

Fig. 4.2
ISOSEISMAL MAP OF
THE 16 JULY 1990 EARTHQUAKES

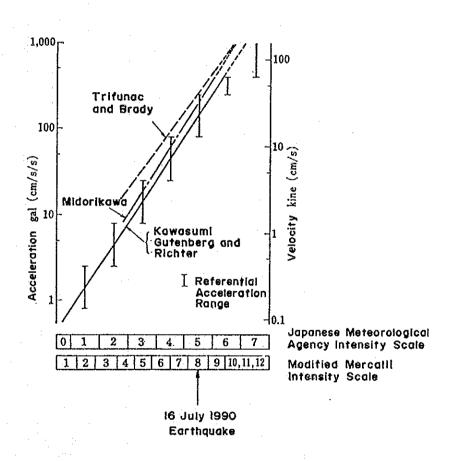
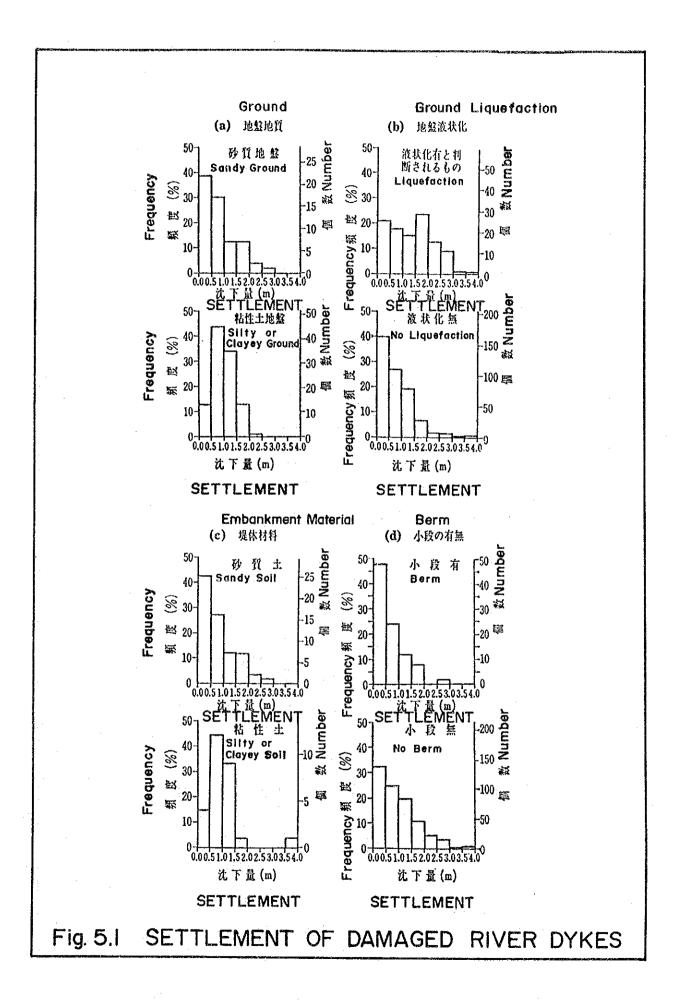


Fig. 4.3 RELATION BETWEEN SEISMIC INTENSITY AND ACCELERATION

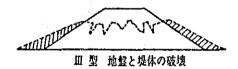




TYPE I Slope Surface Failure



TYPE II Slope Failure



TYPE III Ground and Embankment Failure



Fig. 5.2 DAMAGED SHAPES OF RIVER DYKES

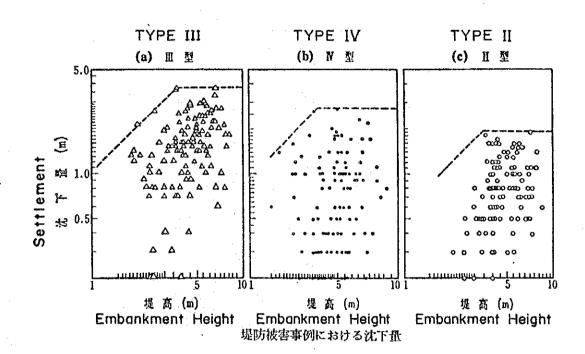
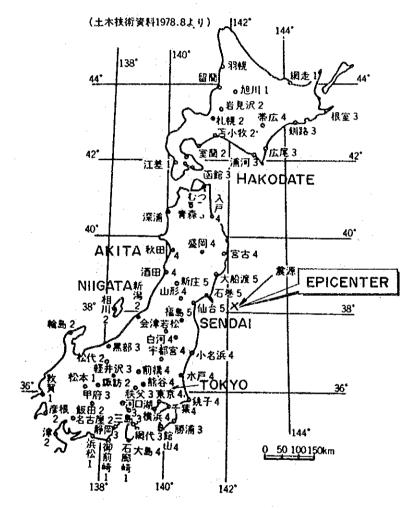
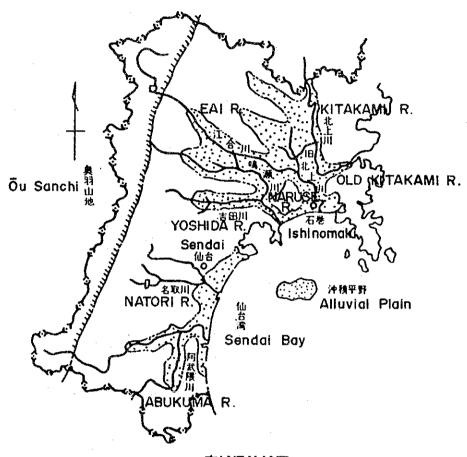


Fig. 5.3 SETTLEMENT OF DAMAGED RIVER DYKES



震源地と各地の震度

Fig. 5.4 LOCATION OF EPICENTER AND INTENSITY



宫城県流域図

県内一級河川

河川名	北上川	旧北上川	江合川	鳴瀬川	吉田川	名取川	阿武隈川	合 計
延長(km)	57.4	35. 0	35. 7	45. 5	36. 9	18. 9	54.6	284.0

Fig. 5.5 SEVEN RIVERS IN MIYAGI - KEN

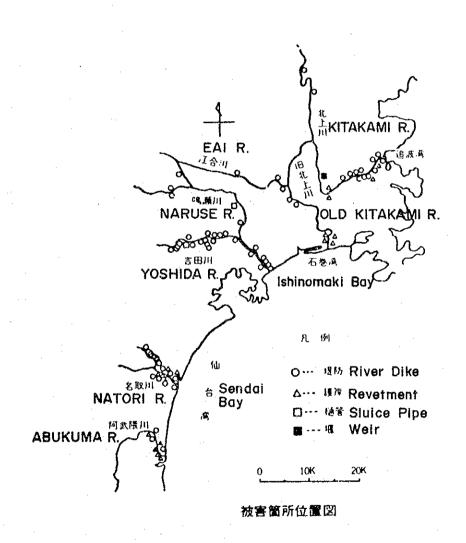


Fig. 5.6 LOCATION OF DAMAGED PLACE

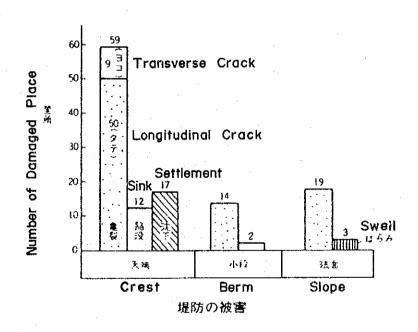


Fig. 5.7 DAMAGE OF RIVER DYKE

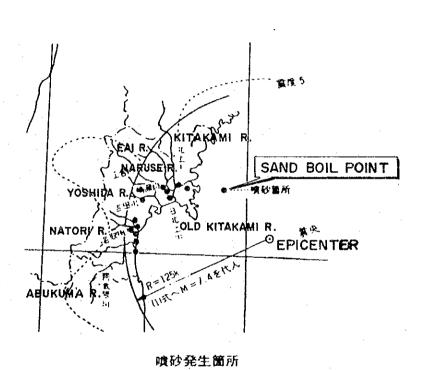
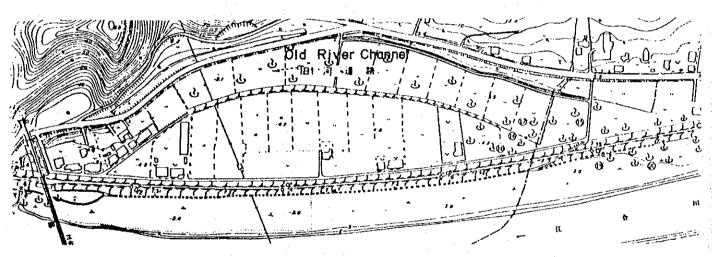


