	CONCENABLE REHABILITATION													ADDING & WIDENING	MINHOM		HAND ENIGHT																FASING GRADE																								
	RIVER VIEW POINT BRIDGE	OPENING															INAUELICALE																INADEQUATE																								
	CAPACSTY	FEAR	2147	2147	2147	2147	7412	2147	2127	2098	2098	2107	2014	<u>1</u> 88	88	2441	R	21/1	20160	N/A	N/A	NIA	2429	2424	2424	2437	2424	242/	1110	1110	1610	2321	2321	2317	2317	2319	218	2020	2669	2669	2195	2028	2028 2028	2222	20202	0202	2028	2028	2028	2028	2028	2028	2028	2116	5222	2225	2116
	VIC 1		0.17	0.17	0.17	0.17	0.17	0.17	0.35	0.18	0.16	0.19	0.29	8	1.15	0	4 0		0 75	120	0000	0:30	0.32	0.34	0.34	8 9	800	3		0.28	0.28	0.32	0.32	ъ С	0.34	80	30	0 0 0 0 0		0.32	80	0.31	0.31		500	10.0	0.33	0.31	0.31	0.31	0.33	0.31	0.01	0.22	0.24	0.24	80
	TRAFFIC VEW POINT	RATE	4.6	4.6	4.5	46	46	46	5.1	6.8	6.8	6.2	31.5	80	8.0	0	0		87	-85	-92	-6.5	1,6	1,6	1.6	1.6	1.6	0.0	0	1	5.4	22	2.2	2.2	22	22	2.2	212	10	1.0	3.5	19.4	19.4	1.9.1	5.0	101	19.4	19.4	19.4	19.4	19.4	18	1.8	57	30	3.0	5.7
	PRESENT	DEMAND	520	382	250	ŝ	092	250	2	307	307	307	469	3008	1992	RCZ	AC	1474	1171	522	522	522	522	522	522	25	522	200	020	791	721	653	653	653	653	653	322		417	417	361	544	3	,	22	102	SAA	544	544	544	544	544	544	352	346	345	346
POINT	TRAFFIC F	7	1514 1514	1514	1497	1497	1497	1512	1560	1711	1711	1624	1843	1854	1730	19//	1/83	1801	1805	1531	1752	1762	1623	1531	1538	1762	1531	15/8	2002	2540	2580	2051	2051	1940	1940	1994	1994	1731	1291	1291	1576	1749	1749	At / 1	86/1	6471	1649	1749	1749	1749	1649	1749	1749	1578	1435	1439	1578
FROM FUNCTIONAL VIEW POINT	I I	PEDESTRIAN												Hoh							-																																+				
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ROMF	SIDE	LOW	990	0.50	0,50	05.0	0.50	3	-				0.39			_		3			2.50	1.70					0.35	0.35		<u> </u>	0.8				0.58		0.55	4 00				0.50	0.36				0.56	0.54	0.55	0.54	0.92			2 2		0.3	
UL.	CARRIAGE	HLIOM	6.70	6.80	0.74	6.85	88	2002	6.19	5.18	6.10	6.10	5.56	0.S	6.75	8.0	0/0	04.0	200 2	8.30	13.70	12.60	7.55	5.84	5.70	7.32	6.76	6.74	9/% 8/%	2A.O	7.28	8.90	6.55	8,45	6.78	6.90	8,10	5 00 S	6.80	6.9	6.70	6.70	6.70	07.7	0.75	-9-10 9-90	6.85	7.20	6.75	6.70	6.60	89	6.85 A 60	3.45	\$70	6,70	6.90
	3 L	BRDGE	S88 ABA	288 -	SBB	SBS	SEB	SBB	SBB	SBB	80g	SBB	- 884	ğ	DBS	200	300	000	and of the second se	SBB	SBB	SBB	SBB	- SBB	PRB	888 8	588	222	0	320	SAC	SBE	SBB	888 8	SBB	SBB	BBS	304	SBB	SBB	SBB	SBC	SBC				SBC	SBC	SBC	SBC	8 B G	288 288	000	302	SBC	RC8	RCB
	CAPACITY		SSAL	SSAL	SSAL	SSAL	SSAL	SSAL	SSAL	SSAL	P/A	SSAL	STAL	STAL	STAL	SIAL	SCAL	2001	SCAL	SSAL	SSAL	SSAL	SSAL	SSAL	STAL	STAL	SSAL	SSAL	21AL	O ML	STAI	SSAL	SSAL	SSAL	SSAL	SSAL	SSAL	STAL	SSAL	SSAL	STAL	STAL	STAL	SIAL	SIAL	014 0	STA	STAL	STAL	STAL	STAL	STAL	STAL	STAL	STAL	STAL	STAL
	STUDY		~	101	2	N	NG	10	0	2	0	5	e	9	0		4 0	20	20	5	e	2	6	6	Ð	0	0	6	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	20		e	0	9	Ċ	e)	3	56	,	2	3	0	ന	3	5		50	0	0	0	e	3		50	9	9	e)
	YEAR BUILT		1950	1950	1950	0350	255	058	1950	1930	1935	1951	0/61	<u>8</u>	1950	0.61	0681	220		1950	1940	1950	1950	1960	1960	1960	1950	1958	1932	0301	1584	1950	1950	1950	1950	1950	1940	1950	1050	1950	1950	1950	1950	0.6	1950	0081	1050	1950	1950	1950	1961	1930	1930	096	1950	1960	1950
	DISTRICT		K PILAH	K PILAH	K PILAH	K PILAH	K PILAH	K PILAH	JEMPUL	JELEBU	JELEBU	BENTONG	JEMPUL	MANJUNG	MANUUNG	UCCAMA	SEGAMAL DALIAT		RATIPAHAT	SEREMBAN	SEREMBAN	SEREMBAN	K PICAH	K PILAH	K PILAH	K PILAH	KPEAH	K PILAH	OT STATES	U.LANGAI	11 ANGAT	- Cc	Dd	PD	SEREMBAN	SEREMBAN	SEREMBAN	PETALING DETALING		HLR PERAK	BTG PADANG	BTG PADANG	BTG PADANG	BIG PADANG	BTG PAUANG	BIG PAUANG	RTG PADANG	BTG PADANG	BTG PADANG	BTG PADANG	Lipis	UPIS	LIPIS 	MANJUNG	LAMSSELAMA	LEWRISELAMA	LEMESELAMA
	STATE		SN N	SN	SN SN		SN					-		-+	1	+	+	╈	╈	T	t	t	t	f					1	+	T	T	Г	Γ			1	SELANGUH	Т	Τ.	Γ	Π		Τ	1	Т	Ŧ		Т	1		PAHANG	PAHANG	PERAK	PERAK	PERAK	PERAK
	٦,		00901420	00010600	00220600	00902360	00902430	0004300	06190600	01020900	00840600	÷	01105770	∽ł			0/23039/0	<u>.</u>		-	+	+	-	2280	102380		03000	05103300		00500540	4870	+	+	301190	$\left \cdot \right $		-+	05403460	+	+	+-		05901070	-t	-ŀ	-h	00000000	+	0590220	1	05905010	05905290	05906010	000001240	CONTRACTOR OF CONTRACTOR	06005220	06005740
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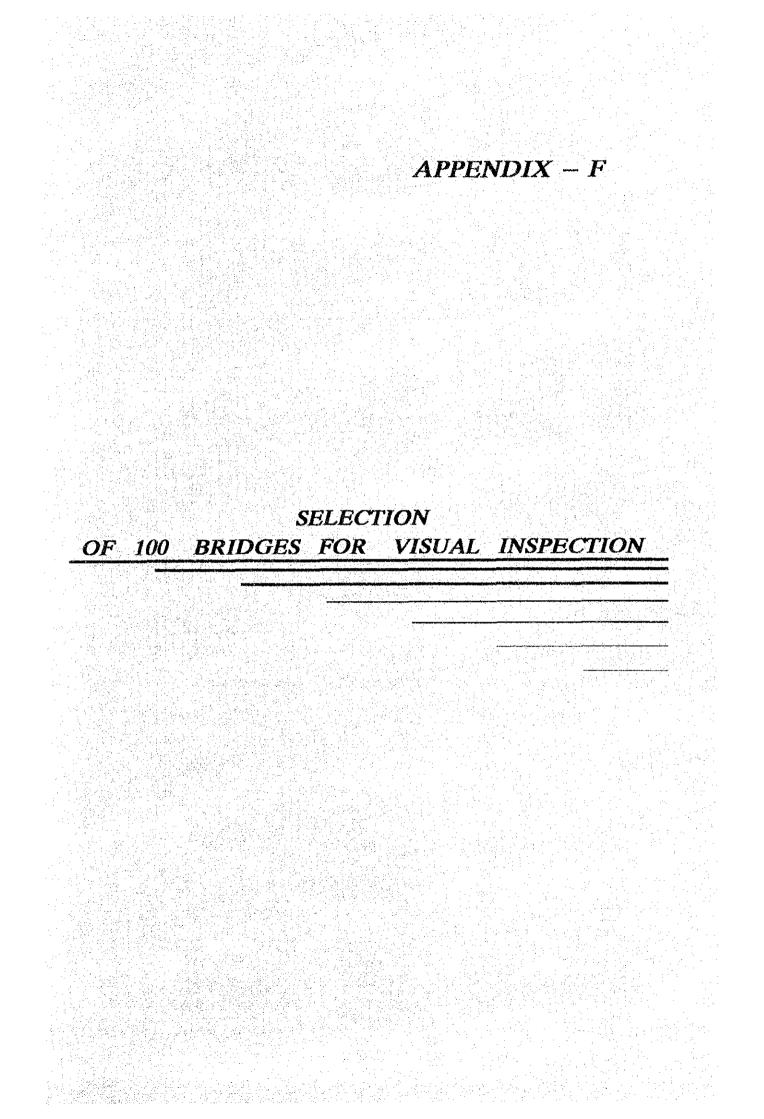
APPENDIX -E PRELIMINARY EVALUATION RESULTS AND ASSIGNMENT RESULTS OF CONCEIVABLE REHABILITATION PLAN

E – 3

APPENDIX-E PRELIMINARY EVALUATION RESULTS AND ASSIGNMENT RESULTS OF CONCEIVABLE REHABILITATION PLAN FROM FUNCTIONAL VIEW POINT

