

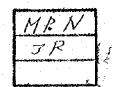
THE SAN KAMPAENG GEOTHERMAL DEVELOPMENT PROJECT IN THE KINGDOM OF THAILAND

DEEP ELECTRIC SURVEY REPORT (SUPPLEMENTARY)



MACH, 1985

JAPAN INTERNATIONAL COOPERATION AGENCY



> > 国際協力事業団 26158

	CONTENTS	
		(Page)
ī.	General Description	
	1.1 Investigation Subject Name	
	1.2 Object of Investigation	1
	1.3 Survey Area	1
	1.4 Particulars of Investigation	1
	1.5 Survey Period	2
	I.6 Surveyors	2
IJ.	Method for Flectromagnetic Sounding	3
	II.1 Method for Measurement by MT Method	3
	11.2 Method for Measurement by CSATM Method	7
111.	Analysis and Results	9
	III.1 Method for Analysis	9
	III.2 Results of Geophysical Analysis	15
1.	III.3 Result of One-Dimensional Analysis	27
	III.4 Result of Two-Dimensional Model Analysis	34
JV,	Summary	37
v.	References	39

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LIST OF APPENDED DRAWINGS

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- Fig. 1 Apparent resistivity isocontour (frequency: 8.75 Hz)
- Fig. 2 Apparent resistivity isocontour period: (11.1304 sec)
- Fig. 3 Apparent resistivity isocontour (period: 39,384 sec)
- Fig. 4 Total conductance isocontour
- Fig. 5 Structure iso-contours for the top of conductive formation (shallow part)
- Pig. 6 Structure iso-contours for the top of conductive formation (deep part)
- Fig. 7 Isopachs of the overburden of high resistivity
- Fig. 8 Electrical foundation
- Fig. 9 Section 1-84
- Fig. 10 Section 2-84

I. General Pescription

I. GENERAL DESCRIPTION

1.1 Investigation Item Name

Kingdom of Thailand San Kampaeng area deep electric survey (MT method)
[Supplementary investigation]

1.2 Object of Investigation

The object of this investigation is to obtain data on the geothermal reservoirs by checking the distribution of resistivity (or conductance) in the survey area by measuring ratios of electric field to magnetic field through execution of magnetotelluric method (MT method) and vertical electromagnetic sounding method (CSAMT method: Controlled Source Audiofrequency Magnetotelluric method). The particular objects of supplementary survey conducted this time are selection of survey well excavating positions for the thirdary investigation as well as investigation of expansion and form of the low resistivity zone in the Ban Mae area located in the Southeastern part of the survey area.

1.3 Survey Area

This survey was conducted in an area of about 50 km² in the San Kampaeng area, located in the Northern part of the Kingdom of Thailand as shown in Fig. 1, and measurements by MT method and CSAMT method were conducted at the counding points indicated in this figure.

The survey area is located at a point of about 30 km to the East from The place where a sign of presence of geothermal energy is located at an intermediate point between Wat Pong Hom and Ban Pong Nok in the Northwestern part of the survey area. It is characterized by springing of high temperature hot springs.

1.4 Particulars of Investigation

The components of measurement by MT method are two components of underground natural electric field (Fx, Fy) and three components of natural magnetic field (Hx, Hy, Hz). The total number of sounding points in this survey by MT method was 20, and sounding points were selected in about 1 km mesh as a rule. In the Ban Pong Nok area, however, the spacing between sounding points was determined as 500 to 600 meters. The components of measurement by CSAMT method are two components of magnetic field (Hx, Hz) and a component of electric field (Fy), which are induced by loop. Four loops, i.e., loops D, F, G and H, were prepared. The same points as used for the survey by MT method were employed for the sounding points of the deep electric survey. The total number of sounding points was 20, which is same as that of the MT method.

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1.5 Survey Period

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1.6 Investigators

Field and analysis engineer

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II. Method for Electromagnetic Sounding

II. METHOD FOR ELECTROMAGNETIC SOUNDING

11.1 Method of measurement of MT survey

11.3.1 Apparatus for measurement

The specification of the apparatus employed in the present MT survey is as follows.

Apparatus	Amount	Specification
Amplifier unit for electric field	2	(1st Stage) Input Level 1 micro V Max. Gain 2 x 10 ² 1.00 Hz High Cut Filter (2nd Stage) Max. Gain 5 x 10 ⁴ 0.33 Hz High Cut Filter
Amplifier unit : for magnetic field	3	Max. Gain 8 x 10 ⁴ 0.33 Hz High Cut Filter
Wave form Recorder	1	Full Scale ± 5V or 10V Chart Speed Slow 1200mm/hour Fast 120mm/min
Data Logger (Double cassette)	1	Full Scale ± 5V Sampling Rate 100ms/1 DATA '5 Sample Multiplexer
Battery	2	12V, 100A
Magnetic sensor (Induction type coil)	3	115mmø x 1050mmL ab. 10 kg Insert

(Accessory) M.T. cable a suit. Electrode a suit

Tools a suit. Others a set

11,1.2 Method of measurement

11.1

The method of measurement in this MT survey is as shown in the following Fig.

Descriptor de la lación de lación de la lación de lación de

a reacht. I d'higher, and ar throthair mheilig Selection of sounding point **Point** Determination of the location of the base selection Determination of the Ex. Ey direction Electrodes laying Prepa-Setting of magnetic sensor ration Connection of cable to electrode Measure-Arrangement of measuring apparatus ment Measurement Remov-Removing ing

Fig. II.1 Measurement of MT survey

Fig. II.2

1) Selection of sounding points

Places which permit measurement were selected in the vicinity of the programmed points, avoiding steep slopes and assuring that noise sources are not located in the neighborhood. Furthermore, the base points were selected in the most appropriate sites in the actual field condition, where it is possible to establish survey lines. Two survey lines of the length of 100 meters were laid out in an L-shape array. Directions, topographical undulation and conditions of surrounding area were recorded on the field note at each point.

The relation of the locations of Ex base and Ey base is as shown. The survey line on the left-hand side as viewed from the vase is Ex and the survey line on the right-hand side is Ey.

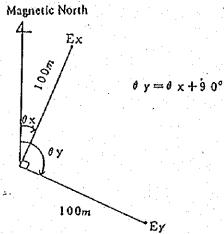


Fig. II Provision of survey lines

2) Preparation

Sensor was placed in a way as shown in Fig. II.2. The electrodes were placed at 5 sites; 3 at the base and one each at the sites of Ex and Ey. The way of laying these electrodes is shown in Fig. II.4. A hole 30 cm deep with diameter of 20 cm was sunk, in which water and soil were thrown in to make mud. After laying non-polarized electrode of CuSO₄ — Cu system, soil was piled as high as 20 cm.

Hx and Hy coils were placed on the wooden stand with the coil axes, Also coil for Hz was buried as deep as about 60 cm with its head upward. To stand it vertically, level was used. After confirming the directions of colls, levelling and perpendicularity, wooden box or polyethylene bucket was put on them and fixed with soil cover to avoid direct sunbeam and wind. (Fig. II.5, 6).

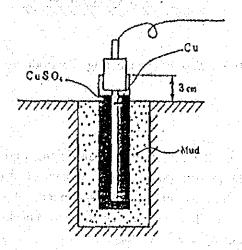


Fig. II.4 Way of laying electrode

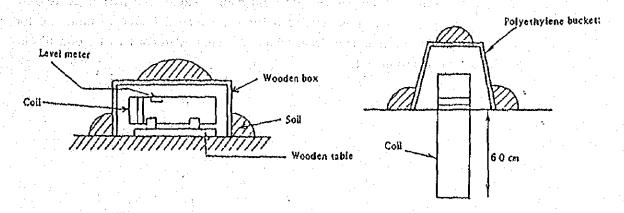


Fig. II.5 Way of setting Hx, Hy coils Fig. II.6 Way of setting Hz coil

The connection of cables to the electrode was by wire-cuts. To avoid direct sun beam, bucket was put on connection box as a covering and weight like soil or stone was placed on it (Fig. II.7).

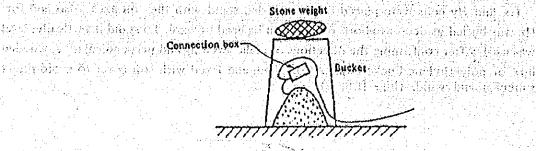


Fig. 11.7 Way of connecting electrode to cable

3) Measurement

As the process of the measurement, apparatus were connected in the first place, followed by the measurement of coil resistance and earthing resistance. After connection of the cables to the pannel, adjustment of the amplifier and setting the cassette tape to the data logger, signals were checked for a while. Then recording began by starting the data logger.

In the course of the measurement, the graphic paper was being watched to check noises. For the analysis of electromagnetic field of the period up to 200 second, recording of data was continued for more than 2 hours 30 min. and for more than 4 files of noiseless data, taking 25 minutes' record to be one file in case of single measurement.

11.2 Measurement of CSAMT method

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II.2.1 Apparatus for measurement

For the measurement of CSAMT method, the following apparatus were employed.

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		Amount	Specification
	Transmitter	model to produce	Frequency 2240, 1120, 560, 280, 140, 70, 35, 17.5, 8.75, 4.38, 2.19, 1.09 Hz Power 1 kW
	Receiver	2	Input level 10 micro V Output Display Digital 4 figures Band Pass Filter, Notch Filter 50 Hz/60 Hz
	Sensor	l set	Telluric Current Sensor x 1 Magnetic Field Sensor x 2

(Accessory)

Handheld Computer a set
Tools a set
Others a set

11.2.2 Method of measurement

Method of measurement by CSAMT survey is shown in Fig. 11.8, roughly.

After generating power by 1 kw generator, electric current of 12 steps of 2240, 1120, 560, 280, 140, 70, 35, 17.5, 8,75, 4.38, 2.19 and 1.09 Hz were input into a square loop of a side of the approximate length of 300 meters to generate artificial magnetic field.

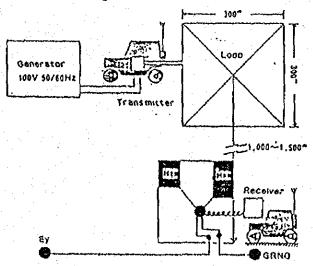


Fig. 11.8 Method of measurement of CSANT survey

A receiver was located at a point that is spaced apart by about 700 to 1,500 meters from those loop, and signals were reveived with sensors of Hx, Hz and Ky. As the reveived signals were as low as 10 to 20 microvolts, they were at first amplified with an amplifier and were then fed through a band-pass filter matched with the frequency of the current flowing through the loop and a 50 Hz notch filter. Finally, an averaged value was digitalized and was directly read out of the display panel. This value was input to a hand-held computer for data processing and simple data processing was executed on the field. Computation of apparent resistivity curve, penetration depth curve and of bostic inversion was made as this data processing. Measurement was taken once again in the case where the result of this computation was judged unsatisfactory.

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III. Analysis and Results

III. ANALYSIS AND RESULTS

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111.1 Method for Analysis and an arrange of the process of the contract of the

The analyzing procedure is indicated below.

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- 1. CSAMT method
 - 2. MT method
- new year 3. w. Figure/table
- Programa 4. De Data had salah sa
- zanto in S. Spectrum analysis para a para a manal take the land and a same
- 6. Tipper, impedance tensor analyses
- 7. Geophysical parameters
- in the Sounding curve
 - 9. Apparent resistivity isocontours
 - 10. One-dimensional analysis
 - 11. Total conductance isocontour
- 12. Division of layers
 - 13. Structure isocontours for the top of conductive formation
 - 14. Electrical foundation
 - 15. Two-dimensional model analysis
- 16. Two-dimensional sectional view

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III.1.1 Results of the CSAMT method

The apparent resistivity was calculated from the field records of the measured values, according to the following formula.

 $\rho a = (K/\mu_0 f) [Ey/Hx]^2$

Here pa: apparent resistivity (ohm-m)

no: magnetic permeability

f: frequency (Hz)

K: correction coefficient

This formula is similar to that used as the base for the MT method. However, in this case of the formula for CSAMT method, correction coefficient K which is a function of (Hx/Hz) is included. The apparent resistivity is obtained according to the following formula, too.

 $\rho a = K' \mu o r^2 2\pi f/(9Hx/Hz)$

Here pa: apparent resistivity (ohm-m)

μο: magnetic permeability

f : frequency (Hz)

K': correction coefficient

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In this formula, K' is also a function of Hx/Hz.

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III.1.2 Method for Analysis of MT Method

The data of five components of electric field and magnetic field obtained through measurement by MT method are at first converted by spectrum analysis into frequency region from time region. In the frequency region, the magnitude and phase of amplitude of each component are expressed as complex numbers.

The following discussions are made in the frequency region?

After the spectrum analysis, the data of these five components are analyzed in accordance with two analysis techniques, that is, impedance tensor analysis and tipper analysis, and geophysical parameters are obtained as a result. Impedance tensor analysis is to obtain various parameters by analyzing the relation of four components of horizontal components of electric field and magnetic field; and tipper analysis is to obtain various parameters through analysis of the relation among three components of magnetic field.

(1) Tipper analysis

The relation between the horizontal components and vertical components of magnetic field is expressed by such a linear coupling that is shown below.

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This is the expression that regulates the action from a horizontal magnetic field to a vertical magnetic field. Txty is the contant that determines the inclination (tip) of pole division of the magnetic field/and is called a tipper. It can be obtained when the following formulas are solved.

$$<$$
Hz Hy*> = TX $<$ Hx Hy*> + Ty $<$ Hy Hy*>

* means a conjugate complex number, and < > means a power spectrum.

