Table 5.4.3 CONTENTS FOR SUB-BASINS IN STORAGE FUNCTION EQUATION

Sub-Basin	Cor	istants	Lag-Time	Sub-Basin	Con	stants	Lag-Time
	К	P	(hr)	•	K	P	(hr)
B-A- 1	31.0	0.333	1.1	B-P- 1	50.0	0.333	3.2
B-A- 2	30.8	0.333	0.9	B-P- 2	30.9	0.333	0.1
B-A- 3	49.5	0.333	2.7	B-P- 3	36.6	0.333	1.6
B-A- 4	30.8	0.333	0.9	B-P- 4	44.1	0.333	2.0
B-A- 5	38.4	0.333	0.9	B-P- 5	42.2	0.333	1.3
B-A- 6	38.4	0.333	0.6	B-P- 6	45.3	0.333	2.3
B-A- 7	103.9	0.333	3.9	B-P- 7	59.3	0.333	0.4
B-A- 8	85.7	0.333	7.9	B-P- 8	62.4	0.333	4.6
B-A- 9	105.4	0.333	1.8	B-P- 9	83.6	0.333	0.6
B-A-10	135.5	0.333	7.2	B-P-10	70.0	0.333	2.0
B-A-11	119.1	0.333	4.8	B-P-11	33.0	0.333	0.9
B-A-12	49.2	0.333	4.1	B-P-12	31.5	0.333	0.4
B-A-13	31.9	0.333	0.9	B-P-13	38.9	0.333	0.9
B-A-14	51.7	0.333	4.6	B-P-14	38.3	0.333	0.6
B-A-15	55.9	0.333	1.8	B-P-15	82.2	0.333	2.5
B-A-16	124.5	0.333	5.8	B-P-16	116.9	0.333	2.7
B-A-17	85.2	0.333	4.8	B-P-17	101.1	0.333	2.3
B-A-18	49.0	0.333	3.4	B-P-18	17.6	0.333	0.0
B-A-19	70.3	0.333	1.1	B-P-19	42.0	0.333	1.8
B-A-20	47.2	0.333	3.7	B-P-20	86.4	0.333	3.0
B-A-21	30.6	0.333	1.3	B-P-21	43.4	0.333	8.1
B-A-22	42.4	0.333	2.0	B-P-22	45.9	0.333	0.4
B-A-23	70.9	0.333	1.6	B-P-23	66.4	0.333	1.3
B-A-24	101.4	0.333	0.9	B-P-24	61.6	0.333	5.3
B-A-25	101.4	0.333	3.4	B-P-25	23.5	0.333	0.0
B-A-26	89.1	0.333	3.0	B-P-26	43.8	0.333	1.3
B-A-27	85.2	0.333	4.8	B-P-27	61.1	0.333	2.0
B-A-28	46.3	0.333	3.9	B-P-28	105.8	0.333	2.5
B-A-29	110.0	0.333	4,4	B-P-29	69.9	0.333	0.9
B-A-30	17.8	0.333	0.4	B-P-30	87.7	0.333	1.8
B-A-31	45.7	0.333	3.2	B-P-31	122.3	0.333	3.2
B-A-32 B-A-33	39.1 115.0	0.333 0.333	2.0 5.1	B P-32	89.3 140.0	0.333	3.2 5.1
B-A-34	38.8	0.333	2.3	B-P-33		0.333	
B-A-35	116.6	0.333	5.3	B-P-34 B-P-35	123.3 75.3	0.333 0.333	3.2 3.9
B-A-35	76.3	0.333	5.8	B-P-36	48.3	0.333	0.1
B-A-37	39.3	0.333	1.6	B-P-37	25.7	0.333	0.1
B-A-38	33.7	0.333	1.6	B-P-38	30.9	0.333	0.4
B-A-39	122.5	0.333	5.3	B-P-39	103.1	0.333	4.4
B-A-40	92.3	0.333	2.0	B-P-40	91.7	0.333	1.8
B-A-41	129.5	0.333	3.9	B-P-41	85.2	0.333	1.3
B-A-42	166.3	0.333	9.5	B-P-42	109.8	0.333	2.7
B-A-43	103.2	0.333	1.8	B-P-43	41.7	0.333	1.3
B-A-44	117.9	0.333	2.7	B-P-44	92.9	0.333	3.4
B-A-45	118.4	0.333	4.4	B-P-45	111.6	0.333	3.7
B-A-46	91.7	0.333	1.8	B-P-46	49.4	0.333	4.4
B-A-47	115.4	0.333	2.7	B-P-47	80.4	0.333	2.0
B-A-48	132.8	0.333	4.1	B-P-48	51.0	0.333	3.7
				B-P-49	26.2	0.333	0.0
				B-P-50	74.5	0.333	1.3
				B-P-51	99.4	0.333	3.0
				B-P-52	91.7	0.333	1.8
				B-P-53	128.3	0.333	4.6
			·	B-P-54	128.3	0.333	4.6
				B-P-55	96.9	0.333	4.4
				B-P-56	137.2	0.333	5.6
				B-P-57	135.4	0.333	2.7
				B-P-58	109.3	0.333	1.8
-				B-P-59	173.8	0.333	2.3

Note B-A-1;Sub-baisn in Apure river basin except Portuguesa river basin B-P-1;Sub-basin in Portuguesa river basin

Table 5.4.4 CONSTANTS FOR RIVER CHANNELS IN STORAGE FUNCTION EQUATION

River	Consta	nts	Lag-Time	River	Consta		_ Lag-Tim
Channel	K +	P	(hr)	Channel	К	P	(hr)
C-A-1	33,342	0.366	0.1	C-P-1	36,347	0.392	0.1
C-A-2	174,258	0.373	0.4	C-P-2	255,185	0.674	0.8
C-A-3	77,958	0.386	0.2	C-P-3	95,068	0.386	0.3
C-A-4	73,808	0.403	0.2	C-P-4	154,718	0.755	0.5
C-A-5	959,462	0.793	2.8	C-P-5	302,178	1.036	1.3
C-A-6	764,542	1.036	2.6	C-P-6	194,668	1.026	1.0
C-A-7	1,981,652	1.000	6.3	C-P-7	45,400	0.359	0.1
C-A-8	262,428	0.539	0.6	C-P-8	150,958	0,403	0.4
C-A-9	1,275,534	0.854	4.7	C-P-9	70,821	0.413	0.2
C - A - 10	264,333	0.741	0.9	C - P - 10	454,765	0.698	1.5
C - A - 11	154,960	0.710	0.5	C - P - 11	724,672	1.026	3.6
C - A - 12	112,146	0.342	0.3	C - P - 12	621,147	1.026	3.1
C - A - 13	303,169	0.677	0.9	C - P - 13	179,000	0.373	0.4
C - A - 14	124,251	0.710	0.3	C - P - 14	502,189	1.060	1.7
C - A - 15	355,910	0.919	1.2	C - P - 15	76,099	0.558	0.3
C - A - 16	959,094	1.036	2.9	C - P - 16	309,056	0.980	1.0
C - A - 17	854,355	0.815	3.3	C - P - 17	278,348	1.250	1.3
C - A - 18	468,933	1.036	1.3	C - P - 18	268,435	0.526	0.7
C - A - 19	127,934	0.333	0.3	C - P - 19	100,413	0.403	0.3
C - A - 20	924,435	0.781	3.7	C - P - 20	664,961	1.420	2.7
C - A - 21	842,774	0.815	3.9	C - P - 21	191,500	1.170	0.9
C - A - 22	399,006	1.036	1.0	C - P - 22	164,443	1.130	0.7
C - A - 23	1,094,702	0.863	4,4	C - P - 23	187,766	0.912	0.8
C - A - 24	2,029,336	1.102	5.9	C - P - 24	1,168,008	1.026	6.1
C - A - 25	1,068,566	1.736	7.8	C - P - 25	386,925	1.036	1.8
C - A - 26	3,852,399	1.167	10.1	C-P-26	93,859	0.663	0.3
C - A - 27	668,273	1.011	3.5	C - P - 27	4,537	0.373	0.1
C - A - 28	985,333	1.036	5.2	C - P - 28	774,890	0.755	2.8
	200,333	1.050	V.2	C - P - 29	372,025	0.880	1.8
				C - P - 30	376,661	0.953	1.7
				C - P - 31	764,205	1.483	4.5
				C - P - 32	596,629	0.726	2.1
				C - P - 33	723,555	0.880	3.1
				C - P - 34	489,726	1.512	2.9
				C - P - 35	386,054	0.726	1.3
				C-P-35		0.720	0.1
				C - P - 30 C - P - 37	25,454 295,196	0.755	
				C - P - 37 C - P - 38	293,196 678,139	0.755	1.1 2.4
				C - P - 39	982,145	0.959	4.9
				C - P - 40	1,179,697	0.971	5.9
				C - P - 41	849,161	1.219	5.2
	•			C - P - 42 C - P - 43	544,994 961,709	1.553 1.736	3.1 7.0

Note: C - A - 1; River channel in Apure river basin except Portuguesa river basin

C - P - 1; River channel in Portuguesa river basin

Table 5.4.5 SPECIFIC FLOOD RUNOFF PEAKS OF OUTFLOWS FROM DAM SPILLWAYS IN THE APURE RIVER BASIN

Dam Name	C.A. (km²)	Effective Storage (MCM)	Flood Control Storage (MCM)	Design Flood for Spillway (m³/s)	Maximum Outflow (m³/s)	Dam Status
Apure River Basin	ı					
1. La Honda	1,340	450.0		940 (0.70) <1	940.6	Existing
2. Sauto Domingo	420	2.6	-	3,200	3,250.0	e .
3. Masparo	500	837.0		(7.62) 300	154.5	11
4. Las Cuevas	150	345.0		(0.60) 325	323.3	Proposed
5. Borde SecoLa Vuatosa	3,090	2,097.0	-	(2.17) 775 (0.25)	814.0	tt.
All Existing Dams	2,260	1,289.6				
All Dams	5,500	3,731.6	_			•
Portuguesa River Basin						
6. Cabuy	44	10.6	4	80 (1.82)	165.2	Existing
7. Las Majaguas	100	303.5	41	60 (0.60)	68.5	10
8. Chachincha	940	165.0	•	760 (0.81)	629.0	и
9. La Balsa	2,700	369.0	56	60 (0.02)	68.6	it it
10. Tisnados	1,490	820.8	229	486 (0.33)	448.5	и.
11. Bocono-Tucupito	$2,020$ $\left\{ \begin{array}{l} 440 \\ 1,580 \end{array} \right.$	2,595.0	249	687 180 (1.56) (0.11)	1,028.0	14
12. Yacambu	335	287.0	26	480 (1.43)	639.7	Proposed
13. Las Palmas	4,325	1,750.0	125	170 (0.04)	453.1	19
14. Mesa de Cavaca	1,377	-		550 (0.42)	Marine .	19
15. Vega Honda	730			460 (0.63)	-	•
All Existing Dams	7,554	4,263.9	579	-		
All Dams	14,321	6,300.9	730	-		
All Existing Dams	9,814	5,553.5				
All Dams	19,821	10,032.5				

Note: <1 Value in parenthesis indicates specific discharge (m³/s/km²)

Table 5.4.6 FLOOD INFLOW OF EXISTING DAMS IN VENEZUELA

The second secon	Gross S	torage	Flood	Spillway	Retarding
Dam Name	(x 10 ⁶ m ³)	CA (km²)	Inflow Peak (m³/s)	Capacity (m³/s)	Effect Ratio
Green Canyon	3.20	84.0	1,777	1,478	0.83
			(21.15)	(17.60)	
Beaver Lake Dam	9.50	29.0	183	81	0.44
			(6.31)	(2.79)	
Regadera Dam	4.10	163.0	1,772	700	0.60
			(7.19)	(4.29)	
Tibble Fork Dam	0.28	93.0	137	132	0.96
			(1.47)	(1.42)	
Loud Thund Er Dam	-	18.6	346	183	0.53
	:		(18.60)	(9.84)	

Note : Value in parenthesis indicates specific discharge $(m^3/s/km^2)$

Table 5.4.7 RELATIONSHIP AMONG PROBABLE FLOOD RUNOFF PEAKS

Return	Unit	Probable Flood	Runoff Peaks	•
Period		(1) Rio Guanare	(2) Rio Anus	((1)+(2))/2
Q2.33	m^3/s	760	1,350	~
Q5	m^3/s	1,240	1,760	-
Q10	m^3/s	1,620	2,075	· •
Q25	m ³ /s	2,100	2,475	~
Q50	m ³ /s	2,464	2,762	مد
Q100	m^3/s	2,829	3,057	. *
Q10/Q100	· ·	(0.57)	(0.68)	(0.63)
Q25/Q100	-	(0.74)	(0.81)	(0.78)
Assumed				
Q20/Q100	-			(0.70)

Source:

"Estudio Hydrologico del Rio Guanare En Puenta Tejeray

Rio Anus en Puenta Salvaje - Estado Portuguesa"

Note:

Value in parenthesis indicates ratio between probable flood

runoff peaks

VERIFIED RESULTS OF SPECIFIC FLOOD RUNOFF PEAKS Table 5.4.8

Dam Name	Catchment Area	Calculated Peak Discharge	Specific Discharge	Re	eference
	(kn ²)	(m ³ /s)	(m ³ /s)	$q (C = 6 \sim 30)$	$q(C = 6\sim30) \times 0.7$
Apure River Basin					
1. La Honda	1,340	1,050	0.78	0,70~3.4	$(0.49 \sim 2.38)$
2. Santo Domingo	420	480	1.14	$1.20 \sim 6.0$	$(0.84 \sim 4.20)$
3. Masparo	500	970	1.94	$1.00 \sim 5.8$	$(0.70\sim4.06)$
4. Las Cuevas	150	400	2.67	1.90~9.2	$(1.33\sim6.44)$
5. Borde Seco La Vuatosa	3,090	1,790	0.58	0.45~2.2	(0.32~1.54)
Portuguesa River Basi	n.				
6. Cabuy	44	40	0.68	$0.76 \sim 3.00$	$(0.53 \sim 0.21)$
7. Las Majaguas	100	80	0.80	$0.58 \sim 2.20$	$(0.41 \sim 1.54)$
8. Chachincha	940	130	0.14	$0.20 \sim 0.85$	$(0.14 \sim 0.60)$
9. La Balsa	2,700	460	0.17	$0.12 \sim 0.50$	$(0.08 \sim 0.35)$
10. Tisnados	1,490	300	0.20	$0.17 \sim 0.68$	$(0.12 \sim 0.48)$
11. Bocono-Tucupito	2,020	3,670	1.82	$0.56 \sim 2.80$	$(0.39 \sim 1.96)$
12. Yacambu	335	990	2.96	1.40~6.60	$(0.98 \sim 4.62)$
	4,325	670	0.15	$0.09 \sim 0.35$	$(0.06 \sim 0.25)$
13. Las Palmas			4 4 4 4	$0.70 \sim 3.40$	$(0.49 \sim 2.38)$
13. Las Palmas14. Mesa de Cavaca	1,377	1,630	1.18	0.70 ~ 3.40	$(0.49^{\circ}2.38)$ $(0.18 \sim 0.67)$

Note: C-constant in Creager's equation. Flood runoff calculated for rainfall in 1981.

Table 5.4.9 PROBABLE DAILY MEAN DISCHARGES

(Unit: m^3/s)

Return		Base	Point	
Period	Bruzual (Apure R.)	El Saman (Apure R.)	Camaguan (Portuguesa R.)	San Fernando (Apure R.)
2-Year	3,322	4,060	1,012	5,464 (4,360
5-Year	3,821	4,625	1,182	7,133 (5,980
10-Year	4,151	4,999	1,295	8,238 (6,880
20-Year	4,467	5,358	1,402	9,298 (7,820
30-Year	4,649	5,564	1,465	9,908 (8,300
50-Year	4,876	5,822	1,542	10,670 (8,920
80-Year	5,085	6,059	1,613	11,368 (9,460
100-Year	5,183	6,170	1,647	11,699 (9,760

Note: Figures in parethes are those estimated from water levels.

Data used for calculation are as follows:

- (1) Bruzual 1975 1990
- (2) El Saman 1975 1990
- (3) Camaguan 1975 1990
- (4) San Fernando 1975 1990 (Discharge), 1945 1992 (Water Level)

Table 7.1.1 RIVER SECTIONS AND MAJOR POINTS OF APURE RIVER

-Sections for Non-Uniform Flow Calculation -

- Major Points of Apure River -

No.	Name	Distance (km)	· :	Points	Distance(kn
110.	Namo	Accumulation	Section		`
1	R.MOUTH	0.00	0.00	MANATI R./CON.	52.35
2	EL PERRO	10.47	10.47	CHIREL R./DIV.	141.69
3	EL MAMON	41.20	30.73	BOQUERONES R./DIV.	150.49
4	LA MACIERA	49.27	8.07	PUERTO DE SAN FERNANDO	167.30
5	66.4K	66.37	17.09	APURITO R./DIV.	178.00
6	EL SAUSAL	83.46	17.10	SAN FERNANDO BRIDGE	182.50
7	570-7(INC)	96.66	13.20	PORTUGUESA R./CON.	192.24
8	556-1(INC)	109.74	13.08	GUANAPARO R./CON.	201.81
9	ARICHUŃA	122,90	13.16	YEGUAS R./CON.	207.17
10	534-9(INC)	133.19	10.30	GARZAS R./CON.	220.64
11	CHIREL I	143.34	10.15	GARZAS R./DIV.	266.32
12	EL JOBAL	152.48	9.13	YEGUAS R./DIV.	272.24
13	EL NEGRO	170.59	18.12	GUARITICO R./CON.	370.98
14	SAN FERNANDO	180.47	9.88	PUERTO DE NUTRIAS	442.21
15	LAS GUANOTAS	191.23	10.76	MASPARRO R./CON.	453.78
16	LAS CULATAS	195.72	4.49	PAGUEY R./CON.	469.37
17	454-2(INC)	211.91	16.19	SURIPA R./CON.	523.60
18	CHAMIZAL	230.36	18.45	LA TIGURA R./CON.	546.99
19	418-9(INC)	248.97	18.61	URIBANTE VIEJO R./CON.	660.42
20	400-7(INC)	266,66	17.69	PUERTO SANTOS LUZARDO	663.38
21	382-5(INC)	284,36	17.70	GUASDUALITO	668.81
22	364-3(INC)	302.05	17.69	REMOLINO BRIDGE	680.96
23	APURITO	319.79	17.74		
24	332-2(INC)	333.89	14.10		
25	EL SAMAN	348.12	14.23		
26	312-4(INC)	364.24	16.12		
27	296-7(INC)	380.74	16.50		
28	EL CHINAL	397.07	16.33		
29	258-8(INC)	412.91	15.84		
30	244-9(INC)	427.07	14.16		
31	BRUZUAL	442.14	15.07		
32	BOCA DEL MASPARRO	453.59	11.45		
33	SAN VICENTE	465.41	11.82		
34	188-5(INC)	482.41	17.00		
35	172-2(INC)	497.89	15.48		
36	QUINTERO	514.01	16.12		
37	BOCA DEL SURIPA	525.68	11.67		
38	ARECOSTON DE LA TIGRA	543.82	18.14		
39	114-12(INC)	557.43	13.61		
40	PALMARITO	570.99	13.56		
41	88-19(INC)	582.64	11.65		
42	SAMANAL	593.45	10.81		
43	64-8(INC)	606.91	13.46		
44	50-3(INC)	620.05	13.14		
45	TOTUMITO	633.36	13.31		
46	HATO LA MIEL	645.79	12.43		
47	ORURITA	652.99	7.20		
48	PUERTO SANTOS LUZARDO	663.38	10.38		
49	PUENTE REMOLINO	404.00	17.64		

Table 7.3.1 BANKFUL CHANNEL CAPACITY OF APURE RIVER

No.	Section	Distance	Ground Elevation	Channel Capacity	
		(km)	(m,MSL)	(m3/s)	
		<u></u>	AND THE PERSON NAMED OF PROPERTY.	-	
1	El Perro	10.47	35.37	2400	
2	El Mamon	41.20	36.56	2250	
3	La Maciera	49.27	36.79	2210	
4	El Sausal	83.46	36.53	1750	(1110)
5	Arichuna	122.90	41.21	3180	(2400)
6	Chirel 1	143.34	42.08	3030	
. 7	El Jobal	152.48	43.14	4260	
8	El Negro	170.59	43.00	3440	
9	San Fernando	180.47	45.19	6890	
10	Las Guanotas	191.23	45.33	4210	
11	Las Culatas	195.72	45.52	2990	
12	Chamizal	230.36	49.39	3150	(1380)
13	Apurito	319.79	61.05	3370	
14	El Saman	348.12	64.92	3820	•
15	El Chinal	397.07	73.70	2500	
16	Bruzual	442.14	80.00	3810	
17	Boca del Masparro	453.59	80.86	2270	
18	San Vicente	465.41	83.00	1800	
19	Quintero	514.01	92.90	2160	•
20	Boca del Suripa	525.68	93,45	1030	
21	Arecoston de la Tigra	543.82	96.10	1060	
22	Palmarito	570.99	104.04	1000	
23	Samanal	593.45	108.90	1060	
24	Totumito	633.36	118.40	900	
25	Hato la Miel	645.79	120.60	600	
26	Orurita	652.99	123.06	840	
27	Puerto Santos Luzardo	663.38	125.79	780	
28	Puente Remolino	681.02	130.70	910	

Remarks: Figure in () denotes channel capacity only for the main Apure river in the anabranch reaches.