Fig. 5.8 SAND BOIL POINT



江会川右岸 (旧北上川合流点~1.0K) 旧河道跡にみられる噴砂箇所 - む……噴砂箇所 - Sand Boil

Fig.5.9 SAND BOIL IN OLD RIVER CHANNEL AT RIGHT BANK OF EAI RIVER

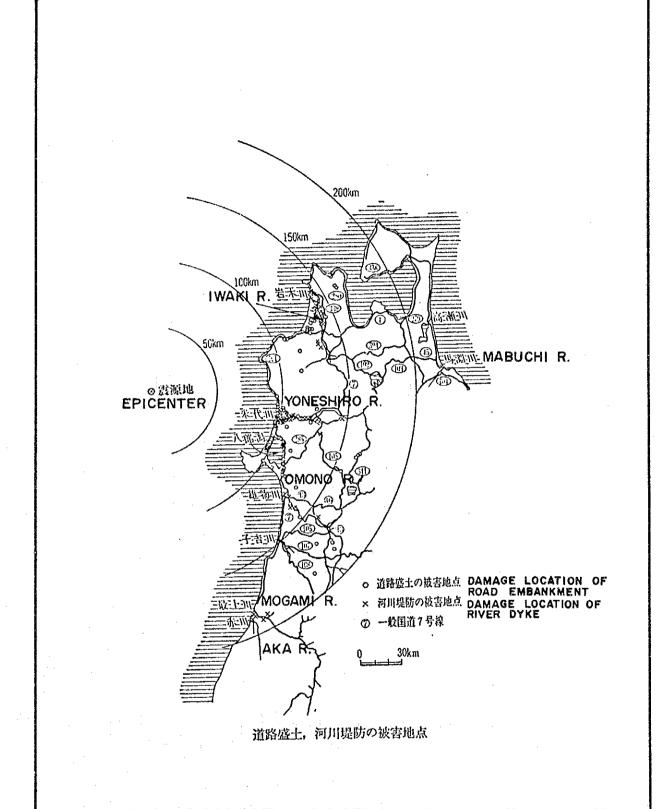


Fig. 5.10 DAMAGE LOCATION OF RIVER DYKE

- (I) NIIGATA E. (SHINANO RIVER)
- (2) NIIGATA E. (AGANO RIVER)
- (3) MIYAGI KENOKI E.
- (4) NIHONKAI CHÜBU E.

M = Magnitude

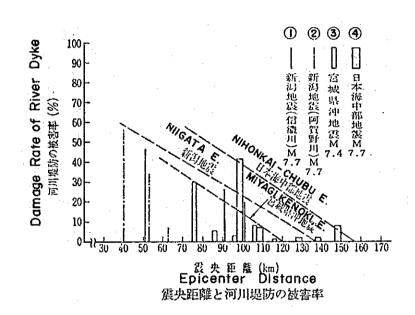


Fig. 5.11 RELATION BETWEEN EPICENTER DISTANCE AND DAMAGE RATIO OF RIVER DYKE

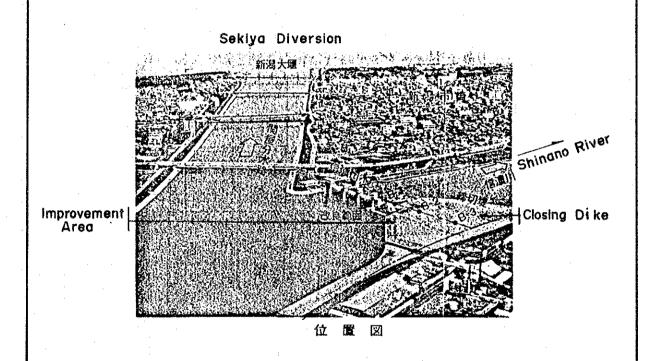
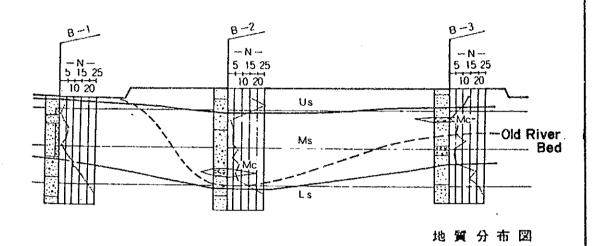
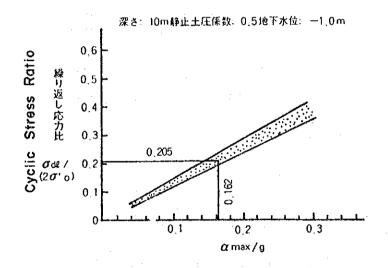


Fig. 5.12 LOCATION MAP



DEPOSIT CLASSIFICATIO	y SOIL	SIGN	N VALUE	REMARKS
Upper Layer	Sandy Soll (Fine Sand)	Us	More than	About Im. of upper part is yellowish grey, a litte compacted.
Middle	Sandy Soll (Fine to Coarse Sand)	Ms	1~10	Much water content, loose, organic materials mixed, small gravels ($\emptyset = 2-3$ mm).
Layer	Clayey Soil (Clay~Sandy Siit)	Mc	1~6	Contain soft and many organic materials irregular layer thickness of Lom.~several cm
Lower Sandy Soll Layer (Medium Sand)		Ls	10	Equal Particle size on the whole, little content of clay and silt.

Fig. 5.13 GEOLOGICAL CROSS SECTION



最大加速度と20回に換算した 一様繰り返し応力比との関係

Fig. 5.14 RELATION BETWEEN MAXIMUM
ACCELERATION AND UNIFORM CYCLIC
STRESS RATIO CONVERTED BY
20 CYCLES

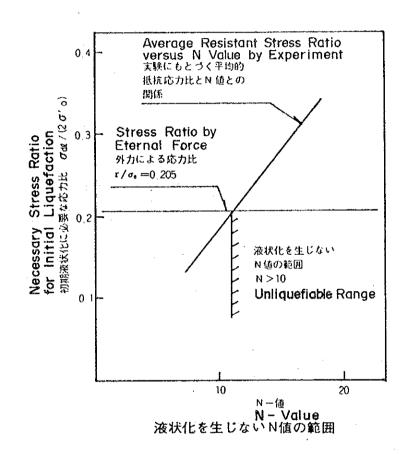


Fig. 5.15 UNLIQUEFIABLE RANGE OF N VALUE

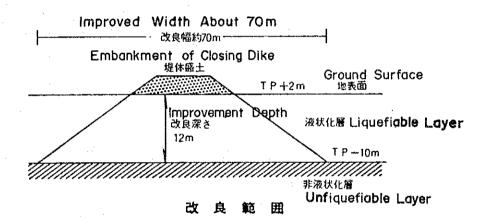


Fig. 5.16 IMPROVEMENT RANGE

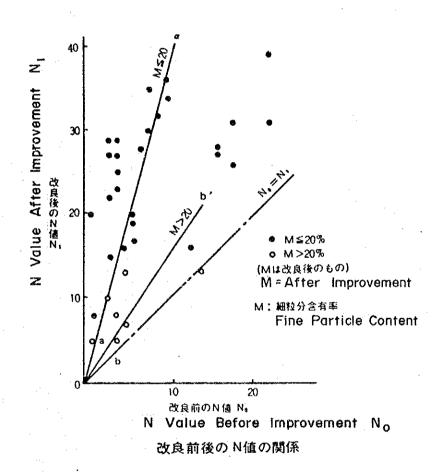


Fig. 5.17 RELATION BETWEEN N VALUE BEFORE AND AFTER IMPROVEMENT

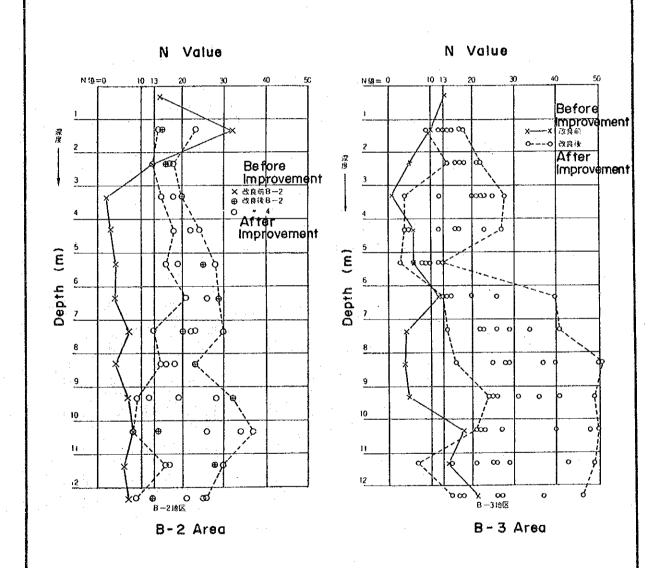
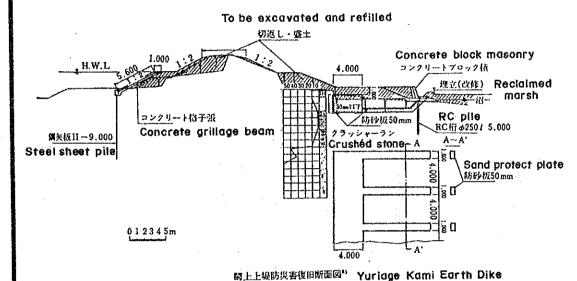


