Table 1-3-4 Summary of Water Balance Computation (Case-3:1968-1987)

YEAR		*<	BANG P	PAKONG	TOTAL	AE)	EXISTING FISH.	THA LAT OTHER	TOTAL I	RRIG.	LAT FISH	EXPANSION-	01AL	ENTI	FISH.	DIHER I	10.1AL
			١.	*	*		i		- 34		Ì	*	*	4	; ;	*	*
1968	⊢ > ⊒ 6	202.2	7.0	77.8	144.4	133	1.4 4.4	200 1.00 1.00 1.00	174.5	22.3	0 0	74.5	36.9	217.8	10.0	122.4	355.7
	- L	267.7	16.7	155.6	1 6	2007	1 2 2		347.0	0.08		• 0	100	5 K K K	0 4	2.772	1 0 7 7 8
1969	1 H	51.6	*	4.7	Į,	100	11.0		141.4	13.0		: :	28.4	165.8	'n	122.4	303.6
	284	191.7	12.2		281	93.9	, d	0	130,1	6.8			61.4	332,3	60	122.3	473.0
404	1 t 1 t 1 t 1	243.4	16.6		415	194.2	2.5	0,	271.5	909	•	٠.	89 7	1.867	M V	244 7	776.6
2	- >- u & z ()	196.7	1 7		780	100.5			136.6	20.0			64.8	347.4	n eo	122.3	488.0
	11	260.8	16.5		433	224.3	17.0	0	301.3	8.99			6.56	551.9	M	244.7	830.1
1971	H N	52.4	4.3		H	116.1	10.8	. 7	156.9	24		٠.	35.7	139	ທ່ເ	122 4	327.3
	A 1	204-2	23		6	102	9 (н k	138,9	22	0 0		70,	2,444	øκ	125.0	2
4 0 7 0	} ⊢ u ⊢ 3	2 0 V V	0 4		1 1	116.3	10.8	¥ +	157.2	18.7		• •	N C	194.2	'n	755.4	331.8
1	780	191.9	12.2		281	100.7		0	137.0	25.5	0		70.1	348.0	αĵ	122.3	488.8
		251.0	16.6		423.	217.0	17.1	0.0	294.2	74.2	0		103.3	542.2	m i	244.7	850.6
1973		40.5	5 7		142	130.6	11.3	4	171.9	22.2	0 0	÷.	7 9 7	213.4	vo o	122.4	351.5
		186.7	7.5		276	12.1	0,	9 0	170	0 4	> 0	; 0	4 4 0	י א אני אני	0 4	777	7 7 7
1077	J F - U - 3				\$ P	101	10,	2 6	14.7	17.6	0		32 -	168.3	'n	122.4	306.2
* * * * * * * * * * * * * * * * * * * *	= C) P			0	1001			.6.921	25.		. 4	66.7	353.1	00	122.3	7.65
		2.076			7.27	202.1	17.2	0	279.4	69.7	0	0	98.8	521.4	33.8	277	799.9
1975		67.6	7		150.		11.2		169.0	19.6	0-0		34.1	214.9	15.8	122.4	353.1
		189.4	12.2		279.		6.2	7.0	128.9	47.1	0	14.7	61.7	329.1	18.4	123.0	470.5
	TTL	257.1	16.8		459.	220.	17.4		297.9	2.99	0	Ġ.	ω (ω (277	34-2	245 4	823.6
1976		50.9	7.7		133.	66	10.8	et :	140-3	13.7	0	4	28	164	M I	7.55	501.7
		2007	12 2		290	104	ر د د	0	140 9	54.1	0 0	•	2 88 7	4,000	18	166.5	9,000
1	<u>-</u>	251.6	16.7		423	N 0	٠,٠ ٠,٠	9	7.107	0.00))) (· <	, « , «	200	1 1	122.4	5.5
1977	⊢ > ₩ £	7 P	4 0		・スカイ	2 1	2.4	10	100	100	0	14.	93.0	338	100	122.3	7.625
	 	י מ מאר			120	237	17.1	0	314.5	71.0	0	٥	1001	566.5	33.7	244 7	6 778
1078		1 K	7		138	117	10.8		158.4	17.4	0	4	31.9	191.2	15.2	122.4	328.9
		200.9	12.2				4.9		140.8	51.9	0.0	14.6	90.5	357,3	18.7	122,3	2.867
	ŢŢ	257.2	16.6		459	222	17.2	o	2662	69	0	٠.	7.86	2 6 2 6 3 6	S	7-557	827.1
1979		84.0	4.7		166	77.5	11.6	-	216	27.4	0.0	· .	1 6	286.0	0 4	1 2 4 4	777
	284	204-2	12.3		294	202	0 0		141	9.0	9 6		7 - 4	,	9 14	7 576	7 6 6 0
		288	7.		197	27.9	200		000	0 4	3 6	1 4 4 5	1 0	0.07	10.	122.4	208.3
1980		5.74	4		7 7		0 1		0 00	1 10	000	7.7	66.1	349.7	100	122.3	5.067
	× 1	0 1	, v		2 4	0	17.0	0	276.0	67.6	0	29.1	7.96	510.7	33.4	244.7	788.8
c		1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	. 4		87.	127	10.9	7	167.9	18.5	0.0	14.5	33.0	211.2	15.3	122.4	348.3
		6 661	(7		289	103	2.0	0.	139.7	54.6	0.0	74.6	69.2	357.7	18	122.3	7.867
	1	265.6	16.6		437	230.	17.3	9	307.6	73.1	0	29.1	102.2	000		, , , ,	047.0
1982		51.5	,		133	114	0. 0.1	- 4	125.6	2.22	5 C	· ·	100	7 772	. α . α	1000	7 7 7
	282	504.6	12.2		767	100	9 6	9 0	0 0 0	77.	90	. 0	106.4	8,450	33.6	244.7	833.1
		256-2	10.7		, ,	7	4 6		200	- F	0	1,4	27.6	135.7	14.2	122.4	272.2
1983		0 10	4 (7 0	ó			132.3	78.	0		65.9	339,5	18.4	123.0	480.9
	X	4 4 4 4 6	4 1		807	177	16.3	٥,	254.2	61.3	0	29.2	90.5	475,1	32.6	572	753.1
1001	- 3 - 3	100	1 -1		145	114	10.7	7.	155.4	16.1	0.0	4	30.6	193.6	5.1	122.4	331.2
•	. > 	7-794	12.2		287		6.3	0	135.9	45.9	0	4	50.5	345,2	יית מיני	144.5	20.0
	Ė	250.7	16.6		5 T		17.0	0	291.3	61.9	0.0	2.6	7,7	, 000 , c	0 C	1,000	7.012
1985		54.7	4.6		137		12.4		4.74	4.	2 0	٠,	7.01	4 4 4 4 4 4 4 6	, «	100	4
		201.6	•		253		0	2 6	# P	, ,	000	. 0	104	553.0	10 42	244.7	832.5
		256.3	•		4 4		ο α ο α) r	117	10.4	0		30.8	188,0	15.2	122.4	325.6
1986		59.7			10		, vo	0	144.4	54.0	0	14.0	69.2	368.5	18.7	122.3	509.5
	× 1	202	7.4		6.10		17.3	0	297.3	. 6 - 0 2	0.0	29.1	100.0	556,4	e M	244.7	835.1
7.40	- 3 - 1 - 1	20.00			747		11.0	0	163.9	7.87	0	4	35.0	200 200 200 200 200 200 200 200 200 200	4.4	7.77.	0.440
•		149.9	10.5		212		2.5		116.9	45.3	00	24.5	87.0	492.7	32.1	204.2	728.9
	14	215.4	14.9			415.0	7 - / 1			,		,				1	
	MINNE	5088	331,	3087.	6507.	4380.	345.	1191.	5916-	1404.	ö	578.	1982.	10872.	676.	4856.	16404.
	,	;	1	·													

