ANNEX B : TABLES

No.	Code	Basin	Name of Station	Class	La	tion	Elevation	Perio	d of D	ata Coll	ected
					Latitude	Longitude	(m)	Year	Mon.	Year	Mon.
1	401	YAQUE D. N.	JARABACOA	1	19 • 7 • 50 *	70 • 38 • 20 *	500	1968	1	1994	4
2	402	YAQUE D. N.		ł	19 17 0 "	70 . 43 ' 5"	300	1968	1	1992	3
3	404	YAQUE D. N.	SANTIAGO ISA	1	19 . 26 . 45 "	70 . 44 . 45 .	160	1967	12	1992	2
4	409	YAQUE D. N.	EL RIO CONSTANZA	2	18 * 58 * 50 *	70 * 37 * 40 *	1120	1960	6	1991	9
5	413	YAQUE D. N.	PINAR QUEMADO	3	19 . 5 ' 30 "	70 • 40 • 30 *	565	1968	11	1972	9
6	414	YAQUE D. N.	вомл	3	19 • 10 * 14 "	70 ' 39 ' 46 "	435	1974	6	1979	7
7	415	YAQUE D. N.	GUANAJUMA	3	19 . 16 ' 30 "	70 • 44 ' 40 *	274	1967	5	1970	8
8	416	YAQUE D. N.		3	19 * 17 ' 50 "	70 * 46 * 39 *	320	1967	6	1989	6
9	417	YAQUE D. N.	BAO	3	19 • 18 ' 20 "	70 . 47 . 20 .	280	1965	12	1970	7
10	418		SABANA IGLESIA	3		70 • 44 • 50 *	229	1967	8	1970	9
11	419		LAS CHARCAS	3.	19 * 24 * 30 *	70 * 42 * 50 *	170	1967	9	1970	8
12	1001	YASICA	JAMAO	3		70 • 27 • 0 "	32	1968	11	1979	6
13	1002	YASICA	CUESTA BARROSA	1	19:39/10"	70 • 24 • 40 *	10	1977	10	1978	10
14	1501	BOBA	LOS JENGIBRES	1	19 . 26 . 50 .	70 2' 50"	15	1969	10	1992	3
15	1601	NAGUA	CINTA NEGRA	2	19 * 16 * 26 *	69 . 58 . 1"	180	1981	1	1991	7
16	1603	NAGUA	NAGUA (MET)	3	19 * 22 * 0 *	69 . 50 ' 0"	3	1943	4	1994	5
17	1801	YUNA	SAN FCO. DE MACORIS	1	19.17.10"	70 • 14 • 25 *	110	1968	2	1990	9
18	1802	YUNA	JUMA BONAO	1	18 . 54 ' 0 "	70 • 23 • 10 *	178	1970	12	1992	1
19	1803	YUNA	LIMON DEL YUNA		19 9 10*	69 . 49 . 10 .	8	1968	7	1975	T
20	1804	YUNA	LOS QUEMADOS	2	18 * 53 ' 30 *	70 • 27 • 30 *	250	1960	6	1992	1
21	1805	YUNA	MAIMON EL PINO	3	18 * 53 * 50 *	70 • 17 • 30 "	. 98	1960	3	1970	8
22	1806	YUNA	HATILLO YUNA	1	18 . 56 1 50 "	70 • 15 ' 10 "	80	1968	1	1971	5
23	1807	YUNA	JIMA RINCON	3		70 • 24 • 20 *	130	1968	5	1975	12
24	1808	YUNA	LOS RANCHITOS	3		70 . 24 . 30 .	56	1968	4	1970	8
25	1809	YUNA	LICEY NARANJAL	3		70 • 30 • 50 *	110	1968	12	1992	2
26		YUNA	LA BIJA	3		70 . 7 45 .	28	1968	4	1970	8
27	1811	YUNA	ABADESA	3	19 0' 50"	69 . 55 ' 30 "	33	1960	3	1992	1
28	1813	YUNA	V. ALTAGRACIA (MET)	3		70.10.0.	156	1938	8	1980	12
29	1814	YUNA	BARRAQUITO	1		69 • 47 ' 20 "	8	1975	2	1992	1
30	1815	YUNA	LA ANGELINA	1		70 • 13 ' 20 "	48	1977	1	1992	· ;
31	1816	YUNA	JOSE CONTRERAS		19 . 28 ' 0 "		685	1978	Ĥ	1992	$-\frac{1}{1}$
32	1817	YUNA	LOS BOTADOS			70 . 34 ' 36 "	1020	1980	8	1992	2
33	1821	YUNA	LA CEIBA RIO BLANCO			70 * 33 * 28 *	970	1978	3	1992	1
34	1826	YUNA	TIREO EN PINALITO		18 . 52 ' 58 "		870	1981	4	1991	5
35	1830	YUNA	EL NOVILLO			70 • 28 ' 21 "	1225	1982	10	1992	3
36	1836	YUNA	EL TALLER · LA VEGA		19 • 13 • 30 *		60	1984	5	1990	3
37	1837	YUNA	LA CABILMA		18 . 59 . 3 .		46	1983	1	1992	$-\frac{5}{1}$ -
38	1838	YUNA	CENOVI SANTA ANA			70 • 20 • 49 •	81	1983	2	1992	i
39	1839	YUNA	CEVICOS (MET)			69 . 58 . 0 .	90	1938	9	1994	6
40		YUNA	LOS TRES PASOS	3	18 * 58 * 25 *		110	1984	5	1991	9
41		YUNA	TALLER LAS MATAS	3	19 6 17	70 10 46 "	47	1984	5	1988	4
42	1842	YUNA	PIEDRA BLANCA			70 . 19 . 43 .	200	1984		1992	$\overline{1}$
43		YUNA	EL AGUACATE		19 • 10 • 19 •		20	1986	3	1991	
44	1844	YUNA	VILLA RIVA (MET)		19 . 10 . 0 .		17	1939	$\frac{1}{1}$	1991	
45.	1845	YUNA	COTUL (MET)		19 . 3' 0 "		60	1938	īt	1991	7
46	1846	YUNA	PIMENTEL (MET)		19 . 11 . 0 .		37	1931	i t	1994	5
47	1847		S.F.DE MACORIS (MET)		19 • 17 • 0 •		110	1931	7	1994	4
48	1848		SALCEDO (MET)		19 . 22 ' 0 '		196	1931	-†-†	1994	6
49	1849		BONAO (MET)		18 . 56 ' 0 "		172	1938	8	1994	7
	1850		LA VEGA (MET)		19 - 13 ' 0 "		97	1931	î	1994	5
51			MOCA (MET)		19 • 23 • 0 •		83	1931		1994	$\frac{3}{7}$
52	3805		LA ESTRECHURA		18 • 43 • 40 *	and the second s	720	1968		1973	2
53			VALLE NUEVO	_		70 • 40 • 58 *	2300	1968	- <u>-</u> +	1993	12
54			CONSTANZA		18 • 54 ' 40 "		1215	1968		1993	
and a	بالمتحد محمد		NAME OF A DESCRIPTION OF A			V 72 V	1213	1708 }	<u> </u>	1774	2

Table B.2.1 List of Rainfall Gauge Stations in and around the Yuna River Basin

Table B.2.2 Summary of Rainfall Data

			T T	F-L I	<u>.</u>	- A	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec	Annual
No.	Code	Name of Station	Jan 102.2	Feb 92.1	Mar 100.1	Apr 170.0	202.0	84.2	85.8	116.1	106.3	143.2	183.2	138.7	1524.0
		JARABACOA	102.2	72.9	74.6	154.0	184.0	74.5	63.6	90.5	103.6	137.5	116.0		1247.3
2		TAVERA SANTIAGO ISA	52.2	43.7	59.8	133.8	150.1	70.1	43.9	70.3	83.3	108.0	100.8	65.0	981.1
		EL RIO CONSTANZA	76.3	76.7	70.3	117.3	139.5	87.1	91.1	130.7	126.5	138.7	145.5	113.6	
		PINAR QUEMADO	65.4	139.9	108.6	176.7	254.3	109.4	102.1	170.7	215.0	168.7	220.6	197.4	
6		BOMA	40.9	80.9	100.9	212.9	147.7	82.3	88.1	86.3	69.6	120.2	165.3	140.6	1335.7
7		GUANAJUMA	81.2	91.2	61.8	127.6	224.8	120.2	78.7	62.1	77.7	77.8	162.9		1363.9
8		PINALITO	\$5.7	47.1	34.2	115.5	297.2	140.2	51.6	55.4	39.0	62.7	157.6	223.3	1279.4
1 9		BAO	82.4	73.0	93.4	143.2	225.5	81.6	50.1	58.8	32.2	111.1	132.3	125.0	1208.4
10		SABANA IGLESIA	49.6	62.2	31.1	66.4	247.7	94.3	57.5	53.4	50.3	48.6	131.7	122.7	1015.4
	1	LAS CHARCAS	52.9	50.5	47.7	69.9	214.5	86.8	57.2	32.8	42.7	50.9	193.8	133.8	
12		JAMAO	126.5	142.5	158.6	249.4	225.1	61.3	70.3	135.3	124.3	188.8	192.6	358.8	2033.6
13		CUESTA BARROSA	419.7	62.6	•	37.1	•	33.6	68.0	75.0	83.0	-	-	•	· •
14		LOS JENGIBRES	177.4	134.6	146.9	201.2	273.9	131.8	153.8	180.5	160.3	244.9	316.9	244.6	2366.9
15		CINTA NEGRA	209.4	165.3	139.2	122.1	251.7	169.8	164.6	191.0	202.1	232.4	289.9	252.7	2390.1
16		NAGUA (MET)	156.6	126.8	115.1	149.3	245.4	128.7	136.5	169.0	157.8	210.3	272.6	234.0	2101.8
17		SAN FCO. DE MACORIS	77.9	87.4	68.2	98.7	165.7	119.0	116.1	148.2	124.5	132.7	169.0		1429.2
18	1802		100.8	105.5	137.2	195.7	283.1	124.6	159.5	178.1	162.9	210.5	247.9		2055.0
19	1803	LIMON DEL YUNA	72.7	148.8	105.2	128.4	200.2	207.8	186.6	224.5	162.5	229.5	136.5		1969.0
20	1804	LOS QUEMADOS	118.8	150.9	148.3	256.0	309.1	163.3	187.6	229.5	231.1	247.5	243.4		2455.9
21	1805		80.9	82.8	86.7	164.4	311.7	162.7	180.8	188.0	137.4	125.5	168.0		1811.6
22	1806	HATILLO YUNA	44.4	157.6	49.5	193.4	550.8	116.3	. 158.6	209.7	197.2	196.3	225.0		
23	1807	JIMA RINCON	39.3	80.4	83.8	105.6	138.4	47.8	61.5	79.5	96.9	95.3	98.3	63.4	. 990.1
24	1808	LOS RANCHITOS	47.4	45.0	84.7	161.4	243.1	85.1	108.4	139.8	141.6	119.5	273.9		1504.0
25	1809	LICEY NARANJAL	59.6	80.0	68.9	116.9	178.9	76.2	\$8.1	103.8	118.5	149.5	153.2	101.2	
26	1810	LA BIJA	34.7	35.1	28.3	62.1	306.7	120.6	190.1	209.6	199.0	140.4	185.7		1631.7
27	1811		62.7	57.9	85.0	108.4	233.6	214.2	186.0	230.0	192.9	168.5	117.0		1742.2
28	1813	V. ALTAGRACIA (MET)	92.5	90.7	93.8	173.7	277.0	270.6	256.7	265.0	237.9	256.1	170.0		2288.9
29	1814	BARRAQUITO	114.7	97.2	118.0	167.7	314.6	184.9	197.0		162.4	178.2	192.4		2065.7
30		LA ANGELINA	79.4	71.9	75.6	147.0	232.4	103.0	138.4	129.9	143.5		153.8		1526.9
31	1816	JOSE CONTRERAS	138.5	124.9	123.2	152.4	230.8	110.6	106.5	136.7	133.8	159.3	197.4		1750.5
32		LOS BOTADOS	209.2	152.0	113.7	155.3	299.4	174.6	217.0		266.1	295.1	268.0		2588 8
33		LA CEIBA RIO BLANCO	201.8	155.9	194.5	195.3	333.1	215.2	248.1	314.4	335.8	302.8			3055.1
34	_	TIREO EN PINALITO	274.3	131.4	101.7	141.2	214.7	154.9	1	94.9	108.3	193.4	272.9	295.7	
35	_	ELNOVILLO	173.9	165.4	183.7	266.1	359.2	153.5	210.1	195.7	250.0	296.4	<u>363.0</u> 184.0	206.6	2823.6 1751.2
36		EL TALLER - LA VEGA	166.4	87.9	77.1	130.8	247.9	93.7	100.5		191.7	172.6			1783.7
37		LA CABILMA	99.7	108.3	78.4	102.2	224.3	132.1	185.0		175.5	193.7	382.2	107.9	b
38		CENOVI SANTA ANA	171.3	135.4	161.3	219.5	169.4 326.4	221.1 231.0	172.5	A normal second	194.7	175.0		106.4	
39		CEVICOS (MET)	84.3	<u>84.9</u> 253.3	<u>94.6</u> 69.0	148.8 31.8		78.6			103.3	57.6	69.4	63.5	
40		LOS TRES PASOS	<u>59.3</u> 72.3	66.5	93.5	93.4	265.5	137.1	91.2		227.6	\$	180.3	81.8	
41	_		133.0		·		230.1	169.4							
42		PIEDRA BLANCA	197.2		26.3	122.1	200.2	212.1	225.8		283.4	142.2	208.4	243.7	
43		EL AGUACATE	· · · · · · · · · · · · · · · · · · ·		f					228.5					2244.4
1		VILLA RIVÁ (MET) COTUL (MET)	135.8 87.3							181.3					1708.9
49	_	PIMENTEL (MET)	100.8												1769.8
40	-	SF.DE MACORIS (MET)	91.2				+	+		145.5	and the second data in second data				1429.6
47		SALCEDO (MET)	80.0												1253,7
40		BONAO (MET)	122.0												2196 3
45		LA VEGA (MET)	84.2					91.7			<u></u>	<u> </u>			1382,8
51		MOCA (MET)	76.8												1193.6
52		LA ESTRECHURA	49.4												1531.0
53		VALLE NUEVO	59.7												951.0
54		CONSTANZA	24.2			76.8	_								947.6
	1.1.1		تستبيعها	,			-lanara						di seneroran	*****	-

Table B.2.3 List of Meteorological Stations in and around the Yuna River Basin

T	Day	2	-		ſ	J.	-1	31	30	-	F	-1	1	-	1	r-4	l:	č	Ŗ
		10	6	01	G		~	12	4	6		^	ব	6	7	3	121		0
Period of Data Collected	Ycar Month	1988	1988	1988	0001		19881	1976	161	1988		1988	1988	1988	1985	1988	1972		1979
of Dati	Day	-4		F	•	╧╋	7	1	1				1	1	F.		-	ł	11
Period	Month	6	6	0		7	=	7	1			7	101	8	10		0		8
	Year 1	1967	1967	1047		896T	1971	1968	1968	1075		1973	1978	1980	1982	1986	10/21		1967
Elevation	Ĥ	500	300	160			178	8	80	ō	5	48	685	1020	1225	20	N.C	3	1215
	Longitude	7 50 70 38 20 1	70 . 43 . 5 -			70 • 14 • 25 7	70 23 10	69 • 49 10 "	70 15 10		07 14 60	70 . 13 . 20 7	70 - 27 - 0 -	70 - 34 - 36 -	170 • 28 • 21 -	- PE . 57 . 07 . 01	ļ	ş	40 170 43 0 1
Location	Latitude	19 - 7 - 50	1~	14	Ť	19 • 17 • 10	18 - 54 - 0 -	19. 9. 10	8			19 * 13 * 20 770 * 13 * 20	19.28.01	18 52 14		0	Ş	10 40 2/	18 54 40
Class	I	-	· -	•		1	-1			, ,	-	1			-	(-		i T	,
Name of Station				IA VENA	SANTIAGUISA	SAN FCO. DE MACORIS	JUMA-BONAO	ET I MON			BARKAQUITO	LA ANGELINA	IOSE CONTRERAS	I OS ROTADOS	ET NOVITIO	EL ACHTACATE		VALLE NUEVO	CONSTANZA
Racin		VACUE DEL NORTE IAPABACOA	TAQUE DELL'NONLE	AUDE DEL NONIE ITAVENA	YAQUE DEL NORIE ISANIJAGO	1801 YUNA	1802 MINA	1902 VTNIA		AND I	1814 YUNA	1815 VINA	1916 VINA	1217 MINA		T UNA	1045 IT UNA	4901 YAQUE DEL SUR	4902 YAOUF DEL SUR
Code Code	3	T		704	404	1801	1802	19/2		9961	1814	1815	1915	101	10201		ctol t	4901	4902
27	2	Ţ,		74	3	4	~				00	0			1 -		-	4	Y

Table B.2.4 Summary of Meteorological Data (1/2)

(1) Temperature (°C)

No.	Code	Name of Station	Item	l Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec	Annual
1	401	JARABACOA	Mean	19.7	20.1			23.0	1. 1. KO (10-	23.7	han to	×	23.2	the second se		22,2
			Max.	28.6	29.2	Contract on the local division of the local		31.4		32 2	32.2		and the second sec		28.5	
			Min.	10.1	10.4	the second s	12.3	14.3	- Lin- Kindson	14.3	14.2	14.3			_	
2	402	TAVERA	Mean	22.3	22.5	accession of	23.9	24.5	A LOCAL DESIGNATION OF THE OWNER	THE R. L.	25.9	100.000	25.3	****	Critesanes:	24.3
			Max.	30.8	30.8					Contra Co	32.9	33.4		31.4		31.9
			Min.	14.7	14.1		16.2	17.7	~~~~~	18.7	18.6			_	15.0	16.9
3	404	SANTIAGO-ISA	Mean	23.3	23.5	CONTRACTOR .		-		A	and the second		26.6			25.6
			Max.	31.2	-		33.8	the second se		the second s	35.2		34.4			33.6
			Min,	14.7	14.6		16.0			and the local division of the local division	20.3		19.0	A CONTRACTOR OF THE OWNER	15.0	17.3
4	1801	SAN FCO. DE MACORIS		-	23.1	100 212 10	24.9		-		26.5			CRATTER .	23.3	25,1
			Max.		31.5	VALUEL IN TRACTO	33.1	 Application spat 	33.7		33.7	33.8	·	_		32.8
			Min.		14.3	and the second second second		17.7				19.1	18.6	-	14.6	17.0
5	1802	JUMA-BONAO	Mean	1000	a destruction of			at sugar and		26.1	26.0		and the second		Construction of the local division of the lo	21.6
Ŭ	1002	John Donato	Max.		30.7		32.3	32.7			33.7		33.5		31.4	32.5
	ĺ		Min.		13.2						18.5	17.7		16.0		16,1
6	1803	EL LIMON	Mean			an property of	- Restartions	STREET.	COLOR PARTY	a strange states	26.4			a carina ana	and the second	Contraction of the local division of the loc
Ň	1005		Max.			Contraction of the local division of the loc	32.8	and the second se	the second se	and the second s				- all of the low rates of		25.4
			Min.	and the second second		16.2	the second second	18.7	-				- transferration of	17.8		<u>32.7</u> 18.3
7	1806	HATILLO - YUNA	Mean		and a second	24.6				WAR BOARD		CARGE COMPANY	and the second second	ALC: 10.000 PM	000.000	ATOMICS & CO. MARK
'	1000	INATILLO - TONA	Max.	and the state of the second		<u>24.0</u> 34.0		<u>20,8</u> 34,5	26.8		26.7					25.6
			Min.	-warman and a	And in case of the local division of the loc	and the second second second	17.0			35.0	34.5 18.5	Statement of the local division of the local		<u>34.0</u> 16.0		<u> </u>
8	1914	BARRAQUITO	Mean	Concession of the local division of the loca		and strategy of Assort	25.4	200 04100.00			-unena al			ALC: NOT THE OWNER		
0	1014	BARRAQUITO	Max.								26.9		26.5		and the second sec	25.6
			Min.	<u>51.2</u> 15.6	31.7	$\frac{32.1}{15.8}$		<u>33.1</u> 19.1	-	33,4	33.3 20.9	Company and the local division of the local	33.3			32.7
9	1915	LA ANGELINA		COLUMN STATE									and the second	18.3	16.6	18.4
"	1013	LA ANGELINA	Mean								27.2					25.8
			Max. Min.		32.2		<u>33.7</u> 17.0	33.7	38.1	a case' water and one of the	34.0			32.8		33.7
10	1816	JOSE CONTRERAS	-	COMPOSITION OF	and the second second	ATT 1. 140 - 14	and the second	17.8		200.00	19.3	19.2		16.6		17.6
10	1010	JOSE CONTRERAS	Mean Mean			COMPANY AND ADDRESS TO A				And in case of the local division of the loc	23.9			22.6		22.4
			Max. Min	26.7 13.7		28.4		28.9		The second s	29.7	and the second se		29.0		29.3
- 11	1917	LOS BOTADOS	THE PARTY OF THE PARTY OF	all statements	13.9	COLUMN DE LO DE	14.9		COLOR DO NO.		17.9	CONTRACTOR OF	CONTRACTOR OF	16.0		15.9
11	1017	LOS BOTADOS	Mcan Mau		19.1	<u>19.7</u>	<u>19.9</u>	COLUMN NO.	A REAL PROPERTY AND A REAL		20.8				19.3	20.2
			Max.	28.9 8.1		29.8		- and the second se			30.6	- de la de la della d		29.6	29.0	30.0
12	1920	EL NOVILLO	Min.	a distance	8.7	8.0	8.7				11.8			10.6	8.4	10.2
12	1030		Mean								20.6					19.8
			Max.								26.9					26.1
	1042	EL ACHACASE	Min.	A DESCRIPTION OF	10000	COLUMN TWO IS NOT	All				14.7				12.9	13.1
13	1043	EL AGUACATE	Mean								26.4			-		
			Max.								32.0		THE OWNER WATCHING IN COMPANY	other Designation of the local division of t		30.9
	1001	VALLE MUEVO	Min.	State of the local division of the local div	the second s	- Contraction of	TABLE AND ADDRESS		Contractor of		20.3			19.5		18.6
14	4301	VALLE NUEVO	Mean	5.8	5.7	6.5		9.5			9.5				6.2	8.0
			Max.						and the second se	and the second	16.5			the second s	and the local division of the local division	14.7
15	1000	CONTRACTOR OF A DESCRIPTION OF A DESCRIP	Min.	0.3	0.1	0.8	1.0	3.0	5.1	4.5		4.2	_	1.5	0.0	2.3
15	490Z	CONSTANZA	Mean								19.7					18.5
			Max.								28.6					29.0
	- 3° 1975 (* 1975 *	an hair a mar ann ann ann an an an an an an an an an	Min.	4.0	4.3	0.1	0.9	10.1	10.9	9.4	9.9	10.5	10.0	8.1	6.5	8.1

Table 8.2.4 Summary of Meteorological Data (2/2)

