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REPUBLIC OF INDONESIA  
DIRECTORATE GENERAL OF  
WATER RESOURCES DEVELOPMENT  
MINISTRY OF PUBLIC WORKS

THE FEASIBILITY STUDY  
ON  
CIDANAU-CIBANTEN  
WATER RESOURCES DEVELOPMENT PROJECT

**FINAL REPORT**

VOLUME IV

SUPPORTING REPORT (2)

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June, 1992  
JAPAN INTERNATIONAL COOPERATION AGENCY  
TOKYO, JAPAN

*This Report consists of*

- |                   |                              |
|-------------------|------------------------------|
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| <i>Volume II</i>  | <i>Main Report</i>           |
| <i>Volume III</i> | <i>Supporting Report (1)</i> |
| <i>Volume IV</i>  | <i>Supporting Report (2)</i> |
| <i>Volume V</i>   | <i>Data Book</i>             |



*Appendix - F      Plan Formulation*

*Appendix - G      Preliminary Design*

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***APPENDIX - F***  
***PLAN FORMULATION***





**APPENDIX - F**  
**PLAN FORMULATION**

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## 1. General

Plans for the schemes were formulated in four (4) steps, incorporating information available at each Field and Home Work throughout First stage and Second stage. Various alternative plans were examined during the course of the Study. Fig. F-5 illustrates the logic and flow of plan formulation studies.

Data and information used at each study step may be summarized as below;

| Stage of Study                    | Phase I   |  | Phase II  |  |
|-----------------------------------|---|--|---|--|
|                                   | 1st Step  | 2nd Step   | 3rd Step  | 4th Step   |
| Report output                     | Progress Report No.1 (March 1991)   | Progress Report No.2 (Aug.1991)                      | Interim Report (Nov.1991)                               | Progress Report No.3(Jan.1992) and Draft Final Report (May 1992)   |
| Topographic information           | 1:50,000(Anyer & Krenceng, Rawa Danau)<br>1:5,000 (Cibanten)<br>1:2,000 (Cidanau)                   | 1:50,000 (Beroeng)<br>1:5,000 (Cidanau & Rawa Danau) | 1:2,000 (Krenceng)<br>1:400 (Cross section of Krenceng) | Revised 1:2000 (Krenceng)<br>1:400 (Profile of Beroeng diversion site)                                     |
| Geological information            | Reconnaissance & core drilling  | Reconnaissance & core drilling                       | Core drilling<br>Seismic Exploration                    | Core drilling  |
| Construction material             | Reconnaissance & test results   | Reconnaissance                                       | Test results  | Test results   |
| Hydrological information          | Records at Kubang Baros & Serut stations<br><br>Anyer & Krenceng: estimated by Kubang Baros station | Anyer & Krenceng: estimated by Kubang Baros station  | Modified rating curve of both Serut station             | Anyer & Krenceng: estimated by Serut station   |
| Discharge Measurement             | Kubang Baros & Serut  | Kubang Baros & Serut                                 |   | Kubang Baros, Serut & Beroeng  |
| Downstream information considered | Cibanten irrigable area   |  | Added Anyer irrigable area                              | Revised Anyer irrigable area and added Beroeng irrigable area and river maintenance flow during dry season |
| Alternative schemes considered    | 5   | 4  | 15  | 3  |

## 2 Identification of Dam Sites

### 2.1 Selection of Proposed Dam Sites

#### 1) First selection of proposed dam sites

Various possible damsites are identified in the study area through the site reconnaissance by the JICA Study Team. The following nine (9) damsites and two (2) intake weir sites are identified.

| Scheme         | Identified dam site & intake site | Name of river | Basin area (km <sup>2</sup> ) | Location (upstream of estuary) |
|----------------|-----------------------------------|---------------|-------------------------------|--------------------------------|
| A-1            | Cibanten                          | Cibanten      | 73.15                         | 22 km                          |
| A-4 & A-5      | Up-Cidanau                        | Cidanau       | 199.5                         | 7.5 km                         |
| A-2            | Mid-Cidanau                       | Cidanau       | 204.1                         | 4.7 km                         |
| A-3            | Down-Cidanau                      | Cidanau       | 208.25                        | 3.5 km                         |
| A-6            | Upstream of Krakatau intake       | Cidanau       | 214.95                        | 1.2 km                         |
| A-4-4          | Up-Anyer                          | Anyer         | 31.2                          | 3.5 km                         |
| A-4-3          | Mid-Anyer                         | Anyer         | 38.6                          | 3.0 km                         |
| A-4-1&A-4-2    | Down-Anyer                        | Anyer         | 41.3                          | 2.0 km                         |
| K-1, K-2 & K-3 | Heightening of Krenceng dam       | Krenceng      | 13.3                          | 4.0 km                         |
|                | Beroeng intake *                  | Beroeng       | 12.1                          | 15.0 km                        |
|                | Anyer intake *                    | Anyer         | 17.5                          | 12.5 km                        |

Note: \* means proposed intake weir site.

#### 2) Final selection of proposed dam sites

Among nine (9) damsites identified, five (5) damsites were discarded based on the following reasons;

##### Anyer dam site (A-4-1, A-4-2, A-4-3 and A-4-4)

There is a lot of irrigated areas and houses in the downstream anyer river basin. Thus the Anyer storaged dam plan will bring the social problem due to the resettlement of inhabitants in the inundation area. Thus the Anyer dam site is not taken up.

#### Middle Cidanau dams site (A-2)

Both abutments above El.50.00 m is covered by thick residual soil of more 10 m depth and the underlying unconsolidated pumice tuff is highly weathered to more than 15 m in thickness. Besides, unconsolidated pumice tuff also develops below the river bed up to more 15 m depth. Serious geotechnical difficulties are envisaged for the stability of dam foundation.

The possible storage volume is very small comparing to the downstream Cidanau dam site even though the sediment is removed by maintenance dredging. Therefore the development cost would be quite high. Thus this dams site is not taken up.

#### Upstream Cidanau dams site (A-4 and A-5)

Based on a rough study, technically, a very large water storage of around 100 million m<sup>3</sup> could be developed by provision of a small dam, 10 m height at the outlet of Rawa Danau and by raising the lake water level up to about El.91.0 m, and the available water supply would be about 8 m<sup>3</sup>/sec. Thus the Rawa Danau storaged dam plan will be the most beneficial with very low water cost comparing to other dams sites. However, this scheme is not taken up as it is beyond the Scope of Work in this Study. It is a prerequisite in the TOR that, the full supply water level of the Cidanau dams site should be settled so as not to submerge the Rawa Danau which is a nature reserve area.

In view of the potential of development of Rawa Danau storage scheme as mentioned above, it is suggested by DGWRD that the development of Rawa Danau should be reconsidered after the environmental problem would be settled.

Also, the free intake located in the upstream of the river which will not submerge Rawa Danau is planned to convey directly through the pipeline and store the water of Cidanau river in the Anyer river or the Krenceng reservoir. From the results of simultaneous discharge measurement carried out in first and second field works, it was not emerged the possibility of decrease in discharge toward the downstream due to infiltration of the flow into the tuffaceous bed rock. Therefore, the free intake is not practical because the downstream Krakatau intake is rather suitable due to that the pipeline will be shorter.

## 2.2 Proposed Dam Sites

### 1) Cibanten dam site

The Cibanten dam site is selected at 150 m downstream of confluence point between Cibanten river about 21.75 km upstream of the river mouth, at 10 km south of Serang. The site is accessible from Serang by the all-weather motorable road.

The dam and reservoir area are characterized by wide open valley and flat topography. The hills with ridges at the dam axis is formed around El.120 m. On the dam axis, the river, about 10 m wide shows a large meander with the riverbed at El.75.0 m. The slopes on both banks rise at around 1/2.0 of gradient almost immediately from the river brinks.

Both abutments are covered by residual soil of only 1 m in thickness. The weathered welded tuff under thin residual soil is about 20 m in depth. The difficulties in foundation treatment are not envisaged.

Annual inflow from the catchment area of 73.15 km<sup>2</sup> is estimated to be 63 x 10<sup>6</sup> m<sup>3</sup>. An area-storage curve of the reservoir is as shown in Fig. F-1.

### 2) Downstream Cidanau dam site

The dam site is selected at about 3.5 km upstream of the Cidanau river mouth, at 15 km south of Anyer. The site is accessible from Anyer by a jeep.

The dam and reservoir area are characterized by narrow valley and steep topography. The hills with ridges at the dam axis is formed around El.80 m. On the dam axis, the river, about 10 m wide shows a small meander with the riverbed at El.20.0 m. The slopes on both banks rise at around 1/1.5 of gradient almost immediately from the river brinks.

Both abutments around El.50 m to El.60 m are covered by residual soil of 5-10 m in thickness. The weakly welded pumice tuff under residual soil is about 10-15 m in depth and the top of CL class is located around El.50.0 m. The welded tuff under weakly welded pumice tuff widely develops around 30-45 m depth. The mudstone develops 2-3 m depth with the dipping downstream, 1/20 around El.0 m. The artesian ground water is observed beneath mudstone.

Permeability is generally high. Treatment including the artesian ground water will be made by ordinal procedure of grouting.

Annual inflow from the catchment area of 208.25 km<sup>2</sup> is estimated to be 429 x 10<sup>6</sup> m<sup>3</sup>. An area-storage curve of the reservoir is as shown in Fig. F-2.

### 3) Cidanau gated weir site

The Cidanau gated weir site is selected at 200 m upstream of existing Cidanau intake weir about 1.2 km upstream of the river mouth, at 13 km south of Anyer. The site is accessible from Anyer by a jeep.

The dam and reservoir area are characterized by wide open valley and flat topography with scattered low hills. The hills with ridges at the dam axis are formed around El.35.0 m. On the dam axis, the river, about 60 m wide flows northeast at the riverbed of El.0 m. The slopes on both banks rise at around 1/3.5 of gradient almost immediately from the river brinks.

Both abutments are covered by residual soil of only 1-2 m in thickness. The unconsolidated pumice tuff under thin residual soil is about 5-7 m in depth. The welded pumice tuff under unconsolidated pumice tuff widely develops and the permeability is low. However, the riverbed is covered by deposited silt, sand and gravel of 15 m in maximum depth. The thick deposited material will be removed and backfilled by the leveling concrete for dam foundation.

Annual inflow from the catchment area of 214.95 km<sup>2</sup> is estimated to be 452 x 10<sup>6</sup> m<sup>3</sup>. An area-storage curve of the reservoir is as shown in Fig. F-3.

### 4) Heightening of Krenceng dam

The Krenceng dam will be heightened at the downstream slope of the existing Krenceng dam. The dam is located about 4 km upstream of the river mouth, at 2.5 km west of Cilegon. The site is accessible from Cilegon by the all-weather motorable road.

The dam and reservoir area are characterized by wide open valley and flat topography with scattered low hills. The hills with ridges at the dam axis are formed around El.30 m.

The downstream foundation along the existing Krenceng dam is covered by residual soil of only 0.5 m in thickness. The weathered pumice tuff under thin residual soil is about 4 m in depth. The weakly welded pumice tuff under weathered pumice tuff is about 4 m in depth. The permeability is low.

Annual inflow from the catchment area of 13.3 km<sup>2</sup> is estimated to be 13.5 x 10<sup>6</sup> m<sup>3</sup>. An area-storage curve of the reservoir is as shown in Fig. F-4.

(5) Beroeng intake weir and diverted tunnel

The Beroeng intake weir is selected at 15 km upstream of mouth, 6 km upstream of the existing Krenceng dam. The site is accessible from Cilegon by a jeep along around on the ridge between Beroeng and Krenceng rivers.

The intake area is characterized by wide open valley and flat topography with scattered low hills. The inlet portal of diverted tunnel is located just upstream of intake weir. The tunnel passes through the gentle hill, the ground covering of which is 20-30 m. The residual deposit is thin around the weir and tunnel site. The weathered pumice tuff is exposed.

Annual inflow from the catchment area of 12.1 km<sup>2</sup> is estimated to be 12.3 x 10<sup>6</sup> m<sup>3</sup>.

(6) Anyer intake weir and diversion tunnel

The Anyer intake weir is selected at 12.5 km upstream of the river mouth, 10 km upstream of the existing Krenceng dam. The site is accessible from Cilegon by the all-weather motorable road along the ridge between Anyer and Krenceng basins.

The intake area is characterized by wide open valley and flat topography with scattered low hills. The inlet portal of diverted tunnel is located just upstream of intake weir. The tunnel passes through the gentle hill, the ground covering of which is 10-15 m. The residual deposit is thin around the weir and tunnel site. The weathered pumice tuff is exposed.

Annual inflow from the catchment area of 17.5 km<sup>2</sup> is estimated to be 18.6 x 10<sup>6</sup> m<sup>3</sup>.



### **3. Comparative Study for Alternative Development Schemes**

#### **3.1 Comparative Study of Alternative Single Development Schemes**

##### **3.1.1 Formulation of Alternative Single Development Schemes**

The following alternative schemes were selected through the site reconnaissance as shown in Fig. F-6. The six alternative development schemes are summarized as below;

1) **A-1: Cibanten dam development scheme**

Construction of a storaged type dam in the Cibanten river, together with a 28 km pipe line to convey water from the dam site to the existing Krenceng receiving reservoir at Cilegon, and an additional water treatment plant.

2) **A-3: Downstream Cidanau dam development scheme**

Construction of a storaged type dam in the Cidanau river, together with an additional water treatment plant. Water is conveyed from the existing Krakatau intake weir to the existing Krenceng receiving reservoir at Cilegon through the existing 27.2 km pipe line.

3) **A-6: Cidanau gated weir development scheme**

Construction of a weir with high gates located at just upstream of existing Krakatau intake weir, together with an additional water treatment plant. Water is conveyed from the existing Krakatau intake weir to the existing Krenceng reservoir at Cilegon through the existing 27.2 km pipeline.

4) **K-1: Krenceng dam heightening scheme without diversion tunnel**

Heightening of Krenceng dam, replacement of the pumping station and construction of an additional water treatment plant. Water is conveyed from the existing Krakatau intake weir to the heightened Krenceng reservoir through the existing 27.2 km pipe line.

5) **K-2: Krenceng dam heightening scheme with one diversion tunnel**

Heightening of Krenceng dam and construction of a diversion tunnel from Beroeng river to the Krenceng basin, replacement of the pumping station at Krakatau intake

and construction of an additional water treatment plant near Krenceng. Water is conveyed from the existing Krakatau intake weir to the heightened Krenceng reservoir

6) K-3: Krenceng dam heightening scheme with two diversion tunnels

Heightening of Krenceng dam along its downstream slope of and construction of two diversion tunnels from Beroeng river to Krenceng basin and Anyer river to Krenceng basin, replacement of the pumping station near Krakatau intake and construction of additional water treatment plant. Water is conveyed from the existing Krakatau intake weir to the heightened Krenceng reservoir through the existing 27.2 km pipe line.

### 3.1.2 Design Criteria

1) Design criteria of dam and appurtenant facilities

The following design criteria is adopted and applied to the Formulation study.

(1) Design flood discharge

- a) The spillway is designed by 120% peak discharge of 200-year flood without reservoir retardation effect.
- b) The energy dissipator is designed by the peak discharge of 100-year flood adopted as the design flood discharge without reservoir retardation effect.
- c) The diameter of diversion tunnel is designed in order to discharge the 25-year inflow flood hydrograph without overtopping the cofferdam under construction.

The same design flood discharge is applied to both concrete and fill types at this stage.

Probable Flood Peak

(unit: m<sup>3</sup>/s)

| Return period (year) | Cibanten dam site | Downstream Cidanau dam site | Cidanau gated weir site | Heightening Krenceng dam site |
|----------------------|-------------------|-----------------------------|-------------------------|-------------------------------|
| 25                   | 814               | 346 <sup>1)</sup>           | 346 <sup>1)</sup>       | 128                           |
| 100                  | 1033              | 444 <sup>1)</sup>           | 444 <sup>1)</sup>       | 171                           |
| 1.2 x 200            | 1324              | 535 <sup>1)</sup>           | 535 <sup>1)</sup>       | 225                           |

Note: 1) means regulated peak outflow at the outlet of Rawa Danau.

(2) Normal high water level and low water level

In the spillway with a non-gated overflow weir being adopted, the normal high water level (NHWL.El.) corresponds to the crest elevation of a spillway overflow weir.

The low water level (LWL.El.) corresponds to the horizontal sedimentation in 100 years

(3) Freeboard and dam crest elevation

The freeboard which provides the highest crest elevation of non-overflow section of a main dam is adopted from the following alternative combination of freeboard and the maximum design water surface.

| Maximum design water surface | Freeboard requirement  |
|------------------------------|--|
| Normal high water level      | $H_f(1) = h_w + h_e + h_a + h_i$<br>or 3 m for fill type and 2 m for concrete type |
| Design flood discharge water | $H_f(2) = h_w + h_a + h_i$<br>or 2 m for fill type and 1m for concrete type        |

where,  $h_w$  : Wave height due to wind  
 $h_e$  : Wave height due to earthquake  
 $h_a$  : Rise of water level due to unexpected accident in operating spillway gates(0.5 m for a gated type and 0 for a non-gated type)

hi : Addition of allowance for safety according to type and importance of dams (1 m for fill dams and 0 m for concrete dams)

The crest elevation of the non-overflow section of a main dam which corresponds to the crest elevation of the impervious core of a fill dam, is the sum of the maximum design water level and the freeboard.

(4) Dam foundation

The depth of the cutoff trench for fill dam is excavated down to the top of CM class. The rock and random zones for fill dam is excavated down to the top of CL class.

The foundation of concrete dam is laid on the top of CM class.

(5) River diversion

The river diversion during the construction is divided into two types, tunnel type and multi-stage diversion type.

(6) Dam

The dam type is divided into three types, rockfill type, earthfill type and concrete gravity type.

Both upstream and downstream slopes for the rockfill dam and earthfill dam are conservatively designed with 1: 3.0, respectively.

In the concrete gravity dam, the upstream is vertical and downstream is 1:0.6.

(7) Spillway

The spillway is divided into two types, gated type and non-gated type.

2) Design criteria of water supply facilities

(1) Outlet works

Intake

The intake tower which is of reinforced concrete is provided in the reservoir and its foundation is laid on the top of CM class.

Shaft and tunnel

The bottom of intake tower is connected to the diversion tunnel through the vertical shaft and horizontal tunnel. The diversion tunnel between the upstream plug portion and downstream plug portion beneath the dam axis is utilized as the permanent waterway after the operation of reservoir.

Steel conduit and outlet facility

The steel conduit is installed in the tunnel between the downstream plug portion and outlet portal. The outlet facility which consist of guard gate valve and hollow jet valve is provided at the downstream of tunnel portal.

In the proposed Cibanten dam, the irrigation water requirement to the downstream is regulated by the hollow jet valve and the water supply pipe line to the existing Krenceng reservoir is branched between the guard gate valve and hollow jet valve.

In the proposed Cidanau dam, the stored water in the reservoir is released to the downstream Cidanau river by the hollow jet valve.

In the proposed Cidanau gated weir, the stored water in the reservoir is directly transmitted to the existing sand trap basin by the steel conduit, about 200 m length between the upstream surface of non-overflow section at the gated weir and the entrance of existing sand trap basin. The regulation is made by hollow jet valve to be installed at the entrance.

- (2) Water supply pipe line and pump station

Water transmission system from cibanten river

The water transmission system from the Cibanten dam to the existing Krenceng reservoir is of an embedded pipe line type because it is difficult to construct the open channel in view of topographic condition. The open channel will cause serious transportation loss and water pollution.

If the foundation condition is normal, pipes are placed on a sand bed of 30 cm in thickness in the excavated trench with a bottom width of 1.70 m. Side slopes of the trench will vary 1:0.3 to 1:0.5 depending on the soil condition. Soil cover of the pipe should be about 1.2 m.

Water conveyance and treatment facility from Cidanau river

- (1) In principle the incremental development due to the Project above the design capacity of existing Krakatau water conveyance and treatment facilities is additionally provided for the intake sand trap basin and Cidanau pump station and the water treatment plant.
- (2) The existing water conveyance facility which consists of Cidanau pump station and 27.2 km long pipe line having the conveyance capacity of 2 m<sup>3</sup>/sec at the maximum pumping head of 67.1 m is operated so as to exceed the design capacity of the existing.
- (3) The additional pumps to be provided at Cidanau pump station should be designed at the total head of 67.1 m.
- (4) In case that the development yield exceeds the existing, full water can not conveyed upto the Krenceng reservoir by using the design head of Cidanau pumps.

Therefore, the booster pump station should be provided at the intermediate point, about 14.25 km from the Cidanau pump station so as to convey the water up to the Krenceng reservoir after receiving of water conveyed from the Cidanau pump station.

- (5) According to the booster pump station, the surge tank is additionally provided at the place between the booster pump station and Krenceng receiving well.
- (6) The existing Krenceng pump station is replaced by the proposed heightening of Krenceng dam.
- (7) Distribution line

The distribution line is not included at this stage.

### 3.1.3 Water Balance Study

- (1) General condition

The basic equation for the water balance study is;

$$ds/dt = O - I$$

where, ds : differential of reservoir capacity between time interval dt,  
 O : Safe yield  
 I : inflow

The general condition for water balance study is summarized as below;

- 1) The inflow at each gauging station is calculated based on five (5)-day mean inflow based on the revised discharge rating curve. The simulation of water balance is carried out for 10 years as below.

Data of five(5)-day mean inflow at Serut : 1980 to 1989

Data of five(5)-day mean inflow at Kubang Baros : 1980 to 1989

- 2) The inflow into the proposed dam site and intake site for diverted tunnel is calculated as below.

$$Q_{site} = Q_{key} \cdot (R_{site}/R_{key}) \cdot (A_{site}/A_{key})$$

where;

$Q_{site}$ ,  $R_{site}$ ,  $A_{site}$  : daily mean discharge, annual rainfall and catchment area at the project site, respectively.

$Q_{key}$ ,  $R_{key}$ ,  $A_{key}$  : daily mean discharge, annual rainfall and catchment area at the key gauge site, respectively.

Annual rainfall and catchment area of the key gauges and project sites are as follows:

| Proposed sites         |                                   |                      | Key gauge     |                                   |                      |
|------------------------|-----------------------------------|----------------------|---------------|-----------------------------------|----------------------|
| Name of site           | Catchment area (km <sup>2</sup> ) | Annual rainfall (mm) | Name of gauge | Catchment area (km <sup>2</sup> ) | Annual rainfall (mm) |
| Cibanten dam           | 73.15                             | 2000                 | Serut         | 73.15                             | 2000                 |
| Cidanau downstream dam | 208.25                            | 3000                 | Kubang Baros  | 199.5                             | 3000                 |
| Krakatau intake        | 214.95                            | 3000                 | Kubang Baros  | 199.5                             | 3000                 |
| Beroeng intake         | 12.10                             | 2250                 | Serut         | 73.15                             | 2000                 |
| Anyer intake           | 17.50                             | 2500                 | Serut         | 73.15                             | 2000                 |
| Krenceng dam           | 13.30                             | 2250                 | Serut         | 73.15                             | 2000                 |
| Cidanau gated weir     | 214.95                            | 3000                 | Kubang Baros  | 199.5                             | 3000                 |

- 3) The basin area of alternative plan is obtained by the topographic map of 1/50,000.
- 4) The evaporation loss on the reservoir and transportation loss of water transmission facilities to the water treatment plant are neglected at this stage.
- 5) The sedimentation volume of reservoir is estimated based on the analysis results of sediment sampling conducted during first field work at the Cidanau and Cibanten rivers.

Cibanten river basin : 900 m<sup>3</sup>/year/km<sup>2</sup>

Cidanau river basin : 500 m<sup>3</sup>/year/km<sup>2</sup>

Krenceng river basin : 900 m<sup>3</sup>/year/km<sup>2</sup>

- 6) The river maintenance flow to the downstream reach is considered only the period of dry season for proposed Beroeng and Anyer intake sites because the wet season is satisfied by the return flow due to the irrigation water to be released from the proposed intake weir.

The river maintenance flow is converted by the annual rainfall, catchment area and 2-yrs probable drought at Serut gauging station.



River maintenance flow during dry season

Downstream Anyer : 0.12 m<sup>3</sup>/sec

Downstream Beroeng : 0.07 m<sup>3</sup>/sec

- 7) The area and storage capacity curves of proposed dam sites were obtained by the following topographic maps;

Cibanten dam site : existing 1/5,000

Cidanau dam site : 1/5,000 by topographic mapping during first field work

Krenceng dam site : 1/2,000 by topographic and hydrographic survey during second field work

- 8) The required effective storage volume for corresponding safe yield was obtained by maximum drought during the period of 10 years.

(2) Specific condition

The specific condition of water balance study for each alternative is summarized as below.

- 1) Downstream conditions of proposed intake

The downstream water requirement at the proposed intake site for the diversion tunnel is obtained as below.

$$Q_r = \frac{IDR}{1000} \times Ha \times 1000$$

where,  $Q_r$  : downstream water requirement (m<sup>3</sup>/day)

$IDR$  : irrigation diversion requirement (mm/ha/day)

$Ha$  : Total irrigable area in the Anyer basin (ha)

Downstream Anyer : 320 ha during wet season

Beroeng : 120 ha during wet season

There is no data of irrigation water requirement for the paddy area in wet season. IDR is tentatively obtained by using the basic design report for rehabilitation of Ciujung irrigation canal system (June 1990) and the effective rainfall is obtained by the data of daily rainfall at Serang gauging station.

2) Operation of diversion tunnel

The basic conditions for the water balance study against the downstream is as follows:

|                   |                |   |                                    |
|-------------------|----------------|---|------------------------------------|
| During wet season | $Q_b \geq IDR$ | : | $Q = Q_b - IDR$<br>$Q_{max} = Q_t$ |
|                   | $Q_b < IDR$    | : | $Q = 0$                            |
| During dry season | $Q_b \geq DRM$ | : | $Q = Q_b - DRM$<br>$Q_{max} = Q_t$ |
|                   | $Q_b < DRM$    | : | $Q = 0$                            |

Where,  $Q_b$  : inflow at diversion site  
 $IDR$  : irrigation diversion requirement  
 $Q_t$  : Maximum discharge capacity of tunnel (4.0 m<sup>3</sup>/sec)  
 $DRM$  : downstream river maintenance flow

3) Downstream condition of Cibanten dam site

The present downstream paddy area of Cibanten dam site through the intake weir is estimated by 1961 ha in wet season and 566 ha in dry season. The IDR is also obtained by the report of Ciujung irrigation canal system mentioned above and the effective rainfall is obtained by the data of daily rainfall at Serang gauging station.

(3) Flow chart of computation procedure

The flow chart of computation procedure is shown in Figs. F-7 to F-9 and its schematic diagram is shown in Figs. F-10 to F-15.

3.1.4 Safe Yield for Existing Krakatau Water Supply System

The principal features of the existing Krakatau water supply system which consist of intake weir at the Cidanau river, pump station, 27.2 km long pipe line, Krenceng

reservoir, suction pump and water treatment plant are presented but there are no design data for safe yield of the existing Krakatau water supply system.

1) Basic conditions

- Water conveyance capacity of a 27.2 km long pipe line : 2.0 m<sup>3</sup>/sec
- Capacity of suction pump and water treatment plant : 2.0 m<sup>3</sup>/sec
- Inflow at the Krenceng dam site from Krenceng own catchment area
- Inflow at the Krakatau intake weir site

2) Revised storage volume

Based on the hydrographic survey results in the Krenceng reservoir carried out during the 2nd Field Work and 4th Field Work, the reservoir storage should be revised as below.

(unit: 10<sup>6</sup>m<sup>3</sup>)

| Storage                 | Original<br>(Krakatau's data) | Revision<br>(Measurement) | Balance |
|-------------------------|-------------------------------|---------------------------|---------|
| Effective <sup>1)</sup> | 1.45                          | 3.155                     | +1.705  |
| Gross <sup>2)</sup>     | 2.50                          | 4.90                      | +2.400  |

- Notes ;
- 1) between LWL.18.50 and NHWL.22.50
  - 2) between LWL.18.50 and Max.WL.24.00

3) Simulation study results of safe yield

According to the water balance study by Scheme K-1, the simulation study for the existing Krakatau water supply system is carried out by two cases so as to justify the safe yield.

Case -1 : with pump station and 27.2 km long pipe line  
(Krenceng own catchment and natural flow at Krakatau intake weir site)

Case -2 : without pump station and 27.2 km long pipe line  
(Only Krenceng own catchment)

3) Safe yield

Case -1 : 1.97 m<sup>3</sup>/sec

Case -2 : 0.235 m<sup>3</sup>/sec

Considering the above simulation results, it is justified that the facility capacity of existing Krakatau water supply system, 2.0 m<sup>3</sup>/sec is well coincided with the safe yield, 1.97 m<sup>3</sup>/sec.

The safe yield of existing Krakatau water supply system is evaluated by 1.97 m<sup>3</sup>/sec.

### 3.1.5 Safe Yield vs. Required Effective Storage and Safe Yield vs. NHWL for Alternative Scheme

The safe yield vs. required effective storage and safe yield vs. normal high water level (NHWL) for alternative development schemes are summarized in Figs. F-16 to F-21.

### 3.1.6 Maximum Exploitable Dam Scale and Development Yield

#### 1) Cibanten dam

From the topographical constraint where the ridge of both abutments is located at El.120.00 m, upper limit (NHWL) of the Cibanten dam site is set at El.115.00 m considering the freeboard of 5 m including the overflow depth. Besides, the geological condition is favourable and with thin top soil. Thus, the maximum exploitable dam scale is limited at NHWL.El.115.00 m. The development yield is 0.45 m<sup>3</sup>/sec under the condition that the design sedimentation has 6.58x10<sup>6</sup> m<sup>3</sup> and the downstream irrigation water requirement be satisfied with an 80% probability of exceedance the drought.

#### 2) Downstream Cidanau dam

From the topographical constraint where the ridge of left abutment is located at El.75.0 m, upper limit (NHWL) of the Cidanau dam site is set at El.70.0 m considering the freeboard of 5 m including the overflow depth. However, the residual soil and unconsolidated pumice tuff (D class) are covered up to El.50.0 m and the underlying weakly welded pumice tuff, CL class develops. The foundation of fill dam should be laid on the top of CL class.

Thus, the maximum exploitable dam scale is limited at NHWL.El.50.00 m and the gross storage is 7.11x10<sup>6</sup> m<sup>3</sup> above the river bed of El.20.0 m.

Adding the design sedimentation, no effective storage is remained. In order to secure possible effective storage, the sediment basin is provided just upstream of outlet of Rawa danau.

Sediment basin : 1 nos x300 wide x300 m length (Wet season)

|                       |       |
|-----------------------|-------|
| Excavation depth      | 2.5 m |
| Total water depth     | 2.0 m |
| Effective water depth | 1.0 m |

1 nos x100 wide x50 m length(dry season)

|                       |       |
|-----------------------|-------|
| Excavation depth      | 2.0 m |
| Total water depth     | 1.5 m |
| Effective water depth | 0.5 m |

Smallest particles to be settled 0.035 mm

Critical velocity  $10 \text{ cm/sec} = V_c = a(d)^{1/2} = 51(0.035)^{1/2}$

Design velocity  $0.1 \text{ m/sec} = Q/A = 30/(1 \times 300)$

Settled particles 60% (above 0.035 mm based on the sediment sample in 1st field work)

Considering the above, the practical sedimentation become  $4.165 \times 10^6 \text{ m}^3$  and the effective storage become  $2.945 \times 10^6 \text{ m}^3$ . The development yield is  $1.825 \text{ m}^3/\text{sec}$ .

### 3) Cidanau gated weir

From the topographical constraint where the ridge of both abutments is located at El.35.00 m, upper limit (NHWL) of the Cidanau gated dam site is set at El.32.00 m considering the freeboard of 3 m with flood regulation by the gate. Besides, the geological condition is favourable but the removal of deposited material below the river bed is needed.

However, the maximum exploitable gate height is limited to around 20 m. Considering the above, the normal high water level is set at El.20.0 m and the development yield is  $1.97 \text{ m}^3/\text{sec}$ .

4) Heightening of Krenceng dam

From the topographical constraint where the ridge of both abutments is located at El.32.00 m, upper limit (NHWL) of the heightened Krenceng dam is set at 29.00 m considering the freeboard of 3 m with flood regulation by the gate. Besides, the geological condition is favourable for foundation of fill dam.

Thus, the maximum exploitable dam scale is limited at NHWL.El.29.00 m. The gross storage is  $12.60 \times 10^6 \text{ m}^3$  above the lowest elevation of El.13.00 m. The effective storage is  $11.40 \times 10^6 \text{ m}^3$  considering the design sedimentation of  $1.20 \times 10^6 \text{ m}^3$ .

| Scheme | Development yield<br>( $\text{m}^3/\text{sec}$ ) |
|--------|--|
| K-1    | 3.10   |
| K-2    | 3.15   |
| K-3    | 3.20   |

3.1.7 Incremental Yield for Alternatives

From the above results, the incremental yield for the alternatives is summarized as below.

| Scheme | Maximum exploitable dam height<br>(m) | Effective storage volume<br>( $10^6 \text{ m}^3$ ) | Development yield<br>(cms) | Existing yield<br>(cms) | Incremental yield<br>(cms) | Total system yield<br>(cms) | Water demand of forecast in 2005<br>(cms) | Surplus /deficit<br>(cms) |
|--------|---------------------------------------|--|----------------------------|-------------------------|----------------------------|-----------------------------|---|---------------------------|
| A-1    | 45 <sup>1)</sup>                      | 14.9   | 0.45                       | 1.97                    | 0.45                       | 2.42                        | 3.67                                      | -1.25                     |
| A-3    | 35 <sup>2)</sup>                      | 2.95   | 1.825                      | 1.97                    | 0.09                       | 2.06                        | 3.67                                      | -1.61                     |
| A-6    | 24.2 <sup>3)</sup>                    | 3.44   | 1.970                      | 1.97                    | 0.235                      | 2.205                       | 3.67                                      | -1.465                    |
| K-1    | 24 <sup>1)</sup>                      | 12.87  | 3.10                       | 1.97                    | 1.03                       | 3.00                        | 3.67                                      | -0.57                     |
| K-2    | 24 <sup>1)</sup>                      | 12.87  | 3.15                       | 1.97                    | 1.15                       | 3.12                        | 3.67                                      | -0.52                     |
| K-3    | 24 <sup>1)</sup>                      | 12.87  | 3.20                       | 1.97                    | 1.28                       | 3.25                        | 3.67                                      | -0.47                     |

Notes : 1) due to topographic constraint  
 2) due to geological constraint  
 3) due to hydro-mechanical constraint

### 3.1.8 Preliminary Design and Principal Features for Alternative Single Development Schemes

The general plan of proposed dam and its reservoir are shown in Figs. F-22 to F-25. The plan, the maximum section and the upstream view of the main structures for the proposed dam are shown in Figs. F-26 to F-29. The plan and profile of conveyance from the proposed Cibanten dam to Krenceng receiving reservoir is shown in Fig. F-30. The principal features for alternative single development scheme are summarized in Table F-2.

## 3.2 Comparative Study on Alternative Combined Development Schemes

### 3.2.1 Necessity of Comparative Study on Combined Development

As seen in the results of Chapter 3.1.7, any single development scheme cannot satisfy the urgent water demand in the year 2005. Therefore, the comparative study on alternative combined development scheme is required so as to increase the total system yield in the Study Area.

### 3.2.2 Formulation of Alternative Combined Development Schemes

The following three alternative combined development schemes are divided into three groups in terms of the type of development for the heightening of Krenceng dam and formulated by nine (9) alternatives as below.

| Scheme | Single scheme to be combined |
|--------|------------------------------|
| B-1    | K-1 plus A-1                 |
| B-2    | K-1 plus A-3                 |
| B-3    | K-1 plus A-6                 |
| C-1    | K-2 plus A-1                 |
| C-2    | K-2 plus A-3                 |
| C-3    | K-2 plus A-6                 |
| D-1    | K-3 plus A-1                 |
| D-2    | K-3 plus A-3                 |
| D-3    | K-3 plus A-6                 |

### 3.2.3 Design Criteria

#### 1) Dam and appurtenant facilities

The design conditions concerned are same as the alternative single development one.

2) Water transmission facilities

(1) Krakatau pump station

The Krakatau pump station should be added by the incremental yield except Scheme B-1, C-1 and D-1.

(2) Booster pump station

The booster pump station should be added by the development yield except Scheme B-1, C-1 and D-1.

(3) Krenceng pump station

The Krenceng pump station should be replaced by the development yield.

(4) Water treatment plant

The water treatment plant should be added by the incremental yield.

3.2.4 Water Balance Study and Incremental Yield

1) Water balance study

The water balance study for the combined development scheme is carried out by the same procedures described in Chapter 3.1.3.

The flow chart of computation procedure and the schematic diagram is shown in Figs. F-31 (1) to F-34.

2) Safe yield

The safe yield, required effective storage volume and normal high water level for each scheme are summarized in Figs. F-35 to F-40.

3) Incremental yield

From the above results, the incremental yield for the alternatives is summarized as below.



(unit: cms)

| Scheme | Development yield | Existing yield | Incremental yield | Total system yield | Water demand forecast in 2005 | Surplus or deficit |
|--------|-------------------|----------------|-------------------|--------------------|-------------------------------|--------------------|
| B-1    | 3.55              | 1.97           | 1.58              | 3.55               | 3.67                          | -0.12              |
| B-2    | 3.40              | 1.97           | 1.43              | 3.4                | 3.67                          | -0.27              |
| B-3    | 3.435             | 1.97           | 1.465             | 3.435              | 3.67                          | -0.235             |
| C-1    | 3.60              | 1.97           | 1.63              | 3.60               | 3.67                          | -0.07              |
| C-2    | 3.445             | 1.97           | 1.475             | 3.445              | 3.67                          | -0.225             |
| C-3    | 3.49              | 1.97           | 1.52              | 3.49               | 3.67                          | -0.18              |
| D-1    | 3.65              | 1.97           | 1.68              | 3.65               | 3.67                          | -0.02              |
| D-2    | 3.49              | 1.97           | 1.52              | 3.49               | 3.67                          | -0.18              |
| D-3    | 3.54              | 1.97           | 1.57              | 3.54               | 3.67                          | -0.13              |

### 3.2.5 Principal Features of Alternative Combined Development Schemes

The principal features of alternative combined development schemes are summarized in Table F-2.

## 3.3 Selection of the Scheme

### 3.3.1 General

Based on the Single and combined Comparative Studies mentioned in Chapter 3.1 and 3.2, the schemes to be selected as the feasibility study are determined by the economic and socio-environmental view-points.

### 3.3.2 Cost Estimate

The construction cost is estimated based on the drawings for basic design and its principal features for the alternatives. The construction period including the tender design is 7 years. The breakdown of construction costs is summarized in Table F-3 to F-26.

### 3.3.3 Economic Cost

#### Disbursement

The construction cost is uniformly disbursed owing to the construction period.

#### O&M costs

The annual O&M costs for the dam and appurtenant structures are 0.5% of the direct cost. Annual O&M costs for water transmission and treatment facilities are taken at 1% of direct cost.

#### Pumping costs

The pumping costs due to difference between "with Project" and "without Project" are estimated by the principal features.

#### Replacement cost

The water conveyance facilities is assumed to be incurred for replacement after the life of 25 years.

#### Conversion factor

The conversion factor is 0.9

#### Economic cost

The cost above is converted by the conversion factor.

### 3.3.4 Economic Benefit

#### Combined water tariff

The combined water tariff which consists of domestic and industrial water is estimated by 1625 Rp/m<sup>3</sup>.

#### Economic benefit

The economic benefit is obtained by multiplying the combined water tariff and incremental yield as shown in Figs. F-41 to F-55.

### 3.3.5 Economic Evaluation

#### Results

The results of economic evaluation are summarized in Table F-27 and F-28.

### Selection of the Schemes as Feasibility Study

The comparative study on the above fifteen (15) alternative schemes was made through comprehensive evaluation from the economic, technical and social aspects. Among alternative above, K-3 is the highest EIRR. Second highest is with the Scheme K-2 third is with the Scheme K-1 and fourth is the Scheme C-3. However, K-3 is discarded because there is more 330 ha of paddy field in the downstream of Anyer main only except the tributary and the diversion to Krenceng reservoir might cause various social effect to the downstream.

Finally, the following three (3) schemes are selected as the feasibility study.

- (i) Scheme K-1: Heightening of Krenceng dam without diversion tunnel
- (ii) Scheme K-2: Heightening of Krenceng dam with Beroeng diversion tunnel
- (iii) Scheme C-3: Heightening of Krenceng dam with Beroeng diversion tunnel and Cidanau gated weir

They were agreed in the Minute of Meeting on the Interim Report between the JICA Study Team, the Advisory Committee and the DGWRD on November 8, 1991.

#### **4. Plan Optimization**

The scales of heightening of Krenceng dam, Beroeng diversion tunnel and Cidanau gated weir have been decided by the maximum exploitable scale due to the topographic constraint and hydro-mechanical constraint.

Herein, the optimal development scale of each project components above was studied by comparing the capitalized net benefit of various alternative scales based on the net benefit maximization criteria.

##### **4.1 Optimal Heightening Scale of Krenceng Dam**

A comparative study of heightening scale of Krenceng dam was worked out on the 3 alternatives (Fig. F-56).

| Description  | Alternative |            |            |
|--|-------------|------------|------------|
|  | H-1         | H-2        | H-3        |
| 1) Dam crest elevation   | EI.32.00    | EI.29.00   | EI.26.00   |
| 2) Normal high water level   | NHWL.29.00  | NHWL.26.00 | NHWL.23.00 |
| 3) Low water level level   | LWL.18.50   | LWL.18.50  | LWL.18.50  |
| 4) Effective storage ( $10^6 \text{ m}^3$ )  | 12.81       | 7.90       | 4.05       |
| 5) Design sediment ( $10^6 \text{ m}^3$ )  | 1.20        | 1.20       | 1.20       |
| 6) Gross storage ( $10^6 \text{ m}^3$ )  | 14.01       | 9.1        | 5.25       |
| 7) Safe yield ( $\text{m}^3/\text{sec}$ )  | 3.10        | 2.65       | 2.105      |
| 8) Incremental yield ( $\text{m}^3/\text{sec}$ )                                   | 1.13        | 0.68       | 0.135      |
| 8) Annual average conveyance from Krakatau intake ( $10^6 \text{ m}^3/\text{yr}$ ) | 83.72       | 70.34      | 53.53      |
| 8) Added pump capacity at Cidanau intake ( $\text{m}^3/\text{sec}$ )               | 1.10        | 0.65       | 0.105      |
| 9) Replaced pump capacity at Krenceng reservoir ( $\text{m}^3/\text{sec}$ )        | 3.10        | 2.65       | 2.105      |
| 10) Added water treatment plant( $\text{m}^3/\text{hr}$ )                          | 3960        | 2340       | 378        |

The design for heightened dam and its spillway is carried out by fixing the following conditions;

- i) The dam axis for the heightening of Krenceng dam is located at the downstream toe of the existing dam so as to keep the slope stability of existing one and secure the operation of ordinary grouting work after cut-off excavation. The heightened dam is planned by the homogeneous earthfill type with the slope of 1:3.0 in both upstream and downstream sides.
- ii) Spillway is located at 60 m leftwards from the centre of existing spillway. The spillway is designed as a gated overflow type having a 15.5 m of net width. Spillway gate consists of two roller gates having an overall dimension of 7.75 m wide and 4.30 m high.

The stilling basin is designed as the hydraulic jump type.

The work quantities for alternatives are summarized as below.

| Item                         | Alternative |            |            |
|------------------------------|-------------|------------|------------|
|                              | H-1         | H-2        | H-3        |
| 1) Dam                       |             |            |            |
| Excavation (m <sup>3</sup> ) | 25590       | 215032     | 173998     |
| Embankment (m <sup>3</sup> ) | 1356001     | 886564     | 550458     |
| Grouting (m)                 | 39953       | 31812      | 28074      |
| 2) Spillway                  |             |            |            |
| Excavation (m <sup>3</sup> ) | 49769       | 49398      | 48225      |
| Concrete (m <sup>3</sup> )   | 17866       | 12268      | 7383       |
| 3) Gate                      |             |            |            |
| Nos.                         | 2           | 2          | 2          |
| Dimension (BxH)              | 7.75 x 4.3  | 7.75 x 4.3 | 7.75 x 4.3 |

The results of the economic comparison are summarized as below.

(unit: 10<sup>6</sup>Rp)

| Description                              | Alternative |        |       |
|--|-------------|--------|-------|
|  | H-1         | H-2    | H-3   |
| 1) Economic cost <sup>1]</sup>           | 112532      | 78034  | 40195 |
| 2) Capitalized cost (C) <sup>2]</sup>    | 91575       | 63293  | 32410 |
| 3) Capitalized benefit (B) <sup>3]</sup> | 243637      | 146614 | 29107 |
| 4) Net benefit (B-C)                     | 152062      | 83320  | -3303 |
| 5) Benefit cost ratio (B/C)              | 2.66        | 2.32   | 0.90  |

- Note:
- 1] Conversion factor: 0.9
  - 2] Included O&M cost and pumping cost  
Capitalized by the discount rate of 12%
  - 3] Water tariff after treatment: 1625 Rp/m<sup>3</sup>

As shown in the table above, the alternative H-1, the maximum heightening scale yields the highest net benefit among the 3 alternatives.

#### 4.2 Optimal Scale of Beroeng Diversion Tunnel

##### (1) Basic approach

The economic diameter was obtained with the least cost criteria, taking into consideration the construction cost of alternative diversion tunnel and the

differential pumping cost of Krakatau intake due to the water conveyance from the Krakatau intake.

(2) Design condition

The diversion tunnel is designed under the hydraulic condition of pressure flow. The downstream water depth at the outlet portal is assumed to set the crown of tunnel because the discharge capacity of downstream hydraulic cross section in the Krenceng river is bigger than that due to prospective tunnel diameter. The upstream water level at the inlet portal is designed to set the water depth of one (1) diameter of the tunnel above the tunnel crown at the inlet portal so as to keep the pressure flow condition. No slope of tunnel is provided.

$$H = \left( \frac{124.5 n^2 L}{D^{4/3}} + f_e + f_o \right) \frac{v^2}{2g} = D$$

where, H : loss head between inlet and outlet (m)  
 g : acceleration of gravity (= 9.8 m/s<sup>2</sup>)  
 n : roughness coefficient for concrete (= 0.014)  
 L : tunnel length (= 280 m)  
 f<sub>e</sub> : coefficient of entrance loss  
 f<sub>o</sub> : coefficient of exit loss (= 1.0)  
 v : flow velocity  
 D : tunnel diameter

(3) Alternatives

Four (4) alternatives are selected as below.

| Description               | Alternative |      |      |      |
|---------------------------|-------------|------|------|------|
|                           | J-1         | J-2  | J-3  | J-4  |
| 1) Tunnel diameter(m)     | 1.50        | 2.00 | 2.50 | 3.00 |
| 2) Maximum discharge(cms) | 4           | 11   | 20.5 | 35   |

The water balance study was carried out by fixing the following conditions;

- i) The water conveyance capacity of Krakatau pump station has 3.15 m<sup>3</sup>/sec which corresponds to the safe yield of heightening of Krenceng reservoir.

- ii) The basic conditions for the water balance study against the downstream Beroeng is as follow.

$$\begin{array}{lll}
 \text{During wet season} & Q_b \geq \text{IDR} & : Q = Q_b - \text{IDR} \\
 & & Q_{\max} = Q_t \\
 & Q_b < \text{IDR} & : Q = 0 \\
 \\ 
 \text{During dry season} & Q_b \geq \text{DRM} & : Q = Q_b - \text{DRM} \\
 & & Q_{\max} = Q_t \\
 & Q_b < \text{DRM} & : Q = 0
 \end{array}$$

where,  $Q_b$  : inflow at Beroeng diversion site  
 IDR : irrigation diversion requirement  
 $Q_t$  : Maximum discharge capacity of tunnel  
 DRM : downstream river maintenance flow

(4) Results of water balance study

| Description  | Alternative |        |        |        |
|--|-------------|--------|--------|--------|
|  | J-1         | J-2    | J-3    | J-4    |
| 1) Development yield(cms)  | 3.15        | 3.15   | 3.15   | 3.15   |
| 2) Required effective storage ( $10^6\text{m}^3$ )                               | 12.83       | 12.83  | 12.83  | 12.83  |
| 3) Design sediment( $10^6\text{m}^3$ )   | 1.20        | 1.20   | 1.20   | 1.20   |
| 4) Gross storage( $10^6\text{m}^3$ )   | 14.03       | 14.03  | 14.03  | 14.03  |
| 5) Normal high water level (El-m)  | 29.00       | 29.00  | 29.00  | 29.00  |
| 6) Water conveyance from Krakatau intake( $10^6\text{m}^3/\text{yr}$ )           | 77.238      | 77.057 | 77.057 | 77.057 |
| 7) Water conveyance thru Beroeng diversion tunnel ( $10^6\text{m}^3/\text{yr}$ ) | 10.062      | 10.243 | 10.243 | 10.243 |
| 8) Total water conveyance to Krenceng reservoir ( $10^6\text{m}^3/\text{yr}$ )   | 87.300      | 87.300 | 87.300 | 87.300 |

The annual equivalent of tunnel construction cost and differential pumping cost are summarized as below.

(unit: 10<sup>6</sup>Rp)

| Description                             | Alternative |        |        |         |
|---|-------------|--------|--------|---------|
|   | J-1         | J-2    | J-3    | J-4     |
| 1) Tunnel diameter(m)                   | 1.5         | 2.0    | 2.5    | 3.0     |
| 2) Direct cost for tunnel               | 422.73      | 599.91 | 803.65 | 1033.94 |
| 3) Annual equivalent cost <sup>1)</sup> | 50.90       | 72.24  | 96.77  | 124.50  |
| 4) Annual pumping cost                  | 2980.9      | 2974.5 | 2974.5 | 2974.5  |
| 5) Total annual cost                    | 3031.8      | 3046.7 | 3071.3 | 3099.0  |

Note: 1) Capital recovery factor, CRF:0.120416  
Discount rate: 12%

As shown in the table above, the alternative J-1, the minimum tunnel diameter in the practical construction yields the lowest cost among the 4 alternatives.

#### 4.3 Optimal Scale of Cidanau Gated Weir

A comparative study of gate height of Cidanau gated weir was worked out on the 2 alternatives (Fig. F-56).

| Description   | Alternative                       |                                   |
|---|-----------------------------------|-----------------------------------|
|   | M-1                               | M-2                               |
| 1) Dam crest elevation  | EI.24.20                          | EI.21.20                          |
| 2) Normal high water level                                      | NHWL.21.20                        | NHWL.18.20                        |
| 3) Low water level  | LWL.1.50                          | LWL.1.50                          |
| 4) Effective storage (10 <sup>6</sup> m <sup>3</sup> )          | 3.44                              | 2.37                              |
| 5) Design sediment (10 <sup>6</sup> m <sup>3</sup> )            | -                                 | -                                 |
| 6) Gross storage (10 <sup>6</sup> m <sup>3</sup> )              | 3.44                              | 2.37                              |
| 7) Safe yield (cms)   | 1.97                              | 1.75                              |
| 8) Total yield (cms)  | 2.205                             | 1.985                             |
| 9) Incremental yield (cms)                                      | 0.235                             | 0.015                             |
| 10) Spillway gate   | 3 nos. x 17 m wide<br>x 20 m high | 3 nos. x 17 m wide<br>x 17 m high |
| 11) Added pump capacity at Cidanau intake (m <sup>3</sup> /sec) | -                                 | -                                 |
| 12) Added water treatment plant (m <sup>3</sup> /hr)            | 738                               | 54                                |



The design for gated weir and its spillway is carried out by fixing the following conditions;

- i) The dam type for both abutments is of concrete gravity one. The upstream is vertical and downstream is 1:0.6.
- ii) The crest elevation and net width for gated weir are set at El.1.50 m and 51 m, respectively.

The work quantities for alternatives are summarized as below.

| Item                        | Alternative |         |
|-----------------------------|-------------|---------|
|                             | M-1         | M-2     |
| 1) Dam                      |             |         |
| Excavation(m <sup>3</sup> ) | 21324       | 20067   |
| Concrete(m <sup>3</sup> )   | 23519       | 18984   |
| Grouting(m)                 | 3806        | 3140    |
| 2) Spillway                 |             |         |
| Excavation(m <sup>3</sup> ) | 24059       | 24059   |
| Concrete(m <sup>3</sup> )   | 22011       | 19884   |
| 3) Gate                     |             |         |
| Nos.                        | 2           | 2       |
| Dimension(BxH)              | 17 x 20     | 17 x 17 |

The results of the economic comparison are summarized as below.

(unit:10<sup>6</sup>Rp)

| Description                              | Alternative |        |
|--|-------------|--------|
|  | M-1         | M-2    |
| 1) Economic cost <sup>1]</sup>           | 67484       | 57927  |
| 2) Capitalized cost (C) <sup>2]</sup>    | 46012       | 39182  |
| 3) Capitalized benefit (B) <sup>3]</sup> | 50668       | 3234   |
| 4) Net benefit value (B-C)               | 4656        | -35948 |
| 5) Benefit cost ratio (B/C)              | 1.10        | 0.08   |

Note: 1] Conversion factor: 0.9  
 2] Included O&M cost and pumping cost  
 Capitalized by the discount rate of 12%  
 3] Water tariff after treatment: 1625 Rp/m<sup>3</sup>

As shown in the table above, the alternative M-1, the maximum gate height is more economical than M-2.

#### 4.4 Final Reservoir Operation and Net Safe Yield

The final reservoir operation was carried out by fixing the development scale of each component determined in the preceding chapter so as to obtain the net safe yield for each scheme which means the supply yield after the evaporation loss from the reservoir.

##### 1) Basic conditions

###### (i) Reservoir operation study

The reservoir operation study was carried out by the following four (4) cases;

Case 1 : Existing Krenceng dam

Case 2 : Scheme K-1 (Heightening of Krenceng dam without Beroeng diversion tunnel)

Case 3 : Scheme K-2 (Heightening of Krenceng dam with Beroeng diversion tunnel)

Case 4 : Scheme C-3 (Heightening of Krenceng dam with Beroeng diversion tunnel and Cidanau gated weir)

| Description                                       | Case 1          | Case 2          | Case 3          | Case 4          |                |
|---|-----------------|-----------------|-----------------|-----------------|----------------|
| 1) Reservoir                                      | <u>Krenceng</u> | <u>Krenceng</u> | <u>Krenceng</u> | <u>Krenceng</u> | <u>Cidanau</u> |
| 2) NHWL   | 22.50           | 29.00           | 29.00           | 29.00           | 21.20          |
| 3) LWL  | 18.50           | 18.00           | 18.00           | 18.00           | 1.50           |
| 4) Capacity of diversion tunnel (m <sup>3</sup> ) | -               | -               | 4.0             | 4.0             | -              |

(ii) Evaporation loss

The evaporation loss from the reservoir surface is estimated to be 70% of the mean pan-evaporation observed at Padarincang.

(unit:mm/day)

| Description            | Jan  | Feb  | Mar  | Apr  | May  | Jun  | Jul  | Aug  | Sep  | Oct  | Nov  | Dec  |
|------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| 1) Observed pan record | 4.5  | 3.7  | 3.3  | 3.4  | 3.4  | 3.1  | 3.4  | 4.4  | 4.0  | 4.1  | 4.5  | 4.1  |
| 2) Evaporation loss    | 3.15 | 2.59 | 2.31 | 2.38 | 2.38 | 2.17 | 2.38 | 3.08 | 2.80 | 2.87 | 3.15 | 2.87 |

2) Results of reservoir operation study

(i) Net supply yield

The net supply yield for each case is summarized as below.

| Case   | Net supply yield (m <sup>3</sup> /sec) | Net incremental supply yield (m <sup>3</sup> /sec) |
|--|--|--|
| i) Existing Krenceng dam   | 1.94                                   | -  |
| ii) Heightening of Krenceng dam without diversion                                    | 3.05                                   | 1.11   |
| iii) Heightening of Krenceng dam with Beroeng diversion tunnel                       | 3.11                                   | 1.17   |
| iv) Heightening of Krenceng dam with Beroeng diversion tunnel and Cidanau gated weir | 3.435                                  | 1.495  |

(ii) Reservoir operation study

The results of reservoir operation study were shown in Figs. F-58 to F-65 and Table F-34 (1) to F-37 (12).