.7 99.9 4.9 61.4 29. .7 33.6 0.0 101.7 4.	. 3 102.8 8.0 22.4 41.0 2	1 139.0 8.0 108.0 55.7 2 5 1.5 6 5 5 5 5 5 6 5 6 5 6 5 6 5 6 6 6 6 6	.6	.3 117.1 4.9 26.7 49.1 249. .0 33.3 2.5 95.9 10.4 16. .3 150 4 7 4 122.7 59.5 265.	3 37.2 2.8 88.7 8.7 16.6.	.\$ 125.6 7.7 144.4 50.8 223. .6 90.1 7.4 66.2 29.8 200. .1 35.3 0.0 84.7 17.6 22.	.7 125.4 7.4 150.9 47.4 223.	.4 37.1 0.1 92.3 10.3 16. .2 143.9 7.4 112.5 48.0 188.	3 37.3 1.0 82.5 16.5 16.5 16.5 16.5 16.5 16.5 16.5 16	.6 95.3 9.8 27.0 49.1 267.	.8 128.2 10.4 126.5 58.7 284.	.6 36.3 0.0 88.7 12.2 47.	3 86.6 4.9 58.7 43.9 298.7 43.9 298.7	0 118.6 4.9 159.3 57.4 314.	.8 37.9 2.0 94.6 5.3 16 .8 37.9 2.0 94.6 5.3 16 .8 135.7 6.9 200.0 38.9 300	11 91.0 9.1 29.7 48.3 313	.6 124.8 9.1 125.9 63.2 364 .7 106.2 5.1 48.3 45.3 392	.6 40.3 2.5 88.7 9.4 22 .3 146.5 7.5 137.1 54.7 415	2 106.4 6.2 34.7 32.3 215 1.1 34.9 2.5 97.9 7.9 19 2 1/1 4 8 7 132 7 40 2 232	10 91.4 7.8 14.7 72.0 3.	.2 132.7 7.8 97.6 80.9 504 .5 88.6 7.6 51.3 45.6 222 .3 x3 2 0 0 6.5 16 0 21	5.8 121.8 7.6 145.7 62.5 243	3.3 138.1 6.6 138.7 50.4 257	7.6 95.9 9.8 59.0 44.7 250	1.5 127.8 9.8 143.4 52.2 267 1.9 121.4 2.9 31.5 33.0 210	2.7 35.5 4.6 71.3 5.6 12 4.6 156.9 7.5 102.8 38.6 222	6186, 2703, 153, 2740, 1074, 5665.
2.9 0.0 259.9 42.0 3	5.6 6.0 38.8 54.9 5	5.9 6.0 276.4 75.1	5,5 0,0 248,5 19.7 55,4 6,0 295,4 81.6	3.2 4.5 33.4 71.9 3 8.2 0.0 263.7 12.5 8.5 / 6.267 12.5	6,9 0.0 242.2 18.4	0.9 4.5 291.7 72.5 9.4 4.5 55.9 38.9 5.6 0.0 207.9 26.0	5.0 4.5 263.8 64.9	3.8 0.0 263.7 13.9 1.6 7.5 306.8 71.6	41.4 0.0 235.7 23.3	26.0 3.0 274.7 07.2	26.4 0.0 233.0 13.2 20.7 7:4 290:0 73.0	41,3 1,5 237,2 19.2	74.5 3.0 57.7 52.1	5.5 3.0 314.0 68.3	5.5 0.0 275.5 9.5	5.2 7.5 35.5 59.8	5.5 9.0 271.1 78.0	3.1 1.5 247.6 17.2 1.5 7.5 289.7 71.0	1.1 6.0 33.2 47.2 4.8 0.0 267.1 10.3	3.8 6.0 29.8 97.9 7.7 0.0 255.3 19.3	1.5 6.0 285.1 117.1 0.3 7.5 54.0 56.0	1.6 .6.0 46.5 45.1	5.5 1.5 233.6 23.8	9.9 4.5 54.1 62.0	6.5 4.5 320.7 72.0 6.5 4.5 320.7 72.0	1.8 0.1 198.1 7.5 9.2 4.0 231.4 51.4	405, 113, 5868, 1412.
8 WET 10.6 288.2 DRY 3.6 29.2	9 WET 13.7 259.2	TTL 21.0 293.2 1	0 WE! 15.0 288.8 DRY 7.5 28.0 TTL 22.5 316.8 1	WET 18.6 346.6	2 WET 12.6 289.5 DRY 7.0 29.8	3 WET: 19.7 319.4 1 05. 8.1 263.3	TTL 17.6 324.8 14 WET 15.0 331.7	DRY 4.1 19.7 TTL 19.1 351.4 1	S WET 8.9 248.1 DRY 7.2 34.2	4 WET 12.5 275.5	TTL 17.9 304.5	DRY 6.8 40.2	8 EET 12.3 255.2	TTL 17.6 281.8 1	9 WES 7.5 140.7 DRY 3.1 13.4 TTI 10.4 160.1	14.8 226.0	TTL 21.4 289.9 1 1 WET 13.7 243.0	DRY 6.9 31.2 TTL 20.6 274.2 1	WET 12.7 169.8 DRY 3.2 21.6	3 WET 25.1 447.3	30.8 469.3 1 12.6 209.9	TTL 17.4 249.5 3	7.6 63.8 TTI 19.8 202.1	WET 16.2 266.2	17L 19.0 290.0	DRY 1.9 9.9	~
	B WET 10.6 288.2 81.4 3.7 52.9 42.0 308.7 99.9 4.9 61.4 2 DRY 3.6 29.2 33.9 0.0 259.9 9.3 44.7 33.6 0.0 101.7	8 WET 10.6 288.2 8.4 3.7 52.9 42.0 308.7 99.9 4.9 61.4 2 DRY 3.2 29.2 32.9 0.0 259.9 9.3 44.7 33.6 0.0 101.7 TIL 14.2 317.4 117.2 3.7 312.8 51.4 553.3 133.6 0.0 101.7 9 WET 13.7 259.2 85.6 6.0 38.8 54.9 272.8 102.8 8.0 22.4 4	B WET 10.6 288.2 81.4 3.7 52.9 42.0 308.7 99.9 4.9 61.4 2 DRY 3.6 29.2 32.9 0.0 259.9 9.3 44.7 33.6 0.0 101.7 TTL 14.2 25.2 32.9 0.0 259.9 9.3 44.7 33.6 4.9 103.1 3 WET 13.7 259.2 85.6 6.0 38.8 54.9 272.8 102.8 8.0 22.4 4 DRY 7.3 34.0 41.3 0.0 237.5 20.2 41.4 36.2 0.0 85.7 1 TTL 21.0 293.2 126.9 6.0 276.4 75.1 319.0 8.0 108.0 5	B WET 10.6 288.2 81.4 3.7 52.9 42.0 308.7 99.9 4.9 61.4 2 DRY 3.6 29.2 32.9 0.0 259.9 9.3 44.7 33.6 0.0 101.7 TLL 21.2 25.2 32.9 0.0 259.9 9.3 44.7 33.6 0.0 101.7 TLL 23.2 25.2 85.6 6.0 33.8 54.9 272.3 133.6 4.0 22.4 4 DRY 7.3 34.0 41.3 0.0 237.5 20.2 41.4 36.2 0.0 85.7 1 TLL 21.0 295.2 126.9 6.0 276.4 75.1 314.1 139.0 8.0 108.0 5 WET 15.0 288.8 95.0 6.0 26.9 61.9 599.2 104.7 9.8 41.9 5 WET 15.0 288.8 95.0 0.0 26.9 61.9 7 77.5 580.0 0.0 90.3 1 TLL 22.5 316.8 125.4 6.0 295.4 81.6 336.8 142.8 9.8 132.3 6	B WET 10.6 288.2 81.6 3.7 52.9 42.0 308.7 99.9 4.9 61.6 2 17. 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A:Tha Lat Expansion

A-1: Irrigation Requirement

A-2:Water Supply Demand

(Domestic Water)

A-3: Water Demand (Total)

B:Existing Tha Lat

B-1: Irrigation Requirement

B-2: Fishery Requirement

B-3: Industial Demand

B-4:Water Supply Demand

(Domestic Water)

B-5: Water Demand (Total)

C:Bang Pakong Block

C-1: Irrigation Requirement

C-2: Fishery Requirement

C-3:Industial Demand

C-4:Water Supply Demand

(Domestic Water)

C-5: Water Demand (Total)

Note: Industial Demand

Tha Lat Expansion OMCM

Existing Tha Lat 20MCM

THA LAT EXPANSION

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THA LAT EXPANSION

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THA LAT EXPANSION

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EXISTING THA LAT

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MAXIMUM DEMAND

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EXISTING THA LAT

FISHERY (CU.M/S)

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THA LAT EXISTING

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ANNUAL WATER DEMAND (CU.M/S)

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IRRIGATION (CU.M/S)

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125 0.920 0.301 7.78310.045 3.73413.244 5.556 0.000

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BANG PAKON

FISHERY (CU.M/S)

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BANG PAKON

WATER-SUPPLY (CU.M/S)

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BANG PAKON

ANNUAL WATER DEMAND (CU.M/S)

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235 5.256 5.827 6.448 5.476 5.10716.45812.79220.50212.087 5.781

285 5.259 5.245 6.17911.017 6.45812.79220.50212.087 5.781

289 5.194 5.698 6.304 8.319 5.47111.65910.73719.64416.192 5.496

259 5.270 5.724 6.078 5.83112.72212.640 4.74212.37115.072 4.682

258 5.226 5.805 6.34811.305 5.75416.16717.647 4.682 9.897 8.822

259 5.353 5.844 5.377 9.180 5.80013.20811.34617.948 6.387 5.668

254 5.396 5.308 6.271 5.279 8.23410.43513.24113.80814.38611.081

264 5.302 5.394 5.577 5.53211.661 9.611 9.16411.625 4.68215.054

252 5.211 5.938 6.049 5.09112.70314.963 8.55018.08710.337 4.682

252 5.211 5.938 6.315 5.13111.07017.87411.89514.854 4.706 5.846

251 5.303 5.790 6.107 5.382 5.46017.57614.02418.243 7.10011.381

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A: Tha Lat Expansion

A-1: Irrigation Requirement

A-2: Water Supply Demand (Domestic Water)

A-3: Water Demand (Total)

B: Existing Tha Lat

B-1: Irrigation Requirement

B-2: Fishery Requirement

B-3:Industial Demand

B-4: Water Supply Demand
(Domestic Water)

B-5: Water Demand (Total)

C: Bang Pakong Block

C-1: Irrigation Requirement

C-2: Fishery Requirement

C-3: Industial Demand

C-4:Water Supply Demand

(Domestic Water)

C-5: Water Demand (Total)

Note:

1) Industial Demand:

Tha Lat Expansion OMCM

Existing Tha Lat 20MCM

2) Water Requirement of Paddy Field

Manthly Mean of Water Requirement

THA LAT EXPANSION IRRIGATION (CU.M/S)

			•																		
5/3	.057	.032	.230	182	.062	291	-287		797.	722	000	.662	000	060	.887	000.	Ø	~	O	980	
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8/1	0.406	2.946		ď	1.96		1.462		3.337		. •	000	.26	0.034		0.00	1.109	2.59	О	1.579	
7/3	0.224	0.380	ы	N	o,	ø	8	32	00.	9	0.5	O	Ö.	17	١,	0.052	0.367	0.000	0.101	0.265	
212	٥.	0.296	M	ņ	0.988	0000.0	0:275	000.0	0.301	e		0.218	0.988	•	0.275	000.0	0.017	0.210		0.298	
11.2	870.0	670.0	0.126	0.113	0.299		0.240	0-104	•	0.063	0		 	N	0.360	0.952	0.343	0.224	0.623	0.020	
6/3	000.0	000-0	000.0	00000	000-0	0.000.0	00000	000.0	000.0	0000.0	0000-0	0.000.0	000.0	00000	000.0	0000.0	0000.0	000.0	000.0	000.0	
6/5	000.0	000.0	0000.0	000.0	000-0	0.000	0000	000.			000.0	000-0	0000-0	000.0	0000.0	0000.0	000.0	0000.0	000.0	000.0	
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7/7	0.54	2.86	0.04	M	0	~	0.222	-	Ö	o	M	ď	'n	-	_;	M	o	∙	e-i	M	
YEAR	1968	1969	1970	1971	1972	1973	1974	1975	1976	1977	1978	1979	1980	1981	1982	1983	1984	1985	1986	1987	

