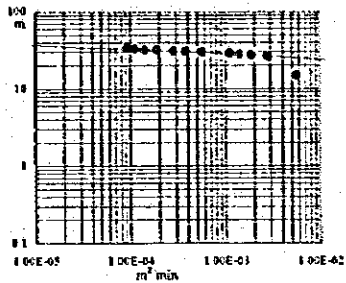


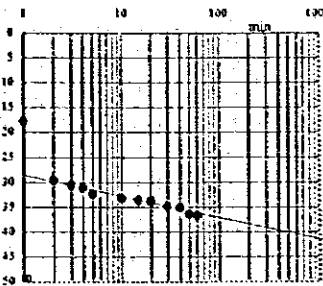
Appendix 2 (3) Result of Pumping Test Analysis

No. 1626D

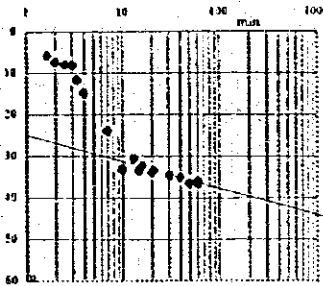
T= 1.33 k= 0.0631 S= 7.91E-08



T= 1.135E+00 k= 0.0631 S= 7.70E-08

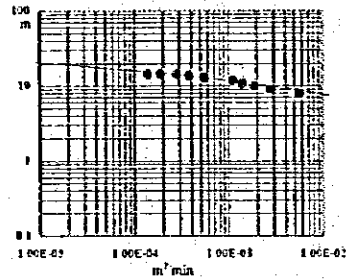


T= 0.892 k= 0.0425

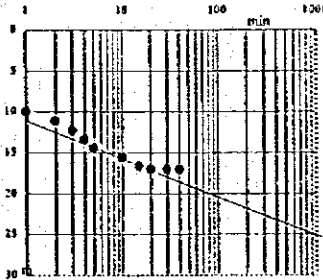


No. 1680A

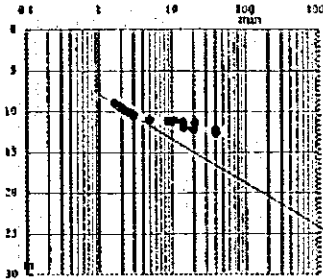
T= 11.3 k= 0.943 S= 0.0122



T= 11.2 k= 0.931 S= 0.0122

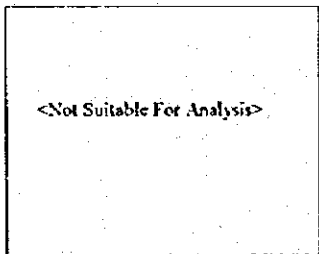


T= 9.58 k= 0.792

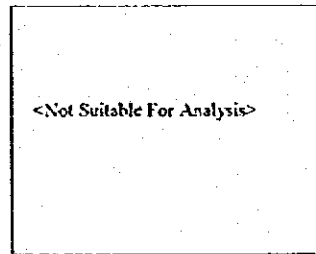


No. 1630

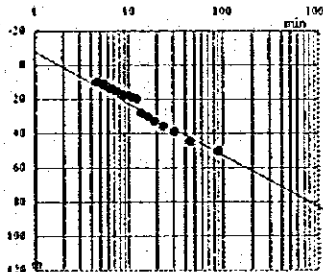
T= k= S=



T= k= S=

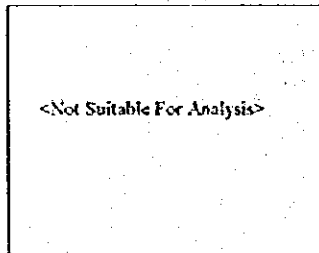


T= 1.41 k= 0.0232

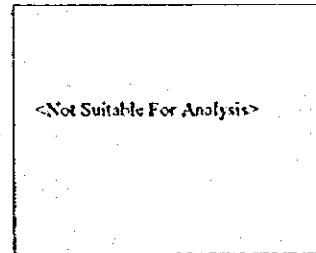


No. 2199

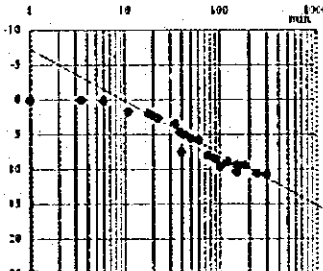
T= k= S=



T= k= S=

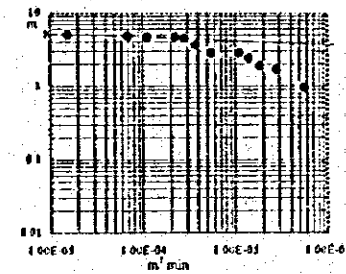


T= 11 k= 0.272

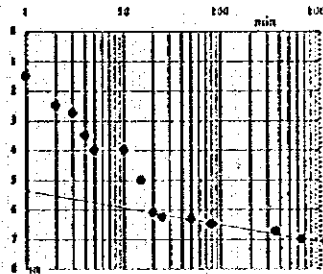


No. 1691

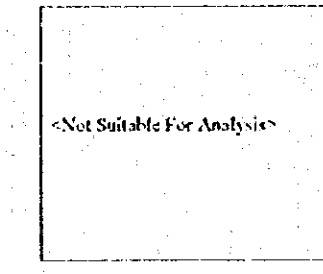
T= 1.31E+01 k= 2.33E+00 S= 1.17E-07



T= 137 k= 2.64 S= 1.82E-08



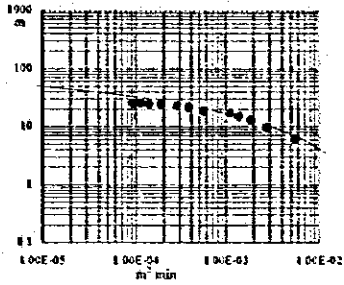
T= k=



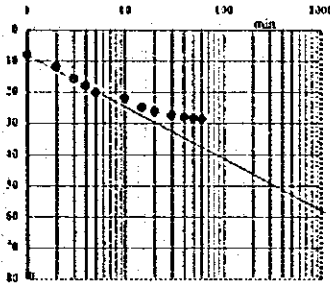
Appendix 2 (4) Result of Pumping Test Analysis

No. 2670-1

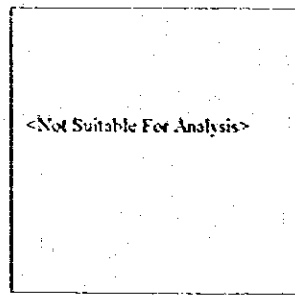
T= 0.383 k= 0.0147 S= 0.0364



T= 3.81E-01 k= 0.0146 S= 1.47E-02

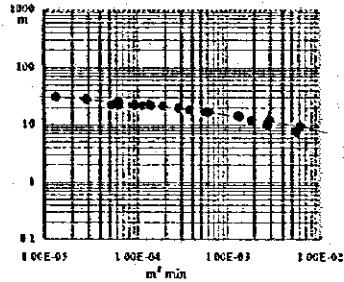


T= k=

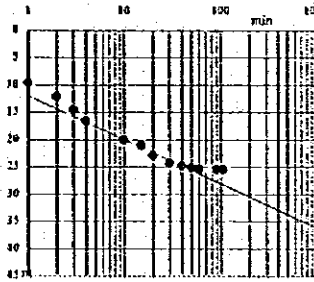


No. 2674-1

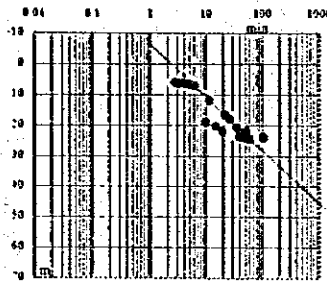
T= 2.29 k= 0.127 S= 0.0221



T= 2.34 k= 0.13 S= 0.0221

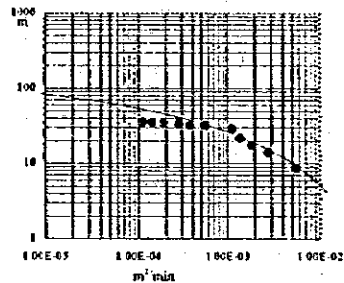


T= 1.1 k= 0.0611

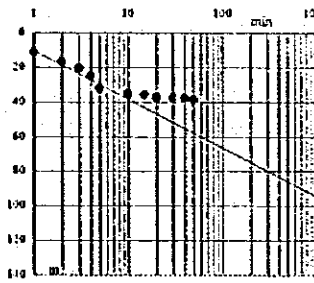


No. 2625-1

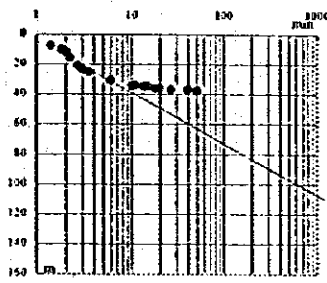
T= 1.60E-01 k= 5.16E-03 S= 2.10E-02



T= 0.158 k= 0.00509 S= 0.0189

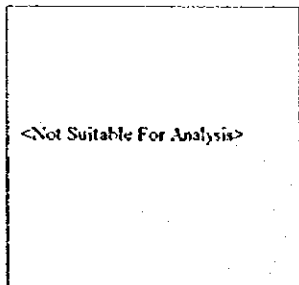


T= 0.129 k= 0.00415

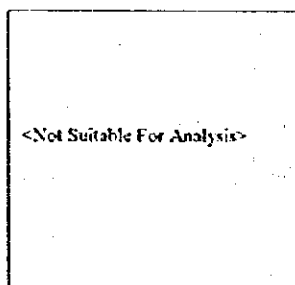


No. 2015

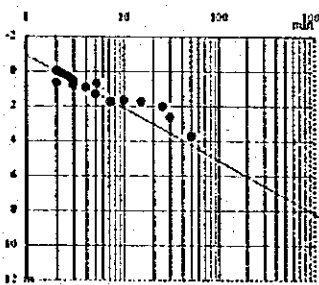
T= k= S=



T= k= S=

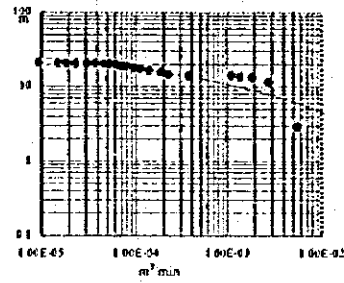


T= 261 k= 13

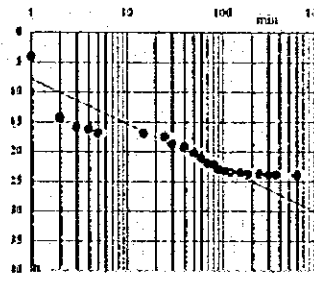


No. 2012

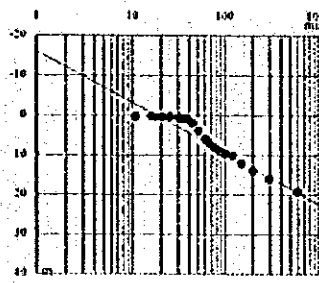
T= 1.05E+01 k= 5.53E-01 S= 6.16E-03



T= 10.5 k= 0.554 S= 0.00618



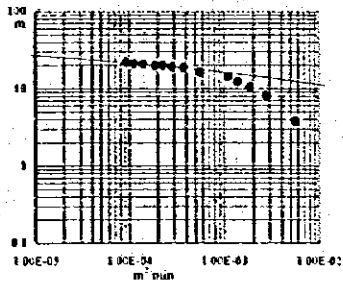
T= 3.25 k= 0.197



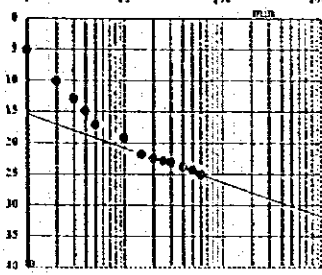
Appendix 2 (5) Result of Pumping Test Analysis

No. 2013

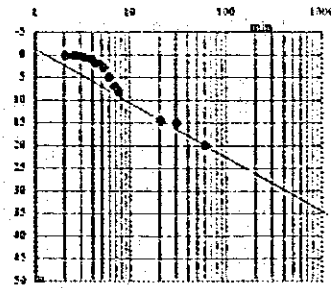
T= 7.65 k= 0.219 S= 0.00372



T= 7.80E+00 k= 0.223 S= 3.33E-03

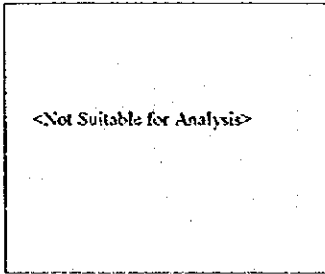


T= 3.37 k= 0.102

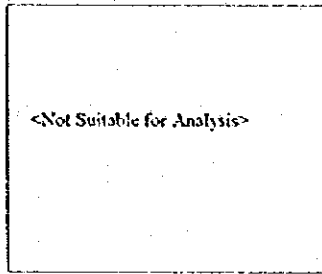


No. C113

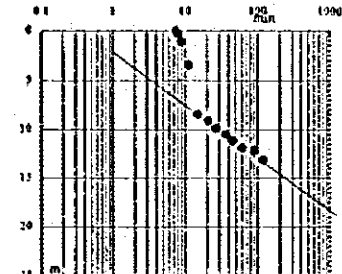
T= k= S=



T= k= S=

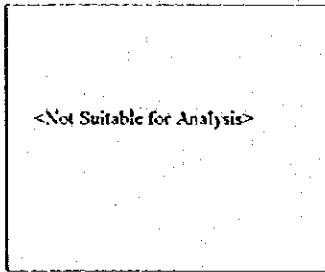


T= 3.51 k= 0.222

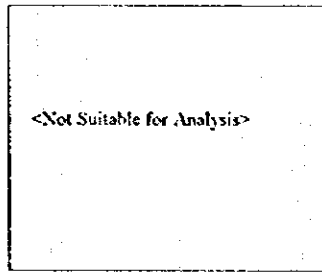


No. M111

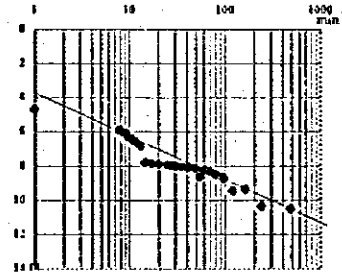
T= k= S=



T= k= S=

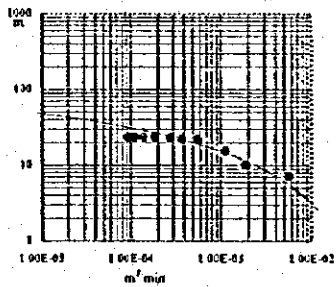


T= 9.349992 k= 1.34

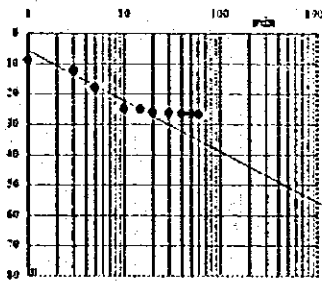


No. 2669-1

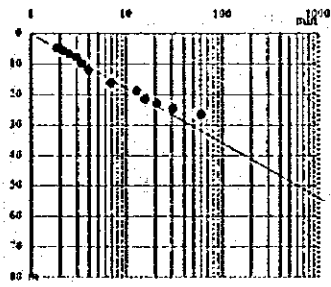
T= 3.79E-01 k= 2.52E-02 S= 4.76E-02



T= 0.379 k= 0.0253 S= 0.0477

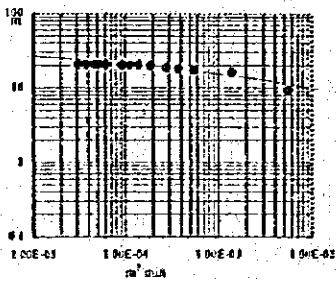


T= 0.354 k= 0.0236

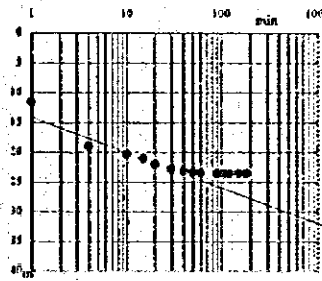


No. 2668-1

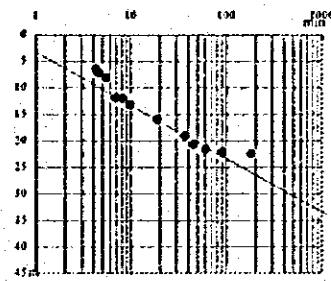
T= 1.06E+00 k= 1.51E-01 S= 1.31E-03



T= 1.06 k= 0.151 S= 0.00128



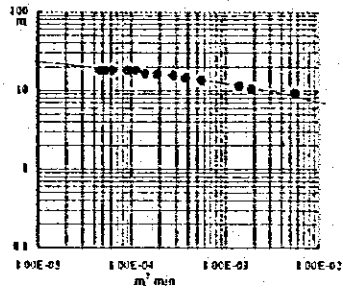
T= 0.628 k= 0.0897



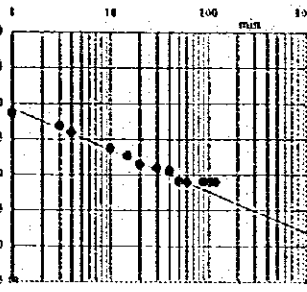
Appendix 2 (6) Result of Pumping Test Analysis

No. 2637

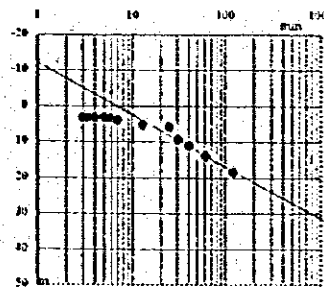
T= 2.74 k= 0.391 S= 0.0104



T= 2.72E+00 k= 0.389 S= 1.07E-02

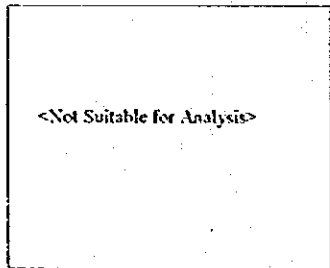


T= 1.09 k= 0.155

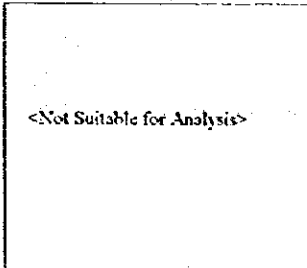


No. MAK13

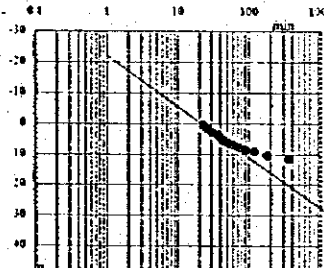
T= k= S=



T= k= S=

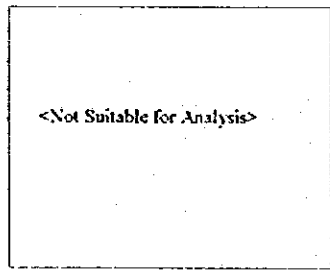


T= 2.86 k= 0.476

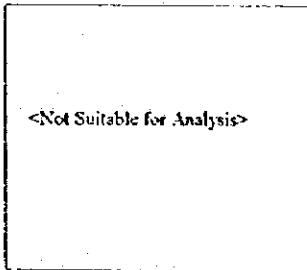


No. LUSC10

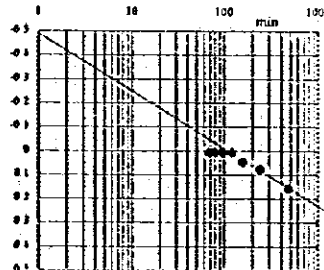
T= k= S=



T= k= S=

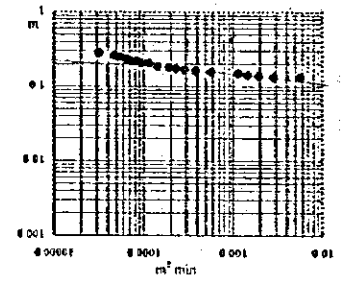


T= 131 k= 263

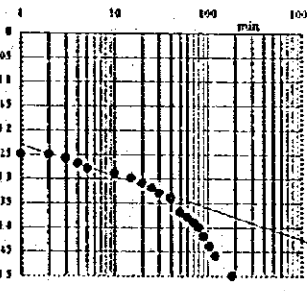


No. LUSC13

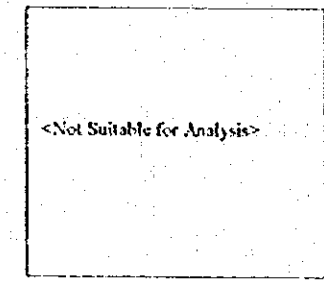
T= 7.33E+02 k= 1.47E+02 S= 5.51E-02



T= 730 k= 146 S= 0.0571

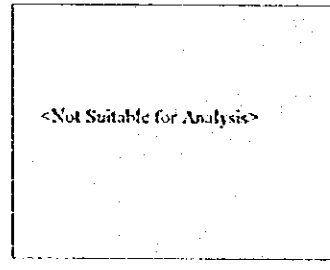


T= k=

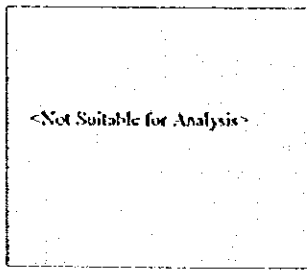


No. LUSC16

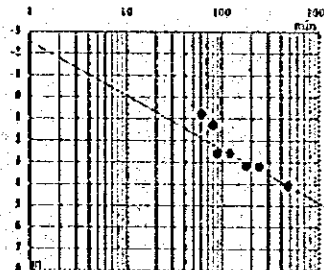
T= k= S=



T= k= S=



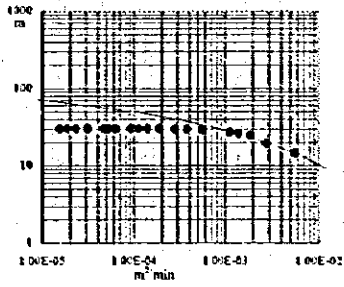
T= 122 k= 407



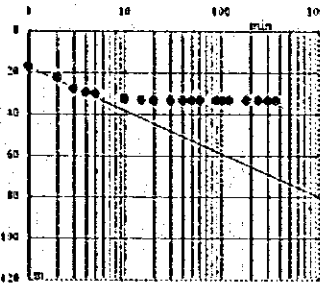
Appendix 2 (7) Result of Pumping Test Analysis

No. 2663

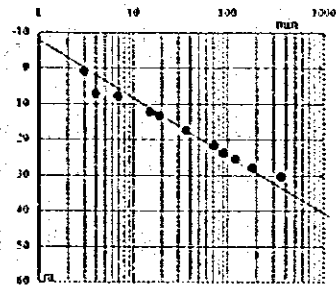
$T = 0.729$ $k = 0.0173$ $S = 0.0299$



$T = 7.18E-01$ $k = 0.0171$ $S = 2.99E-02$

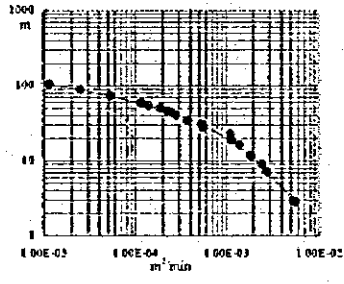


$T = 0.928$ $k = 0.0221$

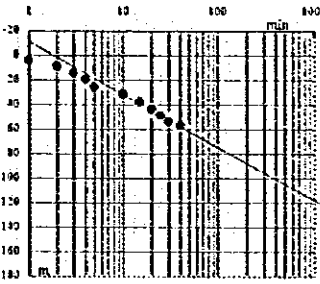


No. 2147-3

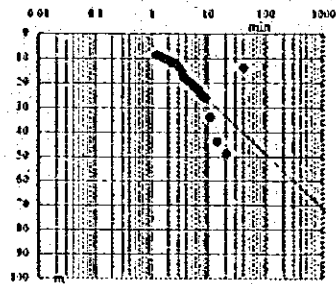
$T = 0.114$ $k = 0.0183$ $S = 0.063$



$T = 0.111$ $k = 0.0186$ $S = 0.0599$

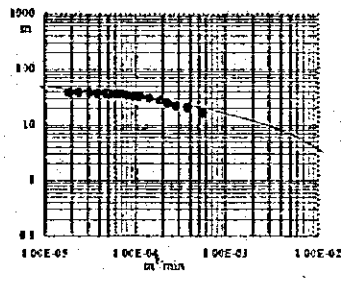


$T = 0.214$ $k = 0.0356$

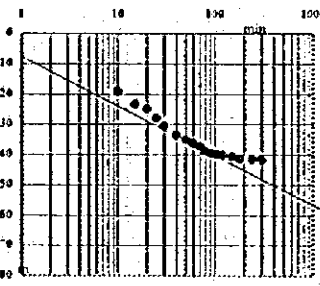


No. LE6

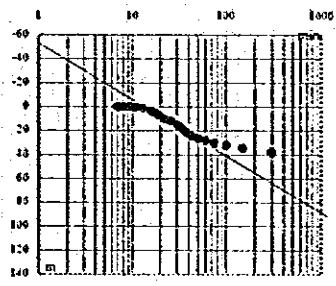
$T = 9.69E-02$ $k = 1.08E-02$ $S = 1.01E-02$



$T = 0.0968$ $k = 0.0108$ $S = 0.00913$

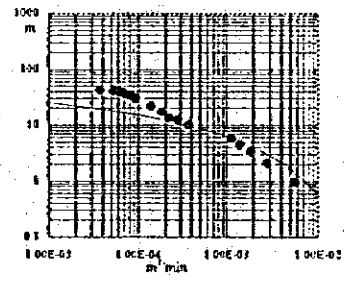


$T = 0.0336$ $k = 0.00173$

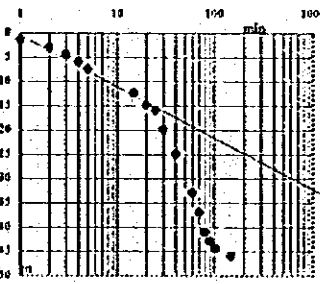


No. 1839

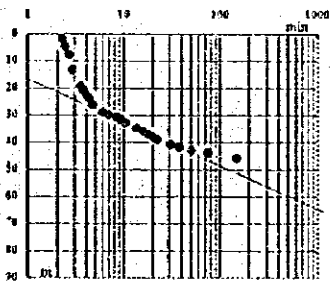
$T = 1.00E+00$ $k = 1.75E-02$ $S = 2.78E-01$



$T = 0.997$ $k = 0.0173$ $S = 0.247$

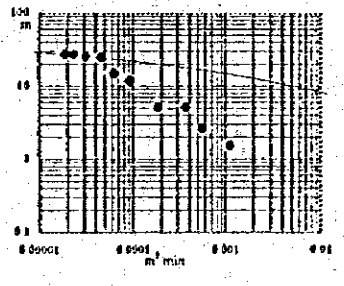


$T = 0.655$ $k = 0.0115$

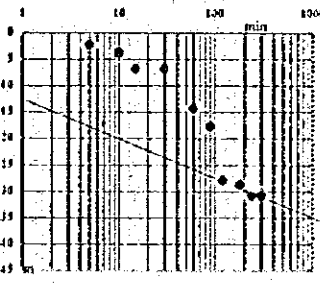


No. 1375

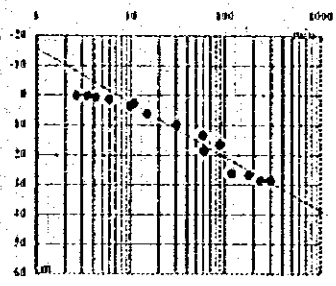
$T = 4.23E+00$ $k = 1.13E-01$ $S = 2.56E-02$



$T = 4.21$ $k = 0.112$ $S = 0.0252$



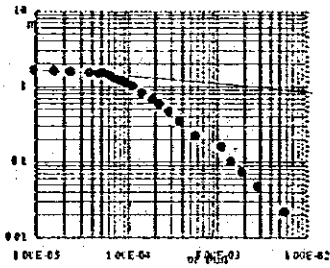
$T = 1.74$ $k = 0.0464$



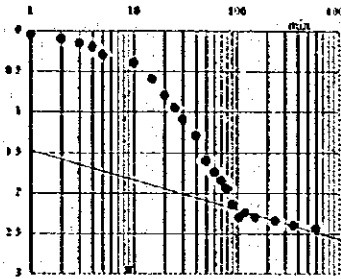
Appendix 2 (8) Result of Pumping Test Analysis

No. 2136C

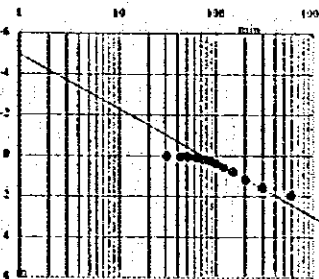
T= 191 k= 12.7 S= 0.00681



T= 1.95E+02 k= 13 S= 5.16E-03

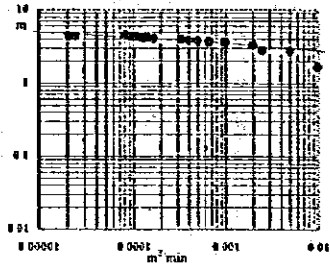


T= 26.7 k= 1.78

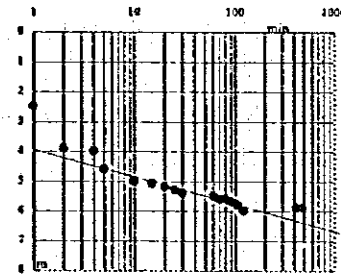


No. 2694

T= 484 k= 16.7 S= 0.00321



T= 484 k= 16.7 S= 0.00324

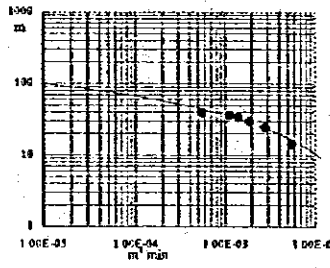


T= k=

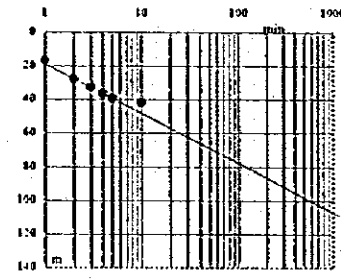
<Not Suitable For Analysis>

No. 1532-1

T= 1.12E+00 k= 2.14E-02 S= 7.68E-02



T= 113 k= 0.0236 S= 0.0706

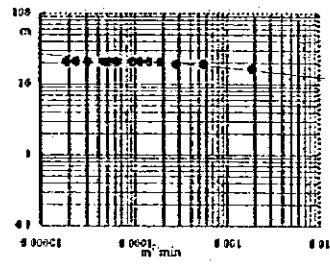


T= k=

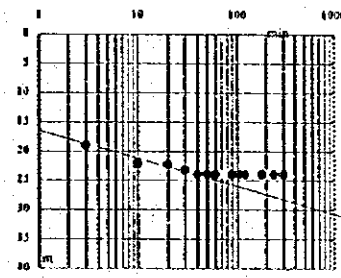
<Not Suitable For Analysis>

No. 2657

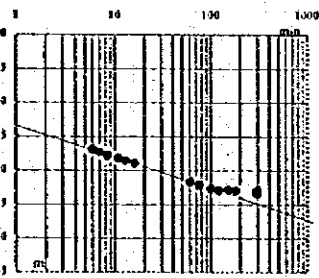
T= 1.33E+00 k= 3.34E-01 S= 1.10E-01



T= 1.34 k= 0.335 S= 0.000119

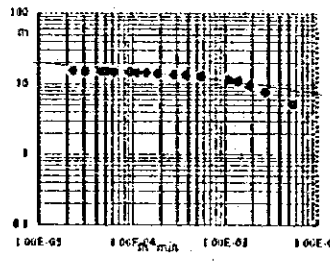


T= 1.36 k= 0.34

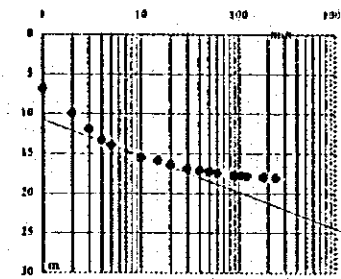


No. 2631-1

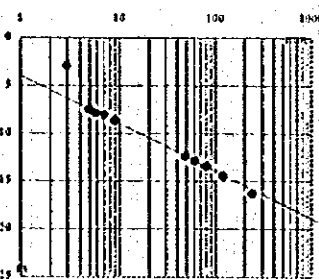
T= 5.39E+00 k= 2.80E-01 S= 1.05E-02



T= 8.3 k= 0.277 S= 0.0103



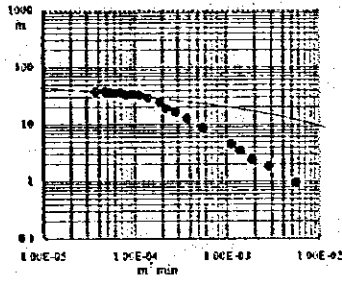
T= 7.6 k= 0.251



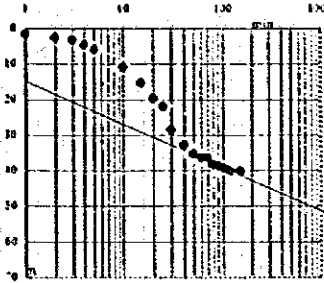
Appendix 2 (9) Result of Pumping Test Analysis

