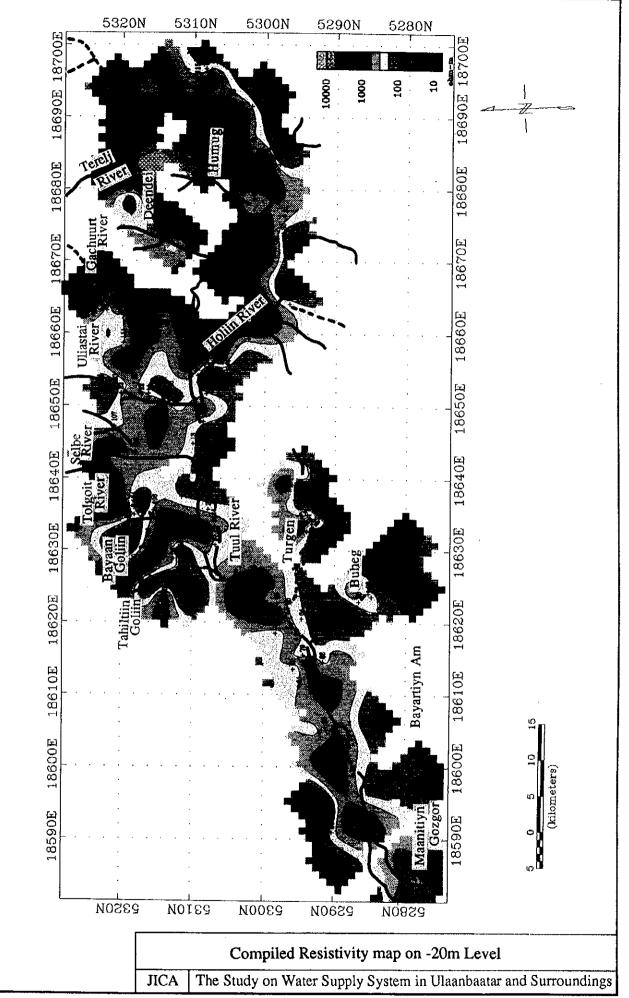
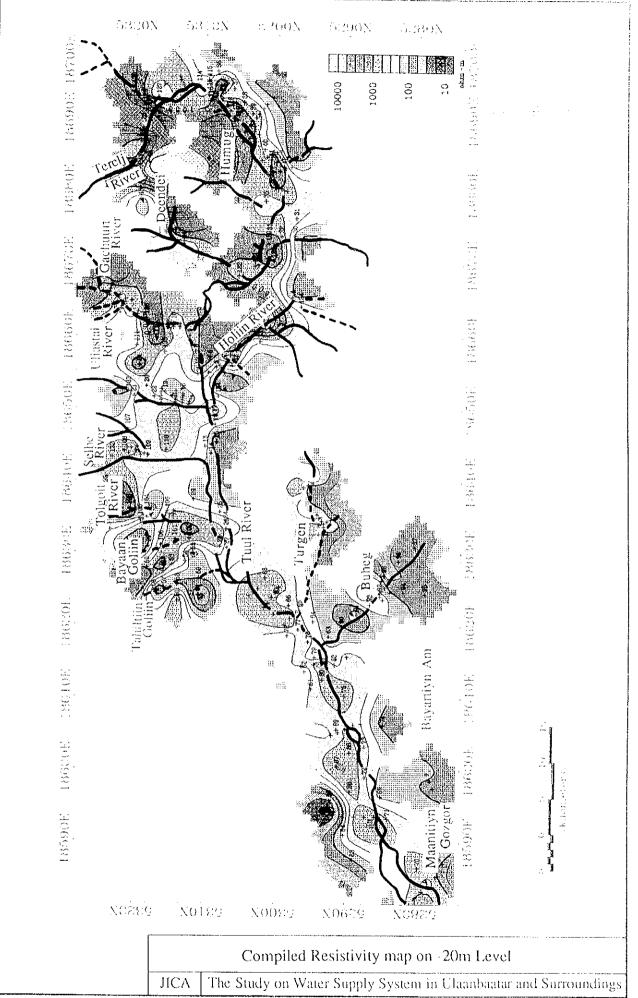
## Appendix I.2.4