The parameters obtained from this topper are explained below.

a) Tipper magnitude

Tipper magnitude = Tx² + Ty²

This magnitude is an index that indicates the structure. One-dimensional character is strong when this value is close to zero and two-dimensional character is strong when this value is larger. Furthermore, this index remains unchanged despite rotation of the coordinates with Z-axis as the center.

b) Minimum value of Tx (MIN Tx)

The value of Tx changes when the orthogonal coordinates system is rotated with Z-axis as the center. When the angle at which the value of Tx is the minimum is selected, this value becomes zero if the earth is of two-dimensional structure. It is possible to learn the

structure of the earth when this value and the tipper magnitude mentioned earlier are considered together.

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c) Tipper strike

Tipper strike indicates the rotating angle of the coordinates that gives the minimum value of Tx mentioned in paragraph b) above, and it is obtained by the following expression.

$$\theta t = 1/2 \tan^{-1} \frac{2\text{Re } (Tx Ty^*)}{|Tx|^2 - |Ty|^2}$$

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When the angle at which the value of Tx is the minimum is selected, it is parallel with the direction of the structure.

d) Tipper's phase

This is the phase of Tx after rotation of coordinates. It indicates the action from a horizontal magnetic field in the direction that is normal to the travelling direction to a vertical magnetic field.

(2) Impedance tensor analysis

The relation among four horizontal components of the electric field and magnetic field is expressed by such a linear coupling that is indicated below.

$$Ex = ZxxHx + ZyyHy$$

 $Ey = ZyxHx + ZyyHy$

The matrix of coefficients is expressed by tensor with the electric field and magnetic field as vectors, and it is called impedance vector.

It can be obtained when the following formulas are solved like the case of tipper.

Either electric field ExEy or magnetic field HxHy may be selected here as AxAy.

Various parameters obtained through this impedance tensor analysis are explained below.

a) Skew

Skew is defined by the following expression.

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$$\frac{|Zxx + Zyy|}{|Zxy - Zyx|}$$

If the earth is of one-dimensional or two-dimensional structure, this value is zero. The magnitude of this value is an index that indicates the three-dimensional property. Further, this value remains unchanged despite rotation of the coordinates.

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b) Rotating angle

$$\Theta z = \frac{1}{4} \arctan \frac{2 \text{ Re } [(Zyy-Zxx)(\hat{Z}xy*+Zyx*)]}{||Zxy+Ayx||^2 - |Zyy-Zxx|^2}$$

This angle means rotating angle Θz at which components Zxy Zyx of impedance stensor become the maximum when the coordinates are rotated with Z-axis as the center, and it is indicated by the angle formed between the measured X direction and the travelling direction.

c) Apparent resistivity and phase

The apparent resistivity and phase are obtained by the following expression by making use of impedance tensor after rotation of the coordinates mentioned above.

- 1. Axial apparent resistivity [(Rhox) = 0.2 | Zxy |²
 - 2. Axial phase (Phasex) = $tan^{-1}[(IMAG(Zxy)/REAL(Zxy))]$
 - 3. Radial apparent resistivityy (Rhoy) = 0.2 + Zyx |²
 - 4. Radial phase $\{(Phasey) = tan^{-1} (IMAG (Zyx)/(REAL (Zyx))\}$

d) Simple coherency (Coh ())

The simple coherency can be obtained by the following expression.

COH (AB) =
$$\frac{\langle AB^* \rangle}{[\langle AA^* \rangle \langle BB^* \rangle]^{1/2}}$$

A and B are components of electric field and magnetic field. Values after rotation of the coordinates were also used here.

e) Multiple coherency (ExPred Ex EyPred Ey)

Multiple coherency =
$$\frac{\langle EQ E^{Q*} \rangle}{[\langle EQ E^{Q*} \rangle \langle E E^* \rangle]^{1/2}}$$

E^Q is this expression is a value that should be called a forecast value of the electric field computed from the impedance tensor obtained through computation and the measured value of the magnetic field. It indicates the coherency between measured value E of the electric field and forecast value E^Q of the electric field obtained through impedance analysis. If no noise has entered the measured data, this value is 1. In other words, the data is better when this value is closer to 1 and that the data is worse when this value is closer to 0.

f) Error bar

The error bar shown in the numeral chart and graph of apparent resistivity expresses the product of each apparent resistivity value and the multiple coherency mentioned above.

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III.1.3 One-Dimensional Model Analysis

First of all, one-dimensional model analysis was conducted at each one of all sounding points based on the apparent resistivity value of each period measured by both CSAMT method and MT method. It was conducted in such a manner that an electrical underground layer model of the bed is assumed, a theoretical apparent resistivity curve is obtained and is compared with the curve obtained through measurement; and if they are not matched, the layer model is automatically changed and this sequence is repeated until both of them are completely matched, in order to obtain the depthwise distribution of the underground resistivity. The total conductance value was computed by the following expression after the depth analysis using the one-dimensional model mentioned above.

$$Ct = \sum_{i=1}^{11} (\triangle Hi/\rho i)$$

Ct : Total conductance 1 \triangle Hi : Thickness of layer i (m) 2 ρ i : Specific resistivity of layer i (Ω -m) 3

III.1.4 Two-dimensional Model Analysis

Two-dimensional model analysis was conducted in order to determine the conductive ground layer and the approximate depth of promising fracture in the area in which abnormality in conductance was observed in the total conductance isocontours.

In the two-dimensional model analysis, computation is made assuming that the conductance value is fixed in the direction that is vertical to the specified section. The reason why two-dimensional model analysis is effective despite presence of such an assumption is that it may be considered that even if the electrical structure of the earth in practice is of a three-dimensional structure, it can be similarly handled as a two-dimensional structure in the case where it has a symmetrical axis along a certain direction. Furthermore, the most effective method for application of a two-dimensional model in practice is to select an area in which sudden changes in the conductance value are observed in the total conductance isocontours.

In this two-dimensional model analysis, model computation of theoretical conductance values was repeated, and the two-dimensional model was determined so as to become close to the conductance value obtained from measured values.

In conductance was observed in the total conductance isocontours.

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III.2 Results of Geophysical Analysis

111.2.1 Computation of Geophysical Parameters

Geophysical parameters were computed in accordance with the method described in the preceding section, i.e., method for analysis by MT method. The obtained results are indicated in the results of computation of geophysical parameters in the appendices in the form as output out of a computer. They are arranged for each sounding point and are described as follows.

	Typical result o	
Table 1		

Table 2 Typical simple coherency of magnetic field Typical tipper coherency

Table 3 Typical plotting of tipper magnitude vs. period

Table 4 Typical plotting of tipper strike vs. period

Table 5 Typical plotting of tipper's phase vs. period

Table 6 Typical result of impedance tensor analysis

Table 7 Typical plotting of apparent resistivity vs. period

Table 8 Typical plotting of phase vs. period

Table 9 Typical plotting of rotating angle vs. period

(All of plottings are with error bar indications.)

Table 1 Typical result of tipper analysis

Tipper Results for Station 103 San Kampaeng, Thailand

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PERIOD	TIPPER	MIN TX	STRIKE	PHASE
2.3	1684 +/~ .0787	.0753/+/+/.0709	124.5 +/-19.1	20.7 +/- 9.6
2.3	.1861 +/0752	.0591 +/~ .0597	137.2 +/-11.3	1000 1707 474 741
2.3	.1871 +/0803	.0967 +/0764	165.1 +/-18.9	22.5 +/- 8.9
2.9	.1322 +/~ .0833	.0750 +/0828	146.4 4/-51.8	1.9. +/-31.5
3.0	.1761 +/0946	.0861 +/0833	176.7 +/-24.6	-26.2 +/-12.4
3.0	.1726 +/0956	70826 +/+ .9815	5.0 +/-24.5	15607 +/-13.2
3.8	.4002 +/1684	.0627 +/0888	139.9 +/- 9.4	4,9,+2-7,5
3.9	.4504 +/1722	.1048 +/1112	143.6 +/- 8.4	4.7 +/- 6.2
4.0	.4786 +/1849	,2016 +ZF ,1591	0142,1 +/+11.3	13.9 +/- 6.7
4.9	.7679 +/- ,2954	.1868 +/1768	159.8 +/- 7.1	73.4 +/~ 6.3
5.2	.5771 +/2730	.0025 +/0205	173.2 +/- 8.5	-2.7 +/- 9.5
5.3	,5927 +/- ,2585	.0418 +/0802	167.6 +/- 7.5	-22.9 +/- 8.1
6.4	.4296 +/3012	.2147 +/2424	170.7 +/-38.3	-53.2 +/-29.0
10.7	.1838 +/1542	.0202 +/0558	174.2 +/-24.7	-16.6 +/-29.9
11.1	.2716 +/1917	.0467 +/1972	84.0 +/-27.5	-40.8 +/-21.2
12.8	.1792 +/1422	.0738 +/1014	168.6 +/-35.2	-104.2 +/-39.0
16.0	.1775 +/1422	.0228 +/0519	6.2 +/-19.9	134.0 +/-27.6
18.3	.1677 +/1224	.0329 +/0563	171.0 +/-18.1	-39.9 +/-23.1
20.1	.1430 +/1143	.0238 +/~ .0481	177.9 +/-20.9	-45.1 +/-27.7
25.6	.2671 +/1210	.0534 +/0797	55.7 +/-13.7	-179.3 +/- 8.8
26.9	,1513 +/1055	.0323 +/0492	141.7 +/-16.0	-95.5 +/-22.7
27.7	.1464 +/1110	.0151 +/0360	134.6 +/-17.2	-103.7 +/-24.9

Table 2 Typical simple coherency of magnetic field Typical tipper coherency

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Magnetic Field Coherencies for Station 103 San Kampaeng, Thailand

PERIOD	Coh(HxHy)	Con(HxHz)	Coh(HyH=)	Hz PredHz
2.3	.316	.079	. 973	.007
2.3	.320	.095	.192	.014
2.3	.313	.067	.097	.008
2.9	.251	.043	. 650	.002
3.0	.250	. 844	.073	.004
3.9	. 251	.038	. 068	.003
3.8	.187	. 187	.119	.821
3.9	.221	.124	. 145	.029
4.0	.227	.123	.136	.022
4,9	103	.096	.180	.036
5.2	131	.034	129	.017
5.3	090	.051	.148	.023
6.4		.040	. 055	.002
18.7	.140	. 897	.048	.892
11.1	.208	.086	.005	.002
12.8		.034	.055	.000
16.0	.323	-014	.067	
18.3	.546	.028	.087	.005
				.010
20.1	.568	.082	.115	.810
25.6	590	217	.171	.061
26.9	613	.125	.126	.015
27.7	.627	.126	.103	.017

Table 3 Typical plotting of tipper magnitude vs. period

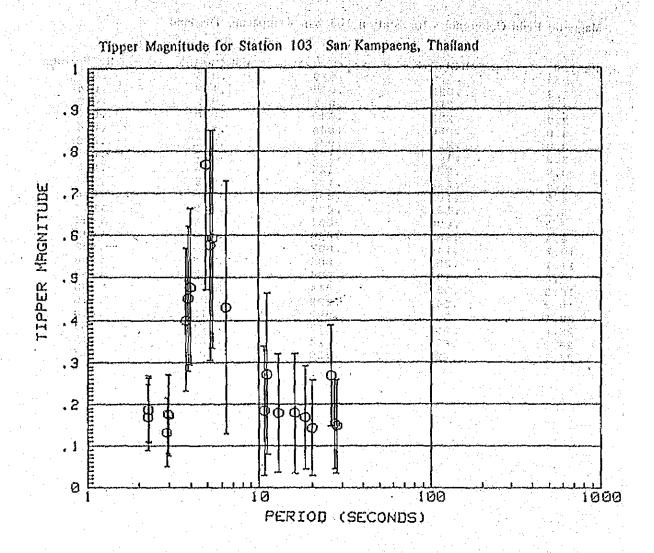


Table 4 Typical plotting of tipper strike vs. period

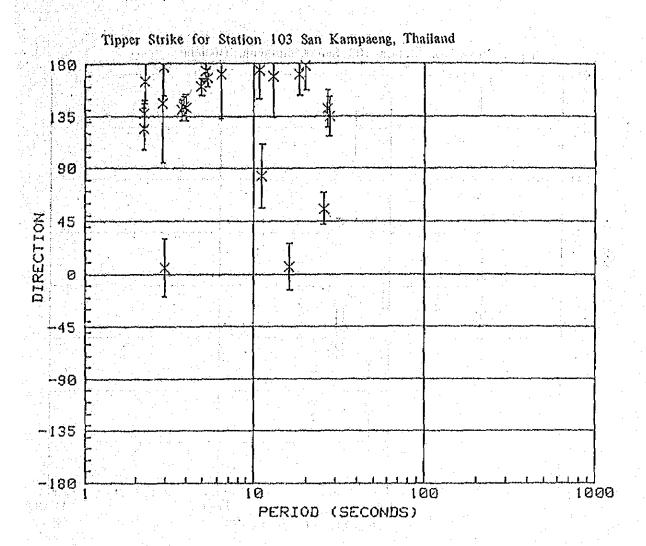
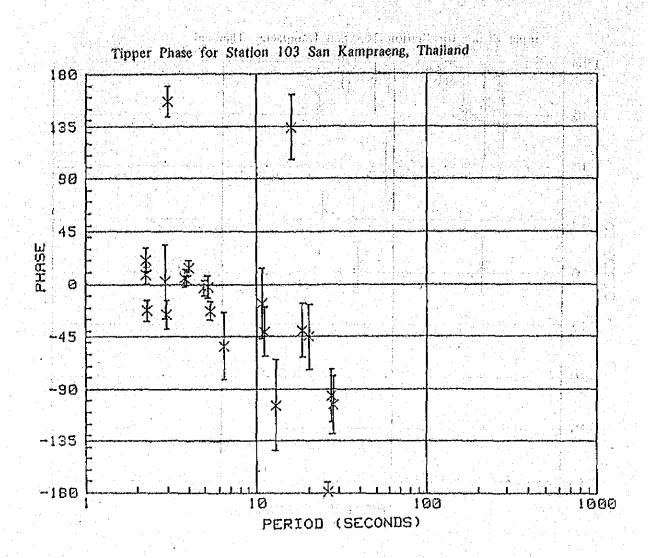


