

6.4.3 Unit Costs of Land and House Acquisition

The land and housing acquisition costs are calculated on the basis of standard rate obtained through Ministry of Housing and Physical Planning as shown in Table 6.5.:

Table 6.5 Unit Cost of Land/House Acquisition Cost

| Description | Unit | Unit Price (NRs.) | Remarks |
|--|------|-------------------|---------|
| Unit Cost of Land Acquisition | | | |
| Residential Area | ha | 40 million | |
| Commercial Area | ha | 80 million | |
| Industry Area | ha | 24 million | |
| Agriculture Area | ha | 12 million | |
| Unit Cost of Building Acquisition | | | |
| Commercial Building | | | |
| (Good Condition) | m2 | 7,000 | |
| (Average Condition) | m2 | 4,250 | |
| (Poor Condition) | m2 | 2,750 | |
| (Bad Condition) | m2 | 1,000 | |
| Residential Building | | | |
| (Good Condition) | m2 | 7,000 | |
| (Average Condition) | m2 | 4,250 | |
| (Poor Condition) | m2 | 2,750 | |
| (Bad Condition) | m2 | 1,000 | |

Source : Kathmandu Urban Development Project

Project Preparation Report, March 1992

6.5 Construction Quantities

Construction quantities are calculated on the basis of preliminary design. Summary of major work quantities is show in Table 6.6. Detailed quantities calculation is presented in Appendix 6.5.1

6.6 Estimated Project Cost

6.6.1 Construction Cost

The estimated construction cost at middle of November 1992 prices for all construction packages are summarized in Table 6.7. Detailed construction cost estimation by section is presented in Appendix 6.6.1.

Table 6.6 Work Quantities for Each Proposed Road

| Description | Unit | South link | Sanepa | Patan Core | Koteswor | Central bus | New Bagnati | Intersections | TOTAL |
|---|---------|-----------------------|--------|------------|----------|--------------------|-------------|---------------|---------|
| | | of Inner Ring Road | Access | Access | Access | terminal Access | Bridge No.2 | (3 Places) | |
| Clear site and stripping | m2 | 76,464 | 8,830 | 3,556 | 45,000 | 38,012 | | 2,500 | 174,362 |
| Removal of existing pavement material | m3 | 100 | | | | | 100 | | 200 |
| Removal of existing bridge at Thaphatali | L.S | | | | | | 1 | | 1 |
| Removal of existing structures | m3 | 100 | | | | | 100 | | 200 |
| Fill in soft material | m3 | 121,575 | 9,582 | 2,511 | 68,173 | 41,384 | 1,300 | 5,000 | 249,525 |
| Spoil in soft material | m3 | 5,655 | 1,373 | 275 | 11,004 | 196 | 130 | | 18,633 |
| Sodding | m2 | 25,648 | 2,414 | 1,086 | 15,599 | 10,856 | | 1,250 | 56,853 |
| Plant selected trees | no. | 744 | | | | | | | 744 |
| Gabion | m3 | 3,460 | | | 620 | | 3,210 | | 7,290 |
| Stone Masonry | m2 | 5,136 | | 490 | 250 | | 1,250 | 150 | 7,276 |
| Excavation in soft material for structures | m3 | 9,390 | | | 2,630 | 120 | 14,610 | | 26,750 |
| Backfilling with selected materials for structures | m3 | 6,900 | | | 2,020 | 40 | 10,460 | | 19,420 |
| Side block | m | 2,840 | | | | | | | 2,840 |
| Kerb stone (A) | m | 2,521 | 990 | 400 | 4,064 | 3,730 | | | 11,705 |
| Kerb stone (B) | m | 1,795 | | | 150 | | 400 | | 2,345 |
| Kerb stone for bridge | m | 546 | | | 120 | | 276 | | 942 |
| Pipe culvert D300 | m | 1,155 | 188 | 80 | 1,600 | 750 | | | 3,773 |
| Pipe culvert D600 | m | 1,770 | 240 | 200 | 1,060 | 760 | 100 | 60 | 4,190 |
| Pipe culvert D1000 | m | 205 | 74 | | 81 | 133 | 80 | | 573 |
| U shaped drain ditch (0.3 x 0.3m) | m | | 940 | 365 | | | | | 1,305 |
| U shaped drain ditch (0.5 x 0.5m) | m | 3,167 | | | 3,615 | 3,572 | | | 10,354 |
| U shaped drain ditch (1.0 x 1.0m) | m | 300 | | | | 132 | | | 432 |
| Side drain with stone pitching | m | 1,934 | | | | | | 500 | 2,434 |
| Catch pit | no. | 158 | 47 | 20 | 206 | 187 | 20 | 3 | 641 |
| Manhole | no. | 96 | 102 | 4 | 114 | 90 | 4 | 3 | 413 |
| Subbase course | m3 | 13,028 | 638 | 423 | 2,894 | 4,875 | 290 | 750 | 22,898 |
| Base course | m3 | 11,298 | 552 | 368 | 2,504 | 4,219 | 310 | 500 | 19,751 |
| Prime coat, 1.0 litre/m2 | m2 | 38,968 | 4,880 | 1,600 | 22,620 | 18,650 | 5,565 | 2,500 | 94,783 |
| Tack coat, 0.4litre/m2 | m2 | 71,288 | 4,880 | 1,600 | 22,140 | 18,650 | 4,185 | 1,000 | 123,743 |
| Asphalt concrete binder course t=6cm | m2 | 1,750 | 4,880 | 1,600 | 22,140 | 18,650 | 2,910 | 2,500 | 54,430 |
| Asphalt concrete binder course t=10cm | m2 | 35,100 | | | | | 1,280 | | 36,380 |
| Asphalt concrete surfase course t=4cm | m2 | 4,480 | 4,880 | 1,600 | 22,620 | 18,650 | 4,700 | 2,500 | 59,430 |
| Asphalt concrete surfase course t=5cm | m2 | 35,100 | | | | | 1,280 | | 36,380 |
| Side walk t=13cm | m2 | 19,335 | 2,440 | 1,600 | 11,370 | 9,325 | 1,490 | | 45,560 |
| Road lighting | no. | 42 | | | | | 22 | | 64 |
| Traffic signal | portion | 4 | 1 | 1 | 1 | 2 | 1 | 2 | 12 |
| Lane marking 15cm | m | 12,694 | 1,575 | 690 | 6,741 | 5,775 | 1,258 | 2,400 | 31,133 |
| Information sign | no. | 19 | 3 | 3 | 3 | 6 | 4 | 9 | 47 |
| Steel pile D800 | m | 4,474 | | | 1,530 | | 1,680 | | 7,684 |
| Steel pile D500 | m | 1,840 | | | | | 1,640 | | 3,480 |
| Concrete class-A, 240kg | m3 | 3,970 | | | 970 | 73 | 2,170 | | 7,183 |
| Concrete class-C, 180kg | m3 | 120 | | | 30 | 8 | 3,136 | | 3,294 |
| Formwork for superstructures | m2 | 4,100 | | | 910 | | 2,170 | | 7,180 |
| Formwork for all structures other than superstructur | m2 | 3,290 | | | 880 | 245 | 8,706 | | 13,121 |
| Reinforcement | ton | 472 | | | 112 | 8 | 250 | | 842 |
| Prate girder (material,assemble,transportation,electi | ton | 678 | | | 117 | | 405 | | 1,200 |
| Bridge railing | m | 546 | | | 120 | | 276 | | 942 |
| Excavation for diversion of the river | m3 | 2,680 | | | | | | | 2,680 |
| Construction and removal of temporary road | m3 | 8,290 | | | 1,670 | | | | 9,960 |
| Temporary bridge | m | 12 | | | | | 70 | | 82 |
| Steel sheet pile | m | | | | | | 8,260 | | 8,260 |

Table 6.7 Summary of Construction Cost

| Description | South Inner | New Bagmati | Sanepa | Koteswor | Patan Core | New Bus | Traffic Manag. | Total |
|--|--------------------|--------------------|-------------------|--------------------|-------------------|-------------------|-------------------|----------------------|
| | Ring Road Incl. | Bridge Incl. | Access | Access Incl. | Access | Terminal Access | at Intersections | |
| | Br.No1&No3, | Thapathali Inter | | Br. No.4 | | | | |
| | Patan Inter. & | Pedestrian Br. | | | | | | |
| | Pedest. Br. | Check Dam | | | | | | |
| Clear site and stripping | 1,529,280 | 0 | 176,600 | 900,000 | 71,120 | 760,240 | 50,000 | 3,487,240 |
| Removal of existing pavement material | 38,500 | 38,500 | 0 | 0 | 0 | 0 | 0 | 77,000 |
| Removal of existing bridge at Thaphatali | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Removal of existing structures | 195,800 | 195,800 | 0 | 0 | 0 | 0 | 0 | 391,600 |
| Fill in soft material | 50,939,925 | 544,700 | 4,014,858 | 28,564,487 | 1,052,109 | 17,339,896 | 2,095,000 | 104,550,975 |
| Spoil in soft material | 1,702,155 | 39,130 | 413,273 | 3,312,204 | 82,775 | 58,996 | 301,000 | 5,909,533 |
| Sodding | 5,001,360 | 0 | 470,730 | 3,041,805 | 211,770 | 2,116,920 | 243,750 | 11,086,335 |
| Plant selected trees | 961,248 | 4,834,200 | 0 | 0 | 0 | 0 | 0 | 5,795,448 |
| Gabion | 7,964,920 | 8,661,220 | 0 | 1,427,240 | 0 | 0 | 0 | 18,053,380 |
| Stone Masonry | 31,400,416 | 2,008,000 | 0 | 1,526,500 | 2,991,940 | 0 | 915,900 | 38,842,756 |
| Excavation in soft material for structures | 438,500 | 571,200 | 0 | 131,500 | 0 | 6,000 | 0 | 1,147,200 |
| Backfilling with selected materials for struc. | 301,500 | 148,500 | 0 | 90,900 | 0 | 1,800 | 0 | 542,700 |
| Side block | 2,263,480 | 0 | 0 | 0 | 0 | 0 | 0 | 2,263,480 |
| Kerb stone (A) | 4,870,572 | 0 | 1,912,680 | 7,851,648 | 772,800 | 7,206,360 | 1,545,600 | 24,159,660 |
| Kerb stone (B) | 6,840,745 | 1,524,400 | 0 | 571,650 | 0 | 0 | 0 | 8,936,795 |
| Kerb stone for bridge | 444,444 | 224,664 | 0 | 97,680 | 0 | 0 | 0 | 766,788 |
| Pipe culvert D300 | 3,481,170 | 0 | 566,632 | 4,822,400 | 241,120 | 2,260,500 | 0 | 11,371,822 |
| Pipe culvert D600 | 9,405,780 | 531,400 | 1,275,360 | 5,632,840 | 1,062,800 | 4,038,640 | 318,840 | 22,265,660 |
| Pipe culvert D1000 | 2,180,175 | 850,800 | 786,990 | 861,435 | 0 | 1,414,455 | 0 | 6,093,855 |
| U shaped drain ditch (0.3 x 0.3m) | 0 | 0 | 1,858,380 | 0 | 721,605 | 0 | 1,581,600 | 4,161,585 |
| U shaped drain ditch (0.5 x 0.5m) | 8,652,244 | 0 | 0 | 9,876,180 | 0 | 9,758,704 | 0 | 28,287,128 |
| U shaped drain ditch (1.0 x 1.0m) | 1,981,800 | 0 | 0 | 0 | 0 | 871,992 | 0 | 2,853,792 |
| Side drain with stone pitching | 3,318,744 | 0 | 0 | 0 | 0 | 0 | 858,000 | 4,176,744 |
| Catch pit | 1,537,340 | 194,600 | 457,310 | 2,004,380 | 194,600 | 1,819,510 | 29,190 | 6,236,930 |
| Manhole | 1,560,576 | 65,024 | 1,658,112 | 1,853,184 | 65,024 | 1,463,040 | 48,768 | 6,713,728 |
| Subbase course | 10,552,680 | 234,900 | 516,780 | 2,344,140 | 342,630 | 3,948,750 | 607,500 | 18,547,380 |
| Base course | 16,562,868 | 454,460 | 809,232 | 3,670,864 | 539,488 | 6,185,054 | 733,000 | 28,954,966 |
| Prime coat, 1.0 litre/m2 | 1,324,912 | 189,210 | 165,920 | 769,080 | 54,400 | 634,100 | 85,000 | 3,222,622 |
| Tack coat, 0.4litre/m2 | 784,168 | 46,035 | 53,680 | 243,540 | 17,600 | 205,150 | 11,000 | 1,361,173 |
| Asphalt concrete binder course t=6cm | 1,160,250 | 1,929,330 | 3,235,440 | 14,678,820 | 1,060,800 | 12,364,950 | 4,972,500 | 39,402,090 |
| Asphalt concrete binder course t=10cm | 39,066,300 | 1,424,640 | 0 | 0 | 0 | 0 | 2,782,500 | 43,273,440 |
| Asphalt concrete surfase course t=4cm | 2,136,960 | 2,241,900 | 2,327,760 | 10,789,740 | 763,200 | 8,896,050 | 3,577,500 | 30,733,110 |
| Asphalt concrete surfase course t=5cm | 20,673,900 | 753,920 | 0 | 0 | 0 | 0 | 1,472,500 | 22,900,320 |
| Side walk t=13cm | 8,932,770 | 688,380 | 1,127,280 | 5,252,940 | 739,200 | 4,308,150 | 254,100 | 21,302,820 |
| Road lighting | 11,546,262 | 6,048,042 | 0 | 0 | 0 | 0 | 5,498,220 | 23,092,524 |
| Traffic signal | 23,461,275 | 4,692,255 | 4,692,255 | 4,692,255 | 4,692,255 | 9,384,510 | 9,384,510 | 60,999,315 |
| Lane marking 15cm | 698,170 | 69,190 | 86,625 | 370,755 | 37,950 | 317,625 | 132,000 | 1,712,315 |
| Information sign | 4,314,672 | 908,352 | 681,264 | 681,264 | 681,264 | 1,362,528 | 2,043,792 | 10,673,136 |
| Steel pile D800 | 100,987,128 | 37,920,960 | 0 | 34,535,160 | 0 | 0 | 0 | 173,443,248 |
| Steel pile D500 | 20,766,240 | 18,509,040 | 0 | 0 | 0 | 0 | 0 | 39,275,280 |
| Concrete class-A, 240kg | 18,627,240 | 10,181,640 | 0 | 4,551,240 | 0 | 342,516 | 0 | 33,702,636 |
| Concrete class-C, 180kg | 444,120 | 11,606,336 | 0 | 111,030 | 0 | 29,608 | 0 | 12,191,094 |
| Formwork for superstructures | 3,702,300 | 1,959,510 | 0 | 821,730 | 0 | 0 | 0 | 6,483,540 |
| Formwork for all struc. other than superstruc | 1,918,070 | 5,075,598 | 0 | 513,040 | 0 | 142,835 | 0 | 7,649,543 |
| Reinforcement | 18,260,736 | 9,672,000 | 0 | 4,333,056 | 0 | 309,504 | 0 | 32,575,296 |
| Plate girder (material,assemble,transp.,etc.) | 348,573,360 | 208,218,600 | 0 | 60,152,040 | 0 | 0 | 0 | 616,944,000 |
| Bridge railing | 12,495,756 | 6,316,536 | 0 | 2,746,320 | 0 | 0 | 0 | 21,558,612 |
| Excavation for diversion of the river | 134,000 | 0 | 0 | 0 | 0 | 0 | 0 | 134,000 |
| Construction and removal of temporary road | 3,473,510 | 0 | 0 | 699,730 | 0 | 0 | 0 | 4,173,240 |
| Temporary bridge | 658,812 | 3,843,070 | 0 | 0 | 0 | 0 | 0 | 4,501,882 |
| Steel sheet pile | 0 | 23,243,640 | 0 | 0 | 0 | 0 | 0 | 23,243,640 |
| TOTAL | 818,267,133 | 376,659,682 | 27,287,161 | 224,522,777 | 16,396,450 | 97,548,383 | 39,541,770 | 1,600,223,356 |

6.6.2 Land Acquisition Cost and Compensation Cost

Table 6.8 shows the summary of the estimated land and house acquisition costs and replacement of public utilities (i.e. local currency component).

6.6.3 Summary of Estimated Project Cost

Summary of estimated project cost including construction cost, land/house acquisition cost, physical and price contingency, engineering cost (detailed design and construction supervision) is presented in Table 6.9.

6.7 Maintenance Cost

Road maintenance cost includes the following three items:

Road maintenance cost:

- (1) Electricity cost ; cost of electricity for lighting and signal operation
- (2) Cleaning cost ; cost of cleaning the road surface, drainage facilities, guardrails, regulatory traffic sign and other traffic devices.
- (3) Repair cost ; cost of road surface repair, overlays, painting of bridges and guardrails, etc. inspection of structures, inspection and repair of electricity and traffic control facilities.

Referring to the annual budget of DOR and relevant data, the annual cost for maintenance and operation required for the Project is roughly estimated at NRs. 20,000 per km of the proposed road for 2 lane. After widening to 4 -lane, it is estimated to increase by 10 %.

Tax and duties which are used for conversion between financial cost and economic cost, are estimated as 10 % of the financial cost.

Table 6.8 Land and House Acquisition Cost

Unit: NRs. x 1,000

| Description | Unit | Unit Price (NRs.x1,000) | South link of inner ring road | | Sanepa access | | Patan access | | Koteswor access | | Central bus terminal access | | Intersection at Thaphatali side | | Intersection at Patan side | |
|-------------------------------------|------|----------------------------|-------------------------------|---------|---------------|--------|--------------|--------|-----------------|---------|-----------------------------|--------|---------------------------------|------|----------------------------|-------|
| | | | Area | Cost | Area | Cost | Area | Cost | Area | Cost | Area | Cost | Area | Cost | Area | Cost |
| Cost of Land Acquisition | | | | | | | | | | | | | | | | |
| Residential Area | m2 | 4.00 | 29,250 | 117,000 | 2,440 | 9,760 | 3,110 | 12,440 | 26,200 | 104,800 | 5,900 | 23,600 | 220 | 880 | 580 | 2,320 |
| Commercial Area | m2 | 8.00 | | | | | | | | | | | | | | |
| Industry Area | m2 | 2.50 | | | | | | | | | | | | | | |
| Agriculture Area | m2 | 1.20 | 29,940 | 35,928 | 7,830 | 9,396 | | | 21,040 | 25,248 | 33,030 | 39,636 | | | | |
| Cost of Building Acquisition | | | | | | | | | | | | | | | | |
| Commercial Building | | | | | | | | | | | | | | | | |
| (Good Condition) | m2 | 7.00 | | | | | | | | | | | | | | |
| (Average Condition) | m2 | 4.25 | | | | | | | | | | | | | | |
| (Poor Condition) | m2 | 2.75 | | | | | | | | | | | | | | |
| (Bad Condition) | m2 | 1.00 | | | | | | | | | | | | | | |
| Residential Building | | | | | | | | | | | | | | | | |
| (Good Condition) | m2 | 7.00 | | | | | | | | | | | | | | |
| (Average Condition) | m2 | 2.75 | 11,000 | 30,250 | 730 | 2,008 | 580 | 1,595 | 2,410 | 6,628 | 5,430 | 14,933 | 80 | 220 | 1,110 | 3,053 |
| (Poor Condition) | m2 | 2.75 | | | | | | | | | | | | | | |
| (Bad Condition) | m2 | 1.00 | | | | | | | | | | | | | | |
| TOTAL | | | | 183,178 | | 21,164 | 14,035 | | 136,676 | | 78,169 | 1,100 | | | 5,373 | |

Source : Kathmandu Urban Development Project

Project Preparation Report, March 1992

Table 6.9 Estimated Project Cost

| No. | Sub-project | Amount | | | (1,000yen) |
|--|--|------------------|----------------|------------------|------------------|
| | | Foreign Portion | Local Portion | Total | |
| Unit : 1,000NRs. | | | | | |
| A-1 NEW BAGMATI BRIDGE WITH TWO INTERSECTIONS | | | | | |
| | Demolishing of existing old truss bridge | 4,802 | 1,201 | 6,003 | 15,959 |
| | Construction of New Bagmati Bridge at Thaphatali | 215,142 | 10,700 | 225,842 | 600,401 |
| | Construction of Patan side Intersection | 9,288 | 1,572 | 10,860 | 28,871 |
| | Construction of Thaphatali side Intersection with signal | 20,536 | 2,571 | 23,107 | 61,430 |
| | Pedestrian bridge at Thaphatali side Intersection | 87,734 | 4,026 | 91,760 | 243,944 |
| | River Improvement, scoring protection by check dam | 31,948 | 4,003 | 35,951 | 95,576 |
| | Relocation of water main, electrical wire, telephone line, etc. | 36,868 | 752 | 37,620 | 100,013 |
| | TOTAL | 406,318 | 24,825 | 431,143 | 1,146,194 |
| A-2 WESTERN SECTION OF SOUTH INNER RING ROAD | | | | | |
| | Construction of road with 2 lanes | 107,909 | 22,617 | 130,526 | 347,003 |
| | Construction of No.1 Bridge | 243,722 | 11,594 | 255,316 | 678,758 |
| | Riverside protection (1000m x 2.5m = 2500m ² stone masonry) | 12,213 | 3,053 | 15,266 | 40,585 |
| | TOTAL | 363,844 | 37,264 | 401,108 | 1,066,346 |
| A-3 SANEPA ACCESS | | | | | |
| | Construction of road with 2 lanes | 22,467 | 4,820 | 27,287 | 72,542 |
| A-4 EASTERN SECTION OF SOUTH INNER RING ROAD | | | | | |
| | Construction of road with 2 lanes | 107,909 | 22,617 | 130,526 | 347,003 |
| | Pedestrian bridge at Patan side Intersection and signal | 102,833 | 4,599 | 107,432 | 285,608 |
| | Construction of No.3 Bridge | 174,153 | 9,455 | 183,608 | 488,122 |
| | Riverside protection (1000m x 2.5m = 2500m ² stone masonry) | 12,213 | 3,053 | 15,266 | 40,585 |
| | TOTAL | 397,108 | 39,724 | 436,832 | 1,161,318 |
| A-5 KOETSWOR ACCESS | | | | | |
| | Construction of road with 2 lanes | 89,899 | 22,500 | 112,399 | 298,813 |
| | Construction of No.4 Bridge | 106,927 | 5,197 | 112,124 | 298,082 |
| | Riverside protection (1000m x 2.5m = 2500m ² stone masonry) | 12,213 | 3,053 | 15,266 | 40,585 |
| | TOTAL | 209,039 | 30,750 | 239,789 | 637,479 |
| A-6 PATAN ACCESS | | | | | |
| | Construction of road with 2 lanes | 13,977 | 2,419 | 16,396 | 43,589 |
| | TOTAL | 1,412,753 | 139,802 | 1,552,555 | 4,127,467 |
| | Consultant Fee 10% | | | 155,256 | 412,747 |
| | A-TOTAL | | | 1,707,811 | 4,540,214 |
| B-1 CENTRAL BUS TERMINAL ACCESS | | | | | |
| | Construction of road with 2 lanes | 79,188 | 18,360 | 97,548 | 259,331 |
| | Consultant Fee 10% | | | 9,755 | 25,933 |
| | B-TOTAL | | | 107,303 | 285,264 |
| C-1 IMPROVEMENT OF INTERSECTIONS | | | | | |
| | Intersections at Mitighar, Tripureswar and Koteswor | 35,282 | 4,260 | 39,542 | 105,122 |
| | Consultant Fee 10% | | | 3,954 | 10,512 |
| | C-TOTAL | | | 43,496 | 115,635 |
| | GRAND TOTAL | | | 1,858,610 | 4,941,113 |

CHAPTER 7
IMPLEMENTATION PLAN



CHAPTER 7 IMPLEMENTATION PLAN

7.1 Executing Agency

The Director General of Department of Roads (DOR), Ministry of Works and Transport, is the government agency responsible for the execution of the construction of the project roads.

The land acquisition and compensation required for the implementation of the project will be undertaken by the same agency prior to the start of construction.

7.2 Construction Packages

The project is divided into three packages with three (3) sub packages taking into consideration the nature of project feature, scale of the work volume and ease of implementation from the land acquisition view point as follows:

Package A : Improvement of Bagmati Transport Corridor, dividing into;

- A-1 New Bagmati Bridge at Thapathali
- A-2 Western Section of South Link of Inner Ring Road including Sanepa Access
- A-3 Eastern Section of South Link of Inner Ring Road including Koteswor Access and Patan Access

Package B : Construction of New Bus Terminal Access at Balaju

Package C : Improvement of Intersections at Maitighar, Tripureswar and Koteswor

7.3 Implementation Programme

Construction period is set up taking into account the work volume, weather condition required funds for each package and urgency of the project, etc. as follows:

| | | |
|-----------|--|------------|
| Package A | : Improvement of Bagmati Transport Corridor | |
| | Package A-1 Construction of New Bagmati Bridge | ; 2 years |
| | Package A-2 Construction of Western Section of South Link of Inner Ring Road | ; 2 years |
| | Package A-3 Construction of Eastern Section of South Link of Inner Ring Road | ; 2 years |
| Package B | : Construction of New Bus Terminal Access at Balaju | ; 2 years |
| Package C | : Improvement of Intersections at Mitighar, Tripureswar and Koteswor | ; 6 months |

The recommended implementation time schedule is as shown in Fig. 7.1.

7.4 Investment Programme

Investment programme of the project is prepared on the basis of the implementation time schedule and summarized in Table 7.1.

Fig. 7.1: Proposed Implementation Schedule of High Priority Projects

| Package No. | Proposed Roads and Bridges To be Improved | Target for Development: | High Priority projects to be Implemented in the Short-term Plan | | | | |
|------------------|---|-------------------------|---|-----------------|-----------------|-----------------|-----------------|
| | | | Improvement of Bottlenecks in Urban Traffic Conditions | | | | |
| | | | Relief of Transportation-Poor | | | | |
| | | Year: | 1st Year | 2nd Year | 3rd Year | 4th Year | 5th Year |
| (1) Package A-1: | Construction of New Bagmati Bridge (2 Lanes) with Improvement of Thapathali Intersection, Existing Bagmati Bridge and River Protection | | 1993 | 1994 | 1995 | 1996 | 1997 |
| (2) Package B: | Construction of Access to New Bus Terminal | | xxxxxxxxxxxxxxx | xxxxxxxxxxxxxxx | | | |
| (3) Package A-2: | Western Section of South Inner Ring Road including Bagmati Bri. No.1 Sanepa Access | | | xxxxxxxxxxxxxxx | xxxxxxxxxxxxxxx | | |
| (4) Package A-3: | Eastern Section of South Inner Ring Road including Bagmati Bri. No.3 Patan Intersection, Patan Access and Koteswor Access including Bagmati Bri. No.3 | | | | | xxxxxxxxxxxxxxx | xxxxxxxxxxxxxxx |
| (5) Package C: | Improvement of Intersections at Maitighar, Tripureswar and Koteswor | | xxxxxxx | | | | |

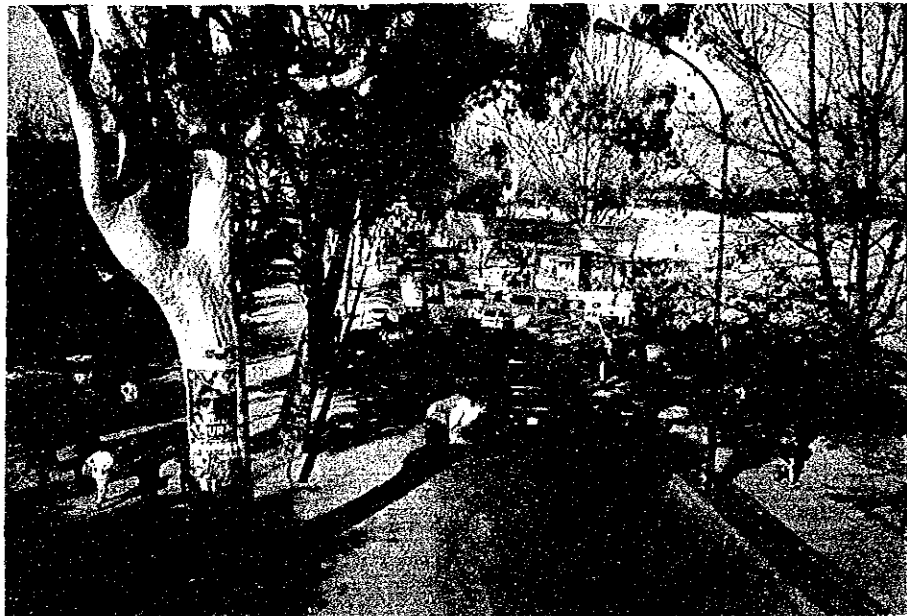
Table 7.1: Tentative Investment Programme of High Priority Projects

Unit: NRs. million

| Phase | Target for Development: | High Priority projects to be Implemented in the Short-term Plan | | | | | | | | | | | |
|------------------|---|---|------------|------------------|------------|------------------|------------|------------------|------------|------------------|------------|-------|-----|
| | | (2) Relief of Bottlenecks in Urban Traffic Conditions | | | | | | | | | | | |
| | | 1st. Year 1993 | | 2nd Year 1994 | | 3rd Year 1995 | | 4th Year 1996 | | 5th Year 1997 | | Total | |
| Const. Cost | Land/House | Construction | Land/House | Construction | Land/House | Construction | Land/House | Construction | Land/House | Construction | Land/House | | |
| (1) Package A-1: | Construction of Bagmati Bridge No.2 (2lanes) including: Construction of New Bagmati Bridge Improv. of Existing Bagmati Bridge & River Protection Thapathali Intersection with Pedestrian Bridge. Demolishing of Existing Old Truss Bridge, Relocation of Water Main, Electric Line, etc. | 250 | 6 | 181 | | | | | | | | 431 | 6 |
| (2) Package B: | Construction of Access to New Bus Terminal | 59 | 78 | 39 | | | | | | | | 98 | 78 |
| (3) Package A-2: | Western Section of South Inner Ring Road including: Bagmati Bridge No.1 (2 lane), Sanepa Access, Riverside Protection. | | 204 | 150 | | 278 | | | | | | 428 | 204 |
| (4) Package A-3: | Eastern Section of South Inner Ring Road including: Bagmati Bridge No.3 (2 lane) and River Protection Patan Intersection including Pedestrian Bridge Patan Access Koteswor Access including Bagmati Bri. No.4 | | | | | | 151 | 350 | | 343 | | 693 | 151 |
| (5) Package C: | Improvement of 3 Intersections (Maitighar, Tripureswar and Koteswor) | 40 | | | | | | | | | | 40 | |
| | Total: | 349 | 289 | 370 | 0 | 278 | 151 | 350 | 0 | 343 | 0 | 1,690 | 439 |
| | Consultant Fee : D/D & S/N = 10 % of Construction cost in each phase | 35 | | 37 | | 28 | | 35 | | 34 | | 169 | |
| | Grand Total: | 383 | 289 | 407 | 0 | 306 | 151 | 385 | 0 | 377 | 0 | 1,859 | 439 |
| | Equiv. to Yen (Million) | 1,019 | | 1,082 | | 814 | | 1,024 | | 1,003 | | 4,942 | |

Exchange Rate: 1US\$ = NRs. 46.568 = ¥ 123.3 (Average rate in the past 6 months from June, 1992 to December, 1992), or 1 NRs. 1.0 = ¥ 2.6585

CHAPTER 8
ECONOMIC EVALUATION



CHAPTER 8 ECONOMIC EVALUATION

8.1 General

8.1.1 Introduction

In this chapter, the two proposed high priority packages as introduced in the previous chapter are economically evaluated. Initially, estimated project costs for each package of the project were economically evaluated in relation to the expected amount of benefit produced by each package to ascertain the overall economic feasibility in national economy. Second, the estimated project costs for these high priority projects have also been evaluated financially in terms of financial program of the eighth national development plan.

8.1.2 Procedure for Economic Evaluation

The procedure for economic evaluation is given in Fig. 8.1, and projects are evaluated through such indicators as Benefit/Cost Ratio (B/C ratio), Net Present Value (NPV) and Internal Rate of Return (IRR). For the application of these indicators, cost and benefit expressed in economic term and stream of them throughout the project life must be prepared as well as the premise of evaluation.

8.1.3 Indicators for Economic Evaluation

Three indicators are used for the evaluation of road construction projects as explained below :

(1) B/C Ratio

$$\text{B/C ratio} = \text{B/C}$$

$$B = \sum_{t=1}^n B_t/(1+r)^t,$$

$$C = \sum_{t=1}^n C_t/(1+r)^t$$

Where

B_t : Benefit in the year t

C_t : Cost in the year t

r : Discount rate

n : Project life in years

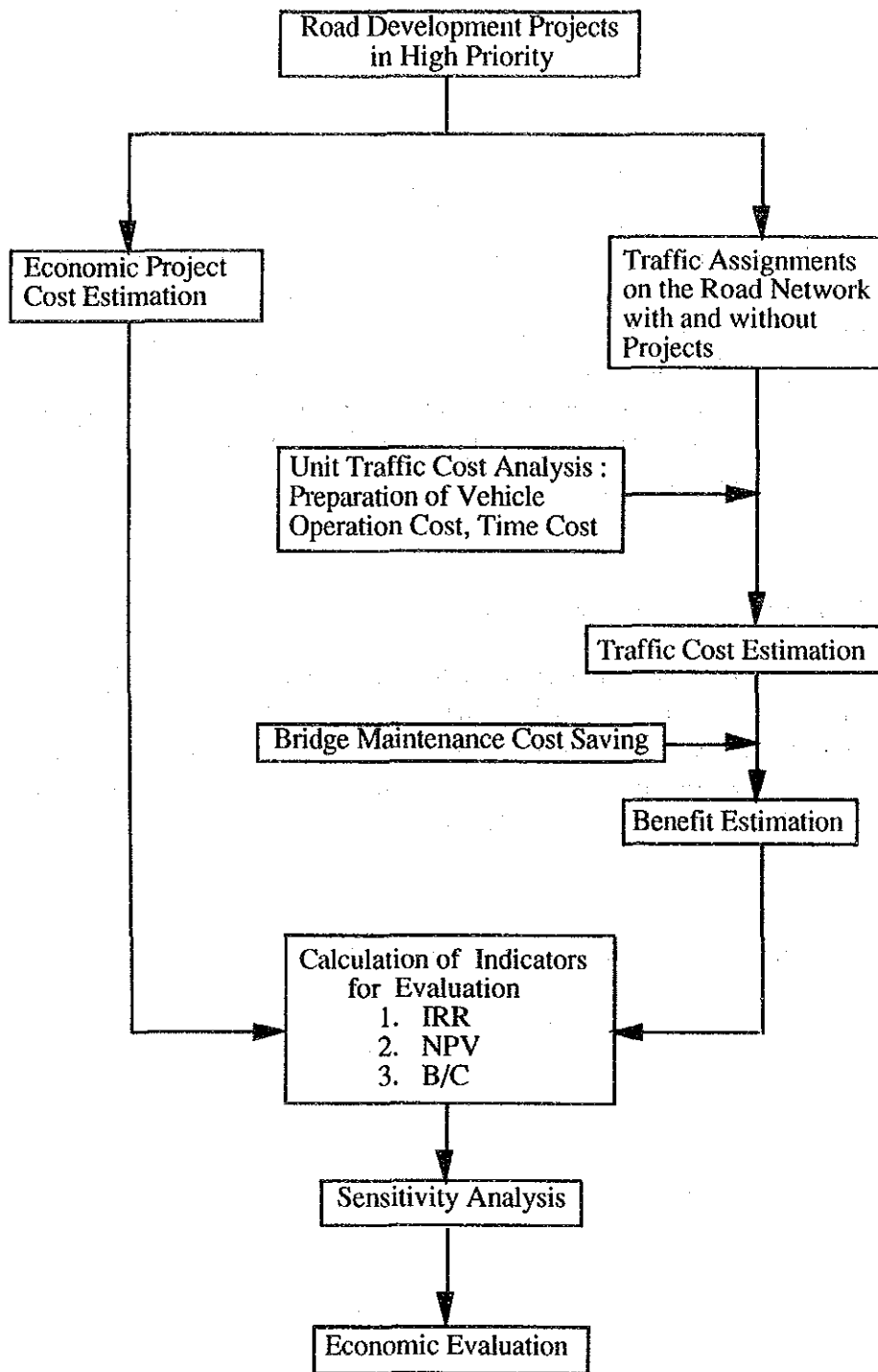


Fig. 8.1 Procedure for Economic Evaluation

The B/C ratio is the ratio of discounted benefit to discounted cost. Consequently, a ratio which is greater than 1.0 means a project is economically feasible.