No.	Code	Name of Station	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec	Annual
1	401	JARABACOA	84.4	83.1	81.2	81.4	82.4	79.8	78.9	79.5	80.9	83.2	85.6	85.8	82.2
2	402	TAVERA	80.2	75.9	72.4	75.2	79.2	76.9	74.1	74.2	75.2	77.0	78.9	79.6	76.6
3	404	SANTIAGO-ISA	77.1	75.3	72.6	73.5	75.3	73,8	72.2	72.4	74.3	75.2	79.5	79.5	75.1
4	1801	SAN FCO. DE MACORIS	80,1	76.7	75.6	75.8	77.4	77.0	78.6	79.0	78.8	80.1	82.5	83.5	78.8
5	1802	JUMA-BONAO	83.8	83.3	80.9	81.1	80.1	81.2	81.1	82.9	82.0	84.5	85.3	85.4	82.6
6	1803	EL LIMON	88,0	85.5	•	79.9	80.6	81.9	84.0	88.0	87.4	86.6	88.2	91.0	-
7	1806	HATILLO - YUNA	-	•	•	-	-	-	-	•	-	•	-	•	-
8	1814	BARRAQUITO	83.6	83.3	80.4	79.4	82.5	76.8	83.7	83.7	83.8	84.4	85.2	84.8	82.6
9	1815	LA ANGELINA	84.4	81.3	80.5	80.6	82.2	80.7	82.1	82.7	82.6	83.6	84.9	86.0	82.6
10		JOSE CONTRERAS	86.6	86.8	86.2	85.2	87.1	83.7	82.4	83,1	84.3	85.0	86.9	86.8	85.3
11		LOS BOTADOS	70.6	72.2	73.6	81,3	76.0	75.2	76.6	96.1	79.1	86.7	77.7	68.6	77.8
12	1830	EL NOVILLO	93.1	92.0	89.1	87.1	86.3	87.1	85.6	87.3	86.9	86.8	88.3	90.0	88.3
13	1843	EL AGUACATE	88.4	88.6	87.2	86.2	84.6	85.1	85.0	84.9	86.0	84.5	85,9	91.8	86.5
14	the second se	VALLE NUEVO	-	-	•	-	-	-	•	-	•	-	-	•	•
15	4902	CONSTANZA	81.9	78.2	76.2	76.3	76.7	76.1	71.1	75.0	76.9	79.0	79.1	78.8	77.1

(2) Relative Humldity (%)

(3) Evaporation (mm)

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No.	Code	Name of Station	Jan	Feb	Mar	Apr	May	Jun	Jui	Aug	Scp	Oct	Nov	Dec	Annual
1	401	JARABACOA	83	78	118	110	129	130	147	132	\$20	111	82	76	1317
2		TAVERA	116	135	177	171	169	181	209	206	172	153	119	102	1910
3	A second second	SANTIAGO-ISA	130	131	208	198	203	230	219	211	233	175	134	128	2199
4		SAN FCO. DE MACORIS	93	100	143	151	146	166	157	139	137	127	84	87	1532
5	the second second	JUMA-BONAO	101	125	165	147	186	172	178	173	155	143	110	103	1756
6	and the second second	EL LIMON	101	102	131	148	150	114	125	127	115	91	96	•	•
7	A DESCRIPTION OF A DESC	HATILLO - YUNA	-	117	148	•	•	-	•	-	-	•	-	•	•
8		BARRAQUITO	91	101	₹30	133	160	140	150	142	127	113	. 92	78	1457
9		LA ANGELINA	116	131	169	183	173	176	169	202	177	158	121	100	1877
10		JOSE CONTRERAS	88	117	142	148	£27	164	174	143	137	134	111	119	1606
11		LOS BOTADOS	120	108	129	129	129	148	•	126	123	•	-	150	-
12	And in case of the local division of the loc	EL NOVILLO	141	176	166	164	181	185	173	173	172	154	156	149	1989
13	COLOR DOCUMENTS	EL AGUACATE	-	-	•	•	•	•	-	•	-	•	-	-	-
14	the second s	VALLE NUEVO	121	-	4	•	-	-	-	149	-	•	-	119	•
15	4902	CONSTANZA	92	74	102	91	96	103	124	107	138	127	103	123	1279

(4) Wind Velocity (m/s)

						and the second state and							
E T 1	12.1	N								Contraction and the	Contract of the state of the st	And in case of the local division of the loc	
i ian	i Fen	I Mari	I AND	I MIAV I	լ (ստ կ	1 161	6 6 110	Non-	1 (1)-4	E MAU	D AA	[A nous]	
	A						TUB	0.00				rannuar	
Carlo company	NAMES AND ADDRESS	COLUMN TRADE OF	Contraction in such as	ALCOHOL: NAME	CONTRACTOR OF THE OWNER, NAME	THE OWNER WAS ADDRESS OF	distant of the local division of the local d	ACC PROFESSION	A DECK OF A				
1 1 2	1 1 (1 6	17			1 1 1	\$ 0	1 0					
1 1.4	1.4	1.3	1.1	1	1 1.Z		F 5 11						
	Jan I.4	Jan Feb	Concernance construction and the second	Jan Feb Mar Apr 1.4 1.4 1.5 1.7	COLUMN CONTRACTOR DO DO NOT A TRACTOR	Care with care and a series of the series of	CONCRETE CARGE CONCRETE CONCRE	CONCRETE CONTRACTOR DE LA	COLORING CARDINE COLORING THE SOUTH OF CALL AND	and and a second a second a second of a second of a second	and and a second provide a	Concerning Concerning and the Concerning Con	

Table B.2.5 List of Hydrological Stations in the Yuna River Basin

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Γ	Dav	1	- 5		31	31	8	31	31	31	31	31	31	17	14	Ī	1	5	31	31	31	୍ଲ	30	30	14	31	31	5		14
ted	म्		، ۱		77	12	4	12	12	12	12	12	7	11	6	2	7	2	12	12	12	4	9	11	10	12	12	1	3	17
Collected	les.		10201	19/01	1988	1988	1982	1990	1988	1988	1988	1988	1986	1987	1988	8	1785	1988	1988	1988	1990	1981	1661	1987	1976	1988	1988	0001	2021	1990
Period of Data	Dav 1		╤┠╤		T	5	15	20		-	6	1		-	-	ł	77	-		1	ĩ	16	I	1	1	-	ľ) •	•	4
Deriv	Month		;			T.	4	12	~	80	12			11	F			F	F	1	4	2	I	1	6			ſ		2
	Vost 1		707	1955	1956	1968	1721	1982	1982	1983	1978	1980	1980	1979	1077		1881	1980	1980	1968	1961	1968	1968	1964	1957	1982	1002			1984
Conchener			S S	1071	4680	5130	1167	43	14	78	21	3	8	10	101	7/1	58	134	3	134	143	1160	2335	333	159	70			7	79
		<u> </u>	250	76	10	8	65	470	760	218	630	100	1002	009	220	100+	1165	660	630	8	130	56	28	8	8	18			33	17
-	Location	3	70°27	70° 15 ' 10 -	1 69° 54 ' 20 "	-6.67.69-0	- 20 - 13 - 50 -	- 36 - 06 -		- 66 0.06 =	12 004	47003113	- 12 0.02 +	10 01 1		51	8 70 37 58	3 70° 34 6	4 70 33 29	7-70°17.21	70°35	12	0 70° 7 45	47 70° 30° 51"	- 70 0 24			/0 18 . 7	0 69°55 36	47 47 20 4 21
	ַר <u>ן</u>	Latitud	18°53 * 30	18° 56 ' 50	01.01.61	19° 9' 10	. 05 0	104 0	1 24 0		3	- - - - -		1 1 2 0		18 ~ 52 ~ 51	18°55 •	18°53	18°53'1	0	- 13	- 11 .	000	010.4	, v			19°14.4	19° 1'	18°56'4
	Class			1	4	_			* •	• •	* *	*	+	, , ,	• t	2	4	4	4	·	- - -	- - - - - - -	·	┨┑	┝╢╍		₽ -	4	12	2
	Name of Station		LOS QUEMADOS	HATULO	VM I A RIVA		T OC DI ATANOS	LUS FLAIANUS	PIEDKA LOS VEGANOS	EL TOKTO	LOS AKKUES	ILUS GUAZAKUS	EL MECHE	ARROYON AKKIBA	ARROYON ABAJO	BLANCO	PINALITO	TREO	BT ANCO	DECTOR DE	NINIMUM STIFFS	DALACANES DANTERTO	× .		INARALUAU			LA BOCA	ABADESA II	LOS TRES PASOS
	eç O		100081	180002	1	[100001	12000/				1	182101	182201	182202	183001	183101	183102	102201	1070101	100401	100001	200201	concot	101021	185201	185502	185602	187002	188002
	No			6	 11 (*	- ^ -	→ ↓ ↓		9	~	~	9	10	7	72	13	4	i i		9 !		<u>8</u>		3	17	57	23	24	25	26

Table B.2.6 Summary of River Discharge Data (1/2)

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	Amual	18.46	88.79	9.31	31.39	84.77	17.08	90.86	267.10	38.01	95.21	241.23	43.40	36.47	200.96	17.48	4.44	26.80	2.26	1.12	17.63	0.53	6.36	16.87	3.86	2.75	13.63	1.15	0.32	1.50	0.12	0.67	2.91	0.31	1.12	4.26	0.56	5.79	18.02	3.73
h		24.37	94.24	11.41	41.15	112.60	20.00	100.83		46.69	113.45	282.81	54.18	44.35	180.49	21.52	4.35	-	3.16	1.66	20.80	0.58		8.80	3.92		~		0.27	1.05	0.13	0.44	11.0	0.33	1.08	2.86	0.47	6.30	15.48	3.97
1	Nov.	21.36	109.06	10.98	44.87	126.44	21.54	127.25	370.66	46.74	130.21	307.69	55.14	49.46	212.49	24.03	5.90	38.40	2.35	1.45	13.14	0.73	10.10	32.45	5.68	4.20	20.09	1.58	0.46		0.21	0.80	5.46	0.35	1.04	2.73	0.50	7.79	26.46	4.59
	ธี	20.24	109.32	10.16	33.98	101.44	17.63	88.84	275.26	38.16	99.69	258.40	47.64	40.76	252.62	18.22	4.61	24.10	2.22	0.97	6.74	0.42	6.04	7.63	4.69	3.00	10.80	1.38	0.43	1.89	0.18	0.83	2.15	0.35	1.71	5.79	0.87	6.60	17.91	4.42
	8	18.60	83.69	9.95	24.10	56.61	14.93	60.64	236.98	32.60	88.72	232.97	44.01	39.41	222.67	18.42	4.63	66.46	1.96	1.77	68.65	0.30	8.05	34.15	3.21	2.27	17.50	0.89	0.40	1.82	0.15	0.50	3.43	0.21	1.30	6.00	0.61	5.84	28.37	3.50
	Aug	16.70	139.12	7.31	28.26	94.32	14.99	84.06	260.95	32.43	84.50	246.09	38.09	37.46	392.87	17.78	3.93	28.82	1.93	0.55	3.82	0.35	5.70	28.56	3.29	1.86	17.96	0.67	0.32	3.00	0.09	0.56	3.38	0:30	1.52	7.75	0.81	5.73	~	3.31
- - -	Ę	13.05	56.85	7.24	24.97	61.20	14.91	74.42	171.06	38.14	67.77	151.31	34.81	25.11	120.94	14.51	2.90	17.31	1.85	0.64	1.28	0.48	5.18	6.78	3.66	2.02	13.50	0.97	0.21	1.56	0.08	0.37	1.77	0.23	1.15	4.84	0.77	5.28	17.28	3.54
ļ	шŗ	16.01	70.62	8.76	33.11	75.13	20.71	116.23	329.52	47.23	104.34	240.07	47.52	34.36	208.05	16.22			2.40	•		0.52		14.10	3.35	3.47	14.40	1.47	0.28	0.92	0.11	1.11	3.91	0.60	1.39	3.91	0.83	6.78	18.67	4.03
	Mav	24.27	107.66	12.03	45.24	123.30	21.84	155.52	411.68	48.92	142.60	348.89	49.82	46.78	257.69	17.72	5.14	33.62	1.90	1.23	6.26	0.56	6.43	14.31	3.49	3.33	13.60	1.38	0.43	2.14	0.16	1.06	5.77	0.32	1.45	6.32	0.50	7.03	20.55	3.76
	Apr	20.29	86.16	8.69	28.96	84.87	13.16	80.25	242.85	26.31	75.09	228.58	30.30	33.44	207.26	13.73	4.12	20.71	2.21	1.14	3.50	0.83	4.92	8.29	3.33	2.74	12.58	1.22	0.27	1.02	0.10	0.56	1.72	0.31	0.71	2.48	0.32	4.45	12.58	2.87
	Mar	13.65	81.38	6.26	18.75	49.06	11.99	56.30	186.93	24.82	65.53	172.19	30.53	29.68	143.95	14.37	4.14	16.21	2.36	0.62	3.48	0.51	6.10	11.26	3.89	2.52	11.48	1.04	0.19	0.82	0.07	0.42	1.57	0.12	0.54	2.45	0.33	3.63		2.82
• •	Feb	17.42	87.16	8.95	25.25	68.19	15.58	74.35	205.33	34.36	90.04	230.75	43.41	27.99	116.27	14.91	4.27	18.87	2.34	1.39	74.95	0.49	7.27	16.57	4.26	2.41	9.68	86.0	0.28	1.03	0.08	0.80	3.48	0.29	0.84		0.36	4.81	10.83	4.60
	Jan J	15.49	40.28	9.93	28.06	64.02	17.72	71.58	186.65	39.69	80.57	195.04	45.37	28.86	96.19	18.32	4.70	21.63	2.50	0.95	2.18	0.56	5.80	19.49	3.61	2.41	10.62	06.0	0.25	0.86	0.11	0.57	1.56	0.34	0.74	2.56	0.37	5.27	15.68	3.34
ļ	Item	Mean	Max.	MuN	Mcan	Max.	Min.	Mean	Max	N. N	Mean	Max	Min.	Mean	Max.	Min.	Mean	Max	Min.	Mean	Max.	Nii	Mean	Max.	Nin.	Mean	Max.	Min.	Mean	Max.	Min.	Mean	Max	Mi Mi	Mean	Max	Min.	Mean	Max.	Min.
	Name of Station	180001 ILOS QUEMADOS	, ,		HATILO			VILLA RIVA			180004 EL LIMON			180007 LOS PLATANOS			PIEDRA LOS VEGANOS			EL TORITO			181101 LOS ARROCES			LOS GUAZAROS			EL MECHE	·		182201 ARROYON ARRIBA			182202 ARROYON ABAJO			BLANCO		
	Code	180001			180002			180003			180004			.180007			180011			181001			101181			182001			182101			182201			182202			183001		
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Table B.2.6 Summary of River Discharge
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No.	Code	I Name of Station	Item	Jan	Feb	Mar	Apr	Mav 1	Jun	Jel Let	Aug 1	- By	т Ю О	NoV	- 280 D	Annual
4	183101	183101 PINALITO	Mean	0.61	0.52	0.30	0.46	1.19	1.26	0.50	0.57	1.42	1.15	1.03	9	0.80
			Max.	6.04	2.93	1.53	9.32	12.46	17.26	3.59	7.30	14.25	12.24	7.56	4.89	8.28
			Min.	0.19	0.15	0.14	0.14	0.27	0.14	0.14	0.12	0.18	0.26	0.29	0.21	0.19
15	183102	TIREO	Mean	4.56	4.09	3.12	3.19	4.61	3.37	2.66	3.00	4.28	4.10	5.46	4.71	3.93
			Max.	17.58	12.18	6.71	6.71	15.67	7 94	4.78	21.59	20.23	11.65	24.56	14.73	13.69
			Min.	2.70	2.81	2.33	3.37	2.65	2.44	2.29	2.20	2.27	2.68	3.11}	3.12	2.66
16	183201	BLANCO	Mean	0.27	0.20	0.13	0.13	0.17	0.15	0.11	0.18	0.19	0.30	0.16	0.16	0.18
			Max.	0.41	0.47	0.20	0.36	0.36	0.28	0.22	0.81	0.83	0.96	0.38	0.47	0.48
			Min.	0.21	0.10	0.10	0.10	0.10	0.10	0.07	0.09	01.0	0.13	0.22	0.23	0.13
17	184001	184001 MAIMON	Mean	3.51	4.48	3.22	3.95	7.50	4.45	3.35	5.62	6.53	4.44	5.31	4.89	4.77
			Max.	16.73	33.69	18.15		110.08	37.94	32.86	92.76	53.38	65.06	51.13	28.97	47.70
0.2960.3			Min.	2.06	2.03	1.70	1.71	2.14	1.84	1.62	1.66	2.27	1.73	2.09	2.31	1:93
81	135001	BAYACANES	Mean	3.51	3.87	3.66	4.89	7.14	3.84	2.73	3.29	2.98	4.10	5.10	5.81	4.24
			Max.	29.33	36.96	53.59	64.05	108.66	47.89	23.90	46.02	47.30	64.77	64.1.1	53.88	53.37
			Min.	1.52	1.42	1.16	1.33	1.87	1.81	1.46	1.49	1.33	1.44	1.65	1.87	1.53
19	185002	RANCHITO	Mean	8.48	9.72	8.98	15.03	21.06	9.20	4.85	6.10	8.67	9.97	15.57	12.77	10.87
			Max.	39.00	47.97	61.56	85.59	97.57	42.17	20.33	51.36	55.53	67.69	79.49	76.06	60.36
			Nin.	3.07	2.52	1.76	2.44	4.34	2.90	1.22	1.20	1.62)	1.63	3.30	2.44	2.37
20	185003	185003 [LA BUA	Mean	33.36	37.66	29.14	37.74	69.74	36.90	26.05	29.19	28.59	34.70	52.60	43.11	38.23
		-	Max	105.57	124.57	98.08	143 04	211.46	123.58	74.11	110.37	124.15	126.69	178.60	142.67	130.24
			Min.	18.71	17.87	14.54	14.40	22.45	17.65	13.97	13.76	17.58	15.75	20.10	20.44	17.27
51	185101	NARANJAL	Mcan	1.04	1.31	1.24	1.84	3.97	1.33	0.85	0.91	1.35	1.40	2.33	1.76	19.1
			Max.	2.38	9.28	17.18	28.14	40.22	10.68	6.64	6.04	15.73	13.67	16.52	20.71	15.60
			Min.	0.74	0.68	0.60	0.58	0.72	1.08	0.67	0.61	0.61	0.61	0.69	0.00	0.71
22	185201	185201 RINCON	Mean	11.35	9.43	7.68	9.28	14.75	9.28	7.63	7.70	8.62	9.89	12.71	13.98	10.19
			Max.	44.28	75.92	35.09	75.00	71.35	30.14	27.22	58.88	49.56	63.52	77.07	65.08	56.09
			Min.	5.92	5.04	4.46	4.45	6.68	5.58	4.89	4.61	4.98	5.75	6.30	6.48	5.43
.23	185502	SANTA ANA	Mean	1.33	1.02	0.82	1.07	1.50	0.75	0.51	0.54	0.80	1.62	2.40	0.93	1.11
			Max.	5.75	5.21	3.54	9.92	10.51	4.SI	2.66	2.81	4.23	12.98	14.96	2.50	6.63
			Mun.	0.52	0.66	0.44	0.33	0.30	0.27	0.27	0.18	0.27	0.34	0.43	0.48	0.37
24	185602	185602 LA BOCA	Mcan	2.05	1.72	1.22	0.87	2.59	1.26	0.71	0.90	1.34	1.31	4.52	2.93	1.79
			Max.	18.59	11.34	8.30	10.18	26.35	15.41	5.13	7.87	14.23	14.34	38.40	20.22	15.86
			Min.	0.41	0.62	0.41	0.33	0.29	0.34	0.27	0.17	0.20	0.14	0.55	0.66	0.37
25	187002	187002 ABADESA II	Mean	2.46	2.61	2.82	3.66	9.22	10.79		10.57		8.76	6.84	3.99	6.66
			Max.	12.96	18.54	30.24	46.64	72.10	95.84		100.86	117.87	102.28	72.85	31.36	65.42
			Min.	1.58	1.38	1.17	1.08	1.70	2.81	2.55	2.75	3.11	2.95	2.50	1.97	2.13
78	188002	188002 LOS TRES PASOS	Mean	1.05	1.91	1.09	1.13	1.31	1.04	1.31	2.20	5.14	2.20	1.24	2.07	1.81
			Max.	3.96	36.64	5.27	14.92	80.46	21.47	10.69	67.39	209.22	52.83	19.53	29.95	46.03
			Min.	0.49	0.49	0.57	0.34	0.28	0.44	0.38	0.43	0.49	0.68	0.35	0.59	0.46

Table B.2.7	Summary	y of Spring	i Discharge Da	ıta
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No.	Name of Spring	Period of Data Collected	Number of Data
	Guaraguao Main Canal	10/1/75 - 18/7/94	110
1	Guaraguao Second Canal	17/2/76 - 12/11/91	14
3	Cercado	17/2/76 - 25/4/76	10
4	Laguna Cristal	27/3/76 - 25/4/76	5

Table B.2.8 Summary of Suspended Sediment Data

No.	Station Code	Name of Station	Period of Data Collected	Number of Data
1	180003	Villa Riva	8/4/80 - 26/3/84	18
2	180004	El Limon	20/1/80 - 25/3/84	25
3	187002	Abadesa	23/5/78 - 20/11/85	35

Table B.2.9 List of Discharge Measurement Sites in the Study Area

No.	Location	Code	Remark
1	Laguna Cristal	LG	Natural river
2	Lagunita Cristal	LP-I	Irrigation canal 1
3	Lagunita Cristal	LP-II	Irrigation canal 2
4	Lagunita Cristal	LP-III	Drainage canal
5	Lagunita Cristal	LP-IV	Irrigation canal 1
6	Laguna Cueva	LC-I	Irrigation canal 1
7	Laguna Cueva	LC-II	Irrigation canal 2
8	Caño Cercado	CC	Small Stream
9	Caño Barraco	СВ	Small Stream
10	Drenaje Cascarilla (road bridge)	DC-I	Main drainage canal (upper)
11	Drenaje Cascarilla (Los Caprices)	DC-II	Main drainage canal (lower)
12	Cueva Guaraguao	CG-I	Main stream
13	Cueva Guaraguao	CG·II	Irrigation canal
14	Rio Payabo (Represa)	RP-I-A	Main stream
15	Rio Payabo (Cano Ponton)	RP-I-B	Intake site of Ponton irrigation cana
16	Rio Payabo (Puente La Verde)	RP-II	Road bridge
17	Rio Payabo (Desembocadura)	RP-III	Confluence at Yuna river
	Caño Ponton	PT	Ponton irrigation canal

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Table B.4.1 Summary of Climate Condition in the Study Area