Table 5 Typical plotting of tipper's phase vs. period



	(1) (1) (2) (3) (4) (4)					٠.
						. :
		Table & Trust				
		Taole o Typic	ai result of	Impedance tenso	or analysis	
	MT Resul	ts for Station	103 San Ka	mpaeng, Thailan	d	
	PERIOD	Ex PredEx	Rho X	+/-3.33E+09	PHASE X	
	2.3 2.3	.420		+/-3.15E+00	53.4 +/- 55.4 +/-	
	2.3	.422	9.00E+01		55.8 +/-	
	2.9	. 437	100000	+/-4.43E+00	62.0 +/-	
ilstive 2. p. M. Novike — ne 2.	3,0	. 444		+/-4,70E+00	61.6 +/-	
	3.0 3.8	. 448 . 346	and the second second	*+/~4.36E+00 *+/~4.75E+00	62.5 +/- 62.0 +/-	
क्षिति । यस्ति	3.9	.364	and the second second	+/-4.65E+08	61.6 +/-	
231	4.8	. 379		+/-4.61E+00	63.2 +/-	
	4.9	.361	20 14 14 17 17	+/-4.60E+00	62.2 +/-	
	5.2 5.3	.379 .403		+/-4.29E+00 +/-4.44E+00	65.7 +/- .65.6 +/-	
(B) # . 7 () W	5.4	.324	And the second second	+/-5.35E+00	66.3 +/~	
	6.9	. 366	8.74E+01	+/-5.01E+00	65.7 +/-	1
	7.3	.330		+2-4.88E+00	63.9 +/~	
	8.4 9.3	.333 .352		+/-5.39E+00 +/-5.84E+00	62,6 +/- 59.8 +/-	
	19.7	.538	The second of th	+/-6.20E+60	62.8 +/-	
	11.1	. 564		+/-7.68E+80	62.1 +/-	-
ingstate in the second	12.8	.740		+/~5.72E+00	62.8 +/-	
	14.8 16.0	.860 .873		+/-6.49E+00 +/-9.56E+00	61.3 +/- 62.0 +/-	
海龙 医	18.3	1.018	the second second	+/-8.59E+00	62.1 +/~	
	20.1	1.018	1.96E+02	+/-9.43E+00	62.2 +/-	. 1
	26.9	1.060	the second secon	+/-1.14E+01	60.0 +/-	
	27.7 39.4	1.093 .887	the state of the s	+/-1.35E+01 +/-7.16E+00	59.9 +/-	
i da di kacamata	42.7			+/~1.83E+01		-
States St.	60.2			+/-5.57E+00	51.8 +/-	
	102.4 204.8	.542 .610		+/-1:20E+01	47.8 +/-	
ar en e	204.5	.010	1.036702	+/~1.16E+01	41.3 +/	3
	PERIOD	Ey PredEy	Rho Y		PHASE Y	
$\mathcal{A}_{ij}^{(n)} = \mathcal{A}_{ij}$	2.3	.408 .398		+/-8,66E-01 +/-8,63E-01	-117.6 +/-	
	2.3	. 392		+/-8.07E-01	-117,1 +/-	
	2.9			+/-1.02E+00	-124.7 +/-	
	3.8 3.9	.386		+/-1.17E+00 +/-1.21E+00	-129.2 +/- -128.4 +/-	
	4.8	.390 .378		+/-1,215+00 +/-1,16E+00	-129.7 +/-	
	4.9	.347		+/-1.24E+00	-125.3 +/-	3
•	5.2	.364		+/-1.25E+00	-126.8 +/-	
	5.3 6.4	,370 ,377		+/~1.16E+00 +/~1.39E+00	~126.1 +/~ -135.6 +/~	
	6.9	.381		+/-1.48E+00	-130.3 +/-	
	7.3	.367	1.125+01	+/-1.27E+00	-128.5 +/-	3
	8.4	.326		+/-1.56E+00	-121.2 +/-	
	9.3 12.8	.312 .755		+/-1.47E+00 +/-1.03E+00	-119.8 +/- -116.4 +/-	_
	14.8			+/-3.77E-01	-118.9 +/-	
	18.3	. 996	1.88E+01	+/-1.268+00	-114.2 +/-	3
	26.1	1.019	and the second s	+/-1.54E+00	-112.5 +/-	
	26.9 27.7	1.060		+/-1,84E+00 +/-2,18E+00	-111.3 +/- -113.5 +/-	
	39.4	.884		+/-2.89E-01	-111.4 +/-	,
			8.91E+90			

PERIOD SKEN ROT ANG Con(HxHy) (ExHx) (ExHy) (EyHy) (EyHy) 2.3 14 +/02 -60.4 +/- 1.3 .316 .458 .603 .631 .297 .20 .14 +/02 -61.4 +/- 1.3 .316 .458 .603 .631 .297 .20 .14 +/02 -61.4 +/- 1.3 .313 .449 .592 .625 .297 .20 .20 .47 .02 -61.4 +/- 1.2 .251 .461 .573 .619 .241 .30 .21 .47 .02 -64.1 .47 .22 .251 .461 .573 .619 .241 .30 .21 .47 .02 -64.1 .47 .22 .251 .464 .576 .623 .266 .266 .38 .21 .47 .02 .47 .47 .47 .47 .47 .48 .480 .623 .21 .47 .02 .47 .47 .47 .47 .47 .48 .480 .623 .21 .49 .24 .47									
PERIOD SKEM ROT ANG Con(HxHy) (ExHx) (ExHy) (EyHx) (EyHy) 2.3									
PERIOD SKEM ROT ANG Coh(HxHy) (ExHx) (ExHy) (EyHx) (EyHy) 2.3									
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2.3	1 415 4 4 4		** **********************************		はんじつんじゅう ごくじいしつか	计二十分 化二二甲甲烷 有原始的 建氯	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		A STATE OF THE STA
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3.0							and the second of the second		
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7.3						.429	.465		
8.4			64:1 +/-	1.8	. 101				
9.3			-63.1 +/-	2.8	.052		and the second of the second		
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12.8	11.1					2 22 2 32 4	2 S 2 S 2 S 3		
14.8						The state of the s			
16.8							5 4 5 4 5 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		
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102.4 .60 +/05 -40.0 +/- 1.5 .270 .255 .655 .684 .372								12.74	
706								.684	.372
	204.8	· · · · · · · · · · · · · · · · · ·				.468	.759	183.	.706

Table 7 Typical plotting of apparent resistivity vs. period

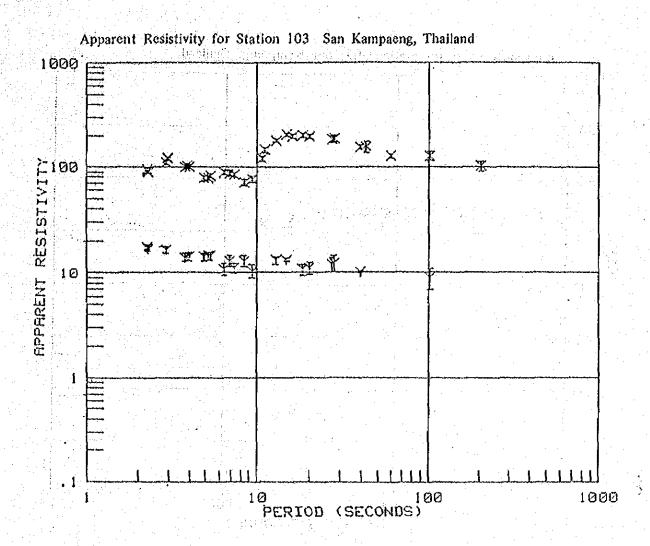


Table 8 Typical plotting of phase vs. period

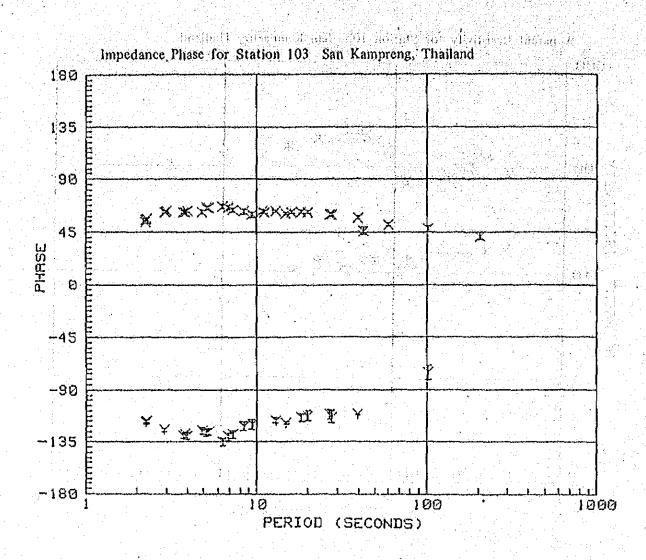
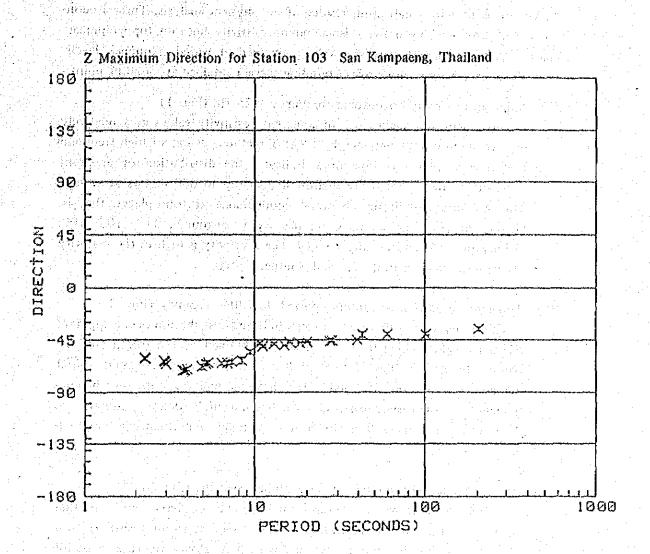


Table 9 Typical plotting of rotating angle vs. period



III.2.2 Drawings Indicating Results of Analysis

Apparent resistivity isocontours at three frequency (period) levels were drawn up as drawings indicating results of geophysical analysis. These isocontours were produced by drawing iso-apparent-resistivity lines on topographical maps with the apparent resistivity values obtained at varied frequency levels from the apparent resistivity curves (sounding curves) obtained at sounding points.

(1) Apparent resistivity isocontour; frequency 8,75 Hz (Fig. 1)

This isocontour makes use of apparent resistivity values at a relatively high frequency level obtained by CSAMT method. Being of high frequency level means that this isocontour indicates the distribution of apparent resistivity values at relatively shallow depths (up to 600 meters at average). This isocontour indicates abnormal conductance at four places, that is, vicinity of sounding points 0-1; place that surrounds 2-2, 105' 109; vicinity of 2-7; and vicinity of 119. The resistivity is high in the majority of western part, central part and southern part.

(2) Apparent resistivity isocontour; period 11.1304 secounds (Fig. 2)

This apparent resistivity isocontours indicates distribution of the apparent resistivity values along the main direction obtained by the rotation of the coordinates axis in the MT method. The central area that surrounds sounding points 2-2, 106, 109 and 110 indicates a major abnormality in conductance. In the eastern part, the area that surrounds sounding points 4-5, 3-6, 112, 118 and 119 is also a zone of major abnormality in conductance.

(3) Apparent resistivity contour; period 39.384 seconds (Fig. 3)

This isocontour was also drawn up in a manner that is equal to that of Fig. 2. However, it indicates distribution of apparent resistivity at a very deep depth because of use of apparent resistivity values at a period of 39.384 seconds.

When a comparison is made with the results obtained in 1983, it is learned that the area of abnormal conductance at the central part has become slightly small and that the area of abnormal conductance in the eastern part has considerably become large.

III.3 Results of One-Dimensional Analysis

111.3.1 One-Dimensional Model Analysis

The underground layer models for this survey were determined as shown in the computer output forms of results of depth analysis attached to the end of this report. They are arranged for each sounding point.

The details of the matters indicated in the attached computer output forms showing the results of analysis are as follows.

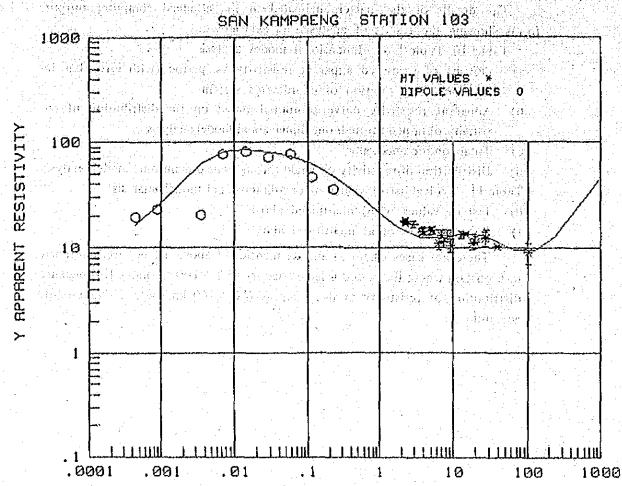
Table 10 Typical one-dimensional model analysis

- a) Plotting of measured apparent resistivity vs. period (with error bar indication) after rotation of coordinates system
- b) Apparent resistivity curve computed based on the distribution of resistivity obtained through one-dimensional model analysis
- c) Total conductance value
- d) Distribution of resistivity obtained through one-dimensional model analysis Table 11 Typical list of values of one-dimensional model analysis
- e) List of values of b) mentioned above
- f) List of values of a) mentioned above

There are cases where a) and b) mentioned above are not well matched in a portion where the period is large (vicinity of T = 100 seconds). It is because distribution of resistivity at deep depths (40 to 60 km) was not taken into account.