Fig. 5.18 N VALUE BEFORE AND AFTER IMPROVED BY SAND COMPACTION PILE



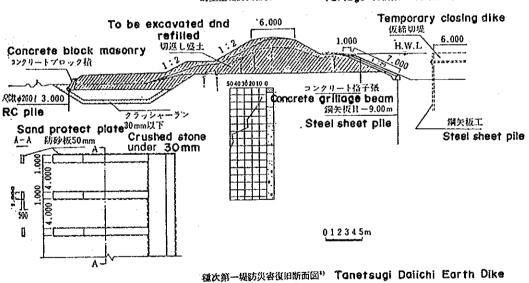


Fig. 5.19 REHABILITATED SECTION OF EARTH DIKES

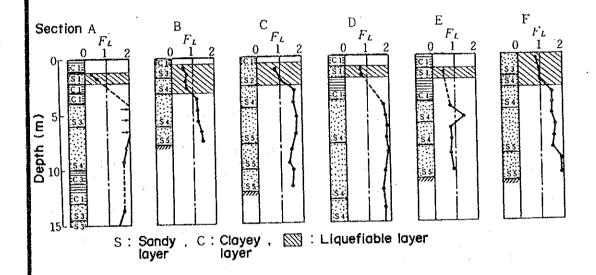


Fig. 5.20 LIQUEFACTION ANALYSIS ON HORIZONTAL GROUND

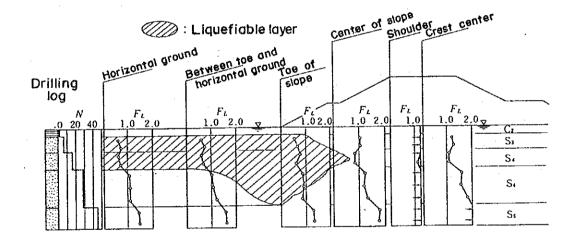
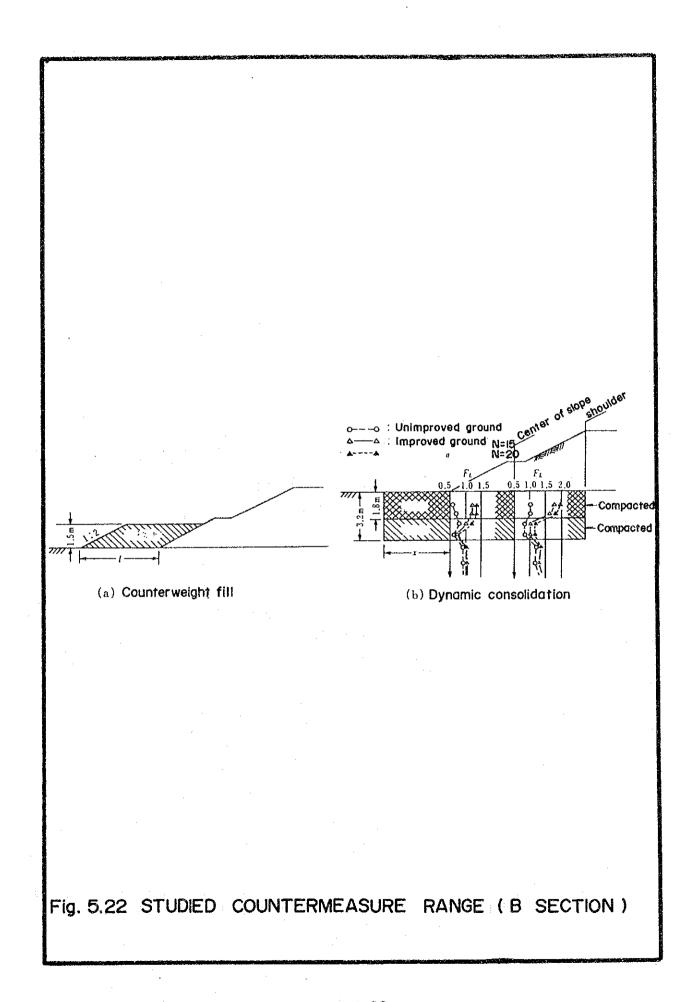
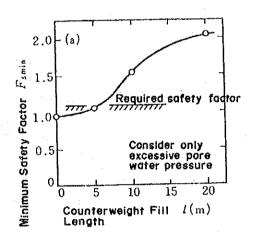


Fig. 5.21 LIQUEFACTION ANALYSIS IN TWO DIMENSIONAL SECTION (B SECTION)





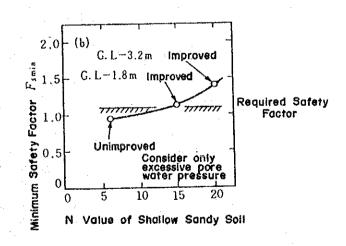
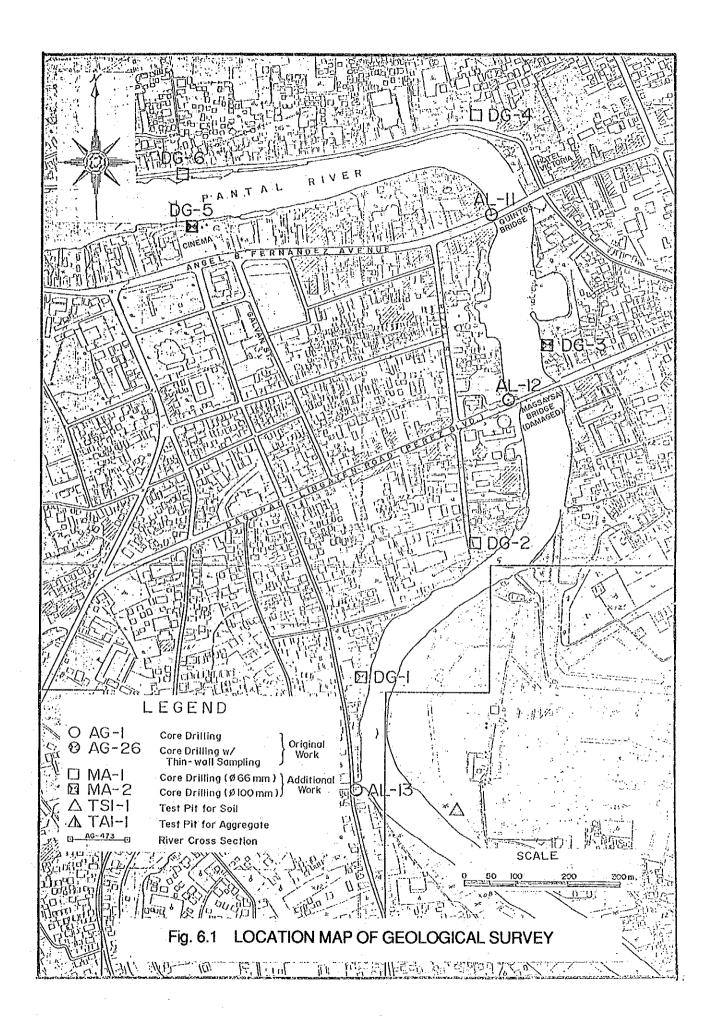
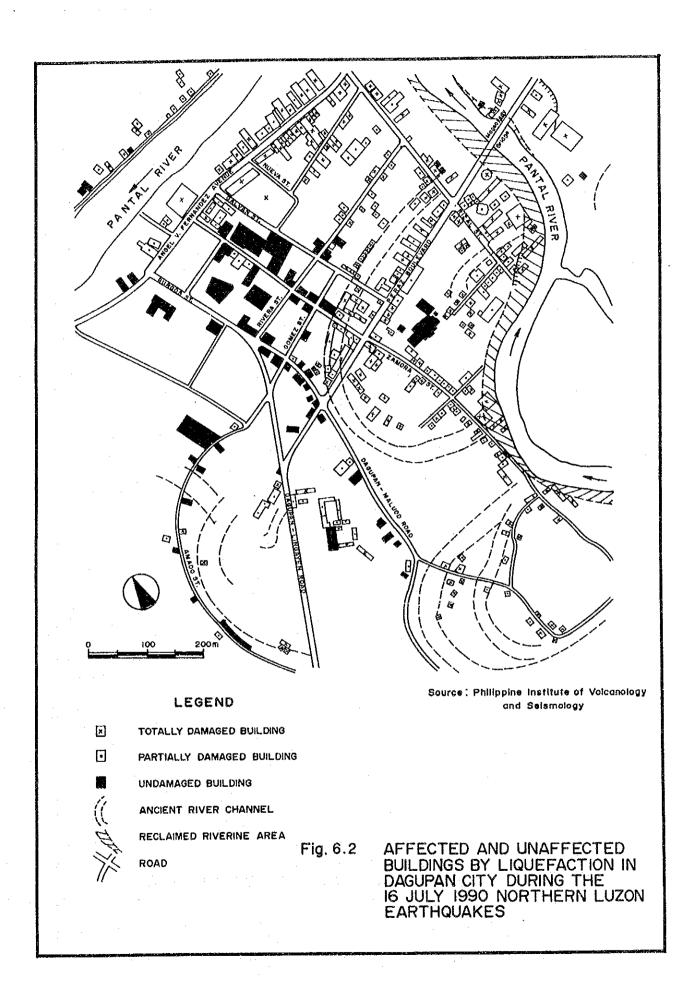
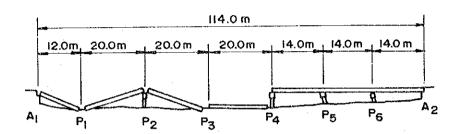


