

3. Structural Calculation of Building

3.1 General

The major design criteria applied in this calculations are standard requirements conforming to "Architectural Institute of Japan Standard for Structural Calculation of Reinforced Concrete Structures and Commentary" and "Architectural Institute of Japan Standard for Structural Calculation of Steel Structures".

3.2 Design Criteria

3.2.1 Loading Conditions

In this structural calculations, the load and external forces that act on the structure are the following.

- (A) Dead load
- (B) Live load
- (C) Seismic load

The design stress are determined from temporary stresses and permanent stresses for main structural parts of building by the above mentioned loads and external forces, according to table and the combination of the forces that make the structural member most disadvantageous are used in the design.

Table 1. Combination of Load

Conditions of Stresses		Combination of Stresses
Permanent stresses	Normal time	$G + P$
Temporary stresses	Earthquake	$G + P + K$

where;

- G; Stress due to dead load
- P; Stress due to live load
- K; Stress due to seismic load

The dead and live loads of each part of building are applied in accordance with the Japanese Building Standard Law Enforcement Order.

3.2.2 Seismic Force

The seismic coefficient shall be set down and applied to the building structure as follows;

Seismic coefficient	$K = 0.05$
Horizontal force to the building	$H = 0.05 \times W$ (Dead load of building plus adjusted live load)

3.3 Design of Members

The design of reinforced concrete structure shall be based on "AIJ Standard for Structural Calculation of Reinforced Concrete Structure".

Compressive strength of concrete at 28 days shall be 210 kg/cm^2 and more.

Reinforcement bar materials shall comply with deformed bar, "SD30". (JIS G 3112)

Weight of reinforced concrete shall be calculated as 2.4 t/m^3 and the "Young Ratio" of reinforcement bar to concrete shall be " $n=15$ ".

The design of steel beam depends on the "AIJ Standard for Structural Calculation of Steel Structure".

The materials of steel shall comply with "SS41". (JIS G 3101)

3.4 Allowable Stress

3.4.1 Allowable Design Stress of Materials

Allowable design stresses of the structural materials will be as summarized below:

1) Concrete and Reinforcing Bar

Allowable Design Stress of Concrete and Reinforcing (kg/cm²)

Type of stress	For permanent load			For temporary load		
Materials	Tension	Compression	Shear	Tension	Compression	Shear
Concrete ($F_c=210 \text{ kg/cm}^2$)	-	$F_c/3 = 70$	4.25	-	$2F_c/3=105$	12.75
Rein. - bar (JIS G 3112)	1,800	1,800	1,000	2,700	2,700	1,500

Allowable Bond Stress per Unit Surfaces of Reinforcing Bar (kg/cm²)

Type of stress	For permanent load		For temporary load	
Materials	Top bar	Other bars	Top bar	Other bars
Deformed bar	$F_c/15$ 14.0	$F_c/10$ 21.0	$1.5F_c/15$ 21.0	$1.5F_c/10$ 31.5

2) Structural Steel

(kg/cm²)

Type of stress	For permanent load			For temporary load		
Materials	Tension	Compression	Shear	Tension	Compression	Shear
Structural steel (SS 41)	1,400	1,400	900	2,100	2,100	1,350

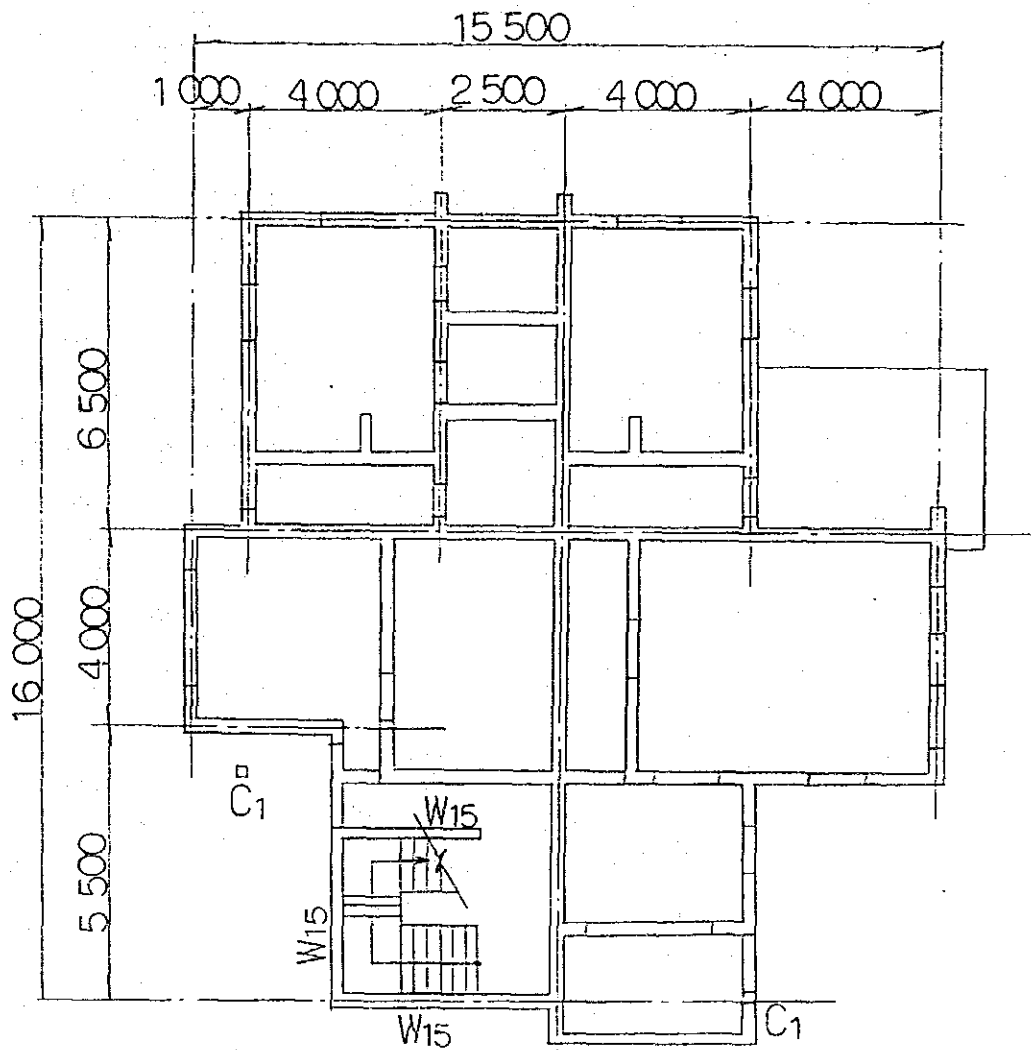
3.4.2 Allowable Bearing Capacity of Soil

The bearing capacity of soil is 30 t/m^2 for permanent load.

3.5 Structural Calculation

3.5.1 Utility Building A

Framing Plan



GROUND FLOOR PLAN

1). Assumed Load

A: To floor
B: To frame
C: To seismic
D.L: Dead load
T.L: Total load

1.1 Floor Load Table

Title	Material	Thick (cm)	Weight (kg/m ²)		D.L (kg/m ²)	L.L (kg/m ²)	T.L (kg/m ²)	Note
Roof	Concrete	60	140	A	570	90	660	
	Water Proofing		20					
	Cement Mortar	15	30	B		70	640	
	Concrete Slab	150	360					
	Ceiling		20	C		30	600	
1st Floor	Terrazzo		80	A	460	180	640	
	Concrete Slab	150	360	B		130	590	
	Ceiling		20	C		60	520	

1.2 Dead Load of Girder and Wall

	Title	Size(cm)	Weight(kg/cm ²)
	Girder	15 x 60	162 + 42 → 210
		15 x 40	90 + 26 → 120
		15 x 85	252 + 62 → 320
		15 x 45	108 + 30 → 140
	Column	15 x 15	54 + 24 → 80
	Wall	CB 15	200 + 80 → 280

2). Calculation of Axial Force of Columns

No.	Floor	Title	Calculation					W (t)	ΣW (t)
			Load(t/m ² & t.m)	Area (m ²)	Length (m)	Length (m)	W' (t)		
W1	1F	Roof	0.64	16.16			10.4		
		G	0.21		11.5		2.4		
		W	0.28		1.2	11.5	3.9	16.7	
	F	W	0.28		1.2	11.5	3.9	3.9	20.6
W2	1F	Roof	0.64	10.65			6.9		
		G	0.21		6.5		1.4		
		W	0.28		1.2	6.5	2.2	10.5	
	F	W	0.28		1.2	6.5	2.2	2.2	12.7
W3	1F	Roof	0.64	8.16			5.3		
		G	0.21		5.25		1.1		
		W	0.28		1.2	4.0	1.4	7.8	
	F	W	0.28		1.2	4.0	1.4	1.4	9.2
W4	1F	Roof	0.64	8.25			5.3		
		G	0.21		5.0		1.1		
		W	0.28		1.2	3.2	1.1	7.5	
	F	W	0.28		1.2	3.2	1.1	1.1	8.6
W5	1F	Roof	0.64	3.0			2.0		
		G	0.21		2.5		0.6		
		W	0.28		1.2	2.5	0.9	3.5	
	F	W	0.28		1.2	2.5	0.9	0.9	4.4
W6	2F	Roof	0.64	9.58			6.2		
		G	0.21		7.5		1.6		
		W	0.28		1.2	7.5	2.6		
		Parapet	0.67		6.6		4.4	14.8	
	1F	W	0.28		1.2	7.5	2.6	2.6	17.4
W7	2F	Parapet	0.67	4.6			3.1		
		Roof	0.64		6.58		4.2		
		G	0.21		4.0		0.9		
		W	0.28		1.2	4.0	1.4	9.6	
	1F	W	0.28		1.2	4.0	1.4	1.4	11.0

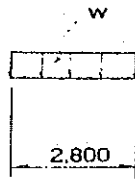
No.	Floor	Title	Calculation					W (t)	ΣW (t)
			Load(t/m ² & t-m)	Area (m ²)	Length (m)	Length (m)	W' (t)		
W8	2F	Parapet	0.67	6.2			4.2		
		Roof	0.64	6.0			3.9		
		G	0.21		5.0		1.1		
		W	0.28		0.85	5.0	1.2	10.4	
	1F	W	0.28		0.85	5.0	1.2		
		G	0.32		5.0		1.6	2.8	13.2
W9	2F	Roof	0.64	8.56			5.8		
		G	0.21		5.0		1.1		
		W	0.28		1.2	3.2	1.1	8.0	
	1F	W	0.28		1.2	3.2	1.1	1.1	9.1
W10	2F	Roof	0.64	8.56			5.8		
		G	0.21		5.0		1.1		
		W	0.28		1.2	4.0	1.4	8.3	
	1F	1st Floor	0.59	7.88			4.7		
		G	0.21		5.0		1.1		
		W	0.28		1.2	4.0	1.4		
			0.28		1.2	5.0	1.7	8.9	17.2
	F	W	0.28		1.2	5.0	1.7	1.7	18.9
W11	2F	Parapet	0.67	4.5			3.0		
		Roof	0.64	7.77			5.0		
		G	0.21		4.5		1.0		
		W	0.28		1.2	4.5	1.5	10.5	
	1F	1st Floor	0.59	5.07			3.0		
		G	0.21	5.5			1.2		
		W	0.28		1.2	4.5	1.5		
			0.28		1.2	5.5	1.8	7.5	18.0
	F	W	0.28		1.2	5.5	1.8	1.8	19.8

No.	Floor	Title	Calculation					W (t)	ΣW (t)
			Load(t/m ² & t·m)	Area (m ²)	Length (m)	Length (m)	W' (t)		
W12	2F	Parapet	0.67	6.5			4.4		
		Roof	0.64	12.1			7.8		
		G	0.21		6.5		1.4		
			0.14		2.25		0.3		
		W	0.28		1.2	4.5	1.5	15.4	
	1F	1st Floor	0.59	3.38			2.0		
		G	0.21		6.5		1.4		
		W	0.28		2.4	4.5	3.1	6.5	21.9
	F	W	0.28		1.2	4.5	1.5	1.5	23.4
W13	2F	Parapet	0.67	3.95			2.7		
		Roof	0.64	2.28			1.5		
		G	0.21		2.75		0.6		
		W	0.28		1.2	2.75	0.9	5.7	
	1F	G	0.21		2.75		0.6		
		C	0.08		1.2		0.1		
		W	0.28		1.2	2.75	0.9	1.6	7.3
	F	C	0.08		1.2		0.1	0.1	7.4
W14	2F	Parapet	0.67	3.75			2.5		
		Roof	0.64	6.96			4.5		
		G	0.21		3.75		0.8		
		W	0.28		1.2	3.75	1.3	9.1	
	1F	1st Floor	0.59	1.33			0.8		
		G	0.21		3.75		0.8		
		W	0.28		1.2	3.75	1.3		
			0.28		1.2	3.0	1.0	3.9	13.0
	F	W	0.28		1.2	3.0	1.0	1.0	14.0
W15	1F	Parapet	0.34	4.0			1.4		
		Roof	0.64	1.75			1.2		
		G	0.21		4.0		0.9		
		W	0.28		1.2	4.0	1.4	4.9	
	F								
		W	0.28		1.2	4.0	1.4	1.4	6.3

No.	Floor	Title	Calculation					W (t)	ΣW (t)
			Load(t/m ² & t·m)	Area (m ²)	Length (m)	Length (m)	W' (t)		
W16	1F	1st Floor	0.59	6.38			3.8		
		G	0.21		5.5		1.2		
		W	0.28		1.2	5.0	1.7	6.7	
	F	W	0.28		1.2	5.0	1.7	1.7	8.4
W17	1F	1st Floor	0.59	7.88			4.7		
		G	0.21		5.0		1.1		
		W	0.28		1.2	5.0	1.7	7.5	
	F	C	0.28		1.2	5.0	1.7	1.7	9.2
W18	1F	Roof	0.64	9.54			6.1		
		G	0.21		5.6		1.2		
		W	0.28		1.2	5.6	1.9	9.2	
	F	W	0.28		1.2	5.6	1.9	1.9	11.1
W19	1F	Roof	0.64	6.28			4.0		
		1st Floor	0.59	9.69			5.7		
		G	0.21		8.25		7.8		
		B	0.21		2.5		0.6		
		W	0.28		1.2	7.5	2.6	14.7	
	F	W	0.28		1.2	7.5	2.6	2.6	17.3
W20	1F	Roof	0.64	4.92			3.2		
		1st Floor	0.59	10.91			6.6		
		G	0.21		7.25		1.6		
		B	0.21		2.5		0.6		
		W	0.28		1.2	6.5	2.2	14.1	
	F	W	0.28		1.2	6.5	2.2	2.2	16.3
W21	1F	Parapet	0.34		1.0		0.4		
		Roof	0.64	1.13			0.8		
		1st Floor	0.59		5.13		3.0		
		G	0.21		4.0		0.9		
		B	0.21		2.5		0.6		
		W	0.28		1.2	3.0	1.0	6.7	
	F	W	0.28		1.2	3.0	1.0	1.0	7.7

No.	Floor	Title	Calculation					W (t)	ΣW (t)
			Load(t/m ² & t·m)	Area (m ²)	Length (m)	Length (m)	W' (t)		
W22	2F	Parapet	0.67	9.03	2.0		1.4	9.7	
		Roof	0.64				5.8		
		G	0.21		5.25		1.1		
		W	0.28		1.2	4.0	1.4		
	1F	1st Floor	0.59		8.72		5.2	9.7	19.4
		G	0.21		5.95		1.3		
		B	0.21		2.5		0.6		
		W	0.28		1.2	4.0	1.4		
			0.28		1.2	3.5	1.2		
	F	W	0.28		1.2	3.5	1.2	1.2	20.6
W23	2F	Roof	0.64	10.85			6.9	9.7	
		G	0.21		5.25		1.1		
		B	0.12		2.25		0.3		
		W	0.28		1.2	4.0	1.4		
	1F	1st Floor	0.59		5.75		3.4	16.8	26.5
		Roof	0.64		11.8		7.6		
		G	0.21		7.25		1.6		
		B	0.21		2.5		0.6		
		W	0.28		1.2	4.0	1.4		
			0.28		1.2	6.5	2.2		
	F	W	0.28		1.2	6.5	2.2	2.2	28.7

3). Design of Girder and Beam



$$W = 0.64 \times 1.25 + 0.21 = 1.01 \text{ t/m}$$

$$M = 1/12 \times 1.01 \times 2.8^2 = 0.66 \text{ t-m}$$

$$Q = 1/2 \times 1.01 \times 2.8 = 1.425$$

<G>

$$B \times D = 15 \times 40 \text{ cm}$$

$$d = 35 \text{ cm}$$

$$j = 30.63 \text{ cm}$$

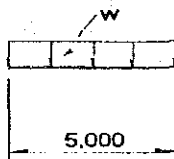
$$A_t = 66 / (1.8 \times 30.63) = 1.20 \text{ cm}^2$$

2-D13

$$\phi = 1420 / (14 \times 30.63) = 3.31 \text{ cm}$$

$$\tau = 1420 / (15 \times 30.63) = 3.1 < 4.25 \text{ kg/cm}^2$$

OK



$$W = 9.1/5.0 + 0.64 \times 1.39 + 0.21 = 2.92 \text{ t/m}$$

$$M = 1/8 \times 2.92 \times 5.0^2 = 9.13 \text{ t-m}$$

$$Q = 1/2 \times 2.92 \times 5.0 = 7.3 \text{ t}$$

<B1>

$$B \times D = 30 \times 60$$

$$d = 55$$

$$j = 48.13$$

End

$$\phi = 7300 / (14 \times 48.13) = 10.83 \text{ cm}$$

3-D19

$$\tau = 7300 / (30 \times 48.13) = 5.05 > 4.25 \text{ kg/cm}^2$$

NG

$$DQ = 7.3 - 30 \times 48.13 \times 4.25 \times 10^{-3} = 1.17 \text{ t}$$

$$DQ/bj = 0.9$$

$$P_w = 0.30$$

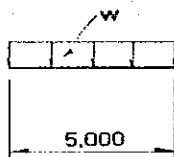
$$D10 \quad x = 1.43 / (30 \times 0.003) = 15.8 \text{ cm}$$

∴ D10 - @150

Center

$$A_t = 913 / (1.8 \times 48.13) = 10.54 \text{ cm}^2$$

5-D19



$$W = 13.2/5.0 + 0.64 \times 2.14 + 0.38 = 4.39 \text{ t/m}$$

$$M = 1/8 \times 4.39 \times 5.0^2 = 13.72 \text{ t-m}$$

$$Q = 1/2 \times 4.39 \times 5.0 = 10.98 \text{ t}$$

<B2>

$$B \times D = 35 \times 60$$

$$d = 55$$

$$j = 48.13$$

End

$$\phi = 10980 / (14 \times 48.13) = 16.30 \text{ cm}$$

4-D19

$$\tau = 10980 / (35 \times 48.13) = 6.52 > 4.25 \text{ kg/cm}^2$$

NG

$$DQ = 10.98 - 35 \times 48.13 \times 4.25 \times 10^{-3} = 3.83 \text{ t}$$

$$DQ/bj = 2.3$$

$$P_w = 0.46$$

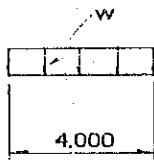
$$D13 \quad x = 15.7 \text{ cm}$$

D13-@150

Center

$$A_t = 1372 / (1.8 \times 48.13) = 15.84 \text{ cm}^2$$

6-D19



$$W = 13.2/5.0 + 0.64 \times 1.38 + 0.38 = 3.91 \text{ t/m}$$

$$M = 1/8 \times 3.91 \times 4.0^2 = 7.82 \text{ t-m}$$

$$Q = 1/2 \times 3.91 \times 4.0 = 7.82 \text{ t}$$

<B1>

$$B \times D = 30 \times 60$$

$$j = 48.13$$

End

$$\phi = 7820/(14 \times 48.13) = 11.61 \text{ cm } 3\text{-D19}$$

$$\tau = 7820/(30 \times 48.13) = 5.42 > 4.25 \text{ kg/cm}^2$$

N G

$$DQ = 7.82 - 6.13 = 1.69 \text{ t}$$

$$DQ/bj = 1.2$$

$$Pw = 0.31$$

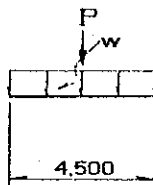
$$D13 \quad x = 2.54/(30 \times 0.0031) = 27.3 \text{ cm}$$

$$\therefore D13 - @200$$

Center

$$At = 782/(1.8 \times 48.13) = 9.03 \text{ cm}^2$$

$$5\text{-D19}$$



$$W = 0.21 + 0.64 \times 1.12 = 0.93 \text{ t/m}$$

$$P = 0.64 \times 2.25 \times 2.25 = 3.24 \text{ t}$$

$$M = 1/8 \times 0.93 \times 4.5^2 + 1/4 \times 3.24 \times 4.5 = 6.0 \text{ t-m}$$

$$Q = 1/2 \times 0.93 \times 4.5 + 1/2 \times 3.24 = 3.72 \text{ t}$$

<B3>

$$B \times D = 18 \times 60$$

$$d = 55$$

$$j = 48.13$$

End

$$\phi = 3720/(14 \times 48.13) = 5.52 \text{ cm}$$

$$2\text{-D16}$$

$$\tau = 3720/(75 \times 48.13) = 5.15 > 4.25 \text{ kg/cm}^2$$

N G

$$DQ = 3.72 - 15 \times 48.13 \times 4.25 \times 10^{-3} = 0.65 \text{ t}$$

$$DQ/bj = 0.9$$

$$Pw = 0.32$$

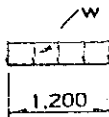
$$D10 \quad x = 1.43/(15 \times 0.0032) = 29.7 \text{ cm}$$

$$\therefore D10 - @200$$

Center

$$At = 600/(1.8 \times 48.13) = 6.92 \text{ cm}^2$$

$$4\text{-D16}$$



$$W = 0.66 \text{ t/m/}$$

$$M = 1/2 \times 0.66 \times 1.2^2 = 0.48 \text{ t-m}$$

$$Q = 0.66 \times 1.2 = 0.80 \text{ t}$$

<CS1>

$$D = 15 \text{ cm} \quad d = 12 \text{ cm} \quad j = 10.5 \text{ cm}$$

$$A_t = 48 \times 1.5 / (1.8 \times 10.5) = 3.81 \text{ cm}^2$$

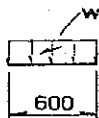
D10&13

$$x = \frac{0.99 \times 100}{3.81} = 25.9 \text{ cm}$$

$$\phi = 800 \times 1.5 / (14 \times 10.5) = 8.16 \text{ cm}$$

$$x = \frac{3.5 \times 100}{8.16} = 42.8 \text{ cm}$$

∴ D10&13-@200



$$W = 0.66 \text{ t/m}$$

$$M = 1/2 \times 0.66 \times 0.6^2 = 0.12 \text{ t-m}$$

$$Q = 0.66 \times 0.6 = 0.40 \text{ t}$$

<CS2>

$$D = 15 \text{ cm} \quad d = 12 \text{ cm} \quad j = 10.5 \text{ cm}$$

$$A_t = 12 \times 1.5 / (1.8 \times 10.5) = 0.96 \text{ cm}^2$$

D10

$$x = \frac{0.71 \times 100}{0.96} = 73.9 \text{ cm}$$

$$\phi = 400 \times 1.5 / (14 \times 10.5) = 4.08 \text{ cm}$$

$$x = \frac{3.0 \times 100}{4.08} = 73.5 \text{ cm}$$

∴ D10-@200

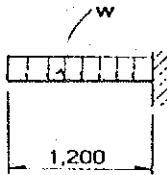
4). Design of Slab

		Lx(m)	Ly(m)	t(Cm)	w(t/m ²)
D10,D13	S01	4.0	5.0	15.0	0.660
	S02	4.5	4.5	15.0	0.660
	S03	4.0	5.0	15.0	0.870
	S04	4.0	4.0	15.0	0.760

		Lx(m)	Ly(m)	t(Cm)	w(t/m ²)	
41	D10,D13	S01	4.0	5.0	15.0	0.660
		LAMBDA=	1.25	wLx2(t*m)=	10.560	f t(Kg/cm ²)=2000.0
		ALPHA	M(t*m/m ²)	at(Cm ² /m)	D10	D10&D13 D13
	X-E	-0.059	-0.624	2.97	@23.9	@33.3 @42.7)D10,D13-@200
	X-C	0.039	0.416	1.98	@35.8	@50.0 @64.1
	Y-E	-0.042	-0.440	2.29	@31.1	@43.3 @55.6)D10,D13-@200
	Y-C	0.028	0.293	1.52	@46.6	@65.0 @83.3
41		Lx(m)	Ly(m)	t(Cm)	w(t/m ²)	
	S02	4.5	4.5	15.0	0.660	
		LAMBDA=	1.00	wLx2(t*m)=	13.365	f t(Kg/cm ²)=2000.0
		ALPHA	M(t*m/m ²)	at(Cm ² /m)	D10	D10&D13 D13
	X-E	-0.042	-0.557	2.65	@26.8	@37.3 @47.9)D10,D13-@200
	X-C	0.028	0.371	1.77	@40.2	@56.0 @71.8
	Y-E	-0.042	-0.557	2.89	@24.5	@34.2 @43.9)D10,D13-@200
	Y-C	0.028	0.371	1.93	@36.8	@51.3 @65.9
41		Lx(m)	Ly(m)	t(Cm)	w(t/m ²)	
	S03	4.0	5.0	15.0	0.870	
		LAMBDA=	1.25	wLx2(t*m)=	13.920	f t(Kg/cm ²)=2000.0
		ALPHA	M(t*m/m ²)	at(Cm ² /m)	D10	D10&D13 D13
	X-E	-0.059	-0.823	3.92	@18.1	@25.3 @32.4)D10,D13-@200
	X-C	0.039	0.549	2.61	@27.2	@37.9 @48.6
	Y-E	-0.042	-0.580	3.01	@23.6	@32.9 @42.2)D10,D13-@200
	Y-C	0.028	0.387	2.01	@35.3	@49.3 @63.2
41		Lx(m)	Ly(m)	t(Cm)	w(t/m ²)	
	S04	4.0	4.0	15.0	0.760	
		LAMBDA=	1.00	wLx2(t*m)=	12.160	f t(Kg/cm ²)=2000.0
		ALPHA	M(t*m/m ²)	at(Cm ² /m)	D10	D10&D13 D13
	X-E	-0.042	-0.507	2.41	@29.4	@41.0 @52.6)D10,D13-@200
	X-C	0.028	0.338	1.61	@44.1	@61.5 @79.0
	Y-E	-0.042	-0.507	2.63	@27.0	@37.6 @48.3)D10,D13-@200
	Y-C	0.028	0.338	1.75	@40.5	@56.4 @72.4

5). Design of Stair

Floor load	D.L		L.L	T.L
Terrazzo	60	660	300	960
Concrete slab	600		180	840
			80	740



$$W = 0.25 \times 0.96 = 0.24$$

$$M = 1/2 \times 0.24 \times 1.2^2 = 0.18 \text{ t}\cdot\text{m}$$

$$Q = 0.24 \times 1.2 = 0.29$$

$$D = 25\text{cm}$$

$$d = 20\text{cm}$$

$$j = 17.5\text{cm}$$

$$A_t = \frac{18 \times 1.5}{1.8 \times 17.5} = 0.86 \text{ cm}^2$$

1-D13

$$\phi = \frac{290 \times 1.5}{21 \times 17.5} = 1.18 \text{ cm}$$

6). Design of Foundation

Allowable bearing capacity

$$f_c = 30 \text{ t/m}^2 \text{ (permanent)}$$

Dead load

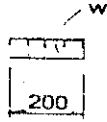
$$2.4 \times 0.19 \times 0.75 = 0.35 \text{ t/m}$$

$$2.0 \times (1.0 - 0.19) \times 0.6 = 0.98 \text{ t/m}$$

$$\text{Total} = 1.33 \text{ t/m}$$

No.	LF (m)	N (t)	$P' = N/LF$ (t/m)	P (t/m)
W1	10.5	20.6	1.96	3.29
W2	6.0	12.7	2.12	3.45
W3	4.75	9.2	1.94	3.27
W4	4.5	8.6	1.92	3.25
W5	2.0	4.4	2.2	3.53
W10	4.0	18.9	4.73	6.06
W11	5.0	19.8	3.96	5.29
W12	4.5	23.4	5.2	6.53
W14	2.5	14.0	5.6	6.93
W15	4.0	6.3	1.58	2.91
W16	4.0	8.4	2.1	3.43
W17	4.0	9.2	2.3	3.63
W18	5.0	11.1	2.22	3.55
W19	8.25	45.85	5.56	6.89
W20	7.25	33.9	4.68	6.01
W21	3.5	14.3	4.09	5.42
W22	4.75	25.15	5.30	6.63
W23	7.25	35.3	4.87	6.20

No.	L' (m)	L (m)	α_c	P'' (t/m)	α_c' (t/m ²)
W1	0.11	0.40			
W2	0.12	"			
W3	0.11	"			
W4	0.11	"			
W5	0.12	"			
W10	0.21	"			
W11	0.18	"			
W12	0.22	"			
W14	0.23	"	$17.4\text{t/m}^2 < 30\text{t/m}^2$	5.95	14.9
W15	0.10	"			
W16	0.12	"			
W17	0.13	"			
W18	0.12	"			
W19	0.23	"			
W20	0.20	"			
W21	0.18	"			
W22	0.22	"			
W23	0.21	"			



$$W = 14.9 \text{ t/m}$$

$$M = 1/2 \times 14.9 \times 0.2^2 = 0.30 \text{ t-m}$$

$$Q = 14.9 \times 0.2 = 2.98 \text{ t}$$

<F1>

$$D = 18 \text{ cm} \quad d = 12 \text{ cm} \quad j = 10.5 \text{ cm}$$

$$A_t = 30/1.8 \times 10.5 = 1.59 \text{ cm}^2$$

D10

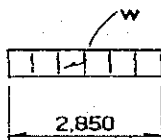
$$x = \frac{0.71 \times 100}{1.59} = 44.6 \text{ cm}$$

$$\phi = 2980/21 \times 10.5 = 13.5$$

∴ D10-@200

$$x = \frac{3.0 \times 100}{13.5} = 22.2 \text{ cm}$$

$$\tau = 2980/100 \times 10.5 = 2.9 \text{ kg/cm}^2 < 4.25 \text{ kg/cm}^2 \text{ OK}$$



$$W = 5.6 \text{ t/m}$$

$$M = 1/2 \times 5.6 \times 2.85^2 = 3.80 \text{ t-m}$$

$$Q = 1/2 \times 5.6 \times 2.85 = 7.98 \text{ t}$$

<FG1>

$$B \times D = 19 \times 75 \text{ cm}$$

$$d = 67 \text{ cm}$$

$$j = 58.63 \text{ cm}$$

$$A_t = 380/1.8 \times 58.63 = 3.60 \text{ cm}^2$$

2-D16

$$\phi = 7980/21 \times 58.63 = 6.48 \text{ cm}$$

$$\tau = 7980/19 \times 58.63 = 7.16 > 4.25 \text{ kg/cm}^2$$

NG

$$DQ = 7.98 - 19 \times 58.63 \times 4.25 \times 10^{-3} = 3.25 \text{ t}$$

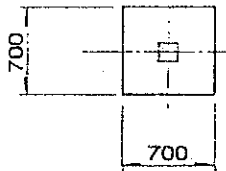
$$DQ/bj = 2.92$$

$$P_w = 0.49$$

$$D10 \quad x = 1.43/19 \times 0.0049 = 15.3 \text{ cm}$$

∴ D10 - @150

<W13>



$$N' = 7.4t$$

$$A = 7.4/28.5 = 0.26 \text{ m}^2 \quad 1 \times 1' = 0.7 \times 0.7$$

$$N = 7.4 \times 2.0 \times 0.7 \times 0.7 \times 0.75 = 8.2 \text{ t}$$

$$\sigma_c = 8.2/0.7 \times 0.7 = 16.8 < 30.0 \text{ t/m}^2 \quad \text{OK}$$

$$l/a = 4.7$$

$$M = 0.37 \times 0.15 = 0.06 \text{ t}\cdot\text{m}$$

$$Q = 0.39 \times 7.4 = 2.89 \text{ t}$$

<F2>

$$D = 25 \text{ cm}$$

$$d = 17 \text{ cm}$$

$$j = 14.88 \text{ cm}$$

$$A_t = 6/1.8 \times 14.88 = 0.22 \text{ cm}^2$$

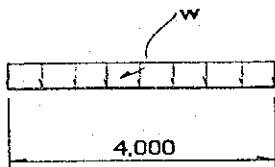
4-D10

$$\phi = 2890/21 \times 14.88 = 9.25 \text{ cm}$$

$$\tau = 2890/65 \times 14.88 = 3.0 < 4.25 \text{ kg/cm}^2$$

7). Design of Steel Roof

Asbestos cement board	30	60	70	90
Purline	10			
Ceiling	20			
Beam	10			
Girder	20			



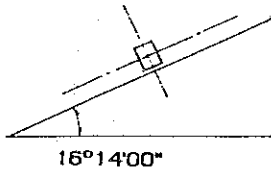
(G) $W = 0.06 \text{ t/m}$

90 cm interval

$$W = 0.06 \times 0.9 = 0.054$$

$$W_x = 0.054 \times \cos q = 0.052$$

$$W_y = 0.054 \times \sin q = 0.016$$



$$M_x = 0.052 \times 4.0^2 \times 1/8 = 0.104 \text{ tm}$$

$$M_y = 0.016 \times 4.0^2 \times 1/8 = 0.032 \text{ tm}$$

use C - 100 x 50 x 20 x 1.6

$$Z_x = 11.6 \text{ (16.1)}$$

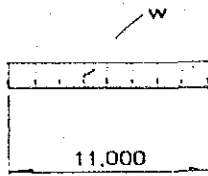
$$Z_y = 4.30 \text{ (6.06)}$$

$$\frac{\sigma_x + \sigma_y}{f_b} = 10.4/11.6 \times 1.4 + 3.2/4.3 \times 1.4 = 0.84 < 1.0 \quad \text{OK}$$

$$\delta_x = \frac{5 \times 0.52 \times 4.0^4 \times 10^8}{384 \times 2.1 \times 10^6 \times 80.7} = 1.01 \text{ cm}$$

$$\delta = 1.63 \text{ cm (1/245)}$$

$$\delta_y = \frac{5 \times 0.16 \times 4.0^4 \times 10^8}{384 \times 2.1 \times 10^6 \times 19.0} = 1.29 \text{ cm}$$



$$W = 0.09 \times 4.0 = 0.36 \text{ t/m}$$

$$M = 1/8 \times 0.36 \times 11.0^2 = 5.46 \text{ t.m}$$

$$Q = 1/2 \times 0.36 \times 11.0 = 1.98 \text{ t}$$

<SB1>

use H - 400 x 200 x 8 x 13

$$I=23700 \quad z=1190$$

$$l_b = 367$$

$$f_b = 900 \times 20 \times 1.3/40 \times 367 = 1.59$$

$$\therefore f_b = 1.4$$

$$\sigma_b/f_b = 546/1190 \times 1.4 = 0.33 < 1.0$$

OK

$$\delta = \frac{5 \times 3.6 \times 11.0^4 \times 10^8}{384 \times 2.1 \times 10^6 \times 23700} = 1.38 \text{ cm}$$

(1/797)

8). Design of Foundation (for F2)

(a)	Parapet	0.34×4.0	=	1.4	
	Roof	$0.64 \times 1.8 \times 4.0$	=	4.6	6.3 t
	C	0.08×3.0	=	0.3	
(b)	Roof	$0.09 \times 4.0 \times 6.0$	=	2.2	
	"	$0.64 \times 1.5 \times 4.0$	=	3.9	8.6
	G	0.53×4.0	=	2.2	
	C	0.08×3.0	=	0.3	

$$A = 8.6/28.5 = 0.302 \quad \rightarrow l \times l' = 0.7 \times 0.7$$

<F2>

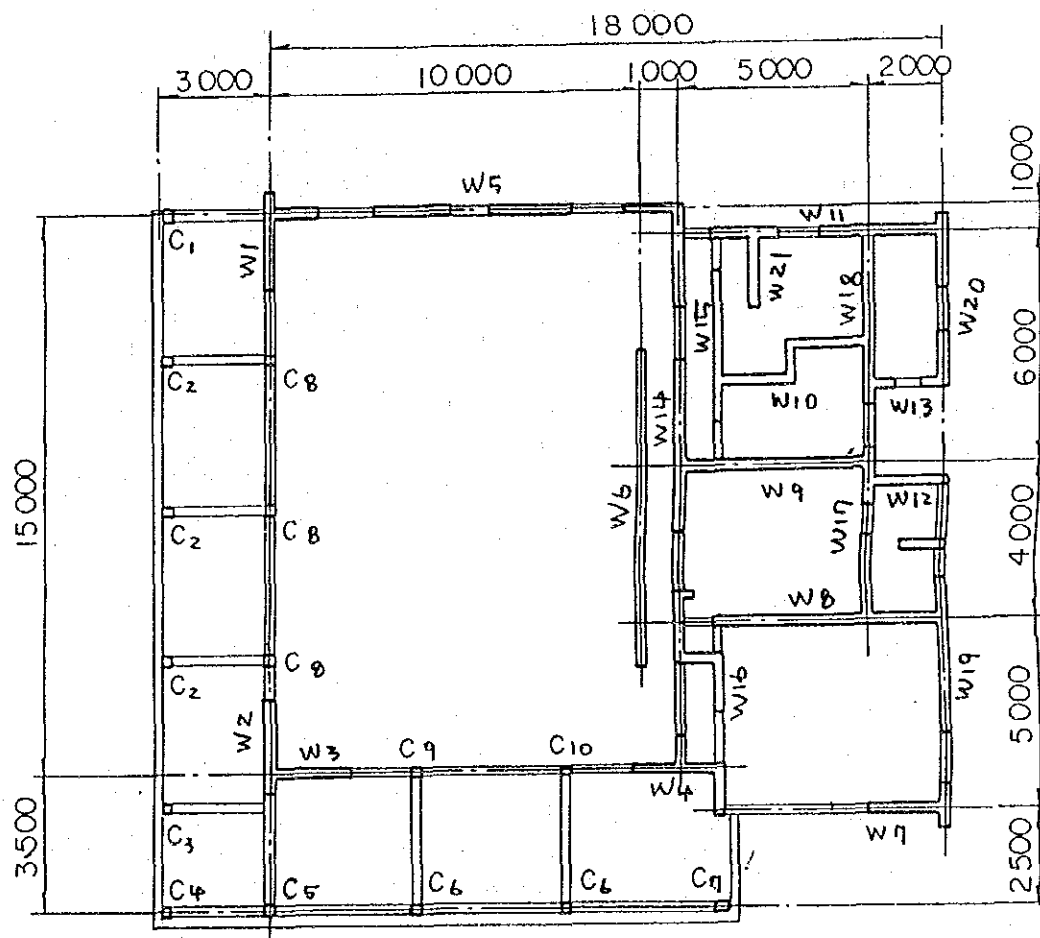
$$N = 8.6 + 2.0 \times 0.7 \times 0.7 \times 0.75 = 9.4 \text{ t}$$

$$\sigma = 9.4/0.7 \times 0.7 = 19.1 < f_c = 30.0 \text{ t/m}^2$$

OK

3.5.2 Utility Building B

Framing Plan



GROUND FL PLAN

1). Assumed Load

A : To floor
B : To frame
C : To seismic

1-1 Floor Load Table

D.L : Dead load
L.L : Live load
T.L : Total load

Title	Material	Thick (cm)	Weight (kg/m ²)		D.L (kg/m ²)	L.L (kg/m ²)	T.L (kg/m ²)	Note
Roof (1) (concrete)	Concrete	60	140	A	570	90	660	
	Water Proofing		20					
	Cement Mortar	15	30	B		70	640	
	Concrete Slab	150	360					
	Ceiling		20	C		30	600	
Roof (2) (steel)	Asbestos Cement Board		30	A	60	-	60	
	Puline		10					
	Ceiling		20	B	90	-	90	
	Beam		10					
	Girder		20	C	90	-	90	