No. 2135B

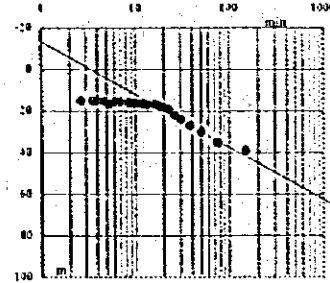
T= 21 k= 0.0533 S= 0.0354



T= 207E+00 k= 0.0575 S= 3.71E-02

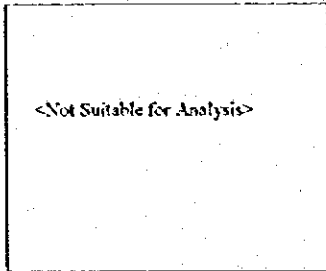


T= 0.956 k= 0.0265

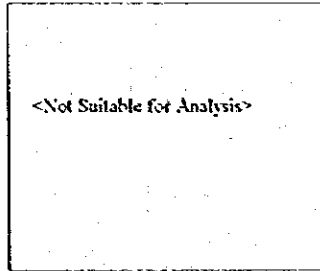


No. 1947A

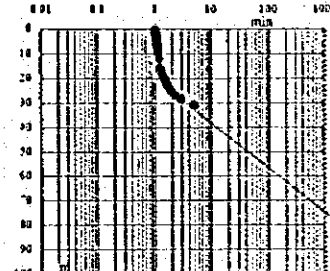
T= 5.16 k= 0.344 S= 1.43



T= 1.44 k= 0.0958 S= 0.399

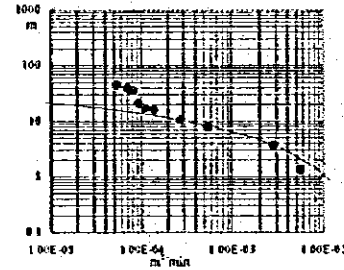


T= 0.884 k= 0.0587

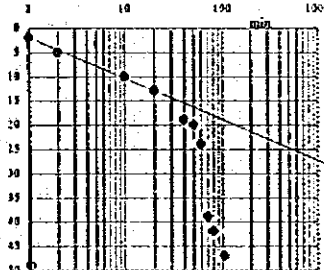


No. 1945-2

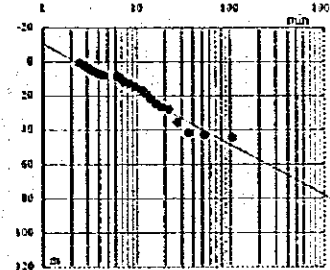
T= 1.25E+00 k= 1.05E-02 S= 2.03E-01



T= 1.23 k= 0.0304 S= 0.21

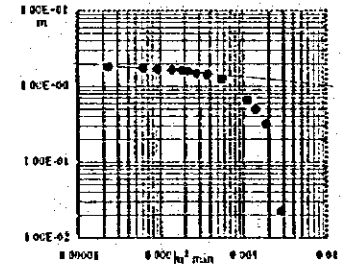


T= 0.363 k= 0.00864

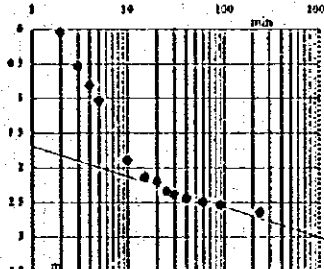


No. 1229-1

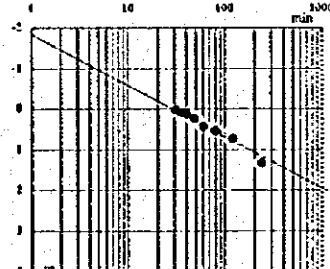
T= 7.30E+01 k= 1.52E+00 S= 2.16E-03



T= 72.7 k= 2.51 S= 0.00286

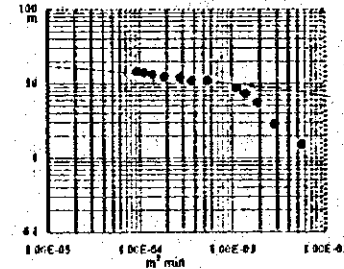


T= 27.6178 k= 0.252

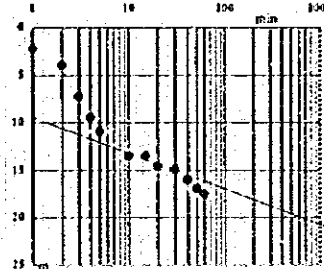


No. 2615-1

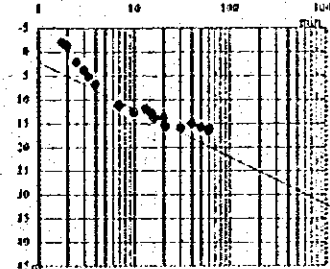
T= 5.37E+00 k= 1.07E+00 S= 3.92E-03



T= 6.98 k= 0.105 S= 0.000326



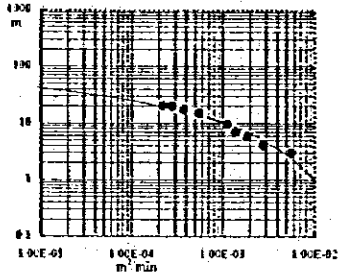
T= 3.06 k= 0.412



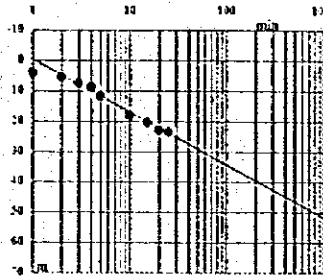
Appendix 2 (10) Result of Pumping Test Analysis

No. 2228-2

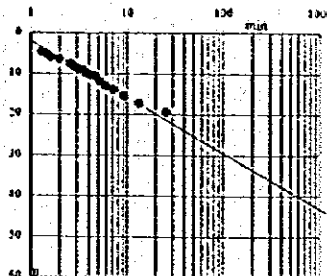
I = 1.72 k = 0.0367 S = 0.479



I = 1.64E+00 k = 0.0349 S = 3.82E-01

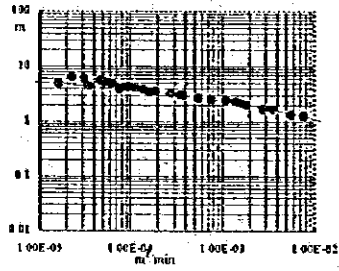


I = 2.62 k = 0.0557

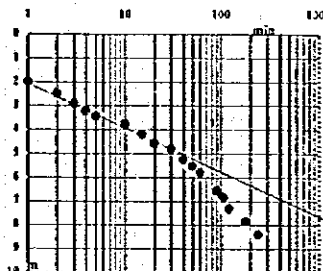


No. 2605C

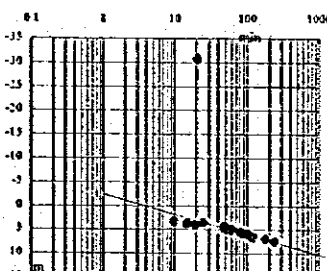
I = 3.53 k = 2.27 S = 0.0763



I = 1.26 k = 2.13 S = 0.0907

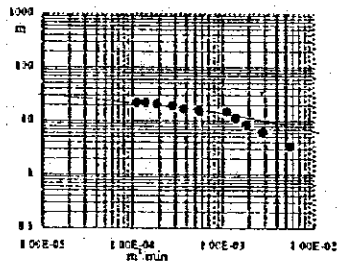


I = 1.89 k = 0.947

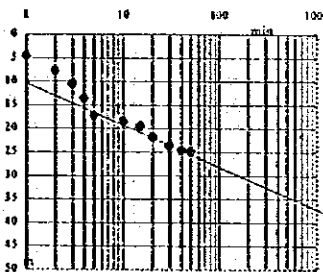


No. 2607B

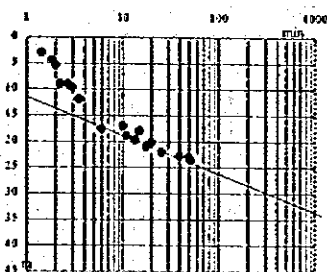
I = 2.18E+00 k = 7.03E-02 S = 3.64E-02



I = 2.07 k = 0.0668 S = 0.0394

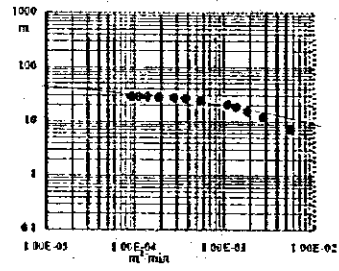


I = 2.51 k = 0.081

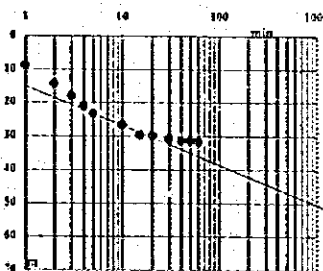


No. 2608A

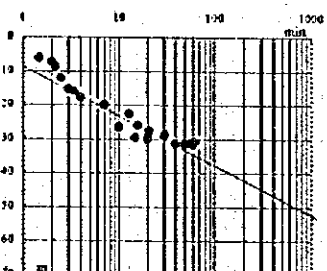
I = 2.36E-01 k = 7.86E-02 S = 1.58E-02



I = 0.933 k = 0.0778 S = 0.0142

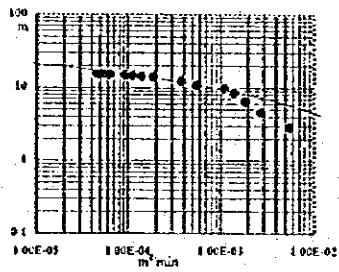


I = 0.739 k = 0.0633

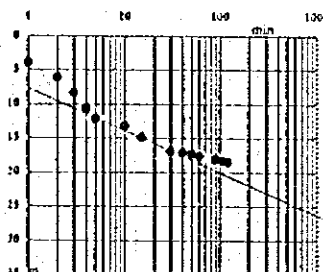


No. 2613A

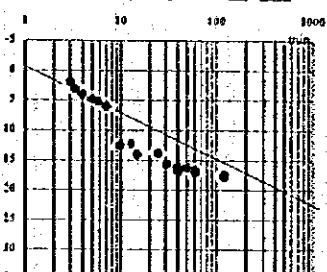
I = 7.74E+00 k = 1.29E+00 S = 1.25E-01



I = 7.65 k = 1.28 S = 0.122



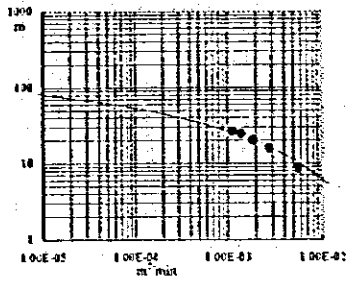
I = 6.15 k = 1.02



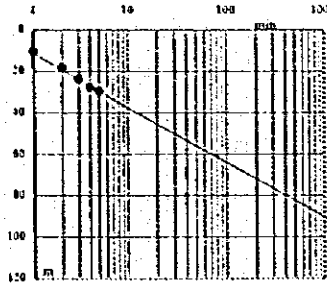
Appendix 2 (11) Result of Pumping Test Analysis

No. 1662

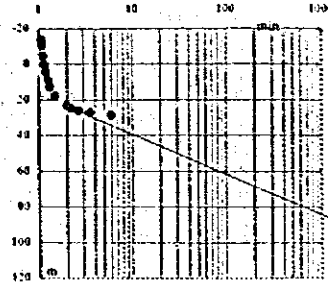
T= 13 k= 0.0341 S= 0.164



T= 1.53E+00 k= 0.0341 S= 1.53E-01

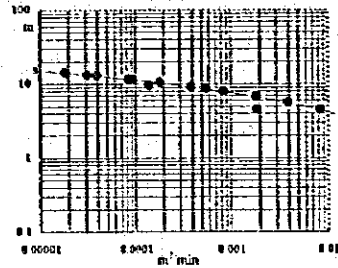


T= 1.76 k= 0.04

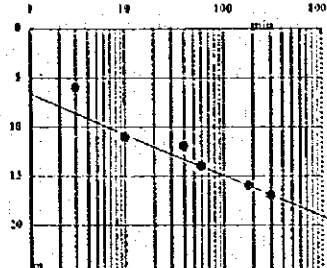


No. 1948-2

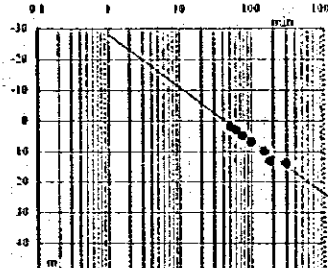
T= 6.02 k= 2.01 S= 0.0126



T= 6.08 k= 2.03 S= 0.0435

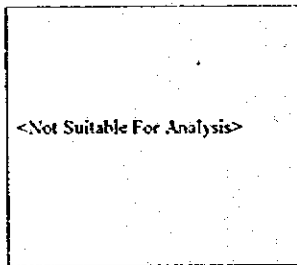


T= 1.43 k= 0.483

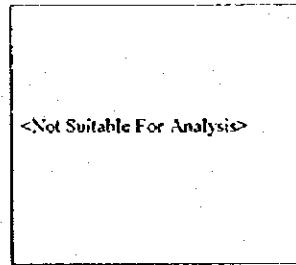


No. 2088

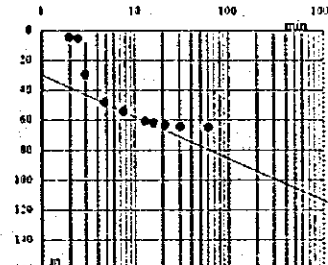
T= k= S=



T= k= S=

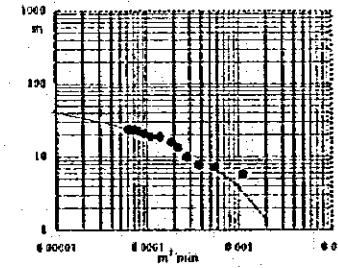


T= 0.186 k= 0.186

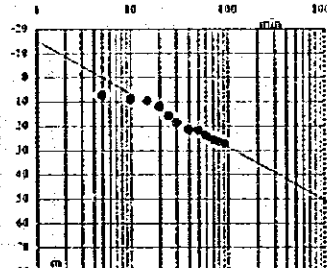


No. 2286-1

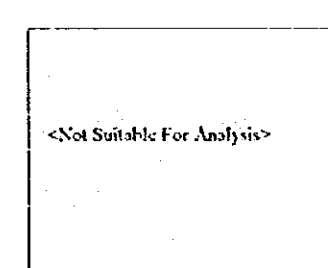
T= 6.66E-01 k= 1.86E-02 S= 2.05E-01



T= 0.654 k= 0.0131 S= 0.526

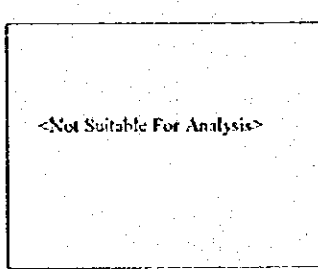


T= k=

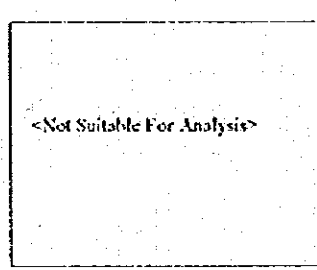


No. 2462-1

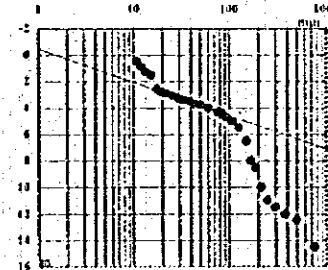
T= k= S=



T= k= S=



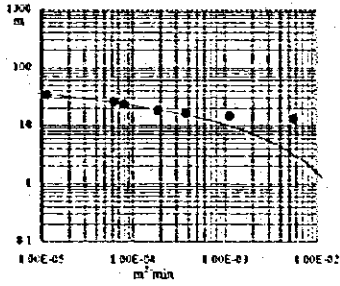
T= 7.55 k= 5.52



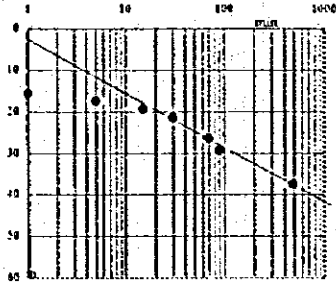
Appendix 2 (12) Result of Pumping Test Analysis

No. 3003

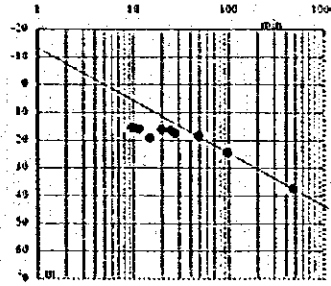
T= 0.706 k= 0.0223 S= 0.125



T= 1.26E-01 k= 0.0234 S= 1.28E-01

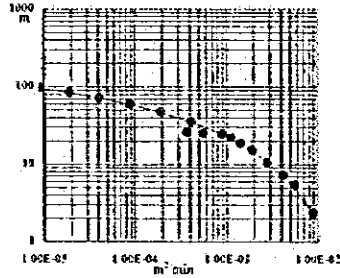


T= 0.5 k= 0.0161

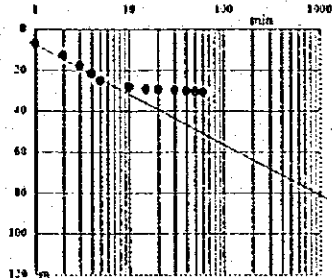


No. 1678-1

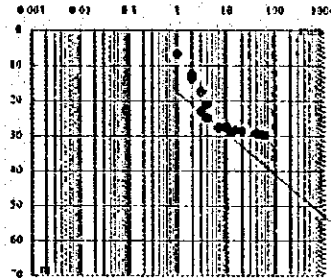
T= 0.0739 k= 0.00217 S= 0.0235



T= 0.109 k= 0.00312 S= 0.0153

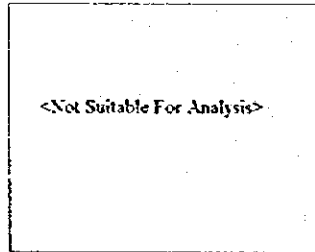


T= 0.23 k= 0.00656

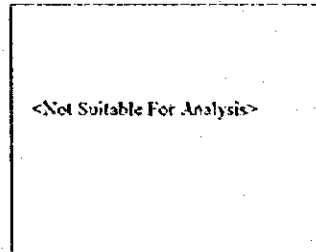


No. MB-14

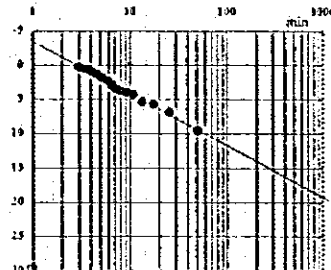
T= k= S=



T= k= S=

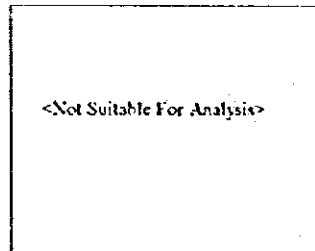


T= 2.03 k= 0.11

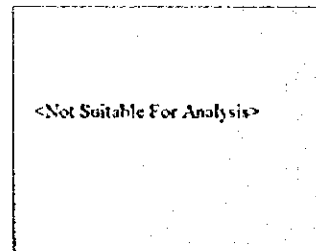


No. 1429

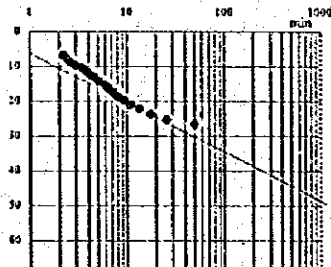
T= k= S=



T= k= S=

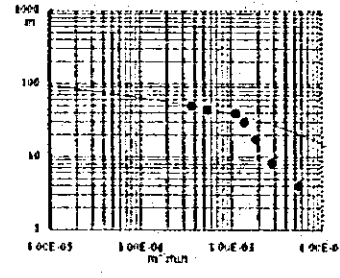


T= 0.561 k= 0.0137

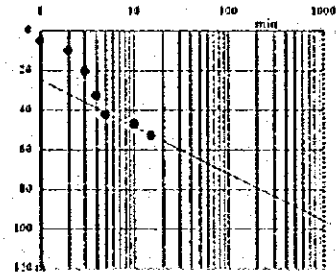


No. 1679

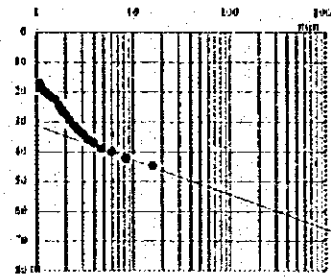
T= 2.31E-01 k= 1.92E-02 S= 1.61E-03



T= 0.247 k= 0.0206 S= 0.00617



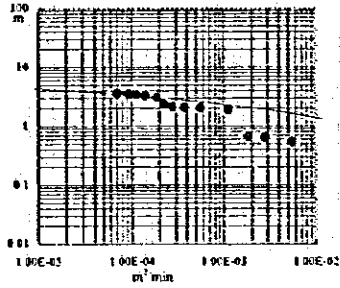
T= 0.805 k= 0.0321



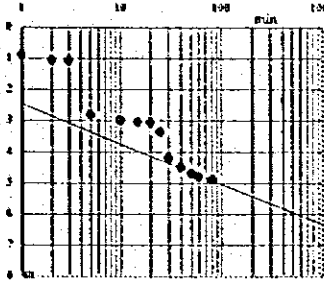
Appendix 2 (13) Result of Pumping Test Analysis

No. 2037

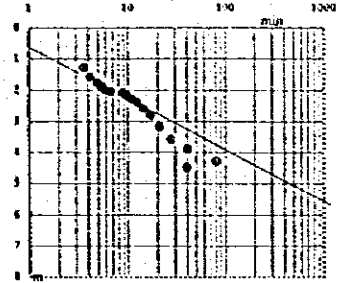
T= 44 k= 0.62 S= 0.139



T= 4.39E+01 k= 0.618 S= 1.54E-01

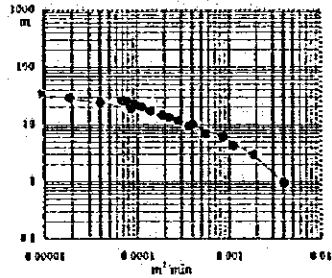


T= 34.6 k= 0.487

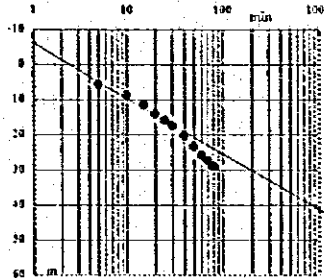


No. 2205

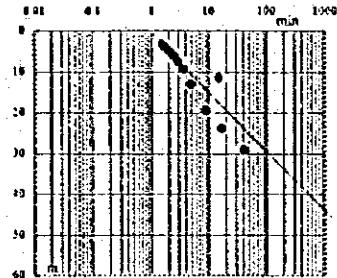
T= 0.374 k= 0.0187 S= 0.256



T= 0.37 k= 0.0185 S= 0.252

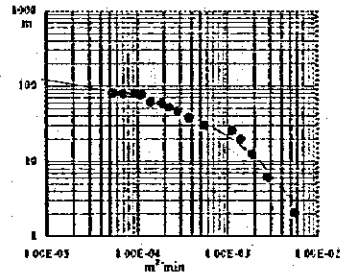


T= 0.403 k= 0.0202

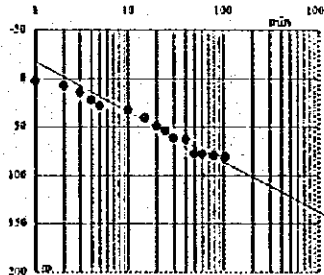


No. 2204

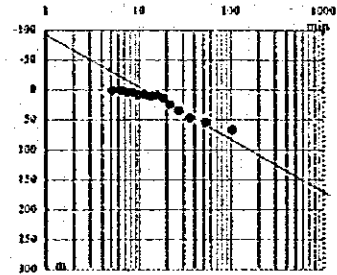
T= 2.17E-01 k= 8.70E-03 S= 1.27E-01



T= 0.208 k= 0.00833 S= 0.125

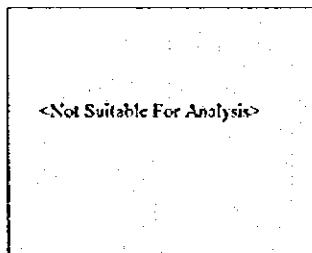


T= 0.123 k= 0.0039

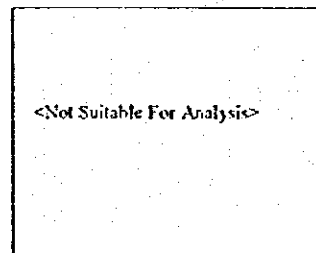


No. 2555

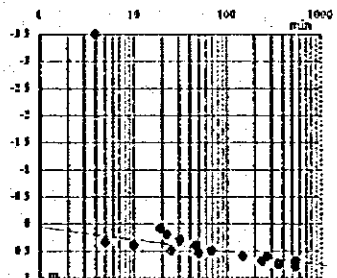
T= k= S=



T= k= S=

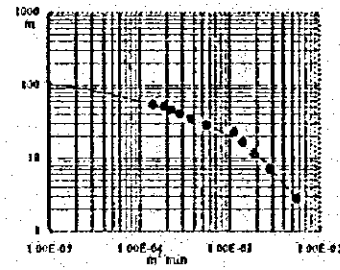


T= 682 k= 31

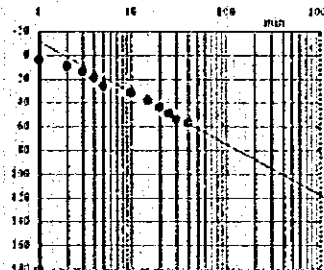


No. 2147

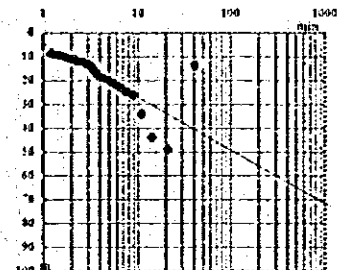
T= 1.14E-01 k= 1.90E-02 S= 5.90E-02



T= 0.113 k= 0.0189 S= 0.0589



T= 0.21 k= 0.0367



Appendix 2 (14) Result of Pumping Test Analysis

No. 2136C

T=

k=

S=

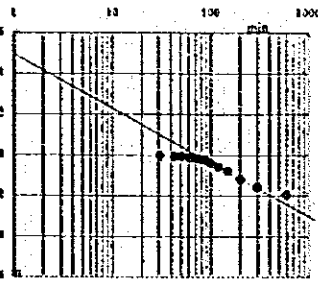
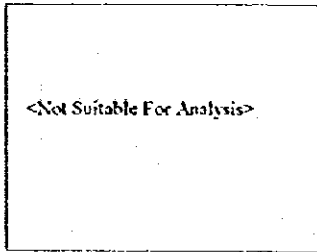
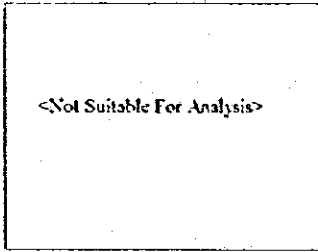
T=

k=

S=

T= 2.2

k= 1.95



No. 2012

T= 2.07

k= 0.372

S= 0.168

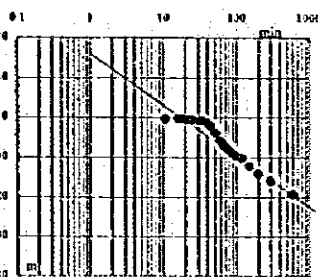
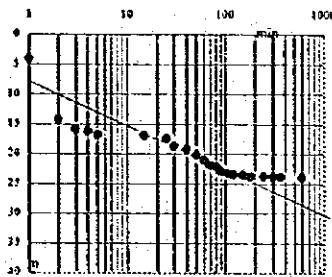
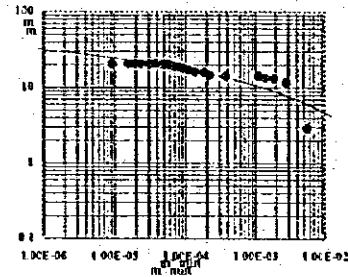
T= 6.99

k= 0.368

S= 0.171

T= 4.08

k= 0.218



No. 1648

T= 2.27E+00

k= 8.89E-02

S= 3.75E-02

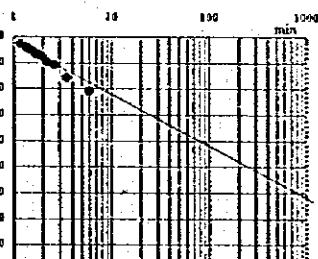
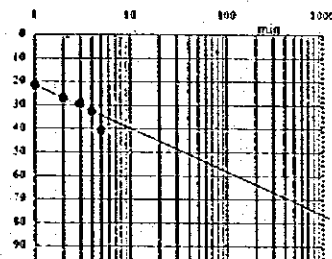
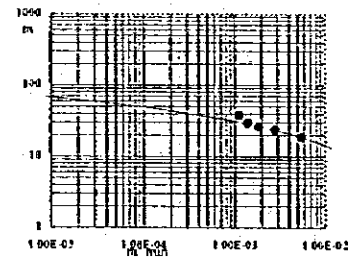
T= 2.15

k= 0.086

S= 0.0408

T= 1.98

k= 0.0793



No. 1532

T= 1.12E+00

k= 2.34E-02

S= 7.68E-02

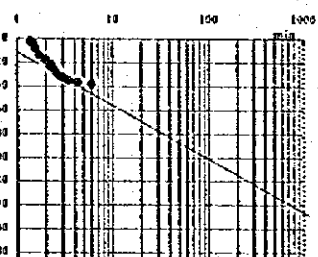
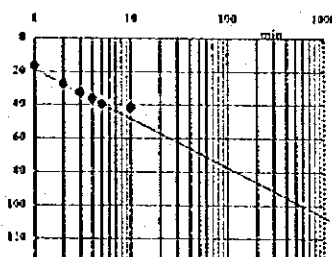
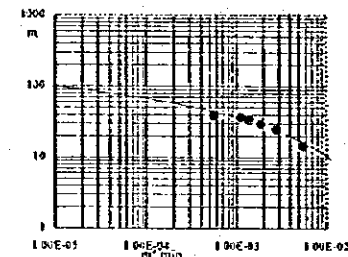
T= 1.13

k= 0.0236

S= 0.0706

T= 0.74

k= 0.0154



No. 1428

T=

k=

S=

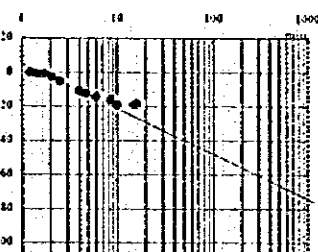
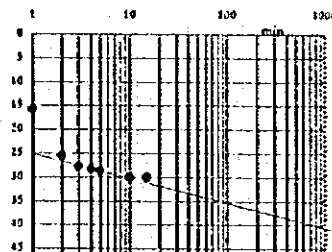
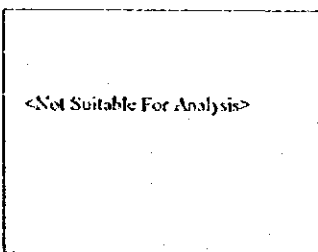
T= 4

k= 0.114

S= 0.0000138

T= 0.772

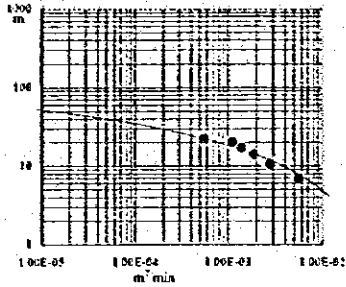
k= 0.0523



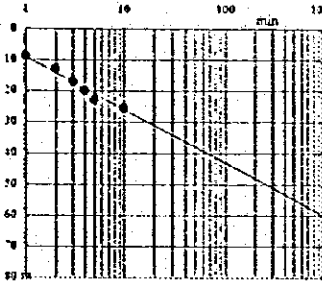
Appendix 2 (15) Result of Pumping Test Analysis

No. 1432

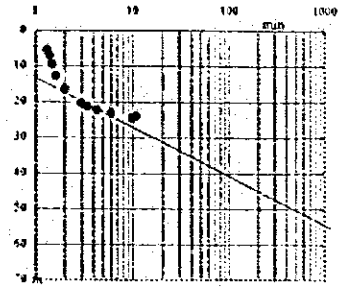
T = 1.87 k = 0.0693 S = 0.154



T = 1.86E+00 k = 0.0687 S = 1.55E-01

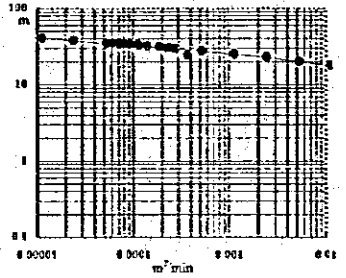


T = 2.3 k = 0.0852

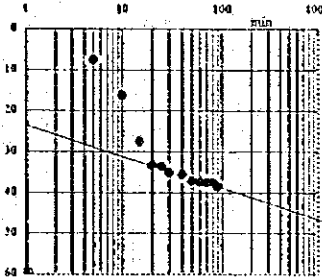


No. 2603

T = 1.65 k = 0.165 S = 0.0004



T = 1.66 k = 0.166 S = 0.000372

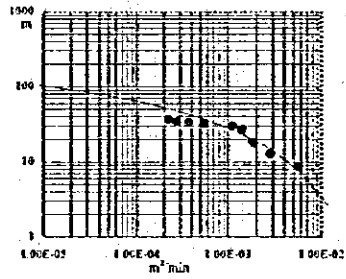


T = 50.6 k = 5.06

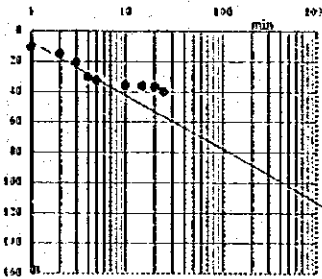
<Not Suitable For Analysis>

No. 1743

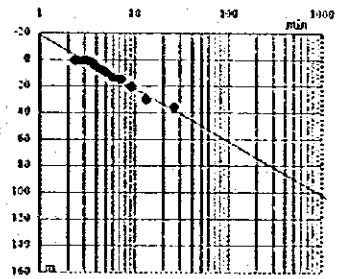
T = 2.19E+01 k = 7.43E-03 S = 4.82E-02



T = 0.224 k = 0.00761 S = 0.0385

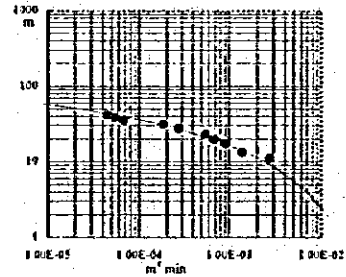


T = 0.196 k = 0.06665

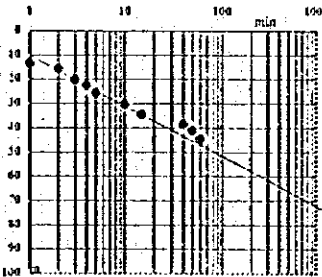


No. 1724

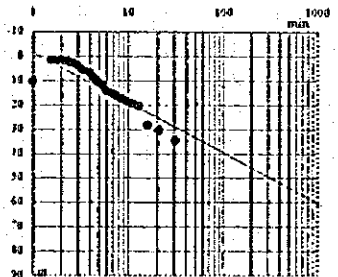
T = 1.23E+00 k = 1.23E-01 S = 2.24E-01



T = 1.22 k = 0.122 S = 0.222

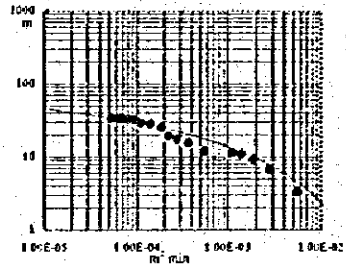


T = 1.23 k = 0.123

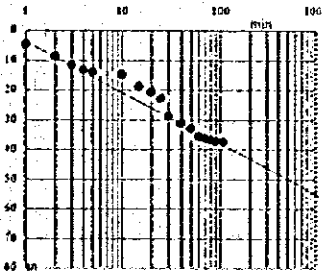


No. 1679

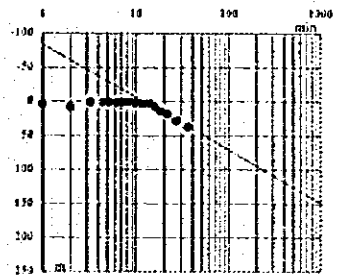
T = 1.28E+00 k = 1.45E-02 S = 2.03E-01



T = 1.24 k = 0.0386 S = 0.204



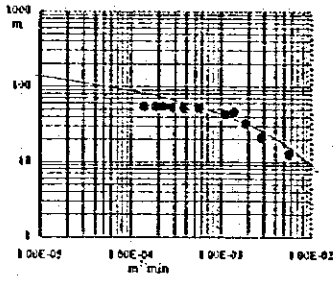
T = 0.273 k = 0.09744



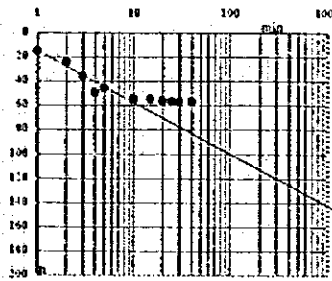
Appendix 2 (16) Result of Pumping Test Analysis

