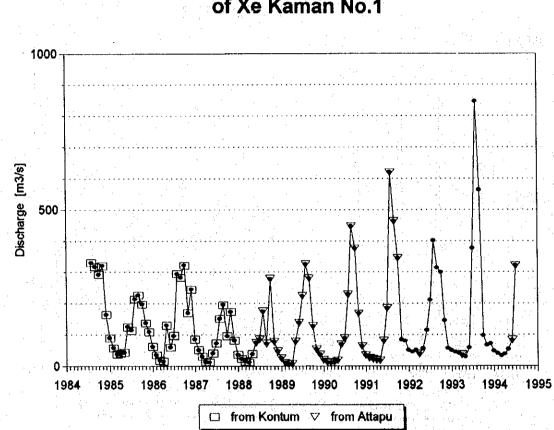
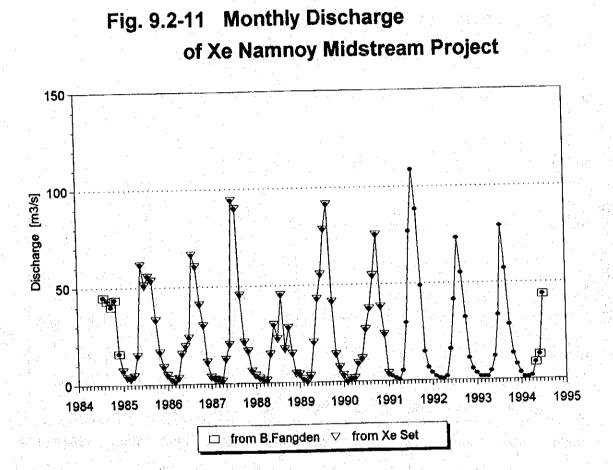
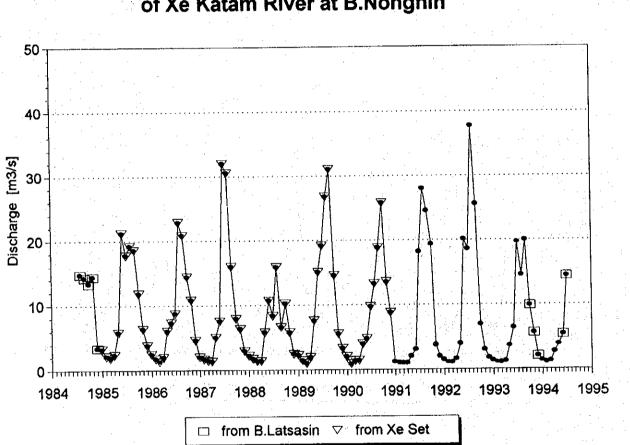
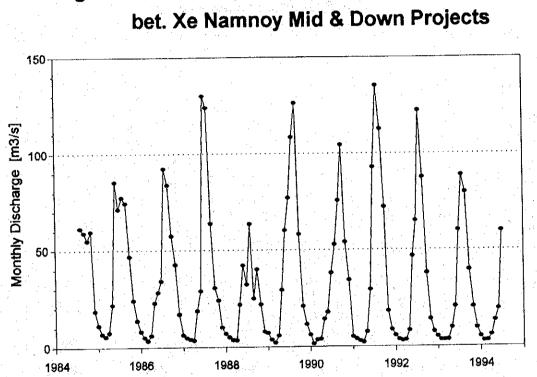


Fig. 9.2-10 Monthly Discharge of Xe Kaman No.1 

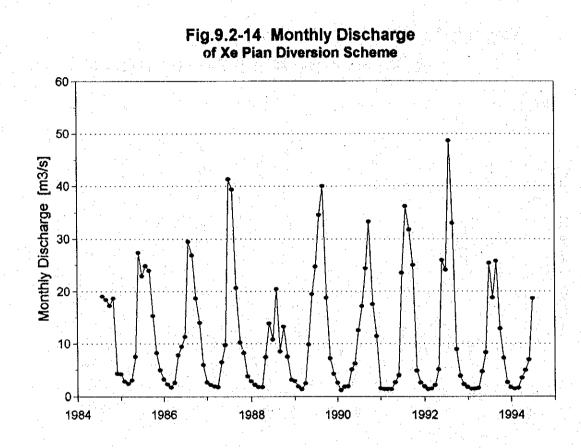
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### Fig. 9.2-12 Monthly Discharge of Xe Katam River at B.Nonghin

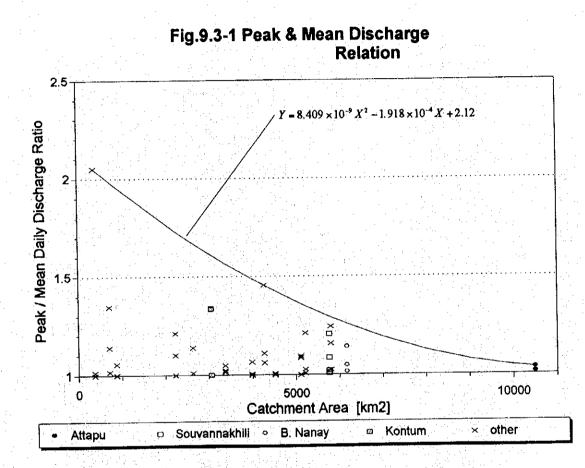


# Fig. 9.2-13 Monthly Discharge

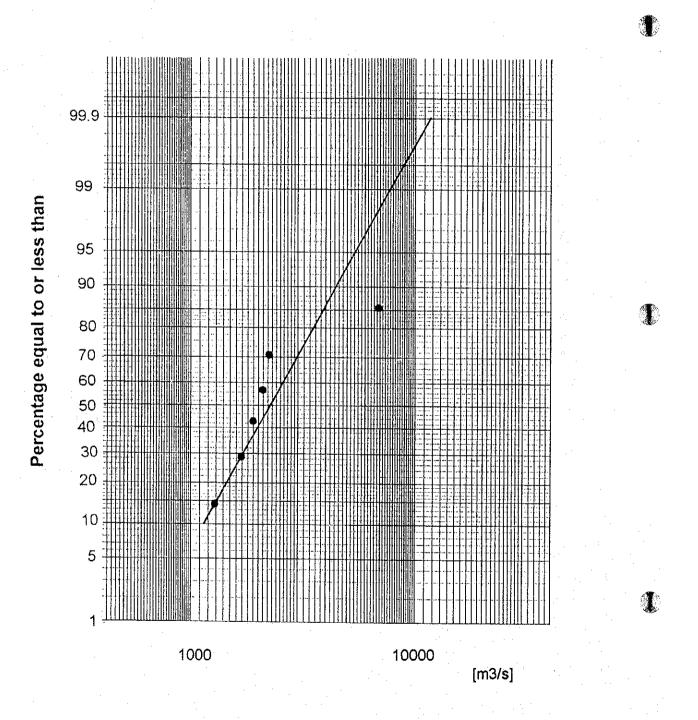


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**B** 



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### Fig. 9.3 - 2 Probable Flood of Se Kong No.4