Table 7.4.1 SIGNIFICANT GRAIN SIZE (1/4)

	MATERIAL SAMPLES	Si				BORE HOLE	SAMPLES					
SAMPLE	(dam)	(mm)	d65 (mm)	d75 (mm)	sq.root (d75/d25)	SAMPLE	(am)	(BB)	d65 (mm)	d75 (mm)	sq.root (d75/d25)	
M- 1	0.022	0.029	0.046	0.07	1.78	p-1-1	1	0.0074	0.0226	0.042		
Z - 2	0.023	0.054	0.084	0.11	2.00	0 c	0.0049	0.02	0.026	0.034	2.63	
0 11 1	0.11		0.70	0.5	. 09.1	7 t 1 L	1 1	0.003	0.00	0.0093	1 +	
(O)	0.029	0.053	0.07	0.086	1.72	. c.	1	: 1 :	1	0.0015	1	
* X- 6	0.19	0.26	0.32	0.37	1.40	P-1-6	t	1		0.0018	١.	
· · · · · · · · · · · · · · · · · · ·	0.028	0.046	0.057	0.065	1.52	p-1-7	1	0.0082	0.085	0.18	1	
50 o	0.014	0.04	0.061	0.082	27.5	3 T 1 C 1		0.028		0.5	1 ;	
* 20 C	0.5	0.28	0.35	4.8		o cilid	000	0.24		0.34	1.41	
M-10	1 12 10 0	0.002	600.0	0.03	0		1000	77.0		2.0	1. 4. 9.	
M-12	0.0016	0.018	0.038	0.059	6.07		0.17	0.27	0.36	0,45	1.63	
M-13	0.041	0.091	0.13	0.016	0.62	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	0.17	0.3		0.53	1.75	
N-14	0.002	0.012	0.031	0.043	4.64	# P-1-14	0.19	0.31		0.52	1.65	
M-15	,	0.0039	0.008	0.015	1	* P-1-15	0.16	0.27		0.44	1.66	
* M-16	0.14	0.3	0.26	0.29	1.44	* P-1-16	0.16	0.25		0.37	1.52	
	•	0.0031	0.0088	0.031	1 1	p-1-17	1	0.028		0.085	1	
SC 00	0.012	0.038	0.12	0.18	3.87	P-1-18	0.04	0.039		0.014	0.59	
の C 1 : E 2 : A	0.0	0.0 0.0	O7 10	ອກ ພ •	4. c	# P-1-19	860.0	0.23	0.0	24.0	2.07	
N-20	0 0 0	0.00	68.0	n t-	2,40	# P-1-20	0 . L9	٠, د د. د		90.0	7.7	
N-22	20.0	30	56	37	20.00	1911 LV +	0	2		•	20.1	
M-23	0.2	0.68		- t-	2.93	AVG.0F"*"	0.150	0.258	0.343	0.416	1.674	
M-24	0.13	0.35	10	23	13.30		ł			11111		
N-25	0.64	ţ~	10 10 10	31	6.96							
M-26	0.014	0.052	0.14	1.2	9.26	P-2-1	0.025	0.049	0.07	0.089	1.89	
M-27	20	30	39	44	1.48	P-2- 2	•	0.0026	0.0061	0.012	1	
M-28	0.27	0.56	0.95	က က	3.60	P-2-3	0.0058	0.041	0.064	0.085		
* M-28A	0.0	0.33	0.45	0.56	1.67	* + + + + + + + + + + + + + + + + + + +	0.045	0.085	0.12	0.15		
4 24 40 5 4 1 2 0 5	2.0	25.0	G -	40.0	1.0-1	C + + +	70.0	۵. د دیر د	0.18	57.0		
N-30	333	0	#I.O	0 10 10 10	13.11	0 10 4 4	0.12	0.21	0.27	200	1,6,1	
M-31	0.26	61	, es) t~	13.45		; I	0.008	0.022	0.03		
M-32	0.65	13	33	£-	8.50	P-2-9	1	0.0074	0.024	0.04	•	
K-23		23	37	20	6.45	P-2-10	· t	0.0025	0.01	0.029	,	
34-34 34-34 31-34	0.43	0.91	61 F	न्द्र ;	3.05	P-2-11	1	0.0053	0.03	0.04	,	
3-30	0.0017	0.014	0.037	0.06	0.0	p-2-12	•	0.002	600.0	0.03	1	
# N-36	0.27	0.47	0.03	0.64	1.54	P-2-13	٠	0.019	0.041	0.06	3	
-01E		7.7.0	0.13	0.34	1.56	4 14 15 15 15 15 15 15 15 15 15 15 15 15 15	1	0.015	0.026	140.0		
AVG.0F"*"	0.175	0.272	0.348	0.410	1.532	01111111111111111111111111111111111111	0.0027	0.045	0.11	0.19	8.39	
1 1 1 1 1	- !			1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		p-2-17	'	0,008	0.02	0.039	1	
						p-2-18	t	0.008	0.025	0.041	•	
						P-2-19	1	0.0068	0.017	0.035	•	
						DZ-2-2	l	200.0	0.0042	0.0095		
						V-2-41	1	0.0019	80000	0,00	ı	

Table 7.4.1 SIGNIFICANT GRAIN SIZE (2/4)

BORE HOLE	SAMPLES	:		!		BORE HOLE S	SAMPLES				
SAMPLE	425 (mm)	920 (mm)	d65 (mm)	d75 (mm)	sq.root (d75/d25)	SAMPLE	d25 (sm)	d50 (mm)	d65 (mm)	d75 (BB)	sq.root (d75/d25)
P-3- 1	•	0.008	0.029	0.045		D 5 1	0.0013	0.025	0.053	0.084	8.04
P-3- 2	0.0047	0.021	0.029	0.037	2.81	p-5- 2	0.022	0.08	0.15	0.22	3,16
5-4.	i	0.0038	0.0076	0.013	ı	P-5-3	0.035	0.089	0.15	0.22	2.51
	1	0.0016	0.0047	0.013	,	* P-5-4	0.19	0.32	0.45	0.55	1.70
	0.18	0.25	0.31	0.36	1.41	P-3- 5		ı	0.002	0.0035	
	0.18	0.25	0.31	0.38	1.45	p-5- 6	ı	0.0078	0.022	0.033	ı
	0.17	0.27	0.37	0.48	1.68	p-5- 7	0.0074	0.039	0.055	0.07	3.08
* p-3- 8	0.18	0.27	0.35	0.4	1.49	8-5-0	0.0089	0.044	0.059	0.07	2,80
P-3- 9	1	0.0065	0.0021	0.03		5 - G-d	0.003	0.034	0.041	0.053	4 20
P-3-10	1	0.025	0.043	0.062	ı	P-5-10	0.0013	0.031	0.04	0.053	30
* P-3-11	0.15	0.21	0.27	0.3	1.43	* p-5-11	0.095	0.28	38	0.10	9 25
* P-3-12	0.075	0.18	0.22	0.27	06.1		0.18	0.35) #7 	9 0) (C
P-3-13	ı	0.0049	0.023	0.032) !	6 6 6 6 6 6 6 6) r	2000		9 6	
P-3-14	•	0.0058	0.023	0.00	,	0	::		000) u	2 0
D-3-15	•	0 0 0	0.0	1 1000	1	• u		? .	9 6	,	2.30
2 4 2	1	0000	0.00	0000	•	0 4 4	2.14	67.0		4.0	1.69
2 5	r	2000	0.010	0.031	ı	31 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	0-11		0.27	0.31	1.68
- C	!	0.0058	0.022	0.035	•	71-5-d					•
2-12	1	0.0041	0.015	0.031		# p-5-18	0.22	0.47	0.57	0.65	1.72
P-3-19	ι	0.085	0.5	0.26	•	# P-5-19	0.12	0.31	0.48	0.59	2.22
P-3-20	0.0043	0.2	0.26	0.32	8,53	* P-5-20	0.16	0.31	0.48	65.0	1 92
* P-3-21	0.16	0.22	0.3	0,35	1.48	* 9-5-21	0.18	0	0.52	0.61	1.84
					•	•) •	;	1		
AVG.0F"*"	0.151	0.234	0.301	0.357	1.547	AVG.OF"*"	0.142	0.306	0.425	0.521	1.932
			 	 		· L L L T L T L T L T L T L T L T L T L		1	1	1	
P-4- 1	0.0029		0.015	0.017	2.42	1 -9-d	ı	0.0049	0.015	0.025	1
* p-4- 2	0.11	0.15	0.24	0.28	1.60	10 - 0 0 - 0		0.0012	0.0047	0.01	ı
P-4- 3	0.03		0.12	0.15	2,24	-9-d		0.0012	0.004	0.0078	,
P-4-4	0.029		0.11	0.14	2.20	7 -9-6	1	0.0092	0.00	0.042	•
# p-4- 5	0.16		0.28	0.3	1.37	19-0	1	0.0073	0.018	0.031	١
# p-4- 6	0.14		0.25	0.29	1.44	9 1910	١	6.0.0	0.021	0.035	1
	0.17		0.28	0.3	1.33	1910	0.002	0.012	210	0.00	4
	0.17		0.28	0.3	.33	. o e o	1,000	0.0		200	
# P-1-9	0.17		0.29	0.33	30			0.00	3	0 0	2 0
	Č.		0 0	1000	2.5	יי ו	700.0	170.0	1.0	20.0	3.04
	0		1 4) L	(1)01-0-4		200	***	0.00	•
* CL110			3 4	* (0.1	P-0-10(2)	970.0	/00-0	60.0	0.12	2.74
	0		Q	90.0	10.7	P-6-11	0.017	0.035	0.14	0.16	1.85
	22.0		9.0	0 7	1.58	* P-6-12	0.18	0.26	0.33	0.39	1. 17
	0.28		9.0	0.7	1.58	* P-6-13	0.12	0.36	0.51	0.61	2.25
	0.23		0.53	0.65	1.68	* P-6-14	0.31	0.64	0.87	1.2	1.97
	0.28		9.0	0.7	1.58	* P-6-15	0.25	0.54	0.69	0.8	1.79
	0.25		0.56	0.66	1.62	91-9-d *	0.21	0.38	0.5	0.59	1.68
* P-1-18	0.37	0.57	0.7	0.8	1.47	* P-6-17	0.19	0.35	0.5	0.59	1.76
	0.31		0.67	0.78	1.59	00 TO		•	,		
	0.31		0.65	0.73	1.53	or - 9 - 0 + +	0.49	ď		0	50.6
	0.36		0.7	8.0	1.49	00-3-0 *	91.0	7	0 69	• •	
				,	?	0 = 0 = 0 = 0 = 0 = 0 = 0 = 0 = 0 = 0 =	2		•	•	, , , , , , , , , , , , , , , , , , ,
AVG.OF"#"	0.220	0.343	0.431	0.495	1.506	17-6-1					
1 1 1 1 1 1 1 1 1	1 1 1 1 1 1 1				1111111	AVG.0F"#"	0.215	0,447	0.615	0.763	1.903
						•			:	;	2

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T
\otimes
SIZE
GRAIN
SIGNIFICANT GRAIN SIZE (3/4)
SIGNE
7.4.1
Table 7.4.

AMPLE (mm) (mm) -7-1 0.085 0.14 -7-2 0.0031 0.018 -7-4 0.003 0.018 -7-5 0.0032 0.008 -7-7 0.009 0.02 -7-12 0.009 0.12 -7-13 0.009 0.12 -7-14 0.009 0.12 -7-15 0.09 0.17 -7-16 0.09 0.17 -7-17 0.09 0.17 -7-18 0.103 0.187 -7-19 0.117 0.29 -7-20 0.18 0.045 -8-2 0.18 0.22 -8-3 0.25 0.27 -8-3 0.27	4655 (mm) 0.19 0.034 0.017 0.015 0.015 0.023 0.023 0.023 0.024 0.034 0.035 0.12 0.13 0.35 0.35	0.00 0.00	4,56 4,50 1,68 3,81 4,56 4,56 3,87 3,20 1,54 1,57 1,53 1,53	X	425 0.043 0.0021 0.055 0.055 0.055 0.054 0.17 0.17 0.16 0.0023 0.0023 0.0088 0.088 0.088	0.08 0.0095 0.0095 0.025 0.021 0.23 0.23 0.23 0.24 0.209 0.0095 0.0095 0.0095 0.0095	465 (EB) 0.016 3.4 0.025 0.035 0.28 0.28 0.29 0.29 0.27 0.27 0.27	0.12 0.12 0.12 0.15 0.15 0.33 0.33 0.33 0.33 0.33 0.34 0.37	475/425) 1.67 3.24 14.14 1.98 3.24 1.98 1
10.0085 11.00.0031 12.00.0031 13.00.0031 14.00.0031 15.00.0031 16.00.0031 17.00.0031 18.00.0031 19.00.0031 10.		0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	1.68 3.81 4.56 1.54 1.57 1.57 1.57	****** * *****************************	0.043 0.0021 0.055 0.028 0.004 0.17 0.18 0.16 0.0023 0.0023 0.0088 0.088 0.088	0.0095 0.0096 0.0086 0.0071 0.023 0.23 0.24 0.220 0.0096 0.0096 0.0096	0.016 0.017 0.0093 0.0093 0.028 0.029 0.029 0.018 0.018 0.018	0.112 0.022 0.151 0.111 0.032 0.32 0.33 0.33 0.33 0.026 0.026 0.026 0.026	1.67 1.67 1.94 1.98 1.98 1.98 1.37 1.37 1.39 1.39 1.39 1.45 1.45 1.45 1.45 1.45 1.45
0.0031 0.0085 0.0085 0.0098 0.0099 0.009 0.017 0.17 0.103 0.018 0.018 0.018 0.018 0.018 0.018 0.018 0.018		2000.00 2000.0	3.81 4.06 3.87 3.28 3.28 3.28 1.57 1.57 1.53	****** * * * * * * * * * * * * * * * *	0.0021 0.055 0.028 0.028 0.017 0.17 0.18 0.19 0.0023 0.0023 0.008 0.088 0.088	0.0096 0.0286 0.023 0.023 0.024 0.024 0.029 0.009 0.009 0.009	0.016 0.012 0.0093 0.0093 0.028 0.028 0.028 0.038 0.018 0.018	0.022 0.111 0.001132 0.232 0.332 0.332 0.033 0.034 0.026 0.026 0.026 0.026 0.026	3.24 11.14 11.98 11.98 11.98 11.93 11.93 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39 11.39
** 0.0085 0.0085 0.009 0.009 0.009 0.017 0.103 0.018 0.018 0.018 0.018 0.018 0.018 0.018 0.018 0.018 0.018 0.018 0.018		0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	4.06 4.56 3.20 3.20 1.54 1.57 1.53 1.53	****** * * * * * * * * * * * * * * * *	0.055 0.028 0.0028 0.001 0.17 0.18 0.16 0.0023 0.0088 0.088 0.088	0.085 0.021 0.022 0.023 0.023 0.024 0.024 0.009 0.009 0.009	8.4 0.0033 0.0033 0.025 0.028 0.023 0.018 0.019	0.000 0.032 0.032 0.032 0.032 0.032 0.032 0.032 0.032 0.032 0.032 0.032 0.032 0.032	41.41 1.944 1.944 1.37 1.37 1.39 1.39 1.39 1.39 1.39 1.39 1.39 1.39
0.0085 0.0013 0.0013 0.056 0.056 0.056 0.056 0.056 0.017 0.17 0.17 0.17 0.118 0.12 0.12 0.13 0.13 0.15 0.15		0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	4.06 4.56 3.87 3.87 1.54 1.57 1.53 1.57	****** * ***** **********************	0.04 0.028 0.034 0.17 0.118 0.18 0.0023 0.088 0.088 0.088 0.088	0.086 0.021 0.023 0.024 0.024 0.009 0.00985 0.00985 0.00985	0.012 0.0035 0.025 0.028 0.023 0.023 0.018 0.018	00.00 00.332 00.332 00.332 00.333 00.033 00.034 00.	1094 1000 1000 1000 1000 1000 1000 1000
0.0085 0.0013 0.0018 0.009 0.09 0.09 0.17 0.17 0.17 0.18 0.018 0.018 0.018 0.018 0.018 0.018 0.018		7440	4.06 4.56 3.87 3.20 1.54 1.70 1.70 1.53 1.53	****** * *****************************	0.028 0.17 0.17 0.18 0.18 0.16 0.0023 0.0022 0.088 0.088 0.088	0.02 0.02 0.02 0.023 0.024 0.024 0.039 0.099 0.0985	0.093 0.035 0.25 0.25 0.23 0.27 0.019 0.15	0.000 0.332 0.332 0.333 0.333 0.033 0.026 0.026 0.026 0.026 0.026	1.98 1.77 1.73 1.35 1.35 1.35 1.35 1.35 1.35 1.35 1.3
0.0085 0.0013 0.0018 0.009 0.009 0.009 0.17 0.17 0.118 0.018 0.018 0.018 0.018 0.018 0.018		7.000000000000000000000000000000000000	4.06 4.56 3.87 3.20 3.20 1.57 1.97 1.53 1.57	****** * * * * * * * * * * * * * * * *	0.004 0.17 0.17 0.18 0.18 0.19 0.0023 0.0023 0.0088 0.088	0.02 0.23 0.23 0.22 0.022 0.030 0.032 0.032	0.035 0.228 0.228 0.033 0.018 0.019 0.334	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	3.54 1.30 1.30 1.30 1.30 1.30 1.30 1.30 1.30
** 0.0018 0.0055 0.009 0.009 0.17 0.112 0.018 0.018 0.018 0.018 0.018 0.018 0.018 0.018 0.018 0.018 0.018		0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	4,56 3,287 3,287 1,54 1,57 1,53 1,57 1,57	****** * * * * * * * * * * * * * * * *	0.17 0.17 0.18 0.19 0.0023 0.0023 0.008 0.088 0.088 0.17	0.23 0.24 0.23 0.24 0.02 0.009 0.009 0.009 0.018	0 0 0 2 2 3 3 3 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	0.22 0.32 0.32 0.33 0.33 0.03 0.02 0.02	1.70 1.37 1.37 1.39 3.36 3.36 1.72 1.72 1.73 1.74 1.75 1.75 1.75 1.75 1.75 1.75 1.75 1.75
0.0013 0.0042 0.0055 0.056 0.059 0.099 0.17 0.17 0.118 0.018 0.018 0.018 0.018 0.018 0.018		00000 00000 000000 000000 000000 000000	4.56 3.20 3.20 - 1.54 1.70 2.11 1.53 1.53	***** * * * * * * * * * * * * * * * *	0.17 0.16 0.18 0.19 0.16 0.0021 0.0088 0.088 0.19	0.23 0.022 0.022 0.009 0.0095 0.112 0.123 0.123 0.123 0.123	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.32 0.32 0.33 0.33 0.03 0.02 0.02 0.02	1.37 1.47 1.45 1.45 1.75 1.75 1.75 1.75 1.75 1.75 1.75 1.7
0.0018 0.0042 0.0055 0.009 0.009 0.017 0.17 0.17 0.018 0.018 0.018 0.018 0.018 0.018 0.018 0.018		744 - 100 -	4.56 3.87 3.20 1.54 1.97 1.70 2.11 1.53 1.53	* * * * * * * * * * * * * * * * * * *	0.118 0.118 0.119 0.0021 0.0022 0.0088 0.088 0.119 0.119	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.33 0.33 0.03 0.03 0.02 0.02 0.02 0.02	1.4.1 1.30 1.30 1.30 1.30 1.30 1.30 1.30 1.
** 0.0042 0.0042 0.0053 0.009 0.017 0.103 0.018 0.018 0.018 0.018 0.018 0.018 0.019 0.018 0.019 0.019		00000 00000000000000000000000000000000	3.80 3.20 1.54 1.67 1.57 1.53 1.63	**** * * * * * * * * * * * * * * * * *	0.15 0.0023 0.0023 0.0023 0.0088 0.088 0.088	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.00 0.033 0.018 0.019 0.134 0.34	0.00 0.00 0.00 0.00 0.00 0.00 0.26 0.26	1.40 1.40 1.40 1.40 1.40 1.40 1.40 1.40
0.0042 0.055 0.056 0.099 0.17 0.112 0.108 0.125 0.125 0.126 0.126 0.126 0.127 0.127 0.128		00.00 00	3.20 1.54 1.67 1.97 1.53 1.53 1.63	** * * * * * * * * * * * * * * * * * *	0.19 0.19 0.0023 0.0021 0.088 0.088 0.19	0.00 0.00 0.00 0.00 0.12 0.12 0.13	0.00 0.0133 0.019 0.015 0.034	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	3.36 3.36 3.36 3.37 3.37 3.37 1.58 1.45 1.45 1.45 1.45 1.45 1.45
0.0042 0.055 0.099 0.099 0.17 0.17 0.018 0.018 0.018 0.018 0.018 0.018 0.018		0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	3.20 1.54 1.67 1.70 2.11 1.53 1.53	* * * * * * * * * * * * * * * * * * *	0.19 0.16 0.0023 0.0021 0.088 0.088 0.17	0.22 0.022 0.0090 0.0085 0.12 0.15	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.37 0.31 0.026 0.029 0.22 0.26 0.4	1.40 1.37 1.38 1.58 1.58 1.45 1.45 1.45 1.45 1.45 1.45 1.45 1.45
*** 0.055 0.068 0.099 0.099 0.177 0.103 0.018 0.018 0.018 0.018 0.018 0.018 0.018 0.018 0.018 0.018 0.018 0.018 0.018		0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	1.54 1.67 1.97 1.70 2.11 1.53 1.57	P P P P P P P P P P P P P P P P P P P	0.16 0.0023 0.0021 0.088 0.088 0.19	0.22 0.022 0.0095 0.0085 0.12 0.12 0.27	0.27 0.018 0.018 0.019 0.15 0.34	0.31 0.026 0.029 0.229 0.25	1,37 1,39 3,36 3,36 1,58 1,45 1,45 1,45 1,45 1,45
0.055 0.068 0.099 0.099 0.17 0.17 0.018 0.018 0.018 0.018 0.016 0.016 0.025 0.025 0.025 0.025 0.030		00000 00000000000000000000000000000000	1,54 1,67 1,97 1,70 2,11 1,53 1,63	* * * * * * * * * * * * * * * * * * *	0.0023 0.0021 0.0028 0.088 0.199 0.17	0.022 0.0095 0.0085 0.12 0.16	0.018 0.018 0.13 0.34 0.34	0.31 0.026 0.029 0.22 0.25 0.25	23.36 23.36 24.72 24.45 24.63 25.63
0.09 0.09 0.09 0.09 0.17 0.17 0.018 0.018 0.018 0.018 0.016 0.12 0.12 0.13		00000 00 11.0000 00 11.00000000000000000	1.67 1.97 2.11 1.53 1.53 1.63	2 + 1 + 1 + 2 + 3 + 3 + 3 + 3 + 3 + 3 + 3 + 3 + 3	0.16 0.0023 0.0021 0.088 0.088 0.19 0.115	0.022 0.0095 0.0085 0.12 0.16	0.27 0.018 0.019 0.15 0.34 0.34	0.31 0.026 0.029 0.22 0.26 0.4	1,39
*, 0.099 0.099 0.099 0.17 0.17 0.018 0.018 0.018 0.018 0.018 0.018 0.018 0.018		00000 000 0000000000000000000000000000	1,67 1,70 2,11 1,53 1,57 1,63	+ + + + + + + + + + + + + + + + + + +	0.0023 0.0021 0.088 0.088 0.19 0.15	0.009 0.0095 0.12 0.13 0.27	0.018 0.018 0.15 0.34 0.34	0.026 0.029 0.22 0.26 0.26	1111133
0.09 0.099 0.17 0.17 0.18 0.018 0.25 0.12 0.12 0.12 0.13 0.12 0.13		00.00 0.26 0.44 0.44 1.44 1.54	1.97 1.70 2.11 1.53 1.63	* * * * * * * * * * * * * * * * * * *	0.0021 0.0021 0.088 0.088 0.19	0.0095 0.0085 0.12 0.18 0.27	0.018 0.019 0.15 0.34 0.34	0.026 0.029 0.22 0.26 0.44	11.72
*** 0.09 0.099 0.17 0.17 0.018 0.018 0.018 0.018 0.018 0.018 0.018 0.018 0.018 0.018 0.018 0.018		0.26 0.44 0.42 0.45	1.70 2.11 1.53 1.53 1.57	* * * * * * * * * * * * * * * * * * *	0.0021 0.08 0.088 0.19 0.17	0.0085	0.019 0.15 0.34 0.34	0.029 0.2 0.26 0.4	11.172
*** 0.099 0.17 0.17 0.103 0.018 0.018 0.018 0.018 0.018 0.018 0.018 0.018 0.018 0.018 0.018 0.018	į	0.44	2:11 1:53 1:57 1:63	* * * * * * * * * * * * * * * * * * *	0.08 0.088 0.19 0.17 0.15	00000	0.15 0.34 0.34	0.26	1.58
** 0.103 0.018 0.018 0.018 0.018 0.12 0.13 0.15 0.15		0.42	1.53 1.53 1.63	71.00 C C C C C C C C C C C C C C C C C C	0.088 0.088 0.19 0.17	00.27	0.00	0.26	11111
*" 0.17 0.17 0.018 0.018 0.018 0.12 0.13 0.16 0.16		0.42	1.53 1.57 1.63	;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;	0.088 0.19 0.17 0.15	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 2 4 6 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	0.25	1.45
*" 0.17 0.018 0.018 0.018 0.25 0.12 0.13 0.16 0.16		0.42	1.57	* P-9-19 * P-9-20 * P-9-21 * P-9-21	0.19 0.17 0.15	0.25	0,0 6,0 8,0 8,0	0.4	1,45 1,48 1,63
** 0.17 0.018 0.018 0.018 0.12 0.12 0.13 0.16 0.16	0.35	0.42	1.57 1.63	* P-9-20 * P-9-21	$0.17 \\ 0.15$	0.25	0°	0.37	1.48
** 0.17 0.018 0.018 0.018 0.12 0.13 0.15 0.15	0.36	0.45	1,63	10-6-4 + 10-6-4 + +	0.15		c		1,63
** 0.103 0.018 0.25 0.12 0.13 0.16 0.16 0.16 0.12 0.12 0.12 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16	0.241		<u>.</u>		;	C 7 :0	50.0	0.4	
0.103 0.018 0.018 0.12 0.12 0.16 0.16	0.241			*******		,	:		
0.018 0.018 0.25 0.12 0.13 0.16 0.2		0.297	1.711	AVG.OF *	0.144	0.217	0.269	0.317	1.488
0.00 0.00 0.00 0.12 0.16 0.16		90	6	c c		0	9,00	6	;
0.018 0.12 0.13 0.16 0.16 0.2		000	1001	7 = 01 = 3	1	0.0010	00000	1000	
0.25 0.12 0.13 0.16 0.2 0.2		0.069	1.96	P-10- 2	1	0.0019	0,0038	0.0065	
0.12 0.13 0.16 0.22 0.22		0.69	1.66	P-10- 3	0.004	0.024	0.037	0.047	
0.13 0.16 0.16 0.2		0.29	1.55	P-10- 4	0.0017	0.021	0.037	0.049	
0.16 0.16 0.2 0.2	0.26	0.3	1.52	D=10+ 5	1	0.0046	600.0	0.015	1
0.16			1 30	27.0		2000	0.10	0.023	
0.00				P-10+ 0	•	2100.0		3 6	
0 O		5.0	1.39	P-10-7	•	0.027	0.043	740.0	ŀ
0.2		0.57	1.69	P-10-8	1	0.013	0.037	0.055	
		٠. د		P-10- 9	0.0029	0.021	0.045	0.072	
6.0		0.55	1,67	01-01-0	0.027	o C	c	0.10	
				0710111	0000	0 0) c	
77.0		0	10.4	11-01-4	0.0029	0.020	6.0.0	4.0	
2.0		·	- 	P-10-12	0.0019	0.021	0.038	0.049	
				P-10-13	0.0045	0.029	0.051	0.072	4.00
6		C 44	1.50	0-10-14	0.47	-	91.0	0.05	
n c				+1-01-4) t) (
7.0		* >	7	* P-10-13	0 17	0.22	0.27		
81. O		0.51	1.60	* P-10-16	0.18	0.54	0.29	0.33	
0.2		0.45	1.50	* D110113	0 17	0.23	0.28	0.32	
		0.00	1	01-01-2		0	000	0 39	
		9000		0110110 4		0	0 0	1 6	
0.18		0.32	1.33	* P-10-19	0.18	0.23	0.23	0.32	
0.18		0.32	1.33	P-10-20					
-21 0.2 0.3	0.37	0.47	1.53	* 2-10-21	0.12	0.21	0.27	0.33	1.61
AVG.OF"*" 0.186 0.263	0.354	0.418	1.502	"*"#O. DVA	0.163	0.226	0.278	0,317	1.395