Fig. 5.23 EFFECTIVENESS OF COUNTERMEASURE (B SECTION)







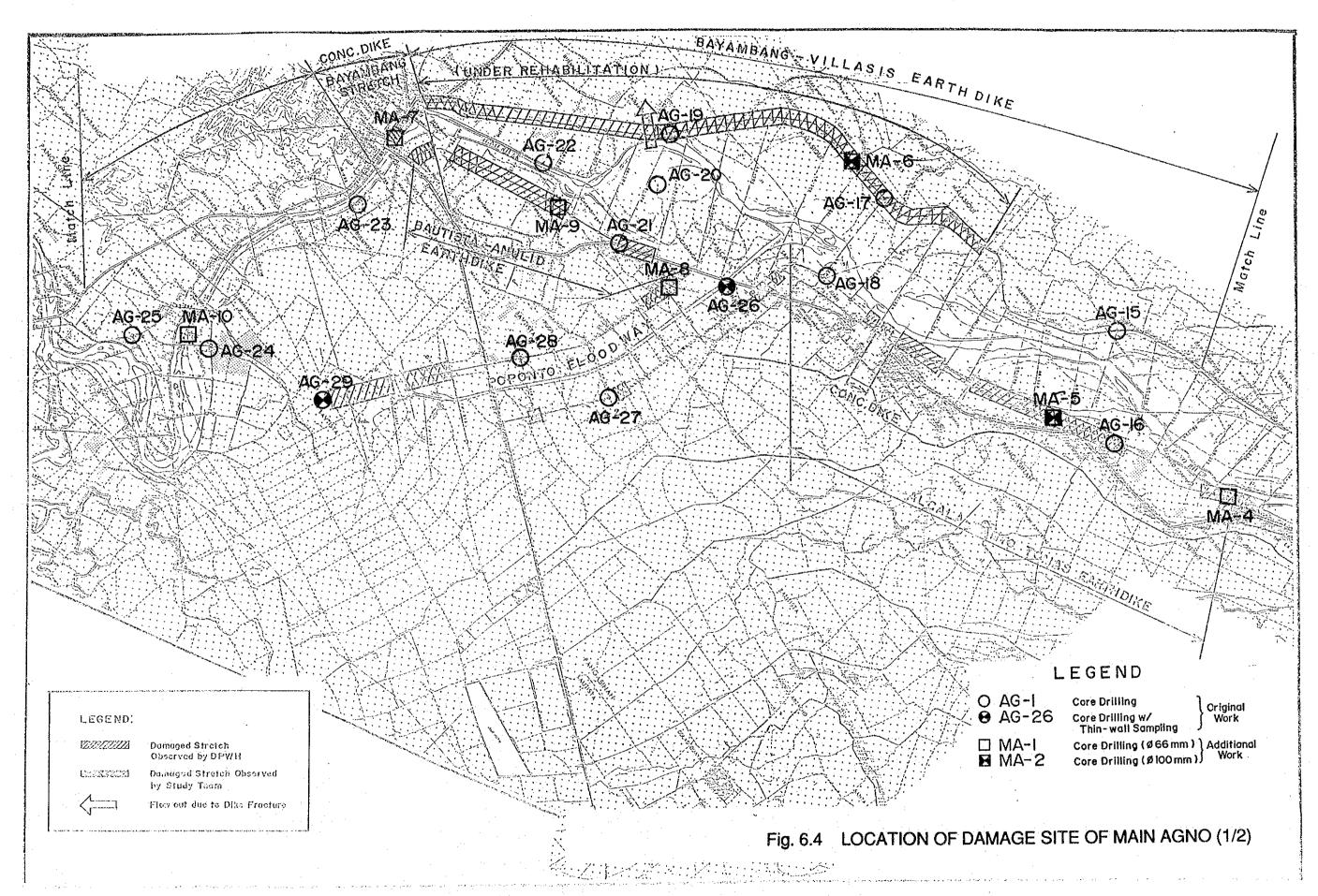
SImple Steel I Beam
B RCDG Combination

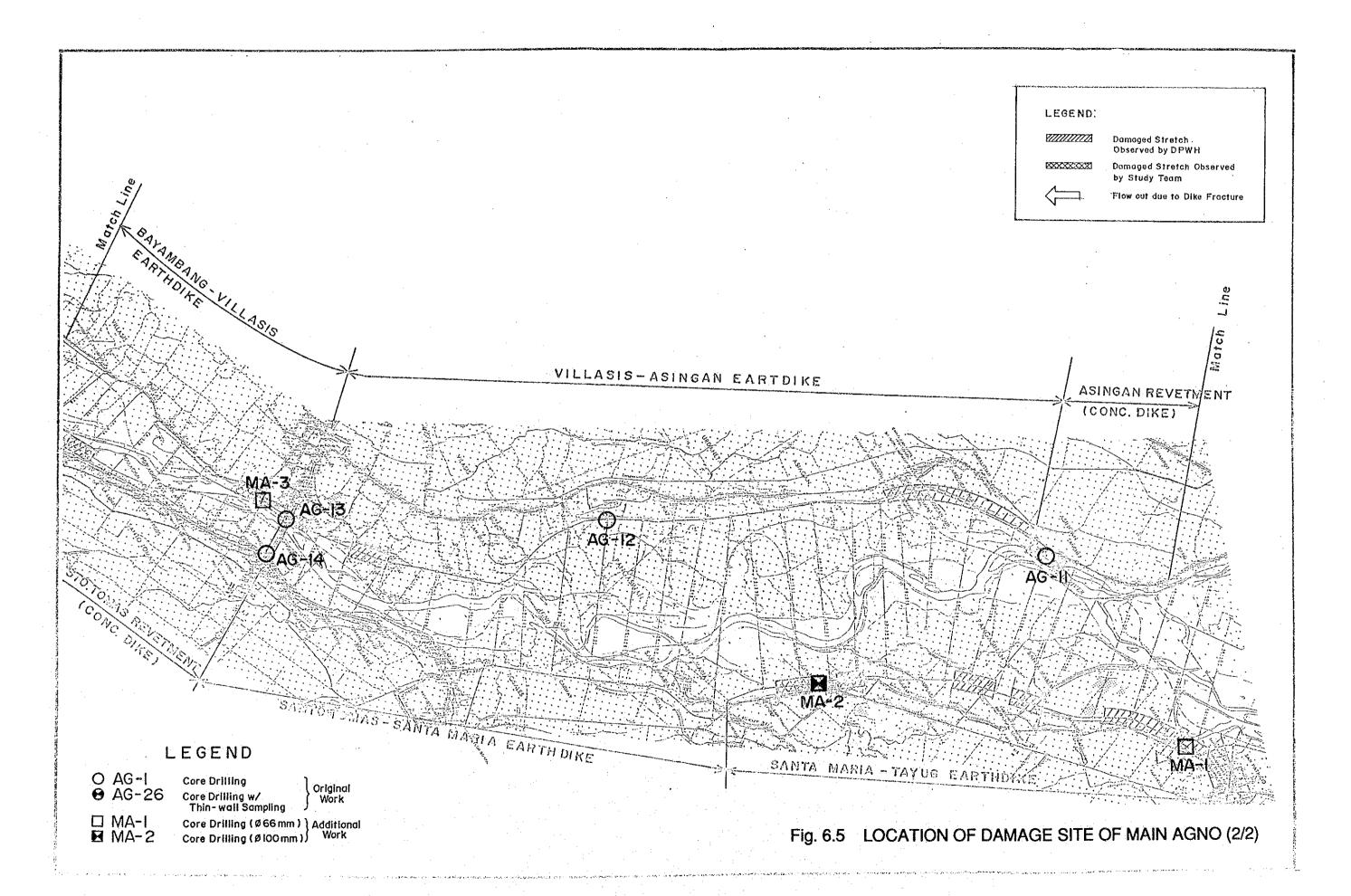
Simple RCDG

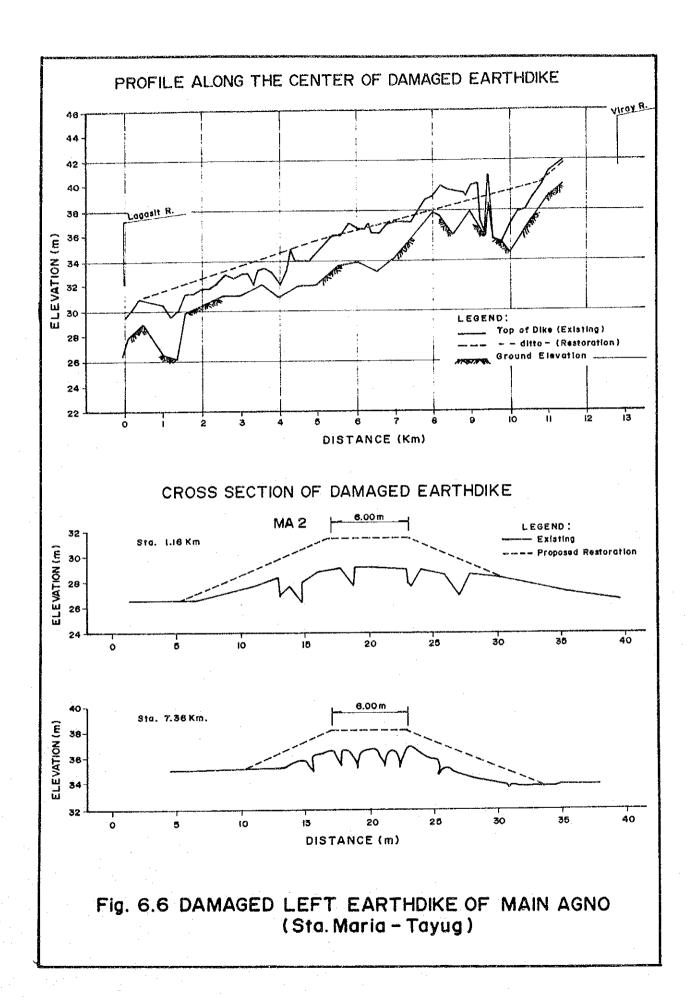
