mm/day	BASIN 21	18.2	4.1	40	o (c	2	0 0	4.6	73.4	12.6		5	7:5	200		5 3	0.0	8.7	8.7	4	3) 3)			က	6		0.0	9 0	39.8	1.2	0		0 7 8	2 . 6	; e-	U	U U	5.7	1.4	0.5	1.7	2	တ (2	, ·
	20		4	~ 0	2 6	0	0	1	1		-1	-1	-1	1	1			ŀ	1	- 1		. [1		_[. 1	_1		i	8.		716	0 0) u	α	=		2.5	2	0	8			= e	n
unit	BASIN 20			+	+-	┾	 _			-1	+		20 9	7	7	16	3		6					9	∸∤	8	0	3	38	0			7 6	100			2	3	2				9 6	4 21	-
	BASIN 19	15, 6	13.6	2	7 4	37.5	4.1	6.4	27.1	22.8	4.5	-	2				3	7 0	0	46.	3	4	7	2	=	0	9	4	20.	3. (-	٠,	ċ	·	, [-	-	c	10	65	-	6	ادی	~;		-
	BASIN 18	23.0	13. 7	c .	2 ° °	1.6	0.2	1.8	27.9	4.5	0.2	4. 2	0.4	10.1	1.4	6.3	0.0	3.3	3.4	2.6	0.0	29. 2	2.1	5.6	0.4	0	0.0	0.7	15.0	0.4	0	(D)	- 0	- 0 - 0	0 0 0	0	0	. 65	9.0	0.0	16.7	2.2	2	20 -	ר. ד
	2		\exists		_	-					_		_			و م	٥	60	دی.			۵	5		6	_	2	_	2		0.4	+	2) 0	10	3 -	- G		2	100	0.0	7		0	9	0.5
	N BASIN				1.	1	-	_	_		力	_	,	_						6			~			_	S	_	. 0	0	0	0	× c		- -		. ~		2	0	0	ري ا	د.		-
	BASI	17.	28.	ء اد	287	3	6	4.	0	Ö		<u>.</u>]	-		9		4	4	_	\downarrow	_	4				4	_			_	4	4	4	o Le	L	+	L	L	L	_		7	7	_
	BASIN 15	37.0	14.4	=	T:-	3.2	12.1	14.7	1.4	9.0	0	0	0.2	0		0.0	0.0	1		0.4		11.5	- 4	9.	1	0	9.8			0.2	2.3	4	- 1	-1			0						3.5		
	BASIN 14	23.1	27.1	9.0	7 07	29.4	10.7	5.2	1.1	0.2	0			0	9.7	0.0	0	0.0	0.0	9.7	0	0.0		1.7	0.3					0.1	0.0	5	9	,	2	6	9 0	0.0	2.9	0.0	0.0	13.5	2.1	13.0	7. p
	BASIN E			500	9 - P	2	1.0	(4.9	5.6	2.2	æ.	7:7	6	8	0	0	- -	0	0		0	7.5	-3	6.1	3.0	0.0	0.9	1.1	0.4	0.2	1.6	7		7 6	ים מי	- - -	2	ار د د		0.0	0.0	7.1	4-1	2	7 7 7
	z	z,	0		8.7.7	1_	8 1				1.4	7.5	8		7 0	3.4	3 3	2.6	1.2	2.3		0.4	4.8	2.0	0.4	0	1.2	8.0	0.2	0.0	0.0	4.0		7	- L		7 0	2 2	2.9	0.0	0.0	1.6	3.5	2.2	7:7
	N 8AS	~	1		20 1-	. 6	4	6	2	7	æ	6	3	∞		80	2	9	8	0	65	- -	2	9		_ 			0	0	9	50	_	7.	ďα					0			6,	.1	
•	BAS1 11	15.	17.		4. 4	0	S	22.	39.	Н	4	4	-	\dashv	-1	4	4	4	-	_	-	4		\vdash	Н	Н	Н	_	-	H	0	\dashv	+	+	+	╀	╁	+	╁	+-	-	5	6	·	
	BASIN 10		26.0	8.3			7.5	11.7	15.2	0.8	1.3	0.6	1.4	3.2	ω 8	8	7 8	6.3	2.9	1.9	0.2	0.	5.7	4.8	0.6	0.0	1.0	1.3	0.0	0.0	0.0	3.2	3.4	2	2 4	, ,	9 6	2	2.1	0.0		9.4	4.3	10.0	
	BASIN 9	24.3	13.8	17.9	22.2	2 6	19.1	23, 3	23.2	4.2	5.2	2.1	1.3	4.5	2.4	7.4	7. 1	5.7	4, 3	0.0	0.2	3.5	6.2	4.4	1.4	0.0	0.0	2.2	9.0	0.0	3.6	3.0	4.2	7.7	2.3	, ,	9.9	9 6	1.8	0.0	0.0	7.9	1 .6	-1	J. 5
	BASIN 8	18.9	4.3	12. 4	9.0	7 0	18.5	14.6	3.5	5.8	0.5	0.0	0.0	1.4		0.0	0.7	0.1	0.5	0.4				0.8	1.8	0.0	3.4					1. 2			- 0			0 10					ę. 8		
	BASIN E	6	LD.	2	5.5	1-1	- ~	~		2	5	-	-	5	٥	0	~	2	0	9.3	9.2	1.8	0.2	0.0	1.3	0.0	3.8	0.0	0.1	0.2	5.2	1.0		~	- -	100	-		7 0	0.0	2.7	6.4	7.5	3	70°. 1
		L			+	+]	_	2. 6	2.4	3.2	0	0	9.0	1	7.0 [3.6	5.5	0.3	0.4	7.5	0.9	0.7	0.0	1.1	80	0 0	0.0	0.0	2. 6	8		7) u		,0	2 0	1.0	0.1	2.6	
	N BASIN	+-	2 16	9	2			t -	9 6	7	4	2) 0	0	0	0	0	0	4	0	0	9	1	4	0	2	0	0	0		0	2	0	4	4	1	+	0 0	-	· LC?	L	- 12		5	2
	BASIN	13	30.	70.	21:2		3	62.	7.	9.	3.	0.	9.	0	0	0.	0	0	16.	13.	0.	15.	4	6	0	ö	9	0	6	0	G		တ်	·	**		= -	<i>-</i>	-	-	-	- -	က		
	BASIN 4	28.7	46.4		49.3	2 ×			18.1	65.7	25. 1		1.3	0.0	0.0	0.0	1.5	1 3	0.4	9.0		6.3	1.	0.5	0.1	0.3	3.0	0.6		1.8	5.1	6.7	4.5		7.57	1	7	5 4				10.9		7.	3.6
	BAS IN	1.4	14.9		9 6	3 2	2 6		13.9	0.1	0.2	2.1	0.0	0.0	0.0	0.0	0.0	0 0		1.0	0.0	12.9	17.6	3.8	0.0	0 0	0.0	1.5	0.0	0.0	0.0	0.4	9 0		-	7 6	- -	- C	, c	4.8		0.0		12. 5	1.2
	BASIN B	4	2, 5	5.4		0 4° 0	1 1	5	0	8.8	0.3		0.0		0.0	0.0	0.0	0.0	0.0	3.0	0.0	1.5	4.4		0.0	0 0	0.0				0.1	0.0	8.0		× 0		2	1.1		9 6	.I.	0.1	6.	9 .	9
		GT.	9		1	70	\perp	2		_	4							0	L	Ļ	L.				L		L	L		L	7	Ц		_	4	1	1	2	-	1 4	\downarrow	_			
88	BASIN	17.	9.	Н	\perp	4	26.	ļ.,	39	_		-	L	L		0	Ö	0	0	2	_	L	L	0.8		o	0	L	Ļ	Ö	H	0		_	zi o	4	Š			\downarrow	Ļ	1	Ц	ė.	
YEAR 1968	TE	16		81	13	9 6	32	23	24	25	26	27	28	29	8		-	<u></u>	4	מו	۵	_	ω	5	Ē	Ξ	12	13	-	15	12	17	18	73		7	77	7	36	2,8	22	287	53		-
(1) YE.	DATE	APR	! ! 													MAY												-	·-	· .										:	:				

ESTIMATED DAILY RAINFALL FOR HIGH FLOW ANALYSIS

(1) YEAR 1968

	***********						-			_	_	_		-	_		-	-	-		_,		_	,		_		_		_	_
	BASIN 21	4.7	0.2	22.7	9.2	0.0	0.3	0.0	10.0	0.0	1.6	1.2	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	BASIN 20	4.9	1.4	24.6	8.7	0.0	1.8	0.3	16.0	0.0	0.0	0.8	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.5	0.5	0.0	0.0	0.0
	.	13.7	1.7	16.4	19.6	1.7	0.0		3.3	2.2	10.9	3.5	0.0	0.0	0 0	0 0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.0	0.0
		2.5	0.0	7.1	7.1	0.1	0.4	3.8	3.8	0.1	0.4	0.4	0.0	0.0	0 0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	6.9	7.7	0.0	0.1	0.0
	<u>π</u>	9	0	ď	6.7	0.9	0.1	4.9	0.9	0.4		0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		0.0	0.0	0.0		8.6	9.8	0.2	0.2	0.0
	IN BASI 17		H	2	2	7	: 0	0	0	6	0.0	0	0.0	9	. 0	0	0	0.0	0	0.0	0.	0.0	0.0	0.0	0.0	0.0	0.0	0.01	0.0	2.3	0.1
	N BASIN 16	_		8	9 27.	3	2 0.	0	20	5 4.	0	0	0	0		0 0		0 0	:.	0 0	Ц	0	L		_	. 0	3 1	3 7	4 (2 2	0 0
	N BASI 15	2	7 15.	18.)	1 3.	1 0.) [4 3.		L	0.	0			0 0		0	0 0	0 0	0	0	0.0	0	0 0	0 0	0 1.	7 9.	$0 \mid 1$.	0 0	0 0
	BASI	26.	-	12	-	3.	0	0.0	0	4.3	L	0	0.1	L	L	0	0.0	0.	_	0.	0.	9.		0	0.1	0.	0		0	2.	0.
	BASIN 13	2	11.0	13.0	8.9	3.8	0.5		2.9	0.8	0.0	0.0	0 0	0 0	0.0	0 0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0 0	0.0	0.0	8.8	1.0	0.4	0.0
	BASIN 12	25.8	1.2	9.3	23.4	4.9	0.1	0.0	0.3	4. 2	0.0	0.0	0.0	0 0	0.0	0 0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.8	0.0
	BASIN 11	6 3	5	88	12.5	7 9	1.4	0.1	1.8	1.2	0.0	0.0	0.0	0 0	0.0	0.0	0.0	0 0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.6	0.3	0.0	0.0
	BASIN 10	24.8	2 8	7.4		6.7	0.0	0.0	0.7	4.2		0.0		0.0	0.0	0.0	0.0	0.0		0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.5	0.0
	BASIN E	, ,	6.3	15.1	8.4	5.0	9.0	8.0		1.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.3	0.1	1.8	0.0	0.0
:	BASIN B	2.5	0.0	0.4	0.9	2.4	0.0	7.3	3.1	0.5	0.3	0.2	0.0	0.0	0.1	0.0	0.0	0.5	0.0	0.0	0.0	0.0	0.0	0.1	0.0	0.0	5.2	4.9	1.7	0.0	9.0
		9	-	5.2	2.2	2, 1].1	5.9	7.6	1.5	0.8	0.8	0.0	0.0	7.3	0.0	0.0	1.4	0.0	0.0	0.0	0.0		0.2	0.0	0.0	5, 3	5.7	5.2	0.0	0.7
	IN BASI)	- 2			2.6					, 4·	L	_			L	0.2		0.	_	Ц			Ĺ				0.	. 8	0.8	. 8	0 :
	N BASIN 6	5 11	7	6 1	7 2	1 12	2 0		8 0	3	2 0	0 - 0	0	0 - 0	0 0	7 0	2 0	0 0	0 0	0 0	0 0	0 0	0 0	0 0	0 0	0 0	0 0	$1 \mid 1$	0 6	0 0	0 0
	BAS1	Н	Ц	22.	L	1.		0.		2.	1.	0	0	0		89			θ.			_	0.	0.			0	12.	2.	0.	0
	BASIN 4	51.9	7.0	11 1	8 2	3.8	3.3	1.3	10.8	16.3	8.1	5.0	0.0	0.0	2.4	0.1	2.3	11.2			0.0	0.0	0.0	1.8	0.0	0.0	0.1	14.0	11.2	0.0	0.0
	BASIN 3	5.5	13.8	3.1	20.6	6.2	0.0	0.0		0.0	0.0	0.0	0.0	0.0	0.0	0.7		0.0		0.0	0.0	0.0	0.0		0.0	0.0	0.0	13.9	8.9	0.1	0.0
	BASIN 2	4.6		2.3	14.8	5.1	0.0		2.8	0.0	0.0	0.0	0.0	0.0	0.0	0.3	0.0	0.0	0.0	0.0		0.0	0.0	0.0	0.0	0.0	0.0	10. 5		0.0	0.0
	BASIN 1	4.7		15.2	4.5			8.7	2.6	0.0	0.0	0.0	6.0	0.0	0.0	1.7	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		3.0	0.0	0.0
	DAY	1	2	60	*	ī.	9	1	8	6	10	11	12	13	14	15	1.6	17	18	19	20	21	22	23	2.4	2.5	28	2.3	28	29	30
	DATE MONTH	JUN.					_																	_		-		_		_	
		_	_									_			_					_	-	_					_	_			_,

ESTIMATED DAILY RAINFALL FOR HIGH FLOW ANALYSIS

1/day	BASIN 21	0.0	0.0	0 0	200) (7	12. 7.		0	9	5.7	0.2	9 6) ()	0	2	3 6	17		9 0	9 6	200))	3	3	⇒ c	5	5 . 4	13.0	0 0	0.0	23.3	0.0	0	9	17.5	3 6))	9	2.	-10	3	7	33.0	2 . 2 .
- 1.	BASIN 1	0.0	0.0	0.4	0.2))	5.5	12.6	ري دي	0	0.0	. J	0 0	0 0) c	3 6	2 0	7 0	7 4	7 0	, 0		7.0) c	200	20 0		0	2 0	0.7) C	0.0	24. 1	0 0	0 0	3 P	12. 9		5	0.5	2 0	7		7:1	2000	7.77
- 13	BASIN 19		0.0	0.0	0.0	3.0	15.	14.5	15.8	21.2	12.3	2.0	1 3	0))) c	30	7 6	- -	7 6	10	7 . 7 .	110	0 7	7.0	0,0	0'7	= c	22.8	5 07	α 7		4.1	0	0.0	4	3	200	i	9.4	8.4	24. 5	15.5	10.7	13.	ö
l.	58.51N 18	0.0	0	5.8		0.2					0.2	4 6	0.0	0,0	o .c	500	3 4	-	100	o c	7	1 0	200	7.0	2	3	7		ר נ	2 C	200	0.0	9.1	0.0	0.0	0.2	80	S.	3 6	3.4	7.3	5.4	5.4	2,5	19.4	14.4
į	BASIN 17	0.0	0.0	7.3	3	6.0	13.4	3.7	18.1	3.7	1.4	3.5	0.0			⇒ c	5	» «	-		7 4	13.0	o c	7.0	1.3) ;	2	16.5	10.	× 0	0 a	0.9	1.5	0.0	0 0	0.0	5	8 8	4 5	5.4	8.9	11.1	7.5	23.9	207	0.0
ļ	æ		0			. 8	28.6	30.0	34.3	46.3	2.8	0.7	0.0	0.0	90) c) 0			2	*	0 1	3	9) -	,		25.0	13.3	7 7	0.0	7.6	0.0	0	0	0	0	0.0	14.2	18.0	37.0	33. 2	7.77	5	U, U
Ī	BASIN 15	0	0.0		1.8	5	<u>س</u>	~	۵		0	.5	0, 5	4	- 6	ء ء د		2 10	,	9	4	-[•	7	13.2	. 3	=	اٍد	- -	14.3	7.7	5 U	4.4	0.8	0.0	0	0	- t	- 1	ات		5.3			13.8		-
	BASIN 14	0.0	0.0	0.0	0.0						5.3	3.6	0.0	0.3	0,0	3 c	9 0	3-	1 -	7 0	0 0	6.11	7	2	0.0	0.0		- 0			0 0	0.0	6.8		0	٠.,	0.0	٠,١	٠,١	13.9		35.0	31.7	25.0	77.7	ء\ د
	BASIN 13		0.0	0.0	1. 2	3.7	11.8	5.1	9.1	10.0	9.1	1.9	6 0	2.4	0.0	9 0	3	-	100	0 5	7 0	2 5	5	15. 2	e. 8	0.0		3.0	16.1	2.3	, ,	7.8	1.4	0.0	0.0		0.0	0.0	0	3 8	6. 2	21.8	23. 7	17.4	21.3	2
Ì	BASIN 12		0.0	0.0	0.0	9	22. 1	24. 1	27.6	36.6	2.8	3.6	0.3	0.5	0.0) (0 0) c	-	1 2		7) L	C.		0.5	0.0	7	0 0	15 0	10.0	7 0	0 -	5.8	0.4	0.0	0.0	0	0	0	11.3				23.4		7 7
	BASIN 11	0.0	0.0	0.0	0.0	0.4	2. 1			t .		7.2		6.4	0, 1	0.0	0.0		-	0 0	S 0) c	4		3.4	0		9	2.5	_ c	7 ° ⊃ •	20.5	0.4	1.1	0.0	0.3	0.0		0.0		3.5		34.9	35.4		7
	BASIN 10	0.0	0.0	0.0	0 0	4.9	18, 7	21, 9	23.9	29. 9	3.5	2.5	0.0	0.0	0.0) ;	= °) c	2	- - -	- ·	-	4. 5	6	0.0	0	3.5	0.0	12.2	80 1	0	÷ c	4.7	0.9	0.0	0.0	0 0	0 0	0 0	10.2	13.1	24.9	20.8	17. U	13.2	- - -
	BASIN 9	0.0	0.0	0.0	0.0	0.0	1.0	4.1	17.8	22.0	1.6	∞ ~	4.3	4.3	0.8	0		- -		200	0.77			2.8		-	8	0.0	9	0.0	-	- v	0.2	8.8	0.0	0.1	0.0	0	0.0	14.7	2.3	26.8	25.4	26.5	7.64	14.6
	BASIN					2.8			11.9	8.	ļ.,				- 1	-1.	. 1		L	1	╝.	_					ei	o	6	_	Ţ.	4	L	0	Ц		0	30.	89	18.	23.	19.	25.	2	_	17.4
	BASIN 7	0.4	2.8	2.2	0.7	3.5	6, 1	4.6	11.7	2.3	2.2	ω. 	3.5	0.0	0.4	0	5.4	70°		× :		13.3	19.1	12.7	2, 5	3.8	3.5	1.7	4.6	12.0	15.		3.8	5,3	3.9	3.0	0.0	35.5	10.6	22. 1	31.6	5.0	21.4	13, 9	28.3	13.
	BASIN	0.0	0.1	0.0	0.4	0,5	2.7	5. 5.	10.3	16.0	2.2	7.8	4.5	9.8	0.0	0	0	= - - - -	7		23.8	9	 	5.5	3.4	0.0	0.4	6.1		0.8		2.1	0.9	1.0	0.0	0.3	0.0	0.0	0.0	2.8	4.1	111.1	34.5	35.5	9.9	
	BASIN	0.0	2.9	0	19.0	0.1	11.4	11.8	16.9	2.1	4.5	13.0	4.5	0 3	0.0	4.0	1.6	2]		?	17.6	20.3	27.2	6.1	5.7	22. 2	3.8	2.8	1.5		21.7	0 1	0.0	0.3	9.2	0.0	0.0	7	17.3	20.1	41.7	5.8	21.0		ļ
	BASIN 4	3.2	20.5	17.2	0.8	8.0	13.5	7.8	30, 1	9		18.2		0.5	3.1	0.7	_1	با ص ح	4	4	4		4	Ц	ш	ш	57.4	Щ	2	5.2	5	200		ω ω	9.0		0.0	26.6	13.4	24.0	34.0	49.9	20.4	31.9	47.8	28. b
	BASIN	0.0	3.6	ö	23.	.0	5.		Ġ		v	12.	ιςi	0.0	0.0	0 0	_	4	4	1	4	4	_	Ш	_	0.1	0.0	Н	_	4.5	- 1	23.3	0	0.2	1.6	9,5	0.0	0.0	5.4	21.9	12.7	14.2	23.7	28.3	17.7	23.4
	BASIN	0	3.4	0.5	22.9	9.0		10.3	10.4	5.2	2	12.0	4.5	0.4	0.0	0.0	-4	0			}-	-		-	-	0.4		L	21.	5.4		21.5	9	L	L	1.6	_	0.0	ς,	Ľ	16.0	15.5	20.0		19.9	22.8
,	BASIN		0.8		10.9	4.1	5.2	7.3	36. 7	34. 2	8	8,1	3.4	2.7	0.0	0		0	2	12.6	10.6	35.2	8	25.3	11.5	2.4	41.7	7.7	20.5	8. 7	4	υ - -		Ļ	10.5	<u> </u> _	L	_	L	L	33.6	27.	10.	Ц	32.	_
YEAR 1973	ATE H Day	187	-	2	19	20	21	22	23	24	25	26	27	28	29	8	3			~ ·			ء،	-1	∞	6	10	Ξ	12			12	17	(2)	19	20	2	22	23	2	25	26	27	28	29	30
(2)	DATE	MAR										,.						APR.						:							-			-	 -			-					<u>.</u>			

TIMATED DAILY RAINFALL FOR HIGH FLOW ANALYSIS

(2) YEAR 1973		-		_ -	- 1-	-	- [_ ⊢		-	2		=	2	RASIN	RECTN		-	iz:	unit : E	ER / day
BASIN BASIN BASI	BASI 3	84S1	z	BASIN 4	BASIN	BASIN 5	BASIN B	BASIN B	BASIN D			BASIN 1	=		15 15	16 16	_	_	= I	207	21
1 33.5	L,	∞	5	18.6	10.4	4.8	_	9.6	_	32. 2			il		13.6	42.5	29.3			0	8
0 61.2	~	18	7			5.6	24.3	16.5	3	5.2		5.2			12. 6	8	10.9	11.4		10	13 6
20.4	-				18.3	7.1		0.5		9		4	5.0		က်	- 1	19.0	17. 2		00 C	χ) (C
6) 8)	0.0	7	5			0 1		20	-	000	٦,	5 c	- 0			5 C	7 7	0 0		2 4 2	110
1. 2 6. 0. 10	5 6	- =	-	7 0	23 1) P	e) c	9 4	o ~	5 0		- - - -		0	0 00		0.7	. 69	2	0.0	1
7.0	1	3		ر دي دي	c.	0 2		3 0	- 00	0.0		0.0	0 0	1	0.1			2.5		6.8	6.8
0.0 0.0 0.	0	0	0		0.0	0.0		0.3		0.0		0.0	0.0		0.0	卢	0.0	0.0	0.0	0.0	0.0
0.0	9	0	0.0		0.0	0.0	0.0	0.0	0	0.0	ᆿ	0.0	0.0		0.0		0.0	0.0		0.0	0.0
0 0 0	0		0.0			0.3	0.3			2.9	ᆸ	3.3	0.7	4	0.4			0		0	0.0
0.0	0	٦		0.0	0.0	0.0	0.0	0.0	ا	0.0	_	0	0.0	9	0.0	0	9 0	χ, α		72	15.1
0 0 0	e (Ĩ		8.9		0.5	1,1	-	ا .	2 .		(7) (2	0, 3	ri ·		100		⇒ ¢	⊃ a
0,0	5	٦)	7		χ 2		0.0	-		7,7	٦,	7 0		٦,	7	ءاد		0.7	1 6	7 0 6	0 0
0.0			-		8	9 0	3.2	0 0 0 0 0		= c	٦,	ر د د	24.0	۰	24.5			7 0	7 0	# C	0 C
0.0			200	æ 6	0		ص د د		4,	= c			-	5	0	⇒ļe	3 C) (0 0	2 C	90
)) (ī.L	9 6	n o	9 6)))		7 0	- -))	٦.,	0 0	0 0	50	0 0	- 1		9 6	2 4	0 0) C
000	0 .	Т	7 0	7 0	7 0	000	500	000	5 0	000	1	> C	2 -	- ار	70	i	-1) C) =	0
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		1			-		; c	0			1			0	0.0	ŀ	0.0	0.0	0.0	0.0	0.0
-	1.0	1	0.0	3.0		8.4	5.3	7.1	6	0.0	١.,	0.4		0	0.0	0	0.0	0.0	0.0	0.0	0
1 18.			5.0	0.9	0.7		0.0	0.0	_	0.0		0.0		0	0.0	0	1	0 3	88		0
0		l	0.5	0.2	0.2	4.4		0.0	ص	0.0	3.9	0.4	80	0	0	۰	- 11	2.7	200	7.2	ω c
0		- 1	0	0 0	0.0		0.0	0.0	4	0.0	0.0			0	0 0	=	_ (0.0	0.0) 0
∞ 6	9 6	- [000			4 0	0 0	000	06	4, c	000	4 C		N C	ء ت	ų.	o -	100	0 7 0	9 0) c
90	7.0	1	9 0	9 6	9 0) -	3 -	5 6		9 0			-		-	4		0		0.0
- c	900		0 0	7.4	2 4		- C	9 0	-		0	0	0	-	0	9		0.0	0.0		0.0
	0.0	1	0	10.4	2.7		0.7	0.2	-	4.3	0.0			5.2	0.0	'n	0.5	0.1	2.6		0.0
0		ı		0.0	0.0	0.0	0.0	0.0	0	0.0	0.0			-	0.0	j		0.0	0.0	- 1	0
0		1	2.5	0.0	14.4		0.0	0.0		1 .	11.9		2.0		0.0	0		0.0	0 0		0
0 0			0.0	0.0	0.0		0.0	0.0	0.0	0.0	0.0		1		0	힉	. 1	0	0.0	9	= =
0 0.		ll		0 0	0.0		0.0	0	0.0		0	0.0	0 0	0.0	0.0	ان	0.0	0	0.0	- 11) ()
0		. [0	0	0	0.0	0.0	0 0	F	0.0))) = 	= 0	⇒¦(0.0))	3 0))))
0,0				= °	0.0	= 0 = 0))	0.0		9 0	0.0))	ء د د)) (0	3 0) c	3 0	900)
) 		- 1) c) (500) - - - -) o o		000	- - - -	0 0) c	9 6			9		9 0		ι.	0
0.0	.1	- 1) c	-1	0 0	0 0) -					0 0				0	0.0	0.0		0.0
		ŀ		2						0	0	-		-	-	ı		0.0	0.0		0
90	900	1		.1	0		3		. ŧ .	0 0	0	0.0	0	0	0	0	0	0.0	0 0	0	0.0
				-			0	-	C	0	0	0	0.0	0.0	0.0	0	0	0	0.0	ι.	0.0
; -							0.0	0.0		0.0	0	0.0		0.0	0.0		0.0	0 0	0.0		0.0
	-1			и.			1.7	1 2	0	0 0	0	0	0	0.0	0.0	0.0	0.0	0 0	0.0		0.0
8		1		0		0.0	2.6	2.5	0.0	0.0	0.0	0.0	0.0	0:0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.1		1.4	3.4	2.8	9.0	7.6	ις • ·	0.1	3.2	0	7.3	0.0	0.4	0.0	2.8	0.0	0	0,0	0.0	0.0
1.5 0.0			1.4	5 9		10.2	5.4	0,0	0.1	0.6	0 0	0.5	0.21	0	0.2	0, 2	0.2		9. 1	8	4.6
		1						-													

ESTIMATED DAILY RAINFALL FOR HIGH FLOW ANALYSIS

n/day	BASIN 21	0.0	0.0	0.0) (9 6	0.0	0.0	0.5	0.5	0.0		200	e e	5 C	7		2.8	5.4	9.8	0.3	-7.	13.2	0.0	B (15.0	2 .	11.7	; ; ;	14.6	0	& 8	2.2	4	27 7	0	1 4	12. 3	16.1	3 C) - 	3 6	3 0	2
			0	0.0)))) C		0.5	0.0	0.1	0.2	0	0.0	= c	9 -	¥ 20	r	. 2	5.7	0.4	0.4	0.0	13. 7		0 0		n c	7 7	9 0	13,5	0.0			4.9					24.0		2 0	- -		
- 1	BASIN B	0.0	0.0	0 0	= c) = =	. 4	0.0	4.8		0.0	တ လ (ب م	- - -		. u	2 G	2.5	2.3	6.3	3, 4	1.4	0.4	0	0	3.2	~ .	20.00	200	13.4	6.1	16.0	10.0	6.7	10.4	5.0	71.0	30.0	22.4	δ. α	25.5	44.3	2 0	,
- 1	BASEN B.			-	0 0	2 C	200	2.8	0.9	1.2	3.3	0.3	2.0	, , ,		2 c	2 00	2 -	33.3	6.6	6.0	0.1	5. 1	0	0.0	21.6	χ (Э	2 c	3 11	i ri	0.3	3.4	3.7	2.1	14.2	0.5	7.79	13.8	6.4		4. ¢	7 7	2 L	,
ł	BASIN BA	0	0	0	56	2 0	5 ~	٦,	2.1	35	H	0.3	٥,	۵,	-i e	یاد	- C	۳.	ω,		9	1.8	7	-		ı,	٦,	7 %	-	0.9	1:1	1.0	4.1	1.3	0	80	4			7.5		17.7		2
	_	0	0.	0	5) = c	-	. =		r.			0,	_ .			# C	2 (5) 		6.6	6.	0		_	۳,	4	- 4	-	6	5.5	3.1		3. 3	4		∞ (5 6	7	LD (, ,	+	
ŀ	IN BASII	0 0	0 0	\perp	_) - -	\downarrow	2	3	25	5	7 0.		.,	- 6	.	1.	1_		1	Ĺ.		Ш		_1	_1	┙	4.0	_L	L	_	6	. 0	.4 1:		<u></u>			ار	- ·		Lu		
1	N BASII	0	0 0	0 0	0				2 7.		1 0.		28	_	-	+	+	+	+	-	 _	-	Н		_	_		-	+		0	0 9	1 1	7 1	8 1		2 26	82	7 41	9 18	+	7 2	+	4
	BASI 14	0	0	0	CD 6	5 6	ے - -	_			0.	0	اد،	ام	-	, 1	10	+	┧	∤ _	L	L	2 0.	Ц		4	+	+	╀	7			9 5.	4 12.	5.		_	4	4	4	4	:i:	1	4
	BASIN 13	0.0	0 0) 0	-	٦	∞	Ġ	æ		31		٥	1	2 5	1		67	<u></u>	ij	4		0	0	9	יי ני	- 6	-	~	i	1.	2	1	-			43.	22.	5	2 3.5	0	7
	BASIN 12	0.0	0.0	0.0	00	0 0	9 6	ic	3.2	9	2.	Ö	œ	;;;\ 		٦	7	100		14.	20.	7	I.	0		0 7	1.9	 4. c	- "	1.2	8	5.4	4.0	8.2	2 0	2 5	9 3	17.5	11.1	15.2	3.5	27.3	2 0	10.
	BASIN 11	0.0	0.0	0.0))	9 6	9 00	 	0.0	0.0	9.4	37.0	42.9	e e) (7 0	9 6	107	4.7	1.6	9, 1	7.8	1.0	0	0.0	4.1) ; ;	0		0.0	1.3	0.0	0.7	1.3	22. 4	26.2	57.6	31.5	0.5	12.1	2 5	17.3
-	BASIN	0.0	0.0	0.0	0) 5) c	000	3.1	0.0	3.2	0.0	7.8	29. 4	0	ء د د		9 0 4		18.9		2.2	1.3	0.0	0.0	0.0	0.0	1.0		0.0	6.3	3.9	3.8	5.8	0.6	0.0	9	4.8	2.3	12.4	0.0	2.1	6.5	4.0
	BASIN 9		0.0	0.0	0) - -	n c) - -	7.5	0.1	0.8	0.0	27.0	17.3	5	, ,		1 - 6	3 6	2	0.9	80	4.8	0.4	0.2	0.7	10.0	3.2	7 6	3	0.7	0.0	1.3	0.0	0.5	7. 2	15, 2	49.5	68.9	13.4	0.0	14.8		
	BASIN B	6	0.0			7.7		o oc	0 0	-i	0.0	0.0	19.4	50.9	2	77	- 1	15.7	- A		6.9	4.2	8.0	11.3	10.0	14.6		0 0	0 0	7 7		0.0	10.5	0.3	9.0	5.3	40.2	19.6	37.5	19. 2	8.4	27.4	- 0	100
	BASIN BI	0.0	0.0	0.0	0.0	2.2	0.0	- a	0.0	╀	L	ω ω	4	-		<u>.</u>	-		15.0	, -	Ļ	L.	ص	2	9	8	~	5 c		* 0	, ~		5	_		97	L)		60	62	ω.	39.1	,	5
	_	L							-			5	8	6.0	٠,			200	3 10		2	6	L	0	0	2	_	6,	20 0	7 . 0		# 0	-		0.7		_	8	8		4	6	٥	4
	IN BASI		6	0	0	귺.	4 0	5 C	2 0	65	-	0	.6	_	7	٦.	- (- 4	ο α <u>ς</u>	0 00	0 00		147	_	2	0	6	دي و		٠,٠	-	. 0	2.	0.0	_	3.8		9.4	1 4	. 5	87	.8	٦,	
	N BASIN	0	0		0 0		4 ×	* -	Ľ	Ļ.,		2 0.	0 1		4	ລ ເ ຂ	7,	7 3	ļ	, -	╀	5 25	80	3 0.	7 E	Н	30	∞ (- -	9 0	, 6		2 16	_				3	4 35	5 13	5 20	1 23	40	3 23
	BASIN 4	6	=	0.0	\dashv	0 2	0 c	.	3 60.	╄	32.8	Н	5.	4			-	1	3 6	1	9 16.	_	L	5 15.	H	Ц	3 16	4	2 C	, - , -	2	1	Ľ	_	0 14.	7 5.1	Н	Н	Ц	\$ 54.	4	4	22.0	8
	æ				0.	4	+	5 6			L	0	Ц	5.5	4	4	7	0	-	,	2	12	5	Ö	4	∞	£	0 9	≘ °	9	, -		7		6		Ŋ	15	31.	5.	7	45.	۽ اُت	٥
	BASIN 2	6		0.0	0.0	6.		5 0			0.0		Ö	9		اٰ	7	23.5	9 1	200		17.9	5.2	0.7	9.9	12.5	72. 2	0.5	47. 7	0.0		0	3.3	0.0	9	-	θ.	42.8	34.	Ą			4.8	105.8
	BASIN	0		0.0	0.0	60 t	7	-10	2 4	3 6	0	2.4	9	0.0	9.3		= -		ς .	7 2	43.7	28.5	9	5.8	24.8	19.1	19.7	5.5	14	0 0	i u		6		-	5.7	17.8	167.3	15.5	20.8	8.7	33.9	30 c	38.5
(3) YEAR 1974	E DAV	1		18	13	20	7	77	67	35	28	27	28	28	e		1	7	7 <	,	عا د		. ∞	6	2	=	12	13	-	13	1	18	10	20	1-	22	_	1	-	26	—	28	57	30
(3) YE.	DATE	MAR										···				-	APR.															,								:				

