(3) Results of 3rd Stage Evaluation

 Adjustment with Power Development Plan (including Power Generation Plan)

The term of the 5-year Master Plan for power plant rehabilitation is set to be 1994 to 1998. The power development plan and power generation plan up to 2005 are shown in Tables 4-1 -- 4-5, Table 6-1-15 and Fig. 6-1-8. As is clearly indicated in these tables, it is estimated that the existing thermal power plants need to be operated at the annual capacity factor of 70% on an average.

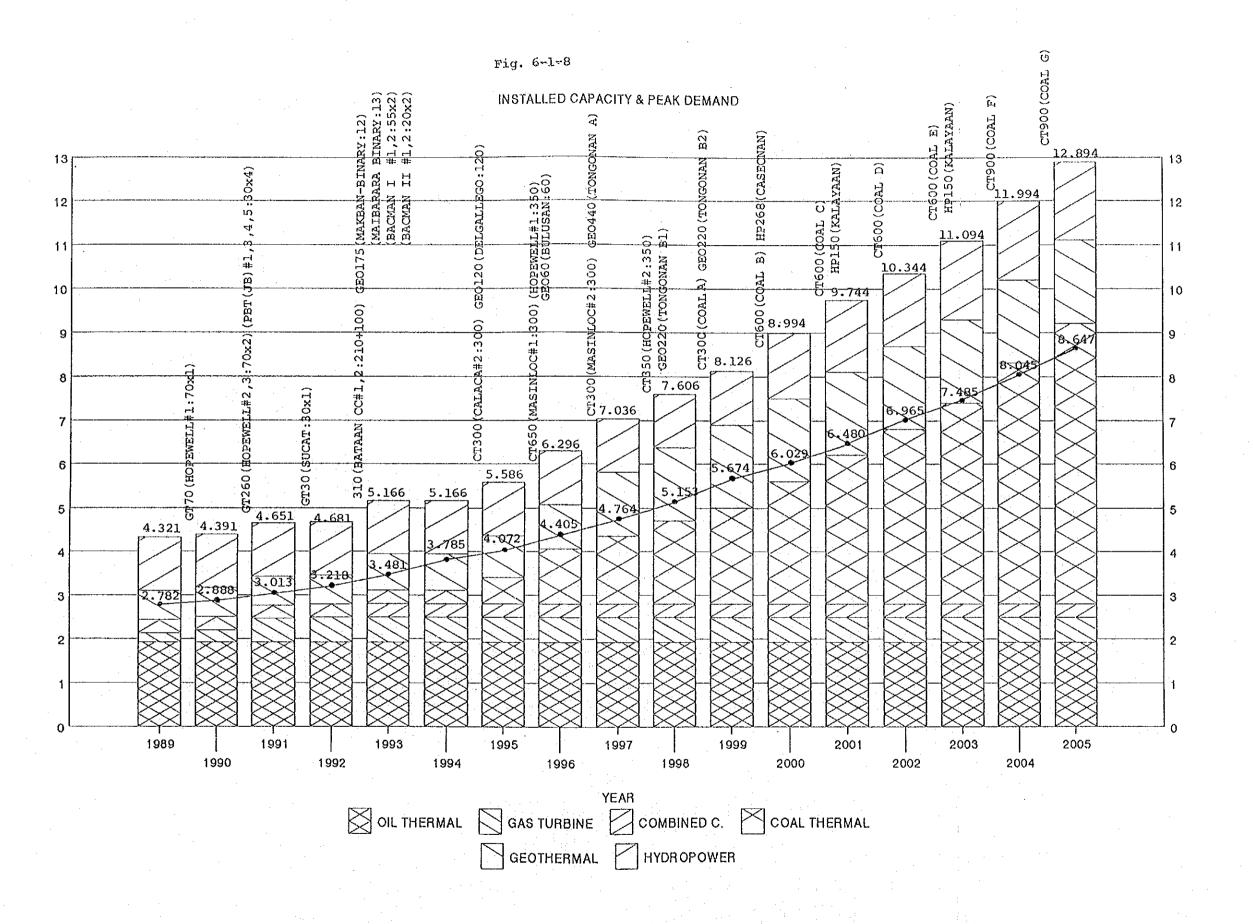
b. Adjustment with Maintenance Plan

The implementation period for rehabilitation of Sucat No. 2 & No. 3 Units is scheduled as shown in Fig. 6-1-5. Therefore, in reference to the 2nd stage evaluation results, the rehabilitation schedule was arranged for the other power plant units.

The periodic overhaul for each power plant should be scheduled, in principle, for once a year. Also, periodic overhaul should be coordinated to minimize the overlapping periods between the power plants and, in addition, not to increase shutdown capacity during the overlapping period. The final rehabilitation work schedule was drawn up as shown in Fig. 6-1-5 after discussions with NAPOCOR during the 2nd stage field investigation.

Tebie 6-1-15 POWER DEVELOPMENT AND PEAK LOAD IN LUZON GRID

75.00	§ (FORECAST	(MM)	2,732	2,888	**************************************	3,013			3,218		3,431					3,785	4,072		4,405			4,764	_	5,153		5,674		6,029		6,480		596'9		7,485		8,045		8,647	
-	00000	CAPACITY	(MMA)	4,321	4,391	-(:	4,651			4,681		5,166					5,166	5,586		6,296			7,036	. :	7,606		8,126		8,994	-	9.744		10,344		11.092		11,994		12,894	
TOTAL	7	NA PLANT	(MM)		8		260			8		485	٠.				Ó	8		012	<u> </u>	<u>:</u>	740		570		220		898		750		88		750		8		006	-
	10.00	CAPACITY	(BARA)	1,226	1,226		1,226			1,226		1,226					1,226	1,226	-	1,226			1,226		1,226		1,226		1,494		1,644		1,844		1,794		1,794		1,794	
OEWOOD OUT	Pro Carolina	NATA ALVA	(MMV)												<u> </u>													•	588	(CASECNAN)	55	(KALAYAAN)			8	(KALAYAAN)			<u> </u>	-
	MICTALIER	CAPACITY	(AVVV)	098	099	-	883		-	089		835	7Y: 12)	1AFY: 13)	: 55 x 2)	2: 20 × 2)	835	956	3EO: 120)	1,015	8		1,455	4403	1,675		1,895		1,885		1,895		1,895		1,895		1,695		1,895	
GEO TLEBALA	NEW DISTRICT	ANGEL ANGEL	(BANA)									175	(MAKBAN-BINARY: 12)	(MAJBARARA BINARY: 13)	(BACMAN!#1,2:55x2)	(BACMAN II #1, 2: 20 x 2)		120	DEL GALLEGO GEO: 120)	8	(BULLISAN GEO: 60)		440	TONGONAN A: 440)	220	(TONGONAN B1: 220)	220	(TONGONAN B2: 220)												
	ther Alven	CAPACITY	(MM)	300	300		300	-		8		900					8	8		1250		350)	1,550	300	006'1	350	2,200		2,800		3,400		4,000		4,800		5,500		6,400	
COAL THERMAI	NEW DI ANT		(MM)			-::												006	CALACA #2:300	650	(MASINEOCI#11:300)	(HOPEWELL:#1: 350)	300	(MASINLOC:#2:300)	350	HOPEWELL #2: 350	300	COAL A: 300)	909	COAL B: 600	009	COAL C: 600)	009	COAL D: 600)	000	COM E: 600)	006	COAL F: 800	006	(COALG: 900)
	METALLED	CAPACITY	(MW)	210	280	70 X 1)	540	3:70×2)	5:30×4)	210		220			*:	7 .	270	220		210			0.25	· ₹	570		920		570		220	-	570		220		025		570	Τ.
FINESCIT SAS	NEW OF ANT		(MM)		<u>Š</u>	(HOPEWELL #1: 70	280 280	(HOPEWELL #2, 3:	(PBT(JB) #1,3,4,5	8	(SUCAT:30x1)							- 41															•							
ACIE.	MICTALIED	CAPACITY	(MW)	O	Ö	<u>~</u>	0			O		310	2:210+100)				310	9.0		310	-		310		310		310		310		310		310		310		310		310	
COMBINED CYCLE	NEW DI ANT	3	(MM)	-						-		310	(BATAAN CC #1, 2:210 + 100)					*****						TION				7	~ 											
	INCTALLED	CAPACITY	(MW)	1,925	1,925		1,925			1,925		1,925	~				1,925	1,925		1,925	·.		1,925	- LEYTE INTERCONNECTION	1,925		1.925		1 925		1,925		1,925		1,925		1,925		1,925	
ON THERMAN	NEW DI ANT		(MM)		•					-			• • •											(LUZON - LEYTE																
				1989	98		1981			1982		1988				7	282 282	986		1998			1997		1998		88		2008		200		800		802 208		2007		5002	



ANNEX 1. PLANT OPERATIONAL DATA

Bataan Thermal Power Plant
Manila Thermal Power Plant
Sucat Thermal Power Plant
Malaya Thermal Power Plant
Batangas Coal Fired Thermal Power Plant
Bataan Gasturbine Power Plant
Malaya Gasturbine Power Plant

ANNEX 1. PLANT OPERATIONAL DATA

BATAAN THERMAL POWER PLANT UNIT NO. 1

	ITEMS		1986	1987	1988	1989	1990
7.	RATED CAPACITY	(MM)	75	75	7.5	75	75
2	DEPENDABLE CAPACITY	(MM)	69	89	69	68	99
т •	AVERAGE LOAD	(MM)	62.19	66.53	65.42	65.86	62.86
4.	GROSS GENERATION	(MWH)	417,898.18	475,291.6	429,782.9	521,140.8	454,038.3
ń	OPERATING HOURS	(Hr)	6,872.03	7,144.07	6,569.16	7,911.71	7,223.40
9	TOTAL OPERATING HOURS SINCE INITIAL SYNCHRO.	(Hr)	91,923.66	99,067.73	105,636.89	113,548.60	120,772.00
7.	TOTAL OUTAGE HOURS	(Hr)	1,887.97	1,615.93	2,214.84	848.29	1,536.60
	(1) FORCED OUTAGE	(Hr)	302.03	176.63	687.43	261.97	237.77
	(2) MAINTENANCE OUTAGE	(Hr)	689.18	537.00	543.84	247.18	111.40
	(3) PLANNED OUTAGE	(Hr)	799.60	882.47	966.03	305.63	1,120.30
	(4) ECONOMIC SHUTDOWN	(Hr)	88.71	0	0		41.00
٠	(5) OUTSIDE TROUBLE	(Hr)	8.45	19.83	17.54	33.51	26.13
∞	STATION USED POWER RATIO	(%)	07.9	6.27	5.84	5.66	6.18
o.	CAPACITY FACTOR	(%)	63.67	72.51	65.32	79.63	69.31
10.	AVAILABILITY FACTOR	(2)	79.40	81.74	74.89	91.09	83.18
11.	HEAT RATE (GROSS)	(BTU/KWH)	9,861	9,799	9,93I	10,113	10,518
12.	THERMAL EFFICIENCY (GROSS)	(2)	34.61	34.83	34.37	33.73	32.45
13.	NUMBER OF STARTS (YEAR/TOTAL)	~	22/319	10/329	25/354	19/373	13/386

COMMISSIONING: MAY 1972

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BATAAN THERMAL POWER PLANT UNIT No. 2

			,				
, · ·	ITEMS		1986	1987	1988	1989	1990
r-i	RATED CAPACITY	(MM)	150	150	150	150	150
2	DEPENDABLE CAPACITY	(MM)	141	145	146	142	HE T
m	AVERAGE LOAD	(MM)	112.91	137.27	132.19	130.39	129.24
7	GROSS GENERATION	(MWH)	766,139	966,899	811,229	983,933	588,618
Ŋ,	OPERATING HOURS	(Hr)	7,248.14	6,958.38	6,211.78	7,503.60	4,554.62
vo C	TOTAL OPERATING HOURS SINCE INITIAL SYNCHRO.	(Hr)	66,077.23	73,035.61	79,247.39	86,750,99	91,305.61
7.	TOTAL OUTAGE HOURS	(Br)	1,511.86	1,801.62	2,572.22	1,256.40	4,205.38
	(1) FORCED OUTAGE	(Hr)	164.71	292.61	779.41	452.63	2,508.61
	(2) MAINTENANCE OUTAGE	(Hr.)	169.86	447.13	730.21	268:45	84.22
	(3) PLANNED OUTAGE	(Hr)	730.35	986.73	1,062.60	300.85	1,552.83
	(4) ECONOMIC SHUTDOWN	(Hr.)	405.18	61.06	0	209.20	59.72
	(5) OUTSIDE TROUBLE	(Hr)	41.78	14.09	: O	25.27	Ó
œ	STATION USED POWER RATIO	(%)	φ. φ	5.83	6.20	6.47	6.67
<u>ი</u>	CAPACITY FACTOR	(2)	58,59	73.72	61.57	75.10	44.80
10.	AVAILABILITY FACTOR	(%)	82.91	80.28	70.52	88.79	52.68
11.	HEAT RATE (GROSS)	(BTU/KWH)	9,464	9,485	9,532	9,702	9,868
12.	THERMAL EFFICIENCY (GROSS)	(%)	36.06	35.98	35.81	35.18	34.20
13.	NUMBER OF STARTS (YEAR/TOTAL)		24/293	15/308	17/325	24/349	24/373

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MANILA THERMAL POWER PLANT UNIT NO. 1

į		ITEMS		1986	1987	1988	1989	1990
	H.	RATED CAPACITY	(MM)	100	100	100	100	100
	2	DEPENDABLE CAPACITY	(MM)	56	96	86	. 26	ଷ ପ
	m	AVERAGE LOAD	(MM)	58	80	71.16	71.45	86.45
•	4	GROSS GENERATION	(MWH)	393,095	590,842	564,729	508,951	663,660
	۲,	OPERATING HOURS	(Hr)	6,739.85	7,266.46	8,092.44	7,122.75	7,676.89
	9.	TOTAL OPERATING HOURS SINCE INITIAL SYNCHRO.	(Hr)	170,346.75	177,613.21	185,705.65	192,828.40	200,505.29
	7.	TOTAL OUTAGE HOURS	(Hr)	2,020.15	1,493.54	691.56	1,637.25	1,083.11
	÷	(1) FORCED OUTAGE	(Hr)	447.43	298.31	30.47	146,98	114.94
	٠.	(2) MAINTENANCE OUTAGE	(Hr.)	12.70	0	413.70	0	59.78
	:	(3) PLANNED OUTAGE	(Hr)	1,293.85	942.10	O	1,414.47	837.50
		(4) ECONOMIC SHUTDOWN	(Br)	259.50	238.93	202.83	75.32	0
		(5) OUTSIDE TROUBLE	(Hr)	6.67	14.20	44.56	0.48	70.89
	ω	STATION USED POWER RATIO	(%)	8.26	6.55	7.00	6.91	5.75
	o	CAPACITY FACTOR	(4)	44.91	67.45	64.29	58.10	75.76
	10.	AVAILABILITY FACTOR	(2)	80.24	86.09	76.96	82.18	88.44
	11.	HEAT RATE (GROSS)	(BTU/KWH)	10,361	9,196	10,101	10,212	7964
	12.	THERMAL EFFICIENCY (GROSS)	(%)	32.94	37.11	33.8	33.4	34.2
	13.	NUMBER OF STARTS (YEAR/TOTAL)	I.)	14/260	8/268	12/280	11/291	8/299

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MANILA THERMAL POWER PLANT UNIT No. 2

						-		
		ITEMS		1986	1987	1988	1989	1990
	rd	RATED CAPACITY	(MM)	100	100	100	100	001
		DEPENDABLE CAPACITY	(MM)	68	T6	66	97	26
	ฑ์	AVERAGE LOAD	(MM)	58	7.7	71.28	75.10	86.92
	,	GROSS GENERATION	(MWH)	366.265	592,334	569,693	483,076	714,216
	5.	OPERATING HOURS	(Hr)	6,299.61	7,859.97	7,940.61	6,483.63	8,217.18
e.	9	TOTAL OPERATING HOURS SINCE INITIAL SYNCHRO.	(Hr)	155,434.26	163,294.23	171,234.84	177,718.47	185,935.65
1 =	7.	TOTAL OUTAGE HOURS	(Hr)	2,460.39	900.03	843.39	2,276.37	542.82
٠.		(1) FORCED OUTAGE	(Hr)	328.66	218.37	0	227.23	79.71
	•	(2) MAINTENANCE OUTAGE	(Hr)	0	385.49	607.95	157.95	232.35
		(3) PLANNED OUTAGE	(Hr)	1,298.30	288.00	0	1,757.25	0
		(4) ECONOMIC SHUTDOWN	(Hr)	833.43	° o	224.19	112.33	59.27
	•	(5) OUTSIDE TROUBLE	(Hr)	0	8.17	11.25	21.61	171.49
	ώ	STATION USED POWER RATIO	(%)	7.74	6.25	6.54	6.26	5.88
	σ,	CAPACITY FACTOR	(2)	41.81	67.62	64.86	55.15	81.53
	10.	AVAILABILITY FACTOR	(%)	83.07	88.04	93.08	75.54	96.44
	11.	HEAT RATE (GROSS)	(BTU/KWH)	10,243	10,113	10,085	060.01	9,021
	12.	THERMAL EFFICIENCY (GROSS)	(%)	33.32	33.75	33.8	33.8	34.4
·	13.	NUMBER OF STARTS (YEAR/TOTAL)		10/247	8/255	10/265	15/280	12/292

	टामचा		1980	T98/	1988	1989	O & & T
•	RATED CAPACITY	(MM)	150	150	150	150	150
2.	DEPENDABLE CAPACITY	(MM)	100	თ თ	86	130	150
m	AVERAGE LOAD	(MM)	60.38	74.10	7.1	79	135
:	GROSS GENERATION	(MWH)	504,960	624,540	395,290	356,690	1,044,680
ς.	OPERATING HOURS	(Hr)	8,318.60	8,427.46	5,403.63	4,540.66	7,735.15
ú	TOTAL OPERATING HOURS SINCE INITIAL SYNCHRO.	(Hr)	123,632.78	132,060.24	137,463.87	142,004.53	149,739.68
	TOTAL OUTAGE HOURS	(Hr)	441.40	332.54	3,380.37	4,219.34	1,024.85
	(1) FORCED OUTAGE	(Hr)	78.65	7.35	504.28	0	68.27
	(2) MAINTENANCE OUTAGE	(Hr)	0	215.92	717.34	0	677.93
	(3) PLANNED OUTAGE	(Hr)	0	0	2,002.95	4,018.83	266.05
	(4) ECONOMIC SHUTDOWN	(Hr)	241.26	109.27	92.50	200.51	0
	(5) OUTSIDE TROUBLE	(Hr)	121.49	0	63.30	o	12.60
œ,	STATION USED POWER RATIO	(z)	10.02	8.38	10.13	8.95	5.28
თ .	CAPACITY FACTOR	(%)	38.48	47.53	30.00	27.15	79.62
10.	AVAILABILITY FACTOR	(%)	98.86	97.45	64.98	54.12	88.43
11.	HEAT RATE (GROSS)	(BTU/KWH)	11,007	10,720	11,269	10,825	9,871
12.	THERMAL EFFICIENCY (GROSS)	(%)	31.01	31.84	30.29	31.53	34.58
13.	NUMBER OF STARTS (YEAR/TOTAL)	G	10/330	6/336	7/343	9/352	21/373