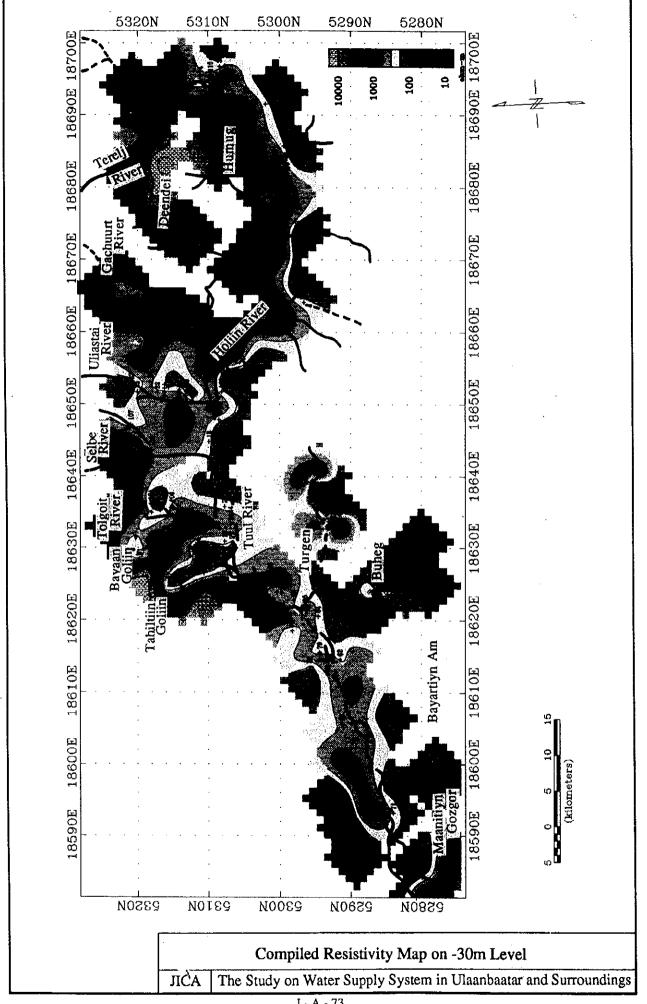
## Compiled Resistivity Map



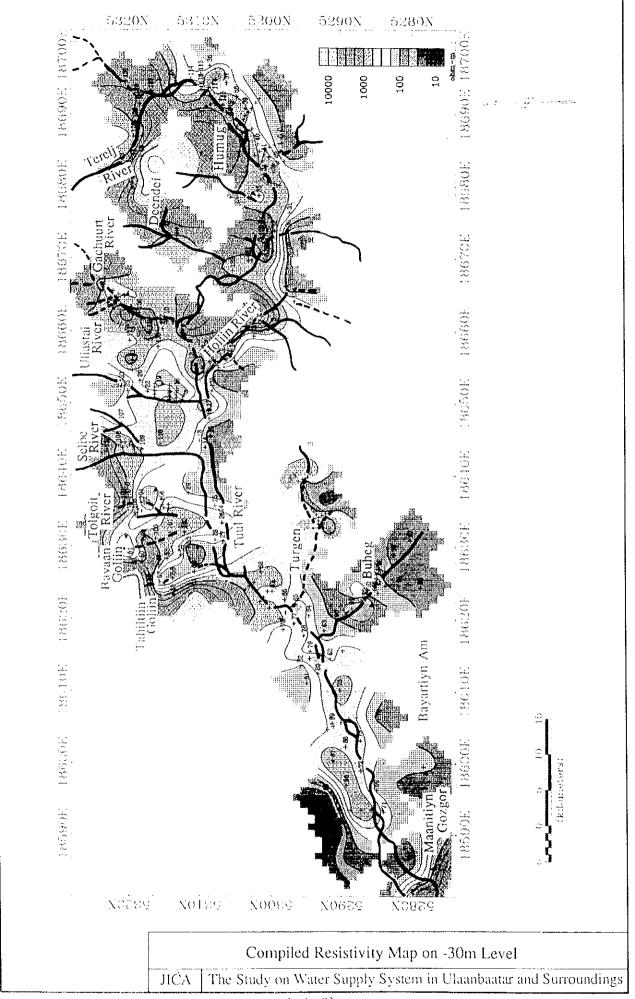


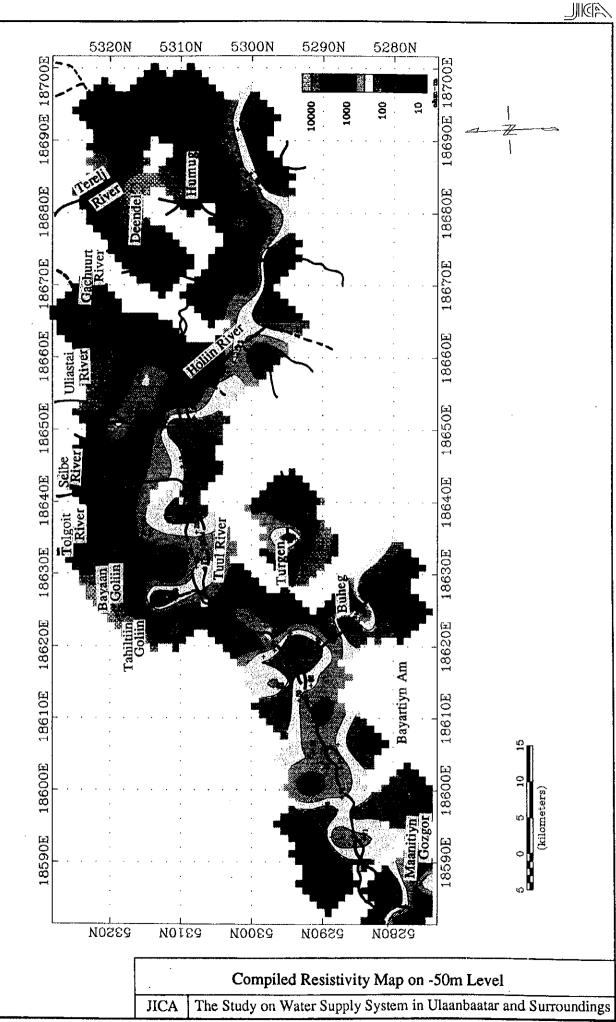


JIIGA

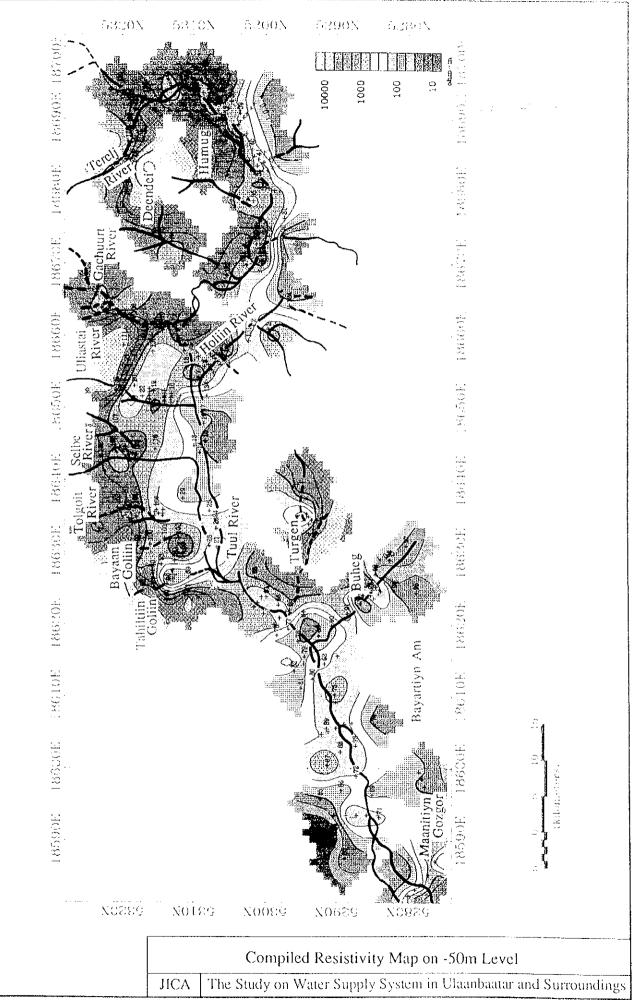




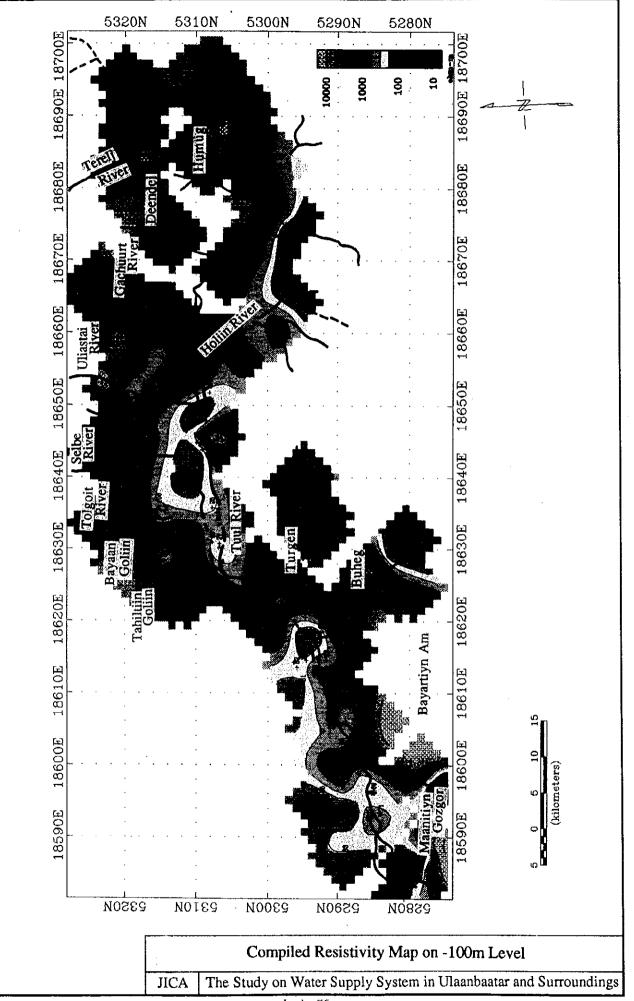




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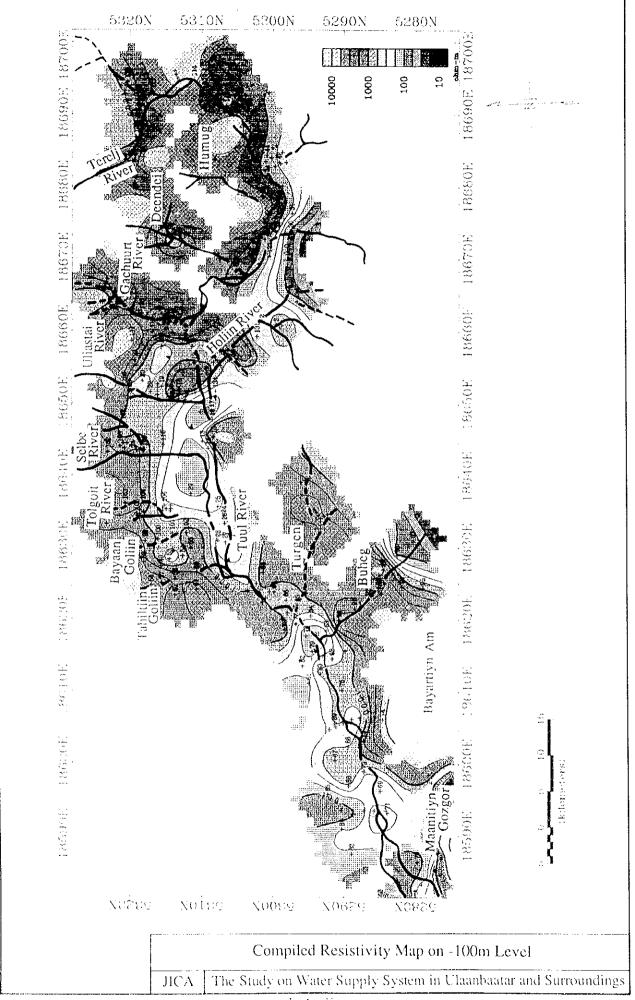


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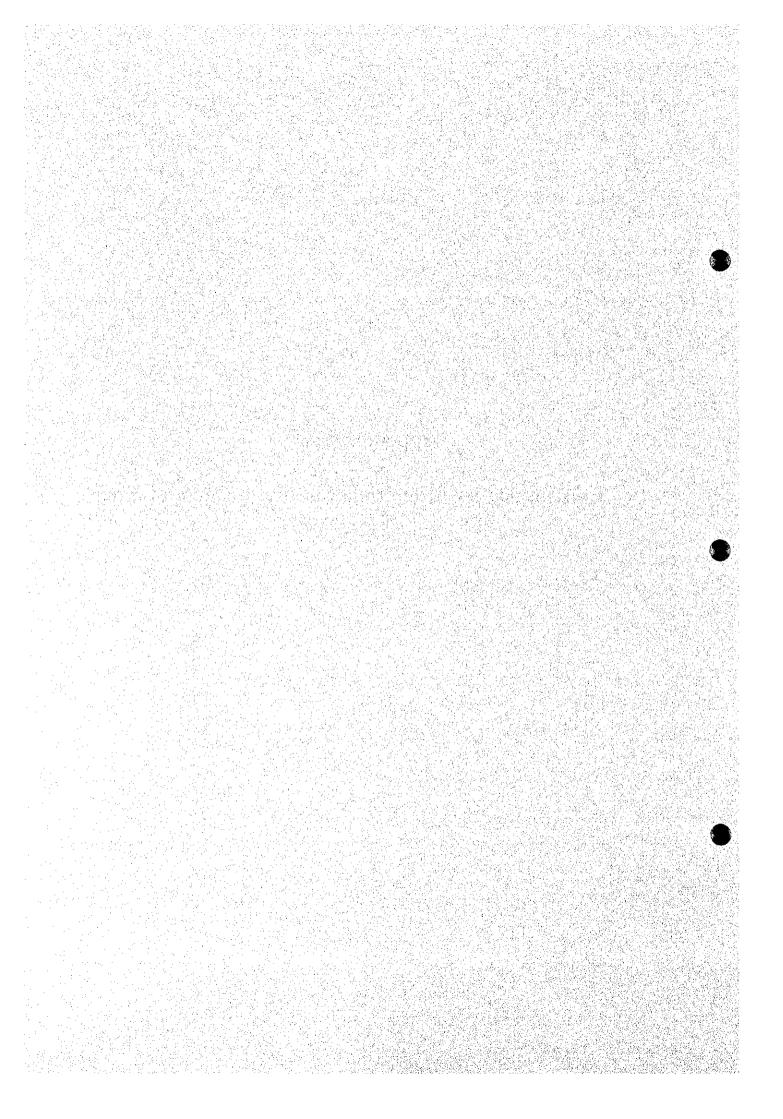
**.** 