No. 1633

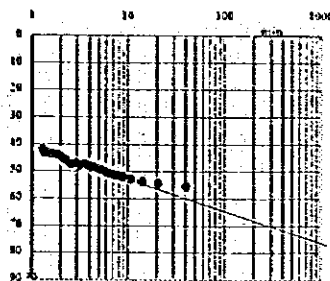
T= 0.104 k= 0.00651 S= 0.0131



T= 1.04E-01 k= 0.00651 S= 1.30E-02

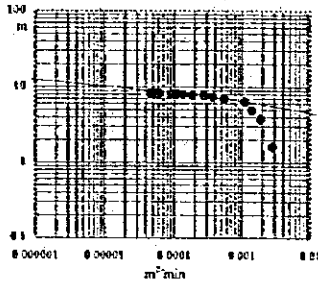


T= 0.376 k= 0.0235

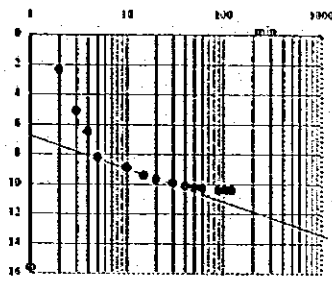


No. 2627

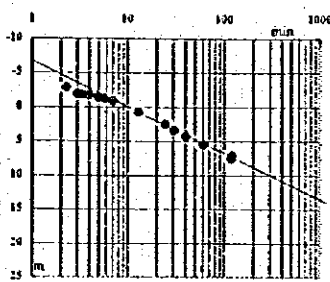
T= 71.2 k= 30.3 S= 0.0172



T= 71.4 k= 30.4 S= 0.0174

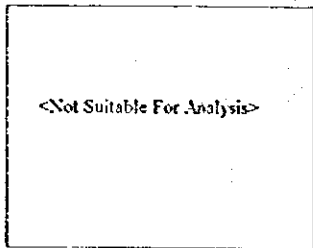


T= 23.3 k= 9.92

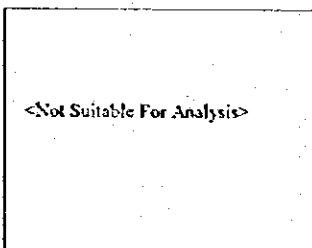


No. KB05

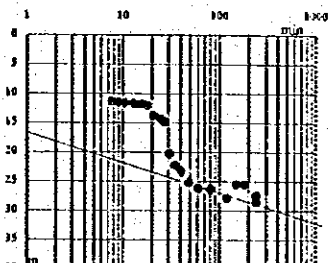
T= k= S=



T= k= S=

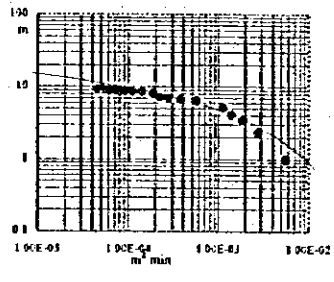


T= 3.06 k= 0.383

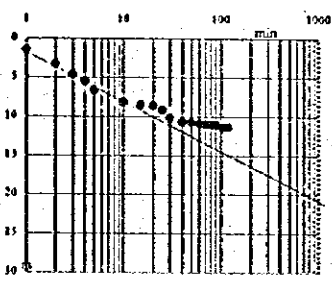


No. KB02

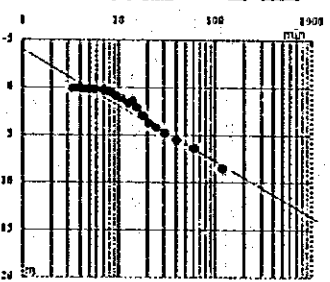
T= 1.86E+00 k= 9.32E-01 S= 2.33E-01



T= 1.74 k= 0.872 S= 0.255

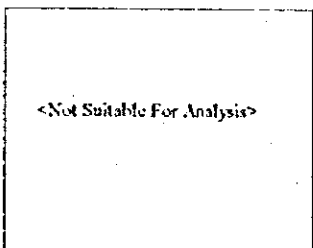


T= 1.82 k= 0.943

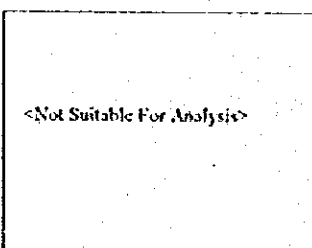


No. C11

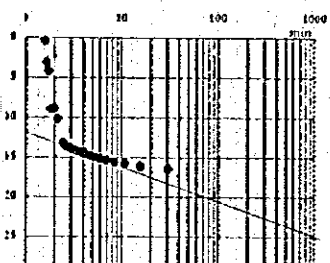
T= k= S=



T= k= S=



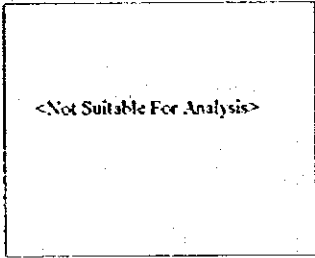
T= 1.97 k= 0.328



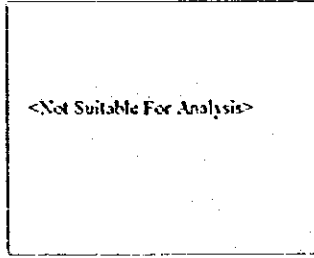
Appendix 2 (17) Result of Pumping Test Analysis

No. MW2

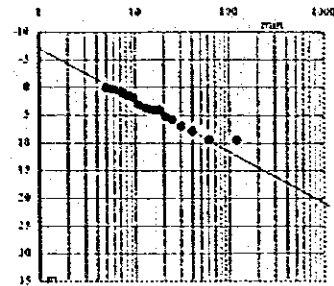
I= k= S=



I= k= S=

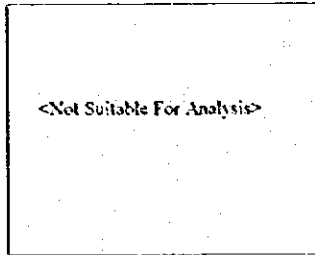


I= 5.08 k= 0.232

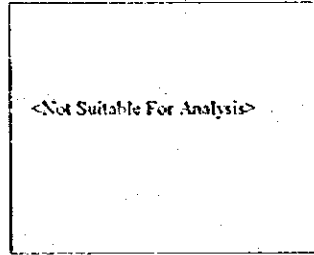


No. MW03

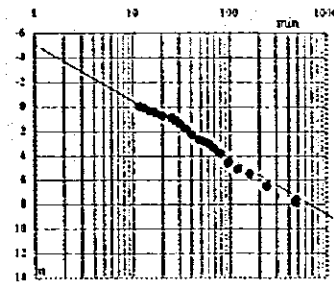
I= k= S=



I= k= S=

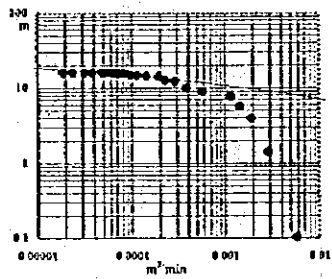


I= 23.2 k= 1.55

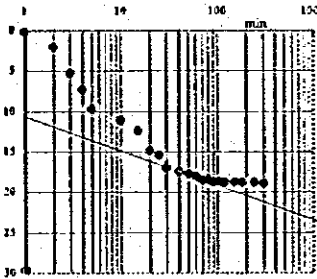


No. MW04

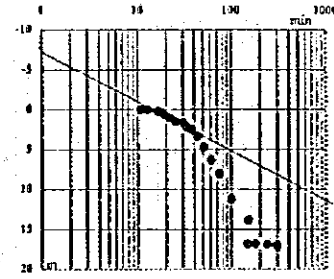
I= 4.45E+00 k= 2.27E-01 S= 4.56E-03



I= 4.45 k= 0.228 S= 0.00377

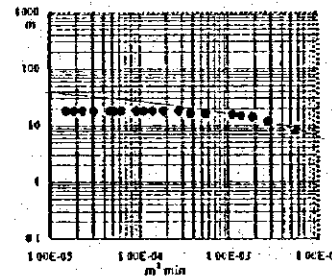


I= 3.04 k= 0.155

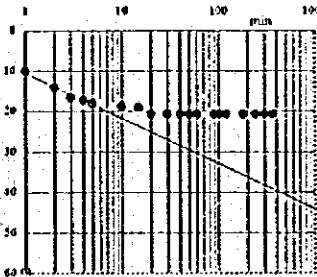


No. 2638

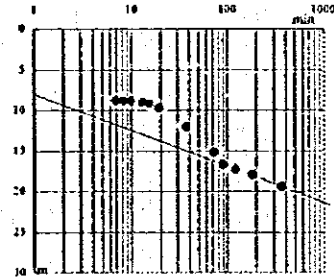
I= 2.46E+00 k= 1.08E-01 S= 7.63E-02



I= 2.47 k= 0.302 S= 0.0785

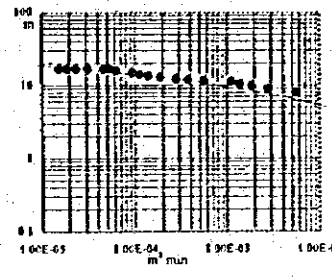


I= 6.24 k= 0.272

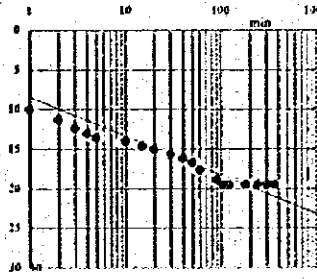


No. 1640

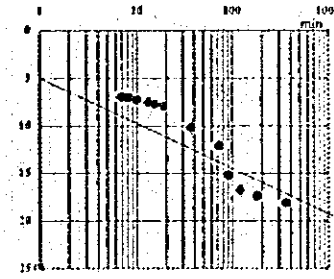
I= 2.55E+00 k= 1.83E-01 S= 1.47E-02



I= 2.56 k= 0.183 S= 0.0142



I= 2.66 k= 0.19



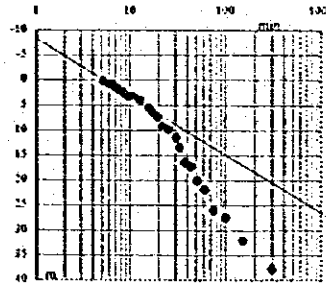
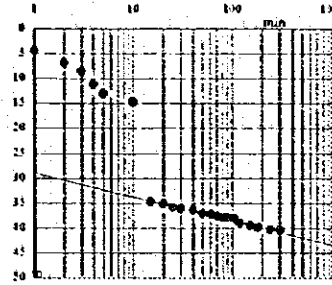
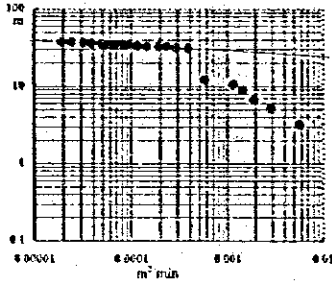
Appendix 2 (18) Result of Pumping Test Analysis

No. IUSC3

T = 8.15 k = 0.34 S = 2.26E-06

T = 3.16E+00 k = 0.34 S = 2.38E-06

T = 3.4 k = 0.142

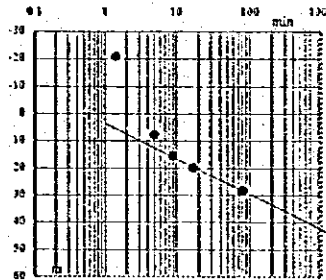
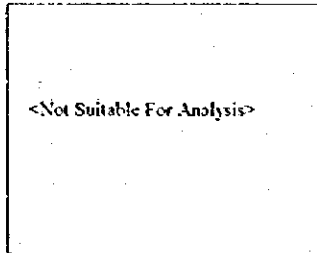
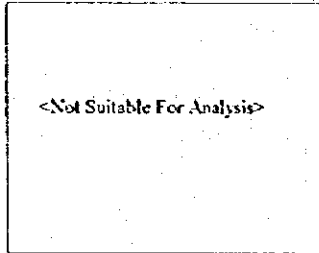


No. IUSC12

T = k = S =

T = k = S =

T = 0.541 k = 0.136

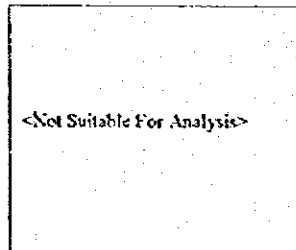
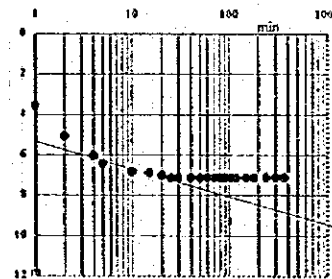
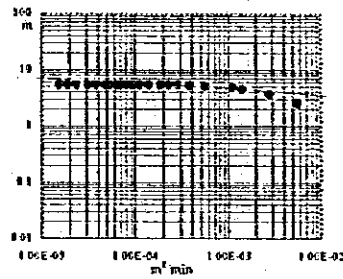


No. 2634

T = 3.49E+01 k = 2.05E+00 S = 1.19E-03

T = 34.9 k = 2.05 S = 0.00115

T = k =

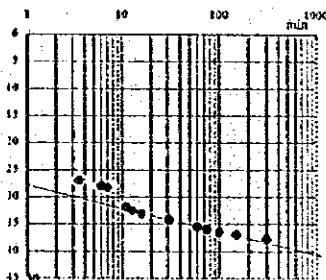
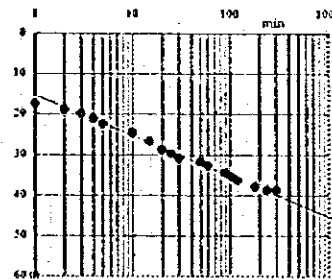
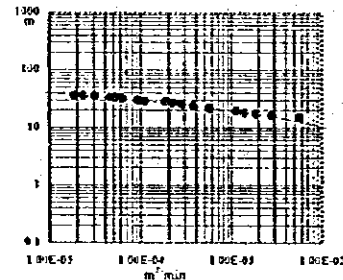


No. 2635

T = 2.53E-01 k = 1.27E-02 S = 2.02E-03

T = 0.253 k = 0.0127 S = 0.00202

T = 0.592 k = 0.0296

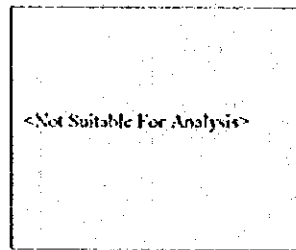
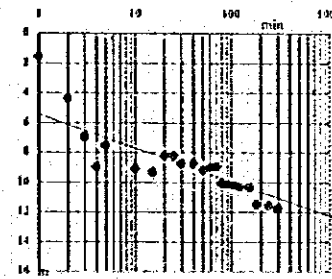
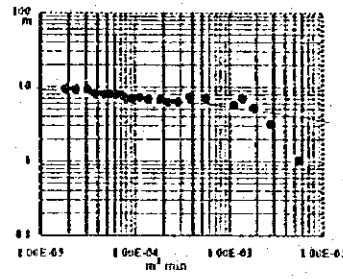


No. 1N5

T = 3.29E+01 k = 3.44E+00 S = 4.47E-02

T = 38.5 k = 3.5 S = 0.0436

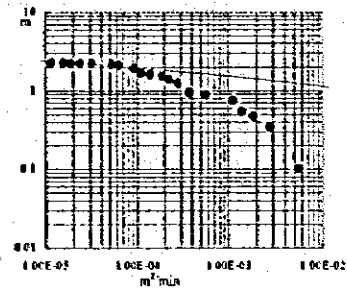
T = k =



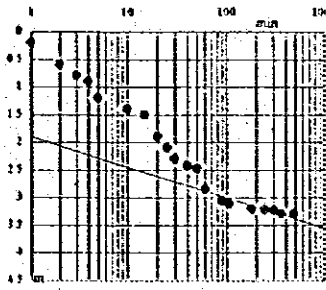
Appendix 2 (19) Result of Pumping Test Analysis

No. 1N-6

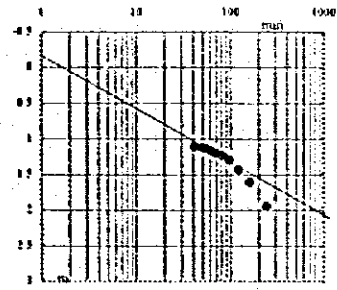
T= 225 k= 207 S= 0.0232



T= 231E+02 k= 21 S= 2.34E-02

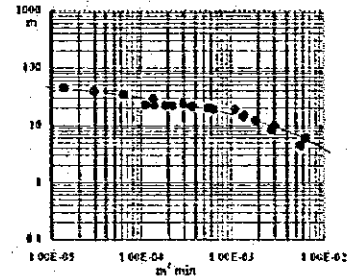


T= 171 k= 13.6

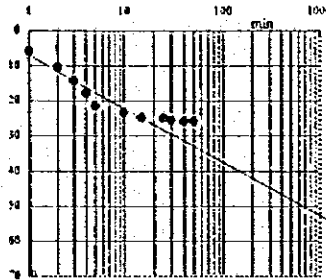


No. 2273

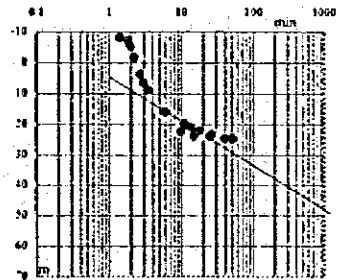
T= 402 k= 134 S= 0.00413



T= 404 k= 135 S= 0.00406

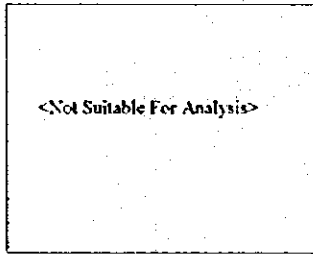


T= 202 k= 0.672

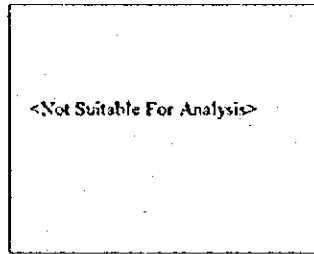


No. KAL02

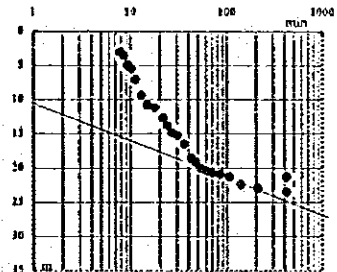
T= k= S=



T= k= S=

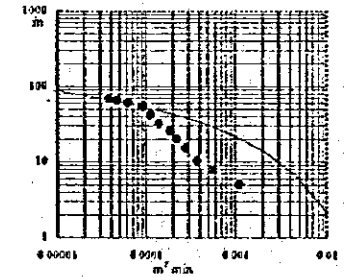


T= 3.46 k= 0.0836

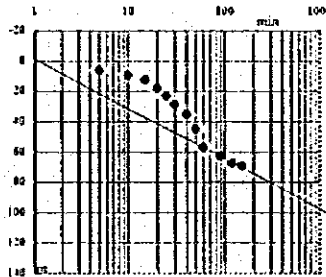


No. 2282

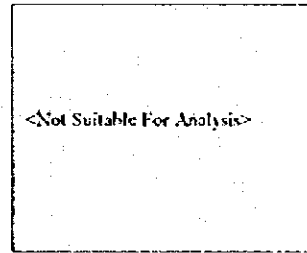
T= 3.69E-01 k= 4.10E-02 S= 1.03E-01



T= 0.352 k= 0.0392 S= 0.11

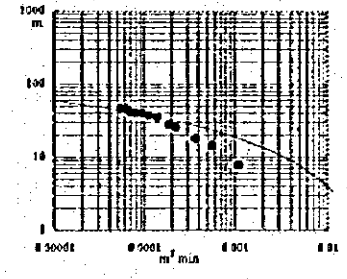


T= k=

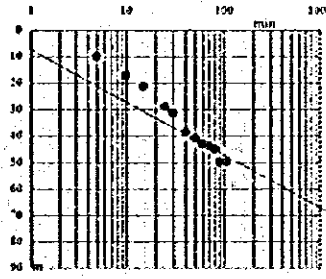


No. 2127

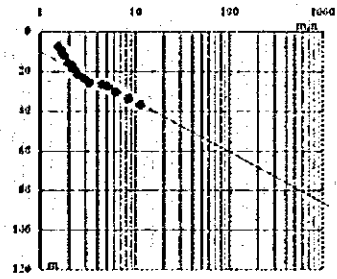
T= 2.93E-01 k= 2.93E-02 S= 3.57E-02



T= 0.293 k= 0.0293 S= 0.0358



T= 0.311 k= 0.0231



Appendix 2 (20) Result of Pumping Test Analysis

No. KAI01

T=

k=

S=

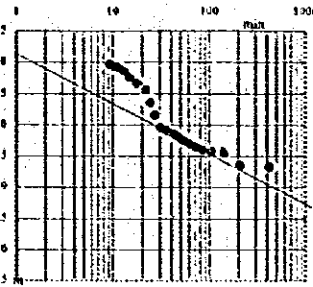
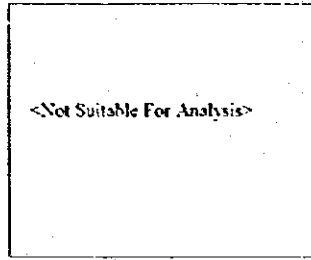
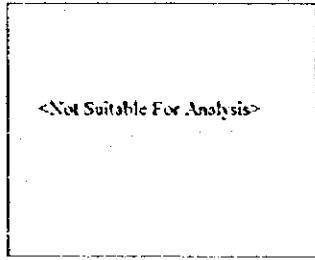
T=

k=

S=

T= 2.36

k= 0.147



No. 2660-3

T= 1.67

k= 0.0316

S= 0.0282

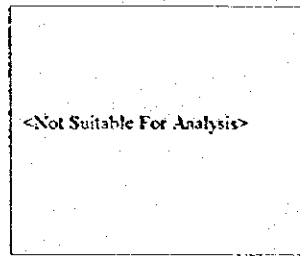
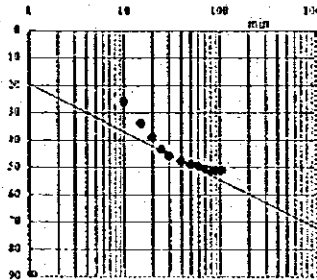
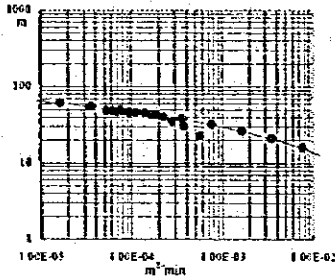
T= 1.62

k= 0.0307

S= 0.0386

T=

k=



No. 2619

T=

k=

S=

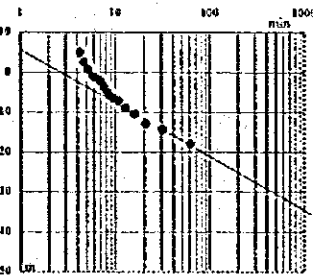
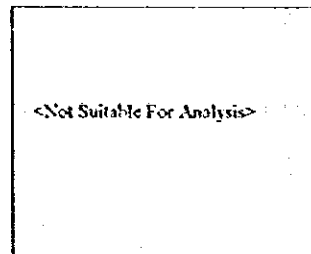
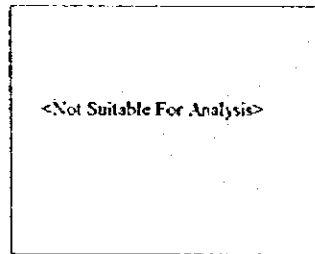
T=

k=

S=

T= 1.88

k= 0.313



No. 2618

T= 3.86E+00

k= 4.82E-01

S= 2.72E-01

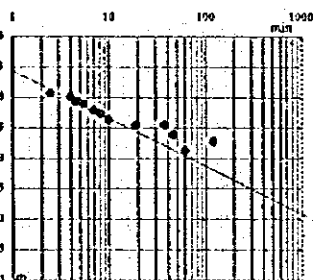
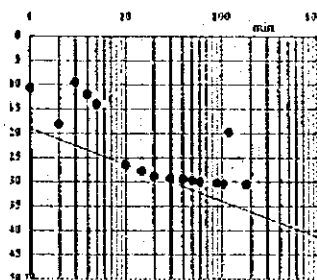
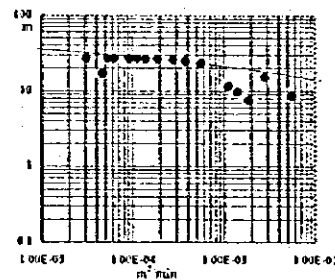
T= 3.82

k= 0.477

S= 0.06295

T= 3.63

k= 0.453



No. CHS03

T= 1.24E+01

k= 6.22E+00

S= 1.47E-02

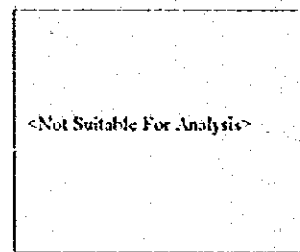
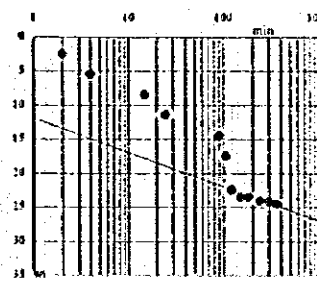
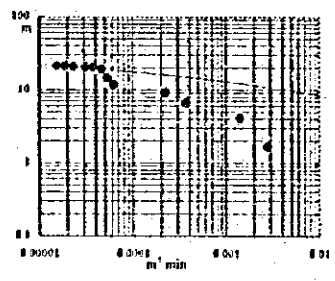
T= 12.5

k= 6.27

S= 0.0154

T=

k=



Appendix 2 (21) Result of Pumping Test Analysis

No. 2070

T=

k=

S=

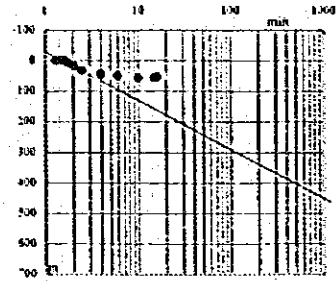
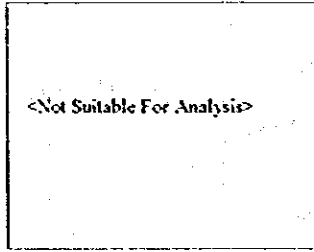
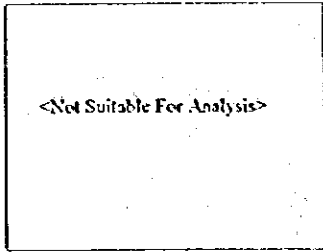
T=

k=

S=

T= 0.687

k= 0.0312



No. 2151

T= 191

k= 0.616

S= 0.0547

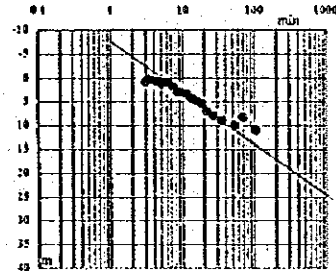
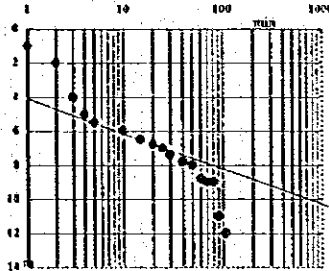
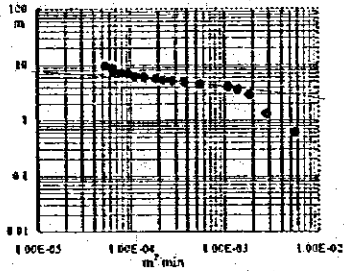
T= 191

k= 0.615

S= 0.0558

T= 367

k= 0.118



No. 2155

T= 6.02E+00

k= 2.31E-01

S= 3.02E-02

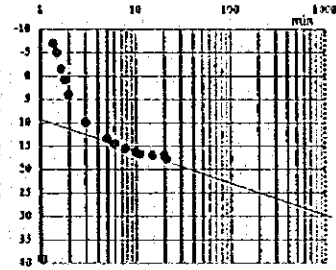
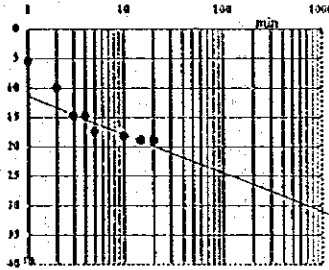
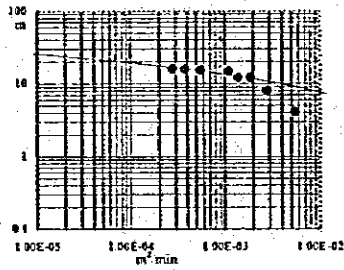
T= 6.06

k= 0.233

S= 0.0301

T= 5.8

k= 0.223



No. 1957-1

T= 1.37E+00

k= 2.43E-01

S= 2.47E-03

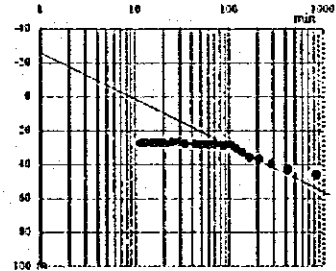
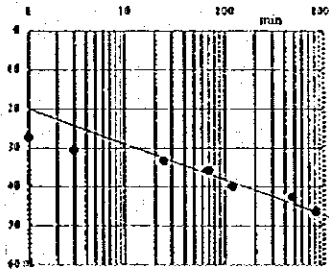
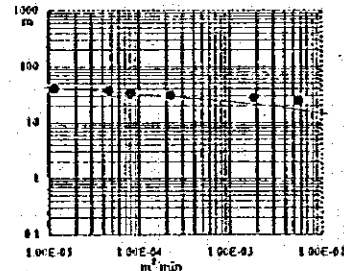
T= 1.4

k= 0.351

S= 0.0923

T= 0.462

k= 0.116



No. 2148-1

T= 1.09E+00

k= 1.37E-01

S= 5.66E-02

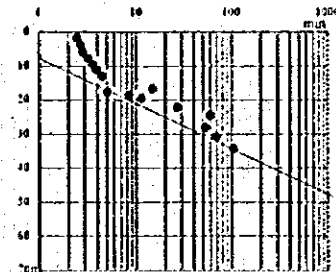
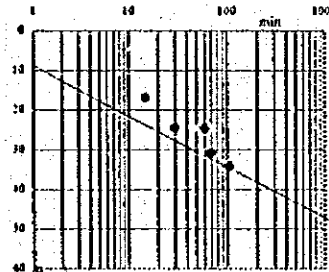
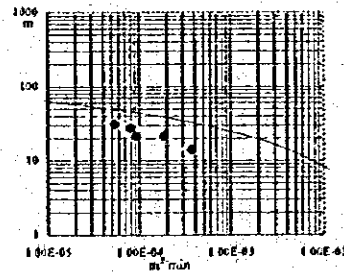
T= 1.046

k= 0.131

S= 0.0692

T= 0.466

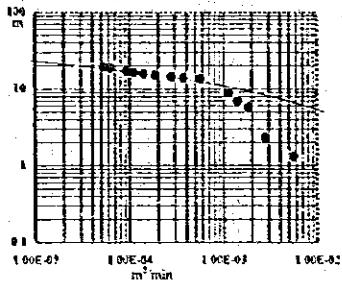
k= 0.0582



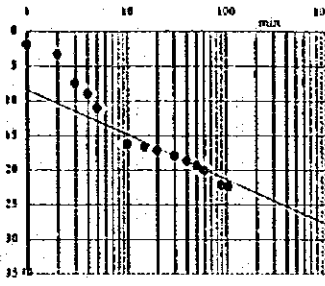
Appendix 2 (22) Result of Pumping Test Analysis

