| | CONCENABLE REHABILITATION | | | | | | | | | | | | | ADDING & WIDENING | MINHOM | | HAND ENIGHT | | | | | | | | | | | | | | | | FASING GRADE | | | | | | | | | | | | | | | | | | | | | | | | |
|----------------------------|------------------------------|-------------|--------------|----------|----------|----------|----------|---------|----------|----------|----------|---------|----------|-------------------|---------|--------|-------------------|----------|---|----------|----------|----------|---------|---------|---------|----------|-------|----------|---|----------|----------|------|--------------|----------|------------------------|----------|----------|-----------------------|------|-----------|------------|------------|--------------|------------|------------|---------------|------------|------------|------------|------------|-------------|------------|--------------|-----------|--------------------------|-------------|------------|
| | RIVER VIEW POINT BRIDGE | OPENING | | | | | | | | | | | | | | | INAUELICALE | | | | | | | | | | | | | | | | INADEQUATE | | | | | | | | | | | | | | | | | | | | | | | | |
| | CAPACSTY | FEAR | 2147 | 2147 | 2147 | 2147 | 7412 | 2147 | 2127 | 2098 | 2098 | 2107 | 2014 | <u>1</u> 88 | 88 | 2441 | R | 21/1 | 20160 | N/A | N/A | NIA | 2429 | 2424 | 2424 | 2437 | 2424 | 242/ | 1110 | 1110 | 1610 | 2321 | 2321 | 2317 | 2317 | 2319 | 218 | 2020 | 2669 | 2669 | 2195 | 2028 | 2028 2028 | 2222 | 20202 | 0202 | 2028 | 2028 | 2028 | 2028 | 2028 | 2028 | 2028 | 2116 | 5222 | 2225 | 2116 |
| | VIC 1 | | 0.17 | 0.17 | 0.17 | 0.17 | 0.17 | 0.17 | 0.35 | 0.18 | 0.16 | 0.19 | 0.29 | 8 | 1.15 | 0 | 4 0 | | 0 75 | 120 | 0000 | 0:30 | 0.32 | 0.34 | 0.34 | 8 9 | 800 | 3 | | 0.28 | 0.28 | 0.32 | 0.32 | ъ С | 0.34 | 80 | 30 | 0 0 0 0 0 | | 0.32 | 80 | 0.31 | 0.31 | | 500 | 10.0 | 0.33 | 0.31 | 0.31 | 0.31 | 0.33 | 0.31 | 0.01 | 0.22 | 0.24 | 0.24 | 80 |
| | TRAFFIC VEW POINT | RATE | 4.6 | 4.6 | 4.5 | 46 | 46 | 46 | 5.1 | 6.8 | 6.8 | 6.2 | 31.5 | 80 | 8.0 | 0 | 0 | | 87 | -85 | -92 | -6.5 | 1,6 | 1,6 | 1.6 | 1.6 | 1.6 | 0.0 | 0 | 1 | 5.4 | 22 | 2.2 | 2.2 | 22 | 22 | 2.2 | 212 | 10 | 1.0 | 3.5 | 19.4 | 19.4 | 1.9.1 | 5.0 | 101 | 19.4 | 19.4 | 19.4 | 19.4 | 19.4 | 18 | 1.8 | 57 | 30 | 3.0 | 5.7 |
| | PRESENT | DEMAND | 520 | 382 | 250 | ŝ | 092 | 250 | 2 | 307 | 307 | 307 | 469 | 3008 | 1992 | RCZ | AC | 1474 | 1171 | 522 | 522 | 522 | 522 | 522 | 522 | 25 | 522 | 200 | 020 | 791 | 721 | 653 | 653 | 653 | 653 | 653 | 322 | | 417 | 417 | 361 | 544 | 3 | , | 22 | 102 | SAA | 544 | 544 | 544 | 544 | 544 | 544 | 352 | 346 | 345 | 346 |
| POINT | TRAFFIC F | 7 | 1514 1514 | 1514 | 1497 | 1497 | 1497 | 1512 | 1560 | 1711 | 1711 | 1624 | 1843 | 1854 | 1730 | 19// | 1/83 | 1801 | 1805 | 1531 | 1752 | 1762 | 1623 | 1531 | 1538 | 1762 | 1531 | 15/8 | 2002 | 2540 | 2580 | 2051 | 2051 | 1940 | 1940 | 1994 | 1994 | 1731 | 1291 | 1291 | 1576 | 1749 | 1749 | At / 1 | 86/1 | 6471 | 1649 | 1749 | 1749 | 1749 | 1649 | 1749 | 1749 | 1578 | 1435 | 1439 | 1578 |
| FROM FUNCTIONAL VIEW POINT | I I | PEDESTRIAN | | | | | | | | | | | | Hoh | | | | | | | - | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | + | | | | |
| L N N | 5 | σ | 22 | | ┝┥ | -1 | H R S | 1 | | | | ÷ | Lan | | | | \dagger | | ╈ | | | e. | - | | | | 89 | + | | 3 | f | | | H | Н 20 | 1 | 5 | 12.0 | 1 | | H | | R S S | + | 1 | | t | 1 | ł | F | | | a | ╋ | | L&P | |
| ROMF | SIDE | LOW | 990 | 0.50 | 0,50 | 05.0 | 0.50 | 3 | - | | | | 0.39 | | | _ | | 3 | | | 2.50 | 1.70 | | | | | 0.35 | 0.35 | | <u> </u> | 0.8 | | | | 0.58 | | 0.55 | 4 00 | | | | 0.50 | 0.36 | | | | 0.56 | 0.54 | 0.55 | 0.54 | 0.92 | | | 2 2 | | 0.3 | |
| UL. | CARRIAGE | HLIOM | 6.70 | 6.80 | 0.74 | 6.85 | 88 | 2002 | 6.19 | 5.18 | 6.10 | 6.10 | 5.56 | 0.S | 6.75 | 8.0 | 0/0 | 04.0 | 200 2 | 8.30 | 13.70 | 12.60 | 7.55 | 5.84 | 5.70 | 7.32 | 6.76 | 6.74 | 9/% 8/% | 2A.O | 7.28 | 8.90 | 6.55 | 8,45 | 6.78 | 6.90 | 8,10 | 5 00 S | 6.80 | 6.9 | 6.70 | 6.70 | 6.70 | 07.7 | 0.75 | -9-10 9-90 | 6.85 | 7.20 | 6.75 | 6.70 | 6.60 | 89 | 6.85 A 60 | 3.45 | \$70 | 6,70 | 6.90 |
| | 3 L | BRDGE | S88 ABA | 288 - | SBB | SBS | SEB | SBB | SBB | SBB | 80g | SBB | - 884 | ğ | DBS | 200 | 300 | 000 | and of the second se | SBB | SBB | SBB | SBB | - SBB | PRB | 888 8 | 588 | 222 | 0 | 320 | SAC | SBE | SBB | 888 8 | SBB | SBB | BBS | 304 | SBB | SBB | SBB | SBC | SBC | | | | SBC | SBC | SBC | SBC | 8 B G | 288 288 | 000 | 302 | SBC | RC8 | RCB |
| | CAPACITY | | SSAL | SSAL | SSAL | SSAL | SSAL | SSAL | SSAL | SSAL | P/A | SSAL | STAL | STAL | STAL | SIAL | SCAL | 2001 | SCAL | SSAL | SSAL | SSAL | SSAL | SSAL | STAL | STAL | SSAL | SSAL | 21AL | O ML | STAI | SSAL | SSAL | SSAL | SSAL | SSAL | SSAL | STAL | SSAL | SSAL | STAL | STAL | STAL | SIAL | SIAL | 014 0 | STA | STAL | STAL | STAL | STAL | STAL | STAL | STAL | STAL | STAL | STAL |
| | STUDY | | ~ | 101 | 2 | N | NG | 10 | 0 | 2 | 0 | 5 | e | 9 | 0 | | 4 0 | 20 | 20 | 5 | e | 2 | 6 | 6 | Ð | 0 | 0 | 6 | ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,, | 20 | | e | 0 | 9 | Ċ | e) | 3 | 56 | , | 2 | 3 | 0 | ന | 3 | 5 | | 50 | 0 | 0 | 0 | e | 3 | | 50 | 9 | 9 | e) |
| | YEAR BUILT | | 1950 | 1950 | 1950 | 0350 | 255 | 058 | 1950 | 1930 | 1935 | 1951 | 0/61 | <u>8</u> | 1950 | 0.61 | 0681 | 220 | | 1950 | 1940 | 1950 | 1950 | 1960 | 1960 | 1960 | 1950 | 1958 | 1932 | 0301 | 1584 | 1950 | 1950 | 1950 | 1950 | 1950 | 1940 | 1950 | 1050 | 1950 | 1950 | 1950 | 1950 | 0.6 | 1950 | 0081 | 1050 | 1950 | 1950 | 1950 | 1961 | 1930 | 1930 | 096 | 1950 | 1960 | 1950 |
| | DISTRICT | | K PILAH | K PILAH | K PILAH | K PILAH | K PILAH | K PILAH | JEMPUL | JELEBU | JELEBU | BENTONG | JEMPUL | MANJUNG | MANUUNG | UCCAMA | SEGAMAL DALIAT | | RATIPAHAT | SEREMBAN | SEREMBAN | SEREMBAN | K PICAH | K PILAH | K PILAH | K PILAH | KPEAH | K PILAH | OT STATES | U.LANGAI | 11 ANGAT | - Cc | Dd | PD | SEREMBAN | SEREMBAN | SEREMBAN | PETALING DETALING | | HLR PERAK | BTG PADANG | BTG PADANG | BTG PADANG | BIG PADANG | BTG PAUANG | BIG PAUANG | RTG PADANG | BTG PADANG | BTG PADANG | BTG PADANG | Lipis | UPIS | LIPIS | MANJUNG | LAMSSELAMA | LEWRISELAMA | LEMESELAMA |
| | STATE | | SN N | SN | SN SN | | SN | | | | | - | | -+ | 1 | + | + | ╈ | ╈ | T | t | t | t | f | | | | | 1 | + | T | T | Г | Γ | | | 1 | SELANGUH | Т | Τ. | Γ | Π | | Τ | 1 | Т | Ŧ | | Т | 1 | | PAHANG | PAHANG | PERAK | PERAK | PERAK | PERAK |
| | ٦, | | 00901420 | 00010600 | 00220600 | 00902360 | 00902430 | 0004300 | 06190600 | 01020900 | 00840600 | ÷ | 01105770 | ∽ł | | | 0/23039/0 | <u>.</u> | | - | + | + | - | 2280 | 102380 | | 03000 | 05103300 | | 00500540 | 4870 | + | + | 301190 | $\left \cdot \right $ | | -+ | 05403460 | + | + | +- | | 05901070 | -t | -ŀ | -h | 00000000 | + | 0590220 | 1 | 05905010 | 05905290 | 05906010 | 000001240 | CONTRACTOR OF CONTRACTOR | 06005220 | 06005740 |
| | Č, | _+ | 1. | 127 | | | | 1 | I | | | | 137 0 | - 1 | - | - 1 | | 1 | | | | 147 | L. | - | | | 152 | 153 | 4 | 24 | 157 | -l | <u> </u> | 160 | | 162 | _1 | ł | 391 | | 4 | L | · I | ł | _[| | | 2 | | 178 | 1.1 | 180 | | ZD Cal | 1 | · · · | 186 |

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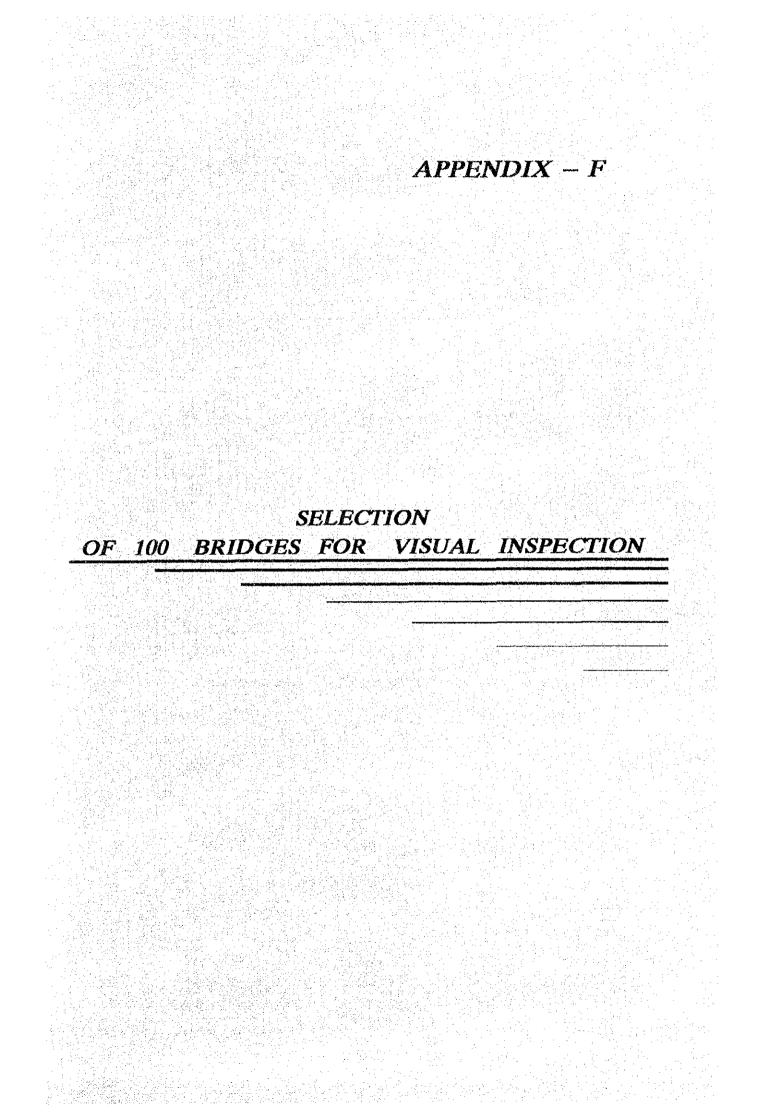
APPENDIX -E PRELIMINARY EVALUATION RESULTS AND ASSIGNMENT RESULTS OF CONCEIVABLE REHABILITATION PLAN

E – 3

APPENDIX-E PRELIMINARY EVALUATION RESULTS AND ASSIGNMENT RESULTS OF CONCEIVABLE REHABILITATION PLAN FROM FUNCTIONAL VIEW POINT

