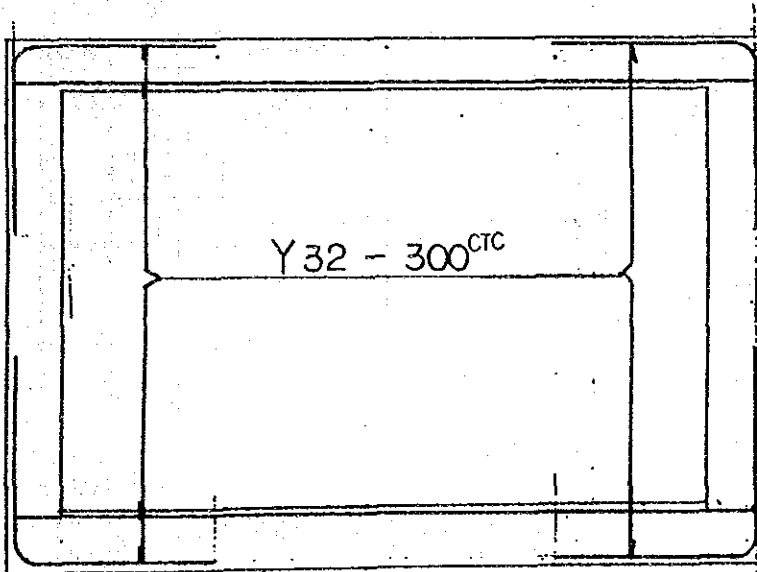
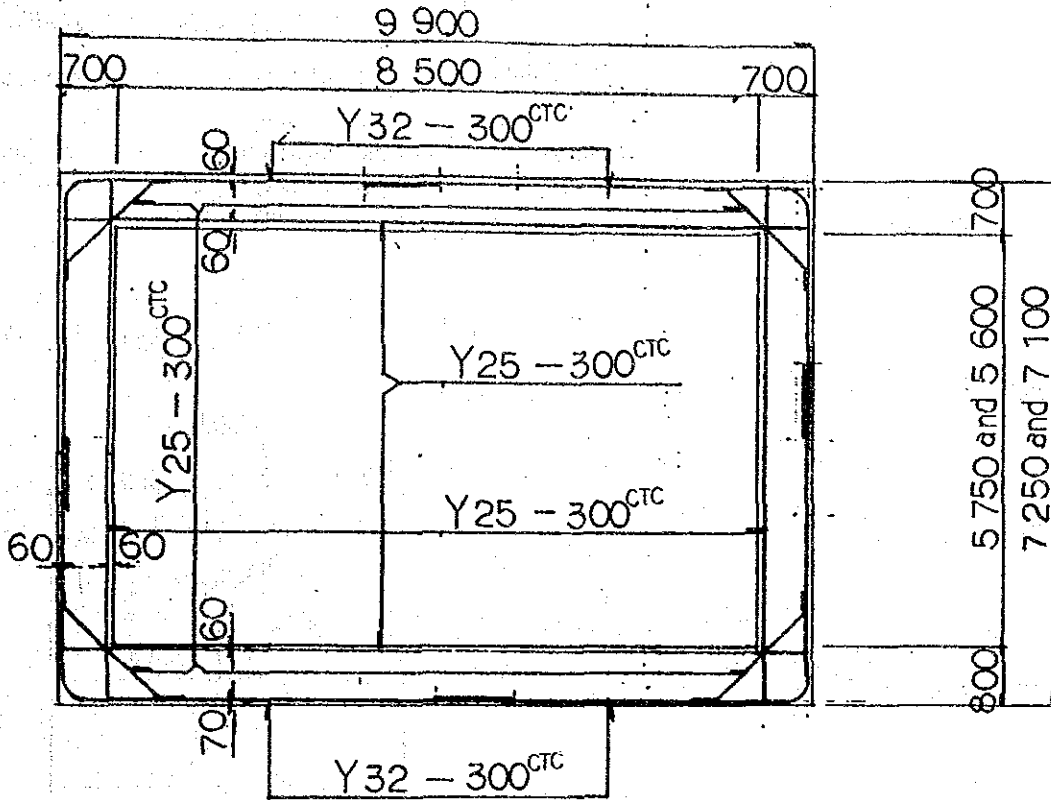


NO ④⑤⑥ BOX CULVERT FOR ROAD



NO④ BOX FOR ROAD
(similar Box - NO⑤, NO⑥)

B. Type-2 D= 2.000 m

(1) Dead load

a) vertical load ----- (case-1)

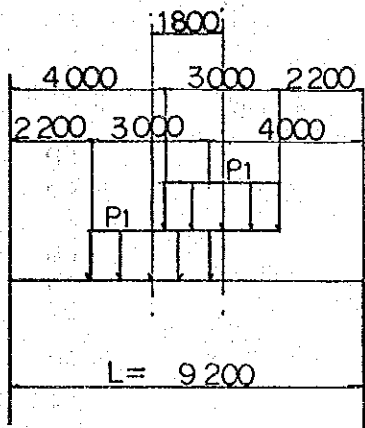
For upper slab $w_1 = 22.6 \times 0.50 + 19.6 \times 1.50 + 23.6 \times 0.70 = 57.220 \text{ kN/m}$
 For side wall $w_2 = 23.6 \times 0.70 = 16.520 \text{ ''}$
 For bottom slab $w_3 = 57.220 + \frac{2 \times 16.520 \times 6.40}{9.20} = 80.204 \text{ ''}$

b) Horizontal load --- earth pressure ----- (case-2)

For side wall $P_1 = (22.6 \times 0.50 + 19.60 \times 1.85) \times 0.50 = 23.780 \text{ kN/m}$
 $P_2 = (22.6 \times 0.50 + 19.60 \times 8.25) \times 0.50 = 86.500 \text{ ''}$

(2) Live load

a) Vertical load of center ----- (case-3)

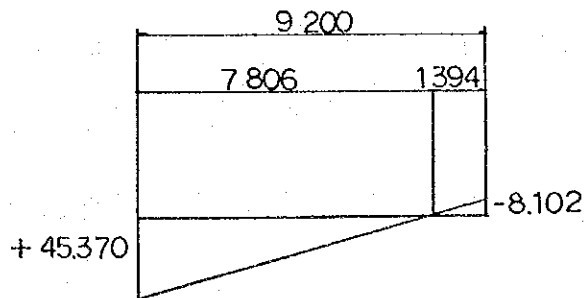
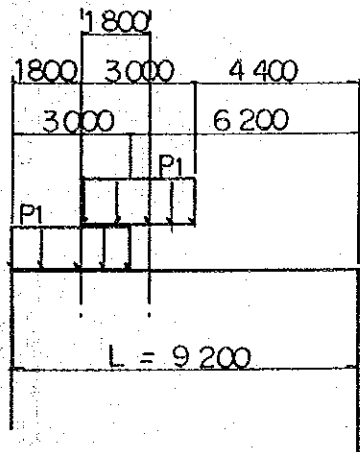


$B = 0.300 + 2.000 + 0.700 = 3.000 \text{ m}$
 $P_1 = \frac{10 \text{ kN/axle} \times 30 \text{ unit}}{3.50 \times B} = \frac{10 \times 30}{3.50 \times 3.00} = 28.572 \text{ KN/m}$

For bottom slab

$P_2 = \frac{2 \times 28.572 \times 3.00}{9.20} = 18.634 \text{ KN/m}$

b) Vertical load of partial ----- (case-4)



For bottom slab

$P_2 = \frac{2 \times 28.572 \times 3.00}{9.20} \pm \frac{6 \times 28.572 \times 3.00 (3.10 + 1.30)}{9.20^2}$
 $= 18.634 \pm 26.736 = \begin{cases} P_2-1 = +45.370 \text{ KN/m} \\ P_2-2 = -8.102 \text{ KN/m} \end{cases}$

c) Horizontal load (earth pressure of live load surcharge) ----- (case-5)

$g_0 = \frac{40 \text{ kN/vehicle} \times 30 \text{ unit}}{3.50 \times 10.0} = 34.300 \text{ KN/m}$
 $P_e = g_0 \times 0.50 = 34.300 \times 0.50 = 17.150 \text{ KN/m}$

BOX FOR ROAD NO 4 Depth = 2.000 APPLICATION BOXS NO 5.N06

No	X (m)	Y (m)
1	0.0000	0.0000
2	0.0000	6.4000
3	9.2000	6.4000
4	9.2000	0.0000

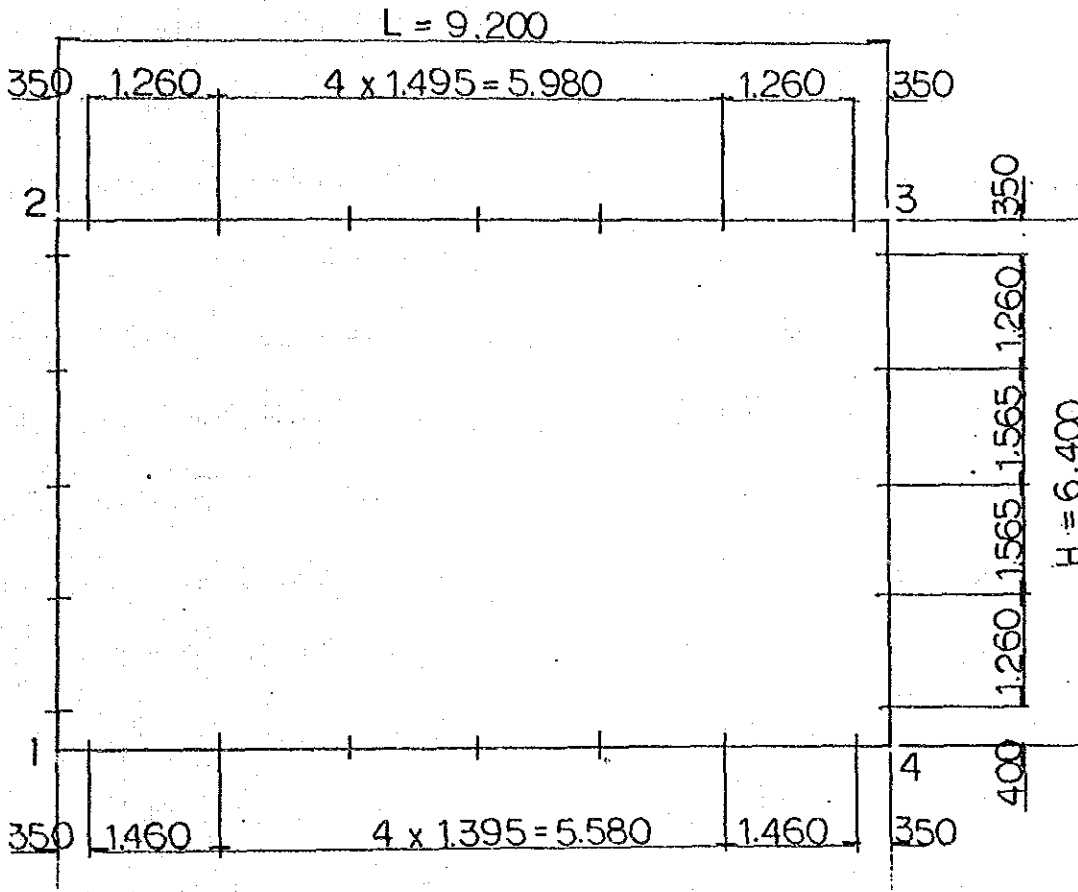
NOTE: THE DIMENSION(I) BE EXCHANG TO
DIMENSION(KN) INTO THIS CALCULATION

No	I	J	A (m2)	I (m4)	I - J	L (m)	E (t/m2)	EPS
1	1	2	0.70000	0.028580	Fix - Fix	6.400	2.50E+07	1.00E-05
2	2	3	0.70000	0.028580	Fix - Fix	9.200	2.50E+07	1.00E-05
3	3	4	0.70000	0.028580	Fix - Fix	6.400	2.50E+07	1.00E-05
4	4	1	0.80000	0.042870	Fix - Fix	9.200	2.50E+07	1.00E-05

	X (t/m)	Y (t/m)	M (tm/Rad)
1	Fix	Fix	Free
4	Free	Fix	Free

No	L-No	L-No	L-No	L-No	L-No	L-No	L-No	L-No
1	11	12	13	14	15	16	17	18
2	1	2	3	4	5	6	7	8
3	9	10	11	12	13	14	15	16
4	17	18	19	20	21	22	23	24

CALCULATION POINTS OF EACH FORCE



: Dead load
No. : 1

No	i - j	Li (m)	Lo (m)	Pi (t/m)	Pj (t/m)
1	1- 2	-Y 0.000	6.400	-16.520	-16.520
3	3- 4	-Y 0.000	6.400	-16.520	-16.520
2	2- 3	-Y 0.000	9.200	-57.220	-57.220
4	4- 1	-Y 0.000	9.200	80.204	80.204

$\Sigma V = -0.003 (t)$
 $\Sigma H = 0.000 (t)$

: Earth pressure
No. : 2

No	i - j	Li (m)	Lo (m)	Pi (t/m)	Pj (t/m)
1	1- 2	-X 0.000	6.400	86.500	23.780
3	3- 4	-X 0.000	6.400	-23.780	-86.500

$\Sigma V = 0.000 (t)$
 $\Sigma H = 0.000 (t)$

: HB live load-VL-
No. : 3

No	i - j	Li (m)	Lo (m)	Pi (t/m)	Pj (t/m)
2	2- 3	-Y 2.200	3.000	-28.572	-28.572
2	2- 3	-Y 4.000	3.000	-28.572	-28.572
4	4- 1	-Y 0.000	9.200	18.634	18.634

BOX FOR ROAD NO 4

: HB live load-VL-
No. : 4

No	i	-j	Li (m)	Lo (m)	Pi (t/m)	Pj (t/m)
2	2-	3	-Y 0.000	3.000	-28.572	-28.572
2	2-	3	-Y 1.800	3.000	-28.572	-28.572
4	4-	1	-Y 0.000	1.394	-8.102	0.000
4	4-	1	-Y 1.394	7.806	0.000	45.370

$\Sigma V = 0.000 (t)$
 $\Sigma H = 0.000 (t)$

: HB live load-HL-
No. : 5

No	i	-j	Li (m)	Lo (m)	Pi (t/m)	Pj (t/m)
1	1-	2	-X 0.000	6.400	17.150	17.150
3	3-	4	-X 0.000	6.400	-17.150	-17.150

$\Sigma V = 0.000 (t)$
 $\Sigma H = 0.000 (t)$

BOX FOR ROAD NO 4

C-No 1 C-No 2 C-No 3
No 5 No 7 No 8

No 1 1.3800 1.3800 1.3800
No 2 1.6500 1.6500 1.6500
No 3 1.4300 0.0000 0.0000
No 4 0.0000 1.4300 0.0000
No 5 0.0000 0.0000 1.6500

No 1 : 6 7 8

No.	Case. 1			Case. 2			Case. 3		
	RX (t)	RY (t)	RM (tm)	RX (t)	RY (t)	RM (tm)	RX (t)	RY (t)	RM (tm)
1.	0.000	0.002	0.000	0.000	0.000	0.000	0.000	0.000	0.000
4.	0.000	0.002	0.000	0.000	0.000	0.000	0.000	0.000	0.000
No.	Case. 4			Case. 5			Case. 6		
	RX (t)	RY (t)	RM (tm)	RX (t)	RY (t)	RM (tm)	RX (t)	RY (t)	RM (tm)
1.	0.000	-0.001	0.000	0.000	0.000	0.000	0.000	0.002	0.000
4.	0.000	0.001	0.000	0.000	0.000	0.000	0.000	0.002	0.000
No.	Case. 7			Case. 8					
	RX (t)	RY (t)	RM (tm)	RX (t)	RY (t)	RM (tm)			
1.	0.000	0.001	0.000	0.000	0.002	0.000			
4.	0.000	0.003	0.000	0.000	0.002	0.000			

BOX FOR ROAD NO 4

No.	Case. 1			Case. 2			Case. 3		
	X-DIS. (mm)	Y-DIS. (mm)	ROTA. (mmRad)	X-DIS. (mm)	Y-DIS. (mm)	ROTA. (mmRad)	X-DIS. (mm)	Y-DIS. (mm)	ROTA. (mmRad)
1.	0.00000	0.00000	12.01597	0.00000	0.00000	-4.54327	0.00000	0.00000	3.3386
2.	-0.04369	-1.15594	-11.15536	-0.13444	0.00000	4.48011	0.04783	-0.31348	-4.2808
3.	0.00291	-1.15594	11.15536	-0.85681	0.00000	-4.48011	-0.00319	-0.31348	4.2808
4.	-0.04078	0.00000	-12.01597	-0.99124	0.00000	4.54327	0.04464	0.00000	-3.3386

No.	Case. 4			Case. 5			Case. 6		
	X-DIS. (mm)	Y-DIS. (mm)	ROTA. (mmRad)	X-DIS. (mm)	Y-DIS. (mm)	ROTA. (mmRad)	X-DIS. (mm)	Y-DIS. (mm)	ROTA. (mmRad)
1.	0.00000	0.00000	3.41742	0.00000	0.00000	-1.34866	0.00000	0.00000	13.8599
2.	1.44103	-0.47367	-4.22449	0.01154	0.00000	1.47088	-0.21371	-2.04346	-14.1238
3.	1.42140	-0.15328	2.62255	-0.27005	0.00000	-1.47088	-1.41428	-2.04346	14.1238
4.	0.01718	0.00000	-2.70462	-0.25851	0.00000	1.34866	-1.62799	0.00000	-13.8599

No.	Case. 7			Case. 8		
	X-DIS. (mm)	Y-DIS. (mm)	ROTA. (mmRad)	X-DIS. (mm)	Y-DIS. (mm)	ROTA. (mmRad)
1.	0.00000	0.00000	13.97254	0.00000	0.00000	6.86036
2.	1.77857	-2.27254	-14.04324	-0.26307	-1.59519	-5.57526
3.	0.62289	-1.81438	11.75247	-1.85529	-1.59519	5.57526
4.	-1.66726	0.00000	-12.95325	-2.11836	0.00000	-6.86036

BOX FOR ROAD NO 4

No	L(m)	Case 1 Dead load			Case 2 Earth pressure			Case 3 HB live load-VI-			
		M (tm)	N (t)	S (t)	M (tm)	N (t)	S (t)	M (tm)	N (t)	S (t)	
1-	2	0.000	-287.053	8.864	-368.940	-105.359	215.488	0.000	-54.008	-9.705	-85.716
*	1	0.400	-283.507	8.864	-362.332	-25.980	181.672	0.000	-57.890	-9.705	-85.716
*	2	1.660	-272.338	8.864	-341.517	140.642	85.400	0.000	-70.119	-9.705	-85.716
*	3	3.225	-258.465	8.864	-315.663	194.548	-12.511	0.000	-85.307	-9.705	-85.716
*	4	4.790	-244.592	8.864	-289.809	114.003	-86.421	0.000	-100.495	-9.705	-85.716
*	5	6.050	-233.422	8.864	-268.994	-23.022	-128.485	0.000	-112.723	-9.705	-85.716
2-	1	6.400	-230.320	8.864	-263.212	-69.588	-137.408	0.000	-116.120	-9.705	-85.716
2-	3	0.000	-230.320	263.212	8.864	-69.588	0.000	-137.408	-116.120	85.716	-9.705
*	1	0.350	-141.700	243.185	8.864	-69.588	0.000	-137.408	-86.119	85.716	-9.705
*	2	1.610	119.291	171.088	8.864	-69.588	0.000	-137.408	21.883	85.716	-9.705
*	3	3.105	311.124	85.544	8.864	-69.588	0.000	-137.408	138.328	59.858	-9.705
*	4	4.600	375.068	0.000	8.864	-69.588	0.000	-137.408	190.743	0.000	-9.705
*	5	6.095	311.124	-85.544	8.864	-69.588	0.000	-137.408	138.328	-59.858	-9.705
*	6	7.590	119.291	-171.088	8.864	-69.588	0.000	-137.408	21.883	-85.716	-9.705
*	7	8.850	-141.700	-243.185	8.864	-69.588	0.000	-137.408	-86.119	-85.716	-9.705
3-	2	9.200	-230.320	-263.212	8.864	-69.588	0.000	-137.408	-116.120	-85.716	-9.705
3-	4	0.000	-230.320	-8.864	-263.212	-69.588	137.408	0.000	-116.120	9.705	-85.716
*	1	0.350	-263.422	-8.864	-268.994	-23.022	128.485	0.000	-112.723	9.705	-85.716
*	2	1.610	-244.592	-8.864	-289.809	114.003	86.421	0.000	-100.495	9.705	-85.716
*	3	3.175	-258.465	-8.864	-315.663	194.548	12.511	0.000	-85.307	9.705	-85.716
*	4	4.740	-272.338	-8.864	-341.517	140.642	-83.400	0.000	-70.119	9.705	-85.716
*	5	6.000	-283.507	-8.864	-362.332	-25.980	-181.672	0.000	-57.890	9.705	-85.716
4-	3	6.400	-287.053	-8.864	-368.940	-105.359	-215.488	0.000	-54.008	9.705	-85.716
4-	1	0.000	-287.053	368.938	-8.864	-105.359	0.000	-215.488	-54.008	85.716	9.705
*	1	0.350	-162.837	340.867	-8.864	-105.359	0.000	-215.488	-25.149	79.194	9.705
*	2	1.810	249.348	223.769	-8.864	-105.359	0.000	-215.488	70.615	51.989	9.705
*	3	3.205	483.466	111.885	-8.864	-105.359	0.000	-215.488	125.008	25.994	9.705
*	4	4.600	561.506	0.000	-8.864	-105.359	0.000	-215.488	143.139	0.000	9.705
*	5	5.995	483.466	-111.885	-8.864	-105.359	0.000	-215.488	125.008	-25.994	9.705
*	6	7.390	249.348	-223.769	-8.864	-105.359	0.000	-215.488	70.615	-51.989	9.705
*	7	8.850	-162.837	-340.867	-8.864	-105.359	0.000	-215.488	-25.149	-79.195	9.705
1-	4	9.200	-287.053	-368.938	-8.864	-105.359	0.000	-215.488	-54.008	-85.716	9.705

BOX FOR ROAD NO 4

No	L(m)	Case 4 HB live load-VL-		Case 5 HB live load-HL-		Case 6		S (t)	N (t)	N (t)
		M (tm)	S (t)	M (tm)	S (t)	M (tm)	S (t)			
1-	2	0.000	-3.734	-129.520	-31.276	56.197	0.000	-647.208	353.910	-631.711
*	1	0.400	-3.734	-129.520	-10.169	49.337	0.000	-516.889	298.114	-622.592
*	2	1.650	-3.734	-129.520	38.382	27.728	0.000	-244.036	139.266	-593.867
*	3	3.225	-3.734	-129.520	60.774	0.888	0.000	-157.666	-22.289	-558.189
*	4	4.790	-3.734	-129.520	41.162	-25.951	0.000	-293.140	-144.240	-522.511
*	5	6.050	-3.734	-129.520	-5.150	-47.560	0.000	-521.903	-213.645	-493.786
2-	1	6.400	-3.734	-129.520	-22.847	-53.563	0.000	-598.713	-228.368	-485.806
2-	3	0.000	129.520	-3.734	-22.847	0.000	-53.563	-598.713	485.806	-228.368
*	1	0.350	119.519	-3.734	-22.847	0.000	-53.563	-433.517	458.169	-228.368
*	2	1.610	74.233	-3.734	-22.847	0.000	-53.563	81.095	358.675	-228.368
*	3	3.105	142.991	-3.734	-22.847	0.000	-53.563	512.339	203.648	-228.368
*	4	4.600	120.805	-3.734	-22.847	0.000	-53.563	675.537	0.000	-228.368
*	5	6.055	58.717	-3.734	-22.847	0.000	-53.563	512.339	-203.648	-228.368
*	6	7.590	-3.942	-3.734	-22.847	0.000	-53.563	81.095	-358.675	-228.368
*	7	8.850	-56.752	-3.734	-22.847	0.000	-53.563	-433.517	-458.169	-228.368
3-	2	9.200	-71.421	-3.734	-22.847	0.000	-53.563	-598.713	-485.806	-228.368
3-	4	0.000	3.734	-41.912	-22.847	53.563	0.000	-598.713	228.368	-485.806
*	1	0.350	-70.114	-41.912	-5.150	47.560	0.000	-521.903	213.645	-493.786
*	2	1.610	-65.410	-41.912	41.162	25.951	0.000	-293.140	144.240	-522.511
*	3	3.175	-59.566	-41.912	60.774	-0.888	0.000	-157.666	22.289	-558.189
*	4	4.740	-53.723	-41.912	38.382	-27.728	0.000	-244.036	-139.266	-593.867
*	5	6.000	-49.018	-41.912	-10.169	-49.337	0.000	-516.889	-298.114	-622.592
4-	3	6.400	-47.525	-41.912	-31.276	-56.197	0.000	-647.208	-353.910	-631.711
4-	1	0.000	41.912	3.734	-31.276	0.000	-56.197	-647.208	631.709	-353.910
*	1	0.350	44.392	3.734	-31.276	0.000	-56.197	-434.521	583.645	-353.910
*	2	1.810	35.863	3.734	-31.276	0.000	-56.197	271.236	383.146	-353.910
*	3	3.205	96.524	3.734	-31.276	0.000	-56.197	672.102	191.573	-353.910
*	4	4.600	136.701	3.734	-31.276	0.000	-56.197	805.724	0.000	-353.910
*	5	5.995	140.616	3.734	-31.276	0.000	-56.197	672.102	-191.573	-353.910
*	6	7.390	92.491	3.734	-31.276	0.000	-56.197	271.236	-383.146	-353.910
*	7	8.850	-30.772	3.734	-31.276	0.000	-56.197	-434.521	-583.645	-353.910
1-	4	9.200	-73.366	3.734	-31.276	0.000	-56.197	-647.208	-631.709	-353.910

BOX FOR ROAD NO 4

No	L(m)	Case 7			Case 8			
		M (tm)	S (t)	N (t)	M (tm)	S (t)	N (t)	
1-	2	0.000	-674.890	362.449	-694.350	-621.580	460.513	-509.137
*	1	0.400	-541.156	306.652	-685.231	-450.884	393.398	-500.018
*	2	1.660	-237.543	147.804	-656.506	-80.436	198.893	-471.293
*	3	3.225	-157.811	-13.750	-620.828	64.600	-6.945	-455.615
*	4	4.790	-279.922	-135.701	-585.150	-81.514	-173.181	-399.937
*	5	6.050	-497.326	-205.106	-556.425	-368.606	-278.242	-371.212
2-	1	6.400	-571.747	-219.830	-548.445	-470.358	-302.869	-363.233
2-	3	0.000	-571.747	548.445	-219.830	-470.358	363.233	-302.869
*	1	0.350	-387.130	506.508	-219.830	-348.063	335.595	-302.869
*	2	1.610	155.955	355.533	-219.830	12.105	236.101	-302.869
*	3	3.105	519.009	127.370	-219.830	275.834	118.031	-302.869
*	4	4.600	575.525	-51.763	-219.830	365.077	0.000	-302.869
*	5	6.095	398.496	-177.985	-219.830	275.834	-118.031	-302.869
*	6	7.590	44.105	-296.036	-219.830	12.105	-236.101	-302.869
*	7	8.850	-391.521	-395.530	-219.830	-348.063	-335.595	-302.869
3-	2	9.200	-534.794	-423.167	-219.830	-470.358	-363.233	-302.869
3-	4	0.000	-534.794	219.830	-423.167	-470.358	302.869	-363.233
*	1	0.350	-460.372	205.106	-431.147	-368.606	278.242	-371.212
*	2	1.610	-242.968	135.701	-459.872	-81.514	173.181	-359.997
*	3	3.175	-120.857	13.750	-495.550	64.600	6.945	-455.615
*	4	4.740	-220.550	-147.804	-531.228	-80.436	-198.893	-471.293
*	5	6.000	-504.202	-306.652	-559.953	-450.884	-393.398	-500.018
4-	3	6.400	-637.936	-362.449	-569.072	-621.580	-460.513	-509.137
4-	1	0.000	-637.936	569.069	-362.449	-621.580	509.135	-460.513
*	1	0.350	-444.891	533.876	-362.449	-450.162	470.390	-460.513
*	2	1.810	221.541	376.092	-362.449	118.652	308.801	-460.513
*	3	3.205	631.370	208.780	-362.449	441.735	154.401	-460.513
*	4	4.600	796.518	25.295	-362.449	549.430	0.000	-460.513
*	5	5.995	694.422	-174.365	-362.449	441.735	-154.401	-460.513
*	6	7.390	302.519	-390.199	-362.449	118.652	-308.801	-460.513
*	7	8.850	-442.501	-633.412	-362.449	-450.162	-470.396	-460.513
1-	4	9.200	-674.890	-694.349	-362.449	-621.580	-509.135	-460.513

M. MAXIMUM

M. MINIMUM

No.	L (m)	Case	M (tm)	S (t)	N (t)	Case	M (tm)	S (t)	N (t)
1 - 2	0.000	C-8	-621.580	460.513	-509.137	C-7	-674.890	362.449	-694.550
* 1	0.400	C-8	-450.884	393.398	-500.018	C-7	-541.156	306.652	-585.231
* 2	1.660	C-8	-80.436	198.895	-471.293	C-7	-257.543	147.804	-656.506
* 3	3.225	C-8	64.600	-6.945	-435.615	C-7	-157.811	-13.750	-620.828
* 4	4.790	C-8	-81.514	-173.181	-399.937	C-6	-293.140	-144.240	-522.511
* 5	6.050	C-8	-368.606	-278.242	-371.212	C-6	-521.303	-213.645	-493.786
2 - 1	6.400	C-8	-470.358	-302.869	-363.233	C-6	-598.713	-228.368	-485.806
2 - 3	0.000	C-8	-470.358	363.233	-302.869	C-6	-598.713	465.806	-228.368
* 1	0.350	C-8	-348.063	335.595	-302.869	C-6	-433.517	458.169	-228.368
* 2	1.610	C-7	155.955	355.533	-219.830	C-8	12.105	256.101	-302.869
* 3	3.105	C-7	519.009	127.370	-219.830	C-8	276.834	118.051	-302.869
* 4	4.600	C-6	675.537	0.000	-228.368	C-8	365.077	0.000	-302.869
* 5	6.095	C-6	512.339	-203.648	-228.368	C-8	276.834	-118.051	-302.869
* 6	7.590	C-6	81.095	-358.675	-228.368	C-8	12.105	-236.101	-302.869
* 7	8.850	C-8	-348.063	-335.533	-302.869	C-6	-433.517	-458.169	-228.368
3 - 2	9.200	C-8	-470.358	-363.233	-302.869	C-6	-598.713	-485.806	-228.368
3 - 4	0.000	C-8	-470.358	302.869	-363.233	C-6	-598.713	228.368	-485.806
* 1	0.350	C-8	-368.606	278.242	-371.212	C-6	-521.303	213.645	-493.786
* 2	1.610	C-8	-81.514	173.181	-399.937	C-6	-293.140	144.240	-522.511
* 3	3.175	C-8	64.600	6.945	-435.615	C-6	-157.666	22.289	-558.189
* 4	4.740	C-8	-80.436	-198.895	-471.293	C-6	-244.036	-139.266	-593.807
* 5	6.000	C-8	-450.884	-393.398	-500.018	C-6	-516.889	-298.114	-622.592
4 - 3	6.400	C-8	-621.580	-460.513	-509.137	C-6	-647.208	-333.910	-631.711
4 - 1	0.000	C-8	-621.580	509.135	-460.513	C-6	-647.208	631.709	-353.910
* 1	0.350	C-6	-434.521	583.645	-353.910	C-8	-450.162	470.396	-460.513
* 2	1.810	C-6	271.236	383.146	-353.910	C-8	118.652	308.801	-460.513
* 3	3.205	C-6	672.102	191.573	-353.910	C-8	441.735	154.401	-460.513
* 4	4.600	C-6	805.724	0.000	-353.910	C-8	549.430	0.000	-460.513
* 5	5.995	C-7	694.422	-174.365	-362.449	C-8	441.735	-154.401	-460.513
* 6	7.390	C-7	302.519	-390.199	-362.449	C-8	118.652	-308.801	-460.513
* 7	8.850	C-6	-434.521	-583.645	-353.910	C-8	-450.162	-470.396	-460.513
1 - 4	9.200	C-8	-621.580	-509.135	-460.513	C-7	-674.890	-694.549	-392.449