SIGNIFICANT GRAIN SIZE (4/4)	BORE HOLE SAMPLES
Table 7.4.1	

BORE HOLE	HOLE SAMPLES	and and	able 7.4.1		TINIO	PICIALITY OF THE BONE HOLE SAMPLES	BORE HOLE SAMPLES	AMPLES				
SAMPLE	d25 (mm)	d50 (mm)	d65 (mm)	475 (mm)	sq.root (d75/d25)	KVS	SAMPLE	d25 (mm)	d50 (mm)	d65 (mm)	යිට්ට (ama)	sq.root (d75/d25)
P-11-1	0.004	0.016	0.026	0.037	3.04	p-13-	3- 1	0.002	0.016	0.03	0.042	4.58
P-111-2	0.005	0.02	0,029	0.0	8 8 8 8	P-1	3- 2	0.007	0.037	0.089	0.11	3.96
	0.0029	0.015	0.026	0.037	3.57	p-13-	ري دي دي	0.0025	0.012	0.023	0.037	3,00
1	1	0.0015	0.011	0.03	ı	l-d		0.019	0.045	0.058	0.068	1.89
0 1 1 1 0	•	0.0022	0.015	0.033	ı	[] ;	P-13- 5	0.0019	0.013	0.03	0.043	7.57
	1 4 5	0.010	40.0 60.0	0.00	1 6	1-2	ر ا ا	0.0000	0.036	0.000		
- 0 I I I I	20.0	8 00 00 00 00 00 00 00 00 00 00 00 00 00	5 C	27.0	7 .	1, 6	- c	0.0043	0.034	0.00	0.000	3.80
0 11 1 d	0.00	0.000	0 to		000	T		000	0.0046	#TO:0	3 6	1 11
P-11-10	0.0013	0.019	0 0	0.080	7.53			2000	# F C C	0.00	0.0	. 60
P-11-11	0.075	1000	0.00 0.10	0000	10 10 10 10 10 10 10 10 10 10 10 10 10 1	*	0410110	16.0	200	000	36.0	- C
5-11-12	0.035	0.07	0.082	0.12	0 1/1 - 00 	. A		0.16	800	20.28	3 6	000
P-11-13))	0.022	0.045	0.064	> t	1 2 N		0.13	? ? ?	100	0.99	1.65
P-11-14	1	0.036	0.065	0.32	ı	*			200	200	200	1.00
* p-11-15	0.16	0.42	0.62	18.0	20.0	*		0.15	0.21	0.26	0	1.4.
P-11-16	0,003	0-049	60.0	2.13	7.0.7	*		0.16	0 0	0.20	0.35	60
P-11-17						. 5.	p-13-17					•
	0.18	0.27	0.35	0.4	1.49	*	P-13-18	0.05	0.17	0.22	0.27	2.32
* P-11-19	0.16	0.27	0.35	0	1.58	*	P-13-19	0.05	0 17	0.26	0.36	2.68
	0.15	0.28	0.41	0.51	1.84	1-d	3-20					
P-11-21						-d *	3-21	0.055	0.13	0.18	0.25	2.13
AVG.OF"*"	0.162	0.304	0.420	0.507	1.791	AVG	AVG.0F"*"	0.100	0.195	0.252	0.307	1.797
		; 1 1 1 1 1 1 1	1 1 1 1 1 1 1	; ; ; ; ; ;		AAV	AVERAGE	0.149	0.260	0.344	0.414	1.684
P-12- 1	,	0.0036	0.0098	0.022	1			1 1 1 1 1 1				* * * *
P-12-2	t	0.0018	0.0046	0.01	ı							
P-12- 3	1	0.0012	0.004	0.009	1							
P-12- 4	ı	0.0012	0.0098	0.032								
P-12- 5	ı	ı	0.0058	0.023	1							
P-12- 6	0.0026	0.024	0.034	0.046								
P-12- 7	•	0.0038	0.0091	0.018	i							
8 -21-4	3	0.0036	0.0075	0.012	1							
	1 6 6	0.005	0.010	0.023	• . •							
	2000	7.7		⊃ t								
4 5114 4	`	* 6 O	20.0	· .	27.03							
		200	a (
		0 0	2		n :							
* P=12=14 * P=12=15	- L	97.0	. c. c.	÷ ;;	7 - O							
	71.0	20000	· c	200	77.							
P-12-17	0.0014	0.021	0.028	0.037	5.14							
P-12-18	0.0029	0.035	0.038	0.06	4.55							
P-12-19	ì	0.012	0.022	0.028	ŧ							
* P-12-20	0.076	0.17	0.23	0.28	1.92							
* P-12-21	0.045	0.16	0.21	0,26	2.40							
14 12 ON	6	5	0	•	6							
10.00 F	01110	. 167.0	0.000	0.455	1 1 2 2 2 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1							

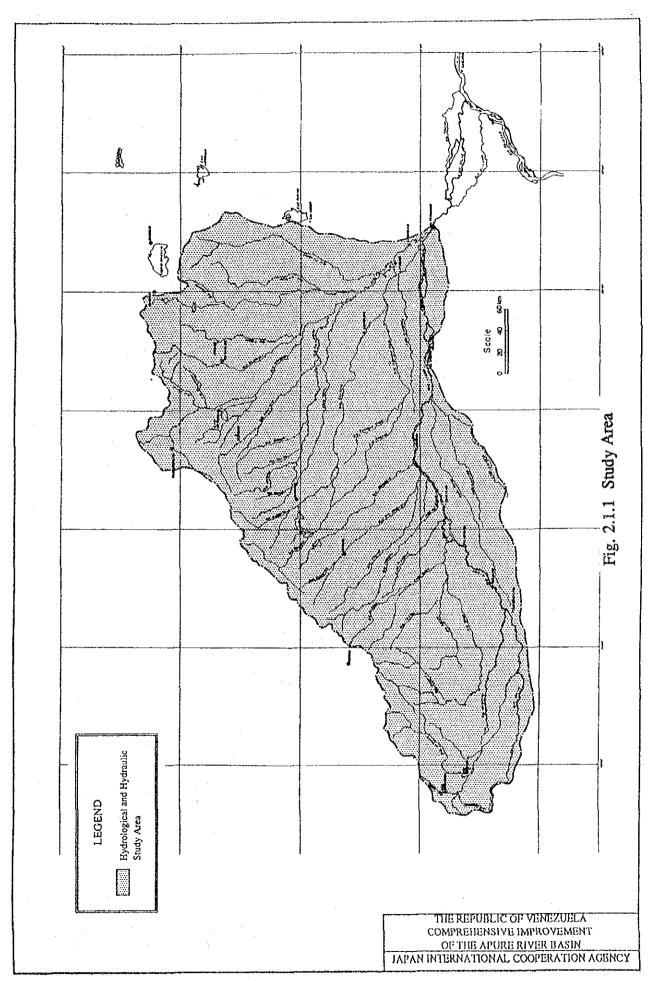
Table 7.4.2 BED MATERIAL FOR SEDIMENT CALCULATION

No.	Site	d25 (mm)	d50 (mm)	d65 (mm)	d75 (mm)	√d75/d25
1	Puente Remolino	0,150	0.258	0.343	0.416	1.665
2	Totumito	0.082	0.147	0.195	0.236	1.696
3	Palmarito	0.151	0.234	0.301	0.357	1.538
	Average	0.128	0.213	0.280	0.336	1.623
4	Suripa	0.220	0.343	0.431	0.495	1.500
5	San Vicente	0.142	0.306	0.425	0.521	1,915
6	Bruzual	0.215	0.447	0.615	0.763	1.884
	Average	0.192	0.365	0.490	0.593	1.756
7	El Saman	0.103	0.187	0.241	0.297	1.698
8	Apurito	0.186	0.263	0.354	0.418	1.499
9	San Fernando	0.144	0.217	0.269	0.317	1.484
10	Arichuna	0.163	0.226	0.278	0.317	1.395
	Average	0.149	0.223	0.286	0.337	1.504
	Composition Rate	37.5%	20.0%	12.5%	30.0 g	

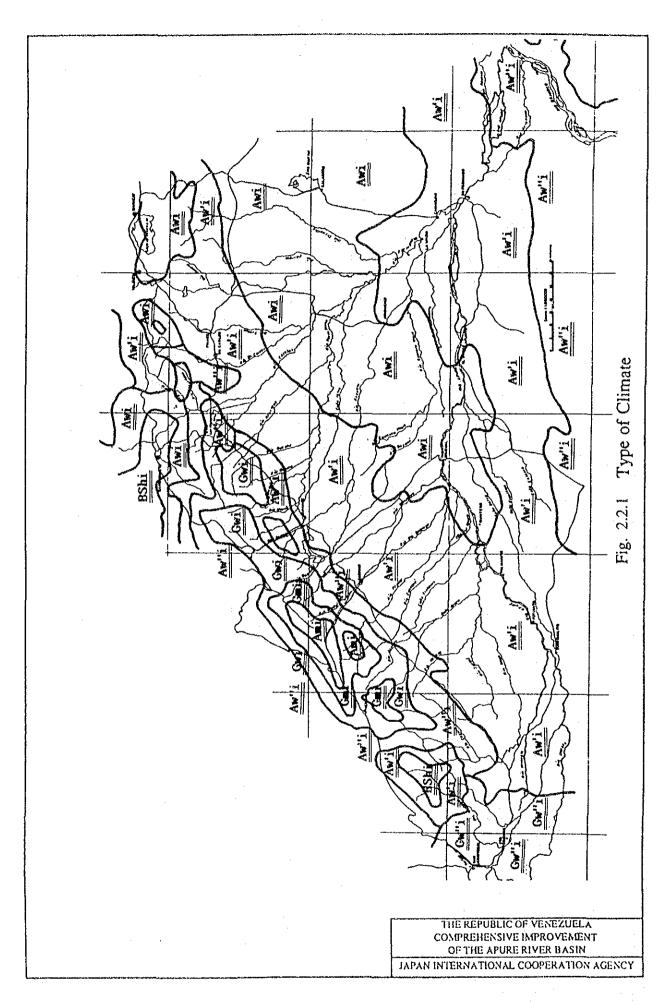
Table 7.4.3 CHANNEL CHARACTERISTICS FOR SEDIMENT FLOW

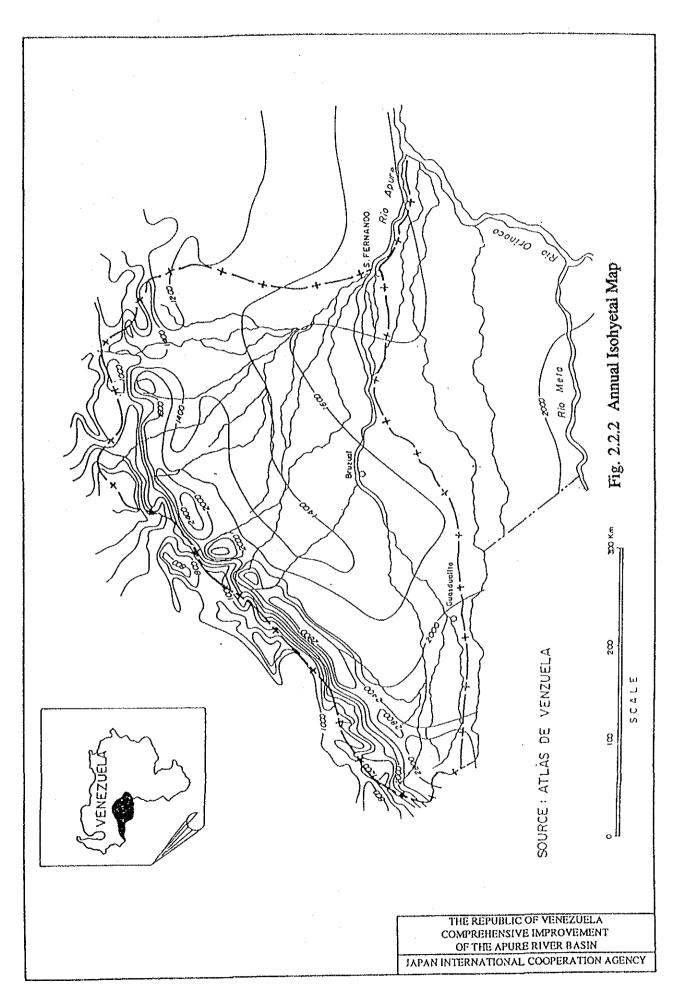
Site		Ie	B (m)	(m)	u* (cm/s)	tau*	u*/wo	h/d	B/h	Bì /h
Guasdualito	1/	3500	258	3.58	10.01	2.07	2,40	1.19E+04	72.07	14.09
Bruzual	1/	5000			9.97	2.05	2.39	1.69E+04	81.85	14.90
Camaguan	1/	16700	139	7.49	6.63	0.91	1.59	2.50E+04	18.56	2.65
San Feranando	1/	8500	577	7.39	9.23	1.76	2.21	2.46E+04	78.08	12.78
						u*c(cı	n/s)	wo(cm/s)		d(cm)
						1.59		4.17		0.03