| Sinter Sinter< | $ \begin{array}{ c $ | LSIQ | DISTRICT | REAR Built | STUDY | CAPACITY | ž z | CARRINGE | | _, ¢ | ç Ş | TRACCIO | TRAFFIC | TRAFFIC VEW POINT | INT VIC | VEMORY | RIVER VEW POINT | CONCEIVABLE REHARTERIZATION |
|---|---|---------------------|----------|---------------|---------|-------------|-------|----------|--------|------|----------|----------|---------|-------------------|------------|--------|-----------------|--------------------------------|
| 0 55/4 55 5 <th>$\begin{array}{ c c c c c c c c c c c c c c c c c c c$</th> <th></th> <th>3</th> <th>i</th> <th></th> <th></th> <th>Beege</th> <th>HIGHA</th> <th>HIOM</th> <th>5 er</th> <th>CESTRIAN</th> <th>CAPACITY</th> <th>DEMAND</th> <th>RATE</th> <th>2</th> <th></th> <th>OPENNING</th> <th>SWIG</th> | $ \begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | 3 | i | | | Beege | HIGHA | HIOM | 5 er | CESTRIAN | CAPACITY | DEMAND | RATE | 2 | | OPENNING | SWIG |
| 85% 888 6.5 1.6 1 | 0 SSAL SSAL <t< td=""><td>LAMASELAMA</td><td>-</td><td>950</td><td></td><td>Ľ</td><td>SBB</td><td>5.34</td><td></td><td>1</td><td></td><td>1405</td><td>345</td><td>5.7</td><td>0.25</td><td>2114</td><td></td><td></td></t<> | LAMASELAMA | - | 950 | | Ľ | SBB | 5.34 | | 1 | | 1405 | 345 | 5.7 | 0.25 | 2114 | | |
| 0 55.4 58 50.0 1 105 106 106 54.4 0.0 7.M 588 50.0 1 105 50.0 106 54.4 0.0 7.M 589 50.0 1 105 50.0 106 54.4 0.0 7.M 589 50.0 106 54.4 0.0 106 54.4 0.0 7.M 509 500 0< | Sinch Sinch <th< td=""><td>PAHANG I JERANTUT 1</td><td>-</td><td>930</td><td>6</td><td></td><td>SBB</td><td>6.30</td><td></td><td></td><td></td><td>1405</td><td>169</td><td>5,4</td><td>0.12</td><td>2123</td><td></td><td></td></th<> | PAHANG I JERANTUT 1 | - | 930 | 6 | | SBB | 6.30 | | | | 1405 | 169 | 5,4 | 0.12 | 2123 | | |
| 3 874 888 500 10 106 | 3 874 888 500 10 100 54 0.01 3 874 886 500 10 100 100 54 0.01 3 75 600 500 100 100 100 100 100 3 874 886 500 100 100 100 100 100 3 874 886 500 100 100 100 100 100 3 874 886 500 100 100 100 100 100 3 874 886 500 100 100 100 100 100 3 874 886 500 100 100 100 100 100 3 874 886 500 100 100 100 100 100 3 874 886 500 100 100 100 100 100 3 814 816 500 100 100 100 100 3 814 816 500 100 100 100 100 3 814 816 500 616 616 | JERANTUT | | 1930 | 3 | | SBB | 6.15 | | | | 1405 | 169 | 5.4 | 0.12 | 2123 | | |
| 3 974 56 57 10 105 3 974 566 500 100 100 9 974 566 500 100 100 9 974 566 500 100 100 9 974 566 500 100 100 9 974 566 500 100 100 9 974 566 500 100 100 9 974 100 100 100 100 9 974 100 100 100 100 9 974 100 100 100 100 9 974 100 100 100 100 9 974 100 100 100 100 9 974 100 100 100 100 9 974 100 100 100 100 9 974 100 100 100 100 9 974 100 100 100 100 9 974 100 100 100 100 9 974 100 100 100 | 9 9 <td>JERANTUT</td> <td></td> <td>1930</td> <td>Ð</td> <td>STAL</td> <td>SBB</td> <td>5.60</td> <td></td> <td></td> <td></td> <td>1405</td> <td>169</td> <td>5.4</td> <td>0.12</td> <td>2123</td> <td></td> <td></td> | JERANTUT | | 1930 | Ð | STAL | SBB | 5.60 | | | | 1405 | 169 | 5.4 | 0.12 | 2123 | | |
| 9 PAA 589 566 1 140 146 168 573 169 574 100 100 574 100 576 100 576 100 576 100 576 100 576 100 576 100 576 100 | 0 P/M 588 656 1 </td <td>JERANTUT</td> <td></td> <td>1930</td> <td>0</td> <td>STAL</td> <td>SBB</td> <td>5.70</td> <td></td> <td></td> <td></td> <td>1405</td> <td>169</td> <td>5.4</td> <td>0.12</td> <td>2183</td> <td></td> <td></td> | JERANTUT | | 1930 | 0 | STAL | SBB | 5.70 | | | | 1405 | 169 | 5.4 | 0.12 | 2183 | | |
| 3 PAR R58 558 146 145 3 PAR R58 558 138 146 3 Sixt Sixt Sixt Sixt 36 44 23 3 Sixt Sixt Sixt Sixt 185 147 146 3 Sixt Sixt Sixt Sixt 185 147 146 3 Sixt Sixt Sixt Sixt 185 147 146 3 Sixt Sixt Sixt Sixt Sixt 185 147 146 3 Sixt Sixt Sixt Sixt Sixt Sixt 146 185 3 Sixt Sixt Sixt Sixt Sixt Sixt Sixt 144 Sixt 3 Sixt Sixt Sixt Sixt Sixt Sixt Sixt 144 3 Sixt Sixt Sixt Sixt Sixt Sixt Sixt 144 Sixt 3 Sixt Sixt Sixt Sixt Sixt Sixt Sixt Sixt Sixt 3 Sixt Sixt Sixt Sixt Sixt | 9 PAR RSB 550 Par | | | 1930 | 8 | P/A | SBB | 6.65 | | | | 1490 | 169 | 5.4 | | 2125 | | |
| 3 5 7.4 7.33 0.50 1.54 7.33 0.50 3 5.14 7.33 0.50 1.54 7.33 0.50 1.54 7.33 3 5.14 7.33 0.50 1.56 1.46 1.55 1.73 0.50 3 5.14 7.33 0.50 1.56 1.47 7.33 1.56 1.47 3 5.50 5.50 1.56 1.56 1.46 1.55 1.7 2.33 0.17 3 5.50 5.50 1.56 7.34 1.56 7.34 1.56 7.34 0.73 3 5.51 7.34 1.56 7.34 1.56 7.35 0.74 3 5.51 1.56 7.34 1.56 7.35 0.74 3 5.51 1.56 7.34 1.55 7.35 0.17 5 5.51 1.56 7.36 1.56 7.35 0.17 5 5.51 5.56 1.56 7.35 1.55 7.35 0.17 5 5.51 5.56 1.56 7.35 1.55 7.35 0.17 5 5.51 5.56 1.56 1.55 1.5 | 2 3 5 4 0 <td></td> <td>-+</td> <td>1930</td> <td>5</td> <td>P/A</td> <td>SBB</td> <td>5.60</td> <td></td> <td>-</td> <td></td> <td>1405</td> <td>169</td> <td>5.4</td> <td>0.12</td> <td>2123</td> <td></td> <td></td> | | -+ | 1930 | 5 | P/A | SBB | 5.60 | | - | | 1405 | 169 | 5.4 | 0.12 | 2123 | | |
| 3 5/1 7/1 7/2 7/20 7/20 7/20 7/20 3 5/1/L 7/2 7/20 7/20 7/20 7/20 7/20 7/20 3 5/1/L 7/2 7/20 7/20 7/20 7/20 7/20 7/20 2 5/1/L 7/2 7/20 7/20 7/20 7/20 7/20 7/20 2 5/1/L 7/2 7/20 7/20 7/20 7/20 7/20 7/20 2 5/1/L 7/2 7/20 7/20 7/20 7/20 7/20 7/20 2 5/1/L 7/20 7/20 7/20 7/20 7/20 7/20 7/20 2 5/1/L 7/20 7/20 7/20 7/20 7/20 7/20 7/20 2 7/2/L 5/20 7/20 7/20 7/20 7/20 7/20 7/20 2 7/2/L 5/20 7/20 7/20 7/20 7/20 7/20 7/20 2 7/2/L 5/20 7/20 7/20 7/20 7/20 7/20 7/20 2 5/2/L 5/20 1/1/20 5/20 1/1/20 5/20 7/2 | 3 5 5 7 7 <td>-</td> <td>· 🕴</td> <td>1995</td> <td></td> <td></td> <td>200</td> <td>000</td> <td></td> <td></td> <td></td> <td>1022</td> <td>0/0</td> <td>4.4</td> <td>200</td> <td>3</td> <td></td> <td></td> | - | · 🕴 | 1995 | | | 200 | 000 | | | | 1022 | 0/0 | 4.4 | 200 | 3 | | |
| 3 3 3 3 4 4 0 3 3 4 4 0 3 3 3 3 4 4 4 4 4 4 3 3 3 4 4 4 4 4 4 3 3 3 4 4 4 4 4 4 3 3 5 6 4 6 6 6 0 3 5 6 6 6 6 6 0 3 5 6 6 6 6 0 1 4 5 6 6 6 6 0 1 5 5 6 6 6 6 0 1 6 6 6 6 6 6 0 1 7 8 6 6 6 6 0 1 1 7 8 6 6 6 6 0 1 8 6 6 6 6 6 0 1 8 6 6 6 6 6 0 7 <td>2 5 5 5 5 5 5 5 5 2 5 5 5 5 5 5 5 5 2 5 5 5 5 5 5 5 5 3 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5<td>KMUUASIK</td><td>~t-</td><td>1040</td><td></td><td>P/A STAL</td><td>222</td><td>080</td><td>-†</td><td>001</td><td></td><td>1822</td><td>5/6</td><td>4 4</td><td></td><td>855</td><td></td><td></td></td> | 2 5 5 5 5 5 5 5 5 2 5 5 5 5 5 5 5 5 2 5 5 5 5 5 5 5 5 3 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 <td>KMUUASIK</td> <td>~t-</td> <td>1040</td> <td></td> <td>P/A STAL</td> <td>222</td> <td>080</td> <td>-†</td> <td>001</td> <td></td> <td>1822</td> <td>5/6</td> <td>4 4</td> <td></td> <td>855</td> <td></td> <td></td> | KMUUASIK | ~t- | 1040 | | P/A STAL | 222 | 080 | -† | 001 | | 1822 | 5/6 | 4 4 | | 855 | | |
| 2 2 <td>3 3<td>BALING</td><td></td><td>1950</td><td>2</td><td>STAL</td><td>24</td><td>394</td><td>$^{+}$</td><td>5</td><td></td><td>1800</td><td>578</td><td>200</td><td>0.30</td><td>2153</td><td></td><td></td></td> | 3 3 <td>BALING</td> <td></td> <td>1950</td> <td>2</td> <td>STAL</td> <td>24</td> <td>394</td> <td>$^{+}$</td> <td>5</td> <td></td> <td>1800</td> <td>578</td> <td>200</td> <td>0.30</td> <td>2153</td> <td></td> <td></td> | BALING | | 1950 | 2 | STAL | 24 | 394 | $^{+}$ | 5 | | 1800 | 578 | 200 | 0.30 | 2153 | | |
| 0 5/K F 7/3 7/0 L8 11 7/3 1/0 0 5/K F 7/3 7/0 L8 11 1/3 1/3 1/3 0/3 5/K 5/K 5/K 5/K 1/3 1/3 1/3 1/3 1/3 1/3 1/3 5/K 5/K 5/K 5/K 1/3 1/3 1/3 1/3 1/3 1/3 5/K 5/K 5/K 5/K 5/K 5/K 1/3 1/3 1/3 5/K 5/K 5/K 5/K 5/K 1/3 1/3 1/3 5/K 5/K 5/K 5/K 5/K 1/3 1/3 5/K 5/K 5/K 5/K 5/K 5/K 0/1 5/K 5/K | 0 5/K 1 1 2/3 1 0 0 0 5/K 1 5/3 1 1 1 1 1 1 1 5/K 5/K 1 5/K 1 1 1 1 1 1 5/K 5/K 1 1 1 1 1 1 1 1 5/K 1 1 1 1 1 1 1 1 1 1 5/K 1 1 1 1 1 1 1 1 1 1 1 5/K 1 1 1 1 1 1 1 1 1 1 1 5/K 1 1 1 1 1 1 1 1 1 1 1 5/K 1 1 1 1 1 1 1 1 1 1 1 5/K 1 1 1 1 1 1 1 1 1 1 1 1 5/K 1 1 1 1 1 1 1 1 1 1 1 1< | HLR PERAK | + | 1950 | 0 | STAL | SBB | 7.02 | Ť | | | 1551 | 417 | -3.3 | 0.27 | NIA | | |
| $ \begin{array}{ c c c c c c c c c c c c c c c c c c c$ | 2 2 2 1 2 <td>HLR PERAK</td> <td>-}-</td> <td>1970</td> <td>8</td> <td>STAL</td> <td>11</td> <td>7 34</td> <td>1.08</td> <td>18.9</td> <td></td> <td>1551</td> <td>412</td> <td>-33</td> <td>0.27</td> <td>A/N</td> <td></td> <td></td> | HLR PERAK | -}- | 1970 | 8 | STAL | 11 | 7 34 | 1.08 | 18.9 | | 1551 | 412 | -33 | 0.27 | A/N | | |
| 20 SSAL SSB 570 1.36 2.36 5.0 0.1 21 SSAL SSB 5.00 1.36 2.36 0.1 1.46 2.36 5.0 0.1 21 SSAL SSB 5.00 1.36 2.36 5.00 0.1 1.46 2.36 5.0 0.1 21 SSAL SSB 5.00 1.36 2.36 5.00 0.1 1.46 2.36 0.1 21 SSAL SSB 5.00 1.36 2.36 0.0 0.1 1.46 2.36 0.1 21 SSAL SSB 5.00 1.46 1.46 2.36 0.1 1.46 2.36 0.1 1.46 22 SSAL SSB 5.00 1.46 1.46 2.36 0.1 1.46 23 SSAL SSB 6.0 0.33 1.46 2.36 0.1 1.46 23 SSAL SSB 6.0 0.36 1.46 1.46 2.36 0.1 24 SSAL SSB 6.0 0.36 1.46 1.46 2.36 0.1 25 SSAL SSB 6.0 0.36 0.36 0.36 | No. Solu | BTG PADANG | +- | 1950 | 0 | STAL | SBB | 5 60 | | | | 1463 | 417 | 5.6- | 020 | AIN | | |
| x STA SSB Field A SSB 5.80 7.00 R SS SS <ths< th=""> SS <t< td=""><td>x x</td><td>K KANGSAR</td><td></td><td>1950</td><td>2</td><td>SSAL</td><td>SBB</td><td>5.70</td><td></td><td>-</td><td></td><td>1431</td><td>258</td><td>5.0</td><td>0.18</td><td>2133</td><td></td><td></td></t<></ths<> | x | K KANGSAR | | 1950 | 2 | SSAL | SBB | 5.70 | | - | | 1431 | 258 | 5.0 | 0.18 | 2133 | | |
| 0 554 1550 258 55 0 554 560 1550 258 55 0 574 586 570 1550 258 55 0 574 586 570 144 256 61 0.1 1 144 586 5.00 1144 256 66 0.2 1 144 586 5.00 1144 256 66 0.2 1 144 586 5.00 1160 256 66 0.2 1 506 506 1160 256 66 0.2 1 506 506 1160 256 66 0.2 1 506 506 1150 256 66 0.2 1 506 506 1550 1550 256 66 0.2 1 506 506 1550 1550 256 66 0.2 1 506 506 1550 1550 256 61 0.2 1 506 61 1550 1550 1550 1550 150 1 507 506 1550 1550 155 | 0 354 396 556 1550 258 55 0.1 0 574 396 556 1550 258 55 0.1 1550 574 396 570 1550 258 55 0.1 1550 574 396 570 110 355 55 0.1 1550 554 396 570 110 355 55 0.1 1550 554 396 570 110 355 55 0.1 1650 554 396 570 110 355 55 0.1 1650 554 396 570 110 355 55 0.1 1650 554 396 570 110 355 55 0.1 1650 554 396 570 110 355 35 110 355 1714 356 6.23 4.85 4.85 4.85 35 35 36 0.0 1744 356 6.23 4.85 4.85 4.85 37 4.9 0.35 1745 356 6.23 4.95 1.550 271 274 0.05 < | K KANGSAR | 1- | 1950 | 4 | STAL | SBB | 5.80 | 1.06 | æ | | 1550 | 258 | 5.5 | 6.17 | 2122 | | |
| 3 554 569 570 1550 259 55 0.1 3 574 588 570 1104 559 55 0.1 3 574 588 570 1104 559 55 0.1 3 574 588 500 1104 559 55 0.1 3 574 588 500 1104 555 6.0 0.1 3 534 588 500 1104 555 6.0 0.2 5 50 536 500 1104 555 6.0 0.2 5 50 536 50 1104 555 55 0.1 5 534 588 5.0 1104 555 55 0.1 5 534 588 5.0 1104 555 1104 0.25 5 5 5 5 5 5 5 5 0.1 5 5 5 6 5 5 5 5 5 5 5 5 6 5 5 5 5 5 5 5 6 6 5 5 | 0 554 560 1550 258 55 0.17 1 570 1 1550 258 55 0.17 2 554 570 1 144 255 0.17 353 556 1 1 144 255 0.17 353 556 1 1 1 144 255 0.17 353 556 1 1 1 1 255 0.17 353 556 1 1 1 1 255 0.17 353 556 536 66 0.23 1 0.22 353 556 64 1 1 1 1 0.22 354 358 6.36 6.6 0.16 0.23 1 1 355 556 6.40 1 1 1 1 1 355 556 6.40 1 1 1 0.27 1 355 556 6.55 1 1 1 1 0 355 556 6.55 1 1 1 1 1 355 554 556 6.55 1 </td <td>HULU PERAK</td> <td>┝</td> <td>1950</td> <td>0</td> <td>SSAL</td> <td>See</td> <td>5.60</td> <td></td> <td></td> <td></td> <td>1550</td> <td>258</td> <td>5.5</td> <td>10.17</td> <td>2122</td> <td></td> <td></td> | HULU PERAK | ┝ | 1950 | 0 | SSAL | See | 5.60 | | | | 1550 | 258 | 5.5 | 10.17 | 2122 | | |
| 0 51AL 36i 700 1500 256 600 011 1 31AL 36i 570 1104 256 60 021 2 55AL 36i 5.00 1104 355 66 0.22 2 55AL 36i 5.00 1104 355 66 0.22 3 55AL 36i 6.00 0.11 1046 355 0.0 3 55AL 36i 6.00 0.12 1104 355 0.0 3 55AL 36i 6.00 0.16 1104 355 0.0 3 55AL 36i 6.00 0.16 0.22 0.17 3 55AL 36i 6.00 0.16 0.16 0.22 3 55AL 36i 6.00 0.16 0.16 3 55AL 566 6.00 0.16 3 | 0 51AL 361 700 1150 253 60 0.1 2 53AL 386 5.0 1104 253 66 0.2 2 53AL 386 5.0 1104 253 66 0.2 2 53AL 386 5.0 1104 253 66 0.2 3 53AL 386 5.0 1104 253 146 0.2 3 53AL 386 5.0 1105 277 7.4 0.2 3 53AL 586 6.1 0.2 1550 277 7.4 0.2 3 53AL 586 6.1 0.2 1550 1550 277 7.4 0.2 3 53A 53A 1350 4.6 0.2 0.2 0.7 3 53A | HULUPERAK | ╄ | 1950 | 0 | SSAL | SBB | 5,60 | | | | 1550 | 258 | 5.5 | 0.17 | 2122 | | |
| 3 57.4L 589 570 1445 258 6.0 0.19 3 53.4L 589 5.00 1104 583 6.0 0.29 3 53.4L 589 5.00 1104 583 6.0 0.29 5 55.4L 589 5.00 1104 583 6.0 0.29 5 55.4L 589 6.27 1.104 583 6.0 0.29 5 55.4L 589 6.27 1.104 583 6.0 0.29 5 55.4L 589 6.27 1.104 583 7.4 0.29 5 55.4L 589 6.27 1.105 233 7.4 0.29 5 55.4L 589 6.27 1.106 533 7.4 0.29 5 55.4L 589 6.21 1.106 233 7.4 0.29 5 5 5 6.16 0.29 277 7.4 0.29 5 5 5 6.16 0.29 277 7.4 0.29 5 5 5 1.106 5 1.106 5 0.10 5 5 5 < | 3 574. 388 570 11645 258 6.0 0.19 3 514. 388 5.00 1164 258 6.0 0.29 3 534. 388 5.00 1164 258 6.0 0.29 3 534. 388 5.00 1164 258 6.0 0.29 3 534. 388 5.00 1164 258 6.0 0.29 3 534. 388 5.00 1164 258 6.0 0.29 3 534. 388 5.00 1164 258 6.0 0.29 3 534. 388 6.0 1164 258 6.0 0.29 3 534. 388 6.29 4.0 1164 258 2.1 1164 3 534. 388 6.8 0.8 1164 2.28 0.6 0.29 3 534. 388 6.8 0.8 1156 2.1 114 0.02 3<54. | HULU PERAK | - | 1950 | 0 | STAL | SBB | 2.00 | | | | 1530 | 258 | 8.0 | 0.17 | 2081 | | |
| 3 57AL 589 6.65 1104 553 6.6 0.032 5 500 500 1104 553 6.6 0.032 5 500 500 1104 553 6.6 0.032 5 500 500 1104 553 174 0.03 5 5 6 6.0 5 170 175 174 0.03 5 5 6 6 6 0.03 175 174 0.03 5 5 6 6 6 0.03 175 174 0.03 5 5 6 6 6 0.03 175 174 0.03 5 7 889 6.21 1750 277 174 0.03 5 7 5 0.14 1550 277 174 0.03 5 7 5 0.21 1550 4.15 0.16 0.02 5 7 5 0.21 1550 4.16 0.17 0.02 5 7 5 0.21 1550 4.16 0.16 0.02 7 7 5 0.21 1550 4 | 3 5:AL 539 6.65 1104 553 6.6 0.032 3 5:AL 539 5.06 1104 553 6.6 0.032 3 5:AL 539 5.06 1104 553 6.6 0.032 5 5:AL 539 6.50 1104 553 14 0.16 5 5:AL 539 6.50 1104 553 154 0.02 5 5:AL 539 6.50 1104 553 154 0.02 5 5 6.6 6.75 1550 217 7.4 0.16 5 5 5 6.8 6.25 1550 217 7.4 0.016 5 5 5 5 6.8 1.025 1.164 5<5 | HULUPERAK | \vdash | 19SC | 0 | STAL | 888 | 5.70 | | | | 1443 | 258 | 8.0 | 0.18 | 2080 | | - |
| 2 SSAL SSB 5.00 11(44) 855 6.6 0.022 3 SSAL SSB 5.00 11(52) 353 7.4 0.022 3 SSAL SSB 6.02 353 7.4 0.022 3 STAL SSB 6.02 353 7.4 0.022 3 STAL SSB 6.02 353 7.4 0.021 3 STAL SSB 6.03 4.65 4.15 9.15 7.4 0.021 3 STAL SSB 6.03 4.65 4.15 9.15 2.7 7.4 0.021 3 STAL SSB 4.65 4.15 11500 2.77 7.4 0.021 3 STAL SSB 4.65 4.15 11500 2.77 7.4 0.021 3 STAL SSB 6.23 4.16 9.16 0.021 9.021 3 STAL SSB 6.23 4.16 9.16 0.021 3 STAL SSB 6.23 6.23 0.01 0.01 3 STAL SSB 6.23 6.23 0.01 0.021 3 STAL | 2 SSAL 383 5.00 1104 383 6.6 0.02 3 SSAL 389 5.05 1104 383 7.4 0.02 3 SSAL 389 5.36 1520 353 7.4 0.02 3 SSAL 389 5.36 1520 353 7.4 0.03 3 SSAL 389 5.36 1520 353 7.4 0.03 3 SSAL 389 5.31 1530 353 7.4 0.03 3 SSAL 389 6.40 1530 353 7.4 0.03 3 SSAL 389 6.31 1530 415 9.1 0.7 3 SSAL 389 6.21 1530 415 9.1 0.7 3 SSAL 389 6.21 1530 415 9.1 0.7 3 SSAL 389 6.21 1530 416 0.03 3 STAL 589 6.21 1530 416 0.01 3 STAL 589 6.21 0.1 0.21 0.21 3 STAL F63 6.1 0.21 0.21 | SEREMBAN | | 1950 | e) | STAL | SBB | 6.95 | | | | 1104 | 353 | 6.6 | 0.32 | 2089 | | |
| 3 SSAL SS6 5.06 1104 SS3 5.0 3 SSAL SS6 6.02 7.4 0.22 3 SSAL SS6 6.02 3.33 7.4 0.22 3 SSAL SS6 6.02 4.05 0.02 3.33 7.4 0.22 3 SSAL SS6 6.03 6.03 7.4 0.23 7.4 0.22 3 SSAL SS6 4.05 0.05 4.05 0.05 3.33 7.4 0.22 3 SSAL SS6 4.01 1500 4.15 7.7 0.16 0.21 3 SSAL SS6 4.01 1500 4.15 1500 4.15 0.17 3 SSAL SS6 4.01 1500 4.16 1500 2.1 0.27 3 SSAL SS6 4.01 1500 4.16 0.27 0.17 3 SSAL SS6 4.01 1500 4.16 0.27 3 SSAL SS6 4.01 1500 4.16 0.27 3 SSAL SS6 4.01 1.02 1.02 3 SS6 4.01 | 3 SSAL S86 5.06 1104 353 6.6 0.32 3 SSAL S89 6.34 589 6.34 0.02 3 SSAL S89 6.34 1104 353 7.4 0.22 3 SSAL S89 6.34 1530 353 7.4 0.22 3 SSAL S89 6.34 1530 353 7.4 0.22 3 SSAL S89 4.45 1.530 2.77 7.4 0.27 3 SSAL S89 4.45 1.530 2.77 7.4 0.27 3 SSAL S89 4.45 1.530 2.77 7.4 0.27 3 SSAL S89 4.45 1.530 4.15 9.1 0.27 3 SAL S89 4.45 1.530 4.15 9.1 0.27 3 SAL S89 4.45 1.530 4.15 9.1 0.27 3 SAL S89 4.15 9.1 0.27 1.24 0.27 3 SAL S89 4.16 1.530 4.16 0.27 3 SAL POS SAL < | SEREMBAN | _ | 1950 | 2 | SSAL | 888 | 5.00 | | | | 1.04 | 353 | 6.6 | 0.32 | 2089 | | 1 |
| 3 SSAL SSB 632 1622 333 7.4 0.02 3 SSAL SSB 6.34 4.65 LMR 1715 7.4 0.02 3 SSAL SSB 6.33 4.65 LMR 1715 277 7.4 0.02 3 SSAL SSB 4.65 LMR 1715 277 7.4 0.02 3 SSAL SSB 4.65 LMR 1550 277 7.4 0.02 3 SSAL SSB 4.65 LMR 1550 277 7.4 0.02 3 SSAL SSB 4.65 1550 4.16 0.27 24 0.02 3 SSAL SSB 4.65 1550 4.16 0.27 24 0.02 3 SSAL SSAL SSB 4.65 1.550 4.16 0.27 24 3 SSAL SSA SSA SSA 1.550 4.16 0.27 27 3 SSAL SSA SSA SSA 1.550 4.16 0.27 0.27 3 SSAL SSA SSA SSA 1.550 4.16 0.27 0.27 < | 3 SSAL SSB 632 74 022 3 SSAL SSB 633 1713 74 023 3 SSAL SSB 633 455 LMR 74 033 3 SSAL SSB 455 LMR 713 023 3 STAL SSB 4.65 LMR 713 023 3 SSAL SSB 4.65 LMR 714 013 3 SSAL SSB 4.65 LMR 714 013 3 SSAL SSB 4.65 LMR 1550 217 7.4 013 3 SSAL SSB 4.65 L 1550 4.16 0.17 1550 217 0.27 3 SSAL SSB 6.21 1550 4.16 0.17 0.27 1550 A.16 SSAL SS6 0.21 1550 0.16 0.27 1 NLL SS6 0.21 1550 4.16 0.17 0.27 1 SS6 0.21 SSAL SS6 0.21 0.27 1 NLL SS6 0.21 1550 4.16 0.17 | SEREMBAN | - | 1950 | n | SSAL | SBB | 5.05 | | | | 1104 | 353 | 6.B | 0.32 | 2089 | | |
| 3 SSAL 388 6.34 1530 335 7.4 0.020 3 STAL 888 6.34 1550 277 7.4 0.03 3 SSAL 888 6.23 1550 277 7.4 0.03 3 SSAL 888 4.85 1550 277 7.4 0.03 3 SSAL 888 4.81 1550 215 7.4 0.03 3 SSAL 888 4.81 1550 215 7.4 0.03 3 SSAL 888 6.231 1550 216 0.02 4 1550 4.16 1550 4.16 0.02 1550 6.231 1550 4.16 0.02 1550 6.231 1550 4.16 0.02 1550 6.231 1550 4.16 0.02 1550 6.23 1550 4.15 0.02 1550 6.1 1550 4.15 0.02 1550 6.1 1550 4.15 0.02 1550 110 215 140 1550 140 1550 110 1550 150 150 1 | 334 338 6.34 1530 335 7.4 0.05 574 838 6.34 1530 335 7.4 0.05 574 838 6.23 4.55 0.63 277 7.4 0.05 74 838 6.24 1530 355 1550 277 7.4 0.05 754 838 4.40 1550 4.55 4.65 4.60 1550 277 7.4 0.05 754 838 4.40 1550 4.65 4.65 4.65 4.65 0.07 754 838 6.21 1550 4.15 9.1 0.07 9.1 0.07 755 838 6.21 1550 4.15 9.1 0.07 755 838 6.21 1550 4.15 0.07 755 838 6.21 1550 4.15 0.07 755 74 9.05 1550 4.15 0.07 755 74 74 0.07 1550 4.15 0.07 755 74 765 74 0.07 1550 1550 755 74 765 74 76 77 155 | SEREMBAN | | 1950 | e | SSAL | SBB | 6.92 | | | | 1622 | 353 | 7.4 | 80 | 2068 | | |
| 3 SML SSE 6.20 4.65 4.86 1.715 2.77 7.4 0.16 3 SSAL SSE 4.20 4.65 4.65 4.65 4.77 7.4 0.16 3 SSAL SSE 4.65 4.65 4.65 4.65 4.67 7.4 0.16 3 SSAL SSE 4.67 1.500 4.13 1.500 4.13 0.27 3 SSAL SSE 4.61 1.500 4.19 1.500 4.19 0.27 3 SSAL SSE 6.21 1.500 4.19 1.500 4.19 0.27 3 SSAL SSE 6.21 1.500 4.19 0.27 0.27 1 ROS 6.21 1.500 4.19 0.27 0.27 1 ROS 6.21 1.500 4.19 0.27 1 ROS 6.21 1.500 4.19 0.27 1 ROS 6.21 1.600 1.100 0.27 2 MrAL ROS 8.10 0.16 0.16 2 MrAL ROS 1.000 1.000 2 MrAL ROS 1.000 </td <td>3 SSAL SS8 6.20 4.65 4.66 1.715 2.77 7.4 0.16 3 SSAL SS8 4.69 1.50 2.77 7.4 0.16 3 SSAL SS8 4.69 1.50 2.77 7.4 0.16 3 SSAL SS8 4.69 1.50 2.77 7.4 0.16 3 SSAL SS8 4.69 1.500 4.13 0.27 0.27 3 SSAL SS8 6.21 1.500 4.19 0.27 0.27 3 SSAL SS6 6.21 1.500 4.19 0.27 0.27 3 SSAL SS6 6.21 1.500 4.19 0.27 0.27 1 RC8 6.21 1.500 4.19 0.27 0.27 1 RC8 6.21 1.500 4.19 0.27 0.27 1 RC8 6.21 1.600 1.600 1.600 0.16 2 STAL RC8 6.21 1.600 1.600 0.16 2 STAL RC8 6.21 1.600 1.600 0.16 2 STAL RC8 6.100<td>SEREMBAN-</td><td></td><td>1950</td><td>6</td><td>SSAL</td><td>SBB</td><td>6.34</td><td></td><td></td><td></td><td>1530</td><td>353</td><td>7.4</td><td>80</td><td>2087</td><td></td><td></td></td> | 3 SSAL SS8 6.20 4.65 4.66 1.715 2.77 7.4 0.16 3 SSAL SS8 4.69 1.50 2.77 7.4 0.16 3 SSAL SS8 4.69 1.50 2.77 7.4 0.16 3 SSAL SS8 4.69 1.50 2.77 7.4 0.16 3 SSAL SS8 4.69 1.500 4.13 0.27 0.27 3 SSAL SS8 6.21 1.500 4.19 0.27 0.27 3 SSAL SS6 6.21 1.500 4.19 0.27 0.27 3 SSAL SS6 6.21 1.500 4.19 0.27 0.27 1 RC8 6.21 1.500 4.19 0.27 0.27 1 RC8 6.21 1.500 4.19 0.27 0.27 1 RC8 6.21 1.600 1.600 1.600 0.16 2 STAL RC8 6.21 1.600 1.600 0.16 2 STAL RC8 6.21 1.600 1.600 0.16 2 STAL RC8 6.100 <td>SEREMBAN-</td> <td></td> <td>1950</td> <td>6</td> <td>SSAL</td> <td>SBB</td> <td>6.34</td> <td></td> <td></td> <td></td> <td>1530</td> <td>353</td> <td>7.4</td> <td>80</td> <td>2087</td> <td></td> <td></td> | SEREMBAN- | | 1950 | 6 | SSAL | SBB | 6.34 | | | | 1530 | 353 | 7.4 | 80 | 2087 | | |
| 3 STAL RCB 6.28 1500 277 7.4 0.16 3 PiA SSAL S86 4.40 1500 277 7.4 0.16 3 PiA S86 4.61 1500 277 7.4 0.74 3 SSAL S86 4.61 1500 4.15 0.16 2 MiAL S86 6.21 1560 4.15 0.27 2 STAL S86 6.21 1560 4.16 0.27 3 S5AL S86 6.21 1560 4.16 0.27 2 MiAL R386 6.21 1560 4.16 0.27 2 STAL R386 6.21 1.00 1.16 2 STAL R08 9.1 0.27 2 STAL R08 9.1 0.27 2 STAL R08 9.1 0.27 2 STAL R | 3 STAL RC8 6.29 11500 277 7.4 0.16 3 PIA SSAL SSAL SSA 6.1 0.17 3 PIA SSA SSA 1500 277 7.4 0.16 3 PIA SSA SSAL SSA 6.1 0.27 3 SSAL SSA SSA 1500 4.15 6.1 0.27 3 SSAL SSA SSA 1550 4.15 6.1 0.27 1 SSA SSA SSA 1550 4.16 0.27 1 PC3 SSA SSA 1550 4.16 0.27 1 PC3 SSA SSA 1550 4.16 0.27 1 PC3 PC3 PC3 PC3 PC3 PC3 1 PC3 PC3 PC3 PC4 PC3 1 PC3 PC3 PC4 PC4 1 PC4 PC3 PC4 </td <td>JELEBU</td> <td>-</td> <td>1950</td> <td>0</td> <td>SSAL</td> <td>SBB</td> <td>8.20</td> <td>4.85</td> <td>L&R</td> <td></td> <td>1715</td> <td>277</td> <td>7.4</td> <td>0,16</td> <td>2090</td> <td></td> <td></td> | JELEBU | - | 1950 | 0 | SSAL | SBB | 8.20 | 4.85 | L&R | | 1715 | 277 | 7.4 | 0,16 | 2090 | | |
| 3 3 <td>3 35AL 386 440 1500 45 5 55AL 586 440 1500 45 6 1 100 1500 45 6 1 100 1500 45 6 1 100 1500 45 7 1 100 1500 45 8 621 1 100 1 1 100 1 1 1 100 1 1 1 1 0 1 1 1 0 1 1 1 0 1 1 1 0 1 1 1 0 1 1 1 0 1 1 1 0 1 1 1 0 1 1 1 0 1 1 1 0 1 1 1 0 1 1 1 0 1 1 1 0 1 1 1 0 1 1 1 0 1 1 0</td> <td>I JELEBU</td> <td>÷</td> <td>980</td> <td>Ø</td> <td>STAL</td> <td>RCB</td> <td>6.29</td> <td></td> <td></td> <td></td> <td>1530</td> <td>277</td> <td>7.4</td> <td>0.18</td> <td>2088</td> <td></td> <td></td> | 3 35AL 386 440 1500 45 5 55AL 586 440 1500 45 6 1 100 1500 45 6 1 100 1500 45 6 1 100 1500 45 7 1 100 1500 45 8 621 1 100 1 1 100 1 1 1 100 1 1 1 1 0 1 1 1 0 1 1 1 0 1 1 1 0 1 1 1 0 1 1 1 0 1 1 1 0 1 1 1 0 1 1 1 0 1 1 1 0 1 1 1 0 1 1 1 0 1 1 1 0 1 1 1 0 1 1 1 0 1 1 0 | I JELEBU | ÷ | 980 | Ø | STAL | RCB | 6.29 | | | | 1530 | 277 | 7.4 | 0.18 | 2088 | | |
| 3 3 <td>3 5 5 1 3 5 5 1 1 3 5 5 5 <t< td=""><td></td><td>+</td><td>1950</td><td>6</td><td>SSAL</td><td>SBB</td><td>4.40</td><td></td><td></td><td></td><td>1530</td><td>415</td><td>6</td><td>0.27</td><td>8/02</td><td></td><td></td></t<></td> | 3 5 5 1 3 5 5 1 1 3 5 5 5 <t< td=""><td></td><td>+</td><td>1950</td><td>6</td><td>SSAL</td><td>SBB</td><td>4.40</td><td></td><td></td><td></td><td>1530</td><td>415</td><td>6</td><td>0.27</td><td>8/02</td><td></td><td></td></t<> | | + | 1950 | 6 | SSAL | SBB | 4.40 | | | | 1530 | 415 | 6 | 0.27 | 8/02 | | |
| | | | + | 0261 | <u></u> | r/A | ABS | 4.61 | | | | 0221 | 415 | | 12.0 | 20/02 | | |
| 2 2 STAL MTAL | 2 STAL MTAL 2 STAL | | - | 1850 | 2 | NOAL | 202 | 12.0 | | _ | | 1989 | 410 | 0 | 12 1 | 0/02 | | |
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| NTAL NTAL | 2 STAL MTAL | P.PINANG SBG PRALU | [] | 1954 | 2 | STAL | CAR | | | | | | | | | | | |
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| 2 STAL | 2 STAL | KELANTAN KEHARU | | Yahya P | | | RCB | | 1 | | | | | | · | | | |
| | | BATUPAHAT | i - 1 | 1965 | 2 | STAL | PCB | | | | | | | | | | | |
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FINAL SELECTION REMARKS SELECTED SA SECTED G G G G SELECTED SA SELECTED SA SELECTED SA SELECTED CA SELECTED CA SELECTED CA SELECTED CA SELECTED CA Š SELECTED [SA 88853388 STRUCTURAL CONDITION CONCEIVABLE REHABILITATION CONCEIVABLE REHABILITATION BEAM SCOU- CONCEIVABLE PLANS PLANS DECK RING AVERAGE FROM STRUCTURAL VIEW POINT FROM RUNCTIONAL VIEW POINT fotal no's of bridges selected = 0 Total no's of bridges selected = 4 Total no's of bridges selected = 1 Total no's of bridges selected = 1 otal no's of bridges selected = 5 ADDING SDE WALK ADDING & RAISING ADDING SDE WALK ADDING SDE WALK 1.5 (SPRE SFRE 2.0 (JPRE BPRE) 2.0 (JPRE BPRE) 2.0 (JPRE BPRE) 2.5 (SRFE APRE SFRE 2.5 SELECTION OF 100 BRIDGES FOR VISUAL INSPECTION 1.3 BRP,SRPR 1.3 EJRP 20 NON 23 ARF 23 ARF 23 ARF 23 ARF 25 ARF 25 ARF 20 ARF 30 ARF 30 ARF 30 CRF 33 DCRF 33 DCRF 33 DCRF 33 DCRF 3.3 ARF 8 30.431 PCB 2 1 1 1 0 e PIER 4 ABUT. 24.80 24.80 152.88 122.88 1122.98 1122.99 122.99 122.99 122.99 122.18 122.99 122.18 122.99 122.18 122.99 122.18 122.99 122.18 122.99 122.18 122.99 1 2,18 BOX RPGE BRDGE 2.40 BOX 4.88 BOX 3.69 BOX 3.69 BOX 3.69 BOX 3.68 BOX 2.288 BOX 2.298 BOX 2. PCB PCB PCB 25.91 26.24 26.17 26.17 26.17 26.17 26.17 27.00 24.57 21.98 24.57 21.98 BRIDGE LENGTH (M) B 219.13 35.21 18.40 APPENDIX-F - 0 MAX. NO. 1 SPAN OF 1 (M) SPAN 9 12.13 15.08 15.08 16.45 12.09 11.209 11.50 11.50 14.60
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APPENDIX-F SELECTION OF 100 BRIDGES FOR VISUAL INSPECTION