S. MAXIMUM

S. MINIMUM

No.	L (m)	Case	M (tm)	S (t)	N (t)	Case	M (tm)	S (t)	N (t)
1 -	0.000	C- 8	-621.580	460.513	-509.137	C- 6	-647.208	353.910	-631.711
* 1	0.400	C- 8	-450.984	393.398	-400.018	C- 6	-516.889	298.114	-522.592
* 2	1.650	C- 8	-80.436	198.895	-471.292	C- 6	-244.036	139.266	-593.867
* 3	3.225	C- 8	64.600	-6.945	-435.615	C- 6	-157.666	-22.289	-558.189
* 4	4.790	C- 7	-279.922	-135.701	-585.150	C- 8	-81.514	-173.181	-399.937
* 5	6.050	C- 7	-497.326	-205.106	-556.425	C- 8	-368.606	-278.242	-371.212
2 -	6.400	C- 7	-571.747	-219.830	-548.445	C- 8	-470.358	-302.869	-363.233
2 -	0.000	C- 7	-571.747	548.445	-219.830	C- 8	-470.358	363.233	-302.869
* 1	0.350	C- 7	-387.130	506.508	-219.830	C- 8	-348.063	335.595	-302.869
* 2	1.610	C- 6	81.095	<u>358.675</u>	-228.368	C- 8	12.105	236.101	-302.869
* 3	3.105	C- 6	512.339	203.648	-228.368	C- 8	276.834	118.051	-302.869
* 4	4.600	C- 6	675.537	0.000	-228.368	C- 7	575.525	-51.763	-219.830
* 5	6.095	C- 8	276.834	-118.051	-302.869	C- 6	512.339	-203.648	-228.368
* 6	7.590	C- 8	12.105	-236.101	-302.869	C- 6	81.095	<u>358.675</u>	-228.368
* 7	8.850	C- 8	-348.063	-335.595	-302.869	C- 6	-433.517	-458.169	-228.368
3 -	9.200	C- 8	-470.358	-363.233	-302.869	C- 6	-598.713	-485.806	-228.368
3 -	0.000	C- 8	-470.358	302.869	-363.233	C- 7	-534.794	219.830	-423.167
* 1	0.350	C- 8	-368.606	278.242	-371.212	C- 7	-460.372	205.106	-431.147
* 2	1.610	C- 8	-81.514	173.181	-399.937	C- 7	-242.968	135.701	-459.872
* 3	3.175	C- 6	-157.666	22.289	-558.189	C- 8	64.600	6.945	-435.615
* 4	4.740	C- 6	-244.036	-139.266	-393.867	C- 8	-80.436	-198.895	-471.293
* 5	6.000	C- 6	-516.889	-298.114	-622.592	C- 8	-450.884	-393.398	-500.018
4 -	6.400	C- 6	-647.208	-353.910	-631.711	C- 8	-621.580	-460.513	-509.137
4 -	0.000	C- 6	-647.208	631.709	-353.910	C- 8	-621.580	509.135	-460.513
* 1	0.350	C- 6	-434.521	583.645	-353.910	C- 8	-450.162	470.396	-460.513
* 2	1.810	C- 6	271.236	<u>383.146</u>	-353.910	C- 8	118.652	308.801	-460.513
* 3	3.205	C- 7	631.370	208.780	-362.449	C- 8	441.735	154.401	-460.513
* 4	4.600	C- 7	796.518	25.295	-362.449	C- 6	805.724	0.000	-353.910
* 5	5.995	C- 8	441.735	-154.401	-460.513	C- 6	672.102	-191.573	-353.910
* 6	7.390	C- 8	118.652	-308.801	-460.513	C- 7	302.519	<u>390.199</u>	-362.449
* 7	8.850	C- 8	-450.162	-470.396	-460.513	C- 7	-442.561	-633.412	-362.449
1 -	9.200	C- 8	-621.580	-509.135	-460.513	C- 7	-674.890	-694.349	-362.449

N. MAXIMUM

N. MINIMUM

No.	L (m)	Case	M (tm)	S (t)	N (t)	Case	M (tm)	S (t)	N (t)
1 - 2	0.000	C- 8	-621.580	460.513	-509.137	C- 7	-674.890	362.449	-694.350
* 1	0.400	C- 8	-450.884	393.398	-500.018	C- 7	-541.156	306.652	-585.231
* 2	1.660	C- 8	-80.436	198.855	-471.293	C- 7	-257.543	147.804	-556.500
* 3	3.225	C- 8	64.600	-6.945	-435.615	C- 7	-157.811	17.750	-620.828
* 4	4.790	C- 8	-81.514	-173.181	-399.937	C- 7	-279.922	-133.701	-585.130
* 5	6.050	C- 8	-368.606	-278.242	-371.212	C- 7	-497.326	-205.106	-556.425
2 - 1	6.400	C- 8	-470.358	-302.869	-363.233	C- 7	-571.747	-219.830	-548.445
2 - 3	0.000	C- 7	-571.747	548.445	-219.830	C- 8	-470.358	363.233	-302.869
* 1	0.350	C- 7	-387.130	506.508	-219.830	C- 8	-348.063	395.595	-302.869
* 2	1.610	C- 7	155.955	355.533	-219.830	C- 8	12.105	236.101	-302.869
* 3	3.105	C- 7	519.009	127.370	-219.830	C- 8	276.834	118.051	-302.869
* 4	4.600	C- 7	575.525	-51.763	-219.830	C- 8	365.077	0.000	-302.869
* 5	6.095	C- 7	398.496	-177.985	-219.830	C- 8	276.834	-118.051	-302.869
* 6	7.590	C- 7	44.165	-296.036	-219.830	C- 8	12.105	-236.101	-302.869
* 7	8.850	C- 7	-391.521	-395.530	-219.830	C- 8	-348.063	-335.595	-302.869
3 - 2	9.200	C- 7	-534.794	-423.167	-219.830	C- 8	-470.358	-363.233	-302.869
3 - 4	0.000	C- 8	-470.358	302.869	-363.233	C- 6	-598.713	228.368	-485.806
* 1	0.350	C- 8	-368.606	278.242	-371.212	C- 6	-521.303	213.645	-493.786
* 2	1.610	C- 8	-81.514	173.181	-399.937	C- 6	-293.140	144.240	-522.511
* 3	3.175	C- 8	64.600	6.945	-435.615	C- 6	-157.666	22.289	-558.189
* 4	4.740	C- 8	-80.436	-198.895	-471.293	C- 6	-241.036	-139.266	-593.867
* 5	6.000	C- 8	-450.884	-393.398	-500.018	C- 6	-516.889	-298.114	-622.592
4 - 3	6.400	C- 8	-621.580	-460.513	-509.137	C- 6	-647.208	-353.910	-631.711
4 - 1	0.000	C- 6	-647.208	631.709	-353.910	C- 8	-621.580	509.135	-460.513
* 1	0.350	C- 6	-434.521	583.645	-353.910	C- 8	-450.102	470.396	-400.513
* 2	1.810	C- 6	271.236	383.146	-353.910	C- 8	118.652	308.801	-460.513
* 3	3.205	C- 6	672.102	191.573	-353.910	C- 8	441.735	154.401	-490.513
* 4	4.600	C- 6	805.724	0.000	-353.910	C- 8	549.430	0.000	-460.513
* 5	5.995	C- 6	672.102	-191.573	-353.910	C- 8	441.735	-154.401	-460.513
* 6	7.390	C- 6	271.236	-383.146	-353.910	C- 8	118.652	-308.801	-460.513
* 7	8.850	C- 6	-434.521	-583.645	-353.910	C- 8	-450.102	-470.396	-460.513
1 - 4	9.200	C- 6	-647.208	-631.709	-353.910	C- 8	-621.580	-509.135	-460.513

NO④ BOX FOR ROAD

(similar Box - NO⑤, NO⑥)

D = 0.500 m

(1) Dead load

a) vertical load ----- (case-1)

For upper slab $w_1 = 22.6 \times 0.50 + 23.60 \times 0.70 = 27.820 \text{ kN/m}$

For side wall $w_2 = 23.6 \times 0.70 = 16.520 \text{ ''}$

For bottom slab $w_3 = 27.820 + \frac{2 \times 16.520 \times 6.40}{9.20} = 50.804 \text{ ''}$

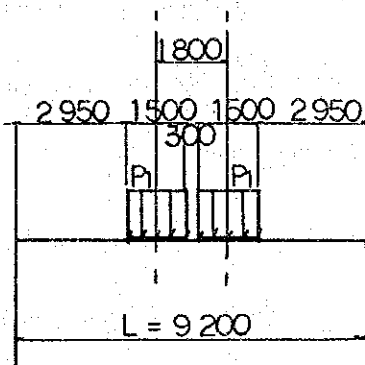
b) Horizontal load --- earth pressure ----- (case-2)

For side wall $P_1 = (22.6 \times 0.50 + 19.60 \times 0.35) \times 0.500 = 9.080 \text{ kN/m}$

$P_2 = (22.6 \times 0.50 + 19.60 \times 6.75) \times 0.500 = 71.800 \text{ ''}$

(2) Live load

a) Vertical load of center ----- (case-3)



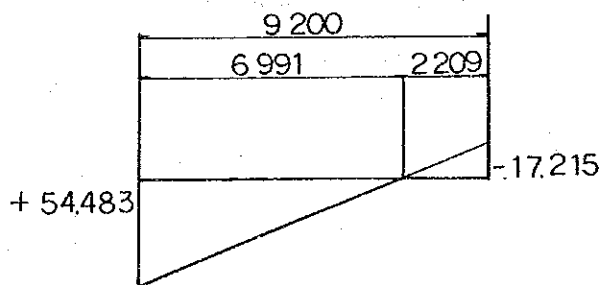
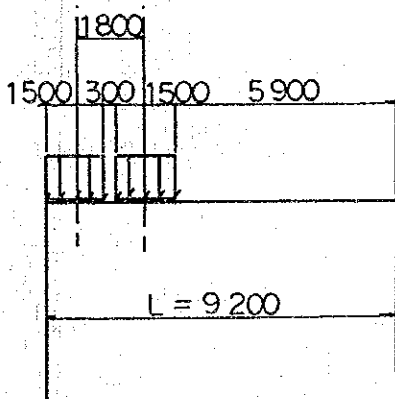
B = wide of despersion of HB-load
 $= 0.30 + 0.50 + 0.70 = 1.500 \text{ m}$

$P_1 = \frac{10 \text{ kN/axle} \times 30 \text{ unit}}{3.50 \times B}$
 $= \frac{10 \times 30}{3.50 \times 1.50} = 57.143 \text{ KN/m}$

For bottom slab

$P_2 = \frac{2 \times 57.143 \times 1.50}{9.20} = 18.634 \text{ KN/m}$

b) Vertical load of partial ----- (case-4)



For bottom slab

$P_2 = \frac{2 \times 57.143 \times 1.50}{9.20} \pm \frac{6 \times 57.143 \times 1.50 (3.85 + 2.050)}{9.20^2}$

$= 18.634 \pm 35.849 = \begin{cases} P_2-1 = +54.483 \text{ KN/m} \\ P_2-2 = -17.215 \text{ KN/m} \end{cases}$

c) Horizontal load (earth pressure of live load surcharge) ----- (case-5)

$g_0 = \frac{40 \text{ kN/rib/ole} \times 30 \text{ unit}}{3.50 \times 10.0} = 34.300 \text{ KN/m}$

$P_e = g_0 \times 0.500 = 17.150 \text{ KN/m}$

BOX FOR ROAD NO 4' Depth = 0.500 For Check

NOTE: THE DIMENSION(t)BE EXCHANG TO
DIMENSION(KN)INTO THIS CALCULATION

No	X (m)	Y (m)
1	0.0000	0.0000
2	0.0000	6.4000
3	9.2000	6.4000
4	9.2000	0.0000

No	I	J	A (m2)	I (m4)	I - J	L (m)	E (t/m2)	EPS
1	1	2	0.70000	0.028580	Fix - Fix	6.400	2.50E+07	1.00E-05
2	2	3	0.70000	0.028580	Fix - Fix	9.200	2.50E+07	1.00E-05
3	3	4	0.70000	0.028580	Fix - Fix	6.400	2.50E+07	1.00E-05
4	4	1	0.80000	0.042670	Fix - Fix	9.200	2.50E+07	1.00E-05

X (t/m) Y (t/m) M(tm/Rad)

1	Free	Fix	Free
4	Free	Fix	Free

No	L-No	L-No	L-No	L-No	L-No	L-No	L-No	L-No
1	11	2	3	4	5	6	7	8
2	12	13	14	15	16	17	18	19
3	1	2	3	4	5	6	7	8
4	9	10	11	12	13	14	15	16

: Dead load
No. : 1

No	i - j	Li (m)	Lo (m)	Pi (t/m)	Pj (t/m)
1	1- 2	0.000	6.400	-16.520	-16.520
3	3- 4	0.000	6.400	-16.520	-16.520
2	2- 3	0.000	9.200	-27.820	-27.820
4	4- 1	0.000	9.200	50.804	50.804

$\Sigma V = -0.003 (t)$
 $\Sigma H = 0.000 (t)$

: Earth pressure
No. : 2

No	i - j	Li (m)	Lo (m)	Pi (t/m)	Pj (t/m)
1	1- 2	0.000	6.400	71.800	9.080
3	3- 4	0.000	6.400	-9.080	-71.800

$\Sigma V = 0.000 (t)$
 $\Sigma H = 0.000 (t)$

: HB live load-VL-
No. : 3

No	i - j	Li (m)	Lo (m)	Pi (t/m)	Pj (t/m)
2	2- 3	2.950	1.500	-57.143	-57.143
2	2- 3	4.750	1.500	-57.143	-57.143
4	4- 1	0.000	9.200	18.634	18.634

$\Sigma V = 0.004 (t)$
 $\Sigma H = 0.000 (t)$

BOX FOR ROAD NO 4

: HB live load-VL-
No. : 4

No	i	-j	Li (m)	Lc (m)	Pi (t/m)	Pj (t/m)
2	2-	3	-Y 0.000	1.500	-57.143	-57.143
2	2-	3	-Y 1.800	1.500	-57.143	-57.143
4	4-	1	-Y 0.000	2.209	-17.215	0.000
4	4-	1	-Y 2.209	6.991	0.000	54.483

$\Sigma V = 0.002$ (t)
 $\Sigma H = 0.000$ (t)

: HB live load-HL-
No. : 5

No	i	-j	Li (m)	Lo (m)	Pi (t/m)	Pj (t/m)
1	1-	2	-X 0.000	6.400	17.150	17.150
3	3-	4	-X 0.000	6.400	-17.150	-17.150

$\Sigma V = 0.000$ (t)
 $\Sigma H = 0.000$ (t)

BOX FOR ROAD NO 4.

No	C-No 1	C-No 2	C-No 3
No	No 6	No 7	No 8
No 1	1.3800	1.3800	1.3800
No 2	1.6500	1.6500	1.6500
No 3	1.4300	0.0000	0.0000
No 4	0.0000	1.4300	0.0000
No 5	0.0000	0.0000	1.6500

No 1 : 6 7 8

No.	Case. 1			Case. 2			Case. 3		
	RX (t)	RY (t)	RM (tm)	RX (t)	RY (t)	RM (tm)	RX (t)	RY (t)	RM (tm)
1.	0.000	0.002	0.000	0.000	0.000	0.000	0.000	-0.002	0.000
4.	0.000	0.002	0.000	0.000	0.000	0.000	0.000	-0.002	0.000

No.	Case. 4			Case. 5			Case. 6		
	RX (t)	RY (t)	RM (tm)	RX (t)	RY (t)	RM (tm)	RX (t)	RY (t)	RM (tm)
1.	0.000	-0.001	0.000	0.000	0.000	0.000	0.000	-0.001	0.000
4.	0.000	-0.002	0.000	0.000	0.000	0.000	0.000	-0.001	0.000

No.	Case. 7			Case. 8		
	RX (t)	RY (t)	RM (tm)	RX (t)	RY (t)	RM (tm)
1.	0.000	0.001	0.000	0.000	0.002	0.000
4.	0.000	0.000	0.000	0.000	0.002	0.000

BOX FOR ROAD NO 4

No.	Case. 1			Case. 2			Case. 3		
	X-DIS.(mm)	Y-DIS.(mm)	ROTA.(mmRad)	X-DIS.(mm)	Y-DIS.(mm)	ROTA.(mmRad)	X-DIS.(mm)	Y-DIS.(mm)	ROTA.(mmRad)
1.	0.00000	0.00000	7.24551	0.00000	0.00000	-3.38728	0.00000	0.00000	3.3709
2.	-0.06646	-0.66134	-5.93643	-0.14433	0.00000	3.21935	0.05125	-0.31347	-4.3804
3.	0.00443	-0.66134	5.93643	-0.62534	0.00000	-3.21935	-0.00342	-0.31347	4.3804
4.	-0.06203	0.00000	-7.24551	-0.76967	0.00000	3.38728	0.04783	0.00000	-3.3709

No.	Case. 4			Case. 5			Case. 6		
	X-DIS.(mm)	Y-DIS.(mm)	ROTA.(mmRad)	X-DIS.(mm)	Y-DIS.(mm)	ROTA.(mmRad)	X-DIS.(mm)	Y-DIS.(mm)	ROTA.(mmRad)
1.	0.00000	0.00000	3.38152	0.00000	0.00000	-1.34866	0.00000	0.00000	9.2301
2.	1.06514	-0.52651	-3.68212	0.01154	0.00000	1.47088	-0.25656	-1.36092	-9.1443
3.	1.06691	-0.10043	1.99578	-0.27005	0.00000	-1.47088	-1.03058	-1.36092	9.1443
4.	-0.00155	0.00000	-2.36193	-0.25851	0.00000	1.34866	-1.28715	0.00000	-9.2301

No.	Case. 7			Case. 8		
	X-DIS.(mm)	Y-DIS.(mm)	ROTA.(mmRad)	X-DIS.(mm)	Y-DIS.(mm)	ROTA.(mmRad)
1.	0.00000	0.00000	9.24536	0.00000	0.00000	2.18451
2.	1.19330	-1.66556	-8.14578	-0.31081	-0.91263	-0.45339
3.	0.49999	-1.05627	5.73431	-1.47128	-0.91265	0.45339
4.	-1.35777	0.00000	-7.78736	-1.78208	0.00000	-2.18451

BOX FOR ROAD NO 4'

No	L(m)	Case 1 Dead load		Case 2 Earth pressure		Case 3 HB live load-VL-		N (t)	S (t)	N (t)	S (t)
		M (tm)	S (t)	M (tm)	S (t)	M (tm)	S (t)				
1-	2	0.000	13.484	-233.700	-78.552	167.319	0.000	-53.261	-10.398	0.000	-10.398
*	1	0.400	13.484	-227.092	-17.264	139.383	0.000	-37.420	-10.398	0.000	-10.398
*	2	1.660	13.484	-206.277	107.743	61.634	0.000	-70.522	-10.398	0.000	-10.398
*	3	3.225	13.484	-180.423	142.453	-13.273	0.000	-85.715	-10.398	0.000	-10.398
*	4	4.790	13.484	-154.569	78.721	-64.177	0.000	-103.069	-10.398	0.000	-10.398
*	5	6.050	13.484	-133.754	-18.607	-87.719	0.000	-116.171	-10.398	0.000	-10.398
2-	1	6.400	13.484	-127.972	-50.005	-91.497	0.000	-119.811	-10.398	0.000	-10.398
2-	3	0.000	127.972	13.484	-50.005	0.000	-91.497	-119.811	85.715	-91.497	85.715
*	1	0.350	118.235	13.484	-50.005	0.000	-91.497	-89.811	85.715	-91.497	85.715
*	2	1.610	83.182	13.484	-50.005	0.000	-91.497	18.190	85.715	-91.497	85.715
*	3	3.105	159.231	13.484	-50.005	0.000	-91.497	145.646	76.857	-91.497	76.857
*	4	4.600	190.320	13.484	-50.005	0.000	-91.497	197.333	0.000	-91.497	0.000
*	5	6.095	159.231	13.484	-50.005	0.000	-91.497	145.646	-76.857	-91.497	-76.857
*	6	7.590	65.963	13.484	-50.005	0.000	-91.497	18.190	-85.715	-91.497	-85.715
*	7	8.850	-60.929	13.484	-50.005	0.000	-91.497	-89.811	-85.715	-91.497	-85.715
3-	2	9.200	-127.972	13.484	-50.005	0.000	-91.497	-119.811	-85.715	-91.497	-85.715
3-	4	0.000	-13.484	-127.972	-50.005	91.497	0.000	-119.811	10.398	0.000	10.398
*	1	0.350	-13.484	-133.754	-18.607	87.719	0.000	-116.171	10.398	0.000	10.398
*	2	1.610	-13.484	-134.569	78.721	64.177	0.000	-103.069	10.398	0.000	10.398
*	3	3.175	-13.484	-180.423	142.453	13.273	0.000	-86.796	10.398	0.000	10.398
*	4	4.740	-13.484	-206.277	107.743	-61.634	0.000	-70.522	10.398	0.000	10.398
*	5	6.000	-13.484	-227.092	-17.264	-139.383	0.000	-57.420	10.398	0.000	10.398
4-	3	6.400	-13.484	-233.700	-78.552	-167.319	0.000	-53.261	10.398	0.000	10.398
4-	1	0.000	233.698	-13.484	-78.552	0.000	-167.319	-53.261	85.716	-167.319	85.716
*	1	0.350	215.917	-13.484	-78.552	0.000	-167.319	-24.401	79.194	-167.319	79.194
*	2	1.810	149.462	-13.484	-78.552	0.000	-167.319	71.363	51.989	-167.319	51.989
*	3	3.205	297.761	-13.484	-78.552	0.000	-167.319	125.756	25.994	-167.319	25.994
*	4	4.600	347.194	0.000	-78.552	0.000	-167.319	143.887	0.000	-167.319	0.000
*	5	5.995	297.761	-70.872	-78.552	0.000	-167.319	125.756	-25.994	-167.319	-25.994
*	6	7.390	149.462	-141.743	-78.552	0.000	-167.319	71.363	-51.989	-167.319	-51.989
*	7	8.850	-111.630	-215.917	-78.552	0.000	-167.319	-24.401	79.195	-167.319	79.195
1-	4	9.200	-233.598	-13.484	-78.552	0.000	-167.319	-53.261	-85.716	-167.319	-85.716

No	Case 4 HB live load-VL-			Case 5 HB live load-HL-			Case 6			
	L(m)	M (tm)	S (t)	N (t)	M (tm)	S (t)	N (t)	M (tm)	S (t)	N (t)
1- 2	0.000	-79.939	0.338	-143.967	-31.276	56.197	0.000	-468.404	279.815	-445.078
* 1	0.400	-79.804	0.338	-143.967	-10.169	49.337	0.000	-365.720	233.720	-435.959
* 2	1.660	-79.379	0.338	-143.967	38.382	27.728	0.000	-154.813	105.433	-407.234
* 3	3.225	-78.850	0.338	-143.967	60.774	0.888	0.000	-91.688	-18.162	-371.555
* 4	4.790	-78.322	0.338	-143.967	41.162	-25.951	0.000	-191.000	-102.154	-335.877
* 5	6.050	-77.897	0.338	-143.967	-5.150	-47.560	0.000	-346.881	-140.998	-307.152
2- 1	6.400	-77.779	0.338	-143.967	-22.847	-53.563	0.000	-397.379	-147.232	-299.173
2- 3	0.000	-77.779	143.967	0.338	-22.847	0.000	-53.563	-397.379	299.173	-147.232
* 1	0.350	-30.890	123.967	0.338	-22.847	0.000	-53.563	-295.020	285.736	-147.232
* 2	1.610	80.294	58.253	0.338	-22.847	0.000	-53.563	34.532	237.363	-147.232
* 3	3.105	118.724	-16.319	0.338	-22.847	0.000	-53.563	345.505	167.301	-147.232
* 4	4.600	78.755	-27.462	0.338	-22.847	0.000	-53.563	462.320	0.000	-147.232
* 5	6.095	37.699	-27.462	0.338	-22.847	0.000	-53.563	345.505	-167.301	-147.232
* 6	7.590	-3.356	-27.462	0.338	-22.847	0.000	-53.563	34.532	-237.363	-147.232
* 7	8.850	-37.958	-27.462	0.338	-22.847	0.000	-53.563	-295.020	-285.736	-147.232
3- 2	9.200	-47.570	-27.462	0.338	-22.847	0.000	-53.563	-397.379	-299.173	-147.232
3- 4	0.000	-47.570	-0.338	-27.462	-22.847	53.563	0.000	-397.379	147.232	-299.173
* 1	0.350	-47.688	-0.338	-27.462	-5.150	47.560	0.000	-346.881	140.998	-307.152
* 2	1.610	-48.113	-0.338	-27.462	41.162	25.951	0.000	-191.000	102.154	-335.877
* 3	3.175	-48.641	-0.338	-27.462	60.774	-0.888	0.000	-91.688	18.162	-371.555
* 4	4.740	-49.170	-0.338	-27.462	38.382	-27.728	0.000	-134.813	-105.433	-407.234
* 5	6.000	-49.595	-0.338	-27.462	-10.169	-49.337	0.000	-363.784	-233.720	-435.959
4- 3	6.400	-49.730	-0.338	-27.462	-31.276	-56.197	0.000	-468.404	-279.815	-445.078
4- 1	0.000	-49.730	27.463	-0.338	-31.276	0.000	-56.197	-468.404	445.078	-279.815
* 1	0.350	-39.119	33.011	-0.338	-31.276	0.000	-56.197	-318.553	411.214	-279.815
* 2	1.810	20.476	45.857	-0.338	-31.276	0.000	-56.197	178.696	269.950	-279.815
* 3	3.205	83.946	42.612	-0.338	-31.276	0.000	-56.197	461.131	134.975	-279.815
* 4	4.600	132.311	24.201	-0.338	-31.276	0.000	-56.197	553.276	0.000	-279.815
* 5	5.995	144.414	-9.376	-0.338	-31.276	0.000	-56.197	461.131	-134.975	-279.815
* 6	7.390	99.099	-58.119	-0.338	-31.276	0.000	-56.197	178.696	-269.950	-279.815
* 7	8.850	-32.832	-125.376	-0.338	-31.276	0.000	-56.197	-318.553	-411.214	-279.815
1- 4	9.200	-79.939	-143.968	-0.338	-31.276	0.000	-56.197	-468.404	-445.078	-279.815

BOX FOR ROAD NO 4'

No	L(m)	Case 7		Case 8		S (t)	N (t)	S (t)	N (t)
		M (tm)	S (t)	M (tm)	S (t)				
1- 2	0.000	-506.555	295.167	-443.847	-528.379	387.409	-322.506		
* 1	0.400	-397.793	249.073	-300.452	-519.260	329.996	-313.387		
* 2	1.660	-167.478	120.786	9.365	-490.535	166.054	-284.662		
* 3	3.225	-80.326	-2.810	132.708	-454.857	-1.827	-248.984		
* 4	4.790	-155.612	-86.801	24.307	-419.179	-130.104	-213.303		
* 5	6.050	-292.148	-125.545	-189.254	-390.454	-204.603	-184.581		
2- 1	6.400	-337.273	-131.879	-263.746	-382.474	-220.741	-176.601		
2- 3	0.000	-337.273	362.474	-263.746	-131.879	176.601	-220.741		
* 1	0.350	-210.763	340.437	-204.287	-131.879	163.164	-220.741		
* 2	1.610	123.342	198.092	-29.176	-131.879	114.791	-220.741		
* 3	3.105	307.006	34.059	99.534	-131.879	57.395	-220.741		
* 4	4.600	292.753	-39.270	142.437	-131.879	0.000	-220.741		
* 5	6.095	191.141	-96.666	99.534	-131.879	-57.395	-220.741		
* 6	7.590	3.722	-154.061	-29.176	-131.879	-114.791	-220.741		
* 7	8.850	-230.870	-202.435	-204.287	-131.879	-163.164	-220.741		
3- 2	9.200	-294.074	-215.872	-263.746	-131.879	-176.601	-220.741		
3- 4	0.000	-294.074	131.879	-263.746	-215.872	220.741	-176.601		
* 1	0.350	-248.949	125.645	-189.254	-223.851	204.603	-184.581		
* 2	1.610	-112.413	86.801	24.307	-252.576	130.104	-213.305		
* 3	3.175	-37.127	2.810	132.708	-288.254	1.827	-248.984		
* 4	4.740	-124.279	-120.786	9.365	-323.932	-166.054	-284.662		
* 5	6.000	-354.594	-249.073	-300.452	-352.657	-329.996	-313.387		
4- 3	6.400	-463.356	-255.167	-443.847	-361.776	-387.409	-322.506		
4- 1	0.000	-463.356	361.777	-443.847	-295.167	322.504	-387.409		
* 1	0.350	-339.600	345.172	-335.264	-295.167	297.965	-387.409		
* 2	1.810	105.928	261.181	25.042	-295.167	195.606	-387.409		
* 3	3.205	401.343	158.738	229.695	-295.167	97.803	-387.409		
* 4	4.600	538.722	34.607	297.912	-295.167	0.000	-387.409		
* 5	5.995	487.812	-111.211	229.695	-295.167	-97.803	-387.409		
* 6	7.390	218.359	-278.716	25.042	-295.167	-195.606	-387.409		
* 7	8.850	-330.609	-477.253	-335.264	-295.167	-297.965	-387.409		
1- 4	9.200	-506.555	-528.378	-443.847	-295.167	-322.504	-387.409		

PICK-UP No. 1 *

M. MAXIMUM

M. MINIMUM

No.	L (m)	Case	M (tm)	S (t)	N (t)	Case	M (tm)	S (t)	N (t)
1 -	0.000	C-8	-443.847	387.409	-322.506	C-7	-506.555	295.167	-528.379
* 1	0.400	C-8	-300.452	329.996	-313.387	C-7	-397.793	249.073	-519.260
* 2	1.660	C-8	9.365	166.054	-284.662	C-7	-167.478	120.786	-490.535
* 3	3.225	C-8	132.708	-1.827	-248.984	C-6	-91.688	-18.162	-371.555
* 4	4.790	C-8	24.307	-130.104	-213.305	C-6	-191.000	-102.154	-335.877
* 5	6.050	C-8	-189.254	-204.603	-184.581	C-6	-346.881	-140.998	-307.152
2 -	6.400	C-8	-263.746	-220.741	-176.601	C-6	-397.379	-147.232	-299.173
2 -	0.000	C-8	-263.746	176.601	-220.741	C-6	-397.379	299.173	-147.232
* 1	0.350	C-8	-204.287	163.164	-220.741	C-6	-295.020	285.736	-147.232
* 2	1.610	C-7	123.342	198.092	-131.879	C-8	-29.176	114.791	-220.741
* 3	3.105	C-6	345.505	167.301	-147.232	C-8	99.534	57.395	-220.741
* 4	4.600	C-6	462.320	0.000	-147.232	C-8	142.437	0.000	-220.741
* 5	6.095	C-6	345.505	-167.301	-147.232	C-8	99.534	-37.395	-220.741
* 6	7.590	C-6	34.532	-237.363	-147.232	C-8	-29.176	-114.791	-220.741
* 7	8.850	C-8	-204.287	-163.104	-220.741	C-6	-295.020	-285.736	-147.232
3 -	9.200	C-8	-263.746	-176.601	-220.741	C-6	-397.379	-299.173	-147.232
3 -	0.000	C-8	-263.746	220.741	-176.601	C-6	-397.379	147.232	-299.173
* 1	0.350	C-8	-189.254	204.603	-184.581	C-6	-346.881	140.998	-307.152
* 2	1.610	C-8	24.307	180.104	-213.305	C-6	-151.000	102.154	-335.877
* 3	3.175	C-8	132.708	1.827	-248.984	C-6	-91.688	18.162	-371.555
* 4	4.740	C-8	9.365	-166.054	-284.662	C-6	-154.813	-105.433	-407.234
* 5	6.000	C-8	-300.452	-329.996	-313.387	C-6	-365.784	-233.720	-435.959
4 -	6.400	C-8	-443.847	-387.409	-322.506	C-6	-468.404	-279.815	-445.078
4 -	0.000	C-8	-443.847	322.504	-387.409	C-6	-468.404	445.078	-279.815
* 1	0.350	C-6	-318.553	411.214	-279.815	C-7	-339.600	345.172	-295.167
* 2	1.810	C-6	178.696	269.950	-279.815	C-8	25.042	195.606	-387.409
* 3	3.205	C-6	461.131	134.975	-279.815	C-8	229.695	97.803	-387.409
* 4	4.600	C-6	555.276	0.000	-279.815	C-8	297.912	0.000	-387.409
* 5	5.995	C-7	487.812	-111.211	-295.167	C-8	225.695	-97.803	-387.409
* 6	7.390	C-7	218.359	-278.716	-295.167	C-8	25.042	-195.606	-387.409
* 7	8.850	C-6	-318.553	-411.214	-279.815	C-8	-335.264	-297.565	-387.409
1 -	9.200	C-8	-443.847	-322.504	-387.409	C-7	-506.555	-528.378	-295.167

BOX FOR ROAD NO 4.