STIMATED DAILY RAINFALL FOR HIGH FLOW ANALYSIS

(3) YEAR 1974

BASIN	21	20.1	0.7	0.0		0.4	7.5	4.7	2.9	2	5		00 i	ස ල	0.3	9. Đ	6.0	0.0	0	0.0	0.0	0	0.0	4	13.6	0.5	0.3	0.0	0.1	4	3,3	0.0
BASIN	-		0.1	0.0	ე.	0.0	7 8	4.9	0.0	0.6	0.0	0.0	0.5	0.0	0.0	9. 7	6.2	0.0	0.0	0.0	0.0	0.0	0.0	0.0	13.7	- 8 0	0.4	0.3	0.0	4.		
BASIN		3.3			3.3	3.0	0.2	0.1	20.2	8.2	32. 3	4.9	13.7	5.3	6.1	1.0	4.9	0.0	9.0	0.0	0.0	0.0	0.5	3.0		3.3	1.9		3.5	3.1	.1	0.0
-		8.7	2.2	0.1	0.1	0.1	2.9	1.8	0.7	9.0	1.2	0.2	3.1	0.3	0 3	7.4	2.5	0.0	0.0	0.0	0.0	0.0	0.0	6.1	5.2	12.0	5.5	4.8	0.2	1.7	10.2	5.4
BASIN		2.0	5, 8	1. 2	0.0	0.0	0.4	0.2	0.1	11.7	0.1	0.1	3.4	0.4	0.7	5 3	1.1	0.0	0.0	0.0	0.0	0.0	0.1	0 0	0.5	14.9	8.9	6.0			11.2	
₽~	1.6	0.0	33.0	2.8	0.0	0.0	0.0	0.0	0.0	11.3	1.7	1.1	2.8	4.5	9.6	1.7	10.7	0.0	0.0	0.0	0.0	0.0	1.1		0.0	0.0	0.0	0.0	5.2	3.4		0.0
BASIN	15	0.5	14.7	5.8	0.0	0.0	9.0	0.3	0.3	3. 2		0.2		0.7	1.5	0.9	1.7	0.2	0.0	0.0	0.0	0.0	0.2	0.0	0.0	1, 9	0.9	0.8	1.0	0.7	1.4	3 D
	14		30.5	**		_	0.1	0.0	0.1	9.9	1, 5	0 -1	2.5	د. م	8.4	1.5	9.4	0.0	0.0	0.0	0.0	0.0	1.0	0.0	0.0	0.0	0.0	0.0	5.4	3.0	0.0	1.5
	5		15.7	6.4	0.0	0.0	0.7	0, 3	0.4	2.0	0.3	0.2	0.5	ر ص	9	0 3	. 8	0.2	0.0	0.0	0.0	0.0	0.2	0.0	0.0	0.0	0.0	0.0	1.0	0.8	0.0	9.0
	12		27.3	2.6	0.0	0.0	0.0	0.0	0.0	9.5	1.4	0.9	2.3	3.7	8	1.4	8.7	0.0	0.0	0.0	0.0	0.0	6.0	0 0	0.0	0.0	0.0	0.0	5.0	2.8		
BASIN		-	3.5	4.1	0.0	0.0	0.4	0.2	0.2	1.1	0.1	0.1	0.2	0.4	8.0	0.1	6 0	0.1	0.0	0.0	0.0	0.0	0.1	0.0	0.0	0.0	0.0	0.0	0.5	0.4	0.0	5.8
2	2	0.0	23. 1	2.0	0.0	0.0	0 0	0.0	0 0	7.9	1.2	8.0	2.0	3.2	6.7	1.2	7.5	0.0	0.0	0.0	0.0	0.0	0.8	0.0	0 0	0.0	0.0	0.0	4.3	2.4	0.0	0.0
BASIN		L	18.4	2.8	0.0		0.2	0.1	0.1	5, 6	0,9	8.0	1.4	2.5	5.0	8 0	5.2	0.0	0.0	0.0	0.1		0.5		0.0	0.0	0.1	0.0	3.0	1.7	0.0	2. 1
₽-	00	6.9	10.6	6,3	9.0	0.3	1.5	10.2	5.9	25.1	2.7	5.2	1.4	5.6	1.4	0.2	2.2	0.1	0.0	0.0	0.0	0.8	0.3	0.1	1.1	1.2	13, 6	9.0	9.0	0.5	0.0	3, 8
BASIN	:	9. 2	5	۵	5.4	2.0	3.6	10.4	9.0	35.7	13.7	7.5	5.5	9.7	5.5	8	2.1	0.0	0.0	0.0	0.0	2.2	0.3	0.2	1.1	1, 2	15.7	0.8	2.7	1.4	0.1	1,4
_	ص	0.0	10.3	4.8	0.0	0.0	0.5	0.2	0.3	0.9	0.5	0.2	0,3	0,8	0.3	0.1	0.8	0.5	0.0	0.0	0.0	0.0	0	0.0	0.0	0.0	0.1	0.0	0.4	9.4	0.0	7.0 T
BASIN		5.0	4.4	6.0	0.1	0.0	1.7	0.0	1:1	2.2	5.3	Ι.		31.9	10.6	9.0	0.0	16.9	0.0	0.0	3.9	0.0	0.0		0.6	0.5	8, 1	1. 8	0.4	0.4	0.0	0.3
BASIN		25.5		20.6	15.0	20,	31.1	0.2	1.9	10, 1	4.8	15.1	8,7	15. 2	20.0	2.1	17.4	0.0	0.0	0.1	7.2	17.1	2.5	- 6	1.4	0.0	28.5	4.1	1.6	0.9	9.0	0.1
		54.8	5.2	9.0	0.0	0.0	0.1	0 0	0.0	1.4	0.4	0.5	13.4	7.7	11.4	0 5	0.0	1.3	0.0	0.0	0.1	0.0	0.0	0.0	0.0	0.0	7.9	13.0	0.1	4.6	0.0	0.0
BASIN BASIN	64	222. 3	24. 1	0.0		0 0				5.7	0.4	0.8	52.9	24.0	48.8	- 6	0 0	0.0	0.0	0.0		0.0	0.0	0 0	0 0	0.0	30.5	52.0	1.8	18.5	0.0	0.0
BASIN		69. 2	-	1.2	1.2	0.3	0.0	0.0	24.7	4.8	3.1	5.9	14.0	10.5	32.0	3.1	0 0	0.0	0.0	0.0	0.1	0.0	0.0	0.0	0.0	0.0		11.2	9.8		0.0	9.4
	DAY	-	L	~		2	ے	-	8	6	10	=	122	13	-	15	9	17	18	13	20	21	22	23	24	52	26	27	28	29	30	31
DATE	MONTH	MAY								_																						

ESTIMATED DAILY RAINFALL FOR HIGH FLOW ANALYSIS

(3) YEAR 1974

10 / C/3/y	BASIN	21	0.6	- t	ŀ	0	- 1	- 1	0	- 1	- 1			- 1	•			- 1	0	0.8	0.0			0.0	9	0.0		0.0	3.7	0.2	7 2	15.0
1016	SASIN	20	0.0	0.0	0.0	0.0	0	0 0	0 0	0	0.0	0.0	0.0	0	0.0	1.4	0.0	0	0.0	0.0	0.0	0.0	0 0	0.0	0.0	0.0	0	0 0	4.7	0 0	8.5	14. 9
	N S	19	4.4	4,4	6.5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0	0	5 3	8 8	- 1	- !
	BASIN	18	0.2	0.2	0.3	0.0	0.0	0.	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0	0.0	20.3	0.4	3.6	5.7
									0.0		0.0	0.0	0.0	0.0	0.0	0.1	0.0	0.0	0.0	0.0	0	0.0	0.0	0.0	0	0	0.0	0.0	24.4	2.4	3.0	0.0
	BASIN	16	0.0	8.3	13.4	0.0	0.0	0.0		0.0	0.0	0 0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0 0	0.0	0.0	0.0	0.0	0	0	4.5	16.4	18.5	0.0
																				٠	L					0.0					8.4	_
	BASIN	14	0.0	7.7	12. 4	0.0	0.0	0.0	0 0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	4.3	15.2	17.1	0.0
	BASIN	13	0.	4.8	7	0.	0	0	0			0.0			0.0		Ш				1	ŀ	0.0		. 1	0.0						0.0
	BASIN	13	0.0	7.3	11.7	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0	0 0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	4.0	14.4	16.2	0.0
	BASIN								0.0																							
	BASIN			L	L	L		L	0.0		L		Ŀ	L	L	<u> </u>		L	L	L	L	L	L	L	Ц	L	Ш	Ц		Щ		0.0
				ŀ					0.0		L	_	_	L	L	L	_	L		L	-	L	L	L	_		_	L	L	L		0.0
	BASIN	∞		2.1						L	L	L		L	L	L	L	L	6	9		L	ö		0	0.7		Ë	1.	4	6.2	1.3
	BASIN		ı	l					0.0	١.	ŀ			l				1				١.		1		l	L	L	L		5, 5	6.7
	BASIN	ء	0 0	3.4	5.4	0.0	0.0	0.0	0.0	0.0		0.0	0.0	0.0	0	0.0	0.0	9	0		0	0	0.0	0.0	0.0	0.0	0.2	6	1.9	9.9	7.4	0.0
	BASIN	L?	1 8	5	0.2	0.0	0.8	0	0	-	0	0 0	0.0	7.3	8 1	8	0.5	-	0	2		L	0.0	0.0	0.0	L	Г	4.8	2.4	9.3	0.3	0.0
	BASIN	4	5.4	7	-	0	-	2	ļ.,	2.5	L	L	L	=	╂-	3.4	0.9	17.4	9	╀	╀	╀	╀	20.2	0.0	6.7	-	╀	-	7	16.	0
÷	PASIN	۳.	=	32.7	9	0.0	0.0			0		0.0	L	-	0.0	0	0.0	-		-		6	0.0	c	0	0	2.8	0	L	~	8	
	BASIN	2	-		L	0	0 0	L	L.	L	-	L	L	c	_	L	L	L	6	L	-	L	c	L	c	0		L	-	0	0.0	Н
	BASIN	-		Ľ	L	2.2		L	0 0	L	L	ļ_	L	Ļ	ļ.	ļ.,	Ļ	ļ.	Ļ	╀	L	╀	L	<u> </u>	ļ.,	0.0	٥	~	_	6	0	
	DATE	TH DAY	1	٠	6	7	100	2	-	00		=	=	-2	12	7	-	-	E	-	=	12	6	22	23	24	25	26	27	28	29	30
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ESTIMATED DAILY RAINFALL FOR HIGH FLOW ANALYSIS

(4)-a at 1H8 and Mkombzi Dam Site for 5 Year Return Period (YEAR 1974 Type)

ME/day	BASIN 21	0.0	0.0	0) c		0.0	0.0	6.4	0.4	0.0	8	9	4	0	7:1	0.3	6.3	2.0	3.9	9	0.2		9.	0	0.0	11.1	0.0	12.4	9	9 9	10.6	0	5.4		3.4	20.1	0.1	1.0	8. 3	11.7	0.3	7.3	0.1	0.0	0.0
	10er i	0.0	0 0	0	000	0	0.0	0.4	0.0	0.1	0.2	0.0			0	7.3	0.3	5.0	2.5	4.2	3	0	0.0	9.9	0.0	0.0	12. 1	0.0	12.9	0.0	0.0	8	0	5.	0	3,57	20.3	0.0	3.3	8.8	10.7	0.0	ფ	0.5	0.5	0.0
	BASIN 19	0 0	0.0	000) c	0 0	3.0	0.0	3.4	3, 7	0.0	2			8	1.9	S 9	9.0	3.8	1.7	ري دي		0	3	0.0	0.0	2.3	2.2	3.5	15.1	8. B	9.7	4.4	11.5	7.2	4.8	7.5	3.5	15.2	21.7	16.2	4.9	23. 9	32. 1	6.3	7.6
	BASIN 18	0.0	0.0	0 0) C	8	0.1	5.5	0.8	0.3	2.4	0.2	0.5	7 0	0 0	6.0	4.6	7.1	∞ ∞	2.4	4.8	4.3	0.0	3.7	0	0.0	15.7	0.5	4.9	0.7	6.4	0.4	0.5	2.4	2 7	1.6	10.3	0.2	48.7	10.0	4.6	0.2	3.5	3.5	7.2	0.4
	BASIN 17	0.0	0.0	0.0)		0.5	7.1	1.5	1.1	3.0	0.5		4.2				7.6		1.9	6.2	5.5	1.3	8 0	0		14.8	1.5	1.5	6 7	0.8	0.7	0	0.7	3.0	1.0	4.3	9.0		12. 6	8.2	3.1	3.0	16.0	10.3	2.4
	BASIN 16	0.0	0.0	0.0	3 C	9 0	5.3	0.0	2.4	1.8	0, 7	0.0	1.5	8 7	1.7	0.0	9.0	6.7	15.0	3.4	4.8	7.2	1.4	0.0	0.0	0.0	1.7	3.9	5.6	12.7	8.8	2.8	9.0	ς; σ	က	9 6	3 9	5.6	14.3	28.9	11.7	8.3	22. 4	55.5	12.2	14.4
	BASIN	0.0	0.0	0.0	= c	0	0.5	0.3	5.4	0, 3	0.4	1.2	20.8	20.6	4.2	0.3	7.5	8.0	2. 1	3.5	2.8	1.6	7.7	2.6	0.4	0.0	2.0	5.1	2.9	3.4	1.2	0.6		0.0	0.7	1.0	6 0	1.3	19.0	20.3	30.2	13.1	4.6	13.3	6.2	7.9
	BASIN 14	0.0	0.0	0.0	⇒ c		5.7	0.0	3.8	1.9	0.1	0.5	2.7	4.6				6.9		1		2.6	3.0	0.1	0 0	0.0	1.8	5.3	9.0	16.8	9.1	3.0		5	3.7	9. 2	4, 2	9	15.4	32.3	14.3	6.4	24.7	60.3	12.7	15. 1
	BASIN 13	0.0	0.0	0.0))	9 0		0.0	6.0	0.4	0.0	1.4	23. 1	24.8	4.5	0.0	7.6	1.8	1. 2	3.8	2.2	0.7	8.4		0.5		0.4	5.0	3.9	5.1	1.8	0	2.0		0	1.8	0.8	1.2			31.5			17.0		
	BASIN 12	0.0	0.0	0.0	⇒ c		1.7	0.0	2.3		1.8	0.0	6.3	20.6	0.3	0.0	4.2	8.2	29. 7	2.5	10.4	15.1	1.7	0.8	0.1		9 0	1.4	2.5	5.3	3.7	0.9			2.9	0.9	1.4	æ.	8	12.7	8.0	11.1	7.2	19.8	9 2	7. B
	BASIN 11	0.0	0.0	0.0	3 0	9 0	0.0	0.0	1.1	0.0	0.0	0.3	26.8	3	4.5	0.6	1.9	9.4	1.9	2.3	3.4	1.2	9.9	5.7	0.7	0.0	0.0	3.0	5.0	2.7	0.3	0.2	~ O	0	1.0	0.0	9 0	0.9	16.3	19.0	41.8	22.9		8. 8	4.4	9.0
	BASIN 10	0 0	0.0	0.0	= c	9 0	0.0	0.0	2.2	0.0	2.3	0.0	5.6	21.3	0.0	0.0	1.9	9.0	36.0	1.9	12.2	18.2	1. 8	0.9	0.0	0.0	0.0	0.0	0.7	0.0	1.3	0.0	4.6		2.6	1 7	7 0	0.0	1.1	3.5	1.7	0.6	0 '0	1.5	3.3	3.3
	BASIN 9	0.0	0.0	0.0	0 0	7 0	0.0	0,0	0.9	0.1	0.5	0.0	9.61	12.5	4.7	3.3	4.6	8.1	2.2	2.3	3.8	4.4	8.2	3.5	0.3	0.1		7.3	2.4	1.4	1.7	1.0	0.5		0.9	0 0	10	5 2	11.8	35.9	50.0	9.7	0.0	10.7	7.2	10.2
	BASIN 8	0.0	0.0	0.0	0,0	0	0.0	5.2	0.0	3.0	0.0	0.0	14.1	15.2	3.6	8.9	5.2	12.7	11.4										L.,			0.3	0.7	0	7.6	0 2	† 0	3.8	29. 2	14.2	27.2	13, 9	6.1	19, 9	3.4	5.8
	BASIN 7	0.0	0.0	0.0))		3.0	6.4	0.0	12.7	0.0	 	12.7	-	0.8	10.6	11. 7	12. 7	16.6	11.5	$L^{*}L^{*}$	1 9	1.8	7.0	20.1	8.8	15.8	3.2	6.5	15.4	1, 0	0.0		0	8.0	2.3	4.0	5.7	22.9	12.8		17.6	10.7	28.3	13.4	16.7
	BASIN 6	0.0	0.0	0.0		90	0.0	0 0	0.7	0.0	0.3	0.0	25.2	34.0			0.2	5.0					5.3		0.7	0.0	_	1.5		2.8		0.0		1			0.5		15.6	12.9		24.3	0.3	7.9	4.0	
	BASIN	0.0	0.0	0.0	9 -	110	0 0	0	45.3	1.7	12.8	0.0	1.2	7	0.3	0.1	9.8	1.2	ж Э	2.0	2, 1	P . G	18.2	22.8	0.1	4.5	10.1	22. 4	0.2	7.5	3.0	4	10.1	0	11.8	0.0	0.0	2.7	2.9	21. 3	25.5	9.8	14.7	17.2	33, 5	21, 1
	BASIN 4	0.0	0.0	0.0	0 0	3.06		0	43.8	4.0	23.8	0.2	3.6		0.9	1.3	3.1	2.7	9.2	4.3	0.8	12.2	8.4	12.9	11.6	8.5	3.2	12.0	0.5	13.0	12.7	0.9	1.5	0	11.7	2.0	10.2	3.7	4.4	36, 5	33.6	33.6	14.8	29.8	18.5	26.3
	BASIN	0.0	0.0) 	9 0		0.0		0.0	0.0	0 0				0.0	2.0	12.0			10.9	2.3					5.9	38.6	9.0	22.3	0.0	0.1	7.	0	1.7	0 0	0.0	0.5	3.9	11.3	23. 1	4.1	1.6	33. 1	4.8	
	BASIN 2	0.0	0.0	0 0) 	× ×	0.0	0.0		0.0	0.0		0.2	0	0.7	0.3	3.6	17.0	1.3	1.5	14.7	12.5	13.0	3.8	0 5	7.2	9.1	52. 4	0.4	30.9	0.0	0.3	1.1	0	2.4	0 0	0 0	1.0	þ þ	31.1	25.3	3.3	1.4	46.2	3, 5	76. 7
	BASIN 1	0.0	0.0	0.0	0 0	4 P.	0.8	0.0	10.4	2.6	0.0	1.7	5.0	0 3	4.7	2.7	8.3	8.3	9.9	10.7	3.8	31. 7	20.8	4.8	4.2	18.0	13.9	14.3	4.1	10.8	0.0	1.5		0.0	5.0	0.4	1 0	4.1	12.9	121.3		15.0	5.3	24. 6	1 1	27.9
	DATE TH DAY	•	-1	8	2	3 2	22	23	24	25	26	27	88	53	39	31		2	m	-5	'n	9	_	∞	6	10	11	12	13	14	15	16	12	18	19	20	21	22	23	24	25	2.6	27	28	29	30
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ESTIMATED DAILY RAINFALL FOR HIGH FLOW ANALYSIS

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BAS IN	21	14.5	C)	0.0	9.3	0.3	2	3.4	2.1	0.3	23	0.5	13	9.4	8.2	5.6		0	8	0	0	0	0.0	0.3	8.8	0.3	0.2	0.0	0	3.2	2 8	ć
BASIN B	20	14.8	0 1	0.0	0.0	0.0	5	. c.	9.0	0.4	0.0	0 0	0.1	0.0	0.0	7.0	4.5			6		0.0	0.0	0.0	65 65	1.		0.2	0.0		2.8	
BASIN	ď	4	4 3	1.1	2.4	2.1	0.2	0.1	14. 6	6.0	23.4	3.5	10.0	4.6	4, 5	0.7	3.5	0.0	0.0	0.0	0.0	0.0	0.4	2.2	2.2	2.4	1.4	0.0	2.5	2.3	4.0	c
BASIN	82	5.3	1.6	0.1	0.1	0.1	2.	1.3		6.5		0.1	2.2	0.2	0.2		1,8	0.0				0.0	0.0	0.1	3.8	8. 7	9	3.5	0	1.3	7.4	٥
BASIN	=	1.4	4. 2	0.8	0.0	0.0	0.3	0.2	0.0	8.5	0.1	0.1	2.5	0.3	0.5	3.9	0.8	0.0	0.0	0.0	0.0	0.0	0.1	0.0	0.4	10.8	4.9	4.4	0.4	0.3	8, 1	3
BASIN	9	9	23.9	2.0	0.0	0.0	0.0	0.0	0.0	8.2	1.2		2.0		8.9	1.2	7.8	0.0	0.0	0.0	0.0	0.0	0.8	0.0	0.0	0.0	0.0	0.0	4.5	2.4	0.0	U
BASIN	-1	9	10.6	4.2	0.0	0.0	1 .			2, 3	0.5	0.1	0.8	0.5	1.1	0.6	1.2	0.1	0.0	0.0	0.0	0.0	0.1	0.0	0.0	1.4	0.6	0.6	0.7	0.5	1.0	is (e
BASIN	4))	22. 1	2.5	0.0	0.0	-	0.0	0.0	7.2	-	0.7	1.8	2.9	6.1	1.1	6.8	0.0	0.0	0.0	0.0	0.0	0.7	0.0	0.0	0.0	0.0	0.0	3 9	2.2	0.0	-
BASIN	2) - -	11.4	4 7	0.0	0.0	0.5	0.2	0.3	7	0 2	0	0.3	0.5	1.2	0.2	1.3	0.1	0.0	0.0	0.0	0.0	0.1	0.0	0.0	0.0	0.0	0.0	0.7	0.5	0.0	رد. دو
BASIN	77	0.0	2 K	5		0.0	0.0		اہا	9 9	-	0.7	1.7	2.7	5.6	-1	6.3	0.0	0 0	0 0	0.0	0.0	0.7	0.0	0.0	00	0	0.0	3.7	2.0	0.0	~
BASIN	7 0		2		0	0.0	0.3	0, 1	0.2		0.1		0.7		9.0		-	0.1	0	0.0		0.0	0,1	0	0.0	0	0		0.4	0.3	0.0	2
BASIN	2	ء د د	- T	1.4	0	0.0	0.0	0.0	0	5.7	5 0	0.0	1.4	2.3	4.9	6.0	5.	0.0	0.0	0.0	0.0	0.0	9.0	0	0	0	0.0	0.0	3.	1.7	0.0	
BASIN	, ,	7 .	2.5	7.0	0,0	9	0.2	0.0	0	9,0		<u>ء</u>		2	3.5	9	8	0.	0	0	0,1	0.0	÷	0	9	0.0		0.0	7.7	7 7	o .	
BASIN	-			4		7.0		7.4	4.3	79.7	7,0	× ,	3	-	-	7.7			0.0	0	0.0	ے د	7.7		æ ,	χ. Ο	5		م ت	4.0) (7
BASIN 7	0				-	7.	2.6	.5	4.3	53.9	27 L	2.5	3.	-	7	2	1:3	0,0	9	0.0	0.0	ο (7.0	7.5			-1	9 0	0.7	7. G	- i	-
BASIN	 -	u S		2	3	3	0.4	0.5	70	o .	,	7.0	7.0	اء	ς, Ξ	- -	ر د ا	4.0		0.0	90	9,	5			∃ .	- 6	5	200	2 c	a .).
BASIN	, e	900	7 .	3	3	=	7		æ .			10.0	7.6	7.53	- 1	2	= =	2,3	0.0	- C	7	1	1	7	5	0 2	200	7 0	2 0	200	3 0	7.0
BASIN 4	- X			7 7	, 2	- 1	22. 5	0	4 0		200	200		11:0	14°		2	0 0))		2.5	5 .71		4	٠l.		2 6	5.7	7 .7	- u	5 6	٦.
BASIN 3	30 7	α ~	3		2 0	5	a (9 .	7:0		7 .					- -		o 0		3 6) 	300) :		e .	7 .	40		9.0
BASIN 2	161 2	٠.	9 0	9 6	3 0	5 0	200	9 6	8.7	7 0	2 0	300	0	,	7		2 0) ()))	3 c	200	90		5 6	5 6) -) :	77.7	3/- 2	7.5	2 0	3 6	;
BASIN 1	50.2	An A	0 0		2 0	7 0	0 0	0.0	, c	2 6	3 0	, 0	3 4	0000	7 6	2 0		900	000) j	100				3 6	9 9		0 6			5 0	
DAY	_			-	* 14	, ,		•	0 0	2		1	-		ű		-	10	9 =	r ç	3	1	16	,	,	36	07	770	3 6	3 6	3	1
MONTH	Ž																			-												

ESTIMATED DAILY RAINFALL FOR HIGH FLOW ANALYSIS

(4)-a at 1H8 and Mkombzi Dam Site for 5 Year Return Period (YEAR 1974 Type)

	-			,														,			_		_			,		_		,	-	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,
ma/day	BASIN	21	0.5	0	0.1	0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	9.0	0.0	1.0	0.0	0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	2.7	0.2	5.0	10, 9
nit: #	BASIN	20	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.8	0.0	0.0	0.0	1.0	0.0	0.0	0.0	0.0		0.0	0.0	0.0	0.0	0.0	0.0	0.0	3.4	0.0	6.2	16.8
		5		3.2	4.7	0.0	0 0	0 0	0 0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	ට ප	0 0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	3.8	6.4	6.0	3.3
				0.2	0.5	0 0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0 0	0.4	0.0	0.0	0 0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	14.7	0.3	9 2	4.1
	BASIN		6	0.9	4		0		0.0	0.0	0.0		0.0	B. B	0.0	0.0		0.0	0.0	0.0		0.0	0.0	0.0	0.0	0.0	0.0	0.0	17.7	1.7	2.2	0 4
		. ,			9.7	0.0			0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	3.3	11.9	13.4	0.0
	z	15	5	١.,		0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	3.9	5.1	6.8	0.0
-	BASIN B		5	5.6		0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	3.1	1.0	2.4	0.0
		-	5	3.5	5.7	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0 0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.9	6.9	7.8	0.0
1	_	13	5	L	8.5	_			0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0), 0	0.0	0.0	0.0	2.9	10.4	1.7	0.0
	*	12	0.0	8	1.	0.0	0 1	0 (0 0	0 (0 .	0.0	. 0 .	0	0.0	0 (0.0	0 (0 (0.0	0	0 (0.0	0.0	0.0	0.0	0 (0.0	1	1 1	1 2 1	0.0
	IN BASI		_	9	·	0 0	0	0 0	0 0	0 0	0	0	. 0	0 0	0	0 0	0 0.	0	0 0	0	0 0	0 0	0 0	0.	0 0 .	0.0	0	0 (. 6	1	. 2	0 0
- 1	-	10	L	4	7 7	0 0	0	0 0	0 0	0 0	9	0 0.	0	2	0 0	0 0.	0	0 0	0 0	0 0	0 0	0	0	0 0.	0 0.	1	2 0	0 0	3	5 9	1 10	0 0
	z	5	_	2	2 3.	0 0	0	1 0	0 0	0	0	0 0.	0	0	0	0	0 0	5 0	0 0.	0	0	0	0 0.	7	0	1 0.	0 0.	3 0.	9	1 4.	5	9 0.
	-	_	1 6.	⊢	L	8 0.		3 0.				0	0		0 0.		0 0		0 0	0 0	0 0.	0 0.	0 0.	9	0 0.	0	0 0.	7 0.	0		0	9 0
ı	-		-	9	7.	5.	0	0	0.	0	0			.0	0.	0	0) 0.	0.	0.		\perp	0.		0.	6	9		4	4
	BA		0	~;	3.9	0.0	-	0 (0.0		0.0	0.0	-		0.(0.0		0.0	0.0		0.0			0	0.	0.0	0	-	1.4	4.8	5.4	0
	BASIN	ဆ	1	1.0		0.0	9.0	0.0	0.0		_		<u>-</u>		0.1					0.0	Ц			9. 0. 0.	_			3.5	1.7		0.2	-
	BASIN	4	3.9	5.5	1.2	0.5	1.1	2.1	0.1		<u>-</u>	0.0		8.4	0.2			1	0	0.0	0.0		<u>-</u>	14	0.0	4.9	- 1	8.0	0.9	1.2	11.9	0.4
	BASIN	3	0.0	23.7	9.4	0	0 0	0.0	0.0	0.0	9	0.0	0.0	0.1	0.0	0.0	0	0	0	0.0	0.0	0.0	0	9	6.7		2.1		ري س		0.0	0
	BASIN	2		8.8	0 0	0	0	0	0.0		0.0	0		0	0	0.0	0	0 0	0	0 0	0.0	0.0		0		0	0 2	10	1	0	0.0	0 0
	BASIN		0.0	17.6	1.8		0 0	0.0	0.0	0.0	0			F		0	0 0		0.0	0.0		0.0	0.0		0.0	0.0	- 1	6.4	9.3		0.2	1.1
	DATE	i DAY		2	6	4	ĸ	ص	-	∞	50	=		7	13	-	2	16	=	18	13	20	71	22	2	24	25	<u>5</u> 2	27	82	29	30
	á	MONTH	JUN.															_			<u> </u>											

ESTIMATED DAILY RAINFALL FOR HIGH FLOW ANALYSIS

(4)-b at 1H8 and Mkombzi Dam Site for 10 Year Return Period (YEAR 1974 Type)