Sinter Sinter<	$ \begin{array}{ c $	LSIQ	DISTRICT	REAR Built	STUDY	CAPACITY	ž z	CARRINGE		_, ¢	ç Ş	TRACCIO	TRAFFIC	TRAFFIC VEW POINT	INT VIC	VEMORY	RIVER VEW POINT	CONCEIVABLE REHARTERIZATION
0 55/4 55 5 <th>$\begin{array}{ c c c c c c c c c c c c c c c c c c c$</th> <th></th> <th>3</th> <th>i</th> <th></th> <th></th> <th>Beege</th> <th>HIGHA</th> <th>HIOM</th> <th>5 er</th> <th>CESTRIAN</th> <th>CAPACITY</th> <th>DEMAND</th> <th>RATE</th> <th>2</th> <th></th> <th>OPENNING</th> <th>SWIG</th>	$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$		3	i			Beege	HIGHA	HIOM	5 er	CESTRIAN	CAPACITY	DEMAND	RATE	2		OPENNING	SWIG
85% 888 6.5 1.6 1	0 SSAL SSAL <t< td=""><td>LAMASELAMA</td><td>-</td><td>950</td><td></td><td>Ľ</td><td>SBB</td><td>5.34</td><td></td><td>1</td><td></td><td>1405</td><td>345</td><td>5.7</td><td>0.25</td><td>2114</td><td></td><td></td></t<>	LAMASELAMA	-	950		Ľ	SBB	5.34		1		1405	345	5.7	0.25	2114		
0 55.4 58 50.0 1 105 106 106 54.4 0.0 7.M 588 50.0 1 105 50.0 106 54.4 0.0 7.M 589 50.0 1 105 50.0 106 54.4 0.0 7.M 589 50.0 106 54.4 0.0 106 54.4 0.0 7.M 509 500 0<	Sinch Sinch <th< td=""><td>PAHANG I JERANTUT 1</td><td>-</td><td>930</td><td>6</td><td></td><td>SBB</td><td>6.30</td><td></td><td></td><td></td><td>1405</td><td>169</td><td>5,4</td><td>0.12</td><td>2123</td><td></td><td></td></th<>	PAHANG I JERANTUT 1	-	930	6		SBB	6.30				1405	169	5,4	0.12	2123		
3 874 888 500 10 106	3 874 888 500 10 100 54 0.01 3 874 886 500 10 100 100 54 0.01 3 75 600 500 100 100 100 100 100 3 874 886 500 100 100 100 100 100 3 874 886 500 100 100 100 100 100 3 874 886 500 100 100 100 100 100 3 874 886 500 100 100 100 100 100 3 874 886 500 100 100 100 100 100 3 874 886 500 100 100 100 100 100 3 874 886 500 100 100 100 100 100 3 814 816 500 100 100 100 100 3 814 816 500 100 100 100 100 3 814 816 500 616 616	JERANTUT		1930	3		SBB	6.15				1405	169	5.4	0.12	2123		
3 974 56 57 10 105 3 974 566 500 100 100 9 974 566 500 100 100 9 974 566 500 100 100 9 974 566 500 100 100 9 974 566 500 100 100 9 974 566 500 100 100 9 974 100 100 100 100 9 974 100 100 100 100 9 974 100 100 100 100 9 974 100 100 100 100 9 974 100 100 100 100 9 974 100 100 100 100 9 974 100 100 100 100 9 974 100 100 100 100 9 974 100 100 100 100 9 974 100 100 100 100 9 974 100 100 100	9 9 <td>JERANTUT</td> <td></td> <td>1930</td> <td>Ð</td> <td>STAL</td> <td>SBB</td> <td>5.60</td> <td></td> <td></td> <td></td> <td>1405</td> <td>169</td> <td>5.4</td> <td>0.12</td> <td>2123</td> <td></td> <td></td>	JERANTUT		1930	Ð	STAL	SBB	5.60				1405	169	5.4	0.12	2123		
9 PAA 589 566 1 140 146 168 573 169 574 100 100 574 100 576 100 576 100 576 100 576 100 576 100 576 100 576 100	0 P/M 588 656 1 </td <td>JERANTUT</td> <td></td> <td>1930</td> <td>0</td> <td>STAL</td> <td>SBB</td> <td>5.70</td> <td></td> <td></td> <td></td> <td>1405</td> <td>169</td> <td>5.4</td> <td>0.12</td> <td>2183</td> <td></td> <td></td>	JERANTUT		1930	0	STAL	SBB	5.70				1405	169	5.4	0.12	2183		
3 PAR R58 558 146 145 3 PAR R58 558 138 146 3 Sixt Sixt Sixt Sixt 36 44 23 3 Sixt Sixt Sixt Sixt 185 147 146 3 Sixt Sixt Sixt Sixt 185 147 146 3 Sixt Sixt Sixt Sixt 185 147 146 3 Sixt Sixt Sixt Sixt Sixt 185 147 146 3 Sixt Sixt Sixt Sixt Sixt Sixt 146 185 3 Sixt Sixt Sixt Sixt Sixt Sixt Sixt 144 Sixt 3 Sixt Sixt Sixt Sixt Sixt Sixt Sixt 144 3 Sixt Sixt Sixt Sixt Sixt Sixt Sixt 144 Sixt 3 Sixt Sixt Sixt Sixt Sixt Sixt Sixt Sixt Sixt 3 Sixt Sixt Sixt Sixt Sixt	9 PAR RSB 550 Par			1930	8	P/A	SBB	6.65				1490	169	5.4		2125		
3 5 7.4 7.33 0.50 1.54 7.33 0.50 3 5.14 7.33 0.50 1.54 7.33 0.50 1.54 7.33 3 5.14 7.33 0.50 1.56 1.46 1.55 1.73 0.50 3 5.14 7.33 0.50 1.56 1.47 7.33 1.56 1.47 3 5.50 5.50 1.56 1.56 1.46 1.55 1.7 2.33 0.17 3 5.50 5.50 1.56 7.34 1.56 7.34 1.56 7.34 0.73 3 5.51 7.34 1.56 7.34 1.56 7.35 0.74 3 5.51 1.56 7.34 1.56 7.35 0.74 3 5.51 1.56 7.34 1.55 7.35 0.17 5 5.51 1.56 7.36 1.56 7.35 0.17 5 5.51 5.56 1.56 7.35 1.55 7.35 0.17 5 5.51 5.56 1.56 7.35 1.55 7.35 0.17 5 5.51 5.56 1.56 1.55 1.5	2 3 5 4 0 <td></td> <td>-+</td> <td>1930</td> <td>5</td> <td>P/A</td> <td>SBB</td> <td>5.60</td> <td></td> <td>-</td> <td></td> <td>1405</td> <td>169</td> <td>5.4</td> <td>0.12</td> <td>2123</td> <td></td> <td></td>		-+	1930	5	P/A	SBB	5.60		-		1405	169	5.4	0.12	2123		
3 5/1 7/1 7/2 7/20 7/20 7/20 7/20 3 5/1/L 7/2 7/20 7/20 7/20 7/20 7/20 7/20 3 5/1/L 7/2 7/20 7/20 7/20 7/20 7/20 7/20 2 5/1/L 7/2 7/20 7/20 7/20 7/20 7/20 7/20 2 5/1/L 7/2 7/20 7/20 7/20 7/20 7/20 7/20 2 5/1/L 7/2 7/20 7/20 7/20 7/20 7/20 7/20 2 5/1/L 7/20 7/20 7/20 7/20 7/20 7/20 7/20 2 5/1/L 7/20 7/20 7/20 7/20 7/20 7/20 7/20 2 7/2/L 5/20 7/20 7/20 7/20 7/20 7/20 7/20 2 7/2/L 5/20 7/20 7/20 7/20 7/20 7/20 7/20 2 7/2/L 5/20 7/20 7/20 7/20 7/20 7/20 7/20 2 5/2/L 5/20 1/1/20 5/20 1/1/20 5/20 7/2	3 5 5 7 7 <td>-</td> <td>· 🕴</td> <td>1995</td> <td></td> <td></td> <td>200</td> <td>000</td> <td></td> <td></td> <td></td> <td>1022</td> <td>0/0</td> <td>4.4</td> <td>200</td> <td>3</td> <td></td> <td></td>	-	· 🕴	1995			200	000				1022	0/0	4.4	200	3		
3 3 3 3 4 4 0 3 3 4 4 0 3 3 3 3 4 4 4 4 4 4 3 3 3 4 4 4 4 4 4 3 3 3 4 4 4 4 4 4 3 3 5 6 4 6 6 6 0 3 5 6 6 6 6 6 0 3 5 6 6 6 6 0 1 4 5 6 6 6 6 0 1 5 5 6 6 6 6 0 1 6 6 6 6 6 6 0 1 7 8 6 6 6 6 0 1 1 7 8 6 6 6 6 0 1 8 6 6 6 6 6 0 1 8 6 6 6 6 6 0 7 <td>2 5 5 5 5 5 5 5 5 2 5 5 5 5 5 5 5 5 2 5 5 5 5 5 5 5 5 3 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5<td>KMUUASIK</td><td>~t-</td><td>1040</td><td></td><td>P/A STAL</td><td>222</td><td>080</td><td>-†</td><td>001</td><td></td><td>1822</td><td>5/6</td><td>4 4</td><td></td><td>855</td><td></td><td></td></td>	2 5 5 5 5 5 5 5 5 2 5 5 5 5 5 5 5 5 2 5 5 5 5 5 5 5 5 3 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 <td>KMUUASIK</td> <td>~t-</td> <td>1040</td> <td></td> <td>P/A STAL</td> <td>222</td> <td>080</td> <td>-†</td> <td>001</td> <td></td> <td>1822</td> <td>5/6</td> <td>4 4</td> <td></td> <td>855</td> <td></td> <td></td>	KMUUASIK	~t-	1040		P/A STAL	222	080	-†	001		1822	5/6	4 4		855		
2 2 <td>3 3<td>BALING</td><td></td><td>1950</td><td>2</td><td>STAL</td><td>24</td><td>394</td><td>$^{+}$</td><td>5</td><td></td><td>1800</td><td>578</td><td>200</td><td>0.30</td><td>2153</td><td></td><td></td></td>	3 3 <td>BALING</td> <td></td> <td>1950</td> <td>2</td> <td>STAL</td> <td>24</td> <td>394</td> <td>$^{+}$</td> <td>5</td> <td></td> <td>1800</td> <td>578</td> <td>200</td> <td>0.30</td> <td>2153</td> <td></td> <td></td>	BALING		1950	2	STAL	24	394	$^{+}$	5		1800	578	200	0.30	2153		
0 5/K F 7/3 7/0 L8 11 7/3 1/0 0 5/K F 7/3 7/0 L8 11 1/3 1/3 1/3 0/3 5/K 5/K 5/K 5/K 1/3 1/3 1/3 1/3 1/3 1/3 1/3 5/K 5/K 5/K 5/K 1/3 1/3 1/3 1/3 1/3 1/3 5/K 5/K 5/K 5/K 5/K 5/K 1/3 1/3 1/3 5/K 5/K 5/K 5/K 5/K 1/3 1/3 1/3 5/K 5/K 5/K 5/K 5/K 1/3 1/3 5/K 5/K 5/K 5/K 5/K 5/K 0/1 5/K 5/K	0 5/K 1 1 2/3 1 0 0 0 5/K 1 5/3 1 1 1 1 1 1 1 5/K 5/K 1 5/K 1 1 1 1 1 1 5/K 5/K 1 1 1 1 1 1 1 1 5/K 1 1 1 1 1 1 1 1 1 1 5/K 1 1 1 1 1 1 1 1 1 1 1 5/K 1 1 1 1 1 1 1 1 1 1 1 5/K 1 1 1 1 1 1 1 1 1 1 1 5/K 1 1 1 1 1 1 1 1 1 1 1 5/K 1 1 1 1 1 1 1 1 1 1 1 1 5/K 1 1 1 1 1 1 1 1 1 1 1 1<	HLR PERAK	+	1950	0	STAL	SBB	7.02	Ť			1551	417	-3.3	0.27	NIA		
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	2 2 2 1 2 <td>HLR PERAK</td> <td>-}-</td> <td>1970</td> <td>8</td> <td>STAL</td> <td>11</td> <td>7 34</td> <td>1.08</td> <td>18.9</td> <td></td> <td>1551</td> <td>412</td> <td>-33</td> <td>0.27</td> <td>A/N</td> <td></td> <td></td>	HLR PERAK	-}-	1970	8	STAL	11	7 34	1.08	18.9		1551	412	-33	0.27	A/N		
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x STA SSB Field A SSB 5.80 7.00 R SS SS <ths< th=""> SS <t< td=""><td>x x</td><td>K KANGSAR</td><td></td><td>1950</td><td>2</td><td>SSAL</td><td>SBB</td><td>5.70</td><td></td><td>-</td><td></td><td>1431</td><td>258</td><td>5.0</td><td>0.18</td><td>2133</td><td></td><td></td></t<></ths<>	x x	K KANGSAR		1950	2	SSAL	SBB	5.70		-		1431	258	5.0	0.18	2133		
0 554 1550 258 55 0 554 560 1550 258 55 0 574 586 570 1550 258 55 0 574 586 570 144 256 61 0.1 1 144 586 5.00 1144 256 66 0.2 1 144 586 5.00 1144 256 66 0.2 1 144 586 5.00 1160 256 66 0.2 1 506 506 1160 256 66 0.2 1 506 506 1160 256 66 0.2 1 506 506 1150 256 66 0.2 1 506 506 1550 1550 256 66 0.2 1 506 506 1550 1550 256 66 0.2 1 506 506 1550 1550 256 61 0.2 1 506 61 1550 1550 1550 1550 150 1 507 506 1550 1550 155	0 354 396 556 1550 258 55 0.1 0 574 396 556 1550 258 55 0.1 1550 574 396 570 1550 258 55 0.1 1550 574 396 570 110 355 55 0.1 1550 554 396 570 110 355 55 0.1 1550 554 396 570 110 355 55 0.1 1650 554 396 570 110 355 55 0.1 1650 554 396 570 110 355 55 0.1 1650 554 396 570 110 355 55 0.1 1650 554 396 570 110 355 35 110 355 1714 356 6.23 4.85 4.85 4.85 35 35 36 0.0 1744 356 6.23 4.85 4.85 4.85 37 4.9 0.35 1745 356 6.23 4.95 1.550 271 274 0.05 <	K KANGSAR	1-	1950	4	STAL	SBB	5.80	1.06	æ		1550	258	5.5	6.17	2122		
3 554 569 570 1550 259 55 0.1 3 574 588 570 1104 559 55 0.1 3 574 588 570 1104 559 55 0.1 3 574 588 500 1104 559 55 0.1 3 574 588 500 1104 555 6.0 0.1 3 534 588 500 1104 555 6.0 0.2 5 50 536 500 1104 555 6.0 0.2 5 50 536 50 1104 555 55 0.1 5 534 588 5.0 1104 555 55 0.1 5 534 588 5.0 1104 555 1104 0.25 5 5 5 5 5 5 5 5 0.1 5 5 5 6 5 5 5 5 5 5 5 5 6 5 5 5 5 5 5 5 6 6 5 5	0 554 560 1550 258 55 0.17 1 570 1 1550 258 55 0.17 2 554 570 1 144 255 0.17 353 556 1 1 144 255 0.17 353 556 1 1 1 144 255 0.17 353 556 1 1 1 1 255 0.17 353 556 1 1 1 1 255 0.17 353 556 536 66 0.23 1 0.22 353 556 64 1 1 1 1 0.22 354 358 6.36 6.6 0.16 0.23 1 1 355 556 6.40 1 1 1 1 1 355 556 6.40 1 1 1 0.27 1 355 556 6.55 1 1 1 1 0 355 556 6.55 1 1 1 1 1 355 554 556 6.55 1 </td <td>HULU PERAK</td> <td>┝</td> <td>1950</td> <td>0</td> <td>SSAL</td> <td>See</td> <td>5.60</td> <td></td> <td></td> <td></td> <td>1550</td> <td>258</td> <td>5.5</td> <td>10.17</td> <td>2122</td> <td></td> <td></td>	HULU PERAK	┝	1950	0	SSAL	See	5.60				1550	258	5.5	10.17	2122		
0 51AL 36i 700 1500 256 600 011 1 31AL 36i 570 1104 256 60 021 2 55AL 36i 5.00 1104 355 66 0.22 2 55AL 36i 5.00 1104 355 66 0.22 3 55AL 36i 6.00 0.11 1046 355 0.0 3 55AL 36i 6.00 0.12 1104 355 0.0 3 55AL 36i 6.00 0.16 1104 355 0.0 3 55AL 36i 6.00 0.16 0.22 0.17 3 55AL 36i 6.00 0.16 0.16 0.22 3 55AL 36i 6.00 0.16 0.16 3 55AL 566 6.00 0.16 3	0 51AL 361 700 1150 253 60 0.1 2 53AL 386 5.0 1104 253 66 0.2 2 53AL 386 5.0 1104 253 66 0.2 2 53AL 386 5.0 1104 253 66 0.2 3 53AL 386 5.0 1104 253 146 0.2 3 53AL 386 5.0 1105 277 7.4 0.2 3 53AL 586 6.1 0.2 1550 277 7.4 0.2 3 53AL 586 6.1 0.2 1550 1550 277 7.4 0.2 3 53A 53A 1350 4.6 0.2 0.2 0.7 3 53A	HULUPERAK	╄	1950	0	SSAL	SBB	5,60				1550	258	5.5	0.17	2122		
3 57.4L 589 570 1445 258 6.0 0.19 3 53.4L 589 5.00 1104 583 6.0 0.29 3 53.4L 589 5.00 1104 583 6.0 0.29 5 55.4L 589 5.00 1104 583 6.0 0.29 5 55.4L 589 6.27 1.104 583 6.0 0.29 5 55.4L 589 6.27 1.104 583 6.0 0.29 5 55.4L 589 6.27 1.104 583 7.4 0.29 5 55.4L 589 6.27 1.105 233 7.4 0.29 5 55.4L 589 6.27 1.106 533 7.4 0.29 5 55.4L 589 6.21 1.106 233 7.4 0.29 5 5 5 6.16 0.29 277 7.4 0.29 5 5 5 6.16 0.29 277 7.4 0.29 5 5 5 1.106 5 1.106 5 0.10 5 5 5 <	3 574. 388 570 11645 258 6.0 0.19 3 514. 388 5.00 1164 258 6.0 0.29 3 534. 388 5.00 1164 258 6.0 0.29 3 534. 388 5.00 1164 258 6.0 0.29 3 534. 388 5.00 1164 258 6.0 0.29 3 534. 388 5.00 1164 258 6.0 0.29 3 534. 388 5.00 1164 258 6.0 0.29 3 534. 388 6.0 1164 258 6.0 0.29 3 534. 388 6.29 4.0 1164 258 2.1 1164 3 534. 388 6.8 0.8 1164 2.28 0.6 0.29 3 534. 388 6.8 0.8 1156 2.1 114 0.02 3<54.	HULU PERAK	-	1950	0	STAL	SBB	2.00				1530	258	8.0	0.17	2081		
3 57AL 589 6.65 1104 553 6.6 0.032 5 500 500 1104 553 6.6 0.032 5 500 500 1104 553 6.6 0.032 5 500 500 1104 553 174 0.03 5 5 6 6.0 5 170 175 174 0.03 5 5 6 6 6 0.03 175 174 0.03 5 5 6 6 6 0.03 175 174 0.03 5 5 6 6 6 0.03 175 174 0.03 5 7 889 6.21 1750 277 174 0.03 5 7 5 0.14 1550 277 174 0.03 5 7 5 0.21 1550 4.15 0.16 0.02 5 7 5 0.21 1550 4.16 0.17 0.02 5 7 5 0.21 1550 4.16 0.16 0.02 7 7 5 0.21 1550 4	3 5:AL 539 6.65 1104 553 6.6 0.032 3 5:AL 539 5.06 1104 553 6.6 0.032 3 5:AL 539 5.06 1104 553 6.6 0.032 5 5:AL 539 6.50 1104 553 14 0.16 5 5:AL 539 6.50 1104 553 154 0.02 5 5:AL 539 6.50 1104 553 154 0.02 5 5 6.6 6.75 1550 217 7.4 0.16 5 5 5 6.8 6.25 1550 217 7.4 0.016 5 5 5 5 6.8 1.025 1.164 5<5	HULUPERAK	\vdash	19SC	0	STAL	888	5.70				1443	258	8.0	0.18	2080		-
2 SSAL SSB 5.00 11(44) 855 6.6 0.022 3 SSAL SSB 5.00 11(52) 353 7.4 0.022 3 SSAL SSB 6.02 353 7.4 0.022 3 STAL SSB 6.02 353 7.4 0.022 3 STAL SSB 6.02 353 7.4 0.021 3 STAL SSB 6.03 4.65 4.15 9.15 7.4 0.021 3 STAL SSB 6.03 4.65 4.15 9.15 2.7 7.4 0.021 3 STAL SSB 4.65 4.15 11500 2.77 7.4 0.021 3 STAL SSB 4.65 4.15 11500 2.77 7.4 0.021 3 STAL SSB 6.23 4.16 9.16 0.021 9.021 3 STAL SSB 6.23 4.16 9.16 0.021 3 STAL SSB 6.23 6.23 0.01 0.01 3 STAL SSB 6.23 6.23 0.01 0.021 3 STAL	2 SSAL 383 5.00 1104 383 6.6 0.02 3 SSAL 389 5.05 1104 383 7.4 0.02 3 SSAL 389 5.36 1520 353 7.4 0.02 3 SSAL 389 5.36 1520 353 7.4 0.03 3 SSAL 389 5.36 1520 353 7.4 0.03 3 SSAL 389 5.31 1530 353 7.4 0.03 3 SSAL 389 6.40 1530 353 7.4 0.03 3 SSAL 389 6.31 1530 415 9.1 0.7 3 SSAL 389 6.21 1530 415 9.1 0.7 3 SSAL 389 6.21 1530 415 9.1 0.7 3 SSAL 389 6.21 1530 416 0.03 3 STAL 589 6.21 1530 416 0.01 3 STAL 589 6.21 0.1 0.21 0.21 3 STAL F63 6.1 0.21 0.21	SEREMBAN		1950	e)	STAL	SBB	6.95				1104	353	6.6	0.32	2089		
3 SSAL SS6 5.06 1104 SS3 5.0 3 SSAL SS6 6.02 7.4 0.22 3 SSAL SS6 6.02 3.33 7.4 0.22 3 SSAL SS6 6.02 4.05 0.02 3.33 7.4 0.22 3 SSAL SS6 6.03 6.03 7.4 0.23 7.4 0.22 3 SSAL SS6 4.05 0.05 4.05 0.05 3.33 7.4 0.22 3 SSAL SS6 4.01 1500 4.15 7.7 0.16 0.21 3 SSAL SS6 4.01 1500 4.15 1500 4.15 0.17 3 SSAL SS6 4.01 1500 4.16 1500 2.1 0.27 3 SSAL SS6 4.01 1500 4.16 0.27 0.17 3 SSAL SS6 4.01 1500 4.16 0.27 3 SSAL SS6 4.01 1500 4.16 0.27 3 SSAL SS6 4.01 1.02 1.02 3 SS6 4.01	3 SSAL S86 5.06 1104 353 6.6 0.32 3 SSAL S89 6.34 589 6.34 0.02 3 SSAL S89 6.34 1104 353 7.4 0.22 3 SSAL S89 6.34 1530 353 7.4 0.22 3 SSAL S89 6.34 1530 353 7.4 0.22 3 SSAL S89 4.45 1.530 2.77 7.4 0.27 3 SSAL S89 4.45 1.530 2.77 7.4 0.27 3 SSAL S89 4.45 1.530 2.77 7.4 0.27 3 SSAL S89 4.45 1.530 4.15 9.1 0.27 3 SAL S89 4.45 1.530 4.15 9.1 0.27 3 SAL S89 4.45 1.530 4.15 9.1 0.27 3 SAL S89 4.15 9.1 0.27 1.24 0.27 3 SAL S89 4.16 1.530 4.16 0.27 3 SAL POS SAL <	SEREMBAN	_	1950	2	SSAL	888	5.00				1.04	353	6.6	0.32	2089		1
3 SSAL SSB 632 1622 333 7.4 0.02 3 SSAL SSB 6.34 4.65 LMR 1715 7.4 0.02 3 SSAL SSB 6.33 4.65 LMR 1715 277 7.4 0.02 3 SSAL SSB 4.65 LMR 1715 277 7.4 0.02 3 SSAL SSB 4.65 LMR 1550 277 7.4 0.02 3 SSAL SSB 4.65 LMR 1550 277 7.4 0.02 3 SSAL SSB 4.65 1550 4.16 0.27 24 0.02 3 SSAL SSB 4.65 1550 4.16 0.27 24 0.02 3 SSAL SSAL SSB 4.65 1.550 4.16 0.27 24 3 SSAL SSA SSA SSA 1.550 4.16 0.27 27 3 SSAL SSA SSA SSA 1.550 4.16 0.27 0.27 3 SSAL SSA SSA SSA 1.550 4.16 0.27 0.27 <	3 SSAL SSB 632 74 022 3 SSAL SSB 633 1713 74 023 3 SSAL SSB 633 455 LMR 74 033 3 SSAL SSB 455 LMR 713 023 3 STAL SSB 4.65 LMR 713 023 3 SSAL SSB 4.65 LMR 714 013 3 SSAL SSB 4.65 LMR 714 013 3 SSAL SSB 4.65 LMR 1550 217 7.4 013 3 SSAL SSB 4.65 L 1550 4.16 0.17 1550 217 0.27 3 SSAL SSB 6.21 1550 4.16 0.17 0.27 1550 A.16 SSAL SS6 0.21 1550 0.16 0.27 1 NLL SS6 0.21 1550 4.16 0.17 0.27 1 SS6 0.21 SSAL SS6 0.21 0.27 1 NLL SS6 0.21 1550 4.16 0.17	SEREMBAN	-	1950	n	SSAL	SBB	5.05				1104	353	6.B	0.32	2089		
3 SSAL 388 6.34 1530 335 7.4 0.020 3 STAL 888 6.34 1550 277 7.4 0.03 3 SSAL 888 6.23 1550 277 7.4 0.03 3 SSAL 888 4.85 1550 277 7.4 0.03 3 SSAL 888 4.81 1550 215 7.4 0.03 3 SSAL 888 4.81 1550 215 7.4 0.03 3 SSAL 888 6.231 1550 216 0.02 4 1550 4.16 1550 4.16 0.02 1550 6.231 1550 4.16 0.02 1550 6.231 1550 4.16 0.02 1550 6.231 1550 4.16 0.02 1550 6.23 1550 4.15 0.02 1550 6.1 1550 4.15 0.02 1550 6.1 1550 4.15 0.02 1550 110 215 140 1550 140 1550 110 1550 150 150 1	334 338 6.34 1530 335 7.4 0.05 574 838 6.34 1530 335 7.4 0.05 574 838 6.23 4.55 0.63 277 7.4 0.05 74 838 6.24 1530 355 1550 277 7.4 0.05 754 838 4.40 1550 4.55 4.65 4.60 1550 277 7.4 0.05 754 838 4.40 1550 4.65 4.65 4.65 4.65 0.07 754 838 6.21 1550 4.15 9.1 0.07 9.1 0.07 755 838 6.21 1550 4.15 9.1 0.07 755 838 6.21 1550 4.15 0.07 755 838 6.21 1550 4.15 0.07 755 74 9.05 1550 4.15 0.07 755 74 74 0.07 1550 4.15 0.07 755 74 765 74 0.07 1550 1550 755 74 765 74 76 77 155	SEREMBAN		1950	e	SSAL	SBB	6.92				1622	353	7.4	80	2068		
3 SML SSE 6.20 4.65 4.86 1.715 2.77 7.4 0.16 3 SSAL SSE 4.20 4.65 4.65 4.65 4.77 7.4 0.16 3 SSAL SSE 4.65 4.65 4.65 4.65 4.67 7.4 0.16 3 SSAL SSE 4.67 1.500 4.13 1.500 4.13 0.27 3 SSAL SSE 4.61 1.500 4.19 1.500 4.19 0.27 3 SSAL SSE 6.21 1.500 4.19 1.500 4.19 0.27 3 SSAL SSE 6.21 1.500 4.19 0.27 0.27 1 ROS 6.21 1.500 4.19 0.27 0.27 1 ROS 6.21 1.500 4.19 0.27 1 ROS 6.21 1.500 4.19 0.27 1 ROS 6.21 1.600 1.100 0.27 2 MrAL ROS 8.10 0.16 0.16 2 MrAL ROS 1.000 1.000 2 MrAL ROS 1.000 </td <td>3 SSAL SS8 6.20 4.65 4.66 1.715 2.77 7.4 0.16 3 SSAL SS8 4.69 1.50 2.77 7.4 0.16 3 SSAL SS8 4.69 1.50 2.77 7.4 0.16 3 SSAL SS8 4.69 1.50 2.77 7.4 0.16 3 SSAL SS8 4.69 1.500 4.13 0.27 0.27 3 SSAL SS8 6.21 1.500 4.19 0.27 0.27 3 SSAL SS6 6.21 1.500 4.19 0.27 0.27 3 SSAL SS6 6.21 1.500 4.19 0.27 0.27 1 RC8 6.21 1.500 4.19 0.27 0.27 1 RC8 6.21 1.500 4.19 0.27 0.27 1 RC8 6.21 1.600 1.600 1.600 0.16 2 STAL RC8 6.21 1.600 1.600 0.16 2 STAL RC8 6.21 1.600 1.600 0.16 2 STAL RC8 6.100<td>SEREMBAN-</td><td></td><td>1950</td><td>6</td><td>SSAL</td><td>SBB</td><td>6.34</td><td></td><td></td><td></td><td>1530</td><td>353</td><td>7.4</td><td>80</td><td>2087</td><td></td><td></td></td>	3 SSAL SS8 6.20 4.65 4.66 1.715 2.77 7.4 0.16 3 SSAL SS8 4.69 1.50 2.77 7.4 0.16 3 SSAL SS8 4.69 1.50 2.77 7.4 0.16 3 SSAL SS8 4.69 1.50 2.77 7.4 0.16 3 SSAL SS8 4.69 1.500 4.13 0.27 0.27 3 SSAL SS8 6.21 1.500 4.19 0.27 0.27 3 SSAL SS6 6.21 1.500 4.19 0.27 0.27 3 SSAL SS6 6.21 1.500 4.19 0.27 0.27 1 RC8 6.21 1.500 4.19 0.27 0.27 1 RC8 6.21 1.500 4.19 0.27 0.27 1 RC8 6.21 1.600 1.600 1.600 0.16 2 STAL RC8 6.21 1.600 1.600 0.16 2 STAL RC8 6.21 1.600 1.600 0.16 2 STAL RC8 6.100 <td>SEREMBAN-</td> <td></td> <td>1950</td> <td>6</td> <td>SSAL</td> <td>SBB</td> <td>6.34</td> <td></td> <td></td> <td></td> <td>1530</td> <td>353</td> <td>7.4</td> <td>80</td> <td>2087</td> <td></td> <td></td>	SEREMBAN-		1950	6	SSAL	SBB	6.34				1530	353	7.4	80	2087		
3 STAL RCB 6.28 1500 277 7.4 0.16 3 PiA SSAL S86 4.40 1500 277 7.4 0.16 3 PiA S86 4.61 1500 277 7.4 0.74 3 SSAL S86 4.61 1500 4.15 0.16 2 MiAL S86 6.21 1560 4.15 0.27 2 STAL S86 6.21 1560 4.16 0.27 3 S5AL S86 6.21 1560 4.16 0.27 2 MiAL R386 6.21 1560 4.16 0.27 2 STAL R386 6.21 1.00 1.16 2 STAL R08 9.1 0.27 2 STAL R08 9.1 0.27 2 STAL R08 9.1 0.27 2 STAL R	3 STAL RC8 6.29 11500 277 7.4 0.16 3 PIA SSAL SSAL SSA 6.1 0.17 3 PIA SSA SSA 1500 277 7.4 0.16 3 PIA SSA SSAL SSA 6.1 0.27 3 SSAL SSA SSA 1500 4.15 6.1 0.27 3 SSAL SSA SSA 1550 4.15 6.1 0.27 1 SSA SSA SSA 1550 4.16 0.27 1 PC3 SSA SSA 1550 4.16 0.27 1 PC3 SSA SSA 1550 4.16 0.27 1 PC3 PC3 PC3 PC3 PC3 PC3 1 PC3 PC3 PC3 PC4 PC3 1 PC3 PC3 PC4 PC4 1 PC4 PC3 PC4 </td <td>JELEBU</td> <td>-</td> <td>1950</td> <td>0</td> <td>SSAL</td> <td>SBB</td> <td>8.20</td> <td>4.85</td> <td>L&R</td> <td></td> <td>1715</td> <td>277</td> <td>7.4</td> <td>0,16</td> <td>2090</td> <td></td> <td></td>	JELEBU	-	1950	0	SSAL	SBB	8.20	4.85	L&R		1715	277	7.4	0,16	2090		
3 3 <td>3 35AL 386 440 1500 45 5 55AL 586 440 1500 45 6 1 100 1500 45 6 1 100 1500 45 6 1 100 1500 45 7 1 100 1500 45 8 621 1 100 1 1 100 1 1 1 100 1 1 1 1 0 1 1 1 0 1 1 1 0 1 1 1 0 1 1 1 0 1 1 1 0 1 1 1 0 1 1 1 0 1 1 1 0 1 1 1 0 1 1 1 0 1 1 1 0 1 1 1 0 1 1 1 0 1 1 1 0 1 1 0</td> <td>I JELEBU</td> <td>÷</td> <td>980</td> <td>Ø</td> <td>STAL</td> <td>RCB</td> <td>6.29</td> <td></td> <td></td> <td></td> <td>1530</td> <td>277</td> <td>7.4</td> <td>0.18</td> <td>2088</td> <td></td> <td></td>	3 35AL 386 440 1500 45 5 55AL 586 440 1500 45 6 1 100 1500 45 6 1 100 1500 45 6 1 100 1500 45 7 1 100 1500 45 8 621 1 100 1 1 100 1 1 1 100 1 1 1 1 0 1 1 1 0 1 1 1 0 1 1 1 0 1 1 1 0 1 1 1 0 1 1 1 0 1 1 1 0 1 1 1 0 1 1 1 0 1 1 1 0 1 1 1 0 1 1 1 0 1 1 1 0 1 1 1 0 1 1 0	I JELEBU	÷	980	Ø	STAL	RCB	6.29				1530	277	7.4	0.18	2088		
3 3 <td>3 5 5 1 3 5 5 1 1 3 5 5 5 <t< td=""><td></td><td>+</td><td>1950</td><td>6</td><td>SSAL</td><td>SBB</td><td>4.40</td><td></td><td></td><td></td><td>1530</td><td>415</td><td>6</td><td>0.27</td><td>8/02</td><td></td><td></td></t<></td>	3 5 5 1 3 5 5 1 1 3 5 5 5 <t< td=""><td></td><td>+</td><td>1950</td><td>6</td><td>SSAL</td><td>SBB</td><td>4.40</td><td></td><td></td><td></td><td>1530</td><td>415</td><td>6</td><td>0.27</td><td>8/02</td><td></td><td></td></t<>		+	1950	6	SSAL	SBB	4.40				1530	415	6	0.27	8/02		
			+	0261	<u></u>	r/A	ABS	4.61				0221	415		12.0	20/02		
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E – 4