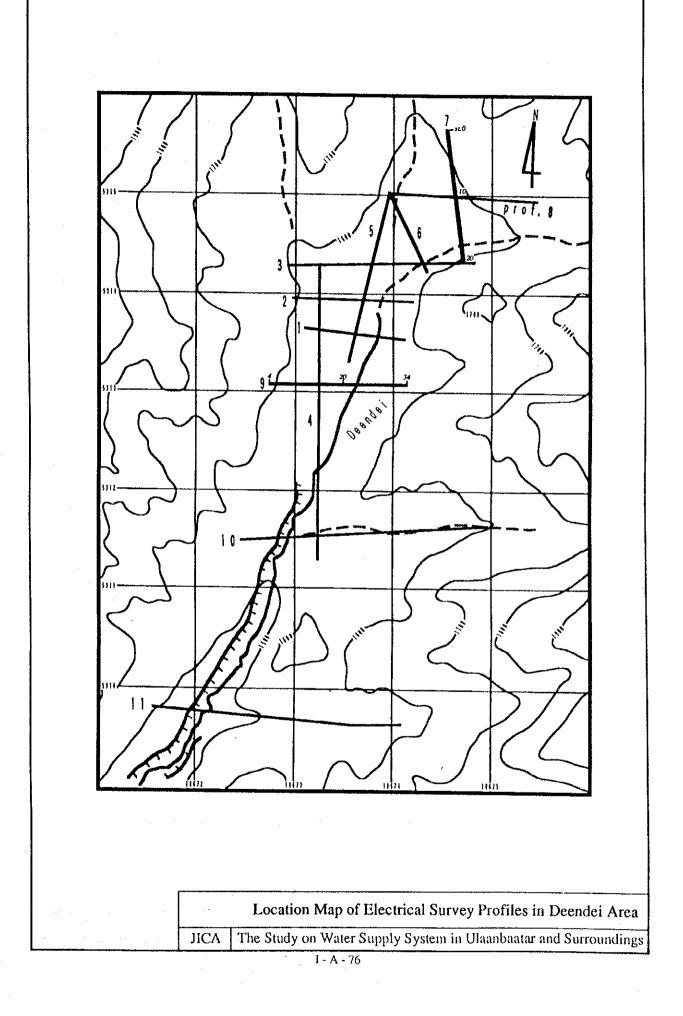


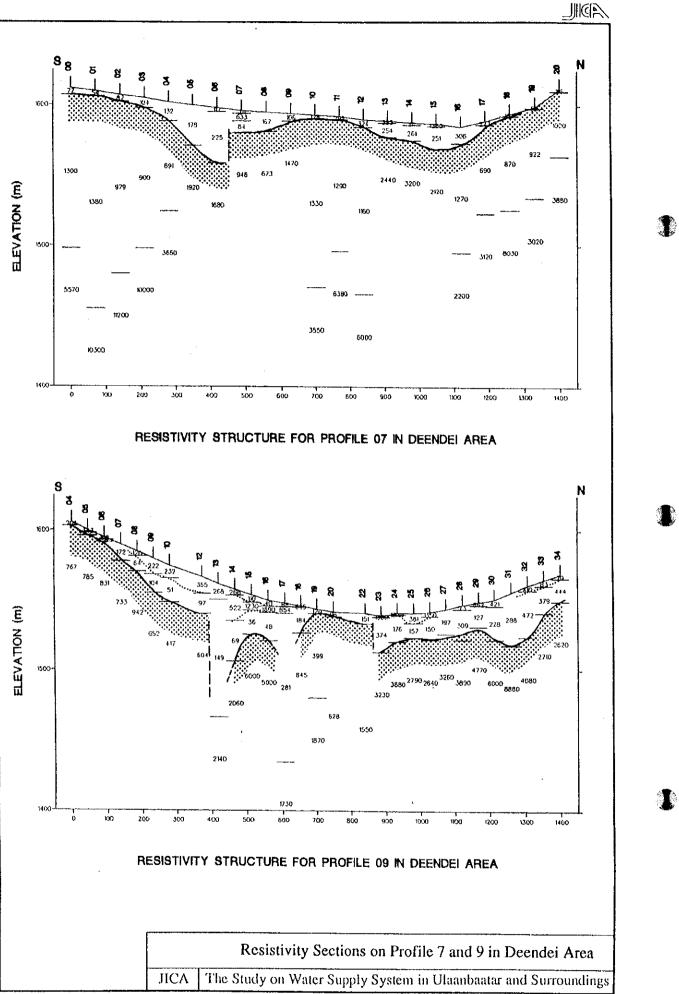
## Appendix I.2.5

Existing Data of Electrical Survey in Deendei Area



AM



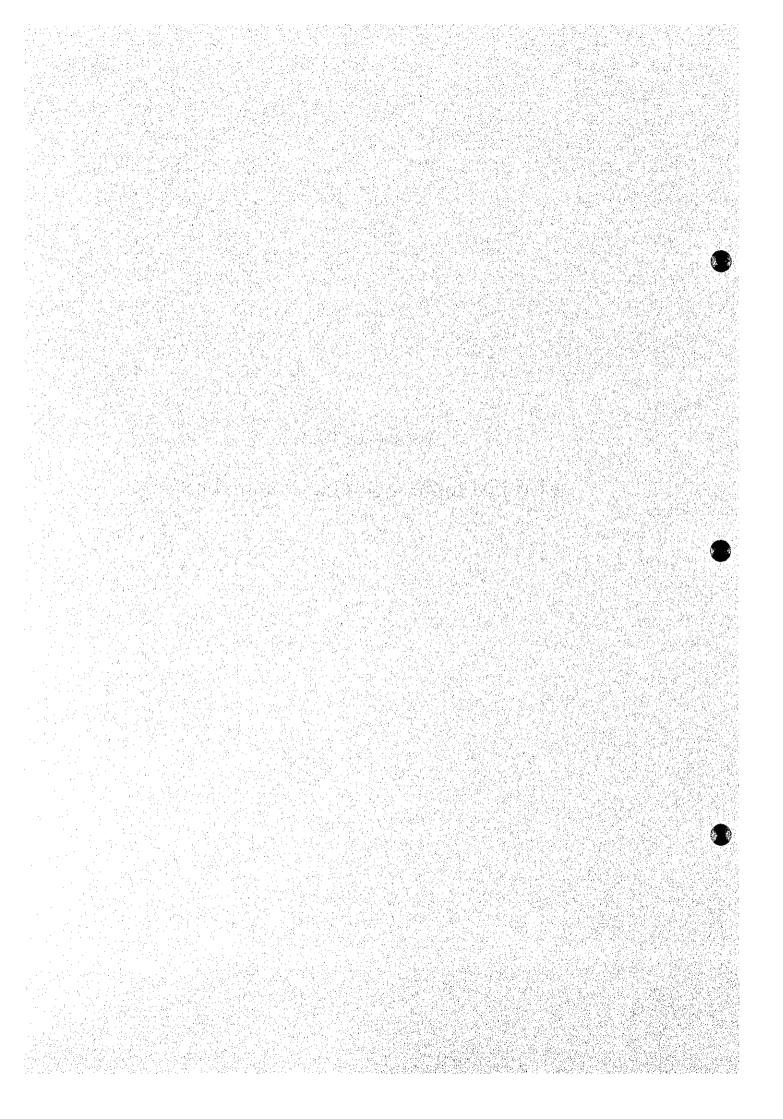


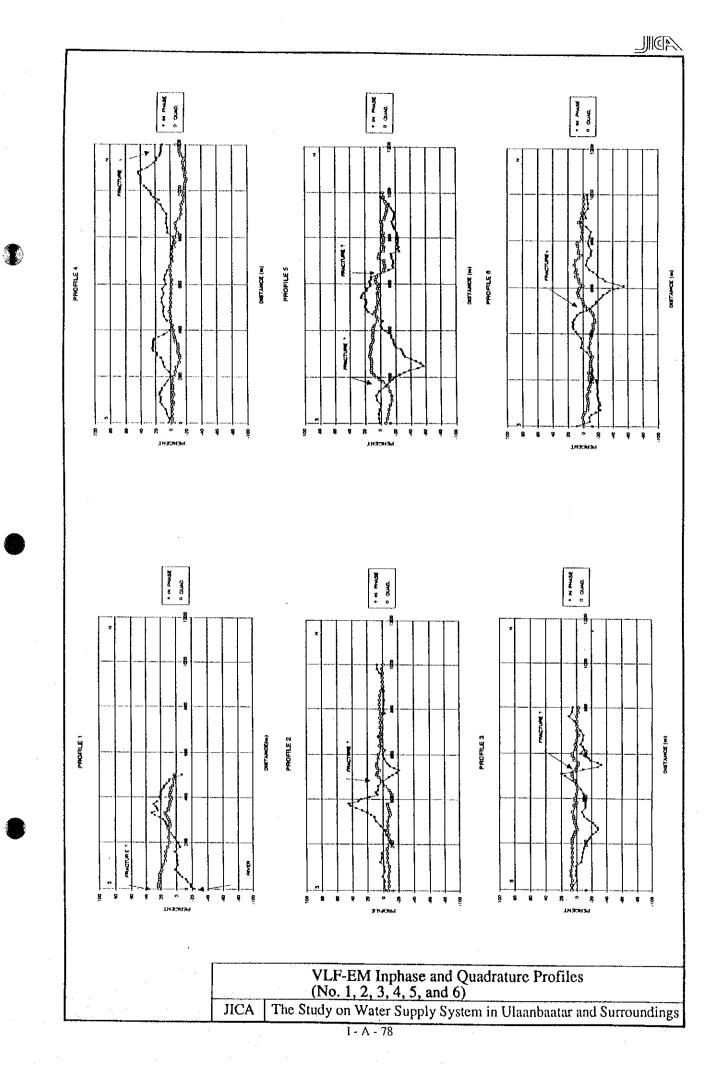
I - A - 77

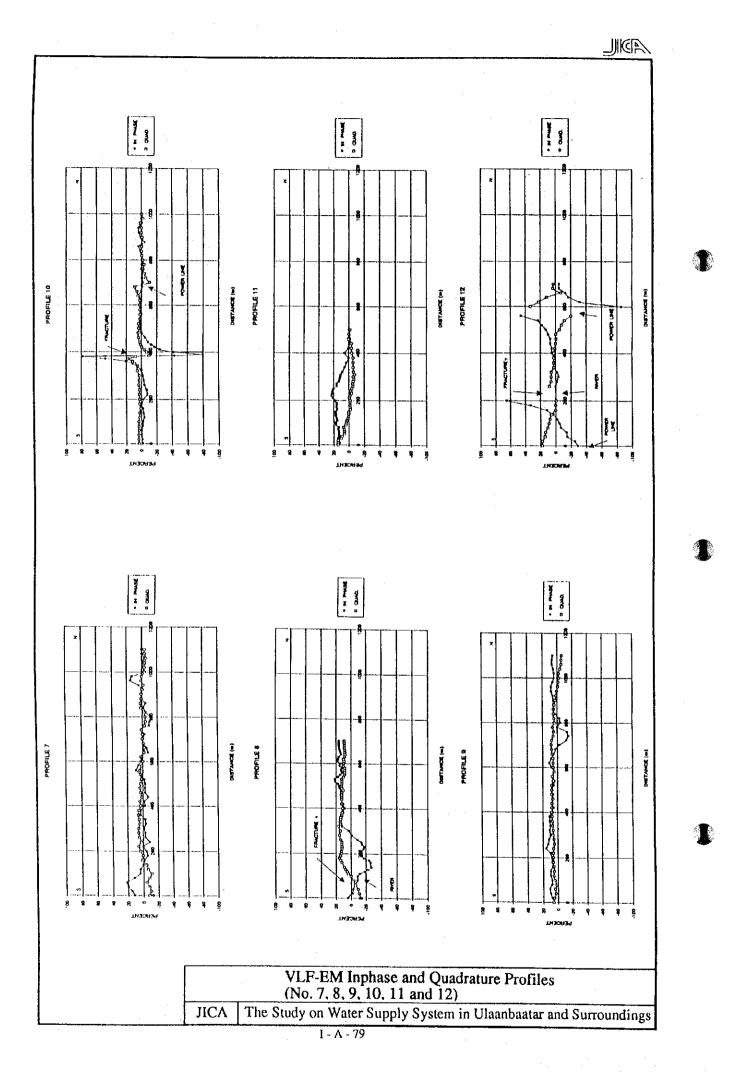
•

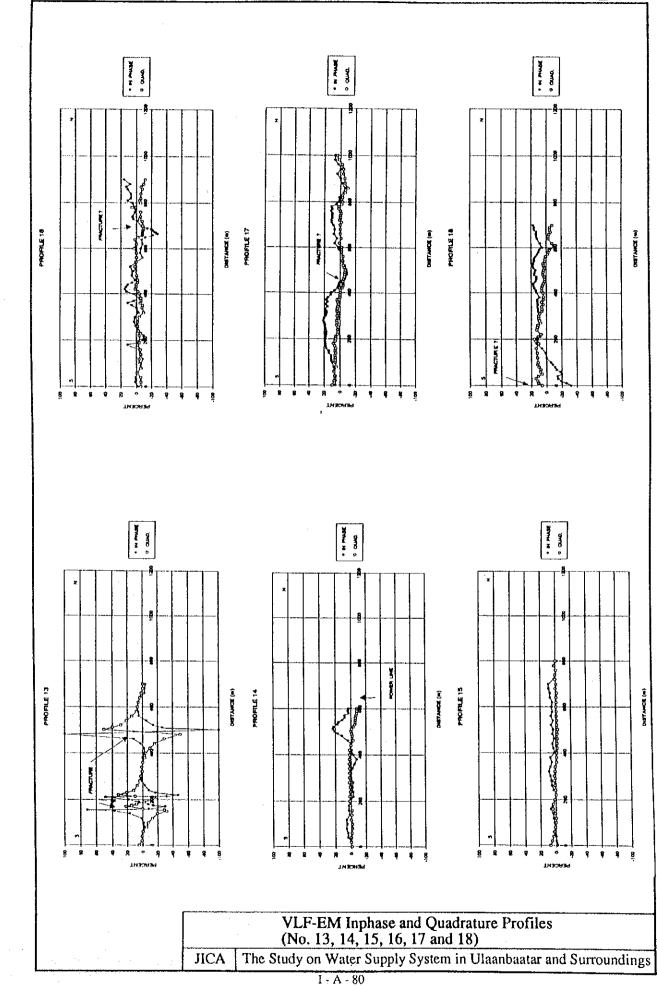
Appendix I 2.6

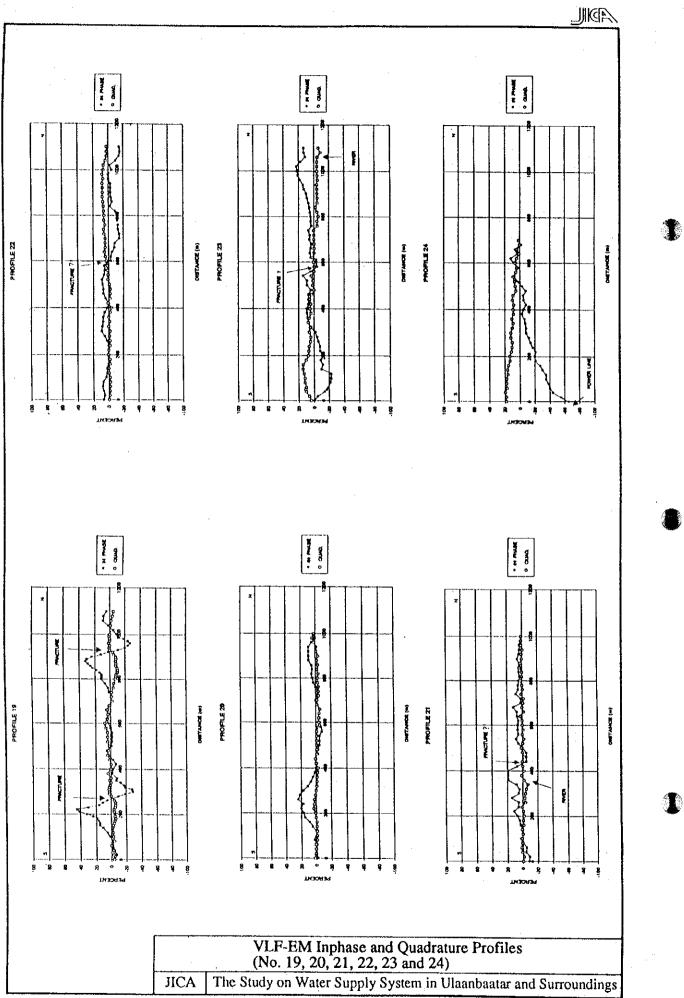
VLF-EM Inphase and Quadrature Profiles

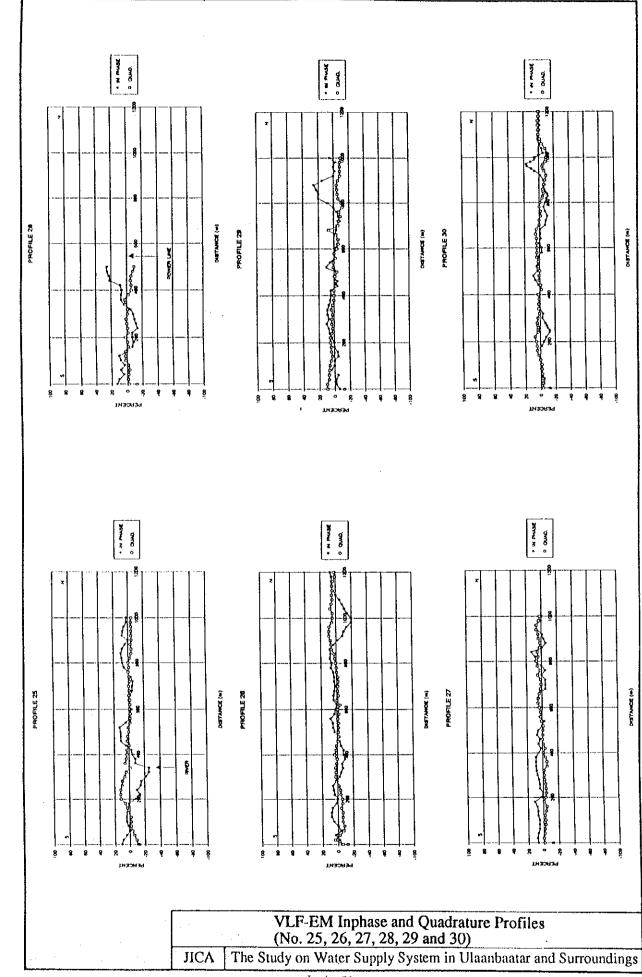




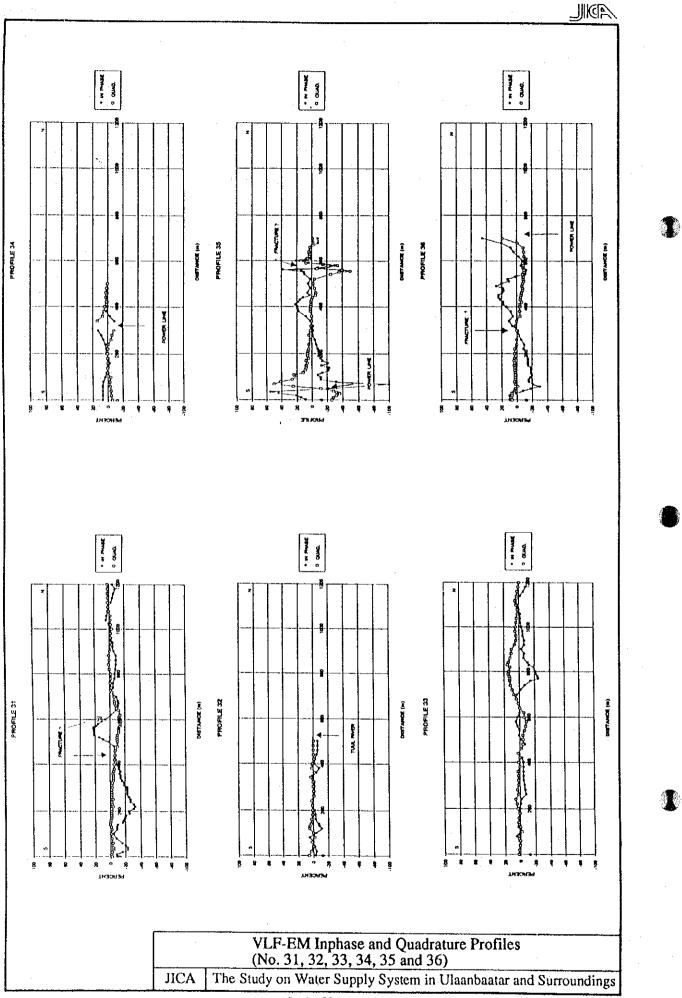






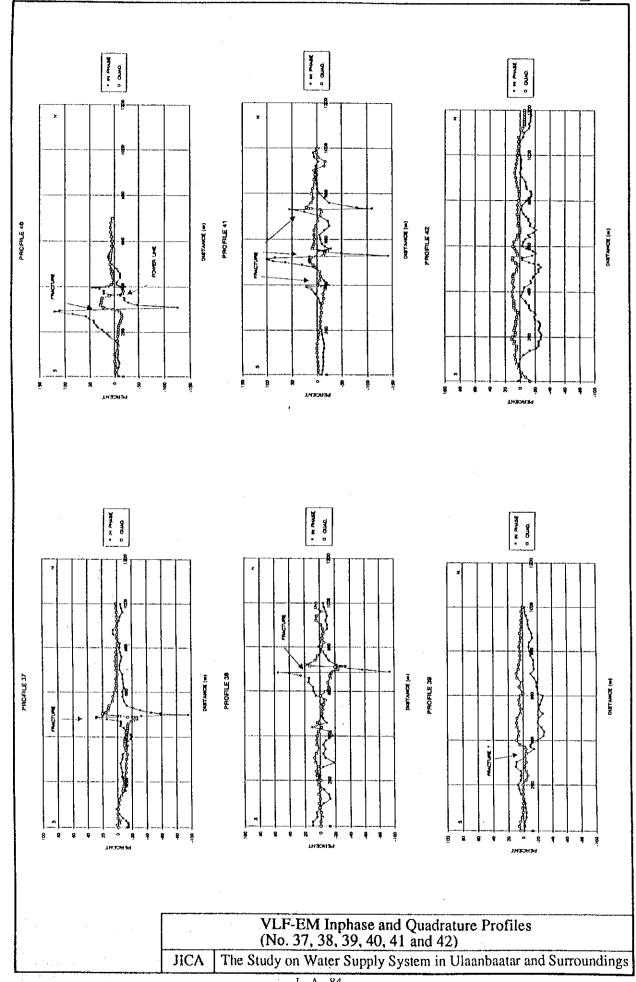


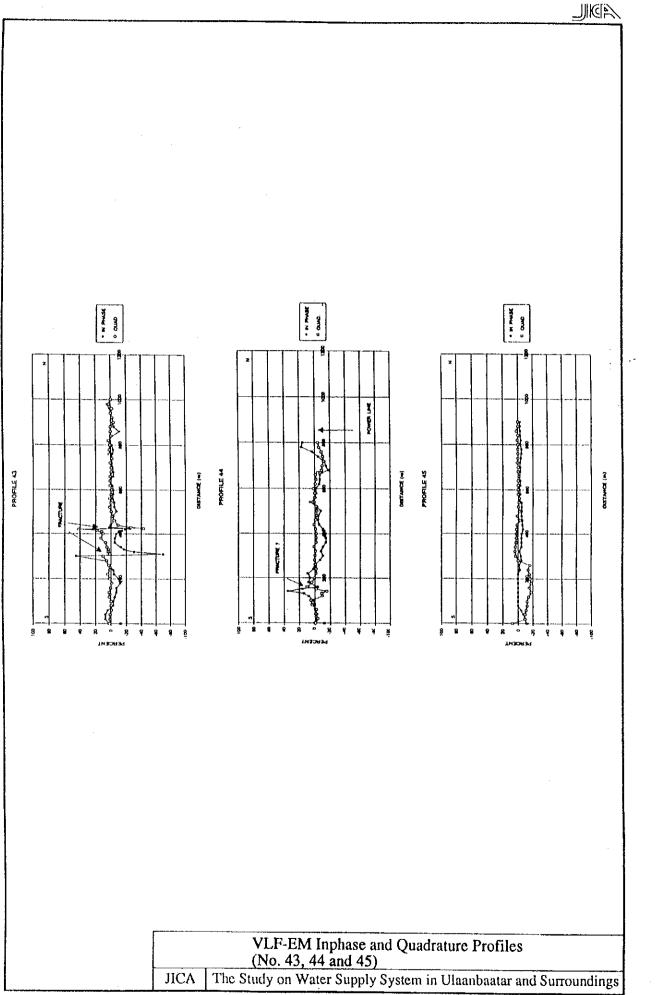
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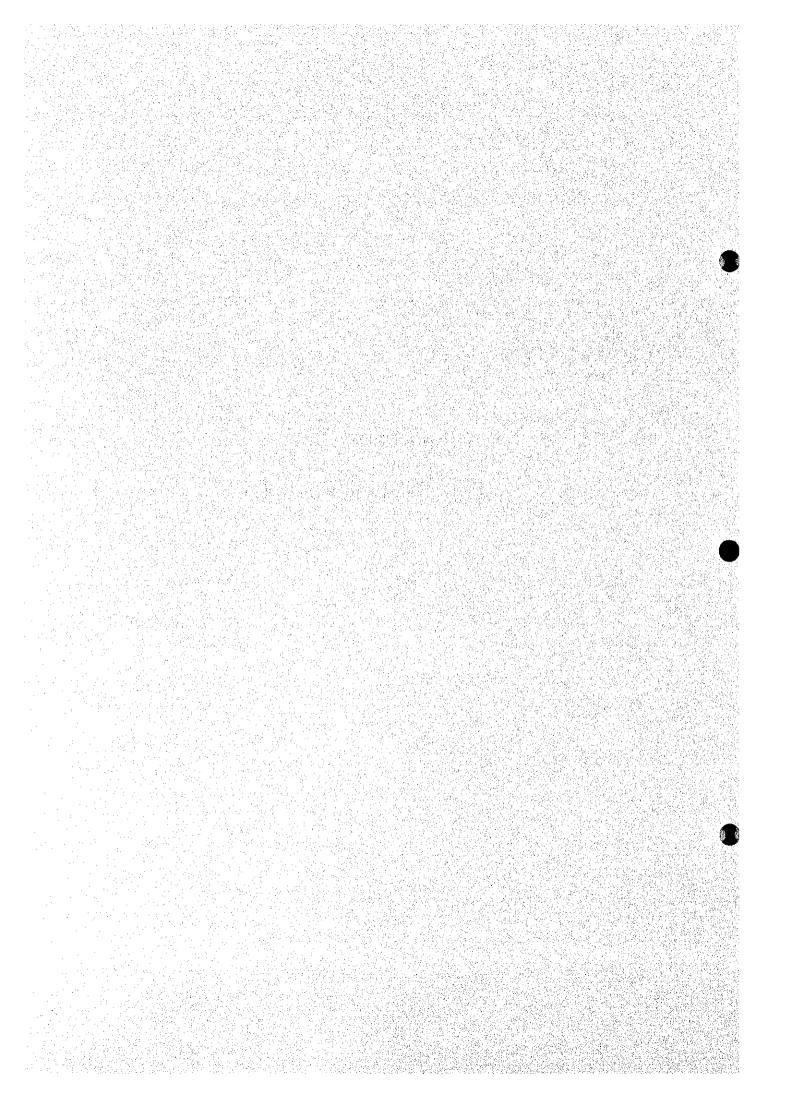




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Appendix I.2.7

Data of VLF-EM Survey



## App. 4.3 Data of VLF-EM survey

64.20

	[]	PR0-41			PR0-42		[]	PRO-43			PR0-44			PRO-45	
	DIST.	IN	QUAD,	DIST.	IN	OWD,	DIST,	IN Nucr	OUAD.	·DIST.		CUAD,	DIST,	IN	QVXD,
	(0)	PHASE (X)	PHASE (X)	(a)	PHASE (X)	PHASE (X)	(n)	PHASE (X)	PHASE (X)	(0)	PHUSE (X)	PHUSE (X)	(6)	PHUSE (X)	PHASE (%)
	0 20		-2	0 20	3 -2	<u>-13</u> 7	0 20		2	0 20	-3	-1	0 20	-11 -10	-9
	40 60	-12	-2	40 60	0	2	40 60	7		40 60	-3	-1	40 60	-7 -4	- 10 11
	80 100	-12		03 100	1	5	80 100	-3 -3	-0 -0	80 100	0	4	80 100	0	-12
	120 140	-14 -14	0	120 140	-5 -13	7	120 140	-5	2	120 130	<u>8</u> 14	-10 -9	120 140	0 0	-14 -18
	160 180	-12	-2	150 160	-22	5	160 180	-7	0	140	35 16	16 ?	160 180	0	-16 -18
	200	-10 -9	-4 -5	170	-25	5 8 7	200	-12 -10	-1	150 160	-4	10	200	0	-17
	220 240	-6	-6	180	-25	11	220 240	-4 -3	4	180 200	6	4	220 240	-3	<u>-16</u> -14
	260 280	-8 -8	-7 -10	200 210	-28 -29	10	260 280	2	3	220 240	9	-2 -2	260 280	-1 -5	-16 -0
	<u>300</u> 320	8 6	-9 ~11	220 230	-27 -25	6 8	300 310	45 -70	10 1	260 280	0 -7	- <u> </u> 0	300 320	-4 -2	3
	<u>. 340</u> 350	-3	-14 -12	240 250	-26 -27	7	320 330	30 -17	4	300 320	-11 -8	-0 -1	340 360	-5	4
	380 390	<u>11</u> 22	-17 -17	260 270	-27 -25	5	340 360	-13 -5	5	340 360	-11 -15	-2	380 400	-5	2
	395	- <u>17</u> -25	<u>-5</u> -2	280	-20 -19	4	380		13 10	380 400	<u>-15</u> -15	-2 -2	420	-7	2