MAX		•	•	•	•	•	•	•	•		•	•	•	•		•	•	•	2.97	4	
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2/3			•		•	•	•				•			•		•			5.975	•	
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2/1	.81	81	.81	.83	.81	.47	8,	.96	8	.41	8,	8,	.65	81	8	.83	8	.58	5.815	() ()	
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7	13	.82	1.3	1.13	13	133	.82	13	13	13	89	1,1	13	5	4	7	8	1.3	13	5.131	
1/1	. 64	.64	.64	.64	.64	49	49.	49	5	65	80	48-	7.9	79	49	49	.64	49	•	.64	
വ	96	96	69.	96	96	96	96	96	6.1	96	96	96	96	96	96	9.6	96	96	96	3.965	
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THA LAT EXPANSION

WATER-SUPPLY (CU.M/S)

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8/3	.330	.330	.330	.330 0	.330	0.330 0	.330	.330	330	.330	.330	.330	.330	.330	.330	.330	.330	.330	.330	.330
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5/3	.330	.330	.330	G	33		.330	.330	.330	.330	.330	.330	088	.330	.33	•	.33	.33	.330	.330
2/5	.330	.330	.330	.330	330	0.330	330	.330	.330	.330	.330	330	.330	980	.330	.330	.330	.330	.330	30
5/1	30	.330	.330	.330	330	0.330	330	.330	.330	.330	330	330	.330	.330	.330	.330	.330	33	M	0.330
4/3	33	.33	0.330	33	33	0.330	Ŋ	M	.43	33	33	.33	W		33	3	η.	33	0.330	M
7/5	33	.33	.33	33	W	0.330	33	33	ŭ,	5	W	κ. Κυ	. 33		33	33	.33	333	•	ξ. (λ)
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YEAR	1968	1969	1970	1971	1975:	1973	1974	1975	1976	1977	1978	1979	1980	1981	1982	1983	1984	1985	1986	1987

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	3/2	0.34	0.34	0.34	0.34	0.34	0.34	0.34	0.34	0.34	0.34	0.34	0.34	0.34	0.34	0.34	0.34	0.34	0.34	0.34	0.34	
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	1/3	0.29	0.29	0.29	0.29	0.29	0.298	0.29	0.29	0.29	0.29	0.29	0.29	0.29	0.29	0.29	0.29	0.29	0,29	0.29	0.29	
	1/	0.29	0.29	0.29	0.29	0.29	0.298	0.29	0.29	0.29	0.29	0.29	0.29	0.29	0.29	0.29	0.29	0.29	0.29	0.29	0.5	
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		29	.29	29	.29	-29	0.298	.29	29	.29	29	29	29	29	. 29	.29	29	29	.29	-29	29	
	1/	0.29	0.29	0.29	0.29	0.29	0.298	0.29	0.29	0.29	0.29	0.29	0.29	0.29	0.29	0.29	0.29	0.29	0.29	0.29	0.29	
	11	0.29	0.29	0.29	0.59	0.29	0.298	0.29	0.29	0.29	0.29	0.29	0.29	0.29	0.29	0.29	0.29	0.25	0.29	0.29	0.29	
	10/	0.29	0.29	0.29	0.29	0.29		0.29	0.29	0.29	0.29	0 29	0.29	0.29	0.29	0.29	0.29	0.29	0.29	0.29	0.29	
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MAXIMUM DEMAND =

ANNUAL WATER DEMAND (CU.M/S) THA LAT EXPANSION

9/3	2.647	2.623	0.820	0.772	1.652	0.881	•	•	4.054	. 9	0.590	•	0.590	2.680	•	S	2.757	2.169	1.898	1.571
3/5	0.702	1.086	3.366	4.207	1.450	1.898	4.658	0.590				0.590	2.425	'n	۲.	2.711	0.590	1.560	4.559	2.145
9/1	4.327	1.816	٠,٠	3.187	0.647	4.260	3.643	2.460	2.575	•	3.668	3.959	5.474	4.021	4.337	1.843	3,415	4.457	0.550	3.268
8/3	4.439	0.799	1.307	0.622	4.901	1.486	1.798	1.261	1.168	1.116	o,	3,190	0.637	4.841	•	3.883	2.912	4.085		3.239
8/5	o.	ò	M	3.635	7.495	3,383	3.332	-4	1.921	S			M	2.615	9	0.622	0.689	4.622	0.655	2.479
8/1	1.028	3.565	0.865		2.584	3.706	2.084	3.718	9.5	3.464				0.655	S		1.730	3.221		2,200
7/3	0.830	0.986		0.833	1.594	726.0	0.606	0.926	909.0	769.0	0.659	0.606	909.0	0.779	0.961	0.658	0.973	0.606	0.707	0.871
7/2	1.594	О		0.915	1.594	0.606	0.881	909.0	0	0.723	0.891	0.824	1.594	0.821		0.606	0.622	0.816	0.865	0.904
7/1	0.654	0.655	0.732	0.719	0.905	0.811	0.846	0.709	0.617	699.0	0.606		0.986			1.558	676.0	0.830		0.626
6/3	909-0	909:0	909-0	0.606	0.606	0.606	909.0	0.606	0.606	0.606	0.606	909:0	909-0	0.606	0.606	909-0	0.606	909-0	0.606	0.606
6/2	0.606	909-0	909.0	909.0	0.606	909.0	909.0	909.0	0.606	0.606	0.606	909:0	909.0	909-0	909.0	909-0	909.0	0.606	0.606	0.606
6/1	909-0	909-0	909.0	909.0	909-0	0.606	0.606	909-0	909.0	0.606	909-0	0.606	0.606	909.0	909.0	0.606	0.606	909.0	0.606	909.0
5/3	2.087	۵.	9	.62	. , .	1.001	.33	-62	0	.63	9	12	ω,	.62	.63	0.622	.76		۲,	.81
 5/5	S	Ņ	5	0.5	0	1.281	S)	Ö	9	13	8	8	4	8	8	1.796	,6	0.632	w	177
5/1	0	ø	ø	v	0	0.622	Ý	o.	M	0	4	v	4	Α,	0	0	М	9	v	1.131
4/3	M	1.949	7.7	·vo	9	1.530	9	52	.62	03	38	62	03	62	76	71	1.844	Ŷ	0.622	.62
7/5	0.622	5.649	2.326	N	1.054	3.266	.66	7.9	2,5	S	.84	80.	76	0.8	- 62	36	o,	0.622	W	Ó
4/1	·O	87	0.662	-67	0	3.209	œ,	.0	٥,	'n	v,	'n	9	'n	0,	9		.76	4	3.670
⋖	. 896	696	970	971	972	973	726	975	926	226	826	626	980	981	982	.983	984	1985	1986	1987

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EXISTING THA LAT

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IRRIGATION (CU.M/S)

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9/3	8.372	5.033	8	.43	8.308	3.481	962.9	72.7	1023.569	5.896	3.78	7	0.000	13.645	13.734	0.000	18-176	14:075	12.452	2.827
2/6	9.526	3.5041	20:507	21.568	10.241	6.563	21.4601	7.8591	0000.0	14.372	0.973	6.202	15.830	0000-0	6.960	16.936	0.00018	000-0	26.157	7.938
9/1	675.9	3.191	33.393	13.1188	0.0003	35.405	767.91	7.597	 -1	19.830	17.481	23.437	12.068	1.27	18.502	8.974	13.465		2.317	17.578
8/3	6.5282	8.291	7.0942	0.0001	3.072	8.5682	. 48	. 59	.796	782	7.2721	677 -	2	Ŷ	5.0481	0.083		17.9561	17.660	17.4341
8/2	0.4021	0.486	9.273	4.895	3.7092	8.647	3.1581	3.181	9.304	2-144	6.551	.686	6.901	797	0	0.00020	0.1521	4.5741	3.8241	1.44017
8/1	0.4712	7.058	2.355	3.1551	9.9722	9-2471	0.5981	9.7531	607.0				9-4892	5.8661	6.5482	000-0	0.573	8.9832	000-0	7-2791
7/3	0.875	4.1471	2.060	1.3972	9.064	2.203	0.0161	•	•	0.2502	0.24716	•	0000-0		1.147		2.0751	0.559	1.007	1.5531
2/2	5.703	1.991	2.232	2.014	4.871	0.253	2.062	0000-0	1.391	1-402	2.311	1.804	5.6.8	1.525	φ	0.000	0.000	1.480	0.717	2.149
7/1	1.115	0.062	1,267	1.294	1.654	1.382	1.013	Š	0.388	1.262	000.0	1.647	2.454	1-764	2.658	5.296	2.283	1.621	4.012	0.374
6/3	000.0	0.000	000.0	000.0	00000	000.0	000.0	0.000	000.0	000.0	00000	0000-0	0000.0	000.0	0000.0	000-0	0000-0	0.019	0000.0	000-0
2/9	0.000	0.000	0.000	000.0	000.0	00000	000.0	000.0	000.0	0000.0	000.0	0000.0	0000-0	00.	000.0	00000	0.000	0.000	0.000	000-0
6/1	00000	000.0	00000	00000	000.0	00000	0.	0.232	0.00	000.0	0.277	0.198	000.0	0.234	00000	0.00	0.000	0.536	0.238	0.221
5/3	1-645	0.002	0.009	0.000	1.644	0.941	•	•	•	•	0.791	•	•	•		•	0.673	3	1.638	776.0
5/5	69	40	8	O	66	N.	37	ĸ	7.0	2	ы	'n	1 /2	ç	2	6	70	6	0	o.
5/1	7		'n	1.019	9	m	w.	4	C	9	Ċ.	143	v,	v,	0	r,	٧.	ς.	ှ	Ψ
4/3	2.326		1.687			0.539														
.214	0.000	2.896	•	0.000	•	0.737	•	•					. •		•	•	•		•	•
4/1	97970	3,317	0000.0	3.926	0.255	3,392	0.232	2.132	0.125	0.783	3.938	3.845	2.607	1.971	2.195	3.938	1.756	3.057	1.223	3.902
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	MAX	6.549	1.519	3.393	3.155	3.709	6.227	3.376	3.972	3.569	2-144	6.551	6.686	6.901	6.656	4.511	1.644	26.227	725-7	6-157	21.022	
	AL	30 2	43 2																	86 2	.660 2	
	ANNUAL	710.3	2225.5	412.7	522.1	450-1	553.9	364.9	578.3	298.8	726.7	558.3	141.0	427.0	576.5	2565.014	039.5	422-1	ά	481.4	2627.6	
	/3	627 2	523 2	929 2	437 2	892 2	651.2	263 2	972 2	970.2	692 2	568 2	7.067	877.2	871 2	987.2	209 2	6.454 2	w	"		
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	3/1	10.96	10.81	9.61	10.96	10.95	10.90	10.74	9.30	9 41	10.90	10.96	10.82	8.50	10.94	9.91	10.96	10.23	10.96	10.95	9.42	
:	2/3	2.004	2.008	9.789	1.822	2.008	8.554	1.956	2.008	1.543	1.832	0.018	1.534	1.071	1.570	2.008	1.392	1.678	1.848	2.008	3.24411.945.9.4	
•	2/2	.9891	.6741	566.	.9251	.9951	513	-6841	7681	.9951	7401	.3401	.9951	.9951	.5551	.7541	.8261	6991	.9951	9951	. 2441	
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	1/1	8.311		9.848		9.84810.	9 848	8.487	8 8 6	9 82	4.953	9.028	9.848	9.848	9.848	9.848	878.6	9.84810	378.6	9.848	378.6	
	2/3	6.641	149.	818	7.594	641	641	641	641	241	641	6.641	641	641	641	641		6.641		5.641	5.641	
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٠.	YEAR	1968	1969	1970	1971	1972	1973	1974	1975	1976	1977	1978	1979	1980	1981	1982	1983	1984	1985	1986	1987	