No. 2612A

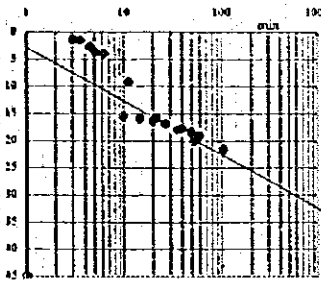
T= 195 k= 0.0609 S= 0.0249



T= 196E+00 k= 0.0614 S= 2.66E-02

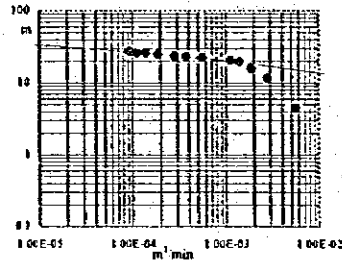


T= 128 k= 0.04

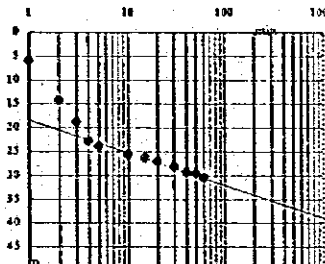


No. 2617C

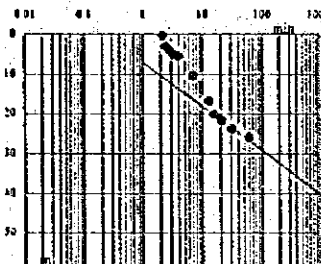
T= 229 k= 0.104 S= 0.00134



T= 231 k= 0.105 S= 0.00129

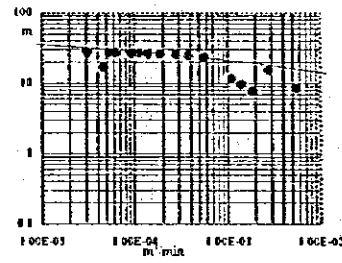


T= 144 k= 0.0654

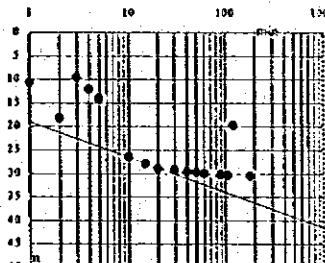


No. 2618B

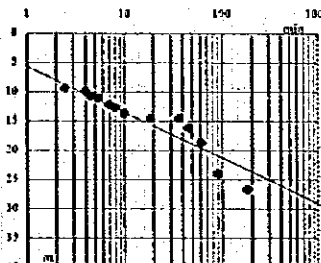
T= 386E+00 k= 4.82E-01 S= 2.72E-03



T= 382 k= 0.477 S= 0.00295

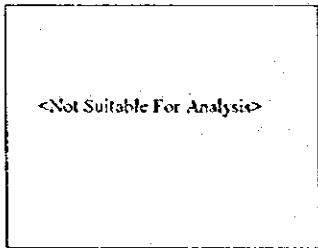


T= 263 k= 0.453

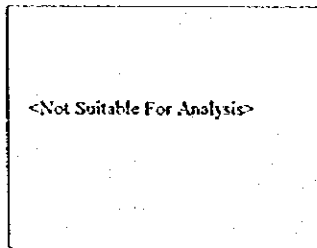


No. 2619B

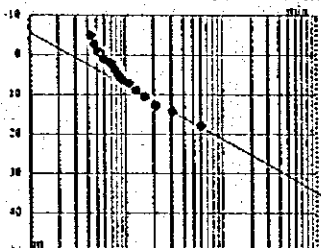
T= k= S=



T= k= S=

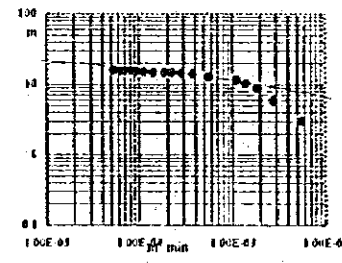


T= 168 k= 0.313

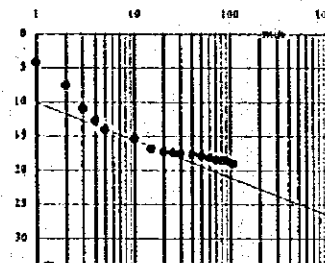


No. 2622C

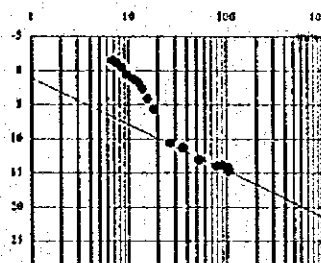
T= 1.90E+00 k= 5.69E-01 S= 3.08E-02



T= 7.4 k= 0.569 S= 0.0303



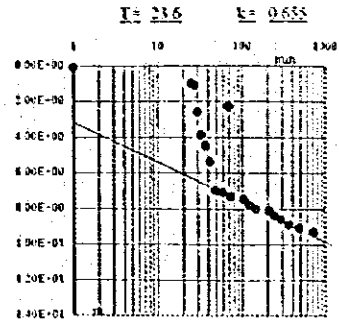
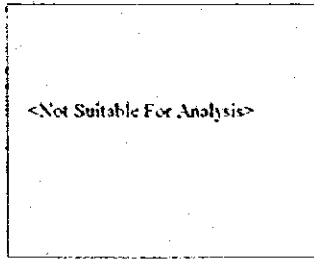
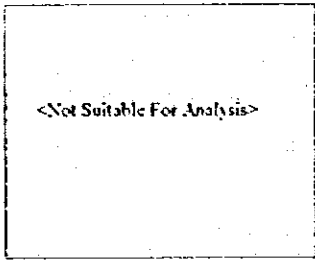
T= 6.04 k= 0.464



Appendix 2 (23) Result of Pumping Test Analysis

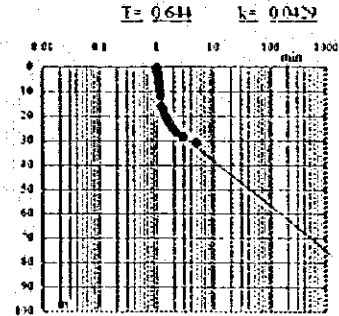
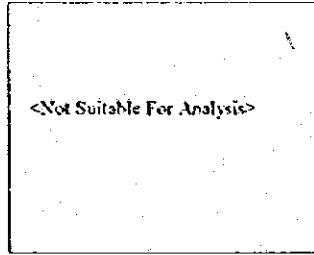
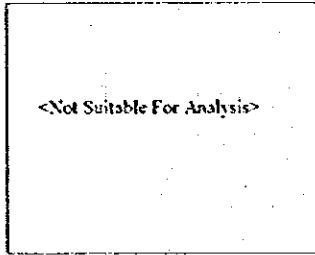
No. 2165

$T =$ $k =$ $S =$ $T =$ $k =$ $S =$



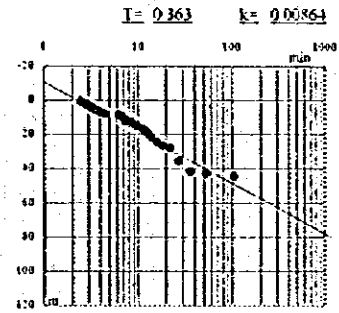
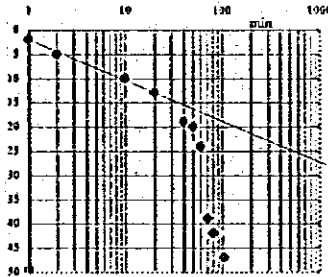
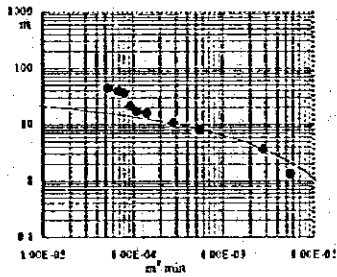
No. 1947

$T =$ $k =$ $S =$ $T =$ $k =$ $S =$



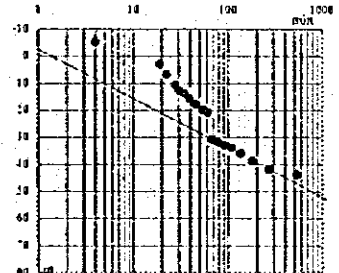
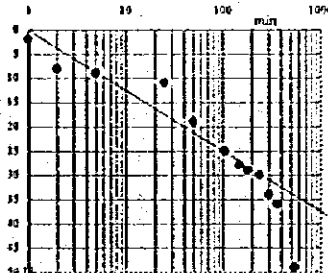
No. 1889

$T = 1.28E+09$ $k = 3.03E-03$ $S = 2.03E-01$ $T = 1.28$ $k = 0.0304$ $S = 0.21$



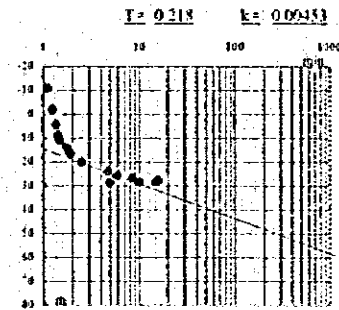
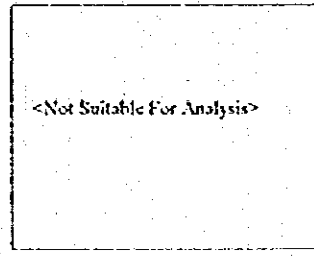
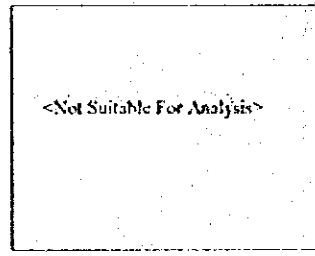
No. 1846

$T =$ $k =$ $S =$ $T = 2.23$ $k = 0.19$ $S = 0.632$ $T = 1.56$ $k = 0.13$



No. 1609

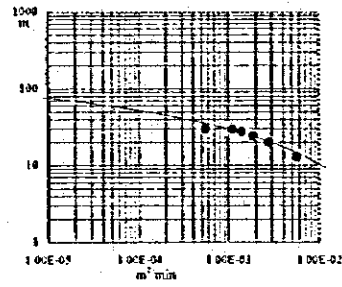
$T =$ $k =$ $S =$ $T =$ $k =$ $S =$



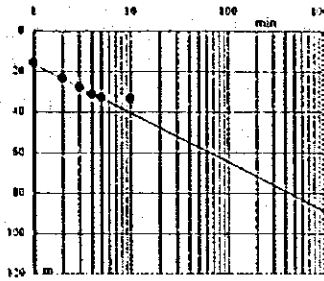
Appendix 2 (24) Result of Pumping Test Analysis

No. 1660

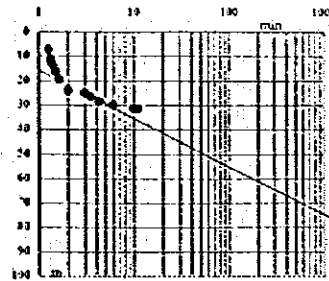
T= 3.58 k= 0.073 S= 0.169



T= 3.25E+00 k= 0.0669 S= 1.90E-01

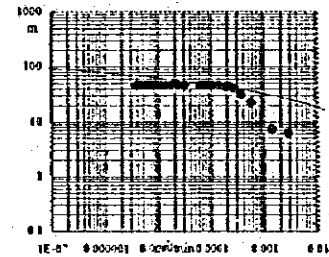


T= 4.03 k= 0.0821

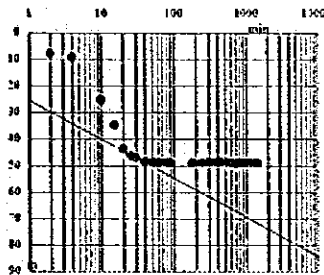


No. 1233

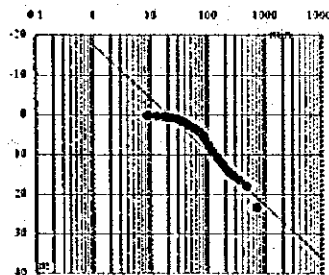
T= 2.36 k= 0.105 S= 0.0124



T= 2.36 k= 0.106 S= 0.0126

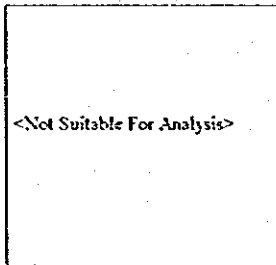


T= 2.57 k= 0.115

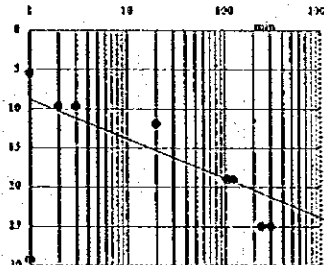


No. 1964-1

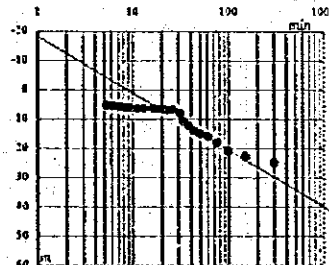
T= k= S=



T= 19.4 k= 0.531 S= 0.0521

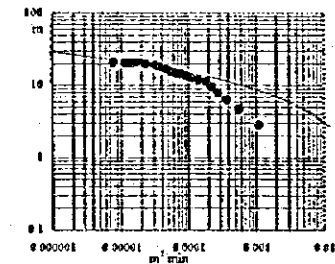


T= 2.69 k= 0.138

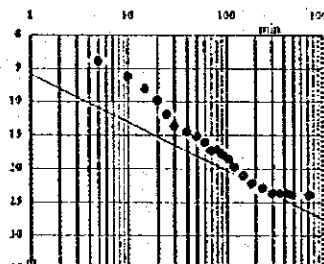


No. 2593

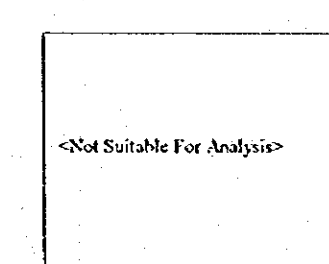
T= 4.71E+00 k= 2.77E+01 S= 2.06E-01



T= 4.72 k= 27.8 S= 0.2

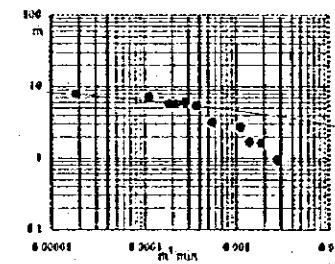


T= k=

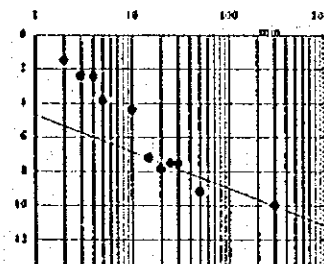


No. 1992

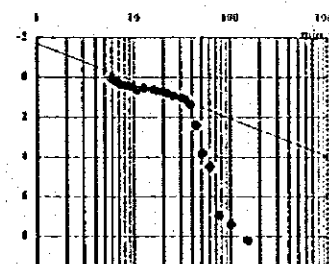
T= 1.18E+01 k= 8.48E-01 S= 2.12E-02



T= 11.8 k= 0.84 S= 0.0213



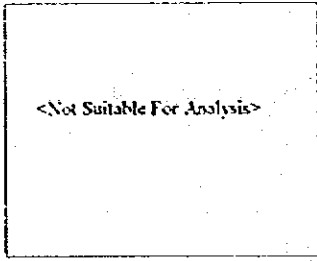
T= 11.4 k= 0.956



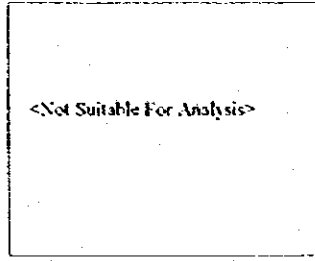
Appendix 2 (25) Result of Pumping Test Analysis

No. 2950

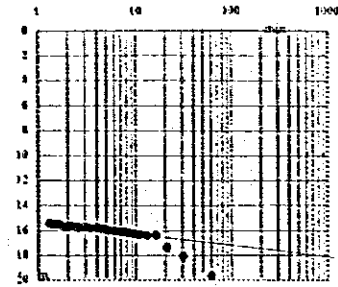
T= k= S=



T= k= S=

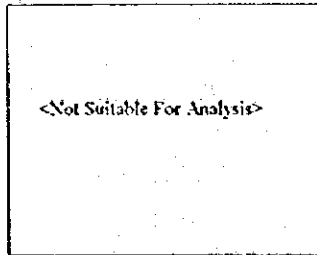


T= 191 k= 3.47

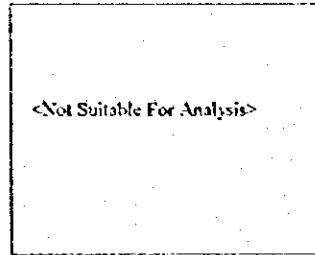


No. 3047

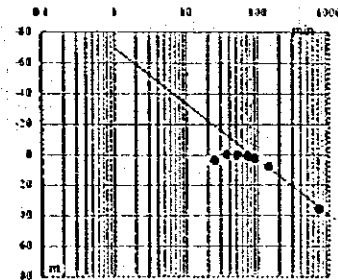
T= k= S=



T= k= S=

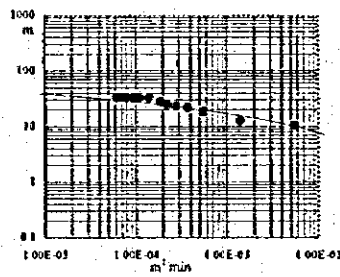


T= 0.684 k= 0.114

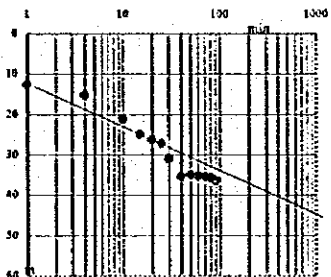


No. 1365

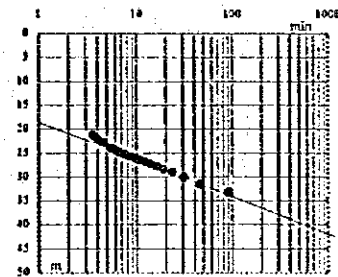
T= 2.36E+02 k= 1.39E-01 S= 1.55E-02



T= 2.34 k= 0.138 S= 0.0482

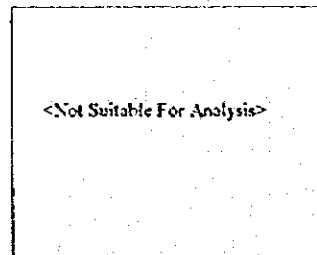


T= 3.24 k= 0.191

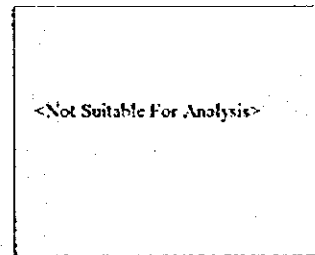


No. 1368

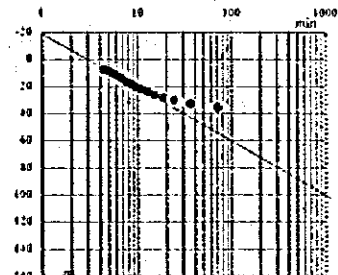
T= k= S=



T= k= S=

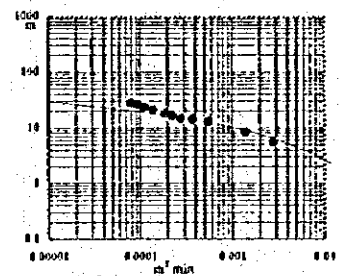


T= 0.477 k= 0.0106

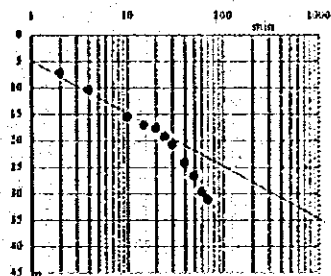


No. 1354

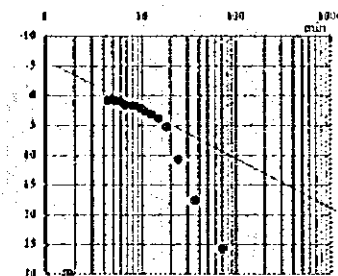
T= 2.85E+00 k= 1.09E-01 S= 2.42E-01



T= 2.86 k= 0.11 S= 0.257



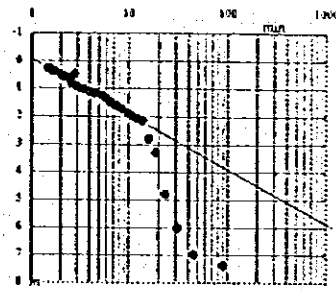
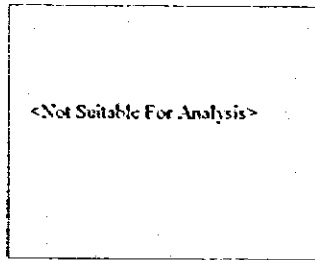
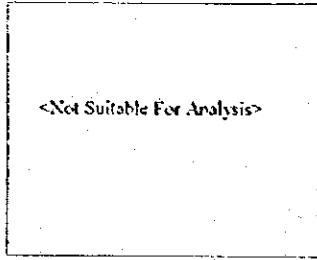
T= 3.45 k= 0.133



Appendix 2 (26) Result of Pumping Test Analysis

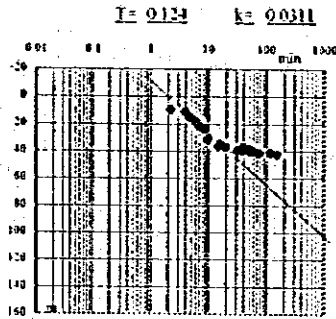
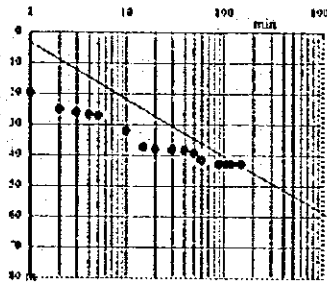
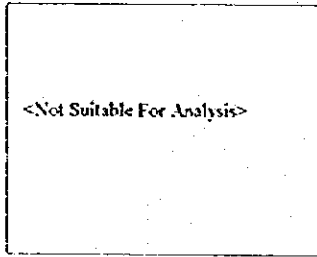
No. 1813

T= k= S= T= k= S=



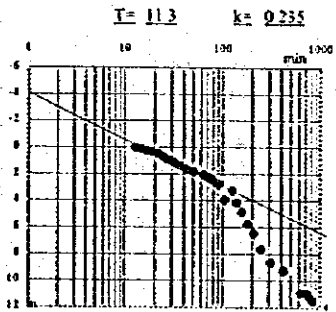
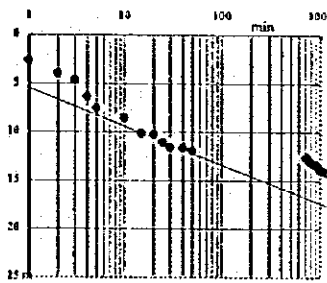
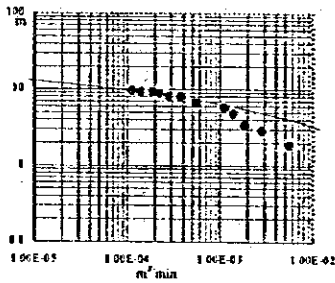
No. 2628

T= k= S= T= 0.237 k= 0.0644 S= 0.0473



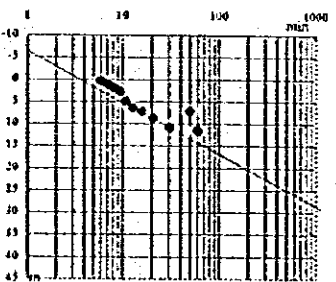
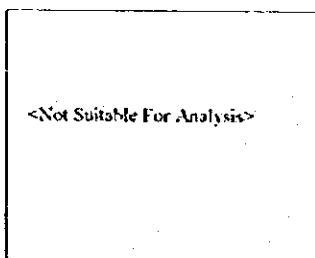
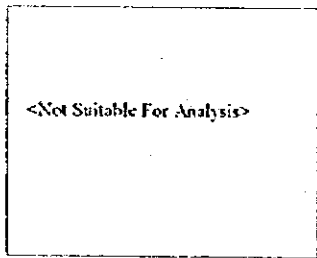
No. 1578

T= 1.04E+01 k= 2.17E-01 S= 1.00E-01 T= 9.92 k= 0.208 S= 0.115



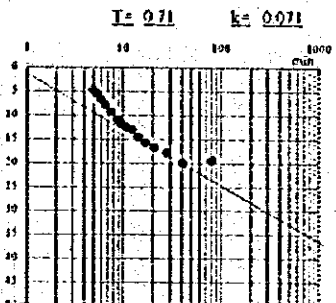
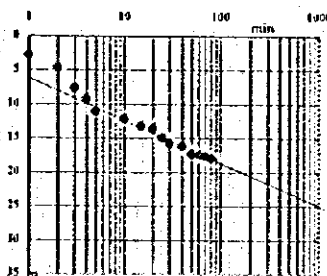
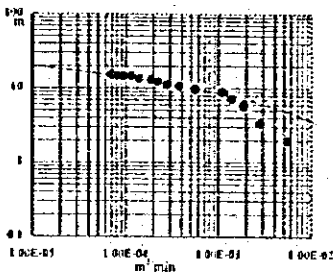
No. MUM03

T= k= S= T= k= S=



No. MB093

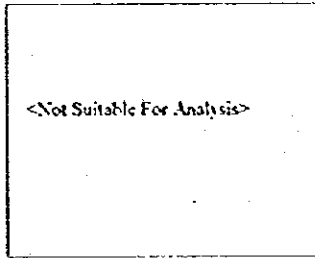
T= 1.36E+00 k= 1.36E-01 S= 1.48E-02 T= 1.32 k= 0.132 S= 0.0382



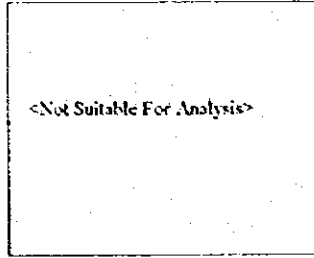
Appendix 2 (27) Result of Pumping Test Analysis

No. MB094

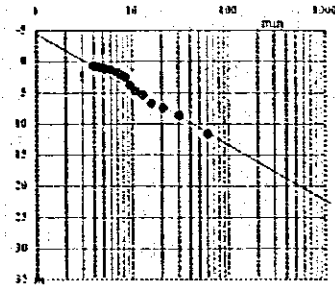
I= k= S=



I= k= S=

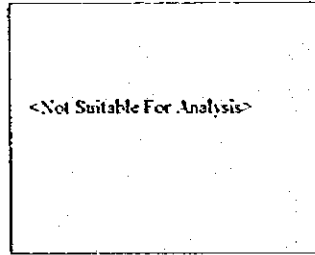


I= 2.65 k= 0.106

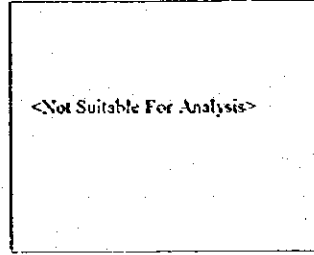


No. MB001

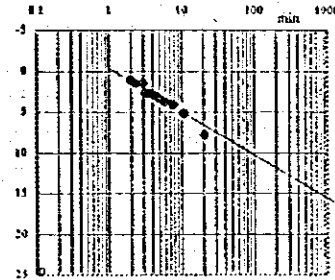
I= k= S=



I= k= S=

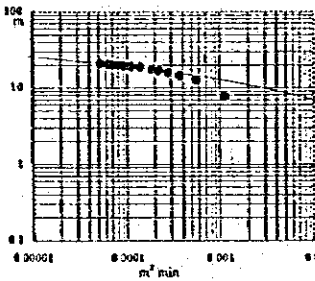


I= 6.91 k= 0.432

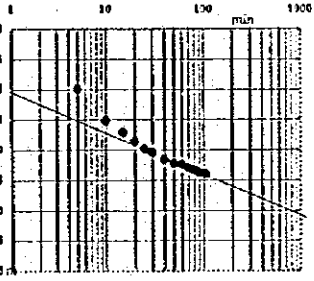


No. 2783

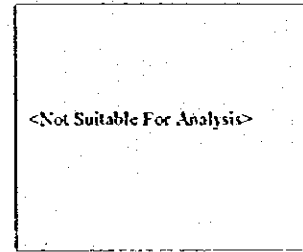
I= 3.69E+00 k= 1.51E-01 S= 2.95E-02



I= 3.73 k= 0.187 S= 0.0299

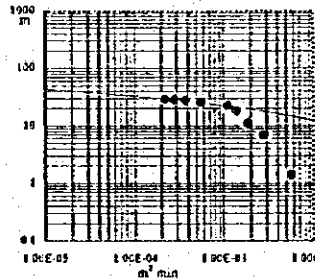


I= k=

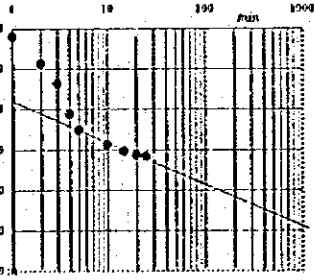


No. 1755

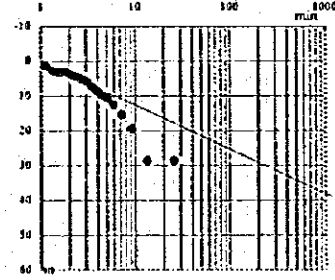
I= 2.95E-01 k= 1.52E-02 S= 1.78E-01



I= 0.306 k= 0.0158 S= 0.00153

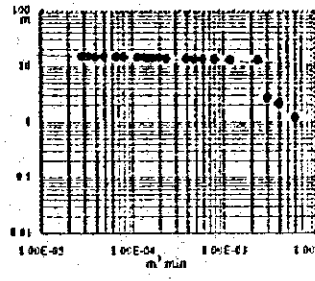


I= 0.243 k= 0.0128

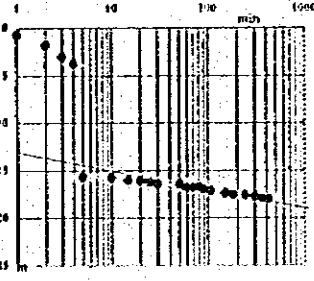


No. 2110

I= 1.88E+01 k= 4.37E-01 S= 3.18E-02



I= 191 k= 0.455 S= 3.88E-02



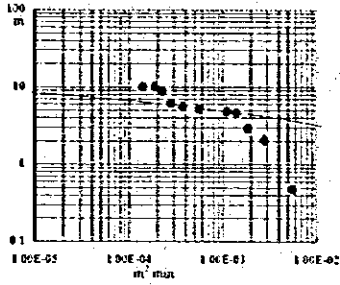
I= k=



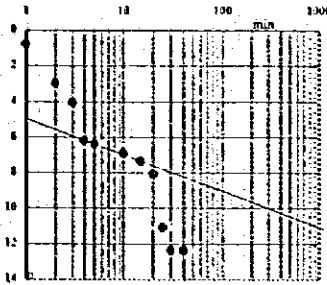
Appendix 2 (28) Result of Pumping Test Analysis

No. KB04

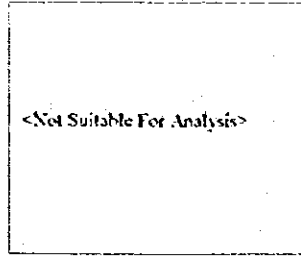
T= 11.3 k= 6.44 S= 0.0116



T= 1.17E+01 k= 6.63 S= 1.16E-02

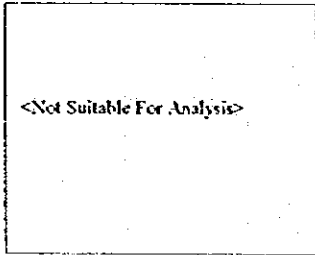


T= k=

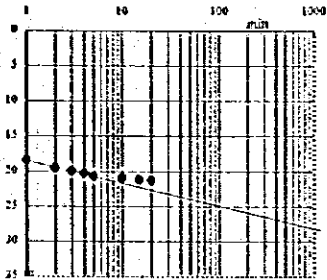


No. 2658.1

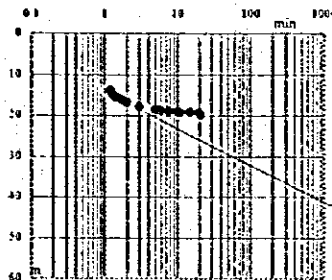
T= k= S=



T= 7.83 k= 1.96 S= 4.13E-06

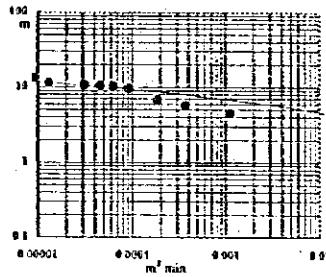


T= 2.8 k= 0.701

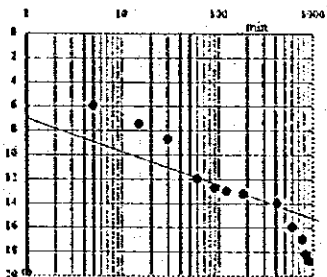


No. LN-13

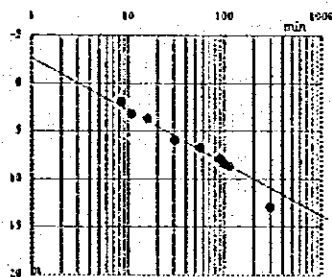
T= 2.88E+00 k= 1.03E-01 S= 2.23E-03



T= 2.87 k= 0.302 S= 0.60233

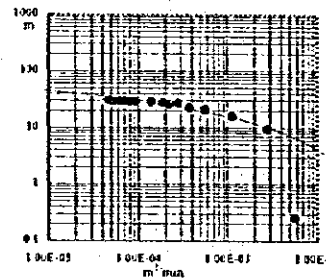


T= 1.41 k= 0.151

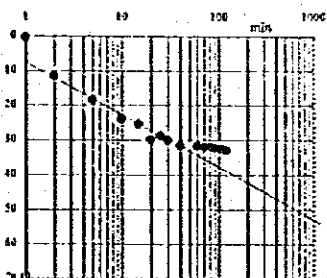


No. 1466

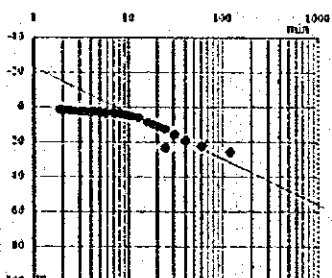
T= 1.94E+00 k= 4.59E-02 S= 1.60E-01



T= 1.82 k= 0.0438 S= 0.163

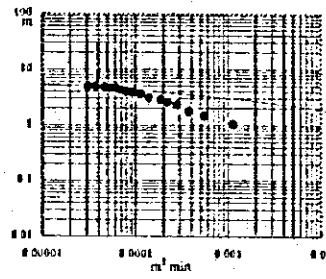


T= 1.03 k= 0.0232

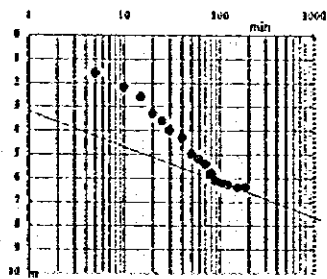


No. 2765

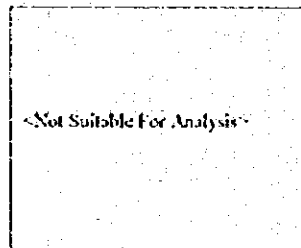
T= 2.79E+01 k= 9.29E+00 S= 5.50E-02



T= 27.6 k= 9.21 S= 0.0555



T= k=



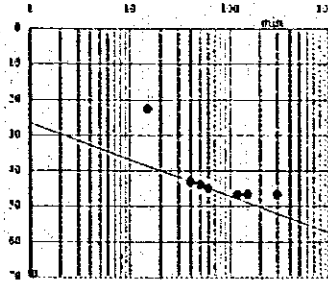
Appendix 2 (29) Result of Pumping Test Analysis