| ON FINAL SELECTION REMARKS | | SELECTED CG | SELECTED SELECTED | | Stearte Steart | SELECTED SA SELECTED CA 2 | SELECTED SEL |
|---|-------------------------|------------------------------------|---|--|---|--|---|
| CONCEIVABLE REHABILITATION PLANS FROM FUNCTIONAL VIEW POINT | | Total no's of bridges selected # 1 | | ADDING SDE WALK ADDING SDE WALK ADDING & WDE NIKS | ADDING & PAUSING ADDING & PAUSING Total no's of brogges selected = 1 | FAISING GPADE | ADDING SDE WALK ADDING SDE WALK ADDING SDE WALK ADDING SDE WALK ADDING SDE WALK |
| CONCEIVABLE REHABILITATION PLANS AVERAGE FROM STRUCTURAL VIEW POINT | | 2.7] PRF | 2.0 (AFPR.APPR.EMP 2.0 Pape.SFAFE 2.0 Capr.SFAFE.AP 2.0 Capr.SFAF 2.0 APPR.EMP 2.0 (APPR.EMP 2.0 (APPR.EMP 2.1 (APPR.EMP | 2.3 (358): CAPR 2.3 (APR.PPR 2.3 (APR.PPR 2.3 (APR 2.3 (APR 2.3 (APR.EJRP.659) 2.5 (APR.EJRP.659) 2.5 (APR.EJRP 2.5 (APR.ESPR 2.5 (APR.ESPR) 2.5 (APR.ESPR 2.5 (APR.ESPR) 2.5 | 2.0 IPPR.E.IPP BSPR 2.0 IAPR.PPR.FEIP 3.0 IAPR.PPR.FEIP 3.1 (2019: APR.APP.R.SFRS.E.ISP 3.1 (2019: APR.APP.R.SFRS.E.ISP | 2.3 00.545 2.3 10.646 2.5 10.646 3.0 1.847.62618 3.7 10847.0074 3.7 10847.0074 | 10 NON 1.8 BPR.AGF 1.8 BPR.AGFPRS.SFF ELRP 1.8 BPR.AGFPRS.SFF ELRP 2.0 CAWT MSPECT 2.1 APR.BPR 2.3 APR.BPR 2.3 APR.BPR 2.3 CGPR 2.3 CGPR 2.4 CGPR 2.5 CGPR 2.5 CGPR 2.5 CGPR 2.5 CGPR 2.5 CGPR 2.1 CGPR 2.1 CGPR 2.1 CGPR 2.2 CGPR 2.2 CGPR 2.3 CGPR 2.3 CGPR 2.3 CGPR 2.4 CGPR 2.3 CGPR 2.4 CGPR 2.5 CGPR |
| STRUCTURAL CONDITION BEAM SCOU- PIER DECK RING | | | 8) - 61 - 61 | <u>60 00 00 00 00 00 00 00 00 00 00 00 00 0</u> | 0 4 4 0 0 0 0 0 0 0 0 0 | <u>00004</u> | - <u>(()))))))))))))))))))))))))))))))))))</u> |
| NO. BRIDGE TYPE ABUT. OF LENGTH OF ABUT. SPAN (M) BRIDGE | | 1 4.95 PRB 4 | | 11.78 PR8 11.08 PR8 6.48 PR8 6.48 PR8 12.12 PR8 13.12 PR8 14.88 PR8 1.51 PR | 88888 | 6 8 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 | 1 3 4 7 5 3 |
| CATEGORY CAPACITY SPAN | ~~ | 3 P/A 4.95 | ┝┼┼┼┿╇╸ | ···································· | 0 0 0 0 27AL 27AL 27AL | 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | 0 0 0 0 0 1 0 0 1 0 |
| DISTRICT BUILT CAT | FRS Precast R.C. beam > | 0061 NISKL | ┝╍┿╼┽╍╄╌┼╼╴ | D KT. (1557 0.050 0.0 | 1 19601 1964 1965 1952 1952 1952 1952 1952 | 6 41.500 K.M.D.A.SiK 1500 K.M.D.A.SiK 1500 T.M.D.N.SiK 1500 K.S.E.U.NG.OR 1500 K.S.E.U.NG.OR 1500 | C 1934 ansr C 1934 ansr CALMTAN 1860 FANT 1860 FANT 1860 FANT 1800 FANT 1900 FANT 1800 FANT < |
| NO. KEY STATE | << TYPE OF BRIDGE | | ***** 1946 YEAR BUIL 1 00200850 PAHANG 1 00500850 FAHANG 2 0056430 FEINGGAIN 4 0057200 FEINGGAIN 4 00557200 FEINGGAIN 6 00557200 TRENGAIN | 7 0005-7270 TRENGGANU KT 8 0072680 0014140 KUMTAN 9 00260140 TRENGGANU KT 10 002630140 TRENGGANU BESUT 11 00563140 TRENGGANU BESUT 11 00563140 TRENGGANU BESUT 11 0056301 MELAKA JASIN 11 0056301 PERAK MINTA 12 00519305 PAHANG ROMEIN 13 00503050 PERAK JASIN 14 00519307 MENAKA JASIN 15 00519377 PAHANG PERAK 16 00519377 PAHANG PERAKA | 17 00552630 MELAKA 18 00314180 JOHOR 19 0036850 PAHANG 20 00368950 MELAKIAN 104 Ino's of bridges a 20 < The OF Shado | 1 0000400 10000400 1 0000400 10000400 2 0070200 1000400 3 00701200 1000400 4 00105200 10016000 5 00050000 17AMPIN 5 000500000 17AMPIN 6 00050500 15004000 7 000150200 10004000 | ••••••• 1945 •••••• ••••••• 1945 YEAR BUILT 1974 •••••• 2 000078500 REDAH RELINTAN 2 000708500 REDAH RELINTAN 3 0005000 REDAH RULINTAN 4 0005000 REDAH RULINTAN 5 0019400 REDAH RULINTAN 7 000512660 DHORR RULINTAN 7 000512661 DHORR RULINTAN 7 000512661 DHORR RULINTAN 10 000512661 DHORN RULINTAN 11 000512661 DELANGON RULINTAN 11 0005520 RELAN RULINTAN 11 0005520 RELANGON RULINTAN 12 0005520 RELAN RULINTAN 13 0005520 RELAN RULINTAN 14 0015030 RELANON RULINAN 14 0005520 RELA |