FINAL SELECTION REMARKS SELECTED SA SECTED G G G G SELECTED SA SELECTED SA SELECTED SA SELECTED CA SELECTED CA SELECTED CA SELECTED CA SELECTED CA Š SELECTED [SA 88853388 STRUCTURAL CONDITION CONCEIVABLE REHABILITATION CONCEIVABLE REHABILITATION BEAM SCOU- CONCEIVABLE PLANS PLANS DECK RING AVERAGE FROM STRUCTURAL VIEW POINT FROM RUNCTIONAL VIEW POINT fotal no's of bridges selected = 0 Total no's of bridges selected = 4 Total no's of bridges selected = 1 Total no's of bridges selected = 1 otal no's of bridges selected = 5 ADDING SDE WALK ADDING & RAISING ADDING SDE WALK ADDING SDE WALK 1.5 (SPRE SFRE 2.0 (JPRE BPRE) 2.0 (JPRE BPRE) 2.0 (JPRE BPRE) 2.5 (SRFE APRE SFRE 2.5 SELECTION OF 100 BRIDGES FOR VISUAL INSPECTION 1.3 BRP,SRPR 1.3 EJRP 20 NON 23 ARF 23 ARF 23 ARF 23 ARF 25 ARF 25 ARF 20 ARF 30 ARF 30 ARF 30 CRF 33 DCRF 33 DCRF 33 DCRF 33 DCRF 3.3 ARF 8 30.431 PCB 2 1 1 1 0 e PIER 4 ABUT. 24.80 24.80 152.88 122.88 1122.98 1122.99 122.99 122.99 122.99 122.18 122.99 122.18 122.99 122.18 122.99 122.18 122.99 122.18 122.99 122.18 122.99 1 2,18 BOX RPGE BRDGE 2.40 BOX 4.88 BOX 3.69 BOX 3.69 BOX 3.69 BOX 3.68 BOX 2.288 BOX 2.298 BOX 2. PCB PCB PCB 25.91 26.24 26.17 26.17 26.17 26.17 26.17 27.00 24.57 21.98 24.57 21.98 BRIDGE LENGTH (M) B 219.13 35.21 18.40 APPENDIX-F - 0 MAX. NO. 1 SPAN OF 1 (M) SPAN 9 12.13 15.08 15.08 16.45 12.09 11.209 11.50 11.50 14.60
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 3 MTAL 30.491 MTAL 2.18 57AL 57AL 57AL 57AL 57AL 57AL 57AL YEAR STUDY BUILT CATEGORY CAPACITY STAL << TYPE OF BRIDGE PCB --- P.C. beam, R.C. stab >> << TYPE OF SPEDGE IT ----Inverted tee beam >> 1980 1965 1972 1972 1972 1972 1976 1976 1976 1982 1965 1964 1970 1970 1961 1968 1974 1963 1001000000 JUCH < 1945 ***** 100100000 JUCHOR [KUUANG] 1827] 100810-05 of bridges = 1 1965 << TYPE OF BRUGE BOX --- RC, box >> 1970