(2) NPV

$$NPV = B - C$$

$$B = \sum_{t=1}^n Bt/(1+r)^t,$$

$$C = \sum_{t=1}^n Ct/(1+r)^t$$

Where

- Bt : Benefit in the year t
- Ct : Cost in the year t
- r : Discount rate
- n : Project life in years

NPV is a balance between discounted benefit and discounted cost. Therefore, a positive value of this indicator means a project is economically feasible.

(3) IRR

IRR is obtained through the following formula :

$$B(R) - C(R) = 0$$

$$B(R) = \sum_{t=1}^n Bt/(1+R)^t,$$

$$C(R) = \sum_{t=1}^n Ct/(1+R)^t$$

Where,

- R: IRR
- Bt : Cost in the year t
- Ct : Cost in the year t
- n : Project life in years

IRR is interpreted as a discount rate which gives a break even point between the discounted benefit and cost. Value greater than the assumed opportunity capital costs in a nation means a project is economically feasible.

8.1.4 Precondition for the Calculation of Economic Indicators

For the calculation of economic indicators, following precondition were given:

(1) Projects to be evaluated

As stated in Chapter 7, two high priority packages, namely Package A: "Improvement of Bagmati Transport Corridor" consisting of New Bagmati Bridge (Corresponding to Package A-1 in Chapter 7) and South Link of Inner Ring Road (Corresponding Package A-2 and A-3 in Chapter 7), and Package B: "Improvement of Access to New Bus Terminal" were recommended to be implemented in the short-term.

Economic calculation has been conducted for the following package:

- Case 1: Construction of New Bagmati Bridge and South Link of Inner Ring Road (Package A-1, A-2 and A-3 combined)
- Case 1-1: New Bagmati Bridge (Package A-1 only)
- Case 1-2: South Link of Inner Ring Road (Package A-2 and A-3 only)
- Case 2: Construction of New Bus Terminal Access

The Package C, consisting of improvements of three intersections, have not been evaluated due to the difficulty of quantification of potential benefits i.e., reduction of traffic accidents, increased increments of traffic safety and a decrease in overall traffic delays at intersections.

(2) Project life

25 years of project life was assumed.

(3) Discount Rate

A 10% discount rate was applied throughout the project life on the basis of estimated opportunity cost of capital in Nepal.

8.2 Estimation of Economic Project Cost

8.2.1 Cost Disbursement Schedule

Cost Disbursement Schedule for the investment of the two high priority project packages in the short-term plan are established in as shown in Table 7-1.

8.2.2 Estimation of Economic Project Cost

The project cost estimated in Chapter 6 was converted into economic cost through the following procedure :

- Deduction of Tax and Duty

Transfer factors included in the project cost, such as taxes and duties, were deducted assuming 10% of the project cost is transfer factors.

- Exemption of Price Escalation

The price escalation portion included in the project cost was deleted.

- Deduction of Land Acquisition Cost

The land acquisition cost was deducted from the total project cost. It is generally accepted that the land acquisition cost is not included in the economic cost, because it is natural to think that increased land values due to the construction of roads will offset the initial land acquisition cost.

The stream of economic costs obtained through the above procedure are given in Table 8.1.

8.2.3 Maintenance Cost

Annual routine maintenance costs required after the opening of the Project Roads was estimated conservatively assuming that 5% of the total project cost is maintenance cost for the entire project life which is assumed 25 years. Based on this information, maintenance costs were allocated throughout the project life as shown in Table 8.1.

8.3 Estimation of Traffic Cost

8.3.1 General

In order to estimate the total benefit from these Projects, road user's costs were estimated. Road user's costs here are composed of two types of cost : Vehicle operating cost and travel time cost.

For the estimation of road user's cost, unit vehicle operating cost and unit time cost, e.g. NRs./km and NRs./minute have been estimated. These unit costs were applied to the traffic volume obtained from the results of traffic assignments.

8.3.2 Vehicle Operating Cost

Vehicle operating costs are composed of fuel, lubricating oil consumption, tire and tube consumption, depreciation and capital cost, repair and maintenance cost (parts and labor), crew cost and overhead. Levels for vehicle operating costs differ by vehicle type, model, driving speed and other factors related to driving conditions.

(1) Representative Vehicle

Representative vehicles for each vehicle type were selected as shown in Table 8.2 primarily based on recent market shares in Nepal.

Table 8.2 Representative Vehicle

| Vehicle Type | Representative Vehicle | Market Share |
|---------------|------------------------------|--------------|
| Motor Cycle | Hero Honda | 50% |
| Passenger Car | Toyota Corolla (Hi-deluxe) | 65% |
| Truck | 7-8 Ton, TATA | 70% |
| Bus | 63 Seats, Long Chassis, TATA | 70% |

Source : The Study Team

(2) Unit Vehicle Operating Cost

Unit vehicle operating costs were estimated by vehicle types as shown in Table 8.3 after the examination of consumption rate of sub components.

(3) Unit Vehicle Operating Cost by Level of Speed

Each component of vehicle operating cost is categorized into two types of costs, i.e. time-related cost and distance-related cost.

- Time-related Vehicle Operating Cost

Those costs, (unit costs/per km) which are affected by the level of vehicle speed, such as fuel, oil, capital and crew costs are classified in this category of costs.

- Distance-related Vehicle Operating Cost

Those costs (unit costs/per km) which are independent from the level of vehicle speed, such as tire costs, depreciation and maintenance costs are classified in this category.

As for time and distance-related vehicle operating costs, unit costs were estimated by speed level applying information about unit vehicle operation cost by speed level in Japan. Estimated unit vehicle operating costs by level of speed are summarized in Table 8.4.

Table 8.3 Unit Vehicle Operating Cost (Economic Cost)*

(Unit : NRs. /1000 km)

| Items | Vehicle Type | | | |
|---------------------|--------------|---------------|--------------|--------------|
| | Motorcycle | Passenger Car | Truck | Bus |
| Fuel | 565 | 1,884 | 1,451 | 1,920 |
| Oil | 204 | 174 | 286 | 315 |
| Tire and Tube | 52 | 166 | 1,700 | 1,700 |
| Maintenance (Parts) | 64 | 1,108 | 1,422 | 1,746 |
| Maintenance (Labor) | 18 | 89 | 83 | 83 |
| Depreciation | 43 | 74 | 47 | 58 |
| Crew Cost | 0 | 150 | 354 | 354 |
| Capital Cost | 18 | 382 | 265 | 326 |
| Overhead | 145 | 605 | 1,402 | 1,625 |
| Total | 1,108 | 4,636 | 7,010 | 8,126 |

Source : The Study Team

* 50 km/h of running speed is assumed considering road condition in Nepal.

Table 8.4 Unit Vehicle Operating Cost by Speed

(Unit : NRs. /1000 km)

| Speed (km/hr) | Vehicle Type | | | |
|---------------|--------------|---------------|--------|--------|
| | Motorcycle | Passenger Car | Truck | Bus |
| 5 | 2,845 | 14,306 | 18,851 | 21,733 |
| 10 | 2,250 | 9,926 | 13,320 | 15,542 |
| 15 | 1,898 | 8,055 | 11,008 | 12,876 |
| 20 | 1,648 | 6,919 | 9,661 | 11,316 |
| 25 | 1,487 | 6,210 | 8,763 | 10,253 |
| 30 | 1,363 | 5,693 | 8,207 | 9,491 |
| 35 | 1,267 | 5,301 | 7,704 | 8,996 |
| 40 | 1,205 | 5,035 | 7,438 | 8,605 |
| 45 | 1,144 | 4,793 | 7,160 | 8,354 |
| 50 | 1,108 | 4,636 | 7,010 | 8,126 |
| 55 | 1,081 | 4,513 | 6,897 | 7,969 |
| 60 | 1,063 | 4,422 | 6,860 | 7,852 |
| 65 | 1,053 | 4,360 | 6,831 | 7,850 |
| 70 | 1,060 | 4,349 | 6,853 | 7,937 |
| 75 | 1,068 | 4,342 | 6,922 | 8,029 |
| 80 | 1,083 | 4,361 | 7,081 | 8,233 |
| 85 | 1,099 | 4,384 | 7,266 | 8,468 |

Source : The Study Team

8.3.3 Time Cost

(1) General

Time costs are another factor which composes total traffic costs. Unit time cost is estimated based on what is called "income approach method" in which time value is closely associated with income level of road users.

(2) Estimation of Time Value of Vehicle - user

1) Per Capita Income in Study Area

Due to lack of data on Gross Regional Product (GRP) in Kathmandu Valley, per capita income in the Study Area was estimated using a proportional formula of the Gross Domestic Product (GDP) per capita in Nepal as explained below:

$$\frac{\text{GRP k. 1991}}{\text{P k. 1991}} = A_{1991} \times \frac{\text{GDP n. 1991}}{\text{P n. 1991}}$$

where

| | | |
|-------------|---|--|
| GRP k. 1991 | : | GRP of Kathmandu Valley in 1991 |
| P k. 1991 | : | Population of Kathmandu Valley in 1991 |
| GDP n. 1991 | : | GDP of Nepal in 1991 |
| P n. 1991 | : | Population of Nepal in 1991 |
| A 1991 | : | Parameter in 1991 |

As for the estimation of the parameter, difference on an average residential land value between Kathmandu and all of Nepal was considered. As the result, per capita income in the Study Area was calculated as follows:

$$A_{1991} = \frac{\text{Average Resident Land Value in Kathmandu Valley in 1991}}{\text{Average Resident Land Value in rural area of Nepal in 1991}}$$

$$\begin{aligned} \frac{\text{GRP k. 1991}}{\text{P k. 1991}} &= \frac{32 \text{ million NRs./ha}}{6 \text{ million NRs./ha}} \times \frac{129,975 \text{ million NRs.}}{18,462 \text{ thousand persons}} \\ &= 5.3 \times 7,040 \text{ NRs./person} \\ &= 37,300 \text{ NRs./person} \end{aligned}$$

2) Estimation of Hourly Income

Assuming the total number of working days in Nepal as 290 and one day's net working hour as 6 hours, total working hours in a year is calculated at about 1,740 hours.

$$6 \text{ hours/day} \times 290 \text{ days} = 1,740 \text{ hours/year}$$

From this, average per capita income for one hour is estimated as below :

Average Per Capita Income for one hour

$$\begin{aligned} &= \text{Per Capita Income in 1991/Working Hours} \\ &= 37,300 \text{ (NRs./person)/1,740 (hours/year)} \\ &= 21.4 \text{ NRs./person hour} \end{aligned}$$

3) Estimation of Unit Time Cost

Unit time costs for each vehicle type were estimated as shown in Table 8.5, applying average number of passengers on board*1, share of economic activities among them*2 and the probability of selecting the productive activities*3 to the hourly per-capita incomes obtained above.

*1 Results of traffic surveys conducted by the Study Team and information from DOR were used for the set-up.

*2 The shares for economic activities such as business trips etc. among passengers were estimated based on share of trip-purposes obtained in the traffic survey (Ref. Article 4.2.2)

*3 Assuming all the time saved will not be used for "income-yielding activity".

Table 8.5 Unit Time Cost by Type of Vehicles

| Vehicle Type | Hourly Per capita Income (NRs.) (1) | Average Number of Passengers*1 (Person) (2) | Share of Business Trip*2 (3) | Probability of income-yielding activity*3 (4) | Unit Time Cost (NRs./hr) (5)=(1)x(2)x(3)x(4) |
|---------------|-------------------------------------|---|------------------------------|---|--|
| Motorcycle | 21.4 | 1.5 | 0.37 | 0.5 | 5.9 |
| Passenger Car | 21.4 | 2.7 | 0.27 | 0.5 | 7.8 |
| Truck | 21.4 | 3.2 | 0.37 | 0.5 | 12.7 |
| Bus | 21.4 | 45.8 | 0.20 | 0.5 | 98.0 |

*1, 2 : Result of traffic survey conducted by the Study Team (Ref. Table A-6-3 of appendix 6 and Article 4.2.2) (Drivers not included).

*3 : One-half of opportunity for selecting productive activity was assumed.

8.4 Benefit Estimate

8.4.1 Benefit Account

Theoretically, a variety of benefits will be brought about by the implementation of the Project. However many of these benefits are difficult to quantify because of the uncertainty in the processes in which these benefits are produced and lack of data. In this study, vehicle operating cost savings, travel time cost savings and bridge maintenance cost saving are quantified.

8.4.2 Estimation of Benefit

Benefit from the projects were estimated through the following procedure :

- 1) Vehicle operating cost (VOC) savings and time cost savings were deemed two of the major sources of benefit (road user benefit) from road development project.
- 2) For the estimation of road user's costs, unit vehicle operating costs, and unit time costs were applied to the total vehicle running distance and travel time simulated in traffic assignment.
- 3) Road user's benefit was obtained as the balance between road user's traffic costs for two different traffic assignment cases, i.e. "without the Project" case and "with the Project case".
- 4) Bridge maintenance cost savings were also estimated as one of the benefits for the bridge improvement project. Bridge maintenance cost savings were obtained as the balance of bridge maintenance costs for two different scenarios, i.e. "without bridge improvements case" and "with bridge improvements case" .

8.4.3 Benefit Flow

Benefit flows throughout the project life were estimated as shown in Table 8.7 in which annual increasing rates of benefit after the opening of the projects were assumed at 3.5% for Case 1, 3.1% for alternative Case 1-1, 2.5% for Case 1-2, and 3.6% for alternative Case 2.

Table 8.6 Road-User Benefit and Bridge Maintenance Benefit by Projects

(Unit: Million NRs.)

| Benefit | Projects | | | | |
|-----------------------|--------------------------|----------|----------|--------|-------|
| | Case 1 | Case 1-1 | Case 1-2 | Case 2 | |
| <u>Year 1997:</u> | | | | | |
| VOC: | Without Project case (1) | 3,099 | 3,054 | 3,088 | 3,067 |
| | With Project case (2) | 3,054 | 3,054 | 3,054 | 3,054 |
| | Saving (3) = (1)-(2) | 45 | 0 | 34 | 12 |
| Time Cost: | Without Project case (4) | 324 | 282 | 295 | 261 |
| | With Project case (5) | 257 | 257 | 257 | 257 |
| | Saving (6) = (4)-(5) | 67 | 25 | 38 | 4 |
| Road User Benefit: | (7) = (3)+(6) | 112 | 25 | 72 | 4 |
| Bridge Maintenance: | Without Project case (8) | 30 | 30 | 30 | - |
| | With Project case (9) | - | - | - | - |
| | Saving (10) = (8)-(9) | 30 | 30 | 30 | - |
| <u>Total Benefit:</u> | Without Project case | 3,453 | 3,366 | 3,413 | 3,328 |
| | With Project case | 3,311 | 3,311 | 3,311 | 3,311 |
| | Saving | 142 | 55 | 102 | 16 |
| <u>Year 2015:</u> | | | | | |
| VOC: | Without Project case (1) | 5,826 | 5,741 | 5,806 | 5,765 |
| | With Project case (2) | 5,741 | 5,741 | 5,741 | 5,741 |
| | Saving (3) = (1)-(2) | 85 | 0 | 65 | 24 |
| Time Cost: | Without Project case (4) | 608 | 537 | 552 | 490 |
| | With Project case (5) | 483 | 483 | 483 | 483 |
| | Saving (6) = (4)-(5) | 125 | 54 | 69 | 7 |
| Road User Benefit: | (7) = (3)-(9) | 210 | 54 | 134 | 31 |
| Bridge Maintenance: | Without Project case (8) | 10 | 10 | 10 | - |
| | With Project case (9) | - | - | - | - |
| | Saving (10) = (8)-(9) | 10 | 10 | 10 | - |
| <u>Total Benefit:</u> | Without Project case | 6,444 | 6,288 | 6,368 | 6,255 |
| | With Project case | 6,224 | 6,224 | 6,224 | 6,224 |
| | Saving | 220 | 64 | 144 | 31 |

Source: The Study Team

Table 8.7 Benefit Stream by Projects

(Unit: Million NRs.)

| Year | Projects | | | | | | | | | | | | | | | |
|-------|----------|-----|-----|-----|----------|-----|-----|-----|----------|-----|-----|-----|--------|-----|-----|-----|
| | Case 1 | | | | Case 1-1 | | | | Case 1-2 | | | | Case 2 | | | |
| | VOC | TC | BMS | T | VOC | TC | BMS | T | VOC | TC | BMS | T | VOC | TC | BMS | T |
| 1993 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1994 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1995 | 0 | 22 | 30 | 52 | 0 | 22 | 30 | 52 | 0 | 0 | 0 | 0 | 11 | 4 | 0 | 15 |
| 1996 | 0 | 23 | 0 | 23 | 0 | 23 | 0 | 23 | 0 | 0 | 30 | 30 | 11 | 4 | 0 | 15 |
| 1997 | 0 | 25 | 30 | 55 | 0 | 25 | 30 | 55 | 0 | 0 | 0 | 0 | 12 | 4 | 0 | 16 |
| 1998 | 47 | 70 | 0 | 117 | 0 | 27 | 0 | 27 | 36 | 40 | 30 | 106 | 13 | 4 | 0 | 17 |
| 1999 | 49 | 73 | 30 | 152 | 0 | 28 | 30 | 58 | 37 | 41 | 0 | 78 | 13 | 4 | 0 | 17 |
| 2000 | 52 | 77 | 0 | 129 | 0 | 30 | 0 | 30 | 39 | 43 | 30 | 112 | 14 | 4 | 0 | 18 |
| 2001 | 54 | 80 | 30 | 164 | 0 | 31 | 30 | 61 | 41 | 45 | 0 | 86 | 15 | 5 | 0 | 20 |
| 2002 | 56 | 83 | 0 | 139 | 0 | 33 | 0 | 33 | 43 | 47 | 30 | 120 | 15 | 5 | 0 | 20 |
| 2003 | 58 | 86 | 30 | 174 | 0 | 35 | 30 | 65 | 44 | 48 | 0 | 92 | 16 | 5 | 0 | 21 |
| 2004 | 61 | 90 | 0 | 151 | 0 | 36 | 0 | 36 | 46 | 50 | 30 | 126 | 17 | 5 | 0 | 22 |
| 2005 | 63 | 93 | 30 | 186 | 0 | 38 | 30 | 68 | 48 | 52 | 0 | 100 | 17 | 5 | 0 | 22 |
| 2006 | 65 | 96 | 0 | 161 | 0 | 39 | 0 | 39 | 49 | 53 | 30 | 132 | 18 | 5 | 0 | 23 |
| 2007 | 67 | 99 | 10 | 176 | 0 | 41 | 10 | 51 | 51 | 55 | 0 | 106 | 19 | 6 | 0 | 25 |
| 2008 | 69 | 102 | 0 | 171 | 0 | 43 | 0 | 43 | 53 | 57 | 10 | 120 | 19 | 6 | 0 | 25 |
| 2009 | 72 | 106 | 10 | 188 | 0 | 44 | 10 | 54 | 55 | 59 | 0 | 114 | 20 | 6 | 0 | 26 |
| 2010 | 74 | 109 | 0 | 183 | 0 | 46 | 0 | 46 | 56 | 60 | 10 | 126 | 21 | 6 | 0 | 27 |
| 2011 | 76 | 112 | 10 | 198 | 0 | 48 | 10 | 58 | 58 | 62 | 0 | 120 | 21 | 6 | 0 | 27 |
| 2012 | 78 | 115 | 0 | 193 | 0 | 49 | 0 | 49 | 60 | 64 | 10 | 134 | 22 | 6 | 0 | 28 |
| 2013 | 81 | 119 | 10 | 210 | 0 | 51 | 10 | 61 | 62 | 66 | 0 | 128 | 23 | 7 | 0 | 30 |
| 2014 | 83 | 122 | 0 | 205 | 0 | 52 | 0 | 52 | 63 | 67 | 10 | 140 | 23 | 7 | 0 | 30 |
| 2015 | 85 | 125 | 10 | 220 | 0 | 54 | 10 | 64 | 65 | 69 | 0 | 134 | 24 | 7 | 0 | 31 |
| 2016 | 87 | 128 | 0 | 215 | 0 | 56 | 0 | 56 | 67 | 71 | 10 | 148 | 25 | 7 | 0 | 32 |
| 2017 | 89 | 131 | 10 | 230 | 0 | 57 | 10 | 67 | 68 | 72 | 0 | 140 | 25 | 7 | 0 | 32 |
| 2018 | 92 | 135 | 0 | 227 | 0 | 59 | 0 | 59 | 70 | 74 | 10 | 154 | 26 | 7 | 0 | 33 |
| 2019 | 94 | 138 | 10 | 242 | 0 | 60 | 10 | 70 | 72 | 76 | 0 | 148 | 27 | 8 | 0 | 35 |
| 2020 | 74 | 78 | 0 | 152 | * | * | * | * | 74 | 78 | 10 | 162 | * | * | * | * |
| 2021 | 75 | 79 | 10 | 164 | * | * | * | * | 75 | 79 | 0 | 154 | * | * | * | * |
| 2022 | 77 | 81 | 0 | 158 | * | * | * | * | 77 | 81 | 10 | 168 | * | * | * | * |
| Total | 177 | 259 | 260 | 463 | 0 | 102 | 250 | 127 | 140 | 150 | 260 | 317 | 467 | 140 | 0 | 607 |

VOC: Vehicle Operation Cost Saving
 TC: Time Cost Saving
 BMS: Bridge Maintenance Cost Saving
 T: Total Cost Saving

8.5 Economic Evaluation

8.5.1 Premise

Premises for economic evaluation was set up as below :

- Implementation Schedule and Cost Disbursement

According to the implementation schedule described in Table 7-1, disbursements of cost by alternative are prepared as shown in Table 8.1.

- Project Life and Discount Rate

25 years of project life after opening of the projects has been assumed.

- Discount Rate

10% of discount rate throughout the project life has been applied.

8.5.2 Evaluation

IRR, B/C and NPV obtained through the above procedure are listed in Table 8.9.

IRR for Case 1, Case 1-1 and Case 2 are higher than 10% of opportunity cost of capital with the maximum of 19.5% in the Case 1-1 scenario. The B/C ratio is over 1.0 in Case 1, Case 1-1 and Case 2.

Table 8.8 Results of Economic Evaluation

| | IRR (%) | B/C * | N.P.V. * (in Million NRs.) |
|----------|---------|-------|-------------------------------|
| Case 1 | 11.5 | 1.13 | 136 |
| Case 1-1 | 19.5 | 1.95 | 189 |
| Case 1-2 | 9.7 | 0.91 | -63 |
| Case 2 | 18.8 | 1.99 | 85 |

8.6 Sensitivity Analysis

Sensitivity analysis was conducted to check the evaluating system and to check the viability of the projects in possible changes in cost and benefit. The result of sensitivity analysis is given in Table 8.9.

Table 8.9 (1) Result of Sensitivity Analysis (Case 1)

| IRR | | | | | | | (%) |
|----------|--|--------|--------|----------|----------|----------|-----|
| | | Cost | | | | | |
| Benefit | | 20% up | 10% up | Original | 10% down | 20% down | |
| 20% up | | 11.5 | 12.6 | 13.8 | 15.4 | 16.9 | |
| 10% up | | 10.5 | 11.5 | 12.7 | 13.9 | 15.7 | |
| Original | | 9.8 | 10.4 | 11.5 | 12.8 | 14.4 | |
| 10% down | | 9.4 | 9.7 | 10.3 | 11.5 | 12.9 | |
| 20% down | | 8.8 | 9.3 | 9.6 | 10.1 | 11.5 | |

| B/C | | | | | | | |
|----------|--|--------|--------|----------|----------|----------|--|
| | | Cost | | | | | |
| Benefit | | 20% up | 10% up | Original | 10% down | 20% down | |
| 20% up | | 1.13 | 1.24 | 1.36 | 1.51 | 1.70 | |
| 10% up | | 1.04 | 1.13 | 1.25 | 1.38 | 1.56 | |
| Original | | 0.94 | 1.03 | 1.13 | 1.26 | 1.42 | |
| 10% down | | 0.85 | 0.93 | 1.02 | 1.13 | 1.27 | |
| 20% down | | 0.75 | 0.82 | 0.90 | 1.01 | 1.13 | |

| NPV | | | | | | | (Million NRs.) |
|----------|--|--------|--------|----------|----------|----------|----------------|
| | | Cost | | | | | |
| Benefit | | 20% up | 10% up | Original | 10% down | 20% down | |
| 20% up | | 163 | 261 | 360 | 459 | 558 | |
| 10% up | | 50 | 149 | 248 | 347 | 445 | |
| Original | | -62 | 37 | 136 | 234 | 333 | |
| 10% down | | -174 | -76 | 23 | 122 | 221 | |
| 20% down | | -287 | -188 | -89 | 10 | 108 | |

Table 8.9 (2) Result of Sensitivity Analysis (Case 1-1)

| IRR | | | | | | | (%) |
|----------|--|--------|--------|----------|----------|----------|-----|
| | | Cost | | | | | |
| Benefit | | 20% up | 10% up | Original | 10% down | 20% down | |
| 20% up | | 19.5 | 20.8 | 22.7 | 24.7 | 27.0 | |
| 10% up | | 17.8 | 19.5 | 20.8 | 22.8 | 25.0 | |
| Original | | 16.5 | 17.7 | 19.5 | 20.9 | 23.6 | |
| 10% down | | 14.8 | 15.9 | 17.6 | 19.5 | 21.5 | |
| 20% down | | 13.3 | 14.5 | 15.7 | 17.5 | 19.5 | |

| B/C | | | | | | | |
|----------|--|--------|--------|----------|----------|----------|--|
| | | Cost | | | | | |
| Benefit | | 20% up | 10% up | Original | 10% down | 20% down | |
| 20% up | | 1.95 | 2.12 | 2.34 | 2.60 | 2.92 | |
| 10% up | | 1.78 | 1.95 | 2.14 | 2.38 | 2.68 | |
| Original | | 1.62 | 1.77 | 1.95 | 2.16 | 2.43 | |
| 10% down | | 1.46 | 1.59 | 1.75 | 1.95 | 2.19 | |
| 20% down | | 1.30 | 1.41 | 1.56 | 1.73 | 1.95 | |

| NPV | | | | | | | (Million NRs.) |
|----------|--|--------|--------|----------|----------|----------|----------------|
| | | Cost | | | | | |
| Benefit | | 20% up | 10% up | Original | 10% down | 20% down | |
| 20% up | | 227 | 246 | 266 | 286 | 306 | |
| 10% up | | 188 | 208 | 228 | 247 | 267 | |
| Original | | 149 | 169 | 189 | 209 | 229 | |
| 10% down | | 110 | 130 | 150 | 170 | 190 | |
| 20% down | | 72 | 92 | 111 | 131 | 151 | |

Table 8.9 (3) Result of Sensitivity Analysis (Case 1-2)

| IRR | | | | | | | (%) |
|----------|--|--------|--------|----------|----------|----------|-----|
| | | Cost | | | | | |
| Benefit | | 20% up | 10% up | Original | 10% down | 20% down | |
| 20% up | | 9.7 | 10.0 | 11.2 | 12.5 | 13.8 | |
| 10% up | | 9.4 | 9.7 | 10.1 | 11.4 | 12.8 | |
| Original | | 9.0 | 9.3 | 9.7 | 10.3 | 11.6 | |
| 10% down | | 8.4 | 8.9 | 9.3 | 9.7 | 10.4 | |
| 20% down | | 7.8 | 8.3 | 8.8 | 9.2 | 9.7 | |

| B/C | | | | | | | |
|----------|--|--------|--------|----------|----------|----------|--|
| | | Cost | | | | | |
| Benefit | | 20% up | 10% up | Original | 10% down | 20% down | |
| 20% up | | 0.91 | 1.00 | 1.10 | 1.22 | 1.37 | |
| 10% up | | 0.84 | 0.91 | 1.01 | 1.12 | 1.26 | |
| Original | | 0.76 | 0.83 | 0.91 | 1.02 | 1.14 | |
| 10% down | | 0.68 | 0.75 | 0.82 | 0.91 | 1.03 | |
| 20% down | | 0.61 | 0.66 | 0.73 | 0.81 | 0.91 | |

| NPV | | | | | | | (Million NRs.) |
|----------|--|--------|--------|----------|----------|----------|----------------|
| | | Cost | | | | | |
| Benefit | | 20% up | 10% up | Original | 10% down | 20% down | |
| 20% up | | -76 | 3 | 82 | 161 | 240 | |
| 10% up | | -148 | -70 | 9 | 88 | 167 | |
| Original | | -221 | -142 | -63 | 16 | 95 | |
| 10% down | | -294 | -215 | -136 | -57 | 22 | |
| 20% down | | -366 | -287 | -208 | -130 | -51 | |

Table 8.9 (4) Result of Sensitivity Analysis (Case 2)

| IRR | | | | | | | (%) |
|----------|--|--------|--------|----------|----------|----------|-----|
| | | Cost | | | | | |
| Benefit | | 20% up | 10% up | Original | 10% down | 20% down | |
| 20% up | | 18.8 | 20.5 | 21.8 | 23.8 | 25.9 | |
| 10% up | | 17.6 | 18.8 | 20.6 | 22.0 | 24.6 | |
| Original | | 16.4 | 17.6 | 18.8 | 20.7 | 22.7 | |
| 10% down | | 14.7 | 15.8 | 17.5 | 18.8 | 20.8 | |
| 20% down | | 13.4 | 14.4 | 15.6 | 17.0 | 18.8 | |

| B/C | | | | | | | |
|----------|--|--------|--------|----------|----------|----------|--|
| | | Cost | | | | | |
| Benefit | | 20% up | 10% up | Original | 10% down | 20% down | |
| 20% up | | 1.99 | 2.17 | 2.39 | 2.66 | 2.99 | |
| 10% up | | 1.83 | 1.99 | 2.19 | 2.44 | 2.74 | |
| Original | | 1.66 | 1.81 | 1.99 | 2.21 | 2.49 | |
| 10% down | | 1.49 | 1.63 | 1.79 | 1.99 | 2.24 | |
| 20% down | | 1.33 | 1.45 | 1.59 | 1.77 | 1.99 | |

| NPV | | | | | | | (Million NRs.) |
|----------|--|--------|--------|----------|----------|----------|----------------|
| | | Cost | | | | | |
| Benefit | | 20% up | 10% up | Original | 10% down | 20% down | |
| 20% up | | 102 | 110 | 119 | 127 | 135 | |
| 10% up | | 85 | 93 | 102 | 110 | 119 | |
| Original | | 68 | 76 | 85 | 93 | 102 | |
| 10% down | | 51 | 59 | 68 | 76 | 85 | |
| 20% down | | 34 | 42 | 51 | 59 | 68 | |

8.7 Financial Analysis/Considerations

8.7.1 Objective

The required amount of implementation cost for all high priority projects analyzed in the economic evaluation is estimated to be NRs. 2,298 million as shown in Table 7-1. It is recommended that the implementation of these projects should be carried out by means of grants and external borrowing as shown in article 9.2.3 of the Master Plan Report of this study. The main purpose of this financial analysis is to check the estimated project cost if it is within the scope of foreign aid in the Eighth Plan and scheduled development expenditure for the transport sector in the Eight Plan.

8.7.2 Analysis of Past Investment for Transport Sector

(1) National Expenditure and Sources of Finance

The overall budgetary situation of His Majesty's Government of Nepal (HMG) shows an excess of expenditures over revenue. In the fiscal year 1990/91, the revenue of HMG was NRs 10,698 million whereas total expenditures were NRs 24,479 million. The internal revenue of HMG is able to cater the country's total general expenditures plus a portion of development expenditure. The remaining development expenditures have been covered by foreign grants, internal and foreign loans. The reliance on external aid sources is steadily increasing. The total expenditure of the governments in the past 6th and 7th Plans is given in the Table 8.10.

(2) Sector Expenditure in Development Expenditure

According to the statistics of HMG for the past ten years, the development expenditure for roads and bridges is on the increase every year so as to achieve development projects for roads and bridges (Refer Table 8.11).

From the recognition of the importance of transportation and communication in the socio-economic development of the country, special attention has been being given to the development of these sectors since the first Five Year Plan. Various efforts have been made in construction of roads and bridges and in the improvement projects of accessibility to isolated small villages in Nepal.

Average shares of allocation to transportation, communication and road bridge sectors in total development expenditures were 14% and 10% respectively during the 7th plan period while maximum of those shares during the same period were 18% and 12% respectively.

(3) Foreign Aid for Transport Sector

The statistics data on foreign loan and grant disbursement for roads and bridges for the past ten years show that grant aid is larger than bilateral loan aid as

shown in Table 8.12. During the 7th plan period, the total amount of foreign aid disbursement was NRs 4,137 million, almost one half of which was for transport and communication sectors. Average compositions of grants and loans were 43% and 57% respectively.

Table 8.10 Government Expenditure and Sources of Finance (Million Rs) *

| | 6th 5-year Plan Period | | | | | 7th 5-year Plan Period | | | | | Total | | |
|-------------------|------------------------|-------|-------|-------|-------|------------------------|--------|--------|--------|--------|--------|--------|---------|
| | 81/82 | 82/83 | 83/84 | 84/85 | 85/86 | Total | 86/87 | 87/88 | 88/89 | 89/90 | | 90/91 | 91/92 |
| Total Expenditure | - | 6,979 | 7,437 | 8,395 | 9,791 | 32,602 | 11,513 | 14,105 | 18,005 | 19,669 | 24,479 | 26,641 | 114,412 |
| Revenue | - | 2,842 | 3,409 | 3,917 | 4,645 | 14,813 | 5,975 | 7,350 | 7,777 | 9,288 | 10,698 | 12,557 | 53,645 |
| Deficit ** | - | 4,137 | 4,028 | 4,478 | 5,146 | 17,789 | 5,538 | 6,755 | 10,228 | 10,381 | 13,781 | 14,084 | 60,767 |

Source : Statistical Pocket Book 1988, 1990 and 1992, Central Bureau of Statistics, Nepal

Table 8.11 Government Development Expenditure for Roads and Bridges *

| | 6th 5-year Plan Period | | | | | 7th 5-year Plan Period | | | | | Total | |
|--|------------------------|-------|-------|-------|-------|------------------------|-------|-------|--------|--------|--------|--------|
| | 81/82 | 82/83 | 83/84 | 84/85 | 85/86 | Total | 86/87 | 87/88 | 88/89 | 89/90 | | 90/91 |
| Total Development Expenditure (Million Rs) | 3,727 | 4,982 | 5,164 | 5,489 | 6,213 | 25,575 | 7,378 | 9,428 | 12,329 | 12,997 | 16,551 | 84,258 |
| Transportation Communication (Million Rs) | 793 | 876 | 844 | 1,013 | 807 | 4,333 | 1,126 | 1,734 | 2,232 | 1,718 | 1,667 | 12,810 |
| Road & Bridge (Million Rs) | 21 | 18 | 16 | 18 | 13 | 17 | 15 | 18 | 18 | 18 | 13 | 14 |
| | - | - | 657 | 573 | 616 | 1,846 | 835 | 1,071 | 1,506 | 1,172 | 1,511 | 7,941 |
| | | | 13 | 10 | 10 | - | 11 | 11 | 12 | 9 | 9 | 10 |

Source : Statistical Pocket Book 1988, 1990 and 1992, Central Bureau of Statistics, Nepal

Table 8.12 Foreign Aid *

| | 6th 5-year Plan Period | | | | | 7th 5-year Plan Period | | | | | Total | |
|---|------------------------|-------|-------|-------|-------|------------------------|-------|-------|-------|-------|-------|-------------|
| | 81/82 | 82/83 | 83/84 | 84/85 | 85/86 | Total | 86/87 | 87/88 | 88/89 | 89/90 | | 90/91 |
| Foreign Aid Disbursement for Transportation | 415 | 265 | 301 | 556 | 343 | 1,880 (100) | 405 | 607 | 1,018 | 750 | 1,357 | 4,173 (100) |
| - Grant | 308 | 171 | 196 | 156 | 227 | 1,058 (56) | 145 | 257 | 334 | 371 | 687 | 1,794 (43) |
| - Loan | 107 | 94 | 105 | 400 | 116 | 822 (44) | 260 | 350 | 684 | 379 | 670 | 2,343 (57) |

* In Million NRs at Current

Source : Economic Survey 1989 and 1992, Ministry of Finance, Nepal

** Foreign Grants, Foreign Loan and Internal Loans

8.7.3 Analysis of Eighth Plan

The total gross fixed investment during the Eighth Plan period is estimated at NRs 170,332 million as shown in Table 8.13. This is 65% of increase of that of Seventh Plan.