Station 1814 Barraquito : Data Period 1975 - 1993

Teen		1an	Feb -	Mar	Apr	Mav	Jun	Jul	Aug	es S	ğ	Nov	282	Amnuai
		16 111	07.7	118.0	1677	314.61	184.9	197.01	209.1	162.4	178.2	192.4	129.5	2065.7
Kannau (nun) Maathu Distribution (%)	(%) unition	\$ 55%	4 70%	5.71%	8.12%	15.23%	8.95%	9.54%	10.12%	7.86%	8.63%	9.31%	6.27%	100.00%
NIOLULY LINU			Leh L	Mar	Δnr	Mav	Inn	luľ	Aug	ŝ	ğ	Nov	Dec	Annual
		12.5	22 6	676	254	2611	26.9	26.9	26.9	27.0	26.5	25.5	24.1	25.6
Montary	Nou:	205	24.8	25.5	301	26.8	28.0	27.7	27.7	27.6	27.0	26.3	25.3	30.1
Mean	Min.	215	000	22.7	23.5	25.2	25.5	26.2	26.3	26.31	25.9	24.7	23.2]	20.9
	Mean	312	31.7	32.1	32.8	33.1	33.5	33.4	33.3	34.0	33.3	32.5	31.6	32.7
	May	32.5	34.0)	34.5	34.5	34.3	35.0	35.5	35.8	38.0	35.5	38.0	39.0	39.0
WEAN.			10.05	24.5	29.5	32.0	32.0	32.0	32.0	33.0	32.0	31.0	29.5	24.5
فالمعدادات	- Nicoso	15.61	151	15.8	17.2	19.11	20.7	20.8	20.9	20.5	20.1	18.3	16.6	18.4
MOULULY	Mose	175	17 51	20.5	19.0	20.5	21.8	21.5	22.0	21.5	21.0	20.0	18.0	22.0
INUT.	Men	811	13.5	115	12.0	15.2	19.5	20.0	20.0	20.0	18.0	15.0	14.0	11.5
	LVALL.	0.14		0.0%	811	84.3	81.3	81.1	82.9	82.0	84.5	85.3	85.4	83.0
Kelauve	Mcan	0.00		0 1	04.7	0 5	808	88.0	96.2	90.4	97.1	9.66	96.0	97.1
Humary	MAX.	7.72	200	75.0	707	73.8	73.5	73.8	72.6	74.0	79.5	78.4	78.3	70.7
(%)	1.1.1.1.1.	5 N	001	120.6	1331	160.2	140.4	150.0	141.8	127.0	113.0	91.5	77.8	1456.8
Evaporanon	WCan	\$1.4 20.00		144.01	15051	1471	159.6	1793	159.9	153.3	123.0	107.7	87.4	179.3
(uu)	Max.	0.72		200	0.20	115.01	1010	9 0 0 1	1 701	5 X0	101 4	16 11	70.2	70.2
	Min.	78.1	86.1	7.011	2.02	140.41	+.177	177.0					-	
Wind Velocity [Mcan	Mcan	1.4	1.4	1.5	1.7	1.3	1.2	1.1	0.1	1.2				
Monthly	Max	2.1	2.2	2.3	2.5	2.1	1.8	2.0	1.6	1.7	1.5	1.6	1.9	
Mean (m/s)	Min.	0.8	0.8	0.6	6.0	0.4	0.6	0.2	0.2	0.7	0.7	0.4	0.5	0.2

N-	Code	Name of Station		Thiesen Pol	ygon Area (k	un2)	and an operation of the second se
INO.		14attie of Station	Villa Riva	ElLimon		Confluence	Payabo
1	1802	JUMA BONAO	757	757	0	757	0
2		JIMA RINCON	635	635	0	635	0
3		BARRAQUITO	156	606	75	418	194
4		LA CEIBA RIO BLANCO	405	405	0	405	0
5		LA CABILMA	714	714	144		199
6	1847	S.F.DE MACORIS (MET)	875	875	0	875	0
$\frac{1}{7}$		Construction of the local division of the lo	479	479	0	479	0
8		the same second s	659	659	0	659	0
		Total	4680	5130	219	5101	393

Table B.5.1 Selected Rainfall Gauge Station for Thiesen Polygon

Table B.5.2 Summary of Estimated Rainfall at Selected Stations1958 to 1993

						warm in source at	even constants	and the second second			a designed and the	the second s	STREET, STREET, STREET, ST		a second second
No	Code	Name of Station	Jan	Feb	Mar	Apr	May		Jul						Annual
-		JUMA BONAO	101.2	97.6	125.2	197.0	270.1	134.3	164.3	169.5	156.2	190.0	2198	137.8	1962.9
F-		JIMA RINCON	75 9	823	771	107.7	185.7	105.1	102.0	134.8	103.5	123.4	139.5	100.9	1337.9
			110.0	100 5	120.1	1516	2637	187 5	1916	203.2	162.1	166.3	189.5	152.3	2001.5
3	1814	BARRAQUITO LA CEIBA RIO BLANCO	170 4	164.7	101 9	239.0	221 9	203.9	224 0	259.0	272.6	285.3	276.0	218.7	2828.4
			1/8.0	104.7	1104.0	230.3	321.7	120 2	2001	216 3	168.9	160.1	1776	150.3	1975.9
				108.2	110.5	100.1	239.0	110.2	116.0	144.0	1111 2	121 5	156.2	124 0	1411.1
6	1847	S.F.DE MACORIS (MET)	84.6	74.2	73.5	102.0	183.6	118.0	110.9	144.9	111.4	121.5	120.2	124.0	1404.2
7	1850	LA VEGA (MET)	83.0	71.7	92.4	151.4	201.2	89.3	96.9	109.4	111.0	144.0	138.4	119.9	1404.2
8	1851	MOCA (MET)	68.5	62.5	67.8	103.0	162.3	71.6	<u> 91.8</u>	93.0	101.6	126.3	130.0	109.3	1194.4

Table B.5.3 Estimated Annual Rainfall Pattern

 $\mathbf{\hat{x}}$

No.	Calculation Point	Jan	Feb	Mar				Jul	Aug					Annual
1	Villa Riva	95.7	91.1	100.3	144.2	222.9	127.2	141.4	159.3	140.6	157.5	174.4	133.2	1687.8
2	El Limon	97.0	91.9	102.1	145.1	226.5	132.5	145.8	163.1	142.5	158.2	175.7	134.9	1715.4
3	Abadesa	106.4	105.6	113.8	151.3	261.0	176.1	197.2	211.8	166.6	162.2	181.7	151.0	1984.7
4	Payabo Confruence at Yuna	96.7	92.1	101.7	144.9	226.1	131.7	145.8	163.3	142.6	158.0	175.3	134.7	1712.9
5	Payabo Basin	107.4	104.4	115.3	151.8	261.6	178.7	195.9	209.8	165.5	163.2	183.5	151.3	1988.6

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Table B.5.4 Rainfall Probability Analysis

			1814 BARRAQUITO				
	Annual	Maximum	Maximum		Continuous days	Continuous days without Rainfall (days)	(days)
F[%]	Rainfall	24 hr Rainfall	3 Day Rainfall	less than	less than 0.1 mm	less th	less than 5.0 mm
_	(mm)	(mm)	(mm)	Rainy Season	Dry Season	Rainy Season	Dry Season
0.50	1262.2	233.1	336.5	12	30	21	51
1.00	1321.1	215.2	308.1	12	27	20	48
2.00	1388.7	197.2	280.1	11	24	61	44
5.00	1496.4	173.0	243.4	IO	21	18	39
10.00	1599.1	154.0	215.4	ro	18	17	35
20.00	1733.0	133.7	186.5	٥	16	16	31
50.00	2021.1	102.1	143.4	~	12	13	24
			1811 Abadesa				
	Annual	Maximum	Maximum		Continuous days	Continuous days without Rainfall (days)	(days)
F[%]	Rainfall	24 hr Rainfall	3 Day Rainfall	less than 0.1 mm	0.1 mm	less th	less than 5.0 mm
	(mm)	(mm)	(mm)	Rainy Season	Dry Season	Rainy Season	Dry Season
0.50	907.2	143.7	212.3	29	67	29	88
1.00	980.7	136.5	203.4	26	58	27	78
2.00	1062.3	128.9	193.8	23	50	25	20
5.00	1186.8	117.9	179.6	5	40	22	9
10.00	1299.9	108.5	167.3	17	33	20	52
20.00	1440.1	97.7	152.8	14	56	18	44
50.00	1718.1	78.6	9 2 6 1	¢,	0	-	

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Table B.5.5 Water Balance in the Yuna River Basin

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-	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	ğ	Nov	2 D	Annual
						Mean Discharge (m3/s)	rge (m3/s)			a da			
1958-1978	71.98	60.41	58.93	86.18	130.57	100.24	74.34	108.64	62.12	87.40	108.22	78.66	84.65
ä	55.55	62.32	67.71	133.13	325.35	219.96	128.48	166.66	45.22	103.77	184.45	80.96	131.13
1661-8861	77.39	121.34	44.76	55.86	154.21	115.29	54.35	60.85	58.41	88.65	165.28	110.19	92.21
1958-1991	71.58	74.35	56.30	80.25	155.52	116.23	74 42	84.06	60.64	88.84	127.25	100.83	90.86
						Runoff (mm)	mure)						
1958-1978	41.19	31.23	33.73	45.41	74.73	55.52	42.54	45.67	34,41	50.02	59.94	57.16	570.44
1979-1982	31.79	32.21	38.75	73.73	186.20	121.82	73.53	95.38	25.04	59.39	102.16	46.33	883.61
1983-1991	44.29	62.72	25.62	30.94	88.25	63.85	31.10	34.82	32.35	50.74	91.54	63.06	621.38
1958-1991	40.97	38.43	32.22	44.44	89.01	64.37	42.59	48.11	33.59	50.84	70.48	57.72	612.23
						Mean Rainfall (mm)	all (mm)						
1958-1978	83.0	85.8	98.5	140.5	192.2	123.4	139.1	153.1	131.2	145.4	164.4	138.8	1595.5
1979-1982	108.0	109.6	97.8	1.24.1	357.8	151.4	169.3	236.3	156.5	145.4	187.0	154.2	2027.4
1983-1991	112.8	101.3	95.3	131.8	203.4	131.4	139.0	146.3	161.7	208.0	199.7	116.3	1747.1
- 16	95.7	91.1	100.3	144.2	222.9	127.2	141.4	159.3	140.6	157.5	174.4	133.2	1687.8
,					1 · ·	Runoff Coefficient (%)	cient (%)						
1958-1978	49.6%	36.4%	34.2%	32.3%		45.0%	30.6%	29.8%	26.2%	34.4%	36.5%	41.2%	35.8%
1979-1982	29.4%	29.4%	39.6%	47.9%	52.0%	80.4%	43.4%	40.4%	16.0%	40.8%	S4.6%	30.0%	43.6%
1983-1991	39.3%	61.9%	26.9%	23.5%	43.4%	48.6%	22.4%	23.8%	20.0%	24.4%	45.9%	54.2%	35.6%
1958-1991	42.8%	42.2%	32.1%	30.8%	39.9%	50.6%	30.1%	30.2%	23.9%	32.3%	40.4%	43.3%	36.3%
					El Limo	El Limon (Catchment Area 5130 km2)	t Area 5130	km2)					
Period	Jan	Feb	Mar	Apr	May	Jun {	Jul	Aug	Sep	or O	Nov	De De	Annual
						Mean Discharge (m3/s)	rge (m3/s)						
969-1978	75.86	68.11	63.88	68.03		48.01	46.18	66.44	77.37	94.77	119.53	126.54	79.12
1979-1982	63.21	69.71	63.95	124.95	286.62	203.84	126.06	160.30	156.70	113.99	173.16	83.77	135.52
1982-1993	90.03	118.75	67.65	67.92	146.79	127.50	69.54	80.24	78.68	100.32	127.77	109.27	98.70
1969-1993	80.57	90.04	65.53	75.09	142.60	104.34	67.77	84.50	88.72	69.66	130.21	113.45	95.21
						Runoff (1	(uuu)						
1969-1978	39.60	32.12	33.35	34.37	49.48	24.26	24.11	34.69	39.09	49.48	60.39	66.07	486.40
ន	33.00	32.87	33.39	63.13	149.65	102.99	65.81	83.70	79.18	59.52	87.49	43.74	833.10
1982-1993	47.00	56.00	35.32	34,32	76.64	64.42	36.30	41.89	39.75	52.38	64.56	57.05	606.77
1969-1993	42.07	42.46	34.21	37.94	74.45	52.72	35.38	44.12	44.83	52.05	65.79	59.23	585.29
						Mean Rainfail (mm)	ail (mm)						2.37
1969-1978	79.9	101.1	101.7	150.7	182.5	105.9	133.5	167.3	139.1	163.3	169.3	151.1	1645.4
1979-1982	108.8	111.5	97.0	154.5	366.7	157.4	172.8	241.5	155.1	146.9	186.8	158.0	2057.2
2	116.5	94.1	107.0	147.5	237.3	130.8	140.5	146.0	155.5	184.4	188.7	113.4	1761.8
1969-1993	100.7	99.7	103.3	149.9	236.1	125.1	142.9	169.8	148.9	170.0	180.6	135.6	1762.5
						Runoff Coefficient (%)	cient (%)						
1969-1978	49.6%	31.8%	32.8%	22.8%	27 1%	22.9%	18.1%	20.7%	28.1%	30.3%	35.7%	43.7%	29.6%
1979-1982	30.3%	29.5%	34.4%	40.9%	40.8%	65.4%	38.1%	34.7%	51.0%	40.5%	46.8%	27.7%	40.5%
1982-1993	40.3%	59.5%	33.0%	23.3%	32.3%	49.2%	25.8%	28.7%	25.6%	28.4%	34.2%	50.3%	34.4%

Table B.5.6 Probability Analysis of Mean and Low Flow at Villa Riva and El Limon

(m3/s)

			Villa Riva	Riva			ELL	El Limon	
Return	F[%]3	Mean	an	Mini	Minimum	Me	Mean	Mini	Minimum
Period		Before	After	Before	After	Before	After	Before	After
1/200	0.50	29.07	46.90	2.15	8.23	48.21	63.43	1.43	4.27
1/100	1.00	32.89	50.42	2.56	9.06	50.26	65.59	2.25	5.59
1/50	2.00	37.30	54.46	3.08	10.07	52.62	68.21	3.20	7.19
1/20	5.00	44.40	60.89	4.03	11.78	56.35	72.70	4.76	9.91
1/10	10.00	51.25	67.00	5.10	13.55	16.92	77.33	6.29	12.72
1/5	20.00	60.29	74,95	6.75	16.05	64.52	83.90	8.34	16.68
1/2	50.00	80.15	91.97	11.42	22.19	74.38	100.10	12.98	26.39

Table B.5.7 Runoff Pattern at Abadesa From 1972 to 1979

Item	Jan.	Feb.	Mar.	Apr.	May	Jun.	Jul	Aug.	Sep.	Oct O	Nov.	Dec.	Amual
Discharge (m3/s)	2.400	2.485	3.867		8.812	17.725	10.041	14.616	17.530	12.866	10.796	5.085	9.269
Runoff (mm)	29.4	27.5	47.3		107.8	209.8	122.8	178.8	207.5	157.3	127.8	62.2	1334.7
Rainfall (mm)	107.7	129.2	136.2		225.7	188.6	207.2	256.1	199.3	204.0	196.1	201.0	2233.0
Runoff Coefficient (%)	27.2%	21.3%	34.7%	31.3%	47.7%	111.2%	59.3%	69.8%	104.1%	77.1%	65.2%	30.9%	59.8%

Table B.5.8 Estimated Runoff Pattern at the Diversion Point of the Payabo River

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Item	Jan.	સુર સુર	Mar.	Apr.	May	Jun.	Jul.	Aug.	Sep.	ъ Ост	Nov.	Х Х С	~
Discharge (m3/s)	3.356	3.338	5.469	7.167	12.960	25.181	14.006	21.036	24.358		15.974	7.267	
Runoff (mm)	26.1	23.4	42.5	53.8	100.6	189.2	108.7	163.3	183.0		120.0	56.4	
Rainfall (mm)	103.7	119.4	132.6	186.5	228.5	184.4	199.0	253.6	190.6	200.4	199.7	197.7	2196.0
Runoff Coefficient (%)	25.1%	19.6%	32.0%	28.9%	44.0%	102.6%	54.7%	64.4%	96.0%		60.1%	28.5%	

Table B.5.9 Probability Analysis of Mean and Low Flow for the Payabo River

		· · · .	•		(m3/s)
	COMPLEX STREET, ST	Aba	desa	Diversion po	int at Payabo
Return	F[%]	Mean	Minimum	Mean	Minimum
Period		Discharge	Discharge	Discharge	Discharge
1/200	0.50	3.82	0.08	5.46	0.21
1/100	1.00	4.13	0.13	5.90	0.30
1/50	2.00	4.49	0.19	6.42	0.41
1/20	5.00	5.12	0.30	7.31	0.59
1/10	10.00	5.75	0.40	8.22	0.76
1/ 5	20.00	6.64	0.53	9.49	0.98
1/2	50.00	8.80	0.85	12.57	1.46

Table B.5.10 Previous Spring Discharge Data

No.	Name of Spring	Period of Data	Number	Dis	charge (m	3/s)
		Collected	of Data	Mean	Max.	Min.
<u> </u>	Guaraguao Main	10/1/75 - 18/7/94	110	1.787	5.019	0.701
2	Guaraguao Second	17/2/76 - 12/11/91	14	0.672	2.123	0.219
3	Cercado	17/2/76 - 25/4/76	10	0.596	1.141	0.363
4	Laguna Cristal	27/3/76 - 25/4/76	5	0.567	0.597	0.54

Table B.5.11 Result of Spring Water discharge Measurement in the Study Area

Year	Month	Date	Guaragao	La Cucva	Lagunita Cristal	Laguna Cristal	Caño Cercado	Source
1994	Aug	19	2.128	0.382	1.481	0.428	0.624	INDRHI
	8	6	1.485	0.511	,			•
		16	1.429	0.654	1.156	0.446	0.538	
!		28	1.268	0.936	1.449	0.684	0.547	
]	ğ	11	1.808	0.913	1.567	0.435	0.495	
	Nov	17	1.510	0.678	2.062	0.541	0.670	2
	р В	6	2.246	0.598	2.353	0.756	1.048	F
1995	Jan	10	1.138	0.373	1.750	0.499	0.639	:
	 Fc5 F	5	1.496	0.400	0.820	0.473	0.895	JICA team
	4	10	1.236	0.323	0.633	0.547	0.871	*
		13	1.694	0.314	0.821	0.519	0.969	2
		16	1.629	0.323	0.654	0.546	0.831	5
	ا محمد	20		0.279	0.760	0.501	0.739	1
	8	23	1.626	0.309		0.536	0.952	1
!		27	1.688	0.356		0.510	0.766	*
	Mar	7	1.535	0.355	0.777	0.506	0.838	2
	1	•	1.863	0.286	0.742	0.528	0.752	E
		- 6	•••••	•	•	0.551	. •	1
Å	Average	- .	1.611	0.470	1.216	0.530	0.761	
Portion for Guraguao	for Gura	enao	100.0%	29.2%	75 50%	22 0%	700 17	

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							unit: m³/s
	Date		Time	Main Canal	Sub Canal	Total	Remark
18	Aug.	94	15:47	1.349	0.277	1.626	
19	Aug.	94	7:01	1.263	0,318	1.581	a Carda der bie fersten en senten de senten per propriet de la pro
19	Aug.	94	4:53	1,458	0,161	1.619	
20	Aug.	94	7:00	1.739	0.234	1.973	
20	Aug.	94	4:52	1.564	0.486	2.050	
21	Aug.	94	7:10	1.289	0.391	1.680	
21	Aug.	94	3:41	1.320	0.298	1.618	
22	Aug.	94	7:24	1.284	0.392	1.676	and the second
22	Aug.	94	4:59	1.209	0.386	1.595	
23	Aug.	94	5:22	1.302	0.260	1.561	
25	Aug.	94	7:03	1.351	0.324	1.675	
26 28	Aug.	<u>94</u> 94	•	1.144	0.324	1.468	
31	Aug. Aug.	94	6:42	1.739	0.486	2.050	
<u> </u>	Sep.	94	7:00	1.356	0.073	1.429	
1	Sep.	94	5:06	1,119	0.243	2.008	
2	Sep.	94	7:00	1.089	0.270	1.394 1.407	
2	Sep.	94	5:00	1.739	0.221	1.407	
3	Sep.	94	7:00	1.198	0.407	1.605	
3	Sep.	94	5:00	1.173	0.250	1.423	
4	Sep.	94	7.00	1.211	0.292	1.503	
4	Sep.	94	5:00	1.224	0.266	1.491	
7	Sep.	94	7:05	1.302	0.218	1.520	
7	Sep.	94	5.00	1.414	0.248	1.662	a an
8	Scp.	94	7:01	1.741	0.211	1.952	
8	Sep.	94	5:00	1.373	nil	1.373	Sub canal is closed
9	Sep.	94	7:00	1.643	nil	1.643	due to gate construction
9	Sep.	94	5:00	1,675	nil	1.675	and the second
10	Sep.	94	7:00	1.518	nil	1.518	
10	Sep.	94	5:00	1.443	nil	1.443	
11	Sep.	94	5:00	1.586	nil	1.586	
14	Sep.	94	7:00	0.497	0.646	1.143	
16	Sep.	94	7:09	1.493	0.385	1.878	
16	Sep.	94	17:00	1.364	0,388	1.752	
17	Sep.	94	7:23	1.534	0.366	1.900	and the second secon
17	Sep.	94	17:10	1.260	0.247	1.507	an a' fan de 'N fan de one a ser an ar gener de fan de 'n de an an an an ar ar
18	Sep.	94	7:19	1.402	0.270	1.672	
18	Sep.	94	17:00	1.193	0.348	1.541	······································
<u>19</u> 19	Sep.	94	7:07	1.309	0.353	1.662	
20	Sep.	<u>94</u> 94	17.00	1.443	0.213	1.656	
20	Sep. Sep.	<u>94</u> 94	7:14	1.328 1.306	0.190	1.518	
20	Sep.	<u>94</u> 94	17:00	1.306	0.226	1.532	· · · · · · · · · · · · · · · · · · ·
23	Sep.	. 94	17:00	1.424	0.029	1.367	
24	Sep.	94	17:00	1.346	0.253	1.599	
25	Sep.	91	17:00	1.641	0.426	2.067	
26	Sep.	94	17:00	1.494	0.448	1.942	ر میں میں میں بنیان کر ان ایک میں میں اور
27	Sep.	94	17:00	1.752	0.652	2.404	
28	Sep.	91	17.00	1.481	0.429	1.910	
29	Sep.	94	17.00	1.295	0.418	1.713	an an faith an
30	Sep.	94	17:00	1.284	0.344	1.628	میں بنیابر میں میں بر خاصی <u>سال کی کر پر سرح میں میں اور کا کا اس</u> ل کر اور میں اسال کر ا
1	Oct.	94	17.00	1.114	0.316	1.430	
2	Oct.	91	17.00	1.255	0.256	1.511	a ann an a
3	Oct.	94	17.00	1.043	0.305	1.348	- Marinia (m. 1920), and a summary of the last and an and a statement of the same of the s
4	Oct.	94	17:00	1.092	0.321	1.413	

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Table B.5.12 Result of Discharge Measurement at Guaraguao (1/3)