SUCAT THERMAL POWER PLANT UNIT No. 1

PLANT OPERATIONAL DATA

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SUCAT THERMAL POWER PLANT UNIT No. 2

	ITEMS		1986	1987	1988	1989	1990
ਜ਼	RATED CAPACITY	(MM)	200	200	200	200	200
2.	DEPENDABLE CAPACITY	(MM)	160	151	145	174	156
m	AVERAGE LOAD	(MM)	125.07	134.59	123	139.0	146.0
4	GROSS GENERATION	(MWH)	124,530	949,750	746,060	703,650	685,690
Ŋ		(Hr)	995.71	7,086.50	6,032.84	5,048.25	4,709,74
٥	IOIAL OPERATING HOURS SINCE INITIAL SYNCHRO.	(Hr)	99,069.22	106,155.72	112,188.56	117,236.81	121,946.55
7.	TOTAL OUTAGE HOURS	(Hr)	7,764.29	1,673.50	2,751.16	3,711.75	4,050.26
.*	(1) FORCED OUTAGE	(Hr)	55.64	383.34	712.60	9.50	628.78
	(2) MAINTENANCE OUTAGE	(Hr)	2,280.37	1,108.84	56.27	161.60	178.45
	(3) PLANNED OUTAGE	(Hr)	5,265.23	0	1,416.00	1,096.30	0
	(4) ECONOMIC SHUIDOWN	(Hr)	1.63.05	126.47	474.61	419.10	63.60
	(5) OUTSIDE TROUBLE	(Hr)	ő	54.85	91.68	2,025.25	3,179.43
·	STATION USED POWER RATIO	(2)	9.83	4.82	5.05	4.09	67.4
9	CAPACITY FACTOR	(%)	7.14	54.21	42.47	51.06	61.44
10.	AVAILABILITY FACTOR	(%)	13.29	82.06	78.85	79.34	85.53
11.	HEAT RATE (GROSS)	(BTU/KWH)	10,899	11,136	11,446	10,975	11,095
12.	THERMAL EFFICIENCY (GROSS)	(%)	31.31	30.65	29.83	31.10	30.76
н Э	NUMBER OF STARTS (YEAR/TOTAL)	^	6/330	12/342	8/350	13/363	11/374

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		ITEMS		1986	1987	1988	1989	1990
		RATED CAPACITY	(MW)	200	200	200	200	200
	2.	DEPENDABLE CAPACITY	(MM)	150	96	158	158	155
	ю	AVERAGE LOAD	(MM)	124.25	93.63	126.66	125	132
	4	GROSS GENERATION	(MWH)	653,490	439,520	629,420	933,350	740,930
	ķ	OPERATING HOURS	(Hr)	5,415.42	4,538.09	5,125.54	7,427.72	5,629.39
	. 9	TOTAL OPERATING HOURS SINCE INITIAL SYNCHRO.	(Hr)	95,706.42	100,244.51	105,370,05	112,797.77	118,427.16
	7.	TOTAL OUTAGE HOURS	(Hr)	3,344.58	4,221.91	3,658.46	1,332.28	3,130.61
		(1) FORCED OUTAGE	(Hr)	420.70	1,143.33	273.00	202.00	1,697.26
		(2) MAINTENANCE OUTAGE	(Hr)	3.40	632.20	301,61	338.61	1,397.92
		(3) PLANNED OUTAGE	(Hr)	0	1,752.00	2,763.97	0	0
		(4) ECONOMIC SHUTDOWN	(Hr.)	2,920.48	65.62	307.28	715.80	0
٠.		(5) OUTSIDE TROUBLE	(Hr)	0	628.76	12.60	75.87	35.43
	œ	STATION USED POWER RATIO	(%)	5.66	9.82	5.06	4.81	5.10
. ' '	9.	CAPACITY FACTOR	(%)	37.30	25.09	35.83	53.74	42.46
	10.	AVAILABILITY FACTOR	(%)	95.02	67.49	60.22	94.34	64.52
	11.	HEAT RATE (GROSS)	(BIU/KWH)	11,936	12,670	11,920	12,210	12,487
 	12.	THERMAL EFFICIENCY (GROSS) (2)	(%)	28.59	26.94	28.63	27.95	27.33
	133	NUMBER OF STARTS (YEAR/TOTAL)	G	14/302	9/311	15/326	14/340	15/355
1		COMMISSIONING: APR 1971						

PLANT OPERATIONAL DATA

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POWER	
THERMAL	
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		ITEMS		1986	1987	1988	1989	1990
	;-i	RATED CAPACITY	(MM)	300	300	300	300	300
	2.	DEPENDABLE CAPACITY	(MW)	228	240	221	240	272
	е. М	AVERAGE LOAD	(MM)	176.14	195.22	164.80	161	212
	4	GROSS GENERATION	(MWH)	815,090	1,181,120	629,770	581,210	300,920
	ι,		(Hr)	4,627.51	6,038.04	3,977.61	3,460.89	1,419.93
	ó	TOTAL OPERATING HOURS SINCE INITIAL SYNCHRO.	(Hr)	81,738.23	87,776.27	91,753.88	95,214.77	96,634.70
	7.	TOTAL OUTAGE HOURS	(Hr)	4,132.49	2,721.96	4,806.39	5,299.11	7,340.07
6 -		(1) FORCED OUTAGE	(Hr)	24.90	895.54	1,884.25	1,004.86	0
81		(2) MAINTENANCE OUTAGE	(Hr)	271.25	728.23	128.33	0	o
		(3) PLANNED OUTAGE	(Hr)	2,322.25	948.83	2,160.00	1,332.00	7,340.07
-		(4) ECONOMIC SHUTDOWN	(Hr)	1,514.09	60.48	478.58	849.92	0
		(5) OUTSIDE TROUBLE	(Hr)	0	88.88	155.23	2,112.33	Ö
	∞	STATION USED POWER RATIO	(%)	4.75	4.32	6.04	5.65	7.11
	o,	CAPACITY FACTOR	(%)	31.02	76.77	23.90	29.14	11.45
	10.	AVAILABILITY FACTOR	(%)	71.75	70.77	51.77	67.19	16.21
	H	HEAT RATE (GROSS)	(BTU/KWH)	11,846	11,328	12,090	12,918	10,490
	12.	THERMAL EFFICIENCY (GROSS)	(%)	28.81	30.13	28.23	26.42	32.54
	13.	NUMBER OF STARTS (YEAR/TOTAL)		7/310	16/326	17/343	6/349	11/360
F .		COMMISSIONING: JUN 1972	REHABILITATION:	N: OCT 1989 -	DEC 1990			

DATA
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MALAYA THERMAL POWER PLANT UNIT No. 1

,• ~	RATED CAPACITY	(MM)	300	300	300	300	300
2	DEPENDABLE CAPACITY	(MM)	234	300	594	299	285
m	AVERAGE LOAD	(MM)	187	245	251	250	268
. 4	GROSS GENERATION	(MWH)	1,132,042	538,224	1,884,324	1,567,670	2,106,026
'n	OPERATING HOURS	(Hr)	5,947.53	2,332.80	7,510.51	6,249.25	7,862.42
ý	TOTAL OPERATING HOURS SINCE INITIAL SYNCHRO.	(Hr)	72,999.54	75,332.34	82,842.85	89,092.10	96,954.52
7.	TOTAL OUTAGE HOURS	(Hr)	2,812.47	6,427.20	1,273.49	2,510.75	897.58
	(1) FORCED OUTAGE	(Hr)	242.95	14.85	166.76	2,003.70	655.56
4	(2) MAINTENANCE OUTAGE	(Hr)	831,75	1,043.30	140.61	372.27	231.37
	(3) PLANNED OUTAGE	(Hr)	1,296.00	5,369.05	923.20	0	0
	(4) ECONOMIC SHUIDOWN	(Hr)	197.37	0	42.92	0	10.65
	(5) OUTSIDE TROUBLE	(Hr)	244.40	0	0	134.78	0
œ	STATION USED POWER RATIO	(%)	3.92	2.71	2.94	2.86	3.00
on.	CAPACITY FACTOR	(2)	43.90	20.48	71.51	60.58	80.14
10.	AVAILABILITY FACTOR	(2)	74.04	25.05	85.82	72.64	68.68
린	HEAT RATE (GROSS)	(BTU/KWH)	10,658	699'6	016,6	10,132	10,556
12.	THERMAL EFFICIENCY (GROSS)	(%)	32.02	35.30	34.44	33.69	32.33
13.	NUMBER OF STARTS (YEAR/TOTAL)	Γ)	17/240	13/253	15/268	22/290	19/309

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MALAYA THERMAL POWER PLANT UNIT No. 2

1			-			: -	
	ITEMS		1986	1987	1988	1989	1990
i,	RATED CAPACITY	(WM)	350	350	350	350	350
6	DEPENDABLE CAPACITY	(MM)	285	326	344	336	324
ຕໍ	AVERAGE LOAD	(MM)	205	260	288	280	292
.4	GROSS GENERATION	(MWH)	1,118,128	2,028,998	2,121,673	2,209,309	2,197,688
5.	OPERATING HOURS	(Hr)	5,464.71	7,654.61	7,368.85	8,039.75	7,352.16
•	TOTAL OPERATING HOURS SINCE INITIAL SYNCHRO.	(Hr)	52,809.63	60,464.24	67,833.09	75,872.84	83,405.00
7.	TOTAL OUTAGE HOURS	(Hr)	3,295.29	1,105.39	1,415.15	720.25	1,227.74
	(1) FORCED OUTAGE	(Hr)	80.28	18.70	68.28	30.65	269.74
	(2) MAINTENANCE OUTAGE	(Hr)	594.22	742.49	201.94	56.15	495.70
·	(3) PLANNED OUTAGE	(Hr)	2,547.08	314.98	1,081.38	594.97	462.30
	(4) ECONOMIC SHUTDOWN	(Hr)	31.77	: o	52.73	0	O
	(S) OUTSIDE TROUBLE	(Hr)	41.94	29.22	10.82	38.48	0
φ	STATION USED POWER RATIO	(%)	5.01	3.67	3.58	3.44	3.44
တ	CAPACITY FACTOR	(%)	36.64	66.18	69.01	72.38	71.68
10.	AVAILABILITY FACTOR	(2)	62.91	89.46	84.48	90.53	85.99
11.	HEAT RATE (GROSS)	(BIU/KWH)	10,212	9,604	9,413	9,568	9,676
12.	THERMAL EFFICIENCY (GROSS)	(%)	33.42	35.54	36.26	35.67	35.27
13.	NUMBER OF STARTS (YEAR/IOTAL)	Т)	17/149	11/160	12/172	7/179	10/189
	COMMISSIONING: MAR 1979	REHABILITATION: JUL	: JUL 1986 -	JAN 1987			

		PLANT OPERATIONAL DATA	ATA		BATA	NGAS COAL FIRE	BATANGAS COAL FIRED THERMAL POWER PLANT	PLANT UNIT No. 1
		ITEMS		1986	1987	1988	1989	1990
	ત	RATED CAPACITY	(MW)	300	300	300	300	300
	2,	DEPENDABLE CAPACITY	(MW)	270	280	280	272	249
	พ	AVERAGE LOAD	(MM)	252.58	263.68	278.51	263.57	245.02
	4.	GROSS GENERATION	(MWH)	1,609,307	1,948,932	1,996,270	2,053,138	1,601,232
	ņ	OPERATING HOURS	(Hr)	6,371.47	7,391.40	7,167.72	7,789.65	6,535.07
·	9	TOTAL OPERATING HOURS SINCE INITIAL SYNCHRO.	(Hr)	14,417.04	21,808.44	28,976.16	36,765.81	43,300.88
	7.	TOTAL OUTAGE HOURS	(Hr)	2,388.53	1,368.6	1,616.28	970.35	2,212.93
6 -		(1) FORCED OUTAGE	(Hr)	158.78	154.54	241.86	577.08	420.08
- 84		(2) MAINTENANCE OUTAGE	(Br)	210.72	186.77	336.38	170.05	311.58
		(3) PLANNED OUTAGE	(Hr)	1,865.70	1,004.83	958.89	0	1,412.20
		(4) ECONOMIC SHUTDOWN	(Hr)	126.36	0	54.24	147.12	47.41
2.5		(5) OUTSIDE TROUBLE	(Hr)	26.97	22.46	24.91	76.10	21.66
	α	STATION USED POWER RATIO	(%)	5.16	5.17	5.07	5.34	5.56
	ď	CAPACITY FACTOR	(2)	61.24	74.16	75.75	78.12	10.19
•	10.	AVAILABILITY FACTOR	(%)	74.41	84.59	82.45	91.40	75.43
	11.	HEAT RATE (GROSS)	(BTU/KWH)	6,704	9,732	9,306	9,592	9,652
٠	12.	. THERMAL EFFICIENCY (GROSS)	(2)	35.17	35.07	36.67	35.58	35.36
	13.	13. NUMBER OF STARTS (YEAR/TOTAL)	î	28/115	25/140	21/161	46/207	28/235

BATAAN GASTURBINE POWER PLANT UNIT NO. 1

PLANT OPERATIONAL DATA

- - -	RATED CAPACITY	(MM)		•	1		31	TE
2.	DEPENDABLE CAPACITY	(MW)	•	1			31	3
m.	AVERAGE LOAD	(MM)	ı		•		31	29
. 4	GROSS GENERATION	(MWH)	ì	1		4	44,588	125,174
'n	OPERATING HOURS	(Hr)	1		ı		1,422.43	4,278.88
٠ ,	TOTAL OPERATING HOURS SINCE INITIAL SYNCHRO.	(Hr)	i	1			1,422.43	5,701.31
7.	TOTAL OUTAGE HOURS	(Hr)					2,194.03	4,481.1
	(1) FORCED OUTAGE	(Hr)		1			473.30	1,014.54
. *	(2) MAINTENANCE OUTAGE	(Hr)	ı	ŗ	1		0	7.75
	(3) PLANNED OUTAGE	(Hr)	•	4 .	ı		. 0	244.00
	(4) ECONOMIC SHUTDOWN	(Hr)		. T	1		1,720.73	3,211.58
	(5) OUTSIDE TROUBLE	(Hr)	•		ı			3.30
ω	STATION USED POWER RATIO	(2)	ŧ	1	ı		, . *	*
o,	CAPACITY FACTOR	(%)	ŀ	ı			39.77	46.11
10.	AVAILABILITY FACTOR	(%)		i			86.91	85.54
11.	HEAT RATE (GROSS)	(BTU/KWH)	1	1	ŧ		11,326	12,073
12.	THERMAL EFFICIENCY (GROSS)	(%)	*	. 1			30.13	28.27
13.	NUMBER OF STARTS (YEAR/TOTAL)	G	ı	1	•		× ×	*

RATED CAPACITY		ITEMS	-	1086	7001	000	7	
AVERD CAPACITY AVERAGE LOAD GROSS GENERATION GROSS GROSS	:	, i		0074	- P 0 0 1	0057	148 <i>y</i>	0661
AVERAGE LOAD GROSS GENERATION GROSS GENERATION GROSS GENERATION GROSS GENERATION (Hr) TOTAL OPERATING HOURS SINCE INITIAL SYNCHRO. (Hr) TOTAL OUTAGE HOURS (Hr) (1) FORCED OUTAGE (Hr) (2) MAINTENANCE OUTAGE (Hr) (3) PLANNED OUTAGE (Hr) (4) ECONOMIC SHUTDOWN (Hr) (5) OUTSIDE TROUBLE (Rr) (5) OUTSIDE TROUBLE (Rr) (7) AVAILABILITY FACTOR (7) HEAT RATE (GROSS) HEAT RATE (GROSS)	H	RATED CAPACITY	(MW)	•		i	31	ਜ
GROSS GENERATION (MWH)	2	DEPENDABLE CAPACITY	(MM)	. I		i	31	30 30
GROSS GENERATION (MWH)	ო	AVERAGE LOAD	(MM)	f		l	29	27
OPERATING HOURS TOTAL OPERATING HOURS SINCE INITIAL SYNCHRO. (Hr) (1) FORCED OUTAGE HOURS (Hr) (2) MAINTENANCE OUTAGE (Hr) (3) PLANNED OUTAGE (Hr) (4) ECONOMIC SHUTDOWN (Hr) (5) OUTSIDE TROUBLE (Hr) (5) OUTSIDE TROUBLE (Hr) (6) OUTSIDE TROUBLE (Hr) (7) CAPACITY FACTOR (7) HEAT RAIE (GROSS) (BTU/KWH) CAPACITY FACTOR (7) HEAT RAIE (GROSS)	4	GROSS GENERATION	(MWH)	ŗ		1	30,744	123,095
TOTAL OPERATION HOURS (Hr)	ι, ·	OPERATING HOURS	(Hr)	i	t	1	1,050.88	4,482.63
(1) FORCED OUTAGE HOURS (1) FORCED OUTAGE (2) MAINTENANCE OUTAGE (3) PLANNED OUTAGE (4) ECONOMIC SHUTDOWN (4) ECONOMIC SHUTDOWN (5) OUTSIDE TROUBLE (5) OUTSIDE TROUBLE (7) CAPACITY FACTOR (2) AVAILABILITY FACTOR (2) HEAT RATE (GROSS) (BTU/KWH)	•	TOTAL OPERATING HOURS SINCE INITIAL SYNCHRO.	(Hr)	i	t	1	1,050.88	5,533.51
(1) FORCED OUTAGE (Hr)	7	TOTAL OUTAGE HOURS	(Hr)	r	. 1	ľ	2,089.27	4,277,37
(2) MAINTENANCE OUTAGE (Hr)	,		(Hr)	i	•	ı	0.50	1,344.03
(4) ECONOMIC SHUTDOWN (Hr)			(Hr)	î .		i	0	48.21
(4) ECONOMIC SHUTDOWN (Hr)	-		(Br)	1		1	0	104.80
(5) OUTSIDE TROUBLE STATION USED POWER RATIO (Z) CAPACITY FACTOR (Z) AVAILABILITY FACTOR (Z) HEAT RATE (GROSS) (BTU/KWH)		ECONOMIC	(Hr.)	i		1	2,088.77	2,780.33
STATION USED POWER RATIO (Z) CAPACITY FACTOR (Z) AVAILABILITY FACTOR (Z) HEAT RATE (GROSS) (BTU/KWH)			(Hr)	ľ	1	1	0	5
CAPACITY FACTOR (2) AVAILABILITY FACTOR (2) HEAT RATE (GROSS) (BTU/KWH)	.	STATION USED POWER RATIO	(%)	ï	1	l	H *∙	 *
AVAILABILITY FACTOR (Z) HEAT RATE (GROSS) (BIU/KWH)	Q)	CAPACITY FACTOR	(%)	í	t		31.58	45.33
HEAT RATE (GROSS) (BTU/KWH)	, 0 1	AVAILABILITY FACTOR	(2)	i		ı	99.98	82.91
VOSCACY WOMALOTAGA TYMARHE	17.	HEAT RATE (GROSS)	(BIU/KWH)	í	ľ		11,414	12,233
THERMAL EFFICIENCY (GROSS)	12.	THERMAL EFFICIENCY (GROSS)	(%)	i	1	1	29.90	27.90
13. NUMBER OF STARTS (YEAR/TOTAL)	13.			•			77 *	*

	ITEMS		1986	1987	1988	1989	0661
H	RATED CAPACITY	(MM)	1	1	1	15	31
5	DEPENDABLE CAPACITY	(MW)	1	1	•	£ 8	30
m	AVERAGE LOAD	(MM)	. ·		ŧ	33	28
	GROSS GENERATION	(MWH)	ŧ	1	ť	41,907	118,990
N.		(Hr)	3	1	t	1,289.20	4,294.87
ė.	TOTAL OPERATING HOURS SINCE INITIAL SYNCHRO.	(Hr)	ı	ı	•	1,289.20	5,584.07
7.	TOTAL OUTAGE HOURS	(Hr)	1	, \$	a ·	1,492.33	4,465.13
	(1) FORCED OUTAGE	(Hr)	i	1	1.	53.86	995.45
	(2) MAINTENANCE OUTAGE	(Hr)	ŧ		ı	0	13.56
	(3) PLANNED OUTAGE	(Hr)	t	1	1.	0	221.65
	(4) ECONOMIC SHUTDOWN	(Hr)	1	t	•	1,385.19	3,230.72
	(5) OUTSIDE TROUBLE	(Hr)	l	.		53.28	
σ ,	STATION USED POWER RATIO	(%)	•		ŧ	← ⊣ *	*
9	CAPACITY FACTOR	(%)	ı	1	ı	49.55	43.84
0 1	AVAILABILITY FACTOR	(%)	1	1	. 1	98.03	85.95
11	HEAT RATE (GROSS)	(BTU/KWH)		4		11,517	12,181
12.	THERMAL EFFICIENCY (GROSS)	(%)	ı	i	1	29.63	
13.	NUMBER OF STARTS (YEAR/TOTAL)	()		1	t	?	