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| SELECTION | SELECTED | | SELECTED | | | | | | | | SA | | SELECTED | | SELECTED | | SELECTED CALON | SELECTED CB | serecien | SELECTED | SELECTED CA | SELECTED 9 | | | SELECTED 1 | | | | SELECTED | 8 | | SELECTED | SELECTED | SELECTED SPI FCTED | | |
|--|---|---|---|--|--|---|---|---|--|---|--|--|--|---|---|---|---|--|--|--|---|---|--|--|--|---|--------------------------|---|--------------|--|---------------|--|--------------------|--|-----------------------------------|---|
| CONCEIVABLE REHABILITATI PLANS FROM FUNCTIONAL VIEW PO | | | ADDING SDE WALK Total no's of bridges selected = | | | WIDENING & RAISING | | | | | RAISING GHADE | | | | | RAISING GRADE | ALUHVA SUC WALLA | ADDING & WDENING | | | | | | | WIDENING | | | | | | | | | | Total tro's of bridges selected = | |
| CONCEIVABLE REHABILITATION PLANS FEMAGE FROM STRUCTURAL VIEW POINT | 3.0 APF.PRF.CBRF 3.0 CBRF.DCRF.SPP R 3.0 CBRF.DCRF.SPP R | 3.5 DCRF.ARPR | 3.7 ARF, CBPR.DCRF | | | 2.7 DCRF | 3.U (Attr | | 1.0 NON | 2.0 BHP.ARF | 2.3 JAH, PAF 2.6 IDCRF, ARPA SFRF | 2.5 SRP,DCPR,APR | 25 DCPR,EJRP,SFRF,CBPR | 2.5 APR.PRF | 2.7 DCRF,APR | 2.7 (ARF | 3.0 DCPR | 3.0 DCRF | 3.0 DCPH,Arr-SHPP, BSPH 3.5 DCRF, AFPR, SFRF | 3.5 ARF,SHPR | 35 PPH 3.5 DCRF,APR,PPR,BSPR | 3.7 OCRF, APR, PPR, SFRF | | 2.0 SBPR | 2.0 DSPR | 2.0 SEPR,SRP,DSPR 2.0 SEPR.DSPR | 2.3 SEPR,DSPR,SRAP | 2.3 SBPR.SRPR | 2.7 SBPR.APR | 2.7 SEPR.CBRF | 2.7 SEPRIDSPR | 2.7 ISBPH,DSPH,APH 2.7 ISBPR,DSPH,ARF | 3.0 DSRP, SFRF | 3.0 I SEPRIDSPR 3.0 I SRUP DSPR SEEF SEPP | 3.3 (CBRF, SBPR | 2.0 SEPR.DSPR 2.0 SEPR.DCRF |
| STRUCTURAL CONDITIO BEAM DECK RIM | 0 4 4 6 11 0 1 | 4 4 3 2 4 4 | 4 | | | | 0 | | 6 | | 8 | | 2 3 | ~ | 4 (V | 2 | • | 6 4 | | _ | 4 | 4 | | 2 2 | 1 51 | 0 | 3 | 50 | 0 | 20 | 0 | 5) E1 | 3 | 0 | 2 | 2 2 2 2 |
| BRIDGE TYPE LENGTH OF (M) BRIDGE | 5.02 | 46.03 | 6.8 | | | 9.72 | o : xi | | 334 | 15.36 | 9.68 | L I | 85 SE | 7.33 | 13.71 | 7.60 | 1. | ŀ I | | 6.58 | 30.55 | 3.60 | | . 1 | 4.77 | 9.62 | | | | ŧ. | | | | | | 1 6.26 S6B 2 18.14 S6B |
| MAX. SPAN | 28 | | | | | 4.98 | 8.4 | | 334 | 15.36 | 4.84 6.27 | s 20 | ŀ | | | | 5.74 | 3.65 | 3.67 | 6.56 | 3.60 | 1,80 | | ŀ | + | ╇ | $\left\{ \cdot \right\}$ | + | + | | ╀┼ | ╉ | $\left\{ \right\}$ | + | H | 6.2% 9.07 |
| SORY CAPACIT | STAL STAL | STAL | STAL | | | | | | | | | | + | | | | | | • | | LS IS | 31 | olate >> | - | | | | | | _ | | + | $\left \right $ | | | SSAL SSAL |
| | | | | slab >> | | | | | | | | ľ | | | | 1950 | 096 1960 | 1980 | 0920 0920 | 1967 | 036 036 | 1960 | t beam, buckle t | 1045 | 1919 | 1930 | 0881 | | | }. | | | | | | 1965 2 1950 2 |
| DISTRICT | MELAKA TGH MANUNG | MUAR | MELAKA TGH | ~ Ø | ***** | MACHANG | | < 1974 withink | KUALA K9A | KOTA SETAR | P.PUTEH BATU PAHAT | KOTA SETAR | K TINGGI | H. PERAK | KUALA KPAI | SEGAMAT | K PILAH | MANUUNG | MEPSING | KUANTAN | MELAKA TGH K.SELANGOR | MERSING | - - | S ***** | BATUPAHAT | JERANTUT | Sidn | LIPIS | KOTA SETAR | SEREMEAN | JERANTUT | LIFRANTUT | BATUPAHAT | SEREMBAN IEPANTI IT | SEREMBAN | K PILAH |
| EY STATE | 1960 MELAKA 1330 PERAK | NEGO JOHOR | 1300 MELAKA to's of bridges = 29 | TPE OF BRIDGE | YEAR BUILT < 1945 | 8100 KELANTAN | to's of bridges = 2 | 1946 < YEAR BUILT | 4950 KELANTAN | 0750 KEDAH | 2000 KELANIAN 2620 JOHOR | 4900 KEDAH | 4060 JOHOR | 6900 PEPAK | 4850 KELANTAN | S970 JOHOR | 1360 NS | COBO PERAK | 67460 SELANGOH | 7240 PAHANG | 44.20 MELAKA | 3620 JOHOR | TYPE OF BRIDGE | YEAR BUILT < 194 6220 [DEPAK | 1070 JOHOR | 25260 PAHANG | 5290 FAHANG | 56510 PAHANG | 16210 KEDAH | 7010 NS | 13300 PAHANG | 2000 PAHANG | POHOL 0050 | X340 NS | 0280 NS | 1 00228540 PAHANG 2 00301960 NS |
| NO. | 25 00521 | 27 00514 | 29 0052 Total n | v v | | 1 00834 | Total n | | 1 00334 | 3 20700 | 5 0015 | 6 0018 | | 9 0055 | 11 20834 | 12 0230 | 14 0080 | 15 0180 | 17 00011 | 16 0033. | 19 0052 20 0054 | 21 0031. 1 0tal : | | MANT | 2 0500 | 0.840 | 5 0560 | 6 0680 | 8 0018 | 9 0080 10 0510 | 11 0640 | 12 0640 | 14 0500 | 15 0530 | 17 0520 | 1 0022 |
| | DISTRICT BUILT CATEGORY CAPACITY SAN OF LENGTH OF ABUT: BEAM SCOU- CONCEVABLE REHABILITATION CONCEVABLE REHABILITATION FINAL DISTRICT BUILT CATEGORY CAPACITY SAN OF LENGTH OF ABUT: BEAM SCOU- PLANS | DISTRICT PULT ONCEVABLE REHABILITATION CONCEIVABLE REHABILITATION CONCEIVABLE REHABILITATION FINAL FINAL DISTRICT BULLT CATEGORY CAPACITY SAN OF LEMIT HOF ABUTE PECKIN PLANS | DISTRICT YEAR STUDY MAX. NO. BRDGE TYPE STRUCTURAL CONDITION CONCEVABLE REHABILITATION CONCEVABLE REHABILITATION FINAL DISTRICT BULT CAFEGORY CAPACITY SAN OF LEWGTH OF ABUT BEAM SCOUT PLANS PLANS PLANS PLANS RELECTION ELAKA TGH 1980 3 STAL 7.13 SAN (M) SAN NO SELECTION SELECTION CONCEVABLE REHABILITATION CONCEVABLE REHABILITATION CONCEVABLE REHABILITATION PLANS RELECTION ELAKA TGH 1980 3 STAL 7.13 SAN (M) SAN NO SELECTION ANUNG 1980 3 SCO 3.3 DOPR.APPRICTINAL NEW POINT SELECTION ANUNG 1980 3 4 2 3.3 DOPR.APPRICTINAL NEW POINT SELECTION ANUNG 1980 3 4 2 3.3 DOPR.APPRICTINAL NEW POINT | NEME TUDY MAX. NO. 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BRDGE STRUCTURAL CONTION TRAC PLANS District 2 3 14.4 SCO PLANS PLANS PLANS District 3 31.4 7/13 2 4.0 5001 PLANS PLANS ELMING 3 31.4 7/13 2 4.0 5001 PLANS PLANS<!--</td--><td>NERTICT YEAR STUDY AMX NC BRDGE The R STRACTURAL CONDITION CONCENTIAL REHABILITATION FINAL PLANS PLANS</td><td>NEMA STUDY MAX MO BRDGE Tread STRACT/DAT STAL STAL MAX MO BRDGE TRACT/DAT STAL STAL MAX MO BRDGE TRACT/DAT STAL MAX MO BRDGE TRACT/DAT MAX MO BRDGE TRACT/DAT MAX MO BRDGE STAL STAL<</td><td>DSTRICT Text STUDY MA MA MA STUDY MA MA</td><td>NEMT YEAR STUDY WAX NO RePORT Terrar Terrar Terrar Terrar Terrar Terrar Description CONCENTION CONCENTION Terrar Terrar Terrar Description CONCENTION CONCENTION Terrar Terrar Terrar Description CONCENTION CONCENTION CONCENTION CONCENTION Second Terrar Second Second</td><td>OBTINICT NUMC NUMC</td><td>Bitting Tech Straturing Straturing</td><td>OBSTRICT VEM STUDY CANCOM STUDY <</td><td>Bistington Situation <</td><td>BERTICT NULL ONCENDER REPAIR/TYTON CONCENDER REPAIR/</td><td>BERRICT NEAR STUDY NEAR ONCENTIAL EFFERABLITATION CONCENTIAL EFFERABLITATION NEAR NEAR</td><td>BERNICT TEAM STUDY <t< td=""><td>NEUTICINAL YEAR CONCENTRAL REPUBLIC/TIONL CONCENTRAL REPUBLIC/TIONL CONCENTRAL REPUBLIC/TIONL NEUTICINAL NEUTICINAL</td><td>NEURICI (MA) YEAR STALE CONTINAL (MA) ONCE UNAL (MA) STALE CONTINAL (MA) ONCE UNAL (MA) STALE CONTINAL (MA) STALE CONTINAL (MA)<</td><td>BERNICT Werk STRUCT/MALL CONCERVERTE FERMER/TITION CONCERVERTE</td><td>NEWL Stand Description Stand Description Stand Stand</td><td>DEFIC: TALE STALE Description Concerned Life Revealer/Tricton Description <thdescription< th=""> <thdescription< th=""></thdescription<></thdescription<></td><td></td><td>DETRICT Tab. 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APPENDIX-F SELECTION OF 100 BRIDGES FOR VISUAL INSPECTION

| Bill Gr. Network Rev Deck Network Rev Rev Deck Network Rev Deck Network Rev Network Network <th>SELECTION REMARKS</th> <th></th> <th>SELECIED</th> <th></th> <th></th> <th>SELECTED</th> <th></th> <th></th> <th></th> <th>SELECTED</th> <th></th> <th></th> <th></th> <th></th> <th>SELECTED</th> <th></th> <th></th> <th></th> <th>SELECTED SA</th> <th>SERTED</th> <th></th> <th></th> <th>Control in the second sec</th> <th></th> <th></th> <th>SELECTED SA</th> <th></th> <th></th> <th>SELECTED SA</th> <th>SELECTED</th> <th>SELECTED </th> <th>SELECTED RA</th> <th></th> <th>SELECTED</th> <th>SELECTED</th> <th>SELECTED</th> <th></th> <th>SELECTED</th> <th></th> <th></th> <th></th> <th></th> <th>5</th> | SELECTION REMARKS | | | | | | | | | | | | | | | | | | | | | SELECIED | | | SELECTED | | | | SELECTED | | | | | SELECTED | | | | SELECTED SA | SERTED | | | Control in the second sec | | | SELECTED SA | | | SELECTED SA | SELECTED | SELECTED | SELECTED RA | | SELECTED | SELECTED | SELECTED | | SELECTED | | | | | 5 |
|---|----------------------------|----------|---------------|-----------|---------------|---------------|-----------|-----------------|------------|-------------|------------|--------------------|---------------|------------|------------|---------|-----|----------|-------------|---|----------|--------------|------------|------------|---------------|------------|------------|------------|--------------------|------------|---------------|------------------------|------------|---------------|-----------------|---------------|---------------|------------------------|----------------|-----------|-----|--|----------------|---------------------|-------------|-----------------|------------------|-------------------|--------------------|---------------------|-------------|---------------------|--------------------|---------------------|---------------|-----------------------------|-------------------------------|---|------|----------------------|-------------|---|
| Mark Mark <th< th=""><th>VIEW POINT</th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th>~</th><th>ADDING SDE WALK</th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th>no's of bridges selected m</th><th></th><th></th><th></th><th>-</th></th<> | VIEW POINT | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | ~ | ADDING SDE WALK | | | | | | | | | | | | | | | | | | | | | | | no's of bridges selected m | | | | - |
| 1 | FROM STRUCTURAL VIEW POINT | 2.0 6898 | 2.0 SBPR | 2.0 8624 | 2.0 SEPR.DSPR | 2.0 SBPR.DCRF | 2.0 CRAP | 2.0 NON | 2.0 SBPR | 2.3 SBPR | 2.3 SBPA | 2.3 SEPEIDSPR SEEP | 0.0 COD 5 COS | 22 000 | | 20 00ra | | | 20100 HUOLA | | | 2/ SUPPLOSPE | 2.7 (SGPR | 2.7 (SGPR | 2.7 SSPR.DSPR | 2.7 DSPR | 2.7 SBPR | 7 | 2.7 SBPR APP. ATTH | 2.7 SEPR | 2.7 DSPR.SBHP | 2.7 SEPR.DSPR.ARF.AFPR | | | | 2.8 SBPR.DSPR | 3.0 SEPR.DSPR | 3.0 SEPP.AW, APP. SPPP | 3.0 (SEPR.SEPR | | | | SEVELOCITA APH | 6.0 (05-14.0014,244 | | A CALCONARY ARE | 3.0 SEPRAPR SFRS | 3.0 SEPR.DSPR.ARF | 3.0 SBPR.DSPR | 3.3 SEPRIDSHP, SFHS | | 3.3 (SBRP DSPR AFPR | 3.3 SEPR.DSPR.AFPR | 3.5 APR, SEPR, DSPR | 3.5 SEPR.DSPR | 3.7 SBPP,DSPR,DCPR,APR,AFRF | 4.0 SEPP.LISPR,APPR,PFPR,SFPS | | | | 2.7 SEPRARF | |
| 1 1 0 <td>BEAM DECK RING</td> <td></td> <td></td> <td></td> <td>Ŀ</td> <td>2</td> <td></td> <td>5</td> <td></td> <td>5</td> <td>0</td> <td></td> <td>3</td> <td></td> <td></td> <td>3 3</td> <td>3 3</td> <td>3 2</td> <td>3 3</td> <td>3 2</td> <td>0 0</td> <td>0 0</td> <td>0 0</td> <td>3 3</td> <td>4</td> <td>4</td> <td></td> <td></td> <td></td> <td>4</td> <td>0</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>L</td> <td>4</td> <td><u></u></td> <td>ŀ</td> <td></td> <td></td> <td></td> <td>*</td> <td>4</td> <td>*</td> <td></td> <td> </td> <td></td> <td>4</td> <td></td> | BEAM DECK RING | | | | Ŀ | 2 | | | | | | | | | | | 5 | | 5 | 0 | | 3 | | | 3 3 | 3 3 | 3 2 | 3 3 | 3 2 | 0 0 | 0 0 | 0 0 | 3 3 | 4 | 4 | | | | 4 | 0 | | | | | | | | L | 4 | <u></u> | ŀ | | | | * | 4 | * | | | | 4 | |
| 1980 2 55AL 0.11 1 970 1980 2 55AL 0.11 1 1 1980 2 55AL 0.11 1 1 1980 2 55AL 0.11 1 1 1980 3 55AL 0.21 1 1 1980 3 55AL 0.21 1 1 1 1980 3 55AL 0.21 1 </td <td>LENGTH OF ABUT.</td> <td>SBG</td> <td>SBE</td> <td>3.26</td> <td></td> <td>16.08</td> <td>4.54</td> <td>3.75 (\$88 (2</td> <td>3.70 SBB 2</td> <td>3.11; SBB 2</td> <td></td> <td></td> <td>3</td> <td>5 8</td> <td>1</td> <td>000</td> <td>200</td> <td>000 1000</td> <td></td> <td>0.000</td> <td>8.12 200</td> <td></td> <td></td> <td>3,001 505</td> <td>5,061 SBB</td> <td></td> <td>8</td> <td></td> <td></td> <td>9.62 538 2</td> <td>3.68 553 2</td> <td>3.00 SEB 2</td> <td>8.51</td> <td>0 31.30 SBB 2</td> <td>36,18 S</td> <td>2.23 338 2</td> <td>3.06 \$88 3</td> <td>6.29 SBB 3</td> <td>3.47 SB8</td> <td>10.94 SBB</td> <td></td> <td>_</td> <td></td> <td>1</td> <td></td> <td>BB BB</td> <td>ļ</td> <td> </td> <td>Steb Seb</td> <td>-</td> <td></td> <td>].</td> <td>$\left \right$</td> <td>24 SBB</td> <td>SEB</td> <td>6.90 SB5 i</td> <td>18.08 SBE</td> <td></td> <td> </td> <td></td> <td>Se SEC</td> <td></td> | LENGTH OF ABUT. | SBG | SBE | 3.26 | | 16.08 | 4.54 | 3.75 (\$88 (2 | 3.70 SBB 2 | 3.11; SBB 2 | | | 3 | 5 8 | 1 | 000 | 200 | 000 1000 | | 0.000 | 8.12 200 | | | 3,001 505 | 5,061 SBB | | 8 | | | 9.62 538 2 | 3.68 553 2 | 3.00 SEB 2 | 8.51 | 0 31.30 SBB 2 | 36,18 S | 2.23 338 2 | 3.06 \$88 3 | 6.29 SBB 3 | 3.47 SB8 | 10.94 SBB | | _ | | 1 | | BB BB | ļ | | Steb Seb | - | |]. | $\left \right $ | 24 SBB | SEB | 6.90 SB5 i | 18.08 SBE | | | | Se SEC | |
| Main Main <th< td=""><td>3</td><td>- </td><td>-</td><td>3.26</td><td>-</td><td>9,62</td><td>4.64</td><td></td><td></td><td>-</td><td>╞</td><td>+</td><td>╀</td><td>╀</td><td>$^{+}$</td><td>21</td><td></td><td></td><td>10.11</td><td>240</td><td>8</td><td>+</td><td>╉</td><td>┥</td><td>+</td><td>-</td><td>-</td><td>-</td><td>ŀ</td><td>┢</td><td>┢</td><td>ŀ</td><td>9.51</td><td>11.50</td><td>\$,00</td><td></td><td>-</td><td>-</td><td>3.47</td><td>5 47</td><td>╉</td><td>+</td><td>╉</td><td>╉</td><td>+</td><td>+-</td><td>╀</td><td></td><td></td><td>╉</td><td>+</td><td>╈</td><td>╀</td><td>+</td><td>-</td><td>Η</td><td>- </td><td></td><td></td><td></td><td>-</td><td></td></th<> | 3 | - | - | 3.26 | - | 9,62 | 4.64 | | | - | ╞ | + | ╀ | ╀ | $^{+}$ | 21 | | | 10.11 | 240 | 8 | + | ╉ | ┥ | + | - | - | - | ŀ | ┢ | ┢ | ŀ | 9.51 | 11.50 | \$,00 | | - | - | 3.47 | 5 47 | ╉ | + | ╉ | ╉ | + | +- | ╀ | | | ╉ | + | ╈ | ╀ | + | - | Η | - | | | | - | |
| | | | 180 | | 1960 | | _ | _ | - | | - | 1950 | 19501 | 1050 | VEN I | 200 | | 8 | 240 | 200 | 200 | 8 | 8 | 8 | 86 | 1860 | 1960 | 1980 | 035 | 1950 | 1950 | 1950 | 1950 | 1948 | 1955 | 981 1380 | 98 | 88 | 8 | 13951 | 200 | ╉ | + | ╉ | 10501 | 0501 | 1980 | 1950 | | | 1 | 1. | 11 | 1950 | 1950 | 1950 | 1950 | a data | | | : | |
| 3 | | 000000 | 4 00902430 NS | 5 0510145 | 6 0510228 | 7 051030 | 8 0860119 | 9 05601 830 | 10 0660216 | 11 0050227 | 12 0090244 | 13 0090433 | 141 00005190 | 15 0510008 | ACTOR OF A | | | | | 1 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 | | 220100 | 22 0000142 | N LOSON BY | | 26 0510205 | 27 0510267 | 28 0530047 | 29 0530216 | 30 0360100 | 31 0360141 | 32 0360260 | 33 0960464 | 34 0015610 | 35 0016120 | 36: 0056363 | 37 0052960 | | | | | | A NONCES | AL DEBUTO | 46 159734 | 47 0700023 | 48 0760233 | 49 0760402 | 50 07604 750 PERAK | 102020 10 | 200000 | 54 0780248 | 55 0760639 | 56 0054100 | 57 0054121 | 56 0081012 | 59 0080000 PAHANG | Total no S | | ***** YEAR BUILT < 1 | 1 201282 | |