A₁ & A₂ : Pile Bent Type

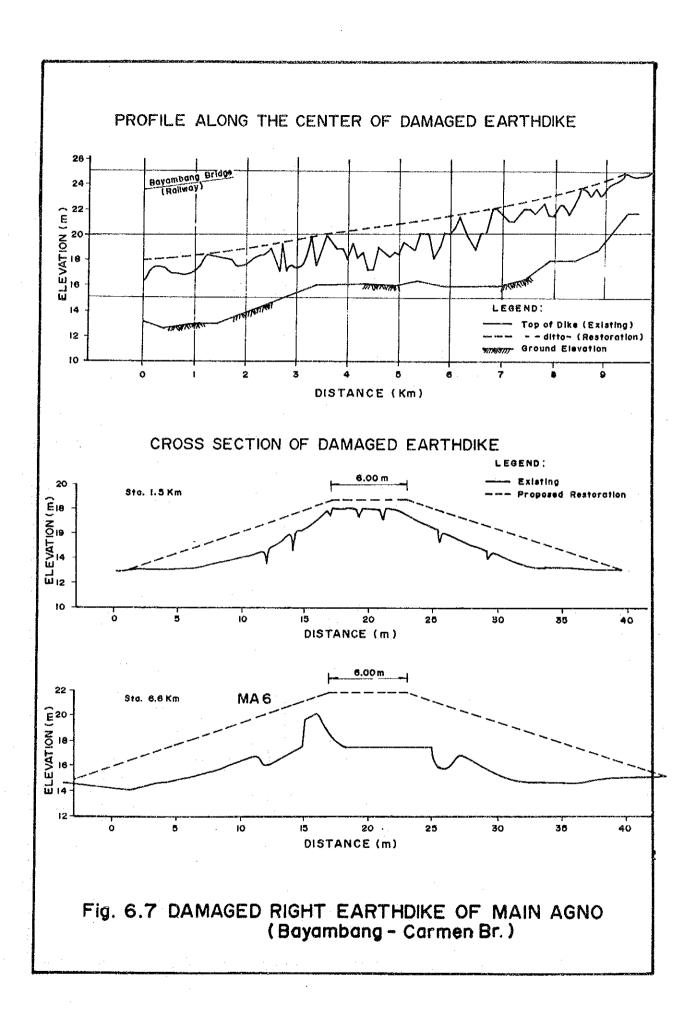
PI~P. : Wall Type

Fig. 6.3 SKETCH OF DAMAGED MAGSAYSAY BRIDGE









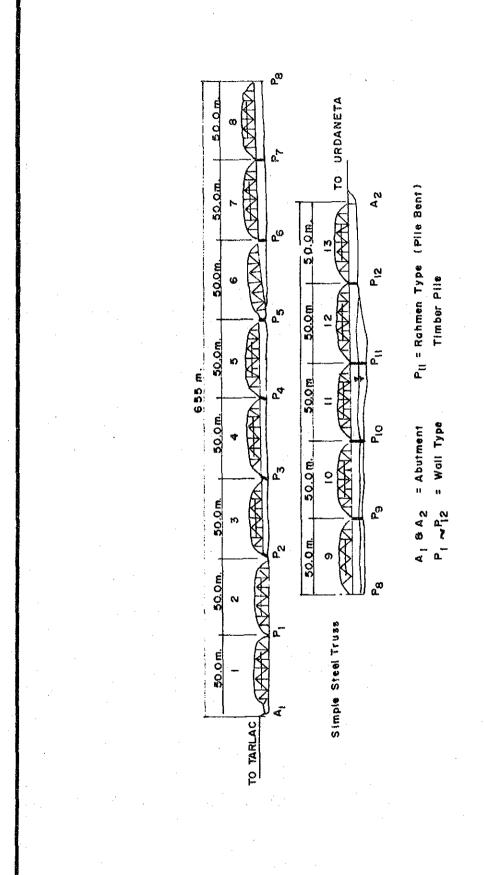
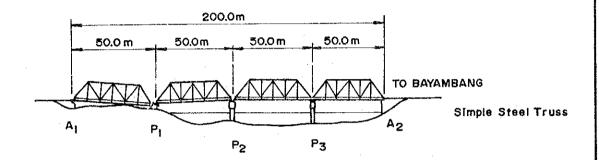