No. 2154

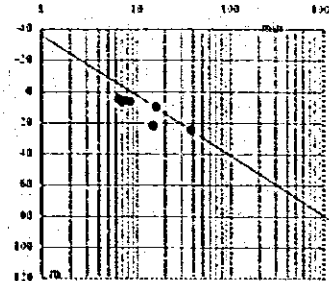
T= **k=** **S=**

<Not Suitable For Analysis>

T= 3.61E-01 **k= 0.0923** **S= 3.33E-04**



T= 0.123 **k= 0.0247**

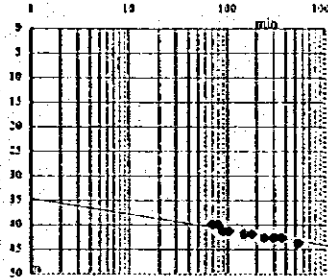


No. 2128

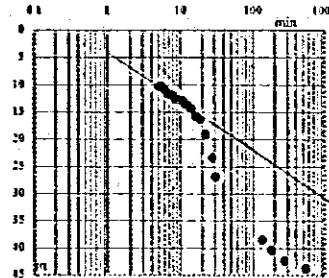
T= **k=** **S=**

<Not Suitable For Analysis>

T= 22.5 **k= 1.61** **S= 6.91E-11**

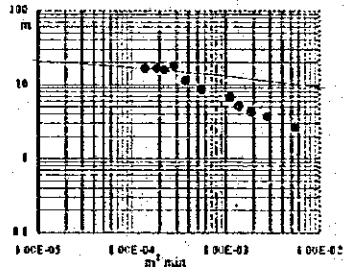


T= 7.96 **k= 0.569**

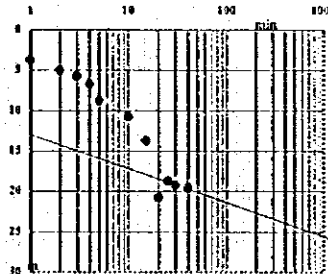


No. 2078

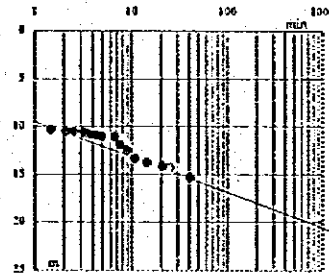
T= 1.43E+01 **k= 1.02E+00** **S= 3.62E-03**



T= 14.3 **k= 1.02** **S= 0.00325**

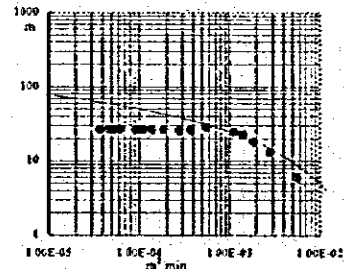


T= 16.2 **k= 1.16**

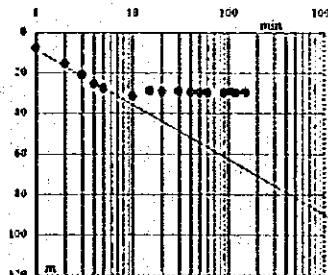


No. 2271

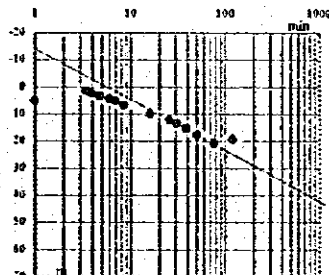
T= 6.10E-01 **k= 2.17E-02** **S= 7.90E-02**



T= 0.531 **k= 0.0206** **S= 0.0793**

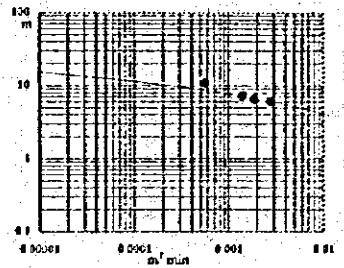


T= 0.831 **k= 0.0599**

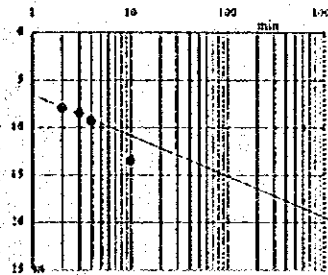


No. 1608MO

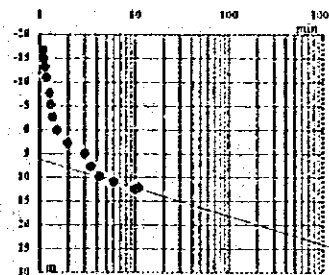
T= 2.19E+00 **k= 2.24E-01** **S= 7.02E-02**



T= 9.22 **k= 0.225** **S= 0.0748**



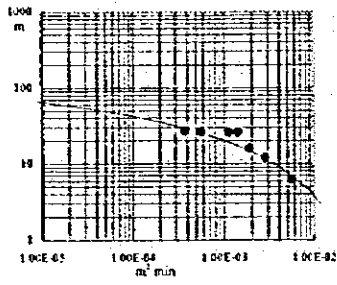
T= 6.66 **k= 0.163**



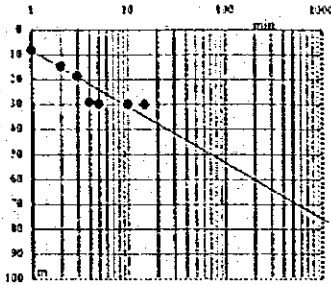
Appendix 2 (30) Result of Pumping Test Analysis

No. 1607M10

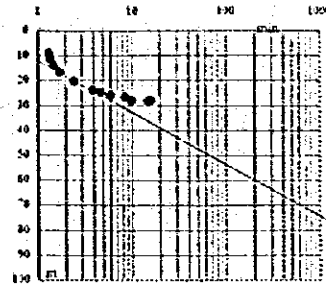
T= 0.14 k= 0.00291 S= 0.0302



T= 1.40E-01 k= 0.00292 S= 1.68E-02

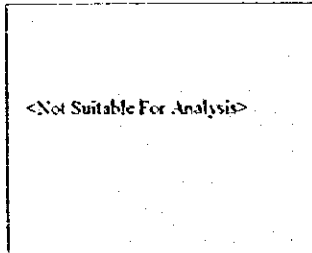


T= 0.152 k= 0.00316

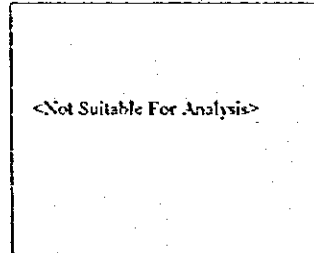


No. 1902

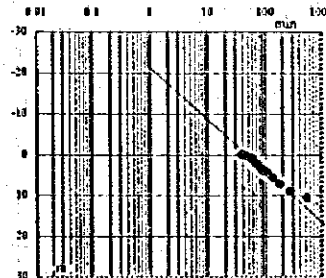
T= k= S=



T= k= S=

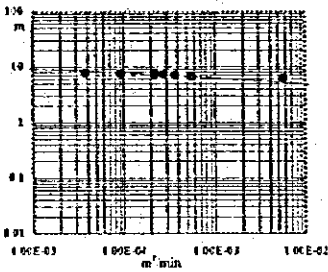


T= 1.12 k= 0.0433

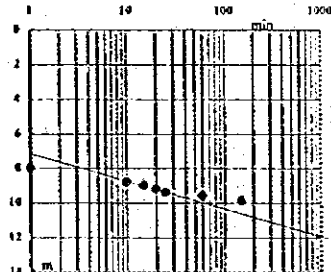


No. 2203

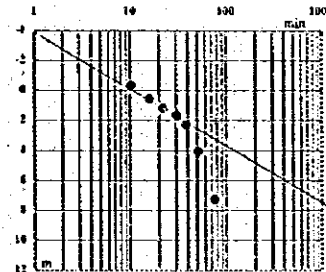
T= 2.32E+01 k= 1.78E+00 S= 4.72E-04



T= 24.7 k= 1.9 S= 0.000242

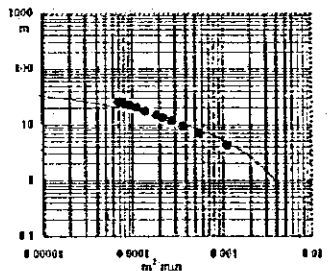


T= 10.4 k= 0.799

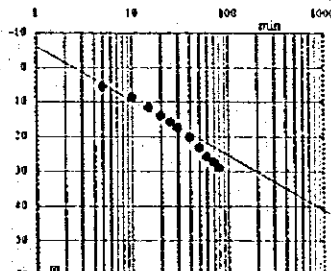


No. 2205

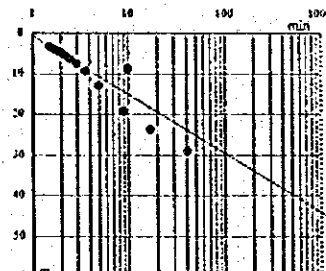
T= 4.37E-01 k= 2.19E-02 S= 2.52E-01



T= 0.426 k= 0.0213 S= 0.246

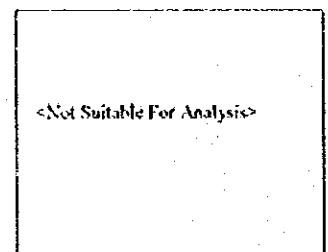


T= 0.419 k= 0.02069

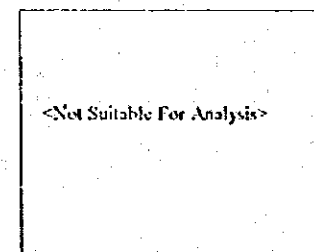


No. 1601

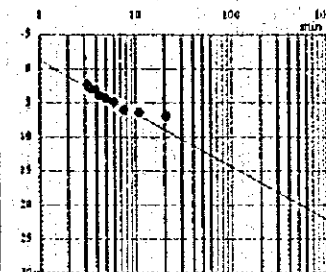
T= k= S=



T= k= S=



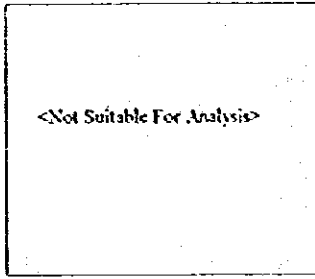
T= 7.24 k= 0.13



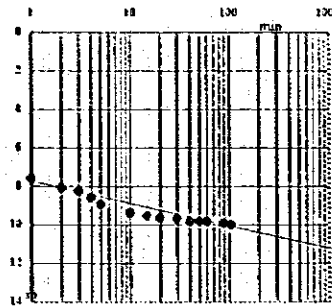
Appendix 2 (31) Result of Pumping Test Analysis

No. 2629C

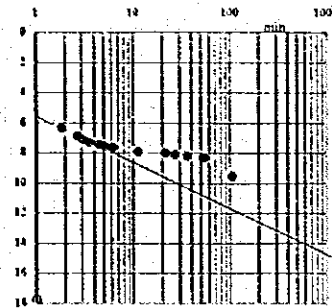
T= k= S=



T= 4.48E+01 k= 1.49 S= 3.51E-06

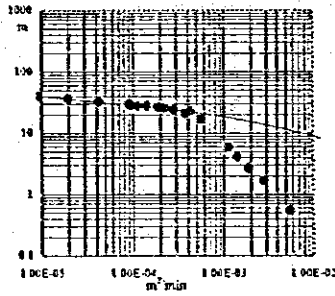


T= 12.1 k= 0.574

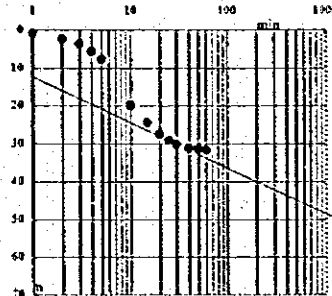


No. 2039

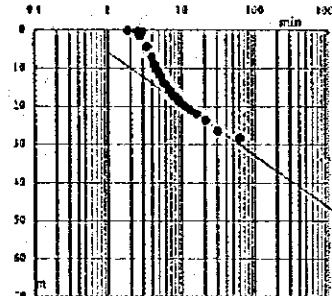
T= 3.11 k= 0.345 S= 0.0435



T= 2.75 k= 0.305 S= 0.0741

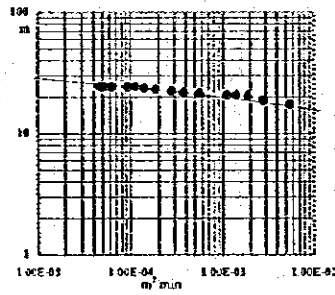


T= 2.45 k= 0.272

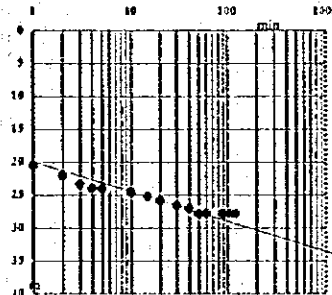


No. 2636

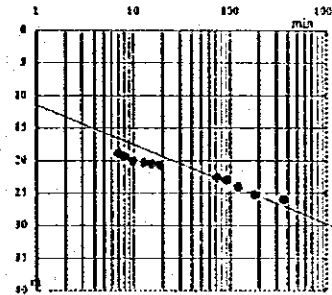
T= 4.55E+00 k= 3.03E-01 S= 5.04E-05



T= 4.53 k= 0.302 S= 0.00005

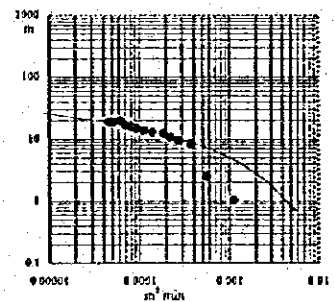


T= 3.35 k= 0.224

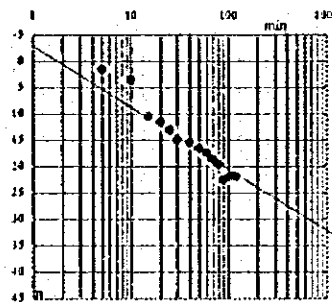


No. 2048

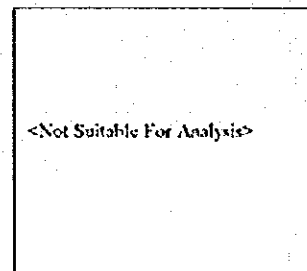
T= 4.03E-01 k= 1.34E-01 S= 1.95E-01



T= 0.406 k= 0.135 S= 0.201

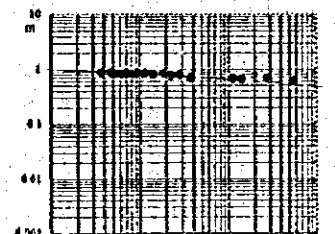


T= k=

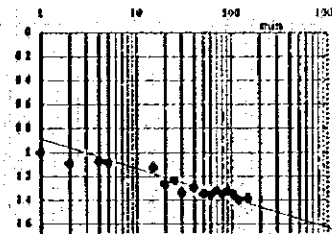


No. 4737

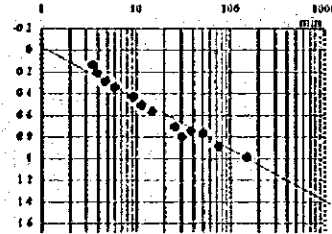
T= 1.34E+02 k= 4.79E+02 S= 1.01E-02



T= 133 k= 477 S= 0.0103



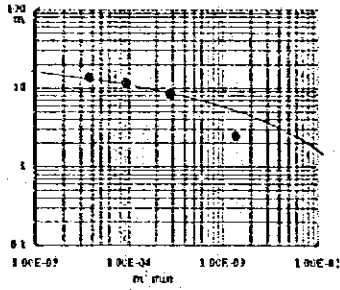
T= 69.2 k= 250



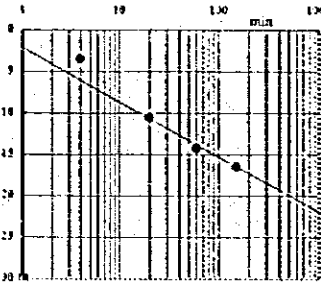
Appendix 2 (32) Result of Pumping Test Analysis

No. 3097

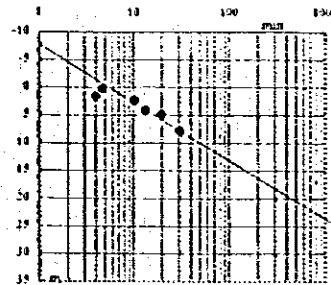
T= 1.76 k= 0.586 S= 0.132



T= 1.56E-00 k= 0.52 S= 2.06E-01



T= 0.984 k= 0.327

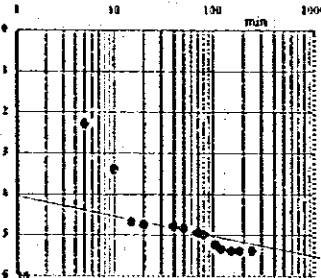


No. 3052

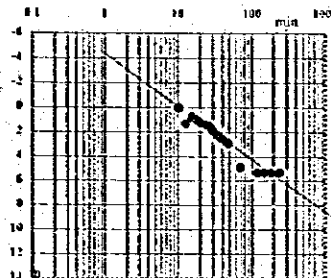
T= k= S=

<Not Suitable For Analysis>

T= 642 k= 5.41 S= 8.87E-08



T= 7.33 k= 0.611



No. 3051

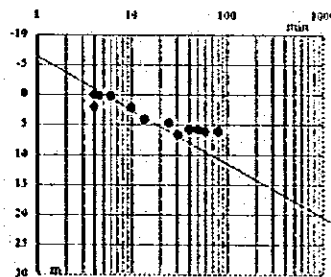
T= k= S=

<Not Suitable For Analysis>

T= k= S=

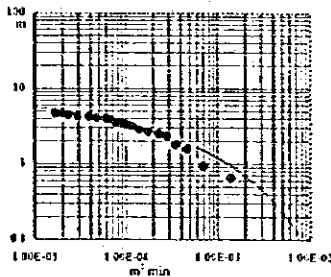
<Not Suitable For Analysis>

T= 1.23 k= 0.457

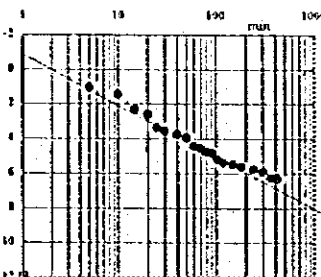


No. 2971

T= 5.32E-01 k= 1.33E-01 S= 2.25E-01



T= 0.531 k= 0.133 S= 0.232



T= k=

<Not Suitable For Analysis>

No. 2162

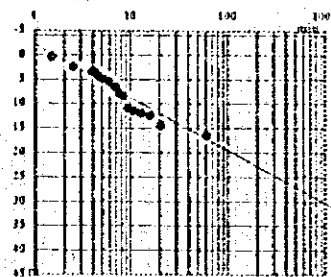
T= k= S=

<Not Suitable For Analysis>

T= k= S=

<Not Suitable For Analysis>

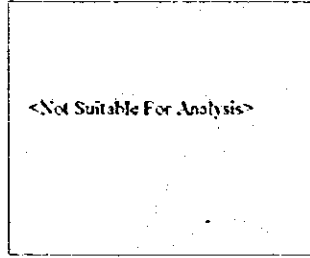
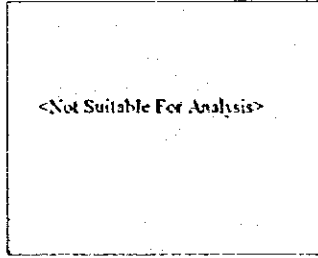
T= 1.17 k= 0.0493



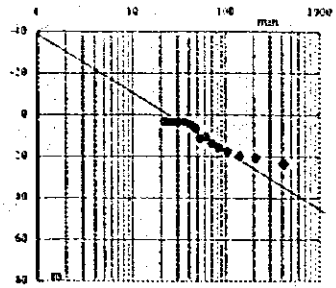
Appendix 2 (33) Result of Pumping Test Analysis

No. 1934

$T=$ $k=$ $S=$ $T=$ $k=$ $S=$

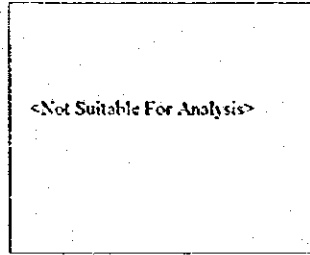
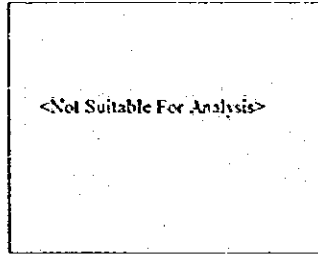


$T= 113$ $k= 0.0451$

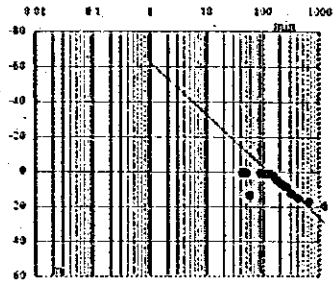


No. 1964

$T=$ $k=$ $S=$ $T=$ $k=$ $S=$

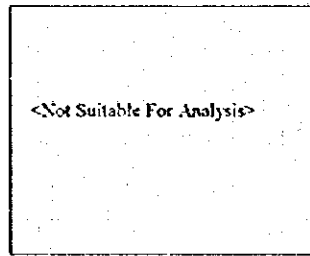
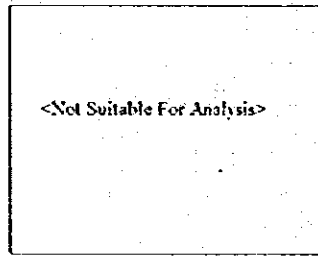


$T= 1.76$ $k= 0.041$

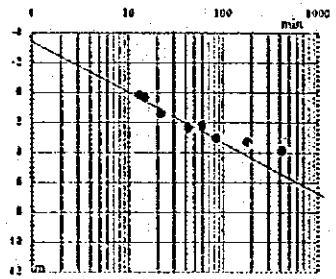


No. 1268

$T=$ $k=$ $S=$ $T=$ $k=$ $S=$

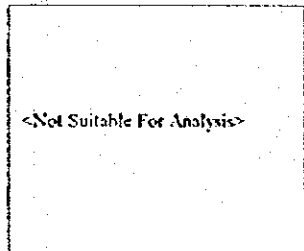
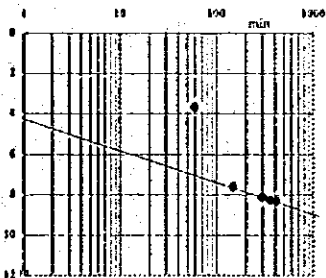
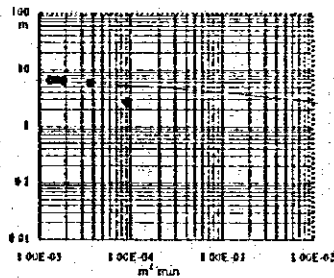


$T= 4.89$ $k= 0.168$



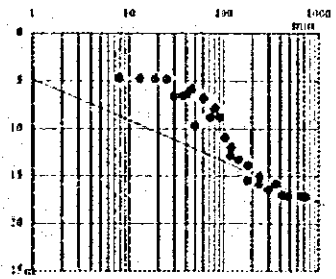
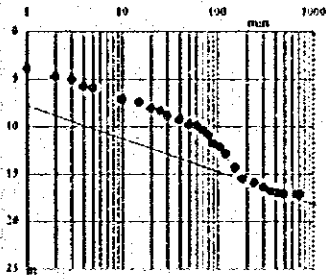
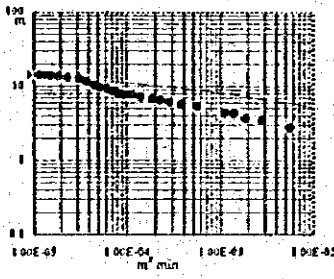
No. 1385

$T= 2.92E+02$ $k= 8.33E-01$ $S= 5.59E-01$ $T= 10$ $k= 0.537$ $S= 0.00556$ $T=$ $k=$



No. 2263

$T= 1.14E+02$ $k= 8.79E+00$ $S= 1.79E-01$ $T= 114$ $k= 8.78$ $S= 0.14$ $T= 91.7$ $k= 7.66$



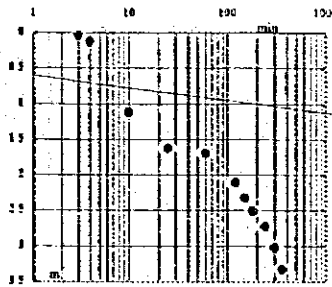
Appendix 2 (34) Result of Pumping Test Analysis

No. MAK15

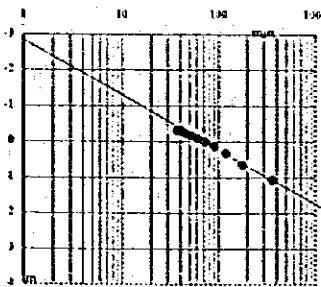
T= k= S=

<Not Suitable For Analysis>

T= 3.79E+02 k= 94.9 S= 3.93E-02



T= 43.4 k= 10.8



No. 2015

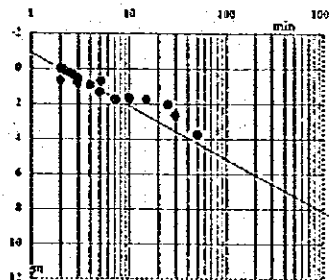
T= k= S=

<Not Suitable For Analysis>

T= k= S=

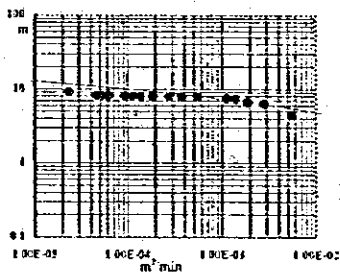
<Not Suitable For Analysis>

T= 26.1 k= 13

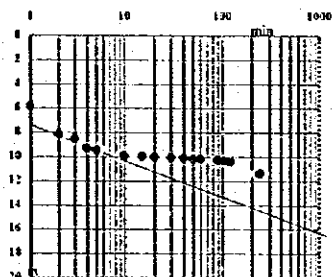


No. 2610A

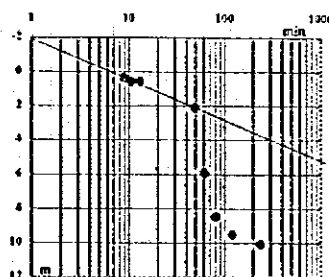
T= 1.99E+01 k= 2.38E-00 S= 1.86E-02



T= 19.2 k= 2.4 S= 0.0122

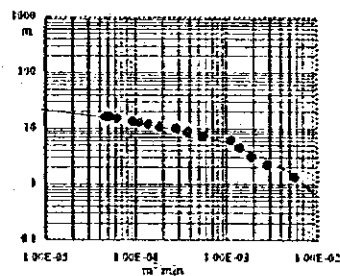


T= 23.9 k= 2.99

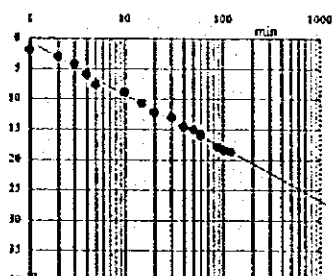


No. 2611A

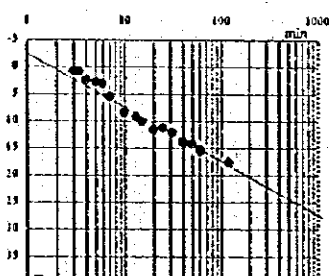
T= 7.28E-01 k= 1.37E-02 S= 1.76E-01



T= 0.726 k= 0.0137 S= 0.171



T= 0.639 k= 0.0121



No. 1710

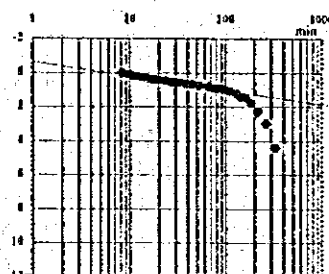
T= k= S=

<Not Suitable For Analysis>

T= k= S=

<Not Suitable For Analysis>

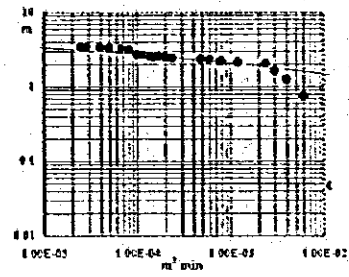
T= 24.0 k= 71.0



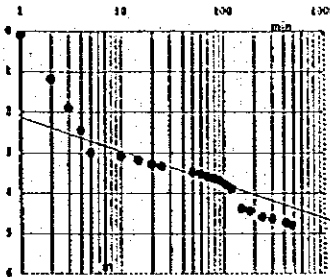
Appendix 2 (35) Result of Pumping Test Analysis

No. 1311

$T = 47.5$ $k = 1.64$ $S = 0.0159$



$T = 4.77E+01$ $k = 1.65$ $S = 1.63E-02$

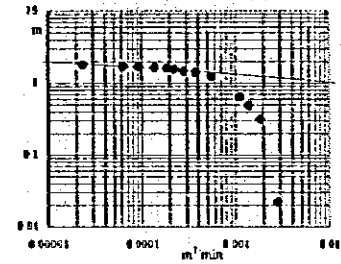


$T =$ $k =$

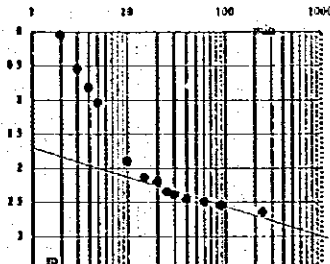
<Not Suitable For Analysis>

No. 1720

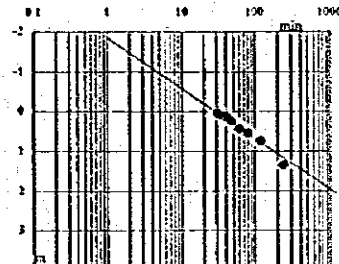
$T = 73$ $k = 2.52$ $S = 0.00216$



$T = 72.7$ $k = 2.51$ $S = 0.00256$



$T = 75$ $k = 0.852$



No. 1842

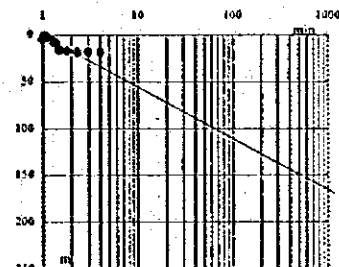
$T =$ $k =$ $S =$

<Not Suitable For Analysis>

$T =$ $k =$ $S =$

<Not Suitable For Analysis>

$T = 0.115$ $k = 0.023$



No. 1843

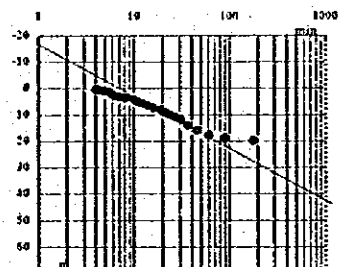
$T =$ $k =$ $S =$

<Not Suitable For Analysis>

$T =$ $k =$ $S =$

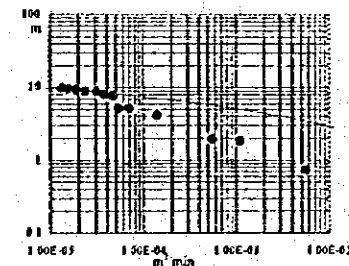
<Not Suitable For Analysis>

$T = 0.762$ $k = 0.0401$

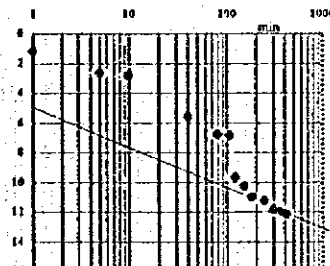


No. 1613

$T = 3.84E+01$ $k = 6.62E-01$ $S = 1.76E-01$



$T = 38.1$ $k = 0.661$ $S = 0.163$



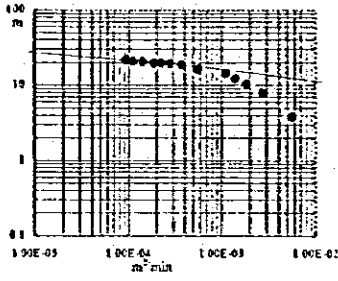
$T =$ $k =$

<Not Suitable For Analysis>

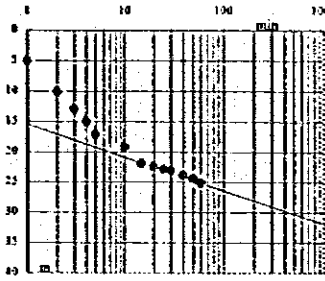
Appendix 2 (36) Result of Pumping Test Analysis