## ***TABLES***



Table F-1 Principal Features for Alternative Single Development Schemes

|  |                                | A-1                          | A-3                              | A-6                      | K-1  | K-2  | K-3  |
|--|--------------------------------|------------------------------|----------------------------------|--------------------------|--|--|--|
|  |                                | Cibanten Dam                 | Down-stream<br>Cibantau<br>Dam   | Cidantau<br>Gated Weir   | Heightening<br>of Krenceng<br>Dam without<br>Diversion | Heightening<br>of Krenceng<br>Dam with<br>One<br>Diversion | Heightening of<br>Krenceng Dam<br>with Two<br>Diversions |
| <b>Reservoir</b>                           |                                |                              |                                  |                          |  |  |  |
| Name of river                              |                                | Cibanten                     | Cidantau                         | Cidantau                 | Krenceng   | Krenceng   | Krenceng   |
| Catchment area                             | km <sup>2</sup>                | 73.15                        | 208.25                           | 214.95                   | 13.3   | 13.3   | 13.3   |
| Reservoir surface area                     | km <sup>2</sup>                | 2.1                          | 0.6                              | 0.41                     | 1.8  | 1.8  | 1.8  |
| Gross capacity                             | 10 <sup>6</sup> m <sup>3</sup> | 21.5                         | 7.11                             | 3.44                     | 14.1   | 14.1   | 14.1   |
| Effective capacity                         | 10 <sup>6</sup> m <sup>3</sup> | 14.9                         | 2.95                             | 3.44                     | 12.9   | 12.9   | 12.9   |
| Development yield                          | m <sup>3</sup> /s              | 0.45                         | 1.825                            | 1.97                     | 3.10   | 3.15   | 3.20   |
| High water level                           | EL-m                           | 115.0                        | 50.0                             | 21.2                     | 29.0   | 29.0   | 29.0   |
| Low water level                            | EL-m                           | 104.5                        | 44.0                             | 0                        | 18.0   | 18.0   | 18.0   |
| Annual rainfall                            | mm/yr                          | 2,250                        | 3,000                            | 3,000                    | 2,250  | 2,250  | 2,250  |
| Mean runoff                                | m <sup>3</sup> /sec            | 2.0                          | 13.63                            | 14.36                    | 0.43   | 0.43   | 0.43   |
| Design peak flood                          | m <sup>3</sup> /sec            |                              |                                  |                          |  |  |  |
| 25 yrs                                     |                                | 814                          | 346                              | 346                      | 128  | 128  | 128  |
| 100 yrs                                    |                                | 1,033                        | 444                              | 44                       | 171  | 171  | 171  |
| 1.2 x 200 yrs                              |                                | 1,324                        | 535                              | 535                      | 225  | 225  | 225  |
| <b>Dam and Rated Facility</b>              |                                |                              |                                  |                          |  |  |  |
| <b>Diversion Work</b>                      |                                |                              |                                  |                          |  |  |  |
| <b>River diversion</b>                     |                                |                              |                                  |                          |  |  |  |
|  |                                | Tunnel<br>scheme             | Tunnel<br>scheme                 | Multi-stage<br>diversion | Multi-stage<br>diversion                               | Multi-stage<br>diversion                                   | Multi-stage<br>diversion                                 |
| Diversion tunnel, L                        | m                              | 410                          | 400                              | -                        | -  | -  | -  |
| D  | m                              | 5                            | 5                                | -                        | -  | -  | -  |
| Diversion gate                             | Nos.                           | 1                            | 1                                | -                        | -  | -  | -  |
| <b>Dam</b>                                 |                                |                              |                                  |                          |  |  |  |
| Type                                       |                                | Main<br>dam<br>Rock-<br>fill | Saddle<br>dam<br>Rando<br>m-fill | Rockfill                 | Gravity  | Impervious<br>random-fill                                  | Impervious<br>random-fill                                |
| Crest elevation                            | EL-m                           | 120                          | 120                              | 55                       | 24.2   | 32   | 32   |
| Height (from river bed)                    | m                              | 45                           | 34                               | 35                       | 24.2   | 16   | 16   |
| Crest length                               | m                              | 340                          | 275                              | 255                      | 299  | 2,800  | 2,800  |
| Embankment/Conc. volume                    | 10 <sup>3</sup> m <sup>3</sup> | 947                          | 168                              | 474                      | 43   | 1,281  | 1,281  |
| <b>Spillway</b>                            |                                |                              |                                  |                          |  |  |  |
| Type                                       |                                | Side overflow                | Side overflow                    | Roller gate              | Roller gate  | Roller gate  | Roller gate  |
| Crest elevation of weir                    | EL-m                           | 115                          | 50                               | 1.5                      | 24   | 24   | 24   |
| Width of weir                              | m                              | 150                          | 120                              | 61                       | 20   | 20   | 20   |
| Gate                                       |                                | -                            | -                                | 17x20x3                  | 8.75x5.5x2   | 8.75x5.5x2   | 8.75x5.5x2   |
| (wide x height x Nos.)                     |                                |                              |                                  |                          |  |  |  |
| <b>Outlet Works</b>                        |                                |                              |                                  |                          |  |  |  |
| Intake type                                |                                | Vertical                     | Vertical                         | Horizontal               | -  | -  | -  |
| Steel conduit, L                           | m                              | 230                          | 285                              | 200                      | -  | -  | -  |
| Guard valve                                | Nos.                           | 1                            | 1                                | 1                        | -  | -  | -  |
| Hollow jet valve                           | Nos.                           | 1                            | 1                                | 1                        | -  | -  | -  |
| <b>Diversion Tunnel</b>                    |                                |                              |                                  |                          |  |  |  |
| Name of river                              |                                | -                            | -                                | -                        | -  | Beroeng  | Beroeng Anyer  |
| Catchment area at weir                     | km <sup>2</sup>                | -                            | -                                | -                        | -  | 12.1   | 12.1 17.5  |
| Mean runoff                                | m <sup>3</sup> /sec            | -                            | -                                | -                        | -  | 0.39   | 0.39 0.59  |
| Maximum discharge capacity                 | m <sup>3</sup> /sec            | -                            | -                                | -                        | -  | 4.0  | 4.0 4.0  |
| Diverted tunnel, L                         | m                              | -                            | -                                | -                        | -  | 300  | 300 700  |
| D  | m                              | -                            | -                                | -                        | -  | 1.5  | 1.5 1.5  |
| <b>Water Transmission Facility</b>         |                                |                              |                                  |                          |  |  |  |
| Transmission pipeline, L                   | km                             | 28.0                         | Existing                         | Existing                 | Existing   | Existing   | Existing   |
| D  | m                              | 0.7                          | Existing                         | Existing                 | Existing   | Existing   | Existing   |
| <b>Krakatau pump station <sup>2/</sup></b> |                                |                              |                                  |                          |  |  |  |
| Pump discharge                             | m <sup>3</sup> /s              | -                            | Existing                         | Existing                 | 1.1  | 1.19   | 1.2  |
| Pump head                                  | m                              | -                            | Existing                         | Existing                 | 67.1   | 67.1   | 67.1   |
| Additional pump                            | kW                             | -                            | Existing                         | Existing                 | 1150   | 1200   | 1250   |
| <b>Booster pump station <sup>3/</sup></b>  |                                |                              |                                  |                          |  |  |  |
| Pump discharge                             | m <sup>3</sup> /s              | -                            | -                                | -                        | 3.1  | 3.15   | 3.20   |
| Pump head                                  | m                              | -                            | -                                | -                        | 75   | 76   | 77   |
| Pump capacity                              | kW                             | -                            | -                                | -                        | 3550   | 3650   | 3750   |
| <b>Krenceng pump station <sup>3/</sup></b> |                                |                              |                                  |                          |  |  |  |
| Pump discharge                             | m <sup>3</sup> /s              | 0.45 <sup>2/</sup>           | 0.06 <sup>3/</sup>               | 0.205 <sup>3/</sup>      | 3.1  | 3.15   | 3.20   |
| Pump head                                  | m                              | 12.0                         | 12.0                             | 12                       | 20   | 20   | 20   |
| Pump capacity                              | kW                             | -                            | -                                | -                        | -  | -  | -  |
| Connection pipeline <sup>2/</sup> , L      | m                              | 160                          | 160                              | 160                      | 160  | 160  | 160  |
| Water treatment plant <sup>3/</sup>        | m <sup>3</sup> /hr             | 1,620                        | 220                              | 740                      | 3960   | 4140   | 4320   |

Notes: 1/ means regulated peak outflow at the outlet of Rawa Danau.  
2/ Facility replaced due to development scheme  
3/ Facility added due to development scheme

Table F-2 Principal Features for Alternative Combined Development Schemes

| Item                            | Unit                | B-1   | B-2          | B-3          | C-1          | C-2          | C-3          | D-1            | D-2          | D-3          |
|---------------------------------|---------------------|---|--------------|--------------|--------------|--------------|--------------|----------------|--------------|--------------|
| Scheme combined                 |                     | K-1<br>& A-1                                    | K-1<br>& A-3 | K-1<br>& A-6 | K-2<br>& A-1 | K-2<br>& A-3 | K-2<br>& A-6 | K-3<br>& A-1   | K-3<br>& A-3 | K-3<br>& A-6 |
| Development yield               | m <sup>3</sup> /sec | 3.55  | 3.40         | 3.435        | 3.60         | 3.445        | 3.49         | 3.65           | 3.49         | 3.54         |
| Reservoir and Dam Facility      |                     | Same as corresponding single development scheme |              |              |              |              |              |                |              |              |
| <b>Transmission Facility</b>    |                     |   |              |              |              |              |              |                |              |              |
| Transmission pipeline, L        | km                  | 28.0  |              |              | 28.0         |              |              | 28.0           |              |              |
| D                               | m                   | 0.7 & Existing                                  | Existing     | Existing     | 0.7          | Existing     | Existing     | 0.7 & Existing | Existing     | Existing     |
| <b>Krakatau pump station 1/</b> |                     |   |              |              |              |              |              |                |              |              |
| pump discharge                  | m <sup>3</sup> /sec | 1.55  | 1.40         | 1.435        | 1.60         | 1.445        | 1.49         | 1.65           | 1.49         | 1.54         |
| pump head                       | m                   | 67.1  | 67.1         | 67.1         | 67.1         | 67.1         | 67.1         | 67.1           | 67.1         | 67.1         |
| Additional pumps                | kW                  | 1,130   | 1,430        | 1,480        | 1,180        | 1,480        | 1,530        | 1,230          | 1,530        | 1,580        |
| <b>Booster pump station 1/</b>  |                     |   |              |              |              |              |              |                |              |              |
| Pump discharge                  | m <sup>3</sup> /sec | 3.55  | 3.40         | 3.435        | 3.60         | 3.445        | 3.49         | 3.65           | 3.49         | 3.54         |
| Pump head                       | m                   | 65  | 82           | 84           | 66           | 83.5         | 85           | 67.5           | 85           | 86           |
| Pump capacity                   | kW                  | 3,510   | 4,240        | 4,380        | 3,630        | 4,380        | 4,520        | 3,750          | 4,520        | 4,650        |
| <b>Krenceng pump station 2/</b> |                     |   |              |              |              |              |              |                |              |              |
| pump discharge                  | m <sup>3</sup> /sec | 3.55  | 3.40         | 3.435        | 3.60         | 3.445        | 3.49         | 3.65           | 3.49         | 3.54         |
| pump head                       | m                   | 20  | 20           | 20           | 20           | 20           | 20           | 20             | 20           | 20           |
| Connection pipeline, L          | m                   | 160   | 160          | 160          | 160          | 160          | 160          | 160            | 160          | 160          |
| Water treatment plant           | m <sup>3</sup> /hr  | 5,580   | 5,040        | 5,170        | 5,760        | 5,200        | 5,370        | 5,950          | 5,370        | 5,500        |

Notes: 1/ Facility added due to development scheme  
 2/ Facility replaced due to heightening of Krenceng dam



Table F-3 Cost Estimate for Cibanten Dam: Scheme A-1

| DESCRIPTION                                      | Unit         | Qty     | UNIT PRICE |             | AMOUNT         |             |                |                |
|--|--------------|---------|------------|-------------|----------------|-------------|----------------|----------------|
|  |              |         | Fe (Yen)   | Le (Rp)     | Fe (Yen)       | Le (Rp)     |                |                |
| <b>1. PREPARATORY WORK</b><br>(20% of 2+3+4+5+6) |              |         |            |             |                |             | 463,304,644    | 2,942,315,206  |
| <b>2. DIVERSION WORK</b>                         |              |         |            |             |                |             |                |                |
| 2.1 Inlet & outlet Excavation                    | Common       | m3      | 1,053      | 276         | 1,651          | 290,626     | 1,738,503      |                |
|  | Wearrock     | m3      | 2,106      | 339         | 1,398          | 713,334     | 2,944,188      |                |
|  | Rock         | m3      | 7,371      | 962         | 3,475          | 2,090,902   | 25,614,225     |                |
|  | Concrete     | m3      | 2,640      | 13,442      | 132,187        | 35,486,880  | 348,973,680    |                |
|  | Rein bar     | t       | 100        | 5,292       | 1,460,955      | 529,200     | 146,095,500    |                |
|  | (Sub-total)  |         |            |             |                | 44,111,544  | 525,366,096    |                |
| 2.2 Tunnel (1=110m, D=5m)                        |              | m3      | 10,462     | 8,744       | 105,122        | 91,479,728  | 1,099,786,364  |                |
|  | Excavation   | m3      | 2,401      | 13,448      | 155,546        | 32,425,152  | 373,932,584    |                |
|  | Lining conc. | m3      | 686        | 13,488      | 155,516        | 9,252,768   | 106,704,556    |                |
|  | Plug conc.   | t       | 246        | 6,500       | 90,000         | 1,599,000   | 22,140,000     |                |
|  | Grouting     | t       | 123        | 5,292       | 1,460,955      | 650,916     | 179,697,465    |                |
|  | Rein bar     | t       |            |             |                |             |                |                |
|  | (Sub-total)  |         |            |             |                | 135,407,564 | 1,782,260,969  |                |
| <b>SUB-TOTAL OF 2.</b>                           |              |         |            |             |                |             | 179,519,108    | 2,307,627,065  |
| <b>3. DAM</b>                                    |              |         |            |             |                |             |                |                |
| 3.1 Cofferdam Excavation                         | Common       | m3      | 2,500      | 276         | 1,651          | 690,000     | 4,127,500      |                |
|  | Wearrock     | m3      | 200,000    | 1,514       | 5,964          | 302,800,000 | 1,192,800,000  |                |
|  | (Sub-total)  |         |            |             |                | 303,490,000 | 1,196,927,500  |                |
| 3.2 Main dam Excavation                          | Common       | m3      | 11,075     | 276         | 1,651          | 3,056,700   | 18,344,825     |                |
|  | Wearrock     | m3      | 22,150     | 339         | 1,398          | 7,598,850   | 30,965,700     |                |
|  | Rock         | m3      | 77,520     | 962         | 3,475          | 74,574,240  | 269,382,000    |                |
|  | Embankment   | m3      | 101,416    | 605         | 2,359          | 61,356,680  | 239,240,344    |                |
|  | Filter       | m3      | 62,644     | 2,285       | 5,756          | 143,141,540 | 360,378,864    |                |
|  | Random Rock  | m3      | 174,900    | 441         | 1,144          | 77,130,900  | 200,085,600    |                |
|  | Rock         | m3      | 408,105    | 1,514       | 5,964          | 617,870,970 | 2,433,938,220  |                |
|  | Grouting     | t       | 474        | 6,500       | 90,000         | 3,081,000   | 42,660,000     |                |
|  | Blanket      | t       | 114        | 6,500       | 90,000         | 741,000     | 10,260,000     |                |
|  | Consoh.      | t       | 1,287      | 6,500       | 90,000         | 8,365,500   | 115,830,000    |                |
|  | Curtain      | t       |            |             |                |             |                |                |
|  | (Sub-total)  |         |            |             |                | 996,827,380 | 3,721,225,553  |                |
| 3.3 Saddle dam Excavation                        | Common       | m3      | 3,595      | 276         | 2,176          | 992,220     | 7,822,720      |                |
|  | Wearrock     | m3      | 7,190      | 339         | 2,585          | 2,437,410   | 16,586,150     |                |
|  | Rock         | m3      | 25,160     | 962         | 4,433          | 24,203,920  | 111,534,280    |                |
|  | Embankment   | m3      | 167,975    | 244         | 1,717          | 40,985,900  | 288,413,075    |                |
|  | Grouting     | t       | 597        | 6,500       | 90,000         | 3,880,500   | 53,730,000     |                |
|  | (Sub-total)  |         |            |             |                | 72,499,950  | 480,086,225    |                |
| <b>SUB-TOTAL OF 3.</b>                           |              |         |            |             |                |             | 1,772,817,330  | 5,398,239,778  |
| <b>4. SPILLWAY</b>                               |              |         |            |             |                |             |                |                |
| 4.1 Side channel Excavation                      | Common       | m3      | 8,100      | 276         | 1,651          | 2,235,600   | 13,373,100     |                |
|  | Wearrock     | m3      | 16,200     | 339         | 1,398          | 5,491,800   | 22,647,600     |                |
|  | Rock         | m3      | 56,700     | 962         | 3,475          | 54,515,400  | 197,032,500    |                |
|  | Concrete     | m3      | 21,170     | 13,442      | 132,187        | 284,567,140 | 2,798,398,790  |                |
|  | Rein bar     | t       | 400        | 5,292       | 1,460,955      | 2,116,800   | 584,382,000    |                |
|  | (Sub-total)  |         |            |             |                | 348,956,740 | 3,615,833,990  |                |
| 4.2 Chute way Excavation                         | Common       | m3      | 14,245     | 276         | 1,651          | 3,931,620   | 23,518,495     |                |
|  | Wearrock     | m3      | 28,490     | 339         | 1,398          | 9,638,110   | 39,829,020     |                |
|  | Rock         | m3      | 99,715     | 962         | 3,475          | 95,925,830  | 346,509,625    |                |
|  | Concrete     | m3      | 11,395     | 13,442      | 132,187        | 153,171,590 | 1,526,270,865  |                |
|  | Rein bar     | t       | 220        | 5,292       | 1,460,955      | 1,164,240   | 319,210,100    |                |
|  | (Sub-total)  |         |            |             |                | 263,851,390 | 2,235,338,105  |                |
| 4.3 Flunge pool Excavation                       | Common       | m3      | 4,032      | 276         | 1,651          | 1,112,832   | 6,656,832      |                |
|  | Wearrock     | m3      | 8,064      | 339         | 1,398          | 2,733,695   | 11,273,472     |                |
|  | Rock         | m3      | 28,224     | 962         | 3,475          | 27,151,488  | 98,078,400     |                |
|  | (Sub-total)  |         |            |             |                | 30,998,016  | 116,008,704    |                |
| <b>SUB-TOTAL OF 4.</b>                           |              |         |            |             |                |             | 643,806,146    | 5,967,180,799  |
| <b>5. OUTLET WORKS</b>                           |              |         |            |             |                |             |                |                |
| 5.1 Intake tower Excavation                      | Common       | m3      | 515        | 276         | 1,651          | 142,140     | 850,265        |                |
|  | Wearrock     | m3      | 1,030      | 339         | 1,398          | 349,170     | 1,439,940      |                |
|  | Rock         | m3      | 3,606      | 962         | 3,475          | 3,468,972   | 12,530,850     |                |
|  | Concrete     | m3      | 760        | 13,442      | 132,187        | 10,215,920  | 100,462,120    |                |
|  | Rein bar     | t       | 29         | 5,292       | 1,460,955      | 153,468     | 47,367,695     |                |
|  | (Sub-total)  |         |            |             |                | 14,329,670  | 157,650,870    |                |
| 5.2 Intake shaft Excavation                      | Common       | m3      | 332        | 276         | 1,651          | 2,903,008   | 33,904,504     |                |
|  | Wearrock     | m3      | 191        | 339         | 1,398          | 2,576,208   | 28,709,286     |                |
|  | Concrete     | m3      | 191        | 13,442      | 132,187        | 2,576,208   | 28,709,286     |                |
|  | Rein bar     | t       | 6          | 5,292       | 1,460,955      | 31,752      | 8,765,730      |                |
|  | (Sub-total)  |         |            |             |                | 5,510,968   | 72,379,520     |                |
| <b>SUB-TOTAL OF 5.</b>                           |              |         |            |             |                |             | 19,840,638     | 230,030,390    |
| <b>6. METAL WORK</b>                             |              |         |            |             |                |             |                |                |
| 6.1 Diversion gate                               | Ls           | 1       |            | 33,040,000  |                | 33,040,000  |                |                |
| 6.2 Steel conduit                                | Ls           | 1       |            |             | 808,500,000    |             | 808,500,000    |                |
| 6.3 Hollow jet valve                             | Ls           | 1       |            | 45,000,000  |                | 45,000,000  |                |                |
| 6.4 Guard valve                                  | Ls           | 1       |            | 22,500,000  |                | 22,500,000  |                |                |
| <b>SUB-TOTAL OF 6.</b>                           |              |         |            |             |                |             | 100,540,000    | 808,500,000    |
| <b>7. WATER SUPPLY PIPE LINE</b>                 |              |         |            |             |                |             |                |                |
| 7.1 Excavation                                   | m3           | 134,400 |            | 276         | 1,651          | 37,094,400  | 221,894,400    |                |
| 7.2 Backfill                                     | m3           | 123,200 |            | 244         | 1,717          | 30,060,800  | 211,534,400    |                |
| 7.3 Add. pump station                            | Ls           | 1       |            | 57,000,000  |                | 57,000,000  | 385,000,000    |                |
| 7.4 Add. purification plant                      | Ls           | 1       |            | 569,000,000 |                | 569,000,000 | 3,805,000,000  |                |
| 7.5 Add. pipe line                               | Ls           | 1       |            |             | 40,040,000,000 |             | 40,040,000,000 |                |
| 7.6 Add. intake & surge tank                     | Ls           | 1       |            |             |                |             |                |                |
| <b>SUB-TOTAL OF 7.</b>                           |              |         |            |             |                |             | 693,155,200    | 44,663,428,800 |
| <b>TOTAL OF DIRECT CONSTRUCTION COST</b>         |              |         |            |             |                |             | 3,472,983,066  | 62,317,321,818 |

Table F-4 Cost Estimate for Downstream Cidanau Dam: Scheme A-3

| DESCRIPTION                                      | Unit      | Qty | UNIT PRICE |            | AMOUNT      |               |                |
|--|-----------|-----|------------|------------|-------------|---------------|----------------|
|  |           |     | Fc (Yn)    | Lc (Rp)    | Fc (Yn)     | Lc (Rp)       |                |
| <b>1. PREPARATORY WORK</b><br>(30% of 2+3+4+5+6) |           |     |            |            |             | 375,176,927   | 2,810,769,979  |
| <b>2. DIVERSION WORK</b>                         |           |     |            |            |             |               |                |
| 2.1 Inlet & outlet                               |           |     |            |            |             |               |                |
| Excavation                                       | Common    | m3  | 997        | 276        | 1,651       | 275,172       | 1,648,047      |
|  | Wear.rock | m3  | 11,970     | 339        | 1,398       | 4,057,830     | 16,734,060     |
|  | Rock      | m3  | 6,982      | 962        | 3,475       | 6,716,684     | 24,382,450     |
| Concrete   |           | m3  | 2,640      | 13,442     | 132,187     | 35,486,840    | 348,973,690    |
| Rein bar   |           | t   | 100        | 5,292      | 1,460,955   | 529,200       | 146,093,500    |
| (Sub-total)                                      |           |     |            |            |             | 47,065,766    | 537,711,737    |
| 2.2 Tunnel (L=400m, D=5m)                        |           |     |            |            |             |               |                |
| Excavation                                       |           | m3  | 10,710     | 8,741      | 105,122     | 93,618,240    | 1,125,856,620  |
| Lining conc.                                     |           | m3  | 2,464      | 13,488     | 155,516     | 33,234,837    | 383,265,364    |
| Pig conc.  |           | m3  | 686        | 13,488     | 155,516     | 9,232,768     | 106,704,556    |
| Grouting   |           | t   | 501        | 6,500      | 90,000      | 3,276,000     | 45,360,000     |
| Rein bar   |           | t   | 126        | 5,292      | 1,460,955   | 666,792       | 184,080,330    |
| (Sub-total)                                      |           |     |            |            |             | 140,078,232   | 1,845,266,850  |
| <b>SUB-TOTAL OF 2.</b>                           |           |     |            |            |             | 187,143,998   | 2,332,978,587  |
| <b>3. DAM</b>                                    |           |     |            |            |             |               |                |
| 3.1 Cofferdam                                    |           |     |            |            |             |               |                |
| Excavation                                       |           | m3  | 2,500      | 276        | 1,651       | 690,000       | 4,127,500      |
| Embankment                                       |           | m3  | 200,000    | 1,514      | 5,964       | 302,800,000   | 1,192,800,000  |
| (Sub-total)                                      |           |     |            |            |             | 303,490,000   | 1,196,927,500  |
| 3.2 Main dam                                     |           |     |            |            |             |               |                |
| Excavation                                       | Common    | m3  | 24,916     | 276        | 1,651       | 6,896,136     | 41,251,886     |
|  | Wear.rock | m3  | 54,136     | 339        | 1,398       | 18,352,104    | 75,682,128     |
|  | Rock      | m3  | 4,164      | 962        | 3,475       | 4,005,768     | 14,469,900     |
| Embankment                                       | Core      | m3  | 49,100     | 605        | 2,359       | 29,705,500    | 115,826,900    |
|  | Filter    | m3  | 31,308     | 2,285      | 5,756       | 71,538,760    | 180,208,848    |
|  | Random    | m3  | 72,975     | 441        | 1,144       | 32,141,975    | 83,483,400     |
|  | Rock      | m3  | 170,275    | 1,514      | 5,964       | 257,798,350   | 1,015,520,100  |
| Grouting   | Blocket   | t   | 56         | 6,500      | 90,000      | 364,000       | 5,040,000      |
|  | Control   | t   | 182        | 6,500      | 90,000      | 1,183,000     | 16,380,000     |
|  | Curtain   | t   | 2,556      | 6,500      | 90,000      | 16,614,000    | 230,040,000    |
| (Sub-total)                                      |           |     |            |            |             | 438,637,613   | 1,777,903,162  |
| 3.3 Sand trap basin                              |           |     |            |            |             |               |                |
| Excavation                                       | Common    | m3  | 306,750    | 276        | 2,176       | 84,663,000    | 667,488,000    |
|  | Wear.rock | m3  |            | 339        | 2,585       |               |                |
|  | Rock      | m3  |            | 962        | 4,433       |               |                |
| Maintenance road (Km)                            |           | m3  | 55,000     | 244        | 1,717       | 13,420,000    | 94,435,000     |
| Concrete   |           | m3  | 1,200      | 13,442     | 132,187     | 16,130,400    | 158,624,400    |
| (Sub-total)                                      |           |     |            |            |             | 114,213,400   | 920,547,400    |
| <b>SUB-TOTAL OF 3.</b>                           |           |     |            |            |             | 856,341,013   | 3,495,378,062  |
| <b>4. SPILLWAY</b>                               |           |     |            |            |             |               |                |
| 4.1 Side channel                                 |           |     |            |            |             |               |                |
| Excavation                                       | Common    | m3  | 103,740    | 276        | 1,651       | 28,632,240    | 171,274,740    |
|  | Wear.rock | m3  | 116,707    | 339        | 1,398       | 39,563,673    | 163,156,316    |
|  | Rock      | m3  | 38,902     | 962        | 3,475       | 37,423,724    | 135,184,450    |
| Concrete   |           | m3  | 22,724     | 13,442     | 132,187     | 302,666,008   | 3,664,752,388  |
| Rein bar   |           | t   | 520        | 5,292      | 1,460,955   | 2,751,840     | 759,696,600    |
| (Sub-total)                                      |           |     |            |            |             | 481,037,485   | 4,894,064,564  |
| 4.2 Chute way                                    |           |     |            |            |             |               |                |
| Excavation                                       | Common    | m3  | 53,093     | 276        | 1,651       | 14,653,668    | 87,656,513     |
|  | Wear.rock | m3  | 127,425    | 339        | 1,398       | 43,197,075    | 178,140,150    |
|  | Rock      | m3  | 31,856     | 962        | 3,475       | 30,615,472    | 110,699,600    |
| Concrete   |           | m3  | 8,775      | 13,442     | 132,187     | 117,933,550   | 1,159,940,925  |
| Rein bar   |           | t   | 175        | 5,292      | 1,460,955   | 926,100       | 253,917,125    |
| (Sub-total)                                      |           |     |            |            |             | 207,375,865   | 1,790,354,343  |
| 4.3 Plunge pool                                  |           |     |            |            |             |               |                |
| Excavation                                       | Common    | m3  | 2,030      | 276        | 1,651       | 560,280       | 3,351,530      |
|  | Wear.rock | m3  | 14,210     | 339        | 1,398       | 4,817,190     | 19,865,580     |
|  | Rock      | m3  | 24,360     | 962        | 3,475       | 23,434,320    | 84,651,000     |
| (Sub-total)                                      |           |     |            |            |             | 28,811,790    | 107,868,110    |
| <b>SUB-TOTAL OF 4.</b>                           |           |     |            |            |             | 717,225,140   | 6,792,287,017  |
| <b>5. OUTLET WORK</b>                            |           |     |            |            |             |               |                |
| 5.1 Intake tower                                 |           |     |            |            |             |               |                |
| Excavation                                       | Common    | m3  | 3,738      | 276        | 1,651       | 1,037,208     | 6,204,458      |
|  | Wear.rock | m3  | 4,176      | 339        | 1,398       | 1,415,661     | 5,838,048      |
|  | Rock      | m3  | 418        | 962        | 3,475       | 402,316       | 1,432,350      |
| Concrete   |           | m3  | 500        | 13,442     | 132,187     | 6,721,000     | 66,093,500     |
| Rein bar   |           | t   | 20         | 5,292      | 1,460,955   | 105,840       | 29,219,100     |
| (Sub-total)                                      |           |     |            |            |             | 9,681,824     | 108,807,656    |
| 5.2 Intake shaft                                 |           |     |            |            |             |               |                |
| Excavation                                       |           | m3  | 299        | 8,741      | 102,122     | 2,614,456     | 30,534,478     |
| Concrete   |           | m3  | 171        | 13,488     | 155,516     | 2,306,448     | 26,598,365     |
| Rein bar   |           | t   | 6          | 5,292      | 1,460,955   | 31,752        | 8,765,730      |
| (Sub-total)                                      |           |     |            |            |             | 4,952,656     | 65,898,574     |
| <b>SUB-TOTAL OF 5.</b>                           |           |     |            |            |             | 14,634,484    | 174,706,230    |
| <b>6. METAL WORK</b>                             |           |     |            |            |             |               |                |
| 6.1 Diversion gate                               |           | Ls  | 1          | 33,040,000 |             | 33,040,000    |                |
| 6.2 Sizer coustik                                |           | Ls  | 1          |            | 808,500,000 |               | 808,500,000    |
| 6.3 Hollow jet valve                             |           | Ls  | 1          | 45,000,000 |             | 45,000,000    |                |
| 6.4 Guard valve                                  |           | Ls  | 1          | 22,500,000 |             | 22,500,000    |                |
| <b>SUB-TOTAL OF 6.</b>                           |           |     |            |            |             | 100,540,000   | 808,500,000    |
| <b>7. WATER SUPPLY PIPELINE</b>                  |           |     |            |            |             |               |                |
| 7.1 Excavation                                   |           | m3  |            | 276        | 1,651       |               |                |
| 7.2 Backfill                                     |           | m3  |            | 244        | 1,717       |               |                |
| 7.3 Add. pump station                            |           | Ls  | 1          | 15,000,000 | 101,000,000 | 15,000,000    | 101,000,000    |
| 7.4 Add. purification plant                      |           | Ls  | 1          | 79,000,000 | 530,000,000 | 79,000,000    | 530,000,000    |
| 7.5 Add. pipe line                               |           | Ls  | 1          |            | 504,000,000 |               | 504,000,000    |
| 7.6 Add. Intake & surge tank                     |           | Ls  | 1          | 11,000,000 | 411,000,000 | 11,000,000    | 411,000,000    |
| <b>SUB-TOTAL OF 7.</b>                           |           |     |            |            |             | 94,000,000    | 1,135,000,000  |
| <b>TOTAL OF DIRECT CONSTRUCTION COST</b>         |           |     |            |            |             | 2,345,061,562 | 17,999,619,875 |

Table F-5 Cost Estimate for Cidanau Gated Weir: Scheme A-6

| DESCRIPTION                                | Unit     | Qty | UNIT PRICE    |             | AMOUNT        |               |                |
|--|----------|-----|---------------|-------------|---------------|---------------|----------------|
|  |          |     | Fc<br>(Yen)   | Lc<br>(Rp)  | Fc<br>(Yen)   | Lc<br>(Rp)    |                |
| 1. PREPARATORY WORK<br>(20% of 2+3+4+5)    |          |     |               |             |               | 414,455,432   | 1,755,702,092  |
| 2. DIVERSION WORK                          |          |     |               |             |               |               |                |
| 2.1 Coffering work<br>Sheet pile & bracing | t        | 159 | 131,583       | 36,915      | 20,921,697    | 5,869,485     |                |
| SUB-TOTAL OF 2.                            |          |     |               |             |               | 20,921,697    | 5,869,485      |
| 3. DAM                                     |          |     |               |             |               |               |                |
| 3.1 Main dam                               |          |     |               |             |               |               |                |
| Excavation                                 | Common   | m3  | 10,662        | 276         | 1,651         | 2,942,712     | 17,602,962     |
|  | Wea.rock | m3  | 8,462         | 339         | 1,398         | 2,868,618     | 11,829,876     |
|  | Rock     | m3  | 2,200         | 962         | 3,475         | 2,116,400     | 7,645,000      |
| Concrete                                   |          | m3  | 21,325        | 5,052       | 118,708       | 107,733,900   | 2,531,448,100  |
| Grouting                                   | Consoli. | t   | 219           | 6,500       | 90,000        | 1,423,500     | 19,710,000     |
|  | Curtain  | t   | 352           | 6,500       | 90,000        | 2,288,000     | 31,680,000     |
| SUB-TOTAL OF 3.                            |          |     |               |             |               | 119,373,130   | 2,619,915,938  |
| 4. SPILLWAY                                |          |     |               |             |               |               |                |
| 4.1 Dental work                            |          |     |               |             |               |               |                |
| Excavation                                 | Common   | m3  | 22,389        | 276         | 1,651         | 6,179,364     | 36,964,239     |
|  | Wea.rock | m3  |               | 339         | 1,398         |               |                |
|  | Rock     | m3  |               | 962         | 3,475         |               |                |
| Concrete                                   |          | m3  | 8,379         | 5,052       | 118,708       | 42,330,708    | 994,654,332    |
| (Sub-total)                                |          |     |               |             |               | 48,510,072    | 1,031,618,571  |
| 4.2 Weir & pier                            |          |     |               |             |               |               |                |
| Excavation                                 | Common   | m3  |               | 276         | 1,651         |               |                |
|  | Wea.rock | m3  | 1,170         | 339         | 1,398         | 396,630       | 1,635,660      |
|  | Rock     | m3  | 500           | 962         | 3,475         | 481,000       | 1,737,500      |
| Concrete                                   |          | m3  | 10,761        | 13,442      | 132,187       | 144,649,362   | 1,422,464,307  |
| Rein bar                                   |          | t   | 1,290         | 5,292       | 1,460,955     | 6,826,680     | 1,884,631,950  |
| Grouting                                   | Consoli. | t   | 126           | 6,500       | 90,000        | 819,000       | 11,340,000     |
|  | Curtain  | t   | 180           | 6,500       | 90,000        | 1,170,000     | 16,200,000     |
| (Sub-total)                                |          |     |               |             |               | 154,342,672   | 3,338,009,417  |
| 4.3 Hoist & bridge                         |          |     |               |             |               |               |                |
| Concrete                                   |          | m3  | 2,871         | 13,442      | 132,187       | 38,591,982    | 379,508,877    |
| Rein bar                                   |          | t   | 374           | 5,292       | 1,460,955     | 3,037,608     | 838,588,170    |
| (Sub-total)                                |          |     |               |             |               | 41,629,590    | 1,218,097,047  |
| SUB-TOTAL OF 4.                            |          |     |               |             |               | 244,482,334   | 5,587,725,035  |
| 5. METAL WORK                              |          |     |               |             |               |               |                |
| 5.1 Roller gate                            | Ls       | 1   | 1,620,000,000 |             |               | 1,620,000,000 |                |
| 5.2 Steel conduit                          | Ls       | 1   |               | 565,000,000 |               |               | 565,000,000    |
| 5.3 Hollow jet valve                       | Ls       | 1   | 45,000,000    |             |               | 45,000,000    |                |
| 5.4 Guard valve                            | Ls       | 1   | 22,500,000    |             |               | 22,500,000    |                |
| SUB-TOTAL OF 5.                            |          |     |               |             |               | 1,687,500,000 | 565,000,000    |
| 6. WATER SUPPLY PIPE LINE                  |          |     |               |             |               |               |                |
| 6.1 Excavation                             |          | m3  |               | 276         | 1,651         |               |                |
| 6.2 Backfill                               |          | m3  |               | 244         | 1,717         |               |                |
| 6.3 Add. pump station                      |          | Ls  | 1             | 30,000,000  | 207,000,000   | 30,000,000    | 207,000,000    |
| 6.4 Add. purification plant                |          | Ls  | 1             | 261,000,000 | 1,747,000,000 | 261,000,000   | 1,747,000,000  |
| 6.5 Add. pipe line                         |          | Ls  | 1             |             | 504,000,000   |               | 504,000,000    |
| 6.6 Add. intake & surge tank               |          | Ls  | 1             | 14,000,000  | 537,000,000   | 14,000,000    | 537,000,000    |
| SUB-TOTAL OF 6.                            |          |     |               |             |               | 305,000,000   | 2,995,000,000  |
| TOTAL OF DIRECT CONSTRUCTION COST          |          |     |               |             |               | 2,791,732,593 | 13,529,212,550 |

Table F-6 Cost Estimate for Heightening of Krenceng Dam without Diversion Tunnel: Scheme K-1

| DESCRIPTION                         | Unit                             | Qty                  | UNIT PRICE        |                              | AMOUNT                           |                          |                            |
|-------------------------------------|----------------------------------|----------------------|-------------------|------------------------------|----------------------------------|--------------------------|----------------------------|
|                                     |                                  |                      | Fe<br>(Yen)       | Lo<br>(Rp)                   | Fe<br>(Yen)                      | Lo<br>(Rp)               |                            |
| 1. PREPARATORY WORK<br>(20% of 2+3) |                                  |                      |                   |                              | 257,537,340                      | 1,466,768,687            |                            |
| 2. DIVERTED TUNNEL                  |                                  |                      |                   |                              |                                  |                          |                            |
| 2.1 Coffering work                  |                                  |                      |                   |                              |                                  |                          |                            |
| Coffering                           | Exca.<br>Embank                  | m3<br>m3             |                   | 276<br>441                   | 1,651<br>1,144                   |                          |                            |
| (Sub-total)                         |                                  |                      |                   |                              |                                  |                          |                            |
| 2.2 Weir                            |                                  |                      |                   |                              |                                  |                          |                            |
| Excavation                          | Common<br>Wea.rock<br>Rock       | m3<br>m3<br>m3       |                   | 276<br>339<br>962            | 1,651<br>1,398<br>3,475          |                          |                            |
| Concrete                            |                                  | m3                   |                   | 5,052                        | 118,708                          |                          |                            |
| Rein bar                            |                                  | t                    |                   | 5,292                        | 1,460,955                        |                          |                            |
| Gate                                |                                  | Ls                   |                   | 2,000,000                    |                                  |                          |                            |
| (Sub-total)                         |                                  |                      |                   |                              |                                  |                          |                            |
| 2.3 Inlet & outlet                  |                                  |                      |                   |                              |                                  |                          |                            |
| Excavation                          | Common<br>Wea.rock<br>Rock       | m3<br>m3<br>m3       |                   | 276<br>339<br>962            | 1,651<br>1,398<br>3,475          |                          |                            |
| Concrete                            |                                  | m3                   |                   | 13,442                       | 132,187                          |                          |                            |
| Rein bar                            |                                  | t                    |                   | 5,292                        | 1,460,955                        |                          |                            |
| Trash rack                          |                                  | Ls                   |                   | 1,000,000                    |                                  |                          |                            |
| (Sub-total)                         |                                  |                      |                   |                              |                                  |                          |                            |
| 2.4 Diverted tunnel                 |                                  |                      |                   |                              |                                  |                          |                            |
| Excavation                          |                                  | m3                   |                   | 8,744                        | 105,122                          |                          |                            |
| Lining conc.                        |                                  | m3                   |                   | 13,488                       | 155,546                          |                          |                            |
| Plug conc.                          |                                  | m3                   |                   | 13,488                       | 155,546                          |                          |                            |
| Grouting                            |                                  | t                    |                   | 6,500                        | 90,000                           |                          |                            |
| Rein bar                            |                                  | t                    |                   | 5,292                        | 1,460,955                        |                          |                            |
| (Sub-total)                         |                                  |                      |                   |                              |                                  |                          |                            |
| SUB-TOTAL OF 2.                     |                                  |                      |                   |                              |                                  |                          |                            |
| 3. HEIGHTENING OF KRENCENG DAM      |                                  |                      |                   |                              |                                  |                          |                            |
| 3.1 Main dam                        |                                  |                      |                   |                              |                                  |                          |                            |
| Excavation                          | Common<br>Wea.rock<br>Rock       | m3<br>m3<br>m3       | 146,652<br>97,768 | 276<br>339<br>962            | 1,651<br>1,398<br>3,475          | 40,475,952<br>33,143,352 | 242,122,452<br>136,679,664 |
| Embankment                          | Core<br>Filter<br>Random<br>Rock | m3<br>m3<br>m3<br>m3 | 1,281,085         | 605<br>2,285<br>441<br>1,514 | 2,359<br>5,756<br>1,144<br>5,964 | 775,056,425              | 3,022,079,515              |
| Grouting                            | Blanket<br>Curtain               | t<br>t               | 1,868<br>3,676    | 6,500<br>6,500               | 90,000<br>90,000                 | 12,142,000<br>23,894,000 | 168,120,000<br>330,840,000 |
| (Sub-total)                         |                                  |                      |                   |                              |                                  | 884,711,729              | 3,899,841,631              |
| 3.2 Spillway                        |                                  |                      |                   |                              |                                  |                          |                            |
| (1) Approach wall & weir            |                                  |                      |                   |                              |                                  |                          |                            |
| Excavation                          | Common<br>Wea.rock<br>Rock       | m3<br>m3<br>m3       | 3,097<br>4,645    | 276<br>339<br>962            | 1,651<br>1,398<br>3,475          | 854,772<br>1,574,655     | 5,113,147<br>6,493,710     |
| Concrete                            |                                  | m3                   | 6,628             | 13,442                       | 132,187                          | 89,093,576               | 876,135,436                |
| Rein bar                            |                                  | t                    | 135               | 5,292                        | 1,460,955                        | 714,420                  | 197,228,925                |
| (2) Chuteway & basin                |                                  |                      |                   |                              |                                  |                          |                            |
| Excavation                          | Common<br>Wea.rock<br>Rock       | m3<br>m3<br>m3       | 11,879<br>17,818  | 276<br>339<br>962            | 1,651<br>1,398<br>3,475          | 3,278,604<br>6,040,302   | 19,612,229<br>24,909,564   |
| Concrete                            |                                  | m3                   | 14,260            | 13,442                       | 132,187                          | 191,682,920              | 1,884,986,620              |
| Rein bar                            |                                  | t                    | 285               | 5,292                        | 1,460,955                        | 1,508,220                | 416,372,175                |
| Grouting                            | Consoli.                         | t                    | 35                | 6,500                        | 90,000                           | 227,500                  | 3,150,000                  |
| (3) Metal work                      |                                  |                      |                   |                              |                                  |                          |                            |
| Spillway gate                       |                                  | Ls                   | 1                 | 108,000,000                  |                                  | 108,000,000              |                            |
| (Sub-total)                         |                                  |                      |                   |                              |                                  | 402,974,969              | 3,434,001,806              |
| SUB-TOTAL OF 3.                     |                                  |                      |                   |                              |                                  | 1,287,686,698            | 7,333,843,437              |
| 4. WATER SUPPLY PIPE LINE           |                                  |                      |                   |                              |                                  |                          |                            |
| 4.1 Excavation                      |                                  | m3                   |                   | 276                          | 1,651                            |                          |                            |
| 4.2 Backfill                        |                                  | m3                   |                   | 244                          | 1,717                            |                          |                            |
| 4.3 Add. pump station               |                                  | Ls                   | 1                 | 1,022,000,000                | 6,833,000,000                    | 1,022,000,000            | 6,833,000,000              |
| 4.4 Add. purification plant         |                                  | Ls                   | 1                 | 1,385,000,000                | 9,263,000,000                    | 1,385,000,000            | 9,263,000,000              |
| 4.5 Add. pipe line                  |                                  | Ls                   |                   |                              | 1,428,000,000                    |                          |                            |
| 4.6 Add. intake & surge tank        |                                  | Ls                   | 1                 | 63,000,000                   | 2,305,000,000                    | 63,000,000               | 2,305,000,000              |
| 4.7 Receiving well                  |                                  | Ls                   | 1                 | 6,000,000                    | 218,400,000                      | 6,000,000                | 218,400,000                |
| SUB-TOTAL OF 4.                     |                                  |                      |                   |                              |                                  | 2,476,000,000            | 18,619,400,000             |
| TOTAL OF DIRECT CONSTRUCTION COST   |                                  |                      |                   |                              |                                  | 4,021,224,038            | 27,420,012,124             |

Table F-7 Cost Estimate for Heightening of Krenceng Dam with One Diversion Tunnel: Scheme K-2

| DESCRIPTION                         | Unit     | Qty | UNIT PRICE  |               | AMOUNT        |               |                |
|-------------------------------------|----------|-----|-------------|---------------|---------------|---------------|----------------|
|                                     |          |     | Fc<br>(Yen) | Lc<br>(Rp)    | Fc<br>(Yen)   | Lc<br>(Rp)    |                |
| 1. PREPARATORY WORK<br>(20% of 2+3) |          |     |             |               |               | 264,175,476   | 1,556,022,425  |
| 2. DIVERTED TUNNEL                  |          |     |             |               |               |               |                |
| 2.1 Coffering work                  |          |     |             |               |               |               |                |
| Coffering                           | Exca.    | m3  | 500         | 276           | 1,651         | 138,000       | 825,500        |
|                                     | Embank   | m3  | 500         | 441           | 1,144         | 220,500       | 572,000        |
| (Sub-total)                         |          |     |             |               |               | 358,500       | 1,397,500      |
| 2.2 Weir                            |          |     |             |               |               |               |                |
| Excavation                          | Common   | m3  | 400         | 276           | 1,651         | 110,400       | 660,400        |
|                                     | Wea.rock | m3  | 400         | 339           | 1,398         | 135,600       | 559,200        |
|                                     | Rock     | m3  | 200         | 962           | 3,475         | 192,400       | 695,000        |
| Concrete                            |          | m3  | 150         | 5,052         | 118,708       | 757,800       | 17,806,200     |
| Rein bar                            |          | t   | 15          | 5,292         | 1,460,955     | 79,380        | 21,914,325     |
| Gate                                |          | Ls  | 1           | 2,000,000     |               | 2,000,000     |                |
| (Sub-total)                         |          |     |             |               |               | 3,275,580     | 41,635,125     |
| 2.3 Inlet & outlet                  |          |     |             |               |               |               |                |
| Excavation                          | Common   | m3  | 1,664       | 276           | 1,651         | 459,264       | 2,747,264      |
|                                     | Wea.rock | m3  | 1,664       | 339           | 1,398         | 564,096       | 2,326,272      |
|                                     | Rock     | m3  | 832         | 962           | 3,475         | 800,384       | 2,891,200      |
| Concrete                            |          | m3  | 100         | 13,442        | 132,187       | 1,344,200     | 13,218,700     |
| Rein bar                            |          | t   | 20          | 5,292         | 1,460,955     | 105,840       | 29,219,100     |
| Trash rack                          |          | Ls  | 1           | 1,000,000     |               | 1,000,000     |                |
| (Sub-total)                         |          |     |             |               |               | 4,273,784     | 50,402,536     |
| 2.4 Diverted tunnel                 |          |     |             |               |               |               |                |
| Excavation                          |          | m3  | 1,600       | 8,744         | 105,122       | 13,990,400    | 168,195,200    |
| Lining conc.                        |          | m3  | 650         | 13,488        | 155,546       | 8,767,200     | 101,104,900    |
| Plug conc.                          |          | m3  |             | 13,488        | 155,546       |               |                |
| Grouting                            |          | t   | 360         | 6,500         | 90,000        | 2,340,000     | 32,400,000     |
| Rein bar                            |          | t   | 35          | 5,292         | 1,460,955     | 185,220       | 51,133,425     |
| (Sub-total)                         |          |     |             |               |               | 25,282,820    | 352,833,525    |
| SUB-TOTAL OF 2.                     |          |     |             |               |               | 33,190,684    | 446,268,686    |
| 3. HEIGHTENING OF KRENCENG DAM      |          |     |             |               |               |               |                |
| 3.1 Main dam                        |          |     |             |               |               |               |                |
| Excavation                          | Common   | m3  | 146,652     | 276           | 1,651         | 40,475,952    | 242,122,452    |
|                                     | Wea.rock | m3  | 97,768      | 339           | 1,398         | 33,143,352    | 136,679,664    |
|                                     | Rock     | m3  |             | 962           | 3,475         |               |                |
| Embankment                          | Core     | m3  | 1,281,085   | 605           | 2,359         | 775,056,425   | 3,022,079,515  |
|                                     | Filler   | m3  |             | 2,285         | 5,756         |               |                |
|                                     | Random   | m3  |             | 441           | 1,144         |               |                |
|                                     | Rock     | m3  |             | 1,514         | 5,964         |               |                |
| Grouting                            | Blanket  | t   | 1,868       | 6,500         | 90,000        | 12,142,000    | 168,120,000    |
|                                     | Curtain  | t   | 3,676       | 6,500         | 90,000        | 23,894,000    | 330,840,000    |
| (Sub-total)                         |          |     |             |               |               | 884,711,729   | 3,899,841,631  |
| 3.2 Spillway                        |          |     |             |               |               |               |                |
| (1) Approach wall & weir            |          |     |             |               |               |               |                |
| Excavation                          | Common   | m3  | 3,097       | 276           | 1,651         | 854,772       | 5,113,147      |
|                                     | Wea.rock | m3  | 4,645       | 339           | 1,398         | 1,574,655     | 6,493,710      |
|                                     | Rock     | m3  |             | 962           | 3,475         |               |                |
| Concrete                            |          | m3  | 6,628       | 13,442        | 132,187       | 89,093,576    | 876,135,436    |
| Rein bar                            |          | t   | 135         | 5,292         | 1,460,955     | 714,420       | 197,228,925    |
| (2) Chuteway & basin                |          |     |             |               |               |               |                |
| Excavation                          | Common   | m3  | 11,879      | 276           | 1,651         | 3,278,604     | 19,612,229     |
|                                     | Wea.rock | m3  | 17,818      | 339           | 1,398         | 6,040,302     | 24,909,564     |
|                                     | Rock     | m3  |             | 962           | 3,475         |               |                |
| Concrete                            |          | m3  | 14,260      | 13,442        | 132,187       | 191,682,920   | 1,884,986,620  |
| Rein bar                            |          | t   | 285         | 5,292         | 1,460,955     | 1,508,220     | 416,372,175    |
| Grouting                            | Consoli. | t   | 35          | 6,500         | 90,000        | 227,500       | 3,150,000      |
| (3) Metal work                      |          |     |             |               |               |               |                |
| Spillway gate                       |          | Ls  | 1           | 108,000,000   |               | 108,000,000   |                |
| (Sub-total)                         |          |     |             |               |               | 402,974,969   | 3,434,001,806  |
| SUB-TOTAL OF 3.                     |          |     |             |               |               | 1,287,686,698 | 7,333,843,437  |
| 4. WATER SUPPLY PIPE LINE           |          |     |             |               |               |               |                |
| 4.1 Excavation                      |          | m3  |             | 276           | 1,651         |               |                |
| 4.2 Backfill                        |          | m3  |             | 244           | 1,717         |               |                |
| 4.3 Add. pump station               |          | Ls  | 1           | 1,043,000,000 | 6,977,000,000 | 1,043,000,000 | 6,977,000,000  |
| 4.4 Add. purification plant         |          | Ls  | 1           | 1,448,000,000 | 9,683,000,000 | 1,448,000,000 | 9,683,000,000  |
| 4.5 Add. pipe line                  |          | Ls  |             |               | 1,428,000,000 |               |                |
| 4.6 Add. intake & surge tank        |          | Ls  | 1           | 65,000,000    | 2,394,000,000 | 65,000,000    | 2,394,000,000  |
| 4.7 Receiving well                  |          | Ls  | 1           | 6,000,000     | 218,400,000   | 6,000,000     | 218,400,000    |
| SUB-TOTAL OF 4.                     |          |     |             |               |               | 2,562,000,000 | 19,272,400,000 |
| TOTAL OF DIRECT CONSTRUCTION COST   |          |     |             |               |               | 4,147,052,858 | 28,608,534,548 |

Table F-8 Cost Estimate for Heightening of Krenceng Dam with Two Diversion Tunnels: Scheme K-3

| DESCRIPTION                         | Unit     | Qty | UNIT PRICE  |               | AMOUNT         |               |                |
|-------------------------------------|----------|-----|-------------|---------------|----------------|---------------|----------------|
|                                     |          |     | Fc<br>(Yen) | Lc<br>(Rp)    | Fc<br>(Yen)    | Lc<br>(Rp)    |                |
| 1. PREPARATORY WORK<br>(20% of 2+3) |          |     |             |               | 277,982,360    | 1,734,709,347 |                |
| 2. DIVERTED TUNNEL                  |          |     |             |               |                |               |                |
| 2.1 Coffering work                  |          |     |             |               |                |               |                |
| Coffering                           | Exca.    | m3  | 1,000       | 276           | 1,651          | 276,000       | 1,651,000      |
|                                     | Embank   | m3  | 1,000       | 441           | 1,144          | 441,000       | 1,144,000      |
| (Sub-total)                         |          |     |             |               |                | 717,000       | 2,795,000      |
| 2.2 Weir                            |          |     |             |               |                |               |                |
| Excavation                          | Common   | m3  | 1,200       | 276           | 1,651          | 331,200       | 1,981,200      |
|                                     | Wea.rock | m3  | 1,200       | 339           | 1,398          | 406,800       | 1,677,600      |
|                                     | Rock     | m3  | 600         | 962           | 3,475          | 577,200       | 2,085,000      |
| Concrete                            |          | m3  | 410         | 5,052         | 118,708        | 2,071,320     | 48,670,280     |
| Rein bar                            |          | t   | 41          | 5,292         | 1,460,955      | 216,972       | 59,899,155     |
| Gate                                |          | Ls  | 2           | 2,000,000     |                | 4,000,000     |                |
| (Sub-total)                         |          |     |             |               |                | 7,603,492     | 114,313,235    |
| 2.3 Inlet & outlet                  |          |     |             |               |                |               |                |
| Excavation                          | Common   | m3  | 4,576       | 276           | 1,651          | 1,262,976     | 7,554,976      |
|                                     | Wea.rock | m3  | 4,576       | 339           | 1,398          | 1,551,264     | 6,397,248      |
|                                     | Rock     | m3  | 2,288       | 962           | 3,475          | 2,201,056     | 7,950,800      |
| Concrete                            |          | m3  | 200         | 13,442        | 132,187        | 2,688,400     | 26,437,400     |
| Rein bar                            |          | t   | 40          | 5,292         | 1,460,955      | 211,680       | 58,438,200     |
| Trash rack                          |          | Ls  | 2           | 1,000,000     |                | 2,000,000     |                |
| (Sub-total)                         |          |     |             |               |                | 9,915,376     | 106,778,624    |
| 2.4 Diverted tunnel                 |          |     |             |               |                |               |                |
| Excavation                          |          | m3  | 5,320       | 8,744         | 105,122        | 46,518,080    | 559,249,040    |
| Lining conc.                        |          | m3  | 2,170       | 13,488        | 155,546        | 29,268,960    | 337,534,820    |
| Plug conc.                          |          | m3  |             | 13,488        | 155,546        |               |                |
| Grouting                            |          | t   | 1,200       | 6,500         | 90,000         | 7,800,000     | 108,000,000    |
| Rein bar                            |          | t   | 76          | 5,292         | 1,460,955      | 402,192       | 111,032,580    |
| (Sub-total)                         |          |     |             |               |                | 83,989,232    | 1,115,816,440  |
| SUB-TOTAL OF 2.                     |          |     |             |               |                | 102,225,100   | 1,339,703,299  |
| 3. HEIGHTENING OF KRENCENG DAM      |          |     |             |               |                |               |                |
| 3.1 Main dam                        |          |     |             |               |                |               |                |
| Excavation                          | Common   | m3  | 146,652     | 276           | 1,651          | 40,475,952    | 242,122,452    |
|                                     | Wea.rock | m3  | 97,768      | 339           | 1,398          | 33,143,352    | 136,679,664    |
|                                     | Rock     | m3  |             | 962           | 3,475          |               |                |
| Embankment                          | Core     | m3  | 1,281,085   | 605           | 2,359          | 775,056,425   | 3,022,079,515  |
|                                     | Filter   | m3  |             | 2,285         | 5,756          |               |                |
|                                     | Random   | m3  |             | 441           | 1,144          |               |                |
|                                     | Rock     | m3  |             | 1,514         | 5,964          |               |                |
| Grouting                            | Blanket  | t   | 1,868       | 6,500         | 90,000         | 12,142,000    | 168,120,000    |
|                                     | Curtain  | t   | 3,676       | 6,500         | 90,000         | 23,894,000    | 330,840,000    |
| (Sub-total)                         |          |     |             |               |                | 884,711,729   | 3,899,841,631  |
| 3.2 Spillway                        |          |     |             |               |                |               |                |
| (1) Approach wall & weir            |          |     |             |               |                |               |                |
| Excavation                          | Common   | m3  | 3,097       | 276           | 1,651          | 854,772       | 5,113,147      |
|                                     | Wea.rock | m3  | 4,645       | 339           | 1,398          | 1,574,655     | 6,493,710      |
|                                     | Rock     | m3  |             | 962           | 3,475          |               |                |
| Concrete                            |          | m3  | 6,628       | 13,442        | 132,187        | 89,093,576    | 876,135,436    |
| Rein bar                            |          | t   | 135         | 5,292         | 1,460,955      | 714,420       | 197,228,925    |
| (2) Chuteway & basin                |          |     |             |               |                |               |                |
| Excavation                          | Common   | m3  | 11,879      | 276           | 1,651          | 3,278,604     | 19,612,229     |
|                                     | Wea.rock | m3  | 17,818      | 339           | 1,398          | 6,040,302     | 24,909,564     |
|                                     | Rock     | m3  |             | 962           | 3,475          |               |                |
| Concrete                            |          | m3  | 14,260      | 13,442        | 132,187        | 191,682,920   | 1,884,986,620  |
| Rein bar                            |          | t   | 285         | 5,292         | 1,460,955      | 1,508,220     | 416,372,175    |
| Grouting                            | Consoli. | t   | 35          | 6,500         | 90,000         | 227,500       | 3,150,000      |
| (3) Metal work                      |          |     |             |               |                |               |                |
| Spillway gate                       |          | Ls  | 1           | 108,000,000   |                | 108,000,000   |                |
| (Sub-total)                         |          |     |             |               |                | 402,974,969   | 3,434,001,806  |
| SUB-TOTAL OF 3.                     |          |     |             |               |                | 1,287,686,698 | 7,333,843,437  |
| 4. WATER SUPPLY PIPE LINE           |          |     |             |               |                |               |                |
| 4.1 Excavation                      |          | m3  |             | 276           | 1,651          |               |                |
| 4.2 Backfill                        |          | m3  |             | 244           | 1,717          |               |                |
| 4.3 Add. pump station               |          | Ls  | 1           | 1,065,000,000 | 7,120,000,000  | 1,065,000,000 | 7,120,000,000  |
| 4.4 Add. purification plant         |          | Ls  | 1           | 1,511,000,000 | 10,103,000,000 | 1,511,000,000 | 10,103,000,000 |
| 4.5 Add. pipe line                  |          | Ls  |             |               | 1,540,000,000  |               |                |
| 4.6 Add. intake & surge tank        |          | Ls  | 1           | 68,000,000    | 2,484,000,000  | 68,000,000    | 2,484,000,000  |
| 4.7 Receiving well                  |          | Ls  | 1           | 6,000,000     | 218,400,000    | 6,000,000     | 218,400,000    |
| SUB-TOTAL OF 4.                     |          |     |             |               |                | 2,650,000,000 | 19,925,400,000 |
| TOTAL OF DIRECT CONSTRUCTION COST   |          |     |             |               |                | 4,317,894,158 | 30,333,656,083 |

Table F-9 Cost Estimate for Cibanten Dam: Scheme B-1

| DESCRIPTION                               | Unit        | Qty | UNIT PRICE |            | AMOUNT         |               |                |
|---|-------------|-----|------------|------------|----------------|---------------|----------------|
|   |             |     | Pc (Ym)    | Lc (Rp)    | Pc (Ym)        | Lc (Rp)       |                |
| 1. PREPARATORY WORK<br>(20% of 2+3+4+5+6) |             |     |            |            |                | 464,133,519   | 2,947,352,634  |
| 2. DIVERSION WORK                         |             |     |            |            |                |               |                |
| 2.1 Inlet & culvert                       |             |     |            |            |                |               |                |
| Excavation                                | Common      | m3  | 1,053      | 276        | 1,651          | 290,628       | 1,738,503      |
|   | Wear rock   | m3  | 2,106      | 339        | 1,398          | 713,934       | 2,914,188      |
|   | Rock        | m3  | 7,371      | 962        | 3,475          | 7,090,902     | 25,614,225     |
|   | Concrete    | m3  | 2,640      | 13,442     | 132,187        | 35,486,830    | 348,973,680    |
|   | Rein bar    | t   | 100        | 5,292      | 1,460,955      | 529,200       | 146,095,500    |
|   | (Sub-total) |     |            |            |                | 44,111,544    | 525,366,096    |
| 2.2 Tunnel (L=410m, D=5m)                 |             |     |            |            |                |               |                |
| Excavation                                |             | m3  | 10,462     | 8,744      | 105,122        | 91,479,728    | 1,099,716,364  |
| Lining conc.                              |             | m3  | 2,404      | 13,488     | 155,516        | 32,425,152    | 373,932,384    |
| Plug conc.                                |             | m3  | 686        | 13,488     | 155,516        | 9,232,768     | 106,704,556    |
| Grouting                                  |             | t   | 246        | 6,500      | 90,000         | 1,599,000     | 22,140,000     |
| Rein bar                                  |             | t   | 123        | 5,292      | 1,460,955      | 650,916       | 179,697,465    |
|   | (Sub-total) |     |            |            |                | 135,407,564   | 1,782,280,969  |
| SUB-TOTAL OF 2.                           |             |     |            |            |                | 179,519,108   | 2,307,627,065  |
| 3. DAM                                    |             |     |            |            |                |               |                |
| 3.1 Cofferdam                             |             |     |            |            |                |               |                |
| Excavation                                |             | m3  | 2,500      | 276        | 1,651          | 690,000       | 4,127,500      |
| Embankment                                |             | m3  | 200,000    | 1,514      | 5,964          | 302,800,000   | 1,192,800,000  |
|   | (Sub-total) |     |            |            |                | 303,490,000   | 1,196,927,500  |
| 3.2 Main dam                              |             |     |            |            |                |               |                |
| Excavation                                | Common      | m3  | 11,075     | 276        | 1,651          | 3,056,700     | 18,284,825     |
|   | Wear rock   | m3  | 22,150     | 339        | 1,398          | 7,508,850     | 30,565,700     |
|   | Rock        | m3  | 77,530     | 962        | 3,475          | 74,371,280    | 269,382,000    |
|   | Core        | m3  | 101,416    | 605        | 2,359          | 61,356,650    | 239,280,344    |
|   | Filter      | m3  | 62,641     | 2,285      | 5,756          | 141,141,580   | 360,378,864    |
|   | Roaden      | m3  | 174,900    | 441        | 1,144          | 77,130,500    | 203,085,600    |
|   | Rock        | m3  | 408,105    | 1,514      | 5,964          | 617,870,970   | 2,433,938,220  |
|   | Blanket     | t   | 474        | 6,500      | 90,000         | 3,081,000     | 42,660,000     |
|   | Cosoli.     | t   | 114        | 6,500      | 90,000         | 741,000       | 10,260,000     |
|   | Curtain     | t   | 1,287      | 6,500      | 90,000         | 8,365,500     | 115,530,000    |
|   | (Sub-total) |     |            |            |                | 996,827,380   | 3,721,225,553  |
| 3.3 Saddle dam                            |             |     |            |            |                |               |                |
| Excavation                                | Common      | m3  | 3,595      | 276        | 2,176          | 992,220       | 7,822,720      |
|   | Wear rock   | m3  | 7,190      | 339        | 2,515          | 2,437,410     | 18,586,150     |
|   | Rock        | m3  | 25,160     | 962        | 4,433          | 24,203,920    | 111,531,280    |
|   | Embankment  | m3  | 167,995    | 234        | 1,717          | 40,985,900    | 238,413,075    |
|   | Grouting    | t   | 597        | 13,442     | 132,187        | 8,024,874     | 78,915,639     |
|   | (Sub-total) |     |            |            |                | 76,644,324    | 505,271,864    |
| SUB-TOTAL OF 3.                           |             |     |            |            |                | 1,376,961,704 | 5,423,424,917  |
| 4. SPILLWAY                               |             |     |            |            |                |               |                |
| 4.1 Side channel                          |             |     |            |            |                |               |                |
| Excavation                                | Common      | m3  | 8,100      | 276        | 1,651          | 2,235,600     | 13,373,100     |
|   | Wear rock   | m3  | 16,200     | 339        | 1,398          | 5,491,800     | 22,647,600     |
|   | Rock        | m3  | 56,700     | 962        | 3,475          | 54,545,400    | 197,032,500    |
|   | Concrete    | m3  | 21,170     | 13,442     | 132,187        | 284,567,140   | 2,798,398,790  |
|   | Rein bar    | t   | 400        | 5,292      | 1,460,955      | 2,116,800     | 584,382,000    |
|   | (Sub-total) |     |            |            |                | 348,956,740   | 3,615,833,990  |
| 4.2 Chaseway                              |             |     |            |            |                |               |                |
| Excavation                                | Common      | m3  | 14,245     | 276        | 1,651          | 3,931,620     | 23,518,495     |
|   | Wear rock   | m3  | 28,490     | 339        | 1,398          | 9,688,110     | 39,829,020     |
|   | Rock        | m3  | 99,715     | 962        | 3,475          | 95,925,830    | 346,509,625    |
|   | Concrete    | m3  | 11,395     | 13,442     | 132,187        | 153,171,580   | 1,506,270,865  |
|   | Rein bar    | t   | 230        | 5,292      | 1,450,955      | 1,164,280     | 319,210,100    |
|   | (Sub-total) |     |            |            |                | 263,851,390   | 2,235,338,105  |
| 4.3 Phuge pool                            |             |     |            |            |                |               |                |
| Excavation                                | Common      | m3  | 4,032      | 276        | 1,651          | 1,112,832     | 6,656,832      |
|   | Wear rock   | m3  | 8,064      | 339        | 1,398          | 2,733,696     | 11,273,472     |
|   | Rock        | m3  | 28,224     | 962        | 3,475          | 27,151,458    | 98,078,400     |
|   | (Sub-total) |     |            |            |                | 30,998,016    | 116,008,704    |
| SUB-TOTAL OF 4.                           |             |     |            |            |                | 643,806,146   | 5,967,160,799  |
| 5. OUTLET WORK                            |             |     |            |            |                |               |                |
| 5.1 Intake tower                          |             |     |            |            |                |               |                |
| Excavation                                | Common      | m3  | 515        | 276        | 1,651          | 142,140       | 850,265        |
|   | Wear rock   | m3  | 1,030      | 339        | 1,398          | 349,170       | 1,433,940      |
|   | Rock        | m3  | 3,606      | 962        | 3,475          | 3,468,972     | 12,530,830     |
|   | Concrete    | m3  | 760        | 13,442     | 132,187        | 10,213,920    | 100,462,120    |
|   | Rein bar    | t   | 29         | 5,292      | 1,460,955      | 153,468       | 42,387,695     |
|   | (Sub-total) |     |            |            |                | 14,329,670    | 157,690,870    |
| 5.2 Intake shaft                          |             |     |            |            |                |               |                |
| Excavation                                |             | m3  | 332        | 8,744      | 102,122        | 2,903,038     | 33,994,504     |
| Concrete                                  |             | m3  | 191        | 13,488     | 155,516        | 2,576,208     | 29,709,288     |
| Rein bar                                  |             | t   | 6          | 5,292      | 1,460,955      | 31,752        | 8,765,730      |
|   | (Sub-total) |     |            |            |                | 5,510,998     | 72,379,520     |
| SUB-TOTAL OF 5.                           |             |     |            |            |                | 19,840,638    | 230,030,390    |
| 6. METAL WORK                             |             |     |            |            |                |               |                |
| 6.1 Diversion gate                        |             | Ls  | 1          | 33,040,000 |                | 33,040,000    |                |
| 6.2 Steel conduit                         |             | Ls  | 1          |            | 808,500,000    |               | 808,500,000    |
| 6.3 Hollow jet valve                      |             | Ls  | 1          | 45,000,000 |                | 45,000,000    |                |
| 6.4 Guard valve                           |             | Ls  | 1          | 22,500,000 |                | 22,500,000    |                |
| SUB-TOTAL OF 6.                           |             |     |            |            |                | 100,540,000   | 808,500,000    |
| 7. WATER SUPPLY PIPE LINE                 |             |     |            |            |                |               |                |
| 7.1 Excavation                            |             | m3  | 134,600    | 276        | 1,651          | 37,091,400    | 221,891,400    |
| 7.2 Backfill                              |             | m3  | 123,200    | 241        | 1,717          | 30,060,800    | 211,531,400    |
| 7.3 Add. pump station                     |             | Ls  |            |            |                |               |                |
| 7.4 Add. purification plant               |             | Ls  |            |            |                |               |                |
| 7.5 Add. pipe line                        |             | Ls  | 1          |            | 39,200,000,000 |               | 39,200,000,000 |
| 7.6 Add. intake & surge tank              |             | Ls  |            |            |                |               |                |
| SUB-TOTAL OF 7.                           |             |     |            |            |                | 67,155,200    | 39,633,928,800 |
| TOTAL OF DIRECT CONSTRUCTION COST         |             |     |            |            |                | 2,851,956,315 | 57,317,544,605 |