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MALAYA GASTURBINE POWER PLANT UNIT NO. 1

						-	
	ITEMS		1986	1987	1988	1989	1990
H	RATED CAPACITY	(MW)				31	EE
	DEPENDABLE CAPACITY	(MW)		ı	. 1	31	30
м	AVERAGE LOAD	(MW)	. 1	1	ŧ	30	26
4	GROSS GENERATION	(MWH)	•	t	1	30,769	112,410
'n	OPERATING HOURS	(Hr)	g		ı	1,025.23	4,269.84
φ	TOTAL OPERATING HOURS SINCE INITIAL SYNCHRO.	(Hr)	1	1	1	1,025.23	5,295.07
7.	TOTAL OUTAGE HOURS	(Hr)	ı	ı		1,902.77	4,490.16
	(1) FORCED OUTAGE	(Hr)	1	ì	I	383.07	2.79
	(2) MAINTENANCE OUTAGE	(Hr)		1	. 1	124.58	251.02
	(3) PLANNED OUTAGE	(Hr)	. .	1	ı	0	O
	(4) ECONOMIC SHUIDOWN	(Hr)	1	1	1	1,389.67	4,187.71
	(5) OUTSIDE TROUBLE	(Hr)	i	ı	1	5.45	48.64
ω	STATION USED POWER RATIO	(%)	i	t	ı	0.26	0.26
9.	CAPACITY FACTOR	(2)	ı	ı	ı	33.96	41.63
10.	AVAILABILITY FACTOR	(2)	t .	i	1	82.63	97.09
77	HEAT RATE (GROSS)	(BTU/KWH)	ı	†	1	11,469	12,033
12.	THERMAL EFFICIENCY (GROSS)	(2)		ŧ	1	29.76	28.36
13	NUMBER OF STARTS (YEAR/TOTAL)		1	1	ï	e-1 *	r-1 *
	COMMISSIONING: AUG 1989	*1: NO DATA AVAILABLE	AILABLE				

		PLANT OPERATIONAL DATA	ата		•	MALAYA GASTURBINE POWER PLANT		UNIT No. 2
		ITEMS		1986	1987	1988	1989	0661
	ri.	RAIED CAPACITY	(MM)	1			31	Te.
	. 2	DEPENDABLE CAPACITY	(MM)	•	ŧ	1	31	15
	. m	AVERAGE LOAD	(MM)	1	ı	t	. 29	27
	4.	GROSS GENERATION	(MMH)	4	ŀ	ı	36,002	119,096
	č,	OPERATING HOURS	(Hr)	ţ	ı	Ι.	1,233.59	4,376.29
	ý	TOTAL OPERATING HOURS SINCE INITIAL SYNCHRO.	(Hz)	•	.		1,233.59	5,609.88
	7.	TOTAL OUTAGE HOURS	(Hr)	•	ı	· 1	1,694.41	4,383.71
6 -		(1) FORCED OUTAGE	(Hr)	t	1	!	171.60	1.47
90		(2) MAINTENANCE OUTAGE	(Hr)	ŧ	. t	1	112.88	39.25
		(3) PLANNED OUTAGE	(Hr)	i t	ľ	1	0	O
		(4) ECONOMIC SHUTDOWN	(Hr)	i	. 1	1 .	1,381.42	4,313.65
		(5) OUTSIDE TROUBLE	(形)	l	I	ı	28.51	29.34
	φ.	STATION USED POWER RATIO	(%)	t	1	1	0.23	0.24
	တ်	CAPACITY FACTOR	(2)	ŧ	ı		40.05	44.00
	10.	AVAILABILITY FACTOR	(%)	i	I .		90.19	99.53
	H	HEAT RATE (GROSS)	(BTU/KWH)		1 . ~		11,459	11,824
	12.	THERMAL EFFICIENCY (GROSS)	(%)		ı	•	29.78	28.87
	13.	NUMBER OF STARTS (YEAR/TOTAL)	(7		1	• • • • • • • • • • • • • • • • • • •	r-4 ≯:	~~ *
•		COMMISSIONING: AUG 1989	*1: NO DATA	NO DATA AVAILABLE				

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	PLANT OPERATIONAL DATA	АТА			MALAYA GASTUR	MALAYA GASTURBINE POWER PLANT	UNIT No. 3
	ITEMS		1986	1987	1988	1989	0661
ļ	RATED CAPACITY	(MM)		1		31	31
5	DEPENDABLE CAPACITY	(MM)	ŧ	1	1	TE S	30
m	AVERAGE LOAD	(MM)		y -		31	28
4	GROSS GENERATION	(MWH)	1	1	•	36,509	112,012
'n	OPERATING HOURS	(Hr)	1	1	•	1,175.14	4,041.90
ý	TOTAL OPERATING HOURS SINCE INITIAL SYNCHRO.	(Hr)	•	.		1,175.14	5,217.04
7.	TOTAL OUTAGE HOURS	(Hr)		*	ì	1,752.86	4,738.10
	(1) FORCED OUTAGE	(Hr)	ı	1	1	160.34	6.53
	(2) MAINTENANCE OUTAGE	(Hr)	ı	. 1	1	45.80	187.50
	(3) PLANNED OUTAGE	(Hr)	1	i	- 1	o	245.67
	(4) ECONOMIC SHUTDOWN	(Hr)	ı	3		1,465.19	4,250.24
	(5) OUTSIDE TROUBLE	(Hr)	i	1		81.53	28.16
ω.	STATION USED POWER RATIO	(2)	1	1	ı	0.23	0.25
ο,	CAPACITY FACTOR	(2)	}	ì	1	41.37	41.38
TO.	AVAILABILITY FACTOR	(%)	1	1	t	92.76	94.96
년 년	HEAT RATE (GROSS)	(BIU/KWH)	ı	ì	, i	11,292	11,711
12.	THERMAL EFFICIENCY (GROSS)	(%)	i.	1	ŧ	30.22	29.14
13.	NUMBER OF STARTS (YEAR/TOTAL)	. (•	1		≓ *	∺ *
	COMMISSIONING: AUG 1989	*1: NO DATA AVAILABLE	AILABLE				

ANNEX 2. SUMMARY RECORD OF FORCED OUTAGE

Bataan Thermal Power Plant

Manila Thermal Power Plant

Sucat Thermal Power Plant

Malaya Thermal Power Plant

Batangas Coal Fired Thermal Power Plant

Bataan Gasturbine Power Plant

Malaya Gasturbine Power Plant

ANNEX 2.
SUMMARY RECORD OF FORCED OUTAGES

BATAAN THERMAL POWER PLANT UNIT No. 1 1986 1987 1988 1989 1990 TOTAL ITEMS 1. BOILER AND AUXILIARY 1) BOILER 2) FUEL OIL SYSTEM 1 2 3) AIR HEATER 2 1 1 4 4) FORCED DRAFT FAN 2 5) GAS RECIRCULATION FAN 6) VALVE AND PIPING 1 1 2 2 7) CONTROL SYSTEM 1 1 4 2. TURBINE AND AUXILIARY 1) MAIN TURBINE 2 2) CONDENSER 1 3) CIRCULATING WATER PUMP 1 2 4) CONTROL SYSTEM 3. CONDENSATE AND FEED WATER SYSTEM 1) CONDENSATE AND MAKE-UP SYSTEM 1 1 2) MOTOR DRIVEN BFP 3 1 3 7 3) TURBINE DRIVEN BFP 4) LOW PRESS. HEATER 5) HIGH PRESS. HEATER 6) CONTROL SYSTEM 1 1 4. ELECTRICAL EQUIPMENT 1) GENERATOR & EXCITER 2 1 2) TRANSFORMER AND SUBSTATION 1 3 2 3) STATION SERVICE SYSTEM 5 4) CONTROL SYSTEM 5. OTHERS 1) B-T INTERLOCK 3 1 2 2 5 2) GENERATOR BACK-UP 1 3) OUTSIDE TROUBLE 1 2 4 TOTAL 18 11 8 55 12

nes in a la receptio per <mark>esperante de la mé</mark>dica de la capación de la completa de la productiva de la completa de

ITEMS	1986	BATAAN T 1987	1988	1989	1990	TOTAL
1. BOILER AND AUXILIARY						<u> </u>
1) BOILER			3		2	
2) FUEL OIL SYSTEM	1					1
3) AIR HEATER	1			2	3	<u> </u>
4) FORCED DRAFT FAN				. 2	2	4
5) GAS RECIRCULATION FAN			1			
6) VALVE AND PIPING	1		1	2	1	
7) CONTROL SYSTEM		1	. 1	1	3	(
2. TURBINE AND AUXILIARY					.*	
1) MAIN TURBINE	1		1	1		
2) CONDENSER	1	1				
3) CIRCULATING WATER PUMP					1 1 1.	
4) CONTROL SYSTEM					1	
3. CONDENSATE AND FEED WATER SYSTEM						
1) CONDENSATE AND MAKE-UP SYSTEM						
2) MOTOR DRIVEN BFP	1	1			2	
3) TURBINE DRIVEN BFP						
4) LOW PRESS. HEATER						<u>:</u>
5) HIGH PRESS. HEATER			145			
6) CONTROL SYSTEM	·					
4. ELECTRICAL EQUIPMENT						<u> </u>
1) GENERATOR & EXCITER	1			2	1	
2) TRANSFORMER AND SUBSTATION	. 1					
3) STATION SERVICE SYSTEM	1	1	2	3	2.1	
4) CONTROL SYSTEM	,					
5. OTHERS						
1) B-T INTERLOCK		1	2		4	
2) GENERATOR BACK-UP				<u>.</u>		
3) OUTSIDE TROUBLE		1				
TOTAL	8	6	11	13	21	5

ITEMS	1986	MANILA T 1987	1988	1989	1990	TOTAL
1. BOILER AND AUXILIARY						
1) BOILER		1			1	. 2
2) FUEL OIL SYSTEM	1			1		2
3) AIR HEATER				1		1
4) FORCED DRAFT FAN	4	2			1	7
5) GAS RECIRCULATION FAN						
6) VALVE AND PIPING	2					2
7) CONTROL SYSTEM						
2. TURBINE AND AUXILIARY					:	
1) MAIN TURBINE						
2) CONDENSER	3		·	1		4
3) CIRCULATING WATER PUMP						
4) CONTROL SYSTEM				·		
3. CONDENSATE AND FEED WATER SYSTEM						
1) CONDENSATE AND MAKE-UP SYSTEM						
2) MOTOR DRIVEN BFP						er (
3) TURBINE DRIVEN BFP						and the second
4) LOW PRESS. HEATER						
5) HIGH PRESS. HEATER						
6) CONTROL SYSTEM				:		
4. ELECTRICAL EQUIPMENT						
1) GENERATOR & EXCITER						
2) TRANSFORMER AND SUBSTATION			3	3		
3) STATION SERVICE SYSTEM				1	1	2
4) CONTROL SYSTEM					:	
5. OTHERS						1
1) B-T INTERLOCK						
2) GENERATOR BACK-UP						
3) OUTSIDE TROUBLE						
TOTAL	10	3	. 3	7	3	20

	T		HERMAL P		f	
ITEMS	1986	1987	1988	1989	1990	TOTAL
1. BOILER AND AUXILIARY	<u> </u>		 			
1) BOILER				1	<u> </u>	1
2) FUEL OIL SYSTEM				· · ·		
3) AIR HEATER						
4) FORCED DRAFT FAN	4			1		5
5) GAS RECIRCULATION FAN						
6) VALVE AND PIPING	<u></u>					
7) CONTROL SYSTEM						
2. TURBINE AND AUXILIARY						
1) MAIN TURBINE				1		1
2) CONDENSER	:	1		1	1	3
3) CIRCULATING WATER PUMP						e e Let
4) CONTROL SYSTEM						
3. CONDENSATE AND FEED WATER SYSTEM						
1) CONDENSATE AND MAKE-UP SYSTEM		1				1
2) MOTOR DRIVEN BFP						
3) TURBINE DRIVEN BFP						
4) LOW PRESS. HEATER						
5) HIGH PRESS. HEATER		1 4			1, 2	
6) CONTROL SYSTEM		1			1	2
4. ELECTRICAL EQUIPMENT						
1) GENERATOR & EXCITER				1		1
2) TRANSFORMER AND SUBSTATION						V V 1
3) STATION SERVICE SYSTEM					2	2
4) CONTROL SYSTEM						
5. OTHERS						
1) B-T INTERLOCK	-			1	1	
				1.1		
2) GENERATOR BACK-UP				1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		
3) OUTSIDE TROUBLE					-	10
TOTAL	4	3	0	6	5	18

ITEMS	1986	SUCAT TH	1988	1989	1990	TOTAL
1. BOILER AND AUXILIARY		-				
1) BOILER						
2) FUEL OIL SYSTEM						
3) AIR HEATER			·			
4) FORCED DRAFT FAN						
5) GAS RECIRCULATION FAN						
6) VALVE AND PIPING					1	1
7) CONTROL SYSTEM		1	1		1	3
2. TURBINE AND AUXILIARY				·		
1) MAIN TURBINE			1		2	3
2) CONDENSER						
3) CIRCULATING WATER PUMP						
4) CONTROL SYSTEM				·		
3. CONDENSATE AND FEED WATER SYSTEM						
1) CONDENSATE AND MAKE-UP SYSTEM				~		
2) MOTOR DRIVEN BFP						
3) TURBINE DRIVEN BFP						. v
4) LOW PRESS. HEATER						
5) HIGH PRESS. HEATER		_		· .	1	1
6) CONTROL SYSTEM						
4. ELECTRICAL EQUIPMENT						
1) GENERATOR & EXCITER	2					2
2) TRANSFORMER AND SUBSTATION					,33	
3) STATION SERVICE SYSTEM	1					1
4) CONTROL SYSTEM			et conscions			
5. OTHERS		:		· .		
1) B-T INTERLOCK		1	. :		3	4
2) GENERATOR BACK-UP						
3) OUTSIDE TROUBLE						
TOTAL	3	2	2	0	8	15

			Γ		
1986	1987	1988	1989	1990	TOTAL
	1			1	2
		1		2	3
					<u> </u>
		1		1.4	1
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		2.31			
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		1.			
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1			1	1	
				1	
1	2	3	2	7	1:
	1986	1986 1987	1986 1987 1988 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1986 1987 1988 1989 1 1	

TMANA		SUCAT TH	T			
ITEMS	1986	1987	1988	1989	1990	TOTAL
1. BOILER AND AUXILIARY						i
1) BOILER		2				· 2
2) FUEL OIL SYSTEM						
3) AIR HEATER	1			1	5	7
4) FORCED DRAFT FAN						· · · · · · · · · · · · · · · · · · ·
5) GAS RECIRCULATION FAN						
6) VALVE AND PIPING			1		. :	. 1
7) CONTROL SYSTEM	1		1			2
2. TURBINE AND AUXILIARY						
1) MAIN TURBINE	1				1	2
2) CONDENSER			1	1		2
3) CIRCULATING WATER PUMP					1	. 1
4) CONTROL SYSTEM			1	1		2
3. CONDENSATE AND FEED WATER SYSTEM						
1) CONDENSATE AND MAKE-UP SYSTEM						
2) MOTOR DRIVEN BFP					1	1
3) TURBINE DRIVEN BFP			·	1		1
4) LOW PRESS. HEATER						
5) HIGH PRESS. HEATER	1					1
6) CONTROL SYSTEM	1		2			3
4. ELECTRICAL EQUIPMENT						
1) GENERATOR & EXCITER						
				····	2	2
2) TRANSFORMER AND SUBSTATION					4	
3) STATION SERVICE SYSTEM				1		1
4) CONTROL SYSTEM						
5. OTHERS						
1) B-T INTERLOCK			1			1
2) GENERATOR BACK-UP						
3) OUTSIDE TROUBLE			,			
TOTAL	5	2	7	5	10	29

ITEMS	1986	1987	1988	1989	T UNIT N 1990	TATOT
1. BOILER AND AUXILIARY						
1) BOILER			3	1	1	4
2) FUEL OIL SYSTEM		1				1
3) AIR HEATER	1		4	2		
4) FORCED DRAFT FAN		1				:
5) GAS RECIRCULATION FAN						
6) VALVE AND PIPING		1	. 1			
7) CONTROL SYSTEM		1	1			
2. TURBINE AND AUXILIARY					and determine the desired about the second s	
1) MAIN TURBINE		1	2			
2) CONDENSER						
3) CIRCULATING WATER PUMP				:		
4) CONTROL SYSTEM						
3. CONDENSATE AND FEED WATER SYSTEM						
1) CONDENSATE AND MAKE-UP SYSTEM						
2) MOTOR DRIVEN BFP						
3) TURBINE DRIVEN BFP			1		1 1 - 14.	
4) LOW PRESS. HEATER						
5) HIGH PRESS. HEATER						
6) CONTROL SYSTEM						
4. ELECTRICAL EQUIPMENT				: :		
1) GENERATOR & EXCITER						***
2) TRANSFORMER AND SUBSTATION						
3) STATION SERVICE SYSTEM						
4) CONTROL SYSTEM						
o. others				·		1 1
1) B-T INTERLOCK		1	1	-		
2) GENERATOR BACK-UP		1		7 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1.	100000000000000000000000000000000000000	
3) OUTSIDE TROUBLE						· ·
TOTAL	1	7	13	-3	0	2