 1346

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APPENDIX-F SELECTION OF 100 BRIDGES FOR VISUAL INSPECTION

ON FINAL SELECTION REMARKS		SELECTED CG	SELECTED SELECTED		Stearte Steart	SELECTED SA SELECTED CA 2	SELECTED SEL
CONCEIVABLE REHABILITATION PLANS FROM FUNCTIONAL VIEW POINT		Total no's of bridges selected # 1		ADDING SDE WALK ADDING SDE WALK ADDING & WDE NIKS	ADDING & PAUSING ADDING & PAUSING Total no's of brogges selected = 1	FAISING GPADE	ADDING SDE WALK ADDING SDE WALK ADDING SDE WALK ADDING SDE WALK ADDING SDE WALK
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3.0 CBRF.DCRF.SPP R
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 | 1.0 NON | 2.0 BHP.ARF

 | 2.3 JAH, PAF
2.6 IDCRF, ARPA SFRF | 2.5 SRP,DCPR,APR | 25 DCPR,EJRP,SFRF,CBPR
 | 2.5 APR.PRF | 2.7 DCRF,APR | 2.7 (ARF | 3.0 DCPR | 3.0 DCRF | 3.0 DCPH,Arr-SHPP, BSPH
3.5 DCRF, AFPR, SFRF | 3.5 ARF,SHPR | 35 PPH
3.5 DCRF,APR,PPR,BSPR

 | 3.7 OCRF, APR, PPR, SFRF | | 2.0 SBPR | 2.0 DSPR | 2.0 SEPR,SRP,DSPR
2.0 SEPR.DSPR | 2.3 SEPR,DSPR,SRAP | 2.3 SBPR.SRPR
 | 2.7 SBPR.APR | 2.7 SEPR.CBRF | 2.7 SEPRIDSPR | 2.7 ISBPH,DSPH,APH
2.7 ISBPR,DSPH,ARF | 3.0 DSRP, SFRF | 3.0 I SEPRIDSPR
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to's of bridges = 29 | TPE OF BRIDGE | YEAR BUILT < 1945 | 8100 KELANTAN | to's of bridges = 2 | 1946 < YEAR BUILT

 | 4950 KELANTAN | 0750 KEDAH

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2620 JOHOR | 4900 KEDAH | 4060 JOHOR
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APPENDIX-F SELECTION OF 100 BRIDGES FOR VISUAL INSPECTION

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APPENDIX--F SELECTION OF 100 BRIDGES FOR VISUAL INSPECTION

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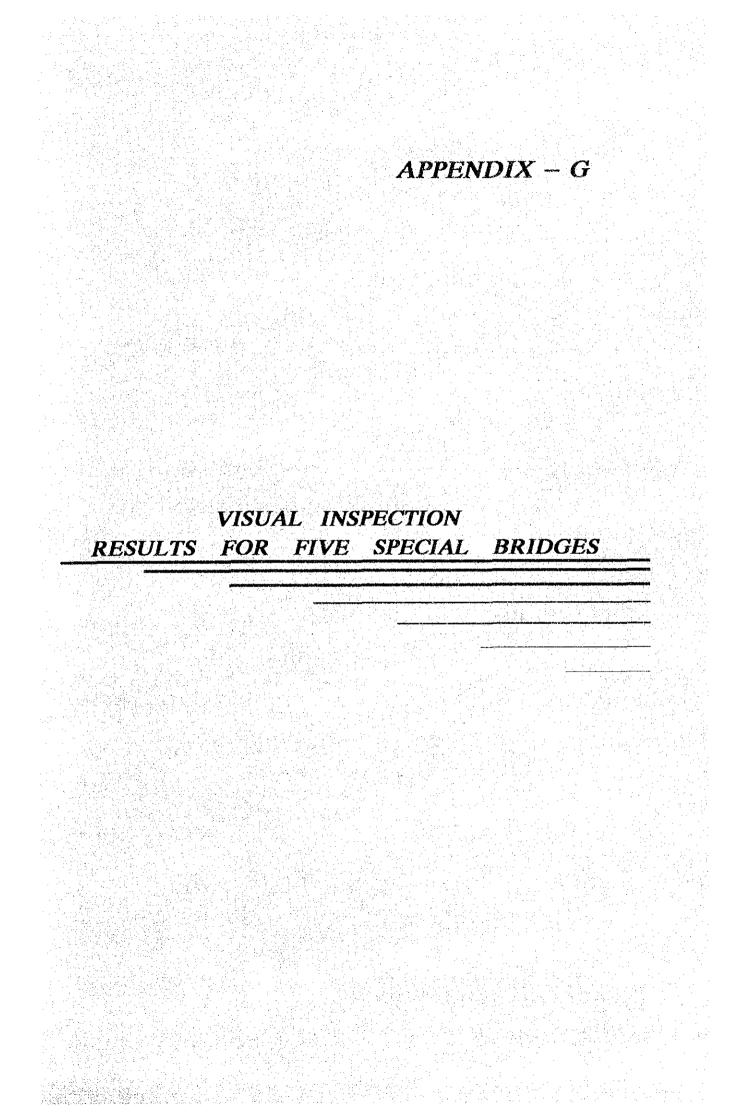


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	TEMERION BRIDGE
E.	KUALA LEPAR BRIDGE G-12

APPENDIX-G VISUAL INSPECTION RESULTS FOR 5 SPECIAL BRIDGES

A. SULTAN YAHYA PETRA BRIDGE

1. Bridge Data

Кеу	*	00371000
Name of River	* -	Sg. Kelantan
State	:	Kelantan
District	:	Kota Bharu
Year Built	- :	1962
No. of Span	. :	29 spans
Bridge Length	:	840m
Type of Superstructure	. . .	RC beam and slab built monoli- thically to the piers
Type of Substructure	•	Pile bankseat (abutment) and rectangular RC columns (piers)

2. General

The bridge links the town of Kota Bharu and Pasir Mas. It was built by the State Government without any consultation with JKR Engineers, as a result JKR has no drawings records with regard to its construction. The bridge was designed by Raymond Wong and Associate and constructed by Kien Huat Construction Company. After construction of the bridge was completed, JKR was directed to maintain it. It has been reported that defects on the bridge starts showing up as early as 1967.

3. Observed Defects

Visual inspection was made by the Study Team in October 1990 and it was observed that all soffit of slab has been repaired by gunite, thus all defects have been covered up. However, the gunite surfaces have cracked at a few location (See Photo A-1), which indicates that repair carried out is not effective. It was reported by JKR Engineers in Kota Bharu that the soffit of deck slab was repaired in 1988 because almost all soffits of deck slab have cracked with concrete spalling at quite an extensive area.

All RC beams have been in distress with vertical crack appearing at regular intervals. The cracks start from soffit of deck slab and propagate vertically down at side of beam to about 200mm from its soffit (See Photo A-2). Some of the RC beams have also cracked horizontally at its side which occurred at about 200mm from soffit of slab.

It has also been reported that most of the expansion joint have failed as early as 1967. The expansion joint has been reported to have cracked and the gap at the half joint has widened with its steel cover plate missing. Expansion joint was subsequently repaired in 1980. During site inspection made by the Study Team, it was observed that the expansion joint could have failed again as crack was observed on premix surfaces (See Photo A-3), especially at the abutment where excessive noise was detected whenever heavy vehicles passed through it.

4. Recommended Rehabilitation and Maintenance Work

It is recommended that further detailed investigation and analysis should be conducted for this bridge which will be carried out in Phase II(A) of the Study.

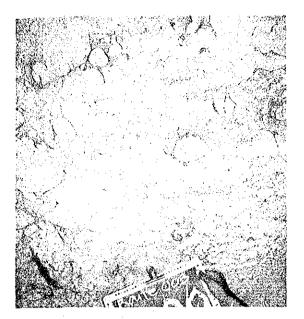


	Photo	A٠
A-1		

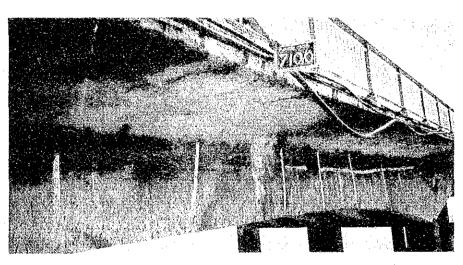
 1 :Crack at gunited surfaces of the soffit of deck slab (The crack does not show up very well in this photo)

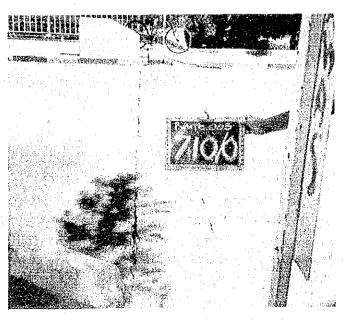
İ	A-2	

A-3

Photo A-2 :Vertical and horizontal crack at side of all RC beams (shown here by the white marking)

Photo A-3 :Crack and wide gap formed on premix surfaces due to failure of expansion joint





B. MERDEKA BRIDGE

1. Bridge Data

Кеу	•	00178210
-	•	
Name of River	1	Sg. Muda
State	:	Pulau Pir
District	;	Seberang
Year Built	:	1954
No. of Span	:	13
Bridge Length	:	271.61 m
Type of Superstructure	:	RC beam a approach

Type of Substructure

Sg. Muda Pulau Pinang Seberang Prai 1954 13 271.61 m RC beam and concrete slab at approach spans and 3 centre spans are of RC bow string arch type of construction

RC wall piers and abutment at approach spans and Masonry wall pier at 3 centre spans

2. General

The bridge is located at the border between the State of Penang and Kedah. The approach span on Penang side consisted of 6 span RC beam and slab bridge while there are only 4 span on Kedah side of the approach. The main span consisted of 3 spans RC bow string arch superstructure with maximum centre span length of 57.32m. Piers and abutments at both approaches are founded on 20m long piles while piers supporting the RC arch is founded on 16m long caisson.

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Very limited information is available with regards to its design or construction except for the drawing which was collected by NALS.

3. Observed Defects

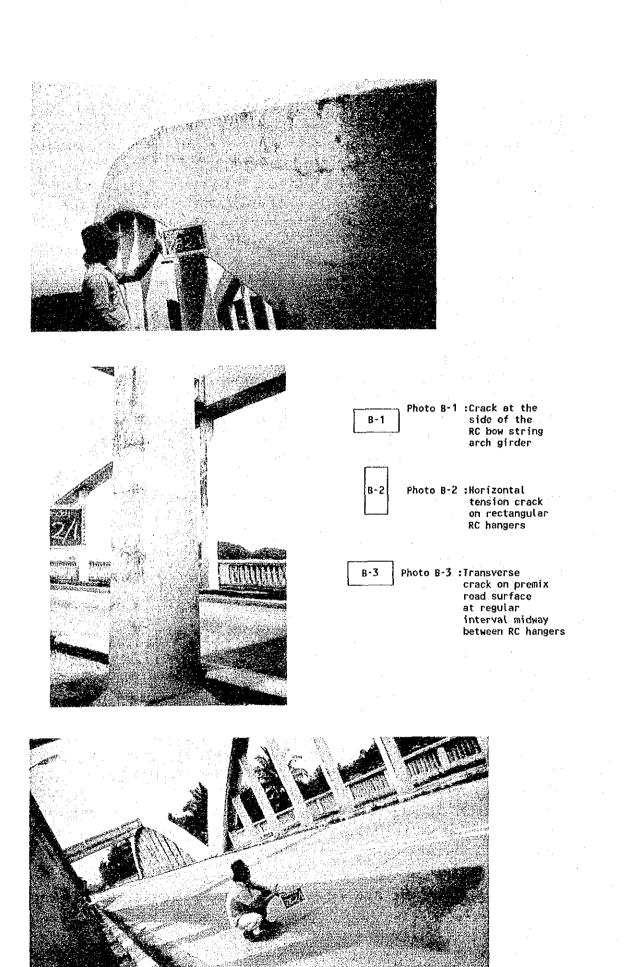
All RC bow arch girder has cracked at its side along the arch line (See Photo B-1), but no rust staining free lime has been observed, thus indicating that the crack could not possibly caused by corrosive expansion of steel. In the opinion of the Study Team the cause of the problem could be due to the fact that the concrete arch is subjected to compressive force, in which the concrete is known to be strong, but at the time the concrete in the arch is also subjected to tensile busting force acting perpendicular to the compressive forces. If inadequate stirrup is provided the concrete will not be able to hold this force especially during the early age of the conrete and thus resulting in cracking of the member.

