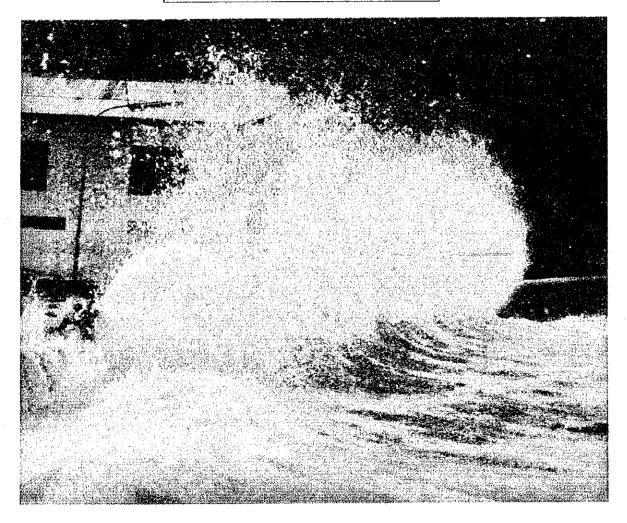
THE DEVELOPMENT STUDY ON THE SEAWALL CONSTRUCTION PROJECT FOR MALE' ISLAND IN THE REPUBLIC OF MALDIVES

SUPPORTING DATA II



DECEMBER 1992

JAPAN INTERNATIONAL COOPERATION AGENCY

SSS
CR (3)
92-125

No. 52



THE DEVELOPMENT STUDY ON THE SEAWALL CONSTRUCTION PROJECT FOR MALE' ISLAND IN THE REPUBLIC OF MALDIVES

SUPPORTING DATA II

DECEMBER 1992

JAPAN INTERNATIONAL COOPERATION AGENCY

国際協力事業団 24467

Composition of the Report

:

This report consists of six volumes as follows;

- Summary Report
- 0 Main Report I
- Main Report II 3

6

- **(4**) Supporting Report
- Report for Male' :

Summary

- Report for Funadhoo ;
- Supplementary Study Report :
- Topo/Hydrographic Maps :
- 6
- Oceanographic Survey Data :
- Supporing Data II

Supporting Data I

Table of Contents

Supporting Data II

Chapter	1	Soil Data	1 - 1
Chapter	2	Oceanographic Data	2 - 1
Chapter	3	Statistical Data of Male' Island (Population and Housing)	3 - 1
Chapter	4	Meteorological Data	4 - 1

- i -

Chapter 1. SOIL DATA

- 1.1 Geology of the Maldives Islands
- 1.2 Geology of Male' Island
- 1.3 Geology of Funadhoo Island
- 1.4 Soil Investigation, Male' Island
- 1.5 Material Tests

APPENDIX

- Photographs of Field Investigation
- Photographs of Rock Cores

1.1 Geology of the Maldives Islands

(1) Formation of Maldive Islands

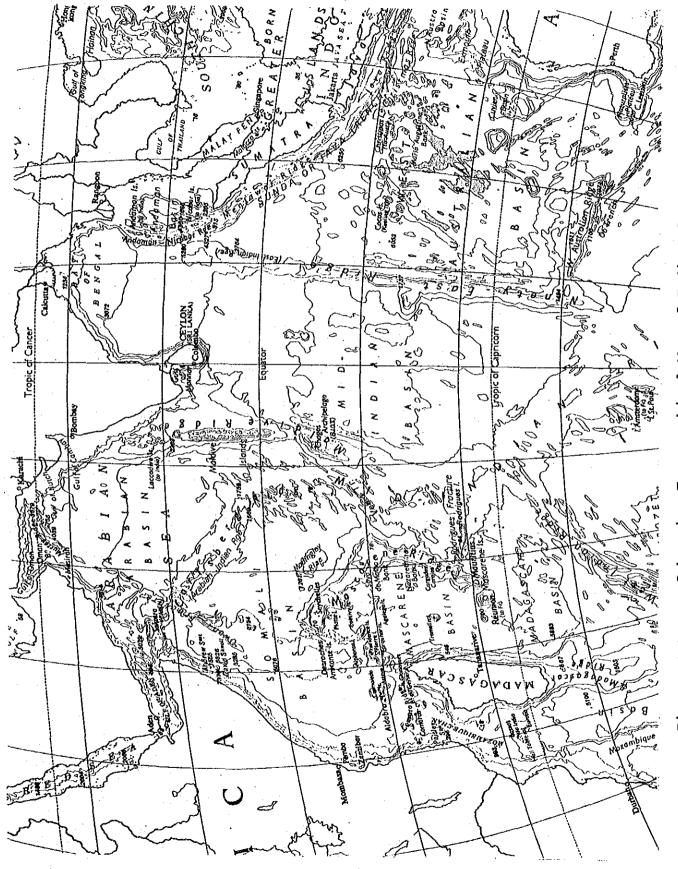
The Maldive Islands form the main part of the Maldive Ridge which extends from the Laccadive Islands into the Chagos Archipelago in the north-south direction. The Maldive Ridge lies between the Arabian Basin and the Mid-Indian Basin and is a chain between the Indian Continent and the Carlsbery-Mid Indian Ridge. (Refer to Figure 1.1)

According to the theory of plate tectonics, the Carlsbery-Mid Indian Ridge is a midoceanic ridge which is a spreading center of ocean plates. While the Maldive Ridge divides both the ocean plates of the Arabian and the Mid Indian Basin, and originated from a transformed fault resulted in a different moving velocity of the both ocean plates. According to Purdy, E.G. (1981), the results of a deep sea drilling by Esso Exploration Inc. Indicated more than 2,100 m of shallow-water carbonate sediments overlying the Eocene volcanic rocks, in the Maldives Islands. Therefore, the Maldive Ridge consists of the thick shallow-water carbonate sediments and the under lying volcanic rocks which erupted along the transformed fault. (Refer to Figure 1.2)

The shallow-water carbonate sediments having a thickness of about 2,100 m were mainly made up of coral and grew continuously up over the shallow submarine volcanic mountain ridge formed in the Eocene age (38 to 55 million years ago). Therefore, it is estimated that the shallow submarine volcanic mountain ridge submerged at least to a depth of 2,100 m during 38 million years and the carbonate sediments consisting mainly of coral grew up 0.06 m/m per year in ratio.

(2) Atolls and Faros

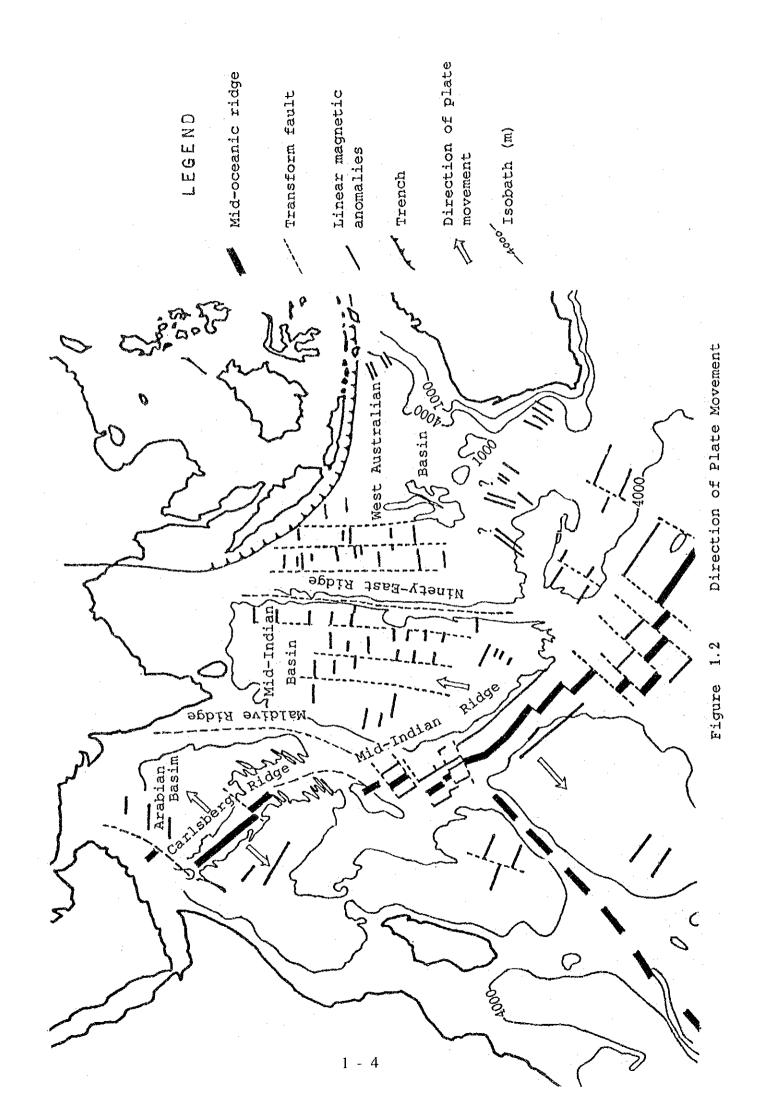
Large or very large atolls in the Maldive Islands are 30 to 80 km long, the lagoons of which being generally $35 \sim 70$ m deep. Between these atolls are channels generally more than 400 m deep. The large or very large atolls contain many faros in their lagoons in addition to those occurring on their outer edge. A faro which indicates the unique features of Maldive atolls, consists of a small circular coral reef and shows a double circular structure together with a large atoll. Some of faros are 10 km or more in length, but the majority are smaller. The smallest are almost circular, but others are elongated parallel to the edges of the large atolls. Their lagoons vary in depth between $4 \sim 6$ m and almost 40 m.