EXISTING THA LAT

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	10/1	000	0.222	0.186	0.068	000	000	0.000	0000	000	0.103	000	0.00	0.041	0.091	0.060	0.00	000	0.114	0.00	0.190
	YEAR	1968	1969	1970	1971	1972	1973	1974	1975	1976	1977	1978	1979	1980	1981	1982	1983	1984	1985	1986	1987

EXISTING THA LAT

INDUSTRY (CU.M/S)

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EXISTING THA LAT WATER-SUPPLY (CU.M/S)

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\sim	105	.105	0.105	.105	110	.105	.105	.105	.105	105	10	170	1.0	100	10		, c) (7.	10	110		7.4	, ,	J (122	122	122	122	1222	.122	122	.122	.122	.122	.122	.122	.122	1122	.122	122	122	.122	122	j
\sim	105	105	0.105 (.105	.105	105	.105	105	.105	.105	.105	105	.105	.105	105) () i	0 I	.105	105		~	, , , ,	VI (755	122	122	122	1225	.122	122	.122	.122	122	.122	122	122	122	.122	122	0.122 0	.122	122	3 3 4
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\sim	0.11	0.11	0.117	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11			1 4	5	0.11	0.11		~	, ,	7	0.11	E .	0.11	0.11	0.11	6.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.111	0.11	0.11	•
8	0.11	0.11	7 0.117	0.11	0.11	0.11	0.13	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	,	1 5	1 °	7	0.11	0.11		- 5) (1 .	11.0	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.13	1 0.111	0.11	1 4 4	4 4 0
`	0.11	0.11	1 0,117	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.1	0.11			- i · · · · · · · · · · · · · · · · · ·	0.17	0.11	0.11		-	, ,	-1 -1 -2	11.0	0.33	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0	50.11	0.17	0 0	
77	10.11	1 0.11	1 0-11	1 0 11	10.11	1 0.11	10.11	1 0.11	10.11	10.11	1 0.11	1 0 11	10.11	10.11	1 0 11		· ·	1.0	T 0 T	10 11	10.11		,	` ` C	2	5 0 1	5 0.1	50.1	5 0.1	5 0.1	5 0.1	5 0.1	50.1	5 0.1	50.7	5 0 1	5 0.1	5 0.1	5 0 1	0.1	C	5 0 10	1 C	1 C	٠
7	10	10.1	10.11	10.1	10.1	10.1	10.1	10.1	10.1	10.1	10.1	ਦਾ 0	10.1	10.1	0		,	- ·	0	0	1 0.1		-	- i c	- - -	0 ·	S 0.17	5 0.1	5 0.1	5 0.1	5 0.1	5 0.1	5 0.1	5 0.1	5 0.1	5 0.1	5 0 1	5.0	5 0 1	5	L C	5 0.10) C) C	
7/	10.1	10.1	11 0.11	10.1	10.1	10.1	10.1	10.1	10.1	10.1	10.1	10.1	10.1	10.1	1		· ·	· ·	1.0	10.1	10.1	-	,	٠ د د	7.5	0.1	5 0.1	5 0.1	5 0.1	5 0.1	5 0.1	5 0.1	5 0.1	5 0.1	5 0.1	5 0.1	5 0.1	5 0.1	5,0	5 0.1		02.0.10	, r	יי יי יי	1 2 0
19	10.1	10.1	11 0.11	10.1	10.1	10.1	10.1	10.1	1 0.1	10.1	10-1	10.1	10.1	10.1			 	7.0	10,1	10.1	1 0.1		,	, , , , , , , , , , , , , , , , , , ,	 	S 0.1	5 0.1	5 0.1	5 0.1	5 0 1	50.1	5 0.1	5 0.1	5 0.1	5 0.1	5 0.1	5	0.1			! c			υ h 2 C	
19	1 0.1	0.1	1.0.1	1.0 t	0.1	10.1	1.0.1	₹*0 ₹	1.0.1	0.1	0.1	0	0	101	C			1.		0.1	0.1		,,	777 1	ا ا ا	05 0.1	05 0.1	05 0.1	05 0.1	05 0.1	05 0 1	05 0.1	05 0.1	05 0.1	05 0.1	05 0 1	05 0 1	0.10	0.0	0.00	1 C	1 - C 0 0 0 0 0	1 0	7.0	0 0 0
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5/7	1.443	1.984	1.811	2.293	3,335	1.585	2.083	2,729	2.358	1.275	2.224	1.630	5.964	1.808	3.327	2.497	2.915	2,258	1.275	2.111
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BANG PAKON

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***** WATER DEMAND FOR KHLONG THA LAT RIVER BASIN DEVEROPMENT PROJECT *****

BANG PAKON

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BANG PAKON

ANNUAL WATER DEMAND (CU.M/S)

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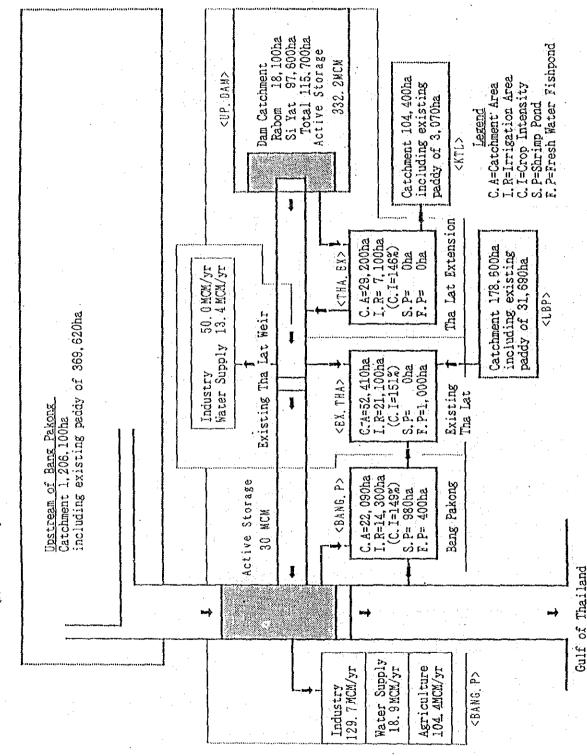
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18,100ha 18, 100ha I.R=Irrigation Area C.I=Crop Intensity S.P=Shrimp Pond F.P=Fresh Water Fishpond Active Storage 32,2MCM Dam Catchment <UP, DAM> Catchment 202,000ha including existing paddy of 3,070ha C. A=Catchment Area Si Yat Total Rabon Legend <KTL> Figure 1-3-1 Annual Water Requirement in Phase-I (Case-1) (After Completion of Phase I Project, Surplus Water: 60MCM) I Tha Lat Extension C. A=29, 200ha I. R= 3, 400ha (C. I=100%) S. P= 0ha F. P= 0ha Catchment 178,600ha including existing paddy of 31,690ha <THA. EX> O. OMCM/yr O. OMCM/yr <LBP> Upstream of Bang Pakong Catchment 1,206,100ha including existing paddy of 369,620ha Existing Tha Lat Weir Industry Water Supply C. A=52, 410ha I. R=21, 100ha (C. I=100%) S. P= 0ha F. P= 0ha Existing Tha Lat <EX. THA> C. A=22, 090ha I. R=14, 300ha (C. I=149%) S. P= 980ha F. P= 400ha <BANG. P> Active Storage Bang Pakong 30 MCM Water Supply 18.9MCM/yr Industry 129.7MCM/yr Agriculture <BANG. P> 0.0 MCM/yr