Sector investment which includes both private and government investments will be NRs. 113,479 million of which the investment for transport and communication sectors will be NRs. 20,030 million which accounts for 17.7 percent of the total development expenditure.

An amount of NRs 95,977 million or 56.3 percent will be financed through national savings, the remaining NRs 74,355 million or 43.7 percent is required to be financed by foreign aid, of which NRs 19,761 million will be by grant and NRs 54,594 million by loan.

Table 8.13 Investment and Financing Sources of Eighth Plan

| | Seventh Plan (1986 '90) | | Eighth Plan (1993-'97) | |
|---|----------------------------|----------|---------------------------|----------|
| | Amount * | Share(%) | Amount * | Share(%) |
| <u>Sector Investment Requirement **</u> | | | | |
| Total Gross Fixed Investment | 103,014 | 100.0 | 170,332 | 100.0 |
| Transport & Communication | 15,881 | 15.4 | 26,119 | 15.4 |
| <u>Sector allocation of Development Expenditure</u> | | | | |
| Total Development expenditure | 74,174 | 100.0 | 113,479 | 100.0 |
| Transport & Communication | 11,657 | 15.7 | 20,030 | 17.7 |
| Transport | - | - | 13,567 | 11.95 |
| <u>Source of finance</u> | | | | |
| Total Gross Fixed Investment | | | 170,332 | 100.0 |
| National Saving | | | 95,977 | 56.3 |
| Foreign Aid | | | 74,355 | 43.7 |
| - Grant | | | 19,761 | 11.6 |
| - Loan | | | 54,954 | 32.1 |

* in million NRs at 1991/92 prices

** Sector investment includes private and government investment

Total cost required for the implementation of the proposed high priority projects is estimated at NRs 2,298 million which is only 3.1% of the total proposed foreign aid in the Eighth Plan. Furthermore, an assumed share of the project cost required in the transport and communication sectors of the Eighth Plan is 11.5% as shown below:

$$S = \frac{PC}{TC} \times 100$$

Where

S : Assumed Share of the Project Cost (%)

PC : Project Cost = 2,298 million NRs

TC : Proposed Development Expenditure on Transport and Communication Sectors
= 20,030 million NRs.

$$S = \frac{2,298 \text{ million NRs}}{20,030 \text{ million NRs}} \times 100$$

$$= 11.5\%$$

8.7.4 Conclusion and Recommendation

Although the assumed share of 11.5% for the projects might be a slightly higher portion in the transportation development expenditure, it could be recommended that the arrangement of the project implementation should be given a high priority taking the role of Kathmandu Valley in the national economy into account.

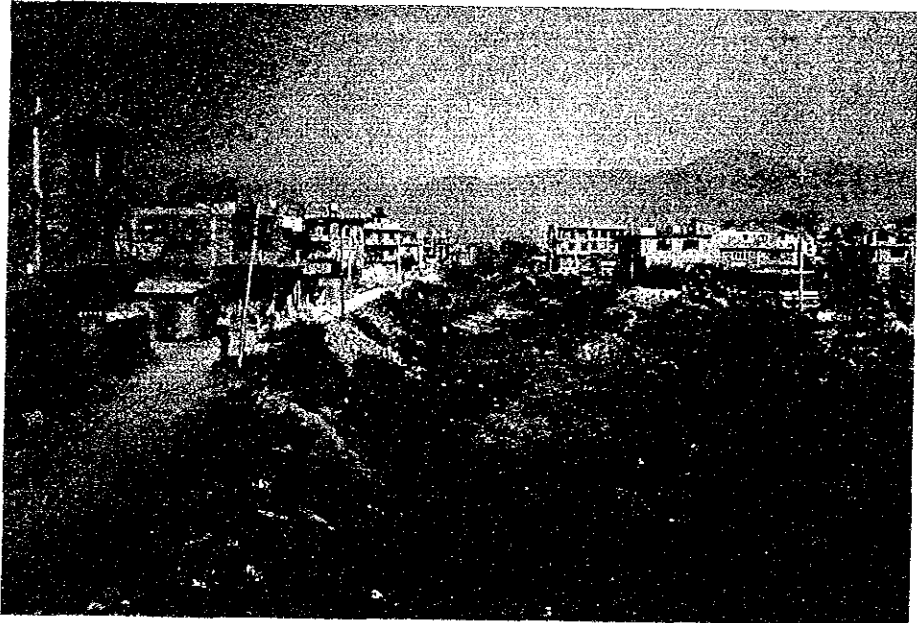
In addition, the required project cost for Package C and other additional works for Package A-1 mentioned in Table 7.1 is estimated at NRs 246 million which is only 1.2% of the development expenditure on transport and communication sectors of the Eighth Plan. Furthermore, it could be assumed that the Improvement Project for intersections and other additional works are economically feasible ; in reference to similar projects in other cities in the world.

On the other hand, the Eighth Plan sets forth the concept of a nation-wide highway network development, along with the policy of feeder and rural road development which was proposed in the previous fifth year plan. However, these road development programs would require a great deal of coordination in terms of scope of plans, reorganization of implementing agencies and implementation schedule. In this context, road development in the Valley should be proceeded in the balance between nationwide and region-oriented scopes of development scheme.

Regarding the individual proposed projects in this study, Case 1 is rather oriented in nation-wide scope of road development while Case 2 rather regional oriented.

CHAPTER 9

ENVIRONMENTAL CONSIDERATION



CHAPTER 9 ENVIRONMENTAL CONSIDERATIONS

9.1 Present Condition of the Bagmati Corridor

The tradition of using the flood-plain areas as the agricultural land is prevalent in Kathmandu Valley. Rapid growth of population and lack of zoning has changed almost all of flood plain into urban area and this trend is continuing at accelerated rate. The settlement in these flood plain has very poor infrastructure facility and living condition there is very poor.

The Bagmati corridor is not homogeneous in terms of land use and activities, however, the area is predominantly used for agricultural purposes. There are presently three squatter sites with about 50 houses within the corridor. Within these squatter areas there exists no public service and standards of the housings is extremely low. The people living in these areas use the river bed as the place of living, washing place and toilet. The river is also used for dumping place of solid waste and discharging urban sewer from surrounding area.

The Bagmati river is a tributary of the Ganges river and is a holy river in Hindu beliefs. Along the river, there exist many temples and places of historical and religious importance. In the vicinity of proposed Bagmati transport corridor, Shankhamul temple, Tripureswor temple complex, Pachli and Ram ghats are important religious places.

People collect sand from the Bagmati river for construction of building. Large amount of sand is taken from the river annually which is lowering the water level of the river. The temples are losing their original approach to the water and religious activities are being hampered.

The sources of air pollution are dust, vehicle emissions and industrial emissions. According to the survey made by the Norwegian Institute of Technology in August, 1991, the level of dust in the air exceeds acceptable level and the lead content in air is at critical level.

9.2 Effect on Economic and Social Activities

Urban sprawl has lead transportation system to very inefficient one and charging high transportation cost to the users. Poor provision of road is one of the causes of the uncontrolled urban development. Due to uncontrolled urban development, the Valley is poorly served with infrastructure. It is expected that better land-use pattern will be realized with the road development.

The rapid population growth, as high as 6 % per annum in Kathmandu, has brought about a great pressure in the housing market in the city. The opening up of areas along the Bagmati Transport Corridor will relieve these tension in housing market.

The project road will improve the accessibility in the area and encourage the economic and social activities and will enhance land value in the areas, while construction or road will accompany the issues of relocation of housing. To minimize these negative effects, the proposed alignment of South Link of Inner Ring road is proposed to pass in the areas nearby the river bank, where the lands are mostly owned by government.

Short-term impacts brought about by the project

The alignment of the proposed roads is proposed along the river bank of the Bagmati river so as to minimize the land acquisition cost, however, the following impacts are expected in a short-term:

- (1) About 110 houses including squatters have to be demolished by the construction of roads and about 92,000 m² (or 9.2 hectare) of the agricultural land will be converted into road. The owner of land will lose their income temporarily.
- (2) The road will hinder religious activity centered around the river.

Long-term impacts brought about by the project

- (1) The project road will open up a new area and will promote new type of socio-economic activities there. The resident will receive some benefit by increased land value.
- (2) The project road will provide access to areas that have poor access or no access at present, which will promote systematized urban development in a long-term.

9.3 Traffic Impacts

- (1) Improvement of transportation-poor

The proposed road will give improved access to the areas which currently have poor road access. The improvement of accessibility to the areas will relieve the transportation-poor in the areas. With improved access, many inhabitants will be able to satisfy their minimum level of transportation need.

(2) **Improvement of traffic flow**

The proposed South Link of Inner Ring Road will provide a new east-west connection in the northern part of Lalitpur, which will reduce the traffic congestion near the existing Bagmati Bridge. Relief of traffic congestion on the Bagmati Bridge at Thapathali is urgent since the bridge is now bottleneck of urban traffic, causing great amount of delays and accidents.

(3) **Formation of urban road network in Kathmandu**

South Link of Inner Ring Road will be a major arterial road forming a basic frame of urban road network in Kathmandu in a long-term. The construction of South Link is epoch-making as the initial step to build up the urban road network in the Valley.

9.4 Improvement on Environment of Bagmati Corridor

The positive impacts on the river environment is described as below:

- (1) The proposed road will prevent further pollution of the river due to clearance of sub-standard housings along the river.
- (2) Open space between the road and river bank could be used for public facilities, such as play ground, park, pedestrian and bicycle road, green belt, open market and so on.

9.5 Negative Impacts on Natural Environment

Air quality

The vehicle exhaust gas is one of the major causes of air pollution. Provision of new road network as well as the improvement of major intersections proposed in this study will streamline the traffic flow in the city greatly and improve the driving condition of road to the level that reduces amount of exhaust gas from the vehicles.

For the more controle of air pollution in the Valley, it is inevitable to introduce air monitoring system based on scientific study. Introduction of car inspection system is another measure to be introduced to relief the issue.

Noise and other environmental problems

Noise will cause sleeping disturbance, build-up of stress and poor concentration for the residents nearby the road. The proposed route, however, is located far from the residential area, so that noise will not be a major issue even after the opening of the road.

CHAPTER 10

CONCLUSION AND RECOMMENDATIONS



CHAPTER 10 CONCLUSION AND RECOMMENDATIONS

The following are the conclusion and recommendations related to the project.

10.1 Conclusion

The feasibility study proved that project roads, both of Package A and B are technically and economically feasible with a high economic internal rate of return of 11.5% and 18.8% respectively.

Therefore, the projects should be realized within the earliest possible time, in the following priority order.

| <u>Priority</u> | <u>Proposed Roads</u> |
|-----------------|--|
| (1) | Construction of New Bagmati Bridge (2 lanes) including; - Thapathali intersection with pedestrian bridge, - Improvement of existing Bagmati Bridge for scoring, - Removal of existing old truss bridge, and - River improvement against lowering river bed |
| (2) | Construction of New Bus Terminal Access at Balaju |
| (3) | Improvement of Intersections at Mitighar, Tripureswar and Koteswor |
| (4) | Construction of Western Section of South Link of Inner Ring Road including, - Snapper Access - Bagmati Bridge No.1 at Sanepa - Riverside Protection |
| (5) | Construction of Eastern Section of South Link of Inner Ring Road including, - Koteswor Access and Patan Access - Bagmati No.3 and No.4 Bridges |

Table 10.1 shows the summary of the project features for the above roads.

Table 10.1: Summary of Project Feature

| Project | Major Work Items | Lane Nos. | Design Speed (Km/hr) | Length (m) | Carriageway (m) | Sidewalk (m) | Right-of-way (m) | Remarks |
|---------|--|-----------|----------------------|------------|-----------------|-------------------|------------------|--|
| 1 | New Bagmati Bridge (No.2 Bagmati Bridge) | 2 | 60 | 140 m | 10 m | 3.0m(one side) | 50 m | |
| | Main Bridge | | | | | | | |
| | Intersection with Pedestrian | | | | | | | |
| | Protection of existing bridge | | | | | | | |
| | Removal of old truss bridge | | | | | | | |
| | Protection against river bed | | | | | | | |
| 2 | South Inner Ring Road | | | | | | | |
| | (i) First stage (2 lanes); | 2 | 60 | 3,750 m | 10 m | 3.0m(one side) | 50m (min. 25m) | Right-of-way shall be acquired for 4 lane roads at this first stage. |
| | Project Road | 2 | | 145 m | 8 m | 2.5m(both side) | | |
| | No. 1 Bagmati Bridge | 2 | | 120 m | 8 m | 2.5m(both side) | | |
| | No. 3 Bagmati Bridge | 2 | | | | | | |
| | Protection of riverside bank | | | | | | | Protection of river bank of Bagmati. |
| | (ii) Second stage; | (total 4) | 60 | | 2 x 8 m | 3.0m(both side) | - | with median slip (3.0m) |
| | Project Road | | | | w/median (3m) | | | |
| | (Widening to 4 lanes) | | | | | | | |
| | No. 1 Bagmati Bridge | 4 | | 145 m | 8 m | 2.5m(one side) | | |
| | No. 3 Bagmati Bridge | 4 | | 120 m | 8 m | 2.5m(one side) | | |
| 3 | Access Roads | | | | | | | |
| | (i) Sanepa Access | 2 | 60 | 510 m | 10 m | 3.0m(both side) | 30m (min. 20m) | |
| | Project Road | | | | | | | |
| | (ii) Koteswar Access | 2 | 60 | 2,180 m | 10 m | 3.0m(both side) | 30m (min. 20m) | |
| | Project Road | | | | | | | |
| | No. 4 Bagmati Bridge | 2 | | 60 m | 8 m | 2.5m(both side) | | |
| | Project Road | | | | | | | |
| | (iii) Patan Core Access | | 40 | 220 m | 8 m | 2.5 m (both side) | 13 m | |
| | Project Road | | | | | | | |
| | (iv) New Bus terminal Access | 2 | 40 | 1,865 m | 10 m | 3.0 m (both side) | 30 m | |
| | Project Road | | | | | | | |
| 4 | Improvement of Intersections | | | | | | | |
| | Mitighar Intersection | 4 | | | | | | Signal with minor improvement |
| | Tripureswar Intersection | 4 | | | | | | Signal with minor improvement |
| | Koteswar Intersection | 4 | | | | | | Improvement of shape of intersection |

The following are the significance and benefits expected from the project:

(1) Removal of Traffic Bottleneck between Kathmandu and Patan

Proposed New Bagmati Bridge will not only facilitate the anticipated traffic demand in between Kathmandu and Lalitpur but also release the traffic congestion and solve the bottleneck of the traffic movement in the areas of Thapathali which will improve economic and social activities in both cities.

(2) Securing the Alternative Route between Kathmandu and Lalitpur

So far, there is the only existing Bagmati Bridge at Thapathali connecting Kathmandu and Lalitpur inside the Ring Road. Since lowering of the Bagmati River is still progressing, securing of new reliable alternative transport routes between Kathmandu and Lalitpur is essential not only for economic activities but also for the daily life of the people in the cities.

(3) Build-up of the Basic Frame of Urban Road Network inside Kathmandu City

South Link of Inner Ring Road is a part of the Inner Ring Road and forms a basic frame of urban road network in Kathmandu city in the long-term. The construction of South Link is significant as the first step to build up the proposed urban road network in Kathmandu Valley.

(4) Improvement of Accessibility and Enhancement of Regional Development

Proposed South Link of the Inner Ring Road including Sanepa and Koteswor Access will improve the accessibility from the existing roads to the inner low density areas, which will enhance the development of these inner areas along the corridor.

(5) Improvement of Environment along Bagmati River

Proposed South Link as well as Koteswor access would improve the environment of Bagmati river-side through the provision of slope protection of river bank. The open space between the proposed road and the river could be used for public facilities, such as, riverside park, pedestrian and bicycle road, green belt, play ground and so on.

10.2 Recommendation

In order to materialize the projects, the Study Team recommends DOR to take the following actions:

(1) Urgent Implementation of New Bagmati Bridge

It is strongly recommended for DOR to implement the construction of New Bagmati Bridge within the earliest possible time.

The traffic condition of existing Bagmati Bridge at Thapathali is getting worse due to rapid increase of traffic between Kathmandu and Lalitpur cities. Moreover, this bridge is in a serious and dangerous situations and requires immediate protection and repair work on the bridge foundation against the lowering of river bed. (It is noted that the traffic was suspended from August 1991 to March 1992 due to the collapse of foundation of the existing Bagmati Bridge.) At least, emergency protection work on pier No.5 (nearest to Lalitpur side) as well as reshaping of gabion checkdam located 20 m downstream should be conducted before coming rainy season which will last from June to September, 1993 this year.

Since the existing Bagmati Bridge is the only vehicular bridge connecting Kathmandu and Lalitpur inside the Ring Road, construction of New Bagmati Bridge is essential not only for facilitating the traffic demands but also for securing a alternative bridge as a detour connecting Kathmandu with Lalitpur.

(2) Securing Bus Route from New Bus Terminal at Balaju

Construction of a new bus terminal project is progressing at Balaju, and is expected to be completed in early March, 1993. Since the new bus terminal is located at Balaju where accessibility from the central area of Kathmandu city is very limited, the provision of suitable access is essential for smooth operation of the New Bus Terminal.

It is, therefore, recommended to construct the New Bus Terminal Access as soon as possible to secure proper and reliable bus route for bus operation, since the bus services is the only means of transportation in Kathmandu.

In the meantime, the Study team also recommends to improve the roads nearby city center which might be utilized as bus routes if proposed New Bus Terminal Access is materialized, especially on the following routes:

- (i) Trisuli Road from Royal Palace to Paknajor (reconstruction of pavement and drainage as well as widening of certain section might be necessary)
- (ii) Feeder road starting from Kanti Path at Ambassador Hotel up to the New Access through U.K. Embassy, Indian Embassy and Samakhusi Road. (This road is recommended to be utilized for bus route employing one-way system from Kanti path up to Samakhusi Road. Pavement and widening of the road from the entrance of Indian Embassy to Samakhusi road is recommended).

Improvement of the above roads is essential for maintaining the smooth operation of bus services between city center and New Bus Terminal.

- (3) Securing of 4 Lane Right-of-way Width for South Link of Inner Ring Road

Staged construction is recommended for the implementation of the Inner Ring Road. Widening of the Inner Ring Road from 2-lane to 4-lane should be done in future when traffic demand exceeds the traffic capacity of 2-lane road, however, right-of way width should be secured for 4-lane at this moment. Additional land acquisition in future might be very difficult because of expected increase of land price.

- (4) Allocation of Local Budget for Acquiring Land/House

It is recommended to allocate the necessary amount of local budget for acquiring the lands and houses which might be necessary for implementation of the project.

Land and house acquisition should be conducted in accordance with the project implementation schedule as follows:

| <u>Year</u> | <u>Schedule of Land/House Acquisition</u> |
|-----------------|--|
| 1st year (1993) | Acquiring lands and houses located in the vicinity of New Bagmati Bridge including the intersections at Thapathali and Patan side |
| 2nd year (1994) | Within the ROW along Western section of South Link of the Inner Ring Road from the beginning point up to the proposed New Bagmati Bridge including Sanepa Access |
| 3rd year (1995) | Within the ROW along Eastern section of South Link of the Inner Ring Road from proposed New Bagmati Bridge up to the end on Arniko Highway including Koteswor Access and Patan Core Access |

(5) Improvement Traffic Management at Intersection

In order to reduce traffic accidents and to secure a smooth traffic movement on the arterial city roads, it is recommended to improve traffic management at the following intersections:

| <u>Location of Intersections</u> | <u>Improvement of Intersections and Traffic Management</u> |
|---|--|
| - Intersection at Maitighar (Beginning of Arniko H'way) | Installation of traffic signals with minor improvement |
| - Tripureswar near National Stadium | Installation of traffic signals with minor improvement |
| - Intersection at Koteswor (Arniko H'way with Ring Road) | Improvement of intersection shape to the roundabout intersection |

APPENDIX



APPENDICES

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- Appendix 4.5.1 Topographic Survey Data

CHAPTER 5 PRELIMINARY DESIGN

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CHAPTER 6 COST ESTIMATES

- Appendix 6.5.1 Detailed Work Quantities
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Appendix 4.2.1 Description of Detailed Geological Conditions

(1) General

A comparative study of the borehole logs shows that the soil in the bridge sites at Koteswor and Kuleswor show similar sequences of deposition and the predominating soil type in these sites is very soft to firm lacustrine deposit of high capacity clayey silt capped with about 1.5 m to 6.5 m thick coarse to medium sand of medium relative density. The clay layer below the sand at the top extends right down up to investigated depth of 40 m and contain seams of silty fine sands at places. On the other hand the soils at Thapathali and Chakupat are of two types and consist mainly of dark grey soft to stiff clayey silt of high plasticity and coarse to medium sand of medium to dense compactness deposited in alternate layers.

A detail description of soil encountered in bore holes is presented below. The cross sections of bridge sites showing subsoil strata presented in Fig. A4.2.1 to Fig. A4.2.4 provide better picture of stratification. To get the general idea of soil of Kathmandu valley, Fig. A 4.2.5 is presented.

Kuleswor

In this site the soil at the top is 1.5 m (right bank) to 3.00 m (left bank) thick deposit of light grey fine to coarse loose sand and fine gravel. Underlying this layer of sand and gravel, the soil upto the investigated depth of 40 m is a deposit of highly plasticity clayey silt of dark grey colour. (Fig. A4.2.1).

Thapathali

The sub-surface soil at this site consists of alternate layers of clayey silt and sand of varying density and thickness. Six different layers are seen. Thickness of individual layers varies from 2 m to 12 m.

At the top most part both the bore holes show the presence of yellow brown fine to medium dense fine to coarse sand. The right bank borehole shows presence of some gravel in the sand. The thickness is 2.5 - 5.0 m.

Further down, the sand is underlain by a 9-18m thickness of dark grey firm to stiff clayey silt of high plasticity. The thickness in the right bank is twice as much as in the left bank.

The layer of clayey silt is underlain further by 2-8.5m thickness of dark grey medium to coarse sand. This layer is also relatively thick, about 2 m in the left bank while it is about 8.5 m in the right bank. Underlying the sand is again the dark grey to light black stiff to very stiff clayey silt of high plasticity. This layer is about 3 m thick in the right bank while it is about 7 m in the left bank.

The clay layer is again underlain by light yellow brown to dark grey medium dense to dense fine to coarse sand which extends down in the right bank from EL. 1251 to EL.

1242 (depth of exploration) whereas in the left bank this sand layer of about 6 m thickness is underlain by more than 17 m thickness of dark grey firm to stiff clayey silt of high plasticity. This clayey silty layer was not encountered in the right bank within the drilled depth.

The soil profile in Fig. A4.2.2 has been prepared by interpolating the logs of the two boreholes located much apart. Given the variation in the thickness of individual of the alternating strata it can not be excluded that some of the layers are in the form of lenses.

Chakupat

In this site also the soil conditions between the left and right bank of the river differ in terms of depositional sequence. (Fig. A4.2.3). In left bank the soil at the top 2.0 m is a mixture of very loose sand and gravel. Below this layer up to a depth of 12 m the soil is a grey soft to firm highly plasticity clayey silt. Following this layer, a layer of light grey coarse to medium sand of medium to dense compactness extends to a depth of 20 m. Up to the investigated depth of 40 m the layer below 20 m is again a layer of dark grey soft to firm highly plastic clayey silt.

The soil at the right bank, on the other hand, right from the surface up to the depth of about 38 m is dark grey soft to firm, highly plastic clayey silt followed by a layer of dark grey medium to coarse sand. Explored thickness of this sand layer is 2 m which obviously may continue beyond the drilled depth.

Koteswor

The soil at this site on both banks of the river are quite similar both in terms of depth and extent (Fig. A4.2.4). The soil encountered at top 6.5 m to 7.0 m in both of the bore holes is light grey medium to fine sand of loose to medium compactness. The soil underlying the to sand layer in both of the bore holes is dark grey soft to firm high plasticity clayey silt.

Table A.4.2.1 Test Result Summary Sheet of Bridge Sites

Bridge No. 1

Location : Kuleshwor

| Sam- ple Type | B. H. No. | Depth m | Percentage | | | | | | NMC % | Bulk Density gm/cm ³ | Specific Gravity gm/cm ³ | SPT Value N | Qu kg/cm ² | Consolidation mv cm ² /kg | Remarks | |
|---------------------|--------------|------------|------------|------|------|------|-------|-------|----------|---------------------------------------|---|-------------------|--------------------------|--|---------|------|
| | | | Gravel | Sand | Silt | Clay | LL % | PL % | | | | | | | | PI % |
| DS | Right | 8 | - | 4 | 84 | 12 | 96.75 | 61.18 | 35.57 | 86.03 | - | 2.52 | 5 | | | |
| DS | Bank | 12 | - | 3 | 82.5 | 14.5 | 95.20 | 63.39 | 31.81 | 86.20 | - | 2.63 | 5 | | | |
| UD | (1) | 7 | - | 3 | 91 | 6 | 85.30 | 59.78 | 25.52 | 86.90 | - | 2.46 | - | | | |
| UD | | 13 | - | 2.5 | 93.5 | 4 | 85.20 | 43.79 | 41.41 | 79.43 | - | 2.43 | - | | | |
| DS | Left | 4 | - | 2 | 75 | 23 | 83.40 | 45.35 | 38.05 | 72.00 | - | 2.49 | 5 | | | |
| DS | Bank | 14 | - | 5 | 76 | 19 | 70.40 | 47.22 | 23.18 | 70.07 | - | 2.53 | 5 | | | |
| UD | (2) | 5 | - | 5 | 72 | 23 | 82.70 | 55.19 | 27.51 | 63.19 | 1.50 | 2.43 | - | 0.55 | | |
| UD | | 9 | - | 7 | 79 | 24 | 83.75 | 43.08 | 40.67 | 78.13 | 1.83 | 2.59 | - | 0.65 | 0.0251 | |

Table A.4.2.2 Test Result Summary Sheet of Bridge Sites

Bridge No. 2

Location : Thapathali

| Sam- ple Type | B. H. No. | Depth m | Percentage | | | | | | NMC % | Bulk Density gm/cm ³ | Specific Gravity gm/cm ³ | SPT Value N | Qu kg/cm ² | Consolidation mv cm ² /kg | Remarks |
|---------------------|--------------|------------|------------|------|------|------|-------|-------|----------|---------------------------------------|---|-------------------|--------------------------|--|---------|
| | | | Gravel | Sand | Silt | Clay | LL % | PL % | | | | | | | |
| DS | Right | 4 | - | 6 | 78.0 | 16.0 | 89.5 | 69.09 | 20.14 | 73.63 | - | 2.56 | 15 | | |
| DS | Bank | 12 | - | 10 | 66.0 | 24.0 | 95.0 | 65.68 | 29.32 | 70.13 | - | 2.65 | 16 | | |
| UD | (1) | 17 | - | 7 | 84.0 | 9.0 | 103.2 | 65.52 | 37.68 | 77.10 | 1.43 | 2.49 | - | 1.63 | 0.0201 |
| UD | | 10 | - | 7 | 80.5 | 12.5 | 100.7 | 60.18 | 40.52 | 79.45 | 1.41 | 2.63 | 15 | 1.32 | 0.0195 |
| DS | Left | 8 | - | 10.5 | 69 | 20.5 | 102.3 | 57.29 | 45.01 | 95.09 | - | 2.66 | 13 | | |
| DS | Bank | 11 | 36.8 | 62.0 | 2 | 1.8 | - | - | - | 30.71 | - | 2.66 | - | | |
| UD | (2) | 9 | - | 8.0 | 80 | 12.0 | 78.2 | 38.78 | 39.42 | 55.95 | - | 2.56 | - | | |
| UD | | 28 | - | 5.0 | 77 | 18.0 | 92.2 | 64.33 | 27.67 | 77.63 | 1.54 | 2.46 | 12 | 1.34 | 0.0212 |

Table A.4.2.3 Test Result Summary Sheet of Bridge Sites

Bridge No. 3

Location : Chakupat

| Sam- ple Type | B. H. No. | Depth m | Percentage | | | | Clay | LL % | PL % | PI % | NMC % | Bulk Density gm/cm ³ | Specific Gravity gm/cm ³ | SPT Value N | Qu kg/cm ² | Consolidation mv cm ² /kg | Remarks |
|---------------------|--------------|------------|------------|------|------|------|--------|-------|-------|--------|----------|---------------------------------------|---|-------------------|--------------------------|--|---------|
| | | | Gravel | Sand | Silt | Clay | | | | | | | | | | | |
| DS | Right | 4 | - | 3 | 74 | 23 | 65.75 | 46.13 | 19.62 | 44.96 | - | 2.65 | 5 | | | | |
| DS | Bank | 8 | - | 8 | 66.5 | 25.5 | 66.55 | 43.02 | 23.53 | 46.86 | - | 2.65 | 8 | | | | |
| UD | (1) | 5 | - | 5 | 76 | 19 | 68.95 | 44.22 | 24.73 | 87.21 | 1.54 | 2.49 | - | 1.05 | | | |
| UD | | 10 | - | 5 | 81 | 14 | 107.15 | 58.53 | 48.62 | 94.21 | 1.41 | 2.38 | 12 | 1.21 | 0.0232 | | |
| DS | Left | 4 | - | 17 | 59 | 24 | 64.75 | 46.68 | 18.07 | 55.94 | - | 2.56 | 7 | | | | |
| DS | Bank | 8 | - | 5 | 78 | 17 | 90.50 | 54.18 | 36.32 | 100.90 | - | 2.66 | 7 | | | | |
| UD | (2) | 6 | - | 3 | 70 | 27 | 66.90 | 43.89 | 23.01 | 68.57 | - | 2.56 | 2 | | | | |
| UD | | 11 | - | 12 | 78 | 10 | 64.00 | 46.11 | 17.90 | 87.18 | - | 2.53 | - | | | | |

Table A.4.2.4 Test Result Summary Sheet of Bridge Sites

Bridge No. 4

Location : Koteswhor

| Sam- ple Type | B. H. No. | Depth m | Percentage | | | | Clay | LL % | PL % | PI % | NMC % | Bulk Density gm/cm ³ | Specific Gravity gm/cm ³ | SPT Value N | Qu kg/cm ² | Consolidation mv cm ² /kg | Remarks |
|---------------------|--------------|------------|------------|------|------|------|------|-------|-------|-------|----------|---------------------------------------|---|-------------------|--------------------------|--|---------|
| | | | Gravel | Sand | Silt | Clay | | | | | | | | | | | |
| DS | Right | 4 | 35 | 61.5 | 3.5 | - | - | - | - | 16.28 | - | 2.62 | 17 | | | | |
| DS | Bank | 10 | - | 7 | 78.5 | 14.5 | 90.8 | 57.57 | 33.23 | 92.71 | - | 2.46 | 7 | | | | |
| UD | (1) | 7.5 | - | 5 | 87.0 | 8.0 | 90.0 | 55.77 | 34.23 | 88.67 | 1.46 | 2.49 | - | 0.84 | 0.0252 | | |
| UD | | 13 | - | 5 | 92.5 | 2.5 | 98.1 | 61.35 | 36.75 | 80.67 | 1.45 | 2.43 | - | 0.76 | 0.0231 | | |
| DS | Left | 4 | 17 | 80 | 3 | - | - | - | - | 15.11 | - | 2.66 | 17 | | | | |
| DS | Bank | 14 | - | 6 | 78 | 16 | 98.0 | 59.93 | 38.07 | 92.46 | - | 2.59 | 7 | | | | |
| UD | (2) | 9 | - | 5 | 83 | 12 | 81.0 | 58.21 | 22.79 | 78.22 | - | 2.49 | - | | | | |
| UD | | 13 | - | 7 | 81 | 12 | 96.9 | 57.38 | 39.52 | 86.36 | - | 2.52 | - | | | | |