No. 2013

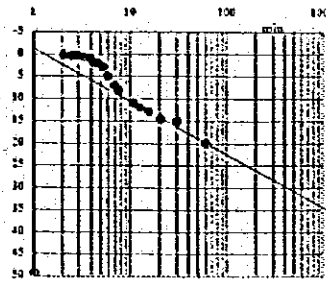
T= 8.02 k= 0.229 S= 0.00268



T= 818E+00 k= 0.234 S= 2.19E-03

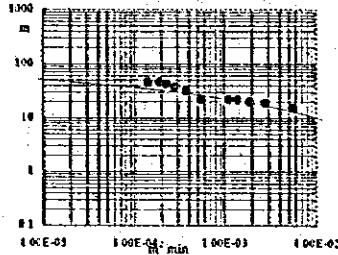


T= 3.99 k= 0.114

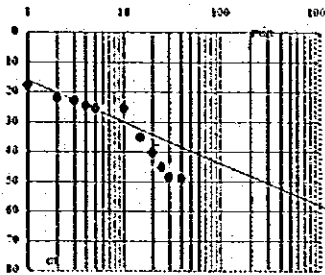


No. 1742

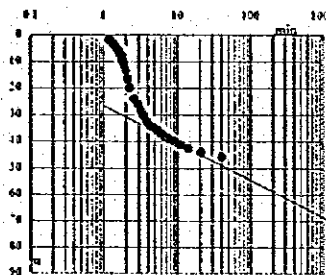
T= 1.13 k= 0.564 S= 0.0229



T= 1.13 k= 0.567 S= 0.022

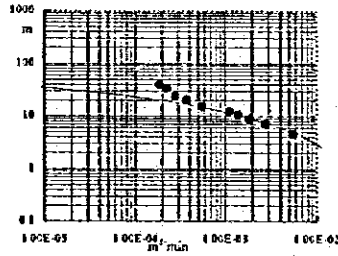


T= 1.13 k= 0.564

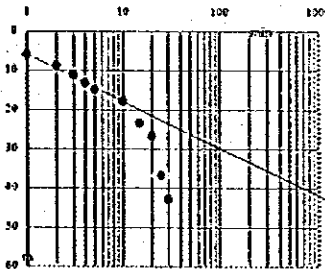


No. 1647

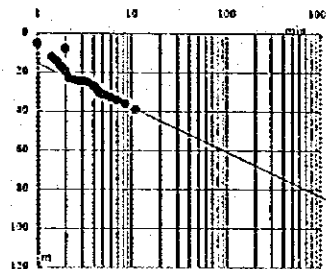
T= 619E-01 k= 1.10E-02 S= 5.79E-02



T= 0.62 k= 0.031 S= 0.0553

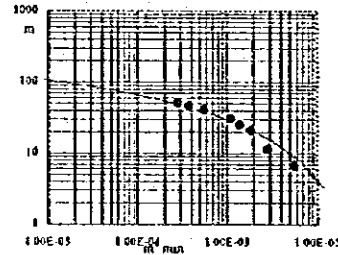


T= 0.327 k= 0.0163

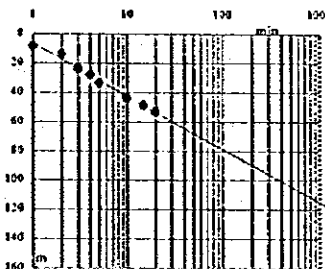


No. 1762

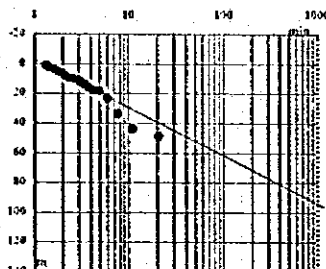
T= 1.28E-01 k= 8.39E-03 S= 4.36E-02



T= 0.227 k= 0.00829 S= 0.0411



T= 0.255 k= 0.0093



No. K803

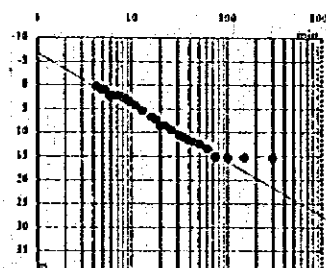
T= k= S=

<Not Suitable For Analysis>

T= k= S=

<Not Suitable For Analysis>

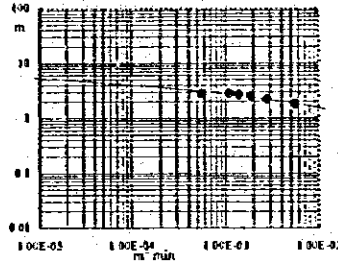
T= 8.29 k= 31.9



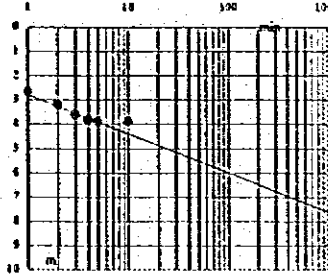
Appendix 2 (37) Result of Pumping Test Analysis

No. 2633-1

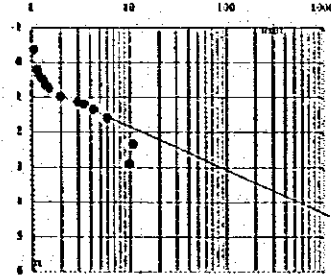
$T = 31.6$ $k = 31.4$ $S = 0.19$



$T = 3.45E+01$ $k = 31.4$ $S = 1.74E-01$

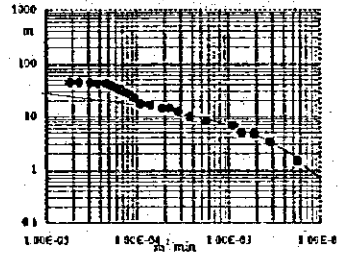


$T = 41.4$ $k = 4.04$

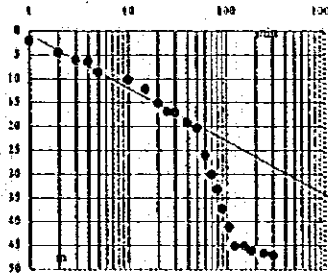


No. 2294

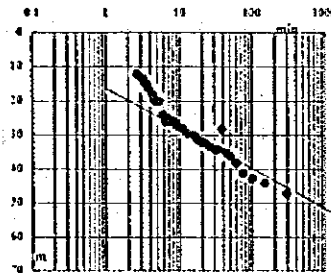
$T = 0.394$ $k = 0.131$ $S = 0.109$



$T = 0.397$ $k = 0.132$ $S = 0.095$

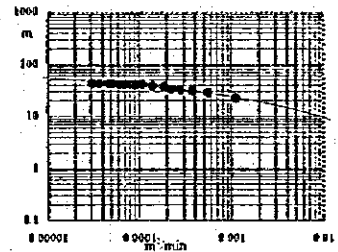


$T = 0.377$ $k = 0.126$

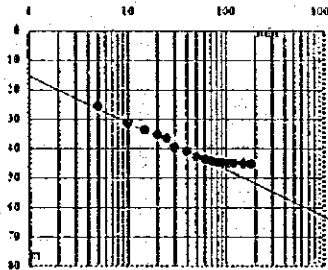


No. 2749

$T = 2.01E+00$ $k = 2.23E-01$ $S = 5.93E-02$



$T = 1.92$ $k = 0.221$ $S = 0.0603$



$T =$ $k =$

<Not Suitable For Analysis>

No. 1621

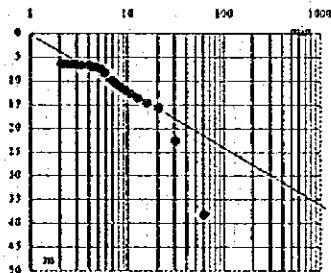
$T =$ $k =$ $S =$

<Not Suitable For Analysis>

$T =$ $k =$ $S =$

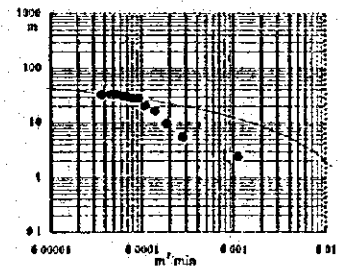
<Not Suitable For Analysis>

$T = 3.44$ $k = 1.32$

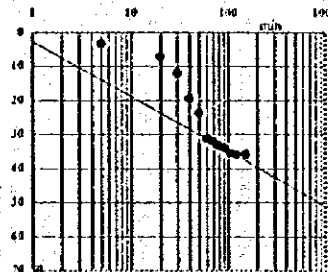


No. 2867

$T = 1.73E-01$ $k = 4.04E-02$ $S = 1.50E-01$



$T = 0.855$ $k = 0.0396$ $S = 0.152$



$T =$ $k =$

<Not Suitable For Analysis>

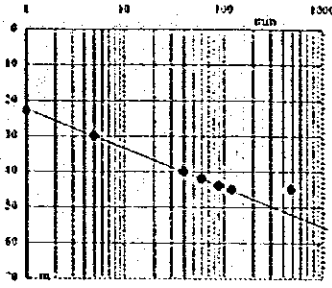
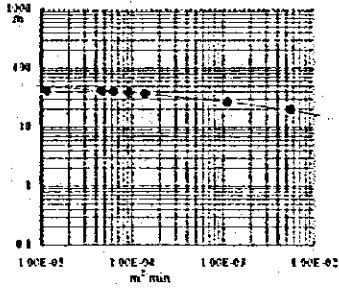
Appendix 2 (38) Result of Pumping Test Analysis

No. KSM108

T= 3.55 k= 0.297 S= 0.00929

T= 3.55E+00 k= 0.295 S= 9.26E-03

T= k=



<Not Suitable For Analysis>

No. 1691

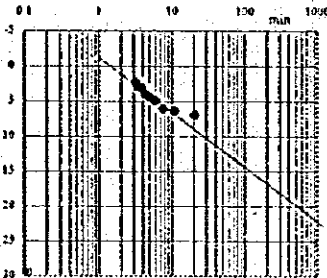
T= k= S=

T= k= S=

T= 7.24 k= 0.13

<Not Suitable For Analysis>

<Not Suitable For Analysis>

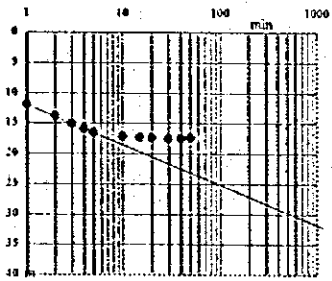
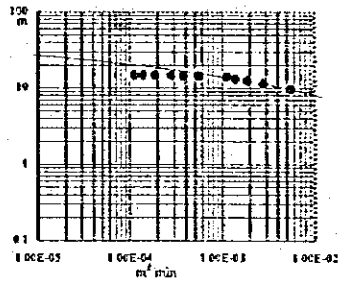


No. 2169

T= 2.85E+01 k= 2.31E+00 S= 1.23E-01

T= 28.7 k= 2.36 S= 0.123

T= k=



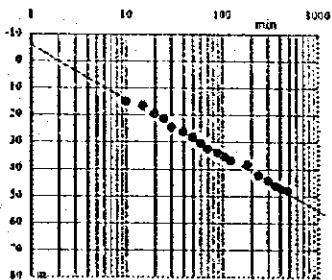
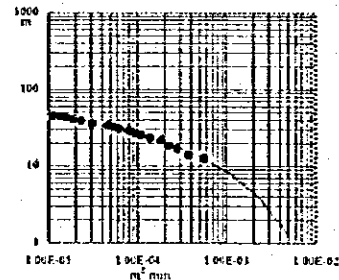
<Not Suitable For Analysis>

No. 1916-1

T= 1.07E-01 k= 4.45E-02 S= 1.72E-01

T= 0.368 k= 0.0447 S= 0.173

T= k=



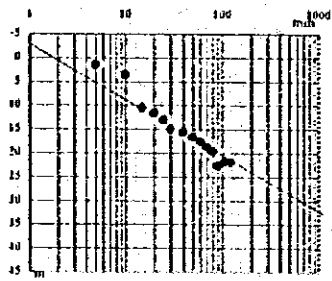
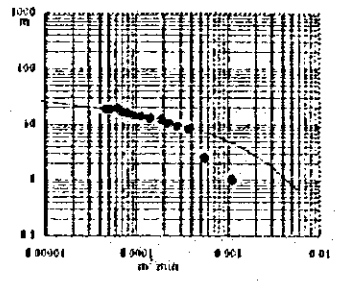
<Not Suitable For Analysis>

No. 2044-1

T= 4.03E-01 k= 1.34E-01 S= 1.96E-01

T= 0.406 k= 0.135 S= 0.201

T= k=

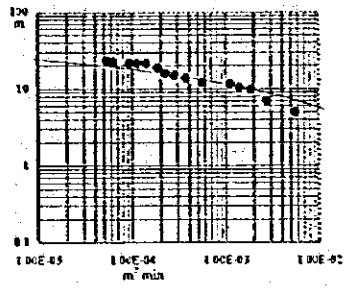


<Not Suitable For Analysis>

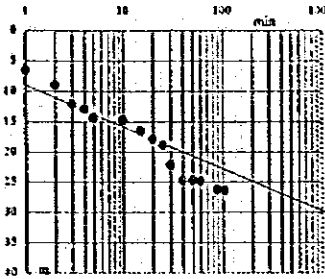
Appendix 2 (39) Result of Pumping Test Analysis

No. 2613A

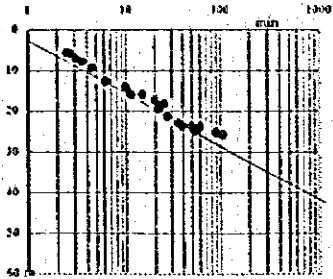
$T = 2.3$ $k = 0.056$ $S = 0.0293$



$T = 2.30E+00$ $k = 0.0561$ $S = 3.08E-02$

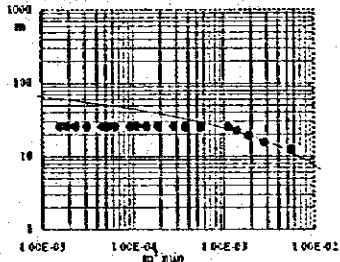


$T = 1.21$ $k = 0.0293$

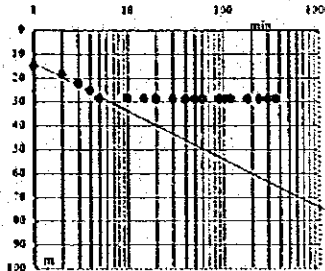


No. 2665B

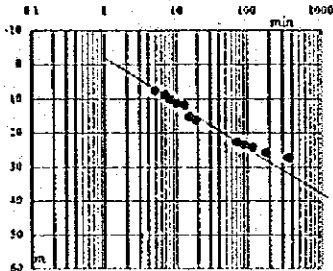
$T = 0.314$ $k = 0.157$ $S = 0.0196$



$T = 0.314$ $k = 0.157$ $S = 0.0182$

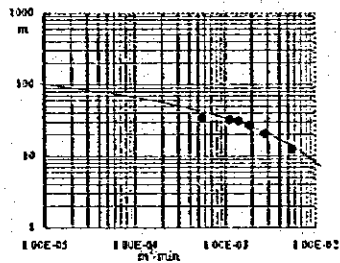


$T = 0.474$ $k = 0.237$

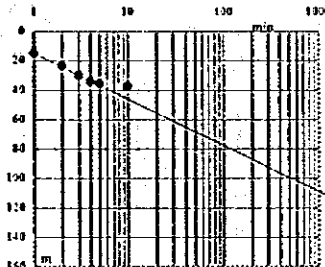


No. 1610

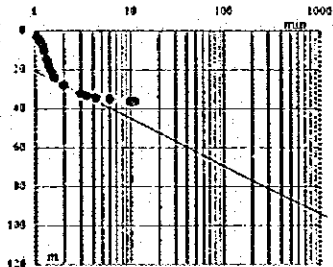
$T = 3.02E-01$ $k = 9.45E-03$ $S = 2.96E-02$



$T = 0.304$ $k = 0.00942$ $S = 0.0272$

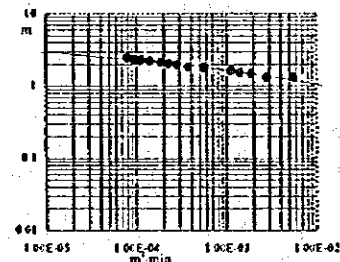


$T = 0.388$ $k = 0.0121$

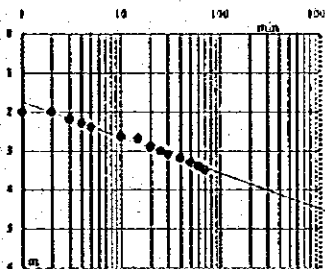


No. 3086

$T = 2.07E+01$ $k = 8.63E-01$ $S = 3.55E-02$



$T = 12$ $k = 0.792$ $S = 0.0662$

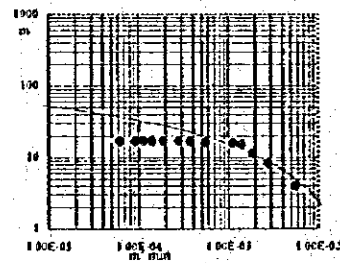


$T =$ $k =$

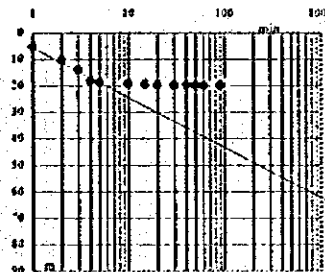
<Not Suitable For Analysis>

No. 226A

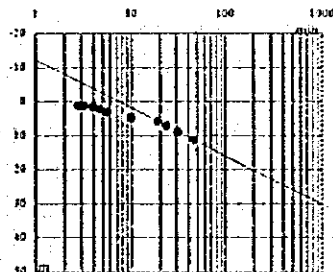
$T = 1.18E+00$ $k = 3.93E-01$ $S = 1.96E-01$



$T = 1.12$ $k = 0.391$ $S = 0.164$



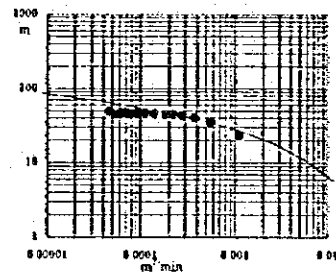
$T = 1.52$ $k = 0.523$



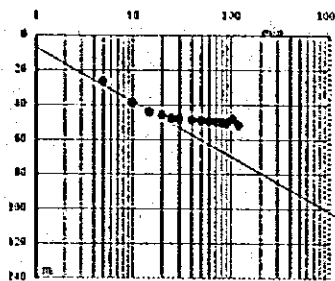
Appendix 2 (40) Result of Pumping Test Analysis

No. 2691

T= 0.352 k= 0.0235 S= 0.0367



T= 3.01E-01 k= 0.02 S= 5.15E-02

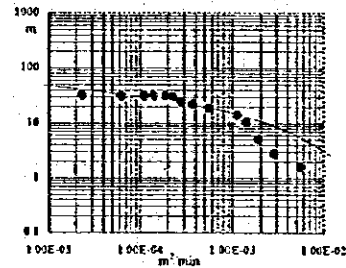


T= k=

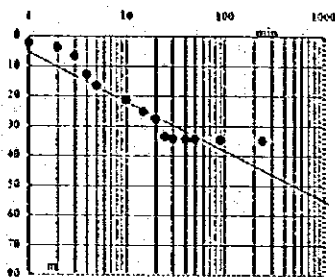
<Not Suitable For Analysis>

No. 2522-1

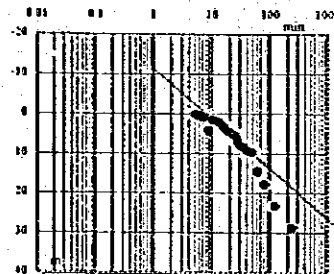
T= 1.12 k= 0.0197 S= 0.141



T= 1.12 k= 0.0197 S= 0.147

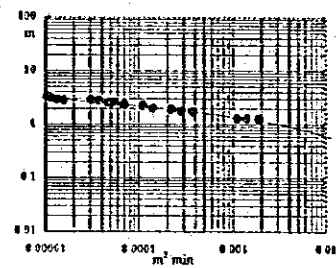


T= 1.37 k= 0.0259

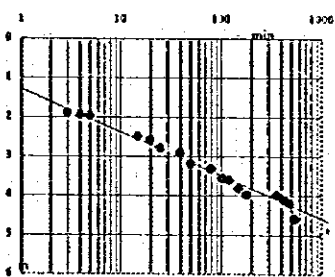


No. 2074

T= 3.13E+00 k= 1.56E+00 S= 6.07E-02



T= 3.13 k= 1.56 S= 0.0606



<Not Suitable For Analysis>

No. 2023

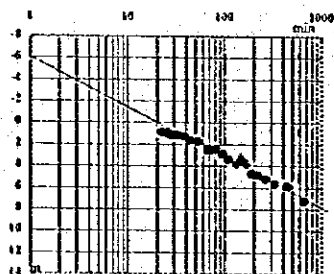
T= k= S=

<Not Suitable For Analysis>

T= k= S=

<Not Suitable For Analysis>

T= 4.26 k= 0.425



No. 1933

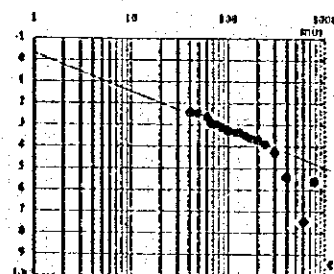
T= k= S=

<Not Suitable For Analysis>

T= k= S=

<Not Suitable For Analysis>

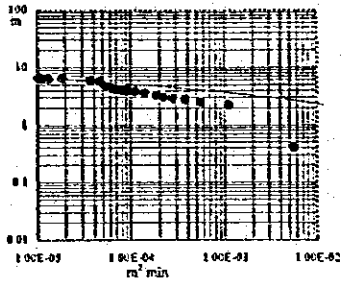
T= 15.6 k= 1.96



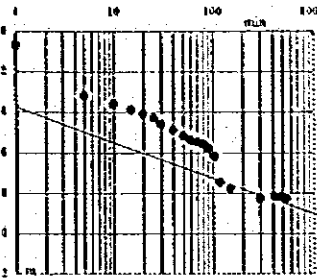
Appendix 2 (41) Result of Pumping Test Analysis

No. 1754

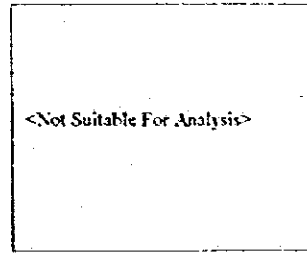
$T = 31.1$ $k = 1.6$ $S = 0.0614$



$T = 3.13E+01$ $k = 1.62$ $S = 6.41E-02$

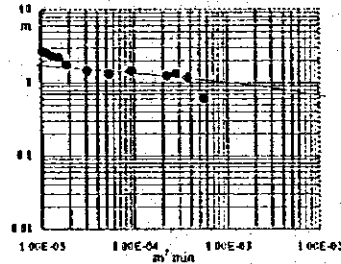


$T =$ $k =$

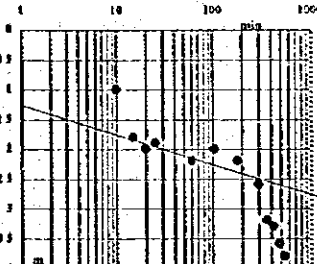


No. 1789

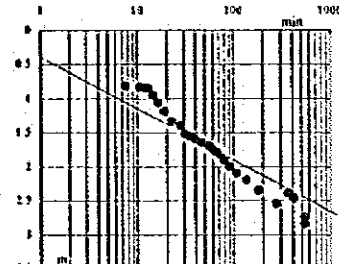
$T = 97.4$ $k = 4.24$ $S = 0.0793$



$T = 94.9$ $k = 4.12$ $S = 0.0796$

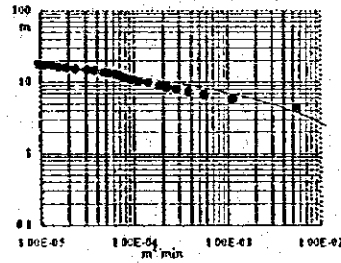


$T = 62.6$ $k = 2.22$

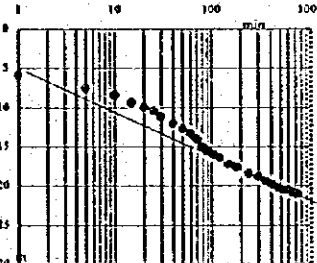


No. 1878

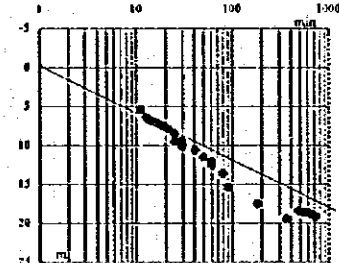
$T = 4.36E+00$ $k = 7.26E-01$ $S = 1.55E-01$



$T = 4.35$ $k = 0.725$ $S = 0.156$

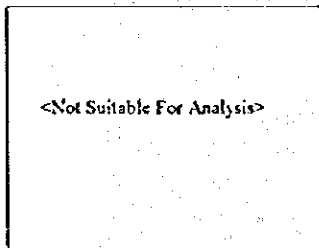


$T = 4.04$ $k = 0.674$

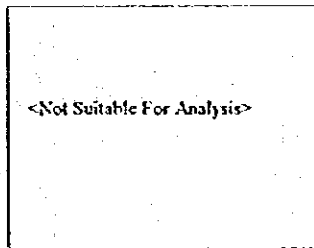


No. 1892

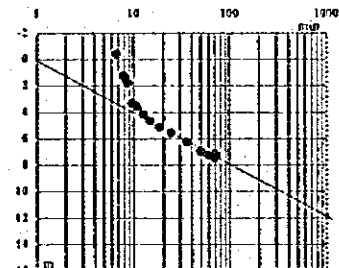
$T =$ $k =$ $S =$



$T =$ $k =$ $S =$

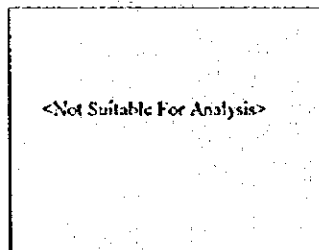


$T = 2.45$ $k = 0.933$

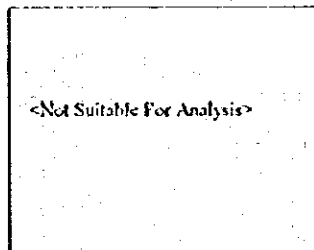


No. 1791

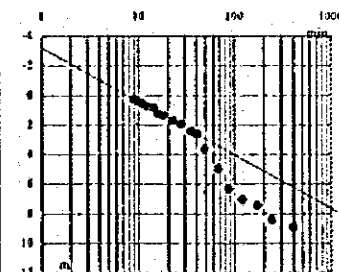
$T =$ $k =$ $S =$



$T =$ $k =$ $S =$



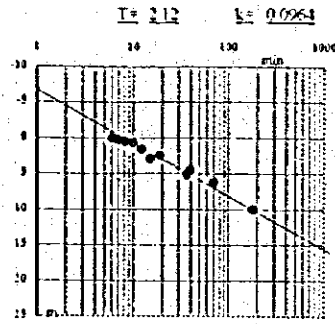
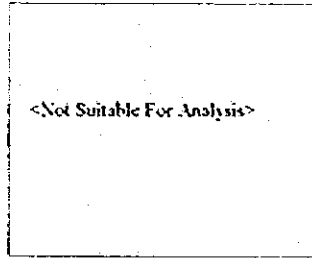
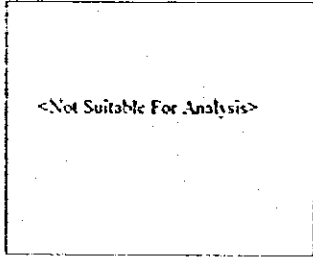
$T = 13.5$ $k = 45.1$



Appendix 2 (42) Result of Pumping Test Analysis

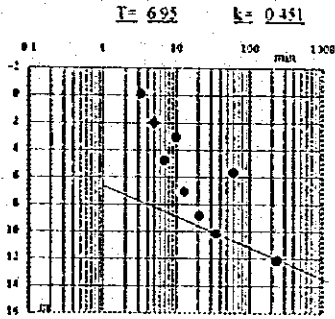
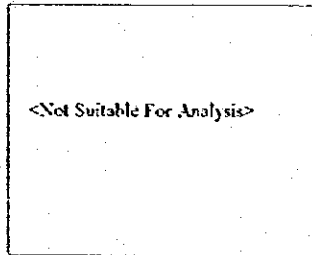
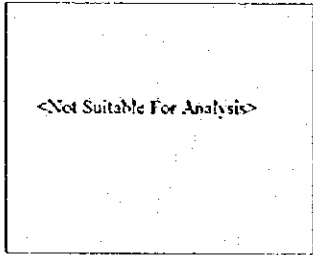
No. 2830

T= k= S= T= k= S=



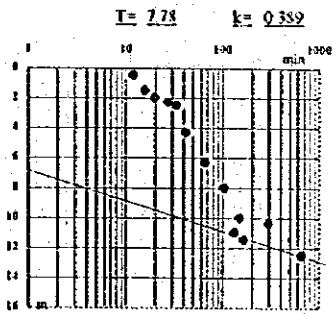
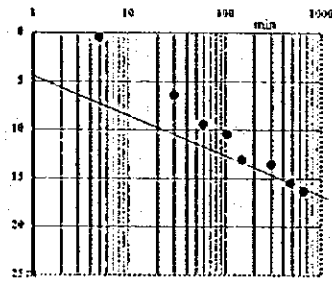
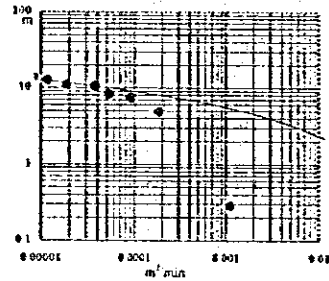
No. 2769

T= k= S= T= k= S=



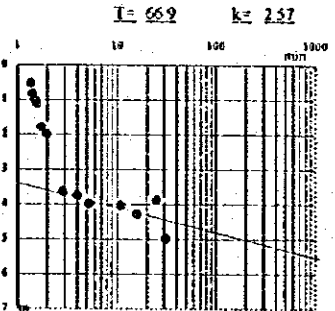
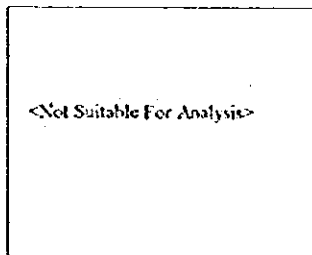
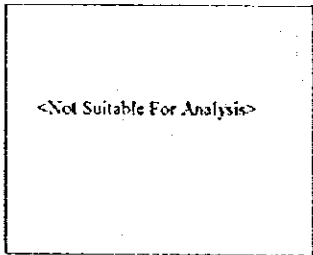
No. 2833

T= 3.85E+00 k= 1.93E-01 S= 9.45E-02 T= 3.84 k= 0.192 S= 0.0902



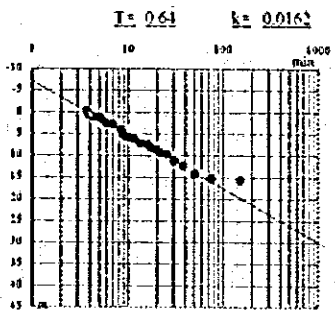
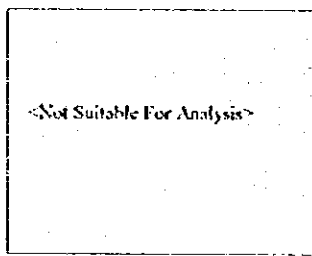
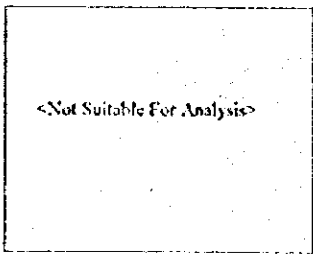
No. 2739

T= k= S= T= k= S=



No. 2734

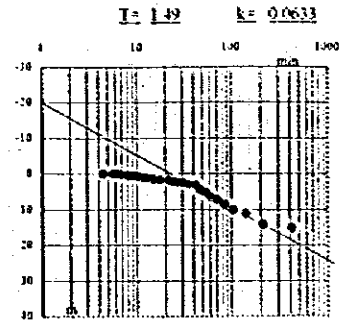
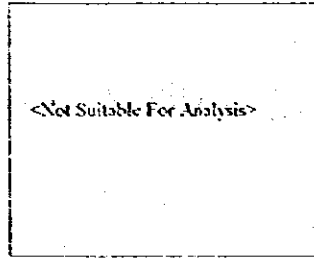
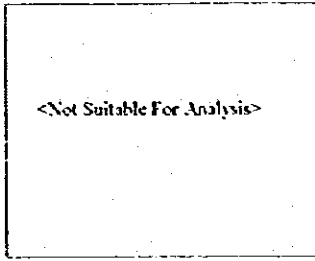
T= k= S= T= k= S=



Appendix 2 (43) Result of Pumping Test Analysis

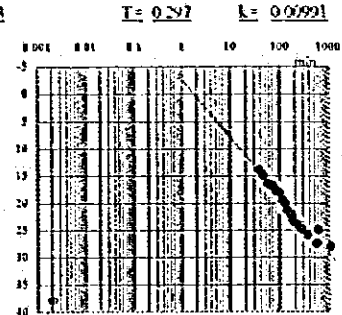
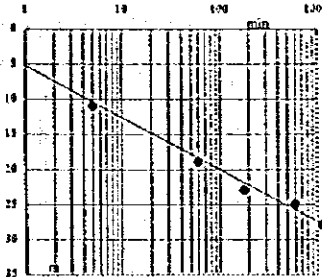
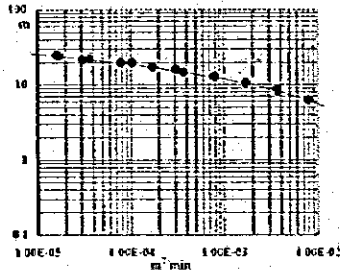
No. 2308

I= k= S= I= k= S=



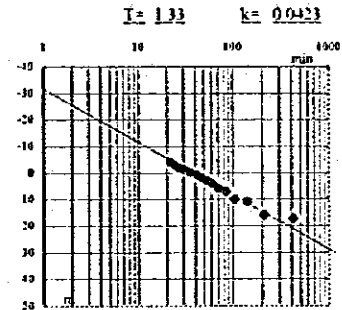
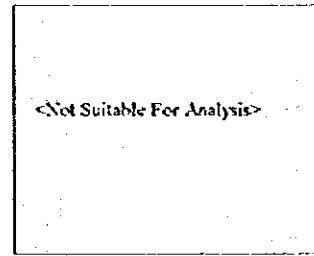
No. 2307

I= 0.428 k= 0.0143 S= 0.0069 I= 0.427 k= 0.0142 S= 0.00723



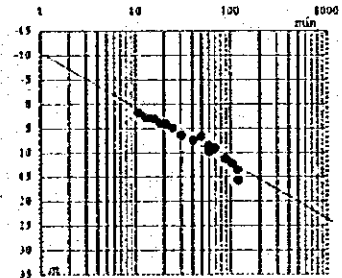
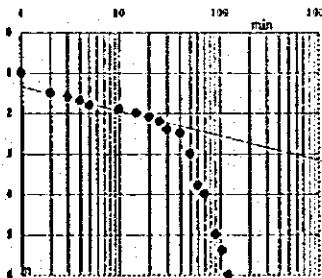
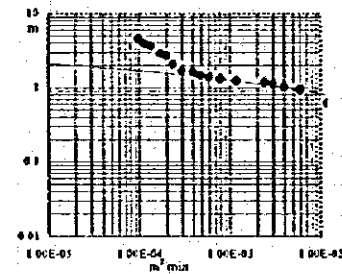
No. 2263

I= k= S= I= k= S=



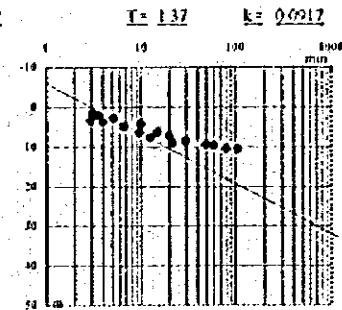
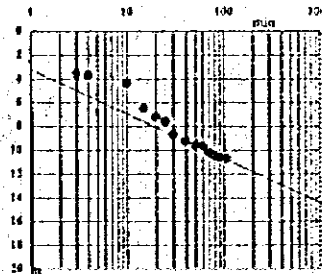
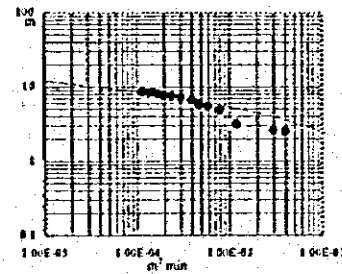
No. 2246