Gulf of Thailand

I.R=Irrigation Area C.I=Crop Intensity S.P=Shrimp Pond F.P=Fresh Water Fishpond 18,100ha 18,100ha Active Storage Dam Catchment 32, 2MCM <UP DAM> Catchment 202,000ha including existing paddy of 3,070ha C. A=Catchment Area Tota] Rabom Si Yat Legend <KTL> Figure 1-3-2. Annual Water Requirement in Phase- I <Case-2>(After Completion of Phase I Project, Surplus Water: 20MCM) Ĭ Tha Lat Extension C. A=29, 200ha I. R= 3, 400ha (C. I=100%) Catchment 178,600ha including existing paddy of 31,690ha <THA EX> 0.0MCM/yr 0.0MCM/yr < L.B.P.> Catchment 1,206,100ha including existing paddy of 369,620ha Existing Tha Lat Weir Į Water Supply C. A=52, 410ha I. R=21, 100ha (C. I=100%) S. P= 0ha F. P= 0ha Industry Existing Tha Lat <EX. THA> į Costream of Bang Pakong C. A=22, 090ha I. R=14, 300ha (C. I=149%) S. P= 980ha F. P= 400ha <BANG, P> Active Storage Bang Pakong 30 MCM Gulf of Thailand Water Supply 18.9MCM/yr Agriculture 0.0 MCM/yr Industry 89.7MCM/yr <BANG, P>

Figure 1-3-3 Annual Water Requirement in Phase-I&IKCase-3> (After Completion of Fhase I & II Project, Surplus Water: 90MCM)



1.4 Project Justification

1.4.1 Table

TABLE 1-4-1 DISBURSEMENT SCHEDULE OF PROJECT COST

							Ē	(Unit: Million Baht)	on Baht)
Work Description	Cost	1992	1993	1994	1995	1996	1997	1998	1999
RID's Facilities							٠.	•	
A. Direct Cost								٠.	
1. Preparatory Work	20			20					
2. Construction Cost			-						
Diversion Dam Project	2,509			180	745	1,005	579		
Canal Project	347				46	63	132	106	
Sub-Total	2,857			180	791	1,068	711	106	
3. Land Acquisition	375		150	150	75				
4. O & M Equipment	11							F1	
5. Survey & Investigation	24	면 7	10				-:		
6. Administration Cost	106	τĊ	χο.	18	22	21	13	16	
7. Engineering Service	216	35	30	43	32	32	22	22	
8. Physical Contingency	359	хO	20	39	92	112	75	16	
Total	3,967	59	215	450	1,012	1,233	827	171	
B. Indirect Cost	271		4	46	46	46	46	83	
C. Rabom Dam ConstructionTotal (A + B + C)	120 4,358	120 179	219	496	1,058	1,279	873	254	
PWA's Facilities		(2%)	(15%)	(25%)	(30%)	(25%)			
	3,140	157	471	785	942	785			
Grand Total	7,498	336	069	1,281	2,000	2,064	873	254	

TABLE 1-4-2 INCREMENTAL BENEFITS

(Unit: Million Baht)

Year	Agriculture	Domestic & Industiral Water	Surplus Water (60 MCM)	Total
1996				1.
1997		133.0		133.0
1998	139.5	266.0	•	405.0
1999	206.4	399.0		605.4
2000	407.2	532.0		939.2
2001	417.5	665.0		1,082.5
2002	426.1	665.0		1,091.1
2003	438.6	665.0		1,103.6
2004	440.0	665.0		1,105.0
2005	442.5	665.0		1,107.5
2006	445.9	665.0	27.0	1,137.9
2007	445.9	665.0	54.0	1,164.9
2008	445.9	665.0	81.0	1,191.9
2009	445.9	665.0	108.0	1,218.9
2010	445.9	665.0	135.0	1,245.9
2011	445.9	665.0	135.0	1,245.9
2012	445.9	665.0	135.0	1,245.9
:	:	•	•	•
2041	445.9	665.0	135.0	1,245.9

TABLE 1-4-3 COMPUTATION OF EIRR (IN THE CASE OF SURPLUS WATER OF 60 MCM)

C UNIT : MILLION BAHRT >

	1	ROJECT COST					PRESERT *	ORTH VALU	E BY DISCOUN	T RATE	
	CAPITAL	⊗	TOTAL		- !		BENEFITS	(COST)	(BENEFITS)	ST)	. €
1.6			302.40	0	302.4	302.40	0	- 4	0	20	1 5
199	621.0	۹	641	oʻ.	-621-0	32.4	9 (2.5	0	500	
> 0 > 0	, c		7 0	000		, v		0 0 0 0		o e	0 0
199	857.6	0	857.	. 0	1857.6	64.2	, 0	53.4	9	1 7	
199	85.7	6.0	836.	33.0	703.6	527.2	83.8	472.2	75.0	423	67.
199	28.6	7-2	5	5 . 50	7.70	75.8	ر د و	24.6	တ္	36.	83.
0.00	9	, .		4.05	22.7		27.0	× 0	4.6	M B	٠,
200	, c	10		7 7 7 7 7	. v	0 K)	ο α	9 6	0.0	ο α Ο Ν
200	9	00	000	1.160	0.10	0.0	7	יו יו	37	· cc	, H
2002	Ó	00	00	103.6	003.5		38.2		51.6	S	M
3 200	0	00.1	00	105.0	004.9	8	06.3	0	20.0	C)	53
7 200	0	00.1	80	107.5	007.4	4.0	77.0	6.3	91.	3	26.
2 200	٥.	00.1	00	137.9	37.8	1.5	58.7	3	72.1	8	07.
5 200	9	00	00	164.9	9.790	9.2	0.04	1.7	53	8	000
7 200	ं	00	80	191,9	091.8	٥.	22.1	6	35	•	73
8 200	٥.	00,1	8	218.9	118.8	o m	0.5	တ လ	6.	m	ω ω
9 201	0,	00	8	245.9	145.8	M.	88.6	M (M	, .	77
201	٠.	100	000	245.9	24 v 20 c	4 (, (ינג וינג	ά (0.0	0 L
202.1	٠,	000	96	747	0 . V . V . V . V . V . V . V . V . V .) (0 t	0 1	٠,	U t
) (C	9.9	2 6		7.47	0 . u . t	100	, r	1.	1 C	4 1.	V .
2 6	9	3 6	9 6	0 0 0 0 0 0	0 t t t t	ייי	, , ,	1 e 1 c			
201	9 0	65.3	6 6	6,1575	580.6	, r	81.9		7.		
5 201	0	53.1	53	245.9	92.8	7	68.4	2.2	. 40	3	
7 201	٥.	00.1	8	245.9	145.8	5	55.9	7.6	95.0	v	~
B .201	°	00.1	00	245.9	145.8	7.6	4. 14	٥,	7.	~	:
202 6	°	00	00	545.9	45.8	\ 0	334	M. I	m .		
202 0	٥.	00.1	00	245.9	145.8	٥.	23.8	۲,	4 .	יוח	
1 202	9	1.00	ġ:	572.9	245.0	vi i	14.6	ďι		ייַט	
2 202	o.	00	8	245.9	145.8	ນ໌ (2.6	٠.		o t	
3 202	9	00	90	245.9	10 to	D, 8	N C	. O		.) £	.,
202	0	200	3 6	7.0	0 0 0 0 0 0 0 0 0 0	1,	C	• "		4 0	1 4
700	9.9		38	0 t t t t t t t t t t t t t t t t t t t	0 4 C 7 C	٠,	J C	, 0	1 (1)	· •	, 0
7 0 0	, (2 6		() () () () ()	747	00 1	. ~	. 0.		w	
200	Ç	000	000	245.9	145.8	M		v	10	M	100
9 203	0	00	00	245.9	145.8	o.	6:	4	5	N	0
0 203	٥.	80.1	00	245.9	145.8	0	M.	N,	<u>رم</u> ،	0 0	ų,
1 203	٥.	00.1	00	245.9	145.8	N, 1		O		У (, C
2 203	٥.	00.1	00	245,9	145	٠,		v, çx	•	0 1	• n
3 203	٥.	00	000	V V V V V V V V V V V V V V V V V V V	0 0 0 u . 0 t	٥H		o v	3 60	- 4	ጎ ሆ
203	0	0 1	0 1	7.0	0.00	j o		•	3 <) C) Y
) () () ()	o, c	٠.	O U	Ç	0 0) N	? ~!	! +	15.54	'n) I
7 6 6 7 6 7 6 7 6 7 6 7 6 7 6 7 6 7 6 7	2 0	1.0		9.14	145.8	9	2.4	+1	*	-4	0
8 203	, 0	1 5	000	245.9	145.8	٧.		0	83	4	-4
9 204	9	100	00	245.9	145.8	M	.6	ø.	0	м	œ
0 204	0	00	100	245.9	1145.8	2.1	26.5	8.0	10.6	M (4.3
TOTA	8.2	5838.8	2587.	155,2	568.2	v.	ر ا ا	o i	0	νı	v i
BENEFIT	COST RATIO	DISCO	RATE (8/C)	1.40 €	8%)/ 1.11.0	06.0 (201)	(12%)				
NTERN	ATE 0	TURN CIRR		•							