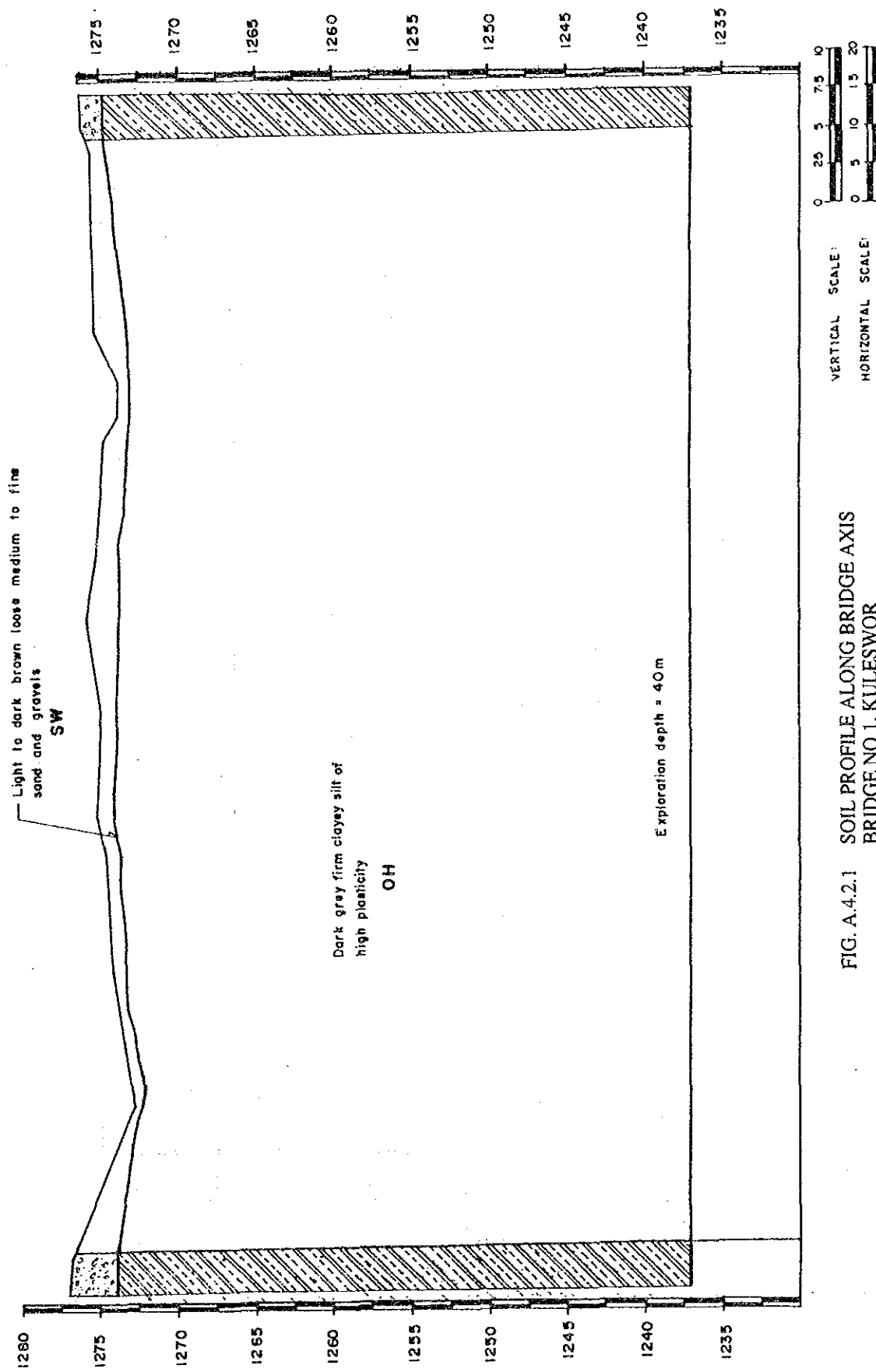


FIG. A.4.2.1 SOIL PROFILE ALONG BRIDGE AXIS
BRIDGE NO 1, KULESWOR

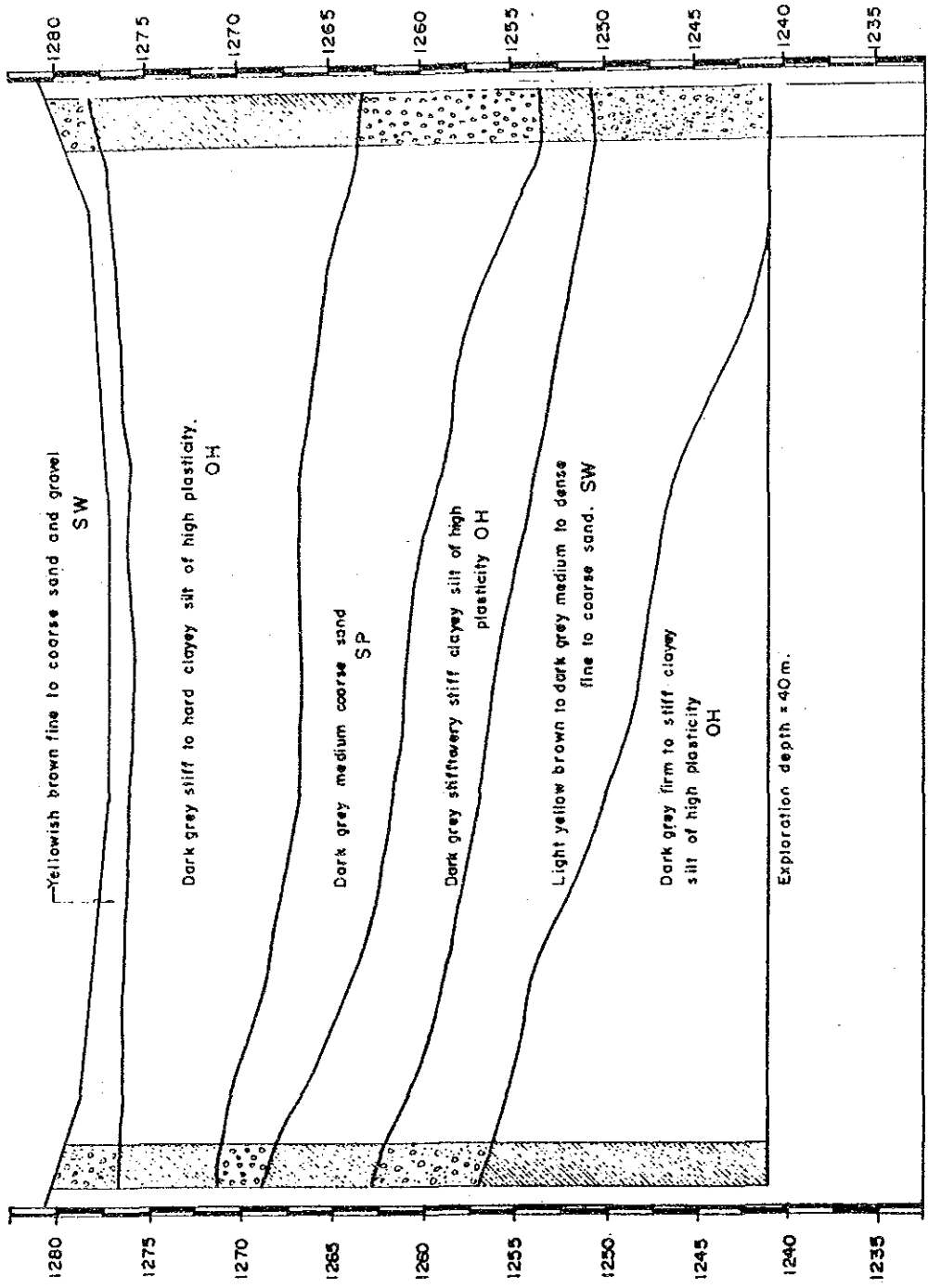
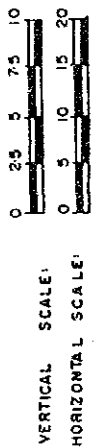


FIG. A.4.2.2 PROFILE ALONG BRIDGE AXIS
BRIDGE NO 2, THAPATHALI



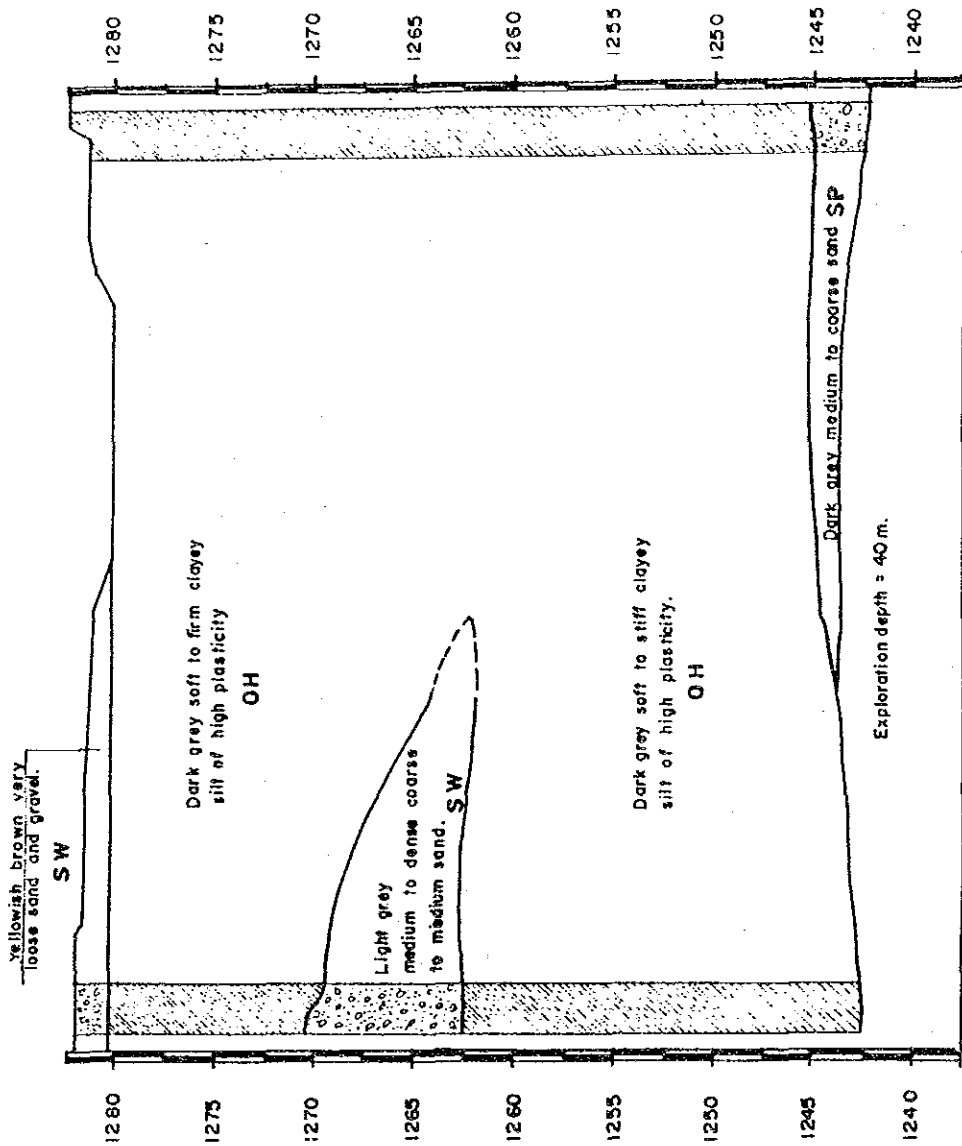
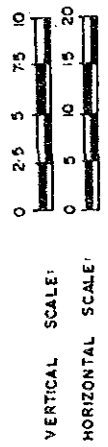


FIG. A.4.2.3 SOIL PROFILE ALONG BRIDGE AXIS
BRIDGE NO 3, CHAKUPAT



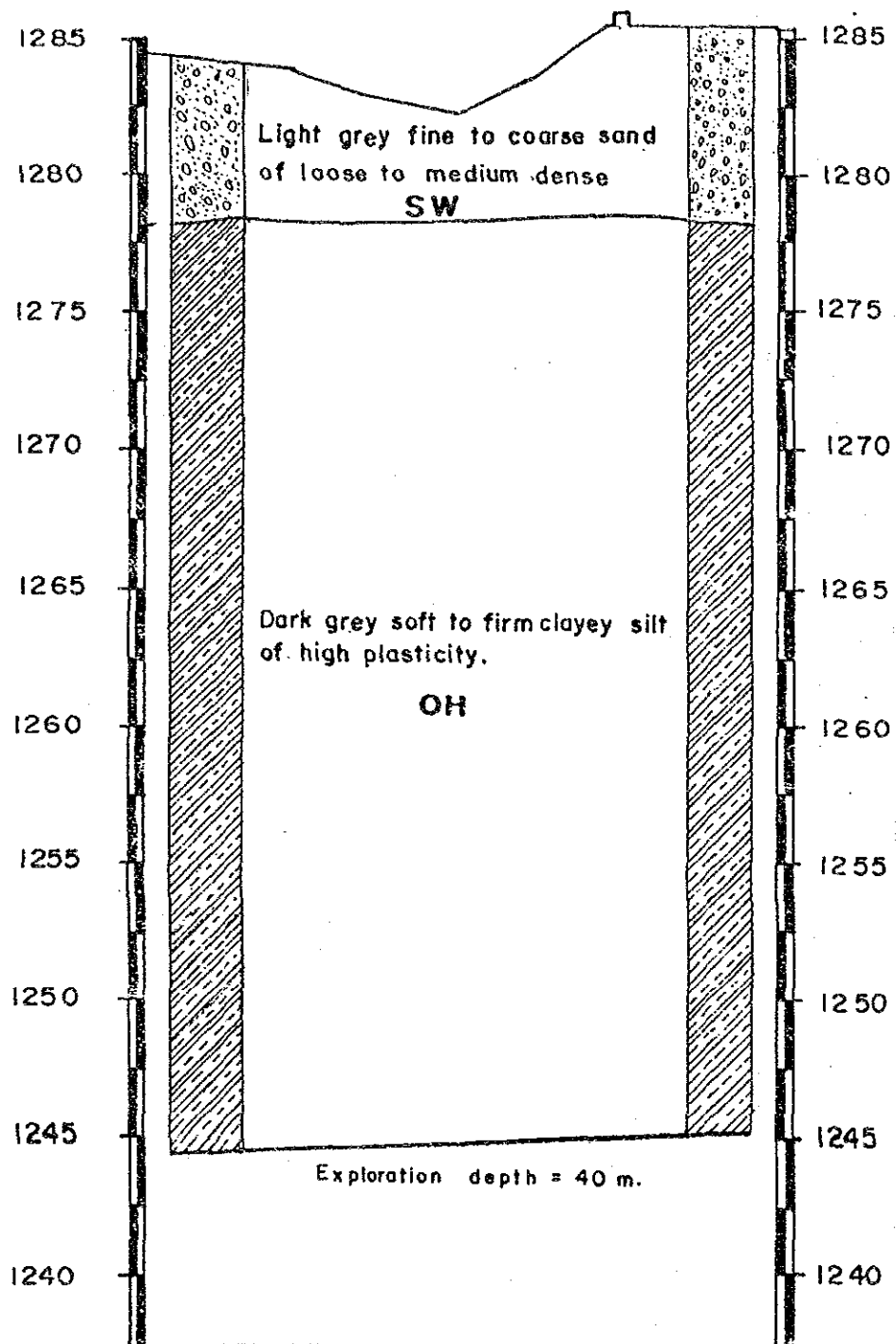


FIG. A.4.2.4 SOIL PROFILE ALONG BRIDGE AXIS
BRIDGE NO 4, KOTESWOR

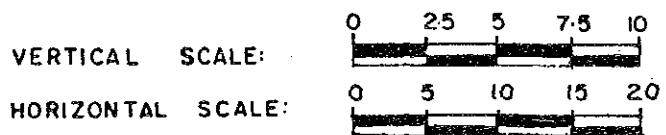


TABLE A.4.2.5 FIELD DENSITY TEST

| Road Pits | RP1 | RP2 | RP3 | RP4 | RP5 | RP6 | RP7 | RP8 | RP9 | RP10 | RP11 |
|----------------------------------|------|------|------|------|------|------|------|------|------|------|------|
| Field Density gm/cm ³ | 1.79 | 1.58 | 1.76 | 1.59 | 1.77 | 1.87 | 1.67 | 1.83 | 1.87 | 1.69 | 1.87 |

TABLE A.4.2.6 LOCATIONS OF DCPT AND NUMBER OF BLOWS TO PENETRATE 80cm

| Location | CP1 | CP2 | CP3 | CP4 | CP5 | CP6 | CP7 | CP8 | CP9 | CP10 | CP11 |
|-------------|------|------|------|------|------|------|------|------|------|------|------|
| No of blows | 10 | 12 | 6 | 15 | 17 | 17 | 12 | 15 | 22 | 13 | 25 |
| Location | CP12 | CP13 | CP14 | CP15 | CP16 | CP17 | CP18 | CP19 | CP20 | CP21 | CP22 |
| No of blows | 1 | 8 | 7 | 7 | 20 | 22 | 8 | 16 | 9 | 11 | 32 |

TABLE A.4.2.7 CBR VALUE COMPUTED FROM GRAPH

| Location | CP2 | CP4 | CP8 | CP10 | CP11 | CP13 | CP14 | CP17 | CP18 | CP20 | CP21 |
|------------------|-----|-----|-----|------|------|------|------|------|------|------|------|
| CBR (Correlated) | 5.0 | 7.4 | 7.8 | 5.4 | 7.0 | 4 | 3.4 | 10.4 | 4.0 | 4.6 | 12 |

Appendix 4.2.2 Description of Subgrade

In total eleven test pits (RP) along the proposed road were excavated at an interval of 1 km. to assess their properties. Samples from those pits were collected from different depths. General description of soil strata upto 1 m for all eleven road pits (RP) are presented in following table.

| Pit No | Depth (cm) | Description of soil |
|--------|-------------|---|
| RP1 | 0-0.15 cm | Light grey silty clay with few fine sand |
| | 0.15-0.35 | Light grey clayey sandy silt with some gravels |
| | 0.35-1.0 m | Light brown micacious silty fine sand with gravels & traces of boulders |
| RP2 | 0.0-0.25 | Grey to light brown silty clay with some fine sand |
| | 0.25-0.50 | Light brown micacious silty clay with fine sand |
| | 0.50-1.0 | Light brown sandy clayey silt with traces of gravel |
| RP3 | 0.0-0.25 | Grey micacious silty clay with fine sand |
| | 0.25-1.0 | Light grey micacious sandy silt with gravels and clay |
| RP4 | 0.0-0.10 | Dark grey silty clay with few micacious sand |
| | 0.10-1.0 | Brown sandy silt with gravels & clay |
| RP5 | 0.0-0.15cm | Light brown micacious silty clay with some sand |
| | 0.15-0.45 | Light grey sandy silt with some gravels & traces of clay |
| | 0.45-0.55 | Light brown micacious medium to fine sand |
| | 0.55-1.0m | Grey & brown colour mixed silty clay with few micacious sand |
| RP6 | 0.0-0.25cm | Light grey micacious silty fine sand with traces of clay |
| | 0.25-0.45cm | Light grey silty sand with clayey gravels |
| | 0.45-1.0m | Light grey to white micacious medium to coarse sand with some gravels |
| RP7 | 0.0-0.25cm | Light grey to brown micacious silty fine sand with clay |
| | 0.25-0.60 | Dark grey micacious sandy silt with clay and gravels |
| | 0.60-1.0 | Light brown micacious fine sand |
| RP8 | 0.0-0.20 | Dark grey silty clay |
| | 0.20-0.50 | Dark grey sandy silt with clay & gravels |
| | 0.50-1.0 | Light grey to brown micacious silty medium to fine sand |
| RP9 | 0.0-0.20 | Dark grey silty clay |
| | 0.20-0.60 | Dark grey sandy silt with traces of gravel & clay |
| | 0.60-1.0 | Light grey micacious silty medium to coarse sand |
| RP10 | 0.0-0.10 | Light grey fine micacious silty clay with fine sand |
| | 0.10-1.0 | Light grey silty sand with traces of clayey gravels |
| RP11 | 0.0-0.15 | Dark grey silty clay |
| | 0.15-1.0 | Light grey to brown sandy silt |

Table A.4.2.8 Test Result Summary Sheet of Road Pits

| S. N. | Road Pit No. | Depth | Description of Soil | Percentage of | | | | Atterberg Limits | | | NMC % | Bulk Density gm/cm ³ | Specific Gravity gm/cm ³ | Compact % | CBR |
|-------|--------------|-------|--|---------------|-------|-------|-------|------------------|-------|-------|-------|---------------------------------|-------------------------------------|-----------|-----|
| | | | | Gravel | Sand | Silt | Clay | LL % | PL % | PI % | | | | | |
| 1. | RP1 | 0.30 | Light Gray Clayey Sandy Silt with some Gravels | 7.20 | 24.68 | 62.62 | 5.50 | 37.25 | | 33.63 | 1.79 | 2.66 | 101.0 | 4.93 | |
| 2. | RP2 | 0.80 | Light Brown Sandy Clayey Silt with Traces of Gravels | 1.18 | 22.00 | 70.32 | 6.50 | 28.20 | | 25.68 | 1.58 | 2.59 | 101.5 | 3.04 | |
| 3. | RP3 | 0.80 | Light Grey Micaceous Sandy Silt with Gravels and Clay | 5.20 | 42.24 | 50.76 | 1.80 | 29.00 | | 25.00 | 1.76 | 2.52 | 101.6 | 12.18 | |
| 4. | RP4 | 0.25 | Brown Sandy Silt with Gravels and Clay | 9.48 | 25.40 | 58.12 | 7.00 | 43.65 | 27.95 | 40.00 | 1.59 | 2.66 | 98.0 | 8.89 | |
| 5. | RP5 | 0.25 | Light Grey Sandy Silt with Gravels and Traces of Clay | 19.23 | 25.00 | 53.27 | 2.50 | 33.80 | | 30.33 | 1.77 | 2.55 | 95.0 | 7.22 | |
| 6. | RP6 | 0.25 | Light Grey Silty Sand with Clay and Gravels | 0.95 | 78.16 | 18.21 | 2.68 | 33.75 | | 4.94 | 1.87 | 2.73 | 96.4 | 12.99 | |
| 7. | RP7 | 0.45 | Dark Grey Micaceous Sandy Silt with Clay and Gravels | 1.07 | 28.70 | 60.77 | 10.00 | 31.35 | | 12.14 | 1.67 | 2.731 | 99.6 | 5.07 | |
| 8. | RP8 | 0.40 | Dark Grey Sandy Silt with Clay and Gravels | 2.97 | 20.16 | 69.37 | 7.50 | 35.08 | | 13.26 | 1.83 | 2.69 | 97.47 | 3.05 | |
| 9. | RP9 | 0.50 | Dark Grey Sandy Silt with Traces of Clay and Gravels and Clay | 4.23 | 44.37 | 48.4 | 3.00 | 22.30 | | 12.32 | 1.87 | 2.63 | 96.2 | 8.96 | |
| 10. | RP10 | 0.70 | Light Grey Silty Sand with Traces of Clay and Gravels and clay | 0.30 | 60.03 | 38.07 | 1.60 | | | 25.38 | | 2.55 | 97.25 | 8.5 | |
| 11. | RP11 | 0.75 | Light Grey to Brown Sandy Silt | 11.30 | 65.15 | 19.75 | 3.80 | | | 13.84 | 1.87 | 2.73 | 100 | 14.98 | |

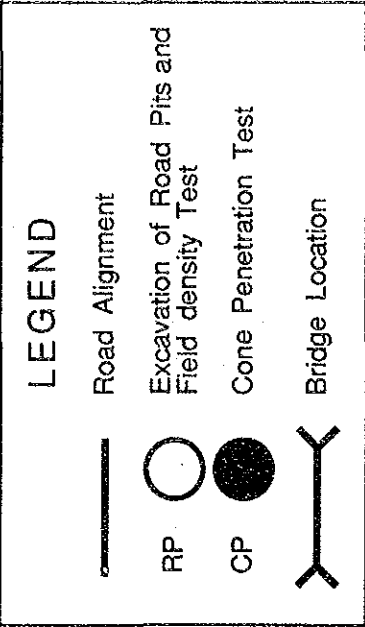
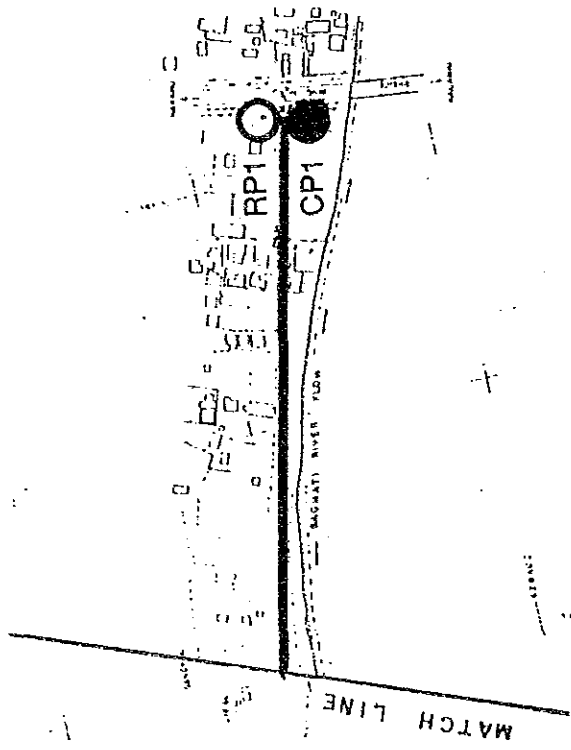


FIGURE A 4.2.1 LOCATION OF ROAD PITS (1/8)

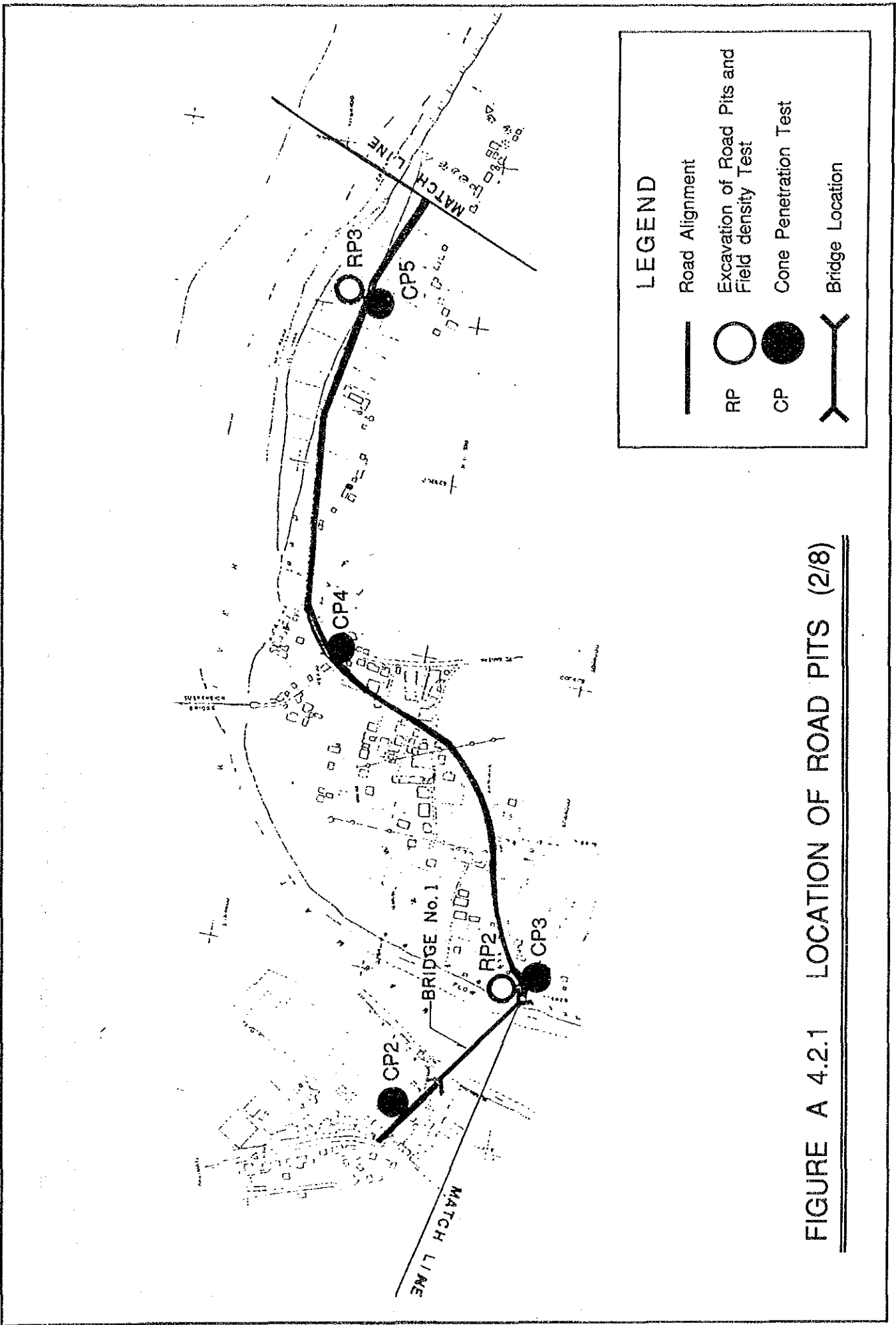


FIGURE A 4.2.1 LOCATION OF ROAD PITS (2/8)

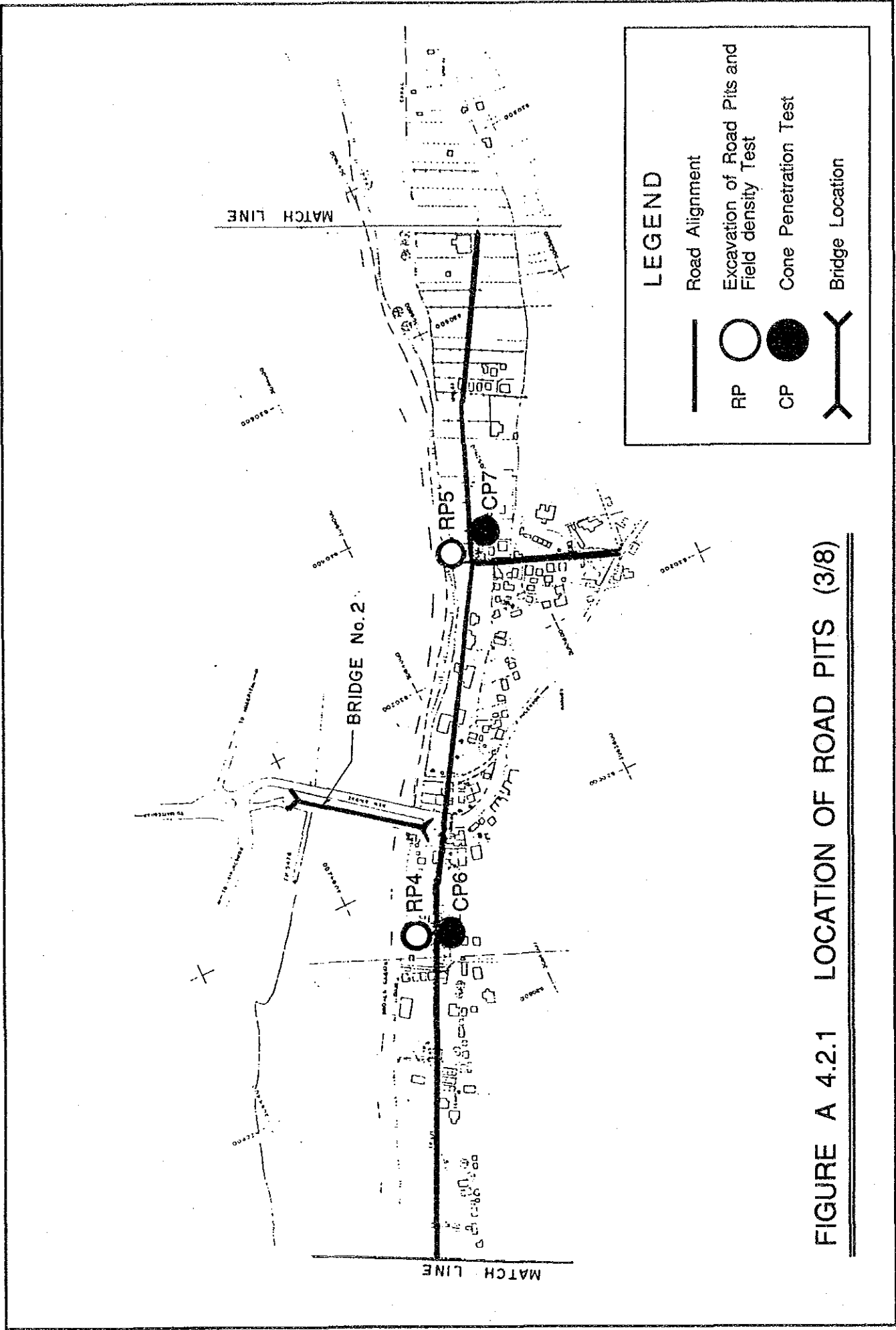
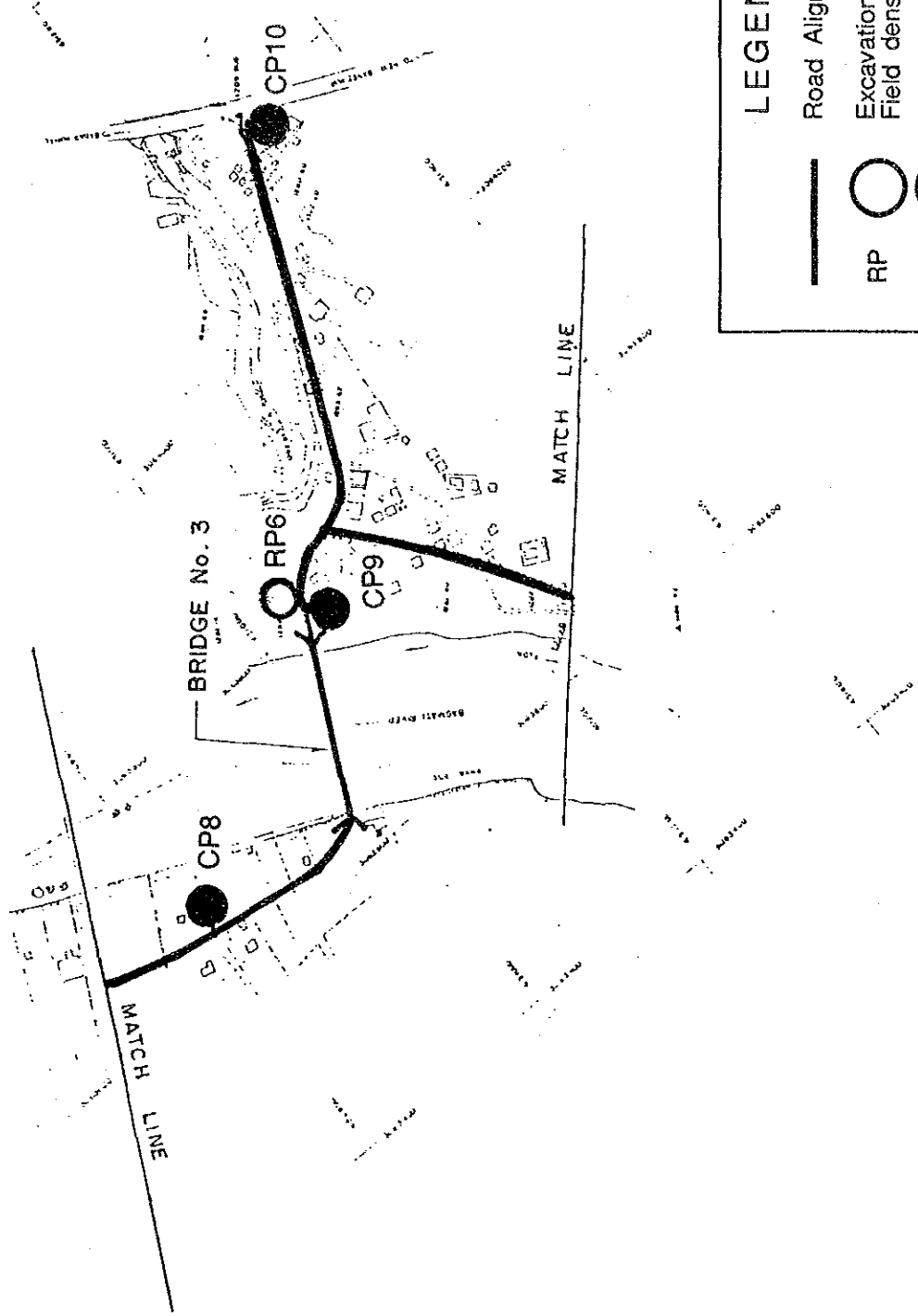


FIGURE A 4.2.1 LOCATION OF ROAD PITS (3/8)



LEGEND





| | |
|---|--|
|  | Road Alignment |
|  | Excavation of Road Pits and Field density Test |
|  | Cone Penetration Test |
|  | Bridge Location |

FIGURE A 4.2.1 LOCATION OF ROAD PITS (4/8)