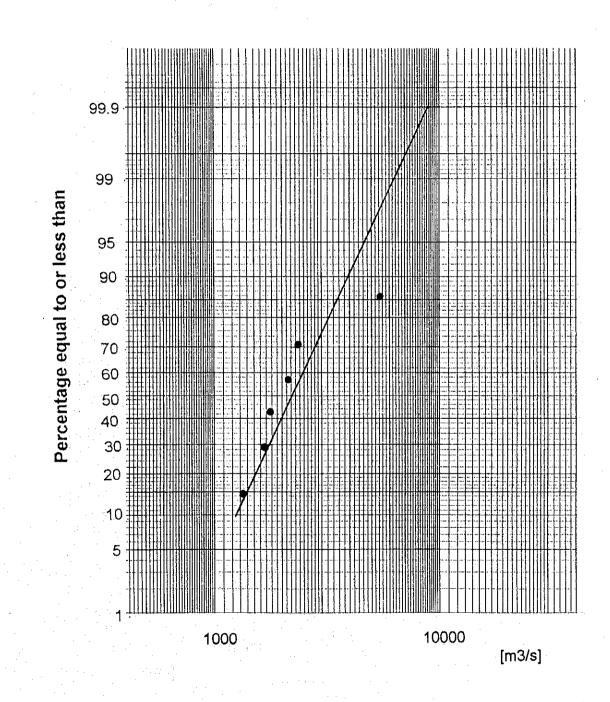
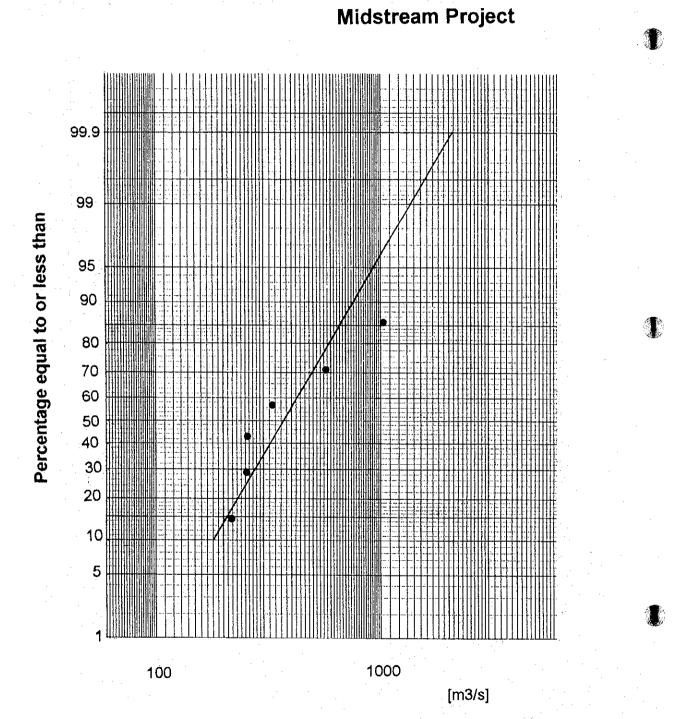


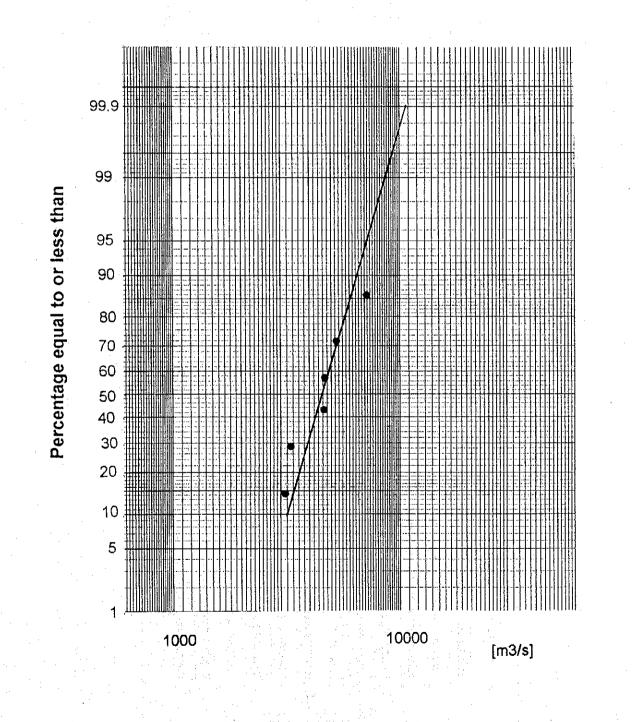
Fig. 9.3 - 3 Probable Flood of Xe Kaman No.1