C UNIT : MILLION BAHRT >

1 1 1 1 1 1 1		1 1 1 1 1 1 1					1			1	1 1 1 1 1 1 1
46.47	XA	colect cost-	1	C T T T T T T T T T T T T T T T T T T T	NOTIFIE	\$4		ORTH VALUE	10 X	T RATE	
; ;	CAPITAL	Σ ⊗	TOTAL		5	•	8	(1502)	BENEFITS	081)	æ
1 6		10	0 1 2	9	302.4	02.4	0.0	02.4	i o	7 60	00.0
564	10	. 0	14	0	621.0	32.4	0	13.2	0	95.0	٥
199	152.9	0	152	0	1152.9	15.2	0	66.2	0	20.6	0
199	9	0	1800.00	ှ	000	0	0	229.4	00.0	143.9	00.0
199	857.6	0	857.	0	1857.6	264.2	0.0	53.4	0	54.0	O
199	785.7	0.9	836.	33.0	703.6	27.2	83.8	72.2	75.0	423.8	M
199	28.6	2.7	0.1	05.5	24.2	75 B	9.6	34.6	0	36.2	83.4
199	0.0	7.7	'n	7.50	22.3	۷.	27.0	.7	32.4	3.5	5-77
200	0	1.6	91.6	939-2	47.6	ຜຸ	8.69	8.8	98.3	м 0.	38.6
0 200	9	00.1	00.1	082.5	32.4	6.3	01.4	Š.	17.3	3	48.5
1 200	9	00.1	00.1	091.1	31.0	2,3	6. 19	5.0	32.4	8.7	13.6
2 200	0	00.1	00	103.6	003.5	۷.	38.2	7.0	51.6	5.6	2.2
3 200	٥.	00.1	00	105.0	004.9	δ.	06.3	٥.	20.0	2.9	53.2
4 200	٥.	00.1	00	107.5	007.4	0.4	77.0	6.3	91.6	7.0	26.6
5 200	0	00.1	00	119.9	019.8	۲. اح.	53.0	3.9	68.1	8.2	04.6
6 200	0	00.1	00	128.9	028.8	9.2	29.5	1.7	45.6	δ. W.	84.1
7 200	9	00,1	90	137.9	037.8	7	07.5	8.6	25.4	4.5	65.7
200	0	00.1	00	146.9	046.8	0.5	87.0	8.0	5.90	50	49.1
9 201	9	00.1	00	155 9	055.8	7,	67.8	6.3	39.0	1.6	34.2
0 201	0	00.1	00	155.9	055.8	7.1	48.0	2.1	71.8	0	19:8
1 201	0	00.1	00	155.9	055.8	8	29.6	3.5	56.2	5,	6.90
2 201	٥,	00.1	90	155.9	55.8	8.4	12.6	2,3	42.0	Ň	95.5
3 201	0	00.1	00	155.9	055.8	7,0	96.8	4.4	29.0	w	5.2
4 201	Ċ.	00.1	8	155.9	055.8	5.7	82.2	9.	17.3	ŗ,	4.5
5 201	0	65.3	65.	155.9	90.6	7.1	68.7	1.4	9.90	9.1	7.9
6 201	0	53.1	53.	155.9	02.8	4.2	56.2	4,2	6.9	Ŋ	7
7 201	0	4.00	ò	155.9	055.8	2	44.7	7.6	8.1	4.6	4.2
8 201	9	1.00	ë,	155.9	055.8	٠٠ ١٠	33.9	٥.	5	7	4.
9. 202	O	00.1	ွ်	155.9	055.8		24.0	1,1	3	۲.	3
0 202	9	1.00	8	155.9	055.8	್ಷ.	14.8	۲.	6.2	'n.	e.
1 202	0	1.00	00	155.9	055.8	ď	06.3	Ŋ	0.2	0	7.
202 2	٩,	00.1	8	155.9	055.8	'n	4	1	7.7	٠,	· 0
3 202	o.	00	8	155.9	055.8	o, i	e1 :	ĸ,	٠,	M)	7.4
7 202	ç	1.00	8	155.9	055.8	M,	7.7	o, i	N :	4	7
5 202	9	00	8	155.9	055.8	ائرا		ďί	41		0) i
6 202	9	00	8	255	055.8	N, C		vi .	7.	ų.	n X
202 2	9	00	8	155.9	8 5 5 6	20 1	O 6	.,	٠, د د	?!	4.1
8 202	9	000	9 6	٠ ١	מית האם	૧ લ	,,	o.	, (7	, c
9 203	9	100	3 6	እ (ለ ! ለ !	200	٠,	- 6 4 L	1	0 4	ÿc	, ~
9 10 1	, ,	2 6) () () ()	N	0,0	ő. L	, 0	, .		, 0	t C
7 604			200	7.0	000	'nc	,,	•) e) C
0 0 0 0 0 0 0 0 0	•	2 6	2 6	V	0 Q	'n×	, v	• 4	10	, r	·α
0 10 0	, (38) a	, א	. 0		. 7	,	α
) () () ()		אנ	665.30	1155.90	09 067	20.84	36.21	6 13	15.86	7.06	7.05
203	0	53.1	8	155.9	02.8	7	N		7.7	-	Ŋ
7 203	0	00	8	155.9	055.8	á	4.0	4	3.1	.4	ď.
8 203	٥.	1.00	8	155.9	055.8	7	5	0	1.9	4	0
9: 204	٩	00	00	155.9	55.8	m	6.5	ŗ.	ο.	e i	4
0 204	9	1001	100	155.9	1055.8	2.1	24.0	0	ω.	0	4.0
TOTAL	N	838.8	2587.	2.560	6508.2	ų,	ω, Ω	ω	αį	17	N
1 1	CILTO TO	FAUGUSTIC X	RATE (B/C)		82> 1.07	(10%) 0.87	7 (12%)				
ű z	RATE OF RE	RN CHRRY	, 1	11			,				
		,									

TABLE 1-4-5 COMPUTATION OF EIRR (CASE-2: 10% INCREASE IN THE PROJECT COST)

C UNIT : MILLION BAHRT >

0 5 4		ROJECT COST			20 H		PRESENT	ORTH VALU	E BY DISCOUR	UNT RATE	1 (
	CAPITAL	X. 33	TOTAL		, ,		α) ∤	COST	BENEFITS	(COST)	(BENEFITS)
41	9	ု လု	32.6	0	332.6	32.6	`	32		2	0
700	683-1	90	ο ν α κ	000	1683.1	285	٧.	4.0	٠, ٠	440	
199	80.0	, 0	80.00	90	980.0	200	. ~	3 6 6		258	
199	043.4	٥,	043.4	0	2043.4	390.7	~	89		59	
199	64.3	٥.,٥	15	33.0	782.2	76.7	83.8	16.4	75.(63.	2
199	51.5	2.7	2	05.5	81.5	89.1	36.0	99	08.	9	833
200	٥٩	 	M t	4.05	22,3		V. 0	·- ·	~ ·	M N	•
0 C	3 0	10	10	ν. ν. ν. ν. ν.	, c)) (~ ·	10	1 c	ģ
7 000	90		000	1.000		ם ני סני	1,7	0 1/	 	vα	4 0 4 0
2 200	0	00	8	103.6	003.5	. ^	80	١.	1 6	י י) M
3 200	0	00	8	105.0	70	. 80	96	. 6	20	٨	M
200	0	00.1	8	107.5	4.700	7	77 (9	91.	0	26.
5 200	٥.	0.0	8	137.9	037.8	7.5	58.	M	72.	m	07.70
6.200	0	00.1	00	164.9	064.8		0.04	7	53	8	90.
7 200	o	00-1	00	191.9	091.8	2.0	22.1	8	35.8		73.
8 200	٥.	1.00	ŝ	218.9	118.8	o.	02.0	8	19.	ň	58.
9 201	٠,	00	ö	245.9	145.8	7	88	8	100	ř	77
0 201	۰.	00	00	245.9	145.8	7.4	24	4	5	6	39
1201	۰,	000	00	245	145	ο. Ο (V (n i	801	•••	in i
102 C	90	0.6	9 6	7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	747	20 L) (N e	71 C		N s
700	, 0	16	3.6	7.0.44	140	, r	7		, ,		
100	, 0	5 6	v	245.9	200		2 0	7 7	2 4	0 0	
707.0	9	53.1	N N	245.9	10 C		68				
7 201	9	00	8	245.9	145.8	N N	55.9		25.0	7	4
8 201	0	1.00	00	245.9	145.8	1.6	44.4	0	4	4-4	5
502 6	٥.	200	00	545.9	145.8	5	33.7	~ 1			"
0 202	0	00	00	545.9	145.8	o.	23.8	r- 1	7	1.1	
1 202	٥.	00	0	245.9	145.8	N, I	14-6	CV I		v,	
2 202	۰,	00	000	245.9	145.8	v	906	~ ı		~ 1	
3 202	٩	000	88	245.9	145.8	0, 1	N (73 (01	41 4	
202	0 0	000	9 6	7.47.7	1 t V . U	٠'n	3 n	y K		-1 U	1 4
700	, (200	8 8	717	74.5	٠,	J ()	ì	'n	, vo	9 0
7 202	9	100	8	245.9	145.8	ω,	S.		0	ഗ	. 00
8 202	٥.	00.1	90.	545.9	145.8	w	80.	v	m	M	ņ
9 203	9	1,00	00	245.9	145.8	۰.	ا م ا نی	4 (יי	∾ (0
0 203	o,	00	000	247.9	145.4	91	√1 •	7 (^ <	9 (, i
200	<u>٠</u> (000	0 6	7,777	747.0	A O	d v	> α) N	×α	` '
7 K 7 C 7 C 7 C	٠,	100	3 8	7.4.4	מיעל. היינילר	` <	• IS	3 40		0 r	9 1/
0 0	ç		90	245.9	00 ('n		S	100	. vo	ւտ
203	, 0		5	245.9	580.6	α	?	ч	0	0	٧û
6 203	? 0	200	53.	245.9	92.8	7.3	7.	₽	Ŋ	м	^
7 203	٥.	00.1	00	245.9	145.8	ø	4.	~	4	à	\circ
8 203	0	00.1	00	572	145.8	41	٥,	0 1	ω, ·	√t 1	-1 · · · · · · · · · · · · · · · · · · ·
9 204	۰.	00.1	00	245.9	145.8	J.	0 11	œο	۰,۰	かい か	M 60 1
TOTAL	00.0	100110	1200-10	52155.20	38894.30	6352.30	8199.57	5722.39	5842,81	5218.06	4303,58
	7 ! ! ? ! ! ? ! !	0 1 0 1	· · · · ·					1 1			
	COST RATIO	BY DISCOUNT TURN (IRR))	= 10.2 %	8%), 1.02	(10%), 0.82	(12%)		-		

TABLE 1-4-6 COMPUTATION OF EIRR (CASE-3: 10% DECREASE IN THE PROJECT COST)