RAST	212	=	0	0	0	0.	9	0.0	0. (0.5	0.5	0.0	1. (0. 8	6	9.0	٥. ها	0	7	2. [5.0	0	5	3	77			2	15.6		0.7	13. 3	0 0	8. [~		25 3	-	1.3	11 2	14.7	0	9.2	0.	0	0.0
unit:	20	0.0	0.0	0.0	0.0	0.0	0 0	0.0	0.5	0.0	0.1	0.2	0.0	0.0	0.0	0	9 2	0.4	7.4	3.1	5.2	0.4	2,0	3)	2) c	- L	7 0	16.2	0.0	0.0	12.3	0.0	6.7	1.2	4 5	25. 6	0.0	4.2	11.1	13.5	0.0	7.5	0.7	0.0	g .
BASIN	19	0.0	0.0	0.0	0.0	0.0	0 0	3.7	0.0	4.3	4.7	0.0	7.3	5.4		1.2	2.4	8 8	11.3	4.8	7.7	· ·	3 4		200	9 6	9 6	2	4.4	19.0	10.3	12. 2	5.6	14.6	9.1		5	9	19,1	27. 4	20.4	6.2		40.4	∞ •	3.6
BASIN	18	0.0	0.0	0.0	0.0	0.0	0.0	0.2	7.1	0.8	1.1	3.0	0.3	0.2	0.5	9.1	2	2	3. O			٦ د		- - - -	; c		10	0.7	6.2	0. 8	0.5	5.0	0.3	3.1	3.4	7.0	13.0				بن 8			9.1.		
+~			0.0	0.0	0.0	0 0	0.0	0.7	8.9	1.9	1.4	3.7	0.5	4			5.	8. 7	9. S	13. 1	7 7	×, c					18.7		1.9	2.3	1.0	0.8			در در	7	S i	7	200	15.5	7.7	رن دو	3.8	20.1	3	- n
	-1	0.0	0.0	0.0	0.0		0.0	9.9	0		2.3	6	0	61		7			×	18. 8	7	-	,				-	4.9	7.0	19.7	11.0	3.5	11.4	-	5	17.7	e (3 ·	18.0	4.4	14	10.5	28. 2	 - - -	13.4	18. 2
<u> </u>		0.0	0.0	0.0	0	0,0	0.0	8		5,7	<u>-</u>	0	9	26.2	70°	2.5	7,	4.	10.1	Q (ع ا د	ء د د	300	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	, ,	, =	2 5	6.4	3.6	4.3	LC:	0.7	9	8.	5,0	-		- 1	6.2.9	20.0	38.0	2	20	16.7	- 1	8.8
BASIN	1	0.0	0.0	0.0	0	0	9	7.1	0.0	7	7.7		9	2		7		20 0	o d) 0	9	7 000	, a		-	0	2.3	6.7	7.6	21.2	11:4	80	10.9	-	9.0	0	200	_ .	13.4	1	0.0	-	_ ,	5 0	200	13. U
BASIN		0	0.0	0	0	0.0	9	4.6	<u>.</u>	7.6	0.5			73.7	7		.1	م د د	2	2	•	ء د د	1	200			0.4	6.3	8	Ť	2.2	6.0	2.5	~ ~	5 6	7 7	0 -	C .	5 - 2	4.	58. 7	٦	٦.	4		
BASIN	+	0	0	0	0	0 0	- - - -	7.7	0,0	5 7		77	+	20 0	,,	-) c	2 6	2 2	9 . 6	3 -	1-	6		-	0.0	0.7	1.7	3.1	9					0 °	0 6	۱. ۵ ، ،	, o	0 0	,,	-10	200	5	5 6 B		2.0
BASIN	-+	0	0	0 0	0)))))))))	4 0	∩ (0) -	7 6	0 -	+	4	1	4	4	4	1	4_	Ļ	L	0.9	0.0	0.0	3.7	3	3.4	G. 4	_))	7.T	٠.	, 6	7 10	2 0	ם מ	0.70) 	_	4	-	4
BASIN		0	0	 ⊃ •	.1))) 	-	000	5 6	,,,		۱.	0 0		-	2 6	-	3 C	, =	22 0	_	1.2	0.0	0	0		6.0	_ ,	٥	اد	ri e	9.0	ر. د -	, u	P 0	3 -	* *			200	֓֞֞֝֞֜֞֜֝֞֜֜֝֞֜֜֜֝֜֜֜֝֟֜֜֜֝֓֓֓֓֓֓֓֓֟֜֜֝֓֓֓֓֜֝֜֜֜֝֜֜֜֝֜	, L	7 0	7 7 7
BASIN	,)))	0 0))))))	n 0) = = =	- -	-1-	7 0	0 0	2 2 2	- a	2 0	2 -	- 4	1	L	,	,	2 12	-∞			0.2	0, 1	3.5	3.0		7,	-i c	- 0) c	70	26	2 4	-1		20 62	200	100	0 0 0		200	77.0
BASIN	∞ 0) ()	D 0)) c	900) 	- 0	9 0	000		17.0	- 0	7 P	11.2	2 2	2 4	12.	, C	100	8 3	3,8	7.3	10.3	9.1	13.3		3.6	7 .		# ·) u) (-	9 4) «			, .	3 1.			1	, .	-
BASIN	-+))))) (_t	T.	1.	1	o -	1	+	1	\pm	+		2	7	╀	╂-	╀	╀	╀	╀	-	ļ.,	L	Н	-	-	- - 		_1_	. 1	1		1.	1.	1	1	1.	1	-	4	1	18.9	1.	7
BASIN	-1-)))	2 c) c) 0 0					5 0	- - - -	1	4.7 A	× •	-	‡	~	,	-	-	1	9 9	-		\dashv	4	6			7 0	╅	+	+	. C.	u	-		16.2	┢	30.5	,		,-	10.3	,
BASIN	٦,	5	ر ا	٦,	J.	1	, 0		200		10.00		- -) (E	, c-	000			C P	-	2.5	8.0	22.9	28. 7	0.1	5.6	12.8	28.2	بر در در	0,0	0 0	6 6	7 0	ν γ.	9 0	0	4	1	1.	1	ı	ı	1	42.2	5.5	
E	1	5		ء اد	5	٦,		3 -	1		20.00	,	4 6	-		9	3	2	Ι.	ur:	6	15.4	10.5	2	14.5		4	-+	7	+	+	- C	╀	8 7		1.		L.	1.	١.	1	1.		23.2	1	
BASIN	70	500	000						37.7	- -	0	0	« «	2.0	9.0	0.0	2.5	-	0	0 3				5.2	0.4	4.2	5	0,0			2 0	1 12			0.0	_	9	5	~	1	Τ.	1-	1-	6.0	┪~~	1
BASIN	+			00) «	-			100	0	0	0.3	0.3	0.0	0.9	4.0	4.6	21.4	1.	6	18.4	5. 7	6.3	4.8	0.7	9.0	1	Ļ	4	┸	L	1	0.0	0	0,0	0	1.3	L		8	01	∞		-	ıc	
BASIN	-	9 0	-		2 4	, c-	=	0.0	L			2	5, 3	65	5.9	L	L	L	L	ļ	L,		_		_	_		┸				1	1	L	L	Į		1		•	1	7.9	1	9.0	ы	
			18	0	200	21	22	23	24	25	26	27	28	29	30	31																12	т	7~-	_		1		_	-	-	←	+	29	_	
DATE	MAR																APR.										le-		-1- .			1,		1		L_	.			L		_	ا	لبا		

ESTIMATED DAILY RAINFALL FOR HIGH FLOW ANALYSIS

(4)-b at 1H8 and Mkombzi Dam Site for 10 Year Return Period (YEAR 1974 Type)

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RAS IN	21	ı	0.7	0.0	0.4	0.4	8	4.3	2. 5	0.4	4.1	0.6	1.6	0.5	0.2	80	5	0.0	0.0	0.0	0.0	0.0	0.0	0.4	12.4	0.4	0.3	0.0	0.1	4.0	3.6	0
RASIA	2	18.7	0.1	0.0	0.0	0 0	7.1	4.5	0.0	0.5	0.0	0.0	0.2	0.0	0.0	8	5.7	0.0	0.0	0.0	0.0	0.0	0.0	0.0	12.5	8.0	0.3	0.3	0.0	3.9	3.5	0.3
lz		les	18.0	1		2 7	0.2	0.1	18.4	7.5	78.4	4.4	12.5	ις 00	5.5	6	4.5	0.0	0.0	0.0	0.0	0.0	0.5	2.7	2.8	3.0	1.8	0.0	3.2	2.8	5.0	0.0
RASIR	00	8 /	2.0	10	0	0.1	2.6	1.7	0.7	8.2	1.1	0.5	8.2	0.5	0.3	6.7	2.3	0.0	0.0	0.0	0.0	0.0	0.0	0.1	4 7	10.9	5.0	4.4	0.1	1.6	9.3	6.3
	- 1		5.3	1.1	0.0	0.0	0.4	0.2	0.1	10.7	0.1	0.1	3.1	0.3	0.7	4.9	1.0	0.0	0.0	0.0	0.0	0.0	1 0	0 0	9.0	13.5	6.2	5.5	0.4	0.4	10.2	7.5
BASTN	-	0.0	30.1	2.6	0.0	0.0	0.0	0.0	0.0	10.3	1.5	1.0	2.6	4.1	8.7	1.5	9.8	0.0	0.0	0.0	0.0	0.0	1.0	0.0	0.0	0.0	0.0	0.0	5. 6	3. 1	0.0	0.0
BASIN	2		13.4	5.3	0.0			0.2		2.9		0.2	0.8	9.0	1.4	0.8 8.0	1.3	0.2	0.0	0.0	0.0	0.0	0.5	0.0	0.0	1.7	9.8	0.7	0.9	0.6	1.3	~ %
BASIN	7	0.0	27.8	3.1	0.0	0.0	0.1	0.0	0.1	9.0	1.3	0.9		3.6		1. 3	8.5	0.0	0.0	0.0	0.0	0.0	0.9	0.0	0.0	0.0	0.0	0.0	4.8	2.7	0.0	1.3
BASIN	13	0.0	14.3	5.9	0.0	0.0	9.0	0.3	0.3	1.8		0.2	0.4	0.7	1.5	0.3	1.6	0.2	0.0	0.0	0.0	0.0	0.2	0.0	0.0	0.0	0.0	0.0	0.9	0.7	0.0	8.2
BASIN	12	0.0	24.9	2.4	0.0	0.0	0.0	0.0	0.0	8.4	1.3	0.8	2.1	3.3	7.1	1.3	7.9	0.0	0.0	0.0	0.0	0.0	0.8	0.0	0.0	0.0	0.0	0.0	4.6	2.5	0.0	0 4
BASIN	1	0.0	8 6		0 0			0.2	0.2	1.0	0.1	0.1	0.2	0.4	8 0	0.1	0.9	0.1	6.0	0.0	0.0	0.0	0.1	0.0	0.0	0.0	0.0	0.0	0.5	0.4	0.0	r.
BASIN	2	0.0	21.1	1.8	0.0	0.0	0.0	0.0	0.0	7.7	1.1	0	1.8	2.9	6.1	1.1	6.8	0.0	0.0	0.0	0.0	0.0	0.7	0.0	0.0	0.0	0.0	0.0	4.0	2.2	0.0	0.0
	6 0		ľ	2.5	١,			0.1		ः	8			2.2	4. 6	0.8	4.7	0.0	0.0	0.0	-	0.0	0.5	0.0	0.0	0.0	0.1	0.0	2.8	1.5	0.0	1.9
BASIN	တ		9.7										-1	2	-	0	2.	0	0.0	0.0	0	0.7	0.5	0.1	1.0	1.1	12.4	0.5	9.8	0.5	0.0	3, 4
BASIN	-	2.4	6.4	8	5.8	1.8	3.3	9.5	5.5	37. 6	12.5	6	5.	8	9.0	8.1	1.9	0.0	0	0.0	0	2° 0	9	0.2	1.0	1.1	14.3	0.7	2.5		0	1.3
BASIN	ع	0.0	9.4	4.4	0.0	0.0	0.5	0.2	0.3	8	7	7	0 2	0	9.0	0.	0.7	0.4	0.0	0 0	0	0.0	- 0	0.0	0.0	0.0	0.1	0	0.4	0	0.0	6. 4
BASIN	LC)	4.6	4.0	0.8	0.1	0.0	1.6	0.0	0	2	2	13.6	5,3	- 2		0.6	0.0	15.4	0.0	e.	2	0.0	0	0.7	9.0	0.4	7.	1.5	0	V 0	0	0
BASIN	₩.	23.3	17.0	18.8	13.7	6.4	28.4	0.1	- -	3.5	- 1		- 11	13.8	18. 3	. 9			0		5 5		2.3	1.7	1.3		24.2	~	2	5)		0.1
BASIN		49.9	8	0.5	0 0	0.0	9	0.0	0.0		0	0.5	12. 3	7.0	10.4	0.4	0.0	7.	0	0	0	0 0	0.0	0 0	0	0	7.2	11.9	0	7 5	0 0	8.8
BASIN	2	202.8	22 0	0	0.0	0.0	2			- 1					44.5	1.8	0.0	0.0	0.0	0.0	0 3	0 0		0.0	0.0	0.0	27.8	47.4	9	200	:: C	0 0
BASIK		63. 1	20.8	1.1				0	22. 5	7	7	2,4	17.8	5	29. 2	2.8	0.0			0	5	0.0	- ·	0.0	0	n :	9	70. 7				0.3
	H DAY		7	~	7	<u>ن</u>	٥	~	ω,				7		14	12	9		2	5		71	77	2	24	22	0.7	7	87	6.7	≅	5
۵	MONTH	MAY						_																			-					

(4)-b at 188 and Mkombzi Dam Site for 10 Year Return Period (YEAR 1974 Type)

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햠	<u> </u>		9	~	_	0	0	0.0	0.0	3.0	9.6	0	0	0	0	~	0	3.8	0.0	0.0	0.0	0.0	0	0	0	0	0	0	3.4	3.2	.5	-
BB/da	3	7	`	_	_	Γ	Γ		Γ	ľ	_		_		_			_	Γ	_	ľ	ľ	_		_	Γ				Ĩ		H
ŀ	SASIA	ñ7	0	8	0 0	0.0	0.0	0.0	0.0	3.0	0.0	0.0	0.0	0.0	0.0		0.0		0.0	0.0	0.0		0.0	0.0	0	0.0	0.0	0.0	4.3	ι.		3.6
Į,	SASIA	£,	4.0	4.0	5.9	0.0	0.0	0.0	0.0	0.0	0.0	0.0		0.0	0.0	0 0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	4.8	8.1	7.5	4.1
	SACIN	18	0 1	0.2				0.0	0.0	0.0		0.0				0.5		0.0		0.0		0.0	0.0	0.0	0.0	0.0	0.0	0.0	18.5		3.3	
	Pasta		0	1.1	1, 8	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	22. 2	2.2	2.7	.5
200	58218		0.0	7.6	12, 2	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	7.5	14.9	16.8	0.0
11.01.01	DASIA			3.9	6.2	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	4.9	7.6	8.6	0.0
1, 1, 1, 1, 1	DEST.	1,4	9	2.0	11.3	0.0	0.0	0.0	0.0		0.0	0.0	0.0	0.0	0.0	0.0		0.0	0.0		0.0	0.0	0.0	_	0.0	0.0	0.0	0.0	3.9	13.8	15.6	0.0
11.000	DASIN		0 0	4.4	7.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0	0	0.0	0.0	0.0	0.0		0.0	0.0	0.0	-	0.0	0.0	0.0	0.0	2.5	8.7	3.8	0.0
21010	200	35	9	9 9	10.7	0.0	0.0	0.0	0.0	0.0	0.0	0	0.0	0	0 0	0.0	_	_		_	0.0	0.0	0	0	0	0.0	0.0	0.0	3.7	13.1	14.8	0 0
7,540	2.0.0	, i			3.8		0.0	0.0			0.0	0	0	0 0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0	0		0 0	0.0	0.0	0.0	1.3	4.2	5.3	0.0
⊢	2 5	+	⊃ ;	2.8	9.3	0.0		0.0	0.0	0.0	0.0	0.0	0	0	0	0.0	0.0	0.0	0.0	9	0:	0.0	0.0	0	0	0.0	0.0	0.0	3.2	11.4	12.8	0.0
ŀ	250	╁	1	7	_	9.0	0.0	0.0	0.0	9.0	9	0.0	4	0.5	4	ej -	6	o	0.0	4	0.0	9	0.0	0.0	0	0.	0.2	-i	1.6	2.5	ē.	0,0
0.40.10	250	,	c o		4.0	4		oj O	-		•		0	4	0	0	0.0	oj 	0			۱.	0.	8.0	0.0	0	0.0	9.3		5 60	(C)	1.1
ŀ	200	╁	+	+	-+	4	_	_	0.0	4	_	4	4	_	_	_	_	_	 		_			\perp		0.2	0 0	_	0	1	2	9.
ľ	- -	1	+	4	4	4	4	4	0.0		0.0	0		0.0	0.0	0.0	4	4	4	0		0.0	0	3	0.0	0	0	5		9	2.8	0
RACTN			1	'n	= ·	= -	9	_		-	4		4	4	0.1	4	_	6	4		6	_	0		=	7.8	11.8		7	0	4	 - -
BACTN		•		1		, i	1.4	2.6	0.5	2.2	4	0.0	1.3	10.5	0.2	r;	6	12	0	4	4	9	0 0	18	4	4	19.0	10.	-			0
BACIN		╀	2	7	4	4	4	_	4	4	=	1	4	4	-	0	oj (; -	=	=	0	0.0	D (_	⇒'	4	\downarrow	7	4. 2		0	2
RACIN		2	3 5	77.	_	=	<u>خ</u>	4	6.9	4	4	4	1	<u> </u>	= ·	.	6	=	=	=		=	=	4	⊃ °	_	ъj.		7.7		0 0) -
RACIN	т	c	╀	1	7	7	4	0.0	1	\downarrow	=	4	4	4	⇒	=	-	3	1	4	= •	=	=	٥	= 0	=	1		4	، اد	= •	7.
DATE	NTH BAY	NIII.		7 0	1		<u>ר</u>			~	20 6]:			-	7		2	1			3	7	72	5.3	74	67	97	17	×7 3	2	Ωg
L	Ş	Ē	3										_			_																

ESTIMATED DAILY RAINFALL FOR HIGH FLOW ANALYSIS

(4)-c at 1H8 and Mkombzi Dam Site for 20 Year Return Period (YEAR 1974 Type)

	IN BASIN		0.0	0.0			0	6.0	.1 0.5	1 0.6	2 0.0	0 1.3	0.0	.0 0.7	0.0	.1 10.7	0.5	<u>.,</u>	Σ	,	200	27 0	÷	-4 (200	, a	r	5	0			0 C		L		1.0 0.1	1.5	1.4 13.5	1.2 17.7	0.0		$1.0 \mid 11.0$
unit	N BASIN 20	0 0		0.0	4) 		0	2 0	7	0 0	8 0	4 0	7	4	S	-			ه م	5) :		о 9) - -							- 4		_	-5"			-	6	5	۱	7
1	8ASI. 19	_		0,	=	╡╸	4	0	ß	'n			Ц	4		-	<u>:</u>	4	4	4	+	4	4	4	-	-	╀	ļ	-	\vdash	14.	17 17	11	7.	3 11.	3.	3 23.	33	24	-	,	3.0
	BASIN 18	0.0	0.0	0.0	2,0) (200	8.5	0.3	1.4	3.6	0.3	0.2	0, 3	0.1	5	6.9	10.8	13.		7 6	e .	9	ų,) (33.0	8 0	7		9 0	6.1) (r	4	2.4	15. 6	0	73.	2	7.0	0	ì	n
	BASIN 17	0.0	0.0	0.0	9	3 c	000	10.7	2.3	1.7	4.5	0.3	5	6.3	1.2	9 2	18.5	11.4	15.8	7	57	xi c	2		0 0	200	2 2	2.3	83 83	1.3		1 7	4.5	1.5	6. 6	0.8	96. 1	19.1	9.3	4.6	ľ	e.
	BASIN	0.0	0.0	0.0	⇒ ⇒	5 C	0	0.0	3.6	2.7	1.1	0.0		13. 2	2.5	0	13.6		22. 7		2		7.7	D ,	000	216	3 11	8.5	23.8	13.3	4.2	. u					21.8			12.8	,	54 U
- 1	BAS1% E	1-	0.0	0.0	300		5 -		86 1.1		9.0	1.9	31.6	31.3	6.3		.11	12:1	3.5	7	2 .	2	11.6	27 C		9 6	2	4.4	5.2	9.1	8 .	7 e		1.6	1.3	2.0	28.7	30.8	45.8	19.8	,	n
	BASIN B	0 0	0.0	0.0)))		300	0.0	5.7	2.9		-	4.2	6	3.6	0:0	2 9	- -	9.6		Z. 6	- - - - - -	9.6	- - -	3 0	,,	100	9 .	LC)	3.8	9 6	13.2	10	9.0	6.4		_	-	 -	 	ŀ	
	 æ.	0	0	0	_ _	- -		0	<u>-</u>	9	0	. 1	. 1	9	8	-			œ ;	χ.	~	5	-	-	- - c	u	2	0.	8.		0			7 1	.3	8 .1	6	5	80	-	ļ	7
	IN BASI	5	0 0	0 0			9	0	5	8	L		5 35.		60			4	0	20) 	6 12	7		ο α			6		- L	200		0	. 2	7	. 3 20		2	~	ļ	. 3 10.
. 1	BAS I	0	Н	4	4	9 0	╀	-	3	L			Ц	_	-	-1	9	-4	9 45.	4	4		0 .	- -	0 0		~ C		83 83	<u>ئ</u>	3	20	2	9.	2.	4 2.	7 10.	19.		7 16.	ľ	5 IU.
	BASIN 13	0.0	9.0	0.0	0	0 0		0.0		0	0	0	40.7	47.	9	6	2.9	5	2		2			æ	i	<i>i</i> c	4	-	-	0		- C		6	- -	1.	24.	28	53.4	34		0.0
	BASIN 10	0.0	0.0	0.0	0.0	0 0		0.0	3.4	0 0	3.5	0.0	8.5	32. 3	0	0.0	2.8	2	54.5	2.8	38	77	2.5	1.4	000	90			0.0	1.8	0.0	o 4	4.0	6.2	0.7	0.0	1.7	5.3	2 6	13.6	c	0.0
	BASIN	0.0	0.0	0.0	0 0	0 0	0	0.0	1.3	0.1	0.7	0.0	29.7	19.0	7.1	5.0	7.0	77.7	3.4	ر د	5.	٥	۳ ت		0.4	7 0	10	3.6	2.1	1.1	-1	× =		0.0	E -		17.9	54.4	75.8	.4.8		0.0
	SASIN 8	0.0	0.0	0.0))	4 0		9.4	0.0	4.5	0.0	0.0	21.4	23.0	5.5	13.6	œ .	13.	17.3		12.6		. d.	8	12.4	12.0	0	4.4	7.5	1.4	4.0	- - -	11.6	0.3	0.7	5.8	44.2	21.6	41.3	21.1		9.2
	BASIN E	-	0.0		= = = =	2.5	-4 	9.7	0.0	19.2	0.0	2.0	19.3	1.5	1.4	19.	17.7	19.	25.2			 	7.7) n	30.5	0 76	8		24.8		0,0	200	12.1	3,4	6.0	8.7	34.7	19.5	5.4	26, 7	,	15.2
. 1	BASIN B	0.0	9.0	0.0		000			1.0	0.0	0.4		38. 2				4	?		8 7	۲	n	0	ς. α	10	0 0	2 3	╀	┞	2.0	+	+	╀	0.6	┞	0		0	┞	6		43*
	BASIN BA	_	0.0	0))	7 0	0	0.0	2.2	u,	4	Ŀ	8	5	P 0	7.	۳,	27	0,0	7	~ (,	ا و	c,	- α - α			65	۳.			000	57	0.0	0.0	4.1	m	-	5	∞	ļ	٠,
1		0	0	0) 	76	1_	L	9	.0			2		m (-	5,	ام	7,	٠,		ر د	n «) «	3 2	6	7	3	4	7 0	8 17	 - -	4			L		┞-	-	.77 0
1	eg G	0 0.	0 0	0	1) C	╁	0 0.1	5 66.	0	0 38	0	5	0	1	┨			1			1			19	1	18	ļ_	Ц	0 19	4	0 0	6 17.	0 7.	0 15.	8 5.	9 6.	ļ.,	1 51.0	2 60		C 77 &
ŀ	BASIN 3	0 (Ц	0	=	=	; es	9	45	0	0	-	4	1	4	4	~	4	4	4	4	•	13	•	ب ا د	1	["	0	33	0	⇒ •	- 0	2.1	0.1	0.	0.	5.	17.	L	L		7 7
	BASIN 2	0.0	1		Ö .		0.0	0	60.1				0.4		- 1	9		25. 8	٦ ۲	7 0	7 77	0 0	19. 7		о О	2 00	79.4	0.0	46.9	0 0	U 2	0 0			0.0	1.6	6.7	47.1	38 3	5.1	c	7.7
	BASIN 1	0.0	0.0	0.0	8. U	0 00		0.0	15.8	4.0	0.0	2. 6	7.5	0.4	7.2	4.	12.8	0 71	12.0	2 1		0.0	31.5	7.7	97.9	21.0	21.7	6.2	16.1	0.0	7.7	n 0	7, 5	0.7	1.1		19.6		17.1	22.8	5	3.0
	λ¥	16	17	138	13		22	23	24	25	97	27	28	23	8	5	1	1	_	4 (۲,		,	٥	20 00	-	121	13	14	12	2	- 8	13	20	21	22	23	24	25	26	٤	7,7
	MONTH 1	MAR.					:										APR.															:	•								_	

(4)-c at 1H8 and Mkombzi Dam Site for 20 Year Return Period (YEAR 1974 Type)

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BASIA	21	22	8 0	0.1	0.5	0.5	8.5	5. 2	3.	0	2	0	2. (9.	0	3.	9.1	0.0	0	0	0	C	0	0	74	0	0	0.1	0	Þ	7	0 (
BASIN	20	22. 5	0.1	0.0	9.6	0.0	8.5	5.4	0.0	0.7	0.0	0.0	0.2	0.0	0.0	10.8	6.8	0.0	0.0	0.0	0.0	0.0	0.0		15. 1	9.3		0.4	0 0	4.7	4.3	0.4
'I		1	1	. 7	1		0.2	-	!—	-	r.	3		8.	7	1.1	Ϋ.	0	0.0	0.	0	0	9.6	3.3	3.4	. 7	-	0.0	∞	4	6.1	0.
BASIN	13	3	21.	1	3	L				ļ		2	L	_	ļ_	Щ	_	L		L	<u> </u> _	L	L	L	Ŀ		2.	0	3	3		L
BASIN	8	9.5	2.4	0, 1	0.1	0.1	3.2	2.0	ω.	6	1.3	0.2	3.4	6.3	0.3	8. 1	2.8	0.0	0.0	0.0	0.0	0.0	0.0	0.1	5.7	13.2	6.0	5.3	0.2	1.9	11.2	8.0
BASIN		2.2	6.4	1.3	0.0	0.0	0.4	0.3	0.1	12.9		0.1	3.7	0.4	0.8	5.9	1.2	0.0	0.0	0.0	0.0	0.0	0.1	0.0	9.0	16.4	7.5	5.5	0.5	0.5	2.3	3.1
!		_	- 2	1		_	_	0		1	6	2	-	6	2	6	∞	0	0		9	0	2	0	0	_	0	10	 	-		_
BASIN	2	0.0	36.	3,	0	0.0	0.	0	6	12.			۳,	4	16.	1	11.	6	0	0.0	0.0	0.0	1.2	0.0	0.0	0	0.0	0.	9	3.7		L
BASIN	12	0.2	16.1	6.4	0.0	0.0	0.7	0.3	0.4	3.5	0.3	2 0	0	0.8	1.7	1.0	1.9	0.2	0	0	0	0.0	0.2	0.0	0.0	2. 1	0.9	9.8	1:1	9.6	1.5	6.6
BASIN		-	3.6	3.8	0.0	0.0	0.1	0.1	1.1	8.0	9 [1.1	2.7	4.3	9.2	1. 8	10.3	0.0	0.0	0.0	0.0	0.0	1.1	0.0	0.0	0.0	0.0	0.0	6.0	3.3	0.0	1.6
1-	-	_		1	L			_	_	2	3	2	ιc	8	7	3	0 1	ļ.,	0	ļ	0	0	2		0	L	_	0	1	8		6
BASIN	13	0 0	17	L	0	0.0	0,	0.	0	2	0	0	0	0	1	0	2.	0	0	0	0	0	0,	0	0.	0		0	-	0	0.	9
BASIN	12	0 0	30.0	2.8	0.0	0.0	0.0	0.0	0.0	10.1	1.5	1.0	2.5	4.0	8.6	1.5	9.6	0.0	0.0	0.0	0.0	0.0	1.0	0.0	0.0	0.0	0.0	0.0	5.5	3 0	0.0	0.5
BASIN	-	0.0	4	4.5	0.0	0.0	0.5	0.2	0.3	1. 2	0.2	0.1	0.3	0.4	0.9	0.2	1.0	0.1	0.0	0.0	0.0	0.0	0.1	0.0	0.0	0.0	0.0	0.0	0.5	0.5	0.0	6.3
				2	0	0	0	0	0	7	3	3	2	5	4	3					L			L					4.8			
BASIN	10	0.0	25.	2.	.0	0.0	0.	0.	0.	8.7	1.	G.	2.	3.	7.	1.	8	.0	0	0	0	.0	0.	.0	0.0	0.	0	0	4.	2.	0.	0
BASIN	6	0, 1	20.2	3, 0	0.0	0.0	0.2	0.1	0.1	6.1	1.0	0.9	1.6	2.7	5.5	0.9	5, 7	0.0	0.0	0.0	0.2	0:0	0.5	0.0	0.0	0.0	0.5	0.0	3.3	1.9	0.0	2, 3
BASIN	8	1.0	11.6	6.9	0.7	0.3	1.7	11.2	6.5	27.6	3.0	5.7	1.5	6.2	1.5	0.3	2.4	0.1	0.0	0.0	0.0	0.8	0.3	0.1	1.2	1.3	15.0	0.7	0.9	0.6	0.0	4.]
BASIN	7	6	7.7	10.5	7.0	2.2	4.0	11.4	6.5	39.3	15.0	8.3	6. 1	10.7	6.0	8	2.3	0.0	0.0	0.0	0.0	2.4	0.3	0.2	1, 2	1.3	17.2	0.9	3.0	1.5	0.1	1.5
SIN B) : . (0.0	1.3	5.3	0.0	0.0	-	-			-			_	_	_	-		0.0	0.1	0 1	0.	. 1	0.0	. 0	. 0	0.1	0.	0.5	4	0.	_
8) 2	1]) () () ;	1	3 (_) !) ()	3) · · · 8) (] [)	0	1	0	_	0 9	0 []	0	_
BASIN	2	5.6	4.8	1. (0.	0 (•	0, (1.7	2.4	5.	16.	P. 9	35. (11.1	0	0.1	18.	0. (0 (4	9	0	0.3	0.	9.	8.	7	3 0	0.5	0.0	0
BASIN	4	28.0	20.5	22. 7	16.5	7.7	34. 2	0.2	2.1	11.1	5	16.8		16.7	22.0	2.3	19.1		0.0		7 9	18.8	2.8	2.1	1. δ	1.0	29. 1	7	1.8	1.0	0.7	0.
	3	60.2	5.8	0.6	0.0	0.0	0.1	0.0	0.0	1.6	0.4	9.0	14.8	8.5	12. 5	0.5	0.0	.5	0.0	0.0	0.1	0.0	0.0	0.0	0	0.0	8. 7	14.3	0	5 1	0.0	-0
BASIN BASIN	2	244.4	26. 5	0.0	0.0	0.0	0.	0.0	4. 2	6.3	0.4	0.0	58. 2	26. 4	53.6	2.1	0.0	0.0	0.0	0.0	0.4	0.0	0.0	0.0	0.0	0.0	33. 5	57.1	2.0	20: 3	0.0	0.0
BASIN	,	. 1	61. 2	1.4	1.4	0.3	0.0	0.0		2	3.4	2	4	4	7	3.4	0	0.0		0.0	0.1	0.0	0.0	0.0	9.0	0:0		-	9	4.8		0.4
\vdash	-	1 7	2 6	₅₃	~	ı,	_		_	50		4	12 1		Ì							٠.		23		Ŀ	Ц	_				
12	TH DAY			_		_]		_					_								~	7	7	7	7	2	7	~]	7	7	~	3
	MONTH	MAY								_									_													

ESTIMATED DAILY RAINFALL FOR HIGH FLOW ANALYSIS

(4)-c at 1H8 and Mkombzi Dam Site for 20 Year Return Period (YEAR 1974 Type)

	_					-	-	-	~~~			-	-				_			-	_	_		_	-7	_	7		-			i
/48y	BASIN	2.1	9.7	0.1	0, 1	0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.5	0.0	0.0	0.0	0.0	0.0	9.9	0.0	0.0	0.0	0.0	0.0	0	4	6	9.0	16.5
սուն ։ յ	BASIN	20	0.0	0.0	0.0	0.6	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.5	0.0	0.0	0.0	9.0	0.0	0.0	0.0	6.0	0.0	0.0	0.0	0.0	5.1	0	9.4	16.4
٦		16	4 9	4.9	7.2	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	S 8	9.7	9.1	4.9
	75.		0.2	0.2	0.3	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0 0	0.0	9 0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	22. 3	2	3.9	6.3
	BASIN B		0.0	1.3	2.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	26.8	2.6	3.3	9.6
	=		0.0	9.1	14.7	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0 0	0.0	0.0	0.0	0.0	0.0	0.0	5.1	18.0	20.3	0.0
	Z	-	0.0	4.7	7.5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0			0.0	0 0	0.0	0.0	0.0	0.0	0.0	0.0	5.9	9. 2	10.4	0.0
	Z		0 0	8.5	3.6	0.0	0.0	0.0	0.0	0.0	0.0	0 0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	_	_	L		-	L	0.0	_	L	1	8.8	_0
	_	1	0	3	8.6	0	0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	3.6	0.5 1	1.8	0.0
	2	13	0	0	2.8	0	0	0.0	0	0.0	9	0	0	0	0	10	_	0	0.0		0	0	0	0	0	0	0	0	5	8	8	0
	22	12	. 0	6	5	L	0	0.	0.0		L	L	L		_	L.,	<u> </u>	L	_	ļ.,	_		L		Ц		Ŀ]		
		==	0	0	2	0			0.0	L			L	_		L.,	ļ	Ŀ	_	_			L						Ц			
	2	_		9	6 1	0				ļ	_			_	Ļ	_		_	Ļ	L	Ŀ	0	0	0	0	1	2	1	Ц		7.7 15	
	N BAS	<i>a</i>	2 0.		8				0.0									8 0.0	1					1			0					
	I BASI						0.0																						1.	_	_	I.
	BASI	_		_	_		0.0	L		L	_	L	L	L	L	_		L			L	_			L			L	0.1	3 0.1	_	7.4
	- 3	-	0.0	_	5	1.0	0.0	0.0	0.0		3	0.0	3.6	0.0	0 0	0	0	9.0	9	0	0	9	0.0	0 (0.0	0	0.5	0.1	2.1	7.	8,	0
	BASIN	ហ	2.1	8.0	0.2	0.0	0.9	0.0	9.0	1.5	0.0	0.0	0.0	8.0	0.1	2.0	0.5	1.1	0.0	0.0	0.0	0.4	0.0	0.0	0.0	3.4	14.2	5.3	2.6	0.		0
	BASIN	7	5 6	8.4	1.8	8 0	1.7	3.2	0.2	2.7	0.0	0 0		12 8	8 2	3.7	1.0	19. 2	0.5	0.0	0.0	0.7	0 0	22. 2	9,0	P 1	12.0	12.1	1.3	1.8	18.1	9.6
	BASIN	9	0 0	35.9	9 0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0 8	6	0.0	0.0	0.0	0 0	0.0	0.0	0.0	0 0	0 0	0.0	0.1	0.0	3.1	0.3	5.0	2.3	0.8	0.0
	BASIN		0.0	14.8	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	9.0	0.0	0.0	0 0		0.0		0.8	1.5	1.5	0.	0.0	0.0
	BASIN	1	0.0	26.7		2. 4			1 3					0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0			0.0	0.0		9.7	0.5	0.2	0.8	1.6
	IE) DAY		2	3	4	2	9		00	6	10	-	12	13	14	15	16	1	2	13	20	2.1	22	2.3	24	25	26	2.7	28	2.9	30
	DATE	MONTH	JUN.													·																

ESTIMATED DAILY RAINFALL FOR HIGH FLOW ANALYSIS

(4)-d at 1H8 and Mkombzi Dam Site for 50 Year Return Period (YEAR 1974 Type)

APR.