All rectangular RC hangers has cracked due to the concrete member being subjected to tensile forces (See Photo B-2). Premix surfaces on the carriageway has cracked transversely at regular interval on mid point between the hangers (See Photo B-e). The crack on premix surfaces could have been caused by the crack which appears at the construction joint in the slab. The construction joint in the slab was constructed at midspan between the transverse girders which is supported by the hangers.

4. Recommended Rehabilitation and Maintenance Work

Transverse crack on deck slab could easily be repaired by injecting polymer modified cementitious mortar and painting of the defective members with water proof coating.

Cracks at RC arch rib and hangers are very small with no free lime and rust staining on its surfaces, thus the crack could have occurred at the early age after completion of the bridge. The immediate step is to monitor the crack width whether the crack is active or not. If the crack is inactive then repair is by painting the concrete surface to protect rusting of reinforcement bar is required. If the crack width widen at a faster rate, then repair by injection of polymer modified cementitious mortar will be required. In the opinion of the Study Team, the observed defect on the bridge is not critical, thus no further detailed study with regard to maintenance and rehabilitation work is required for this bridge.



G – 6

C BATU PAHAT BRIDGE

1. Bridge Data

Key	:	00512940
Name of River	:	Sg. Batu Pahat
State	:	Johor
District	•	Batu Pahat
Year Built	:	1965
No. of Span	. • :	5
Bridge Length	•	196.18m
Type of Superstructure	:	Precast prestressed I-Beam
Type of Substructure	:	Steel tubular column (pile)
		and concrete cross head

2. General

The bridge is located not very far from the estuary of Batu Pahat river and thus it is within the tidal range. It replaces the ferry service which link the town of Batu Pahat and Muar. The end span consisted of 31.30m simply supported beams while the penultimate spans consisted of 31.3m simply supported beam supported on pier on one end and on half joint of a 10.3m cantilever span on the other,. The centre span is 52m long consisted of 31.4m simply supported span and 10.3m cantilever spans at each pier. Both piers at end span and abutments are founded on rectangular RC piles while pier at the centre span is supported on 1.2m diameter tubular steel piles.

3. Observed Defects

Expansion joint is not provided at both abutments and piers. The premix material has dropped from the road surface through the gap formed (See Photo C-1) and collected at the bearing shelf. Plant (jejawi tree) is growing at the side and soffit of deck especially at half joint.

G - 7

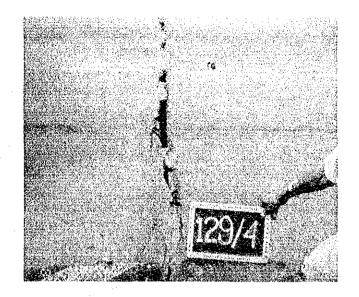
Excessive settlement of the approach embankment has cause pothole with depth greater than 30 cm to be formed (See Photo C-2). Road surface at the approach is very bumpy with excessive rutting of the pavement.

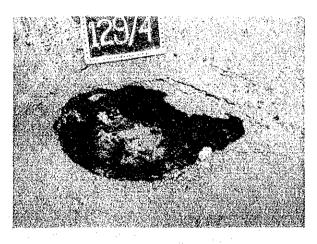
All tubular steel pile at the pier on the centre span has corroded at the splash zone (See Photo C-3). Some of the piles has laminated with rusted steel thickness varies from 5mm to 10mm.

4. Recommended Rehabilitation & Maintenance Work

Bumpy road surface together with non-existence or failure of expansion joint will lead to an excessive impact load on the bridge, thus urgent repair is required. New expansion joint should be installed, debris and plant growing at bearing shelf should be removed. Approach embankment should be repaired, settlement could be reduced by installation of embankment piles at both approaches. Rip rap protection should be provided at the front of abutment to prevent embankment material from being washed out.

Concrete jacket should be constructed to prevent tubular steel cylindrical pile from corroding further. Before concrete jacket is installed all rust should be removed and the steel pile should be blast cleaned.



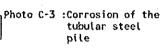


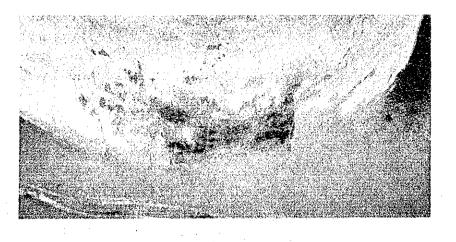
C-1	Ph
C-2	Pho

C-3

noto C-1 ;Expansion joint missing at abutment

noto C-2 :Pot hole formed at approach embankment





D. TEMERLOH BRIDGE

1. Bridge Data

		I I
Кеу	•	00223500
Name of River	• :	Sg. Pahang
State		Pahang
District	•	Temerloh
Year Built	:	1974
No. of Span	:	17 span
Bridge Length		515.21m
Type of Superstructure		Steel box girder on the main span and Inverted T on the approach spans.
Type of Substructure	:	RC wall abutment and V-shaped Rectangular span and RC wall pier at main span.

2. General

The bridge was built at much higher elevation than the old bridge which was severely damaged by flood. It is located on Route 2 which formed a major road link between Kuala Lumpur and Kuantan town. The Kuala Lumpur approach is made of 8 spans inverted T-beam bridge while the Kuantan approach is made up of 7 spans Inverted T-Beam bridge. The centre main span is made of 2 spans continuous steel box girder bridge. All abutments and piers are supported on pile foundation. This bridge is relatively new thus quite a number of drawings is available and collected by the NALS.

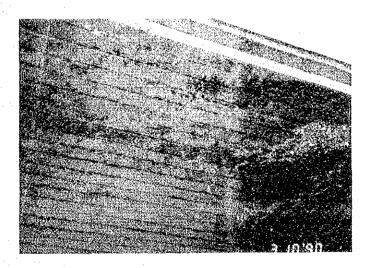
3. Observed Defects

Free lime was detected at soffit of inverted T-Beam on a few of the approach spans (See photo D-1). The defect could be caused by porosity of the bridge deck. Expansion joint on the bridge deck directly above the pier supporting the box girder at Kuala Lumpur side has been in distress. Its epoxy nosing has failed and anchor has loosened (See photo D-2).

4. Recommended Rehabilitation Maintenance Work

Porosity of bridge deck on approach span could be repaired by providing water proof membrane on the RC deck. However, since the porosity is only at a localised areas and to minimise cost of repair, the defect should be repaired by injecting the defected areas of RC slab with polymer modified cementitious grout.

All loose anchor bolts at the defective expansion joint should be tightened and its epoxy nosing repaired by polymer modified cementitious mortar.

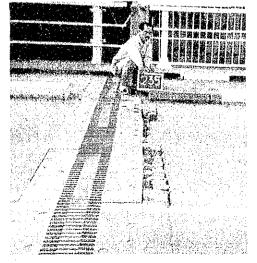




D-2

Photo D-1:Free lime at soffit of Inverted T-beam bridge on the approach span

Photo D-2:Damaged nosing at the expansion joint



G - 11

E. KUALA LEPAR BRIDGE

1. Bridge Data

Key	:	01212140
Name of River	:	Sg. Pahang
State	:	Pahang
District	:	Pekan
Year Built		1976
No. of Span	. :	7 spans
Bridge Length	:	402.3m
Type of Superstructure	:	Precast Prestressed segmental continuous box girder
Type of Substructure	:	RC hollow wall/box abutment and pier

2. General

The bridge is located on the road linking the town of Kuantan on the East Coast to Segamat town on the South Western side of Peninsula Malaysia and it crosses the longest river in Peninsula Malaysia. The bridge is founded on pile foundation.

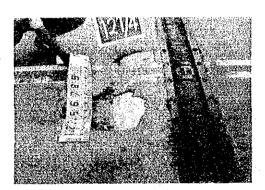
3. Observed Defects

The bridge is relatively new, thus no structural defect was observed except for potholes formed on approach road surface adjacent to expansion joint at both abutments (See Photo E-1).

G = 12

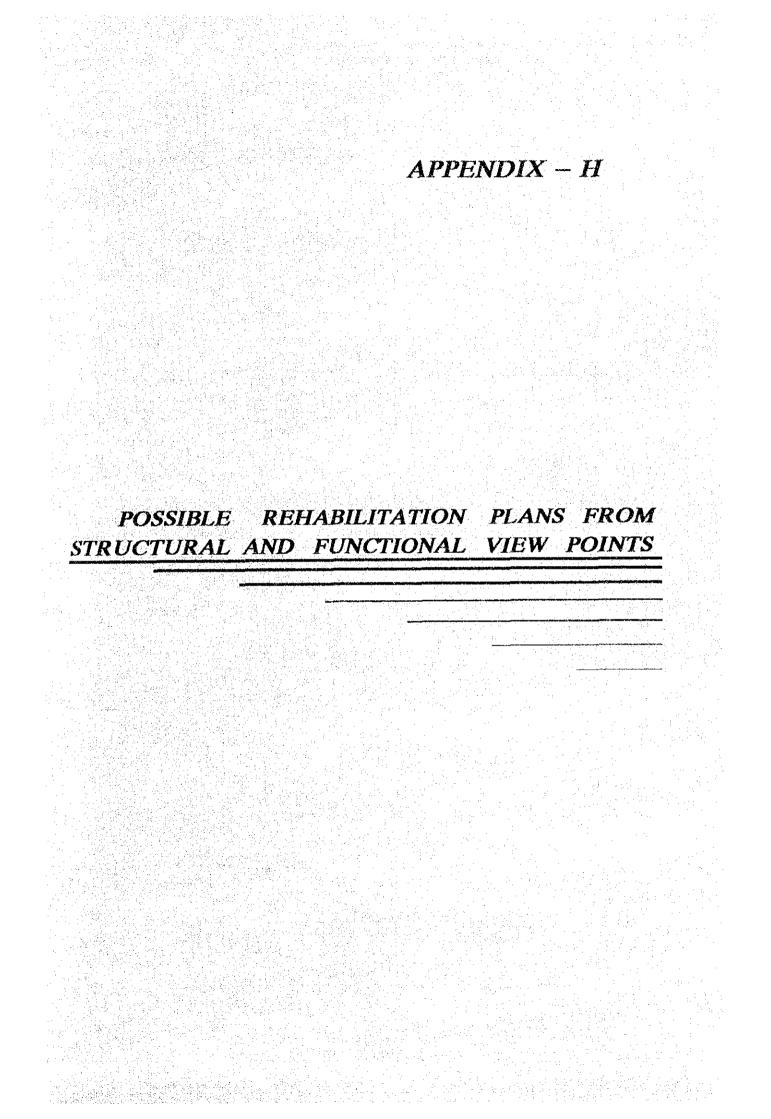
4. Recommended Rehabilitation and Maintenance Work

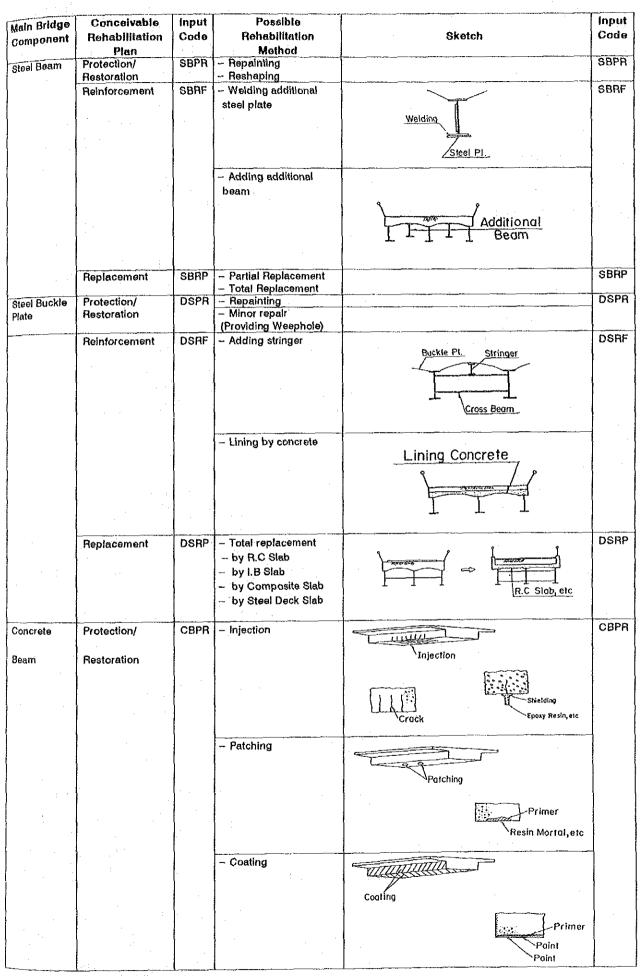
Since NALS report has highlighted this same problem (i.e. potholes) at this bridge, the Study Team concludes that the defect is caused by failure of the road pavement. Therefore, road pavement adjacent to the bridge has to be properly design and reconstructed.