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							unit: m ³ /s
ina, manakati kanakara kati	Date		Time	Main Canal	Sub Canal	Total	Remark
5	Oct.	94	17:00	1,135	0.271	1.406	
6	Oct.	94	17:00	1.083	0.304	1.387	<u>,</u>
7	Oct.	94	17:00	1,285	0.311	1.596	
8	Oct.	94	17:00	1.304	0.305	1.609	
<u> </u>	Oct.	94	17:00	1.204	0.237	1.441	an a
11	Oct.	94	17:00	1.540	0.322	1.862	
14	Oct.	94	17.08	1.363	0.320	1.683	
15	Oct.	94	17:00	1.456	0.275	1.731	and a subscription of the
17	Oct.	94	17:00	1.446	0.315	1.761	an a
18	Oct.	94	17:00	1,951	0.000	1.951	
19	Oct.	94	17:00	1.226	0.412	1.638	
20	Oct.	94	17:00	1.675	0.321	1.996	
21	Oct.	94	17:00	1.397	0.265	1.662	
22	Oct.	94	17:00	1.459	0.260	1.719	an na an a
23	Oct.	94	17:00	1.398	0.229	1.627	an a
25	Oct.	94	17:00	1.777	0.123	1,900	
28	Oct.	94	17:00	1.614	0.222	1.836	
29	Oct.	94	17:00	1.290	0.222	1.523	
30	Oct.	94	17:00	1.423	0.233	1.694	
30	Oct.	94	17:00	1.507	0.129	1.636	n a mar ann an
$\frac{31}{1}$	Nov.	94	17:00	1.465	0.268	1.733	
2	Nov.	94	17:00	1.324	0.323	1.647	
3	Nov.	94	17:00	1.324	0.323	1.486	
4	Nov.	94	17:00	1.321	0.124	1.445	a a an
5	Nov.	94	17:00	1,282	0.124	1.479	
6	Nov.	94	17:00	1.341	0.189	1.530	· · · · · · · · · · · · · · · · · · ·
	Nov.	94	17:00	1.663	0.164	1.827	
- 9	Nov.	94	17:00	1.450	0.104	1.556	
12	Nov.	94	17:00	1.450	nil	1.293	
12	Nov.	94	17.00	1.581	0.375	1.956	
<u>13</u> 14	Nov.	94	17:00	1.569	0.375	1.855	
15	Nov.	94	17:00	1.350	0.257	1.607	
15	Nov.	<u> </u>	17:00	1.299	0.237	1.598	
10	Nov.		17:00	1.577	0.309	1.886	
17	Nov.	94	17:00	1.304	0.309	1.546	
18	Nov.	94	17.00	1.344	0.242	1.634	
20	Nov.	94	17:00	1.387	0.230	1.620	
20	Nov.	94	17:00	1.587	0.233	1.820	
TANK A PROPERTY AND INCOME.		CAPIER PROPERTY AND	CONTRACTOR OF TAXABLE PARTY.	1.298	AND DESCRIPTION OF THE OWNER OWNER OF THE OWNER	COMPANY AND A TRADE OF A DESCRIPTION	
23	Nov.	94	17:00	1.298	0.250	1.548	
28	Nov. Nov.	94	17:00	And the second s	0.280	1.556	
29	A DESCRIPTION OF A DESC	94	17:00	1.188	0,298	1.486	
30	Nov.	<u>94</u> 94	17:00 17:00	1,295 1,289	0.269	1.564 1.565	
2	Dec	<u>94</u> 94		Construction and the second se	0.276	the second s	
- 2 - 3	Dec Dec	94 94	17:00	<u>1.597</u> 1.105	0.304	1.901	
	a di Circletta da anti-	<u>94</u> 94	17:00	1.429	0.292	1.397	
5	Dec Dec	94 94	17:00	1.429	0.257 0.283	1.686 1.728	
6		<u>94</u> 94	17:00	2.059	0.283	2.365	
7	Dec	94	17:00	1.966	0.300	2.365	
	Dec	<u>94</u> 94	17:00		0.229	and the second se	
8	Dec	94	17:00	1.404 1.380	0.242	1.646	
	Dec	94	Contractory of the Roll of the Contractory	the design of the second data of	And the second s	1.668	
The second se	Dec	94	17:00	1.074	0.304	1.378	
14	Dec	and the second s	17:00	1.482	0.332	1.814	
15	Dec	94	17:00	1.381	0.261	1.642	
16	Dec	94	17.00	1.414	0.274	1.688	1

17 18 19								unit: m ³ /s
18		Data	CONTRACTOR OF TAXABLE	Time	Main Canal	Sub Canal	Total	Remark
18		Date	94	17:00	1.159	0.190	1.349	
		Dec	and the second se	17:00	1.130	0.318	1.448	a na an
1 15		Dec	<u>94</u> 94	17:00	1.323	0.262	1.585	an ang ang ang ang ang ang ang ang ang a
A COMPANY AND A DESCRIPTION OF A DESCRIP	a subscription of the local division of the	Dec	94	17:00	1.371	0.250	1.621	
20	and the second se	Dec	<u>94</u> 94	17.00	1.383	0.298	1.681	and the product when produce the product of the second second second second second second second second second s
21	A 1997	Dec	<u>94</u> 94	17:00	1.365	0.292	1.758	a gy ny amin' dia kaominina minina mpikambana amin'
27	and the second	Dec	94	17:00	1.398	0.280	1.678	and have a subject of the subject of
2	the second s	Dec	94	17:00	1.395	0.376	1.771	and all the Constant of the Co
2:	1. X. M. A. C. W.	Dec	94	17:00	1.608	0.000	1.608	an a
2		Dec Dec	94	17:00	1.338	0.194	1.532	
2		and the owner of the local division of the l	94 94	17:00	1.311	0.284	1.595	
3	the second s	Dec Dec	94	17:00	1.256	0.263	1.519	
3	COLUMN TRAVEL TRAVE	Dec	95	17:00	1,181	0.347	1.528	میں باری باری اور
2	ALC: NOT THE OWNER OF THE OWNER	Jan.	95	17:00	1.117	0.210	1.327	
		Jan. Jan.	95	17:00	1.258	0.330	1.588	
		and the second se	- 95	17:00	1.114	0.283	1.397	
· Income	5	Jan. Jan	- 95 - 95	17:00	1.252	0.262	1.514	
	7	Jan.	95	17:00	1.503	0.254	1.757	
	8	Jan.	95	17:00	1.288	0.258	1.546	and and a second se
100 mm	9	Jan.	95	17:00	1.433	0.215	1.648	
and of the state	0	Jan.	95	17:00	1.017	0.380	1,397	and a second
regulation for the	4	Jan.	95	17:00	1.235	0.292	1.527	and the second
	5	Jan.	95	17:00	1.332	0.344	1.676	
	6	Jan.	95	17.00	1.226	0.201	1.427	
Construction of the local division of the lo	18	Jan.	95	17.00	1.263	0.214	1.477	
	19	Jan.	95	17:00	1.262	0.456	1.718	
_	20	Jan.	95	17.00	1.281	0.356	1.637	
	21	Jan.	95	17:00	1.193	0.362	1.555	
	22	Jan.	95	17:00	1.439	0.143	1.582	
	23	Jan.	95	17:00	1.205	0.328	1.533	
	24	Jan.	95	17:00	1.354	0.379	1.733	
	25	Jan.	95	17:00	1.385	0.371	1.756	
	26	Jan.	95	17:00	1.458	0.221	1.679	
and the second se	30	Jan.	95	17:00	1.204	0.300	1.504	
	1	Feb	95	17:00	0.986	0.109	1.095	
	2	Feb	95	17:00	1 285	0,205	1.490	
	3	Feb	95	17:00	1.209	0.216	1.425	
	4	Feb	95	17:00	1.229	0.261	1.490	
	5	Feb	95	17:00	1.371	0.240	1.611	
	6	Feb	95	17:00	1.167	0.251	1.418	
	7	Feb	95	17:00	1.079	0,296	1.375	
	8	Feb	95	17:00	0.804	0.386	1.190	
	9	Feb	95	17:00	0.943	0.259	1.202	
	10	Feb	95	17:00	0.805	0.254	1.059	
	14	Feb	95	17:00	1.402	0.250	1.652	
	15	Feb	95	17:00	1.161	0.211	1.372	
	16	Feb	95	17:00	1.103	0.330	1.433	
and a factor	22	Feb	95	17:00	1.356	0.344	1.700	
	23	Feb	95	17:00	1.112	0.327	1.439	
-	24	Feb	95	17.00	1.094	0.213	1.307	
	25	Feb	95	17:00	1.119	0.295	1.414	
	26	Fcb	95	17:00	1.142	0,223	1.365	
	27	Feb	95	17:00	1.238	0.278	1.516	Constant of the owner owner owner

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Table B.5.12 Result of Discharge Measurement at Guaraguao (3/3)

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Table B.5.13 Estimation of Spring Water Discharge at Caño Ponton

Observation (1) / Date; Feb 7, 1995

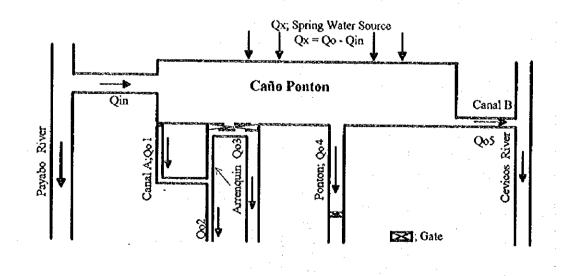
	Location	Discharge Area	Mean Velocity	Discharge	Total (Qin,Qo)	$QI = QO \cdot Qin$
-	a ser a s	A (m2)	V (m/s)	(m3/s)	(m3/s)	(m3/s)
Qin	Payabo River	5.503	0.202	1.112	1.112	
Qol	Canal A	0.000	0.000	0.000		
Q02	Arrenquin Canal	1.128	0.272	0.307		
Q03	Arrenquin Canal	1.817	0.482	0.875	1.753	0.641
Q04	Ponton Canal	1.927	0.296	0.570		
Q05	Canal B	+	+	0.001	1	

Observation (2) / Date: Feb 17, 1995

	Location	Discharge Area	Mean Velocity	Discharge	Total (Qin,Qo)	Q1 = Q0-Qin
		A (m2)	V (m/s)	(m3/s)	(m3/s)	(m3/s)
Qin	Payabo River	6.175	0.164	1.015	1.015	
હો	Canal A					•
205	Arrenquin Canal	0.414	0.297	0.123	1 · [
203	Arrenquin Canal	0.637	0.474	0.302	1.179	0.164
	Pump	0.260	0.169	0.044		
201	Ponton Canal	2.400	0.296	0.710	1. 1	
205	Canal B	*	+	0.000	1 [

Observation (3) /Date; Feb 28, 1995

	Location	Discharge Area	Mean Velocity	Discharge	Total (Qin,Qo)	Qx = Qo - Qin
officially 1, page		A (m2)	V (m/s)	(m3/s)	(m3/s)	(m3/s)
Qin	Payabo River	6.364	0.188	1.195	1.195	CHICK CONTRACTOR OF THE OWNER OF
Qo1	Canal A]				
Q02	Arrenquin Canal	0.769	0.384	0.295		
Q03	Arrenquin Canal	2.313	0.510	1.179	2.340	1,145
Q04	Ponton Canal	3.007	0.288	0.866	1	
QoS	Canal B	*	+	0.000	1	



					(m3/s
Return	F[%]	Villa	Riva	El L	imon
Period		Before	After	Before	After
1/200	0.50	1369.71	1115.23	antan sering tan kana kanalan kana perperata sering dari kana dari pertama kana kana kana kana kana kana kana M	
1/100	1.00	1280.15	1060.77	•	*
1/50	2.00	1187.04	1004.26		*
1/20	5.00	1056.48	925.22	630.00	750.00
1/10	10.00	948.81	860.22	612.63	715.09
1/5	20.00	828.10	787.56	559.10	647.93
1/2	50.00	623.92	665.23	469.38	530.57

Table B.5.14 Probability Analysis of High Flow at Villa Riva and El Limon

Table B.5.15 Probability Analysis of High Flow at the Payabo River

Return	F[%]	Abadesa	Diversion Point at Payabo
Period		Maximum Discharge (m3/s)	Maximum Discharge (m3/s)
1/200	0.50	544.07	600,30
1/100	1.00	494.84	545.98
1/50	2.00	445.21	491.23
1/20	5.00	378.36	417.46
1/10	10.00	325.69	359.35
1/ 5	20.00	269.37	297.21
1/2	50.00	180.94	199.64

Table B.5.16 Estimated Flood Discharge in the Study Area

	CHARLES IN THE OWNER OF THE OWNER			Datura	Maximum 24hr	Runoff	Duration
	Maximum 24hr	Runoff	Duration	Return Period	Rainfall (mm)	Coefficient	Time C
Period	Rainfall (mm)	Coefficient	Time C	1/5	133.7	0.75	220
1/2	102.1	0.75	220 Peak	Catchment	Duration	Rainfall	Pcak
Catchment	Duration	Rainfall	Discharge	Area	Time	Intensity	Discharge
Area	Time	Intensity (mm/hr)	(m3/s)	(km2)	(hr)	(mm/hr)	(m3/s)
(km2)	<u>(hr)</u> 2.46	13.286	27.679	10	2.19	18.422	38.379
10	And the second	12.113	50.471	20	2.64	16 796	69.982
20	2.96	11.475	71.722	30	2.94	15,912	99.448
30	3.56	11.473	92.029	40	3.18	15,313	127.608
<u>40</u> 50	3.78	10.720	111.665	50	3.37	14.864	154.834
	3.97	10.462	130,780	60	3.54	14.507	181.337
70	4.13	10.250	149.472	70	3.69	14.212	207.256
80	4.28	10.069	167.811	80	3.82	13.961	232.684
Return	Maximum 24hr	Runoff	Duration	Return	Maximum 24hr	Runoff	Duration
Period	Rainfall (mm)	Coefficient	Time C	Period	Rainfall (nm)	Coefficient	Time C
1/10	154.0	0.75	220	1/20	173.0	0.75	220
Catchment	Duration	Rainfall	Peak	Catchment	Duration	Rainfall	Peak
Area	Time	Intensity	Discharge	Area	Time	Intensity	Discharge
(km2)	(hr)	(mm/hr)	(m3/s)	(km2)	(hr)	(mm/hr)	(m3/s)
10	Construction of the local division of the lo	21.865	45.552	10	Name of Concession, or other Designation, or	25.176	52.450
20	A DESCRIPTION OF A DESC	19.935	83.062	20	2.37	22.954	95.641
30	and the second s	18.885	118.034	30	2.64	21.746	135.910
40	And the second design of the s	A DESCRIPTION OF A DESC	151.457	40	2.85	20.927	174.394
50	The Party States of the Party o	17.642	183.771	50	3.02	20.314	211.602
60	No. of Concession, name of	17.218	215.229	60	3.17	19.826	247.824
70	A company of the second s	Name and Address of the Owner, where the Party of the Par	245.990	70	3.31	And the second s	283.247
80	And the second state of th		276.170	80	And the second s	Concerns the second	317.998
Return	Maximum 24h	Runoff	Duration	Return	Maximum 24h		Duration
Period	Rainfall (mm)	1	Time C	Period	Rainfall (mm)		
1/50	197.2	0.75	220	1/100	215.2	0.75	220
Catchment	Duration	Rainfall	Peak	Catchment		Rainfall	Peak
Area	Time	Intensity	Discharge	Area	Time	Intensity	Discharge
(km2)	(hr)	(mm/hr)	(m3/s)	(km2)	(hr)	(mm/hr)	(m3/s)
10	1.86	29.507	A REAL PROPERTY AND A REAL PROPERTY A REAL PROPERTY AND A REAL PRO	A REAL PROPERTY AND A REAL	And in case of the local data and the local data an	NAMES OF TAXABLE PARTY.	
20	2.24	26.901				NAME OF TAXABLE PARTY OF TAXABLE PARTY.	
30	2.49		1		the second se	and the supervised of the local division of	NAMES OF TAXABLE PARTY AND ADDRESS OF TAXABLE PARTY.
4	2.69	and the second se		the same range of the second s			
5	the second s	The local division of	the second s	distance of the second se	and the second se		
6	and the second	and the state of t	the second s	and the second se	And Designation of the local data and the local dat	The subscription of the su	the second s
7(and the second s						
8		And in case of the local division of the loc	- A DESCRIPTION OF TAXABLE PARTY OF TAXABLE PARTY.	8	3.12	2 24.859	414.313
Return	Maximum 24h		Duration				1
1	Rainfall (mm)	Coefficient	Time C		Į.		
Period							
1/200	233.1	0.75	220				
1/200 Catchmen	233.1 L Duration	0.75 Rainfall	Peak				
1/200 Catchnien Area	233.1 Duration Time	0.75 Rainfall Intensity	Peak Discharge				
1/200 Catchnien Area (km2)	233.1 t Duration Time (hr)	0.75 Rainfall Intensity (mm/hr)	Peak Discharge (m3/s)				
1/200 Catchmen Area (km2)	233.1 L Duration Time (hr) 0 1.7	0.75 Rainfall Intensity (mm/hr) 3 36.133	Peak Discharge (m3/s) 8 75.28	7		· · · · · · · · · · · · · · · · · · ·	
1/200 Catchmen Area (km2) 1 2	233.1 1 Duration Time (hr) 0 1.7 0 2.0	0.75 Rainfall Intensity (mm/hr) 3 36.133 9 32.94	Peak Discharge (m3/s) 8 75.28 7 137.280	7			
1/200 Catchmen Area (km2) 1 2 3	233.1 Duration Time (hr) 0 1.7 0 2.0 0 2.3	0.75 Rainfall Intensity (mm/hr) 3 36.133 9 32.94 2 31.21	Peak Discharge (m3/s) 8 75.28 7 137.28 3 195.08	7 D 4			
1/200 Catchmen Area (km2) 1 2 3 4	233.1 Duration Time (hr) 0 1.7 0 2.0 0 2.3 0 2.5	0.75 Rainfall Intensity (mm/ht) 3 36.133 9 32.94 2 31.21 1 30.03	Peak Discharge (m3/s) 8 75.28 7 137.28 3 195.08 8 250.32	7 D 4 0			
1/200 Catchmen Area (km2) 1 2 3 4 5	233.1 Duration Time (hr) 0 1.7 0 2.0 0 2.3 0 2.5 0 2.6	0.75 Rainfall Intensity (mm/ht) 3 36.133 9 32.94 2 31.21 1 30.033 6 29.15	Peak Discharge (m3/s) 8 75.28 7 137.280 3 195.08 8 250.320 8 303.72	7 D 4 0 8			
1/200 Catchmen Area (km2) 1 2 3 4 4 5 6	233.1 Duration Time (hr) 0 1.7 0 2.0 0 2.3 0 2.5 0 2.6 0 2.8	0.75 Rainfall Intensity (mm/hr) 3 36.133 9 32.94 2 31.21 1 30.033 6 29.15 0 28.45	Peak Discharge (m3/s) 8 75.28 7 137.280 3 195.08 8 250.320 8 303.72 8 355.720	7 D 4 0 8 0			
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Table B.5.17 Summary of Sediment Runoff

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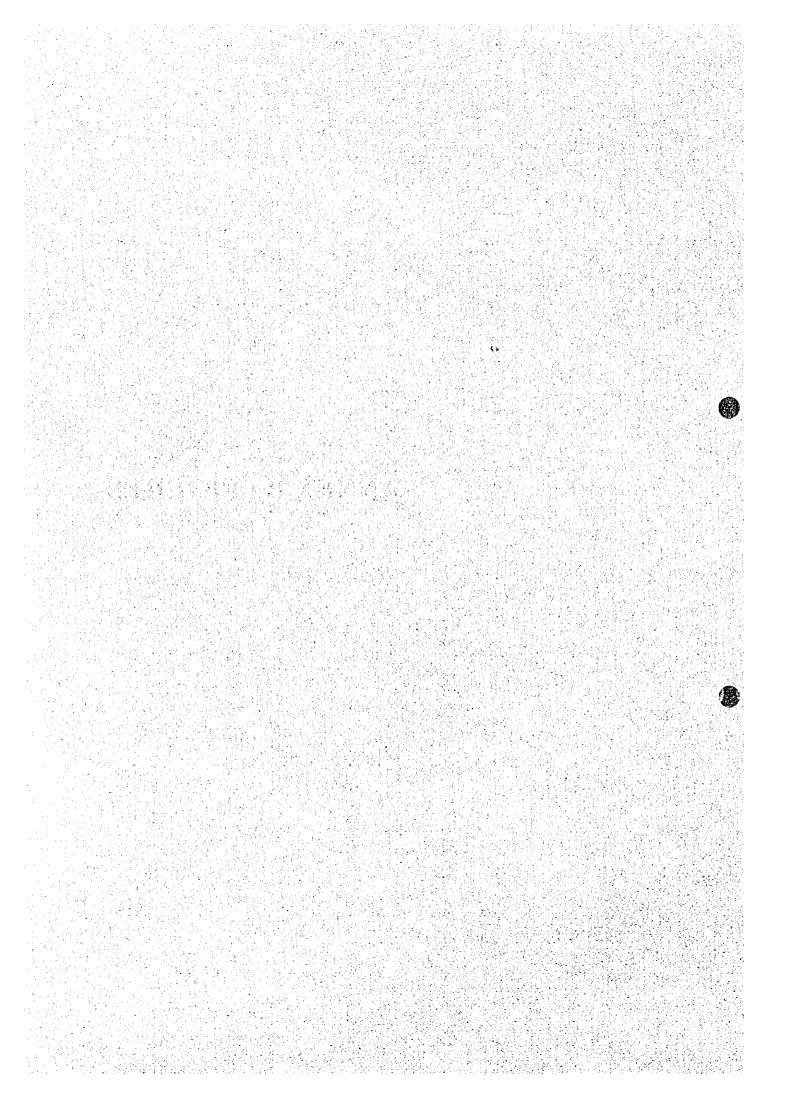
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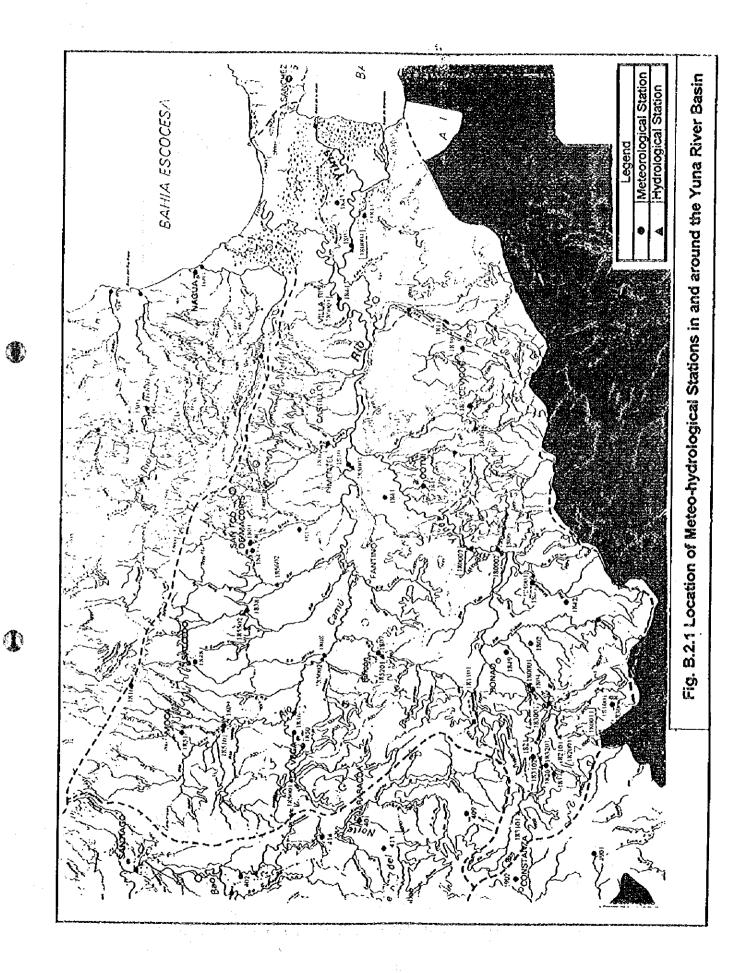
Code	Station	Catchment Area	Jan	Feb	Mar	Apr	May	Jun	Jui	Aug	Sep	Б О	Nov	a A A	Annual
		(kcm2)				Sed	Sediment Runoff (t)	soff (t)			-				
20003	With Rive	4680	417061	45834	32994	53024	135368	89295	44770	53127	30606	58617	95804	70645	751790
	EI Limon	0213	39807	54893	33668	43074	121355	75236	31409	52729	49568	57737	92658	86077	738210
	187007 Ahadees	210	381	383	540	1198	3110	4020	1839	3503	3756	2654	1841	962	24186
7	Davaho	345	009	603	851	1888	4899	6332	2896	5518	5917	4181	2900	1515	38100
						Specific Sc	ediment R	Specific Sediment Runoff (t/km2)	a2)						
- 2000	1/611a Dim	10875	8 91	070	7.05	11.33	28.92	19.08	9.57	11.35	6.54	12.53	20.47	15.10	160.64
	THAT ANY	10213	775		95.9		23.66	14.67	6.12	10.28	9.66	11.25	18.06	16.78	143.90
	TOMIT I	IOLC	2/		747		14 201	18 35	8.40	15.99	17.15	12.12	8.41	4.39	110.44
XN.	10/WZ HURDEN			2.1	247	5 27	14 20	18 35	8 40	15.99	17.15	12.12	8.41	4.39	110.44
	1 raya00	ic+c	*/*/		Ectims	ted Sperit	To Sedime	Estimated Specific Sediment Runoff (m3/km2)	(m3/km2)						
				07 50	107.01	02.00	120 02	25 24	100 01	20 43	11.77	22.55	36.85	27.17	289.15
80003		-	10.04	100.11	140.21		2.42			02.02	02 21	30.00	32 51	30.20	259.02
180004	El Limon	5130	13.97	19.26	11.8.11	11.41	4Z.25	20.40		2.01		24.74			100 70
87002	Abadesa	219	3.13	3.14	44.44	9.85	25.56	33.04	15.11	28.79		21.52	151.61	1.	0/ 0/
		325	3 13	3 14	4.44	9.85	25.56	33.04	15.11	28.79	30.87	21.82	15.13	1.91	198.78