ESTIMATED DAILY RAINFALL FOR HIGH FLOW ANALYSIS

mm/day	BASIN	21	27.0	1.0	0.1	9.0	0.6	10.1	6.3	3.0	0.8	6.1	0.8	2.4	9.8	0.4	12.2	8.1	0.0	0.0	0.0	0.0	0.0	0.0	0.6	18.3	0,6	0.4	0.0	0.1	co co	5.3	0.0
unit : m	Z.	20	27.5	0.1	0.0	0.0	0.0	10.4	მ. მ	0.0	8.0	0.0	0.0	0.2	0.0	0.0	13.0	8.4		0.0	0.8	0.0	0.0	0.0	0.0	18.4		0.5	0.5		5.00		9.5
	æ	18	4.5	26.6	2.1	4.5	4.0	0.3	0.2	27.1	11.1		6.5	18.5	8.5	8.3	1.3	G G	0.0	0.0	0.0	0.0	0.0	0.7	4.1	4.1	4.5	2.6	0.0	4.6	4.2	7.4	0
	BASIN	28	11.6		0.1	0.2	_	3.9	2.4	1.0	12.1		0.2		0.3			3.			L		0.0	0.0		7 0	18.1	7.4	6.5			13.7	7
	BASIN	13	2.7	7.8	1.	0.0	0 0	0.5	Ŀ		15.7	0.2	L	4.6	0.2	1.0	7.2	Ц	0.0		0.	0.0	Ŀ	0 1	0	0 7	20.0	9.1	8.1	3 0.7	9.0	15.0	11.1
	BASIN	15	0.0	44.3	9 3.8		L	8 0.0	3 0.0		3 15.1	4 2.3	2 1.5	L	6,1	0 12.9	2 2.3	3 14.4	2 0.0	0 0 0	0.0	0.0	0.0	2 1.5	0.0		5 0.0	2 0.0	0 0.0	3.8	9 4	9 0.0	0 (
	N BASI	25	0	1 19.	6 7.	0 0. (0.0	1 0.8	1 0	1 0 0	3 4.		3 0.	3	3	3 2.	0 1.	6 2.	0 0.	0 0	ci	0		3 0.	0	0	0 2.	1.	0 1.	3 1.	0 0	0 1.	12.
	N BASI	14	0 0	1 41.	7			9 0	4 0.	5 0.	6 13.	4 2.	3	s	0	11.	4 2.					0 0	0 0	3	- -	0	0	0	0	4 7	0 4	0 0.	1 2.
	IN BASIN		0	7	2	0	0	0	.0	0 0	3		$2 \mid 0$	1.	.9 .1	5 2.	.8 0	-	.0 0.	0	0	0	.0	2	0	0		0 0	0 0	.8	.7 1.	0 0.	6 1 12.
	_	12	0	. 7 35.	5.5 3.	0 0 0	0.0	0.5	0.2 0	3 0	1.4 12.	0.2	0.1 1	0.3	0.5 4.	1 10	0.2	3 11	0.2 0.	0	0	-	0.0 0.0	0.1 1	0 0 0	0	0.0	0.0	0.0 0.0	1.7 6.	3.	0.0 0.0	. 7 0
٠.	E N	0 11	0	31.0 12.	9	0	0.0	0	_	0	9	9	1.1	2.6	~	9.0	ક	1	0	0	0	0.0	0.0	1.1	0	0 0	0	0.0	0.0	5.8	3.2	0.0	0.0
Type)	BASIN BASI	-	0.1	24.7 3	~	0.0	0	0.3	-	0, 1	5	1.2	1.1	_	3.3	L	1.1	7.0 1	0.1	0.0	0.0	0.2	_	0.7	0	0	0	0.2	0.1	4. 1	2. 3	0.0	2.8
AR 1974	BASIN BA		1. 2	14.2	8.4	0.9	9.4	2.1	13.7	8.0	33.8	3.7	7.0	-i -8	7.8		0.3	3.0	0.1	0.0	0,0	0.0	1.0	0.4	0.1	1.4	1.6	18.4	0.8	1.1	0.7	0.0	5.0
rn Period (YEAR 1974 Type)	BASIN B	\neg	2	9.4	57	و	2.7	on.	0	9	1		10.2	 5	13.1	7.3	12.0	2.8	0.0			0.0	3.0	0.4	0.3	1.5	1.6	21.1	1.1	3.7	1.9	0.1	1.9
turn Per	BASIN	_	0.0	13.9	6.5	0.0	0.0	0.7	0.3	0.4	1, 2	0.3	0.3	9.4			0.2	1.0	0.7	0.0	0.0	0.0	0.0	0.1	0.0	0.0	0.0	0.1	0.0	9.0	0.5	0.0	9.4
Year Re	BASIN	2	6.8	5.9	1.2	0.2	0.0	2.3	0.0	1.5	2.9	7.2	20.0	7.8	42.9	14.2	6.0	0.0	22.8	0.0	0.0	5.5	0.0	0.0	0.2	0.8	0.7	10.9	2.2	0.6	0.6	0.0	0.4
for 50	BASIN	4	34.3	25. 1	27.7	20.2	ۍ د	41 8	0.2	2.6	13.6	6,5	20.3	4	20.4	26.9	2.8	23 3	0.0	0.0	0.1	9.6	23.0	3.4	2.5	1 6	1.2	35.6	5.5	2.2	1.3	9.0	0.5
am Site	BASIN	3	73.6	7.1	0.8	0.0	0 0	0.1	0.0	0.0	1.9	0.5	0.7	18.1	10.4	15.3	9 ()	0.0	1.8	0.0	0.0	0.1	0.0	0.0	0 0	0.0	0 0	10.7	17.5	0.1	6.2	0.0	1.2
kombzi D	BASIN	. 2	298.9	32.5	0.0	0.0	0.0	0.0	0.0	5.2	7.7	0.5	1.1	71.2	32. 3	65.6	2.6	Щ	0	.0	0	0.5	0.0	0.0	0.0	0.0	0.0	41.0	69.9	2.4	24.8	0.0	0.0
(4)-d at 188 and Mkombzi Dam Site for 50 Year Retu	BASIN	-	93.1	74.9	1.7	1.7	0.4	0.0	0.0	33.2	5.4	4.2	7.9	18.8	14.2	43.1		Ц	0.0		L	_		0.0		0.0		8.9	ĭ	13.4	_		0.5
d at 1H	Ή	ITH DAY	1 K	2	<u>ن</u>			40		8	6	70	11	12	13	14	12	16	17	18	13	20	21	22	23	24	25	26	27	28	29	8	3
(4)	Ц	MONTH	MAY						_													<u>,</u>		_	-								

ESTIMATED DAILY RAINFALL FOR HIGH FLOW ANALYSIS.

(4)-d at 188 and Mkombzi Dam Site for 50 Year Return Period (YEAR 1974 Type)

Г	-	_	<u> </u>			_	₁											-	_							_			-		
BASIN	21	0.9	0.2	0.1	0.0	0.0	0.0	0 0	0.0	0.0	0.0	0.0	0.0	0.0	1.3	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0	0.0	0	5.0	0.3	11.0	20.2
BASIN	20	0.0	0.0	ຄ. ຕ	0.0	0.0	9.0	0.0	0.0	0.0	0.0	0.0	0.0	0.6	1.9	0.0	0.0	0.0	0.0	0.0	0.0	0.8	0.0	0	0 0	0.0	១	5.3	9.0	11.5	20.1
ž	-	8		8.8	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		0.0	7.1	11.9		0.9
BASIN	18	0.2	0,3	0.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.8	0.0	0.0	0.0	27.3	9.6	4.8	7.7
BASIN	17	0.0	1.6	2.6	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.0	0.0	0 0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	32.8	3.2	4.0	0.8
BASIN	16	0.0	11.2	18.0	0.0	0.0		0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0 0	0 0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	6.2	22.0	24.8	0.0
┡	15	Н	5.7	9.2	0.0	0.0		0.0	0.0	0:0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	7.2	11.3	12.7	0.0
8ASIN		0.0	10,3	16.7	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	5.7	20.4	23.0	0.0
-	13	0.0	6.5	10.5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	3.6	12.8	14.5	0.0
-	12	0.0	9.8		0.0	0.0	0.0	0 0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0 0	0.0	0 0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	5.4	19.3	21.8	0.0
\vdash	~~	Н	3.5	5.7	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0 0	0 0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	2 0	6.9	7.8	0.0
	9	0	8.5	13.7	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0 0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	4.7	16.8	18.9	0.0
\vdash	o,	Н	4.4	6.8	0.0	0.0	0.0	0.0	0.1	0.0	0.0	0.0	0.3	0.0	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	9.3	0.1	2.4	8.3	9.4	0.0
\vdash		12.5	2.9	5.8	0.0	0.0		0.0	0.0	0.0	0.0	0, 1	0.0	0.0	0.0	0.0	0.3	0 0	0.0	0.0	0.0	0.0	1.2	0.0	0, 1	0.0	0.5	1.6	5.7	8.3	1.7
2	~	L	0	13.2	10.8	0.0	0.5	0.0	0.0	0.0	0.0	0.2	0.0	0.0	0.0	0.0	2, 7	0, 1	0.0	0.0	0.0	0.0		0.0	0.3	0.0	1, 4	0.0	0.1	7.4	9.0
-		-	4.5	7.2	0.0		0.0		0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.2	0.1	2.5	8.9	10.0	0.0
BASIN	ú	2.8	7.3	0.3	0.0	1.1	0.0	0.0	1.8	0.0	0.0	0.0	8.8	0.2	2.4	0.7	- -:	0.0	0.0	0.0	0.5	0,0	0.0	0.0	7	17.4	6.5	3.2	0.4	0.4	0.0
BASIN		7.2	10.3	2.2	1.0	2.1	3 8	0.2	3.3	0.0	0.0	2.5	15.6	0.3	4.5	1 2	23.4	9.0	0.0	0.0	0.9	0.0	27. 1	0.0	9.0	14.7	14.8	1.6	2.1	22. 1	0.7
BASIN		0.0	43.9	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1		0.0	0.0	0 0	0 0	0 0	0.0	0.0	0.0	0.0	9.1	0.0	3 8	0.3	6.1	2.9		0.0
BASIN		0.0	18.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.0	1.8	1.8	9 0	0.0	0.0
BASIN		0.0	32. 7	3.3	2.9	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.3	11.9	9.0	0.2	1.0	2.0
in in	DAY	1		"	₹J*	2	9	_	8	6	10	Ξ	12	=======================================	14	15	1.5	17	18	19	20	21	22	23	24	52	5.6	2.2	28	53	30
DATE	HINOM	Jun.							_						oves-																

ESTIMATED DAILY RAINFALL FOR HIGH FLOW ANALYSIS

(4)-e a	t 118	and MK	ombzi Da	(4)-e at 1H8 and Mkombzi Dam Site for 100 Year	for 10		Return Period		(YEAR 1974 Type)	74 Type		.*	ı							•		76
DATE MONTH DAY		BASIN	BASIN	BASIN	BASIN	BASIN	BASIN	BASIN	BASIN 8	BASIN	BASIN 10	BASIN	BASIN 12	BASIN 1	BASIN 14	BASIN 15	BASIN 16	BASIN 17	BASIN 18	BASIN 19	BASIN	BASIN 21
MAR.	1.6	0.0	0.0	0.0	0.0	0.0	0.0	0.0		_	0.0	0.0			1-		0.0	0	0.0	0.0	0.0	0.0
	17	0.0	0.0	0.0	0.0	0.0	0.0	\blacksquare	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0
	138	0.0	0.0	0	0	0	0	0	0.0	0.0	000	0	0.0	0	0.0	000	000	000	200	5) 0	D 6	= C
	5 06	5 0) -	⊋ c	5 5	0 0	50	0 6	3 6) = =				0 0) - -	9 0	5 6) C		
	21	3	- -		43.8	23.7	0.0	0	0 0	8	0	0 0	0.0	0.0	0.0	0.0	0.0	0 0	0.0	0.0	0.0	0.0
	22	1.7	0 0	0.0	0	0.0	0.0	6.3	0.0	0.0	0.0	0.0	3.6	2.4	12.0	1.4	11.2	1.1	0.3	6.3	0.0	0.0
	23	0.0	0.0	0.0		0.0	0.0	13.6	13.1	0.0	0.0	0.0	0.0	0.0	0.0	1.9	0.0	15.0	12.0	0 0	0 0	0.0
	24	22. 1	l ł	83.6	92.9		1.4	0.0		1.8	4.7	2.3	4.9	12.8	8.0	11.3	5.0	33		7.3	0	80
	25-	ניז ניז	0 0	0 0	8 2		0.0	26.9	6.3	0	000		2	8 6	4.	0 2	κή . α	7.4	B) (S 0	0.1	200
- 1 ° · · · · · · · · · · · · · · · · · ·	25	0.0 2	B .0	2 C	5U. 5	27.7	0 0	= « = «	000) c	φ C) u	., c	0 0	7 0	2 6	 	2 0	n c	12 C	2 C) «)
	28	10.5	20	9		2.5	53.5	27.0	29.9	41.6	11.9	56.9		49.1	5.8	44.2	3.2	7.7	3 0	9.0	0.0	1.3
	29	0.6	0.0	8.5	0.2	2.6	72.1	2.1		26.6	45.2	62.8	43.6	52.6	9.7	43.8	18.5	8.3	0.4	9.3	0.0	6.9
	30	10.0	1.6	1.0	1.8	0.5	8.1	2.0	7.7	6.6	0.0	9.6	1.8	9.6	2.0	8.8	3.6	-i	0.1	2.0	0.0	0 0
_	31	5 7	0	0	2 2	6	0.0	22, 5	13.0	2	0.0		0	0	0.0	2,0	0	9	75.7	7	12.3	15.0
APR.		17. 6	- 6	7 7	5	2,	6.4	24.8	10.9	2,	5	4,	S .	100	23.4	5 6) :	- 0		2 0	2	0.0
	~ [21.0	3b 2	5.5 6.5 7.5 7.5 7.5 7.5 7.5 7.5 7.5 7.5 7.5 7	19.4	2 P	10.5 8	35.3	2 b 9	4.1	19.1	13.5	61.4	2 2 2	13.0	10.4	31 7	20 C		2 00	5.3	
	-	22.7	3.2	0.4	9.2	4.3	3.9	24.5	18.2	4 9	3.9	4.9	5.4	8	8	7.3	7.1	4.0	5.1	3.8	8.8	8.4
	S	8.0	31. 1	23. 1	1.7		9.0	16.4	17.7	8.0	26.0	7.2	22. 1	4.6	3.7	5.9	10.3	13.1	10.1	9.6	0.7	1.2
-45-70	9	67.1	26.5	12.1	28.0	13.5	4.9	13.0	10.6		38.6	2.5	32. 1	1.4	5.5	3.4	15.3	11.7	3.2	5.2	0.6	0.5
	7	44.0	27. 5	!	17.8	38.7		3.8	6.4	13.2	3.5	14.0	3.7	17.7	6.5	16.2	2.9	2.8	0	2.2	0	0
	8	10.1	8.0	8.8	27.3	48.3	12.5	14.7	12.3	7.4	2.0	12.0	7.7	6.5	0.0	5.5	0.0	5	œ.	90	21.1	20.3
	5	25 C		- C	24.5	7	200	47.0		0	9.0	1.5	700	= 6	900	200))	7 0	200	3 C	- G	5 C
	7	70 T	7 0	12.6	2 6	21.5	0.0	33.5	20.0			3 C		3 0C	∞ > > >) t	2 6) - -	33.2	0 0	25.7	23.5
O	12	30.4	111.1		25.4	47.6	3.2	6.7	5.8	15.4	0.0	6.3	6	10.6	11.3	10.8	8.3	3.2	1.2	4.7	0.1	0.0
	13	8. 6			1.3	0.4	10.6	13.7	6.1	5.0	1.5	10.5	5.2	8.2	12.8	6.1	11.9	3.2	10.5	7.4	27.3	25.3
	14	22. 6	9 29	47.4	27. 6	15.8	6.0	34.7	10.5	2.9	0.0	5.8	11.2	10.9	35.7	7.2	33. 3	3.9	1.4	32.0	0.0	3
	15	0 0	0.0	0.0	27.0		0.3	2.2		9	2.7	9.0	7.8	3	19.3	2.6	8, 5	8.	χ (C	18.3	0.0	7-16
	9	4.00	F 6	7 6	- C	21.8	9 6	5 0	0 0	7 . 7	2 6		19.8	2	2 G	2.6	200	3 7	0 0	2 0		7 0
	18	700	0.7	ic		T C	9 0				0			3 6			2 2		2	24.6	11.3	13.6
b	5	10.5	5.1	3.8	24.9	25.0		17.0	1 .	2.0	5	2.1	9	.5	7.8	1.6	8.3	63	5.7	15.3	2. 1	3.3
	20		0.0	0.0	10.7	0.0	0.0	4.8		0 0	8.7	0.0	12.6	3.8	19, 5	2.2	20.4	2.1	3.3	10.3	7.	7.2
	21	1.5	0.0	0.0	21.6	0.0	1.0	8.4	0.9	0.8	0.9	1,1	3.0	1.8	8.9	1.9	8.3	9.2	21.9	15.9	43.1	42.8
	22	8.8		1	7.8	5.8	0.1	12. 1	8.1	11 0	0.0	2 0	3	2. 5	12.8	2.8	11.9	1.2	0.4		0	0
	23	27.4	6	α :	2.5	5.1	33.1	48.5	61.9	25.0	2.4	34.5	14.3	29.3	32. 6	40.2	30.4	134. 5	103.3	32.3	7.1	10.2
	57	6.767		2 0 V		4.0. A.R.	75.4	7 0	27.7	106.0	3 6	28. S	170	0 0 49	9 6	24.0	24 R	13.1		34.4	20.7	24.2
	28	31.0	;	8	نداد	20.7	2 15	37.4		20.5	0 5	48.5	23.4	34.7	130	27.8	17.7	2 2	2.0	10.4	0.0	C.
	27	13.4	3.1	33		31.2	9.0	22.7	12.9	0.0	0.0	0.8	15.2	14.3	52.4	9.7		6, 5		50.7	12.6	15.4
	28	52. 1	98.0	70.2	63.3	36.6	16.7	60.1	42. 2	22.7	3.2	18.6	42.1	36.1	128.0	28.2	113.8	33.9	19.6	68. 1	1.1	0.1
	29		7.4	10.2	39. 2	71.7	8.6	28. 5	2	15.2	7	9.3	13.8	12.5	26.9	13.1	25.9	21.8	15.3	13.4	7	D)
	8	59. 2	162.8	117 8	55.8	44.7	17.4	35.4	12.3	21.6	7.0	19.1	16, 2	19.7	32.0 1	16.7	30.6	5. 11	0.8	16.1	0.0	Ð.

ESTIMATED DAILY RAINFALL FOR HIGH FLOW ANALYSIS

						ونبدي						-	-7		<u>-</u>		· · · · · ·		_1		T			_1.	_1	_ [_1	_,[.		, I	<u>_</u>]	
nn/day	BASIN 21	30 30	-	0.1	0	0	11.5	7.5	4.4	0	-	-	2.8	9.	0.4	13.9	9.2	0	0	6	0	0	9,0	0.7	67	3	6	8	2	٥	٥	2	
	25	31, 5	0.1	0.0	0.0	0.0	11.9	7.5	9.0	9	9	0.0	0.3	0.0	0.0	14.9	9.8	0.0	0	0.0	0.0	0.0	0.0	0	21.1				6 6	න න		9	
unit		1	4	4	1	9	3	7.	0.1		9.6	7.5	1.1	7 . 2	9.4	1.5	7.6	0.0	_ ဝ	0.0	0.0	0.0		4.6	4.7	5.1	3.0	0	5		ري دي	0.0	
	H BASIN	3 5	30	1 2	2	7	4 0	_	_	8 12.	8 49.	3		•	4	4	5	0	0	0	0	0	0	7	0		5	4	7	-		.3	:
	BASI)	13	6	0	0	0		2.8		13.	_		<u> </u>	9	-		د.	L	0	6		o	0		Ц	18.	∞ 	3	2	2.	15.	2	
	BASIN 17	-	8	1 8	0.0	0 0	0.6	0.4	0.1	18.0	9.2		2 2	0.5		8 2		0.0		0		9	0	0.0	0.8	22.9	10.5	8		0	17.	12.	
	Z.	2	20.2	4.3	0	0	0.0				2.6	-	2	6		7 6		0				0	7	0.0	9.0	0.0	0 0	0.0	8.5	5.2	0.0	0.0	
	IN BASI	6			_		6	4	٠.		7 0			-			200		-			0	3		0.0			1.2	5	1:1	2.1	3.8	
	BASIN		,		 -			-	1-	16	Ļ	╽	L		0	1	L	1			0 0	L		-	0	0	- -		6	ص		2	
	BASI		9		-	5	٥	e	<i>.</i>	.t	-1		-		•	, 6	7 7	ř	5	1	1	-	ļ	٦	L	6	Ļ	ļ	~	4		L	ļ
	BASIN	100	200					ŀ						-	•		9 6	į	9 0	9 0	5 0	-			-	e e		-		1	0	α 	
	BASIN	10	2 0		200		3	-	5 0) -			, u	20			7 .	2	9 0))) ;	5	-	-			o c	9 0		2	0	-	,
	1	+	-	9 6	-	-	,	+	 	, 0		7 0						000								-11						σ	
	<u>~</u>	1	_[÷ 0				1		3	1	1	70	1	1	1		٥		,				, -) o c				٠	-1		1
· 🕣	BASIN	21	n i	50.0	,	3	٥		; -	÷	*			1	1	1	- -	1	= •	-) -) -	= 0	1	٦	1		+	1	1	s ~	10		-
74 Typ	BASIN	,	- I	5 °	7 6	5		٠ اد	-1	7 '	۰ د	1	2 6		?		-1	>) *	- -) = 	0.0	7 0	3	0 C	٥		֓֞֜֜֜֜֜֜֜֜֜֜֜֜֓֓֓֓֜֜֜֜֜֟֜֜֜֓֓֓֓֓֜֜֜֜֜֜֜֜	7	7 9	4 6	ء د		.1
Period (YEAR 1974 Type)	BASIN	×	1.4	200	2) - (2	7	و د	- 6	٥	7.5	n .	7	8	7:1	-				1	a) •			3	-1,	× 1		, ,	7 0	o c	200	
od (YE	IN B		-				5	٥		2/0	5,	_ 						3.7	=	0	0.0				7		2	24 3	7:	7.7	7.7	1	7 7
Peri	N BASIN	-1	_[9 10		1	0	-	-	5	4	3	4 11.	Ž,		_	-1	~	_		4		0	1	⇒ -		_	7	5	4	وم	5	
Retur	BASI	و	- 41	15.	7.	ei	0	ö	o	٥	-		0	0	1.		0		0	0	Ö	0	0	9	7		٦			=	=	2	2
Year	BASIN	2	7.7	5.7	1.4	0.2		2.5	0	-	3	8.2	22. 9	8.9	49.8	16.2	1.0	0.0	26.0	0.0	0.0	6.0	- 1	- 4		1	0.7	- 1	2.5	0.7	0.7		0.4
r 100	BASIN	4	39.2	28.7	31.7	23.0	10.8	47.8	0.2		15.5	7.4	23. 2	7.4	23.3		3, 3	26.7	0.0	0.0	0.1		26.3		2. 9	2. 2	1.4	40.7	6.2	2 5	1.4		0.2
ite fo	N B	-	~	8.1	6 0	0.0	0	0.1	0.0	0.1	. 2	٠	8	20.7	-	17.5	<u> </u> _	0.0	2.1	0.0	0.0	6.1	0.0			0.0	0.0	2.2	20.0	0.1	7.1	0.0	1.4
Dam	N BASIN		8		0	0	0	0	0	6	8	မ	9	4 2	┞	L			_		_	9	0	0		0	0	6	6		4	0.0	0
2000	BASIN	64	341	3.	0	6	ö	0	0	r,	တ်	٥	-	81	ļ.,	Ļ	ļ.	L	L	_	G	Ö	6	0	0.	0.	Ö	46.	79.	2	7	0 0	
E POR	BASIN	-	105.4	85.5	1		0.5	0.0	0.0	37.9	7.3	4.8	0.6	21.5	16.2	49.3		0.0	0	0		-	0	0.0	0.0	0.0	0.0	16.1	17. 2	15.3	6.7		0.5
1 118		2	1-	~	~	4	r.	Œ	7	8	o,	5	Ξ	:	-	14		16		α <u>.</u>	0	2	21	22	23	24	25	26	27	28	59	30	31
(A) - a + 1HR and Mkombzi Dam Site for 100 Year Return	DATE	MONTH	-			-	•																							-			
Y)		1	1			-		·				_			-										/						-	-	

ESTIMATED DAILY RAINFALL FOR HIGH FLOW ANALYSIS

(4)-e at 1H8 and Mkombzi Dam Site for 100 Year Return Period (YEAR 1974 Type)

M/GBy	BASIN	77	1.0									0.0			i 1	1 3	l i												5. 7	0 4	12. 8	23.0
_	AS IX	22	0.0	0.0	0.0	0.0	0.0	0	0 0	0	0 0	0.0	0.0	0.0	0.0	2. 2	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	7.2	- 1	13.1	
7	BASIN	·	6.8	6.8	10.0	0.0	0.0	0.0	0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.0	0.0	0.0	0 0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	 ω	13.6	12.7	8.9
	BAS N	82	0.3	0.3	0.5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	9.8	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	31.2	0.6	3	8.8
ı	BASIN					_	_	_	-	_	_	0.0	-	•	_		_		_	-		-	ı	$\overline{}$	$\overline{}$	•	_		_	_	_	_
	SASIN	16	0.0	12.8	20.6	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	7.1	25.2	28. 4	0.0
	BASIN	15	0.0	5.5	10.5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	9.0	8.2	12.9	14.5	0.0
İ	BASIN	٦	0		_			_		-		0.0		_	⊢	⊢	┢	-	_	┝	-		_			-	-	_	-	$\overline{}$		Η-
	BASIN		0	7.4	12.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	4.1	14.7	16.5	0.0
	BASIN	-	- 1	11.2	18.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	6.2	22. 1	24.9	0.0
	BASIN	_	0		6.5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0 0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0 0	0.0	0.0	0.0	0.0	0.0	0.0	2.2	7 9	8.9	0.0
	BASIN		0	9. 7	15.7	0.0	0.0	0.0	0.0	0 0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0 0	0.0	0.0	0.0	0.0	0.0	0.0	5.4	19.2	21 6	0 0
	BASIN	6	0.1	5.0	7.8	0.0	0.0	0.0	0.0	0.1	0.0	0.0	0.0	0.3	0.0	0.1	0.0	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	9. 2	0.3	0.1	2.7	9.5	10.8	0 0
	BASIN	œ	14.3	3.3	6. 7	0.0	0.0	0.2	0.0	0.0	0.0	0.0	0.1	0.0	0.0	0.0	0.0	1:1	0.0	0.0	0.0	0.0	0.0	1.4	0.0	0.1	0.0	0.5	1.8	6.5	9.5	1.9
١	BASIN	-	_	-	-			-	-		_	0.0	$\overline{}$	_	-			_		_	_	-	Н		_	-	-	_	-	-	_	-
١	BASIN	-	0.0	5.2	8.3	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0 0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.2	0.1	2.9	10.1	11.4	0.0
1	BASIN	ۍ	3.0	8.4	0.3	0.0	1.3	0.0	0.0	2 0	0.0	0.0	0.0	11. 2	0.2	2.8	0.7		0.0	0.0	0.0	9.0	0.0	0.0	0.0	4.7	19.9	7.4	3.6	0.5	0.4	0.0
1	BASIN		8.3	11.8	2.6		2.4	4.4	0.3	3.8	0 0	0.0	2.1	17.9	0.3	5.2	1.4	26.8	<u>-</u>	0.0	0 0	0	0.0	31.0	0.0	10.3	16.8	17.0	1.8	2.5	25.3	0.8
	BASIN		0.0	50.2	0.8	0.0	0.0	0.0	0.0	0 0	0.0	0 0	0.0	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0	0 0	0.0	0.0	0.1	0.0	4.4	0.4	\vdash	Н	1.2	Ι-
- 1	BASIN	2	0.0	20.7	0.0	0.0	0.0	0.0	0.0	0.0		0 0	0.0		0.0		0.0	0.0		0.0	0.0	0.0	0.0	0.0	0.0	0.0		2.7	2.1	0 7	0.0	0.0
1	BASIN	1	0.0	37.4	3.7	3.4	0.0	0.0	0.0	0.0	0 0	0.0	0.0	0.0	0,0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.4	13. 6	0.7	0.2	1.2	2.3
		DAY	1	7	3	7	цэ	9	7	∞ ∞	on On	10	11	12	13	14	15	19	-	200	13	20	21	22	23	24	52	3.2	27	28	2.9	30
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ESTIMATED DAILY RAINFALL FOR HIGH FLOW ANALYSIS

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BASIN 21	0	0	0	0	င္း	ci	0	ဝ	o	0.	0	2.	1	1.	0	18	c	15	4	6		Θ,	æ	22	0	6	26	0	<u>2</u>	2.	-i	25.	0	12		∞	48	c .	7	37.		=	o	0	ľ
BASIN 20	0.0	0 0	0.0	0.0	0 0	0.0	0 0	0.3	0.1	0.1	0.4	0.0	0.0	0.0	0.0	17.5	0.7	14. 1	9.0	es es	0.8	0.7	0.0	23.8	0.0	0.0	29.0	0	30.7	0.0	0.0	23. 4	0.0	12.8	2	8	48 G	0	: ::	177 25 8		14.2	1.3	-	ŀ
	0.	0	0	0	<u>.</u>	0	-	0	7	0.	0.	8	2	5	. 3	2	4	4	1		8	∞	-	GD.	0		(2)		4	1	7	7	s.	8	~	œ,	0		e, c	⊃ ≪			80		
BASIN 19	0	0	0	Ö	_	ci		_		3.	L	13.	_	1	2	-	_	21	65	╀	-	L	L	_	Ш	4		_	α,	-	\dashv	23	2	23	1	=			e c	+	+	L	L		ľ
BASIN 18	0.0	0.0	0.0	0.0	0	0.0		13. 5	1.5	2.1	5.6	0.5	0.4	0.4	0.1	14, 3	10.9	17.1	20. 8	5.7	11.4	10.4	0.1	8	0.0	0.0	37.4		11.8	1.6	0.8	9.	0.5	5.9	9		24.7		116.5		0.5	8.4		17.3	
BASIN 17	0.0	0.0	0.0	0.0		0.0	1.2	16.9	3, 7	2.7	7.1	0.5	8.7	10.0	1.9	10.5	16.6	18.1	24.9	4.5	14.8	13.2	3.1	2.1	0.2	0.0	35, 5	3.7	3.6	4.4	2.0	1, 6	2.0	1: 7	7.2	2 3	10.4	1.3	151.6	16.7	7.3	7.3	38. 2	24. 6	
BASIN 16	0.0	0.0	0.0	0.0	0.0	0.0	12. 6	0.0	S S	4.3	1.7	0.0	3.6	20.8	4.0	0 0	21.4	16.0	35.8		11.6	17.2	3.3	0.0	0.0	0.0	4.0	9.4	13.4	37.5	21.0		21.6	-	4	23. 1	9.4	13.4	50.00	2 K C	10.0	53.6	135.1	29. 2	
BASIN B	0.0	0.0	0.0			0.0	1.5	2.1	2.8	0.8	0.9	5.8	9.8	9.3	10.0	2.2	7.9			-	┞		18.3	6.2	0.9	0.0	4.8	_	65	4	2.9	.3	3.0	5	1.8	2.5	2. 1	3.2	45.4	900		10.9	80		l
-	0	0	0	0	0		5		_	9	2	1	9	. 6	1	0			_	_	-	2	3	-1	0	0		8	4			6	8	7	ω	_	_	7	z) «	-	-	L	دع		l
BASIN 14	0	0.	0	o 0	<u>-</u>	e O	13	<u>•</u>	6	4,	0 0	1.	9.	10.	_	0	26.	H	15.2	┝	7	9	7	0	0	0	_		\dashv	4	2 21.	4	20.	5	ω ∞	22	10	14	3,5	37	12	59	8 144.	-	ŀ
BASIN 13	0 (0. (0	6		-	2.	-	14.	0.	0 (25 /	59.	10.8	0. (18.	18.6	2.8	6	r.	1.6	20. (7.4	1.	0.0	0.8	12. (- 1	4.4		8	2.		4	2 (2. {	33.	75.7	39	16.	40.		
BASIN 12	0 0	0 0	0 0		0.0		0	0	2.6	1.4	4.4	0		49.2	2.1	0.0	10.0	19. 8	71.0	9	25.0	36.2	4.1	1.9	0.2	0.0	1.3	3.2	5 9	12. 6	ω Θ			6	9			4.3	10. Z	2 0	26.4		47.4	15.6	•
BASIN 11	0 0	0.0	0.0	0.0	0.0	0	0.0	0	2.6	0.0	0.0	9 0	64. 2	74.3	10.9	1.4		15.2	4. 5	5.5	 	2.8	15.8	13.6	1.7		0.0	7.1		9		0	-	0.0	2 3	0.0	1.3		38.3				21.0	10.4	
z	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	5.3	0	S. 55	0.0	3.4	51.0	0.0	0.0	4.4	1.5	86.0	4.4	9.3	3.5	3.9	2.3	0.0	0.0	0.0	0.0		0 0	3.0	0.0	0.0	8.9		89	1.0	4	- 7	-	1	L	L	5	
	0.	0.	0.	0	0	0		0			_	_	6	0		S.	0.		<u>س</u>	2	-	4	∞	4	-	~	-	-	6	~		-		-	7.	0		4	70	, 10		_	မ	~	
RASIN 9			0	0	0	4	4	9	╝	<u>-</u>		0	4	30.	11	4 7	3 11	19.	_	L	L	10		Ц	C	4	Ö		2	2	7	7			7	0		12	, 200	110	-	 	6 25.	ļ.,	
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BASIN 7	0.0	0.0	0.0		က က	0.0	7.	15.3	0	30	0	3.2	30.5	2.4	2.3	25. 4	28.0	30.4	39.8	27.6	18.5	14.7	4.3	16.6	48.1	23.6	37.8	7.5	15.5	38.1	2.5	0	0.4	0	19. 2	2	6	13.7	30.7	10.2	42.2	25.6	67.7	32.1	
BASIN	0.0	0.0	0.0	0.0	0.0	0	0.0	0	9	0	9 0	-1	60.3	81.3	9.1	0.0	0,4	11.9	12.2	4.4	10.2	5.5	نہ	14.1	1. 7	0.0	0.4		11.9	, i	0	0	0	7	2.9	0	1.2	-:I-	30.3	:1-:	58.2		18.8	9. 7	
2	$0, 0$ }	0.0	0.0	0.0	2.0	25.7	0.0	0	8.4	0	9.0			3.0	9.0	0.4	2.0	2.9	8.0	4.8	4.8	5.2	3.6	4.5	0.1	0.7	4.2	3.7	0.5	<u>ہ</u>	7.2	6.9	24.1	0.0	7.8	0.0	0.0	4	0 -	1	┺	_	1.2	0.2	
↦	0.0	0.0	0	0	₩,	7	ام	7	,_		5	0 4	. 7	. 2		. 1	. 3	5.4	8	₽.	3		20.0		_	4	ر ک		4		-	ľ	4	+	-+	ᅪ	-+		27.3	+	 	\vdash	Н	44.2 8	Ŀ
BA	0	0	0		0	0 49	0	0	104	6	0 56	0	2	9	1 2	3	7 7	9 /	0 21.	5 10	1 1	7 29	2 20	-	8 27	4	-	4 28.	7	5	90	4	200		4	4	+	+	0 27	╀	8 94	35	_	5 44	Ļ
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BASIN 2	0		0.0); ;		2.0						0		0 0	1.8	9.8	8. 7	40.8	3.2	3.6	35. 1	29.9	31 0	9 1	1.3	17. 2	21.8	125. 2		ŀ		اد	~	=	χ (200	0	7 .	74.0			3.4	110.5	8, 4	
BASIN	0.0	0.0	0.0	0.0	10.3	27		9	24.9	8.2	0	: .F	- 1	0.7	11.3	6.5	19.8	19.3	23. 7	25.6	9.0	75.7	49.6	11.4	10.1	43.0	33.1	34.3	5	45.4					:			200	2000	26.9	36.0	15, 1		17.1	
	16	17	18	13	707	77	77	23	24	25	26	27	28	29	-	-	1	-	3	Н	2		_	8	6	3	4	4	4	4				+	-	2	7	77	┪~	┪	26	Щ	_	Щ	L
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ESTIMATED DAILY RAINFALL FOR HIGH FLOW ANALYSIS