E-1 Ph

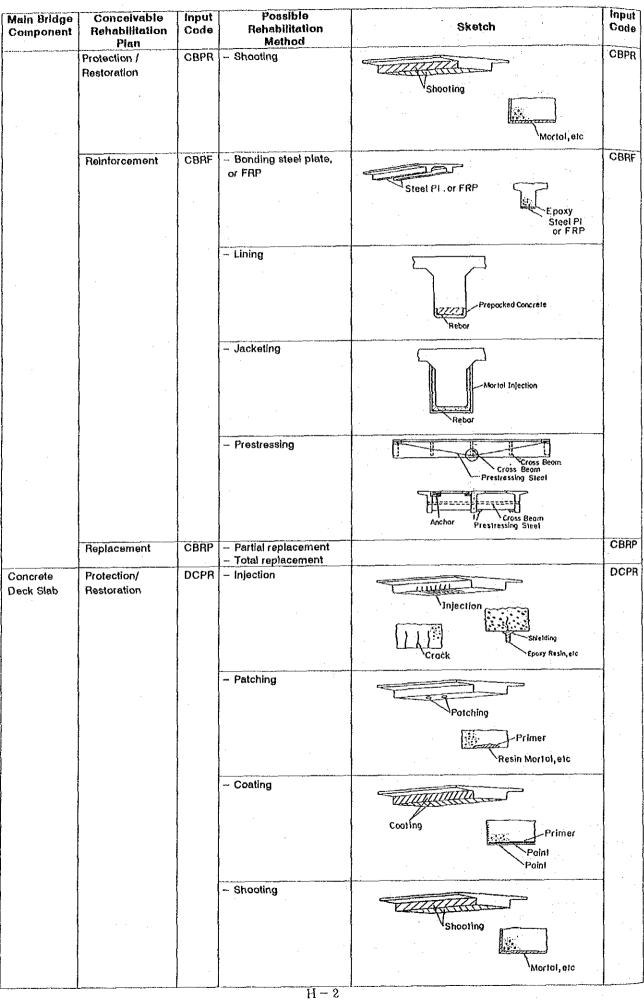
Photo E-1 : Pot holes formed on approach road surface adjacent to expansion joint at the abutment



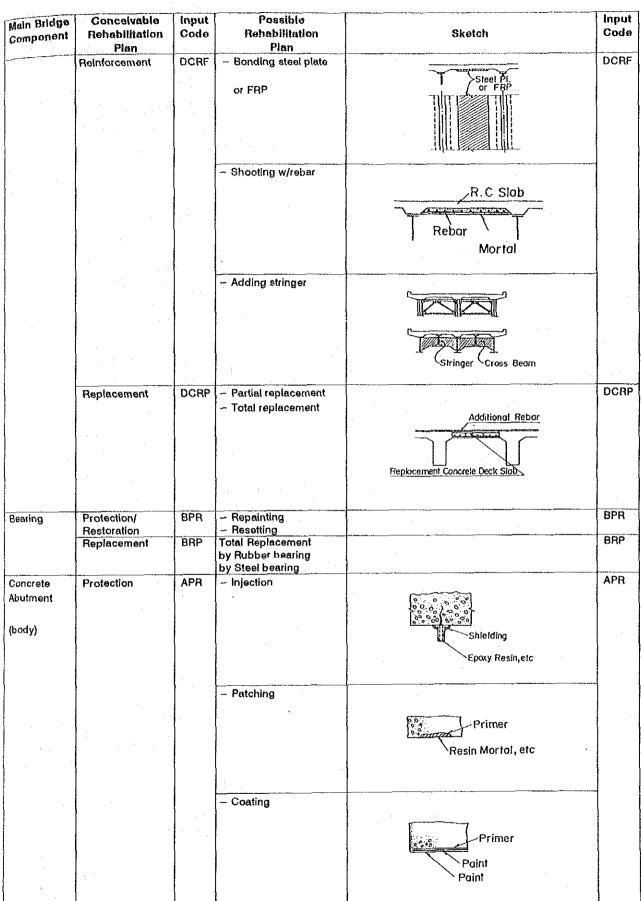


APPENDIX--H POSSIBLE REHABILITATION PLANS FROM STRUCTURAL VIEW POINT

H -- 1

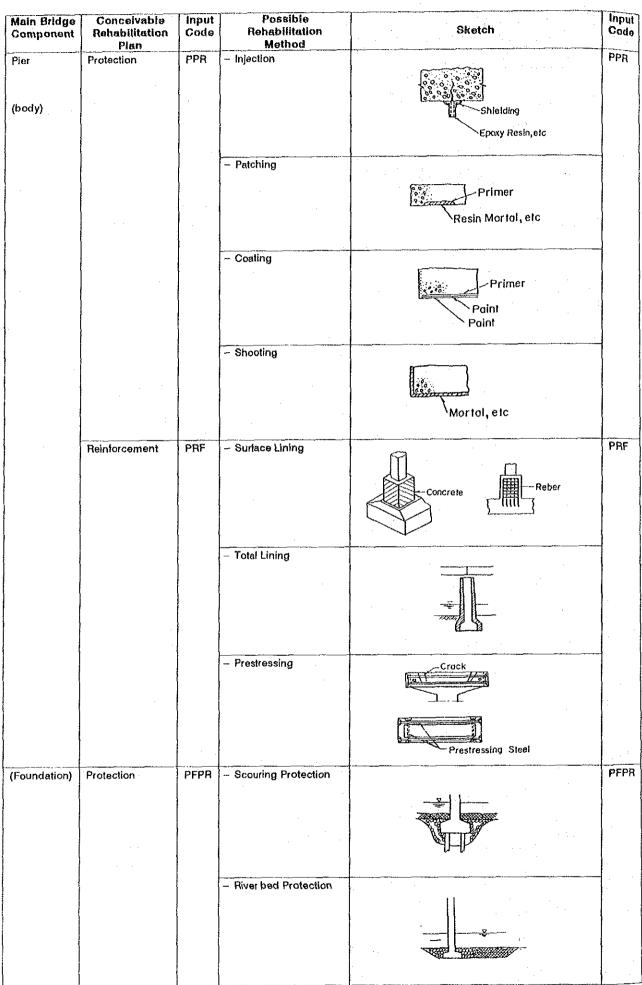


APPENDIX-H POSSIBLE REHABILITATION PLANS FROM STRUCTURAL VIEW POINT



APPENDIX-H POSSIBLE REHABILITATION PLANS FROM STRUCTURAL VIEW POINT

H – 3



APPENDIX-H POSSIBLE REHABILITATION PLANS FROM STRUCTURAL VIEW POINT

H = 4

Main Bridge Component	Conceivable Rehabilitation Plan	input Code	Possible Rehabilitation Method	Sketch	Input Code
	Reinforcement	PFRF	- Under pinning		PFRF
	•	•		265326	
				Additional Pile	
		· ·			
Steel	Protection	SPPR	- Partial Lining		SPPR
Pier (body)					
				Concrete	
			- Repainting		
	Reinforcement	SPRF	- Surface Lining		SPRF
		. *		Stud	
			- Total Lining	Stud	
				Concrete	
				Ψ <u>2.00,101010</u>	

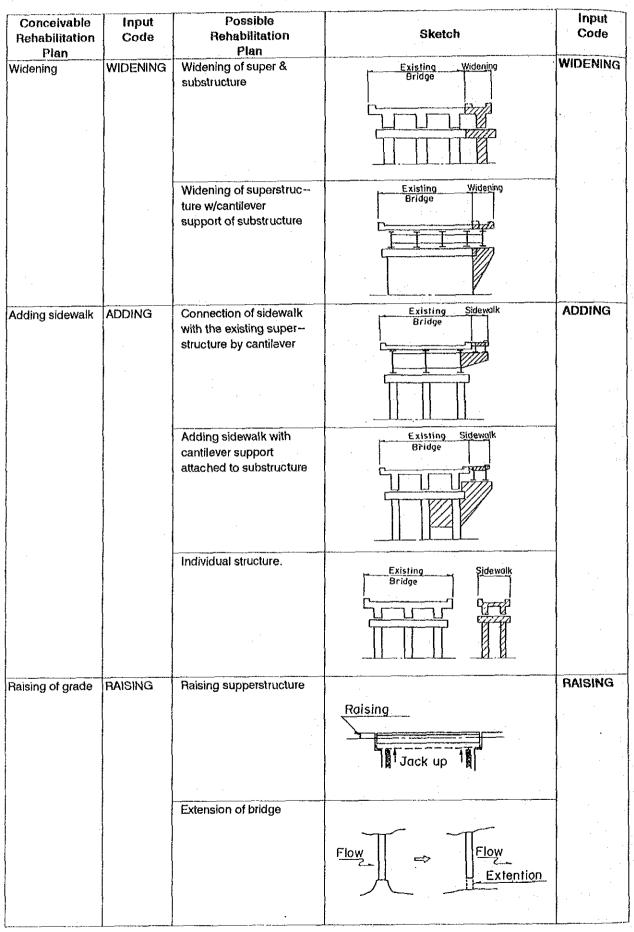
APPENDIX-H POSSIBLE REHABILITATION PLANS FROM STRUCTURAL VIEW POINT

H - 5

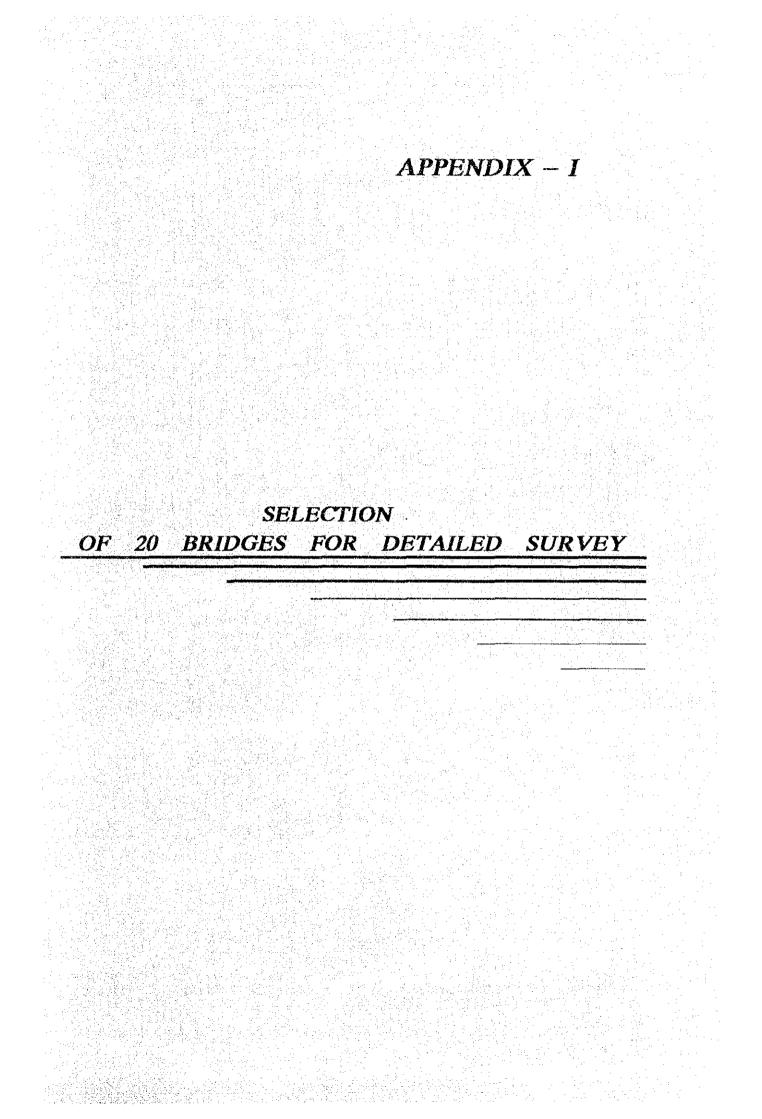
Possible Rehabilitation Plans From Functional View Point

.

APPENDIX-H



H - 6



APPENDIX-1 SELECTION OF 20 BRIDGES FOR DETALED SURVEY

FINAL SELECTION REMARKS		-	SA(6.28)	8	CB SA	SA(6.74) CB					EA SA(7.27)				5 5
RINAL					Selected			Selected				Selected JKR			Selected
POSSIBLE REHABILITATION PLANS T FROM FUNCTIONAL VIEW POINT	ļ				RAISING GRADE	ADDING SIDE WALK WIDENING & RAISING (REPLACEMENT)	No's of bridges selected a 1			PAISING GRADE			No's of bridges selected = 2		
POSSIBLE REHABILITATION PLANS FROM STRUCTURAL VIEW POINT			11 APR	ARF	3 CBRF,DCPR 4 CBRF,DCRF	1 ARF 4 DCRF,PPR		1 SEPRAPR	3 352PA,025FA 1368FF, APR 3 1368FF, APR 3 1368FF, APR 1 138PA, APR 1 138PA,05PA,APR 3 138PA,05PA,APR 3 138PA,05PA,APR	1 SBRF, APR, SFPR	CBRFARF 1]CBRFARF	< SBRF, DCRF, CBRF, APR	· · · ·		PRF.CBPR 1 CBPR PRF 1 CBPR
ABUT RATING OF PARTS ABUT BEAR DECK ING BEAM				4 - 1 - 1 -	+ + + + + + + + + + + + + + + + + +	4 T			1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 0 4 4 0 4 4 4	<u> </u>	3 = + + + + + =	3 4			0
NO. BRIDGE TYPE OF LENGTH OF SPAN (M) BRIDGE			51 11 2.16 BOX 1	-	2	2 8.15		, T	1.9 1.9 1.9 1.9 1.9 1.9 1.9 1.9 1.9 1.9	s 1 3.35 SBC	4 1 3.14 SBE	2 1 10.72 SBC			8 5 47.63 17 8 7 51.96 17 7 9 41.59 17 8 64.57 17
STUDY CATEGORY CAPACITY SPAN			3 MTAL 2.18	3 [P/A 4,95		3 P/A 4.58			STAL 6.21 9 57AL 1.191 9 55AL 10.81 9 57AL 6.70 9 57AL 6.60 9 57AL 6.60 9 55AL 10.81 9 55AL 6.70 9 55AL 4.79 9 55AL 4.79 9 55AL 4.79	<u>3 STAL 3.35</u>	3 P/A 3.14	3 STAL 10.72			3 STAL 12.00 3 STAL 18.80 3 STAL 18.80 3 STAL 19.57 3 STAL 19.57
DISTRICT RUILT CATE			KLUANG 1 1937	JASIN 1940	KSELANSOR 1920 KMUDA/SIK 1940	K. TINGGI 1940 Machang 1941		ATU PAHAT 1919	1920 1920 1920 1920 1940	K. TINGGI [1928]	MANJUNG 1930	[LRT MATANG 1936		n boo na anna an anna anna anna anna ann	PONTIAN 1968 K. Tinggi 1398 MANJUNG 1372 MANJUNG 1374 K. Tinggi 1374
NO. KEY STATE	<< 8efore 1945 >>	R.C. BRIDGE	** BOXR.C.Box Culwert 11 00108950 JOHOR K	E	α		No's of total bridges ≖6 STEEL BRIDGE	ā	B Coefficients PALANIC J B Coefficients PALANIC J B Coefficients PALANIC J B Coefficients PALANIC J 10 Coefficients PALANIC J 11 Coefficients NI S 12 Costocean NIS S 13 Costocean JUHCR F 13 Costocean JUHCR F 13 Costocean JUHCR F 14 Costocean XELDAH F	** SBCSteel Beam R.C.Stab 15 00304330 JJOHOR 1	** SBEEncased Steel Beam 15 06000370 PERAK 1 17 00003220 JOHOR 1	** SBGSteel Box Grider 18 00186510 PERAK	No's of total bridges =12 << 1948 TO 1974 >>	P.C. BRIDGE	