Table 10 Typical one-dimensional model analysis





PERIOD (SECONDS)

TOTAL CONDUCTANCE = 281.8 (MHOS) (FOR TOP 7 LAYERS)
LAYERED MODEL

RESISTIVITY	рертн(ки)	ALTITUDE(N) 360.0 (SURFACE)
23.0	.021	339.0
3.8	.024	336.0
408.8	,350	10.0
40.0	1.000	-640.9
3.0	1.010	-650.0
15.0	1.300	-940.0
5.0	2.500	-2140,0
25.0	8.000	-7640.0
6.0	15.000	-14640.0
	and the second s	

Table II Typical list of values of one-dimensional model analysis

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MODEL.	DATA	Y-AXIS	FIELD DATA
PERIOD	APPARENT	PERIOD	APPARENT
(SECONDS)	RESISTIVITY	(SECONDS)	RESISTIVITY
0004	16.46	.0004	19,33
.0009	24.60	. 0009	22.84
.0018	40.55	.0036	20.49
.0036	62.49	.0071	77.75
.0071	Blatter 80 • 16 and 5 5 and 5 6	.0143	89.73
.0143	84.69	.0286	72.52
. 0286	97 - Sept. 97	.0571	77.14
.0570	[17] · 特别 73。[77] (計畫學》))	1143	46.26
.1143	62.50	.2283	35,43
.2286	6 7976 97×72 9 9000 - 1 1	2.2605	17.37 + .866
.4571	33.48	2.2756	17.52 + .863
.9143	22.18	2.2957	16.84 + ,807
1.8286	15.13	2.9257	16.45 + 1.015
3.6571	12.18	3.7926	14.01 + 1.168
7.3142	12.32	3.9084	14.36 + 1.205
14.6284		4.0000	14.03 + 1.157
29.2569	12.56	4.9231	14.09 + 1.239
64.0000	9.51	5.1717	14.53 + 1.247
128.0000	9.33	5.3333	14.47 + 1.163
234.0550 468.1100	12.59	6.4000	10.88 + 1.386
936.2244	22.27	6.9189	12.95 + 1.483
730.2244	43,08	7.3143	11.15 + 1.268
		8.3934	13.00 + 1.556
		# 19 tale 1	10.41 ± 1.466
وأكلم مواكنك		12.8000	13.13 + 1.033
		14.8406	13.35 + .377
		18.2857	10.78 ± 1.262
		20.6784	11.13 + 1.540
		26.9474	12.04 + 1.838
		27.6757	12.24 + 2.177
		39.3846	10.13289
i ji ey asalka	Statistical Contraction of the	102.4000	8.91 ± 2.011

111.3.2 Electrical Classification of Layers

Next, classification of layers was made using electrical synthetic layers over the entire survey area based on the results of one-dimensional analysis at each of the sounding points mentioned earlier. The resistivity value of each layer was represented by the mean value of resistivity obtained through one-dimensional analysis for each point. Classification was made to the following four combinations from the results of measurements at 53 sounding points in total including the sounding points at which measurements were taken in 1983.

R Indicates a layer of high resistivity and C indicates a layer of high con-

First combination

This combination is composed of the following 7 sounding points at which the total conductance value is up to 50 mho.

Sounding points: 1-3, 2-0, 3-0, 3-4, 4-2, 101 and 108

Mean	resistivity value		Corre	ponding	layer	name
	2170,0 Ω m			Ra 1) 3
All Marie	3,0			Ca		
	2870,0			Rb I		
	5,0			Cb		1
	3417,0			Rc I		
	54,0			Cc 1		
				Founda	tion	

The foundation is of extremely high resistivity. Symbol R indicates a layer of relatively high resistivity and symbol C indicates a bed of high conductance.

Second combination

This combination is composed of the following 12 sounding points at which the total conductance value is over 50 to 100 mho.

Sounding points:
$$0-1$$
, $0-2$, $1-1$, $1-2$, $2-4$, $2-5$, $2-6$, $3-1$, $4-0$, $4-1$, 102 and 111

Mean resistivity value	Corresponding	bed name
533.0 Ω·m	Ra 2	
3.0	Са	
618.0	Rb 2	1.0
5.0	Сь	
4250.0	Rc 2	
35.0	Cc 2	
	 Founde	Hon

Third combination

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(ABSTERVED)

This combination is located on the west side of sounding point 112 and includes sounding points of total conductance value of over 100 mho.

विकास के कार्य के का

This combination is composed of the following 23 sounding points.

Sounding points:
$$0-3$$
, $1-0$, $1-4$, $1-5$, $1-6$, $1-7$, $2-1$, $2-2$, $2-3$, $2-7$, $3-2$, $3-3$, $3-5$, $4-3-2$, $4-3$, $4-4$, 103 , 104 , 105 , 106 , 107 , 109 and 110

Mean resistivity value. Corre	sponding bag name
565.0 Ω·m	Ra 3
30 Burgilian Spring spring and interpretation of the second	Ca
858.0	Rb 3
2001.0	Cb
3961,0	Rc 3
29.0	Cc 3
	Foundation

There occasionally are cases where base Cc 3 is of an extremely large To an thickness. A factor of the control of the con

read Fourth combination to the second

thanker it was begin in the con-

Friedrick Land History Co. Company Co.

This combination is composed of 11 sounding points of total conductance value of over 100 mho. This combination includes sounding point 112 and measuring points located on its east side.

Measuring points: 3-6, 4-5, 112, 113, 114, 115, 116, 117, 118, 119 and 120

Mean resistivity value Corre	sponding bag name
130.0 Ω·m	Ra 4
hold (\$10.00) a feet as it was etter feet etta.	Ca
14 E. Gio 81:0 y a haep feolad His His gira (Yangaya)	Rb 4
ent de la como de la colonida en la como de la colonida en la colo	Cb
5687.0	Rc 4
me and 27.0 g at the entertain and the parties of	Cc 4
et et let totel elikalige et la samma som by lokelige.	Foundation

The foundation is not of so high resistivity, and base Cc 4 is of a very large thickness. Palito de la apart

Salah Salah Salah Salah

111.3.3 Drawings indicating results of one-dimensional analysis

(1) Total conductance isocontour (Fig. 4)

This drawing was drawn based on the total of conductance of each layer obtained through one-dimensional model analysis mentioned earlier.

The total conductance is what was obtained with the Rc¹ layer or the upper layer of the electrical foundation.

(2) Structure isocontours for the top of conductive formation (shallow part and deep part) (Fig. 5, Fig. 6).

Structure isocontours for the top of conductive formation for the shallow part and deep part were drawn up like in the previous year. Structure isocontour for the top of conductive formation for the shallow part (Fig. 5) is what indicates the boundary plane of Ra layer bottom and Ca^2 layer (3 Ω -m) from the sea level. Structure isocontour for the top of conductive formation for the deep part (Fig. 6) is what draws the top of the Cb^2 layer (5 Ω -m).

(3) Isopachs of the high resistivity overburden (Fig. 7)

This drawing indicates changes in the thickness of the overburden of high resistivity that covers conductive layer Cb¹. (It was considered that the thickness of the Ca layer can be ignored because it is thinner than the Cb layer.)

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(4) Electrical foundation drawing (Fig. 8) had been been been a being being

This drawing indicates the depth from the sea level of the lower part of conductive layer Cb. According to the result of this survey there are cases where the resistivity vakue of the electrical foundation is not large.

III.3.4 Results of Analysis

Two major conductive layers were indicated in the survey area as a result of one-dimensional analysis. One is the Ca layer (mean resistivity 3 Ω -m) located in a shallow part, and another is the Cb layer (mean resistivity 5 Ω -m) located in a deeper part.

Two places with abnormal conductivity can be observed in the total conductance isocontour. One is located in the central part that includes sounding points 2-1, 2-2 and 103, and another is located in the south-eastern part that includes sounding points 3-6, 4-5, 112 and 113. The expansion of the place with abnormal conductance is the south-eastern part was clarified as a result of this survey, and it was found out to be of a considerably large area size.

The inclided axis shown in the structure isocontour for the top of conductive formation (deep part) and this place where total conductance is abnormal are almost match. Furthermore, they are also matched with the inclined axis of the electrical foundation. It has become apparent, therefore, that a thickconductive layer is located on top of the raised electrical foundation and that it indicates abnormal conductivity.

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111.4 Results of Two-Dimensional Model Analysis

Results of two-dimensional model analysis of two sections named 1-84 and 2-84 are shown in Fig. 9 and Fig. 10 respectively.

Section 1-84 runs across sounding points 1-2, 105, 2-2, 106 and 3-2; and section 2-84 tuns across sounding points 2-1, 103, 2-2, 109 and 2-3. These two sections make intersection almost vertically to each other.

Symbol F used in the results of two-dimensional model analysis means a fracture zone, and it indicates a narrow and small form of very high conductance. Its resistivity value was assumed as 1 Ω -m here.

Section 1-84 (Fig. 9)

Four new layers $Cb-b_1$, $Cb-b_2$, $Cb-b_3$ and $Cb-b_4$ are required besides layer Cb-b having a resistivity value that is same as what was indicated in the report of the primary investigation, and the range of their resistivity values is 26 to 36 Ω -m.

As for the range of high resistivity, the resistivity values which are same as those of the last time were used for layers Ra, Rb, Rc, Ra-b and Ra-a (it is same as Ra-a mentioned earlier).

Additional layer Ra-a₂, which is of a resistivity that is slightly higher than that of Ra-a₁, was necessary to match the total conductance value.

Use of many additional layers appears to be in conflict with the conception of standard columnar sections of four types described in section 3 of this chapter. But standard columnar sections were determined based on one dimensional hypothesis, and these layers have become necessary in order to cause the measured values to match the computed values of conductance using two-dimensional models.

Section 1-84 indicates that sounding point 2-2 is located almost at the center of a thick conductive layer (a relative narrow zone of about 400 to 500 meters of high resistivity is located in it). Furthermore, a very thick surface soil layer (Ra layer) has developed on the west side of sounding point 1-2 and on the east side of sounding point 3-2.

Section 2-84 (Fig. 10)

Very good match is also observed in this section between the measured values and computed values of conductance like in section 1-84 mentioned earlier. Sounding point 2-2 is located almost at the center of a thick conductive layer located at the depths of 1 to 3 kilometers. It is learned that the conductive layer that is located along this section is considerably larger than that is located along section 1-84.

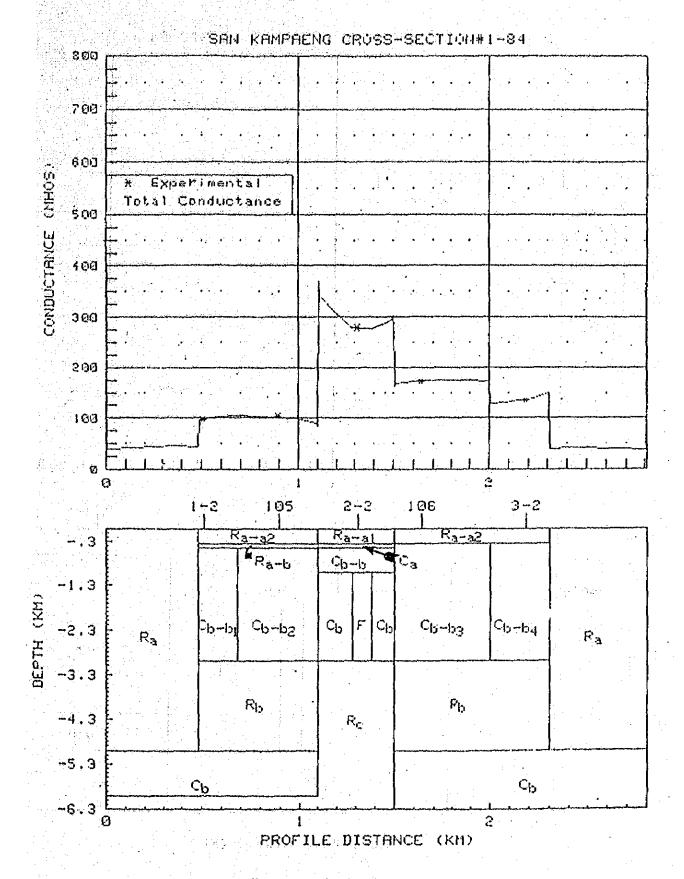


Fig. 9 Section 1-84

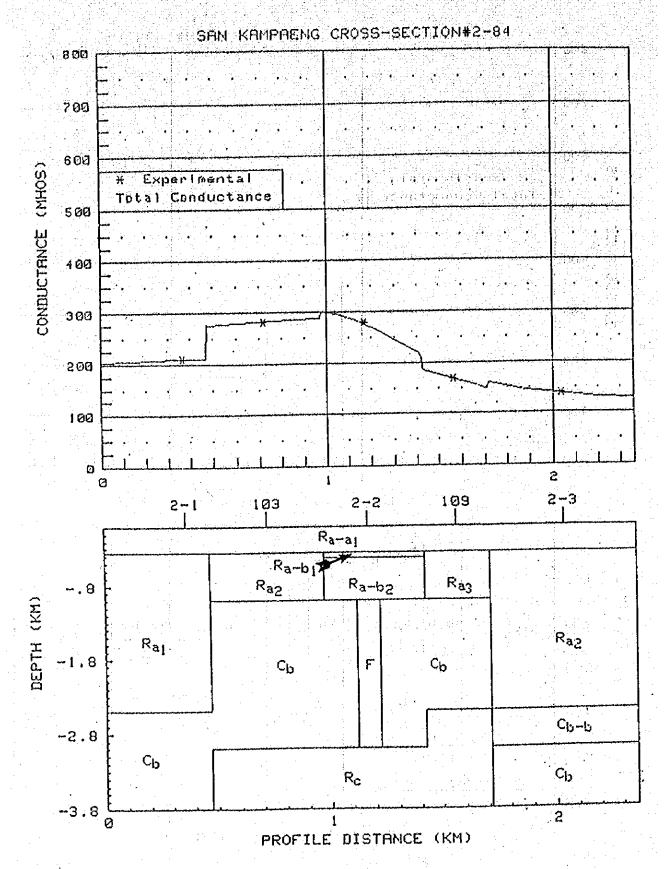


Fig. 10 Section 2-84

IV. Summary

IV. SUMMARY

Two areas which are regarded as promising geothermal zones which can be recommended as the points of excavation can be indicated in the San Kampaeng survey area based on various isocontours obtained earlier and two two-dimensional models. These two interesting areas may be decided as they are drawn with 200 mho contour lines in the total conductance isocontours. The following three promising excavation points can be recommended in these two areas.

i) Sounding point 2-2

Sounding point 2-2 is located in the central part with abnormal conductance that includes sounding points 2-1, 2-2, and 103. This abnormal part is slightly long along the axis in NW-SE direction. (Both of the two two-dimensional sections indicate that this sounding point is located about at the center of the conductive layer and that the conductive layer is as thick as about 2,000 meters. It is considered that the possibility of appearance of a good fracture is very high in such a thick layer.

ii) Sounding point 4-5

The abnormal part in the eastern part is particularly attractive because its scale is large, and it is estimated that sounding point 4-5 is a promising excavation point.