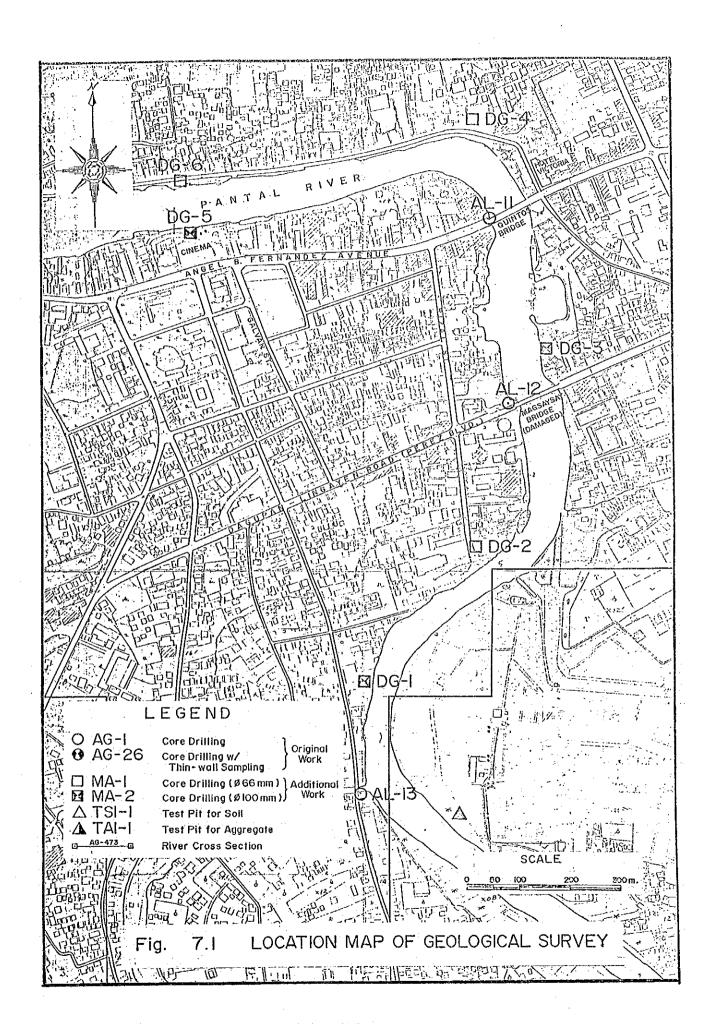
FIG. 6.8 SKETCH OF DAMAGED SISON BRIDGE

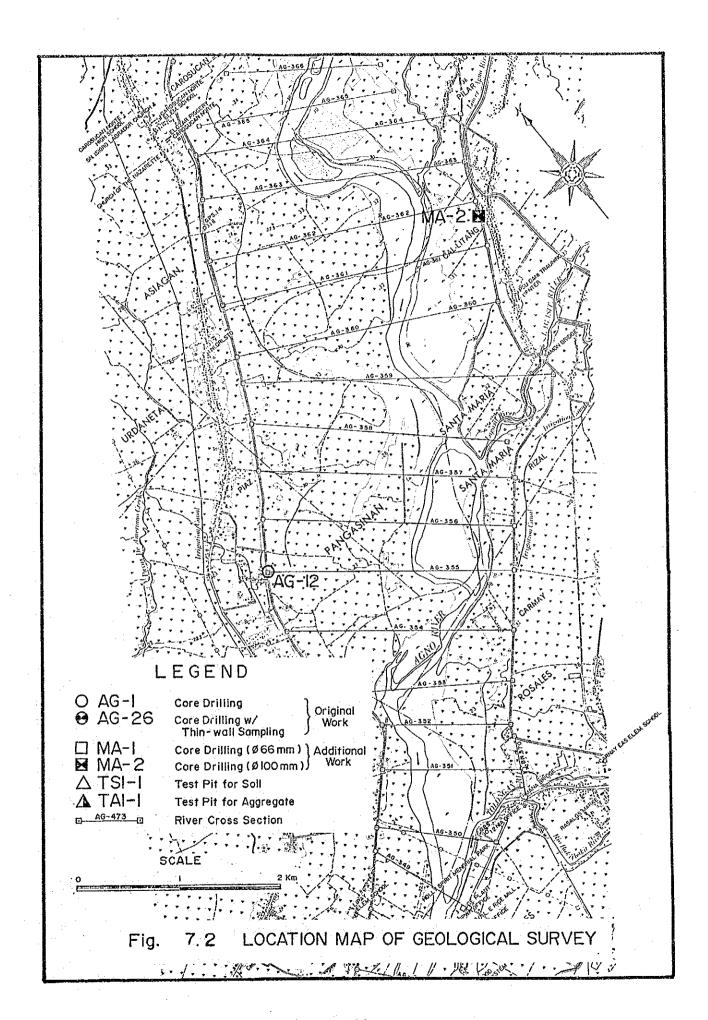


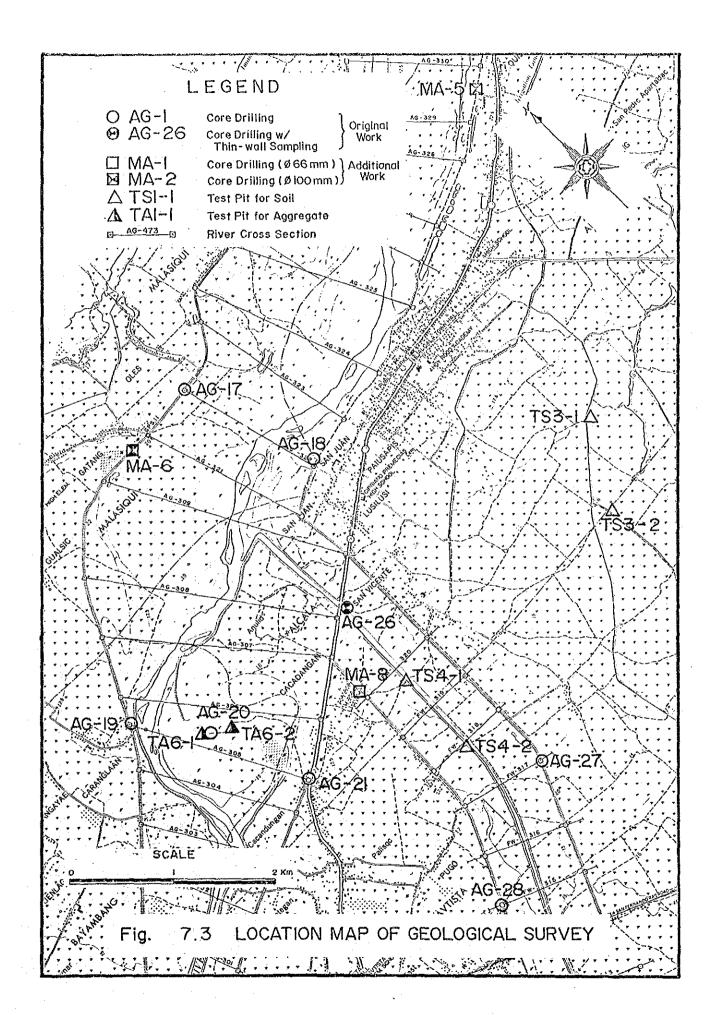
A₁ 8 A₂ : Pile Bent Type

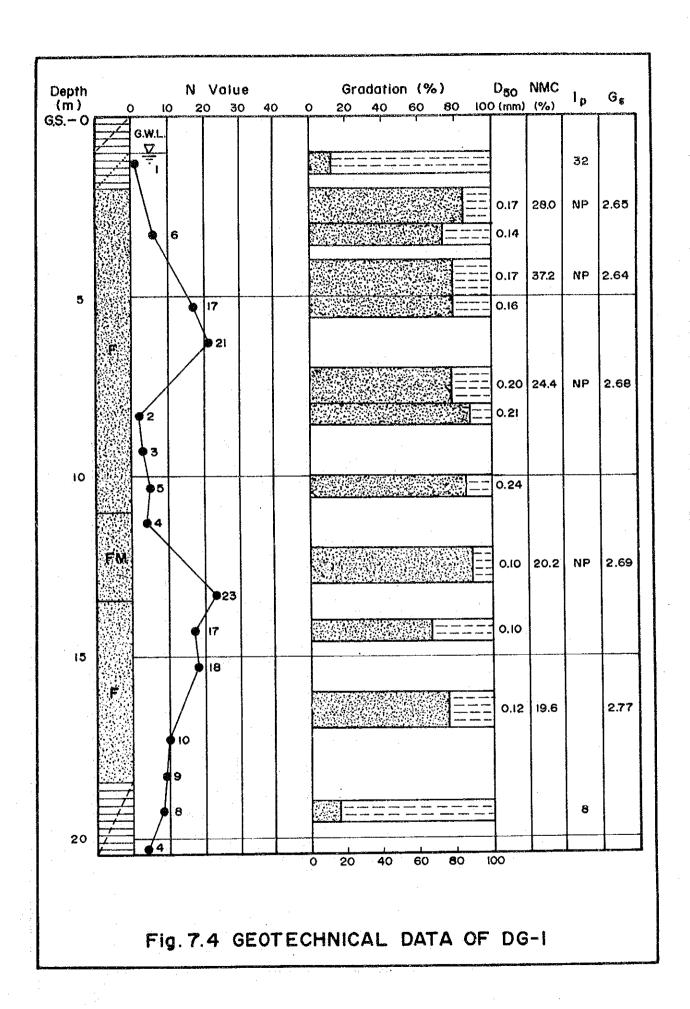
P₁ : Pile Bent
P₂ : Multi Span
P₃ : Wall Type