1-2 Dead Load of Girder and Wall

	Title	Size (cm)	Weight (kg/cm ²)
	Girder	15 x 60	162 + 42 → 210
		15 x 40	90 + 26 → 120
		15 x 85	252 + 62 → 320
		15 x 45	108 + 30 → 140
	Beam	25 x 60	270 + 46 → 320
	Column	15 x 15	54 + 24 → 80
	Wall	W15	360 + 80 → 440
		CB15	200 + 80 → 280

2). Calculation of Axial Force of Columns

G : Girder
W : Wall
C : Column
B : Beam

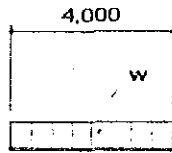
No.	Floor	Title	Calculation					W (t)	ΣW (t)
			Load (t/m ² & t-m)	Area (m ²)	Length (m)	Length (m)	W' (t)		
C1	1F	Roof(1) G C	0.64 0.21 0.08	3.27	3.5 1.4		2.1 0.8 0.2	3.1	
	F	C	0.08		1.4		0.2	0.2	3.3
C2	1F	Roof(1) G C	0.64 0.21 0.08	6.3	5.5 1.4		4.1 1.2 0.2	5.5	
	F	C	0.08		1.4		0.2	0.2	5.7
C3	1F	Roof(1) G C	0.64 0.21 0.08	5.12	4.75 1.4		3.3 1.0 0.2	4.5	
	F	C	0.08		1.4		0.2	0.2	4.7
C4	1F	Roof(1) G C	0.64 0.21 0.08	2.09	2.75 1.4		1.4 0.6 0.2	2.2	
	F	C	0.08		1.4		0.2	0.2	2.4
C5	1F	Roof(1) G C	0.64 0.21 0.08	6.39	5.25 1.4		4.1 1.1 0.2	5.4	
	F	C	0.08		1.4		0.2	0.2	5.6
C6	1F	Roof(1) G C	0.64 0.21 0.08	7.3	5.75 1.4		4.7 1.2 0.2	6.1	
	F	C	0.08		1.4		0.2	0.2	6.3
C7	1F	Roof(1) G C	0.64 0.21 0.08	3.0	3.25 1.4		2.0 0.7 0.2	2.9	
	F	C	0.08		1.4		0.2		3.1
C8	1F	Roof(4) Roof(2) G W(W15) C	0.64 0.09 0.21 0.44 0.08	6.0 22.8	5.5 1.25 1.4	4.0	3.9 2.1 1.2 2.2 0.2	9.6	
	F	C	0.08		1.4		0.2	0.2	9.8

No.	Floor	Title	Calculation					W (t)	ΣW (t)
			Load (t/m ² & t-m)	Area (m ²)	Length (m)	Length (m)	W' (t)		
C9	1F	Roof(1) Roof(2) G W(W15) C	0.64 0.09 0.21 0.44 0.08	4.53 6.0	5.75 1.65 1.4	3.0	2.9 0.6 1.2 2.2 0.2	7.1	
	F	C	0.08		1.4		0.2	0.2	7.3
C10	1F	Roof(1) Roof(2) G W(W15) C	0.64 0.09 0.21 0.44 0.08	4.53 6.0	5.75 1.95 1.4	3.0	2.9 0.6 1.2 2.6 0.2	7.5	
	F	C	0.08		1.4		0.2	0.2	7.7
W1	1F	Roof(1) G W(W15) W(CB15)	0.64 0.21 0.44 0.28	4.5	4.5 1.2 1.2	3.0 3.0	2.9 1.0 1.6 1.0	6.5	
	F	WC(B15)	0.28		1.2	3.0	1.0	1.0	7.5
W2	1F	Roof G W(W15) W(CB15)	0.64 0.21 0.44 0.28	6.0	5.5 1.2 1.2	2.0 1.7	2.9 1.2 1.1 0.6	6.8	
	F	W(CB15)	0.28		1.2	1.7	0.6	0.6	7.4
W3 W4	1F	Roof G W(W15) W(CB15)	0.64 0.21 0.44 0.28	4.97	3.0 1.35 1.2	3.0 2.0	3.2 0.7 1.8 0.7	6.4	
	F	W(CB15)	0.28		1.2	2.0	0.7	0.7	7.1
W5	1F	Roof(2) W(W15) G WC(B15)	0.09 0.44 0.21 0.28	29.64	2.05 11.0 1.2	11.0 11.0	2.7 10.0 2.4 3.7	18.8	
	F	W(CB15)	0.28		1.2	11.0	3.7	3.7	22.5
W6	1F	Roof(1) G W(CB15)	0.64 0.21 0.28	4.25	8.5 1.2	8.5	2.8 1.8 2.9	7.5	
	F	W(CB15)	0.28		1.2	8.5	2.9	2.9	10.4

No.	Floor	Title	Calculation					W (t)	ΣW (t)
			Load (t/m ² & t.m)	Area (m ²)	Length (m)	Length (m)	W' (t)		
W7	1F	Roof(1) W(W15) G B W(CB15)	0.64 0.44 0.21 0.32 0.28	9.75	1.5 6.0 2.5 1.2	6.0	6.3 4.0 1.3 0.8 2.0	14.4	
	F	W(CB15)	0.28		1.2	6.0	2.0	2.0	16.4
W8	1F	Roof(1) W(W15) G B W(CB15)	0.64 0.44 0.21 0.32 0.28	17.25	1.5 6.5 2.5 1.2	6.5 6.0	11.1 4.3 1.4 0.8 2.0	19.6	
	F	W(CB15)	0.28		1.2	6.0	2.0	2.0	21.6
W9	1F	Roof(1) W(W15) " G W(CB15)	0.64 0.44 0.44 0.21 0.28	9.5	1.9 1.0 5.0 1.2	2.0 4.0 5.0	6.1 1.7 1.8 1.1 1.7	12.4	
	F	W(CB15)	0.28		1.2	5.0	1.7	1.7	14.1
W10	1F	Roof(1) W(W15) G W(CB15)	0.64 0.44 0.21 0.28	7.69	1.1 5.0 1.2	5.0 5.0	5.0 2.5 1.1 1.7	10.3	
	F	W(CB15)	0.28		1.2	5.0	1.7	1.7	12.0
W11	1F	Roof(1) W(W15) " G W(CB15)	0.64 0.44 0.44 0.21 0.28	4.0	2.25 1.45 7.0 1.2	2.0 5.0 7.0	2.6 2.0 3.2 1.5 2.4	11.7	
	F	W(CB15)	0.28		1.2	7.0	2.4	2.4	14.1
W12 W13	1F	Roof(1) W(W15) G W(CB15)	0.64 0.44 0.21 0.28	2.0	0.65 2.0 1.2	2.0 2.0	1.3 0.6 0.5 0.7	3.1	
	F	W(CB15)	0.28		1.2	2.0	0.7	0.7	3.8
W14	1F	Roof(2) W(W15) Roof(1) G W(CB15)	0.99 0.44 0.64 0.21 0.28	85.5 12.75	2.7 15.0 1.2	15.0 15.0	7.7 17.9 8.2 3.2 5.1	42.1	
	F	W(CB15)	0.28		1.2	15.0	5.1	5.1	47.2

No.	Floor	Title	Calculation					W (t)	ΣW (t)
			Load (t/m ² & t-m)	Area (m ²)	Length (m)	Length (m)	W' (t)		
W15	1F	Roof(1) W(W15) G W(CB15)	0.64 0.44 0.21 0.28	5.01	1.8 5.0 1.2	5.0 4.0	3.2 4.0 1.1 1.4	9.7	
	F	W(CB15)	0.28		1.2	4.0	1.4	1.4	11.1
W16	1F	Roof(1) W(W15) G W(CB15)	0.64 0.44 0.21 0.28	9.28	1.8 4.0 1.2	4.0 4.0	6.0 3.2 0.9 1.4	11.5	
	F	W(CB15)	0.28		1.2	4.0	1.4	1.4	12.9
W17	1F	Roof(1) W(W15) G W(CB15)	0.64 0.44 0.21 0.28	7.53	0.8 4.75 1.2	4.0 4.0	4.9 1.4 1.0 1.4	8.7	
	F	W(CB15)	0.28		1.2	4.0	1.4	1.4	10.1
W18	1F	Roof(1) W(W15) G W(CB15)	0.64 0.44 0.21 0.28	7.97	0.8 5.5 1.2	5.5 4.5	5.1 2.0 1.2 1.6	9.9	
	F	W(CB15)	0.28		1.2	4.0	1.6	1.6	11.5
W19	1F	Roof(1) W(W15) G W(CB15)	0.64 0.44 0.21 0.28	8.5	1.0 9.75 1.2	9.75 7.0	5.5 4.3 2.1 2.4	14.3	
	F	W(CB15)	0.28		1.2	7.0	2.4	2.4	16.7
W20	1F	Roof(1) W(W15) G W(CB15)	0.64 0.44 0.21 0.28	3.75	1.0 5.25 1.2	5.25 4.5	2.4 2.4 1.1 1.6	7.5	
	F	W(CB15)	0.28		1.2	4.5	1.6	1.6	9.1
W21	1F	Roof(1) W(W15) G W(CB15)	0.64 0.44 0.21 0.28	3.75	2.1 2.0 1.2	2.0 2.0	2.4 1.9 0.5 0.7	5.5	
	F	W(CB15)	0.28		1.2	2.0	0.7	0.7	6.2

3). Design of Girder and Beam



$$W = 0.64 \text{ t/m}^2 \times 0.95 \text{ m} + 0.21 \text{ t/m} = 0.82 \text{ t/m}$$

$$\begin{cases} C = 1/12 \times 0.82 \times 4.0^2 = 1.10 \text{ t-m} \\ M_o = 1/8 \times 0.82 \times 4.0^2 = 1.65 \text{ t-m} \\ Q = 1/2 \times 0.82 \times 4.0 = 1.65 \text{ t} \end{cases}$$

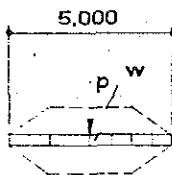
< G1 >

$$B \times D = 15 \text{ cm} \times 60 \text{ cm} \quad d = 55 \text{ cm} \quad j = 48.13 \text{ cm}$$

$$A_t = 165 \text{ t-cm} / 1.8 \times 48.13 = 1.91 \text{ cm}^2 \quad 2 - D13$$

$$\phi = 1650 / 14 \times 48.13 = 2.45 \text{ cm}$$

$$\tau = 1650 / 15 \times 48.13 = 2.3 \text{ kg/cm}^2 < 4.25 \text{ kg/cm}^2 \text{ O.K}$$



$$W = 0.32 \text{ t/m}$$

$$P = 0.64 \times 5.25 \times 2 = 6.72$$

$$\begin{cases} M_o = 1/8 \times 0.32 \times 5.0^2 + 1/4 \times 6.72 \times 5.0 = 9.4 \text{ tm} \\ Q = 1/2 \times 0.32 \times 5.0 + 1/2 \times 6.72 = 4.16 \text{ t} \end{cases}$$

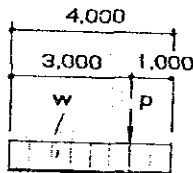
< B1 >

$$B \times D = 30 \times 60 \quad d = 55 \quad j = 48.13$$

$$\text{End} \quad \phi = 4160 / 14 \times 48.13 = 6.17 \text{ cm}^2 \quad 3 - D19$$

$$\tau = 4160 / 30 \times 48.13 = 3.46 \text{ kg/cm}^2 < 4.25 \text{ kg/cm}^2 \text{ O.K}$$

$$\text{Center} \quad A_t = 940 / 1.8 \times 48.13 = 10.85 \text{ cm}^2 \quad 5 - D19$$



$$W = 0.32 \text{ t/m}$$

$$P = 4.16 \text{ t}$$

$$\begin{cases} Q_a = 1/2 \times 0.32 \times 4.0 + \frac{4.16 \times 1.0}{4.0} = 1.68 \text{ t} \\ Q_b = 1/2 \times 0.32 \times 4.0 + \frac{4.16 \times 3.0}{4.0} = 3.76 \text{ t} \\ M = 1/8 \times 0.32 \times 4.0^2 + 1.04 \times 2.0 = 2.72 \text{ t-m} \end{cases}$$

< G2 >

$$B \times D = 25 \times 60 \quad d = 55 \quad j = 48.13$$

$$\text{End} \quad \phi = 3760 / 14 \times 48.13 = 5.58 \text{ cm}^2 \quad 2 - D16$$

$$\tau = 3760 / 25 \times 48.13 = 3.13 \text{ kg/cm}^2 < 4.25 \text{ O.K}$$

$$\text{Center} \quad A_t = 272 / 1.8 \times 48.13 = 2.83 \text{ cm}^2 \quad 2 - D16$$

4). Design of Slab

		Lx(m)	Ly(m)	t(Cm)	w(t/m ²)
D10,D13	S01	3.0	4.0	15.0	0.660
	S02	3.0	5.0	15.0	0.660
	S03	3.5	4.0	15.0	0.660

	Lx(m)	Ly(m)	t(Cm)	w(t/m ²)	
D10,D13	3.0	4.0	15.0	0.660	
	LAMBDA= 1.33	wLx2(t*m)=	5.940	ft(kg/cm ²)=2000.0	
S ₁	ALPHA	M(t*m/m ²)	at(Cm ² /m)	D10	D10&D13 D13
X-E	-0.063	-0.376	1.79	@39.7	@55.3 @70.9
X-C	0.042	0.251	1.19	@59.5	@82.9 @###.#
Y-E	-0.042	-0.247	1.29	@55.2	@77.0 @98.8
Y-C	0.028	0.165	0.86	@82.8	@###.# @###.#
) D10.13-C200
) D10.13-C200
	Lx(m)	Ly(m)	t(Cm)	w(t/m ²)	
S02	3.0	5.0	15.0	0.660	
	LAMBDA= 1.67	wLx2(t*m)=	5.940	ft(kg/cm ²)=2000.0	
S ₁	ALPHA	M(t*m/m ²)	at(Cm ² /m)	D10	D10&D13 D13
X-E	-0.074	-0.438	2.09	@34.0	@47.4 @60.9
X-C	0.049	0.292	1.39	@51.0	@71.2 @91.3
Y-E	-0.042	-0.247	1.29	@55.2	@77.0 @98.8
Y-C	0.028	0.165	0.86	@82.8	@###.# @###.#
) D10.13-C200
) D10.13-C200
	Lx(m)	Ly(m)	t(Cm)	w(t/m ²)	
S03	3.5	4.0	15.0	0.660	
	LAMBDA= 1.14	wLx2(t*m)=	8.085	ft(kg/cm ²)=2000.0	
S ₁	ALPHA	M(t*m/m ²)	at(Cm ² /m)	D10	D10&D13 D13
X-E	-0.053	-0.425	2.02	@35.1	@48.9 @62.8
X-C	0.035	0.283	1.35	@52.7	@73.4 @94.2
Y-E	-0.042	-0.337	1.75	@40.6	@56.6 @72.6
Y-C	0.028	0.225	1.17	@60.9	@84.9 @###.#
) D10.13-C200
) D10.13-C200

5). Design of Foundation

Allowable bearing capacity

$$f_e = 30 \text{ t/m}^2 \text{ (Permanent)}$$

$$\text{Dead load} \quad \left. \begin{array}{l} 2.4 \text{ t/m}^3 \times 0.19 \text{ m} \times 0.75 \text{ m} = 0.35 \text{ t/m} \\ 2.0 \text{ t/m}^3 \times (1.0 - 0.91 \text{ m}) \times 0.6 \text{ m} = 0.98 \text{ t/m} \end{array} \right\} 1.33 \text{ t/m}$$

W : Wall C : Column

No.	LF (m)	N (t)	P'=N/LF (t/m)	P (t/m)
W1	2.4	7.5	3.13	4.46
W2	2.4	7.4	3.09	4.42
W3 (W4)	2.0	7.1	3.55	4.88
W5	11.0	22.5	2.05	3.38
W6	8.5	10.4	1.23	2.56
W7	6.0	16.4	2.74	4.07
W8	6.6	21.6	3.28	4.61
W9	4.6	14.1	3.07	4.40
W10	4.6	12.0	2.61	3.94
W11	6.6	14.1	2.14	3.47
W12 W13	1.6	3.8	2.38	3.71
W14	15.0	47.2	3.15	4.48
W15	6.0	11.1	1.85	3.18
W16	5.0	12.9	2.58	3.91
W17	4.0	10.1	2.53	3.86
W18	6.5	11.5	1.77	3.10
W19	8.5	16.7	1.97	3.30
W20	4.0	9.1	2.28	3.61
W21	2.0	6.2	3.1	4.43

No.	$L' = \frac{P}{f_c}$ (m)	L (l)	$\sigma_c = \frac{P}{L}$ (t/m)	$P''(t/m)$ ($P' + 0.35$)	$\sigma_c' = \frac{P''}{L}$
W1	0.15	0.40			
W2	0.15	"			
W3 (W4)	0.17	"	12.2 t/m ² < 30	3.9	9.75
W5	0.12	"			
W6	0.09	"			
W7	0.14	"			
W8	0.16	"			
W9	0.15	"			
W10	0.14	"			
W11	0.12	"			
W12 W13	0.13	"			
W14	0.15	"			
W15	0.11	"			
W16	0.13	"			
W17	0.13	"			
W18	0.11	"			
W19	0.11	"			
W20	0.12	"			
W21	0.15	0.40			

< F1 >

$$W = 9.75 \text{ t/m}$$



$$\begin{cases} M = 1/2 \times 9.75 \times 0.2^2 = 0.20 \text{ t-m} \\ Q = 9.75 \times 0.12 = 1.95 \text{ t} \end{cases}$$

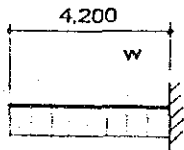
$$D = 18 \text{ cm} \quad d = 12 \text{ cm} \quad j = 10.5 \text{ cm}$$

$$A_t = 20/1.8 \times 10.5 = 1.06 \text{ cm}^2 \quad x = \frac{0.71 \times 100}{1.06} = 66.9 \text{ cm}$$

$$\phi = 1950/21.0 \times 10.5 = 8.85 \text{ cm} \quad x = \frac{3.0 \times 100}{8.85} = 33.8 \text{ cm}$$

$$\tau = 1950/100 \times 10.5 = 1.9 \text{ kg/cm}^2 < 4.25 \text{ kg/cm}^2 \text{ O.K.}$$

D10-@200



$$W = 2.74 \text{ t/m}$$

$$\begin{cases} M = 1/12 \times 2.74 \times 4.2^2 = 4.03 \text{ t-m} \\ Q = 1/2 \times 2.74 \times 4.2 = 5.76 \text{ t} \end{cases}$$

< FG1 >

$$B \times D = 19 \times 75 \quad d = 67 \quad j = 58.63$$

$$A_t = 403/1.8 \times 58.63 = 3.82 \text{ cm}^2$$

$$\phi = 5760/21 \times 58.63 = 4.68 \text{ cm}$$

$$\tau = 5760/19 \times 58.63 = 5.17 > 4.25 \text{ NG}$$

2-D16

$$\Delta Q = 5.76 - 19 \times 58.63 \times 4.25 \times 10^{-3} = 1.03 \text{ t}$$

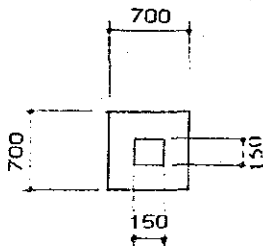
$$\Delta Q/bj = 0.92 \quad P_w = 0.31$$

$$D10 \quad x = 1.43/194 \times 0.0031 = 24.2 \text{ cm}$$

$$\therefore D10-@150$$

< F2 >

(C8)



$$N' = 9.8 \text{ t}$$

$$A = 9.8/28.5 = 0.34 \text{ m}^2 \quad 1 \times 1' = 0.7 \text{ m} \times 0.7 \text{ m}$$

$$N = 9.8 + 2.0 \times 0.7 \times 0.7 \times 0.75 = 10.54 \text{ t}$$

$$\sigma_c = 10.54 \text{ t} / 0.7 \text{ m} \times 0.7 \text{ m} = 21.6 \text{ t/m}^2 < 30.0 \text{ t/m}^2$$

$$l/a = 4.7$$

$$M = 0.37 \times 0.15 \times 9.8 = 0.55 \text{ t-m}$$

$$Q = 0.39 \times 9.8 = 3.83 \text{ t}$$

$$D = 25 \text{ cm} \quad d = 18 \text{ cm} \quad j = 15.75 \text{ cm}$$

$$A_t = 55 / 1.8 \times 15.75 = 1.94 \text{ cm}^2$$

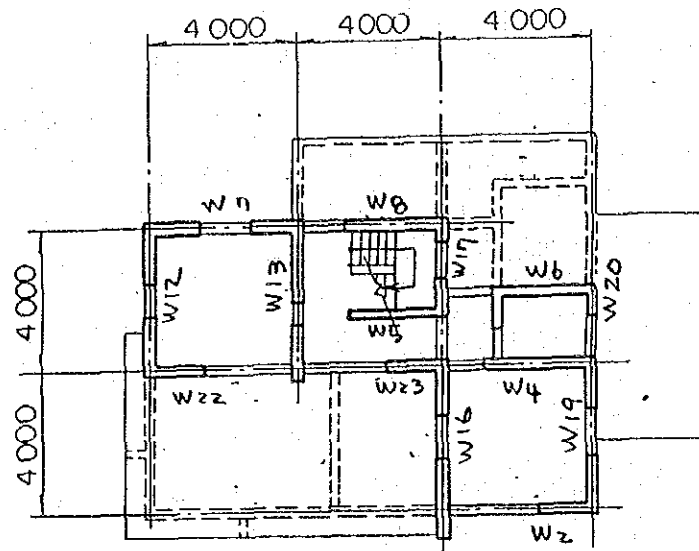
$$\phi = 3830 / 21 \times 15.75 = 11.58 \text{ cm}$$

$$\tau = 3830 / 65 \times 15.75 = 3.75 \text{ kg/cm}^2 < 4.25 \text{ kg/cm}^2 \text{ O.K.}$$

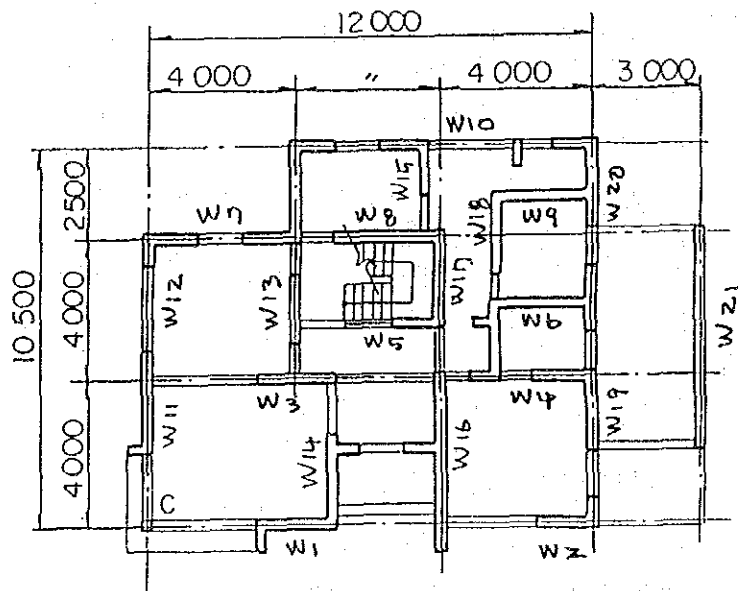
4-D10

3.5.3 Residence Type A

Framing Plan



1st FL PLAN



GROUND FL PLAN

1). Assumed Load

A : To floor
 B : To frame
 C : To seismic
 D.L : Dead load
 L.L : Live load
 T.L : Total load

1-1 Floor Load Table

Title	Material	Thick (cm)	Weight (kg/m ²)		D.L (kg/m ²)	L.L (kg/m ²)	T.L (kg/m ²)	Note
Roof	Concrete	60	140	A	570	90	660	() Balcony
	Water Proofing		20			(180)	(750)	
	Cement Mortar	15	30	B		70	640	
	Concrete Slab	150	360			(130)	(700)	
	Ceiling		20	C		30	600	
						(60)	(630)	
1st Floor	Terrazzo	150	80	A	460	180	640	
	Concrete Slab		360					
			20	B		130	590	
	Ceiling			C		60	520	
Stair	Terazzo	250	60	A	660	180	840	
	Concrete Slab		600					
				B		130	790	
				C		60	720	

1-2 Dead Load of Girder and Wall

Title	Size (cm)	Weight (kg/cm ²)
Girder	15 x 60	162 + 42 → 210
	15 x 40	90 + 26 → 120
	15 x 85	252 + 62 → 320
	15 x 45	108 + 30 → 140
	25 x 60	270 + 46 → 320
Column	15 x 15	54 + 24 → 80
Wall	W25	360 + 80 → 440
	CB15	200 + 80 → 280

2). Calculation of Axial Force of Columns

G : Girder
W : Wall
C : Column
B : Beam

No.	Floor	Title	Calculation					W (t)	ΣW (t)
			Load (t/m ² & t-m)	Area (m ²)	Length (m)	Length (m)	W' (t)		
C1	1F	Roof W(W15) G C	0.70 0.44 0.32 0.08	3.82	1.05 2.5 1.4	3.85	2.7 1.8 0.8 0.2	5.3	
	F	C W	0.08 0.44		1.4 1.3	2.5	0.2 1.5	1.7	7.0
W1	1F	Roof W(W15) G W(CB15)	0.70 0.44 0.32 0.28	10.14	1.05 5.0 1.1	5.0 2.0	7.1 2.4 1.6 0.7	11.8	
	F	W(CB15)	0.28		1.1	2.0	0.7	0.7	12.5
W2	2F	Roof W(W15) G W(CB15)	0.64 0.44 0.21 0.28	5.71	0.75 2.75 1.4	3.28 1.5	3.7 1.1 0.6 0.6	6.0	
	1F	1st Floor W(CB15) G W(CB15)	0.59 0.28 0.21 0.28	3.22	1.4 2.75 1.4	1.5 1.5	1.9 0.6 0.6 0.6	3.7	9.7
	F	W(CB15)	0.28		1.4	1.5	0.6	0.6	10.3
W3	1F	1st Floor Roof G W(CB15)	0.59 0.70 0.21 0.28	5.59 7.62	6.5 1.4	2.0	3.4 5.4 1.4 0.8	11.0	
	F	W(CB15)	0.28		1.4	2.0	0.8	0.8	11.8
W4	2F	Roof G W(CB15)	0.64 0.21 0.28	5.9	4.0 1.4	3.2	3.8 0.9 1.3	6.0	
	1F	1st Floor W(CB15) G W(CB15)	0.59 0.28 0.32 0.28	5.9	1.4 5.5 1.4	3.2 2.5	3.5 1.3 1.8 1.0	7.6	13.6
	F	W(CB15)	0.28		1.4	2.5	1.0	1.0	14.6
W5	1F	1st Floor G W(W15)	0.59 0.21 0.44	2.92	3.3 1.4	2.5	1.8 0.7 1.6	4.1	
	F	W(W15)	0.44		1.4	2.5	1.6	1.6	5.7

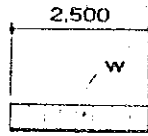
No.	Floor	Title	Calculation					W (t)	ΣW (t)
			Load (t/m ² & t-m)	Area (m ²)	Length (m)	Length (m)	W' (t)		
W6	2F	Roof W(W15) G W(CB15)	0.64 0.44 0.21 0.28	3.82	4.0 3.25 1.4	2.5	2.5 1.8 0.7 1.0	6.0	
	1F	Roof 1st Floor G W(CB15)	0.64 0.59 0.21 0.28	1.57 1.50	2.5 2.8	2.5	1.0 0.9 0.6 2.0	4.5	10.5
	F	W(CB15)	0.28		1.4	2.5	1.0	1.0	11.5
W7	2F	Roof W(W15) G W(CB15)	0.64 0.44 0.21 0.28	6.24	0.75 4.0 1.4	4.53 4.0	4.0 1.5 0.9 1.6	8.0	
	1F	1st Floor G W(CB15)	0.59 0.21 0.28	4.0	4.0 2.8	4.0	2.4 0.9 3.2	6.5	14.5
	F	W(CB15)	0.28		1.4	4.0	1.6	1.6	16.1
W8	2F	Roof W(W15) G W(CB15)	0.64 0.44 0.21 0.28	6.24	0.75 4.0 1.4	4.53 4.0	4.0 1.5 0.9 1.6	8.0	
	1F	Roof Stair G W(CB15) W(W15)	0.64 0.79 0.21 0.28 0.44	2.82 3.44	4.0 1.4 1.4	4.0 3.15	1.8 2.7 0.9 1.6 2.0	9.0	17.0
	F	W(W15)	0.44		1.4	3.15	2.0	2.0	19.0
W9	1F	Roof G W(CB15)	0.64 0.21 0.28	3.44	2.5 1.4	2.5	2.2 0.6 1.0	3.8	
	F	W(CB15)	0.28		1.4	2.5	1.0	1.0	4.8
W10	1F	Roof W(W15) G W(CB15)	0.64 0.44 0.21 0.28	5.64	0.2 8.0 1.4	8.0 8.0	3.6 0.7 1.7 3.2	9.2	
	F	W(CB15)	0.28		1.4	8.0	3.2	3.2	12.4
W11	1F	Roof W(W15) G W(CB15)	0.70 0.44 0.32 0.28	5.98	1.05 3.0 1.4	3.0 2.0	4.2 1.4 1.0 0.8	7.4	
	F	W(CB15)	0.28		1.4	2.0	0.8	0.8	8.2

No.	Floor	Title	Calculation					W (t)	ΣW (t)
			Load (t/m ² & t-m)	Area (m ²)	Length (m)	Length (m)	W' (t)		
W12	2F	Roof W(W15) G W(CB15)	0.64 0.44 0.21 0.28	6.38	0.75 4.0 1.4	5.05 4.0	4.4 1.7 0.9 1.6	8.6	
	1F	1st Floor Roof W(W15) G W(CB15)	0.59 0.70 0.44 0.21 0.28	4.0 0.83	1.05 4.0 2.8	1.83 4.0	2.4 0.6 0.9 0.9 3.2	8.0	16.6
	F	W(CB15)	0.28		1.4	4.0	1.6	1.6	18.2
W13	2F	Roof G W(CB15)	0.64 0.21 0.28	8.0	4.0 1.4	4.0	5.2 0.9 1.6	7.7	
	1F	1st Floor Roof W(W15) G W(CB15) "	0.59 0.64 0.44 0.21 0.28 0.28	6.61 1.57	0.2 7.2 1.4 1.4	2.5 4.0 4.5	3.9 1.0 0.3 1.6 1.6 1.8	10.2	17.9
	F	W(CB15)	0.28		1.4	4.5	1.8	1.8	19.7
W14	1F	Roof G W(CB15)	0.70 0.21 0.28	7.75	4.0 1.4	2.5	5.5 0.9 1.0	7.4	
	F	W(CB15)	0.28		1.4	2.5	1.0	1.0	8.4
W15	1F	Roof G W(CB15)	0.64 0.21 0.28	3.13	2.5 1.4	2.5	2.0 0.6 1.0	3.6	
	F	W(CB15)	0.28		1.4	2.5	1.0	1.0	4.6
W16	2F	Roof W(W15) G W(CB15)	0.64 0.44 0.21 0.28	5.82	0.4 4.9 1.2	4.9 4.9	3.8 0.9 1.1 1.7	7.5	
	1F	Roof 1st Floor G W(CB15)	0.70 0.59 0.21 0.28	4.99 4.72	4.9 2.4	4.9	3.5 2.8 1.1 3.3	10.7	18.2
	F	W(CB15)	0.28		1.2	4.9	1.7	1.7	19.9

No.	Floor	Title	Calculation					W (t)	ΣW (t)
			Load (t/m ² & t-m)	Area (m ²)	Length (m)	Length (m)	W' (t)		
W17	2F	Roof W(W15) G W(CB15)	0.64 0.44 0.21 0.28	4.94	2.1 4.0 1.2	4.0 2.5	3.2 3.7 0.9 0.9	8.7	
	1F	Roof 1st Floor G W(CB15)	0.64 0.59 0.21 0.28	5.41 3.35	6.5 2.4	2.5	3.5 2.0 1.4 1.7	8.6	17.3
	F	W(CB15)	0.28		1.2	2.5	0.9	0.9	18.2
W18	2F	Roof G W(CB15)	0.64 0.21 0.28	1.94	2.0 1.2	2.0	1.3 0.5 0.7	2.5	
	1F	Roof 1st Floor G W(CB15) W(CB15)	0.64 0.59 0.21 0.28 0.28	5.16 2.22	5.0 1.2 1.2	2.0 5.0	3.3 1.3 1.1 0.7 1.7	8.1	10.6
	F	W(CB15)	0.28		1.2	5.0	1.7	1.7	12.3
W19	2F	Roof W(W15) G W(CB15)	0.64 0.44 0.21 0.28	6.32	0.75 4.0 1.2	4.83 4.0	4.1 1.6 0.9 1.4	8.0	
	1F	1st Floor Roof G W(CB15)	0.59 0.64 0.21 0.28	4.0 3.0	4.0 2.4	4.0	2.4 2.0 0.9 2.7	8.0	16.0
	F	W(CB15)	0.28		1.2	4.0	1.4	1.4	17.4
W20	2F	Roof W(W15) G W(CB15)	0.64 0.44 0.21 0.28	2.19	0.75 2.0 1.2	2.53 2.0	1.4 0.9 0.5 0.7	3.5	
	1F	1st Floor Roof W(W15) G W(CB15) W(CB15)	0.59 0.64 0.44 0.21 0.28 0.28	1.0 8.75	0.2 6.5 1.2 1.2	4.5 2.0 6.5	0.6 5.6 0.4 1.4 0.7 2.2	10.9	14.4
	F	W(CB15)	0.28		1.2	6.5	2.2	2.2	16.6

No.	Floor	Title	Calculation					W (t)	ΣW (t)
			Load (t/m ² & t-m)	Area (m ²)	Length (m)	Length (m)	W' (t)		
W21	1F	Roof W(W15) G W(CB15)	0.64 0.44 0.21 0.28	9.0	0.2 6.0 1.2	9.0 6.0	5.8 0.8 1.9 2.0	10.5	
	F	W(CB15)	0.28		1.2	6.0	2.0	2.0	12.5
W22	2F	Roof W(W15) G	0.64 0.44 0.21	6.24	0.75 4.0	4.53	4.0 1.5 0.9	9.0	9.0
		W(W15) W(CB15)	0.44 0.28		0.9 2.4	4.0 1.5	1.6 1.0		
W23	2F	Roof W(W15) G	0.64 0.44 0.21	6.1	0.75 4.0	4.0	3.9 1.4 0.9	9.9	9.9
		W(W15) W(CB15)	0.44 0.28		1.5 2.4	4.0 1.5	2.7 1.0		

3). Design of Girder and Beam



<G1>

$$W = 0.21 \text{ t/m} + 0.64 \text{ t/m}^2 \times 2.88 \text{ m}^2 / 2.5 \text{ m} + 0.64 \text{ t/m}^2 \times 5.25 \text{ m} + 0.44 \text{ t/m}^2 \times 0.75 \text{ m} = 1.61 \text{ t/m}$$

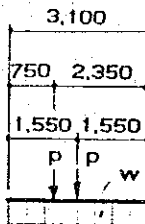
$$\begin{cases} C = 1/12 \times 1.61 \times 2.5^2 = 0.84 \text{ t-m} \\ Q = 1/2 \times 1.61 \times 2.5 = 2.02 \text{ t} \end{cases}$$

$$B \times D = 15 \times 60 \quad d = 55 \quad j = 48.13$$

$$A_t = 84 / 1.8 \times 48.13 = 0.97 \text{ cm}^2$$

$$\phi = 2020 / 14 \times 48.13 = 3.00 \text{ cm}$$

$$\tau = 2020 / 15 \times 48.13 = 2.8 \text{ kg/cm}^2 < 4.25 \text{ kg/cm}^2 \text{ O.K}$$



$$W = 0.32 \text{ t/m}$$

$$P_1 = 9.0 \text{ t}$$

$$P_2 = 0.59 \text{ t/m}^2 \times 3.59 \text{ m}^2 + 0.70 \text{ t/m}^2 \times 4.19 \text{ m}^2 = 5.05 \text{ t}$$

$$\begin{cases} Q_a = 1/2 \times 0.32 \times 3.1 + \frac{9.0 \times 2.35}{3.1} + 1/2 \times 5.05 = 9.84 \text{ t} \\ Q_b = 1/2 \times 0.32 \times 3.1 + \frac{9.0 \times 0.75}{3.1} + 1/2 \times 5.05 = 5.20 \text{ t} \\ M = 1/8 \times 0.32 \times 3.1^2 + 2.18 \times 1.55 + 1/4 \times 5.05 \times 3.1 = 7.68 \text{ t-m} \end{cases}$$

<B2B>

$$B \times D = 30 \times 60 \quad d = 55 \quad j = 48.13$$

$$\text{End } \phi = 9840 / 14 \times 48.13 = 14.60 \quad 3\text{-D19}$$

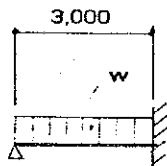
$$\tau = 9840 / 30 \times 48.13 = 6.81 > 4.25 \text{ NG}$$

$$\Delta Q = 9.84 \text{ t} - 6.14 \text{ t} = 3.7 \text{ t}$$

$$\Delta Q / b_j = 3700 / 30 \times 48.13 = 2.6 \quad P_w = 0.50$$

$$D_{13} \quad x = 2.54 / 30 \times 0.0050 = 16.9 \text{ cm} \quad D_{13}\text{-@150}$$

$$\text{Center } A_t = 768 / 1.8 \times 48.13 = 8.86 \quad 4\text{-D19}$$



$$W = 0.32 \text{ t/m}^2 + 0.70 \text{ t/m}^2 \times 0.525 \text{ m} + 0.44 \text{ t/m}^2 \times 1.05 \text{ m} + 0.70 \text{ t/m}^2 \times 1.0 \text{ m} = 1.85 \text{ t/m}$$

$$\begin{cases} M = 1/8 \times 1.85 \times 3.0^2 = 2.09 \text{ t-m} \\ Q = 5/8 \times 1.85 \times 3.0 = 3.47 \text{ t} \end{cases}$$

<G2>

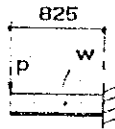
$$B \times D = 25 \times 60 \quad d = 55 \quad j = 48.13$$

$$A_t = 209 / 1.8 \times 48.13 = 2.41 \text{ cm}^2$$

$$\phi = 3470 / 14 \times 48.13 = 5.15 \text{ cm}$$

$$\tau = 3470 / 25 \times 48.13 = 2.88 \text{ kg/cm}^2 < 4.25 \text{ kg/cm}^2$$

2-D16



$$W = 0.75 \text{ t/m}$$

$$P = 0.44 \times 1.05 = 0.46 \text{ t}$$

$$\left[\begin{array}{l} M = 1/2 \times 0.75 \times 0.825^2 + 0.46 \times 0.825 = 0.64 \text{ t-m} \\ Q = 0.75 \times 0.825 + 0.46 = 1.08 \text{ t} \end{array} \right.$$

CS1

$$D = 15 \text{ cm} \quad d = 12 \text{ cm} \quad j = 10.5 \text{ cm}$$

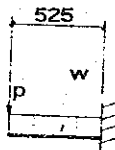
$$A_t = 64 \text{ t-cm} / 1.8 \times 10.5 = 3.39 \text{ cm}^2$$

$$x = \frac{0.99 \times 100}{3.39} = 29.2 \text{ cm}$$

$$\phi = 1080 / 21.0 \times 10.5 = 7.35 \text{ cm}$$

$$x = \frac{3.5 \times 100}{7.35} = 47.6 \text{ cm}$$

∴ D10 & 13-
@200



$$W = 0.66 \text{ t/m}$$

$$P = 0.44 \times 0.75 = 0.33 \text{ t}$$

$$\left[\begin{array}{l} M = 1/2 \times 0.66 \times 0.525^2 + 0.33 \times 0.525 = 0.27 \text{ t-m} \\ Q = 0.66 \times 0.525 + 0.33 = 0.68 \text{ t} \end{array} \right.$$