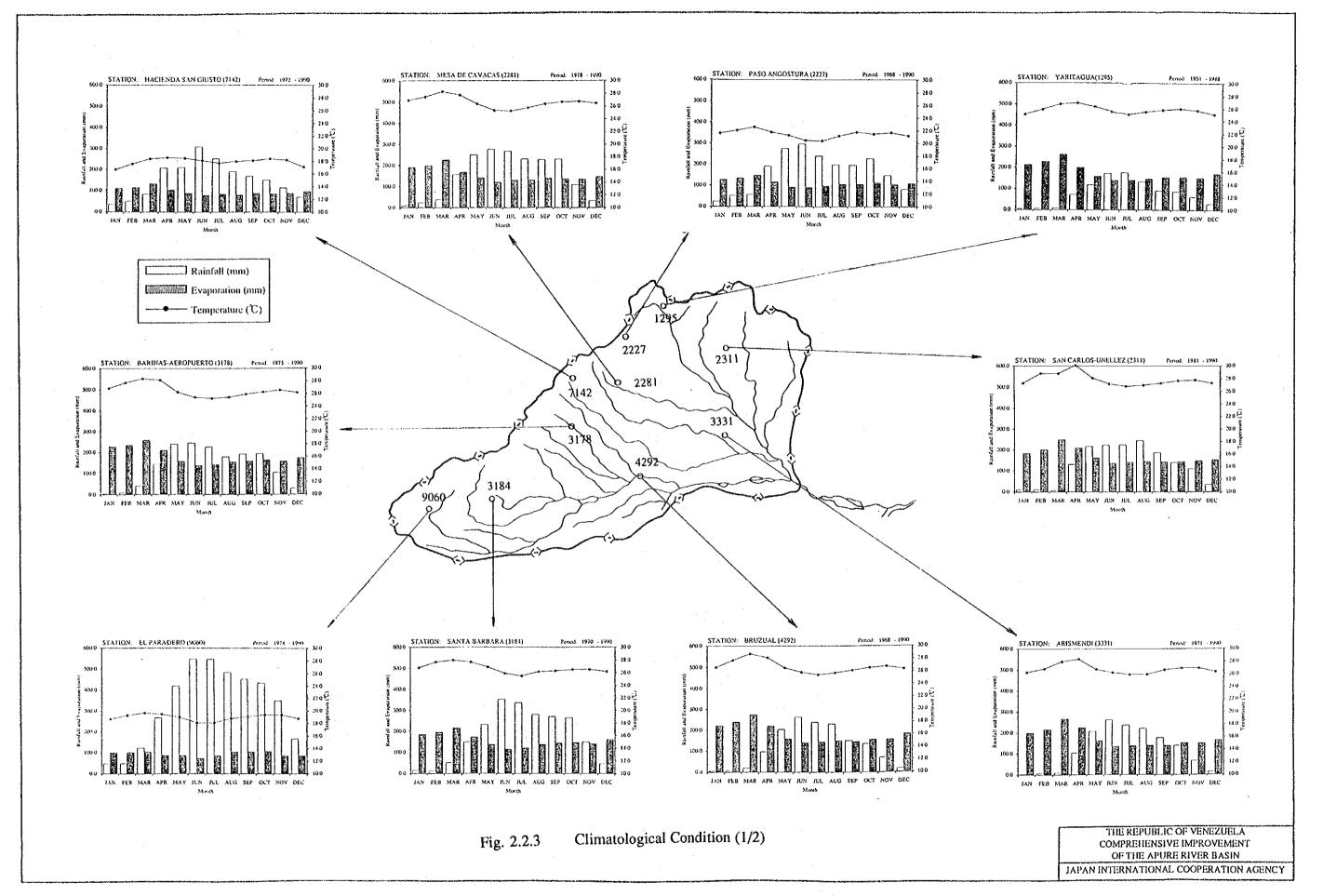
FIGURES

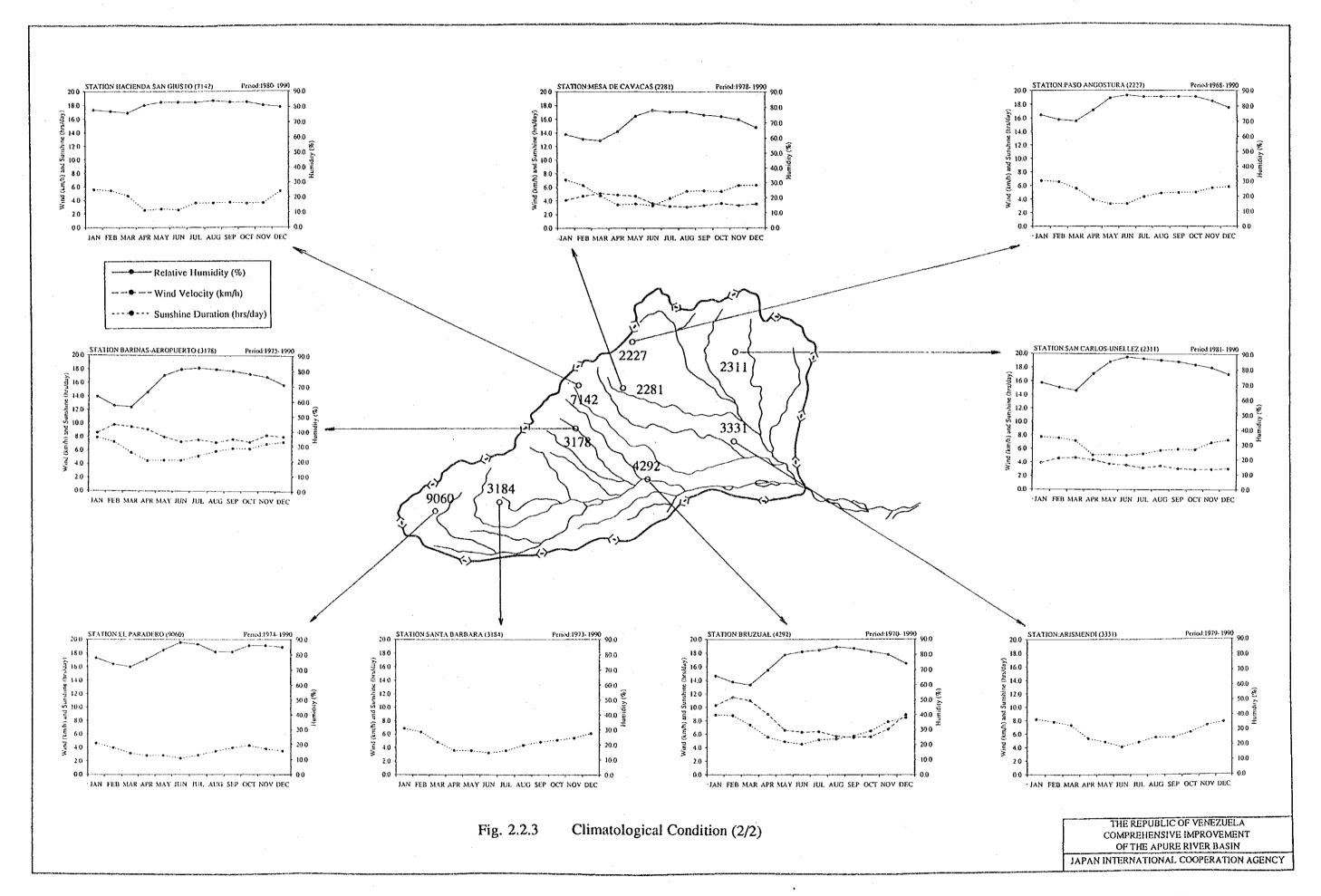


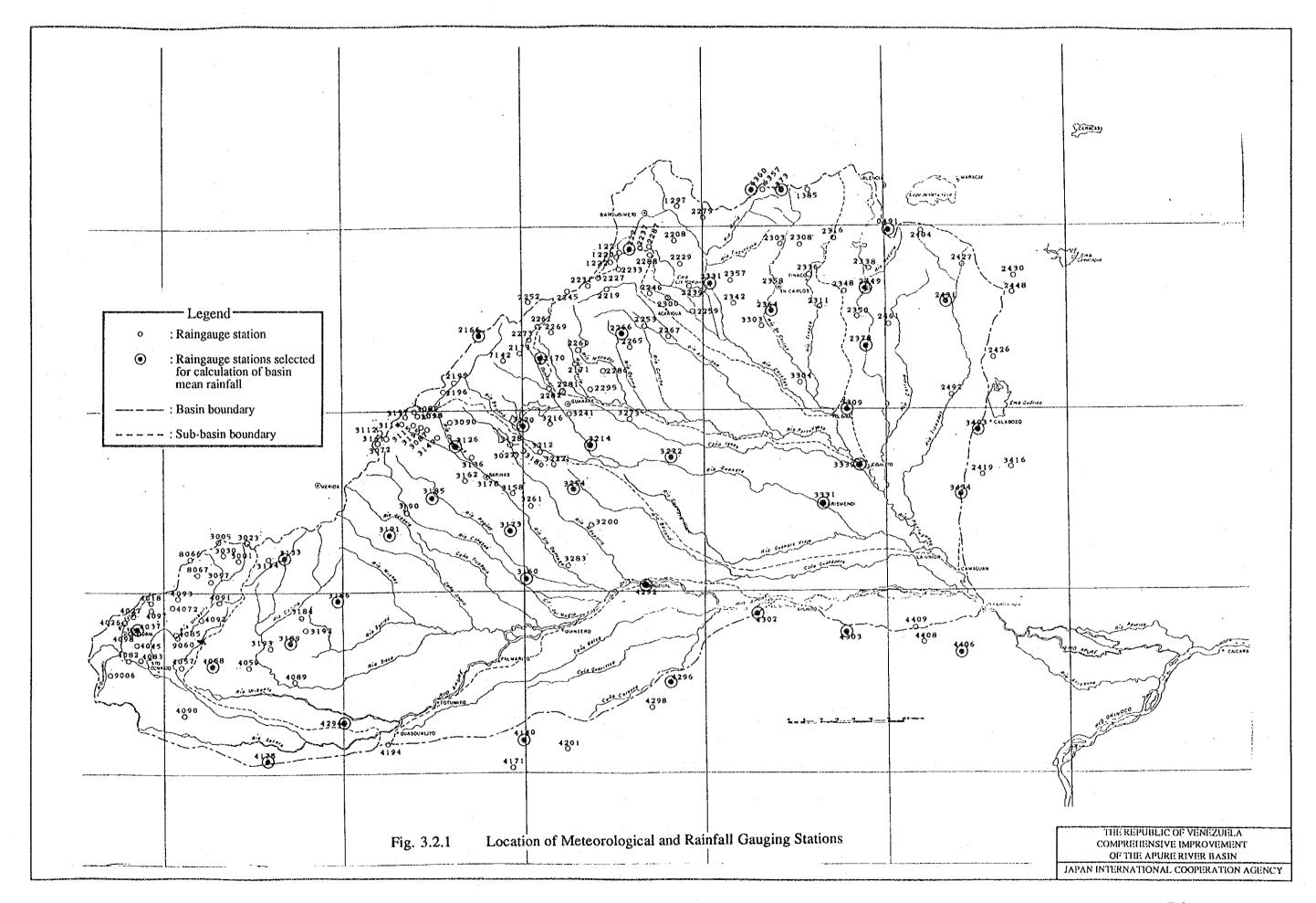
DF.1

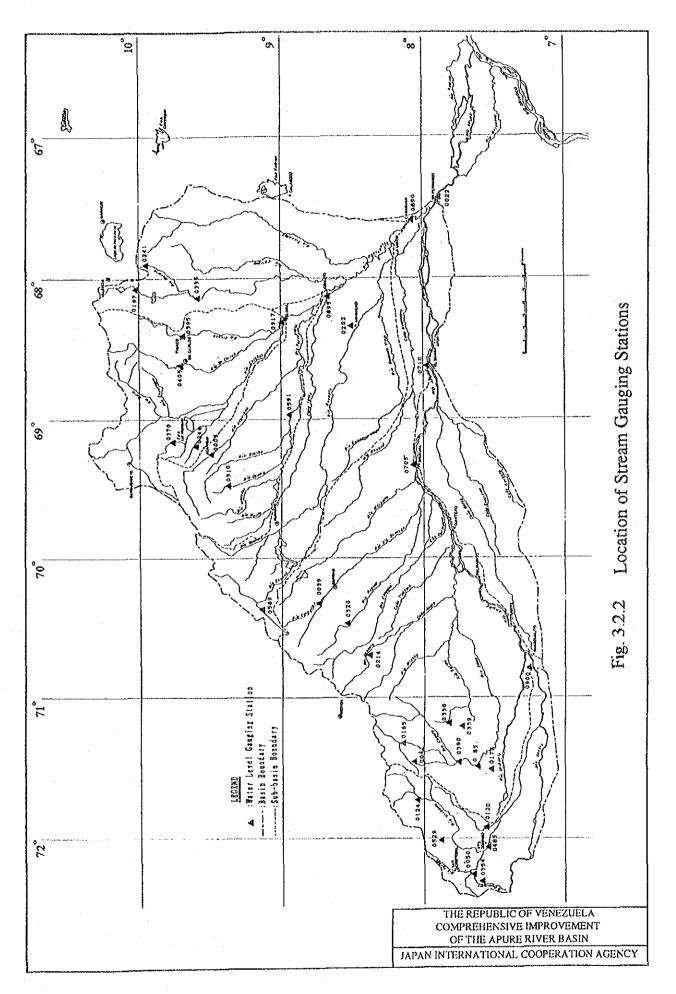


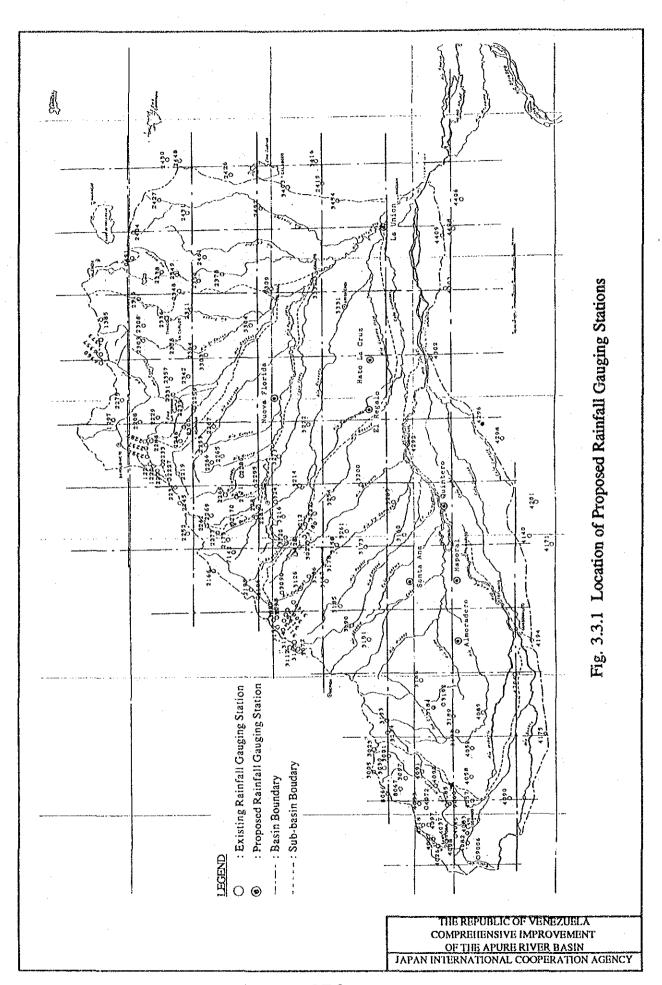


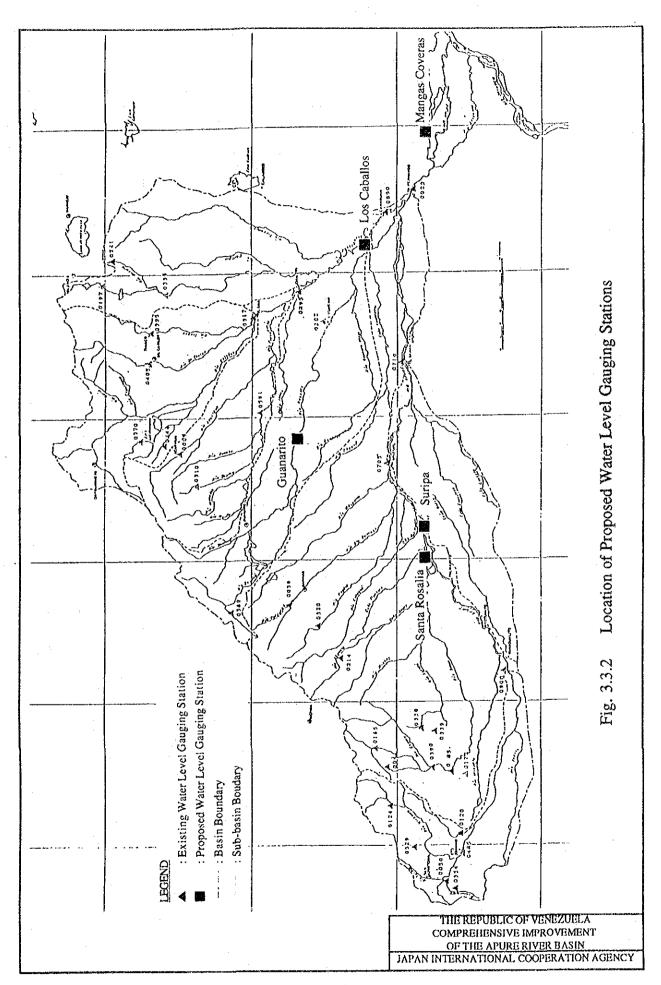


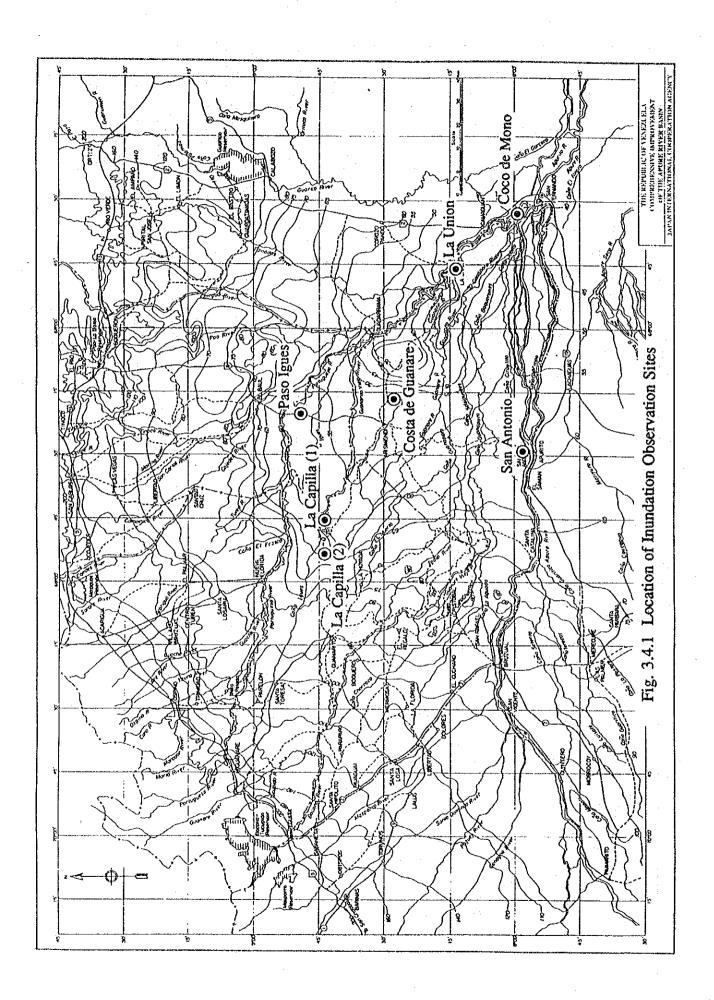


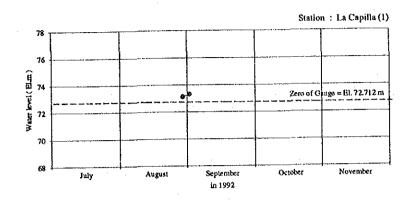


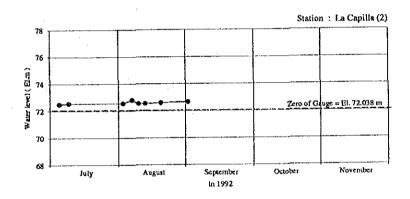












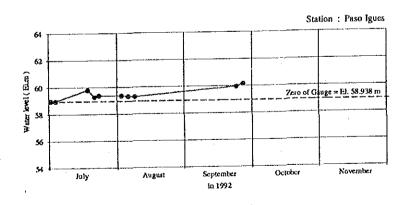
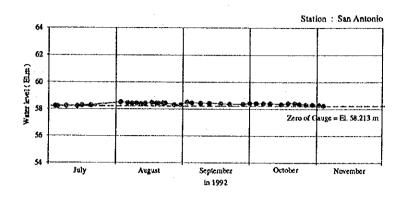
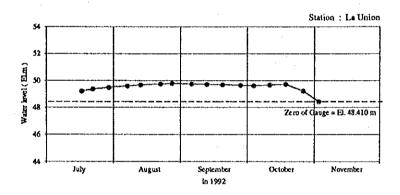


Fig. 3.4.2 Result of Inundation Observation (1/2)

THE REPUBLIC OF VENEZUELA
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OF THE APURE RIVER BASIN
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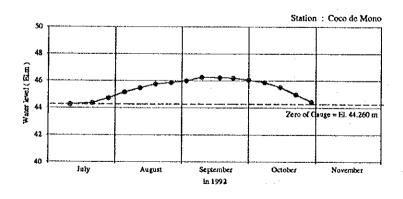
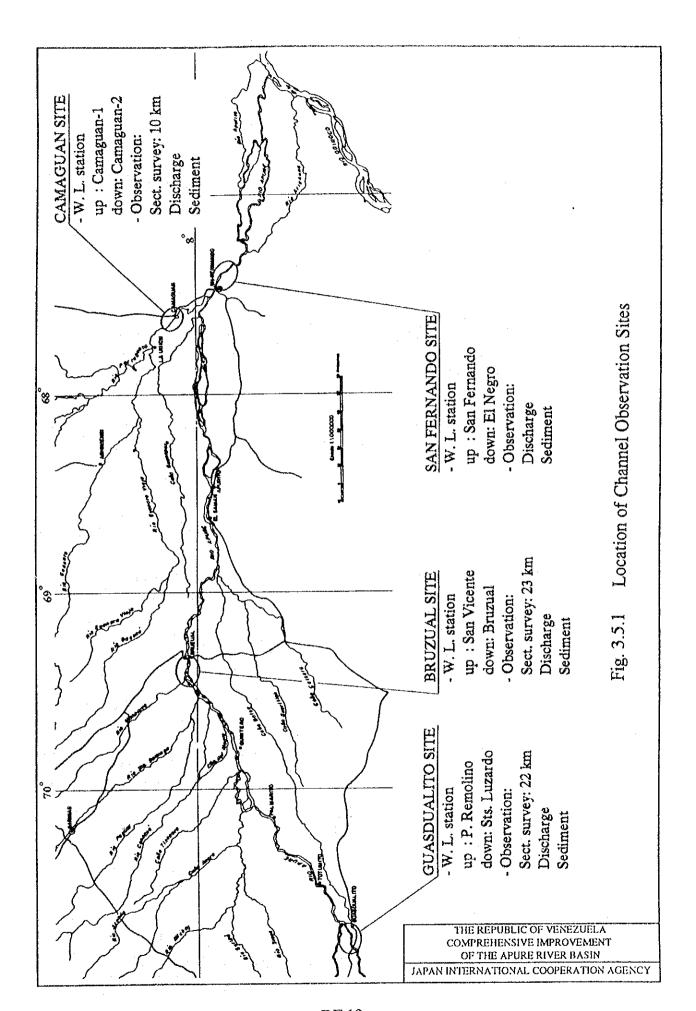
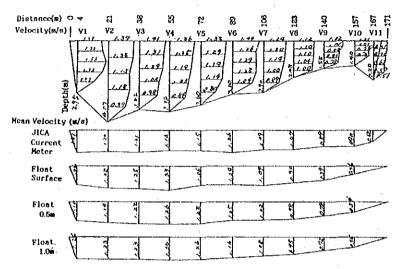


Fig. 3.4.2 Result of Inundation Observation (2/2)

THE REPUBLIC OF VENEZUELA
COMPREHENSIVE IMPROVEMENT
OF THE APURE RIVER BASIN
JAPAN INTERNATIONAL COOPERATION AGENCY







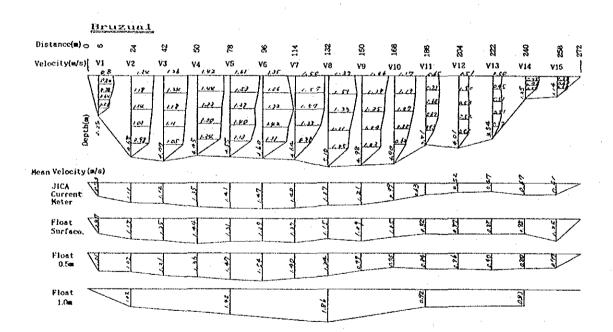
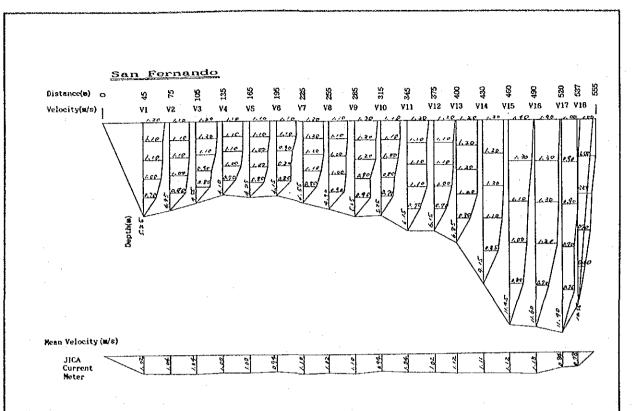