I – 1

	DISTRICT B	BUILT CAT	CATEGORY	CAPACITY	SPAN OF		CENGTH OF	ABUT	8	BEAR	DECK	PLANS PLANS	PLANS	SELECTION	REMARKS
								GE	PIER	ING BEAM		FROM STRUC	FROM FUNCTIONAL VIEW POINT		
Lipis		1961	0	STAL	30.74	4 12	122.36 PCB	+	-	9	-	CBPR, BPR			
1	N	1962	T	SSAL	ł	4		_		-	-	APR PPR CBPR		Selected JKR	Gr AB
(-	KENAMAN	3	T	UTAL DTAL		1		4		1	-	000 - 01-1 000		HXP	
		R S		2104	Ţ			+				200 005 A05			
	K MUDA/SIK	19061		STAL	30.64		PCF PCF	* .		14		DCPR PSPR			s
		10/01	Ι	STAL	30.52	6				*		BRP. APR. PPR		AXP.	SA
12	DUNGUN	1973	Γ	STAL	30.50	9 15		3		-	4	CBRF,APR	PAISING	Selected	
Z!		1974	Π	MTAL	45.78	300	397.32 PCB					CBRF,DCR-		Selected JKR CA	GA
									•.				No's of bridges selected = 4	:	
l															
MARAN		1966	3	STAL	3.00	-	3.03 BOX	9			0	3 DCPR, APR			SA(6.0)
a a	P.PUTEH	1952		STAL	5,411	0		4	4		4	I CBRF, PRF, PFP R, AFPR	TADDING & FAISING (REPLACEMENT)		
¥		1959	Γ	STAL	5.90	" 0	53.10 PRB		-		1	CBPR			
S	×	1960	Π	STAL	6.06	5		0		1	4	CBPR.APR	WIDENING	Selected	св Св
Sil		1960	Ι	STAL	6.01	0		-		1	,	PHF	ADDING SIDE WALK		
	MERSING	1064		STAL	5.50		14.22 PHB			- 	4-	COTH, FFA			K
Ne K		1965	Τ	STAL	5.88			-		-	4	CBPR PRF ARF			RA CA
망	رر. در	1970		STAL	6.18	0					1	CEPRAPRESPR		-ska	
** RCBR.C.Boum										•	-	-			
Ψ	MELAKA TGH	1950	0	STAL	6.90)		1 5	5	•	ł	4		ADDING SIDE WALK		CA.SA
KLUANG	NNG	1964	0	STAL	15.90	00	27.40 RCB	4	4,	-		CBPR, PFPR	-	-	SA(7.04)
	COLORNAT	8 20		2141	20.0				- (*		2 v			Calaman INC	17-01-01
	AMAN	1055		STAL	12.10		36.14 208			4		CERF EPS ARF PRF		Selected	
Ň	er	1995	0	STAL	6.97			ŀ				CBRE,PRF			CA.SA
S B D	SEPANG	1960	9	STAL	6.95			*	4	-	4- -	ARF, PPR		EX	ð
Y	K LANGAT	801		STAL	7 30			1	1	•	ı	this bridge has been repaired			80
	PADANG	1990		SIAL	80.8	1	83.99	+			5	COPH 500 000 ADD		c	
ā i	AVA TON	1801	2,0	0101	¥ £			+					ADDING SIDE WALK		
				STA .	7 43		14 20 10 1					CROF ARE DOF			0000
Å	N	9961		STAL	10 42			. -				APR AFPR PRF			50
Ϋ́	MUAR	1906	3	STAL	8.03		17.82 RCB			4	4	1 CBPR, BPR, PPR		ЯХС	۲ د
1			: :				. :								
130	ALING	1950	8	STAL	6.56			5 3		-		АРВ		JKR	
SEG	AMAT	1,950	4	SSAL	5.68		7.60 RCS	5 4	1	1	3	3 ARF, DCPR	RAISING GRADE		_
SAS	JASIN	1955	0	STAL	6.22	~	42.70 ACS		*			(PRF		EX.	CASA
쥙	NTAN	195	0	STAL	6.58			4	ļ	1	_	1 ARF		-	
<u>S</u>	LA KRAI	8	5	STAL	4.63		13.71 RCS	-		-		4 DCRF, PPR		Selected JXP	
÷.	SING	8		STAL	1.80	1	3.60 1.05	-	0	╎		4 DCHF, APR, PPH			đ
šļ,		1000		CTAL C	8 22							a DCPD		IKP.	
				1	į										

No's of bridges selected = 5

No's of total bridges = 32

APPENDIX-I SELECTION OF 20 BRIDGES FOR DETAILED SURVEY

APPENDIX-1 SELECTION OF 20 BRIDGES FOR DETAILED SURVEY

		BUILTIC	CATEGORY	CAPACITY	SPAN	E E	LENGTH OF	ARLIT	a B	REAR	DECK	PI ANS	DI ANS	NOTCH HS	REMARKS
F	10111010				i	_	യു		PIER	ING BEAM	_	FROM STRUCTURAL VIEW POINT	FROM FUNCTIONAL VIEW POINT	SCLECTION	
												-			
** SBBSteel Beam Buckle Plate	te						2		Ŀ						
	KINTA	1948	0	SSAL	11.50	0			1 0		4		ADDING SIDE WALK		
	HLR PERAK	0561	c	STAL	5.30	-	5.88, SBB	0	1					-	ys S
	BENTONG		0	SSAL	3.47	-	- 1	-	† 			SBPR, DSPR			
	PERLIS		8	SSAL	8.9	-		Ŧ	1		2	2 NON			
	LEMESELAMA		J	SSAL	5.06	-	_	•	1		4				
	SEGAMAT	1950	9	STAL	6.29	2		I I	+		4	SBRF,DSPR			
	PD	096	6	SSAL	4.84	-	4.84 SBB	4			4	SBPR, DSPR, APR			
	BATU PAHAT	0961	0	SSAL	5.05	-		-	1		1				
SELANGOR	K LANGAT	1950	2	SSAL	4.73	F		4	1		4 3	SBPR DSPR, APR			
÷	HULU PERAK	098	6	STAL	9.34	-		4]		9	ISBPR, DSPR, AFPR			
SELANGOR	K. LANGAT	1950	2	SSAL	6.29	-	6.29 SBB	6			Ē	11 APR			SA
ľ	RAUB	1050	4	SSAL	40.0	1			4		0	ISBRE DSPRAFPR PEPR			
	K KANGSAP	0-0	P	SCAL	5 341	-					4	SARE DOR AFOR			
	H, R PERAK	0561	ŕ	SSAL	3.671	-		ŀ	t		ľ	SRPP APR			SA
ľ	SEDEMBAN	10201	16	2641	140	ł	ŧ.	+	+	-					
l	RTC PADANC	20-01		STAL	4 97	+	A 07 SHR					SEDE DERE		Selected IKB	SA
	HI I DEBAK	050		SSAI	8.95	+		~			ſ				SA
.	HURU PERAK		2	STAL	3.07	+	3.07 SEB		+	-		SBRF.DSPR.AFRF			
	K KANGSAR].	0	SSAL	6.35	-	6.35 SBB	ļ	1			SBRF.DSPR			
	Dd	1950	Ð	SSAL	6.27		6.27 SBB				0	SBPR.DSPR.DCPR.APR	RAISING GRADE		
	KINTA		e	STAL	9.77	6	E	ŀ	1 C	•	4 3	SERF DSPR AFPR PPR	ADDING SIDE WALK	Selected JKP	
ŀ	BTG PADANG	1950	0	SSAL	3.88		4			. 		4 SERF, DSRF, ARF			SA
SELANGOR	K LANGAT	88	0	STAL	3.24	-				.		SEPR, DSPR, APR			
	SEREMBAN	0981	0	SSAL	6.31	F	6.3t SB3	-			F	SBPR, APR			
** SBCSteel Feam B.C.SMD															
	BTG PADANG	10561	9	TSTAL	10.88	e	23.18 SBC				4 4	SBPR.DCRF.APR		Selected JKR	
	L&M&SELAMA		0	STAL	7.20	4	27.141 SBC	*	-		ľ				SA
	MANUUNG	1950		STAL	4.78	-	F .	-	1	-	ľ	SBRF, DCRF	WIDENING		CA.CB
00237200 PAHANG	KUANTAN	1900	0	STAL	8,90	6	26.701 SBC	4	4		4	SBPR, AFPR, PRF		Selected	Q
E	U.LANGAT			STAL	18.24	9			F	4	-	SBPR, BPR			
SELANGOR	K.SELANGOR	L		STAL	12.61	9	٢.	F	4	*	1	BPR,PPR		JKR	ð
]		1								
	146DCING	10501		STAL	104 401						-	11498	ADDING SIDE WALK		
		2 C													<u> </u>
	NSSAL	INCR L	0	SIAL	4.4			_	1	-	4			sciecies	¥ C
No's of total bridges = 32													No's of bridges selected = 5		
Service no															

1 - 3

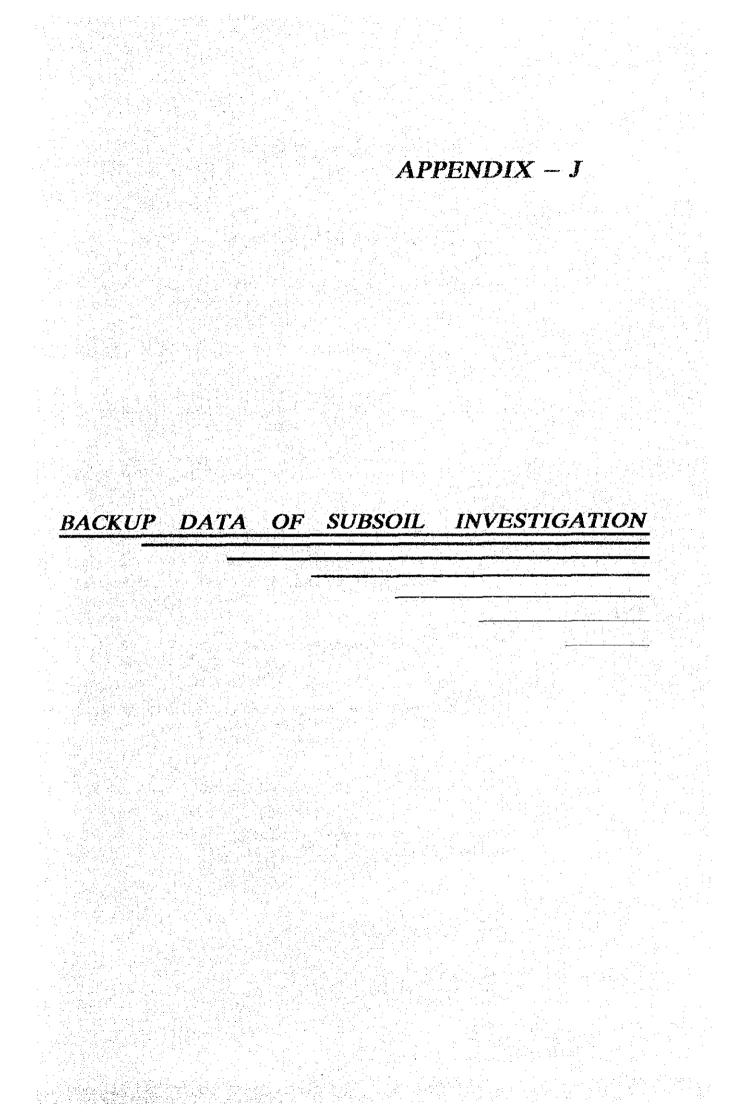
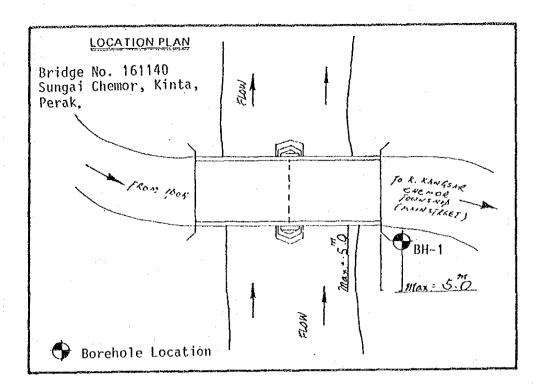
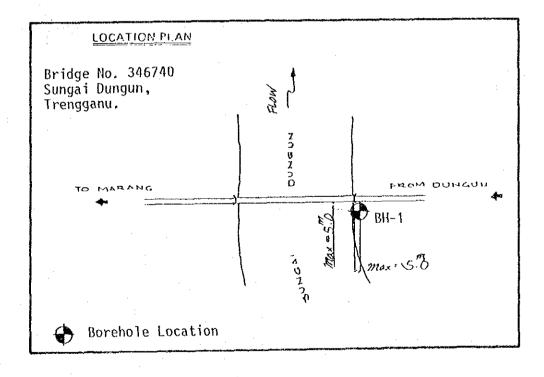


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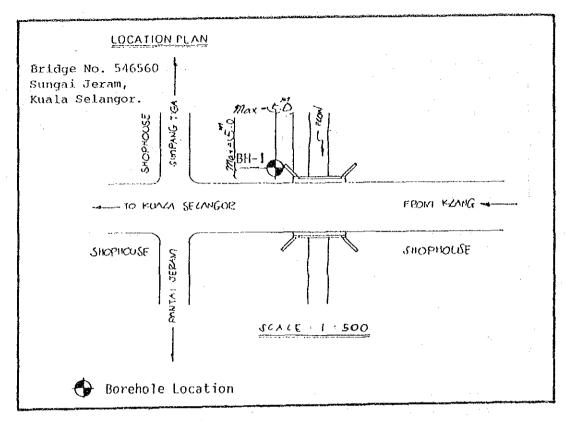
Description	Page
Borehole Layout Location for the 5 Bridges	J- 1
Hand Auger Location for the 10 Selected Bridges for Sulphate Survey	J 4
Drilling Logs for the 5 Selected Bridges	J- 9
Plot of Index Properties Versus Depth at Bridge No. 00546980 (Fig. J-1 to J-3)	J-18
Plot of Index Properties Versus Depth at Bridge No. 00546980 (Fig. J-4 to J-6)	J-19
Pressuremeter Curve at 5 meters depth for Bridge No. 00546980	J-20
Pressuremeter Curve at 10 meters depth for Bridge No. 00546980	J-21
Results of Chemical Tests on Water Samples from Boreholes (Table J-1)	J-22
Results of Chemical Analysis on Soil Samples from Hand Auger Holes (Table J-2)	J-23
Results of Chemical Analysis on Soil Samples from Hand Auger Holes (Table J-3)	J-24
Recommendations for Concrete Exposed to Sulphate Attack (Table J-4)	J-25



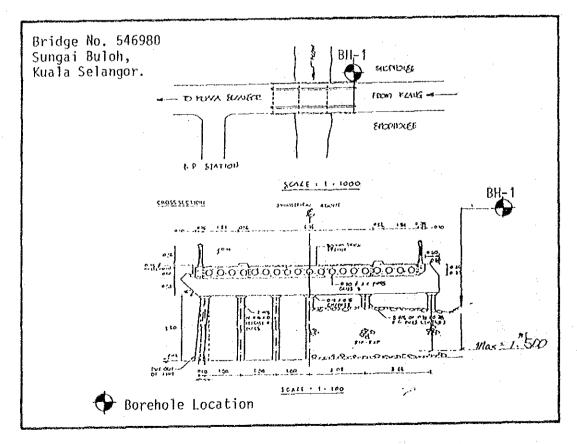
Borehole location at Bridge No. 00161140, Perak.



Borehole location at Bridge No. 00346740, Terengganu.