TINDIA	1986	MALAYA T	HERMAL P	OWER PLAT	1990	TOTAL
ITEMS	1986	1987	1988	1909	1990	TOTAL
1. BOILER AND AUXILIARY						
1) BOILER	,		1		1	2
2) FUEL OIL SYSTEM						
3) AIR HEATER	2					2
4) FORCED DRAFT FAN						
5) GAS RECIRCULATION FAN						
6) VALVE AND PIPING	1	1	1	1		4
7) CONTROL SYSTEM		1	4	3	3	11
2. TURBINE AND AUXILIARY						
1) MAIN TURBINE			1	1	1	3
2) CONDENSER					1	. 1
3) CIRCULATING WATER PUMP	1					1
4) CONTROL SYSTEM		·	1	. 2		. 3
3. CONDENSATE AND FEED WATER SYSTEM		·				
1) CONDENSATE AND MAKE-UP SYSTEM	1	:				1
2) MOTOR DRIVEN BFP	1					1
3) TURBINE DRIVEN BFP						
4) LOW PRESS. HEATER						
5) HIGH PRESS. HEATER						
6) CONTROL SYSTEM			2	1	2	5
4. ELECTRICAL EQUIPMENT					-	
1) GENERATOR & EXCITER	,			2	1	3
2) TRANSFORMER AND SUBSTATION					1	1
						2
3) STATION SERVICE SYSTEM				2	·	
4) CONTROL SYSTEM	1					
5. OTHERS						
1) B-T INTERLOCK			3	1	1	5
2) GENERATOR BACK-UP				*. *	5	5
3) OUTSIDE TROUBLE	. :					
TOTAL	6	2	13	13	16	50

· · · · · · · · · · · · · · · · · · ·		MALAYA T	No. 2			
ITEMS	1986	1987	1988	1989	1990	TOTAL
l. BOILER AND AUXILIARY	:					
1) BOILER					3	
2) FUEL OIL SYSTEM					4	
3) AIR HEATER						
4) FORCED DRAFT FAN						
5) GAS RECIRCULATION FAN	1		- :	: .		
6) VALVE AND PIPING					1	
7) CONTROL SYSTEM			1			
2. TURBINE AND AUXILIARY						
1) MAIN TURBINE		1				
2) CONDENSER				1	1	
3) CIRCULATING WATER PUMP						
4) CONTROL SYSTEM	-					
CONDENSATE AND FEED WATER SYSTEM						
1) CONDENSATE AND MAKE-UP SYSTEM						
2) MOTOR DRIVEN BFP						
3) TURBINE DRIVEN BFP						
4) LOW PRESS. HEATER						
5) HIGH PRESS. HEATER						
6) CONTROL SYSTEM			<u> </u>			
1. ELECTRICAL EQUIPMENT					<u> </u>	
1) GENERATOR & EXCITER			1	· · · · · · · · · · · · · · · · · · ·		
2) TRANSFORMER AND SUBSTATION	<u> </u>					
3) STATION SERVICE SYSTEM	<u> </u>	2				
4) CONTROL SYSTEM			1	1 1 1 1 1		
. OTHERS						
1) B-T INTERLOCK		2			1	
2) GENERATOR BACK-UP						
3) OUTSIDE TROUBLE					: : '	enter in
TOTAL	1	5	3	1	10	2

	դ	BATANGAS	THERMAL	POWER P	LANT UNI	T No. 1
ITEMS	1986	1987	1988	1989	1990	TOTAL
1. BOILER AND AUXILIARY						
1) BOILER	1	1	1	1	6	10
2) FUEL OIL & COAL SYSTEM	2	2	1			5
3) AIR HEATER				1	: '	. 1
4) FORCED DRAFT FAN & IDF	5					5
5) GAS RECIRCULATION FAN						
6) VALVE AND PIPING	1	1		2		4
7) CONTROL SYSTEM	2	2	1	2	1	8
2. TURBINE AND AUXILIARY						
1) MAIN TURBINE		2	:	1	1	4
2) CONDENSER					1	1
3) CIRCULATING WATER PUMP						
4) CONTROL SYSTEM			1		·	1
3. CONDENSATE AND FEED WATER SYSTEM						
1) CONDENSATE AND MAKE-UP SYSTEM				1		1
2) MOTOR DRIVEN BFP			1			1
3) TURBINE DRIVEN BFP				1	1	2
4) LOW PRESS. HEATER						
5) HIGH PRESS. HEATER						
6) CONTROL SYSTEM			1	1		2
4. ELECTRICAL EQUIPMENT						
1) GENERATOR & EXCITER		1		2		3
2) TRANSFORMER AND SUBSTATION			1	~ 		1
3) STATION SERVICE SYSTEM		-		1		1
4) CONTROL SYSTEM	·					
5. OTHERS						
1) B-T INTERLOCK	3	10	5	23	12	53
2) GENERATOR BACK-UP	2					2
3) OUTSIDE TROUBLE						· · ·
TOTAL	16	19	12	36	22	105

TMPMC	1986	1987	1988	1989	PLANT UN 1990	TOTAL
ITEMS	1380	1367	1300	1303	1990	TOTAN
. GAS TURBINE AND AUXILIARY						
1) GAS TURBINE			:		1	
2) AIR COMPRESSOR				:	1	·. :
3) COMBUSTER				-		
4) LOAD GEAR						· · · · · · · · · · · · · · · · · · ·
5) STARTING EQUIPMENT			:		3	
6) FUEL OIL SYSTEM				1	2	
7) CONTROL SYSTEM					2	. <u> </u>
. ELECTRICAL EQUIPMENT						
1) GENERATOR & EXCITER						
2) TRANSFORMER AND SUBSTATION						
3) STATION SERVICE SYSTEM					2	
4) CONTROL SYSTEM	1					
OTHERS						
1) GT INTERLOCK	· ·			44.4		
2) GENERATOR BACK-UP			· ·			
3) OUTSIDE TROUBLE		ļ			1	<u> </u>
	-					
	ļ					
			ļ			
	 					
TOTAL		1		1	12	1

	· · · · · · · · · · · · · · · · · · ·	BATAAN C	GASTURBIN	E POWER	PLANT UN	IT No. 2
ITEMS	1986	1987	1988	1989	1990	TOTAL
1. GAS TURBINE AND AUXILIARY						
1) GAS TURBINE				1	1	2
2) AIR COMPRESSOR					1]
3) COMBUSTER					1	
4) LOAD GEAR		1		1		
5) STARTING EQUIPMENT						
		 	 -			
6) FUEL OIL SYSTEM		<u> </u> -	<u></u>	<u> </u>	1	
7) CONTROL SYSTEM						
2. ELECTRICAL EQUIPMENT			<u> </u>			
1) GENERATOR & EXCITER				1	2	
2) TRANSFORMER AND SUBSTATION				,		
3) STATION SERVICE SYSTEM					. 1	
4) CONTROL SYSTEM						
. OTHERS	ļ E					
1) GT INTERLOCK						- 14
2) GENERATOR BACK-UP						· · · · · · · · · · · · · · · · · · ·
3) OUTSIDE TROUBLE	· · · · · · · · · · · · · · · · · · ·					
			 			
		<u> </u>				
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moma.				i de la companya de l		
TOTAL				2	7	

ITEMS	1986	1987	1988	1989	PLANT UN 1990	TOTAL
1. GAS TURBINE AND AUXILIARY						
1) GAS TURBINE					1	1
2) AIR COMPRESSOR					1	
3) COMBUSTER					2	2
4) LOAD GEAR					1]
5) STARTING EQUIPMENT						
6) FUEL OIL SYSTEM				1	3	
7) CONTROL SYSTEM						
. ELECTRICAL EQUIPMENT						
1) GENERATOR & EXCITER					2	
2) TRANSFORMER AND SUBSTATION						. 1
3) STATION SERVICE SYSTEM						
4) CONTROL SYSTEM						1.4
. OTHERS						
1) GT INTERLOCK						
2) GENERATOR BACK-UP						
3) OUTSIDE TROUBLE						
TOTAL				1	10	1.

ITEMS	1986	1987	ASTURBIN 1988	1989	1990	TOTAL
1. GAS TURBINE AND AUXILIARY						
1) GAS TURBINE				1	1	2
2) AIR COMPRESSOR					3	3
3) COMBUSTER						
4) LOAD GEAR					1	1
5) STARTING EQUIPMENT					<u>=</u>	
6) FUEL OIL SYSTEM		 			1	
7) CONTROL SYSTEM						
2. ELECTRICAL EQUIPMENT					<u> </u>	
1) GENERATOR & EXCITER						· · · · · · · · · · · · · · · · · · ·
2) TRANSFORMER AND SUBSTATION					-	
3) STATION SERVICE SYSTEM					1	1
4) CONTROL SYSTEM	<u> </u>				•	
3. OTHERS	. '					
1) GT INTERLOCK						· · · · · · · · · · · · · · · · · · ·
2) GENERATOR BACK-UP				<u> </u>		
3) OUTSIDE TROUBLE					1 1 1	<u> </u>
J) GOISTEE TROOPING				·	1	
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	· · · · · · · · · · · · · · · · · · ·		·			
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	· · · · · · · · · · · · · · · · · · ·					
TOTAL	ta e e			1	8	9

	1	7	1	1	PLANT UN	
ITEMS .	1986	1987	1988	1989	1990	TOTAL
1. GAS TURBINE AND AUXILIARY						· · · · · · · · · · · · · · · · · · ·
1) GAS TURBINE				2	1	3
2) AIR COMPRESSOR		<u> </u>		1	1	2
3) COMBUSTER						
4) LOAD GEAR						
5) STARTING EQUIPMENT						
6) FUEL OIL SYSTEM	<u> </u>			3		3
7) CONTROL SYSTEM					-	
2. ELECTRICAL EQUIPMENT	:					·
1) GENERATOR & EXCITER					1	1
2) TRANSFORMER AND SUBSTATION						
3) STATION SERVICE SYSTEM			:			
4) CONTROL SYSTEM						
3. OTHERS						
1) GT INTERLOCK						
2) GENERATOR BACK-UP				1	1	. 2
3) OUTSIDE TROUBLE						
			,			
				i A		
					1	
	:					
TOTAL				7	4	11
				<u></u>		

ITEMS		1986	1987	1988	1989	1990	LATOT
1. GAS TURBINE AND AUXILIARY							
1) GAS TURBINE					2	2	
2) AIR COMPRESSOR							
3) COMBUSTER							
4) LOAD GEAR							
5) STARTING EQUIPMENT							
6) FUEL OIL SYSTEM					1		
7) CONTROL SYSTEM						·	
2. ELECTRICAL EQUIPMENT							
1) GENERATOR & EXCITER							
2) TRANSFORMER AND SUBSTATION	1						
3) STATION SERVICE SYSTEM							:
4) CONTROL SYSTEM			1				
3. OTHERS							
1) GT INTERLOCK							
2) GENERATOR BACK-UP					2		
3) OUTSIDE TROUBLE					1		
			·				
				,			
	;			·			
	•				· · · · · · · · · · · · · · · · · · ·		
					<u> </u>		
			<u> </u>				
	: -						
TOTAL					6	2	
		· •,				4	

		MALAYA G	ASTURBIN	E POWER	PLANT UN	IT No. 3
ITEMS	1986	1987	1988	1989	1990	TOTAL
1. GAS TURBINE AND AUXILIARY						
1) GAS TURBINE				1	5	. 6
2) AIR COMPRESSOR	. · ·				1	1
3) COMBUSTER	· ·			1		1
4) LOAD GEAR			,			· · · · · · · · · · · · · · · · · · ·
5) STARTING EQUIPMENT						
6) FUEL OIL SYSTEM						
7) CONTROL SYSTEM				2		7
P. ELECTRICAL EQUIPMENT						
1) GENERATOR & EXCITER						
2) TRANSFORMER AND SUBSTATION					<u> </u>	
3) STATION SERVICE SYSTEM						•
4) CONTROL SYSTEM						·
. OTHERS						
1) GT INTERLOCK						
2) GENERATOR BACK-UP				2	1	
3) OUTSIDE TROUBLE				1		<u>.</u>]
				•		
	· ·					
			-			
		-				
TOTAL				7	7	1.
TOTAL				3.		1.

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ANNEX 3. SUMMARY OF MAJOR REHABILITATION WORKS

	ITEM	MALAYA -1	MALAYA -2	SUCAT	SUCAT -4	SUCAT	SUCAT -3	MANILA -1	MANILA -2	BATAAN -1	BATAAN -2	BATANGAS CF-1	REMARKS
Boiler a. Superheater	Detailed inspection of SH tubes	•	•	•	•	0	0	0	0	0	· (i)	☆ 1992	
	_	● ☆ Par- tial,1992		Partial	(1)	0	0	0	©	0	0		
	Replacement of roof SH tube	Partial			•				ž.			* ☆ 1992	*Primary SH
	Replacement of deteriorated/ thinning tube	•	•	•	(4)	. ©	0	0	0	0	0	☆ 1992	
. Reheater	Detailed inspection of RH tubes	•	•	•	(0)	0	0	O	0	©	0	☆ 1992	
	Replacement of RH tube	Partial	☆ 1992	Partial	(1)	© .	0	⊚ Partial	© Partial	(O)	0	☆ 1992	
 -	Replacement of deteriorated/ thinning tube	•	•	•	(1)	0	0	0	0	0	0	☆ 1992	
. Water Wall	Detailed inspection of W/W tube	•	•	•	•	0	0	©	©	0	©		
	Replacement of W/W tube	\ - /	● ☆ Par- tial,1992	•		0	0						
. Boiler Casing & Gas, Air Duct	Repair of leaking boiler casing and gas, air duct		•	•	(1)	0	0	0	0	0		☆ 1992	
. Attemperator	Replacement of SH and RH attemperator spray nozzle	•		•	. (i)	0	0	0	©	0	©		
. Burner	Modification of steam atomizing burner system	•	· · · •	•	(0)	©	0					* ☆ 1992	*Coal Burner
. Bottom Hopper	Repair of bottom ash hopper					0	0						
. Safety valve	Replacement/repair of safety valve			⊚ SH-3						☆	☆		
oiler Auxiliaries . Forced Draft Fan /Gas Recircu-	Replacement/repair of FDF/GRF	⊚ FDF	● FDF		:			* © FDF	* © FDF		☆ GRF		*Transfer of FDF
lation Fan Air Heater	Replacement of heating elements and parts			•	(1)	0	0	©	0	0	0	☆ 1992	
LEGEND: O-Imple	emented O-1st Priority O-2n	d Priori		To be in	plemente	d in ove	rhaul						6 - 112

en della sektemberak en temperatura pende en endersten en et ende elle Angli ille på ettic alle della schaft schaft state en e	ITEM	MALAYA -1	MALAYA	SUCAT	SUCAT	SUCAT	SUCAT	MANILA	MANILA -2	BATAAN -1	BATAAN -2	BATANGAS CF-1	REMARKS
c. Steam Coil Air Heater	Replacement of heating elements	•		•	•	0	0	*	*	0	•		* Additional of SCAH
	Modification of SCAH drain system	•	•	•	•	0	0	0	0	0	©		
d. Fuel Oil Firing System	Replacement/repair of fuel oil heater	•	•	☆ 1993	•	0	0	0	0	(O)	0		
	Modification of light oil firing system	•	•	•	(1)	0	0						
e. Ash Handling System	Replacement of ash handling system	•	•	•	(6)	0	0	0	0			☆ 1992	
	Replacement/repair of dust collector	•	•	•	•	0	0	0	0			* ☆ 1992	* ^{EP}
f. Auxiliary Steam System	Repair/modification of auxiliary steam line and auxiliary boiler	Aux. B		•	•	0	0	0	0				
g. Soot Blower	Replacement/repair of soot blower	③ ☆ 1992	•	•	•	0	0	0	0	O	0	☆ 1992	
h. Piping System	Inspection and repair of pipe line	•	•	•	*	*	*	0	0	0	0		*Inspection of main steam pipe
i. Smoke stack	Guniting for smoke stack	☆ 1993	☆ 1992		•	0		0	0	☆			
j. Stacker and Reclaimer	Realignment of the rail	:										☆ 1992	
k. Cool Yard	Cement all stockpile flooring											☆	
1. Conveyor	Replacement/repair of conveyor			:								☆ 1992	
m. Transfer Tower	Rehabilitation of transfer tower											∱ 1993	
n. Mill	Replacement/repair of mill											☆ 1992	
													

and the contract to the last the last consecution when a trace of the last the contract of the	ITEM	MALAYA	MALAYA -2	SUCAT	SUCAT	SUCAT	SUCAT	MANILA -1	MANILA -2	BATAAN -1	BATAAN -2	BATANGAS CF-1	REMARKS
Turbine a. HP Turbine	Major inspection	(a)	•	•	•	0	0	© .	©	0	· ©		
	Replacement of inner casing				(a)	0	0	0	(
	Replacement of turbine rotor		∆ Blade 1992	Blade	•	0	(i)	0	0	*	*		*Diagnosis of remaining life
b. IP Turbine	Major inspection	•	•	•	•	0	0	0	0	0	0		
	Replacement of inner casing	•			③	0	0	0	0				
	Replacement of turbine rotor	☆ 1993		Blade	Blade	0	0	0	0	*	*		*Diagnosis of remaining life
c. LP Turbine	Major inspection	•	•	•	•	*	*	0	· ©	(O)	0		
	Replacement of turbine rotor	● ☆ Blade	1	•	©	Blade 1990	© Blade			*	*		*Diagnosis of remaining life
	Replacement of casing				於 1994								
d. Main Stop Valve	Replacement of turbine main valve							© MSV	© MSV		© Parts		
e. BFP Turbine	Reblading of BFP turbine	☆ 1993									3		
Furbine Auxiliaries a. Condenser	Replacement of tubes	● ☆ Aux 1992		Partial	•	© 1991	© Partial	*	⊚ 1991	☆ 1993	☆ 1993	☆ 1992	*Air cooling zone only
	Installation of on-line cleaning and Debris filter system							☆ 1993	☆ 1993	① 1992	☆ 1993		
Feed Water Heater	Replacement of LP heater	⊕ ☆ #3 #3 1993	☆ #2,3 1992				© #3		© #3				
e. High Pressure Feed Water Heater	Replacement of HP heater	⊕ ∱5 <i>I</i> #5A, #5 <i>I</i> #5B #5E	3	☆ #6 1992	#5A,5B #6A,6B	. ~	● ◎ #6A,#6B 1991	#5,1983 #6,1981	● ◎ #5, #6 1983	© ☆ HP#1,#	2 HP#1,2		
	Installation of HP heaters by-pass line	1993				•	•						

VEZZAĞIĞI SAYA CIRA MUNTAKUN ARBASI CIRA PARQAPANÇAR ONUN KUNUN KIRILDEN GERÜNÜN BERM	ITEM	MALAYA	MALAYA -2	SUCAT	SUCAT -4	SUCAT	SUCAT	MANILA -1	MANILA -2	BATAAN -1	BATAAN -2	BATANGAS CF-1	REMARKS
d. Deaerator	Modification of deaerator		•		∱ 1994					☆ 1993			
e. Turbine Oil Pump	Replacement/repair of oil pump	JOB		•	•								
f. Turbine Lube Oil System	Modification of lube. oil purifying system	•											
g. Air ejector	Replacement of air ejector					0	©						•
h. Extraction Steam line	Additional non-return valve at the extraction steam to deaerator	•			•					·			
i. House Service Closed Cycle Heat Exchanger	Replacement of HSCC heat exchanger			☆ 1993	•	0	•	0	0	(i) Tube			
	Additional installation of heat exchanger									(i) 191		
j. Boiler Feed Water Pump	Replacement/repair of BFP	•		•	•					0	*	☆ 1992	*BFP Outlet valve
k. Circulating Water Pump	Replacement/repair of CWP				•			☆ 1993	☆ 1993	© Parts	© Parts	:	
l. Condensate Water Pump	Replacement/repair of CP							☆	☆		A Parts 1992		
m. Piping System	Repair of damaged pipe insulation	•	•	· •	© 2	0	0	0	0	0	0		
n. Others	Installation of travelling crane		:	•									
	Replacement of passenger elevator		:		*					☆	☆		*Additional installation
	Repair/replacement of power house ventilation fans	● ☆ 1993	•	•	•	•	•	©	0				
o. Cooperation with manufacturer	Invitation of Manufacturers supervisor for the above checking/improvement/replacement		•	•	•	0	0	0	0	0	0	0	