CS2

$$D = 15 \text{ cm} \quad d = 12 \text{ cm} \quad j = 10.5 \text{ cm}$$

$$A_t = 27 / 1.8 \times 10.5 = 1.43 \text{ cm}^2$$

$$x = \frac{0.71 \times 100}{1.43} = 49.6 \text{ cm}$$

$$\phi = 680 / 21.0 \times 10.5 = 4.63 \text{ cm}$$

$$x = \frac{3.0 \times 100}{4.63} = 64.7 \text{ cm}$$

∴ D10-
@200

4). Design of Slab

		Lx(m)	Ly(m)	t(Cm)	w(t/m2)
D10,D13	S01	4.0	4.0	15.0	0.660
	S02	4.0	5.0	15.0	0.750
	S03	4.0	4.0	15.0	0.640

		Lx(m)	Ly(m)	t(Cm)	w(t/m2)	/
D10,D13	S01	4.0	4.0	15.0	0.660	
		LAMBDA= 1.00		wLx2(t*m)= 10.560		ft(kg/cm2)=2000.0

		ALPHA	M(t*m/m2)	at(Cm2/m)	D10	D10&D13	D13
X-E	-0.042	-0.440	2.10	@33.9	@47.3	@60.6) D10,13-@200
X-C	0.028	0.293	1.40	@50.8	@70.9	@90.9	
Y-E	-0.042	-0.440	2.29	@31.1	@43.3	@55.6) D10,13-@200
Y-C	0.028	0.293	1.52	@46.6	@65.0	@83.3	

		Lx(m)	Ly(m)	t(Cm)	w(t/m2)	/
S02		4.0	5.0	15.0	0.750	
		LAMBDA= 1.25		wLx2(t*m)= 12.000		ft(kg/cm2)=2000.0

		ALPHA	M(t*m/m2)	at(Cm2/m)	D10	D10&D13	D13
X-E	-0.059	-0.709	3.38	@21.0	@29.3	@37.6) D10,13-@200
X-C	0.039	0.473	2.25	@31.5	@44.0	@56.4	
Y-E	-0.042	-0.500	2.60	@27.3	@38.1	@48.9) D10,13-@200
Y-C	0.028	0.333	1.73	@41.0	@57.2	@73.3	

		Lx(m)	Ly(m)	t(Cm)	w(t/m2)	/
S03		4.0	4.0	15.0	0.640	
		LAMBDA= 1.00		wLx2(t*m)= 10.240		ft(kg/cm2)=2000.0

		ALPHA	M(t*m/m2)	at(Cm2/m)	D10	D10&D13	D13
X-E	-0.042	-0.427	2.03	@34.9	@48.7	@62.5) D10,13-@200
X-C	0.028	0.284	1.35	@52.4	@73.1	@93.8	
Y-E	-0.042	-0.427	2.22	@32.0	@44.7	@57.3) D10,13-@200
Y-C	0.028	0.284	1.48	@48.0	@67.0	@85.9	

5). Design of Stair



$$W = 0.84 \text{ t/m}^2 \times 0.25 \text{ m} = 0.21 \text{ t/m}$$

$$\left[\begin{array}{l} M = \frac{1}{2} \times 0.21 \times 1.25^2 = 0.17 \text{ t-m} \\ Q = 0.21 \times 1.25 = 0.27 \text{ t} \end{array} \right.$$

$$D = 25 \text{ cm} \quad d = 20 \text{ cm} \quad j = 17.5 \text{ cm}$$

$$A_t = \frac{17}{1.8 \times 17.5} = 0.54 \text{ cm}^2$$

$$\phi = \frac{270}{21.0 \times 17.5} = 0.74 \text{ cm}$$

1-D13

6). Design of Foundation

Allowable bearing capacity

$f_e = 30 \text{ t/m}^2$ (Permanent)

Dead load $2.4 \text{ t/m}^3 \times 0.19 \text{ m} \times 0.75 \text{ m} = 0.35 \text{ t/m}$
 $2.0 \text{ t/m}^3 \times (1.0 - 0.19 \text{ m}) \times 0.6 \text{ m} = 0.98 \text{ t/m}$ } 1.33 t/m

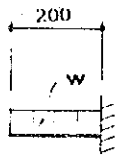
W : Wall C : Column

No.	LF (m)	N (t)	$P' = N/LF$ (t/m)	P (t/m)	No.	LF (m)	N (t)	$P' = N/LF$ (t/m)	P (t/m)
W1	3.5	12.5	3.58	4.91	C1	2.5	7.0	2.8	4.13
W2	2.75	10.3	3.75	5.08					
W3	5.0	11.8	2.36	3.69					
W4	5.5	14.6	2.66	3.99					
W5	3.6	5.7	1.59	2.92					
W6	2.1	11.5	5.48	6.81					
W7	3.6	16.1	4.47	5.80					
W8	3.6	19.0	5.28	6.61					
W9	2.1	4.8	2.29	3.62					
W10	7.6	12.4	1.63	2.96					
W11+ W12+ W22	7.10	8.2+18.2 +9.0= 35.4	5.06	6.39					
W13	5.7	19.7	3.46	4.79					
W14	3.6	8.4	2.34	3.67					
W15	2.1	4.6	2.19	3.52					
W16+ W23	4.0	19.9+9.9 =29.8	7.45	8.78					
W17	3.6	18.2	5.06	6.39					
W18	4.6	12.3	2.68	4.01					
W19	4.0	17.4	4.35	5.68					
W20	5.6	16.6	2.97	4.30					
W21	5.5	12.5	2.28	3.61					

No.	$L' = \frac{P}{f_c}$ (m)	L (i)	$\sigma_c = \frac{P}{L}$ (t/m)	P'' (t/m) (P+0.35)	$\sigma_c' = \frac{P''}{L}$
W1	0.17	0.40			
W2	0.17	"			
W3	0.13	"			
W4	0.14	"			
W5	0.10	"			
W6	0.23	"			
W7	0.20	"			
W8	0.22	"			
W9	0.12	"			
W10	0.10	"			
W11+W12+ W22	0.22	"			
W13	0.16	"			
W14	0.13	"			
W15	0.12	"			
W16+W23	0.30	"	21.95 t/m ² < 30 t/m ²	7.80	19.5
W17	0.22	"			
W18	0.14	"			
W19	0.19	"			
W20	0.14	"			
W21	0.12				
C1	0.14	0.40			

<F1A>

$$W = 19.5$$



$$\begin{cases} M = 1/2 \times 19.5 \times 0.2^2 = 0.39 \text{ t-m} \\ Q = 19.5 \times 0.2 = 3.9 \text{ t/m} \end{cases}$$

$$D = 18 \text{ cm} \quad d = 12 \text{ cm} \quad j = 10.5 \text{ cm}$$

$$A_t = 39/11.8 \times 10.5 = 2.06 \text{ cm}^2$$

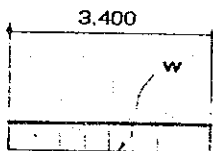
$$x = \frac{0.71 \times 100}{2.06} = 34.4 \text{ cm}$$

$$\phi = 3900/21 \times 10.5 = 17.69 \text{ cm}$$

$$x = \frac{3.0 \times 100}{17.69} = 16.95$$

∴ D10-@150

$$\tau = 3900/100 \times 10.5 = 3.7 \text{ kg/cm}^2 < 4.25 \text{ kg/cm}^2$$



$$W = 3.58$$

$$\begin{cases} M = 1/12 \times 3.58 \times 3.4^2 = 3.45 \text{ t-m} \\ Q = 1/2 \times 3.58 \times 3.4 = 6.09 \text{ t} \end{cases}$$

<FG1>

$$B \times D = 19 \times 75 \quad d = 67 \quad j = 58.63$$

$$A_t = 345/1.8 \times 58.63 = 3.27 \text{ cm}^2$$

$$\phi = 6090/21 \times 58.63 = 4.95 \text{ cm}$$

$$\tau = 6090/19 \times 58.63 = 5.47 \text{ kg/cm}^2 > 4.25 \text{ kg/cm}^2 \text{ NG}$$

$$\Delta Q = 6.09 \text{ t} - 19 \times 58.63 \times 4.25 \times 10^{-3} = 1.36 \text{ t}$$

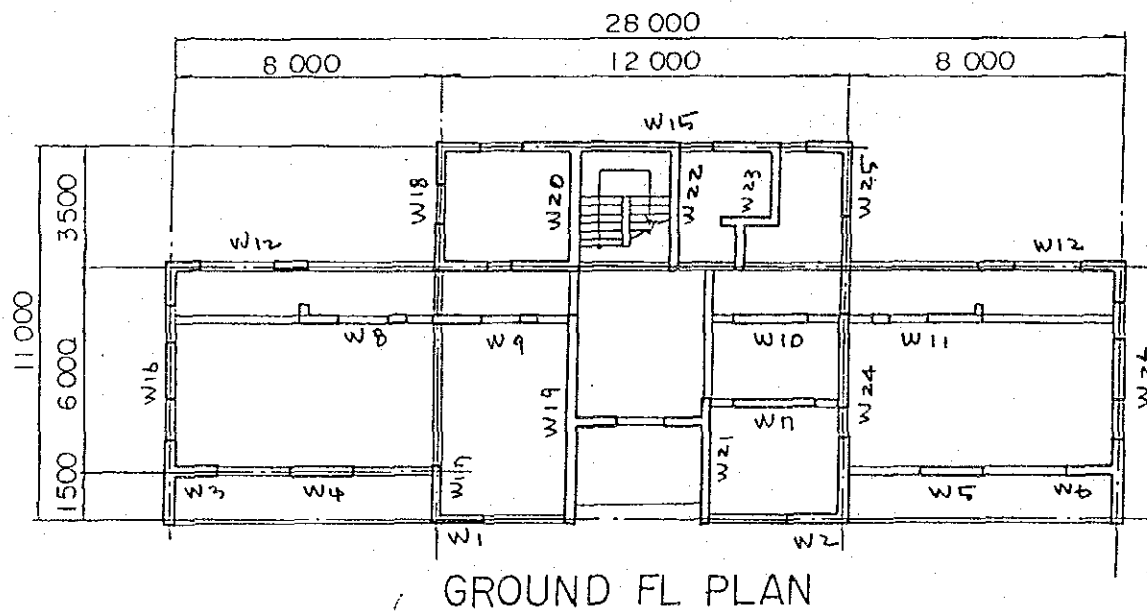
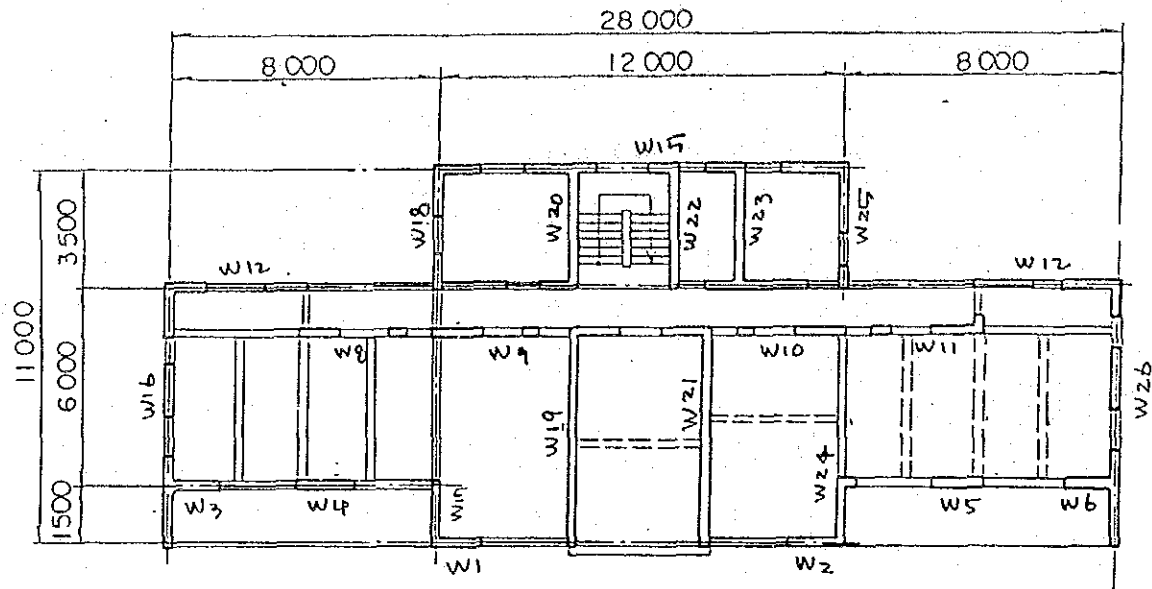
$$\Delta Q/bj = 1.3 \quad Pw = 0.35$$

$$D10 \quad x = 1.43/19 \times 0.0035 = 21.5 \text{ cm}$$

∴ D10-@150

3.5.4 Engineer's Office

Framing Plan



1). Assumed Load

A : To floor
 B : To frame
 C : To seismic
 D.L : Dead load
 L.L : Live load
 T.L : Total load

1-1 Floor Load Table

Title	Material	Thick (cm)	Weight (kg/m ²)		D.L (kg/m ²)	L.L (kg/m ²)	T.L (kg/m ²)	Note
Roof	Concrete Water Proofing Cement Mortar Concrete Slab Ceiling	60	140	A	570	90	660	
		15	20	B		70	640	
		150	30	C		30	600	
			360			20		
1st Floor	Terrazzo Concrete Slab Ceiling	150	80	A	460	300	760	
			360	B		180	640	
			20	C		80	540	
Stair	Terazzo Concrete Slab	250	60	A	660	300	960	
			600	B		180	960	
				C		180	840	

1-2 Dead Load of Girder and Wall

	Title	Size (cm)	Weight (kg/cm ²)
	Girder	15 x 60	162 + 42 → 210
		15 x 40	90 + 26 → 120
		15 x 85	252 + 62 → 320
		15 x 45	108 + 30 → 140
		25 x 60	270 + 46 → 320
	Beam	30 x 60	324 + 48 → 370
	Column	15 x 15	54 + 24 → 80
	Wall	W25	360 + 80 → 440
		CB15	200 + 80 → 280

2). Calculation of Axial Force of Columns

G : Girder
W : Wall
C : Column
B : Beam

No.	Floor	Title	Calculation					W (t)	ΣW (t)
			Load (t/m ² & t.m)	Area (m ²)	Length (m)	Length (m)	W' (t)		
W1	2F	Roof W(W15) G W(CB15)	0.64 0.44 0.32 0.28	3.22	0.9 2.75 1.2	2.75 1.5	2.1 1.1 0.9 0.5	4.6	
	1F	W(CB15) 1st Floor G W(CB15)	0.28 0.64 0.32 0.28	3.22	0.9 2.75 2.4	1.25 1.5	0.4 2.1 0.9 1.0	4.4	9.0
	F	W(CB15) "	0.28 0.28		1.2 0.9	1.5 1.25	0.5 0.4	0.9	9.9
W2	2F	Roof W(W15) G W(CB15)	0.64 0.44 0.32 0.28	3.22	0.6 2.75 1.2	2.75 1.5	2.1 0.8 0.9 0.5	4.3	
	1F	W(CB15) 1st Floor G W(CB15)	0.28 0.64 0.32 0.28	3.94	0.9 2.75 2.4	1.25 1.5	0.4 2.6 0.9 1.0	4.9	9.2
	F	W(CB15) "	0.28 0.28		1.2 0.9	1.5 1.25	0.5 0.4	0.9	10.1
W3 W6	2F	W(W15) Roof G W(CB15)	0.44 0.64 0.32 0.28	6.4	0.9 2.75 1.2	2.75 1.5	1.1 4.1 0.9 0.5	6.6	
	1F	W(W15) 1st Floor G W(CB15)	0.44 0.64 0.32 0.28	6.4	1.2 2.75 2.4	1.25 1.5	0.7 4.1 0.9 1.0	6.7	13.3
	F	W(CB15)	0.28		1.2	1.5	0.5	0.5	13.8
W4 W5	2F	W(W15) Roof G B W(CB15)	0.44 0.64 0.32 0.37 0.28	13.72	0.9 4.0 4.5 1.2	4.0 1.5	1.6 8.8 1.3 1.7 0.5	13.9	
	1F	W(W15) 1st Floor G B W(CB15)	0.44 0.64 0.32 0.37 0.28	13.72	1.2 4.0 4.5 2.4	4.0 1.5	2.2 8.8 1.3 1.7 1.0	15.0	28.9
	F	W(CB15)	0.28		1.2	1.5	0.5	0.5	29.4

No.	Floor	Title	Calculation					W (t)	ΣW (t)
			Load (t/m ² & t-m)	Area (m ²)	Length (m)	Length (m)	W' (t)		
W7	1F	1st Floor G W(CB15)	0.64 0.32 0.28	6.98	3.1 1.2	2.1	4.5 1.0 0.7	6.2	
	F	W(CB15)	0.28		1.2	2.1	0.7	0.7	6.9
W8	2F	Roof G B W(CB15)	0.64 0.32 0.37 0.28	14.72	6.0 6.75 1.2	2.4	9.5 2.0 2.5 0.8	14.8	
	1F	1st Floor G B W(CB15)	0.64 0.32 0.37 0.28	14.72	6.0 6.75 2.4	2.4	9.5 2.0 2.5 1.6	15.6	30.4
	F	W(CB15)	0.28		1.2	2.4	0.8	0.8	31.2
W9	2F	Roof G W(CB15)	0.64 0.32 0.28	11.28	7.0 1.2	2.0	7.3 2.3 0.7	10.3	
	1F	1st Floor G W(CB15)	0.64 0.32 0.28	11.28	7.0 2.4	2.0	7.3 2.3 1.4	11.0	21.3
	F	W(CB15)	0.28		1.2	2.0	0.7	0.7	22.0
W10	2F	Roof G W(CB15)	0.64 0.32 0.28	8.94	7.0 1.2	2.0	5.8 2.3 0.7	8.8	
	1F	1st Floor G W(CB15) "	0.64 0.32 0.28 0.28	6.44	4.0 1.2 1.2	2.0 2.2	4.2 1.3 0.7 0.8	7.0	15.8
	F	W(CB15)	0.28		1.2	2.2	0.8	0.8	16.6
W11	2F	Roof G B W(CB15)	0.64 0.32 0.37 0.28	16.5	6.0 6.38 1.2	2.4	10.6 2.0 2.4 0.8	15.8	
	1F	1st Floor G B W(CB15)	0.64 0.32 0.37 0.28	16.5	6.0 6.38 2.4	2.4	10.6 2.0 2.4 1.6	16.6	32.4
	F	W(CB15)	0.28		1.2	2.4	0.8	0.8	33.2

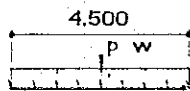
No.	Floor	Title	Calculation					W (t)	ΣW (t)
			Load (t/m ² & t·m)	Area (m ²)	Length (m)	Length (m)	W' (t)		
W12	2F	Roof W(W15) G W(CB15)	0.64 0.44 0.21 0.28	4.22	0.6 6.0 1.2	6.0 1.7	2.7 1.6 1.3 0.6	6.2	
	1F	W(W15) W(CB15) 1st Floor G W(CB15)	0.44 0.28 0.64 0.21 0.28	4.22	0.9 0.9 6.0 2.4	2.0 2.4 1.7	0.8 0.6 2.7 1.3 1.2	6.6	12.8
	F	W(W15) W(CB15) "	0.44 0.28 0.28		0.9 0.9 1.2	2.0 2.4 1.7	0.8 0.6 0.6	2.0	14.8
W13	2F	Roof W(W15) G W(CB15)	0.64 0.44 0.21 0.28	9.57	0.6 7.5 1.2	2.0 3.2	6.2 0.6 1.6 1.1	9.5	
	1F	W(W15) 1st Floor G W(CB15)	0.44 0.64 0.21 0.28	9.57	0.9 7.5 2.4	2.0 3.2	0.8 6.2 1.6 2.2	10.8	20.3
	F	W(W15) W(CB15)	0.44 0.28		0.9 1.2	2.0 3.2	0.8 1.1	1.9	22.2
W14	2F	Roof W(W15) G W(CB15)	0.64 0.44 0.21 0.28	9.63	0.6 8.5 1.2	2.0 3.2	6.2 0.6 1.8 1.1	9.7	
	1F	W(W15) 1st Floor G W(CB15)	0.44 0.64 0.21 0.28	9.63	0.9 8.5 2.4	2.0 3.2	0.8 6.2 1.8 2.2	11.0	20.7
	F	W(W15) W(CB15)	0.44 0.28		0.9 1.2	2.0 3.2	0.8 1.1	1.9	22.6
W15	2F	W(W15) Roof G W(CB15)	0.44 0.64 0.21 0.28	9.44	0.6 12.0 1.2	12.0 12.0	3.2 6.1 2.6 4.1	16.0	
	1F	1st Floor G W(CB15)	0.64 0.21 0.28	9.44	12.0 2.4	12.0	6.1 2.6 8.2	16.9	32.9
	F	W(CB15)	0.28		1.2	12.0	4.1	4.1	37.0

No.	Floor	Title	Calculation					W (t)	ΣW (t)
			Load (t/m ² & t·m)	Area (m ²)	Length (m)	Length (m)	W' (t)		
W16	2F	W(W15) Roof G W(CB15)	0.44 0.64 0.32 0.28	5.19	0.6 7.5 1.2	9.0 6.5	5.4 3.4 2.4 2.2	13.4	
	1F	W(W15) 1st Floor G W(CB15)	0.44 0.64 0.32 0.28	5.19	0.9 7.5 2.4	1.5 6.5	0.6 3.4 2.4 4.4	10.8	24.2
	F	W(CB15)	0.28		1.2	6.5	2.2	2.2	26.4
W17	2F	W(W15) Roof G W(CB15)	0.44 0.64 0.32 0.28	9.85	0.6 5.0 1.2	5.0 1.5	1.4 6.3 1.6 0.5	9.8	
	1F	W(W15) 1st Floor G W(CB15)	0.44 0.64 0.32 0.28	9.85	0.9 5.0 2.4	1.25 1.5	0.5 6.3 1.6 1.0	9.4	19.2
	F	W(CB15)	0.28		1.2	1.5	0.5	0.5	19.7
W18	2F	W(W15) Roof G W(CB15)	0.44 0.64 0.32 0.28	3.06	0.6 3.5 1.2	3.5 3.5	1.0 2.0 0.8 1.2	5.0	
	1F	1st Floor G W(CB15)	0.64 0.21 0.28	3.06	3.5 2.4	 3.5	2.0 0.8 2.4	5.2	10.2
	F	W(CB15)	0.28		1.2	3.5	1.2	1.2	11.4
W19	2F	W(W15) Roof G W(CB15)	0.44 0.64 0.32 0.28	18.78	0.6 9.25 1.2	3.25 6.0	0.9 12.0 3.0 2.0	17.9	
	1F	W(CB15) 1st Floor G W(CB15) W(W15)	0.28 0.64 0.32 0.28 0.44	20.58	0.9 9.25 2.4 1.2	3.25 6.0 2.9	0.9 13.2 3.0 4.0 1.5	22.6	40.5
	F	W(CB15) W(CB15)	0.28 0.28		1.2 0.9	6.0 1.25	2.0 0.4	2.4	42.9

No.	Floor	Title	Calculation					W (t)	ΣW (t)
			Load (t/m ² & t-m)	Area (m ²)	Length (m)	Length (m)	W' (t)		
W20	2F	Roof G W(W15)	0.64 0.21 0.44	7.19	3.5 1.2	3.5	4.6 0.8 1.9	7.3	
	1F	1st Floor Stair G W(W15)	0.64 0.84 0.21 0.44	3.06 4.13	3.5 2.4	3.5	2.0 3.5 0.8 3.8	10.1	17.4
	F	W(W15)	0.44		1.2	3.5	1.9	1.9	19.3
W21	2F	Roof W(W15) G W(CB15)	0.64 0.44 0.32 0.28	18.78	0.6 9.25 1.2	3.25 6.0	12.0 0.9 3.0 2.0	17.9	
	1F	W(CB15) 1st Floor G W(CB15) W(W15) W(CB15)	0.28 0.64 0.32 0.28 0.44 0.28	17.4	0.9 9.7 1.2 1.2 1.2	1.25 6.0 2.9 3.75	0.4 11.2 3.1 2.0 1.5 1.3	19.5	37.4
	F	W(CB15) "	0.28 0.28		1.2 0.9	3.75 1.25	1.3 0.4	1.7	39.1
W22	2F	Roof G W(CB15)	0.64 0.21 0.28	6.63	3.5 1.2	3.5	4.3 0.8 1.2	6.3	
	1F	1st Floor Stair G W(CB15) W(W15)	0.64 0.84 0.21 0.28 0.44	2.5 4.13	3.5 1.2 1.2	3.5 3.5	1.6 3.5 0.8 1.2 1.9	9.0	15.3
	F	W(W15)	0.44		1.2	3.5	1.9	1.9	17.2
W23	2F	Roof G W(CB15)	0.64 0.21 0.28	5.5	3.5 1.2	3.5	3.6 0.8 1.2	5.6	
	1F	1st Floor G W(CB15) "	0.64 0.21 0.28 0.28	5.5	3.5 1.2 1.2	3.5 5.0	3.6 0.8 1.2 1.7	7.3	12.9
	F	W(CB15)	0.28		1.2	5.0	1.7	1.7	14.6

No.	Floor	Title	Calculation					W (t)	ΣW (t)
			Load (t/m ² & t-m)	Area (m ²)	Length (m)	Length (m)	W' (t)		
W24	2F	W(W15) Roof G W(CB15)	0.44 0.64 0.32 0.28	7.72	0.6 5.0 1.2	3.75 1.6	1.0 5.0 1.6 0.6	8.2	
	1F	1st Floor G W(CB15) "	0.64 0.32 0.28 0.28	9.04	8.15 1.2 1.2	 1.6 5.0	5.8 2.6 0.6 1.7	10.7	18.9
	F	W(CB15)	0.28		1.2	5.0	1.7	1.7	20.6
W25	2F	W(W15) Roof G W(CB15)	0.44 0.64 0.21 0.28	3.0	0.6 3.5 1.2	3.5 3.5	1.0 2.0 0.8 1.2	5.0	
	1F	1st Floor G W(CB15)	0.64 0.21 0.28	3.0	3.5 2.4	 3.5	2.0 0.8 2.4	5.2	10.2
	F	W(CB15)	0.28		1.2	3.5	1.2	1.2	11.4
W26	2F	W(W15) Roof G B W(CB15)	0.44 0.64 0.32 0.37 0.28	9.16	0.6 9.5 1.13 1.2	9.0 7.5	2.4 5.9 3.1 0.5 2.6	14.5	
	1F	W(W15) 1st Floor G B W(CB15)	0.44 0.64 0.32 0.37 0.28	9.16	0.9 9.5 1.13 2.4	1.5 7.5	0.6 5.9 3.1 0.5 5.2	15.3	29.8
	F	W(CB15)	0.28		1.2	7.5	2.6	2.6	32.4

3). Design of Girder and Beam



<B1>

$$W = 0.37 \text{ t/m}$$

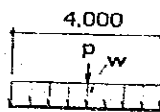
$$P = 0.64 \times 3.5 \times 2 = 4.48 \text{ t}$$

$$\begin{aligned} \left[\begin{aligned} M_o &= 1/8 \times 0.37 \times 4.5^2 + 1/4 \times 4.48 \times 4.5 = 5.98 \text{ t-m} \\ Q &= 1/2 \times 0.37 \times 4.5 + 1/2 \times 4.48 = 3.08 \text{ t} \end{aligned} \right. \end{aligned}$$

$$B \times D = 30 \text{ cm} \times 60 \text{ cm} \quad d = 55 \text{ cm} \quad j = 48.13 \text{ cm}$$

$$\begin{aligned} \text{End} \quad \phi &= 3080/14 \times 48.13 = 4.57 \text{ cm} \quad 3\text{-D19} \\ \tau &= 3080/30 \times 48.13 = 2.14 \text{ kg/cm}^2 < 4.25 \text{ kg/cm}^2 \text{ O.K.} \end{aligned}$$

$$\text{Center} \quad A_t = 598/1.8 \times 48.13 = 6.91 \text{ cm}^2 \quad 5\text{-D19}$$



<G2A>

$$W = 0.32 + 0.64 \times 0.75 = 0.80 \text{ t/m}$$

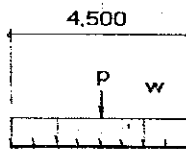
$$P = 3.08 \text{ t}$$

$$\begin{aligned} \left[\begin{aligned} M_o &= 1/8 \times 0.80 \times 4.0^2 + 1/4 \times 3.08 \times 4.0 = 4.68 \text{ t-m} \\ Q &= 1/2 \times 0.80 \times 4.0 + 1/2 \times 3.08 = 3.14 \text{ t} \end{aligned} \right. \end{aligned}$$

$$B \times D = 25 \text{ cm} \times 60 \text{ cm} \quad d = 55 \text{ cm} \quad j = 48.13 \text{ cm}$$

$$\begin{aligned} \text{End} \quad \phi &= 3140/14 \times 48.13 = 4.66 \text{ cm} \quad 3\text{-D16} \\ \tau &= 3140/25 \times 48.13 = 2.6 \text{ kg/cm}^2 < 4.25 \text{ kg/cm}^2 \text{ O.K.} \end{aligned}$$

$$\text{Center} \quad A_t = 468/1.8 \times 48.13 = 5.140 \text{ cm}^2 \quad 3\text{-D16}$$



<G2A>

$$W = 0.32 \text{ t/m}$$

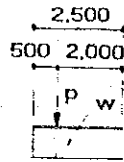
$$P = 0.64 \text{ t/m}^2 \times 10.37 \text{ m}^2 = 6.64 \text{ t}$$

$$\begin{aligned} \left[\begin{aligned} C &= 1/12 \times 0.32 \times 4.5^2 + 1/8 \times 6.64 \times 4.5 = 4.28 \text{ t-m} \\ M_o &= 1/8 \times 0.32 \times 4.5^2 + 1/4 \times 6.64 \times 4.5 = 8.28 \text{ t-m} \\ Q &= 1/2 \times 0.32 \times 4.5 + 1/2 \times 6.64 = 4.04 \text{ t} \end{aligned} \right. \end{aligned}$$

$$B \times D = 25 \text{ cm} \times 60 \text{ cm} \quad d = 55 \text{ cm} \quad j = 48.13 \text{ cm}$$

$$\begin{aligned} \text{End} \quad \phi &= 4040/14 \times 48.13 = 6.0 \text{ cm} \quad 3\text{-D16} \\ \tau &= 4040/25 \times 48.13 = 3.4 \text{ kg/cm}^2 < 4.25 \text{ kg/cm}^2 \text{ O.K.} \\ A_t &= 428/1.8 \times 48.13 = 4.94 \end{aligned}$$

$$\begin{aligned} \text{Center} \quad M &= 8.28 - 4.28 = 4.0 \text{ t-m} \\ A_t &= 400/1.8 \times 48.13 = 4.62 \quad 3\text{-D16} \end{aligned}$$



$$W = 0.32 \text{ t/m} + 0.64 \text{ t/m}^2 \times 1.5 \text{ m} + 0.44 \text{ t/m}^2 \times 1.2 \text{ m} \\ = 1.81 \text{ t/m} \\ P = 3.08 \text{ t}$$

$$\begin{aligned} \left[Q_a &= 1/2 \times 1.81 \times 2.5 + \frac{3.08 \times 2.0}{2.5} = 4.73 \text{ t} \right. \\ \left| Q_b &= 1/2 \times 1.81 \times 2.5 + \frac{3.08 \times 0.5}{2.5} = 2.88 \text{ t} \right. \\ \left[M &= 1/8 \times 1.81 \times 2.5^2 + 0.62 \times 1.25 = 2.19 \text{ t}\cdot\text{m} \right. \end{aligned}$$

<G2>

$$B \times D = 25 \times 60 \text{ cm} \quad d = 55 \text{ cm} \quad j = 48.13 \text{ cm}$$

$$\begin{aligned} \text{End} \quad \phi &= 4730/14 \times 48.13 = 7.02 \text{ cm} \quad 2\text{-D16} \\ \tau &= 4730/25 \times 48.13 = 3.93 \text{ kg/cm}^2 < 4.25 \text{ kg/cm}^2 \text{ O.K.} \end{aligned}$$

$$\text{Center} \quad A_t = 219/1.8 \times 48.13 = 2.53 \text{ cm}^2 \quad 2\text{-D16}$$



$$W = 0.76 \text{ t/m}^2 \\ P = 0.44 \text{ t/m}^2 \times 1.2 = 0.528 \text{ t/m}$$

$$\begin{aligned} \left[M &= 1/2 \times 176 \times 1.425^2 + 0.528 \times 1.425 = 1.524 \text{ t}\cdot\text{m} \right. \\ \left[Q &= 0.76 \times 1.425 + 0.528 = 1.611 \text{ t} \right. \end{aligned}$$

CS3

$$D = 15 \text{ cm} \quad d = 12 \text{ cm} \quad j = 10.5 \text{ cm}$$

$$A_t = 152.4/1.8 \times 10.5 = 8.06 \text{ cm}^2 \\ \text{D13} \quad x = \frac{1.27 \times 100}{8.06} = 15.7 \text{ cm}$$

$$\phi = 1611/14 \times 10.5 = 10.96 \text{ cm} \\ x = \frac{4.0 \times 100}{10.96} = 36.14 \text{ cm}$$

∴ D13 - @ 150

4). Design of Slab

		Lx(m)	Ly(m)	t(Cm)	w(t/m ²)
D10,D13	S01	3.5	4.0	15.0	0.660
	S02	4.0	6.0	15.0	0.660
	S03	3.5	4.0	15.0	0.760
	S04	4.0	6.0	15.0	0.760

		Lx(m)	Ly(m)	t(Cm)	w(t/m ²)	
D10,D13	S01	3.5	4.0	15.0	0.660	
		LAMBDA= 1.14		wLx2(t*m)= 8.085		ft(Kg/cm ²)=2000.0

	ALPHA	M(t*m/m ²)	at(Cm ² /m)	D10	D10&D13	D13	
X-E	-0.053	-0.425	2.02	@35.1	@43.9	@62.8) D10,13-@200
X-C	0.035	0.283	1.35	@52.7	@73.4	@94.2	
Y-E	-0.042	-0.337	1.75	@40.6	@56.6	@72.6) D10,13-@200
Y-C	0.028	0.225	1.17	@60.9	@84.9	@##.##	

		Lx(m)	Ly(m)	t(Cm)	w(t/m ²)	
	S02	4.0	6.0	15.0	0.660	
		LAMBDA= 1.50		wLx2(t*m)= 10.560		ft(Kg/cm ²)=2000.0

	ALPHA	M(t*m/m ²)	at(Cm ² /m)	D10	D10&D13	D13	
X-E	-0.070	-0.735	3.50	@20.3	@28.3	@36.3) D10,13-@200
X-C	0.046	0.490	2.33	@30.4	@42.4	@54.4	
Y-E	-0.042	-0.440	2.29	@31.1	@43.3	@55.6) D10,13-@200
Y-C	0.028	0.293	1.52	@46.6	@65.0	@83.3	

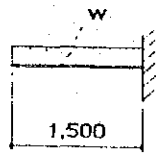
		Lx(m)	Ly(m)	t(Cm)	w(t/m ²)	
	S03	3.5	4.0	15.0	0.760	
		LAMBDA= 1.14		wLx2(t*m)= 9.310		ft(Kg/cm ²)=2000.0

	ALPHA	M(t*m/m ²)	at(Cm ² /m)	D10	D10&D13	D13	
X-E	-0.053	-0.489	2.33	@30.5	@42.5	@54.5) D10,13-@200
X-C	0.035	0.326	1.55	@45.7	@63.8	@81.8	
Y-E	-0.042	-0.388	2.02	@35.2	@49.1	@63.0) D10,13-@200
Y-C	0.028	0.259	1.34	@52.8	@73.7	@94.5	

		Lx(m)	Ly(m)	t(Cm)	w(t/m ²)	
	S04	4.0	6.0	15.0	0.760	
		LAMBDA= 1.50		wLx2(t*m)= 12.160		ft(Kg/cm ²)=2000.0

	ALPHA	M(t*m/m ²)	at(Cm ² /m)	D10	D10&D13	D13	
X-E	-0.070	-0.846	4.03	@17.6	@24.6	@31.5) D10,13-@200
X-C	0.046	0.564	2.69	@26.4	@36.9	@47.3	
Y-E	-0.042	-0.507	2.63	@27.0	@37.6	@48.3) D10,13-@200
Y-C	0.028	0.338	1.75	@40.5	@56.4	@72.4	

5). Design of Stair



$$W = 0.96 \text{ t/m}^2 \times 0.25 \text{ m} = 0.24 \text{ t/m}$$

$$M = 1/2 \times 0.24 \times 1.5^2 = 0.27 \text{ t}\cdot\text{m}$$

$$Q = 0.24 \times 1.5 = 0.36 \text{ t}$$

$$D = 25 \text{ cm} \quad d = 20 \text{ cm} \quad j = 17.5 \text{ cm}$$

$$A_t = \frac{27}{1.8 \times 17.5} = 0.86 \text{ cm}^2$$

$$\phi = \frac{360}{21 \times 17.5} = 0.98 \text{ cm} \quad 1\text{-D13}$$

6). Design of Foundation

Allowable bearing capacity $f_c = 30 \text{ t/m}^2$ (Permanent)

Dead load $2.4 \text{ t/m}^3 \times 0.19 \text{ m} \times 0.75 \text{ m} = 0.35 \text{ t/m}$
 $2.0 \text{ t/m}^3 \times (1.0 - 0.19) \text{ m} \times 0.6 \text{ m} = 0.98 \text{ t/m}$ 1.33 t/m

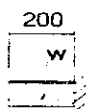
W: wall

C: column

NO	LF (m)	N (t)	P'=N/LF (t/m)	P (t/m)	NO	LF (m)	N (t)	P'=N/LF (t/m)	P (t/m)
W1	3.6	9.9	2.75	4.08	W21	4.75	39.1	8.23	9.56
W2	3.6	10.1	2.81	4.14	W22	3.5	17.2	4.92	6.25
W3•W6	2.55	13.8	5.42	6.75	W23	4.0	14.6	3.65	4.98
W4•W5	5.2	28.9	5.56	6.89	W24	6.0	20.6	3.44	4.77
W7	3.6	6.9	1.92	3.25	W25	3.5	11.4	3.26	4.59
W8	4.0	31.2	7.80	9.13	W26	6.0	32.4	5.4	6.73
W9	3.8	22.0	5.79	7.12					
W10	3.6	16.6	4.61	5.94					
W11	4.0	33.2	8.3	9.63					
W12	4.0	14.8	3.7	5.03					
W13	3.6	22.2	6.17	7.50					
W14	4.6	22.6	4.92	6.25					
W15	11.6	37.0	3.19	4.52					
W16	7.5	26.4	3.52	4.85					
W17	3.75	19.7	5.25	6.58					
W18	3.5	11.4	3.26	4.59					
W19	7.5	42.9	5.72	7.05					
W20	3.5	19.3	5.52	6.85					

NO	$L' = \frac{P}{f_c} \text{ (m)}$	L (m)	$\sigma_c = \frac{P}{L}$	$P'' \text{ (t/m)}$ (P + 0.35)	$\sigma_c' = \frac{P''}{L}$
W1	0.14	0.40			
W2	0.14	"			
W3•W6	0.23	"			
W4•W5	0.29	"			
W7	0.11	"			
W8	0.31	"			
W9	0.24	"			
W10	0.20	"			
W11	0.32	"	24.08 t/m ² < 30 t/m ²	8.65	21.63
W12	0.11	"			
W13	0.25	"			
W14	0.21	"			
W15	0.15	"			
W16	0.17	"			
W17	0.22	"			
W18	0.16	"			
W19	0.24	"			
W20	0.23	"			
W21	0.32	"			
W22	0.21	"			
W23	0.17	"			
W24	0.16	"			
W25	0.16	"			
W26	0.23	"			

<F1A>



$$W = 21.63$$

$$M = \frac{1}{2} \times 21.63 \times 0.2^2 = 0.44 \text{ t}\cdot\text{m}$$

$$Q = 21.63 \times 0.2 = 4.33 \text{ t}$$

$$D = 18 \text{ cm} \quad d = 12 \text{ cm} \quad j = 10.5 \text{ cm}$$

$$A_t = 44 / 1.8 \times 10.5 = 2.33 \text{ cm}^2$$

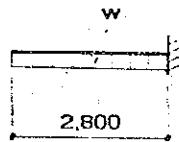
$$D10 \quad x = \frac{0.71 \times 100}{2.33} = 30.4 \text{ cm}^2$$

$$\phi = 4330/21 \times 10.5 = 19.64 \text{ cm}$$

$$x = \frac{3.0 \times 100}{19.64} = 15.2 \text{ cm}$$

D10 - @150

$$\tau = 4330/100 \times 10.5 = 4.12 \text{ kg/cm}^2 < 4.25 \text{ kg/cm}^2 \text{ O.K.}$$