PICK-UP No. 1 *

No.	L (m)	Case	S . M A X I M U M			S . M I N I M U M		
			M (tm)	S (t)	N (t)	M (tm)	S (t)	N (t)
1 -	0.000	C- 8	-443.847	387.409	-322.506	-468.404	279.815	-445.078
* 1	0.400	C- 8	-300.452	329.996	-313.387	-365.784	233.720	-435.959
* 2	1.660	C- 8	9.365	166.054	-284.662	-154.813	105.433	-407.234
* 3	3.225	C- 8	132.708	-1.827	-248.984	-91.688	-18.162	-371.555
* 4	4.790	C- 7	-155.612	-86.801	-419.179	24.307	-130.104	-213.305
* 5	6.050	C- 7	-292.148	-125.645	-390.454	-189.254	-204.603	-184.581
2 -	6.400	C- 7	-337.273	-131.879	-382.474	-263.746	-220.741	-176.601
2 -	0.000	C- 7	-337.273	382.474	-131.879	-263.746	176.601	-220.741
* 1	0.350	C- 7	-210.763	340.437	-131.879	-204.287	163.164	-220.741
* 2	1.610	C- 6	34.532	237.363	-147.232	-29.176	114.791	-220.741
* 3	3.105	C- 6	345.505	167.301	-147.232	307.006	34.059	-131.879
* 4	4.600	C- 6	462.320	0.000	-147.232	292.753	-89.270	-131.879
* 5	6.095	C- 8	99.534	-57.395	-220.741	345.505	-167.301	-147.232
* 6	7.590	C- 8	-29.176	-114.791	-220.741	34.532	-237.363	-147.232
* 7	8.850	C- 8	-204.287	-163.164	-220.741	-295.020	-285.736	-147.232
3 -	9.200	C- 8	-263.746	-176.601	-220.741	-397.379	-299.173	-147.232
3 -	0.000	C- 8	-263.746	220.741	-176.601	-294.074	131.879	-215.872
* 1	0.350	C- 8	-189.254	204.603	-184.581	-248.949	125.645	-223.851
* 2	1.610	C- 8	24.307	130.104	-213.305	-112.413	86.801	-252.576
* 3	3.175	C- 6	-91.688	18.162	-371.555	132.708	1.827	-248.984
* 4	4.740	C- 6	-154.813	-105.433	-407.234	9.365	-166.054	-284.662
* 5	6.000	C- 6	-365.784	-233.720	-435.959	-300.452	-329.996	-313.387
4 -	6.400	C- 6	-468.404	-279.815	-445.078	-443.847	-387.409	-322.506
4 -	0.000	C- 6	-468.404	445.078	-279.815	-443.847	322.504	-387.409
* 1	0.350	C- 6	-318.553	411.214	-279.815	-335.264	297.965	-387.409
* 2	1.810	C- 6	178.696	269.950	-279.815	25.042	195.606	-387.409
* 3	3.205	C- 7	401.343	158.738	-295.167	229.693	97.803	-387.409
* 4	4.600	C- 7	538.722	34.607	-295.167	555.276	0.000	-279.815
* 5	5.995	C- 8	229.693	-97.803	-387.409	461.131	-134.975	-279.815
* 6	7.590	C- 8	25.042	-195.606	-387.409	218.359	-278.716	-295.167
* 7	8.850	C- 8	-335.264	-297.965	-387.409	-330.609	-477.253	-295.167
1 -	9.200	C- 8	-443.847	-322.504	-387.409	-506.555	-528.378	-295.167

BOX FOR ROAD NO 4

PICK-UP No. 1 *

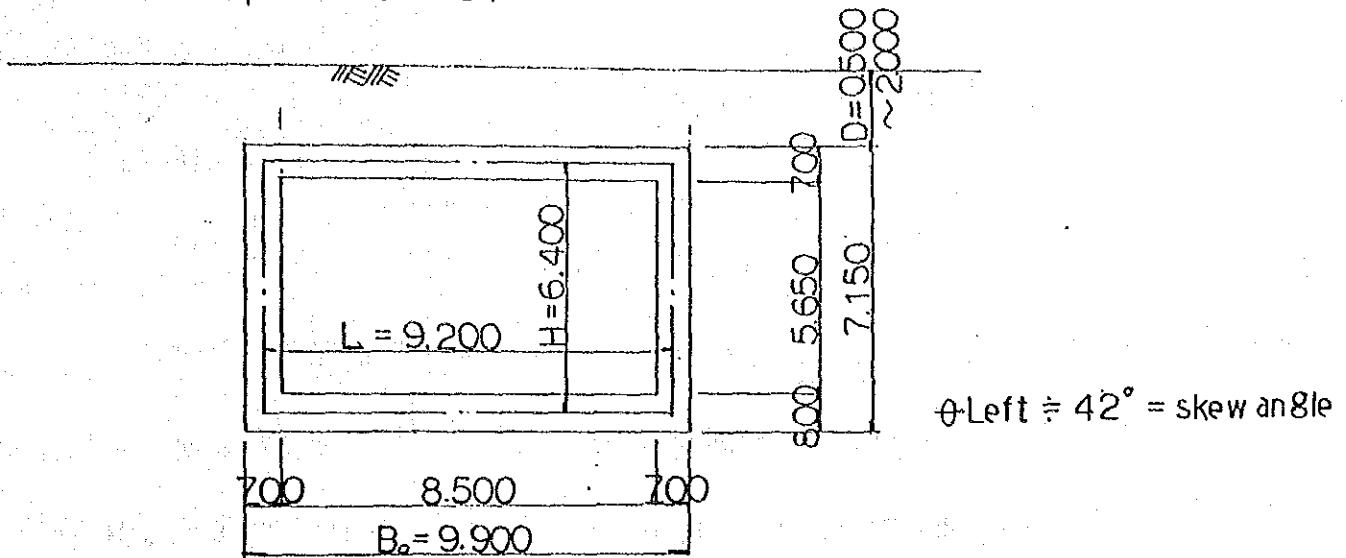
N. MAXIMUM

N. MINIMUM

No.	L (m)	Case	M (tm)	S (t)	N (t)	Case	M (tm)	S (t)	N (t)
1 -	0.000	C- 8	-443.847	387.409	-322.506	C- 7	-506.555	295.167	-528.379
* 1	0.460	C- 8	-300.452	329.996	-313.387	C- 7	-397.793	249.073	-319.260
* 2	1.560	C- 8	9.365	166.054	-284.662	C- 7	-167.478	120.786	-490.535
* 3	3.225	C- 8	132.708	-1.827	-248.984	C- 7	-80.526	-2.810	-454.857
* 4	4.790	C- 8	24.307	-130.104	-213.305	C- 7	-155.612	-86.801	-419.179
* 5	6.050	C- 8	-189.254	-204.603	-184.581	C- 7	-292.148	-126.645	-390.454
2 -	6.400	C- 8	-263.746	-220.741	-176.601	C- 7	-337.273	-131.879	-382.474
2 -	0.000	C- 7	-337.273	382.474	-131.879	C- 8	-263.746	176.601	-220.741
* 1	0.350	C- 7	-210.763	340.437	-131.879	C- 8	-204.287	163.164	-220.741
* 2	1.610	C- 7	123.342	198.092	-131.879	C- 8	-29.176	114.791	-220.741
* 3	3.105	C- 7	307.006	34.059	-131.879	C- 8	99.534	57.395	-220.741
* 4	4.600	C- 7	292.753	-39.270	-131.879	C- 8	142.437	0.000	-220.741
* 5	6.095	C- 7	191.141	-96.666	-131.879	C- 8	99.534	-57.395	-220.741
* 6	7.590	C- 7	3.722	-154.061	-131.879	C- 8	-29.176	-114.791	-220.741
* 7	8.850	C- 7	-220.870	-202.435	-131.879	C- 8	-204.287	-163.164	-220.741
3 -	9.200	C- 7	-294.074	-215.872	-131.879	C- 8	-263.746	-176.601	-220.741
3 -	0.000	C- 8	-263.746	220.741	-176.601	C- 6	-397.379	147.232	-299.173
* 1	0.350	C- 8	-189.254	204.603	-184.581	C- 6	-346.881	140.998	-307.152
* 2	1.610	C- 8	24.307	130.104	-213.305	C- 6	-191.000	102.154	-335.877
* 3	3.175	C- 8	132.708	1.827	-248.984	C- 6	-91.688	18.162	-371.555
* 4	4.740	C- 8	9.365	-166.054	-284.662	C- 6	-154.813	-105.433	-407.234
* 5	6.000	C- 8	-300.452	-329.996	-313.387	C- 6	-365.764	-233.720	-435.959
4 -	6.400	C- 8	-443.847	-387.409	-322.506	C- 6	-468.404	-279.815	-445.078
4 -	0.000	C- 6	-468.404	445.078	-279.815	C- 8	-443.847	322.504	-387.409
* 1	0.350	C- 6	-318.553	411.214	-279.815	C- 8	-335.264	297.965	-387.409
* 2	1.810	C- 6	178.696	269.950	-279.815	C- 8	25.042	195.606	-387.409
* 3	3.205	C- 6	461.131	134.975	-279.815	C- 8	229.695	97.803	-387.409
* 4	4.600	C- 6	555.276	0.000	-279.815	C- 8	297.912	0.000	-387.409
* 5	5.995	C- 6	461.131	-134.975	-279.815	C- 8	229.695	-97.803	-387.409
* 6	7.390	C- 6	178.696	-269.950	-279.815	C- 8	25.042	-195.606	-387.409
* 7	8.850	C- 6	-318.553	-411.214	-279.815	C- 8	-335.264	-297.965	-387.409
1 -	9.200	C- 6	-468.404	-445.078	-279.815	C- 8	-443.847	-322.504	-387.409

NO ⑦ BOX CULVERT FOR RORD

1) Shape and Size



Where

D^m = depth of asphalt and similar surface soil.

2) Factor of section

$$A = 1.00 \times 0.70 = 0.7000 \text{ m}^2$$

$$I = \frac{1.00 \times 0.70^3}{12} = 0.02858 \text{ m}^2$$

$$A = 1.00 \times 0.80 = 0.8000 \text{ m}^2$$

$$I = \frac{1.00 \times 0.80^3}{12} = 0.04267 \text{ m}^2$$

$$A = \quad =$$

$$I = \quad =$$

$$E_c = 25 \text{ KN/mm}^2 = 25 \times 10^7 \text{ KN/m}^2$$

No. ⑦ BOX CULVERT FOR ROAD

1. calculation for bending moment (U.L.S)

1) For upper slab

section $b=100\text{cm}$ $h=70$ $d=64.0$ $d'=6.0$

a) middle point ②~③ $M_{u,max}=631.9\text{KNm}$

$$A_s = \left(\begin{array}{l} Y_{32}-300\text{c}^{\text{t}^{\text{c}}} = 8.042/0.300 \\ Y_{25}-300\text{c}^{\text{t}^{\text{c}}} = 4.909/0.300 \end{array} \right) = 43.17\text{ cm}^2$$

$$X = \frac{0.87 \times 41000 \times 43.17}{0.40 \times 2500 \times 100} = 15.4\text{cm}$$

$$Z = 64.0 - \frac{15.4}{2} = 56.3\text{cm} < 0.95 \times 64.0 = 60.8\text{cm}$$

$$M_{RS} = 0.87 \times 41000 \times 43.17 \times 56.3 \times 10^{-5} = 867.0\text{KNm} > M_u = 631.9\text{KNm}$$

$$M_{RC} = 0.40 \times 2500 \times 100 \times 15.4 \times 56.3 \times 10^{-5} = 867.0\text{KNm} > M_u = 631.9\text{KNm}$$

OK

b) intersection point ②=③ $M_{u,min} = -580.7\text{KNm}$

$$A_s = Y_{25}-150\text{c}^{\text{t}^{\text{c}}} = 4.909/0.150 = 32.73\text{ cm}^2$$

$$X = \frac{0.87 \times 41000 \times 32.73}{0.40 \times 2500 \times 100} = 11.8\text{cm}$$

$$Z = 64.0 - \frac{11.8}{2} = 58.1\text{cm} < 0.95 \times 64.0 = 60.8\text{cm} \quad \text{OK}$$

$$M_{RS} = 0.87 \times 41000 \times 32.73 \times 58.1 \times 10^{-5} = 678.3\text{KNm} > M_u = 580.7\text{KNm}$$

$$M_{RC} = 0.40 \times 2500 \times 100 \times 11.8 \times 58.1 \times 10^{-5} = 685.5\text{KNm} > M_u = 580.7\text{KNm}$$

OK

2) For bottom slab

section $b=100\text{cm}$ $h=80$ $d=73.0(74.0)$ $d'=7.0(6.0)$

a) middle point ④~① $M_{u,max} = 802.1\text{KNm}$

$$A_s = \left(\begin{array}{l} Y_{32}-300\text{c}^{\text{t}^{\text{c}}} = 8.042/0.300 \\ Y_{25}-300\text{c}^{\text{t}^{\text{c}}} = 4.909/0.300 \end{array} \right) = 43.17\text{ cm}^2$$

$$X = \frac{0.87 \times 41000 \times 43.17}{0.40 \times 2500 \times 100} = 15.4\text{cm}$$

$$Z = 73.0 - \frac{15.4}{2} = 65.3\text{cm} < 0.95 \times 73.0 = 69.3\text{cm} \quad \text{OK}$$

$$M_{RS} = 0.87 \times 41000 \times 43.17 \times 65.3 \times 10^{-5} = 1005.5\text{KNm} > M_u = 802.1\text{KNm}$$

$$M_{RC} = 0.40 \times 2500 \times 100 \times 15.4 \times 65.3 \times 10^{-5} = 1005.6\text{KNm} > M_u = 802.1\text{KNm}$$

OK

b) intersection point ④=① $Mu.min = -660.4^{KNm}$

$$A_s = Y_{25} - 150^{ctc} = 4.909 / 0.15 = 32.73 \text{ cm}^2$$

$$X = \frac{0.87 \times 41000 \times 32.73}{0.40 \times 2500 \times 100} = 11.6 \text{ cm}$$

$$Z = 73.0 - \frac{11.6}{2} = 67.2 \text{ cm} < 0.95 \times 73.0 = 69.3 \text{ cm} \quad \text{OK}$$

$$M_{RS} = 0.87 \times 41000 \times 32.73 \times 67.2 \times 10^{-5} = 784.5^{KNm} > Mu = 660.4^{Nm}$$

$$M_{RC} = 0.40 \times 2500 \times 100 \times 11.6 \times 67.2 \times 10^{-5} = 793.0^{KNm} > Mu = 660.4^{Nm}$$

Notice: this bar is decide for shearing force
without bending moments.

2. calculation for shearing force (U.L.S)

a) For upper slab

$$\text{section } b = 100 \text{ cm} \quad h = 70 \quad d = 64.0 \quad d' = 6.0$$

intersection point ②=③ $Su.max = 343.4^{KN}$

$$A_s = \left(\begin{array}{l} Y_{32} - 300^{ctc} = 8.042 / 0.30 \\ Y_{25} - 300^{ctc} = 4.909 / 0.30 \end{array} \right) = 43.17 \text{ cm}^2$$

$$P = \frac{43.17}{100 \times 64.0} \times 100 = 0.675 \%$$

$$V_c = \frac{343.4 \times 10^3}{100 \times 64.0} = 53.7 \text{ N/cm}^2$$

$$< V_{ca} = 50.0 + 15.0 \frac{(0.675 - 0.50)}{0.50} = 55.2 \text{ N/cm}^2 \quad \text{OK}$$

b) For bottom slab

$$\text{section } b = 100 \quad h = 80 \quad d = 73.0 \quad d' = 7.0$$

intersection point ④=① $Su.min = -386.2^{KN}$

$$A_s = \left(\begin{array}{l} Y_{32} - 300^{ctc} = 8.042 / 0.30 \\ Y_{25} - 300^{ctc} = 4.909 / 0.30 \end{array} \right) = 43.17 \text{ cm}^2$$

$$P = \frac{43.17}{100 \times 73.0} \times 100 = 0.592 \%$$

$$V_c = \frac{386.2 \times 10^3}{100 \times 73.0} = 52.8 \text{ N/cm}^2$$

$$< V_{ca} = 50.0 + 15.0 \frac{(0.592 - 0.50)}{0.50} = 52.8 \text{ N/cm}^2 \quad \text{OK}$$

Notice: this bar is decide for shearing force
about point ②, ③ and ④, ①

NO. 1 BOX CULVERT FOR ROAD

D = 2.000 m

(1) Dead load

a) vertical load ----- (case-1)

For upper slab $w_1 = 22.6 \times 0.50 + 19.6 \times 1.50 + 23.6 \times 0.70 = 57.220 \text{ kN/m}$

For side wall $w_2 = 23.6 \times 0.70 = 16.520 \text{ ''}$

For bottom slab $w_3 = 57.220 + \frac{2 \times 16.52 \times 6.40}{9.20} = 80.204 \text{ ''}$

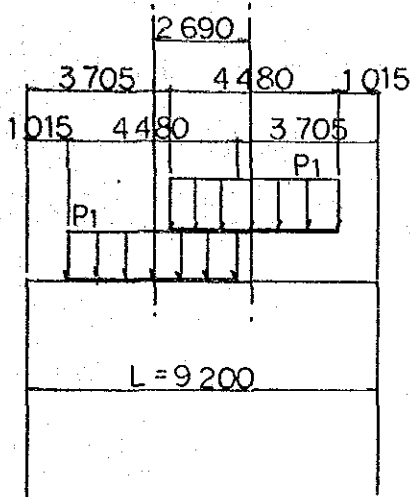
b) Horizontal load --- earth pressure ----- (case-2)

For side wall $P_1 = (22.6 \times 0.50 + 19.60 \times 1.85) \times 0.500 = 23.780 \text{ kN/m}$

$P_2 = (22.6 \times 0.50 + 19.60 \times 8.25) \times 0.500 = 86.500 \text{ ''}$

(2) Live load

a) Vertical load of center ----- (case-3)



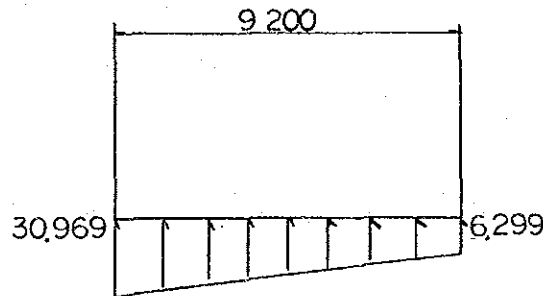
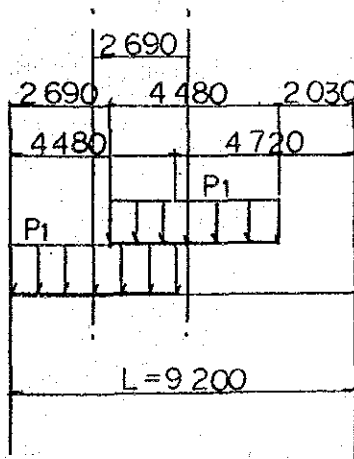
$$B = (0.30 + 2.0 + 0.70) \operatorname{cosec} 42^\circ = 4.480 \text{ m}$$

$$P_1 = \frac{10 \times 30}{3.50 \times B} = \frac{10 \times 30}{3.50 \times 4.48} = 19.133 \text{ KN/m}$$

For bottom slab

$$P_2 = \frac{2 \times 19.133 \times 4.480}{9.20} = 18.634 \text{ KN/m}$$

b) Vertical load of partial ----- (case-4)



For bottom slab

$$P_2 = \frac{2 \times 19.133 \times 4.480}{9.20} \pm \frac{6 \times 19.133 \times 4.480 (2.360 - 0.330)}{9.20^2}$$

$$= 18.634 \pm 12.335 = \begin{cases} P_2-1 = 30.969 \text{ KN/m} \\ P_2-2 = 6.299 \text{ KN/m} \end{cases}$$

C) Horizontal load of live load surcharge ----- (case-5)

$$P_e = g_o k_o = 34.300 \times 0.500 = 17.150 \text{ KN/m}$$

BOX FOR ROAD NO. 7 Depth = 2.000

No	X (m)	Y (m)
1	0.0000	0.0000
2	0.0000	6.4000
3	9.2000	6.4000
4	9.2000	0.0000

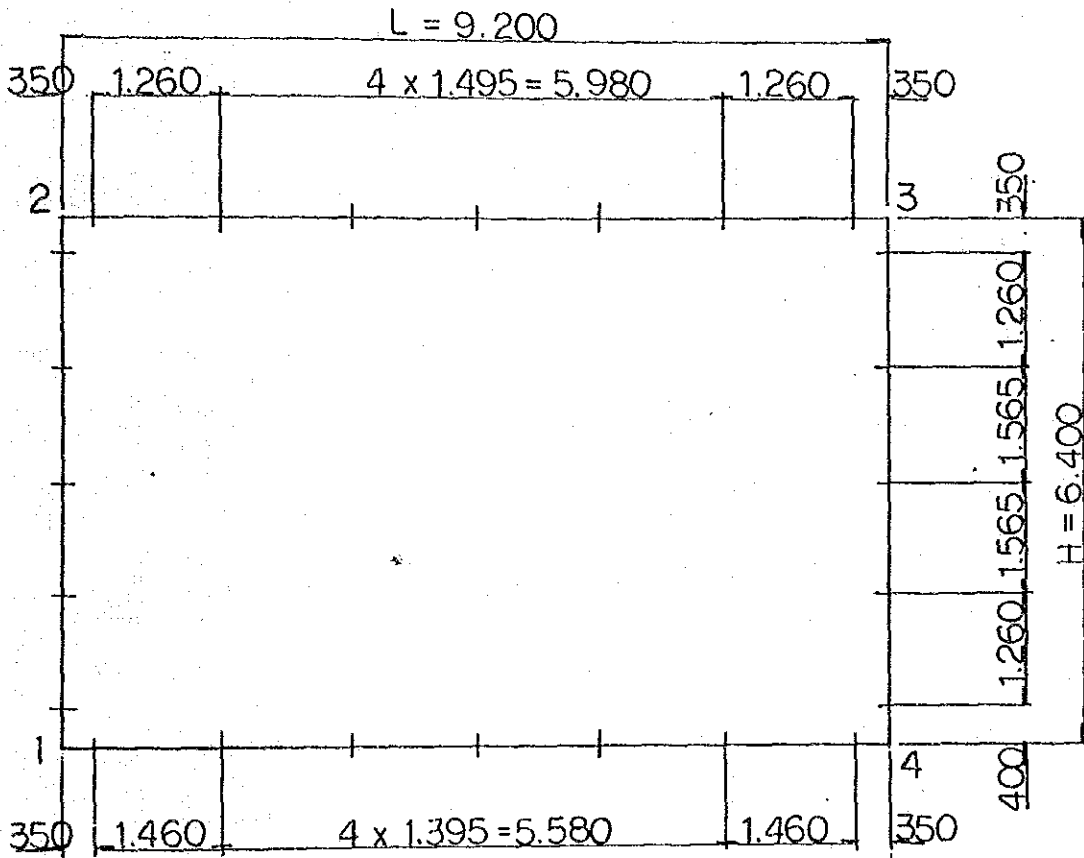
NOTE: THE DIMENSION(K)EE EXCHANG TO
DIMENSION(KN)INTO THIS CALCULATION

No	I	J	A (m ²)	i (m±)	I - J	L (m)	E (t/m ²)	EPS
1	1	2	0.70000	0.028580	Fix - Fix	6.400	2.50E+07	1.00E-05
2	2	3	0.70000	0.028580	Fix - Fix	9.200	2.50E+07	1.00E-05
3	3	4	0.70000	0.028580	Fix - Fix	6.400	2.50E+07	1.00E-05
4	4	1	0.80000	0.042670	Fix - Fix	9.200	2.50E+07	1.00E-05

	X (t/m)	Y (t/m)	M (tm/Rad)
1	Fix	Fix	Free
4	Free	Fix	Free

No	L-No	L-No	L-No	L-No	L-No	L-No	L-No	L-No	L-No
1	11	12	13	14	15	16	17	18	19
2	1	2	3	4	5	6	7	8	9
3	5	6	7	8	9	10	11	12	13
4	13	14	15	16	17	18	19	20	21

CALCULATION POINTS OF EACH FORCE



: Dead load
No. : 1

No	i - j	Li (m)	Lo (m)	Pi (t/m)	Pj (t/m)
1	1- 2	0.000	6.400	-16.520	-16.520
3	3- 4	0.000	6.400	-16.520	-16.520
2	2- 3	0.000	9.200	-57.220	-57.220
4	4- 1	0.000	9.200	80.204	80.204

$\Sigma V = -0.003 (t)$
 $\Sigma H = 0.000 (t)$

: Earth pressure
No. : 2

No	i - j	Li (m)	Lo (m)	Pi (t/m)	Pj (t/m)
1	1- 2	0.000	6.400	86.500	23.780
3	3- 4	0.000	6.400	-23.780	-86.500

$\Sigma V = 0.000 (t)$
 $\Sigma H = 0.000 (t)$

: HB live load-VL-
: 3

No	i - j	Li (m)	Lo (m)	Pi (t/m)	Pj (t/m)
2	2- 3	1.015	4.480	-19.133	-19.133
2	2- 3	3.705	4.480	-19.133	-19.133
4	4- 1	0.000	9.200	18.634	18.634

: HB live load-VL-
No. : 4

No	i - j	Li (m)	Lo (m)	Pi (t/m)	Pj (t/m)
2	2- 3	0.000	4.480	-19.133	-19.133
2	2- 3	2.590	4.480	-19.133	-19.133
4	4- 1	0.000	9.200	6.299	30.969

Σ V = 0.001 (t)
Σ H = 0.000 (t)

: HB live load-HL-
No. : 5

No	i - j	Li (m)	Lo (m)	Pi (t/m)	Pj (t/m)
1	1- 2	0.000	6.400	17.150	17.150
3	3- 4	0.000	6.400	-17.150	-17.150

Σ V = 0.000 (t)
Σ H = 0.000 (t)

No	C-No 1	C-No 2	C-No 3
No	No 6	No 7	No 8
No 1	1.3800	1.3800	1.3800
No 2	1.6500	1.6500	1.6500
No 3	1.4300	0.0000	0.0000
No 4	0.0000	1.4300	0.0000
No 5	0.0000	0.0000	1.6500

No 1 : 6 7 8

No.	Case. 1		Case. 2		Case. 3	
	RX (t)	RY (t)	RM (tm)	RY (t)	RX (t)	RY (t)
1.	0.000	0.002	0.000	0.000	0.000	0.000
4.	0.000	0.002	0.000	0.000	0.000	0.000

No.	Case. 4		Case. 5		Case. 6	
	RX (t)	RY (t)	RM (tm)	RY (t)	RX (t)	RY (t)
1.	0.000	-0.001	0.000	0.000	0.000	0.000
4.	0.000	0.000	0.000	0.000	0.000	0.000

No.	Case. 7		Case. 8	
	RX (t)	RY (t)	RM (tm)	RY (t)
1.	0.000	0.001	0.000	0.002
4.	0.000	0.002	0.000	0.002

No.	Case. 1			Case. 2			Case. 3		
	X-DIS. (mm)	Y-DIS. (mm)	ROTA. (mmRad)	X-DIS. (mm)	Y-DIS. (mm)	ROTA. (mmRad)	X-DIS. (mm)	Y-DIS. (mm)	ROTA. (mmRad)
1.	0.00000	0.00000	12.01597	0.00000	0.00000	-4.54327	0.00000	0.00000	3.2284
2.	-0.04589	-1.15594	-11.15536	-0.13444	0.00000	4.48011	0.03615	-0.31348	-3.9405
3.	0.00291	-1.15594	11.15536	-0.85681	0.00000	-4.48011	-0.00241	-0.31348	3.9405
4.	-0.04078	0.00000	-12.01597	-0.99124	0.00000	4.54327	0.03374	0.00000	-3.2284

No.	Case. 4			Case. 5			Case. 6		
	X-DIS. (mm)	Y-DIS. (mm)	ROTA. (mmRad)	X-DIS. (mm)	Y-DIS. (mm)	ROTA. (mmRad)	X-DIS. (mm)	Y-DIS. (mm)	ROTA. (mmRad)
1.	0.00000	0.00000	3.34363	0.00000	0.00000	-1.34866	0.00000	0.00000	13.7023
2.	0.42620	-0.38684	-4.05612	0.01154	0.00000	1.47088	-0.23042	-2.01346	-13.6371
3.	0.39432	-0.24011	3.45983	-0.27005	0.00000	-1.47088	-1.41316	-2.01346	13.6371
4.	0.02789	0.00000	-2.99503	-0.25851	0.00000	1.34866	-1.64358	0.00000	-13.7023

No.	Case. 7			Case. 8		
	X-DIS. (mm)	Y-DIS. (mm)	ROTA. (mmRad)	X-DIS. (mm)	Y-DIS. (mm)	ROTA. (mmRad)
1.	0.00000	0.00000	13.86702	0.00000	0.00000	6.86036
2.	0.32735	-2.14837	-13.80248	-0.26307	-1.59519	-5.57526
3.	-0.84585	-1.93855	12.94978	-1.85529	-1.59519	5.57526
4.	-1.65194	0.00000	-13.36853	-2.11836	0.00000	-6.86036

I-	No	L(m)	Case 1 Dead load		Case 2 Earth pressure		Case 3 HB live load-VL-		N (t)	M (tm)	S (t)	X (t)
			M (tm)	S (t)	N (t)	M (tm)	S (t)	M (tm)				
1-	2	0.000	-287.053	8.864	-368.940	-105.359	215.488	-56.564	0.000	-7.334	-85.716	
*	1	0.350	-288.507	8.864	-362.332	-25.980	181.672	-59.498	0.000	-7.334	-85.716	
*	2	1.660	-272.338	8.864	-341.517	140.642	85.400	-68.739	0.000	-7.334	-85.716	
*	3	3.225	-258.465	8.864	-315.663	194.548	-12.511	-80.217	0.000	-7.334	-85.716	
*	4	4.790	-244.592	8.864	-289.809	114.003	-86.421	-91.695	0.000	-7.334	-85.716	
*	5	6.050	-233.422	8.864	-268.994	-23.022	-128.485	-100.936	0.000	-7.334	-85.716	
2-	1	6.400	-230.320	8.864	-263.212	-69.588	-137.408	-103.503	0.000	-7.334	-85.716	
2-	3	0.000	-230.320	263.212	8.864	-69.588	0.000	-103.503	-137.408	85.716	-7.334	
*	1	0.350	-141.700	243.185	8.864	-69.588	0.000	-73.503	-137.408	85.716	-7.334	
*	2	1.610	119.291	171.088	8.864	-69.588	0.000	31.112	-137.408	74.532	-7.334	
*	3	3.105	311.124	85.544	8.864	-69.588	0.000	120.857	-137.408	45.728	-7.334	
*	4	4.600	375.068	0.000	8.864	-69.588	0.000	160.170	-137.408	0.000	-7.334	
*	5	6.095	311.124	-85.544	8.864	-69.588	0.000	120.857	-137.408	-45.728	-7.334	
*	6	7.590	119.291	-171.088	8.864	-69.588	0.000	31.112	-137.408	-74.532	-7.334	
*	7	8.850	-141.700	-243.185	8.864	-69.588	0.000	-73.503	-137.408	-85.716	-7.334	
3-	2	9.200	-230.320	-263.212	8.864	-69.588	0.000	-103.503	-137.408	-85.716	-7.334	
3-	4	0.000	-230.320	-8.864	-263.212	-69.588	137.408	-103.503	0.000	7.334	-85.716	
*	1	0.350	-233.422	-8.864	-268.994	-23.022	128.485	-100.936	0.000	7.334	-85.716	
*	2	1.610	-244.592	-8.864	-289.809	114.003	86.421	-91.695	0.000	7.334	-85.716	
*	3	3.175	-258.465	-8.864	-315.663	194.548	12.511	-80.217	0.000	7.334	-85.716	
*	4	4.740	-272.338	-8.864	-341.517	140.642	-85.400	-68.739	0.000	7.334	-85.716	
*	5	6.000	-283.507	-8.864	-362.332	-25.980	-181.672	-59.498	0.000	7.334	-85.716	
4-	3	6.400	-287.053	-8.864	-368.940	-105.359	-215.488	-56.564	0.000	7.334	-85.716	
4-	1	0.000	-287.053	368.938	-8.864	-105.359	0.000	-56.564	-215.488	85.716	7.334	
*	1	0.350	-162.837	340.867	-8.864	-105.359	0.000	-27.705	-215.488	79.194	7.334	
*	2	1.810	249.348	223.769	-8.864	-105.359	0.000	68.059	-215.488	51.989	7.334	
*	3	3.205	483.466	111.885	-8.864	-105.359	0.000	122.452	-215.488	23.994	7.334	
*	4	4.600	561.506	0.000	-8.864	-105.359	0.000	140.584	-215.488	0.000	7.334	
*	5	5.995	483.466	-111.885	-8.864	-105.359	0.000	122.452	-215.488	-23.994	7.334	
*	6	7.390	249.348	-223.769	-8.864	-105.359	0.000	68.059	-215.488	-51.989	7.334	
*	7	8.850	-162.837	-340.867	-8.864	-105.359	0.000	-27.705	-215.488	-79.194	7.334	
1-	4	9.200	-287.053	-368.938	-8.864	-105.359	0.000	-56.564	-215.488	-83.716	7.334	

No	L (m)	Case 4 HB live load-VL-			Case 5 HB live load-HL-			Case 6		
		M (tm)	S (t)	N (t)	M (tm)	S (t)	N (t)	M (tm)	S (t)	N (t)
1- 2	0.000	-63.209	-6.063	-105.776	-31.276	56.197	0.000	-650.862	357.300	-631.711
* 1	0.400	-65.634	-6.063	-105.776	-10.169	49.337	0.000	-519.188	301.504	-622.592
* 2	1.660	-73.274	-6.063	-105.776	38.382	27.728	0.000	-242.063	142.656	-593.867
* 3	3.225	-82.763	-6.063	-105.776	60.774	0.888	0.000	-150.388	-18.899	-558.189
* 4	4.790	-92.252	-6.063	-105.776	41.162	-25.951	0.000	-280.556	-140.849	-522.510
* 5	6.050	-99.892	-6.063	-105.776	-5.150	-47.560	0.000	-504.447	-210.255	-493.785
2- 1	6.400	-102.014	-6.063	-105.776	-22.847	-53.563	0.000	-580.671	-224.978	-485.806
2- 3	0.000	-102.014	105.776	-6.063	-22.847	0.000	-53.563	-580.671	485.806	-224.978
* 1	0.350	-66.164	99.079	-6.063	-22.847	0.000	-53.563	-415.475	458.169	-224.978
* 2	1.610	43.488	74.972	-6.063	-22.847	0.000	-53.563	94.293	342.396	-224.978
* 3	3.105	132.542	38.428	-6.063	-22.847	0.000	-53.563	487.356	183.441	-224.978
* 4	4.600	147.366	-16.484	-6.063	-22.847	0.000	-53.563	631.825	0.000	-224.978
* 5	6.095	101.341	-45.088	-6.063	-22.847	0.000	-53.563	487.356	-183.441	-224.978
* 6	7.590	14.241	-65.656	-6.063	-22.847	0.000	-53.563	94.293	-342.396	-224.978
* 7	8.850	-68.485	-55.656	-6.063	-22.847	0.000	-53.563	-415.475	-458.169	-224.978
3- 2	9.200	-91.465	-65.656	-6.063	-22.847	0.000	-53.563	-580.671	-485.806	-224.978
3- 4	0.000	-91.465	6.063	-65.656	-22.847	53.563	0.000	-580.671	224.978	-485.806
* 1	0.350	-89.343	6.063	-65.656	-3.150	47.560	0.000	-504.447	210.255	-493.785
* 2	1.610	-81.703	6.063	-65.656	41.162	25.951	0.000	-280.556	140.849	-522.510
* 3	3.175	-72.214	6.063	-65.656	60.774	-0.888	0.000	-150.388	18.899	-558.189
* 4	4.740	-62.725	6.063	-65.656	38.382	-27.728	0.000	-242.063	-142.656	-593.867
* 5	6.000	-55.085	6.063	-65.656	-10.169	-49.337	0.000	-519.188	-301.504	-622.592
4- 3	6.400	-52.660	6.063	-65.656	-31.276	-56.197	0.000	-650.862	-357.300	-631.711
4- 1	0.000	-52.660	65.656	6.063	-31.276	0.000	-56.197	-650.862	631.709	-357.300
* 1	0.350	-50.085	63.287	6.063	-31.276	0.000	-56.197	-438.170	583.645	-357.300
* 2	1.810	53.209	49.862	6.063	-31.276	0.000	-56.197	267.561	383.146	-357.300
* 3	3.205	110.703	31.095	6.063	-31.276	0.000	-56.197	668.447	191.573	-357.300
* 4	4.600	139.213	8.310	6.063	-31.276	0.000	-56.197	802.069	0.000	-357.300
* 5	5.995	131.462	-20.293	6.063	-31.276	0.000	-56.197	668.447	-191.573	-357.300
* 6	7.390	80.168	-54.115	6.063	-31.276	0.000	-56.197	267.561	-383.146	-357.300
* 7	8.850	-28.005	-55.102	6.063	-31.276	0.000	-56.197	-438.176	-583.645	-357.300
1- 4	9.200	-63.209	-105.777	6.063	-31.276	0.000	-56.197	-650.862	-631.709	-357.300

