

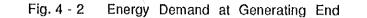
Forecast of GDP (M_Baht)

Forecast of Energy Consumption

Forecast of Energy Demand (GWh)

> Maximum Power Demand (₩₩)

Maximum Power Generation (₩₩)



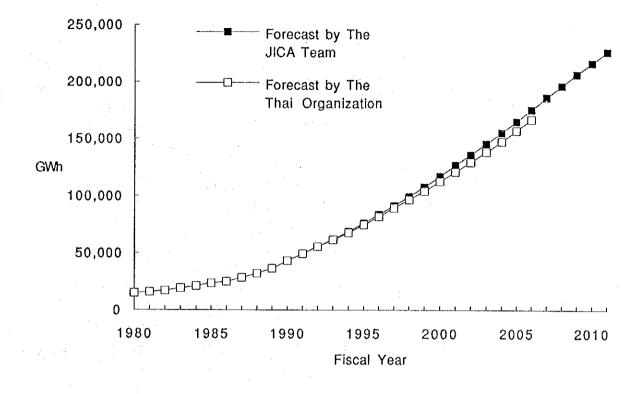
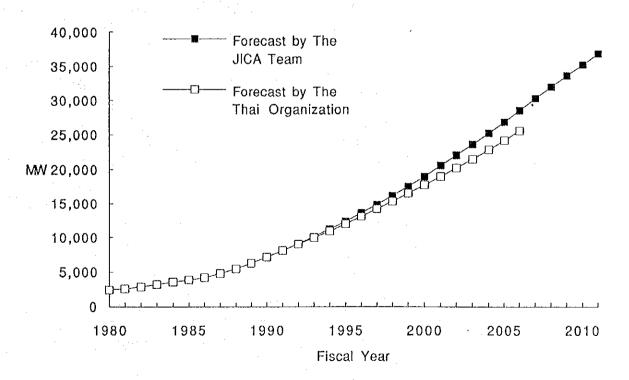


Fig. 4 - 3 Maximum Power Demand at Generating End



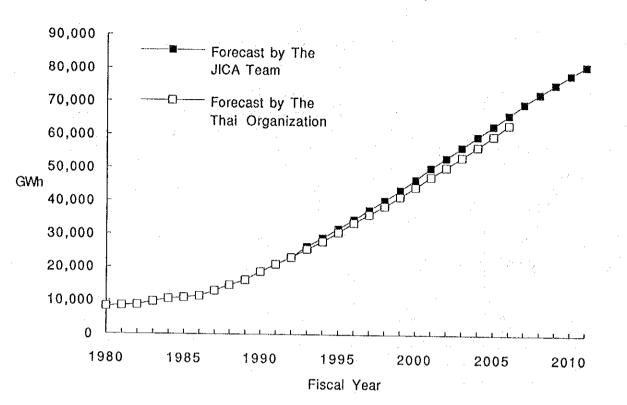


Fig. 4 - 5 Maximum Power Demand by MEA

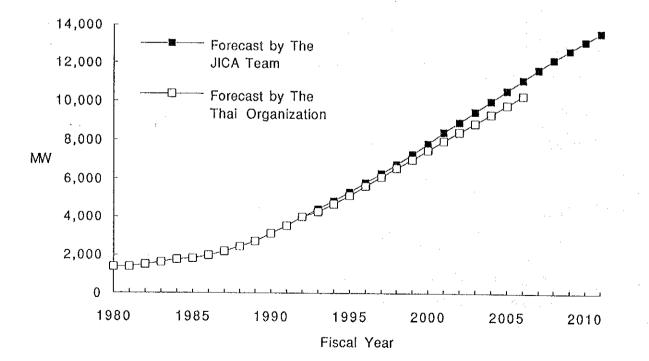


Fig. 4 - 4 Energy Demand by MEA

CHAPTER 5

POWER SYSTEM PLANNING OF THE GREATER BANGKOK AREA

FOR A LONG FUTURE

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CHAPTER 5 POWER SYSTEM PLANNING OF THE GREATER BANGKOK AREA FOR A LONG FUTURE

5.1 The Power System of Thailand - Present Situation

Fig. 5-1 shows the outline of the power system of Thailand. Voltages of the transmission lines forming the power system of Thailand are 500 kV, 230 kV, 115 kV and 69 kV. The frequency of electricity is 50 Hz.

The power system is divided into the following four regions.

Region 1 : Metropolitan Area and its Surrounding Part of Thailand Region 2 : Northeastern Part of Thailand Region 3 : Southern Part of Thailand Region 4 : Northern and Central Part of Thailand

Each region is connected by transmission lines of 500 kV, 230 kV and 115 kV.

The total capacity of power generating facilities is 11,033 MW as of September 1992. It consists of hydro-electric power 2,429.2 MW (accounting for 22.0% of the total), oil/gas and lignite fired thermal 5,506.5 MW (49.9%), combined cycle 2,859.6 MW (25.9%) and gas turbine 238.0 MW (2.2%).

5.1.1 Power Supply Capability And Electric Energy Demand of Each Region

Below is the feature of each region in respect of power supply and demand as of September 1992.

(1) In Region 1, there are thermal power stations and combined cycle plants of large scale such as SOUTH BANGKOK (1,330.0 MW), BANG PAKONG (3,074.6 MW), RAYON (1,130.0 MW), etc., and also reservoir type hydro-electric power stations of large scale such as SRINAGARIND (720.0 MW), KHAO LAEM (300.0 MW), etc. A total capacity of these facilities is 6,973.3 MW, accounting for about 63.2% of the total installed capacity of power sources in this country.

This region has a great demand for electric energy which accounts for about 75% of the total electric energy demand in the country.

(2) In Region 2, there are hydro-electric power stations of medium scale such as CHULABHORN (40.0 MW), SIRINDHORN (36.0 MW), a combined cycle power plant at NAM PONG (355.0 MW) and some gas turbines.

A total capacity of these facilities is 491.3 MW, accounting for 4.5% of the total installed capacity in the country.

These power sources are capable of load-frequency control and used effectively in an ordinal operation especially at the peaking time.

The power supplied for the base load is transmitted mainly from Region 4 through the 230 kV transmission lines and also from Region 1 through the 115 kV transmission lines.

Some of the power required in this region is supplied from Lao PDR, a neighboring country, based on a contract to purchase surplus energy (power) generated by the Nam Ngum hydro-electric power station (150 MW) which belongs to this country.

Demand for electric energy in this region accounts for nine to ten percent of the total demand of the country.

(3)

In Region 3, there are thermal power stations such as KHANOM (150.0 MW), KRABI (34.0 MW), SURATANI (72.0 MW), etc. and also hydro-electric such as RAJJAPRABHA (240.0 MW), BANG LANG (72.0 MW), etc.

A total capacity of these facilities including the gas turbine (42.0 MW) at Hat Yai is 611.3 MW which accounts for 5.5% of the total installed capacity in the country.

Power for base load of this region is supplied from the Khanom and Krabi thermal and from Region 1 as well through the Second Central - Southern Tie line, a 230 kV double-circuit between PRACHUAP KHIRI KHAN and SURAT THANI.

This region and a neighboring country, Malaysia, are mutually exchanging electric power by means of the 115/132 kV power system interconnection which has been in operation between two countries since February 1981.

Demand for electric energy in this region accounts for six to seven percent of the total demand of the country.

(4) Power stations installed in Region 4 are the Mae Moh thermal power plant with the output of 2,025.0 MW, and hydro-electric of large scale such as BHUMIBOL (535.0 MW), SIRIKIT (375.0 MW), etc.

A total output of these facilities is 3,070.0 MW, which is about 28% of the total installed capacity of power sources of this country.

Demand for electric energy in this region accounts for eight to nine percent of the total demand of the country.

5.1.2 The Power Transmission among The Regions

Even though Region 1 has a very large supply capability of power, it cannot meet independently its great demand for power which accounts for approximately 75% of the total demand of the country.

A main load center of the region is the Greater Bangkok Area, namely Bangkok and its surroundings.

A short of power in Region 1 is supplemented by means of interconnection of lines from Region 4 which has a great surplus power due to the recent extension of the Mae Moh power plant in addition to relatively low power demand.

Region 2 is also short of power as mentioned before. To meet its demand some of power must be sent from the neighboring regions, Region 1 and/or Region 4.

On the other hand, Region 3 is well balanced in power supply and demand, and so interchanging power with the other regions will not be needed in ordinal operation of the power system.

A typical power transmission among the regions is estimated by the JICA team in connection with the peaking time of fiscal 1991. That is shown on Fig. 5-2. Region 4 sends a total of 2,200 MW to Region 1 and Region 2, which receive 1,700 MW and 500 MW respectively.

5.2 Development of Power Sources for Future Need

As mentioned before, the total installed generating capacity of Thailand is 11,033 MW as of September 1992. It holds about 18% of reserve margin for the dependable capacity 10,634 MW which takes seasonal output variation of hydroelectric power plants and generation under full rated capacity of thermal power plants into account.

However, a great effort is required to make for continuous development of power sources to hold a sufficient power supply capability to cope with demand for power which is forecast to increase in future with a high growth rate.

Table 5-1 shows the transition of power supply capability in Thailand which is estimated according to EGAT's power development plan, PDP 92-01(1). The sites of power development in near future are centered on the Mae Moh area in the northern district of Region 4 and the eastern seaboard area of Region 1.

Because of the concentrated effort to develop a combined cycle power plant in the lower part of central region and thermal power plants in the eastern seaboard area and on the western coast of the Gulf of Thailand, the total installed generating capacity in Region 1 will be rapidly increased reaching about 18,000 MW in fiscal 2006.

On the other hand, the peak demand in this region is forecast to be about 19,100 MW in the same year, if it is assumed to account for about 75% of the total demand of the country. As a result, there will be still a shortage of power supply of about 1,100 MW which must be offset by power sent from the other regions.

Bang Saphan in the western seaboard, the location of the proposed thermal power plant, is very remote from the Greater Bangkok Area and close to Region 3, even though it belongs to Region 1 geographically. The distance between the project site and Sai Noi substation of the Greater Bangkok Area is about 375 km.

In addition, EGAT is planning to develop nuclear power in the southern seaboard area in Region 3, mostly aiming to send power to the Greater Bangkok Area of Region 1. It is supposed that the western seaboard and southern seaboard areas will become zones to generate great power after 2000. The transmission system must be able to send bulky amount of power from the above two seaboard areas over a long distance to the Greater Bangkok Area. Power system stability will be decisive and a lot of investment will be required to form the transmission system.

Environmental problems will accompany as a very important and serious matter to be solved for developing power sources and building the transmission system. It is conceivable that the transmission system possible to be built will be one of the crucial factors in decision of the scale of power sources.

Region 4 will increase its supply capability due to the continuous development of the lignite mines and thermal power to use lignite as fuel in the Mae Moh and Lampang areas. The surplus power of this region will be sent to Region 1 and Region 2.

The JICA team has estimated power transmission among the regions in 2006. Fig. 5-3 shows an example of this.

5.3 Approach to The Future Power Systems of The Greater Bangkok Area

5.3.1 Present Situation of The Transmission System

In the Greater Bangkok Area, there are two thermal power plants at present, namely NORTH BANGKOK (237.5 MW) and SOUTH BANGKOK (1,330 MW). They are connected to the 230 kV transmission lines which encircle the metropolitan area forming three loops.

Power to serve the Greater Bangkok Area is supplied from these two power plants and from this ring of 230 kV transmission lines.

To this ring of 230 kV transmission lines, electric power is sent not only from the above power plants but also from the power plants located in Region 1, such as BANG PAKONG (2,276.6 MW), SRINAGARIND (720 MW), KHAO LAEM (300 MW) and so forth by means of 230 kV transmission lines.

Further more, some of electric power generated at the power plants located in Region 4, namely MAE MOH (2,025 MW), BHUMIBOL (535 MW) and SIRIKIT (375 MW), is sent to the Greater Bangkok Area by means of 500 kV and 230 kV transmission lines.

Substations connected with the 230 kV transmission lines of the Greater Bangkok Area, such as SAI NOI, NORTH BANGKOK, BANG KAPI, BANGKOK NOI, SOUTH BANGKOK, BANG PHLI and RANGSIT, play currently a very important role to collect electric power from the above power plants and send it to the other substations to distribute in the area.

The transmission system composed of these substations and the 230 kV transmission lines can fulfill its function at the present time and will work for several years to come by adopting measures to increase the capacity of the existing facilities, such as the use of twin conductors on the transmission lines and installation of additional transformer banks in the substations.

5.3.2 The Power Demand of The Project Area

Below is the forecast of future power demand of the MEA service area which covers most part of the Greater Bangkok Area.

Fiscal Year		Maximum Power Demand (MW)
1992	3,993	(actual)
1997	6,089	(forecast by the Thai Organization)
2001	7,952	(forecast by the Thai Organization)
2006	10,264	(forecast by the Thai Organization)
2011	13,569	(forecast by the JICA team)

Such a high growth of power demand of the project area needs to construct new substations and transmission lines, but in recent years there are problems to be encountered due to difficulties in the acquisition of land for substations and rights-of-way for transmission lines to be constructed.

There is another problem that some of the substation buses will encounter excessive fault levels for the interrupting capacity (50 kA) of circuit breakers in the not long distant future.

5.3.3 Requirements for The Future Transmission System

The power system must be kept in adequate condition to generate the energy, convey it to the load areas and deliver it to the customers.

It must, at all times, have enough generation available for service, and enough capacity for power transmission and distribution to assure continuous power supply and good voltage to every customer despite planned outages for inspection and maintenance, while at the same time it should be operated so as to realize the maximum economies.

Therefore, as long as loads continue to increase, the power system must also continue to grow providing sufficient capacity of power generation, transmission and distribution for the increasing load.

5.3.4 Approach to The Transmission Expansion Planning

The plan of reinforcement of the transmission system depends on power demand forecast for the area, location and scale of power sources which will be developed in future, possibility for acquisition of new locations for substations and new rights-of-way for transmission lines in the area, consideration to the environmental aspects and reliability criteria to be considered.

The expansion plan of the transmission system in the Greater Bangkok Area has been made based on the load forecasts predicted by the Thai Organization and JICA team and the power development plan of EGAT.

It has been taken into account in the planned transmission system that the system should optimally sustain the voltage and hold a high reliability of power transmission with facilities of sufficient capacity with a view to realizing reduction of the frequency and duration of power outages.

Planning of future power systems has been implemented by the procedure shown in Fig. 5-4. The approach to be taken to transmission expansion planning begins by stepping from the present power system to the horizon year conditions, say about 20 year ahead.

After developing one or some network designs for the conditions and requirements to be considered in the above horizon year, we return to the present power system and move toward the horizon year system in chronological order to study the network growth.

The horizon year expansion plan of the transmission system of the Greater Bangkok Area has been implemented taking the matters of importance into account, namely conditions of the area for installation of facilities, criteria for power system planning, and problems and requirements to cope with. The matters will be described in the following sections in detail.

The basic designs of transmission lines and substations have been developed for each year of 1997, 2001, 2006 and 2011.

Power flow analyses, short circuit current calculation and stability analyses have been carried out for the power systems covering the whole country in order to define the needs of transmission network expansions and reinforcements of the Greater Bangkok Area.

5.4 Criteria for The Transmission System Planning

Power system facilities are planned against a wide range of potential contingencies, in terms of both their steady state and transient state behavior. The planning criteria are comprised in assumptions of such contingencies and their consequences.

The consequence of contingency generally takes the form of the outage of a certain amount of generation or of an entire power plant, the outage of a critical transmission line, the outage of a significant portion of substation or some combination of these outages of power facilities.

To define the power system reinforcements required, a compromise is generally sought between the quality of service and the cost of generation and transmission of electric power.

To assure against a very rare disturbance will involve too great an investment in power supply facilities, as compared to the resulting improvement in the quality of service.

The planning criteria which assume facility outages and are generally adopted to arrange the transmission expansion program vary from utility to utility depending on the state of load density of the area served and the degree of development of its power supply facilities.

Below are the criteria adopted for the transmission system planning in this study:

(1) The voltage variation in the transmission system should be within 98% - 105% of the nominal voltage under normal condition and 92% - 108% under contingency (emergency) condition.

(2) The transmission system should be planned on the basis of a single contingency (n-1) criterion which is widely used in many developed countries, i.e. each system element such as one circuit of a line or one transformer bank can fail separately without causing loss of load and excessive overloads on the remaining equipment.

(3) The bulk power system should be maintained stable under the condition of a permanent three phase fault on any generator or transmission circuit, with normal fault clearing and without reclosing.

The fault clearing times to be used are as follows:

4 cycles	for 500 kV system
5 cycles	for 230 kV system

(4) Fault levels should below 50 kA at any bus bar both in the 500 kV and in the 230 kV transmission system.

5.5 Measures to Cope with Requirements

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The power demand in the Greater Bangkok Area is anticipated to become more than doubled within the next ten years. Due to such a high growth of demand and resulting heavy load flows on the lines, the existing transmission system will not be able to meet the requirements described in 5.3.3 in near future.

Reinforcements of the power system should be urgently implemented to increase the power supply capability, to maintain the system reliability, to improve voltage conditions, and to reduce system losses.

However, EGAT has encountered severe problems on the acquisition of land for substations and new rights-of-way for transmission lines needed to increase supply capability as well as some technical problems concerning excessive fault level and heavy loaded situation on the parallel 230 kV lines.

The measures, to cope with such problems, are envisaged as below.

(1) To increase transmission capacity

Transmission system of higher voltage, say 500 kV, should be introduced into the urban area. It implies installation of 500 kV transmission lines and substations in this area.

Facilities of larger capacity should be adopted. Some of the aged existing facilities will have to be replaced in consistency with this policy. It is recommendable to adopt transformer units

of larger capacity and gas insulated switchgears (GIS) for substations, and bundle conductors for transmission lines.

(2) To secure spaces for facilities

To obtain rights-of-way and land for 500 kV facilities, the existing transmission lines and substations should be replaced.

A space on the existing right-of-way should be examined to use for a new substation.

It should be examined to install compact substations, or underground or building substations. It is recommendable to adopt GIS equipment to make a substation's space smaller.

Equipment adopted should have larger capacity than the existing one to use the space effectively.

Compact 230 kV lines of large capacity should be constructed adopting multi-conductors and multi-circuits in a narrow right-of-way as well.

Underground transmission should be considered if necessary.

(3)

) To solve excessive short circuit levels

Circuit breakers with a larger interrupting current, say 50 kA, will have to be installed. At the least, at substations where fault levels are predicted to exceed the interrupting current rating, the existing circuit breakers should be replaced by breakers with a higher rating.

Operation with the system split is very effective in reducing short-circuit current, so bus sections will be separated by normally open circuit breakers at a few substations.

The system will be divided into two or three load areas which are bounded by circuit breakers and each of which has sufficient load-carrying capability to supply its load.

Introduction of a higher voltage level (500 kV) should be examined in place of the present voltage level (230 kV).

Adoption of high impedance transformers or current limiting reactors is also conceivable.

5.6 Reliability Criteria and Overloading of Equipment

When a transmission system is planned on the basis of an (n-1) criterion, measures below are usually taken to avoid an interruption of power supply at the single contingency.

For example, more than two circuits are designed on a right-of-way to be operated in parallel with each other, or the transmission system is designed to form loops and more than two transformer banks are used in parallel.

However, from an economical point of view, at the single contingency the remaining facilities are generally allowed to be overloaded to some extent, though limited for short duration.

Fig. 5-5 shows an example of overload operation of a transmission line. Two circuits are operated in parallel, being initially loaded with 80% of its capacity each. When one circuit fails, the remaining circuit is loaded with 160% of its capacity for 10 minutes allowed.

The transmission power should be promptly decreased to 120% and in 20 minutes it should be reduced to the level of its capacity 100%.

Fig. 5-6 is an example of overload operation of a transformer in case three banks are used in parallel.

In the event of loss of either one transformer bank or generating unit connected with a lower voltage transmission system, each of the remaining banks which is initially loaded with 80% of its capacity can be overloaded with up to 150%. In 10 minutes, however, the load should be decreased to 120%, and then in 20 minutes it should be finally reduced to its capacity 100%.

Every electric power company in Japan has a standard of overloading operation for an individual transformer. Some of their standards are based on "A guide for operation of oil filled transformers" which has been issued by The Institute of Electrical Engineers of Japan (IEEJ).

The operation limit of equipment is normally determined from overloading capacity for a short duration, say 10-minute in Japan. This time duration is generally recognized as necessary to control load flows by system operation and to avoid stopping service of the remaining facilities due to overload.

5.7 Capacity of The Transmission Lines and Transformer Banks

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The capacity of equipment at the planning stage depends on utility's way of thinking regarding overloading operation of equipment at the contingency. The equipment will be able to get out of the overloaded state by means of network switching, starting up and bearing a load on hot or spinning reserves and so forth.

In this study, the capacity of equipment is regarded as below, which will lead to a conservative design of transmission system.

If load flow is probable to exceed the following level in normal state, measures for reinforcement shall be taken to solve the problem.

(1) Transmission capacity of the overhead lines

Voltage kV	Conductor MCM ACSR	Transmission Capacity MVA
230	1 x 1272	429
	2 x 1272	858
	4 x 795	1,303
	4 x 1272	1,716
500	4 x 795	2,834
	4 x 1272	3,734

a. Transmission capacity of the single-circuit line

b. Transmission capacity of the double-circuit lines

In case of a loss of one circuit due to a fault, the other circuit should uninterruptedly send the same amount of power before the fault.

Therefore a double-circuit line should be treated as having the same capacity as a single-circuit line with the same conductor size.

c. Transmission capacity of the n circuits

Transmission capacity of the n circuits should be (n-1) times the capacity of a single-circuit line with the same conductor size.

(2) Transmission capacity of the underground lines

Underground lines will be used for sending power from substations on the present 230 kV ring to the substations which will be located in a densely populated area where rights-of-way for overhead transmission lines are not possible to be developed.

One circuit of underground cables and one transformer bank should form one unit and its transmission capacity should be determined from the transformer.

The scheme of this transmission system is shown on Fig.5-7.

Underground cables will also be used for the section of the transmission line placed in the vicinity of the airport where a structure to be installed is regulated by the height restriction.

The size and number of cables to be laid should be decided so as to have sufficient transmission capacity for load flows forecast in future.

(3) Maximum loading capacity of the transformer banks

In regard to transmission capacity of transformer banks, overloading operation of transformers should be taken into account in the event of a single contingency.

In this study, the maximum loading capacity and number of transformer banks are designed in principle according to the table below which refers to the guide issued by IEEJ. Following this, in the event of loss of one transformer bank, the remaining transformer banks could bear resulting overload for about 30 minutes.

We recommend, however, EGAT should study guides for operation of transformers in actual use in connection with the maximum loading to give normal life expectancy and according as the guides installation plan of transformers should be made.

ен. Стала <u>—</u>	Installed Capacity	(MVA)	Maximum Loading (MVA)	
	200 x 2		250	
· · ·	200 x 3		480	
	200 x 4	·	690	
· . · · ·	200 x 5		900	
. 12 . 14 	200 x 6		1,100	
t e de	250 x 2		320	
	250 x 3		600	
general de T Tali sua an	300 x 2	······································	380	
	300 x 3		720	
	300 x 4		1,040	
	300 x 5	<i></i>	1,350	
	600 x 2		760	
•	600 x 3	• .	1,440	
	600 x 4		2,080	
_	600 x 5	· · ·	2,700	
	750 x 2		950	
	750 x 3		1,800	
	750 x 4	,	2,580	
	750 x 5	and and a second se	3,370	

A new substation should start with more than two transformer banks and an additional transformer bank should be installed when the integrated load flow of the paralleled transformer banks is probable to exceed the above maximum loading value.

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5.8 The Present Power Supply Capability of The Greater Bangkok Area

The power supply capability of the Greater Bangkok Area is determined by the total capacity of the maximum loading of 230 kV transformers which supply power to the transmission systems of lower voltage level, namely 115 kV and 66 kV, of this area.

Table 5-2 shows the installed capacity and maximum loading of each substation in the area. Correlation between the installed capacity and maximum loading is as described in the previous section 5.7.

It is assumed in this table that when one transformer bank fails, remaining transformer banks can be loaded for a short term with 120% - 130% of the rated capacity until a prompt power flow control removes that overload situation.

In the Greater Bangkok Area, as of 1992, the total installed capacity and maximum loading of 230 kV transformers are 5,500 MVA and 4,100 MVA, respectively.

Supposing a power factor of transformer is 0.9, the power supply capability of this area is about 3690 MW as of 1992.

5.9 Image of the Transmission System in Future

The maximum power demand of MEA area was 3,993 MW in fiscal 1992. It is increasing at a high rate and forecast to be 7,472 MW in fiscal 2,000 and 10,264 MW in fiscal 2006. If an annual growth rate is assumed to be about 5% for farther years, the maximum power demand will exceed 13,000 MW in 2011.

EGAT has to urgently implement the development of power sources and the reinforcement of the transmission system to meet increasing demand.

Power required in the area is supplied by the power plants in this area, i.e. NORTH BANGKOK, SOUTH BANGKOK and BANG PAKONG, and the 500 kV and 230 kV network surrounding this area.