<FG1A>

$$W = 5.56 \text{ t/m}$$

$$M = 1/12 \times 5.56 \times 2.8^2 = 3.63 \text{ t}\cdot\text{m}$$

$$Q = 1/2 \times 5.56 \times 2.8 = 7.78 \text{ t}$$

$$B \times D = 19 \text{ cm} \times 75 \text{ cm} \quad d = 67 \text{ cm} \quad j = 58.63 \text{ cm}$$

$$A_t = 373/1.8 \times 58.63 = 3.44 \text{ cm}^2$$

$$\phi = 7780/21 \times 58.63 = 6.32 \text{ cm} \quad 2\text{-D16}$$

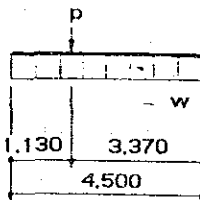
$$\tau = 7780/19 \times 58.63 = 6.98 \text{ kg/cm}^2 > 4.25 \text{ kg/cm}^2 \text{ NG}$$

$$\Delta Q = 7.78 - 19 \times 58.63 \times 4.25 \times 10^{-3} = 3.05 \text{ t}$$

$$\Delta Q/bj = 2.8 \quad PW = 0.50$$

$$D10 \quad x = 1.43/19 \times 0.005 = 15.1 \text{ cm}^2$$

\therefore D10 - @150



<FG1A>

$$P = 5.25 \times 2.25 = 11.82 \text{ t}$$

$$Q_a = 11.82 \times 3.37/4.5 = 8.85 \text{ t}$$

$$Q_b = 11.82 \times 1.13/4.5 = 2.97 \text{ t}$$

$$C_a = \frac{11.82 \times 3.37^2 \times 1.13}{4.5^2} = 7.49 \text{ t}\cdot\text{m}$$

$$C_b = \frac{11.82 \times 3.37 \times 1.13^2}{4.5^2} = 2.52 \text{ t}\cdot\text{m}$$

$$M_o = 2.97 \times 2.25 = 6.69 \text{ t}\cdot\text{m}$$

$$B \times D = 25 \text{ cm} \times 75 \text{ cm} \quad d = 67 \text{ cm} \quad j = 58.6 \text{ cm}$$

$$A_t = 749/1.8 \times 58.63 = 7.10 \text{ cm}^2$$

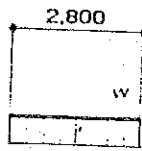
$$\phi = 8850/21 \times 58.63 = 7.19 \text{ cm} \quad 4\text{-D16}$$

$$\tau = 8850/25 \times 58.63 = 6.04 \text{ kg/cm}^2 > 4.25 \text{ kg/cm}^2 \text{ NG}$$

$$\Delta Q = 8.85 - 25 \times 58.63 \times 4.25 \times 10^{-3} = 2.62 \text{ t}$$

$$\Delta Q/bj = 1.8 \quad PW = 0.40 \%$$

$$D10 \quad x = 1.43/25 \times 0.0040 = 14.3 \text{ cm} \quad \therefore \text{D10 - @100}$$



$$W = 3.7 \text{ t/m}$$

$$\lceil M = 1/12 \times 3.7 \times 2.8^2 = 2.42 \text{ t}\cdot\text{m}$$

$$\lfloor Q = 1/2 \times 3.7 \times 2.8 = 5.18 \text{ t}$$

$$B \times D = 19 \text{ cm} \times 75 \text{ cm} \quad d = 67 \text{ cm} \quad j = 58.63 \text{ cm}$$

$$A_t = 242/1.8 \times 58.63 = 2.29 \text{ cm}^2$$

$$\phi = 5180/21.0 \times 58.63 = 4.21 \text{ cm} \quad 2\text{-D16}$$

$$\tau = 5180/19 \times 58.63 = 4.65 \text{ kg/cm}^2 > 4.25 \text{ kg/cm}^2 \text{ NG}$$

$$\Delta Q = 5.18 - 19 \times 58.63 \times 4.25 \times 10^{-3} = 0.45 \text{ t}$$

$$\Delta Q/bj = 0.4 \quad PW = 0.25 \%$$

$$D10 \quad x = 1.43/19 \times 0.0025 = 30.1 \text{ cm} \quad \therefore D10 - @150$$

Table 1.1.1 PRINCIPAL FEATURES OF TUNNEL TYPE

Item	Type I	Type II
1. Internal Diameter (cm)	680	680
2. Lining Thickness (cm)	50	80
3. Rock Properties		
• Rock class	C _M ~ C _H	C _L ~ C _M
• Elastic modulus E _r (kg/cm ²)	30,000	5,000
• Poisson's ratio ν _r	0.2	0.3

Table 1.1.2 LOADING CONDITIONS OF DIVERSION TUNNEL

Item	Upstream Section from Plug	Downstream Section from Plug	Note	Study
1. During diversion, normal	$P_e = \text{GWL} - \text{Tunnel center EL.}$ $= 140 - 131 = 9.0 \text{ t/m}^2$ $P_i = 0$	$P_e = 140 - 128.4 = 11.6 \text{ t/m}^2$ $- \text{do} -$		Check
2. During diversion, flood	$P_e = \text{FWL} - \text{Tunnel center EL.}$ $= 154.5 - 131.0 = 23.5 \text{ t/m}^2$ (just after flowing out)	$P_e = 140 - 128.4 = 11.6 \text{ t/m}^2$		No-check
3. After completion, normal	$P_i = \text{FWL} - \text{Tunnel center EL.} - v^2/2g$ $= 154.5 - 131.0 - 10.5$ $= 13.0 \text{ t/m}^2$ $P_e = 0$ $P_i = 0$	$P_i = \text{FWL} - \text{Tunnel center EL.} - v^2/2g$ $= 154.5 - 128.4 - 10.5 = 15.6 \text{ t/m}^2$ $P_e = 0$ (drained by weep holes) $P_i = 0$		Check
4. After completion, abnormal	$P_e = \text{HWL} - \text{Tunnel center EL.}$ $= 208.0 - 131.0 = 77.0 \text{ t/m}^2$ (dewatered condition)	$P_e = 0$ (drained by weep holes)	65% increment of allowable stresses	Check
5. Grout pressure	$P_i = 208.0 - 131.0 = 77.0 \text{ t/m}^2$ (abnormal condition)	$P_i = 0$	65% increment of allowable stresses	Check
6. Others	The grout pressure of 2 kg/cm^2 is imposed locally around the grout holes for consolidation and curtain. Rock loads are taken by the tunnel supports erected during construction so that no rock load is imposed on the concrete lining. Deal load is neglected because it is rather small than others.		Concrete strength $\sigma_{28} = 210$ Yield strength	Check

Table 1.1.3 CONCRETE AND STEEL PROPERTIES

Increment of Stress (%)	Concrete		Steel
	Compression (kg/cm ²)	Shear (kg/cm ²)	Tension (kg/cm ²)
0	70	8.5	1,800
65	116	14	2,970
for grout pressure	210	18	3,000

Concrete	Strength	$\sigma_{28} = 210 \text{ kg/cm}^2$
	Elastic modulus	$E_c = 255,000 \text{ kg/cm}^2$
	Poisson's ratio	$\nu_c = 0.2$
Steel	Elastic modulus	$E_s = 2,100,000 \text{ kg/cm}^2$

Table 1.1.4 RESULTS OF STRUCTURAL ANALYSES FOR DIVERSION TUNNEL

Item	Type I	Type II	
		U/S	D/S
Lining thickness (cm)	50	80	80
Reinforcement	D16 @300 (inside)	D22 @200 (both sides)	D16 @300 (both sides)
Stress against Internal pressure • re-bar (kg/cm ²)	602	2,675	710
Stress against External pressure • concrete (kg/cm ²)	64	43	7
Stress against Grout pressure			
• concrete inside (kg/cm ²)	32	41	53
• concrete outside	4		
• re-bar inside	-		
• re-bar outside	-	547	1,106

Table 1.1.5(1):TUNNEL ANALYSIS BY OTTO-FREY-BEAR'S THEORY
(Tunnel Type-I)

Elastic modulus (rock)	= 30000	(kg/cm ²)
Elastic modulus (steel)	= 2100000	(kg/cm ²)
Elastic modulus (conc.)	= 255000	(kg/cm ²)
Poisson's ratio (rock)	= .2	
Poisson's ratio (conc.)	= .2	
Lining thickness (cm)	= 50	
Inner diameter (cm)	= 680	
Internal pressure(kg/cm ²)	= 7.7	
External pressure(kg/cm ²)	= 7.7	
Pitch of rein-bar (mm)	= 300	

(Unit:kg/cm ²)	TENSION (*)		COMPRESSION (**)	
Plain conc.	-33.5		64.2	
Rein-bars	SGL	DBL	SGL	DBL
D 13 @ 300	605.1	599.4	63.7	63.3
D 16 @ 300	601.8	593.1	63.6	63.0
D 19 @ 300	597.9	585.4	63.1	62.3
D 22 @ 300	593.2	576.9	62.9	61.8
D 25 @ 300	587.9	567.0	62.5	60.9
D 29 @ 300	582.0	556.2	61.9	60.1

Note : (*) gives the case of internal pressure
(**) gives the case of external pressure

Table 1.1.5(2):TUNNEL ANALYSIS BY OTTO-FREY-BEAR'S THEORY
(Tunnel Type-II, Upstream of Plug)

Elastic modulus (rock)	=	5000	(kg/cm ²)
Elastic modulus (steel)	=	2100000	(kg/cm ²)
Elastic modulus (conc.)	=	255000	(kg/cm ²)
Poisson's ratio (rock)	=	.3	
Poisson's ratio (conc.)	=	.2	
Lining thickness (cm)	=	80	
Inner diameter (cm)	=	680	
Internal pressure(kg/cm ²)	=	7.7	
External pressure(kg/cm ²)	=	7.7	
Pitch of rein-bar (mm)	=	200	

(Unit:kg/cm ²)	TENSION (*)		COMPRESSION (**)	
Plain conc.	-34.7		44.7	
Rein-bars	SGL	DBL	SGL	DBL
D 13 @ 200	3795.3	3529.5	44.5	44.1
D 16 @ 200	3607.2	3243.4	44.3	43.8
D 19 @ 200	3401.1	2950.8	44.1	43.6
D 22 @ 200	3192.7	2674.9	43.7	43.0
D 25 @ 200	2975.5	2406.6	43.6	42.7
D 29 @ 200	2762.6	2161.0	43.1	42.0

Note : (*) gives the case of internal pressure
(**) gives the case of external pressure

Table 1.1.5(3):TUNNEL ANALYSIS BY OTTO-FREY-BEAR'S THEORY
(Tunnel Type-II, Downstream of Plug)

Elastic modulus (rock)	= 5000	(kg/cm ²)
Elastic modulus (steel)	= 2100000	(kg/cm ²)
Elastic modulus (conc.)	= 255000	(kg/cm ²)
Poisson's ratio (rock)	= .3	
Poisson's ratio (conc.)	= .2	
Lining thickness (cm)	= 80	
Inner diameter (cm)	= 680	
Internal pressure(kg/cm ²)	= 1.56	
External pressure(kg/cm ²)	= 1.16	
Pitch of rein-bar (mm)	= 300	

(Unit:kg/cm ²)	(*)		(**)	
	TENSION		COMPRESSION	
Plain conc.	-7.0		6.7	
Rein-bars	SGL	DBL	SGL	DBL
D 13 @ 300	793.3	754.1	6.8	6.8
D 16 @ 300	765.7	710.1	6.8	6.6
D 19 @ 300	734.6	662.7	6.8	6.6
D 22 @ 300	702.2	615.8	6.6	6.7
D 25 @ 300	666.8	567.9	6.6	6.5
D 29 @ 300	631.1	522.0	6.7	6.6

Note : (*) gives the case of internal pressure
(**) gives the case of external pressure

Table 1.1.5(4) :TUNNEL ANALYSIS BY OTTO-FREY-BEAR'S THEORY
(Tunnel Type-I, During River Diversion)

Elastic modulus (rock)	=	30000	(kg/cm ²)
Elastic modulus (steel)	=	2100000	(kg/cm ²)
Elastic modulus (conc.)	=	255000	(kg/cm ²)
Poisson's ratio (rock)	=	.2	
Poisson's ratio (conc.)	=	.2	
Lining thickness (cm)	=	50	
Inner diameter (cm)	=	680	
Internal pressure(kg/cm ²)	=	0	
External pressure(kg/cm ²)	=	1.16	
Pitch of rein-bar (mm)	=	300	

(Unit:kg/cm ²)	(*)		(**)	
	TENSION		COMPRESSION	
Plain conc.	0.0		9.7	
Rein-bars	SGL	DBL	SGL	DBL
D 13 @ 300	0.0	0.0	9.7	9.5
D 16 @ 300	0.0	0.0	9.7	9.6
D 19 @ 300	0.0	0.0	9.5	9.5
D 22 @ 300	0.0	0.0	9.6	9.4
D 25 @ 300	0.0	0.0	9.5	9.3
D 29 @ 300	0.0	0.0	9.3	9.2

Note : (*) gives the case of internal pressure
(**) gives the case of external pressure

Table 1.1.6(1):TUNNEL ANALYSIS FOR GROUT PRESSURE
(Tunnel Type-I)

Elastic modulus (rock) = 30000 (kg/cm²)
 Elastic modulus (conc) = 255000 (kg/cm²)
 Poisson's ratio (rock) = .2
 Poisson's ratio (Conc) = .2
 Lining thickness (cm) = 50
 Inner diameter (cm) = 680
 Grouting press. (kg/cm²) = 2

PHAI (deg)	M (tm)	S (t)	N (t)	sig1 (kg/cm ²)	sig2 (kg/cm ²)
0	0.7	0.0	-69.0	15.1	12.4
5	0.7	0.0	-69.0	15.3	12.5
10	0.7	0.0	-69.0	15.3	12.5
15	0.6	0.0	-69.0	15.2	12.3
20	0.6	0.2	-69.0	15.4	12.2
25	0.8	0.2	-68.8	15.5	12.1
30	0.7	0.2	-68.8	15.5	12.0
35	0.8	0.1	-68.8	15.8	11.8
40	1.0	0.1	-68.9	16.0	11.8
45	0.9	0.2	-68.9	16.0	11.6
50	1.0	0.0	-68.9	16.3	11.3
55	1.0	-0.0	-68.7	16.3	11.3
60	1.1	-0.3	-68.9	16.2	11.4
65	0.9	-0.4	-68.8	15.8	12.0
70	0.6	-0.7	-69.0	14.9	12.6
75	-0.2	-1.2	-69.0	13.9	13.8
80	-0.8	-1.6	-69.4	15.8	12.0
85	-2.0	-1.8	-69.5	18.5	9.4
90	-3.1	-2.1	-70.0	21.5	6.4
95	-4.7	-2.2	-70.4	25.0	3.2
100	-6.0	-2.0	-70.8	28.5	-0.4
105	-7.1	-0.9	-71.1	31.4	-3.0
110	-7.4	1.0	-71.2	32.2	-3.8
115	-6.6	4.7	-70.9	29.8	-1.3
120	-5.1	4.5	-70.5	26.0	2.1
125	-3.7	4.4	-70.0	22.7	5.4
130	-2.4	4.1	-69.6	19.5	8.6
135	-1.0	3.8	-69.3	16.5	11.5
140	0.2	3.5	-69.0	14.0	13.7
145	1.2	3.1	-68.7	16.5	11.1
150	2.1	2.6	-68.6	18.6	8.9
155	2.9	2.2	-68.4	20.4	7.0
160	3.5	1.9	-68.2	21.9	5.6
165	4.0	1.5	-68.1	22.9	4.2
170	4.4	0.9	-68.0	23.9	3.5
175	4.6	0.6	-67.8	24.4	2.8
180	4.5	0.0	-67.9	24.6	2.8

Note: M: Moment, S: Shear, N: Axial Force

Sig 1: Inside Stress, Sig 2: Outside Stress

Table 1.1.6(2) :TUNNEL ANALYSIS FOR GROUT PRESSURE

(Tunnel Type-II)

Elastic modulus (rock) = 5000 (kg/cm²)
 Elastic modulus (conc) = 255000 (kg/cm²)
 Poisson's ratio (rock) = .3
 Poisson's ratio (Conc) = .2
 Lining thickness (cm) = 80
 Inner diameter (cm) = 680
 Grouting press. (kg/cm²) = 2

PHAI (deg)	M (tm)	S (t)	N (t)	sig1 (kg/cm ²)	sig2
0	18.8	0.0	-62.5	25.3	-9.7
5	18.6	-1.1	-62.4	25.1	-9.5
10	17.9	-2.2	-62.6	24.6	-8.8
15	16.6	-3.3	-62.9	23.6	-7.7
20	15.2	-4.3	-63.3	22.0	-6.3
25	13.0	-5.3	-64.0	20.2	-4.2
30	10.6	-6.2	-64.5	18.0	-2.0
35	7.9	-7.0	-65.4	15.6	1.0
40	4.6	-7.8	-66.2	12.7	3.9
45	1.1	-8.3	-67.0	9.4	7.3
50	-2.6	-8.6	-68.1	10.9	6.0
55	-6.5	-8.6	-69.0	14.7	2.5
60	-10.6	-8.3	-70.2	18.7	-1.2
65	-14.5	-7.5	-71.2	22.5	-4.7
70	-18.2	-6.6	-72.2	26.1	-7.9
75	-21.5	-4.9	-72.9	29.3	-10.9
80	-24.1	-2.8	-73.8	31.8	-13.4
85	-26.2	-0.1	-74.3	33.7	-15.3
90	-26.9	3.2	-74.5	34.7	-16.1
95	-26.6	7.2	-74.4	34.2	-15.5
100	-24.3	12.1	-73.7	32.0	-13.7
105	-20.1	12.8	-72.7	27.8	-9.8
110	-15.9	12.6	-71.6	23.7	-6.0
115	-11.7	12.0	-70.5	19.9	-2.3
120	-7.8	11.6	-69.5	16.0	1.3
125	-4.1	11.0	-68.5	12.4	4.8
130	-0.6	10.3	-67.6	9.0	8.0
135	2.6	9.5	-66.6	10.9	6.0
140	5.7	8.5	-65.8	13.6	3.1
145	8.4	7.6	-65.1	16.0	0.5
150	10.6	6.6	-64.5	18.0	-1.9
155	12.8	5.6	-64.1	20.0	-4.0
160	14.5	4.5	-63.5	21.5	-5.5
165	15.8	3.4	-63.3	22.7	-6.9
170	16.6	2.3	-62.9	23.6	-7.7
175	17.3	1.3	-62.9	24.1	-8.4
180	17.5	0.0	-62.7	24.1	-8.6

Note: M: Moment, S: Shear, N: Axial Force

Sig 1: Inside Stress, Sig 2: Outside Stress

Table 1.1.6(3): CALCULATION OF INTERNAL STRESS IN REINFORCED
CONCRETE STRUCTURE: DIVERSION TUNNEL (TYPE-II)
FOR GROUT PRESSURE

Member Spot		D/S	D/S	U/S	U/S
M	t.m	26.90	20.10	26.90	20.10
Q	t	3.20	12.80	3.20	12.80
N	t	74.50	72.70	74.50	72.70
b	cm	100.00	100.00	100.00	100.00
h	cm	80.00	80.00	80.00	80.00
u	cm	30.00	30.00	30.00	30.00
d	cm	70.00	70.00	70.00	70.00
d'	cm	10.00	10.00	10.00	10.00
d' / d		0.14	0.14	0.14	0.14
M' = M+N.u	t.m	49.25	41.91	49.25	41.91
M' / (b.d.d)	kg/cm ²	10.05	8.55	10.05	8.55
Q / (b.d)	kg/cm ²	0.46	1.83	0.46	1.83
f = M/N+u	cm	66.11	57.65	66.11	57.65
f / d		0.94	0.82	0.94	0.82
As		D16@300	D16@300	D22@200	D22@200
	cm ²	6.61	6.61	19.40	19.40
As'		D16@300	D16@300	D22@200	D22@200
	cm ²	6.61	6.61	19.40	19.40
As' / As		1.00	1.00	1.00	1.00
n		15.00	15.00	15.00	15.00
np=n.As/(bd)		0.014	0.014	0.042	0.042
C		5.31	3.98	4.09	3.43
S		7.34	2.57	3.63	1.61
Z		1.16	1.25	1.21	1.28
Sigma c	kg/cm ²	53.3	34.0	41.1	29.4
Sigma s	kg/cm ²	1106.2	329.7	546.6	206.6
Tau	kg/cm ²	0.5	2.3	0.6	2.3
Sigma ca	kg/cm ²	210.0	210.0	210.0	210.0
Sigma sa	kg/cm ²	3000.0	3000.0	3000.0	3000.0
Tau a	kg/cm ²	18.0	18.0	18.0	18.0

Case
Note

- As, As' : Sectional area of reinforcement bar (cm²)
Sigma C : Stress in concrete (kg/cm²)
Sigma S : Stress in reinforcement bar (kg/cm²)
Tau : Shearing stress in concrete (kg/cm²)
Sigma Ca : Allowable stress for concrete (kg/cm²)
Sigma Sa : Allowable stress for reinforcement bar (kg/cm²)
Tau a : Allowable shearing stress for concrete (kg/cm²)

Table 1.1.7(1): STRUCTURAL ANALYSIS OF INLET PORTAL (SECTION A-A)

NOTES: * MEANS MAXIMUM STEEL AREA

MEM	CASE POINT	SIGN	B	H	D1	D2	N	S	M	AS	ASD	SIGC	SIGS	TAU	SIGCA	SIGSA	SIGTAU
1	1 (1)		100.0	200.0	190.0	10.0	67.4	5.5	23.3	0.00	0.00	6.9	0.0	0.4	105.0	2700.0	12.8
1	1 MAX						68.7	0.0	22.1	0.00	0.00	6.8	0.0	0.0			
1	1 (2)						71.2	22.1	38.3	0.00	0.00	9.3	0.0	1.6			
1	2 (1)		100.0	200.0	190.0	10.0	354.7	84.8	149.2	0.01	0.00	40.8	56.9	6.4	105.0	2700.0	12.8
1	2 MAX						352.8	0.0	106.4	0.00	0.00	33.6	0.0	0.0			
1	2 (2)	*					349.6	82.8	146.1	0.01	0.00	40.0	52.9	6.3			
2	1 (2)		100.0	200.0	190.0	10.0	66.0	34.7	38.3	0.00	0.00	9.0	0.0	2.5	105.0	2700.0	12.8
2	1 MAX						0.0	0.0	0.0	0.00	0.00	0.0	0.0	0.0			
2	1 (3)						62.6	20.9	5.0	0.00	0.00	3.9	0.0	1.4			
2	2 (2)	*	100.0	200.0	190.0	10.0	305.7	188.6	146.1	0.01	0.00	39.0	124.8	13.7	105.0	2700.0	12.8
2	2 MAX						0.0	0.0	0.0	0.00	0.00	0.0	0.0	0.0			
2	2 (3)						299.9	112.5	34.4	0.00	0.00	20.2	0.0	7.7			
3	1 (3)		100.0	200.0	190.0	10.0	62.6	20.9	5.0	0.00	0.00	3.9	0.0	1.4	105.0	2700.0	12.8
3	1 MAX						57.1	0.0	15.1	0.00	0.00	5.1	0.0	0.0			
3	1 (4)						52.5	15.8	1.9	0.00	0.00	2.9	0.0	1.0			
3	2 (3)		100.0	200.0	190.0	10.0	299.9	112.5	34.4	0.00	0.00	20.2	0.0	7.7	105.0	2700.0	12.8
3	2 MAX	*					291.1	0.0	137.2	0.01	0.00	36.7	109.0	0.0			
3	2 (4)						282.7	102.4	46.5	0.00	0.00	21.1	0.0	7.3			
4	1 (4)		100.0	200.0	190.0	10.0	52.5	15.8	1.9	0.00	0.00	2.9	0.0	1.0	105.0	2700.0	12.8
4	1 MAX						0.0	0.0	0.0	0.00	0.00	0.0	0.0	0.0			
4	1 (5)						48.9	27.3	26.2	0.00	0.00	6.4	0.0	2.0			
4	2 (4)		100.0	200.0	190.0	10.0	282.7	102.4	46.5	0.00	0.00	21.1	0.0	7.3	105.0	2700.0	12.8
4	2 MAX						0.0	0.0	0.0	0.00	0.00	0.0	0.0	0.0			
4	2 (5)	*					276.4	175.1	134.2	0.01	0.00	35.8	123.9	12.6			
5	1 (5)		100.0	220.0	190.0	10.0	53.9	15.2	26.2	0.00	0.00	5.7	0.0	1.2	105.0	2700.0	12.8
5	1 MAX						52.3	0.0	17.4	0.00	0.00	4.5	0.0	0.0			
5	1 (6)						51.0	10.4	21.7	0.00	0.00	5.0	0.0	0.9			
5	2 (5)		100.0	220.0	190.0	10.0	319.3	71.7	134.2	0.00	0.00	31.1	0.0	5.9	105.0	2700.0	12.8
5	2 MAX						318.0	0.0	101.4	0.00	0.00	27.0	0.0	0.0			
5	2 (6)	*					315.8	82.5	145.4	0.00	0.00	32.4	0.0	6.6			
6	1 (6)		100.0	140.0	130.0	10.0	43.4	28.7	21.7	0.00	0.00	9.7	0.0	3.0	105.0	2700.0	12.8
6	1 MAX						0.0	0.0	0.0	0.00	0.00	0.0	0.0	0.0			
6	1 (7)						43.4	17.8	6.2	0.00	0.00	5.0	0.0	1.9			
6	2 (6)	*	100.0	140.0	130.0	10.0	281.6	164.9	145.4	0.01	0.01	102.2	2081.0	14.8	105.0	2700.0	12.8
6	2 MAX						0.0	0.0	0.0	0.00	0.00	0.0	0.0	0.0			
6	2 (7)						281.6	99.7	13.4	0.00	0.00	24.2	0.0	9.8			
7	1 (7)		100.0	140.0	130.0	10.0	43.4	17.8	6.2	0.00	0.00	5.0	0.0	1.9	105.0	2700.0	12.8
7	1 MAX						0.0	0.0	0.0	0.00	0.00	0.0	0.0	0.0			
7	1 (8)						43.4	6.8	21.0	0.00	0.00	9.5	0.0	0.7			
7	2 (7)		100.0	140.0	130.0	10.0	281.6	99.7	13.4	0.00	0.00	24.2	0.0	9.8	105.0	2700.0	12.8
7	2 MAX						0.0	0.0	0.0	0.00	0.00	0.0	0.0	0.0			
7	2 (8)	*					281.6	34.4	93.8	0.01	0.00	51.2	138.9	3.7			
8	1 (8)		100.0	220.0	210.0	10.0	43.4	6.8	21.0	0.00	0.00	4.6	0.0	0.5	105.0	2700.0	12.8
8	1 MAX						43.4	0.0	23.3	0.00	0.00	4.9	0.0	0.0			
8	1 (9)						43.4	17.6	8.0	0.00	0.00	3.0	0.0	1.1			
8	2 (8)		100.0	220.0	210.0	10.0	281.6	34.4	93.8	0.00	0.00	24.4	0.0	2.5	105.0	2700.0	12.8
8	2 MAX						281.6	0.0	104.3	0.00	0.00	25.7	0.0	0.0			
8	2 (9)	*					281.6	100.7	14.2	0.00	0.00	14.6	0.0	6.0			
9	1 (9)		100.0	220.0	210.0	10.0	43.4	17.6	8.0	0.00	0.00	3.0	0.0	1.1	105.0	2700.0	12.8
9	1 MAX						0.0	0.0	0.0	0.00	0.00	0.0	0.0	0.0			

N : Axial force (t)
S : Shearing force (t)
M : Bending moment (t  m)
AS, ASD : Sectional area of reinforcement bar (cm²)
SIGC : Stress in concrete kg/cm²)

SIGS : Stress in reinforcement bar (kg/cm²)
TAU : Shearing stress in concrete (kg/cm²)
SIGCA : Allowable stress for concrete (kg/cm²)
SIGSA : Allowable stress for reinforcement bar (kg/cm²)
SIGTAU : Allowable shearing stress for concrete (kg/cm²)

Table 1.1.7(2) STRUCTURAL ANALYSIS OF INLET PORTAL (SECTION A-A)

NOTES: * MEANS MAXIMUM STEEL AREA

MEM	CASE	POINT	SIGN	B	K	D1	D2	N	S	H	AS	ASD	SICC	SICS	TAU	SIGCA	SIGSA	SIGTAU
9	1	(10)						43.4	29.9	20.5	0.00	0.00	4.5	0.0	2.1			
9	2	(9)		100.0	220.0	210.0	10.0	281.6	100.7	14.2	0.00	0.00	14.6	0.0	6.0	105.0	2700.0	12.8
9	2	MAX						0.0	0.0	0.0	0.00	0.00	0.0	0.0	0.0			
9	2	(10)	*					281.6	168.3	147.2	0.01	0.00	32.5	103.9	11.1			
10	1	(10)		100.0	220.0	210.0	10.0	51.8	9.5	20.5	0.00	0.00	4.9	0.0	0.7	105.0	2700.0	12.8
10	1	MAX						53.0	0.0	16.9	0.00	0.00	4.5	0.0	0.0			
10	1	(11)						54.7	16.1	26.8	0.00	0.00	5.8	0.0	1.1			
10	2	(10)		100.0	220.0	210.0	10.0	318.1	80.1	147.2	0.00	0.00	32.7	0.0	5.6	105.0	2700.0	12.8
10	2	MAX						320.3	0.0	105.7	0.00	0.00	27.7	0.0	0.0			
10	2	(11)	*					321.6	74.0	140.7	0.00	0.00	32.1	0.0	5.2			
11	1	(11)		100.0	200.0	190.0	10.0	50.1	27.3	26.8	0.00	0.00	6.5	0.0	2.0	105.0	2700.0	12.8
11	1	MAX						0.0	0.0	0.0	0.00	0.00	0.0	0.0	0.0			
11	1	(12)						53.7	15.8	1.4	0.00	0.00	2.9	0.0	1.0			
11	2	(11)	*	100.0	200.0	190.0	10.0	279.8	175.1	140.7	0.01	0.00	37.5	154.3	12.5	105.0	2700.0	12.8
11	2	MAX						0.0	0.0	0.0	0.00	0.00	0.0	0.0	0.0			
11	2	(12)						266.0	102.4	40.0	0.00	0.00	20.3	0.0	7.2			
12	1	(12)		100.0	200.0	190.0	10.0	53.7	15.8	1.4	0.00	0.00	2.9	0.0	1.0	105.0	2700.0	12.8
12	1	MAX						58.3	0.0	14.6	0.00	0.00	5.1	0.0	0.0			
12	1	(13)						63.8	20.9	5.6	0.00	0.00	4.0	0.0	1.4			
12	2	(12)		100.0	200.0	190.0	10.0	286.0	102.4	40.0	0.00	0.00	20.3	0.0	7.2	105.0	2700.0	12.8
12	2	MAX	*					294.4	0.0	130.7	0.01	0.00	35.3	73.4	0.0			
12	2	(13)						303.3	112.5	27.8	0.00	0.00	19.3	0.0	7.6			
13	1	(13)		100.0	200.0	190.0	10.0	63.8	20.9	5.6	0.00	0.00	4.0	0.0	1.4	105.0	2700.0	12.8
13	1	MAX						0.0	0.0	0.0	0.00	0.00	0.0	0.0	0.0			
13	1	(14)						67.2	34.7	38.9	0.00	0.00	9.2	0.0	2.5			
13	2	(13)		100.0	200.0	190.0	10.0	303.3	112.5	27.8	0.00	0.00	19.3	0.0	7.6	105.0	2700.0	12.8
13	2	MAX						0.0	0.0	0.0	0.00	0.00	0.0	0.0	0.0			
13	2	(14)	*					309.0	188.6	152.6	0.01	0.00	40.7	153.5	13.5			
14	1	(14)		100.0	200.0	190.0	10.0	72.1	22.9	38.9	0.00	0.00	9.4	0.0	1.7	105.0	2700.0	12.8
14	1	MAX						69.3	0.0	21.3	0.00	0.00	6.7	0.0	0.0			
14	1	(15)						68.3	4.7	22.2	0.00	0.00	6.7	0.0	0.4			
14	2	(14)		100.0	200.0	190.0	10.0	351.9	85.1	152.6	0.01	0.00	41.4	73.6	6.4	105.0	2700.0	12.8
14	2	MAX						355.3	0.0	110.6	0.00	0.00	34.3	0.0	0.0			
14	2	(15)	*					357.1	82.4	151.0	0.01	0.00	41.3	60.4	6.2			
15	1	(16)		100.0	200.0	190.0	10.0	51.6	25.0	17.9	0.00	0.00	5.3	0.0	2.0	105.0	2700.0	12.8
15	1	MAX						0.0	0.0	0.0	0.00	0.00	0.0	0.0	0.0			
15	1	(15)						51.6	41.8	22.2	0.00	0.00	5.9	0.0	3.2			
15	2	(16)		100.0	200.0	190.0	10.0	310.8	113.3	30.2	0.00	0.00	20.1	0.0	7.7	105.0	2700.0	12.8
15	2	MAX						0.0	0.0	0.0	0.00	0.00	0.0	0.0	0.0			
15	2	(15)	*					310.8	188.7	151.0	0.01	0.00	40.3	140.3	13.6			
16	1	(17)		100.0	200.0	190.0	10.0	51.6	25.4	17.3	0.00	0.00	5.2	0.0	2.1	105.0	2700.0	12.8
16	1	MAX						51.6	0.0	40.3	0.00	0.00	8.6	0.0	0.0			
16	1	(16)						51.6	25.0	17.9	0.00	0.00	5.3	0.0	2.0			
16	2	(17)		100.0	200.0	190.0	10.0	310.8	112.7	31.3	0.00	0.00	20.2	0.0	7.7	105.0	2700.0	12.8
16	2	MAX	*					310.8	0.0	132.5	0.01	0.00	36.1	56.3	0.0			
16	2	(16)						310.8	113.3	30.2	0.00	0.00	20.1	0.0	7.7			
17	1	(1)		100.0	200.0	190.0	10.0	51.6	42.2	23.3	0.00	0.00	6.1	0.0	3.2	105.0	2700.0	12.8
17	1	MAX						0.0	0.0	0.0	0.00	0.00	0.0	0.0	0.0			
17	1	(17)						51.6	25.4	17.3	0.00	0.00	5.2	0.0	2.1			
17	2	(1)	*	100.0	200.0	190.0	10.0	310.8	188.1	149.2	0.01	0.00	39.8	130.3	13.6	105.0	2700.0	12.8
17	2	MAX						0.0	0.0	0.0	0.00	0.00	0.0	0.0	0.0			
17	2	(17)						310.8	112.7	31.3	0.00	0.00	20.2	0.0	7.7			

Table 1.1.8(1) STRUCTURAL ANALYSIS OF INLET PORTAL (SECTION B-B)

NOTES: * MEANS MAXIMUM STEEL AREA

MEM	CASE	POINT	SIGN	B	H	D1	D2	N	S	M	AS	ASD	SIGC	SIGS	TAU	SIGCA	SIGSA	SIGTAU
1	1	(1)		100.0	200.0	190.0	10.0	67.2	43.3	76.4	-3.62	-0.00	42.4	2700.0	2.4	105.0	2700.0	12.8
1	1	MAX						0.0	0.0	0.0	0.00	0.00	0.0	0.0	0.0			
1	1	(2)						64.4	36.8	36.3	0.00	0.00	8.7	0.0	2.7			
1	2	(1)	*	100.0	200.0	190.0	10.0	290.4	273.8	402.5	-38.05	-38.05	100.9	2700.0	16.4	105.0	2700.0	12.8
1	2	MAX						0.0	0.0	0.0	0.00	0.00	0.0	0.0	0.0			
1	2	(2)						285.6	213.3	159.0	0.01	0.00	42.9	275.9	14.6			
1	3	(1)		100.0	200.0	190.0	10.0	92.4	25.9	78.9	0.01	0.00	42.0	2089.7	1.5	91.0	2340.0	11.1
1	3	MAX						0.0	0.0	0.0	0.00	0.00	0.0	0.0	0.0			
1	3	(2)						87.6	25.9	53.0	0.01	0.00	14.8	133.7	1.7			
2	1	(2)		100.0	200.0	190.0	10.0	64.4	36.8	36.3	0.00	0.00	8.7	0.0	2.7	105.0	2700.0	12.8
2	1	MAX						54.6	0.0	26.1	0.00	0.00	6.6	0.0	0.0			
2	1	(3)						45.3	28.4	22.5	0.00	0.00	5.6	0.0	2.1			
2	2	(2)		100.0	200.0	190.0	10.0	285.6	213.3	159.0	0.01	0.00	42.9	275.9	14.6	105.0	2700.0	12.8
2	2	MAX						269.2	0.0	200.9	0.01	0.00	70.7	1583.0	0.0			
2	2	(3)						253.0	192.6	129.5	0.01	0.00	34.5	153.9	13.6			
2	3	(2)	*	100.0	200.0	190.0	10.0	87.6	25.9	53.0	0.01	0.00	14.8	133.7	1.7	91.0	2340.0	11.1
2	3	MAX						69.9	0.0	9.2	0.00	0.00	4.9	0.0	0.0			
2	3	(3)						55.0	11.5	29.5	0.00	0.00	7.2	0.0	0.8			
3	1	(3)		100.0	200.0	190.0	10.0	45.3	28.4	22.5	0.00	0.00	5.6	0.0	2.1	105.0	2700.0	12.8
3	1	MAX						0.0	0.0	0.0	0.00	0.00	0.0	0.0	0.0			
3	1	(4)						42.2	36.6	58.3	-4.20	-0.00	34.8	2700.0	2.0			
3	2	(3)		100.0	200.0	190.0	10.0	253.0	192.6	129.5	0.01	0.00	34.5	153.9	13.6	105.0	2700.0	12.8
3	2	MAX						0.0	0.0	0.0	0.00	0.00	0.0	0.0	0.0			
3	2	(4)	*					247.7	251.5	373.9	-40.63	-0.00	103.3	2700.0	15.1			
3	3	(3)		100.0	200.0	190.0	10.0	55.0	11.5	29.5	0.00	0.00	7.2	0.0	0.8	91.0	2340.0	11.1
3	3	MAX						0.0	0.0	0.0	0.00	0.00	0.0	0.0	0.0			
3	3	(4)						49.7	13.3	43.2	0.01	0.00	25.3	1459.8	0.8			
4	1	(4)		100.0	220.0	210.0	10.0	36.6	42.2	58.3	-4.04	-0.00	30.9	2700.0	2.1	105.0	2700.0	12.8
4	1	MAX						0.0	0.0	0.0	0.00	0.00	0.0	0.0	0.0			
4	1	(5)						36.6	32.6	20.8	0.00	0.00	4.2	0.0	2.2			
4	2	(4)	*	100.0	220.0	210.0	10.0	251.5	247.7	373.9	-31.35	-0.00	93.6	2700.0	13.3	105.0	2700.0	12.8
4	2	MAX						0.0	0.0	0.0	0.00	0.00	0.0	0.0	0.0			
4	2	(5)						251.5	191.4	154.4	0.01	0.00	34.5	227.2	11.9			
4	3	(4)		100.0	220.0	210.0	10.0	13.3	49.7	43.2	6.31	-0.00	21.8	2340.0	2.5	91.0	2340.0	11.1
4	3	MAX						0.0	0.0	0.0	0.00	0.00	0.0	0.0	0.0			
4	3	(5)						13.3	38.4	0.8	0.00	0.00	0.7	0.0	2.3			
5	1	(5)		100.0	220.0	210.0	10.0	36.6	32.6	20.8	0.00	0.00	4.2	0.0	2.2	105.0	2700.0	12.8
5	1	MAX						36.6	0.0	34.6	0.00	0.00	6.0	0.0	0.0			
5	1	(6)						36.6	32.6	20.8	0.00	0.00	4.2	0.0	2.2			
5	2	(5)		100.0	220.0	210.0	10.0	251.5	191.4	154.4	0.01	0.00	34.5	227.2	11.9	105.0	2700.0	12.8
5	2	MAX						251.5	0.0	171.1	0.01	0.00	39.9	399.4	0.0			
5	2	(6)						251.5	191.4	154.4	0.01	0.00	34.5	227.2	11.9			
5	3	(5)		100.0	220.0	210.0	10.0	13.3	38.4	0.8	0.00	0.00	0.7	0.0	2.3	91.0	2340.0	11.1
5	3	MAX	*					13.3	0.0	66.1	11.30	0.00	26.3	2340.0	0.0			
5	3	(6)						13.3	38.4	0.8	0.00	0.00	0.7	0.0	2.3			
6	1	(6)		100.0	220.0	210.0	10.0	36.6	32.6	20.8	0.00	0.00	4.2	0.0	2.2	105.0	2700.0	12.8
6	1	MAX						0.0	0.0	0.0	0.00	0.00	0.0	0.0	0.0			
6	1	(7)						36.6	42.2	58.3	-4.04	0.00	30.9	2700.0	2.1			
6	2	(6)		100.0	220.0	210.0	10.0	251.5	191.4	154.4	0.01	0.00	34.5	227.2	11.9	105.0	2700.0	12.8
6	2	MAX						0.0	0.0	0.0	0.00	0.00	0.0	0.0	0.0			