	ITEM	MALAYA -1	MALAYA -2	SUCAT	SUCAT	SUCAT	SUCAT	MANILA	MANILA -2	BATAAN -1	BATAAN -2	BATANGAS CF-1	REMARKS
Electrical Equipment a. Generator	Replacement/repair of generator stator	* ☆ 1992	☆ Bushing 1992		•			*	*	0	0		*Diagnosis of remaining life
	Replacement/repair of generator rotor	•	*	•	0			0	0	©			*Diagnosis of remaining life
b. Exciter	Replacement/repair of exciter				(1)	0	0						
	Replacement/repair of AVR	<i>:</i>			•	0	0		- 1 C	0	(O)		
c. Gas and Seal oil	Replacement/repair of generator gas and seal oil equipment									0	© *		
d. Batteries and CVCF/UPS	Additional/replacement of batteries	*	*					☆	☆				*Additional silicon dropper
	Additional of CVCF/UPS set				•	0	0	:		☆			
e. Emergency Diesel Generator	Automatic start and cabling of emergency diesel generator		•										
f. Motor	Replacement of 4,160V/480V motor		☆ CWP 1992	RWP	● ☆ RWP CWP			CP, BFP	CP, BFP CWP		© AOP		·
g. Switchgear	Replacement of 4,160V switch- gear							O P/C,Tr	O P/C,Tr	☆ VCB			
	Additional/replacement of MCC	⊚ E				© B,T,SS	B,T,SS, VF			↑ P/C			
h. Power Cable	Replacement of power cable			•	•	◎ 4.16kV 480V	© 4.16kV 480V	0 4.16kV	0 4.16kV	⊚ 15kV			
1. Switchyard	Replacement/repair of switch- yard equipment				☆ GCB	© GCB,DS	© GCB, DS			© GCB, LA	© GCB,LA		
j Communication Facilities	Additional communication facilities	☆	•			☆		☆		☆		☆	
k. Others	Replacement of fire protection system	•											
	Replacement of sootblower electrical control system					0	0	0	0	0		☆ 1992	

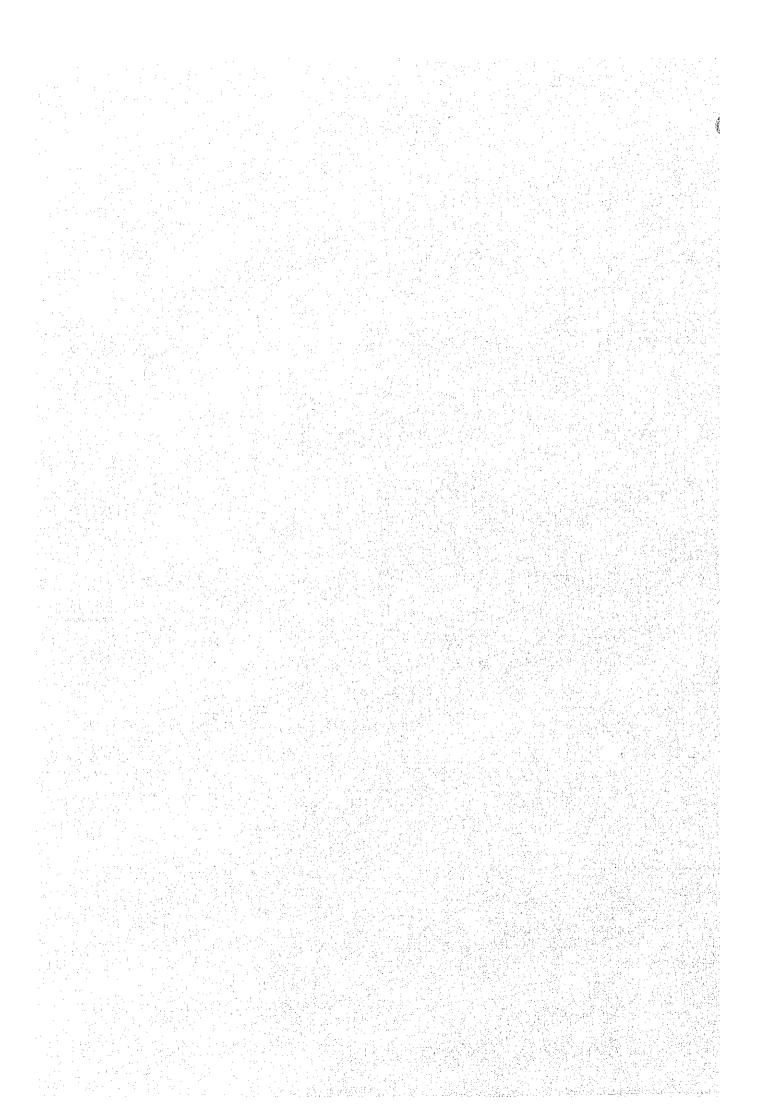
The second secon	ITEM	к Саламин межений по для (по для не при по да при не по да по да по да по да по да по да не по да по да не по С по да не по да по да не по да		MALAYA	SUCAT	SUCAT	SUCAT	SUCAT	MANILA	MANILA -2	BATAAN	BATAAN -2	BATANGAS CF-1	REMARKS
Instrument and Control	sate flow, to	ecorder for conden- irbine speed/cam idenser vacuum &	•	•	•	•	0	0						
		of local gauge and	•	•	•	•	0	· ©				:		
	Replacement of recorder and	of control board indicator	☆ 1993	☆ 1993	•	•	0	0	0	0	0	0		
	Replacement/n ABC and start	nodification of -up system	© и-90	☆ n-90	© N-90	М−90	© N-90	⊚ N-90	© N-90	© и-90	© N-90	© N-90		
	Spare parts		•	(a)	•	•	0	0	0	0	0	0		
	Replacement/m fuel oil cont	nodification of rol system		Burner			0	0						
	Installation monitoring TV	of furnace/smoke	•	•	•	•	0	0	© Smoke	© Smoke	☆	☆		
	Replacement o	f boiler metal easurement		☆ 1993	•	•	0	©						
	ABC and start overhaul/cali tuning	bration and fine	•	•	•	•	0	0	0	©	0	0		
· .		Deaerator, Heater & condensate drain control	•		•	(a)	0	· ©	0	0	0			
	Replacement/ repair of local control	Aux. steam and AH temp. control	•		•	•	0	0	0	0	0			
		Others			•	•	0	0	0	0	0			
	Replacement/re	epair of EHG	•	·		•	©	0		·		(O)		
	Replacement of interlock	f relay for plant	•	•		•	©	©	0	0				
	Inprovement or room air condi	f central control	•	☆ 1992	:						* 19	ر م 92		*Repair
	Additional cor service air co modification o	ompressor and	CONT	☆	•	•					☆ swyd	:	☆ SS 1992	

	ITEM	MALAYA	MALAYA	SUCAT	SUCAT	SUCAT	SUCAT	MANILA -1	MANILA	BATAAN -1	BATAAN -2	BATANGAS CF-1	REMARKS
Instrument and Control	Additional first out indicator	•	•										
	Modification of alarm system	•	•										
	Additional alarm and annunciator	•	•	•	•	0	0				0		
·	Modification for load run-back	● FDF,CWP	● FDF,CWP	● FDF,CWP	● FDF,CWP	⊚ FDF,CWP	○ FDF,CWP						
	Additional/replacement of protective relay	⊚ GEN				© GEN							
	Replacement of fuel oil flow meter	•	•	•	•	0	0	0	0	0	☆		
	Replacement of drum level transmitter/indicator	- 1	•	•				☆	☆	☆	☆		
	Replacement of mercury type float, temp. & press. switches	众 1992				0	0	0	0				
	Replacement of BFP minimum flow and control valve			•		0	0	☆	\triangle				
	Additional sequence of event recorder			•	•	0	0	0	©	0	0		
	Replacement of flue gas O2 measurement			•	•	0	©	0	©	0	0		•
	Replacement of turbine supervisory instruments				•	0	©			©	O		
	Additional generator H ₂ purity meter	•		•	•	0	©	0	0	☆	☆		
	Replacement of turbine wall stress evaluator					©	©						
										· · · · · · · · · · · · · · · · · · ·			

anticanica (a material merce) quantum (et pepulay, magana, pepulanta) material de la Colaterna de Colaterna (e	ITEM	MALAYA -1	MALAYA -2	SUCAT	SUCAT	SUCAT	SUCAT	MANILA	MANILA -2	BATAAN -1	BATAAN -2	BATANGAS CF-1	REMARKS
Demineralizer	Additional demineralizing plant	19) 86		(1) 1934	© 1993	· · · · · · · · · · · · · · · · · · ·			*)		*Replacement of HCl tank
	Additional pre-water treatment plant	19	86		(1991								
	Overhauling and resin make-up	\$	}			© 1992		7	<u>۲</u>		☆	☆	
	Using of Laguna Lake Water	(•		(•		_					
	Neutralizing equipment	19	92		(•		7	^		•	•	
	Replacement of demineralizer instruments							PH, Cond	λ luctivity	PH, Cond	☆ ductivity	y ☆ Silica	
Condensate Polishing Plant	Replacement of control panel including instruments	•			(0)	0	0	_					
	Repair/replacement of control system for automatic operation	•			• 🐠	· •	0	_		<u> </u>	_	<u></u>	
	Using of higher quality caustic soda of rayon grade	•		. -	(1)	•	•						
	Overhauling, and resin make-up	* ☆			☆	0	0					- -	
	Adjustment of resin level		_		<u></u>	©	0	-					
	Installation of condensate magnetic filter	<u> </u>	_	_	(1)	©	0	_			_ :	-	:
Oil Water Separator	Installation of oil water separator									1	☆ 992		

r	PEM	MALAYA	MALAYA	SUCAT	SUCAT	SUCAT	SUCAT	MANILA	MANILA -2	BATAAN -1	BATAAN -2	BATANGAS CF-1	REMARKS
Secondary Water Treatment a. Chemical Feed	Replacement of chemical feed system	•	☆ 1992	•	•	O	0	0	0			•	
System b. Chemical Feed Control	Determination of NH3 injection by the measurement of conductivity	•	☆	•	•	0	0					•	
	Automatic pH control		☆	•	③	0	0					•	
										·			
Sampling Rack	Replacement of sampling rack	•	•	•	•	0	· (©	0	0	☆ 1992	☆ 1992	☆	
							·						
Monitoring Instrument	Additional of chemical monitoring instruments	•	•	•	•	0	©	0	0	☆	☆	☆	
Cooling Water a. House Service Closed Cycle	Change of water quality analysis item	r ⊚	•	•	•	0	0	0	0	©	0	•	
Heat Exchanger	Injection of chemicals	•	•	•	•	•	•	0	0	©	0	. •	
	Check of sacrifical zinc plate	•	•	•	•	0	0	0	0	0	0	•	
b. Condenser Cooling Water	Replacement/repair of cathodic protection equipment	•	•		•	0	0	0	0	0	0	•	
	Replacement of travelling water screen				•			© Wash P	⊚ Wash P	0	0		
	Replacement of raw water pump		☆ 1992		☆ 1992								
	Reinstallation of gantry crane											☆ 1992	
	Replacement/repair of circula- ting water pipe line									*	*	* ☆ 1992	*Including marine pipe
						:							

이 가장 아이들은 현대 만든 사람들은 얼마는 어디를 다고	
보는 하님은 물하는 그리는 물로 함께 보고 있다. 그런 사용 보다는	
그리가 보는 중한 점점을 보고 있다. 그들이 모르는 것은 것으로 모르는	
고하여 보는 이 상품들이 모른 등을 하고 되는 것이 살아요.	
그 소리를 통합하고 있다. 불물하게 하면 함께서 되는 이 불어나	
진행 중 성화를 하는 호텔 발표를 가는 이번 등에 다른 사람이다.	
그런 그는 기를 하는 사람들이 살았다. 그는 사람들은 사람들이 살아갔다.	
사람들 [시골 ^ 주민들은 교통하다] 그 그 모양하는 그는 것이	
보면 발장으로 보고 이번 나는 나를 하고 하는 것이 되는데 그렇게 걸었다.	
그러워 얼마나 되는 아이들에 가르게 되고 있다. 그리를 모습니다 다	
이왕, 경우, 이 소리를 하는 물이 다 가꾸는 것 같아. 그는 사이를 모르는 것이다.	
도 있다. 그들은 그리고 한 경험에 대한 보는 사람이 되는 것을 되었다. 그는 것이 되었다. 그리고 사람들은 그리고 한 경에 전기를 가득했다. 그는 것은 사람들은 사람들이 모르는 것이다.	
: 성도 함께 살아보고 있다면 그런 그렇게 되는 무슨 사람들은 모양하다고 다.	
	경우에 살림생들을 살을 하는 아들은 것.
공격이 한 없다는 전환 공항이 무료하고 문제 항공을 하는데 그렇다.	
- 보통하게 하고 통해 있는 설립 등에는 고향하게 되었다. 그리고 말로 하는 것은 클릭하게 되었다. - 사람이 하면 하는 것 같아 하는 것을 하는 것이 되었다. 그 사람들은 사람들이 되었다. 그 사람들이 되었다.	
됐지도를 하고 하는 하는 것이 되는 모든 사람들이 되었다.	
- 사용 26 등 16 전시 등에 가는 사람들은 물을 하는 것이다. 그는 것이다는 것이다는 것이다. 	발표하면 되었습니다. 그 그리는 이번 시간
그릇 하는 사람이 살아 하는 아들이 얼마를 하고 있다고 있다.	
교회 하는 경험하다는 경기 등에 가는 사람들은 중화가를 사람들이 하지만 중하는 것이라는 사람들이 하지 않는 것을 다 되었다. 물론 사용하다 하는 것은 하는 이 교육 중화가는 회사들이 중국 기류를 가득을 하는 것을 모음을 하는 것을 하는 것이다.	
- 전문 이 이 등 보이 되었습니다. 그는 사람들이 살 경우를 보는 것 같아 되었습니다. 그는 사람들이 다른 사람들이 되었습니다. 	
	네 본 기계를 가득하는 글로그를 가는 것이
	이 보통한 경험 경험 등록 모양 살았다. 그리
하는 이 경험을 가는 것이 하는 것이 되었다. 그 사람들은 이 나는 기를 받는 것이 되었다. 그 모르는 것이 되었다. 그는 이번 물병을 들었다. 2000년 이 전에 되는 것이 같다. 물병에는 이번이는 하면 보였다. 1982년 및	
	얼마 저 그 있는 그를 맞추었다.
마음 사용을 받아 얼굴을 받아 다른 이번 생각 사용하다. 발생들을 하는 것은 말이 되는 것은 말이 되었다. 그는 것은	
- 이번 전 생물에 대한 성격에 되었다고 있는 생생님을 통합하는 이 이번 그 이번 보고 있다. 그 사람들이 하였다. - 이번 - 사람들은 사람들이 가장하는 것이 되었다고 있는 것이 되었다고 있는데 보고 있다. 그 것이 되었다.	
- 15 - 15 - 15 - 15 - 15 - 15 - 15 - 15	생물 다음 가는 사람들은 사람들이 하는 것 같아 있다. 사람들이 다음하는 것 같아. 한 바람들은 생물이 되는 것은 하다 하나라는 것이 하나가 되었다.
	상품을 하는 반장을 보면 하는 생활이 되었다.
그래요 그 항문 동안된 본 하면 하면 하는데 얼마나 되었다.	
고, 배송왕이 교통 프로그램 생각하다. 이 작가 많은 사이 하지는 사람들을 되었다. 얼마 보는 사람이 나를 모르는 것이다. 그런데 사람들 교육사업 사이 하는 사람들은 사람들도 보는 사람들은 사람들이 되었습니다.	
	호텔 (1985년 - 1985년 - 1 1985년 - 1985년
医乳腺囊膜炎 医二氏性 医异对氏 医动物性 医动物性 医多种性病性 医耳耳氏 医脱氧苯甲磺磺胺基氏乳糖尿	医克勒特斯氏 医自肠结肠 医二氏性 医电压性



6.2 Geothermal Power Plant

For the Philippines, not rich in energy resources, the geothermal power is an important indigenous energy source and the potential in the country is said to be 200,000 MW-century. Should one tenth of the potential be effectively developed, the available energy would be as large as 20,000 MW for a century operation.

The Philippines has been suffering from the extreme shortage of foreign exchange since her economic crisis in 1983. In such economic situation, the geothermal power generation, which can produce electric energy from the indigenous energy resource and does not require precious foreign exchange like the thermal power, has come to play an important role year by year. In the Power Expansion Program formulated by National Power Corporation (NAPOCOR) in 1991, the development of the geothermal power makes the center with a high priority together with the coal-fired thermal power plants.

There are two geothermal power plants in the Luzon Grid, Tiwi in Albay Province and Mak-Ban at Bay and Calawan in Laguna Province. The installed capacity of each power plant is 330 MW, or 55 MW x 6 Units (660 MW in total). The installed capacity of these power plants has the share of 15% of the system total and the annual generation 24% in 1990. The capacity factor in 1990 recorded 68% in Tiwi and 88% in Mak-Ban, while 85% is generally used in the installation planning in Japan. Since the average capacity factor of the 10 best power plants in the Luzon Grid was 55.8% (in the same year), both Tiwi and Mak-Ban were operated at more than the average.

The reason why the capacity factor of Tiwi was conspicuously lower than that of Mak-Ban is the insufficient steam supply in the Tiwi geothermal area. If the necessary quantity of steam supply is available, Tiwi may be operated with a capacity factor higher than 85%.

For reliable operation of the geothermal power plants at the rated output, the following essential conditions should be satisfied.

- 1) The necessary quantity of geothermal steam supply is always secured.
- 2) The steam purity at the turbine inlet is sufficiently high.
- 3) The equipment and facilities are properly operated and periodically maintained and there is no factor to hamper the operation.
- 4) The spare parts are readied in the store.

Items 1) and 2) above are excluded from the discussion in this report since these are the matters to be handled by PGI (Philippine Geothermal Incorporated), the steam supplier, and not by Tiwi and Mak-Ban Power Plants. Only the review of the steam supply plan of the steam supplier is made in this report.