Case 7			Case 8				
No	L(m)	M (tm)	S (t)	N (t)	M (tm)	S (t)	N (t)
1-	2	0.000	-660.364	359.118	-660.397	-621.580	460.513
*	1	0.400	-527.963	303.321	-651.278	-450.884	393.398
*	2	1.660	-248.548	144.473	-586.874	64.600	198.895
*	3	3.225	-154.029	-17.081	-551.196	-81.514	-6.945
*	4	4.790	-281.352	-139.032	-522.471	-368.606	-173.181
*	5	6.050	-502.953	-208.437	-514.492	-470.358	-278.242
2-	1	6.400	-578.541	-223.161	-223.161	-470.358	-302.869
2-	3	0.000	-578.541	514.492	-223.161	-348.063	363.233
*	1	0.350	-404.981	477.279	-223.161	12.105	335.595
*	2	1.610	111.990	343.311	-223.161	276.834	236.101
*	3	3.105	504.066	173.002	-223.161	365.077	118.051
*	4	4.600	613.507	-23.572	-223.161	276.834	0.000
*	5	6.095	459.449	-182.526	-223.161	12.105	-118.051
*	6	7.590	70.167	-329.989	-223.161	-348.063	-236.101
*	7	8.850	-408.300	-429.483	-223.161	-470.358	-335.595
3-	2	9.200	-563.456	-457.120	-223.161	-470.358	-363.233
3-	4	0.000	-563.456	223.161	-457.120	-470.358	302.869
*	1	0.350	-487.868	208.437	-485.100	-368.606	278.242
*	2	1.610	-266.267	139.032	-493.825	-81.514	173.181
*	3	3.175	-138.944	17.081	-529.503	64.600	6.945
*	4	4.740	-233.463	-144.473	-565.181	-80.436	-198.895
*	5	6.000	-512.878	-303.321	-593.906	-450.884	-393.398
4-	3	6.400	-645.280	-359.118	-603.025	-621.580	-460.513
4-	1	0.000	-645.280	603.023	-359.118	-621.580	509.135
*	1	0.350	-441.580	560.897	-359.118	-450.162	470.396
*	2	1.810	246.346	380.105	-359.118	118.652	308.801
*	3	3.205	651.645	199.725	-359.118	441.735	154.401
*	4	4.600	800.110	11.984	-359.118	549.430	0.000
*	5	5.995	681.330	-183.420	-359.118	441.735	-154.401
*	6	7.390	284.897	-386.186	-359.118	118.652	-308.801
*	7	8.850	-438.690	-606.392	-359.118	-450.162	-470.396
1-	4	9.200	-660.364	-660.396	-359.118	-621.580	-509.135

M. MAXIMUM

M. MINIMUM

No.	L (cm)	Case	M (tm)	S (t)	N (t)	Case	M (tm)	S (t)	N (t)
1 - 2	0.000	C- 8	-621.580	460.513	-509.137	C- 7	-650.364	359.118	-600.397
* 1	0.400	C- 8	-450.884	393.398	-500.018	C- 7	-527.963	303.321	-651.278
* 2	1.660	C- 8	-80.436	198.895	-471.293	C- 7	-248.548	144.473	-622.553
* 3	3.225	C- 8	64.600	-6.945	-435.615	C- 7	-154.029	-17.081	-586.874
* 4	4.790	C- 8	-81.514	-173.181	-399.937	C- 7	-281.352	-139.032	-531.196
* 5	6.050	C- 8	-368.606	-278.242	-371.212	C- 6	-504.447	-210.255	-493.785
2 - 1	6.400	C- 8	-470.358	-302.869	-363.233	C- 6	-580.671	-224.978	-485.806
2 - 3	0.000	C- 8	-470.358	363.233	-302.869	C- 6	-580.671	485.806	-224.978
* 1	0.350	C- 8	-348.063	335.595	-302.869	C- 6	-415.475	458.169	-224.978
* 2	1.610	C- 7	111.990	343.311	-223.161	C- 8	12.105	236.101	-302.869
* 3	3.103	C- 7	504.066	173.002	-223.161	C- 8	276.834	118.051	-302.869
* 4	4.600	C- 6	631.825	0.000	-224.978	C- 8	365.077	0.000	-302.869
* 5	6.095	C- 6	487.356	-183.441	-224.978	C- 8	276.834	-118.051	-302.869
* 6	7.590	C- 6	94.293	-342.396	-224.978	C- 8	12.105	-236.101	-302.869
* 7	8.850	C- 8	-348.063	-335.595	-302.869	C- 6	-415.475	458.169	-224.978
3 - 2	9.200	C- 8	-470.358	-363.233	-302.869	C- 6	-580.671	-485.806	-224.978
3 - 4	0.000	C- 8	-470.358	302.869	-303.233	C- 6	-580.671	224.978	-485.806
* 1	0.350	C- 8	-368.606	278.242	-371.212	C- 6	-504.447	210.255	-493.785
* 2	1.610	C- 8	-81.514	173.181	-399.937	C- 6	-280.556	140.849	-522.510
* 3	3.175	C- 8	64.600	6.945	-435.615	C- 6	-150.388	18.899	-558.189
* 4	4.740	C- 8	-80.436	-198.895	-471.293	C- 6	-242.093	-142.656	-593.867
* 5	6.000	C- 8	-450.884	-393.398	-500.018	C- 6	-519.188	-301.504	-622.592
4 - 3	6.400	C- 8	-621.580	-460.513	-509.137	C- 6	-650.362	-357.300	-631.711
4 - 1	0.000	C- 8	-621.580	509.135	-460.513	C- 6	-650.362	631.709	-357.300
* 1	0.350	C- 6	-438.176	583.645	-357.300	C- 8	-450.162	470.396	-460.513
* 2	1.810	C- 6	267.561	383.146	-357.300	C- 8	118.652	308.801	-460.513
* 3	3.205	C- 6	668.447	191.573	-357.300	C- 8	441.735	154.401	-460.513
* 4	4.600	C- 6	802.059	0.000	-357.300	C- 8	549.430	0.000	-460.513
* 5	5.995	C- 7	681.330	-183.420	-359.118	C- 8	441.735	-154.401	-460.513
* 6	7.390	C- 7	284.897	-386.166	-359.118	C- 8	118.652	-308.801	-460.513
* 7	8.850	C- 6	-438.176	-583.645	-357.300	C- 8	-450.162	470.396	-460.513
1 - 4	9.200	C- 8	-621.580	-509.135	-460.513	C- 7	-660.364	-660.396	-359.118

S. MAXIMUM

S. MINIMUM

No.	L (m)	Case	M (tm)	S (t)	N (t)	Case	M (tm)	S (t)	N (t)
1 -	0.000	C-8	-621.580	460.513	-509.137	C-6	-650.862	357.300	-631.711
* 1	0.400	C-8	-450.884	393.398	-500.018	C-6	-519.188	301.504	-622.592
* 2	1.660	C-8	-80.436	198.895	-471.293	C-6	-242.063	142.656	-593.867
* 3	3.225	C-8	64.600	-6.945	-435.615	C-6	-150.388	-18.899	-558.189
* 4	4.790	C-7	-281.352	-139.032	-551.196	C-8	-81.514	-173.181	-399.937
* 5	6.050	C-7	-502.953	-208.437	-522.471	C-8	-368.606	-278.242	-371.212
2 -	6.400	C-7	-578.541	-223.161	-514.492	C-8	-470.358	-302.869	-363.233
2 -	0.000	C-7	-578.541	514.492	-223.161	C-8	-470.358	363.233	-302.869
* 1	0.350	C-7	-404.981	477.279	-223.161	C-8	-348.063	335.595	-302.869
* 2	1.610	C-7	111.990	343.311	-223.161	C-8	12.105	236.101	-302.869
* 3	3.105	C-6	487.356	183.441	-224.978	C-8	275.834	118.031	-302.869
* 4	4.600	C-6	631.825	0.000	-224.978	C-7	613.507	-23.572	-223.161
* 5	6.095	C-8	276.834	-118.051	-302.869	C-6	487.356	-183.441	-224.978
* 6	7.590	C-8	12.105	-236.101	-302.869	C-6	94.293	-342.333	-224.978
* 7	8.850	C-8	-348.063	-335.595	-302.869	C-6	-415.475	-458.169	-224.978
3 -	9.200	C-8	-470.358	-363.233	-302.869	C-6	-580.671	-485.806	-224.978
3 -	0.000	C-8	-470.358	302.869	-363.233	C-7	-563.456	223.161	-457.120
* 1	0.350	C-8	-368.606	278.242	-371.212	C-7	-487.868	208.437	-463.100
* 2	1.610	C-8	-81.514	173.181	-399.937	C-7	-266.267	139.032	-493.825
* 3	3.175	C-6	-150.388	18.899	-558.189	C-8	64.600	6.945	-435.615
* 4	4.740	C-6	-242.063	-142.656	-593.867	C-8	-80.436	-198.895	-471.293
* 5	6.000	C-6	-519.188	-301.504	-622.592	C-8	-450.884	-398.398	-600.018
* 6	6.400	C-6	-650.862	-357.300	-631.711	C-8	-621.580	-460.513	-509.137
4 -	0.000	C-6	-650.862	631.709	-357.300	C-8	-621.580	509.135	-460.513
* 1	0.350	C-6	-438.176	583.645	-357.300	C-8	-450.162	470.396	-460.513
* 2	1.810	C-6	267.581	383.146	-357.300	C-8	118.652	308.801	-460.513
* 3	3.205	C-7	651.645	156.725	-359.118	C-8	441.735	154.401	-460.513
* 4	4.600	C-7	800.110	11.884	-359.118	C-6	802.069	0.000	-357.300
* 5	5.995	C-8	441.735	-154.401	-460.513	C-6	668.447	-191.573	-357.300
* 6	7.390	C-8	118.652	-308.801	-460.513	C-7	284.897	-386.186	-359.118
* 7	8.850	C-8	-450.162	-470.396	-460.513	C-7	-438.650	-606.392	-359.118
1 -	9.200	C-8	-621.580	-509.135	-460.513	C-7	-660.396	-660.396	-359.118

N. MAXIMUM N. MINIMUM

No.	L (m)	Case	M (tm)	S (t)	N (t)	Case	M (tm)	S (t)	N (t)
1 -	0.000	C- 8	-621.580	460.513	-509.137	C- 7	-660.364	359.118	-660.397
1 *	0.400	C- 8	-450.884	398.398	-500.018	C- 7	-527.963	303.321	-651.278
1 *	1.660	C- 8	-80.436	198.895	-471.293	C- 7	-248.548	144.473	-622.353
2 *	3.225	C- 8	64.600	-6.945	-435.615	C- 7	-154.029	-17.081	-586.874
2 *	4.790	C- 8	-81.514	-173.181	-399.937	C- 7	-281.332	-139.032	-551.196
2 *	6.050	C- 8	-368.606	-278.242	-371.212	C- 7	-502.955	-208.437	-522.471
2 -	6.400	C- 8	-470.358	-302.869	-363.233	C- 7	-578.541	-223.161	-514.492
2 -	0.000	C- 7	-578.541	514.492	-223.161	C- 8	-470.358	363.233	-302.869
2 *	0.350	C- 7	-404.981	477.279	-223.161	C- 8	-348.063	335.595	-302.869
2 *	1.610	C- 7	111.990	343.311	-223.161	C- 8	12.105	236.101	-302.869
2 *	3.105	C- 7	504.066	173.002	-223.161	C- 8	276.834	118.051	-302.869
2 *	4.600	C- 7	613.507	-23.507	-223.161	C- 8	365.077	0.000	-302.869
2 *	6.095	C- 7	459.449	-182.526	-223.161	C- 8	276.834	-118.051	-302.869
2 *	7.590	C- 7	70.167	-329.989	-223.161	C- 8	12.105	-236.101	-302.869
2 *	8.850	C- 7	-408.300	-429.483	-223.161	C- 8	-348.063	-335.595	-302.869
3 -	9.200	C- 7	-563.456	-457.120	-223.161	C- 8	-470.358	-363.233	-302.869
3 -	0.000	C- 8	-470.358	302.869	-363.233	C- 6	-580.671	224.978	-485.806
3 *	0.350	C- 8	-368.606	278.242	-371.212	C- 6	-504.447	210.255	-493.785
3 *	1.610	C- 8	-81.514	173.181	-399.937	C- 6	-280.556	140.849	-522.510
3 *	3.175	C- 8	64.600	6.945	-435.615	C- 6	-150.388	18.899	-558.189
3 *	4.740	C- 8	-80.436	-198.895	-471.293	C- 6	-242.093	-142.656	-593.807
3 *	6.000	C- 8	-450.884	-398.398	-500.018	C- 6	-519.188	-301.504	-622.592
4 -	6.400	C- 8	-621.580	-460.513	-509.137	C- 6	-650.862	-357.300	-633.711
4 -	0.000	C- 6	-650.862	631.709	-357.300	C- 8	-621.580	509.135	-400.513
4 *	0.350	C- 6	-438.176	583.645	-357.300	C- 8	-450.102	470.396	-460.513
4 *	1.810	C- 6	267.581	383.146	-357.300	C- 8	118.652	308.801	-460.513
4 *	3.205	C- 6	668.447	191.573	-357.300	C- 8	441.735	154.401	-460.513
4 *	4.600	C- 6	802.069	0.000	-357.300	C- 8	549.430	0.000	-460.513
4 *	5.965	C- 6	668.447	-191.573	-357.300	C- 8	441.735	-154.401	-460.513
4 *	7.390	C- 6	267.581	-383.146	-357.300	C- 8	118.652	-308.801	-460.513
4 *	8.850	C- 6	-438.176	-583.645	-357.300	C- 8	-450.102	-470.396	-400.513
1 -	9.200	C- 6	-650.862	-631.709	-357.300	C- 8	-621.580	-509.135	-460.513

NO 7 BOX CULVERT FOR ROAD

D = 0.500 m

(1) Dead load

a) vertical load ----- (case-1)

For upper slab $w_1 = 22.6 \times 0.50 + 23.6 \times 0.70 = 27.820 \text{ kN/m}$

For side wall $w_2 = 23.6 \times 0.70 = 16.520 \text{ ''}$

For bottom slab $w_3 = 27.820 + \frac{2 \times 16.52 \times 6.40}{9.20} = 50.804 \text{ ''}$

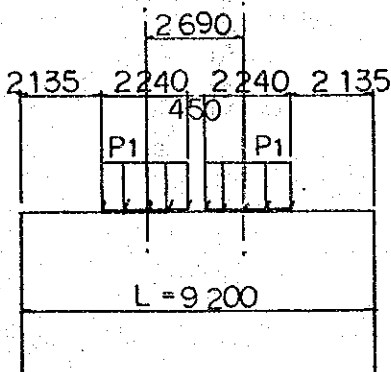
b) Horizontal load --- earth pressure ----- (case-2)

For side wall $P_1 = (22.6 \times 0.50 + 19.60 \times 0.35) \times 0.500 = 9.080 \text{ kN/m}$

$P_2 = (22.6 \times 0.50 + 19.60 \times 6.75) \times 0.500 = 71.800 \text{ ''}$

(2) Live load

a) Vertical load of center ----- (case-3)



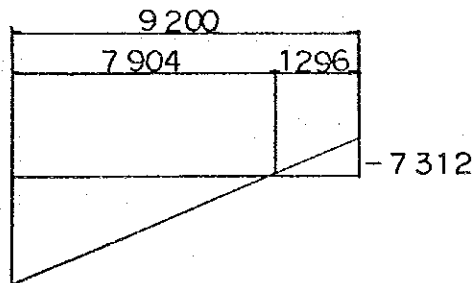
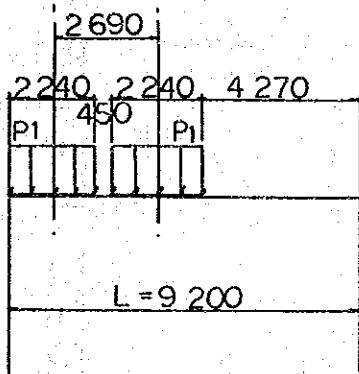
$B = (0.30 + 0.50 + 0.70) \operatorname{cosec} 42^\circ = 2.240 \text{ m}$

$P_1 = \frac{10 \times 30}{3.50 \times B} = \frac{10 \times 30}{3.50 \times 2.24} = 38.265 \text{ KN/m}$

For bottom slab

$P_2 = \frac{2 \times 38.265 \times 2.240}{9.20} = 18.633 \text{ KN/m}$

b) Vertical load of partial ----- (case-4)



For bottom slab

$P_2 = \frac{2 \times 38.265 \times 2.240}{9.20} \pm \frac{6 \times 38.265 \times 2.240 (3.480 + 0.790)}{9.20^2}$
 $= 18.633 \pm 25.945 = \begin{cases} P_2-1 = +44.578 \text{ KN/m} \\ P_2-2 = -7.312 \text{ KN/m} \end{cases}$

C) Horizontal load of live load surcharge ----- (case-5)

$P_e = g_{oko} = 34.300 \times 0.500 = 17.150 \text{ KN/m}$

BOX FOR ROAD NO 7' Depth = 0.500 For Check

NOTE: THE DIMENSION(S) BE EXCHANG TO
DIMENSION(KN) INTO THIS CALCULATION

No	X (m)	Y (m)
1	0.0000	0.0000
2	0.0000	6.4000
3	9.2000	6.4000
4	9.2000	0.0000

No	I	J	A (m ²)	I (m ⁴)	I - J	L (m)	E (t/m ²)	EPS
1	1	2	0.70000	0.028580	Fix - Fix	6.400	2.50E+07	1.00E-05
2	2	3	0.70000	0.028580	Fix - Fix	9.200	2.50E+07	1.00E-05
3	3	4	0.70000	0.028580	Fix - Fix	6.400	2.50E+07	1.00E-05
4	4	1	0.80000	0.042670	Fix - Fix	9.200	2.50E+07	1.00E-05

No	X (t/m)	Y (t/m)	M (tm/Rad)
1	Fix	Fix	Free
4	Free	Fix	Free

No	L-No	L-No	L-No	L-No	L-No	L-No	L-No	L-No	L-No
1	11	12	13	14	15	16	17	18	19
2	1	2	3	4	5	6	7	8	9
3	5	6	7	8	9	10	11	12	13
4	14	15	16	17	18	19	20	21	22

No. : 1
: Dead load

No	i - j	Li (m)	Lo (m)	Pi (t/m)	Pj (t/m)
1	1- 2	0.000	6.400	-16.520	-16.520
3	3- 4	0.000	6.400	-16.520	-16.520
2	2- 3	0.000	9.200	-27.820	-27.820
4	4- 1	0.000	9.200	50.804	50.804

$\Sigma V = -0.003 (t)$
 $\Sigma H = 0.000 (t)$

No. : 2
: Earth pressure

No	i - j	Li (m)	Lo (m)	Pi (t/m)	Pj (t/m)
1	1- 2	0.000	6.400	71.800	9.080
3	3- 4	0.000	6.400	-9.080	-71.800

$\Sigma V = 0.000 (t)$
 $\Sigma H = 0.000 (t)$

No. : 3
: HB live load-VL-

No	i - j	Li (m)	Lo (m)	Pi (t/m)	Pj (t/m)
2	2- 3	2.135	2.240	-38.265	-38.265
3	3- 4	4.825	2.240	-38.265	-38.265
4	4- 1	0.000	9.200	18.633	18.633

BOX FOR ROAD NO 7

: HB live load-VL-
No. : 4

No	i - j	Li (m)	Lo (m)	Pi (t/m)	Pj (t/m)
2	2- 3	Y 0.000	2.240	-38.265	-38.265
2	2- 3	Y 2.690	2.240	-38.265	-38.265
4	4- 1	Y 0.000	1.296	-7.312	0.000
4	4- 1	Y 1.296	7.904	0.000	44.578

$\Sigma V = 0.007 (t)$
 $\Sigma H = 0.000 (t)$

基本荷重ケース
荷重ケース
支点条件ケース
No. : 5

No	i - j	Li (m)	Lo (m)	Pi (t/m)	Pj (t/m)
1	1- 2	X 0.000	6.400	17.150	17.150
3	3- 4	X 0.000	6.400	-17.150	-17.150

$\Sigma V = 0.000 (t)$
 $\Sigma H = 0.000 (t)$

BOX FOR ROAD NO 7

No	C-No 1	C-No 2	C-No 3
No	No 6	No 7	No 8
No 1	1.3800	1.3800	1.3800
No 2	1.6500	1.6500	1.6500
No 3	1.4300	0.0000	0.0000
No 4	0.0000	1.4300	0.0000
No 5	0.0000	0.0000	1.6500

No 1 : 6 7 8

No.	Case. 1			Case. 2			Case. 3		
	RX (t)	RY (t)	RM (tm)	RX (t)	RY (t)	RM (tm)	RX (t)	RY (t)	RM (tm)
1.	0.000	0.002	0.000	0.000	0.000	0.000	0.000	0.002	0.000
4.	0.000	0.002	0.000	0.000	0.000	0.000	0.000	0.002	0.000
No.	Case. 4			Case. 5			Case. 6		
	RX (t)	RY (t)	RM (tm)	RX (t)	RY (t)	RM (tm)	RX (t)	RY (t)	RM (tm)
1.	0.000	-0.002	0.000	0.000	0.000	0.000	0.000	0.005	0.000
4.	0.000	-0.005	0.000	0.000	0.000	0.000	0.000	0.005	0.000
No.	Case. 7			Case. 8					
	RX (t)	RY (t)	RM (tm)	RX (t)	RY (t)	RM (tm)			
1.	0.000	0.000	0.000	0.000	0.000	0.000			

BOX FOR ROAD NO 7

No.	Case. 1			Case. 2			Case. 3		
	X-DIS.(mm)	Y-DIS.(mm)	ROTA.(mmRad)	X-DIS.(mm)	Y-DIS.(mm)	ROTA.(mmRad)	X-DIS.(mm)	Y-DIS.(mm)	ROTA.(mmRad)
1.	0.00000	0.00000	7.24551	0.00000	0.00000	-3.38728	0.00000	0.00000	3.3002
2.	-0.06646	-0.66134	-5.93643	-0.14433	0.00000	3.21935	0.04378	-0.31347	-4.1625
3.	0.00443	-0.66134	5.93643	-0.62534	0.00000	-3.21935	-0.00292	-0.31347	4.1625
4.	-0.06203	0.00000	-7.24551	-0.76967	0.00000	3.38728	0.04086	0.00000	-3.3002

No.	Case. 4			Case. 5			Case. 6		
	X-DIS.(mm)	Y-DIS.(mm)	ROTA.(mmRad)	X-DIS.(mm)	Y-DIS.(mm)	ROTA.(mmRad)	X-DIS.(mm)	Y-DIS.(mm)	ROTA.(mmRad)
1.	0.00000	0.00000	3.40303	0.00000	0.00000	-1.34866	0.00000	0.00000	9.1291
2.	0.91557	-0.46791	-4.00040	0.01154	0.00000	1.47088	-0.26725	-1.36091	-8.8328
3.	0.89844	-0.15902	2.71001	-0.27005	0.00000	-1.47088	-1.02987	-1.36091	8.8328
4.	0.01499	0.00000	-2.67484	-0.25851	0.00000	1.34866	-1.29712	0.00000	-9.1291

No.	Case. 7			Case. 8		
	X-DIS.(mm)	Y-DIS.(mm)	ROTA.(mmRad)	X-DIS.(mm)	Y-DIS.(mm)	ROTA.(mmRad)
1.	0.00000	0.00000	9.27613	0.00000	0.00000	2.18451
2.	0.97941	-1.58177	-8.60091	-0.31081	-0.91265	-0.45339
3.	0.25908	-1.14005	6.75565	-1.47128	-0.91265	0.45339
4.	-1.33412	0.00000	-8.23481	-1.78208	0.00000	-2.18451

No	L(m)	Case 1 Dead load		Case 2 Earth pressure		Case 3 HB live load-VL-		N (t)	S (t)	N (t)	S (t)
		M (tm)	S (t)	M (tm)	S (t)	M (tm)	S (t)				
1-	2	0.000	13.484	-233.700	-78.552	167.319	0.000	0.000	-8.882	-85.714	-8.882
*	1	0.400	13.484	-227.092	-17.264	139.383	0.000	0.000	-8.882	-85.714	-8.882
*	2	1.660	13.484	-206.277	107.743	61.634	0.000	0.000	-8.882	-85.714	-8.882
*	3	3.225	13.484	-180.423	142.455	-13.273	0.000	0.000	-8.882	-85.714	-8.882
*	4	4.790	13.484	-154.569	78.721	-64.177	0.000	0.000	-8.882	-85.714	-8.882
*	5	6.050	13.484	-133.754	-18.607	-87.719	0.000	0.000	-8.882	-85.714	-8.882
2-	1	6.400	13.484	-127.972	-50.005	-91.497	0.000	0.000	-8.882	-85.714	-8.882
2-	3	0.000	127.972	13.484	-50.005	0.000	-91.497	85.714	-8.882	-85.714	-8.882
*	1	0.350	118.235	13.484	-50.005	0.000	-91.497	85.714	-8.882	-85.714	-8.882
*	2	1.610	83.182	13.484	-50.005	0.000	-91.497	26.262	-8.882	-85.714	-8.882
*	3	3.105	159.331	13.484	-50.005	0.000	-91.497	136.402	-8.882	-85.714	-8.882
*	4	4.600	190.320	13.484	-50.005	0.000	-91.497	167.261	-8.882	-85.714	-8.882
*	5	6.095	-41.591	13.484	-50.005	0.000	-91.497	136.402	-8.882	-85.714	-8.882
*	6	7.590	65.963	13.484	-50.005	0.000	-91.497	26.262	-8.882	-85.714	-8.882
*	7	8.850	-60.929	13.484	-50.005	0.000	-91.497	-81.737	-8.882	-85.714	-8.882
3-	2	9.200	-127.972	13.484	-50.005	0.000	-91.497	-111.737	-8.882	-85.714	-8.882
3-	4	0.000	-13.484	-127.972	-50.005	91.497	0.000	0.000	8.882	-85.714	8.882
*	1	0.350	-13.484	-133.754	-18.607	87.719	0.000	0.000	8.882	-85.714	8.882
*	2	1.610	-13.484	-154.569	78.721	64.177	0.000	0.000	8.882	-85.714	8.882
*	3	3.175	-13.484	-180.423	142.455	13.273	0.000	0.000	8.882	-85.714	8.882
*	4	4.740	-13.484	-206.277	107.743	-61.634	0.000	0.000	8.882	-85.714	8.882
*	5	6.000	-13.484	-227.092	-17.264	-139.383	0.000	0.000	8.882	-85.714	8.882
4-	3	6.400	-13.484	-233.700	-78.552	-167.319	0.000	0.000	8.882	-85.714	8.882
4-	1	0.000	233.698	-13.484	-78.552	0.000	-167.319	85.712	8.882	8.882	8.882
*	1	0.350	215.917	-13.484	-78.552	0.000	-167.319	79.190	8.882	8.882	8.882
*	2	1.810	141.743	-13.484	-78.552	0.000	-167.319	51.986	8.882	8.882	8.882
*	3	3.205	297.761	-13.484	-78.552	0.000	-167.319	25.993	8.882	8.882	8.882
*	4	4.600	347.194	-13.484	-78.552	0.000	-167.319	0.000	8.882	8.882	8.882
*	5	5.995	297.761	-13.484	-78.552	0.000	-167.319	-25.993	8.882	8.882	8.882
*	6	7.390	149.462	-13.484	-78.552	0.000	-167.319	-51.986	8.882	8.882	8.882
*	7	8.850	-215.917	-13.484	-78.552	0.000	-167.319	-79.190	8.882	8.882	8.882
1-	4	9.200	-233.698	-13.484	-78.552	0.000	-167.319	-85.712	8.882	8.882	8.882

No	L(m)	Case 4 HB live load-VL-			Case 5 HB live load-HL-			Case 6		
		M (tm)	S (t)	N (t)	M (tm)	S (t)	N (t)	M (tm)	S (t)	N (t)
1-	2	0.000	-3.258	-127.945	-31.276	56.197	0.000	-470.737	281.983	-445.070
*	1	0.400	-3.258	-127.945	-10.169	49.337	0.000	-367.249	235.889	-465.957
*	2	1.660	-3.258	-127.945	38.382	27.728	0.000	-153.546	107.602	-407.232
*	3	3.225	-3.258	-127.945	60.774	0.888	0.000	-87.027	-15.994	-371.554
*	4	4.750	-3.258	-127.945	41.162	-25.951	0.000	-182.946	-99.985	-355.876
*	5	6.050	-3.258	-127.945	-5.150	-47.560	0.000	-336.094	-138.829	-307.151
2-	1	6.400	-3.258	-127.945	-22.847	-53.563	0.000	-385.833	-145.063	-299.172
2-	3	0.000	127.945	-3.258	-22.847	0.000	-53.563	-385.833	299.172	-145.063
*	1	0.350	114.553	-3.258	-22.847	0.000	-53.563	-283.474	285.735	-145.063
*	2	1.610	66.322	-3.258	-22.847	0.000	-53.563	46.076	237.361	-145.063
*	3	3.105	130.757	-3.258	-22.847	0.000	-53.563	332.286	126.889	-145.063
*	4	4.600	127.392	-3.258	-22.847	0.000	-53.563	419.317	0.000	-145.063
*	5	6.095	64.470	-3.258	-22.847	0.000	-53.563	332.286	-126.889	-145.063
*	6	7.590	-0.535	-3.258	-22.847	0.000	-53.563	46.076	-237.361	-145.063
*	7	8.850	-55.322	-3.258	-22.847	0.000	-53.563	-283.474	-285.735	-145.063
3-	2	9.200	-43.482	-3.258	-22.847	0.000	-53.563	-385.833	-299.172	-145.063
3-	4	0.000	3.258	-43.482	-22.847	53.563	0.000	-385.833	145.063	-299.172
*	1	0.350	3.258	-43.482	-5.150	47.560	0.000	-336.094	138.829	-307.151
*	2	1.610	3.258	-43.482	41.162	25.951	0.000	-182.946	99.985	-335.870
*	3	3.175	3.258	-43.482	60.774	-0.888	0.000	-87.027	15.994	-371.554
*	4	4.740	3.258	-43.482	38.382	-27.728	0.000	-153.546	-107.602	-407.232
*	5	6.000	3.258	-43.482	-10.169	-49.337	0.000	-367.249	-235.889	-435.957
4-	3	6.400	3.258	-43.482	-31.276	-56.197	0.000	-470.737	-281.983	-445.070
4-	1	0.000	43.482	3.258	-31.276	0.000	-56.197	-470.737	445.072	-281.983
*	1	0.350	45.700	3.258	-31.276	0.000	-56.197	-320.689	411.206	-281.983
*	2	1.810	35.420	3.258	-31.276	0.000	-56.197	175.953	269.946	-281.983
*	3	3.205	96.281	3.258	-31.276	0.000	-56.197	458.784	134.973	-281.983
*	4	4.600	136.191	3.258	-31.276	0.000	-56.197	552.927	0.000	-281.983
*	5	5.995	-14.042	3.258	-31.276	0.000	-56.197	458.784	-134.973	-281.983
*	6	7.390	-56.500	3.258	-31.276	0.000	-56.197	176.553	-269.946	-281.983
*	7	8.850	-112.691	3.258	-31.276	0.000	-56.197	-320.889	-411.208	-281.983
1-	4	9.200	-127.945	3.258	-31.276	0.000	-56.197	-470.737	-445.072	-281.983

BOX FOR ROAD NO 7

No	L(m)	Case 7			Case 8			N (t)	S (t)	N (t)	S (t)
		L(m)	M (tm)	S (t)	N (t)	M (tm)	S (t)				
1- 2	0.000	-495.528	290.026	-505.468	-443.847	387.409	-322.506				
* 1	0.400	-388.822	243.932	-496.349	-300.452	329.996	-313.387				
* 2	1.660	-164.985	115.645	-467.624	9.365	156.054	-284.662				
* 3	3.225	-85.879	-7.951	-431.946	132.708	-1.827	-248.984				
* 4	4.790	-169.211	-91.942	-396.267	24.307	-130.104	-213.305				
* 5	6.050	-312.225	-130.786	-367.542	-189.254	-204.603	-184.581				
2- 1	6.400	-359.149	-137.020	-359.563	-263.746	-220.741	-176.601				
2- 3	0.000	-359.149	359.563	-137.020	-263.746	176.601	-220.741				
* 1	0.350	-239.005	326.975	-137.020	-204.287	163.164	-220.741				
* 2	1.610	99.072	209.655	-137.020	-29.176	114.791	-220.741				
* 3	3.105	324.213	95.079	-137.020	99.534	57.395	-220.741				
* 4	4.600	362.304	-44.122	-137.020	142.437	0.000	-220.741				
* 5	6.055	229.422	-119.574	-137.020	99.534	-57.395	-220.741				
* 6	7.590	7.756	-176.970	-137.020	-29.176	-114.791	-220.741				
* 7	8.850	-245.702	-225.343	-137.020	-204.287	-163.164	-220.741				
3- 2	9.200	-326.923	-238.780	-137.020	-263.746	-176.601	-220.741				
3- 4	0.000	-326.923	137.020	-238.780	-263.746	220.741	-176.601				
* 1	0.350	-279.999	130.785	-246.759	-189.254	204.603	-184.581				
* 2	1.610	-136.985	91.942	-275.484	24.307	130.104	-213.305				
* 3	3.175	-53.653	7.951	-311.163	132.708	1.827	-248.984				
* 4	4.740	-132.759	-115.645	-346.841	9.365	-166.054	-284.662				
* 5	6.000	-356.597	-243.932	-375.566	-300.452	-329.996	-313.387				
4- 3	6.400	-463.302	-290.026	-384.685	-443.847	-387.409	-322.506				
4- 1	0.000	-463.302	384.689	-290.026	-443.847	322.504	-387.409				
* 1	0.350	-332.372	363.317	-290.026	-335.264	297.965	-387.409				
* 2	1.810	127.297	263.501	-290.026	25.042	195.606	-387.409				
* 3	3.205	418.982	152.068	-290.026	229.695	97.803	-387.409				
* 4	4.600	544.270	24.940	-290.026	297.912	0.000	-387.409				
* 5	5.995	481.267	-117.883	-290.026	229.695	-97.803	-387.409				
* 6	7.390	208.079	-276.400	-290.026	25.042	-195.606	-387.409				
* 7	8.850	-326.755	-459.113	-290.026	-335.204	-297.965	-387.409				
1- 4	9.200	-495.528	-505.469	-290.026	-443.847	-322.504	-387.409				