Fig. 3.5.2 Result of Discharge Measurement (1/2)

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COMPREHENSIVE IMPROVEMENT
OF THE APURE RIVER BASIN

JAPAN INTERNATIONAL COOPERATION AGENCY



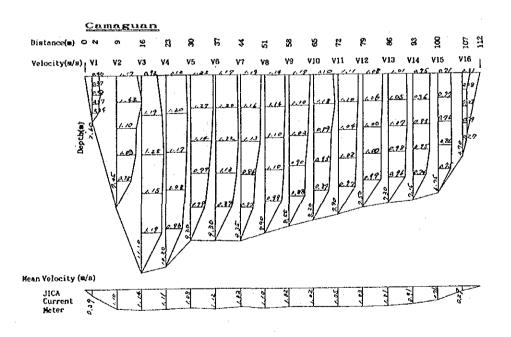
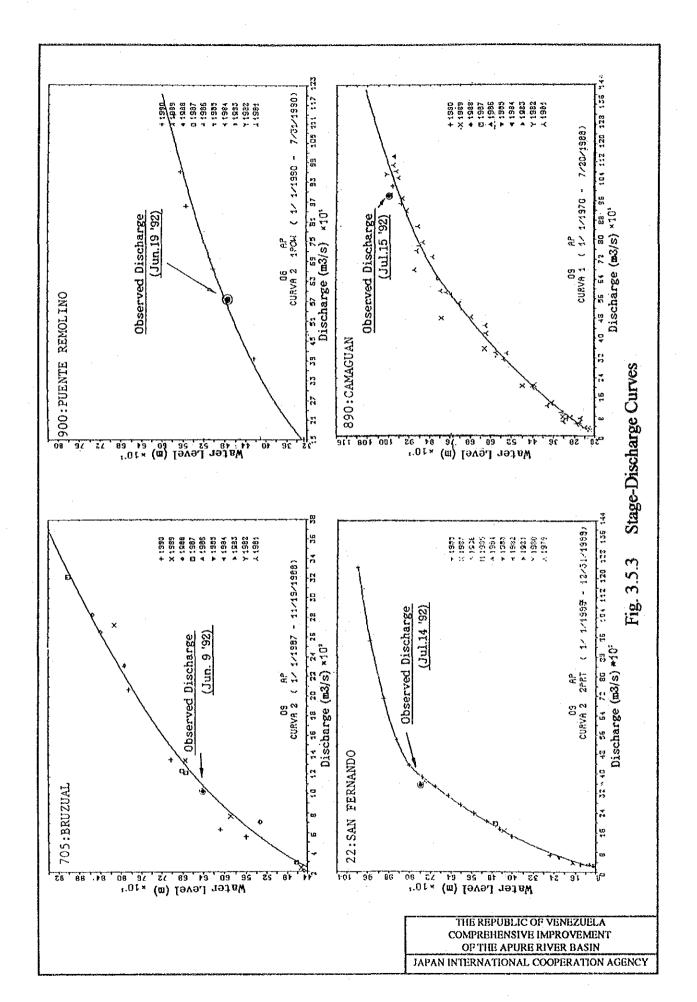
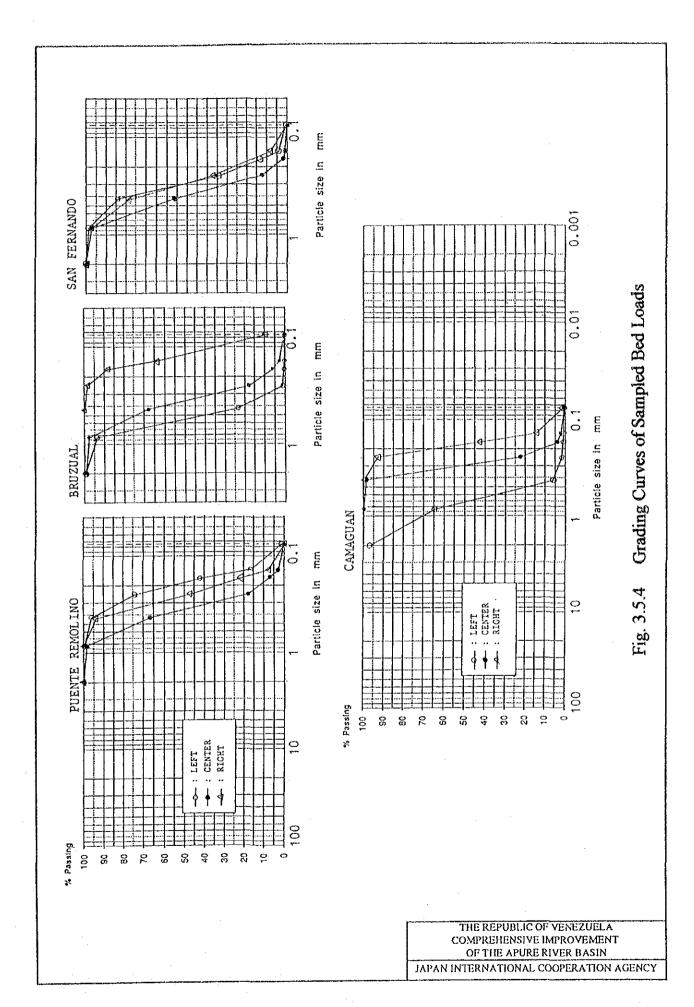
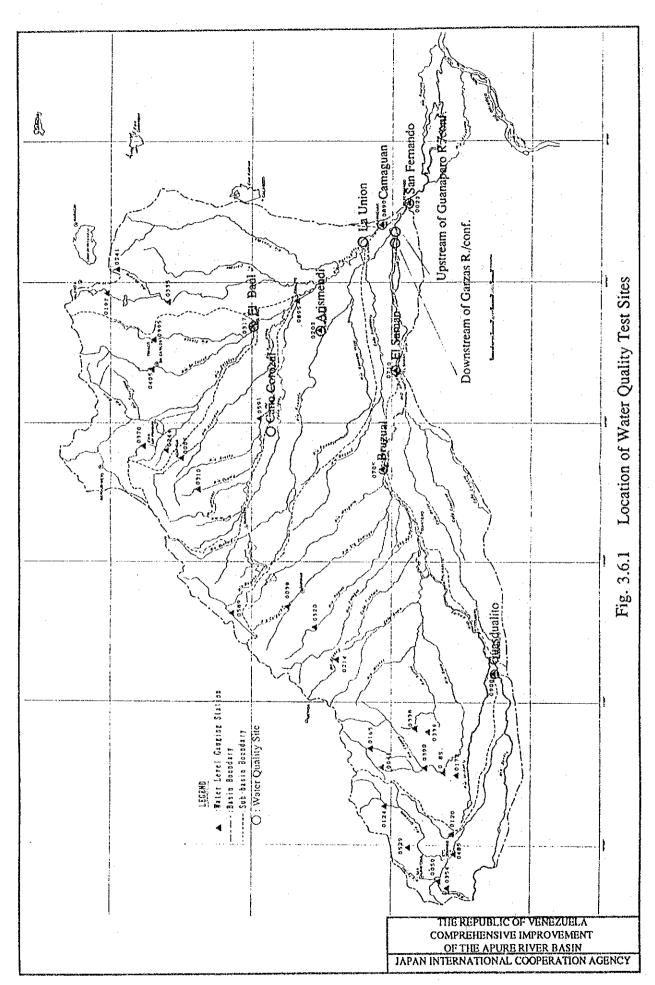


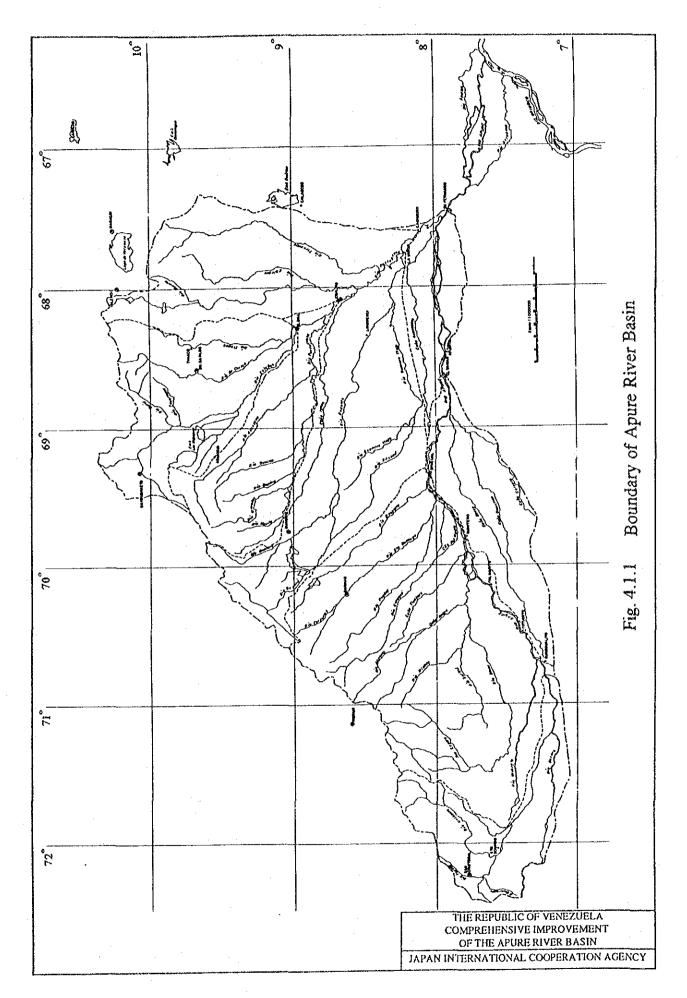
Fig. 3.5.2 Result of Discharge Measurement (2/2)

THE REPUBLIC OF VENEZUELA
COMPREHENSIVE IMPROVEMENT
OF THE APURE RIVER BASIN
JAPAN INTERNATIONAL COOPERATION AGENCY









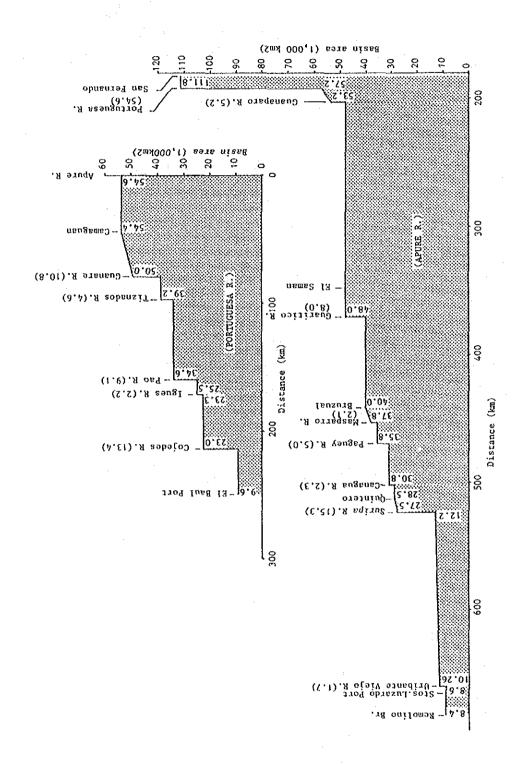
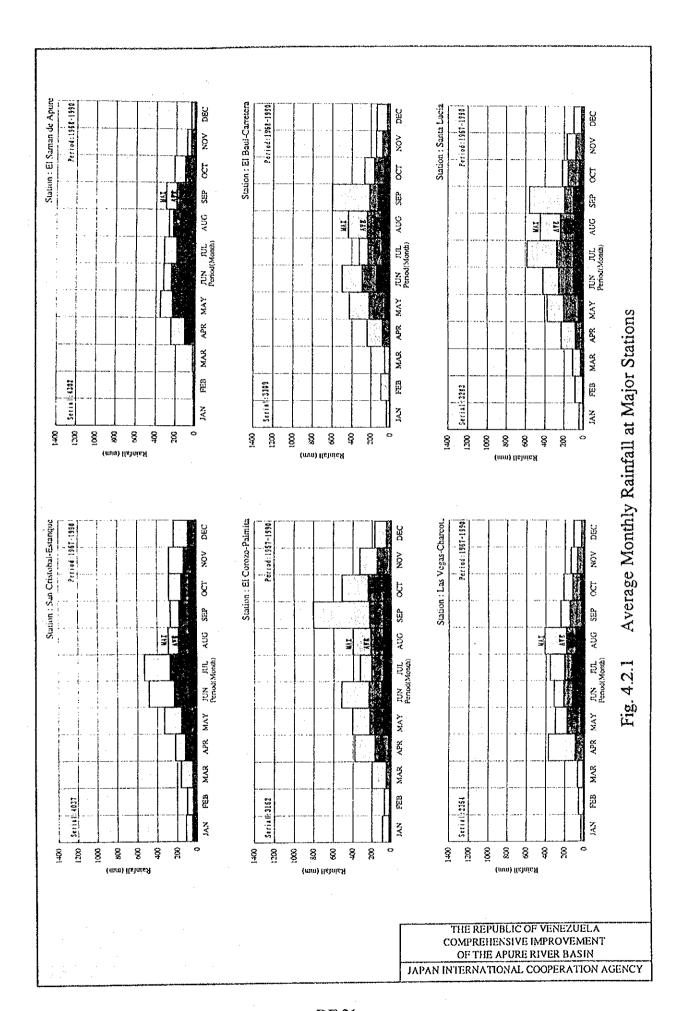
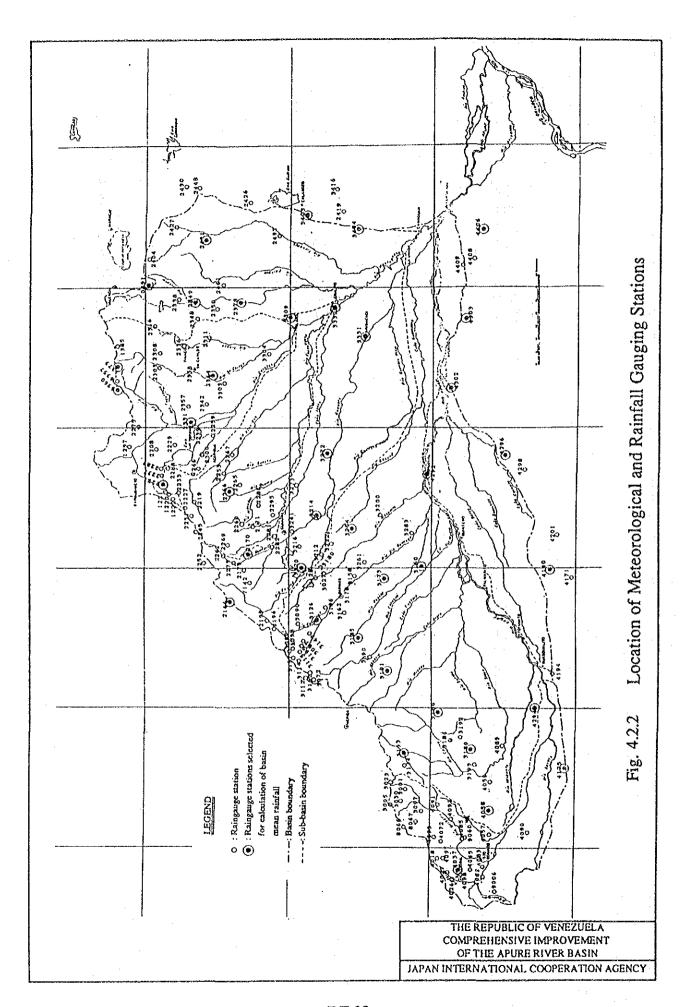


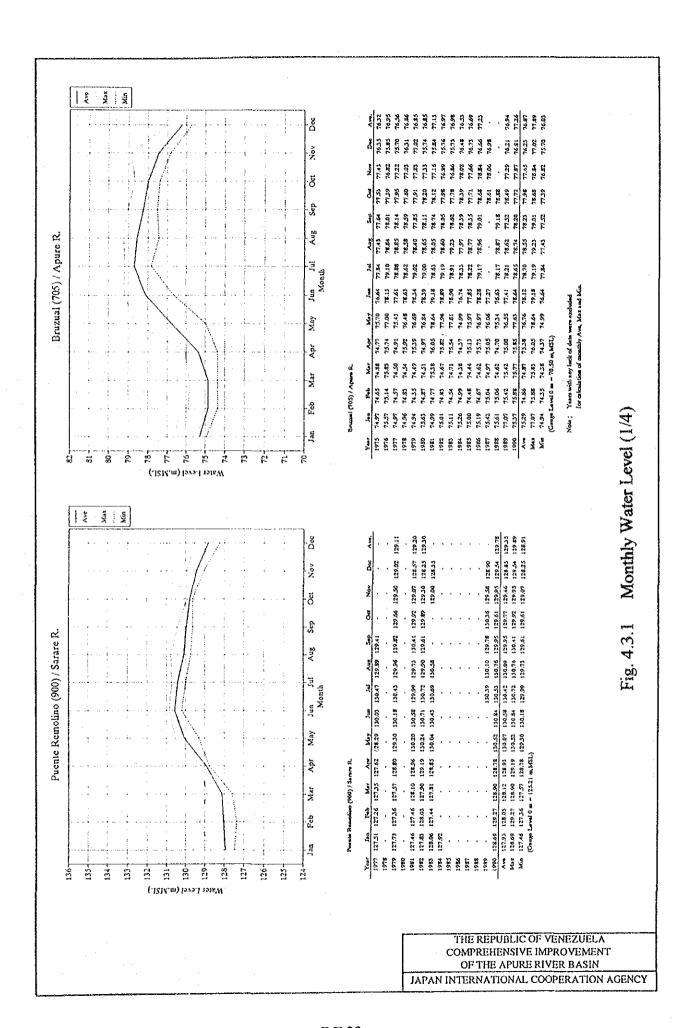
Fig. 4.1.2 Drainage Area of Apure River

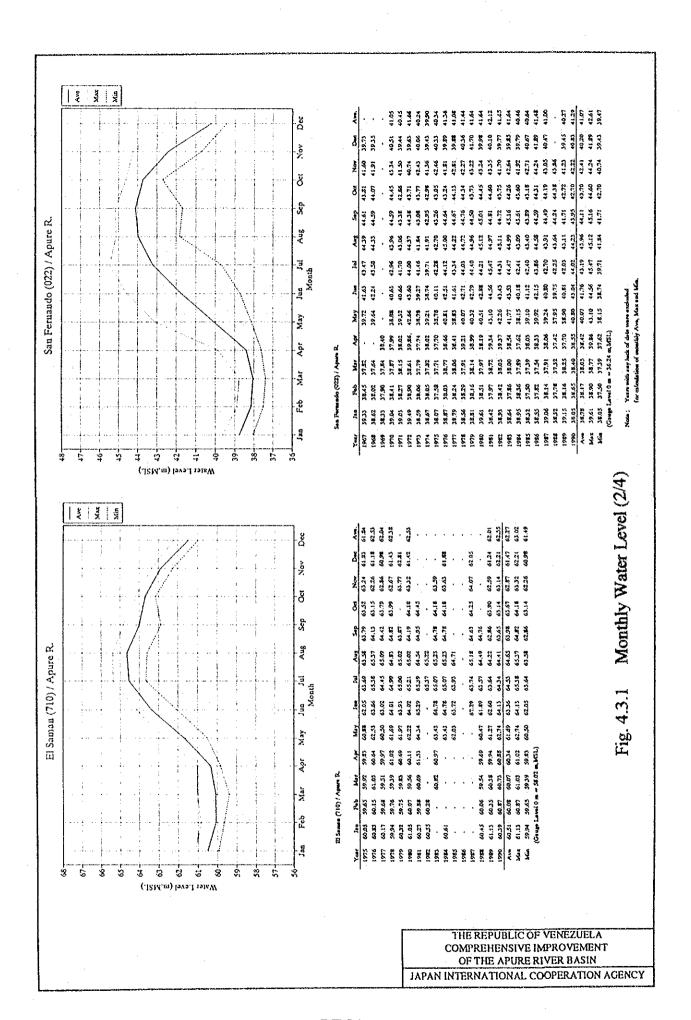
THE REPUBLIC OF VENEZUELA COMPREHENSIVE IMPROVEMENT OF THE APURE RIVER BASIN

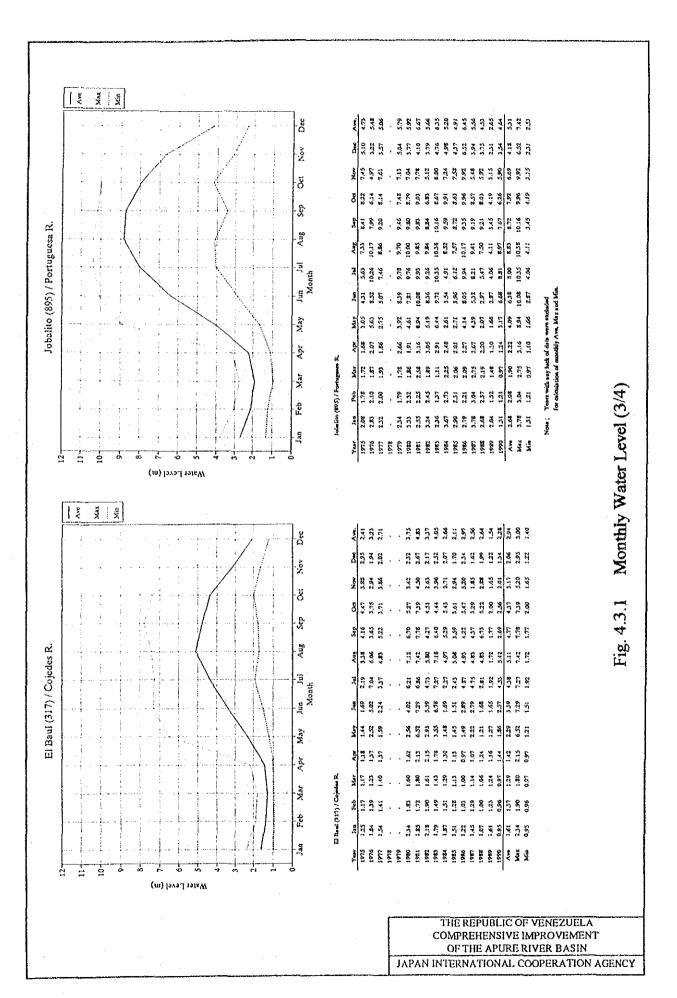
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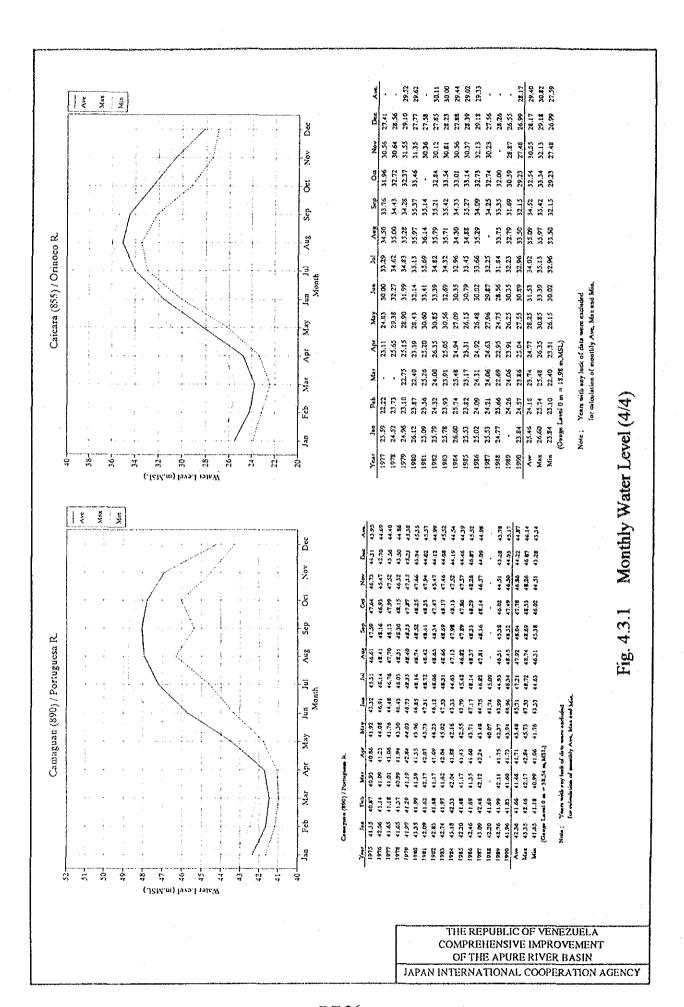