This sounding point is located in a zone where the local geological conditions are equal to what are observed at sounding point 2-2 (high total conductance value, along the inclined axis of electrical foundation and thick conductive layer). This sounding point, therefore, can probably be recommended as a promising excavation point due to the same reasons.

iii) Sounding point 112

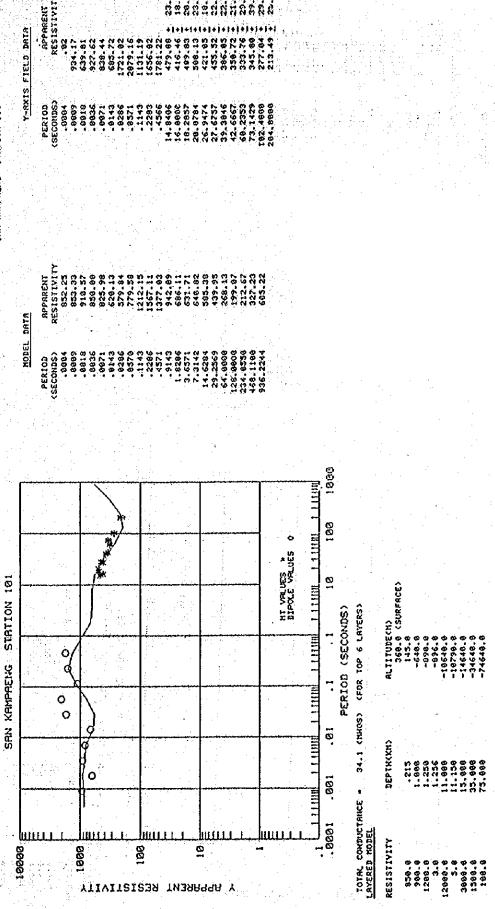
Sounding point 112 located on the north side of the abnormal conductance area in the eastern part indicates that there is a deep but very thick conductive layer. This sounding point, however, is relatively isolated. If additional measurements are taken at a number of points in the vicinity of this sounding point, it will become clear whether a thick conductive layer can be expected in the shallow part of the vicinity of this abnormal conductance area or not.

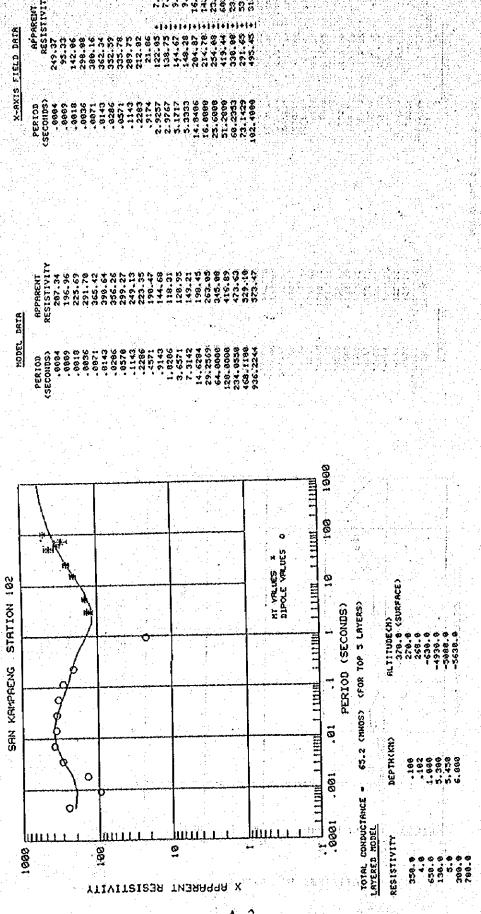
V. References

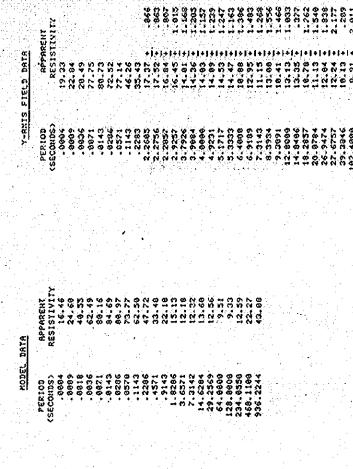
V. References

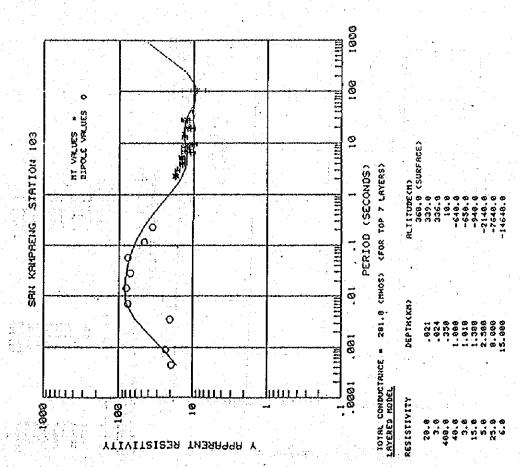
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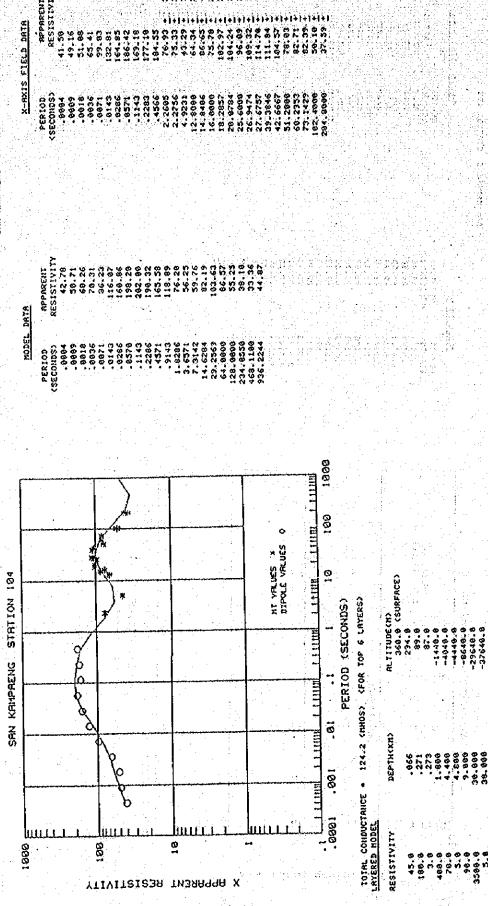
APPENDED DRAWINGS