	420	- 14	-6	300	-21	2	410	-10	12	420	-11	-1	460	-6	-3
	440	-8	<u>-7</u> -6	<u>310</u> 320	-20	3	415	- 15 - 18	18 42	440	-6	1 1	480 500	-5	2
	480 490	30	2	330 340	-12	8	425	<u>-25</u> 2	-43 -26	480 500	-5 -8	-2 -3	<u>520</u> 540	5 -5	-0 -1
	500 505	63 88	14	350 360	<u>-8</u> -7	8	440	0	<u>-9</u> -4	520 540	-3		560 580	-2 -3	2
	510	96	16	380	-1	10	480	-3	-2	560	-1	0	600	-2	0
	515 520	100 84	14	400	-4	10 8	500 520	-7 -4	-0	580 600	-2	2	620 640	-3	0
	525 530	<u>-142</u>	-13	440	-15 -14	10 9	<u>540</u> 560	-4	0	<u>620</u> 640	-6 -7	-1	660 680	-2 -3	-1
	540	-50	-16 -22	460	-17	9 10	<u>580</u> 600	-3	0  -	660 670	-7 -10	-1	700 720	-3	-0
	<u>560</u> 570	-28	10	480	-21 -25	8	520 640	-2		680 700	-18 -15	-9 -10	740 760	-4	0 -0
	580	-10	6	500	-25 -28	4	660	-3	-0	720	-13	-12 -11	780	-5	0
•	<u>600</u> <u>620</u>	<u>-7</u> -5	5	<u>510</u> 520	-25	3	680 700	-2	-0	760	-5	-9	820	-4	1
	640 560	<u>-15</u> -25	6 2	525 530	-18	6	720	-1	<u>-1</u>	780	17	-6	840 860	-3	0
	<u>580</u> 700	-22 -7	-2	540	-3	10 10	760	<u>-2</u> -3	2				880 900		-0 0
	720	25 55	-10 -6	560 570	-16 -21	3	800 820	-1	1						
	735	- <u> 10</u> -80	12	580 590	-17	5	840 860	<u>2</u> -11	0 0						
	760	-25	12	600 620	-3	10	880	-4	-0						
	800	-5	1	630	-7	4	920	-3	-2						
	820	0	9	<u>640</u> <u>650</u>	-13	3	960	-1	0						
	860 880	4		660 670	-18	0 -0	980 1000	4	-0						
	900 920	4 3	-14	680 690	-19 -13	0									
	940 960	-3	-17	700	-14 -11	2									
	980 1000	8	1	720 730	<u>-11</u> -8	2									
			¥	740	-5	. 4					 				
				760	-2	3									
			<u> </u>	800 820	-9	2								· · · ·	
				830 840		2									
	·	<u> </u>	<b> </b>	850 860	-9	4									
1				880 900	-7	5									
				920 940	0	8	[		[						
	·			960	-1	5				<u> </u>					
				1000	0	4			· · · · · · · · ·						
				1020	0	3									
				1060		2				<u> </u>					
		<u> </u>	<u> </u>	1100		-2									
				1130	-13	-6 -6	·								 
				1150	-14	-6								·	
			l	1170	- 14	-6					<b></b>	<b></b>		ļ	
				1180	-14	-6		<u>.</u>		<u> </u>					[]
	l	<u>ن</u>	l	1200	-15	-6		L	l	1	l	J	<u> </u>	l	L]