Table F-10 Cost Estimate for Heightening of Krenceng Dam without Diversion Tunnel: Scheme B-1

| DESCRIPTION                         | Unit     | Qty | UNIT PRICE  |               | AMOUNT        |               |                |
|-------------------------------------|----------|-----|-------------|---------------|---------------|---------------|----------------|
|                                     |          |     | Fc<br>(Yen) | Lc<br>(Rp)    | Fc<br>(Yen)   | Lc<br>(Rp)    |                |
| 1. PREPARATORY WORK<br>(20% of 2+3) |          |     |             |               |               | 257,537,340   | 1,466,768,687  |
| 2. DIVERTED TUNNEL                  |          |     |             |               |               |               |                |
| 2.1 Coffering work                  |          |     |             |               |               |               |                |
| Coffering                           | Exca.    | m3  |             | 276           | 1,651         |               |                |
|                                     | Embank   | m3  |             | 441           | 1,144         |               |                |
| (Sub-total)                         |          |     |             |               |               |               |                |
| 2.2 Weir                            |          |     |             |               |               |               |                |
| Excavation                          | Common   | m3  |             | 276           | 1,651         |               |                |
|                                     | Wea.rock | m3  |             | 339           | 1,398         |               |                |
|                                     | Rock     | m3  |             | 962           | 3,475         |               |                |
| Concrete                            |          | m3  |             | 5,052         | 118,708       |               |                |
| Rein bar                            |          | t   |             | 5,292         | 1,460,955     |               |                |
| Gate                                |          | Ls  |             | 2,000,000     |               |               |                |
| (Sub-total)                         |          |     |             |               |               |               |                |
| 2.3 Inlet & outlet                  |          |     |             |               |               |               |                |
| Excavation                          | Common   | m3  |             | 276           | 1,651         |               |                |
|                                     | Wea.rock | m3  |             | 339           | 1,398         |               |                |
|                                     | Rock     | m3  |             | 962           | 3,475         |               |                |
| Concrete                            |          | m3  |             | 13,442        | 132,187       |               |                |
| Rein bar                            |          | t   |             | 5,292         | 1,460,955     |               |                |
| Trash rack                          |          | Ls  |             | 1,000,000     |               |               |                |
| (Sub-total)                         |          |     |             |               |               |               |                |
| 2.4 Diverted tunnel                 |          |     |             |               |               |               |                |
| Excavation                          |          | m3  |             | 8,744         | 105,122       |               |                |
| Lining conc.                        |          | m3  |             | 13,488        | 155,546       |               |                |
| Plug conc.                          |          | m3  |             | 13,488        | 155,546       |               |                |
| Grouting                            |          | t   |             | 6,500         | 90,000        |               |                |
| Rein bar                            |          | t   |             | 5,292         | 1,460,955     |               |                |
| (Sub-total)                         |          |     |             |               |               |               |                |
| SUB-TOTAL OF 2.                     |          |     |             |               |               |               |                |
| 3. HEIGHTENING OF KRENCENG DAM      |          |     |             |               |               |               |                |
| 3.1 Main dam                        |          |     |             |               |               |               |                |
| Excavation                          | Common   | m3  | 146,652     | 276           | 1,651         | 40,475,952    | 242,122,452    |
|                                     | Wea.rock | m3  | 97,768      | 339           | 1,398         | 33,143,352    | 136,679,664    |
|                                     | Rock     | m3  |             | 962           | 3,475         |               |                |
| Embankment                          | Core     | m3  | 1,281,085   | 605           | 2,359         | 775,056,425   | 3,022,079,515  |
|                                     | Filter   | m3  |             | 2,285         | 5,756         |               |                |
|                                     | Random   | m3  |             | 441           | 1,144         |               |                |
|                                     | Rock     | m3  |             | 1,514         | 5,964         |               |                |
| Grouting                            | Blanket  | t   | 1,868       | 6,500         | 90,000        | 12,142,000    | 168,120,000    |
|                                     | Curtain  | t   | 3,676       | 6,500         | 90,000        | 23,894,000    | 330,840,000    |
| (Sub-total)                         |          |     |             |               |               |               |                |
|                                     |          |     |             |               |               | 884,711,729   | 3,899,841,631  |
| 3.2 Spillway                        |          |     |             |               |               |               |                |
| (1) Approach wall & weir            |          |     |             |               |               |               |                |
| Excavation                          | Common   | m3  | 3,097       | 276           | 1,651         | 854,772       | 5,113,147      |
|                                     | Wea.rock | m3  | 4,645       | 339           | 1,398         | 1,574,655     | 6,493,710      |
|                                     | Rock     | m3  |             | 962           | 3,475         |               |                |
| Concrete                            |          | m3  | 6,628       | 13,442        | 132,187       | 89,093,576    | 876,135,436    |
| Rein bar                            |          | t   | 135         | 5,292         | 1,460,955     | 714,420       | 197,228,925    |
| (2) Chuteway & basin                |          |     |             |               |               |               |                |
| Excavation                          | Common   | m3  | 11,879      | 276           | 1,651         | 3,278,604     | 19,612,229     |
|                                     | Wea.rock | m3  | 17,818      | 339           | 1,398         | 6,040,302     | 24,909,564     |
|                                     | Rock     | m3  |             | 962           | 3,475         |               |                |
| Concrete                            |          | m3  | 14,260      | 13,442        | 132,187       | 191,682,920   | 1,884,986,620  |
| Rein bar                            |          | t   | 285         | 5,292         | 1,460,955     | 1,508,220     | 416,372,175    |
| Grouting                            | Consoli. | t   | 35          | 6,500         | 90,000        | 227,500       | 3,150,000      |
| (3) Metal work                      |          |     |             |               |               |               |                |
| Spillway gate                       |          | Ls  | 1           | 108,000,000   |               | 108,000,000   |                |
| (Sub-total)                         |          |     |             |               |               |               |                |
|                                     |          |     |             |               |               | 402,974,969   | 3,434,001,806  |
| SUB-TOTAL OF 3.                     |          |     |             |               |               | 1,287,686,698 | 7,333,843,437  |
| 4. WATER SUPPLY PIPE LINE           |          |     |             |               |               |               |                |
| 4.1 Excavation                      |          | m3  |             | 276           | 1,651         |               |                |
| 4.2 Backfill                        |          | m3  |             | 244           | 1,717         |               |                |
| 4.3 Add. pump station               |          | Ls  | 1           | 1,145,000,000 | 7,657,000,000 | 1,145,000,000 | 7,657,000,000  |
| 4.4 Add. purification plant         |          | Ls  | 1           | 1,385,000,000 | 9,263,000,000 | 1,385,000,000 | 9,263,000,000  |
| 4.5 Add. pipe line                  |          | Ls  |             |               | 1,540,000,000 |               |                |
| 4.6 Add. intake & surge tank        |          | Ls  | 1           | 74,000,000    | 2,720,000,000 | 74,000,000    | 2,720,000,000  |
| 4.7 Receiving well                  |          | Ls  | 1           | 6,000,000     | 218,400,000   | 6,000,000     | 218,400,000    |
| (Sub-total)                         |          |     |             |               |               |               |                |
|                                     |          |     |             |               |               | 2,610,000,000 | 19,858,400,000 |
| SUB-TOTAL OF 4.                     |          |     |             |               |               | 2,610,000,000 | 19,858,400,000 |
| TOTAL OF DIRECT CONSTRUCTION COST   |          |     |             |               |               | 4,155,224,038 | 28,659,012,124 |



Table F-11 Cost Estimate for Downstream Cidanau Dam: Scheme B-2

| DESCRIPTION                                      | Unit     | Qty | UNIT PRICE |            | AMOUNT      |               |                |
|--|----------|-----|------------|------------|-------------|---------------|----------------|
|  |          |     | Fc (Yn)    | 1c (Rp)    | Fc (Yn)     | 1c (Rp)       |                |
| <b>1. PREPARATORY WORK</b><br>(20% of 2+3+4+5+6) |          |     |            |            | 375,176,927 | 2,810,769,919 |                |
| <b>2. DIVERSION WORK</b>                         |          |     |            |            |             |               |                |
| 2.1 Inlet & outlet                               |          |     |            |            |             |               |                |
| Excavation                                       | Common   | m3  | 997        | 276        | 1,651       | 275,172       | 1,646,017      |
|  | Wearrock | m3  | 11,970     | 339        | 1,398       | 4,037,830     | 16,734,060     |
|  | Rock     | m3  | 6,987      | 962        | 3,475       | 8,716,684     | 24,282,450     |
| Concrete   |          | m3  | 2,640      | 13,442     | 132,187     | 35,446,880    | 348,973,680    |
| Rein bar   |          | t   | 100        | 5,292      | 1,460,955   | 539,330       | 146,695,500    |
| (Sub-total)                                      |          |     |            |            |             | 47,065,766    | 537,711,737    |
| 2.2 Turnock(l=90m,D=5m)                          |          |     |            |            |             |               |                |
| Excavation                                       |          | m3  | 10,710     | 8,744      | 105,122     | 93,618,240    | 1,125,856,620  |
| Lining conc.                                     |          | m3  | 2,465      | 13,488     | 155,546     | 33,234,432    | 383,265,344    |
| Flag conc.                                       |          | m3  | 685        | 13,488     | 155,546     | 9,252,768     | 106,704,556    |
| Grooving   |          | t   | 504        | 6,500      | 90,000      | 3,276,800     | 43,380,000     |
| Rein bar   |          | t   | 126        | 5,292      | 1,460,955   | 666,792       | 184,080,330    |
| (Sub-total)                                      |          |     |            |            |             | 140,078,232   | 1,845,266,850  |
| <b>SUB-TOTAL OF 2.</b>                           |          |     |            |            |             | 187,143,998   | 2,382,978,587  |
| <b>3. DAM</b>                                    |          |     |            |            |             |               |                |
| 3.1 Cofferdam                                    |          |     |            |            |             |               |                |
| Excavation                                       |          | m3  | 2,500      | 276        | 1,651       | 690,000       | 4,127,500      |
| Embankment                                       |          | m3  | 200,000    | 1,514      | 5,964       | 302,800,000   | 1,192,800,000  |
| (Sub-total)                                      |          |     |            |            |             | 303,490,000   | 1,196,927,500  |
| 3.2 Main dam                                     |          |     |            |            |             |               |                |
| Excavation                                       | Common   | m3  | 24,916     | 276        | 1,651       | 6,896,136     | 41,251,886     |
|  | Wearrock | m3  | 54,136     | 339        | 1,398       | 18,352,104    | 75,682,128     |
|  | Rock     | m3  | 4,164      | 962        | 3,475       | 4,005,768     | 14,469,900     |
| Embankment                                       |          | m3  | 49,100     | 605        | 2,359       | 29,705,500    | 115,826,900    |
| Filter   |          | m3  | 31,308     | 2,285      | 5,756       | 71,538,780    | 180,208,848    |
| Random   |          | m3  | 72,975     | 441        | 1,144       | 32,181,975    | 83,483,400     |
| Rock   |          | m3  | 170,275    | 1,514      | 5,964       | 257,796,320   | 1,015,520,100  |
| Grooving   |          | t   | 56         | 6,500      | 90,000      | 364,000       | 5,040,000      |
| Consoli.   |          | t   | 182        | 6,500      | 90,000      | 1,183,000     | 16,380,000     |
| Curtain  |          | t   | 2,556      | 6,500      | 90,000      | 16,614,000    | 230,040,000    |
| (Sub-total)                                      |          |     |            |            |             | 438,637,613   | 1,777,903,162  |
| 3.3 Sand trap basin                              |          |     |            |            |             |               |                |
| Excavation                                       | Common   | m3  | 306,750    | 276        | 2,176       | 84,663,000    | 687,488,000    |
|  | Wearrock | m3  |            | 339        | 2,585       |               |                |
|  | Rock     | m3  |            | 962        | 4,433       |               |                |
| Maintenance road(2km)                            |          | m3  | 55,000     | 244        | 1,717       | 13,420,000    | 94,435,000     |
| Concrete   |          | m3  | 1,200      | 13,442     | 132,187     | 16,130,400    | 158,624,400    |
| (Sub-total)                                      |          |     |            |            |             | 114,213,400   | 920,547,400    |
| <b>SUB-TOTAL OF 3.</b>                           |          |     |            |            |             | 556,341,013   | 3,895,378,062  |
| <b>4. SPILLWAY</b>                               |          |     |            |            |             |               |                |
| 4.1 Side channel                                 |          |     |            |            |             |               |                |
| Excavation                                       | Common   | m3  | 103,740    | 276        | 1,651       | 28,632,240    | 171,274,740    |
|  | Wearrock | m3  | 116,707    | 339        | 1,398       | 39,563,673    | 163,156,366    |
|  | Rock     | m3  | 38,502     | 962        | 3,475       | 37,423,724    | 135,184,450    |
| Concrete   |          | m3  | 27,724     | 13,442     | 132,187     | 372,666,008   | 3,664,752,344  |
| Rein bar   |          | t   | 520        | 5,292      | 1,460,955   | 2,751,840     | 759,696,600    |
| (Sub-total)                                      |          |     |            |            |             | 481,037,485   | 4,894,064,564  |
| 4.2 Chateway                                     |          |     |            |            |             |               |                |
| Excavation                                       | Common   | m3  | 53,693     | 276        | 1,651       | 14,653,668    | 87,656,543     |
|  | Wearrock | m3  | 127,425    | 339        | 1,398       | 43,197,075    | 178,180,150    |
|  | Rock     | m3  | 31,856     | 962        | 3,475       | 30,645,472    | 110,699,600    |
| Concrete   |          | m3  | 8,775      | 13,442     | 132,187     | 117,953,550   | 1,159,940,925  |
| Rein bar   |          | t   | 175        | 5,292      | 1,460,955   | 926,100       | 253,917,125    |
| (Sub-total)                                      |          |     |            |            |             | 207,375,865   | 1,790,354,343  |
| 4.3 Flange pool                                  |          |     |            |            |             |               |                |
| Excavation                                       | Common   | m3  | 2,000      | 276        | 1,651       | 560,280       | 3,351,530      |
|  | Wearrock | m3  | 14,210     | 339        | 1,398       | 4,817,196     | 19,865,580     |
|  | Rock     | m3  | 24,380     | 962        | 3,475       | 23,434,320    | 84,651,000     |
| (Sub-total)                                      |          |     |            |            |             | 28,811,796    | 107,868,110    |
| <b>SUB-TOTAL OF 4.</b>                           |          |     |            |            |             | 717,225,140   | 6,792,287,017  |
| <b>5. OUTLET WORK</b>                            |          |     |            |            |             |               |                |
| 5.1 Intake tower                                 |          |     |            |            |             |               |                |
| Excavation                                       | Common   | m3  | 3,758      | 276        | 1,651       | 1,037,208     | 6,204,438      |
|  | Wearrock | m3  | 4,176      | 339        | 1,398       | 1,415,664     | 5,838,048      |
|  | Rock     | m3  | 418        | 962        | 3,475       | 402,116       | 1,452,530      |
| Concrete   |          | m3  | 500        | 13,442     | 132,187     | 6,721,000     | 66,093,500     |
| Rein bar   |          | t   | 20         | 5,292      | 1,460,955   | 105,840       | 29,219,100     |
| (Sub-total)                                      |          |     |            |            |             | 9,681,828     | 108,807,656    |
| 5.2 Intake shaft                                 |          |     |            |            |             |               |                |
| Excavation                                       |          | m3  | 299        | 8,744      | 102,122     | 2,614,456     | 30,534,478     |
| Concrete   |          | m3  | 171        | 13,488     | 155,546     | 2,306,448     | 26,598,366     |
| Rein bar   |          | t   | 6          | 5,292      | 1,460,955   | 31,752        | 8,765,730      |
| (Sub-total)                                      |          |     |            |            |             | 4,952,656     | 65,898,574     |
| <b>SUB-TOTAL OF 5.</b>                           |          |     |            |            |             | 14,634,484    | 174,706,230    |
| <b>6. METAL WORK</b>                             |          |     |            |            |             |               |                |
| 6.1 Diversion gate                               |          | Ls  | 1          | 33,040,000 |             | 33,040,000    |                |
| 6.2 Steel coeshik                                |          | Ls  | 1          |            | 808,500,000 |               | 808,500,000    |
| 6.3 Hollow jet valve                             |          | Ls  | 1          | 45,000,000 |             | 45,000,000    |                |
| 6.4 Guard valve                                  |          | Ls  | 1          | 22,500,000 |             | 22,500,000    |                |
| <b>SUB-TOTAL OF 6.</b>                           |          |     |            |            |             | 100,540,000   | 808,500,000    |
| <b>7. WATER SUPPLY PIPELINE</b>                  |          |     |            |            |             |               |                |
| 7.1 Excavation                                   |          | m3  |            | 276        | 1,651       |               |                |
| 7.2 Backfill                                     |          | m3  |            | 244        | 1,717       |               |                |
| 7.3 Add pump station                             |          | Ls  |            |            |             |               |                |
| 7.4 Add purification plant                       |          | Ls  |            |            |             |               |                |
| 7.5 Add pipe line                                |          | Ls  | 1          |            | 501,000,000 |               | 501,000,000    |
| 7.6 Add intake & surge tank                      |          | Ls  |            |            |             |               |                |
| <b>SUB-TOTAL OF 7.</b>                           |          |     |            |            |             |               | 501,000,000    |
| <b>TOTAL OF DIRECT CONSTRUCTION COST</b>         |          |     |            |            |             | 2,251,061,562 | 17,368,619,875 |

Table F-12 Cost Estimate for Heightening of Krenceng Dam without Diversion Tunnel: Scheme B-2

| DESCRIPTION                         | Unit     | Qty | UNIT PRICE  |               | AMOUNT         |               |                |
|-------------------------------------|----------|-----|-------------|---------------|----------------|---------------|----------------|
|                                     |          |     | Fe<br>(Yen) | Le<br>(Rp)    | Fe<br>(Yen)    | Le<br>(Rp)    |                |
| 1. PREPARATORY WORK<br>(20% of 2+3) |          |     |             |               | 257,537,340    | 1,466,768,687 |                |
| 2. DIVERTED TUNNEL                  |          |     |             |               |                |               |                |
| 2.1 Coffering work                  |          |     |             |               |                |               |                |
| Coffering                           | Exca.    | m3  |             | 276           | 1,651          |               |                |
|                                     | Embank   | m3  |             | 441           | 1,144          |               |                |
| (Sub-total)                         |          |     |             |               |                |               |                |
| 2.2 Weir                            |          |     |             |               |                |               |                |
| Excavation                          | Common   | m3  |             | 276           | 1,651          |               |                |
|                                     | Wea.rock | m3  |             | 339           | 1,398          |               |                |
|                                     | Rock     | m3  |             | 962           | 3,475          |               |                |
| Concrete                            |          | m3  |             | 5,052         | 118,708        |               |                |
| Rein bar                            |          | t   |             | 5,292         | 1,460,955      |               |                |
| Gate                                |          | Ls  |             | 2,000,000     |                |               |                |
| (Sub-total)                         |          |     |             |               |                |               |                |
| 2.3 Inlet & outlet                  |          |     |             |               |                |               |                |
| Excavation                          | Common   | m3  |             | 276           | 1,651          |               |                |
|                                     | Wea.rock | m3  |             | 339           | 1,398          |               |                |
|                                     | Rock     | m3  |             | 962           | 3,475          |               |                |
| Concrete                            |          | m3  |             | 13,442        | 132,187        |               |                |
| Rein bar                            |          | t   |             | 5,292         | 1,460,955      |               |                |
| Trash rack                          |          | Ls  |             | 1,000,000     |                |               |                |
| (Sub-total)                         |          |     |             |               |                |               |                |
| 2.4 Diverted tunnel                 |          |     |             |               |                |               |                |
| Excavation                          |          | m3  |             | 8,744         | 105,122        |               |                |
| Lining conc.                        |          | m3  |             | 13,488        | 155,546        |               |                |
| Plug conc.                          |          | m3  |             | 13,488        | 155,546        |               |                |
| Grouting                            |          | t   |             | 6,500         | 90,000         |               |                |
| Rein bar                            |          | t   |             | 5,292         | 1,460,955      |               |                |
| (Sub-total)                         |          |     |             |               |                |               |                |
| SUB-TOTAL OF 2.                     |          |     |             |               |                |               |                |
| 3. HED HEIGHTENING OF KRENCENG DAM  |          |     |             |               |                |               |                |
| 3.1 Main dam                        |          |     |             |               |                |               |                |
| Excavation                          | Common   | m3  | 146,652     | 276           | 1,651          | 40,475,952    | 242,122,452    |
|                                     | Wea.rock | m3  | 97,768      | 339           | 1,398          | 33,143,352    | 136,679,664    |
|                                     | Rock     | m3  |             | 962           | 3,475          |               |                |
| Embankment                          | Core     | m3  | 1,281,085   | 605           | 2,359          | 775,056,425   | 3,022,079,515  |
|                                     | Filter   | m3  |             | 2,285         | 5,756          |               |                |
|                                     | Random   | m3  |             | 441           | 1,144          |               |                |
|                                     | Rock     | m3  |             | 1,514         | 5,964          |               |                |
| Grouting                            | Blanket  | t   | 1,868       | 6,500         | 90,000         | 12,142,000    | 168,120,000    |
|                                     | Curtain  | t   | 3,676       | 6,500         | 90,000         | 23,894,000    | 330,840,000    |
| (Sub-total)                         |          |     |             |               |                | 884,711,729   | 3,899,841,631  |
| 3.2 Spillway                        |          |     |             |               |                |               |                |
| (1) Approach wall & weir            |          |     |             |               |                |               |                |
| Excavation                          | Common   | m3  | 3,097       | 276           | 1,651          | 854,772       | 5,113,147      |
|                                     | Wea.rock | m3  | 4,645       | 339           | 1,398          | 1,574,655     | 6,493,710      |
|                                     | Rock     | m3  |             | 962           | 3,475          |               |                |
| Concrete                            |          | m3  | 6,628       | 13,442        | 132,187        | 89,093,576    | 876,135,436    |
| Rein bar                            |          | t   | 135         | 5,292         | 1,460,955      | 714,420       | 197,228,925    |
| (2) Chute way & basin               |          |     |             |               |                |               |                |
| Excavation                          | Common   | m3  | 11,879      | 276           | 1,651          | 3,278,604     | 19,612,229     |
|                                     | Wea.rock | m3  | 17,818      | 339           | 1,398          | 6,040,302     | 24,909,564     |
|                                     | Rock     | m3  |             | 962           | 3,475          |               |                |
| Concrete                            |          | m3  | 14,260      | 13,442        | 132,187        | 191,682,920   | 1,884,986,620  |
| Rein bar                            |          | t   | 285         | 5,292         | 1,460,955      | 1,508,220     | 416,372,175    |
| Grouting                            | Consoli. | t   | 35          | 6,500         | 90,000         | 227,500       | 3,150,000      |
| (3) Metal work                      |          |     |             |               |                |               |                |
| Spillway gate                       |          | Ls  | 1           | 108,000,000   |                | 108,000,000   |                |
| (Sub-total)                         |          |     |             |               |                | 402,974,969   | 3,434,001,806  |
| SUB-TOTAL OF 3.                     |          |     |             |               |                | 1,287,686,698 | 7,333,843,437  |
| 4. WATER SUPPLY PIPE LINE           |          |     |             |               |                |               |                |
| 4.1 Excavation                      |          | m3  |             | 276           | 1,651          |               |                |
| 4.2 Backfill                        |          | m3  |             | 244           | 1,717          |               |                |
| 4.3 Add. pump station               |          | Ls  | 1           | 1,146,000,000 | 7,665,000,000  | 1,146,000,000 | 7,665,000,000  |
| 4.4 Add. purification plant         |          | Ls  | 1           | 1,749,000,000 | 11,699,000,000 | 1,749,000,000 | 11,699,000,000 |
| 4.5 Add. pipe line                  |          | Ls  |             |               | 1,540,000,000  |               |                |
| 4.6 Add. intake & surge tank        |          | Ls  | 1           | 77,000,000    | 2,824,000,000  | 77,000,000    | 2,824,000,000  |
| 4.7 Receiving well                  |          | Ls  | 1           | 6,000,000     | 218,400,000    | 6,000,000     | 218,400,000    |
| SUB-TOTAL OF 4.                     |          |     |             |               |                | 2,978,000,000 | 22,406,400,000 |
| TOTAL OF DIRECT CONSTRUCTION COST   |          |     |             |               |                | 4,523,224,038 | 31,207,012,124 |

Table F-13 Cost Estimate for Cidanau Gated Weir: Scheme B-3

| DESCRIPTION                                | Unit     | Qty | UNIT PRICE    |             | AMOUNT      |               |                |
|--|----------|-----|---------------|-------------|-------------|---------------|----------------|
|  |          |     | Fc<br>(Yen)   | Le<br>(Rp)  | Fc<br>(Yen) | Le<br>(Rp)    |                |
| 1. PREPARATORY WORK<br>(20% of 2+3+4+5)    |          |     |               |             | 414,455,432 | 1,755,702,092 |                |
| 2. DIVERSION WORK                          |          |     |               |             |             |               |                |
| 2.1 Coffering work<br>Sheet pile & bracing | t        | 159 | 131,583       | 36,915      | 20,921,697  | 5,869,485     |                |
| SUB-TOTAL OF 2.                            |          |     |               |             | 20,921,697  | 5,869,485     |                |
| 3. DAM                                     |          |     |               |             |             |               |                |
| 3.1 Main dam                               |          |     |               |             |             |               |                |
| Excavation                                 | Common   | m3  | 10,662        | 276         | 1,651       | 2,942,712     | 17,602,962     |
|  | Wea.rock | m3  | 8,462         | 339         | 1,398       | 2,868,618     | 11,829,876     |
|  | Rock     | m3  | 2,200         | 962         | 3,475       | 2,116,400     | 7,645,000      |
| Concrete                                   |          | m3  | 21,325        | 5,052       | 118,708     | 107,733,900   | 2,531,448,100  |
| Grouting                                   | Consoli. | t   | 219           | 6,500       | 90,000      | 1,423,500     | 19,710,000     |
|  | Curtain  | t   | 352           | 6,500       | 90,000      | 2,288,000     | 31,680,000     |
| SUB-TOTAL OF 3.                            |          |     |               |             | 119,373,130 | 2,619,915,938 |                |
| 4. SPILLWAY                                |          |     |               |             |             |               |                |
| 4.1 Dental work                            |          |     |               |             |             |               |                |
| Excavation                                 | Common   | m3  | 22,389        | 276         | 1,651       | 6,179,364     | 36,964,239     |
|  | Wea.rock | m3  |               | 339         | 1,398       |               |                |
|  | Rock     | m3  |               | 962         | 3,475       |               |                |
| Concrete                                   |          | m3  | 8,379         | 5,052       | 118,708     | 42,330,708    | 994,654,332    |
| (Sub-total)                                |          |     |               |             |             | 48,510,072    | 1,031,618,571  |
| 4.2 Weir & pier                            |          |     |               |             |             |               |                |
| Excavation                                 | Common   | m3  |               | 276         | 1,651       |               |                |
|  | Wea.rock | m3  | 1,170         | 339         | 1,398       | 396,630       | 1,635,660      |
|  | Rock     | m3  | 500           | 962         | 3,475       | 481,000       | 1,737,500      |
| Concrete                                   |          | m3  | 10,761        | 13,442      | 132,187     | 144,649,362   | 1,422,464,307  |
| Rein bar                                   |          | t   | 1,290         | 5,292       | 1,460,955   | 6,826,680     | 1,884,631,950  |
| Grouting                                   | Consoli. | t   | 126           | 6,500       | 90,000      | 819,000       | 11,340,000     |
|  | Curtain  | t   | 180           | 6,500       | 90,000      | 1,170,000     | 16,200,000     |
| (Sub-total)                                |          |     |               |             |             | 154,342,672   | 3,338,009,417  |
| 4.3 Hoist & bridge                         |          |     |               |             |             |               |                |
| Concrete                                   |          | m3  | 2,871         | 13,442      | 132,187     | 38,591,982    | 379,508,877    |
| Rein bar                                   |          | t   | 574           | 5,292       | 1,460,955   | 3,037,608     | 838,588,170    |
| (Sub-total)                                |          |     |               |             |             | 41,629,590    | 1,218,097,047  |
| SUB-TOTAL OF 4.                            |          |     |               |             |             | 244,482,334   | 5,587,725,035  |
| 5. METAL WORK                              |          |     |               |             |             |               |                |
| 5.1 Roller gate                            | Ls       | 1   | 1,620,000,000 |             |             | 1,620,000,000 |                |
| 5.2 Steel conduit                          | Ls       | 1   |               | 565,000,000 |             |               | 565,000,000    |
| 5.3 Hollow jet valve                       | Ls       | 1   | 45,000,000    |             |             | 45,000,000    |                |
| 5.4 Guard valve                            | Ls       | 1   | 22,500,000    |             |             | 22,500,000    |                |
| SUB-TOTAL OF 5.                            |          |     |               |             |             | 1,687,500,000 | 565,000,000    |
| 6. WATER SUPPLY PIPE LINE                  |          |     |               |             |             |               |                |
| 6.1 Excavation                             |          | m3  |               | 276         | 1,651       |               |                |
| 6.2 Backfill                               |          | m3  |               | 244         | 1,717       |               |                |
| 6.3 Add. pump station                      |          | Ls  |               |             |             |               |                |
| 6.4 Add. purification plant                |          | Ls  |               |             |             |               |                |
| 6.5 Add. pipe line                         |          | Ls  |               |             |             |               |                |
| 6.6 Add. intake & surge tank               |          | Ls  |               |             |             |               |                |
| SUB-TOTAL OF 6.                            |          |     |               |             |             |               |                |
| TOTAL OF DIRECT CONSTRUCTION COST          |          |     |               |             |             | 2,486,732,593 | 10,534,212,550 |

Table F-14 Cost Estimate for Heightening of Krenceng Dam without Diversion Tunnel: Scheme B-3

| DESCRIPTION                         | Unit     | Qty | UNIT PRICE  |               | AMOUNT         |               |                |
|-------------------------------------|----------|-----|-------------|---------------|----------------|---------------|----------------|
|                                     |          |     | Fc<br>(Yen) | Lc<br>(Rp)    | Fc<br>(Yen)    | Lc<br>(Rp)    |                |
| 1. PREPARATORY WORK<br>(20% of 2+3) |          |     |             |               |                | 257,537,340   | 1,466,768,687  |
| 2. DIVERTED TUNNEL                  |          |     |             |               |                |               |                |
| 2.1 Coffering work                  |          |     |             |               |                |               |                |
| Coffering                           | Exca.    | m3  |             | 276           | 1,651          |               |                |
|                                     | Embank   | m3  |             | 441           | 1,144          |               |                |
| (Sub-total)                         |          |     |             |               |                |               |                |
| 2.2 Weir                            |          |     |             |               |                |               |                |
| Excavation                          | Common   | m3  |             | 276           | 1,651          |               |                |
|                                     | Wea.rock | m3  |             | 339           | 1,398          |               |                |
|                                     | Rock     | m3  |             | 962           | 3,475          |               |                |
| Concrete                            |          | m3  |             | 5,052         | 118,708        |               |                |
| Rein bar                            |          | t   |             | 5,292         | 1,460,955      |               |                |
| Gate                                |          | Ls  |             | 2,000,000     |                |               |                |
| (Sub-total)                         |          |     |             |               |                |               |                |
| 2.3 Inlet & outlet                  |          |     |             |               |                |               |                |
| Excavation                          | Common   | m3  |             | 276           | 1,651          |               |                |
|                                     | Wea.rock | m3  |             | 339           | 1,398          |               |                |
|                                     | Rock     | m3  |             | 962           | 3,475          |               |                |
| Concrete                            |          | m3  |             | 13,442        | 132,187        |               |                |
| Rein bar                            |          | t   |             | 5,292         | 1,460,955      |               |                |
| Trash rack                          |          | Ls  |             | 1,000,000     |                |               |                |
| (Sub-total)                         |          |     |             |               |                |               |                |
| 2.4 Diverted tunnel                 |          |     |             |               |                |               |                |
| Excavation                          |          | m3  |             | 8,744         | 105,122        |               |                |
| Lining conc.                        |          | m3  |             | 13,488        | 155,546        |               |                |
| Plug conc.                          |          | m3  |             | 13,488        | 155,546        |               |                |
| Grouting                            |          | t   |             | 6,500         | 90,000         |               |                |
| Rein bar                            |          | t   |             | 5,292         | 1,460,955      |               |                |
| (Sub-total)                         |          |     |             |               |                |               |                |
| SUB-TOTAL OF 2.                     |          |     |             |               |                |               |                |
| 3. HEIGHTENING OF KRENCENG DAM      |          |     |             |               |                |               |                |
| 3.1 Main dam                        |          |     |             |               |                |               |                |
| Excavation                          | Common   | m3  | 146,652     | 276           | 1,651          | 40,475,952    | 242,122,452    |
|                                     | Wea.rock | m3  | 97,768      | 339           | 1,398          | 33,143,352    | 136,679,664    |
|                                     | Rock     | m3  |             | 962           | 3,475          |               |                |
| Embankment                          | Core     | m3  | 1,281,085   | 605           | 2,359          | 775,056,425   | 3,022,079,515  |
|                                     | Filter   | m3  |             | 2,285         | 5,756          |               |                |
|                                     | Random   | m3  |             | 441           | 1,144          |               |                |
|                                     | Rock     | m3  |             | 1,514         | 5,964          |               |                |
| Grouting                            | Blanket  | t   | 1,868       | 6,500         | 90,000         | 12,142,000    | 168,120,000    |
|                                     | Curtain  | t   | 3,676       | 6,500         | 90,000         | 23,894,000    | 330,840,000    |
| (Sub-total)                         |          |     |             |               |                |               |                |
|                                     |          |     |             |               |                | 884,711,729   | 3,899,841,631  |
| 3.2 Spillway                        |          |     |             |               |                |               |                |
| (1) Approach wall & weir            |          |     |             |               |                |               |                |
| Excavation                          | Common   | m3  | 3,097       | 276           | 1,651          | 854,772       | 5,113,147      |
|                                     | Wea.rock | m3  | 4,645       | 339           | 1,398          | 1,574,655     | 6,493,710      |
|                                     | Rock     | m3  |             | 962           | 3,475          |               |                |
| Concrete                            |          | m3  | 6,628       | 13,442        | 132,187        | 89,093,576    | 876,135,436    |
| Rein bar                            |          | t   | 135         | 5,292         | 1,460,955      | 714,420       | 197,228,925    |
| (2) Chuteway & basin                |          |     |             |               |                |               |                |
| Excavation                          | Common   | m3  | 11,879      | 276           | 1,651          | 3,278,604     | 19,612,229     |
|                                     | Wea.rock | m3  | 17,818      | 339           | 1,398          | 6,040,302     | 24,909,564     |
|                                     | Rock     | m3  |             | 962           | 3,475          |               |                |
| Concrete                            |          | m3  | 14,260      | 13,442        | 132,187        | 191,682,920   | 1,884,986,620  |
| Rein bar                            |          | t   | 285         | 5,292         | 1,460,955      | 1,508,220     | 416,372,175    |
| Grouting                            | Consoli. | t   | 35          | 6,500         | 90,000         | 227,500       | 3,150,000      |
| (3) Metal work                      |          |     |             |               |                |               |                |
| Spillway gate                       |          | Ls  | 1           | 108,000,000   |                | 108,000,000   |                |
| (Sub-total)                         |          |     |             |               |                |               |                |
|                                     |          |     |             |               |                | 402,974,969   | 3,434,001,806  |
| SUB-TOTAL OF 3.                     |          |     |             |               |                |               |                |
|                                     |          |     |             |               |                | 1,287,686,698 | 7,333,843,437  |
| 4. WATER SUPPLY PIPE LINE           |          |     |             |               |                |               |                |
| 4.1 Excavation                      |          | m3  |             | 276           | 1,651          |               |                |
| 4.2 Backfill                        |          | m3  |             | 244           | 1,717          |               |                |
| 4.3 Add. pump station               |          | Ls  | 1           | 1,167,000,000 | 7,808,000,000  | 1,167,000,000 | 7,808,000,000  |
| 4.4 Add. purification plant         |          | Ls  | 1           | 1,812,000,000 | 12,118,000,000 | 1,812,000,000 | 12,118,000,000 |
| 4.5 Add. pipe line                  |          | Ls  |             |               | 1,540,000,000  |               |                |
| 4.6 Add. intake & surge tank        |          | Ls  | 1           | 80,000,000    | 2,914,000,000  | 80,000,000    | 2,914,000,000  |
| 4.7 Receiving well                  |          | Ls  | 1           | 6,000,000     | 218,400,000    | 6,000,000     | 218,400,000    |
| SUB-TOTAL OF 4.                     |          |     |             |               |                |               |                |
|                                     |          |     |             |               |                | 3,065,000,000 | 23,058,400,000 |
| TOTAL OF DIRECT CONSTRUCTION COST   |          |     |             |               |                | 4,610,224,038 | 31,859,012,124 |

Table F-15 Cost Estimate for Cidanau Dam: Scheme C-1

| DESCRIPTION                                      | Unit      | Qty | UNIT PRICE |            | AMOUNT         |               |                |
|--|-----------|-----|------------|------------|----------------|---------------|----------------|
|  |           |     | Fc (Yen)   | Le (Rp)    | Fc (Yen)       | Le (Rp)       |                |
| <b>1. PREPARATORY WORK</b><br>(20% of 2+3+4+5+6) |           |     |            |            | 464,133,519    | 2,947,352,634 |                |
| <b>2. DIVERSION WORK</b>                         |           |     |            |            |                |               |                |
| 2.1 Inlet & outlet                               |           |     |            |            |                |               |                |
| Excavation                                       | Common    | m3  | 1,053      | 276        | 1,651          | 290,628       | 1,738,593      |
|  | Wear/rock | m3  | 2,106      | 339        | 1,398          | 713,934       | 2,944,148      |
|  | Rock      | m3  | 7,371      | 962        | 3,475          | 7,090,902     | 25,614,225     |
| Concrete   |           | m3  | 2,640      | 13,442     | 132,187        | 35,486,880    | 348,973,680    |
| Rein bar   |           | t   | 100        | 5,292      | 1,460,955      | 529,200       | 146,095,500    |
| (Sub-total)                                      |           |     |            |            |                | 44,111,544    | 525,366,096    |
| 2.2 Turnout (=11(m), D=5(m))                     |           |     |            |            |                |               |                |
| Excavation                                       |           | m3  | 10,462     | 8,744      | 105,122        | 91,479,728    | 1,099,716,364  |
| Lining conc.                                     |           | m3  | 2,804      | 13,418     | 155,546        | 32,425,152    | 373,932,584    |
| Flag conc.                                       |           | m3  | 686        | 13,488     | 155,546        | 9,252,768     | 106,704,556    |
| GROUTING   |           | t   | 246        | 6,500      | 90,000         | 1,599,000     | 22,140,000     |
| Rein bar   |           | t   | 123        | 5,292      | 1,460,955      | 650,916       | 179,697,465    |
| (Sub-total)                                      |           |     |            |            |                | 135,407,564   | 1,742,260,969  |
| SUB-TOTAL OF 2.                                  |           |     |            |            |                | 179,519,108   | 2,307,627,065  |
| <b>3. DAM</b>                                    |           |     |            |            |                |               |                |
| 3.1 Cofferdam                                    |           |     |            |            |                |               |                |
| Excavation                                       |           | m3  | 2,500      | 276        | 1,651          | 690,000       | 4,127,500      |
| Embankment                                       |           | m3  | 200,000    | 1,514      | 5,964          | 302,800,000   | 1,192,800,000  |
| (Sub-total)                                      |           |     |            |            |                | 303,490,000   | 1,196,927,500  |
| 3.2 Main dam                                     |           |     |            |            |                |               |                |
| Excavation                                       | Common    | m3  | 11,075     | 276        | 1,651          | 3,056,700     | 18,244,825     |
|  | Wear/rock | m3  | 22,150     | 339        | 1,398          | 7,508,850     | 30,965,700     |
|  | Rock      | m3  | 77,520     | 962        | 3,475          | 74,574,240    | 269,282,000    |
| Embankment                                       | Core      | m3  | 101,416    | 605        | 2,359          | 61,356,580    | 239,240,344    |
|  | Filter    | m3  | 62,644     | 2,285      | 5,756          | 143,141,540   | 360,478,664    |
|  | Random    | m3  | 174,500    | 441        | 1,144          | 77,130,500    | 200,085,600    |
|  | Rock      | m3  | 408,105    | 1,514      | 5,964          | 617,870,970   | 2,433,938,220  |
| GROUTING   | Blanket   | t   | 474        | 6,500      | 90,000         | 3,081,000     | 42,660,000     |
|  | Control   | t   | 114        | 6,500      | 90,000         | 741,000       | 10,260,000     |
|  | Curtain   | t   | 1,287      | 6,500      | 90,000         | 8,365,500     | 115,630,000    |
| (Sub-total)                                      |           |     |            |            |                | 996,627,380   | 3,721,225,553  |
| 3.3 Saddle dam                                   |           |     |            |            |                |               |                |
| Excavation                                       | Common    | m3  | 3,595      | 276        | 2,176          | 992,220       | 7,822,720      |
|  | Wear/rock | m3  | 7,190      | 339        | 1,398          | 2,437,410     | 18,246,150     |
|  | Rock      | m3  | 25,160     | 962        | 3,475          | 24,203,920    | 111,534,280    |
| Embankment                                       |           | m3  | 167,975    | 244        | 1,717          | 40,985,900    | 288,413,075    |
| GROUTING   |           | t   | 597        | 13,442     | 132,187        | 8,024,874     | 78,915,639     |
| (Sub-total)                                      |           |     |            |            |                | 76,644,324    | 505,271,864    |
| SUB-TOTAL OF 3.                                  |           |     |            |            |                | 1,376,961,704 | 5,423,424,917  |
| <b>4. SPILLWAY</b>                               |           |     |            |            |                |               |                |
| 4.1 Side channel                                 |           |     |            |            |                |               |                |
| Excavation                                       | Common    | m3  | 8,100      | 276        | 1,651          | 2,235,600     | 13,373,100     |
|  | Wear/rock | m3  | 16,200     | 339        | 1,398          | 5,491,800     | 22,647,600     |
|  | Rock      | m3  | 56,700     | 962        | 3,475          | 54,545,400    | 197,632,500    |
| Concrete   |           | m3  | 21,170     | 13,442     | 132,187        | 284,567,140   | 2,794,398,790  |
| Rein bar   |           | t   | 400        | 5,292      | 1,460,955      | 2,116,800     | 584,382,000    |
| (Sub-total)                                      |           |     |            |            |                | 348,956,740   | 3,615,833,990  |
| 4.2 Chute way                                    |           |     |            |            |                |               |                |
| Excavation                                       | Common    | m3  | 14,245     | 276        | 1,651          | 3,931,620     | 23,514,495     |
|  | Wear/rock | m3  | 28,490     | 339        | 1,398          | 9,658,110     | 39,829,620     |
|  | Rock      | m3  | 99,715     | 962        | 3,475          | 95,925,830    | 346,509,625    |
| Concrete   |           | m3  | 11,395     | 13,442     | 132,187        | 153,171,590   | 1,506,270,885  |
| Rein bar   |           | t   | 220        | 5,292      | 1,460,955      | 1,164,240     | 319,210,100    |
| (Sub-total)                                      |           |     |            |            |                | 263,851,390   | 2,235,338,105  |
| 4.3 Plunge pool                                  |           |     |            |            |                |               |                |
| Excavation                                       | Common    | m3  | 4,032      | 276        | 1,651          | 1,112,832     | 6,656,832      |
|  | Wear/rock | m3  | 8,064      | 339        | 1,398          | 2,733,696     | 11,273,672     |
|  | Rock      | m3  | 28,224     | 962        | 3,475          | 27,131,488    | 98,078,400     |
| (Sub-total)                                      |           |     |            |            |                | 30,978,016    | 116,008,704    |
| SUB-TOTAL OF 4.                                  |           |     |            |            |                | 643,806,146   | 5,967,110,799  |
| <b>5. OUTLET WORK</b>                            |           |     |            |            |                |               |                |
| 5.1 Intake tower                                 |           |     |            |            |                |               |                |
| Excavation                                       | Common    | m3  | 515        | 276        | 1,651          | 142,140       | 850,265        |
|  | Wear/rock | m3  | 1,030      | 339        | 1,398          | 349,170       | 1,439,940      |
|  | Rock      | m3  | 3,606      | 962        | 3,475          | 3,468,972     | 12,530,850     |
| Concrete   |           | m3  | 760        | 13,442     | 132,187        | 10,215,520    | 100,462,120    |
| Rein bar   |           | t   | 29         | 5,292      | 1,460,955      | 153,468       | 42,361,695     |
| (Sub-total)                                      |           |     |            |            |                | 14,329,670    | 157,650,870    |
| 5.2 Intake shaft                                 |           |     |            |            |                |               |                |
| Excavation                                       |           | m3  | 332        | 8,744      | 102,122        | 2,903,008     | 33,904,504     |
| Concrete   |           | m3  | 191        | 13,488     | 155,546        | 2,576,208     | 29,769,288     |
| Rein bar   |           | t   | 6          | 5,292      | 1,460,955      | 31,752        | 8,765,730      |
| (Sub-total)                                      |           |     |            |            |                | 5,510,968     | 72,379,520     |
| SUB-TOTAL OF 5.                                  |           |     |            |            |                | 19,840,638    | 230,030,390    |
| <b>6. METAL WORK</b>                             |           |     |            |            |                |               |                |
| 6.1 Diversion gate                               |           | Lr  | 1          | 33,040,000 |                | 33,040,000    |                |
| 6.2 Steel conduit                                |           | Lr  | 1          |            | 808,500,000    |               | 808,500,000    |
| 6.3 Hollow jet valve                             |           | Lr  | 1          | 45,000,000 |                | 45,000,000    |                |
| 6.4 Guard valve                                  |           | Lr  | 1          | 22,500,000 |                | 22,500,000    |                |
| SUB-TOTAL OF 6.                                  |           |     |            |            |                | 100,540,000   | 808,500,000    |
| <b>7. WATER SUPPLY PIPELINE</b>                  |           |     |            |            |                |               |                |
| 7.1 Excavation                                   |           | m3  | 134,400    | 276        | 1,651          | 37,094,400    | 221,894,400    |
| 7.2 Backfill                                     |           | m3  | 123,200    | 244        | 1,717          | 30,060,800    | 211,534,400    |
| 7.3 Add. pump station                            |           | Lr  |            |            |                |               |                |
| 7.4 Add. purification plant                      |           | Lr  |            |            |                |               |                |
| 7.5 Add. pipe line                               |           | Lr  | 1          |            | 39,200,000,000 |               | 39,200,000,000 |
| 7.6 Add. intake & surge tank                     |           | Lr  |            |            |                |               |                |
| SUB-TOTAL OF 7.                                  |           |     |            |            |                | 67,155,200    | 39,633,428,800 |
| TOTAL OF DIRECT CONSTRUCTION COST                |           |     |            |            |                | 2,651,956,315 | 57,317,544,605 |

Table F-16 Cost Estimate for Heightening of Krenceng Dam with One Diversion Tunnel: Scheme C-1

| DESCRIPTION                         | Unit     | Qty | UNIT PRICE  |               | AMOUNT        |               |                |
|-------------------------------------|----------|-----|-------------|---------------|---------------|---------------|----------------|
|                                     |          |     | Fe<br>(Yen) | Le<br>(Rp)    | Fe<br>(Yen)   | Le<br>(Rp)    |                |
| 1. PREPARATORY WORK<br>(20% of 2+3) |          |     |             |               |               | 264,175,476   | 1,556,022,425  |
| 2. DIVERTED TUNNEL                  |          |     |             |               |               |               |                |
| 2.1 Coffering work                  |          |     |             |               |               |               |                |
| Coffering                           | Exca.    | m3  | 500         | 276           | 1,651         | 138,000       | 825,500        |
|                                     | Embank   | m3  | 500         | 441           | 1,144         | 220,500       | 572,000        |
| (Sub-total)                         |          |     |             |               |               | 358,500       | 1,397,500      |
| 2.2 Weir                            |          |     |             |               |               |               |                |
| Excavation                          | Common   | m3  | 400         | 276           | 1,651         | 110,400       | 660,400        |
|                                     | Wea.rock | m3  | 400         | 339           | 1,398         | 135,600       | 559,200        |
|                                     | Rock     | m3  | 200         | 962           | 3,475         | 192,400       | 695,000        |
| Concrete                            |          | m3  | 150         | 5,052         | 118,708       | 757,800       | 17,806,200     |
| Rein bar                            |          | t   | 15          | 5,292         | 1,460,955     | 79,380        | 21,914,325     |
| Gate                                |          | Ls  | 1           | 2,000,000     |               | 2,000,000     |                |
| (Sub-total)                         |          |     |             |               |               | 3,275,580     | 41,635,125     |
| 2.3 Inlet & outlet                  |          |     |             |               |               |               |                |
| Excavation                          | Common   | m3  | 1,664       | 276           | 1,651         | 459,264       | 2,747,264      |
|                                     | Wea.rock | m3  | 1,664       | 339           | 1,398         | 564,096       | 2,326,272      |
|                                     | Rock     | m3  | 832         | 962           | 3,475         | 800,384       | 2,891,200      |
| Concrete                            |          | m3  | 100         | 13,442        | 132,187       | 1,344,200     | 13,218,700     |
| Rein bar                            |          | t   | 20          | 5,292         | 1,460,955     | 105,840       | 29,219,100     |
| Trash rack                          |          | Ls  | 1           | 1,000,000     |               | 1,000,000     |                |
| (Sub-total)                         |          |     |             |               |               | 4,273,784     | 50,402,536     |
| 2.4 Diverted tunnel                 |          |     |             |               |               |               |                |
| Excavation                          |          | m3  | 1,600       | 8,744         | 105,122       | 13,990,400    | 168,195,200    |
| Lining conc.                        |          | m3  | 650         | 13,488        | 155,546       | 8,767,200     | 101,104,900    |
| Plug conc.                          |          | m3  |             | 13,488        | 155,546       |               |                |
| Grouting                            |          | t   | 360         | 6,500         | 90,000        | 2,340,000     | 32,400,000     |
| Rein bar                            |          | t   | 35          | 5,292         | 1,460,955     | 185,220       | 51,133,425     |
| (Sub-total)                         |          |     |             |               |               | 25,282,820    | 352,833,525    |
| SUB-TOTAL OF 2.                     |          |     |             |               |               | 33,190,684    | 446,268,686    |
| 3. HEIGHTENING OF KRINCENG DAM      |          |     |             |               |               |               |                |
| 3.1 Main dam                        |          |     |             |               |               |               |                |
| Excavation                          | Common   | m3  | 146,652     | 276           | 1,651         | 40,475,952    | 242,122,452    |
|                                     | Wea.rock | m3  | 97,768      | 339           | 1,398         | 33,143,352    | 136,679,664    |
|                                     | Rock     | m3  |             | 962           | 3,475         |               |                |
| Embankment                          | Core     | m3  | 1,281,085   | 605           | 2,359         | 775,056,425   | 3,022,079,515  |
|                                     | Filter   | m3  |             | 2,285         | 5,756         |               |                |
|                                     | Random   | m3  |             | 441           | 1,144         |               |                |
|                                     | Rock     | m3  |             | 1,514         | 5,964         |               |                |
| Grouting                            | Blanket  | t   | 1,868       | 6,500         | 90,000        | 12,142,000    | 168,120,000    |
|                                     | Curtain  | t   | 3,676       | 6,500         | 90,000        | 23,894,000    | 330,840,000    |
| (Sub-total)                         |          |     |             |               |               | 884,711,729   | 3,899,841,631  |
| 3.2 Spillway                        |          |     |             |               |               |               |                |
| (1) Approach wall & weir            |          |     |             |               |               |               |                |
| Excavation                          | Common   | m3  | 3,097       | 276           | 1,651         | 854,772       | 5,113,147      |
|                                     | Wea.rock | m3  | 4,645       | 339           | 1,398         | 1,574,655     | 6,493,710      |
|                                     | Rock     | m3  |             | 962           | 3,475         |               |                |
| Concrete                            |          | m3  | 6,628       | 13,442        | 132,187       | 89,093,576    | 876,135,436    |
| Rein bar                            |          | t   | 135         | 5,292         | 1,460,955     | 714,420       | 197,228,925    |
| (2) Chuteway & basin                |          |     |             |               |               |               |                |
| Excavation                          | Common   | m3  | 11,879      | 276           | 1,651         | 3,278,604     | 19,612,229     |
|                                     | Wea.rock | m3  | 17,818      | 339           | 1,398         | 6,040,302     | 24,909,564     |
|                                     | Rock     | m3  |             | 962           | 3,475         |               |                |
| Concrete                            |          | m3  | 14,260      | 13,442        | 132,187       | 191,682,920   | 1,884,986,620  |
| Rein bar                            |          | t   | 285         | 5,292         | 1,460,955     | 1,508,220     | 416,372,175    |
| Grouting                            | Consoli. | t   | 35          | 6,500         | 90,000        | 227,500       | 3,150,000      |
| (3) Metal work                      |          |     |             |               |               |               |                |
| Spillway gate                       |          | Ls  | 1           | 108,000,000   |               | 108,000,000   |                |
| (Sub-total)                         |          |     |             |               |               | 402,974,969   | 3,434,001,806  |
| SUB-TOTAL OF 3.                     |          |     |             |               |               | 1,287,686,698 | 7,333,843,437  |
| 4. WATER SUPPLY PIPE LINE           |          |     |             |               |               |               |                |
| 4.1 Excavation                      |          | m3  |             | 276           | 1,651         |               |                |
| 4.2 Backfill                        |          | m3  |             | 244           | 1,717         |               |                |
| 4.3 Add. pump station               |          | Ls  | 1           | 1,166,000,000 | 7,800,000,000 | 1,166,000,000 | 7,800,000,000  |
| 4.4 Add. purification plant         |          | Ls  | 1           | 1,448,000,000 | 9,683,000,000 | 1,448,000,000 | 9,683,000,000  |
| 4.5 Add. pipe line                  |          | Ls  |             |               | 1,540,000,000 |               |                |
| 4.6 Add. intake & surge tank        |          | Ls  | 1           | 77,000,000    | 2,810,000,000 | 77,000,000    | 2,810,000,000  |
| 4.7 Receiving well                  |          | Ls  | 1           | 6,000,000     | 218,400,000   | 6,000,000     | 218,400,000    |
| SUB-TOTAL OF 4.                     |          |     |             |               |               | 2,697,000,000 | 20,511,400,000 |
| TOTAL OF DIRECT CONSTRUCTION COST   |          |     |             |               |               | 4,282,052,858 | 29,847,534,548 |

Table F-17 Cost Estimate for Downstream Cidanau Dam: Scheme C-2

| DESCRIPTION                             | Unit      | Qty | UNIT PRICE |            | AMOUNT      |               |                |
|---|-----------|-----|------------|------------|-------------|---------------|----------------|
|   |           |     | Fe (Yen)   | Le (Rp)    | Fe (Yen)    | Le (Rp)       |                |
| <b>1. PREPARATORY WORK</b>              |           |     |            |            |             |               |                |
| (20% of 2+3+4+5+6)                      |           |     |            |            |             |               |                |
|   |           |     |            |            | 375,176,927 | 2,810,769,979 |                |
| <b>2. DIVERSION WORKS</b>               |           |     |            |            |             |               |                |
| <b>2.1 Inlet &amp; outlet</b>           |           |     |            |            |             |               |                |
| Excavation                              | Common    | m3  | 997        | 276        | 1,651       | 275,172       | 1,646,017      |
|   | Wear,rock | m3  | 11,970     | 339        | 1,398       | 4,057,830     | 16,734,060     |
|   | Rock      | m3  | 6,982      | 962        | 3,475       | 6,716,684     | 24,262,450     |
| Concrete                                |           | m3  | 2,640      | 13,442     | 132,187     | 35,486,880    | 318,973,680    |
| Rein bar                                |           | t   | 100        | 5,292      | 1,460,955   | 529,200       | 146,095,500    |
| (Sub-total)                             |           |     |            |            |             | 47,065,766    | 537,711,737    |
| <b>2.2 Tunnel (D=400cm, D=5m)</b>       |           |     |            |            |             |               |                |
| Excavation                              |           | m3  | 10,710     | 4,744      | 105,122     | 93,618,240    | 1,125,856,620  |
| Lining conc.                            |           | m3  | 2,464      | 13,488     | 155,546     | 33,234,432    | 383,265,344    |
| Plug conc.                              |           | m3  | 646        | 13,488     | 155,546     | 9,252,768     | 106,704,556    |
| Grouting                                |           | t   | 501        | 6,500      | 90,000      | 3,276,000     | 45,360,000     |
| Rein bar                                |           | t   | 126        | 5,292      | 1,460,955   | 666,792       | 181,080,130    |
| (Sub-total)                             |           |     |            |            |             | 140,074,232   | 1,845,266,650  |
| SUB-TOTAL OF 2.                         |           |     |            |            |             | 187,143,998   | 2,382,978,587  |
| <b>3. DAM</b>                           |           |     |            |            |             |               |                |
| <b>3.1 Cofferdam</b>                    |           |     |            |            |             |               |                |
| Excavation                              |           | m3  | 2,500      | 276        | 1,651       | 690,000       | 4,177,500      |
| Embankment                              |           | m3  | 200,000    | 1,514      | 5,964       | 302,800,000   | 1,192,800,000  |
| (Sub-total)                             |           |     |            |            |             | 303,490,000   | 1,196,977,500  |
| <b>3.2 Main dam</b>                     |           |     |            |            |             |               |                |
| Excavation                              | Common    | m3  | 24,986     | 276        | 1,651       | 6,896,136     | 41,251,886     |
|   | Wear,rock | m3  | 54,136     | 339        | 1,398       | 18,352,104    | 75,682,128     |
|   | Rock      | m3  | 4,164      | 962        | 3,475       | 4,005,768     | 14,489,500     |
| Embankment                              | Core      | m3  | 49,100     | 605        | 2,359       | 29,705,500    | 115,825,500    |
|   | Filter    | m3  | 31,308     | 2,285      | 5,756       | 71,538,780    | 180,208,848    |
|   | Random    | m3  | 72,975     | 441        | 1,144       | 32,181,975    | 83,483,400     |
|   | Rock      | m3  | 170,275    | 1,514      | 5,964       | 257,796,350   | 1,015,520,100  |
| Grouting                                | Blanket   | t   | 36         | 6,500      | 90,000      | 364,000       | 5,040,000      |
|   | Coccolit  | t   | 182        | 6,500      | 90,000      | 1,183,000     | 16,340,000     |
|   | Curtain   | t   | 2,556      | 6,500      | 90,000      | 16,614,000    | 230,040,100    |
| (Sub-total)                             |           |     |            |            |             | 438,637,613   | 1,777,803,162  |
| <b>3.3 Sand trap basin</b>              |           |     |            |            |             |               |                |
| Excavation                              | Common    | m3  | 306,750    | 276        | 1,651       | 84,663,000    | 667,488,000    |
|   | Wear,rock | m3  |            | 339        | 1,398       | 2,585         |                |
|   | Rock      | m3  |            | 962        | 3,475       | 4,433         |                |
| Maintenance road (2km)                  |           | m3  | 55,000     | 244        | 1,717       | 13,420,000    | 94,435,000     |
| Concrete                                |           | m3  | 1,200      | 13,442     | 132,187     | 16,130,400    | 138,624,400    |
| (Sub-total)                             |           |     |            |            |             | 114,213,400   | 920,547,400    |
| SUB-TOTAL OF 3.                         |           |     |            |            |             | 856,341,013   | 3,895,378,062  |
| <b>4. SPILLWAY</b>                      |           |     |            |            |             |               |                |
| <b>4.1 Side channel</b>                 |           |     |            |            |             |               |                |
| Excavation                              | Common    | m3  | 103,740    | 276        | 1,651       | 28,632,240    | 171,274,740    |
|   | Wear,rock | m3  | 116,707    | 339        | 1,398       | 39,563,673    | 163,156,386    |
|   | Rock      | m3  | 38,502     | 962        | 3,475       | 37,423,724    | 135,184,450    |
| Concrete                                |           | m3  | 27,734     | 13,442     | 132,187     | 372,666,008   | 3,654,752,388  |
| Rein bar                                |           | t   | 320        | 5,292      | 1,460,955   | 2,751,840     | 759,696,600    |
| (Sub-total)                             |           |     |            |            |             | 481,037,485   | 4,894,064,564  |
| <b>4.2 Chute way</b>                    |           |     |            |            |             |               |                |
| Excavation                              | Common    | m3  | 53,093     | 276        | 1,651       | 14,653,668    | 87,656,513     |
|   | Wear,rock | m3  | 127,425    | 339        | 1,398       | 43,197,075    | 178,140,150    |
|   | Rock      | m3  | 31,856     | 962        | 3,475       | 30,645,472    | 110,699,600    |
| Concrete                                |           | m3  | 4,775      | 13,442     | 132,187     | 117,933,550   | 1,159,940,925  |
| Rein bar                                |           | t   | 175        | 5,292      | 1,460,955   | 926,100       | 253,917,125    |
| (Sub-total)                             |           |     |            |            |             | 207,375,865   | 1,790,354,343  |
| <b>4.3 Flange pool</b>                  |           |     |            |            |             |               |                |
| Excavation                              | Common    | m3  | 2,030      | 276        | 1,651       | 560,280       | 3,251,530      |
|   | Wear,rock | m3  | 14,210     | 339        | 1,398       | 4,817,190     | 19,865,580     |
|   | Rock      | m3  | 24,360     | 962        | 3,475       | 23,434,320    | 84,651,000     |
| (Sub-total)                             |           |     |            |            |             | 28,811,790    | 107,868,110    |
| SUB-TOTAL OF 4.                         |           |     |            |            |             | 717,225,140   | 6,792,287,017  |
| <b>5. OUTLET WORK</b>                   |           |     |            |            |             |               |                |
| <b>5.1 Intake lower</b>                 |           |     |            |            |             |               |                |
| Excavation                              | Common    | m3  | 3,758      | 276        | 1,651       | 1,037,208     | 6,204,458      |
|   | Wear,rock | m3  | 4,176      | 339        | 1,398       | 1,415,654     | 5,838,018      |
|   | Rock      | m3  | 418        | 962        | 3,475       | 402,116       | 1,457,530      |
| Concrete                                |           | m3  | 500        | 13,442     | 132,187     | 6,721,000     | 65,093,500     |
| Rein bar                                |           | t   | 20         | 5,292      | 1,460,955   | 105,840       | 29,219,100     |
| (Sub-total)                             |           |     |            |            |             | 9,681,828     | 108,807,656    |
| <b>5.2 Intake shaft</b>                 |           |     |            |            |             |               |                |
| Excavation                              |           | m3  | 259        | 4,744      | 102,122     | 2,614,456     | 30,534,478     |
| Concrete                                |           | m3  | 171        | 13,488     | 155,546     | 2,306,448     | 26,598,366     |
| Rein bar                                |           | t   | 6          | 5,292      | 1,460,955   | 31,752        | 8,765,730      |
| (Sub-total)                             |           |     |            |            |             | 4,952,656     | 65,898,574     |
| SUB-TOTAL OF 5.                         |           |     |            |            |             | 14,634,484    | 174,706,230    |
| <b>6. METAL WORK</b>                    |           |     |            |            |             |               |                |
| <b>6.1 Diversion gate</b>               |           |     |            |            |             |               |                |
|   |           | Lt  | 1          | 33,040,000 |             | 33,040,000    |                |
| <b>6.2 Steel cocks</b>                  |           |     |            |            |             |               |                |
|   |           | Lt  | 1          |            | 808,500,000 |               | 808,500,000    |
| <b>6.3 Hollow jet valve</b>             |           |     |            |            |             |               |                |
|   |           | Lt  | 1          | 45,000,000 |             | 45,000,000    |                |
| <b>6.4 Guard valve</b>                  |           |     |            |            |             |               |                |
|   |           | Lt  | 1          | 22,500,000 |             | 22,500,000    |                |
| SUB-TOTAL OF 6.                         |           |     |            |            |             | 100,540,000   | 808,500,000    |
| <b>7. WATER SUPPLY PIPELINE</b>         |           |     |            |            |             |               |                |
| <b>7.1 Excavation</b>                   |           |     |            |            |             |               |                |
|   |           | m3  |            | 276        | 1,651       |               |                |
| <b>7.2 Backfill</b>                     |           |     |            |            |             |               |                |
|   |           | m3  |            | 244        | 1,717       |               |                |
| <b>7.3 Add. pump station</b>            |           |     |            |            |             |               |                |
|   |           | Lt  |            |            |             |               |                |
| <b>7.4 Add. purification plant</b>      |           |     |            |            |             |               |                |
|   |           | Lt  |            |            |             |               |                |
| <b>7.5 Add. pipe line</b>               |           |     |            |            |             |               |                |
|   |           | Lt  |            |            |             |               |                |
| <b>7.6 Add. intake &amp; surge tank</b> |           |     |            |            |             |               |                |
|   |           | Lt  | 1          |            | 504,000,000 |               | 504,000,000    |
| SUB-TOTAL OF 7.                         |           |     |            |            |             |               | 504,000,000    |
| TOTAL OF DIRECT CONSTRUCTION COST       |           |     |            |            |             | 2,251,061,562 | 17,368,619,875 |