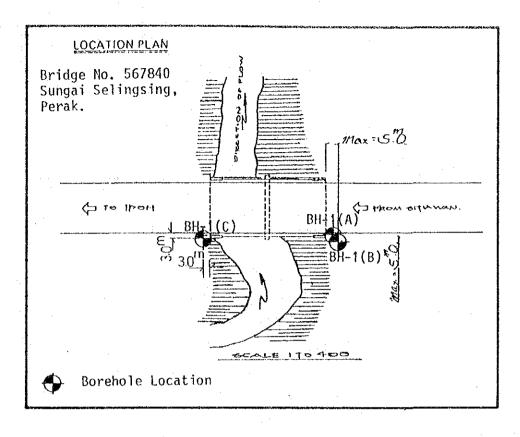


Borehole location at Bridge No. 00546560, Selangor



Borehole Location at Bridge No.00546980, Selangor

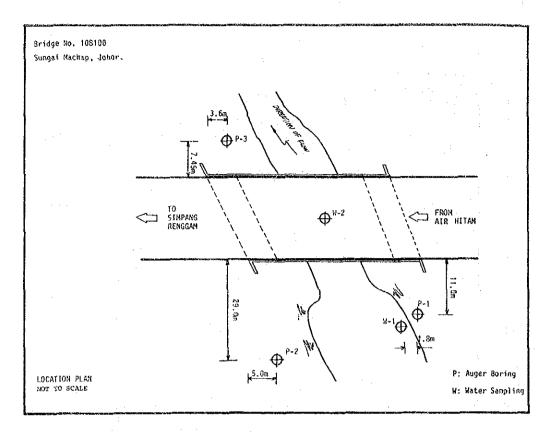
J – 2



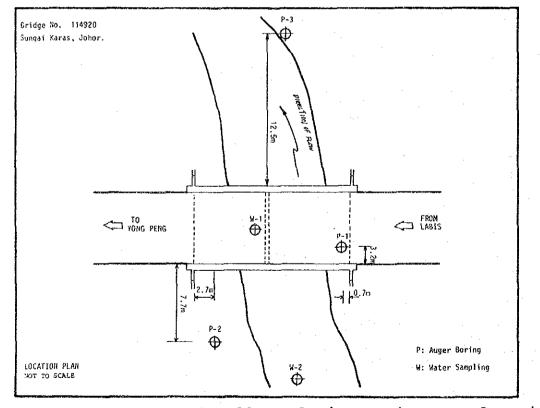
Borehole location at Bridge No. 00567840, Perak

J - 3

Append-J

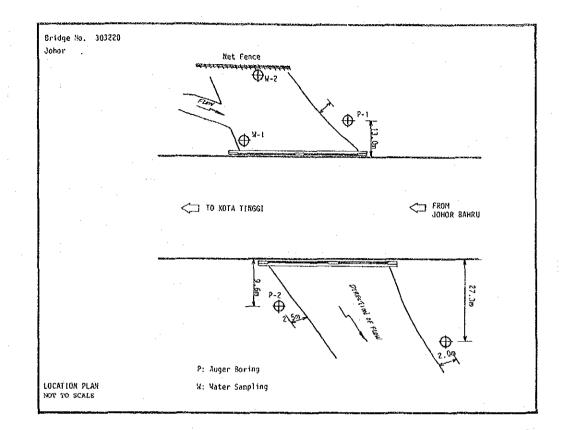


Locations of Hand Augers and collected river water samples at Bridge No. 00108100, Johor

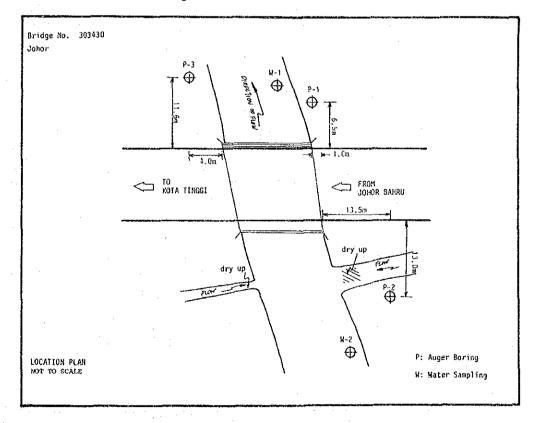


Locations of Hand Augers and collected river water samples at Bridge No. 00114920, Johor

J – 4

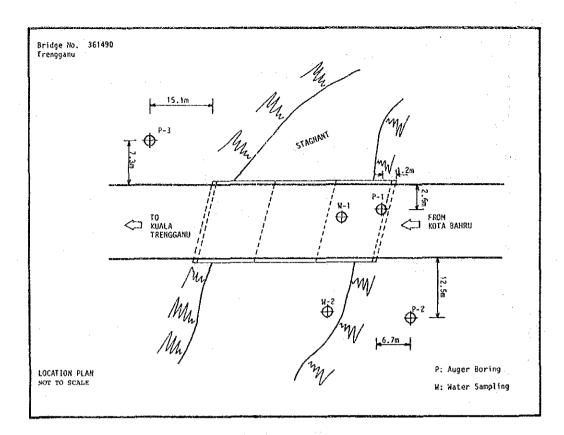


Locations of Hand Augers and collected river water samples at Bridge No. 00303220, Johor

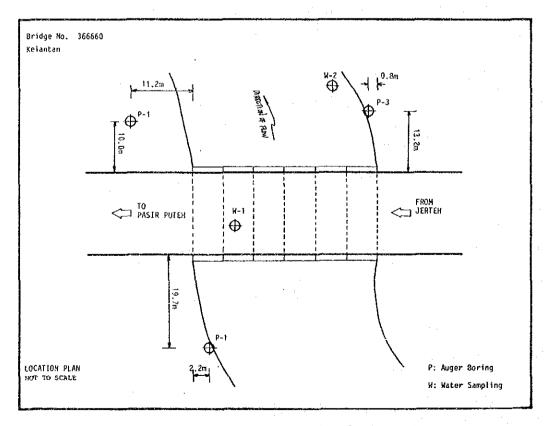


Locations of Hand Augers and collected river water samples at Bridge No. 00303430, Johor

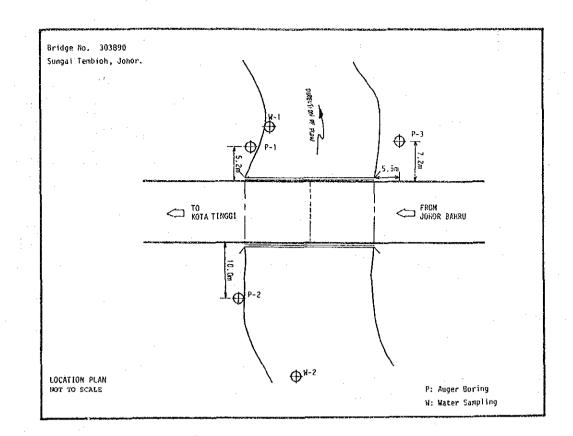
Append J



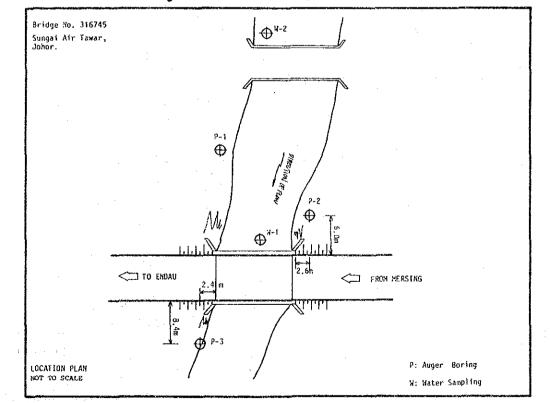
Locations of Hand Augers and collected river water samples at Bridge No. 00361490, Terengganu



Locations of Hand Augers and collected river water samples at Bridge No. 00366660, Kelantan



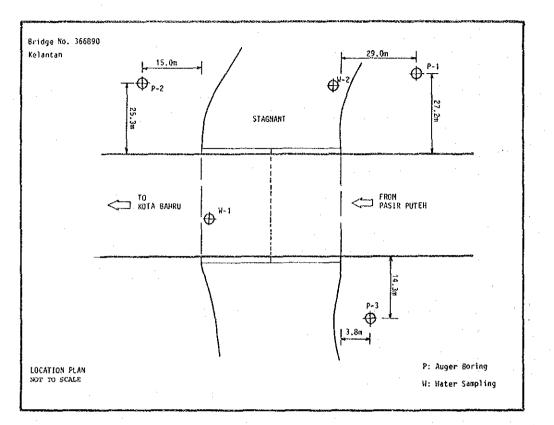
Locations of Hand Augers and collected river water samples at Bridge No. 00303890, Johor



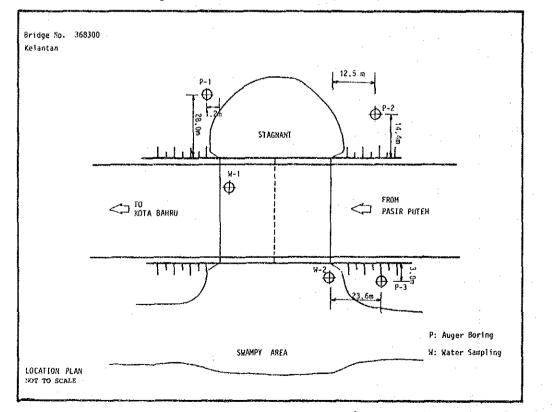
Locations of Hand Augers and collected river water samples at Bridge No. 00316745, Johor

J - 7

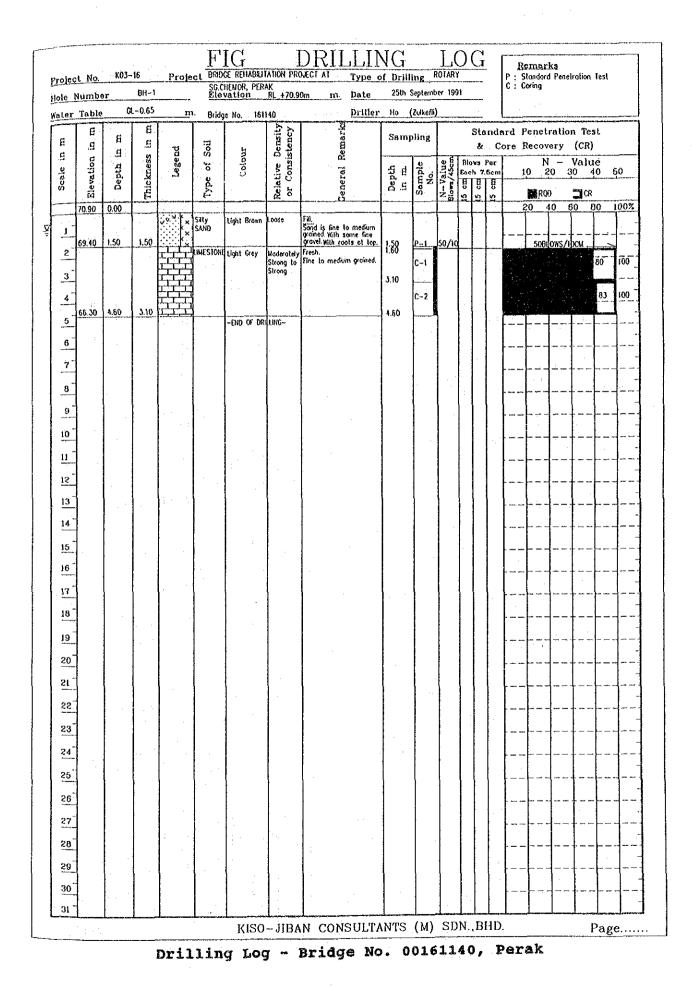
Append J



Locations of Hand Augers and collected river water samples at Bridge No. 00366890, Kelantan



Locations of Hand Augers and collected river water samples at Bridge No. 00368300, Kelantan



J — 9

Append-J

Ducing	. N.	K03-	- 16	Proie		IG ABILITATION	-	DRILLII AI Type o		ing)		<u>1</u>		lema: Stonilar		tration	Iest	
Projec Usia			8H-1			UNGUN IER Vation							 emhe	- L	a rondo	u rene	ti otion	1036 -	
<u>Hole I</u> Water				 11		•		Driller		(Leon		<u>sept</u>							
E	6	E E	E		[Density is tency 0,125	Remarks	Sam			5	Star	dard	Penel	tratio	n Te	şL	
Ë	u u	E.		Legend	Soil	Colour	ttive Density Consistency			l u	w E	Blot	rs Pe	r I		4 —	Valu	ie	
Scale	Elevation	Depth	Thickness	3	Type of	පී	Relative or Cons	General	Depth in m	Sample No.	N-Value Elows/45cm		7.5c			20	30 . 4		<u>50</u>
	5.60	0.00		× 1-		Whitish Grey with		// #1				-	_		1	1	r	<u>ر</u>	
1	4.30	1.30	1.30		Clovey SR T	Grey with Reddish and Yellowish	ĺ.	(Fill). Traces of fine sond and gravel.						·				- <u>-</u> -	
2				×*	SAND	Yellowish Brown		Fine to coorse sand. Silly up to 1.8m.	1:85	<u>P=1-</u> 1	5.	1		2.9.					
3			:	* 				Fine sond predominates up to 4m.	3.15			ः 1		14.					
4		- 14						With some fine gravel below Am.	3.15 3.45	P=2]	4	2	4	╘╻				L	
5				7 °					1.63 4.93	P=3	3	0	0.	┊┥┥╴		-	. 		
6									6.15 6.45	P-4-	3	0 0	1	·	· - ·				
7									U,9J	-	-	0 (-	−][·				
8	-1.95 -2.50	7.55 8.10	6.25 0.55	<u>, v ⊻</u> [×	STLY CLAY	Derk grey	Soft	With organic matter and fine sand. Traces of mica fragment/	3.85	P=3-1	2	0		- -	· 		 		
9				•	SAND	light brown	Varu traa-	Fine to coase sout	9.15 9.45	P-6	3		0				 	 - -; -	
10 11				e o	DAM	la Light la Light Grey la Grey	to Medium	with the to medium sond. Slightly clayey at battom. With the gravel below 10m	10.65 10.95	P-7	15	3 3		3					
15				<i>©</i>				Noz.da.8mm. Irace of sit below 10m.				7	5		[[[
13 T	-6.60	12.20	4,10	××××	<u> </u>			Sandy clay lense with shell fragments at bottom	12.15 12.30	P-8-			17		508	107/1	5CM		
14				Qîx^x	SiLT with rock fregments	Red to Grey Motiled Yellow and Brown		Completely Weathered sedimentary rock Frioble to sill with hord rock fragments.	13.88	P_9_	50/15	18 32	_		508	ows/1	БСМ		
<u>15</u>				* * * * * * * 0 0 * • *		Li Cint			18:58	P-10	<u>50/22</u>	20 5 25	15 2 10	، 	506	iows/2	2.5C#		
16				× × × × × ×					16.50 16.55	<u> 2-11</u>	50/5	50		_}	508	10#\$/!	см _		}
17 18	~12.46	18 06	5.86	***** ******					16.55 18.00 18.06	P-12	50/6	50			508	10%S/6			
19						-END OF	DRALING-		18.06	-				1	[]			
50																1			
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						KISO-	- JIBAN	N CONSULTAN	VTS ((M)	ŚDN	I.,E	HL)	i		Р	age	