EGAT has a plan to build up 500 kV transmission system which links three substations, NONG CHOK, WANG NOI and SAI NOI outside the 230 kV transmission lines which encircle the Greater Bangkok Area. When this 500 kV link is completed, it will function to supply power to the Greater Bangkok Area together with the existing 230 kV transmission system and the power plants, i.e. SOUTH BANGKOK and BANG PAKONG, which are located in this area and its vicinity.

According to EGAT's power development plan, PDP 92-01(1), which was issued in September 1992, as shown in Table 5-3, the total capacity of power plants connected to 230 kV system of the Greater Bangkok Area will be 5,779 MW as of 2006. It is just about 56% of the forecasted peak demand of the MEA service area for the same year.

Supposing the power demand of the MEA service area after twenty years is a little less than 14,000 MW and power of 4,500 MW to 5,000 MW is supplied from the above power plants, the shortage of 9,000 MW to 9,500 MW must be supplemented by power generated in other areas. It means that such a large amount of power must be sent through the 500 kV transmission network from the power sources to the Greater Bangkok Area and supplied by means of 500 kV/230 kV transformers at the 500 kV substations.

If a 500 kV substation comprises four transformer banks, 1,000 MVA each, the transmission system in and around the Greater Bangkok Area will need four 500 kV substations at least and eight rights-of-way for 230 kV transmission lines with a capacity 1,600 MW each to distribute the above power in this area.

In addition to the Nong Chok substation, EGAT is planning to build two 500 kV substations, SAI NOI and WANG NOI, on the outskirts of the metropolis.

Besides these three substations, however, another 500 kV substation should be installed in order to enhance a power supply capability from the west of the Greater Bangkok Area, and the Bangkok Noi substation is recommended to be strengthened by the introduction of 500 kV for this purpose.

Fig. 5-8 shows a preliminary image of the transmission system of the Grater Bangkok Area in future. The JICA team has developed this image to horizon-year power systems taking account of several factors and requirements peculiar to power system expansion of the area.

5.10 Main Points for Planning Horizon Year Transmission Systems

5.10.1 Expansion of the 500 kV System

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- Here are the matters the JICA team has especially paid attention to for planning the future transmission system of the Greater Bangkok Area.
 - (1) To make a great increase of power supply capability especially to the center of the city.

(2) Only the existing rights-of-way will be available for strengthening the transmission system, because it is extremely difficult or impossible to obtain new rights-of-way, especially inside the existing 230 kV ring.

(3) To control a fault level below 50 kA without losing merits of interconnection between substations as much as possible.

In full knowledge of these matters, the JICA team has examined measures for reinforcement of the transmission system. The plan of the future transmission system of high reliability has been made by introducing 500 kV voltage into the inside of the present 230 kV transmission line loops of the Greater Bangkok Area. The plan has been confirmed as reasonable by the power system analyses.

Besides the before-mentioned four substations, namely WANG NOI, NONG CHOK, SAI NOI and BANGKOK NOI, one or two 500 kV substations will be necessitated in the Greater Bangkok Area in future, if these substations have to supply some power to the substations located on the outside of the project area such as ANG THONG, SARABURI and so forth.

And also, to increase capability of supplying power to the center of Bangkok without obtaining new rights-of way, it will be indispensable to replace the existing line with a 500 kV line to introduce 500 kV system inside the project area.

Short-circuit currents in the transmission system of the Greater Bangkok Area will be effectively reduced by the introduction of 500 kV system and operation with the split of 230 kV system.

5.10.2 Main Points of the Planned Horizon Year Transmission System

The main points of the planned horizon year transmission system are as follows.

(1) Introduction of 500 kV system into the Bangkok Noi substation

It is desirable to increase supply capability from the west side of the Greater Bangkok Area. For this purpose the voltage of 500 kV should be introduced into the Bangkok Noi substation.

To introduce 500 kV into the Bangkok Noi substation, the existing 230 kV SAI NOI - BANGKOK NOI line should be replaced by a 500 kV double-circuit line because it is extremely difficult or rather impossible to obtain a new route for the 500 kV line. The conductor of the line should be ACSR 1272 MCM x 4.

When the 500 kV line is completed, the 500 kV system in the Greater Bangkok Area will be formed linking the Nong Chok, Wang Noi, Sai Noi and Bangkok Noi substations.

(2) Introduction of 500 kV system into the North Bangkok substation

500 kV should be introduced into the North Bangkok substation in order to increase power supply capability for the area which is to be supplied by the North Bangkok, Lat Phrao and Ratchada Phisek substations.

A 500 kV double-circuit line should be installed using the rightof-way of the existing 230 kV SAI NOI - RANGSIT - NORTH BANGKOK line for this purpose.

The 500 kV line will connect the two substations, SAI NOI and NORTH BANGKOK, directly, because the Rangsit substation is not large enough to install necessary 500 kV equipment to connect with the 500 kV system.

In the section between the Rangsit substation and North Bangkok substation, the structures of the line should be equipped with four circuits, a 500 kV double-circuit and 230 kV double-circuit, except for a restricted area on the height of structures between the Rangsit substation and Chaeng Wattana substation in the vicinity of the Don Muang airport.

In this area, the structures are restricted below 45 meters in height and so should be equipped with a 500 kV double-circuit only. Therefore, for the 230 kV line, underground cables will have to be used.

The 230 kV double-circuit placed in juxtaposition with the 500 kV double-circuit should be connected with the Rangsit substation, Chaeng Wattana substation in the course of construction, a proposed substation " A ", and the North Bangkok substation.

Conductors ACSR 1272 MCM x 4 should be used for the 500 kV line and also for the 230 kV line in the section of overhead transmission. For the section of underground transmission, cross linked polyethylene cables with load carrying capability of about 600 MW per circuit will be used as the initial scale. In future, however, additional cables should be laid in accordance with the increase of power demand at the Chaeng Wattana substation.

It is desirable that the present 230 kV single-circuit line between BANGKOK NOI and NORTH BANGKOK is replaced by a 500 kV line regarding reliability of the system and flexibility of system operation.

The 230 kV double-circuit should be placed in juxtaposition with the 500 kV double-circuit between the North Bangkok substation and the substation " F " (TALINGCHAN) which will be installed in around 2010.

(3) Installation of a new 230 kV substation " A "

A new substation " A " will be installed at the spot where the 230 kV line to the Lat Phrao substation is branched by 1 pi (π) connection from the RANGSIT - NORTH BANGKOK line at present.

The 230 kV transmission lines should connect this substation with the Chaeng Wattana, North Bangkok and Lat Phrao substations. That will balance power flow of each circuit and increase loading capability of the lines especially to the Chaeng Wattana and Lat Phrao substations.

In addition, the installation of the A substation will make it easier to develop routes of transmission lines to send power to the substations which will be built in a populated area in future.

(4) Reinforcement of the NONG CHOK - ON NUCH line

In order to increase power supply capability of the Nong Chok substation, the present 230 kV line between the Nong Chok and On Nuch substations should be reinforced with a four-circuit line, the conductor of which will be ACSR 1272 MCM x 2.

(5)

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) Installation of a new substation " C ", and reinforcement of the BANG PAKONG - NONG CHOK and BANG PAKONG - ON NUCH Lines

In addition to reinforcement of the NONG CHOK - ON NUCH line, a new 500 kV substation " C " should be installed at the crossing where the BANG PAKONG - NONG CHOK line and the BANG PAKONG 2 - ON NUCH line meet, and the existing 230 kV lines should be reinforced in the sections between C and the On Nuch substation and between C and the Nong Chok substation.

This will increase capability and reliability of power supply to the eastern area of Bangkok, which is to be supplied from ON NUCH, BANG KAPI, CHIDLOM and new substations, H and B, which will be installed in future.

One of the 230 kV transmission line (double-circuit) which run from the Bang Pakong power station to the Nong Chok substation should be replaced in the section of NONG CHOK - site of C by a 230 kV four-circuit line which will be connected to the existing lines coming from the Bang Pakong power station.

The other 230 kV transmission line constructed between the Bang Pakong power station and the Nong Chok substation should be replaced in the section of NONG CHOK - C by a 500 kV-designed transmission line and should be pulled into the C substation.

The present 230 kV BANG PAKONG - ON NUCH line should be pulled into the C station as well to form a pass of power flow from NONG CHOK to ON NUCH together with the above 500 kV-designed transmission line by way of the C station. 500 kV will be introduced into the C substation in around 2010.

The 230 kV double-circuit transmission line between the On Nuch and C substations should be replaced with four circuits using the conductor ACSR 1272 MCM \times 2.

The present right-of-way of this line is so adjacent to the proposed site of a new international airport that the line route will have to be moved to avoid the area controlled by the regulation concerning height restriction of structures built around an airport.

Otherwise it will be necessary to lay underground cables instead of an overhead line near the site of the airport. In this case, cross linked polyethylene cables with load carrying capability of about 600 MW per circuit will be laid as the initial scale and an additional cable will be laid in accordance with the increase of power flow of the line.

(6) Power supply to the Rangsit area and its vicinity

In order to increase capability of power supply to the Rangsit area, one more substation, e.g. RANGSIT 2, will be necessary. Installation of the new substation should be examined concerning 115 kV and 69 kV transmission system, i.e. capacity of the present lines, possibility of their reinforcement, acquisition of rights-of-way of new lines from the existing substation to the distribution substations.

230 kV four circuits using ACSR 1272 MCM x 2 should be installed between WANG NOI and RANGSIT. These circuits will assure power supply with high reliability together with the other 230 kV NONG CHOK - RANGSIT line.

(7) Installation of substations in populated areas

In order to increase power supply capability for densely populated areas, new 230 kV substations G, H, and J should be installed.

The final scale of the transformer banks which supply power to the secondary voltage 115 kV or 69 kV of these substations should be 300 MVA x 3 or 4 banks.

Power will be supplied to these substations from the key stations such as, A, BANG KAPI, SOUTH THONBURI and BANGKOK NOI by 230 kV underground cables.

The transmission system should adopt unit system in which the above substations are not equipped with circuit breakers and bus bars at the side of 230 kV transmission lines so as to be simply and compactly designed as shown on Fig. 5-7.

The capacity of 230 kV cable used should correspond to the capacity of transformer bank.

Replacement of the 230 kV BAN PONG 2 - SAI NOI Line by a 500 kV Double-circuit Transmission Line

A 500 kV transmission system will have to be constructed to send power from the power plants located in the western seaboard and/or southern seaboard to Sai Noi substation. To secure a right-of-way for the transmission system, the existing 230 kV BAN PONG 2 - SAI NOI line should be replaced by a 500 kV transmission line.

That is also effective to control an increasing fault level at the 230 kV bus of the Sai Noi substation.

(9)

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Reinforcement of the 230 kV BANGKOK NOI - SAM PHRAN 1 - SOUTH THONBURI line

The above transmission line will be heavily loaded as demand for power increases in the areas situated to the southwest of the Greater Bangkok Area. Reinforcement of this line will be necessary about the middle of 2000s.

The single circuit between BANGKOK NOI and SAM PHRAN 1 and also the one between SAM PHRAN 1 and SOUTH THONBURI should be strengthened with two circuits of 230 kV lines using a conductor ACSR 1272MCM x 4.

In the section between SAM PHRAN 1 and the present right-of-way of the BANGKOK NOI - SOUTH THONBURI line, structures of the line will have to be equipped with four circuits because of only one right-of-way available.

It is recommended the line which links directly between BANGKOK NOI and SOUTH THONBURI is reinforced with a conductor ACSR 1272MCM x 4.

5.10.3 Description of the Study Cases of a Horizon Year Transmission System

For the study on a 2011 year (a horizon year) transmission system of the Greater Bangkok Area, the JICA team has supposed several cases with regard to power sources and connection of transmission lines.

Figs. 5-9 and 5-10 are typical power flow diagrams obtained as a result of the study on a horizon year power system.

In Case 1, power sources are developed mainly in the western seaboard and southern seaboard, while in Case 2, power sources are developed in the eastern seaboard and western seaboard almost equally. In either case there will be many rights-of-way necessary for the 500 kV lines to send power from the sources to the Greater Bangkok Area.

Table 5-4 shows the study results of fault levels at the 230 kV bus of each substation in the Greater Bangkok Area.

The transmission system shown as Fig.5-11 will be fundamentally adaptable to the future requirements of power supply, reliability and fault levels, irrespective of configuration of power sources developed in future.

In case most of the power sources are developed in the western and/or southern areas, the 500 kV transmission system between SAI NOI and WANG NOI will need three circuits due to the heavy load flow.

Tables 5-5 and 5-6 show transmission lines and transformer banks and line equipment of the substations respectively which are proposed to be installed or reinforced to form the 2011 year transmission system of the Greater Bangkok Area.

Fig. 5-12 shows the transmission systems of the Greater Bangkok Area at present and in horizon year.

Tab!e 5 • 1

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POWER DEVELOPMENT PLAN AND TRANSITION OF POWER SUPPLY CAPABILITY OF THAILAND

			Rated			ed Installed	Capacity		P 92-01(1) Peak
Fiscal Year	Developed Power Plant	Fuel,Type			Regioni	Region2	Region3	Region4	Gonerati
			(MW)	(MW)	(MW)	(MW)	(MW)	(MW)	(MW)
1991	Existing			9,610.3	5,550.3	378.3	611.3	3,070.4	8,045
1992	Rayong cc Block 1(ST) Unit 1	Gas	102	9,712.3	5,652.3				
•	Bang Pakong Unit 3	Oll/Gas	600	10,312.3	6,252.3				l
	Bang Pakong cc Block 3 (ST) Unit 1	Gas	99	10,411.3	6,351.3		1.1.1.1.1.1.1		i i
1. A.	Rayong co Block 2 (ST) Unit 1	Gas	102	10,513.3	6,453.3				
	Bang Pakong cc Block 4 (ST) Unit 1 Rayong cc Block 3 (ST) Unit 1	Gas	99	10,612.3	6,552.3				
		Gas Gas	102 113	10,714.3 10,827.3	6,654.3	491.3			ĺ
	Nam Phong cc Block 1 (ST) Unit 1 Rayong cc Block 4 (GT) Unit 1-2	Gas	206	11,033.3	6,860.3	491.5			9,000
1993	Bang Pakong Unit 4	Oil/Gas	600	11,633.3	7,460.3			·····	9,000
1335	Nam Phong cc Block2 (GT) Unit 1-2	Gas	242	11,875.3	7,400.3	733.3			
	South Bangkok cc Block1(GT) Unit 1-2	Gas	220	12,095.3	7,680.3	100.0			1
	Rayong cc Block 4 (ST) Unit 1	Gas	102	12,197.3	7,782.3				9,924
1994	R2 Gas Turbine Retired	Gas	-28	12,169.3		705.3			0,024
	Khanom cc Block 1(GT) Unit 1-4	Gas	448	12,617.3		10010	1,059.3		1
	Nam Phong cc Block2 (ST) Unit 1	Gas	113	12,730.3		818.3	1,000.0		
•	Pak Mun Unit 1-2	Hydro	68	12,798.3		886,3			i
	South Bangkok cc Block1(ST) Unit 1	Gas	115	12,913.3	7,897.3				1
	Khanom cc Block 1(ST) Unit 1	Gas	226	13,139.3			1,285.3		10,89
1995	Pak Mun Unit 3-4	Hydro	68	13,207.3		954.3			
	Sirikit Unit 4	Hydro	125	13,332.3				3,195.4	
	South Bangkok cc Block1(GT) Unit 1-2	Gas	400	13,732.3	8,297.3				
	Mae Moh Unit 12	Lignite	300	14,032.3	-			3,495.4	11,94
1996	R3 Gas Turbine Retired	Gas	70	13,962.3			1,215.3		
	Krabl Reilred	Lignite	-34	13,928.3			1,181.3		
	Mae Moh Unit 13	Lignite	300	14,228.3				3,795.4	ł
	Bhumibol Unit 8	Hydro	175	14,403.3				3,970.4	
	Wang Noi Gas Turbine	Oil/Gas	600	15,003.3	8,897.3				13,07
1997	Mae Kham F8C Unit 1	Lignite	150	15,153.3			· ·	4,120.4	
	Kaeng Krung Unit 1-2	Hydro	80	15,233.3			1,261.3	-	
1	Lower Central cc Block1	Gas	600	15,833.3	9,497.3		•		
	South Bangkok cc . Block2(ST) Unit 1	Gas	200	16,033.3	9,697.3				
	Mae Kham FBC Unit 2	Lignite	150	16,183.3				4,270.4	
	Lower Central cc Block2	Gas	600	16,783.3	10,297.3				14,20
1998	Lam Takhong Unit 1-2	Hydro	500	17,283.3		1,454.3			
	Lower Central cc Block3	Gas	600	17,883.3	10,897.3				15,35
1999	Ao Phai Unit 1	Oil/Çoal	700	18,583.3	11,597.3				
•	Surat Than! Unit! Retired	Oil	-30	18,553.3			1,231.3		
1.000	Mae Lama Luang Unit 1-2	Hydro	- 160 -	18,713.3				4,430.4	
. :	Ao Phai Unit 2	Oil/Coal	700	19,413.3	12,297.3	·			16,53
2000	Ao Phai Unit 3	Oil/Coal	- 700	20,113.3	12,997.3				
	New Thormal Unit 1	Oil/Coal	1000	21,113.3	13,997.3				17,76
2001	Region 3 cc Block1	Gas	300	21,413.3			1,531.3		
	Mae Taeng Unit 1-2	Hydro	26	21,439.3	, i i i i i i i i i i i i i i i i i i i			4,456.4	
	New Thermal Unit 2	Oil/Coal		22,439.3	14,997.3				19,00
2002	Lampang Unit 1	Lignite	300	22,739.3				4,756.4	
	Lam Takhong Unit 3-4	Hydro	500	23,239.3		1,954.3			1
	Lampang Unit 2	Lignite	300	23,539.3		.		5,056.4	1
1	Lampang Unit 3	Lignite	300	23,839.3				5,356.4	20,21
2003	Bang Pakong cc Block 1 Retired	Gas	-380.3	23,459.0	14,617.0				1
	Lan Krabu Gas Turbine Retirad	Gas	-140	23,319.0				5,216.4	
· · ·	Lampang Unit 4	Lignite	300	23,619.0				5,516.4	i i
	Region 3 cc Block2	Gas	. 300	23,919.0			1,831.3		
	New Thermal Unit 3	Oil/Coal	1000	24,919.0	15,617.0				1
	Lampang Unit 5	Lignite	300	25,219.0				5,816.4	1
	Nam Khek Pumped-Storage Unit 1-2	Hydro	300	25,519.0				6,116,4	
	Lampang Unit 6	Lignite	300	25,819.0				6,416.4	21,48
2004	North Bangkok Unit 1-3 Retired	OII	-237.5	25,581.5	15,379.5				1
	Bang Pakong cc Block 2 Retired	Gas	-380.3	25,201.2	14,999.2				1
1.111	Mae Moh Unit 1-2 Retired	Lignite	-150	25,051.2				6,266.4	1
44 1.4.14 1.4.14	New Thermal Unit 4	Oil/Coal	1000	26,051.2	15,999.2			1. T	1
	New Thermal Unit 5	Oil/Coal	1000	27,051.2	16,999.2	·····			22,79
2005	New Thermal Unit 6	Oil/Coal	1000	28,051.2	17,999.2				
	Lampang Unit 7	Lignite	300	28,351.2				6,566.4	
	Lampang Unit 8	Lignite	300	28,651.2				6,866.4	24,15
2006	Nuclear Unit 1	Nuclear Nuclear	1000	29,651.2			2,831.3		
	Nuclear Unit 2	Auchar	1000	30,651.2			3,831.3		25,51

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			As of 1992
		Transformer Banks	
Substation	Voltage (kV)	Installed Capacity (MVA)	Max. loading (MVA)
North Bangkok	230/72.5	1 x 200 3 x 33.3	135
BANG KAPI	230/69	3 x 200	480
BANGKOK NOI	230/69 '	2 x 200 6 x 33.3	480
SOUTH BANGKOK	230/72.5 230/115	4 x 200 1 x 200	690 200
BANG PHLI	230/69 230/115	2 x 200 2 x 200	250 250
LAT PHRAO	230/69	3 x 200	480
RANGSIT	230/72.5 230/115	3 x 200 1 x 200 1 x 100	480 135
NONG CHOK	230/115	1 x 200	200
CHIDLOM Total	230/69	2 x 250	320
Total	<u>ا ا</u>	5,500	4,100

Table 5-2 CAPACITY OF TRANSFORMER BANKS AT 230KV SUBSTATIONS IN THE GREATER BANGKOK AREA

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Table	5	- 3	CAPACITY		τμε	
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OF THE POWER SOURCES IN THE GREATER BANGKOK AREA

Power Plant	Existing (as of 1991) (MW)	Additional Installation (MW)	Retired (MW)	Total (as of 2006) (MW)
North Bangkok	237.5	0	237.5	Ó
South Bangkok	1330	335 (Combined Cycle Block 1) 600 (Combined Cycle Block 2)	0	2265
Bang Pakong	2276.6	198 (Combined Cycle Block 3-4 Steam) 2 x 600 (Thermal Units 3-4)	760.6	2914
Wang Noi	-	600 (Gas turbinə)	-	600
Total	3844.1	2933	998.1	5779

Table 5 - 4

COMPARISON OF THREE-PHASE SHORT CIRCUIT CURRENTS OF THE 2011 YEAR SYSTEMS REGARDING POWER PLANT CONFIGURATION

	Case 1	Case 2
230kV bus	kA	kA
SAI NOI	24.9	25.4
WANG NOI	44.9	47.2
BANGKOK NOI	44.6	44.3
NONG CHOK (bus A)	44.7	48.8
NONG CHOK (bus B)	22.8	23.3
NORTH BANGKOK	30.1	30.6
С	40.5	42.9
A Distance	26.9	27.2
RANGSIT	26.6	27.3
LAT PHRAO	25.2	25.6
RATCHADA PHISEK	29.3	30.7
BANG KAPI	36.6	38.9
ON NUCH	41.7	44.6
BANG PHLI	32.0	33.6
SOUTH TONBURI	37.9	37.8
SOUTH BANGKOK	35.2	35.1

Note

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The 230 kV system is split at CHAENG WATTANA, RATCHADA PHISEK, KHLONG MAI, BANG PHLI and NONG CHOK as shown on Fig.s 5-9 and 5-10.

Case 1 : Power sources are developed mainly in the western seaboard and southern seaboard areas.

Case 2 : Power sources are developed in the eastern seaboard and western seaboard areas almost equally.