Table F-18 Cost Estimate for Heightening of Krenceng Dam with One Diversion Tunnel: Scheme C-2

| DESCRIPTION                         | Unit                             | Qty                  | UNIT PRICE            |                              | AMOUNT                           |                               |                                     |
|-------------------------------------|----------------------------------|----------------------|-----------------------|------------------------------|----------------------------------|-------------------------------|-------------------------------------|
|                                     |                                  |                      | Fc<br>(Yen)           | Lc<br>(Rp)                   | Fc<br>(Yen)                      | Lc<br>(Rp)                    |                                     |
| 1. PREPARATORY WORK<br>(20% of 2+3) |                                  |                      |                       |                              | 264,175,476                      | 1,556,022,425                 |                                     |
| 2. DIVERTED TUNNEL                  |                                  |                      |                       |                              |                                  |                               |                                     |
| 2.1 Coffering work                  |                                  |                      |                       |                              |                                  |                               |                                     |
| Coffering                           | Exca.<br>Embank                  | m3<br>m3             | 500<br>500            | 276<br>441                   | 1,651<br>1,144                   | 138,000<br>220,500            | 825,500<br>572,000                  |
| (Sub-total)                         |                                  |                      |                       |                              | 358,500                          | 1,397,500                     |                                     |
| 2.2 Weir                            |                                  |                      |                       |                              |                                  |                               |                                     |
| Excavation                          | Common<br>Wea.rock<br>Rock       | m3<br>m3<br>m3       | 400<br>400<br>200     | 276<br>339<br>962            | 1,651<br>1,398<br>3,475          | 110,400<br>135,600<br>192,400 | 660,400<br>559,200<br>695,000       |
| Concrete                            |                                  | m3                   | 150                   | 5,052                        | 118,708                          | 757,800                       | 17,806,200                          |
| Rein bar                            |                                  | t                    | 15                    | 5,292                        | 1,460,955                        | 79,380                        | 21,914,325                          |
| Gate                                |                                  | Ls                   | 1                     | 2,000,000                    |                                  | 2,000,000                     |                                     |
| (Sub-total)                         |                                  |                      |                       |                              | 3,275,580                        | 41,635,125                    |                                     |
| 2.3 Inlet & outlet                  |                                  |                      |                       |                              |                                  |                               |                                     |
| Excavation                          | Common<br>Wea.rock<br>Rock       | m3<br>m3<br>m3       | 1,664<br>1,664<br>832 | 276<br>339<br>962            | 1,651<br>1,398<br>3,475          | 459,264<br>564,096<br>800,384 | 2,747,264<br>2,326,272<br>2,891,200 |
| Concrete                            |                                  | m3                   | 100                   | 13,442                       | 132,187                          | 1,344,200                     | 13,218,700                          |
| Rein bar                            |                                  | t                    | 20                    | 5,292                        | 1,460,955                        | 105,840                       | 29,219,100                          |
| Trash rack                          |                                  | Ls                   | 1                     | 1,000,000                    |                                  | 1,000,000                     |                                     |
| (Sub-total)                         |                                  |                      |                       |                              | 4,273,784                        | 50,402,536                    |                                     |
| 2.4 Diverted tunnel                 |                                  |                      |                       |                              |                                  |                               |                                     |
| Excavation                          |                                  | m3                   | 1,600                 | 8,744                        | 105,122                          | 13,990,400                    | 168,195,200                         |
| Lining conc.                        |                                  | m3                   | 650                   | 13,488                       | 155,546                          | 8,767,200                     | 101,104,900                         |
| Plug conc.                          |                                  | m3                   |                       | 13,488                       | 155,546                          |                               |                                     |
| Grouting                            |                                  | t                    | 360                   | 6,500                        | 90,000                           | 2,340,000                     | 32,400,000                          |
| Rein bar                            |                                  | t                    | 35                    | 5,292                        | 1,460,955                        | 185,220                       | 51,133,425                          |
| (Sub-total)                         |                                  |                      |                       |                              |                                  | 25,282,820                    | 352,833,525                         |
| SUB-TOTAL OF 2.                     |                                  |                      |                       |                              |                                  | 33,190,684                    | 446,268,686                         |
| 3. HEIGHTENING OF KRENCENG DAM      |                                  |                      |                       |                              |                                  |                               |                                     |
| 3.1 Main dam                        |                                  |                      |                       |                              |                                  |                               |                                     |
| Excavation                          | Common<br>Wea.rock<br>Rock       | m3<br>m3<br>m3       | 146,652<br>97,768     | 276<br>339<br>962            | 1,651<br>1,398<br>3,475          | 40,475,952<br>33,143,352      | 242,122,452<br>136,679,664          |
| Embankment                          | Core<br>Filter<br>Random<br>Rock | m3<br>m3<br>m3<br>m3 | 1,281,085             | 605<br>2,285<br>441<br>1,514 | 2,359<br>5,756<br>1,144<br>5,964 | 775,056,425                   | 3,022,079,515                       |
| Grouting                            | Blanket<br>Curtain               | t<br>t               | 1,868<br>3,676        | 6,500<br>6,500               | 90,000<br>90,000                 | 12,142,000<br>23,894,000      | 168,120,000<br>330,840,000          |
| (Sub-total)                         |                                  |                      |                       |                              |                                  | 884,711,729                   | 3,899,841,631                       |
| 3.2 Spillway                        |                                  |                      |                       |                              |                                  |                               |                                     |
| (1) Approach wall & weir            |                                  |                      |                       |                              |                                  |                               |                                     |
| Excavation                          | Common<br>Wea.rock<br>Rock       | m3<br>m3<br>m3       | 3,097<br>4,645        | 276<br>339<br>962            | 1,651<br>1,398<br>3,475          | 854,772<br>1,574,655          | 5,113,147<br>6,493,710              |
| Concrete                            |                                  | m3                   | 6,628                 | 13,442                       | 132,187                          | 89,093,576                    | 876,135,436                         |
| Rein bar                            |                                  | t                    | 135                   | 5,292                        | 1,460,955                        | 714,420                       | 197,228,925                         |
| (2) Chute way & basin               |                                  |                      |                       |                              |                                  |                               |                                     |
| Excavation                          | Common<br>Wea.rock<br>Rock       | m3<br>m3<br>m3       | 11,879<br>17,818      | 276<br>339<br>962            | 1,651<br>1,398<br>3,475          | 3,278,604<br>6,040,302        | 19,612,229<br>24,909,564            |
| Concrete                            |                                  | m3                   | 14,260                | 13,442                       | 132,187                          | 191,682,920                   | 1,884,986,620                       |
| Rein bar                            |                                  | t                    | 285                   | 5,292                        | 1,460,955                        | 1,508,220                     | 416,372,175                         |
| Grouting                            | Consoli.                         | t                    | 35                    | 6,500                        | 90,000                           | 227,500                       | 3,150,000                           |
| (3) Metal work                      |                                  |                      |                       |                              |                                  |                               |                                     |
| Spillway gate                       |                                  | Ls                   | 1                     | 108,000,000                  |                                  | 108,000,000                   |                                     |
| (Sub-total)                         |                                  |                      |                       |                              |                                  | 402,974,969                   | 3,434,001,806                       |
| SUB-TOTAL OF 3.                     |                                  |                      |                       |                              |                                  | 1,287,686,698                 | 7,333,843,437                       |
| 4. WATER SUPPLY PIPE LINE           |                                  |                      |                       |                              |                                  |                               |                                     |
| 4.1 Excavation                      |                                  | m3                   |                       | 276                          | 1,651                            |                               |                                     |
| 4.2 Backfill                        |                                  | m3                   |                       | 244                          | 1,717                            |                               |                                     |
| 4.3 Add. pump station               |                                  | Ls                   | 1                     | 1,167,000,000                | 7,808,000,000                    | 1,167,000,000                 | 7,808,000,000                       |
| 4.4 Add. purification plant         |                                  | Ls                   | 1                     | 1,812,000,000                | 12,118,000,000                   | 1,812,000,000                 | 12,118,000,000                      |
| 4.5 Add. pipe line                  |                                  | Ls                   |                       |                              | 1,540,000,000                    |                               |                                     |
| 4.6 Add. intake & surge tank        |                                  | Ls                   | 1                     | 80,000,000                   | 2,914,000,000                    | 80,000,000                    | 2,914,000,000                       |
| 4.7 Receiving well                  |                                  | Ls                   | 1                     | 6,000,000                    | 218,400,000                      | 6,000,000                     | 218,400,000                         |
| SUB-TOTAL OF 4.                     |                                  |                      |                       |                              |                                  | 3,065,000,000                 | 23,058,400,000                      |
| TOTAL OF DIRECT CONSTRUCTION COST   |                                  |                      |                       |                              |                                  | 4,650,052,858                 | 32,394,534,548                      |



Table F-19 Cost Estimate for Cidanau Gated Weir: Scheme C-3

| DESCRIPTION                                    | Unit     | Q'ty | UNIT PRICE    |             | AMOUNT        |                |               |
|--|----------|------|---------------|-------------|---------------|----------------|---------------|
|  |          |      | Fc<br>(Yen)   | Lc<br>(Rp)  | Fc<br>(Yen)   | Lc<br>(Rp)     |               |
| <b>1. PREPARATORY WORK</b><br>(20% of 2+3+4+5) |          |      |               |             |               |                |               |
|  |          |      |               |             | 414,455,432   | 1,755,702,092  |               |
| <b>2. DIVERSION WORK</b>                       |          |      |               |             |               |                |               |
| 2.1 Coffering work<br>Sheet pile & bracing     | t        | 159  | 131,583       | 36,915      | 20,921,697    | 5,869,485      |               |
| SUB-TOTAL OF 2.                                |          |      |               |             | 20,921,697    | 5,869,485      |               |
| <b>3. DAM</b>                                  |          |      |               |             |               |                |               |
| <b>3.1 Main dam</b>                            |          |      |               |             |               |                |               |
| Excavation                                     | Common   | m3   | 10,662        | 276         | 1,651         | 2,942,712      | 17,602,962    |
|  | Wea.rock | m3   | 8,462         | 339         | 1,398         | 2,868,618      | 11,829,876    |
|  | Rock     | m3   | 2,200         | 962         | 3,475         | 2,116,400      | 7,645,000     |
| Concrete                                       |          | m3   | 21,325        | 5,052       | 118,708       | 107,733,900    | 2,531,448,100 |
| Grouting                                       | Consoli. | t    | 219           | 6,500       | 90,000        | 1,423,500      | 19,710,000    |
|  | Curtain  | t    | 352           | 6,500       | 90,000        | 2,288,000      | 31,680,000    |
| SUB-TOTAL OF 3.                                |          |      |               |             | 119,373,130   | 2,619,915,938  |               |
| <b>4. SPILLWAY</b>                             |          |      |               |             |               |                |               |
| <b>4.1 Dental work</b>                         |          |      |               |             |               |                |               |
| Excavation                                     | Common   | m3   | 22,389        | 276         | 1,651         | 6,179,364      | 36,964,239    |
|  | Wea.rock | m3   |               | 339         | 1,398         |                |               |
|  | Rock     | m3   |               | 962         | 3,475         |                |               |
| Concrete                                       |          | m3   | 8,379         | 5,052       | 118,708       | 42,330,708     | 994,654,332   |
| (Sub-total)                                    |          |      |               |             | 48,510,072    | 1,031,618,571  |               |
| <b>4.2 Weir &amp; pier</b>                     |          |      |               |             |               |                |               |
| Excavation                                     | Common   | m3   |               | 276         | 1,651         |                |               |
|  | Wea.rock | m3   | 1,170         | 339         | 1,398         | 396,630        | 1,635,660     |
|  | Rock     | m3   | 500           | 962         | 3,475         | 481,000        | 1,737,500     |
| Concrete                                       |          | m3   | 10,761        | 13,442      | 132,187       | 144,649,362    | 1,422,464,307 |
| Rein bar                                       |          | t    | 1,290         | 5,292       | 1,460,955     | 6,826,680      | 1,884,631,950 |
| Grouting                                       | Consoli. | t    | 126           | 6,500       | 90,000        | 819,000        | 11,340,000    |
|  | Curtain  | t    | 180           | 6,500       | 90,000        | 1,170,000      | 16,200,000    |
| (Sub-total)                                    |          |      |               |             | 154,342,672   | 3,338,009,417  |               |
| <b>4.3 Hoist &amp; bridge</b>                  |          |      |               |             |               |                |               |
| Concrete                                       |          | m3   | 2,871         | 13,442      | 132,187       | 38,591,982     | 379,508,877   |
| Rein bar                                       |          | t    | 574           | 5,292       | 1,460,955     | 3,037,608      | 838,588,170   |
| (Sub-total)                                    |          |      |               |             | 41,629,590    | 1,218,097,047  |               |
| SUB-TOTAL OF 4.                                |          |      |               |             | 244,482,334   | 5,587,725,035  |               |
| <b>5. METAL WORK</b>                           |          |      |               |             |               |                |               |
| 5.1 Roller gate                                | Ls       | 1    | 1,620,000,000 |             |               | 1,620,000,000  |               |
| 5.2 Steel conduit                              | Ls       | 1    |               | 565,000,000 |               |                | 565,000,000   |
| 5.3 Hollow jet valve                           | Ls       | 1    | 45,000,000    |             |               | 45,000,000     |               |
| 5.4 Guard valve                                | Ls       | 1    | 22,500,000    |             |               | 22,500,000     |               |
| SUB-TOTAL OF 5.                                |          |      |               |             | 1,687,500,000 | 565,000,000    |               |
| <b>6. WATER SUPPLY PIPE LINE</b>               |          |      |               |             |               |                |               |
| 6.1 Excavation                                 |          | m3   |               | 276         | 1,651         |                |               |
| 6.2 Backfill                                   |          | m3   |               | 244         | 1,717         |                |               |
| 6.3 Add. pump station                          |          | Ls   |               |             |               |                |               |
| 6.4 Add. purification plant                    |          | Ls   |               |             |               |                |               |
| 6.5 Add. pipe line                             |          | Ls   |               |             |               |                |               |
| 6.6 Add. intake & surge tank                   |          | Ls   |               |             |               |                |               |
| SUB-TOTAL OF 6.                                |          |      |               |             |               |                |               |
| <b>TOTAL OF DIRECT CONSTRUCTION COST</b>       |          |      |               |             | 2,486,732,593 | 10,534,212,550 |               |

Table F-20 Cost Estimate for Heightening of Krenceng Dam with One Diversion Tunnel: Scheme C-3

| DESCRIPTION                         | Unit     | Qty | UNIT PRICE  |               | AMOUNT         |               |                |
|-------------------------------------|----------|-----|-------------|---------------|----------------|---------------|----------------|
|                                     |          |     | Fc<br>(Yen) | Lc<br>(Rp)    | Fc<br>(Yen)    | Lc<br>(Rp)    |                |
| 1. PREPARATORY WORK<br>(20% of 2+3) |          |     |             |               |                | 264,175,476   | 1,556,022,425  |
| 2. DIVERTED TUNNEL                  |          |     |             |               |                |               |                |
| 2.1 Coffering work                  |          |     |             |               |                |               |                |
| Coffering                           | Exca.    | m3  | 500         | 276           | 1,651          | 138,000       | 825,500        |
|                                     | Embank   | m3  | 500         | 441           | 1,144          | 220,500       | 572,000        |
| (Sub-total)                         |          |     |             |               |                | 358,500       | 1,397,500      |
| 2.2 Weir                            |          |     |             |               |                |               |                |
| Excavation                          | Common   | m3  | 400         | 276           | 1,651          | 110,400       | 660,400        |
|                                     | Wea.rock | m3  | 400         | 339           | 1,398          | 135,600       | 559,200        |
|                                     | Rock     | m3  | 200         | 962           | 3,475          | 192,400       | 695,000        |
| Concrete                            |          | m3  | 150         | 5,052         | 118,708        | 757,800       | 17,806,200     |
| Rein bar                            |          | t   | 15          | 5,292         | 1,460,955      | 79,380        | 21,914,325     |
| Gate                                |          | Ls  | 1           | 2,000,000     |                | 2,000,000     |                |
| (Sub-total)                         |          |     |             |               |                | 3,275,580     | 41,635,125     |
| 2.3 Inlet & outlet                  |          |     |             |               |                |               |                |
| Excavation                          | Common   | m3  | 1,664       | 276           | 1,651          | 459,264       | 2,747,264      |
|                                     | Wea.rock | m3  | 1,664       | 339           | 1,398          | 564,096       | 2,326,272      |
|                                     | Rock     | m3  | 832         | 962           | 3,475          | 800,384       | 2,891,200      |
| Concrete                            |          | m3  | 100         | 13,442        | 132,187        | 1,344,200     | 13,218,700     |
| Rein bar                            |          | t   | 20          | 5,292         | 1,460,955      | 105,840       | 29,219,100     |
| Trash rack                          |          | Ls  | 1           | 1,000,000     |                | 1,000,000     |                |
| (Sub-total)                         |          |     |             |               |                | 4,273,784     | 50,402,536     |
| 2.4 Diverted tunnel                 |          |     |             |               |                |               |                |
| Excavation                          |          | m3  | 1,600       | 8,744         | 105,122        | 13,990,400    | 168,195,200    |
| Lining conc.                        |          | m3  | 650         | 13,488        | 155,546        | 8,767,200     | 101,104,900    |
| Plug conc.                          |          | m3  |             | 13,488        | 155,546        |               |                |
| Grouting                            |          | t   | 360         | 6,500         | 90,000         | 2,340,000     | 32,400,000     |
| Rein bar                            |          | t   | 35          | 5,292         | 1,460,955      | 185,220       | 51,133,425     |
| (Sub-total)                         |          |     |             |               |                | 25,282,820    | 352,833,525    |
| SUB-TOTAL OF 2.                     |          |     |             |               |                | 33,190,684    | 446,268,686    |
| 3. HEIGHTENING OF KRENCENG DAM      |          |     |             |               |                |               |                |
| 3.1 Main dam                        |          |     |             |               |                |               |                |
| Excavation                          | Common   | m3  | 146,652     | 276           | 1,651          | 40,475,952    | 242,122,452    |
|                                     | Wea.rock | m3  | 97,768      | 339           | 1,398          | 33,143,352    | 136,679,664    |
|                                     | Rock     | m3  |             | 962           | 3,475          |               |                |
| Embankment                          | Core     | m3  | 1,281,085   | 605           | 2,359          | 775,056,425   | 3,022,079,515  |
|                                     | Filter   | m3  |             | 2,285         | 5,756          |               |                |
|                                     | Random   | m3  |             | 441           | 1,144          |               |                |
|                                     | Rock     | m3  |             | 1,514         | 5,964          |               |                |
| Grouting                            | Blanket  | t   | 1,868       | 6,500         | 90,000         | 12,142,000    | 168,120,000    |
|                                     | Curtain  | t   | 3,676       | 6,500         | 90,000         | 23,894,000    | 330,840,000    |
| (Sub-total)                         |          |     |             |               |                | 884,711,729   | 3,899,841,631  |
| 3.2 SPILLWAY                        |          |     |             |               |                |               |                |
| (1) Approach wall & weir            |          |     |             |               |                |               |                |
| Excavation                          | Common   | m3  | 3,097       | 276           | 1,651          | 854,772       | 5,113,147      |
|                                     | Wea.rock | m3  | 4,645       | 339           | 1,398          | 1,574,655     | 6,493,710      |
|                                     | Rock     | m3  |             | 962           | 3,475          |               |                |
| Concrete                            |          | m3  | 6,628       | 13,442        | 132,187        | 89,093,576    | 876,135,436    |
| Rein bar                            |          | t   | 135         | 5,292         | 1,460,955      | 714,420       | 197,228,925    |
| (2) Chute-way & basin               |          |     |             |               |                |               |                |
| Excavation                          | Common   | m3  | 11,879      | 276           | 1,651          | 3,278,604     | 19,612,229     |
|                                     | Wea.rock | m3  | 17,818      | 339           | 1,398          | 6,040,302     | 24,909,564     |
|                                     | Rock     | m3  |             | 962           | 3,475          |               |                |
| Concrete                            |          | m3  | 14,260      | 13,442        | 132,187        | 191,682,920   | 1,884,986,620  |
| Rein bar                            |          | t   | 285         | 5,292         | 1,460,955      | 1,508,220     | 416,372,175    |
| Grouting                            | Consoli. | t   | 35          | 6,500         | 90,000         | 227,500       | 3,150,000      |
| (3) Metal work                      |          |     |             |               |                |               |                |
| Spillway gate                       |          | Ls  | 1           | 108,000,000   |                | 108,000,000   |                |
| (Sub-total)                         |          |     |             |               |                | 402,974,969   | 3,434,001,806  |
| SUB-TOTAL OF 3.                     |          |     |             |               |                | 1,287,686,698 | 7,333,843,437  |
| 4. WATER SUPPLY PIPE LINE           |          |     |             |               |                |               |                |
| 4.1 Excavation                      |          | m3  |             | 276           | 1,651          |               |                |
| 4.2 Backfill                        |          | m3  |             | 244           | 1,717          |               |                |
| 4.3 Add. pump station               |          | Ls  | 1           | 1,189,000,000 | 7,951,000,000  | 1,189,000,000 | 7,951,000,000  |
| 4.4 Add. purification plant         |          | Ls  | 1           | 1,875,000,000 | 12,538,000,000 | 1,875,000,000 | 12,538,000,000 |
| 4.5 Add. pipe line                  |          | Ls  |             |               | 1,540,000,000  |               |                |
| 4.6 Add. intake & surge tank        |          | Ls  | 1           | 82,000,000    | 3,003,000,000  | 82,000,000    | 3,003,000,000  |
| 4.7 Receiving well                  |          | Ls  | 1           | 6,000,000     | 218,400,000    | 6,000,000     | 218,400,000    |
| SUB-TOTAL OF 4.                     |          |     |             |               |                | 3,152,000,000 | 23,710,400,000 |
| TOTAL OF DIRECT CONSTRUCTION COST   |          |     |             |               |                | 1,585,052,858 | 9,336,134,548  |

Table F-21 Cost Estimate for Cibanten Dam: Scheme D-1

| DESCRIPTION                                      | Unit         | Qty | UNIT PRICE |            | AMOUNT         |               |                |
|--|--------------|-----|------------|------------|----------------|---------------|----------------|
|  |              |     | Fe (Cen)   | Le (Rp)    | Fe (Cen)       | Le (Rp)       |                |
| <b>1. PREPARATORY WORK</b><br>(20% of 2+3+4+5+6) |              |     |            |            |                |               |                |
|  |              |     |            |            | 464,132,519    | 2,947,352,634 |                |
| <b>2. DIVERSION WORK</b>                         |              |     |            |            |                |               |                |
| 2.1 Inlet & outlet Excavation                    | Common       | m3  | 1,051      | 276        | 1,651          | 290,628       | 1,738,501      |
|  | Wear rock    | m3  | 2,106      | 339        | 1,398          | 713,934       | 2,944,118      |
|  | Rock         | m3  | 7,371      | 962        | 3,475          | 7,090,502     | 25,614,225     |
|  | Concrete     | m3  | 2,640      | 13,442     | 132,187        | 35,466,880    | 348,973,680    |
|  | Rein bar     | t   | 100        | 5,292      | 1,460,955      | 529,200       | 146,095,500    |
| (Sub-total)                                      |              |     |            |            |                | 44,111,544    | 525,366,096    |
| 2.2 Tunnel (Ø=430cm, D=5cm) Excavation           |              | m3  | 10,462     | 8,744      | 105,122        | 91,479,728    | 1,099,786,364  |
|  | Lining conc. | m3  | 2,404      | 13,488     | 155,546        | 32,425,152    | 373,932,584    |
|  | Plug conc.   | m3  | 686        | 13,488     | 155,546        | 9,252,768     | 106,704,556    |
|  | Grouing      | t   | 246        | 6,500      | 90,000         | 1,595,000     | 22,140,000     |
|  | Rein bar     | t   | 123        | 5,292      | 1,460,955      | 650,916       | 179,697,465    |
| (Sub-total)                                      |              |     |            |            |                | 135,407,564   | 1,782,260,969  |
| SUB-TOTAL OF 2.                                  |              |     |            |            |                | 179,519,108   | 2,307,627,065  |
| <b>3. DAM</b>                                    |              |     |            |            |                |               |                |
| 3.1 Cofferdam Excavation                         |              | m3  | 2,500      | 276        | 1,651          | 690,000       | 4,127,500      |
|  | Backhoe rock | m3  | 200,000    | 1,514      | 5,964          | 302,600,000   | 1,192,600,000  |
| (Sub-total)                                      |              |     |            |            |                | 303,490,000   | 1,196,927,500  |
| 3.2 Main dam Excavation                          | Common       | m3  | 11,075     | 276        | 1,651          | 3,056,700     | 18,284,825     |
|  | Wear rock    | m3  | 22,150     | 339        | 1,398          | 7,535,850     | 30,965,200     |
|  | Rock         | m3  | 77,520     | 962        | 3,475          | 74,574,240    | 269,382,000    |
|  | Embankment   |     |            |            |                |               |                |
|  | Core         | m3  | 101,416    | 605        | 2,359          | 61,336,680    | 239,240,344    |
|  | Filter       | m3  | 62,694     | 2,285      | 5,756          | 143,141,540   | 360,578,864    |
|  | Random Rock  | m3  | 174,900    | 441        | 1,144          | 77,130,900    | 200,085,600    |
|  | Rock         | m3  | 488,105    | 1,514      | 5,964          | 617,870,970   | 2,433,938,220  |
|  | Grouing      |     |            |            |                |               |                |
|  | Blanket      | t   | 474        | 6,500      | 90,000         | 3,081,000     | 42,660,000     |
|  | Control      | t   | 114        | 6,500      | 90,000         | 741,000       | 10,260,000     |
|  | Chain        | t   | 1,287      | 6,500      | 90,000         | 8,365,500     | 115,830,000    |
| (Sub-total)                                      |              |     |            |            |                | 996,827,380   | 3,721,225,553  |
| 3.3 Saddle dam Excavation                        | Common       | m3  | 3,595      | 276        | 1,651          | 992,220       | 7,822,720      |
|  | Wear rock    | m3  | 7,190      | 339        | 1,398          | 2,437,410     | 18,585,150     |
|  | Rock         | m3  | 25,160     | 962        | 4,433          | 24,233,920    | 111,594,280    |
|  | Embankment   |     |            |            |                |               |                |
|  | Rock         | m3  | 167,975    | 264        | 1,717          | 40,985,900    | 284,413,075    |
|  | Grouing      | t   | 597        | 13,442     | 132,187        | 8,024,874     | 78,913,639     |
| (Sub-total)                                      |              |     |            |            |                | 76,644,324    | 505,271,864    |
| SUB-TOTAL OF 3.                                  |              |     |            |            |                | 1,376,961,704 | 5,423,424,917  |
| <b>4. SPILLWAY</b>                               |              |     |            |            |                |               |                |
| 4.1 Side channel Excavation                      | Common       | m3  | 8,100      | 276        | 1,651          | 2,235,600     | 13,373,100     |
|  | Wear rock    | m3  | 16,200     | 339        | 1,398          | 5,491,800     | 22,647,600     |
|  | Rock         | m3  | 56,700     | 962        | 3,475          | 54,545,400    | 197,002,500    |
|  | Concrete     | m3  | 21,170     | 13,442     | 132,187        | 284,967,140   | 2,798,398,790  |
|  | Rein bar     | t   | 400        | 5,292      | 1,460,955      | 2,116,800     | 584,382,000    |
| (Sub-total)                                      |              |     |            |            |                | 348,956,740   | 3,615,833,990  |
| 4.2 Chute way Excavation                         | Common       | m3  | 14,245     | 276        | 1,651          | 3,931,620     | 23,518,495     |
|  | Wear rock    | m3  | 28,490     | 339        | 1,398          | 9,658,110     | 39,829,020     |
|  | Rock         | m3  | 99,715     | 962        | 3,475          | 95,925,830    | 346,509,825    |
|  | Concrete     | m3  | 11,395     | 13,442     | 132,187        | 153,171,590   | 1,506,270,865  |
|  | Rein bar     | t   | 220        | 5,292      | 1,460,955      | 1,164,240     | 319,210,100    |
| (Sub-total)                                      |              |     |            |            |                | 263,851,390   | 2,235,338,105  |
| 4.3 Plunge pool Excavation                       | Common       | m3  | 4,032      | 276        | 1,651          | 1,112,832     | 6,655,832      |
|  | Wear rock    | m3  | 8,064      | 339        | 1,398          | 2,733,696     | 11,273,472     |
|  | Rock         | m3  | 28,224     | 962        | 3,475          | 27,151,433    | 98,078,400     |
| (Sub-total)                                      |              |     |            |            |                | 30,998,016    | 116,008,704    |
| SUB-TOTAL OF 4.                                  |              |     |            |            |                | 643,806,146   | 5,967,180,799  |
| <b>5. OULET WORK</b>                             |              |     |            |            |                |               |                |
| 5.1 Intake tower Excavation                      | Common       | m3  | 515        | 276        | 1,651          | 142,140       | 850,365        |
|  | Wear rock    | m3  | 1,030      | 339        | 1,398          | 349,170       | 1,439,840      |
|  | Rock         | m3  | 3,606      | 962        | 3,475          | 3,468,972     | 12,530,840     |
|  | Concrete     | m3  | 760        | 13,442     | 132,187        | 10,215,920    | 100,462,120    |
|  | Rein bar     | t   | 29         | 5,292      | 1,460,955      | 153,468       | 42,367,695     |
| (Sub-total)                                      |              |     |            |            |                | 14,329,670    | 157,660,870    |
| 5.2 Intake shaft Excavation                      |              | m3  | 332        | 8,744      | 103,122        | 2,903,038     | 33,904,504     |
|  | Concrete     | m3  | 191        | 13,488     | 155,546        | 2,576,208     | 29,709,286     |
|  | Rein bar     | t   | 6          | 5,292      | 1,460,955      | 31,752        | 8,765,730      |
| (Sub-total)                                      |              |     |            |            |                | 5,510,998     | 72,379,520     |
| SUB-TOTAL OF 5.                                  |              |     |            |            |                | 19,840,668    | 230,030,390    |
| <b>6. METAL WORK</b>                             |              |     |            |            |                |               |                |
| 6.1 Diversion gate                               |              | Lt  | 1          | 33,040,000 |                | 33,040,000    |                |
| 6.2 Steel conduit                                |              | Lt  | 1          |            | 808,500,000    |               | 808,500,000    |
| 6.3 Hollow jet valve                             |              | Lt  | 1          | 45,000,000 |                | 45,000,000    |                |
| 6.4 Guard valve                                  |              | Lt  | 1          | 22,500,000 |                | 22,500,000    |                |
| SUB-TOTAL OF 6.                                  |              |     |            |            |                | 100,540,000   | 808,500,000    |
| <b>7. WATER SUPPLY PIPELINE</b>                  |              |     |            |            |                |               |                |
| 7.1 Excavation                                   |              | m3  | 134,400    | 276        | 1,651          | 37,094,400    | 221,894,400    |
| 7.2 Backfill                                     |              | m3  | 123,200    | 244        | 1,717          | 30,060,800    | 211,534,400    |
| 7.3 Add. pump station                            |              | Lt  |            |            |                |               |                |
| 7.4 Add. purification plant                      |              | Lt  |            |            |                |               |                |
| 7.5 Add. pipe line                               |              | Lt  | 1          |            | 39,200,000,000 |               | 39,200,000,000 |
| 7.6 Add. intake & storage tank                   |              | Lt  |            |            |                |               |                |
| SUB-TOTAL OF 7.                                  |              |     |            |            |                | 67,155,200    | 39,633,428,800 |
| TOTAL OF DIRECT CONSTRUCTION COST                |              |     |            |            |                | 2,851,956,315 | 57,317,514,605 |

Table F-22 Cost Estimate for Heightening of Krenceng Dam with Two Diversion Tunnels: Scheme D-1

| DESCRIPTION                         | Unit     | Q'ty | UNIT PRICE  |               | AMOUNT         |               |                |
|-------------------------------------|----------|------|-------------|---------------|----------------|---------------|----------------|
|                                     |          |      | Fc<br>(Yen) | Lc<br>(Rp)    | Fc<br>(Yen)    | Lc<br>(Rp)    |                |
| 1. PREPARATORY WORK<br>(20% of 2+3) |          |      |             |               | 277,982,360    | 1,734,709,347 |                |
| 2. DIVERTED TUNNEL                  |          |      |             |               |                |               |                |
| 2.1 Coffering work                  |          |      |             |               |                |               |                |
| Coffering                           | Exca.    | m3   | 1,000       | 276           | 1,651          | 276,000       | 1,651,000      |
|                                     | Embank   | m3   | 1,000       | 441           | 1,144          | 441,000       | 1,144,000      |
| (Sub-total)                         |          |      |             |               |                | 717,000       | 2,795,000      |
| 2.2 Weir                            |          |      |             |               |                |               |                |
| Excavation                          | Common   | m3   | 1,200       | 276           | 1,651          | 331,200       | 1,981,200      |
|                                     | Wea.rock | m3   | 1,200       | 339           | 1,398          | 406,800       | 1,677,600      |
|                                     | Rock     | m3   | 600         | 962           | 3,475          | 577,200       | 2,085,000      |
| Concrete                            |          | m3   | 410         | 5,052         | 118,708        | 2,071,320     | 48,670,280     |
| Rein bar                            |          | t    | 41          | 5,292         | 1,460,955      | 216,972       | 59,899,155     |
| Gate                                | Ls       | 2    |             | 2,000,000     |                | 4,000,000     |                |
| (Sub-total)                         |          |      |             |               |                | 7,603,492     | 114,313,235    |
| 2.3 Inlet & outlet                  |          |      |             |               |                |               |                |
| Excavation                          | Common   | m3   | 4,576       | 276           | 1,651          | 1,262,976     | 7,554,976      |
|                                     | Wea.rock | m3   | 4,576       | 339           | 1,398          | 1,551,264     | 6,397,248      |
|                                     | Rock     | m3   | 2,288       | 962           | 3,475          | 2,201,056     | 7,950,800      |
| Concrete                            |          | m3   | 200         | 13,442        | 132,187        | 2,688,400     | 26,437,400     |
| Rein bar                            |          | t    | 40          | 5,292         | 1,460,955      | 211,680       | 58,438,200     |
| Trash rack                          | Ls       | 2    |             | 1,000,000     |                | 2,000,000     |                |
| (Sub-total)                         |          |      |             |               |                | 9,915,376     | 106,778,624    |
| 2.4 Diverted tunnel                 |          |      |             |               |                |               |                |
| Excavation                          |          | m3   | 5,320       | 8,744         | 105,122        | 46,518,080    | 559,249,040    |
| Lining conc.                        |          | m3   | 2,170       | 13,488        | 155,546        | 29,268,960    | 337,534,820    |
| Plug conc.                          |          | m3   |             | 13,488        | 155,546        |               |                |
| Grouting                            |          | t    | 1,200       | 6,500         | 90,000         | 7,800,000     | 108,000,000    |
| Rein bar                            |          | t    | 76          | 5,292         | 1,460,955      | 402,192       | 111,032,580    |
| (Sub-total)                         |          |      |             |               |                | 83,989,232    | 1,115,816,440  |
| SUB-TOTAL OF 2.                     |          |      |             |               |                | 102,225,100   | 1,339,703,299  |
| 3. HEIGHTENING OF KRENCENG DAM      |          |      |             |               |                |               |                |
| 3.1 Main dam                        |          |      |             |               |                |               |                |
| Excavation                          | Common   | m3   | 146,652     | 276           | 1,651          | 40,475,952    | 242,122,452    |
|                                     | Wea.rock | m3   | 97,768      | 339           | 1,398          | 33,143,352    | 136,679,664    |
|                                     | Rock     | m3   |             | 962           | 3,475          |               |                |
| Embankment                          | Core     | m3   | 1,281,085   | 605           | 2,359          | 775,056,425   | 3,022,079,515  |
|                                     | Filter   | m3   |             | 2,285         | 5,756          |               |                |
|                                     | Random   | m3   |             | 441           | 1,144          |               |                |
|                                     | Rock     | m3   |             | 1,514         | 5,964          |               |                |
| Grouting                            | Blanket  | t    | 1,868       | 6,500         | 90,000         | 12,142,000    | 168,120,000    |
|                                     | Curtain  | t    | 3,676       | 6,500         | 90,000         | 23,894,000    | 330,840,000    |
| (Sub-total)                         |          |      |             |               |                | 884,711,729   | 3,899,841,631  |
| 3.2 SPILLWAY                        |          |      |             |               |                |               |                |
| (1) Approach wall & weir            |          |      |             |               |                |               |                |
| Excavation                          | Common   | m3   | 3,097       | 276           | 1,651          | 854,772       | 5,113,147      |
|                                     | Wea.rock | m3   | 4,645       | 339           | 1,398          | 1,574,655     | 6,493,710      |
|                                     | Rock     | m3   |             | 962           | 3,475          |               |                |
| Concrete                            |          | m3   | 6,628       | 13,442        | 132,187        | 89,093,576    | 876,135,436    |
| Rein bar                            |          | t    | 135         | 5,292         | 1,460,955      | 714,420       | 197,228,925    |
| (2) Chute-way & basin               |          |      |             |               |                |               |                |
| Excavation                          | Common   | m3   | 11,879      | 276           | 1,651          | 3,278,604     | 19,612,229     |
|                                     | Wea.rock | m3   | 17,818      | 339           | 1,398          | 6,040,302     | 24,909,564     |
|                                     | Rock     | m3   |             | 962           | 3,475          |               |                |
| Concrete                            |          | m3   | 14,260      | 13,442        | 132,187        | 191,682,920   | 1,884,986,620  |
| Rein bar                            |          | t    | 285         | 5,292         | 1,460,955      | 1,508,220     | 416,372,175    |
| Grouting                            | Consoli. | t    | 35          | 6,500         | 90,000         | 227,500       | 3,150,000      |
| (3) Metal work                      |          |      |             |               |                |               |                |
| Spillway gate                       | Ls       | 1    |             | 108,000,000   |                | 108,000,000   |                |
| (Sub-total)                         |          |      |             |               |                | 402,974,969   | 3,434,001,806  |
| SUB-TOTAL OF 3.                     |          |      |             |               |                | 1,287,686,698 | 7,333,843,437  |
| 4. WATER SUPPLY PIPE LINE           |          |      |             |               |                |               |                |
| 4.1 Excavation                      |          | m3   |             | 276           | 1,651          |               |                |
| 4.2 Backfill                        |          | m3   |             | 244           | 1,717          |               |                |
| 4.3 Add. pump station               |          | Ls   | 1           | 1,188,000,000 | 7,943,000,000  | 1,188,000,000 | 7,943,000,000  |
| 4.4 Add. purification plant         |          | Ls   | 1           | 1,511,000,000 | 10,103,000,000 | 1,511,000,000 | 10,103,000,000 |
| 4.5 Add. pipe line                  |          | Ls   |             |               | 1,540,000,000  |               |                |
| 4.6 Add. intake & surge tank        |          | Ls   | 1           | 79,000,000    | 2,899,000,000  | 79,000,000    | 2,899,000,000  |
| 4.7 Receiving well                  |          | Ls   | 1           | 6,000,000     | 218,400,000    | 6,000,000     | 218,400,000    |
| SUB-TOTAL OF 4.                     |          |      |             |               |                | 2,784,000,000 | 21,163,400,000 |
| TOTAL OF DIRECT CONSTRUCTION COST   |          |      |             |               |                | 4,451,894,158 | 31,571,656,083 |

Table F-23 Cost Estimate for Downstream Cidanau Dam: Scheme D-2

| DESCRIPTION                                      | Unit                  | Qty | UNIT PRICE |            | AMOUNT      |               |                |
|--|-----------------------|-----|------------|------------|-------------|---------------|----------------|
|  |                       |     | Fc (Yen)   | Lc (Rp)    | Fc (Yen)    | Lc (Rp)       |                |
| <b>1. PREPARATORY WORK</b><br>(20% of 2+3+4+5+6) |                       |     |            |            |             | 375,176,927   | 2,810,769,979  |
| <b>2. DIVERSION WORK</b>                         |                       |     |            |            |             |               |                |
| 2.1 Inlet & outlet                               |                       |     |            |            |             |               |                |
| Excavation                                       | Common                | m3  | 997        | 276        | 1,651       | 275,172       | 1,646,047      |
|  | Wearrock              | m3  | 11,970     | 339        | 1,398       | 4,057,830     | 16,734,060     |
|  | Rock                  | m3  | 6,982      | 962        | 3,475       | 6,716,684     | 24,267,430     |
|  | Concrete              | m3  | 2,640      | 13,442     | 132,187     | 35,486,850    | 348,973,680    |
|  | Rein bar              | t   | 100        | 5,292      | 1,460,955   | 529,200       | 146,095,500    |
|  | (Sub-total)           |     |            |            |             | 47,065,766    | 337,711,737    |
| 2.2 Trench(1-400m,D=5m)                          |                       |     |            |            |             |               |                |
| Excavation                                       | Common                | m3  | 10,710     | 8,744      | 105,122     | 93,641,240    | 1,125,856,620  |
|  | Wearrock              | m3  | 2,454      | 13,488     | 155,516     | 33,234,432    | 383,265,344    |
|  | Lining conc.          | m3  | 656        | 13,488     | 155,516     | 8,852,768     | 106,701,536    |
|  | Plg conc.             | m3  | 656        | 13,488     | 155,516     | 8,852,768     | 106,701,536    |
|  | Grouting              | t   | 504        | 6,500      | 90,000      | 3,276,000     | 45,369,000     |
|  | Rein bar              | t   | 126        | 5,292      | 1,460,955   | 666,792       | 184,080,330    |
|  | (Sub-total)           |     |            |            |             | 140,078,232   | 1,845,266,850  |
| SUB-TOTAL OF 2.                                  |                       |     |            |            |             | 187,143,998   | 2,382,978,587  |
| <b>3. DAM</b>                                    |                       |     |            |            |             |               |                |
| 3.1 Cofferdam                                    |                       |     |            |            |             |               |                |
| Excavation                                       | Common                | m3  | 2,500      | 276        | 1,651       | 690,000       | 4,127,500      |
|  | Wearrock              | m3  | 200,000    | 1,514      | 5,964       | 302,800,000   | 1,192,800,000  |
|  | (Sub-total)           |     |            |            |             | 303,490,000   | 1,196,927,500  |
| 3.2 Main dam                                     |                       |     |            |            |             |               |                |
| Excavation                                       | Common                | m3  | 24,986     | 276        | 1,651       | 6,896,135     | 41,251,886     |
|  | Wearrock              | m3  | 51,136     | 339        | 1,398       | 14,352,104    | 75,682,128     |
|  | Rock                  | m3  | 4,164      | 962        | 3,475       | 4,005,768     | 14,469,900     |
|  | Core                  | m3  | 49,100     | 605        | 2,359       | 29,705,500    | 115,826,900    |
|  | Filter                | m3  | 31,308     | 441        | 5,756       | 71,538,780    | 180,208,848    |
|  | Random Rock           | m3  | 72,975     | 1,514      | 5,964       | 32,181,975    | 83,483,400     |
|  | Grouting              | t   | 170,275    | 6,500      | 90,000      | 257,796,320   | 1,015,320,100  |
|  | Blanket               | t   | 56         | 6,500      | 90,000      | 364,000       | 5,040,000      |
|  | Course                | t   | 182        | 6,500      | 90,000      | 1,183,000     | 16,380,000     |
|  | Curain                | t   | 2,556      | 6,500      | 90,000      | 16,614,000    | 230,040,000    |
|  | (Sub-total)           |     |            |            |             | 438,637,613   | 1,777,903,162  |
| 3.3 Sand trap basin                              |                       |     |            |            |             |               |                |
| Excavation                                       | Common                | m3  | 306,750    | 276        | 1,651       | 84,663,000    | 667,448,000    |
|  | Wearrock              | m3  |            | 339        | 1,398       |               |                |
|  | Rock                  | m3  |            | 962        | 3,475       |               |                |
|  | Maintenance road(2km) | m3  | 55,000     | 244        | 1,717       | 13,420,000    | 94,435,000     |
|  | Concrete              | m3  | 1,200      | 13,442     | 132,187     | 16,130,400    | 158,624,400    |
|  | (Sub-total)           |     |            |            |             | 114,213,400   | 929,547,400    |
| SUB-TOTAL OF 3.                                  |                       |     |            |            |             | 456,341,013   | 3,895,378,082  |
| <b>4. SPILLWAY</b>                               |                       |     |            |            |             |               |                |
| 4.1 Side channel                                 |                       |     |            |            |             |               |                |
| Excavation                                       | Common                | m3  | 103,740    | 276        | 1,651       | 28,632,240    | 171,274,740    |
|  | Wearrock              | m3  | 116,207    | 339        | 1,398       | 39,563,673    | 163,156,346    |
|  | Rock                  | m3  | 38,902     | 962        | 3,475       | 37,423,724    | 135,184,450    |
|  | Concrete              | m3  | 27,724     | 13,442     | 132,187     | 372,666,038   | 3,664,552,314  |
|  | Rein bar              | t   | 520        | 5,292      | 1,460,955   | 2,751,840     | 759,696,630    |
|  | (Sub-total)           |     |            |            |             | 481,037,485   | 4,894,064,564  |
| 4.2 Chute way                                    |                       |     |            |            |             |               |                |
| Excavation                                       | Common                | m3  | 53,093     | 276        | 1,651       | 14,653,668    | 87,656,543     |
|  | Wearrock              | m3  | 127,425    | 339        | 1,398       | 43,197,075    | 176,140,150    |
|  | Rock                  | m3  | 31,856     | 962        | 3,475       | 30,645,472    | 110,699,600    |
|  | Concrete              | m3  | 8,775      | 13,442     | 132,187     | 117,953,550   | 1,159,940,925  |
|  | Rein bar              | t   | 175        | 5,292      | 1,460,955   | 926,100       | 253,917,125    |
|  | (Sub-total)           |     |            |            |             | 207,375,865   | 1,790,354,313  |
| 4.3 Flange pool                                  |                       |     |            |            |             |               |                |
| Excavation                                       | Common                | m3  | 2,030      | 276        | 1,651       | 560,280       | 3,351,530      |
|  | Wearrock              | m3  | 14,210     | 339        | 1,398       | 4,817,190     | 19,865,350     |
|  | Rock                  | m3  | 24,360     | 962        | 3,475       | 23,434,320    | 84,651,000     |
|  | (Sub-total)           |     |            |            |             | 28,811,790    | 107,868,110    |
| SUB-TOTAL OF 4.                                  |                       |     |            |            |             | 717,225,140   | 6,792,287,017  |
| <b>5. OUTLET WORK</b>                            |                       |     |            |            |             |               |                |
| 5.1 Intake tower                                 |                       |     |            |            |             |               |                |
| Excavation                                       | Common                | m3  | 3,758      | 276        | 1,651       | 1,037,208     | 6,291,458      |
|  | Wearrock              | m3  | 4,176      | 339        | 1,398       | 1,415,664     | 5,834,018      |
|  | Rock                  | m3  | 418        | 962        | 3,475       | 402,116       | 1,452,550      |
|  | Concrete              | m3  | 500        | 13,442     | 132,187     | 6,721,000     | 66,093,500     |
|  | Rein bar              | t   | 20         | 5,292      | 1,460,955   | 105,840       | 29,219,100     |
|  | (Sub-total)           |     |            |            |             | 9,681,828     | 108,807,656    |
| 5.2 Intake shaft                                 |                       |     |            |            |             |               |                |
| Excavation                                       | Common                | m3  | 299        | 8,744      | 102,122     | 2,614,456     | 30,534,478     |
|  | Concrete              | m3  | 171        | 13,488     | 155,516     | 2,306,448     | 26,598,366     |
|  | Rein bar              | t   | 6          | 5,292      | 1,460,955   | 31,752        | 8,765,730      |
|  | (Sub-total)           |     |            |            |             | 4,952,656     | 65,898,574     |
| SUB-TOTAL OF 5.                                  |                       |     |            |            |             | 14,634,484    | 174,706,230    |
| <b>6. METAL WORK</b>                             |                       |     |            |            |             |               |                |
| 6.1 Diversion gate                               | Lr                    | 1   |            | 33,040,000 |             | 33,040,000    |                |
| 6.2 Steel cordvik                                | Lr                    | 1   |            |            | 808,500,000 |               | 808,500,000    |
| 6.3 Hollow jet valve                             | Lr                    | 1   |            | 45,000,000 |             | 45,000,000    |                |
| 6.4 Guard valve                                  | Lr                    | 1   |            | 22,500,000 |             | 22,500,000    |                |
| SUB-TOTAL OF 6.                                  |                       |     |            |            |             | 100,540,000   | 808,500,000    |
| <b>7. WATER SUPPLY PIPE LINE</b>                 |                       |     |            |            |             |               |                |
| 7.1 Excavation                                   | m3                    |     |            | 276        | 1,651       |               |                |
| 7.2 Backfill                                     | m3                    |     |            | 244        | 1,717       |               |                |
| 7.3 Add. pump station                            | Lr                    | 1   |            |            |             |               |                |
| 7.4 Add. purification plant                      | Lr                    | 1   |            |            |             |               |                |
| 7.5 Add. pipe line                               | Lr                    | 1   |            |            | 501,000,000 |               | 501,000,000    |
| 7.6 Add. intake & surge tank                     | Lr                    | 1   |            |            |             |               |                |
| SUB-TOTAL OF 7.                                  |                       |     |            |            |             |               | 501,000,000    |
| <b>TOTAL OF DIRECT CONSTRUCTION COST</b>         |                       |     |            |            |             | 2,251,061,562 | 17,368,619,875 |

Table F-24 Cost Estimate for Heightening of Krenceng Dam with Two Diversion Tunnels: Scheme D-2

| DESCRIPTION                                | Unit     | Qty | UNIT PRICE  |               | AMOUNT         |               |                |
|--|----------|-----|-------------|---------------|----------------|---------------|----------------|
|  |          |     | Fc<br>(Yen) | Lo<br>(Rp)    | Fc<br>(Yen)    | Lo<br>(Rp)    |                |
| <b>1. PREPARATORY WORK</b><br>(20% of 2+3) |          |     |             |               |                | 277,982,360   | 1,734,709,347  |
| <b>2. DIVERTED TUNNEL</b>                  |          |     |             |               |                |               |                |
| 2.1 Coffering work                         |          |     |             |               |                |               |                |
| Coffering                                  | Exca.    | m3  | 1,000       | 276           | 1,651          | 276,000       | 1,651,000      |
|  | Embank   | m3  | 1,000       | 441           | 1,144          | 441,000       | 1,144,000      |
| (Sub-total)                                |          |     |             |               |                | 717,000       | 2,795,000      |
| 2.2 Weir                                   |          |     |             |               |                |               |                |
| Excavation                                 | Common   | m3  | 1,200       | 276           | 1,651          | 331,200       | 1,981,200      |
|  | Wea.rock | m3  | 1,200       | 339           | 1,398          | 406,800       | 1,677,600      |
|  | Rock     | m3  | 600         | 962           | 3,475          | 577,200       | 2,085,000      |
| Concrete                                   |          | m3  | 410         | 5,052         | 118,708        | 2,071,320     | 48,670,280     |
| Rein bar                                   |          | t   | 41          | 5,292         | 1,460,955      | 216,972       | 59,899,155     |
| Gate                                       |          | Ls  | 2           | 2,000,000     |                | 4,000,000     |                |
| (Sub-total)                                |          |     |             |               |                | 7,603,492     | 114,313,235    |
| 2.3 Inlet & outlet                         |          |     |             |               |                |               |                |
| Excavation                                 | Common   | m3  | 4,576       | 276           | 1,651          | 1,262,976     | 7,554,976      |
|  | Wea.rock | m3  | 4,576       | 339           | 1,398          | 1,551,264     | 6,397,248      |
|  | Rock     | m3  | 2,288       | 962           | 3,475          | 2,201,056     | 7,950,800      |
| Concrete                                   |          | m3  | 200         | 13,442        | 132,187        | 2,688,400     | 26,437,400     |
| Rein bar                                   |          | t   | 40          | 5,292         | 1,460,955      | 211,680       | 58,438,200     |
| Trash rack                                 |          | Ls  | 2           | 1,000,000     |                | 2,000,000     |                |
| (Sub-total)                                |          |     |             |               |                | 9,915,376     | 106,778,624    |
| 2.4 Diverted tunnel                        |          |     |             |               |                |               |                |
| Excavation                                 |          | m3  | 5,320       | 8,744         | 105,122        | 46,518,080    | 559,249,040    |
| Lining conc.                               |          | m3  | 2,170       | 13,488        | 155,546        | 29,268,960    | 337,534,820    |
| Plug conc.                                 |          | m3  |             | 13,488        | 155,546        |               |                |
| Grouting                                   |          | t   | 1,200       | 6,500         | 90,000         | 7,800,000     | 108,000,000    |
| Rein bar                                   |          | t   | 76          | 5,292         | 1,460,955      | 402,192       | 111,032,580    |
| (Sub-total)                                |          |     |             |               |                | 83,989,232    | 1,115,816,440  |
| <b>SUB-TOTAL OF 2.</b>                     |          |     |             |               |                | 102,225,100   | 1,339,703,299  |
| <b>3. HEIGHTENING OF KRENCENG DAM</b>      |          |     |             |               |                |               |                |
| 3.1 Main dam                               |          |     |             |               |                |               |                |
| Excavation                                 | Common   | m3  | 146,652     | 276           | 1,651          | 40,475,952    | 242,122,452    |
|  | Wea.rock | m3  | 97,768      | 339           | 1,398          | 33,143,352    | 136,679,664    |
|  | Rock     | m3  |             | 962           | 3,475          |               |                |
| Embankment                                 | Core     | m3  | 1,281,085   | 605           | 2,359          | 775,056,425   | 3,022,079,515  |
|  | Filter   | m3  |             | 2,285         | 5,756          |               |                |
|  | Random   | m3  |             | 441           | 1,144          |               |                |
|  | Rock     | m3  |             | 1,514         | 5,964          |               |                |
| Grouting                                   | Blanket  | t   | 1,868       | 6,500         | 90,000         | 12,142,000    | 168,120,000    |
|  | Curtain  | t   | 3,676       | 6,500         | 90,000         | 23,894,000    | 330,840,000    |
| (Sub-total)                                |          |     |             |               |                | 884,711,729   | 3,899,841,631  |
| 3.2 Spillway                               |          |     |             |               |                |               |                |
| (1) Approach wall & weir                   |          |     |             |               |                |               |                |
| Excavation                                 | Common   | m3  | 3,097       | 276           | 1,651          | 854,772       | 5,113,147      |
|  | Wea.rock | m3  | 4,645       | 339           | 1,398          | 1,574,655     | 6,493,710      |
|  | Rock     | m3  |             | 962           | 3,475          |               |                |
| Concrete                                   |          | m3  | 6,628       | 13,442        | 132,187        | 89,093,576    | 876,135,436    |
| Rein bar                                   |          | t   | 135         | 5,292         | 1,460,955      | 714,420       | 197,228,925    |
| (2) Chute-way & basin                      |          |     |             |               |                |               |                |
| Excavation                                 | Common   | m3  | 11,879      | 276           | 1,651          | 3,278,604     | 19,612,229     |
|  | Wea.rock | m3  | 17,818      | 339           | 1,398          | 6,040,302     | 24,909,564     |
|  | Rock     | m3  |             | 962           | 3,475          |               |                |
| Concrete                                   |          | m3  | 14,260      | 13,442        | 132,187        | 191,682,920   | 1,884,986,620  |
| Rein bar                                   |          | t   | 285         | 5,292         | 1,460,955      | 1,508,220     | 416,372,175    |
| Grouting                                   | Consoli. | t   | 35          | 6,500         | 90,000         | 227,500       | 3,150,000      |
| (3) Metal work                             |          |     |             |               |                |               |                |
| Spillway gate                              |          | Ls  | 1           | 108,000,000   |                | 108,000,000   |                |
| (Sub-total)                                |          |     |             |               |                | 402,974,969   | 3,434,001,806  |
| <b>SUB-TOTAL OF 3.</b>                     |          |     |             |               |                | 1,287,686,698 | 7,333,843,437  |
| <b>4. WATER SUPPLY PIPE LINE</b>           |          |     |             |               |                |               |                |
| 4.1 Excavation                             |          | m3  |             | 276           | 1,651          |               |                |
| 4.2 Backfill                               |          | m3  |             | 244           | 1,717          |               |                |
| 4.3 Add. pump station                      |          | Ls  | 1           | 1,167,000,000 | 7,808,000,000  | 1,167,000,000 | 7,808,000,000  |
| 4.4 Add. purification plant                |          | Ls  | 1           | 1,812,000,000 | 12,118,000,000 | 1,812,000,000 | 12,118,000,000 |
| 4.5 Add. pipe line                         |          | Ls  |             |               | 1,540,000,000  |               |                |
| 4.6 Add. intake & surge tank               |          | Ls  | 1           | 80,000,000    | 2,914,000,000  | 80,000,000    | 2,914,000,000  |
| 4.7 Receiving well                         |          | Ls  | 1           | 6,000,000     | 218,400,000    | 6,000,000     | 218,400,000    |
| (Sub-total)                                |          |     |             |               |                | 3,065,000,000 | 23,058,400,000 |
| <b>SUB-TOTAL OF 4.</b>                     |          |     |             |               |                | 3,065,000,000 | 23,058,400,000 |
| <b>TOTAL OF DIRECT CONSTRUCTION COST</b>   |          |     |             |               |                | 4,732,894,158 | 33,466,656,083 |

Table F-25 Cost Estimate for Cidanau Gated Weir: Scheme D-3

| DESCRIPTION                                | Unit     | Q'ty | UNIT PRICE    |             | AMOUNT      |               |                |
|--|----------|------|---------------|-------------|-------------|---------------|----------------|
|  |          |      | Fe<br>(Yen)   | Lc<br>(Rp)  | Fe<br>(Yen) | Lc<br>(Rp)    |                |
| 1. PREPARATORY WORK<br>(20% of 2+3+4+5)    |          |      |               |             | 414,455,432 | 1,755,702,092 |                |
| 2. DIVERSION WORK                          |          |      |               |             |             |               |                |
| 2.1 Coffering work<br>Sheet pile & bracing | t        | 159  | 131,583       | 36,915      | 20,921,697  | 5,869,485     |                |
| SUB-TOTAL OF 2.                            |          |      |               |             | 20,921,697  | 5,869,485     |                |
| 3. DAM                                     |          |      |               |             |             |               |                |
| 3.1 Main dam                               |          |      |               |             |             |               |                |
| Excavation                                 | Common   | m3   | 10,662        | 276         | 1,651       | 2,942,712     | 17,602,962     |
|  | Wea.rock | m3   | 8,462         | 339         | 1,398       | 2,868,618     | 11,829,876     |
|  | Rock     | m3   | 2,200         | 962         | 3,475       | 2,116,400     | 7,645,000      |
| Concrete                                   |          | m3   | 21,325        | 5,052       | 118,708     | 107,733,900   | 2,531,448,100  |
| Grouting                                   | Consoli. | t    | 219           | 6,500       | 90,000      | 1,423,500     | 19,710,000     |
|  | Curtain  | t    | 352           | 6,500       | 90,000      | 2,288,000     | 31,680,000     |
| SUB-TOTAL OF 3.                            |          |      |               |             | 119,373,130 | 2,619,915,938 |                |
| 4. SPILLWAY                                |          |      |               |             |             |               |                |
| 4.1 Dental work                            |          |      |               |             |             |               |                |
| Excavation                                 | Common   | m3   | 22,389        | 276         | 1,651       | 6,179,364     | 36,964,239     |
|  | Wea.rock | m3   |               | 339         | 1,398       |               |                |
|  | Rock     | m3   |               | 962         | 3,475       |               |                |
| Concrete                                   |          | m3   | 8,379         | 5,052       | 118,708     | 42,330,708    | 994,654,332    |
| (Sub-total)                                |          |      |               |             |             | 48,510,072    | 1,031,618,571  |
| 4.2 Weir & pier                            |          |      |               |             |             |               |                |
| Excavation                                 | Common   | m3   |               | 276         | 1,651       |               |                |
|  | Wea.rock | m3   | 1,170         | 339         | 1,398       | 396,630       | 1,635,660      |
|  | Rock     | m3   | 500           | 962         | 3,475       | 481,000       | 1,737,500      |
| Concrete                                   |          | m3   | 10,761        | 13,442      | 132,187     | 144,649,362   | 1,422,464,307  |
| Rein bar                                   |          | t    | 1,290         | 5,292       | 1,460,955   | 6,826,680     | 1,884,631,950  |
| Grouting                                   | Consoli. | t    | 126           | 6,500       | 90,000      | 819,000       | 11,340,000     |
|  | Curtain  | t    | 180           | 6,500       | 90,000      | 1,170,000     | 16,200,000     |
| (Sub-total)                                |          |      |               |             |             | 154,342,672   | 3,338,009,417  |
| 4.3 Hoist & bridge                         |          |      |               |             |             |               |                |
| Concrete                                   |          | m3   | 2,871         | 13,442      | 132,187     | 38,591,982    | 379,508,877    |
| Rein bar                                   |          | t    | 574           | 5,292       | 1,460,955   | 3,037,608     | 838,588,170    |
| (Sub-total)                                |          |      |               |             |             | 41,629,590    | 1,218,097,047  |
| SUB-TOTAL OF 4.                            |          |      |               |             |             | 244,482,334   | 5,587,725,035  |
| 5. METAL WORK                              |          |      |               |             |             |               |                |
| 5.1 Roller gate                            | Ls       | 1    | 1,620,000,000 |             |             | 1,620,000,000 |                |
| 5.2 Steel conduit                          | Ls       | 1    |               | 565,000,000 |             |               | 565,000,000    |
| 5.3 Hollow jet valve                       | Ls       | 1    | 45,000,000    |             |             | 45,000,000    |                |
| 5.4 Guard valve                            | Ls       | 1    | 22,500,000    |             |             | 22,500,000    |                |
| SUB-TOTAL OF 5.                            |          |      |               |             |             | 1,687,500,000 | 565,000,000    |
| 6. WATER SUPPLY PIPE LINE                  |          |      |               |             |             |               |                |
| 6.1 Excavation                             |          | m3   |               | 276         | 1,651       |               |                |
| 6.2 Backfill                               |          | m3   |               | 244         | 1,717       |               |                |
| 6.3 Add. pump station                      |          | Ls   |               |             |             |               |                |
| 6.4 Add. purification plant                |          | Ls   |               |             |             |               |                |
| 6.5 Add. pipe line                         |          | Ls   |               |             |             |               |                |
| 6.6 Add. intake & surge tank               |          | Ls   |               |             |             |               |                |
| SUB-TOTAL OF 6.                            |          |      |               |             |             |               |                |
| TOTAL OF DIRECT CONSTRUCTION COST          |          |      |               |             |             | 2,486,732,593 | 10,534,212,550 |