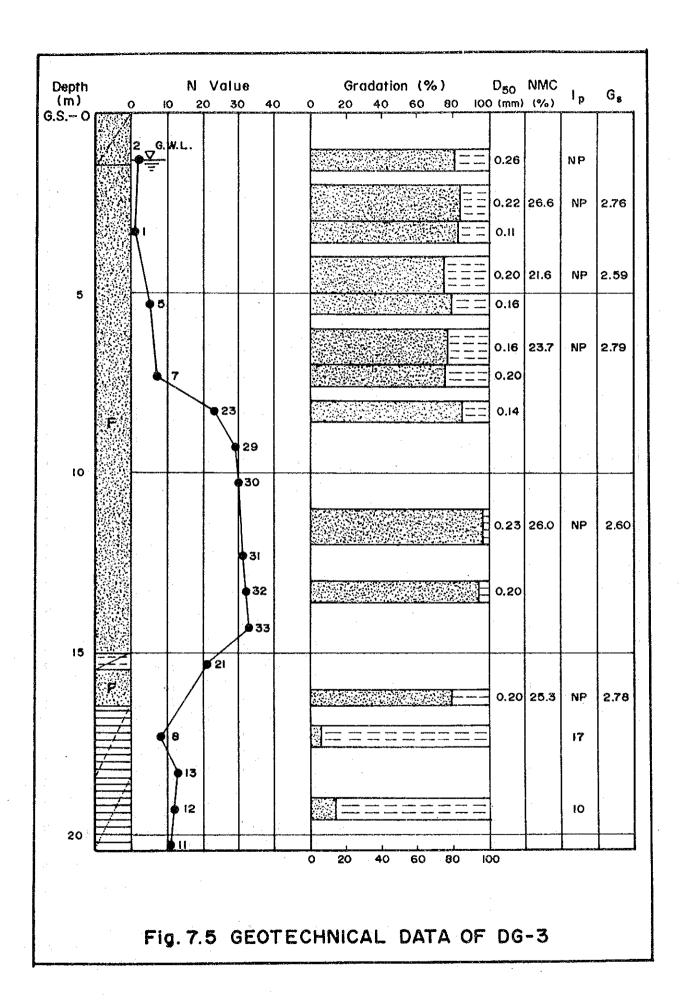
Fig. 6.9 SKETCH OF DAMAGED CALVO BRIDGE

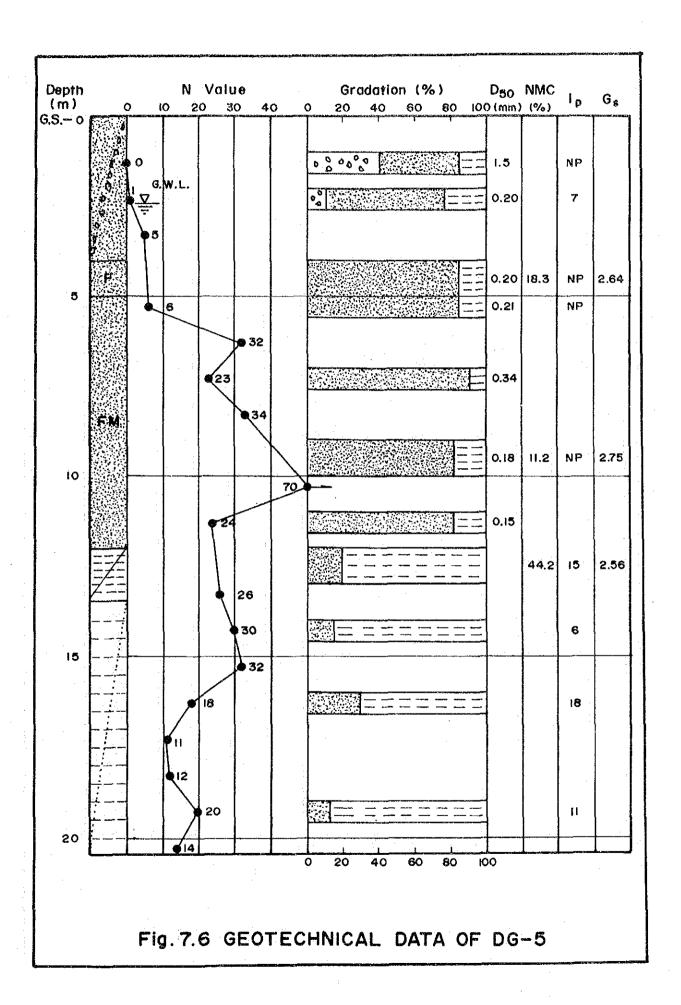


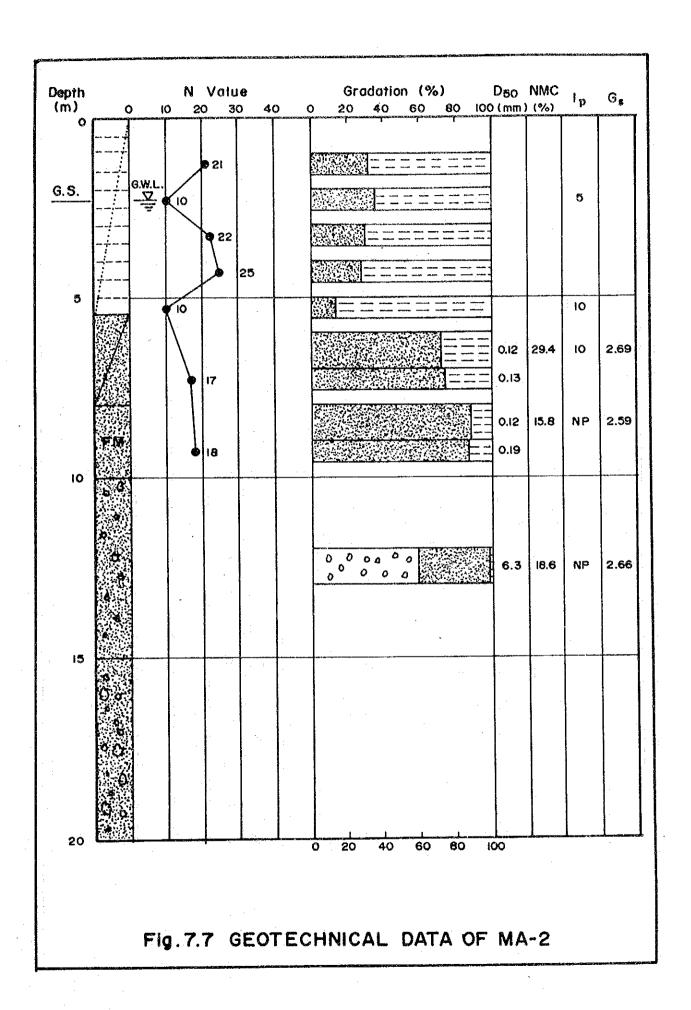


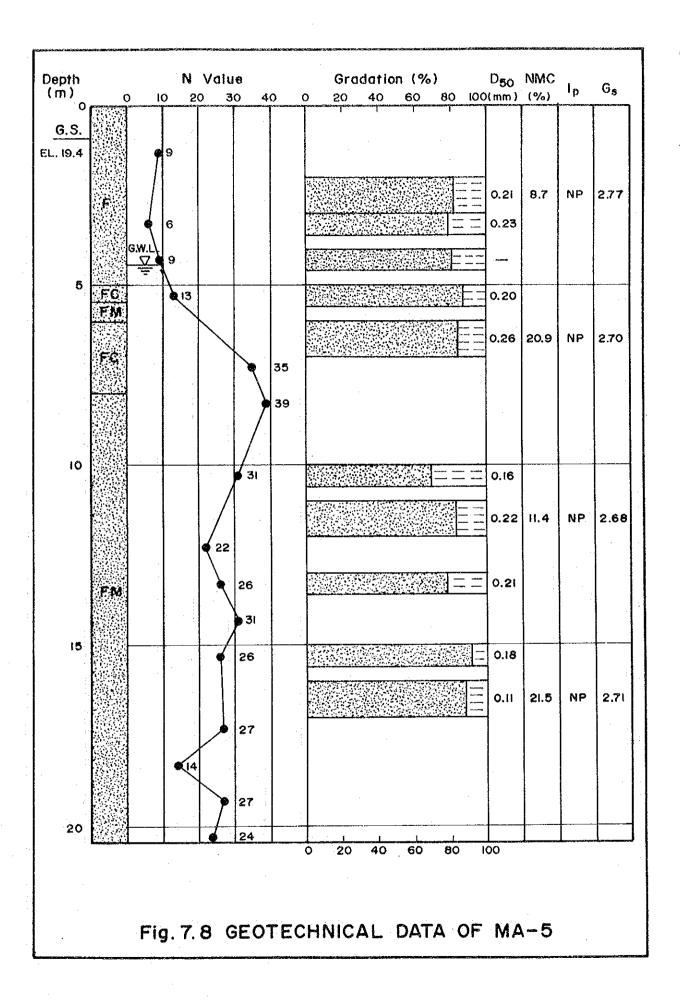


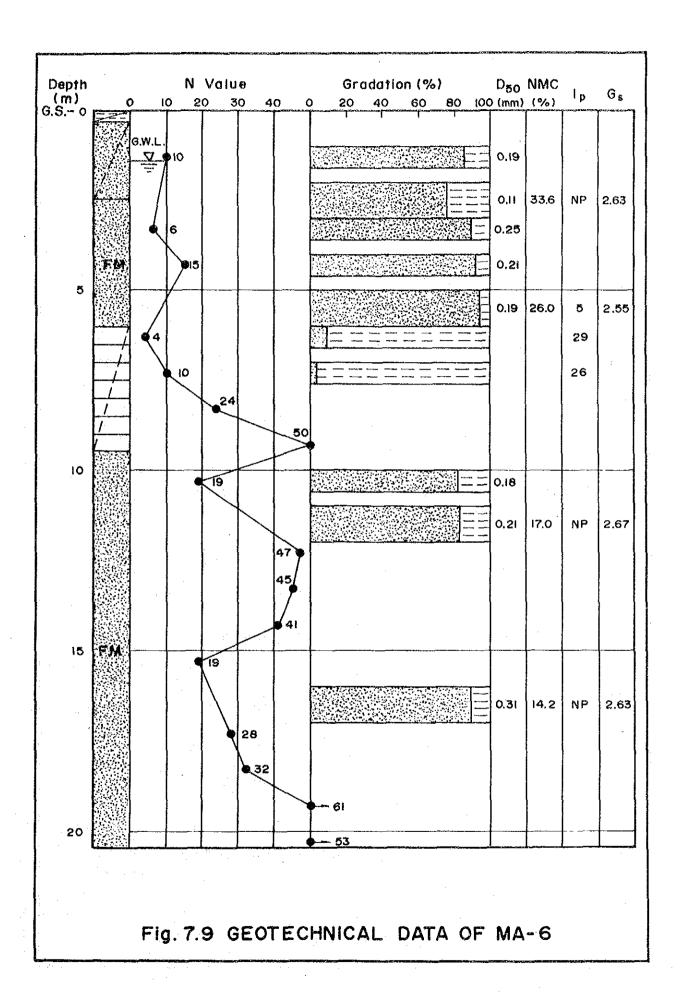












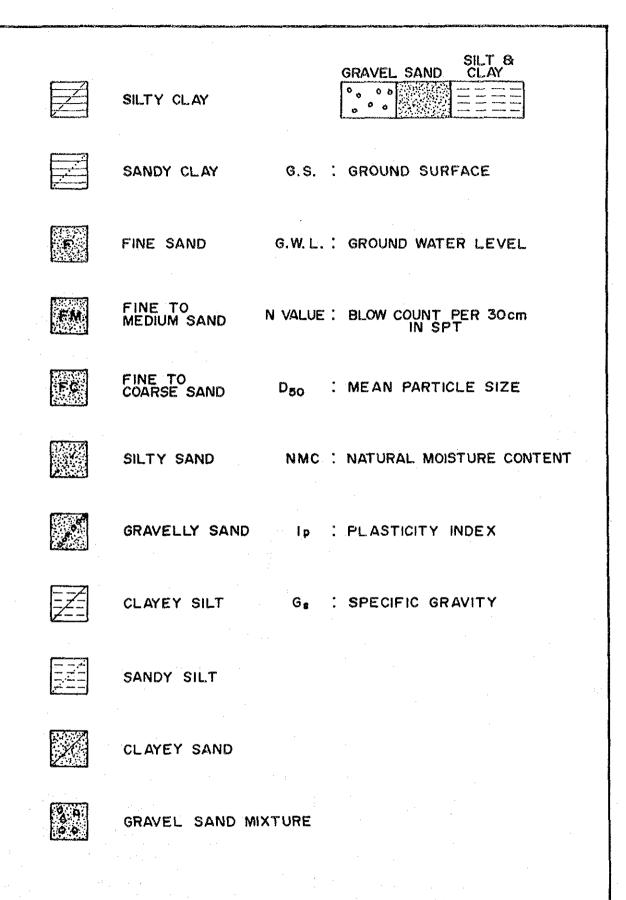
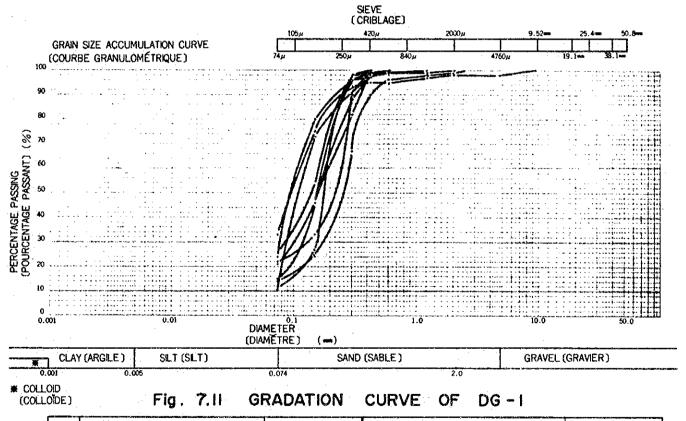


Fig. 7.10 LEGEND

· (A	FOR REPORTING (POUR LE RAPPORT)						
NAME OF SURVEY & LOCALITY (DÉNOMINATION DE L'ENQUÊTE ET LOCALITÉ)	Agno Flood		g og farsker ekke sereni og krisensek	walka ku mana (zha shan)	DATE (DATE)		aterialistic Collisions become, payor direct, est property and property also should be
SAMPLE NO. & DEPTH (N° DE L'ÉCHANTILLON ET PROFONDEUR)	DG - I	(m ~	m)	TESTED BY (ESSAI PAR)		*

> SPECIFIC GRAVITY (POIDS SPÉCIFIQUE) Gs

/E AGE	GRAIN SIZE (∞) (GRANUROMÉTRIE)	50.8	38.1	25.4	19.1	9.52	4.76	2.00	0.84	0.42	0.25	0.105	0.074
SIEVE	TOTAL PASSING(%) (TOTAL PASSANT)							-					
METER (ÉTRE)	GRAIN SIZE() (GRANULOMÉTRIE)									-			
[Q 🕉	TOTAL PASSING(%) (TOTAL PASSANT)												



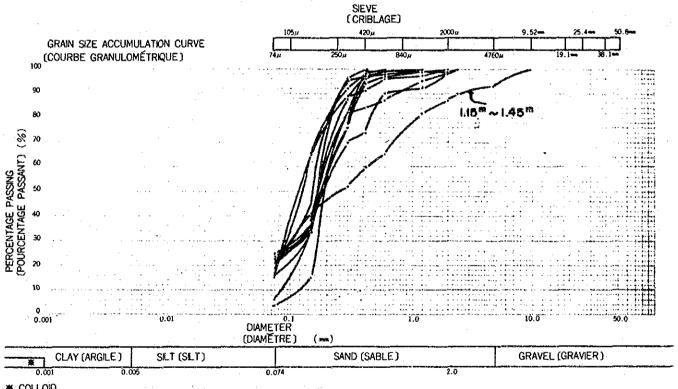
	4.76mm<	%	MAXMUM DIAMETER (DIAMETRE MAXIMUM)	ma
22	4.76~2.00****	%	60% DIAMETER (DIAMÉTRE60%)	mm