Table 5 - 5 REINFORCEMENT OF TRANSMISSION LINES IN THE GREATER BANGKOK AREA

	I ransm.	I ransmission lines		2001	2 7441 393181						
ź	From	10	Length (km)	Voltage (kV)	No. of Circuits	Conductor n x MCM	Length (km)	Voitage (kV)	No. of Circuits	Conductor n x MCM	Remarks
58	WANG NOI	NONG CHOK					64	500	2	4 x 795	500kV line construction
28	SAI NOI	WANG NO	•	•	•		56	500	2	4 x 795	500kV line construction
Γ	BANG PHLI	BANG PAKONG	44.1	230	2	2 x 1272	•	•	r	•	
2 6	BANG PHLI	D (BANG BOR!)	•	,	•		17.5	230	(N	2 × 1272	Ê
26	D (BANG BOH)	BANG PAKONG	,			-	27.5	230	~	2 x 1272	$12 \text{ pi} (\pi) \text{ connection at D}$
22	ONNOH	BANG PHU	10.5	230	N	1 × 1272	10.5	230	2	2 x 1272	Change to the bundle-conductor
15	ONNCH	BANG KAPI	-	230	N	2 × 1272	10	230	+	2 X 1272	Increase of the number of circuits
	CONNUCH	BANG KAPI	10	230	ev.	2 x 1272	0	230	N	2 x 1272	
16	B (PATANAKARN)	BANG KAPI	-	1	'	•	۰ ۲	230	5	2 x 1272	New line construction for the new substation
[LAT PHRAO	BANG KAPI	10.4	230	~	2 x 1272	•			-	
	LAT PHRAC	RATCHADA PHISEK	•	•			4.5	230	~	2 × 1272	2 pi (x) connection at RATCHADA PHISEIX
	RATCHADA PHISEK	BANG KAPI		•		•	6.5	230	2	2 x 1272	2 pi (x) connection at RATCHADA PHISEIX
	SOUTH BANGKOK	BANG PHL	15.9	230	N	2 x 1272	,		•		
7	SOUTH BANGKOK	E (TEPARAK)	•	•	•		11.5	230	ŝ	2 x 1272	2 pi (π) connection at E
27	E (TEPARAK)	BANG PHU	•	•	•	•	5.5	230	N	2 x 1272	2 pi(π) connection at E
[NONG CHOK	BANG PAKONG 2	42.3	230	N	2 x 1272					
24	NONG CHOK	BANG PAKONG 2	,	•	•		÷.	230	~	2 x 1272	Change of a line connection
23 25	NONG CHOK	BANG PAKONG 2					55	230	(1	2 × 1272	Change of a line connection
Γ	XCHC UNCN	KHLONG MA	34,3	230	N	2 x 1272	•			•	
	SCHO UNCN	c	,				đ	200	~	4 × 1272	500kV line construction using the right-of-way of the axisting 230kV ine
					•		, v			0 × 1070	
T		RANG PAKONG 2	4	090		2 X 1279	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	, , , , , , , , , , , , , , , , , , ,			1.1
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T	NU CAO UN	DANC DAKONO	,	0.50		0.1070		000		5 × 1275	
T	VICTOR WH			000		2101 2 2	•	202	 -	277 V 2	
	SAL NOI	NORTH BANGKIN	0.42	020	N -	2/21 X 2		• . •		•••	
	LOOMAL				•	+ + 1775	,				
	HANGSII		2.	0.00		2/21 X 1		•	•	•	
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					3	n —					
	CHAENG WALLAWA		•		•	•			v	4 1 1/2	
 юн	< •	NOHIH BANGKOK	•		•	•	4 6	200	N ¢	2/21 2 4	
	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~		4	0.00		0.201 2 0				1070	finances of the humber of analyse
100			10.00	000		1975	200	200	Contraction of the local division of the loc	5 0 15/5 6 0 0 3 3 3	A particular of the second
	ICH INS		30.5	0.00		0 1070	300	500	-	4 × 1275	500kV line construction steine the victoretway of the existing 230kV line
, . , .				000	, 	1 1 1 2 7 2	1 8 1		1 0	4 \ 1270	Ennky line construction restor the right-of-way of the existing 2304V line
 t		C THE INCOMENT		2	- 1	+/3) V -	1 6	0000		64.01 2 6	poor in construction for the new enterstice
T,		- I I.					2		,	0 ~ 1070	
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Ť,		2 ISONOL					, , ,	222	u t	2/21 / 2	
5,5	ENNEXCX NO	CAM PHHAN I				2/21 X 2		230		4 X 12/2	Sunsixe eus
•••••	SAM PHRAN	SOUTH THONBURN	19.8	230	-	2/21 X 2	19.61	022	N	4 X 1272	Heimorcement of the existing ine
	BANGKOK NOI	SOUTH THONBURI	8	230	~	1 x 1272	8.1	230	-	4 x 1272	Reinforcement of the existing line
	×.	G (SANAMPAO)	•	•	•	•	<b>9</b> 2	230	\$	Cable	New line construction for the new substation
	SOUTH TONBUR	I (THANONTOK)	•	•	r.	 -	0	230	4	Cable	New line construction for the new substation
	BANGKOK NOI	(INUGNOURI)	•	. •	•	•	F	230	0	Cable	New line construction for the new substation
-					-	-	•				

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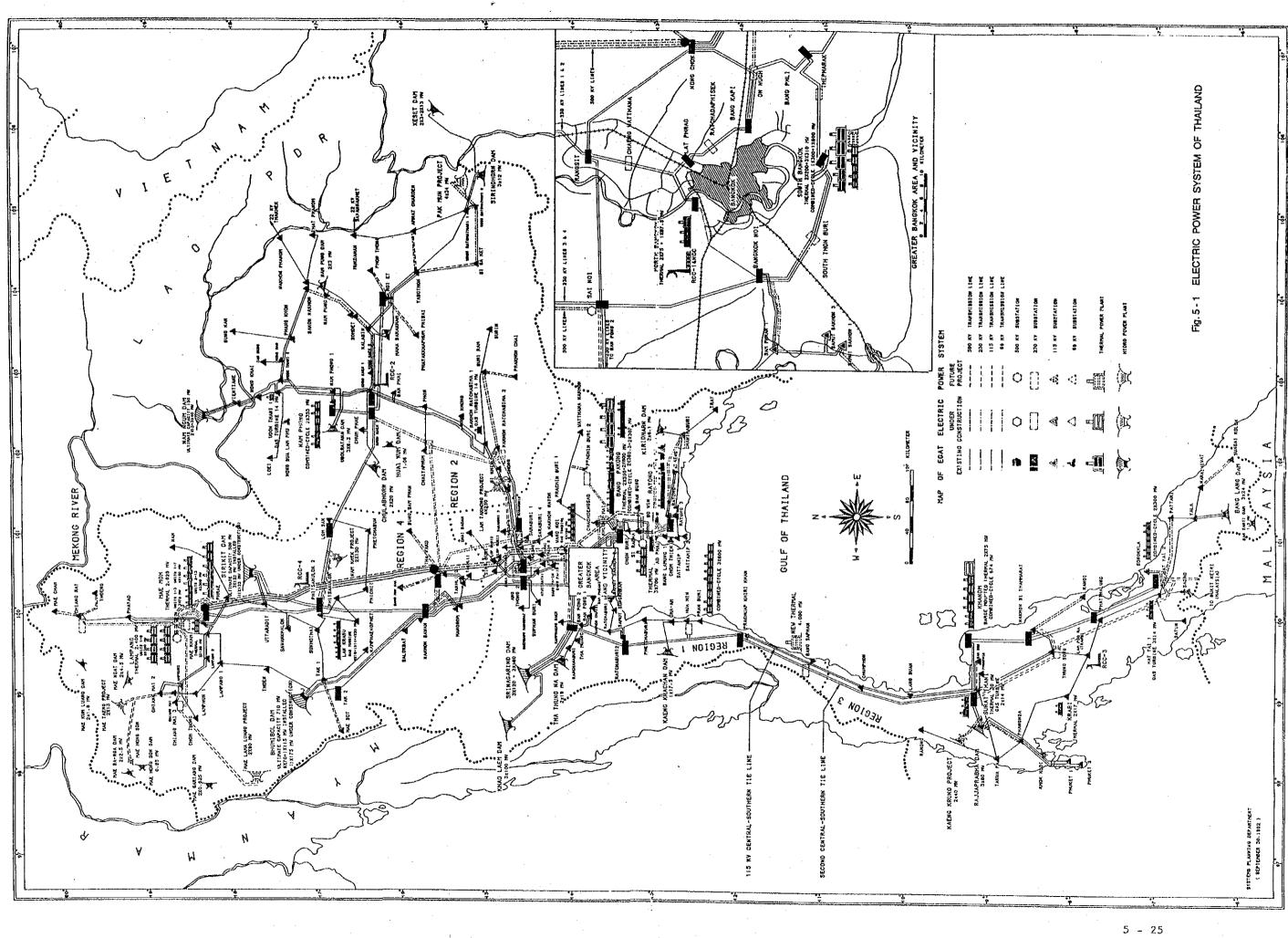
CONSTRUCTION PLAN OF SUBSTATIONS FOR POWER SYSTEM REINFORCEMENT IN THE GREATER BANGKOK AREA Table 5 - 6

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			1992 year system	(Stern	1				ZUTI Year system		
	Line	equipment		Transformer			õ		Transformer		Ind. peak
Substation	Voltage (kV)		Voltage (kV)	Capacity (MVA)	Max. loading (MVA)	Voltage (kV)	No. of Circuits	Voltage (kV)	Capacity (MVA)	Max. loading (MVA)	(MVA)
NONG CHOX	500	- 1	500/230	2x600	760	500	8	500/230	2x600 + 2x750	2270	
	230	2	121/022		200	230		011/052	3X3UU	120	670
WANG NO	1 1	•••	•: •			230 230	2 4	062/004	4 X /50	2080	1
SAI NOI		•				500	14 - 16 - 4	500/230	4 x 750	2580	
-	230	•	•	-	· •	230	2	230/115	4 × 200	690	511
						500	4	500/230	5X750	3370	
BANGKOK NOI	230	60	230/69	2x200 + 2x100	480	230	G	230/69	3x200 + 2x100	690	565
NCHENNA HERMA			G11/062	Z X 200	062	500	4	511/115 500/230	3 X 200	480 2580	480
VOUNNE LIVON	230	e7	230/72 5	1 x 200 + 1 x 100	135	230	+ vo	230/72.5	3x200+1x300	720	712
U				1		500	0	500/230	4 x 750	2580	
	•	•		•	-	230	6		•	•	
BANG KAPI	230	. 8	230/69	3 x 200	480	230	18	230/69	6 x 200	1100	973
BANG PHLI	230	9	230/69	2 × 200	250	230	9	230/69	3 x 200	480	481
			230/115	2 x 200	250			230/115	3 x 200	480	474
CHIDLOM	230	N N	230/66	2 x 250	320	230	N	230/66	2 x 250	320	343
CHAENG WATTANA			-	-		230	4	230/115	Q	1040	777
LAT PHRAO	230	. 4	230/69	3 x 200	480	230	4	230/69	4 × 300 1	1040	777
ON - NUCH	,	•	•	1	-	230	16	230/115	4 × 300	1040	1063
	-	•	•	•		230	12		4	•	-
RANGSIT '3	080	a	230/72.5		480	000	o	230/72.5	5 × 300 5 × 300	1350	1133
DATCHADA DUICEN	200	0	C11/007	001 X 1 + 007 X 1	00	000	• •	001000	0 4 300	Dec:	/ <del>+</del>
HAICHAUA PHINER	0.52		• .	•		230	4	230/115	3 X 200	480	4/9
SOUTH BANGKOK	230	5	230/72.5	4 x 200	690	230	5	230/72.5	5 x 200	006	893
		,	230/115	1 × 200	200			230/115	3 X 200	480	220
SOUTH LONBURI	230	0	-	-		052	2,	C.2///22	4 X 200	690	209
B (PAIANAKAHN)	ı 		,	1	ı	230	4	230/66	006 X 8	720	477
D (BANG BOR)	  -	,  -				230	4	230/115	3 × 300	720	647
H (KHLONG TOEY)		•		-		230	9	230/66	3 x 300	720	444
							•	230/115	3 x 300	720	401
F (TALINGCHAN)		-	-	-	-	230	2	230/115	3 x 300	720	581
E (TEPARAK)	,	1	,	•		230	ষ	230/66	3 × 300	720	469
			-	1	,			230/115	3 x 300	720	498
I (THANONTOK)	,	•	1	1	-	230	4	230/56	4 × 300	1040	793
J (THONBURI)	,	1	•	•	•	230	ო	230/66	3 x 300	720	601
G (SANAMPAO)	•	,	1	,	1	230	9	230/66	3 × 300	720	467
	~							211/052	3 X 300	120	438
SAM PHRAN 1	230	~		•		230	و م	230/115	5 × 200	000	

1 The transformer banks should be replaced by larger ones.
2 Two circuits of eight are for the power source developed following the Ao Phai project.
3 It is required that the substation load which includes PEA's load is divided into two or three, and new substations are constructed in future.
4 Number of circuits depends on the development of the power sources in the west and south.
5 Two circuits of six are for a future-built substation, e.g. SAMUT SAKHON 3.

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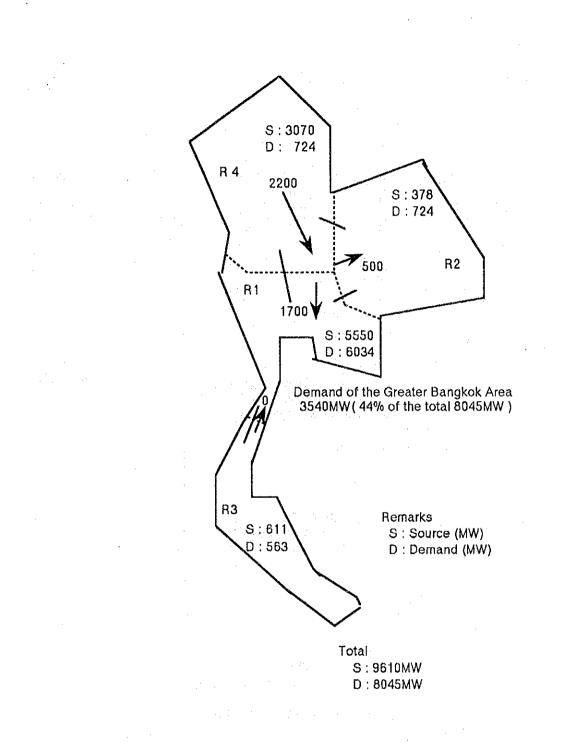
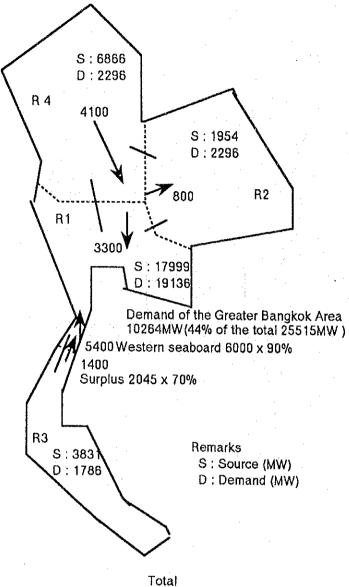


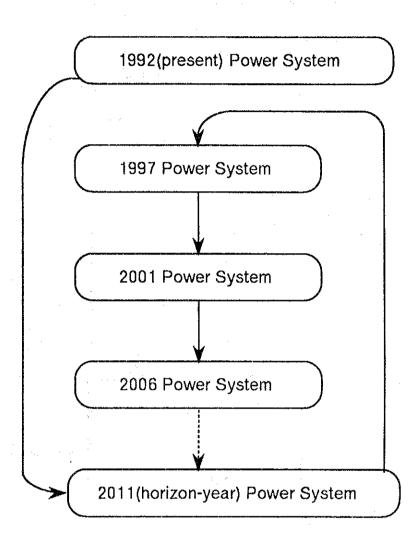
Fig. 5 - 2 ESTIMATED POWER TRANSMISSION AMONG REGIONS IN 1991



S: 30651MW D: 25515MW(Thai estimation)

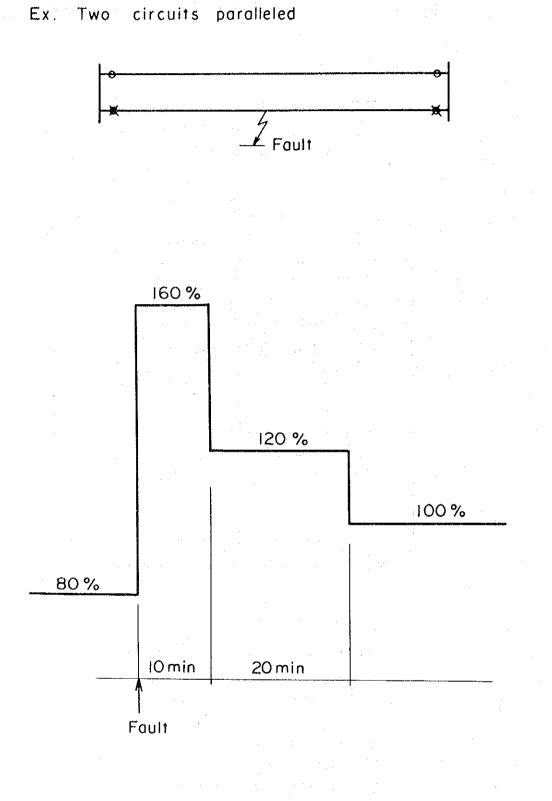
Fig. 5 - 3

ESTIMATED POWER TRANSMISSION AMONG REGIONS IN 2006

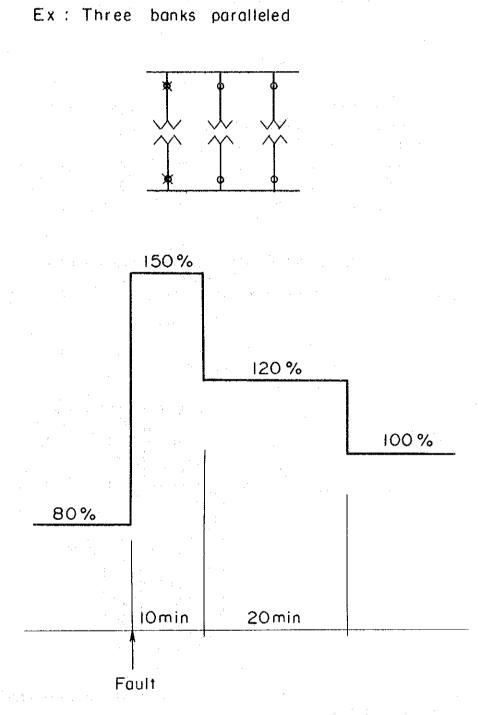


Factors for future power system planning

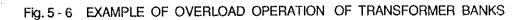
- 1 Power demand forecast
  - 2 Power development plan
  - 3 Capacity of equipment
  - 4 Short circuit current
  - 5 Power system stability
  - 6 Reliability of power supply
  - 7 Environmental restrictions

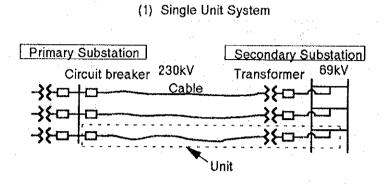


# Fig. 5 - 5 EXAMPLE OF OVERLOAD OPERATION OF A TRANSMISSION LINE



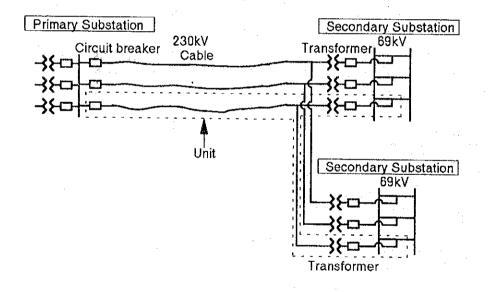
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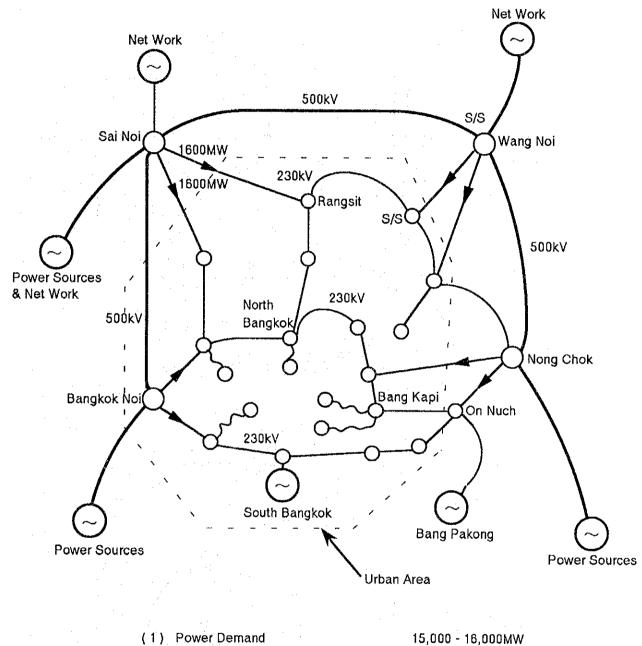


- 1. Load of the secondary substation should be restricted so as to supply power continuously even at a fault of one unit.
- 2. The system has high reliability due to its simplicity.





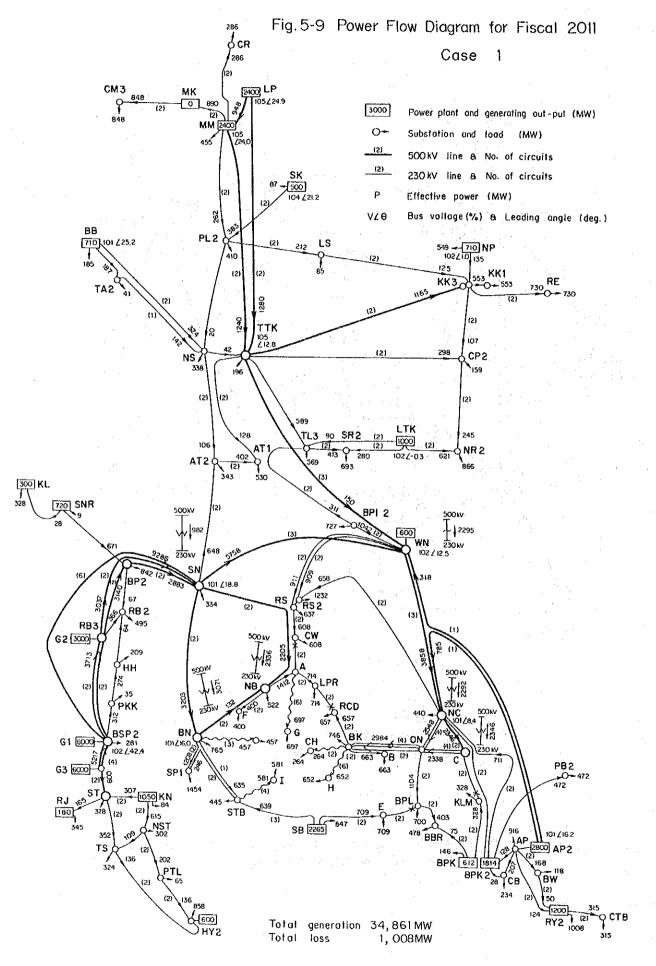
- 1. The number of secondary substations which are comprised in a unit should bematch the capacity of the cable.
- 2. At a fault of a unit, transformers which belong in the fault unit stop operation simultaneously.
- 3. Load of the secondary substations should be restricted so that at a contingency the same amount of power as before the fault can be supplied continuously.



	~	10,000 10,00010144
(2) Supply From T	he 230kV System	4,000 - 5,000MW
(3) Supply From T	he 500kV System	10,500 - 12,500MW
= ( 1 ) - ( 2 )		

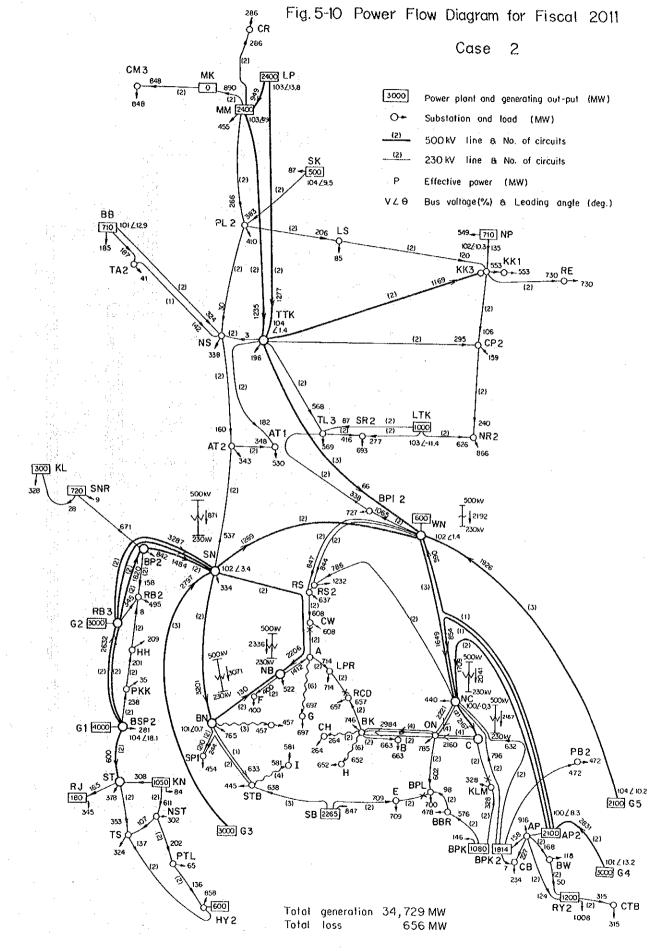


PRELIMINARY IMAGE OF THE FUTURE TRANSMISSION SYSTEM OF THE GREATER BANGKOK AREA (AFTER 2011)



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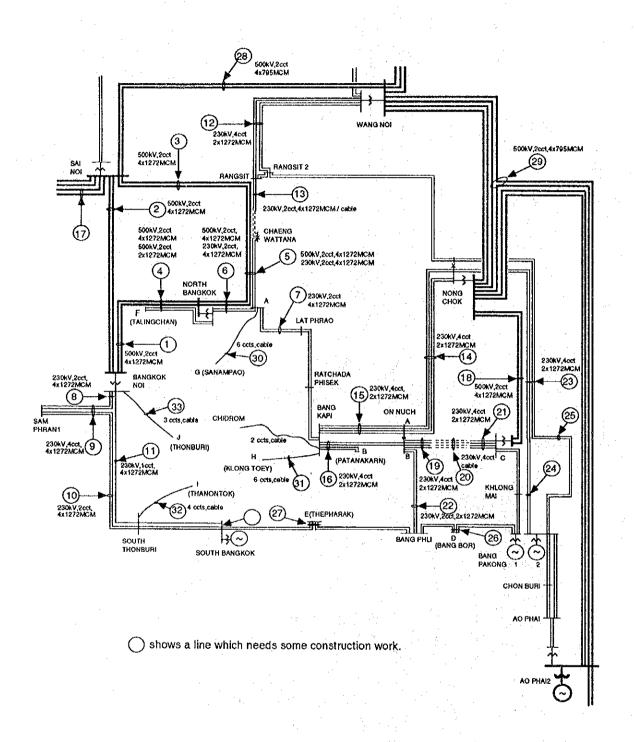
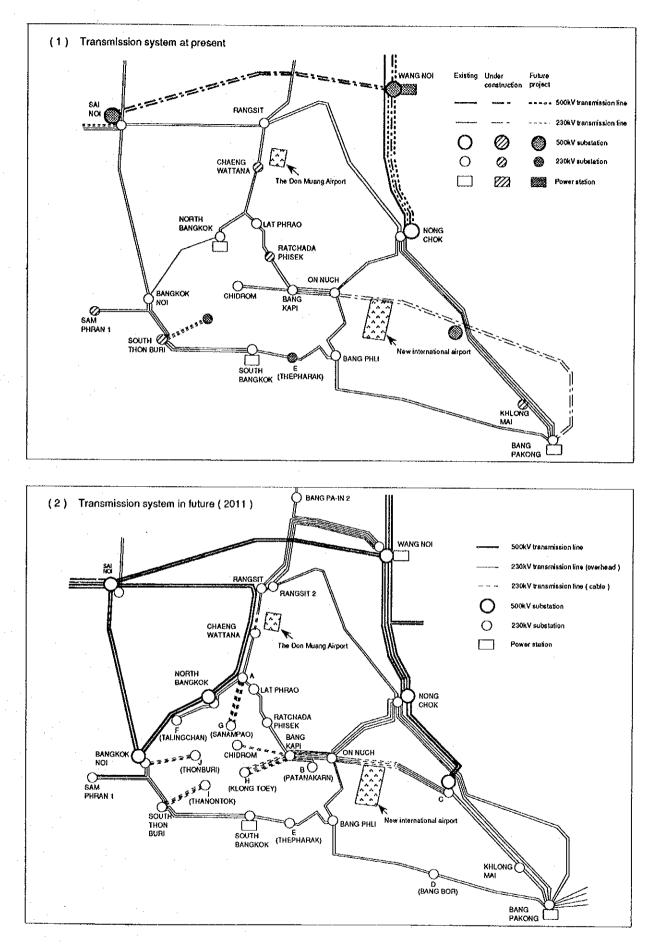


Fig. 5-11 TRANSMISSION SYSTEM OF THE GREATER BANGKOK AREA AFTER 2011





**CHAPTER 6** 

POWER SYSTEM ANALYSIS

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### 6.1 Conditions of Analysis

(1) Fiscal Year under Study

Year 1997, 2001, 2006, 2011

Network System of Each Year under Study

(2)

Year 1997, 2001, 2006

The existing plans for expansion of the power system, which has been formulated by EGAT are reviewed and investigated. Investigations are focused on the capacity appraisal of transmission lines and transformers, and in reducing the short circuit current level, and maintaining power system stability.