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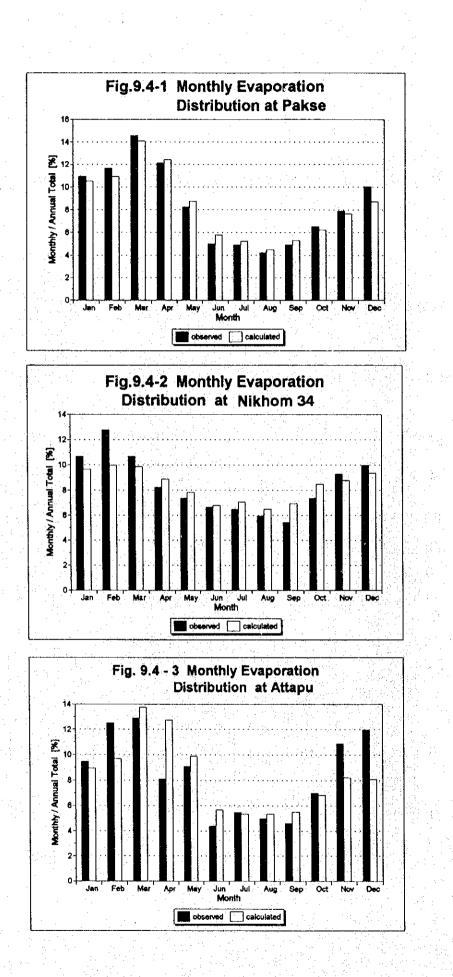
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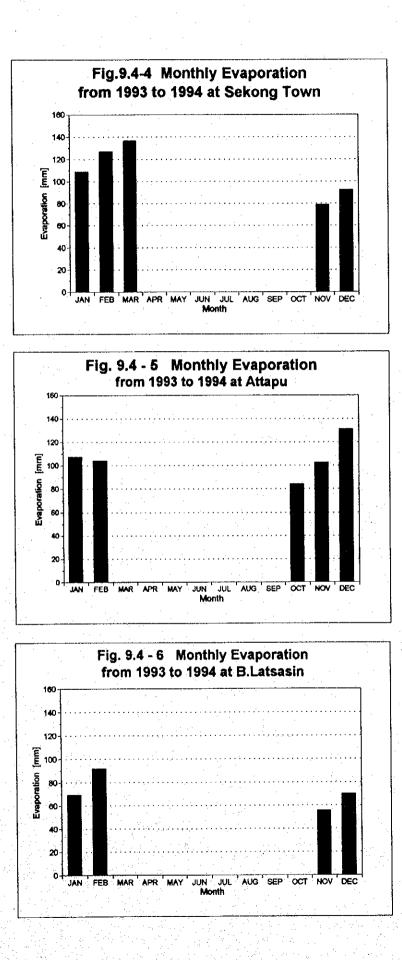


## Fig. 9.3 - 4 Probable Flood of Xe Namnoy



### Fig. 9.3 - 5 Probable Flood of Se Kong River at Attapu





### 10. Geology of Each Project

# 10. Geology of Each Project

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Table 10.1-3	Standard of Rock Mass Evaluation
Table 10.1-4	Relation of Rock Mass Evaluation and Classification for Drilled Core

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DWG. 10.2-1	Se Kong No. 4 Project, Geology, Plan of Dam Site and it's Vicinity		
DWG. 10.2-2	Se Kong No. 4 Project, Geology, Profile of Dam Site		
DWG. 10.3-1	Xe Kaman No. 1 Project, Geology, Plan of Dam Site and it's Vicinity		
DWG. 10.3-2	Xe Kaman No. 1 Project, Geology, Profile of Dam Site		
DWG. 10.4-1	Xe Namnoy Midstream Project, Geology, Plan of Dam Site and it's Vicinity		
DWG. 10.4-2	Xe Namnoy Midstream Project, Geology, Profile of Dam Site and it's Vicinity		

#### 10. Geology of Each Project

#### 10.1 Outline of Geologic Data

Investigations carried out in Pre-Feasibility Stage in Se Kong No. 4, Xe Kaman No. 1 and Xe Namnoy Midstream Project Area are shown briefly in Table 10.1-1. These investigations are in the vicinity of dam sites.

The field geological survey was executed with topographic maps of scale 1:10,000, some of them are enlarged from 1:50,000 topographic maps published by National Geographic Department of Lap PDR. Aerial photographes are interpreted prior to this survey. Seismic prospecting and core boring are already described in Chapter 8.

Drilled cores are classified by the standard shown in Table 10.1-2. This standard consists of three fundamental factors such as weathering, hardness and crack spacing and each factor has 5 grades. The rock mass evaluation was tried by standards shown in Table 10.1-3 and 10.1-4, which are tentative and would be modified in later study stages.

Based on these data, geological plan of scale 1:10,000 and profile of scale 1:2,000 are provided in the vicinity of dam sites.

Other area or sites have no geological information except for those obtained in master plan stage by literature study interpretation of landsat images and aerial photographes and helicopter survey.

Project	Geological Survey	Seismic Prospecting	Core Drilling
Se Kong No. 4	Dam site and its vicinity	Dam site	Dam site
· · · ·		1 line, 1000 m	3 holes, 260 m
Xe Kaman No. 1	Dam site and its vicinity	Dam site	Dam site
		2 lines, 1000m	3 holes, 260m
Xe Namnoy Midstream	Dam site and its vicinity	Downstream of Dam site	Downstream of Dam site
		1 line, 1000 m	6 holes, 380m

# Table 10.1-1 Outline of Geological Investigation in Pre Feasibility Stage

## Table 10.1-2 Standard of Classification for Drilled Core

	Weathering		Hardness	C	rack spacing
1	Very fresh. No weathering of mineral component.	1	Very hard. Broken into knifeedged pieces by strong hammer blow.	1	Over 30 cm
2	Fresh. Some minerals are weathered slightly. Usually no brown crack.	2	Hard. Broken into pieces by strong hammer blow.	2	10 - 30 cm
3	Fairly fresh. Some minerals are weathered. Cracks are stained and with weathered material.	3	Brittle. Broken into pieces by medium hammer blow.	3	3 - 10 cm
4	Weathered. Fresh portions still remain partially.	4	Very brittle. Easy broken into pieces by medium hammer blow.	4	1 - 3 cm
5	Strongly weathered. Most minerals are weathered and altered to second minerals.	5	Soft. Able to dig with hammer.	5	Under 1 cm

This standard has been used by EPDC.