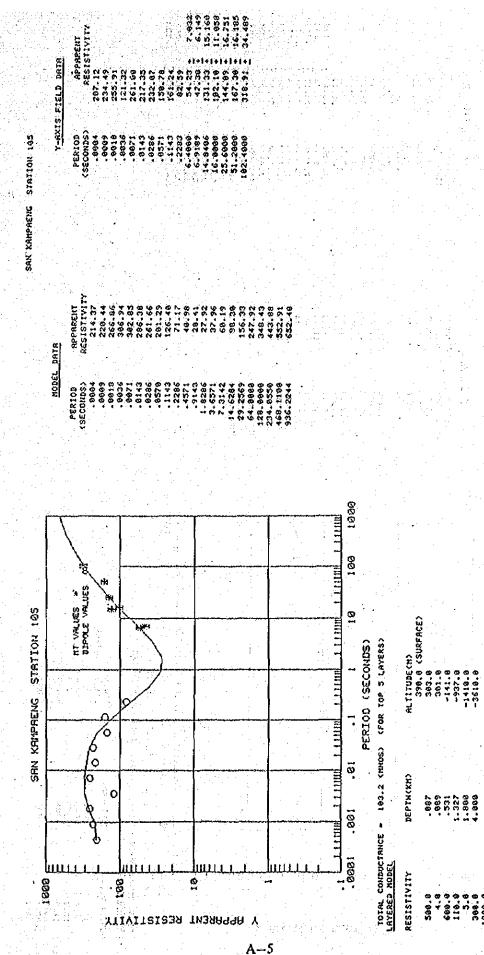


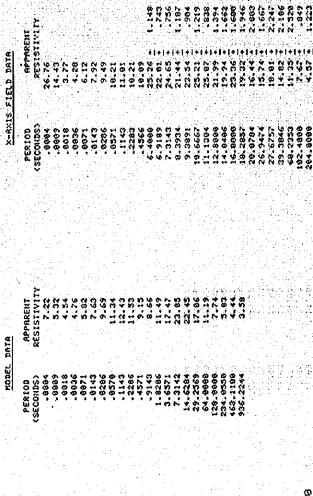


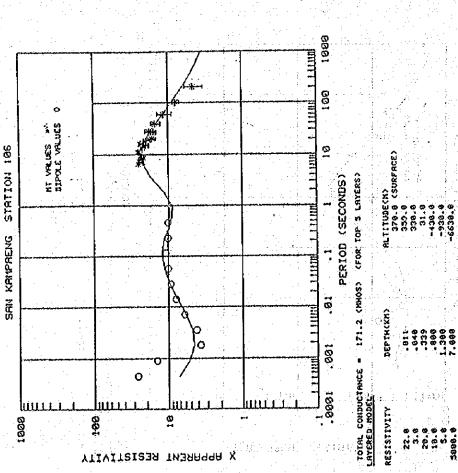


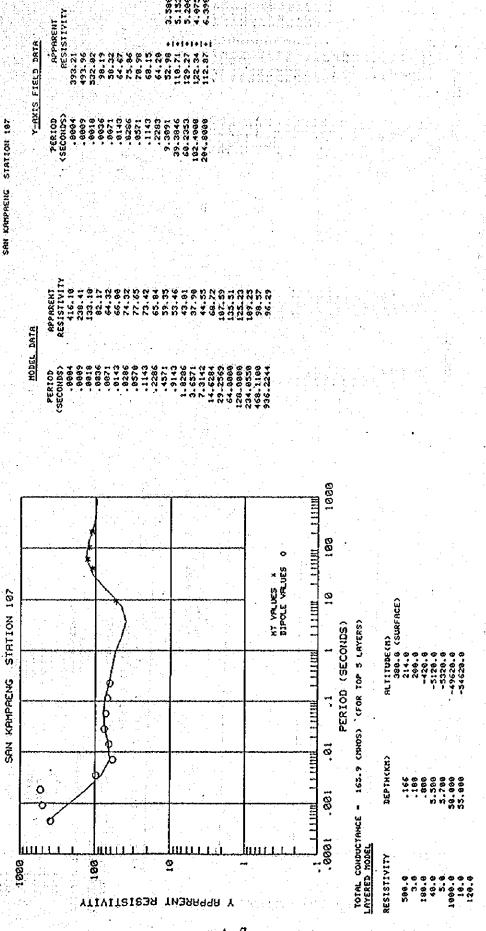


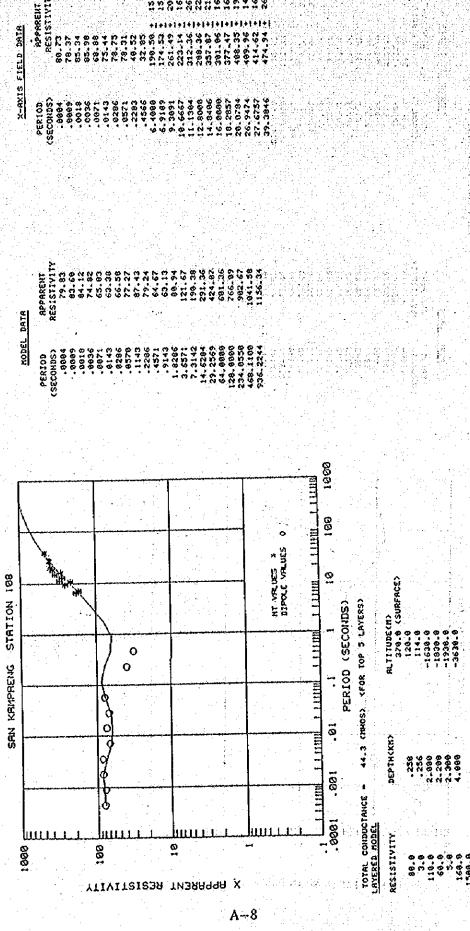




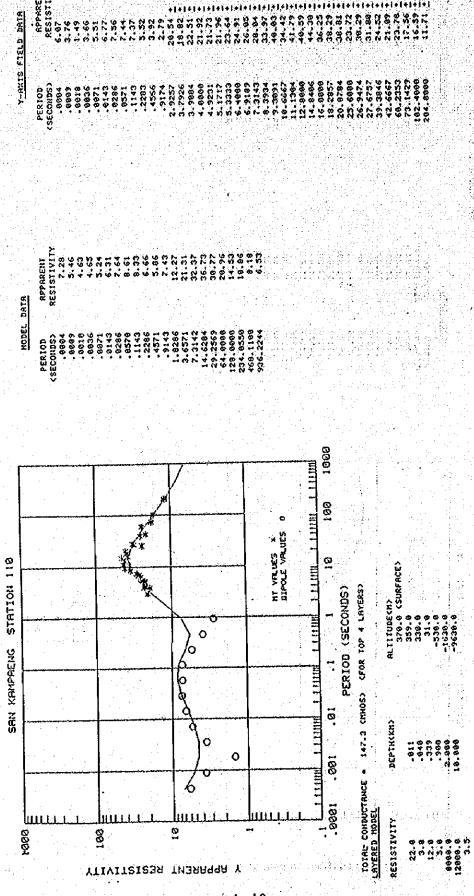


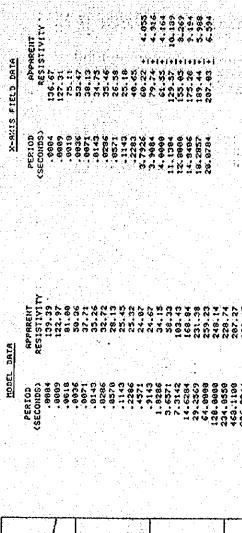


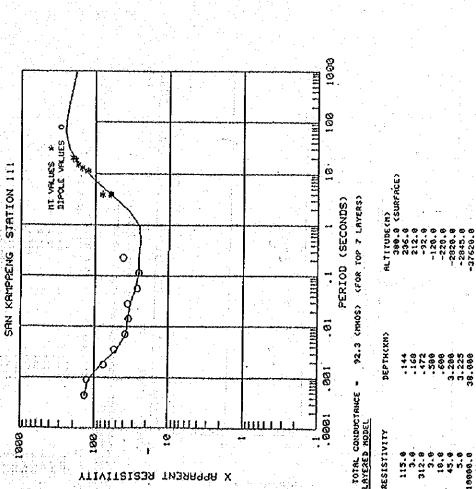


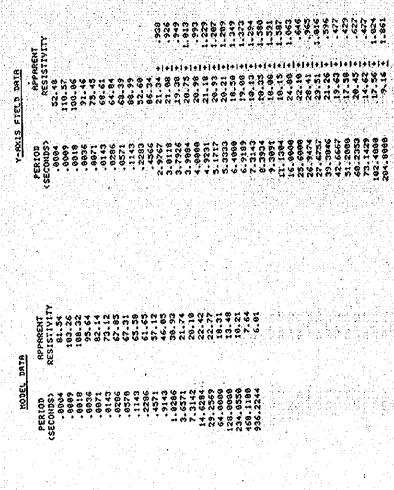


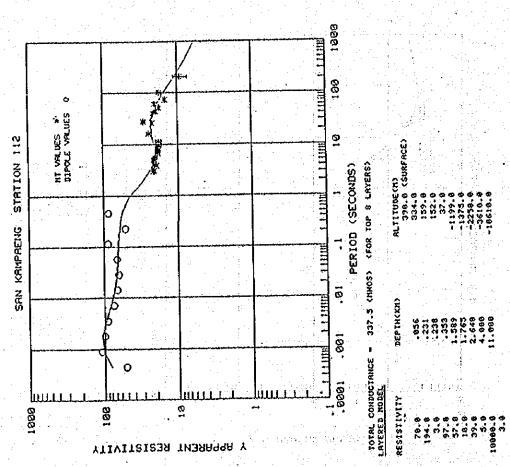
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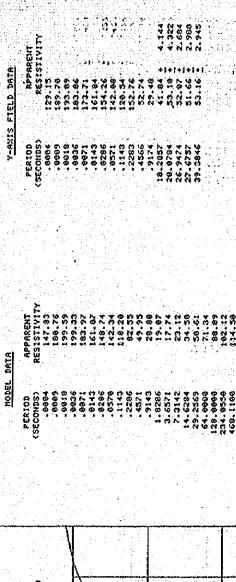


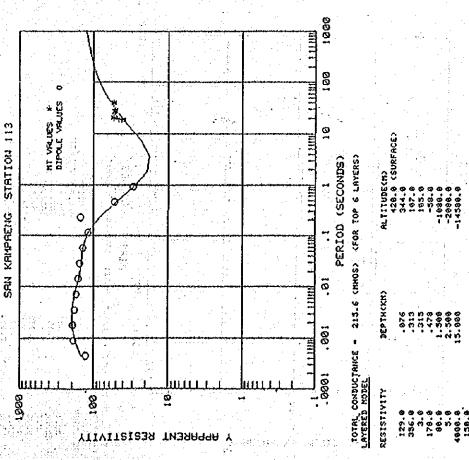






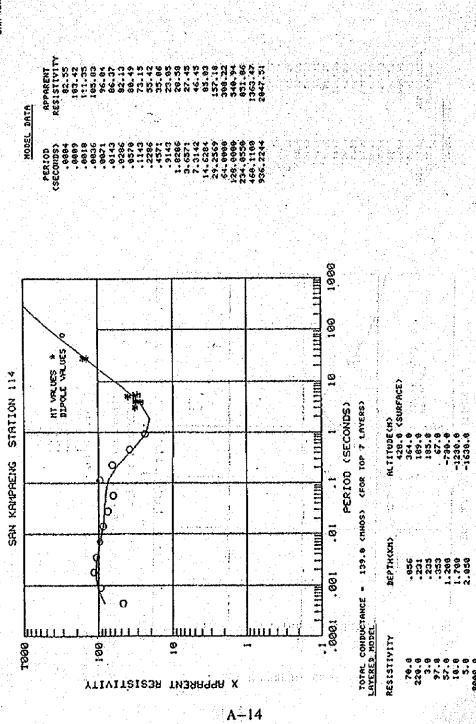




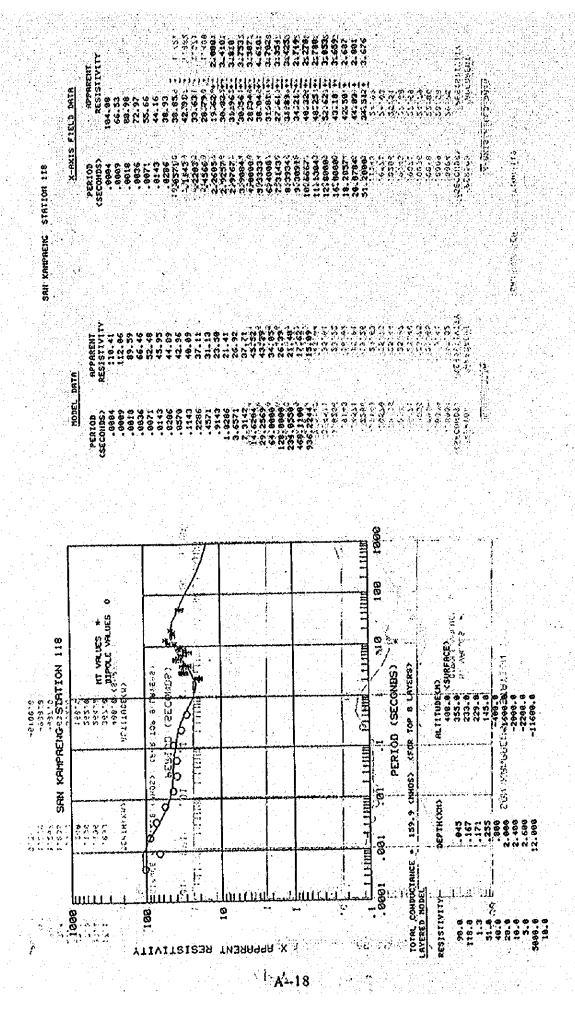


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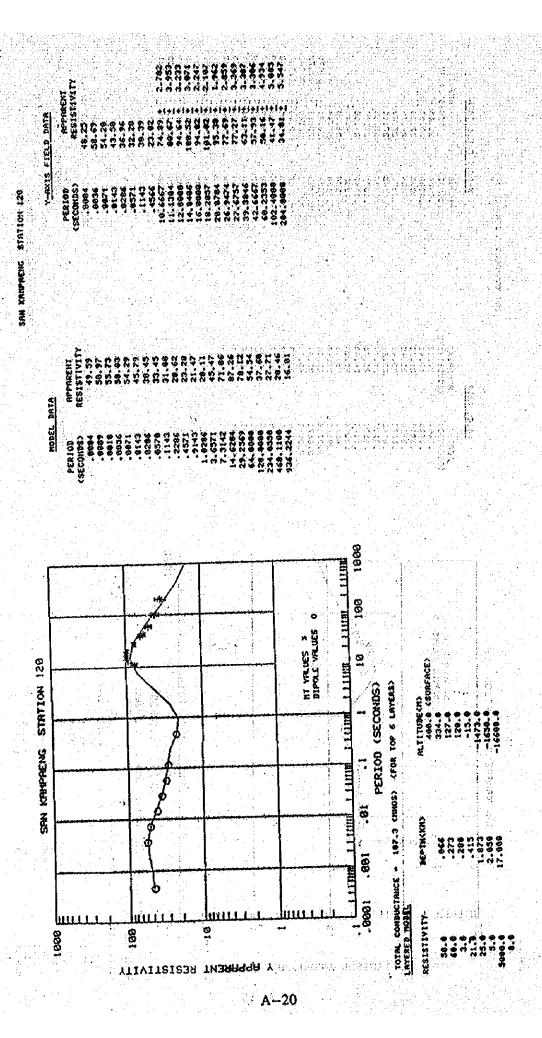


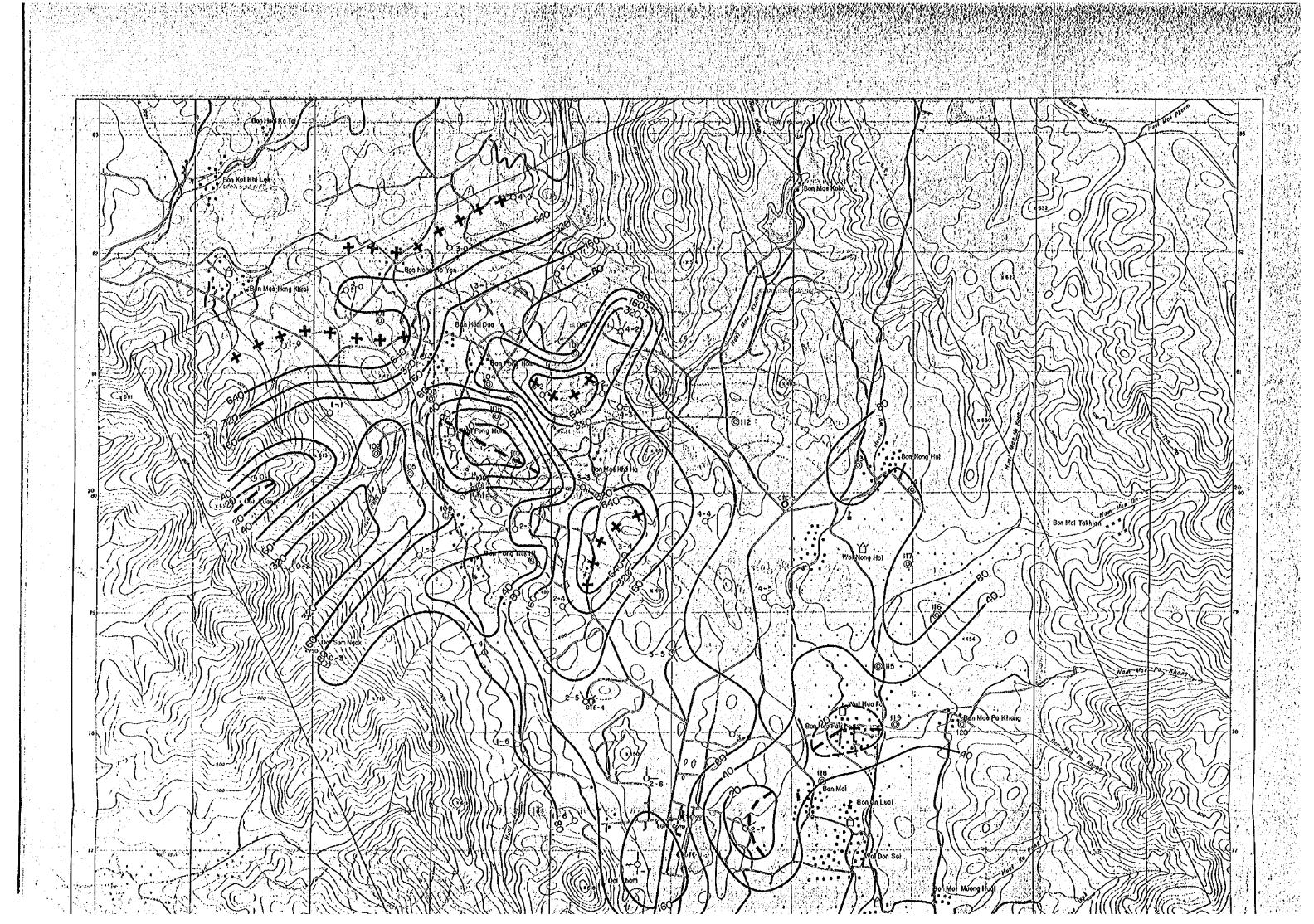
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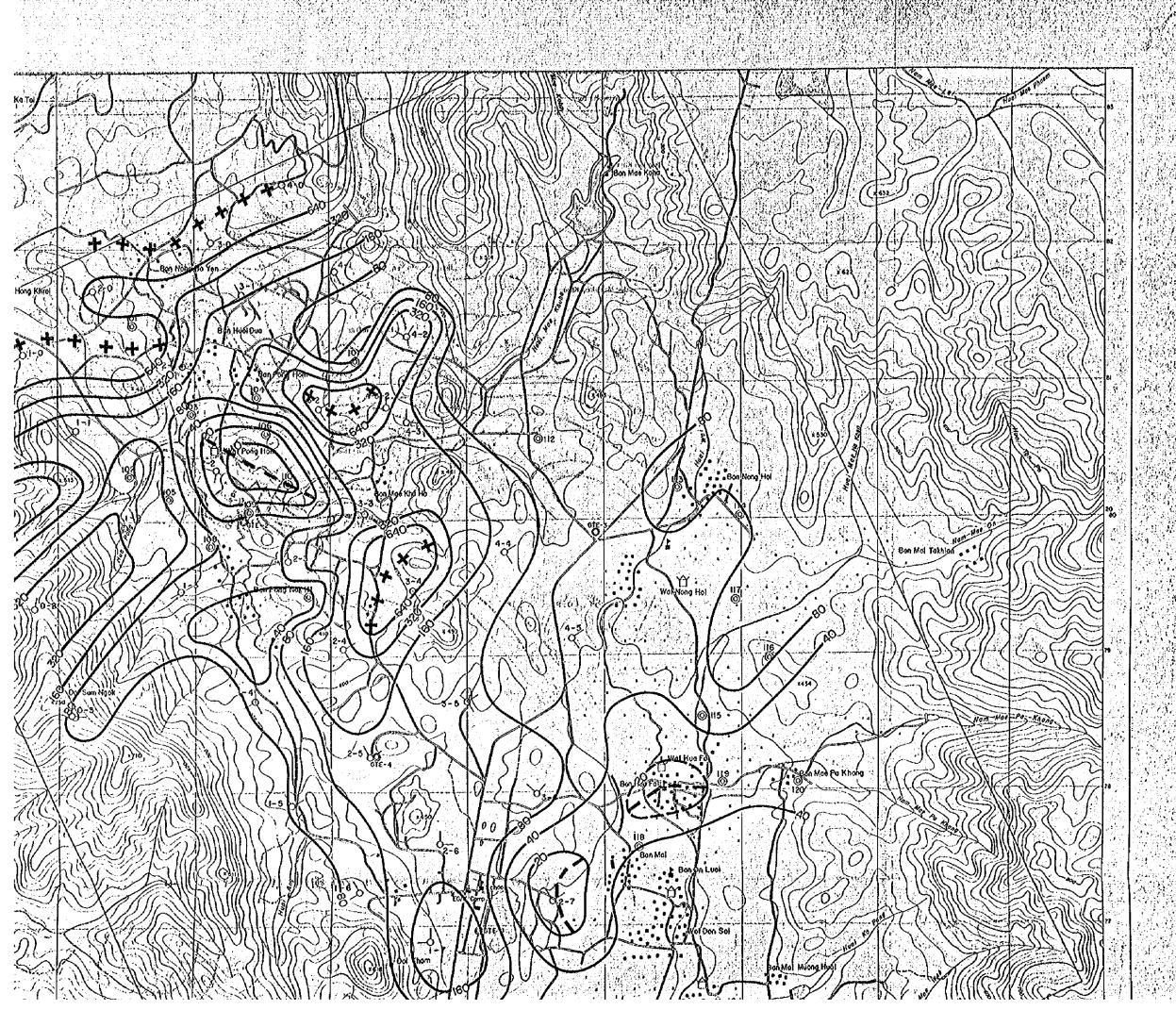