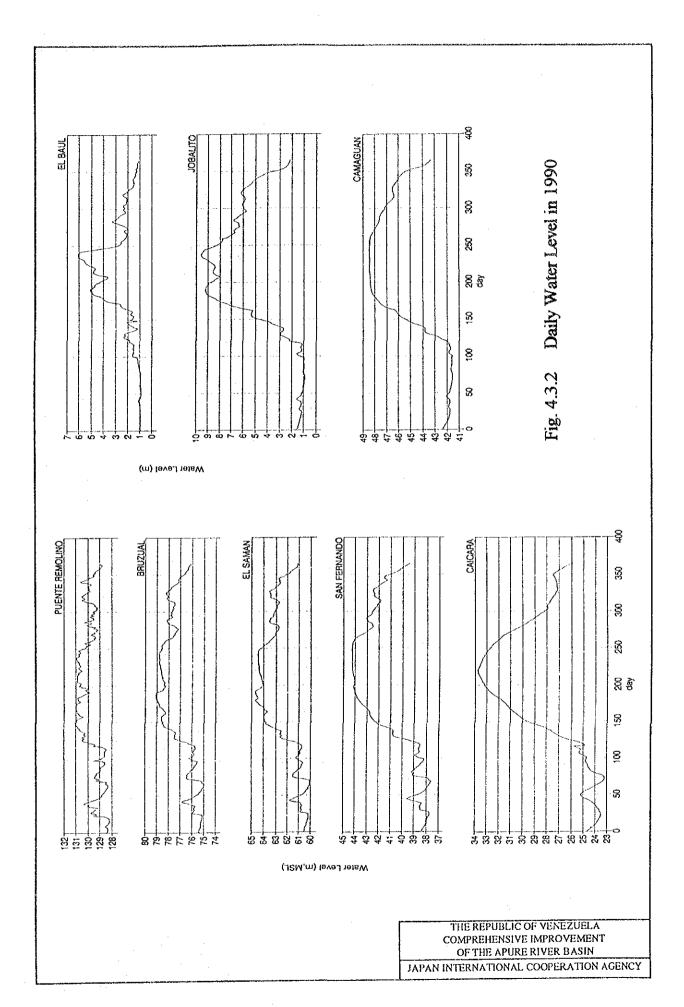


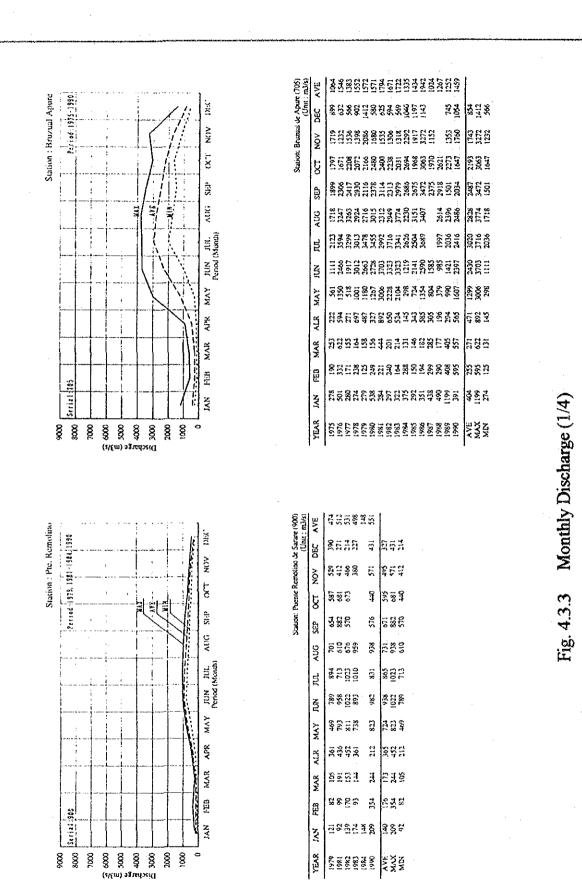






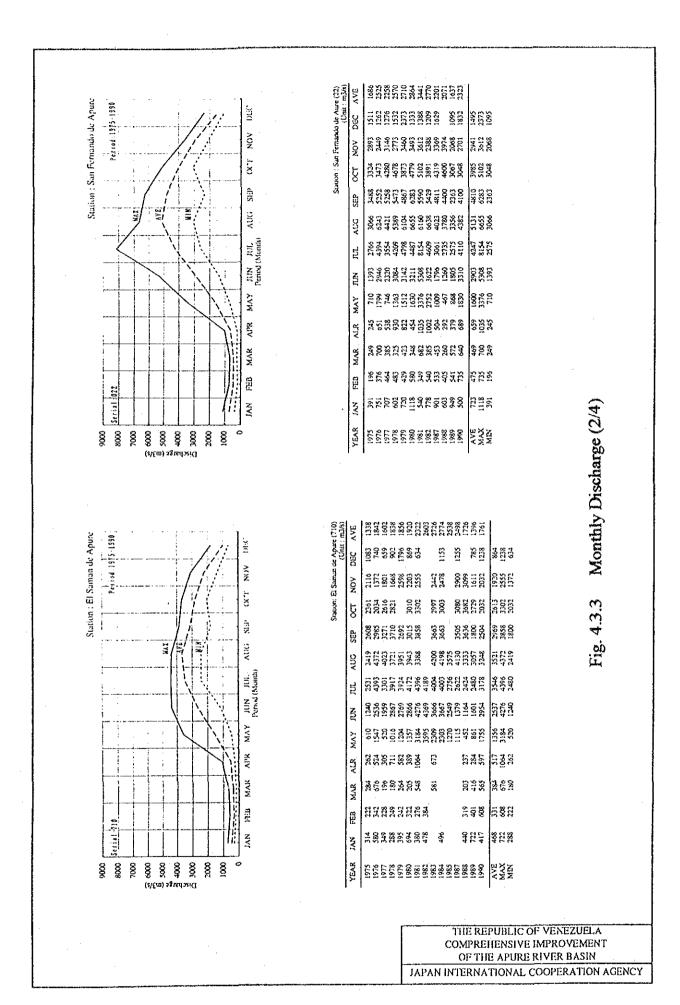


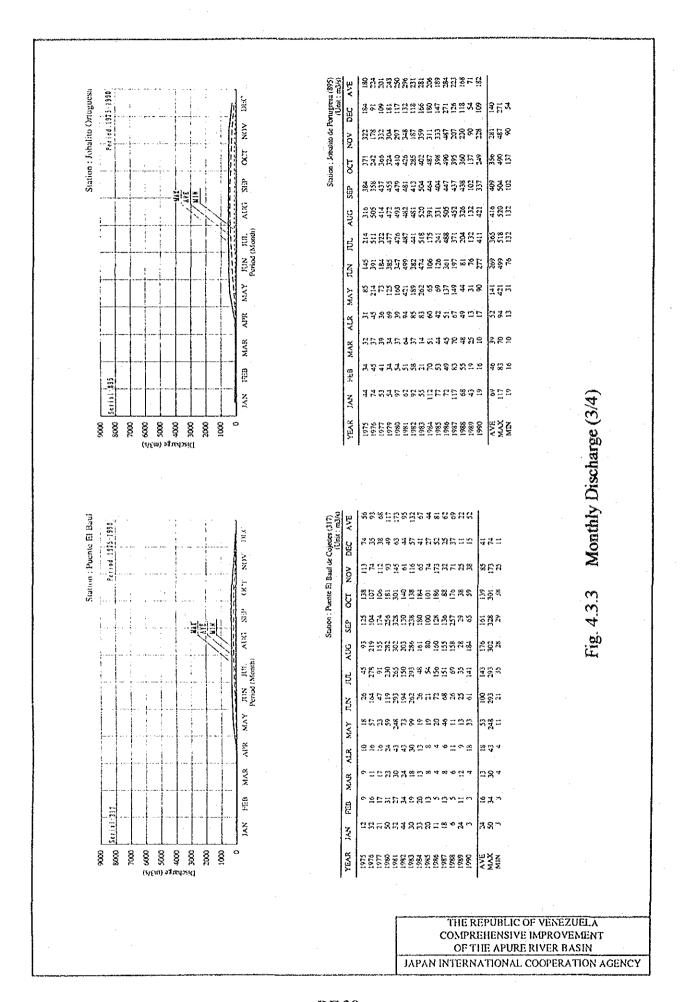


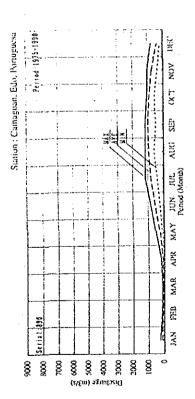


THE REPUBLIC OF VENEZUELA COMPREHENSIVE IMPROVEMENT OF THE APURE RIVER BASIN

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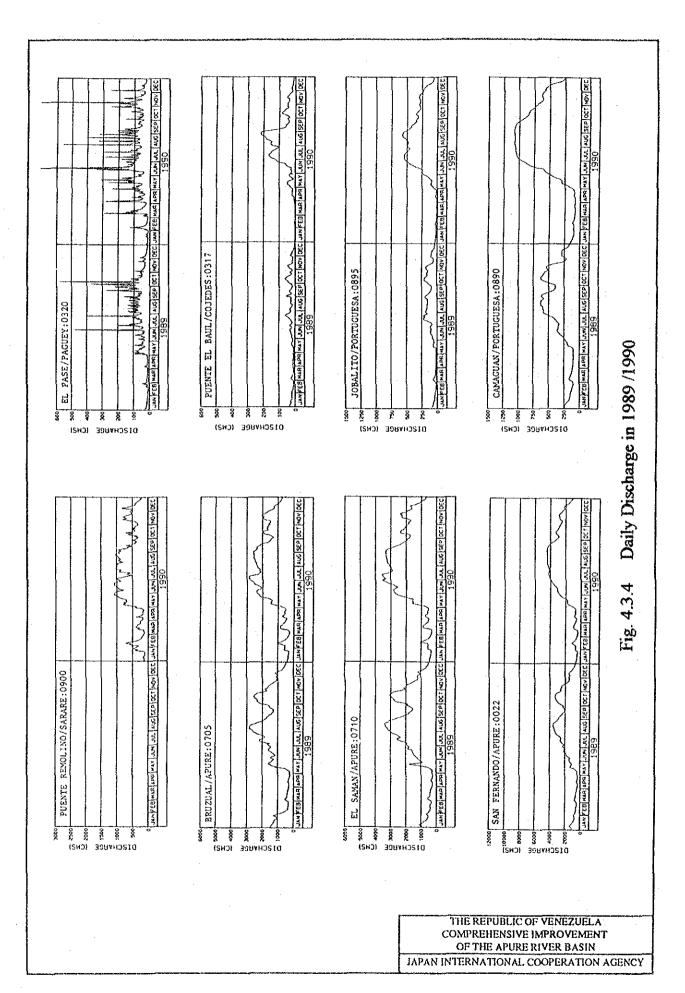


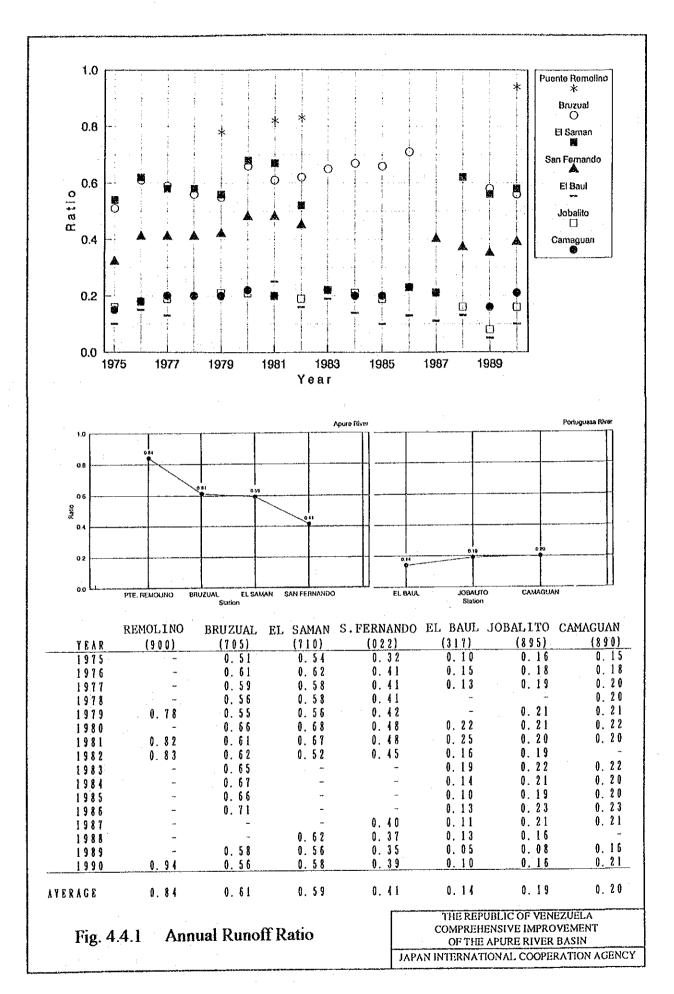
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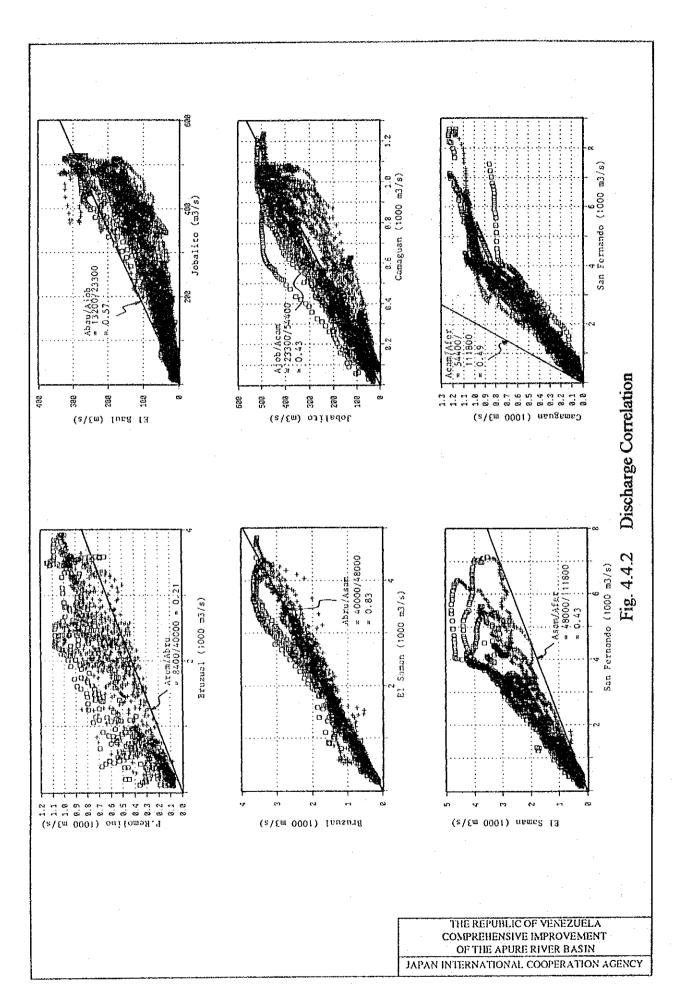
Fig. 4.3.3 Monthly Discharge (4/4)