Class	Rock Mass Condition
а.	Fresh, sound, cracky in part
<b>b</b> .	Weathered, brittle, cracky
с. с.	Strongly weathered, soft or very cracky

ta a ser e <u>ser e</u> s

#### Table 10.1-3 Standard of Rock Mass Evaluation

Table 10.1-4 Relatiion of Rock Mass Evaluation and Classification for Drilled Core

$\square$		Grade of Weathering and Hardness		
		1 2 3 4 5		
	1			
Grade of	2	$\mathbf{a}_{1}$ , $\mathbf{a}_{2}$ , $\mathbf{a}_{2}$ , $\mathbf{a}_{3}$ , $\mathbf{a}_{4}$ , $\mathbf{a}_{2}$ , $\mathbf{a}_{3}$ , $\mathbf{a}_{4}$ , $a$		
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#### 10.2 Se Kong No. 4 Project

#### (1) General Topography and Geology

Project area is in the upper course of Se Kong river. The altitude of mountains in the upstreammost area of the reservoir reached 1,500m, and the valleys are V shaped, those in remaining area are from 600 to 900 and valleys become wider with gentle slopes, and those in area downstream of the project area are about 400 m. Landslide topography, large scale slope failure and karst topography are subtle in the project area.

According to the geologic map (scale 1/1 million, Tien P.C. 1988) the project area is underlain by sedimentary rocks and volcanic rocks of Paleozoic and Mesozoic Age. In the neighboring area downstream of the project area is underlaine by younger strata composed of Jurassic to Cretaceous sandstone and shale which fold structure are readily traced by topography. But it is more difficult to interpret the geological structures by topography in the project area.

The bedrock of the project area is mainly composed of Ordovician sandstone and shist, Devonian red sandstone shale and conglomerate, Carboniferous shale chert and limestone, Permo-Carboniferous limestone, and Triassic conglomerate sandstone and rhyorite. Among them, limestone which sometimes affect the watertightness of the reservoir and dam site is judged to be limited and not continuous by the topographic information. The topographies indicating the limestone body in the project area was narrow discontinuous ridges. Coal seams are reported from Carboniferous strata.

#### Dam Site

(2)

NNW-SSE trending mountain of some 500 m in elevation was cut by the Se Kong river at Se Kong No. 4 dam site. At dam site, river bed is elevation 140 m and around 100 m wide. The valley is about 900 m wide of high water level (El. 290 m). The slope on the right bank is 30° in average and steeper than that of right bank (20°).

According to the information obtained by aerophoto interpretation and geological survey along Se Kong river by boat, the dam site is located at the core of anticline formed by Post-Triassic strata. The dam axis is almost parallel to the anticline axis. But further detailed geologic structures are not obtained by aerophoto-interpretation. The filed geological survey, seismic prospecting and core boring provided the following information.

The geology in the vicinity of the dam site is shown in DWG. 10.1-1 and 10.1-2. Dam site is underlain by sandstone, shale and tuff. Sandstone and shale are distributed on the river bed and upstream of the dam site. Sandstone is gray in color, medium grained, thick bedded and with intercalation of carbonaceous shale. Shale is reddish grey in color, and distributed in the upstream of a gully on the right bank upstream of the dam site. Basalts are found on the river bed and in drillhole SK-1. Sandstone and shale dip downstream at  $35 - 36^{\circ}$  at the dam site and dip upstream in the upstream of the dam site. Though, existing geologic map (1:1 million, 1988) show the dam site with Triassic Manggiang. Formation, these sandstone and shale might belong to older formation.

Tuff layer accompanied by tuff breccia are andesitic and distributed on both banks of dam site and river bed downstream of the dam axis. They dip to the right bank. These tuff layers are supposed to unconformably overlie the sandstone and shale, which evidence have not obtained yet. Limestone block and fragments are rich in some layers and contain Permian Fusulina. Large limestone block are outcropped on the ridge at El. some 350 m on the right bank of the dam axis and at the river bank on the right bank about 1 km downstream of the dam axis. These blocks are up to 20 m thick and 200 m long, but not continuous. Tuff layers are overlain by conglomerate which is characterizey by dense white gravels, and maybe the lowermost layer of Jurassic series. These tuff layers are supposed to be of Manggian Formation because they contain Permian limestone blocks and are overlain by Jurrassic strata.

In the vicinity of the dam site, few lineament are interpreted and no fault sheared zone is confirmed by field geological survey.

Surface deposits such as talus deposits and recent river deposits are thin. The talus deposits in drillhole are less than 2 m in thickness, and correlating velocity layer of less than 700 m/sec provided by seismic prospecting does not exceed 4 m in thickness. Exceptionally, lower slope on the right bank of the dam axis would be covered by 10 - 20 m thick talus deposits judging from the existence of many blocks up to 5 m across and thick velocity layer of 1,500 m/sec.

The recent river deposits are inferred to be 10 m deep in maximum from abundant outcrops of tuff on the river bed downstream of the dam axis.

Weathering on the both banks are confirmed to be less than 5 m below rock surface in drillholes, 1.5 km/sec layer is some 10 m thick in general. The rock mass (tuff) below that depth has velocities more than 4 km/sec on the left bank and lower slope on the right bank,

Drillhole SK-1 penetrating these depth confirmed the rock mass to be fresh hard and intact in general. Most permeability test section in this drillhole are of less than 1 Lu, except from 50 to 70 m depth, where is characterized by fractuation of water level in drillhole during drilling, some dissolved calcite veins and the lugeon value up to 13.4 Lu. On the upper slope on the right bank 1.5 km/sec layer is underlain by 3.5 km/sec layer which is confirmed to be relatively loosened rock mass by the drillhole SK-3 providing the permeability from 5 - 10 Lu at the corresponding depth. Further below, from  $70 \sim 90$  m depth, the same drillhole has also permeability from 5 - 10 Lu.

Sandstone on the river bed has velocities of 4.5 to 5 km/sec, and revealed to be fresh, but cracky and somewhat permeable. (about half of luggeon test sections show some 10 Lu.)

The distribution of the limestone at the dam site is neither continuous nor wide.