PICK-UP No. 1 *

M. MAXIMUM

M. MINIMUM

No.	L (m)	Case	M (tm)	S (t)	N (t)	Case	M (tm)	S (t)	N (t)
1	0.000	C-8	-443.847	387.409	-322.506	C-7	-495.528	290.026	-505.468
*	0.400	C-8	-300.452	329.996	-313.387	C-7	-388.822	243.932	-496.349
*	1.660	C-8	9.365	166.054	-284.662	C-7	-164.985	115.645	-467.624
*	3.225	C-8	152.708	-1.827	-248.984	C-6	-87.027	-15.994	-371.554
*	4.790	C-8	24.307	-130.104	-213.305	C-6	-182.946	-99.985	-335.876
*	6.050	C-8	-189.254	-204.603	-184.581	C-6	-336.094	-138.829	-307.151
2	6.400	C-8	-263.746	-220.741	-176.601	C-6	-385.833	-145.063	-299.172
2	0.000	C-8	-263.746	176.601	-220.741	C-6	-385.833	299.172	-145.063
*	0.350	C-8	-204.287	163.164	-230.741	C-6	-283.474	285.735	-145.063
*	1.610	C-7	99.072	209.655	-137.020	C-8	-29.176	114.791	-220.741
*	3.105	C-6	332.286	126.889	-145.063	C-8	99.534	57.395	-220.741
*	4.600	C-6	419.317	0.000	-145.063	C-8	142.437	0.000	-220.741
*	6.095	C-6	332.286	-126.889	-145.063	C-8	99.534	-57.395	-220.741
*	7.590	C-6	46.076	-237.361	-145.063	C-8	-29.176	-114.791	-220.741
*	8.850	C-8	-204.287	-163.164	-220.741	C-6	-283.474	-283.735	-145.063
3	9.200	C-8	-263.746	-176.601	-220.741	C-6	-385.833	-299.172	-145.063
3	0.000	C-8	-263.746	220.741	-176.601	C-6	-385.833	145.063	-299.172
*	0.350	C-8	-189.254	204.603	-184.581	C-6	-336.094	138.829	-307.151
*	1.610	C-8	24.307	130.104	-213.305	C-6	-182.946	99.985	-335.876
*	3.175	C-8	132.708	1.827	-248.984	C-6	-87.027	15.994	-371.554
*	4.740	C-8	9.365	-166.054	-284.662	C-6	-153.546	-107.602	-407.232
*	6.000	C-8	-300.452	-329.996	-313.387	C-6	-367.249	-235.889	-435.957
4	6.400	C-8	-443.847	-387.409	-322.506	C-6	-470.737	-281.983	-445.076
4	0.000	C-8	-443.847	322.504	-387.409	C-6	-470.737	445.072	-281.983
*	0.350	C-6	-320.889	411.208	-281.983	C-8	-335.264	297.965	-387.409
*	1.810	C-6	176.353	269.946	-281.983	C-8	25.042	195.606	-387.409
*	3.205	C-6	458.784	134.973	-281.983	C-8	229.695	97.803	-387.409
*	4.600	C-6	552.927	0.000	-281.983	C-8	297.912	0.000	-387.409
*	5.995	C-7	481.267	-117.883	-290.026	C-8	229.695	-97.803	-387.409
*	7.390	C-7	208.079	-276.400	-290.026	C-8	25.042	-195.606	-387.409
*	8.850	C-6	-320.889	-411.208	-281.983	C-8	-335.264	-297.965	-387.409
1	9.200	C-8	-443.847	-322.504	-387.409	C-7	-495.528	-505.469	-290.026

PICK-UP No. 1 *

S. MAXIMUM

S. MINIMUM

No.	L (m)	Case	M (tm)	S (t)	N (t)	Case	M (tm)	S (t)	N (t)
1 -	0.000	C- 8	-443.847	387.409	-322.506	C- 6	-470.737	281.983	-445.076
* 1	0.400	C- 8	-300.452	329.996	-313.387	C- 6	-367.249	235.889	-435.957
* 2	1.660	C- 8	9.365	166.054	-284.662	C- 6	-153.546	107.602	-407.232
* 3	3.225	C- 8	132.708	-1.827	-248.984	C- 6	-87.027	-15.994	-371.554
* 4	4.790	C- 7	-169.211	-91.942	-396.267	C- 8	24.307	-130.104	-213.305
* 5	6.050	C- 7	-312.225	-130.786	-367.542	C- 8	-189.254	-204.603	-184.581
2 -	6.400	C- 7	-359.149	-137.020	-359.563	C- 8	-263.746	-220.741	-176.601
2 -	0.000	C- 7	-359.149	359.563	-137.020	C- 8	-263.746	176.601	-220.741
* 1	0.350	C- 7	-239.005	326.975	-137.020	C- 8	-204.287	163.164	-220.741
* 2	1.610	C- 6	46.076	237.361	-145.063	C- 8	-29.176	114.791	-220.741
* 3	3.105	C- 6	332.286	126.889	-145.063	C- 8	99.534	57.395	-220.741
* 4	4.600	C- 8	142.437	0.000	-220.741	C- 7	362.304	-44.122	-137.020
* 5	6.095	C- 8	99.534	-57.395	-220.741	C- 6	332.286	-126.889	-145.063
* 6	7.590	C- 8	-29.176	-114.791	-220.741	C- 6	46.076	-237.361	-145.063
* 7	8.850	C- 8	-204.287	-163.164	-220.741	C- 6	-283.474	-285.735	-145.063
3 -	9.200	C- 8	-263.746	-176.601	-220.741	C- 6	-385.833	-299.172	-145.063
3 -	0.000	C- 8	-263.746	220.741	-176.601	C- 7	-326.923	137.020	-238.780
* 1	0.350	C- 8	-189.254	204.603	-184.581	C- 7	-279.999	130.786	-246.759
* 2	1.610	C- 8	24.307	130.104	-213.305	C- 7	-136.985	91.942	-275.484
* 3	3.175	C- 6	-87.027	15.994	-371.554	C- 8	132.708	1.827	-248.984
* 4	4.740	C- 6	-153.546	-107.602	-407.232	C- 8	9.365	-166.054	-284.662
* 5	6.000	C- 6	-367.249	-235.889	-435.957	C- 8	-300.452	-329.996	-313.387
4 -	6.400	C- 6	-470.737	-281.983	-445.076	C- 8	-443.847	-387.409	-322.506
4 -	0.000	C- 6	-470.737	445.076	-281.983	C- 8	-443.847	322.504	-387.409
* 1	0.350	C- 6	-320.889	411.208	-281.983	C- 8	-335.264	297.965	-387.409
* 2	1.810	C- 6	176.353	269.946	-281.983	C- 8	25.042	195.606	-387.409
* 3	3.205	C- 7	418.982	152.068	-290.026	C- 8	229.695	97.803	-387.409
* 4	4.600	C- 7	544.270	24.940	-290.026	C- 6	552.927	0.000	-281.983
* 5	5.995	C- 8	229.695	-97.803	-387.409	C- 6	458.784	-134.973	-281.983
* 6	7.390	C- 8	25.042	-195.606	-387.409	C- 7	208.079	-276.400	-290.026
* 7	8.850	C- 8	-335.264	-297.965	-387.409	C- 7	-326.755	-459.113	-290.026
1 -	9.200	C- 8	-443.847	-322.504	-387.409	C- 7	-495.528	-505.469	-290.026

BOX FOR ROAD NO 7'

PICK-UP No. 1 *

No.	L (m)	Case	N. MAXIMUM			N. MINIMUM		
			M (tm)	S (t)	N (t)	M (tm)	S (t)	N (t)
1 -	0.000	C- 8	-443.847	387.409	-322.506	-495.538	290.026	-505.468
* 1	0.400	C- 8	-300.452	329.996	-313.387	-388.822	243.822	-496.349
* 2	1.660	C- 8	9.365	166.054	-284.662	-164.985	115.645	-467.624
* 3	3.225	C- 8	132.708	-1.827	-248.984	-85.879	-7.951	-431.946
* 4	4.750	C- 8	24.307	-130.104	-213.305	-169.211	-91.942	-396.267
* 5	6.050	C- 8	-189.254	-204.603	-184.581	-312.225	-130.786	-367.542
2 -	6.400	C- 8	-263.746	-220.741	-176.601	-359.149	-137.020	-359.563
2 -	0.000	C- 7	-359.149	359.563	-137.020	-263.746	176.601	-220.741
* 1	0.350	C- 7	-239.005	326.975	-137.020	-204.287	163.164	-220.741
* 2	1.610	C- 7	99.072	209.655	-137.020	-29.176	114.791	-220.741
* 3	3.105	C- 7	324.213	95.079	-137.020	99.534	57.395	-220.741
* 4	4.600	C- 7	362.304	-44.122	-137.020	142.457	0.000	-220.741
* 5	6.095	C- 7	229.422	-119.574	-137.020	99.534	-57.395	-220.741
* 6	7.590	C- 7	7.756	-176.970	-137.020	-29.176	-114.791	-220.741
* 7	8.850	C- 7	-245.702	-225.343	-137.020	-204.287	-163.164	-220.741
3 -	9.200	C- 7	-326.923	-238.780	-137.020	-263.746	-176.601	-220.741
3 -	0.000	C- 8	-263.746	220.741	-176.601	-385.833	145.063	-299.172
* 1	0.350	C- 8	-189.254	204.603	-184.581	-336.094	138.829	-307.151
* 2	1.610	C- 8	24.307	130.104	-213.305	-182.946	99.985	-335.876
* 3	3.175	C- 8	132.708	1.827	-248.984	-87.027	15.994	-371.554
* 4	4.740	C- 8	9.365	-166.054	-284.662	-153.546	-107.602	-407.232
* 5	6.000	C- 8	-300.452	-329.996	-313.387	-367.249	-235.889	-435.957
4 -	6.400	C- 8	-443.847	-387.409	-322.506	-470.737	-281.983	-445.076
4 -	0.000	C- 6	-470.737	445.072	-281.983	-443.847	322.504	-387.409
* 1	0.350	C- 6	-320.889	411.208	-281.983	-335.264	297.965	-387.409
* 2	1.810	C- 6	176.353	269.946	-281.983	25.042	195.606	-387.409
* 3	3.205	C- 6	458.784	134.973	-281.983	229.695	97.803	-387.409
* 4	4.600	C- 6	552.927	0.000	-281.983	297.912	0.000	-387.409
* 5	5.995	C- 6	458.784	-134.973	-281.983	229.695	-97.803	-387.409
* 6	7.390	C- 6	176.353	-269.946	-281.983	25.042	-195.606	-387.409
* 7	8.850	C- 6	-320.889	-411.208	-281.983	-335.264	-297.965	-387.409
1 -	9.200	C- 6	-470.737	-445.072	-281.983	-443.847	-322.504	-387.409

CALCULATION OF WINGWALL

Calculation formula for wingwalls

bending moment

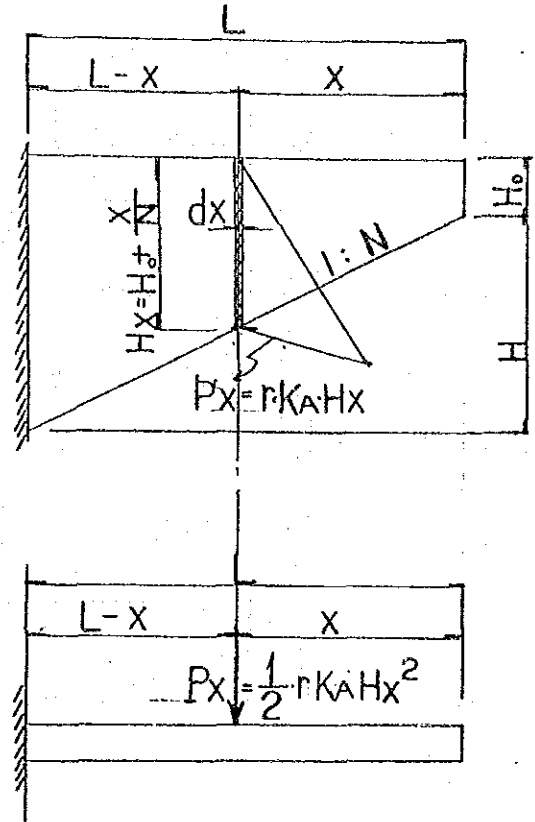
$$M_x = \int_0^L P_x (L-x) dx$$

$$= \int_0^L \frac{1}{2} r K_A \left(H_0 + \frac{x}{N} \right)^2 (L-x) dx$$

shearing force

$$S_x = \int_0^L P_x \cdot dx$$

$$= \int_0^L \frac{1}{2} r K_A \left(H_0 + \frac{x}{N} \right)^2 dx$$



∴ Analysis of upper formula for earth pressure

$$M_x = \frac{1}{2} r K_A \left(\frac{H_0 \cdot x^2}{2} + \frac{H_0 \cdot x^3}{3 \cdot N} + \frac{x^4}{12 \cdot N^2} \right)$$

$$S_x = \frac{1}{2} r K_A \left(H_0^2 \cdot x + \frac{H_0 \cdot x^2}{N} + \frac{x^3}{3 \cdot N^2} \right)$$

Calculation of bending moment and shearing force

Lx (m)	Hx (m)	S . L . S		U . L . S		Area of reinforced	thickness of member	
		Mx (KNm/m)	Sx (KN/m)	Mx (KNm/m)	Sx (KN/m)		D cm	d cm
5.0	4.633	67.975	41.159	117.257	71.000	Y ₁₆ -150 ^{ctc}	40	34.0
5.5	4.967	84.802	47.489	146.283	81.919	Y ₁₆ -150 ^{ctc}	40	34.0
6.0	5.300	104.088	54.256	179.552	93.592	Y ₁₆ -150 ^{ctc}	50	44.0
8.0	6.633	208.876	85.618	360.312	147.691	Y ₂₀ -150 ^{ctc}	60	54.0
8.5	6.967	242.772	94.528	418.782	163.061	Y ₂₅ -150 ^{ctc}	60	53.5
9.0	7.300	280.116	103.885	483.200	179.202	Y ₂₅ -150 ^{ctc}	60	53.5
9.5	7.633	321.039	113.675	553.792	196.090	Y ₂₅ -150 ^{ctc}	60	53.5
10.0	7.967	365.658	123.884	630.760	213.700	Y ₂₅ -150 ^{ctc}	70	63.5
10.5	8.300	414.225	134.541	714.538	232.083	Y ₂₀ -300 ^{ctc} Y ₃₂ -300 ^{ctc}	70	63.0
11.0	8.633	466.858	145.634	805.330	251.219	Y ₂₅ -300 ^{ctc} Y ₃₂ -300 ^{ctc}	70	63.0
11.5	8.967	523.665	157.143	903.322	271.072	Y ₃₂ -150 ^{ctc}	70	63.0

Each calculation of

Resisting moment and shearing intension for U.L.S and S.L.S

1) $L_x = 5.0^m$ and 5.5^m

$b = 100^{cm}$ $h = 40$ $d = 34.0$ $d' = 6.0$

$A_s = Y_{16} - 150^{cc} = 2.011/0.15 = 13.41 \text{ cm}^2$

$p = A_s \times 100/bd = 13.41 \times 100 / 100 \times 34.0 = 0.394 \%$

a) S.L.S

$$x = \frac{0.8 f_y \cdot A_s}{0.25 f_{cu} \cdot b} = \frac{0.8 \times 41000 \times 13.41}{0.25 \times 2500 \times 100} = 7.0 \text{ cm}$$

$$Z = d - x/3 = 34.0 - 7.0/3 = 31.7 \text{ cm}$$

$M_{RS} = 0.8 f_y A_s Z$

$$= 0.8 \times 41000 \times 13.41 \times 31.7 \times 10^{-5}$$

$$= 139.4 \text{ KNm} = M_s = 67.975 \text{ KNm or } 84.802 \text{ KNm}$$

$M_{RC} = 0.25 f_{cu} \cdot b \cdot x Z$

$$= 0.25 \times 2500 \times 100 \times 7.0 \times 31.7 \times 10^{-5}$$

$$= 138.7 \text{ KNm} > M$$

OK

b) U.L.S

$$x = \frac{0.87 f_y \cdot A_s}{0.40 f_{cu} \cdot b} = \frac{0.87 \times 41000 \times 13.41}{0.40 \times 2500 \times 100} = 4.8 \text{ cm}$$

$$Z = d - x/2 = 34.0 - 4.8/3 = 31.6 \text{ cm} < 0.95 \times 34.0 = 32.3 \text{ cm}$$

$M_{RS} = 0.87 f_y A_s Z$

$$= 0.87 \times 41000 \times 13.41 \times 31.6 \times 10^{-5}$$

$$= 151.1 \text{ KNm} > M_u = 117.257 \text{ KNm or } 146.283 \text{ KNm}$$

$M_{RC} = 0.40 f_{cu} \cdot b \cdot x Z$

$$= 0.40 \times 2500 \times 100 \times 4.8 \times 31.6 \times 10^{-5}$$

$$= 151.7 \text{ KNm} > M_u$$

OK

Notice : the U.L.S is critical from result of both calculation of resisting moment and the other case is exclude calculation of resisting moment for S.L.S

Shearing intension (U.L.S)

$$\tau = \frac{Su}{bd} = \frac{81.919 \times 10^3}{100 \times 34.0} = 24.1 \text{ N/cm}^2$$

$$< \tau_a = 35.0 + \frac{15.00}{0.25} (0.394 - 0.25) = 43.6 \text{ N/cm}^2$$

2) $L_x = 6.0^m$ (for U.L.S)

$$b = 100^{\text{cm}} \quad h = 50 \quad d = 44.0 \quad d' = 6.0$$

$$A_s = Y_{16-150} \rho = 2.011 / 0.15 = 13.41 \text{ cm}^2$$

$$P = 13.41 \times 100 / 100 \times 44.0 = 0.305$$

$$X = \frac{0.87 \times 41000 \times 13.41}{0.40 \times 2500 \times 100} = 4.8 \text{ cm}$$

$$Z = 44.0 - 4.8 / 2 = 41.6^{\text{cm}} < 0.95 \times 44.0 = 41.8 \text{ cm}$$

$$M_{RS} = 0.87 \times 41000 \times 13.41 \times 41.6 \times 10^5 = 199.0^{\text{KNm}} > M_u = 179.552^{\text{KNm}}$$

$$M_{RC} = 0.40 \times 2500 \times 100 \times 4.8 \times 41.6 \times 10^5 = 199.7^{\text{KNm}} > M_u = 179.552^{\text{KNm}}$$

OK

$$\tau = \frac{93.592 \times 10^3}{100 \times 44.0} = 21.3 \text{ N/cm}^2$$

$$< \tau_a = 35.0 + \frac{15.0}{0.25} (0.305 - 0.25) = 38.3 \text{ N/cm}^2$$

OK

3) $L_x = 8.0^m$ (for U.L.S)

$b = 100^{cm}$ $h = 60$ $d = 54.0$ $d' = 6.0$

$A_s = Y_{20-150}^{ctc} = 3.141/0.15 = 20.94 \text{ cm}^2$

$P = 20.94 \times 100 / 100 \times 54.0 = 0.388$

$X = \frac{0.87 \times 41000 \times 20.94}{0.40 \times 2500 \times 100} = 7.4 \text{ cm}$

$Z = 54.0 - 7.4/2 = 50.3^{cm} < 0.95 \times 54.0 = 51.3 \text{ cm}$ OK

$M_{RS} = 0.87 \times 41000 \times 20.94 \times 50.3 \times 10^{-5} = 375.7^{KNm} > M_u = 360.312^{KNm}$

$M_{RC} = 0.40 \times 2500 \times 100 \times 7.4 \times 50.3 \times 10^{-5} = 372.2^{KNm} > M_u = 360.312^{KNm}$
OK

$\tau = \frac{147.691 \times 10^3}{100 \times 54.0} = 27.4 \text{ N/cm}^2$

$< \tau_a = 35.0 + \frac{15.0}{0.25} (0.388 - 0.25) = 43.3 \text{ N/cm}^2$

4) $L_x = 8.5^m$ 9.0^m and 9.5^m (for U.L.S)

$b = 100^{cm}$ $h = 60$ $d = 53.5$ $d' = 6.5$

$A_s = Y_{25-150}^{ctc} = 4.909/0.15 = 32.73 \text{ cm}^2$

$P = 32.73 \times 100 / 100 \times 53.5 = 0.612$

$X = \frac{0.87 \times 41000 \times 32.73}{0.40 \times 2500 \times 100} = 11.8 \text{ cm}$

$Z = 53.5 - 11.8/2 = 47.6^{cm} < 0.95 \times 53.5 = 50.8 \text{ cm}$ OK

$M_{RS} = 0.87 \times 41000 \times 32.73 \times 47.6 \times 10^{-5} = 555.7^{KNm} > M_u = 418.782^{KNm}$

$M_{RC} = 0.40 \times 2500 \times 100 \times 11.8 \times 47.6 \times 10^{-5} = 561.7^{KNm} >$
 $\sim 553.792^{KNm}$

OK

$\tau = \frac{196.090 \times 10^3}{100 \times 53.5} = 36.7 \text{ N/cm}^2$

$< \tau_a = 50 + \frac{15.0}{0.50} (0.612 - 0.50) = 53.4 \text{ N/cm}^2$ OK

5) $L_x = 10.0^m$ (for U.L.S)

$$b = 100^{cm} \quad h=70 \quad d=63.5 \quad d' = 6.5$$

$$A_s = Y_{25-150}^{ctc} = 4.909/0.15 = 32.73 \text{ cm}^2$$

$$P = 32.73 \times 100 / 100 \times 63.5 = 0.515$$

$$X = \frac{0.87 \times 41000 \times 32.73}{0.40 \times 2500 \times 100} = 11.8 \text{ cm}$$

$$Z = 63.5 - 11.8/2 = 57.6^{cm} < 0.95 \times 63.5 = 60.3 \text{ cm} \quad \text{OK}$$

$$M_{RS} = 0.87 \times 41000 \times 32.73 \times 57.6 \times 10^{-5} = 672.5^{KNm} > M_u = 630.760^{KNm}$$

$$M_{RC} = 0.40 \times 2500 \times 100 \times 11.8 \times 57.6 \times 10^{-5} = 679.7^{KNm} > M_u = 630.760^{KNm} \quad \text{OK}$$

$$\tau = \frac{263.700 \times 10^3}{100 \times 63.5} = 33.7 \text{ N/cm}^2$$

$$< \tau_a = 50 + \frac{15.0}{0.50} (0.515 - 0.50) = 50.4 \text{ N/cm}^2$$

6) $L_x = 10.5^m$ (for U.L.S)

$$b = 100^{cm} \quad h=70 \quad d=63.0 \quad d' = 7.0$$

$$A_s = \begin{matrix} Y_{20-300}^{ctc} \\ Y_{32-300}^{ctc} \end{matrix} = \begin{bmatrix} 3.142/0.300 \\ 8.042/0.300 \end{bmatrix} = 37.28 \text{ cm}^2$$

$$P = 37.28 \times 100 / 100 \times 63.0 = 0.592$$

$$X = \frac{0.87 \times 41000 \times 37.28}{0.40 \times 2500 \times 100} = 13.4 \text{ cm}$$

$$Z = 63.0 - 13.4/2 = 56.3^{cm} < 0.95 \times 63.0 = 59.8 \text{ cm} \quad \text{OK}$$

$$M_{RS} = 0.87 \times 41000 \times 37.28 \times 56.3 \times 10^{-5} = 748.6^{KNm} > M_u = 714.538^{KNm}$$

$$M_{RC} = 0.40 \times 2500 \times 100 \times 13.4 \times 56.3 \times 10^{-5} = 754.4^{KNm} > M_u = 714.538^{KNm} \quad \text{OK}$$

$$\tau = \frac{232.083 \times 10^3}{100 \times 63.0} = 36.8 \text{ N/cm}^2$$

$$< \tau_a = 50 + \frac{15.0}{0.50} (0.592 - 0.50) = 52.7 \text{ N/cm}^2 \quad \text{OK}$$

$$7) L_x = 11.0^m \text{ (for U.L.S)}$$

$$b = 100^{\text{cm}} \quad h = 70 \quad d = 63.0 \quad d' = 7.0$$

$$A_s = \frac{Y_{25} - 300^{\text{ctc}}}{Y_{32} - 300^{\text{ctc}}} = \left[\frac{4.909/0.300}{8.042/0.300} \right] = 43.17 \text{ cm}^2$$

$$P = 43.17 \times 100 / 100 \times 63.5 = 0.685$$

$$\chi = \frac{0.87 \times 41000 \times 43.17}{0.40 \times 2500 \times 100} = 15.4 \text{ cm}$$

$$Z = 63.0 - 15.4/2 = 55.3^{\text{cm}} < 0.95 \times 63.0 = 59.8^{\text{cm}} \quad \text{OK}$$

$$M_{RS} = 0.87 \times 41000 \times 43.17 \times 55.3 \times 10^{-5} = 851.5^{\text{KNm}} > M_u = 805.330^{\text{KNm}}$$

$$M_{RC} = 0.40 \times 2500 \times 100 \times 15.4 \times 55.3 \times 10^{-5} = 851.6^{\text{KNm}} > M_u = 805.330^{\text{KNm}} \\ \text{OK}$$

$$\tau = \frac{251.219 \times 10^3}{100 \times 63.0} = 39.9 \text{ N/cm}^2$$

$$< \tau_a = 50.0 + \frac{15.0}{0.50} (0.685 - 0.50) = 55.4 \text{ N/cm}^2$$

check of S.L.S

$$\chi = \frac{0.80 \times 41000 \times 43.17}{0.25 \times 2500 \times 100} = 22.8 \text{ cm}$$

$$Z = 63.0 - 22.8/3 = 55.4^{\text{cm}}$$

$$M_{RS} = 0.80 \times 41000 \times 43.17 \times 55.4 \times 10^{-5} = 784.4^{\text{KNm}} > M_u = 466.858^{\text{KNm}}$$

$$M_{RC} = 0.25 \times 2500 \times 100 \times 22.8 \times 55.4 \times 10^{-5} = 789.4^{\text{KNm}} > M_u = 466.858^{\text{KNm}} \\ \text{OK}$$

$$8) L_x = 11.5^m \quad (\text{for U.L.S})$$

$$b = 100^{\text{cm}} \quad h = 70 \quad d = 63.0 \quad d' = 7.0$$

$$A_s = Y_{32-150}^{\text{ctc}} = 8.042/0.15 = 53.61 \quad \text{cm}^2$$

$$P = 53.61 \times 100 / 100 \times 63.0 = 0.851$$

$$X = \frac{0.87 \times 41000 \times 53.61}{0.40 \times 2500 \times 100} = 19.2 \quad \text{cm}$$

$$Z = 63.0 - 19.2/2 = 53.4^{\text{cm}} < 0.95 \times 63.0 = 59.8 \quad \text{cm} \quad \text{OK}$$

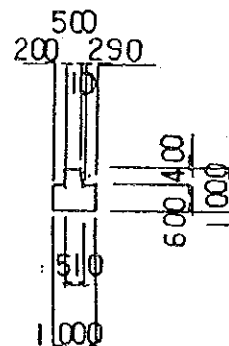
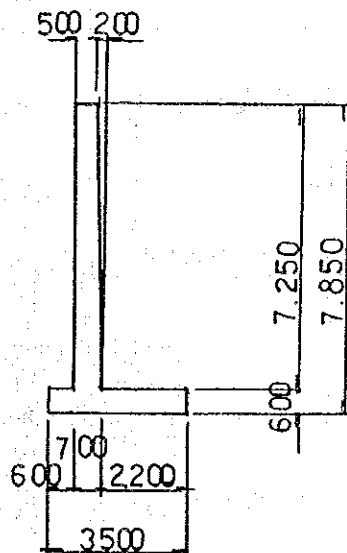
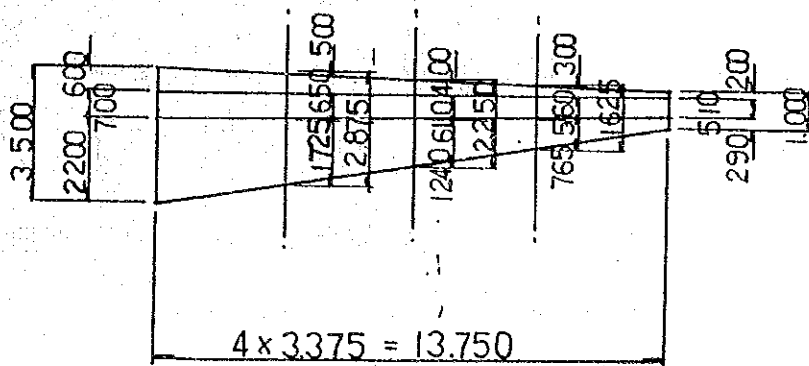
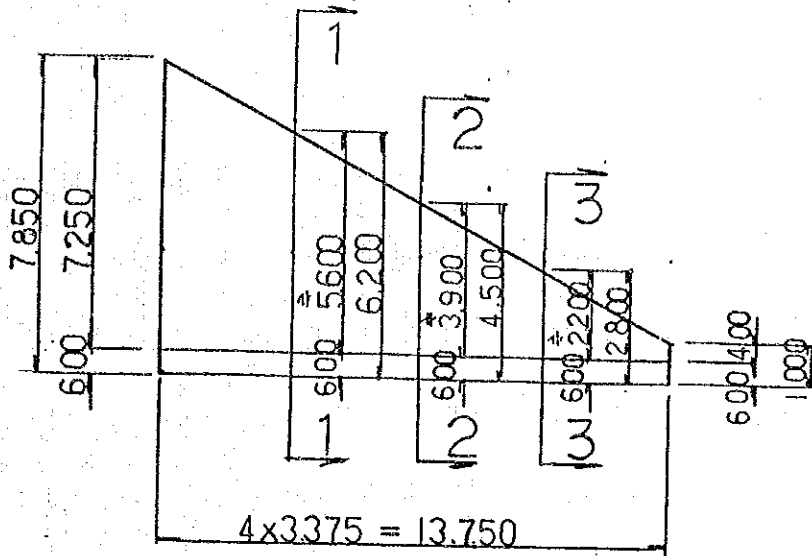
$$M_{RS} = 0.87 \times 41000 \times 53.61 \times 53.4 \times 10^{-5} = 1021.1^{\text{KNm}} > M_u = 903.322^{\text{KNm}}$$

$$M_{RC} = 0.40 \times 2500 \times 100 \times 19.2 \times 53.4 \times 10^{-5} = 1025.8^{\text{KNm}} > M_u = 903.322^{\text{KNm}} \quad \text{OK}$$

$$\tau = \frac{271.072 \times 10^3}{100 \times 63.0} = 43.1 \quad \text{N/cm}^2$$

$$< \tau_a = 50.0 + \frac{15.0}{0.50} (0.851 - 0.50) = 60.5 \quad \text{N/cm}^2$$

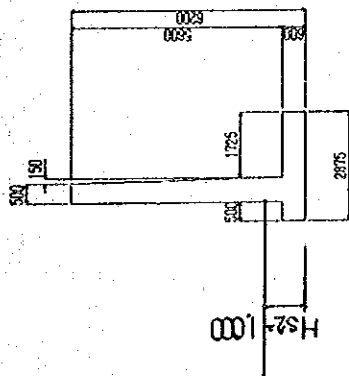
Retaining wall of NO 7 Boxcluvvert for road



BOTH EDGE

CALCULATION OF RETAINING WALLS
FOR ROAD STRUCTURE

(1) SHAPE AND SIZE



(2) Earth height and

Water level

HS2 = 1.000 (m)

HS1 = 0.000 (m)

(3) Each Factor

Unit volume weights KN
 for concrete $G_{MC} = 23.600 \text{ (t/m}^3\text{)}$
 for back fill $G_{M1} = 19.600 \text{ (t/m}^3\text{)}$
 " (underwater) $G_{M1S} = 10.780 \text{ (t/m}^3\text{)}$
 Internal friction angle $FA1 = 30.000 \text{ (}^\circ\text{)}$
 for above toe slab $G_{M2} = 18.600 \text{ (t/m}^3\text{)}$
 " (underwater) $G_{M2S} = 9.780 \text{ (t/m}^3\text{)}$
 for water $WATS = 9.800 \text{ (t/m}^3\text{)}$

For Foundation Ground
 Cohesive power $C = 0.000 \text{ (t/m}^2\text{)}$
 Friction factor $\tan \phi B = 0.600$
 Allowable Pressure $Q_a = 350.000 \text{ (t/m}^2\text{)}$

NOTE: THE DIMENSION (t) BE EXCHANG TO DIMENSION (KN) INTO

THIS CALCULATION

EARTH PRESSURE (COULOMB FORMULA)

EARTH PRESSURE COEFFICIENT: K_a

ϕ : ϕ_1 = 30.000 (°)
 δ : = 0.000 (°)
 β : 0.000 (°)
 θ : 0.000 (°)

$$K_a = \frac{\cos^2(\phi - \theta)}{\cos^2 \theta \cdot \cos(\theta + \delta) \cdot \left[1 + \sqrt{\frac{(\sin(\phi + \delta) \cdot \sin(\phi - \beta))}{(\cos(\theta + \delta) \cdot \cos(\theta - \beta))}} \right]^2}$$

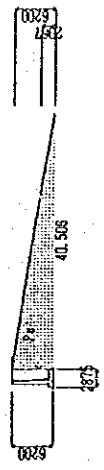
= 0.333

K_a = 0.333
 H = Structure High = 5.200 (m)
 GAM_1 = 19.600 (t/m³)
 $P = K_a \cdot \gamma_0 \cdot H = 2 \cdot C \cdot \sqrt{K_a} + K_a \cdot Q$
 $p_1 = 0.000$ (t/m²)
 $p_2 = 40.507$ (t/m²)

EARTH PRESSURE

$P = (p_1 + p_2) \cdot H / 2 = 125.571$ (t/m)
 $Ph = 125.571$ (t/m)
 $Pv = 0.000$ (t/m)

$y = 2.067$ (m)
 $x = 0.000$ (m)



CALCULATION OF WEIGHT OR FORCE

(1) CONCRETE

NO.	V(t)	H(t)	x(m)	y(m)	Mx(t·m)	My(t·m)
1	40.710	0.000	1.438	0.900	58.521	0.000
6	56.080	0.000	0.750	3.400	49.560	0.000
7	9.912	0.000	1.050	2.467	10.408	0.000
Σ	116.702	0.000			118.488	0.000

$V = \Sigma X_i \cdot Y_i \cdot \text{GAMC}$
 $Mx = V \cdot X$

$H = V \cdot KH1$
 $My = H \cdot y$

(2) BACK FILLING

NO.	V(t)	H(t)	x(m)	y(m)	Mx(t·m)	My(t·m)
2	8.232	0.000	1.100	4.333	9.055	0.000
3	189.336	0.000	2.013	3.400	381.039	0.000
Σ	197.568	0.000			390.094	0.000

$V = \Sigma X_i \cdot Y_i \cdot \text{GAM1}$
 $Mx = V \cdot X$

$H = V \cdot KH11$
 $My = H \cdot y$

(3) SURCHARGE OF JOE SLAB

NO.	V(t)	H(t)	x(m)	y(m)	Mx(t·m)	My(t·m)
2	3.720	0.000	0.250	0.000	0.930	0.000
Σ	3.720	0.000			0.930	0.000

$V = \Sigma X_i \cdot Y_i \cdot \text{GAM2}$
 $Mx = V \cdot X$

$H = V \cdot KH12$
 $My = H \cdot y$

(4) EARTH PRESSURE

	V(t)	H(t)	x(m)	y(m)	Mx(t·m)	My(t·m)
Σ	0.000	125.571	2.875	2.067	0.000	259.513

TOTAL OF ACTION FORCE FOR FOUNDATION EDGE

LOADS	V(t)	H(t)	Mx(t·m)	My(t·m)
$\Sigma 1$	116.702		118.488	
$\Sigma 2$	197.568		390.094	
$\Sigma 3$	3.720		0.930	
$\Sigma 4$	0.000	125.571	0.000	259.513
Total	317.990	125.571	509.512	259.513

$M_0 = \Sigma Mx - \Sigma My = 249.999 \text{ (t·m)}$

TOTAL FORCE FOR UNDER FOUNDATION CENTER

	V(t)	H(t)	e(m)	Mc(t·m)
	317.990	125.571	0.651	207.111

$e = B_0/2 - M_0/V \quad ; \quad M_c = V \cdot e$

B_0 : STRUCTURE WIDTH

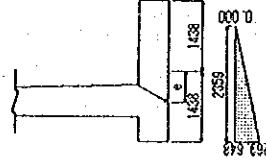
CALCULATION OF SECURITY OF DIRECTION FOUNDATION(SLS)

FOR CONTACT PRESSURE UNDER FOUNDATION.