 $\mathbf{F} = \mathbf{4}$

APPENDIX--F SELECTION OF 100 BRIDGES FOR VISUAL INSPECTION

| K FINAL SELECTION REMARKS | | | SELECTED | SELECTED CA | _ | | | | | - T | SETEVED CAN | | | SELECTED CA | 1 | SELECTED | | - | | | SELECTED SA | Sci Portes CA | | | SELECTED | | CA | | | | SELECTED 1 | | | | | | | | |
|---|-------------------------|-------------------|---------------------|-------------------|---------------------------|----------------------------|--------------|---------------|----------------|------------------------|-------------------|-----------------|---------------|----------------------|--------------------|-------------------|------------------------------------|----------------------------------|------------------|--------------|--------------------|-----------------------|-------------------------------------|--|------------------------|-------------------|-------------------|-------------------------------------|--------------------|--------------|---------------------|--|-----------------------|---------------------------------------|--------------------|------------|------------------|------------|---------------------------------------|
| CONCEIVABLE REMABILITATION CONCEIVABLE REMABILITATION PLANS FROM STRUCTUARL VIEW POINT FROM FUNCTIONAL VIEW POINT | | | | | | | | | | | | | | | | | Total no's of bridges selected = 6 | | | | | | Total note of believes selected = 0 | | ADDING SDE WALK | | | Total no's of bridges selected == 2 | | | | Total no's of bridges selected = 1 Grand Total S5 Bridges | | | | | | | Total & Bridney calamed by COM |
| AVERAGE | | | | 2.3 | 2.3 DCRF, SBPR, SFRS, PRF | 2.7 SBPR, DCRF, AFPR, SFRS | 2.7 SBPR | 2.7 SBPP,CBRF | 2.7 SEPR,EJPPO | 2.5 SEPR.DCRF,APPR,PRF | 3.0 UCHT SBFH AFH | A.O.I SAPE NCRE | 3.0 SEPRINCE | 3.3 SEPR.EPR.SFRF | 3.3 DCRF,SBPR,EJRP | 3.5 DCRF,SBPR | | | | 3.0 DCRF | 3.7 CBRF,DCPR,EJRP | 3.7 CBRFDCRF | 0./ 0011.0011.0011.011.011 | | 3.0 APR.EJRP,SFRF,CBPR | 0.0 CONFUCKF, ANT | 3.3 DCRF, CBRF | | | | 2.7 SEPR, DCPR, APR | | | | | | | | |
| JT. BEAM CONNITION | | | 2 2 2 2 | 4 2 1 | 2 3 | 2 | 2 3 3 | 4 | 3 3 2 | 2 3 | * * * | 5 | - 4 | 3 | | 3 4 | | | | 3 | 4 | 3 4 4 | * | | 5 | | | | | | 3 3 3 | | | · · · · · · · · · · · · · · · · · · · | | | | | · · · · · · · · · · · · · · · · · · · |
| LENGTH OF ABUT. | | • | 54.50 | 26.70 | Ι. | | | 1 | 6.80 | | 1 4./51 SBC | | 1 | ļ | L | | | | | L | 4,84 | 1 7.47 SBE | | | 4.40 | | 1 9.33 SBE | 11 | | | 1 10.72 SBG | | | 271.81 | 19 515.21 500 | 1710 | 5 196.18 PCB | I | |
| SPAN OF (M) SPAN | | - | 18.24 | 8.90 | | 4.40 | 763 | 8.21 | 6.80 | | 4 50 | 000 | 3.56 | | | 10.88 | | | | 1.85 | | | 141.0 | | 4.40 | | 9.33 | | | | 10.72 | | | | 151 50 | | 52.02 | 56.20 | |
| CATEGORY CAPACITY | | | STAL | STAL | STAL | STAL | STAL | STAL | STAL | 81AL | STAL | STAL | STAL | STAL | STAL | STAL | | v < data | | MTAL | A/A | P/A | | | STAL | SIAL | STAL | | • | | STAL | | | STAI | MTAI | | STAL | MTAL | |
| | | : | 1964 3 | | | | 1950 3 | | 380 | | 0.001 10501 | | ŀ. | | | | | Steel beam, R.C. | | | | 12001 3 | | | | 0.00 | 1950 3 | | girder >> | | 1905 3 | | | 1954 | | etra | Ł | 1976 2 | |
| DISTRICT BUILT | | ***** \$28 | | KUANTAN 19 | | | | 1 | BTG PADANG 19 | 1 | | 1 | BTG PADANG 19 | | Ŀ | | | Encased Steel beam, R.C. slab >> | | | | | | | | - | MELAKA TGH 15 | | i Steel box girder | | ATANG | | | · | TFRMFI OH 1 | + | BATUP AHAT 1 | - | - |
| | vidges = 3 | YEAR BUILT < 1974 | | U | • | • | 1 | | 1 | | | | | ١ <u></u> | | | vidges = 15 | SBE | ULT < 1945 ***** | ELANGOR ULL | OHOR K. | 3 00522760 MELAKA MPM | ridnes = 4 | | | | | | F BRIDGE SBG | UILT < 1945 | ERAK LA | Total no's of bridges = 1 Grand Total 218 Briddes | << SPECIAL Bridges >> | | 1 | | 1 | I 1 | t. |
| NO. KEY | Total no's of bridges = | 1945 < YEAR BUILT | 1 05204870 SELANGOR | 2 00237200 PAHANG | 3 0000070 PERAK | 4 05901000 PERAK | 5 05001580 P | 6 06902230 F | 1 0550550 1 | 2 02400400 2 | 10 05001070 PERAK | 11 05001690 P | 12 06602000 P | 13 00549550 SELANGOR | 14 05902920 PERAK | 15 05000120 PERAK | Total no's of bridges = 15 | << TYPE OF BRIDGE | BAAR VEAR | 1 00145100 5 | 2 00303220 J | 3 00622760 1 | Total ho's of bridges # 4 | | 11 00313150 JOHOH | 3 DR702060 KETAH | 4 00523000 MELAKA | Total no's of k | << TYPE OF BRIDGE | B HASY ***** | 1 00186510 F | Total no's of t Grand Total | << SPECI | 1 00178210 [P. PINANG | 21 DOPPED 1 PAHANG | 3 00371000 | 4 00512340 JOHOR | 5 01212140 | |

F – 5

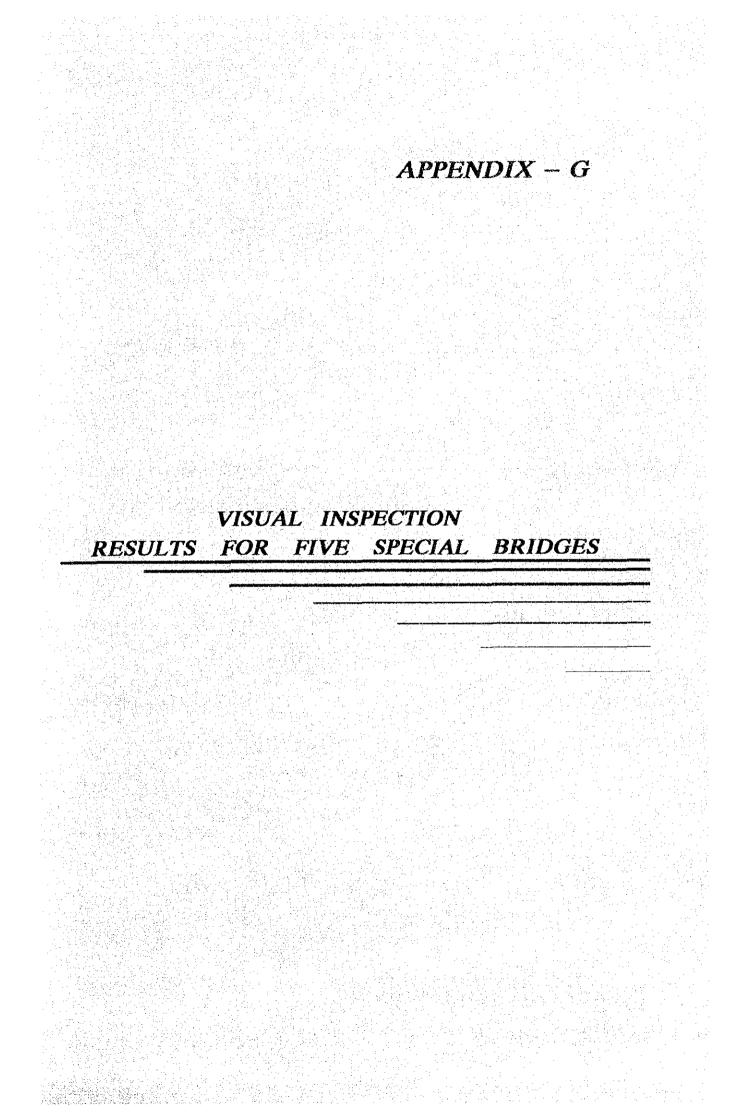


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| В. | MERDEKA BRIDGE G- 4 |
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| с. | BATU PAHAT BRIDGE G- 7 |
| | |
| | |
| D. | TEMERLOH BRIDGE G-10 |
| | TEMERION BRIDGE |
| | |
| | |
| E. | KUALA LEPAR BRIDGE G-12 |
| | |
| | |
| | |

APPENDIX-G VISUAL INSPECTION RESULTS FOR 5 SPECIAL BRIDGES

A. SULTAN YAHYA PETRA BRIDGE

1. Bridge Data

| Кеу | * | 00371000 |
|------------------------|--------------|--|
| Name of River | * - | Sg. Kelantan |
| State | : | Kelantan |
| District | : | Kota Bharu |
| Year Built | - : | 1962 |
| No. of Span | . : | 29 spans |
| Bridge Length | : | 840m |
| Type of Superstructure | . . . | RC beam and slab built monoli- thically to the piers |
| Type of Substructure | • | Pile bankseat (abutment) and rectangular RC columns (piers) |

2. General

The bridge links the town of Kota Bharu and Pasir Mas. It was built by the State Government without any consultation with JKR Engineers, as a result JKR has no drawings records with regard to its construction. The bridge was designed by Raymond Wong and Associate and constructed by Kien Huat Construction Company. After construction of the bridge was completed, JKR was directed to maintain it. It has been reported that defects on the bridge starts showing up as early as 1967.

3. Observed Defects

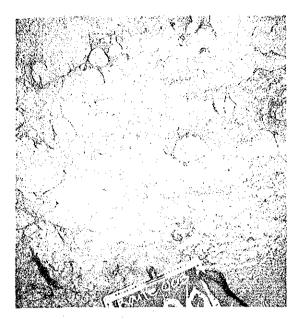
Visual inspection was made by the Study Team in October 1990 and it was observed that all soffit of slab has been repaired by gunite, thus all defects have been covered up. However, the gunite surfaces have cracked at a few location (See Photo A-1), which indicates that repair carried out is not effective. It was reported by JKR Engineers in Kota Bharu that the soffit of deck slab was repaired in 1988 because almost all soffits of deck slab have cracked with concrete spalling at quite an extensive area.

All RC beams have been in distress with vertical crack appearing at regular intervals. The cracks start from soffit of deck slab and propagate vertically down at side of beam to about 200mm from its soffit (See Photo A-2). Some of the RC beams have also cracked horizontally at its side which occurred at about 200mm from soffit of slab.

It has also been reported that most of the expansion joint have failed as early as 1967. The expansion joint has been reported to have cracked and the gap at the half joint has widened with its steel cover plate missing. Expansion joint was subsequently repaired in 1980. During site inspection made by the Study Team, it was observed that the expansion joint could have failed again as crack was observed on premix surfaces (See Photo A-3), especially at the abutment where excessive noise was detected whenever heavy vehicles passed through it.

4. Recommended Rehabilitation and Maintenance Work

It is recommended that further detailed investigation and analysis should be conducted for this bridge which will be carried out in Phase II(A) of the Study.



| | Photo | A٠ |
|-----|-------|----|
| A-1 | | |
| | | |

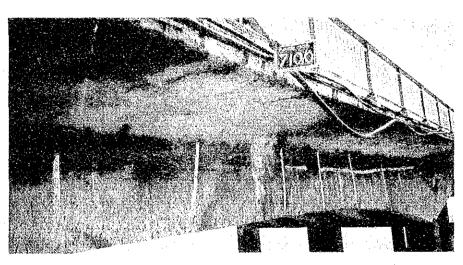
 1 :Crack at gunited surfaces of the soffit of deck slab (The crack does not show up very well in this photo)

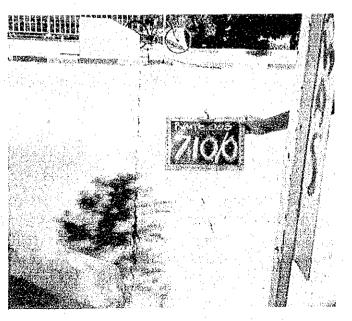
| İ | A-2 | |
|---|-----|--|
| | | |

A-3

Photo A-2 :Vertical and horizontal crack at side of all RC beams (shown here by the white marking)

Photo A-3 :Crack and wide gap formed on premix surfaces due to failure of expansion joint





B. MERDEKA BRIDGE

1. Bridge Data

| Кеу | • | 00178210 |
|------------------------|---|-----------------------|
| - | • | |
| Name of River | 1 | Sg. Muda |
| State | : | Pulau Pir |
| District | ; | Seberang |
| Year Built | : | 1954 |
| No. of Span | : | 13 |
| Bridge Length | : | 271.61 m |
| Type of Superstructure | : | RC beam a approach |

Type of Substructure

Sg. Muda Pulau Pinang Seberang Prai 1954 13 271.61 m RC beam and concrete slab at approach spans and 3 centre spans are of RC bow string arch type of construction

RC wall piers and abutment at approach spans and Masonry wall pier at 3 centre spans

2. General

The bridge is located at the border between the State of Penang and Kedah. The approach span on Penang side consisted of 6 span RC beam and slab bridge while there are only 4 span on Kedah side of the approach. The main span consisted of 3 spans RC bow string arch superstructure with maximum centre span length of 57.32m. Piers and abutments at both approaches are founded on 20m long piles while piers supporting the RC arch is founded on 16m long caisson.

:

Very limited information is available with regards to its design or construction except for the drawing which was collected by NALS.

3. Observed Defects

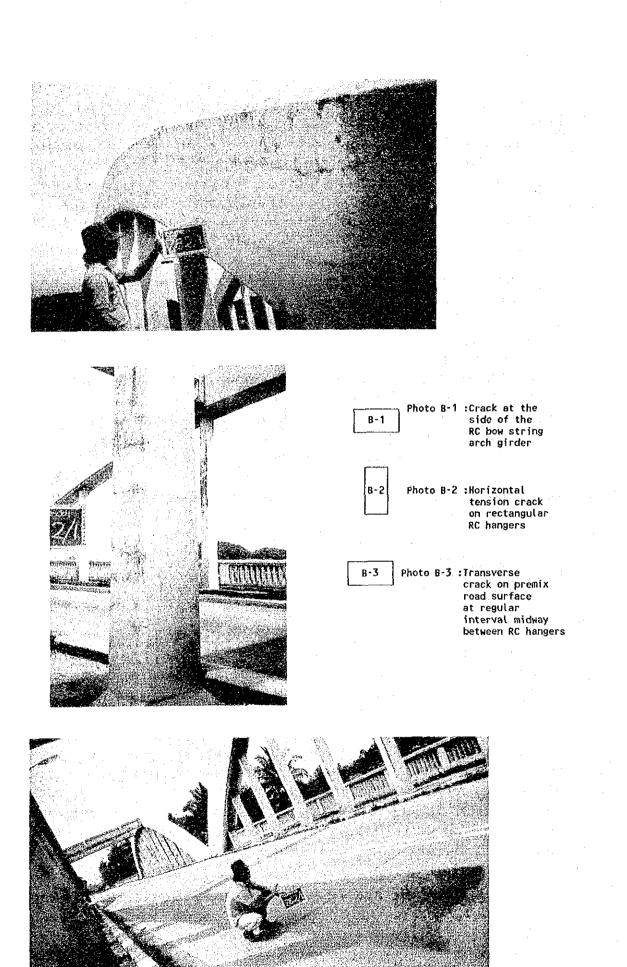
All RC bow arch girder has cracked at its side along the arch line (See Photo B-1), but no rust staining free lime has been observed, thus indicating that the crack could not possibly caused by corrosive expansion of steel. In the opinion of the Study Team the cause of the problem could be due to the fact that the concrete arch is subjected to compressive force, in which the concrete is known to be strong, but at the time the concrete in the arch is also subjected to tensile busting force acting perpendicular to the compressive forces. If inadequate stirrup is provided the concrete will not be able to hold this force especially during the early age of the conrete and thus resulting in cracking of the member.

All rectangular RC hangers has cracked due to the concrete member being subjected to tensile forces (See Photo B-2). Premix surfaces on the carriageway has cracked transversely at regular interval on mid point between the hangers (See Photo B-e). The crack on premix surfaces could have been caused by the crack which appears at the construction joint in the slab. The construction joint in the slab was constructed at midspan between the transverse girders which is supported by the hangers.

4. Recommended Rehabilitation and Maintenance Work

Transverse crack on deck slab could easily be repaired by injecting polymer modified cementitious mortar and painting of the defective members with water proof coating.

Cracks at RC arch rib and hangers are very small with no free lime and rust staining on its surfaces, thus the crack could have occurred at the early age after completion of the bridge. The immediate step is to monitor the crack width whether the crack is active or not. If the crack is inactive then repair is by painting the concrete surface to protect rusting of reinforcement bar is required. If the crack width widen at a faster rate, then repair by injection of polymer modified cementitious mortar will be required. In the opinion of the Study Team, the observed defect on the bridge is not critical, thus no further detailed study with regard to maintenance and rehabilitation work is required for this bridge.



G – 6

C BATU PAHAT BRIDGE

1. Bridge Data

| Key | : | 00512940 |
|------------------------|----------|-----------------------------|
| Name of River | : | Sg. Batu Pahat |
| State | : | Johor |
| District | • | Batu Pahat |
| Year Built | : | 1965 |
| No. of Span | . • : | 5 |
| Bridge Length | • | 196.18m |
| Type of Superstructure | : | Precast prestressed I-Beam |
| Type of Substructure | : | Steel tubular column (pile) |
| | | and concrete cross head |

2. General

The bridge is located not very far from the estuary of Batu Pahat river and thus it is within the tidal range. It replaces the ferry service which link the town of Batu Pahat and Muar. The end span consisted of 31.30m simply supported beams while the penultimate spans consisted of 31.3m simply supported beam supported on pier on one end and on half joint of a 10.3m cantilever span on the other,. The centre span is 52m long consisted of 31.4m simply supported span and 10.3m cantilever spans at each pier. Both piers at end span and abutments are founded on rectangular RC piles while pier at the centre span is supported on 1.2m diameter tubular steel piles.

3. Observed Defects

Expansion joint is not provided at both abutments and piers. The premix material has dropped from the road surface through the gap formed (See Photo C-1) and collected at the bearing shelf. Plant (jejawi tree) is growing at the side and soffit of deck especially at half joint.