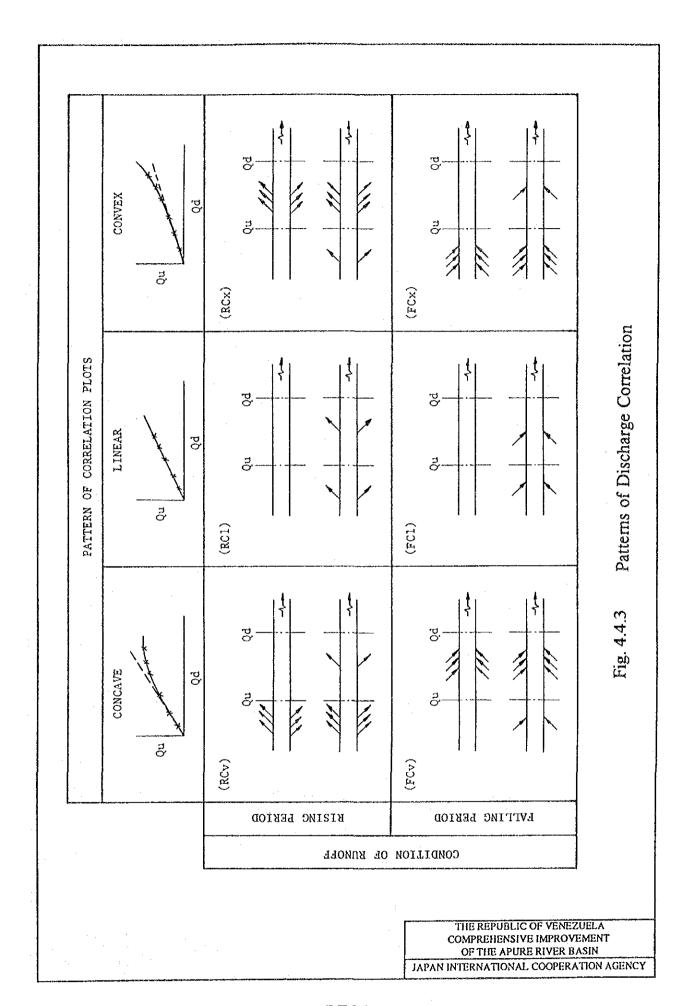
THE REPUBLIC OF VENEZUELA COMPREHENSIVE IMPROVEMENT OF THE APURE RIVER BASIN

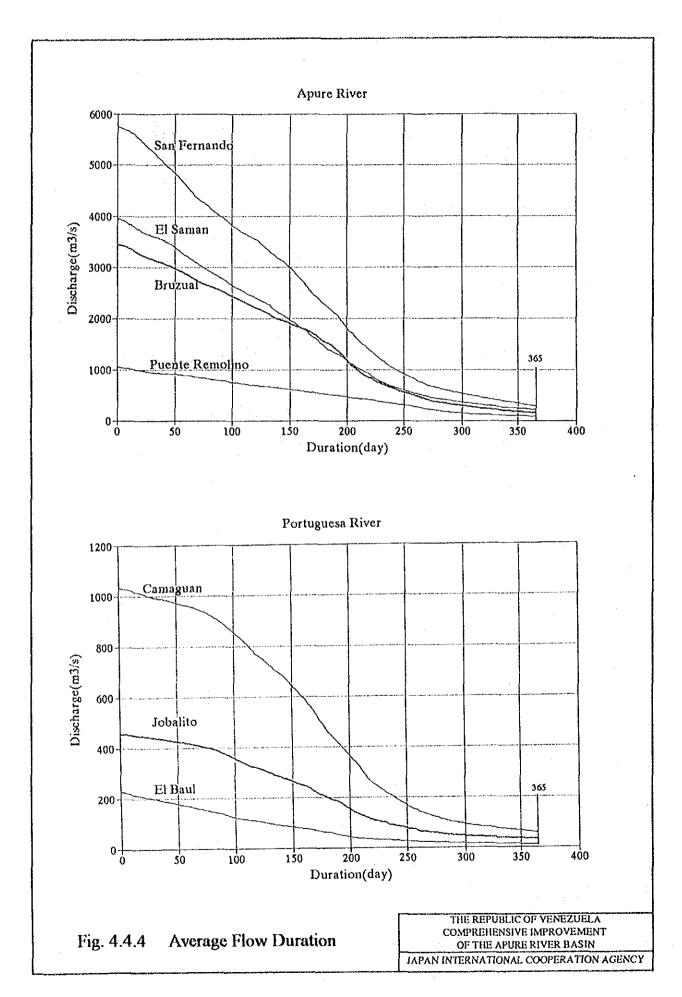
JAPAN INTERNATIONAL COOPERATION AGENCY

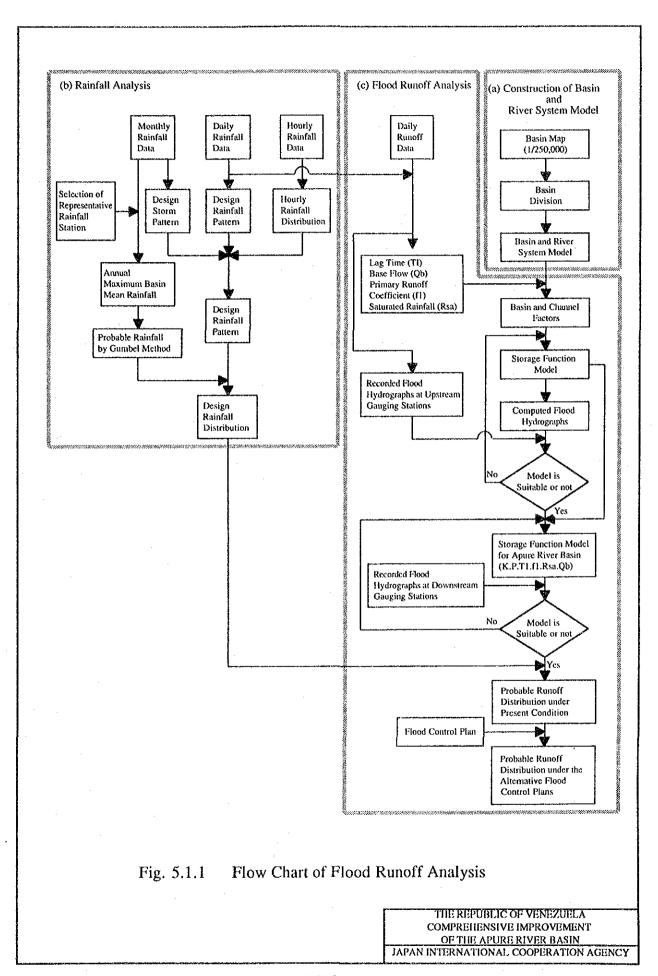


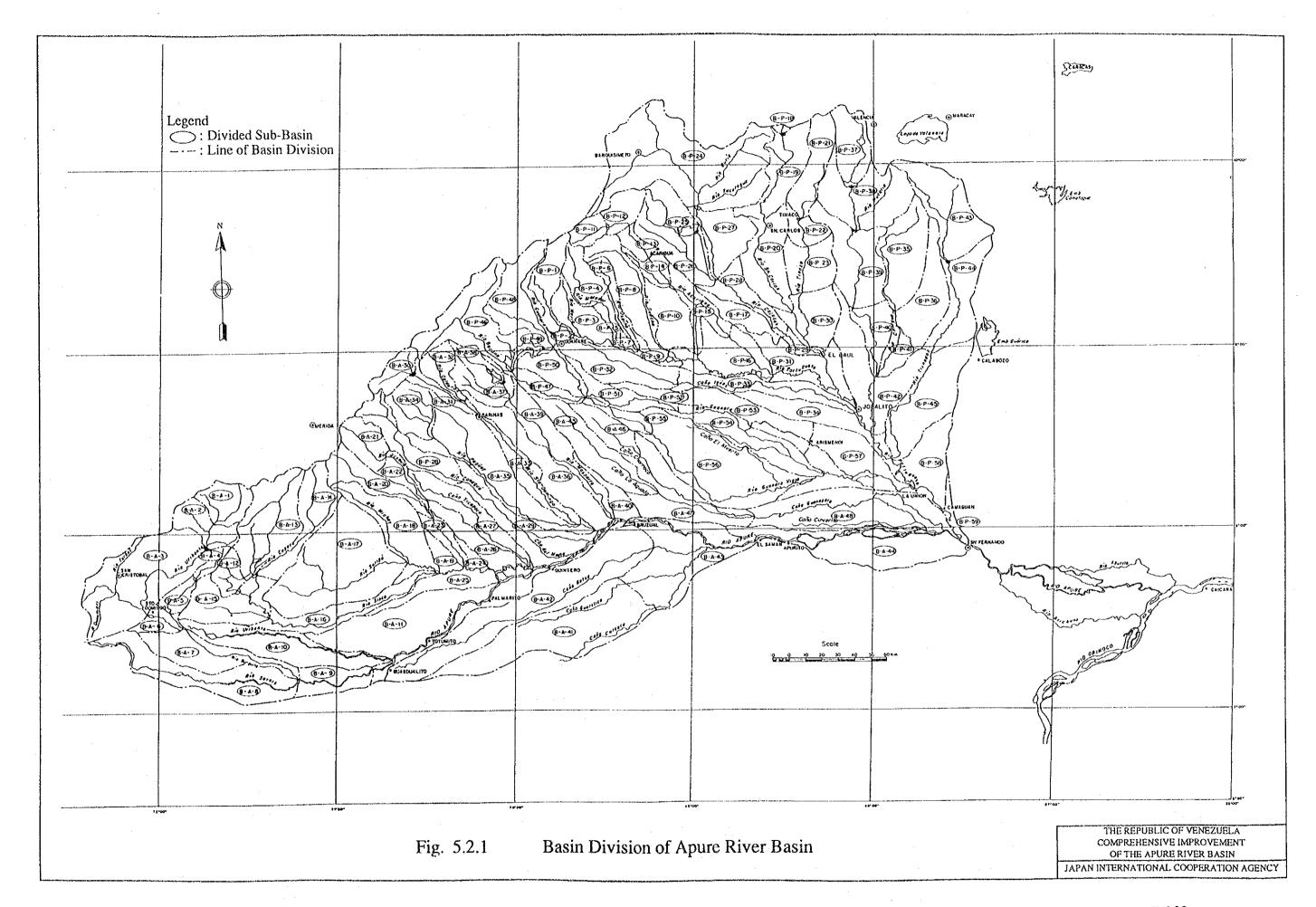












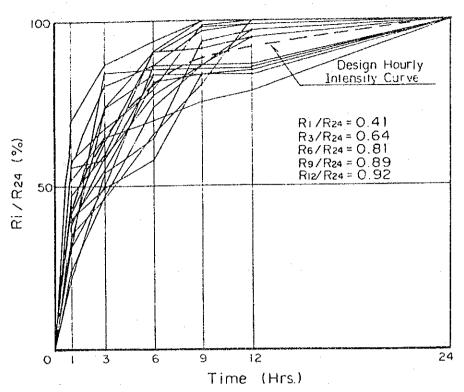


Fig. 5.3.1 Design Hourly Intensity Curve

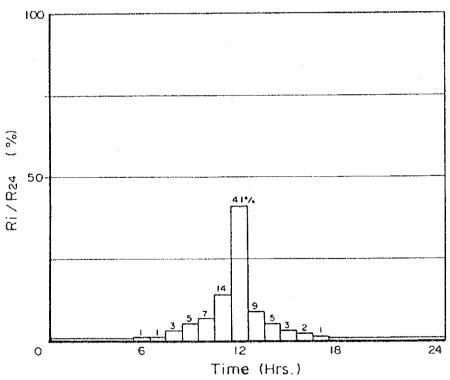
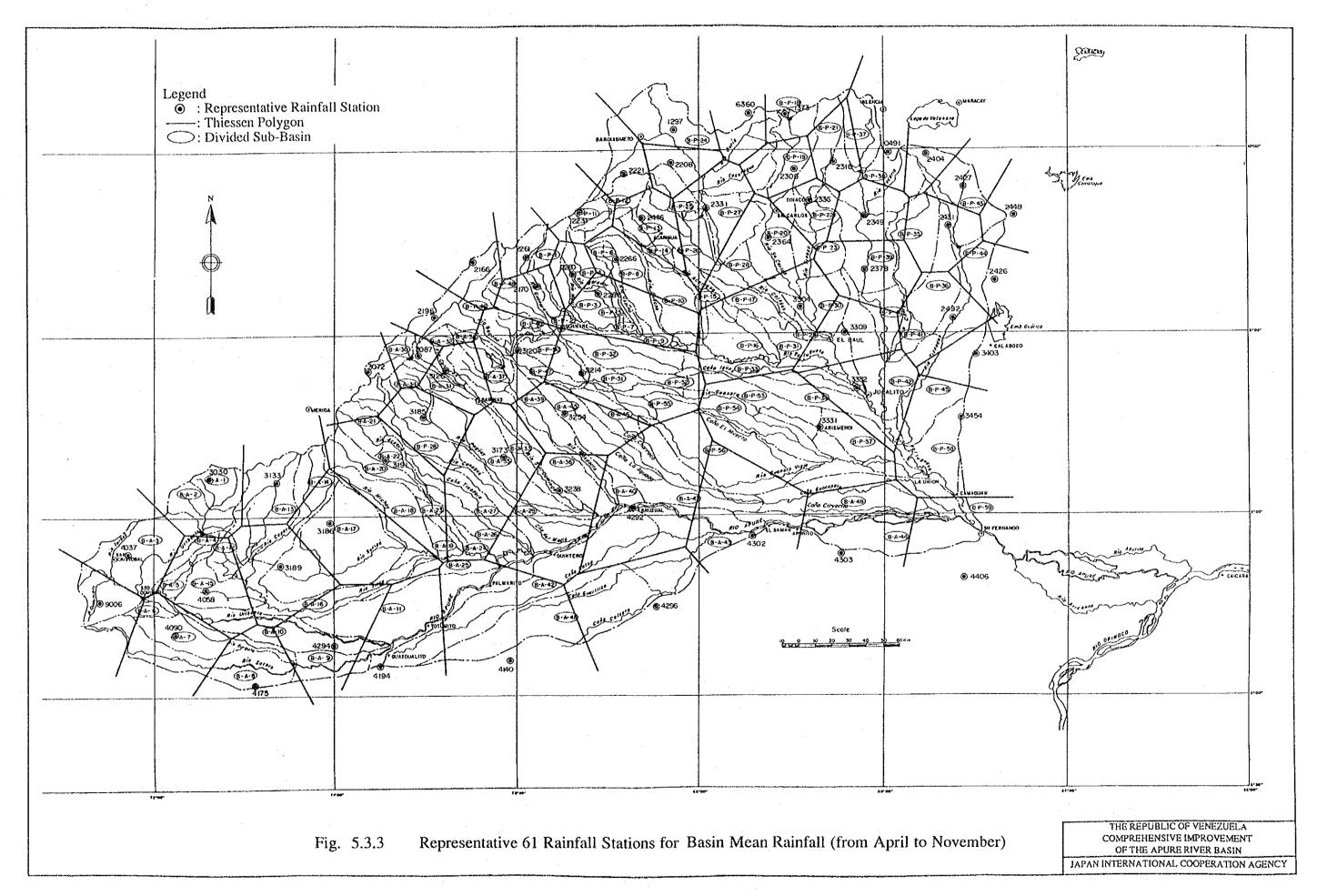
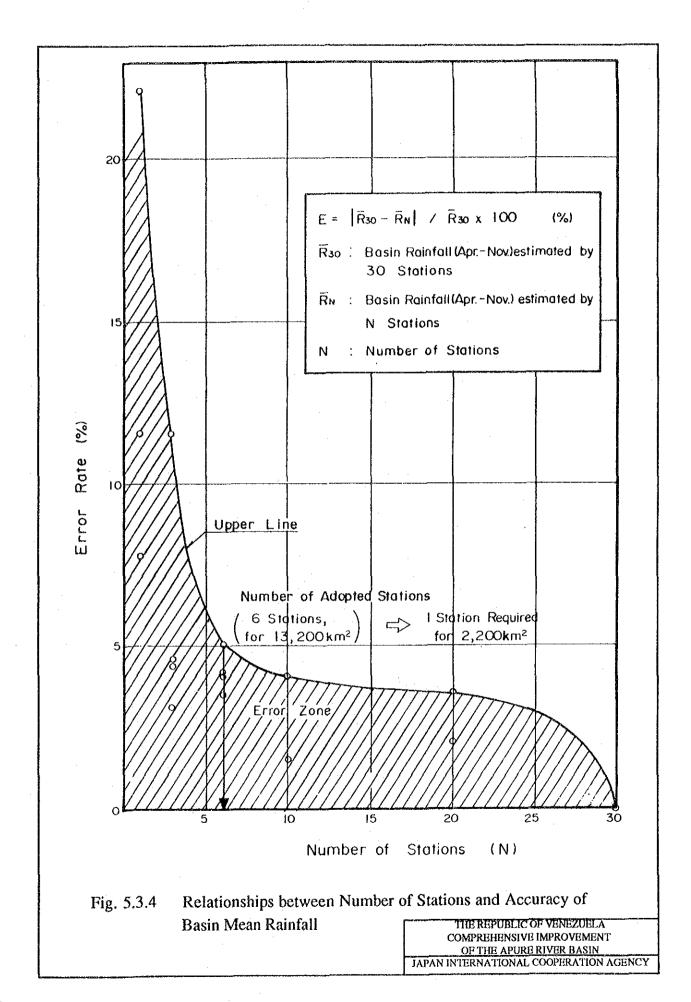
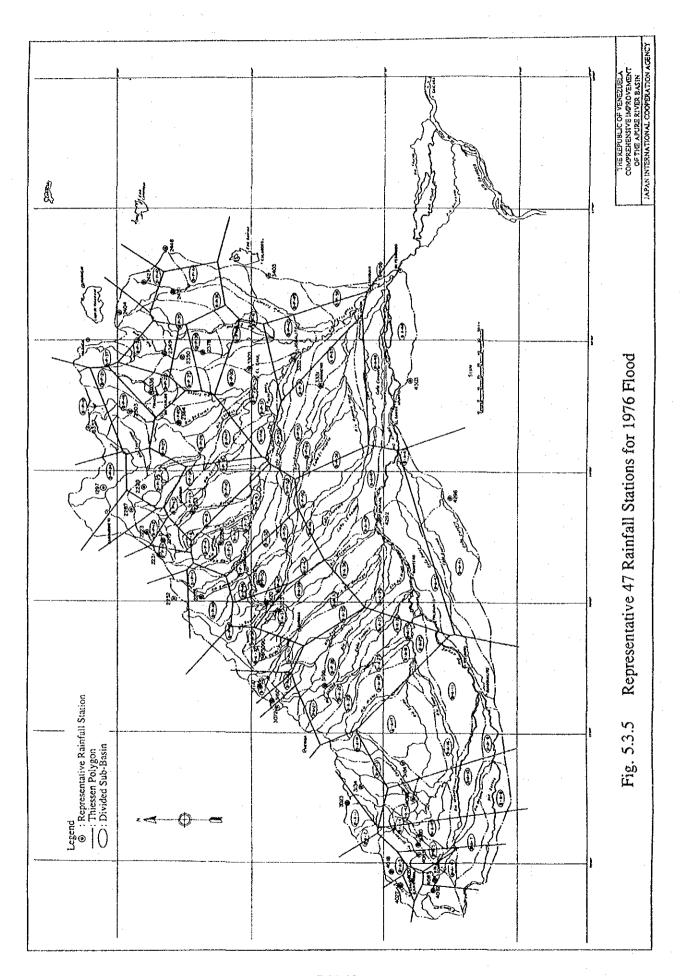
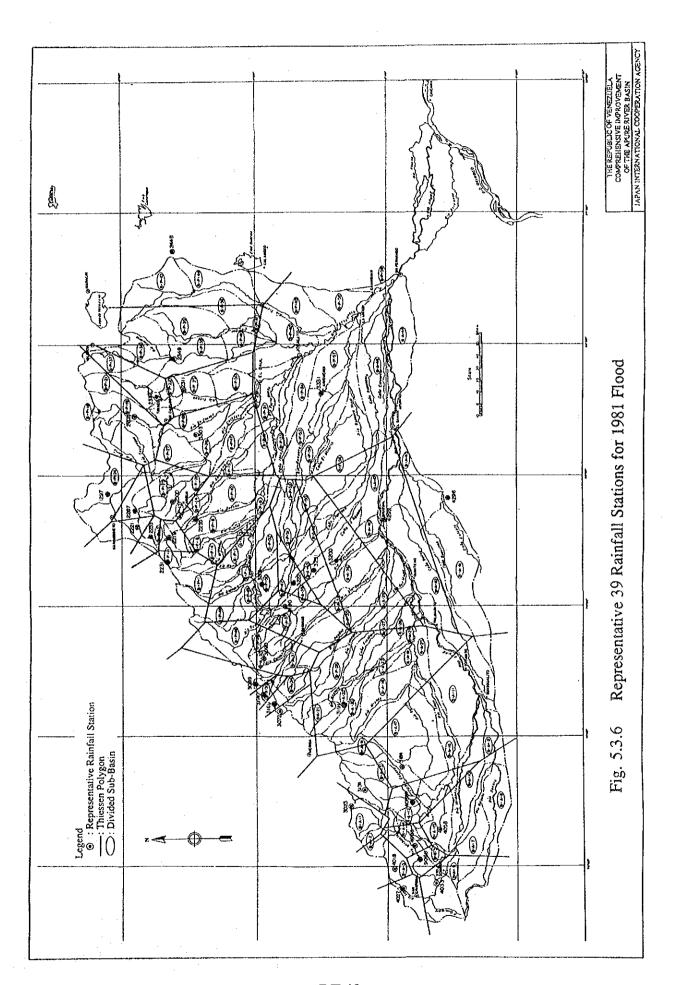