B (m)	2.875
L (m)	1.000
V (t)	317.990
H (t)	125.571
Mc (t.m)	207.111
e (m)	0.651
X (m)	2.359
Q _{max} (t/m ²)	269.648
Q _{min} (t/m ²)	0.000
Q _a	29 4000

$Q = V/(B*L) + 6*Mc/(L*B*B)$

$Q = 2*V/(L*X) : X = 3*(B/2-Mc/V)$



FOR INVERSION

V(t)	Mc(t.m)	e(m)
317.990	207.111	0.651 > 0.479

$e = Mc/V$

FOR SLIDE

D(m)	V(t)	H(t)	Hu(t)	Fs
2.359	317.990	125.571	190.794	1.519 > 1.5

$C = 0.00 \text{ (t/m}^2\text{)} \quad \tan(\delta) = 0.60$

$Hu = C*D + V*\tan(\delta)$

$Fs = Hu/H$

A. for section 1)

1 calculation of stability

1) for S.L.S

load	N(KN)	H(KN)	MX(KNm)	Mg(KNm)
concrete of structure, surcharge of heel slab and toe slab	317.990	—	509.512	—
earth pressure	—	125.571	—	259.513
total	317.990	125.571	509.512	259.513

a) for inversion — U.L.S

$$F_{in} = \frac{509.512}{259.513 \times 1.50 \times 1.15} = 1.14 > 1.0$$

b) for sliding — S.L.S

$$F_{sl} = \frac{317.990 \times 0.60}{125.571} = 1.519 > 1.5$$

c) for pressure of bottom — S.L.S

$$X = \frac{509.512 - 259.513}{317.990} = 0.786 > \frac{B}{3} = \frac{2.875}{3} = 0.958 \text{ m}$$

$$< \frac{B}{6} = \frac{2.875}{6} = 0.480 \text{ m}$$

$$q_{max} = \frac{2 \times 317.990}{3 \times 0.786 \times 1.00} = 269.8 \text{ KN/m}^2 < q_a = 350 \text{ KN/m}^2$$

1 calculation of stability

2) for U.L.S

load	N(KN)	H(KN)	MX(KNm)	Mg(KNm)
concrete of structure, surcharge of heel slab and toe slab	$317.990 \times 1.2 \times 1.15$	—	$509.512 \times 1.2 \times 1.15$	—
earth pressure	—	$125.571 \times 1.5 \times 1.1 = 216.610$	—	$259.513 \times 1.5 \times 1.1 = 447.660$
total	438.827	216.610	703.126	447.660

a) for inersion

$$X = \frac{703.126 - 447.660}{438.827} = 0.582 \text{ m} > \frac{B}{3} = \frac{2.875}{3} = 0.958 \text{ m}$$

$$< \frac{B}{6} = \frac{2.875}{6} = 0.480 \text{ m}$$

$$F_{in} = \frac{509.512}{447.660} = 1.138 > 1.00 \quad \text{OK}$$

b) for sliding

$$F_{sl} = \frac{438.827 \times 0.60}{216.610} = 1.215 > 1.1$$

c) for pressure of bottom

$$q_{max} = \frac{2 \times 438.827}{3 \times 0.582 \times 1.00} = 502.7 \text{ KN/m}^2 < q_a = 525 \text{ KN/m}^2$$

2. calculation of each section

1) Vertical wall for U, L, S

a) bending moment and shearing force

$$M = \frac{1}{6} \times 19.6 \times 0.333 \times 5.60^3 \times 1.5 \times 1.15 = 329.6 \text{ KNm}$$

$$S = \frac{1}{2} \times 19.6 \times 0.333 \times 5.60^2 \times 1.5 \times 1.15 = 176.6 \text{ KN}$$

b) calculation of stress

$$b=100\text{cm} \quad h=65 \quad d=59.0 \quad d'=6.0$$

$$AS = Y20-150^{\text{CTC}} = 3.1416 / 0.15 = 20.944 \text{ cm}^2$$

$$P = \frac{20.944}{100 \times 59.0} \times 100 = 0.355\%$$

$$X = \frac{0.87 \times 41000 \times 20.944}{0.40 \times 2500 \times 100} = 7.4 \text{ cm}$$

$$Z = 59.0 - \frac{1}{2} \times 7.4 = 55.3 \text{ cm} < 0.95 \times 5.90 = 56.0 \text{ cm}$$

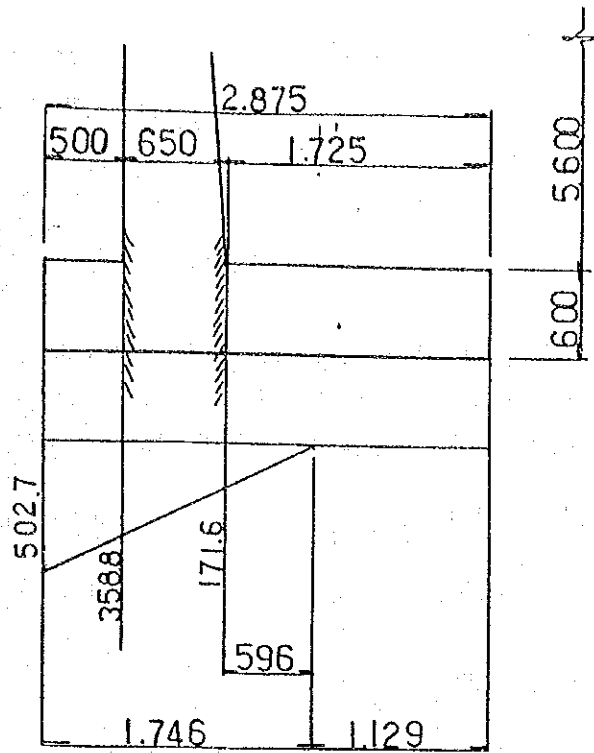
$$MRS = 0.87 \times 41000 \times 20.944 \times 55.3 \times 10^{-5} = 413.1 \text{ KNm} > 329.6 \text{ KNm}$$

$$MRC = 0.40 \times 2500 \times 100 \times 7.4 \times 55.3 \times 10^{-5} = 409.2 \text{ KNm} > 329.6 \text{ KNm}$$

$$\tau = \frac{176.6 \times 10^3}{100 \times 59.0} = 30.0 \text{ N/cm}^2 < \tau_a = 50 + 15 \frac{0.355 - 0.25}{0.25} = 56.3 \text{ cm}^2 \quad \text{OK}$$

2) Footing slab for U.L.S

a) load of surcharge



$$W1 = (23.6 \times 0.60 + 18.6 \times 0.40) \times 1.2 \times 1.15 = 19.8 \text{ KN/m}$$

$$W2 = (23.6 \times 0.60 + 19.6 \times 5.60) \times 1.2 \times 1.15 = 171.1 \text{ KN/m}$$

b) for toe footing slab

$$M = \frac{0.50^2}{6} (2 \times 502.7 + 358.8) - \frac{0.50^2}{2} \times 29.8 = 53.2 \text{ KNm}$$

$$S = \frac{0.50}{2} (502.7 + 358.8) 29.8 \times 0.500 = 200.15 \text{ KN}$$

c) for heel footing slab

$$M = \frac{1.725^2}{2} \times 171.1 - \frac{0.596^2}{6} \times 171.6 = 244.4 \text{ KNm}$$

$$S = 171.1 \times 1.725 - \frac{1}{2} \times 171.6 \times 0.596 = 44.1 \text{ KN}$$

d) calculation of stress

(1) for toe footing slab

$$b=100\text{cm} \quad h=60 \quad d=54.0 \quad d'=60$$

$$AS = Y20 - 150^{ctc} = 20.944 \text{ cm}^2$$

$$P = \frac{20.944}{100 \times 54.0} \times 100 = 0.388\%$$

$$X = \frac{0.87 \times 41000 \times 20.944}{0.40 \times 2500 \times 100} = 7.4 \text{ cm}$$

$$Z = 54.0 - \frac{1}{2} \times 7.4 = 50.3 \text{ cm} < 54.0 \times 0.95 = 51.3 \text{ cm}$$

$$MRS = 0.87 \times 41000 \times 20.944 \times 50.3 \times 10^{-5} = 375.8 \text{ KNm} > 53.2 \text{ KNm}$$

$$MRc = 0.40 \times 2500 \times 100 \times 7.4 \times 50.3 \times 10^{-5} = 372.2 \text{ KNm} > 53.2 \text{ KNm}$$

$$\tau = \frac{200.15 \times 10^3}{100 \times 54.0} = 37.2 \text{ N/cm}^2 < \tau_a = 50 + 15 \times \frac{(0.388 - 0.25)}{0.25} = 58.3 \text{ cm}^2$$

(2) for feel footing slab

$$b=100\text{cm} \quad h=60 \quad d=54.0 \quad d'=60$$

$$A_s = Y20-150^{c/c} = 20.944 \text{ cm}^2$$

$$P = \frac{20.944}{100 \times 54.0} \times 100 = 0.388\%$$

$$X = \frac{0.87 \times 41000 \times 20.944}{0.40 \times 2500 \times 100} = 7.4 \text{ cm}$$

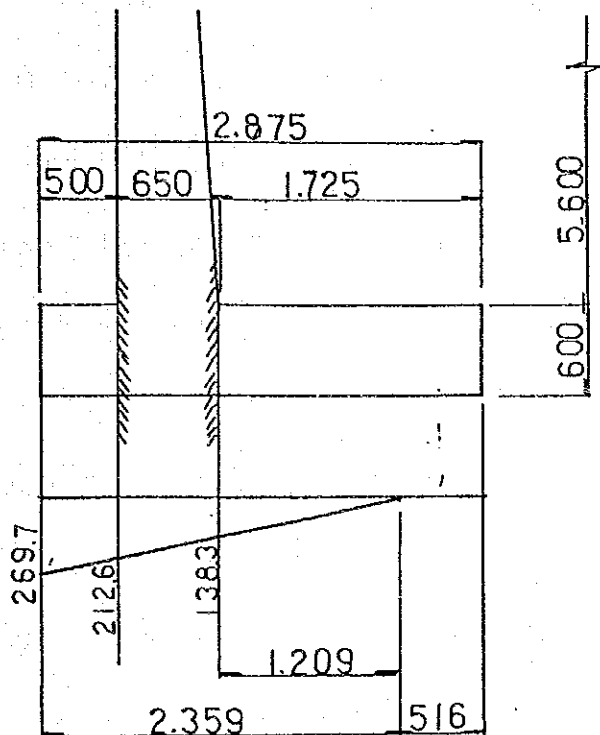
$$Z = 54.0 - \frac{1}{2} \times 7.4 = 50.3 \text{ cm} < 0.95 \times 54.0 = 51.3 \text{ cm} \quad \text{OK}$$

$$M_{RS} = 0.87 \times 41000 \times 20.944 \times 50.3 \times 10^{-5} = 375.8 \text{ KNm} > 244.1 \text{ KNm}$$

$$M_{Rc} = 0.40 \times 2500 \times 100 \times 7.4 \times 50.3 \times 10^{-5} = 372.2 \text{ KNm} > 244.1 \text{ KNm} \quad \text{OK}$$

$$\tau = \frac{244.1 \times 10^3}{100 \times 54.0} = 45.2 \text{ N/cm}^2 < \tau_a = 50 + 15 \times \frac{(0.388 - 0.25)}{0.25} = 58.3 \text{ cm}^2 \quad \text{OK}$$

3) footing slab for S, L, S



a) load of surcharge

$$W1 = 23.6 \times 0.6 + 18.6 \times 0.40 = 21.600 \text{ KN/m}$$

$$W2 = 23.6 \times 0.6 + 19.6 \times 5.60 = 123.920 \text{ KN/m}$$

b) for toe footing slab

$$M = \frac{0.50^2}{6} (2 \times 269.7 + 212.6) - \frac{0.50^2}{2} \times 21.60 = 28.7 \text{ KN}$$

$$S = \frac{0.50^2}{2} (289.7 + 212.6) - 21.60 \times 0.50 = 109.8 \text{ KN}$$

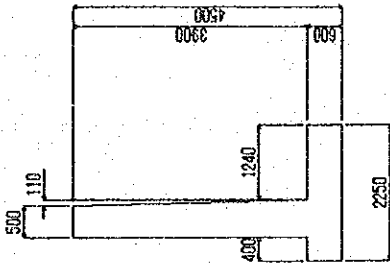
c) for heel footing slab

$$M = \frac{1.725^2}{2} \times 123.920 - \frac{1.209^2}{6} \times 138.3 = 150.7 \text{ KNm}$$

$$S = 123.920 \times 1.725 - \frac{1}{2} \times 138.3 \times 1.209 = 130.2 \text{ KN}$$

note: this case is abridge

(1)



(2)

GAMC = 23.600 (t/m³)
 GAM1 = 19.600 (t/m³)
 GAM1S = 10.780 (t/m³)
 FAI = 30.000 (°)
 GAM2 = 18.600 (t/m³)
 GAM2S = 9.780 (t/m³)
 WATS = 9.800 (t/m³)

C = 0.000 (t/m²)
 tanφB = 0.600
 Qa = 29.400 (t/m²)

β = 0.000 (°)

HS2 = 1.000 (m)

HW1 = 0.000 (m)

0.333
 0.000 (°)
 0.000 (°)
 4.500 (m)
 19.600 (t/m³)
 0.000 (t/m²)
 0.000 (t/m²)

$$p = K_a \gamma_o H - 2C \sqrt{K_a} + K_a Q$$

$$p_1 = 0.000 \text{ (t/m}^2\text{)}$$

$$p_2 = 29.400 \text{ (t/m}^2\text{)}$$

$$P = (p_1 + p_2) * H / 2 = 66.150 \text{ (t/m)}$$

$$P_h = 66.150 \text{ (t/m)}$$

$$P_v = 0.000 \text{ (t/m)}$$

$$y = 1.500 \text{ (m)}$$

$$x = 0.000 \text{ (m)}$$

$$30.000 \text{ (}^\circ\text{)}$$

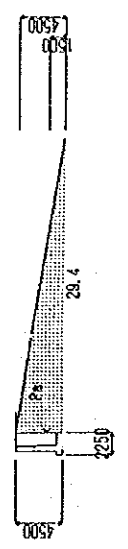
$$= 0.000 \text{ (}^\circ\text{)}$$

$$0.000 \text{ (}^\circ\text{)}$$

$$0.000 \text{ (}^\circ\text{)}$$

$$K_a = \frac{\cos^2(\phi - \theta)}{\cos^2 \theta * \cos(\theta + \delta) * \left[1 + \frac{(\sin(\phi + \delta) * \sin(\phi - \beta))}{(\cos(\theta + \delta) * \cos(\theta - \beta))} \right]^2}$$

$$= 0.333$$



(4)

	V(t)	H(t)	x(m)	y(m)	Mx(t·m)	My(t·m)
	0.000	66.150	2.250	1.500	0.000	99.225

	V(t)	H(t)	Mx(t·m)	My(t·m)
	82.942		70.497	
	98.990		158.593	
	2.976		0.595	
	0.000	66.150	0.000	99.225
	184.908	66.150	229.685	99.225

$M_0 = \sum Mx - \sum My = 130.460 \text{ (t·m)}$

	V(t)	H(t)	e(m)	Mc(t·m)
2	184.908	66.150	0.419	77.562

$e = B_0/2 - M_0/V$; $M_c = V * e$

$B_0 :$

(1)

NO.	V(t)	H(t)	x(m)	y(m)	Mx(t·m)	My(t·m)
1	31.860	0.000	1.125	0.300	35.843	0.000
6	46.020	0.000	0.650	2.550	29.913	0.000
7	5.062	0.000	0.937	1.900	4.742	0.000
	82.942	0.000			70.497	0.000

$V = X_1 * Y_1 * GAMC$; $H = V * KII1$
 $Mx = V * x$; $My = H * y$

(2)

NO.	V(t)	H(t)	x(m)	y(m)	Mx(t·m)	My(t·m)
2	4.204	0.000	0.978	3.200	4.092	0.000
3	94.786	0.000	1.630	2.550	154.501	0.000
	98.990	0.000			158.593	0.000

$V = X_1 * Y_1 * GAM1$; $H = V * KII1$
 $Mx = V * x$; $My = H * y$

(3)

NO.	V(t)	H(t)	x(m)	y(m)	Mx(t·m)	My(t·m)
2	2.976	0.000	0.200	0.000	0.595	0.000
	2.976	0.000			0.595	0.000

$V = X_1 * Y_1 * GAM2$; $H = V * KII2$
 $Mx = V * x$; $My = H * y$

V(t)	Mc(t-m)	e(m)
184.908	77.562	0.419 > 0.375

$$e = Mc/V$$

D(m)	V(t)	H(t)	Hu(t)	Fs
2.117	184.908	66.150	110.945	1.677 > 1.5

$$C = 0.00 \text{ (t/m}^2\text{)} \quad \tan(\delta) = 0.60$$

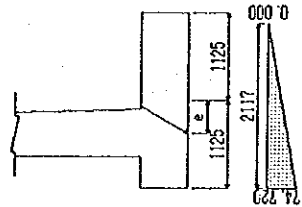
$$Hu = C \cdot D + V \cdot \tan(\delta)$$

$$Fs = Hu/H$$

常 時	
B (m)	2.250
L (m)	1.000
V (t)	184.908
H (t)	66.150
Mc (t-m)	77.562
e (m)	0.419
X (m)	2.117
Qmax(t/m ²)	174.720
Qmin(t/m ²)	0.000
	29.400

$$Q = V/(B \cdot L) + 6 \cdot Mc/(L \cdot B \cdot B)$$

$$Q = 2 \cdot V/(L \cdot X) : X = 3 \cdot (B/2 - Mc/V)$$



B. for section 2)

1. calculation of stability

2) for U, L, S

load	N(KN)	H(KN)	MX(KNm)	Mg(KNm)
concrete of structure, surcharge of heel slab and toe slab	$184.908 \times 1.2 \times 1.15 = 255.2$	—	$229.685 \times 1.2 \times 1.15 = 317.0$	—
earth pressure	—	$66.150 \times 1.5 \times 1.10 = 114.1$	—	$99.225 \times 1.5 \times 1.10 = 171.2$
total	255.2	114.1	317.0	171.2

a) for inversion

$$F_{in} = \frac{229.685}{171.2} = 1.34 > 1.00 \quad \text{OK}$$

b) for sliding

$$F_s = \frac{255.2 \times 0.6}{114.1} = 1.3 > 1.1$$

c) for pressure of bottom

$$X = \frac{317.0 - 171.2}{255.2} = 0.571 \text{ m} < \frac{2.250}{3} = 0.750 \text{ m}$$

$$< \frac{4.250}{6} = 0.375 \text{ m}$$

$$q = \frac{2 \times 255.2}{3 \times 0.571 \times 1.00} = 298.0 \text{ kN/m}^2$$

2. calculation of each section (U, L, S)

1) vertical wall

a) bending moment and shearing force

$$M = \frac{1}{6} \times 19.6 \times 0.333 \times 3.90^3 \times 1.5 \times 1.15 = 111.3 \text{ KNm}$$

$$S = \frac{1}{2} \times 19.6 \times 0.333 \times 3.90^2 \times 1.5 \times 1.15 = 85.7 \text{ KN}$$

b) calculation of stress

$$b=100\text{cm} \quad h=61 \quad d=55.0 \quad d'=6.0$$

$$AS = Y20 - 300^{ctc} = 3.1416 / 0.30 = 10.472\text{cm}^2$$

$$P = \frac{10.472}{100 \times 55.0} \times 100 = 0.190\% > 0.15\%$$

$$X = \frac{0.87 \times 41000 \times 10.472}{0.40 \times 2500 \times 100} = 5.6 \text{ cm}$$

$$Z = 55.0 - \frac{1}{2} \times 5.6 = 52.2 \text{ cm} = 0.95 \times 5.40 = 52.2 \text{ cm}$$

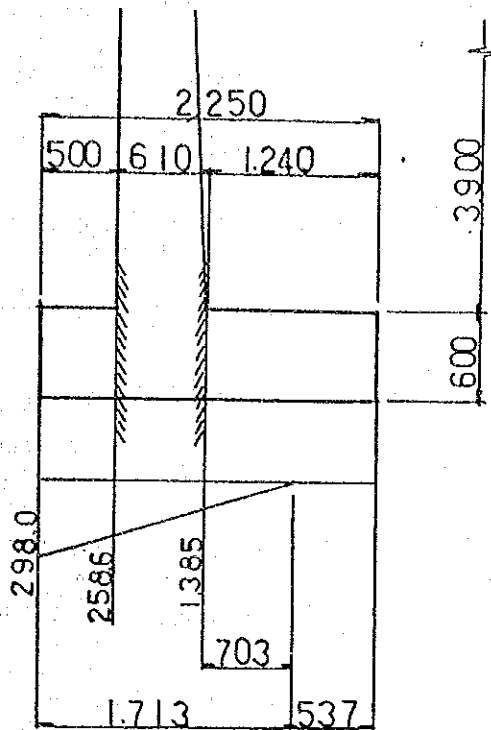
$$MRS = 0.87 \times 41000 \times 10.472 \times 52.2 \times 10^{-6} = 195.0 \text{ KNm} > 111.3 \text{ KNm}$$

$$MRc = 0.40 \times 2500 \times 100 \times 5.6 \times 52.2 \times 10^{-5} = 292.3 \text{ KNm} > 111.3 \text{ KNm}$$

$$\tau = \frac{85.7 \times 10^3}{100 \times 55.0} = 15.6 \text{ N/cm}^2 = \tau_a = 35.0 \times \frac{0.19}{0.25} = 26.6 \text{ N/cm}^2$$

2) footing slab

a) load of surcharge



$$W1 = (23.6 \times 0.60 + 18.6 \times 0.40) \times 1.20 \times 1.15 = 29.8 \text{ KN/m}$$

$$W2 = (23.6 \times 0.60 + 19.6 \times 3.90) \times 1.20 \times 1.15 = 125.1 \text{ KN/m}$$

b) for toe footing slab

$$M = \frac{0.40^2}{6} (2 \times 298.0 + 258.6) - \frac{0.40^2}{2} \times 29.8 = 20.4 \text{ KN/m}$$

$$S = \frac{0.40}{2} (298.0 + 258.6) - 29.8 \times 0.40 = 99.4 \text{ KN}$$

c) for heel footing slab

$$M = \frac{1.24^2}{2} \times 125.1 - \frac{0.703^2}{6} \times 138.5 = 84.8 \text{ KN/m}$$

$$S = 125.1 \times 1.24 - \frac{1}{2} \times 138.5 \times 0.703 = 106.5 \text{ KN}$$

d) calculation of stress

(1) for toe footing slab

$$b=100 \quad h=60 \quad d=54.0 \quad d' = 6.0$$

$$\tau = \frac{99.4 \times 10^3}{100 \times 54.0} = 18.4 \text{ N/cm}^2 < \tau_a = 27.2 \text{ N/cm}^2$$

$$A_s = Y20-300^{ctc} = 10.472 \text{ cm}^2$$

$$P = \frac{10.472}{100 \times 54.0} \times 100 = 0.194\% > 0.15\%$$

$$\tau_a = 35.0 \times \frac{0.194}{0.25} = 27.2 \text{ N/cm}^2$$

(2) for heel footing slab

$$b=100\text{cm} \quad h=60 \quad d=54.0 \quad d'=6.0$$

$$A_s = Y20-300^{ctc} = 10.472$$

$$P = \frac{10.472}{100 \times 54.0} \times 100 = 0.194\% > 0.15\%$$

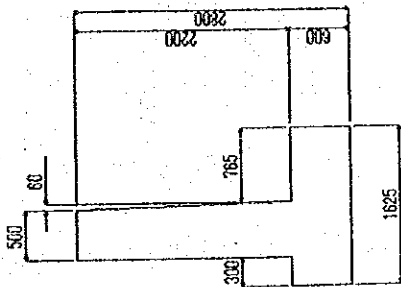
$$X = \frac{0.87 \times 41000 \times 10.472}{0.40 \times 2500 \times 100} = 5.4 \text{ cm}$$

$$Z = 54.0 - \frac{1}{2} \times 5.4 = 51.3 \text{ cm} = 0.95 \times 54.0 = 51.3 \text{ cm}^2$$

$$MRS = 0.87 \times 41000 \times 10.472 \times 51.3 \times 10^5 = 191.6 \text{ KNm} > 84.8 \text{ KNm}$$

$$MRC = 0.40 \times 2500 \times 100 \times 5.4 \times 51.3 \times 10^5 = 277.0 \text{ KNm} > 84.8 \text{ KNm} \quad \text{OK}$$

$$\tau = \frac{106.5 \times 10^3}{100 \times 54.4} = 19.8 \text{ N/cm}^2 < \tau_a = 35.0 \times \frac{0.194}{0.25} = 27.2 \text{ N/cm}^2$$



GAMC = 23.500 (t/m³)
 GAM1 = 19.600 (t/m³)
 GAMIS = 10.780 (t/m³)
 FAI = 30.000 (°)
 GAM2 = 18.600 (t/m³)
 GAM2S = 9.780 (t/m³)
 WATS = 9.800 (t/m³)

HS2 = 1.000 (m)
 HW1 = 0.000 (m)

C = 0.000 (t/m²)
 tan φB = 0.600
 Qa = 29.400 (t/m²)

$\phi = 30.000 (^{\circ})$
 $\delta = 0.000 (^{\circ})$
 $\beta = 0.000 (^{\circ})$
 $\theta = 0.000 (^{\circ})$

$$K_a = \frac{\cos^2(\phi - \theta)}{\cos^2 \theta \cdot \cos(\theta + \delta) \cdot \left[1 + \sqrt{\frac{(\sin(\phi + \delta) \cdot \sin(\phi - \beta))}{(\cos(\theta + \delta) \cdot \cos(\theta - \beta))}} \right]^2}$$

= 0.333

0.333
 0.000 ($^{\circ}$)
 0.000 ($^{\circ}$)
 2.800 (m)
 19.600 (t/m^2)
 0.000 (t/m^2)
 0.000 (t/m^2)

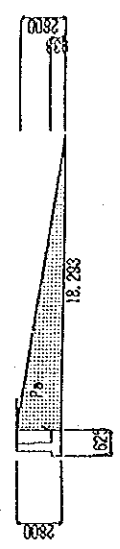
$$p = K_a \cdot \gamma \cdot 0 \cdot H - 2 \cdot C \cdot \sqrt{K_a} + K_a \cdot Q$$

$p_1 = 0.000 (t/m^2)$
 $p_2 = 18.293 (t/m^2)$

$$P = (p_1 + p_2) \cdot H / 2 = 25.611 (t/m)$$

$P_h = 25.611 (t/m)$
 $P_v = 0.000 (t/m)$

$y = 0.933 (m)$
 $x = 0.000 (m)$



(1)

NO.	V(t)	H(t)	x(m)	y(m)	Mx(t·m)	My(t·m)
1	23.010	0.000	0.813	0.300	18.596	0.000
6	25.960	0.000	0.550	1.700	14.278	0.000
7	1.558	0.000	0.820	1.333	1.277	0.000
	50.528	0.000			34.251	0.000

V = Xi*Yi*GAMC
 Mx = V*x

H = V*KH1
 My = H*y

(2)

NO.	V(t)	H(t)	x(m)	y(m)	Mx(t·m)	My(t·m)
2	1.294	0.000	0.840	2.067	1.087	0.000
3	32.987	0.000	1.249	1.700	40.986	0.000
	34.280	0.000			42.073	0.000

V = Xi*Yi*GAM1
 Mx = V*x

H = V*KH1
 My = H*y

(3)

NO.	V(t)	H(t)	x(m)	y(m)	Mx(t·m)	My(t·m)
2	2.232	0.000	0.150	0.000	0.335	0.000
	2.232	0.000			0.335	0.000

V = Xi*Yi*GAM2
 Mx = V*x

H = V*KH2
 My = H*y

(4)

	V(t)	H(t)	x(m)	y(m)	Mx(t·m)	My(t·m)
	0.000	25.611	1.625	0.933	0.000	23.903

	V(t)	H(t)	Mx(t·m)	My(t·m)
	50.528		34.251	
	34.280		42.073	
	2.232		0.335	
	0.000	25.611	0.000	23.903
	87.040	25.611	76.658	23.903

Mo = ΣMx - ΣMy = 52.755 (t·m)

	V(t)	H(t)	e(m)	Mc(t·m)
2	87.040	25.611	0.206	17.965

e = B0/2 - Mo/V : Mc = V * e

V(t)	Mc(t·m)	e(m)
87.040	17.965	0.206 < 0.271

$$e = Mc/V$$

D(m)	V(t)	H(t)	Hu(t)	Fs
1.625	87.040	25.611	52.224	2.039 > 1.5

$$C = 0.00 \text{ (t/m}^2\text{)} \quad \tan(\delta) = 0.60$$

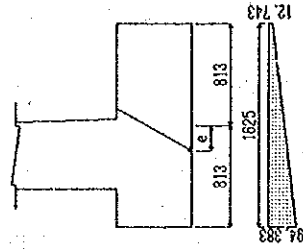
$$Hu = C \cdot D + V \cdot \tan(\delta)$$

$$Fs = Hu/H$$

B (m)	1.625
L (m)	1.000
V (t)	87.040
H (t)	25.611
Mc (t·m)	17.965
e (m)	0.206
X (m)	1.625
Qmax(t/m ²)	94.383
Qmin(t/m ²)	12.743
	29.400

$$Q = V/(B \cdot L) + 6 \cdot Mc/(L \cdot B \cdot B)$$

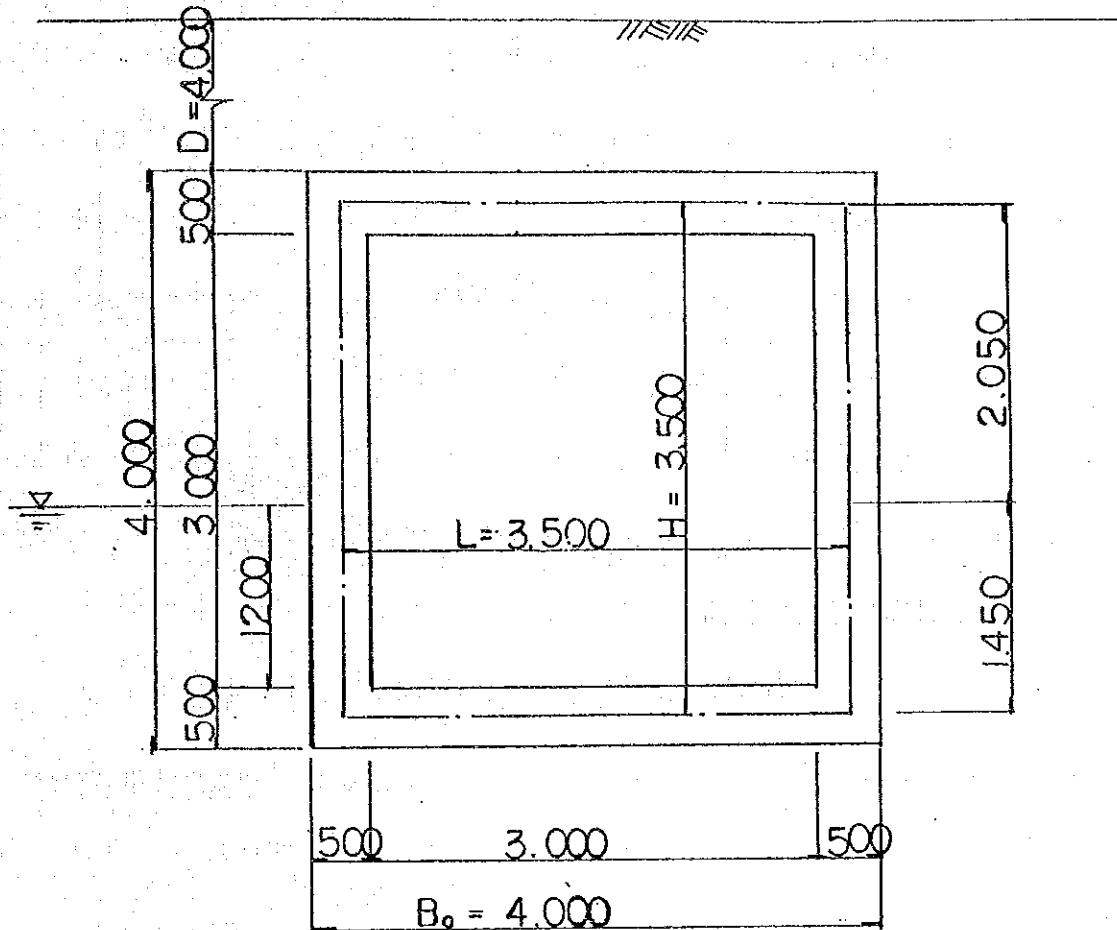
$$Q = 2 \cdot V/(L \cdot X) ; X = 3 \cdot (B/2 - Mc/V)$$



WATER BOX CULVERTS

NO Ø BOX CULVERT FOR DRAINAGE

1) Shape and Size



Where ... D^m = depth of asphalt and
similar surface soil.