Table F-26 Cost Estimate for Heightening of Krenceng Dam with Two Diversion Tunnels: Scheme D-3

| DESCRIPTION                                | Unit     | Q'ty | UNIT PRICE  |               | AMOUNT         |               |                |
|--|----------|------|-------------|---------------|----------------|---------------|----------------|
|  |          |      | Fc<br>(Yen) | Lc<br>(Rp)    | Fc<br>(Yen)    | Lc<br>(Rp)    |                |
| <b>1. PREPARATORY WORK</b><br>(20% of 2+3) |          |      |             |               |                | 277,982,360   | 1,734,709,347  |
| <b>2. DIVERTED TUNNEL</b>                  |          |      |             |               |                |               |                |
| 2.1 Coffering work                         |          |      |             |               |                |               |                |
| Coffering                                  | Exca.    | m3   | 1,000       | 276           | 1,651          | 276,000       | 1,651,000      |
|  | Embank   | m3   | 1,000       | 441           | 1,144          | 441,000       | 1,144,000      |
| (Sub-total)                                |          |      |             |               |                | 717,000       | 2,795,000      |
| 2.2 Weir                                   |          |      |             |               |                |               |                |
| Excavation                                 | Common   | m3   | 1,200       | 276           | 1,651          | 331,200       | 1,981,200      |
|  | Wea.rock | m3   | 1,200       | 339           | 1,398          | 406,800       | 1,677,600      |
|  | Rock     | m3   | 600         | 962           | 3,475          | 577,200       | 2,085,000      |
| Concrete                                   |          | m3   | 410         | 5,052         | 118,708        | 2,071,320     | 48,670,280     |
| Rein bar                                   |          | t    | 41          | 5,292         | 1,460,955      | 216,972       | 59,899,155     |
| Gate                                       |          | Ls   | 2           | 2,000,000     |                | 4,000,000     |                |
| (Sub-total)                                |          |      |             |               |                | 7,603,492     | 114,313,235    |
| 2.3 Inlet & outlet                         |          |      |             |               |                |               |                |
| Excavation                                 | Common   | m3   | 4,576       | 276           | 1,651          | 1,262,976     | 7,554,976      |
|  | Wea.rock | m3   | 4,576       | 339           | 1,398          | 1,551,264     | 6,397,248      |
|  | Rock     | m3   | 2,288       | 962           | 3,475          | 2,201,056     | 7,950,800      |
| Concrete                                   |          | m3   | 200         | 13,442        | 132,187        | 2,688,400     | 26,437,400     |
| Rein bar                                   |          | t    | 40          | 5,292         | 1,460,955      | 211,680       | 58,438,200     |
| Trash rack                                 |          | Ls   | 2           | 1,000,000     |                | 2,000,000     |                |
| (Sub-total)                                |          |      |             |               |                | 9,915,376     | 106,778,624    |
| 2.4 Diverted tunnel                        |          |      |             |               |                |               |                |
| Excavation                                 |          | m3   | 5,320       | 8,744         | 105,122        | 46,518,080    | 559,249,040    |
| Lining conc.                               |          | m3   | 2,170       | 13,488        | 155,546        | 29,268,960    | 337,534,820    |
| Plug conc.                                 |          | m3   |             | 13,488        | 155,546        |               |                |
| Grouting                                   |          | t    | 1,200       | 6,500         | 90,000         | 7,800,000     | 108,000,000    |
| Rein bar                                   |          | t    | 76          | 5,292         | 1,460,955      | 402,192       | 111,032,580    |
| (Sub-total)                                |          |      |             |               |                | 83,989,232    | 1,115,816,440  |
| <b>SUB-TOTAL OF 2.</b>                     |          |      |             |               |                | 102,225,100   | 1,339,703,299  |
| <b>3. HEIGHTENING OF KRENCENG DAM</b>      |          |      |             |               |                |               |                |
| 3.1 Main dam                               |          |      |             |               |                |               |                |
| Excavation                                 | Common   | m3   | 146,652     | 276           | 1,651          | 40,475,952    | 242,122,452    |
|  | Wea.rock | m3   | 97,768      | 339           | 1,398          | 33,143,352    | 136,679,664    |
|  | Rock     | m3   |             | 962           | 3,475          |               |                |
| Embankment                                 | Core     | m3   | 1,281,085   | 605           | 2,359          | 775,056,425   | 3,022,079,515  |
|  | Filter   | m3   |             | 2,285         | 5,756          |               |                |
|  | Random   | m3   |             | 441           | 1,144          |               |                |
|  | Rock     | m3   |             | 1,514         | 5,964          |               |                |
| Grouting                                   | Blanket  | t    | 1,868       | 6,500         | 90,000         | 12,142,000    | 168,120,000    |
|  | Curtain  | t    | 3,676       | 6,500         | 90,000         | 23,894,000    | 330,840,000    |
| (Sub-total)                                |          |      |             |               |                | 884,711,729   | 3,899,841,631  |
| 3.2 Spillway                               |          |      |             |               |                |               |                |
| (1) Approach wall & weir                   |          |      |             |               |                |               |                |
| Excavation                                 | Common   | m3   | 3,097       | 276           | 1,651          | 854,772       | 5,113,147      |
|  | Wea.rock | m3   | 4,645       | 339           | 1,398          | 1,574,655     | 6,493,710      |
|  | Rock     | m3   |             | 962           | 3,475          |               |                |
| Concrete                                   |          | m3   | 6,628       | 13,442        | 132,187        | 89,093,576    | 876,135,436    |
| Rein bar                                   |          | t    | 135         | 5,292         | 1,460,955      | 714,420       | 197,228,925    |
| (2) Chute way & basin                      |          |      |             |               |                |               |                |
| Excavation                                 | Common   | m3   | 11,879      | 276           | 1,651          | 3,278,604     | 19,612,229     |
|  | Wea.rock | m3   | 17,818      | 339           | 1,398          | 6,040,302     | 24,909,564     |
|  | Rock     | m3   |             | 962           | 3,475          |               |                |
| Concrete                                   |          | m3   | 14,260      | 13,442        | 132,187        | 191,682,920   | 1,884,986,620  |
| Rein bar                                   |          | t    | 285         | 5,292         | 1,460,955      | 1,508,220     | 416,372,175    |
| Grouting                                   | Consoli. | t    | 35          | 6,500         | 90,000         | 227,500       | 3,150,000      |
| (3) Metal work                             |          |      |             |               |                |               |                |
| Spillway gate                              |          | Ls   | 1           | 108,000,000   |                | 108,000,000   |                |
| (Sub-total)                                |          |      |             |               |                | 402,974,969   | 3,434,001,806  |
| <b>SUB-TOTAL OF 3.</b>                     |          |      |             |               |                | 1,287,686,698 | 7,333,843,437  |
| <b>4. WATER SUPPLY PIPE LINE</b>           |          |      |             |               |                |               |                |
| 4.1 Excavation                             |          | m3   |             | 276           | 1,651          |               |                |
| 4.2 Backfill                               |          | m3   |             | 244           | 1,717          |               |                |
| 4.3 Add. pump station                      |          | Ls   | 1           | 1,208,000,000 | 8,080,000,000  | 1,208,000,000 | 8,080,000,000  |
| 4.4 Add. purification plant                |          | Ls   | 1           | 1,931,000,000 | 12,916,000,000 | 1,931,000,000 | 12,916,000,000 |
| 4.5 Add. pipe line                         |          | Ls   |             |               | 1,540,000,000  |               |                |
| 4.6 Add. intake & surge tank               |          | Ls   | 1           | 84,000,000    | 3,084,000,000  | 84,000,000    | 3,084,000,000  |
| 4.7 Receiving well                         |          | Ls   | 1           | 6,000,000     | 218,400,000    | 6,000,000     | 218,400,000    |
| <b>SUB-TOTAL OF 4.</b>                     |          |      |             |               |                | 3,229,000,000 | 24,298,400,000 |
| <b>TOTAL OF DIRECT CONSTRUCTION COST</b>   |          |      |             |               |                | 4,896,894,158 | 34,706,656,083 |



Table F-27 Economic Cost and Economic Evaluation for Alternative Single Development Schemes

(Unit : Million)

| Description                                 | Scheme  |         |        |         |         |         |       |        |       |        |       |        |
|---|---------|---------|--------|---------|---------|---------|-------|--------|-------|--------|-------|--------|
|   | A-1     |         | A-3    |         | A-6     |         | K-1   |        | K-2   |        | K-3   |        |
|   | F/C*5   | L/C*6   | F/C    | L/C     | F/C     | L/C     | F/C   | L/C    | F/C   | L/C    | F/C   | L/C    |
| 1) Direct Const. cost                       | 3,473   | 62,317  | 2,345  | 18,000  | 2,792   | 13,529  | 4,021 | 27,420 | 4,147 | 28,609 | 4,318 | 30,334 |
| Dam and related facility                    | 2,780   | 17,654  | 2,251  | 16,865  | 2,487   | 10,534  | 1,545 | 8,801  | 1,585 | 9,336  | 1,668 | 10,408 |
| Water transmission facility                 | 693     | 44,663  | 94     | 1,135   | 305     | 2,995   | 2,476 | 18,619 | 2,562 | 19,272 | 2,650 | 19,925 |
| 2) Land acquisition cost                    | 0       | 210     | 0      | 12      | 0       | 28      | 0     | 3,722  | 0     | 3,722  | 0     | 3,722  |
| 3) Administration *1                        | 0       | 6,253   | 0      | 1,801   | 0       | 1,356   | 0     | 3,114  | 0     | 3,233  | 0     | 3,406  |
| 4) Engineering Services *2                  | 521     | 3,116   | 352    | 900     | 419     | 676     | 603   | 1,371  | 622   | 1,430  | 648   | 1,517  |
| 5) Physical contingency *3                  | 599     | 10,753  | 405    | 3,105   | 482     | 2,334   | 694   | 4,786  | 715   | 4,991  | 745   | 5,288  |
| 6) Grand Total                              | 4,593   | 82,649  | 3,101  | 22,818  | 3,692   | 17,924  | 5,318 | 40,413 | 5,484 | 41,985 | 5,710 | 44,266 |
| (Rp) *4                                     | 154,300 | 72,199  | 75,520 | 123,375 | 127,542 | 133,348 |       |        |       |        |       |        |
| 7) Economic cost *7                         | 138,681 | 64,968  | 67,943 | 107,688 | 111,439 | 116,664 |       |        |       |        |       |        |
| 8) Capitalized cost *8                      | 106,165 | 48,612  | 51,116 | 96,189  | 98,398  | 101,167 |       |        |       |        |       |        |
| 9) Capitalized benefit *8                   | 97,024  | 19,405  | 50,668 | 243,637 | 254,418 | 265,198 |       |        |       |        |       |        |
| 10) Net benefit                             | -9,141  | -29,208 | -448   | 147,449 | 156,019 | 164,031 |       |        |       |        |       |        |
| 11) Benefit cost ratio                      | 0.91    | 0.40    | 0.99   | 2.53    | 2.59    | 2.62    |       |        |       |        |       |        |
| 12) Economic internal rate of return (EIRR) | 11.16   | 5.22    | 11.92  | 24.02   | 24.22   | 24.26   |       |        |       |        |       |        |

Note : \*1 F/C 0%, LC 10% of 1) + 2)

\*2 F/C 15%, LC 5% of 1)

\*3 F/C 15%, LC 15% of 1) + 3) + 4)

\*4 Y1 = Rp.15.6

\*5 F/C: Japanese Yen

\*6 L/C: Rupiah

\*7 Conversion factor : 0.9 / Excluded land acquisition cost

\*8 Capitalized by discount rate of 12%

Excluded Land acquisition cost

Table F-28 Economic Cost and Economic Evaluation for Alternative Combined Development Schemes

(Unit: Million)

| Description                                 | Scheme  |         |         |        |         |        |         |         |         |        |         |        |         |         |         |        |         |        |
|---|---------|---------|---------|--------|---------|--------|---------|---------|---------|--------|---------|--------|---------|---------|---------|--------|---------|--------|
|   | B-1     |         | B-2     |        | B-3     |        | C-1     |         | C-2     |        | C-3     |        | D-1     |         | D-2     |        | D-3     |        |
|   | F/C     | L/C     | F/C     | L/C    | F/C     | L/C    | F/C     | L/C     | F/C     | L/C    | F/C     | L/C    | F/C     | L/C     | F/C     | L/C    | F/C     | L/C    |
| 1) Direct Const. cost                       | 7,007   | 85,977  | 6,774   | 48,576 | 7,097   | 42,393 | 7,134   | 87,165  | 6,901   | 49,763 | 7,224   | 43,381 | 7,504   | 88,889  | 6,984   | 50,853 | 7,384   | 45,241 |
| Dam and related facility                    | 4,330   | 26,485  | 3,796   | 25,665 | 4,032   | 19,335 | 4,270   | 27,020  | 3,836   | 26,201 | 4,072   | 19,870 | 4,453   | 28,092  | 3,919   | 27,273 | 4,155   | 20,942 |
| Water transmission facility                 | 2,677   | 59,492  | 2,978   | 22,910 | 3,065   | 23,058 | 2,764   | 60,145  | 3,065   | 23,562 | 3,152   | 23,710 | 2,851   | 60,797  | 3,065   | 23,562 | 3,229   | 24,298 |
| 2) Land acquisition cost                    | 0       | 5,372   | 0       | 5,174  | 0       | 5,190  | 0       | 5,362   | 0       | 5,174  | 0       | 5,190  | 0       | 5,372   | 0       | 5,174  | 0       | 5,190  |
| 3) Administration *1                        | 0       | 9,135   | 0       | 5,375  | 0       | 4,758  | 0       | 9,253   | 0       | 5,494  | 0       | 4,877  | 0       | 9,426   | 0       | 5,601  | 0       | 5,043  |
| 4) Engineering Services *2                  | 1,051   | 4,299   | 1,016   | 2,429  | 1,065   | 2,120  | 1,070   | 4,358   | 1,035   | 2,488  | 1,084   | 2,179  | 1,096   | 4,444   | 1,048   | 2,542  | 1,108   | 2,262  |
| 5) Physical contingency *3                  | 1,209   | 14,912  | 1,169   | 8,457  | 1,224   | 7,391  | 1,231   | 15,116  | 1,190   | 8,662  | 1,246   | 7,596  | 1,260   | 15,414  | 1,205   | 8,847  | 1,274   | 7,882  |
| 6) Grand Total                              | 9,267   | 119,693 | 8,959   | 70,010 | 9,386   | 61,852 | 9,435   | 121,254 | 9,127   | 71,361 | 9,553   | 63,422 | 9,659   | 123,545 | 9,256   | 72,998 | 9,765   | 65,618 |
| (Rp) *4                                     | 264,259 |         | 209,770 |        | 208,269 |        | 268,436 |         | 213,957 |        | 268,436 |        | 274,231 |         | 217,084 |        | 274,231 |        |
| 7) Economic cost *7                         | 232,998 |         | 184,137 |        | 182,771 |        | 236,767 |         | 187,905 |        | 186,540 |        | 241,974 |         | 190,720 |        | 241,974 |        |
| 8) Capitalized cost *8                      | 192,065 |         | 156,747 |        | 153,174 |        | 194,280 |         | 156,491 |        | 155,149 |        | 197,046 |         | 157,051 |        | 197,046 |        |
| 9) Capitalized benefit *8                   | 330,235 |         | 305,286 |        | 313,873 |        | 334,925 |         | 313,873 |        | 321,535 |        | 343,026 |         | 321,535 |        | 328,184 |        |
| 10) Net benefit                             | 138,170 |         | 148,539 |        | 160,699 |        | 142,635 |         | 157,382 |        | 166,386 |        | 145,980 |         | 164,484 |        | 170,905 |        |
| 11) Benefit cost ratio                      | 1.72    |         | 1.95    |        | 2.05    |        | 1.73    |         | 2.01    |        | 2.07    |        | 1.74    |         | 2.05    |        | 2.09    |        |
| 12) Economic internal rate of return (EIRR) | 18.00   |         | 19.01   |        | 20.60   |        | 18.04   |         | 20.22   |        | 20.54   |        | 18.00   |         | 20.36   |        | 20.58   |        |

Note: \*1 F/C 0%, L/C 10% of (1) + 2)  
 \*2 F/C 15%, L/C 5% of (1)  
 \*3 F/C 15%, L/C 15% of (1) + 3) + 4)  
 \*4 V1 = Rp.15.6  
 \*5 F/C: Japanese Yen  
 \*6 L/C: Rupiah  
 \*7 Conversion factor: 0.9 / Excluded land acquisition cost  
 \*8 Capitalized by discount rate of 12%

Table F-29 Water Conveyance and Treatment Facilities for Alternative Development Scale of Heightening of Krenceng Dam

|                                    | Alternative                              |  |  |
|------------------------------------|--|--|--|
|                                    | H-1                                      | H-2  | H-3                                      |
| Required Additional Pump Capacity* | 1.10 m <sup>3</sup> /s                   | 0.65 m <sup>3</sup> /s                     | 0.105 m <sup>3</sup> /s                  |
| Intake Facilities (Cidanau)        |  |  |  |
| Intake*                            | L = 40 m<br>B = 2.0 m H = 2.2 m          | L = 40 m<br>B = 1.0 m H = 2.2 m            | -  |
| Sand trap basin*                   | L = 80 m<br>B = 6.5 m H = 3.0 m          | L = 80 m<br>B = 4 m H = 3.0 m              | -  |
| Water Conveyance Facilities        |  |  |  |
| Cidanau Pump station*              | 0.55 m <sup>3</sup> /s x 2 units         | 0.33 m <sup>3</sup> /s x 2 units           | 0.105 m <sup>3</sup> /s x 1 unit         |
| Booster pump station*              | 1.03 m <sup>3</sup> /s x 4 <sup>1)</sup> | 0.88 x m <sup>3</sup> /s x 4 <sup>1)</sup> | 0.70 m <sup>3</sup> /s x 4 <sup>1)</sup> |
| Surge tank                         | 2 units                                  | 2 units                                    | 1 unit                                   |
| Purification Facilities            |  |  |  |
| Pump station**                     | 1.03 m <sup>3</sup> /s x 4 <sup>1)</sup> | 0.88 m <sup>3</sup> /s x 4 <sup>1)</sup>   | 0.105 m <sup>3</sup> /s x 1              |
| Receiving well**                   | Replaced                                 | Replaced                                   | Replaced                                 |
| Water purification plant**         | 1.10 m <sup>3</sup> /s                   | 0.65 m <sup>3</sup> /s                     | 0.105 m <sup>3</sup> /s                  |

Note: 1) included one standby.  
\* additional facilities  
\*\* replaced facilities

Table F-30 Water Conveyance and Treatment Facilities for  
Alternative Development Scale of Cidanau Gated Weir

|                                    | Alternative                      |                                  |
|------------------------------------|----------------------------------|----------------------------------|
|                                    | M-1                              | M-2                              |
| Required Additional Pump Capacity* | 0.205 m <sup>3</sup> /s          | 0                                |
| Intake Facilities (Cidanau)        |                                  |                                  |
| Intake*                            | -                                | -                                |
| Sand trap basin*                   | -                                | -                                |
| Pump station*                      | -                                | -                                |
| Conveyance Facilities              |                                  |                                  |
| Booster pump station*              | -                                | -                                |
| Surge tank                         | -                                | -                                |
| Purification Facilities            |                                  |                                  |
| Pump station*                      | 0.205 m <sup>3</sup> /s x 1 unit | 0.015 m <sup>3</sup> /s x 1 unit |
| Receiving well                     | -                                | -                                |
| Water purification plant           | 0.205 m <sup>3</sup> /s          | 0.015 m <sup>3</sup> /s          |

Note: \* additional facilities

Table F-31 Five (5)-day Mean Inflow Discharge at Existing Cidanau Weir Site

|      |              | (Unit: m <sup>3</sup> /sec) |       |       |       |       |       |       |       |       |       |        |       |       |
|------|--------------|-----------------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|--------|-------|-------|
| Year | Period (day) | Jan.                        | Feb.  | Mar.  | Apr.  | May   | Jun.  | Jul.  | Aug.  | Sep.  | Oct.  | Nov.   | Dec.  | Mean  |
| 1980 | 1st - 5th    | 9.02                        | 7.63  | 10.49 | 5.16  | 1.9   | 8.89  | 3.78  | 5.07  | 6.12  | 1.98  | 21.75  | 64.63 | 12.20 |
|      | 6th - 10th   | 9.22                        | 11.72 | 7.95  | 4.09  | 0.42  | 10.17 | 6.52  | 10.38 | 62.58 | 1.47  | 25.6   | 73.43 | 18.63 |
|      | 11th - 15th  | 9.38                        | 11.6  | 32.45 | 15.05 | 2.04  | 4.36  | 6.51  | 15.84 | 66.5  | 5.88  | 31.05  | 75.87 | 23.04 |
|      | 16th - 20th  | 9.07                        | 11.72 | 22.15 | 11.21 | 4.42  | 7.34  | 10.99 | 29.73 | 28.67 | 14.2  | 35.87  | 97.76 | 23.59 |
|      | 21st - 25th  | 9.02                        | 11.78 | 5.29  | 7.57  | 12.4  | 8.74  | 6.11  | 12.25 | 5.73  | 15.9  | 42.38  | 68.39 | 17.13 |
|      | 26th - 31st  | 6.86                        | 14.65 | 3.35  | 4.61  | 9.63  | 5.49  | 5.29  | 4.09  | 3.78  | 19.05 | 49.61  | 91.21 | 18.14 |
| 1981 | 1st - 5th    | 143.78                      | 42.67 | 28.32 | 28.78 | 14.89 | 6.52  | 9.97  | 18.6  | 5.04  | 96.83 | 10.68  | 29.59 | 36.31 |
|      | 6th - 10th   | 167.61                      | 49.8  | 4.05  | 28.48 | 10.24 | 8.54  | 2.94  | 7.15  | 15.09 | 33.15 | 9.34   | 26.9  | 30.27 |
|      | 11th - 15th  | 66.59                       | 32.67 | 5.24  | 26.98 | 6.84  | 11.8  | 6.44  | 5.13  | 16.4  | 11.46 | 56.21  | 19.97 | 22.14 |
|      | 16th - 20th  | 70.21                       | 24.47 | 8.51  | 23.48 | 10.07 | 22    | 12.86 | 3.65  | 3.8   | 8.17  | 157.94 | 7.96  | 29.43 |
|      | 21st - 25th  | 32.2                        | 4.33  | 5.41  | 20.12 | 7.49  | 9.99  | 17.02 | 8.72  | 2.63  | 4.25  | 60.02  | 13.4  | 15.46 |
|      | 26th - 31st  | 33.02                       | 43.04 | 22.74 | 18.03 | 2.12  | 9.78  | 22.06 | 10.29 | 22.8  | 20.99 | 21.64  | 72.94 | 24.95 |
| 1982 | 1st - 5th    | 49.48                       | 6.42  | 21.14 | 24.15 | 12.58 | 5.62  | 3.25  | 3.88  | 1.95  | 2.92  | 1.13   | 3.15  | 11.31 |
|      | 6th - 10th   | 26.97                       | 2.63  | 73.45 | 24.62 | 8.29  | 8.78  | 2.95  | 2.95  | 1.33  | 1.29  | 12.36  | 0.98  | 13.88 |
|      | 11th - 15th  | 10.12                       | 4     | 29.24 | 16.71 | 7.78  | 5.92  | 2.88  | 1.89  | 1.23  | 0.84  | 3.98   | 5.15  | 7.48  |
|      | 16th - 20th  | 41.99                       | 3.63  | 39.29 | 40.02 | 4.48  | 5.88  | 4.14  | 1.61  | 1.05  | 2.22  | 1.8    | 6.45  | 12.71 |
|      | 21st - 25th  | 36.65                       | 7.71  | 56.8  | 12.54 | 3.94  | 4.37  | 5.11  | 1.31  | 2.22  | 2.17  | 6.13   | 6.78  | 12.14 |
|      | 26th - 31st  | 7.07                        | 10.93 | 15.69 | 17.23 | 4.46  | 3     | 9.21  | 1.03  | 2.48  | 1.22  | 5.88   | 16.55 | 7.90  |
| 1983 | 1st - 5th    | 15.68                       | 18.28 | 12.53 | 11.42 | 4.78  | 9.32  | 18.42 | 3.31  | 1.14  | 0.87  | 16.39  | 44.79 | 13.08 |
|      | 6th - 10th   | 16.16                       | 21.76 | 6.29  | 10.11 | 4.7   | 7.94  | 11.4  | 1.57  | 1.76  | 0.67  | 13.21  | 23.81 | 9.95  |
|      | 11th - 15th  | 14.29                       | 6     | 5.37  | 8.8   | 14.13 | 6.23  | 5.87  | 2.78  | 1.96  | 0.75  | 17.05  | 10.13 | 7.78  |
|      | 16th - 20th  | 25.58                       | 6.53  | 4.6   | 10.47 | 7.12  | 9.07  | 7.77  | 3.44  | 1.63  | 0.85  | 90.38  | 10.25 | 14.81 |
|      | 21st - 25th  | 46.39                       | 7.22  | 4.57  | 8.87  | 9.33  | 11.23 | 5.69  | 9.1   | 1.63  | 5.81  | 1.49   | 8.64  | 10.00 |
|      | 26th - 31st  | 26.34                       | 9.6   | 6.81  | 10.93 | 6     | 11.91 | 6.5   | 2.04  | 1.25  | 12.64 | 50.62  | 13.61 | 13.19 |
| 1984 | 1st - 5th    | 13.13                       | 17.21 | 13.6  | 27.51 | 13.54 | 14.43 | 5.3   | 5.79  | 3.86  | 24.07 | 3.73   | 46.23 | 15.70 |
|      | 6th - 10th   | 3.19                        | 28.98 | 24.73 | 6.62  | 24.73 | 8.04  | 11.33 | 4.46  | 11.56 | 10.2  | 6.39   | 44.47 | 15.39 |
|      | 11th - 15th  | 14.45                       | 13.05 | 29.99 | 8.87  | 36.17 | 7.25  | 7.62  | 3.43  | 14.49 | 4.69  | 11.28  | 18.37 | 14.14 |
|      | 16th - 20th  | 16.08                       | 9.61  | 24.88 | 7.79  | 13.42 | 6.04  | 4.98  | 3.5   | 11.67 | 5.54  | 11.43  | 16.23 | 10.93 |
|      | 21st - 25th  | 16.33                       | 6.64  | 44.2  | 10.14 | 9.18  | 7.22  | 6.4   | 3.24  | 10.14 | 5.35  | 8.25   | 7.7   | 11.23 |
|      | 26th - 31st  | 18.98                       | 17.45 | 50.95 | 15.02 | 24.37 | 3.22  | 7.21  | 4.19  | 8.05  | 6.53  | 8.69   | 33.45 | 16.51 |
| 1985 | 1st - 5th    | 21.96                       | 11.95 | 13.08 | 4.25  | 15.15 | 5.23  | 4.75  | 12.42 | 2.74  | 4.04  | 9.46   | 33.72 | 11.56 |
|      | 6th - 10th   | 19.4                        | 11.84 | 42.17 | 5.48  | 11.79 | 4.76  | 4.82  | 12.07 | 2.78  | 6.16  | 8.98   | 28.56 | 13.23 |
|      | 11th - 15th  | 37.45                       | 14.6  | 32.83 | 10.57 | 9.33  | 5.76  | 5.32  | 7.34  | 10.2  | 13.03 | 9.98   | 9.68  | 13.84 |
|      | 16th - 20th  | 12.81                       | 7.56  | 11.11 | 21.81 | 7.82  | 7.11  | 5.69  | 6.28  | 7.87  | 16.73 | 6.94   | 4.41  | 9.68  |
|      | 21st - 25th  | 8.72                        | 13.14 | 6.93  | 15.98 | 8.38  | 7.34  | 13.79 | 4.77  | 5.53  | 21.81 | 8.6    | 4.08  | 9.92  |
|      | 26th - 31st  | 13.47                       | 14.16 | 5.11  | 17.61 | 6.73  | 6.71  | 15.19 | 3.51  | 5.15  | 10.44 | 15.24  | 4.25  | 9.80  |
| 1986 | 1st - 5th    | 15.11                       | 28.46 | 11.96 | 24.45 | 12.69 | 5.92  | 2.81  | 6.07  | 1.89  | 7.88  | 21.24  | 11.94 | 12.54 |
|      | 6th - 10th   | 48.59                       | 18.48 | 10.04 | 24.03 | 9.79  | 5.33  | 3.19  | 7.26  | 3.09  | 5.27  | 32.92  | 4.67  | 14.41 |
|      | 11th - 15th  | 51.29                       | 24.43 | 8.07  | 18.98 | 9.8   | 5.06  | 4.65  | 8.59  | 5.97  | 8.81  | 53.45  | 14.23 | 17.78 |
|      | 16th - 20th  | 26.19                       | 20.85 | 6.83  | 17.98 | 9.4   | 5.17  | 3.21  | 5.66  | 6.65  | 9.6   | 23.06  | 22.26 | 13.07 |
|      | 21st - 25th  | 53.9                        | 17.23 | 29.23 | 11.07 | 5.97  | 5.94  | 2.49  | 2.89  | 6.82  | 6.08  | 9.45   | 11.96 | 13.59 |
|      | 26th - 31st  | 51.05                       | 13.74 | 53.76 | 8.67  | 5.28  | 3.66  | 4.93  | 2.31  | 9.29  | 15.9  | 12.24  | 7.32  | 15.68 |
| 1987 | 1st - 5th    | 11.51                       | 17.83 | 36.37 | 11.65 | 22.55 | 6.91  | 5.4   | 2.92  | 1.22  | 1.16  | 1.54   | 1.95  | 10.08 |
|      | 6th - 10th   | 44.13                       | 28.18 | 36.32 | 15.09 | 17.38 | 7.01  | 4.13  | 2.14  | 1.13  | 1.13  | 2.66   | 3.34  | 13.55 |
|      | 11th - 15th  | 61.24                       | 25.46 | 19.54 | 16.16 | 19.87 | 7.63  | 3.32  | 2.36  | 1.13  | 2.81  | 5.79   | 7.32  | 14.39 |
|      | 16th - 20th  | 34.2                        | 20.36 | 8.49  | 15.64 | 16.83 | 7.59  | 2.46  | 1.82  | 1.13  | 2.15  | 5.31   | 9.12  | 10.43 |
|      | 21st - 25th  | 21.03                       | 42.99 | 10.47 | 6.91  | 8.75  | 6.91  | 2.56  | 1.53  | 1.13  | 2.53  | 3.29   | 13.2  | 10.11 |
|      | 26th - 31st  | 20.56                       | 44.32 | 10.85 | 11.22 | 7.99  | 6.1   | 3.17  | 1.28  | 1.13  | 1.55  | 2      | 7.33  | 9.79  |
| 1988 | 1st - 5th    | 3.34                        | 38.29 | 15.24 | 47.82 | 17.99 | 7.23  | 4.65  | 2.39  | 2.01  | 3.32  | 8.32   | 33.61 | 15.35 |
|      | 6th - 10th   | 1.79                        | 48.05 | 24.94 | 23.5  | 19.95 | 13.23 | 3.18  | 4.39  | 2.65  | 2.67  | 10.41  | 21.84 | 14.72 |
|      | 11th - 15th  | 1.96                        | 34.22 | 15.25 | 16.91 | 15.6  | 14.51 | 2.11  | 3.48  | 3.47  | 2.61  | 13.72  | 31.22 | 12.92 |
|      | 16th - 20th  | 4.87                        | 50.13 | 14.61 | 16.79 | 21.4  | 12.64 | 2.49  | 3.21  | 3.06  | 4.65  | 12.61  | 58.7  | 17.10 |
|      | 21st - 25th  | 7.52                        | 25.29 | 16.7  | 19.45 | 17.94 | 10.34 | 2.14  | 3.43  | 3     | 5.25  | 18.37  | 28.63 | 13.17 |
|      | 26th - 31st  | 15.99                       | 7.87  | 22.49 | 14.13 | 8.59  | 7.25  | 2.22  | 2.23  | 2.89  | 4.98  | 31.08  | 14.3  | 11.17 |
| 1989 | 1st - 5th    | 10.35                       | 9.84  | 57.46 | 7.82  | 7.82  | 7.63  | 3.17  | 2.67  | 3.89  | 3.17  | 3.88   | 5.28  | 10.25 |
|      | 6th - 10th   | 7.94                        | 36.72 | 39.68 | 7.82  | 7.82  | 9.29  | 6.28  | 1.79  | 2.39  | 2.67  | 3.33   | 6.51  | 11.02 |
|      | 11th - 15th  | 6.52                        | 24.09 | 21.83 | 7.82  | 7.82  | 9.3   | 10.52 | 2.26  | 4.34  | 2.19  | 5.15   | 9.45  | 9.27  |
|      | 16th - 20th  | 8.52                        | 74.81 | 18.76 | 7.82  | 7.82  | 6.35  | 12.33 | 1.44  | 5.45  | 1.89  | 4.85   | 10.6  | 13.39 |
|      | 21st - 25th  | 9.03                        | 30.83 | 10.8  | 7.82  | 7.82  | 3.75  | 8.72  | 1.63  | 3.54  | 2.01  | 5.35   | 9.9   | 8.43  |
|      | 26th - 31st  | 7.36                        | 82.69 | 7.54  | 7.82  | 7.82  | 3.24  | 4.44  | 2.46  | 1.93  | 4.69  | 4.05   | 10.03 | 12.01 |
| Mean |              | 26.71                       | 21.70 | 20.64 | 15.14 | 10.76 | 7.74  | 6.51  | 5.22  | 7.20  | 8.32  | 19.09  | 23.30 | 14.36 |

Table F-32 Five (5)-day Mean Inflow Discharge at Krenceng Dam Site

|      |              | (Unit: m <sup>3</sup> /sec) |      |      |      |      |      |      |      |      |      |      |      |      |
|------|--------------|-----------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Year | Period (day) | Jan.                        | Feb. | Mar. | Apr. | May  | Jun. | Jul. | Aug. | Sep. | Oct. | Nov. | Dec. | Mean |
| 1980 | 1st - 5th    | 0.27                        | 0.43 | 0.34 | 0.14 | 0.25 | 0.26 | 0.09 | 0.27 | 0.53 | 0.25 | 0.41 | 0.11 | 0.28 |
|      | 6th - 10th   | 0.46                        | 1.11 | 0.53 | 0.15 | 0.22 | 0.13 | 0.09 | 0.43 | 0.46 | 0.28 | 0.23 | 0.15 | 0.35 |
|      | 11th - 15th  | 0.68                        | 1.14 | 0.36 | 0.66 | 0.25 | 0.17 | 0.1  | 0.66 | 0.74 | 0.28 | 0.29 | 0.12 | 0.45 |
|      | 16th - 20th  | 0.67                        | 1.8  | 0.38 | 0.23 | 0.24 | 0.11 | 0.12 | 0.87 | 0.26 | 0.19 | 0.73 | 0.41 | 0.50 |
|      | 21st - 25th  | 0.67                        | 1.07 | 0.16 | 0.39 | 0.17 | 0.14 | 0.11 | 0.12 | 0.18 | 0.28 | 0.17 | 1.23 | 0.39 |
|      | 26th - 31st  | 0.76                        | 0.54 | 0.21 | 0.25 | 0.12 | 0.12 | 0.12 | 0.1  | 0.33 | 0.22 | 0.15 | 1.23 | 0.35 |
| 1981 | 1st - 5th    | 3.96                        | 0.92 | 1.52 | 0.32 | 0.49 | 0.15 | 0.14 | 0.38 | 0.42 | 0.77 | 0.32 | 0.71 | 0.84 |
|      | 6th - 10th   | 2.72                        | 0.81 | 0.77 | 0.37 | 0.38 | 0.13 | 0.13 | 0.4  | 0.39 | 0.77 | 0.64 | 0.46 | 0.66 |
|      | 11th - 15th  | 1.65                        | 1.19 | 1.18 | 0.22 | 0.48 | 0.28 | 0.49 | 0.24 | 1.09 | 0.59 | 0.97 | 0.39 | 0.73 |
|      | 16th - 20th  | 0.96                        | 1.19 | 0.74 | 0.31 | 0.67 | 0.47 | 0.74 | 0.34 | 0.26 | 0.25 | 2.28 | 0.39 | 0.72 |
|      | 21st - 25th  | 0.68                        | 1.07 | 0.39 | 0.32 | 0.25 | 0.21 | 0.82 | 0.34 | 0.23 | 0.28 | 0.4  | 0.78 | 0.48 |
|      | 26th - 31st  | 0.95                        | 2.88 | 0.6  | 0.24 | 0.19 | 0.27 | 1.29 | 0.23 | 0.36 | 0.42 | 1.07 | 1.49 | 0.83 |
| 1982 | 1st - 5th    | 0.9                         | 1.1  | 0.68 | 0.64 | 0.55 | 0.57 | 0.19 | 0.25 | 0.11 | 0.15 | 0.09 | 0.1  | 0.44 |
|      | 6th - 10th   | 2.07                        | 0.52 | 0.86 | 0.52 | 0.49 | 0.43 | 0.15 | 0.19 | 0.11 | 0.1  | 0.15 | 0.09 | 0.47 |
|      | 11th - 15th  | 3.25                        | 0.67 | 1.4  | 0.49 | 0.38 | 0.31 | 0.15 | 0.09 | 0.1  | 0.1  | 0.14 | 0.1  | 0.60 |
|      | 16th - 20th  | 2.09                        | 0.51 | 1.36 | 0.8  | 0.26 | 0.26 | 0.38 | 0.07 | 0.1  | 0.23 | 0.14 | 0.1  | 0.53 |
|      | 21st - 25th  | 1.49                        | 0.41 | 1.02 | 0.53 | 0.26 | 0.17 | 0.4  | 0.05 | 0.09 | 0.11 | 0.14 | 0.11 | 0.40 |
|      | 26th - 31st  | 1.06                        | 0.5  | 0.8  | 0.76 | 0.32 | 0.26 | 0.39 | 0.04 | 0.12 | 0.1  | 0.13 | 0.24 | 0.39 |
| 1983 | 1st - 5th    | 0.43                        | 0.5  | 1    | 0.43 | 0.58 | 0.34 | 0.36 | 0.05 | 0.01 | 0.01 | 0.09 | 0.86 | 0.39 |
|      | 6th - 10th   | 0.25                        | 0.51 | 0.45 | 0.68 | 1.07 | 2.24 | 0.05 | 0.04 | 0.02 | 0    | 0.18 | 0.83 | 0.53 |
|      | 11th - 15th  | 0.18                        | 0.13 | 0.36 | 0.14 | 0.66 | 0.84 | 0.04 | 0.03 | 0.02 | 0    | 0.02 | 0.27 | 0.22 |
|      | 16th - 20th  | 0.28                        | 0.32 | 0.15 | 0.31 | 0.65 | 0.5  | 0.11 | 0.03 | 0.03 | 0.01 | 1.08 | 0.18 | 0.30 |
|      | 21st - 25th  | 0.75                        | 0.19 | 0.16 | 1.37 | 0.41 | 0.28 | 0.1  | 0.06 | 0.02 | 0.09 | 3.17 | 0.13 | 0.56 |
|      | 26th - 31st  | 0.11                        | 1.02 | 0.6  | 1.04 | 0.53 | 0.62 | 0.12 | 0.02 | 0.01 | 0.09 | 9.05 | 0.15 | 1.11 |
| 1984 | 1st - 5th    | 0.28                        | 1.06 | 0.87 | 0.41 | 1.16 | 0.46 | 0.56 | 0.2  | 0.26 | 1.1  | 0.34 | 0.24 | 0.58 |
|      | 6th - 10th   | 0.54                        | 0.79 | 2.34 | 0.56 | 0.98 | 0.38 | 0.39 | 0.16 | 0.9  | 0.31 | 0.19 | 0.2  | 0.65 |
|      | 11th - 15th  | 0.19                        | 0.92 | 3.27 | 0.37 | 0.52 | 0.5  | 0.21 | 0.36 | 0.93 | 0.52 | 0.19 | 0.34 | 0.69 |
|      | 16th - 20th  | 0.3                         | 1.84 | 2.14 | 0.56 | 0.35 | 0.48 | 0.19 | 0.22 | 0.63 | 0.42 | 0.43 | 0.27 | 0.65 |
|      | 21st - 25th  | 2.07                        | 1.67 | 4.11 | 0.42 | 0.55 | 0.32 | 0.38 | 0.2  | 0.42 | 0.5  | 0.33 | 0.23 | 0.93 |
|      | 26th - 31st  | 3.25                        | 1.33 | 3.9  | 1.06 | 0.43 | 0.23 | 0.34 | 0.36 | 0.97 | 0.26 | 0.18 | 0.75 | 1.09 |
| 1985 | 1st - 5th    | 0.26                        | 0.23 | 0.39 | 0.25 | 0.24 | 0.14 | 0.16 | 0.58 | 0.09 | 0.27 | 0.19 | 0.7  | 0.29 |
|      | 6th - 10th   | 0.94                        | 0.2  | 0.88 | 0.35 | 0.18 | 0.19 | 0.32 | 0.22 | 0.19 | 0.24 | 0.34 | 0.28 | 0.36 |
|      | 11th - 15th  | 0.27                        | 0.17 | 0.33 | 0.57 | 0.2  | 0.12 | 0.39 | 0.14 | 0.13 | 0.16 | 0.14 | 0.11 | 0.23 |
|      | 16th - 20th  | 0.2                         | 0.11 | 0.35 | 1.33 | 0.14 | 0.13 | 0.4  | 0.14 | 0.11 | 0.78 | 0.1  | 0.18 | 0.33 |
|      | 21st - 25th  | 0.28                        | 0.42 | 0.18 | 0.41 | 0.12 | 0.49 | 0.62 | 0.11 | 0.1  | 0.16 | 0.14 | 0.28 | 0.28 |
|      | 26th - 31st  | 0.45                        | 0.11 | 0.29 | 0.42 | 0.18 | 0.13 | 0.21 | 0.13 | 0.22 | 0.15 | 0.24 | 0.22 | 0.23 |
| 1986 | 1st - 5th    | 0.18                        | 0.78 | 0.61 | 0.68 | 0.24 | 0.14 | 0.22 | 0.11 | 0.14 | 0.41 | 0.24 | 0.14 | 0.32 |
|      | 6th - 10th   | 1.94                        | 0.64 | 0.37 | 0.49 | 0.36 | 0.25 | 0.21 | 0.12 | 0.33 | 0.29 | 0.46 | 0.11 | 0.46 |
|      | 11th - 15th  | 0.68                        | 1.11 | 0.55 | 0.64 | 0.39 | 0.51 | 0.7  | 0.36 | 0.32 | 0.16 | 0.39 | 0.51 | 0.53 |
|      | 16th - 20th  | 0.99                        | 0.39 | 0.44 | 0.38 | 0.19 | 0.21 | 0.34 | 0.16 | 0.17 | 0.15 | 0.57 | 0.65 | 0.39 |
|      | 21st - 25th  | 2.78                        | 0.53 | 0.41 | 0.3  | 0.25 | 0.12 | 0.19 | 0.11 | 0.12 | 0.1  | 0.24 | 0.15 | 0.44 |
|      | 26th - 31st  | 1.76                        | 0.58 | 0.29 | 0.49 | 0.2  | 0.14 | 0.27 | 0.15 | 0.14 | 0.58 | 0.43 | 0.22 | 0.44 |
| 1987 | 1st - 5th    | 0.37                        | 0.32 | 0.58 | 0.29 | 0.46 | 0.2  | 0.14 | 0.1  | 0.09 | 0.09 | 0.1  | 0.1  | 0.24 |
|      | 6th - 10th   | 1.42                        | 0.87 | 0.33 | 0.23 | 0.61 | 0.23 | 0.12 | 0.09 | 0.09 | 0.09 | 0.24 | 0.11 | 0.37 |
|      | 11th - 15th  | 1.13                        | 0.35 | 0.25 | 0.24 | 0.43 | 0.31 | 0.1  | 0.09 | 0.09 | 0.09 | 0.13 | 0.16 | 0.28 |
|      | 16th - 20th  | 0.41                        | 0.46 | 0.22 | 0.23 | 0.34 | 0.18 | 0.1  | 0.09 | 0.11 | 0.09 | 0.09 | 0.66 | 0.25 |
|      | 21st - 25th  | 0.53                        | 0.3  | 0.29 | 0.21 | 0.17 | 0.18 | 0.1  | 0.09 | 0.09 | 0.09 | 0.09 | 0.14 | 0.19 |
|      | 26th - 31st  | 0.57                        | 1.78 | 0.31 | 0.72 | 0.17 | 0.15 | 0.1  | 0.09 | 0.09 | 0.09 | 0.09 | 0.09 | 0.35 |
| 1988 | 1st - 5th    | 0.09                        | 2.92 | 0.19 | 0.37 | 0.13 | 0.18 | 0.19 | 0.11 | 0.09 | 0.09 | 0.64 | 0.12 | 0.43 |
|      | 6th - 10th   | 0.17                        | 2.02 | 0.16 | 0.22 | 0.11 | 0.12 | 0.13 | 0.12 | 0.09 | 0.09 | 0.21 | 0.12 | 0.30 |
|      | 11th - 15th  | 0.17                        | 0.37 | 0.15 | 0.17 | 0.13 | 0.11 | 0.08 | 0.14 | 0.09 | 0.51 | 0.16 | 0.88 | 0.25 |
|      | 16th - 20th  | 0.27                        | 0.18 | 0.15 | 0.16 | 0.16 | 0.09 | 0.1  | 0.12 | 0.09 | 0.32 | 0.11 | 0.21 | 0.16 |
|      | 21st - 25th  | 0.19                        | 0.16 | 0.19 | 0.19 | 0.13 | 0.09 | 0.08 | 0.11 | 0.09 | 0.15 | 0.12 | 0.09 | 0.13 |
|      | 26th - 31st  | 0.77                        | 0.16 | 0.17 | 0.14 | 0.1  | 0.09 | 0.09 | 0.1  | 0.09 | 0.36 | 0.11 | 0.09 | 0.19 |
| 1989 | 1st - 5th    | 0.09                        | 0.5  | 0.8  | 0.08 | 0.05 | 0.04 | 0.13 | 0.14 | 0.12 | 0.09 | 0.09 | 0.09 | 0.19 |
|      | 6th - 10th   | 0.1                         | 0.5  | 0.69 | 0.1  | 0.04 | 0.16 | 0.13 | 0.18 | 0.16 | 0.09 | 0.09 | 0.17 | 0.20 |
|      | 11th - 15th  | 0.13                        | 0.21 | 0.51 | 0.1  | 0.02 | 0.21 | 0.14 | 0.14 | 0.12 | 0.09 | 0.09 | 1.14 | 0.24 |
|      | 16th - 20th  | 0.14                        | 0.62 | 0.24 | 0.04 | 0.03 | 0.18 | 0.13 | 0.14 | 0.09 | 0.09 | 0.1  | 0.38 | 0.18 |
|      | 21st - 25th  | 0.27                        | 1.75 | 0.08 | 0.03 | 0.04 | 0.18 | 0.12 | 0.13 | 0.09 | 0.09 | 0.09 | 0.17 | 0.25 |
|      | 26th - 31st  | 0.16                        | 1.49 | 0.1  | 0.03 | 0.04 | 0.18 | 0.15 | 0.29 | 0.09 | 0.09 | 0.09 | 0.47 | 0.27 |
| Mean |              | 0.86                        | 0.81 | 0.72 | 0.41 | 0.33 | 0.28 | 0.25 | 0.19 | 0.23 | 0.25 | 0.50 | 0.36 | 0.43 |

Table F-33 Five (5)-day Mean Inflow Discharge at Beroeng Intake Weir Site

|      |              | (Unit: m <sup>3</sup> /sec) |      |      |      |      |      |      |      |      |      |      |      |      |
|------|--------------|-----------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Year | Period (day) | Jan.                        | Feb. | Mar. | Apr. | May  | Jun. | Jul. | Aug. | Sep. | Oct. | Nov. | Dec. | Mean |
| 1980 | 1st - 5th    | 0.25                        | 0.39 | 0.31 | 0.13 | 0.23 | 0.23 | 0.08 | 0.25 | 0.48 | 0.23 | 0.38 | 0.1  | 0.26 |
|      | 6th - 10th   | 0.42                        | 1.01 | 0.48 | 0.14 | 0.2  | 0.12 | 0.08 | 0.39 | 0.41 | 0.26 | 0.21 | 0.14 | 0.32 |
|      | 11th - 15th  | 0.62                        | 1.03 | 0.33 | 0.6  | 0.23 | 0.16 | 0.09 | 0.6  | 0.67 | 0.26 | 0.27 | 0.11 | 0.41 |
|      | 16th - 20th  | 0.61                        | 1.64 | 0.34 | 0.21 | 0.22 | 0.1  | 0.11 | 0.79 | 0.23 | 0.17 | 0.66 | 0.37 | 0.45 |
|      | 21st - 25th  | 0.61                        | 0.97 | 0.15 | 0.36 | 0.15 | 0.12 | 0.1  | 0.11 | 0.17 | 0.25 | 0.16 | 1.12 | 0.36 |
|      | 26th - 31st  | 0.69                        | 0.49 | 0.19 | 0.23 | 0.11 | 0.11 | 0.11 | 0.09 | 0.3  | 0.2  | 0.13 | 1.12 | 0.31 |
| 1981 | 1st - 5th    | 3.61                        | 0.84 | 1.38 | 0.29 | 0.45 | 0.14 | 0.13 | 0.35 | 0.38 | 0.7  | 0.29 | 0.65 | 0.77 |
|      | 6th - 10th   | 2.48                        | 0.73 | 0.7  | 0.34 | 0.34 | 0.12 | 0.12 | 0.36 | 0.36 | 0.7  | 0.58 | 0.41 | 0.60 |
|      | 11th - 15th  | 1.5                         | 1.09 | 1.07 | 0.2  | 0.44 | 0.26 | 0.45 | 0.22 | 0.99 | 0.54 | 0.88 | 0.35 | 0.67 |
|      | 16th - 20th  | 0.88                        | 1.08 | 0.68 | 0.28 | 0.61 | 0.43 | 0.67 | 0.31 | 0.24 | 0.22 | 2.07 | 0.35 | 0.65 |
|      | 21st - 25th  | 0.62                        | 0.98 | 0.35 | 0.29 | 0.22 | 0.19 | 0.75 | 0.31 | 0.21 | 0.26 | 0.36 | 0.71 | 0.44 |
|      | 26th - 31st  | 0.86                        | 2.62 | 0.54 | 0.22 | 0.17 | 0.25 | 1.18 | 0.21 | 0.33 | 0.38 | 0.97 | 1.35 | 0.76 |
| 1982 | 1st - 5th    | 0.82                        | 1    | 0.61 | 0.58 | 0.5  | 0.52 | 0.17 | 0.23 | 0.1  | 0.13 | 0.08 | 0.09 | 0.40 |
|      | 6th - 10th   | 1.88                        | 0.47 | 0.78 | 0.48 | 0.45 | 0.39 | 0.14 | 0.17 | 0.1  | 0.09 | 0.13 | 0.08 | 0.43 |
|      | 11th - 15th  | 2.96                        | 0.61 | 1.28 | 0.45 | 0.34 | 0.28 | 0.14 | 0.08 | 0.09 | 0.09 | 0.13 | 0.09 | 0.55 |
|      | 16th - 20th  | 1.9                         | 0.47 | 1.24 | 0.73 | 0.24 | 0.24 | 0.35 | 0.06 | 0.09 | 0.21 | 0.13 | 0.09 | 0.48 |
|      | 21st - 25th  | 1.35                        | 0.37 | 0.93 | 0.48 | 0.24 | 0.16 | 0.36 | 0.05 | 0.08 | 0.1  | 0.12 | 0.1  | 0.36 |
|      | 26th - 31st  | 0.97                        | 0.45 | 0.73 | 0.69 | 0.29 | 0.24 | 0.35 | 0.03 | 0.11 | 0.09 | 0.12 | 0.22 | 0.36 |
| 1983 | 1st - 5th    | 0.39                        | 0.46 | 0.91 | 0.39 | 0.53 | 0.31 | 0.32 | 0.04 | 0.01 | 0.01 | 0.09 | 0.78 | 0.35 |
|      | 6th - 10th   | 0.23                        | 0.46 | 0.41 | 0.62 | 0.97 | 2.04 | 0.05 | 0.03 | 0.02 | 0    | 0.17 | 0.75 | 0.48 |
|      | 11th - 15th  | 0.17                        | 0.12 | 0.33 | 0.13 | 0.6  | 0.76 | 0.04 | 0.03 | 0.02 | 0    | 0.02 | 0.25 | 0.21 |
|      | 16th - 20th  | 0.25                        | 0.29 | 0.13 | 0.29 | 0.59 | 0.45 | 0.1  | 0.03 | 0.02 | 0.01 | 0.98 | 0.17 | 0.28 |
|      | 21st - 25th  | 0.68                        | 0.17 | 0.14 | 1.24 | 0.37 | 0.26 | 0.09 | 0.06 | 0.02 | 0.08 | 2.89 | 0.12 | 0.51 |
|      | 26th - 31st  | 0.1                         | 0.93 | 0.55 | 0.94 | 0.48 | 0.56 | 0.11 | 0.02 | 0.01 | 0.08 | 8.23 | 0.13 | 1.01 |
| 1984 | 1st - 5th    | 0.26                        | 0.96 | 0.79 | 0.37 | 1.06 | 0.42 | 0.51 | 0.18 | 0.24 | 1    | 0.31 | 0.22 | 0.53 |
|      | 6th - 10th   | 0.49                        | 0.72 | 2.13 | 0.51 | 0.89 | 0.35 | 0.35 | 0.15 | 0.82 | 0.28 | 0.17 | 0.18 | 0.59 |
|      | 11th - 15th  | 0.18                        | 0.84 | 2.98 | 0.34 | 0.47 | 0.45 | 0.19 | 0.32 | 0.85 | 0.47 | 0.18 | 0.31 | 0.63 |
|      | 16th - 20th  | 0.27                        | 1.68 | 1.94 | 0.51 | 0.32 | 0.44 | 0.18 | 0.2  | 0.57 | 0.38 | 0.4  | 0.25 | 0.60 |
|      | 21st - 25th  | 1.89                        | 1.52 | 3.74 | 0.39 | 0.5  | 0.29 | 0.34 | 0.18 | 0.39 | 0.45 | 0.3  | 0.21 | 0.85 |
|      | 26th - 31st  | 2.96                        | 1.21 | 3.55 | 0.96 | 0.39 | 0.21 | 0.31 | 0.33 | 0.88 | 0.24 | 0.16 | 0.68 | 0.99 |
| 1985 | 1st - 5th    | 0.24                        | 0.21 | 0.36 | 0.23 | 0.22 | 0.13 | 0.15 | 0.53 | 0.09 | 0.24 | 0.17 | 0.63 | 0.27 |
|      | 6th - 10th   | 0.86                        | 0.18 | 0.8  | 0.32 | 0.16 | 0.17 | 0.29 | 0.2  | 0.18 | 0.22 | 0.31 | 0.26 | 0.33 |
|      | 11th - 15th  | 0.24                        | 0.16 | 0.3  | 0.52 | 0.18 | 0.11 | 0.36 | 0.13 | 0.12 | 0.15 | 0.13 | 0.1  | 0.21 |
|      | 16th - 20th  | 0.18                        | 0.1  | 0.32 | 1.21 | 0.13 | 0.12 | 0.36 | 0.13 | 0.1  | 0.71 | 0.09 | 0.16 | 0.30 |
|      | 21st - 25th  | 0.26                        | 0.38 | 0.17 | 0.37 | 0.11 | 0.44 | 0.56 | 0.1  | 0.09 | 0.15 | 0.13 | 0.25 | 0.25 |
|      | 26th - 31st  | 0.41                        | 0.1  | 0.26 | 0.38 | 0.16 | 0.12 | 0.19 | 0.11 | 0.2  | 0.14 | 0.21 | 0.2  | 0.21 |
| 1986 | 1st - 5th    | 0.16                        | 0.71 | 0.55 | 0.62 | 0.21 | 0.13 | 0.2  | 0.1  | 0.13 | 0.38 | 0.22 | 0.12 | 0.29 |
|      | 6th - 10th   | 1.77                        | 0.58 | 0.34 | 0.44 | 0.33 | 0.23 | 0.19 | 0.11 | 0.3  | 0.27 | 0.42 | 0.1  | 0.42 |
|      | 11th - 15th  | 0.62                        | 1.01 | 0.5  | 0.58 | 0.35 | 0.46 | 0.64 | 0.32 | 0.29 | 0.14 | 0.35 | 0.47 | 0.48 |
|      | 16th - 20th  | 0.9                         | 0.35 | 0.4  | 0.35 | 0.17 | 0.19 | 0.31 | 0.14 | 0.15 | 0.13 | 0.52 | 0.6  | 0.35 |
|      | 21st - 25th  | 2.53                        | 0.48 | 0.37 | 0.27 | 0.23 | 0.11 | 0.17 | 0.1  | 0.11 | 0.09 | 0.22 | 0.13 | 0.40 |
|      | 26th - 31st  | 1.6                         | 0.53 | 0.27 | 0.44 | 0.18 | 0.12 | 0.25 | 0.14 | 0.13 | 0.53 | 0.39 | 0.2  | 0.40 |
| 1987 | 1st - 5th    | 0.34                        | 0.29 | 0.53 | 0.26 | 0.41 | 0.18 | 0.13 | 0.09 | 0.08 | 0.08 | 0.09 | 0.09 | 0.21 |
|      | 6th - 10th   | 1.29                        | 0.79 | 0.3  | 0.21 | 0.55 | 0.21 | 0.1  | 0.08 | 0.08 | 0.08 | 0.22 | 0.1  | 0.33 |
|      | 11th - 15th  | 1.03                        | 0.32 | 0.23 | 0.22 | 0.39 | 0.28 | 0.09 | 0.08 | 0.08 | 0.08 | 0.12 | 0.14 | 0.26 |
|      | 16th - 20th  | 0.37                        | 0.42 | 0.2  | 0.21 | 0.31 | 0.16 | 0.09 | 0.08 | 0.1  | 0.08 | 0.08 | 0.6  | 0.23 |
|      | 21st - 25th  | 0.48                        | 0.27 | 0.27 | 0.19 | 0.16 | 0.17 | 0.09 | 0.08 | 0.08 | 0.08 | 0.08 | 0.13 | 0.17 |
|      | 26th - 31st  | 0.51                        | 1.62 | 0.28 | 0.66 | 0.16 | 0.14 | 0.09 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 | 0.32 |
| 1988 | 1st - 5th    | 0.08                        | 2.66 | 0.17 | 0.34 | 0.12 | 0.16 | 0.17 | 0.1  | 0.09 | 0.08 | 0.58 | 0.11 | 0.39 |
|      | 6th - 10th   | 0.15                        | 1.84 | 0.15 | 0.2  | 0.1  | 0.11 | 0.12 | 0.11 | 0.08 | 0.08 | 0.19 | 0.11 | 0.27 |
|      | 11th - 15th  | 0.15                        | 0.33 | 0.14 | 0.15 | 0.12 | 0.1  | 0.07 | 0.13 | 0.08 | 0.46 | 0.14 | 0.8  | 0.22 |
|      | 16th - 20th  | 0.24                        | 0.16 | 0.13 | 0.15 | 0.14 | 0.08 | 0.09 | 0.11 | 0.08 | 0.29 | 0.1  | 0.19 | 0.15 |
|      | 21st - 25th  | 0.17                        | 0.15 | 0.17 | 0.18 | 0.12 | 0.08 | 0.07 | 0.1  | 0.08 | 0.14 | 0.11 | 0.08 | 0.12 |
|      | 26th - 31st  | 0.7                         | 0.14 | 0.16 | 0.13 | 0.1  | 0.08 | 0.08 | 0.09 | 0.08 | 0.32 | 0.1  | 0.08 | 0.17 |
| 1989 | 1st - 5th    | 0.08                        | 0.46 | 0.73 | 0.08 | 0.04 | 0.04 | 0.12 | 0.13 | 0.11 | 0.08 | 0.08 | 0.08 | 0.17 |
|      | 6th - 10th   | 0.09                        | 0.46 | 0.63 | 0.1  | 0.03 | 0.15 | 0.12 | 0.17 | 0.15 | 0.08 | 0.08 | 0.08 | 0.18 |
|      | 11th - 15th  | 0.12                        | 0.19 | 0.47 | 0.09 | 0.02 | 0.19 | 0.13 | 0.13 | 0.11 | 0.08 | 0.08 | 0.08 | 0.14 |
|      | 16th - 20th  | 0.13                        | 0.56 | 0.21 | 0.03 | 0.03 | 0.16 | 0.12 | 0.13 | 0.08 | 0.08 | 0.09 | 0.09 | 0.14 |
|      | 21st - 25th  | 0.25                        | 1.59 | 0.08 | 0.03 | 0.04 | 0.17 | 0.11 | 0.11 | 0.08 | 0.08 | 0.08 | 0.08 | 0.23 |
|      | 26th - 31st  | 0.14                        | 1.35 | 0.09 | 0.02 | 0.04 | 0.16 | 0.14 | 0.26 | 0.08 | 0.08 | 0.08 | 0.08 | 0.21 |
| Mean |              | 0.78                        | 0.73 | 0.65 | 0.37 | 0.30 | 0.26 | 0.23 | 0.17 | 0.21 | 0.22 | 0.45 | 0.30 | 0.39 |

Table F-34 (1) Reservoir Operation Study for Existing Krenceng Dam (1/12)

Net supply yield: 1.94m<sup>3</sup>/sec  
 Water conveyance capacity: 2.00 m<sup>3</sup>/sec  
 at 27.2 km pipe line

(Unit: 10<sup>6</sup> m<sup>3</sup>)

| Year | Month | Serial No. of 5 day period | Inflow discharge |                 | Supply yield | Evapo | Water conveyance from Cida | Krenceng Storage volume | Reservoir Water level (El-m) | Spillout |
|------|-------|----------------------------|------------------|-----------------|--------------|-------|----------------------------|-------------------------|------------------------------|----------|
|      |       |                            | Krenceng         | Cidansau intake |              |       |                            |                         |                              |          |
| 1980 | 1     | 1                          | 0.12             | 3.9             | 0.84         | 0.02  | 0.74                       | 4.66                    | 22.5                         | 0        |
| 1980 | 1     | 2                          | 0.2              | 3.98            | 0.84         | 0.02  | 0.66                       | 4.66                    | 22.5                         | 0        |
| 1980 | 1     | 3                          | 0.29             | 4.05            | 0.84         | 0.02  | 0.56                       | 4.66                    | 22.5                         | 0        |
| 1980 | 1     | 4                          | 0.29             | 3.92            | 0.84         | 0.02  | 0.56                       | 4.66                    | 22.5                         | 0        |
| 1980 | 1     | 5                          | 0.29             | 3.9             | 0.84         | 0.02  | 0.57                       | 4.66                    | 22.5                         | 0        |
| 1980 | 1     | 6                          | 0.39             | 3.56            | 1.01         | 0.02  | 0.66                       | 4.66                    | 22.5                         | 0        |
| 1980 | 2     | 1                          | 0.19             | 3.3             | 0.84         | 0.01  | 0.66                       | 4.66                    | 22.5                         | 0        |
| 1980 | 2     | 2                          | 0.48             | 5.06            | 0.84         | 0.01  | 0.37                       | 4.66                    | 22.5                         | 0        |
| 1980 | 2     | 3                          | 0.49             | 5.01            | 0.84         | 0.01  | 0.36                       | 4.66                    | 22.5                         | 0        |
| 1980 | 2     | 4                          | 0.78             | 5.06            | 0.84         | 0.01  | 0.07                       | 4.66                    | 22.5                         | 0        |
| 1980 | 2     | 5                          | 0.46             | 5.09            | 0.84         | 0.01  | 0.39                       | 4.66                    | 22.5                         | 0        |
| 1980 | 2     | 6                          | 0.19             | 5.06            | 0.84         | 0.01  | 0.5                        | 4.66                    | 22.5                         | 0        |
| 1980 | 3     | 1                          | 0.15             | 4.53            | 0.84         | 0.01  | 0.7                        | 4.66                    | 22.5                         | 0        |
| 1980 | 3     | 2                          | 0.23             | 3.44            | 0.84         | 0.01  | 0.62                       | 4.66                    | 22.5                         | 0        |
| 1980 | 3     | 3                          | 0.15             | 14.02           | 0.84         | 0.01  | 0.7                        | 4.66                    | 22.5                         | 0        |
| 1980 | 3     | 4                          | 0.16             | 9.57            | 0.84         | 0.01  | 0.69                       | 4.66                    | 22.5                         | 0        |
| 1980 | 3     | 5                          | 0.07             | 2.29            | 0.84         | 0.01  | 0.78                       | 4.66                    | 22.5                         | 0        |
| 1980 | 3     | 6                          | 0.11             | 1.74            | 1.01         | 0.01  | 0.91                       | 4.66                    | 22.5                         | 0        |
| 1980 | 4     | 1                          | 0.06             | 2.23            | 0.84         | 0.01  | 0.79                       | 4.66                    | 22.5                         | 0        |
| 1980 | 4     | 2                          | 0.07             | 1.77            | 0.84         | 0.01  | 0.78                       | 4.66                    | 22.5                         | 0        |
| 1980 | 4     | 3                          | 0.28             | 6.5             | 0.84         | 0.01  | 0.57                       | 4.66                    | 22.5                         | 0        |
| 1980 | 4     | 4                          | 0.11             | 4.84            | 0.84         | 0.01  | 0.75                       | 4.66                    | 22.5                         | 0        |
| 1980 | 4     | 5                          | 0.17             | 3.27            | 0.84         | 0.01  | 0.68                       | 4.66                    | 22.5                         | 0        |
| 1980 | 4     | 6                          | 0.11             | 1.99            | 0.84         | 0.01  | 0.74                       | 4.66                    | 22.5                         | 0        |
| 1980 | 5     | 1                          | 0.11             | 0.82            | 0.84         | 0.01  | 0.74                       | 4.66                    | 22.5                         | 0        |
| 1980 | 5     | 2                          | 0.09             | 0.18            | 0.84         | 0.01  | 0.18                       | 4.66                    | 22.5                         | 0        |
| 1980 | 5     | 3                          | 0.11             | 0.88            | 0.84         | 0.01  | 0.86                       | 4.2                     | 22.01                        | 0        |
| 1980 | 5     | 4                          | 0.11             | 1.91            | 0.84         | 0.01  | 0.86                       | 4.32                    | 22.14                        | 0        |
| 1980 | 5     | 5                          | 0.07             | 5.36            | 0.84         | 0.01  | 0.86                       | 4.41                    | 22.23                        | 0        |
| 1980 | 5     | 6                          | 0.06             | 4.99            | 1.01         | 0.01  | 1.04                       | 4.49                    | 22.32                        | 0        |
| 1980 | 6     | 1                          | 0.11             | 3.84            | 0.84         | 0.01  | 0.86                       | 4.61                    | 22.45                        | 0        |
| 1980 | 6     | 2                          | 0.06             | 4.39            | 0.84         | 0.01  | 0.84                       | 4.66                    | 22.5                         | 0        |
| 1980 | 6     | 3                          | 0.08             | 1.89            | 0.84         | 0.01  | 0.77                       | 4.66                    | 22.5                         | 0        |
| 1980 | 6     | 4                          | 0.05             | 3.17            | 0.84         | 0.01  | 0.8                        | 4.66                    | 22.5                         | 0        |
| 1980 | 6     | 5                          | 0.06             | 3.77            | 0.84         | 0.01  | 0.79                       | 4.66                    | 22.5                         | 0        |
| 1980 | 6     | 6                          | 0.05             | 2.37            | 0.84         | 0.01  | 0.8                        | 4.66                    | 22.5                         | 0        |
| 1980 | 7     | 1                          | 0.04             | 1.63            | 0.84         | 0.01  | 0.81                       | 4.66                    | 22.5                         | 0        |
| 1980 | 7     | 2                          | 0.04             | 2.82            | 0.84         | 0.01  | 0.81                       | 4.66                    | 22.5                         | 0        |
| 1980 | 7     | 3                          | 0.04             | 2.81            | 0.84         | 0.01  | 0.81                       | 4.66                    | 22.5                         | 0        |
| 1980 | 7     | 4                          | 0.05             | 4.75            | 0.84         | 0.01  | 0.8                        | 4.66                    | 22.5                         | 0        |
| 1980 | 7     | 5                          | 0.05             | 2.64            | 0.84         | 0.01  | 0.8                        | 4.66                    | 22.5                         | 0        |
| 1980 | 7     | 6                          | 0.06             | 2.74            | 1.01         | 0.01  | 0.96                       | 4.66                    | 22.5                         | 0        |
| 1980 | 8     | 1                          | 0.12             | 2.19            | 0.84         | 0.02  | 0.74                       | 4.66                    | 22.5                         | 0        |
| 1980 | 8     | 2                          | 0.19             | 4.48            | 0.84         | 0.02  | 0.67                       | 4.66                    | 22.5                         | 0        |
| 1980 | 8     | 3                          | 0.28             | 6.84            | 0.84         | 0.02  | 0.57                       | 4.66                    | 22.5                         | 0        |
| 1980 | 8     | 4                          | 0.38             | 12.84           | 0.84         | 0.02  | 0.48                       | 4.66                    | 22.5                         | 0        |
| 1980 | 8     | 5                          | 0.05             | 5.29            | 0.84         | 0.02  | 0.8                        | 4.66                    | 22.5                         | 0        |
| 1980 | 8     | 6                          | 0.05             | 2.12            | 1.01         | 0.02  | 0.98                       | 4.66                    | 22.5                         | 0        |
| 1980 | 9     | 1                          | 0.25             | 2.64            | 0.84         | 0.01  | 0.62                       | 4.66                    | 22.5                         | 0        |
| 1980 | 9     | 2                          | 0.2              | 27.03           | 0.84         | 0.01  | 0.66                       | 4.66                    | 22.5                         | 0        |
| 1980 | 9     | 3                          | 0.32             | 28.73           | 0.84         | 0.01  | 0.53                       | 4.66                    | 22.5                         | 0        |
| 1980 | 9     | 4                          | 0.11             | 12.39           | 0.84         | 0.01  | 0.74                       | 4.66                    | 22.5                         | 0        |
| 1980 | 9     | 5                          | 0.08             | 2.48            | 0.84         | 0.01  | 0.77                       | 4.66                    | 22.5                         | 0        |
| 1980 | 9     | 6                          | 0.14             | 1.63            | 0.84         | 0.01  | 0.71                       | 4.66                    | 22.5                         | 0        |
| 1980 | 10    | 1                          | 0.11             | 0.86            | 0.84         | 0.01  | 0.66                       | 4.66                    | 22.5                         | 0        |
| 1980 | 10    | 2                          | 0.12             | 0.63            | 0.84         | 0.01  | 0.63                       | 4.56                    | 22.39                        | 0        |
| 1980 | 10    | 3                          | 0.12             | 2.54            | 0.84         | 0.01  | 0.63                       | 4.66                    | 22.5                         | 0        |
| 1980 | 10    | 4                          | 0.08             | 6.13            | 0.84         | 0.01  | 0.77                       | 4.66                    | 22.5                         | 0        |
| 1980 | 10    | 5                          | 0.12             | 6.87            | 0.84         | 0.01  | 0.73                       | 4.66                    | 22.5                         | 0        |
| 1980 | 10    | 6                          | 0.11             | 9.88            | 1.01         | 0.02  | 0.91                       | 4.66                    | 22.5                         | 0        |