G - 7

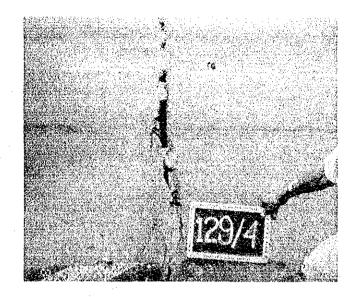
Excessive settlement of the approach embankment has cause pothole with depth greater than 30 cm to be formed (See Photo C-2). Road surface at the approach is very bumpy with excessive rutting of the pavement.

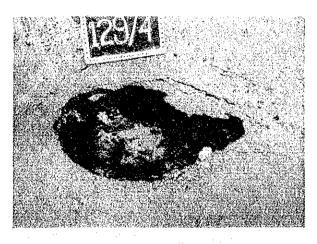
All tubular steel pile at the pier on the centre span has corroded at the splash zone (See Photo C-3). Some of the piles has laminated with rusted steel thickness varies from 5mm to 10mm.

4. Recommended Rehabilitation & Maintenance Work

Bumpy road surface together with non-existence or failure of expansion joint will lead to an excessive impact load on the bridge, thus urgent repair is required. New expansion joint should be installed, debris and plant growing at bearing shelf should be removed. Approach embankment should be repaired, settlement could be reduced by installation of embankment piles at both approaches. Rip rap protection should be provided at the front of abutment to prevent embankment material from being washed out.

Concrete jacket should be constructed to prevent tubular steel cylindrical pile from corroding further. Before concrete jacket is installed all rust should be removed and the steel pile should be blast cleaned.



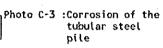


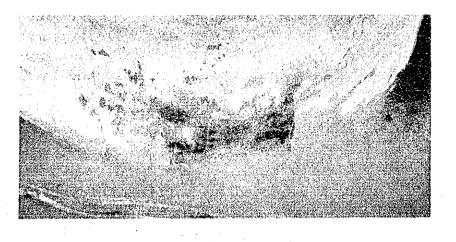
| C-1 | Ph |
|-----|-----|
| C-2 | Pho |

C-3

noto C-1 ;Expansion joint missing at abutment

noto C-2 :Pot hole formed at approach embankment





D. TEMERLOH BRIDGE

1. Bridge Data

| | | I I |
|------------------------|-----|---|
| Кеу | • | 00223500 |
| Name of River | • : | Sg. Pahang |
| State | | Pahang |
| District | • | Temerloh |
| Year Built | : | 1974 |
| No. of Span | : | 17 span |
| Bridge Length | | 515.21m |
| Type of Superstructure | | Steel box girder on the main span and Inverted T on the approach spans. |
| Type of Substructure | : | RC wall abutment and V-shaped Rectangular span and RC wall pier at main span. |

2. General

The bridge was built at much higher elevation than the old bridge which was severely damaged by flood. It is located on Route 2 which formed a major road link between Kuala Lumpur and Kuantan town. The Kuala Lumpur approach is made of 8 spans inverted T-beam bridge while the Kuantan approach is made up of 7 spans Inverted T-Beam bridge. The centre main span is made of 2 spans continuous steel box girder bridge. All abutments and piers are supported on pile foundation. This bridge is relatively new thus quite a number of drawings is available and collected by the NALS.

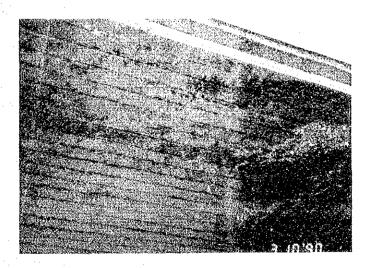
3. Observed Defects

Free lime was detected at soffit of inverted T-Beam on a few of the approach spans (See photo D-1). The defect could be caused by porosity of the bridge deck. Expansion joint on the bridge deck directly above the pier supporting the box girder at Kuala Lumpur side has been in distress. Its epoxy nosing has failed and anchor has loosened (See photo D-2).

4. Recommended Rehabilitation Maintenance Work

Porosity of bridge deck on approach span could be repaired by providing water proof membrane on the RC deck. However, since the porosity is only at a localised areas and to minimise cost of repair, the defect should be repaired by injecting the defected areas of RC slab with polymer modified cementitious grout.

All loose anchor bolts at the defective expansion joint should be tightened and its epoxy nosing repaired by polymer modified cementitious mortar.

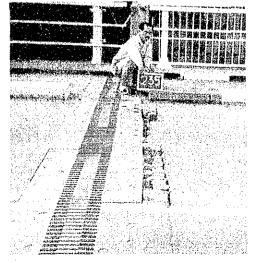




D-2

Photo D-1:Free lime at soffit of Inverted T-beam bridge on the approach span

Photo D-2:Damaged nosing at the expansion joint



G - 11

E. KUALA LEPAR BRIDGE

1. Bridge Data

| Key | : | 01212140 |
|------------------------|-----|---|
| Name of River | : | Sg. Pahang |
| State | : | Pahang |
| District | : | Pekan |
| Year Built | | 1976 |
| No. of Span | . : | 7 spans |
| Bridge Length | : | 402.3m |
| Type of Superstructure | : | Precast Prestressed segmental continuous box girder |
| Type of Substructure | : | RC hollow wall/box abutment and pier |

2. General

The bridge is located on the road linking the town of Kuantan on the East Coast to Segamat town on the South Western side of Peninsula Malaysia and it crosses the longest river in Peninsula Malaysia. The bridge is founded on pile foundation.

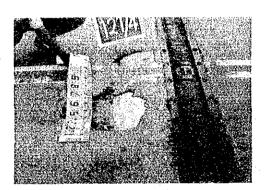
3. Observed Defects

The bridge is relatively new, thus no structural defect was observed except for potholes formed on approach road surface adjacent to expansion joint at both abutments (See Photo E-1).

G = 12

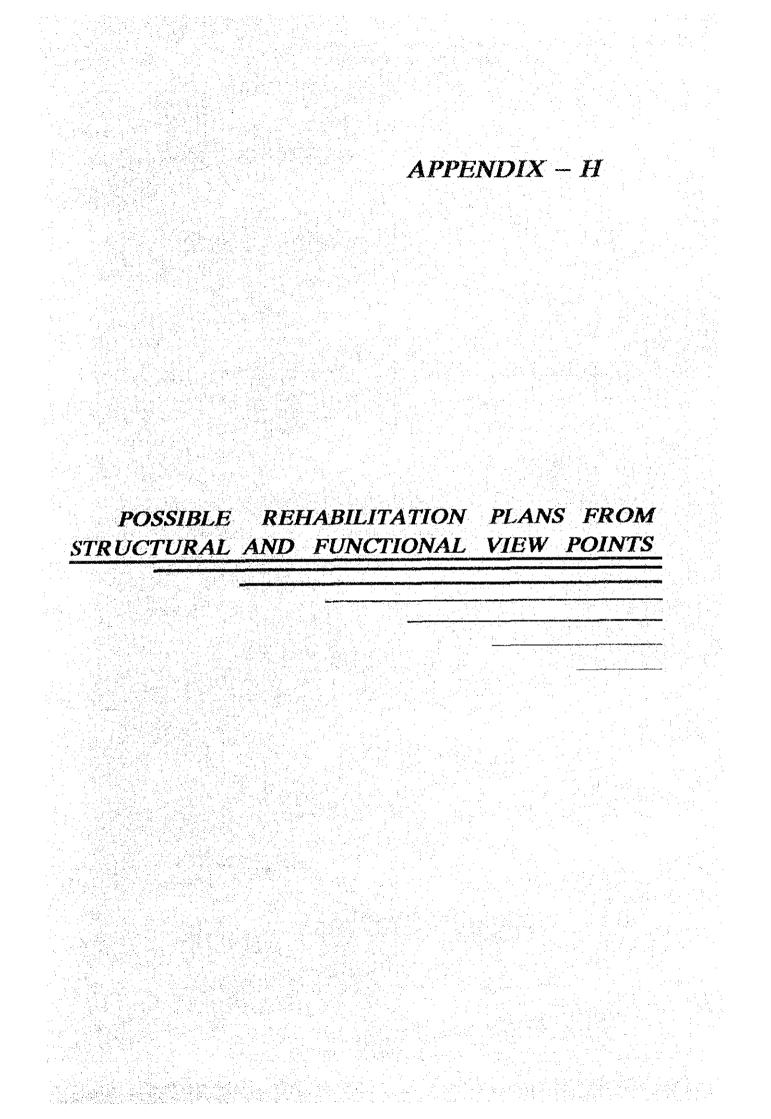
4. Recommended Rehabilitation and Maintenance Work

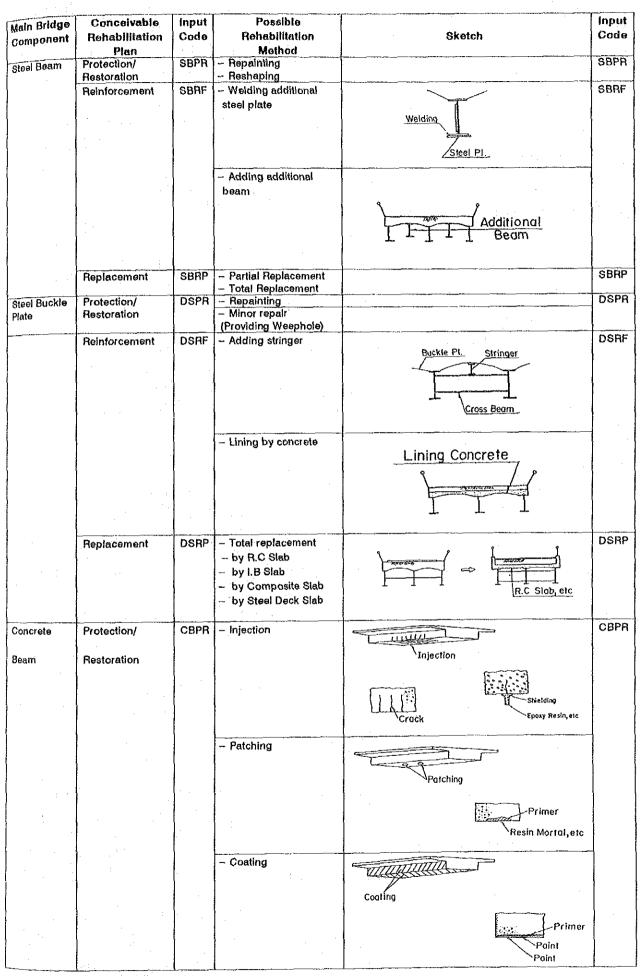
Since NALS report has highlighted this same problem (i.e. potholes) at this bridge, the Study Team concludes that the defect is caused by failure of the road pavement. Therefore, road pavement adjacent to the bridge has to be properly design and reconstructed.



E-1 Ph

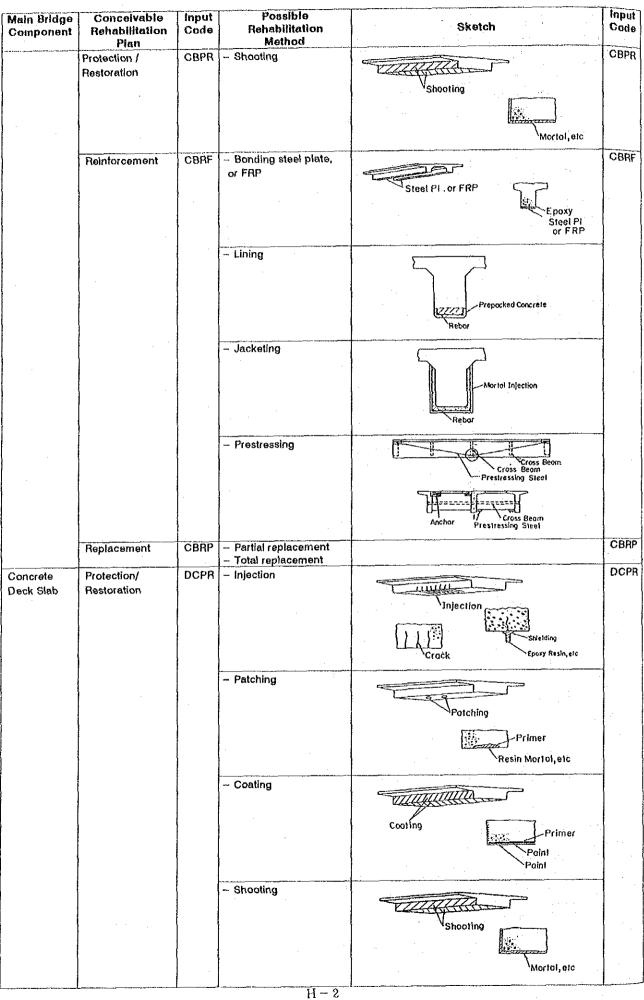
Photo E-1 : Pot holes formed on approach road surface adjacent to expansion joint at the abutment



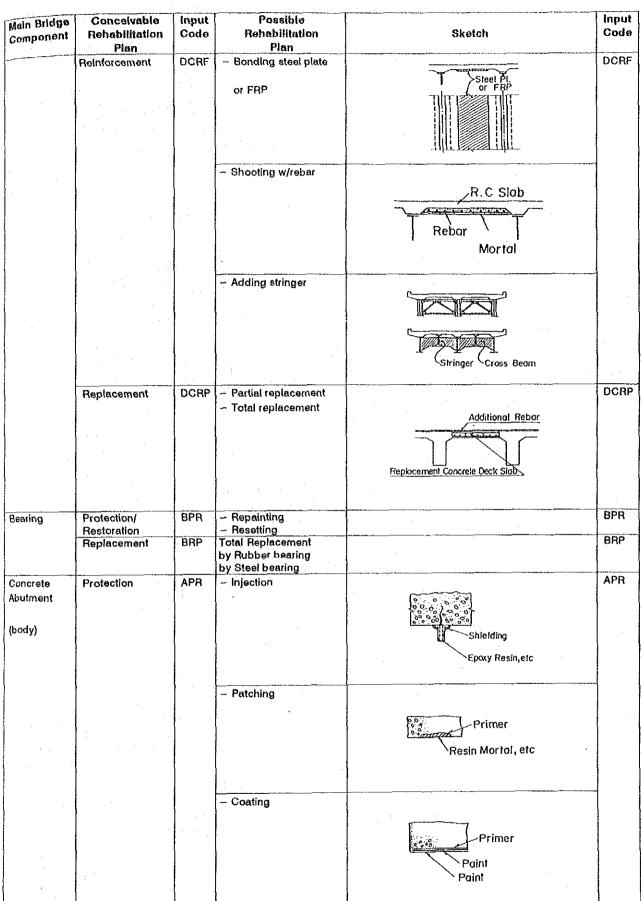


APPENDIX--H POSSIBLE REHABILITATION PLANS FROM STRUCTURAL VIEW POINT

H -- 1

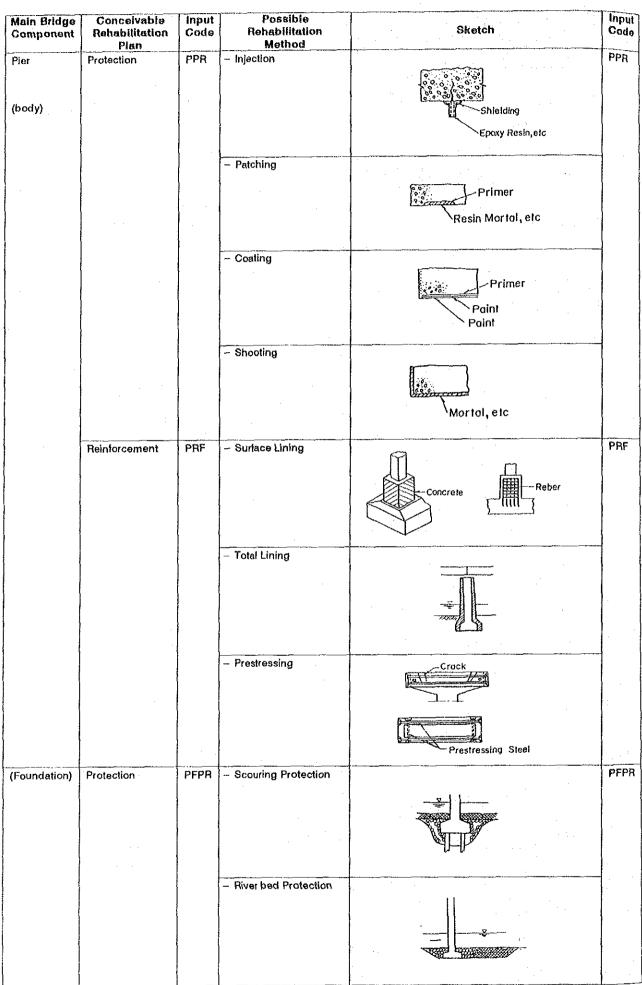


APPENDIX-H POSSIBLE REHABILITATION PLANS FROM STRUCTURAL VIEW POINT



APPENDIX-H POSSIBLE REHABILITATION PLANS FROM STRUCTURAL VIEW POINT

H – 3



APPENDIX-H POSSIBLE REHABILITATION PLANS FROM STRUCTURAL VIEW POINT

H = 4

| Main Bridge Component | Conceivable Rehabilitation Plan | input Code | Possible Rehabilitation Method | Sketch | Input Code |
|--------------------------|---------------------------------------|---------------|--------------------------------------|----------------------|---------------|
| | Reinforcement | PFRF | - Under pinning | | PFRF |
| | • | • | | 265326 | |
| | | | | Additional Pile | |
| | | · · | | | |
| Steel | Protection | SPPR | - Partial Lining | | SPPR |
| Pier (body) | | | | | |
| | | | | | |
| | | | | Concrete | |
| | | | - Repainting | | |
| | Reinforcement | SPRF | - Surface Lining | | SPRF |
| | | . * | | Stud | |
| | | | | | |
| | | | | | |
| | | | - Total Lining | Stud | |
| | | | | Concrete | |
| | | | | Ψ <u>2.00,101010</u> | |

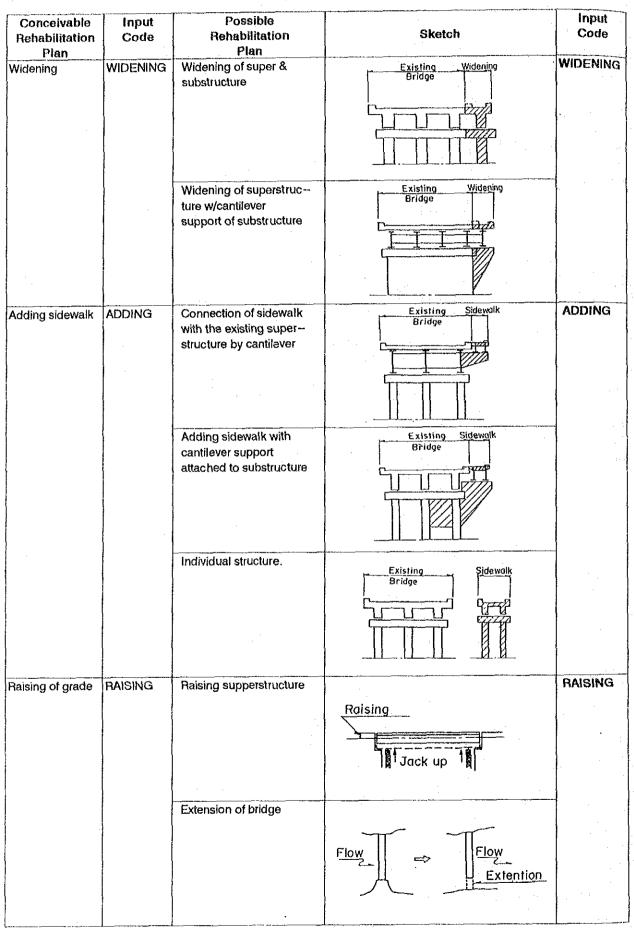
APPENDIX-H POSSIBLE REHABILITATION PLANS FROM STRUCTURAL VIEW POINT

H - 5

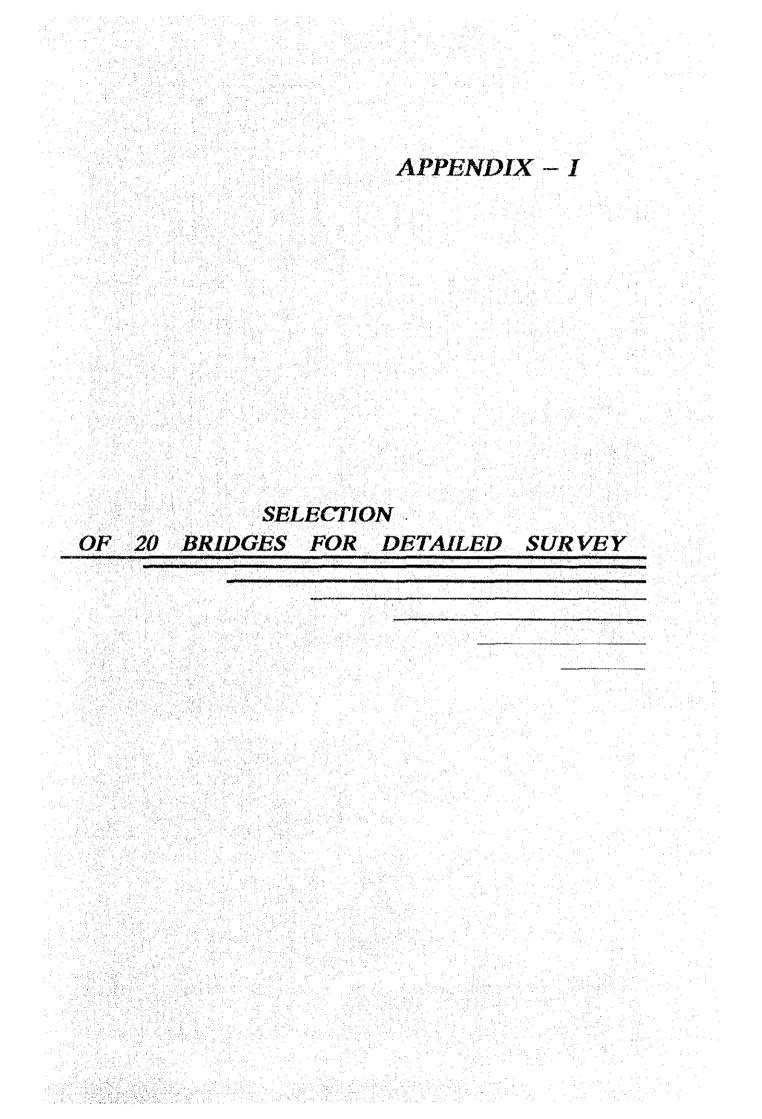
Possible Rehabilitation Plans From Functional View Point

.