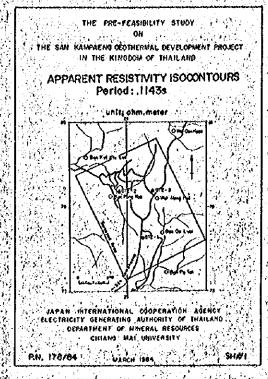
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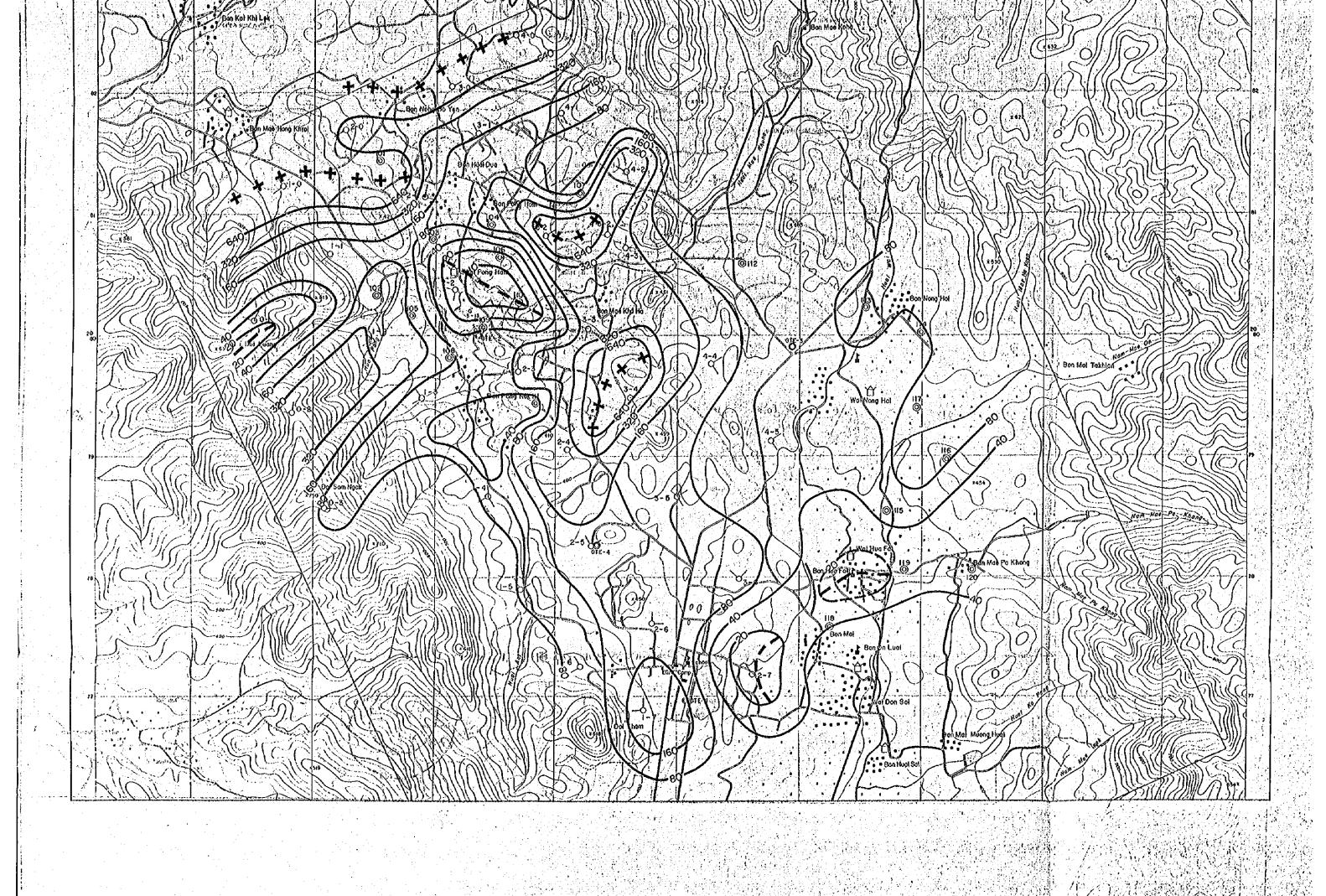
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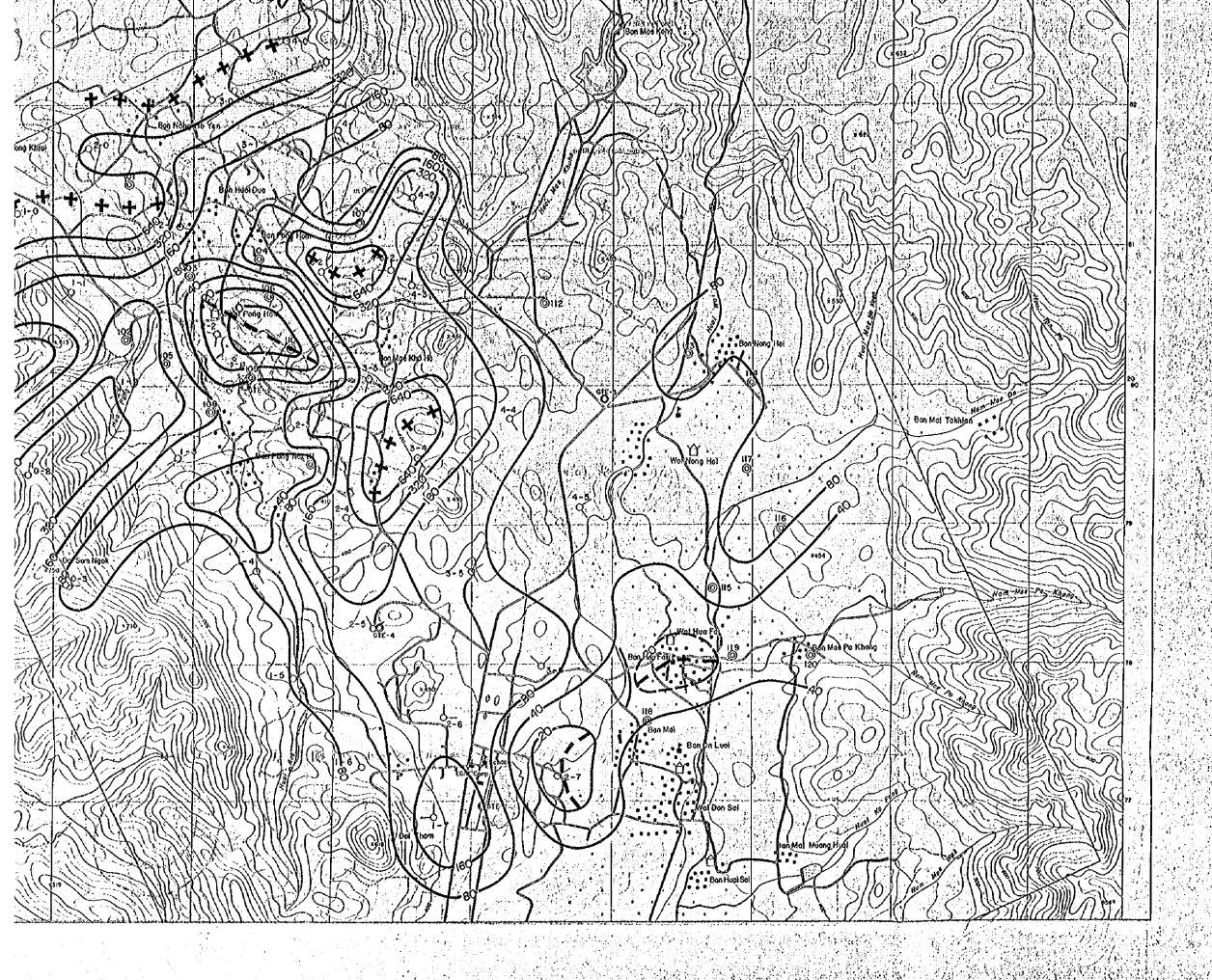
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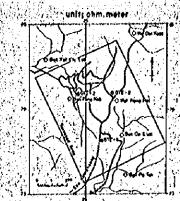
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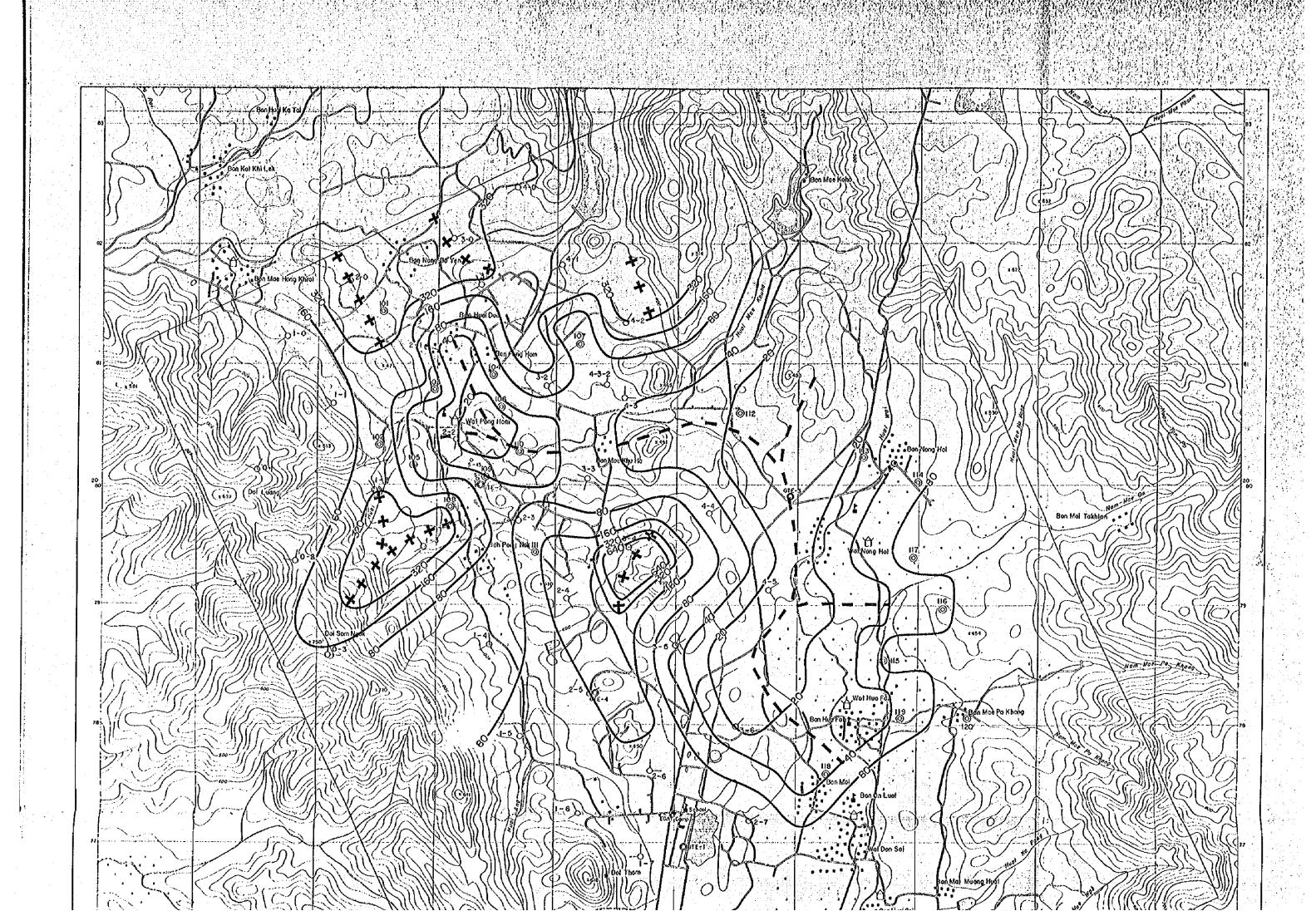
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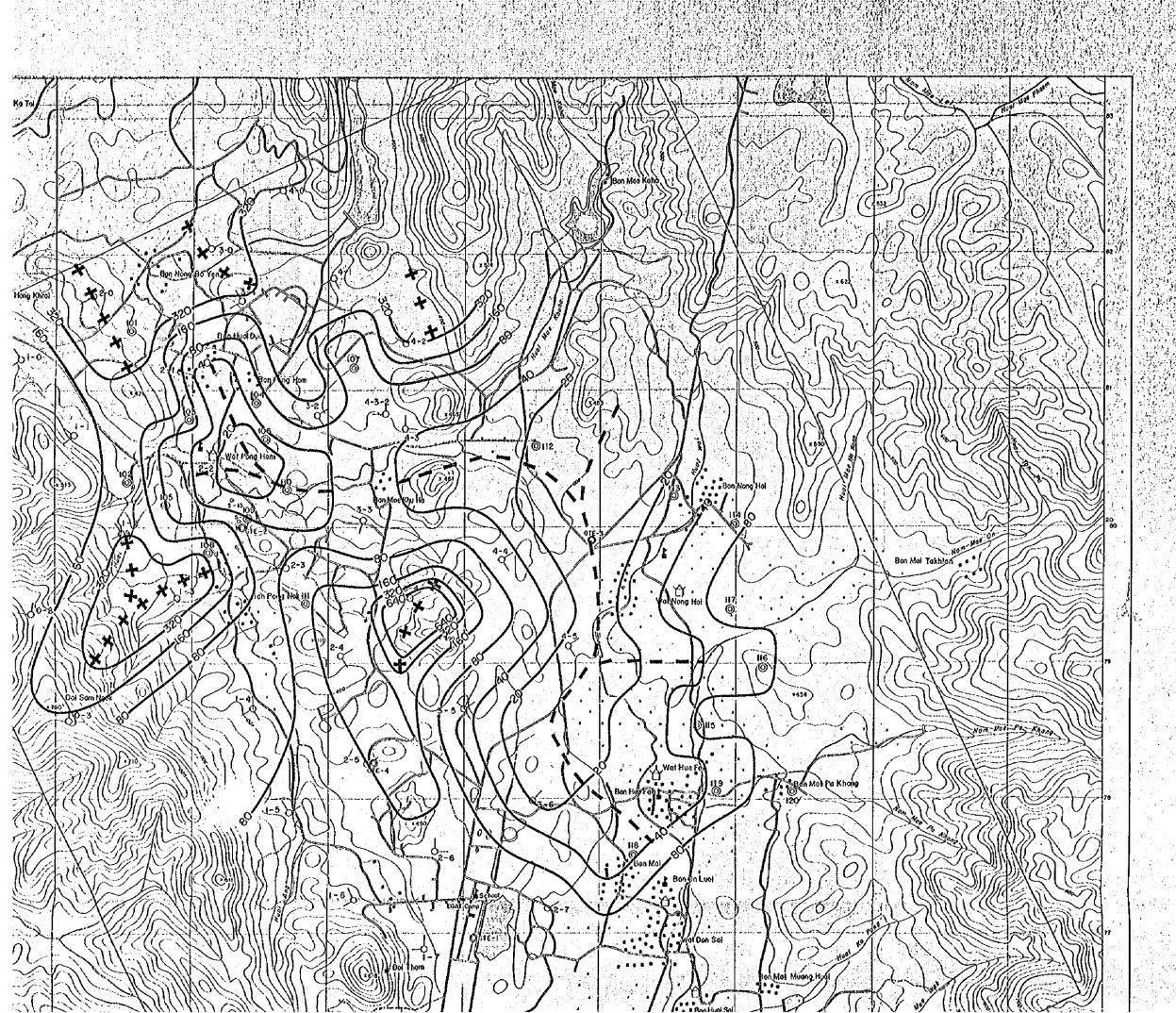