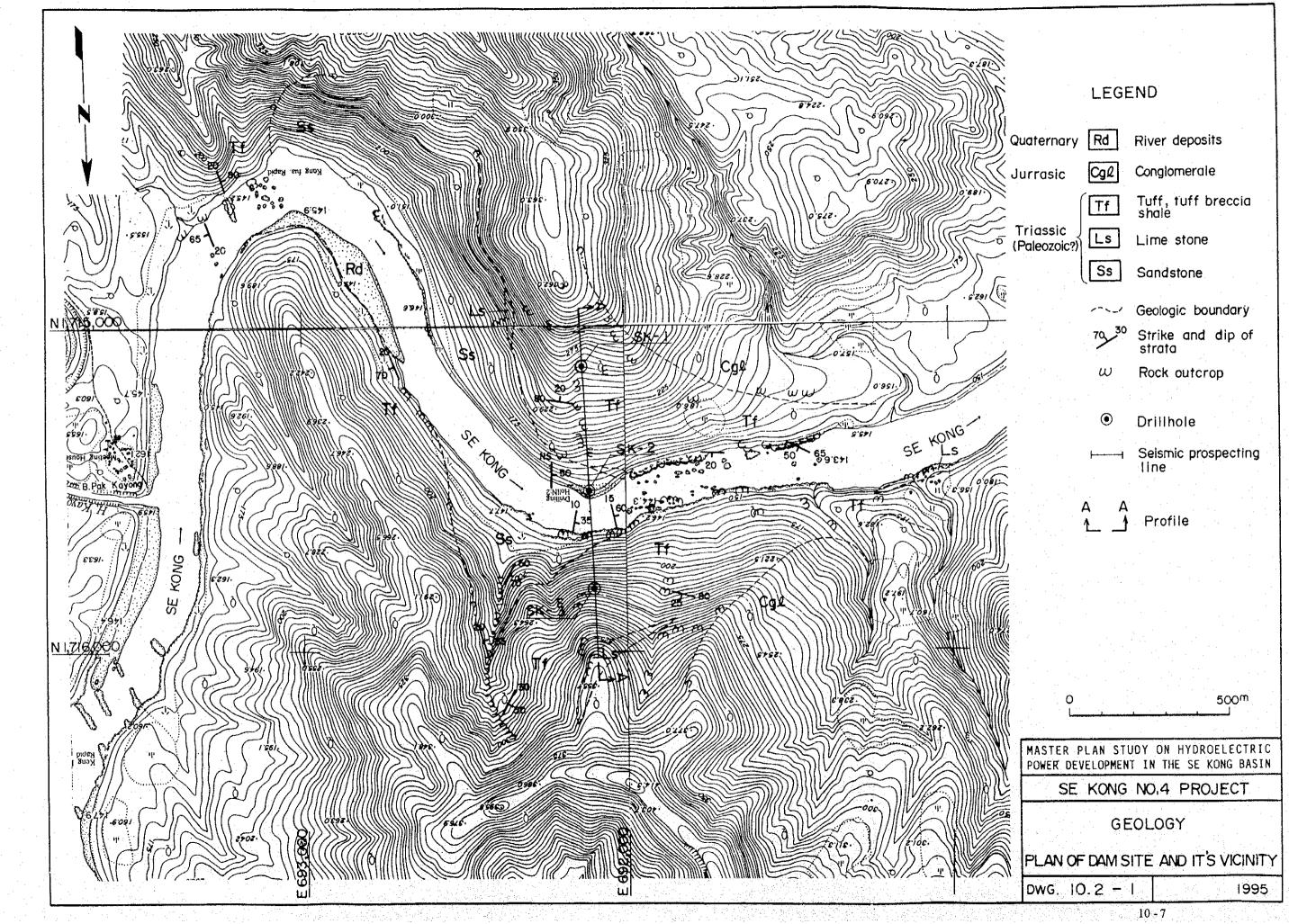
This dam site will not provide any serious geotechnical problems, because of shallow surface deposits and weathering, and generally low permeability.