APPENDIX-H



H - 6



APPENDIX-1 SELECTION OF 20 BRIDGES FOR DETALED SURVEY

| FINAL SELECTION REMARKS | | - | SA(6.28) | 8 | CB SA | SA(6.74) CB | | | | | EA SA(7.27) | | | | 5 5 |
|--|-------------------|-------------|---|--------------|-------------------------------------|--|--|------------------|--|---|--|---|---|--|--|
| RINAL | | | | | Selected | | | Selected | | | | Selected JKR | | | Selected |
| POSSIBLE REHABILITATION PLANS T FROM FUNCTIONAL VIEW POINT | ļ | | | | RAISING GRADE | ADDING SIDE WALK WIDENING & RAISING (REPLACEMENT) | No's of bridges selected a 1 | | | PAISING GRADE | | | No's of bridges selected = 2 | | |
| POSSIBLE REHABILITATION PLANS FROM STRUCTURAL VIEW POINT | | | 11 APR | ARF | 3 CBRF,DCPR 4 CBRF,DCRF | 1 ARF 4 DCRF,PPR | | 1 SEPRAPR | 3 352PA,025FA 1368FF, APR 3 1368FF, APR 3 1368FF, APR 1 138PA, APR 1 138PA,05PA,APR 3 138PA,05PA,APR 3 138PA,05PA,APR | 1 SBRF, APR, SFPR | CBRFARF 1]CBRFARF | < SBRF, DCRF, CBRF, APR | · · · · | | PRF.CBPR 1 CBPR PRF 1 CBPR |
| ABUT RATING OF PARTS ABUT BEAR DECK ING BEAM | | | | 4 - 1 - 1 - | + + + + + + + + + + + + + + + + + + | 4 T | | | 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 0 4 4 0 4 4 4 | <u> </u> | 3 = + + + + + = | 3 4 | | | 0 |
| NO. BRIDGE TYPE OF LENGTH OF SPAN (M) BRIDGE | | | 51 11 2.16 BOX 1 | - | 2 | 2 8.15 | | , T | 1.9 1.9 1.9 1.9 1.9 1.9 1.9 1.9 1.9 1.9 | s 1 3.35 SBC | 4 1 3.14 SBE | 2 1 10.72 SBC | | | 8 5 47.63 17 8 7 51.96 17 7 9 41.59 17 8 64.57 17 |
| STUDY CATEGORY CAPACITY SPAN | | | 3 MTAL 2.18 | 3 [P/A 4,95 | | 3 P/A 4.58 | | | STAL 6.21 9 57AL 1.191 9 55AL 10.81 9 57AL 6.70 9 57AL 6.60 9 57AL 6.60 9 55AL 10.81 9 55AL 6.70 9 55AL 4.79 9 55AL 4.79 9 55AL 4.79 | <u>3 STAL 3.35</u> | 3 P/A 3.14 | 3 STAL 10.72 | | | 3 STAL 12.00 3 STAL 18.80 3 STAL 18.80 3 STAL 19.57 3 STAL 19.57 |
| DISTRICT RUILT CATE | | | KLUANG 1 1937 | JASIN 1940 | KSELANSOR 1920 KMUDA/SIK 1940 | K. TINGGI 1940 Machang 1941 | | ATU PAHAT 1919 | 1920 1920 1920 1920 1940 | K. TINGGI [1928] | MANJUNG 1930 | [LRT MATANG 1936 | | n boo na anna an anna anna anna anna ann | PONTIAN 1968 K. Tinggi 1398 MANJUNG 1372 MANJUNG 1374 K. Tinggi 1374 |
| NO. KEY STATE | << 8efore 1945 >> | R.C. BRIDGE | ** BOXR.C.Box Culwert 11 00108950 JOHOR K | E | α | | No's of total bridges ≖6 STEEL BRIDGE | ā | B Coefficients PALANIC J B Coefficients PALANIC J B Coefficients PALANIC J B Coefficients PALANIC J 10 Coefficients PALANIC J 11 Coefficients NI S 12 Costocean NIS S 13 Costocean JUHCR F 13 Costocean JUHCR F 13 Costocean JUHCR F 14 Costocean XELDAH F | ** SBCSteel Beam R.C.Stab 15 00304330 JJOHOR 1 | ** SBEEncased Steel Beam 15 06000370 PERAK 1 17 00003220 JOHOR 1 | ** SBGSteel Box Grider 18 00186510 PERAK | No's of total bridges =12 << 1948 TO 1974 >> | P.C. BRIDGE | |

I – 1

| | DISTRICT B | BUILT CAT | CATEGORY | CAPACITY | SPAN OF | | CENGTH OF | ABUT | 8 | BEAR | DECK | PLANS PLANS | PLANS | SELECTION | REMARKS |
|----------------|------------|-----------|----------|--------------|---------|--------|------------|---------|------|----------|---------|-------------------------------|---------------------------------|-----------------|----------|
| | | | | | | | | GE | PIER | ING BEAM | | FROM STRUC | FROM FUNCTIONAL VIEW POINT | | |
| | | | | | | | | | | | | | | | |
| Lipis | | 1961 | 0 | STAL | 30.74 | 4 12 | 122.36 PCB | + | - | 9 | - | CBPR, BPR | | | |
| 1 | N | 1962 | T | SSAL | ł | 4 | | _ | | - | - | APR PPR CBPR | | Selected JKR | Gr AB |
| (- | KENAMAN | 3 | T | UTAL DTAL | | 1 | | 4 | | 1 | - | 000 - 01-1 000 | | HXP | |
| | | R S | | 2104 | Ţ | | | + | | | | 200 005 A05 | | | |
| | K MUDA/SIK | 19061 | | STAL | 30.64 | | PCF PCF | * . | | 14 | | DCPR PSPR | | | s |
| | | 10/01 | Ι | STAL | 30.52 | 6 | | | | * | | BRP. APR. PPR | | AXP. | SA |
| 12 | DUNGUN | 1973 | Γ | STAL | 30.50 | 9 15 | | 3 | | - | 4 | CBRF,APR | PAISING | Selected | |
| Z! | | 1974 | Π | MTAL | 45.78 | 300 | 397.32 PCB | | | | | CBRF,DCR- | | Selected JKR CA | GA |
| | | | | | | | | | •. | | | | No's of bridges selected = 4 | : | |
| l | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | |
| MARAN | | 1966 | 3 | STAL | 3.00 | - | 3.03 BOX | 9 | | | 0 | 3 DCPR, APR | | | SA(6.0) |
| a a | P.PUTEH | 1952 | | STAL | 5,411 | 0 | | 4 | 4 | | 4 | I CBRF, PRF, PFP R, AFPR | TADDING & FAISING (REPLACEMENT) | | |
| ¥ | | 1959 | Γ | STAL | 5.90 | " 0 | 53.10 PRB | | - | | 1 | CBPR | | | |
| S | × | 1960 | Π | STAL | 6.06 | 5 | | 0 | | 1 | 4 | CBPR.APR | WIDENING | Selected | св Св |
| Sil | | 1960 | Ι | STAL | 6.01 | 0 | | - | | 1 | , | PHF | ADDING SIDE WALK | | |
| | MERSING | 1064 | | STAL | 5.50 | | 14.22 PHB | | | - | 4- | COTH, FFA | | | K |
| Ne K | | 1965 | Τ | STAL | 5.88 | | | - | | - | 4 | CBPR PRF ARF | | | RA CA |
| 망 | رر. در | 1970 | | STAL | 6.18 | 0 | | | | | 1 | CEPRAPRESPR | | -ska | |
| ** RCBR.C.Boum | | | | | | | | | | • | - | - | | | |
| Ψ | MELAKA TGH | 1950 | 0 | STAL | 6.90) | | 1 5 | 5 | • | ł | 4 | | ADDING SIDE WALK | | CA.SA |
| KLUANG | NNG | 1964 | 0 | STAL | 15.90 | 00 | 27.40 RCB | 4 | 4, | - | | CBPR, PFPR | - | - | SA(7.04) |
| | COLORNAT | 8 20 | | 2141 | 20.0 | | | | - (* | | 2 v | | | Calaman INC | 17-01-01 |
| | AMAN | 1055 | | STAL | 12.10 | | 36.14 208 | | | 4 | | CERF EPS ARF PRF | | Selected | |
| Ň | er | 1995 | 0 | STAL | 6.97 | | | ŀ | | | | CBRE,PRF | | | CA.SA |
| S B D | SEPANG | 1960 | 9 | STAL | 6.95 | | | * | 4 | - | 4- - | ARF, PPR | | EX | ð |
| Y | K LANGAT | 801 | | STAL | 7 30 | | | 1 | 1 | • | ı | this bridge has been repaired | | | 80 |
| | PADANG | 1990 | | SIAL | 80.8 | 1 | 83.99 | + | | | 5 | COPH 500 000 ADD | | c | |
| ā i | AVA TON | 1801 | 2,0 | 0101 | ¥ £ | | | + | | | | | ADDING SIDE WALK | | |
| | | | | STA . | 7 43 | | 14 20 10 1 | | | | | CROF ARE DOF | | | 0000 |
| Å | N | 9961 | | STAL | 10 42 | | | . - | | | | APR AFPR PRF | | | 50 |
| Ϋ́ | MUAR | 1906 | 3 | STAL | 8.03 | | 17.82 RCB | | | 4 | 4 | 1 CBPR, BPR, PPR | | ЯХС | ۲ د |
| 1 | | | : : | | | | . : | | | | | | | | |
| 130 | ALING | 1950 | 8 | STAL | 6.56 | | | 5 3 | | - | | АРВ | | JKR | |
| SEG | AMAT | 1,950 | 4 | SSAL | 5.68 | | 7.60 RCS | 5 4 | 1 | 1 | 3 | 3 ARF, DCPR | RAISING GRADE | | _ |
| SAS | JASIN | 1955 | 0 | STAL | 6.22 | ~ | 42.70 ACS | | * | | | (PRF | | EX. | CASA |
| 쥙 | NTAN | 195 | 0 | STAL | 6.58 | | | 4 | ļ | 1 | _ | 1 ARF | | - | |
| <u>S</u> | LA KRAI | 8 | 5 | STAL | 4.63 | | 13.71 RCS | - | | - | | 4 DCRF, PPR | | Selected JXP | |
| ÷. | SING | 8 | | STAL | 1.80 | 1 | 3.60 1.05 | - | 0 | ╎ | | 4 DCHF, APR, PPH | | | đ |
| šļ, | | 1000 | | CTAL C | 8 22 | | | | | | | a DCPD | | IKP. | |
| | | | | 1 | į | | | | | | | | | | |

No's of bridges selected = 5

No's of total bridges = 32

APPENDIX-I SELECTION OF 20 BRIDGES FOR DETAILED SURVEY

APPENDIX-1 SELECTION OF 20 BRIDGES FOR DETAILED SURVEY

| | | BUILTIC | CATEGORY | CAPACITY | SPAN | E E | LENGTH OF | ARLIT | a B | REAR | DECK | PI ANS | DI ANS | NOTCH HS | REMARKS |
|-------------------------------|------------|---------|----------|----------|---------|-----|------------|-------|--------|----------|------|----------------------------|------------------------------|--------------|----------|
| F | 10111010 | | | | i | _ | യു | | PIER | ING BEAM | _ | FROM STRUCTURAL VIEW POINT | FROM FUNCTIONAL VIEW POINT | SCLECTION | |
| | | | | | | | | | | | | - | | | |
| | | | | | | | | | | | | | | | |
| ** SBBSteel Beam Buckle Plate | te | | | | | | 2 | | Ŀ | | | | | | |
| | KINTA | 1948 | 0 | SSAL | 11.50 | 0 | | | 1 0 | | 4 | | ADDING SIDE WALK | | |
| | HLR PERAK | 0561 | c | STAL | 5.30 | - | 5.88, SBB | 0 | 1 | | | | | - | ys S |
| | BENTONG | | 0 | SSAL | 3.47 | - | - 1 | - | † | | | SBPR, DSPR | | | |
| | PERLIS | | 8 | SSAL | 8.9 | - | | Ŧ | 1 | | 2 | 2 NON | | | |
| | LEMESELAMA | | J | SSAL | 5.06 | - | _ | • | 1 | | 4 | | | | |
| | SEGAMAT | 1950 | 9 | STAL | 6.29 | 2 | | I I | + | | 4 | SBRF,DSPR | | | |
| | PD | 096 | 6 | SSAL | 4.84 | - | 4.84 SBB | 4 | | | 4 | SBPR, DSPR, APR | | | |
| | BATU PAHAT | 0961 | 0 | SSAL | 5.05 | - | | - | 1 | | 1 | | | | |
| SELANGOR | K LANGAT | 1950 | 2 | SSAL | 4.73 | F | | 4 | 1 | | 4 3 | SBPR DSPR, APR | | | |
| ÷ | HULU PERAK | 098 | 6 | STAL | 9.34 | - | | 4 |] | | 9 | ISBPR, DSPR, AFPR | | | |
| SELANGOR | K. LANGAT | 1950 | 2 | SSAL | 6.29 | - | 6.29 SBB | 6 | | | Ē | 11 APR | | | SA |
| ľ | RAUB | 1050 | 4 | SSAL | 40.0 | 1 | | | 4 | | 0 | ISBRE DSPRAFPR PEPR | | | |
| | K KANGSAP | 0-0 | P | SCAL | 5 341 | - | | | | | 4 | SARE DOR AFOR | | | |
| | H, R PERAK | 0561 | ŕ | SSAL | 3.671 | - | | ŀ | t | | ľ | SRPP APR | | | SA |
| ľ | SEDEMBAN | 10201 | 16 | 2641 | 140 | ł | ŧ. | + | + | - | | | | | |
| l | RTC PADANC | 20-01 | | STAL | 4 97 | + | A 07 SHR | | | | | SEDE DERE | | Selected IKB | SA |
| | HI I DEBAK | 050 | | SSAI | 8.95 | + | | ~ | | | ſ | | | | SA |
| . | HURU PERAK | | 2 | STAL | 3.07 | + | 3.07 SEB | | + | - | | SBRF.DSPR.AFRF | | | |
| | K KANGSAR |]. | 0 | SSAL | 6.35 | - | 6.35 SBB | ļ | 1 | | | SBRF.DSPR | | | |
| | Dd | 1950 | Ð | SSAL | 6.27 | | 6.27 SBB | | | | 0 | SBPR.DSPR.DCPR.APR | RAISING GRADE | | |
| | KINTA | | e | STAL | 9.77 | 6 | E | ŀ | 1 C | • | 4 3 | SERF DSPR AFPR PPR | ADDING SIDE WALK | Selected JKP | |
| ŀ | BTG PADANG | 1950 | 0 | SSAL | 3.88 | | 4 | | | . | | 4 SERF, DSRF, ARF | | | SA |
| SELANGOR | K LANGAT | 88 | 0 | STAL | 3.24 | - | | | | . | | SEPR, DSPR, APR | | | |
| | SEREMBAN | 0981 | 0 | SSAL | 6.31 | F | 6.3t SB3 | - | | | F | SBPR, APR | | | |
| ** SBCSteel Feam B.C.SMD | | | | | | | | | | | | | | | |
| | BTG PADANG | 10561 | 9 | TSTAL | 10.88 | e | 23.18 SBC | | | | 4 4 | SBPR.DCRF.APR | | Selected JKR | |
| | L&M&SELAMA | | 0 | STAL | 7.20 | 4 | 27.141 SBC | * | - | | ľ | | | | SA |
| | MANUUNG | 1950 | | STAL | 4.78 | - | F . | - | 1 | - | ľ | SBRF, DCRF | WIDENING | | CA.CB |
| 00237200 PAHANG | KUANTAN | 1900 | 0 | STAL | 8,90 | 6 | 26.701 SBC | 4 | 4 | | 4 | SBPR, AFPR, PRF | | Selected | Q |
| E | U.LANGAT | | | STAL | 18.24 | 9 | | | F | 4 | - | SBPR, BPR | | | |
| SELANGOR | K.SELANGOR | L | | STAL | 12.61 | 9 | ٢. | F | 4 | * | 1 | BPR,PPR | | JKR | ð |
| | | | | |] | | 1 | | | | | | | | |
| | 146DCING | 10501 | | STAL | 104 401 | | | | | | - | 11498 | ADDING SIDE WALK | | |
| | | 2 C | | | | | | | | | | | | | <u> </u> |
| | NSSAL | INCR L | 0 | SIAL | 4.4 | | | _ | 1 | - | 4 | | | sciecies | ¥ C |
| No's of total bridges = 32 | | | | | | | | | | | | | No's of bridges selected = 5 | | |
| | | | | | | | | | | | | | | | |
| Service no | | | | | | | | | | | | | | | |

1 - 3

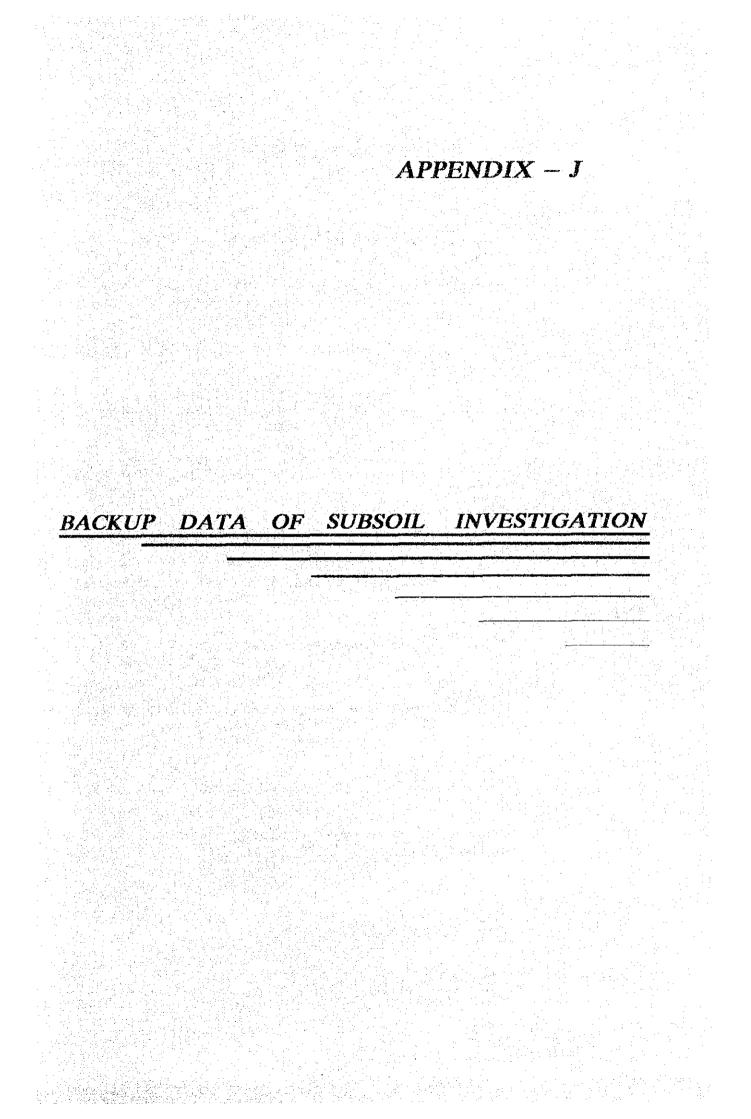
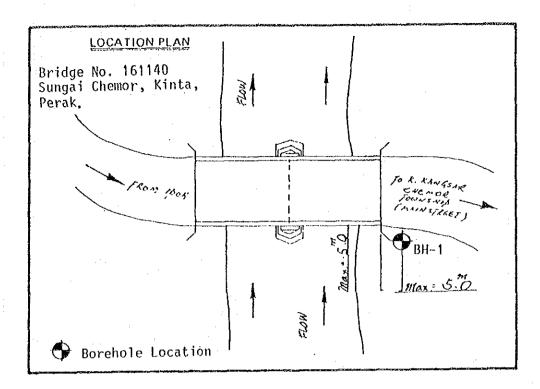
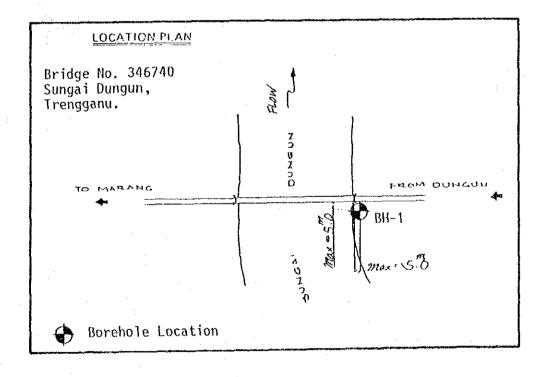