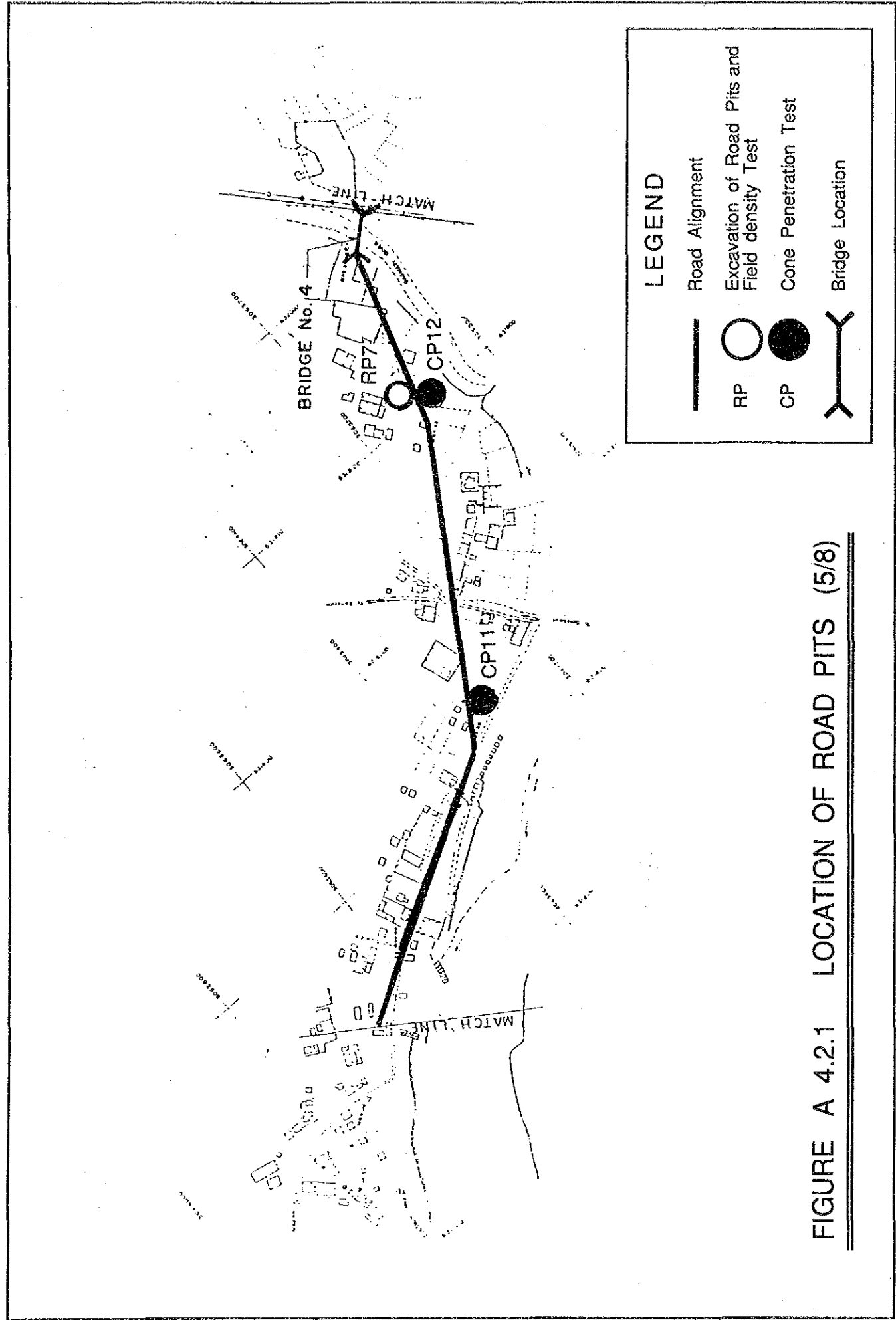


FIGURE A 4.2.1 LOCATION OF ROAD PITS (5/8)

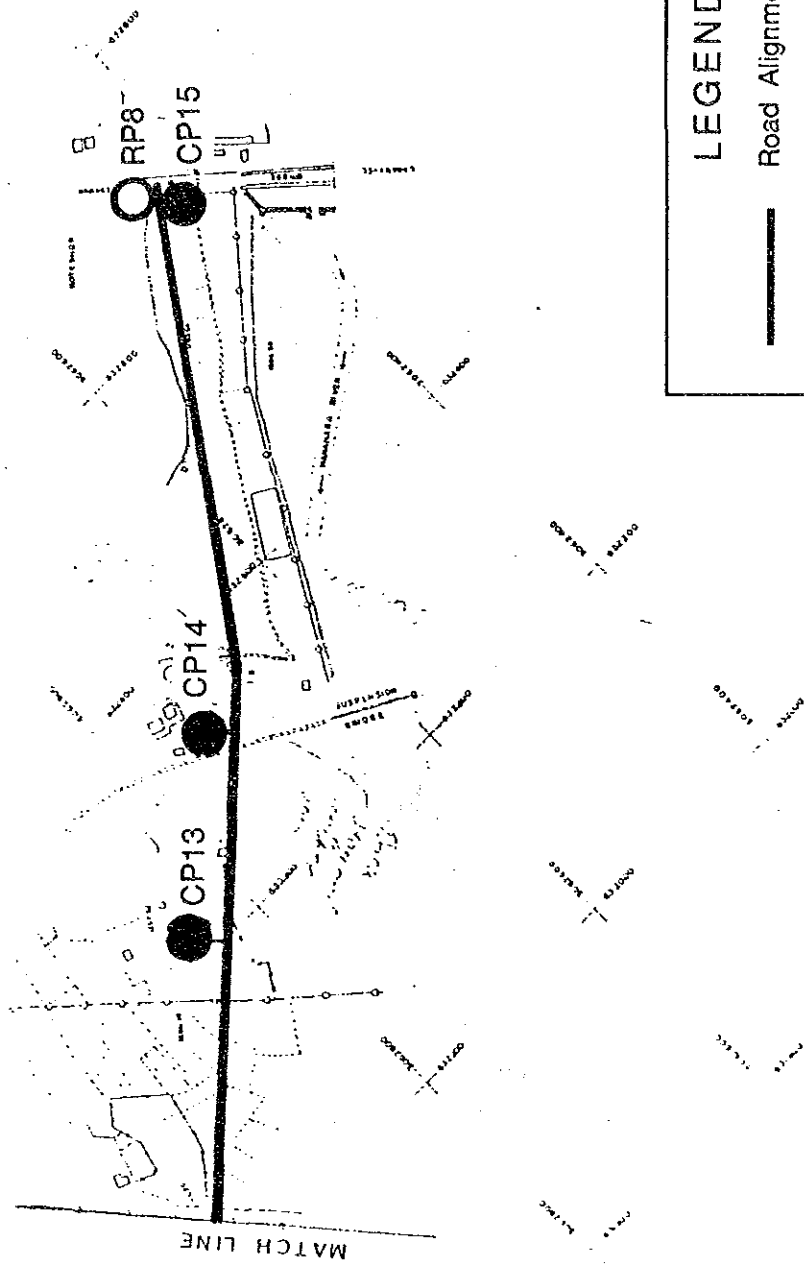


FIGURE A 4.2.1 LOCATION OF ROAD PITS (6/8)

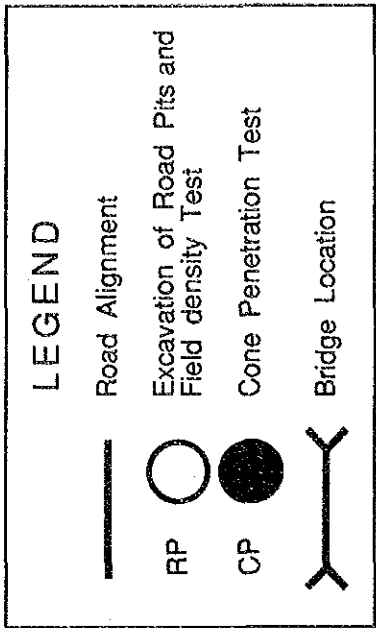
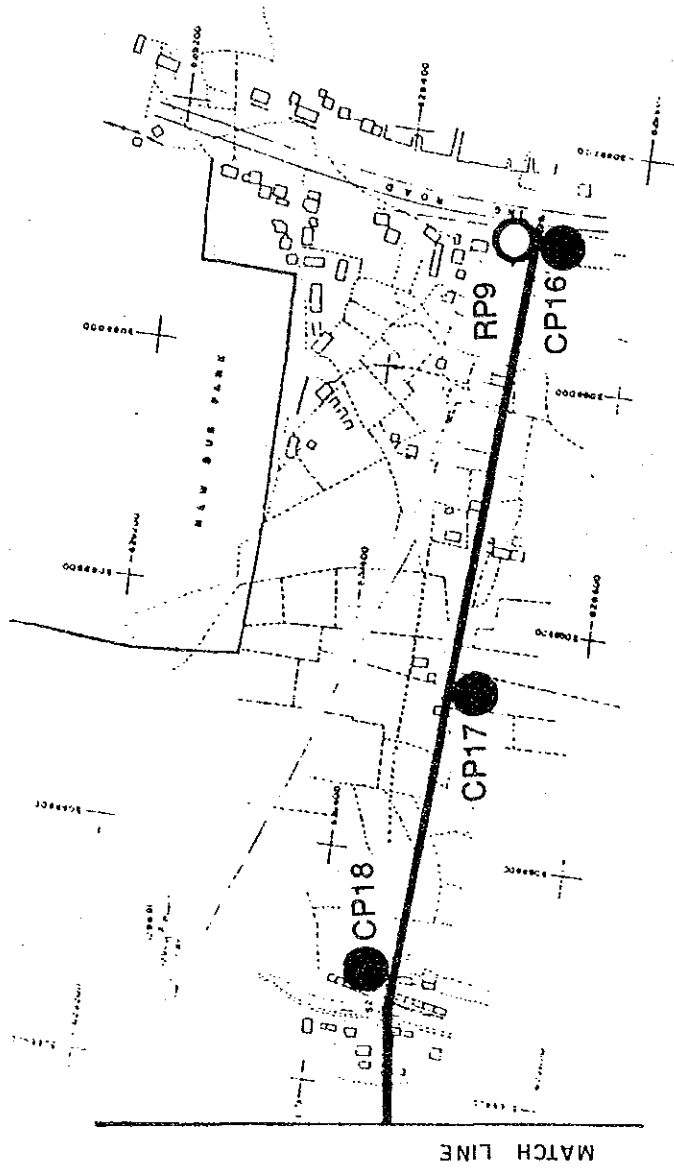


FIGURE A 4.2.1 LOCATION OF ROAD PITS (7/8)

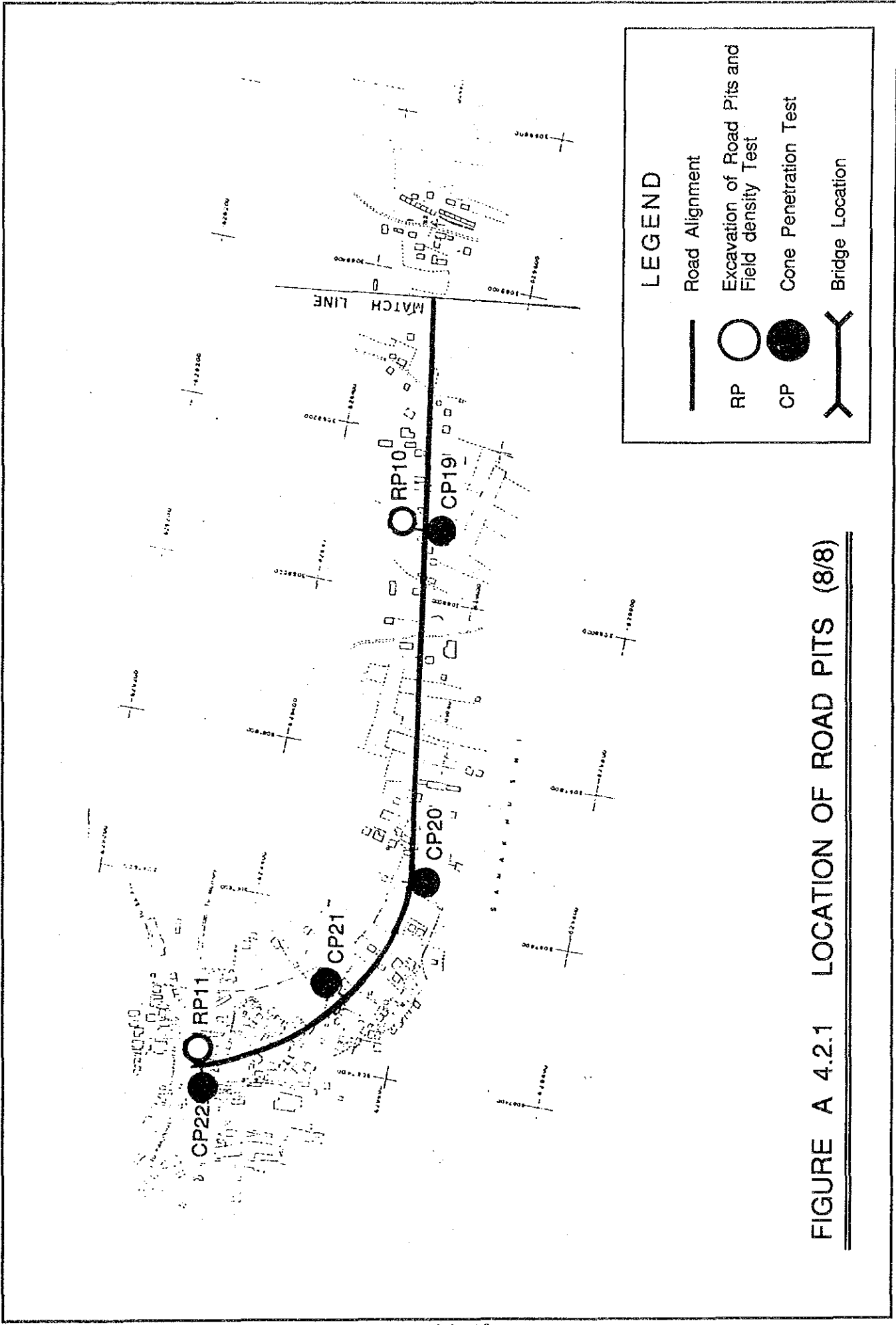


FIGURE A 4.2.1 LOCATION OF ROAD PITS (8/8)

Appendix 4.2.3 Description of Construction Materials

(1) Borrow Pits of Soils

Three sites were identified for the borrow pits of soil (subgrade materials). They were: Thimi, Gokarna Ban and Kapan:

Thimi borrow pit

Thimi borrow pit is located along the Kathmandu-Bhaktapur road. The quarry site is in the form of hillock approximately 15-20m high from surrounding ground level. Huge quantity of soil were already excavated from that part as a filling material for construction of building complexes.

Two samples were collected from that borrow pit, one from 3 m high from ground level and another from the toe of the hillock. Both the samples were similar and according to visual classification they were classified as light grey to grey sandy silt with some clay.

It is estimated that around 15,00,000 m³ of soil can be excavated from that area.

Gokarna Ban

The site lies just opposite of Gokarna Safari Park along Kathmandu-Sankhu road. One sample was collected from there. The soil was classified as dark grey clayey silt with medium to fine sand.

The site is accessible throughout the year and the estimated quantity which could be borrowed from there is approximately 20,00,000 m³.

Kapan

The site is located one kilometer north from the Mahankal Chaur. At present the borrow pit is being used for extraction of sands, which is underlain by 3-5m thick soil. The soil is classified as light grey silty sand with traces of gravels. It is estimated that approximately 50,000 m³ of soil can be borrowed from there.

(2) Borrow Pit for Gravels

Two samples of gravels were collected from chunnikhel, which is located 4 kilometer south from Nakkhu. The samples collected were dark brown sandy gravels. The estimated quantity of gravels, which can be extracted from there is approximately 1,00,000 m³ to 2,00,000 m³.

(3) Borrow Pit of Sands

Three sites namely Pikhel, Kapan and Basundhara were identified for quarrying of sands. Two samples were extracted from each site. Brief description of site and visual classification of sands are presented below.

Pikhel

The site is situated 4 km north from Bhaktapur, Unlike in other borrow pit areas, the sands at Pikhel is being extracted by digging holes. The sand of the area is of very good quality containing less than 1% of silt. Samples were extracted from two holes. The samples collected are classified as white micaceous medium to fine sand. Available quantity is estimated to be around 1,00,000 m³ (Deposit unlimited)

Kapan

Sands were extracted from the same area, from where the soil sample was collected. Two samples; one from the lower part and another from the top was extracted for assessment of their basic properties. The sands which were available were light grey white micaceous gravelly sand with traces of silt. The estimated quantity of sand, which could be extracted from there is 1,00,000 m³ and further extension of 1,00,000 m³ is possible.

Basundhara

The site is located close to the Ring Road near Marajganj. Two samples were collected from there, which were similar and are classified as light grey to white micaceous sand with gravels and traces of silt. Approximately from 50,000 m³ of sand can be extracted from that borrow area. Further extension of 1,00,000 m³ is possible.

(4) Borrow Pits for Crushed Stone

Three sites were identified for borrow areas of crushed stones. They were:

- Godavari Marble Industries, Godavari
- Thankot crushing plants, Thankot
- Purna Roda Dhunga Udyog, Jhalungtar

Brief description about the sites and their daily capacity is given below.

Godavari Marble Industries, Godavari

The crushing plant is located 12 km south from Kathmandu. The plant produces mainly two sizes of stones; from 12.5 mm to 19.05 mm and from 19.05 mm to 50 mm. The capacity of plant in average is 60 m³ per day.

Thankot crushing plant

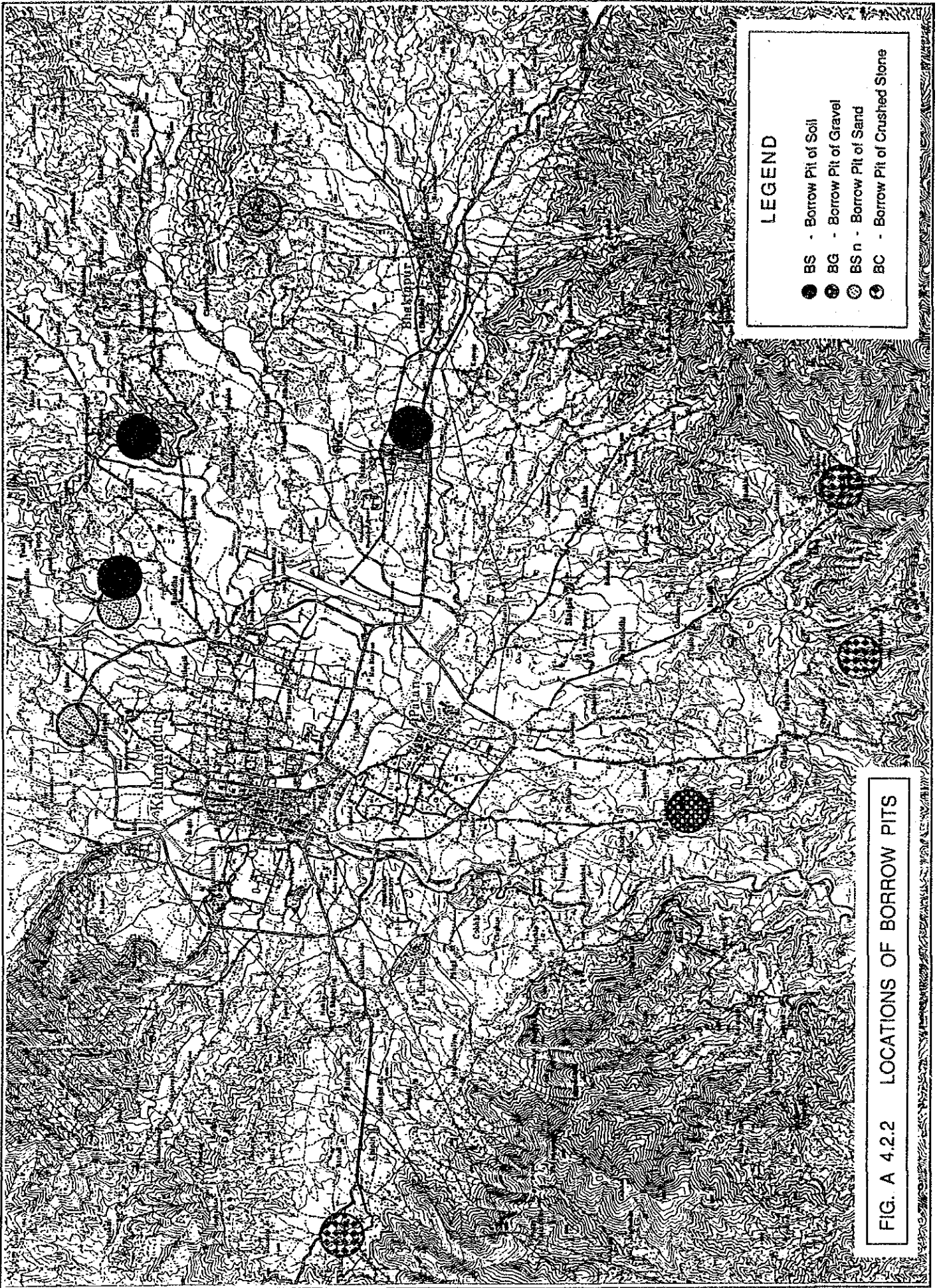
In Thankot areas, there are seven crushing plant. Sources of stone quarry for all the plants is Mahadev Besi. The sizes of aggregate which they produce is also same as from Godavari. Total capacity of all the plants is 40m³ per day.

Purna Road Dhunga Udyog

The Purna Roda Udyog is located near Bajrabarahi and is approximately 12 km south of Kathmandu. The sizes of aggregate which they produce is also from 12.50 mm to 40.00 mm and from 19.05 mm to 50.00 mm. The estimated capacity of plant is 50 m³ per day.

Table A.4.2.9 Test Result Summary Sheet of Borrow Pits

| Location | No. | Description of Soil | Percentage of | | | | Atterberg Limits | | | NMC % | Bulk Density gm/cm ³ | Specific Gravity gm/cm ³ | Compact % | CBR |
|------------|-------|---|---------------|-------|-------|------|------------------|------|-------|-------|---------------------------------|-------------------------------------|-----------|-----|
| | | | Gravel | Sand | Silt | Clay | LL % | PL % | PI % | | | | | |
| Gokarna | 2. | Dark Grey Clayey Silt Medium to Fine Sand | 2.12 | 30.88 | 60.20 | 6.80 | | | 31.36 | 1.93 | 2.73 | 97.6 | 3.13 | |
| Thimi | 1. | Grey Clayey Silt with Fine Sand | | 21.30 | 78.70 | | | | 32.98 | 2 | 2.63 | 95.3 | 4.13 | |
| Thimi | 2. | Light Grey Micaceous Sandy Silt with Clay | | 16.77 | 81.18 | 3.05 | 38.95 | | 21.98 | 1.87 | 2.69 | 102.4 | 4.5 | |
| Kapan | 3. | Light Grey Silty Sand and Traces Gravels | 9.46 | 63.47 | 25.07 | 2.00 | 25.45 | | 18.84 | | 2.66 | 97.6 | 6.73 | |
| Chunikhel | 1. | Dark Brown Sandy Gravels | 76.70 | 20.15 | 2.35 | 0.75 | | | 12.89 | 1.87 | 2.58 | 98.4 | 38.3 | |
| Chunikhel | 2. | Dark Brown Sandy Gravels | 77.80 | 19.25 | 2 | 0.95 | | | 14.99 | 1.59 | 2.62 | 98.75 | 45.33 | |
| Kapan | Upper | Light Grey to White Micaceous Gravelly Sand | 14.53 | 84.12 | 1.35 | | | | 5.4 | 1.77 | 2.66 | | | |
| Thankot | 1. | Bluish Grey Fourty Down Gravels | 100.00 | | | | | | 0.435 | | 2.67 | | | |
| Thankot | 2. | Blush Grey Fifty Down Gravels | 100.00 | | | | | | 0.1 | | 2.71 | | | |
| Godawari | 1. | Redish Brown Fourty Down Gravels | 100.00 | | | | | | 0.24 | | 2.64 | | | |
| Godawari | 2. | Radish Brown fifty Down Gravels | 100.00 | | | | | | 0.32 | | 2.61 | | | |
| Jhalungtar | 1. | Light Brown Fourty Down Gravels | 100.00 | | | | | | 0.1 | | 2.63 | | | |
| Jhalungtar | 2. | Light Brown Fifty Down Gravels | 100.00 | | | | | | 0.2 | | 2.73 | | | |



Appendix 4.2.4 Pile Foundation Analysis

The foundation analysis was carried out for precast and driven and bored and cast-in-place piles. For both pile types analysed, the diameter assumed in case of bored and cast in place pile is 600 mm and in case of precast and driven pile, it has been assumed as 450 mm. At this stage when the actual load coming on foundation is not known, a tentative load of 1000 tons likely to be imposed on foundation soil from bridge super-structure and sub-structure, has been assumed in the analysis.

(1) Piles in clay

Piles in clay may fail individually or as a group. The capacity of the pile was computed considering both of the above cases and the minimum value obtained was taken as the capacity of the pile.

(a) Carrying Capacity of a Single Pile

The ultimate capacity for a single pile in clay was computed using the relation, as recommended by Simons and Menzies, 1974 (Ref. 2).

$$Q_u = A_s \cdot \alpha \cdot S_u + A_b \cdot S_u \cdot N_c \text{ ----- Eq. (2.1)}$$

Where,

| | | |
|----------|---|------------------------------------|
| Q_u | = | ultimate capacity of a single pile |
| A_s | = | Area of shaft |
| α | = | adhesion factor |
| | = | 0.8 for driven piles (assumed) |
| | = | 0.45 for bore piles (assumed) |
| S_u | = | Shear strength at base |
| A_b | = | Area at base |
| N_c | = | bearing capacity factor |

The total capacity of pile in a group on the basis of piles failing individually was computed as given in Tomlinson, 1967 (Ref. 3).

$$Q_g = n Q_s \text{ ----- Eq. (2.2)}$$

Where,

| | | |
|-------|---|-------------------------------------|
| Q_g | = | carrying capacity of the pile group |
| n | = | number of piles |
| Q_s | = | carrying capacity of a single pile |

(b) Carrying Capacity of Pile in a Group

The capacity of the pile foundation with the piles in group was computed by carrying out block analysis as suggested by Terzaghi and Peck (1967) (Ref. 1).

A pile spacing equal to the perimeter of the pile was used in the analysis. The recommended relationship which was utilised in the present analysis is

$$Q_g = \frac{\alpha S_u 2(L+B) \times D + N_c \cdot S_b \cdot L \times B}{3} - E_q \quad (2.3)$$

Where,

| | | |
|----------|---|--|
| α | = | adhesion factor |
| S_u | = | average shear strength over the peripheral area of the group |
| S_b | = | shear strength at base |
| Q_g | = | carrying capacity of pile group |
| L | = | length of group |
| B | = | width of group |
| D | = | depth of pile |

The minimum value obtained from E_q (2.2) and E_q (2.3) was taken as the capacity of group.

(c) Settlement of pile group

The settlement of a pile group in clay was computed using the relation proposed by Tomlinson, 1969 (Ref. 3).

$$\delta = 0.55 q_n \times m_v \times 1.5 B \text{ ----- } E_q \quad (2.4)$$

Where,

| | | |
|----------|---|--|
| δ | = | settlement of pile group |
| q_n | = | net increase in pressure |
| m_v | = | co-efficient of volume compressibility |
| B | = | width of foundation |

The settlement of the pile groups was estimated on the assumption that the group behaves as a raft having dimensions in plan equal to the overall dimensions of the group plus the additional width given by the 1 in 4 spread of load. The base of the "virtual raft foundation" was assumed to be at a depth of two-third of the length of piles.

(2) Piles in sand

(a) Ultimate capacity of a single pile

The ultimate capacity of a single pile was computed using the following relation as given in Simons & Menzies, 1974 (Ref. 2).

$$Q_u = A_s K p_{avg} \tan \delta + A_b p_o (N_q - 1) \text{ --- } E_q \quad (2.5)$$

Where,

- Q_u = Ultimate pile capacity
- A_s = Area of the shaft
- K = Co-efficient of earth pressure
- p_{avg} = Average effective overburden pressure over the embedded length of pile.
- \tan = Co-efficient of friction between soil and pile material.
- A_b = Area of base
- p_o = Effective overburden pressure at base
- N_q = Bearing capacity factor as suggested by Berezantsev (1961).

To obtain pile capacity, a factor of safety of 2.5 was used.

The capacity of the pile group is computed by the relation.

$$Q_g = n Q_s \text{ ----- } E_q \text{ (2.6)}$$

Where,

- n = number of piles
- Q_s = capacity of a single pile

In sands, driving of piles increases the relative density of sand considerably and the average load per pile in a group at failure is more than that for the failure of single comparable pile. Therefore, check of pile group against block failure was not necessary.

b) Settlement

The settlement of the pile group in sand was computed by assuming a virtual raft foundation at the level of the base of piles. The area of "virtual raft" was taken to be equal to the plan area of the pile group, (Tomlinson, 1969) (Ref. 3) and the settlement of the pile group was estimated using the Eq. 3.

Table A.4.2.10 Foundation Analysis

| Bridge Site | Type of Pile Foundation | | | | | | | | | | | |
|-------------|----------------------------------|--------------------------|--------------|-----------------|----------------------------------|------------------------------|------------------------------------|--------------------------|--------------|-----------------|----------------------------------|------------------------------|
| | Precast and Driven 450 mm square | | | | | | Bored and cast in place 600 mm dia | | | | | |
| | Length m | Pile Capacity tons | Spacing m | No. of Piles | Size of Group m \times m | Expected settlement mm | Length m | Pile Capacity tons | Spacing m | No. of Piles | Size of Group m \times m | Expected settlement mm |
| Kuleswar | 24 | 22.5 | 1.9 | 45 | 15.8 by 8.2 | 94 | 27 | 22.5 | 1.9 | 45 | 15.8 by 8.2 | 94 |
| Thapathali | 12 | 22.5 | 1.9 | 45 | 15.8 by 8.2 | 85 | 14 | 22.5 | 1.9 | 45 | 15.8 by 8.2 | 87 |
| Chakupat | 14 | 22.5 | 1.9 | 45 | 15.8 by 8.2 | 89 | 15 | 22.5 | 1.9 | 45 | 15.8 by 8.2 | 100 |
| Koteswor | 19 | 22.5 | 1.9 | 45 | 15.8 by 8.2 | 95 | 20 | 22.5 | 1.9 | 45 | 15.8 by 8.2 | 98 |

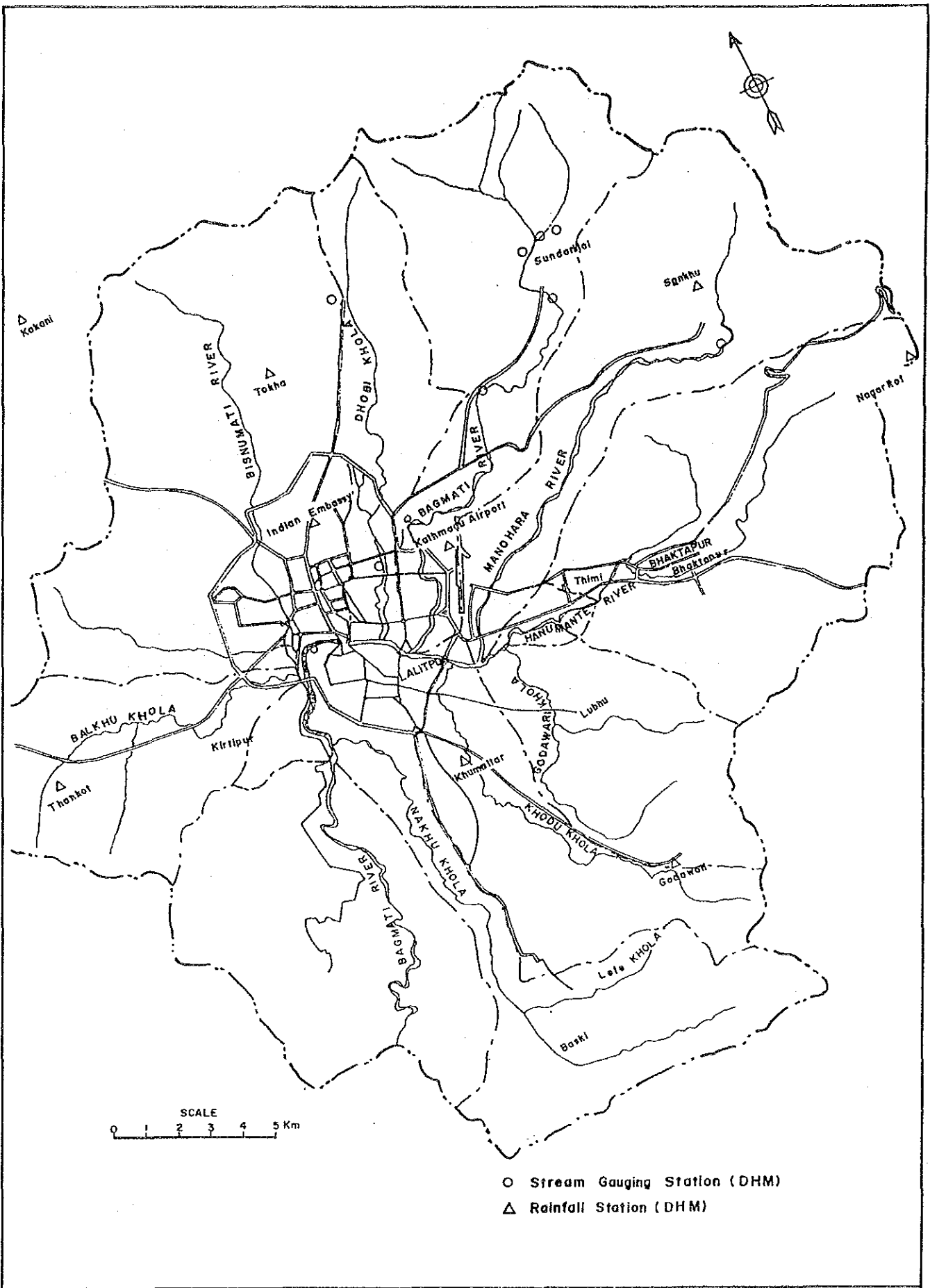


Figure A 4.3.1 LOCATION MAP OF RAINFALL STATION AND STREAM GAUGING STATION

Table A4.3.1 RAINFALL RECORD IN KATHMANDU VALLEY

| YEAR | ANNUAL TOTAL | | | | | | | |
|------|--------------|----------|--------|-----------|-----------|--------|---------|----------|
| | KTM. Airport | Godavari | Kakani | Khumaltar | Bhaktapur | Sankhu | Thankot | Nagarkot |
| 1977 | 1298.0 | 1617.0 | 2392.0 | 1145.0 | * | * | * | 1798.0 |
| 1978 | 1556.0 | 2211.0 | 3241.0 | 1698.0 | * | * | * | 2700.0 |
| 1979 | 1356.0 | 1584.0 | 1734.0 | 950.0 | * | * | * | 1658.0 |
| 1980 | 1341.0 | 1548.0 | 2843.0 | 1009.0 | * | * | * | 1783.0 |
| 1981 | 1370.0 | 1698.0 | 2375.0 | 1159.0 | * | * | * | 1066.0 |
| 1982 | 1168.0 | 1672.0 | * | 1158.0 | * | * | * | 1045.0 |
| 1983 | 1449.0 | 1918.0 | 2986.0 | 1309.0 | * | * | * | 1266.0 |
| 1984 | 1313.0 | 2214.0 | 2672.0 | 1330.0 | * | * | * | 1435.0 |
| 1985 | 1786.0 | 2553.0 | 3288.0 | 1535.0 | * | * | * | * |
| 1986 | 1495.0 | 1910.0 | 3054.0 | 1367.0 | * | * | * | 2089.0 |
| 1987 | 1395.2 | 2061.1 | 2322.0 | 1449.2 | 1484.6 | 1728.0 | 2254.0 | 1645.2 |
| 1988 | 1373.8 | 1973.7 | 2774.9 | 1496.8 | 1784.8 | 1905.5 | 2024.4 | 1581.2 |
| 1989 | 1132.0 | 1644.7 | 3162.0 | 996.3 | 1095.0 | 2117.2 | 2029.6 | * |
| 1990 | 1532.7 | 2086.7 | 2993.8 | 1173.9 | 1752.7 | 2372.7 | 2111.6 | 2132.0 |
| 1991 | 997.5 | 1509.1 | 2689.5 | 870.0 | 896.9 | 1439.0 | 1619.6 | 1742.2 |
| MEAN | 1370.9 | 1880.0 | 2751.9 | 1243.1 | 1402.8 | 1912.5 | 2007.8 | 1687.7 |