Submarine Topographical Map of Indian Ocean

Figure 1.1

1 - 3



The lagoons of atolls having depths 35~70 m can be explained by the glacial control theory. During the Last Glacial Stage, the floors of the present lagoons were erosion surface as the result of sea-level falls. Having emerged above the surface, the floors become karstified by rainfall and percolating water. Subsequent submergence of such a structure resulted in revival of coral growth at the knolls and along the outer edges of the lagoons. While the lagoons in faros having a depth of 4~6 m, are explained by the sea level change during Holocene age (10,000 years before~present) after the Last Glacial Stage. The lagoon floors in the faros become erosion surface as the result of sea level stop and fall, at a point of time during Holocene age. After that, coral reefs grew up along the edges of faros as the result of subsequent rise in the sea level. (Refer to Figure 1.3)

1.2 Geology of Male' Island

Male' Island is a faro which is located at the southeastern end of the North Male' Atoll. The faro of Male' Island is composed of a horseshoe shaped coral reef, a lagoon enclosed with the reef, and an island in the lagoon. (Refer to Figure 1.4)

The coral reef is made up of submarine outer edges, detrital outer ridges with coral detritus which are indicated by breaker zone, and reef flats in the inside of outer ridges.

The horseshoe shape of the coral reef in Male' Island probably resulted from contrasts in the rates of reef growth, which are related to the waves generated by the south-east monsoon wind. Therefore the coral reef grew up well at the southeastern outer edges, but developed poorly along the northern outer edges.

The inner reef flats having many deep wave furrows, were found between the outer ridge and the lagoon as shown in Photographs 1.1 and 1.2 taken in 1980~1982. At the present time, the lagoon naturally remains along the east coast only. On the other coasts, the lagoon changes into the northern harbor and the southwestern domestic harbor as a result of the reclamation.

The original island having a 2 m height, is made up of the lagoon sediments (coral silt, sand and gravel) and the accumulation of coral detritus resulting from transportation by wave action.

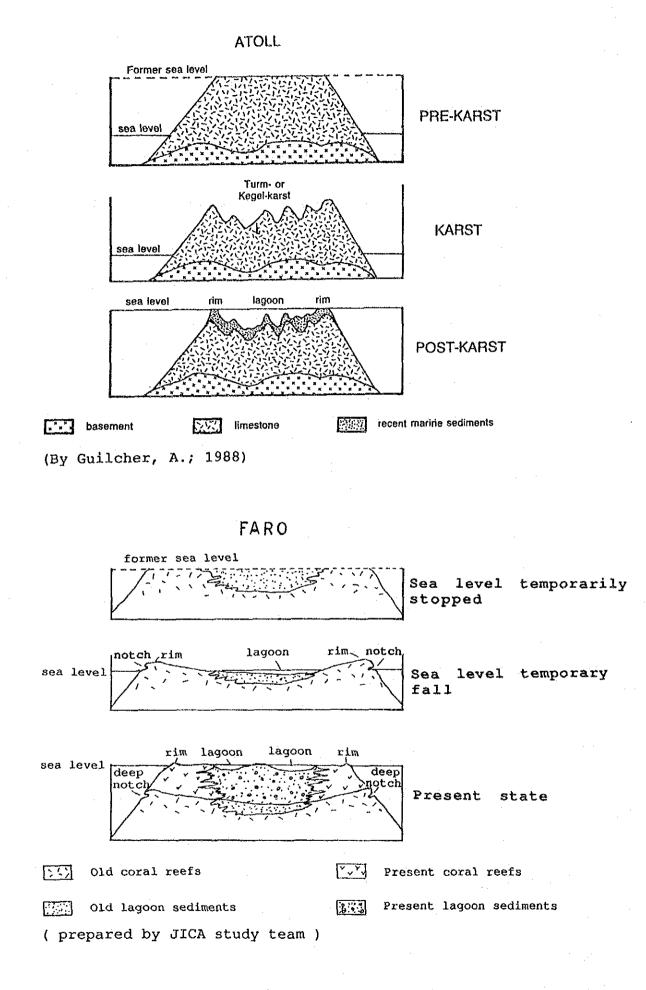


Figure 1.3 Formation of Atoll and Faro

1.3 Geology of Funadhoo Island

Funadhoo Island is a small faro which is located about 700 m northeast of Male' Island. Funadhoo Island consists of a circular shaped coral reef with a diameter of about 400 m, an island having a diameter of about 200 m and lagoons between them. (Refer to Photograph 1.3 and Figure 1.5)

The coral reef is composed of submarine outer edges extending to the southeast, and detrital outer ridges which are indicated by breaker zones resulting from the southeast monsoon winds. The reef flats and the lagoons were disturbed by the breakwater construction and the dredging for the two boat harbors, but the reef flats are widely exposed along the south and the east coast of the island. The sandy beaches are scattered around the island. The island is made up of a sand cay covering the reef flats and has vegetation of coconut.

1.4 Soil Investigation, Male'

(1) **Previous Investigations**

The bore holes and the test pits for the previous foundation investigation are shown in Table 1.1. Also, the locations of the bore holes are shown in Figure 1.10 mentioned later. Both tables and figures include the three bore holes of this soil investigation for the Seawall Construction Project. The previous bore holes totalled 44 holes and 719 linear-meters. Their drill logs are summarized in Figure 1.6.

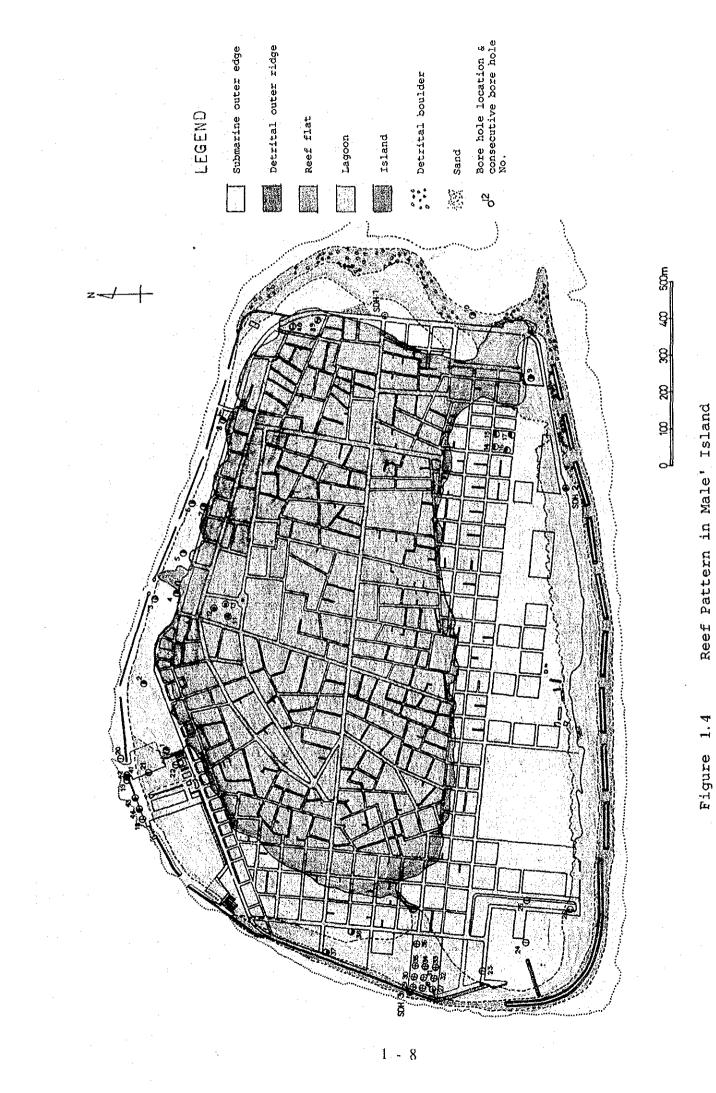
(2) Field Work and Laboratory Tests

The core drilling with a standard penetration test (S.P.T.) were performed for the purpose of obtaining geotechnical and soil data about sub-surface conditions along the proposed seawall alignments. The three bore holes (SDH 1, SDH 2, and SDH 3) were drilled by a hydraulic feed, rotary type core drilling machine at the east coast, the south coast and the west coast of Male'.