Table 1.1.8(2) STRUCTURAL ANALYSIS OF INLET PORTAL (SECTION B-B)

NOTES: * MEANS MAXIMUM STEEL AREA

MEM	CASE	POINT	SIGN	B	H	D1	D2	N	S	M	AS	ASD	SICC	SIGS	TAU	SIGCA	SIGSA	SIGTAU
6	2	(7)	*					251.5	247.7	373.9	31.35	0.00	93.6	2700.0	13.3			
6	3	(6)		100.0	220.0	210.0	10.0	13.3	38.4	0.8	0.00	0.00	0.7	0.0	2.3	91.0	2340.0	11.1
6	3	MAX						0.0	0.0	0.0	0.00	0.00	0.0	0.0	0.0			
6	3	(7)						13.3	49.7	43.2	-6.31	0.00	21.8	2340.0	2.5			
7	1	(7)		100.0	200.0	190.0	10.0	42.2	36.6	58.3	4.20	0.00	34.8	2700.0	2.0	105.0	2700.0	12.8
7	1	MAX						0.0	0.0	0.0	0.00	0.00	0.0	0.0	0.0			
7	1	(8)						45.3	28.4	22.5	0.00	0.00	5.6	0.0	2.1			
7	2	(7)	*	100.0	200.0	190.0	10.0	247.7	251.5	373.9	-40.69	0.00	103.3	2700.0	15.1	105.0	2700.0	12.8
7	2	MAX						0.0	0.0	0.0	0.00	0.00	0.0	0.0	0.0			
7	2	(8)						253.0	192.6	129.5	0.01	0.00	34.5	153.9	13.6			
7	3	(7)		100.0	200.0	190.0	10.0	49.7	13.3	43.2	0.01	0.00	25.3	1459.9	0.8	91.0	2340.0	11.1
7	3	MAX						0.0	0.0	0.0	0.00	0.00	0.0	0.0	0.0			
7	3	(8)						55.0	11.5	29.5	0.00	0.00	7.2	0.0	0.8			
8	1	(8)		100.0	200.0	190.0	10.0	45.3	28.4	22.5	0.00	0.00	5.6	0.0	2.1	105.0	2700.0	12.8
8	1	MAX						54.6	0.0	26.1	0.00	0.00	6.6	0.0	0.0			
8	1	(9)						64.4	36.8	36.3	0.00	0.00	8.7	0.0	2.7			
8	2	(8)		100.0	200.0	190.0	10.0	253.0	192.6	129.5	0.01	0.00	34.5	153.9	13.6	105.0	2700.0	12.8
8	2	MAX						269.2	0.0	200.9	0.01	0.00	70.7	1583.0	0.0			
8	2	(9)						285.6	213.3	159.0	0.01	0.00	42.9	275.9	14.6			
8	3	(8)		100.0	200.0	190.0	10.0	55.0	11.5	29.5	0.00	0.00	7.2	0.0	0.8	91.0	2340.0	11.1
8	3	MAX						69.9	0.0	9.2	0.00	0.00	4.9	0.0	0.0			
8	3	(9)	*					87.6	25.9	53.0	0.01	0.00	14.8	133.7	1.7			
9	1	(9)		100.0	200.0	190.0	10.0	64.4	36.8	36.3	0.00	0.00	8.7	0.0	2.7	105.0	2700.0	12.8
9	1	MAX						0.0	0.0	0.0	0.00	0.00	0.0	0.0	0.0			
9	1	(10)						67.2	43.3	76.4	-3.62	0.00	42.4	2700.0	2.4			
9	2	(9)		100.0	200.0	190.0	10.0	285.6	213.3	159.0	0.01	0.00	42.9	275.9	14.6	105.0	2700.0	12.8
9	2	MAX						0.0	0.0	0.0	0.00	0.00	0.0	0.0	0.0			
9	2	(10)	*					280.4	273.8	402.5	-38.05	-38.05	100.9	2700.0	16.4			
9	3	(9)		100.0	200.0	190.0	10.0	87.6	25.9	53.0	0.01	0.00	14.8	133.7	1.7	91.0	2340.0	11.1
9	3	MAX						0.0	0.0	0.0	0.00	0.00	0.0	0.0	0.0			
9	3	(10)						92.4	25.9	78.9	0.01	0.00	42.0	2089.7	1.5			
10	1	(11)		100.0	200.0	190.0	10.0	43.3	44.5	25.3	0.00	0.00	6.0	0.0	3.2	105.0	2700.0	12.8
10	1	MAX						0.0	0.0	0.0	0.00	0.00	0.0	0.0	0.0			
10	1	(10)						43.3	57.6	76.4	-7.86	0.00	38.5	2700.0	3.2			
10	2	(11)		100.0	200.0	190.0	10.0	273.8	211.8	159.5	0.01	0.00	43.7	339.1	14.3	105.0	2700.0	12.8
10	2	MAX						0.0	0.0	0.0	0.00	0.00	0.0	0.0	0.0			
10	2	(10)	*					273.8	274.1	402.5	-40.61	-40.61	98.7	2700.0	16.4			
10	3	(11)		100.0	200.0	190.0	10.0	25.9	58.8	11.4	0.00	0.00	3.0	0.0	4.5	91.0	2340.0	11.1
10	3	MAX						0.0	0.0	0.0	0.00	0.00	0.0	0.0	0.0			
10	3	(10)						25.9	76.1	78.9	-13.37	0.00	33.8	2340.0	4.3			
11	1	(12)		100.0	200.0	190.0	10.0	43.3	44.5	25.3	0.00	0.00	6.0	0.0	3.2	105.0	2700.0	12.8
11	1	MAX						43.3	0.0	50.4	2.33	0.00	33.4	2700.0	0.0			
11	1	(11)						43.3	44.5	25.3	0.00	0.00	6.0	0.0	3.2			
11	2	(12)		100.0	200.0	190.0	10.0	273.8	211.8	159.5	0.01	0.00	43.7	339.1	14.3	105.0	2700.0	12.8
11	2	MAX						273.8	0.0	200.6	0.01	0.00	68.2	1399.0	0.0			
11	2	(11)						273.8	211.8	159.5	0.01	0.00	43.7	339.1	14.3			
11	3	(12)		100.0	200.0	190.0	10.0	25.9	58.8	11.4	0.00	0.00	3.0	0.0	4.5	91.0	2340.0	11.1
11	3	MAX	*					25.9	0.0	88.6	15.75	0.00	35.6	2340.0	0.0			
11	3	(11)						25.9	58.8	11.4	0.00	0.00	3.0	0.0	4.5			
12	1	(1)		100.0	200.0	190.0	10.0	43.3	57.6	76.4	-7.86	0.00	38.5	2700.0	3.2	105.0	2700.0	12.8
12	1	MAX						0.0	0.0	0.0	0.00	0.00	0.0	0.0	0.0			
12	1	(12)						43.3	44.5	25.3	0.00	0.00	6.0	0.0	3.2			
12	2	(1)	*	100.0	200.0	190.0	10.0	273.8	274.1	402.5	-40.61	-40.61	98.7	2700.0	16.4	105.0	2700.0	12.8
12	2	MAX						0.0	0.0	0.0	0.00	0.00	0.0	0.0	0.0			
12	2	(12)						273.8	211.8	159.5	0.01	0.00	43.7	339.1	14.3			
12	3	(1)		100.0	200.0	190.0	10.0	25.9	76.1	78.9	-13.37	0.00	33.8	2340.0	4.3	91.0	2340.0	11.1
12	3	MAX						0.0	0.0	0.0	0.00	0.00	0.0	0.0	0.0			
12	3	(12)						25.9	58.8	11.4	0.00	0.00	3.0	0.0	4.5			

Table 1.1.9(1) CALCULATION OF INTERNAL STRESS IN REINFORCED
CONCRETE STRUCTURE: INLET PORTAL SECTION B-B

Member		1	2	3	4	5
Spot		2(outside)	mid(inside)	3(outside)	5(outside)	mid(inside)
M	t.m	159.00	200.90	129.50	154.40	66.10
Q	t	213.30	0.00	192.60	191.40	0.00
N	t	285.60	269.20	253.00	251.50	13.30
b	cm	100.00	100.00	100.00	100.00	100.00
h	cm	200.00	200.00	200.00	220.00	220.00
u	cm	90.00	90.00	90.00	100.00	100.00
d	cm	190.00	190.00	190.00	210.00	210.00
d'	cm					
d' / d		0.00	0.00	0.00	0.00	0.00
M' = M+N.u	t.m	416.04	443.18	357.20	405.90	79.40
M' / (b.d.d)	kg/cm ²	11.52	12.28	9.89	9.20	1.80
Q / (b.d)	kg/cm ²	11.23	0.00	10.14	9.11	0.00
f = M/N+u	cm	145.67	164.63	141.19	161.39	596.99
f / d		0.77	0.87	0.74	0.77	2.84
As		D19@150	D19@300	D19@150	D19@150	D19@150
	cm ²	19.10	9.54	19.10	19.10	19.10
As'						
	cm ²	0.00	0.00	0.00	0.00	0.00
As' / As		0.00	0.00	0.00	0.00	0.00
n		15.00	15.00	15.00	15.00	15.00
np=n.As/(bd)		0.015	0.008	0.015	0.014	0.014
C		3.61	4.91		3.63	11.67
S		1.31	5.20		1.36	52.26
Z		1.32	-		1.32	-
Sigma c	kg/cm ²	41.6	60.3	32.1	33.4	21.0
				-6.8		
Sigma s	kg/cm ²	225.8	957.1	618.6	188.3	1411.5
Tau	kg/cm ²	14.9	0.0	11.6	12.0	0.0
Sigma ca	kg/cm ²	105.0	105.0	105.0	105.0	91.0
Sigma sa	kg/cm ²	2700.0	2700.0	2700.0	2700.0	2340.0
Tau a	kg/cm ²	12.8	12.8	12.8	12.8	11.1
Case		2	2	2	2	3
Note						

*

Table 1.1.9(2) CALCULATION OF INTERNAL STRESS IN REINFORCED
CONCRETE STRUCTURE: INLET PORTAL SECTION B-B

Member		11	12
Spot		mid(inside)	12(outside)
M	t.m	88.60	159.50
Q	t	0.00	211.80
N	t	25.90	273.80
b	cm	100.00	100.00
h	cm	200.00	200.00
u	cm	90.00	90.00
d	cm	190.00	190.00
d'	cm		
d' / d		0.00	0.00
M' = M+N.u	t.m	111.91	405.92
M' / (b.d.d)	kg/cm2	3.10	11.24
Q / (b.d)	kg/cm2	0.00	11.15
f = M/N+u	cm	432.08	148.25
f / d		2.27	0.78
As		3.00	D19@150
	cm2	19.10	19.10
As'			
	cm2	0.00	0.00
As' / As		0.00	0.00
n		15.00	15.00
np=n.As/(bd)		0.015	0.015
C		10.62	3.72
S		41.94	1.58
Z		-	1.31
Sigma c	kg/cm2	32.9	41.8
Sigma s	kg/cm2	1950.4	266.5
Tau	kg/cm2	0.0	14.6
Sigma ca	kg/cm2	91.0	105.0
Sigma sa	kg/cm2	2340.0	2700.0
Tau a	kg/cm2	11.1	12.8
Case		3	2
Note			stirrup
			*

Table 1.1.10 STRUCTURAL ANALYSIS OF OUTLET TRANSITION

NOTES: * NEARS MAXIMUM STEEL AREA

HEI	CASE	POINT	SIGN	B	H	D1	D2	N	S	M	AS	ASD	SIGC	SIGS	TAU	SIGCA	SIGSA	SIGTAU
1	1	(1)	*	100.0	100.0	90.0	10.0	69.1	39.8	68.0	21.63	0.00	79.1	2340.0	5.0	91.0	2340.0	11.1
1	1	MAX						60.9	0.0	0.4	0.00	0.00	6.3	0.0	0.0			
1	1	(2)						59.8	5.4	0.9	0.00	0.00	6.5	0.0	0.8			
1	2	(1)		100.0	100.0	90.0	10.0	77.3	5.0	41.5	3.69	0.00	73.2	3000.0	0.6	210.0	3000.0	18.0
1	2	MAX						0.0	0.0	0.0	0.00	0.00	0.0	0.0	0.0			
1	2	(2)						67.9	5.0	60.8	13.45	0.00	82.4	3000.0	0.6			
2	1	(2)		100.0	100.0	90.0	10.0	59.1	10.2	0.9	0.00	0.00	6.5	0.0	1.4	91.0	2340.0	11.1
2	1	MAX						57.2	0.0	3.4	0.00	0.00	7.8	0.0	0.0			
2	1	(3)						54.5	14.4	5.1	0.00	0.00	8.5	0.0	2.3			
2	2	(2)	*	100.0	100.0	90.0	10.0	66.9	12.8	60.8	13.62	0.00	82.2	3000.0	1.6	210.0	3000.0	18.0
2	2	MAX						0.0	0.0	0.0	0.00	0.00	0.0	0.0	0.0			
2	2	(3)						62.2	11.5	36.2	3.94	0.00	66.2	3000.0	1.4			
3	1	(3)		100.0	100.0	90.0	10.0	54.4	14.7	5.1	0.00	0.00	8.5	0.0	2.3	91.0	2340.0	11.1
3	1	MAX						52.5	0.0	3.0	0.00	0.00	7.1	0.0	0.0			
3	1	(4)						50.9	12.1	2.5	0.00	0.00	6.6	0.0	1.8			
3	2	(3)	*	100.0	100.0	90.0	10.0	46.1	41.1	36.2	6.28	0.00	62.5	3000.0	5.0	210.0	3000.0	18.0
3	2	MAX						0.0	0.0	0.0	0.00	0.00	0.0	0.0	0.0			
3	2	(4)						44.7	17.3	32.9	5.48	0.00	59.4	3000.0	2.1			
4	1	(3)		100.0	100.0	90.0	10.0	50.2	15.0	2.5	0.00	0.00	6.5	0.0	2.2	91.0	2340.0	11.1
4	1	MAX						49.5	0.0	5.6	0.00	0.00	8.3	0.0	0.0			
4	1	(5)						48.9	13.1	0.6	0.00	0.00	5.2	0.0	1.8			
4	2	(3)		100.0	100.0	90.0	10.0	30.0	37.3	32.9	7.93	0.00	55.3	3000.0	4.5	210.0	3000.0	18.0
4	2	MAX						29.0	0.0	64.2	21.21	0.00	75.3	3000.0	0.0			
4	2	(5)						28.8	7.7	62.8	20.68	0.00	74.4	3000.0	0.9			
5	1	(5)		100.0	100.0	90.0	10.0	48.9	13.1	0.6	0.00	0.00	5.2	0.0	1.8	91.0	2340.0	11.1
5	1	MAX						49.5	0.0	5.6	0.00	0.00	8.3	0.0	0.0			
5	1	(6)						50.2	15.0	2.5	0.00	0.00	6.5	0.0	2.2			
5	2	(5)		100.0	100.0	90.0	10.0	28.8	7.7	62.8	20.68	0.00	74.4	3000.0	0.9	210.0	3000.0	18.0
5	2	MAX						29.0	0.0	64.2	21.21	0.00	75.3	3000.0	0.0			
5	2	(6)						30.0	37.3	32.9	7.93	0.00	55.3	3000.0	4.5			
6	1	(6)		100.0	100.0	90.0	10.0	50.9	12.1	2.5	0.00	0.00	6.6	0.0	1.8	91.0	2340.0	11.1
6	1	MAX						52.5	0.0	3.0	0.00	0.00	7.1	0.0	0.0			
6	1	(7)						54.4	14.7	5.1	0.00	0.00	8.5	0.0	2.3			
6	2	(6)		100.0	100.0	90.0	10.0	44.7	17.3	32.9	5.48	0.00	59.4	3000.0	2.1	210.0	3000.0	18.0
6	2	MAX						0.0	0.0	0.0	0.00	0.00	0.0	0.0	0.0			
6	2	(7)	*					48.1	41.1	36.2	6.28	0.00	62.5	3000.0	5.0			
7	1	(7)		100.0	100.0	90.0	10.0	54.5	14.4	5.1	0.00	0.00	8.5	0.0	2.3	91.0	2340.0	11.1
7	1	MAX						57.2	0.0	3.4	0.00	0.00	7.8	0.0	0.0			
7	1	(8)						59.1	10.2	0.9	0.00	0.00	6.5	0.0	1.4			
7	2	(7)		100.0	100.0	90.0	10.0	62.2	11.5	36.2	3.94	0.00	66.2	3000.0	1.4	210.0	3000.0	18.0
7	2	MAX						0.0	0.0	0.0	0.00	0.00	0.0	0.0	0.0			
7	2	(8)	*					66.9	12.8	60.8	13.62	0.00	82.2	3000.0	1.6			
8	1	(8)		100.0	100.0	90.0	10.0	59.8	5.4	0.9	0.00	0.00	6.5	0.0	0.8	91.0	2340.0	11.1
8	1	MAX						60.9	0.0	0.4	0.00	0.00	6.3	0.0	0.0			
8	1	(9)	*					69.1	39.8	68.0	21.63	0.00	79.1	2340.0	5.0			
8	2	(8)		100.0	100.0	90.0	10.0	67.9	5.0	60.8	13.45	0.00	82.4	3000.0	0.6	210.0	3000.0	18.0
8	2	MAX						0.0	0.0	0.0	0.00	0.00	0.0	0.0	0.0			
8	2	(9)						77.3	5.0	41.5	3.69	0.00	73.2	3000.0	0.6			
9	1	(1)		100.0	100.0	90.0	10.0	39.8	65.5	68.0	27.58	0.00	72.9	2340.0	8.1	91.0	2340.0	11.1
9	1	MAX						39.8	0.0	59.7	22.96	0.00	68.3	2340.0	0.0			
9	1	(9)						39.8	65.5	68.0	27.58	0.00	72.9	2340.0	8.1			
9	2	(1)		100.0	100.0	90.0	10.0	-5.0	67.5	41.5	17.35	0.00	51.3	3000.0	8.0	210.0	3000.0	18.0
9	2	MAX						-5.0	0.0	90.1	37.79	0.00	82.5	3000.0	0.0			
9	2	(9)						-5.0	67.5	41.5	17.35	0.00	51.3	3000.0	8.0			

Table 1.1.11 CALCULATION OF INTERNAL STRESS IN REINFORCED
CONCRETE STRUCTURE: OUTLET TRANSITION

Member		1	4	4	9	9
Spot		1(outside)	5(outside)	mid(inside)	9(outside)	mid(inside)
M	t.m	68.00	62.80	64.20	68.00	90.10
Q	t	39.80	7.70	0.00	65.50	0.00
N	t	69.10	28.80	29.00	39.80	-5.00
b	cm	100.00	100.00	100.00	100.00	100.00
h	cm	100.00	100.00	100.00	100.00	100.00
u	cm	40.00	40.00	40.00	40.00	40.00
d	cm	90.00	90.00	90.00	90.00	90.00
d'	cm					
d' / d		0.00	0.00	0.00	0.00	0.00
M' = M+N.u	t.m	95.64	74.32	75.80	83.92	88.10
M' / (b.d.d)	kg/cm2	11.81	9.18	9.36	10.36	10.88
Q / (b.d)	kg/cm2	4.42	0.86	0.00	7.28	0.00
f = M/N+u	cm	138.41	258.06	261.38	210.85	-1762.00
f / d		1.54	2.87	2.90	2.34	-19.58
As		D22@150	D22@150	D22@150	D25@150	D29@150
	cm2	25.80	25.80	25.80	33.80	42.90
As'						
	cm2	0.00	0.00	0.00	0.00	0.00
As' / As		0.00	0.00	0.00	0.00	0.00
n		15.00	15.00	15.00	15.00	15.00
np=n.As/(bd)		0.043	0.043	0.043	0.056	0.072
C		6.33	7.48	7.49	6.56	7.24
S		11.30	17.70	17.80	12.48	16.30
Z		1.14	1.11	-	1.13	-
Sigma c	kg/cm2	74.7	68.6	70.1	67.9	78.8
Sigma s	kg/cm2	2000.5	2436.0	2498.1	1939.1	2659.1
Tau	kg/cm2	5.0	0.9	0.0	8.2	0.0
Sigma ca	kg/cm2	91.0	210.0	210.0	91.0	210.0
Sigma sa	kg/cm2	2340.0	3000.0	3000.0	2340.0	3000.0
Tau a	kg/cm2	11.1	18.0	18.0	11.1	18.0
Case		1	2	2	1	2
Note						

Table 1.1.12 STRUCTURAL ANALYSIS OF OUTLET PORTAL

NOTES: * MEANS MAXIMUM STEEL AREA

NEM	CASE	POINT	SIGN	B	H	D1	D2	N	S	M	AS	ASD	SIGC	SIGS	TAU	SIGCA	SIGSA	SIGTAU
1	1	(1)		100.0	100.0	90.0	10.0	49.3	7.4	6.9	0.00	0.00	9.0	0.0	1.2	70.0	1800.0	8.5
1	1	MAX						0.0	0.0	0.0	0.00	0.00	0.0	0.0	0.0			
1	1	(2)	*					45.4	17.0	13.3	0.01	0.00	14.5	96.5	2.4			
2	1	(2)	*	100.0	100.0	90.0	10.0	44.1	20.1	13.3	0.01	0.00	14.7	111.7	2.9	70.0	1800.0	8.5
2	1	MAX						35.0	0.0	4.3	0.00	0.00	6.1	0.0	0.0			
2	1	(3)						29.5	11.9	4.4	0.00	0.00	5.6	0.0	2.0			
3	1	(3)		100.0	100.0	90.0	10.0	29.2	12.4	4.4	0.00	0.00	5.5	0.0	2.1	70.0	1800.0	8.5
3	1	MAX						29.2	0.0	5.7	0.00	0.00	6.3	0.0	0.0			
3	1	(4)	*					29.2	12.4	4.4	0.00	0.00	5.5	0.0	2.1			
4	1	(4)		100.0	100.0	90.0	10.0	29.5	11.9	4.4	0.00	0.00	5.6	0.0	2.0	70.0	1800.0	8.5
4	1	MAX						35.0	0.0	4.3	0.00	0.00	6.1	0.0	0.0			
4	1	(5)	*					44.1	20.1	13.3	0.01	0.00	14.7	111.7	2.9			
5	1	(5)	*	100.0	100.0	90.0	10.0	45.4	17.0	13.3	0.01	0.00	14.5	96.5	2.4	70.0	1800.0	8.5
5	1	MAX						0.0	0.0	0.0	0.00	0.00	0.0	0.0	0.0			
5	1	(6)						49.3	7.4	6.9	0.00	0.00	9.0	0.0	1.2			

Table 1.1.13 CALCULATION OF INTERNAL STRESS IN REINFORCED
CONCRETE STRUCTURE: OUTLET PORTAL

Member		2
Spot		2(outside)
M	t.m	13.30
Q	t	20.10
N	t	44.10
b	cm	100.00
h	cm	100.00
u	cm	40.00
d	cm	90.00
d'	cm	
d' / d		0.00
M' = M+N.u	t.m	30.94
M'/(b.d.d)	kg/cm ²	3.82
Q/(b.d)	kg/cm ²	2.23
f = M/N+u	cm	70.16
f / d		0.78
As		D16@300
	cm ²	6.61
As'		
	cm ²	0.00
As' / As		0.00
n		15.00
np=n.As/(bd)		0.011
C		3.75
S		1.65
Z		1.30
Sigma c	kg/cm ²	14.3
Sigma s	kg/cm ²	94.7
Tau	kg/cm ²	2.9
Sigma ca	kg/cm ²	70.0
Sigma sa	kg/cm ²	1800.0
Tau a	kg/cm ²	8.5
Case		
Note		

Table 1.1.14 STRUCTURAL ANALYSIS OF STEEL SUPPORT
(TUNNEL TYPE-I)

Point	α_i (Degree)	α_i (Radian)	θ_i (Radian)	X_i (m)	Y_i (m)	W_i (ton)	A_i (ton)	$\sin(\theta_i, \theta_{i+1})$	$\cos(\theta_i, \alpha_i)$	$\cos(\theta_{i+1}, \alpha_i)$	\overline{T}_i (ton)	\overline{F}_i (ton)	$\frac{A_i}{\overline{F}_i}$	T_i (ton)
1	90.00	1.57	1.57	0.00	-0.00			0.1189	1.0000	0.9928	1.0000			
2	76.15	1.33	1.45	0.11	0.91	1.59	2.29	0.2393	0.9926	0.9928	0.9998	0.2410	9.51	24.12
3	62.31	1.09	1.21	0.43	1.76	3.08	3.52	0.2393	0.9926	0.9928	0.9996	0.2410	14.59	24.12
4	48.46	0.85	0.97	0.95	2.52	4.40	4.35	0.2393	0.9926	0.9928	0.9994	0.2409	18.06	24.11
5	34.62	0.60	0.73	1.64	3.13	5.47	5.03	0.2393	0.9926	0.9928	0.9992	0.2409	20.87	24.11
6	20.77	0.36	0.48	2.45	3.55	6.21	5.81	0.2393	0.9926	0.9928	0.9990	0.2408	24.13	24.10
7	6.92	0.12	0.14	3.34	3.77	4.92	4.89	0.2401	0.9926	0.9927	0.9989	0.2416	20.03	24.10
8	0.00	0.00		3.80	3.80	0.00								
												MAX	24.13	

where,

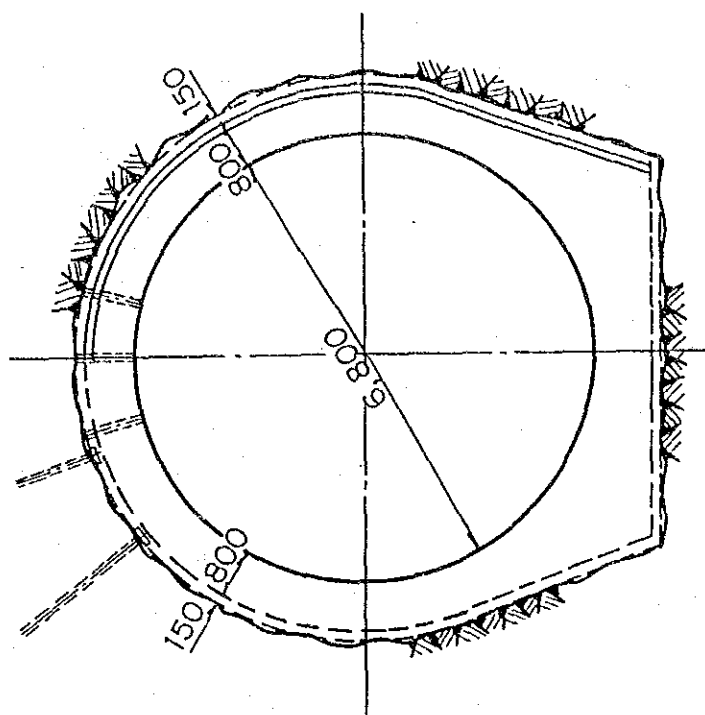
- $W_i = \Delta l_i \cdot H \cdot b \cdot \gamma$
 H : Height of rock to act as load (= 1.95 m)
 b : Interval of steel support (= 1.5 m)
 γ : Unit weight of rock (= 2.5 t/m³)
 A_i : $A_i = W_i \cdot \cos \alpha_i$ (For $\alpha_i \leq \phi = 25^\circ$)
 $A_i = \frac{W_i}{\sin 65^\circ} \cdot \sin(115^\circ - \alpha_i)$ (For $\alpha_i > \phi = 25^\circ$)
 $\overline{T}_{i+1} = \frac{\overline{T}_i \cdot \cos(\theta_i - \alpha_i)}{\cos(\theta_{i+1} - \alpha_i)}$
 $\overline{F}_i = \frac{\overline{T}_i \cdot \sin(\theta_i - \alpha_{i+1})}{\cos(\theta_{i+1} - \alpha_i)}$
 $\overline{T}_i = \frac{\overline{T}_i \cdot (A_i / \overline{F}_i)_{\max}}{24.12 \text{ (ton)}}$
 $T_{\max} = 0.86 \times T_{\max} \times h = 0.86 \times 24.12 \times 0.0277 = 0.57 \text{ (t}\cdot\text{m)}$

Table 1.1.15 STRUCTURAL ANALYSIS OF STEEL SUPPORT
(TUNNEL TYPE-II)

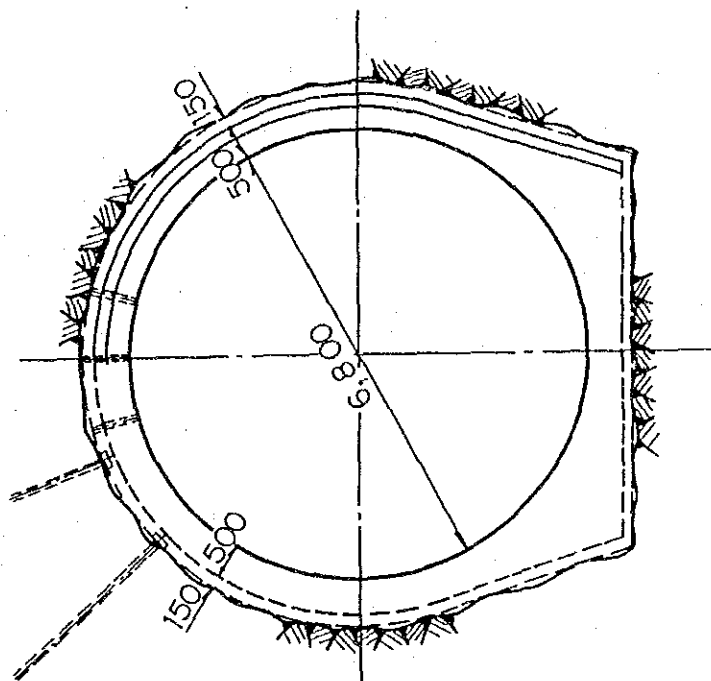
Point	α_i (Degree)	α_i (Radian)	θ_i (Radian)	X_i (m)	Y_i (m)	W_i (ton)	A_i (ton)	$\sin(\theta_i - \theta_{i+1})$	$\cos(\theta_i - \alpha_i)$	$\cos(\theta_{i+1} - \alpha_i)$	\bar{T}_i (ton)	\bar{F}_i (ton)	$\frac{A_i}{\bar{F}_i}$	T_i (ton)
1	90.00	1.57	1.57	0.00	-0.00			0.1189	1.0000	0.9928	1.0000			
2	76.15	1.33	1.45	0.11	0.91	2.98	4.32	0.2393	0.9926	0.9928	0.9998	0.2410	17.89	50.98
3	62.31	1.09	1.21	0.43	1.76	5.80	6.61	0.2393	0.9926	0.9928	0.9996	0.2410	27.44	50.97
4	48.46	0.85	0.97	0.95	2.52	8.28	8.19	0.2393	0.9926	0.9928	0.9994	0.2409	33.98	50.96
5	34.62	0.60	0.73	1.64	3.13	10.29	9.45	0.2393	0.9926	0.9928	0.9992	0.2409	39.25	50.95
6	20.77	0.36	0.48	2.45	3.55	11.69	10.93	0.2393	0.9926	0.9928	0.9990	0.2408	45.38	50.94
7	6.92	0.12	0.14	3.34	3.77	12.41	12.32	0.2401	0.9926	0.9927	0.9989	0.2416	50.99	50.94
8	0.00	0.00		3.80	3.80	0.00								
												MAX	50.99	

where,

- W_i = $\Delta l_i \cdot H \cdot b \cdot \gamma$
 H : Height of rock to act as load (= 5.5 m)
 b : Interval of steel support (= 1.50m)
 γ : Unit weight of rock (= 2.5 t/m³)
 A_i : $A_i = W_i \cdot \cos \alpha_i$ (For $\alpha_i \leq \phi = 25^\circ$)
 $A_i = \frac{W_i \sin 65^\circ}{\sin(115^\circ - \alpha_i)}$ (For $\alpha_i > \phi = 25^\circ$)
 $\bar{T}_{i+1} = \frac{\bar{T}_i \cdot \cos(\theta_i - \alpha_i)}{\cos(\theta_{i+1} - \alpha_i)}$
 $\bar{F}_i = \frac{\bar{T}_i \cdot \sin(\theta_i - \alpha_{i+1})}{\cos(\theta_{i+1} - \alpha_i)}$
 $\bar{T}_i = \frac{\bar{T}_i \cdot (A_i / \bar{F}_i)_{\max}}{50.98 \text{ (ton)}}$
 $T_{\max} = 50.98 \text{ (ton)}$
 $M_{\max} = 0.86 \times T_{\max} \times h = 0.86 \times 50.98 \times 0.0277 = 1.21 \text{ (t}\cdot\text{m)}$



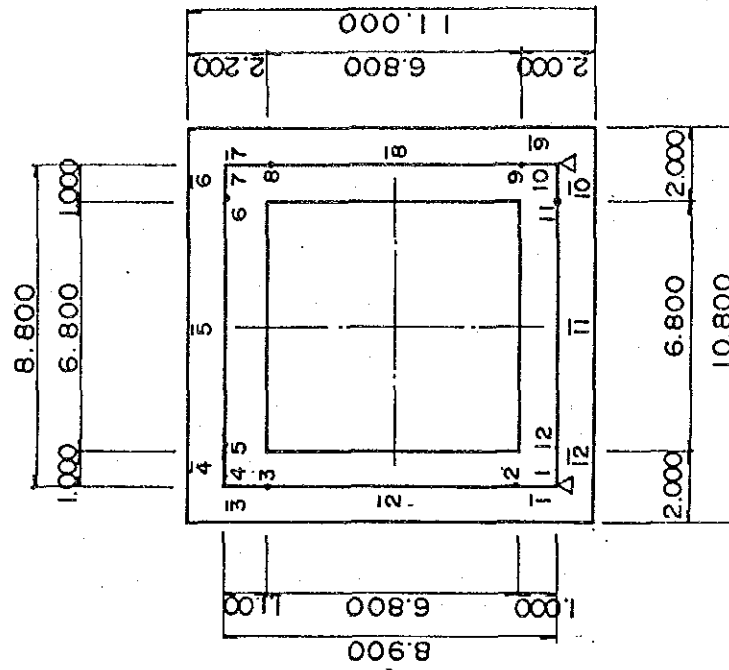
TYPE - II



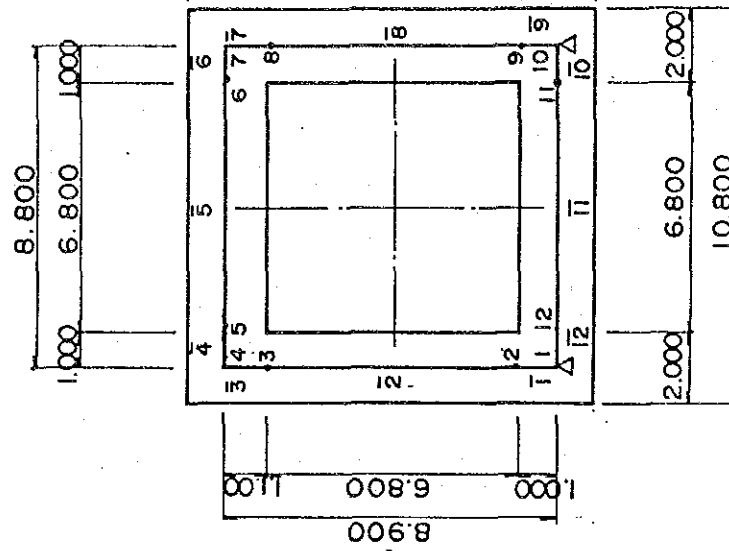
TYPE - I

Types of diversion tunnel

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SECTION A - A

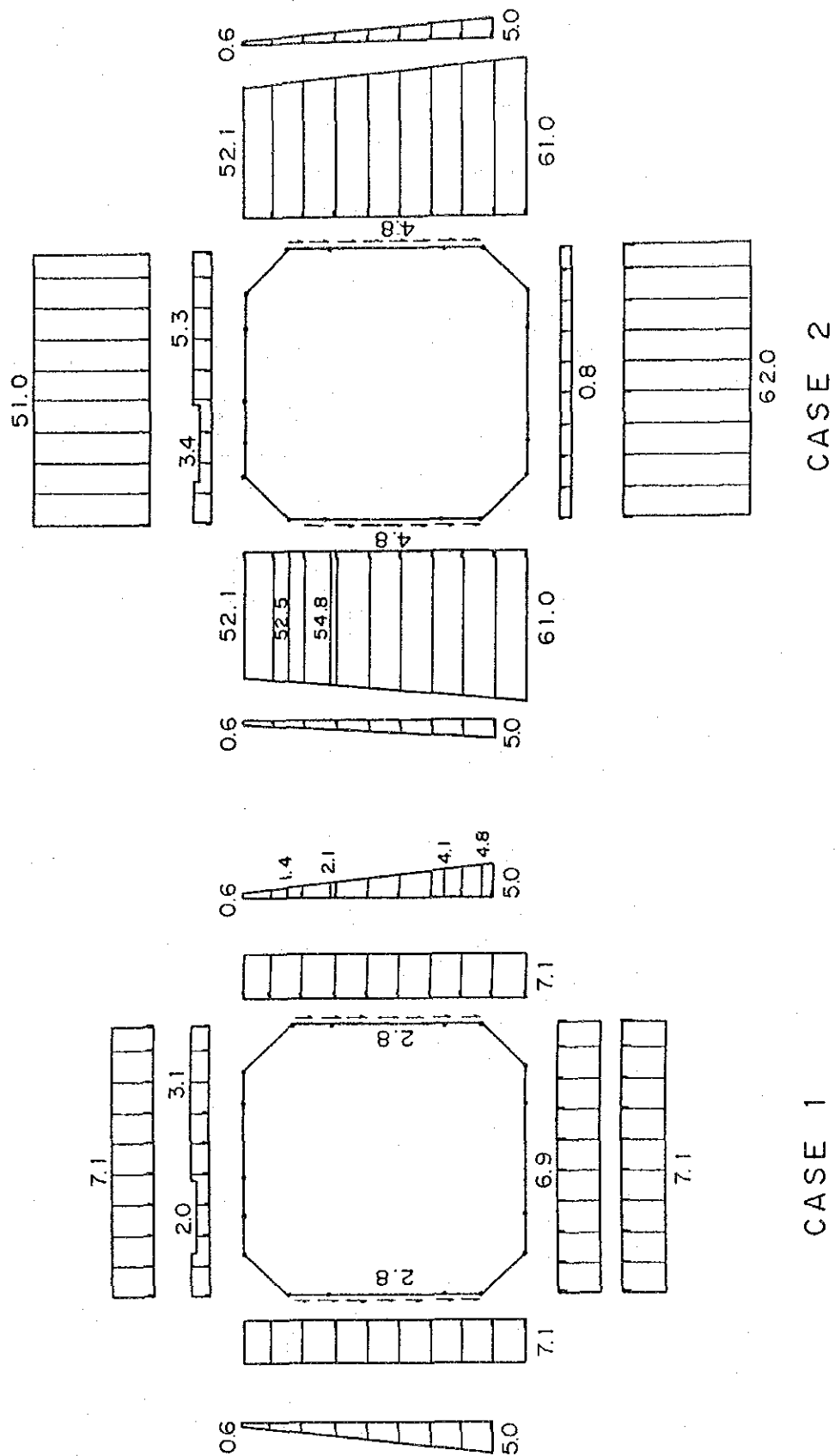


SECTION B - B

Section and dimension of inlet portal

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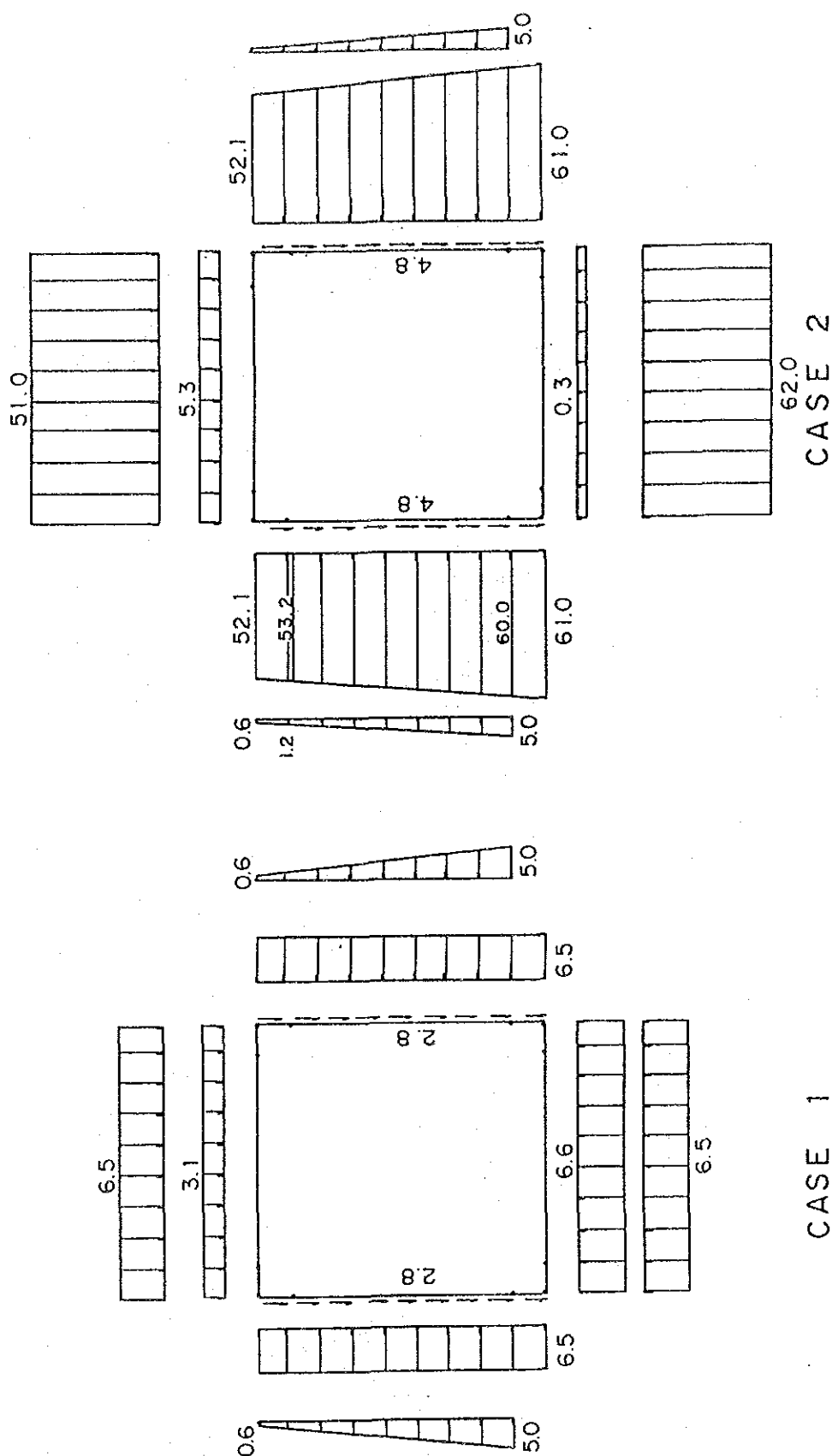
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Loading diagram of inlet portal (section A-A)