Table A.4.3.2 RAINFALL AT KATHMANDU AIRPORT

| Year | Jan. | | Feb. | | Mar. | | Apr. | | May. | | Jun. | | Jul. | | Aug. | | Sep. | | Oct. | | Nov. | | Dec. | | Annual | | | | | | | | | | | | | | | |
|------|------|------|------|------|------|------|------|------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|------|--------|-------|-------|-------|-------|-------|--------|--------|------|--------|--------|-------|--------|--------|--------|-----|
| | max | mean | max | mean | max | mean | max | mean | max | mean | max | mean | max | mean | max | mean | max | mean | max | mean | max | mean | max | mean | max | Total | max | | | | | | | | | | | | | |
| 1977 | 12.0 | 0.4 | 12.0 | 0.4 | 9.0 | 17.0 | 0.5 | 21.0 | 104.0 | 3.5 | 27.0 | 90.0 | 2.9 | 50.0 | 266.0 | 8.9 | 51.0 | 323.0 | 10.4 | 38.0 | 10.9 | 18.0 | 79.0 | 2.6 | 10.0 | 29.0 | 0.9 | 8.0 | 14.0 | 0.5 | 38.0 | 1298.0 | 58.0 | | | | | | | |
| 1978 | 3.0 | 5.0 | 8.0 | 11.0 | 4.0 | 39.0 | 69.0 | 2.2 | 14.0 | 42.0 | 1.4 | 18.0 | 143.0 | 4.6 | 36.0 | 299.0 | 10.0 | 67.0 | 324.0 | 10.5 | 71.0 | 392.0 | 12.6 | 30.0 | 160.0 | 5.3 | 71.0 | 109.0 | 3.5 | 0.0 | 0.0 | 2.0 | 0.1 | 71.0 | 1556.0 | 1.0 | | | | |
| 1979 | 2.0 | 6.0 | 2.0 | 22.0 | 39.0 | 1.4 | 0.6 | 1.0 | 0.0 | 12.0 | 4.0 | 12.0 | 37.0 | 1.2 | 48.0 | 258.0 | 8.6 | 86.0 | 447.0 | 14.4 | 76.0 | 320.0 | 10.3 | 52.0 | 99.0 | 3.3 | 12.0 | 36.0 | 1.2 | 4.0 | 6.0 | 0.2 | 51.0 | 65.0 | 2.1 | 86.0 | 1356.0 | 0.0 | | |
| 1980 | 1.0 | 1.0 | 0.0 | 9.0 | 18.0 | 0.6 | 19.0 | 46.0 | 1.5 | 7.0 | 10.0 | 0.3 | 32.0 | 124.0 | 4.0 | 100.0 | 349.0 | 11.6 | 50.0 | 296.0 | 9.5 | 31.0 | 238.0 | 7.7 | 54.0 | 184.0 | 6.1 | 38.0 | 69.0 | 2.2 | 0.0 | 0.0 | 0.0 | 6.0 | 0.2 | 100.0 | 1341.0 | 0.0 | | |
| 1981 | 11.0 | 14.0 | 0.5 | 0.0 | 0.0 | 22.0 | 60.0 | 1.9 | 38.0 | 101.0 | 3.4 | 54.0 | 216.0 | 7.0 | 35.0 | 141.0 | 4.7 | 36.0 | 304.0 | 9.8 | 47.0 | 257.0 | 8.6 | 50.0 | 225.0 | 7.5 | 0.0 | 0.0 | 0.0 | 16.0 | 42.0 | 1.4 | 0.0 | 0.0 | 0.0 | 54.0 | 1370.0 | 0.0 | | |
| 1982 | 9.0 | 14.0 | 0.5 | 10.0 | 22.0 | 0.8 | 16.0 | 36.0 | 1.2 | 10.0 | 49.0 | 1.6 | 14.0 | 40.0 | 1.3 | 88.0 | 200.0 | 6.7 | 52.0 | 238.0 | 7.7 | 52.0 | 384.0 | 12.4 | 38.0 | 155.0 | 5.2 | 8.0 | 9.0 | 0.3 | 18.0 | 18.0 | 0.6 | 3.0 | 3.0 | 0.1 | 88.0 | 1168.0 | 0.0 | |
| 1983 | 16.0 | 18.0 | 0.6 | 2.0 | 4.0 | 0.1 | 15.0 | 30.0 | 1.0 | 14.0 | 79.0 | 2.6 | 29.0 | 110.0 | 3.5 | 39.0 | 81.0 | 9.7 | 72.0 | 300.0 | 16.1 | 45.0 | 194.0 | 6.3 | 44.0 | 283.0 | 9.6 | 43.0 | 130.0 | 4.2 | 0.0 | 0.0 | 15.0 | 15.0 | 0.5 | 72.0 | 1449.0 | 0.0 | | |
| 1984 | 14.0 | 14.0 | 0.5 | 14.0 | 17.0 | 0.6 | 14.0 | 14.0 | 0.5 | 21.0 | 60.0 | 2.0 | 19.0 | 96.0 | 3.1 | 70.9 | 275.0 | 9.7 | 45.0 | 302.0 | 9.7 | 45.0 | 302.0 | 9.7 | 45.0 | 302.0 | 9.7 | 17.0 | 18.0 | 0.6 | 0.0 | 0.0 | 7.0 | 7.0 | 0.2 | 77.0 | 1313.0 | 0.0 | | |
| 1985 | 6.0 | 10.0 | 0.3 | 3.0 | 3.0 | 0.1 | 4.0 | 4.0 | 0.1 | 13.0 | 25.0 | 0.8 | 22.0 | 133.0 | 4.3 | 36.0 | 161.0 | 5.4 | 51.0 | 418.0 | 13.5 | 52.0 | 434.0 | 14.0 | 69.0 | 376.0 | 12.5 | 52.0 | 167.0 | 5.4 | 0.0 | 0.0 | 28.0 | 55.0 | 1.8 | 69.0 | 1786.0 | 0.0 | | |
| 1986 | 0.0 | 0.0 | 0.0 | 20.0 | 23.0 | 0.8 | 7.0 | 16.0 | 0.5 | 24.0 | 93.0 | 3.1 | 21.0 | 97.0 | 3.1 | 65.0 | 316.0 | 10.5 | 78.0 | 381.0 | 12.3 | 62.0 | 219.0 | 7.1 | 48.0 | 221.0 | 7.4 | 26.0 | 80.0 | 2.6 | 0.0 | 0.0 | 0.0 | 32.0 | 49.0 | 1.6 | 78.0 | 1495.0 | 0.0 | |
| 1987 | 2.7 | 3.2 | 0.1 | 25.0 | 43.3 | 1.5 | 9.6 | 35.9 | 1.2 | 11.0 | 34.4 | 1.1 | 18.0 | 57.6 | 1.9 | 16.8 | 116.4 | 3.9 | 86.5 | 498.8 | 16.1 | 39.3 | 256.3 | 8.3 | 45.6 | 171.2 | 5.7 | 124.4 | 159.3 | 5.1 | 0.0 | 0.0 | 18.3 | 18.8 | 0.6 | 124.4 | 1395.2 | 0.0 | | |
| 1988 | 0.6 | 0.6 | 0.0 | 9.7 | 19.1 | 0.4 | 21.9 | 68.0 | 2.2 | 14.7 | 42.3 | 1.4 | 37.3 | 152.9 | 4.9 | 36.5 | 239.5 | 8.0 | 66.0 | 397.3 | 12.8 | 60.5 | 278.7 | 9.0 | 27.0 | 134.4 | 4.5 | 11.5 | 17.6 | 0.6 | 7.4 | 11.7 | 0.4 | 7.4 | 11.7 | 0.4 | 66.0 | 1373.8 | 0.0 | |
| 1989 | 31.3 | 47.4 | 1.5 | 9.7 | 10.7 | 0.4 | 5.8 | 12.1 | 0.4 | 3.3 | 4.0 | 0.1 | 46.0 | 148.7 | 4.8 | 29.3 | 135.5 | 4.5 | 57.0 | 328.0 | 10.6 | 27.0 | 206.0 | 6.6 | 38.7 | 196.5 | 6.6 | 18.9 | 42.4 | 1.4 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 57.0 | 1132.0 | 0.0 |
| 1990 | 0.0 | 0.0 | 0.0 | 18.0 | 42.2 | 1.5 | 15.3 | 59.5 | 1.9 | 26.2 | 116.2 | 3.9 | 73.2 | 108.3 | 3.5 | 47.0 | 285.5 | 9.5 | 56.4 | 345.6 | 11.1 | 53.8 | 308.5 | 10.0 | 39.2 | 188.2 | 6.3 | 48.2 | 78.7 | 2.5 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 73.2 | 1532.7 | 0.0 |
| 1991 | 14.6 | 20.7 | 0.7 | 10.0 | 11.4 | 0.4 | 19.2 | 45.2 | 1.5 | 17.1 | 26.3 | 0.9 | 42.8 | 145.3 | 4.7 | 24.4 | 114.4 | 3.8 | 36.9 | 190.3 | 6.1 | 44.7 | 280.7 | 9.1 | 27.6 | 137.7 | 4.6 | 0.4 | 0.4 | 0.0 | 0.2 | 0.2 | 0.0 | 21.5 | 24.9 | 0.8 | 44.7 | 997.5 | 0.0 | |
| Max | 31.3 | 11.1 | 0.4 | 25.0 | 18.4 | 0.7 | 34.2 | 1.1 | 55.2 | 1.8 | 73.2 | 100.0 | 86.5 | 349.4 | 11.3 | 294.5 | 9.5 | 69.0 | 191.7 | 6.4 | 124.4 | 63.0 | 2.0 | 18.0 | 51.0 | 124.4 | 18.1 | 18.1 | 0.5 | 124.4 | 1786.0 | 0.0 | 74.6 | 1370.9 | 0.0 | | | | | |
| Mean | 33.3 | 15.3 | 0.5 | 30.5 | 28.2 | 0.9 | 36.0 | 1.2 | 58.2 | 1.9 | 51.0 | 120.9 | 3.9 | 103.9 | 274.3 | 9.1 | 110.0 | 442.4 | 14.3 | 269.6 | 9.0 | 172.0 | 70.0 | 2.3 | 24.7 | 169.0 | 172.0 | 30.5 | 30.5 | 1.0 | 104.4 | 1890.0 | 0.0 | | | | | | | |

Table A.4.3.3 RAINFALL AT GODAVARI

| Year | Jan. | | Feb. | | Mar. | | Apr. | | May. | | Jun. | | Jul. | | Aug. | | Sep. | | Oct. | | Nov. | | Dec. | | Annual | | | | | | | | | | | | | | | | |
|------|------|------|------|------|------|------|------|------|------|------|-------|------|-------|-------|------|-------|-------|------|--------|-------|------|-------|-------|-------|--------|-------|------|-------|-------|------|------|------|------|------|-------|-------|--------|--------|-------|--------|-----|
| | max | mean | max | mean | max | mean | max | mean | max | mean | max | mean | max | mean | max | mean | max | mean | max | mean | max | mean | max | mean | max | Total | max | | | | | | | | | | | | | | |
| 1977 | 7.0 | 12.0 | 0.4 | 15.0 | 18.0 | 0.6 | 6.0 | 11.0 | 0.4 | 20.0 | 104.0 | 3.5 | 26.0 | 135.0 | 4.4 | 56.0 | 194.0 | 6.5 | 114.0 | 656.0 | 21.2 | 51.0 | 299.0 | 9.6 | 28.0 | 90.0 | 3.0 | 12.0 | 35.0 | 1.1 | 7.0 | 7.0 | 0.2 | 56.0 | 56.0 | 1.8 | 114.0 | 1617.0 | 0.0 | | |
| 1978 | 2.0 | 2.0 | 0.1 | 10.0 | 25.0 | 0.9 | 51.0 | 78.0 | 2.5 | 34.0 | 86.0 | 2.2 | 21.0 | 128.0 | 4.1 | 71.0 | 368.0 | 12.3 | 83.0 | 414.0 | 13.4 | 87.0 | 626.0 | 20.2 | 67.0 | 374.0 | 12.5 | 99.0 | 124.0 | 4.0 | 0.0 | 0.0 | 4.0 | 5.0 | 0.2 | 99.0 | 2211.0 | 0.0 | | | |
| 1979 | 5.0 | 6.0 | 0.2 | 30.0 | 32.0 | 1.9 | 1.0 | 1.0 | 0.0 | 16.0 | 48.0 | 1.6 | 24.0 | 64.0 | 2.1 | 81.0 | 330.0 | 11.0 | 97.0 | 548.0 | 17.7 | 93.0 | 345.0 | 11.1 | 21.0 | 70.0 | 2.3 | 14.0 | 34.0 | 1.1 | 5.0 | 7.0 | 0.2 | 63.0 | 79.0 | 2.5 | 97.0 | 1584.0 | 0.0 | | |
| 1980 | 0.0 | 0.0 | 0.0 | 7.0 | 12.0 | 0.4 | 8.0 | 25.0 | 0.8 | 15.0 | 19.0 | 0.6 | 31.0 | 111.0 | 3.6 | 103.0 | 440.0 | 14.7 | 88.0 | 439.0 | 14.2 | 45.0 | 390.0 | 12.6 | 54.0 | 75.0 | 2.5 | 16.0 | 31.0 | 1.0 | 0.0 | 0.0 | 0.0 | 6.0 | 6.0 | 0.2 | 103.0 | 1548.0 | 0.0 | | |
| 1981 | 10.0 | 30.0 | 1.0 | 0.0 | 0.0 | 12.0 | 45.0 | 1.5 | 24.0 | 96.0 | 3.2 | 24.0 | 138.0 | 4.5 | 32.0 | 186.0 | 6.2 | 36.0 | 420.0 | 11.3 | 58.0 | 350.0 | 11.3 | 169.0 | 413.0 | 13.8 | 0.0 | 0.0 | 0.0 | 18.0 | 20.0 | 0.7 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 169.0 | 1698.0 | 0.0 |
| 1982 | 10.0 | 15.0 | 0.5 | 6.0 | 16.0 | 0.6 | 31.0 | 55.0 | 1.8 | 16.0 | 44.0 | 1.5 | 20.0 | 80.0 | 2.6 | 55.0 | 304.0 | 10.1 | 84.0 | 375.0 | 12.1 | 65.0 | 523.0 | 16.9 | 66.0 | 229.0 | 7.6 | 6.0 | 11.0 | 0.4 | 14.0 | 18.0 | 0.6 | 2.0 | 2.0 | 0.1 | 68.0 | 1672.0 | 0.0 | | |
| 1983 | 18.0 | 21.0 | 0.7 | 4.0 | 8.0 | 0.3 | 7.0 | 7.0 | 0.2 | 17.0 | 59.0 | 2.0 | 51.0 | 214.0 | 6.9 | 23.0 | 91.0 | 3.0 | 84.0 | 387.0 | 18.9 | 65.0 | 455.0 | 14.7 | 48.0 | 298.0 | 9.9 | 56.0 | 164.0 | 5.3 | 0.0 | 0.0 | 14.0 | 14.0 | 0.5 | 84.0 | 1918.0 | 0.0 | | | |
| 1984 | 26.0 | 26.0 | 0.8 | 17.0 | 20.0 | 0.7 | 12.0 | 12.0 | 0.0 | 0.0 | 0.0 | 0.0 | 16.0 | 27.0 | 0.9 | 42.0 | 226.0 | 7.5 | 120.0 | 847.0 | 14.5 | 61.0 | 490.0 | 15.8 | 110.0 | 538.0 | 17.9 | 25.0 | 28.0 | 0.9 | 0.0 | 0.0 | 10.0 | 11.0 | 0.4 | 110.0 | 2214.0 | 0.0 | | | |
| 1985 | 9.0 | 20.0 | 0.6 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 16.0 | 27.0 | 0.9 | 42.0 | 226.0 | 7.5 | 120.0 | 847.0 | 14.5 | 61.0 | 490.0 | 15.8 | 110.0 | 538.0 | 17.9 | 25.0 | 28.0 | 0.9 | 0.0 | 0.0 | 10.0 | 11.0 | 0.4 | 110.0 | 2214.0 | 0.0 | | | |
| 1986 | 0.0 | 0.0 | 0.0 | 20.0 | 24.0 | 0.9 | 10.0 | 26.0 | 0.8 | 24.0 | 85.0 | 2.8 | 35.0 | 133.0 | 4.3 | 80.0 | 461.0 | 15.4 | 96.0 | 432.0 | 13.9 | 60.0 | 316.0 | 10.2 | 51.0 | 314.0 | 10.5 | 13.0 | 56.0 | 1.8 | 3.0 | 3.0 | 0.1 | 56.0 | 60.0 | 1.9 | 96.0 | 1910.0 | 0.0 | | |
| 1987 | 2.0 | 3.0 | 0.1 | 30.5 | 74.9 | 2.7 | 19.8 | 60.5 | 2.0 | 23.5 | 56.3 | 1.9 | 12.6 | 38.2 | 1.2 | 79.0 | 198.5 | 6.6 | 83.6 | 801.1 | 22.8 | 86.4 | 430.2 | 13.9 | 46.0 | 181.9 | 6.1 | 172.0 | 201.0 | 6.5 | 0.0 | 0.0 | 15.0 | 15.5 | 0.5 | 172.0 | 2061.1 | 0.0 | | | |
| 1988 | 2.0 | 3.0 | 0.1 | 16.0 | 25.0 | 0.9 | 28.9 | 81.3 | 2.6 | 23.2 | 68.8 | 2.3 | 21.7 | 125.4 | 4.0 | 48.5 | 279.5 | 9.3 | 37.5 | 465.1 | 15.0 | 52.5 | 323.7 | 16.9 | 53.5 | 233.7 | 8.5 | 14.0 | 15.3 | 0.5 | 24.7 | 30.7 | 1.0 | 63.5 | 102.2 | 3.3 | 63.5 | 1973.7 | 0.0 | | |
| 1989 | 33.3 | 53.0 | 1.7 | 9.7 | 12.3 | 0.4 | 11.3 | 16.3 | 0.5 | 2.8 | 2.8 | 0.1 | 30.2 | 155.3 | 5.0 | 27.7 | 150.0 | 5.0 | 61.8</ | | | | | | | | | | | | | | | | | | | | | | |

Table A4.3.4 TEMPERATURE AT KATHMANDU AIRPORT

| Year | Jan. | | Feb. | | Mar. | | Apr. | | May. | | Jun. | | Jul. | | Aug. | | Sep. | | Oct. | | Nov. | | Dec. | | Mean in Year | | | | | | | | | | | | |
|------|------|------|------|------|------|------|------|-----|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|--------------|------|------|------|------|------|------|-----|------|------|-----|------|------|
| | max | min | max | min | max | min | max | min | max | min | max | min | max | min | max | min | max | min | max | min | max | min | max | min | | max | min | | | | | | | | | | |
| 1977 | 16.8 | 0.5 | 8.7 | 20.3 | 3.0 | 11.7 | 25.4 | 7.1 | 16.3 | 25.0 | 11.3 | 18.2 | 25.7 | 13.5 | 19.6 | 27.9 | 17.6 | 22.8 | 27.8 | 19.7 | 23.8 | 27.6 | 19.0 | 23.3 | 27.1 | 17.4 | 22.3 | 24.0 | 11.6 | 17.8 | 21.7 | 8.6 | 15.2 | 17.6 | 2.2 | 9.9 | 17.4 |
| 1978 | 16.1 | -0.4 | 7.9 | 18.7 | 2.0 | 10.4 | 21.6 | 5.1 | 13.4 | 25.6 | 10.4 | 18.0 | 27.2 | 17.0 | 22.1 | 27.4 | 19.2 | 23.3 | 27.4 | 19.8 | 23.6 | 28.4 | 20.0 | 24.2 | 26.7 | 18.5 | 22.6 | 24.6 | 13.8 | 19.2 | 21.0 | 9.0 | 15.0 | 19.8 | 3.3 | 11.6 | 17.6 |
| 1979 | 18.4 | 2.5 | 10.5 | 18.8 | 4.1 | 11.5 | 24.0 | 6.2 | 15.1 | 27.4 | 12.6 | 20.0 | 30.4 | 15.6 | 23.0 | 28.9 | 19.2 | 24.1 | 27.7 | 20.5 | 24.1 | 27.2 | 20.1 | 23.7 | 26.7 | 17.6 | 22.2 | 24.9 | 13.3 | 19.1 | 22.7 | 9.8 | 16.3 | 17.9 | 5.0 | 11.5 | 18.4 |
| 1980 | 17.5 | 1.9 | 9.7 | 19.5 | 4.9 | 12.2 | 23.0 | 8.0 | 15.5 | 29.4 | 12.1 | 20.8 | 28.2 | 16.9 | 22.6 | 27.8 | 20.2 | 24.0 | 27.8 | 20.8 | 24.3 | 27.8 | 20.4 | 24.1 | 26.9 | 19.0 | 23.0 | 24.5 | 12.1 | 18.3 | 22.4 | 7.2 | 14.8 | 19.3 | 4.1 | 11.7 | 18.4 |
| 1981 | 16.8 | 2.9 | 9.9 | 20.3 | 4.8 | 12.6 | 22.2 | 8.2 | 15.2 | 24.2 | 12.5 | 18.4 | 26.1 | 16.3 | 21.2 | 28.0 | 19.1 | 23.6 | 27.0 | 20.6 | 23.8 | 27.8 | 20.4 | 24.1 | 26.7 | 18.6 | 22.7 | 25.6 | 13.3 | 19.5 | 22.7 | 6.8 | 14.8 | 19.4 | 2.1 | 10.8 | 18.0 |
| 1982 | 18.9 | 2.8 | 10.9 | 18.5 | 3.5 | 11.0 | 22.8 | 7.5 | 15.2 | 26.5 | 10.9 | 18.7 | 29.9 | 14.4 | 22.2 | 28.5 | 18.5 | 23.5 | 28.7 | 19.6 | 24.2 | 28.9 | 20.2 | 24.6 | 27.3 | 17.8 | 22.6 | 25.6 | 11.2 | 18.4 | 21.3 | 7.9 | 14.6 | 18.8 | 3.9 | 11.4 | 18.1 |
| 1983 | 17.1 | 0.1 | 8.6 | 20.7 | 2.4 | 11.6 | 26.0 | 8.3 | 17.2 | 28.3 | 11.2 | 19.8 | 27.5 | 17.1 | 22.3 | 28.2 | 20.0 | 24.1 | 28.1 | 20.3 | 24.2 | 29.2 | 19.8 | 24.5 | 26.3 | 17.3 | 21.8 | 27.2 | 14.4 | 20.8 | 22.6 | 5.8 | 14.2 | 19.4 | 3.4 | 11.4 | 18.4 |
| 1984 | 16.7 | 1.0 | 8.9 | 19.0 | 1.6 | 10.3 | 23.4 | 5.8 | 14.6 | 25.1 | 10.2 | 17.7 | 26.8 | 15.3 | 21.1 | 30.4 | 18.1 | 24.3 | 28.3 | 20.5 | 24.4 | 28.7 | 20.2 | 24.5 | 27.8 | 19.1 | 23.5 | 26.0 | 13.7 | 19.9 | 22.9 | 7.0 | 15.0 | 18.9 | 1.5 | 10.2 | 17.8 |
| 1985 | 18.1 | 2.4 | 10.3 | 20.1 | 3.7 | 11.9 | 26.3 | 9.0 | 17.7 | 28.6 | 12.1 | 20.4 | 28.0 | 15.5 | 21.8 | 28.9 | 19.2 | 24.1 | 27.1 | 19.6 | 23.4 | 28.8 | 20.2 | 24.5 | 26.7 | 18.3 | 22.5 | 24.4 | 13.7 | 19.1 | 22.2 | 7.0 | 14.6 | 19.3 | 4.8 | 12.1 | 18.5 |
| 1986 | 18.3 | 2.7 | 10.5 | 20.1 | 3.5 | 11.8 | 24.6 | 7.2 | 15.9 | 26.4 | 11.1 | 18.8 | 27.1 | 13.9 | 20.5 | 28.9 | 18.9 | 23.9 | 28.2 | 20.1 | 24.2 | 28.7 | 19.5 | 24.1 | 26.9 | 18.0 | 22.5 | 24.8 | 12.3 | 18.6 | 22.3 | 8.1 | 15.2 | 18.7 | 2.8 | 10.8 | 18.0 |
| 1987 | 18.5 | 2.4 | 10.5 | 20.6 | 5.3 | 13.0 | 23.2 | 8.0 | 15.6 | 27.1 | 10.9 | 19.0 | 29.1 | 13.4 | 21.3 | 28.8 | 19.0 | 23.9 | 27.6 | 20.1 | 23.9 | 27.5 | 19.4 | 23.5 | 27.4 | 18.4 | 22.9 | 25.6 | 12.9 | 19.3 | 23.4 | 7.8 | 15.6 | 20.6 | 4.2 | 12.4 | 18.4 |
| 1988 | 19.1 | 3.0 | 11.1 | 21.6 | 5.3 | 13.5 | 23.9 | 7.6 | 15.8 | 28.6 | 10.9 | 19.8 | 28.9 | 15.7 | 22.3 | 28.4 | 18.5 | 23.5 | 28.3 | 19.9 | 24.1 | 27.9 | 19.7 | 23.8 | 28.6 | 18.5 | 23.6 | 28.4 | 13.3 | 20.9 | 24.4 | 6.4 | 15.4 | 20.3 | 5.0 | 12.7 | 18.8 |
| 1989 | 17.5 | 2.7 | 10.1 | 21.7 | 2.3 | 12.0 | 25.6 | 7.0 | 16.3 | 30.0 | 8.6 | 19.3 | 29.7 | 15.6 | 22.7 | 29.4 | 18.9 | 24.2 | 28.1 | 19.5 | 23.8 | 29.5 | 19.2 | 24.4 | 28.9 | 18.6 | 23.8 | 28.6 | 13.3 | 21.0 | 23.7 | 6.0 | 14.9 | 20.7 | 1.8 | 11.3 | 18.6 |
| 1990 | 22.2 | 3.2 | 12.7 | 19.9 | 5.2 | 12.6 | 22.1 | 7.0 | 14.6 | 26.2 | 10.8 | 18.5 | 27.1 | 16.1 | 21.6 | 29.2 | 19.6 | 24.4 | 27.6 | 20.1 | 23.9 | 28.3 | 19.4 | 23.9 | 27.5 | 18.5 | 23.0 | 25.6 | 13.0 | 19.3 | 24.4 | 7.3 | 15.9 | 20.2 | 3.7 | 12.0 | 18.5 |
| Mean | 18.0 | 2.0 | 10.0 | 20.0 | 3.7 | 11.8 | 23.9 | 7.3 | 15.6 | 27.0 | 11.1 | 19.1 | 28.0 | 15.5 | 21.7 | 28.6 | 19.0 | 23.8 | 27.8 | 20.1 | 24.0 | 28.3 | 19.8 | 24.1 | 27.3 | 18.3 | 22.8 | 25.7 | 13.0 | 19.3 | 22.7 | 7.5 | 15.1 | 19.4 | 3.4 | 11.4 | 18.2 |
| Max | 22.2 | | 21.7 | | | | 26.3 | | | 30.4 | | | 30.4 | | | 30.4 | | | 28.7 | | 29.5 | | | 28.9 | | | 28.6 | | 28.6 | | 24.4 | | | 20.7 | | | |
| Mini | -0.4 | | 1.6 | | | | 5.1 | | 8.6 | | | 17.6 | | 19.5 | | 19 | | | 19.5 | | 19 | | | 17.3 | | | 11.2 | | 11.2 | | 5.8 | | | 1.5 | | | |

Table A4.3.5 RELATIVE HUMIDITY AT KATHMANDU AIRPORT

| Year | Jan. | | Feb. | | Mar. | | Apr. | | May. | | Jun. | | Jul. | | Aug. | | Sep. | | Oct. | | Nov. | | Dec. | | Mean in Year | | | | | | | | | | | | |
|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|--------------|------|------|------|------|------|------|------|------|------|------|------|------|
| | max | min | max | min | max | min | max | min | max | min | max | min | max | min | max | min | max | min | max | min | max | min | max | min | | max | min | | | | | | | | | | |
| 1977 | 96.0 | 66.0 | 81.0 | 90.0 | 50.0 | 70.0 | 79.0 | 46.0 | 62.5 | 78.0 | 57.0 | 67.5 | 78.0 | 58.0 | 68.0 | 77.0 | 71.0 | 74.0 | 86.0 | 80.0 | 83.0 | 86.0 | 80.0 | 83.0 | 86.0 | 76.0 | 81.0 | 89.0 | 72.0 | 80.5 | 91.0 | 75.0 | 83.0 | 96.0 | 73.0 | 84.5 | 76.5 |
| 1978 | 94.0 | 65.0 | 79.5 | 92.0 | 59.0 | 75.5 | 83.0 | 51.0 | 67.0 | 81.0 | 54.0 | 64.5 | 81.0 | 67.0 | 74.0 | 83.0 | 74.0 | 78.5 | 90.0 | 65.0 | 77.5 | 90.0 | 82.0 | 89.0 | 96.0 | 80.0 | 85.0 | 94.0 | 75.0 | 84.5 | 95.0 | 77.0 | 86.0 | 97.0 | 65.0 | 81.0 | 77.9 |
| 1979 | 99.0 | 66.0 | 82.5 | 96.0 | 61.0 | 78.5 | 85.0 | 41.0 | 63.0 | 92.0 | 56.0 | 74.0 | 87.0 | 46.0 | 66.5 | 90.0 | 65.0 | 77.5 | 94.0 | 80.0 | 87.0 | 96.0 | 82.0 | 89.0 | 96.0 | 75.0 | 85.5 | 98.0 | 76.0 | 87.0 | 97.0 | 72.0 | 84.5 | 97.0 | 74.0 | 85.5 | 80.6 |
| 1980 | 95.0 | 64.0 | 79.5 | 90.0 | 52.0 | 71.0 | 80.0 | 50.0 | 65.0 | 85.0 | 41.0 | 53.0 | 72.0 | 58.0 | 65.0 | 82.0 | 74.0 | 78.0 | 84.0 | 78.0 | 81.0 | 84.0 | 77.0 | 80.5 | 88.0 | 79.0 | 83.5 | 91.0 | 72.0 | 81.5 | 92.0 | 72.0 | 82.0 | 97.0 | 68.0 | 82.5 | 75.2 |
| 1981 | 96.0 | 65.0 | 80.5 | 90.0 | 55.0 | 72.5 | 84.0 | 57.0 | 70.5 | 78.0 | 56.0 | 67.0 | 80.0 | 66.0 | 73.0 | 89.0 | 68.0 | 73.5 | 86.0 | 81.0 | 83.5 | 85.0 | 78.0 | 81.5 | 89.0 | 75.0 | 82.0 | 91.0 | 67.0 | 81.5 | 95.0 | 78.0 | 86.5 | 97.0 | 73.0 | 85.0 | 77.9 |
| 1982 | 97.0 | 67.0 | 82.0 | 95.0 | 62.0 | 78.5 | 88.0 | 52.0 | 66.0 | 71.0 | 47.0 | 59.0 | 61.0 | 44.0 | 52.5 | 76.0 | 67.0 | 71.5 | 83.0 | 71.0 | 77.0 | 83.0 | 81.0 | 82.0 | 88.0 | 79.0 | 83.5 | 93.0 | 71.0 | 82.0 | 95.0 | 77.0 | 86.0 | 97.0 | 70.0 | 83.5 | 75.3 |
| 1983 | 94.0 | 68.0 | 81.0 | 91.0 | 65.0 | 78.0 | 81.0 | 61.0 | 71.0 | 78.0 | 60.0 | 69.0 | 77.0 | 73.0 | 75.0 | 73.0 | 64.0 | 68.5 | 87.0 | 83.0 | 85.0 | 82.0 | 81.0 | 81.5 | 85.0 | 80.0 | 82.5 | 89.0 | 76.0 | 82.5 | 98.0 | 72.0 | 85.0 | 98.0 | 70.0 | 84.0 | 78.6 |
| 1984 | 96.0 | 62.0 | 79.0 | 95.0 | 52.0 | 73.5 | 81.0 | 48.0 | 64.5 | 66.0 | 43.0 | 54.5 | 78.0 | 68.0 | 73.0 | 82.0 | 77.0 | 79.5 | 85.0 | 82.0 | 83.5 | 82.0 | 79.0 | 80.5 | 90.0 | 78.0 | 84.0 | 88.0 | 71.0 | 79.5 | 89.0 | 64.0 | 76.5 | 93.0 | 67.0 | 80.0 | 75.7 |
| 1985 | 94.0 | 66.0 | 80.0 | 90.0 | 58.0 | 74.0 | 74.0 | 41.0 | 57.5 | 65.0 | 38.0 | 51.5 | 72.0 | 58.0 | 65.0 | 76.0 | 68.0 | 72.0 | 84.0 | 82.0 | 83.0 | 84.0 | 79.0 | 81.5 | 87.0 | 79.0 | 83.0 | 91.0 | 77.0 | 84.0 | 98.0 | 72.0 | 85.0 | 97.0 | 72.0 | 84.5 | 75.1 |
| 1986 | 97.0 | 65.0 | 81.0 | 96.0 | 58.0 | 77.0 | 79.0 | 43.0 | 61.0 | 74.0 | 54.0 | 64.0 | 73.0 | 58.0 | 65.0 | 79.0 | 71.0 | 75.0 | 84.0 | 81.0 | 82.5 | 84.0 | 78.0 | 81.0 | 87.0 | 81.0 | 84.0 | 93.0 | 71.0 | 82.0 | 97.0 | 72.0 | 84.5 | 98.0 | 68.0 | 83.0 | 76.7 |
| 1987 | 97.7 | 64.5 | 81.1 | 95.8 | 58.0 | 76.9 | 93.2 | 58.4 | 75.8 | 74.8 | 50.8 | 62.8 | 65.0 | 50.5 | 57.8 | 75.6 | 70.2 | 72.9 | 86.2 | 84.8 | 85.5 | 87.3 | 79.4 | 83.4 | 87.3 | 76.9 | 82.1 | 92.3 | 75.9 | 83.1 | 96.1 | 68.7 | 82.4 | 96.6 | 64.3 | 80.5 | 77.0 |
| 1988 | 96.3 | 57.8 | 77.1 | 92.2 | 52.6 | 72.4 | 86.3 | 49.5 | 67.9 | 69.6 | 45.0 | 57.3 | 75.1 | 58.6 | 66.9 | 78.8 | 70.9 | 74.9 | 83.4 | 80.7 | 82.1 | 87.6 | 80.2 | 83.9 | 87.3 | 74.8 | 81.1 | 91.5 | 73.0 | 82.3 | 91.6 | 60.2 | 75.9 | 93.3 | 67.2 | 80.3 | 75.1 |
| 1989 | 96.1 | 72.2 | 84.2 | 93.9 | 56.3 | 75.1 | 82.5 | 45.4 | 64.0 | 61.8 | 30.7 | 46.3 | 69.7 | 60.8 | 65.3 | 75.6 | 71.4 | 73.5 | 83.9 | 79.1 | 81.5 | 85.4 | 77.9 | 81.7 | 85.8 | 79.6 | 82.7 | 89.6 | 74.5 | 82.1 | 94.0 | 67.3 | 80.7 | 94.5 | 66.9 | 80.7 | 74.8 |
| 1990 | 95.6 | 64.8 | 80.2 | 95.5 | 59.3 | 76.7 | 81.1 | 84.7 | 53.5 | 69.1 | 76.5 | 66.8 | 75.4 | 62.2 | 68.8 | 77.5 | 74.1 | 75.8 | 84.4 | 81.8 | 83.1 | 86.1 | 78.1 | 76.2 | 86.9 | 77.3 | 82.1 | 87.0 | 71.9 | 79.5 | 92.4 | 62.6 | 77.5 | 95.4 | 61.2 | 78.3 | 76.1 |
| Mean | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |

Table A.4.3.6 TEMPERATURE AT GODAVARI

| Year | Jan. | | Feb. | | Mar. | | Apr. | | May. | | Jun. | | Jul. | | Aug. | | Sep. | | Oct. | | Nov. | | Dec. | | Mean in Year | | | | | | | | | | | | | |
|------|------|-----|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|--------------|------|------|------|------|------|------|-----|------|------|-----|------|------|--|
| | max | min | max | min | max | min | max | min | max | min | max | min | max | min | max | min | max | min | max | min | max | min | max | min | | max | min | | | | | | | | | | | |
| 1977 | 14.2 | 2.1 | 8.2 | 17.4 | 4.3 | 10.9 | 23.0 | 10.6 | 16.8 | 23.0 | 12.2 | 17.6 | 25.6 | 15.7 | 20.7 | 24.8 | 17.6 | 21.2 | 25.0 | 17.0 | 21.0 | 24.2 | 16.2 | 20.2 | 21.1 | 12.2 | 16.7 | 18.7 | 9.1 | 13.9 | 15.0 | 4.7 | 9.9 | 16.1 | | | | |
| 1978 | 12.9 | 2.0 | 7.5 | 15.9 | 4.4 | 10.2 | 18.6 | 7.6 | 13.1 | 23.4 | 11.7 | 17.6 | 24.7 | 17.4 | 21.1 | 24.8 | 12.6 | 18.7 | 25.1 | 18.1 | 21.6 | 23.8 | 16.0 | 19.9 | 22.2 | 12.4 | 17.3 | 18.4 | 8.2 | 13.3 | 16.8 | 4.3 | 10.8 | 15.9 | | | | |
| 1979 | 15.3 | 3.9 | 9.6 | 15.6 | 4.3 | 10.0 | 21.2 | 7.2 | 14.2 | 24.8 | 12.2 | 18.5 | 27.6 | 14.8 | 21.2 | 26.3 | 17.4 | 21.9 | 25.0 | 18.4 | 21.7 | 24.1 | 15.6 | 19.9 | 21.6 | 12.2 | 16.9 | 19.5 | 9.9 | 14.7 | 14.1 | 4.8 | 9.5 | 16.6 | | | | |
| 1980 | 13.9 | 2.9 | 8.4 | 16.0 | 4.9 | 10.5 | 20.3 | 8.2 | 14.3 | 27.1 | 13.0 | 20.1 | 25.7 | 14.9 | 20.3 | 24.9 | 18.1 | 21.5 | 24.5 | 18.5 | 21.5 | 24.2 | 18.1 | 21.2 | 21.9 | 16.0 | 19.0 | 19.7 | 10.5 | 15.1 | 18.4 | 7.9 | 13.2 | 15.2 | 5.4 | 10.3 | 16.3 | |
| 1981 | 13.0 | 3.9 | 8.5 | 17.6 | 6.1 | 11.9 | 19.6 | 8.7 | 14.2 | 22.0 | 11.8 | 16.9 | 23.9 | 14.7 | 19.3 | 25.8 | 17.5 | 21.7 | 24.0 | 18.9 | 21.5 | 24.7 | 18.5 | 21.5 | 23.5 | 16.8 | 20.2 | 22.1 | 12.5 | 17.3 | 17.7 | 7.6 | 12.7 | 13.7 | 4.3 | 9.0 | 16.2 | |
| 1982 | 15.1 | 3.7 | 9.4 | 14.8 | 4.1 | 9.5 | 19.2 | 8.4 | 13.8 | 23.3 | 11.7 | 17.5 | 26.3 | 15.1 | 20.7 | 25.2 | 17.6 | 21.4 | 24.9 | 18.4 | 21.7 | 23.2 | 16.7 | 20.0 | 21.3 | 11.9 | 16.6 | 16.8 | 8.5 | 12.7 | 14.4 | 4.9 | 9.7 | 16.2 | | | | |
| 1983 | 12.5 | 2.7 | 7.6 | 15.4 | 3.4 | 9.4 | 20.9 | 8.0 | 14.5 | 22.8 | 11.3 | 17.1 | 24.0 | 14.3 | 19.2 | 26.9 | 17.5 | 22.2 | 25.2 | 18.6 | 21.9 | 24.9 | 18.5 | 21.7 | 23.9 | 17.5 | 20.7 | 21.2 | 13.1 | 17.2 | 17.3 | 8.3 | 12.8 | 13.9 | 3.4 | 8.7 | 16.1 | |
| 1984 | 12.9 | 1.8 | 7.4 | 16.7 | 4.1 | 10.4 | 22.3 | 9.8 | 16.1 | 24.9 | 12.5 | 18.7 | 24.5 | 16.0 | 20.3 | 25.0 | 18.4 | 21.7 | 23.8 | 18.6 | 21.2 | 24.9 | 17.9 | 21.4 | 22.3 | 15.6 | 19.0 | 22.2 | 13.9 | 18.1 | 17.1 | 7.5 | 12.3 | 14.6 | 4.3 | 9.5 | 16.3 | |
| 1985 | 13.8 | 3.5 | 8.7 | 16.2 | 4.6 | 10.4 | 23.4 | 10.7 | 17.1 | 25.6 | 13.6 | 19.6 | 24.9 | 14.6 | 19.8 | 25.7 | 17.8 | 21.8 | 23.2 | 18.3 | 20.8 | 24.9 | 18.7 | 21.8 | 22.6 | 16.6 | 19.6 | 20.5 | 13.1 | 16.8 | 17.2 | 7.7 | 12.5 | 14.8 | 5.0 | 9.9 | 16.5 | |
| 1986 | 13.8 | 3.6 | 8.7 | 16.5 | 5.0 | 10.8 | 20.9 | 8.6 | 14.8 | 23.4 | 11.7 | 17.6 | 24.1 | 13.5 | 18.8 | 25.6 | 18.3 | 22.0 | 24.7 | 16.0 | 20.4 | 25.0 | 14.9 | 20.9 | 22.7 | 13.4 | 18.1 | 20.4 | 10.2 | 15.3 | 17.3 | 8.4 | 12.9 | 14.5 | 4.3 | 9.4 | 15.7 | |
| 1987 | 14.3 | 3.9 | 9.1 | 16.7 | 5.9 | 11.3 | 19.5 | 8.2 | 13.9 | 24.0 | 12.1 | 18.1 | 26.0 | 15.0 | 20.6 | 24.1 | 15.7 | 19.9 | 24.2 | 15.2 | 19.7 | 23.8 | 15.8 | 19.8 | 21.3 | 12.2 | 16.8 | 18.3 | 7.3 | 12.8 | 15.8 | 4.4 | 10.1 | 16.0 | | | | |
| 1988 | 14.7 | 4.1 | 9.4 | 17.2 | 5.7 | 11.5 | 20.3 | 8.0 | 14.2 | 25.1 | 11.4 | 18.3 | 25.4 | 15.4 | 20.4 | 25.2 | 17.8 | 21.5 | 24.8 | 19.1 | 22.0 | 24.1 | 18.6 | 21.4 | 24.4 | 17.4 | 20.9 | 22.8 | 12.8 | 17.8 | 18.8 | 7.4 | 13.1 | 15.5 | 5.7 | 10.6 | 16.7 | |
| 1989 | 12.7 | 3.0 | 7.9 | 16.5 | 3.5 | 10.0 | 20.8 | 8.5 | 14.7 | 25.9 | 11.9 | 18.9 | 26.0 | 16.0 | 21.0 | 23.6 | 17.8 | 21.7 | 24.5 | 18.4 | 21.5 | 24.4 | 18.2 | 21.3 | 23.5 | 17.5 | 20.5 | 22.3 | 13.1 | 17.7 | 17.6 | 7.3 | 12.5 | 14.7 | 3.8 | 9.3 | 16.4 | |
| 1990 | 16.4 | 5.5 | 11.0 | 15.1 | 5.4 | 10.3 | 18.2 | 7.3 | 12.8 | 23.4 | 11.1 | 17.3 | 24.3 | 15.1 | 19.7 | 26.6 | 18.6 | 22.6 | 24.0 | 18.9 | 21.5 | 24.7 | 18.6 | 21.7 | 23.7 | 17.5 | 20.6 | 21.1 | 12.7 | 16.9 | 19.5 | 8.8 | 14.2 | 15.8 | 5.5 | 10.7 | 16.6 | |
| Mean | 14.0 | 3.3 | 8.6 | 16.3 | 4.7 | 10.5 | 20.6 | 8.4 | 14.5 | 24.2 | 11.9 | 18.0 | 25.1 | 14.7 | 19.9 | 25.7 | 17.5 | 21.6 | 24.5 | 17.7 | 21.1 | 24.7 | 17.8 | 21.2 | 23.4 | 16.3 | 19.9 | 21.4 | 12.3 | 16.9 | 18.0 | 8.1 | 13.1 | 14.9 | 4.7 | 9.8 | 16.3 | |
| Max | 16.4 | | | 17.6 | | 3.4 | | | 7.2 | | | 23.4 | | | 27.6 | | | 25.1 | | | 24.4 | | | 24.4 | | | 22.8 | | | 19.5 | | | 16.8 | | | 3.4 | | |
| Min | 1.8 | | | 17.6 | | 3.4 | | | 7.2 | | | 23.4 | | | 27.6 | | | 25.1 | | | 24.4 | | | 24.4 | | | 22.8 | | | 19.5 | | | 16.8 | | | 3.4 | | |

Table A.4.3.7 RELATIVE HUMIDITY AT GODAVARI

| Year | Jan | | Feb. | | Mar. | | Apr. | | May. | | Jun. | | Jul. | | Aug. | | Sep. | | Oct. | | Nov. | | Dec. | | Mean in Year | |
|------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|--------------|-------|
| | '0845 | '0845 | '0845 | '0845 | '0845 | '0845 | '0845 | '0845 | '0845 | '0845 | '0845 | '0845 | '0845 | '0845 | '0845 | '0845 | '0845 | '0845 | '0845 | '0845 | '0845 | '0845 | '0845 | '0845 | | '0845 |
| 1977 | 78.0 | 72.0 | 75.0 | 75.0 | 67.0 | 66.0 | 66.0 | 66.0 | 69.0 | 74.0 | 74.0 | 78.0 | 84.0 | 85.0 | 81.0 | 81.0 | 81.0 | 81.0 | 81.0 | 81.0 | 82.0 | 82.0 | 82.0 | 82.0 | 81.0 | 76.2 |
| 1978 | 75.0 | 72.0 | 72.0 | 72.0 | 66.0 | 64.0 | 64.0 | 64.0 | 66.0 | 69.0 | 69.0 | 83.0 | 85.0 | 83.0 | 83.0 | 84.0 | 81.0 | 81.0 | 81.0 | 81.0 | 82.0 | 82.0 | 82.0 | 82.0 | 82.0 | 75.8 |
| 1979 | 76.0 | 78.0 | 78.0 | 78.0 | 65.0 | 57.0 | 57.0 | 57.0 | 60.0 | 69.0 | 69.0 | 83.0 | 89.0 | 89.0 | 89.0 | 90.0 | 90.0 | 90.0 | 90.0 | 90.0 | 90.0 | 90.0 | 90.0 | 90.0 | 90.0 | 73.4 |
| 1980 | 85.0 | 81.0 | 81.0 | 81.0 | 78.0 | 78.0 | 78.0 | 78.0 | 80.0 | 81.0 | 81.0 | 92.0 | 93.0 | 93.0 | 92.0 | 92.0 | 91.0 | 91.0 | 91.0 | 91.0 | 91.0 | 91.0 | 91.0 | 91.0 | 91.0 | 77.5 |
| 1982 | 77.0 | 79.0 | 79.0 | 79.0 | 77.0 | 69.0 | 69.0 | 69.0 | 65.0 | 85.0 | 85.0 | 86.0 | 86.0 | 86.0 | 86.0 | 86.0 | 86.0 | 86.0 | 86.0 | 86.0 | 86.0 | 86.0 | 86.0 | 86.0 | 86.0 | 83.4 |
| 1983 | 80.0 | 75.0 | 75.0 | 75.0 | 70.0 | 68.0 | 68.0 | 68.0 | 82.0 | 80.0 | 80.0 | 95.0 | 95.0 | 95.0 | 95.0 | 94.0 | 93.0 | 93.0 | 93.0 | 93.0 | 93.0 | 93.0 | 93.0 | 93.0 | 93.0 | 80.6 |
| 1984 | 74.0 | 70.0 | 70.0 | 70.0 | 80.0 | 72.0 | 72.0 | 72.0 | 84.0 | 90.0 | 90.0 | 94.0 | 94.0 | 94.0 | 94.0 | 94.0 | 94.0 | 94.0 | 94.0 | 94.0 | 94.0 | 94.0 | 94.0 | 94.0 | 94.0 | 81.7 |
| 1985 | 83.0 | 84.0 | 84.0 | 84.0 | 71.0 | 68.0 | 68.0 | 68.0 | 82.0 | 86.0 | 86.0 | 95.0 | 95.0 | 95.0 | 95.0 | 93.0 | 93.0 | 93.0 | 93.0 | 93.0 | 93.0 | 93.0 | 93.0 | 93.0 | 93.0 | 83.4 |
| 1986 | 83.0 | 78.0 | 78.0 | 78.0 | 73.0 | 74.0 | 74.0 | 74.0 | 79.0 | 85.0 | 85.0 | 91.0 | 91.0 | 91.0 | 91.0 | 86.0 | 86.0 | 86.0 | 86.0 | 86.0 | 86.0 | 86.0 | 86.0 | 86.0 | 86.0 | 84.8 |
| 1987 | 82.1 | 81.1 | 81.1 | 81.1 | 84.9 | 72.1 | 72.1 | 72.1 | 65.7 | 91.1 | 91.1 | 92.3 | 92.3 | 92.3 | 92.3 | 90.6 | 90.6 | 90.6 | 90.6 | 90.6 | 90.6 | 90.6 | 90.6 | 90.6 | 90.6 | 82.6 |
| 1988 | 84.1 | 82.2 | 82.2 | 82.2 | 81.4 | 72.2 | 72.2 | 72.2 | 84.8 | 91.1 | 91.1 | 95.1 | 95.1 | 95.1 | 95.1 | 94.9 | 94.9 | 94.9 | 94.9 | 94.9 | 94.9 | 94.9 | 94.9 | 94.9 | 94.9 | 82.7 |
| 1989 | 86.2 | 86.2 | 86.2 | 86.2 | 76.2 | 63.0 | 63.0 | 63.0 | 76.7 | 86.5 | 86.5 | 88.2 | 88.2 | 88.2 | 88.2 | 86.5 | 86.5 | 86.5 | 86.5 | 86.5 | 86.5 | 86.5 | 86.5 | 86.5 | 86.5 | 85.9 |
| 1990 | 85.3 | 81.0 | 81.0 | 81.0 | 81.1 | 76.2 | 76.2 | 76.2 | 84.8 | 87.9 | 87.9 | 93.3 | 93.3 | 93.3 | 93.3 | 93.9 | 93.9 | 93.9 | 93.9 | 93.9 | 93.9 | 93.9 | 93.9 | 93.9 | 93.9 | 81.9 |
| Mean | 80.3 | 77.1 | 77.1 | 77.1 | 73.3 | 67.8 | 67.8 | 67.8 | 75.5 | 83.0 | 83.0 | 89.1 | 89.1 | 89.1 | 89.1 | 87.7 | 87.7 | 87.7 | 87.7 | 87.7 | 87.7 | 87.7 | 87.7 | 87.7 | 87.7 | 84.4 |
| Max | 89.0 | 84.0 | 84.0 | 84.0 | 84.9 | 78.0 | 78.0 | 78.0 | 84.8 | 91.1 | 91.1 | 95.1 | 95.1 | 95.1 | 95.1 | 94.9 | 94.9 | 94.9 | 94.9 | 94.9 | 94.9 | 94.9 | 94.9 | 94.9 | 94.9 | 81.0 |
| Min | 72.0 | 70.0 | 70.0 | 70.0 | 55.0 | 50.0 | 50.0 | 50.0 | 60.0 | 69.0 | 69.0 | 83.0 | 83.0 | 83.0 | 83.0 | 81.0 | 81.0 | 81.0 | 81.0 | 81.0 | 81.0 | 81.0 | 81.0 | 81.0 | 81.0 | 74.0 |

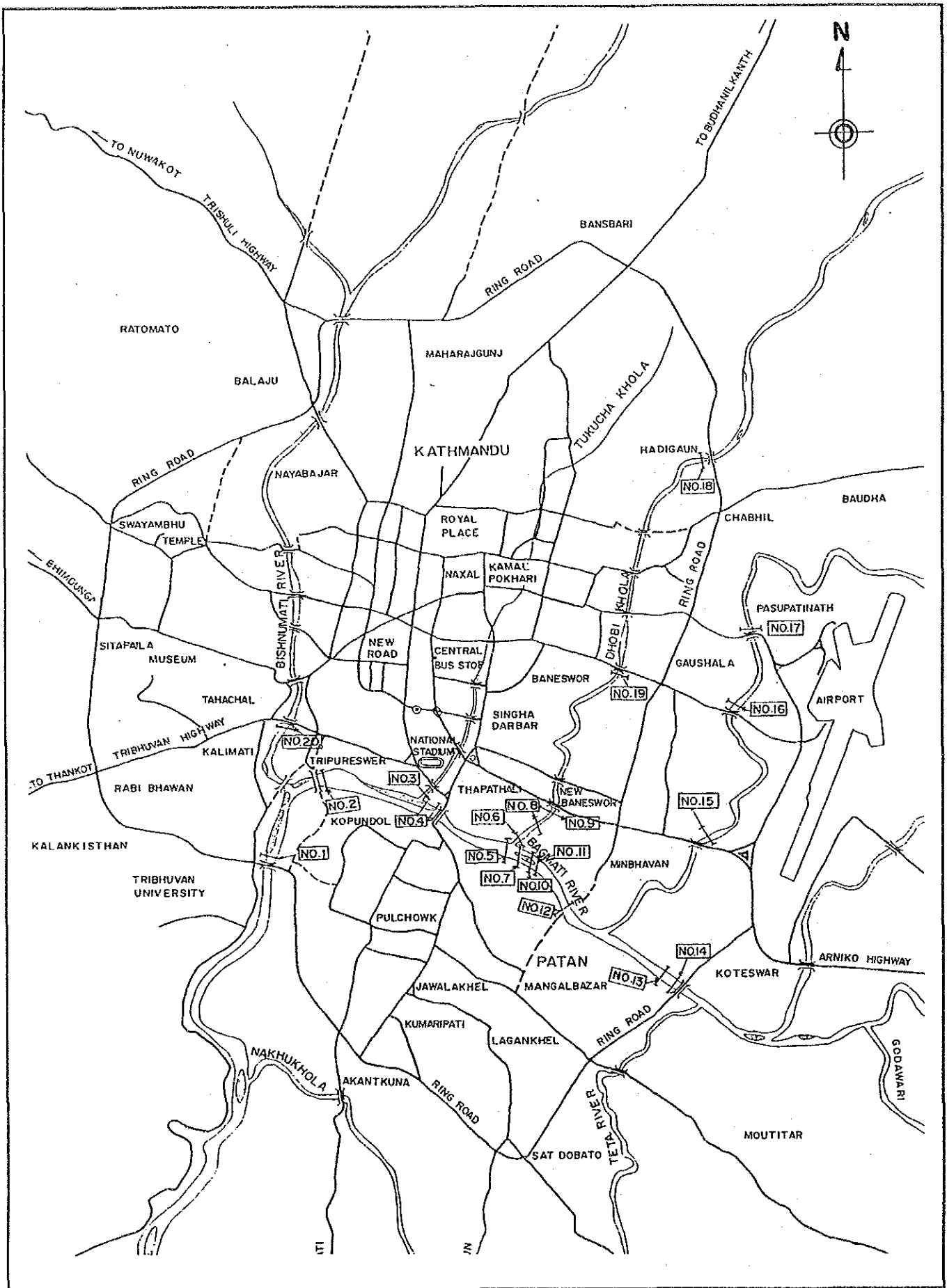
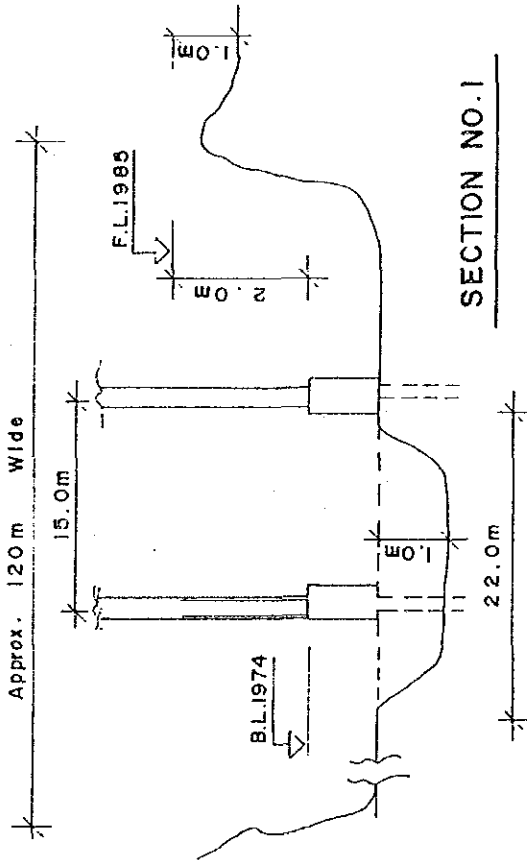


Figure A 4.3.2 LOCATION OF REFERED FLOOD LEVEL ENQUIRY SECTION

DATE : 6 | 9 | 92

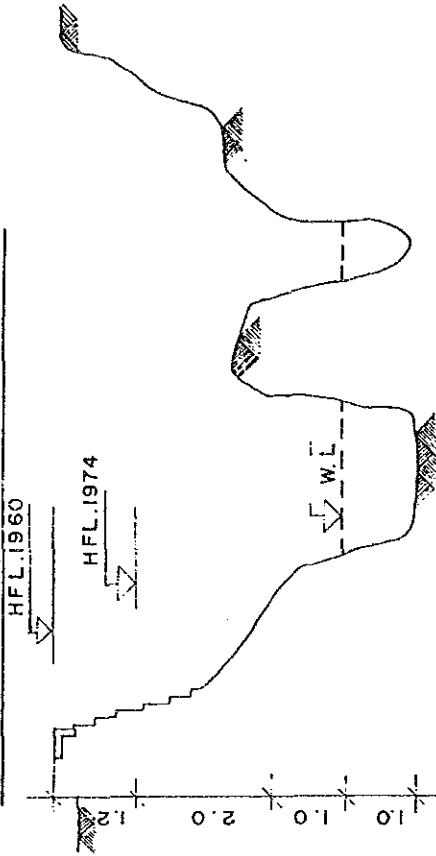
BAGMATI BRIDGE; BALKHU, RING ROAD (Br.No.7)



SECTION NO.1

DATE: 14 | 9 | 92

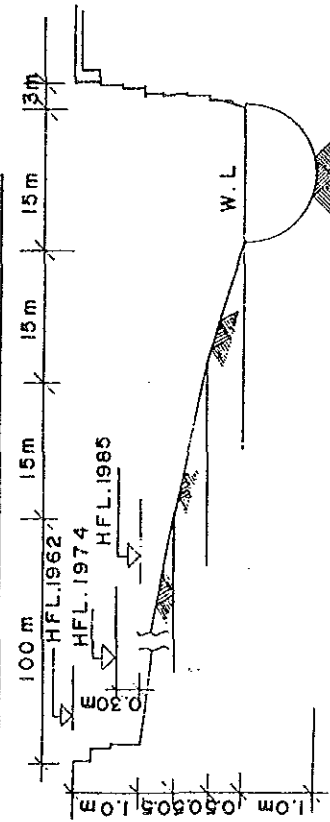
BAGMATI RIVER; BIRAUTA, KOPUNDOL



SECTION LOCATION: 200m D S OF BAGMATI BRIDGE
SECTION NO.3

DATE: 14 | 9 | 92

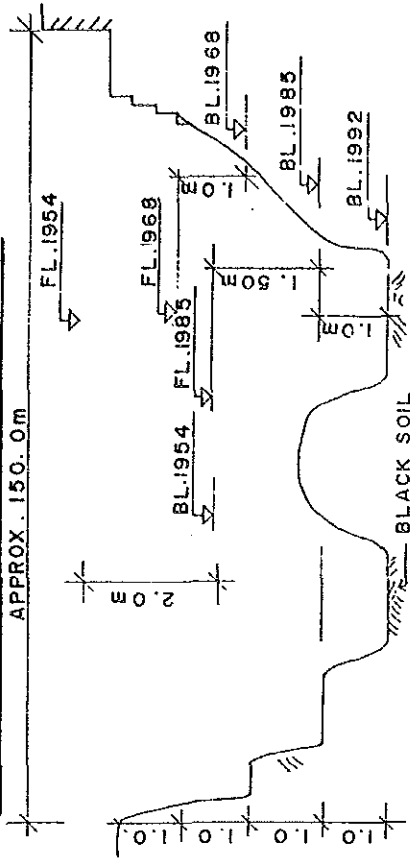
BAGMATI RIVER; RAJDAHA TIRTHA, SANERA



SECTION LOCATION: 100m U/S OF SUSPERISION BRIDGE, TEKU
SECTION NO.2

DATE: 7 | 9 | 92

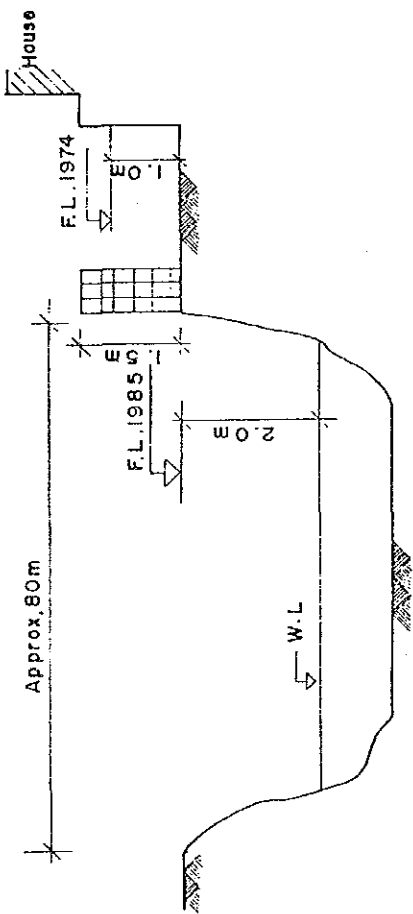
BAGMATI BRIDGE; THAPATHALI, Br. No.5



SECTION LOCATION: 40m R/S OF BRIDGE
SECTION NO.4

DATE: 8/9/92

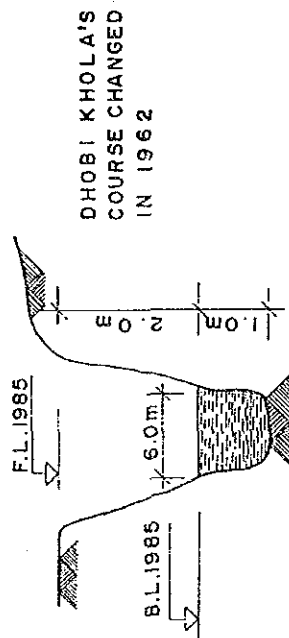
BAGMATI RIVER; D/S OF DHOBIKHOLA



SECTION LOCATION: 20m D/S OF CONFLUENCE OF DHOBI KHOLA
SECTION NO. 5 (SURVEY SECTION NO 7)

DATE: 8/9/92

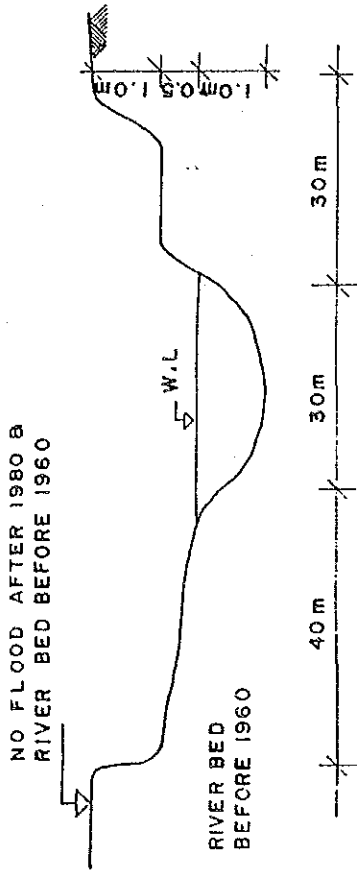
DHOBI KHOLA; CONFLUENCE WITH BAGMATI



SECTION LOCATION: 15m U/S OF CONFLUENCE WITH BAGMATI
SECTION NO. 6

DATE: 11/9/92

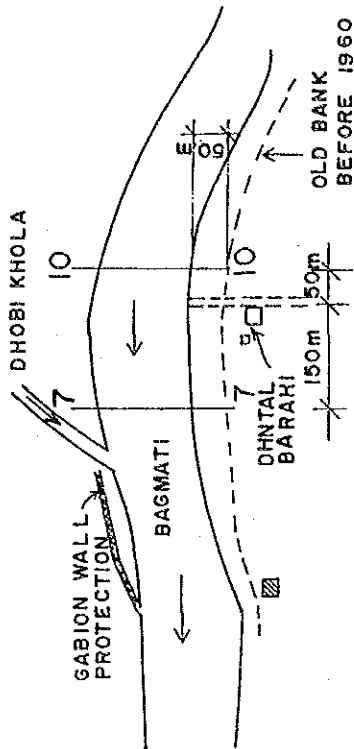
BAGMATI RIVER U/S OF DHOBI KHOLA CONFLUENCE



SECTION LOCATION: 150m DIS OF PHANTAL BARAHI AT L/S
SECTION NO. 7

DATE: 11/9/92

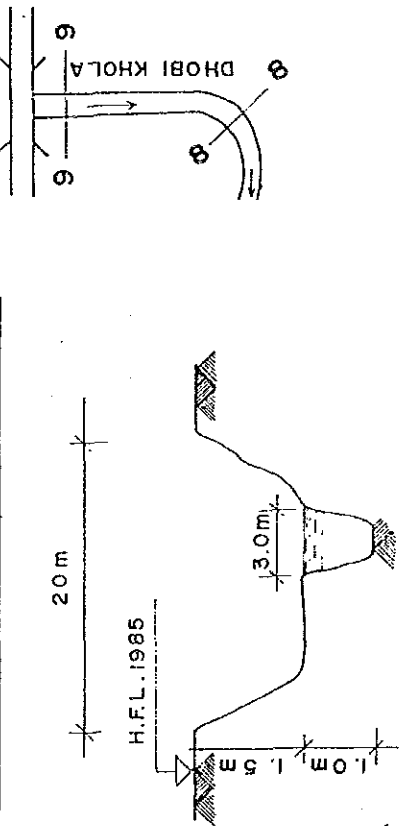
LOCATION PLAN OF SECTIONS AT DHNTAL BARAHI



LOCATION: DHOBI KHOLA CONFLUENCE WITH BAGMATI
FOR SECTION NO. 7 & 10

DATE: 8/9/92

DHOBI KHOLA; BUDDHA NAGER + BABARMAHAL

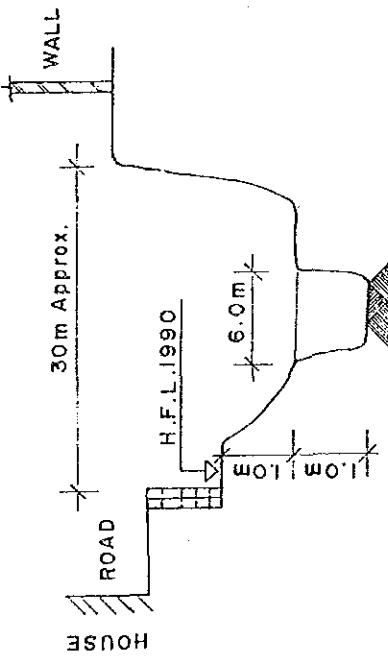


SECTION LOCATION: 500m D/S OF BRIDGE (BABARMAHAL)

SECTION NO. 8

DATE: 8/9/92

DHOBI KHOLA BRIDGE BABAR MAHAL BR. NO

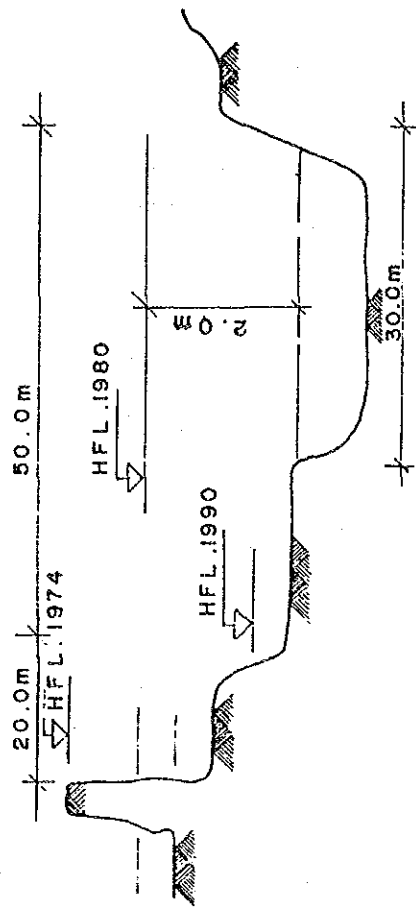


SECTION LOCATION: 15m D/S OF DHOBIKHOLA BRIDGE

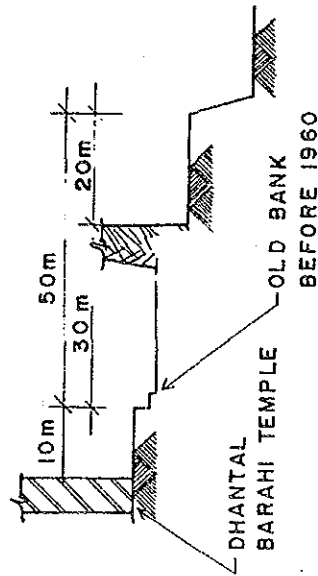
SECTION NO.9 (SURVEY SECTION NO.10)