C UNIT : MILLION BAHRT

0747	-		i i	STIBERER	Nailtaa	1		107111 200	ST DISCO	N KAIE III	
Č S	CAPITAL	Σ: Θ3	TOTAL		ر ا ا	OST	BEN	(0001)	N N N N N N N N N N N N N N N N N N N	31.7 S1.5	(BENEFITS
0	62.4	0	02.4	0	302.4	0214	0.0	302,4	0,0	02.4	
99	21.0	0	621.0	0	621.0	32.4	٥.	13,2	9	95.0	
7661	152	00-0	1152.90	0	-1152.90	915.21	00.0	866,19	00.0	820.61	ó
O I	0 0	9	0.008	9	800.0	23.0	9	29.	9	43.9	٠.
8	857-6	0 0	857.0	9.0	1857.6	404))	4.001	0 1	0.750	ď.
9	85.7	6.1	9	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	7.16.9	27.2	4.0	777	67.5	23.8	60
6	28.6	2.7	01.3	0.0	63.7	75.8	· ·	14,0	w.	36.2	
<u>٠</u>	٠,	4	1	, , , , , , , , , , , , , , , , , , ,	91.0	4 i	4.0	0 0	7.1	'n	20
8	۰.	91.6	9.5	1 L	75.	1.00	,,,	o c	58.4	0	0
8	o,	00	500	3 (74.2	9	7.4	ນ ເ ທີ່	75.6	2.2	r M
8	9	00	00	82.0	81.9	5	21.1	Š	44.1	8.7	∞
8	٥.	00.1	00°.	93.2	93.7	7	7-76	1,9	16.4	5.6	2,5
8	ं	00-1	90	5.76	7.76	8.00	65.6	6	88.0	2.9	5
8	0	00.1	00-1	96.8	7.96	7.0	39.3	6,3	62.4	4,0	8
မ္မ	0	00	00	024.1	24.0	1.5	22.8	φ,	45.1	8	ω
ô	0	00.1	00 1	7.870	48.3	8	0.00		28.1	17	K
ć	C	1.00	00	072.7	77.6	7.0	89.9	8	7 7	2	5
	9	00.1	00	0.790	0.40	, r	74.5	8,0	10		3
7	9	000	o	121.3	021		50.00	4	, K	, v	۲
3 6	•	, ,	70	707	100	•) (X) Y	4 (3 4
3 1	? '		•) h		1 (1 1	; ; ;		, ,	4 (
5	٠.	0	5	7.434	247		, , ,	^ '		٧.	2 (
o	0	100	2	141	21.2	.	90		37.	7	26
ö	•	00	00	121.3	021.2	0	6 06		22.5	M,	82
\ddot{c}	٥.	00	0	121.3	021,2	2.7	76.8	Ö	13.8	٥.5	73.
S	0	65	65.3	121.3	26.0	7:1	63.7	4	03.4	**	59
g	9	33	53.1	121.3	68.2	4:2	51.6	1.2	.4	2,5	58.
2	٥.	00	9	121.3	021.2	2	40.3	ó	Š	٠,	N
5	٥.	00.1	00.1	121 3	021.2	1.6	29.9	Ò,	7	***	795
0	0	00.1	8	121.3	021.2	0.7	20.3	ų	0.6	۲,	н
02	0	00	00.1	121.3	021.2	6.6	11.4	۲.	. 4	M	Ν
022	0	100.1	00	121.3	021.2	Ŋ	03.1	'n	4.	٥,	м
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APPENDIX - 2 : TOPOGRAPHY AND GEOLOGY

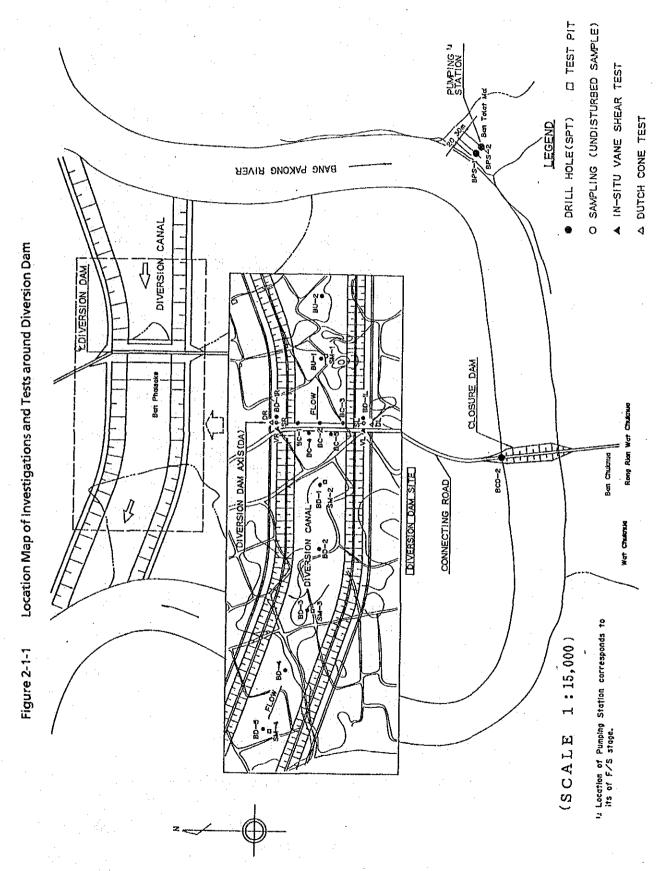
APPENDIX - 2. TOPOGRAPHY AND GEOLOGY

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2. 1 Location Map of Investigations and Tests

2.1.1 Figure



2. 2 Bore-Hole Logs

2. 2. 1 Figure

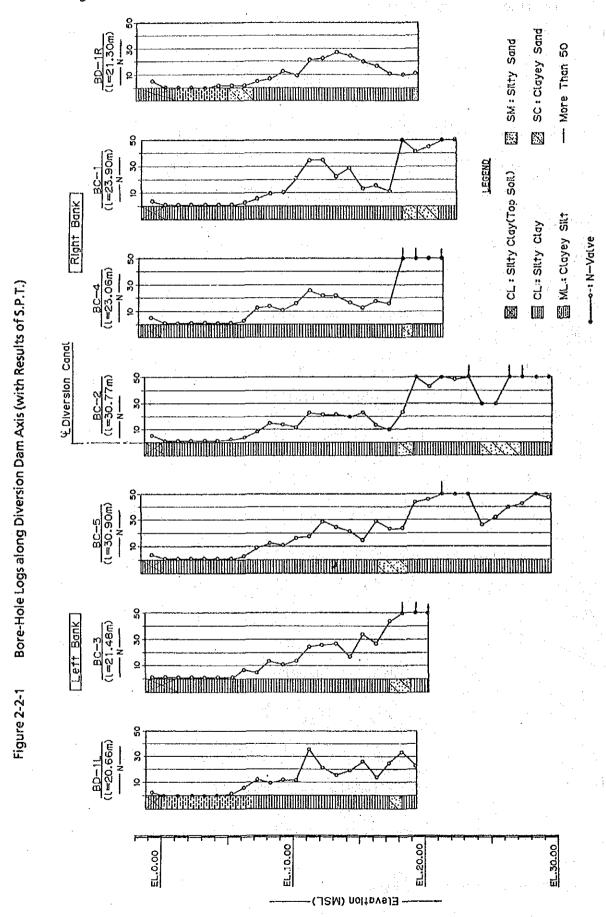


Figure 2-2-2 Bore-Hole Logs along Diversion Canal (with Results of S.P.T.)

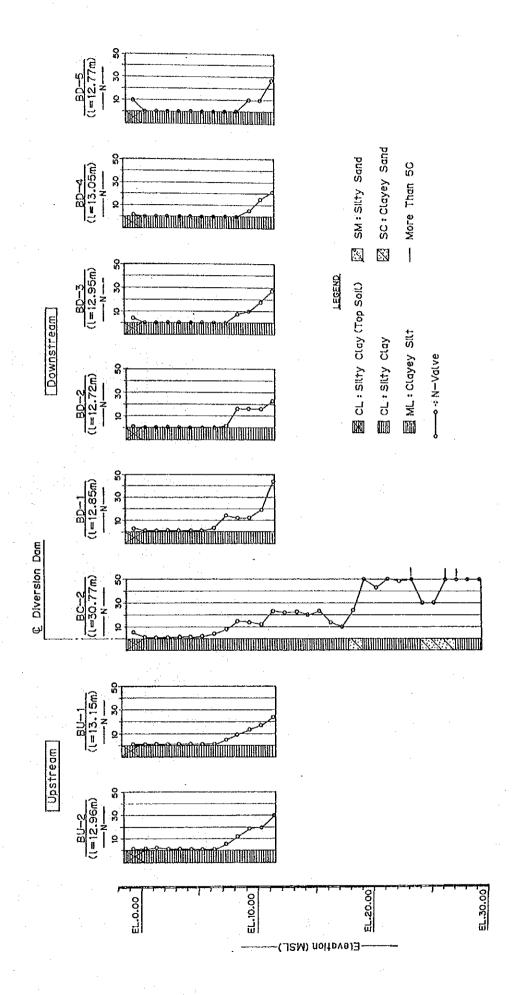
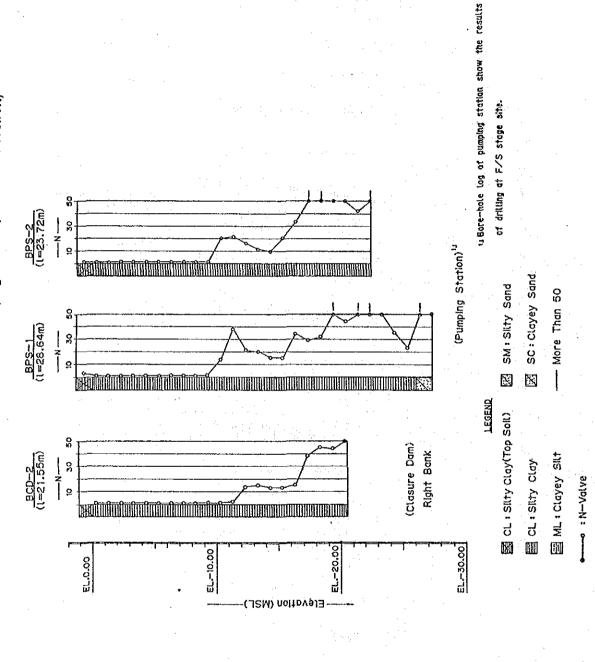


Figure 2-2-3 Bore-Hole Logs at Closure Dam and Pumping Station (with Results of S.P.T.)