Load flow, short circuit current and power stability analysis have to be carried out for the whole EGAT system in each studied year in order to identify the needs of transmission network expansions and reinforcements.

Year			Single Line Diagram Impedance Map
Year	2001	Fig.6-1-3	Single Line Diagram and Impedance Map
Year	2006	Fig.6-1-4	Single Line Diagram and Impedance Map
Year	2011		

The 2011's network system is assumed to be based on expanded 2006's network system. However, the power development will be required because of increasing power demands. According to latest EGAT's Power Development Plan (PDP 92-01), the new power plants from 2006 to 2011 are assumed that four units of nuclear power plant rated 1000MW each will be located in the southern part of Thailand, that is located at same site as Nuclear Unit 1-2.

(3) Load Forecast at each substation

Table 6-1-1 shows system peak load and MEA peak load of each substation in Thailand. This load forecast is formulated by EGAT. The load factor of system peak is 85% at each substation.

(4) Transmission System Planning Critera of EGAT

- a) The steady state system voltage at any busbar in transmission system should be 98-105% of the nominal voltage under normal condition and 92-108% under contingency (emergency) condition.
- b) The transmission system must be designed so that it will operate satisfactorily under both normal and contingency

conditions. According to EGAT's practice, the single contingency (n-1) criterion is adopted, i.e. the system must be stable during and after the disturbances in the system resulting in the loss of one generating unit or one circuit of transmission line, as well as no loss of load is allowed.

c)

e)

The bulk power system can be maintained stable during and after most severity of following contingency:

A permanent three-phase fault on any generator or transmission circuit, with normal fault clearing and without reclosing.

d) Normal fault clearing time to be used shall be as follows:

500KV system : 4 cycles 230KV system : 5 cycles

Less probable, more severe disturbances, involving multiple contingencies; or the following unlikely contingencies are not evaluated.

Loss of an entire generating plant Loss of all circuits on common right-of-way Loss of one busbar section Three-phase fault with delayed fault clearing

### 6.2 Year 1997

(1) Year 1997's Network System

Fig. 6-1-1 shows network system in year 1997.

The capacities of reactive power compensator (shunt reactor) for each 500kV transmission line installed at substations within the Greater Bangkok Area shows at following table.

Substation Shunt Reactor		Transmission Line		
NONG CHOK	40MVA 2units 75MVA 2units	NONG CHOK-SAI NOI 120.0km 2cct NONG CHOK-THA TAKO 208.0km 1cct NONG CHOK-THA TAKO 215.0km 1cct		
SAI NOI	40MVA 2units	NONG CHOK-SAI NOI 120.0km 2cct		

(2) Load Flow

Fig. 6-2-1 shows the load flow of 500kV and 230kV system in the case of system peak.

### The results of load flow:

The busbar-voltage at each substation can be maintained within steady state voltage criteria (98 - 105%). The required capacities of reactive power compensator (shunt capacitor) at each substation in the Greater Bangkok Area are shown at Table 6-1-2, capacities of shunt capacitor in year 1997 are planned by EGAT.

No transmission line is overloaded under normal condition.

### Short Circuit Current (3)

The short circuit current levels at all 500kV and 230kV busbars are less than 50kA that is the interrupting rating of 500kV and 230kV circuit breakers. Fig. 6-2-2 shows the short circuit current and short circuit capacity of the whole 500kV and 230kV system in Thailand.

(4) Load Flow under Contingency Condition

> According to EGAT's transmission system planning criteria, under loss of one circuit of transmission lines or loss of one bank of 500kV/230kV transformers, no loss of load is allowed. So, load flow under contingency condition, i.e. loss of one bank of 500kV/230kV transformers or one circuit of transmission lines, should be checked that any transformers and any transmission lines can be maintained within allowable capacity.

### Contingency Condition;

500kV transformer transmission line

: Out-of service of one bank : Out-of service of one circuit Thermal limit of conductors 1x1272MCM ACSR 230KV 429MVA An and the second s 2X1272MCM ACSR 230KV 858MVA

Contingency Condition	Under Normal Condition	Under Contingency Condition
out-of service of one NONG CHOK 500kV/230kV transformers 600MVA 2-banks	296MW+j 63MVar (303MVA:50.5%) ( per bank )	436MW+j87MVar ( 445MVA:74%)
out-of service of one SAI NOI 500kV/230kV transformers 600MVA 2-banks	450MW+j161MVar (478MVA:80%) (per bank)	643MW+j220MVar ( 680MVA:1132)
one circuit of 230kV NONG CHOK - ON NUCH double circuit is tripped 2x1272MCM ACSR 2cct	463 MW/cct	673 MW
one circuit of 230kV BANG KAPI - RATCHADA double circuit is tripped 2x1272MCM ACSR 2cct	421 MW/cct	764 MW
one circuit of 230kV BANGKOK NOI - SAI NOI double circuit is tripped 1x1272MCM ACSR 2cct	233 MW/cct	323 MW
one circuit of 230kV BANG PHLI -BANG PAKONG double circuit is tripped 2x1272MCM ACSR 2cct	435 MW/cct	619 MW

No trasmission line is overloaded under contingency condition.

The 500kV/230kV 600MVA transformer at Sai Noi substation is expected to be overloaded during one bank outage. In the case of system peak, remaining transformer is expected to be 113% overloading. Taking account of short-time overloading requirement upon transformer, 113% overloading (advanced loading is 80%) is allowed.

• In the case of 500kV/230kV 750MVA transformer at Sai Noi substation:

Impedance of 750MVA transformer is adopted the same value as that of 600MVA transformer on the base of machine MVA, that is 13.06%.

Fig. 6-2-3 shows the result of load flow and short circuit current in the Greater Bangkok Area. No transmission line is overloaded under normal condition. The short circuit current levels are less than 50kA at whole 500kV and 230kV bus in the case of 750MVA 2-bank transformers at SAI NOI substation.

Contingency Condition	Under Normal Condition	Under Contingency Condition
out-of service of one SAI NOI 500kV/230kV transformers 750MVA 2-banks	489MW+j174MVar (519MVA:69%) (per bank)	725MW+j245MVar (765MVA:102%)

• Taking account of load flow under contingency condition and increasing power demands in future, adopting 750MVA unit transformer at Sai Noi substation is recommended.

(5) System Stability

Generator constants are shown at Table 6-2-1.

AVR and GOV block and control constans are used EGAT's data.

The generators with PSS (Power System Stabilizer) are following:

REGION-3	BANG LANG	3x 24MW
	RAJJAPRABHA	3x 80MW
and the second	KAENG KRUNG	2x 40MW
	KHANOM	2x 75MW + C.C. 674MW
REGION-4	MAE MOH unit 4-7	4x150MW
	unit 8-13	6x300MW
	MAE KHAM	2x150MW
REGION-1	EASTERN	
	BANG PAKONG thermal	2x550MW + 2x600MW
REGION-1	WESTERN	
· ·,	SRINAGARIND unit 4-5	2x180MW
and the second	KHAO LAEM	3x100MW
	LOWER CENTRAL C.C.	2x600MW

PSS-block and constants are used EGAT's data.

Pg—

 $-0.75 \frac{5.0 \text{ } \text{S}(1+0.06\text{S})(1+0.06\text{S})}{(1+5.0\text{S})(1+0.18\text{S})(1+0.18\text{S})} \qquad 0.1\text{pu}$ 

• The bulk power system can be maintained stable during and after 500KV transmission line contingency (three-phase fault with normal fault clearing).

Fig.6-2-4 shows the results of the system stability in the case of 500kV transmission line fault. Figures show relative rotor angles of typical generators in each region. The basis of angle is assumed Bang Pakong thermal generator.

CASE-No.	Fault Transmission Line (fault point)	Stability Result
97-TMM	MAE MOH - THA TAKO (MAE MOH)	stable
97-NTT	THA TAKO - NONG CHOK (THA TAKO)	stable
97-SNN	SAI NOI - NONG CHOK (NONG CHOK)	stable
97-SRR	SAI NOI - RATCHABURI 3 (RATCHABURI 3)	stable

Fig. 6-2-5 shows fluctuation of 230kV bus voltage at each substation in the Greater Bangkok Area during and after a permanent three-phase fault at Bang Pakong bus and one unit of Bang Pakong thermal plant (600MW) tripped with normal fault clearing. The steady state system voltage at any busbar in the Greater Bangkok Area can be maintained within voltage criteria (92~108%) under contingency condition.

### 6.3 Year 2001

(1) Year 2001's Network System

500kV transmission system

Fig. 6-1-3 shows single line diagram of 2001's network system.

The expansion plan in the Greater Bangkok Area from 1997 to 2001, which has been formulated by EGAT are following:

AO PHAI 2 - NONG CHOK	4x 795MCM ACSR 1cct 170km
AO PHAI 2 - SAI NOI	4x 795MCM ACSR 1cct 256km
BANG SAPHAN - RATCHABURI 3	4x1272MCM ACSR 2cct 275km

The capacities of reactive power compencator (shunt reactor) for each 500kV transmission line installed at substations in the Greater Bangkok Area shows at following table.

Substation	Shunt Reactor	Transmission Line
NONG CHOK	40MVA 75MVA 2units 55MVA	NONG CHOK-SAI NOI120km lcctNONG CHOK-THA TAKO208km lcctNONG CHOK-THA TAKO215km lcctNONG CHOK-AO PHAI170km lcct
SAI NOI	40MVA 95MVA	NONG CHOK-SAI NOI 120km leet SAI NOI-AO PHAI 256km leet

 500kV/230kV transformer NONG CHOK 3x600MVA SAI NOI 4x600MVA

6 ~ 6

 230kV transmission system BANG KAPI - RATCHADAPHISEK 2x1272MCM ACSR 2cct (totally 4cct) NONG CHOK - ON NUCH 2x1272MCM ACSR 2cct (totally 4cct) RANGSIT - CHAENG WATTHANA 2x1272MCM ACSR 2cct BANGKOK NOI - SAI NOI 2x1272MCM ACSR 2cct

(2)Load Flow

> Fig. 6-3-1 shows load flow based on EGAT's expansion plan. Under normal condition, 500kV/230kV 600MVA transformer at Sai Noi substation (4-banks) are overloaded. Sai Noi substation requires 5-banks of 600MVA transformer in year 2001.

> • Fig. 6-3-2 shows load flow in the case of 5-bank transformers at Sai Noi substation. The busbar voltage at each substation can be maintained within steady state voltage criteria (98-105%).

The required capacities of reactive power compensators (shunt capacitor) at each substation in the Greater Bangkok Area are shown at table 6-1-2.

• No transmission line is overloaded under normal condition.

(3) Short Circuit Current

Fig. 6-3-3 shows the short circuit current and short circuit capacity of whole 500kV and 230kV system in the case of 5-bank transformers at Sai Noi substation. The short circuit currents at Nong Chok and On Nuch 230kV busbar exceed 50kA.

NONG CHOK 230KV busbar 56.9kA ON NUCH 230KV busbar 55.1kA

(4)

Countermeasures for Reducing Short Circuit Current Level

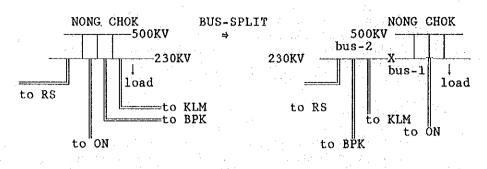
In order to reduce the short circuit current levels at Nong Chok and On Nuch substation, it will be necessary to make reconfiguration of 230kV system in the Greater Bangkok Area.

Basically, maintaining EGAT's expansion plan in year 2001. following countermeasures can be taken for reducing short circuit currents levels.

a)

NONG CHOK 230kV BUS-SPLIT

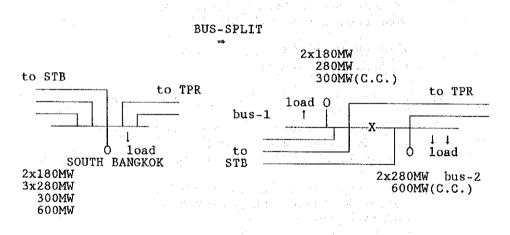
The method of splitting 230kV busbar at Nong Chok substation is referred to EGAT's planning in year 2006. Nong Chok 230kV bus is split with quadruple circuit to On Nuch, three 500kV/230kV transformers and distribution transformers connected to bus 1; while double circuit to Rangsit, double circuit to Bang Pakong and double circuit to Khlong Mai connected to bus 2. The configuration of Nong Chok 230kV bus is shown at following figure.



SOUTH BANGKOK BUS-SPLIT

b)

The method of splitting 230kV busbar at South Bangkok substation and power station is adopted EGAT's plan (referred to REPORT NO. 81200-3533 "TRANSMISSION SYSTEM FOR POWER PLANT PROJECT BLOCK 2 (600MW)"). The 230kV bus at South Bangkok substation is split with two circuits of triple circuit to South Thon Buri, one circuit of double circuit to Thepharak, thermal power plants (2x200MW and 310MW), combined cycle plant block-1 (300MW) and 69kV distribution transformers connected to bus 1; while one circuit of triple circuit to South Thon Buri, one circuit of double circuit to Thepharak, thermal power plants (2x310MW), combined cycle plant block-2 (600MW), 69kV and 115kV distribution transformers connected to bus 2. The configuration of South Bangkok 230kV bus is shown at following figure.



• The results of short circuit current levels which have been taken above mentioned countermeasures are summarized at following table.

	BASE-CASE	CASE-1	CASE-2	CASE-3
NONG CHOK BUS-1 BUS-2	56.9 kA	56.9 kA	41.4 kA 36.1 kA	41.1 kA 36.1 kA
ON NUCH	55.1 kA	55.0 kA	49.6 kA	49.6 kA
SAI NOI	49.9 kA	49.8 kA	49.8 kA	49.7 kA
SOUTH BANGKOK BUS-1 BUS-2	49.8 kA	40.4 kA 38.8 kA	49.3 kA	40.1 kA 38.5 kA

*countermeasures for reducing short circuit level

BASE-CASE : EGAT's plan

CASE-1 : SOUTH BANGKOK BUS-SPLIT CASE

CASE-2 : NONG CHOK 230KV BUS-SPLIT CASE

CASE-3 : SOUTH BANGKOK and NONG CHOK 230KV BUS-SPLIT CASE

• For reducing short circuit current level at Nong Chok 230kV busbar, splitting of Nong Chok 230kV bus by year 2001 is recommended, with quadruple circuit to On Nuch, three 500kV/230kV transformers and distrubution transformers connected to bus 1; while double circuit to Rangsit, double circuit to Bang Pakong and double circuit to Khlong Mai connected to bus 2.

Fig. 6-3-4 shows the result of load flow and short circuit current in the case of splitting of both Nong Chok 230kV bus and South Bangkok bus. No transmission line is overloaded under normal condition.

(5) Load Flow under Contingency Condition

In the configuration (Fig. 6-3-4) for reducing short circuit current levels, load flow under contingency condition should be checked that any transformers and any transmission lines can be maintain within allowable capacity to prevent cascaded tripping during single circuit outage.

Contingency Condition

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500kV transformer	:	Out-of service of one bank
transmission line	:	Out-of service of one circuit
an An an Anna an Anna Anna Anna Anna Ann		Thermal limit of conductors
an a		1x1272MCM ACSR 230kV 429MVA
na an a		2x1272MCM ACSR 230kV 858MVA
		4x1272MCM ACSR 230kV 1716MVA

		and the second
Contingency Condition	Load Flow under Normal Condition	Load Flow under Contingency Condition
out-of service of one 500kV/230kV SAI NOI transformer 750MVA 4-banks	639MW+j 78MVar (644MVA: 86%) ( per bank )	795MW+j103MVar ( 802MVA: 107%) ( per bank )
one circuit of 230kV BANGKOK NOI - SAI NOI double circuit is tripped 2x1272MCM 2cct	643.5MW+j84MVar ( per cct )	933MW+j165MVar overload
one circuit of 230kV SAI NOI - RANGSIT double circuit is tripped 2x1272MCM 2cct	572MW+j83MVar ( per cct )	840MW+j 83MVar critical load
one circuit of 230kV RANGSIT- CAENG WATTHANA double circuit is tripped 2x1272MCM 2cct	438.5MW+j68MVar ( per cct )	783MW+j134MVar
one circuit of 230kV BANG PHLI - BANG PAKONG double circuit is tripped 2x1272MCM 2cct	439.6MW+j87MVar ( per cct )	661MW+j135MVar
one circuit of 230kV ON NUCH - BANG PAKONG double circuit is tripped 2x1272MCM 2cct	486MW+j 70MVar ( per cct )	656MW+j104MVar

- The 500kV/230kV transformers at Sai Noi substation are operated with overloading during one bank outage. Taking account of short-time overloading requirement upon transformers, 107% overloading (advanced loading is 86%) is allowable operation.
- This network system (Fig. 6-3-4) will pose 230kV Bangkok Noi -Sai Noi line (2x1272MCM ACSR conductor :858MVA) overloading problems during single circuit outage contingency (single circuit trip on Bangkok Noi - Sai Noi 230kV line).
- (6) Transmission System Expansion Plan

• BANGKOK NOI - SAI NOI 29.6km

According to EGAT's transmission system expansion plan, existing 230kV double circuit is modified from 1x1272MCM ACSR conductor per phase to 2x1272MCM ACSR conductor per phase upto year 2001. However, these conductors will cause overloading problem during single circuit outage in 2001's network system. Therefore, this section should be reinforced with 230kV fourcircuit steel tower with 2x1272MCM ACSR conductor per phase or with 230kV double circuit steel tower with 4x1272MCM ACSR conductor per phase to save right-of way, or be augmentated with 500kV transmission line. From Chapter-5 this section should be augmentated with 500kV transmission line for a long future.  Construction schedule related to augmentation of BANGKOK NOI -SAI NOI line designed with 500kV specification

During construction for augmentation of Bangkok Noi - Sai Noi line designed with 500kV specification, existing 230kV double circuit will be removed. In the configuration under construction on Bangkok Noi - Sai Noi line section, routes to deliver power at Bangkok Noi substation are single circuit with lx1272MCM ACSR conductor on North Bangkok - Bangkok Noi, and double circuit with 2x1272MCM ACSR conductor on Soutuh Thon Buri - Bangkok Noi. In decision of construction schedule, load flow analysis under construction schedule in order to check overloading problems.

Year 1997

···a)

When Bangkok Noi - Sai Noi line is constructed at first, Rangsit - Chaeng Watthana line (1x1272MCM ACSR 429MVA) is expected to be overloaded at system peak in year 1997. The construction of Rangsit - Chaeng Watthana line at first solves line overloading ploblems. However, construction of Rangsit - Chaeng Watthana line in year 1998 cause overloading on Bangkok Noi - Sai Noi line (1x1272MCM ACSR 429MVA).

Fig. 6-3-5 shows the result of load flow under construction of Rangsit - Chaeng Watthana line section in year 1997.

From Chapter-5, Rangsit - Chaeng Watthana line (8.0km) is reinforced with 500kV double circuit with 4x1272MCM ACSR conductor per phase and 230kV double circuit with 2x1272MCM ACSR conductor per phase in common steel tower. However, in the area controlled by regulation concerning height restriction of structures built around the airport, 230kV double circuit is constructed by underground cable. The double circuit designed with 500kV specification will be a portion of North Bangkok - Sai Noi 500kV transmission line and will be operated with 500kV after completion of North Bangkok - Sai Noi 500kV transmission line.

Year 1998

b)

Fig. 6-3-6 shows the result of load flow under construction of Nong Chok - On Nuch line section in 1998's network system.

The Nong Chok - On Nuch line (16.8km) is expanded from 230kV double circuit to quadruple circuit with 2x1272MCM ACSR conductor per phase. The expansion plan of the 230kV Nong Chok - On Nuch line from 230kV double circuit to quadruple circuit is same as expansion plan formulated by EGAT. The short circuit current at Nong Chok 230kV bus will exceed 50kA at the commissioning dates (year 1999) of Ao Phai power plants, by this time Nong Chok 230kV bus should be split for reducing short circuit current at Nong Chok 230kV bus. Therefore, reinforcement of Nong Chok - On Nuch line is recommended prior to commissioning date of Ao

Phai power plants. According to EGAT PDP 92-01, 500kV lines link between Nong Chok, Sai Noi and Ao Phai have been proposed for commissioning in 1998. In this year, construction of Nong Chok - On Nuch 230kV four-circuit steel tower with 2x1272MCM ACSR conductor per phase and splitting of Nong Chok 230kV busbar are recommended.

The 1998's network system under construction of Nong Chok -On Nuch line is the weakest system configuration in recommended construction schedule. In this network, if one circuit of Bangkok Noi - Sai Noi double circuit will be occurred fault-tripping, the remaining circuit will be expected to be overloaded and be caused cascaded tripping. Following route tripping of Bangkok Noi - Sai Noi line, North Bangkok - Chaeng Watthana (1x1272MCM ACSR) and Lat Phrao - Chaeng Watthana (1x1272MCM ACSR) line will be expected to be overloaded. The control of loading as load shedding will be required to avoid system collapse in the Greater Bangkok Area.

Year 1999

c)

Fig. 6-3-7 shows the result of load flow under construction of Bangkok Noi - Sai Noi line in 1999's network system.

The Bangkok Noi - Sai Noi line section is reinforced with 500kV designed double circuit with 4x1272MCM ACSR conductor per phase. After completion of construction, this line section is operated with 230kV at first.

d) Year 2000

Fig. 6-3-8 shows the result of power flow under construction of North Bangkok - Bangkok Noi line (18.4km) in 2000's network system.

From Chapter-5, in consideration of system reliability in the Greater Bangkok Area, the North Bangkok - Bangkok Noi line is recommended to be augmentated with 500kV double circuit with 4x1272MCM ACSR conductor per phase. After completion of construction, this line section is operated with 230kV for a while.

### e) Year 2001

Fig.6-3-9 shows the result of load flow and short circuit current after above mentioned reinforcement in year 2001. No transmission line is overloaded under normal condition and no transmission has any problem to cause cascaded tripping during single circuit outage. And, short circuit current levels are less than 50kA at all 500kV and 230kV busbar.

# Load flow under contingency condition

Contingency Condition : Out-of service of one bank Contineed of the service of the serv

Contingency Condition	Power Flow under Normal Condition	Power Flow under Contingency Condition
out of service of NONG CHOK 500kV/230kV 750MVA transformer 600MVA 2 banks 750MVA 1 bank	750MVA 571MW+j65MVar 600MVA 458MW+j55MVar (461MVA: 77%) (per bank)	600MVA 633MW + j 88MVar ( 639MVA:106.5%) ( per bank )
out of service of SAI NOI 500kV/230kV transformer 750MVA 4 banks	640.7MW+j79MVar (646MVA: 862) (per unit)	801MW + j106MVar ( 808MVA:108% ) ( per bank )
one circuit of 230kV SAI NOI - RANGSIT double circuit is tripped 2x1272MCM ACSR 2cct	555MW+j48MVar ( per cct )	805MW +j 76MVar
one circuit of 230kV ON NUCH - BANG PAKONG double circuit is tripped 2x1272MCM ACSR 2cct	475.9MW+j64MVar ( per cct )	649MW +j101MVar
one circuit of 230kV BANGKOK NOI - SAI NOI double circuit is tripped 4x1272MCM ACSR 2cct	663MW +j88MVar ( per cct )	946MW+j168MVar

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System Stability (7)

The generators with PSS are following:

REGION-3	BANG LANG	3x 24MW
	RAJJAPRABHA	
	KAENG KRUNG	2x 40MW
		2x 75MW + C.C. 674MW
	COMBINED CYCLE	1x300MW
REGION-4	MAE MOH unit 4-7	4x150MW
	unit 8-13	6x300MW
	MAE KHAM	2x150MW
REGION-1	EASTERN	
	BANG PAKONG thermal	2x550MW + 2x600MW
		3x700MW
REGION-1	WESTERN	
	SRINAGARIND unit 4-5	2x180MW
	KHAO LAEM	
and the second	LOWER CENTRAL C.C.	
	NEW THERMAL unit 1-2	

The bulk power system can be maintained stable during and after 500kV transmission line contingency (three-phase fault with normal fault clearing) in power system of EGAT's plan.