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Table

Site	Date	ပ် လ	Gauge Height (m)	Flow Area (m2)	Mean Velocity (m/s)	Discharge (m3/s)	Remark
Laguna Cristal	19/8/94	TG	0.33	1.410	0.304	0.428	
	16/9/94	rG	0.33	1.120	0.398	0.446	
Lagunita Cristal	19/8/94	I-dT	0.52	1.350	0.191	0,258	
		ILP-II	0.47	0.810	0.246	0.199	
		III-471	0.15	0.280	0.168	0.047	
		LP-IV	0.67	4.320	0.226	0.977	1.481
	16/9/94	L-P-1	0.43	0.240	0.304	0.073	
		II-4-J	0.54	0.900	0.137	0.123	
•		日-4-1	•	0.000	0.000	0.000	•
-		LP-N	0.70	4,140	0.232	0.960	1.156
Cano Cercado	19/8/94	SC	•	5.620	0.111	0.624	
	16/6/91			4.600	0.117	0.538	
Cano Barraco	19/8/94	B		1.910	0.043	0.082	
	15/9/94		-	0.950	0.056	0.053	
Drenaje Cascarilla	19/8/94	DC-I	•	5.950	0.101	0.598	
(road bridge)	15/9/94		•	9.620	0.087	0.837	
Drenaje Cascanilla	19/8/94	DC-II		13.910	0.081	1.128	
(Los Caprices)	15/9/94		•	21.480	0.050	1.068	
Laguna Cueva	19/8/94	rc-r		1.250	0.284	0.355	
		LC-II	•	0.240	0.113	0.027	0.382
	16/9/94	1-5-1	0.59	1.460	0.440	0.642	
		LC-II	0.31	0.170	0.071	0.012	0.654
Cueva	19/8/94	CG-1	1	3.980	0.429	1.708	
Guaraguao		CG-II	-	2.360	0 178	0.420	2.128
	16/9/94	ЧЧ СС-	06'0	2.590	0.401	1.038	
	-	11-00 СС-П	0.70	2.840	0.138	0.391	1.429
Rio Payabo	15/9/94	RP-I-A	-	8.410	0.181	1.522	
Diversion Point	15/9/94	RP-I-B		S.330	0.610	5.080	6.602
Rio Payabo (Puente La Verde)	15/9/94	RP-II	1.54	17.600	0.423	677°L	
Rio Pavabo (Desembocadura)	15/9/94	PR-III	•	12.680	0.607	7.699	

ANNEX B : FIGURES





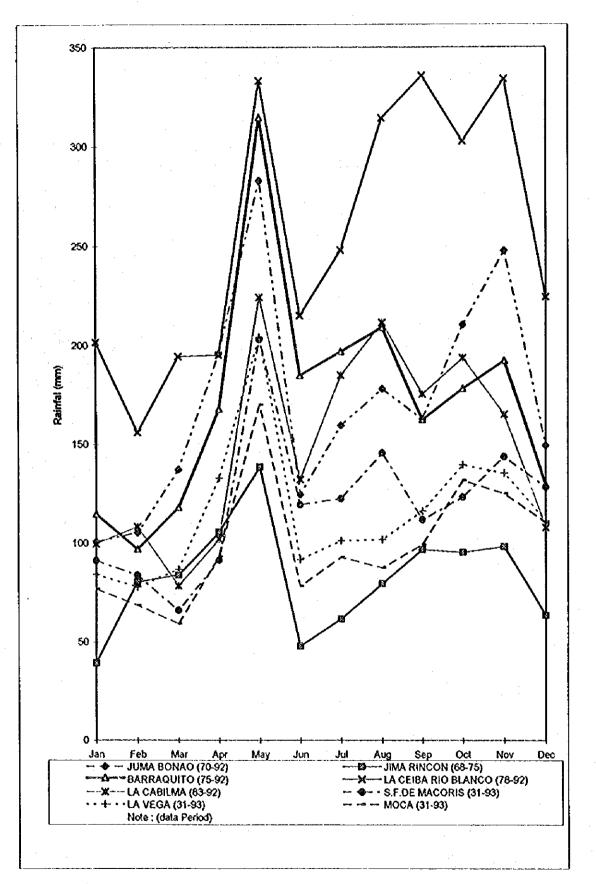
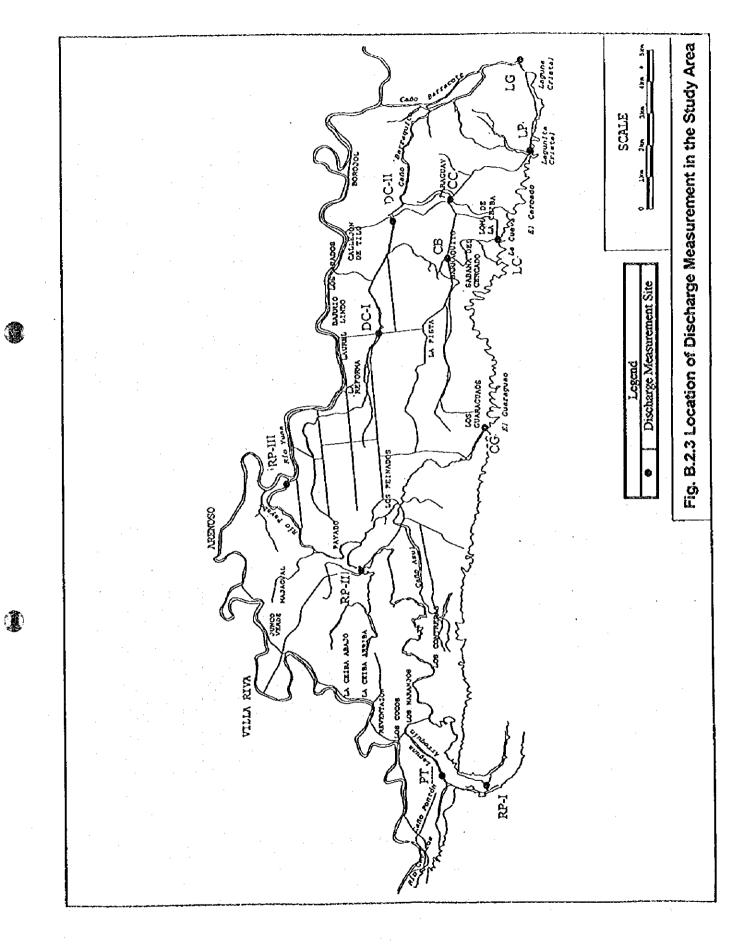


Fig. B.2.2 Typical Rainfall Pattern in the Yuna River Basin



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No.	TRACKS, MARKED	Name of Station	1930	1940	1950	1960	1970	1980	1990
1		JARABACOA		i					
2		TAVERA				8			000
3		SANTIAGO ISA							
4		EL RIO CONSTANZA					the second s		<u> </u>
5	413	PINAR QUEMADO				0	a ()		
6		BOMA							
7	415	GUANAJUMA					00		
8		PINALITO				8			
9	417	BAO					D		
10	418	SABANA IGLESIA					מ		
11	419	LAS CHARCAS				8	0		
12		JAMAO				Ö			
13		CUESTA BARROSA					ā		
14	1501	LOS JENGIBRES				n			13
		CINTA NEGRA							
		NAGUA (MET)							
		SAN FCO. DE MACORIS							
		JUMA BONAO			· · ·		the second se		the second se
		LIMON DEL YUNA							<u></u>
		LOS QUEMADOS		i					
									<u> </u>
		MAIMON EL PINO		·					
		HATILLO YUNA				0			
		JIMA RINCON		······································					
		LOS RANCHITOS		· · · · · · · · · · · · · · · · · · ·	· · · · · · · · · · · · · · · · · · ·	0			
		LICEY NARANJAL							B
		LA BIJA				0			
		ADADESA							ם
		V. ALTAGRACIA (MET)	0	8 0 0 0 8				ä	
29	1814	BARRAQUITO			· · · ·				
30	1815	LA ANGELINA					•00		.00
31	1816	JOSE CONTRERAS					a		00
32	1817	LOS BOTADOS				u		00000	
		LA CEIBA RIO BLANCO					. 0		
		TIREO EN PINALITO		i		·			ñ
		EL NOVILLO						0 # 0 #	ñ 🖬 n
		EL TALLER • LA VEGA				· · · · · · · · · · · · · · · · · · ·		000	
		LA CABILMA							
		CENOVI SANTA ANA		··· ··· ·····		·			
		CEVICOS (MET)	r1	прода					
		LOS TRES PASOS			4 8 8 8 9				
		TALLER LAS MATAS		_ .					
		PIEDRA BLANCA						000	
		EL AGUACATE				<u> </u>		00	00
44	1844	VILLA RIVA (MET)							
		COTUI (MET)	0						
		PIMENTEL (MET)							4 8 0
		S.F.DE MACORIS (MET)							000
		SALCEDO (MET)							8 H ()
		BONAO (MET)	. 0			8 () 8 8 A			000
		LA VEGA (MET)							n n n
- 51	1851	MOCA (MET)				8 4 8 8 []			
		LA ESTRECHURA					M ()		
53	4901	VALLE NUEVO							
		CONSTANZA							in n
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Fig. B.3.1 Bar Chart of Data Continuity (1/3) (1) Rainfall Data

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2	402	TAVERA		• •		•	•	0																	
3	404	SANTIAGO-ISA	•	9 0	0	•	•	Ħ			0	10				$\overline{\overline{0}}$	<u>u</u>		믪	<u></u>		12	<u>u</u>	UI.	
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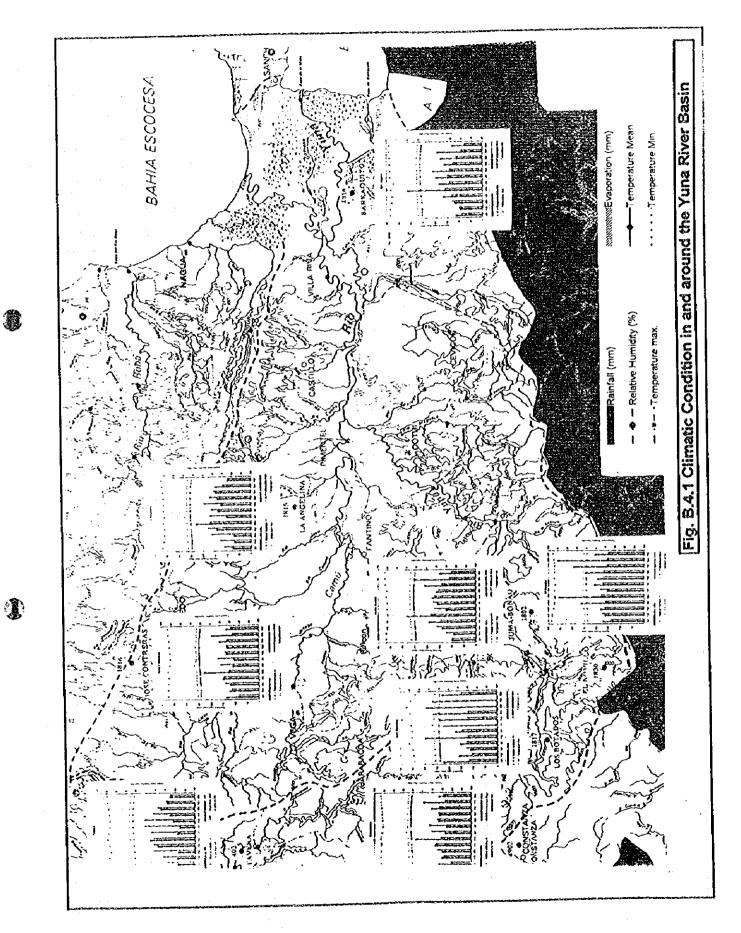
(5) Wind Velocity

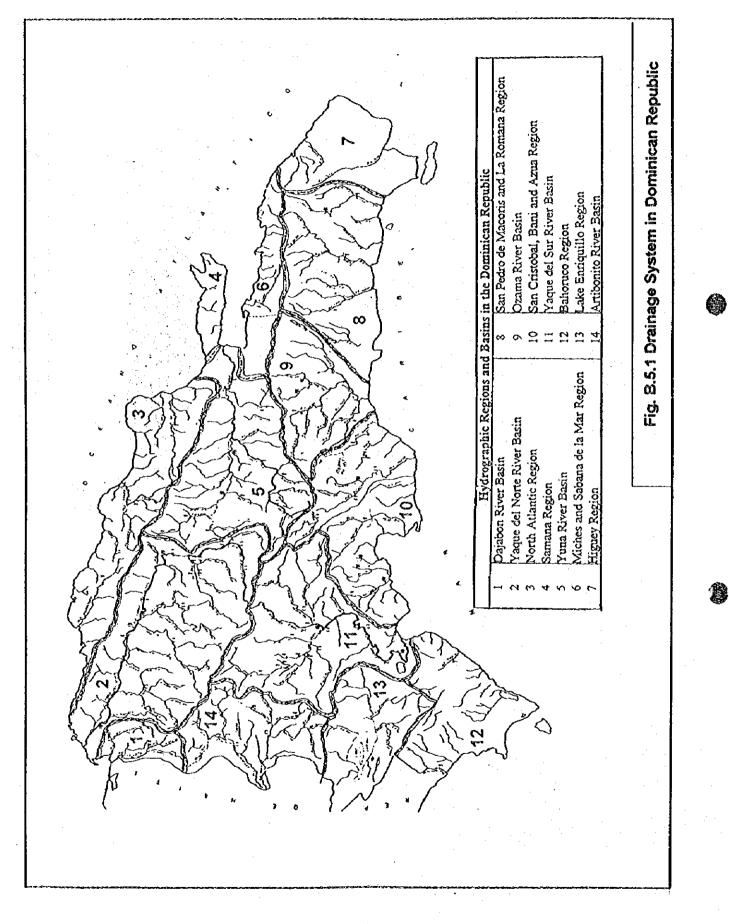
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Fig. 8.3.1 Bar Chart of Data Continuity (2/3)

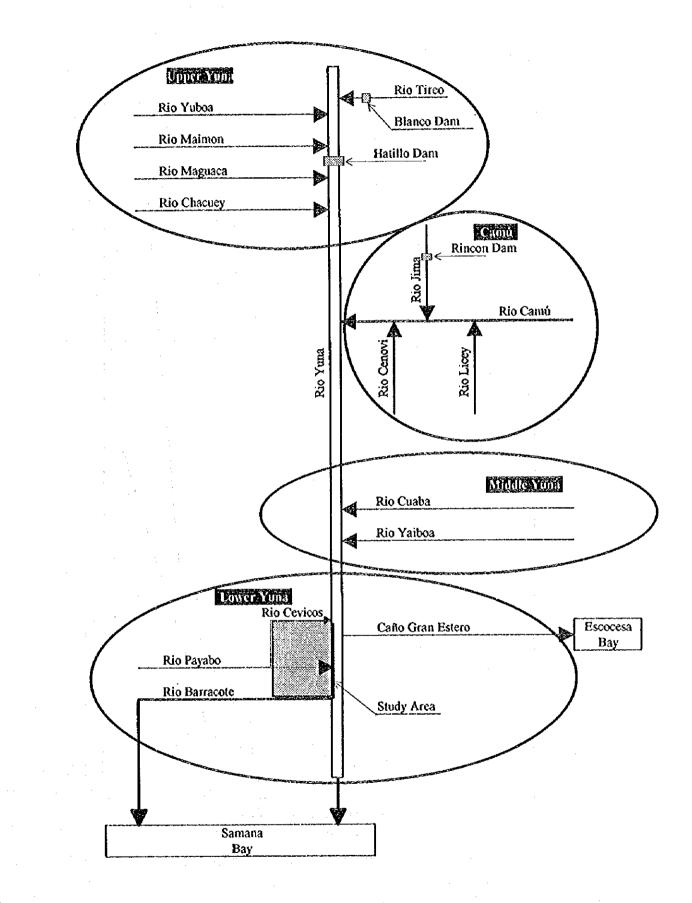
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Fig. B.3.1 Bar Chart of Data Continuity (3/3) (6) Hydrological Data





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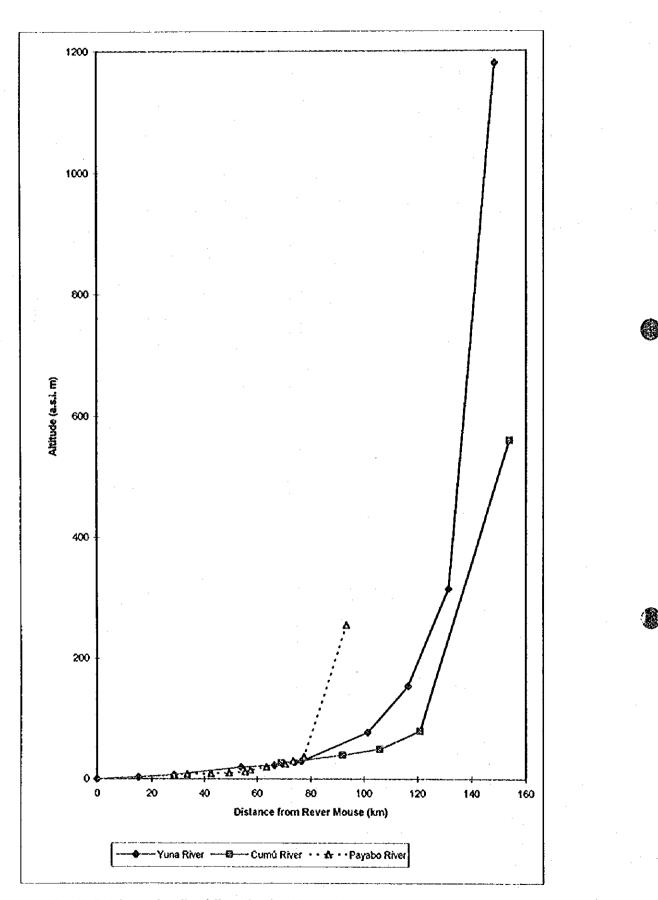
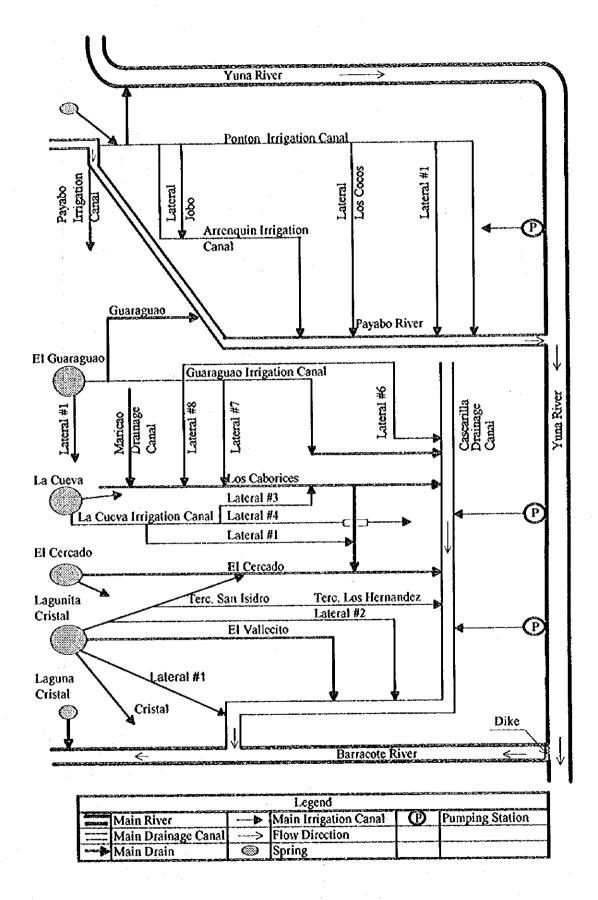


Fig. B.5.3 Longitudinal Profile the Yuna, Camu and Payabo River



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Fig. B.5.4 Drainage Condition in the Study Area