Table 6-2-1
SUMMARY OF GEOTHERMAL POWER PLANT FACILITIES

				OTHERMAL		γ							TURBIN	E					GENEF	RATOR		
POWER PLANT	PLANT OUTPUT	PRO		MAX.MIN	WELL	TOTAL STEAM FLOW	HOT- WATER	CYCLE	COOLING TOWER	UNIT No.	TYPE	RATED OUTPUT	PRESSURE	STEAM TEMPERA- TURE	EXHAUST PRESSURE		MANUFAC- TURER	RATED CAPACITY			MANUFAC- TURER	COMMISS
	kW		DEPTH m	DEPTHS m		t/h	FLOW t/h					kW	kg/cm2	C	mmHg.abs	rpm		kVA	kV	Hz	· - · · · · · · · · · · · · · · · · · ·	
	KW .			Att				SINGLE FLASH	CROSS FLOW INDUCED DRAFT	1	DOUBLE FLOW	55,000	5.68	162.3	101.6	3,600	M.H.I.	68,750	13.8	60	MITSU- BISHI ELECTRIC	SEP 1979
								DO	ро	2	DO	55,000	5.68	162.3	101.6	3,600	DO	68,750	13.8	60	DO	NOV 1979
	222 222	E 0		MAX. 3,141	21	3,249		DO	DO	3	DO	55,000	5.68	162.3	101.6	3,600	DO	68,750	13.8	60	DO	AUG 1980
AK-BAN	330,000	58		MIN. 655		3,243		DO	DÇ	4	DO	55,000	5.68	162.3	101.6	3,600	DO	68,750	13.8	60	DO	OCT 1980
·			:					DO	DO	5	DO	55,000	5.68	162.3	101.6	3,600	DO	68,750	13.8	60	DO	SEP 1984
		(SEP) (1991)						DO	DO	6	DO	55,000	5.68	162.3	101.6	3,600	DO	68,750	13.8	60	DO	DEC 198
								SINGLE FLASH	CROSS FLOW INDUCED DRAFT	1	DOUBLE FLOW	55,000	6.10	160.6	101.6	3,600	тоѕніва	69,000	13.8	60	TOSHIBA	JAN 197
								DO	DO	2	DO	55,000	6.10	160.6	101.6	3,600	DO	69,000	13.8	60	DO	MAY 197
				MAX.				ро	DO	3	DO	55,000		160.6	101.6	3,600	DO	69,000	13.8	60	DO	JAN 198
TIWI	330,000	77		2,970 MIN. 457		2,360		DO	DO	4	DO	55,000	6.10		101.6	3,600	DO	69,000	13.6	60	ОО	APF 198
	-							DO	DO	5	DO	55,000	6.00	164.4	101.6	3,600	DO	69,000	13.	3 60	ро	DE 6
								DO	DO	6	DO	55,000	6.00	164.4		3,600	DO	69,000	13.	8 60	DO	MAI 198

6.2.1 Present Situation and Problems in Tiwi Geothermal Power Plant

1. Outline of Tiwi Geothermal Power Plant

The Tiwi Geothermal Power Plant is located in Albay Province at the southernmost part of Luzon Island. The area is famous as the hot spring resorts since old times. The rated output of the 6 units is 55 MW each, and the commissioning dates are as tabulated below:

<u>Plant</u>	<u>Unit</u>	Commissioned in
A	Unit-1	January 1979
A	Unit-2	May 1979
В	Unit-3	January 1980
В	Unit-4	April 1980
С	Unit-5	December 1981
C	Unit-6	March 1982

Units 1 to 4 were originally designed as the double flash system, but converted later to the single flash system. Units 5 and 6 were designed as the single flash system from the beginning.

For extraction of the non-condensable gas (NCG), the steam ejector system was adopted and no gas compressor was installed for all the 6 units.

It is essential to increase the emission height for better dispersion into the air and decreased ground concentration of the non-condensable gas (NCG). For this purpose, the utilization of the heat of the secondary steam of the steam ejector was intended, and the after-condenser was omitted. As a result, the steam from the ejector is discharged directly into the air, and the condensed water wets the surrounding and causes accelerated corrosion of outdoor equipment, piping, structures, measuring instruments, etc.

2. Geothermal Steam Supply

(1) Steam Requirement

The steam supply necessary for operation at the installed capacity of 330 MW (55 MW x 6 Units) is 3,125 t/hr, and the steam consumption is 9.47 kg/kWh. (Refer to Table 6-2-2)

(2) Steam Supply

The geothermal steam available from PGI, the steam supplier, is 2,360 t/hr as of the end of July 1991. Thus, it is short of the steam requirement by 765 t/hr, or 80 MW equivalent. According to the plant operation log on July 29, 1991, the peak load was 251 MW and the capacity factor was 70% as shown in Table 6-2-3.

As for the steam production, the past records show that the production declines by 7% or more per year as shown in Fig. 6-2-1.

(3) Geothermal Reservoir Capacity

a. Geothermal Reservoir and Production Wells

(a) The volume of the geothermal reservoir is estimated at 15 km³ (16.5 km² x 0.9 km). The mass of geothermal fluid is estimated to be 6.5 x 10¹¹ kg with a heating value of 2.75 x 10¹⁸ J, or 6.75 x 10¹⁷ kcal. Assuming that the plant operation life of 35 years, the area was assessed to have the possibility of development of a 500 to 800 MW power plant. Based on the assessment, the well drilling was started in 1971 and a total of 134 wells have been drilled to date. The largest depth of drilling was 2,970 m and the shallowest 457 m, and the highest temperature was recorded at 300°C and the average output per production well was 7 MW.

- (b) The number of the wells currently used for power generation is 77 of production wells and 7 of reinjection wells. The remaining 50 wells have been discarded. The main reason of the desertion is the intrusion of cold water into the reservoir, and about 40% of the reservoir was deteriorated by the cold water as shown in Fig. 6-2-2.
- (c) Steam is now extracted from the west side area of the reservoir, and 75% of the total steam consumption is extracted from the area equivalent to 30% of the total reservoir. The remaining 25% of the steam is extracted from the reservoir deteriorated by the cold water intrusion and the average output per production well in this area has decreased to 3.3 MW. Because of the transfer of the steam extraction area to the west, the pipelines of the gathering system became longer, and the longest gathering system is 9 km and the shortest 4 km, and the total piping length is 56 km.

Reassessment of Geothermal Reservoir

Recently, Electroconsult of Italy (ELC), carried out the study and investigation of the potential of the reservoir and power development scale in Tiwi Area, and presented the final report with the title of "Reservoir Assessment of Tiwi Geothermal Field". According to the report, the stored heat in Tiwi Geothermal Reservoir is estimated at 46,000 GWh in electrical energy and 250 MW x 25 years in plant capacity.

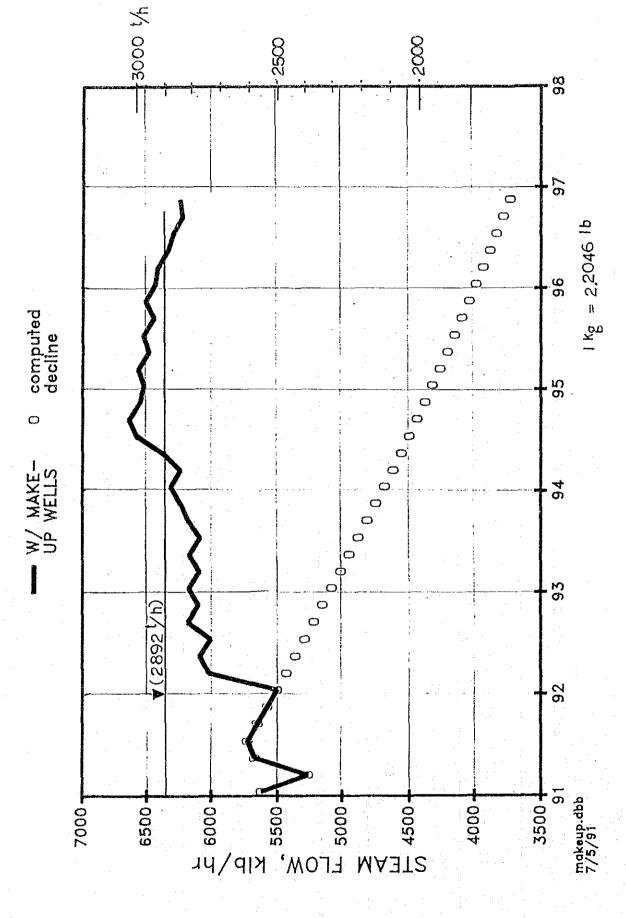
Table 6-2-2 Steam Requirement of Tiwi Geothermal Power Plant

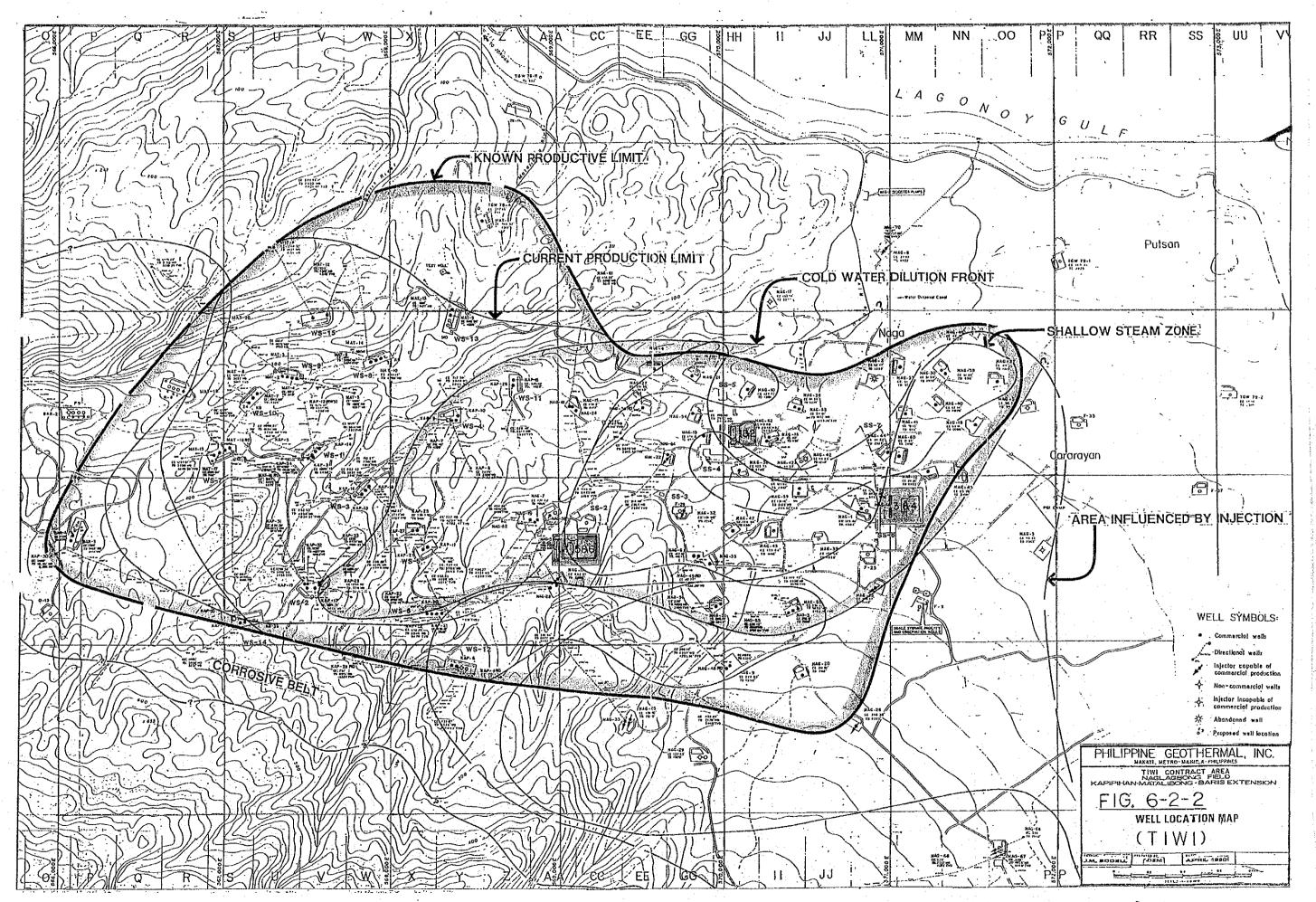
Unit No.	Turbine	Steam Ejecto	Ejector (t/hr)	Gland Steam	Total
	(t/hr)	1st Stage	2nd Stage	(t/hr)	(t/hr)
1	447.93	32.64	38.36	1.12	520.05
2	447.93	32.64	38.36	1.12	520.05
ĸ	447.93	32.64	38.36	1.12	520.05
7	447.93	32.64	38.36	1.12	520.05
Z.	432.47	36.42	52.39	1.12	522.4
9	432.47	36.42	52.39	1.12	522.4
Total	2,656.66	203.4	258.22	6.72	3,125.0

Table 6-2-3 The Generation Record of Tiwi Geothermal Power Plant on July 29, 1991

		·						
	Remarks							
	Daily Net Generation (MWh)	1,182.7	1,182.5	1,078.1	•	1,250.9	521.3	5,216.5
	Daily Gross Generation (MM)	1,221.9	1,221.5	1,178.5	•	1,300.3	553.6	5,475.8
,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	Bowl Press. (kg/cm2g)	5.95	5.95	5.95	t	5.65	5.65	
	Condenser Vacuum (mmHg)	665	654	249	I	654	663	
	Peak load (MW)	52	51	48	•	55	45	251
	Capability (MW)	50.92	49.83	48.47	Stop	52.66	43.70	
	Unit No.	.	2	ମ	7	ıŊ	9	Total

FIG. 6-2-1 TIWI STEAM SUPPLY PROJECTION





3. Present Status of Steam Supply and Power Plant Facilities

(1) General

The total number of shutdowns of Units 1 to 6 in Tiwi Geothermal Power Plant in 5 years from 1986 to 1990 was 325 and the total shutdown period was 1,476 days, which is equivalent to 13.5% of the total operating days as shown in Table 6-2-4. (A plant shutdown of shorter duration than one day is counted as one day.)

The causes of shutdown are classified in the following: (Ratio is shown in the percentage of shutdown days.)

Cause of the Plant Shutdown	<u>Ratio</u>
Plant overhaul/maintenance	57.4%
Power System faults	12.42
Troubles of PGI steam supply system	10.2%
Cleaning of steam strainers	7.12
Sticking of MSV and CV, and governor troubles	4.42
Hotwater pump troubles	3.0%
Troubles of exhaust stack	1.8%
Plant electrical system faults	1.6%
Condenser vacuum low	0.7%
Instrument air supply system troubles	0.7%
Cooling water pipeline troubles	0.5%
Spark of generator slip ring carbon brushes	0.2%

(2) Mechanical Facilities

a. Shutdown for Plant Overhaul and Maintenance

The number of plant shutdown days for the plant overhaul/maintenance accounts for 57.4% of the total shutdown days. The frequency of overhauls varies depending on the units, and the period of overhaul also varies greatly from 2 to 13 weeks depending on the units. The frequency of overhauls in Japan is generally

standardized to be once in two years and the period required for the overhaul is 16 days for a plant with a spare rotor and 22 days for one without a spare rotor as shown in Fig. 6-2-3.

The period of overhaul depends on the restoration of the turbine rotor/diaphragms, and even in the worst case of rubbing of the rotor due to the accumulation of scale, the unit could be put back into operation by replacing the rotor with the spare rotor, if one is available in stock. Then the damaged rotor can be repaired later, and the damage by the trouble could be minimized.

Therefore, if PGI can guarantee the supply of sufficient steam for the operation of all the 6 units of Tiwi Power Plant into the future, it is advisable to purchase one spare rotor and one set of spare diaphragms in this rehabilitation project.

It is said that at the power plant where the total silica (SiO₂) and chloride (Cl) content in the steam is 1 to 2 ppm, satisfactory operation of the plant can be maintained with an overhaul per 2 years. Thus, further improvement of steam quality and securing of the necessary steam is imperative for decreasing the frequency of overhauls by half and increasing the capacity factor.

In 1990, the steam scrubber system was installed in the 1st stage drain scrubber steam outlet pipes of Units 1, 2, 4, 5 and 6, and the test of removal of scaling elements in the steam has been continued. The effect of the steam scrubber system is not known definitely, since the test period is not long enough. It is expected, however, that the plant derating rate due to scaling, which was about 25% to 27% per year before the installation, is likely to decrease by half.

b. Troubles on PGI Steam Supply System

In case where the rupture disc installed as the safety device on the pressure vessel of the steam gathering system was burst, it was necessary to shutdown the unit for the replacement. Now, however, the device has been improved and the replacement of burst rupture discs can be made without unit shutdown.

c. Steam Quality

The clogging of the steam strainer at the turbine inlet and mal-functioning of MSV and CV would be eliminated if the steam quality is improved. And also the sticking of the sliding parts of MSV and CV would be prevented by adding the oiling device.

d. Condenser Vacuum Low and Cooling Water Pipeline Troubles

Carbon steel (SM-41A) is used for U-seal pipes and cooling water pipes. It was judged that the carbon steel material could be used without troubles for the cooling water system, if the pH control of the cooling water was made satisfactorily. Occasionally, however, for lack of chemicals for pH control, the pH of the cooling water dropped to less than 3. As a result, the cooling water pipe was corroded and punctured, entailing vacuum low and water leakage.

Corrosion of the cooling water pipes and hot water pipes is so serious that more than 40% of the pipe wall thickness has been lost, and in the extreme case the corrosion has reached more than 74% of the original thickness as shown in Fig. 6-2-4.

(3) Electrical facilities

The plant electrical facilities can be grouped into those within the powerhouse and those in the switchyard. Problems common to both facilities in this power plant are corrosion of conductors, terminals, insulations, supports, overhead ground wires, etc., due to $\rm H_2S$ gas contained in NCG, which cause misoperation of relays, mal-operation of the equipment, broken cables, insulation breakdown of insulators, etc.

Tiwi Power Plant is located at the southernmost part of Luzon Island, and it is connected to the major power demand area of Metropolitan Manila by quite long transmission lines of 341 km. The longer transmission lines involve higher probability of troubles in the power system, and the power plant experiences an annual average of 4 to 5 plant trips due to the power system faults.

The problems with electrical facilities and countermeasures are discussed in Section 4.

The frequency and number of days of the plant trips by causes are shown in Table 6-2-4 "Summary of Plant Shutdowns".