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E ■/03y	BASIN	77	34.8	1.3	0.1	0	0.7	13.0	8.2	5.0	0.8	7.8	-	رب س		0.5	15.7	16.4	0.0	0.0	0.0	0.0	0.0	0.0	0.7	23.6	0.8	5	0.0	0.2	7.6	8	c
unit:	BASIN	22	35, 5	0.2	0.0	0 0	0.0	13.5		9.6	1.0	0.0	0.0	3	0.0	0	16.8	10.8	0.0	0.0	0.0	0.0	0.0	0.0	0.0	23 8	1 4		9.8		7.5	6.7	2
1	BASIN	52	5.8	34.3	2.7	5	5.1	0.4	0.2	35.0	14.3	56.9	3.4	23.8	10.9	10.6	1.7	8	0.0	0.0	0.0	0.0	0.0	0.0	5.2	7.	22	3.4	0.0	6.0	5.4	3.6	9
	BASIN	2	15.6	33	0.1	0.2	0 2	5.0	3,1	1.3	15.8	2. 1	0.3	5.3	0.4	5	12.8	4.4	0.0	0.0	0.0	0.0	0,0	0	0 2	0 6	20.8	9.5	8.4	0.3	3.0	17.7	70
	BASIN		3.4	10.1	2.1	0	0.0	0.7	0.4	0.1	20.3	0.2	0.2	г. Б	0.6	7.3	9.2	1.9	0.1	0.0	0.0	0.0	0.0	0.2	0.0	0.3	25.8	11.8	10.5			18.3	
ŀ	5AS.	┪	0.0	57.2	4.9	0	0.0	0.0	0.0	0.0	19.5	2.3	2.0	4.9	7.8	16.6	2.9	18.5	0.0	0.0	0.0	0.0	0.0	2.0	0.0	0	0.0	0.0	0.0	10.7	5.9	0.0	0
ŀ	BASIN	-1	3	25. 4	10.1	0.0	0.0	1.0	0.4	9.0	5.6	0.5	0.3	1.5	1.2	2.8	1.5	2.9	0.3	0.0	0.0	0.0	0.0	0	0.0	0	3.3	. 5	1.3	1.7	1.2		
1	BASIN	1		6	5.9	0.0	0.0	0.2	0.1	0.1	17.1	2.6	1.7	4.3	6, 8	14.5	2, 5	16.2	0, 1	0 0	0.0	0.0	0.0	I. 7	0.0	0.0	0.0	0.0	0.0	9.4	5.2	0.0	2 5
ł	B NISA	-1	_		11.2	0.0	0.0	1.2	0.5	0.7	3.4	0.5	0.3	9.8		2.8	2	L				Н	0.0	0.3	0.0	0.0	0.0	0.0	0.0	1.8	1.3	0.0	9 2
ŀ	BASIN	7	_	-	2	0.0	0.0	0.1	0.0	0.0	15.9	2. 4	1.6	4.0	6.3	3.5	2.4	15.1	0.0	0.0	0.0	0.0	0.0	1.6		-0	0.0	0.0	0.0	8. 7	4.8	0.0	8
Ì.	DASIN	7	0	4	7.1	0.0	0.0	0.7	0.3	0.4	1.8	0.3	7	0.4	7	2	0.3	-	_	Ŀ	Н	Н		0 2	0.0	0.0	0.0	0.0	0.0	0.9	0.7	0.0	U
F	BASIN B	4	=	0.0	3.4	0.0	0.0	0.0	0.0	0.0	13. 7	2.0		3.4	5 5	1.5	2.0	13.0	0.0				_ ,	1.4	0.0	0.0	0.0	0.0		7.5			L
L	DASLN BA	TÌ.	_			0	0.0			2		1.5	1.4	2	4.3				_		_		_	4		_				Ц	4		_
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(5)-a at 1H10, Rudete, Mgcta and kidunda Dam Sites (YEAR 1974 Type)

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28 21.8 41.0 29.4 26.5 15.3 26.9 50.6 36.3 32.7 18.9 34.1 64.1 45.9 41.4 23.9 29 6.3 3.1 4.3 16.4 29.8 7.8 3.8 5.2 20.2 36.7 9.9 4.9 6.6 25.6 46.5	100														2. 2		25.4
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30 24.8 68.1 49.3 23.3 18.7 30.6 84.0 60.8 28.8 23.1 38.7 106.4 77.0 36.5 29.3	1	29															
	L	30	24.8	68.1	49.3	23.3	18.7	30.8	84.0	60.8	28.8	23. 1	38.7	106.4	77.0	36.5	29.3

(5)-a at 1H10, Rudete, Mgeta and kidunda Dam Sites (YEAR 1974 Type)

(5)-a at	1H10,	Rudete,	Mgeta	and kid	unda Da	■ Sites	(YEAR	1974 Ty	pe)	•				5.50	unit :	am/dov.
Return Pe	riod	1		1/5			Γ—		1/10					1/20	UILL	NB/ Gay
DATE		BASIN	BASIN	BASIN	BASIN	BASIN	BASIN	BASIN	BASIN	BASIN	BASIN	BASIN	BASIN	BASIN	BASIN	BASIN
MONTH	DAY	1	2	3	4	5	11	2	3	4	5	1	2	3	4	5
MAY	1	44.5	143.0	35.2	16.4	3. 2	55.0	176.5	43.5	20. 2	4.0	69.6	223, 6	55. 1	25.6	5, 1
Ī	2	35.8	15.5	3.4	12.0	2.8	44. 2 1. 0	19.2 0.0	4. 2 0. 5	14.8	3, 5 0, 7	56.0 1.2	24. 3 0. 0	5.3 0.6	18.8 20.7	4, 4 0, 9
:	$\frac{3}{4}$	0.8	0.0	0, 4	13. 3 9. 6	0.6	1.0	0.0	0.0	11.9	0, 7	1.2	0.0	0.0	15.1	0.1
	5	0.2	0.0	0.0	4. 5	0.0	0.2	0.0	0.0	5.6	0.0	0, 3	0.0	0.0	7.1	0.0
	6	0.0	0.0	0.0	20.0	1 1	0.0	0.0	0.1	24.7	1.4	0.0	0.0	0.1	31.3	1.7
	7	0.0	0.0	0.0	0.1	0.0	0.0	0.0	0, 0	0.1	0.0	0.0	0.0	0.0	0.2	0.0
	8	15.9	2, 5	0.0	1. 3	0.7	19.6	3.0	0.0	1.5	0.9	24.8	3.9	0.0	2.0	1.1 2.2
	10	3, 1 2, 0	3. 7 0. 2	0. 9 0. 2	6. 5 3. 1	1. 4 3. 4	3.8 2.5	4. 6 0. 3	1. 1 0. 3	8. 0 3. 8	1. 7	4. 8 3. 1	5. 8 0. 4	0.4	10.1	5.4
1	11	3.8	0. 5	0. 3	9. 7	9.6	4.7	0.6	0.4	12.0	11.8	5. 9	0.8	0.5	15. 2	15.0
1	12	9. 0	34. 1	8, 6	3, 1	3. 7	11.1	42.0	10.7	3.8	4.6	14.1	53. 3	13.5	4.8	5.8
	13	6.8	15.5	5.0	9, 8	20.5	8.4	19.1	6. 1	12.1	25. 3	10.6	24. 2	7.8	15.3	32. 1
	14	20.6	31.4	7.3	12. 9	6.8	25.4	38.8	9, 1	15.9	8.4	32. 2	49.1	11.5	20.1	10.6
	15	2.0	1.2	0.3	1.4	0.4	2.5	1.5	0.4	1.7	0.5	3.1	1.9	0.5	2.1	0.6
	16 17	0.0	0.0	0.0	11. 2 0. 0	10.9	0.0	0.0	0.0 1.1	13.8	0.0 13.4	0.0	0.0	0.0 1.4	17.5 0.0	0.0 17.0
-}	18	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-]	19	0.0	0.0	0.0	0. 1	0.0	0.0	0.0	0.0	0.1	0.0	0.0	0.0	0.0	0.1	0.0
	20	0.1	0.2	0.1	4.6	2. 5	0.1	0.3	0.1	5. 7	3. 1	0. 1	0.4	C. 1	7. 2	3.9
1	21	0.0	0.0	0.0	11.0	0.0	0.0	0.0	0.0	13.6	0.0	0.0	0.0	0.0	17. 2	0.0
:	22	0.0	0.0	0.0	1.6 1.2	0.0 0.1	0.0	0.0	0.0	2. 0 1. 5	0, 0	0.0	0. 0 0. 0	0.0	2. 5 1. 9	0.0
Į.	24	0.0	0.0	0.0	0.9	0.1	0.0	0.0	0.0	1.1	0. 1 0. 5	0.0	0.0	0.0	1.4	0.1 0.6
	25	0.0	0.0	0.0	0.6	0.3	0.0	0.0	0.0	0. 7	0.4	0.0	0.0	0.0	0. 9	0.5
	26	4, 2	19.6	5. 1	17.0	5. 2	5.2	24. 2	6.3	21.0	6. 4	6.6	30.7	8.0	26.6	8. 1
	27	7.2	33.5	8. 4	2.6	1.0	8. 9	41.3	10.3	3.2	1, 3	11.3	52. 3	13.1	4.1	1.6
	28	6.4	1. 2	0.1	1.1	0.3	7. 9	1.4	0.1	1.3	0.3	10.0	1.8	0.1	1.6	0.4
	29 30	2. 8 0. 0	11.9	3. 0 0. 0	0, 6 0, 4	0. 3 0. 0	3, 5 0. 0	14. 7 0. 0	3. 7 0. 0	0.7	0.4	4. 4 0. 0	18. 6 0. 0	4.7 0.0	0.9 0.7	0. 4 0. 0
	31	0.0	0.0	0. 6	0. 1	0. 2	0.3	0.0	0. 7	0.3	0.0	0. 4	0. 0 0. 0	0.0	0.1	0. 3
JUN.	1	0.0	0.0	0.0	3.5	1.2	0.0	0.0	0.0	4, 3	1, 5	0, 0	0.0	0.0	5. 4	1.9
	2	15.6	8. 7	21.0	4.9	3.5	19.3	10.7	25.9	[6. 1]	4. 3	24.5	13. 6	32, 9	7.7	5.5
	3	1.6	0.0	0.4	1.1	0.1	1.9	0.0	0.4	1.3	0.2	2.4	0.0	0.6	1.7	0, 2
	5	1.4 0.0	0.0	0.0	0. 5 1. 0	0.0	1.7	0.0	0.0	0.6	0. 0 0. 7	2. 2	0.0	0.0	0.7	0.0
	6	0.0	0.0	0.0	1.8	0. 0	0.0	0.0	0.0	1.2	0.7	0.0	0. 0 0. 0	0.0	1.6 2.9	0.9 0.0
	7	0.0	0.0	0.0	0.1	0.0	0.0	0.0	0.0	0.1	0.0	0.0	0.0	0.0	0. 2	0.0
	8	0.0	0.0	0.0	1.6	0.9	0.0	0.0	0.0	2.0	1, 1	0.0	0.0	0.0	2. 5	1.3
1	9	0.0	0.0	0.0	0. 0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
}	10	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1	11 12	0.0	0.0	0. 0 0. 1	0. 9 7. 5	0.0 4.7	0.0	0.0	0. 0 0. 1	9.2	0. 0 5. 8	0.0	0. O 0. O	0.0 0.1	1. 4 11. 7	0.0
1	13	0.0	0.0	9.0	0.1	0.1	0.0	0.0	0.0	0.2	0.1	0.0	0.0	0.0	0. 2	7.4
j	14	0, 0	0.0	0.0	2. 2	1.2	0.0	0.0	0. 0	2. 7	1.4	0.0	0.0	Ö.Ö.	3. 4	1.8
	15	0.0	0.0	0.0	0.6	6.3	0.0	0.0	0.0	0.7	0.4	0.0	0.0	0.0	0.9	0.5
1	16	0.0	0.0	0.0	11. 2	0.6	0.0	0.0	0.0	13.8	0.8	0.0	0.0	0.0	17.5	1.0
1	17 18	0.0	0.0	0.0	0, 3 0, 0	0.0	0.0	0.0	0.0	0.4	0.0	0.0	0.0	0.0	0.5	0.0
j	19	$0.0 \\ 0.0$	0.0	0.0	0.0	0.0	0.0	0.0	0.0 0.0	0.0	0.0	0.0	0. 0 0. 0	0.0	0.0	0.0
	20	0.0	0.0	0.0	0.4	0. 2	0.0	0.0	0.0	0.5	0.3	0.0	0.0	0.0	0.7	0.4
	21	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		Ŏ. O	0.0
	22	0.0	0.0	0, 0	13.0	0.0	0.0	0.0	0.0	16.0	0.0	0.0	0.0	0.0	20.3	0.0
	23	0.0	0.0	0.1	0.0	0.0	0.0	0.0	0.1	0.0	0.0	0.0	0.0	0.1	0.0	0.0
l .	24 25	0.0	0.0	0.0 1.8	4. 3 7. 0	2. 0 8. 3	0.0	0.0	0.0	5.3	2.4	0.0	0.0	0.0	6.8	3.1
	26	5.7	0. 9	0.2	7. 1	3.1	0. 2 7. 0	0.6 1.1	2. 3 0. 2	8.7	10. 3 3. 8	0. 2 8. 9	0. 7 1. 4	2. 9 0. 2	11.0 11.1	13.0
'	27	0.3	0.9	2. 9	0.8	1.5	0.3	1.1	3. 6	0. 9	1.9	0. 9	1. 4	4. 6	11.1	4.8
	28	0.1	0.3	1.4	1. 0	0. 2	0.1	0.4	1, 7	1.3	0. 2	0.1	0.5	2. 1	1.6	0.3
1	29	0.5	0.0	0.5	10.6	0.2	0.6	0.0	0, 6	13.0	0, 2	0.8	0.0	0. 8	18.5	0.3
L	30	0, 9	0.0	0.0	0.3	0.0	1.2	0.0	0.0	0.4	0.0	1.5	0.0	0,0	0.5	0.0

(5)-a at 1H10, Rudete, Mgeta and kidunda Dam Sites (YEAR 1974 Type)

(5)-a at	THIU,	naus ts,	MRaca	anu niu	anaa Pa	M D1003	(+Dim	2011 13	,		100		•		unit :	mm/day
Return Pe	rind			1/50					1/100					1/200		
DATE	1100	BASIN	BASIN	BASIN	BASIN	BASIN	BASIN	BASIN	BASIN	BASIN	BASIN	BASIN	BASIN	BASIN	BASIN	BASIN
MONTH	DAY	1	2	3	4	5	1	2	3	4	5	1	2	3	4	5
MAR.	16	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0,0	0.0	0.0	0.0	0, 0	0.0	0, 0	0.0
	17	0.0	0, 0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	18	0.0	0.0	0, 0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0, 0	0.0
	19	0.0	0.0	0.0	0.0	0.0	0.0	0,0	0.0	0.0	0.0	0.0	0,0	0.0	0.0	0.0
ľ	20	7.3	1.1	0.0	0.3	0.1	8.5	1.3	0.0	0.3	0.2	9.0	1.4	0.0	0.3	0.2
1	21	9.2	1.4	0.0	35. 2	19.1	10.6	1.6	0.0	40.7	22.1	11.2	1.7	0.0	43. 2	23.4
1	22	1.4	0.0	0.0	0.5	0.0	1.6	0.0	0.0	0.5	0.0	1.7	0.0	0.0	0.6	0.0
1	23	0.0	0.0	0.0	0, 2	0.0	0.0	0.0	0.0	0. 2	0.0	0.0	0.0	0.0	0.2	0.0
1	24	17. 8	67. 9	51.3	74. 9	77.6	20.6	78. 5	59.3	86. 7	89.7	21. 9	83.3	63.0	92. 0	95. 2
} .	25	4.5	0.0	0.0	6.8	2. 9	5. 2	0.0	0.0	7. 9	3. 3	5. 5	0.0	0.0	8.4	3.5
1	26	0.0	0.0	0.0	40.7	21. 9	0.0	0.0	0.0	47. 1	25. 3	0.0	0.0	0.0	50.0	26.9
1	27	2. 9	0.4	0.0	0.3	0.0	3.4	0,4	0.0	0.3	0.1	3.6	0.4	0.0	0.3	0.1
1	28	8.5	0.4	5. 1	6. 2	2.0	9.8	0.5	5.9	7.2	2.4	10.4	$\frac{0.5}{0.0}$	6.3	7.7	2.5
1	29	0.5 8.1	0.0	6. 8 0. 8	0. 2 1. 5	2. 1 0. 4	0.5 9.3	0.0 1.5	7. 9 0. 9	0. 2 1. 7	2. 5 0. 5	9.9	0.0 1.5	8.4 1.0	0. 2 1. 8	2.6 0.5
1	30		1.3 0.6	0.0	2, 2	0.4	5.4	0.6	0.0	2.6	0.3	5.7	0.7	0.0	2.7	0.3
165	31	4.6 14.2	6.2	3, 4	5.3	1.4	16.4	7.2	3.9	6. 1	1.6	17.4	7.6	4.1	6.5	1.7
APR.	1 2	14. 3	29. 2	20.5	4.6	2.1	16.5	33.7	23.7	5. 3	2.4	17.5	35.8	25. 2	5. 7	2.6
1	3	17.0	2. 3	0.0	15. 7	5.7	19.6	2.6	0.0	18. 1	6.6	20.8	2.8	0.0	19. 2	7.0
1	4	18. 3	2.6	0.4	7.4	3, 4	21. 2	3.0	0.4	8.6	4.0	22.5	3, 1	0.4	9. 1	4. 2
1 :	5	6.5	25. 1	18.7	1.3	3.5	7.5	29.0	21.6	1.6	4. 1	7.9	30.8	22. 9	1.7	4.3
	6	54.2	21.4	9.8	20.9	10.9	62.7	24.7	11.3	24. 2	12.6	68.5	26, 2	12.0	25.7	13.4
	7	35.5	22. 2	15. 2	14.3	31.2	41.1	25. 7	17.5	16.6	36.1	43.6	27.3	18.6	17. 6	38.3
	8	8. 1	6. 5	7.1	22.1	39.0	9.4	7.5	8. 2	25. 5	45.1	10.0	8.0	8.7	27. 1	47.8
	9	7. 2	0, 9	0.6	19.8	0.1	8.4	1.0	0.7	22. 9	0.1	8.9	1.1	0.7	24. 3	0.1
1	10	30.8	12. 3	5. 7	14.5	7. 7	35. 6	14. 2	6.5	16.8	8. 9	37. 7	15.1	6. 9	17. 8	9.4
j	11	23. 7	15. 6	10. 2	5. 5	17.4	27.4	18.0	11.8	6. 3	20. 1	29, 1	19.1	12.5	6. 7	21.3
1 .	12	24. 5	89.6	66.1	20.5	38. 4	28. 3	103.6	76.4	23.7	44.4	30.1	110.0	81.1	25. 2	47.1
	13	7.0	0.7	0, 9	1.0	0.4	8.0	0.8	1.0	1.2	0.4	8. 5	0.8	1.1	1. 2	0.4
	14	18. 2	52. 9	38. 2	22. 3	12.8	21.0	51. 2	44.2	25.8	14.8	22. 3	65.0	46.9	27.4	15.7
1	15	0.0	0.0	0.0	21.8	5. 1	0.0	0.0	0.0	25. 2	5.9	0.0	0.0	0.0	26. 7	6. 3
	16	2.5	0.5	0.1	1.6	0.7	2.9	0.6	0.1	1. 8	0.8	3. 1	0.7	0.1	1. 9	0.8
1	17	6.6	1. 9	2, 0	2.5	17. 3	7.7	2. 2	2.3	2. 9	20.0	8.2	2.4	2. 4	3. 1	21.2
1	18	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1	19	8. 5	4.1	2. 9	20.1	20. 2	9.8	4.8	3.3	23. 2	23. 3	10.5	5.1	3. 5	24. 7	24. 7
1	20	0.8	0.0	0.0	8.6	0.0	0.9	0.0	0.0	10.0	0.0	0.9	0, 0	0.0	10. 6	0.0
-1	21	1. 2	0.0	0.0	17. 4	0.0	1.4	0.0	0.0	20.1	0.0	1.5	0.0	0.0	21.4	0.0
1	22	7.1	1.8	0.9	6.3	4.7	8. 2	2.0	1.0	7.3	5. 4	8.7	2. 1	1.0	7.7	5. 7
f .	23	22. 1	7.6	6.7	7.5	4, 9	25. 6	8.8	7.8	8, 6	5. 6	27. 1	9. 3	8. 2	9, 2	6.0
1	24	207.7	53.2	19.3	62.4	36.5	240.2	61.5	22.3	72.2	42. 2	254. 9	65.3	23.7	76.6	44.8
1	25	19.3	43.2	39.6	57. 6	43. 6	22.3	50.0	45.8	66.6	50.4	23.7	53.1	48. 6	70.7	53.5
1	26	25.8	5.7	7.0	67.7	18.7	29.8	6.6	8.1	78.3	19.3	31.6	$\frac{7.0}{2.0}$	8, 6	83.1	20.5
	27	10.8	2.5	2.7	25.4	25. 2 29. 5	12.5	2.9	3.1	29. 4 59. 0	29.1	13.2	3.0	3.3	31. 2	30.9
1	28 29	42. 1 12. 2	79. 1 6. 0	56. 7 8. 2	51. 1 31. 6	57.4	48.7 14.1	91. 4 7. 0	65, 5 9, 5	36. 6	34. 1 66. 4	51. 6 15. 0	97.1	69.5 10.1	62. 7 38. 8	36. 2 70. 5
į.	30	47.8	131. 3	95. 1	45.0	36, 1	55. 2	151. 9	109.9	52. 1	41.8	58. 6	7.4 161.2	116.7	55. 3	44.3
	1 30	47.0	1 1 1 1	33.1	*J. U	00, 1	1 33.4	1101.2	103.3	1. 16. 1	1 41.0	30.0	101.2	110.1	<u> </u>	1 44. 3

(5)-a at 1H10, Rudete, Mgeta and kidunda Dam Sites (YEAR 1974 Type)

(5)-a at	1810,	Kudete,	Mgeta	and Kid	unda va	m orres	(1EBN	1914 IA	pe)	φħ			i		unit :	mm/day
Return Pe	riod			1/50				(1) (1) (1) (1) (1) (1) (1)	1/100	11				1/200		
DATE		BASIN	BASIN		BASIN	BASIN	BASIN	BASIN	BASIN	BASIN	BASIN	BASIN		BASIN 3	BASIN 4	
MONTH	DAY	00 0	275 0	3	31.6	5 6. 2	99.3	319.0	78.6	4 36.6	7. 2	105.4	338. 6	83.4	38, 8	$\frac{5}{7.7}$
MAY	$\frac{1}{2}$	85. 9 69. 1	275. 9 29. 9	68. 0 6. 5	23. 2	5. 4	79.9	34. 6	7. 5	26, 8	6. 3	84. 8	36.8	8.0	28. 4	6.6
1 .	3	1. 5	0, 0	0.7	25.6	1, 1	1.8	0.0	0.8	29.6	1.3	1. 9	0, 0	0, 9	31.4	1.4
	4	1.5	0.0	0.0	18, 6	0. 2	1.8	0.0	0.0	21.5	0.2	1.9	0.0	0.0	22. 8	0.2
	5 6	0.4	0.0	0.0	8.7	0.0	0.4	0,0	0.0	10.1	0.0	0.4	0.0	0.0	10.7	0.0
	6	0.0	0.0	0.1	38.6	2.1	0.0	0.0	0. 1 0. 0	44. 6 0. 2	2. 5 0. 0	0.0	0.0	0.1	47. 4 0. 2	2. 6 0. 0
1	- 7 8	0.0 30.6	0.0 4.8	0.0	0. 2 2. 4	$0.0 \\ 1.3$	0.0 35.4	0, 0 5, 5	0.1	2.8	1.6	37.6	5.8	0.1	3, 0	1.7
1	9	5. 9	7.1	1.8	12.5	2. 7	6.8	8. 2	2.0	14. 5	3. 1	7. 3	8.7	2. 2	15. 4	3. 3
	10	3. 9	0.5	0.4	6.0	6.6	4.5	0.5	0.5	6.9	7.7	4. 7	0.6	0.5	7. 3	8, 1
	11	7.3	1.0	0.7	18.7	18.5	8.4	1.2	0, 8	21.7	21.4	9.0	1, 2	0.8	23.0	22. 7
	12	17.4	65. 7	16. 7	6.0	7.2	20.1	76.0 34.5	19. 3 11. 1	6. 9 21. 8	8. 3 45. 7	21.3 16.0	80. 7 36, 6	20. 5 11. 8	7. 3 23. 1	8. 8 48. 6
	13 14	13.1 39.8	29. 8 60. 6	9, 6 14. 2	18.8 24.9	39.6 13.1	15.1 46.0	70.0	16.4	28.7	15.1	48.8	74.3	17.4	30.5	16.1
1 .	15	3, 9	2. 4	0.6	2. 6	0.8	4. 5	2.8	0.7	3, 0	0.9	4.7	2, 9	0.7	3. 2	1.0
	16	0.0	0.0	0.0	21.5	0. 0	0.0	0.0	0.0	24.9	0.0	0.0	0.0	0.0	26.4	0.0
	17	0.0	0.0	1.7	0.0	21.0	0.0	0.0	1.9	0.0	24, 3	0.0	0.0	2.0	0.0	25.8
	18	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0,0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	19	0.0	0.0	0. 0 0. 1	0. 1 8. 9	0. 0 4. 8	0.0 0.1	0.0 0.5	0.0 0.1	0. 1 10. 3	0. 0 5. 6	0.0	0.0	0.0	0. 1 10. 9	0. 0 5. 9
	20 21	0. 1 0. 0	0.0	0. 0	21.3	0.0	0.0	0.0	0.0	24. 6	0.0	0.0	0.0	0.0	26. 1	0.0
	22	0.0	0.0	0.0	3. 1	0. Ŏ	0.0	0.0	<u>0. ŏ</u>	3.6	0.0	0.0	0.0	0, 0	3. 9	0.0
	23	0.0	0.0	0.0	2. 3	0. 2	0.0	0.0	0.0	2.7	0.2	0.0	0.0	0.0	2. 9	0.2
	24	0.0	0.0	0.0	1.8	0.8	0.0	0.0	0.0	2.0	0.9	0.0	0.0	0.0	2.1	0, 9
i	25	0.0	0.0	0.0	1.1	0.6	0.0	0.0	0.0	1.3	0.7	0.0	0.0	0.0	1.4	0.7
1	26 27	8. 2 13. 9	37. 9 64. 5	9.8 16.1	32. 9 5. 0	10.0 2.0	9. 4 16. 1	43. 8 74. 6	11. 4 18. 7	38. 0 5. 8	11.6 2.3	10.0 17.1	46. 5 79. 2	12.1 19.8	40. 4 6. 2	12. 3 2. 5
1	28	12.3	2. 2	0.1	2.0	0.5	14.3	2.6	0.1	2. 4	0.6	15. 1	2.7	0. 1	2. 5	0.7
1 .	29	5. 4	22. 9	5, 8	1. 2	0.5	6. 3	26. 5	6, 7	1, 3	0.6	6.6	28. 1	7.1	1.4	0.7
	30	0.0	0.0	0.0	0.8	0.0	0.0	0.0	0.0	0. 9	0.0	0.0	0.0	0.0	1.0	0.0
	31	0.5	0.0	1.1	0.2	0.3	0, 5	0.0	1.3	0.2	0.4	0.6	0.0	1.3	0, 2	0.4
JUN.	1	0.0	0.0	0.0	6.7	2.4	0.0	0.0	0.0	7.7	2.8	0.0	0.0	0.0	8. 2	2.9
	3	30. 2 3. 0	16.7 0.0	40. 5 0. 7	9. 5 2. 1	6, 8 0, 2	34. 9 3. 5	19.3 0.0	46. 9 0. 8	11.0 2.4	7. 8 0. 3	37. 0 3. 7	20. 5 0. 0	49.8 0.8	11. 6 2. 5	8. 3 0. 3
1	4	2.7	0.0	0.0	0.9	0.0	3.1	0.0	0.0	1.0	0.0	3.3	0.0	0.0	1.1	0.0
	5	0.0	0.0	0.0	1.9	1.1	0.0	0.0	0.0	2. 2	1. 2	0.0	0.0	0.0	2.4	1.3
	6	0.0	0.0	0, 0	3, 6	0.0	0.0	0.0	0.0	4.1	0.0	0.0	0,0	0.0	4.4	0, 0
	7	0.0	0.0	0.0	0.2	0.0	0.0	0.0	0.0	0.3	0.0	0.0	0.0	0.0	0.3	0.0
	8	0.0	0.0	0.0	3.1	1.7	0.0	0.0	0.0	3, 5	1.9	0.0	0.0	0.0	3.7	2.0
	10	0.0	0.0	0. 0 0. 0	0. 0 0. 0	0. 0 0. 0	0. 0 0. 0	0.0	0. 0 0. 0	0. 0 0. 0	0. 0 0. 0	0.0	0, 0 0, 0	0.0	0.0	0. 0 0. 0
	11	0.0	0.0	0.0	1.7	0.0	0.0	0.0	0.0	2.0	0.0	0.0	0.0	0.0	2. 1	0.0
	12	0.0	0.0	0.1	14.4	9. 1	0.0	0.0	0.1	16.7	10.5	0.0	0.0	0.1	17.7	11.1
	13	0.0	0.0	0.0	0.3	0. 2	0.0	0.0	0.0	0.3	0.2	0.0	0.0	0.0	0.3	0, 2
	14	0.0	0.0	0.0	4. 2 1. 1	2.3	0.0	0.0	0.0	4. 8 1. 3	2.6	0.0	0.0	0.0	5.1	2.8
ŀ	15 16	0. 0 0. 0	0.0	0. 0 0. 0	21.6	0. 6 1. 2	0.0	0.0	0.0	25. 0	0.7 1.4	0.0	0. 0 0. 0	0.0	1. 4 26. 6	0.7 1.5
	17	0.0	0.0	0.0	0.6	0.0	0.0	0.0	0.0	0.7	0.0	0.0	0.0	0.0	0.7	0.0
	18	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	19	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1	20	0.0	0.0	0.0	0.8	0.5	0.0	0.0	0.0	1.0		0.0	0.0	0.0	1.0	0.5
ŀ	21	0.0	0.0	0.0	0.0 25.0	0.0	0.0	0.0	0.0	0. 0 29. 0	0.0	0.0 0.0	0. 0 0. 0	0.0	30.7	0.0 0.0
1	23	0.0	0.0	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.0	0.0
	24	0.0	0.0	0.0	8. 3	3.8	0.0	0.0	0.0	9. 6	4. 4	0.0	0.0	0.0	10. 2	4.7
	25	0.3	0.9	3, 5	13.6	16.1	0.3	1.0	4. 1	15. 7	18.6	0.4	1.1	4.3	16.7	19.7
	26	11.0	1.7	0.3	13. 7	6.0	12.7	2.0	0.3	15.8	6. 9	13.5	2. 1	0.4	16.8	7. 3
]	27	0.5	1.7	5. 7	$\frac{1.5}{2.0}$	2. 9	0.6	1.9	6.6	1.7	3.4	0.7	2.0	7, 0	1.8	3.6
	28	0.2	0.6	2. 6 0. 9	2. 0 20. 4	0.4	0. 2 1. 1	0.7	3. 0 1, 1	2. 3 23. 5	0.4	0.2 1.2	0.7	3. 2	2. 4 25. 0	0. 5 0. 4
	30	1.8	0.0	0. 3	0.6	0.0	2. 1	0.0	$\frac{1, 1}{0, 0}$	0.7	0.0	2.2	0.0	0.0	0.8	0. 0
					`											