Table F-34 (2) Reservoir Operation Study for Existing Krenceng Dam (2/12)

Net supply yield: 1.94m<sup>3</sup>/sec  
 Water conveyance capacity: 2.00 m<sup>3</sup>/sec  
 of 27.2 km pipe line

(Unit: 10 m<sup>3</sup>)

| Year | Month | Serial No. of 5 day period | Inflow discharge |                | Supply yield | Evapo | Water conveyance from Cida | Krenceng Storage volume | Reservoir Water level (El-m) | Spillout |
|------|-------|----------------------------|------------------|----------------|--------------|-------|----------------------------|-------------------------|------------------------------|----------|
|      |       |                            | Krenceng         | Cidauau intake |              |       |                            |                         |                              |          |
| 1980 | 11    | 1                          | 0.18             | 9.4            | 0.84         | 0.02  | 0.68                       | 4.66                    | 22.5                         | 0        |
| 1980 | 11    | 2                          | 0.1              | 11.06          | 0.84         | 0.02  | 0.75                       | 4.66                    | 22.5                         | 0        |
| 1980 | 11    | 3                          | 0.13             | 13.41          | 0.84         | 0.02  | 0.73                       | 4.66                    | 22.5                         | 0        |
| 1980 | 11    | 4                          | 0.31             | 15.5           | 0.84         | 0.02  | 0.54                       | 4.66                    | 22.5                         | 0        |
| 1980 | 11    | 5                          | 0.08             | 18.31          | 0.84         | 0.02  | 0.78                       | 4.66                    | 22.5                         | 0        |
| 1980 | 11    | 6                          | 0.06             | 21.43          | 0.84         | 0.02  | 0.79                       | 4.66                    | 22.5                         | 0        |
| 1980 | 12    | 1                          | 0.05             | 27.92          | 0.84         | 0.01  | 0.81                       | 4.66                    | 22.5                         | 0        |
| 1980 | 12    | 2                          | 0.07             | 31.72          | 0.84         | 0.01  | 0.79                       | 4.66                    | 22.5                         | 0        |
| 1980 | 12    | 3                          | 0.05             | 32.78          | 0.84         | 0.01  | 0.8                        | 4.66                    | 22.5                         | 0        |
| 1980 | 12    | 4                          | 0.18             | 42.23          | 0.84         | 0.01  | 0.68                       | 4.66                    | 22.5                         | 0        |
| 1980 | 12    | 5                          | 0.53             | 29.54          | 0.84         | 0.01  | 0.32                       | 4.66                    | 22.5                         | 0        |
| 1980 | 12    | 6                          | 0.64             | 47.28          | 1.01         | 0.02  | 0.39                       | 4.66                    | 22.5                         | 0        |
| 1981 | 1     | 1                          | 1.71             | 62.12          | 0.84         | 0.02  | 0                          | 4.66                    | 22.5                         | 0.86     |
| 1981 | 1     | 2                          | 1.18             | 72.41          | 0.84         | 0.02  | 0                          | 4.66                    | 22.5                         | 0.32     |
| 1981 | 1     | 3                          | 0.71             | 28.77          | 0.84         | 0.02  | 0.14                       | 4.66                    | 22.5                         | 0        |
| 1981 | 1     | 4                          | 0.42             | 30.33          | 0.84         | 0.02  | 0.44                       | 4.66                    | 22.5                         | 0        |
| 1981 | 1     | 5                          | 0.29             | 13.91          | 0.84         | 0.02  | 0.56                       | 4.66                    | 22.5                         | 0        |
| 1981 | 1     | 6                          | 0.49             | 17.12          | 1.01         | 0.02  | 0.53                       | 4.66                    | 22.5                         | 0        |
| 1981 | 2     | 1                          | 0.4              | 18.43          | 0.84         | 0.01  | 0.45                       | 4.66                    | 22.5                         | 0        |
| 1981 | 2     | 2                          | 0.35             | 21.51          | 0.84         | 0.01  | 0.5                        | 4.66                    | 22.5                         | 0        |
| 1981 | 2     | 3                          | 0.32             | 14.11          | 0.84         | 0.01  | 0.34                       | 4.66                    | 22.5                         | 0        |
| 1981 | 2     | 4                          | 0.51             | 10.57          | 0.84         | 0.01  | 0.34                       | 4.66                    | 22.5                         | 0        |
| 1981 | 2     | 5                          | 0.46             | 1.87           | 0.84         | 0.01  | 0.39                       | 4.66                    | 22.5                         | 0        |
| 1981 | 2     | 6                          | 0.75             | 11.16          | 0.5          | 0.01  | 0                          | 4.66                    | 22.5                         | 0.24     |
| 1981 | 3     | 1                          | 0.66             | 12.23          | 0.84         | 0.01  | 0.19                       | 4.66                    | 22.5                         | 0        |
| 1981 | 3     | 2                          | 0.33             | 1.75           | 0.84         | 0.01  | 0.52                       | 4.66                    | 22.5                         | 0        |
| 1981 | 3     | 3                          | 0.51             | 2.26           | 0.84         | 0.01  | 0.34                       | 4.66                    | 22.5                         | 0        |
| 1981 | 3     | 4                          | 0.32             | 3.68           | 0.84         | 0.01  | 0.53                       | 4.66                    | 22.5                         | 0        |
| 1981 | 3     | 5                          | 0.17             | 2.34           | 0.84         | 0.01  | 0.68                       | 4.66                    | 22.5                         | 0        |
| 1981 | 3     | 6                          | 0.31             | 11.79          | 1.01         | 0.01  | 0.71                       | 4.66                    | 22.5                         | 0        |
| 1981 | 4     | 1                          | 0.14             | 12.43          | 0.84         | 0.01  | 0.71                       | 4.66                    | 22.5                         | 0        |
| 1981 | 4     | 2                          | 0.16             | 12.3           | 0.84         | 0.01  | 0.69                       | 4.66                    | 22.5                         | 0        |
| 1981 | 4     | 3                          | 0.1              | 11.66          | 0.84         | 0.01  | 0.75                       | 4.66                    | 22.5                         | 0        |
| 1981 | 4     | 4                          | 0.13             | 10.14          | 0.84         | 0.01  | 0.72                       | 4.66                    | 22.5                         | 0        |
| 1981 | 4     | 5                          | 0.14             | 8.69           | 0.84         | 0.01  | 0.71                       | 4.66                    | 22.5                         | 0        |
| 1981 | 4     | 6                          | 0.11             | 7.79           | 0.84         | 0.01  | 0.74                       | 4.66                    | 22.5                         | 0        |
| 1981 | 5     | 1                          | 0.21             | 6.43           | 0.84         | 0.01  | 0.64                       | 4.66                    | 22.5                         | 0        |
| 1981 | 5     | 2                          | 0.16             | 4.42           | 0.84         | 0.01  | 0.69                       | 4.66                    | 22.5                         | 0        |
| 1981 | 5     | 3                          | 0.23             | 2.96           | 0.84         | 0.01  | 0.64                       | 4.66                    | 22.5                         | 0        |
| 1981 | 5     | 4                          | 0.29             | 4.35           | 0.84         | 0.01  | 0.56                       | 4.66                    | 22.5                         | 0        |
| 1981 | 5     | 5                          | 0.11             | 3.23           | 0.84         | 0.01  | 0.74                       | 4.66                    | 22.5                         | 0        |
| 1981 | 5     | 6                          | 0.1              | 1.1            | 1.01         | 0.01  | 0.92                       | 4.66                    | 22.5                         | 0        |
| 1981 | 6     | 1                          | 0.06             | 2.82           | 0.84         | 0.01  | 0.78                       | 4.66                    | 22.5                         | 0        |
| 1981 | 6     | 2                          | 0.06             | 3.69           | 0.84         | 0.01  | 0.79                       | 4.66                    | 22.5                         | 0        |
| 1981 | 6     | 3                          | 0.12             | 5.1            | 0.84         | 0.01  | 0.73                       | 4.66                    | 22.5                         | 0        |
| 1981 | 6     | 4                          | 0.2              | 9.5            | 0.84         | 0.01  | 0.65                       | 4.66                    | 22.5                         | 0        |
| 1981 | 6     | 5                          | 0.09             | 4.31           | 0.84         | 0.01  | 0.76                       | 4.66                    | 22.5                         | 0        |
| 1981 | 6     | 6                          | 0.12             | 4.23           | 0.84         | 0.01  | 0.73                       | 4.66                    | 22.5                         | 0        |
| 1981 | 7     | 1                          | 0.06             | 4.31           | 0.84         | 0.01  | 0.79                       | 4.66                    | 22.5                         | 0        |
| 1981 | 7     | 2                          | 0.06             | 1.77           | 0.84         | 0.01  | 0.79                       | 4.66                    | 22.5                         | 0        |
| 1981 | 7     | 3                          | 0.21             | 2.78           | 0.84         | 0.01  | 0.64                       | 4.66                    | 22.5                         | 0        |
| 1981 | 7     | 4                          | 0.32             | 5.56           | 0.84         | 0.01  | 0.53                       | 4.66                    | 22.5                         | 0        |
| 1981 | 7     | 5                          | 0.36             | 7.35           | 0.84         | 0.01  | 0.49                       | 4.66                    | 22.5                         | 0        |
| 1981 | 7     | 6                          | 0.67             | 11.43          | 1.01         | 0.01  | 0.35                       | 4.66                    | 22.5                         | 0        |
| 1981 | 8     | 1                          | 0.16             | 8.03           | 0.84         | 0.02  | 0.69                       | 4.66                    | 22.5                         | 0        |
| 1981 | 8     | 2                          | 0.17             | 3.09           | 0.84         | 0.02  | 0.68                       | 4.66                    | 22.5                         | 0        |
| 1981 | 8     | 3                          | 0.11             | 2.22           | 0.84         | 0.02  | 0.75                       | 4.66                    | 22.5                         | 0        |
| 1981 | 8     | 4                          | 0.15             | 1.58           | 0.84         | 0.02  | 0.71                       | 4.66                    | 22.5                         | 0        |
| 1981 | 8     | 5                          | 0.15             | 3.77           | 0.84         | 0.02  | 0.71                       | 4.66                    | 22.5                         | 0        |
| 1981 | 8     | 6                          | 0.12             | 5.33           | 1.01         | 0.02  | 0.91                       | 4.66                    | 22.5                         | 0        |

Table F-34 (3) Reservoir Operation Study for Existing Krenceng Dam (3/12)

Net supply yield: 1.94m<sup>3</sup>/sec  
 Water conveyance capacity: 2.00 m<sup>3</sup>/sec  
 of 27.2 km pipe line

(Unit: 10<sup>6</sup> m<sup>3</sup>)

| Year | Month | Serial No. of 5 day period | Inflow discharge |              | Supply yield | Evapo | Water conveyance from Cida | Krenceng Storage volume | Reservoir Water level (El-m) | Spillout |
|------|-------|----------------------------|------------------|--------------|--------------|-------|----------------------------|-------------------------|------------------------------|----------|
|      |       |                            | Krenceng         | Cidau intake |              |       |                            |                         |                              |          |
| 1981 | 9     | 1                          | 0.13             | 2.18         | 0.84         | 0.01  | 0.67                       | 4.66                    | 22.5                         | 0        |
| 1981 | 9     | 2                          | 0.17             | 6.52         | 0.84         | 0.01  | 0.68                       | 4.66                    | 22.5                         | 0        |
| 1981 | 9     | 3                          | 0.47             | 7.08         | 0.84         | 0.01  | 0.38                       | 4.66                    | 22.5                         | 0        |
| 1981 | 9     | 4                          | 0.11             | 1.64         | 0.84         | 0.01  | 0.74                       | 4.66                    | 22.5                         | 0        |
| 1981 | 9     | 5                          | 0.1              | 1.14         | 0.84         | 0.01  | 0.75                       | 4.66                    | 22.5                         | 0        |
| 1981 | 9     | 6                          | 0.16             | 9.85         | 0.84         | 0.01  | 0.7                        | 4.66                    | 22.5                         | 0        |
| 1981 | 10    | 1                          | 0.33             | 41.85        | 0.84         | 0.01  | 0.52                       | 4.66                    | 22.5                         | 0        |
| 1981 | 10    | 2                          | 0.33             | 14.32        | 0.84         | 0.01  | 0.52                       | 4.66                    | 22.5                         | 0        |
| 1981 | 10    | 3                          | 0.25             | 4.95         | 0.84         | 0.01  | 0.6                        | 4.66                    | 22.5                         | 0        |
| 1981 | 10    | 4                          | 0.11             | 3.53         | 0.84         | 0.01  | 0.75                       | 4.66                    | 22.5                         | 0        |
| 1981 | 10    | 5                          | 0.12             | 1.83         | 0.84         | 0.01  | 0.73                       | 4.66                    | 22.5                         | 0        |
| 1981 | 10    | 6                          | 0.22             | 10.88        | 1.01         | 0.02  | 0.8                        | 4.66                    | 22.5                         | 0        |
| 1981 | 11    | 1                          | 0.14             | 4.61         | 0.84         | 0.02  | 0.72                       | 4.66                    | 22.5                         | 0        |
| 1981 | 11    | 2                          | 0.28             | 4.04         | 0.84         | 0.02  | 0.58                       | 4.66                    | 22.5                         | 0        |
| 1981 | 11    | 3                          | 0.42             | 24.28        | 0.84         | 0.02  | 0.44                       | 4.66                    | 22.5                         | 0        |
| 1981 | 11    | 4                          | 0.98             | 68.23        | 0.84         | 0.02  | 0                          | 4.66                    | 22.5                         | 0.13     |
| 1981 | 11    | 5                          | 0.17             | 25.93        | 0.84         | 0.02  | 0.68                       | 4.66                    | 22.5                         | 0        |
| 1981 | 11    | 6                          | 0.46             | 9.55         | 0.84         | 0.02  | 0.39                       | 4.66                    | 22.5                         | 0        |
| 1981 | 12    | 1                          | 0.31             | 12.78        | 0.84         | 0.01  | 0.55                       | 4.66                    | 22.5                         | 0        |
| 1981 | 12    | 2                          | 0.2              | 11.62        | 0.84         | 0.01  | 0.66                       | 4.66                    | 22.5                         | 0        |
| 1981 | 12    | 3                          | 0.17             | 8.62         | 0.84         | 0.01  | 0.69                       | 4.66                    | 22.5                         | 0        |
| 1981 | 12    | 4                          | 0.17             | 3.44         | 0.84         | 0.01  | 0.69                       | 4.66                    | 22.5                         | 0        |
| 1981 | 12    | 5                          | 0.34             | 5.79         | 0.84         | 0.01  | 0.52                       | 4.66                    | 22.5                         | 0        |
| 1981 | 12    | 6                          | 0.77             | 37.81        | 1.01         | 0.02  | 0.25                       | 4.66                    | 22.5                         | 0        |
| 1982 | 1     | 1                          | 0.39             | 21.37        | 0.84         | 0.02  | 0.47                       | 4.66                    | 22.5                         | 0        |
| 1982 | 1     | 2                          | 0.89             | 11.65        | 0.84         | 0.02  | 0                          | 4.66                    | 22.5                         | 0.04     |
| 1982 | 1     | 3                          | 1.4              | 4.37         | 0.84         | 0.02  | 0                          | 4.66                    | 22.5                         | 0.35     |
| 1982 | 1     | 4                          | 0.9              | 18.14        | 0.84         | 0.02  | 0                          | 4.66                    | 22.5                         | 0.05     |
| 1982 | 1     | 5                          | 0.64             | 15.83        | 0.84         | 0.02  | 0.21                       | 4.66                    | 22.5                         | 0        |
| 1982 | 1     | 6                          | 0.55             | 3.66         | 1.01         | 0.02  | 0.47                       | 4.66                    | 22.5                         | 0        |
| 1982 | 2     | 1                          | 0.48             | 2.77         | 0.84         | 0.01  | 0.37                       | 4.66                    | 22.5                         | 0        |
| 1982 | 2     | 2                          | 0.22             | 1.14         | 0.84         | 0.01  | 0.63                       | 4.66                    | 22.5                         | 0        |
| 1982 | 2     | 3                          | 0.29             | 1.73         | 0.84         | 0.01  | 0.56                       | 4.66                    | 22.5                         | 0        |
| 1982 | 2     | 4                          | 0.22             | 1.57         | 0.84         | 0.01  | 0.63                       | 4.66                    | 22.5                         | 0        |
| 1982 | 2     | 5                          | 0.18             | 3.33         | 0.84         | 0.01  | 0.67                       | 4.66                    | 22.5                         | 0        |
| 1982 | 2     | 6                          | 0.13             | 2.83         | 0.5          | 0.01  | 0.38                       | 4.66                    | 22.5                         | 0        |
| 1982 | 3     | 1                          | 0.29             | 9.13         | 0.84         | 0.01  | 0.56                       | 4.66                    | 22.5                         | 0        |
| 1982 | 3     | 2                          | 0.37             | 31.73        | 0.84         | 0.01  | 0.48                       | 4.66                    | 22.5                         | 0        |
| 1982 | 3     | 3                          | 0.61             | 12.63        | 0.84         | 0.01  | 0.24                       | 4.66                    | 22.5                         | 0        |
| 1982 | 3     | 4                          | 0.59             | 16.98        | 0.84         | 0.01  | 0.26                       | 4.66                    | 22.5                         | 0        |
| 1982 | 3     | 5                          | 0.44             | 24.54        | 0.84         | 0.01  | 0.41                       | 4.66                    | 22.5                         | 0        |
| 1982 | 3     | 6                          | 0.42             | 8.13         | 1.01         | 0.01  | 0.6                        | 4.66                    | 22.5                         | 0        |
| 1982 | 4     | 1                          | 0.27             | 10.43        | 0.84         | 0.01  | 0.58                       | 4.66                    | 22.5                         | 0        |
| 1982 | 4     | 2                          | 0.23             | 10.64        | 0.84         | 0.01  | 0.62                       | 4.66                    | 22.5                         | 0        |
| 1982 | 4     | 3                          | 0.21             | 7.22         | 0.84         | 0.01  | 0.64                       | 4.66                    | 22.5                         | 0        |
| 1982 | 4     | 4                          | 0.34             | 17.29        | 0.84         | 0.01  | 0.51                       | 4.66                    | 22.5                         | 0        |
| 1982 | 4     | 5                          | 0.23             | 5.42         | 0.84         | 0.01  | 0.62                       | 4.66                    | 22.5                         | 0        |
| 1982 | 4     | 6                          | 0.33             | 7.44         | 0.84         | 0.01  | 0.52                       | 4.66                    | 22.5                         | 0        |
| 1982 | 5     | 1                          | 0.24             | 5.44         | 0.84         | 0.01  | 0.61                       | 4.66                    | 22.5                         | 0        |
| 1982 | 5     | 2                          | 0.21             | 3.58         | 0.84         | 0.01  | 0.64                       | 4.66                    | 22.5                         | 0        |
| 1982 | 5     | 3                          | 0.16             | 3.36         | 0.84         | 0.01  | 0.69                       | 4.66                    | 22.5                         | 0        |
| 1982 | 5     | 4                          | 0.11             | 1.94         | 0.84         | 0.01  | 0.74                       | 4.66                    | 22.5                         | 0        |
| 1982 | 5     | 5                          | 0.11             | 1.7          | 0.84         | 0.01  | 0.74                       | 4.66                    | 22.5                         | 0        |
| 1982 | 5     | 6                          | 0.17             | 2.31         | 1.01         | 0.01  | 0.86                       | 4.66                    | 22.5                         | 0        |
| 1982 | 6     | 1                          | 0.25             | 2.43         | 0.84         | 0.01  | 0.6                        | 4.66                    | 22.5                         | 0        |
| 1982 | 6     | 2                          | 0.18             | 3.79         | 0.84         | 0.01  | 0.67                       | 4.66                    | 22.5                         | 0        |
| 1982 | 6     | 3                          | 0.13             | 2.56         | 0.84         | 0.01  | 0.72                       | 4.66                    | 22.5                         | 0        |
| 1982 | 6     | 4                          | 0.11             | 2.54         | 0.84         | 0.01  | 0.74                       | 4.66                    | 22.5                         | 0        |
| 1982 | 6     | 5                          | 0.07             | 1.89         | 0.84         | 0.01  | 0.78                       | 4.66                    | 22.5                         | 0        |
| 1982 | 6     | 6                          | 0.11             | 1.29         | 0.84         | 0.01  | 0.74                       | 4.66                    | 22.5                         | 0        |

Table F-34 (4) Reservoir Operation Study for Existing Krenceng Dam (4/12)

Net supply yield: 1.94m<sup>3</sup>/sec  
 Water conveyance capacity: 2.00 m<sup>3</sup>/sec  
 of 27.2 km pipe line

| Year | Month | Serial No. of 5 day period | Inflow discharge |              | Supply yield | Evapo | Water conveyance from Cida | Krenceng Storage volume | Reservoir Water level (Bt-m) | Spillout |
|------|-------|----------------------------|------------------|--------------|--------------|-------|----------------------------|-------------------------|------------------------------|----------|
|      |       |                            | Krenceng         | Cidau intake |              |       |                            |                         |                              |          |
| 1982 | 7     | 1                          | 0.08             | 1.41         | 0.84         | 0.01  | 0.77                       | 4.66                    | 22.5                         | 0        |
| 1982 | 7     | 2                          | 0.07             | 1.28         | 0.84         | 0.01  | 0.79                       | 4.66                    | 22.5                         | 0        |
| 1982 | 7     | 3                          | 0.07             | 1.24         | 0.84         | 0.01  | 0.79                       | 4.66                    | 22.5                         | 0        |
| 1982 | 7     | 4                          | 0.17             | 1.79         | 0.84         | 0.01  | 0.68                       | 4.66                    | 22.5                         | 0        |
| 1982 | 7     | 5                          | 0.17             | 2.21         | 0.84         | 0.01  | 0.68                       | 4.66                    | 22.5                         | 0        |
| 1982 | 7     | 6                          | 0.2              | 4.78         | 1.01         | 0.01  | 0.82                       | 4.66                    | 22.5                         | 0        |
| 1982 | 8     | 1                          | 0.11             | 1.68         | 0.84         | 0.02  | 0.75                       | 4.66                    | 22.5                         | 0        |
| 1982 | 8     | 2                          | 0.08             | 1.28         | 0.84         | 0.02  | 0.77                       | 4.66                    | 22.5                         | 0        |
| 1982 | 8     | 3                          | 0.04             | 0.81         | 0.84         | 0.02  | 0.81                       | 4.65                    | 22.5                         | 0        |
| 1982 | 8     | 4                          | 0.03             | 0.69         | 0.84         | 0.02  | 0.69                       | 4.52                    | 22.35                        | 0        |
| 1982 | 8     | 5                          | 0.02             | 0.57         | 0.84         | 0.02  | 0.57                       | 4.26                    | 22.06                        | 0        |
| 1982 | 8     | 6                          | 0.02             | 0.54         | 1.01         | 0.02  | 0.54                       | 3.79                    | 21.55                        | 0        |
| 1982 | 9     | 1                          | 0.05             | 0.84         | 0.84         | 0.01  | 0.84                       | 3.83                    | 21.59                        | 0        |
| 1982 | 9     | 2                          | 0.05             | 0.57         | 0.84         | 0.01  | 0.57                       | 3.6                     | 21.34                        | 0        |
| 1982 | 9     | 3                          | 0.04             | 0.53         | 0.84         | 0.01  | 0.53                       | 3.32                    | 21.04                        | 0        |
| 1982 | 9     | 4                          | 0.04             | 0.45         | 0.84         | 0.01  | 0.45                       | 2.96                    | 20.65                        | 0        |
| 1982 | 9     | 5                          | 0.04             | 0.96         | 0.84         | 0.01  | 0.86                       | 3.02                    | 20.71                        | 0        |
| 1982 | 9     | 6                          | 0.05             | 1.67         | 0.84         | 0.01  | 0.86                       | 3.08                    | 20.78                        | 0        |
| 1982 | 10    | 1                          | 0.06             | 1.26         | 0.84         | 0.01  | 0.86                       | 3.16                    | 20.86                        | 0        |
| 1982 | 10    | 2                          | 0.04             | 0.56         | 0.84         | 0.01  | 0.56                       | 2.91                    | 20.59                        | 0        |
| 1982 | 10    | 3                          | 0.04             | 0.36         | 0.84         | 0.01  | 0.36                       | 2.47                    | 19.98                        | 0        |
| 1982 | 10    | 4                          | 0.1              | 0.96         | 0.84         | 0.01  | 0.86                       | 2.58                    | 20.15                        | 0        |
| 1982 | 10    | 5                          | 0.05             | 0.94         | 0.84         | 0.01  | 0.86                       | 2.65                    | 20.24                        | 0        |
| 1982 | 10    | 6                          | 0.05             | 0.63         | 1.01         | 0.01  | 0.63                       | 2.31                    | 19.75                        | 0        |
| 1982 | 11    | 1                          | 0.04             | 0.49         | 0.84         | 0.01  | 0.49                       | 1.99                    | 19.29                        | 0        |
| 1982 | 11    | 2                          | 0.06             | 5.34         | 0.84         | 0.01  | 0.86                       | 2.07                    | 19.4                         | 0        |
| 1982 | 11    | 3                          | 0.06             | 1.72         | 0.84         | 0.01  | 0.86                       | 2.15                    | 19.52                        | 0        |
| 1982 | 11    | 4                          | 0.06             | 0.78         | 0.84         | 0.01  | 0.78                       | 2.13                    | 19.5                         | 0        |
| 1982 | 11    | 5                          | 0.06             | 2.65         | 0.84         | 0.01  | 0.86                       | 2.21                    | 19.61                        | 0        |
| 1982 | 11    | 6                          | 0.06             | 2.54         | 0.84         | 0.01  | 0.86                       | 2.28                    | 19.71                        | 0        |
| 1982 | 12    | 1                          | 0.04             | 1.36         | 0.84         | 0.01  | 0.86                       | 2.34                    | 19.79                        | 0        |
| 1982 | 12    | 2                          | 0.04             | 0.42         | 0.84         | 0.01  | 0.42                       | 1.95                    | 19.24                        | 0        |
| 1982 | 12    | 3                          | 0.04             | 2.22         | 0.84         | 0.01  | 0.86                       | 2.01                    | 19.32                        | 0        |
| 1982 | 12    | 4                          | 0.04             | 2.79         | 0.84         | 0.01  | 0.86                       | 2.07                    | 19.41                        | 0        |
| 1982 | 12    | 5                          | 0.05             | 2.93         | 0.84         | 0.01  | 0.86                       | 2.13                    | 19.5                         | 0        |
| 1982 | 12    | 6                          | 0.13             | 8.58         | 1.01         | 0.01  | 1.04                       | 2.28                    | 19.71                        | 0        |
| 1983 | 1     | 1                          | 0.19             | 6.77         | 0.84         | 0.01  | 0.86                       | 2.48                    | 20                           | 0        |
| 1983 | 1     | 2                          | 0.11             | 6.98         | 0.84         | 0.01  | 0.86                       | 2.6                     | 20.18                        | 0        |
| 1983 | 1     | 3                          | 0.08             | 6.17         | 0.84         | 0.01  | 0.86                       | 2.7                     | 20.31                        | 0        |
| 1983 | 1     | 4                          | 0.12             | 11.05        | 0.84         | 0.01  | 0.86                       | 2.83                    | 20.5                         | 0        |
| 1983 | 1     | 5                          | 0.32             | 20.04        | 0.84         | 0.01  | 0.86                       | 3.17                    | 20.87                        | 0        |
| 1983 | 1     | 6                          | 0.06             | 13.66        | 1.01         | 0.02  | 1.04                       | 3.24                    | 20.95                        | 0        |
| 1983 | 2     | 1                          | 0.22             | 7.9          | 0.84         | 0.01  | 0.86                       | 3.47                    | 21.2                         | 0        |
| 1983 | 2     | 2                          | 0.22             | 9.4          | 0.84         | 0.01  | 0.86                       | 3.71                    | 21.46                        | 0        |
| 1983 | 2     | 3                          | 0.06             | 2.59         | 0.84         | 0.01  | 0.86                       | 3.78                    | 21.54                        | 0        |
| 1983 | 2     | 4                          | 0.14             | 2.82         | 0.84         | 0.01  | 0.86                       | 3.95                    | 21.7                         | 0        |
| 1983 | 2     | 5                          | 0.08             | 3.12         | 0.84         | 0.01  | 0.86                       | 4.02                    | 21.81                        | 0        |
| 1983 | 2     | 6                          | 0.26             | 2.49         | 0.5          | 0.01  | 0.52                       | 4.3                     | 22.11                        | 0        |
| 1983 | 3     | 1                          | 0.43             | 5.41         | 0.84         | 0.01  | 0.78                       | 4.66                    | 22.5                         | 0        |
| 1983 | 3     | 2                          | 0.19             | 2.72         | 0.84         | 0.01  | 0.66                       | 4.66                    | 22.5                         | 0        |
| 1983 | 3     | 3                          | 0.16             | 2.52         | 0.84         | 0.01  | 0.69                       | 4.66                    | 22.5                         | 0        |
| 1983 | 3     | 4                          | 0.06             | 1.99         | 0.84         | 0.01  | 0.79                       | 4.66                    | 22.5                         | 0        |
| 1983 | 3     | 5                          | 0.07             | 1.97         | 0.84         | 0.01  | 0.78                       | 4.66                    | 22.5                         | 0        |
| 1983 | 3     | 6                          | 0.31             | 3.53         | 1.01         | 0.01  | 0.71                       | 4.66                    | 22.5                         | 0        |
| 1983 | 4     | 1                          | 0.19             | 4.93         | 0.84         | 0.01  | 0.67                       | 4.66                    | 22.5                         | 0        |
| 1983 | 4     | 2                          | 0.3              | 4.37         | 0.84         | 0.01  | 0.55                       | 4.66                    | 22.5                         | 0        |
| 1983 | 4     | 3                          | 0.06             | 3.8          | 0.84         | 0.01  | 0.79                       | 4.66                    | 22.5                         | 0        |
| 1983 | 4     | 4                          | 0.14             | 4.52         | 0.84         | 0.01  | 0.72                       | 4.66                    | 22.5                         | 0        |
| 1983 | 4     | 5                          | 0.59             | 3.83         | 0.84         | 0.01  | 0.26                       | 4.66                    | 22.5                         | 0        |
| 1983 | 4     | 6                          | 0.45             | 4.72         | 0.84         | 0.01  | 0.4                        | 4.66                    | 22.5                         | 0        |

(Unit: 10 m<sup>3</sup>)

Table F-34 (5) Reservoir Operation Study for Existing Krenseng Dam (5/12)

Net supply yield: 1.94m<sup>3</sup>/sec  
Water conveyance capacity: 2.00 m<sup>3</sup>/sec  
of 27.2 km pipe line

(Unit: 10<sup>6</sup> m<sup>3</sup>)

| Year | Month | Serial No. of 5 day period | Inflow discharge |                | Supply yield | Evapo | Water conveyance from Cida | Krenseng Storage volume | Reservoir Water level (El-m) | Spillover |
|------|-------|----------------------------|------------------|----------------|--------------|-------|----------------------------|-------------------------|------------------------------|-----------|
|      |       |                            | Krenseng         | Ciganau intake |              |       |                            |                         |                              |           |
| 1983 | 5     | 1                          | 0.25             | 2.07           | 0.84         | 0.01  | 0.6                        | 4.66                    | 22.5                         | 0         |
| 1983 | 5     | 2                          | 0.46             | 2.03           | 0.84         | 0.01  | 0.39                       | 4.66                    | 22.5                         | 0         |
| 1983 | 5     | 3                          | 0.28             | 6.1            | 0.84         | 0.01  | 0.57                       | 4.66                    | 22.5                         | 0         |
| 1983 | 5     | 4                          | 0.28             | 3.08           | 0.84         | 0.01  | 0.57                       | 4.66                    | 22.5                         | 0         |
| 1983 | 5     | 5                          | 0.18             | 4.03           | 0.84         | 0.01  | 0.67                       | 4.66                    | 22.5                         | 0         |
| 1983 | 5     | 6                          | 0.27             | 3.11           | 1.01         | 0.01  | 0.75                       | 4.66                    | 22.5                         | 0         |
| 1983 | 6     | 1                          | 0.15             | 4.03           | 0.84         | 0.01  | 0.7                        | 4.66                    | 22.5                         | 0         |
| 1983 | 6     | 2                          | 0.97             | 3.43           | 0.84         | 0.01  | 0                          | 4.66                    | 22.5                         | 0.12      |
| 1983 | 6     | 3                          | 0.36             | 2.69           | 0.84         | 0.01  | 0.49                       | 4.66                    | 22.5                         | 0         |
| 1983 | 6     | 4                          | 0.21             | 3.92           | 0.84         | 0.01  | 0.63                       | 4.66                    | 22.5                         | 0         |
| 1983 | 6     | 5                          | 0.12             | 4.85           | 0.84         | 0.01  | 0.73                       | 4.66                    | 22.5                         | 0         |
| 1983 | 6     | 6                          | 0.27             | 5.14           | 0.84         | 0.01  | 0.58                       | 4.66                    | 22.5                         | 0         |
| 1983 | 7     | 1                          | 0.15             | 7.96           | 0.84         | 0.01  | 0.7                        | 4.66                    | 22.5                         | 0         |
| 1983 | 7     | 2                          | 0.02             | 4.92           | 0.84         | 0.01  | 0.83                       | 4.66                    | 22.5                         | 0         |
| 1983 | 7     | 3                          | 0.02             | 2.54           | 0.84         | 0.01  | 0.83                       | 4.66                    | 22.5                         | 0         |
| 1983 | 7     | 4                          | 0.05             | 3.36           | 0.84         | 0.01  | 0.8                        | 4.66                    | 22.5                         | 0         |
| 1983 | 7     | 5                          | 0.05             | 2.46           | 0.84         | 0.01  | 0.81                       | 4.66                    | 22.5                         | 0         |
| 1983 | 7     | 6                          | 0.06             | 3.37           | 1.01         | 0.01  | 0.96                       | 4.66                    | 22.5                         | 0         |
| 1983 | 8     | 1                          | 0.02             | 1.43           | 0.84         | 0.02  | 0.83                       | 4.66                    | 22.5                         | 0         |
| 1983 | 8     | 2                          | 0.02             | 0.68           | 0.84         | 0.02  | 0.68                       | 4.5                     | 22.33                        | 0         |
| 1983 | 8     | 3                          | 0.01             | 1.2            | 0.84         | 0.02  | 0.86                       | 4.52                    | 22.35                        | 0         |
| 1983 | 8     | 4                          | 0.01             | 1.48           | 0.84         | 0.02  | 0.86                       | 4.54                    | 22.38                        | 0         |
| 1983 | 8     | 5                          | 0.03             | 3.93           | 0.84         | 0.02  | 0.86                       | 4.58                    | 22.42                        | 0         |
| 1983 | 8     | 6                          | 0.01             | 1.06           | 1.01         | 0.02  | 1.04                       | 4.6                     | 22.44                        | 0         |
| 1983 | 9     | 1                          | 0                | 0.49           | 0.84         | 0.01  | 0.49                       | 4.25                    | 22.06                        | 0         |
| 1983 | 9     | 2                          | 0.01             | 0.76           | 0.84         | 0.01  | 0.76                       | 4.17                    | 21.96                        | 0         |
| 1983 | 9     | 3                          | 0.01             | 0.85           | 0.84         | 0.01  | 0.85                       | 4.16                    | 21.97                        | 0         |
| 1983 | 9     | 4                          | 0.01             | 0.7            | 0.84         | 0.01  | 0.7                        | 4.63                    | 21.82                        | 0         |
| 1983 | 9     | 5                          | 0.01             | 0.7            | 0.84         | 0.01  | 0.7                        | 3.89                    | 21.66                        | 0         |
| 1983 | 9     | 6                          | 0.01             | 0.54           | 0.84         | 0.01  | 0.54                       | 3.59                    | 21.33                        | 0         |
| 1983 | 10    | 1                          | 0                | 0.38           | 0.84         | 0.01  | 0.38                       | 3.11                    | 20.81                        | 0         |
| 1983 | 10    | 2                          | 0                | 0.29           | 0.84         | 0.01  | 0.29                       | 2.55                    | 20.11                        | 0         |
| 1983 | 10    | 3                          | 0                | 0.33           | 0.84         | 0.01  | 0.33                       | 2.03                    | 19.35                        | 0         |
| 1983 | 10    | 4                          | 0                | 0.37           | 0.84         | 0.01  | 0.37                       | 1.56                    | 18.58                        | 0         |
| 1983 | 10    | 5                          | 0.04             | 2.51           | 0.84         | 0.01  | 0.86                       | 1.61                    | 18.68                        | 0         |
| 1983 | 10    | 6                          | 0.05             | 6.55           | 1.01         | 0.01  | 1.04                       | 1.68                    | 18.81                        | 0         |
| 1983 | 11    | 1                          | 0.04             | 7.08           | 0.84         | 0.01  | 0.86                       | 1.74                    | 18.91                        | 0         |
| 1983 | 11    | 2                          | 0.08             | 5.71           | 0.84         | 0.01  | 0.86                       | 1.83                    | 19.06                        | 0         |
| 1983 | 11    | 3                          | 0.01             | 7.36           | 0.84         | 0.01  | 0.86                       | 1.86                    | 19.1                         | 0         |
| 1983 | 11    | 4                          | 0.47             | 39.04          | 0.84         | 0.01  | 0.86                       | 2.34                    | 19.8                         | 0         |
| 1983 | 11    | 5                          | 1.37             | 0.64           | 0.84         | 0.01  | 0.64                       | 3.5                     | 21.24                        | 1.91      |
| 1983 | 11    | 6                          | 3.91             | 21.87          | 0.84         | 0.01  | 0                          | 4.66                    | 22.5                         | 0         |
| 1983 | 12    | 1                          | 0.37             | 19.35          | 0.84         | 0.01  | 0.48                       | 4.66                    | 22.5                         | 0         |
| 1983 | 12    | 2                          | 0.36             | 10.29          | 0.84         | 0.01  | 0.5                        | 4.66                    | 22.5                         | 0         |
| 1983 | 12    | 3                          | 0.12             | 4.38           | 0.84         | 0.01  | 0.74                       | 4.66                    | 22.5                         | 0         |
| 1983 | 12    | 4                          | 0.08             | 4.43           | 0.84         | 0.01  | 0.77                       | 4.66                    | 22.5                         | 0         |
| 1983 | 12    | 5                          | 0.06             | 3.73           | 0.84         | 0.01  | 0.8                        | 4.66                    | 22.5                         | 0         |
| 1983 | 12    | 6                          | 0.08             | 7.05           | 1.01         | 0.02  | 0.95                       | 4.66                    | 22.5                         | 0         |
| 1984 | 1     | 1                          | 0.12             | 5.67           | 0.84         | 0.02  | 0.73                       | 4.66                    | 22.5                         | 0         |
| 1984 | 1     | 2                          | 0.23             | 1.38           | 0.84         | 0.02  | 0.62                       | 4.66                    | 22.5                         | 0         |
| 1984 | 1     | 3                          | 0.08             | 6.24           | 0.84         | 0.02  | 0.77                       | 4.66                    | 22.5                         | 0         |
| 1984 | 1     | 4                          | 0.13             | 6.94           | 0.84         | 0.02  | 0.72                       | 4.66                    | 22.5                         | 0         |
| 1984 | 1     | 5                          | 0.9              | 7.06           | 0.84         | 0.02  | 0                          | 4.66                    | 22.5                         | 0.04      |
| 1984 | 1     | 6                          | 1.69             | 9.84           | 1.01         | 0.02  | 0                          | 4.66                    | 22.5                         | 0.66      |
| 1984 | 2     | 1                          | 0.46             | 7.43           | 0.84         | 0.01  | 0.39                       | 4.66                    | 22.5                         | 0         |
| 1984 | 2     | 2                          | 0.34             | 12.52          | 0.84         | 0.01  | 0.51                       | 4.66                    | 22.5                         | 0         |
| 1984 | 2     | 3                          | 0.4              | 5.64           | 0.84         | 0.01  | 0.45                       | 4.66                    | 22.5                         | 0         |
| 1984 | 2     | 4                          | 0.8              | 4.15           | 0.84         | 0.01  | 0.06                       | 4.66                    | 22.5                         | 0         |
| 1984 | 2     | 5                          | 0.72             | 2.87           | 0.84         | 0.01  | 0.13                       | 4.66                    | 22.5                         | 0         |
| 1984 | 2     | 6                          | 0.46             | 6.03           | 0.67         | 0.01  | 0.22                       | 4.66                    | 22.5                         | 0         |

Table F-34 (6) Reservoir Operation Study for Existing Krenceng Dam (6/12)

Net supply yield: 1.94m<sup>3</sup>/sec  
 Water conveyance capacity: 2.00 m<sup>3</sup>/sec  
 of 27.2 km pipe line

(Unit: 10<sup>6</sup> m<sup>3</sup>)

| Year | Month | Serial No. of 5 day period | Inflow discharge |                | Supply yield | Evapo | Water conveyance from Cida | Krenceng Storage volume | Reservoir Water level (El-m) | Spillout |
|------|-------|----------------------------|------------------|----------------|--------------|-------|----------------------------|-------------------------|------------------------------|----------|
|      |       |                            | Krenceng         | Cidanan intake |              |       |                            |                         |                              |          |
| 1984 | 3     | 1                          | 0.38             | 5.87           | 0.84         | 0.01  | 0.48                       | 4.66                    | 22.5                         | 0        |
| 1984 | 3     | 2                          | 1.01             | 10.68          | 0.84         | 0.01  | 0                          | 4.66                    | 22.5                         | 0.16     |
| 1984 | 3     | 3                          | 1.41             | 12.95          | 0.84         | 0.01  | 0                          | 4.66                    | 22.5                         | 0.56     |
| 1984 | 3     | 4                          | 0.92             | 10.75          | 0.84         | 0.01  | 0                          | 4.66                    | 22.5                         | 0.07     |
| 1984 | 3     | 5                          | 1.78             | 19.09          | 0.84         | 0.01  | 0                          | 4.66                    | 22.5                         | 0.93     |
| 1984 | 3     | 6                          | 2.02             | 26.41          | 1.01         | 0.01  | 0                          | 4.66                    | 22.5                         | 1        |
| 1984 | 4     | 1                          | 0.18             | 11.88          | 0.84         | 0.01  | 0.67                       | 4.66                    | 22.5                         | 0        |
| 1984 | 4     | 2                          | 0.24             | 2.86           | 0.84         | 0.01  | 0.61                       | 4.66                    | 22.5                         | 0        |
| 1984 | 4     | 3                          | 0.16             | 3.83           | 0.84         | 0.01  | 0.69                       | 4.66                    | 22.5                         | 0        |
| 1984 | 4     | 4                          | 0.24             | 3.37           | 0.84         | 0.01  | 0.61                       | 4.66                    | 22.5                         | 0        |
| 1984 | 4     | 5                          | 0.18             | 4.38           | 0.84         | 0.01  | 0.67                       | 4.66                    | 22.5                         | 0        |
| 1984 | 4     | 6                          | 0.46             | 6.49           | 0.84         | 0.01  | 0.39                       | 4.66                    | 22.5                         | 0        |
| 1984 | 5     | 1                          | 0.5              | 5.85           | 0.84         | 0.01  | 0.35                       | 4.66                    | 22.5                         | 0        |
| 1984 | 5     | 2                          | 0.42             | 10.68          | 0.84         | 0.01  | 0.43                       | 4.66                    | 22.5                         | 0        |
| 1984 | 5     | 3                          | 0.22             | 15.63          | 0.84         | 0.01  | 0.63                       | 4.66                    | 22.5                         | 0        |
| 1984 | 5     | 4                          | 0.15             | 5.8            | 0.84         | 0.01  | 0.7                        | 4.66                    | 22.5                         | 0        |
| 1984 | 5     | 5                          | 0.24             | 3.97           | 0.84         | 0.01  | 0.61                       | 4.66                    | 22.5                         | 0        |
| 1984 | 5     | 6                          | 0.22             | 12.63          | 1.01         | 0.01  | 0.8                        | 4.66                    | 22.5                         | 0        |
| 1984 | 6     | 1                          | 0.2              | 6.23           | 0.84         | 0.01  | 0.65                       | 4.66                    | 22.5                         | 0        |
| 1984 | 6     | 2                          | 0.17             | 3.47           | 0.84         | 0.01  | 0.68                       | 4.66                    | 22.5                         | 0        |
| 1984 | 6     | 3                          | 0.21             | 3.15           | 0.84         | 0.01  | 0.64                       | 4.66                    | 22.5                         | 0        |
| 1984 | 6     | 4                          | 0.21             | 2.61           | 0.84         | 0.01  | 0.64                       | 4.66                    | 22.5                         | 0        |
| 1984 | 6     | 5                          | 0.14             | 3.12           | 0.84         | 0.01  | 0.71                       | 4.66                    | 22.5                         | 0        |
| 1984 | 6     | 6                          | 0.1              | 1.39           | 0.84         | 0.01  | 0.75                       | 4.66                    | 22.5                         | 0        |
| 1984 | 7     | 1                          | 0.34             | 2.29           | 0.84         | 0.01  | 0.61                       | 4.66                    | 22.5                         | 0        |
| 1984 | 7     | 2                          | 0.17             | 4.9            | 0.84         | 0.01  | 0.68                       | 4.66                    | 22.5                         | 0        |
| 1984 | 7     | 3                          | 0.09             | 3.29           | 0.84         | 0.01  | 0.76                       | 4.66                    | 22.5                         | 0        |
| 1984 | 7     | 4                          | 0.08             | 2.15           | 0.84         | 0.01  | 0.77                       | 4.66                    | 22.5                         | 0        |
| 1984 | 7     | 5                          | 0.16             | 2.76           | 0.84         | 0.01  | 0.69                       | 4.66                    | 22.5                         | 0        |
| 1984 | 7     | 6                          | 0.18             | 3.74           | 1.01         | 0.01  | 0.85                       | 4.66                    | 22.5                         | 0        |
| 1984 | 8     | 1                          | 0.09             | 2.5            | 0.84         | 0.02  | 0.79                       | 4.66                    | 22.5                         | 0        |
| 1984 | 8     | 2                          | 0.07             | 1.93           | 0.84         | 0.02  | 0.7                        | 4.66                    | 22.5                         | 0        |
| 1984 | 8     | 3                          | 0.15             | 1.48           | 0.84         | 0.02  | 0.76                       | 4.66                    | 22.5                         | 0        |
| 1984 | 8     | 4                          | 0.09             | 1.51           | 0.84         | 0.02  | 0.77                       | 4.66                    | 22.5                         | 0        |
| 1984 | 8     | 5                          | 0.08             | 1.4            | 0.84         | 0.02  | 0.84                       | 4.66                    | 22.5                         | 0        |
| 1984 | 8     | 6                          | 0.19             | 2.17           | 1.01         | 0.02  | 0.84                       | 4.66                    | 22.5                         | 0        |
| 1984 | 9     | 1                          | 0.11             | 1.67           | 0.84         | 0.01  | 0.74                       | 4.66                    | 22.5                         | 0        |
| 1984 | 9     | 2                          | 0.39             | 4.99           | 0.84         | 0.01  | 0.46                       | 4.66                    | 22.5                         | 0        |
| 1984 | 9     | 3                          | 0.4              | 6.26           | 0.84         | 0.01  | 0.45                       | 4.66                    | 22.5                         | 0        |
| 1984 | 9     | 4                          | 0.27             | 5.04           | 0.84         | 0.01  | 0.58                       | 4.66                    | 22.5                         | 0        |
| 1984 | 9     | 5                          | 0.18             | 4.38           | 0.84         | 0.01  | 0.67                       | 4.66                    | 22.5                         | 0        |
| 1984 | 9     | 6                          | 0.42             | 3.48           | 0.84         | 0.01  | 0.43                       | 4.66                    | 22.5                         | 0        |
| 1984 | 10    | 1                          | 0.48             | 10.4           | 0.84         | 0.01  | 0.38                       | 4.66                    | 22.5                         | 0        |
| 1984 | 10    | 2                          | 0.13             | 4.41           | 0.84         | 0.01  | 0.72                       | 4.66                    | 22.5                         | 0        |
| 1984 | 10    | 3                          | 0.22             | 2.02           | 0.84         | 0.01  | 0.63                       | 4.66                    | 22.5                         | 0        |
| 1984 | 10    | 4                          | 0.18             | 2.39           | 0.84         | 0.01  | 0.67                       | 4.66                    | 22.5                         | 0        |
| 1984 | 10    | 5                          | 0.22             | 2.31           | 0.84         | 0.01  | 0.64                       | 4.66                    | 22.5                         | 0        |
| 1984 | 10    | 6                          | 0.13             | 3.38           | 1.01         | 0.02  | 0.89                       | 4.66                    | 22.5                         | 0        |
| 1984 | 11    | 1                          | 0.15             | 1.61           | 0.84         | 0.01  | 0.71                       | 4.66                    | 22.5                         | 0        |
| 1984 | 11    | 2                          | 0.08             | 2.76           | 0.84         | 0.02  | 0.77                       | 4.66                    | 22.5                         | 0        |
| 1984 | 11    | 3                          | 0.08             | 4.87           | 0.84         | 0.02  | 0.77                       | 4.66                    | 22.5                         | 0        |
| 1984 | 11    | 4                          | 0.19             | 4.94           | 0.84         | 0.02  | 0.67                       | 4.66                    | 22.5                         | 0        |
| 1984 | 11    | 5                          | 0.14             | 3.57           | 0.84         | 0.02  | 0.71                       | 4.66                    | 22.5                         | 0        |
| 1984 | 11    | 6                          | 0.08             | 3.76           | 0.84         | 0.02  | 0.78                       | 4.66                    | 22.5                         | 0        |
| 1984 | 12    | 1                          | 0.1              | 19.91          | 0.84         | 0.01  | 0.75                       | 4.66                    | 22.5                         | 0        |
| 1984 | 12    | 2                          | 0.09             | 19.21          | 0.84         | 0.01  | 0.77                       | 4.66                    | 22.5                         | 0        |
| 1984 | 12    | 3                          | 0.15             | 7.94           | 0.84         | 0.01  | 0.71                       | 4.66                    | 22.5                         | 0        |
| 1984 | 12    | 4                          | 0.12             | 7.01           | 0.84         | 0.01  | 0.74                       | 4.66                    | 22.5                         | 0        |
| 1984 | 12    | 5                          | 0.1              | 3.33           | 0.84         | 0.01  | 0.75                       | 4.66                    | 22.5                         | 0        |
| 1984 | 12    | 6                          | 0.39             | 17.34          | 1.01         | 0.02  | 0.64                       | 4.66                    | 22.5                         | 0        |

Table F-34 (7) Reservoir Operation Study for Existing Krenceng Dam (7/12)

Net supply yield: 1.94m<sup>3</sup>/sec  
 Water conveyance capacity: 2.00 m<sup>3</sup>/sec  
 of 27.2 km pipe line

(Unit: 10<sup>6</sup> m<sup>3</sup>)

| Year | Month | Serial No. of 5 day period | Inflow discharge |              | Evapo | Water conveyance from Cida | Krenceng Storage volume | Reservoir Water level (EL-m) | Spillout |
|------|-------|----------------------------|------------------|--------------|-------|----------------------------|-------------------------|------------------------------|----------|
|      |       |                            | Krenceng         | Cidau intake |       |                            |                         |                              |          |
| 1985 | 1     | 1                          | 0.11             | 9.49         | 0.02  | 0.74                       | 4.66                    | 22.5                         | 0        |
| 1985 | 1     | 2                          | 0.41             | 8.38         | 0.02  | 0.45                       | 4.66                    | 22.5                         | 0        |
| 1985 | 1     | 3                          | 0.11             | 16.18        | 0.02  | 0.74                       | 4.66                    | 22.5                         | 0        |
| 1985 | 1     | 4                          | 0.09             | 5.53         | 0.02  | 0.77                       | 4.66                    | 22.5                         | 0        |
| 1985 | 1     | 5                          | 0.12             | 3.77         | 0.02  | 0.73                       | 4.66                    | 22.5                         | 0        |
| 1985 | 1     | 6                          | 0.23             | 6.98         | 0.02  | 0.79                       | 4.66                    | 22.5                         | 0        |
| 1985 | 2     | 1                          | 0.1              | 5.16         | 0.01  | 0.75                       | 4.66                    | 22.5                         | 0        |
| 1985 | 2     | 2                          | 0.09             | 5.12         | 0.01  | 0.77                       | 4.66                    | 22.5                         | 0        |
| 1985 | 2     | 3                          | 0.07             | 6.31         | 0.01  | 0.78                       | 4.66                    | 22.5                         | 0        |
| 1985 | 2     | 4                          | 0.05             | 3.27         | 0.01  | 0.8                        | 4.66                    | 22.5                         | 0        |
| 1985 | 2     | 5                          | 0.18             | 5.68         | 0.01  | 0.67                       | 4.66                    | 22.5                         | 0        |
| 1985 | 2     | 6                          | 0.03             | 3.67         | 0.01  | 0.48                       | 4.66                    | 22.5                         | 0        |
| 1985 | 3     | 1                          | 0.17             | 5.65         | 0.01  | 0.68                       | 4.66                    | 22.5                         | 0        |
| 1985 | 3     | 2                          | 0.38             | 18.22        | 0.01  | 0.47                       | 4.66                    | 22.5                         | 0        |
| 1985 | 3     | 3                          | 0.14             | 14.18        | 0.01  | 0.71                       | 4.66                    | 22.5                         | 0        |
| 1985 | 3     | 4                          | 0.15             | 4.8          | 0.01  | 0.7                        | 4.66                    | 22.5                         | 0        |
| 1985 | 3     | 5                          | 0.08             | 2.99         | 0.01  | 0.77                       | 4.66                    | 22.5                         | 0        |
| 1985 | 3     | 6                          | 0.15             | 2.65         | 0.01  | 0.87                       | 4.66                    | 22.5                         | 0        |
| 1985 | 4     | 1                          | 0.11             | 1.83         | 0.01  | 0.74                       | 4.66                    | 22.5                         | 0        |
| 1985 | 4     | 2                          | 0.15             | 2.37         | 0.01  | 0.7                        | 4.66                    | 22.5                         | 0        |
| 1985 | 4     | 3                          | 0.25             | 4.57         | 0.01  | 0.6                        | 4.66                    | 22.5                         | 0        |
| 1985 | 4     | 4                          | 0.57             | 9.42         | 0.01  | 0.28                       | 4.66                    | 22.5                         | 0        |
| 1985 | 4     | 5                          | 0.18             | 6.9          | 0.01  | 0.67                       | 4.66                    | 22.5                         | 0        |
| 1985 | 4     | 6                          | 0.18             | 7.61         | 0.01  | 0.67                       | 4.66                    | 22.5                         | 0        |
| 1985 | 5     | 1                          | 0.1              | 6.54         | 0.01  | 0.67                       | 4.66                    | 22.5                         | 0        |
| 1985 | 5     | 2                          | 0.08             | 5.09         | 0.01  | 0.75                       | 4.66                    | 22.5                         | 0        |
| 1985 | 5     | 3                          | 0.09             | 4.03         | 0.01  | 0.77                       | 4.66                    | 22.5                         | 0        |
| 1985 | 5     | 4                          | 0.56             | 3.38         | 0.01  | 0.76                       | 4.66                    | 22.5                         | 0        |
| 1985 | 5     | 5                          | 0.05             | 3.62         | 0.01  | 0.8                        | 4.66                    | 22.5                         | 0        |
| 1985 | 5     | 6                          | 0.09             | 3.49         | 0.01  | 0.93                       | 4.66                    | 22.5                         | 0        |
| 1985 | 6     | 1                          | 0.06             | 2.26         | 0.01  | 0.79                       | 4.66                    | 22.5                         | 0        |
| 1985 | 6     | 2                          | 0.08             | 2.06         | 0.01  | 0.77                       | 4.66                    | 22.5                         | 0        |
| 1985 | 6     | 3                          | 0.05             | 2.49         | 0.01  | 0.8                        | 4.66                    | 22.5                         | 0        |
| 1985 | 6     | 4                          | 0.06             | 3.07         | 0.01  | 0.79                       | 4.66                    | 22.5                         | 0        |
| 1985 | 6     | 5                          | 0.21             | 3.17         | 0.01  | 0.64                       | 4.66                    | 22.5                         | 0        |
| 1985 | 6     | 6                          | 0.06             | 2.9          | 0.01  | 0.79                       | 4.66                    | 22.5                         | 0        |
| 1985 | 7     | 1                          | 0.07             | 2.05         | 0.01  | 0.68                       | 4.66                    | 22.5                         | 0        |
| 1985 | 7     | 2                          | 0.14             | 2.08         | 0.01  | 0.71                       | 4.66                    | 22.5                         | 0        |
| 1985 | 7     | 3                          | 0.17             | 2.3          | 0.01  | 0.68                       | 4.66                    | 22.5                         | 0        |
| 1985 | 7     | 4                          | 0.17             | 2.46         | 0.01  | 0.68                       | 4.66                    | 22.5                         | 0        |
| 1985 | 7     | 5                          | 0.27             | 5.96         | 0.01  | 0.58                       | 4.66                    | 22.5                         | 0        |
| 1985 | 7     | 6                          | 0.11             | 7.88         | 0.01  | 0.91                       | 4.66                    | 22.5                         | 0        |
| 1985 | 8     | 1                          | 0.25             | 5.37         | 0.02  | 0.6                        | 4.66                    | 22.5                         | 0        |
| 1985 | 8     | 2                          | 0.09             | 5.21         | 0.02  | 0.76                       | 4.66                    | 22.5                         | 0        |
| 1985 | 8     | 3                          | 0.06             | 3.17         | 0.02  | 0.79                       | 4.66                    | 22.5                         | 0        |
| 1985 | 8     | 4                          | 0.06             | 2.71         | 0.02  | 0.79                       | 4.66                    | 22.5                         | 0        |
| 1985 | 8     | 5                          | 0.05             | 2.06         | 0.02  | 0.8                        | 4.66                    | 22.5                         | 0        |
| 1985 | 8     | 6                          | 0.07             | 1.82         | 0.02  | 0.96                       | 4.66                    | 22.5                         | 0        |
| 1985 | 9     | 1                          | 0.04             | 1.18         | 0.01  | 0.81                       | 4.66                    | 22.5                         | 0        |
| 1985 | 9     | 2                          | 0.08             | 1.2          | 0.01  | 0.77                       | 4.66                    | 22.5                         | 0        |
| 1985 | 9     | 3                          | 0.06             | 4.41         | 0.01  | 0.8                        | 4.66                    | 22.5                         | 0        |
| 1985 | 9     | 4                          | 0.05             | 3.4          | 0.01  | 0.81                       | 4.66                    | 22.5                         | 0        |
| 1985 | 9     | 5                          | 0.04             | 2.39         | 0.01  | 0.81                       | 4.66                    | 22.5                         | 0        |
| 1985 | 9     | 6                          | 0.1              | 2.22         | 0.01  | 0.76                       | 4.66                    | 22.5                         | 0        |
| 1985 | 10    | 1                          | 0.12             | 1.75         | 0.01  | 0.74                       | 4.66                    | 22.5                         | 0        |
| 1985 | 10    | 2                          | 0.1              | 2.66         | 0.01  | 0.75                       | 4.66                    | 22.5                         | 0        |
| 1985 | 10    | 3                          | 0.07             | 5.63         | 0.01  | 0.78                       | 4.66                    | 22.5                         | 0        |
| 1985 | 10    | 4                          | 0.34             | 7.23         | 0.01  | 0.51                       | 4.66                    | 22.5                         | 0        |
| 1985 | 10    | 5                          | 0.07             | 9.42         | 0.01  | 0.78                       | 4.66                    | 22.5                         | 0        |
| 1985 | 10    | 6                          | 0.08             | 5.41         | 0.02  | 0.94                       | 4.66                    | 22.5                         | 0        |

Table F-34 (8) Reservoir Operation Study for Existing Krenceng Dam (8/12)

Net supply yield: 1.94m<sup>3</sup>/sec  
 Water conveyance capacity: 2.00 m<sup>3</sup>/sec  
 of 27.2 km pipe line