2. 3. 1 Figure

Soil Profile of Diversion Dam Axis

Figure 2-3-1

RIGHT BANK 8 8 8 ± 2 = V X (17) Sity sand, non-low sand (18) plasticity, very dense, sand (18) fine, moist, brown (SM) 9 37.50m වි \$ 2 kg n x = e % % % +1.66 7/15 Clayey sand, medium plasticity, dense to very dense, sand is fine, moist. yearicity, medium sand is the to coarse, maist, brown (SC) ĝ 9 ភូ 50/25cm 8 80.2 131 25 Silty sand, non-plastic, 22 medium to very dense, sand was it into to coarse, moist, 23 prown (SM) Lean cley, sity clay,
s tow-medium plasticity, very
is sort to hard, moist, black
in gray, reddish brown (CL) (30) Ground Surface 37.50m ਹੁ و ور -18.70 1-29.45 Sifty clay, medium plasticity, hard, moist, reddish brown (CL) (SMS) clay, medium plasticit soft to medium.moist rize Clayey sand, medium. rzr, plasticity, very dense, so rzrr is fine to coarse, moist, 9 g 52 - trait -17.27 1,000 -20.00 --------LEFT BANK -18.00 +0.00 ⊢ -2.8 +2,00 -4.00 9.00 -10,00 -26.00 400 -8.00 -12.00 -14.00 -16.00 -28.00 -22.00 -24.00 30.00

CL'* Sity clay medium plasticity, very soft to soft to medium to stiff, moist, brown.

Elevation (MSL.)

CL. Lean clay, sity clay, low-medium, plasticity, very soft to medium, siff to very siff, moist, black gray brown.

SC= Clayey sand, medium plasticity, medium, sand is tine to coarse, moist, brown.

Figure 2-3-2 Soil Profile of Diversion Canal

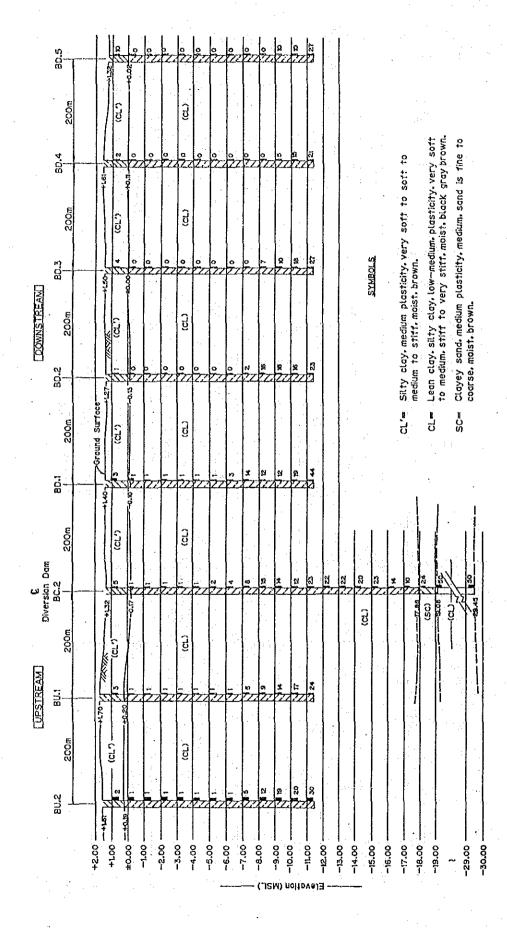
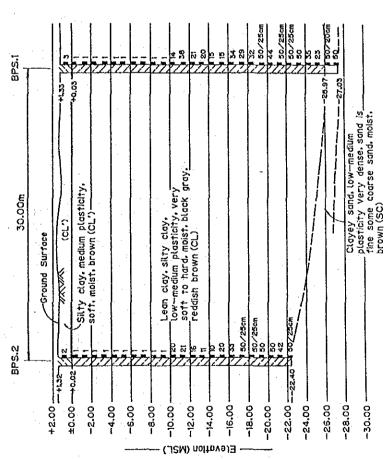


Figure 2-3-3 Soil Profile at Pumping Station



ij Bore-hole logs of pumping station show the results of drilling at ${\sf F}/{\sf S}$ stage site.

CL'= Silty clay, medium plasticity, very soft to soft to medium to stiff, moist, brown.

SYMBOLS

CL= Lean clay, sitty clay, low-medium, plasticity, very soft to medium, stiff to very stiff, maist, black gray brown.

SC= Clayey sand, medium plasticity. medium. sand is fine to coarse. moist, brown.

2.4 Result of Soil Tests

2. 4. 1 Figure

Figure 2-4-1 Distribution of N-Value in Depth around Diversion Dam

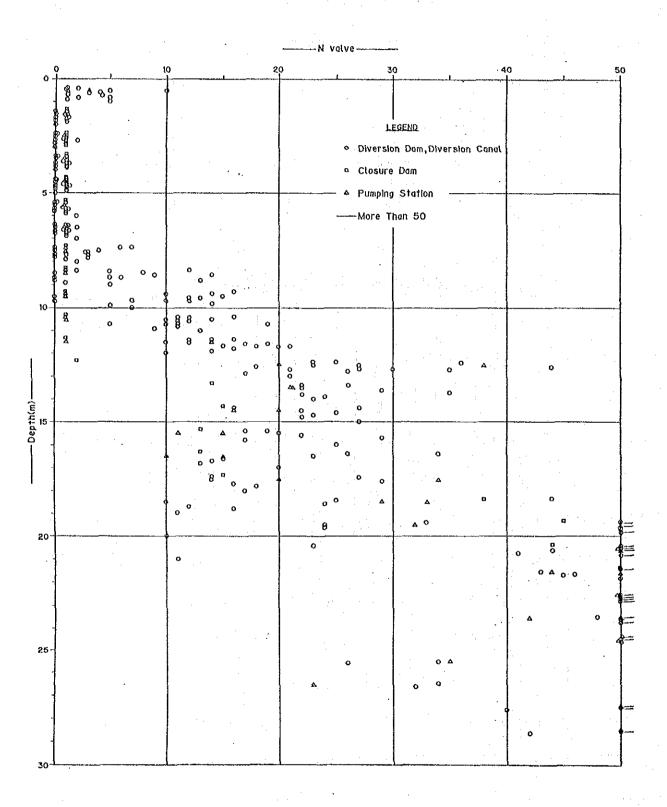


Figure 2-4-2 Result of In-situ Vane Shear Test in Depth

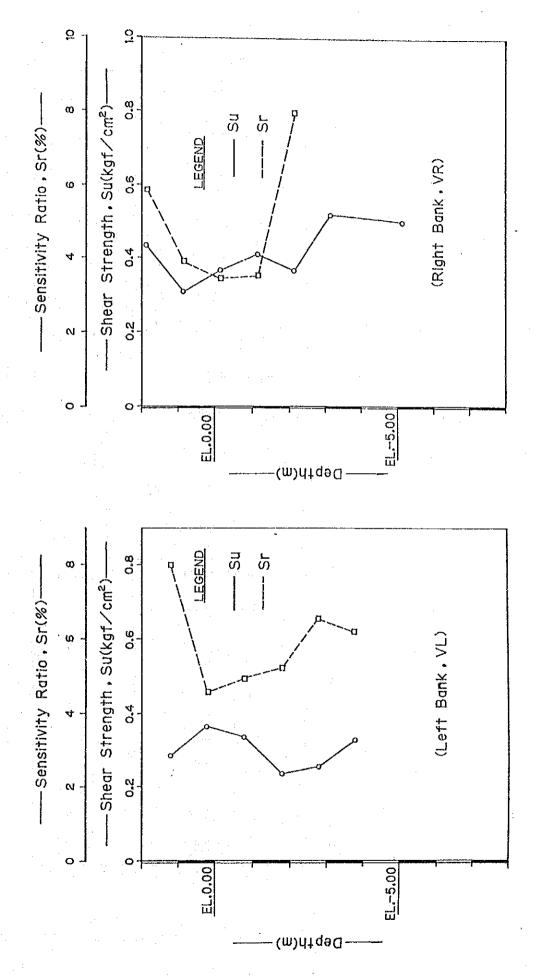


Figure 2-4-3 Result of Cone Penetration Test in Depth by Dutch Cone

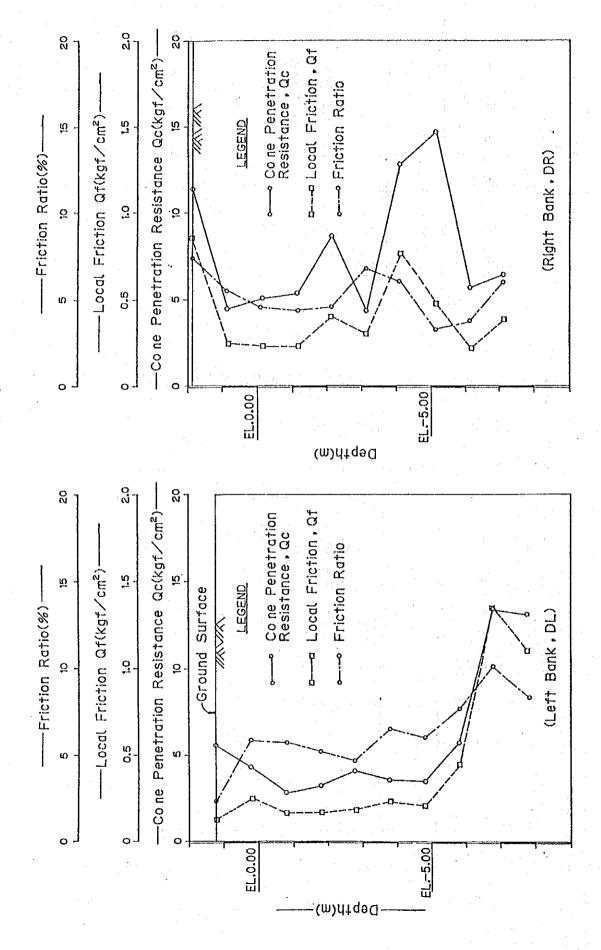


Figure 2-4-4 Result of Soil Test in Depth by Undistributed Samples