I= 6.9E+01 k= 2.33E+02 S= 5.90E-02 I= 67.6 k= 5.2 S= 0.6573



No. 2309

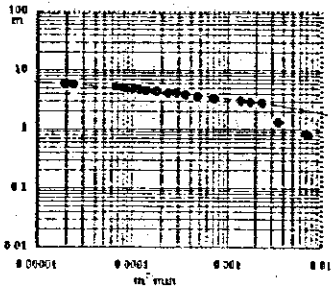
I= 4.6E+00 k= 3.0E-01 S= 1.46E-02 I= 4.61 k= 0.309 S= 0.0817



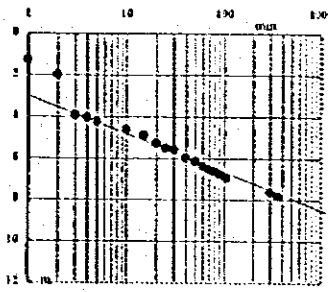
Appendix 2 (44) Result of Pumping Test Analysis

No. 2161

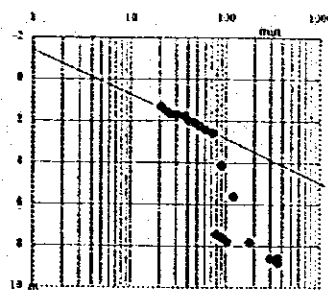
T= 241 k= 0.985 S= 0.11



T= 2.42E+01 k= 0.987 S= 1.25E-01



T= 209 k= 0.852



No. 2139

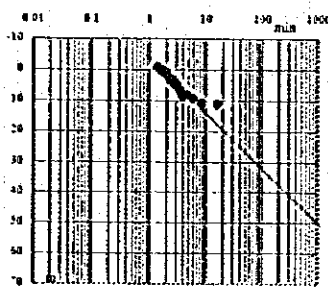
T= k= S=

<Not Suitable For Analysis>

T= k= S=

<Not Suitable For Analysis>

T= 0.977 k= 0.0385



No. 3131

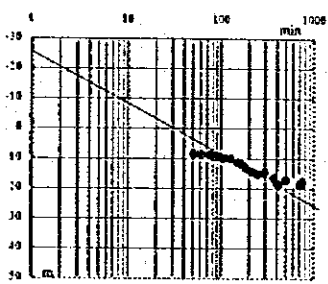
T= k= S=

<Not Suitable For Analysis>

T= k= S=

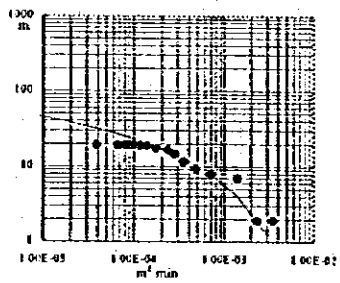
<Not Suitable For Analysis>

T= 1.84 k= 0.92

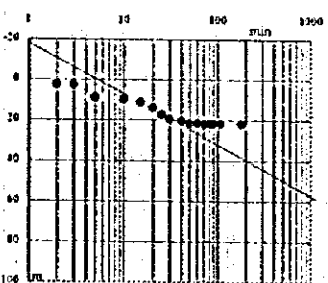


No. 2949

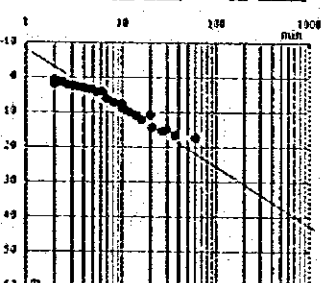
T= 2.86E-01 k= 2.95E-02 S= 2.80E-01



T= 0.251 k= 0.0258 S= 0.288

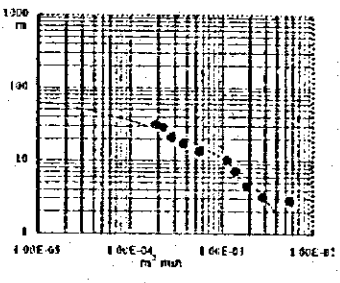


T= 0.375 k= 0.0386

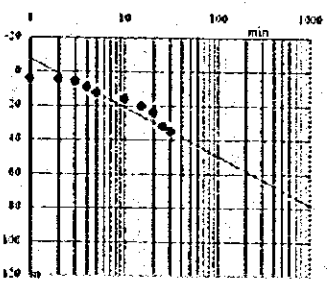


No. 1859

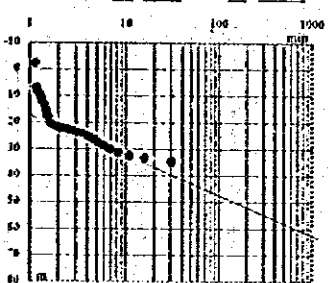
T= 1.98E-01 k= 8.63E-03 S= 1.34E-01



T= 0.128 k= 0.0086 S= 0.101



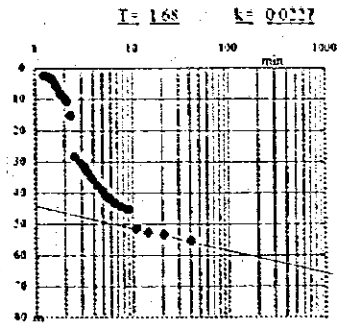
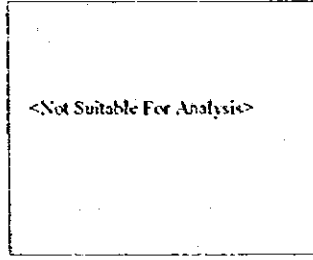
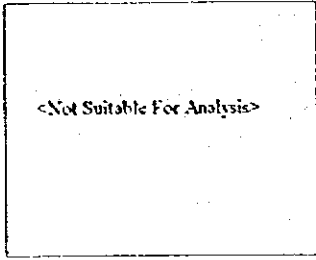
T= 0.377 k= 0.0164



Appendix 2 (45) Result of Pumping Test Analysis

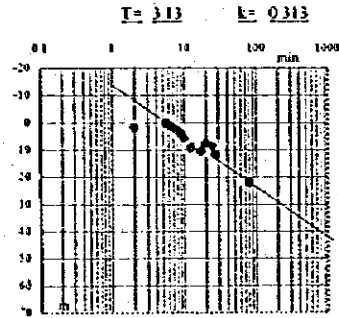
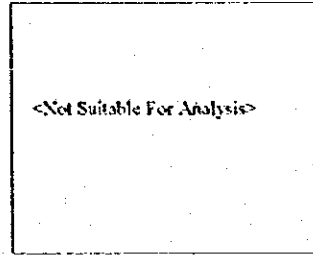
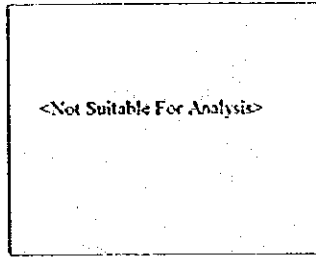
No. 1793

T= k= S= T= k= S=



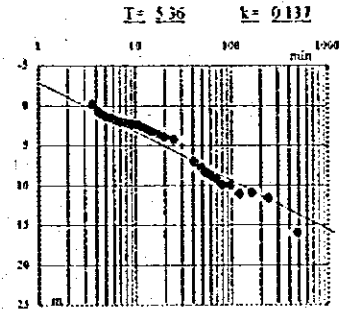
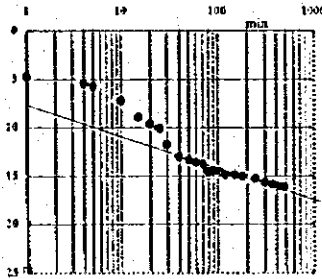
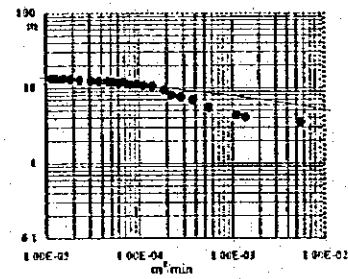
No. 1794

T= k= S= T= k= S=



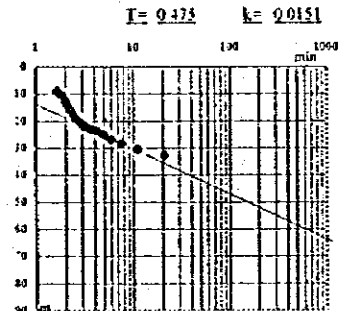
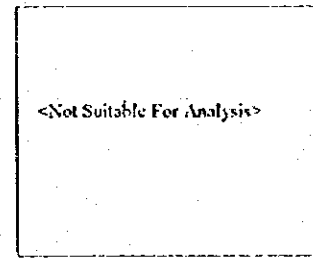
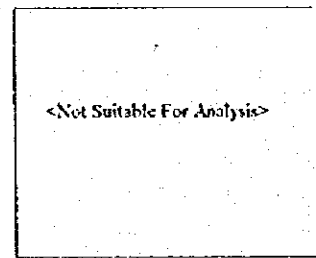
No. 1823

T= 1.01E+01 k= 2.59E-01 S= 1.27E-02 T= 10.3 k= 0.262 S= 0.0122



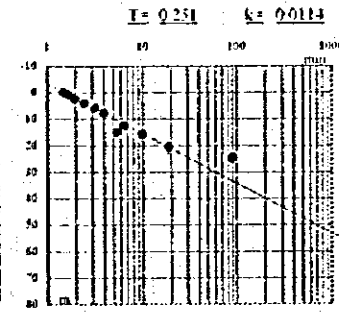
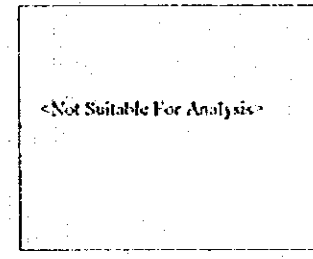
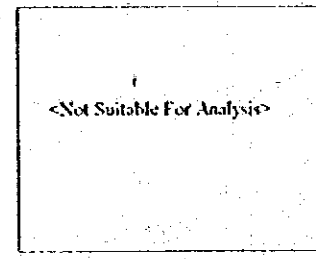
No. 1490

T= k= S= T= k= S=



No. 1477

T= k= S= T= k= S=



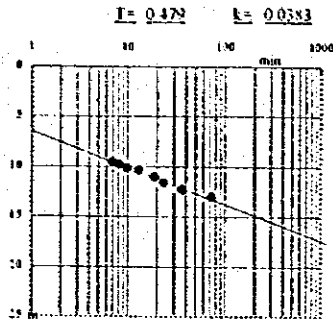
Appendix 2 (46) Result of Pumping Test Analysis

No. 1456

I= k= S= I= k= S=

<Not Suitable For Analysis>

<Not Suitable For Analysis>

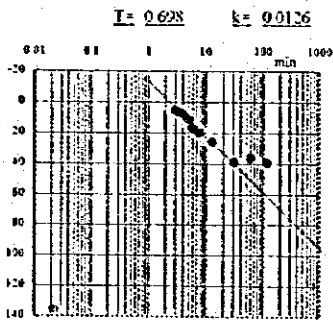


No. 1479

I= k= S= I= k= S=

<Not Suitable For Analysis>

<Not Suitable For Analysis>

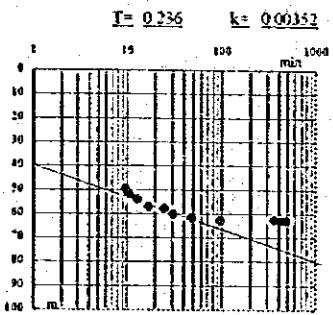


No. 1475

I= k= S= I= k= S=

<Not Suitable For Analysis>

<Not Suitable For Analysis>

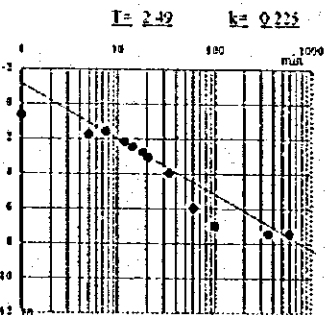


No. 2052

I= k= S= I= k= S=

<Not Suitable For Analysis>

<Not Suitable For Analysis>

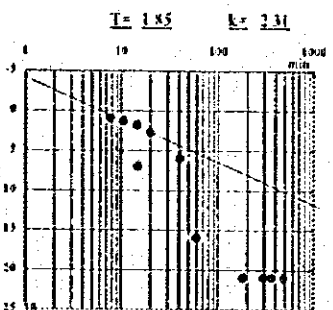


No. 3092

I= k= S= I= k= S=

<Not Suitable For Analysis>

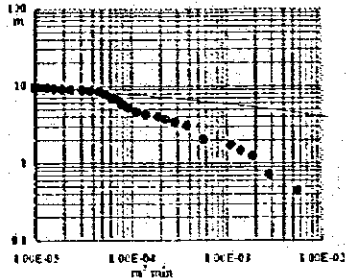
<Not Suitable For Analysis>



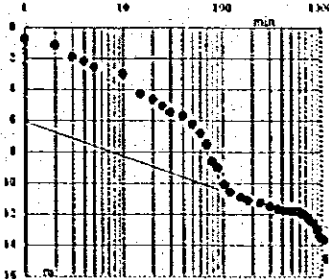
Appendix 2 (47) Result of Pumping Test Analysis

No. 2266

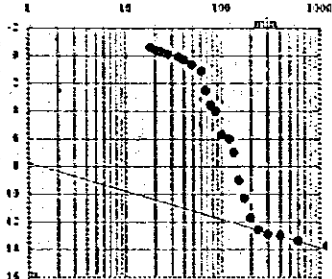
T= 2.86 k= 0.448 S= 0.00526



T= 1.00E+01 k= 0.453 S= 4.98E-03

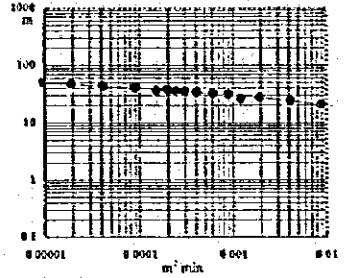


T= 10.8 k= 0.489

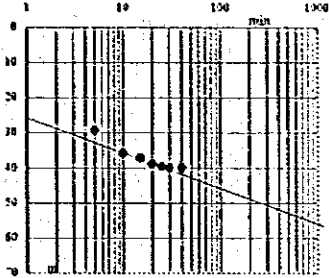


No. 1862

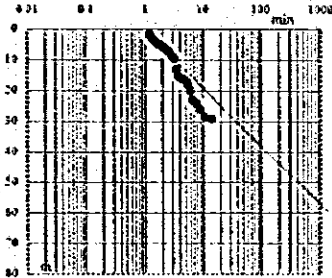
T= 3 k= 0.116 S= 0.00199



T= 2.98 k= 0.115 S= 0.00214

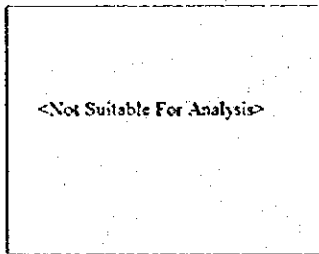


T= 1.58 k= 0.0608

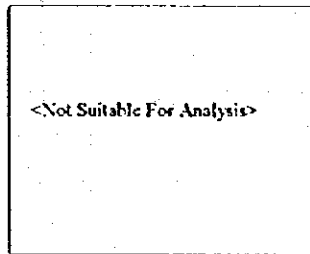


No. 1856

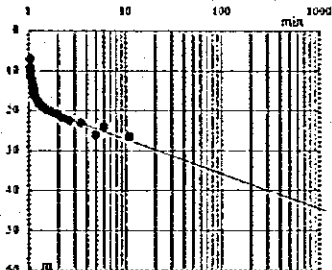
T= k= S=



T= k= S=

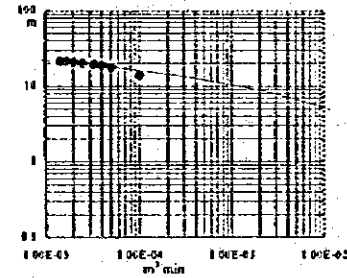


T= 0.208 k= 0.0139

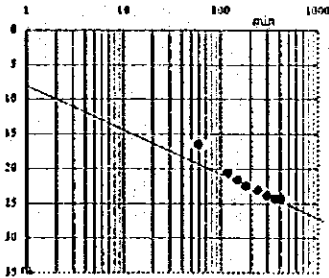


No. 1325

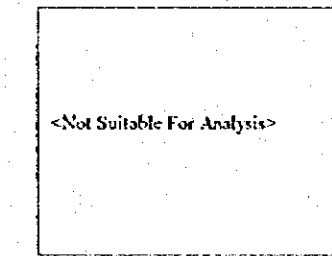
T= 7.65E+00 k= 1.83E-01 S= 2.25E-02



T= 7.44 k= 0.178 S= 0.104

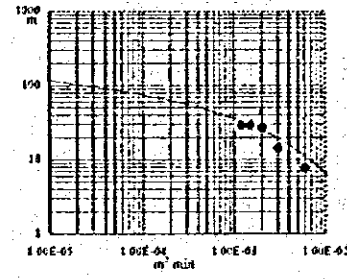


T= k=

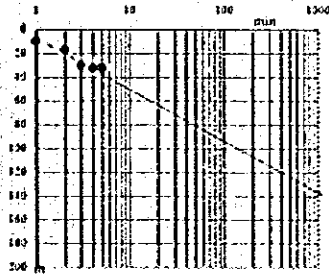


No. 1804

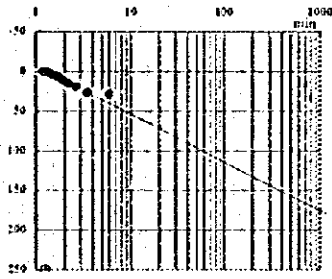
T= 6.49E-01 k= 2.31E-02 S= 9.37E-02



T= 0.561 k= 0.0203 S= 0.0981



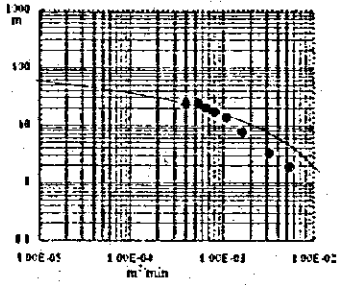
T= 0.434 k= 0.0144



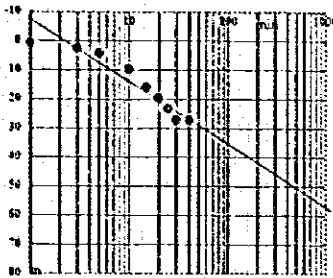
Appendix 2 (48) Result of Pumping Test Analysis

No. 1889

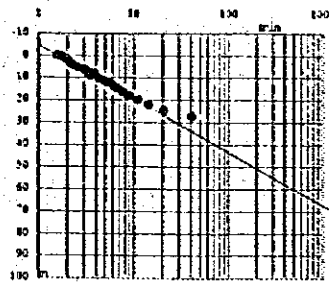
T= 1.13 k= 0.0626 S= 0.248



T= 1.14E+00 k= 0.0631 S= 2.40E-01

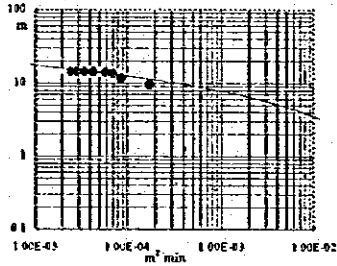


T= 1.01 k= 0.0563

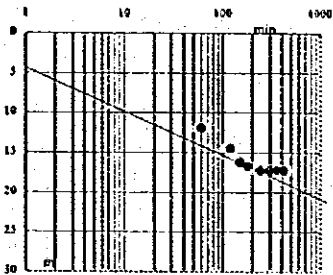


No. 1334

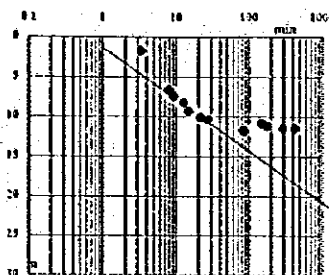
T= 1.45 k= 0.185 S= 0.0296



T= 1.43 k= 0.179 S= 0.0351

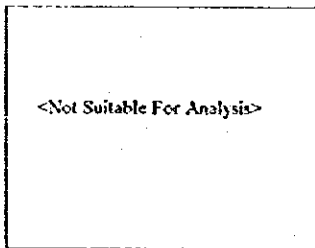


T= 1.22 k= 0.152

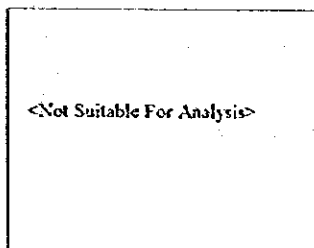


No. 1294

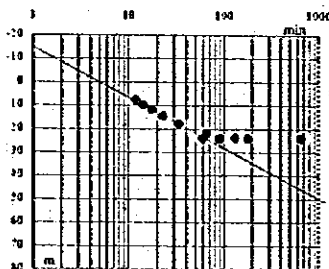
T= k= S=



T= k= S=

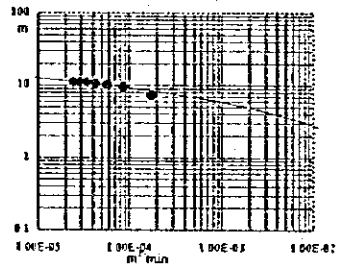


T= 3.66 k= 0.173

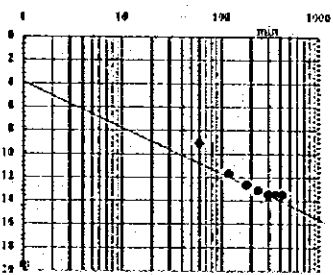


No. 1312

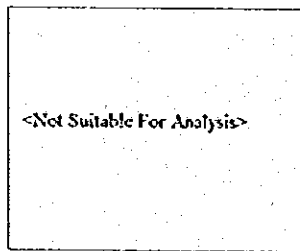
T= 4.46E+00 k= 1.06E+00 S= 6.96E-02



T= 4.47 k= 1.06 S= 0.0668

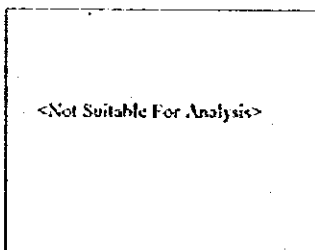


T= k=

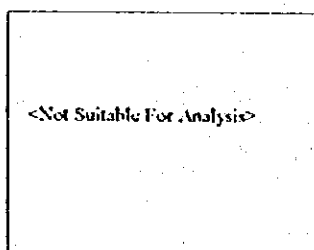


No. 1326

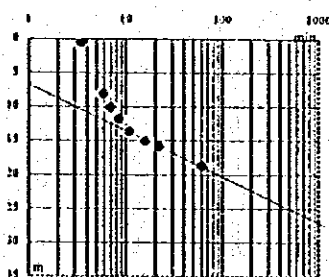
T= k= S=



T= k= S=



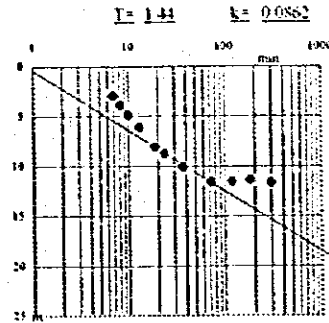
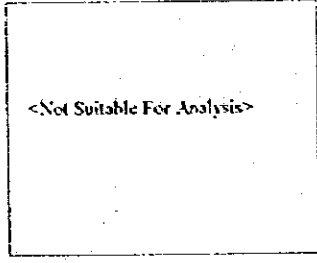
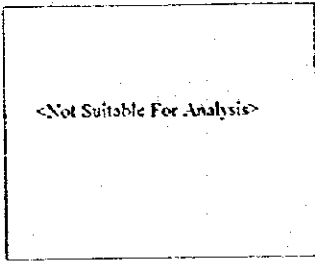
T= 0.933 k= 0.0066



Appendix 2 (49) Result of Pumping Test Analysis

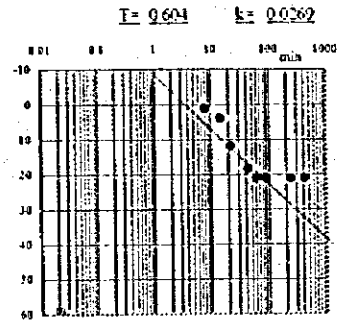
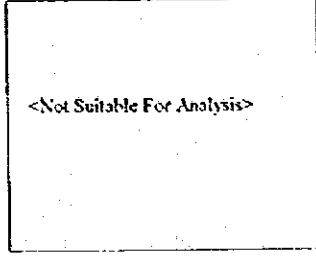
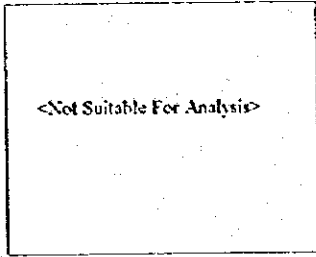
No. 1272

T= k= S= T= k= S=



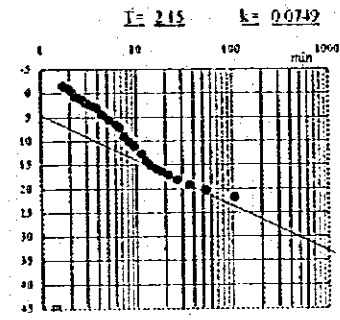
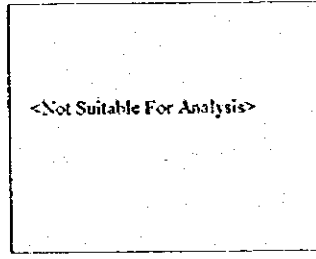
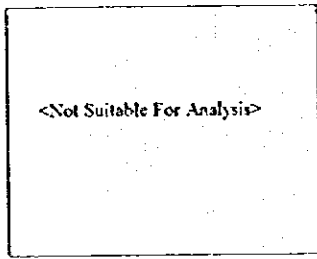
No. 1275

T= k= S= T= k= S=



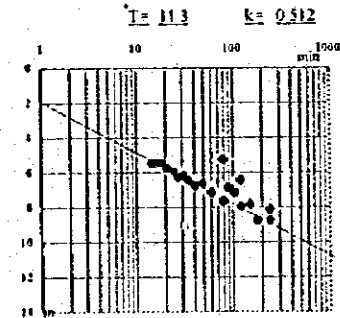
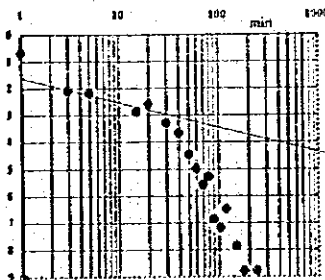
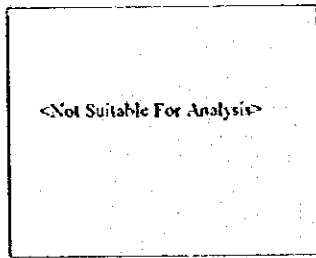
No. 2210

T= k= S= T= k= S=



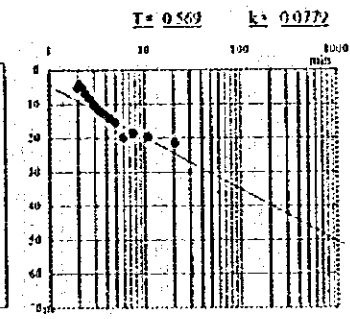
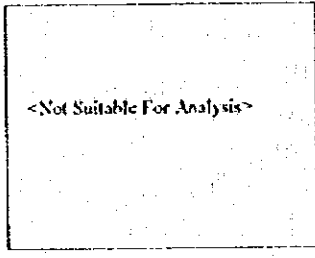
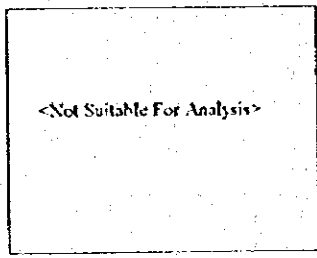
No. 1753

T= k= S= T= 352 k= 1.65 S= 0.152



No. 1558

T= k= S= T= k= S=



Appendix 2 (50) Result of Pumping Test Analysis

No. 1296

T=

k=

S=

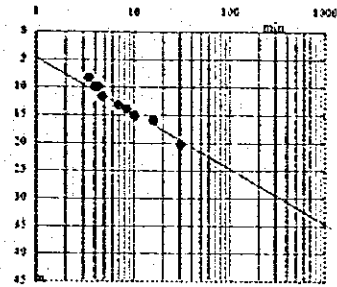
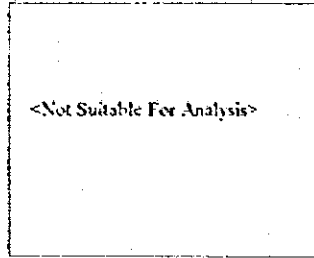
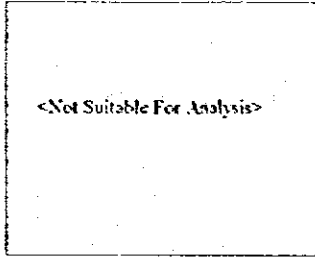
T=

k=

S=

T= 1.11

k= 0.0437



No. 1297

T=

k=

S=

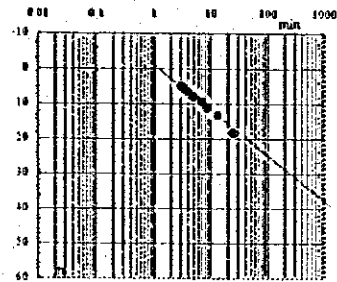
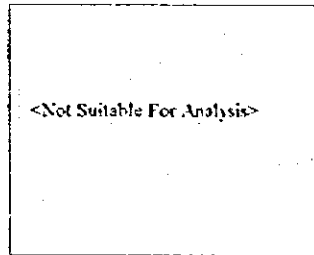
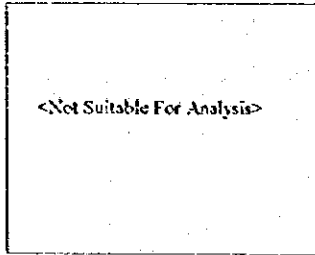
T=

k=

S=

T= 0.889

k= 0.0347

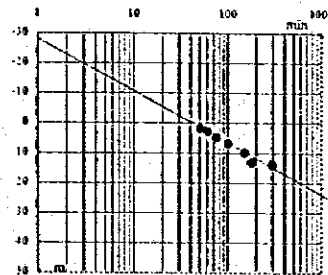
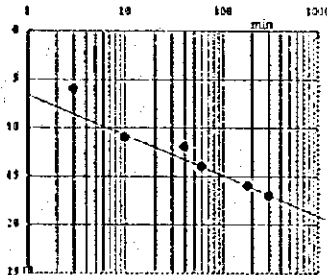
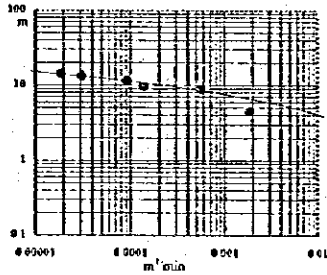


No. 1919

T= 6.02E+00 k= 2.01E+00 S= 4.26E-02

T= 6.03 k= 2.03 S= 0.0435

T= 1.45 k= 0.485

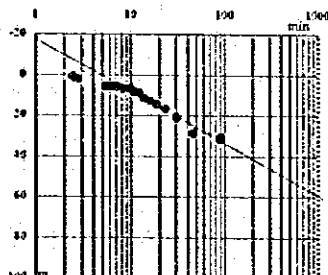
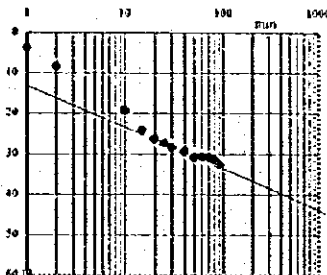
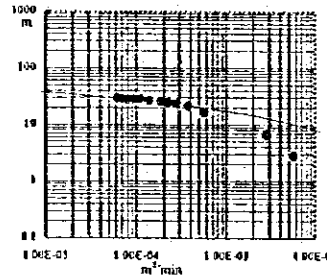


No. 2931

T= 3.86E+02 k= 1.15E-01 S= 5.94E-02

T= 3.86 k= 0.115 S= 0.0563

T= 1.54 k= 0.046

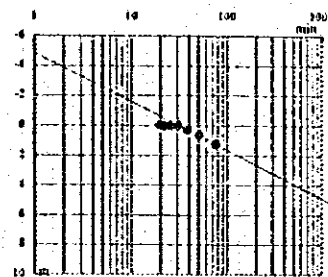
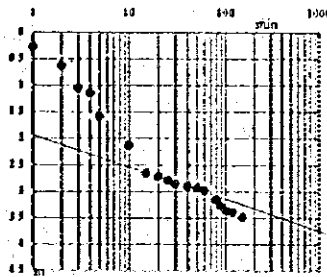
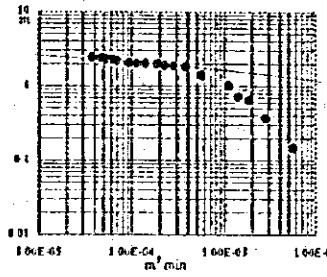


No. 318117

T= 2.00E+01 k= 5.00E+00 S= 1.35E-02

T= 91.8 k= 5.1 S= 0.0154

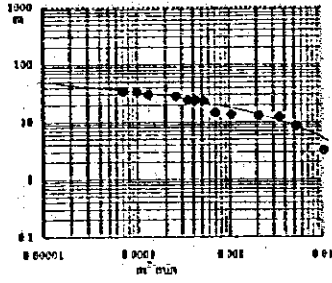
T= 17 k= 0.946



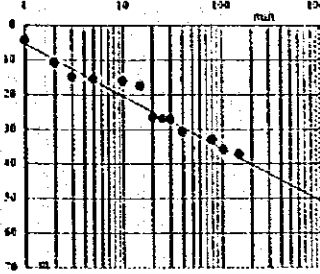
Appendix 2 (51) Result of Pumping Test Analysis

No. 5803

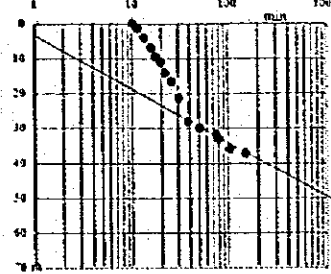
$T = 0.00103$ $k = 0.000147$ $S = 0.0000671$