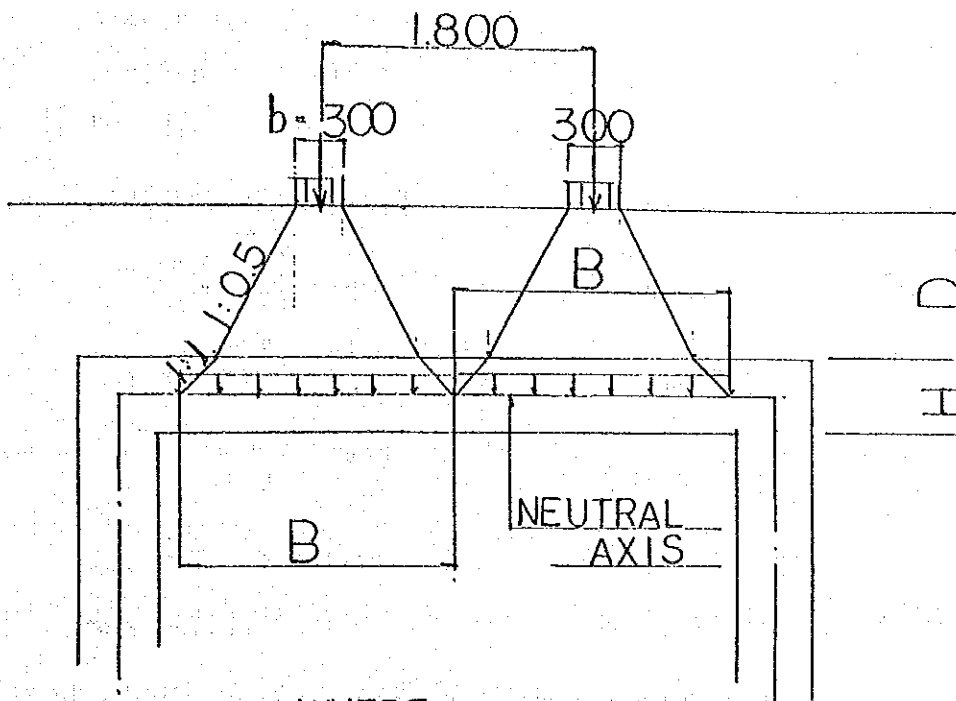
2) Factor of section

$$A = 1.00 \times 0.50 = 0.5000 \text{ m}^2$$

$$I = \frac{1.00 \times 0.50^3}{12} = 0.01041 \text{ m}^4$$

$$EC = 25 \text{ kN/mm}^2 = 25 \times 10^7 \text{ kN/m}^2$$

LIVE LOAD --- HB loading



WHERE

D = DEPTH OF ASPHALT AND
SIMILAR SURFACE SOIL

H = DEPTH OF CONCRTE SLAB

DISPERSAL OF WHEEL

$$B^m = b + D + H$$

LOADED STRENGTH

$$P = \frac{100.0 \times U_{no}}{B \times L} \quad (\text{KN/m}^2)$$

WHERE

U_{no} = NUMBER OF UNITS = 30

L = WIDTH OF HB-VEHICLE = 3.500^m

No. ① BOX CULVERT FOR DRAINAGE

1. calculation for bending moment (U.L.S)

section $b=100\text{cm}$ $h=50$ $d=44.0$ $d'=6.0$

1) For upper slab

a) intersection point ②=③ $M_{u,\min} = -133.9\text{KNm}$

$$A_s = \left[\begin{array}{l} Y_{12} - 300\text{ctc} = 1.131/0.300 \\ Y_{16} - 300\text{ctc} = 2.011/0.300 \end{array} \right] = 10.47\text{ cm}^2$$

$$X = \frac{0.87 \times 41000 \times 10.47}{0.40 \times 2500 \times 100} \doteq 4.0\text{cm}$$

$$Z = 44.0 - \frac{4.0}{2} = 42.0\text{cm} \doteq 41.8\text{cm} \doteq 0.95 \times 44.0 = 41.8\text{cm} \quad \text{OK}$$

$$M_{RS} = 0.87 \times 41000 \times 10.47 \times 41.8 \times 10^{-5} = 156.1\text{KNm} > M_u = 133.9\text{KNm}$$

$$M_{RC} = 0.40 \times 2500 \times 100 \times 4.0 \times 41.8 \times 10^{-5} = 167.2\text{KNm} > M_u = 133.9\text{KNm} \quad \text{OK}$$

b) middle point ②~③ $M_{u,\max} = 135.1\text{KNm}$

$$M_R = 156.1\text{KNm} > M_u = 135.1\text{KNm}$$

(Where: M_R : From calculation of point ②)

2) For bottom slab

a) intersection point ④=① $M_{u,\min} = -160.9\text{KNm}$

$$A_s = Y_{16} - 150\text{ctc} = 2.011/0.150 = 13.41\text{ cm}^2$$

$$X = \frac{0.87 \times 41000 \times 13.41}{0.40 \times 2500 \times 100} \doteq 4.8\text{m}$$

$$Z = 44.0 - \frac{4.8}{2} = 41.6\text{cm} < 0.95 \times 44.0 = 41.8\text{cm} \quad \text{OK}$$

$$M_{RS} = 0.87 \times 41000 \times 13.41 \times 41.6 \times 10^{-5} = 199.0\text{KNm} > M_u = 160.9\text{KNm}$$

$$M_{RC} = 0.40 \times 2500 \times 100 \times 4.8 \times 41.6 \times 10^{-5} = 199.0\text{KNm} > M_u = 160.9\text{KNm} \quad \text{OK}$$

b) middle point ④~① $M_{u,\max} = -157.9\text{KNm}$

$$M_R = 199.0\text{KNm} > M_u = 157.9\text{KNm}$$

(Where: M_R : From calculation of point ④)

2. calculation for shearing force (U.L.S)

section $b=100\text{cm}$ $h=50$ $d=44.0$ $d'=6.0$

a) For upper slab

intersection point ②=③ $S_{u,\max} = 123.0\text{KN}$

$$A_s = \left(\begin{array}{l} Y_{12} - 300^{ctc} = 1.131/0.300 \\ Y_{16} - 300^{ctc} = 2.011/0.300 \end{array} \right) = 10.47 \text{ cm}^2$$

$$P = \frac{10.47}{100 \times 44.0} \times 100 = 0.238 \%$$

$$V_c = \frac{123.0 \times 10^3}{100 \times 44.0} = 28.0 \text{ N/cm}^2$$

$$< V_{ca} = 35.0 \times \frac{0.238}{0.250} = 33.3 \text{ N/cm}^2 \quad \text{OK}$$

b) For bottom slab

intersection point ④ = ① $S_u.\text{max} = 145.8 \text{ kN}$

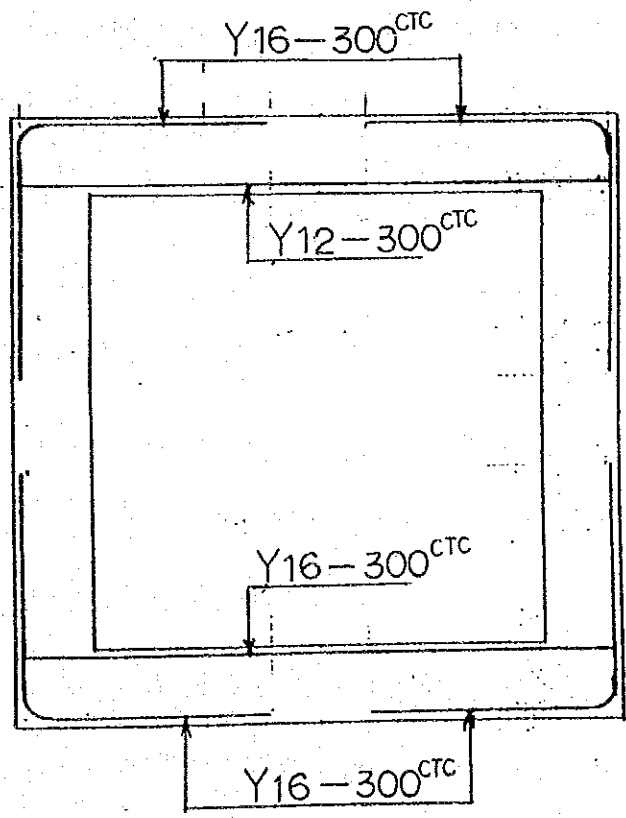
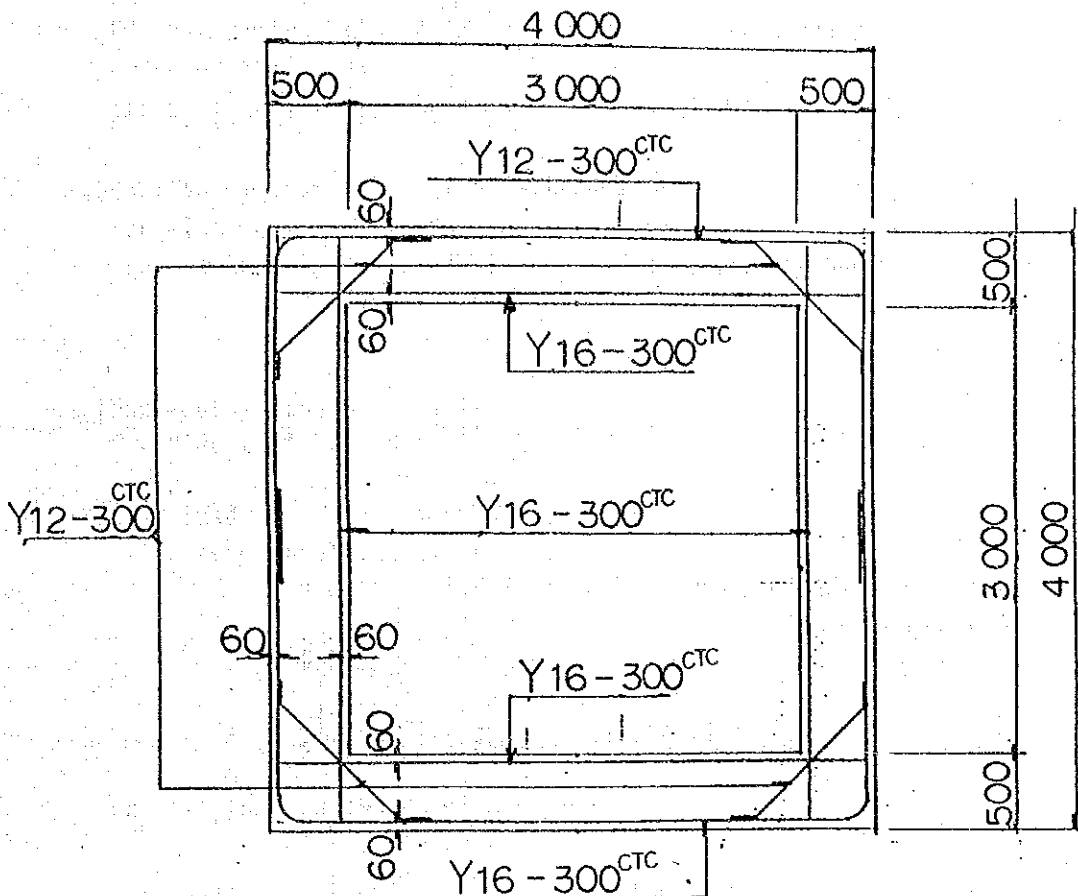
$$A_s = Y_{16} - 150^{ctc} = 13.41 \text{ cm}^2$$

$$P = \frac{13.41}{100 \times 44.0} \times 100 = 0.305 \%$$

$$V_c = \frac{145.8 \times 10^3}{100 \times 44.0} = 33.2 \text{ N/cm}^2$$

$$< V_{ca} = 35.0 + \frac{15}{0.25} (0.305 - 0.25) = 38.3 \text{ N/cm}^2 \quad \text{OK}$$

NO ① BOX CULVERT FOR DRAINAGE



NO ① BOX FOR DRAINAGE

Load

(1) Dead load

a) Vertical load Where $\alpha = 1.0$ (earth pressure factor of vertical) $\therefore \frac{D}{B_0} = 1.00$

For upper slab $w_1 = 22.6 \times 0.50 + 19.6 \times 3.50 + 23.60 \times 0.50 = 91.700 \text{ kN/m}$

For side wall $w_2 = 23.6 \times 0.50 = 11.800 \text{ ''}$

For bottom slab $w_3 = 91.700 + \frac{2 \times 11.800 \times 3.50}{3.50} = 115.300 \text{ ''}$

b) Horizontal load ----- earth pressure

For side wall $P_1 = (22.6 \times 0.50 + 19.6 \times 3.75) \times 0.500 = 42.400 \text{ kN/m}$

'' $P_2 = (22.6 \times 0.50 + 19.6 \times 5.80) \times 0.500 = 62.490 \text{ ''}$

'' $P_3 = (22.6 \times 0.50 + 19.6 \times 5.80 + 10.8 \times 14.5) \times 0.500 = 70.320 \text{ ''}$

c) Horizontal load water Pressure

For side wall $P_w = 9.80 \times 1.45 = 14.210 \text{ kN/m}$

(2) Live load

live load surcharge of axle

$$P = \frac{\text{KN/axle} \times \text{unite}}{3.50 \times B} \quad \text{width of despersal of wheel} \\ B = 0.300 + 4.00 + 0.500 = 4.80 \text{ m}$$

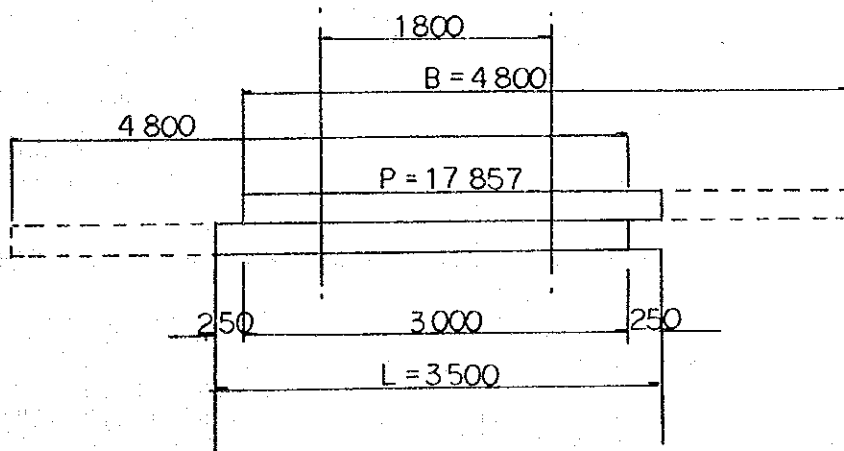
$$= \frac{10 \times 30}{3.50 \times 4.80} = 17.857 \text{ KN/m}^2$$

or live load surcharge of a vehicle

$$g_0 = \frac{\text{kN/vehicle} \times \text{unit}}{3.50 \times 10.0} = 34.300 \text{ KN/m}^2 < 2P = 35.714 \text{ KN/m}^2$$

OF course the loaded of live load is consider as following

case-1 Vaertical load



For bottom slab

$$P_1 = P_2 = \frac{2 \times 17.857 \times 3.25}{3.500} = 33.163 \text{ kN/m} < 34.300 \text{ kN/m}$$

case-2 Horizontal load eath pressure of live load surcharge

For side wall: $p_e = g_0 \cdot k_0 = 34.300 \times 0.500 = 17.150 \text{ KN/m}$

BOX FOR DRAINAGE-NO 1 Depth= 4.000

COORDINATES

No	X (m)	Y (m)
1	0.0000	0.0000
2	0.0000	3.5000
3	3.5000	3.5000
4	3.5000	0.0000

Where

NO : Each intersecting points.
X,Y : Abscissa and Ordinate

CONDITION OF MEMBER

No	I	J	A (m ²)	I (m ⁴)	I - J	L (m)	E (t/m ²)	EPS
1	1	2	0.50000	0.010417	Fix - Fix	3.500	2.50E+07	1.00E-05
2	2	3	0.50000	0.010417	Fix - Fix	3.500	2.50E+07	1.00E-05
3	3	4	0.50000	0.010417	Fix - Fix	3.500	2.50E+07	1.00E-05
4	4	1	0.50000	0.010417	Fix - Fix	3.500	2.50E+07	1.00E-05

CONDITION OF FULCRUM

No	kN ↑ X (t/m)	kN ↓ Y (t/m)	kN ↑ M (tm/Rad)
1	Fix	Fix	Free
4	Free	Fix	Free

CALCULATION POINTS

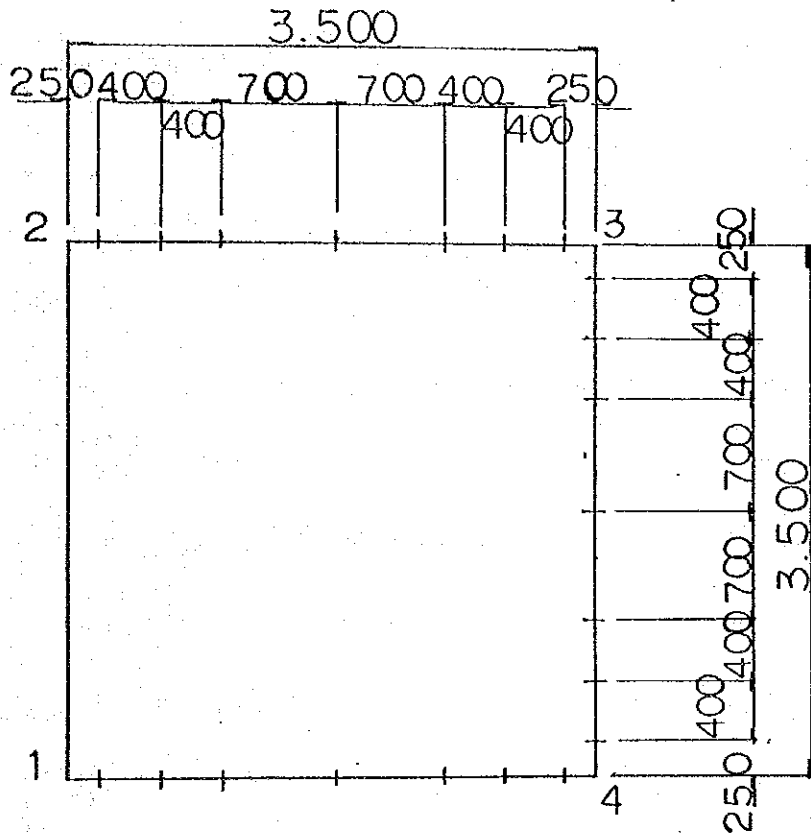
NO	no	L-No 1	L-No 2	L-No 3	L-No 4	L-No 5	L-No 6	L-No 7
		11	12	13	14	15	16	17
		m						
1	7	0.250	0.650	1.050	1.750	2.450	2.850	3.250
2	7	0.250	0.650	1.050	1.750	2.450	2.850	3.250
3	7	0.250	0.650	1.050	1.750	2.450	2.850	3.250
4	7	0.250	0.650	1.050	1.750	2.450	2.850	3.250

NOTE : THE DIMENSION (t) BE EXCHANG TO

DIMENSION (kN) INTO THIS CALCULATION.

CALCULATION POINTS

OF EACH FORCE



BOX FOR DRAINAGE-NO 1

LOAD
LOAD CASE No. : Dead load
: 1

No	i - j		Li (m)	Lo (m)	$\overset{\text{KN}}{\uparrow}$ Pi (t/m)	$\overset{\text{KN}}{\uparrow}$ Pj (t/m)
1	1- 2	Y	0.000	3.500	-11.800	-11.800
3	3- 4	Y	0.000	3.500	-11.800	-11.800
2	2- 3	Y	0.000	3.500	-91.700	-91.700
4	4- 1	Y	0.000	3.500	115.300	115.300
$\Sigma V =$			0.000 (t)			
$\Sigma H =$			0.000 (t)			

BOX FOR DRAINAGE-NO 1

No. : Earth pressure load
: 2

No	i - j		Li (m)	Lo (m)	$\overset{\text{KN}}{\uparrow}$ Pi (t/m)	$\overset{\text{KN}}{\uparrow}$ Pj (t/m)
1	1- 2	X	0.000	1.450	70.320	62.490
1	1- 2	X	1.450	2.050	62.490	42.400
3	3- 4	X	0.000	2.050	-42.400	-62.490
3	3- 4	X	2.050	1.450	-62.490	-70.320
$\Sigma V =$			0.000 (t)			
$\Sigma H =$			0.000 (t)			

BOX FOR DRAINAGE-NO 1

No. : Water pressure load
: 3

No	i - j		Li (m)	Lo (m)	$\overset{\text{KN}}{\uparrow}$ Pi (t/m)	$\overset{\text{KN}}{\uparrow}$ Pj (t/m)
1	1- 2	X	0.000	1.450	14.210	0.000
3	3- 4	X	2.050	1.450	0.000	-14.210
$\Sigma V =$			0.000 (t)			
$\Sigma H =$			0.000 (t)			

BOX FOR DRAINAGE-NO 1

: HB live load-VL-

LOAD CASE No. : 4

No	i - j	Li (m)	Lo (m)	Pi (t/m)	Pj (t/m)
2	2-3	0.000	3.500	-34.300	-34.300
4	4-1	0.000	3.500	34.300	34.300

$\Sigma V = 0.000$ (t)
 $\Sigma H = 0.000$ (t)

BOX FOR DRAINAGE-NO 1

: HB live load-HL-

No. : 5

No	i - j	Li (m)	Lo (m)	Pi (t/m)	Pj (t/m)
1	1-2	0.000	3.500	17.150	17.150
3	3-4	0.000	3.500	-17.150	-17.150

$\Sigma V = 0.000$ (t)
 $\Sigma H = 0.000$ (t)

BOX FOR DRAINAGE-NO 1

COMBINATION (ULS)

No	C-No 1	C-No 2
No	No 6	No 7

<u>CASE OF</u>	No 1	1.3800	1.3800
<u>CALCULATION</u>	No 2	1.6500	1.6500
<u>AND LOAD</u>	No 3	0.0000	1.6500
<u>FACTOR</u>	No 4	1.4300	0.0000
	No 5	0.0000	1.6500

SELECTED CASE FOR MAX OR MIN FORCE

No 1 : 6.7

DEFLECTION

No.	Case. 1			Case. 2			Case. 3		
	X-DIS.(mm)	Y-DIS.(mm)	ROTA.(mmRad)	X-DIS.(mm)	Y-DIS.(mm)	ROTA.(mmRad)	X-DIS.(mm)	Y-DIS.(mm)	ROTA.(mmRad)
1.	0.00000	0.00000	3.75538	0.00000	0.00000	-2.05728	0.00000	0.00000	-0.0841
2.	-0.01438	-0.50715	-3.34449	-0.02439	0.00000	1.96817	-0.01086	0.00000	0.0485
3.	0.00000	-0.50715	3.34449	-0.28532	0.00000	-1.96817	-0.01442	0.00000	-0.0485
4.	-0.01438	0.00000	-3.75538	-0.30970	0.00000	2.05728	-0.02529	0.00000	0.0841

No.	Case. 4			Case. 5			Case. 6		
	X-DIS.(mm)	Y-DIS.(mm)	ROTA.(mmRad)	X-DIS.(mm)	Y-DIS.(mm)	ROTA.(mmRad)	X-DIS.(mm)	Y-DIS.(mm)	ROTA.(mmRad)
1.	0.00000	0.00000	1.17645	0.00000	0.00000	-0.58823	0.00000	0.00000	3.4703
2.	0.00000	-0.16807	-1.17645	0.00000	0.00000	0.58823	-0.06008	-0.94021	-3.0503
3.	0.00000	-0.16807	1.17645	-0.08404	0.00000	-0.58823	-0.47078	-0.94021	3.0503
4.	0.00000	0.00000	-1.17645	-0.08404	0.00000	0.58823	-0.53086	0.00000	-3.4703

No.	Case. 7		
	X-DIS.(mm)	Y-DIS.(mm)	ROTA.(mmRad)
1.	0.00000	0.00000	0.67852
2.	-0.07801	-0.69987	-0.31731
3.	-0.63323	-0.69987	0.31731
4.	-0.71124	0.00000	-0.67852

REACTION FOR BALANCE

No.	Case. 1			Case. 2			Case. 3		
	RX (t)	RY (t)	RM (tm)	RX (t)	RY (t)	RM (tm)	RX (t)	RY (t)	RM (tm)
1.	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
4.	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000

No.	Case. 4			Case. 5			Case. 6		
	RX (t)	RY (t)	RM (tm)	RX (t)	RY (t)	RM (tm)	RX (t)	RY (t)	RM (tm)
1.	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
4.	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000

No.	Case. 7		
	RX (t)	RY (t)	RM (tm)
1.	0.000	0.000	0.000
4.	0.000	0.000	0.000

NOTE : DIMENSIONS (t) BE EXCHANGE TO (KN)

No	Case 1 Dead load			Case 2 Earth pressure load			Case 3 Water pressure load				
	L(m)	M (tm)	S (t)	N (t)	M (tm)	S (t)	N (t)	M (tm)	S (t)	N (t)	
1-	2	0.000	-61.817	5.136	-201.775	-30.615	110.609	0.000	-1.252	9.031	0.000
*	1	0.250	-60.533	5.136	-198.825	-5.146	93.198	0.000	0.587	5.785	0.000
*	2	0.650	-58.478	5.136	-194.105	26.673	66.042	0.000	2.065	1.865	0.000
*	3	1.050	-56.424	5.136	-189.385	47.802	39.750	0.000	2.288	-0.487	0.000
*	4	1.750	-52.828	5.136	-181.125	60.116	-3.984	0.000	1.503	-1.271	0.000
*	5	2.450	-49.233	5.136	-172.865	43.297	-45.268	0.000	0.613	-1.271	0.000
*	6	2.850	-47.178	5.136	-168.145	21.879	-63.560	0.000	0.104	-1.271	0.000
*	7	3.250	-45.124	5.136	-163.425	-7.342	-82.284	0.000	-0.404	-1.271	0.000
2-	1	3.500	-43.840	5.136	-160.475	-29.289	-93.191	0.000	-0.722	-1.271	0.000
2-	3	0.000	-43.840	160.475	5.136	-29.289	0.000	-93.191	-0.722	0.000	-1.271
*	1	0.250	-6.586	137.550	5.136	-29.289	0.000	-93.191	-0.722	0.000	-1.271
*	2	0.650	41.098	100.870	5.136	-29.289	0.000	-93.191	-0.722	0.000	-1.271
*	3	1.050	74.110	64.190	5.136	-29.289	0.000	-93.191	-0.722	0.000	-1.271
*	4	1.750	96.576	0.000	5.136	-29.289	0.000	-93.191	-0.722	0.000	-1.271
*	5	2.450	74.110	-64.190	5.136	-29.289	0.000	-93.191	-0.722	0.000	-1.271
*	6	2.850	41.098	-100.870	5.136	-29.289	0.000	-93.191	-0.722	0.000	-1.271
*	7	3.250	-6.586	-137.550	5.136	-29.289	0.000	-93.191	-0.722	0.000	-1.271
3-	2	3.500	-43.840	-160.475	5.136	-29.289	0.000	-93.191	-0.722	0.000	-1.271
3-	4	0.000	-43.840	-5.136	-160.475	-29.289	93.191	0.000	-0.722	1.271	0.000
*	1	0.250	-45.124	-5.136	-163.425	-7.342	82.284	0.000	-0.404	1.271	0.000
*	2	0.650	-47.178	-5.136	-168.145	21.879	63.560	0.000	0.104	1.271	0.000
*	3	1.050	-49.233	-5.136	-172.865	43.297	43.268	0.000	0.613	1.271	0.000
*	4	1.750	-52.828	-5.136	-181.125	60.116	3.984	0.000	1.503	1.271	0.000
*	5	2.450	-56.424	-5.136	-189.385	47.802	-39.750	0.000	2.288	0.487	0.000
*	6	2.850	-58.478	-5.136	-194.105	26.673	-66.042	0.000	2.065	-1.865	0.000
*	7	3.250	-60.533	-5.136	-198.825	-5.146	-93.198	0.000	0.587	-5.785	0.000
4-	3	3.500	-61.817	-5.136	-201.775	-30.615	-110.609	0.000	-1.252	-9.031	0.000
4-	1	0.000	-61.817	201.775	-5.136	-30.615	0.000	-110.609	-1.252	0.000	-9.031
*	1	0.250	-14.976	172.950	-5.136	-30.615	0.000	-110.609	-1.252	0.000	-9.031
*	2	0.650	44.980	126.830	-5.136	-30.615	0.000	-110.609	-1.252	0.000	-9.031
*	3	1.050	86.488	80.710	-5.136	-30.615	0.000	-110.609	-1.252	0.000	-9.031
*	4	1.750	114.736	0.000	-5.136	-30.615	0.000	-110.609	-1.252	0.000	-9.031
*	5	2.450	86.488	-80.710	-5.136	-30.615	0.000	-110.609	-1.252	0.000	-9.031
*	6	2.850	44.980	-126.830	-5.136	-30.615	0.000	-110.609	-1.252	0.000	-9.031
*	7	3.250	-14.976	-172.950	-5.136	-30.615	0.000	-110.609	-1.252	0.000	-9.031
1-	4	3.500	-61.817	-201.775	-5.136	-30.615	0.000	-110.609	-1.252	0.000	-9.031