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	PR0-1_			PR0-2	· · · · ·		PRO-3			PRO-4	]		PRO-5	
DIST.	IN	OUAD	OI\$T.	IN	OUAD	DIST.	IN	OUAD	DIST.	IN	QUAD. PHASE	DIST.	IN PHASE	QUAD PHASE
(m)	PHASE (\$)	(%)	(m)	<u>PHASE</u> (%)	(%)	(m)	PHASE(%)	PHASE (%)	(m)	PHASE (%)	(%)	(m)	(%)	(%)
0	-23	23	0	-3	-7	0	6	1	0	3	-4	0	2 3	
10 20	<u>-18</u> -18	<u>24</u> 23	<u>20</u> 40	<u>1</u> -2	-8 -7	<u>20</u> 40	<u>5</u>	7	20 40	2	-2	<u>20</u> 40	3	-1
30	14	22	60	1	-7	60	2	8	60	7	-2	60	2	-1
40 50		22	80	2	-8	80 100	1		80 90	12 14	-3	80 100	0 5	
60	7_ 4	22 22	<u>100</u> 120		6	120	-6	6	100	13	-1	120	6	
70	-2	20	140	2	-6	140	-7	6	110	13	-2	140	2	1
80	-2	19 17	160 180	<u>2</u> -6	<u>-6</u> -5	160 180	8 -10	6 6	120	15	-4	<u>160</u> 180	-6 -12	
120	-1	. 14	200	-10	-9	200	-13	6	140	12	-2	190	-16	
140	l.	14	220	-9	-8	210	-15		150	1	-3	200	-18	
160 180	<u>2</u> -5	<u>14</u> 11	240 260	-4	<u>-8</u> -6	220	-17 -19	6	160 180	8	-3 -2	<u>210</u> 220	<u>-25</u> -31	1
200	-2	8	280	3	-7	240	-22	3	200	0	-4	230	-38	
220 240	2	10 8	300 320	9	~6 -8	250 260	-26 -29	-1	220 240	2	-6 -8	240	-50 -57	
260	<u> </u>		330	15	-10	270	-28	0	260	10	-11	260	-53	1
270	11	8	340	20	-9	280	-25	· 1	280	13	-12	2.70	-47	
280 290	13	8 8	350 360	<u>27</u> 35	-8	290 300	<u>-22</u> -17	3	290	18 18	-12 -10	280 290	<u>-40</u> -32	1
300	17	10	370	43	-6	310		4	310	23	-9	300	-30	
310	21	1L	380	45	-6	320	-10	4	320	24	-10	310	-29	
320 330	28 32	13	390	<u>32</u> 28	<u>-12</u> -11	340 360	7 -12	<u>6</u> 2	330	23 23	<u>-10</u> -9	<u>320</u> 330	- <u>27</u> -20	•
340	24	10	400	17	-11	370	-12	4	340	23	-9	340	-18	
350	25	10	420		-12	380	-12	-0	360	22	-6	350	-17	
360 370	<u>21</u> 30	<u>8</u>	430	9 6	-10	390 400	-9	3	<u>370</u> 380	16	<u>-4</u>	360 370	-17	
380	25	8	460	6	-8	420	-9	1	400		-4	380	-14	
390	20	. 6	480	0	2	440	-6	-1	420	-3	-2	390	-10	
400	22 20	7	<u>500</u> 510	<u>-8</u> -13	5 8	460 480	0	0	440 460	5 9	0 0	400 410	6 2	
420	20	, i	520	-18	1	500	15	6	480	10	2	420	Ō	
430	19	6	530	-21	4	510	20	6	500	9	0	440	-3	
440 450	<u>    16</u> 15.	1	540 550	-15 -9	- 7 8	520 530	5 9		<u>520</u> 540	12	<u>0</u> 0	460 470	5 10	
460	12	2	560	-6	8	540	-28	-0	560	9	-1	480	16	
470	9	2	580	2	6	550	-33	-2	580		-1	490	18	
480 500	<u> </u>	3	600 620	0 -3		560 570	-28	-2	600 620	6	<u>-1</u> -2	<u>500</u> 510	20 19	
	£		640	3	4	580	-16	4	640	7	-0	520	18	
ł			660	3	2	590	-10	6	660		0	530	19	
[			680 700	6 3	2	600 620	-5	6	680 700	-3	0 -2	<u>540</u> \$50	25 24	
			720	3	3	630	-8	1	720	-3	-i	560	22	
			740		3	640	-5	2	740	<u>l</u>	-2	570	18	
			760	-3	4	660 680	-8 -9	-3	760 780	-2	-5	<u>580</u> 590	<u> </u>	
			800	-1	4	700	-5	-0	800	-4	-6	600	13	
			820	-1		720	0	-0	820	4	-9	610	14	
		<b>.</b>	<u>840</u> 860	-2	4	740 760	3	-0 0	<u>840</u> 860	4	<u>-1</u> -7	<u>620</u> 630	12 12	
			880	-2	2	780	6	-2	880	5	-11	640	3	
			900		0	800	5	-3	900	5		660	-11	
			920 940	<u> </u>	0			ł	920	10	~14	<u>670</u> 680	<u>-17</u> -16	
		· · · · · ·	950	4		I	[		950	18	-16	690	-17	
			980 1000		-1				960	15	-18	700	-17	
		<u> </u>		l	-1.		<u> </u>		970 980	22 25	<u>-18</u> -16	710	-15 -15	
			ļ						990	26	-18	730	-14	
		I	<u> </u>			<u> </u>	<b>-</b>		1000	29 32	-18 -18	740	-25	ļ
								<u> </u>	1020	32	-18	760	-23	
								ļ	1030	40	-19	770	-22	
······································					·····		ł	·	1040	40	-20	780	-23	
									1060	40	-19	800	-23	
						Į			1070	43	-19 -20	810	-22	
							1	<u> </u>	1080	43	-20	820 840	<u>-22</u> 	
		ļ					1		1100	30	-17	850	-17	
		·}		ļ	l			<u> </u>	1120		-16	860	-16	
							1	1	1130		-17	870	-15	
							Į		1150	14	-14	890	-18	
• · · · · · · · · · · · · · · · · · · ·						·	· [	<u> </u>	1160		-13	900	-18	
				ł <i>-</i>			ł		1170		-12	910 920	<u>-18</u> -16	
			1		·		1	1	1190	12	-12	930	-10	·
		ł						ļ	1200		-8	940	-12	
······································														
						1	-			<b>+</b>		950	-11	