Table 6-2-4 Summary of Plant Shutdowns

										:					(1/2)
						Tiwi	i Power	er Plant	ınt						
Cause of Shutdown	Year	ď	Unit 1	Unit	t 2	Unit	ب ب	Uni	Unit 4	Unit	t 5	Unit	0 It	Tot	Total
		Times	Days	Times	Days 1	Times	Days	Times	Days	Times	Days	Times	Days	Times	Days
Troubles of PGT Steam	1986	,	,	,	,		-	c	c	-	-	-	-		
Supply System	1987	l M	1 4	1 (1	1 4	თ	71	, го	26	4 0	1 4	4 0	4 0		
	1988		H	 	H	H	Ŋ	ന	ന	m	ဖ	~ ~	7		
	1989	8	11	m	m	0	0	0	0	0	0	0	0		
	1990	0	0	èΩ	4	4	10	0	0	0	0	-1	ન :		
	Sub-	80	18	77	14	8	32	8	62	٥	21	4	4	45	151
	total			٠										(13.8%)	(10.2)
Plant Overhaul/	1986	0	0	0	0	2	6		25	0	0	0	0		
Maintenance	1987	m	4	ო	97	Н	26	Н	31	H	61	0	0		
	1988	Н	~ 1	67	46	, -1	83	н	35	2	36	0	0		
	1989	7	11	7	27	Н	0	H	15	0	0	~1	w		
	066T	0	0	Н	74	Н	54	гH	4	0	0	2	¢8		
	-qns	∞	18	80	244	4	177	5	110	9	100	8	54	28	846
	total	:												(8.7%)	(57.4%
Power System Faults	1986		:												
	1987	н (ਜ (i ¢	급 (e-	i f	ស្ត	٥ ا	⊣ \	37	~ 1 T	~ l		
	1 4 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	4 v u	ი « ⊣	5 Y	າ ແ	~ ~	- σ	7 6	7 6	٦ ۲	۲ ا	ر د	77		
	0661	0 0	'nν) 	0.04	. 2	n en	1 (1)	l M	н	8	,	. 23		
	-qns	19	22	21	24	17	20	21	36	21	56	13	25	118	183
	total													(36.4%)	(12.42)

Table 6-2-4 Summary of Plant Shutdowns

(2/5)

						Tiwi	Power	r Plant	L L						
Cause of Shutdown	Vear	Unit	1t 1	Unit	2	Unit	3	Unit	7	Unit	t 5	Unit	t 6	Total	8.1
		Times	Days	Times D	Days T.	Times Da	Days Ti	Times D	Days T	Times I	Days T	Times	Days	Times	Days
Cleaning of Steam Strainers	1986	8	34	н	2	0	0	0	0	0	0	0	0		
	1987	4.	ф.	Н (- 1 (0 :	0.	⊢ •	ന (٥,	0.	· •	٥,		
	988	or (*	4 0	ባ ጣ	×		ታ -	N C	N C	ı c	-1 C	⊣ ⊢	ч с		
	0661) ri	- 2 1) <†	ιŃ	10	40	0	0	> r1	วฑ	40	10		
									}						
	Sub-	24	89	14	20	2	lΩ,	m	ω:	7	-3*	7	m	747	105
	total								. •	-				(I4·4Z)	(7.1%)
Sticking of MSV & CV	1986														
	1987	0	0	H	ന്	0		0	0	:	0	0	0		
	1988	0	0	⊢ 1	m	0	0	0	0	r-i	H	0	0		
	1989	 1	Н	0	0	-4	2	0	0	0	0	гĦ	7	٠	
	1990	Н	r-i	0	0	0	0	0	0	0	0	~	ģ		
	Cith		6	,	y	6	,	c	c		۲	٠		α	3/6
	10 4	1.	3	1	>	1	ı	,	>	4	-	1	1	, ,	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
	T S C C S T													(46.7%)	(V) . I /
Governor Troubles	1986	0	0	0	0	-	H	0	0	0	0	0	0		
	1987	0	0	Ö	0	0	0	0	0	0	0	0	0		
	1988	w	Q,	0	0	H		,I	, -1	rH	0	۵	0		
	1989	9	11	2	7	ന	4	H	2	0	10	0	0		
	1990	0	0	0	0		0	0	0	0	0	0	0		
1	Sub-	12	20	2	2	2	9	2	6	1	01	0	0	22	77
	total	l _{an} r			•									(6.8%)	(2.8%

Table 6-2-4 Summary of Plant Shutdowns

(3/2)

Cause of Shutdown Year Unit 1 Unit 2 Unit 4 Unit 5 Unit 6 U		•	•				Tiwi	i Power	er Plant	nt		• •		•		
Pump Troubles 1986 0	Cause of Shutdown	Year	Uni	r :	Unit	,	Uni	1 1	Uni	t 4	Uni		Uni	j i	Tot	Total
Pump Troubles 1986 0 0 0 0 0 0 0 0 1 1 0 0 0 0 0 1 1 1 0				ays	imes I									Days	Times	Days
Vacuum Low 1986 0 0 1 1 1 1 2 0 0 0 0 0 0 0 0 0 0 0 0 0	Hot Water Pump Troubles	1986	O	٥	0	0	0	٥	0	0	r-!	H	Q	0		
Vacuum Low 1986 0 0 1 1 1 2 1 4 1 1 0 0 0 0 1 1 1 1 2 1 4 1 1 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	•	1987	0	0	Н	H	· H	8	o	0	0	0	0	0		
Vacuum Low 1989 0 0 0 0 1 17 1 1 0 0 0 0 0 0 0 0 0 0 0		1988	0	0	Н	러	Н	8		4	٦	~	0	0		
Vacuum Low 1986 Vacuum Low 1986 1989		1989	o-c	0 0	۰,	٥ ،	нс	77	H -	ન. 동	00		00	00		
Sub-total 0 0 3 3 21 3 19 2 2 2 0 0 Vacuum Low 1986 1987 0		7	,	>	4	d:	,	•	₹ .	t 1	>	>	>	•		
Vacuum Low 1986 1986 0 0 1 2 0 0 0 1 1 1 0 0 0 0 1 1 1 0 0 0 0		Sub-	0	0	ო	е	en .	21	m	1.9	2	2	0	0	11	45
Vacuum Low 1986 1987		total													(3.42)	(3.0%)
1987 0 0 1 2 0 0 0 1 1 1 1 1 1 0 0 0 1 1 1 1	1	1986														
1988 0 0 0 0 0 1 1 1 1 1 0 0 0 1 1 1 1 1 1		1987	0	0	П	2	0	0	0	0	Н	Н	0	0		
1989 1 3 0 0 0 0 0 0 0 0 0		1988	0	0	0	0	0	o	러	H	Н	Н	0	0		
Sub- 1 3 2 3 1 2 1 1 2 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		1989	H	ന്	φ	0	0	0	0	0	0	0	0	0		
Electrical System 1986 0 0 1 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		1990	O	0	·H		Н	8	0	0	0	0	0	0		
Electrical System 1986 0 0 1 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		-qns	П	3	2	3		2	П	н	2	2	0	0	7	11
Electrical System 1986 0 0 1 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		total							٠.						(2.21)	(0.7%)
1987 0 0 1 1 1 1 0 0 2 2 2 2 2 2 1 1988 1 1 2 3 0 0 1 1 1 1 2 2 2 2 2 2 2 1989 0 0 0 0 0 0 0 2 2 2 0 0 0 0 1990 1 1 0 0 0 1 1 1 0 0 0 1 1 2 2 2 2 3 3 3 3 5 5 5 5 5 5 5 5 5 5 5 5	Electrical	1986	0	0	Н	гч	0	0	0	0	0	o	0	0		
1988 1 1 2 3 0 0 1 1 1 3 2 2 2 1 1 1 1 3 2 2 2 2 1 1 1 1		1987	0	0	Н	н	-d	H	0	0	7	2	2	7		
0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 1 1 1 0 0 0 0 0 1 2 2 0 0 0 0		1988	 1	Н	2	ന	0	0	H	,	Ħ	m	7	2		
1 1 0 0 1 1 0 0 0 1 2 2 2 4 5 2 2 3 3 5 5 6		1989	0	0	0	0	0	0	. 7	~	0	0	0	0		
2 2 4 5 2 2 3 3 3 5 5 6		1990	H	н	0	0		ਜ	0	0	0	0	러	2		
		-qns	2	2	7	ß	2	2	m	60	m	5	ľ	٥	61	23
		total										-			(2.8%)	(1.6%)

Table 6-2-4 Summary of Plant Shutdowns

(4/2)

Cause of Shutdown Year Instrument Air Supply 1986 System Troubles 1987			1												
Supply	T	Unit	I	Unit	8	Unit	ო	Unit	7	Unit	20	Unit	t 6	Total	F
Supply		Times D	Days T:	Times D	Days T	Times Da	Days T.	Times Da	Days Ti	Times Da	Days T.	Times	Days	Times	Days
	36	0	0	: -1	-	Н	r=1	٥	0	0	0	0	0		
-	37	0	0	0	0	0	0	0	0	· r-i	r	Н	н		
1988	88	0	0	0	, O	Ο.	0	0	0	0	0	0	0		
1989	60	0	0	0	0	o,	0	0	0	7	4	М	2		
1,990	06	0	0	o ,	0	o ;	0	O	0	0	0	0	0		
-qns	-0	0		-	-			0	0	m	2	2	3	7	100
total	tal													(2.1%)	(0.72)
Cooling Water Pipeline 1986	36	0	0	0	0	0	0	o	0	0	0	0	0		
	87	0	0	0	O	2	4	0	0	O	٥	0	٥		
1988	28	0	0	0	0	0	0	0	0	۳ł	н	0	0		
1989	ტ	- -1	ო	0	0	0	0	0	0	0	0	0	0		
066T	06	0	0	0	0	0	0	0	0	0	O	0	0		
Sub-	p-	1	m	0	0	2	4	0	0			0	0	4	80
	total	•	- 1. - 1.		1,	÷ ,								(1.2%)	(0.5%)
Spark of Generator Slipring 1986	36	0	0	0	0	0	0	0	0	0	0	0	0		
1.1	87		0	0	0	0	0	0	0	0	0	0	0		
1988	88	0	0	0	Ö	0	0	دا	~1	0	0	0	0		
1989	89	0	0	0	0	7	 7	0	0	0	0	0	0		
1990	06	0	0	o , ,	0	0	0	0	0	: ¹	0	0	O _P		
Sub-	<u>-</u> 0	0	0	0	0	2	2			0	0	0	0	3	m
tot	total		i											(26.0)	(0.22)

Ash Vice

Times Days Times Days Times Days Times Days Times Days Unit 6 Unit 5 Table 6-2-4 Summary of Plant Shutdowns Unit 4 Tiwi Power Plant Unit 3 Unit 2 Unit 1 Year 1988 1989 1990 1987 Troubles of Exhaust Stack Cause of Shutdown

Days

Times

Total

(2/2)

	Sub- total	0	0	2	21 0	0	0	0	0	m	e.	н .	2	6 (1.8%)	26 (1.8%)
														-	
Grand Total		2.2	382	99	260	64	274	4.7	240	48	260 49 274 47 240 48 210 38	88	110	325	1,476
	14			;	٠		-				•				

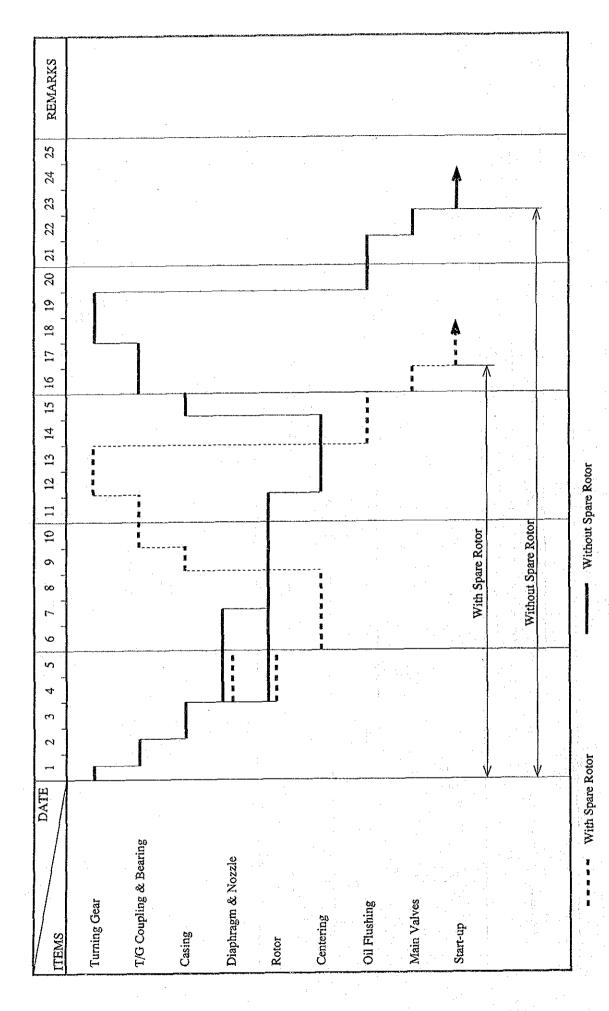


Fig. 6-2-3 Rehabilitation Work Schedule on 55MW × 1 unit Geothermal Power Plant (Actual Results)

HOT WATER PIPE THICKNESS RECORD

(EMBEDDED PIPE)

Equipment -

TO POWERHOUSE DRIFICE

TO COXUME TOWER

NOTE: Im interval ong. thickness. IT mm

COLD WATER THICKNESS RECORD (EMBEDDED PIPE) UNIT # 1

Equipment.

TO CUCLING JOWER KEIERENCE ORIFICE TO POWERIORISE

orly. thickness - 1510m

וויניםנאפן	
Ë	
NOTE;	
~	

MEYERS	-	TO POWE	POWERHOUSE		F	TO COOLING TOWER	IG TOWER	
	Ą	8	ပ	۵	٧	8	υ	٥
: 15					13.1	9.7	8.5	11.60
-					13.68	13.10	8. °	10.0
¥						8.96	8.9	
12							6. 23.	9.80
==					13.32	10.58	6.23	11.72
		-				12.9	8.30	12.74
7						8.5	74	11.13
ź						2.5	8,48	4
72						7.2	6.9	
×		. :						
j.								

2-0-0
<u>ن</u>
ட

9.7Z 10.6T

13:1 4:1

12.4

Average 12.06 12.41 10.43

<u>=</u>

Total Average

MB GEOTHERMAL PLANT UNIT NO.

PLANT

HOT B COLD PIPELINE

DATE

PANT	MB GEOTHERMAL ILANT	ILANT UNIT No. 1
EQUIPT.	HOT & COLD PIPE LINE	
TYPE		
PREP'D BY.	LANG! DATE	
CHECK'D BY.	DATE	

		TO	POWERHOUSE	USE	_	TO COOL	COOLING TOWER	*
2	¥	ø)	ပ	O	×	Ø	U	۵
_	12.6	13.8	12.1	13.3.	11.3	11.6	6.5	6.5
7	12.7	14.6	9.9	12.7	10.6	11.5	0.9	10.6
E)	12.5	င် ရ	10.2	12.4	12.1	11-7	7.6	10.2
₹	11.5	11.4	10.1	10.6	11.2	12.0	6.7	9.4
ĸ	11.5	12.8	10.3	11.9	12.14	13.6	10.2	11.0
9	11.5	10.8	11.2	10.9	13.9	6-41	10	13.7
7	11.1	11.6	9.6	11.1	10.1	13.1	10,2	12.5
8	12.1	12.7	10.1	11.7	13.8	7.8	6.74	9.34
G	12.7	12.1	8.6	12.1		4.3	5.2	5.6
10	13.2	14.5	4.6	12.9	7.2	12.7	11.5	0.0
- 1	12.5	12.1	10.7	12.7	9.3	12.2	12.3	10.3
12	10.6	13.1	11.6	14.6	11.1	9.8	9.6	11.3
13	12.3	11.4	10.5	13.08	12.2	11.6	12.1	16.4
4	12.4	12.1	-9-01	14.4	12.2	11.0	6.7	11.6
õ	11.7	12.4	10.4	12.1	11.8	0"Z1	12.4	4.21
õ					12.7	2.41	1.2.1	11.3
17					13.6	14.8	11.52	17.3
9	_				14.7	13.6	11.08	15.6
6					13.1	13.7	11.6	13.6
50					9.5	12.0	11.2	12.3
						7.7	10.9	8,2
					¥		0 1	¥

4. Problems with Steam Supply System and Power Plant Facilities and Countermeasures

(1) Mechanical Facilities

a. Overhaul

The steam quality at Tiwi Geothermal Power Plant has been improved since the commissioning, and further in 1990, the steam scrubbing system was added and good results are obtained. Based on the operation records to date, it is judged that the safety of the plant will be maintained with the overhaul once or twice a year. Actually, however, there occur the clogging of the turbine inlet steam strainers and sticking of MSV and CV rather frequently, and further improvement of steam quality is needed.

b. Improvement of Steam Quality

With some units in Tiwi and Mak-Ban Power Plants, the tests of the steam scrubbing system as a means of steam quality improvement have been continued. As one year has passed since the tests were started, the test results were processed and the advisability of the addition of the steam scrubbing system to other units was studied. The past record revealed that there was decline of the output due to scaling even with the steam scrubbing system. The improvement and maintenance of the steam quality should be made on the responsibility of PGI, the steam supplier.

Recently, the water washing system was developed, and it became possible to remove the scale deposited on the turbine nozzles and blades without shutting down the unit. As a means of protection of the plant, the water washing system should be added for the extension of the continuous operation time, prevention of decline of the output and prevention of rubbing of the rotor due to scaling.

c. Lining of Main Cooling Water Pipes

The corrosion of the main cooling water pipes and hot water pipes are conspicuous, and in the extreme case, as much as 75% of the tube wall thickness is corroded. These pipes are buried underground, over which the hybrid type gas compressors are located. Therefore, if the corrosion progresses at the present rate, it is feared that the pipes may collapse under the earth pressure and heavy loads.

It is necessary to line the pipes with stainless steel (SUS 304) pipes of wall thicknesses corresponding to the lost thicknesses and prevent the collapsing and the progress of corrosion.

d. Replacement of Auxiliary Cooling Water Pipes

Epoxy-lined carbon steel pipes are used for the auxiliary cooling water pipes, and the lining has peeled off and the pipes have been corroded.

The Supercoat lined carbon steel pipe has been proved to be very stable against the cooling water in Tiwi Power Plant, and has a high anti-corrosive property. Therefore, it is advisable to replace the cooling water pipes with Supercoat lined pipes, SUS pipes or FRP pipes.

e. Suppression of Algae

Algae growth and mud deposit in the generator hydrogen gas cooler tubes decrease the coefficient of overall heat

transmission. To recover this, tube cleaning is carried out with a decreased output or unit shutdown.

The following two methods are considered as the means of preventing this decrease of the coefficient, and the selection should be made in consideration of the economy and reliability.

Plan 1.

The cooling water system to the H_2 gas cooler and lubricating oil cooler will be modified from the existing open cycle to the closed cycle and the growth of algae will be suppressed by shielding from the sun light.

Plan 2.

The H₂ gas cooler will be equipped with cleaning brushes so that the interior of the tubes may be cleaned automatically and continuously.

f. Improvement of Labyrinth Packing Material

The labyrinth packings of the main shaft of the turbine suffered from severe corrosion, but since the packings were replaced with stainless steel packings, the trouble of the labyrinth packings has been remedied.

g. Installation of Hybrid Type Gas Extractors including $\mathrm{H}_2\mathrm{S}$ Gas Diffusion System

The installation of the hybrid type gas extractors for No. 1, No. 2, No. 5 and No. 6 Units is under way, by which an increase of the output (approx. 29 MW), lowered ground concentration of $\rm H_2S$ gas and prevention of corrosion due to scattered steam condensate, etc. are expected. No. 3 and No. 4 Units still use the steam ejectors which consume a large volume of steam for the extraction of NCG and the condensate

wets the surrounding and causes corrosion.

To solve these problems, one (1) set of hybrid type gas extractor for common use should be added to No. 3 and No. 4 Units also, and an increase of the output (approx. 11 MW) and prevention of the corrosion due to scattered condensate should be achieved. (Refer to Fig. 6-2-5 (1), (2))

h. Partial Modification of Cooling Towers

The forced draft fans, hubs and such rotating parts have suffered drain attacks and the fillers have been severely damaged by long use, and they are already in the condition needing drastic repair.

The cooling towers are of wooden structures and the ceiling boards, side boards, louvers, etc. have been corroded severely by the sputtering water and strong acid droplets scattered from the steam ejectors.