(Unit: 10<sup>6</sup> m<sup>3</sup>)

| Year | Month | Serial No. of 5 day period | Inflow discharge |               | Supply yield | Evapo | Water conveyance from Cida | Krenceng Storage volume | Reservoir Water level (El.m) | Spillover |
|------|-------|----------------------------|------------------|---------------|--------------|-------|----------------------------|-------------------------|------------------------------|-----------|
|      |       |                            | Krenceng         | Cidaru intake |              |       |                            |                         |                              |           |
| 1985 | 11    | 1                          | 0.08             | 4.09          | 0.84         | 0.02  | 0.77                       | 4.66                    | 22.5                         | 0         |
| 1985 | 11    | 2                          | 0.15             | 3.88          | 0.84         | 0.02  | 0.71                       | 4.66                    | 22.5                         | 0         |
| 1985 | 11    | 3                          | 0.06             | 4.31          | 0.84         | 0.02  | 0.8                        | 4.66                    | 22.5                         | 0         |
| 1985 | 11    | 4                          | 0.04             | 3             | 0.84         | 0.02  | 0.81                       | 4.66                    | 22.5                         | 0         |
| 1985 | 11    | 5                          | 0.06             | 3.71          | 0.84         | 0.02  | 0.79                       | 4.66                    | 22.5                         | 0         |
| 1985 | 11    | 6                          | 0.1              | 6.58          | 0.84         | 0.02  | 0.75                       | 4.66                    | 22.5                         | 0         |
| 1985 | 12    | 1                          | 0.3              | 14.57         | 0.84         | 0.01  | 0.55                       | 4.66                    | 22.5                         | 0         |
| 1985 | 12    | 2                          | 0.12             | 12.34         | 0.84         | 0.01  | 0.73                       | 4.66                    | 22.5                         | 0         |
| 1985 | 12    | 3                          | 0.05             | 4.18          | 0.84         | 0.01  | 0.8                        | 4.66                    | 22.5                         | 0         |
| 1985 | 12    | 4                          | 0.08             | 1.9           | 0.84         | 0.01  | 0.78                       | 4.66                    | 22.5                         | 0         |
| 1985 | 12    | 5                          | 0.12             | 1.76          | 0.84         | 0.01  | 0.73                       | 4.66                    | 22.5                         | 0         |
| 1985 | 12    | 6                          | 0.11             | 2.2           | 1.01         | 0.02  | 0.91                       | 4.66                    | 22.5                         | 0         |
| 1986 | 1     | 1                          | 0.08             | 6.53          | 0.84         | 0.02  | 0.78                       | 4.66                    | 22.5                         | 0         |
| 1986 | 1     | 2                          | 0.84             | 20.99         | 0.84         | 0.02  | 0.02                       | 4.66                    | 22.5                         | 0         |
| 1986 | 1     | 3                          | 0.29             | 22.16         | 0.84         | 0.02  | 0.56                       | 4.66                    | 22.5                         | 0         |
| 1986 | 1     | 4                          | 0.43             | 11.32         | 0.84         | 0.02  | 0.43                       | 4.66                    | 22.5                         | 0         |
| 1986 | 1     | 5                          | 1.2              | 23.29         | 0.84         | 0.02  | 0                          | 4.66                    | 22.5                         | 0.94      |
| 1986 | 1     | 6                          | 0.91             | 26.46         | 1.01         | 0.02  | 0.11                       | 4.66                    | 22.5                         | 0         |
| 1986 | 2     | 1                          | 0.34             | 1.229         | 0.84         | 0.01  | 0.51                       | 4.66                    | 22.5                         | 0         |
| 1986 | 2     | 2                          | 0.27             | 7.98          | 0.84         | 0.01  | 0.58                       | 4.66                    | 22.5                         | 0         |
| 1986 | 2     | 3                          | 0.48             | 10.55         | 0.84         | 0.01  | 0.37                       | 4.66                    | 22.5                         | 0         |
| 1986 | 2     | 4                          | 0.17             | 9.01          | 0.84         | 0.01  | 0.68                       | 4.66                    | 22.5                         | 0         |
| 1986 | 2     | 5                          | 0.23             | 7.44          | 0.84         | 0.01  | 0.62                       | 4.66                    | 22.5                         | 0         |
| 1986 | 2     | 6                          | 0.15             | 3.56          | 0.5          | 0.01  | 0.36                       | 4.66                    | 22.5                         | 0         |
| 1986 | 3     | 1                          | 0.26             | 5.17          | 0.84         | 0.01  | 0.59                       | 4.66                    | 22.5                         | 0         |
| 1986 | 3     | 2                          | 0.16             | 4.34          | 0.84         | 0.01  | 0.69                       | 4.66                    | 22.5                         | 0         |
| 1986 | 3     | 3                          | 0.24             | 3.49          | 0.84         | 0.01  | 0.61                       | 4.66                    | 22.5                         | 0         |
| 1986 | 3     | 4                          | 0.19             | 2.95          | 0.84         | 0.01  | 0.66                       | 4.66                    | 22.5                         | 0         |
| 1986 | 3     | 5                          | 0.18             | 12.63         | 0.84         | 0.01  | 0.67                       | 4.66                    | 22.5                         | 0         |
| 1986 | 3     | 6                          | 0.15             | 27.87         | 1.01         | 0.01  | 0.65                       | 4.66                    | 22.5                         | 0         |
| 1986 | 4     | 1                          | 0.3              | 10.56         | 0.84         | 0.01  | 0.56                       | 4.66                    | 22.5                         | 0         |
| 1986 | 4     | 2                          | 0.21             | 10.38         | 0.84         | 0.01  | 0.64                       | 4.66                    | 22.5                         | 0         |
| 1986 | 4     | 3                          | 0.28             | 8.2           | 0.84         | 0.01  | 0.57                       | 4.66                    | 22.5                         | 0         |
| 1986 | 4     | 4                          | 0.17             | 7.77          | 0.84         | 0.01  | 0.68                       | 4.66                    | 22.5                         | 0         |
| 1986 | 4     | 5                          | 0.13             | 4.78          | 0.84         | 0.01  | 0.72                       | 4.66                    | 22.5                         | 0         |
| 1986 | 4     | 6                          | 0.21             | 3.75          | 0.84         | 0.01  | 0.64                       | 4.66                    | 22.5                         | 0         |
| 1986 | 5     | 1                          | 0.1              | 5.48          | 0.84         | 0.01  | 0.75                       | 4.66                    | 22.5                         | 0         |
| 1986 | 5     | 2                          | 0.15             | 4.23          | 0.84         | 0.01  | 0.7                        | 4.66                    | 22.5                         | 0         |
| 1986 | 5     | 3                          | 0.17             | 4.24          | 0.84         | 0.01  | 0.68                       | 4.66                    | 22.5                         | 0         |
| 1986 | 5     | 4                          | 0.08             | 4.06          | 0.84         | 0.01  | 0.74                       | 4.66                    | 22.5                         | 0         |
| 1986 | 5     | 5                          | 0.11             | 2.58          | 0.84         | 0.01  | 0.77                       | 4.66                    | 22.5                         | 0         |
| 1986 | 5     | 6                          | 0.1              | 2.74          | 1.01         | 0.01  | 0.92                       | 4.66                    | 22.5                         | 0         |
| 1986 | 6     | 1                          | 0.06             | 2.56          | 0.84         | 0.01  | 0.79                       | 4.66                    | 22.5                         | 0         |
| 1986 | 6     | 2                          | 0.11             | 2.39          | 0.84         | 0.01  | 0.74                       | 4.66                    | 22.5                         | 0         |
| 1986 | 6     | 3                          | 0.22             | 2.19          | 0.84         | 0.01  | 0.63                       | 4.66                    | 22.5                         | 0         |
| 1986 | 6     | 4                          | 0.09             | 2.23          | 0.84         | 0.01  | 0.76                       | 4.66                    | 22.5                         | 0         |
| 1986 | 6     | 5                          | 0.05             | 2.56          | 0.84         | 0.01  | 0.8                        | 4.66                    | 22.5                         | 0         |
| 1986 | 6     | 6                          | 0.06             | 1.38          | 0.84         | 0.01  | 0.79                       | 4.66                    | 22.5                         | 0         |
| 1986 | 7     | 1                          | 0.1              | 1.21          | 0.84         | 0.01  | 0.76                       | 4.66                    | 22.5                         | 0         |
| 1986 | 7     | 2                          | 0.09             | 1.38          | 0.84         | 0.01  | 0.76                       | 4.66                    | 22.5                         | 0         |
| 1986 | 7     | 3                          | 0.3              | 2.01          | 0.84         | 0.01  | 0.55                       | 4.66                    | 22.5                         | 0         |
| 1986 | 7     | 4                          | 0.15             | 1.39          | 0.84         | 0.01  | 0.7                        | 4.66                    | 22.5                         | 0         |
| 1986 | 7     | 5                          | 0.08             | 1.08          | 0.84         | 0.01  | 0.77                       | 4.66                    | 22.5                         | 0         |
| 1986 | 7     | 6                          | 0.14             | 2.56          | 1.01         | 0.01  | 0.88                       | 4.66                    | 22.5                         | 0         |
| 1986 | 8     | 1                          | 0.05             | 2.62          | 0.84         | 0.02  | 0.81                       | 4.66                    | 22.5                         | 0         |
| 1986 | 8     | 2                          | 0.05             | 3.14          | 0.84         | 0.02  | 0.8                        | 4.66                    | 22.5                         | 0         |
| 1986 | 8     | 3                          | 0.15             | 3.71          | 0.84         | 0.02  | 0.7                        | 4.66                    | 22.5                         | 0         |
| 1986 | 8     | 4                          | 0.07             | 2.44          | 0.84         | 0.02  | 0.79                       | 4.66                    | 22.5                         | 0         |
| 1986 | 8     | 5                          | 0.05             | 1.25          | 0.84         | 0.02  | 0.81                       | 4.66                    | 22.5                         | 0         |
| 1986 | 8     | 6                          | 0.08             | 1.2           | 1.01         | 0.02  | 0.94                       | 4.66                    | 22.5                         | 0         |

Table F-34 (9) Reservoir Operation Study for Existing Krenceng Dam (9/12)

Net supply yield: 1.94m<sup>3</sup>/sec  
 Water conveyance capacity: 2.00 m<sup>3</sup>/sec  
 of 27.2 km pipe line

(Unit: 10<sup>6</sup> m<sup>3</sup>)

| Year | Month | Serial No. of 5 day period | Inflow discharge |                | Evapo | Water conveyance from Cida | Krenceng Storage volume | Reservoir Water level (El-m) | Spillover |
|------|-------|----------------------------|------------------|----------------|-------|----------------------------|-------------------------|------------------------------|-----------|
|      |       |                            | Krenceng         | Cidamau Inlake |       |                            |                         |                              |           |
| 1986 | 9     | 1                          | 0.06             | 0.81           | 0.01  | 0.79                       | 4.66                    | 22.5                         | 0         |
| 1986 | 9     | 2                          | 0.14             | 1.34           | 0.01  | 0.71                       | 4.66                    | 22.5                         | 0         |
| 1986 | 9     | 3                          | 0.14             | 2.58           | 0.01  | 0.71                       | 4.66                    | 22.5                         | 0         |
| 1986 | 9     | 4                          | 0.07             | 2.87           | 0.01  | 0.78                       | 4.66                    | 22.5                         | 0         |
| 1986 | 9     | 5                          | 0.05             | 2.95           | 0.01  | 0.8                        | 4.66                    | 22.5                         | 0         |
| 1986 | 9     | 6                          | 0.06             | 4.01           | 0.01  | 0.79                       | 4.66                    | 22.5                         | 0         |
| 1986 | 10    | 1                          | 0.18             | 3.4            | 0.01  | 0.67                       | 4.66                    | 22.5                         | 0         |
| 1986 | 10    | 2                          | 0.13             | 2.28           | 0.01  | 0.73                       | 4.66                    | 22.5                         | 0         |
| 1986 | 10    | 3                          | 0.07             | 3.81           | 0.01  | 0.78                       | 4.66                    | 22.5                         | 0         |
| 1986 | 10    | 4                          | 0.06             | 4.15           | 0.01  | 0.79                       | 4.66                    | 22.5                         | 0         |
| 1986 | 10    | 5                          | 0.04             | 2.63           | 0.01  | 0.81                       | 4.66                    | 22.5                         | 0         |
| 1986 | 10    | 6                          | 0.3              | 8.24           | 0.02  | 0.72                       | 4.66                    | 22.5                         | 0         |
| 1986 | 11    | 1                          | 0.1              | 9.17           | 0.02  | 0.75                       | 4.66                    | 22.5                         | 0         |
| 1986 | 11    | 2                          | 0.2              | 14.22          | 0.02  | 0.66                       | 4.66                    | 22.5                         | 0         |
| 1986 | 11    | 3                          | 0.17             | 23.09          | 0.02  | 0.69                       | 4.66                    | 22.5                         | 0         |
| 1986 | 11    | 4                          | 0.25             | 9.96           | 0.02  | 0.61                       | 4.66                    | 22.5                         | 0         |
| 1986 | 11    | 5                          | 0.1              | 4.08           | 0.02  | 0.61                       | 4.66                    | 22.5                         | 0         |
| 1986 | 11    | 6                          | 0.19             | 5.29           | 0.02  | 0.67                       | 4.66                    | 22.5                         | 0         |
| 1986 | 12    | 1                          | 0.06             | 5.16           | 0.01  | 0.79                       | 4.66                    | 22.5                         | 0         |
| 1986 | 12    | 2                          | 0.05             | 2.02           | 0.01  | 0.81                       | 4.66                    | 22.5                         | 0         |
| 1986 | 12    | 3                          | 0.22             | 6.15           | 0.01  | 0.63                       | 4.66                    | 22.5                         | 0         |
| 1986 | 12    | 4                          | 0.28             | 9.62           | 0.01  | 0.57                       | 4.66                    | 22.5                         | 0         |
| 1986 | 12    | 5                          | 0.06             | 5.17           | 0.01  | 0.79                       | 4.66                    | 22.5                         | 0         |
| 1986 | 12    | 6                          | 0.11             | 3.79           | 0.02  | 0.91                       | 4.66                    | 22.5                         | 0         |
| 1987 | 1     | 1                          | 0.16             | 4.97           | 0.02  | 0.69                       | 4.66                    | 22.5                         | 0         |
| 1987 | 1     | 2                          | 0.61             | 19.07          | 0.02  | 0.24                       | 4.66                    | 22.5                         | 0         |
| 1987 | 1     | 3                          | 0.49             | 26.46          | 0.02  | 0.36                       | 4.66                    | 22.5                         | 0         |
| 1987 | 1     | 4                          | 0.18             | 14.77          | 0.02  | 0.68                       | 4.66                    | 22.5                         | 0         |
| 1987 | 1     | 5                          | 0.23             | 9.09           | 0.02  | 0.63                       | 4.66                    | 22.5                         | 0         |
| 1987 | 1     | 6                          | 0.29             | 10.66          | 0.02  | 0.73                       | 4.66                    | 22.5                         | 0         |
| 1987 | 2     | 1                          | 0.14             | 7.7            | 0.01  | 0.71                       | 4.66                    | 22.5                         | 0         |
| 1987 | 2     | 2                          | 0.38             | 12.17          | 0.01  | 0.48                       | 4.66                    | 22.5                         | 0         |
| 1987 | 2     | 3                          | 0.15             | 11             | 0.01  | 0.7                        | 4.66                    | 22.5                         | 0         |
| 1987 | 2     | 4                          | 0.2              | 8.8            | 0.01  | 0.65                       | 4.66                    | 22.5                         | 0         |
| 1987 | 2     | 5                          | 0.13             | 18.57          | 0.01  | 0.72                       | 4.66                    | 22.5                         | 0         |
| 1987 | 2     | 6                          | 0.46             | 11.49          | 0.01  | 0.05                       | 4.66                    | 22.5                         | 0         |
| 1987 | 3     | 1                          | 0.25             | 15.71          | 0.01  | 0.6                        | 4.66                    | 22.5                         | 0         |
| 1987 | 3     | 2                          | 0.14             | 15.69          | 0.01  | 0.71                       | 4.66                    | 22.5                         | 0         |
| 1987 | 3     | 3                          | 0.11             | 8.44           | 0.01  | 0.74                       | 4.66                    | 22.5                         | 0         |
| 1987 | 3     | 4                          | 0.09             | 3.67           | 0.01  | 0.76                       | 4.66                    | 22.5                         | 0         |
| 1987 | 3     | 5                          | 0.13             | 5.62           | 0.01  | 0.86                       | 4.66                    | 22.5                         | 0         |
| 1987 | 3     | 6                          | 0.16             | 5.03           | 0.01  | 0.73                       | 4.66                    | 22.5                         | 0         |
| 1987 | 4     | 1                          | 0.12             | 6.52           | 0.01  | 0.75                       | 4.66                    | 22.5                         | 0         |
| 1987 | 4     | 2                          | 0.1              | 6.98           | 0.01  | 0.75                       | 4.66                    | 22.5                         | 0         |
| 1987 | 4     | 3                          | 0.1              | 6.76           | 0.01  | 0.75                       | 4.66                    | 22.5                         | 0         |
| 1987 | 4     | 4                          | 0.09             | 2.98           | 0.01  | 0.76                       | 4.66                    | 22.5                         | 0         |
| 1987 | 4     | 5                          | 0.31             | 4.85           | 0.01  | 0.54                       | 4.66                    | 22.5                         | 0         |
| 1987 | 4     | 6                          | 0.09             | 9.74           | 0.01  | 0.65                       | 4.66                    | 22.5                         | 0         |
| 1987 | 5     | 1                          | 0.2              | 7.51           | 0.01  | 0.59                       | 4.66                    | 22.5                         | 0         |
| 1987 | 5     | 2                          | 0.26             | 8.58           | 0.01  | 0.66                       | 4.66                    | 22.5                         | 0         |
| 1987 | 5     | 3                          | 0.19             | 7.27           | 0.01  | 0.7                        | 4.66                    | 22.5                         | 0         |
| 1987 | 5     | 4                          | 0.15             | 3.78           | 0.01  | 0.78                       | 4.66                    | 22.5                         | 0         |
| 1987 | 5     | 5                          | 0.07             | 4.14           | 0.01  | 0.93                       | 4.66                    | 22.5                         | 0         |
| 1987 | 5     | 6                          | 0.09             | 2.98           | 0.01  | 0.76                       | 4.66                    | 22.5                         | 0         |
| 1987 | 6     | 1                          | 0.09             | 3.03           | 0.01  | 0.75                       | 4.66                    | 22.5                         | 0         |
| 1987 | 6     | 2                          | 0.1              | 3.3            | 0.01  | 0.72                       | 4.66                    | 22.5                         | 0         |
| 1987 | 6     | 3                          | 0.13             | 3.28           | 0.01  | 0.77                       | 4.66                    | 22.5                         | 0         |
| 1987 | 6     | 4                          | 0.08             | 2.98           | 0.01  | 0.77                       | 4.66                    | 22.5                         | 0         |
| 1987 | 6     | 5                          | 0.08             | 2.63           | 0.01  | 0.78                       | 4.66                    | 22.5                         | 0         |
| 1987 | 6     | 6                          | 0.07             | 2.63           | 0.01  | 0.78                       | 4.66                    | 22.5                         | 0         |



Table F-34 (10) Reservoir Operation Study for Existing Krenceng Dam (10/12)

Net supply yield: 1.94m<sup>3</sup>/sec  
 Water conveyance capacity: 2.00 m<sup>3</sup>/sec  
 of 27.2 km pipe line

(Unit: 10<sup>6</sup> m<sup>3</sup>)

| Year | Month | Serial No. of 5 day period | Inflow discharge |               | Supply yield | Evapo | Water conveyance from Cida | Krenceng Storage volume | Reservoir Water level (El-m) | Spillout |
|------|-------|----------------------------|------------------|---------------|--------------|-------|----------------------------|-------------------------|------------------------------|----------|
|      |       |                            | Krenceng         | Cidahu intake |              |       |                            |                         |                              |          |
| 1987 | 7     | 1                          | 0.06             | 2.33          | 0.84         | 0.01  | 0.79                       | 4.66                    | 22.5                         | 0        |
| 1987 | 7     | 2                          | 0.05             | 1.78          | 0.84         | 0.01  | 0.8                        | 4.66                    | 22.5                         | 0        |
| 1987 | 7     | 3                          | 0.04             | 1.43          | 0.84         | 0.01  | 0.81                       | 4.66                    | 22.5                         | 0        |
| 1987 | 7     | 4                          | 0.04             | 1.06          | 0.84         | 0.01  | 0.81                       | 4.66                    | 22.5                         | 0        |
| 1987 | 7     | 5                          | 0.05             | 1.11          | 0.84         | 0.01  | 0.81                       | 4.66                    | 22.5                         | 0        |
| 1987 | 7     | 6                          | 0.05             | 1.64          | 1.01         | 0.01  | 0.97                       | 4.66                    | 22.5                         | 0        |
| 1987 | 8     | 1                          | 0.04             | 1.26          | 0.84         | 0.02  | 0.81                       | 4.66                    | 22.5                         | 0        |
| 1987 | 8     | 2                          | 0.04             | 0.93          | 0.84         | 0.02  | 0.82                       | 4.66                    | 22.5                         | 0        |
| 1987 | 8     | 3                          | 0.04             | 1.02          | 0.84         | 0.02  | 0.82                       | 4.66                    | 22.5                         | 0        |
| 1987 | 8     | 4                          | 0.04             | 0.79          | 0.84         | 0.02  | 0.79                       | 4.63                    | 22.47                        | 0        |
| 1987 | 8     | 5                          | 0.04             | 0.66          | 0.84         | 0.02  | 0.66                       | 4.47                    | 22.3                         | 0        |
| 1987 | 8     | 6                          | 0.05             | 0.66          | 1.01         | 0.02  | 0.66                       | 4.16                    | 21.95                        | 0        |
| 1987 | 9     | 1                          | 0.04             | 0.59          | 0.84         | 0.01  | 0.59                       | 3.87                    | 21.64                        | 0        |
| 1987 | 9     | 2                          | 0.04             | 0.49          | 0.84         | 0.01  | 0.49                       | 3.55                    | 21.29                        | 0        |
| 1987 | 9     | 3                          | 0.04             | 0.49          | 0.84         | 0.01  | 0.49                       | 3.22                    | 20.93                        | 0        |
| 1987 | 9     | 4                          | 0.05             | 0.49          | 0.84         | 0.01  | 0.49                       | 2.91                    | 20.59                        | 0        |
| 1987 | 9     | 5                          | 0.04             | 0.49          | 0.84         | 0.01  | 0.49                       | 2.59                    | 20.16                        | 0        |
| 1987 | 9     | 6                          | 0.04             | 0.49          | 0.84         | 0.01  | 0.49                       | 2.27                    | 19.69                        | 0        |
| 1987 | 10    | 1                          | 0.04             | 0.5           | 0.84         | 0.01  | 0.5                        | 1.96                    | 19.25                        | 0        |
| 1987 | 10    | 2                          | 0.04             | 0.49          | 0.84         | 0.01  | 0.49                       | 1.64                    | 18.74                        | 0        |
| 1987 | 10    | 3                          | 0.04             | 1.21          | 0.84         | 0.01  | 0.86                       | 1.7                     | 18.84                        | 0        |
| 1987 | 10    | 4                          | 0.04             | 0.93          | 0.84         | 0.01  | 0.86                       | 1.75                    | 18.94                        | 0        |
| 1987 | 10    | 5                          | 0.04             | 1.09          | 0.84         | 0.01  | 0.86                       | 1.81                    | 19.05                        | 0        |
| 1987 | 10    | 6                          | 0.05             | 0.8           | 1.01         | 0.01  | 0.8                        | 1.64                    | 18.74                        | 0        |
| 1987 | 11    | 1                          | 0.04             | 0.67          | 0.84         | 0.01  | 0.67                       | 1.5                     | 18.49                        | 0        |
| 1987 | 11    | 2                          | 0.1              | 1.15          | 0.84         | 0.01  | 0.86                       | 1.63                    | 18.71                        | 0        |
| 1987 | 11    | 3                          | 0.05             | 2.5           | 0.84         | 0.01  | 0.86                       | 1.7                     | 18.94                        | 0        |
| 1987 | 11    | 4                          | 0.04             | 2.29          | 0.84         | 0.01  | 0.86                       | 1.75                    | 18.94                        | 0        |
| 1987 | 11    | 5                          | 0.04             | 1.42          | 0.84         | 0.01  | 0.86                       | 1.81                    | 19.05                        | 0        |
| 1987 | 11    | 6                          | 0.04             | 0.87          | 0.84         | 0.01  | 0.86                       | 1.86                    | 19.11                        | 0        |
| 1987 | 12    | 1                          | 0.04             | 0.84          | 0.84         | 0.01  | 0.86                       | 1.86                    | 19.16                        | 0        |
| 1987 | 12    | 2                          | 0.05             | 1.44          | 0.84         | 0.01  | 0.86                       | 1.97                    | 19.26                        | 0        |
| 1987 | 12    | 3                          | 0.07             | 3.16          | 0.84         | 0.01  | 0.86                       | 2.05                    | 19.38                        | 0        |
| 1987 | 12    | 4                          | 0.23             | 3.94          | 0.84         | 0.01  | 0.86                       | 2.35                    | 19.81                        | 0        |
| 1987 | 12    | 5                          | 0.06             | 5.7           | 0.84         | 0.01  | 0.86                       | 2.43                    | 19.92                        | 0        |
| 1987 | 12    | 6                          | 0.05             | 3.8           | 1.01         | 0.01  | 1.04                       | 2.49                    | 20.02                        | 0        |
| 1988 | 1     | 1                          | 0.04             | 1.44          | 0.84         | 0.01  | 0.86                       | 2.55                    | 20.09                        | 0        |
| 1988 | 1     | 2                          | 0.07             | 0.77          | 0.84         | 0.01  | 0.77                       | 2.54                    | 20.09                        | 0        |
| 1988 | 1     | 3                          | 0.07             | 0.85          | 0.84         | 0.01  | 0.85                       | 2.61                    | 20.19                        | 0        |
| 1988 | 1     | 4                          | 0.12             | 2.1           | 0.84         | 0.01  | 0.86                       | 2.74                    | 20.38                        | 0        |
| 1988 | 1     | 5                          | 0.08             | 3.25          | 0.84         | 0.01  | 0.86                       | 2.84                    | 20.51                        | 0        |
| 1988 | 1     | 6                          | 0.4              | 8.29          | 1.01         | 0.01  | 1.04                       | 3.25                    | 20.97                        | 0        |
| 1988 | 2     | 1                          | 1.26             | 16.54         | 0.84         | 0.01  | 0.86                       | 4.53                    | 22.36                        | 0        |
| 1988 | 2     | 2                          | 0.87             | 20.76         | 0.84         | 0.01  | 0.86                       | 4.66                    | 22.5                         | 0        |
| 1988 | 2     | 3                          | 0.16             | 14.78         | 0.84         | 0.01  | 0.69                       | 4.66                    | 22.5                         | 0        |
| 1988 | 2     | 4                          | 0.08             | 21.66         | 0.84         | 0.01  | 0.78                       | 4.66                    | 22.5                         | 0        |
| 1988 | 2     | 5                          | 0.07             | 10.92         | 0.84         | 0.01  | 0.78                       | 4.66                    | 22.5                         | 0        |
| 1988 | 2     | 6                          | 0.05             | 2.72          | 0.67         | 0.01  | 0.63                       | 4.66                    | 22.5                         | 0        |
| 1988 | 3     | 1                          | 0.08             | 6.38          | 0.84         | 0.01  | 0.77                       | 4.66                    | 22.5                         | 0        |
| 1988 | 3     | 2                          | 0.07             | 10.78         | 0.84         | 0.01  | 0.78                       | 4.66                    | 22.5                         | 0        |
| 1988 | 3     | 3                          | 0.06             | 6.59          | 0.84         | 0.01  | 0.79                       | 4.66                    | 22.5                         | 0        |
| 1988 | 3     | 4                          | 0.06             | 6.31          | 0.84         | 0.01  | 0.79                       | 4.66                    | 22.5                         | 0        |
| 1988 | 3     | 5                          | 0.08             | 7.21          | 0.84         | 0.01  | 0.77                       | 4.66                    | 22.5                         | 0        |
| 1988 | 3     | 6                          | 0.09             | 11.66         | 1.01         | 0.01  | 0.93                       | 4.66                    | 22.5                         | 0        |
| 1988 | 4     | 1                          | 0.16             | 20.66         | 0.84         | 0.01  | 0.69                       | 4.66                    | 22.5                         | 0        |
| 1988 | 4     | 2                          | 0.1              | 10.15         | 0.84         | 0.01  | 0.75                       | 4.66                    | 22.5                         | 0        |
| 1988 | 4     | 3                          | 0.07             | 7.3           | 0.84         | 0.01  | 0.78                       | 4.66                    | 22.5                         | 0        |
| 1988 | 4     | 4                          | 0.07             | 7.25          | 0.84         | 0.01  | 0.78                       | 4.66                    | 22.5                         | 0        |
| 1988 | 4     | 5                          | 0.08             | 8.4           | 0.84         | 0.01  | 0.77                       | 4.66                    | 22.5                         | 0        |
| 1988 | 4     | 6                          | 0.06             | 6.1           | 0.84         | 0.01  | 0.79                       | 4.66                    | 22.5                         | 0        |

Table F-34 (11) Reservoir Operation Study for Existing Krenceng Dam (11/12)

Net supply yield: 1.94m<sup>3</sup>/sec  
 Water conveyance capacity: 2.00 m<sup>3</sup>/sec  
 of 27.2 km pipe line

(Unit: 10<sup>6</sup> m<sup>3</sup>)

| Year | Month | Serial No. of 5 day period | Inflow discharge |                | Supply yield | Evapo | Water conveyance from Cida | Krenceng Storage volume | Reservoir Water level (El-m) | Spillout |
|------|-------|----------------------------|------------------|----------------|--------------|-------|----------------------------|-------------------------|------------------------------|----------|
|      |       |                            | Krenceng         | Cidamau intake |              |       |                            |                         |                              |          |
| 1988 | 5     | 1                          | 0.05             | 7.77           | 0.24         | 0.01  | 0.8                        | 4.66                    | 22.5                         | 0        |
| 1988 | 5     | 2                          | 0.05             | 8.62           | 0.84         | 0.01  | 0.8                        | 4.66                    | 22.5                         | 0        |
| 1988 | 5     | 3                          | 0.06             | 6.74           | 0.84         | 0.01  | 0.79                       | 4.66                    | 22.5                         | 0        |
| 1988 | 5     | 4                          | 0.07             | 9.24           | 0.84         | 0.01  | 0.78                       | 4.66                    | 22.5                         | 0        |
| 1988 | 5     | 5                          | 0.06             | 8.84           | 0.84         | 0.01  | 0.79                       | 4.66                    | 22.5                         | 0        |
| 1988 | 5     | 6                          | 0.05             | 4.45           | 1.01         | 0.01  | 0.97                       | 4.66                    | 22.5                         | 0        |
| 1988 | 6     | 1                          | 0.08             | 3.12           | 0.84         | 0.01  | 0.77                       | 4.66                    | 22.5                         | 0        |
| 1988 | 6     | 2                          | 0.05             | 5.72           | 0.84         | 0.01  | 0.8                        | 4.66                    | 22.5                         | 0        |
| 1988 | 6     | 3                          | 0.05             | 6.27           | 0.84         | 0.01  | 0.8                        | 4.66                    | 22.5                         | 0        |
| 1988 | 6     | 4                          | 0.04             | 5.46           | 0.84         | 0.01  | 0.81                       | 4.66                    | 22.5                         | 0        |
| 1988 | 6     | 5                          | 0.04             | 4.47           | 0.84         | 0.01  | 0.81                       | 4.66                    | 22.5                         | 0        |
| 1988 | 6     | 6                          | 0.04             | 3.13           | 0.84         | 0.01  | 0.81                       | 4.66                    | 22.5                         | 0        |
| 1988 | 7     | 1                          | 0.08             | 2.01           | 0.84         | 0.01  | 0.77                       | 4.66                    | 22.5                         | 0        |
| 1988 | 7     | 2                          | 0.06             | 1.37           | 0.84         | 0.01  | 0.79                       | 4.66                    | 22.5                         | 0        |
| 1988 | 7     | 3                          | 0.03             | 0.91           | 0.84         | 0.01  | 0.82                       | 4.66                    | 22.5                         | 0        |
| 1988 | 7     | 4                          | 0.04             | 1.08           | 0.84         | 0.01  | 0.81                       | 4.66                    | 22.5                         | 0        |
| 1988 | 7     | 5                          | 0.04             | 0.93           | 0.84         | 0.01  | 0.82                       | 4.66                    | 22.5                         | 0        |
| 1988 | 7     | 6                          | 0.04             | 1.15           | 1.01         | 0.01  | 0.98                       | 4.66                    | 22.5                         | 0        |
| 1988 | 8     | 1                          | 0.05             | 1.03           | 0.84         | 0.02  | 0.81                       | 4.66                    | 22.5                         | 0        |
| 1988 | 8     | 2                          | 0.05             | 1.89           | 0.84         | 0.02  | 0.8                        | 4.66                    | 22.5                         | 0        |
| 1988 | 8     | 3                          | 0.06             | 1.5            | 0.84         | 0.02  | 0.79                       | 4.66                    | 22.5                         | 0        |
| 1988 | 8     | 4                          | 0.05             | 1.39           | 0.84         | 0.02  | 0.8                        | 4.66                    | 22.5                         | 0        |
| 1988 | 8     | 5                          | 0.05             | 1.48           | 0.84         | 0.02  | 0.81                       | 4.66                    | 22.5                         | 0        |
| 1988 | 8     | 6                          | 0.05             | 1.16           | 1.01         | 0.02  | 0.97                       | 4.66                    | 22.5                         | 0        |
| 1988 | 9     | 1                          | 0.04             | 0.87           | 0.84         | 0.01  | 0.81                       | 4.66                    | 22.5                         | 0        |
| 1988 | 9     | 2                          | 0.04             | 1.15           | 0.84         | 0.01  | 0.81                       | 4.66                    | 22.5                         | 0        |
| 1988 | 9     | 3                          | 0.04             | 1.5            | 0.84         | 0.01  | 0.82                       | 4.66                    | 22.5                         | 0        |
| 1988 | 9     | 4                          | 0.04             | 1.32           | 0.84         | 0.01  | 0.82                       | 4.66                    | 22.5                         | 0        |
| 1988 | 9     | 5                          | 0.04             | 1.29           | 0.84         | 0.01  | 0.82                       | 4.66                    | 22.5                         | 0        |
| 1988 | 9     | 6                          | 0.04             | 1.25           | 0.84         | 0.01  | 0.81                       | 4.66                    | 22.5                         | 0        |
| 1988 | 10    | 1                          | 0.04             | 1.43           | 0.84         | 0.01  | 0.81                       | 4.66                    | 22.5                         | 0        |
| 1988 | 10    | 2                          | 0.04             | 1.13           | 0.84         | 0.01  | 0.82                       | 4.66                    | 22.5                         | 0        |
| 1988 | 10    | 3                          | 0.22             | 1.13           | 0.84         | 0.01  | 0.63                       | 4.66                    | 22.5                         | 0        |
| 1988 | 10    | 4                          | 0.14             | 2.01           | 0.84         | 0.01  | 0.71                       | 4.66                    | 22.5                         | 0        |
| 1988 | 10    | 5                          | 0.07             | 2.27           | 0.84         | 0.01  | 0.79                       | 4.66                    | 22.5                         | 0        |
| 1988 | 10    | 6                          | 0.19             | 2.58           | 1.01         | 0.02  | 0.84                       | 4.66                    | 22.5                         | 0        |
| 1988 | 11    | 1                          | 0.28             | 3.59           | 0.84         | 0.02  | 0.58                       | 4.66                    | 22.5                         | 0        |
| 1988 | 11    | 2                          | 0.09             | 4.5            | 0.84         | 0.02  | 0.77                       | 4.66                    | 22.5                         | 0        |
| 1988 | 11    | 3                          | 0.07             | 5.93           | 0.84         | 0.02  | 0.79                       | 4.66                    | 22.5                         | 0        |
| 1988 | 11    | 4                          | 0.05             | 5.45           | 0.84         | 0.02  | 0.81                       | 4.66                    | 22.5                         | 0        |
| 1988 | 11    | 5                          | 0.05             | 7.94           | 0.84         | 0.02  | 0.8                        | 4.66                    | 22.5                         | 0        |
| 1988 | 11    | 6                          | 0.05             | 13.43          | 0.84         | 0.02  | 0.81                       | 4.66                    | 22.5                         | 0        |
| 1988 | 12    | 1                          | 0.05             | 14.52          | 0.84         | 0.01  | 0.8                        | 4.66                    | 22.5                         | 0        |
| 1988 | 12    | 2                          | 0.05             | 9.43           | 0.84         | 0.01  | 0.8                        | 4.66                    | 22.5                         | 0        |
| 1988 | 12    | 3                          | 0.38             | 15.49          | 0.84         | 0.01  | 0.47                       | 4.66                    | 22.5                         | 0        |
| 1988 | 12    | 4                          | 0.09             | 25.36          | 0.84         | 0.01  | 0.76                       | 4.66                    | 22.5                         | 0        |
| 1988 | 12    | 5                          | 0.04             | 12.37          | 0.84         | 0.01  | 0.81                       | 4.66                    | 22.5                         | 0        |
| 1988 | 12    | 6                          | 0.05             | 7.41           | 1.01         | 0.02  | 0.98                       | 4.66                    | 22.5                         | 0        |
| 1989 | 1     | 1                          | 0.04             | 4.47           | 0.84         | 0.02  | 0.81                       | 4.66                    | 22.5                         | 0        |
| 1989 | 1     | 2                          | 0.04             | 3.43           | 0.84         | 0.02  | 0.81                       | 4.66                    | 22.5                         | 0        |
| 1989 | 1     | 3                          | 0.05             | 2.82           | 0.84         | 0.02  | 0.8                        | 4.66                    | 22.5                         | 0        |
| 1989 | 1     | 4                          | 0.06             | 3.68           | 0.84         | 0.02  | 0.79                       | 4.66                    | 22.5                         | 0        |
| 1989 | 1     | 5                          | 0.12             | 3.9            | 0.84         | 0.02  | 0.74                       | 4.66                    | 22.5                         | 0        |
| 1989 | 1     | 6                          | 0.08             | 3.81           | 1.01         | 0.02  | 0.94                       | 4.66                    | 22.5                         | 0        |
| 1989 | 2     | 1                          | 0.22             | 4.23           | 0.84         | 0.01  | 0.63                       | 4.66                    | 22.5                         | 0        |
| 1989 | 2     | 2                          | 0.22             | 15.86          | 0.84         | 0.01  | 0.64                       | 4.66                    | 22.5                         | 0        |
| 1989 | 2     | 3                          | 0.09             | 10.41          | 0.84         | 0.01  | 0.76                       | 4.66                    | 22.5                         | 0        |
| 1989 | 2     | 4                          | 0.27             | 32.32          | 0.84         | 0.01  | 0.58                       | 4.66                    | 22.5                         | 0        |
| 1989 | 2     | 5                          | 0.75             | 13.32          | 0.84         | 0.01  | 0.1                        | 4.66                    | 22.5                         | 0        |
| 1989 | 2     | 6                          | 0.39             | 21.43          | 0.5          | 0.01  | 0.13                       | 4.66                    | 22.5                         | 0        |

Table F-34 (12) Reservoir Operation Study for Existing Krenceng Dam (12/12) Net supply yield: 1.94m<sup>3</sup>/sec  
Water conveyance capacity: 2.00 m<sup>3</sup>/sec  
of 27.2 km pipe line

6  
(Unit: 10 m<sup>3</sup>)

| Year | Month | Serial No. of 5 day period | Inflow discharge |                | Supply yield | Evapo | Water conveyance from Cida | Krenceng Storage volume | Reservoir Water level (El-m) | Spillout |
|------|-------|----------------------------|------------------|----------------|--------------|-------|----------------------------|-------------------------|------------------------------|----------|
|      |       |                            | Krenceng         | Cidanau intake |              |       |                            |                         |                              |          |
| 1989 | 3     | 1                          | 0.35             | 24.82          | 0.84         | 0.01  | 0.5                        | 4.66                    | 22.5                         | 0        |
| 1989 | 3     | 2                          | 0.3              | 17.14          | 0.84         | 0.01  | 0.55                       | 4.66                    | 22.5                         | 0        |
| 1989 | 3     | 3                          | 0.22             | 9.43           | 0.84         | 0.01  | 0.63                       | 4.66                    | 22.5                         | 0        |
| 1989 | 3     | 4                          | 0.1              | 8.1            | 0.84         | 0.01  | 0.75                       | 4.66                    | 22.5                         | 0        |
| 1989 | 3     | 5                          | 0.04             | 4.66           | 0.84         | 0.01  | 0.81                       | 4.66                    | 22.5                         | 0        |
| 1989 | 3     | 6                          | 0.05             | 3.91           | 1.01         | 0.01  | 0.97                       | 4.66                    | 22.5                         | 0        |
| 1989 | 4     | 1                          | 0.04             | 3.38           | 0.84         | 0.01  | 0.81                       | 4.66                    | 22.5                         | 0        |
| 1989 | 4     | 2                          | 0.05             | 3.38           | 0.84         | 0.01  | 0.81                       | 4.66                    | 22.5                         | 0        |
| 1989 | 4     | 3                          | 0.04             | 3.38           | 0.84         | 0.01  | 0.81                       | 4.66                    | 22.5                         | 0        |
| 1989 | 4     | 4                          | 0.02             | 3.38           | 0.84         | 0.01  | 0.83                       | 4.66                    | 22.5                         | 0        |
| 1989 | 4     | 5                          | 0.01             | 3.38           | 0.84         | 0.01  | 0.84                       | 4.66                    | 22.5                         | 0        |
| 1989 | 4     | 6                          | 0.01             | 3.38           | 0.84         | 0.01  | 0.84                       | 4.66                    | 22.5                         | 0        |
| 1989 | 5     | 1                          | 0.02             | 3.38           | 0.84         | 0.01  | 0.83                       | 4.66                    | 22.5                         | 0        |
| 1989 | 5     | 2                          | 0.02             | 3.38           | 0.84         | 0.01  | 0.83                       | 4.66                    | 22.5                         | 0        |
| 1989 | 5     | 3                          | 0.01             | 3.38           | 0.84         | 0.01  | 0.84                       | 4.66                    | 22.5                         | 0        |
| 1989 | 5     | 4                          | 0.01             | 3.38           | 0.84         | 0.01  | 0.84                       | 4.66                    | 22.5                         | 0        |
| 1989 | 5     | 5                          | 0.02             | 3.38           | 0.84         | 0.01  | 0.83                       | 4.66                    | 22.5                         | 0        |
| 1989 | 5     | 6                          | 0.02             | 4.06           | 1.01         | 0.01  | 1                          | 4.66                    | 22.5                         | 0        |
| 1989 | 6     | 1                          | 0.02             | 3.3            | 0.84         | 0.01  | 0.83                       | 4.66                    | 22.5                         | 0        |
| 1989 | 6     | 2                          | 0.07             | 4.01           | 0.84         | 0.01  | 0.78                       | 4.66                    | 22.5                         | 0        |
| 1989 | 6     | 3                          | 0.09             | 4.02           | 0.84         | 0.01  | 0.76                       | 4.66                    | 22.5                         | 0        |
| 1989 | 6     | 4                          | 0.08             | 2.74           | 0.84         | 0.01  | 0.77                       | 4.66                    | 22.5                         | 0        |
| 1989 | 6     | 5                          | 0.08             | 1.62           | 0.84         | 0.01  | 0.77                       | 4.66                    | 22.5                         | 0        |
| 1989 | 6     | 6                          | 0.08             | 1.4            | 0.84         | 0.01  | 0.77                       | 4.66                    | 22.5                         | 0        |
| 1989 | 7     | 1                          | 0.06             | 1.37           | 0.84         | 0.01  | 0.8                        | 4.66                    | 22.5                         | 0        |
| 1989 | 7     | 2                          | 0.06             | 2.71           | 0.84         | 0.01  | 0.79                       | 4.66                    | 22.5                         | 0        |
| 1989 | 7     | 3                          | 0.06             | 4.54           | 0.84         | 0.01  | 0.79                       | 4.66                    | 22.5                         | 0        |
| 1989 | 7     | 4                          | 0.06             | 5.32           | 0.84         | 0.01  | 0.79                       | 4.66                    | 22.5                         | 0        |
| 1989 | 7     | 5                          | 0.05             | 3.77           | 0.84         | 0.01  | 0.8                        | 4.66                    | 22.5                         | 0        |
| 1989 | 7     | 6                          | 0.08             | 2.3            | 1.01         | 0.01  | 0.94                       | 4.66                    | 22.5                         | 0        |
| 1989 | 8     | 1                          | 0.06             | 1.15           | 0.84         | 0.02  | 0.79                       | 4.66                    | 22.5                         | 0        |
| 1989 | 8     | 2                          | 0.08             | 0.77           | 0.84         | 0.02  | 0.77                       | 4.66                    | 22.5                         | 0        |
| 1989 | 8     | 3                          | 0.06             | 0.98           | 0.84         | 0.02  | 0.8                        | 4.66                    | 22.5                         | 0        |
| 1989 | 8     | 4                          | 0.06             | 0.62           | 0.84         | 0.02  | 0.62                       | 4.49                    | 22.32                        | 0        |
| 1989 | 8     | 5                          | 0.05             | 0.7            | 0.84         | 0.02  | 0.7                        | 4.39                    | 22.21                        | 0        |
| 1989 | 8     | 6                          | 0.15             | 1.27           | 1.01         | 0.02  | 1.04                       | 4.55                    | 22.39                        | 0        |
| 1989 | 9     | 1                          | 0.05             | 1.68           | 0.84         | 0.01  | 0.86                       | 4.61                    | 22.46                        | 0        |
| 1989 | 9     | 2                          | 0.07             | 1.03           | 0.84         | 0.01  | 0.82                       | 4.66                    | 22.5                         | 0        |
| 1989 | 9     | 3                          | 0.05             | 1.88           | 0.84         | 0.01  | 0.8                        | 4.66                    | 22.5                         | 0        |
| 1989 | 9     | 4                          | 0.04             | 2.36           | 0.84         | 0.01  | 0.81                       | 4.66                    | 22.5                         | 0        |
| 1989 | 9     | 5                          | 0.04             | 1.53           | 0.84         | 0.01  | 0.82                       | 4.66                    | 22.5                         | 0        |
| 1989 | 9     | 6                          | 0.04             | 0.83           | 0.84         | 0.01  | 0.81                       | 4.66                    | 22.5                         | 0        |
| 1989 | 10    | 1                          | 0.04             | 1.37           | 0.84         | 0.01  | 0.81                       | 4.66                    | 22.5                         | 0        |
| 1989 | 10    | 2                          | 0.04             | 1.15           | 0.84         | 0.01  | 0.82                       | 4.66                    | 22.5                         | 0        |
| 1989 | 10    | 3                          | 0.04             | 0.94           | 0.84         | 0.01  | 0.82                       | 4.66                    | 22.5                         | 0        |
| 1989 | 10    | 4                          | 0.04             | 0.81           | 0.84         | 0.01  | 0.81                       | 4.65                    | 22.5                         | 0        |
| 1989 | 10    | 5                          | 0.04             | 0.87           | 0.84         | 0.01  | 0.82                       | 4.66                    | 22.5                         | 0        |
| 1989 | 10    | 6                          | 0.05             | 2.43           | 1.01         | 0.02  | 0.98                       | 4.66                    | 22.5                         | 0        |
| 1989 | 11    | 1                          | 0.04             | 1.68           | 0.84         | 0.02  | 0.82                       | 4.66                    | 22.5                         | 0        |
| 1989 | 11    | 2                          | 0.04             | 1.44           | 0.84         | 0.02  | 0.82                       | 4.66                    | 22.5                         | 0        |
| 1989 | 11    | 3                          | 0.04             | 2.22           | 0.84         | 0.02  | 0.82                       | 4.66                    | 22.5                         | 0        |
| 1989 | 11    | 4                          | 0.04             | 2.09           | 0.84         | 0.02  | 0.81                       | 4.66                    | 22.5                         | 0        |
| 1989 | 11    | 5                          | 0.04             | 2.31           | 0.84         | 0.02  | 0.82                       | 4.66                    | 22.5                         | 0        |
| 1989 | 11    | 6                          | 0.04             | 1.75           | 0.84         | 0.02  | 0.81                       | 4.66                    | 22.5                         | 0        |
| 1989 | 12    | 1                          | 0.04             | 2.28           | 0.84         | 0.01  | 0.81                       | 4.66                    | 22.5                         | 0        |
| 1989 | 12    | 2                          | 0.08             | 2.81           | 0.84         | 0.01  | 0.78                       | 4.66                    | 22.5                         | 0        |
| 1989 | 12    | 3                          | 0.49             | 4.08           | 0.84         | 0.01  | 0.36                       | 4.66                    | 22.5                         | 0        |
| 1989 | 12    | 4                          | 0.16             | 4.58           | 0.84         | 0.01  | 0.69                       | 4.66                    | 22.5                         | 0        |
| 1989 | 12    | 5                          | 0.07             | 4.28           | 0.84         | 0.01  | 0.78                       | 4.66                    | 22.5                         | 0        |
| 1989 | 12    | 6                          | 0.24             | 5.2            | 1.01         | 0.02  | 0.78                       | 4.66                    | 22.5                         | 0        |

Table F-35 (1) Reservoir Operation Study for Heightening of Krenceng Dam (without Diversion Tunnel) (1/12)

Net supply yield: 3.05 m<sup>3</sup>/sec  
 Water conveyance capacity: 3.05 m<sup>3</sup>/sec  
 of 27.2 km pipe line

(Unit: 10 m<sup>3</sup>)

| Year | Month | Serial No. of 5 day period | Inflow discharge |               | Supply yield | Evapo | Water conveyance from Cida | Krenceng Storage volume | Reservoir Water level (El-m) | Spillout |
|------|-------|----------------------------|------------------|---------------|--------------|-------|----------------------------|-------------------------|------------------------------|----------|
|      |       |                            | Krenceng         | Cidamu intake |              |       |                            |                         |                              |          |
| 1980 | 1     | 1                          | 0.12             | 3.9           | 1.32         | 0.03  | 1.23                       | 14.07                   | 29                           | 0        |
| 1980 | 1     | 2                          | 0.2              | 3.98          | 1.32         | 0.03  | 1.15                       | 14.07                   | 29                           | 0        |
| 1980 | 1     | 3                          | 0.29             | 4.05          | 1.32         | 0.03  | 1.06                       | 14.07                   | 29                           | 0        |
| 1980 | 1     | 4                          | 0.29             | 3.92          | 1.32         | 0.03  | 1.06                       | 14.07                   | 29                           | 0        |
| 1980 | 1     | 5                          | 0.29             | 3.9           | 1.32         | 0.03  | 1.06                       | 14.07                   | 29                           | 0        |
| 1980 | 1     | 6                          | 0.39             | 3.56          | 1.58         | 0.03  | 1.22                       | 14.07                   | 29                           | 0        |
| 1980 | 2     | 1                          | 0.19             | 3.3           | 1.32         | 0.02  | 1.15                       | 14.07                   | 29                           | 0        |
| 1980 | 2     | 2                          | 0.48             | 5.06          | 1.32         | 0.02  | 0.86                       | 14.07                   | 29                           | 0        |
| 1980 | 2     | 3                          | 0.49             | 5.01          | 1.32         | 0.02  | 0.85                       | 14.07                   | 29                           | 0        |
| 1980 | 2     | 4                          | 0.78             | 5.06          | 1.32         | 0.02  | 0.56                       | 14.07                   | 29                           | 0        |
| 1980 | 2     | 5                          | 0.46             | 5.09          | 1.32         | 0.02  | 0.88                       | 14.07                   | 29                           | 0        |
| 1980 | 2     | 6                          | 0.19             | 5.06          | 1.05         | 0.02  | 0.89                       | 14.07                   | 29                           | 0        |
| 1980 | 3     | 1                          | 0.15             | 4.53          | 1.32         | 0.02  | 1.19                       | 14.07                   | 29                           | 0        |
| 1980 | 3     | 2                          | 0.23             | 3.44          | 1.32         | 0.02  | 1.11                       | 14.07                   | 29                           | 0        |
| 1980 | 3     | 3                          | 0.15             | 14.02         | 1.32         | 0.02  | 1.18                       | 14.07                   | 29                           | 0        |
| 1980 | 3     | 4                          | 0.16             | 9.57          | 1.32         | 0.02  | 1.18                       | 14.07                   | 29                           | 0        |
| 1980 | 3     | 5                          | 0.07             | 2.29          | 1.32         | 0.02  | 1.27                       | 14.07                   | 29                           | 0        |
| 1980 | 3     | 6                          | 0.11             | 1.74          | 1.58         | 0.03  | 1.5                        | 14.07                   | 29                           | 0        |
| 1980 | 4     | 1                          | 0.06             | 2.23          | 1.32         | 0.02  | 1.28                       | 14.07                   | 29                           | 0        |
| 1980 | 4     | 2                          | 0.07             | 1.77          | 1.32         | 0.02  | 1.27                       | 14.07                   | 29                           | 0        |
| 1980 | 4     | 3                          | 0.28             | 6.5           | 1.32         | 0.02  | 1.06                       | 14.07                   | 29                           | 0        |
| 1980 | 4     | 4                          | 0.1              | 4.84          | 1.32         | 0.02  | 1.24                       | 14.07                   | 29                           | 0        |
| 1980 | 4     | 5                          | 0.17             | 3.27          | 1.32         | 0.02  | 1.17                       | 14.07                   | 29                           | 0        |
| 1980 | 4     | 6                          | 0.11             | 1.99          | 1.32         | 0.02  | 1.23                       | 14.07                   | 29                           | 0        |
| 1980 | 5     | 1                          | 0.11             | 0.82          | 1.32         | 0.02  | 0.82                       | 15.66                   | 28.74                        | 0        |
| 1980 | 5     | 2                          | 0.09             | 0.18          | 1.32         | 0.02  | 0.18                       | 12.6                    | 28.08                        | 0        |
| 1980 | 5     | 3                          | 0.11             | 0.88          | 1.32         | 0.02  | 0.88                       | 12.25                   | 27.86                        | 0        |
| 1980 | 5     | 4                          | 0.11             | 1.91          | 1.32         | 0.02  | 1.32                       | 12.34                   | 27.91                        | 0        |
| 1980 | 5     | 5                          | 0.07             | 5.36          | 1.32         | 0.02  | 1.32                       | 12.39                   | 27.95                        | 0        |
| 1980 | 5     | 6                          | 0.06             | 4.99          | 1.58         | 0.02  | 1.58                       | 12.42                   | 27.97                        | 0        |
| 1980 | 6     | 1                          | 0.11             | 3.84          | 1.32         | 0.02  | 1.32                       | 12.52                   | 28.03                        | 0        |
| 1980 | 6     | 2                          | 0.06             | 4.39          | 1.32         | 0.02  | 1.32                       | 12.55                   | 28.05                        | 0        |
| 1980 | 6     | 3                          | 0.08             | 1.89          | 1.32         | 0.02  | 1.32                       | 12.61                   | 28.09                        | 0        |
| 1980 | 6     | 4                          | 0.05             | 3.17          | 1.32         | 0.02  | 1.32                       | 12.64                   | 28.1                         | 0        |
| 1980 | 6     | 5                          | 0.06             | 5.77          | 1.32         | 0.02  | 1.32                       | 12.88                   | 28.15                        | 0        |
| 1980 | 6     | 6                          | 0.05             | 2.37          | 1.32         | 0.02  | 1.32                       | 12.71                   | 28.15                        | 0        |
| 1980 | 7     | 1                          | 0.04             | 1.63          | 1.32         | 0.02  | 1.32                       | 12.73                   | 28.16                        | 0        |
| 1980 | 7     | 2                          | 0.04             | 2.82          | 1.32         | 0.02  | 1.32                       | 12.75                   | 28.17                        | 0        |
| 1980 | 7     | 3                          | 0.04             | 2.81          | 1.32         | 0.02  | 1.32                       | 12.77                   | 28.19                        | 0        |
| 1980 | 7     | 4                          | 0.05             | 4.75          | 1.32         | 0.02  | 1.32                       | 12.8                    | 28.21                        | 0        |
| 1980 | 7     | 5                          | 0.05             | 2.64          | 1.32         | 0.02  | 1.32                       | 12.85                   | 28.22                        | 0        |
| 1980 | 7     | 6                          | 0.06             | 2.74          | 1.58         | 0.02  | 1.58                       | 12.86                   | 28.25                        | 0        |
| 1980 | 8     | 1                          | 0.12             | 2.19          | 1.32         | 0.03  | 1.32                       | 12.96                   | 28.3                         | 0        |
| 1980 | 8     | 2                          | 0.19             | 4.48          | 1.32         | 0.03  | 1.32                       | 13.12                   | 28.4                         | 0        |
| 1980 | 8     | 3                          | 0.28             | 6.84          | 1.32         | 0.03  | 1.32                       | 13.37                   | 28.56                        | 0        |
| 1980 | 8     | 4                          | 0.38             | 12.84         | 1.32         | 0.03  | 1.32                       | 13.72                   | 28.78                        | 0        |
| 1980 | 8     | 5                          | 0.05             | 5.29          | 1.32         | 0.03  | 1.32                       | 13.75                   | 28.8                         | 0        |
| 1980 | 8     | 6                          | 0.05             | 2.12          | 1.58         | 0.03  | 1.58                       | 13.76                   | 28.81                        | 0        |
| 1980 | 9     | 1                          | 0.23             | 2.64          | 1.32         | 0.03  | 1.32                       | 13.96                   | 28.93                        | 0        |
| 1980 | 9     | 2                          | 0.2              | 27.03         | 1.32         | 0.03  | 1.25                       | 14.07                   | 29                           | 0        |
| 1980 | 9     | 3                          | 0.32             | 28.73         | 1.32         | 0.03  | 1.02                       | 14.07                   | 29                           | 0        |
| 1980 | 9     | 4                          | 0.11             | 12.39         | 1.32         | 0.03  | 1.23                       | 14.07                   | 29                           | 0        |
| 1980 | 9     | 5                          | 0.08             | 2.48          | 1.32         | 0.03  | 1.26                       | 14.07                   | 29                           | 0        |
| 1980 | 9     | 6                          | 0.14             | 1.63          | 1.32         | 0.03  | 1.2                        | 14.07                   | 29                           | 0        |
| 1980 | 10    | 1                          | 0.11             | 0.86          | 1.32         | 0.03  | 0.86                       | 13.7                    | 28.76                        | 0        |
| 1980 | 10    | 2                          | 0.12             | 0.63          | 1.32         | 0.03  | 0.63                       | 13.11                   | 28.4                         | 0        |
| 1980 | 10    | 3                          | 0.12             | 2.54          | 1.32         | 0.03  | 1.32                       | 13.2                    | 28.46                        | 0        |
| 1980 | 10    | 4                          | 0.08             | 6.13          | 1.32         | 0.03  | 1.32                       | 13.26                   | 28.49                        | 0        |
| 1980 | 10    | 5                          | 0.12             | 6.87          | 1.32         | 0.03  | 1.32                       | 13.36                   | 28.55                        | 0        |
| 1980 | 10    | 6                          | 0.11             | 9.88          | 1.58         | 0.03  | 1.58                       | 13.44                   | 28.6                         | 0        |

Table P-35 (2) Reservoir Operation Study for Heightening of Krenceng Dam (without Diversion Tunnel) (2/12)

Net supply yield: 3.05 m<sup>3</sup>/sec  
 Water conveyance capacity: 3.05 m<sup>3</sup>/sec  
 of 27.2 km pipe line