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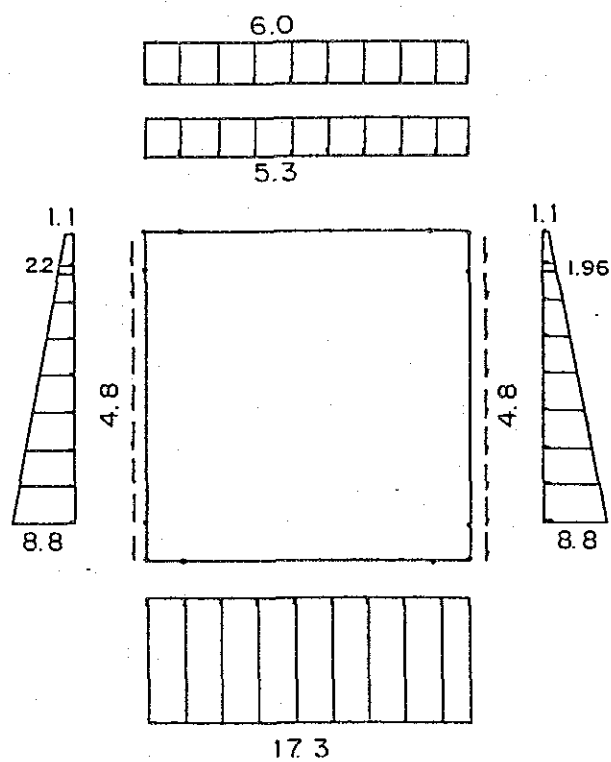
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Loading diagram of inlet portal (section B-B)

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CASE 3

Fig. 1.1.5

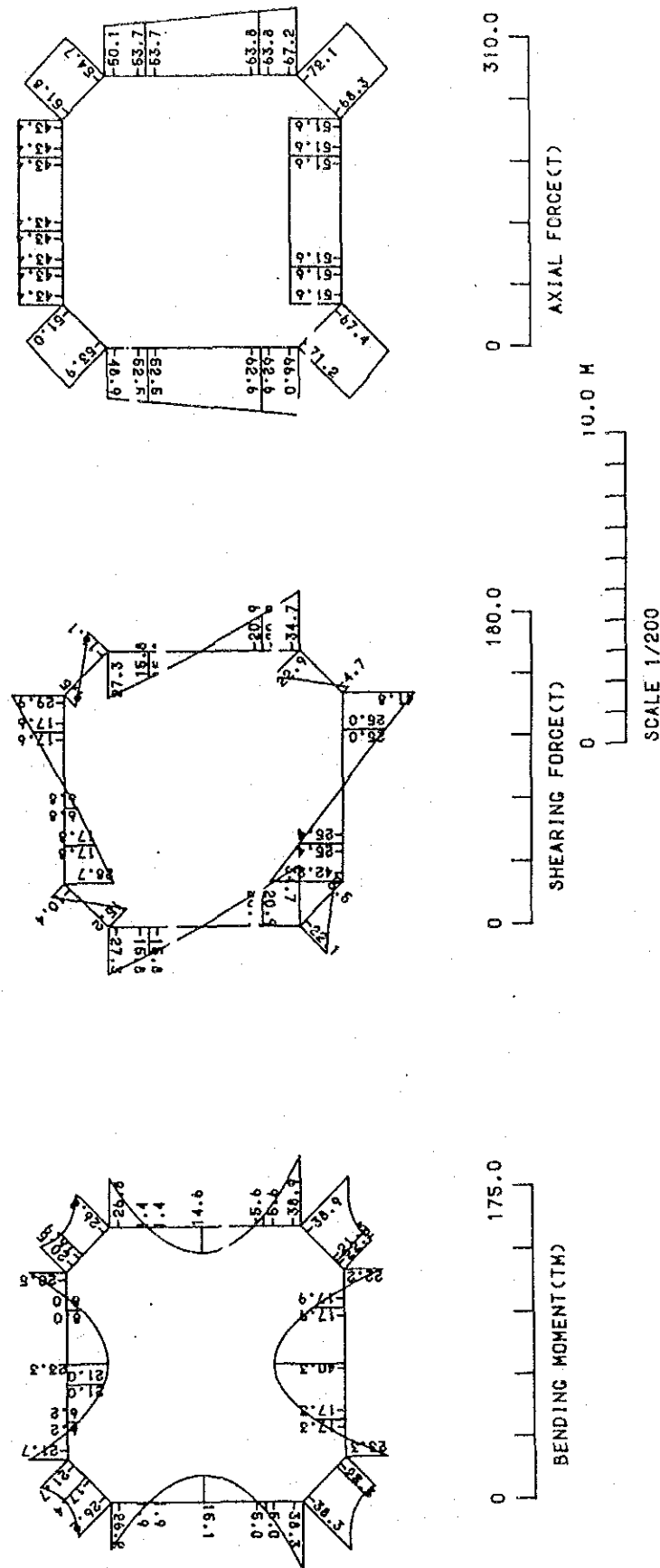
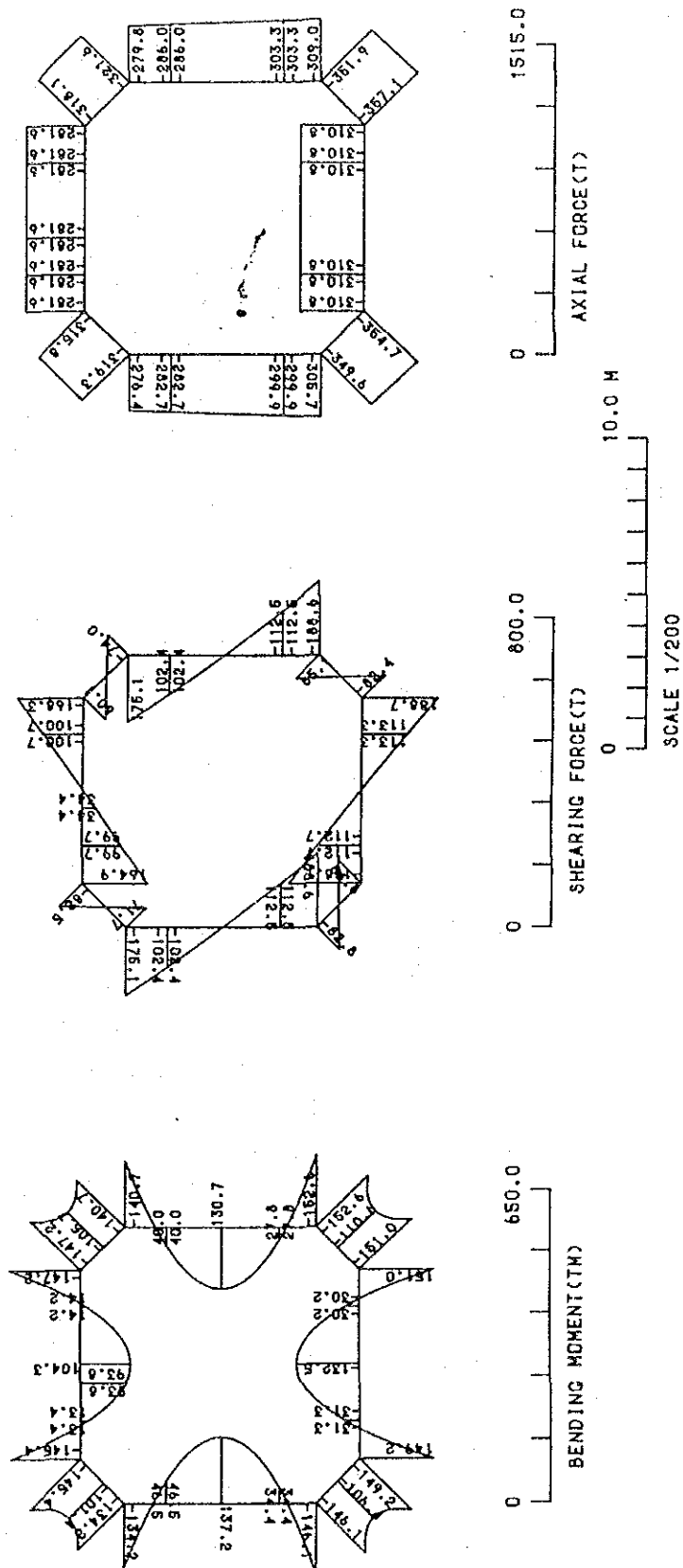


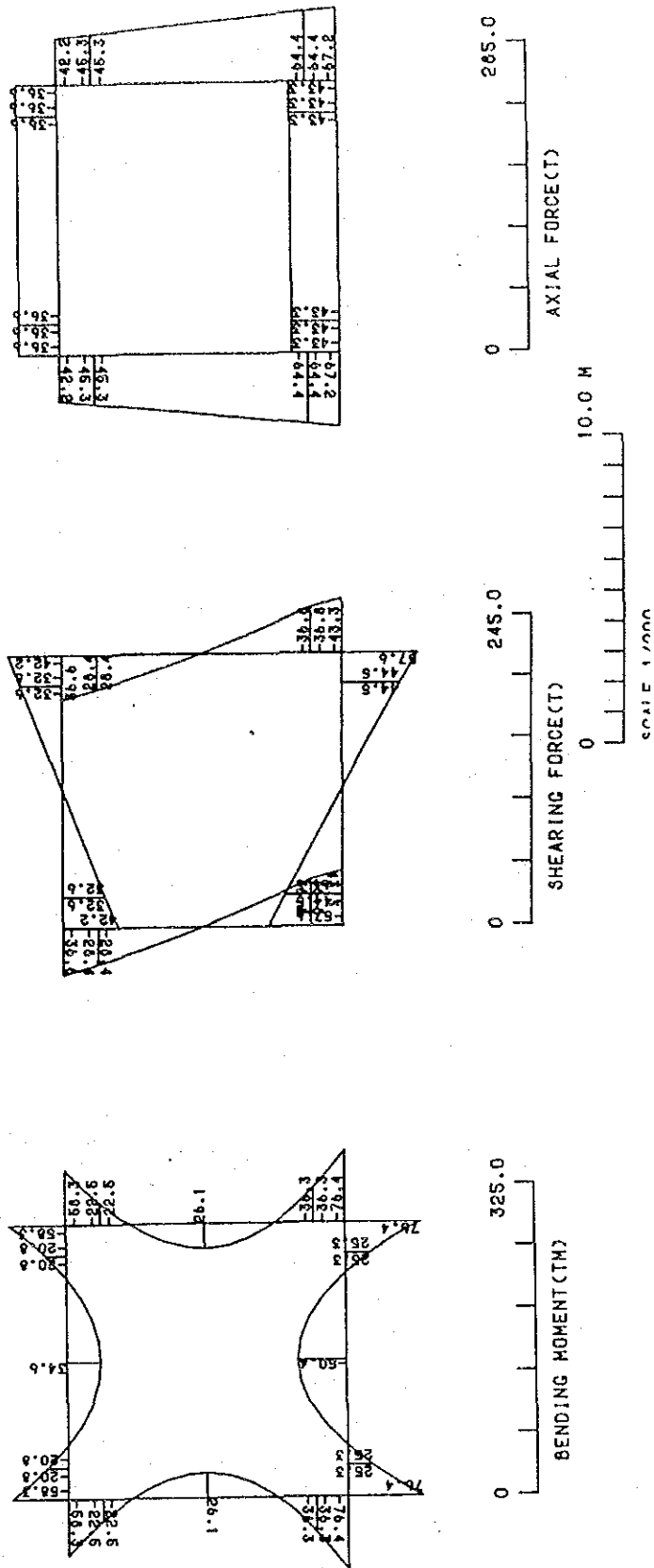
Fig. 1.1.6



Bending moment shearing and axial force diagram
inlet portal section A-A (case -2)

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PORT LOUIS WATER SUPPLY PROJECT

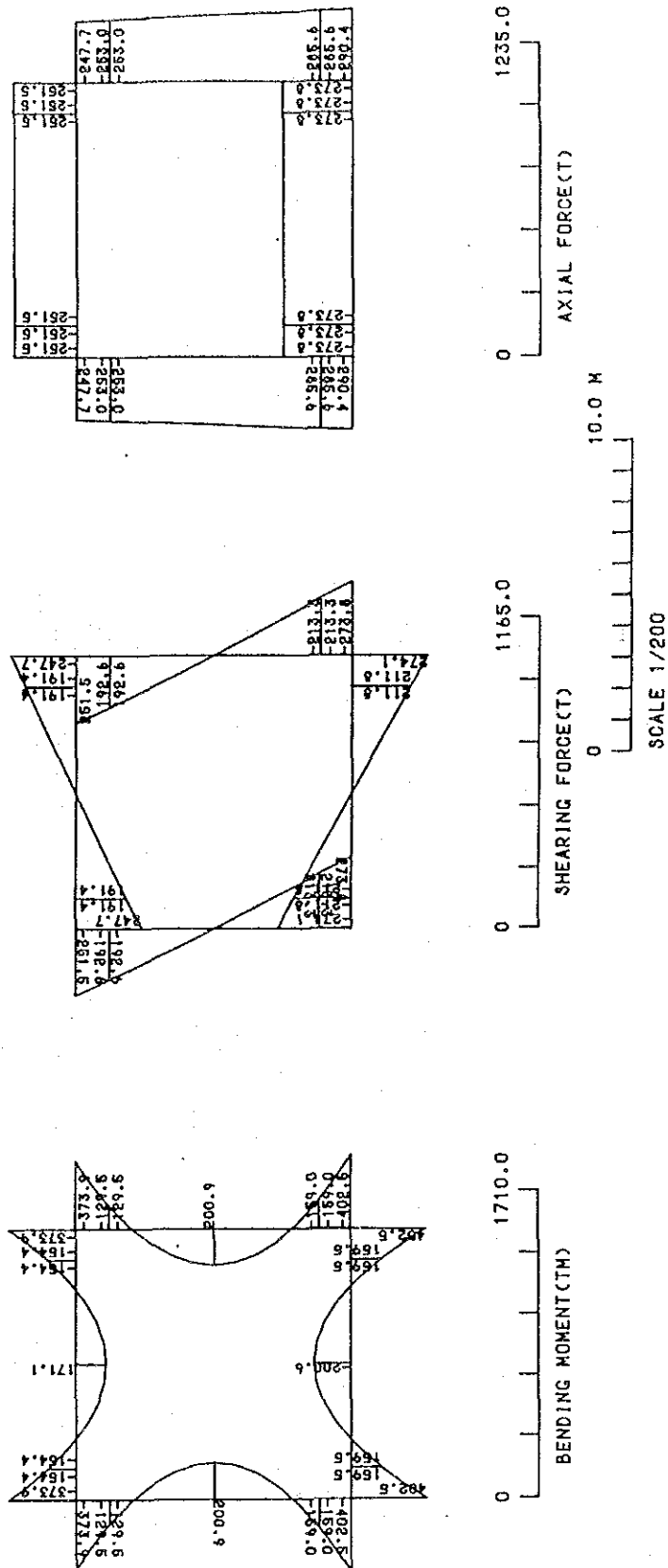
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**Bending moment shearing and axial force diagram
inlet portal section B-B (case -1)**

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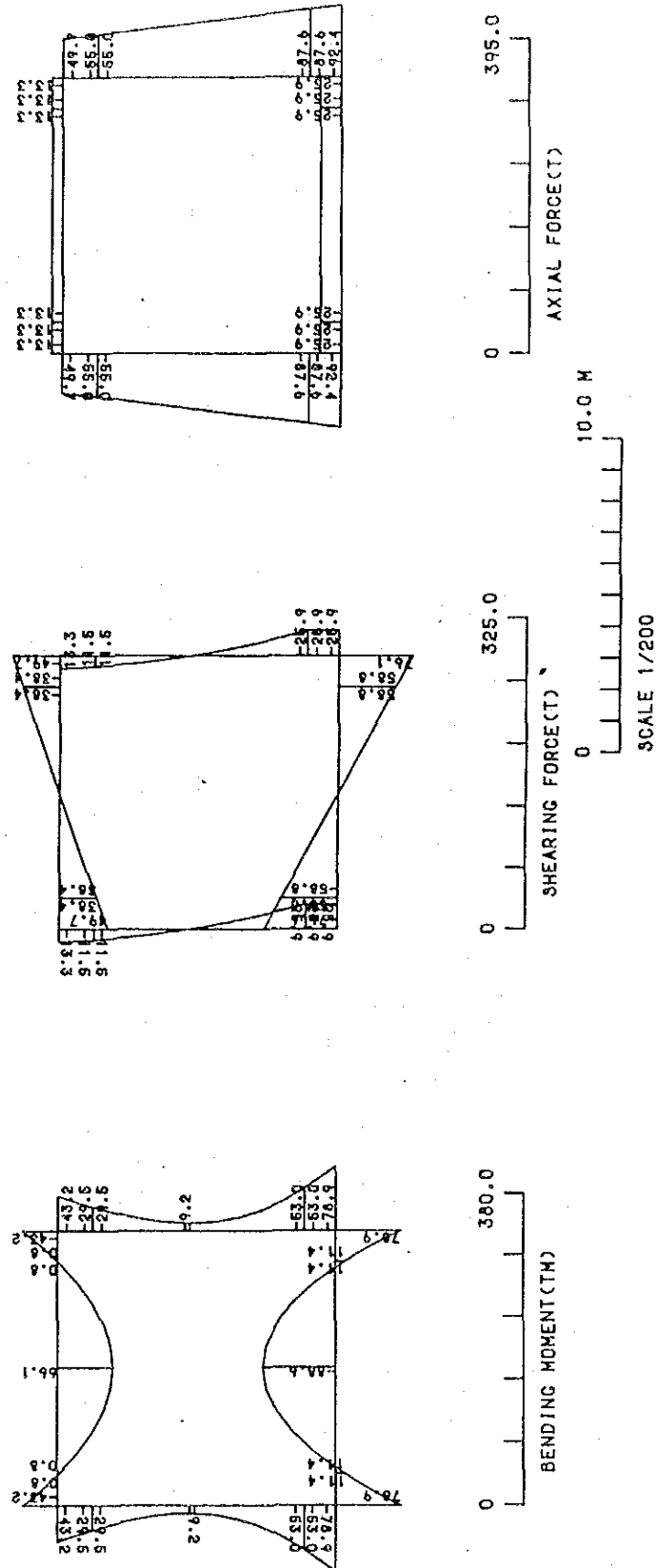
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Bending moment shearing and axial force diagram
inlet portal section B-B (case -2)

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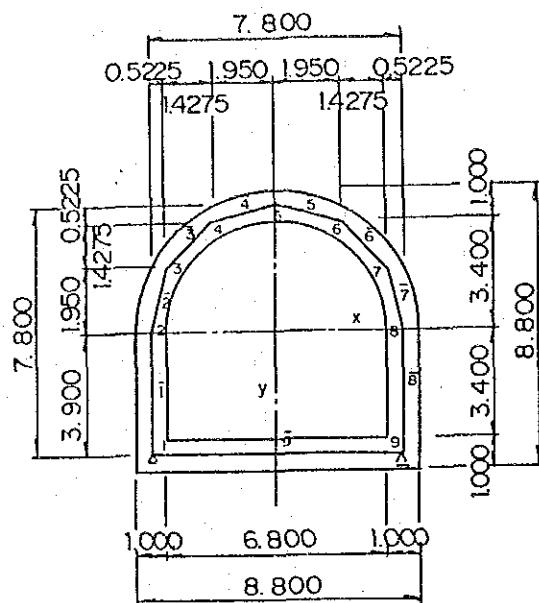
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Bending moment shearing and axial force diagram
inlet portal section B-B (case -3)

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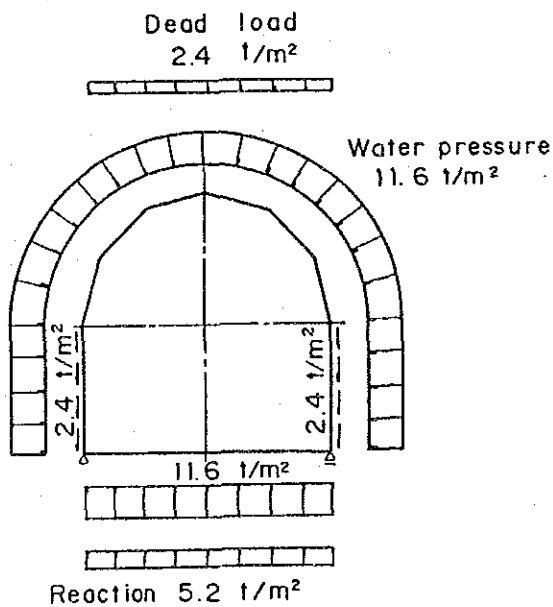
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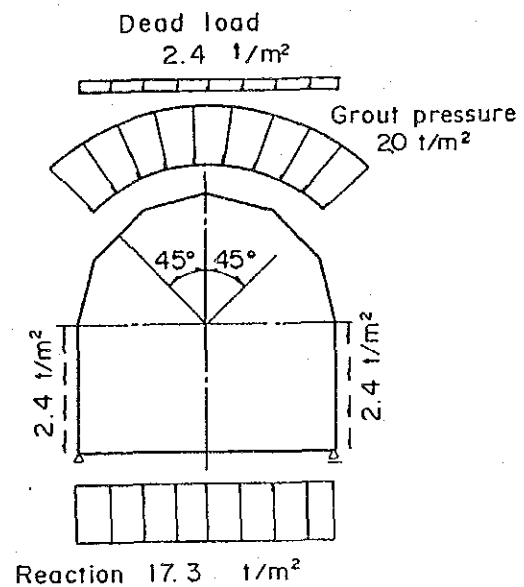
$$A = 1.0 \text{ m}^2$$

$$I = 0.0833 \text{ m}^2$$

	x (m)	y (m)
1	-3.900	3.900
2	-3.900	0.000
3	-3.3775	-1.950
4	-1.950	-3.3775
5	0.000	-3.900
6	1.950	-3.3775
7	3.3775	-1.950
8	3.900	0.000
9	3.900	3.900



(1) During diversion



(2) Grouting condition

Fig. 1.1.11

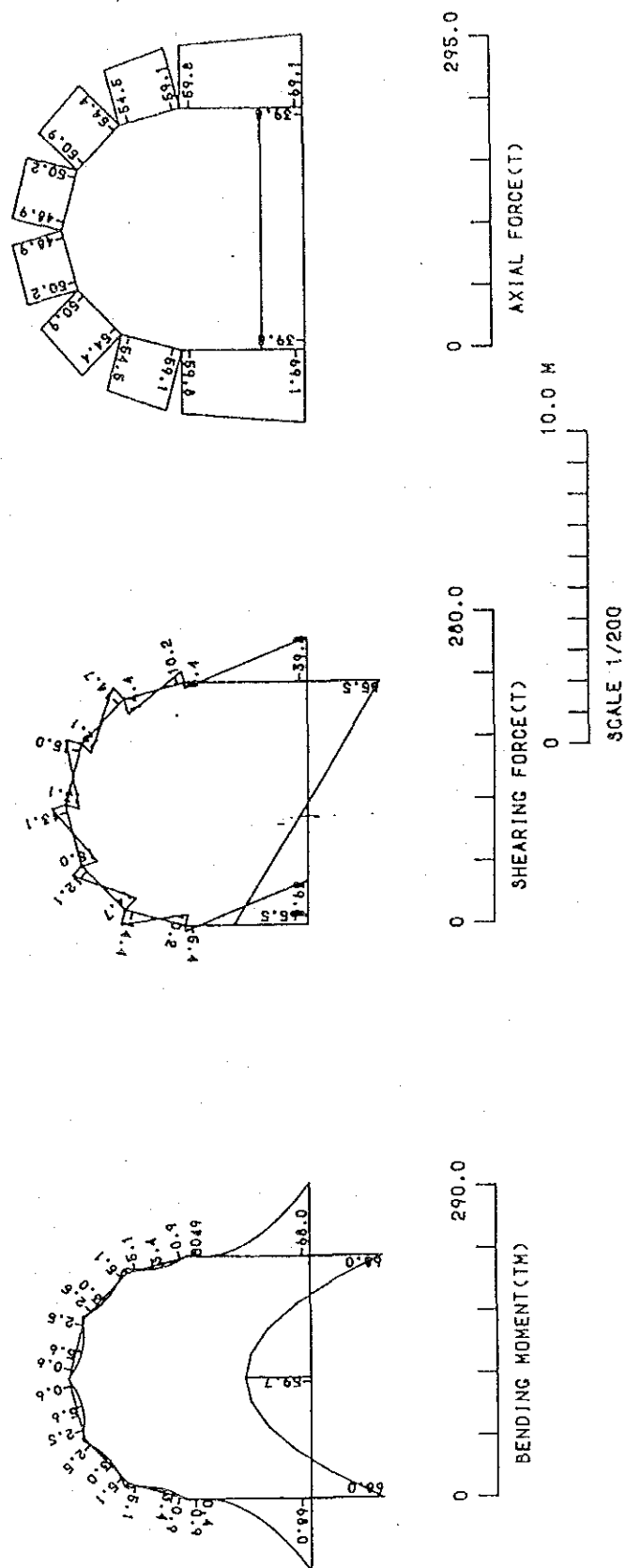
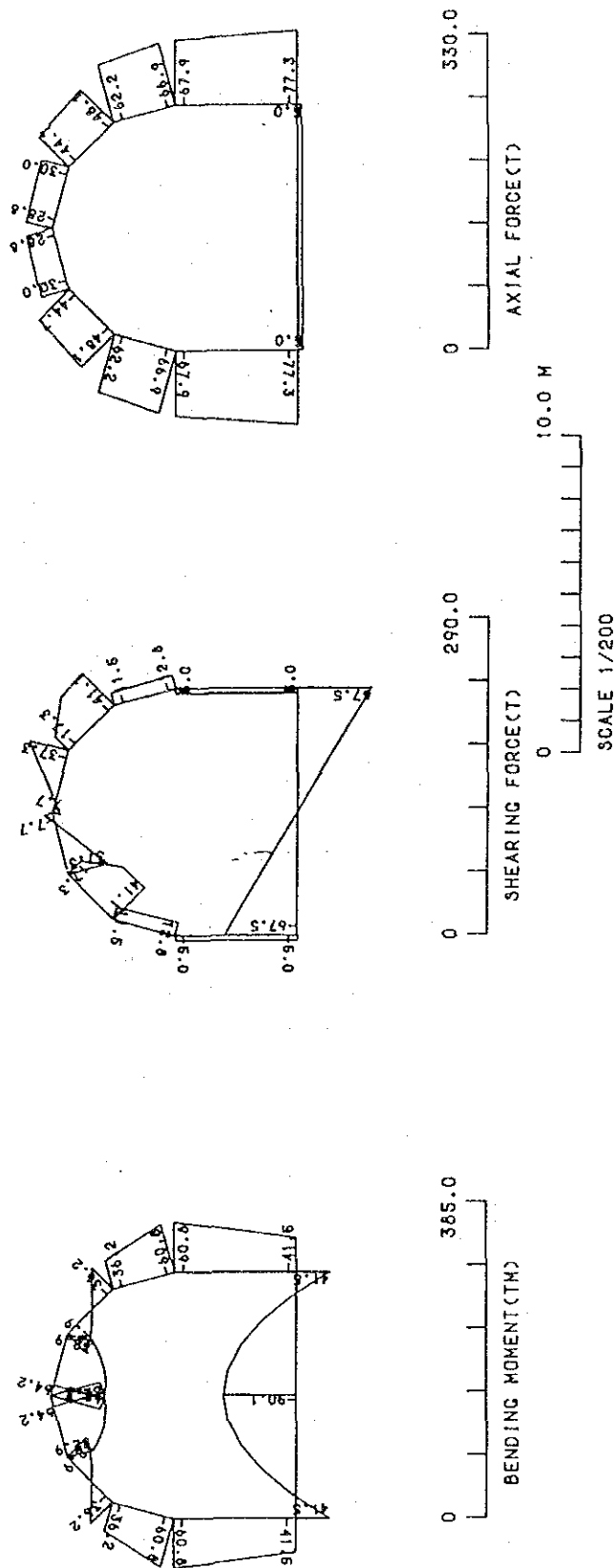


Fig. 1.1.12

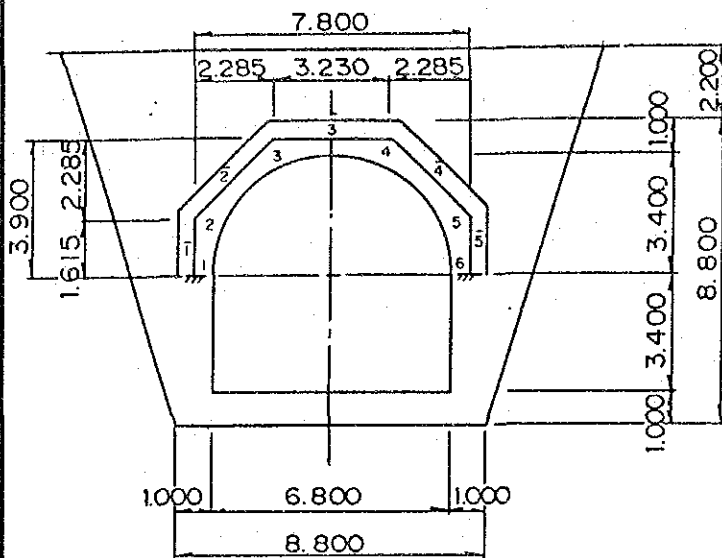


Bending moment shearing and axial force diagram
transition of diversion outlet (case-2)

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PORT LOUIS WATER SUPPLY PROJECT

JAPAN INTERNATIONAL COOPERATION AGENCY

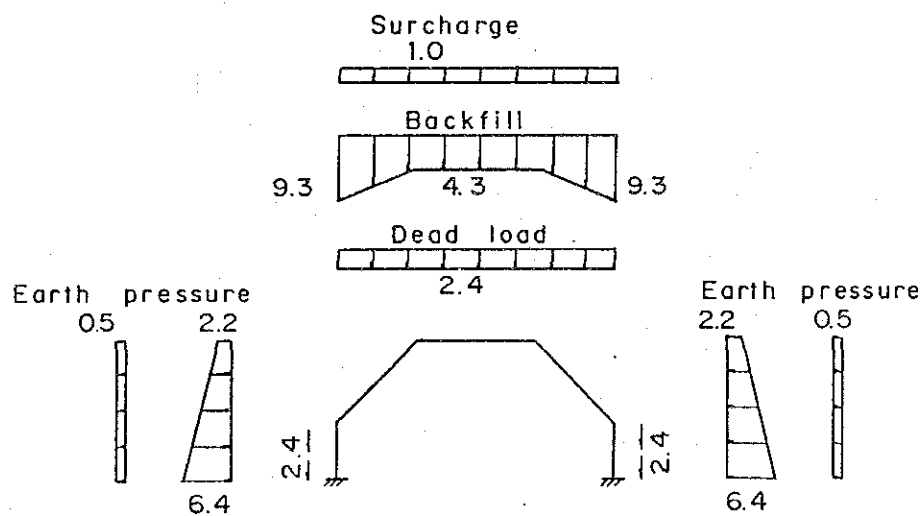
Fig. 1.1.13



$$A = 1.0 \text{ m}^2$$

$$I = 0.0835 \text{ m}^4$$

	x (m)	y (m)
1	-3.900	3.900
2	-3.900	2.285
3	-1.615	0.000
4	1.615	0.000
5	3.900	2.285
6	3.900	3.900

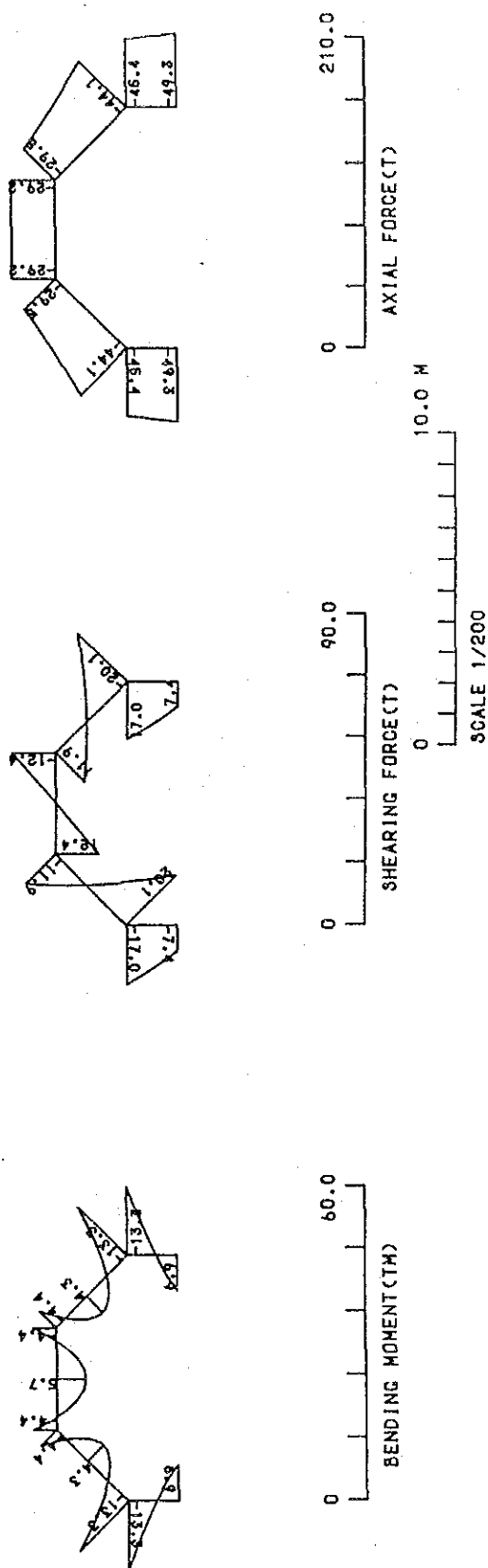


Load diagram of outlet portal

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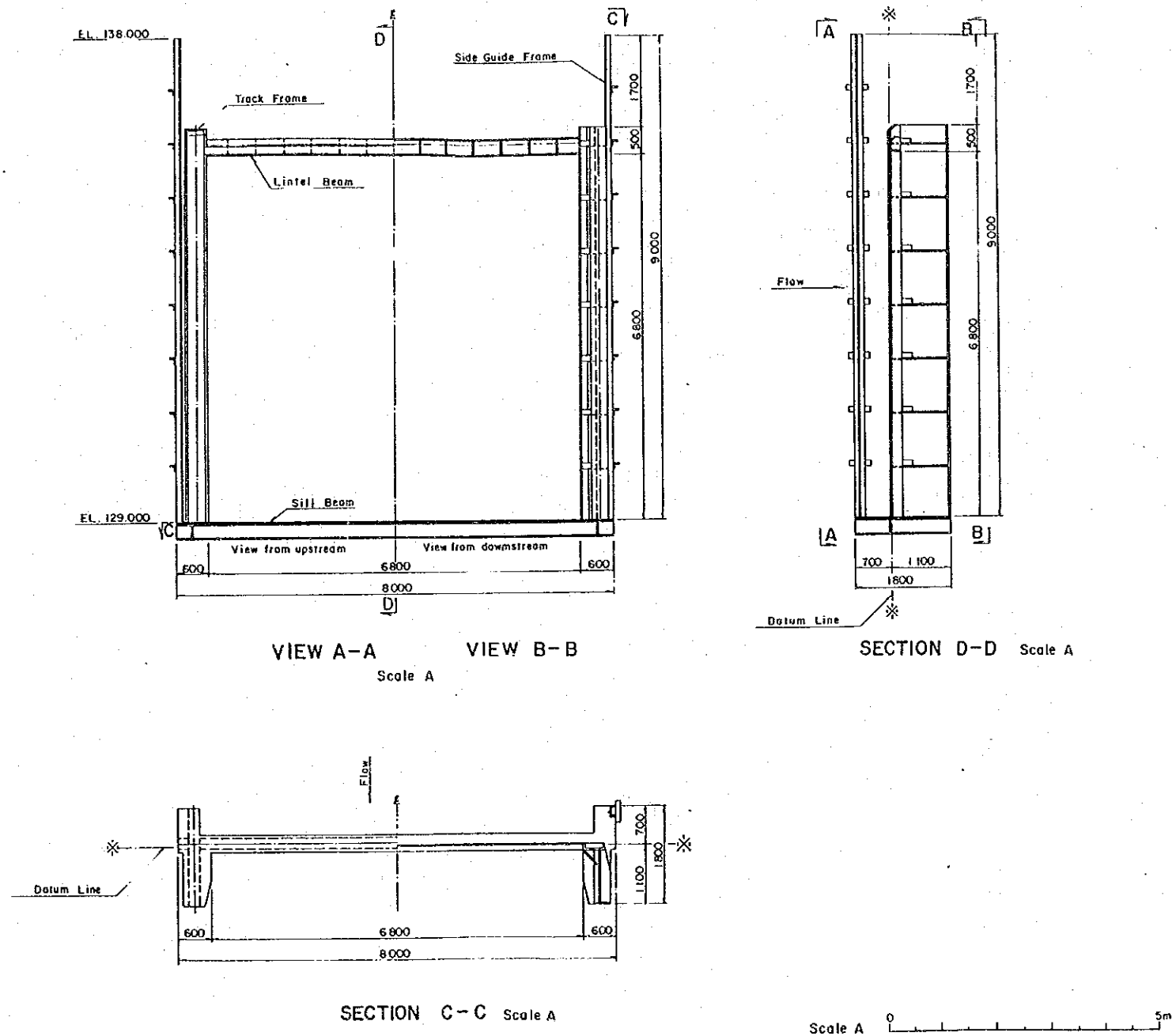
Fig. 1.1.14