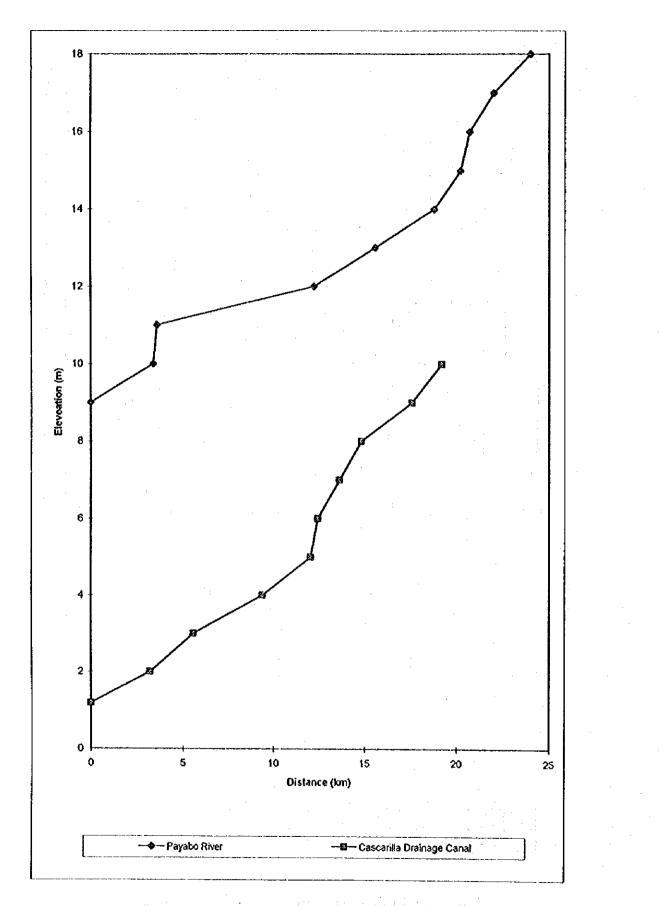
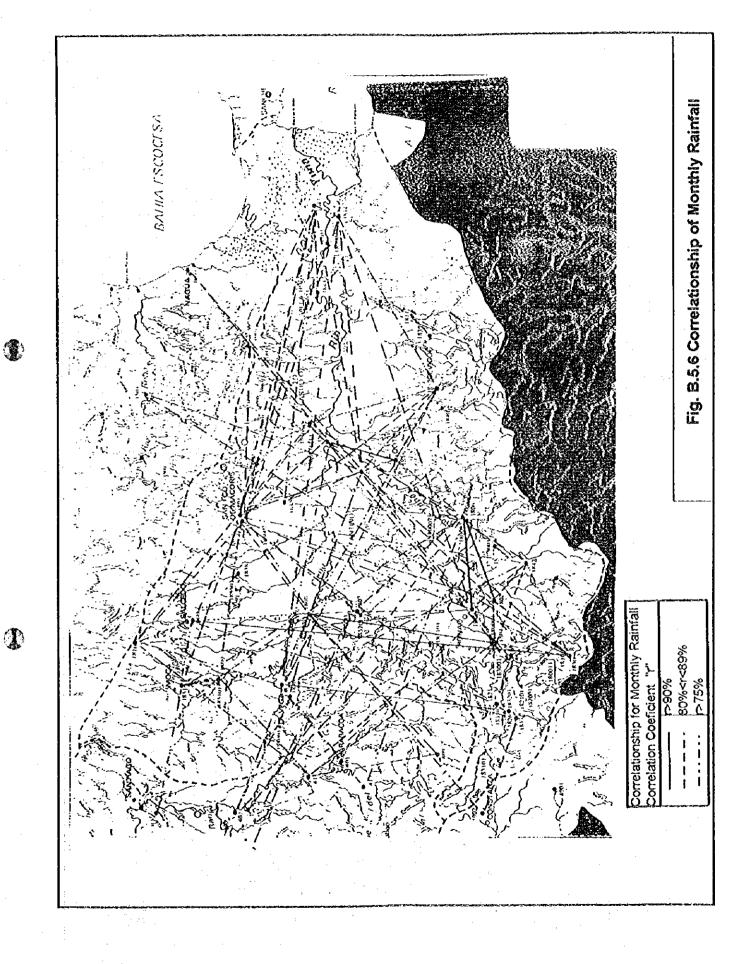
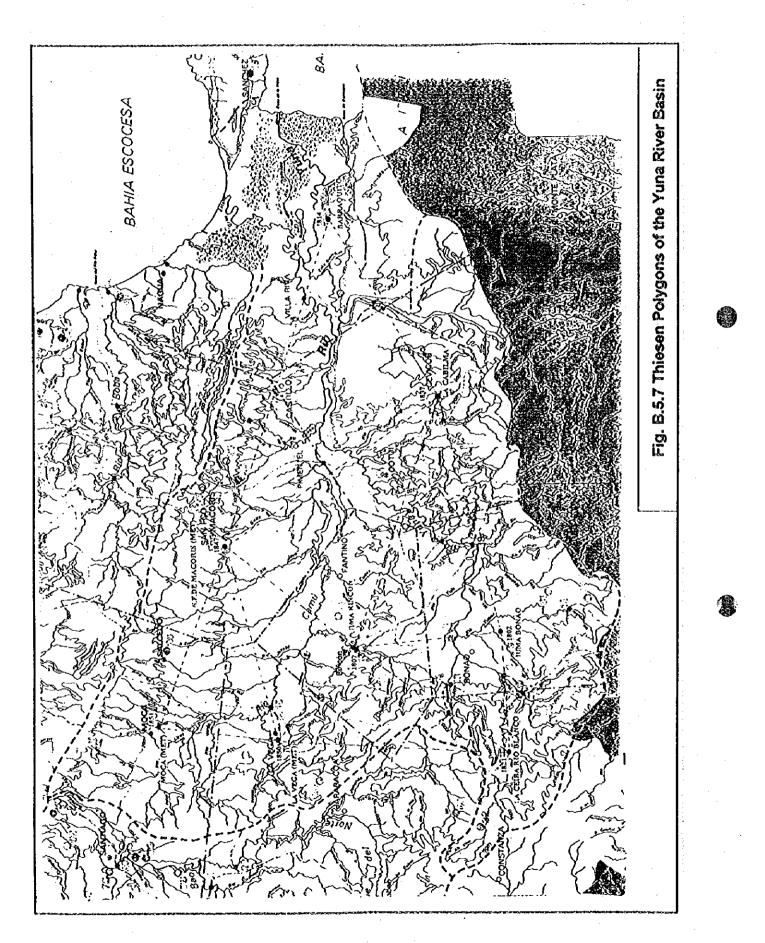
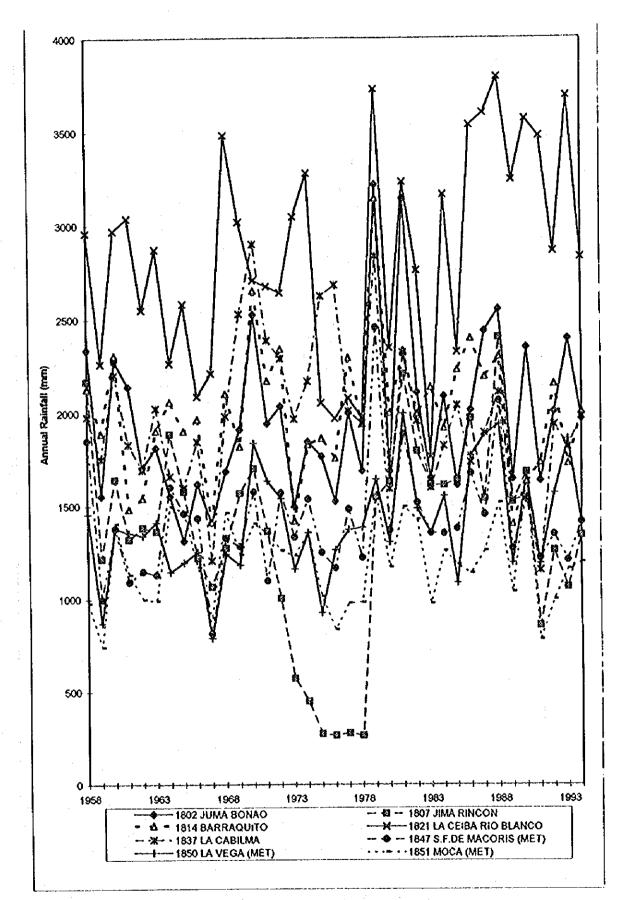


Fig. B.5.5 Profile of the Payabo River and the Cascarilla Canal in the Study Area









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Fig. B.5.8 Annual Rainfall at Selected Stations from 1958 to 1993

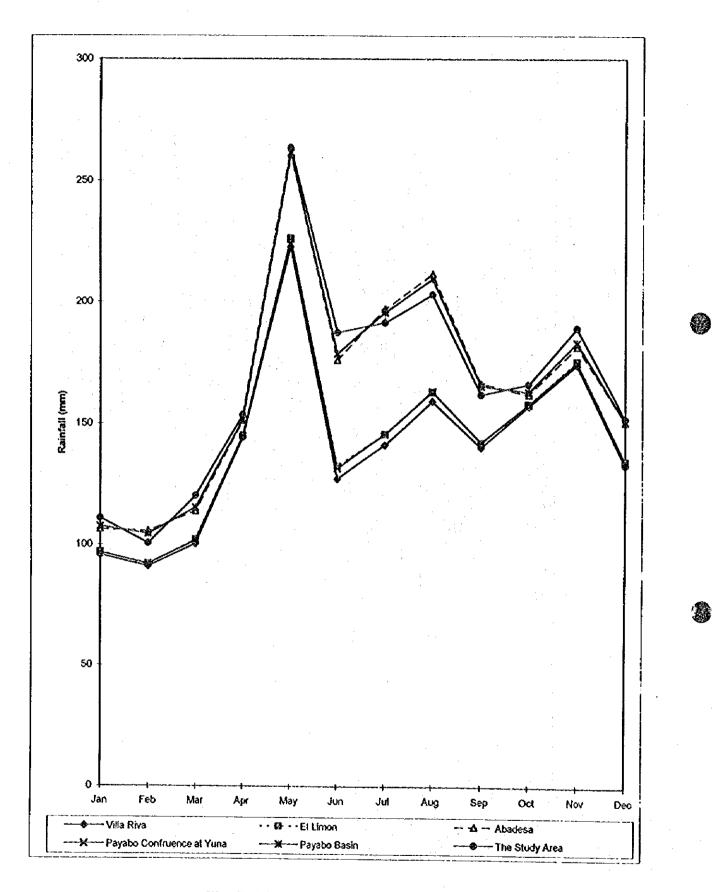
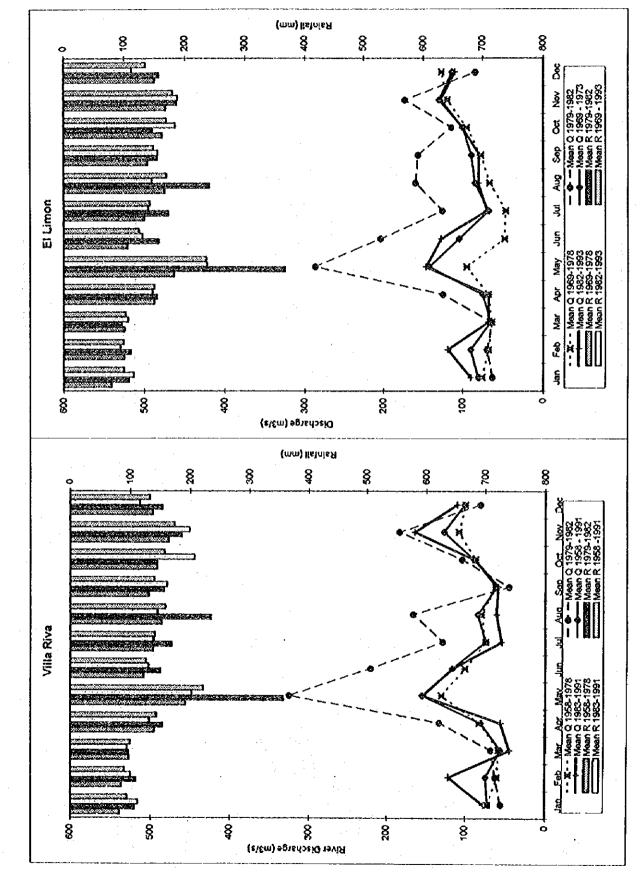


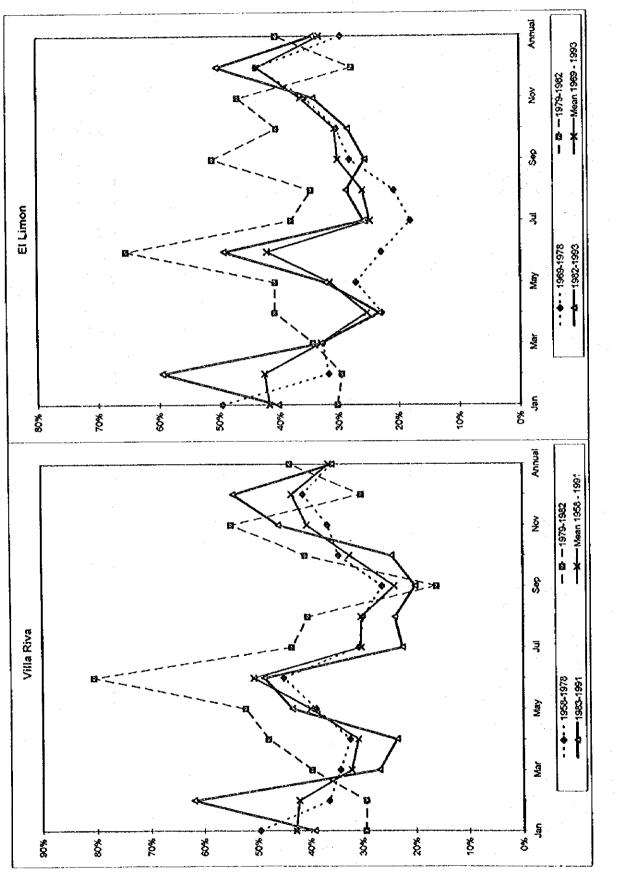
Fig. B.5.9 Estimated Rainfall Patterm



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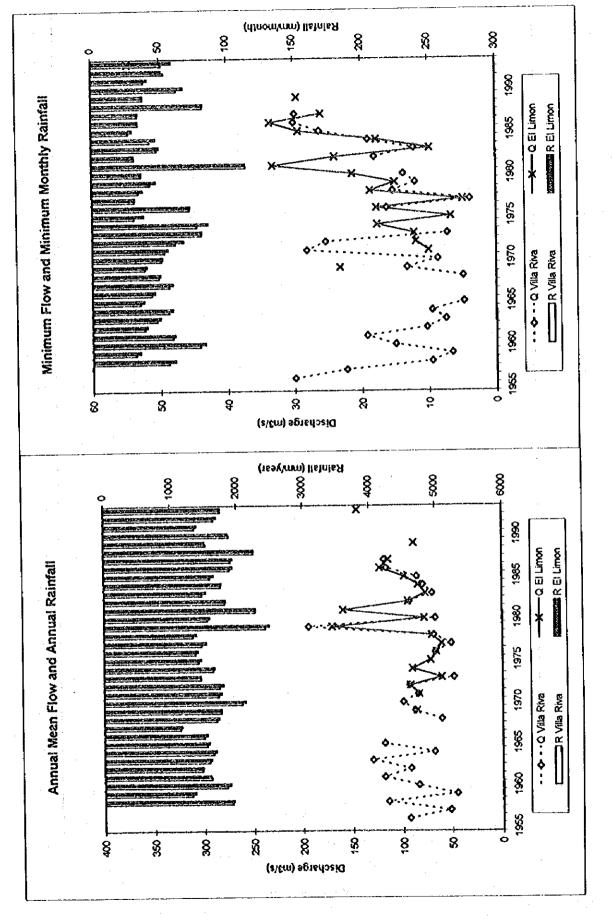
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Fig. B.5.10 Water Balance in the Yuna River Basin



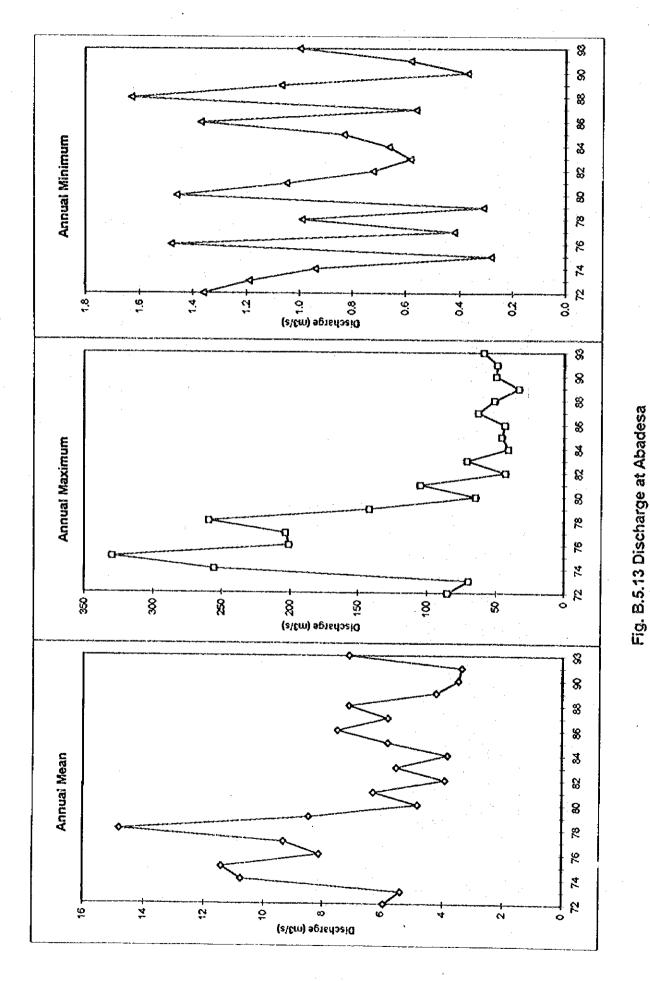


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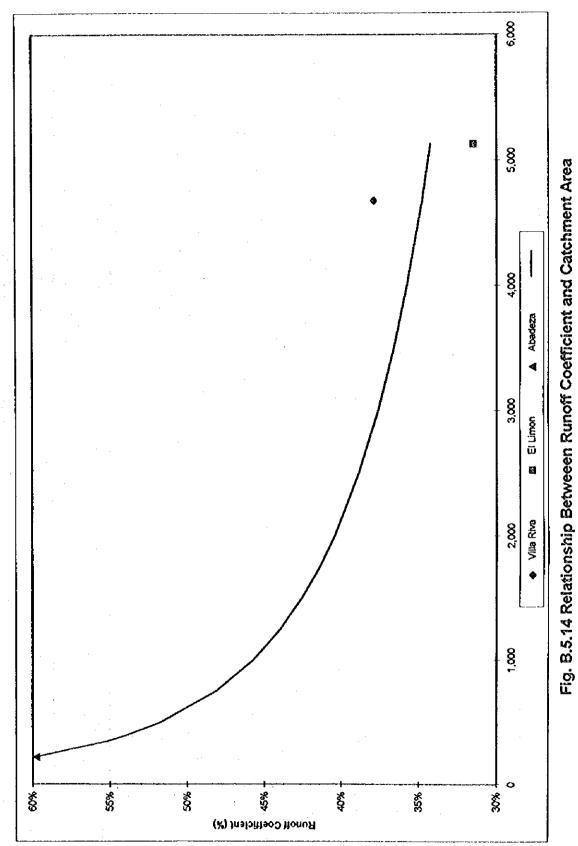


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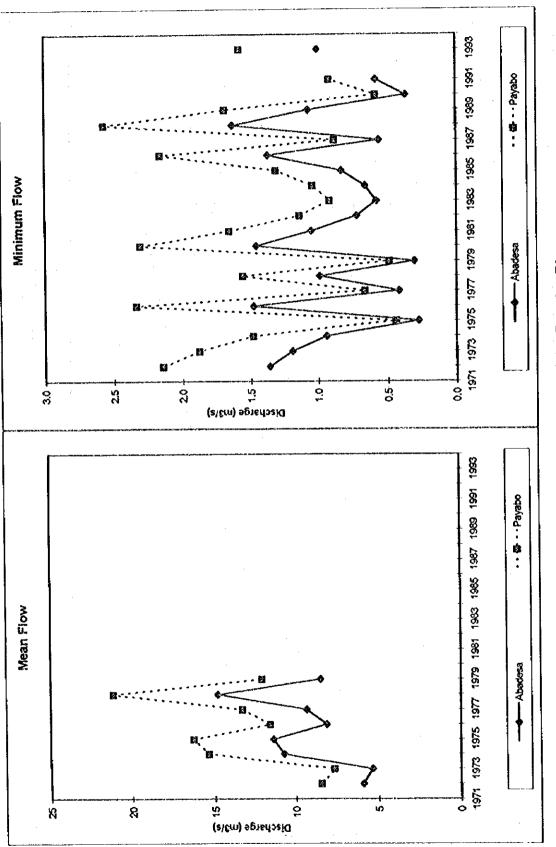
Fig. B.5.12 Annual Mean and Minimum Flow at Villa Riva and El Limon





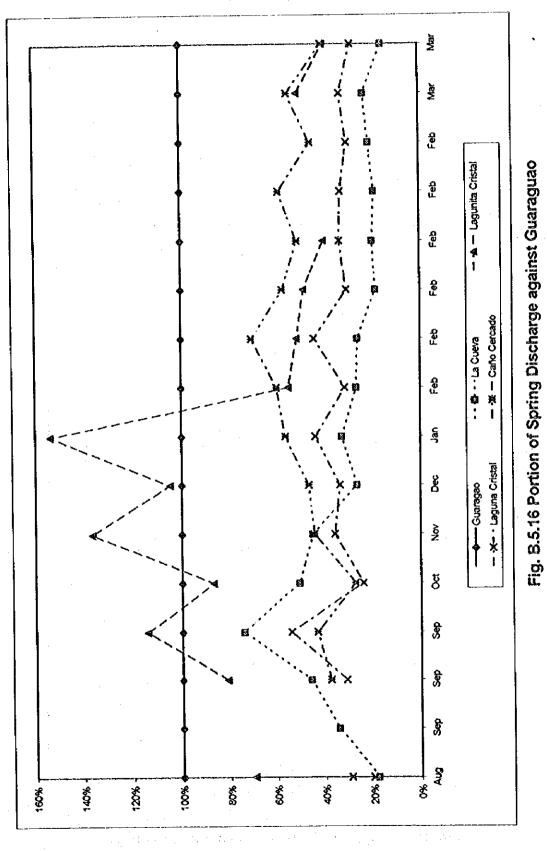


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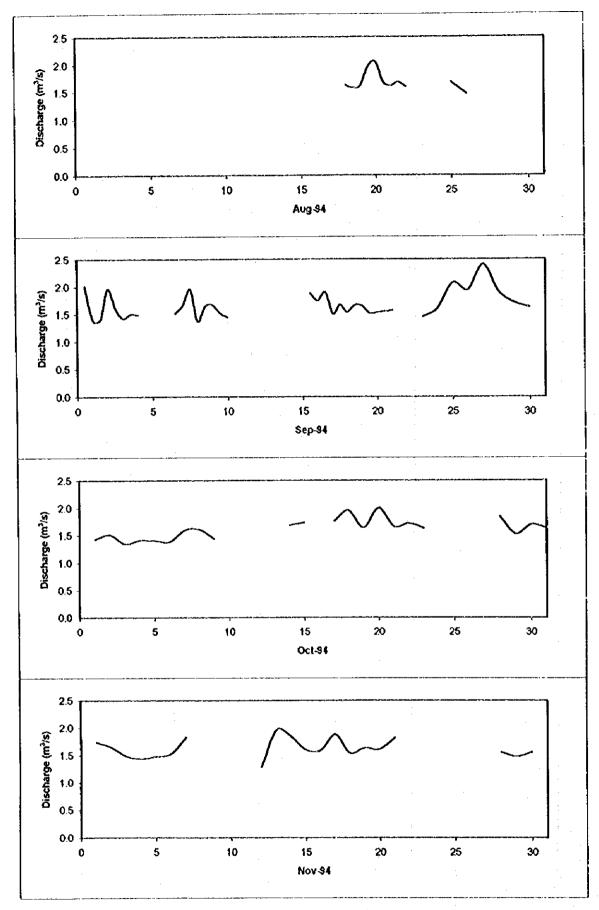