(Unit: 10<sup>6</sup> m<sup>3</sup>)

| Year | Month | Serial No. of 5 day period | Inflow discharge |                | Supply yield | Evapo | Water conveyance from Cide | Krenceng Storage volume | Reservoir Water level (El-m) | Spillover |
|------|-------|----------------------------|------------------|----------------|--------------|-------|----------------------------|-------------------------|------------------------------|-----------|
|      |       |                            | Krenceng         | Cidenua intake |              |       |                            |                         |                              |           |
| 1980 | 11    | 1                          | 0.18             | 9.4            | 1.32         | 0.03  | 1.32                       | 13.59                   | 28.7                         | 0         |
| 1980 | 11    | 2                          | 0.1              | 11.06          | 1.32         | 0.03  | 1.32                       | 13.66                   | 28.74                        | 0         |
| 1980 | 11    | 3                          | 0.13             | 13.41          | 1.32         | 0.03  | 1.32                       | 13.76                   | 28.8                         | 0         |
| 1980 | 11    | 4                          | 0.31             | 15.5           | 1.32         | 0.03  | 1.32                       | 14.05                   | 28.98                        | 0         |
| 1980 | 11    | 5                          | 0.08             | 18.31          | 1.32         | 0.03  | 1.3                        | 14.07                   | 29                           | 0         |
| 1980 | 11    | 6                          | 0.06             | 21.43          | 1.32         | 0.03  | 1.28                       | 14.07                   | 29                           | 0         |
| 1980 | 12    | 1                          | 0.05             | 27.92          | 1.32         | 0.03  | 1.3                        | 14.07                   | 29                           | 0         |
| 1980 | 12    | 2                          | 0.07             | 31.72          | 1.32         | 0.03  | 1.28                       | 14.07                   | 29                           | 0         |
| 1980 | 12    | 3                          | 0.03             | 32.78          | 1.32         | 0.03  | 1.29                       | 14.07                   | 29                           | 0         |
| 1980 | 12    | 4                          | 0.18             | 42.23          | 1.32         | 0.03  | 1.17                       | 14.07                   | 29                           | 0         |
| 1980 | 12    | 5                          | 0.53             | 29.54          | 1.32         | 0.03  | 0.81                       | 14.07                   | 29                           | 0         |
| 1980 | 12    | 6                          | 0.64             | 47.28          | 1.32         | 0.03  | 0.97                       | 14.07                   | 29                           | 0         |
| 1981 | 1     | 1                          | 1.71             | 62.12          | 1.32         | 0.03  | 0                          | 14.07                   | 29                           | 0.37      |
| 1981 | 1     | 2                          | 1.18             | 72.41          | 1.32         | 0.03  | 0.17                       | 14.07                   | 29                           | 0         |
| 1981 | 1     | 3                          | 0.71             | 28.77          | 1.32         | 0.03  | 0.63                       | 14.07                   | 29                           | 0         |
| 1981 | 1     | 4                          | 0.42             | 30.33          | 1.32         | 0.03  | 0.95                       | 14.07                   | 29                           | 0         |
| 1981 | 1     | 5                          | 0.29             | 13.91          | 1.32         | 0.03  | 1.05                       | 14.07                   | 29                           | 0         |
| 1981 | 1     | 6                          | 0.49             | 17.12          | 1.32         | 0.03  | 1.12                       | 14.07                   | 29                           | 0         |
| 1981 | 2     | 1                          | 0.4              | 18.43          | 1.32         | 0.02  | 0.94                       | 14.07                   | 29                           | 0         |
| 1981 | 2     | 2                          | 0.35             | 21.51          | 1.32         | 0.02  | 0.99                       | 14.07                   | 29                           | 0         |
| 1981 | 2     | 3                          | 0.52             | 14.11          | 1.32         | 0.02  | 0.83                       | 14.07                   | 29                           | 0         |
| 1981 | 2     | 4                          | 0.51             | 10.57          | 1.32         | 0.02  | 0.83                       | 14.07                   | 29                           | 0         |
| 1981 | 2     | 5                          | 0.46             | 1.87           | 1.32         | 0.02  | 0.88                       | 14.07                   | 29                           | 0         |
| 1981 | 2     | 6                          | 0.75             | 11.16          | 0.79         | 0.01  | 0.06                       | 14.07                   | 29                           | 0         |
| 1981 | 3     | 1                          | 0.66             | 12.23          | 1.32         | 0.02  | 0.68                       | 14.07                   | 29                           | 0         |
| 1981 | 3     | 2                          | 0.33             | 1.75           | 1.32         | 0.02  | 1.01                       | 14.07                   | 29                           | 0         |
| 1981 | 3     | 3                          | 0.51             | 2.26           | 1.32         | 0.02  | 0.83                       | 14.07                   | 29                           | 0         |
| 1981 | 3     | 4                          | 0.32             | 3.68           | 1.32         | 0.02  | 1.02                       | 14.07                   | 29                           | 0         |
| 1981 | 3     | 5                          | 0.17             | 2.34           | 1.32         | 0.02  | 1.17                       | 14.07                   | 29                           | 0         |
| 1981 | 3     | 6                          | 0.31             | 11.79          | 1.58         | 0.03  | 1.3                        | 14.07                   | 29                           | 0         |
| 1981 | 4     | 1                          | 0.14             | 12.43          | 1.32         | 0.02  | 1.2                        | 14.07                   | 29                           | 0         |
| 1981 | 4     | 2                          | 0.16             | 12.3           | 1.32         | 0.02  | 1.18                       | 14.07                   | 29                           | 0         |
| 1981 | 4     | 3                          | 0.1              | 11.66          | 1.32         | 0.02  | 1.24                       | 14.07                   | 29                           | 0         |
| 1981 | 4     | 4                          | 0.13             | 10.14          | 1.32         | 0.02  | 1.2                        | 14.07                   | 29                           | 0         |
| 1981 | 4     | 5                          | 0.14             | 8.69           | 1.32         | 0.02  | 1.2                        | 14.07                   | 29                           | 0         |
| 1981 | 4     | 6                          | 0.11             | 7.79           | 1.32         | 0.02  | 1.23                       | 14.07                   | 29                           | 0         |
| 1981 | 5     | 1                          | 0.21             | 6.43           | 1.32         | 0.02  | 1.13                       | 14.07                   | 29                           | 0         |
| 1981 | 5     | 2                          | 0.16             | 4.42           | 1.32         | 0.02  | 1.18                       | 14.07                   | 29                           | 0         |
| 1981 | 5     | 3                          | 0.21             | 2.96           | 1.32         | 0.02  | 1.13                       | 14.07                   | 29                           | 0         |
| 1981 | 5     | 4                          | 0.29             | 4.35           | 1.32         | 0.02  | 1.05                       | 14.07                   | 29                           | 0         |
| 1981 | 5     | 5                          | 0.11             | 3.23           | 1.32         | 0.02  | 1.23                       | 14.07                   | 29                           | 0         |
| 1981 | 5     | 6                          | 0.1              | 1.1            | 1.38         | 0.03  | 1.1                        | 13.67                   | 28.73                        | 0         |
| 1981 | 6     | 1                          | 0.06             | 2.82           | 1.32         | 0.02  | 1.32                       | 13.71                   | 28.77                        | 0         |
| 1981 | 6     | 2                          | 0.06             | 3.69           | 1.32         | 0.02  | 1.32                       | 13.75                   | 28.8                         | 0         |
| 1981 | 6     | 3                          | 0.12             | 5.1            | 1.32         | 0.02  | 1.32                       | 13.85                   | 28.86                        | 0         |
| 1981 | 6     | 4                          | 0.2              | 9.5            | 1.32         | 0.02  | 1.32                       | 14.03                   | 28.98                        | 0         |
| 1981 | 6     | 5                          | 0.09             | 4.31           | 1.32         | 0.02  | 1.29                       | 14.07                   | 29                           | 0         |
| 1981 | 6     | 6                          | 0.12             | 4.23           | 1.32         | 0.02  | 1.22                       | 14.07                   | 29                           | 0         |
| 1981 | 7     | 1                          | 0.06             | 4.31           | 1.32         | 0.02  | 1.28                       | 14.07                   | 29                           | 0         |
| 1981 | 7     | 2                          | 0.06             | 1.27           | 1.32         | 0.02  | 1.27                       | 14.06                   | 28.99                        | 0         |
| 1981 | 7     | 3                          | 0.21             | 2.78           | 1.32         | 0.02  | 1.14                       | 14.07                   | 29                           | 0         |
| 1981 | 7     | 4                          | 0.32             | 5.56           | 1.32         | 0.02  | 1.02                       | 14.07                   | 29                           | 0         |
| 1981 | 7     | 5                          | 0.36             | 7.35           | 1.32         | 0.02  | 0.98                       | 14.07                   | 29                           | 0         |
| 1981 | 7     | 6                          | 0.67             | 11.43          | 1.38         | 0.03  | 0.94                       | 14.07                   | 29                           | 0         |
| 1981 | 7     | 7                          | 0.16             | 8.03           | 1.32         | 0.03  | 1.18                       | 14.07                   | 29                           | 0         |
| 1981 | 8     | 1                          | 0.17             | 3.09           | 1.32         | 0.03  | 1.17                       | 14.07                   | 29                           | 0         |
| 1981 | 8     | 2                          | 0.11             | 2.22           | 1.32         | 0.03  | 1.24                       | 14.07                   | 29                           | 0         |
| 1981 | 8     | 3                          | 0.11             | 1.58           | 1.32         | 0.03  | 1.2                        | 14.07                   | 29                           | 0         |
| 1981 | 8     | 4                          | 0.15             | 3.77           | 1.32         | 0.03  | 1.2                        | 14.07                   | 29                           | 0         |
| 1981 | 8     | 5                          | 0.15             | 5.33           | 1.32         | 0.03  | 1.2                        | 14.07                   | 29                           | 0         |
| 1981 | 8     | 6                          | 0.12             | 5.33           | 1.58         | 0.03  | 1.5                        | 14.07                   | 29                           | 0         |

Table F-35 (3) Reservoir Operation Study for Heightening of Krenceng Dam (without Diversion Tunnel) (3/12)

Net supply yield: 3.05m<sup>3</sup>/sec  
 Water conveyance capacity: 3.05 m<sup>3</sup>/sec  
 of 27.2 km pipe line

| Year | Month | Serial No. of 5 day period | Inflow discharge |                | Supply yield | Evapo | Water conveyance from Cida | Krenceng       |                              | Spillout |
|------|-------|----------------------------|------------------|----------------|--------------|-------|----------------------------|----------------|------------------------------|----------|
|      |       |                            | Krenceng         | Cidanau intake |              |       |                            | Storage volume | Reservoir Water level (El-m) |          |
| 1981 | 9     | 1                          | 0.18             | 2.18           | 1.32         | 0.03  | 1.16                       | 14.07          | 29                           | 0        |
| 1981 | 9     | 2                          | 0.17             | 6.52           | 1.32         | 0.03  | 1.17                       | 14.07          | 29                           | 0        |
| 1981 | 9     | 3                          | 0.47             | 7.08           | 1.32         | 0.03  | 0.87                       | 14.07          | 29                           | 0        |
| 1981 | 9     | 4                          | 0.11             | 1.64           | 1.32         | 0.03  | 1.23                       | 14.07          | 29                           | 0        |
| 1981 | 9     | 5                          | 0.1              | 1.14           | 1.32         | 0.03  | 1.14                       | 14.07          | 29                           | 0        |
| 1981 | 9     | 6                          | 0.16             | 9.85           | 1.32         | 0.03  | 1.29                       | 14.07          | 28.93                        | 0        |
| 1981 | 10    | 1                          | 0.33             | 41.83          | 1.32         | 0.03  | 1.01                       | 14.07          | 29                           | 0        |
| 1981 | 10    | 2                          | 0.33             | 14.32          | 1.32         | 0.03  | 1.01                       | 14.07          | 29                           | 0        |
| 1981 | 10    | 3                          | 0.25             | 4.95           | 1.32         | 0.03  | 1.09                       | 14.07          | 29                           | 0        |
| 1981 | 10    | 4                          | 0.11             | 3.55           | 1.32         | 0.03  | 1.24                       | 14.07          | 29                           | 0        |
| 1981 | 10    | 5                          | 0.12             | 1.83           | 1.32         | 0.03  | 1.22                       | 14.07          | 29                           | 0        |
| 1981 | 10    | 6                          | 0.22             | 10.88          | 1.58         | 0.03  | 1.39                       | 14.07          | 29                           | 0        |
| 1981 | 11    | 1                          | 0.14             | 4.61           | 1.32         | 0.03  | 1.21                       | 14.07          | 29                           | 0        |
| 1981 | 11    | 2                          | 0.28             | 4.04           | 1.32         | 0.03  | 1.07                       | 14.07          | 29                           | 0        |
| 1981 | 11    | 3                          | 0.42             | 24.28          | 1.32         | 0.03  | 0.93                       | 14.07          | 29                           | 0        |
| 1981 | 11    | 4                          | 0.98             | 68.23          | 1.32         | 0.03  | 0.36                       | 14.07          | 29                           | 0        |
| 1981 | 11    | 5                          | 0.17             | 25.93          | 1.32         | 0.03  | 1.18                       | 14.07          | 29                           | 0        |
| 1981 | 11    | 6                          | 0.46             | 9.35           | 1.32         | 0.03  | 0.88                       | 14.07          | 29                           | 0        |
| 1981 | 12    | 1                          | 0.31             | 12.78          | 1.32         | 0.03  | 1.04                       | 14.07          | 29                           | 0        |
| 1981 | 12    | 2                          | 0.2              | 11.62          | 1.32         | 0.03  | 1.15                       | 14.07          | 29                           | 0        |
| 1981 | 12    | 3                          | 0.17             | 8.62           | 1.32         | 0.03  | 1.18                       | 14.07          | 29                           | 0        |
| 1981 | 12    | 4                          | 0.17             | 3.44           | 1.32         | 0.03  | 1.18                       | 14.07          | 29                           | 0        |
| 1981 | 12    | 5                          | 0.34             | 5.79           | 1.32         | 0.03  | 1.01                       | 14.07          | 29                           | 0        |
| 1981 | 12    | 6                          | 0.77             | 37.81          | 1.58         | 0.03  | 0.84                       | 14.07          | 29                           | 0        |
| 1982 | 1     | 1                          | 0.39             | 21.37          | 1.32         | 0.03  | 0.96                       | 14.07          | 29                           | 0        |
| 1982 | 1     | 2                          | 0.89             | 11.65          | 1.32         | 0.03  | 0.45                       | 14.07          | 29                           | 0        |
| 1982 | 1     | 3                          | 1.4              | 4.37           | 1.32         | 0     | 0                          | 14.07          | 29                           | 0.06     |
| 1982 | 1     | 4                          | 0.9              | 18.14          | 1.32         | 0.03  | 0.44                       | 14.07          | 29                           | 0        |
| 1982 | 1     | 5                          | 0.64             | 15.83          | 1.32         | 0.03  | 0.7                        | 14.07          | 29                           | 0        |
| 1982 | 1     | 6                          | 0.55             | 3.66           | 1.32         | 0.03  | 1.06                       | 14.07          | 29                           | 0        |
| 1982 | 2     | 1                          | 0.48             | 2.77           | 1.32         | 0.02  | 0.86                       | 14.07          | 29                           | 0        |
| 1982 | 2     | 2                          | 0.22             | 1.14           | 1.32         | 0.02  | 1.12                       | 14.07          | 29                           | 0        |
| 1982 | 2     | 3                          | 0.29             | 1.73           | 1.32         | 0.02  | 1.05                       | 14.07          | 29                           | 0        |
| 1982 | 2     | 4                          | 0.22             | 1.57           | 1.32         | 0.02  | 1.12                       | 14.07          | 29                           | 0        |
| 1982 | 2     | 5                          | 0.18             | 3.33           | 1.32         | 0.02  | 1.16                       | 14.07          | 29                           | 0        |
| 1982 | 2     | 6                          | 0.13             | 2.83           | 1.32         | 0.01  | 1.05                       | 14.07          | 29                           | 0        |
| 1982 | 3     | 1                          | 0.29             | 9.13           | 1.32         | 0.02  | 0.97                       | 14.07          | 29                           | 0        |
| 1982 | 3     | 2                          | 0.37             | 31.73          | 1.32         | 0.02  | 0.75                       | 14.07          | 29                           | 0        |
| 1982 | 3     | 3                          | 0.61             | 12.63          | 1.32         | 0.02  | 0.75                       | 14.07          | 29                           | 0        |
| 1982 | 3     | 4                          | 0.59             | 16.98          | 1.32         | 0.02  | 0.99                       | 14.07          | 29                           | 0        |
| 1982 | 3     | 5                          | 0.44             | 24.54          | 1.32         | 0.02  | 1.19                       | 14.07          | 29                           | 0        |
| 1982 | 3     | 6                          | 0.42             | 8.13           | 1.58         | 0.03  | 1.06                       | 14.07          | 29                           | 0        |
| 1982 | 4     | 1                          | 0.27             | 10.43          | 1.32         | 0.02  | 1.11                       | 14.07          | 29                           | 0        |
| 1982 | 4     | 2                          | 0.23             | 10.64          | 1.32         | 0.02  | 1.13                       | 14.07          | 29                           | 0        |
| 1982 | 4     | 3                          | 0.21             | 7.22           | 1.32         | 0.02  | 1.13                       | 14.07          | 29                           | 0        |
| 1982 | 4     | 4                          | 0.34             | 17.29          | 1.32         | 0.02  | 1.1                        | 14.07          | 29                           | 0        |
| 1982 | 4     | 5                          | 0.23             | 5.42           | 1.32         | 0.02  | 1.01                       | 14.07          | 29                           | 0        |
| 1982 | 4     | 6                          | 0.33             | 7.44           | 1.32         | 0.02  | 1.01                       | 14.07          | 29                           | 0        |
| 1982 | 5     | 1                          | 0.24             | 5.44           | 1.32         | 0.02  | 1.1                        | 14.07          | 29                           | 0        |
| 1982 | 5     | 2                          | 0.21             | 3.58           | 1.32         | 0.02  | 1.13                       | 14.07          | 29                           | 0        |
| 1982 | 5     | 3                          | 0.16             | 3.36           | 1.32         | 0.02  | 1.18                       | 14.07          | 29                           | 0        |
| 1982 | 5     | 4                          | 0.11             | 1.94           | 1.32         | 0.02  | 1.23                       | 14.07          | 29                           | 0        |
| 1982 | 5     | 5                          | 0.11             | 1.7            | 1.32         | 0.02  | 1.23                       | 14.07          | 29                           | 0        |
| 1982 | 5     | 6                          | 0.17             | 2.31           | 1.58         | 0.03  | 1.44                       | 14.07          | 29                           | 0        |
| 1982 | 6     | 1                          | 0.25             | 2.43           | 1.32         | 0.02  | 1.09                       | 14.07          | 29                           | 0        |
| 1982 | 6     | 2                          | 0.18             | 3.79           | 1.32         | 0.02  | 1.15                       | 14.07          | 29                           | 0        |
| 1982 | 6     | 3                          | 0.13             | 2.56           | 1.32         | 0.02  | 1.2                        | 14.07          | 29                           | 0        |
| 1982 | 6     | 4                          | 0.11             | 2.54           | 1.32         | 0.02  | 1.22                       | 14.07          | 29                           | 0        |
| 1982 | 6     | 5                          | 0.07             | 1.89           | 1.32         | 0.02  | 1.26                       | 14.07          | 29                           | 0        |
| 1982 | 6     | 6                          | 0.11             | 1.29           | 1.32         | 0.02  | 1.22                       | 14.07          | 29                           | 0        |

Table F-35 (4) Reservoir Operation Study for Heightening of Krenceng Dam (without Diversion Tunnel) (4/12)

Net supply yield: 3.05m<sup>3</sup>/sec  
 Water conveyance capacity: 3.05 m<sup>3</sup>/sec  
 of 27.2 km pipe line

| Year | Month | Serial No. of 5 day period | Inflow discharge |               | Supply yield | Evapo | Water conveyance from Cida | Krenceng Storage volume | Reservoir Water level (El-m) | Spillout |
|------|-------|----------------------------|------------------|---------------|--------------|-------|----------------------------|-------------------------|------------------------------|----------|
|      |       |                            | Krenceng         | Cidahu intake |              |       |                            |                         |                              |          |
| 1982 | 7     | 1                          | 0.08             | 1.41          | 1.32         | 0.02  | 1.26                       | 14.07                   | 29                           | 0        |
| 1982 | 7     | 2                          | 0.07             | 1.28          | 1.32         | 0.02  | 1.27                       | 14.07                   | 29                           | 0        |
| 1982 | 7     | 3                          | 0.07             | 1.24          | 1.32         | 0.02  | 1.24                       | 14.04                   | 28.98                        | 0        |
| 1982 | 7     | 4                          | 0.17             | 1.79          | 1.32         | 0.02  | 1.24                       | 14.07                   | 29                           | 0        |
| 1982 | 7     | 5                          | 0.17             | 2.21          | 1.32         | 0.02  | 1.17                       | 14.07                   | 29                           | 0        |
| 1982 | 7     | 6                          | 0.2              | 4.78          | 1.58         | 0.03  | 1.41                       | 14.07                   | 29                           | 0        |
| 1982 | 8     | 1                          | 0.11             | 1.68          | 1.32         | 0.03  | 1.24                       | 14.07                   | 29                           | 0        |
| 1982 | 8     | 2                          | 0.08             | 1.28          | 1.32         | 0.03  | 1.26                       | 14.07                   | 29                           | 0        |
| 1982 | 8     | 3                          | 0.04             | 0.81          | 1.32         | 0.03  | 0.81                       | 13.58                   | 28.69                        | 0        |
| 1982 | 8     | 4                          | 0.03             | 0.69          | 1.32         | 0.03  | 0.69                       | 12.96                   | 28.3                         | 0        |
| 1982 | 8     | 5                          | 0.02             | 0.57          | 1.32         | 0.03  | 0.57                       | 12.2                    | 27.83                        | 0        |
| 1982 | 8     | 6                          | 0.02             | 0.54          | 1.58         | 0.03  | 0.54                       | 11.14                   | 27.17                        | 0        |
| 1982 | 9     | 1                          | 0.05             | 0.84          | 1.32         | 0.02  | 0.84                       | 10.69                   | 26.89                        | 0        |
| 1982 | 9     | 2                          | 0.05             | 0.57          | 1.32         | 0.02  | 0.57                       | 9.97                    | 26.44                        | 0        |
| 1982 | 9     | 3                          | 0.04             | 0.53          | 1.32         | 0.02  | 0.53                       | 9.21                    | 25.96                        | 0        |
| 1982 | 9     | 4                          | 0.04             | 0.45          | 1.32         | 0.02  | 0.45                       | 8.36                    | 25.43                        | 0        |
| 1982 | 9     | 5                          | 0.04             | 0.96          | 1.32         | 0.02  | 0.96                       | 8.02                    | 25.22                        | 0        |
| 1982 | 9     | 6                          | 0.05             | 1.07          | 1.32         | 0.02  | 1.07                       | 7.81                    | 25.09                        | 0        |
| 1982 | 10    | 1                          | 0.06             | 1.26          | 1.32         | 0.02  | 1.26                       | 7.8                     | 25.08                        | 0        |
| 1982 | 10    | 2                          | 0.04             | 0.56          | 1.32         | 0.02  | 0.56                       | 7.06                    | 24.5                         | 0        |
| 1982 | 10    | 3                          | 0.04             | 0.36          | 1.32         | 0.02  | 0.36                       | 6.13                    | 23.72                        | 0        |
| 1982 | 10    | 4                          | 0.11             | 0.96          | 1.32         | 0.02  | 0.96                       | 5.85                    | 23.49                        | 0        |
| 1982 | 10    | 5                          | 0.05             | 0.94          | 1.32         | 0.02  | 0.94                       | 5.5                     | 23.2                         | 0        |
| 1982 | 10    | 6                          | 0.05             | 0.63          | 1.58         | 0.02  | 0.63                       | 4.58                    | 22.42                        | 0        |
| 1982 | 11    | 1                          | 0.04             | 0.49          | 1.32         | 0.02  | 0.49                       | 3.78                    | 21.54                        | 0        |
| 1982 | 11    | 2                          | 0.06             | 5.34          | 1.32         | 0.01  | 1.32                       | 3.87                    | 21.59                        | 0        |
| 1982 | 11    | 3                          | 0.06             | 1.72          | 1.32         | 0.01  | 1.32                       | 3.87                    | 21.65                        | 0        |
| 1982 | 11    | 4                          | 0.06             | 0.78          | 1.32         | 0.01  | 0.78                       | 3.38                    | 21.1                         | 0        |
| 1982 | 11    | 5                          | 0.06             | 2.65          | 1.32         | 0.01  | 1.32                       | 3.42                    | 21.15                        | 0        |
| 1982 | 11    | 6                          | 0.06             | 2.54          | 1.32         | 0.01  | 1.32                       | 3.47                    | 21.2                         | 0        |
| 1982 | 12    | 1                          | 0.04             | 1.36          | 1.32         | 0.01  | 1.32                       | 3.5                     | 21.23                        | 0        |
| 1982 | 12    | 2                          | 0.04             | 0.42          | 1.32         | 0.01  | 0.42                       | 2.63                    | 20.21                        | 0        |
| 1982 | 12    | 3                          | 0.04             | 2.22          | 1.32         | 0.01  | 1.32                       | 2.66                    | 20.26                        | 0        |
| 1982 | 12    | 4                          | 0.04             | 2.79          | 1.32         | 0.01  | 1.32                       | 2.69                    | 20.31                        | 0        |
| 1982 | 12    | 5                          | 0.05             | 2.93          | 1.32         | 0.01  | 1.32                       | 2.73                    | 20.36                        | 0        |
| 1982 | 12    | 6                          | 0.13             | 8.58          | 1.58         | 0.01  | 1.58                       | 2.84                    | 20.51                        | 0        |
| 1983 | 1     | 1                          | 0.19             | 6.77          | 1.32         | 0.01  | 1.32                       | 3.02                    | 20.7                         | 0        |
| 1983 | 1     | 2                          | 0.11             | 6.98          | 1.32         | 0.01  | 1.32                       | 3.11                    | 20.81                        | 0        |
| 1983 | 1     | 3                          | 0.08             | 6.17          | 1.32         | 0.01  | 1.32                       | 3.18                    | 20.88                        | 0        |
| 1983 | 1     | 4                          | 0.12             | 11.05         | 1.32         | 0.01  | 1.32                       | 3.28                    | 21                           | 0        |
| 1983 | 1     | 5                          | 0.32             | 20.04         | 1.32         | 0.01  | 1.32                       | 3.59                    | 21.34                        | 0        |
| 1983 | 1     | 6                          | 0.06             | 13.66         | 1.58         | 0.02  | 1.58                       | 3.63                    | 21.38                        | 0        |
| 1983 | 2     | 1                          | 0.22             | 7.9           | 1.32         | 0.01  | 1.32                       | 3.84                    | 21.61                        | 0        |
| 1983 | 2     | 2                          | 0.22             | 9.4           | 1.32         | 0.01  | 1.32                       | 4.05                    | 21.83                        | 0        |
| 1983 | 2     | 3                          | 0.06             | 2.59          | 1.32         | 0.01  | 1.32                       | 4.09                    | 21.88                        | 0        |
| 1983 | 2     | 4                          | 0.14             | 2.82          | 1.32         | 0.01  | 1.32                       | 4.21                    | 22.02                        | 0        |
| 1983 | 2     | 5                          | 0.08             | 3.12          | 1.32         | 0.01  | 1.32                       | 4.23                    | 22.09                        | 0        |
| 1983 | 2     | 6                          | 0.26             | 2.49          | 0.79         | 0.01  | 0.79                       | 4.54                    | 22.37                        | 0        |
| 1983 | 3     | 1                          | 0.43             | 5.41          | 1.32         | 0.01  | 1.32                       | 4.96                    | 22.75                        | 0        |
| 1983 | 3     | 2                          | 0.19             | 2.72          | 1.32         | 0.01  | 1.32                       | 5.14                    | 22.9                         | 0        |
| 1983 | 3     | 3                          | 0.16             | 2.32          | 1.32         | 0.01  | 1.32                       | 5.29                    | 23.02                        | 0        |
| 1983 | 3     | 4                          | 0.06             | 1.99          | 1.32         | 0.01  | 1.32                       | 5.34                    | 23.06                        | 0        |
| 1983 | 3     | 5                          | 0.07             | 1.97          | 1.32         | 0.01  | 1.32                       | 5.39                    | 23.11                        | 0        |
| 1983 | 3     | 6                          | 0.31             | 3.53          | 1.58         | 0.02  | 1.58                       | 5.69                    | 23.36                        | 0        |
| 1983 | 4     | 1                          | 0.19             | 4.93          | 1.32         | 0.01  | 1.32                       | 5.86                    | 23.5                         | 0        |
| 1983 | 4     | 2                          | 0.3              | 4.37          | 1.32         | 0.01  | 1.32                       | 6.14                    | 23.73                        | 0        |
| 1983 | 4     | 3                          | 0.06             | 3.8           | 1.32         | 0.01  | 1.32                       | 6.19                    | 23.77                        | 0        |
| 1983 | 4     | 4                          | 0.14             | 4.52          | 1.32         | 0.01  | 1.32                       | 6.31                    | 23.87                        | 0        |
| 1983 | 4     | 5                          | 0.59             | 3.83          | 1.32         | 0.01  | 1.32                       | 6.88                    | 24.35                        | 0        |
| 1983 | 4     | 6                          | 0.45             | 4.72          | 1.32         | 0.02  | 1.32                       | 7.32                    | 24.71                        | 0        |

(Unit: 10 m<sup>3</sup>)

Table F-35 (5) Reservoir Operation Study for Heightening of Krencong Dam (without Diversion Tunnel) (5/12)

Net supply yield: 3.05m<sup>3</sup>/sec  
 Water conveyance capacity: 3.05 m<sup>3</sup>/sec  
 of 27.2 km pipe line

(Unit: 10 m<sup>3</sup>)

| Year | Month | Serial No. of 5 day period | Inflow discharge |               | Evapo | Supply yield | Water conveyance from Cida | Krencong Storage volume | Reservoir Water level (Bt-m) | Spillover |
|------|-------|----------------------------|------------------|---------------|-------|--------------|----------------------------|-------------------------|------------------------------|-----------|
|      |       |                            | Krencong         | Cidahu Intake |       |              |                            |                         |                              |           |
| 1983 | 5     | 1                          | 0.25             | 2.07          | 0.02  | 1.32         | 1.32                       | 7.55                    | 24.9                         | 0         |
| 1983 | 5     | 2                          | 0.46             | 2.03          | 0.02  | 1.32         | 1.32                       | 8                       | 25.2                         | 0         |
| 1983 | 5     | 3                          | 0.28             | 6.1           | 0.02  | 1.32         | 1.32                       | 8.26                    | 25.37                        | 0         |
| 1983 | 5     | 4                          | 0.28             | 3.08          | 0.02  | 1.32         | 1.32                       | 8.53                    | 25.53                        | 0         |
| 1983 | 5     | 5                          | 0.18             | 4.03          | 0.02  | 1.32         | 1.32                       | 8.69                    | 25.63                        | 0         |
| 1983 | 5     | 6                          | 0.27             | 3.11          | 0.02  | 1.32         | 1.32                       | 8.94                    | 25.79                        | 0         |
| 1983 | 5     | 1                          | 0.15             | 4.03          | 0.02  | 1.32         | 1.32                       | 9.07                    | 25.87                        | 0         |
| 1983 | 6     | 2                          | 0.97             | 3.43          | 0.02  | 1.32         | 1.32                       | 10.02                   | 26.47                        | 0         |
| 1983 | 6     | 3                          | 0.36             | 2.69          | 0.02  | 1.32         | 1.32                       | 10.37                   | 26.69                        | 0         |
| 1983 | 6     | 4                          | 0.21             | 3.92          | 0.02  | 1.32         | 1.32                       | 10.57                   | 26.81                        | 0         |
| 1983 | 6     | 5                          | 0.12             | 4.85          | 0.02  | 1.32         | 1.32                       | 10.67                   | 26.88                        | 0         |
| 1983 | 6     | 6                          | 0.27             | 5.14          | 0.02  | 1.32         | 1.32                       | 10.92                   | 27.03                        | 0         |
| 1983 | 7     | 1                          | 0.15             | 7.96          | 0.02  | 1.32         | 1.32                       | 11.06                   | 27.12                        | 0         |
| 1983 | 7     | 2                          | 0.02             | 4.92          | 0.02  | 1.32         | 1.32                       | 11.06                   | 27.12                        | 0         |
| 1983 | 7     | 3                          | 0.02             | 2.54          | 0.02  | 1.32         | 1.32                       | 11.06                   | 27.12                        | 0         |
| 1983 | 7     | 4                          | 0.05             | 3.36          | 0.02  | 1.32         | 1.32                       | 11.09                   | 27.14                        | 0         |
| 1983 | 7     | 5                          | 0.05             | 2.46          | 0.02  | 1.32         | 1.32                       | 11.12                   | 27.15                        | 0         |
| 1983 | 7     | 6                          | 0.06             | 3.27          | 0.02  | 1.32         | 1.32                       | 11.16                   | 27.18                        | 0         |
| 1983 | 8     | 1                          | 0.02             | 1.43          | 0.02  | 1.32         | 1.32                       | 11.15                   | 27.17                        | 0         |
| 1983 | 8     | 2                          | 0.02             | 0.68          | 0.02  | 1.32         | 1.32                       | 10.5                    | 26.77                        | 0         |
| 1983 | 8     | 3                          | 0.01             | 1.2           | 0.02  | 1.32         | 1.32                       | 10.38                   | 26.69                        | 0         |
| 1983 | 8     | 4                          | 0.01             | 1.48          | 0.02  | 1.32         | 1.32                       | 10.37                   | 26.68                        | 0         |
| 1983 | 8     | 5                          | 0.03             | 3.93          | 0.02  | 1.32         | 1.32                       | 10.37                   | 26.68                        | 0         |
| 1983 | 8     | 6                          | 0.01             | 1.06          | 0.03  | 1.32         | 1.32                       | 10.6                    | 26.35                        | 0         |
| 1983 | 9     | 1                          | 0                | 0.49          | 0.02  | 1.32         | 1.32                       | 9.88                    | 25.82                        | 0         |
| 1983 | 9     | 2                          | 0.01             | 0.76          | 0.02  | 1.32         | 1.32                       | 8.41                    | 25.46                        | 0         |
| 1983 | 9     | 3                          | 0.01             | 0.85          | 0.02  | 1.32         | 1.32                       | 8.85                    | 25.16                        | 0         |
| 1983 | 9     | 4                          | 0.01             | 0.7           | 0.02  | 1.32         | 1.32                       | 7.31                    | 24.7                         | 0         |
| 1983 | 9     | 5                          | 0.01             | 0.7           | 0.02  | 1.32         | 1.32                       | 6.68                    | 24.18                        | 0         |
| 1983 | 9     | 6                          | 0.01             | 0.54          | 0.02  | 1.32         | 1.32                       | 5.89                    | 23.53                        | 0         |
| 1983 | 10    | 1                          | 0                | 0.38          | 0.02  | 1.32         | 1.32                       | 4.94                    | 22.74                        | 0         |
| 1983 | 10    | 2                          | 0                | 0.29          | 0.02  | 1.32         | 1.32                       | 3.9                     | 21.67                        | 0         |
| 1983 | 10    | 3                          | 0                | 0.33          | 0.01  | 1.32         | 1.32                       | 2.89                    | 20.57                        | 0         |
| 1983 | 10    | 4                          | 0                | 0.37          | 0.01  | 1.32         | 1.32                       | 1.96                    | 19.25                        | 0         |
| 1983 | 10    | 5                          | 0.04             | 2.51          | 0.01  | 1.32         | 1.32                       | 2                       | 19.3                         | 0         |
| 1983 | 10    | 6                          | 0.05             | 6.55          | 0.01  | 1.32         | 1.32                       | 2.03                    | 19.35                        | 0         |
| 1983 | 11    | 1                          | 0.04             | 7.08          | 0.01  | 1.32         | 1.32                       | 2.1                     | 19.45                        | 0         |
| 1983 | 11    | 2                          | 0.08             | 5.71          | 0.01  | 1.32         | 1.32                       | 2.1                     | 19.44                        | 0         |
| 1983 | 11    | 3                          | 0.01             | 7.36          | 0.01  | 1.32         | 1.32                       | 2.55                    | 20.1                         | 0         |
| 1983 | 11    | 4                          | 0.47             | 39.04         | 0.01  | 1.32         | 1.32                       | 3.24                    | 20.95                        | 0         |
| 1983 | 11    | 5                          | 1.37             | 0.64          | 0.01  | 1.32         | 1.32                       | 7.13                    | 24.55                        | 0         |
| 1983 | 11    | 6                          | 3.91             | 21.87         | 0.01  | 1.32         | 1.32                       | 7.48                    | 24.84                        | 0         |
| 1983 | 12    | 1                          | 0.37             | 19.35         | 0.02  | 1.32         | 1.32                       | 7.82                    | 25.09                        | 0         |
| 1983 | 12    | 2                          | 0.36             | 10.29         | 0.02  | 1.32         | 1.32                       | 7.92                    | 25.15                        | 0         |
| 1983 | 12    | 3                          | 0.12             | 4.38          | 0.02  | 1.32         | 1.32                       | 7.98                    | 25.19                        | 0         |
| 1983 | 12    | 4                          | 0.08             | 4.43          | 0.02  | 1.32         | 1.32                       | 8.02                    | 25.21                        | 0         |
| 1983 | 12    | 5                          | 0.06             | 3.73          | 0.02  | 1.32         | 1.32                       | 8.07                    | 25.25                        | 0         |
| 1983 | 12    | 6                          | 0.08             | 7.05          | 0.02  | 1.32         | 1.32                       | 8.17                    | 25.31                        | 0         |
| 1984 | 1     | 1                          | 0.12             | 5.67          | 0.02  | 1.32         | 1.32                       | 8.38                    | 25.44                        | 0         |
| 1984 | 1     | 2                          | 0.23             | 1.38          | 0.02  | 1.32         | 1.32                       | 8.44                    | 25.48                        | 0         |
| 1984 | 1     | 3                          | 0.08             | 6.24          | 0.02  | 1.32         | 1.32                       | 8.55                    | 25.55                        | 0         |
| 1984 | 1     | 4                          | 0.13             | 6.94          | 0.02  | 1.32         | 1.32                       | 9.42                    | 26.09                        | 0         |
| 1984 | 1     | 5                          | 0.9              | 7.06          | 0.02  | 1.32         | 1.32                       | 11.08                   | 27.13                        | 0         |
| 1984 | 1     | 6                          | 1.69             | 9.84          | 0.03  | 1.32         | 1.32                       | 11.52                   | 27.4                         | 0         |
| 1984 | 2     | 1                          | 0.46             | 7.43          | 0.02  | 1.32         | 1.32                       | 11.83                   | 27.6                         | 0         |
| 1984 | 2     | 2                          | 0.94             | 12.52         | 0.02  | 1.32         | 1.32                       | 12.21                   | 27.84                        | 0         |
| 1984 | 2     | 3                          | 0.4              | 5.84          | 0.02  | 1.32         | 1.32                       | 12.98                   | 28.32                        | 0         |
| 1984 | 2     | 4                          | 0.8              | 4.15          | 0.02  | 1.32         | 1.32                       | 13.68                   | 28.76                        | 0         |
| 1984 | 2     | 5                          | 0.72             | 2.87          | 0.02  | 1.32         | 1.32                       | 14.07                   | 29                           | 0         |
| 1984 | 2     | 6                          | 0.46             | 6.03          | 1.05  | 1.05         | 1.01                       |                         |                              |           |



Table F-35 (6) Reservoir Operation Study for Heightening of Krenceng Dam (without Diversion Tunnel) (6/12)

Net supply yield: 3.05m<sup>3</sup>/sec  
 Water conveyance capacity: 3.05 m<sup>3</sup>/sec  
 of 27.2 km pipe line

(Unit: 10<sup>6</sup> m<sup>3</sup>)

| Year | Month | Serial No. of 5 day period | Inflow discharge |                | Supply yield | Evapo | Water conveyance from Cida | Krenceng Storage volume | Reservoir Water level (El-m) | Spillout |
|------|-------|----------------------------|------------------|----------------|--------------|-------|----------------------------|-------------------------|------------------------------|----------|
|      |       |                            | Krenceng         | Cidaman intake |              |       |                            |                         |                              |          |
| 1984 | 3     | 1                          | 0.33             | 5.87           | 1.32         | 0.02  | 0.96                       | 14.07                   | 29                           | 0        |
| 1984 | 3     | 2                          | 1.01             | 10.68          | 1.32         | 0.02  | 0.33                       | 14.07                   | 29                           | 0        |
| 1984 | 3     | 3                          | 1.41             | 12.95          | 1.32         | 0.02  | 0                          | 14.07                   | 29                           | 0.08     |
| 1984 | 3     | 4                          | 0.92             | 10.75          | 1.32         | 0.02  | 0.42                       | 14.07                   | 29                           | 0        |
| 1984 | 3     | 5                          | 1.78             | 19.09          | 1.32         | 0.02  | 0                          | 14.07                   | 29                           | 0.44     |
| 1984 | 3     | 6                          | 2.02             | 26.41          | 1.58         | 0.03  | 0                          | 14.07                   | 29                           | 0.42     |
| 1984 | 4     | 1                          | 0.18             | 11.88          | 1.32         | 0.02  | 1.16                       | 14.07                   | 29                           | 0        |
| 1984 | 4     | 2                          | 0.24             | 2.36           | 1.32         | 0.02  | 1.1                        | 14.07                   | 29                           | 0        |
| 1984 | 4     | 3                          | 0.16             | 3.83           | 1.32         | 0.02  | 1.18                       | 14.07                   | 29                           | 0        |
| 1984 | 4     | 4                          | 0.24             | 3.37           | 1.32         | 0.02  | 1.1                        | 14.07                   | 29                           | 0        |
| 1984 | 4     | 5                          | 0.18             | 4.38           | 1.32         | 0.02  | 1.16                       | 14.07                   | 29                           | 0        |
| 1984 | 4     | 6                          | 0.46             | 6.49           | 1.32         | 0.02  | 0.88                       | 14.07                   | 29                           | 0        |
| 1984 | 5     | 1                          | 0.5              | 5.85           | 1.32         | 0.02  | 0.84                       | 14.07                   | 29                           | 0        |
| 1984 | 5     | 2                          | 0.42             | 10.68          | 1.32         | 0.02  | 0.92                       | 14.07                   | 29                           | 0        |
| 1984 | 5     | 3                          | 0.22             | 15.63          | 1.32         | 0.02  | 1.12                       | 14.07                   | 29                           | 0        |
| 1984 | 5     | 4                          | 0.15             | 5.8            | 1.32         | 0.02  | 1.19                       | 14.07                   | 29                           | 0        |
| 1984 | 5     | 5                          | 0.24             | 3.97           | 1.32         | 0.02  | 1.1                        | 14.07                   | 29                           | 0        |
| 1984 | 5     | 6                          | 0.22             | 12.63          | 1.58         | 0.03  | 1.39                       | 14.07                   | 29                           | 0        |
| 1984 | 6     | 1                          | 0.2              | 6.23           | 1.32         | 0.02  | 1.14                       | 14.07                   | 29                           | 0        |
| 1984 | 6     | 2                          | 0.17             | 3.47           | 1.32         | 0.02  | 1.17                       | 14.07                   | 29                           | 0        |
| 1984 | 6     | 3                          | 0.21             | 3.15           | 1.32         | 0.02  | 1.12                       | 14.07                   | 29                           | 0        |
| 1984 | 6     | 4                          | 0.21             | 2.61           | 1.32         | 0.02  | 1.13                       | 14.07                   | 29                           | 0        |
| 1984 | 6     | 5                          | 0.14             | 3.12           | 1.32         | 0.02  | 1.2                        | 14.07                   | 29                           | 0        |
| 1984 | 6     | 6                          | 0.1              | 1.39           | 1.32         | 0.02  | 1.24                       | 14.07                   | 29                           | 0        |
| 1984 | 6     | 7                          | 0.24             | 2.29           | 1.32         | 0.02  | 1.1                        | 14.07                   | 29                           | 0        |
| 1984 | 7     | 1                          | 0.17             | 4.9            | 1.32         | 0.02  | 1.17                       | 14.07                   | 29                           | 0        |
| 1984 | 7     | 2                          | 0.09             | 3.29           | 1.32         | 0.02  | 1.25                       | 14.07                   | 29                           | 0        |
| 1984 | 7     | 3                          | 0.08             | 2.15           | 1.32         | 0.02  | 1.26                       | 14.07                   | 29                           | 0        |
| 1984 | 7     | 4                          | 0.16             | 2.76           | 1.32         | 0.02  | 1.18                       | 14.07                   | 29                           | 0        |
| 1984 | 7     | 5                          | 0.18             | 3.74           | 1.58         | 0.03  | 1.43                       | 14.07                   | 29                           | 0        |
| 1984 | 7     | 6                          | 0.09             | 2.5            | 1.32         | 0.03  | 1.26                       | 14.07                   | 29                           | 0        |
| 1984 | 8     | 1                          | 0.07             | 1.93           | 1.32         | 0.03  | 1.28                       | 14.07                   | 29                           | 0        |
| 1984 | 8     | 2                          | 0.15             | 1.48           | 1.32         | 0.03  | 1.19                       | 14.07                   | 29                           | 0        |
| 1984 | 8     | 3                          | 0.09             | 1.51           | 1.32         | 0.03  | 1.25                       | 14.07                   | 29                           | 0        |
| 1984 | 8     | 4                          | 0.08             | 1.4            | 1.32         | 0.03  | 1.26                       | 14.07                   | 29                           | 0        |
| 1984 | 8     | 5                          | 0.19             | 2.17           | 1.58         | 0.03  | 1.45                       | 14.07                   | 29                           | 0        |
| 1984 | 8     | 6                          | 0.11             | 1.67           | 1.32         | 0.03  | 1.23                       | 14.07                   | 29                           | 0        |
| 1984 | 9     | 1                          | 0.39             | 4.99           | 1.32         | 0.03  | 0.96                       | 14.07                   | 29                           | 0        |
| 1984 | 9     | 2                          | 0.4              | 6.26           | 1.32         | 0.03  | 0.94                       | 14.07                   | 29                           | 0        |
| 1984 | 9     | 3                          | 0.27             | 5.04           | 1.32         | 0.03  | 1.07                       | 14.07                   | 29                           | 0        |
| 1984 | 9     | 4                          | 0.18             | 4.38           | 1.32         | 0.03  | 1.16                       | 14.07                   | 29                           | 0        |
| 1984 | 9     | 5                          | 0.42             | 3.48           | 1.32         | 0.03  | 0.92                       | 14.07                   | 29                           | 0        |
| 1984 | 9     | 6                          | 0.48             | 10.4           | 1.32         | 0.03  | 0.87                       | 14.07                   | 29                           | 0        |
| 1984 | 10    | 1                          | 0.13             | 4.41           | 1.32         | 0.03  | 1.21                       | 14.07                   | 29                           | 0        |
| 1984 | 10    | 2                          | 0.22             | 2.02           | 1.32         | 0.03  | 1.12                       | 14.07                   | 29                           | 0        |
| 1984 | 10    | 3                          | 0.18             | 2.39           | 1.32         | 0.03  | 1.16                       | 14.07                   | 29                           | 0        |
| 1984 | 10    | 4                          | 0.22             | 2.31           | 1.32         | 0.03  | 1.13                       | 14.07                   | 29                           | 0        |
| 1984 | 10    | 5                          | 0.13             | 3.38           | 1.58         | 0.03  | 1.48                       | 14.07                   | 29                           | 0        |
| 1984 | 10    | 6                          | 0.15             | 1.61           | 1.32         | 0.03  | 1.2                        | 14.07                   | 29                           | 0        |
| 1984 | 11    | 1                          | 0.08             | 2.76           | 1.32         | 0.03  | 1.26                       | 14.07                   | 29                           | 0        |
| 1984 | 11    | 2                          | 0.08             | 4.87           | 1.32         | 0.03  | 1.26                       | 14.07                   | 29                           | 0        |
| 1984 | 11    | 3                          | 0.19             | 4.94           | 1.32         | 0.03  | 1.16                       | 14.07                   | 29                           | 0        |
| 1984 | 11    | 4                          | 0.14             | 5.57           | 1.32         | 0.03  | 1.2                        | 14.07                   | 29                           | 0        |
| 1984 | 11    | 5                          | 0.08             | 3.76           | 1.32         | 0.03  | 1.27                       | 14.07                   | 29                           | 0        |
| 1984 | 11    | 6                          | 0.1              | 19.97          | 1.32         | 0.03  | 1.24                       | 14.07                   | 29                           | 0        |
| 1984 | 12    | 1                          | 0.09             | 19.21          | 1.32         | 0.03  | 1.26                       | 14.07                   | 29                           | 0        |
| 1984 | 12    | 2                          | 0.12             | 7.94           | 1.32         | 0.03  | 1.2                        | 14.07                   | 29                           | 0        |
| 1984 | 12    | 3                          | 0.12             | 7.01           | 1.32         | 0.03  | 1.23                       | 14.07                   | 29                           | 0        |
| 1984 | 12    | 4                          | 0.1              | 3.33           | 1.32         | 0.03  | 1.24                       | 14.07                   | 29                           | 0        |
| 1984 | 12    | 5                          | 0.39             | 17.34          | 1.58         | 0.03  | 1.23                       | 14.07                   | 29                           | 0        |
| 1984 | 12    | 6                          |                  |                |              |       |                            |                         |                              |          |

Table F-35 (7) Reservoir Operation Study for Heightening of Krenceng Dam (without Diversion Tunnel) (7/12)

Net supply yield: 3.05m<sup>3</sup>/sec  
 Water conveyance capacity: 3.05 m<sup>3</sup>/sec  
 at 27.2 km pipe line

(Unit: 10<sup>6</sup> m<sup>3</sup>)

| Year | Month | Serial No. of 5 day period | Inflow discharge |                | Supply yield | Evapo | Water conveyance from Cites | Krenceng Storage volume | Reservoir Water level (El-m) | Spillout |
|------|-------|----------------------------|------------------|----------------|--------------|-------|-----------------------------|-------------------------|------------------------------|----------|
|      |       |                            | Krenceng         | Cidraou Intake |              |       |                             |                         |                              |          |
| 1985 | 1     | 1                          | 0.11             | 9.49           | 1.32         | 0.03  | 1.23                        | 14.07                   | 29                           | 0        |
| 1985 | 1     | 2                          | 0.41             | 8.38           | 1.32         | 0.03  | 0.94                        | 14.07                   | 29                           | 0        |
| 1985 | 1     | 3                          | 0.11             | 16.18          | 1.32         | 0.03  | 1.23                        | 14.07                   | 29                           | 0        |
| 1985 | 1     | 4                          | 0.09             | 5.53           | 1.32         | 0.03  | 1.26                        | 14.07                   | 29                           | 0        |
| 1985 | 1     | 5                          | 0.12             | 3.77           | 1.32         | 0.03  | 1.23                        | 14.07                   | 29                           | 0        |
| 1985 | 1     | 6                          | 0.23             | 6.98           | 1.38         | 0.03  | 1.38                        | 14.07                   | 29                           | 0        |
| 1985 | 2     | 1                          | 0.1              | 5.16           | 1.32         | 0.02  | 1.24                        | 14.07                   | 29                           | 0        |
| 1985 | 2     | 2                          | 0.69             | 5.12           | 1.32         | 0.02  | 1.26                        | 14.07                   | 29                           | 0        |
| 1985 | 2     | 3                          | 0.07             | 6.31           | 1.32         | 0.02  | 1.27                        | 14.07                   | 29                           | 0        |
| 1985 | 2     | 4                          | 0.05             | 3.27           | 1.32         | 0.02  | 1.29                        | 14.07                   | 29                           | 0        |
| 1985 | 2     | 5                          | 0.18             | 5.68           | 1.32         | 0.02  | 1.16                        | 14.07                   | 29                           | 0        |
| 1985 | 2     | 6                          | 0.53             | 3.67           | 0.79         | 0.01  | 0.78                        | 14.07                   | 29                           | 0        |
| 1985 | 3     | 1                          | 0.17             | 5.65           | 1.32         | 0.02  | 1.17                        | 14.07                   | 29                           | 0        |
| 1985 | 3     | 2                          | 0.38             | 18.22          | 1.32         | 0.02  | 0.96                        | 14.07                   | 29                           | 0        |
| 1985 | 3     | 3                          | 0.14             | 14.18          | 1.32         | 0.02  | 1.19                        | 14.07                   | 29                           | 0        |
| 1985 | 3     | 4                          | 0.15             | 4.8            | 1.32         | 0.02  | 1.19                        | 14.07                   | 29                           | 0        |
| 1985 | 3     | 5                          | 0.08             | 2.99           | 1.32         | 0.02  | 1.26                        | 14.07                   | 29                           | 0        |
| 1985 | 3     | 6                          | 0.15             | 2.65           | 1.58         | 0.03  | 1.46                        | 14.07                   | 29                           | 0        |
| 1985 | 4     | 1                          | 0.11             | 1.83           | 1.32         | 0.02  | 1.23                        | 14.07                   | 29                           | 0        |
| 1985 | 4     | 2                          | 0.15             | 2.37           | 1.32         | 0.02  | 1.19                        | 14.07                   | 29                           | 0        |
| 1985 | 4     | 3                          | 0.25             | 4.57           | 1.32         | 0.02  | 1.09                        | 14.07                   | 29                           | 0        |
| 1985 | 4     | 4                          | 0.57             | 9.42           | 1.32         | 0.02  | 0.77                        | 14.07                   | 29                           | 0        |
| 1985 | 4     | 5                          | 0.18             | 6.9            | 1.32         | 0.02  | 1.16                        | 14.07                   | 29                           | 0        |
| 1985 | 4     | 6                          | 0.18             | 7.61           | 1.32         | 0.02  | 1.16                        | 14.07                   | 29                           | 0        |
| 1985 | 5     | 1                          | 0.1              | 6.54           | 1.32         | 0.02  | 1.23                        | 14.07                   | 29                           | 0        |
| 1985 | 5     | 2                          | 0.08             | 5.09           | 1.32         | 0.02  | 1.26                        | 14.07                   | 29                           | 0        |
| 1985 | 5     | 3                          | 0.09             | 4.03           | 1.32         | 0.02  | 1.25                        | 14.07                   | 29                           | 0        |
| 1985 | 5     | 4                          | 0.06             | 3.38           | 1.32         | 0.02  | 1.28                        | 14.07                   | 29                           | 0        |
| 1985 | 5     | 5                          | 0.05             | 3.62           | 1.32         | 0.02  | 1.29                        | 14.07                   | 29                           | 0        |
| 1985 | 5     | 6                          | 0.09             | 3.49           | 1.38         | 0.03  | 1.51                        | 14.07                   | 29                           | 0        |
| 1985 | 6     | 1                          | 0.06             | 2.26           | 1.32         | 0.02  | 1.28                        | 14.07                   | 29                           | 0        |
| 1985 | 6     | 2                          | 0.08             | 2.06           | 1.32         | 0.02  | 1.26                        | 14.07                   | 29                           | 0        |
| 1985 | 6     | 3                          | 0.05             | 2.49           | 1.32         | 0.02  | 1.28                        | 14.07                   | 29                           | 0        |
| 1985 | 6     | 4                          | 0.06             | 3.07           | 1.32         | 0.02  | 1.28                        | 14.07                   | 29                           | 0        |
| 1985 | 6     | 5                          | 0.21             | 3.17           | 1.32         | 0.02  | 1.13                        | 14.07                   | 29                           | 0        |
| 1985 | 6     | 6                          | 0.06             | 2.9            | 1.32         | 0.02  | 1.28                        | 14.07                   | 29                           | 0        |
| 1985 | 7     | 1                          | 0.07             | 2.05           | 1.32         | 0.02  | 1.27                        | 14.07                   | 29                           | 0        |
| 1985 | 7     | 2                          | 0.14             | 2.08           | 1.32         | 0.02  | 1.2                         | 14.07                   | 29                           | 0        |
| 1985 | 7     | 3                          | 0.17             | 2.3            | 1.32         | 0.02  | 1.17                        | 14.07                   | 29                           | 0        |
| 1985 | 7     | 4                          | 0.17             | 2.46           | 1.32         | 0.02  | 1.17                        | 14.07                   | 29                           | 0        |
| 1985 | 7     | 5                          | 0.27             | 5.96           | 1.32         | 0.02  | 1.07                        | 14.07                   | 29                           | 0        |
| 1985 | 7     | 6                          | 0.11             | 7.88           | 1.38         | 0.03  | 1.5                         | 14.07                   | 29                           | 0        |
| 1985 | 8     | 1                          | 0.25             | 5.37           | 1.32         | 0.03  | 1.1                         | 14.07                   | 29                           | 0        |
| 1985 | 8     | 2                          | 0.09             | 5.21           | 1.32         | 0.03  | 1.25                        | 14.07                   | 29                           | 0        |
| 1985 | 8     | 3                          | 0.06             | 3.17           | 1.32         | 0.03  | 1.28                        | 14.07                   | 29                           | 0        |
| 1985 | 8     | 4                          | 0.06             | 2.71           | 1.32         | 0.03  | 1.28                        | 14.07                   | 29                           | 0        |
| 1985 | 8     | 5                          | 0.05             | 2.06           | 1.32         | 0.03  | 1.3                         | 14.07                   | 29                           | 0        |
| 1985 | 8     | 6                          | 0.07             | 1.82           | 1.58         | 0.03  | 1.55                        | 14.07                   | 29                           | 0        |
| 1985 | 9     | 1                          | 0.04             | 1.18           | 1.32         | 0.03  | 1.18                        | 13.95                   | 28.92                        | 0        |
| 1985 | 9     | 2                          | 0.08             | 1.2            | 1.32         | 0.03  | 1.2                         | 13.89                   | 28.89                        | 0        |
| 1985 | 9     | 3                          | 0.06             | 4.41           | 1.32         | 0.03  | 1.32                        | 13.92                   | 28.91                        | 0        |
| 1985 | 9     | 4                          | 0.05             | 3.4            | 1.32         | 0.03  | 1.32                        | 13.95                   | 28.92                        | 0        |
| 1985 | 9     | 5                          | 0.04             | 2.39           | 1.32         | 0.03  | 1.32                        | 13.96                   | 28.93                        | 0        |
| 1985 | 9     | 6                          | 0.1              | 2.22           | 1.32         | 0.03  | 1.32                        | 14.03                   | 28.98                        | 0        |
| 1985 | 10    | 1                          | 0.12             | 1.75           | 1.32         | 0.03  | 1.27                        | 14.07                   | 29                           | 0        |
| 1985 | 10    | 2                          | 0.1              | 2.66           | 1.32         | 0.03  | 1.24                        | 14.07                   | 29                           | 0        |
| 1985 | 10    | 3                          | 0.07             | 5.63           | 1.32         | 0.03  | 1.27                        | 14.07                   | 29                           | 0        |
| 1985 | 10    | 4                          | 0.34             | 7.23           | 1.32         | 0.03  | 1.01                        | 14.07                   | 29                           | 0        |
| 1985 | 10    | 5                          | 0.07             | 9.42           | 1.32         | 0.03  | 1.27                        | 14.07                   | 29                           | 0        |
| 1985 | 10    | 6                          | 0.08             | 5.41           | 1.58         | 0.03  | 1.53                        | 14.07                   | 29                           | 0        |

Table F-35 (8) Reservoir Operation Study for Heightening of Krenceng Dam (without Diversion Tunnel) (8/12)

Net supply yield: 3.05m<sup>3</sup>/sec  
 Water conveyance capacity: 3.05 m<sup>3</sup>/sec  
 of 27.2 km pipe line

| Year | Month | Serial No. of 5 day period | Inflow discharge |                | Supply yield | Evapo | Water conveyance from Cida | Krenceng Storage volume | Reservoir Water level (El-m) | Spillout |
|------|-------|----------------------------|------------------|----------------|--------------|-------|----------------------------|-------------------------|------------------------------|----------|
|      |       |                            | Krenceng         | Cidmanu intake |              |       |                            |                         |                              |          |
| 1985 | 11    | 1                          | 0.08             | 4.09           | 1.32         | 0.03  | 1.26                       | 14.07                   | 29                           | 0        |
| 1985 | 11    | 2                          | 0.15             | 3.88           | 1.32         | 0.03  | 1.2                        | 14.07                   | 29                           | 0        |
| 1985 | 11    | 3                          | 0.06             | 4.31           | 1.32         | 0.03  | 1.29                       | 14.07                   | 29                           | 0        |
| 1985 | 11    | 4                          | 0.04             | 3              | 1.32         | 0.03  | 1.3                        | 14.07                   | 29                           | 0        |
| 1985 | 11    | 5                          | 0.06             | 3.71           | 1.32         | 0.03  | 1.29                       | 14.07                   | 29                           | 0        |
| 1985 | 11    | 6                          | 0.1              | 6.58           | 1.32         | 0.03  | 1.24                       | 14.07                   | 29                           | 0        |
| 1985 | 12    | 1                          | 0.3              | 14.57          | 1.32         | 0.03  | 1.04                       | 14.07                   | 29                           | 0        |
| 1985 | 12    | 2                          | 0.12             | 12.34          | 1.32         | 0.03  | 1.22                       | 14.07                   | 29                           | 0        |
| 1985 | 12    | 3                          | 0.05             | 4.18           | 1.32         | 0.03  | 1.29                       | 14.07                   | 29                           | 0        |
| 1985 | 12    | 4                          | 0.08             | 1.9            | 1.32         | 0.03  | 1.27                       | 14.07                   | 29                           | 0        |
| 1985 | 12    | 5                          | 0.12             | 1.76           | 1.32         | 0.03  | 1.22                       | 14.07                   | 29                           | 0        |
| 1985 | 12    | 6                          | 0.11             | 2.2            | 1.58         | 0.03  | 1.5                        | 14.07                   | 29                           | 0        |
| 1986 | 1     | 1                          | 0.08             | 6.55           | 1.32         | 0.03  | 1.27                       | 14.07                   | 29                           | 0        |
| 1986 | 1     | 2                          | 0.84             | 20.99          | 1.32         | 0.03  | 0.51                       | 14.07                   | 29                           | 0        |
| 1986 | 1     | 3                          | 0.29             | 22.16          | 1.32         | 0.03  | 1.05                       | 14.07                   | 29                           | 0        |
| 1986 | 1     | 4                          | 0.43             | 11.32          | 1.32         | 0.03  | 0.92                       | 14.07                   | 29                           | 0        |
| 1986 | 1     | 5                          | 1.2              | 23.29          | 1.32         | 0.03  | 0.15                       | 14.07                   | 29                           | 0        |
| 1986 | 1     | 6                          | 0.91             | 26.46          | 1.58         | 0.03  | 0.71                       | 14.07                   | 29                           | 0        |
| 1986 | 2     | 1                          | 0.34             | 12.29          | 1.32         | 0.02  | 1                          | 14.07                   | 29                           | 0        |
| 1986 | 2     | 2                          | 0.27             | 7.98           | 1.32         | 0.02  | 1.07                       | 14.07                   | 29                           | 0        |
| 1986 | 2     | 3                          | 0.48             | 10.55          | 1.32         | 0.02  | 0.86                       | 14.07                   | 29                           | 0        |
| 1986 | 2     | 4                          | 0.17             | 9.01           | 1.32         | 0.02  | 1.17                       | 14.07                   | 29                           | 0        |
| 1986 | 2     | 5                          | 0.23             | 7.44           | 1.32         | 0.02  | 1.11                       | 14.07                   | 29                           | 0        |
| 1986 | 2     | 6                          | 0.15             | 3.56           | 0.79         | 0.01  | 0.65                       | 14.07                   | 29                           | 0        |
| 1986 | 3     | 1                          | 0.26             | 5.17           | 1.32         | 0.02  | 1.08                       | 14.07                   | 29                           | 0        |
| 1986 | 3     | 2                          | 0.16             | 4.34           | 1.32         | 0.02  | 1.18                       | 14.07                   | 29                           | 0        |
| 1986 | 3     | 3                          | 0.24             | 3.49           | 1.32         | 0.02  | 1.1                        | 14.07                   | 29                           | 0        |
| 1986 | 3     | 4                          | 0.19             | 2.95           | 1.32         | 0.02  | 1.15                       | 14.07                   | 29                           | 0        |
| 1986 | 3     | 5                          | 0.18             | 12.63          | 1.32         | 0.02  | 1.16                       | 14.07                   | 29                           | 0        |
| 1986 | 3     | 6                          | 0.15             | 27.87          | 1.58         | 0.03  | 1.46                       | 14.07                   | 29                           | 0        |
| 1986 | 4     | 1                          | 0.3              | 10.56          | 1.32         | 0.02  | 1.04                       | 14.07                   | 29                           | 0        |
| 1986 | 4     | 2                          | 0.21             | 10.38          | 1.32         | 0.02  | 1.13                       | 14.07                   | 29                           | 0        |
| 1986 | 4     | 3                          | 0.23             | 8.2            | 1.32         | 0.02  | 1.06                       | 14.07                   | 29                           | 0        |
| 1986 | 4     | 4                          | 0.17             | 7.77           | 1.32         | 0.02  | 1.17                       | 14.07                   | 29                           | 0        |
| 1986 | 4     | 5                          | 0.13             | 4.78           | 1.32         | 0.02  | 1.21                       | 14.07                   | 29                           | 0        |
| 1986 | 4     | 6                          | 0.21             | 3.75           | 1.32         | 0.02  | 1.13                       | 14.07                   | 29                           | 0        |
| 1986 | 5     | 1                          | 0.1              | 5.48           | 1.32         | 0.02  | 1.24                       | 14.07                   | 29                           | 0        |
| 1986 | 5     | 2                          | 0.15             | 4.23           | 1.32         | 0.02  | 1.18                       | 14.07                   | 29                           | 0        |
| 1986 | 5     | 3                          | 0.17             | 4.24           | 1.32         | 0.02  | 1.17                       | 14.07                   | 29                           | 0        |
| 1986 | 5     | 4                          | 0.08             | 4.06           | 1.32         | 0.02  | 1.26                       | 14.07                   | 29                           | 0        |
| 1986 | 5     | 5                          | 0.11             | 2.58           | 1.32         | 0.02  | 1.23                       | 14.07                   | 29                           | 0        |
| 1986 | 5     | 6                          | 0.1              | 2.74           | 1.58         | 0.03  | 1.5                        | 14.07                   | 29                           | 0        |
| 1986 | 6     | 1                          | 0.06             | 2.56           | 1.32         | 0.02  | 1.28                       | 14.07                   | 29                           | 0        |
| 1986 | 6     | 2                          | 0.11             | 2.39           | 1.32         | 0.02  | 1.23                       | 14.07                   | 29                           | 0        |
| 1986 | 6     | 3                          | 0.22             | 2.19           | 1.32         | 0.02  | 1.12                       | 14.07                   | 29                           | 0        |
| 1986 | 6     | 4                          | 0.09             | 2.23           | 1.32         | 0.02  | 1.25                       | 14.07                   | 29                           | 0        |
| 1986 | 6     | 5                          | 0.05             | 2.56           | 1.32         | 0.02  | 1.28                       | 14.07                   | 29                           | 0        |
| 1986 | 6     | 6                          | 0.06             | 1.58           | 1.32         | 0.02  | 1.28                       | 14.07                   | 29                           | 0        |
| 1986 | 7     | 1                          | 0.1              | 1.21           | 1.32         | 0.02  | 1.21                       | 14.04                   | 28.98                        | 0        |
| 1986 | 7     | 2                          | 0.09             | 1.38           | 1.32         | 0.02  | 1.28                       | 14.07                   | 29                           | 0        |
| 1986 | 7     | 3                          | 0.3              | 2.01           | 1.32         | 0.02  | 1.04                       | 14.07                   | 29                           | 0        |
| 1986 | 7     | 4                          | 0.15             | 1.39           | 1.32         | 0.02  | 1.19                       | 14.07                   | 29                           | 0        |
| 1986 | 7     | 5                          | 0.08             | 1.08           | 1.32         | 0.02  | 1.08                       | 13.89                   | 28.89                        | 0        |
| 1986 | 7     | 6                          | 0.14             | 2.56           | 1.58         | 0.03  | 1.58                       | 14.01                   | 28.96                        | 0        |
| 1986 | 8     | 1                          | 0.05             | 2.62           | 1.32         | 0.03  | 1.32                       | 14.03                   | 28.97                        | 0        |
| 1986 | 8     | 2                          | 0.05             | 3.14           | 1.32         | 0.03  | 1.32                       | 14.05                   | 28.99                        | 0        |
| 1986 | 8     | 3                          | 0.15             | 3.71           | 1.32         | 0.03  | 1.21                       | 14.07                   | 29                           | 0        |
| 1986 | 8     | 4                          | 0.07             | 2.44           | 1.32         | 0.03  | 1.28                       | 14.07                   | 29                           | 0        |
| 1986 | 8     | 5                          | 0.05             | 1.25           | 1.32         | 0.03  | 1.25                       | 14.02                   | 28.97                        | 0        |
| 1986 | 8     | 6                          | 0.08             | 1.2            | 1.58         | 0.03  | 1.2                        | 13.68                   | 28.76                        | 0        |

(Unit: 10 m<sup>3</sup>)