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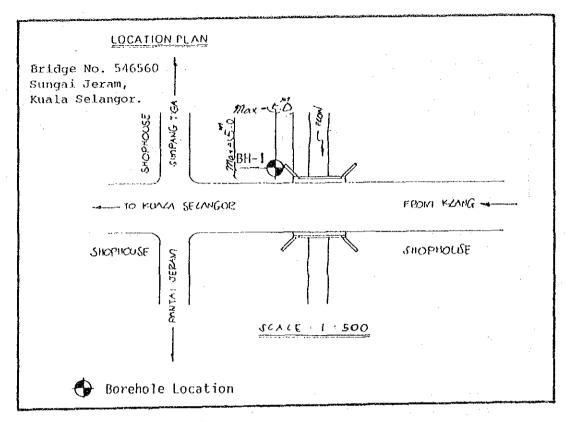
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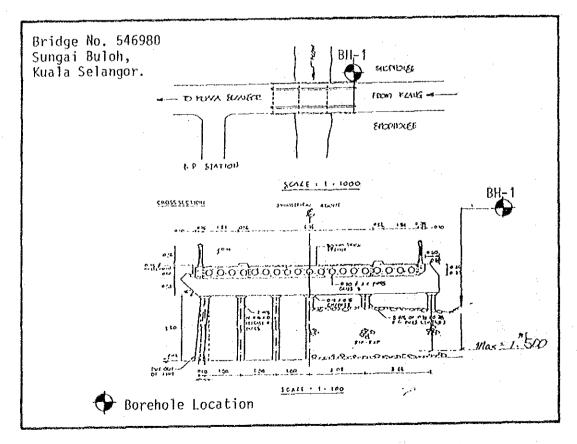
Borehole location at Bridge No. 00161140, Perak.



Borehole location at Bridge No. 00346740, Terengganu.

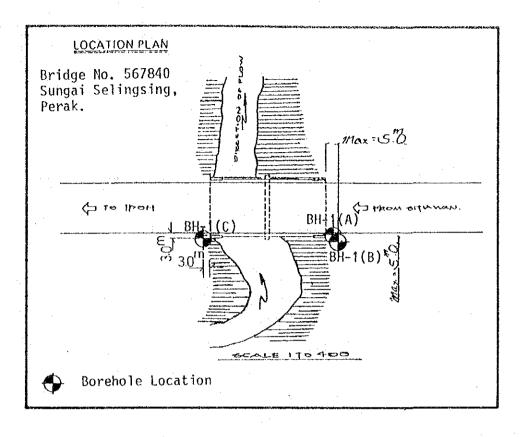


Borehole location at Bridge No. 00546560, Selangor



Borehole Location at Bridge No.00546980, Selangor

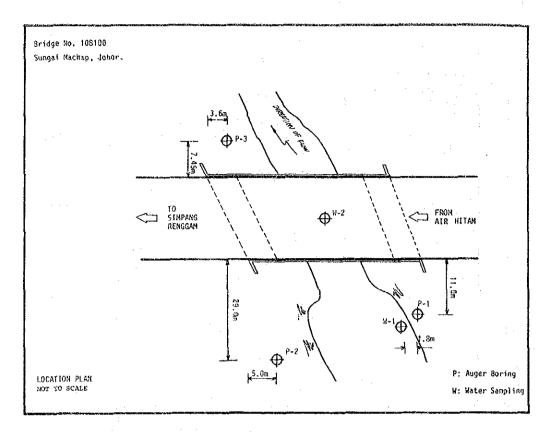
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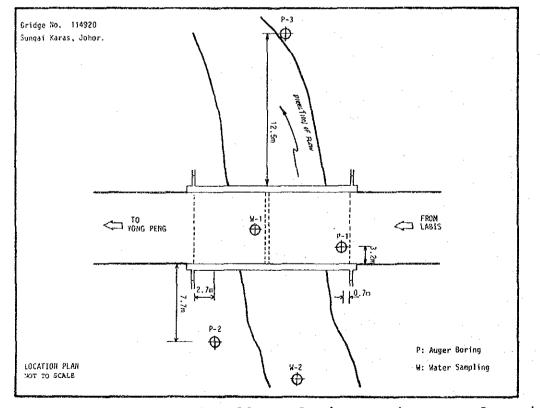
Borehole location at Bridge No. 00567840, Perak

J - 3

Append-J

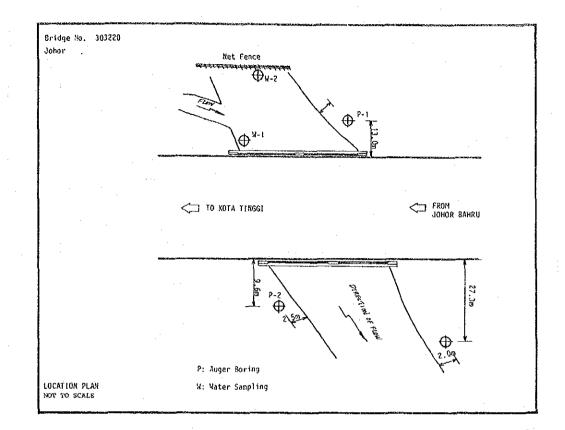


Locations of Hand Augers and collected river water samples at Bridge No. 00108100, Johor

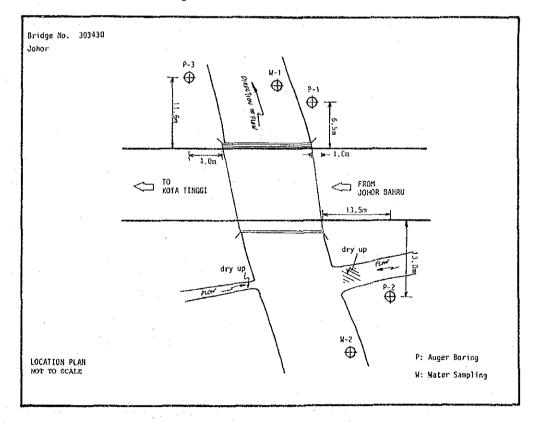


Locations of Hand Augers and collected river water samples at Bridge No. 00114920, Johor

J – 4

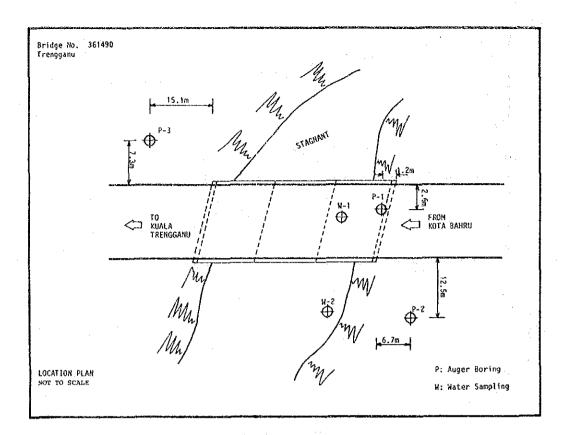


Locations of Hand Augers and collected river water samples at Bridge No. 00303220, Johor

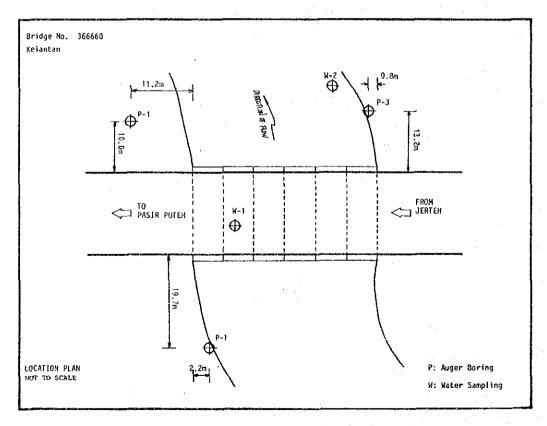


Locations of Hand Augers and collected river water samples at Bridge No. 00303430, Johor

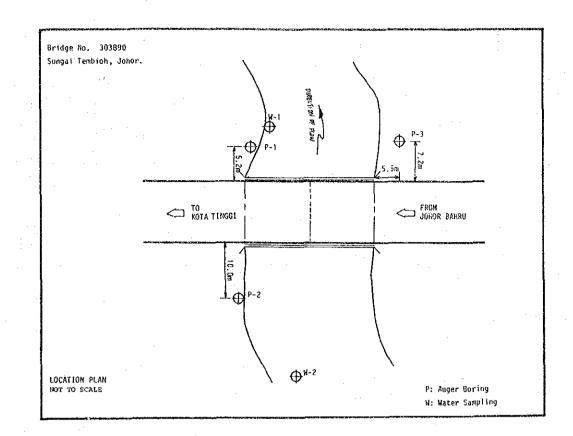
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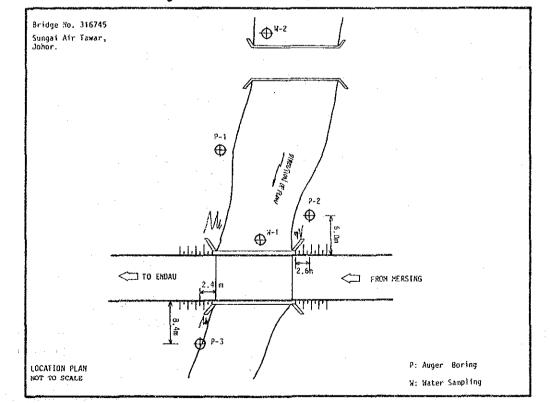
Locations of Hand Augers and collected river water samples at Bridge No. 00361490, Terengganu



Locations of Hand Augers and collected river water samples at Bridge No. 00366660, Kelantan



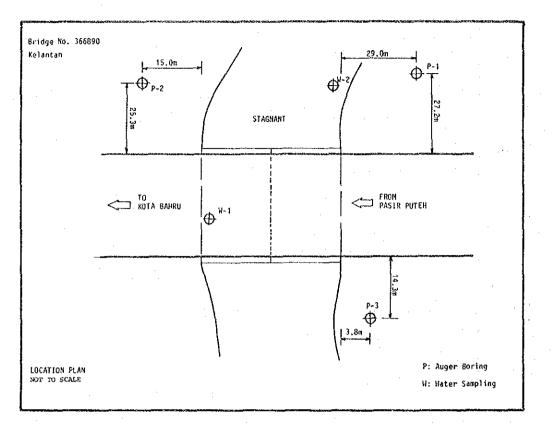
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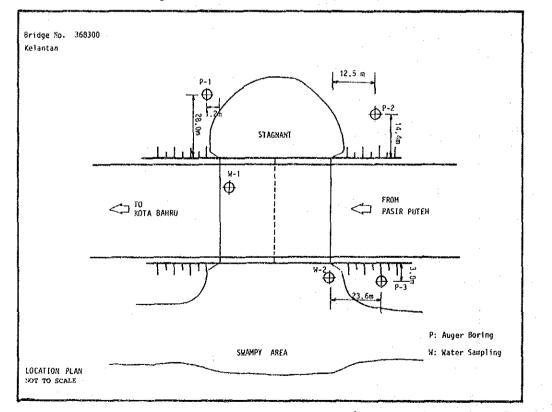
Locations of Hand Augers and collected river water samples at Bridge No. 00316745, Johor

J - 7

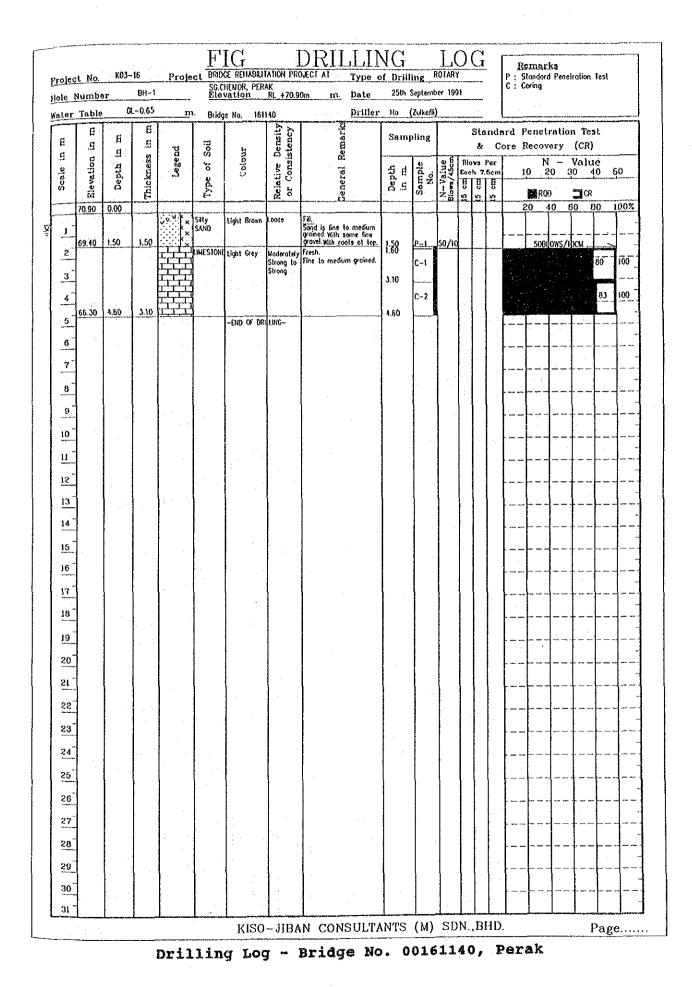
Append J



Locations of Hand Augers and collected river water samples at Bridge No. 00366890, Kelantan



Locations of Hand Augers and collected river water samples at Bridge No. 00368300, Kelantan



J — 9

Append-J

| Ducing | . N. | K03- | - 16 | Proie | | IG ABILITATION | - | DRILLII AI Type o | | ing |) | | <u>1</u> | | lema: Stonilar | | tration | Iest | |
|------------------------|----------------|--------------|--------------|-------------------------------|--------------------------------|---|------------------------------|--|-------------------------|---------------|-----------------------|-------------|------------|-------------|-------------------|------------|--------------|----------------|-----------|
| Projec Usia | | | 8H-1 | | | UNGUN IER Vation | | | | | | | emhe | - L | a rondo | u rene | ti otion | 1036 - | |
| <u>Hole I</u> Water | | | | 11 | | • | | Driller | | (Leon | | <u>sept</u> | | | | | | | |
| E | 6 | E E | E | | [| | Density is tency 0,125 | Remarks | Sam | | | 5 | Star | dard | Penel | tratio | n Te | şL | |
| Ë | u u | E. | | Legend | Soil | Colour | ttive Density Consistency | | | l u | w E | Blot | rs Pe | r I | | 4 — | Valu | ie | |
| Scale | Elevation | Depth | Thickness | 3 | Type of | පී | Relative or Cons | General | Depth in m | Sample No. | N-Value Elows/45cm | | 7.5c | | | 20 | 30 . 4 | | <u>50</u> |
| | 5.60 | 0.00 | | × 1- | | Whitish Grey with | | // #1 | | | | - | _ | | 1 | 1 | r | <u>ر</u> | |
| 1 | 4.30 | 1.30 | 1.30 | | Clovey SR T | Grey with Reddish and Yellowish | ĺ. | (Fill). Traces of fine sond and gravel. | | | | | | · | | | | - <u>-</u> - | |
| 2 | | | | ×* | SAND | Yellowish Brown | | Fine to coorse sand. Silly up to 1.8m. | 1:85 | <u>P=1-</u> 1 | 5. | 1 | | 2.9. | | | | | |
| 3 | | | : | * | | | | Fine sond predominates up to 4m. | 3.15 | | | ः 1 | | 14. | | | | | |
| 4 | | - 14 | | | | | | With some fine gravel below Am. | 3.15 3.45 | P=2] | 4 | 2 | 4 | ╘╻ | | | | L | |
| 5 | | | | 7 ° | | | | | 1.63 4.93 | P=3 | 3 | 0 | 0. | ┊┥┥╴ | | - | . | | |
| 6 | | | | | | | | | 6.15 6.45 | P-4- | 3 | 0 0 | 1 | · | · - · | | | | |
| 7 | | | | | | | | | U,9J | - | - | 0 (| - | −][| · | | | | |
| 8 | -1.95 -2.50 | 7.55 8.10 | 6.25 0.55 | <u>, v ⊻</u> [× | STLY CLAY | Derk grey | Soft | With organic matter and fine sand. Traces of mica fragment/ | 3.85 | P=3-1 | 2 | 0 | | - - | · | | | | |
| 9 | | | | • | SAND | light brown | Varu traa- | Fine to coase sout | 9.15 9.45 | P-6 | 3 | | 0 | | | | | - -; - | |
| 10 11 | | | | e o | DAM | la Light la Light Grey la Grey | to Medium | with the to medium sond. Slightly clayey at battom. With the gravel below 10m | 10.65 10.95 | P-7 | 15 | 3 3 | | 3 | | | | | |
| 15 | | | | <i>©</i> | | | | Noz.da.8mm. Irace of sit below 10m. | | | | 7 | 5 | | [| | [| [| |
| 13 T | -6.60 | 12.20 | 4,10 | ×××× | <u> </u> | | | Sandy clay lense with shell fragments at bottom | 12.15 12.30 | P-8- | | | 17 | | 508 | 107/1 | 5CM | | |
| 14 | | | | Qîx^x | SiLT with rock fregments | Red to Grey Motiled Yellow and Brown | | Completely Weathered sedimentary rock Frioble to sill with hord rock fragments. | 13.88 | P_9_ | 50/15 | 18 32 | _ | | 508 | ows/1 | БСМ | | |
| <u>15</u> | | | | * * * * * * * 0 0 * • * | | Li Cint | | | 18:58 | P-10 | <u>50/22</u> | 20 5 25 | 15 2 10 | ، | 506 | iows/2 | 2.5C# | | |
| 16 | | | | × × × × × × | | | | | 16.50 16.55 | <u> 2-11</u> | 50/5 | 50 | | _} | 508 | 10#\$/! | см _ | | } |
| 17 18 | ~12.46 | 18 06 | 5.86 | ***** ****** | | | | | 16.55 18.00 18.06 | P-12 | 50/6 | 50 | | | 508 | 10%S/6 | | | |
| 19 | | | | | | -END OF | DRALING- | | 18.06 | - | | | | 1 | [|] | | | |
| 50 | | | | | | | | | | | | | | | | 1 | | | |
| 21 | | | | | | | | | | | | | | 1 | | [| | | |
| 22 | | | | | | | | | | | | | | 1 | † | 1 | † | | |
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| 28 | | | | | | | | | | | | | | | <u> </u> | · | _;_ | | |
| 58 | | | | | | | | | | | | | | | | | | | |
| 30 | | | | | | | | | | | | | | | | | · · · · · | | |
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| | | | | | | KISO- | - JIBAN | N CONSULTAN | VTS (| (M) | ŚDN | I.,E | HL |) | i | | Р | age | |