Fig.6-3-10 shows the results of the system stability in the case of 500kV transmission line fault. Figures show relative rotor angles of typical generator in each region. The basis of angle is assumed Bang Pakong thermal generator.

CASE-No.	Fault Transmission Line (Fault Point)	Stability
01-MTM	MAE MOH - THA TAKO ( MAE MOH )	stable
01-NTT	NONG CHOK - THA TAKO ( THA TAKO )	stable
01-NSN	NONG CHOK - SAT NOI ( SAI NOI )	stable
01-NAA	NONG CHOK - AO PHAI ( AO PHAI )	stable
01-SAA	SAI NOI - AO PHAI ( AO PHAI )	stable
01-SRR	SAI NOI - RATCHABURI 3 ( RATCHABURI 3)	stable
01-RBB	RATCHABURI3 - BANG SAPHAN(BANG SAPHAN)	stable

### 6.4 Year 2006

(1)Year 2006's Network System

> Fig. 6-1-4 shows single line diagram of 2006's network system. The transmission system expansion plan in the Greater Bangkok Area from 2001 to 2006, which has been formulated by EGAT are following:

500kV transmission system	
	4x 795MCM ACSR 2cct 50km
	4x 795MCM ACSR 1cct 64km
SAI NOI - WANG NOI	4x 795MCM ACSR 2cct 56km
AO PHAI - WANG NOI	4x 795MCM ACSR 1cct 200km
BANG SAPHAN - SAI NOI	4x1272MCM ACSR 2cct 375km
BANG SAPHAN - BANGKOK NOI	4x1272MCM ACSR 2cct 350km

The capacities of reactive power compensator (shunt reactor) for each 500kV transmission line installed at substations in the Greater Bangkok Area shows at following table.

Substation	Shunt Reactor	Transmission Line
NONG CHOK	75MVA 2units 40MVA 55MVA	NONG CHOK-WANG NOI 50km 2cct NONG CHOK-WANG NOI 64km 1cct NONG CHOK-AO PHAI 170km 1cct
SAI NOI	40MVA 95MVA 100MVA 2units	SAI NOI-WANG NOI 56km lcct SAI NOI-WANG NOI 56km lcct SAI NOI-BANG SAPHAN 375km 2cct
BANGKOK NOI	100MVA 2units	BANGKOK NOI-BANG SAPHAN 350km 2cct
WANG NOI	75MVA	WANG NOI-THA TAKO 165km 1cct

500kV/230kV transformer

6x600MVA
6x600MVA
4x600MVA
2x600MVA

• 230kV transmission system

NORTH BANGKOK - LAT PHRAO	2x1272MCM AC	SR 1cct
NORTH BANGKOK - BANGKOK NOI	2x1272MCM A	
NORTH BANGKOK - CHAENG WATTHANA	2x1272MCM AC	SR lcct
LAT PHRAO - CHAENG WATTANA	2x1272MCM AC	SR 2cct
RANGSIT - CHAENG WATTHANA	2x1272MCM AC	SR 4cct
RANGSIT - WANG NOI	2x1272MCM AC	SR 2cct
BANG PHLI - ON NUCH	2x1272MCM AC	SR 2cct

### (2) Load Flow

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Fig. 6-4-1 shows load flow of EGAT's expansion plan. The busbar voltage at each substation can be maintained within steady state voltage criteria (98-105%). The required capacities of reactive power compensator (shunt capacitor) at each substation in the Greater Bangkok Area are shown at Table 6-1-2.

No transmission line is overloaded under normal condition.

(3) Short Circuit Current

Fig. 6-4-2 shows the short circuit current and capacity of whole 500kV and 230kV system in the case of EGAT's expansion plan. The short circuit current levels at following 230KV busbar exceed 50kA.

NONG CHOK 230KV bus	56.4	KA
ON NUCH	57.8	KA
BANG KAPI	51.6	KA
BANG PHLI	51.1	KA
SOUTH BANGKOK	54.3	KA
SOUTH THON BURI	50.9	KA
BANGKOK NOI 230KV bus	54.0	KA

### (4) Transmission System Expansion Plan

In order to reduce the short circuit current level less than 50kA, it is necessary to make reconfiguration of 230kV system in the Greater Bangkok Area. The year 2006's power system will be expanded from modified power system in year 2001 for reducing short circuit current and correcting overloading during single circuit outage. In addition to EGAT's transmission system expansion plan, upto 2001 following reinforcements and expansions will have been completed.

RANGSIT - CAENG WATTHANA (8.0km)

To be reinforced with 230kV double circuit with 4x1272MCM ACSR conductor per phase and 500kV double circuit with 4x1272MCM ACSR conductor per phase.

• NONG CHOK - ON NUCH (16.8km)

To be reinforced with 230kV quadruple circuit with 2x1272MCM ACSR conductor per phase.

• BANGKOK NOI - SAI NOI (29.6km)

To be reinforced with double circuit designed 500kV specification with 4x1272MCM ACSR conductor per phase.

• NORTH BANGKOK - BANGKOK NOI (18.4km)

To be reinforced with double circuit designed 500kV specification with 4x1272MCM ACSR conductor per phase.

For reducing short circuit current, Nong Chok 230kV bus and South Bangkok bus are split.

As a result of discussion with EGAT, it will be difficult to get new right-of-way from Bang Saphan to Bangkok Noi. So, transmission system expansion plans to deliver power from new thermal and nuclear generating plants are adopted EGAT's PDP 92-01, that is following:

New Thermal Switchyard - Sai Noi 500kV 4x1272MCM ACSR 4cct 375km (commissioning date 2001)

New Thermal Switchyard - Sai Noi 500kV 4x1272MCM ACSR 2cct 375km (commissioning date 2004)

Nuclear Switchyard - New Thermal Switchyard 500kV 4x1272MCM ACSR 2cct 125km (commissioning date 2005)

The power system configuration above-mentioned transmission system relevant to new thermal and nuclear plants is shown as following.

	BS	SP	RB3	SNO
	6x1000MW	4x1272MCM 2cct	0 4x1272	2cct
	0	275km	100ki	m
0				
NUCLEAR 2x1000MW		4x1272MCM ACSR	6cct 3751	km

non

Fig. 6-4-3 shows the result of load flow and short circuit current in 2006's power system expanded with above-mentioned expansion plan in addition to EGAT's transmission system expansion plan from 2001's power system.

Sai Noi - Rangsit 230kV-line (2x1272MCM ACSR conductor) is overloaded during normal condition. And even though Sai Noi 230kV-bus is split by the EGAT's method, the short circuit current at Sai Noi 230kV bus exceeds 50kA. Scheduled outage on North Bangkok - Chaeng Watthana 230kV line and Lat Phrao - Chaeng Watthana 230kV line is expected to correct Sai NOi - Rangsit 230kV line overload and to reduce short circuit current at Sai Noi 230kV bus less than 50kA. However, another overloading problems is expected, for example, Bangkok Noi - Sai Noi 230kV problems is expected, for example, Bangkok Noi - Sai Noi 230kV line overloading problem under contingency condition. Essentially, Sai Noi - Rangsit line should be expanded from 230kV double circuit 2x1272MCM ACSR conductor per phase to 230kV double double circuit 2x1272MCM ACSR conductor per phase to 230kV double circuit 4x1272MCM ACSR conductor per phase or 500kV double circuit 4x1272MCM ACSR conductor per phase. Taking account of future demand increase at Rangsit and Chaeng Watthana substation, the augmentation as 500kV substation is recommended. But, Rangsit substation has no space for augmentation with 500kV, so using right-of-way on Sai Noi - Rangsit - Chaeng Watthana - North Bangkok, construction of Sai Noi - North Bangkok 500kV double circuit with 4x1272MCM ACSR conductor per phase is recommended.

(5) Transmission System Construction Schedule 1.1.1.1

For avoiding overloading problems during construction of transmission line, power flow and short circuit current analysis have to be carried out at each construction schedule year.

a) ... Year 2001

> Fig. 6-4-4 shows the result of load flow under construction of North Bangkok - Lat Phrao - Chaeng Watthana line section in 2001's power system.

According to Chapter-5 "long future plan" a new substation "A" is constructed at location between North Bangkok and Lat Phrao. The North Bangkok - new substation "A" line section (4.4km)

is rebuilt with 500kV designed double circuit and 230kV double circuit steel tower with 4x1272MCM ACSR conductor per phase, respectively.

The Lat Phrao - new substation "A" line section (2.7km) is reinforced with 230kV double circuit steel tower with 4x1272MCM ACSR conductor per phase.

The Chaeng Watthana - new substation "A" line section (7.1km) is rebuilt with 500kV designed double circuit and 230kV double circuit with 4x1272MCM ACSR codnductor per phase, respectively.

### Year 2002

b)

Fig. 6-4-5 shows the result of load flow under construction of North Bangkok - Lat Phrao - Chaeng Watthana in 2002's network system.

Fig. 6-4-6 shows the result of load flow under construction of Rangsit - Wang Noi and Bangkok Noi - Sam Phran 1 line section in 2002's power system.

The Sai Noi - Rangsit line is modified from tap to Rangsit to via Rangsit due to the augmentation of North Bangkok -Sai Noi with 500kV double circuit. The Rangsit - Wang Noi line needs more double circuit to correct the overloading of Rangsit - Wang Noi line after completion of North Bangkok - Sai Noi 500kV transmission line. Taking account of reliability of feeding to Rangsit substation, the Rangsit - Wang Noi line should be expanded before construction of Sai Noi - Rangsit line.

The Rangsit - Wang Noi line section (49.9km) is expanded with double circuit steel tower with 2x1272MCM ACSR conductor per phase in parallel with existing right-of-way.

According to EGAS's PDP 92-01, Wang Noi substation will be terminated to 230kV Bang Pa-In 2 - Rangsit lines on Wang Noi gas turbine project (600MW for proposed commissioning in 1966). On this project, Wang Noi - Rangsit will be expanded with 230kV double-circuit steel towers with 2x1272MCM ACSR conductor per phase. In order to save right-of-way, construction of four-circuit steel towers for Wang Noi - Rangsit transmission lines is recommended on this project and in year 2002, double circuit with 2x1272MCM ACSR conductor per phase will be strung at fourcircuit steel towers.

The Bangkok Noi - Sam Phran 1 line section (11.7km) is reinforced with quadruple circuit steel tower with 4x1272MCM ACSR conductor conductor per phase. At this time existing double circuit steel towers have to be removed, therefore Sam Phran 1 substation has no 230kV feeder line. Before removal of existing 230kV double circuit steel towers, the South Thon Buri - Sam Phran 1 transmission line has to be constructed and operated by temporary route from branched point on South Thon Buri - Bangkok Noi line to Sam Phran 1.

If 230kV network system in region-3 will be expanded and Sam Phran 1 substation will be integrated in region-3 230kV network system, existing South Thon Buri - Sam Phran 1 -Bangkok Noi line sections (2x1272MCM ACSR conductor) have sufficient thermal capacity throughout year 2011.

### Year 2003

c)

Fig. 6-4-7 shows the result of load flow under construction of Rangsit - Wang Noi and Bangkok Noi - Sam Phran 1 line section in 2003's power system in the case of operation of Bangkok Noi - Sai Noi with 230KV. The short circuit current at Sai Noi 230kV bus exceeds 50kA. Splitting of Sai Noi 230kV bus can reduce short circuit current less than 50kA, but 500kV/230kV transformer banks will increase from 4 banks to 6 banks taking account of contingency condition overloading problem (one bank is tripped). The boost of Bangkok Noi substation with 500kV is recommended and Bangkok Noi - Sai Noi transmission line should be operated with 500kV in year 2003. Fig. 6-4-8 shows the result of load flow and short circuit current under construction of Rangsit - Wang Noi and Bangkok Noi - Sam Phran 1 in the case of boost of Bangkok Noi substation with 500kV. However, the Lat Phrao - Ratchadaphisek line is put into scheduled outage due to reducing short circuit current at On Nuch less than 50kA.

The requrired capacity of 500kV/230kV transformer banks at each substation is following:

NONG CHOK substation 600MVA 2 banks and 750MVA 2 banks

SAI NOI substation	750MVA 3 banks
BANGKOK NOI substation	750MVA 4 banks
WANG NOI substation	600MVA 3 banks

### d) Year 2004

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Fig. 6-4-9 shows the result of load flow under construction of Sai Noi - Rangsit line section and South Thon Buri - Sam Phran 1 - Bangkok Noi line section in 2004's power system.

The Sai Noi - Rangsit line section (24.5km) is expanded with 500KV designed double circuit with 4x1272MCM ACSR conductor per phase, after copmletion of construction this line section will be operated as the North Bangkok - Sai Noi 500kV double circuit (36km) via Rangsit, Chaeng Watthana and new substation "A".

> The South Thon Buri - Sam Phran 1 (19.8km) is reinforced from single circuit 2x1272MCM ACSR conductor per phase to double circuit with 4x1272MCM ACSR conductor per phase. The temporary route from branched point to Sam Phran 1 is removed and double circuits are strung at four circuit

steel tower. The line section from branched point to South Thon Buri is rebuilt with double circuit steel tower with 4x1272MCM ACSR conductor per phase.

The South Thon Buri - Bangkok Noi line section (8.1km) is modified from double circuit with 2x1272MCM ACSR per phase to single circuit with 4x1272MCM ACSR conductor per phase.

e) Year 2005

Fig. 6-4-10 shows the result of load flow under construction of South Thon Buri - Sam Phran 1 - Bangkok Noi and Bang Phli - On Nuch line section in 2005's power system.

The Bang Phli - On Nuch line (10.5km) is modified from 230kV double circuit steel tower with 1x1272MCM ACSR per phase to 2x1272MCM ACSR conductor per phase.

Fig. 6-4-11 shows the result of load flow and short circuit current under construction of Bang Phli - On Nuch line in 2005's power system.

In order to reduce the short circuit current, the boost of North Bangkok substation with 500kV is recommended and North Bangkok - Bangkok Noi (18.4km) and North Bangkok -Sai Noi (36km) transmission lines are operated with 500kV. The requrired capacity of 500kV/230kV transformer banks at each substation is following:

NONG CHOK substation

SAI NOI substation 7 BANGKOK NOI substation 7 NORTH BANGKOK substation 7 WANG NOI substation 6

600MVA 2 banks and 750MVA 2banks 750MVA 3 banks 750MVA 4 banks 750MVA 3 banks 600MVA 3 banks

### f) Year 2006

Fig.6-4-12 shows the result of load flow in 2006's power system after above mentioned reinforcements and expansions.

The South Bangkok - Thepharak transmission lines are put into scheduled outage without South Bangkok bus-split and either the Lat Phrao - Ratchadaphisek (Fig. 6-4-12) or Chaeng Watthana -new substation "A" (Fig. 6-4-13) transmission lines are put into scheduled outage due to reducing short circuit current.

The requried capacity of 500KV/230KV transformer banks at each substation is as following:

NONG CHOK substatio

SAI NOI substation

BANGKOK NOI substation

WANG NOI substation

NORTH BANGKOK substation

600MVA 2 banks and 750MVA 2 banks 750MVA 3 or 2 banks 750MVA 4 banks 750MVA 4 banks 600MVA 3 banks

No transmission line is overloaded under normal condition and contingency condition.

The bus-voltage at each substation can be maintained within steady state criteria (98 - 105%). The required capacities of reactive power compensator (shunt capacity) at each substation in the Greater Bangkok Area shows at Table 6-1-2.

Because of boost at Bangkok Noi and North Bangkok substation with 500KV, bus-voltage at each substation is improved.

### (6) System Stability

The generators with PSS are following:

REGION-3	BANG LANG	3x 24MW
	RAJJAPRABHA	
	KAENG KRUNG	2x 40MW
and the second	KHANOM	2x 75MW + C.C. 674MW
· . ·	COMBINED CYCLE	2x300MW
REGION-4	MAE MOH unit 4-7	4x150MW
	unit 8-13	6x300MW
e de la composición d	LAMPANG	8x300MW
	MAE KHAM	2x150MW
REGION-1		
	BANG PAKONG thermal	2x550MW + 2x600MW
	AO PHAI	2x700MW
REGION-1	WESTERN	: ·
	SRINAGARIND unit 4-5	2x180MW
and the second second	KHAO LAEM	3x100MW
1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 -	LOWER CENTRAL C.C.	
	NEW THERMAL unit 1-6	6x1000MW
	NUCLEAR unit 1-2	2x1000MW

The bulk power system can be maintained stable during and after 500kV transmission line contingency (three-phase fault with normal fault clearing) in power system of EGAT's plan.

Fig.6-4-14 shows the results of the system stability in the case of 500kV transmission line fault. Figures show relative rotor angles of typical generators in each region.

CASE-No.	Fault Transmission Line (fault point)	Stability
06MTM	MAE MOH - THA TAKO ( MAE MOH )	stable
06-MLL	MAE MOH - LAMPANG ( LAMPANG )	stable
06-TLL	THA TAKO - LAMPAMG ( LAMPANG )	stable
06-TWT	THA TAKO - WANG NOI ( THA TAKO )	stable
06-NWW	NONG CHOK - WANG NOI ( WANG NOI )	stable
06-WAA	WANG NOI - AO PHAI ( AO PHAI )	stable
06-NAA	NONG CHOK - AO PHAI ( AO PHAI )	stable
06-NSS	NONG CHOK - SAI NOI ( SAI NOI )	stable
06-SRR	SAI NOI - RATCHABURI 3 (RATCHABURI 3)	stable
06-SBB	SAI NOI - BANG SAPHAN (BANG SAPHAN)	stable
06-RBB	RATCHABURI 3- BANG SAPHAN(BANG SAPHAN)	stable
06-BNN	NUCLEAR - BANG SAPHAN(BANG SAPHAN)	stable

Fig. 6-4-15 shows the comparision of system stability between EGAT's transmission system expansion plan and power system augmentated North Bangkok and Bangkok Noi with 500kV. The fault condition is a permanent three-phase fault on Sai Noi -Bang Saphan 500kV transmission line at Bang Saphan with normal fault clearing without reclosing.

The reconfiguration of transmission system in the Greater Bangkok Area has little influence on system stability.

Fig. 6-4-16 shows fluctuation of 230kV bus voltage at each substation in the Greater Bangkok Area during and after a permanent three-phase fault at Bang Pakong bus and one unit of thermal generator (600MW) tripped with normal fault clearing. The steady state system voltage at any busbar can be maintained within voltage criteria (92 - 108%) under contingency condition.

EGAT's PDP (power development plan and transmission expansion plan) and recommended construction schedule from year 1997 to year 2006 for transmission system and 500kV substation in the Greater Bangkok Area are shown at Table 6-4-1.

### 6.5 Year 2011

(1) Power Development Plan

According to latest EGAT's PDP 92-01, power development planning from 2006 to 2011 will be assumed Nuclear Unit 3 - 6 (4x1000MW).

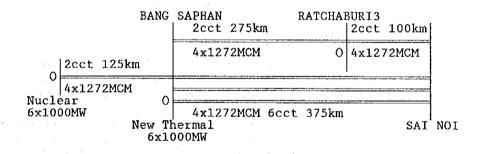
Proposed Commissioning Date

			1		
Nuclear W		- ·	1x1000MW	January	2007
Nuclear I	Unit	4	1x1000MW	July	2007
Nuclear U	Unit	5	1x1000MW	January	2008
Nuclear 1	Unit	6	1x1000MW	July	2008

In this study, new power development projects will be assumed above mentioned power sources which will be located in the same site as nuclear unit 1-2, that is at the southern part of Thailand.

According to latest EGAT's PDP, following 500kV transmission lines relevant to Nuclear project will be constructed upto 2006.

New Thermal Switchyard - Sai Noi 4x1272MCM ACSR 6cct 375km Nuclear Switchyard - New Thermal Switchyard 4x1272MCM ACSR 2cct 125km

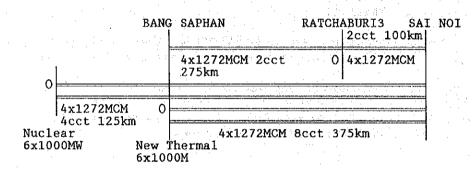


Nuclear Switchyard - New Thermal Switchyard (Bang Saphan)

In final nuclear-unit commissioning date, 5700MW ( 6x1000MW-6x50MW : 50MW station service ) in full output of nuclear generating units should be transmitted on nuclear switchyard new thermal switchyard 500kV double circuit transmission line. The thermal limit of 500kV 4x1272MCM ACSR transmission line is 3730MVA per circuit, so in the case of single circuit outage the remaining circuit is expected to be overloaded. Untill commissioning date of nulear unit-4, nuclear switchyard - new thermal switchyard (Bang Saphan) 500kV transmission line should be expanded with four circuits. According to latest EGAT's PDP, upto 2006 this section will be expanded with six circuits. The comparision of transient stability study between six circuit and eight circuit Sai Noi - Bang Saphan line for a fault at Bang Saphan on Sai Noi -Bang Saphan 500kV line are shown at Fig.6-5-1. The condition of load flow is selected the severest case.

New Thermal6x(1000-50)MW = 5700MWNuclear6x(1000-50)MW = 5700MW

The six circuit system is transiently unstable. On the other hand, the eight circuit system is transiently stable. Therefore, until the commitioning date of final nuclear unit Bang Saphan - Sai Noi 500kV transmission line should be constructed one more double circuit, totally expanded with eight circuits.



New Thermal (BANG SAPHAN) - Ratchaburi 3 - Sai Noi

Fig. 6-5-2 shows the result of power stability in the case of tap to Ratchaburi 3 of Sai Noi - Bang Saphan 500kV transmission lines. From the result of transient stability study, for maintaining stable during and after a permanent three-phase fault on Bang Saphan - Ratchaburi 3 500kV transmission line with normal fault clearing and without reclosing, Bang Saphan - Ratchaburi 3 500kV lines are required 10 circuits. In the case of 8-circuits on Bang Saphan -Ratchaburi 3 transmission, the performance of power stability is enhanced by interconnection between region-1 and region-3 strongly. Fig. 6-5-3 shows the result of power stability interconnected between Bang Saphan and Surat Thani (310km) with 500kV transmission line.

	BANG SA	PHAN R.	ATCHABURI 3
Nuc	lear 6x1000MW O		0
6x1000MW	4x1272MCM		
4x1272MC SURAT THANI	4cct 125km M ACSR 2cct 310km	4x1272MCM ACSR 8cc 275km	t       SAI NOI 4x1272MCM 8cct 100km

(2)

Year 2011's network system and load flow

In addition to EGAT's expansion plan by year 2006, following modifications, reinforcements and expansions in the Greater Bangkok Area have been completed by year 2006 for reducing short circuit current and correcting overloading ploblems under normal and contingency condition.

٠	500kV transmission line	
	BANGKOK NOI - SAI NOI (29.6km)	500kV 4x1272MCM ACSR 2cct
	NORTH BANGKOK - SAI NOI (36km)	500kV 4x1272MCM ACSR 2cct
	NORTH BANGKOK - BANGKOK NOI (18.4km)	500kV 4x1272MCM ACSR 2cct

• 23	0kV transmission line		
	NGSIT - CHAENG WATTHANA(10km)	4x1272MCM ACSR	2cct
	RTH BANGKOK - A S/S (4.4km)	4x1272MCM ACSR	2cct
	T PHRAO - A S/S $(2.7 \text{km})$	4x1272MCM ACSR	2cct
	AENG WATTHANAN - A S/S (7.1km)	4x1272MCM ACSR	2cct
	NGSIT - WANG NOI (49.9km)	2x1272MCM ACSR	4cct
	NGKOK NOI - SAM PHRAN 1 (11.7km)	4x1272MCM ACSR	2cct
	UTH THON BURI - SAM PHRAN 1 (19.8km)	4x1272MCM ACSR	2cct
SO	UTH THON BURI - BANGKOK NOI (8.1km)	4x1272MCM ACSR	1cct

Fig. 6-5-4 shows the results of load flow and short circuit current in 2011's network system expanded from 2006's network system based on EGAT's load forecast (Table 6-1-1). The short circuit current levels at whole 230kV and 500kV bus in the Greater Bangkok Area are less than 50kA. However, North Bangkok new substation "A" 230kV double circuit with 4x1272MCM ACSR conductor ( conductor thermal limit : 1716MVA ) per phase is expected to be overloaded under single circuit tripped.