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[	PRO-6			PRO-7			<u>P</u> R0-8			PRO-9			PR0-10	
DIST.	IN	QUAD.	DIST.	IN	QUAD.	DIST.	IN	OUAD.	DIST.	IN	OUAD.	DIST.	IN	QUAD.
	PHASE	PHASE		PHASE	PHASE		PHASE	PHASE		PHASE	PHASE	0107	PHASE	PHASE
(m)	(%)	(%)	<u>(m)</u>	(%)	(%)	(m)	(%)	(%)	(m)	(%)		(11)	(%)	(%)
0		-1	0	12	-8	0	4	-14	0	5	6	0	-2	4
<u>20</u> 40	<u>-9</u> -8	0	<u>20</u> 40	15 20	<u>-10</u> -8	<u>20</u> 40	<u>-2</u> -3	<u>-11</u> -10	<u>20</u> 40	<u> </u>	5	20 40	- <u>1</u> 0	4
50	-11	-0	60	22	-4	60	-5	-6	60	11	4	60	0	<del>4</del> . 4
60	-17	-2	80	12	-8	80	-9	-4	80	8	2	80	-2	4
70	-23	-6	100	4	-11	100	-9	0	100	8	4	100	-2	4
80	-20	-6	120	4	-6	110	-12	4	120	10	6	120	-4	2
90	-23	-6	140	0	-4	120	-18	5	140	<u>    10    </u>	5	140	-3	3
<u>100</u> 110	22	<u>-7</u> -6	<u>160</u> 180	1 -6		<u>130</u> 140	-23 -27	7	<u>160</u> 180	7	<u>6</u>	<u>160</u> 180	<u>-2</u> 0	1
120	-20	-6	200	-4	4	160	-26	12	200	8	6	200	-3	3
130	-19	-5	220	0	6	170	<b>-</b> -24	14	220	10	6	220	-8	3
140	-19	-7	240	-9	3	180	-17	16	240	16	6	240	-7	2
150	-20		260	-3	5	190	-15	14	260	13	5	260	-4	4
<u> </u>	<u>-19</u> -19	-7	280 300	-3	6	200	-14 -14	<u>13</u> 13	280 300	12	5	<u>280</u> 300	<u>-3</u> -2	3
180	-19	-10	320	-4	4	220	-17	12	320	11	6	320	Ô	6
190	-18	-10	340	-3		230	-18	12	340	10	7	340	5	5 9
200	-17	-8	360	3		240	-15	12	360	11	1	350	12	9
210	-14	-8	380	3	6	250	-14	12	380	<u>11</u>	8	360	20	12
220 230	<u>-13</u> -12	<u>-9</u> -7	<u>400</u> 420	-3	<u>3</u> 4	260 280	- <u>9</u> -1	<u>14</u> 15	400 420	7 5	8	<u>370</u> 380	<u>48</u> 78	18 8
230	-13	-10	420	<u></u>	<u>4</u> 1	300	3	13	440	7	8	385	-43	-10
250	- 12	-10	460	-3	3	320	12	17	460	7	6	390	-80	-12
260	-11	-10	480	-3	4	330	13	14	480	6	8	400	-42	-7
270	-11	~10	500	-3	3	340	14	14	500	1	8	410	-24	-4
280	<u>-11</u> -11	<u>-10</u> -11	520	-2	2	350	<u>13</u> 12	14	520	5	8	420 430	-17	-1
300	-10	-13	<u>540</u> 560	3.9	3	<u>360</u> 370	13	<u>14</u> 12	<u>540</u> 560	<u>4</u> 6	<u>6</u> 7	430	-13 -9	2
320	-5	-10	580	6	1	380	10	12	580	4	5	460	-5	4
340	3	-8	600	2	-0	400	8	11	600	.8	6	480	0	4
360	11	-10	620	3		420	10	12	620	11_	6	500	2	4
380	3	<u>-10</u> -10	640	-7	-2	440	<u>13</u> 13	12	640	8	6	520 540		4
400	10	-12	<u>660</u> 680	<u>-5</u> -1	-2	<u>450</u> 460	13	<u>12</u> 13	660 680	5	8 8	560	0	2
420	13	-14	700	-1	1	470	13	12	700	-3	9	580	2	2
430	14	-14	720	-3	0	480	13	10	720	-12	8	600	1	3
440	13	-14	740		1	490	15	12	740	-15	6	620	0	2
450	14	-16	760	-9	-3	500	16	. 12	760	-13	5	640	5	4
460	8	-16	780 800	<u>-10</u> -11	-4	510 520	<u>17</u> 21	12	780 800	-4	7	660 680	0	<u>6</u> 9
490	4	-13	820	-5	-3	530	22	12	820	-3	4	700	-2	-11
500	-5	-10	840	-2	2	540	17	10	840	3	5	720	-1	~6
510	-10	-6	860	-5	2	550	14	8	860	4	5	740	-2	-4
520	<u>-13</u> -17		880	0	<u>├</u> ¦-	560	12	8	880	5	4	760	0	-2
530 540	-18	<u>-0</u> 0	<u>900</u> 920	-2	-0	<u>570</u> 580	13	8	900 920	5	2	780	<u>-1</u> -1	-4
550	-22	1	940	4	-2	590	15	10	940	8	0	820	0	-1
560	25	6	960	15	1	600	14	10	960	8	-1	840	1	-0
570	-27	6	980	13	0	610		9	980	6	-2	860	4	-1
<u>580</u> 590	-33	8	1000	-4	-4	620	17	10	1000	44-		880	-4	-2
600	-36	5	1020	<u>-2</u> -1	-4	<u>630</u> 640	<u>16</u> 13	8	1020	4	<u>-2</u> -4	900 920	1	0
605	-55	1	1060	-4	-6	650	14	8	1060	7	-6	940	4	0
610	-55	0	1080	0	-4	660	15	8	1080	7	-6	960	-1	2
620	-41	4	1100	0	4	670	16	9	1100		-6	980	0	2
630 640	-30	6 6				<u>680</u> 690	16 16	9 9				1000	Q	0.
650	-27	10				700	10	9			1	t		
660	-19	8						· · · · · · · · · · · · · · · · · · ·						
670	-14	11												
680		9	<b>]</b>	ļ				Į	ļ	<u> </u>			<u> </u>	
700	-4	12	l						<u> </u>	<u> </u>				
730	-8	5				{				<u> </u>				
740	-11	3		<b></b>										
750	-11	. 6					ļ		ļ					
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780	8	7		·····			<u> </u>						·[	
800	-12	3			<u> </u>	1		1	<u> </u>			<u> </u>		t
820	-9	2						1			1	1		
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980		-1							ļ				1	
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	PR0-11			PR0-12			PR0-13			PRO-14			PR0-15	
								01110	DIAT		QUAD.	DIST.	ÍN	QUAD,
DIST.	<u>N</u>	OUAD.	DIST.	IN	QUAD.	DIST.	IN	QUAD.	DIST.			DIŞI		
<u> </u>	PHASE	PHASE		PHASE	PHASE		PHASE	PHASE		PHASE	PHASE		PHASE	PHASE
(m)	(%)	(%)	<u>(ņ)</u>	(%)	(%)	(m)	(%)	(%)	(m)	(%)	(%)	(0)	(%)	(%)
	14_	14	0	-29		0	0	5	0	0	-1	0	-2	
10	12	14	20	-25		20	1	1	20	0	0	20	0	5
20	14	14	40	-15	14	40	1	1	40	4	0	40	0	3
30	14	10	60	-14		60	-1	-0	60	4	-1	60	3	2
40	. 13	. 9	80	-7	11	80	-2	-5	80	. 6	-2	80	1	1
50	13	6	100	-5	9	100	-1	-7	100	5	-2	100	2	0
<u>    60  </u>	13		120	-2		120	2	-13	120	6	0	120	3	-0
70	14	6	140	3	6	140	17	-20	140	2	1	140	4	1
80	13		160	12	0	150	37	-32	160	3	-1	160	<u> </u>	4
90	17	4	180	33	-0	155	72	-29	180	3	1	180	4	4
100	17	4	200	65	-1	160	8	0	200	2	2	200	0	2
110	15	2	220			170	-30	22	220	-3	2	220	0	-0
120	16	1	240			175	-14	15	240	-3	1	240	3	0
130	17	0	260	0	9	180	-7	9	260	-2	1	260	5	1
140	17	-0	280	-2	6	190	5	-2	280	-3	. 2	280	6	2
150	17	0	300	-4	6	200	18	-12	300	0	. 2	300	7	2
160	15	-2	320	-2	6	210	48	- 19	320	0	2	320	9	1
170	16	-2	340	2	2	215	-32	10	340	-2	2	340	7	1
180	16	-2	360	2	3	220	-47	32	360	-5	3	360	5	-1
190	16	-2	380	2	3	230	-17	21	380	-8	2	380	7	-1
200	19	-2	400	5	2	240	-8	12	400	-3	2	400	2	-1
210	21	<u>-</u>	420	5	<u> </u>	260	-3	7	420	-1	2	420	3	-2
220	23	-2	440	7	-0	280	i	4	440	0	0	440	4	2
230	22	-4	460	7	-1	300	3	3	460	4	-3	460	2	-2
240	21	-3	480	10	-0	320	1	0	480	12	-2	480	4	-2
250	20	-4	500	13	-6	340	2	1	490	17	-1	500	3	-3
260	16	-6	520	18	-8	360	0	-0	500	21	0	520	6	-2
270	16	-6	540	23	-12	380	0	-3	510	23	. –1	540	3	2
280	13	-6	560	46	-20	400	-3	-4	520	22	-3	560	6	-1
290	12	-7	580	-10	20	420	-2	-10	530	17	-6	580	4	-1
300	11	-6	600	-86	33	440	3	-16	540	16	-6	600	5	-1
310	10	-8	620	-32	22	460	12	-29	550	11	-6	620	4	-1
320	8	6	640	-17	12	480	100	-50	560	8	-6	640	1	-1
340	5	-6	660	-13	-8	500	-100	50	570	. 8	-7	660	1	-2
360	3	~6	680	-5	4	510	-26	40	580	3	-8	680	9	Ó
380	0	~6	700	-5	3	520	-14	29	590	4	-8	700	9	-1
400	5	-4	1	<u> </u>	l	540	-5	21	600	3	-8	720	2	
400	0	-4				560	-5	14	1 000		-0	740	0	č
440	-1	-4	· · · · · · · · · · · · · · · · · · ·	·[		580	6	8	<b> </b>	·		760	l õ	-1
440	-2	0	<u> </u>	I		600	7	- °	· [	+		780	2	 1
480		-0		1		620	6	6	+	<u>                                      </u>		800	-3	-0
<u>480</u> 500	0	-2				640	3	4	+	t				<b>-</b>
000	<u>-</u>					660	-3	2						
	<u> </u>					680	-3			<u> </u>		· · ·	· · ·	
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1 3	PRO-16			PR0-17		I	PR0-18			PRO-19		[	PR0-20	
					QUAD.	DIST.	111	QUAD.	DIST.	1N	QUAD.	DIST.	IN	QUAD
DIST.	IN PHASE	OUAD. PHASE	DIST.	IN PHASE	PHASE		PHASE	PHASE	0101.	PHASE	PHASE		PHASE	PHASE
(m)	(%)	(%)	(m)	(%)	(%)	(m) 0	(%) -32	(%) 6	(m) Q	(%)4	(%) -4	(m)0	(%) -2	(%)
0 20	<u>2</u> 2	-6 -6	0 20	6 5	<u> </u>	10	-32	11	20	-7	-3	20	0	
40	1	-6	40	5	1	20	-19	12	40	-4	-3	40	0	
60 80	<u>-2</u> -7	-1 -6	<u>60</u> 80	8	8	<u>30</u> 40	<u>-15</u> -14	<u>14</u> 11	<u>60</u> 80	-2	0 4	<u>60</u> 80	-1	
100	-6	-4	100	10	6	50	-20	6	100	2	-3	100	Û	
120	-9	-4	110		6	60	-18	8_	120	5		120	0 c	
140	<u>-5</u> -4	-6 -6	120	<u> </u>	6 6	70 80	-13	8	140	<u>11</u> 15	<u>-2</u> _3	140	<u>5</u> 9	
180	11	-2	140	14	5	90	-8	12	160	15	-4	180	15	
190	-3	-4	150		6	100	-6	11	170	17	-5	200	<u>17</u> 20	•-
200	<u>-9</u> -10	-6 -4	160	<u>17</u> 18	5	<u>120</u> 140	0	12	180 190	19	-6 -5	240	17	
230	-\$	-6	180	18	8	160	6	14	200	32	8	260	24	
240		-3	190	19	6 5	<u>180</u> 190	13	<u>10</u> 14	210 220	41	-4	280	22	
260	3	-2	210	18	5		11	16	230	30	-6	320	11	
300	2	-4	220	17	3	210	8	11	240	16	-6	340	7	
320	<u>-3</u> 0	-10	230	17	2	220 240	6 12	13	250	11	-6	360	4	
340	6	8	240	10	2	240	11	13	280	-10	-0	400	Ō	
360	.11	-5	260	19	4	260	12	11	290	19	2	420	-1	
370	3	-6	270	20	4	270	9	<u>8</u> 9	300	<u>-29</u> -28	2	440	-3	
380_ 400	-5	-6	280	21 20	4	280	10	10	310	-19	2	480	-3	
410	13	-2	300	18	4	300	11	10	330	-17	1	500	-5	
420	15	2	310	17	2	310	9	9	<u>340</u> 350	<u>-13</u> -7	0	<u>520</u> 540	-5 -5	
<u>430</u> 440	13	0	320	19	4	330	11	6	360	-8	0		-8	
450	5	-2	340	16	3		12	6	380	-2				ļ
460 480	2 6		350	18	2		11			-3	0-0		<u>-5</u> -5	+
500	5	2	370	17	4		12	4		-3	2		-5	
520	8	2	380	15		380	9	4	460	3	4		-5	·
<u>540</u> 560	-8	0	390 400	12		400	13	6		5	3		-1	
580	-5	0		7	-0		16	6	520	-2	4	720	-2	
600	-6			3				5		-2	4		-3	
620 640	-8	0		2	-4	440		4			4			·
650	-12	-2		0	-4	460	13	2	600	3	8		4	
660	-22	-8		-3				3		4			5	
<u>665</u> 670	-28 -26	-8		-6	-6			4		6			5	1
675	-24	-8		-9	-6			3					9	
680 685	-22	-9		-9 -8				2		-3			9	
690	-15			-5				4						
700	-7	-9	520	-6				2	760	3	-4	960		·
720	-2			-4				1			-5		0	
740	5	-6	580	-1	-2	570	12	-2	810	111	-8			
760	23	-6		2				-3			-8			
800				7				-10						1
810	11	-4	640		-!!	620		-8						
820 840	7	-6		8				-3					-	·[· ··· ·
860			700	9	0	660	13	-4	880	32	-8			
870								-6						
880 900													-	
			740	10	-0	700			920	2	-4			
			750					-  <u>.</u>	930					
			770	10	2			<u> </u>	950	-24	(	)		_
L			780		2	L	_		960	-27	2		+	
	-		790						970					-1
			820	1	-3				990	-11				-
	-		840	-4	-6	;			1000					
	·  ·····	-	860						1020				-	1
<u> </u>			900	0	) -6	3			1060	9 9	-/	2		
			920						1080			<u> </u>		
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	DIST.	IN	OUAD	DIST.	IN	QUAD.	DIST.	 IN	QUAD.	DIST.		QUAD.	DIST.	IN	QUAD.
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1040  -10  4  1000  22  -4    1060  -15  2  1020  23  -4    1080  -16  2  1040  17  -4	1000	·}	·			// 6	980		-5				1000	2	-3
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	PR0-26	·		PR0-27			PR0-28			PR0-29			PR0-30	
DIST.	IN DUACE	QUAD.	DIST.	IN Duter	QUAD.	DIST.		OUAD. Phase	DIST.		QUAD.	DIST.	N N	QUAD. Phase
	PHASE	PHASE (%)	(n)	PHASE (%)	PHASE (%)	(m)	PHASE(%)	(%)	(m)	PHASE (%)	PHASE (%)	(m)	PHASE (%)	(%)
(m) 0	(%)		(n)0		-1	0	13	-2	0	-6	10	0	-3	-3
20	-2	4	20	8	-0	20	10	-1	20	-2	10	20	-4	-3
40	3	-2	40		-2	40	4	-2	40	-2	7	40	-5	-2
60	-4	-7	60	5	-2	60	8	-3	60	-5	<u> </u>	60	3	-2
80	0	-9	80	5	-3	80	3	-2	80	4	7	80	Ő	-2
100	5	-6	100	5	-3	100	8	2	100	0	6	100	0	-2
120	8	-6	120	ĵ.	-2	120	10	2	120	Ū.	4	120	1	0
140	8	-6	140	7	-4	140	0	2	140	-5	3	140	2	2
160	7	-4	160	8	-5	160	-7	-2	160	-4	4	160	4	4
180	2	-6	180	11	-1	180	-9	-1	180	0	4	180	-2	4
200	0	-6	200	2	-4	200	-7	2	200	0	5	200	-5	5
220	4	-4	220	0	-4	220	-7	-2	220	3	5	220	-8	7
240	5	-4	240	4	-1	240	14	-1	240	6	3	240	-13	3
260	6	-2	260	4	-4	260	12	0	260	7	2	250	-13	3
280	2	2	280	5	-2	280	-10	1	260	10	3	260	-10	3_
	-3		300	1	-2	300	-8	-1	300	7	3	270	-9	3
320	-5	2	320		-2	320	-5	-1	320	9	2	280	-7	4
340	-7	2	340	9	-6	340	3	2	340	9	<u> </u>	300	~3	3
360	-6	1	360	. 9	-5	360	7	2	360		2	320	-4	1
380	~10	<u> </u>	380	9	-4	380	1	-2	380	5	0	340	0	
400	8	4	400	5	<u>-</u> Į.	400	6	-6	400	4	0	360	0	2
420	-8	2	420	<u>2</u>	-4	420	8	-6	420	4	0	380	1 1	2
440		·	440	5	-1	440	22	-5	440	-4	-2	400	3	2
460	-3	-1	460	3	-0	460	23	-6	460	-4		420	<u>1</u> 2	-2
480	-3	-2	480	<u> </u>	<u>-1</u> -1	480	25	<u>-8</u> -10	<u>480</u> 500	-4		440	6	
<u> </u>	5	<u>-2</u> _2	<u>500</u> 520	0	-1		25	-10	520	10	<u>-4</u> 1	480	9	1
540	5	-2	540	-3	<u>~</u> 1				540	10	1	500	3	0
560	8	<u>-1</u>	560	3	2				560	-1	-2	520	4	2
580	3	-3	580	2	2				580	0	-0	540	i	2
600	2	-1	600	3	4				600	-2	-4	560	2	4
620	0	-4	620	5	6				620	-5	-6	580	-3	4
640	4	-0	640	4	5				640	-5	-6	600	-3	4
660	4	-2	660	3	4				660	-3	-3	620	0	4
680	3	-1	680	-5	2				680	-3	7	640	-2	
700	2	-2	700	-5	<u> </u>	1			700	-4	-6	660	-1	4
720	3	-2	720	-5	1				720	~8	-6	680	-1	4
740	3	-2	740	0	5				740	-6	-9	700	8	0
760	4	-0	760	-5	2				760	-4	-7	720	-9	0
780	1	0	780	0	6		{		780	0	-11	740	-11	-2
800	6	1	800	8	6				800	8	-10	760	-8	-2
820	8		820	8	4		l		820	20	-6	780	-6	-0
840	<u> </u>	3	840	13	5				840	20	-5	800	-8	-1
860	8	6	860	-1	2		<u> </u>		860	23	4	820	-10	-4
880	3	6	880	-6	2	····	<b> </b>		880	26	-4	830	-12	-5
900	-2	7	900	-3	4	<u> </u>	l		900	15	-6	840	-11	-7
920	-8	9	920		4		<u> </u>		920	0	-8	850	-9	-6
940	-10	9	940		6		· · · · ·		940	-2	-8	860	-7	-5
960	-14	9	960	17	6		ł		960	0	-8	880	-8	-6
980 1000	-20	5	980 1000	0	3			·····	980 1000	-3	-9	900	-6 -2	
1020		4	1000	<u>-</u>  -	<i>-</i>	<u> </u>		<u> </u>	1000	0	-10	940	6	
1020	-11	7				·	t	1	· · -	†	<u> </u>	950	10	6
1040	-8	6				t	<u> </u>			t		960	16	-4
1080	-5	4				h	1	<u> </u>				970	17	-6
1100	Ŭ Ŭ	5	I	· · · · ·								980	11	-9
1120	3	4	1		····			1	i —			990	6	-10
1140	5	5		l'	· · · ·		·	1		1	1	1000	5	-10
1160	5	3				[	Ι.			1	]	1010	0	-11
1180	5	1										1020	-6	-11
1200		2	[				<u> </u>					1040	-4	-9
	1											1060	-1	-4
	L				1							1080	1	-2
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	<u> PRO-31</u>			-1280-32 -			_PR0-33			PRO34				
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	PHASE	PHASE	(-)	PHASE	PHASE	(-)	PHASE	PHASE	(.)	PHASE	PHASE	(-)	PHASE	PHASE
(m)0	(%) 9	(%) 2	(m) 0	(%) -3	(%) 6	(m) 0	(%) 2	(§)	(m) 0	(\$)	(%) -6	(m) 0	<u>(%)</u> 9	(%) 2
10	-8	-1	20	-4	3	20	2	2	20	7	-4	10	15	-2
20	-16	-2	40	-2	0	40	1	1	40	1	-4	20	21	
30	-23	-4	60	0		60	. 2	0	60	l	3	30	44	-
<u>40</u> 50	23 20	-4	<u>80</u> 100	-4	2 0	80	5 0	-2	80 100	<u>6</u> 3	-3 -4	40	55 -28	
60	-16	-3	120	-11	5	120	3	ç	120	1	0	50	-21	
80	-8	-2	130	-8	5	140	3	2	140	-1	0	60	25	
100	-4	-1	140	-7	3	160	2	2	160	-3	-0	70	-100	
120	-9	-2	160	-3	2	180			180	-1	0	80	-32	
<u>130</u> 140	-9 -10	-1	180	-3	1	200	-1		200	2	-0 -0	90 100	-12 -12	· · · · · ·
150	-17	-0	220	<u> </u>	1	240	-2	6	240	3	-1	110	-8	
160	-18	-1	240	0	2	260	-8	2	260	6	-4	120	-14	
170	20	2	260	-2	1	260	-1		280		-6	130	-22	
180	-21		280	~?	-1	300	-6	2	300	13	-8	140	-23	
<u>190</u> 200	-26 -25	<u>2</u> -2	<u>300</u> 320	-2	0	320	-5	2	320 340	<u>100</u> -9	<u>-50</u> 14	<u>150</u> 160	<u>-13</u> -21	
210	-31	-2	340	0	3	360	-5	3	340	-3	7	170	-14	
220	-33	-4	360	-4	-2	380	-5	Q	380	2	5	180	-12	
230	-31	-2	380	-8	2	400	-5	2	400	0	4	190	-9	
240	-21	-2	400_	-2	<u>1</u>	420	-3	. 0	420	0	2	200	-10	
250	-27	-4	420		-1	440		2	440		2	210	9	· · · ·
260 270	-25 -23	-2	440 460	-5	-1	460 480	-3 -7	-2	460	0 0	2	220 240	-8	
280	-23	-2	480	-6	-1	500	-2	-4	500	1	0	240	-4	
290	-23	-2	500	-6	-1	520	Ĩ	-4				280	-1	
300	-23	-3		ļ		540	0	-6				300	-2	
310		-2		<b> </b>		560	3	-8				320		
<u>320</u> 330	-19 -16	-3	[		<u> </u>	<u>580</u> 600	<u>5</u> 3	9 -6				<u>340</u> 360	2	
340	-14	-4				620	ŏ	-6				380	18	
350	-14	-4				640	0	-0				390	19	
360	-13	-4		ļ		660	1	2				400	20	
370	-14	-5	ļ			680	5	4	L	ļ		410	22	
380		-6	i			700		8	· · ·			420	18	
400	-9 -8	-6 -6		· · ·		720	-2	10			<u> </u>	430	16	}
440	-8	-7				760	-15	13				450	3	
460	-7	-7				770	-25	12				460	6	
480	-6	-10				780	-24	13				480	2	ļ
500		-10	·	I		790	-22	15		·		500	5	
<u>510</u> 520	9	-10 -10	·			800 820	<u>-21</u> -19	<u>14</u> 12				520 540	2	<u> </u>
530	21	-10		1		830	-13	15				550	11	
540	21	-12				840	-11	14				555	14	· -
550	22	-12	<u> </u>	ļ		860	-6	12				560	38	
560	. 22	-12				880	-7	10	ļ		<u> </u>	565	-5	<b> </b>
565 570	<u>22</u> 18	-12			}	900 920	-3	10				570	-8	
580	16	-14	·			940	-1	9			<u> </u>	<u>580</u> 585	<u>-30</u> -17	
590	11	-15				960	-5	4			· ···	590	4	
600	6	-14	ļ			980	-5	5		1		600	21	
620	<u> </u>	-14		·		1000	-3	5				610	1	
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660	-11	-8	1	1		1040	-2	2			1	640	3	
670	-12	-6	<u> </u>			1080	0	2				660	2	
680	<u> </u>	6				1100		4				680	-9	<u> </u>
700 720	-9	-6		·	·	1120		5		·	<u> </u>	700	-8	
740	-2	-2		1	1	1140	-6	3			<u> </u>		1	
760	-5	-1			1	1180		1	L					
780	-7	-2		<u> </u>		1200		0			1		1	
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900	-6	-1	1				1			[				1
920						<u> </u>		Į	<b> </b>		<u> </u>	ļ		ļ
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1080   100			·}		-[			<b> </b>		·[·- · · · ·		1	.   <i></i>	<u> </u>
1120			1	-	-	-	·{	·	+ • •	1	·		+	<b>}</b>
1140	-5				1			1	1	1	1	· ··	1	<u>†</u>
1160		2											1	1
1180	-8													