ESTIMATED DAILY RAINFALL FOR HIGH FLOW ANALYSIS

unit : mm/day	RACIN		0.0	0 0	-	2.7	0.0	0.0 0.0	10.5	0.0		9 6	24.0	25.9	6.2	15, 2	α ∞	21.6	13.4	14° 0	7	χ) u	100	13.4	12.3	18.0	4.6	27 L	0	0.5	o,	0.0	6 13.0 1.6	0.4	800	6.5	43.	2 64. 6 01. c	23.7	10.3	2 33.9 18.2	•
	NRACTN		0.0 0.0	- -	3 0	2 2	0	0 5.1	0 10.3	7	77	9.0	200	1	S	3 18.	4	1	_		-	3	,	34.2		_	H	× 5	1	- (5	- ∞	0	5 13.	~; 	9	5	33.		5 30	0 18.	2 48.	
5	RACIN RACIN		0.0	e	5 0		0.0	0.0	3.9		_) c	ļ.	1.3 20.	ļ			0.3 12.	1	\perp	_	1	1		L	16.9	4		1.0	5	0, 1	0.0 0.0	2, 2 1.	4		_	+	1 5 80		Н	1.9 17.	
-	BACIN BAG	+	0.0) C	2 45	<u> </u>	8	,,,) r		٥	1.5	L			_1	_1.	Ŧ	ᆚ	L	39 2 1	L	L	Ll	┙	\perp	0	0.3	0.0	12.8 1		_	_L		_	2	Н	4	L.
_	MINA	<u>.</u> -	0.0	0.0) c	o =	0.6						1.	L	7.0	LJ		Ш	_		⊥.	1	_	200	↓.	L	Ц	4	_	↓_	╄-	L	L		9,0			20.00	9 4	0.0	16.1	•
1 /50		000	0.0	0.0	3 C	2 6	0.0	0.0	9.3	0.0	4.5	0 0	21.0	22.8	5.5	13.4	7.7	19, 1	7.7	2.9	12.5	7.5	7	18.7	9 00	15.9	4.1		2 -	8 4	0.1	0.0	11.5	0.3	0.7		43.8	7 × 7	20.9	9 1	29.8	
	RACTE	┽		4	1	9.0	Ö	4	Ц	Ц	7) c	Ţ	1	i	15.9	17.	13.1	+	4	4	4	4	30.4	Ļ	╄	4.7	4	2 7 6	╀	7 0.3	0.0	Ц	3.4	3	-	4	7 5	╀	Н	7 42.5	•
	N PACIN	+	0.0	0	-	5 -	00	0 0.	5 0.		o •		3 4	1	ė	4	_		<u>~</u>	_	n	ه ام	o ·	4 -		5	7	e;	9		0	0.	1.	ö	o)	4		2		e	14.	2
(G/ F	TN BACTA	_	0.1	0.0	1	9 6	. 0			0.0	1	0.0	0 14	7	╀	9	16.0 7.	1.4 17.4		15.8 11.		4 6	٠,٠	6 1 2 0	13.5	. 7 14.	65	8 8	27. 4 D		2	0.0	0		5.4		40.	2,00	2	4.7 8.3	38.8 27.	
(1)	NETA BACTA	0 0 000	Ц	0	-	1	0.5	Н	0.0	Ц	4	900	ľ	L	5.9	Ш	L	Ц	_	4	20	2 2	,	4.4	1		9.2	0	7		0.7		1	1	-	ľ	8 1	1	1~	0.0		
Sites (YEAR 1974 Type)	01/10			0	0 0	0.0 0	0.0	0.0	7.8		┙	4	L	L	L	L	L	Ц	_	_	16.5	e e	0,0	16.4	6 0	13.4	3.4	e c	2 -	0.4	0.1	0.0	7	3	\rightarrow	+	+	2 2	╁┈	1	25. 2	,
s (YEAR	BACTU	+-	0.0	0.0	0.0	0 -	0.0	3,8	8 1	0.0	18.1	0 0	6 3	1.3	1.2	13. 5	14.8	16.1	21.1	14.5	20 (8 6	2.5	25. &	19.5	20.0	4. 0	8 6	7 0.7	9 0	0.2	0.0	10.2	5.8	2, 0	7.2	23.0	10.3	22 3	13.6	35.9	
	BACTN	9	0.0	0.0	0.0) c	0.4	0.0	0.0	╌┥	-+	-		12.7	4.7	3.3	-	-		2.3	20				-	0.0		2.4	1 7	1 1	0.5	0.0	1 .1	0.0	ö	65	1	+		0.0	10	
rengere 1	C/I	2 00	0.0		0.0	10.0	o	0	5 6.3	Ц	4	0 0	ľ	15.	۳,	8 9.1	5.	12.	11.6	æ •	1	2 5.1	٠,	7 7	; -	Г	2	2.		.1	6		1 7.7	0	ات	e		3 22 6	1	H	20.	
and Nge	DACTN	T	16 0.0	0	18 0.	= -	6	6.5	ε.	٥	2	26 0.	- 6		Ľ	10.		12.					1	20,00		16	6	بات	15	-	0	0		2.	Ť	أنا	23:	25 1 13.	-	10.	28 28.	
(5) at 1HA1A and Ngerengere Da	neturn Feriod	MONTH DAY	H		1	I]		1				APR.		.]	1		1	1	1	Ĺ		∐	<u>]</u>	<u> </u>							1		1				_

ESTIMATED DAILY RAINFALL FOR HIGH FLOW ANALYSIS

(6) at 1HA1A and Ngerengere Dam Sites (YEAR 1974 Type)

mm/day		BASIN	5	0.1	22.7	3.4	0.0	0.0	0.3	0.1	0.1	6.9		1.0	1.8	3.0	6.2	1.0	5.4	0.1	0.0	0.0	0.2	0.0	0.7	0.0	0.0	0.0	0.2	0.0	3.7	2.1	0.0	2.5
	/200	BASIN	8	1.1	13.1	7.7	0.8	0.4	1.9	12.8	7.3	31.0	3.4	6.5	1.7	7.0	1.7	0.3	2.7	0.1	0.0	0.0	0.0	0.8	0.3	0.1	1, 3	1.4	16.9	0.7	1,1	0.3	0.0	4.6
מו		BASIN	2	3.3	8.6		7.9	2.4	2	8	4	2			3	-		11.0	2.6	0.0	0.0	0.0	0.0	2.7	0.4	0.3	1.4	1.5	19.4	1.0	3,4	1.7	0.1	1.7
		BASIN	6	0.1	21 4	3.2	0.0	0.0	0.2	0.1	0.11	6.5	1.0	101	1.7	2.9	5.8	1.0	6.0			0.0		0.0	0.6	0.0	0.0	0.0	0.2	0.0	3.5	2.0	0.0	2.4
	1/100	BASIN	8	1.1	12.3	7.3	0.7	9.4	1.8	11.8	6.9	29.2	3.2	6.1	1.8	9	1. 6	0.3	2.6	0.1	0.0	0.0	0.0	6 0	0.3	0.1	1.2	1.3	15.9	0.7	1.0	9.0	0.0	4.4
		BASIR	7	3 1	8.1	11.1	7.4	2.3	4. 2	12. 1	6.9	41.5	15.9	8 8	6.5	11.3	6, 3	10.4	2.4	0.0	0.0	0.0	0.0	2.8	0.4	0.3	1.3	1.4	18.2	0.0	3.2	1.6	0.1	1.8
		BASIN	50	0.1	20.0	3.0	0.0	0.0	0.2	0.1	0.1	5.1	1.0	0.9		2.7	5.4	0.9	2. 1	0.0	0.0	0.0	0.2	0 0	0.6	0.0	0.0	0.0	0.2	0.0	3.3	1.8	0.0	2. 2
	1/50	BASIN	æ	1.0	11.5	8.8	0.7	0.3	1.7	11.1	6.5	27.3	3.0	5.7	1.5	6.1	1.5	0.3	2.4	0.1	0.0	9.0	0.0	0.8	0.3	0.1	1. 2	1.3	14.8	0.6	0.9		0.0	4.1
		BASIN	_	2, 9	7.6	10.4			3.9			38.9		8.2	9	10.6	5.9	9.7	2.3	0.0	0.0	0.0	0.0	2.4	0.3	0.2	1.2	1.3		6.0	3.0	1.5	0 1	1.5
		BASIN	5	0.1	18.3		0.0	0.0	0.2	0.1	0.1		0.9	0.8	7	2.4	5.0	0.8	5.2		0.0	0	0,1	0.0	0.5	0.0	0.0	0.0	0.1	0.0	3.0	1.7	0.0	2.0
	1/20	BASIN	∞	0.3	10.5	6.2	0.6	0.3	1.5	10.1	5.9	25.0	2.7	5.2	1.4	5.6		0.2	2.2	0.1	0.0	0.0	0.0	0.8	0.3	0.1	1.1	1.1	13.6	9.0	0.8	0.5	0.0	3, 7
		BASIN	-	2.8	6.9	5 6	6.4	2.0	3.6		5.9	35.5	13.8	2 /	9.5	9.7	5.4	8.9	2.1	0.0	0.0	0	0.0	2.2	0.3	0.2	1.1	1.2	15.6	0.8	2.7	1 4	0 1	1.4
		BASIN	6	0.1	16.9	2.5	0.0	0.0	9.2	0.1	0.1	5. 1	0.8	8 0		2.3	4.6	9.0	4.8	0.0	0.0	0.0	0.1	0 0	9 0	0.0	0.0	0.0	0.1	0.0	2.8	1.6	0.0	1.9
	1/10	BASIN	80	0 8	9.7	5.8	9.6	0.3	1.4	9.3	5.5	23.1	2.5	4.8	1.3	5.2	1.3	0.2	2.0	0.1	0.0	9.0	0.0	0.7	0.2	0.1	1.0	1.1	12. 5	0.5		0.5	0.0	3.4
1		BASIN	-	2.4	9 4	88	5.9	1.8	3.3	9.6	5.5	32.9	12.6	6 9	3.	9.8	5.0	8.2	1.9	0.0	0.0	0.0	0 0	2.0	0.3	0.2	1.0	1.1	14.4	0.7	2.5	1.3	0.1	1.3
		BASIN	o,	0.1	13.5	2.0	0.0		0.2		0.1	4.1	0.7	9.0	1,1		3.7	9.0	3.8		0.0	0.0	0.1	0.0	0.4	0.0	0.0	0.0	0.1	0.0	2.2	1.2	0.0	1.5
	1/5	BASIN	∞	0.7	~	4.6	0.5	0.5	1.1	7.5	4.4	18.5	2.0	က	1.0	4.2		0.2	1,6	9.1	0	0.0	0.0	0.6	0.2	0.1	9,8	0.8	10.0	0.4	9.6	0.4	0.0	2.8
		BASIN	~	1.9	5.1	7.1	4.7	1.5	2.7	7.6	4.4	26.3	10.1	5.5	4.1	7.2		6.6	1.5	0.0	0.0	0.0	0.0	1.6	0.2	0.2	0.8	0.9	11.5	9.0	2.0	9.	-	1.0
	eriod		DΑΥ	-	2	3	4	ιΩ	9	-	œ)	6	10	=	12	13	14	15	16	17	18	13	20	21	22	23	24	25	56	27	28	23	39	3.1
	Return Period	DATE	HONTH	ΜΑΥ															•															

ESTIMATED DAILY RAINFALL FOR HIGH FLOW ANALYSIS

(6) at 1HAIA and Wgerengere Dam Sites (YEAR 1974 Type)

								-	-			-			3 (3 00 0)									برعبد					٠.,	وعده		_
	BASIN	8	0.1	4.0	6.3	0.0	0.0	0.0	0.0	0.1	0.0	0.0	0.0	0.3	0.0	0.1	0.0	0.0	0.0	0.0			0.0	0.0	0.0	0.1	0.3	0.1	2.2	7.7	8 8	0.0
1/200	2	8		2.8	5.4	0.0	0.0			0.0	0.0	0.0	0.1	0.0				0.9				0.0	0.0	1.1	0.0	0.1	0.0	4	1.5	5.2	-2	1.6
	BASIN		12,0	0.0	12.1	9.8	0.0		0.0		0.0		0.2	0.0				2.5		0.0	0.0		0.0				0.0		0			ж С
	BASIN	8	0.1	3.8	5.9	0.0	0.0	0.0	0.0	0.1]	0.0	0.0		0.3	0.0		0.0	0.0	0.0	0.0	0.0	0.0			0.0		0.2	0.1		7.2	8.1	0.0
1/100	BASIN	8	10.8	2.5	5.0	0.0	0.0	0.1	0.0	0.0	0.0	0.0	0.1	0.0	0.0	0.0		8.0		0.0	0.0		0.0	1.0	0.0		0.0	0.4	1.4	4.9	7.2	.5
	BASIN	7	11.3	0.0	11.4	9.3	0.0	0.4		0.0	0.0		0.2	0.0	0.0		0.0	2.4		0.0			0.0		0.0	0.2		1.2	0.0	0.1	9	7 8
l	BASIN	6	0.1	3.8	5.5	0.0	0.0		0.0	0.1	0.0	0.0	0.0	0.2	0.0	0.1	0.0	0.0		0.0	0.0	0 0			0.0	0.1	9.2	0.1		6.8		0.0
1/50	-	-	10.1	2.3	4.7	0.0	0.0		0.0	0.0	0.0	0.0	0.1	0.0	0.0			9.8		0.0	0.0	0.0		1.0	0.0	0.1	0.0	0.4	1.3		6.7	1.4
	BASIN	-	10.6	0.0	10.7	8. 7	0.0	0.4 0	0.0	0.0	0.0	0.0			0.0			2.2	0.1	0.0		0.0	0.0	2.8	0.0	0.2	0.0	1.1	0.0	0.1	0.9	7.3
	BASIN	1	0.1	3,3	5.0	0.0	9.0		0.0	0.0	0.0	_	0.0	1 .	0.0	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.2	0.1		6.2		0.0
/20	BASIN	_	9. 2		4.3	0.0	1.	0.1	0.0	0.0	0.0	0.0	0.1	0.0		0.0		0.7		0.0			0.0		0.0		0.0	0.3	1.2	4.2	6.1	1.2
	BASIN	T	6.7	0.0	8.6	8.0	0.0	0.4	0 0	0.0	0.0	0.0	0.2	0.0	0.0		0.0	2.0	0.1	0.0	0.0	0	0.0	2. 6	0.0	0.2	0.0	1.0	0.0	0.1	ភេ	6 7
	BASIN	8	0.1	3.0		0.0	9.0	0.0	0.0	0.0	0.0	0.0	0.0	0.2			0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.2	0.1	1.6	5.7	6.4	
/10	BASIN		8.5	Ι.	4.0	0.0	0.0	0.1	0.0	0.0	0.0	0.0	0	0 0	0.0	0.0		9.0		0.0				0.8			0.0	0.3	1.1	3.9	2 3	1.2
	BASIN		8.9	0.0	8.8	7.4	0.0	0.3	0.0	0.0	0.0	0.0	0.2		0.0	0.0	0.0	1.9	0, 1	0.0	0.0	0.0	0.0	2.4	0.0		0.0	0.9	0.0	0.1	5.0	6. 2
	ASIN	Ī	0.1	2.4	3.7	0.0			0.0	0.0	0.0	0.0		0.2		0.0			0.0				0.0						1.3		5.1	0
1/5	BASIN	80	8		3.2		0.0	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0		0.0	0.5	1 1	0.0	0.0	0.0	0.0	0.7	0.0	0.1	0.0	0.3	0. 3	3. 1	4.5	
	BASIN		7.2	0.0	7.2	5.9		9.3	0.0	0.0	0.0	0.0	0.1	0.0	0.0		1.	1.5						1.9	0.0		0.0	0.7	0.0	0.1	4.0	6.9
T Poi		DAY	-	2	3	4	Ľ	9	2	8	6	10	=	12	13	14	15	91	17	18	13	20	21	22	23	24	25	28	2.7	28	28	30
Paring Paring	DATE	т	T-			L		•		-		•									•						:					

(1)-a at Hydrological Stations

		-						33.5			unit : n	3/s
: :						11[8				7.00		
YEAR		196	8			197				197		
DAY	MAR.	APR.	MAY	JUN.	MAR.	APR.	MAY	JUN.	MAR.	APR.	MAY	JUN.
1	37.79	352.96	616.79	129.57		75. 82	242.68	107.19		25.05	197. 32	132.85
2	37.79	368.15	590.35	131.29		78. 36	285, 98	102.54		28, 68	240.92	129, 21
3	37, 80	375. 46	560.76	134.96		79.97	339, 07	98, 32		32.25	298.74	125.85
4	37. 82	377.03	532.16	140.66		81.02	401.37	94.42		36.00	371. 74	122. 26
5	37.89	375.87	502, 21	147.75		82. 32	471.52	90.76		40.19	458.59	118. 55
6	38.07	374, 53	468.59	155.64		84. 62	542.50	87. 32		45.08	547.08	115. 10
7	38.42	375.07	431. 21	163.41	7 + 7	88. 35	604.19	84.06		50.72	617.10	111.83
8	38. 94	386.03	392. 78	168.93		94, 53	649.06	80.98		57.00	649.68	108, 63
9	39.60	408, 34	357.87	170.88		105. 52	672.45	78.06		63.95	639.24	105. 32
10	40.39	438.99	328.99	170.62		123. 26	673.67	75.40		71.59	595. 27	101.76
11	41.39	485.57	305.77	169,81		145. 19	653.14	73.11		79.27	535.28	98. 02
12	42.98	562.11	285.76	168.41		167, 69	610.86	71.02		86.05	473.73	94.16
13	45. 78	659.32	267.48	166.09		189.12	554.14	69.00		91.93	417.92	90. 29
14	49.81	740.99	250.57	162.96		208.87	493.40	67.00		97. 96	372.17	86.49
15	54.83	782.53	234.77	158, 80	-	225.01	435.51	65.03	٠.	105. 12	337. 39	82. 84
16	61.32	788. 99	219.90	153.44	47. 91	236.03	384.74		11. 39	113.51	311.56	79.39
17	69.36	782.07	205.99	147.24	47. 91	242.02	341.62		11.39	122.79	292.46	76.18
18	79.29	775. 57	193.15	140.76	47. 91	244.73	304.68		11.39	132.28	278. 71	73. 21
19	92. 20	767.73	181.46	134.48	47. 91	246.83	272.82		11, 39	140, 43	268.34	70.43
20	108, 41	752.05	171.06	128.62	47. 91	248.38	245.63		11.39	145, 80	259.76	67, 84
21	125.80	728.14	162.15	123.15	47. 91	247. 19	222, 43		11.39	147.56	251. 19	65.40
22	142. 32	700.94	155. 24	118.00	47. 91	241. 98	202. 67		11.39	145, 85	240,66	63.08
23	156, 76	673.45	150.51	113.14	47.91	233. 58	185.88		11.41	141.67	227. 76	60.86
24	169, 26	647.28	147. 12	108.58	48.01	223.76	171. 58		11.49	136.13	213, 37	58.79
25	180.03	623.85	144. 12	104.28	48.71	213. 25	159.39		11.69	130.15	198. 55	56.87
26	192.59	607.57	141. 22	100.21	50.58	202, 37	148. 92		12.03	124, 61	184.07	55.09
27	210.81	607.41	138.44	96, 36	53.75	192.88	139.84		12. 63	121.49	170.50	53.45
28	236.72	621.86	135. 73	92.77	57, 98	187.89	131.84		13.76	125. 25	158. 45	51.96
29	268.89	633.91	133. 15	89.53	62.79	192.05	124.66		15. 56	140.03	148.66	50.65
30	301.12	631.99	130.99	86, 88	67.70	210.47	118.17		18. 12	164.73	141.62	49.53
31	330.00		129.62		72, 20		112. 38		21.40		136.75	
												- 1

								<u> </u>			unit : m	3/s
						111	0					
YEAR		196	8			197	3			197		
DAY	MAR.	APR.	MAY	JUN.	MAR.	APR.	MAY	JUN.	MAR.	APR.	MAY	JUN.
	30.00	368.55	250.59	103.14		150.78	594.58	96.00		105.81	555.73	132.50
2	30.01	304.31	199.12	106.70		131. 37	674.44	90.73	1	95. 59	571.30	132.69
3	30.68	250.02	155. 79	137.96		117.56	620.68	85. 95		89. 24	607.63	127. 42
4	34. 50	233. 80	124.84	149.74		112.76	520.70	79.91		86.46	783. 62	120.99
5	38. 59	309.58	103.43	144.06		115.13	497.16	72.92		94.33	827.02	119.54
δ	40.21	363.01	89.51	150.60		136.74	487. 95	66.72	·	107.56	699.19	120.37
7	41.90	418.48	87. 23	151.68		178.04	432.08	61.62		114.89	584.86	117.34
8	42.47	457.36	96. 20	151.21		235. 28	375.05	57.49		130, 85	478.01	115. 17
9	41.98	552.69	100.95	145.74		284.76	338.36	54.14	1.	163. 60	356, 58	108. 22
10	42.68	833.99	105.60	137.56		308.34	295. 72	51.46		214. 28	259.37	99,07
11	50.55	948. 26	106.69	134.64		297. 12	242.81	49.84		266, 35	200.18	89.84
12	82.42	790.69	103.71	130.58		307.77	203.86	48.69	100	279.09	166,07	81, 24
13	115.77	607.78	98, 24	121.36		293.09	173.54	47, 33		264.66	154.92	74.18
14	128.84	493.70	91.47	107.63		239.54	154.76	46.02		258.45	158.66	71.06
15	136,68	598, 68	84.89	93. 53	111	212.55	144. 40	44.92		296.00	180.01	70.12
16	172.61	678.66	80.56	82.34	30.00	215.64	131.34		31.90	330.24	231.48	67. 96
17	210.95	596.64	75. 92	74. 16	30.00	228.63	116.44		31.90	348.40	261.06	65. 59
18	228.55	503, 23	70, 86	69.82	30.10	250.54	102. 38		31, 90	335.33	262.86	67.77
19	239.98	457.02	67, 43	68, 88	32.56	241.46	90.31		31, 90	285. 53	246.26	68. 87
20	256, 91	426.50	66. 92	67.10	41.05	210.41	82. 20		31. 90	241.78	228. 52	64. 55
21	256.83	430.04	74.43	62.89		181.65	82. 38		31.90	207. 82	195.84	59.39
22	247.74	430.54	90.75	58. 34	53.73	157.00	83.87		32.02	189.57	164.08	55. 10
23	239.95	402.17	99. 53	54. 33	65.05	135.69	82.49		35, 48	172, 51	146.12	52. 19
24	225. 27	377.24	93. 27	51.00	79. 23	129.75	79.58		41.43	152, 91	130.73	55.23
25	210.56	559.78	83.14	48.50	108.75	133. 30	77.04		46.09	139. 23	113.15	58. 29
26	223.30	568.73	76.66	46, 51	130.77	142, 41	75.41		93. 99	170. <u>48</u>	98. 10	58. 37
27	240. 94	494.89	74.49	44.72	129, 57	177.13	73. 29	<u> </u>	166, 76	258.74	87, 16	62. 21
28	305.77	417.47	74.06	43.34	138. 35	247. 49	71.03		188, 95	357.61	89.57	70, 89
29	392. 92	333.01	76.83	45. 37	163, 91	304, 26	69.55		176, 96	447.44	99.84	73.99
30	441.63	287. 97	85.14	54.53		390.31	73.81		146.44	550.77	114, 99	70.95
31	424.16		96.53		169.46		88.64		122. 24		127.94	

(1)-a at Hydrological Stations

12/	34 117414		:							استسمي	unit : ∎	3/s
					1HA1A					100		
YEAR		196				197				197		71131
DAY	MAR.	APR.	MAY	JUN.	MAR.	APR.	MAY	JUN.	MAR.	APR.	MAY	JUN.
1	2, 00	39, 36	30, 20	9.44		9, 32	41, 86	5, 97		8, 55	59.04	10.79
2	2.00	32. 39	25. 18	10,02		9.89	45.44	5. 69		10.94	55. 37	10.92
3	2.00	32.05	24.47	<u>12.49</u>		12.77	49.21	5, 38		16.15	48. 17	9, 07
4	2.00	39.39	24. 93	16.01		13.42	52.56	4. 91		24. 54	58. 67	7. 25
. 5	2.01	50.03	21, 86	18.24		14.15	55.03	4. 42		27. 52	68.46	6.58
6	2. 22	50.17	17. 32	15.64		19.99	53.49	3, 98		28.86	57.07	7.96
7	3.09	49.68	13.72	14.93		26. 24	51,60	3, 63		33, 77	41.12	10.48
. 8	3.91	46. 22	10.94	17.36		38. 03	47. 23	3. 37		42.73	35. 70	13.04
9	4, 12	49.07	9.71	18.97		44. 92	41. 59	3, 18		44.02	32, 57	13.14
10	4, 57	62.84	10.48	16.53		43. 20	36.51	3. 38		39.13	27.40	10.48
11	5.77	65. 23	12.04	14. 98		38. 92	29.49	3.57	J	33. 93	22. 38	7, 87
12	6.45	56. 29	12.89	16.89		33.61	23.62	3.41		29.49	22. 36	6.40
13	6.87	40.97	13.89	19.05		29. 28	19.41	3. 20		29. 24	27.90	5. 92
14	14.34	33.80	13.86	18.79		28. 37	16.67	3.03		32.42	35. 67	5. 47
15	37. 19	30.02	12. 10	16. 15		25. 38	15.01	2.89		33, 27	36, 57	4.80
16	52.96	30.11	10.17	12.86	2.01	20.49	12, 59		2.00	34. 12	29, 27	4. 25
17	36.74	33. 34	9, 28	10.12	2.01	17.42	10.05	100	2.00	31. 98	22.04	3.84
18	27. 33	40.30	9. 35	8.63	2.01	17.61	8, 29		2.00	29. 97	18. 15	3. 52
19	41.03	38. 24	9, 24	7.58	2, 01	19. 38	8.69		2.00	27, 17	16. 55	3. 27
20	55. 17	34. 94	8, 48	6, 45	2.01	19.99	13.62	4	2.00	20. 32	15. 13	3. 10
21	53. 97	35, 28	7.93	5.51	2. 03	18. 17	14.15	1.0	2.00	14.75	11. 92	3.04
22	50.14	36.03	8.00	4.87	2.13	15.64	10.94		2.00	11.95	9. 37	3.02
23	45.66	34.11	8, 23	4.40	2. 37	13.07	9. 01		2.00	10.98	7.87	2. 97
24	43, 45	32, 71	8, 53	4.01	2, 68	10.58	8.74		2.01	11.51	7, 11	2.87
25	40.05	34.18	10, 21	3, 67	3.47	8. 76	8.71		2. 05	13.08	6. 54	2.76
26	34.62	37.88	14. 40	3.40	5.01	11. 30	9.04		2. 21	13. 57	6, 39	2, 70
27	29. 55	40.44	15. 25	3, 18	6.89	19.66	9, 50		2. 94	16.29	6. 16	2.76
28	26.00	46. 20	13.17	3, 00	8.92	28. 36	8.97		4. 42	23.71	5. 54	2. 83
29	24.94	46.84	11. 30	2, 87	10.69	37. 73	7.48		6. 73	36. 27	5.04	2. 81
30	31, 02	39. 70	10.75	2.86	11, 55	42.05	6.14		9. 78	47.85	5, 63	2.76
31	46.44	7	10. 21		10.49		5. 94		8.99		8, 36	

(1)-b at Hydrological Stations for Return Period (YEAR 1974 Type)

1)-0	at nyaroto	Ricai ,	364610119	TOT HOLE	1111 1014	ou (ILIII		P 0 7			unit : m	3/s
		,				1 1 1 8						
	Re	tun Per	riod 1/5			Retun Pe	riod 1/1	0			riod $1/2$	0
)AY		APR.	MAY	JUN.	MAR.	APR.	MAY	JUN.	MAR.	APR.	MAY	JUN.
*****		91.14	316, 65	137.31		117.03	407.09	155.10		146, 11	500.81	172.00
2	1	06. 22	371.53	135.14		136, 50	484, 96	153, 87		169, 49	604.26	172. 23
- ĵ		15.04	423.80	134.52		146.63		154.49		180. 22	690.57	174. 44
4		20.58	471.03	134.91		152.25	610.95	156.08		185.34	760.49	177.4
5		26.54	520, 12	134.59		158.76	674, 33	156.41		192.04	840.10	178.4
- 6		33.10	578, 69	134.64		166.35	753. 59	157.01		200.49	939.61	
7	1	39.46	622, 59	135.20		173.97	807.31	158. 23		209, 35	998.84	181. 54
8		46.23	635, 54	135, 13		182.43	812.89	158. 52		219.65	991.22	182.19
9		54. 59	620, 47	134.92		193.47	779, 61	158. 52		233.67	935.16	182. 3
10		63.94	583, 90	134, 21		206, 05	719.64	157.65		249.82	848.96	181. 2
11		74.08	532. 27	132.34		219, 96	643.16	155.02		267.96	746. 28	177.6
12		84.59	474.48	129.16		234.97	562.72	150.53		288. 12	643.11	171.6
13		96.81	419.19	124.97		252.54	489.45	144, 71		311.56	552.59	163. 9
14		10.68	371.08	120, 18		271. 61	428.35	138, 17		335, 75	479.58	155.5
15		24.82	332. 42	115.11		289, 65	380.99	131.36		357.00		146, 8
16		39.08	302, 56	110.03	37, 83	307.03	345.72	124. 67	37. 83	376. 79	386.20	138.4
17		53. 76	280.68	105.16	37. 83	325, 14	321.67	118.38	37. 83	398.07	361.53	130.7
18		69.14	266.74	100, 62	37. 83	344, 42	308.63	112.61	37. 83	421.24	350.51	123.8
19		83.00	259.26	96.50	37.83	361.27	303.83	107.48	37.83	440.84	349.21	11 <u>7. 7</u>
20		92.05	255.77	92.90	37.83	370.38	303. 18	103.10	37. 83	449.14	351.78	112, 6
21		93. 52	252. 47	89.77	37. 83	368. 12	301.31	99. 35	37. 83	441.87	351.22	108.3
22		87.01	247.02	86.94	37, 83	355.05	295, 19	95. 97	37.83	421.09	343.89	104.4
23		75. 31	238.39	84. 23	37, 83	335. 95	283, 85	92, 69	37, 83	393.90	329.12	100.6
24		81. 55	227, 04	81.56	37, 88	315.36	268.51	89.40	37. 92	366. 25	309.12	96.7
25		47. 43	214, 18	78.98	38.11	295. 39	251. 26	86. 22	38, 27	340.49	287.01	92.9
26		34. 86	200. 73	76.65	38. 73	278, 37	233.48	83. 39	39. 21	319.25	264.61	89.6
27		28. 31	187.15	74.68	40.50	270.44	215. 78	81.05	41.85	310.54	242. 64	87.0
28		30. 70	173.87	73.11	45. 86	275. 98	198, 69	79.30	49.77	320.27	221.71	85.1
29		46.54	161. 39	72.09	56. 58	301.35	182.93	78. 29	65. 43	355. 90	202.74	84. 2
30		74. 80	150.54	71.81	73.48	344.76	169.63	78.30	89.30	415.34	187.17	84.6
31			142. 27		94. 49	· · · · · · · · · · · · · · · · · · ·	160.05		117. 53		176.59	l

			:								unit : m	3/s
						1H8						
		Retun Pe	riod 1/50)		Retun Pe	riod 1/1	00			riod 1/2	
DAY	MAR.	APR.	MAY	JUN.	MAR.	APR.	MAY	JUN,	MAR.	APR.	MAY	JUN.
1		188, 23	639.34	193.53		223. 92	754. 75	210.00		262, 16	876.82	226.58
2		215.93	776.04	196.13		254, 32	917.42	214.97		294.72		234. 32
3		226.44	882. 21	200, 89		263. 92	1037. <u>07</u>	222.03			1197.90	243. <u>95</u>
4		230.13	965.60	205. 98		265, 99	1129. 24	228, 87			1297.96	252.62
5		236.67	1066. 21	207. 95			1247.50	231. 52			1435. 20	255.89
6		246.09		209, 81		282. 25		233.85			1605.71	258.60
7		256.63		212.55			1456, 96	237. 20		332.73		262. 53
8			1223.06	213.61		308.53		238. 55		349.55		264.10
9		200.00	1132. 55	213.88			1282.43	238.83	<i>2</i>	373.39		264.31
10			1009.48	212, 18			1129. 15	236, 54			1245.76	261.30
11		333.67	871.62	207.07		383, 96	983.44	230.01			1051.82	253.16
12		361.44	739.12	198.76		419.51	808.47	219.68	+1	482.68	874.57	240.62
13		393.03	627. 30	188. 45		458. <u>65</u>	680. 91	207. 13		528.71	731.85	225, 66
14		422.49	540.65	177. 31		493.50	584. 42	193. 77		567.50	626, 34	209.95
15		444.37	478.68	166, 14		518. 24	517.28	180.55	· · · · · · · · · · · · · · · · · · ·	592.89	554.94	194, 63
16	37. 83	465.53	436, 60	155. 57	37, 83	541.36	473.53	168. 25	37.83	616.99	510.29	180.59
17	37, 83	491.87	412.23	146,03	37. 83	570.49	450.68	157. 32	37.83	649.71	489.74	168.28
18	37.83	521,64	405, 29	137.58	37. 83	603.95	448. 29	147.76	37.83	687.88	492.77	157.64
19	37.83	545, 48	409.79	130.33	37. 83	629.74	458.31	139.66	37.83	715.85	508, 92	148.75
20	37.83	552.01	417.14	124.42	37. 83	633. 23	469.71	133. 19	37.83	715.70	524. 45	141.78
21	37, 83	536.76	418, 04	119.53	37. 83	610, 16	471.46	127. 89	37. 83	683.86	526, 64	136.11
22	37.83	504, 67	408. 32	115.03	37. 83	568. 20	459.18	122.94	37.83	631. 24	511.09	130.72
23	37.84	466.28	388. 01	110.47	37.84	520. 65	433.74	117. 83	37.8 5	574, 17	479,77	125.04
24	37. 97	429.34	361.02	105.76	38.03	476, 47	400.69	112. 48	38. 10	522.69	440.08	119,03
25	38. 54	396. 22	332.01	101.21	38.80	437.79	365. 94	107.33	39.11	478. 52	399.28	113.28
26	40.01	369.84	303.29	97. 35	40, 75	407, 68	332, 13	103.05	41.63	444.86	360.23	108.61
27	44.06	360.95	275. 61	94.38	46.13	399. 31	299, 94	99, 87	48. 54	437.52	323, 47	105. 25
28	56.09	377.82	249.65	92.38	62.03	423.60	270.07	97. 83	68.94	470.07	289.69	103.23
29	79.58	431.46	226.60	91.68	92.70	494, 16	243. 95	97. 39	107.82	558. 71	260.57	103.10
30	113. 92	519 <u>.06</u>	208, 36	92. 72	136.15	605, 72	223.84	99.04	161.22	696.45	238.74	105.46
31	152. 12		196. 91		182.35	<u> </u>	212.04	<u> </u>	215.55	<u> </u>	226.88	<u> </u>