Contingency Condition	Load Flow under Normal Condition	Load Flow under Contingency Condition
single circuit of 230kV	1086.4MW-	2073.7MW-
North Bangkok - "A" double	j123.8MVar	j190.7MVar
circuit is tripped	( per cct )	overload

The load flow on Bangkok Noi - Sai Noi 500kV transmission line and North Bangkok - new substation "A" 230kV transmission line are restricted by thermal limit of conductors (4x1272MCM ACSR) under contingency condition, that are 3730MVA and 1716MVA, respectively. In order to control load flow on Bangkok Noi - Sai Noi 500kV transmission line and North Bangkok - new substation "A" 230kV transmission line, sectionalizing of 230kV nertwork system in the Greater Bangkok Area is recommended. The South Bangkok - Thepharak line is put into scheduled outage due to control load flow on the Bangkok Noi - Sai Noi 500kV transmission line, while the Rangsit - Chaeng Watthana line and Lat Phrao -Ratchadaphisek line (Fig. 6-5-5), or Chaeng Watthana - new substation "A" line and Bang Kapi - Ratchadaphisek line (Fig. 6-5-6) are put into scheduled outage due to control load flow on the North Bangkok - new substation "A" 230kV transmission line.

The 2011's network system in the case of more increasing demand than EGAT's load forecast is described in detail in Chapter-5.

# Table 6-1-1 load forecast at each substation

| . Table 6-1-1 LOau

1997 (MVA) sys-peak MEA peak
E. [
149.681 2×200 449.501
0.000 548 779
257 143 514.286
355.938 375.712 3x200 281 871 275 668 2×200
137.832
137.832 551.330
188.909
1/8.955 138.909 2×200 0.980 0.000 2×200
377.817
367,684
255.880 270.096 2×2 511.760 540.191
81.775 86.318 300
329.960 348.291
08.140   536.370
4753.759 5017.857
240 039
11
+
179.507
40.533
253.209 267.276 2x200
133.438
192.729
190.255 200.825 2×300
86.323
404,105 1482,111 2×200
6157.864 6499.968
Growth Rate

Load Forecast of Region-2

								:									•				•										. •														•
ſ	MF3 AAAV	4 186	53.471	57.723	159.797	65.087	15.664	60-803	32.197	55.418	62.150	33.605	37.983	36.399	38.352	50.375	65.483	51.904	37.070	8.916	21.714	26.334	0.264	44.743	34-441	29.024	22.704	15.065	31.938 ]	24.255	40.161	34.876	29.574	42.169	54.708	27.363	34.667	27.654	4.675	22.886	23.320	28.160	14.163	1571.482	4.189
		7 230	92.359	99.703	275.013	112.423	27.056	105.023	55.613	95.722	107.350	58.045	65.607	52.871	56.244	87.011	113.107	89.652	64.030	15.400	37.506	45.486	0:456	77.282	59.489	50.132	39.216	26.021	55.252	41.895	69.369	60.239	51.082	72.837	111.753	47.252	59.878	47.756	8.075	39.530	40.280	48.640	24.463	_	06-11 (%)
		7 610	97.220	104.350	290.540	118.340	28.480	110.550	58.540	100, 760	113.000	61.100	69.050	66.180	69.730	91.590	119.060	94.370	57.400	16.210	39.480	47.880	0.480	81.350	62.6201	52.770	41.280	27.390	58.150	44.100	73.020	63.410	53.770	76.670	117.650	49.750	63.030	50.280	8.500	41.610	42.400	51.200	25.750		1
-	100 V2N	2888	41.399	•	133.062	52.734	13.101	49.731	$\sim$	44.759	50.034	27.060	29.398	29.139	29.590	40.920	53.273	42.257	30.184	7.524	17.415	21.544	0,209	36.003	28.441	23.980	18.821	12.546	26.587	19.932	32.742	28.651	24.998	34.452	56,540	22.319	28.771	22.897	4.675	18.337	09.6		11:352	279.993 2	4.961
		SVS-PEAN 0	71.506	73.881	229.334	91.086	22.629	85.899	45.353	77.311	86.422	46.740	50.778	50.331	51.110	70.580	92.017	72.989	52.136	12.996	30.077	37.212	0.361	62.187	49.125	41.420 1	32.509	21.670	45.923	34.428	56.554	49.505	43.178	59.508	97.660	38.551	49.695	39.549	8.075	31.673	32.984	39.900		1	01-06 (%)
	-	E 160	75.270	77.770	~	95.880	23.820	90.420	47.740	81.380	90.970	49.200	53:450	52.980	53.800	74.400	56.860	76.830	54.880	13.680	31.560	39.170	0.380	65.460	51.710	43.600	34.220	22.810	48.340	36.240	59:530	52.110	45.450	62.640	102.800	40.580	52.310	41.630	8.500	33.340	34.720	42,000	•	327.260 2	0
	NCA ACAY	7 640	30.718	30.657	104.346	41.718	10.461	39.017	20.631	34.331	39.237	21.219	22.038	22.358	22.143	31.801	41.784	32.868	23.474	6.072	13.398	17.039	0.154	28.023	22.853	19.272	15:021	10.027	21.318	15.846	25-801	22.765	20.911	27.011	48.356	17.540	22.974	18.365	4.675	14.064	15.032	18.040	8.679		6.515
	1002		53.058	52.953	180.234	72.857	18.069	67.393	35.634	59.384	67.773	36.651	38.152	38.618	38.247	54.929	72.172	56.772	40.546	10.488	23.142	29.431	0.266	48.403	39.473	33.288	25,944	17.319	36.822	27.370	44.554	39.320	36.119	46-655	83.524	30-296	39.682	31.720	8.075	24.292		31.160	14.8.9.1	735.508 1	97-01 (%)
	1 0 0 0 0 0 0 0		55.850 1	55.740	189.720	75.850	19.020	70.940 1	37.510	62.510	71.340	38.580	40.150	40.650	40.260	57.820	75.970	59.760	42.580	11.040	24.360	30.980	0.280	50.950	41.550	35.040	27.310	18.230	38.750	28.810	45.910	41.390	38.0201	49. II0 I	87.920.1	31.890	41.770	33.390		25.570	27.330	32.800	15.780	1826.850 1	8
	NEA DOOL	. 946 S	23.007	22.831	70.136	33.726	8.217	30.734	16.165		31.290	16.924	17.045	17.177	17.012	24.613	32.412	25.383	18.128	4.829	10.313	13.563	0.110	21.973	18.455	15.571	11.902	7.926.	16.979	12.617	20.357	18.084	17.958	21.148	41.502	13.739	18.046	14.768	4.675	10.791	11.765	13.745		780.588 1	Rate
	133/		39.738	39.434	121.144	58.254	14.193	53.086	27.921 (	45.220	54.046	29.231	29.440	29.668	29.383	42.512	55.984	43.842	31.312	8.341	17.813	23.427	0.190	37.953	31.901	26.394	20.558	13.689	29.327	21.793	35.179	31.236	31.018	36.528	71.858	23.731	31.170	25.508	8.075	18.639	20.321	23.740	11 457	348.288	Growth R
	0100-000		41.830	41.510	127.520	61.329	4	55.830	29.390	47.600	56.890	30.770	30.990	31.230	30.930	44.750	58.930	46.150	32.960	8.780	18.750	24.660	0.200	39.950	33.580	28.310	21 640	14.410	30.870	22.940	37.030	32.880	32.650	38.458	75, 640	24.980	32.810	26.850	8.500	19.620	21.390	24.990	12.050	(419.250	verage (
	on node	e 2603			col.	ati		2706	2707		n-1 2710	n-2 2711	akha2712	2713	2714	2715	t 2716-	cha12717	cha22718	rn 2720 i	aroe2721	2722	rn 2723	e 2724		\$		2729	akho 2730	Lam2731	2732		2736	aphui2737	c 2738		rakhon Chail2745	2746	2747	ng 2748	nano2751	2752	10m 2750		<b>N</b>
į	substation	Nam Phine	Pak Chong	Sikhui	Nakhon Rat2	Nakhon Rat	Buri Ram	Surin	Phon	Chaiyaphum	Khon Kzen-1	Khon Kaen-2	Maha Sarakha2712	Yasothon	Kalasin	Roi Et	Si Sa Ket	Whon Ratchal271	Ubon Ratcha22718	Sirindhorn	Amnat Charoe2721	Mukdahan	Coulabhorn	Chum Phae	Udon Thani	Udon Thani2	Phang Khon	Bung Kan	Sakhon Nakhol2730	Nong Bua Lam273]	Loei	Nong Khai	Khong	Phayakkhaphu2737	Nam Phone	Ban Phai	Prakhon (	Nong Han	Ban Dung	Phon Thong	Nakhon Phano2751	Sondet	That Phanom		

Load Forecast of Region-3 

$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	0000	-	1007			1 1 1 1							
55       770       72       31       35       37       70       10       31       32       33       53       10       10       11       30       11       30       11       30       11       30       11       30       11       30       11       30       11       30       11       30       11       30       11       30       11       30       11       30       11       30       11       30       11       30       11       30       11       30       11       30       11       30       11       30       11       30       11       30       11       30       11       30       11       30       11       30       11       30       11       30       10       11       30       11       30       11       30       11       30       11       30       11       30       11       30       11       11       30       11       30       11       11       30       11       30       11       30       11       30       10       11       30       10       11       30       10       11       30       10       10 <t< th=""><th>1</th><th>hon-coin b</th><th></th><th>beak</th><th></th><th>s-peak</th><th>beak</th><th>-coin.</th><th>s-peak</th><th>Jeac</th><th>non-coin</th><th></th><th>MEA peak</th></t<>	1	hon-coin b		beak		s-peak	beak	-coin.	s-peak	Jeac	non-coin		MEA peak
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	3701	55.070		8.549	1 1	70.101	. 653	5.820	91.979	1.774	119.390	1	83.573
	3702	15.530	14.753	10.871	20.810	19.769		27.310		19.117	33.680	31.996	23.576
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	3704	63.240	60.078	44.268	83.970	177.97		111.500		78.050	•	134.093	98.805
46         710         45         713         45         713         45         713         10         13         513         10         13         513         10         13         513         110         13         513         110         13         513         110         13         513         110         13         513         110         13         513         110         13         513         110         13         513         110         13         513         110         13         513         110         13         13         100         13         513         110         13         13         100         13         101         101         101         101         101         101         101         101         101         101         101         101         101         101         101         101         101         101         101         101         101         101         101         101         101         101         101         101         101         101         101         101         101         101         101         101         101         101         101         101         101         101         101	105	2.940	2.793	2.058		3.734				3.780	7.210		
9.630         9.145 $5.741$ 13.030         15.310         17.300         12.747         24.440         23.218         11.000           60.300         61.34         42.750         15.01         11.310         12.770         12.771         13.570         13.4         42.550         136.371         100.36         23.441         13.570         13.4         42.550         136.371         100.36         33.100         33.450         13.1         100.36         33.1         100.36         33.1         100.36         33.1         100.36         33.1         100.36         33.1         100.36         33.1         100.36         33.1         100.36         33.1         100.36         33.1         100.36         33.1         100.36         33.1         100.36         33.1         100.36         33.1         100.36         33.1         100.36         33.1         100.36         33.1         100.36         100.36         100.36         100.36         100.36         100.36         100.36         100.36         100.36         100.36         100.36         100.36         100.36         100.36         100.36         100.36         100.36         100.36         100.36         100.36         100.36         100.36         10	3706	48.	46.332	34.139		63.318				62.578			I
125.0011.8 f53.70013.8 f53.10023.45015.31023.10023.45023.00023.45023.00023.45023.00023.45023.00023.45023.00023.45025.31023.00023.450143.271100.63.80060.61044.66036.64087.84411.73011.184382.411114.271100.63.80080.14755.31573.77075.21553.539104.5700114.271100.64.80080.14755.31573.77075.73356.939104.50087.44413.5701143.261139.45087.73083.34095.23358.839104.510105.709140.757101.467131.471100.87.73083.34093.24093.265105.101105.166101.466156.41391.2687.73083.34093.265115.665104.6160.661104.666107.471100.87.73083.24151.661109.40286.831116.610106.766107.456136.45587.73083.240151.661104.6555.65146105.266107.456137.565147.56687.77072.666103.26555.01657.61126.436136.456126.458137.565147.56687.77072.666139.651126.461129.463151.666107.466126.488137.565137.56687.77072.666137.656137.656137.656 <t< td=""><td>3707</td><td>9.630</td><td>9.149</td><td></td><td></td><td>12.378</td><td>-</td><td></td><td></td><td>12.747</td><td></td><td>23.218</td><td>7</td></t<>	3707	9.630	9.149			12.378	-			12.747		23.218	7
60.300 $57.314$ $42.231$ $81.300$ $77.824$ $57.344$ $111.310$ $105.745$ $77.97$ $111.343$ $82.411$ $154.250$ $144.277$ $100.$ 61.300         56.813 $43.570$ $32.516$ $32.916$ $55.433$ $32.701$ $57.732$ $118.43$ $32.701$ $55.433$ $44.377$ $100.$ $54.300$ $56.142$ $17.720$ $118.43$ $32.2016$ $55.439$ $103.932$ $32.016$ $31.570$ $124.4277$ $101.244.277$ $100.$ $87.730$ $33.344$ $51.400$ $12.65$ $33.948$ $75.400$ $42.510$ $44.387$ $83.870$ $157.730$ $112.459$ $142.520$ $142.870$ $142.770$ $124.66.110$ $157.730$ $145.730$ $112.657$ $145.730$ $142.357$ $142.357$ $145.357$ $145.357$ $145.357$ $145.357$ $145.357$ $145.357$ $145.357$ $145.357$ $145.357$ $145.357$ $145.357$ $145.357$ $145.357$ $145.357$ $145.357$ <td>3708</td> <td>12</td> <td></td> <td></td> <td></td> <td>15.017</td> <td>11.802</td> <td></td> <td>: .</td> <td>16.345</td> <td></td> <td></td> <td></td>	3708	12				15.017	11.802		: .	16.345			
63. 500         60. 60         61. 41         61. 51. 67         62. 500         62. 500         62. 513         41. 51. 870         144. 277         104. 51. 87         144. 277         104. 51. 87         13. 570         55. 450         43. 55         13. 570         13. 570         134. 57         13. 570         134. 57         13. 570         134. 57         13. 570         134. 57         13. 570         134. 57         13. 570         134. 570         134. 570         134. 570         134. 570         134. 570         134. 570         134. 570         134. 570         134. 570         134. 570         134. 570         134. 570         134. 570         134. 570         134. 570         134. 570         134. 570         134. 570         134. 570         134. 570         134. 570         134. 570         134. 570         134. 570         134. 570         134. 570         134. 570         134. 570         134. 570         134. 570         134. 570         134. 570         134. 570         134. 570         134. 570         134. 570         134. 570         134. 570         134. 570         134. 570         134. 570         134. 570         134. 570         134. 570         134. 570         134. 570         134. 570         134. 570         134. 570         134. 570         134. 570         134. 57	3.7.09	60				77.824	57.344	111.310	i	77.917			100.485
24.890         23.646         17.73         35.700         37.70         37.70         37.71         15.77         15.77         15.77         15.77         15.77         15.77         15.77         15.77         15.77         15.77         15.77         15.77         15.77         15.77         15.77         15.77         15.77         15.77         15.77         15.77         15.77         15.77         15.77         15.77         15.77         15.77         15.77         15.77         15.77         15.77         15.77         15.77         15.77         15.77         15.77         15.77         15.77         15.77         15.77         15.77         15.77         15.77         15.77         15.77         15.77         15.77         15.77         15.77         15.77         15.77         15.77         15.77         15.77         15.77         15.77         15.77         15.77         15.77         15.77         15.77         15.77         15.77         15.77         15.77         15.77         15.77         15.77         15.77         15.77         15.77         15.77         15.77         15.77         15.77         15.77         15.77         15.77         15.77         15.77         15.77         15.77	3710-	63.800	60-610	44,660	36.640	82:308	60.648	117.730	111.843	82.411	151.870	144.277	106.309
61.930         58.833         43.551         79.770         75.782         55.833         103.930         98.734         72.751         131.570         124.931         92.           84.700         30.145         16         1411         117.950         122.053         88.2155         115.160         103.157         104.05.052         144.05         179.50         122.055         15.160         103.11.66         179.50         127.05         15.50         179.50         127.05         15.51         141.01         157.05         155.160         157.50         155.160         157.60         157.50         155.160         157.60         157.50         155.160         157.60         157.50         157.10         179.50         157.10         157.50         157.70         158.71         158.71         158.71         158.71         158.71         158.71         158.71         158.71         158.71         158.71         158.71         158.71         158.71         158.71         158.71         158.71         158.71         158.71         158.71         158.71         158.71         158.71         158.71         158.71         158.71         158.71         158.71         158.71         158.71         158.71         158.71         158.71         158	111	24.890	23.646	17.423	33.700	32.015	23,590	45.720		32.004	59.450	55.478	41.615
84.360       80.142       59.052       93.134       0.93.233       68.698       115.160       105.405       136.700       136.750       136.750       136.750       136.750       136.750       136.750       136.750       136.750       136.750       136.750       136.750       136.750       136.750       136.750       136.750       136.750       136.750       136.750       136.750       136.750       136.750       136.750       136.750       136.750       136.750       136.750       136.750       136.750       136.750       136.750       136.750       136.750       146.750       136.750       146.756       136.750       146.750       136.750       146.750       146.750       146.750       146.750       146.750       146.750       146.750       146.743       33.160       35.750       146.750       146.743       33.160       146.750       146.743       33.160       35.750       146.730       146.743       130.710       111.436       36.750       141.310       151.725       34.950       111.936.950       146.750       146.743       130.750       146.750       146.743       130.750       146.750       146.743       130.750       141.317       121.720       121.720       121.730       121.730       121.730 <t< td=""><td>712</td><td>61.</td><td>58.833</td><td>43.351</td><td>79.770</td><td>75.782</td><td>55.839</td><td>103.930</td><td></td><td>72.751</td><td></td><td>124.991</td><td>92.099</td></t<>	712	61.	58.833	43.351	79.770	75.782	55.839	103.930		72.751		124.991	92.099
877         730         83.344         61.411         117         950         112.053         82.565         159.480         151.506         111.636         206.370         195.870         776.77         55.           33.050         31.397         23.1397         25.135         45.440         43.1387         35.570         75.570         51.905         51.905         51.905         51.905         51.905         51.905         51.905         51.905         51.905         51.905         51.905         51.905         51.905         51.905         51.905         51.905         51.905         51.905         51.905         51.905         51.905         51.905         51.905         51.905         51.905         51.905         51.905         51.905         51.905         51.905         51.905         51.905         51.905         51.905         51.905         51.905         51.905         51.905         51.905         51.905         55.933         31.056         51.940         20.2         51.940         20.2         51.940         20.2         51.940         21.604         51.165         51.16         51.16         51.16         51.16         51.16         51.16         51.16         51.16         51.16         51.16         51.20	713	84.360	80.142	59.052	98.140	93.233	68.698	115.160	109.402	80.612	I32.750	125.113	92.925
33.050         31.397         33.87         33.870         73.671         58.870         73.671         58.871         58.871         58.871         58.871         58.871         58.871         58.871         58.871         58.871         58.871         58.871         58.871         58.871         58.871         58.871         58.871         58.871         58.871         58.871         58.871         58.871         58.871         58.871         58.871         58.871         58.871         58.871         58.871         58.871         58.871         58.871         58.871         58.871         58.871         58.871         58.871         58.871         58.871         58.871         58.871         58.871         58.871         58.871         58.871         58.871         58.871         58.871         58.871         58.871         58.871         58.871         58.871         58.871         58.871         58.871         58.871         58.871         58.871         58.871         58.871         58.871         58.871         58.871         58.871         58.871         58.871         58.871         58.871         58.871         58.871         58.871         58.871         58.871         58.871         58.871         58.871         58.871         58.871<	714	87.730	83.344	61.411	117.350	112-053	8.2.565	159.480	151-506	111 536	206, 370	196.052	144.459
31       410       22, 968       22, 008       40, 310       38, 235       28, 317       55, 46       55, 150       65, 150       65, 160       157, 805       146         74       77.0       71, 077       53, 803       38, 210       38, 210       56, 47       130, 510       157, 805       146       157, 805       146       157, 805       146       157, 805       146       157, 805       146       157, 805       146       157, 805       146       157, 805       146       157, 805       146       157, 805       146       157, 805       146       157, 805       146       157, 805       146       157, 805       146       157, 805       146       157, 805       146       157, 805       146       157, 805       146       157, 805       146       157, 805       146       157, 805       146       157, 805       151, 100       157, 805       154, 100       157, 805       154, 100       157, 805       154, 100       157, 805       154, 100       157, 805       161, 100       157, 805       141, 300       161, 100       157, 805       161, 100       157, 805       164, 131       157, 805       144, 317       26, 204       141, 317       32, 336       35, 336       35, 336       35, 336 <td>9 T L</td> <td>33.050</td> <td>31.397</td> <td>23.135</td> <td>45.440</td> <td>43.168</td> <td>3.1.80.8</td> <td>63.410</td> <td></td> <td>44.387</td> <td></td> <td>79.677</td> <td>58.709</td>	9 T L	33.050	31.397	23.135	45.440	43.168	3.1.80.8	63.410		44.387		79.677	58.709
74       71       71.032       52.339       88.210       53.610       157.805       110       157.805       110       157.805       116.48       88.98       110       157.805       116.48       88.98       110       157.805       116.48       88.98       110       157.805       116.48       88.98       110       157.805       116.439       188.91       110       157.805       116.439       138.91       138.91       138.91       138.91       138.91       138.91       138.91       138.91       138.91       138.91       138.91       138.91       138.91       138.91       138.91       138.91       138.91       138.91       138.91       138.91       138.91       138.91       138.91       138.91       138.91       138.91       138.91       138.91       138.91       138.91       138.91       138.91       138.91       138.91       138.91       138.91       138.91       138.91       138.91       138.91       138.91       138.91       138.92       138.93       138.93       138.93       138.93       138.93       138.93       138.93       138.93       138.93       138.93       138.93       138.93       138.93       138.93       138.93       138.93       138.93       138.93	717	31.440	29.858	22.008		38.295				36.554		61-902	45.612
66.640       53.803       39.648       74.300       70.671       52.073       98.850       93.917       69.202       125.840       119.648       88.         65.640       10.800       20.800       88.206       55.015       13.956       15.450       16.439       110.         65.650       16.800       27.556       55.053       55.750       25.354       47.80       15.439       33.         38.910       30.566       13.010       17.10       17.10       17.65       13.010       17.143       26.349       110.       25.730       25.310       56.350       56.360       56.350       56.360       56.350       56.310       26.339       33.530       56.310       27.143       20.202       113.250       87.590       56.1490       114.430       88.590       56.149       114.330       88.590       56.143       114.330       88.550       56.140       114.330       88.550       56.743       46.750       66.756       43.17       32.700       28.700       28.700       28.700       28.700       28.700       28.700       28.700       28.700       28.700       28.700       28.700       28.700       28.700       28.700       28.700       28.710       28.710       28.710<	719	74.	71.032	52.339	98.210	93.300	68.747			91.357	166:110		116.277
65.690       56.206       48.733       92.830       88.235       65.016       124.250       155.420       155.420       156.430       48.539       33.         31.90       55.946       71.537       50.480       87.530       55.435       55.435       55.436       65.436       65.436       65.436       65.436       65.436       65.436       65.436       65.436       65.436       51.400       21.433       21.433       21.433       21.433       21.433       21.433       21.433       21.433       21.433       21.433       21.433       21.235       32.546       31.210       21.235       32.546       31.210       21.235       35.513       55.436       55.436       55.740       13.135       21.400       28.5700       21.235       32.553       56.435       55.401       71.336       84.317       21.7       21.700       21.7       21.7       21.27       740       59.353       55.35       55.35       55.35       55.35       55.35       55.35       55.35       55.35       55.710       21.2       22.210       21.2       22.21       21.25       21.25       21.25       21.25       21.25       21.25       21.25       21.25       21.25       21.25       21.21       22.55	720	56.640	53.808	39.648	74.390	70.671	52.073	9.8.860			125.840		
21<990	721	69.69	56.206	48.783	92.880	88.235	65.016				158-420	L 4	110.894
38.910       38.964       27.237       50.730       48.250       58.880       51.435       48.216       83.590       81.30       20       21       82.700       21       25.700       21       25.700       21       25.700       21       25.700       21       25.700       21       23.700       21       23.250       17.456       17.065       17.062       12.10       23.160       17.055       12.450       23.560       25.450       17.950       21.10       23.700       21       30.210       25.700       21.20       30.210       25.700       21.20       30.210       25.700       21.20       30.210       25.700       21.20       30.210       31.7052       12.10       31.7052       12.10       32.595       24.110       32.595       24.117       32.595       24.117       32.595       24.117       32.700       31.7052       32.730       30.912       55.140       46.517       32.255       34.116       32.555       34.116       32.555       34.116       32.555       34.116       32.555       34.116       32.555       34.116       32.555       32.5750       32.5750       32.537       34.116       32.555       34.165       31.720       35.5533       34.165       31.720	722	21 990	20.890	15.393	28.480	27.056	19.936	37.620		26.334	47-830		33.481
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	7.2.3		36.964	27.237	50.790	48.2.5.0	35.553	68.880	65.436	48.216		83-590	61.593
56.490       53.656       39.543       72.740       69.103       50.918       95.380       80.611       66.766       120.400       114.380       84.         7.420       7.420       7.049       5.355       6.355       13.550       12.756       17.950       17.950       17.956       17.950       17.950       17.950       17.950       17.950       17.950       17.950       17.950       17.950       17.950       17.950       17.950       17.950       17.950       17.950       17.950       17.950       17.950       17.950       17.950       17.950       17.950       17.950       17.950       17.950       17.950       17.950       17.950       17.950       17.950       17.950       17.950       17.950       17.950       17.950       17.950       17.950       17.950       17.950       17.950       17.950       17.950       17.950       17.950       17.950       17.950       17.950       17.950       17.950       17.950       17.950       17.950       17.950       17.950       17.950       17.950       17.950       17.950       17.950       17.950       10.651       10.750       10.750       10.651       10.753       10.953       10.753       10.753       10.1655 <td< td=""><td>724</td><td></td><td>13.253</td><td>9.765</td><td>18.010</td><td>17.110</td><td>12.607</td><td>23.780</td><td>22.591</td><td>16.646</td><td></td><td>28.700</td><td></td></td<>	724		13.253	9.765	18.010	17.110	12.607	23.780	22.591	16.646		28.700	
7.420       7.043       5.194       9.550       9.555       13.550       12.873       9.455       17.962       17.953       12.         17.100       12.815       12.330       23.430       22.535       54.317       33.440       55.334       44.317       32.         29.100       27.545       20.370       38.360       55.31       15.933       34.46       55.334       46.57       34.41       55.334       46.57       33.44       46.57       33.44       55.334       35.334       35.334       35.334       35.334       35.334       35.334       35.334       35.334       35.334       35.334       35.334       35.334       35.334       35.334       35.334       35.334       35.334       35.334       35.334       35.334       35.334       35.334       35.334       35.334       35.334       35.334       35.334       35.334       35.334       35.334       35.334       35.334       35.334       35.334       35.334       35.334       35.334       35.334       35.334       35.334       35.334       35.334       35.334       35.334       35.334       35.334       35.334       35.334       35.334       35.334       35.334       35.3337       35.333       35.334	7.25		53.655	39.543	72.740	69.103	50.918	ഹ	90.6II	66.756	120.400	114.380	84.280
17.700       16.815       12.390       24.190       22.811       16.933       34.310       32.595       24.017       46.650       44.317       32.         29.100       27.545       52.370       38.260       35.470       36.543       46.       47.         25.900       24.655       18.130       38.260       36.347       26.434       46.         25.900       24.651       38.260       36.340       31.768       23.403       41.50       41.952       56.140       56.233       46.         25.900       24.651       18.130       33.460       31.768       23.462       4.767       9.040       8.588       6.328       11.430       10.853       8.         41.830       33.738       72.091       6.469       4.767       9.040       8.588       6.128       10.853       8.         41.830       33.738       72.091       71.250       55.301       56.140       91.233       57.132         114.730       1058.994       780.311       1465.451       1026.793       136.231       247.412       10.853       321.402       1732.         114.777       1058.994       70.017       71.250       55.344       91.252       14.712	72.6	_	7.049	5.194	9.850	9:358			12-873	9 485	17-950	17.062	12.572
29.100       27.645       20.370       38.260       35.347       25.732       55.434       65.434       46.         25.900       24.605       18.130       33.440       31.788       23.405       44.150       42.56       30.912       55.140       55.333       39.         25.130       24.605       18.130       33.440       31.788       23.405       44.150       41.563       30.912       55.140       55.333       59.33       59.       39.         25.331       53.306       54.103       51.788       23.405       54.160       10.859       98.       98.       78.       89.       89.       89.       89.       89.       89.       89.       89.       89.       89.       89.       89.       89.       89.       89.       89.       89.       89.       89.       89.       89.       89.       89.       89.       89.       89.       89.       89.       89.       89.       89.       89.       89.       89.       89.       89.       89.       89.       89.       89.       89.       89.       89.       89.       89.       89.       89.       89.       89.       89.       89.       89.       89.	728	_				22.981				24.017	46.650	44.317	32.655
25.900       24.605       18.130       33.440       31.758       23.405       44.150       41.952       30.912       56.140       55.333       39.         5.130       4.874       3.591       56.810       6.455       4.757       9.040       8.568       5.328       11.430       10.859       8.         41       5.30       31.378       12.531       55.810       56.346       9.040       8.568       6.328       11.430       10.859       8.         41       5.301       31.378       12.5351       55.800       53.001       71.250       55.500       9.475.160       91.238       167.257         1114       730       1058.994       78.011       12.55       104.75       14.465       8351.402       1738       67.172         Average       Growth       Rate       97-01(%)       7.104       01-05(%)       5.834       06-11(%)       4.	3731				38.250	36.347				81		62.434	
130     4.874     3.591     6.810     6.469     4.757     9.040     8.583     6.328     11.430     10.859     8.       830     39.738     29.201     55.800     58.040     51.238     67.       730     1058.934     78.001     71.238     67.     60.1186     531.432     172.33     67.       730     1058.934     780.01     11.455     50.810     1393.517     417.510     1732.       730     1058.934     780.01     1393.507     50.410     11732     67.       730     1058.934     780.01     1393.507     2475.150     2531.402     1732.       730     1058.934     780.01     1365.507     55.534     97-01.50     73.142     1732.       105     6704hh     8102.50     1393.507     97-01.50     7.104     01-05.53     135.534     96-11.50     1373.142	Kolok3734				33.440	31.768						53.333	· · ·
41.830   33.738   29.231   55.890   53.096   39.123   75.000   71.250   55.500   96.040   91.233   67  114.730   1055.934   780.311   466.350   1393.508   1026.795   1947.610   1860.230   1363.327 2475.160   2851.402   1732. Average : Growth Rate   4.000   1466.350   1283.508   1044   4.000   166   3   5.834   7.000   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.44   4.	3735	ی. ی	4.874	3.591	6.810	6.459	•		•	6.328	11.430	10.859	8.001
730 [1058: 934   780. 311 [1465. 850 [1393. 508 ]1926. 795 [1947. 610 [1850. 230 [1353. 327 2475. 150 2351. 402 [1732. ge . Growth Rate 97-01 (%) 7. 104 01-05 (%) 5. 834 7. 06-11 (%) 4.	3736	41.	39.738	29.281		53.096	123	75.000	71.250	52-500		91.238	67.228
-Growth Rate   97-01(%) 7,104 01-05(%) 5.334 06-11(%)			058:994			1393.508	795	610	850.230		475.1	11	
	l	ŀ	म	Rate		1-01			11-05(%)			7	4.911