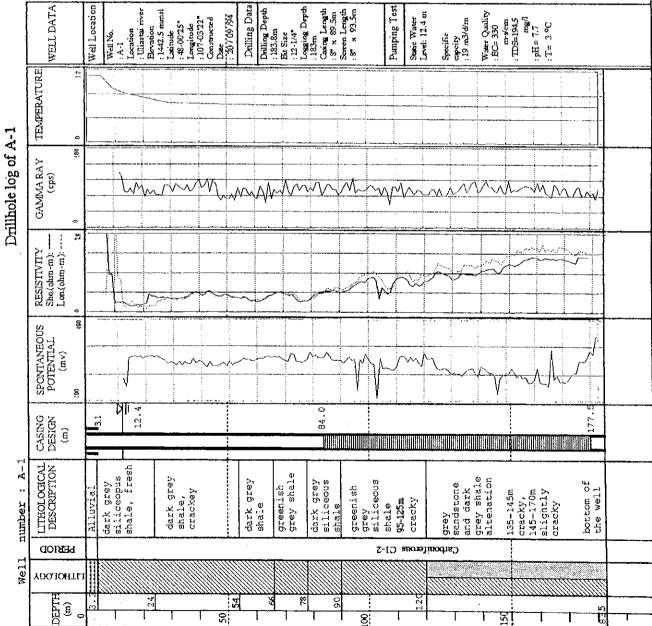
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I - A - 93

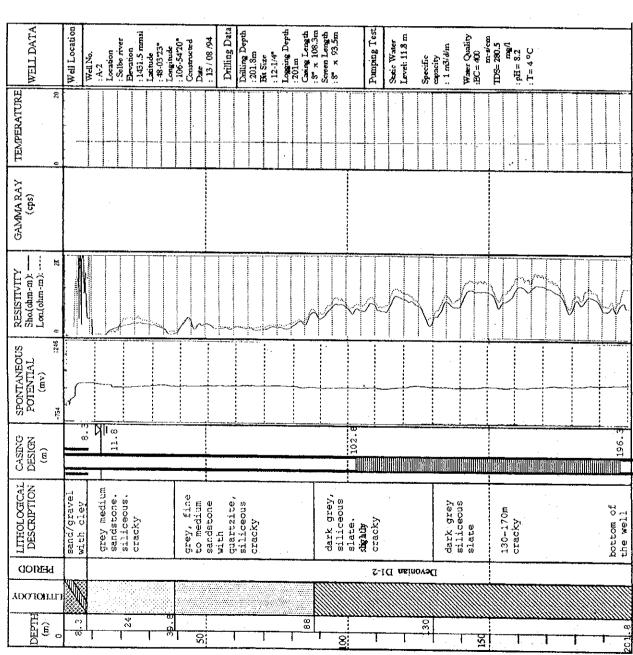
	PR0-36			PR0-37			PR0-38_			PR0-39			PR0-40	
						- ALOT		QUAD.	DIST.	 IN	QUAD.	DIST.		QUAD
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· (~)	PHASE	PHASE (%)	(n)	PHASE (%)	(%)	(m)	(%)	(%)	(m)	(%)	(%)	(m)	(%)	(%)
( <u>m)</u> 0	(%) 10		0	-15		0	10	-0	0	-1	4	0	-10	
20	10		10	-15	i i	20	10	-0	20	-2	6	20	-4	
30	1	1	20	-14	-2	40	4	-2	40	-2	4-	40	-9	
40	-8	4	30	-11	-3_	60	5	-1	60			60		<del>-</del>
50	18		40	-7	0	80	-4		80	-4	0	70 80	-9	
60	-30	<u></u>	60	2	0	<u>100</u> 120	-13	2	<u>100</u> 120	-3	0	100	-8	
70 80	-21	2	<u>80</u> 100	-2	- <u>1</u> -2	140	-11	2	140	-1	0	120	-8	
90	-16	2	120	-1	3	160	-5	Ō	160	3	0	140	-7	
100	-18	2	140	-5	-6	180	2	2	180	5	0	160_	-2.	
110	-20	2	160	-11	-7	200	4	-1	200	7	0	180	10	·
120	-19		170	-10	-8	220		4	220	3	-4	190_	14	
130	-19	3	180	-13	-9	240	<u>5</u>	5	240	3	-6	200 210	21 25	
140	-19	2	190	-11	-10	260	-4	3	260	3	-4	220	34	-
150	-15	4	200	-11	-10	280	<u>-18</u> -7		300	9	-4	230	37	-
160	-15	3	210	-8	<u>-10</u> -10_	320	-4	5	320	-2	-3	240	41	
170	<u>-15</u> -15	4	240	-7	-12	340	-7	1	340	5	-4	250	42	
200	-13	3	260	-5	-12	360	-4	4	360	-15	-4	260	52	-
220	-9	3	280	-4	-12	380	8	4	370	-10	-2	270	58	
240	-10	0	300	-7	-13	400	-17	4	380	-10	5	280	84	-
260	-6	0	320	-7	-14	420	-14	2	400	-20	9	290	120	
280	-3	-2	340	-12	-12	440	10	-2	420	-28	7	295	110	
	-2	0	350	-13	-11	460	-9	4	440	-29	6		-126	1
320	6	2	360	-14	-10	480	4	-2	460 480	-25	<u> </u>		-120	
340	10	· 0	370	<u>-12</u> -14	<u>-10</u> -10	500 520	-3	-4	500		8		-30	
360 380	5	-5	380	-14	-10	540	-2	-5	520	-27	4		-22	
400	14	-4	400	-20	-12	560	-6	-7	540	-21	3		-22	
410	18	-4	410	-18	-13	580	5	-1	560	-23	5		-13	
420	18	-7	420	-14	-12	600	8	-8	580	-25	6		21	
430	22	5	430	<u>-12</u>	-14	620	9	-12	600	-27	3		21	<del>.</del>
440	24	-5	440	-9	-14	640	15	-10	<u>§10</u>	-20	<u></u>		30	
450	24	-6	450	-4	-14	660	14	-14	640	-18	5		45	
460	19	-7	460	-5	-15			-14	680		8		-5	
470	17	8	475	0				-16					-5	
480	27	-7	480	14				-18	720			1	-13	
500	20	-8	485	29	-26		-57	-24	740		6		-12	
510	10	-10	490	28	-14	710							-12	
520	12	9	495	-33	-3			13					-8	
530	2	-9	500	-96				19					-5	
540	-12	-8	505	-58	20			6		- t			11	
<u>550</u> 560	-12	<u>-10</u> -10	510 520	-40	12			-3						
570	-8	-9		-22	12			-2						
580	-6	-9	540	-13	11			-6			2			
600	8	-11	560	-9	7	840	-4	-4	920					
620	-3	-10	580	7	6					-7				
640	4			-7	3									
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			940											-1
			940 960 980	-8	1						_			

Appendix I.2.8

Drillhole Logs of JICA Test Wells



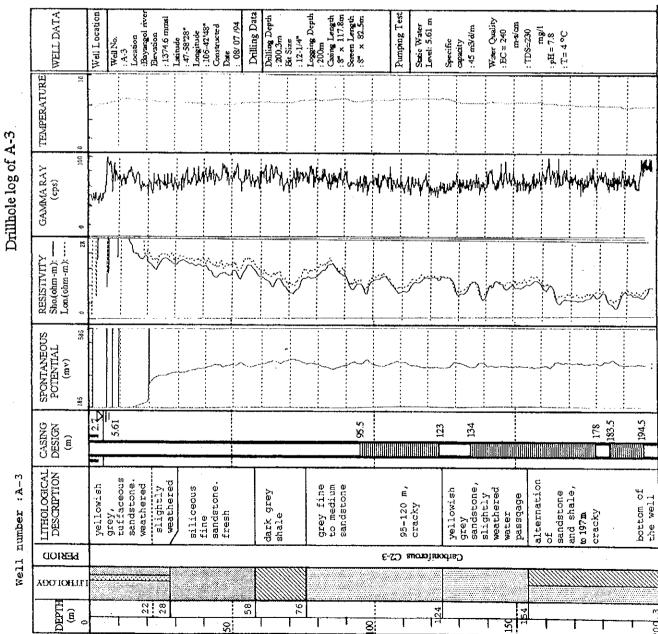
Well number : A-2



	ALC: N

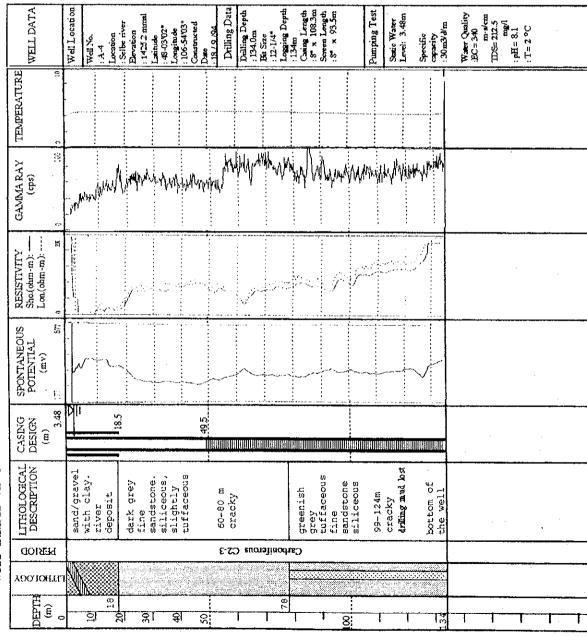
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Well number : A-3



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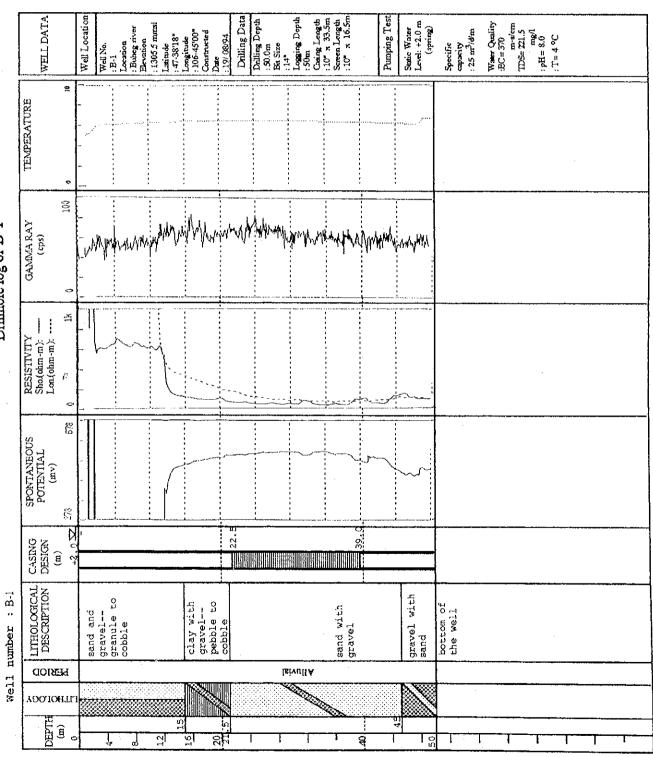
Well number : A-4