Their locations are shown in Figure 1.10 mentioned later. The depth and the number of S.P.T. of each bore hole are shown in Table 1.2. Also, the drilling log of each bore hole is shown in Figure 1.7 t o 1.9.

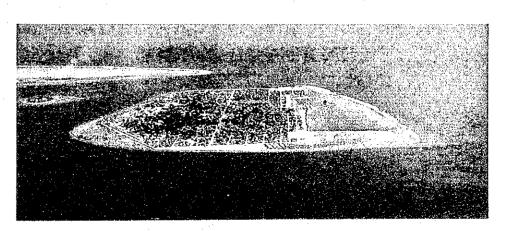
The unconfined compression test and the unit weight test concerning the nine core samples taken from the bore holes, were carried out in accordance with JIS and test standards based thereon at the laboratory in Singapore. These core samples were

1 - 7





Photograph 1.1The East Coast and the South Coast Viewtaken in 1980 ~ 1982

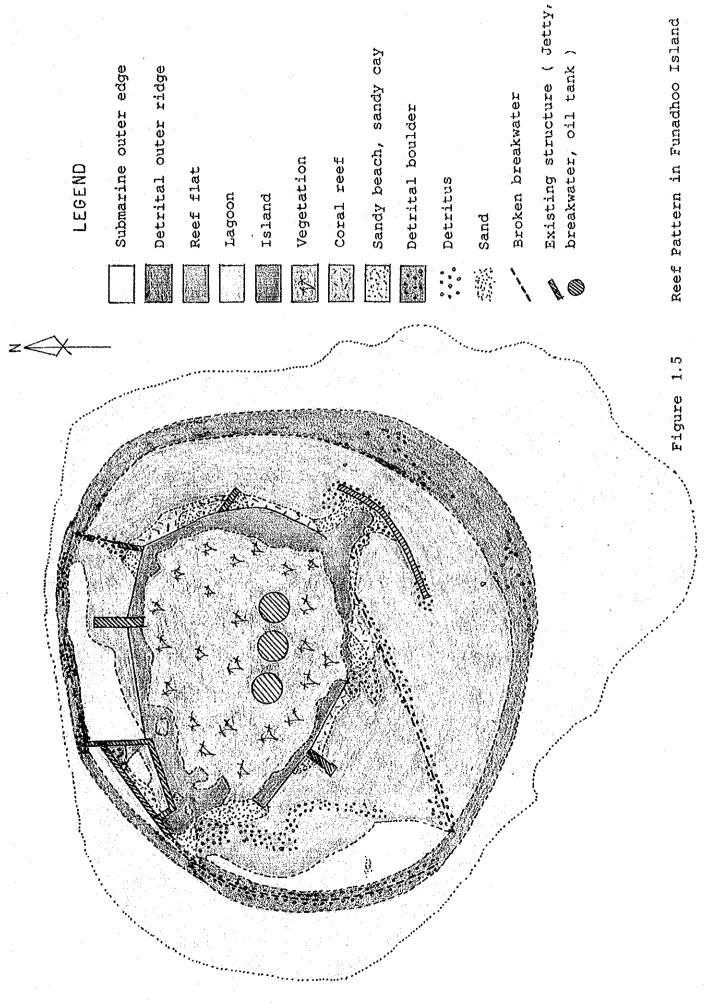


Photograph 1.2The South Coast and the West Coast View
taken in 1980 ~ 1982

1 - 9



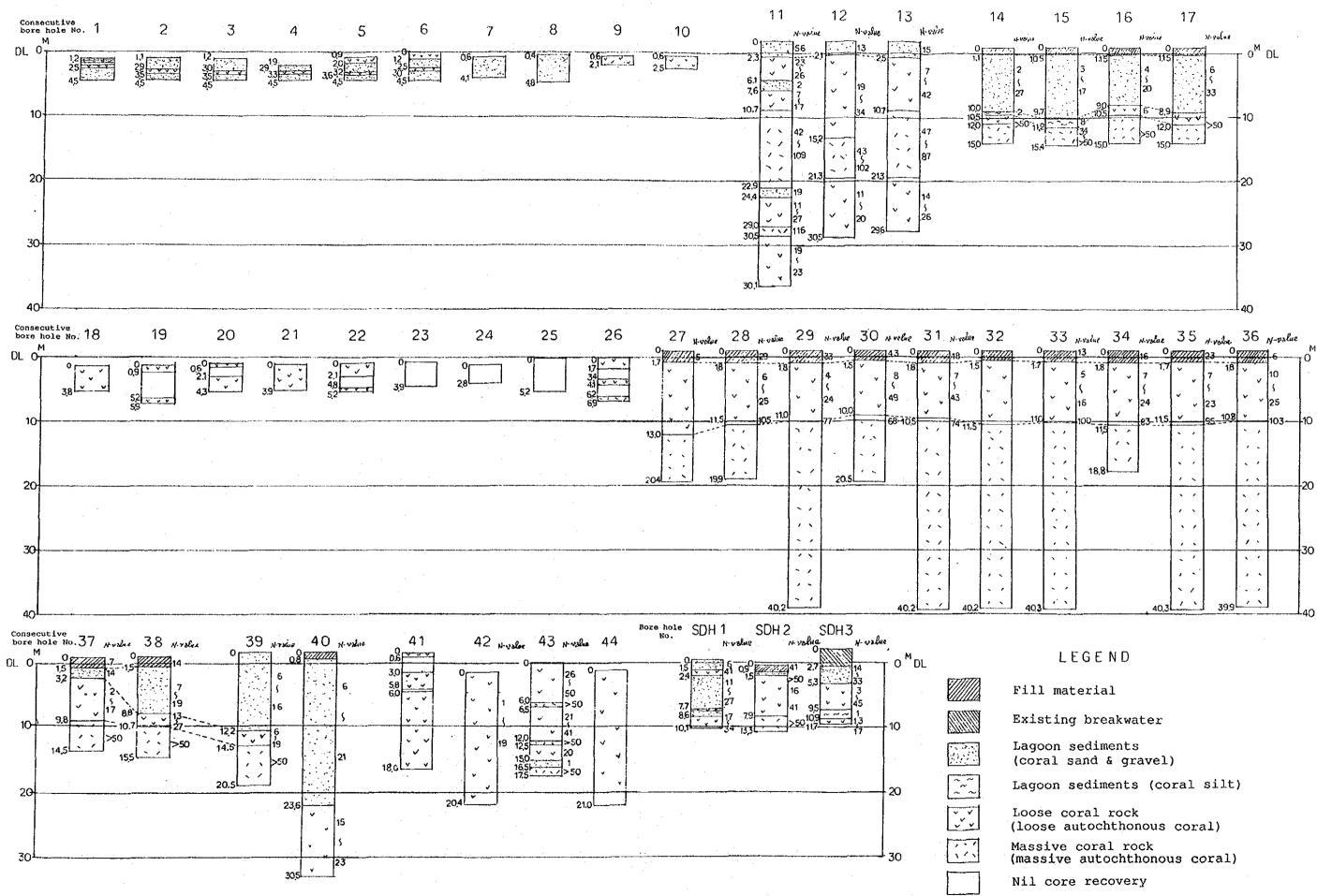
Photograph 1.3 Bird's Eye View of Funadhoo Island at the Present Time