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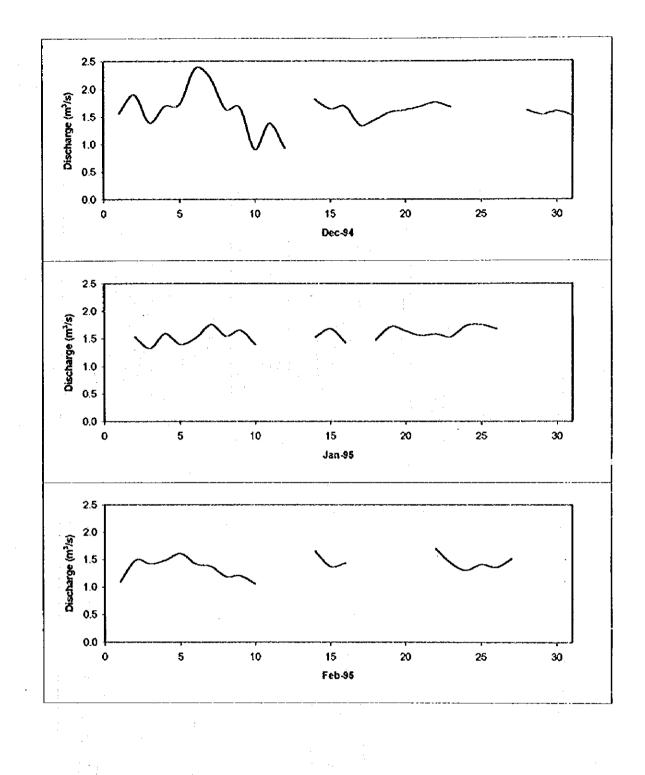
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Fig. B.5.17 Spring Discharge at Guaraguao (1/2)

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Fig. B.5.17 Spring Discharge at Guaraguao (2/2)

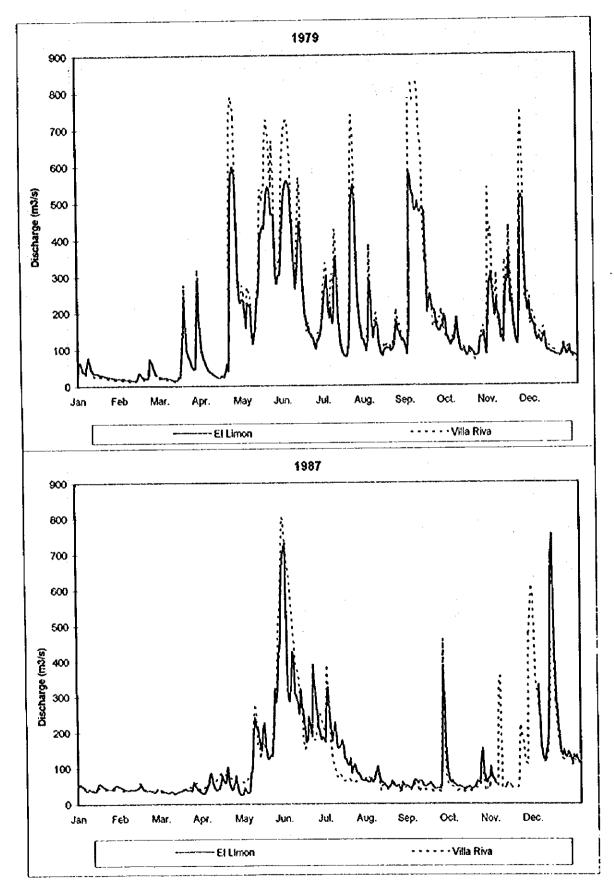


Fig. B.5.18 Daily Mean Discharge at Villa Riva and El Limon

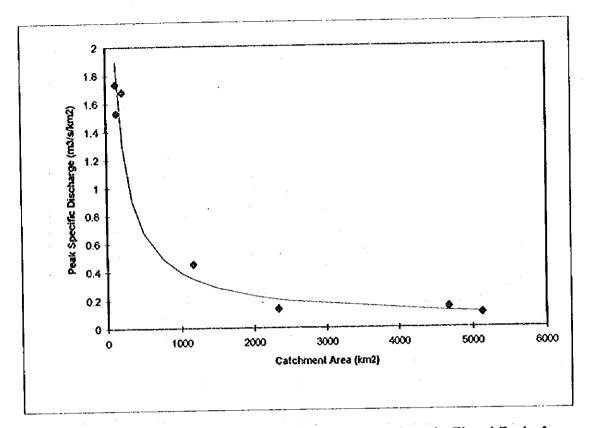
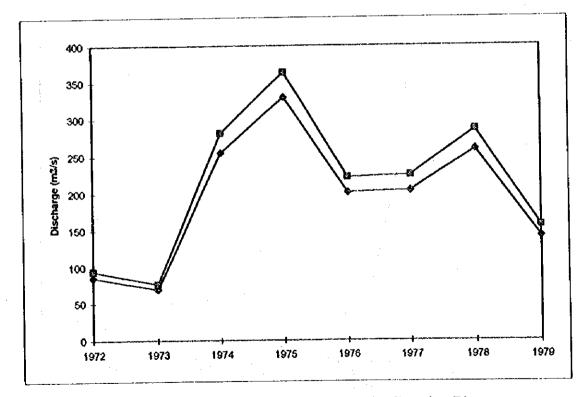
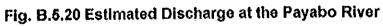


Fig. B.5.19 Specific Discharge and Catchment Area in Flood Period





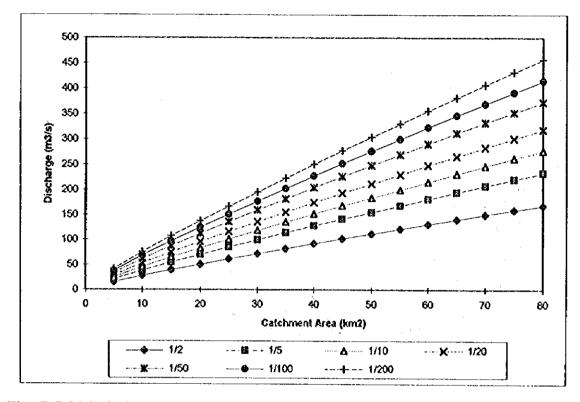
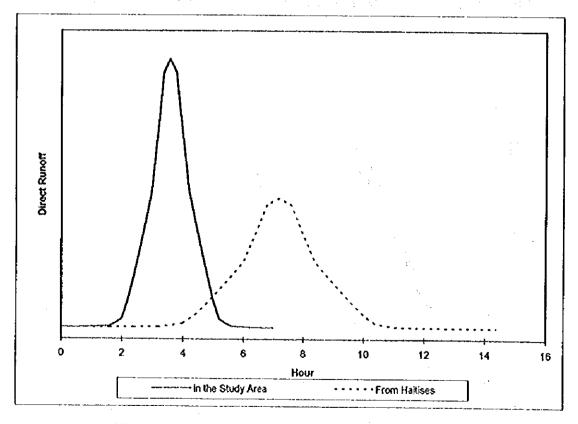
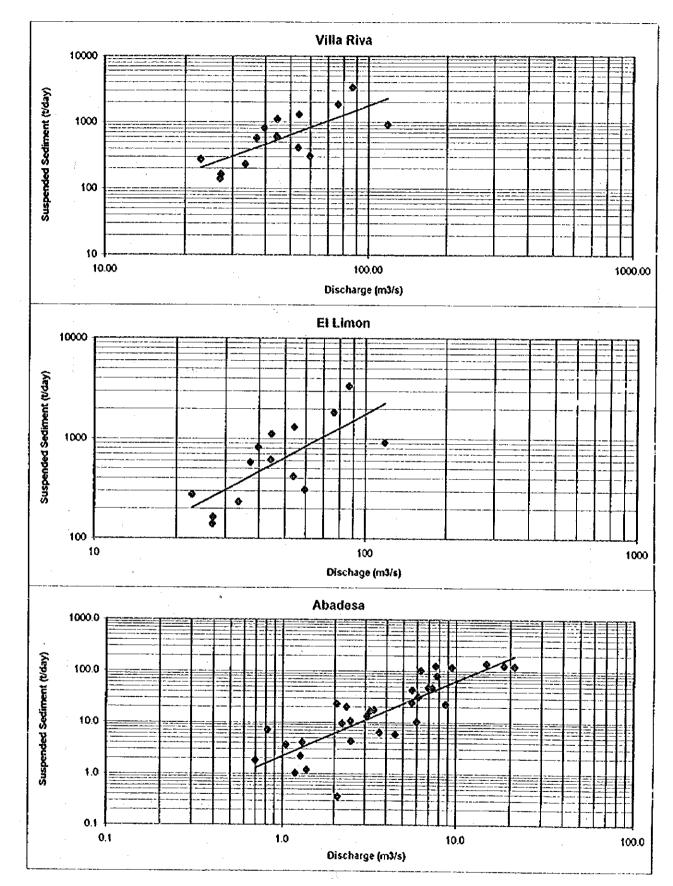
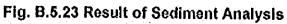


Fig. B.5.21 Relationship between Peak Flood Discharge and Catchment Area









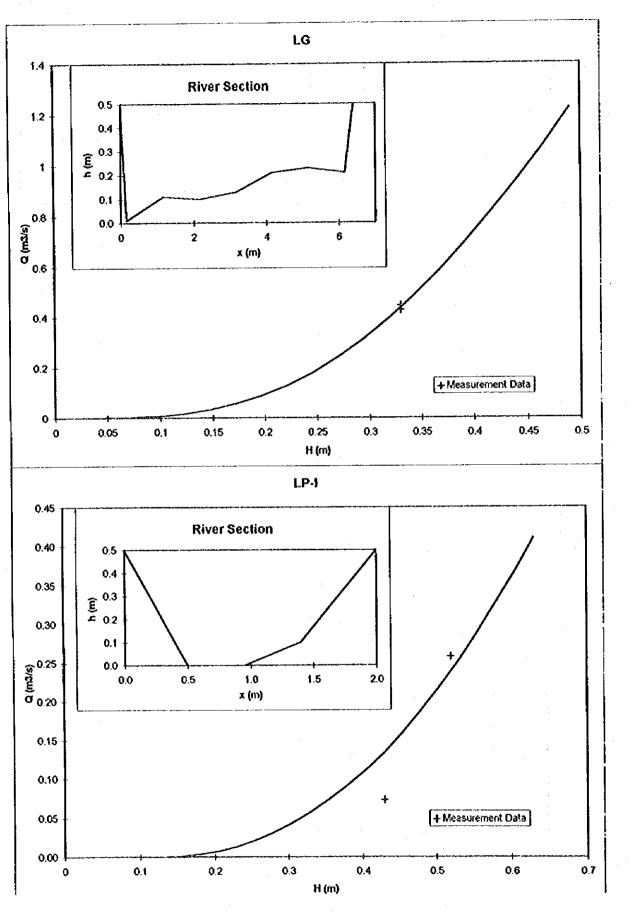
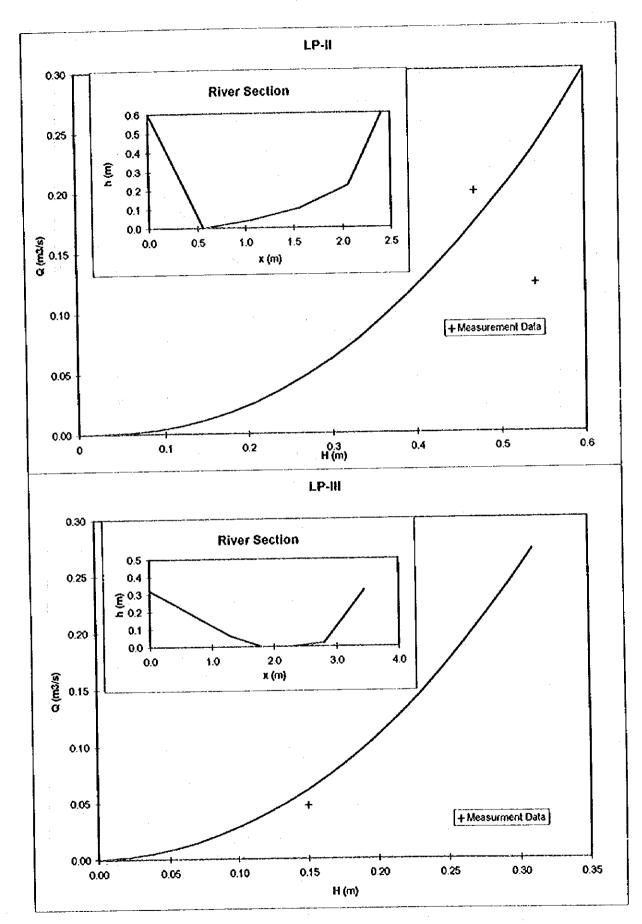


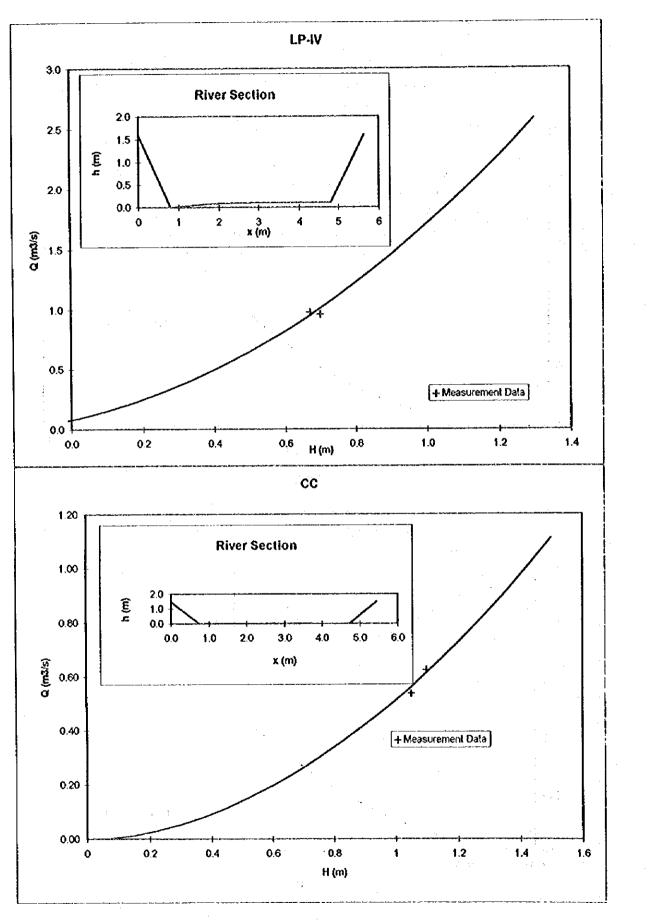
Fig. B.5.24 Estimated H-Q Rating Curve (1/9)

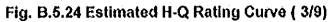
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Fig. B.5.24 Estimated H-Q Rating Curve (2/9)





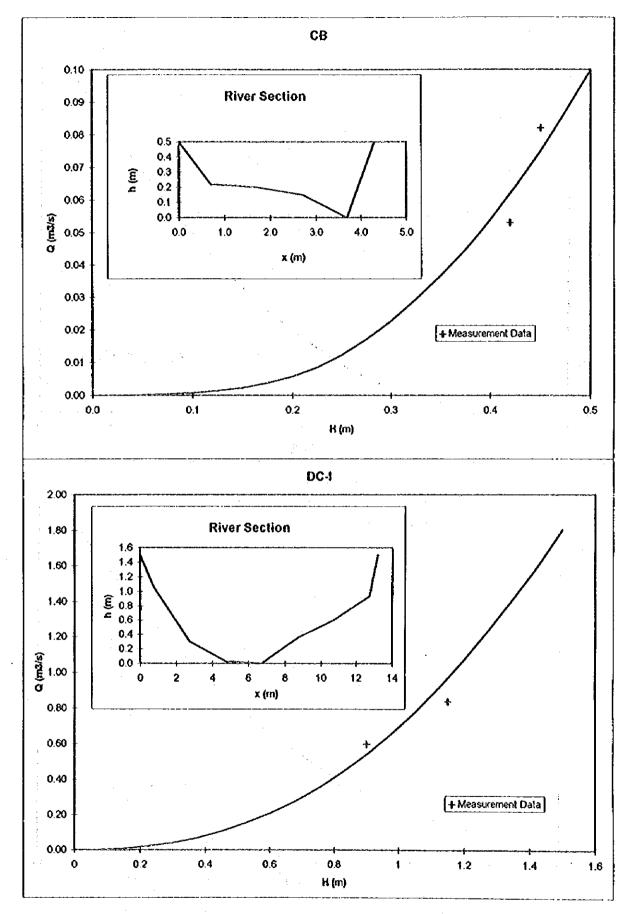
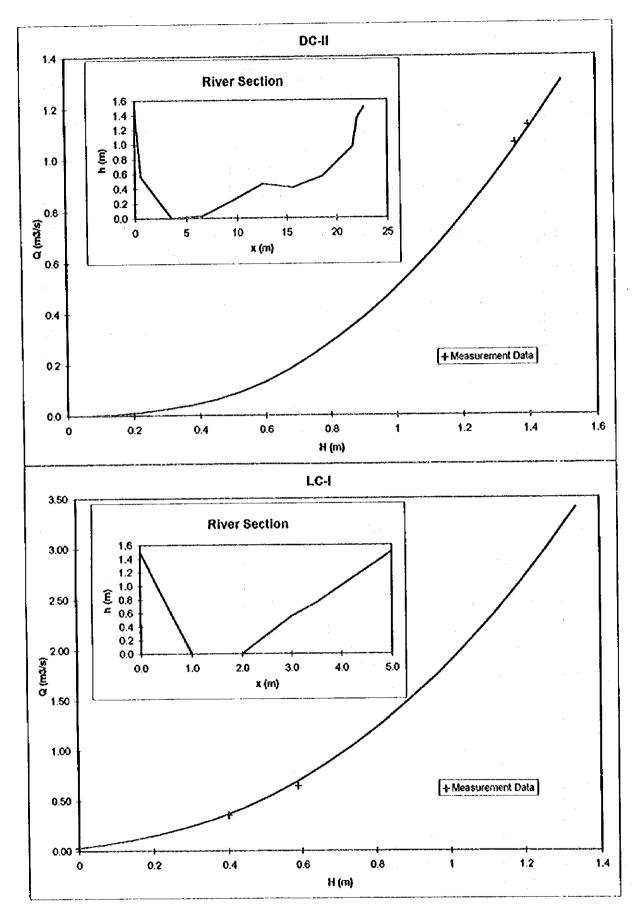
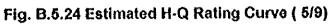


Fig. B.5.24 Estimated H-Q Rating Curve (4/9)





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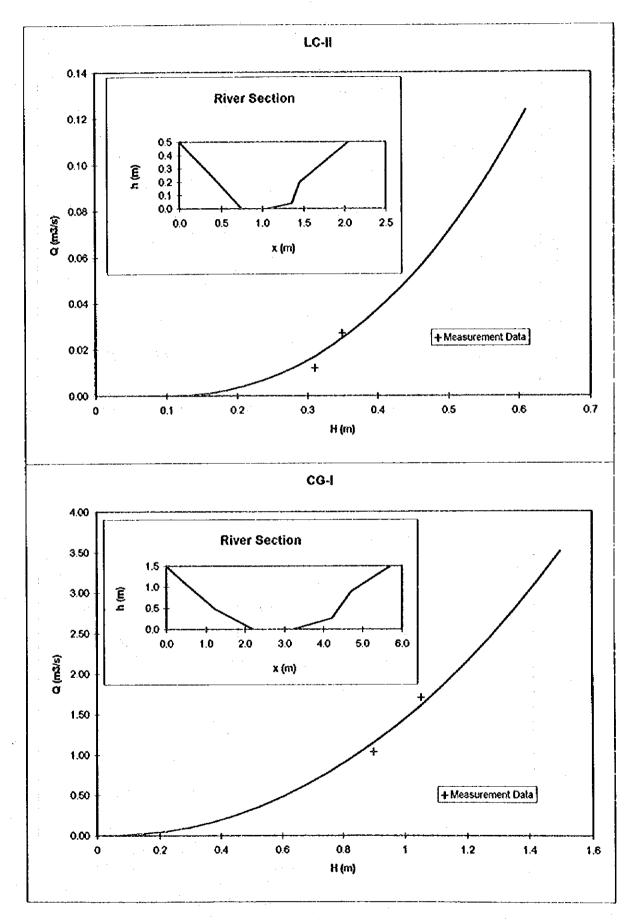
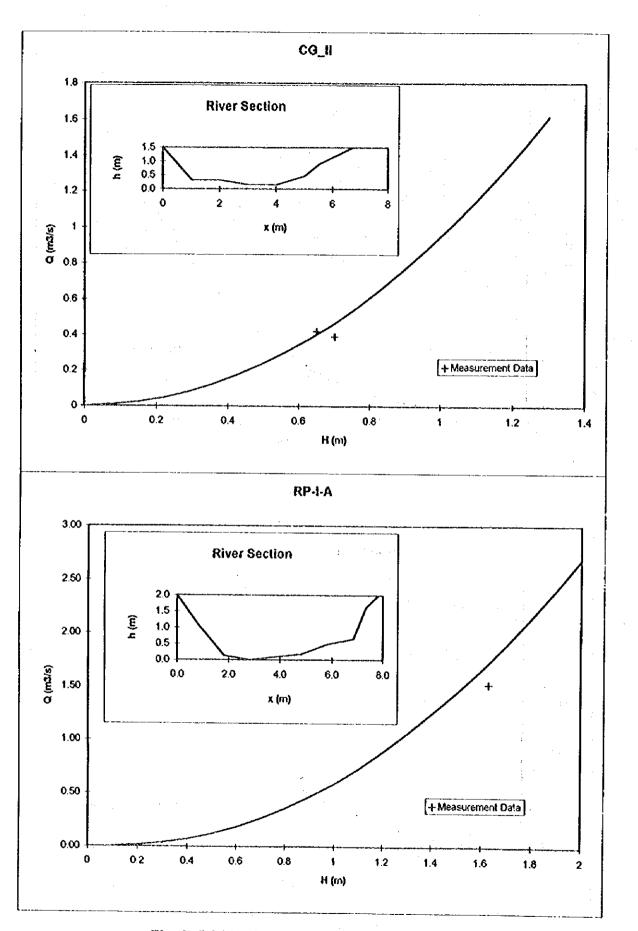


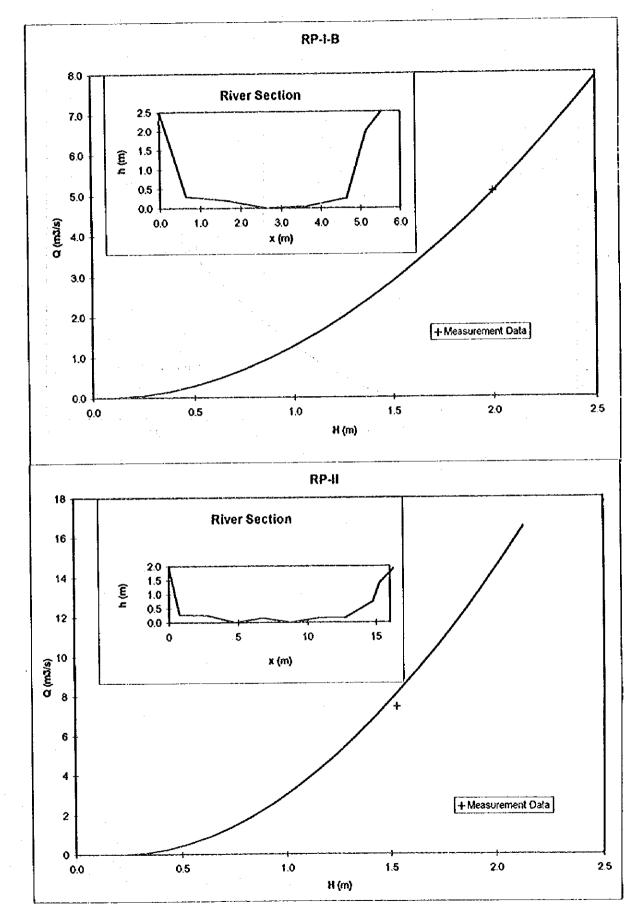
Fig. B.5.24 Estimated H-Q Rating Curve (6/9)