Load Forecast of Region-4

Dome         Dome <thdome< th="">         Dome         Dome         <thd< th=""><th>node</th><th></th><th>1997</th><th></th><th></th><th>2001</th><th></th><th></th><th>2:00.6</th><th></th><th></th><th>2011</th><th></th></thd<></thdome<>	node		1997			2001			2:00.6			2011	
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $		4		peak	non-coin		-	non-coin			non-coin	sys-peak	MEA peak
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	4625	-	I2.350	8.450	13.000	***	8.450	13.000	12.350	8.450	13.000	12.350	8.450
22.160         23.161         24.464         27.010         24.164         27.01         24.164         27.010         24.161         24.161         24.161         24.161         24.161         24.161         24.161         24.161         24.161         24.161         24.161         24.161         24.161         24.161         24.161         24.161         24.161         24.161         24.161         24.161         24.161         24.161         24.161         24.161         24.161         24.161         24.161         24.161         24.161         24.161         24.161         24.161         24.161         24.161         24.161         24.161         24.161         24.161         24.161         24.161         24.161         24.161         24.161         24.161         24.161         24.161         24.161         24.161         24.161         24.161         24.161         24.161         24.161         24.161         24.161         24.161         24.161         24.161         24.161         24.161         24.161         24.161         24.161         24.161         24.161         24.161         24.161         24.161         24.161         24.161         24.161         24.161         24.161         24.161         24.161         24.161         24.161 </td <td>4701</td> <td>~</td> <td>1.900</td> <td>I.300</td> <td>2.550</td> <td>~</td> <td>1.658</td> <td>3.290</td> <td>3.125</td> <td>2.139</td> <td>4 110</td> <td>3.905</td> <td>2.572</td>	4701	~	1.900	I.300	2.550	~	1.658	3.290	3.125	2.139	4 110	3.905	2.572
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	4702	ļ	20.824	14.404	28.760	27.	18.694	37.300	35.036	24.245	46.490	44.166	30.219
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	4703		14.934	10.218	20.400	19.380	13.260	26.450	25.137	17.199	33.000	31.350	21.450
73         630         21         25         877         26         95         15         65         93         55         87         56         93         55         87         56         93         55         87         56         93         55         56         93         55         83         171         56         93         55         56         55         56         56         56         56         56         56         56         56         56         56         56         56         56         56         56         56         56         56         56         56         56         56         56         56         56         56         56         56         56         56         56         56         56         56         56         56         56         56         56         56         56         56         56         56         56         56         56         56         56         56         56         56         56         56         56         56         56         56         56         56         56         56         56         56         56         56         56         56	t4704		30.847	21.106	44.420	42.199	28.873	62.230	59.176	40.489	83.640	79.458	54.356
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	4705	_	21.926	I5.002	30.280	28.755		39,810	37.820	25.877	50.090	47.585	32.559
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	c24706	29	28.092	19.221	38.780	36.841		52.540	49.913	34.151	68.930	65.484	44.805
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	k14707	42.170	40.062	27.411	55.700	52.915	_	76.790	72.951	49.914	102.690	97.555	66.749
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	4708	33	31.683	21.678	45.680	43.396		66,020	62.719	42.913	92.380	87.751	50.047
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	Natchabun 1209	+	42.836	29.309	56.520	53, 694		71.850	68.258	46.703	88.180	83.771	57.317
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		∔	17.471	11.954	23,150	21.992	15.048	29.460	27.987	19.149	36.230	34.418	23.550
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	4711	╉	3.372			4.583	3.140	6.820	.6.479	4.433	9.280	8.815	6.032
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	4715		33.231	22 737	45.800	43.510	29.770	60.730	57.693	39.475		73.492	50.284
32         730         31.093         21.275         43.800         41.610         28.470         60.610         57.579         30.371         50.670         16.637         55.73           55.920         55.920         55.921         55.921         55.921         55.921         55.920         15.027         10.304         75.55           55.920         55.027         73.365         55.040         14.610         28.616         31.135         65.23         31.60         15.027         71.260         73.37         59         167.739         160.830         150.830         155.789         145.789         146.759         31.135         160.532         33.789         147.739         10.61.610         55.447         56.620         73.789         147.7420         10.5.23         23.789         147.7420         146.639         288.260         275.847         187.365         33.789         23.17         20.01         55.789         147.7420         70.24         56.73         147.7420         70.24         56.73         56.73         56.73         56.73         56.73         56.73         56.73         56.73         56.74         57.73         56.75         167.743         71.320         71.73         56.73         56.75         16.	4719	┢	45 353	31.031	62.520	59.394	40.638	84.050	79.857	54.639		103.284	70.558
55         520         53         124         36         72         060         68         45         330         83         473         60         55         116         110         110         304         75           81         470         77         396         52         55         13         80         93         668         67         52         131         80         147         87         72         100         133         37         397         501           92         090         87         486         55         55         120         55         13         136         145         57         55         133         136         137         53         37         39         37         53         37         39         37         55         13         15         13         56         13         145         160         44         160         41         55         13         56         17         26         13         15         13         13         15         13         13         13         13         13         13         13         13         13         13         13         13	4714	+-	31,093	21.275	43.800	41.610	28.470	60.610	57.579	39,397	80.670	_	52.436
81         470         77         356         52.356         103.880         98.666         67.522         131.550         125.258         83.733         733         75.337         75.337         75.337         75.337         75.337         75.337         75.337         75.337         75.337         75.337         75.337         75.337         75.337         75.337         75.337         75.337         75.337         75.337         75.337         75.337         75.337         75.337         75.337         75.337         75.337         75.337         75.337         75.337         75.337         75.337         75.337         75.337         75.337         75.337         75.337         75.337         75.337         75.337         75.337         75.337         75.337         75.337         75.337         75.337         75.337         75.337         75.337         75.337         75.337         75.337         75.337         75.337         75.337         75.337         75.337         75.337         75.337         75.337         75.337         75.337         75.337         75.337         75.337         75.337         75.337         75.337         75.337         75.337         75.337         75.337         75.337         75.337         75.337         <	1717	╞	53.124	36.348	72.050	58.457	46.839	93 130	88.473	60.535	116.110	_	75.472
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $		81 470	77.396	52.956	103.880	98.686	67.522	131.850	125.258	85 703	160.830	152.789	104.540
92         030         87.486         59.855         120.640         114.608         78.416         149.570         141.807         97.026         178.040         160         155.254         355.534         355.354         355.354         355.354         355.354         355.354         355.354         355.354         355.354         355.354         355.354         355.354         355.354         355.354         355.354         355.354         355.354         355.354         355.354         355.354         355.354         355.354         355.354         355.354         355.354         355.354         355.354         355.354         355.354         355.354         355.354         355.354         355.354         355.354         355.354         355.354         355.354         355.354         355.354         355.354         355.354         355.354         355.354         355.354         355.354         355.354         355.354         355.354         351.750         351.750         361.430         351.750         361.430         351.750         351.430         351.750         351.430         351.750         351.430         351.750         351.430         351.750         351.430         351.750         351.430         351.750         351.430         351.750         351.430	ł	0	35 027	23.966	47.980	45.505	31.135	62.050	58.948	40.332	77.260	73.397	50.219
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	4720	┢	87.485	59.853	120.640	114.608	78.416	149.	141.807	97.026	178.040		115.726
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		26.240	24.928	17.056	34.050	32.357	22.139	44.150	41.952	28.704		_	
51         780         49         191         33         65         67         74         80         83         105         56         81         105         105         70         103         71         46         73         56         87         71         80         81         15         64         15         56         81         105         10         13         017         24         610         23         37         46         71         46         53         23         27         10         10         13         017         24         610         23         33         410         23         33         41         23         31         15         60         61         73         33         31         56         64         13         017         440         53         33         418         26         50         11         17         440         53         43         23         31         17         430         17         440         53         43         26         56         51         10         10         10         10         10         10         10         10         10         10         10 <td>-34725</td> <td>177.42.0</td> <td>168.549</td> <td>115.323</td> <td>225.690</td> <td>214.406</td> <td>146.699</td> <td>288.260</td> <td>273.847</td> <td>187.369</td> <td></td> <td></td> <td></td>	-34725	177.42.0	168.549	115.323	225.690	214.406	146.699	288.260	273.847	187.369			
32         600         30.970         21.130         42.730         40.553         27.775         56.330         53.551         35.647         71.320         6.7746         84.10           11<510	-24723	51.780	49.191	33.657	57.500	64.125	43.875	87.480	\$3.105	56.362	108.790	103.351	70.714
11.610         11.029         7.647         15.350         14.533         9.978         20.010         13.010         13.007         24.510         23.379         15.504         15.504         15.506         11.506         11.506         11.506         11.506         11.507         24.510         23.378         15.504         9.308         17.480         15.506         11.566         11.566         11.566         11.566         11.566         11.566         11.566         11.566         11.566         11.566         11.566         11.566         11.566         11.566         11.566         11.566         11.566         11.566         11.566         11.566         11.566         11.566         11.566         11.566         11.566         11.566         11.566         11.566         11.566         11.566         11.566         11.566         11.566         11.566         11.566         11.566         11.566         11.566         11.566         11.566         11.566         11.566         11.566         11.566         11.566         11.566         11.566         11.566         11.566         11.566         11.566         11.566         11.566         11.566         11.566         11.566         11.566         11.566         11.566         11.566 <td>0447.26</td> <td>32</td> <td>30.970</td> <td>21.190</td> <td>42.730</td> <td>40.593</td> <td>27.775</td> <td>56.380</td> <td>53.561</td> <td>35.547</td> <td>71.320</td> <td>67.754</td> <td>46.358</td>	0447.26	32	30.970	21.190	42.730	40.593	27.775	56.380	53.561	35.547	71.320	67.754	46.358
8         7:50         8.313         5.688         11.250         10.688         7.313         14.320         13.604         9.308         17.480         77.406         52.           38         880         36.936         25.272         50.510         47.995         32.832         65.440         62.168         42.536         81.480         77.406         52.           51         780         93.101         33.677         50.610         54.377         18.650         54.377         18.83         18.480         77.406         52.           51         780         93.101         13.673         87.887         87.480         83.106         52.333         40.440         18.370         70.           51         760         52.156         12.7370         121.002         82.781         162.300         10.           54<90	4730	=	11.029	7.547	15.350	14.583	9.978	20.010	19.010	13.007	24.610	23.379	15,997
38         88         936         25         27         61         47         985         31         480         77         496         57         490         57         490         57         490         57         490         51         480         77         490         51         480         77         490         51         56         50         51         56         56         55         56         103         310         70         490         21         20         105         31         156         56         56         56         56         56         56         56         56         56         56         56         56         56         56         56         56         56         56         56         56         56         56         56         56         56         56         56         56         56         56         56         56         56         56         56         56         56         56         56         56         56         56         56         56         56         56         56         56         56         56         56         56         56         56         56         56 <td>4731</td> <td>8</td> <td>8.313</td> <td>5.638</td> <td>11.250</td> <td>10:588</td> <td>7.313</td> <td>14.320</td> <td>13.604</td> <td>9.308</td> <td>- 7</td> <td>97</td> <td>11.362</td>	4731	8	8.313	5.638	11.250	10:588	7.313	14.320	13.604	9.308	- 7	97	11.362
20.020         19.019         12.013         25.660         24.377         16.679         32.820         31.179         21.333         40.440         33.416         70.           61.780         49.191         33.657         67.500         64.877         10.337         70.70         70.55         82.791         103.370         70.           61.780         49.191         33.657         67.500         69.977         47.879         99.810         82.791         162.000         153.960         70.           74.674         95.667         87.475         99.810         82.791         152.000         153.933         23.353         23.353         23.563         23.563         23.563         23.563         23.563         23.563         23.563         23.563         23.563         23.563         23.563         23.563         23.563         23.563         23.563         23.563         23.563         23.563         23.563         23.563         23.563         23.563         23.563         23.563         23.563         23.563         23.563         23.563         23.563         23.563         23.563         23.563         23.563         23.563         23.563         23.563         23.563         23.563         23.563         23.5	4732	38	36.936	25.272	50.510	47.985	32.832	65.440	62.168	42.536	81.480	1	52.962
51         74         71         53         106         56.862         103.810         103.370         103.370         103.370         103.370         103.370         103.370         103.370         103.370         103.370         103.370         103.370         103.370         103.370         103.370         103.370         103.370         103.370         103.370         103.370         103.370         103.370         103.370         103.370         103.370         103.370         103.370         103.370         103.370         103.370         103.370         103.370         103.370         103.370         103.370         103.370         103.370         103.370         103.370         103.370         103.370         103.370         103.370         103.370         103.370         103.370         103.370         103.370         103.370         103.370         103.370         103.370         103.370         103.370         103.370         103.370         103.370         103.370         103.370         103.370         103.370         103.370         103.370         103.370         103.370         103.370         103.370         103.370         103.370         103.370         103.370         103.370         103.370         103.370         103.363         103.323 <t< td=""><td>4733</td><td>1</td><td>19.019</td><td>13.013</td><td>25.660</td><td>24.377</td><td>5</td><td>32,820</td><td>31.179</td><td>21 333</td><td>40 440</td><td>38.418</td><td>26.286</td></t<>	4733	1	19.019	13.013	25.660	24.377	5	32,820	31.179	21 333	40 440	38.418	26.286
74         710         70.557         48.276         96.400         91.580         62.660         127.370         121.002         82.781         162.000         123.389         83.953         123.389         83.953         122.389         83.953         122.389         83.953         122.389         83.953         122.389         83.953         122.389         83.953         122.389         83.953         122.389         83.953         83.953         83.953         83.953         83.953         83.953         83.953         83.953         83.953         83.953         83.953         83.953         83.953         83.953         83.953         83.953         83.953         83.953         83.953         83.355         83.136         83.355         83.17.01         11.01.17         11.01.11         11.01.11         11.01.11         11.01.11         11.01.11         11.01.11         11.01.11         11.01.11         11.01.11         11.01.11         11.01.11         11.01.11         11.01.11         11.01.11         11.01.11         11.01.11         11.01.11         11.01.11         11.01.11         11.01.11         11.01.11         11.01.11         11.01.11         11.01.11         11.01.11         11.01.11         11.01.11         11.01.11         11.01.11         11.01.11 <td>1-12734</td> <td></td> <td>49.191</td> <td>33.657</td> <td></td> <td>64.125</td> <td>43.875</td> <td>87.480</td> <td>83.106</td> <td>56.862</td> <td>108.810</td> <td>103.370</td> <td>70.727</td>	1-12734		49.191	33.657		64.125	43.875	87.480	83.106	56.862	108.810	103.370	70.727
54         900         52.155         35.655         73.660         69         97.87         47.879         99.810         94.819         64.877         128.830         132.533         53.953         23.953         23.953         23.953         23.953         23.953         23.953         23.953         23.953         23.953         23.953         23.953         23.953         23.953         23.953         23.953         23.953         23.953         23.953         23.953         23.953         23.953         23.953         23.953         23.953         23.953         23.953         23.953         23.953         23.953         23.953         23.953         23.953         23.953         23.953         23.953         23.711         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         11.1         <	wan4741	74 270	70.557	48.276	96.400	91.580	62.660	127.370	121.002	82.791	162.000	153.900	105.300
15         650         14         905         10         19         475         13         225         27         53         560         33         563         33         563         33         563         35         75         35         35         75         76         35         76         35         76         35         76         35         76         35         35         35         35         35         35         35         35         35         35         35         35         35         35         35         35         35         35         35         35         35         35         35         35         35         35         35         35         35         35         35         35         35         35         35         35         35         35         35         35         35         35         35         35         35         35         35         35         35         35         35         35         35         35         35         35         35         35         35         35         35         35         35         35         35         35         35         35         35	4743	54	52.155	35.685	73.660	69.977	47.879		94.819	64.877	128-830	122, 389	
8         250         7         837         5.363         10.710         10.175         6.962         14.150         13.442         9.198         17.970         17.971           19<000	4744	15	14.905	10.199	20.500	19.475	13.325		26.154	17.895	35.750	33.963	23.238
19.000         18.005         12.935         26.450         25.127         17.193         35.930         34.134         23.355         96.920         44.574           35.050         34.286         22.459         45.838         31.355         67.070         55.16         23.355         90.200         44.574           35.050         34.286         22.450         45.838         31.355         67.070         55.16         23.455         90.200         45.139           37.55         56.045         31.755         31.975         31.555         67.513         39.551         74.180         74.413           37.590         35.426         42.239         47.600         45.720         30.940         60.561         57.513         39.351         74.180         70.471           37.290         35.426         40.320         38.304         26.208         30.820         38.399         26.273         38.494           40.240         38.228         261.461         40.320         38.304         26.208         38.399         26.273         240.520         38.494           1393         50.1164         38.304         25.228         38.398         26.273         29.39.560         27.80.176         176.471	4748	α.	7.837	5.363	10.710	10.175	6.962	14.150	13 442	9.198	17-970		11.681
36.050         34.286         23.459         48.250         45.838         31.563         67.070         63.715         43.595         90.230         85.719           25.560         24.255         15.410         31.757         27.257         30.940         25.560         27.157         25.450         43.595         43.595         43.595         43.595         43.595         43.595         43.551         43.551         47.500         48.595         47.600         48.595         47.600         48.595         47.600         48.595         47.600         48.595         47.600         48.595         47.600         48.595         47.600         48.520         48.546         47.471         47.600         48.595         47.471         47.600         48.595         47.471         47.471         47.600         48.595         47.471         47.471         47.471         47.471         47.471         47.471         47.471         47.471         47.471         47.471         47.471         47.471         47.471         47.471         47.471         47.471         47.471         47.471         47.471         47.471         47.471         47.471         47.471         47.471         47.471         47.471         47.471         47.471         47.471	4751	• • •	18 905	12 935	26.450	25.127	17.193	35-930	34.134	23.355	46.920		30.498
25         560         24         282         15         161         31         07         167         51         43         859         1         77         157         51         430         48.859         1         37         157         51         430         70         47.11         37         157         51         33         351         74         180         70         71         37         157         51         33         351         74         180         70         71         36         39         351         74         180         70         71         36         39         351         74         50         70         434         434         133         351         35         351         33         351         74         50         70         434         434         133         353         351         340         70         361         434         434         1393         353         351         340         350         320         38         383         383         383         383         383         383         383         383         383         383         383         383         383         383         383<	Va 1.1752	-	34, 286	23.459	48.250	45.838	31.363	67.070	63 716	43 595	90.230	85.719	58.650
37         290         35.426         24.239         47.600         45.220         30.940         60.540         57.513         39.351         74.180         70.411           1         40.240         38.238         26.116         40.320         38.904         25.208         40.420         38.399         26.213         40.353         40.41           1         39.351         26.116         40.320         38.904         25.208         30.40         26.210         38.44           1         39.351         151.1432         20395         26.210         28.494         175.19         175.19           1         39.351         31.757         52.0164         93.8338         28.028         28.114.11         37.757         175.19         175.19           1         39.351         31.55         50.743         39.338         28.028         28.028         28.028         28.028         28.028         28.028         28.028         28.028         28.028         28.028         28.028         28.028         28.028         28.028         28.028         28.028         28.028         28.028         28.028         28.028         28.028         28.028         28.028         28.028         28.028         28.028	4754	+-	24.282	15.514	32.710	31-075	21.262	· •	39.	27.157	51.430	48.859	33.430
46.240         38.228         26.156         40.320         38.304         26.208         38.309         26.273         40.520         38.494           1335.520         131.402         132.323         232.338         230.4126         28.238         201.412         28.2012         28.1111.432         24.1111.431         28.233         201.125         21.1128	4755		35.426	24.239		45.220	30.940	60.540		39.351	74.180		48.217
1393.620 1311.361 397 403 1797 520 1694 990 1159 938 238 236 2208 617 1511 432 2939 500 2780 175 1 	4882	4	38.228	26.156	320	38.304	26.208			26.273	40 520		25.338
$\frac{1}{2}$	3 2 7	+=	1311 361	\$97.403	520	1694 990	1159.938		2208.617	1511.432	2939 500	2780.	1902.225
		].		0.4.0		- 10-2 b	5.222		01-96 (%)			_	4.683