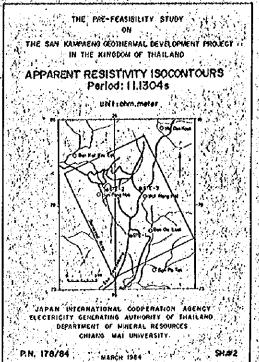
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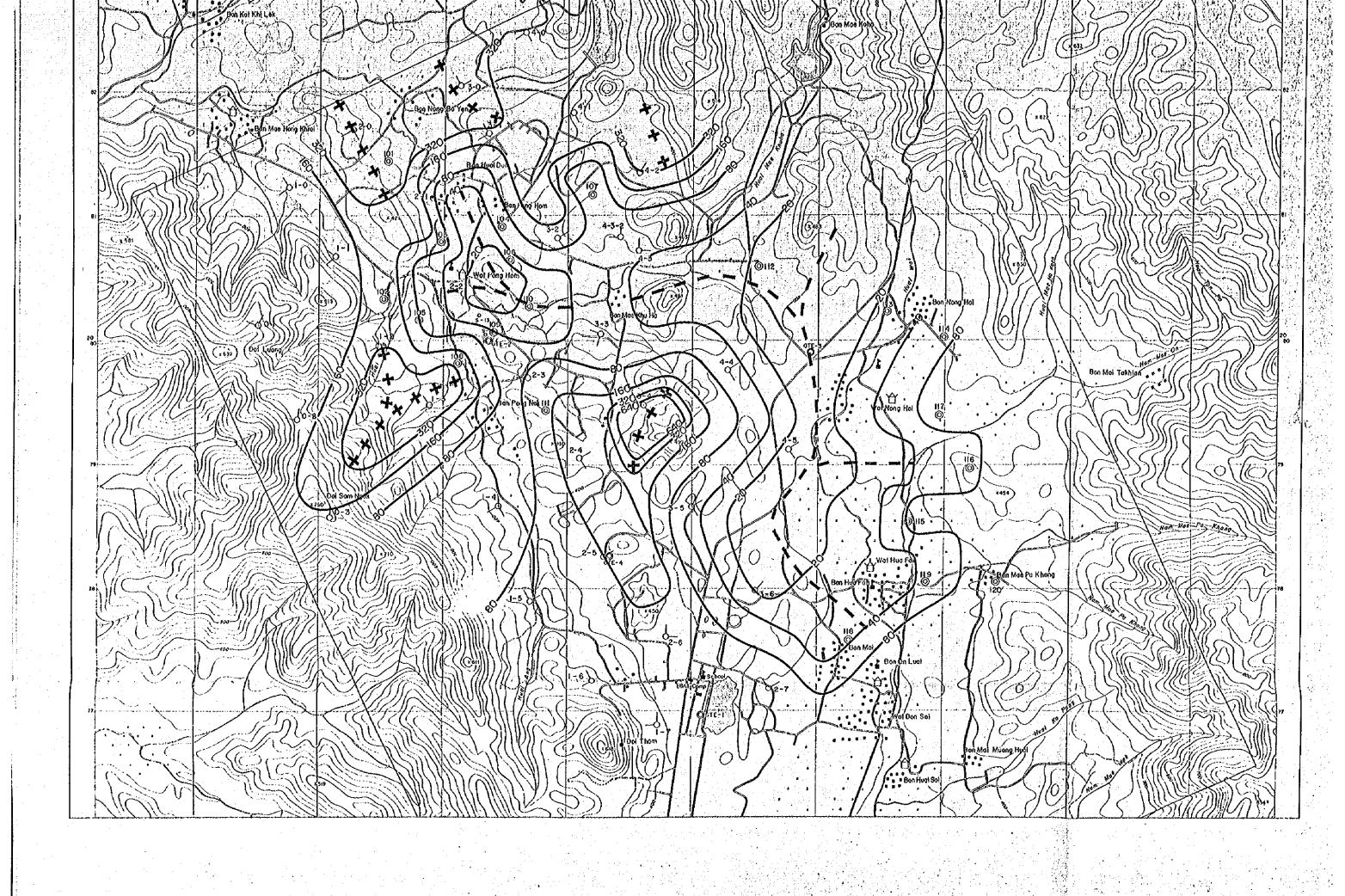


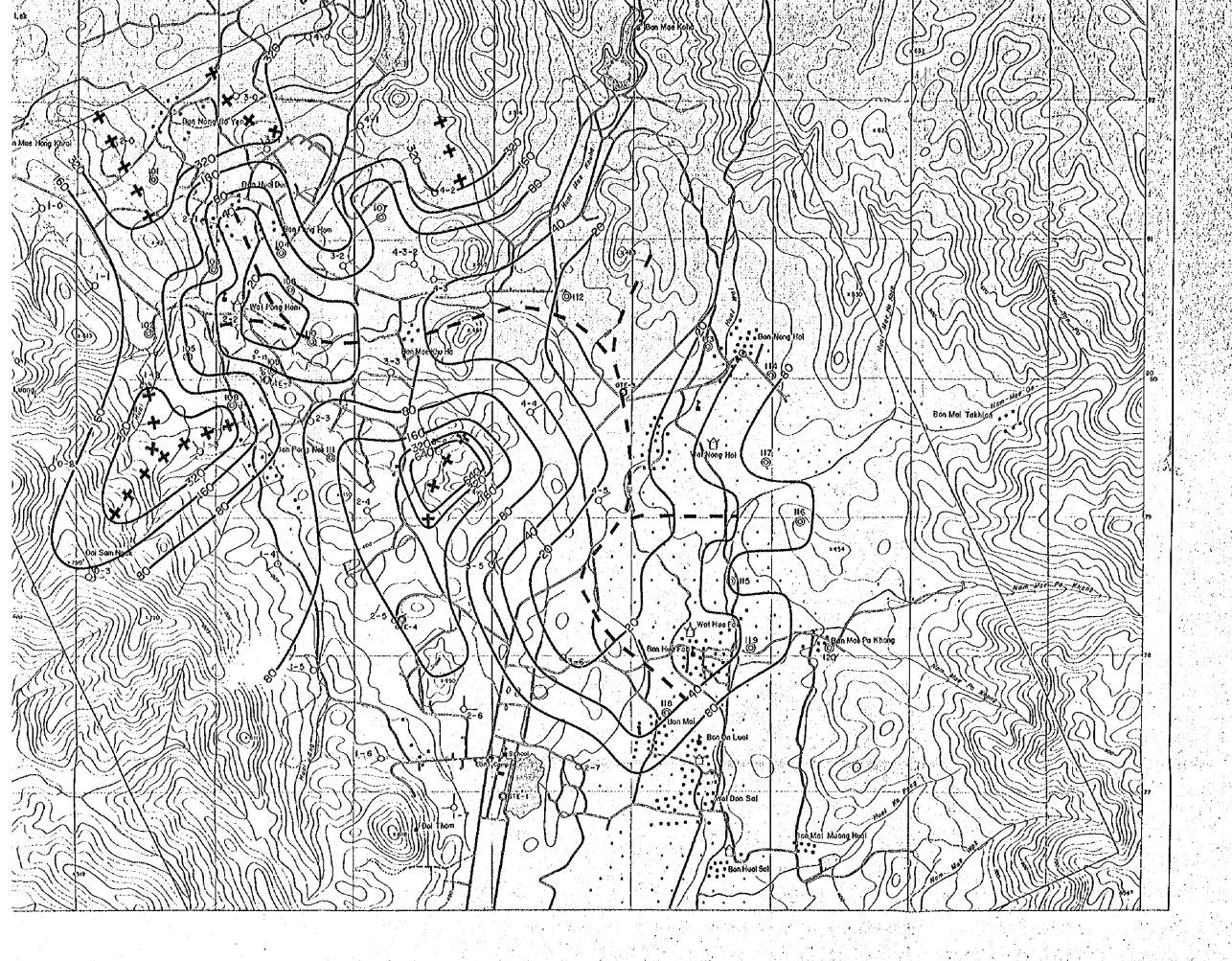
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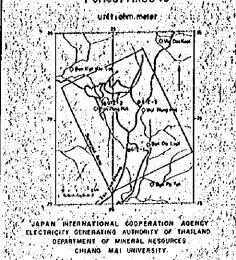
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