DATE: 11/9/92

BAGMATI AT DHANTAL BARAHI



SECTION LOCATION: 50m U/S OF DHANTAL BARAHI AT L/B
SECTION NO. 10

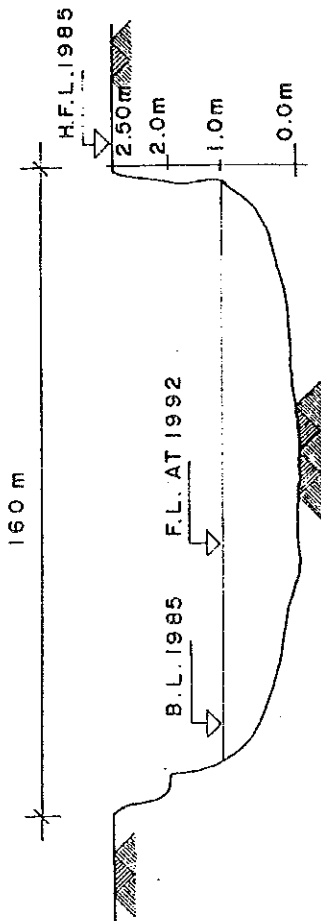


SECTION LOCATION: 50m U/S OF DHANTAL BARAHI AT L/B

SECTION: NO. 10 CONTINUED

DATE: 8/9/92

BAGMATI RIVER, BUDDHANAGAR

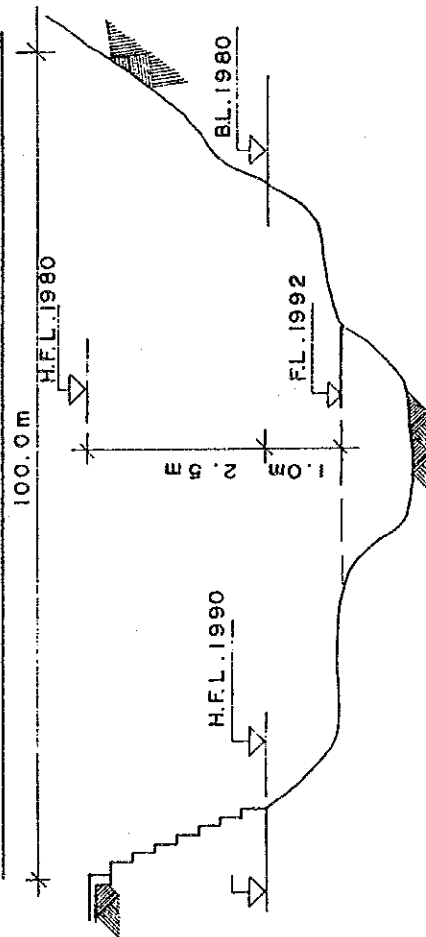


SECTION LOCATION: 400 m U/S OF DHOBIKHOLA CONFLUENCE

SECTION NO. 11

DATE: 8/9/92

BAGMATI BRIDGE SANKHAMUL PEDESTRIAN CROSSING

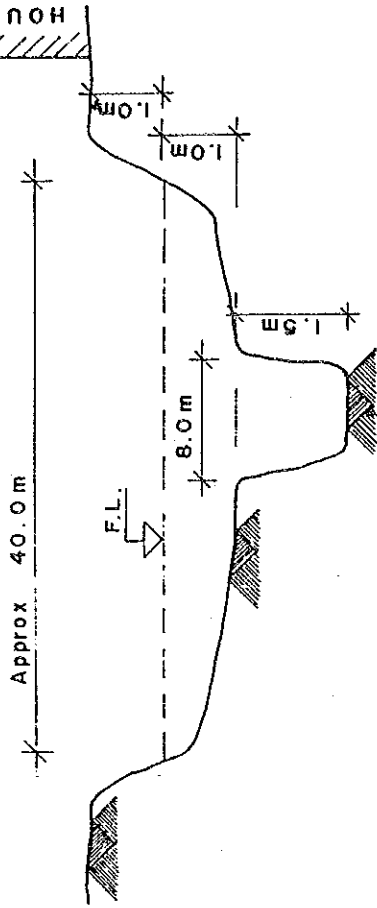


SECTION LOCATION: 10m D/S OF PEDESTRIAN CROSSING

SECTION NO.12

DATE: 8/9/92

MANOHARA BRIDGE (NEAR SUSPENSION BRIDGE)

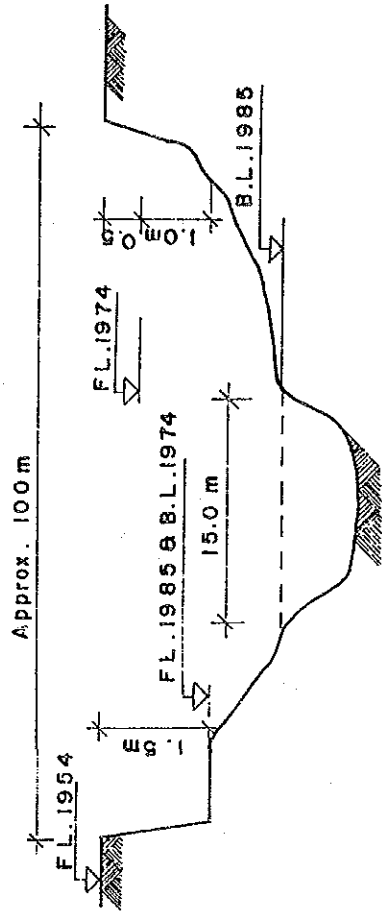


SECTION LOCATION: 100m U/S OF SUSPENSION BRIDGE

SECTION NO.13

DATE: 7/9/92

MANOHARA BRIDGE; RING ROAD, BALKUMARI

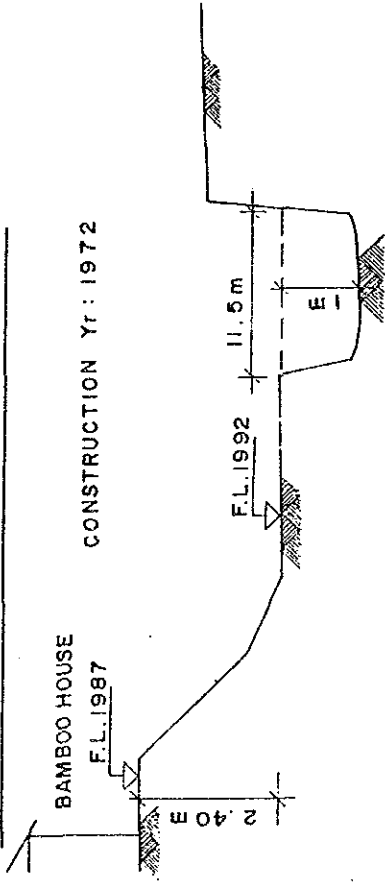


SECTION LOCATION: 15m D/S OF BRIDGE

SECTION NO.14

DATE: 6/9/92

BAGMATI BRIDGE; MINBHAWAN (Br. No.3)



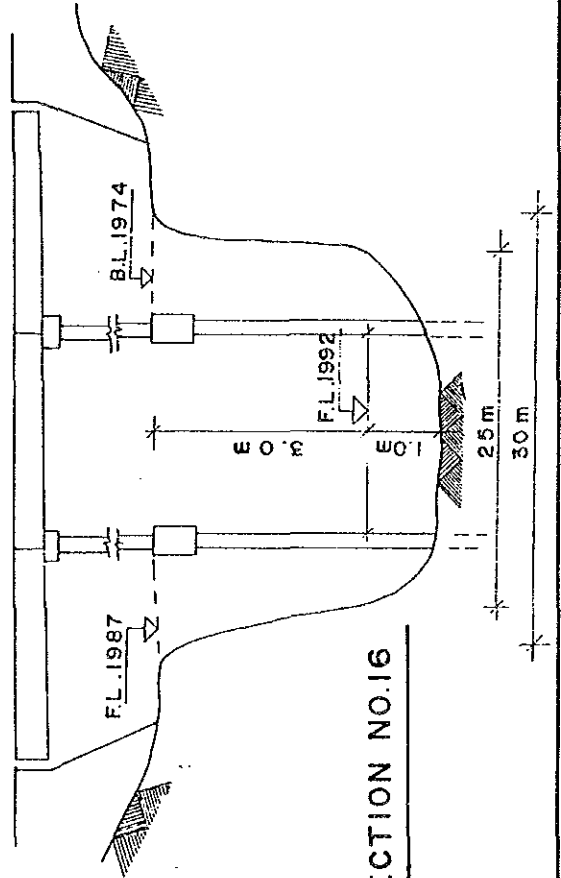
SECTION LOCATION: 30m U/S OF BRIDGE

SECTION NO.15

DATE: 6/9/92

BAGMATI BRIDGE; TIL GANGA, PASUPATI (Br. No.1)

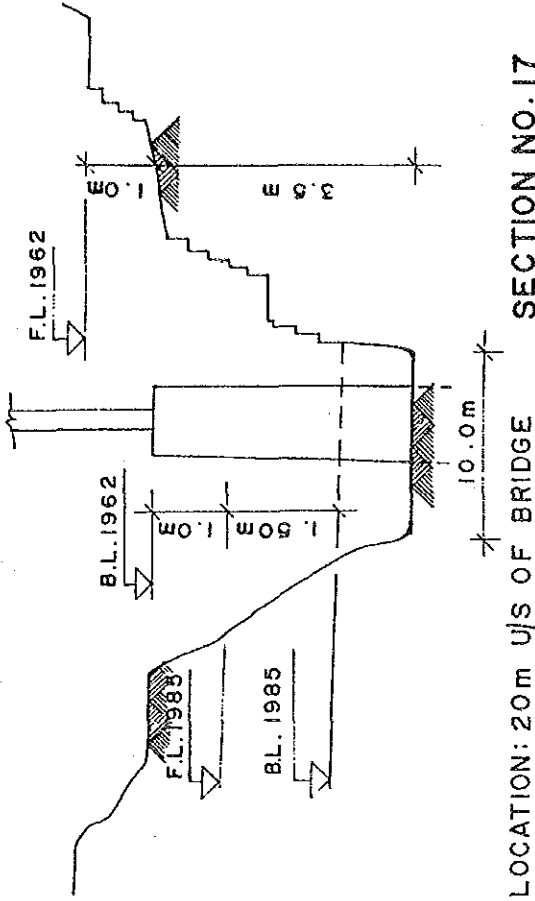
CONSTRUCTION 1974



SECTION NO.16

DATE: 7/9/92

BAGMATI BRIDGE, PRAYAG GHAT (Br. No.2)

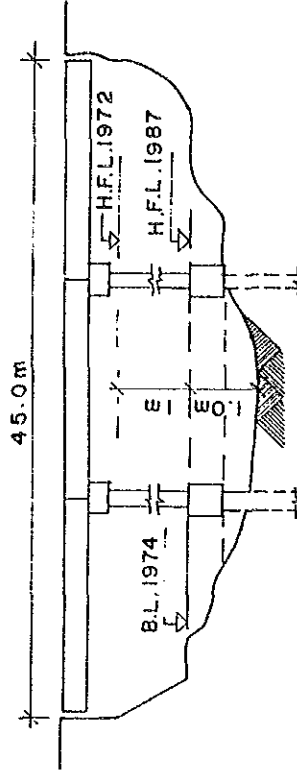


LOCATION: 20m U/S OF BRIDGE

SECTION NO.17

DATE: 6/9/92

DHOBI KHOLA; CHABAHIL RING ROAD (Br.No11)

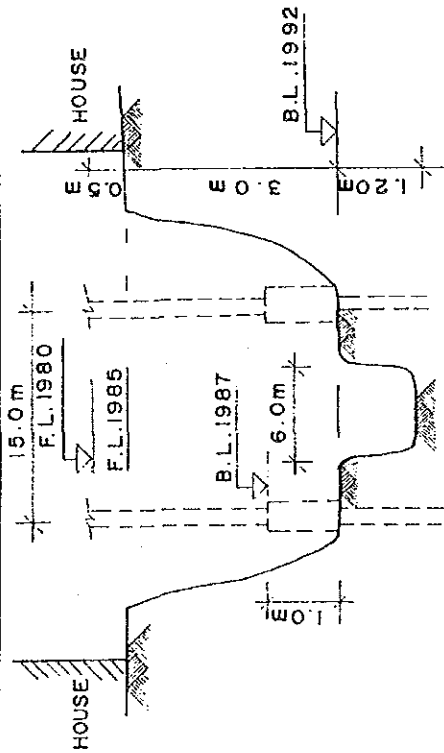


SECTION LOCATION: 15m D/S OF BRIDGE

SECTION NO.18

DATE: 7/9/92

DHOBI KHOLA; MAITI DEVI (Br. No.13)

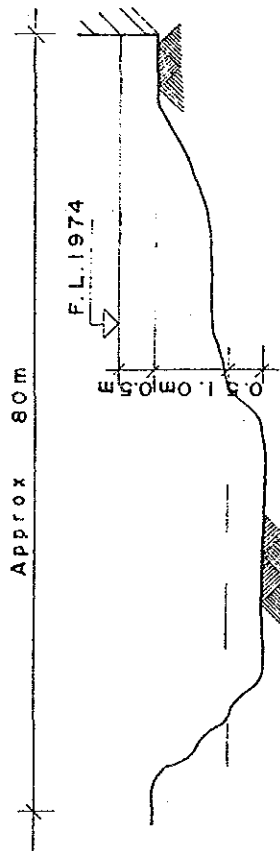


SECTION LOCATION: 10m D/S OF BRIDGE

SECTION NO.19

DATE: 6/9/92

BISHNUMATI BRIDGE; TEKU (Br. No.10)

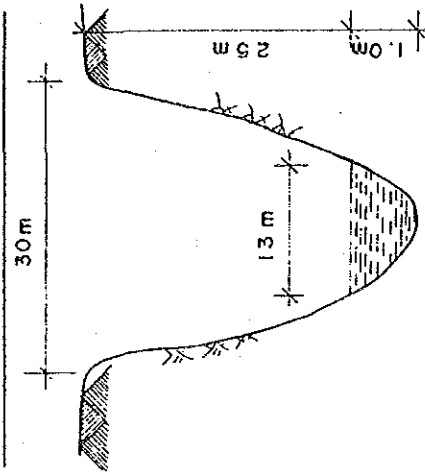


SECTION LOCATION: 15m D/S OF BRIDGE.

SECTION NO.20

DATE: 24/9/92

BAGMATI RIVER, CHOVAR

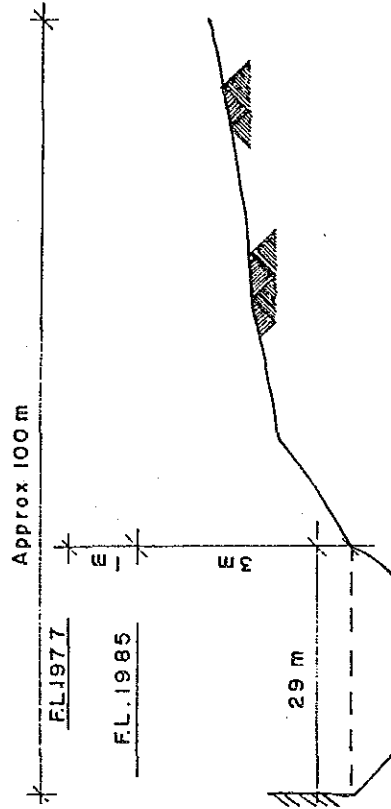


SECTION LOCATION: 15m U/S OF BRIDGE AT CHOVAR

SECTION NO.21

DATE: 24/9/92

BAGMATI RIVER, KHOKANA VILLAGE, KHOKANA BRIDGE



SECTION LOCATION: 10m U/S OF KHOKANA BRIDGE

SECTION NO.22

Table A.4.3.3(1)

MAXIMUM DAILY RAINFALL RECORD (1)

| YEAR | KAKANI | | TOKHA | | SUNDARIJAL | | INDIAN EMBASSY | |
|------|---------|----------|---------|----------|------------|----------|----------------|----------|
| | DATE | RAINFALL | DATE | RAINFALL | DATE | RAINFALL | DATE | RAINFALL |
| 1940 | - | - | - | - | * | * | - | - |
| 1941 | - | - | - | - | AUG.08 | 102.1 | - | - |
| 1942 | - | - | - | - | AUG.14 | 111.8 | - | - |
| 1943 | - | - | - | - | JUL. 20 | 137.4 | - | - |
| 1944 | - | - | - | - | AUG. 10 | 91.4 | - | - |
| 1945 | - | - | - | - | AUG. 02 | 126.5 | - | - |
| 1946 | - | - | - | - | JUL. 05 | 147.6 | - | - |
| 1947 | - | - | - | - | * | * | * | * |
| 1948 | - | - | - | - | AUG.26 | 95.0 | AUG. 27 | 81.8 |
| 1949 | - | - | - | - | JUL. 01 | 58.0 | MAY. 18 | 61.0 |
| 1950 | - | - | - | - | JUL. 14 | 87.1 | JUN. 21 | 104.6 |
| 1951 | - | - | - | - | AUG. 17 | 51.3 | JUN. 30 | 66.0 |
| 1952 | - | - | - | - | AUG.27 | 74.7 | AUG. 27 | 58.7 |
| 1953 | - | - | - | - | JUL. 01 | 105.9 | JUL. 02 | 115.6 |
| 1954 | - | - | - | - | JUL. 27 | 162.6 | JUL. 27 | 173.2 |
| 1955 | - | - | - | - | * | * | JUL. 26 | 52.8 |
| 1956 | - | - | - | - | AUG.17 | 72.4 | MAY. 25 | 54.4 |
| 1957 | - | - | - | - | AUG. 30 | 58.4 | AUG. 06 | 57.9 |
| 1958 | - | - | - | - | * | * | SEP. 06 | 58.9 |
| 1959 | - | - | - | - | AUG.11 | 86.4 | JUL. 14 | 48.1 |
| 1960 | - | - | - | - | JUL. 25 | 61.0 | JUL. 29 | 59.4 |
| 1961 | - | - | - | - | MAR. 16 | 127.0 | AUG. 13 | 87.4 |
| 1962 | JUN. 13 | 146.8 | - | - | JUN. 10 | 116.8 | JUN.10 | 72.4 |
| 1963 | AUG. 19 | 92.2 | - | - | AUG.31 | 121.9 | JUL. 21 | 54.0 |
| 1964 | AUG. 18 | 127.5 | - | - | JUL. 14 | 83.8 | JUN. 21 | 84.2 |
| 1965 | JUL. 09 | 73.4 | - | - | JUL. 08 | 66.5 | JUN. 18 | 72.0 |
| 1966 | - | - | - | - | JUN. 30 | 86.4 | AUG. 24 | 115.2 |
| 1967 | - | - | - | - | AUG. 23 | 85.0 | JUL. 10 | 134.0 |
| 1968 | - | - | - | - | JUL. 15 | 82.0 | OCT. 05 | 75.4 |
| 1969 | - | - | - | - | AUG.19 | 77.4 | AUG. 19 | 59.1 |
| 1970 | - | - | - | - | MAY. 21 | 95.2 | JUL. 15 | 68.0 |
| 1971 | - | - | - | - | JUN. 11 | 93.1 | JUN. 12 | 109.0 |
| 1972 | JUL. 28 | 161.0 | - | - | NOV. 27 | 92.4 | JUL. 28 | 107.4 |
| 1973 | SEP. 18 | 160.0 | JUL. 19 | 120.0 | * | * | AUG. 11 | 96.9 |
| 1974 | MAR. 30 | 100.0 | JAN. 15 | 83.5 | MAY. 31 | 90.2 | SEP.11 | 53.4 |
| 1975 | JUL. 08 | 74.0 | JUL. 30 | 94.4 | AUG. 03 | 131.2 | JUL. 28 | 89.9 |
| 1976 | JUL. 23 | 80.0 | JUL. 10 | 71.2 | MAY. 21 | 99.4 | | |
| 1977 | JUL. 04 | 100.0 | AUG. 01 | 80.4 | AUG. 22 | 87.4 | | |
| 1978 | JUN. 06 | 148.7 | MAR.12 | 61.4 | | | | |
| 1979 | JUL. 02 | 139.0 | JUL. 23 | 90.6 | | | | |
| 1980 | JUN. 25 | 156.0 | JUN. 19 | 130.0 | | | | |
| 1981 | AUG. 30 | 131.0 | | | | | | |
| 1982 | * | * | | | | | | |
| 1983 | JUN. 24 | 144.0 | | | | | | |
| 1984 | AUG. 26 | 124.0 | | | | | | |
| 1985 | AUG. 04 | 100.0 | | | | | | |
| 1986 | JUL. 16 | 116.0 | | | | | | |
| 1987 | OCT. 20 | 88.0 | | | | | | |
| 1988 | AUG. 07 | 83.2 | | | | | | |
| 1989 | JUL. 30 | 132.0 | | | | | | |
| 1990 | AUG. 15 | 97.6 | | | | | | |
| 1991 | AUG. 07 | 85.5 | | | | | | |

Table A.4.3.3(2)

MAXIMUM DAILY RAINFALL RECORD (2)

| YEAR | SANKHU | | KATHMANDU AIRPORT | | NAGARKOT | | THANKOT | |
|------|---------------|----------|-------------------|----------|----------|----------|---------|----------|
| | DATE | RAINFALL | DATE | RAINFALL | DATE | RAINFALL | DATE | RAINFALL |
| 1940 | - | - | - | - | - | - | - | - |
| 1941 | - | - | - | - | - | - | - | - |
| 1942 | - | - | - | - | - | - | - | - |
| 1943 | - | - | - | - | - | - | - | - |
| 1944 | - | - | - | - | - | - | - | - |
| 1945 | - | - | - | - | - | - | - | - |
| 1946 | - | - | - | - | - | - | - | - |
| 1947 | - | - | - | - | - | - | - | - |
| 1948 | - | - | - | - | - | - | - | - |
| 1949 | - | - | - | - | - | - | - | - |
| 1950 | - | - | - | - | - | - | - | - |
| 1951 | - | - | - | - | - | - | - | - |
| 1952 | - | - | - | - | - | - | - | - |
| 1953 | - | - | - | - | - | - | - | - |
| 1954 | - | - | - | - | - | - | - | - |
| 1955 | - | - | - | - | - | - | - | - |
| 1956 | - | - | - | - | - | - | - | - |
| 1957 | - | - | - | - | - | - | - | - |
| 1958 | - | - | - | - | - | - | - | - |
| 1959 | - | - | - | - | - | - | - | - |
| 1960 | - | - | - | - | - | - | - | - |
| 1961 | - | - | - | - | - | - | - | - |
| 1962 | - | - | - | - | - | - | - | - |
| 1963 | - | - | - | - | - | - | - | - |
| 1964 | - | - | - | - | - | - | - | - |
| 1965 | - | - | - | - | - | - | - | - |
| 1966 | - | - | - | - | - | - | * | * |
| 1967 | - | - | - | - | - | - | * | * |
| 1968 | - | - | OCT. 05 | 80.4 | - | - | * | * |
| 1969 | - | - | AUG. 19 | 48.5 | - | - | AUG.12 | 46.2 |
| 1970 | - | - | JUL. 16 | 73.5 | - | - | May-18 | 92.0 |
| 1971 | AUG.07 | 44.0 | JUN. 12 | 83.6 | * | * | JUN. 12 | 126.8 |
| 1972 | JUN. 03 | 90.0 | JUL. 28 | 102.8 | JUL. 16 | 60.8 | JUL. 28 | 134.8 |
| 1973 | JUL. 05 | 46.0 | JUL. 25 | 102.0 | AUG. 07 | 94.0 | OCT. 13 | 112.0 |
| 1974 | JUL. 31 | 46.0 | AUG. 21 | 71.2 | JUL. 23 | 80.8 | May-02 | 132.4 |
| 1975 | SEP. 27 | 44.0 | AUG. 03 | 89.2 | JUL. 28 | 81.2 | JUL. 28 | 100.4 |
| 1976 | May-11 | 40.8 | JUN. 10 | 73.2 | AUG. 23 | 82.0 | JUN. 02 | 106.4 |
| 1977 | JUL. 02 | 40.8 | AUG. 05 | 57.6 | JUN. 20 | 88.5 | AUG. 10 | 60.8 |
| 1978 | JUL. 16 | 126.0 | AUG.10 | 71.2 | JUL. 28 | 92.1 | JUL. 16 | 135.0 |
| 1979 | AUG. 14 | 90.0 | JUL. 24 | 86.0 | JUL. 24 | 96.4 | JUL. 24 | 132.0 |
| 1980 | JUL. 14 | 80.0 | JUN. 09 | 100.1 | JUN. 09 | 95.5 | JUN. 09 | 84.4 |
| 1981 | May-16 | 67.5 | May-21 | 53.5 | JUL. 29 | 79.3 | SEP. 29 | 100.3 |
| 1982 | JUL. 06 | 60.0 | JUN. 28 | 87.6 | AUG. 15 | 69.0 | SEP. 14 | 41.3 |
| 1983 | JUL. 22 | 102.0 | JUL. 17 | 72.0 | AUG. 02 | 72.5 | SEP. 22 | 75.9 |
| 1984 | AUG. 13 | 85.0 | AUG. 16 | 76.5 | JUN. 28 | 85.0 | SEP. 08 | 75.1 |
| 1985 | May-01 | 80.5 | SEP. 17 | 69.3 | * | * | SEP. 15 | 80.1 |
| 1986 | JUL. 31 | 80.0 | JUL. 16 | 77.6 | JUL. 31 | 179.4 | JUN. 24 | 100.5 |
| 1987 | OCT. 20 | 95.5 | OCT. 20 | 124.4 | OCT. 20 | 90.6 | OCT. 20 | 157.4 |
| 1988 | AUG.1, JUN18 | 65.0 | JUL. 12 | 66.0 | AUG. 01 | 72.4 | SEP. 08 | 122.4 |
| 1989 | AUG. 08 | 82.0 | JUL. 30 | 57.0 | AUG. 08 | 97.6 | JUL. 16 | 70.3 |
| 1990 | JUL.9, AUG. 9 | 92.0 | May-29 | 73.2 | JUL. 14 | 101.2 | AUG. 27 | 116.2 |
| 1991 | AUG. 08 | 91.0 | AUG. 15 | 44.7 | JUN.01 | 92.5 | AUG.28 | 54.3 |

Table A.4.3.3(3)

MAXIMUM DAILY RAINFALL RECORD (3)

| YEAR | BHAKTAPUR | | KHUMALTAR | | GODAVARI | |
|------|-----------|----------|-----------|----------|----------|----------|
| | DATE | RAINFALL | DATE | RAINFALL | DATE | RAINFALL |
| 1940 | - | - | - | - | - | - |
| 1941 | - | - | - | - | - | - |
| 1942 | - | - | - | - | - | - |
| 1943 | - | - | - | - | - | - |
| 1944 | - | - | - | - | - | - |
| 1945 | - | - | - | - | - | - |
| 1946 | - | - | - | - | - | - |
| 1947 | - | - | - | - | - | - |
| 1948 | - | - | - | - | - | - |
| 1949 | - | - | - | - | - | - |
| 1950 | - | - | - | - | - | - |
| 1951 | - | - | - | - | - | - |
| 1952 | - | - | - | - | - | - |
| 1953 | - | - | - | - | JUL. 27 | 57.2 |
| 1954 | - | - | - | - | JUL. 26 | 174.0 |
| 1955 | - | - | - | - | AUG. 06 | 83.2 |
| 1956 | - | - | - | - | May-24 | 90.0 |
| 1957 | - | - | - | - | AUG. 05 | 66.2 |
| 1958 | - | - | - | - | OCT. 03 | 60.7 |
| 1959 | - | - | - | - | JUL. 25 | 111.5 |
| 1960 | - | - | - | - | JUL. 06 | 77.5 |
| 1961 | - | - | - | - | * | * |
| 1962 | - | - | - | - | JUN. 28 | 97.2 |
| 1963 | - | - | - | - | * | * |
| 1964 | - | - | - | - | * | * |
| 1965 | - | - | - | - | * | * |
| 1966 | - | - | - | - | * | * |
| 1967 | - | - | - | * | * | * |
| 1968 | - | - | OCT. 05 | 117.0 | * | * |
| 1969 | - | - | AUG. 19 | 45.0 | - | - |
| 1970 | - | - | JUL. 16 | 100.0 | * | * |
| 1971 | * | * | JUN. 12 | 90.0 | JUN.11 | 123.0 |
| 1972 | JUL. 28 | 58.8 | JUL. 28 | 48.0 | JUL. 20 | 109.4 |
| 1973 | * | * | JUL. 25 | 85.0 | JUL. 25 | 122.2 |
| 1974 | * | * | - | - | JUL. 15 | 88.0 |
| 1975 | JUN. 28 | 41.6 | JUL. 28 | 101.6 | JUL. 28 | 159.6 |
| 1976 | AUG. 08 | 54.4 | SEP. 19 | 62.0 | JUN. 10 | 117.4 |
| 1977 | AUG. 28 | 67.2 | JUN. 07 | 60.2 | JUL. 08 | 114.2 |
| 1978 | OCT. 06 | 74.3 | JUL. 03 | 135.0 | OCT. 06 | 99.4 |
| 1979 | JUL. 24 | 73.8 | AUG. 21 | 86.0 | JUL. 24 | 96.8 |
| 1980 | JUN. 09 | 69.5 | JUN. 09 | 58.2 | JUN. 19 | 103.1 |
| 1981 | SEP.29 | 51.9 | SEP. 29 | 85.5 | SEP. 30 | 168.5 |
| 1982 | JUL. 04 | 41.3 | APR. 27 | 76.0 | JUL. 07 | 68.0 |
| 1983 | JUL. 16 | 80.5 | JUL. 05 | 70.0 | JUL. 04 | 84.0 |
| 1984 | AUG. 26 | 69.1 | SEP. 06 | 65.5 | SEP. 06 | 110.0 |
| 1985 | SEP. 05 | 78.6 | SEP. 05 | 71.5 | JUL. 07 | 119.5 |
| 1986 | JUN.29 | 107.6 | JUN. 29 | 73.0 | JUL. 26 | 96.0 |
| 1987 | AUG. 06 | 62.0 | OCT. 21 | 118.0 | OCT. 20 | 172.0 |
| 1988 | JUN. 18 | 96.0 | DEC. 27 | 78.0 | DEC. 26 | 63.5 |
| 1989 | SEP. 21 | 68.8 | JUL. 01 | 51.0 | AUG. 07 | 68.2 |
| 1990 | AUG. 12 | 62.6 | JUL. 14 | 62.6 | AUG. 13 | 110.0 |
| 1991 | JUL. 08 | 41.0 | APR. 01 | 44.2 | JUL. 08 | 92.8 |

Table A.4.3.3(4) PROBLE DAILY RAINFALL

| Return Period (Years) | Method | | |
|--------------------------|--------|--------|-------------|
| | Hazen | Gambel | Pearson III |
| 2 | 98.79 | 98.60 | 98.29 |
| 5 | 128.26 | 130.90 | 127.43 |
| 10 | 146.35 | 152.29 | 146.48 |
| 20 | 164.45 | 172.80 | 164.23 |
| 50 | 186.89 | 199.35 | 188.18 |
| 80 | 198.40 | 212.86 | 200.05 |
| 100 | 203.71 | 219.25 | 205.94 |
| 200 | 220.30 | 239.07 | 223.91 |

Table A.4.3.8 Calculation Of Flood Water Level

| | Return Period (Years) | W.D. (m) | A (Sq. m.) | P (m) | R (m) | I | V (m/s) | Q=A.V (m ³ /s) | Design F.D. (m ³ /s) | W.L. Of Flood |
|--------------|-----------------------|----------|------------|--------|-------|-------|---------|---------------------------|---------------------------------|---------------|
| Bagmati | 100 | 4.30 | 500.00 | 220.00 | 2.27 | 1/400 | 2.88 | 1440.51 | 1367.49 | 1277.30 |
| Bridge NO. 1 | 10 | 4.10 | 410.00 | 210.00 | 1.95 | 1/400 | 2.60 | 1067.44 | 972.66 | 1277.10 |
| Bagmati | 100 | 4.20 | 354.00 | 129.18 | 2.74 | 1/400 | 3.26 | 1155.38 | 1121.01 | 1280.10 |
| Bridge NO. 2 | 10 | 3.70 | 285.00 | 125.00 | 2.28 | 1/400 | 2.89 | 822.84 | 797.35 | 1279.60 |
| Bagmati | 100 | 4.20 | 390.00 | 182.00 | 2.14 | 1/400 | 2.77 | 1080.38 | 1061.28 | 1284.20 |
| Bridge NO. 3 | 10 | 3.48 | 324.54 | 182.09 | 1.78 | 1/400 | 2.45 | 795.13 | 754.86 | 1283.68 |
| Bagmati * | 100 | | | | | | | | 217.17 | 1286.45 |
| Bridge NO. 4 | 10 | | | | | | | | 154.47 | 1285.94 |
| Manahara Ri. | 100 | 4.64 | 280.00 | 117.00 | 2.39 | 1/400 | 2.98 | 834.94 | 822.14 | 1286.07 |
| (C.S.-16-16) | 10 | 4.14 | 240.00 | 107.00 | 2.24 | 1/400 | 2.86 | 685.40 | 584.77 | 1285.57 |
| Dhobi Khola | 100 | 3.01 | 60.72 | 62.45 | 0.97 | 1/250 | 2.07 | 125.63 | 104.68 | 1284.15 |
| (C.S. 18-18) | 10 | 2.50 | 45.00 | 50.00 | 0.90 | 1/250 | 1.97 | 88.43 | 74.45 | 1283.60 |

* Given by non-uniform flow calculation

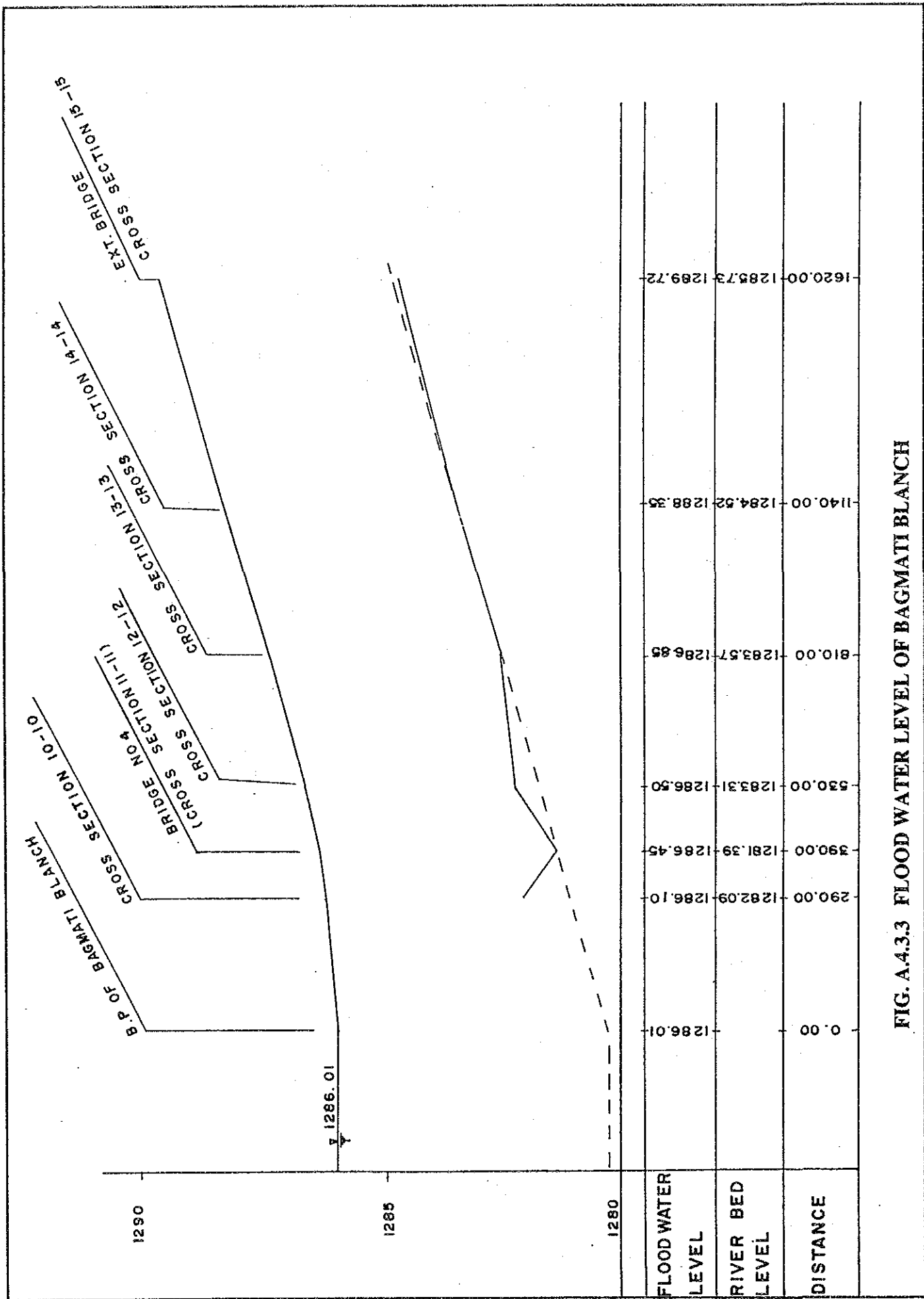


FIG. A.4.3.3 FLOOD WATER LEVEL OF BAGMATI BLANCH