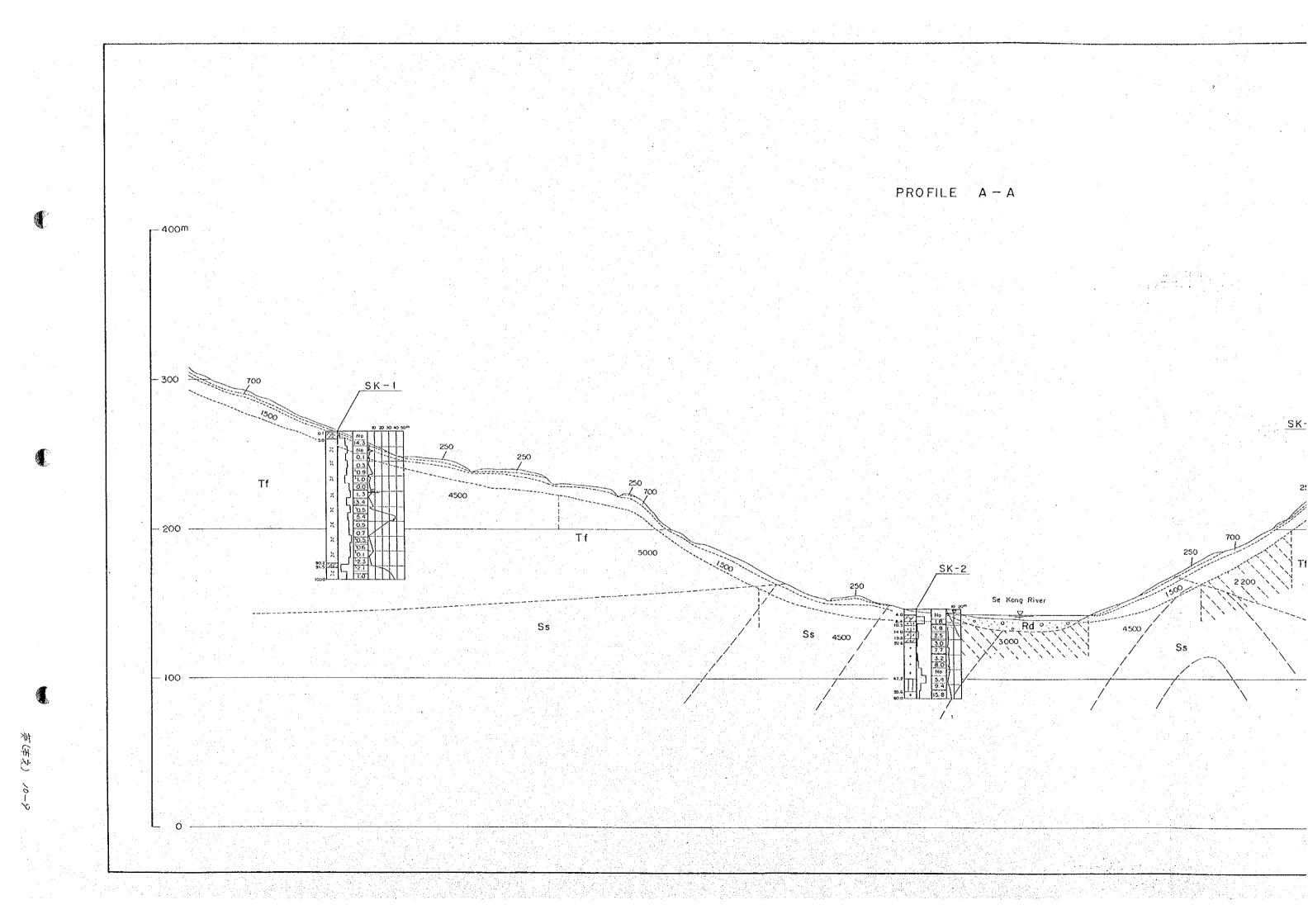
(3) Reservoir Area

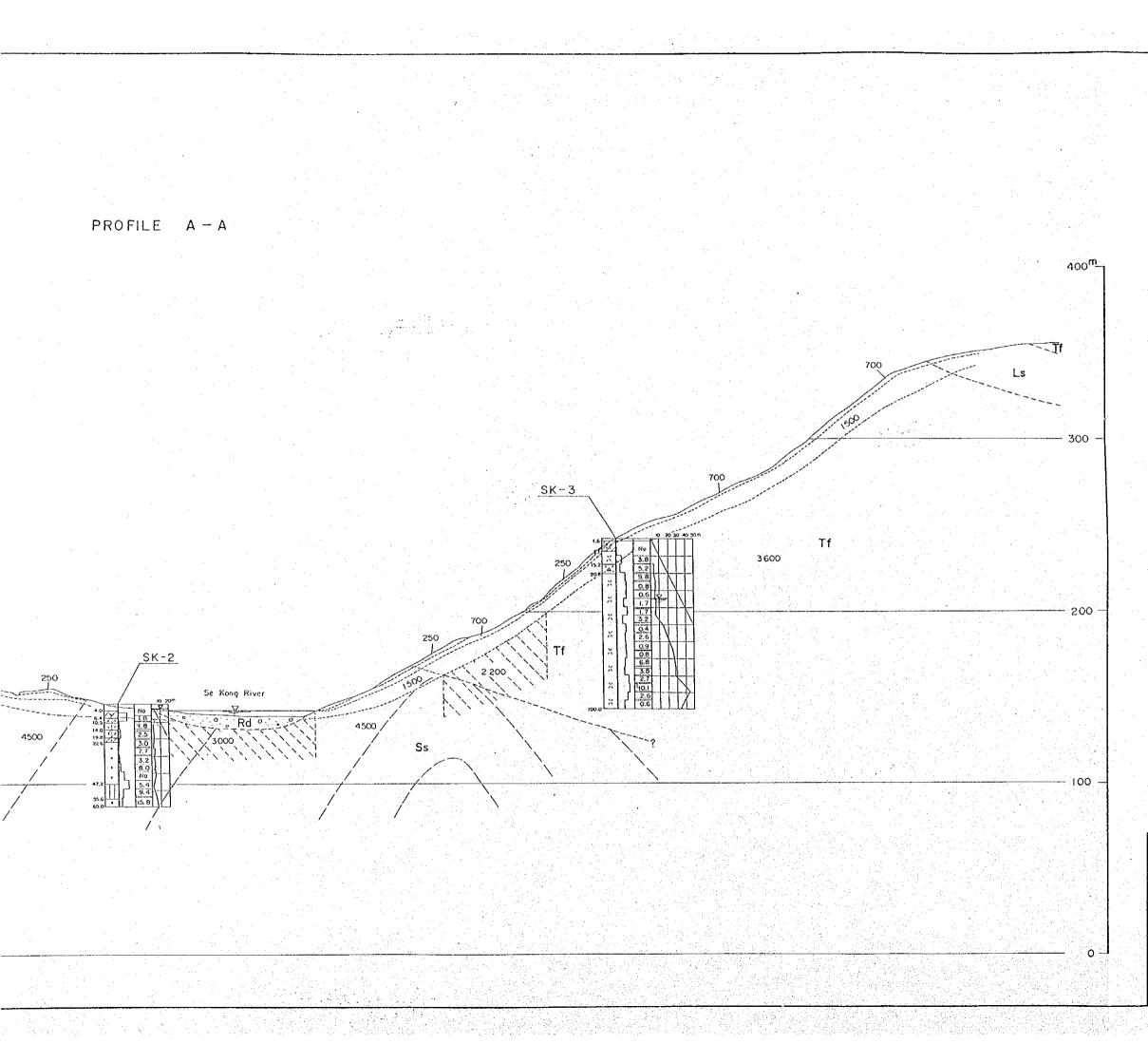
Upstream reservoir area is characterized by narrow valley and steep slopes rising up to El. 1,500 m. While, in remaining reservoir area, surrounding mountains are 400 to 600 m above sea level, valleys are widened and with gentle slopes. There is no distinct landslide topography, large scale slope failure and extensive karst topography.

According to the existing geological map (1:1 million, 1988), the reservoir area is underlain by the strata from Paleozoic to Triassic; mainly composed to shale and sandstone. Limestone distribution is judged from topography to be so limited and discontinuous that it will not cause any problem on reservoir watertightness, but farther investigations are still necessary. Coal seams distributed in the vicinity of B. Chakeui are reported to be the most favorable in Lao P.D.R., but their occurrence and altitude are not confirmed in this study.