NOTE: DIMENSIONS(t),(tm) BE EXCHANGE TO (KN),(KNM) AT AFTER PAGE

BOX FOR DRAINAGE-NO 1

No	Case 4 HB live load-VL-			Case 5 HB live load-HL-			Case 6			
	L(m)	M (tm)	S (t)	N (t)	M (tm)	S (t)	N (t)	M (tm)	S (t)	N (t)
1- 2	0.000	-17.507	0.000	-60.025	-8.754	30.012	0.000	-160.857	189.593	-364.285
* 1	0.250	-17.507	0.000	-60.025	-1.786	25.725	0.000	-117.062	160.864	-360.214
* 2	0.650	-17.507	0.000	-60.025	7.132	18.865	0.000	-61.725	116.057	-353.701
* 3	1.050	-17.507	0.000	-60.025	13.306	12.005	0.000	-24.027	72.675	-347.187
* 4	1.750	-17.507	0.000	-50.025	17.507	0.000	0.000	1.253	0.514	-335.788
* 5	2.450	-17.507	0.000	-60.025	13.306	-12.005	0.000	-21.536	-64.305	-324.389
* 6	2.850	-17.507	0.000	-60.025	7.132	-18.865	0.000	-54.041	-97.787	-317.876
* 7	3.250	-17.507	0.000	-60.025	-1.786	-25.725	0.000	-99.420	-128.681	-311.362
2- 1	3.500	-17.507	0.000	-60.025	-8.754	-30.013	0.000	-133.861	-146.677	-307.291
2- 3	0.000	-17.507	60.025	0.000	-8.754	0.000	-30.013	-133.861	307.291	-146.677
* 1	0.250	-3.573	51.450	0.000	-8.754	0.000	-30.013	-62.526	263.392	-146.677
* 2	0.650	14.263	37.730	0.000	-8.754	0.000	-30.013	28.784	193.154	-146.677
* 3	1.050	26.611	24.010	0.000	-8.754	0.000	-30.013	91.998	122.917	-146.677
* 4	1.750	35.015	0.000	0.000	-8.754	0.000	-30.013	135.019	0.000	-146.677
* 5	2.450	26.611	-24.010	0.000	-8.754	0.000	-30.013	91.998	-122.917	-146.677
* 6	2.850	14.263	-37.730	0.000	-8.754	0.000	-30.013	28.784	-193.155	-146.677
* 7	3.250	-3.573	-51.450	0.000	-8.754	0.000	-30.013	-62.526	-263.393	-146.677
3- 2	3.500	-17.507	-60.025	0.000	-8.754	0.000	-30.013	-133.861	-307.291	-146.677
3- 4	0.000	-17.507	0.000	-60.025	-8.754	30.012	0.000	-133.861	146.677	-307.291
* 1	0.250	-17.507	0.000	-60.025	-1.786	25.725	0.000	-99.420	128.681	-311.362
* 2	0.650	-17.507	0.000	-60.025	7.132	18.865	0.000	-54.041	97.787	-317.876
* 3	1.050	-17.507	0.000	-60.025	13.306	12.005	0.000	-21.536	64.305	-324.389
* 4	1.750	-17.507	0.000	-60.025	17.507	0.000	0.000	1.253	-0.514	-335.788
* 5	2.450	-17.507	0.000	-60.025	13.306	-12.005	0.000	-24.027	-72.675	-347.187
* 6	2.850	-17.507	0.000	-60.025	7.132	-18.865	0.000	-61.725	-116.057	-353.701
* 7	3.250	-17.507	0.000	-60.025	-1.786	-25.725	0.000	-117.062	-160.864	-360.214
4- 3	3.500	-17.507	0.000	-60.025	-8.754	-30.013	0.000	-160.857	-189.593	-304.285
4- 1	0.000	-17.507	60.025	0.000	-8.754	0.000	-30.013	-160.857	364.285	-189.593
* 1	0.250	-3.573	51.450	0.000	-8.754	0.000	-30.013	-76.291	312.245	-189.593
* 2	0.650	14.263	37.730	0.000	-8.754	0.000	-30.013	31.954	228.979	-189.593
* 3	1.050	26.611	24.010	0.000	-8.754	0.000	-30.013	106.892	145.714	-189.593
* 4	1.750	35.015	0.000	0.000	-8.754	0.000	-30.013	157.892	0.000	-189.593
* 5	2.450	26.611	-24.010	0.000	-8.754	0.000	-30.013	106.892	-145.714	-189.593
* 6	2.850	14.263	-37.730	0.000	-8.754	0.000	-30.013	31.954	-228.979	-189.593
* 7	3.250	-3.573	-51.450	0.000	-8.754	0.000	-30.013	-76.291	-312.245	-189.593
1- 4	3.500	-17.507	-60.025	0.000	-8.754	0.000	-30.013	-160.857	-364.285	-189.593

BOX FOR DRAINAGE-NO 1

		Case 7			
No	L(m)	M (tm)	S (t)	N (t)	
1-	2	0.000	254.014	-278.449	
*	1	0.250	212.855	-274.879	
*	2	0.650	150.261	-267.865	
*	3	1.050	91.679	-261.351	
*	4	1.750	-1.584	-249.953	
*	5	2.450	-86.211	-238.554	
*	6	2.850	-131.011	-232.040	
*	7	3.250	-173.225	-225.527	
2-	1	3.500	-198.295	-221.456	
2-	3	0.000	221.455	-198.295	
*	1	0.250	189.819	-198.295	
*	2	0.650	139.201	-198.295	
*	3	1.050	88.582	-198.295	
*	4	1.750	0.000	-198.295	
*	5	2.450	-88.582	-198.295	
*	6	2.850	-139.201	-198.295	
*	7	3.250	-189.819	-198.295	
3-	2	3.500	-221.456	-198.295	
3-	4	0.000	198.295	-221.455	
*	1	0.250	173.225	-225.527	
*	2	0.650	131.011	-232.040	
*	3	1.050	86.211	-238.554	
*	4	1.750	1.584	-249.953	
*	5	2.450	-91.679	-261.351	
*	6	2.850	-150.261	-267.865	
*	7	3.250	-212.855	-274.379	
4-	3	3.500	-254.014	-278.450	
4-	1	0.000	278.450	-254.014	
*	1	0.250	238.671	-254.014	
*	2	0.650	175.025	-254.014	
*	3	1.050	111.380	-254.014	
*	4	1.750	0.000	-254.014	
*	5	2.450	-111.380	-254.014	
*	6	2.850	-175.025	-254.014	
*	7	3.250	-238.671	-254.014	
1-	4	3.500	-278.449	-254.014	

PICK-UP No. 1 *

M. MAXIMUM

M. MINIMUM

No.	L (m)	Case	M (tm)	S (t)	N (t)	Case	M (tm)	S (t)	N (t)
1 -	0.000	C-7	-152.331	254.014	-278.449	C-6	-160.857	189.593	-364.285
* 1	0.250	C-7	-94.005	212.855	-274.379	C-6	-117.062	160.864	-360.214
* 2	0.650	C-7	-21.516	150.261	-267.865	C-6	-61.725	116.057	-353.701
* 3	1.050	C-7	26.738	91.679	-261.351	C-6	-24.027	72.675	-347.187
* 4	1.750	C-7	57.655	-1.584	-249.953	C-6	1.253	0.514	-335.788
* 5	2.450	C-7	26.465	-86.211	-238.554	C-6	-21.536	-64.305	-324.389
* 6	2.850	C-7	-17.066	-131.011	-232.040	C-6	-54.041	-97.787	-317.876
* 7	3.250	C-7	-77.999	-173.225	-225.527	C-6	-99.420	-128.681	-311.362
2 -	3.500	C-7	-124.460	-198.295	-221.456	C-6	-133.861	-146.677	-307.291
2 -	0.000	C-7	-124.460	221.455	-198.295	C-6	-133.861	307.291	-146.677
* 1	0.250	C-6	-62.526	263.392	-146.677	C-7	-73.051	189.819	-198.295
* 2	0.650	C-6	28.784	193.154	-146.677	C-7	-7.247	139.201	-198.295
* 3	1.050	C-6	91.998	122.917	-146.677	C-7	38.309	88.582	-198.295
* 4	1.750	C-6	135.019	0.000	-146.677	C-7	69.313	0.000	-198.295
* 5	2.450	C-6	91.998	-122.917	-146.677	C-7	38.309	-88.582	-198.295
* 6	2.850	C-6	28.784	-193.155	-146.677	C-7	-7.247	-139.201	-198.295
* 7	3.250	C-6	-62.526	-263.393	-146.677	C-7	-73.051	-189.819	-198.295
3 -	3.500	C-7	-124.460	-221.456	-198.295	C-6	-133.861	-307.291	-146.677
3 -	0.000	C-7	-124.460	198.295	-221.455	C-6	-133.861	146.677	-307.291
* 1	0.250	C-7	-77.999	173.225	-225.527	C-6	-99.420	128.681	-311.302
* 2	0.650	C-7	-17.066	131.011	-232.040	C-6	-54.041	97.787	-317.876
* 3	1.050	C-7	26.465	86.211	-238.554	C-6	-21.536	64.305	-324.389
* 4	1.750	C-7	57.655	1.584	-249.953	C-6	1.253	-0.514	-335.788
* 5	2.450	C-7	26.738	-91.679	-261.351	C-6	-24.027	-72.675	-347.187
* 6	2.850	C-7	-21.516	-150.261	-267.865	C-6	-61.725	-116.057	-353.701
* 7	3.250	C-7	-94.005	-212.855	-274.379	C-6	-117.062	-160.864	-360.214
4 -	3.500	C-7	-152.331	-254.014	-278.450	C-6	-160.857	-189.593	-364.285
4 -	0.000	C-7	-152.331	278.450	-254.014	C-6	-160.857	364.285	-189.593
* 1	0.250	C-6	-76.291	312.245	-189.593	C-7	-87.691	238.671	-254.014
* 2	0.650	C-6	31.954	228.979	-189.593	C-7	-4.952	175.025	-254.014
* 3	1.050	C-6	106.892	145.714	-189.593	C-7	52.329	111.380	-254.014
* 4	1.750	C-6	157.892	0.000	-189.593	C-7	91.312	0.000	-254.014
* 5	2.450	C-6	106.892	-145.714	-189.593	C-7	52.329	-111.380	-254.014
* 6	2.850	C-6	31.954	-228.979	-189.593	C-7	-4.952	-175.025	-254.014
* 7	3.250	C-6	-76.291	-312.245	-189.593	C-7	-87.691	-238.671	-254.014
1 -	3.500	C-7	-152.331	-278.449	-254.014	C-6	-160.857	-364.285	-189.593

BOX FOR DRAINAGE-NO 1

PICK-UP No. 1 *

S . M A X I M U M

S . M I N I M U M

No.	L (m)	Case	M (tm)	S (t)	N (t)	Case	M (tm)	S (t)	N (t)
1 - 2	0.000	C- 7	-152.331	254.014	-278.449	C- 6	-160.857	189.593	-364.285
* 1	0.250	C- 7	-94.005	212.855	-274.379	C- 6	-117.062	160.864	-360.214
* 2	0.650	C- 7	-21.516	150.261	-267.865	C- 6	-61.725	116.057	-353.701
* 3	1.050	C- 7	26.738	91.679	-261.351	C- 6	-24.027	72.675	-347.187
* 4	1.750	C- 6	1.253	0.514	-335.788	C- 7	57.655	-1.584	-249.953
* 5	2.450	C- 6	-21.536	-64.305	-324.389	C- 7	26.465	-86.211	-238.554
* 6	2.850	C- 6	-54.041	-97.787	-317.876	C- 7	-17.066	-131.011	-232.040
* 7	3.250	C- 6	-99.420	-128.681	-311.362	C- 7	-77.999	-173.225	-225.527
2 - 1	3.500	C- 6	-133.861	-146.677	-307.291	C- 7	-124.460	-198.295	-221.456
2 - 3	0.000	C- 6	-133.861	307.291	-146.677	C- 7	-124.460	221.455	-198.295
* 1	0.250	C- 6	-62.526	263.392	-146.677	C- 7	-73.051	189.819	-198.295
* 2	0.650	C- 6	28.784	193.154	-146.677	C- 7	-7.247	139.201	-198.295
* 3	1.050	C- 6	91.998	122.917	-146.677	C- 7	38.309	88.582	-198.295
* 4	1.750	C- 7	69.313	0.000	-198.295	C- 6	135.019	0.000	-146.677
* 5	2.450	C- 7	38.309	-88.582	-198.295	C- 6	91.998	-122.917	-146.677
* 6	2.850	C- 7	-7.247	-139.201	-198.295	C- 6	28.784	-193.155	-146.677
* 7	3.250	C- 7	-73.051	-189.819	-198.295	C- 6	-62.526	-263.393	-146.677
3 - 2	3.500	C- 7	-124.460	-221.456	-198.295	C- 6	-133.861	-307.291	-146.677
3 - 4	0.000	C- 7	-124.460	198.295	-221.455	C- 6	-133.861	146.677	-307.291
* 1	0.250	C- 7	-77.999	173.225	-225.527	C- 6	-99.420	128.681	-311.362
* 2	0.650	C- 7	-17.066	131.011	-232.040	C- 6	-54.041	97.787	-317.876
* 3	1.050	C- 7	26.465	86.211	-238.554	C- 6	-21.536	64.305	-324.389
* 4	1.750	C- 7	57.655	1.584	-249.953	C- 6	1.253	-0.514	-335.788
* 5	2.450	C- 6	-24.027	-72.675	-347.187	C- 7	26.738	-91.679	-261.351
* 6	2.850	C- 6	-61.725	-116.057	-353.701	C- 7	-21.516	-150.261	-267.865
* 7	3.250	C- 6	-117.062	-160.864	-360.214	C- 7	-94.005	-212.855	-274.379
4 - 3	3.500	C- 6	-160.857	-189.593	-364.285	C- 7	-152.331	-254.014	-278.450
4 - 6	0.000	C- 6	-160.857	364.285	-189.593	C- 7	-152.331	278.450	-254.014
* 1	0.250	C- 6	-76.291	312.245	-189.593	C- 7	-87.691	238.671	-254.014
* 2	0.650	C- 6	31.954	228.979	-189.593	C- 7	-4.952	175.025	-254.014
* 3	1.050	C- 6	106.892	145.714	-189.593	C- 7	52.329	111.380	-254.014
* 4	1.750	C- 7	91.312	0.000	-254.014	C- 6	157.892	0.000	-189.593
* 5	2.450	C- 7	52.329	-111.380	-254.014	C- 6	106.892	-145.714	-189.593
* 6	2.850	C- 7	-4.952	-175.025	-254.014	C- 6	31.954	-228.979	-189.593
* 7	3.250	C- 7	-87.691	-238.671	-254.014	C- 6	-75.291	-312.245	-189.593
1 - 4	3.500	C- 7	-152.331	-278.449	-254.014	C- 6	-160.857	-364.285	-189.593

BOX FOR DRAINAGE-NO 1

PICK-UP No. 1 *

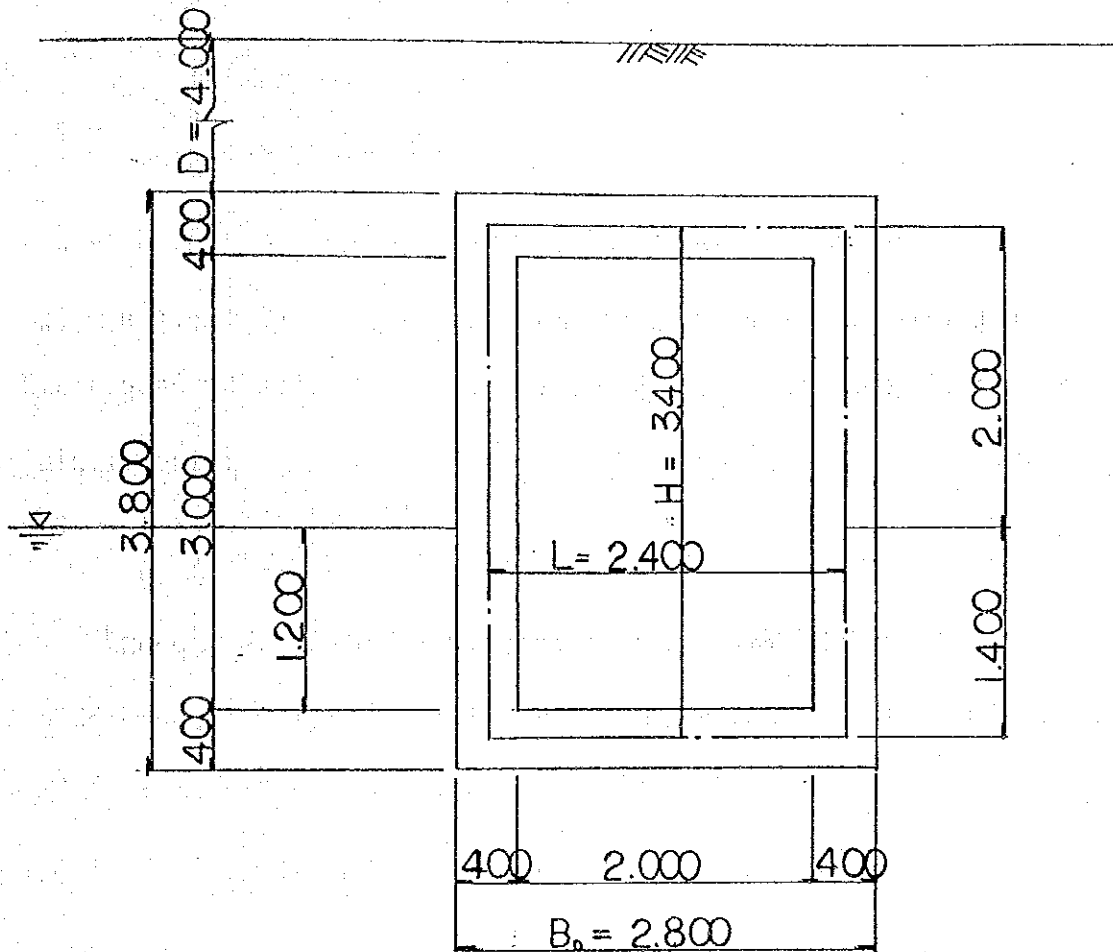
N. MAXIMUM

N. MINIMUM

No.	L (m)	Case	M (tm)	S (t)	N (t)	Case	M (tm)	S (t)	N (t)
1 -	0.000	C-7	-152.331	254.014	-278.449	C-6	-160.857	189.593	-364.285
* 1	0.250	C-7	-94.005	212.855	-274.379	C-6	-117.062	160.884	-360.214
* 2	0.650	C-7	-21.516	150.261	-267.865	C-6	-61.725	116.057	-353.701
* 3	1.050	C-7	26.738	91.679	-261.351	C-6	-24.027	72.675	-347.187
* 4	1.750	C-7	57.655	-1.584	-249.953	C-6	1.253	0.514	-335.788
* 5	2.450	C-7	26.465	-86.211	-238.554	C-6	-21.536	-64.305	-324.389
* 6	2.850	C-7	-17.066	-131.011	-232.040	C-6	-34.041	-97.787	-317.876
* 7	3.250	C-7	-77.999	-173.225	-225.527	C-6	-99.420	-128.681	-311.362
2 -	3.500	C-7	-124.460	-198.295	-221.456	C-6	-133.861	-146.677	-307.291
2 -	0.000	C-6	-133.861	307.291	-146.677	C-7	-124.460	221.455	-198.295
* 1	0.250	C-6	-62.526	263.392	-146.677	C-7	-73.051	189.819	-198.295
* 2	0.650	C-6	28.784	193.154	-146.677	C-7	-7.247	139.201	-198.295
* 3	1.050	C-6	91.998	122.917	-146.677	C-7	38.309	88.582	-198.295
* 4	1.750	C-6	135.019	0.000	-146.677	C-7	69.313	0.000	-198.295
* 5	2.450	C-6	91.998	-122.917	-146.677	C-7	38.309	-88.582	-198.295
* 6	2.850	C-6	28.784	-193.155	-146.677	C-7	-7.247	-139.201	-198.295
* 7	3.250	C-6	-62.526	-263.393	-146.677	C-7	-73.051	-189.819	-198.295
3 -	3.500	C-6	-133.861	-307.291	-146.677	C-7	-124.460	-221.456	-198.295
3 -	0.000	C-7	-124.460	198.295	-221.455	C-6	-133.861	146.677	-307.291
* 1	0.250	C-7	-77.999	173.225	-225.527	C-6	-99.420	128.681	-311.362
* 2	0.650	C-7	-17.066	131.011	-232.040	C-6	-34.041	97.787	-317.876
* 3	1.050	C-7	26.465	86.211	-238.554	C-6	-21.536	64.305	-324.389
* 4	1.750	C-7	57.655	1.584	-249.953	C-6	1.253	-0.514	-335.788
* 5	2.450	C-7	26.738	-91.679	-261.351	C-6	-24.027	-72.675	-347.187
* 6	2.850	C-7	-21.516	-150.261	-267.865	C-6	-61.725	-116.057	-353.701
* 7	3.250	C-7	-94.005	-212.855	-274.379	C-6	-117.062	-160.884	-360.214
4 -	3.500	C-7	-152.331	-254.014	-278.450	C-6	-160.857	-189.593	-364.285
4 -	0.000	C-6	-160.857	364.285	-189.593	C-7	-152.331	278.450	-254.014
* 1	0.250	C-6	-76.291	312.245	-189.593	C-7	-87.691	238.671	-254.014
* 2	0.650	C-6	31.954	228.979	-189.593	C-7	-4.952	175.025	-254.014
* 3	1.050	C-6	106.892	145.714	-189.593	C-7	52.329	111.380	-254.014
* 4	1.750	C-6	157.892	0.000	-189.593	C-7	91.312	0.000	-254.014
* 5	2.450	C-6	106.892	-145.714	-189.593	C-7	52.329	-111.380	-254.014
* 6	2.850	C-6	31.954	-228.979	-189.593	C-7	-4.952	-175.025	-254.014
* 7	3.250	C-6	-76.291	-312.245	-189.593	C-7	-87.691	-238.671	-254.014
1 -	3.500	C-6	-160.857	-364.285	-189.593	C-7	-152.331	-278.449	-254.014

NO ② BOX-CULVERT FOR DRAINAGE

1) Shape and Size



Where D^m = depth of asphalt and
similar surface soil.

2) Factor of section

$$A = 1.00 \times 0.40 = 0.4000 \text{ m}^2$$

$$I = \frac{1.00 \times 0.40^3}{12} = 0.00533 \text{ m}^4$$

$$E_c = 25 \text{ kN/mm}^2 = 2.5 \times 10^7 \text{ kN/m}^2$$

No. ② BOX CULVERT FOR DRAINAGE

1. calculation for bending moment (U.L.S)

section $b=100\text{cm}$ $h=40$ $d=34.0$ $d'=6.0$

a) intersection point ①=④ (②=③) $Mu.\min = -111.4\text{KNm}$ (-95.5KNm)

$$A_s = Y_{1.6} - 150\text{c}^{\text{t}^{\text{c}}} = 13.41 \text{ cm}^2$$

$$X = \frac{0.87 \times 41000 \times 13.41}{0.40 \times 2500 \times 100} \cong 4.8\text{cm}$$

$$Z = 34.0 - \frac{4.8}{2} = 31.6\text{cm} < 0.95 \times 34.0 = 32.3\text{cm} \text{ OK}$$

$$M_{RS} = 0.87 \times 41000 \times 13.41 \times 31.6 \times 10^{-5} = 151.2\text{KNm} > Mu = 111.4\text{KNm}$$

$$M_{RC} = 0.40 \times 2500 \times 100 \times 4.8 \times 31.6 \times 10^{-5} = 151.6\text{KNm} > Mu = 111.4\text{KNm} \text{ OK}$$

b) middle point ①~②=③~④ $Mu.\max = 79.2\text{KNm}$

$$A_s = Y_{1.2} - 150\text{c}^{\text{t}^{\text{c}}} = 7.54 \text{ cm}^2$$

$$M_R = 87.4\text{KNm} > Mu = 79.2\text{KNm}$$

(Where: M_R : From calculation of point ④~①)

c) middle point ④~①= (②~③) $Mu.\max = 63.1\text{KNm}$ (51.3KNm)

$$A_s = Y_{1.2} - 150\text{c}^{\text{t}^{\text{c}}} = 1.131/0.15 = 7.54 \text{ cm}^2$$

$$X = \frac{0.87 \times 41000 \times 7.54}{0.40 \times 2500 \times 100} \cong 3.0\text{cm}$$

$$Z = 34.0 - \frac{3.0}{2} = 32.5\text{cm} \cong 0.95 \times 34.0 = 32.3\text{cm} \text{ OK}$$

$$M_{RS} = 0.87 \times 41000 \times 7.54 \times 32.5 \times 10^{-5} = 87.4\text{KNm} > Mu = 63.1\text{KNm}$$

$$M_{RC} = 0.40 \times 2500 \times 100 \times 3.0 \times 32.5 \times 10^{-5} = 97.5\text{KNm} > Mu = 63.1\text{KNm}$$

2. calculation for shearing force (U.L.S)

section $b=100\text{cm}$ $h=40$ $d=34.0$ $d'=6.0$

a) side wall ①, ④ $Su.\max = 116.3\text{KN}$

$$V_c = \frac{116.3 \times 10^3}{100 \times 34.0} = 34.2 \text{ N/cm}^2 < V_{ca} = 43.6 \text{ N/cm}^2 \text{ OK}$$

b) upper slab ②, ③ $Su.\max = 77.8\text{KN}$

$$V_c = \frac{77.8 \times 10^3}{100 \times 34.0} = 22.9 \text{ N/cm}^2 < V_{ca} = 43.6 \text{ N/cm}^2 \text{ OK}$$

c) bottom slab ①, ④ $S_u \max = 92.6 \text{ kN}$

$$V_c = \frac{92.6 \times 10^3}{100 \times 34.0} = 27.3 \text{ N/cm}^2 < V_{ca} = 43.6 \text{ N/cm}^2 \text{ OK}$$

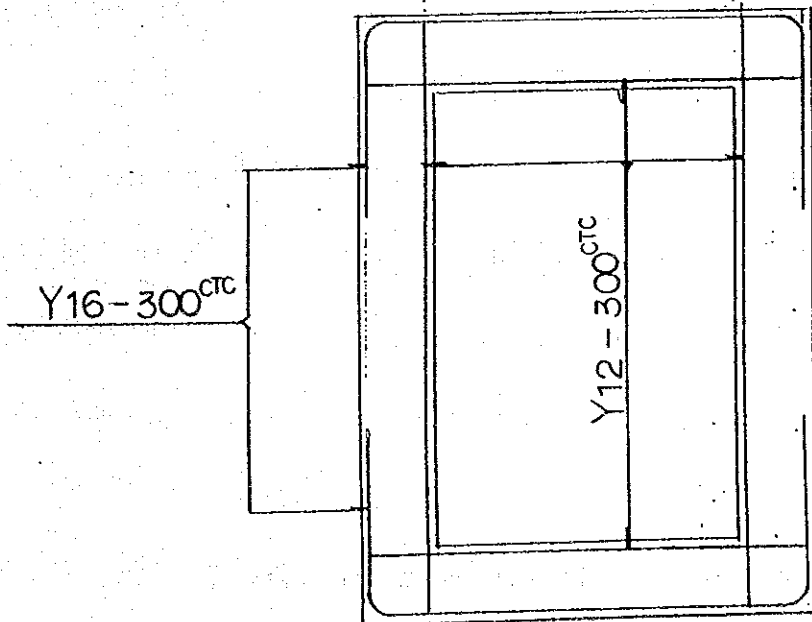
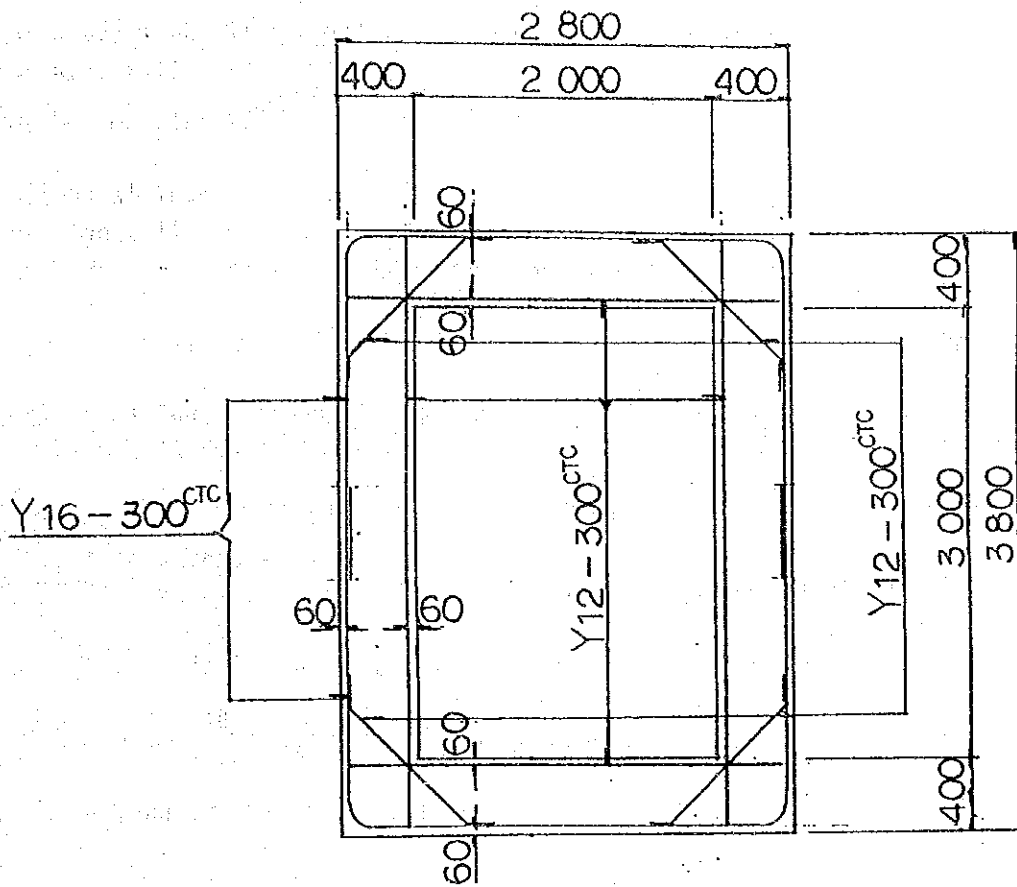
where

$$A_s = Y_{16} - 150^{c+c} = 13.41 \text{ cm}^2$$

$$P = \frac{13.41}{100 \times 34.0} \times 100 = 0.394 \%$$

$$\therefore V_{ca} = 35.0 + \frac{15}{0.25} (0.394 - 0.25) = 43.6 \text{ N/cm}^2$$

NO ② BOX CULVERT FOR DRAINAGE



NO② BOX FOR DRAINAGE

Load

(1) Dead load

a) Vertical load Where $\alpha = 1.2$ (earth pressure factor of vertical) $\therefore \frac{D}{B_0} = \frac{4.0}{2.8} = 1.4 > 1.0$
 < 2.0

For upper slab $w_1 = 22.6 \times 0.50 + 19.6 \times 3.50 \times 1.20 + 23.60 \times 0.400 = 103.060 \text{ kN/m}$

For side wall $w_2 = 23.6 \times 0.40 = 9.440 \text{ ''}$

For bottom slab $w_3 = 103.060 + \frac{2 \times 9.440 \times 3.40}{2.40} = 129.807 \text{ ''}$

b) Horizontal load ----- earth pressure

For side wall $P_1 = (22.6 \times 0.50 + 19.60 \times 3.70) \times 0.500 = 41.910 \text{ kN/m}$

'' $P_2 = (22.6 \times 0.50 + 19.60 \times 5.70) \times 0.500 = 61.510 \text{ ''}$

'' $P_3 = (22.6 \times 0.50 + 19.60 \times 5.70 + 10.8 \times 1.40) \times 0.500 = 69.070 \text{ ''}$

c) Horizontal load ----- water Pressure

For side wall $P_w = 9.80 \times 1.40 = 13.720 \text{ kN/m}$

(2) Live load

live load surcharge of axle

$$P = \frac{\text{KN/axle} \times \text{unit}}{3.50 \times B} \quad \text{width of dispersal of wheel}$$

$$B = 0.300 + 4.00 + 0.400 = 4.700 \text{ m}$$

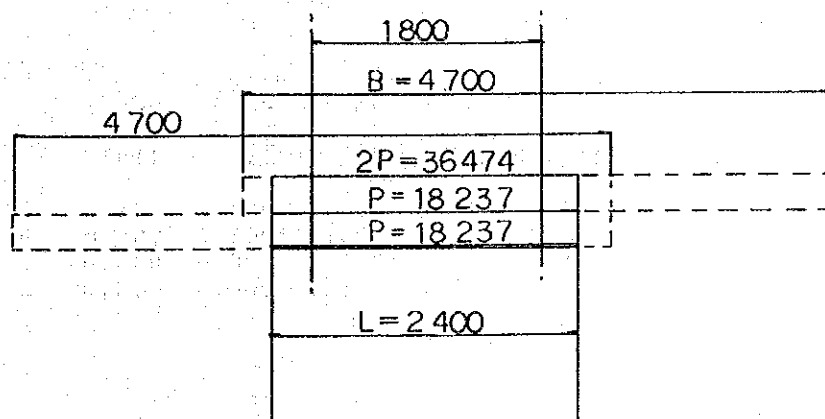
$$= \frac{10 \times 30}{3.50 \times 4.70} = 18.237 \text{ KN/m}^2$$

or live load surcharge of vehicle

$$g_o = \frac{\text{KN/vehicle} \times \text{unit}}{3.50 \times 10.0} = 34.300 \text{ KN/m}^2 < 2P = 36.474 \text{ KN/m}^2$$

OF course the loaded of live load is consider as following

case-1 Vaertical load



For upper slab and bottom slab $w_1 = w_2 = 36.474 \text{ KN/m}$

case-2 Horizontal load ----- eath pressure of live load surcharge

For side wall: $p_e = g_o \cdot k_o = 34.300 \times 0.500 = 17.150 \text{ KN/m}$

No	X (m)	Y (m)
1	0.0000	0.0000
2	0.0000	3.4000
3	2.4000	3.4000
4	2.4000	0.0000

No	I	J	A (m2)	I (m4)	I - J	L (m)	E (t/m2)	EPS
1	1	2	0.40000	0.005330	Fix - Fix	3.400	2.50E+07	1.00E-05
2	2	3	0.40000	0.005330	Fix - Fix	2.400	2.50E+07	1.00E-05
3	3	4	0.40000	0.005330	Fix - Fix	3.400	2.50E+07	1.00E-05
4	4	1	0.40000	0.005330	Fix - Fix	2.400	2.50E+07	1.00E-05

No. 1

No	X (t/m)	Y (t/m)	M (tm/Rad)
1	Fix	Fix	Free
4	Free	Fix	Free

No	L-No	L-No	L-No	L-No	L-No	
	1	2	3	4	5	
	11	12	13	14	15	
1	5	0.200	0.800	1.700	2.600	3.200
2	5	0.200	0.800	1.200	1.600	2.200
3	5	0.200	0.800	1.700	2.600	3.200
4	5	0.200	0.800	1.200	1.600	2.200

NOTE: THE DIMENSION(t) BE EXCHANG TO
DIMENSION(KN) INTO THIS CALCULATION

CALCULATION POINTS OF EACH FORCE