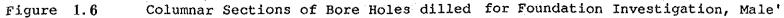


^{1 - 11}

Project Name	Date		Bore Hole	S	Test	Project Name	Date		Bore Hole	s	m
TOJECT HUNG	Date	Symbol & Consecu- tive No.	llole No.	Depth	Pits	rroject Name	Date	Symbol & Consecu- tive No.	Hole No.	Depth	- Test Pits
Male' Ilarbour	Mar. 29) Apr. 1 1973	1 2 3 4 5 6 7 8 9 10	BII 2 3 4 5 6 7 8 9 10 11	(m) 4.50 4.50 4.50 4.50 4.50 4.50 4.50 4.10 4.80 2.10 2.50		Indira Gandhi Memorial Hospital	Jun.) Jui. 1989	 ⊕ 27 28 29 30 31 32 33 34 35 36 	BH 1 2 3 4 5 6 7 8 9 10	(m) 20. 40 19. 85 40. 15 20. 50 40. 15 40. 20 40. 30 18. 80 40. 30 39. 85	
			tal	40. 50					tal	320.50	
Grand Friday	Dec. 29 1982 2	• 11 12	BH 1 2	(m) 38, 10 30, 48		Centre for Social Edication	Feb. 4 2 7	37 38	BH 1 2	(m) 14. 50 15. 50	2Pits Depti 1.5m
Mosque	Jan. 11	13	3	29. 57			1990	 To	tal	30.00	each
	1983	10	tal	98.15			Feb.	Θ		(m)	
Kalaafaanu Primary School	Jul. 18 21	14 15 16	BH 1 2 3	(m) 15.00 15.38 15.00	4Pits, Depth; 1.5m	Private Client	8 2 12 1990	39 40	BH 1 2	20. 50 30. 45	
	1987	17	4	15.00	each		1000	To	tal	50.95	
		То	tal	60. 38		Male'	Feb.				0.0.1
Male' Port Development	Oct. 1987	① 18 19 20 21	BH 1 2 3 4	(m) 3. 80 5. 85 4. 25 3. 90		Nate Port Development	18 21 1990				9Pits Depti 0.5m 2 1.4m
		22 23 24 25 26	5 7 13 14 16	5. 20 3. 85 2. 80 5. 20 - 6. 85			Nov. 28 1990 2 Mar.	41 42 43 44	BII 1 2 3 4	(m) 18. 00 20. 35 17. 46 21. 00	
		То	tal	41.70			12 1991		4 tal	76, 81	4
Blectric Power Station	Oct. 1988				5Pits, Depth; 2.5m each	Seawall Construc- tion	Sep. 25 } Oct.	0	SDH 1 2 3	(m) 10. 45 10. 32 11. 57	
1						1	3				-

Table 1.1 List of Bore Holes and Test Pits excavated for Poundation Investigations, Male'





Bore Hole No.	Location	Depth	Number of S.P.T.
SDH 1	East coast	(m) 10.45	10
SDH 2	South coast	10.32	10
SDH 3	West coast	11.57	10
То	otal	32.34	30

 Table 1.2
 The Depth and the Number of S.P.T of Each Bore Hole

coated with paraffin on samples wrapped in transparent vinyl sheet, in order to keep the natural condition. The results of the above-said tests are shown in Table 1.3.

(3) Geological Classification

The geological classification which is summarized in the above-mentioned Figure 1.6, is defined as follows.

Fill material : The fill material consists of coral detritus including many kinds of rubbish.

Existing breakwater : The concrete body of the existing breakwaters located on the east, the south and the west coasts.

Lagoon sediments (coral sand and gravel) : The lagoon sediments consist of coral sand and gravel, including seashells in many cases. Sometimes, grading and sorting are found in the sediments. The N-values of S.P.T. in the sediments range from 3 to 33.

Lagoon sediments (coral silt) : The lagoon sediments consist mainly of coral silt, and include clay and fine coral sand. Seashells and organic materials are occasionally found in the sediments. the N-values of S.P.T. in the sediments range from 1 to 3.

Loose coral rock (loose autochthonous coral) : The loose coral rock is the reef building coral which grows up in-situ, with a many pores and cavities. therefore, its physical property is weak, the N-values of S.P.T in the loose coral rock range from 2 to 50 and the core recoveries are low. Based on the data of the previous and this investigations, the unconfined compressive strength on the core samples in the loose coral rock ranges from 5 to 135 kgf/cm², with an average of 70 kgf/cm². But the values may not be typical because the test was performed on the core samples only.

· · · · ·	lumbe Table		SDH- L Séo L		<u>Ele</u>	valion	DL +0.	4 <u>m. Date</u> Drillei		5 - 28 Shah)	, 1991	~-~-	6 114		C : Corine	•			
E	1401e E	B	3 19		Soil		ensity tency	eneral Remarks	Sam						rd Pen ore Rec				
Scale in	Elevation	Depth in	Thickness	Legend	õ	Colour	Relative Density or Consistency	ral Re	Depth in p	Sample No.	N-Value 210-m/30cm	Esc	₩J 8 h 10	em	10	N 20			50
Š					Type		Rela	en e	ļ	5 5 5 5 7 5 7 7 7 7 7 7 7 7 7 7 7	N-N Blogs	од Ю	10 cm	10 - CH					1002
1	-1.10		-0.20 1.30	1914 (A) 1914 (A) 191	Corol Gravel Ind Goulder	Grey to while	Very dense	Water transported well rounded well graded gravels and boulders of moderately strong	1.92	8-1	6	1	2	3		40	60	<u> </u>	
2	-2.00	2.40	0.90			d Yellowish	Loose	cord rock. Well graded. With Iol of seashelf debris.	2255 2200 2255 2200 2255	P-2	41	17	13	11				180 1	
<u>3</u> 4				200	foral Roc	gray Grayish white	Moderately weak to	<i></i>	3.15 3.15 3.15 3.15 4.15 4.45	P=3-	27	8	8	<u>11</u>				180	
5				4	Cordi San	dGravish	weak Medium	graded sond seams.	4.15 4.45 5.15	P-4			_	4 - 3	·	1			
8			i	220		while	dense	Well graded with some medium to coarse gravels (Diamax.=35mm; Calcareous and weak	5050200 5050200	P-6				5			60	80	
7 	=7.30	1.20	6.49	20 20 20 20 20				cord fragments.) Presence of s21 (?). With red honeycombed cord rock at 2.40m.	6500 500 500 500 500 500 500 500 500 500	P=7-	18	6	7	<u>5 ·</u>	10	¥		-	
9	-8.20	8.60	0.80		ord Roc	White	ife ok	fractured, weak,	8.45 8.79 9.15	P-8 G-1- P-9	18 34		7 15			1145			
10	-10.05	10.45	1.85		forat San	Croyish white	Wedium dense	Well graded. With some medium to coarse corol fragments	8:18 9:91 18:15	6-2 P-10			4	.11				85	
<u>11</u> 12	- EN	DOFDR	LLING		Coral Roc	While	Weak	(Dia max.= 30mm). Highly traclured calcoteous corol.	10.45						┝━┶┝╴╴		-+	╞╌╴	
13	1							caccoreous corol. Presence of well graded corol sand pockets at top portion.							┝╺═╺╌┠╌╺ ┝╶╴				
14					ا		+	J							┝╾━┝╌╴	·			
<u>15</u>					-											•		┥╌	
16 17														•		· 	•+		
18																·	<u> </u>		<u> </u>
<u>19</u>					.*: 											· - - ,-	•		
20 21																			
22																·	·+		
23					:												<u> </u>]
24																•			<u> </u>
25 26																· -	• + - •		
27															╷┈╺┝╸┙		1		
28										- -					;; ; ; ; ;		· <u></u>		
29 30														•			•		<u> </u>
31									5. - 5.						┝╼╼┝╸╸	·	+	•	