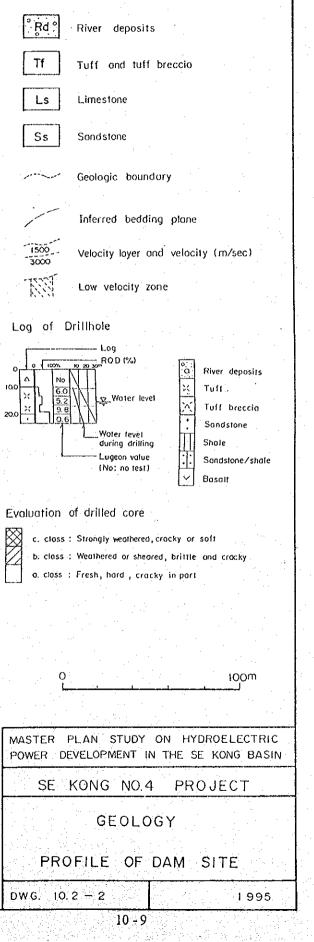
It seems like that the reservoir area has few problems on stability of surrounding slopes and watertightness.

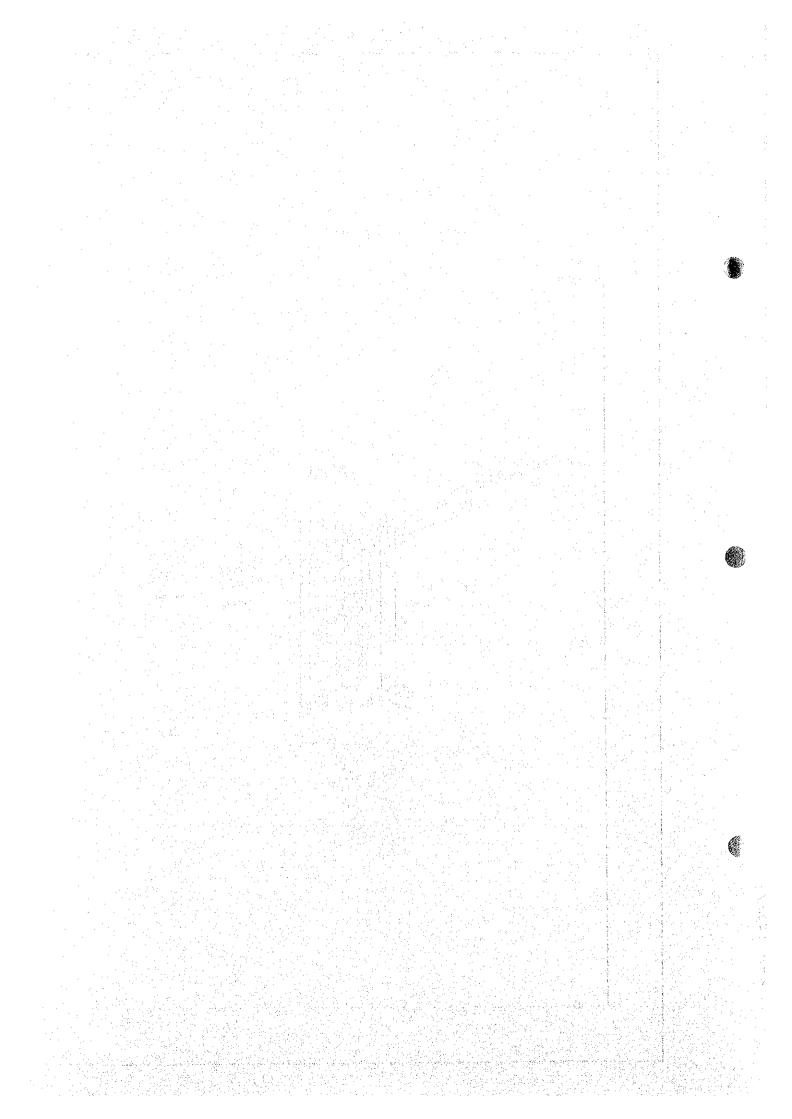






#### LEGEND





#### 10.3 Xe Kaman No. 1 Project

### (1) General Topography and Geology

The project area is located in the middle course of Xe Kaman river. The altitude of the mountains are 1,000 to 1,400 m on the left bank and some 1,000 m on the right bank. Xe Kaman river in the project area is El. 130 to 260 m and connects small basins separated by narrow gorges. Areas of gentle slope as high as some 1,000 m are remained in the vicinity of upstream to midstream project area. But close to the dam site mountains are eroded to have narrow ridges and steep slopes instead of gentle slopes.

Landslide topography and large-scale slope failure and remarkable karst topography are not observed in aerial photographs.

The project area underlain mainly by Padeozoic and Mesozoic rocks as shown in existing geologic map (1:1 million, 1988). They are Cambrian-Ordovician shist and sandstone, Devonian red sandstone, chert and shale, Carboniferous shale, chert and sandstone and Triassic Manggian Formation composed of conglomerate, siltstone and sandstone in descending order. Carboniferous strata are intruded by plutonic rocks. Basalt covers the plateau of elevation about 1,000 m on the right bank and seems to overline Mesozoic and Paleozoic strata.

#### Dam site

(2)

The dam site is located on the second downstreamost gorge of Xe Kaman river. River bed is at elevation of about 130 m and 80 m wide. Valley is about 500 m wide at high water level (El. 260 m). The slopes below an elevation of some 240 m have an average gradient of 40° on the left bank and 50° on the right bank. The slopes above that elevation are 30° on the left bank and 40° on the right bank. Tributary valley on the right bank downstream of the dam site is deep and with steep slopes, and makes the mountain body on the right bank slender. A gentle slope at 25 to 30° is distributed locally just upstream of the dam site.

The dam site is underlain by sandstone and intercalating conglomerate and shale. Sandstone is reddish grey in color, medium to coarse grained, thick bedded. (each bed is usually 50 cm to 1 m thick) and some times get coarser to conglomerate. Shale are distributed locally outside of dam site, and less than 10 m in thickness, those found 400 m downstream from dam axis are reddish in color and found 600 m upstream are black.

Strata composed of sandstone, conglomerate and shale are wound in the vicinity of the dam site, but generally inclined downstream at 70° to 80° at the dam site.

Talus deposits are limited on the upper slope of the dam site, where they are 12.9 m thick in Drillhole XK-1. Their velocity of 1.7 km/sec, however indicate them to be strongly weathered rock.

Recent river deposits are inferred to be some 5 m thick by the cutcrops on the river bed both downstream and upstream of the dam site.