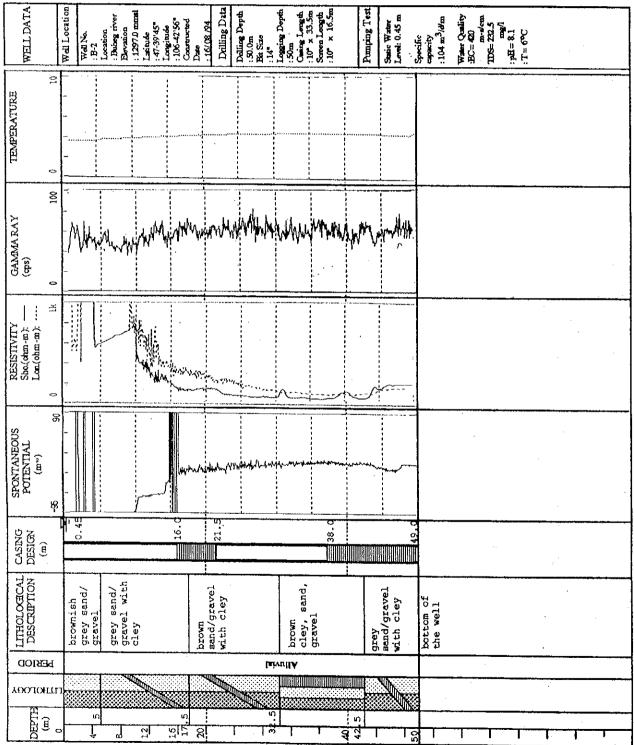
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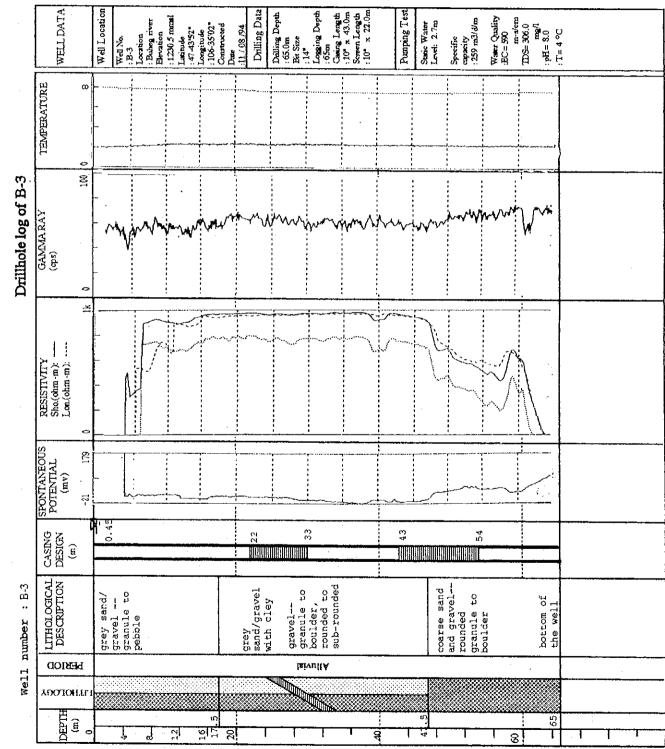
ALC: NO





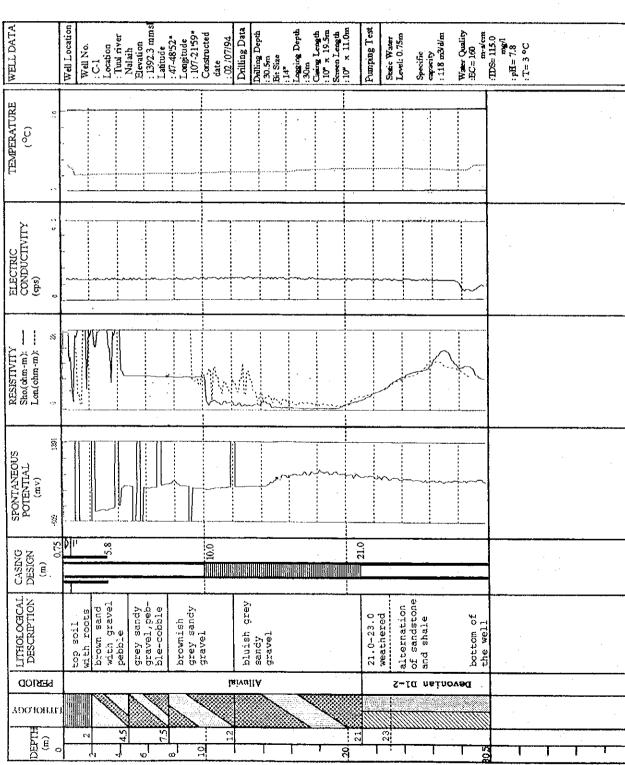


I - A - 100



I - A - 101

Well number : C-1



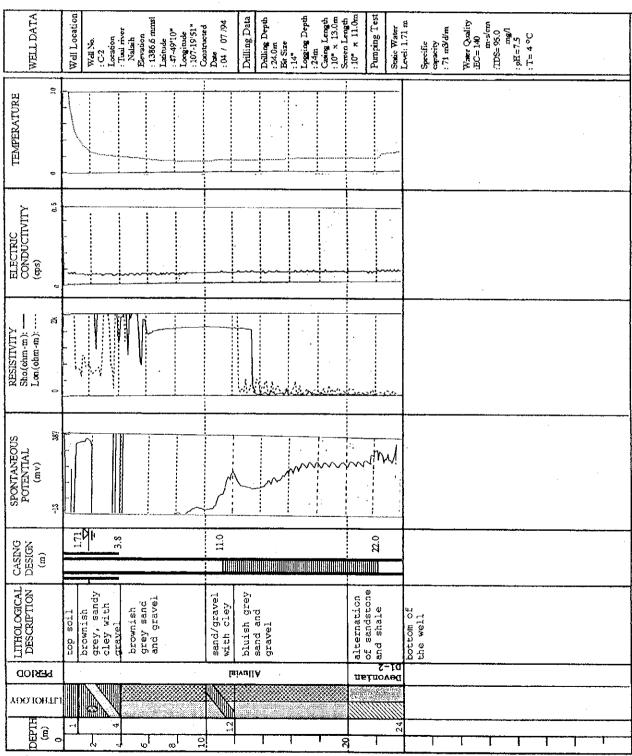
I - A - 102

3

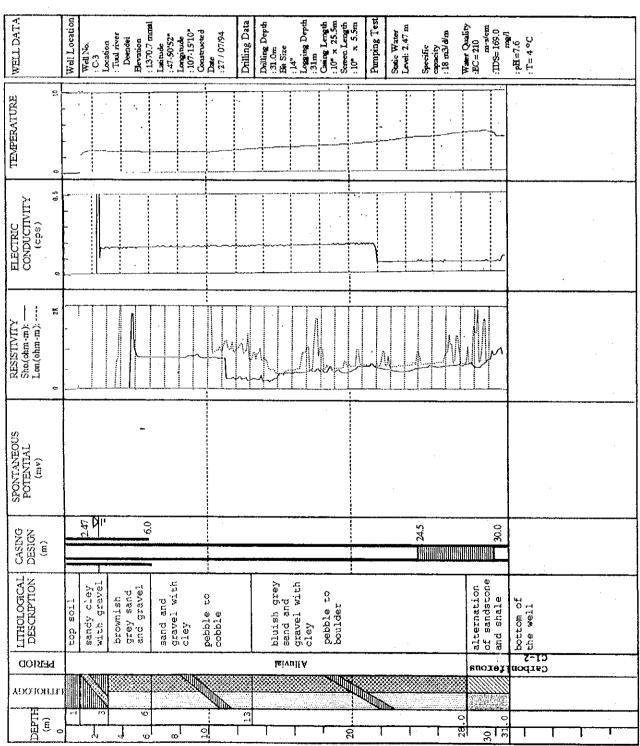
Drillhole log of C-2

Well number : C-2

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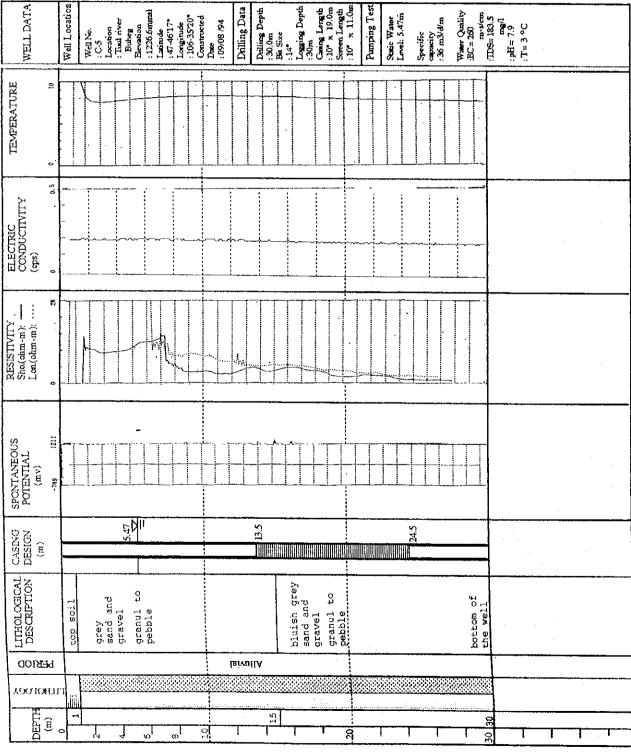
Well number : C-3



I - A - 104

	WELL DATA	Well Location Well No. : C-4 Location : C-4 Gashuurt Bevation : 1331.7 mmsl : 1317.9555 : Constructed Date : 14" Drilling Data Drilling Data Data Drilling Data Drilling Data Data Drilling Data Data Drilling Data Data Drilling Data Drilling Data Data Data Drilling Data Data Data Data Drilling Data Data Data Data Data Data Data Data
	TEMPERATURE 0	
Drillhole log of C-4	ELECTRIC CONDUCTIVITY (cps) 0.5	
DHI	RESISTIVITY Sho(ohm-m): Lon.(ohm-m): ò \$3*: 2x	
	SPONTANEOUS POTENTIAL (mv) -289 1211	
	CASING DESIGN (m)	9,1 9,1 9,1 9,1 9,1 9,1 9,1 9,1
Well number : C4	DESCRIPTION	top soil sand with gravel gravel yellowish brown sandand gravel i4.0-15.5 weathered shale bottom of the well
Well	BERIOD FILHOLOGY	
	DEPTH (m)	
		I - A - 105

Well number : C-5



I - A - 106

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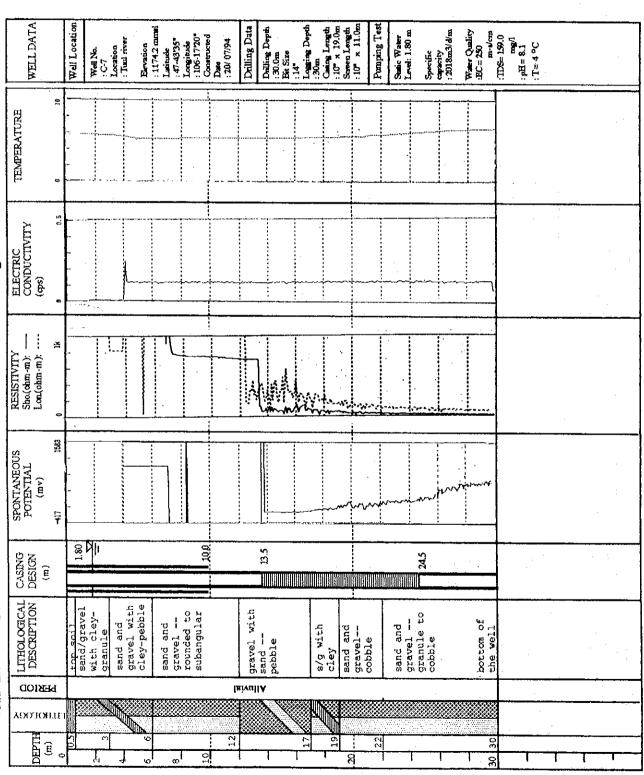
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	WELLDATA	Well Location	Well No. : C-6 Location : Toul river	Bevation : 1204.5 turnel Latitudo : 47.45'52* Longitudo Longitudo Con turnel	Date: :31/07/94	Drilling Data Driling Depth : 32.0m Bit Size : 14*	Logging Depth :32m Caing Longth :10" x 15.5m Saven Longth	Pumping Test	Static Water Lovel: 1.93 m Specific capacity	: 1227m3/d/m	.EC=260 	. pH= 8.0	) S = = T ::	
	TEMPERATURE													-
	ELECTRIC CONDUCTIVITY (aps)											~		
	RESISTIVITY Sho(ohm-m): Lon(ohm-m):						A. J.							
	PONTANEOUS POTENTIAL (mv)	-563 1037		M	 -	_^^~	wit	~	_L	w	M	M		
	CASING DESIGN (m)		<u>8</u> pµ	· · · · · · · · · · · · · · · · · · ·	10.0	13.5						30.0		
Well number : C-6	LITHOLOGICAL DESCRIPTION	top soil	light grey gravel with cley	grey sand and gravel granule to pebble	s/g with cley	bluish grey sand and	gravei pebble	bluish grey sand	gravel cobble		sand and gravel	granule	bottom of the well	
a lie	PFRIOD				13 13 13 14 14 14 14 14 14 14 14 14 14 14 14 14	ivullA								
We	A90 IOHJ							<u></u>			<u></u>			
	(m)	-							· · ·	38	- <u>6</u>	32 32	<u> </u>	

Well number : C-7



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	WELL DATA	Well Location Well No.	: C-8 Location : Tuul river	Elevation : 1173.0 mmsl	Latitude : 47-42'50	: 106-18'10" Constructed	Date : 27/07 /94	Driling Data	Dalling Depth : 30.0m Bit Size	. 14 Logging Depth : 30m	Caing Length : 10" × 19.0m Somen Length	:10 × 11.0т	Pumping Test	Jewel: 1.20m	Specific	: 56 m3/d/m	Warr Quality EC= 240 m-scm	:105=146.5 mg/l : pH= 7.9 : T= 4 °C			 
	TEMPERATURE 0 10									-											 
	ELECTRIC CONDUCTIVITY (cps) 0.5														~~~~~	~~~~~					
	RESISTIVITY Sho(ohm-m): Lon(ohm-m): ¢ x						~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~										-				
	SPONTANEOUS POTENTIAL (mv) 161 1161					~	\							~	<u> </u>						
	CASING DESIGN (m)					100				I6.0			- Advergence - Adv			Z7.0					 
Well number : C-8	DESCRIPTION	top soil light arev	sand and gravel with cley-	granule	blue s/g with cley	grey sand and	gravel pebble		grey sand and gravel	granule to pebble		grey	sand and gravel	cobble			yellowish s/g -pebble	bottom of the well	<u> </u>		
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