Projec	t No.	\$03-	31	Proje	CL SEAI	VALL CONST	RUCTION -	DRILLI MALE Type	NG of Drill	ing f	L.()(<u>.</u>	P : 1	temer) Standard		ration	Test	
Hole	Numbe	r	SOH-	2	Ele	vation	0L -0.	4 m. Date	SEP.29) - 00	1.01 19	91	-	U :	Coring				
Water	Table	A	t Sea L	evel m				Driller	LOR	(SHAH)		-	L					
E	ŭ E	E E	ů B	দু	Soil	by	ensity tency	Remark	Samp	oling					Penetr Recove				i in an a takat
Scale in	Elevation	Depth 1	Thickness	Lægend	jo	Colour	Relative Density or Consistency	jeneral Re	Depth in m	Sample No.	N-Value Blows/Jocm	Blove Each	l0cm		N 10 2		Valu 0 4	e 0 (50
<i>w</i>			<u>Å</u>		Type	 	Rela	ğ	83	S.	-N N N	10 cm					C R		
	-0.40	0.00	0.60		Coral	Gray	Dense	Fill (Reclamation	100				+	-	20 4		<u>0</u>	0 1	00%
1	-1.00 -1.30 -1.90	0.60 0.90 1.50	0.50	000	Boulder			area). With concrete	1:89							42			
2	-1.30	1.50	0.00			Dark gray	Dense	plastic refuse etc. Medium to coarse	000	P-1		12 15				50			
3			. · ·		jora Gravel	Dar guy	Dense	subangular gravels (Dia.max.=25mm), With some coral sand and		P-2 1	50/21	17 21	12/		5060	S₩S72	704		
4							ł	some coral sand and lot of argonic decays.	315	P-3-	38	8 14	16						100 ~
					Coral San	Grayish white	Dense	Woll graded. With some fine (Dia, max, = 6mm)	4.45	P=1-1	41	12 11	18		+			l	
5	1						<u> </u>	coral grovels.	5.0046	C-4 P-5	17	65	6						100
6					Corol Roc	l Grayish while la while	Very weak to weak	Weakly to moderately strong comented, binbly factured	5.58			14 7		<u>}</u>		<u> </u>			
7	1]	strong comented, highly troctured. Disintegrated into well graded sand and grades under hommer.	2000 2000 2000 2000 2000 2000 2000 200	P-6						\geq		80	
a	-8.30	7.90	6.40					grovels under hommer blows.		P=7		6 5		-		<u>, </u>			
9		-			Corol Roc	Gravish while	Meak to	Moderately fractured. Occassionally with		P-8-			7-		5.80	JWS/1	<u></u>	82	
				XX			strong	well groded sond seams.	8.97	ř=9- C 6	<u>50/17</u>	4010	/}		3000	211.377		-	
10	-10.72	10.32	2.42	XX	ļ					с <u>о</u> Р=10,	50/15	50/15		<u> </u>	5080	J#571	SCN		
<u>11</u>]	:			- END	of driling			10.02					<u>}</u> -					
12	1																		
<u>:13</u>	<u> </u> .																		-
14			{											[
													ł						
<u>15</u>	1.		• •	r.											•				
18]]] .	1							<u> </u>	
17	1																		
18				(÷	Į									l					· ·
19				[[~			 -
	ļ`									:	1		1	}	-			<u>├</u>	 _
20	1													<u> </u>	╌┝╴╸┥		<u> </u>	┣	<u> </u>
21	ŀ										1			 - -					 '
22	1																		
23	1		1	1		l					1							1	
24	1.		:	1										[T	[1
25]													†			t		-{
	1.]] .	1			1				}			t	<u>}</u>	
26	1													<u> </u>			+	 -	┨
27]: ;		l		ļ					1							l	L	`
28	1	-									1			Į					
29	l.	:	ľ							{				[T	–	1
l ···	1:	4 				[:		· ·		{	1			<u>}</u>			t	<u>├</u>	
30					· .						[+		-
31	Ľ		<u> </u>	L	<u> </u>	<u> </u>		<u></u>			<u> </u>	Ц							

Figure 1.8 Drilling Log of SDH 2

Hole Number SDH-J Elevation DL +2.2 m. Date Water Table CL -1.5 m. Driller			OTARY			Ρ.	A	n				
Water Table Q1.5 m. Drille	**************************************	310.00				C : (staniara i Soring	reastro	ition I	lest		
	p con	(SHAH)			~							Т.
	T			Q		ard i	Penetra	ation	Tes	}		
Remark Com a com	Samp	ling					Recove		Sec. 2.	-		
cele in m wation in m epth in m legend Legend colour Colour Consistency consistency	मन	ä	9 g		s Per jūen		10 50 N	- V		9. 0 51		
Scale in m Elevation in m Depth in m Legend Type of Soil Type of Soil Relative Density or Consistency ieneral Remarke	Depth In p	Semple No.	N-Value Blows/30cm	8	8 6			الهوال وجود يرك مست	L CR			· :
2.20 0.00	00		28	8			20 40) 8	0 10	20%	: · _
1 2 2 2 2 2 2 2 2 2 2 2 2 2	1.00							50				
2 - Concrete creamy whitestrong sizes (Predominant of Concrete creamy sizes (Predomi	2.00						19		ł			
	2.50							50 50				
Corol Son&Greyish Wedium Net grooted sand with white dense to lot of corol groves	2.50 3.89 3.45 3.93 3.93 3.45 3.93 3.45 3.93 3.45 3.93 3.45 3.93 3.45 3.93 3.45 3.93 3.45 3.93 3.45 3.93 3.45 3.93 3.45 3.45 3.45 3.45 3.45 3.45 3.45 3.4	P≈t∸n	22	9 7	6							
rock fragments. Coccessionally with		6-7 P-2 1	33	9 1	6 8			50	• -			- 4 L
	386	C-8 P-3 1	14	1 3	7			H2				
6 between 1.70m to 1.80m		C-9 P-4	3.	2 1	0		f - f	- - -		~ - -		
7 7 6 6 7 7 7 7 7 7 7 7 7 7 7 7 7		P-3	9	5 2	2	7		45]	
8 well graded sond and grades under hommer				0 1		Ħ	1 3	+	<u></u>			
9 Wors		P-6				Ê	╞╼╼╅	\leq		89	ہے۔ انسانیہ	
-7.30 9.50 4.20 4.20 4.20 10		P-7-	45	25 /	<u>/ 13</u>	0			-1	≥●	:	
10	10.00 10.67 10.82	P-8 P-9	1/67		5 5	\leq			.			
-9.37 11.57 0.67 Court Part Caulta View wat Highly Borling	113	P=10	17	5 1	6	-1		†		1		
12 - END OF GRILING -	1						·}{·	-֠				
						}	┢╺┥	†				
							· ·	}				
15			{				┝╴╴┤					
16							· - -					
17		ļ						<u> </u>			- 	. .
16		[.									•	ľ
								T				
20						1		†				
						}	┢╴╸┥	+				
						}	┢╺┤	{				
22					ł		╌┟╴╼╶┨	+				
23			Į			}	┝╼┤					ļ
24						. 					-	
25											• •	
26								_ · [-	
27						1	1-1		~-		-	
			1					†				
28						}	╺╞╴╤╺┨	{				
29		[.:				}	╶┟╴╸┥					
30					Į						- 	l
31		L		Ш							-	ļ
		·						·				

Figure 1.9 Drilling Log of SDH 3

	<u></u>										
SS	Unit Weight Paraffin	g/cm ³	2.13	2.47	2.41	2. 48	1.53	2. 33	2.12	2. 26	2.47
Tetst on the Core Samples	Water Content in	bry Weight	18.0	10.4	17.5	29. 7	35. 5	26.2	13.4	12. 7	13.4
t Tetst on t	Strain	rai jure	3.95	4.15	3.70	1. 91	1.68	4.08	4.04	8. 78	3.93
and Unit Weight	Unconfined Compessive	otrengtn kgf/cm ²	66. 1	61.6	16.8	ۍ ي	14.0	19.4	57.5	109.4	35. 5
sion Test	S.P.T. N-value	Lower Level	34	17	41	17	>50 (12cm)	> 50 (15cm)	33	14	က
Compres	N-N N-V	Upper Level	18	34	×	41	>50 (18cm)	> 50 (12cm)	22	33	14
The Results of Unconfined Compression Test	Locality		8.79~9.00m depth	9.70~9.91m depth	3. 70~3. 95m depth	4.60~4.75m depth	8. 75~8. 97m depth	9.98~10.17m depth	3.98~4.00m depth	4.87~5.00m depth	5. 30~6. 00m depth
THC W			THOS	Do	SDH2	Do	Do	Do	SDH3	Do	Bo
Table 1.3	Sample		Loose coral rock	qo	qo	do	Massive coral rock	ф У	Loose coral rock	do	do
ı	Sample	NG.	C-1	C-2	C-3	C-4	C-5	9 	C-7	6-8 2	6-3 C-8

): A penetration advance at 50 blows by S.P.T.