(1)-b at Hydrological Stations for Return Period (YEAR 1974 Type)

1 74. 54 330. 90 89. 79 85. 01 410. 31 103. 95 95. 84 4 2 68. 41 344. 67 90. 19 77. 41 424. 64 104. 35 86. 73 5 3 64. 49 365. 01 87. 92 72. 63 450. 25 101. 08 81. 07 5 4 62. 56 447. 92 84. 85 70. 40 565. 51. 12 88. 9 78. 55. 66 5 65. 67 484. 66 83. 85 75. 12 605. 68 95. 72 85. 23 7 6 71. 72 434. 87 83. 89 83. 67 529. 04 96. 02 96. 63 6. 7 75. 63 378. 01 82. 28 88. 84 451. 47 93. 94 103. 10 5 8 83. 42 320. 55 81. 01 99. 48 376. 19 92. 36 116. 97 4 9 99. 19 253. 32 77. 60 121. 15 289. 52 87. 75 145. 35 3 10<				Stations		-	11 11				وبيسم جهيون جسيديات	unit : m	3/s
DAY MAR. APR. MAY JUN. MAR. APR. MAY JUN. MAR. APR. 1 74.54 330.90 89.79 85.01 410.31 103.95 95.84 4 2 68.41 344.67 90.19 77.41 424.64 104.35 86.73 5 3 64.49 365.01 87.92 72.63 450.25 101.08 81.07 5 4 62.56 447.92 84.85 70.40 565.12 96.89 78.55 6 5 65.67 484.66 83.85 75.12 605.68 95.72 85.23 7 6 71.72 434.87 83.89 83.67 529.04 96.02 96.63 6 7 75.63 378.01 82.28 88.84 451.47 93.94 103.10 5 8 83.42 320.55 81.01 99.48 376.19 92.36 115.97 4									<u> </u>				
1 74, 54 330, 90 89, 79 85, 01 410, 31 103, 95 95, 84 4 2 68, 41 344, 67 90, 19 77, 41 424, 64 104, 35 86, 73 5 3 64, 49 365, 01 87, 92 72, 63 450, 25 101, 93 81, 07 5 4 62, 56 447, 92 84, 85 70, 40 565, 12 96, 89 78, 55 6 5 65, 67 484, 66 83, 85 75, 12 605, 68 95, 72 85, 23 7 6 71, 72 434, 87 83, 89 83, 67 529, 04 96, 02 96, 63 6 7 75, 63 378, 01 82, 28 88, 84 451, 47 93, 94 103, 10 5 8 83, 42 320, 55 81, 01 99, 48 378, 19 92, 36 116, 37 4 9 99, 19 253, 32 77, 60 121, 15 289, 52 87, 75 145, 35 3	_												
2 68. 41 344. 67 90. 19 77. 41 424. 64 104. 35 85. 73 5 3 64. 49 365. 01 87. 92 72. 63 450. 25 101. 09 81. 07 5 4 62. 56 447. 92 84. 85 70. 40 565. 12 96. 89 78. 55 6 5 65. 67 484. 66 83. 85 75. 12 605. 68 95. 72 85. 23 7 6 71. 72 434. 87 83. 89 83. 67 529.04 96. 02 96. 63 6 7 75. 63 378. 01 82. 28 88. 84 451. 47 93. 94 103. 10 5 8 83. 42 230. 55 81. 01 99. 48 376. 19 92. 36 116. 97 4 9 99. 19 253. 32 77. 60 121. 15 289. 52 87. 75 145. 35 3 10 124. 06 195. 28 72. 99 155. 05 217. 29 81. 57 189. 42 2	Αl	R.	APR.			MAR.				MAR.		MAY	JUN.
3 64.49 365.01 87.92 72.63 450.25 101.09 81.07 5 4 62.56 447.92 84.85 70.40 565.12 96.89 78.55 6 5 65.67 484.66 83.85 75.12 605.68 95.72 85.23 7 6 71.72 434.87 83.89 83.67 529.04 96.02 96.63 6 7 75.63 378.01 82.28 88.84 451.47 93.94 103.10 5 8 83.42 320.55 81.01 99.48 376.19 92.36 116.97 4 9 99.19 253.32 77.60 121.15 289.52 87.75 145.35 3 10 124.06 195.28 72.99 155.05 217.29 81.57 189.42 2 11 152.65 156.21 68.12 192.24 170.83 75.17 235.44 1 12 165.46 <td></td> <td></td> <td>74.54</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>10 000</td> <td></td> <td>494.03</td> <td>119. 2</td>			74.54							10 000		494.03	119. 2
4 62. 56 447. 92 84. 85 70. 40 565. 12 96. 89 78. 55 6 5 65. 67 484. 66 83. 85 75. 12 605. 68 95. 72 85. 23 7 6 71. 72 434. 87 83. 89 83. 67 529. 04 96. 02 96. 63 6 7 75. 63 378. 01 82. 28 88. 84 4451. 47 93. 94 103. 10 5 8 83. 42 320. 55 81. 01 99. 48 376. 19 92. 36 116. 97 4 9 99. 19 253. 32 77. 60 121. 15 289. 52 87. 75 145. 35 3 10 124. 06 195. 28 72. 99 155. 05 217. 29 81. 57 189. 42 2 11 152. 65 156. 21 68. 12 192. 24 170. 83 75. 17 235. 44 1 12 165. 46 131. 46 63. 38 205. 50 142. 62 69. 06 247. 93 1			68.41	344, 67	90, 19				104.35			508.61	119.53
4 62. 56 447. 92 84. 85 70. 40 565. 62 72. 85 75. 12 605. 68 95. 72 85. 23 77. 65 65. 67 484. 66 83. 85 75. 12 605. 68 95. 72 85. 23 77. 65 71. 72 434. 87 83. 89 83. 67 529. 04 96. 02 96. 63 6. 7 75. 63 378. 01 82. 28 88. 84 451. 47 93. 94 103. 10 5. 8 83. 42 320. 55 81. 01 99. 48 376. 19 92. 36 116. 97 4 9 99. 19 253. 32 77. 60 121. 15 289. 52 87. 75 145. 35 3 10 124. 06 195. 28 72. 99 155. 05 217. 29 81. 57 189. 42 2 11 152. 65 156. 21 68. 12 192. 24 170. 83 75. 17 235. 44 11 12 165. 46 131. 46 63. 38 205. 50 142. 62 69. 06 247. 93 11 13 163. 66 119. 81 59. 28 199. 44 1			64.49	365.01	87.92		72.63	450.25	101.09	L.,_,		540.47	115.04
6 71,72 434,87 83.89 83.67 529.04 96.02 96.63 6.7 7 75,63 378.01 82.28 88.84 451.47 93.94 103.10 5 8 83,42 320.55 81.01 99.48 376.19 92.36 116.97 4 9 99.19 253.32 77.60 121.15 289.52 87.75 145.35 3. 10 124.06 195.28 72.99 155.05 217.29 81.57 189.42 2. 11 152.65 156.21 68.12 192.24 170.83 75.17 235.44 1 12 165.46 131.46 63.38 205.50 142.62 69.06 247.93 1 13 163.66 119.81 59.28 199.44 131.02 63.90 236.42 1 14 162.84 117.27 57.00 196.56 130.62 61.28 231.32 1 15	_		62.56	447. 92	84.85		70.40	565. 12	96.89			692.52	109.49
6 71, 72 434, 87 83. 89 83. 67 529, 04 96. 02 96. 63 6. 7 75, 63 378, 01 82, 28 88. 84 451, 47 93. 94 103. 10 5 8 83, 42 320. 55 81. 01 99. 48 376. 19 92. 36 116, 97 4 9 99. 19 1523, 32 77. 60 121, 15 289. 52 87. 75 145. 35 3 10 124. 06 195. 28 72. 99 155. 05 217. 29 81. 57 189. 42 2 11 152. 65 156. 21 68. 12 192. 24 170. 83 75. 17 235. 44 1 12 165. 46 131, 46 63. 38 205. 50 142. 62 69. 06 247. 93 1 13 163. 66 119. 61 59. 28 199. 44 131. 02 63. 90 236. 42 1 14 162. 84 117. 27 57. 00 196. 56 130. 62 61. 28 231. 32	_		65.67	484.66	83.85		75. 12	605.68	95. 72	1	85. 23	733.85	108.1
8 83, 42 320, 55 81.01 99.48 376, 19 92.36 116, 97 4 9 99.19 253, 32 77.60 121, 15 289, 52 87.75 145, 35 3 10 124, 06 195, 28 72, 99 155, 05 217, 29 81, 57 189, 42 2 11 152, 65 156, 21 68, 12 192, 24 170, 83 75, 17 235, 44 11 12 165, 46 131, 46 63, 38 205, 50 142, 62 69, 06 247, 93 11 13 163, 66 119, 81 59, 28 199, 44 131, 02 63, 90 236, 42 1 14 162, 84 117, 27 57, 00 196, 56 130, 62 61, 28 231, 32 1 15 180, 75 124, 56 55, 87 220, 99 142, 78 80, 18 263, 68 1 16 30, 00 193, 00 147, 51 54, 37 30, 00 224, 81 50, 18	•		71.72	434, 87	83.89		83.67	529.04	96. 02		96.63	625. 28	108.8
9 99.19 253.32 77.60 121.15 289.52 87.75 145.35 3. 10 124.06 195.28 72.99 155.05 217.29 81.57 189.42 2. 11 152.65 156.21 68.12 192.24 170.83 75.17 235.44 14 12 165.46 131.46 63.38 205.50 142.62 69.06 247.93 11 13 163.66 119.81 59.28 199.44 131.02 63.90 236.42 1 14 162.84 117.27 57.00 196.56 130.62 61.28 231.32 1 15 180.75 124.56 55.87 220.99 142.78 60.18 263.68 1 16 30.00 199.00 147.51 54.37 30.00 244.81 175.70 58.45 30.00 293.70 2 17 30.00 210.89 164.05 52.83 30.00 253.05 <td< td=""><td>_</td><td>-</td><td>75.63</td><td>378, 01</td><td>82. 28</td><td></td><td>88.84</td><td>451.47</td><td>93. 94</td><td></td><td>103.10</td><td>525.42</td><td>106.1</td></td<>	_	-	75.63	378, 01	82. 28		88.84	451.47	93. 94		103.10	525.42	106.1
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11 152, 65 156, 21 68, 12 192, 24 170, 83 75, 17 235, 44 1.1 12 165, 46 131, 46 63, 38 205, 50 142, 62 69, 06 247, 93 1.1 13 163, 66 119, 81 59, 28 199, 44 131, 02 63, 90 236, 42 1.1 14 162, 84 117, 27 57, 00 196, 56 130, 62 61, 28 231, 32 1.1 15 180, 75 124, 56 55, 87 220, 99 142, 78 60, 18 263, 68 11 16 30, 00 199, 00 147, 51 54, 37 30, 00 244, 81 175, 70 58, 45 30, 00 293, 70 21 17 30, 00 210, 89 164, 05 52, 83 30, 00 259, 04 197, 17 56, 62 30, 00 310, 10 2 18 30, 00 208, 39 167, 29 53, 28 30, 00 259, 04 197, 17 56, 62 30, 00 310, 10		:-	124.06				155, 05	217. 29	81.57	I	189.42	237. 54	90. 2
12 165, 46 131, 46 63. 38 205, 50 142, 62 69. 06 247, 93 1 13 163, 66 119, 81 59, 28 199, 44 131, 02 63, 90 236, 42 1 14 162, 84 117, 27 57, 00 196, 56 130, 62 61, 28 231, 32 1 15 180, 75 124, 56 55, 87 220, 99 142, 78 60, 18 283, 68 1 16 30, 00 199, 00 147, 51 54, 37 30, 00 244, 81 175, 70 58, 45 30, 00 293, 70 2 17 30, 00 210, 89 164, 05 52, 83 30, 00 259, 04 197, 17 56, 62 30, 00 310, 10 23 18 30, 00 208, 39 167, 29 53, 28 30, 00 253, 05 200, 12 57, 64 30, 00 299, 56 2 19 30, 00 186, 40 160, 24 53, 64 30, 00 221, 38 189, 83 <	_				68, 12		192. 24	170.83			235.44	184. 10	82. 1
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15 180, 75 124, 56 55, 87 220, 99 142, 78 60, 18 263, 68 1 16 30, 00 199, 00 147, 51 54, 37 30, 00 244, 81 175, 70 58, 45 30, 00 293, 70 2 17 30, 00 210, 83 164, 05 52, 83 30, 00 259, 04 197, 17 56, 62 30, 00 310, 10 22 18 30, 00 208, 39 167, 29 53, 28 30, 00 253, 05 200, 12 57, 64 30, 00 299, 56 2 19 30, 00 168, 40 160, 24 53, 64 30, 00 221, 38 189, 83 58, 28 30, 00 299, 56 2 20 30, 00 164, 22 151, 38 51, 69 30, 00 181, 44 177, 90 55, 55 30, 00 218, 46 2 21 30, 00 145, 23 135, 01 49, 07 30, 00 166, 97 155, 90 52, 05 30, 00 188, 39 1											231. 32	144. 47	65. 4
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17 30.00 210.88 164.05 52.83 30.00 259.04 197.17 56.62 30.00 310.10 2 18 30.00 208.39 167.29 53.28 30.00 253.05 200.12 57.64 30.00 29.56 2 19 30.00 186.40 160.24 53.64 30.00 221.38 189.83 58.28 30.00 256.74 2 20 30.00 164.22 151.38 51.69 30.00 191.44 177.90 55.55 30.00 218.46 2 21 30.00 145.23 135.01 49.07 30.00 166.97 155.90 52.05 30.00 188.39 11 22 30.03 133.44 117.95 46.69 30.06 152.70 133.66 48.99 30.09 171.90 12 23 31.10 122.86 106.79 44.87 31.87 139.77 119.99 46.77 32.94 156.63 11	ñ.	. 00	199.00			30.00				30,00	293.70	206.76	62.5
18 30.00 208.39 167.29 53.28 30.00 253.05 200.12 57.64 30.00 299.56 2 19 30.00 186.40 160.24 53.64 30.00 221.38 188.83 58.28 30.00 255.74 2 20 30.00 164.22 151.38 51.69 30.00 191.44 177.90 55.55 30.00 218.46 21 21 30.00 145.23 135.01 49.07 30.00 186.97 155.90 52.05 30.00 10.01 186.97 30.00 186.97 155.90 52.05 30.00 10.01 186.97 155.90 52.05 30.00 10.01 10.02 10.02 10.02 10.02 10.02 10.02 10.02 10.02 10.02 10.02 10.02 10.02 10.02 10.02 10.02 10.02 10.02 10.02 11.02 10.02 10.02 10.02 10.02 10.02 10.02 10.02 10.02	Ō.	. 00	210.89			30.00	259, 04	197, 17	56.62	30.00	310.10	233.04	60.4
19 30,00 186,40 160,24 53,64 30,00 221,38 189,83 58,28 30,00 256,74 2.2 20 30,00 164,22 151,38 51,69 30,00 191,44 177,90 55,55 30,00 218,46 2 21 30,00 145,23 135,01 49,07 30,00 166,97 155,90 52,05 30,00 188,39 1 22 30,03 133,44 117,95 46,69 30,06 152,70 133,66 48,99 30,09 171,90 1 23 31,10 122,86 106,79 44,87 31,87 139,77 119,99 46,77 32,94 156,63 1 24 33,15 111,42 97,26 45,77 35,19 125,44 108,36 48,37 37,91 139,26 1 25 35,14 102,64 86,95 47,05 38,15 114,87 95,49 50,27 41,93 126,95 1						30.00		200.12		30.00	299. 56	235.13	62. 1
20 30.00 164.22 151.38 51.69 30.00 191.44 177.90 55.55 30.00 218.46 24 21 30.00 145.23 135.01 49.07 30.00 166.97 155.90 52.05 30.00 188.39 1 22 30.03 133.44 117.95 46.69 30.06 152.70 133.66 48.99 30.09 171.90 1 23 31.10 122.86 106.79 44.87 31.87 139.77 119.99 46.77 32.94 156.63 1 24 33.15 111.42 97.26 45.77 35.19 125.44 108.36 48.37 37.91 139.26 1 25 35.14 102.64 86.95 47.05 38.15 114.87 95.49 50.27 41.93 126.95 1 26 53.75 114.37 77.78 47.15 66.68 133.19 84.23 50.40 82.52 153.34 1 27 87.84 157.01 70.63 48.87 114.78 191.88 75.71 52.85 145.76 230.00 4			186, 40	160, 24		30.00	221. 38	189.83	58. 28	30.00	256.74	220.95	63. 1
21 30.00 145.23 135.01 49.07 30.00 166.97 155.90 52.05 30.00 188.39 1 22 30.03 133.44 117.95 46.69 30.06 152.70 133.66 48.99 30.09 171.90 1 23 31.10 122.86 106.79 44.87 31.87 139.77 119.99 46.77 32.94 156.63 1 24 33.15 111.42 97.26 45.77 35.19 125.44 108.36 48.37 37.91 139.26 1 25 35.14 102.64 86.95 47.05 38.15 114.87 95.49 50.27 41.93 126.95 1 26 53.75 114.37 77.78 47.15 66.68 133.19 84.23 50.40 82.52 153.34 1 27 87.84 157.01 70.63 48.87 114.78 191.88 75.71 52.85 145.76 230.00 4						30.00	191.44	177.90	55. 55	30.00	218.46	205. 53	59.4
22 30.03 133.44 117.95 46.69 30.06 152.70 133.66 48.99 30.09 171.90 1.23 23 31.10 122.86 106.79 44.87 31.87 139.77 119.99 46.77 32.94 156.63 1.24 24 33.15 111.42 97.26 45.77 35.19 125.44 108.36 48.37 37.91 139.26 125.43 25 35.14 102.64 86.95 47.05 38.15 114.87 95.49 50.27 41.93 126.95 14 26 53.75 114.37 77.78 47.15 66.68 133.19 84.23 50.40 82.52 153.34 13 27 87.84 157.01 70.63 48.87 114.78 191.88 75.71 52.85 145.76 230.00 4	Ō.	. 00		135.01	49.07	30.00	166. 97	155.90	52.05	30.00	188. 39	177.09	54. 9
24 33.15 111.42 97.26 45.77 35.19 125.44 108.36 48.37 37.91 139.26 1 25 35.14 102.64 86.95 47.05 38.15 114.87 95.49 50.27 41.93 126.95 11 26 53.75 114.37 77.78 47.15 66.68 133.19 84.23 50.40 82.52 153.34 27 87.84 157.01 70.63 48.87 114.78 191.88 75.71 52.85 145.76 230.00 48.87	Ō.	. 03	133, 44	117.95	46.69	30.06	152. 70	133.66	48.99	30.09	171.90	149, 20	51.1
24 33. 15 111. 42 97. 26 45. 77 35. 19 125. 44 108. 36 48. 37 37. 91 139. 26 1 25 35. 14 102. 64 86. 95 47. 05 38. 15 114. 87 95. 49 50. 27 41. 93 126. 95 1 26 53. 75 114. 37 77. 78 47. 15 66. 68 133. 19 84. 23 50. 40 82. 52 153. 34 1 27 87. 84 157. 01 70. 63 48. 87 114. 78 191. 88 75. 71 52. 85 145. 76 230. 00 4	ĩ.	. 10	122.86	106, 79	44.87	31, 87	139.77	119.99	46.77	32.94	156, 63	133.09	48. 5
26 53.75 114.37 77.78 47.15 66.68 133.19 84.23 50.40 82.52 153.34 527 87.84 157.01 70.63 48.87 114.78 191.88 75.71 52.85 145.76 230.00 1	3,	. 15	111.42	97. 26	45.77	35.19	125.44	108.36	48. 37	37.91	139. 26	119.33	51.0
27 87.84 157.01 70.63 48.87 114.78 191.88 75.71 52.85 145.76 230.00	5.	. 14	102.64	86. 95	47.05	38. 15	114.87	95.49	50.27	41.93	126.95	103.74	53.6
27 87.84 157.01 70.63 48.87 114.78 191.88 75.71 52.85 145.76 230.00 3	3,	. 75	114. 37	77. 78	47.15	66. 68	133.19	84. 23	50.40	82. 52	153.34	90. 32	53.7
	7,	. 84	157.01	70.63	48.87	114. 78	191.88	75.71	52.85	145.76	230.00	80.46	57. 0
_ ZO [101, 41 Z11, Z1 U3, D3 UZ, O4 130, ZZ Z0Z, 14 13, 33 30, 43 101, U0 311, 10 (211.27	69. 85	52.84	136. 22	262.14	75. 95	58. 43	167.08	317. 18	82. 15	64. 5
						132.75	324. 21	82. 23	60.80	157.89	395.72	90. 91	67. 3
												104.02	64. 8

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		7 : .		1. T		181	0			1		
		Retun Pe	riod 1/5	0		Retun Pe	riod 1/1	00	1	Retun Pe	riod 1/2	00
DAY	MAR.	APR.	HAY	JUN.	MAR.	APR.	MAY	JUN.	MAR.	APR.	MAY	JUN.
1		110.67	610.23	141.26		122.82	706.48	160.10		135.01	804.17	179.78
2		99.48	625.05	141.08		109.88	721.65	159. 33		120.25	820.01	178.19
3		92.58	666.89	134. 54		101.93	772.99	150.81		111, 23	882.14	167.43
4		89.68	875.81	126.89		98.74	1033.12	141. 24			1197.63	155.77
5		99.47	912.59	125, 43		111.47	1061.21	139.75			1212, 44	154. 32
6	1.2	115. 22	754.73	126.66		131, 10	859.01	141.54		147.65	962. 57	156.75
7		123, 41	623, 64	123. 14		140.63	702.06	137. 18		158.44	779, 52	151.46
8		142.08	503.60	120.70		163.58	560.63	134, 30		186.01	616.54	148.09
g		180.60	367, 87	112.49		211. 13	401.19	124.08		243. 28	432, 92	135. 68
10		239.64	262.08	101, 84		283. 22	280.08	111, 06		329.08	296.73	120.13
11		297.38	200.04	91. 31		<u>350, 09</u>	211.72	98. 45		404.68	222. 53	105.35
12		307.03	165, 58	81.67		356.08	175.13	87.09		405, 94	184, 24	92. 26
13		286, 71	156.65	73.91		327.64	168.49	78. 14		368, 62	180.48	82.12
.14		278.69	163.81	70,86		317. 45	180.13	75. 10		356.55	197.10	79. 24
15		323.80	190.76	70.27		374.59	215.22	74. 93		427. 20	241.02	79.61
16	30.00	382.85	252, 16	68.01	30,00	421. 39	291.68	72.42	30.00	482.00	333. 45	76.81
17	30.00	381.72	284. 38	65.47	30.00	441.76	328.18	69, 53	30.00	503.38	373.74	73.56
18	30.00	363.48	284. 51	68.49	30.00	416.01	326, 11	73.76	30.00	469.03	368. 95	79.18
19	30.00	303.84	264. 20	69.80	30.00	341.46	300.13	75. 31	<u> 30.00</u>	378. 58	336.72	80.89
20	30.00	253.86	243. 52	64. 52	30.00	281.76	274, 77	68.53	30.00	309.03	306.35	72. 42
21	30.00	216.35	205. 40	58. 53	30.00	238. 38	228.02	61.26	30.00	259.97	250.32	63.83
22	30.16	197.35	169, 40	53.77	30.23	217.73	185. 15	55. 70	30.33	237. 97	200, 37	57, 47
23	34, 88	178.96	150, 26	50.66	36. 90	196.78	163, 82	52. 23	39. 36	214.41	177.12	53.69
24	42.60	157.27	133.65	54.71	47. 25	171.42	144.89	57.81	52.62	185. 25	155, 86	61.03
25	48.04	142.80	114.20	58.40	53. 73	155.38	122.19	62.41	59.99	167. 78	129.78	66.55
26	107.67	182.09	97.85	58.36	130.87	206.71	103.47	62, 13	156.33	232.48	108.72	65.95
27	191.95	285.09	86. 31	62.98	232. 30	332.53	90.67	67.97	274.76	382.26	94.76	73.14
28	210.41	395.92	90.60	73, 38	246.68	463.14	97.59	81.06	283.89	533.14	104.77	89.17
29	192.50	499.62	103.08	76.61	221. 21	589.71	113, 35	84, 49	250.55	684. 78	123.96	92. 64
30	156.31	614, 87	121.01	72.54	176.71	723.84	135.62	78.89	197.48	836, 70	151.00	85. 27
31	128. 92		136.30		144. 21	<u> </u>	154.57		159.71		173.86	

(1)-b at Hydrological Stations for Return Period (YEAR 1974 Type)

						·	2 2 1 1 2				<u>unit e</u>	<u>3/s</u>
						1114						
		Retun Pe					riod 1/1				riod 1/2	
DAY	MAR.	APR.	MAY	JUN.	MAR.	APR.	MAY	JUN.	MAR.	APR.	MAY	JUN.
1		6.80	39. 13	7.17		8. 20	49, 57	8, 80		8.76	51. 33	9.48
2		7.60	42. 23	8.00		9. 29	52, 60	9, 75		9, 99	56, 15	10.48
3		10.18	42, 49	7.64		12.86	50.94	9.09		13.99	55.89	9, 68
4		14. 34	45.48	6.65		18.43	52.14	7.69		20.15	59. 55	8.09
5		18. 24	49.47	5.89		23. 25	57. 13	6.71		25. 32	65, 34	7.03
6		20, 72	46.08	6.07		25, 98	54.85	7.05		28. 12	60, 82	7.46
7		23.84	36. 10	7. 25		29.82	43, 30	8, 72		32, 27	46.83	9, 34
8		28.53	29.10	8.81		35, 94	34.99	10.80		39.00	37.50	11.64
9		31.49	25.88	9.72		39.54	31. 24	11.87		42.86	33, 43	12.76
10		30.42	22. 77	9. 11		37, 74	27, 33	10.86		40.72	29.17	11.56
11		27. 42	19.37	7. 55		33. 62	23.03	8. 70		36. 13	24.50	9, 15
12		24. 30	17.67	6. 21		29.54	21.11	6.98		31.65	22, 50	7, 27
13	:	22, 53	19.09	5.44		27, 44	23. 32	6.07		29.43	25.09	6.31
14	7.1	23. 14	23.01	4.96		28.47	28. 35	5. 51		30.65	31, 13	5.72
15		24.48	25. 94	4. 45		30. 22	31. 16	4. 90		32, 57	34. 92	5.07
16	2.00	25. 17	24.16	3, 99	2.00	31.04	28. 12	4, 33	2.00	33. 44	31.40	4.47
17	2.00	24.79	19.86	3.63	2.00	30.46	22. 87	3.89	2.00	32. 78	24. 91	4.00
18	2.00	23.30	16, 20	3.35	2.00	28.47	18.75	3, 56	2.00	30.57	20.05	3.64
19	2.00	21.50	14.07	3.14	2.00	26.12	16.42	3. 30	2.00	27.99	17.44	3.36
20	2.00	18, 27	12, 66	2. 97	2.00	21.83	14. 83	3. 11	2.00	23. 24	15.72	3.16
21	2.00	14. 14	10.89	2.88	2.00	16.47	12.62	3.00	2.00	17. 39	13. 32	3, 05
22	2, 00	11. 22	8.91	2, 83	2.00	12.89	10.14	2, 96	2.00	13.54	10.63	3.01
23	2.00	9, 68	7.43	2.79	2.00	11, 13	8. 34	2. 92	2.00	11, 71	8. 70	2.98
24	2.00	9.19	6, 50	2.73	2.00	10.73	7. 27	2. 85	2. 01	11.36	7. 57	2, 90
25	2.02	9. 61	5. 92	2.66	2.03	11.45	6. 62	2.76	2.03	12, 21	6.89	2.80
26	2.08	10. 20	5. 56	2, 60	2. 13	12. 27	6. 23	2.69	2.16	13. 13	6. 50	2.73
27	2. 35	11. 42	5. 31	2.59	2. 54	13.92	5. 96	2.69	2.63	14. 87	6. 22	2.73
28	3.02	16.14	4. 92	2.61	3. 52	20.43	5. 48	2.73	3.74	20.76	5. 71	2.78
29	4. 25	24. 45	4.53	2, 62	5. 24	31.50	5. 02	2. 75	5. 67	30.03	5. 21	2.80
30	5.93	32.47	4. 57	2.60	7. 47	41.59	5. 15	2, 72	8.12	40, 42	5.39	2.77
31	8.85		5, 59		8, 48		6, 64		9, 15		7.09	· ·

	1HA1A											
	Re	tun Per	riod 1/50	0		Retun Pe	riod 1/1	30		Retun Pe	riod 1/2	00
DAY	MAR.	APR.	MAY	JUN.	HAR.	APR.	YAK	JUN.	MAR.	APR.	MAY	JUN.
1		9.47	56.75	10.37		10.02	62.41	11, 07		10, 57	66.69	11.79
2		10.87	61.53	11.40		11.57	66. 16	12. 12	-	12. 27	70.32	12.85
3		15.44	61.06	10.41		16, 59	65.56	10.98		17. 76	69, 58	11.54
4		22.34	65, 48	8.59	1 1	24. 08	71. 13	8.98		25. 84	75.80	9. 35
5		27. 93	72.01	7.42		29.98	78. 12	7, 72		32, 03	83, 36	8. 02
6		30.80	66.55	7. 96		32.89	71. 31	8.36		34. 98	75.76	8.76
7		35. 34	50.76	10.12		37.76	53.86	10.74	-	40.17	56.87	11.37
8	T 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	42.87	40.52	12.69		45. 91	42, 87	13.53		48. 98	45.19	14.37
9		47.04	36, 14	13.87		50.32	38. 25	14.74		53. 62	40, 35	15.61
10		44.46	31. 44	12. 42		47.38	33. 20	13.09		50.30	34. 95	13.75
11		39. 26	26, 32	9.70		41.69	27, 72	10, 12		44. 11	29. 11	10.53
12		34. 29	24. 23	7.64		36. 34	25. 58	7. 91		38. 37	26.93	8. 18
13		31. 92	27. 30	6.61		33. 77	29.04	6.84		35, 70	30.79	7.07
14		33. 39	34. 20	5. 99		34, 10	36, 66	6. 20		36, 17	39.09	6.41
15		35, 52	38. 39	5. 29		33.61	41. 25	5.46		35.76	43.97	5.62
16		36, 46	34. 23	4.63	2, 00	33, 98	36. 54	4, 76	2.00	36. 24	38. 72	4.89
17		35, 68	26.84	4. 12	2.00	35, 46	28. 37	4. 22	2.00	37.74	29.83	4.31
18		33, 20	21.47	3.74	2.00	34.59	22.56	3.81	2.00	36.66	23.63	3.88
19		30.32	18.66	3. 44	2.00	32.02	19.60	3, 50	2,00	33, 83	20.53	3.56
20		25.00	16.81	3. 23	2, 00	26. 34	17.66	3. 27	2.00	27.68	18.50	3, 32
21		18. 51	14. 17	3. 11	2.00	19.37	14. 84	3.16	2.00	20. 22	15.49	3, 20
22		14, 34	11. 22	3, 08	2.00	14, 96	11.67	3.13	2.00	15. 57	12.12	3. 17
23		12.43	9.14	3.04	2, 00	12.98	9.48	3, 09	2.00	13. 53	9. 81	3.14
24		12. 15	7. 95	2.96	2. 01	12.77	8. 24	3.00	2.01	13, 39	8, 52	3.05
25		13. 18	7. 24	2.85	2.05	13, 93	7, 51	2, 89	2.05	14. 70	7.77	2.93
26		14. 20	6.83	2, 77	2, 21	15.05	7.09	2. 81	2. 24	15.90	7.36	2.84
27		16. 17	6.55	2.78	2.84	17. 24	6. 80	2, 82	2. 93	18. 27	7.06	2.86
28		22. 93	6.00	2.85	4. 27	25. 61	6. 22	2. 90	4. 52	27. 45	6.44	2.95
29		33. 52	5.45	2.87	6, 68	39.09	5. 64	2. 92	7.15	42, 16	5.83	2. 97
30		45.04	5.69	2.83	9.62	51.65	5.93	2, 88	10.30	55. 51	6. 17	2, 93
31	9.99		7.67		10, 65		8, 13		11. 32		8, 60	

(1)-c at Hydrological Stations in Case of 5 Year Probable Flood (YEAR 1974 Type)