Bending moment shearing and axial force diagram,
Outlet portal

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METAL WORK
GUIDE FRAME OF DIVERSION GATE

GOVERNMENT OF MAURITIUS
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PART II WATER PRESSURE TEST

RECORD OF WATER PRESSURE TEST
DEPTH(m): 2-5

HOLE NO. JD-3

GAUGE PRESS.	INJECTION Q'ty	TEST LENGTH	HOLE DIA.	GAUGE HEIGHT	WATER LEVEL	TEST PRESS.	LUGEON VALUE	k-VALUE
kg/cm2	lit/min	lit/min/m	m	mm	m	kg/cm2		cm/sec
0.5	51.4	17.13	3.0	66.0	1.20	3.50	1.0	176.6
1.0	65.4	21.80	3.0	66.0	1.20	3.50	1.5	148.3
1.5	70.4	23.47	3.0	66.0	1.20	3.50	2.0	119.1
2.0	76.6	25.53	3.0	66.0	1.20	3.50	2.5	103.4
1.5	69.0	23.00	3.0	66.0	1.20	3.50	2.0	116.8
1.0	51.0	17.00	3.0	66.0	1.20	3.50	1.5	115.6
0.5	36.0	12.00	3.0	66.0	1.20	3.50	1.0	123.7

AVERAGE 129.1 0.001544
k-VALUE: COEFFICIENT OF PERMEABILITY

RECORD OF WATER PRESSURE TEST
DEPTH(m): 5-10

HOLE NO. JD-3

GAUGE PRESS.	INJECTION Q'ty	TEST LENGTH	HOLE DIA.	GAUGE HEIGHT	WATER LEVEL	TEST PRESS.	LUGEON VALUE	k-VALUE
kg/cm2	lit/min	lit/min/m	m	mm	m	kg/cm2		cm/sec
1.0	12.2	2.44	5.0	66.0	1.20	7.50	1.9	13.0
2.0	29.2	5.84	5.0	66.0	1.20	7.50	2.9	20.3
3.0	49.8	9.96	5.0	66.0	1.20	7.50	3.9	25.7
4.0	41.6	8.32	5.0	66.0	1.20	7.50	4.9	17.1
3.0	53.4	10.67	5.0	66.0	1.20	7.50	3.9	27.6
2.0	36.0	7.20	5.0	66.0	1.20	7.50	2.9	25.1
1.0	25.0	5.00	5.0	66.0	1.20	7.50	1.9	26.7

AVERAGE 22.2 0.000296
k-VALUE: COEFFICIENT OF PERMEABILITY
k-VALUE: COEFFICIENT OF PERMEABILITY

RECORD OF WATER PRESSURE TEST
DEPTH(m): 10 - 15

HOLE NO. JD-3

GAUGE PRESS.	INJECTION Q'ty	TEST LENGTH	HOLE DIA.	GAUGE HEIGHT	WATER LEVEL	TEST PRESS.	LUGEON VALUE	k-VALUE
kg/cm2	lit/min	lit/min/m	m	mm	m	kg/cm2		cm/sec
1.0	42.4	8.48	5.0	66.0	1.20	12.50	2.4	35.8
2.0	50.0	10.00	5.0	66.0	1.20	12.50	3.4	29.7
4.0	73.4	14.68	5.0	66.0	1.20	12.50	5.4	27.3
6.0	98.0	19.60	5.0	66.0	1.20	12.50	7.4	26.6
4.0	76.0	15.20	5.0	66.0	1.20	12.50	5.4	28.3
2.0	57.0	11.40	5.0	66.0	1.20	12.50	3.4	33.8
1.0	45.0	9.00	5.0	66.0	1.20	12.50	2.4	38.0

AVERAGE 31.4 0.000418
k-VALUE: COEFFICIENT OF PERMEABILITY

RECORD OF WATER PRESSURE TEST
DEPTH(m): 15-20

HOLE NO. JD-3

GAUGE PRESS.	INJECTION Q'ty	TEST LENGTH	HOLE DIA.	GAUGE HEIGHT	WATER LEVEL	TEST PRESS.	LUGEON VALUE	k-VALUE
kg/cm2	lit/min	lit/min/m	m	mm	m	kg/cm2		cm/sec
2.0	44.4	8.88	5.0	66.0	1.20	16.45	3.8	23.6
4.0	65.6	13.12	5.0	66.0	1.20	16.45	5.8	22.8
6.0	82.2	16.44	5.0	66.0	1.20	16.45	7.8	21.2
8.0	97.4	19.48	5.0	66.0	1.20	16.45	9.8	19.9
6.0	84.0	16.80	5.0	66.0	1.20	16.45	7.8	21.6
4.0	71.0	14.20	5.0	66.0	1.20	16.45	5.8	24.6
2.0	55.5	11.10	5.0	66.0	1.20	16.45	3.8	29.5

AVERAGE 23.3 0.000311
k-VALUE: COEFFICIENT OF PERMEABILITY

RECORD OF WATER PRESSURE TEST
DEPTH(m): 20-25

HOLE NO. JD-3

GAUGE PRESS.	INJECTION Q'ty	TEST LENGTH	HOLE DIA.	GAUGE HEIGHT	WATER LEVEL	TEST PRESS.	LUGEON VALUE	k-VALUE
kg/cm2	lit/min	lit/min/m	m	mm	m	kg/cm2		cm/sec
2.0	0.9	0.18	5.0	66.0	1.20	19.42	4.1	0.000006
4.0	1.2	0.24	5.0	66.0	1.20	19.42	6.1	0.000005
7.0	41.2	8.24	5.0	66.0	1.20	19.42	9.1	0.000121
10.0	72.2	14.44	5.0	66.0	1.20	19.42	12.1	0.000159
7.0	59.0	11.80	5.0	66.0	1.20	19.42	9.1	0.000173
4.0	38.0	7.60	5.0	66.0	1.20	19.42	6.1	0.000167
2.0	24.0	4.80	5.0	66.0	1.20	19.42	4.1	0.000157

AVERAGE
k-VALUE: COEFFICIENT OF PERMEABILITY

8.5 0.000113

RECORD OF WATER PRESSURE TEST
DEPTH(m): 25-30

HOLE NO. JD-3

GAUGE PRESS.	INJECTION Q'ty	TEST LENGTH	HOLE DIA.	GAUGE HEIGHT	WATER LEVEL	TEST PRESS.	LUGEON VALUE	k-VALUE
kg/cm2	lit/min	lit/min/m	m	mm	m	kg/cm2		cm/sec
2.0	47.8	9.56	5.0	66.0	1.20	19.41	4.1	0.000314
4.0	67.6	13.52	5.0	66.0	1.20	19.41	6.1	0.000297
7.0	89.2	17.84	5.0	66.0	1.20	19.41	9.1	0.000262
10.0	107.0	21.40	5.0	66.0	1.20	19.41	12.1	0.000236
7.0	88.0	17.60	5.0	66.0	1.20	19.41	9.1	0.000259
4.0	73.5	14.70	5.0	66.0	1.20	19.41	6.1	0.000323
2.0	56.5	11.30	5.0	66.0	1.20	19.41	4.1	0.000371

AVERAGE
k-VALUE: COEFFICIENT OF PERMEABILITY

22.1 0.000294

RECORD OF WATER PRESSURE TEST
DEPTH(m): 30-35

HOLE NO. JD-3

GAUGE PRESS.	INJECTION Q'ty	TEST LENGTH	HOLE DIA.	GAUGE HEIGHT	WATER LEVEL	TEST PRESS.	LUGEON VALUE	k-VALUE
kg/cm2	lit/min	lit/min/m	m	mm	m	kg/cm2		cm/sec
2.0	52.2	10.44	5.0	66.0	1.20	19.66	4.1	0.000340
4.0	67.4	13.48	5.0	66.0	1.20	19.66	6.1	0.000295
7.0	90.2	18.04	5.0	66.0	1.20	19.66	9.1	0.000264
10.0	107.2	21.44	5.0	66.0	1.20	19.66	12.1	0.000236
7.0	86.0	17.20	5.0	66.0	1.20	19.66	9.1	0.000252
4.0	61.5	12.30	5.0	66.0	1.20	19.66	6.1	0.000269
2.0	46.0	9.20	5.0	66.0	1.20	19.66	4.1	0.000300

AVERAGE
k-VALUE: COEFFICIENT OF PERMEABILITY

21.0 0.000280

RECORD OF WATER PRESSURE TEST
DEPTH(m): 35-40

HOLE NO. JD-3

GAUGE PRESS.	INJECTION Q'ty	TEST LENGTH	HOLE DIA.	GAUGE HEIGHT	WATER LEVEL	TEST PRESS.	LUGEON VALUE	k-VALUE
kg/cm2	lit/min	lit/min/m	m	mm	m	kg/cm2		cm/sec
2.0	49.8	9.96	5.0	66.0	1.20	28.02	4.9	0.000269
4.0	66.4	13.28	5.0	66.0	1.20	28.02	6.9	0.000256
7.0	88.4	17.68	5.0	66.0	1.20	28.02	9.9	0.000237
10.0	104.8	20.96	5.0	66.0	1.20	28.02	12.9	0.000216
7.0	84.0	16.80	5.0	66.0	1.20	28.02	9.9	0.000225
4.0	59.0	11.80	5.0	66.0	1.20	28.02	6.9	0.000227
2.0	43.5	8.70	5.0	66.0	1.20	28.02	4.9	0.000235

AVERAGE
k-VALUE: COEFFICIENT OF PERMEABILITY

17.9 0.000238

RECORD OF WATER PRESSURE TEST
DEPTH(m): 6-10

HOLE NO. JD-4

GAUGE PRESS.	INJECTION Q'ty	TEST LENGTH	HOLE DIA.	GAUGE HEIGHT	WATER LEVEL	TEST PRESS.	LUGEON VALUE	k-VALUE
kg/cm2	lit/min	lit/min/m	m	mm	m	kg/cm2		cm/sec
0.5	18.6	4.65	4.0	66.0	0.80	2.57	0.8	55.6
1.0	33.2	8.30	4.0	66.0	0.80	2.57	1.3	62.1
1.5	41.8	10.45	4.0	66.0	0.80	2.57	1.8	56.9
2.0	49.6	12.40	4.0	66.0	0.80	2.57	2.3	53.1
1.5	33.0	8.25	4.0	66.0	0.80	2.57	1.8	44.9
1.0	28.0	7.00	4.0	66.0	0.80	2.57	1.3	52.4
0.5	11.5	2.88	4.0	66.0	0.80	2.57	0.8	34.3

AVERAGE

51.3 0.000653

k-VALUE: COEFFICIENT OF PERMEABILITY

RECORD OF WATER PRESSURE TEST
DEPTH(m): 10-15

HOLE NO. JD-4

GAUGE PRESS.	INJECTION Q'ty	TEST LENGTH	HOLE DIA.	GAUGE HEIGHT	WATER LEVEL	TEST PRESS.	LUGEON VALUE	k-VALUE
kg/cm2	lit/min	lit/min/m	m	mm	m	kg/cm2		cm/sec
1.0	34.0	6.80	5.0	66.0	0.80	12.80	2.4	28.8
1.5	49.4	9.88	5.0	66.0	0.80	12.80	2.9	34.5
2.0	56.6	11.32	5.0	66.0	0.80	12.80	3.4	33.7
2.5	68.0	13.60	5.0	66.0	0.80	12.80	3.9	35.2
2.0	57.0	11.40	5.0	66.0	0.80	12.80	3.4	33.9
1.5	50.5	10.10	5.0	66.0	0.80	12.80	2.9	35.3
1.0	33.0	6.60	5.0	66.0	0.80	12.80	2.4	28.0

AVERAGE

32.8 0.000437

k-VALUE: COEFFICIENT OF PERMEABILITY

k-VALUE: COEFFICIENT OF PERMEABILITY

RECORD OF WATER PRESSURE TEST
DEPTH(m): 15-20

HOLE NO. JD-4

GAUGE PRESS.	INJECTION Q'ty	TEST LENGTH	HOLE DIA.	GAUGE HEIGHT	WATER LEVEL	TEST PRESS.	LUGEON VALUE	k-VALUE
kg/cm2	lit/min	lit/min/m	m	mm	m	kg/cm2		cm/sec
1.0	29.2	5.84	5.0	66.0	0.80	16.80	2.8	21.2
2.0	43.6	8.72	5.0	66.0	0.80	16.80	3.8	23.2
3.0	56.2	11.24	5.0	66.0	0.80	16.80	4.8	23.6
4.0	68.6	13.72	5.0	66.0	0.80	16.80	5.8	23.8
3.0	56.5	11.30	5.0	66.0	0.80	16.80	4.8	23.7
2.0	45.0	9.00	5.0	66.0	0.80	16.80	3.8	23.9
1.0	28.5	5.70	5.0	66.0	0.80	16.80	2.8	20.7

AVERAGE

22.9 0.000305

k-VALUE: COEFFICIENT OF PERMEABILITY

RECORD OF WATER PRESSURE TEST
DEPTH(m): 20-25

HOLE NO. JD-4

GAUGE PRESS.	INJECTION Q'ty	TEST LENGTH	HOLE DIA.	GAUGE HEIGHT	WATER LEVEL	TEST PRESS.	LUGEON VALUE	k-VALUE
kg/cm2	lit/min	lit/min/m	m	mm	m	kg/cm2		cm/sec
1.0	29.2	5.84	5.0	66.0	0.80	18.40	2.9	20.0
2.0	56.8	11.36	5.0	66.0	0.80	18.40	3.9	29.0
4.0	73.8	14.76	5.0	66.0	0.80	18.40	5.9	24.9
5.0	89.6	17.92	5.0	66.0	0.80	18.40	6.9	25.9
4.0	73.0	14.60	5.0	66.0	0.80	18.40	5.9	24.7
2.0	56.0	11.20	5.0	66.0	0.80	18.40	3.9	28.6
1.0	44.5	8.90	5.0	66.0	0.80	18.40	2.9	30.5

AVERAGE

26.2 0.000349

k-VALUE: COEFFICIENT OF PERMEABILITY

RECORD OF WATER PRESSURE TEST
DEPTH(m): 25-30

HOLE NO. JD-4

GAUGE PRESS.	INJECTION Q'ty	TEST LENGTH	HOLE DIA.	GAUGE HEIGHT	WATER LEVEL	TEST PRESS.	LUGEON VALUE	k-VALUE
kg/cm2	lit/min	lit/min/m	m	mm	m	kg/cm2		cm/sec
1.0	33.2	6.64	5.0	66.0	0.80	20.60	3.1	21.1
2.0	41.0	8.20	5.0	66.0	0.80	20.60	4.1	19.8
4.0	61.6	12.32	5.0	66.0	0.80	20.60	6.1	20.1
5.0	76.0	15.20	5.0	66.0	0.80	20.60	7.1	21.3
4.0	62.0	12.40	5.0	66.0	0.80	20.60	6.1	20.2
2.0	40.5	8.10	5.0	66.0	0.80	20.60	4.1	19.6
1.0	37.5	7.50	5.0	66.0	0.80	20.60	3.1	23.9

AVERAGE
k-VALUE: COEFFICIENT OF PERMEABILITY

20.9 0.000278

RECORD OF WATER PRESSURE TEST
DEPTH(m): 29-35

HOLE NO. JD-4

GAUGE PRESS.	INJECTION Q'ty	TEST LENGTH	HOLE DIA.	GAUGE HEIGHT	WATER LEVEL	TEST PRESS.	LUGEON VALUE	k-VALUE
kg/cm2	lit/min	lit/min/m	m	mm	m	kg/cm2		cm/sec
1.0	21.6	3.60	6.0	66.0	0.80	21.64	3.2	11.1
2.0	26.6	4.43	6.0	66.0	0.80	21.64	4.2	10.4
4.0	47.2	7.87	6.0	66.0	0.80	21.64	6.2	12.6
6.0	67.2	11.20	6.0	66.0	0.80	21.64	8.2	13.6
4.0	51.0	8.50	6.0	66.0	0.80	21.64	6.2	13.6
2.0	37.0	6.17	6.0	66.0	0.80	21.64	4.2	14.5
1.0	12.0	2.00	6.0	66.0	0.80	21.64	3.2	6.2

AVERAGE
k-VALUE: COEFFICIENT OF PERMEABILITY

11.7 0.000162

RECORD OF WATER PRESSURE TEST
DEPTH(m): 35-40

HOLE NO. JD-4

GAUGE PRESS.	INJECTION Q'ty	TEST LENGTH	HOLE DIA.	GAUGE HEIGHT	WATER LEVEL	TEST PRESS.	LUGEON VALUE	k-VALUE
kg/cm2	lit/min	lit/min/m	m	mm	m	kg/cm2		cm/sec
2.0	56.4	11.28	5.0	66.0	0.80	24.79	4.6	24.7
4.0	75.8	15.16	5.0	66.0	0.80	24.79	6.6	23.1
7.0	89.6	17.92	5.0	66.0	0.80	24.79	9.6	18.7
9.0	101.4	20.28	5.0	66.0	0.80	24.79	11.6	17.5
7.0	94.5	18.90	5.0	66.0	0.80	24.79	9.6	19.8
4.0	76.0	15.20	5.0	66.0	0.80	24.79	6.6	23.2
2.0	60.0	12.00	5.0	66.0	0.80	24.79	4.6	26.3

AVERAGE
k-VALUE: COEFFICIENT OF PERMEABILITY

21.9 0.000292

RECORD OF WATER PRESSURE TEST
DEPTH(m): 40-45

HOLE NO. JD-4

GAUGE PRESS.	INJECTION Q'ty	TEST LENGTH	HOLE DIA.	GAUGE HEIGHT	WATER LEVEL	TEST PRESS.	LUGEON VALUE	k-VALUE
kg/cm2	lit/min	lit/min/m	m	mm	m	kg/cm2		cm/sec
2.0	43.2	8.64	5.0	66.0	0.80	25.75	4.7	18.6
4.0	56.4	11.28	5.0	66.0	0.80	25.75	6.7	16.9
7.0	67.2	13.44	5.0	66.0	0.80	25.75	9.7	13.9
9.0	75.6	15.12	5.0	66.0	0.80	25.75	11.7	13.0
7.0	70.5	14.10	5.0	66.0	0.80	25.75	9.7	14.6
4.0	57.0	11.40	5.0	66.0	0.80	25.75	6.7	17.1
2.0	46.0	9.20	5.0	66.0	0.80	25.75	4.7	19.8

AVERAGE
k-VALUE: COEFFICIENT OF PERMEABILITY
k-VALUE: COEFFICIENT OF PERMEABILITY

16.3 0.000217

RECORD OF WATER PRESSURE TEST
DEPTH(m): 45-50

HOLE NO. JD-4

GAUGE PRESS.	INJECTION Q'ty	TEST LENGTH	HOLE DIA.	GAUGE HEIGHT	WATER LEVEL	TEST PRESS.	LUGEON VALUE	k-VALUE
kg/cm2	lit/min	lit/min/m	m	mm	m	kg/cm2		cm/sec
2.0	38.4	7.68	5.0	66.0	0.80	26.80	4.8	16.1
4.0	69.6	13.92	5.0	66.0	0.80	26.80	6.8	20.6
7.0	94.6	18.92	5.0	66.0	0.80	26.80	9.8	19.4
4.0	74.0	14.80	5.0	66.0	0.80	26.80	6.8	21.9
2.0	55.5	11.10	5.0	66.0	0.80	26.80	4.8	23.3

AVERAGE
k-VALUE: COEFFICIENT OF PERMEABILITY

20.3 0.000270

RECORD OF WATER PRESSURE TEST
DEPTH(m): 15-20

HOLE NO. JD-11

GAUGE PRESS.	INJECTION Q'ty	TEST LENGTH	HOLE DIA.	GAUGE HEIGHT	WATER LEVEL	TEST PRESS.	LUGEON VALUE	k-VALUE
kg/cm2	lit/min	lit/min/m	m	mm	m	kg/cm2		cm/sec
1.0	35.2	7.04	5.0	66.0	0.83	14.31	2.5	28.0
2.0	52.8	10.56	5.0	66.0	0.83	14.31	3.5	30.1
3.0	61.4	12.28	5.0	66.0	0.83	14.31	4.5	27.2
4.0	76.4	15.28	5.0	66.0	0.83	14.31	5.5	27.7
3.0	71.0	14.20	5.0	66.0	0.83	14.31	4.5	31.5
2.0	56.0	11.20	5.0	66.0	0.83	14.31	3.5	31.9
1.0	41.0	8.20	5.0	66.0	0.83	14.31	2.5	32.6

AVERAGE
k-VALUE: COEFFICIENT OF PERMEABILITY

29.8 0.000397

RECORD OF WATER PRESSURE TEST
DEPTH(m): 20-25

HOLE NO. JD-11

GAUGE PRESS.	INJECTION Q'ty	TEST LENGTH	HOLE DIA.	GAUGE HEIGHT	WATER LEVEL	TEST PRESS.	LUGEON VALUE	k-VALUE
kg/cm2	lit/min	lit/min/m	m	mm	m	kg/cm2		cm/sec
2.0	27.8	5.56	5.0	66.0	1.83	17.27	3.9	14.2
4.0	54.4	10.88	5.0	66.0	1.83	17.27	5.9	18.4
7.0	68.6	13.72	5.0	66.0	1.83	17.27	8.9	15.4
10.0	85.6	17.12	5.0	66.0	1.83	17.27	11.9	14.4
7.0	69.0	13.80	5.0	66.0	1.83	17.27	8.9	15.5
4.0	51.5	10.30	5.0	66.0	1.83	17.27	5.9	17.4
2.0	38.5	7.70	5.0	66.0	1.83	17.27	3.9	19.7

AVERAGE
k-VALUE: COEFFICIENT OF PERMEABILITY

16.4 0.000219

RECORD OF WATER PRESSURE TEST
DEPTH(m): 25-30

HOLE NO. JD-11

GAUGE PRESS.	INJECTION Q'ty	TEST LENGTH	HOLE DIA.	GAUGE HEIGHT	WATER LEVEL	TEST PRESS.	LUGEON VALUE	k-VALUE
kg/cm2	lit/min	lit/min/m	m	mm	m	kg/cm2		cm/sec
2.0	34.4	6.88	5.0	66.0	1.33	21.82	4.3	15.9
4.0	43.4	8.68	5.0	66.0	1.33	21.82	6.3	13.7
7.0	63.8	12.76	5.0	66.0	1.33	21.82	9.3	13.7
10.0	78.8	15.76	5.0	66.0	1.33	21.82	12.3	12.8
7.0	65.5	13.10	5.0	66.0	1.33	21.82	9.3	14.1
4.0	46.5	9.30	5.0	66.0	1.33	21.82	6.3	14.7
2.0	35.0	7.00	5.0	66.0	1.33	21.82	4.3	16.2

AVERAGE
k-VALUE: COEFFICIENT OF PERMEABILITY

14.5 0.000193

RECORD OF WATER PRESSURE TEST
DEPTH(m): 30-35

HOLE NO. JD-11

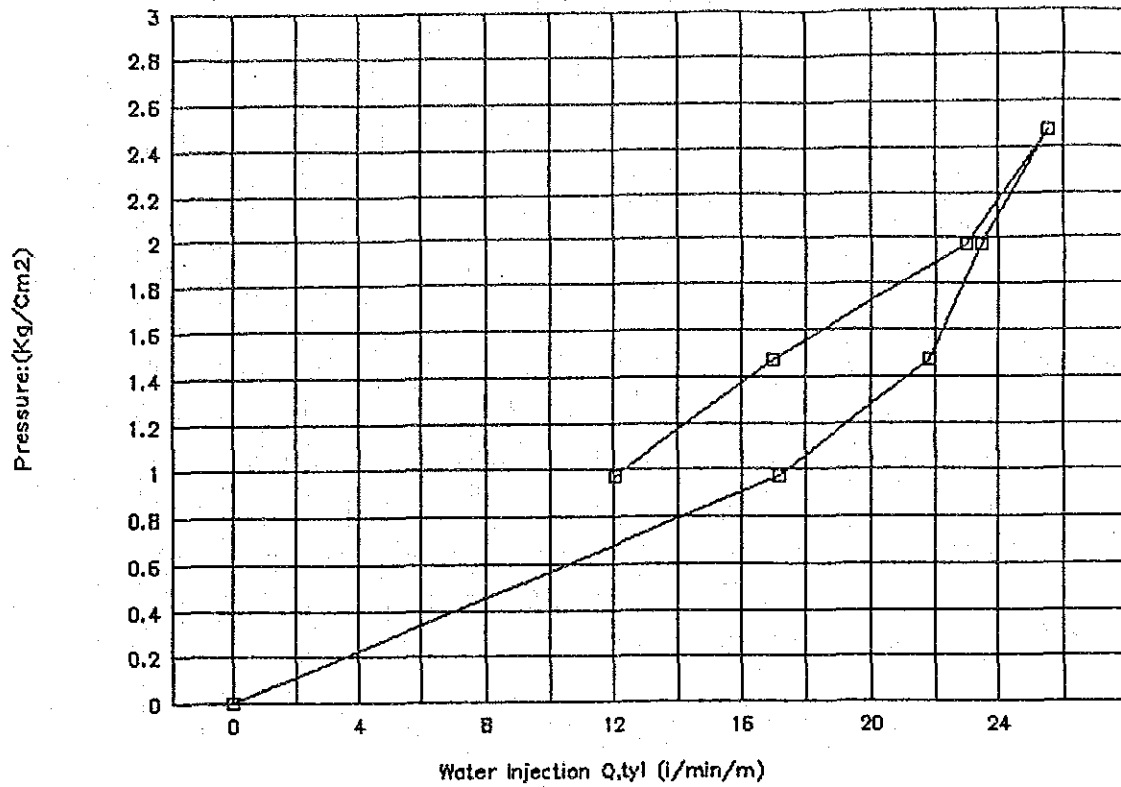
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kg/cm2	lit/min	lit/min/m	m	mm	m	kg/cm2		cm/sec
2.0	15.2	3.04	5.0	66.0	0.83	26.59	4.7	6.4
4.0	22.2	4.44	5.0	66.0	0.83	26.59	6.7	6.6
7.0	43.9	8.78	5.0	66.0	0.83	26.59	9.7	9.0
10.0	59.4	11.88	5.0	66.0	0.83	26.59	12.7	9.3
7.0	34.5	6.90	5.0	66.0	0.83	26.59	9.7	7.1
4.0	27.0	5.40	5.0	66.0	0.83	26.59	6.7	8.0
2.0	12.0	2.40	5.0	66.0	0.83	26.59	4.7	5.1