 \cup

Massive coral rock (massive autochthonous coral) : The massive coral rock is the reef building coral which grows up in-situ too. But the massive coral rock is slightly more stronger than the above-said loose coral rock, because of the compaction by the load of upper sediments and the cementation resulting from the movement of calcareous matter by percolating water. The N-values of S.P.T. in the massive coral rock show a value above 50, and the core recoveries are higher than in the loose coral rock and sometimes reach 100 %. Based on the data of the previous and this investigations, the unconfined compressive strength on the core samples in the massive coral rock ranges from 14 to 210 kgf/cm², with an average of 90 kgf/cm². These values are slightly higher than those in the loose coral rock.

(4) Geotechnical Situation of the Foundation along the Proposed Seawall Alignments

The geological sections along the proposed seawall alignments and their cross sections are prepared on the basis of the reef pattern in Figure 1.4, the columnar sections in Figure 1.6 and the above-mentioned geological classification. The location of the geological section lines are shown in Figure 1.10 and the geological sections are shown in Figure 1.11.

a) The Gelogical Section A-A'

Based on the geological section A-A' along the proposed seawall alignment on the east coast, the foundation of the proposed seawall consists of the lagoon sediments in the northern side and the loose coral rock in the southern side. The lagoon sediments are distributed in the northern side from 75 m south of SDH 1 bore hole position, and mainly underlie the existing breakwater and occasionally intercalate thin fill material between both of them. While, the loose coral rock which forms the reef flat is extended in the southern side of the lagoon sediments. The loose coral rock underlies the existing breakwater and frequently includes an intercalated thin sandy sediment between both of them.

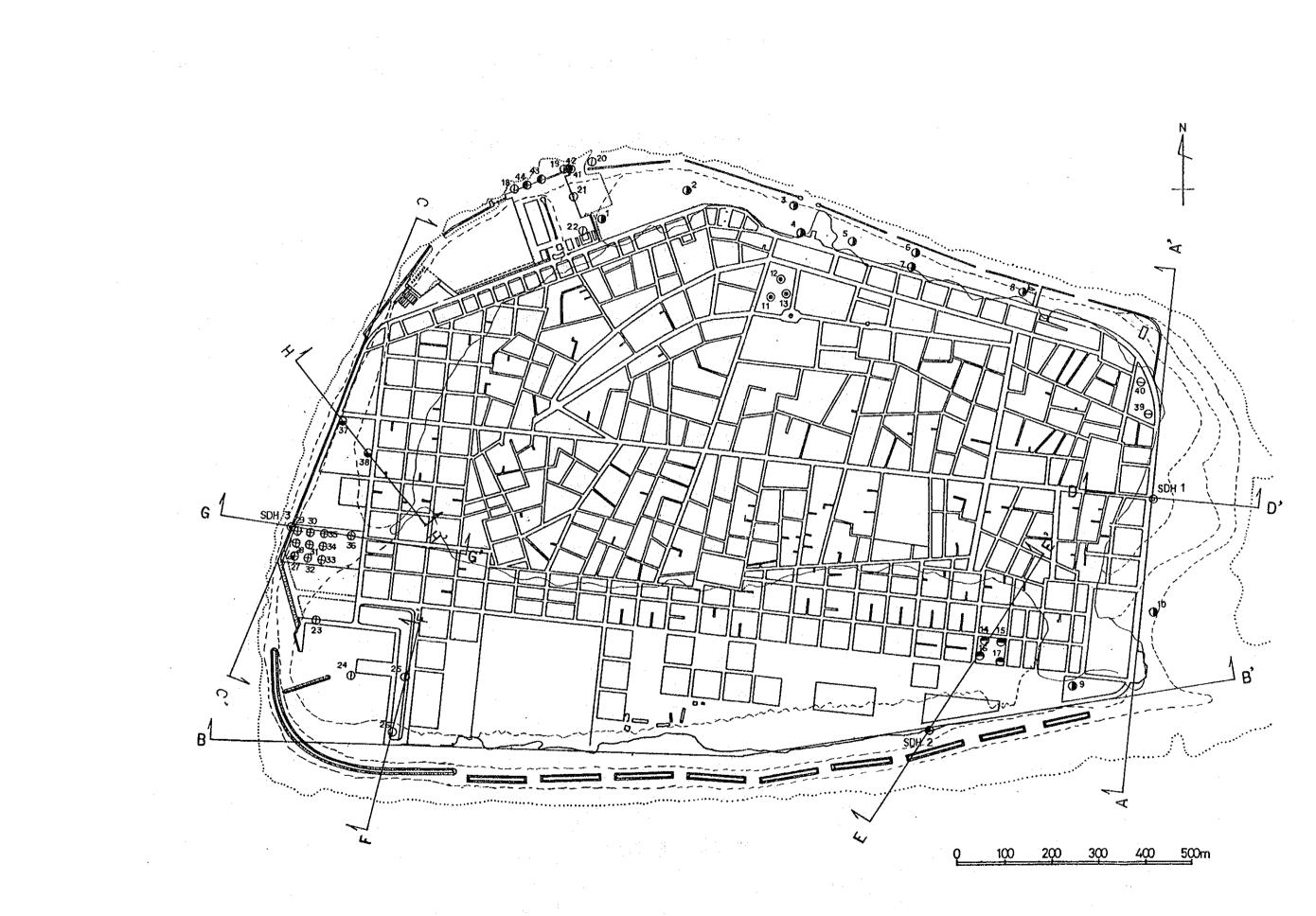
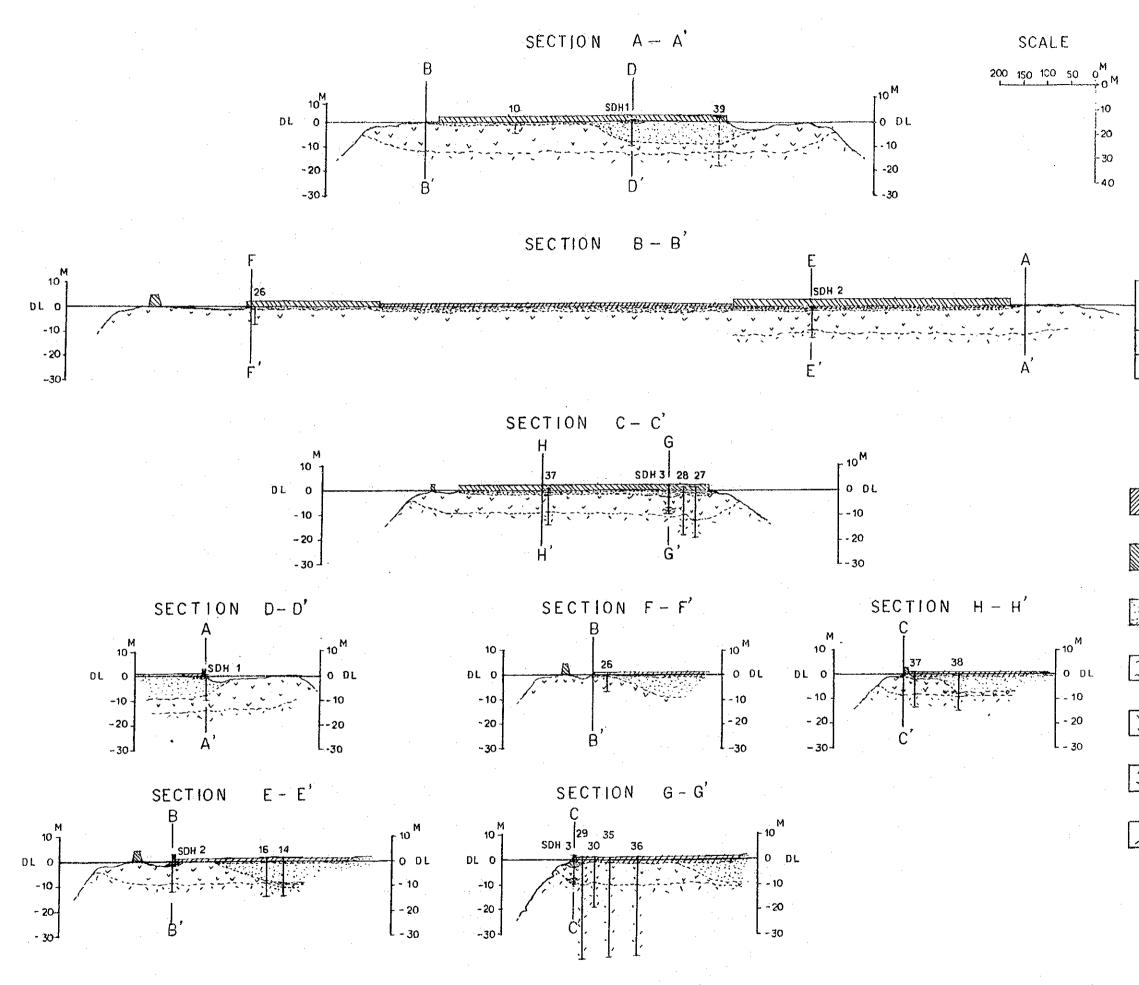
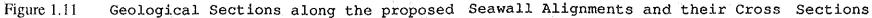