Strongly weathered rock mass on the upper slope on the left bank are found above 19.3 m depth in Drillhole XK-1. Because this depth is in 3 km/sec layer, upper part of 3 km/sec layer corresponds to weathered rock. Below this depth XK-1 got fresh and hard core, low permeability (most test sections are less than 2 Lu) and small fractuation of water level in drillhole during drilling. Velocity layer of 3 km is supposed to represent the rock mass above 12.9 m depth, and rockmass below that depth has a velocity of 5 km/sec as obtained on the lower slope.

On the middle slope on the right bank Drillhole XK-3 met weathered zone down to 10 m depth, which corresponds to 1.4 km/sec layer. The depth of 1.4 km/sec layer is down to 10 to 20 m. This hole obtained fresh and hard cores but permeable bed rock (more than 10 Lu) down to 35 m depth, final water level at 40.2 m, continuous decrease in water level during drilling above 50 m depth. These data suggest the bed rock above 40 m depth to be loosened. This suggestion are supported by 3.5 km/sec velocity layer.

On the lower slope, bed rock is free of weathering but loosened. The velocity obtained by seismic prospecting is 3.2 km/sec.

On the river bed, fresh and hard rock are exposed and also confirmed in Drillhole XK-3. But permeability of that hole is rather high (4 out of 9 sections are 5 to 15 Lu).

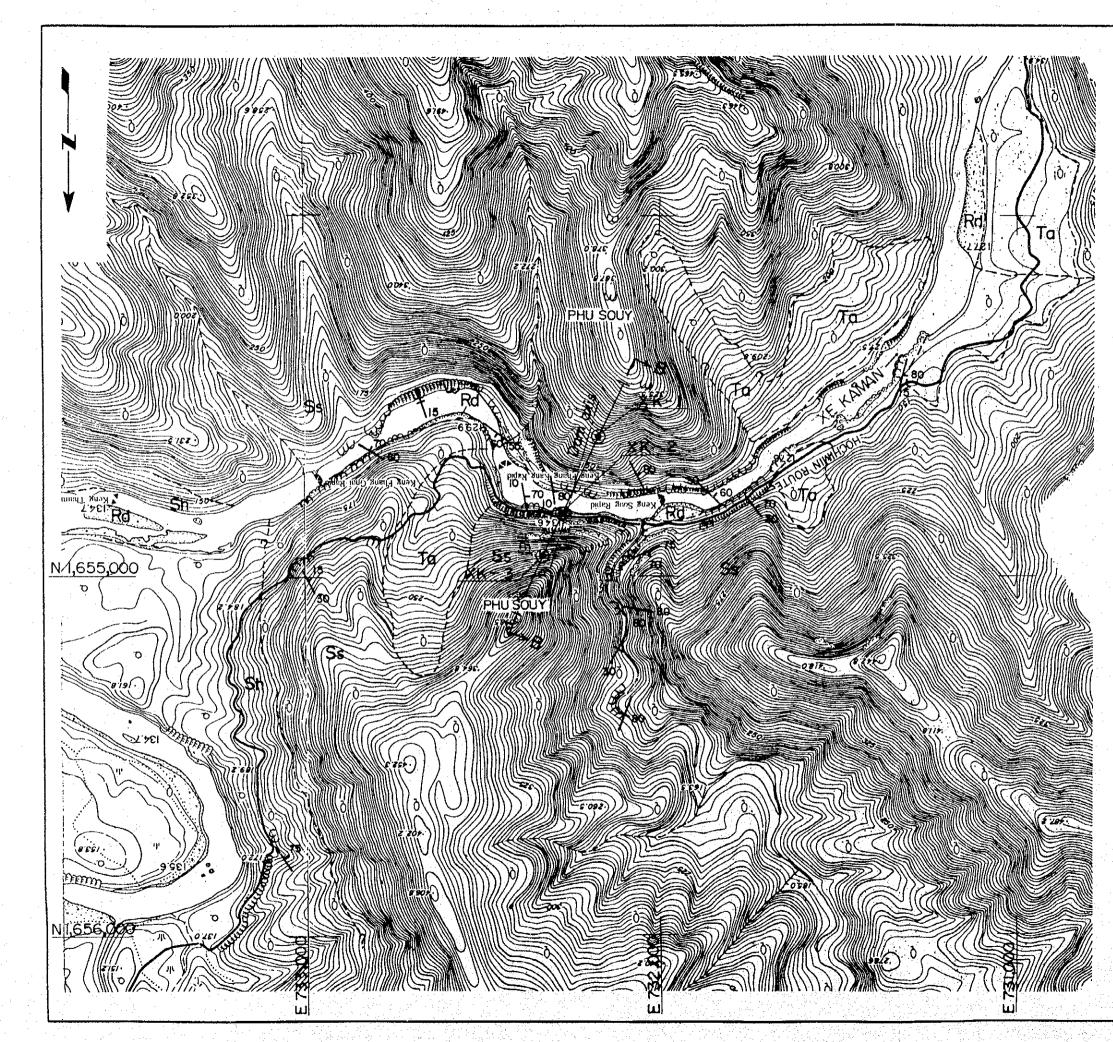
On the gentle slope on the right bank upstream of the dam site, any outcrop of bed rock is not confirmed. At the foot of this slope, at the river bank, black clay with rock fragment is found. This slope is supposed to be covered by thick talus deposits or coluvium and require consideration on slope stability in case of empond of the reservoir.

The reservoir area is surrounded by the mountain having elevations from 1,000 to 1,400 m. Valleys are generally narrow and V shaped in the upstream reservoir area, some basins separated by short gorges appear in the downstream reservoir area. The ridges trend NW-SE and make gorges. The slopes surrounding the reservoir are usually high and some of them rise up to 1,000 m, but any distinct landslide topography or large slope failure is not observed. Close to the backwater of the reservoir, high white cliffs are continued along the Xe Kaman river and seems to be composed by limestone, but typical karst topographies are not found. This area should be further investigated in order to make clear the hydro geological role. Basalt on the right bank seems to cover Mesozoic and Paleozoic strata and be above high water level. Remaining strata are mainly composed of shale and sandstone and supposed to be watertight.

A NW-SE fault is shown in existing geological map (1:1 million, 1988) about 5 km upstream of the dam site. This fault is recognized in aerial photograph as a sharp strait lineament and one of the largest in the reservoir area, but don't bring any serious problems on slope stability, watertightness and seismotectonics.

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