$T = 1.05E-03$ $k = 0.00015$ $S = 6.85E-05$

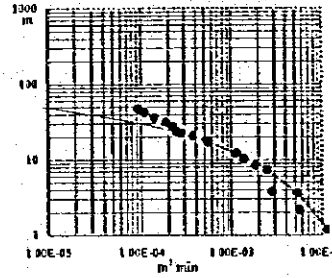


$T = 0.00102$ $k = 0.000146$

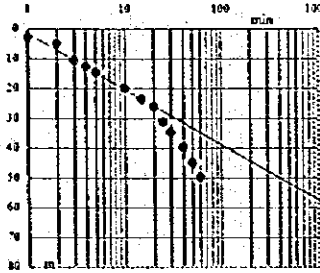


No. 1866

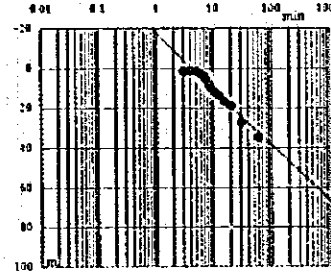
$T = 1.05$ $k = 0.102$ $S = 0.234$



$T = 1.06$ $k = 0.102$ $S = 0.241$

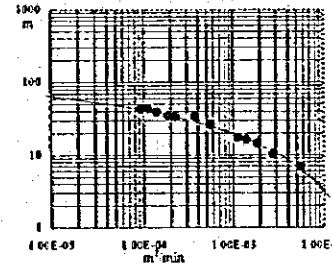


$T = 0.706$ $k = 0.0682$

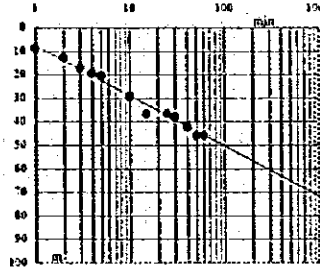


No. 1726

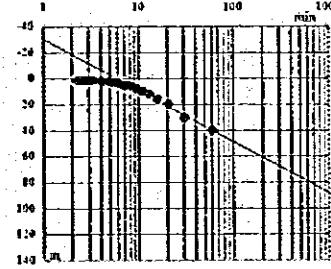
$T = 5.73E-01$ $k = 9.70E-02$ $S = 1.39E-01$



$T = 0.924$ $k = 0.103$ $S = 0.116$

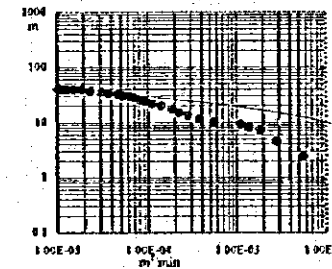


$T = 0.498$ $k = 0.0553$

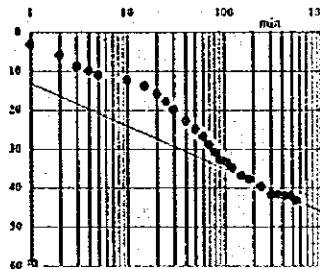


No. 2146

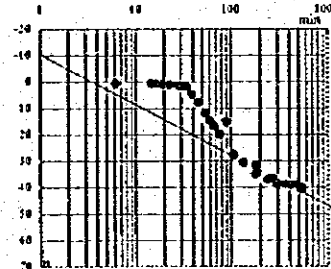
$T = 3.82E+00$ $k = 1.53E-01$ $S = 3.74E-02$



$T = 3.61$ $k = 0.144$ $S = 0.0624$

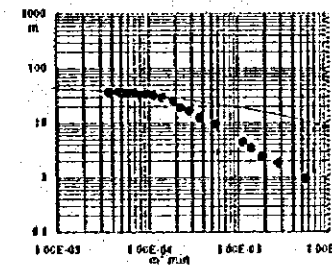


$T = 2.07$ $k = 0.0827$

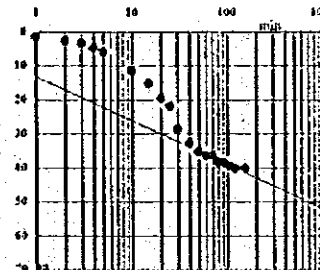


No. 2135

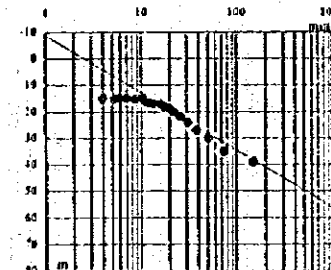
$T = 1.98E+00$ $k = 5.50E-02$ $S = 5.00E-02$



$T = 1.95$ $k = 0.0543$ $S = 0.0516$



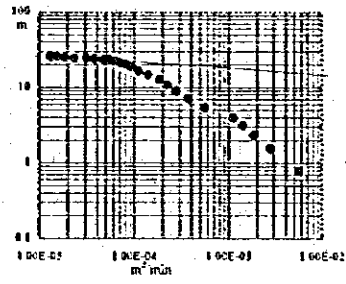
$T = 1.16$ $k = 0.0323$



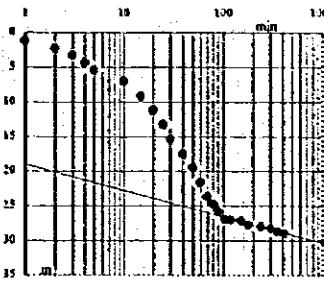
Appendix 2 (52) Result of Pumping Test Analysis

No. 2017

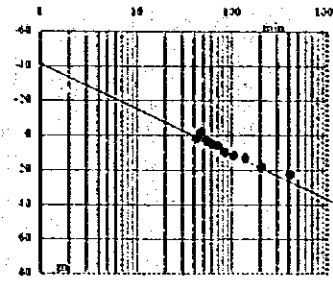
T= 11 k= 0.366 S= 0.00368



T= 1.15E+01 k= 0.382 S= 2.27E-03

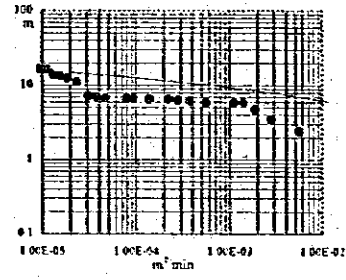


T= 2.25 k= 0.0749

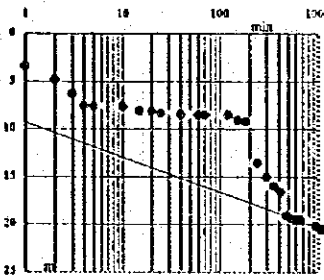


No. 1773

T= 15.2 k= 0.371 S= 0.00892



T= 15.2 k= 0.37 S= 0.0116

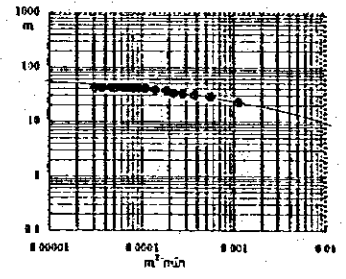


T= k=

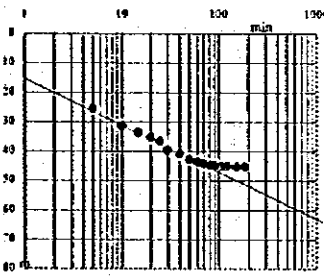
<Not Suitable For Analysis>

No. 2749-1

T= 1.79E+02 k= 1.98E-01 S= 9.24E-02



T= 1.83 k= 0.204 S= 0.0838

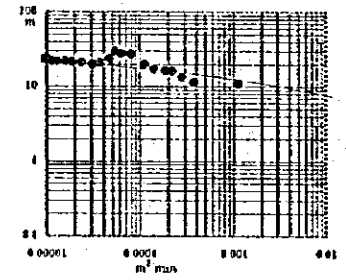


T= k=

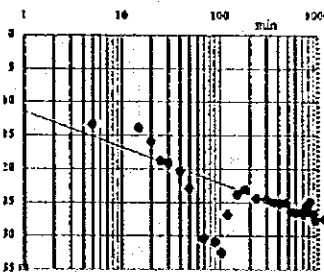
<Not Suitable For Analysis>

No. 2716

T= 1.13E+01 k= 2.82E+01 S= 2.23E-02



T= 11.2 k= 28.1 S= 0.0223

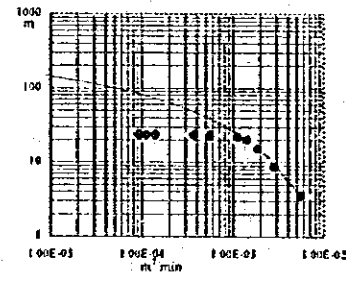


T= k=

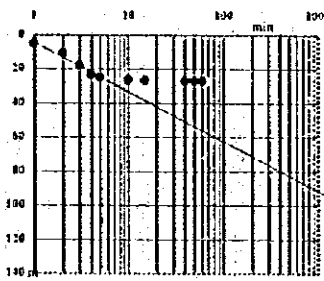
<Not Suitable For Analysis>

No. 2231

T= 9.84E-02 k= 9.84E-03 S= 5.25E-02



T= 0.19 k= 0.019 S= 0.0375



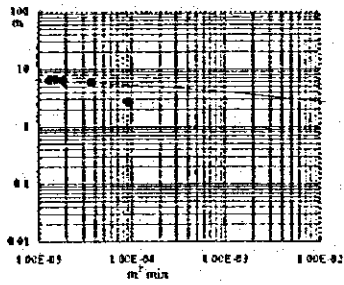
T= k=

<Not Suitable For Analysis>

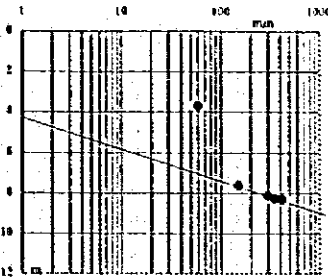
Appendix 2 (53) Result of Pumping Test Analysis

No. 13051.K

T= 9.537 k= 0.795 S= 0.0107



T= 9.53E+00 k= 0.795 S= 9.59E-03

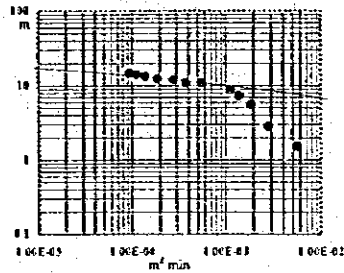


T= k=

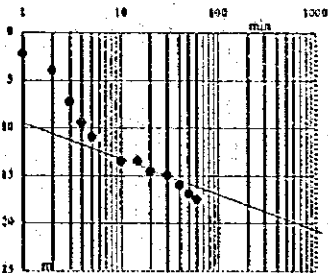
<Not Suitable For Analysis>

No. 2615B

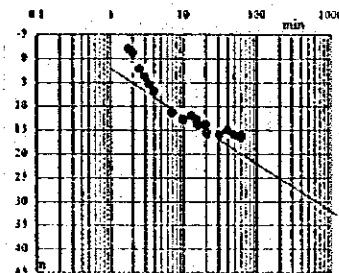
T= 5.37 k= 1.07 S= 0.00392



T= 5.47 k= 1.09 S= 0.00364



T= 2.06 k= 0.412

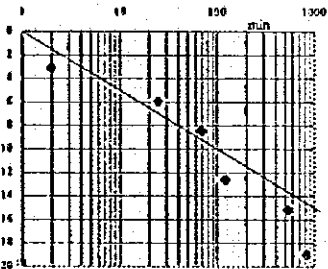


No. 1957

T= k= S=

<Not Suitable For Analysis>

T= 2.53 k= 0.12 S= 0.56



T= k=

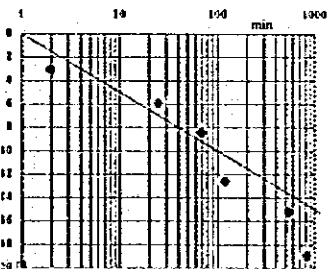
<Not Suitable For Analysis>

No. 2212

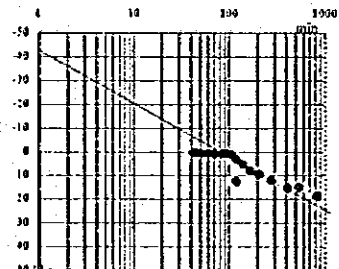
T= k= S=

<Not Suitable For Analysis>

T= 3.72 k= 0.177 S= 0.261



T= 0.564 k= 0.0268



No. 15-2

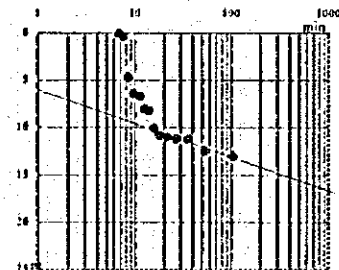
T= k= S=

<Not Suitable For Analysis>

T= k= S=

<Not Suitable For Analysis>

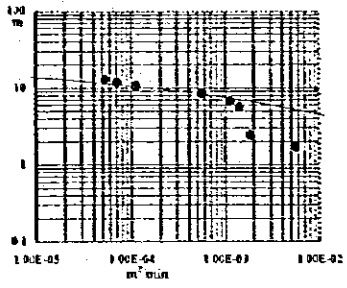
T= 7.21 k= 0.831



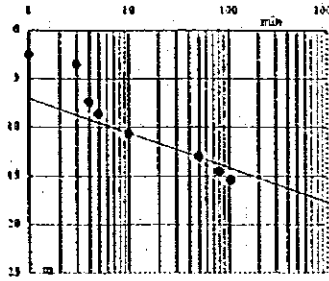
Appendix 2 (54) Result of Pumping Test Analysis

No. 2158

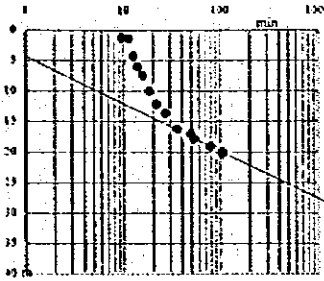
T= 2.56 k= 0.0883 S= 0.00769



T= 2.58E+00 k= 0.0891 S= 7.46E-03

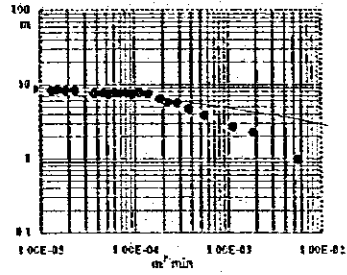


T= 1.18 k= 0.0406

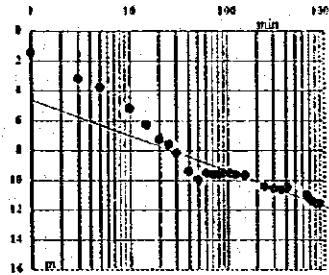


No. 1890

T= 8.37 k= 19.5 S= 0.0247



T= 8.42 k= 19.6 S= 0.027

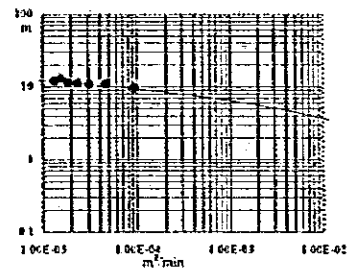


T= k=

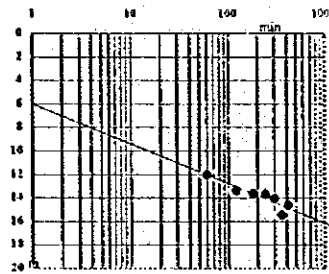
<Not Suitable For Analysis>

No. 1450

T= 3.79E+00 k= 8.71E-02 S= 1.73E-02



T= 3.74 k= 0.086 S= 0.0174



T= k=

<Not Suitable For Analysis>

No. 1497

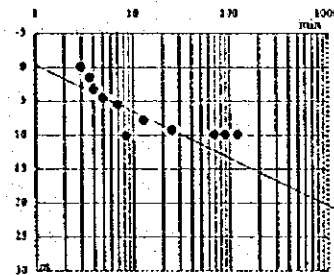
T= k= S=

<Not Suitable For Analysis>

T= k= S=

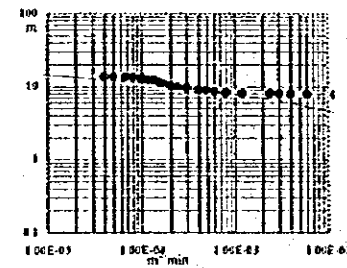
<Not Suitable For Analysis>

T= 0.528 k= 0.0664

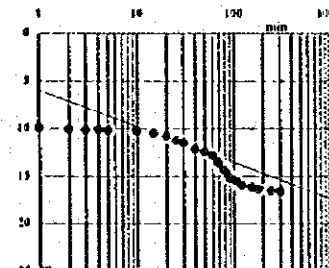


No. 2140

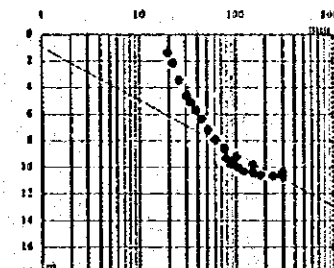
T= 1.26E+01 k= 3.54E-01 S= 3.98E-02



T= 12.5 k= 0.351 S= 0.0426



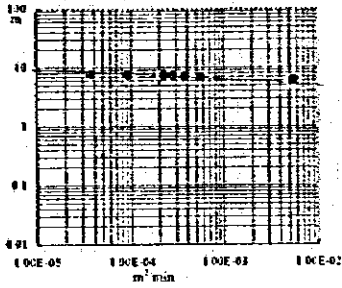
T= 11.8 k= 0.33



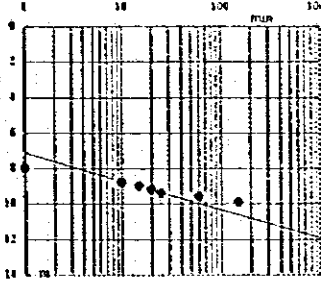
Appendix 2 (55) Result of Pumping Test Analysis

No. 2203

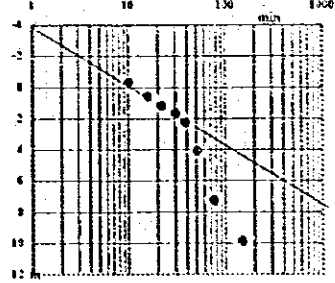
T = 43.7 k = 3.36 S = 161E-08



T = 4.36E+01 k = 3.36 S = 1.69E-08

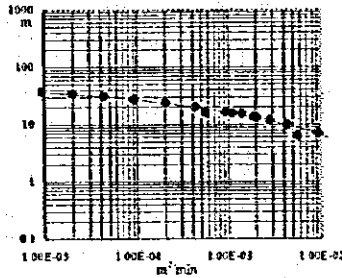


T = 12.3 k = 0.987

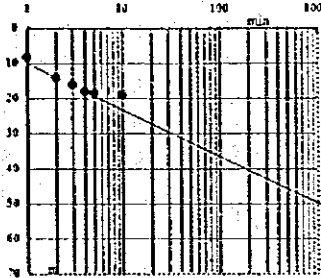


No. 1667

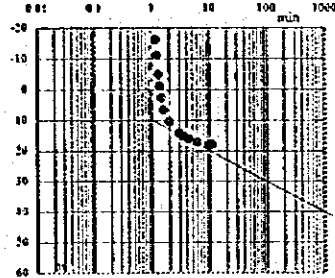
T = 0.356 k = 0.0297 S = 0.0105



T = 0.258 k = 0.0249 S = 0.0147

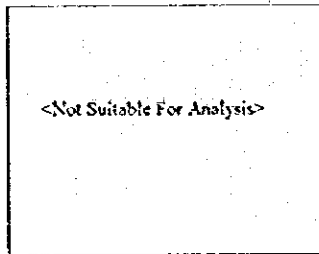


T = 0.391 k = 0.0326

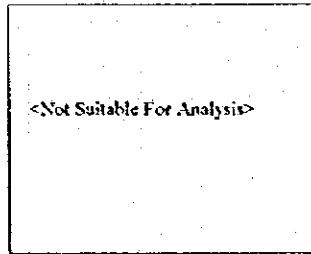


No. 1666

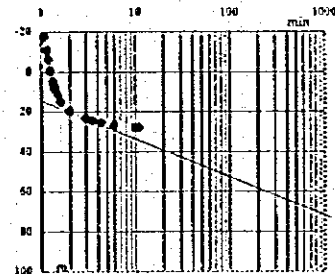
T = k = S =



T = k = S =

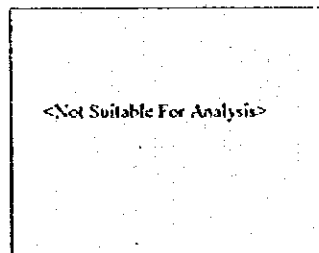


T = 2.06 k = 0.229

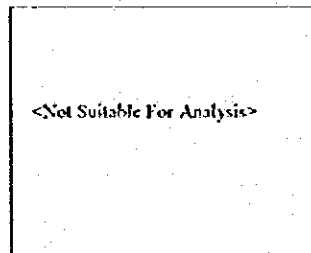


No. 1665

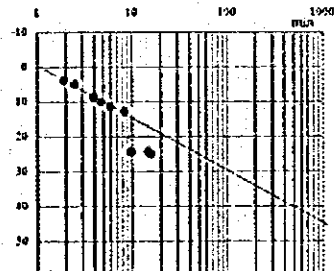
T = k = S =



T = k = S =

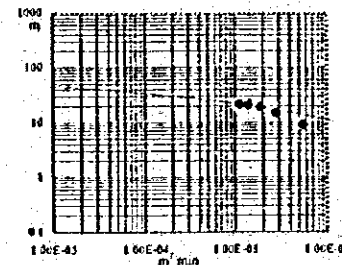


T = 10.5 k = 0.269

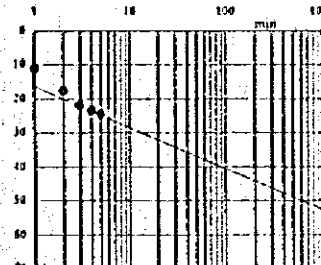


No. 1653

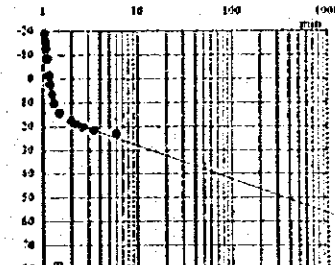
T = 6.53E+00 k = 1.26E-01 S = 7.60E-02



T = 6.53 k = 0.126 S = 0.0806



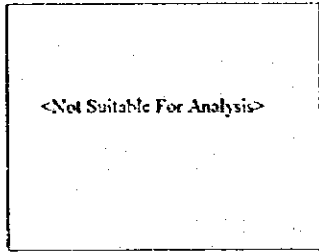
T = 5.61 k = 0.108



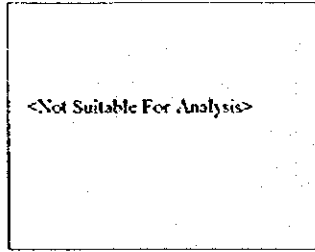
Appendix 2 (56) Result of Pumping Test Analysis

No. 2937

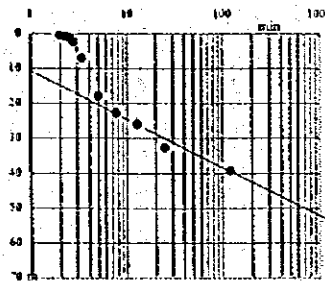
$T =$ $k =$ $S =$



$T =$ $k =$ $S =$

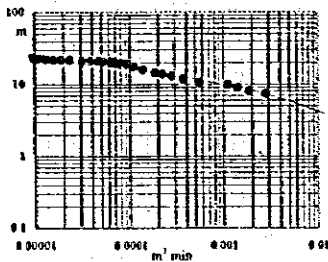


$T = 457$ $k = 0.117$

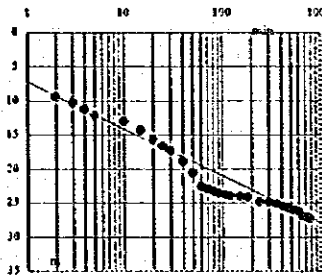


No. 2630

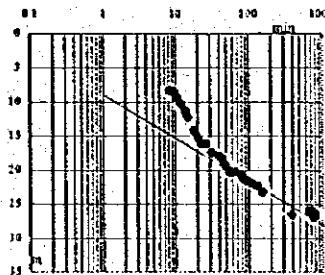
$T = 291$ $k = 0.121$ $S = 0.0713$



$T = 291$ $k = 0.121$ $S = 0.0728$

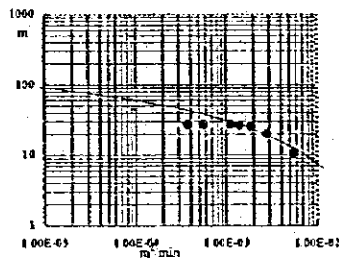


$T = 316$ $k = 0.132$

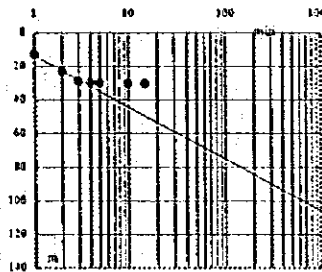


No. 2617

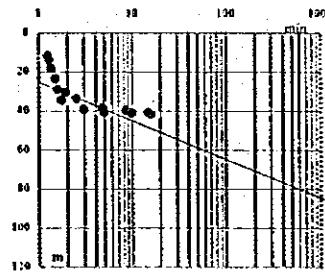
$T = 1.06E-01$ $k = 3.10E-03$ $S = 1.00E-02$



$T = 0.0973$ $k = 0.00286$ $S = 0.00924$

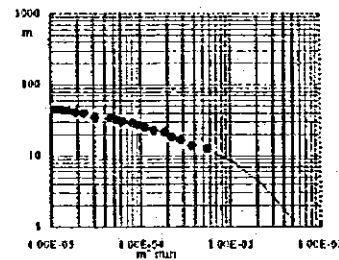


$T = 0.152$ $k = 0.00416$

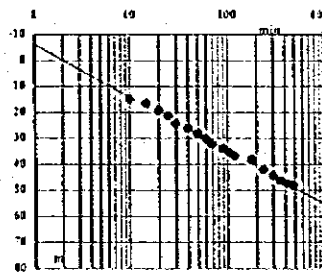


No. 1916

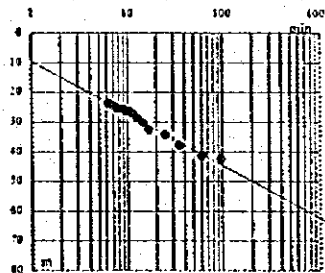
$T = 3.07E-01$ $k = 4.45E-02$ $S = 1.72E-01$



$T = 0.308$ $k = 0.0447$ $S = 0.173$

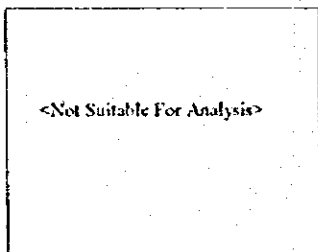


$T = 0.361$ $k = 0.0523$

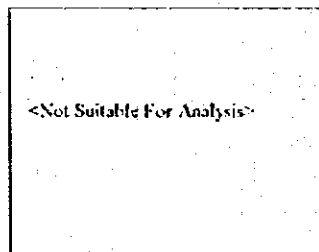


No. 1917

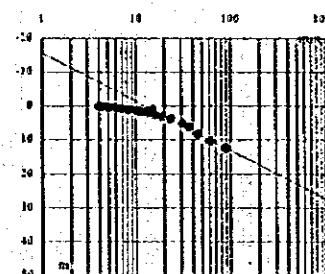
$T =$ $k =$ $S =$



$T =$ $k =$ $S =$



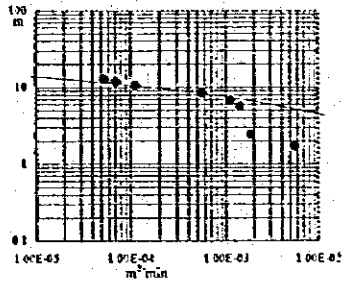
$T = 42$ $k = 0.346$



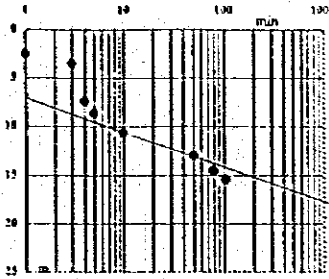
Appendix 2 (57) Result of Pumping Test Analysis

No. 2158

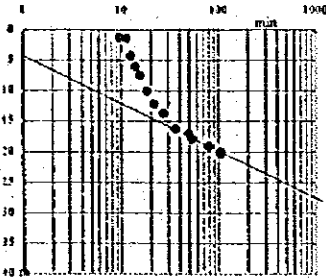
T= 2.56 k= 0.0883 S= 0.00769



T= 2.58E+00 k= 0.0891 S= 7.46E-03

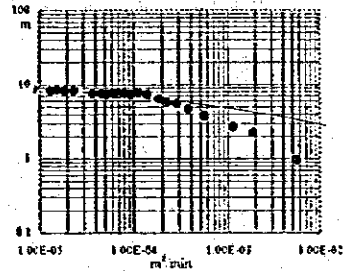


T= 1.18 k= 0.0406

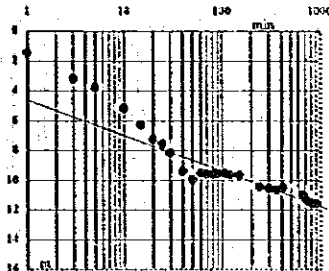


No. 1880

T= 8.37 k= 19.5 S= 0.0247



T= 8.42 k= 19.6 S= 0.027

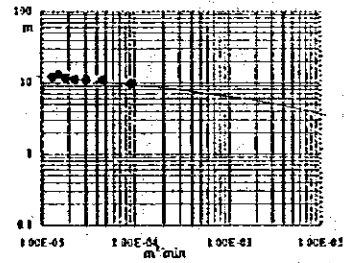


T= k=

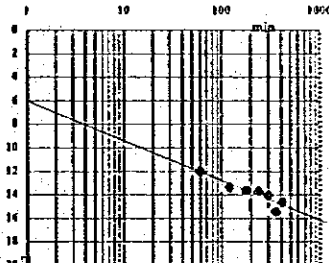
<Not Suitable For Analysis>

No. 1450

T= 3.79E+02 k= 8.71E-02 S= 1.73E-02



T= 3.74 k= 0.086 S= 0.0174



T= k=

<Not Suitable For Analysis>

No. 1487

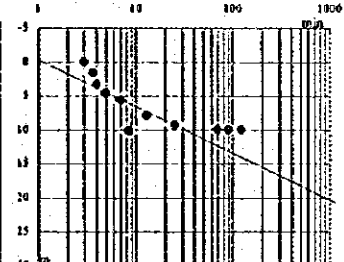
T= k= S=

<Not Suitable For Analysis>

T= k= S=

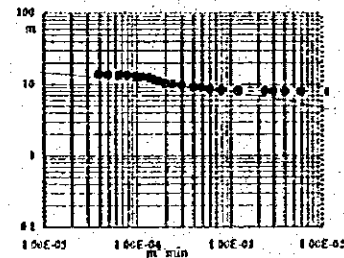
<Not Suitable For Analysis>

T= 0.598 k= 0.0664

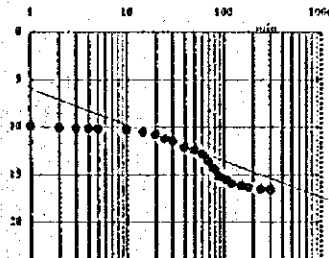


No. 2140

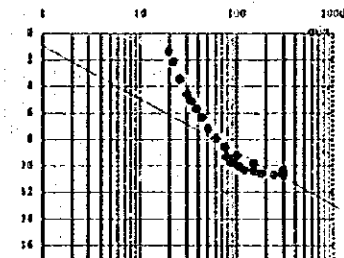
T= 1.26E+01 k= 1.54E-01 S= 3.98E-02



T= 12.5 k= 0.351 S= 0.0426



T= 11.8 k= 0.33



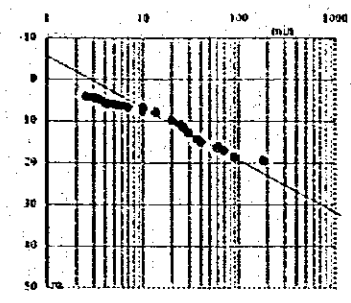
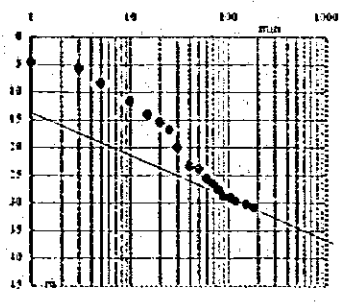
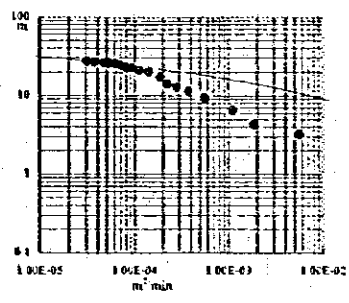
Appendix 2 (58) Result of Pumping Test Analysis

No. 1787

I= 7.15 k= 0.14 S= 0.0359

I= 7.18E+00 k= 0.141 S= 1.39E-02

I= 4.42 k= 0.0867



No. 1476

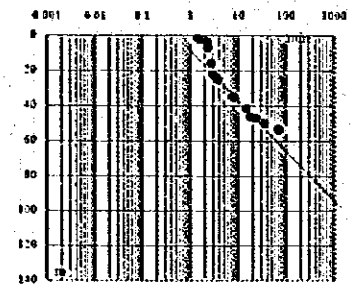
I= k= S=

I= k= S=

I= 0.111 k= 0.00202

<Not Suitable For Analysis>

<Not Suitable For Analysis>



No. 1459

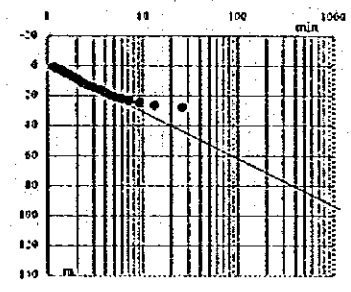
I= k= S=

I= k= S=

I= 0.353 k= 0.0165

<Not Suitable For Analysis>

<Not Suitable For Analysis>



No. 1524

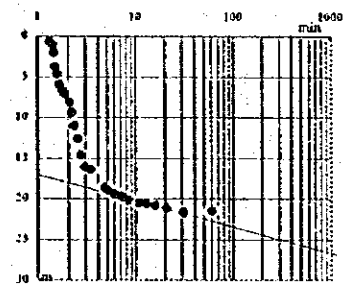
I= k= S=

I= k= S=

I= 1.24 k= 0.0337

<Not Suitable For Analysis>

<Not Suitable For Analysis>



No. 1860

I= k= S=

I= k= S=

I= 0.73 k= 0.0457

<Not Suitable For Analysis>

<Not Suitable For Analysis>