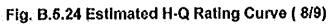
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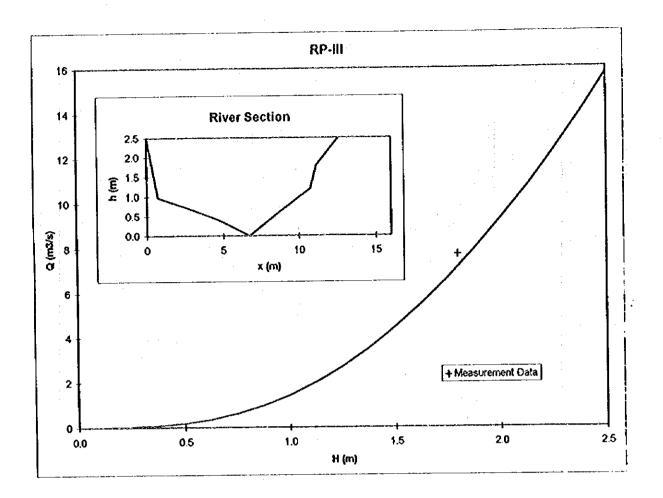
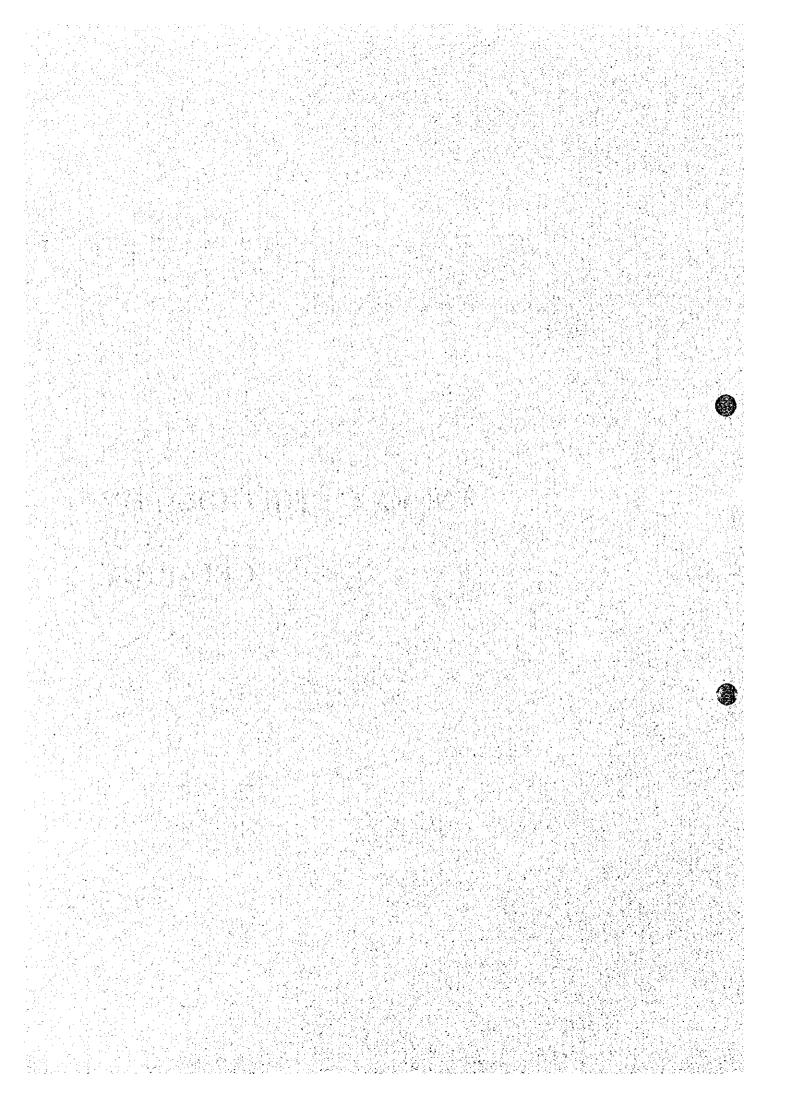


Fig. B.5.24 Estimated H-Q Rating Curve (9/9)

ANNEX C : TOPOGRAPHY AND GEOLOGY



ANNEX C: TOPOGRAPHY AND GEOLOGY

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ANNEX C: TOPOGRAPHY AND GEOLOGY

C.1 Introduction

A geological survey was carried out to verify the geological foundation and geotechnical properties of the study area.

C.2 Topography

The area is surrounded by mountains more than several thousand meters high; to the north the Septentrional mountain range and to the south the Central and Oriental mountain ranges. These mountains gradually ascend from west to the east. In the vicinity of the study area they are only about 100-300m. The study area itself is on a low lying alluvial plain about 5 - 20 meters above sea level, situated in between these mountains and formed from the deposits of the Yuna River, Payabo River, and Cevicos River which flow eastward. With a gradient of 1/1000, the area descends in the direction of the Samana Bay.

The south of the study area is bordered by the Los Haitises mountains where a karst region is found. A precipice originated by fault developments separates these two areas.

C.3 Geology

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The study area is geologically divided into the northern mountains and southern mountains. The former is made up of metamorphic rocks, which are distributed on the northern side of the Nagua River, intercalated with composite cretaceous rocks. The latter is made up of the La Tabela and Las Sombrerito formations from the lower Eocene to the Middle Oligocene epochs. The southern slope of this mountain is distributed with Lagurabo formations of the Pliocene to the Pleistocene epochs.

These metamorphic rocks mainly consist of amphibolites and gneiss. The La Tabela formation and Las Sombrerito formation are mainly made up of conglomerates such as limestone, shale, andesites and sandstone. The La Gurabo formation is mainly made up of the stratification bedding plane layers of shale, tuff, and sandstone. The northern side of the study area is basically made up of metamorphic and composite rocks.

Composite cretaceous rocks widely distributed in the upstream area of the Yuna River make up the basement rock layer of the southern mountains. Limestone and calcareous sandstone of the Pliocene and Pleistocene epochs make up the Los Haitises mountains to the south of the study area.

Tertiary volcanic rocks distributed in the upstream area of the Yuna River, limestones that form the Los Haitises mountains, and the metamorphic rocks of the northern area all constitute the basement rock layer of the study area. Overlying this basement rock is a layer of Quaternary diluvial thin gravel, sands and clay, which in turn is overlain by alluvial sediments of the Yuna and Payabo rivers. The alluvial sediments are from the Holocene epoch and mainly consist of clay and sand.

The geological map of the study area is in Figure C.3.1.

C.4 Field Investigation

Field investigation was carried out by excavating 10 exploratory boreholes and 2 borrow pits. Eleven (11) undisturbed samples were taken from the boreholes while two (2) samples of embankment material were taken from the borow pit. The extracted samples were analysed. Figure C.4.1 shows the location of exploratory boreholes and borrow pits in the study area.

C.4.1 Exploratory Boring

The quantity of exploratory boring carried out is shown in Table C.4.1.

No.	Location	Depth (m)	Standard Penetration Tests	Number of Undisurbed Samples
1	Payabo River	19.50	14	2
2	Ponton Pond	24.00	17	2
3	Cevicos River	12.00	9	-
4	Arrenquin Pond	12.50	10	1
5	PAYABO	15.00	12	-
6	Canal Guaranguao	10.50	8	2
7	REFORMA	10.50	8	1
8	Cascarilla Pond	12.00	9	
9	Payabo River	24.50	18	2
10	Los Cocos	21.65	15	_
	Total	163.05	120	11

Table C.4.1 Quantity of Exploratory Boring

C.4.2 Test Pit

Of the structures planned for the study area, the most important is the disaster prevention dam to be constructed on the Payabo River.

Two (2) types of soil material from the two borrow pits were selected based on the field survey results: soil consisting of flood sediments of the Payabo River, distributed in the vicinity of the study area, and soil made up of weathered limestone, namely Caliche, which is usually used as an embankment material of roads in the vicinity.

The dimensions of the borrow pit are $1 \times 1 \times 1.5$ m, and the embankment material was extracted from a depth of more than 1.5m. Table C.4.2 shows the number of borrow pits dug.

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Table C.4.2 Number of Borrow Pits

No.	Location	Number of Samples
Tp-1	Rio Payabo	1
Tp-2	Rio Cevicos	1
	Total	2

C.4.3 Laboratory Soil Testing

The undisturbed samples from the boreholes and the samples taken from the borrow pits were analysed in a laboratory in accordance with ASTM methods (American Society for Testing and Materials). Table C.4.3 shows the soil tests carried out.

	1	Number of Samples	
Type of Test	Undisturbed Samples	Embankment Materials	Total
Physical Property Test			
Specific Gravity		2	13
Water Content	11	2	13
Grading Analysis	11 .	2	13
Allerbert's Limits	11	-	13
Unit Weight	11	2	11
Mechanical Property Test			
• Triaxial Compression (UU)	11	2	13
Consolidation	11	-	11
Compaction	-	2	2

		Table C.4.3	Laboratory Soil Test	\$
(1, 2, 3, 3)		1.	and the second	

C.5 Study Results

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C.5.1 Exploratory Boring

The exploratory boring results are shown in Table C.5.1, while Figure C.5.1 shows the geological profile. The results of the standard penetration test are shown in figures C.5.2 and C.5.3. The details of the results are shown in Appendix C.1.

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Geological Period	Epoch	Symbol	Soil Quality	Thickness of Layer (m)	N-Value	Average N-Value
Quaternaly	Alluvium		Gravely Clay	0.8		
		Bs	Clay	-	3 - 17	8
			Sandy Clay	0.5		
		Ac	Clay-Sandy Silt	2.0 - 18.0	2 - 20	5
		As	Sand	3.0	10 - 41	27
		Ag	Gravel	2.0 - 4.0	37 - 50<	50<
	Diluvium	Dc	Clay	- ·	13 - 50<	28
		Ds	Sand-Clayey Sand	30-40	42 - 50<	50<
		Dg	Gravel	-	50<	
Tertiary	Pliocene	Tc	Clay	-	34 - 50<	46

Table C.5.1 Results of the Exploratory Boring

As indicated in the geological profile, the ground foundation in the study area is divided into 8 layers.

(1) Topsoil (Bs)

The topsoil in the study area is mainly used for the banking of roads and rivers. Caliche, weathered limestone, is usually used for road embankments, while river levees are formed of clayey soil.

(2) Alluvium

The alluvial layer is made up of sub-layers of clay, gravel, and sand.

The clay sub-layer is distributed over the entire study area. It is 20m thick in the vicinity of Ponton pond, averages about 10m thick from Los Cocos to the Cevicos River to the west, and is 13m at the Payabo River where the disaster prevention dam will be constructed.

The thickness of this sub-layer increases in the northerly direction from the downstream section of the Arrenquin canal. But it is only 3 - 7m from Los Cocos to the direction of the Cascarilla drainage canals to the east. The N value ranges from 2 - 20, averaging 5.

The distribution of the sand (As) and gravel (Ag) sub-layers were investigated at the Arrenquin canal and Los Cocos area. The sand layer is made up of homogeneous fine sands, while the gravel layer mainly consists of rounded gravel. The N value in the sand layer ranges from 10 - 41, averaging 27, and 37 to more than 50 for gravel.

(3) Diluvium

The diluvial layer consists of three sub-layers: clay, sand and gravel.

The clay of this layer is distributed over the whole study area, except in the Cevicos River site, and is overlain by the clay sub-layer of the alluvial deposits. The clay in this layer is extremely hard with an N value ranging widely from 13 to more than 50; averaging 28.

The terrain is undulating and sedimentary changes are quite irregular due to the erosion and inundation brought about by the rivers Cevicos, Yuna and Payabo. In particular, a deep gorge has developed in the vicinity of the Ponton pond at the mouth of the Payabo River.

The sand layer (Ds) is evenly distributed in the Payabo River area and partially intercalated with clay. The N value has a narrow range, from 42 to more than 50.

The gravel layer (Dg) lies underneath the sand layer in the Los Cocos area. Gravel in this layer is round and measures 5 - 20 mm. The N value is more than 50.

(4) Tertiary Pliocene

Clay (Tc) of the Tertiary Pliocene is restricted to the western end of the study area, the Cevicos River area. The core of this layer is made up of reddish brown clay. Underlying this layer is the basement rock that along with limestone constitutes the Los Haitises mountain. This basement rock layer has become clayey due to weathering. The limestone rock layer is mixed with a tot of gravel.

Caliche is the soil material most commonly used for road embankments in the study area.

C.5.2 Laboratory Test Results

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The results of the analysis on the undisturbed samples and the samples of embankment materials are as shown below. The details are summarized in Appendix C.2.

(1) Results of the analysis of undisturbed samples

The results of the analysis are shown in Table C.5.2 and are summarized in Fig. C.5.4 - C.5.8

						Numt	er of Boreho	oles		· · ·
	Characteristic			No.1	No.2	No.4	No.6	No.7	No.8	No.9
	Gravel		(%)	1-2	0-2	0	0-5	4	3	2
Gradiation	Sand		(%)	6-3	10-11	5	11	14	13	8.17
	Silt+Clay		(%)	90-93	89-90	95	84-89	82	82	81-90
	Liquid Limit	WL	(%)	45-46	42-44	50	43-47	48	43	39-50
Consistency	Plastic Limit	Wp	(%)	21-23	22-24	22	22-24	22	22	20-23
	Plasticity Index	Ip	(%)	23-24	20-22	28	21-23	26	21	19-27
Specific Ora-	vity of Soil	ps	(g'cm')	2 43 -2.62	2.49-2.65	2.49	2.60-2.62	2.55	2.65	2.55-2.6
	Water Content	W'n	(%)	15-21	37-42	20	21-26	20	28	25-31
Natural	Wel Density	ρt	(g'cm')	1.79-1.81	1.79-1.80	1.86	1.80-1.84	1.79	1.77	1.83-1.8
State	Void Ratio	è		0.56-0.75	0.91-1.09	0.60	0.75-0.79	0,71	0.91	0.74-0.8
	Degree of Saturation	Sr	(**)	65.1-73.3	100	83	72.8-86.2	71.8	82.6	86.1-10
Triaxial	Cohesion	¢	(kgf'cm')	0.9-1.2	0.70	0.65	0.4-0.55	0.95	•	0.7-1.0
Compression	Angle of Internal Friction	¢	0	0	0	0	5-6	0	-	0
Consoli-	Consolidation Yield Stress	Pc	(kgf'cm')	1.40	1.30	1.10	1.40	1.30	1.40	1.30-2.3
dation	Compression Index	Cc	/	0.225	0.14	0.17	0.23	0.17	0.15	0.06-0.1

T	a	ble	e (C.	5	.2	,	R	es	ul	its	0	f	tł	ie	Å	h	a	lv:	sis	0	f	U	11	di	ist	tu	rb	e	d	S	am	ole	es

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1) Physical Characteristics

The gradation curve of alluvial clay in Fig. C.5.4 shows that more than 80% of the alluvial clay is made up of fine grained soil (silt and clay). The consistency properties of this clay type: liquid limit (WL) of 39-50%, plasticity limit (Wp) of 20-24%, plasticity index (Ip) of 19-29. These figures are classified under "CL" in the plasticity chart shown in Fig. C.5.5.

Soil density (ps) was observed at 2.43 - 2.65 g/cm³. The natural water content (*Wn*), 15-42%, was considered low for a clay layer. Wet density was measured at 1.77-1.89 g/cm³.

2) Mechanical Properties

The shear strength properties of the alluvial clay (Ac) are shown in Figures C.5.6 and C.5.7. Although the values range widely, the average cohesion, $c = 0.90 \text{ kgf/cm}^2$ led to the conclusion that the angle of internal friction (ϕ) is 0.

Figure C.5.8 shows the relationship between the preconsolidation pressure and depth plot of alluvial clay. Although the values vary widely, consolidation shearing strength was found to increase with depth, a condition that exceeds the limits of the effective overburden pressure (ov). Therefore, clay in this layer is considered to be excessively consolidated with an average overconsolidation ratio of 2.

(2) Embankment Material

The results of the analysis of embankment materials are shown in Table C.5.3 and summarized in the figures (Fig. C.5.9 - 12).

		Number of	Boreholes		
	Characteristic			Tp-1	Tp-2
	Gravel		(%)	64	7
Gradiation	Sand		(%)	24	14
	Silt+Clay		(%)	12	79
	Liquid Limit	WL	(%)	34	39
Consistency	Plastic Limit	Wp	(%)	18	21
•	Plasticity Index	Ір	(%)	16	18
Specific Gravit	y of Soil	ρs	(g/cm ³)	2.67	2.60
Natural Water	Content	Wa	(%)	18	29
Triaxial	Cohesion	c	(kgf/cm ²)	0.6	0.4
Compression	Angle of Internal Friction	\$	(°)	8	3
Compaction	Maximum Dry Density	ρ dmax	(g/cm ³)	1.927	1,531
· ·	Optimum Moisture Content	Wopt	(%)	12.0	23.0

1) Physical Properties

The gradation curve of embankment materials shown in Figure C.5.9 indicates that 64% of Tp-1 is gravel and 24% is sand. On the other hand, Tp-2 is considered clayey as it is 80% fine grained soil (silt and clay). The consistency properties are: liquid limit (WL), 34-39%, plasticity limit (Wp), 18-21%, and plasticity index (Ip), 16-18. These figures are classified under "CL" in the plasticity chart.

Soil density (ps) ranges from 2.60-2.67 g/cm³ and natural water content (Wn) is 18% for Tp-1 and 29% for Tp-2.

2) Mechanical Properties

The relationship between soil moisture and density was assessed using a rammer and is shown in Figure C.5.11. The figure shows Tp-1 having a maximum dry density (ρ dmax) of 1.927 g/cm³ and an optimum moisture content (Wopt) of 12.0%. The maximum dry density (ρ dmax) and optimum moisture content (Wopt) of Tp-2 are 1.531 g/cm³ and 23.0%, respectively.

The results of the compaction test shows that compaction takes place when the maximum dry density is 95%. A triaxial compression test was then carried out on the compacted materials, the results of which are shown in Figure C.5.12.

	Shear Strength	
Borrow Pit	Cohsion (kgf/cm²)	Angle of Internal Friction (°)
Tp-1	0.6	8
Tp-2	0.4	3

The shear strength of the materials used are shown below.

(the shear strength figures shown above were obtained when the wet side of the materials was subjected to a 95% compaction).

If the wet weight of the materials was subjected to 90% compaction, the shear strength of these materials will significantly decrease as the water content exceeds the optimum water content by more than 5%. Accordingly, a compaction of 95% is required.

The shear strength of the embankment material is influenced by the degree the field is compacted. Therefore, it is necessary to re-examine field conditions and the construction works in the site.

C.5.3 Foundation Construction Plan

(1) From the Cevicos River to the Guaraguao Area

The construction of a spillway, cut-off gate, diversion weir, and drainage pipe and levee are planned for this area. As mentioned in the test boring results, the alluvial clay layer is thick in this area.

Hence countermeasures required for the construction of these structures are as follows:

1) Spillway • Cut-off Gate

As these are structures to be permanently constructed in the Cevicos River and Payabo River areas, their foundations should be stable to prevent ground subsidence. Accordingly, piled foundations are proposed.

In the Cevicos River area, the bearing layer will be the clay layer (Tc) of the Tertiary Pliocene, while the clay layer (Dc) of the Quaternary Diluvium will be the bearing layer in the Payabo River area.

2) Diversion Weir • Drainage Pipe • Levee Embankment

These structures will be constructed in the area of the Ponton pond, Arrenquin canal, and the Guaraguao drainage canal.

Since soil tests were not carried out on the surface layer, a bearing force of 5 tf/m² is estimated assuming the average N value five (5) meters from the surface layer.

The construction of the diversion weir and drainage pipe is possible in these sites as they are both comparatively small in scale and load. To construct a secure levee on soft grounds, a stable gradient should be established.

As to consolidation settlement, the construction of the levee is estimated to put an additional pressure of 1 - 2 tf/m² on the ground thereby compressing the clay layer reducing the original thickness by about 5 - 10%.

Given these conditions, extra banking methods are proposed.

(2) From the Reforma to the Cascarilla Drainage Canal

The construction of main roads is planned for these areas.

According to the exploratory boring results, the alluvial clay layer in this area is 1.5 - 2m thick. However, the roads in the vicinity of the study area and the boring sites are 1-2m lower than the paddy fields presumably because of the road embankments and consolidation due to traffic load.

The thickness of the alluvial clay layer in the paddy field area is estimated to range from 3-4m. Therefore, it is assumed that 50 - 60% of the alluvial clay (Ac) in the study area, according to the exploratory boring results, has been compacted. The laboratory tests also prove that this alluvial layer is made up of overconsolidated clay with a consolidation ratio of 2.

It is assumed that only about 5 - 10% of the clay layer will be compressed by the construction of the planned road embankment because the banking height will be limited to 1m, and the load, including traffic load, will only amount to $1 - 2tf/m^2$.

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(3) Payabo River Area

An intake weir and an earth disaster prevention dam are to be constructed in this site.

Outline of Dam Structure:

Length:550mHeight:12.2 ~14.8mGradient unstream:1.2.0	Type of dam:	Homogeneous dam
•	Length:	550m
Gradiant unstroom: 1.2.0	Height:	12.2 ~14.8m
Oracient upstream, 1,5,0	Gradient upstream:	1:3.0
Gradient downstream: 1:2.5	Gradient downstream:	1:2.5

1) Stability of the dam

The embankment of a homogeneous earth dam is made of soil, and the dam itself is usually constructed on soft grounds. The slope gradient of this dam type is greatly influenced by the ground foundation and the strength of the bearing layer. Basically the gradient upstream is 1:3.0 \sim 4.0 and 1:2.0 \sim 3.5 downstream.

The dam will be constructed on soft grounds as the study area is distributed with the thick clay (Ac) layer. Therefore, the planned dam design should be followed to construct a stable dam.

2) Consolidation Settlement

The construction of the dam will result in an additional ground pressure of 20 - 25tf/m². The clay layer that will remain after the excavation work for the dam is expected to settle by 10%. However the settlement may be greater if the clay layer is intercalated with a heterogeneous layer having a low N-value.

b.

Given these conditions, the following methods were proposed:

Replacement Method

a.

1

Complete Replacement

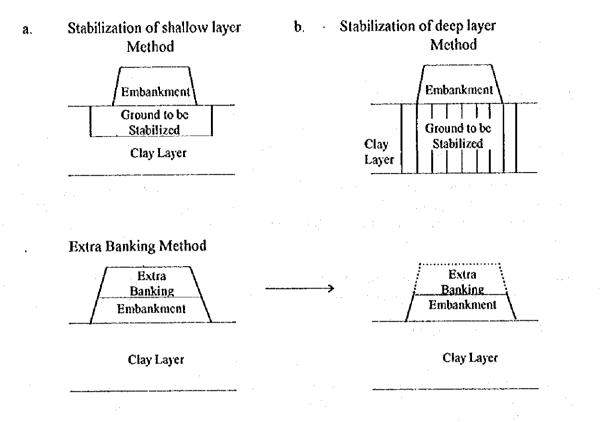
Embankment Replacement Soil Clay Layer

Partial Replacement

Embankment Replacement Soil Clay Layer

C:- 9

Stabilization Method



The replacement and stabilization methods in contrast with the extra banking method are not economical in terms of design or construction.