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Load Forecast of Region-1 Central Area

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	MEA peak	29-592	2.000	47.152	98.808	38.400	466.944	87.360	77.632	98.984	69.352	58.424	51.840	49.544	46.784	25.580	33.936		121.168	51.184	33.152	278.480	460.344				2.952
2011	2	35.141	2.375	55.993	117.335	45.600	554.496	103.740	92.188	117.544	82.	69.379	81.560	58.833	55-556	30.495	40.299	74.053	143.887-	60.781	39-368	330.695	546.658			330	05-11 (%)
	ĉ	36.990		58.940	123.510	48.000	583.580	109.200	97.040	123.730	86, 690	73.030	84.800		58.480	: 32.100	42.420	77.950	151.460	63.980	41.440	348.100	575.430	577.400	654.310	4093.110	
	MEA peak	23.736		46.616	88.975	38:400	448.352	87.360	65.440	76.232	58.992	47.552	42.280	39.895	36,720	19.280	28-568	50.008	96.112	43.112	26.448	265.600	410.944			2042.624	3.724
2006	sys-peak	28.187		55.357	105,659	45.600	532.418	103.740	11.710	90.526	70.053	56.468	50.207	47.376	43.605	22.895	33.925	59.384	114.133	51.195	31.407	315.400	487.996			2425.616	01-06(%)
	non-coin	29.570	2.500	58.270	111.220	48.000	560.440	109.200	81.800	95.290	73.740	59.440	52:850	49.870	45.900	24.100	35.710	62.510	120.140	53.890	33.060	332.000	513.680	460.690	523.270	3537.240	
	MEA peak	18.248	2.000	46.040	80,712	38,400	407.592	87:360	54.368	56.400	49.144	37.648	32.696	31.120	28.248	13.888	22-944	38.448	70.184	34.624	20.088	235.984	346.872			1753.008	5.145
2001	sys-peak	21.670	2.375	54.672	95.846	45.600	484.016	103.740	64.562	66.975	58.359	44.707	38.826	36.355	33.545	16.492	27.246	45-657	83.344	41.116	23.854	280.231	411.910			2081.697	97-01 (%)
	non-coin	22.810	2.500	57.550	100.890	48.000	509.490	109.200	67.960	70.500	61.430	47-060	40.870	38,900	35.310	17.360	28.680	48.060	87.730	43.280	25.110	294.980	433.590		Ξ.	2946.250	
· ·	MEA peak	14.096	2.000	33.552	75, 160	38.400	384.800	87:350	45.584		41.576	30-352		24.648	22.584	10.328	18, 295	29.704	50.232	27.608	15.376	187.840	254.752			1463.104	Rate
1997	sys-peak &	16 739	2.375	39.843	89.253	45.600	456 950		55.318	50.673	49.372	36.043	29.906	29.269	26.819	12.265	21 727	35.274	59.650	32.784	18.259	223.060	302.518			1737.436	Growth
	non-coin	17.620	2.500	41.940	93.950	48.000	481-000	109.200	58.230	53-340	51.970	37 940	31.480	30.810	28.230	12.910	22.870	37,130	62.790	34.510		234.800	318 440	271 880	309.830	× .	986
node		5604	5605	5701	5703	5704	5705	5706	5707	5708	5709	5710	5711	5712	5713	5714	5715	5716	5717	5719	5724	5726	5727				
substation hode		Avutthava-2 5604	Phachi (VOA)	1.			2	.		1 ×		-	1	Ŀ.	Phraphutthab5713	Chaibadan 571	Doembarg Nan5715	Avutthaya-1 5716	Bang Pa In-1671	Suphan Buri 5719	Nakhon Nayok572	Ifhalan-3	- 0	Ranesit-69	Rangsit-115		

Load Forecast of Region-1 Eastern Area

Ť	×	~	~	22	2	9	30	36	32	2	7	85	88	2	32	و	56	26	272	10	Ţ	44	
	MEA peak	116.672	42.312	56.832	113.120	57.896	87.256	309.855	184.032	8.080	54.544	42.368	103.488	91.312	174.592	77.456	89.056	278.576	94.27	262.640	425.864	2670.144	3.743
2011	sys-peak	138.548	58-246	67.488		68.752	103.515	367.954	218.538	9.500	64.771	50.312	122-892	108.433	207.328	91:979	105.754	330.809	긞	311.885		3170.756	06-11 (%)
	- 1	145.840	52.890	71.040	141.400	72.370	109.070 ⁻	387.320	230.040	10.000	68.180	52.960	129.360	114.140	218.240	96.820	111.320	348.220	117.840	328.300	711.710	3517.050	-
	٩	91.575	34.888	46.152	85.936	45.384	\$7.304	270.640	143.334	8.000	42.128	39.952	87.600	70.000	132.768	59.016	70.352	204.224	81.280	224.440	401.224		4 717
2005	beak	108.747	41.430	54.805	102.049	53.893	79.923	321.385	170.174	9.500	50.027	47.443	104.025	83.125	157.662	70.081	83.543	242.516	96.520	266.523	476.453	2515.824 2205.158	01-06 (%)
		114.470	43.610	57,690	107.420	56.730	84.130	338.300	179.130	10.000	52.660	49.940	109.500	87.500	165.960	73.770	87.940	255.280	101.600	280.550	670.530	2326.7I0	
	WEA peak	69.648	27.288	36.440	62.712	34.784	50.128	227.344	107.152	8.000	31.280	33.056	73.600	51.504	96-744	43.200	53.736	124.088	51.440	181.000	369.072	1732.216	505 9
2001	sys-peak	82.707	32:405	43.272	74.471	41.306	59-527	269.971	127.243	9.500	37.145	39.254	87.400	61.161	114.884	51 300	63.811	147.355	61.085	214.938	438.273	2057-007	97-01 (%)
	non-coin	87.050	34.110	45.550	78.390	43.480	62.660	284.180	133.940	10.000	39.100	41.320	92,000	64.380	120.930	54.000	67.170	155.110	64.300	226.250	620.340	2324.270	
	MEA peak	54.144	21.224	29.432	47.176	27.680	37.952	186.350	80.560	8.000	23.840	24.544	63.384	38.464	71.192	32,552	41.512	60.384	22.000	133.656	313.624	1317.680	
1997	sys-peak	64.296	25.204	34.951	56.021		45.068		95.665	9.500	28.310	29.145	75.269	45.676	84 541	38.655		1.	26.125	158.717	372.428	1564.745	Growth
	non-coin	67.680	26 530	36 790	58.970	34.600	47.440	232 950	100.700	10.000	29.800	30.680				40.690	51.890	75.480	27.500	167.070		18.06 100	1
n inode		sao6702	1156703	Nak6704	6706	6707	6708	87.09			t.		5715	6716	I.,		1	T	6734	1	Ι.	r	
substation		hachoengsao6702	rachin Buri6703	2441400	hon Buri	i Bacha	an Rune	o Phai	and lamune	attahin-	attahin-2	2-100 a	avon - 1	2010	4004 Pahin	1011 01101	hom Thien	rachin Bi		lone Mai	10	2 22 22	

Load Forecast of Region-1 Western Area

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	MEA peak	532.488	181.040	177-216	84.952	102.480	59.520	302.488	68.416	47.920	84.792	1.400	52,520	182.096	76.792	72.192	35.768	28.240	5.784	114.600	59.336	129.176	157.616	2564.832	4.238
2011	sys-peak	632.329	214.985	210.444	100:881	121.695	82.555	359.205	78.869	56.905	100.690	1.562	62.368	216.239	91.190	85.728	42.475	33.535	6.859	136-058	70.462	153.397	187.169	3045.738	06-11 (%)
	non-coin	655.610	226.300	221.520	106.190	128:100	85.900	378.110	83.020	59, 900	105.990	- 1.750	65.650	227.620	95.99D	90.240	44.710	35-300	7.230	143.250	74.170	161.470	197.020	3206.040	
	MEA peak	429.272	148.328	144.768	61.792	82 640	55.368	240.055	52.512	44 524	71.728	1,152	41.556	141.912	63.264	57 912	28.240	22.200	5.576	92.384	46.864	122.064	130.056	2084.158	5.059
2006	sys-peak	509.761	I76.140	171.912	73 378	<b>S8.135</b>	65 750 {	285.965	62.358	52.991	85.177	1.358	49.465	168.520	75.126	68.771	33.535	26.352	6-521-	109.706	55.414	144.951	154.442	2474.949	01-06(%)
	hon-coin b	536.590	185.410	180.950	77.240	103.300	69.210	300.070	65,640	55.780	89.660	1.440	52.070	177.390	79.080	72.350	35.300	27.750	6 970	115.480	58.330	152.580	162.570	2605.210 2	
	MEA peak k	331.608	115.048	109.016	42.664	63.840	42.488	183.624	39.760	40.368	57.123	0.380	32.120	195.936	49 896	45 160	21.440	16.768	5.296	71.368	35.272	115.680	102.056	528.416 2	6.882
2001	sys-peak	393.785	136.520	129.457	51.851	75.810	50.454	218.053	47.215	47.937	67.839	I.045	38.143	125.799	55.251	53.628	25.460	19.312	5.289	84.749	41.885	137.370	121.191	933.744	97-01 (%)
	non-coin s	414.510	143.810	136.270	54:580	79.800	53.110	229.530	49.700	50.450	71.410	1.100	40.150	132.420	62.370	56.450	26.800	2.0.96.0	6.620	89.210	44.090	144.500	127.570	035.520 1	6
	MEA peak h	257.008	88.216	75.424	32.480	49.480	32.992	142.408	30.328	36.336	44.568	0.664	25.120	79.408	38.728	35.896	16.304	12.784	5.008	55.312	26.832	83.008	79.488	1247.792 2	Rate
1997	sys-peak M		104.756	39.566	38.570	58.758	39.178	169.110	35.015	43.149	52.925	0.789	29.830	94.297	45.989	42.526	19.361	15.181	5.947	65.683	31.863	98.572	94.392	481.753 1	Growth R
	non-coin s		110.270	94.280	40.600	61.850	41.240	178.010	37.910	45.420	55.710	0.830	31.400	99.260	48.410	44.870	20.380	15.980	6.260	69.140	33.540	103.760	99.360	559.740 1	Average G
on hode	Ŀ	n-1 1702	Sakhon7703	Sakhon7704	Songkh7705	Chais7706		7708	amphaene Sal709	g 7710	anchanaburi[711]	ind 7713	atchaburi-17714	atchabur i-27715	uri 7716	1	1719	Кh	m 7724	n-2 7727	7728	han 7729	Sakhon 730 i		Ÿ
kubstation		Sam Phran-1	+	Samut Sa			Banbong"	Banpong-2	Kamphaen	Tha Muang	Kanchana	Srinagarind	Ratchabu	Ratchabu	Phetchabur	Cba Am	Pranburi	Prachuan	Khao Laem	Sam Phran-2	Hua Hin	Bang Saphan	Samut Sal		

## Table 6-1-2

total capacity of reactive power compensator (shunt capacitor) at each substation in the Greater Bangkok Area and vicinity area

CHECTATION	HODE CODE			ACITY OF	SHUNT CAP		(MVA)
SUBSTATION	NUDE CODE	BUS VOLTAGE		plan		this	study
NORTH BANGKOK	1801	230KV	1997	2001	2006	000 00	2011
HOUTH BUNGLOV	1601		0.00	0.00	300.00	300.00	360.00
	1611	69KV	90.00	120.00	150.00	120.00	210.00
LAT PHRAO	1802	69KV 230KV	63.06	120.00	150.00	120.00	210.00
LAI FIINAU	1602	230KV 69KV	0.00	120.00	240.00	210.00	360.00
	1612	69KV	97.80	120.00 120.00	120.00	.90.00	150.00
and a second	1622	69KV	33.13	60.00	$120.00 \\ 120.00$	90.00 90.00	150.00 150.00
BANG KAPI	1803	230KV	132.25	120.00	240.00	240.00	300.00
	1603	69KV	132.25	150.00	180.00	210.00	210.00
and the second	1613	69KV	99.19	150.00	180.00	210.00	210.00
BANG PHLI	1804	230KV	132.25	120.00	300.00	150.00	360.00
	1704	115KV	66.13	120.00	90.00	90.00	90.00
and the second	1714	115KV	33.06	60.00	90.00	90.00	90.00
	1604	69KV	130.93	150.00	150.00	150.00	180.00
SOUTH BANGKOK	1805	230KV	132.25	240.00	300.00	270.00	300.00
	1705	115KV	66.12	120.00	60.00	60.00	60.00
	1715	115KV			30.00	30.00	30.00
	1605	69KV	93.07	150.00	150.00	120.00	
	1615	69 K V	66.13	90.00	150.00	120.00	150.00
	1625	69KV	66.13	90.00	120.00	120.00	150.00
SOUTH THON BURI	1806	230KV	132.25	240.00	300.00	300.00	360.00
	1606	69KV	99.19	60.00	90.00	90.00	
	1616	69 K V	66.13	60.00	90.00	90.00	
	1626	69KV		30.00	90.00	90.00	
BANGKOK NOI	1807	230 K V	132.25	180.00	240.00	240.00	
	1707	115KV	0.00	0.00	0.00	0.00	
	1607	69KV	66.13	120.00	120.00	120.00	180.00
017 VO7	1617	69KV	66.13	120.00	120.00	120.00	
SAI NOI	1808	2 3 0 K V	0.00	180.00	240.00	210.00	
	1828	230KV		~~	0.00	~~	
RANGSIT	1708	115KV 230KV	132.25	0.00	0.00	0.00	
NANUSII	1709	230KV 115KV	99.19	120.00 120.00	240.00	240.00	300.00
	1719	115KV	66.13	90.00	150.00 150.00	150.00 150.00	180.00 180.00
Participant de la composition de la comp	1609	69KV	131.59	120.00	150.00 150.00	150.00 150.00	210.00
	1619	69KV	66.13	120.00	150.00	150.00	210.00
NONG CHOK	1810	230KV	198.38	240.00	240.00	240.00	
	1820	230KV			0.00	0.00	0.00
	1710	115KV	66.13	90.00	90.00	60.00	90.00
ON NUCH	1811	230KV	0.00	0.00	0.00	0.00	0.00
	1741	115KV		90.00	120.00	90.00	120.00
RATCHADAPHISEK	1834	230KV	0.00	0.00	0.00	0.00	120.00
	1634	69 K V	99.19	240.00	120.00	120.00	240.00
	1644	69KV		·	120.00	120.00	240.00
CHAENG WATTHANA	1835	2 3 0 K V	0.00	0.00	0.00	0.00	120.00
	1735	115KV	132.25	180.00	240.00	210.00	360.00
THEPARAK	1836	230 K V	0.00	0.00	0.00	0.00	0.00
	1736	115KV	33.06	30.00	60.00	60.00	60.00
	1636	69KV	33.06	30.00	60.00	60.00	60.00
ANGTON 1	5801	2 3 0 K V	66.13	120.00	120 00	100 00	150 00
ANGTON 2	5802	230KV 230KV	132.25	120.00	120.09 120.00	120.00	150.00
SARABURI 2	5802	230KV 230KV	132.25	120.00	180.00	120.00 180.00	210.00
BANG PA-IN 2	5804	230KV 230KV	66.13	60.00	120.00	120.00	210.00
THALAN 3	5805	230KV	132.25	120.00	180.00	120.00	150.00
e an	0000	LUUNY	192.20	120.00	100.00	100.00	610.00
BAN PONG 2	7.801	230KV	0.00	0.00	0.00	0.00	0.00
RATCHABURI 2	7802	230KV	0.00	120.00	120.00	120.00	120.00

# Table 6-2-1 generator constants

enerator		TIRE	МУА	H	Xd	Xď	Xď	Xq	<u>Xq</u>	Xq' X	<u>X1</u> X	Tdo	Tdo' sec.	Tqo	Tqo' sec.
EGION-1				sec.	<u>×</u>	<u>×</u>	*	X	<u>, y</u>		<u></u>	SEC.	sec.	sec.	sec.
ORTH BANGKOK		2	96	1.9277	196.7	18.3		194.5	25.8	11	9.8	6	0.05	1.5	0.0
UNITE DATIONUA	······		105	1.7624	196.7	17.4	10.4	194.5	24.7	11	8.7	6	0.05	1.5	0.0
OUTIL BANGKOK		2	250	3.2688	215.2	38.1	26.5	211.8	55	26.5	22.3	5.7	0.05	1.5	0.0
		3	415	3.1273	204	42.3	27.6	201.8	60.6	27.6	22	6.5	0.05	1.5	0.0
	C.C1(GT) C.C1(ST)	2	119.3	8.4	158	26	18	161	32	18	10	5.5	0.04	1.5	0.0
	C.C. 1 (ST)		135.5	3.2	166	26	18	159	56.5	18	14	-5.	0.04	1.5	0.0
	C.C2(GT) C.C2(ST)	2	238.52	8.4	168	26	18	161	32	18	10	5.5	0.04	1.5	0.0
	C.C2(ST)		271.06	3.2	166	26	18	159	56.5	18	14	5	0.04	1.5	0.0
RESION-2		2	22.5	3,0002	118	26	21	77		21	16	5.3	0.06		0.
HULABHURN		3	14	2.6828	84.2	40.8	30.8	64		30.8	15.6	4.9	0.05		0.
SIRINDHORN JBOLRATANA		3	10.5	2.1767	110	23	18	65		18	14	5	0.05		0.
VAH PUNG		2	3.5	3.5248	120	32.9	22	70		22	15	8	0.03	·	0.2
YAN NGUN		2	17.5	1.9313	120	35	28.5	70		28.5	21	5	0.05	11.0	0.
		3	50	2.878	110	33.3	21.9	55	11.	21.9	14	5	0.06	·	Ū,
NAM PHONG	C.C. 1.2(GT)	4	. 133.6	7.6281	168	19.5	16	161	32	16	10	5.5	0.04	1.5	0.0
	C.C. 1.2(SI)	2	142.4	5.3383	166	19.1	15.6	159	56.5	15.6	14	5	0.04	1.5	0.0
PAK HUN		4	36	1.3327	99	29	22	62	<u> </u>	22	19	5.3	0.06	<u> </u>	0.
LAM TAKHONG		4	278	6.8624	106	29.4	18.9	60		18.9	12	7.4	0.05	1	0.
REGION-3	· · · · · · · · · · · · · · · · · · ·	<u>-</u> -	28.2			- 17 - 0	17.4	65		17.4	13	5	0.06		D.
BANG LANG		3		5.8628	110	27.8 28.8	19.5	<u>05</u>		19.5	13	7.4	0.08		0
RAJJAPRABHA		- 3	89	3.3169 2.8252	102	20.0	21	68		21	20	6.5	0.06	1	0.
KAENG KRUNC KHANON	C.C (GT)	4	132	8.4	168	26	18	161	32	18	10	5.5	0.04	1.5	0.0
NUAUUN	C.C. (ST)		265	3.2	166	32.2	23	159	56.5	23	14	5	0.04	15	0.0
	<u>и</u> т		88.3	3.08	218.6	31.8	24.6	207.7	41.3	24.6	18.6	6	0.05	1 5	0.0
	N.T.		88.3	3.08	180	22.2	17	170	. 30	14.6	17	6	0.05	1.5	0.0
R-3 C.C.	C.C1.2(GT)	4	119.26	8.4	158	26	18	161	32	18	10	5.5	0.04	1.5	0.0
	C.C1.2(ST)	2	135.53	3.2	166	26	18	159	56.5	18	14	5	0.04	1.5	0.0
SURAT THANI			42	3.9138	201.3	20.6	13.1	190.7	29	13.1	8.5	6	0.05	1.5	0.0
REGION-4					11 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1			· .		· ·	de la tra	1		1 · · · · · ·	
BILUMIBOL	unit 1-6	6	13.7	2.8046	100.6	33.9	21.8	65.6	· · · ·	21.8	16.4	6	0.05		0.
	unit-7		121.8	3.7999	120.2	30.4	20	71	فمعنجب	20	15.3	7.8	0.05		0.1
	unit-8		186.7	6.8624	105	34	23	65 60		23	<u>12</u> 17	7.4	0.05		0.1
SIRIKIT		4	132	7.4941	101	27.8	22.2	66		22.2	16	5.4	0.05		0.1
MAE TAENG		2	15.3	2.8	107.	32	22	65		22	10	7.4	0.05		Û.
NAM KHEK Lan krabu		3	20.8	7.6759	200	20	14	190	26	14		6	0.05	15	0.0
LAN MARDU		4	32	6.3073	180	20.2	11.5	178	26 3	11.5	9	6	0.05	1.5	0.0
NAE HOH 2		3	83.3	3.0143	186.5	22.1	15.7	183.1	31 7	15.7	11.4	6	0.05	1.5	0.0
MAE HOH 3		4	167	2.7641	159.	23.6	17.4	152	30.7	17.4	16	5.85	0.05	1.5	0.0
1110 1101 0		6	333.3	4.5934	198	25.9	19.5	180	30	19.5.	10	8.37	0.05	1.5	0.0
LAMPANG		8	333.3	4.5934	198	26.9	19.5	180	30	19.5	10	8.37	0.05	1.5	0.0
NAE LANA LUA	łĠ	2	: 90	3.55	102	28.8	19.5	65	· · ·	19.5	12	7.4	0.07		0.
NAE KHAM		2	167	2.7641	159	23.6	17.4	152	30.7	17.4	16	5.85	0.05	1.5	0.0
R-I CENTRAL												<u> </u>			
MANG NOI		6	119.3	6.72	168	26	18	161	32	18	10	5.5	0.04	1.5	0.0
R-1 EASTERN		<u> </u>		2 5 7 0 7	1 200 0	20 5	22 0	205 0	40.6	22.9	22	6.5	0.05	1.5	0.0
BANG PAKONG	thermal :	2	680 706	2.5707	208.5	28.5	22.9	205.2	40.6	22.9	16	0.5	0.05	1.5	0.0
	<u>thermal</u> C.C. (GT)	2	706	6.5957	221.6	18.5	12.9	219.4	23.8	12.9	- 10	8	0.04	2	0.0
	C.C. (ST)	2	162	3.0171	221.0	21,2	15.1	213.7	27.3	15.1	9	6	0.05	1.5	0.0
	C.C. (GI)	4	128.6	8.4	168	23.2	16.5	161	32	16.5	10	5.5		1.5	0.0
	C.C. (SI)	2	145	3.2	166	23.4	15.7	159	56 5	15.7	14	5	0.04	1.5	0.0
AO PHAL		3	850	3.5707	210	32.6	21.2	202	49	21.2	16	5	0.04		0.0
KIRIDHARN		2	7.8	0,9877	110	34.7	28.3	65		28.3	-14	5	0.05		0.
RAYONG	C.C.1-4(GT)	8	119.3	8.4	168	26	18	161	32	-18	10	5.5	0.04	1.5	0.0
	C.C.1-4(GT) C.C.1-4(ST)	4	135.5	3.2	166	26	18	159	56.5	18	14	- 5	0.04	1.5	0.0
R-1 WESTERN			·						·	L	<u> </u>		1	<b></b>	+
SRINAGARIND		3	150	3.3905	110	29	22.7		<b> </b>	22.7	19	5	0.06	1	0
		2	200	6.8624	106	29.4	18.9		1	18.9	12	7.4	0.05	1	0
THA THUNG NA		2	20.5	3.0814	140	41.5	32.7	80	+	32.7	25	5	0.06		0
KHAO LAEM	N	1 3	21.2	4 3.6048	114	33	21.3	70	+	17.6	13	5	0.06	1	0
KAENG KRACHA	N L C.C.1-3(GT)	6	238.52	3.5048	168	26	18	161	32	21.3	16	4.5	0.05	1.5	
LUNCH CENTRA	<u>C.C.1-3(ST)</u>	3	271.06	3.2	166	26	18	159	56.5	18	14	5	0.04	1.5	0.0
NEW THERMAL	0.0.1 0(01)	6	1200	3.5	210	33	22	202	49	22	16	5	0.04	1.5	0.0
		6	1200	3.5	210	33	22	202	49	22	16	5			0.0

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