Fig. 5.3.2 Design Hourly Rainfall Distribution









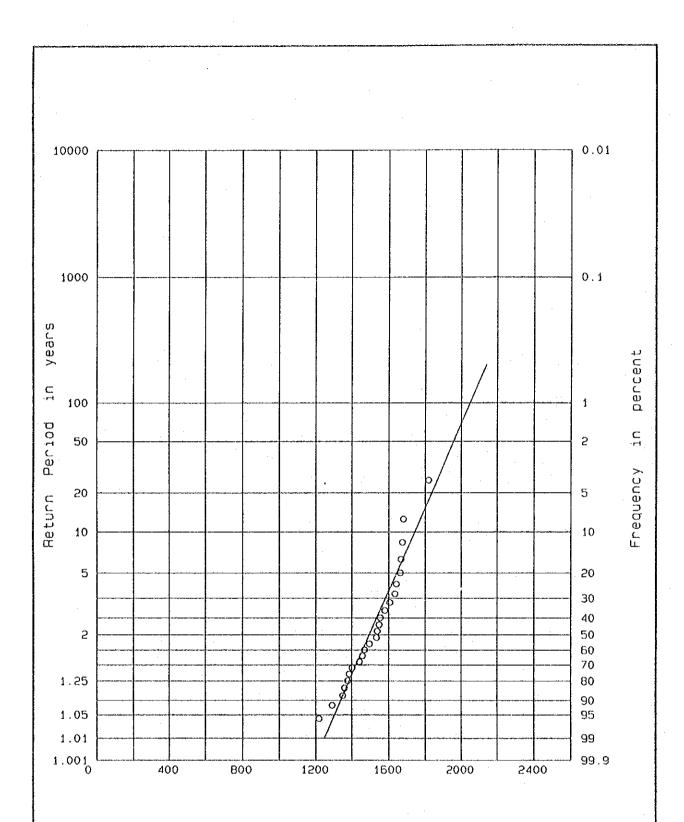


Fig. 5.3.7 Frequency Curve of 8-month Basin Mean Rainfall at San Fernando

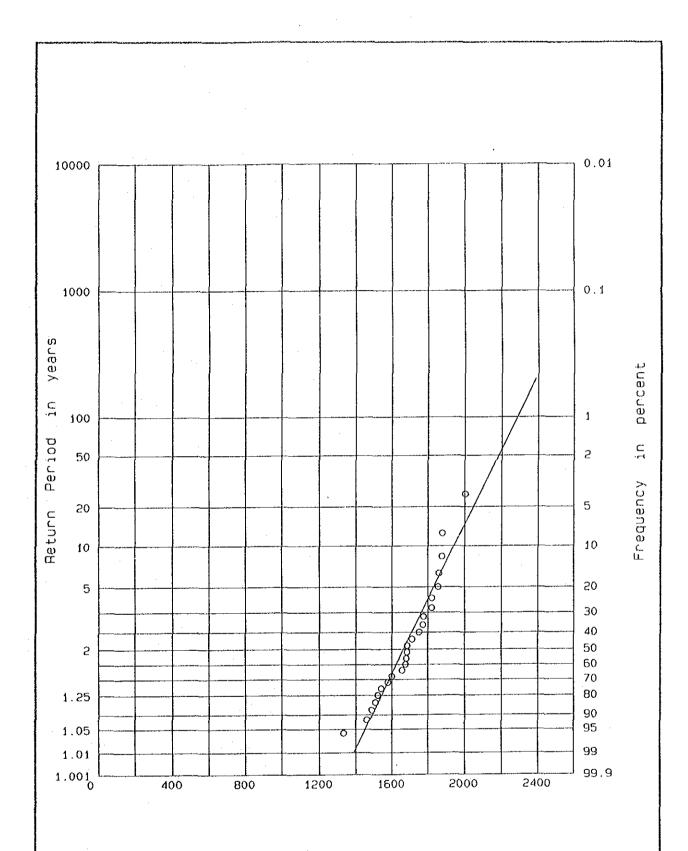


Fig. 5.3.8 Frequency Curve of 8-month Basin Mean Rainfall at El Saman

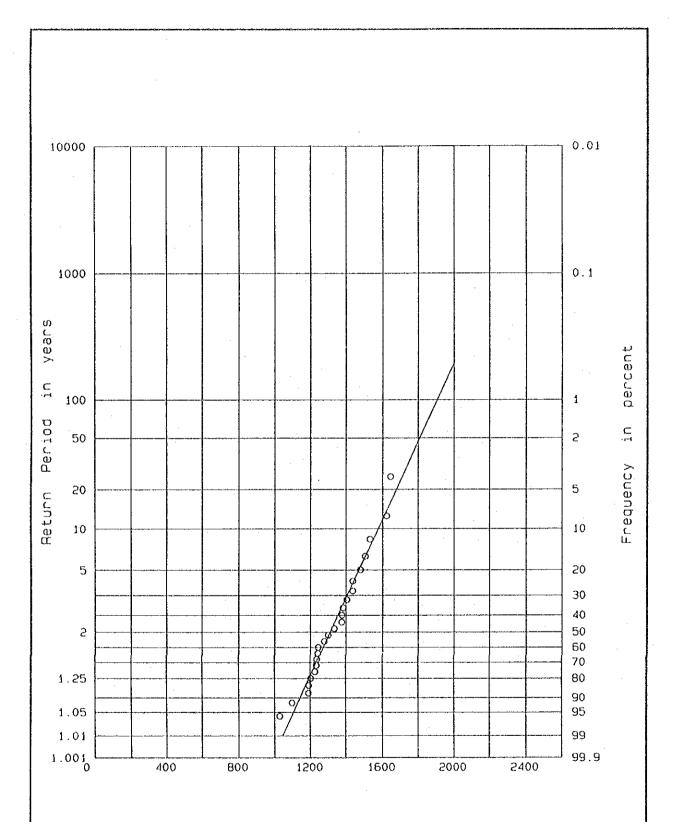
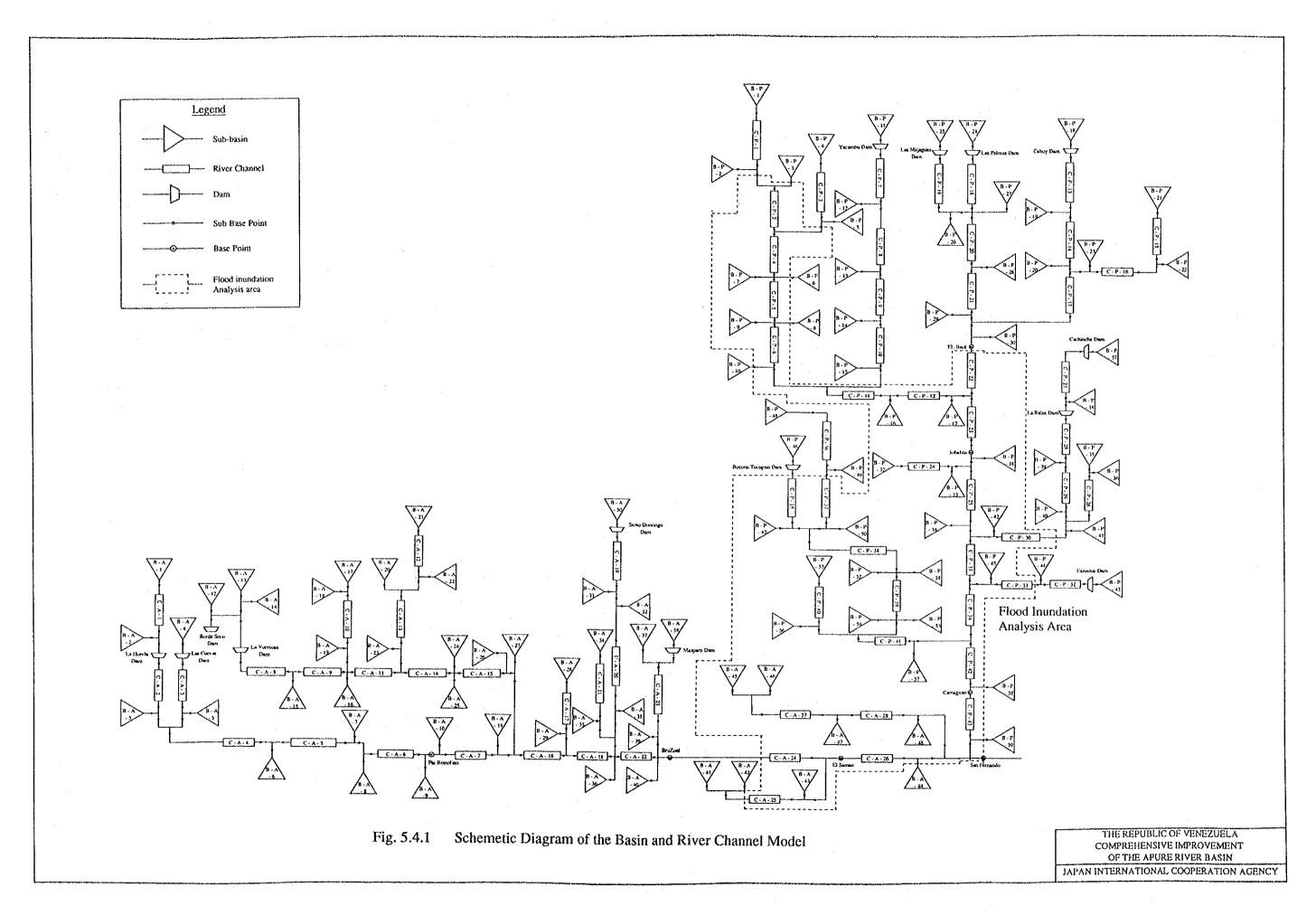
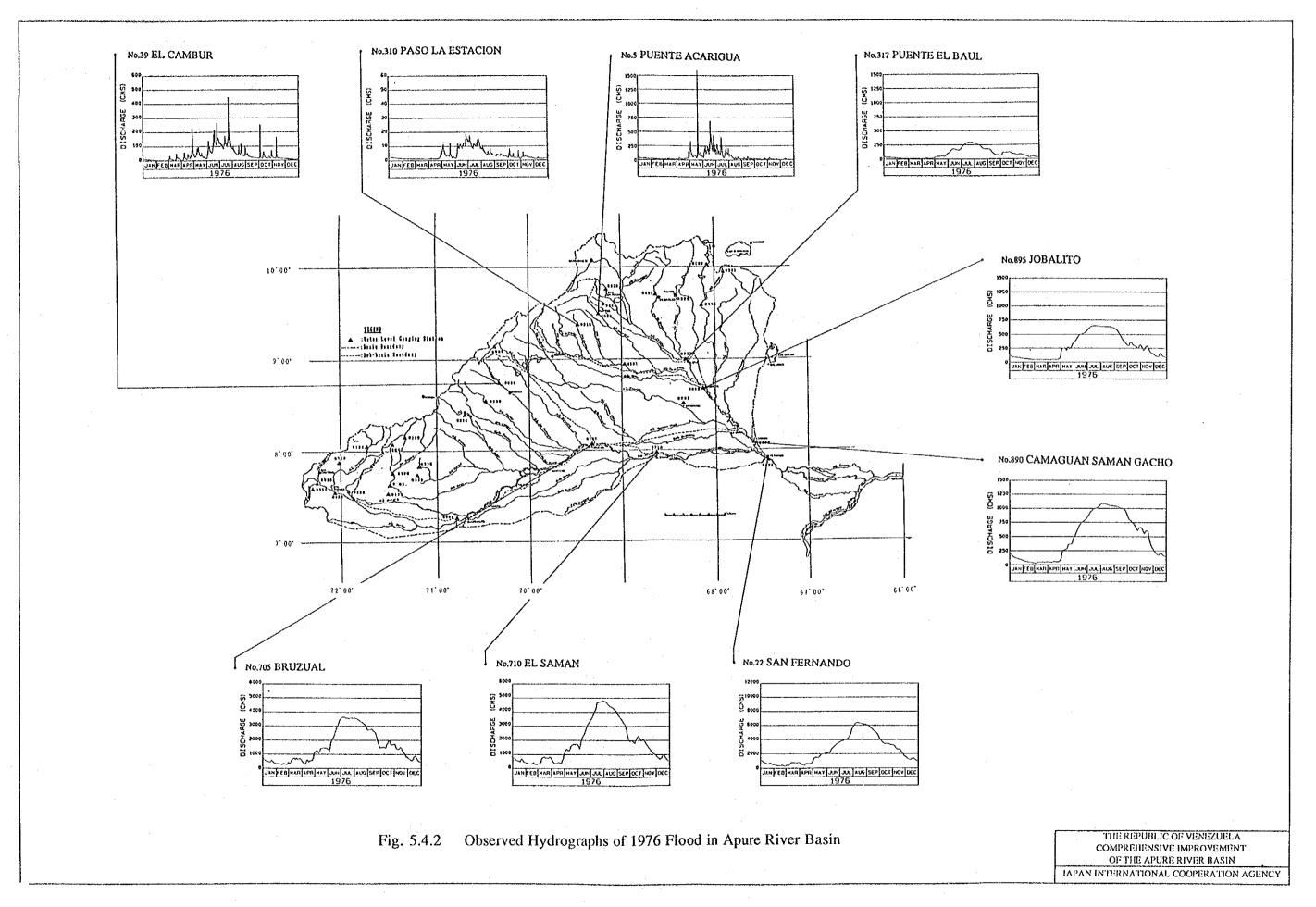
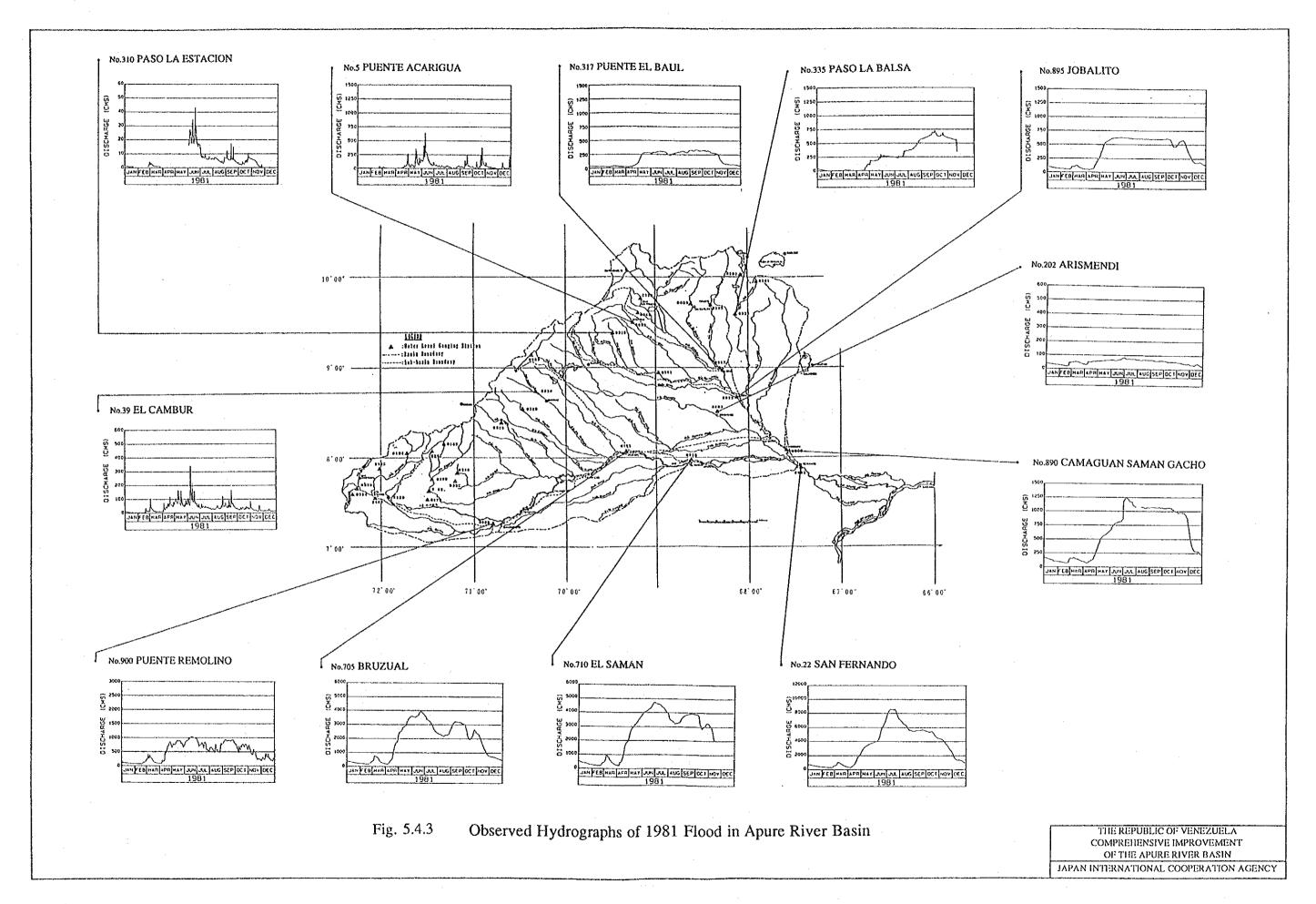


Fig. 5.3.9 Frequency Curve of 8-month Basin Mean Rainfall at Camaguan







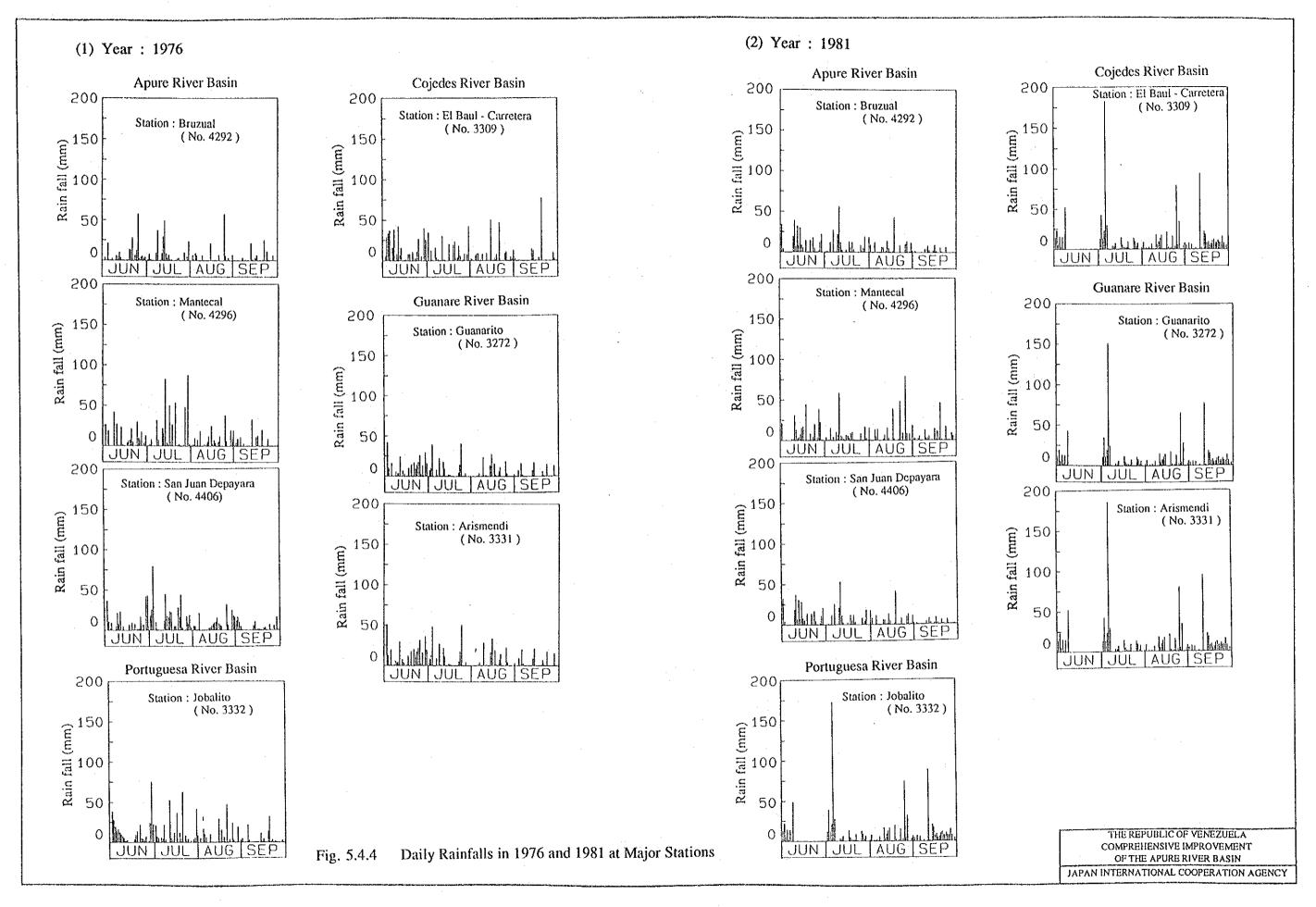
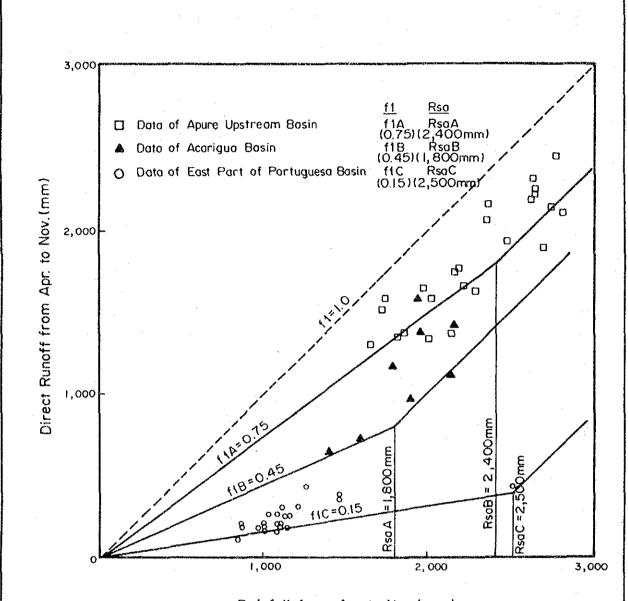


Fig. 5.4.5 List of Water Level Gauging Stations for Flood Study

	Catchment	Vear	Selection Criteria Selected	ed Remarks
No. St. No. Station Name		70 71 72 73 74 75 76 77 78 79 80 81 82 83 84 85 86 87		
1 0005 Acarigua		00000000000	0000	·
2 0022 San Fernando		0000000	0 0 0 0 0 0 0 0 0	Effective to Pond Model
3 0039 El Cambur		0000000000	0000	
4 0050 Puente Junin			0 0 00	Data reliability is low
5 0120 Puente Doradas	Jas	000000000	00 00	
6 0124 Puente El Molino		0000	0000	
7 0172 Puente Navay		•	0	Data resiability is sow
8 0202 Arismendi	1,2	1,290	.000	Data reliability is low
9 0214 Puente La Acequia		00000000000	000	No rainfall data is available.
10 0310 Paso La Acequia		200 000 0000	0	Catchment area is small
11 0317 El Baul		0000000000	0000 000	
12 0320 El Paso		0000000000	0000	
13 0335 La Balsa Dam		2,700	0	
14 0338 La Balsera	3(000000000000000000000000000000000000000	0.00	Catchment area is small
15 0339 Puente Suripa	:	200 00000000000000000000000000000000000	0	Catchment area is small
16 0395 Tinaco	9	OOOOO	000	
17 0405 San Carlos	1,490	000000000	0	1
18 0485 Sto.Domingo		00000000000		Data reliability is low
19 0589 La Cavita	æ	300	0	Data reliability is low
20 0591 Nueva Florida		5,210	0	Data reliability is low
21 0687 El Tambo	w.	320	00	Data reliability is low
22 0705 Bruzual	40,000	00000000000	0000	0
23 0710 El Saman	48,000	0 0000000000	0000	O Effective to Pond Model
24 0890 Camaguan		00000 00000	0 0 0	D Effective to Pond Model
25 0895 Jobalito	23,3	00000000000	0000	O Effective to Pond Model
26 0900 Guasdualito		000	0	
Note:	Ē	11.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1		

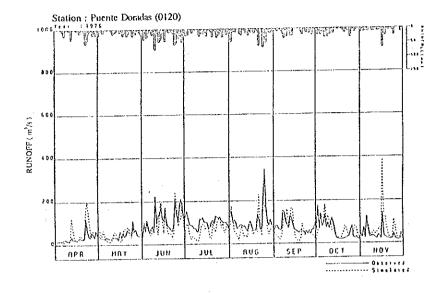
Flood hydrograph in 1976 or 1981 is available. Selection criteria (a):
Selection criteria (b):
Selection criteria (c):
Selection criteria (d):

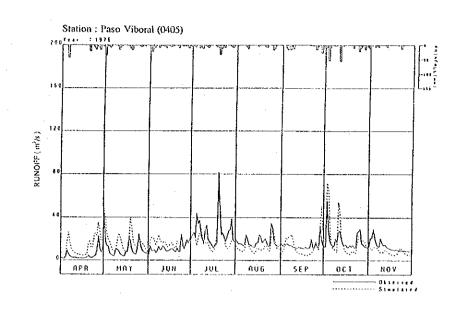
Long period data (around 10 years) is available, and there is a few lack of data (Reliability of data is considered to be high). No effect of existing dam/reservoir is expected. Reliable rainfall data in and around the water level gauging basin is available.

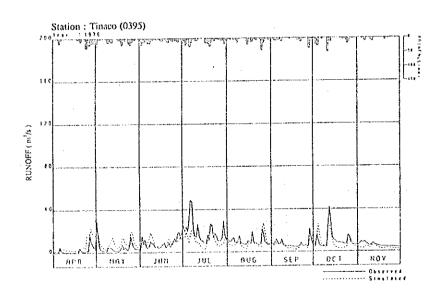


Rainfall from Apr. to Nov (mm)

Fig. 5.4.6 Primary Runoff Coefficient (f1) and Saturated Rainfall (Rsa)







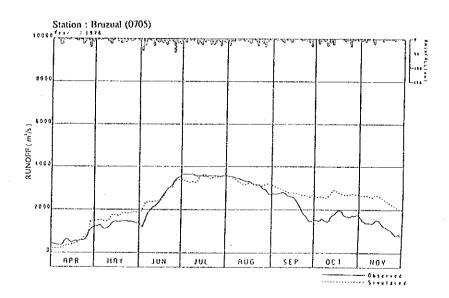


Fig. 5.4.7 Observed and Simulated Hydrographs in 1976