AVERAGE
k-VALUE: COEFFICIENT OF PERMEABILITY

7.4 0.000098

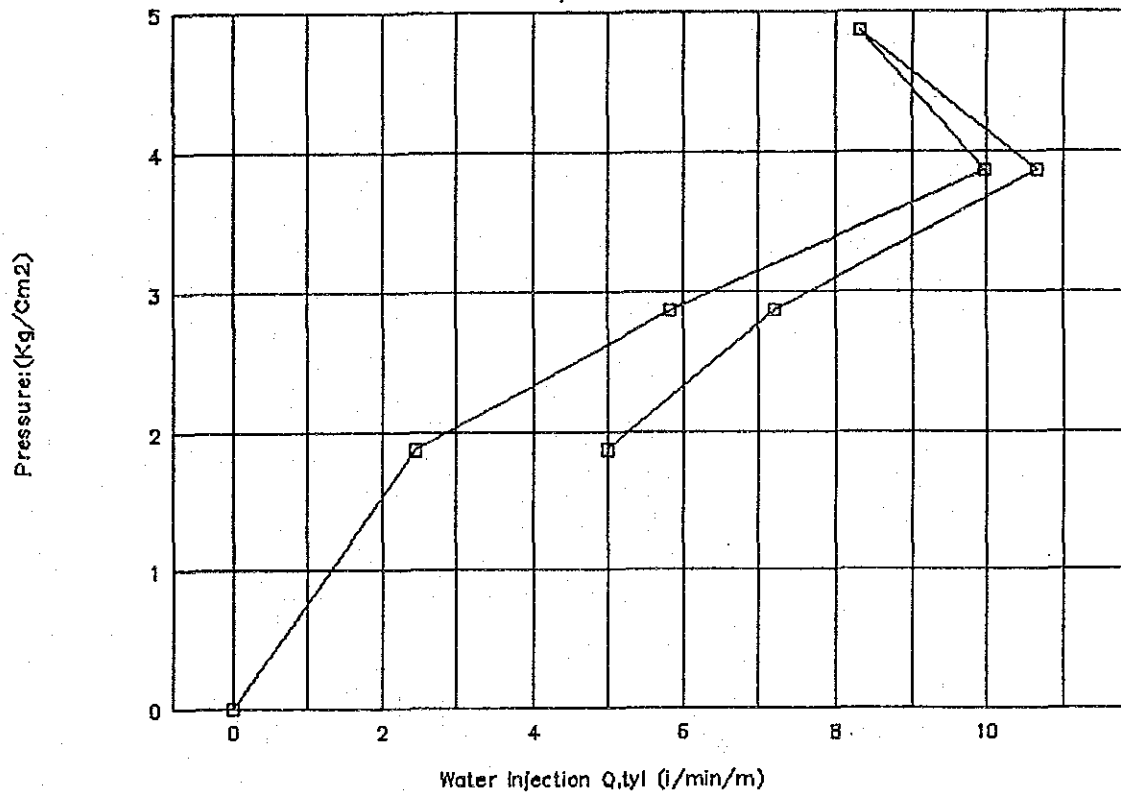
P/Q.Curve: Hole No.JD-3

Depth:2-5m



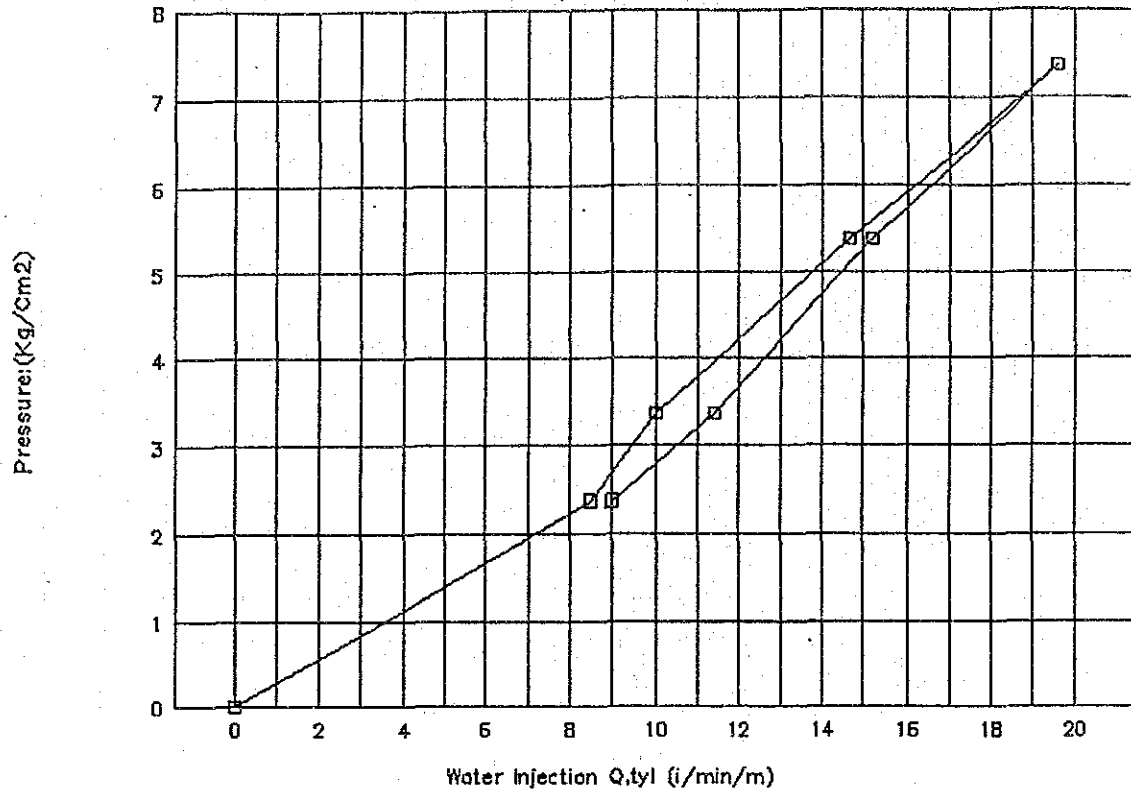
P/Q.Curve: Hole No.JD-3

Depth:5-10m



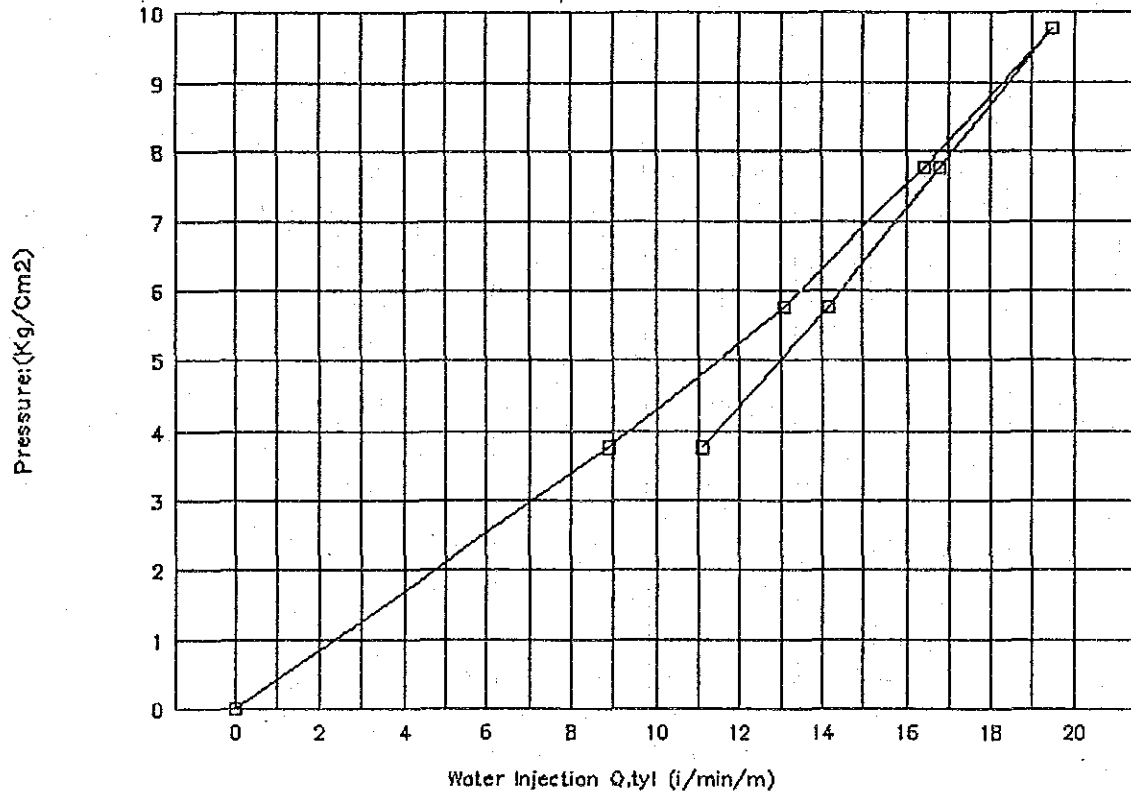
P/Q.Curve: Hole No.JD-3

Depth:10-15m



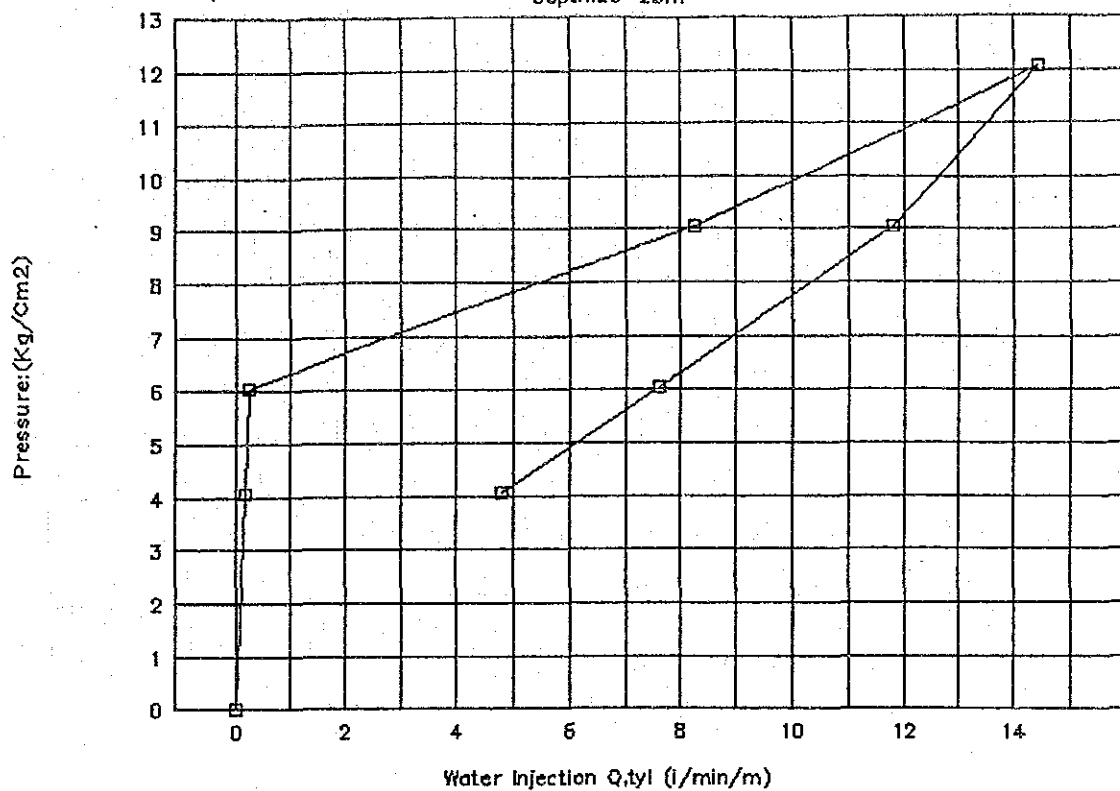
P/Q.Curve: Hole No.JD-3

Depth:15-20m



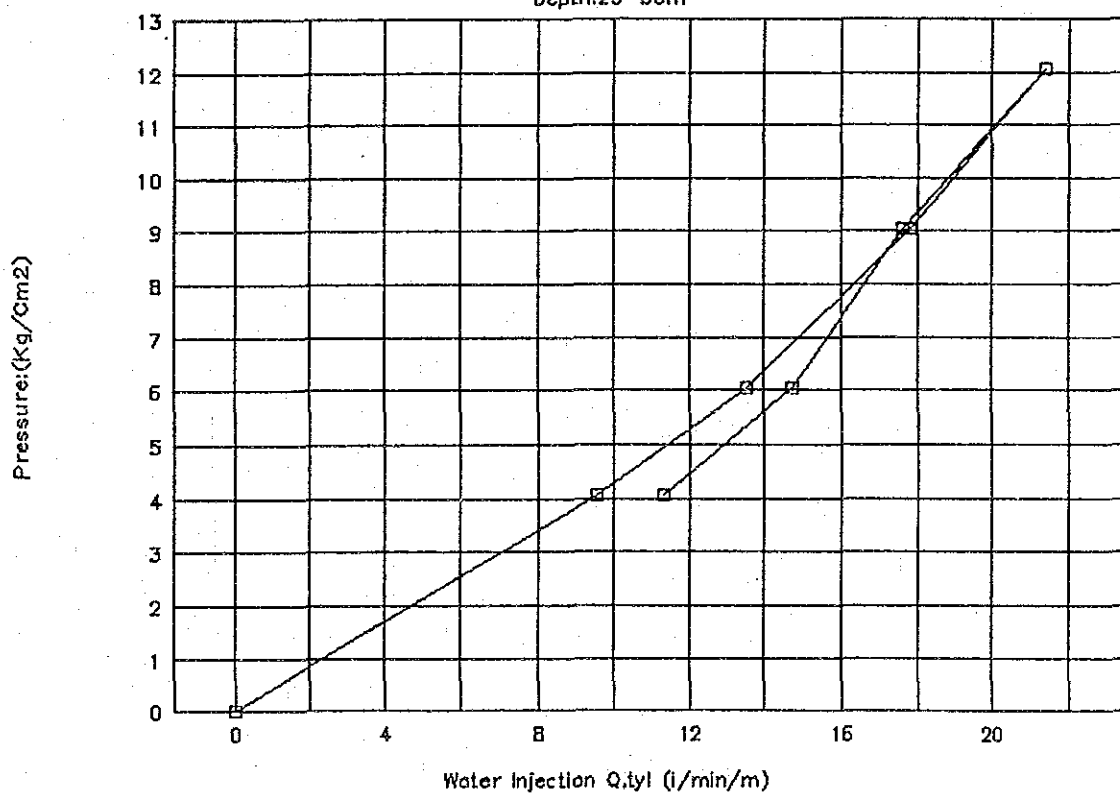
P/Q.Curve: Hole No.JD-3

Depth:20-25m



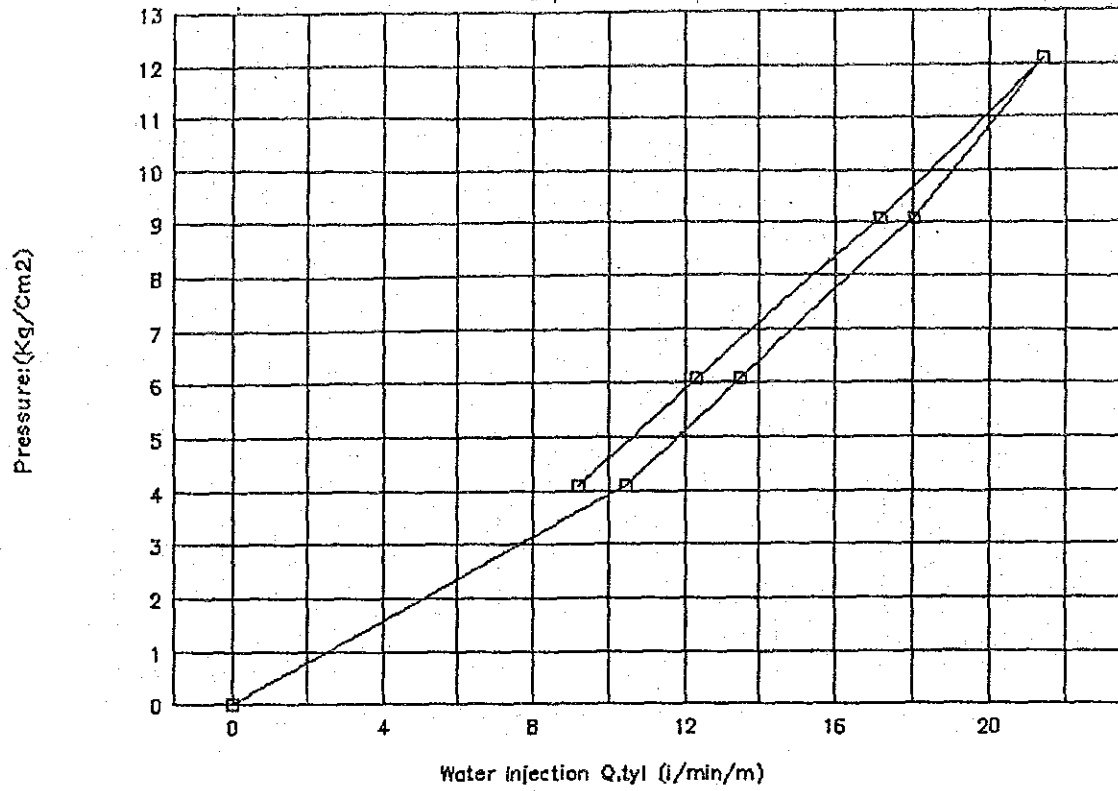
P/Q.Curve: Hole No.JD-3

Depth:25-30m



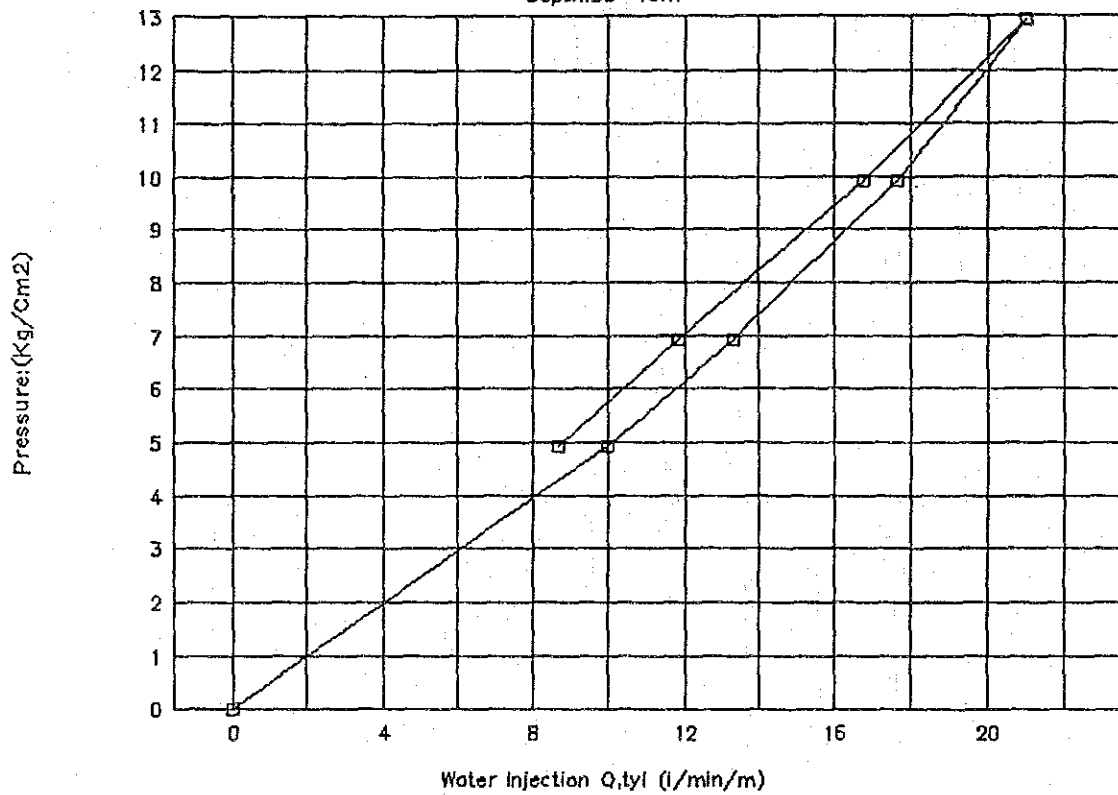
P/Q.Curve: Hole No.JD-3

Depth:30-35m



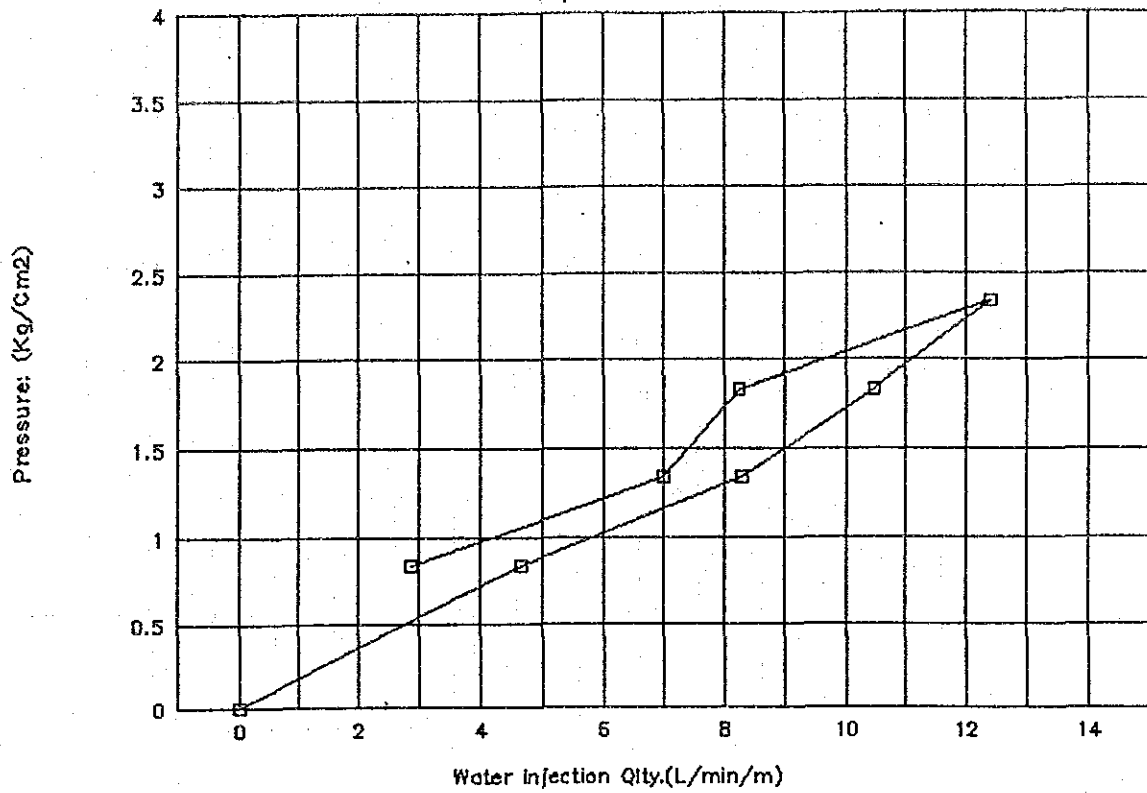
P/Q.Curve: Hole No.JD-3

Depth:35-40m



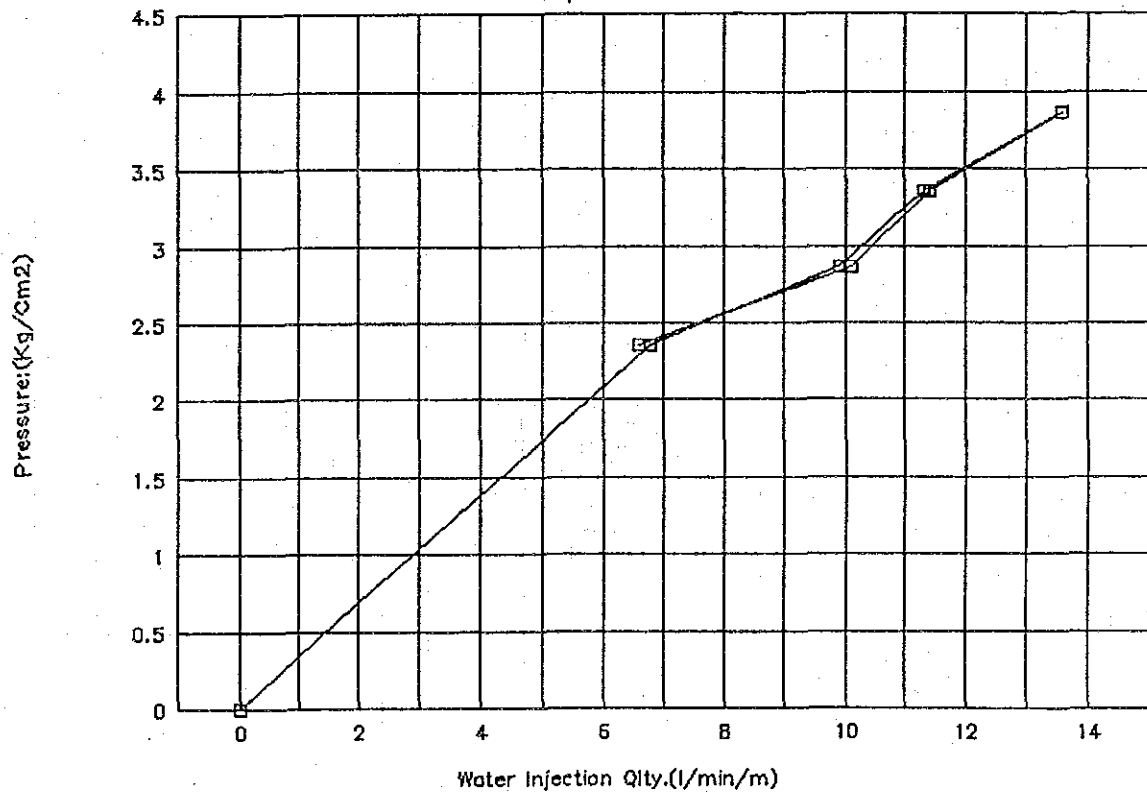
P/Q.Curve: Hole No.JD-4

Depth : 6-10m



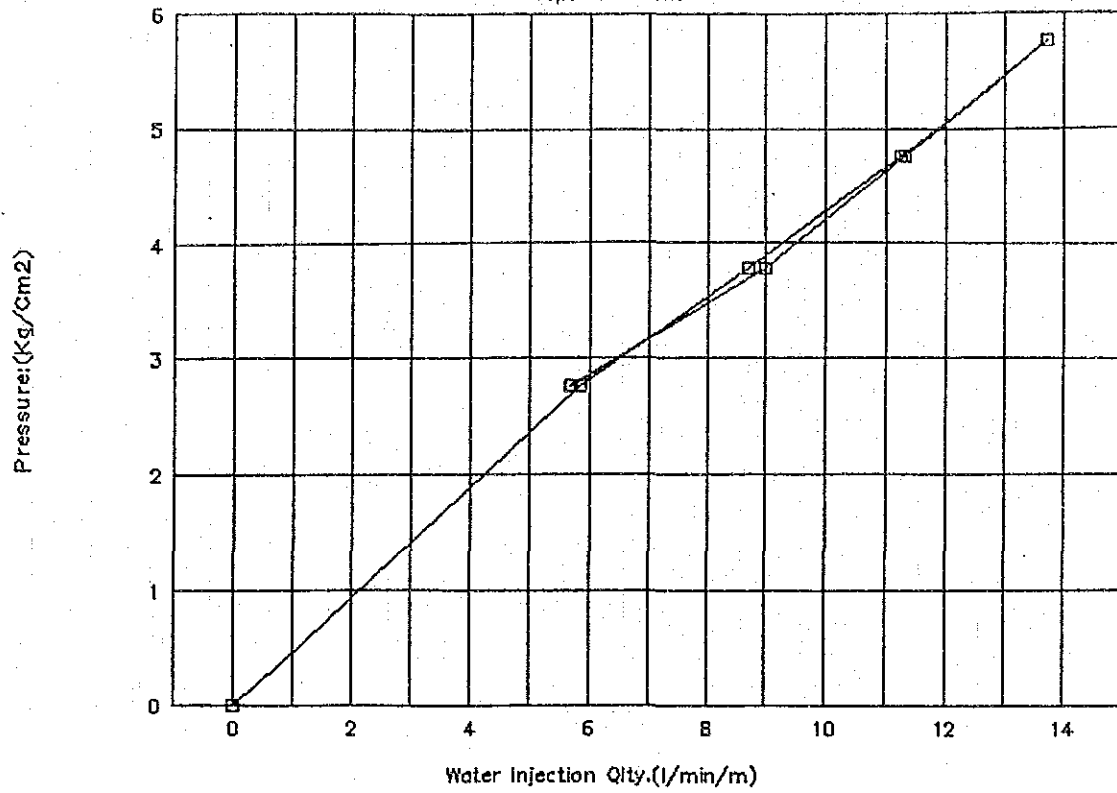
P/Q.Curve: Hole No.JD-4

Depth:10-15m



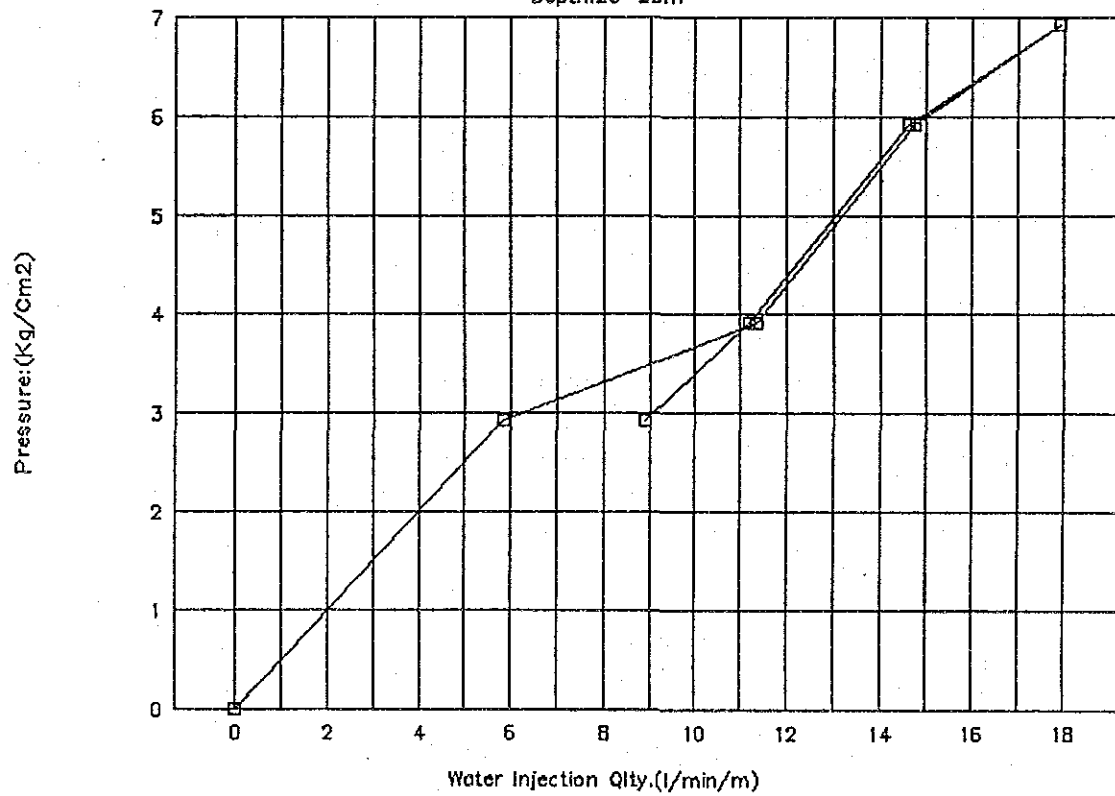
P/Q.Curve: Hole No.JD-4

Depth:15-20m



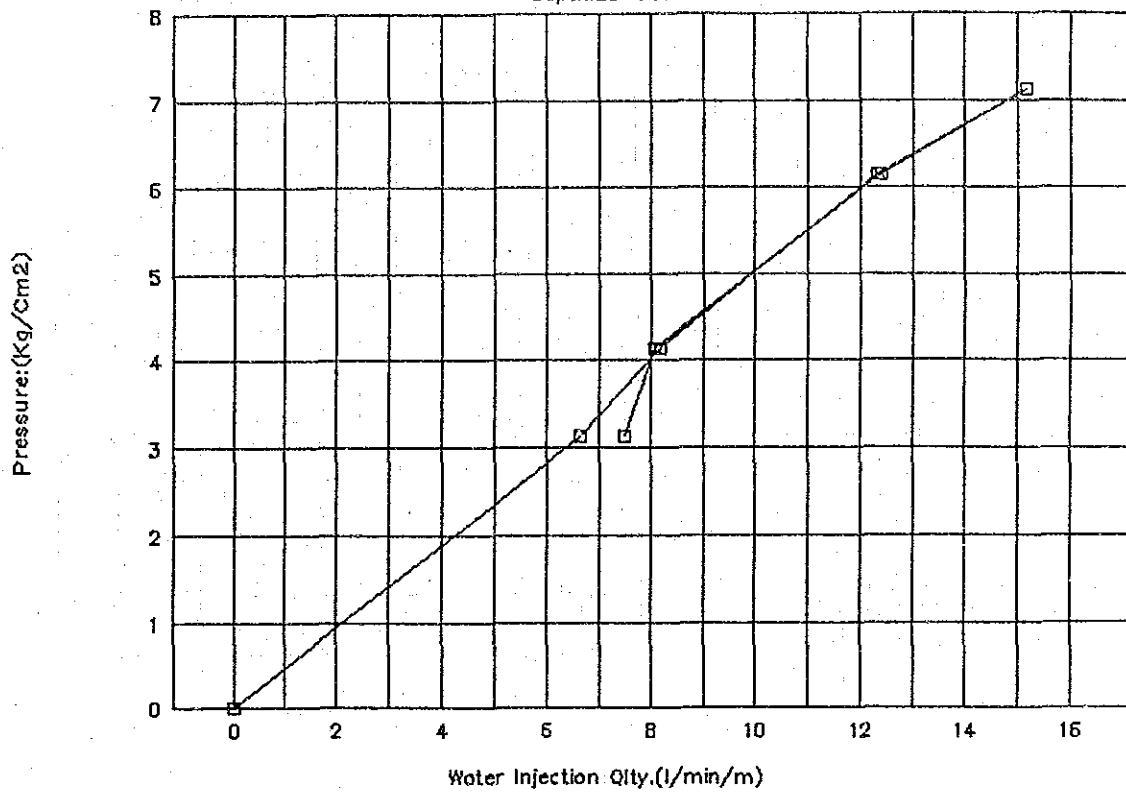
P/Q.Curve: Hole No.JD-4

Depth:20-25m



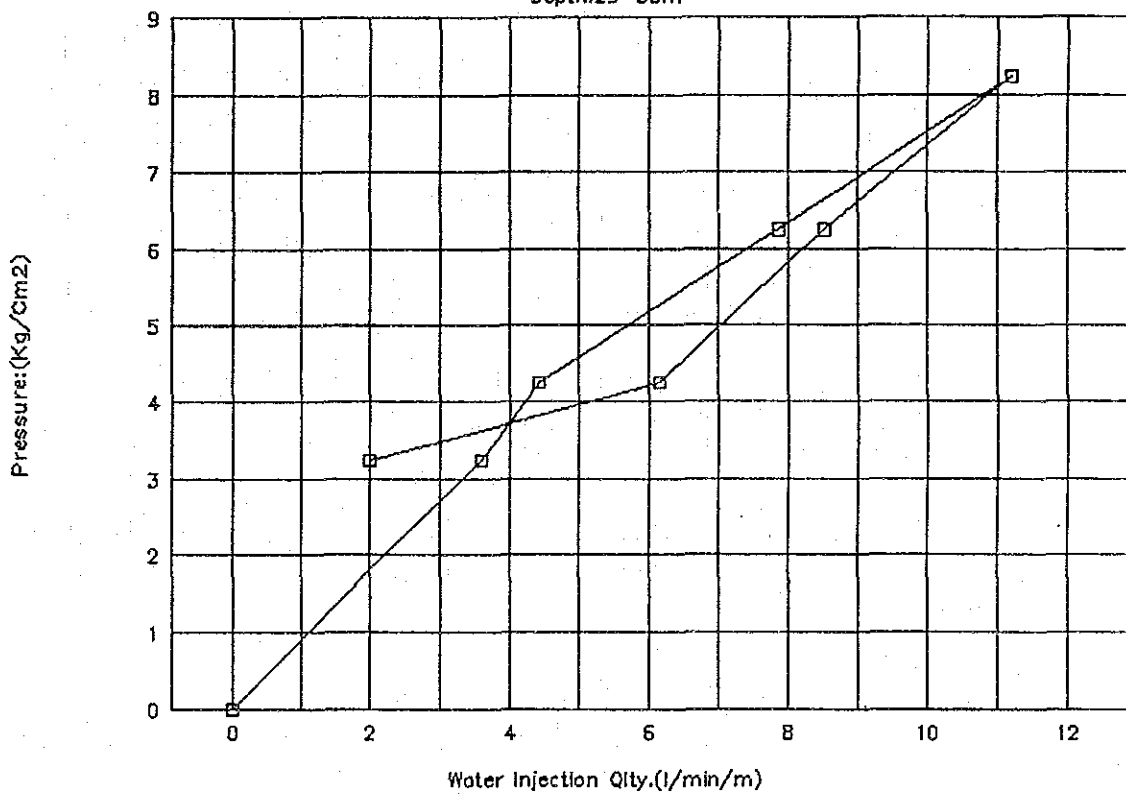
P/Q.Curve: Hole No.JD-4

Depth:25-30m



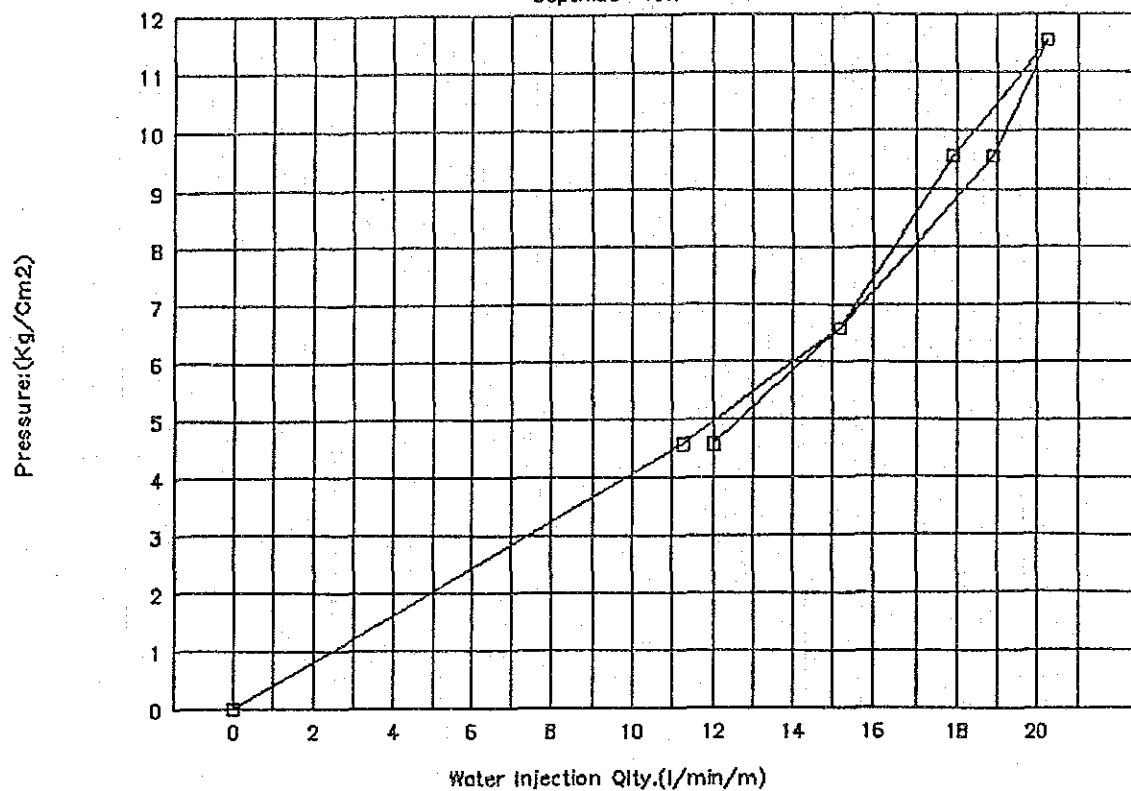
P/Q.Curve: Hole No.JD-4

Depth:29-35m



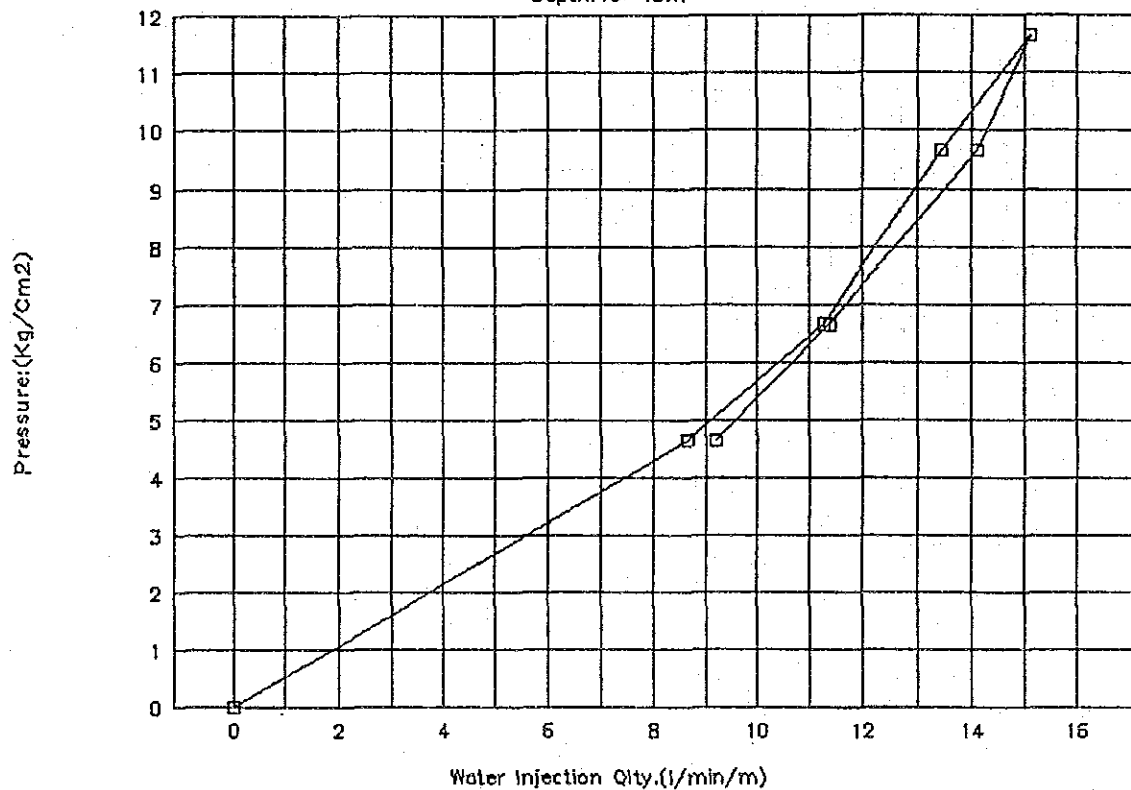
P/Q.Curve: Hole No.JD-4

Depth:35-40m



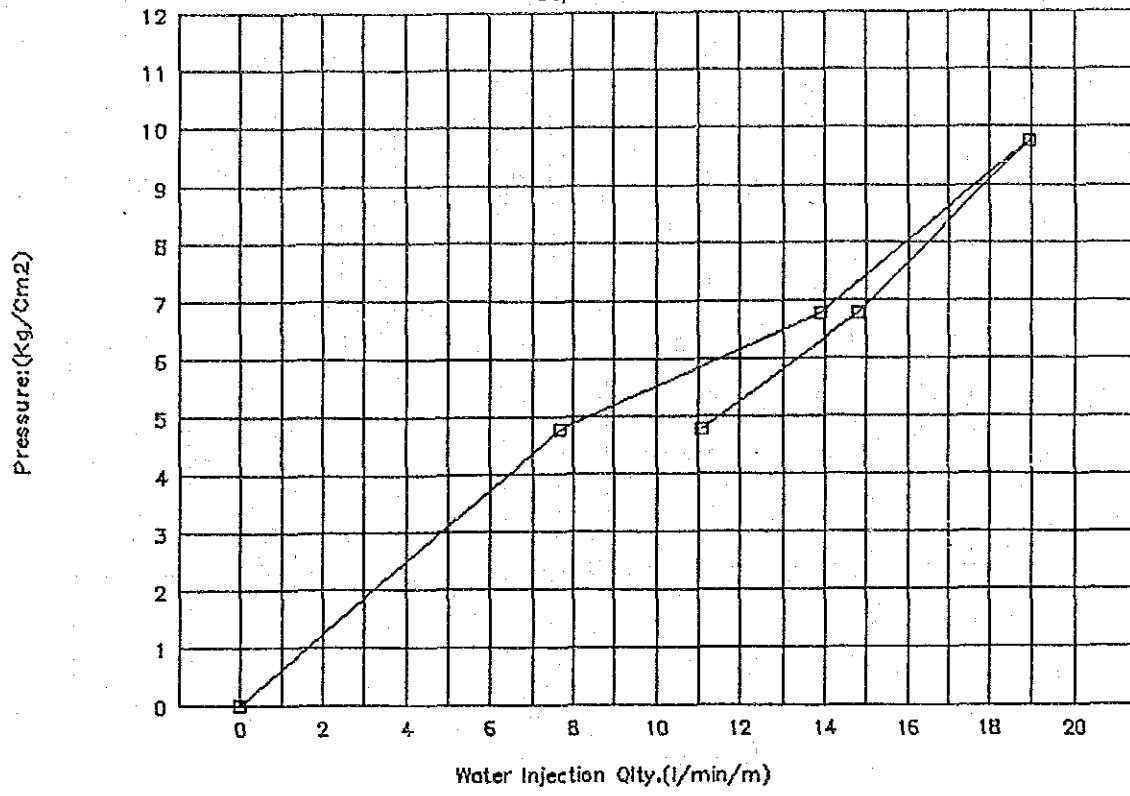
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Depth:40-45m



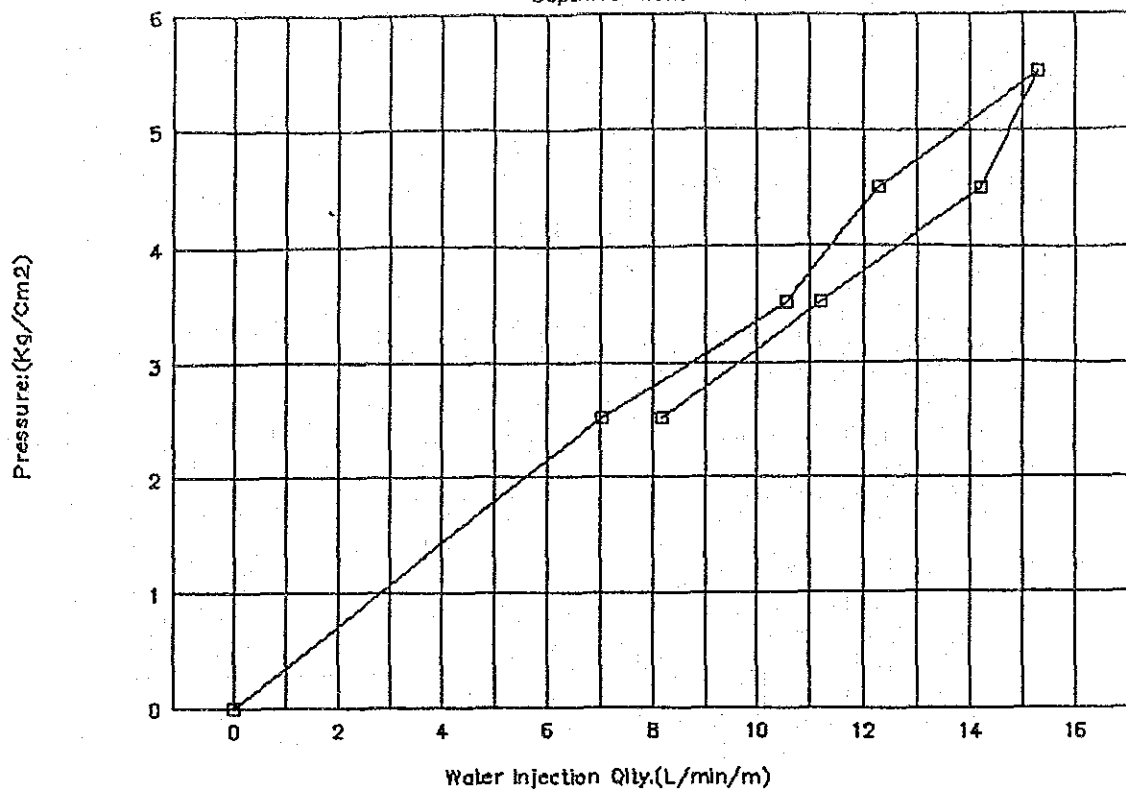
P/Q.Curve: Hole No.JD-4

Depth:45-50m



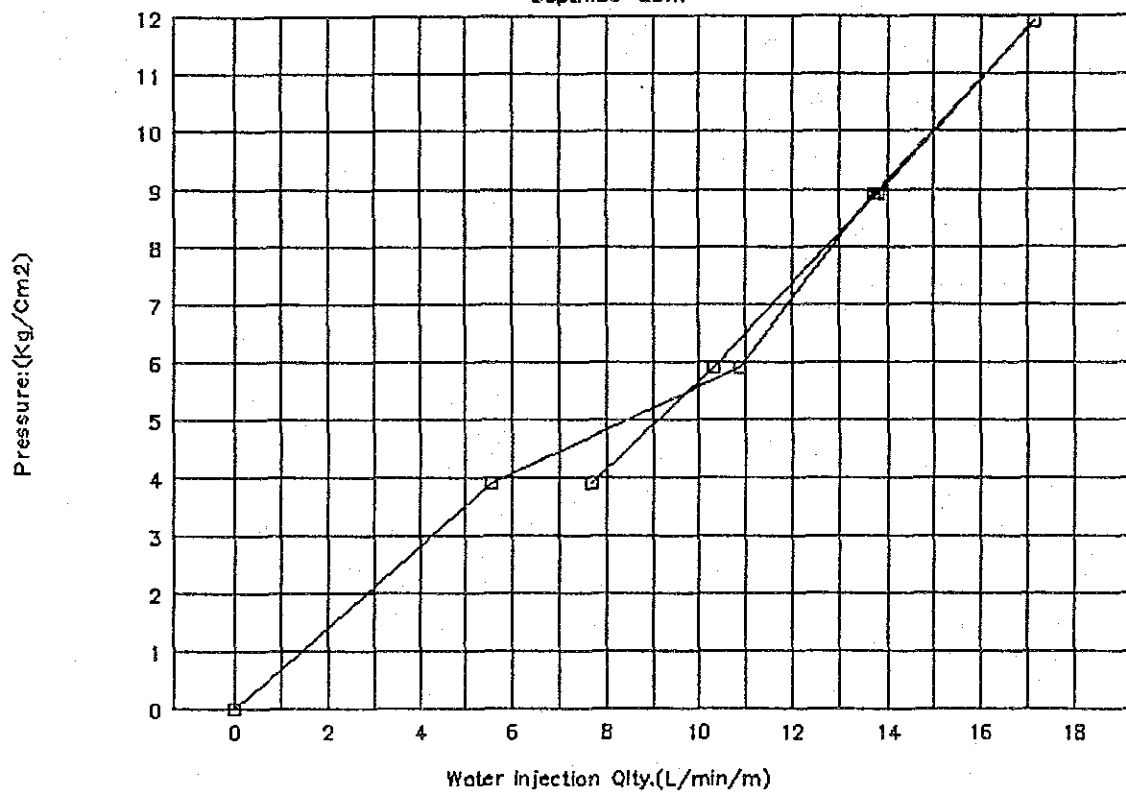
P/Q.Curve: Hole No.JD-11

Depth:15-20m



P/Q.Curve: Hole No.JD-11

Depth:20-25m



P/Q.Curve: Hole No.JD-11

Depth:25-30m