(1) 0	at 115 a 10										unit : m	3/s
						Case	1					
		111	8			1H					A1A	
DAY	MAR.	APR.	MAY	JUN.	MAR.	APR.	MAY	JUN.	MAR.	APR.	MAY	JUN.
1		91.14	316.65	137. 31		83, 32	370.72	96. 31		6, 80	39.13	7, 17
2		106. 22	371.53	135. 14		75. 42	386. 32	97.43		7.60	42, 23	8.00
3		115.04	423.80	134. 52		70.34	414.14	95.69		10.18	42.49	7.64
: 4		120.58	471.03	134. 91		68, 04	481.83	92. 62		14. 34	45.48	6.65
5		126.54	520.12	134. 59		70, 28	530.12	90.83		18. 24	49.47	5.89
6		133. 10	578.69	134.64		76, 15	498. 98	90.41		20.72	46.08	6.07
7		139.46	622.59	135. 20		82.04	436.50	89.16	-:	23.84	36.10	7. 25
8		146.23	635.54	135, 13		90.50	368, 47	87. 47		28.53	29.10	8. 81
9		154.59	620, 47	134. 92		107.22	293, 81	84.09		31.49	25.88	9, 72
10		163.94	583, 90	134. 21		134.18	225. 98	79.07		30, 42	22.77	9.11
11		174.08	532. 27	132.34		164.49	177, 01	73.48		27.42	19.37	7.55
12		184.59	474.48	129.16		182.18	146.07	67.99		24.30	17, 67	6.21
13		196.81	419.19	124.97		184. 25	130.11	63.25		22.53	19.09	5.44
14		210.68	371.08	120. 18		184.49	126.38	60.16		23.14	23.01	4.96
15		224. 82	332.42	115, 11		198, 18	134, 20	58.55	10.71	24. 48	25. 94	4.45
16	37.83	239.08	302.56	110.03	30.00	218.14	155.78	57.00	2.00	25. 17	24. 16	3, 99
17	37.83	253. 76	280.68	105.16	30.00	232. 12	175. 88	55.63	2.00	24.79	19.86	3.63
18	37. 83	269.14	266.74	100.62	30.00	231.91	182. 51	55, 51	2.00	23.30	16. 20	3.35
19	37. 83	283.00	259.26	98. 50	30.00	212.00	178.13	55. 82	2.00	21.50	14.07	3.14
20	37.83	292.05	255.77	92, 90	30.00	186.37	168.14	54. 29	2.00	18. 27	12.66	2.97
21	37.83	293. 52	252.47	89.77	30.00	163.63	151. 24	51.52	2.00	14.14	10.89	2.88
22	37.83	287.01	247.02	86.94	30. 21	147.84	132. 29	48.71	2.00	11. 22	8. 91	2, 83
23.	37. 83	275. 31	238.39	84. 23	31. 34	135.08	117.55	46.84	2.00	9.68	7.43	2. 79
24	37.86	261.55	227.04	81.56	33.40	122. 54	106.07	46.98	2.00	9. 19	6.50	2.73
25	37.99	247. 43	214.18	78.98	37.84	114.08	94. 73	48. 29	2.02	9, 61	5. 92	2.66
26	38, 36	234.86	200.73	76.65	56.69	123.77	84. 17	49, 00	2.08	10.20	5. 56	2.60
27	39. 42	228. 31	187. 15	74.68	91. 52	164. 91	76, 29	50.80	2. 35	11. 42	5.31	2. 59
28	42, 73	230.70	173.87	73. 11	115. 20	222.07	73. 97	54. 51	3.02	16.14	4. 92	2, 61
29	49, 41	246.54	161.39	72, 09	120.55	281.40	77.87	57. 20	4. 25	24. 45	4. 53	2. 62
30	60.36	274.80	150.54	71.81	109.14	341, 44	84.95	57. 29	5.93	32.47	4. 57	2.60
31	74.72	1	142.27		94. 82		92. 20	· .	6. 85		5. 59	

					·					1	unit : 🖪	3/s
						Case						
		111				111					A1A	:
DAY	MAR.	APR.	MAY	JUN.	MAR.	APR.	MAY	JUN.	MAR.	APR.	MAY	JUN.
1		72. 21	272, 28	147. 35	L	83. 32	100.00	96. 31		6.80	39.13	7.17
2		87.29	305.86	141.05		75.42	100.00	97.43		7.60	42. 23	8.00
3		99. 24	349.30	137. 26	<u> </u>	70.34	100.00	95.69		10.18	42. 49	7.64
- 4		108.40	397. 99	135.80	<u> </u>	68.04	100.00	92.62		14.34	45.48	6.65
5		117.01	447.10	135.03	<u> </u>	70. 28	100.00	90.83		18, 24	49.47	5.89
6		125.16	498.70	135.05		76. 15	100.00	90.41		20.72	46.08	6.07
7		132.68	548. 31	135, 51		82.04	100.00	89.16		23.84	36, 10	7, 25
8	ļ.,	139. 20	588. 18	135.35		90.50	100.00	87.47		28. 53	29.10	8. 81
9	1 1 1	146.00	610, 07	134, 93		100,00	100.00	84.09		31.49	25.88	9.72
10		153.67	609.13	134. 42		100.00	100.00	79.07		30.42	22.77	9. 11
11		162, 63	586, 23	133.60	<u> </u>	100.00	100, 00	73.48		27.42	19.37	7. 55
12		171. 15	546.54	132, 05		100,00	100.00	67, 99		24.30	17. 67	6. 21
13	. :-	179.81	497. 23	129.50		100.00	100.00	63. 25		22.53	19.09	5, 44
14	<u> 1400.</u>	190.05	445.12	125.97		100.00	100.00	60.16		23.14	23.01	4.96
15	11	202.41	396.14	121.69		100.00	100.00	58. 55		24.48	25.94	4, 45
16	37.83	216.63	354.09	116.95	30.00	100.00	100, 00	57, 00	2.00	25. 17	24.16	3. 99
17	37. 83	231. 37	320.36	112.04	30.00	100.00	100,00	55.63	2.00	24, 79	19.86	3, 63
18	37. 83	246. 28	294.84	107.19	30.00	100.00	100.00	55. 51	2.00	23. 30	16.20	3. 35
19	37.83	260. 6G	276, 71	102.58	30,00	100.00	100.00	55.82	2.00	21.50	14.07	3.14
20	37.83	273.50	265.08	98. 33	30.00	100.00	100.00	54. 29	2.00	18. 27	12.66	2. 97
21	37. 83	283. 42	257. 82	94.51	30.00	100.00	100.00	51. 52	2.00	14.14	10.89	2. 88
22	37, 83	287. 87	252. 52	91.12	30.21	100.00	100.00	48, 71	2.00	11. 22	8. 91	2.83
23	37.83	285. 79	246.94	88.08	31, 34	100.00	100.00	46.84	2.00	9,68	7.43	2.79
24	37.84	278. 22	239, 56	85. 27	33.40	100.00	100,00	46.98	2, 00	9. 19	6. 50	2.73
25	37.89	267.05	229.93	82. 59	37.84	100.00	94. 73	48. 29	2.02	9. 61	5. 92	2.66
26	38.05	255. 12	218.45	80.04	56.69	100.00	84, 17	49,00	2.08	10.20	5, 56	2.60
27	38. 53	246, 32	205, 81	77. 67	91.52	100,00	76. 29	<u>50, 80</u>	2. 35	11.42	5. 31	2. 59
28	39.90	242.50	192.68	75. 60	100.00	100.00	73. 97	54.51	3, 02	16.14	4. 92	2.61
29	42, 71	245. 29	179.64	73. 91	100.00	100,00	77. 87	57. 20	4, 25	24. 45	4. 53	2.62
30	48. 21	253.80	167. 24	72, 79	100,00	100.00	84, 95	57, 29	5, 93	32.47	4. 57	2.60
31	57.74	<u> </u>	156, 21		94.82	L	92, 20		6, 85		5. 59	

(1)-c at Hydrological Stations in Case of 5 Year Probable Flood (YEAR 1974 Type)

											<u>init: m</u>	1/S
	Case 3											
		11				<u> 1 H</u>					AIA	
DAY	MAR,	APR.	MAY	JUN.	MAR.	APR.	MAY	JUN.	MAR.	APR.	MAY	JUN.
1		72. 29	246. 29	149, 98		83. 32	150.00	96. 31		6, 80	39.13	7.17
2		88. 96	258.00	144.49		75, 42	150.00	97.43		7.60	42. 23	8.00
3		101.83	268.97	141, 39		70.34	150.00	95.69		10, 18	42.49	7.64
. 4		111.01	278. 31	140.52		68.04	150.00	92.62		14. 34	45. 48	6.65
5	: .	118.97	284. 78	140.26		70.28	150.00	90.83		18, 24	49.47	5.89
6		126, 15	291.51	140.70		76.15	150.00	90.41	1.	20.72	46.08	6.07
7		132, 60	295.34	141.46		82.04	150.00	89.16		23, 84	36. 10	7. 25
8		139. 20	294.39	141.53		90.50	150.00	87.47		28. 53	29. 10	8. 81
9		146,00	289.48	141. 25		107. 22	150.00	84.09		31.49	25. 88	9. 72
10		153, 67	282, 28	140.82		134.18	150.00	79.07		30.42	22. 77	9, 11
11		162.63	274.34	140.01		150.00	150.00	73.48		27.42	19. 37	7. 55
12		171.15	266.74	138. 42		150.00	146.07	67.99		24.30	17.67	6. 21
13		179.81	260.07	135, 76		150.00	130.11	63. 25		22. 53	19.09	5. 44
14		190.05	254. 17	132, 05		150.00	126.38	60.16		23.14	23.01	4, 96
15		200.49	249.16	127.54		150.00	134. 20	58. 55		24. 48	25. 94	4. 45
16	37.83	208. 29	245.09	122.55	30.00	150.00	150.00	57,00	2, 00	25. 17	24.16	3, 99
17	37.83	215. 37	241.74	117.39	30.00	150.00	150.00	55.63	2.00	24. 79	19.86	3.63
18	37. 83	221. 33	238.71	112. 29	30.00	150.00	150.00	55. 51	2.00	23. 30	16. 20	3. 35
19	37.83	225. 34	235. 52	107.45	30.00	150.00	150.00	55. 82	2.00	21.50	14.07	3, 14
20:	37.83	227. 53	232. 36	103.01	30.00	150.00	150.00	54. 29	2.00	18. 27	12.66	2, 97
21	37. 83	228. 41	229.09	99.02	30.00	150.00	150.00	51.52	2.00	14. 14	10.89	2. 88
22	37. 83	227, 88	225. 72	95.49	30. 21	147.84	132, 29	48.71	2.00	11, 22	8. 91	2.83
23	37, 83	226.16	222.15	92.33	31. 34	135.08	117. 55	46.84	2.00	9.68	7.43	2. 79
24	37.84	223. 93	218.00	89.40	33.40	122.54	106.07	46.98	2.00	9.19	6.50	2. 73
25	37.89	221.39	212.75	86. 61	37.84	114.08	94.73	48. 29	2. 02	9.61	5. 92	2.66
26	38. 05	219.38	206.03	83.95	56.69	123.77	84.17	49.00	2. 08	10.20	5.56	2.60
27	38. 53	220.04	197.75	81.48	91.52	150.00	76. 29	50.80	2. 35	11.42	5. 31	2, 59
28	39.90	223. 96	188.20	79. 32	115.20	150.00	73.97	54. 51	3. 02	16.14	4. 92	2. 61
29	42.71	231. 22	177.86	77. 58	120.55	150.00	77. 87	57. 20	4. 25	24. 45	4.53	2. 62
30	48. 21	238. 33	167, 43	76.44	109.14	150.00	84. 95	57. 29	5. 93	32.47	4. 57	2. 60
31	57.74		157.81		94. 82		92. 20		6. 85		5. 59	

											unit:m3	I/s
		- 11	0			Case		 		411		
NIV	MAR.	APR.	MAY	JUN.	MAR.	APR.	MAY	JUN.	NAD.		A1A	71101
DAY	nan.	72. 29	268.35	153. 79	MAK.		200.00	96. 31	MAR.	APR. 6, 80	MAY 39,13	JUN.
2		88.96	285.89	147. 31		83. 32 75. 42	200.00	97.43		7. 60	42.23	7, 17 8, 00
3		101.83	303.42	147. 31		70.34	200.00	95. 69		10.18	42. 49	7. 64
4		111.01	318.83	142.08		68. 04	200.00	92.62		14. 34	45.48	
<u> </u>		118. 97	330.27	141.42	l	70. 28	200.00	90.83		18. 24	49.47	6.65 5.89
6		126. 15	340.82	141. 55		76. 15	200.00	90.41		20, 72	46.08	6.07
$-\frac{3}{7}$		132, 60	347.39	142. 10	 	82. 04	200.00	89 16		23, 84	36.10	7. 25
- 8		139. 20	348. 22	141. 99	 	90.50	200.00	87. 47		28, 53	29.10	8. 81
9		146.00	344. 38	141. 59	 	107, 22	200.00	84. 09		31, 49	25.88	9.72
10	·	153.67	337. 82	141.07	-	134. 18	200.00	79.07		30.42	22.77	9. 11
11		162.63	330, 26	140. 19	 	164. 49	177.01	73.48		27, 42	19.37	7. 55
12		171. 15	322. 66	138. 55		182. 18	146.07	67. 99		24. 30	17.67	6, 21
13	·	179.81	314.88	135.85		184. 25	130.11	63. 25		22. 53	19.09	5. 44
14		190.05	305.69	132.12		184. 49	126.38	60.16		23.14	23.01	4. 96
15		202.41	294. 82	127. 59		198.18	134. 20	58. 55		24. 48	25.94	4. 45
16	37, 83	216.63	283, 23	122. 59	30.00	200.00	155.78	57.00	2.00	25. 17	24. 16	3. 99
17	37. 83	231. 37	272. 37	117, 41	30.00	200.00	175.88	55.63	2.00	24.79	19.86	3, 63
18	37, 83	246.28	263, 52	112.31	30.00	200.00	182, 51	55. 51	2.00	23, 30	16.20	3. 35
19	37. 83	260.60	257.49	107.47	30.00	200.00	178.13	55, 82	2.00	21. 50	14.07	3. 14
20	37. 83	272. 20	254, 73	103.02	30.00	186.37	168.14	54. 29	2.00	18. 27	12.66	2. 97
21	37. 83	276. 76	254.03	99. 03	30,00	163.63	151, 24	51.52	2. 00	14.14	10.89	2. 88
22	37.83	278, 38	253.50	95.50	30, 21	147.84	132.29	48. 71	2.00	11. 22	8. 91	2. 83
23	37. 83	276. 65	251. 24	92. 34	31, 34	135.08	117. 55	46, 84	2.00	9. 68	7, 43	2. 79
24	37. 84	271.59	246.00	89, 41	33, 40	122.54	106, 07	46. 98	2.00	9, 19	6. 50	2, 73
25	37.89	263.65	237.57	86, 62	37. 84	114.08	94, 73	48.29	2. 02	9, 61	5. 92	2.66
26	38.05	254.72	226.61	83. 95	56.69	123.77	84. 17	49.00	2.08	10. 20	5.56	2.60
27	38. 53	248. 31	214.03	81.48	91.52	164, 91	76. 29	50.80	2. 35	11, 42	5. 31	2.59
28	39, 90	246. 27	200.67	79.32	115, 20	200.00	73, 97	54. 51	3. 02	16.14	4. 92	2. 61
29	42.71	249.96	187.23	77.58	120.55	200.00	77.87	57.20	4, 25	24. 45	4, 53	2. 62
30	48. 21	256.96	174.40	76.44	109, 14	200.00	84. 95	57. 29	5. 93	32. 47	4.57	2, 60
31	57.74		162.95		94.82		92. 20		6, 85		5. 59	

(2) at Proposed Dam Site for Return Period (YEAR 1974 Type)

											unit : m	3/s
						Rude						
		Retun Pe					riod 1/5			<u>Retun Pe</u>		
DAY	MAR.	APR.	MAY	JUN.	MAR.	APR.	MAY	JUN.	MAR.	APR.	MAY	JUN.
1		3, 44	19.96	12.45		4, 01	25. 22	15, 33		4. 47	29.67	17.71
2		3. 21	26.48	10.01		3.70	33.69	11.96		4.07	39.81	13.52
3	1	3. 15	64, 59	7, 87		3.61	84.53	9. 13		3, 96	101, 69	10.10
4		4.11	94.05	7.08		4. 92	121.13	8.16		5. 60	143.93	8, 99
- 5		5.58	60.65	7. 15	<u> </u>	6.92	73.17	8. 31		8.06	82.86	9. 24
6		5. 52	33. 29	8. 24		6.78	38.06	7.16		7. 80	41.51	7, 88
7		5.87	20, 67	5. 27		7.19	22. 87	5. 92		8, 30	24. 39	6.43
8		7.74	14. 26	4. 55	,	9. 71	15.45	5, 04		11.39	16.25	5.40
9		9. 62	10.55	4, 01		12, 17	11. 27	4. 38		14. 34	11.75	4. 65
10		10, 37	8. 42	3, 59		13.03	8.94	3. 87		15. 27	9. 29	4.08
11		9, 24	7, 47	3, 26		11, 34	8, 01	3, 48		13, 06	8.40	3. 65
12		8.09	6. 81	2.99		9.72	7.36	3. 17		11.02	7.79	3. 30
13		8. 25	5.88	2.77		9, 93	6.33	2. 92		11. 29	6.68	3.03
14		13. 28	7.99	2.59		16.79	9. 31	2.72	1 1 1 1	19.80	10.44	2.80
15		19.92	13.81	2.44		25.60	17. 14	2. 55		30.47	20.04	2.62
16	1. 26	19.77	18, 89	2, 32	1, 26	24.84	23.87	2.40	1.26	29, 05	28. 17	2.47
17	1.26	20.13	21. 53	2. 21	1.26	25.07	27. 13	2. 28	1.26	29. 15	31.90	2.34
18	1.26	15.54	16, 82	2. 12	1, 26	18, 70	20.45	2. 18	1. 26	21. 20	23. 39	2. 23
19	1. 26	11.47	12. 15	2.04	1, 26	13.35	14. 23	2.09	1.26	14. 78	15.84	2.13
20	1.26	9.01	9. 25	1.97	1, 26	10.25	10.54	2.02	1. 26	11.17	_ 11.50	2.05
21	1.26	7.40	7, 36	1.91	1.26	8, 29	8. 21	1, 95	1, 26	8. 94	8.84	1.98
22	1.26	6.41	6.08	1.86	1.26	7. 12	6.68	1.89	1. 26	7.65	7.11	1.92
23	1. 27	5.47	5. 18	1, 81	1. 27	6.00	5.62	1.84	1.27	6. 39	5.94	1.86
24	1.27	4. 75	4. 50	1.77	1. 28	5. 16	4. 83	1.80	1. 28	5. 46	5.06	1.82
25	1. 27	4.50	3, 97	1.73	1. 28	4. 91	4. 22	1.76	1. 28	5. 22	4.39	1.78
26	2. 62	6.61	3, 58	1. 70	3. 25	7.81	3.75	1.72	3.85	8.84	3.89	1.74
27	5. 22	12. 15	3, 23	1. 68	6. 97	15. 32	3. 39	1.70	8. 60	18.08	3. 49	1.72
28	5. 53	15. 20	4. 14	1, 70	7. 24	19.26	4. 65	1,73	8.77	22.76	5.08	1.76
29	4.76	13.00	9. 12	1.74	6.00	16.00	11.43	1.79	7.06	18.48	13, 47	1.83
30	4. 20	14. 72	14.04	1.77	5. 14	18. 28	18.01	1.83	5. 91	21, 26	21.48	1.88
31	3, 77		13.48		4.49		16.89		5.07		19.77	

				<u> </u>							unit : m	3/s :
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		Retun Pe				Retun Pe				Retun Pe	riod 1/1	00
DAY	MAR.	APR.	MAY	JUN.	MAR.	APR.	MAY	JUN.	MAR.	APR.	MAY	JUN.
1		8. 67	50, 78	9, 38	L	9. 37	56.14	10. 26		9. 91	61.74	10.95
2		9.88	55, 55	10.36		10.75	60.87	11. 27		_ 11. 44	65.44	11.99
3		13.84	55. 29	9. 57		15. 27	60.40	10.30		16, 41	64.85	10.86
4		19.93	58.90	8.01	1.5	22.10	64.77	8.50		23.82	70.36	8, 88
5		25.05	63.06	6, 95	L	27.63	71.21	7.34		29.65	76.95	7.64
6		27. 82	60.16	7. 38		30.47	_65.83	7.88		32.54	70.54	8. 27
7		31, 92	46.33	9. 23		34.96	50. 21	10.01		37. 35	53. 27	10.63
8		38, 58	37. 10	11.51		42.41	40.08	12.55		45. 42	42.41	13. 38
9		42, 40	33.07	12. 62		46.53	35. 75	13.72		49.78	37.84	14.58
10		40.28	28.85	11.43		43, 98	31.10	12. 29		46.87	32.85	12. 95
11		35. 74	24, 24	9, 05		38.83	26.03	9. 59		41. 24	27.42	10.01
12		31. 31	22. 26	7. 20		33, 92	23, 97	7. 55		35. 94	25. 31	7. 83
13		29.12	24.82	6. 24		31.58	27.01	6. 54		33. 41	28.73	6.77
14		30. 32	30.79	5.66	100	33.03	33. 83	5. 93		33. 73	36.26	6.13
15	1.00	32. 22	34.54	5. 02		35.14	37. 98	5. 23	1.0	33. 25	40.80	5.40
16	1.98	33.08	31.06	4.42	1, 98	36.06	33.86	4. 58	1. 98	33. 61	36. 15	4. 71
17	1.98	32. 42	24.64	3, 95	1, 98	35. 29	26, 55	4.08	1.98	35.08	28, 06	4. 17
18	1.98	30. 24	19, 84	3.60	1.98	32.84	21. 23	3.70	1.98	34. 22	22. 32	3.77
19	1. 98	27.69	17. 26	3, 33	1. 98	29.99	18.46	3.40	1. 98	31, 67	19.39	3.46
20	1.98	22. 99	15. 55	3. 13	1.98	24.73	16.63	3. 19	1.98	26.05	17, 47	3, 24
21	1.98	17. 20	13.17	3. 02	1.98	18.31	14. 02	3. 08	1. 98	19, 16	14.68	3. 12
22	1.98	13.39	10.51	2. 98	1.98	14.19	11. 10	3.04	1.98	14.80	11, 55	3, 09
23	1.98	11. 59	8. 60	2.94	1.98	12.30	9.04	3.01	1.98	12. 84	9. 37	3.06
24	1. 98	11. 24	7.49	2, 87	1.98	12.02	7.86	2, 93	1.99	12.63	8. 15	2.97
25	2. 01	12.08	6. 82	2.77	2.02	13.03	7.16	2. 82	2.03	13.78	7, 43	2.86
26	2, 13	12, 99	6, 43	2. 70	2.16	14.05	6.76	2,74	2.19	14.89	7.02	2. 78
27	2.60	14. 71	ճ. 15	2. 70	2. 71	15. 99	6.48	2.75	2.80	17.06	δ. 73	2. 79
28	3.70	20.53	5, 65	2. 75	3, 99	22.68	5.93	2. 82	4.23	25, 33	6. 15	2.86
29	5. 61	29.70	5. 15	2.77	6, 17	33.16	5, 39	2.84	6. 61	38, 67	5. 58	2.89
30	8. 03	39, 99	5. 33	2, 74	8, 86	44. 55	5.63	2. 80	9, 52	51.09	5. 87	2. 85
31	9.05		7.01		9, 88		7, 58		10.54		8, 04	- A, 50

(2) at Proposed Dam Site for Return Period (YEAR 1974 Type)

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	h	Retun Period 1/20				Retun Period 1/50				Retun Period 1/100		
DAY	MAR.	APR.	MAY	JUN,	MAR.	APR,	MAY	JUN.	MAR.	APR.	MAY	JUN.
ī		1, 39	18.05	5, 36		1.81	22.58	8, 50		2. 16	26. 17	7.40
2		1. 87	19.57	4.94		2.45	24.50	5.96		2, 93	28, 41	6, 76
3		1. 99	20.50	5.79		2.60	<u>25.63</u>	7.07		3.11	29.69	8.09
4		2.41	18. 93	6.65		3.14	23.48	8. 20		3.75	27.05	9.44
5		3. 30	16.82	6. 32		4. 32	20, 67	7.75		5. 17	23.66	8. 90
6		4, 42	15.63	5, 86		5.79	19.09	7.14		6.93	21,77	8, 16
7		6.03	14.08	5. 57		7.90	17.07	6, 77		9.46	19.37	7. 72
8		6, 31	12. 37	5.13		8. 22	14.87	6. 20		9. 79	16, 77	7.03
9		6.84	10.88	4. 67		8.86	12.97	5.61		10.52	14, 54	6. 33
10		7.45	9.68	4. 27		9.62	11.46	5.09		11.39	12.78	5. 73
11		7. 22	8.66	3.91		9.26	10.18	4, 64		10.90	11.30	5. 19
12		6.72	7. 75	3. 60		8.54	9.05	4. 24		9, 99	10.01	4. 73
13	!	6. 12	8. 47	3. 31		7.71	10.03	3.89		8. 97	11.21	4. 32
14		5. 54	8.07	3.06		6. 93	9.55	3. 57		8.01	10. 67	3, 96
15		7. 51	7. 25	2.84		9.51	8. 52	3.29		11.10	9.47	3.63
16	0.12	7.84	6. 94	2.63	0.12	9.90	8.16	3.04	0.12	11.54	9.07	3. 35
17	0.12	7. 37	6.43	2.45	0, 12	9.25	7.53	2.82	0.12	10.73	8.36	3.09
18	0.12	7.03	5. 91	2. 29	0.12	8.76	6.89	2. 62	0.12	10.13	7.63	2.87
19	0.12	6.57	6.01	2.14	0.12	8.14	7.05	2.44	0.12	9. 37	7.84	2.66
20	0.12	6.08	5.76	2.00_	0.12	7, 49	6.76	2. 28	0.12	8. 58	7. 52	2.48
21	0.12	5. 67	5. 27	1.88	0.12	6.94	6.15	2.13	0.12	7. 92	6.82	2. 31
22	0.12	5. 30	4.80	1.76	0.12	6.45	5. 57	1, 99	0.12	7.34	6. 15	2. 16
23	0.12	5. 32	4. 38	1.66	0, 12	6.48	5.06	1.87	0. 12	7. 38	5. 57	2.02
24	0.12	5. 14	4.01	1.56	0.12	6.24	4.61	1. 75	0.12	7.09	5, 05	1.89
25	0.12	5.40	3.68	1.47	0.12	6.59	4. 21	1.65	0.12	7, 51	4.61	1. 78
26	0.12	5. 23	3.40	1.39	0.13	6.37	3. 87	1. 55	0.13	7. 25	4.22	1. 67
27	0.45	17.39	3. 14	1. 32	0.57	22.44	3.56	1.47	0.67	26.60	3, 88	1.57
28	0.69	22.65	2.96	1.25	0.89	29, 29	3. 35	1, 39	1.06	34, 59	3.64	1.48
29	0.79	21.84	4. 24	1.19	1.02	27.89	5, 02	1.31	1. 22	32. 79	5.63	1.40
30	1.04	19, 90	5.13	1.13	1.35	25. 14	6, 19	1. 25	1.62	29. 32	7.03	1.33
31	1.09		5, 60		1.42		6, 81		1.69		7.78	

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	uiit. #3/S										<u>v/ </u>	
L	Mgeta										70	
		Retun Pe			Retun Period 1/50				Retun Period 1/100			
DAY	MAR.	APR.	MAY	JUN.	MAR.	APR.	MAY	JUN.	MAR.	APR.	MAY	JUN.
1		11.89	96, 89	15, 63		14.43	112. 16	18.57	0.00	16, 54	123.79	21. 18
2	·	13, 57	70.56	20.01		16.64	81.35	24. 52	0.00	19. 21	89.86	28.49 27.75
3		13. 29	78. 29	19.96		15.99	94. 17	24. 16	0.00	18. 20	107.44	
4		14.68	68, 56	16.86		17, 78	81.84	19.71	0.00	20.34	92.75	22. 05 17. 79
5		16.08	98, 36	14. 33		19.55	120.16	16, 26	0.00	22.42	140.38	18, 69
6		20.90	157. 37	14.69		26.09	200.47	16.89	0.00	30.47	237.07	
7		26.68	160.19	25. 29		33.71	198.60	31.53	0.00	39.66	230.00	36.98
8		33,00	84. 88	25.00		41.80	97.54	30.55	0.00	49. 22	106.90	35. 22
9		37.59	47.87	20.94		47. 26	52. <u>60</u>	24.73	0.00	55. 32	55.93	27. 79
10		39.64	31.85	17. 15	<u></u>	49. 25	34. 16	19.60	0.00	57.17	35.75	21. 49 17. 17
11		71.00	23.30	14. 35		91.66	24.57	15.96	0.00	109.33	25. 43	
12		81, 49	20.99	12.43		102.86	22.63	13.55	0.00	120.53	23. 91	14. 36
13	<u> </u>	59. 28	32.38	11.04		70.99	38. 35	11.85	0.00	80.09	43.50 42.11	12. 44
14		46. 52	31, 51	10.01		54.55	37. 26	10.62	0.00	60.80		11.05
15	1 00	55. 72	26.52	9. 22	4 00	67.72	30.75	9, 69	0.00	77.69	34, 21 33, 71	10.02 9,23
16	4. 80	60, 64	25. 84	8, 60	4.80	74.24	30.15	8. 97	4, 80	85. 55		
17	4.80	60.20	30, 93	8, 11	4.80	73. 37	37. 25	8.40	4.80	84. 25	42.62	8.61
18	4.80	48. 20	37.08	7. 71	4. 80	57.14	45. 56	7, 95	4.80	64. 29	52.78	8, 11
19	4.80	44. 50	54. 35	7. 38	4, 80	52.80	68.84	7. 58	4.80	59. 52	81. 31	7.71
20	4.80	32. 98	43. 73	7. 10	4.80	37. 83	52.88	7. 27	4. 80	41.60	60.25	7.38
21	4.80	25. 71	30.03	6. 87 6. 67	4.80	28. 85 26. 11	34. 51	7. 01 6. 79	4.80 4.80	31. 26 28. 40	37, 90	7.10
22 23	4.80	23. 20 19. 70	22.24 17.63	6.50	4.80	21. 90	24.69 19.13		4. 80	23.63	26.47 20.19	6. 87 6. 67
	4. 80		14.68	6. 35	4. 84	22. 15	15. 67	6.60		24. 22		
24	4.83	19.61 17.34		6. 22	5, 35			6.44	4.86	21.03	16.35	6. 50 6. 35
25	5. 15 6. 13		12.69 11.25	6.11	6.88	19.39 17.15	13.39 11.75	6.30 6.18	5.55 7.62		13.86 12.09	6. 35
26 27		15.48 17.56	10.17	6.01	7, 50	20.31	10.54	6.07	8.41	18. 48 22. 55		
	6, 56 7, 16			5. 92	8.34	85.86		5.98				6.11
28		65.35 257.37	9.34 8.70	5, 9Z 5, 85	14.04	345. 20	9, 63 8, 93	5. 98 5. 90	9.45 16.89	103.87	9.83	6.01
29	11,00			6, 11	16.22	183. 94	8, 81	6. 27		421.53	9.08	5. 93
30	12.70 11.79	155. 29	8. 52	0, 11	14.51	103.94	11.83	0. Z1	19.38 16.83	204.69	9.02	6.41
31	11.79	<u> </u>	10.73	·	14.51		11, 61	<u> </u>	10.83		12.76	<u> </u>

(2) at Proposed Dam Site for Return Period (YEAR 1974 Type)

											<u>unit : m</u>	3/s	
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		Retun Pe	riod 1/2	0		Retun Pe	riod 1/5		Retun Period 1/100				
DAY	MAR.	APR.	MAY	JUN.	MAR.	APR.	MAY	JUN.	MAR.	APR.	MAY	JUN.	
1	***************************************	102, 41	514.85	121.03		119.44	643.02	144.37		133.29	749. 12	164, 30	
2		91, 39	528. 80	122, 38		105, 68	654.36	145.62		117. 23	757. 79	165.23	
3		84, 53	569.05	119.14		97. 23	707.32	140.66		107, 45	822.53	158. 57	
4		81, 77	676.46	114.05		94. 12	853.49	133.47		104, 11	1003.14	149, 44	
.5		86. 22	739, 10	111, 44		100.87	928. 33	130.11			1084.24	145, 48	
6		96.19	673.86	111.22		114.87	824.61	130.16		130, 64	946.49	145.82	
Ť		105, 46	571.18	109, 46		127. 21	685.02	127.89		145. 58	775.63	143.07	
8		118, 75	468.49	106.98		145.01	551.90	124.63		167. 29	617.44	139.10	
9		145, 56	359.78	101.67		181.55	413.47	117.38		212.45	454.61	130.10	
10		188. 20	265.30	93, 82		238. 91	296. 37	106.78	1	282.50	319.33	117.08	
11		232, 81	201. 30	85. 33		295.65	220.44	95.60		348. 88	234. 37	103.59	
12		253, 23	163.77	77. 27		316.62	178.26	85. 23		369.19	189.08	91.31	
13		249.14	147.42	70.61		305. 59	162.64	76.93		351, 51	174.76	81.71	
14		245, 69	148.00	66, 68		298, 86	168.03	72.46		342.14	184, 79	76. 91	
15		266. 91	165, 15	65, 05	15	328. 25	194.48	71.01		379.37	219.59	75.77	
16	29.44	297. 41	202.34	63. 27	29.44	369.01	246.56	69. 10	29.44	429, 20	284.69	73.76	
17	29, 44	316.01	232, 99	61.69	29.44	391.16	286.12	67.37	29.44	453.80	331.33	71.93	
18	29.44	311.01	240.41	62. 17	29.44	380.58	293. 22	68.51	29.44	437.65	337. 53	73.72	
19	29.44	275.76	231.67	63.05	29.44	330.26	279.80	69.93	29.44	373, 87	319.71	75. 58	
20	29.44	235. 12	215. 43	60.51	29, 44	276.00	257.40	66.26	29.44	308.15	291.77	70. 31	
21	29.44	201.73	188.89	56.13	29.44	233. 59	221.51	60.31	29.44	258. 54	247, 59	63.47	
22	29. 92	180.41	160.44	52.00	30.24	208.08	184.30	54.99	30, 57	229.97	202. 91	57.19	
23	32. 37	163.41	139.85	49.55	34. 27	187, 62	158, 76	52. 15	36. 20	206. 79	173. 49	54.09	
24	36.63	146.23	124.48	50.46	40.97	166.37	140. 21	53.96	45. 27	182. 17	152. 48	56.82	
25	44.68	135.66	108.89	52, 97	52.43	154.27	120.85	57.69	59.60	169.01	129. 98	61.65	
26	79, 27	154. 81	94. 51	54.11	102.74	183. 22	103.16	59.13	124.00	207.04	109. 60	63.26	
27	137.55	222.00	84.47	57. 12	182.45	275. 27	91.46	63.32	221.79	320.88	96. 70	68.49	
28	165. 51	307. 19	83. 23	63. 29	211.00	385.44	91.69	71.93	249, 13	451.91	98. 52	79. 32	
29	164.72	395.68	91.07	67. 30	203.64	501.58	103. 52	77.04	235.86	592. 29	113. 98	85. 29	
30	142.11	484. 81	102.84	66.76	171, 04	616.94	119.78	75.65	194, 82	729, 40	134. 18	82. 99	
31	119.27	T	114.66		140.91		136,06		158, 65		154.45		