Figure 1.10 Location Map of Bore Holes drilled for Foundation Investigation and Geological Section Lines, Male'





- 10^M O DL -10 -20 -30

LEGEND

Fill material Existing breakwater illilla Lagoon sediments (coral sand & gravel) Lagoon sediments ~~~~ (coral silt) Loose coral rock ڒ؞ڒ (loose autochthonous coral) Massive coral rock (massive autochthonous coral) Geological boundary 12 Bore hole & consecutive No.

b) The Geological Section B-B'

Based on the geological section B-B' along the proposed seawall alignment on the south coast, the foundation of the proposed seawall is made up mainly of the loose coral rock which forms the reef flat. The loose coral rock underlies the existing breakwater in half of the section. SDH 2 bore hole intersected the fill material of about 1 m thick and the underlying sandy sediments of about 50 cm thick between the existing breakwater and the loose coral rock. Therefore, the fill material and the sandy sediment are intercalated between the existing breakwater and the loose coral rock, or cover on the loose coral rock. their thicknesses probably depend upon the surface shape (for example wave furrow) of the reef flat and the situation of reclamation.

c) The Geological Section C-C'

Based on the geological section C-C' along the proposed seawall alignment in the west coast, the foundation of the proposed seawall is composed mainly of the loose coral rock which forms the outer ridge. The loose coral rock underlies the existing breakwater and frequently includes an intercalated sandy sediment between both of them. SDH 3 bore hole intersected the sandy sediment of 2.6 m thick between the existing breakwater concrete body and the loose coral rock. The thickness of the sandy sediment at geological section H-H' is estimated to be from 1.5 m to 2.0 m. Such a thick sandy sediment may be caused by the sedimentation at deep wave furrow on the outer ridge.

(5) Geotechnical Analysis

a) The Lagoon Sediments and the Loose Coral Rock

The foundation of the proposed seawall consists mainly of the lagoon sediments (in the north side of the east coast), the loose coral rock which forms the reef flat (in the south side of the east coast and the south coast) and the loose coral rock which forms the outer ridge (on the west coast).

The physical properties of the lagoon sediments and the loose coral rock are summarized in Table 1.4.

The ultimate bearing capacity of the lagoon sediments in the Table 1.4 was taken on the basis of the previous plate load test for the Kalaafanu Primary School

Project. Also, the ultimate bearing capacity of the loose coral rock in Table 1.4 was taken on the basis of the previous plate load test for the Indira Gandhi Memorial Hospital Project. Both plate load tests are performed on the lagoon sediments and on the loose coral rock respectively.

 Table 1.4
 The Physical Properties of the Lagoon Sediments and the Loose Coral Rock

Name of Fundation Rock	Description	N-value (S.P.T)	Unconfined Compressive Strength kgf/cm ²	Ultimate Bearing Capacity t/m ²
Lagoon Sediments	Coral sand and gravel, median grain size : 0.4~0.6 m/m	3 ~ 33	-	16 ~ 22
Loose Coral Rock	Leef building coral which grow up in- situ, with many pores and cavities	2 ~ 50	5 ~ 135 (average 70) The test was performed on core samples only	45 ~ 60

b) Damage of Coral Reef on the West Coast

The Proposed seawall alignment on the west coast is planned on the outer ridge of the coral reef, and it is not the same as on the reef flat or on the lagoon sediments in case of the east and the south coast. The alignment is very near from the outer slope of coral reef and its distance ranges from 7 m to 30 m.

It is estimated that the coral reef on the west coast is probably damaged by wave erosion and surface erosion during the period of sea level change, because the submarine notches are found on the outer slope at 5 m to 10 m depth from D.L.

SDH 3 bore hole intersected the sandy silt sediment of 1.4 m thick at 7.3 m to 8.7 m depth from D.L. The sandy silt sediment which underlies the loose coral rock having 45 in N-value (S.P.T.), shows a penetration advance of 67 cm at one blow by S.P.T. Therefore, the sandy silt sediment may be deposits in the cave.

1.5 Material Test

(1) Sample

Five coarse aggregate samples (E1~E5) which were taken from the concrete body of the existing breakwaters, were coated with paraffin on samples wrapped in transparent vinyl sheet, because to keep its natural condition. Ten dredged coral lump samples (R-1~R-10) were collected at the pile area of the domestic harbor. The unconfined compression test and the unit weight test concerning the above-mentioned fifteen samples were carried out in accordance with JIS and test standards based thereon, at the laboratory in Singapore. The results of the said tests are shown in Table 1.5.

Seven dredged coral sand samples for fine aggregate (S-1~S-7), were collected at the same pile area. Three river sand samples for fine aggregate (S-8~S~10), imported from Lumut Port, Malaysia, were collected at the pile area of the tetrapod plant. The grading analysis and the specific gravity test for the above-mentioned ten samples were conducted in accordance with the test standards based on JIS, at the same laboratory. The results of the said tests are shown in Table 1.6.

(2) The Coral Coarse Aggregate Samples Taken from the Existing Breakwaters.

As compared with JIS A 5005 for "crushed stone for concrete", the values of unit weight concerning the coral coarse aggregate samples range from 1.1 to 2.2, and all those values are lower than the specific gravity above 2.5 provided by the said JIS standard. The values of water content concerning the said samples range from 13 to 32 % in natural condition, but all those values are higher than the absorption value below 3 % prescribed by the said JIS standard.

The results of the unconfined compression test range from 6 to 56 kgf/cm² in unconfined compressive strength. All these' values are classified as "soft rock" (below 200 kgf/cm² in unconfined compressive strength). However, coarse aggregate for concrete should generally be "hard rock" (above 600 kgf/cm² in unconfined compressive strength). Therefore, because of "soft rock", lower unit weight and higher adsorption, all the said coral coarse aggregate samples taken from the existing breakwater are not suitable for structural coarse aggregates, but the coral coarse aggregate are sufficiently possible to be used as packing for the proposed seawall.

The Results of Unconfined Compression Test and Unit Weight Test on the Coarse Aggregate Samples from the Existing Breakwaters and the Dredged Coral Samples Table 1.5

Sample No.		Sample	Locality	Unconfined Compressive Strength kgf/cm ²	Strain at Failure	Water Content in Percent of Dry Weight	Unit Weight Paraffin Method g/cm ³
г Ш		Bee hive-like coral	80m west from SDH2 position	6.4	2.50	17.3	1.08
Е- 2	Coarse aggregate	Massive porous coral	do	34. 7	3.80	12.6	2.19
ы В С	the existing breakwater	Massive coral	SDH3, 0.88 \sim 1.00m depth in the existing breakwater body	56.1	5.00	31.9	1. 93
E- 4		Bee hive-like coral	SDH3. 2.28 \sim 2.50m depth in the existing breakwater body	20.1	2.16	21.6	1.81
E- 5		Massive porous coral	10m south from SDH3 position	48. 2	3.03	19.4	1.93
R- 1		Bee hive-like coral	Taken by the domestic harbour dredging	9.5	1.11	1.9	1.85
R- 2	Dreaged coral	Massive coral	qo	74.5	3.42	0.6	1.46
R- 3		Bar-like coral	qo	135.5	4.93	1.2	2. 25
R- 4	SCI eening	qo	đo	82.0	3.09	6.0	2.39
R- 5	· · · · · · · · · · · · · · · · · · ·	Massive porous coral	qo	31.2	3.62	6.5	1.98
R- 6		Bee hive-like coral	do	13.8	2.83	7.6	1.66
R- 7	coral	Massive coral	do	46.6	3. 79	0.6	1.74
R- 8	(40~100m/m	Bar-like coral	do	48.4	2.22	1.6	2.18
R- 9	after	qo	d!0	57.6	3.13	1.8	2. 35
R-10	SULEENING	Massive porous coral	d.o	47.3	4.42	5.0	2.10

(3) The Dredged Coral Lump Samples for Coarse Aggregate

As compared with JIS A 5005 for "crushed stone for concrete", the values of unit weight concerning the dredged coral lump samples range from 1.5 to 2.4, and all those values are lower than the specific gravity above 2.5 prescribed in the said JIS standard. The value of water content among the said samples are higher than the absorption value below 3 % provided by the said JIS standard.