Since the power plant is located right under the route of typhoons, the side boards, louvers, railings, stairs, etc. have been broken or deformed, and the performance of the cooling towers have been damaged and the safety of the cooling towers is in danger.

All the fans, hubs, fillers, side boards, louvers, ceiling boards, railings, stairs, etc. that have been severely damaged should be replaced for recovering the performance of the cooling towers.

Also one third of the upper part of the cooling tower structures and one third of the cooling fan motors should be replaced with new ones.

i. Procurement of Vehicles

At Tiwi Power Plant, there are 255 employees composed of 123 operators, 70 maintenance crew and 62 others. And the power plant has one mobile allocated to Plants A, B and C combined, and the shift operators are reporting to the job getting a lift in the day-shift employees' cars.

The working mode of operators is by the 4 group 3 shift system, but the shift changes are difficult to be made regularly because of difficult transportation.

In some cases, operators cannot help working two shifts continuously. This is a serious problem in the operation of the power plant.

Since the power plant and the residential quarters of the employees are located in the remote area, there is no public transportation available.

And the number of vehicles assigned to the power plants is short, and they are all dilapidated by age and need to be replaced.

For smooth transportation of shift operators and speedy transportation of maintenance crew and security personnel in care of power plant troubles and emergency.

It is advisable to purchase one small bus (capacity: 29 persons) and a jeep (capacity: 7 persons) equipped with a winch.

(2) Electric Facilities

a. Electric Facilities within Powerhouse

(a) Generator equipment

No problem was found with both the stators and the rotors of the generators proper so far. However, as it is more than 10 years already since the commissioning of No. 1 to 4 units, the detailed study on the necessity of the rewedging of stator windings is essential and study on rewinding of rotors, and detail inspection of retaining rings are necessary. Slip rings of the excitation circuit were found to have abrasion by sparks and the brush holders were also damaged by corrosion. Repair of the slip rings, and replacement of the brush holders and brushes are necessary. It was informed by the plant that H2 gas leakage was larger than usual. Therefore, H2 gas seal at the generator stator temperature sensor terminals should be thoroughly inspected. Parts of the AVR also have been corroded to the degree needing replacement.

(b) 4.16 kV and 480 V switchgears and 480 V motor control centers

These equipment are installed in the electric room partitioned from the other sections in the powerhouse and kept at a little higher pressure than the atmosphere by the air conditioners to prevent the atmospheric air from entering. Because the central air conditioners are now out of order and the doors of the electric room are left open, the air of the powerhouse containing H₂S gas enters and gives adverse affects of corrosion and deterioration of the electric equipment, relays, instruments, etc. Though the damage has not been serious so far, the replacement of the air conditioners is imperative.

(c) Addition of generator circuit breaker

As there occur frequent plant trips due to the power system faults, it is advisable to install the generator circuit breakers to facilitate the operation of the plant with the station service load only and to raise the flexibility in the plant operation.

b. Electric Facilities in Switchyard

As mentioned before, the steam and H₂S gas in the ejector exhaust cause corrosion, insulation drop, and malfunctioning of the electric facilities in the switchyard, especially the exposed parts of conductors, insulators, disconnecting switches, overhead ground wires, circuit breakers, control equipment, etc. It is noted especially that soon after the commissioning of the plant, the dielectric strength of insulators dropped because of impurities in steam and steam mist deposited on the surface of insulators, and frequent flash-overs occurred. At present, the problem is minimized by H.V.I.C. (High Voltage Insulation Compound) coated on the surfaces of insulators.

As a fundamental measures, the more effective means of diffusion of the ejector exhaust should be established.

(3) Instrumentation and Control Equipment

Because the H₂S containing NCG discharged from the condenser is not dispersed in the air satisfactorily, several problems have occurred on the control and instrumentation facilities. Especially, the windows of the central control room are kept open to take in the outside air, because all the air conditioners of Plant A, B and C are out of order. Thus, the air contaminated with H₂S comes into the room and causes adverse effects of corrosion and insulation deterioration on the instruments and control equipment in the room. The restoration of the air conditioners is urgently needed. The

details of major problems on instrumentation and control equipment are described in the following.

a. Hotwell Level Control

The automatic level control sometimes malfunctions due to the poor quality of control air. Detailed inspection of the control air system is necessary.

b. Control Board Recorders

Several sets of recorders have been out of order because of servomotor trouble, etc. These recorders should be replaced.

c. Control Board Indicators and Transmitters

Several control board indicators are malfunctioning owing to corrosion and deterioration, and need repair or replacement.

d. Control Air Supply

There are problems with the quality of the control air. Detailed inspection of the air supply system, replacement of filters, and check of dryers are necessary. Inspections of air filters and drain system of the back-up system are necessary, too.

At present, two control air compressors are in operation at each plant, and there is no spare compressor. One spare compressor each for Plants A, B and C should be provided.

e. Chemical Dosing System

The automatic control has been out of order and the system is being operated manually without particular

problems. However, the automatic control system should be restored.

The above problems and their countermeasures are summarized in Tables 6-2-5 and 6-2-6.

Table 6-2-5 Problems and Basic Countermeasures (Mechanical)

Iiwi (1/2)	Remarks							•				
Power Plant:	Reh OH		0	i o	0		0	0	0	0		
Pov	1				•		÷		-			
		ø		0	1		0	0	O	0		
		S	0	0	1		O	0	O	o .		
. :	Unit No.	4	. 1	0	1		0	0	0	0		
	Unit	т	i i	0	Ö		0	o ;	O	0		
		2	l .	•	1		0	0	0	0	- :	
·		Н	F .	O	· I		0	0	o .	0		
	Basic Countermeasure		Procurement of turbine spare rotor, nozzle and diaphragms	Installation of water washing system with demineralizers	Procurement of honing machine		Internal lining of main cooling water pipe with stainless steel	Additional installation of electrolytic protection system	Replacement of aux. cooling water pipeline including the headers	Installation of automatic tube cleaner or modification of cooling water system from open cycle to closed cycle		OH = Overhaul
			(T)	(2)	(3)	4 1		(2)	(3)	(1)		tion
	Problem		Frequent and long overhaul/maintenance shutdowns				Corroded cooling water pipe and vacuum low and water leakage,	in the future		Decreased performance of H ₂ gas cooler by algae growth		Note: Reh = Rehabilitation
	No.		M-1				M-2			M-3		

Table 6-2-5 Problems and Basic Countermeasures (Mechanical)

No.	Problem	Basic Countermeasure		Unit	t No.			R te t	HO.	Remarks
			1	2 3	7	2	و			
И-4	Decreased performance of cooling tower resulting in high cooling water temperature	Replacement of erroded and poor materials	0	0	0	0	٥	o	ì	
K-5	Corroded surrounding equipment by steam splutter from steam ejector	Installation of hybrid type gas extraction system including removal of exhaust steam discharge point to down-stream of cooling tower fans	ı.	0	I	. t	•	o		Common use with unit No.4
M-6 M-7	Difficult operator shift change because of car shortage Steam supplier trouble	Procurement of new vehicles	0	1	1	1	1	o	•	
	1) Geothermal steam short by 80 MW equivalent of output power	Drilling of additional steam production wells	0	0	0	0	O	ı	1	By PGI, steam supplier
	2) Low steam quality	Installation of steam addition scrubber system	1	0	'	į	1	1	1	-Ditto-
	3) Steam supply system trouble	Three (3) small size rupture disks to be fitted instead of one (1) large size rupture disk	o	. 0	0	0	0	ľ	ı	-Ditto-

Table 6-2-6 Problems and Basic Countermeasures (Electrical and I&C)

Power Plant: Tiwi (1/2)

	No.	Problem	Basic Countermeasure		Þ	Unit No.	No.			Reh	НО	Remarks
				H	2	ო	4	۲۷	9			
ja:	(x	Vestly deteriorstion	1) Democratic of respective states					١.,				
1	.	of generator	5	5	5	5	>	5	,	כ		
			(2) Detail inspection of generator	0	0	0	0	ı		o		
•			ind:				•					
의	Z-2	Leakage of ${ m H}_2$ gas		0	٥	0	0	1	ŧ	ı	0	
			cemp. sensor cerminal board, erc.									
(23)	E-3	Generator rotor	Repair and machining of the slip	0	0	0	o	0	0	ŧ,	0	
		slip ring spark and	ring, and replacement of brushes									
		brush and brush holder	and brush holders									
	ļ.	corrosion										
ध्य	7− ∃	Generator exciter	Replacement of corroded parts	0	o	o	o	٥	٥	5	0	
		AVR malfunction										
		> T										
មា	E-5	4.16 kV & 480 V	acement of	0	o	0	0	0	0		0	
		switchgears and	and servicing of contactors,	÷								
		480 V M.C.C. corrosion	relays, etc.									
			(2) Replacement of air conditioner	0	0	0	0	0	0	o	1	
មា	E-6	Switchyard equipment										
		corrosion										
		(1) Corroded	(1) Replacement of defective	0	0	0	0	1	1 -	ı	0	
-		disconnecting	disconnecting switches								÷	
		switches										,
		(2) Circuit breaker	(2) Replacement of circuit breaker	o ·	0	;	t -	,	1	0	ı	
		malfunction										CB for PlantA
			(3) Installation of N.C.G.	0	0	0	Ö	0	0	0	1	
			abatement system									
Įz.	7.7	Thflexible	Installation of ST6 generator	c		c	c	c	c	c	1	1 1 1 1
	. :	Generator Operation	ker	•	; 1	ı)		,		planning

Table 6-2-6 Problems and Basic Countermeasures (Electrical and I&C)

Mo. Problems Basic Countermeasure This is a statement of the control of control system control level control system including piping control air system including piping control air system including piping control air compressors (4) Additional installation of exist. 10-2 Deterioration/corrosion (1) Replacement/repair of recorders control air compressors (2) Repair of air conditioners or o control board (2) Repair of air conditioners or o control board (2) Repair of air conditioners or o control board transmitters (1) Overhaul/servicing of turbine covernor (1) Overhaul/servicing of turbine covernor (2) Training of IkC personnel of challenction of TSI Replacement of automatic or challence of chancel dosing system dosing system dosing system dosing system dosing system dosing system dosing control)												
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hotwell level control system control instrument/control air system including piping (3) Rehabilitation of exist- ing control air compressors (4) Additional installation of control air compressor (5) Replacement/repair of recorders of control board (2) Replacement/repair of recorders Deterioration/corrosion (1) Replacement/repair of indicators/ of control board (2) Replacement/repair of indicators/ of control board transmitters Malfunction of TSI Replacement of TSI Malfunction of (1) Overhaul/servicing of turbine of turbine governor system Malfunction of (2) Training of I&C personnel of the plant Malfunction of (3) Training of I&C personnel of the plant Malfunction of Replacement of automatic ochemical dosing system (PH control)	f.C-1	Malfunction of		0	٥	. 0	0	0	0	e e	0	
including piping (3) Rehabilitation of exist- ing control air compressors (4) Additional installation of		hotwell level control	control system Servicing and repaid	. 0	. 0	0	٥	0	0	ı	0	
Ing control air compressors (4) Additional installation of			including piping Rehabilitation of e	0	0	0	o	o	0	f	0	
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recorders (2) Repair of air conditioners o o of control board transmitters indicators/transmitters Malfunction of TSI Replacement of TSI Malfunction of (1) Overhaul/servicing of turbine system System (2) Training of 1&C personnel of the plant the plant Malfunction of Replacement of automatic o o themical dosing system dosing system dosing system(PH control)	IC-2	Deterioration/corrosion of control board	ent/repair of	0	٥	o	0	. 0	o	o ·	1	Detailed investigation
Deterioration/corrosion Replacement/repair of indicators/ o o control board transmitters indicators/transmitters Malfunction of TSI Replacement of TSI o o governor system (1) Overhaul/servicing of turbine o turbine governor system (2) Training of 1&C personnel of the plant the plant Malfunction of Replacement of automatic o chemical dosing system dosing system dosing system(PH control)	:	recorders	air	0	0	0	o	0		0	ŧ	is needed.
Malfunction of TSI Replacement of TSI 0 0 0 Malfunction of (1) Overhaul/servicing of turbine 0 0 cturbine governor system system (2) Training of 1&C personnel of the plant che plant Malfunction of Replacement of automatic 0 0 chemical dosing system dosing system dosing system(PH control)	IC-3	Deterioration/corrosion of control board indicators/transmitters	Replacement/repair of indicators/ transmitters	0	0	0	· O	0	0	0	i	-Ditto-
Malfunction of (1) Overhaul/servicing of turbine o o turbine governor system (2) Training of I&C personnel of the plant the plant (2) Replacement of automatic o chemical dosing system dosing system (PH control)	IC-4			,	0	o	0	1		0		
system (2) Training of 1&C personnel of chains of 1&C personnel of chains of 1&C personnel of chains of the plant (2) Training of 1&C personnel of chains system dosing system (PH control)	IC-5	Malfunction of	-	0	o	0	.0	o	۰.	ı	0	-Ditto-
Malfunction of Replacement of automatic o o chemical dosing system dosing system(PH control)			Training of I&C personnel the plant	٥		0		O		0	1	· .
	IC-6		Replacement of automatic dosing system(PH control)	0	0	0	0	0	O	0	I ,	

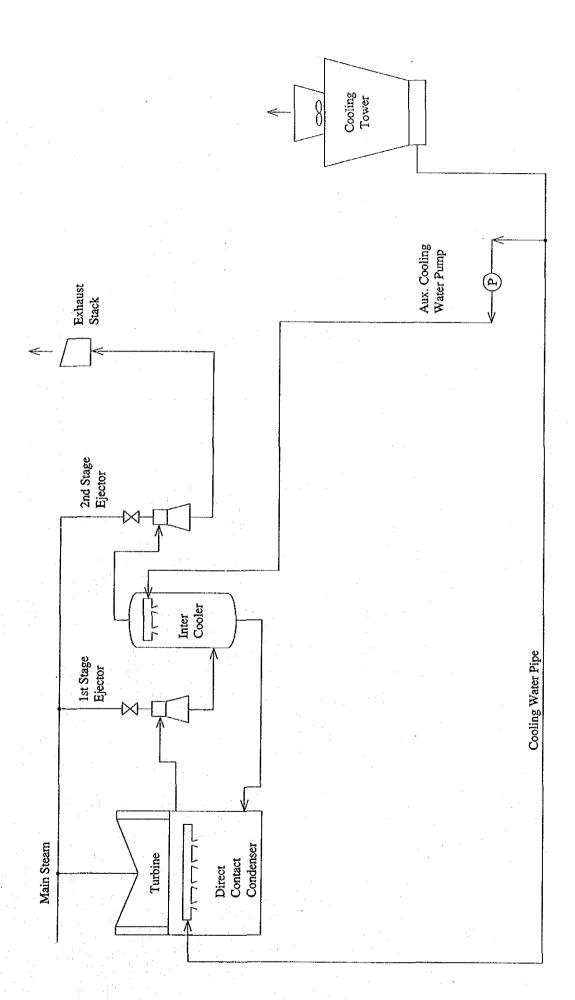


Fig. 6-2-5 (1) Tiwi Geothermal Power Plant Gas Extraction System Diagram (Existing) (No.1 \sim No.6 Unit)

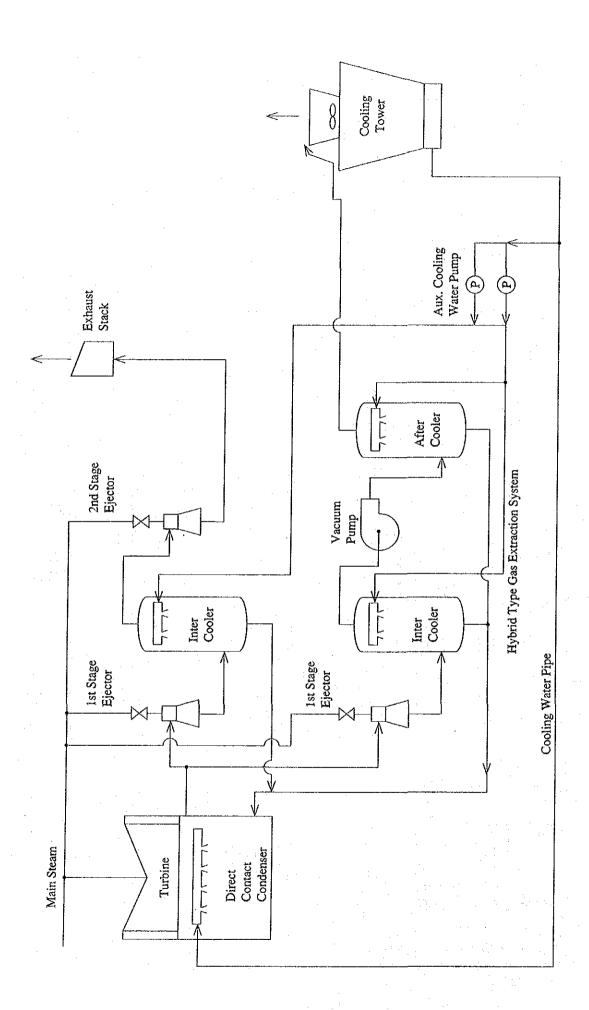


Fig. 6-2-5 (2) Tiwi Geothermal Power Plant Gas Extraction System Diagram (Improvement Plan) (No.1, 2, 5, 6 Unit: Under Construction) (No.3 Unit: Planning) (Common use with No. 4 Unit)

6.2.2 Present Situation and Problems in Mak-Ban Geothermal Power Plant

1. Outline of Mak-Ban Geothermal Power Plant

Mak-Ban Geothermal Power Plant is located at Bay & Calawan in Laguna Province, Luzon, at about 70 km south from Metropolitan Manila. The power plant consists of 3 plants, Plants A, B and C, and each plant has 55 MW x 2 units. The commissioning dates are as tabulated below:

Plant	<u>Unit</u>	Commissioned in
A	Unit-1	September 1979
A	Unit-2	November 1979
В	Unit-3	August 1980
В	Unit-4	October 1980
С	Unit-5	September 1984
C	Unit-6	December 1984

The design of Plant A (Units 1 and 2) and Plant B (Units 3 and 4) is nearly the same. As Tiwi Power Plant, Units 1 to 4 were originally designed as the double flash system but were converted later to the single flash system. Units 5 and 6 of Plant C were designed as the single flash system from the beginning.

With the units in Plants A and B, 3 units each of the non-condensable gas extraction compressors (1st stage to 3rd stage) are installed, but since surging occurs among the compressors and the operation becomes unsteady sometimes, the steam ejectors are used normally.

As a means of getting better diffusion of noncondensable gas from the steam ejector and lower ground concentration of $\rm H_2S$ gas, the exhaust steam from the 2nd stage ejector is directly discharged into the atmosphere, and the condensate of steam wets the surrounding and accelerates the corrosion of the outdoor equipment, piping, structures, measuring instruments, etc.

In Plant C (Units No. 5 and 6), packaged gas compressors are used for NCG extraction and the NCG exhaust is discharged from the top of the cooling tower. Because of the sufficient $\rm H_2S$ gas diffusion, there has been no problems experienced with Plants A and B.

2. Geothermal Steam Supply

There is no indication of shortage of geothermal steam supply as shown in Fig. 6-2-6, (1), (2) and (3). The geothermal reservoir area and the locations of the wells are shown in Fig. 6-2-7.