The results of the unconfined compression test range from 10 kgf/cm² to 136 kgf/cm². All these values are classified as "soft rock" (below 200 kgf/cm² in unconfined compressive strength). However "hard rock" (above 600 kgf/cm² in unconfined compressive strength) is more suitable for coarse aggregate for concrete. So, by reason of "soft rock" and lower unit weight, all the said dredged coral lump samples are not suitable for structural coarse aggregate. But, these dredged coral lump samples are sufficiently possible to be used as packing for the proposed seawall.

(4) The Dredged Coral Sand Samples for Fine Aggregate.

Median grain size :

As compared with JIS A 5004 for "manufactured sand for concrete", the four values of specific gravity among the dredged coral sand samples are lower in comparison with the specific gravity above 2.5 prescribed by the said JIS standard. While, all the values of adsorption regarding the said samples are lower than the absorption value below 3 % provided by the said JIS standard.

Compared with the river sand sample from Malaysia, the average values of specific gravity, absorption, median grain size and coefficient of uniformity concerning the dredged coral sand sample are as follows.

Specific gravity : Coral sand (2.50) is lower than the river sand (2.61)

Absorption : The coral sand (0.3 %) is the same as the river sand (0.3 %)

The coral sand (0.71 m/m) is smaller than the river sand (0.86 m/m)

Coefficient of uniformity: The coral sand (4.1) is higher than the river sand (2.8). It means that the uniformity of river sand is higher than that of coral sand, because of sorting by river water flow. The Results of Grading Analysis and Specific Gravity Test on the Dredged Coral Sand Table 1.6

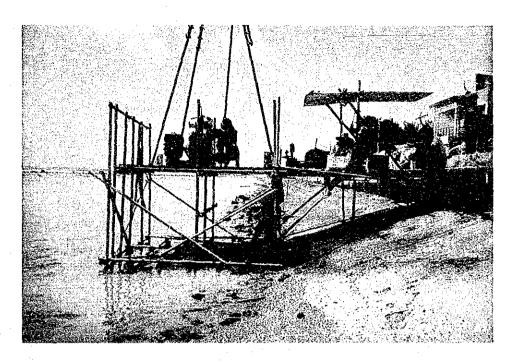
				Grading Analysis	S		
mple	Sample	Incality				Sperific	Absorption
No.			Median	Coefficient	Coefficient	Gravi ty	2
			size m/m	Uniformity	Curvature	6/ CIII	2
-1-5	Dredged coral sand (before screening)	taken by the domestic harbour dredging	0.64	4.3	0.93	2.51	0.3
S- 2	do	qo	0.66	4.1	0.98	<u>2.51</u>	0.3
S- 3	do	qo	0.54	3.9	0. 70	2.55	0, 3
S- 4	do	op	0.85	4.6	1.10	2. 49	0.5
S- 5	Dredged coral sand (under 5m/m in size)	do	0. 78	4.1	0, 97	2. 49	0.2
S- 6	do	qo	0.76	4.1	0, 94	2.47	0.5
S- 7	do	op	0.73	3.9	0.95	2.49	0.3
	Average	lge	0.71	4.1	0.94	2.50	0.3
S- 8	River sand (under 5m/m in size)	imported from Lumut Port, Malaysia	0.89	2.6	0.95	2.60	0.3
S- 9	do	đo	0.90	3.1	0.85	2.61	0.3
S-10	do	do	0.80	2.6	1.04	2.61	0.2
	Average	ıge	0.86	2.8	0.95	2.61	0.3
Note	 e : Median grain size(m/m): 50% grain 10% grain size(D₁₀), 30% grain si 60% grain size(D₆₀) 	(m/m); 50% grain size(Dso)), 30% grain size(Dso),		Coefficient Coefficient	of	uniformity: $D_{\varepsilon_0}/D_{1,0}^{\tau_0} \times D_{\varepsilon_0}$ curvature : $(D_{s_0})^2/D_{1,0} \times D_{\varepsilon_0}$	×Dډه

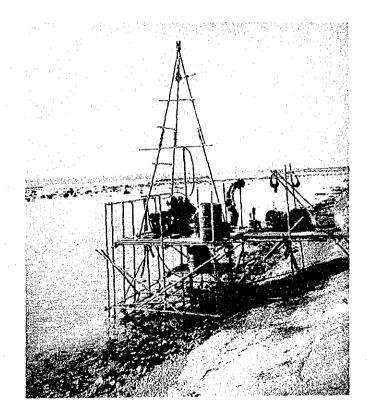
Because the coral sand has a softer grain and lower specific gravity than river sand from Malaysia, the coral sand is not so suitable for fine aggregate for concrete in comparison with the river sand from Malaysia.

APPENDIX

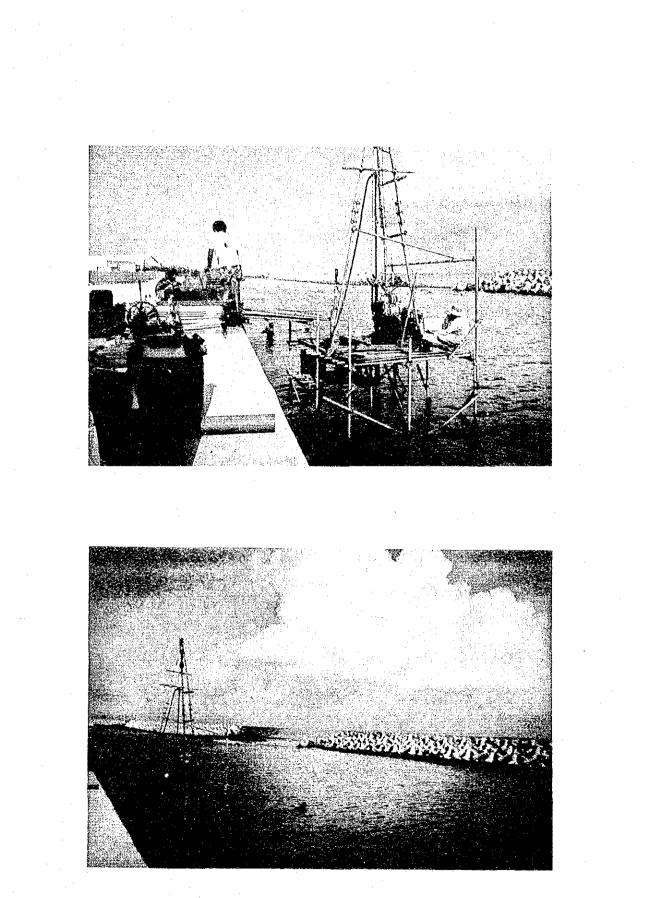
(SOIL DATA)

- 1. Photograph of Field Investigation
- 2. Photograph of Rock Cores

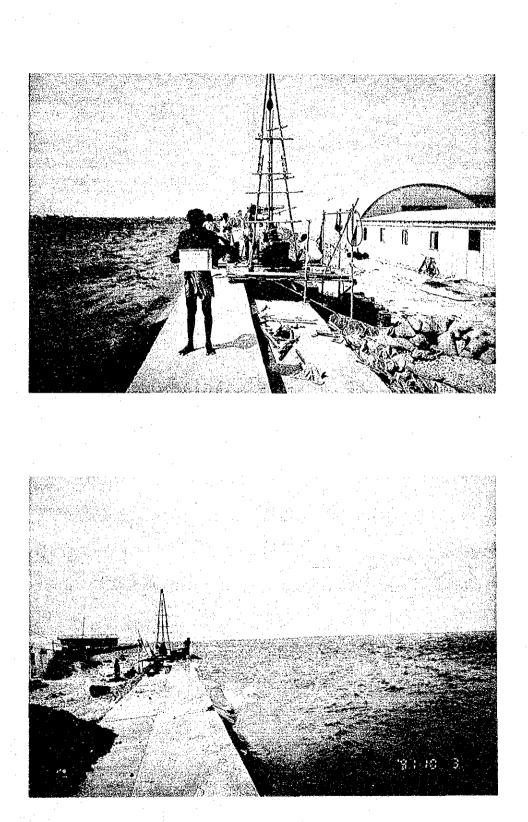




Set-up Drilling Machine at Borehole Location SDH-1



Set-up Drilling Machine at Borehole Location SDH-2



Set-up Drilling Machine at Borehole Location SDH-3