PATRO PATRO	2.00~0.42mm	%	30% DIAMETER (DIAMETRE 30%)	(AME.
8 8 8 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	0.42~0.074mm	%	10% DIAMETER (DIAMETRE 10%)	men.
1. 6	0.074~0.005	%	COEFFICIENT OF UNIFORMITY (COEFFICIENT D'UNIFORMITÉ)	
	0,005***>	%	COEFFICIENT OF CURVATURE (COEFFICIENT DE COURBURE)	

GRADATION ANALYSIS FOR REPORTING (ANALYSE GRANULOMÉTRIQUE) (POUR LE RAPPORT) DATE NAME OF SURVEY & LOCALITY Agno Flood Control (DÉNOMINATION DE L'ENQUÊTE ET LOCALITÉ) (DATE) TESTED BY SAMPLE NO. & DEPTH DG ~ 3 (ESSAI PAR)

PARTICLE SIZE & WEIGHT PERCENTAGE OF PARTICLES UNDER THE SIZE (DIMENSION DES PARTICULES ET POURCENTAGE DE POIDS DES PARTICULES DE DIMENSION INFÉRIEURE AUX PRÉCÉDENTES)

SPECIFIC GRAVITY (POIDS SPÉCIFIQUE) Gs

- ևս է	GRAIN SIZE (***) (GRANUROMÉTRIE)	50.8	38.1	25.4	19.1	9.52	4.76	2.00	0.84	0.42	0.25	0.105	0.074
SEV	TOTAL PASSING(%) (TOTAL PASSANT)												
ÆTER	GRAIN SIZE(==) (GRANULOMÉTRIE)												
HYDRO	TOTAL PASSING(%) (TOTAL PASSANT)							-					



₩ COLLOID (COLLO DE)

(N° DE L ÉCHANTILLON ET PROFONDEUR)

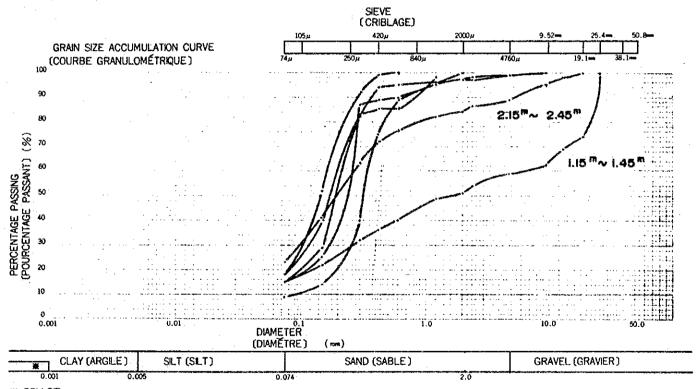
Fig. 7.12 GRADATION CURVE OF DG - 3

	4.76mm<	%	MAXMUM DIAMETER (DIAMETRE MAXIMUM)	****
و ندا	4.76~2.00mm	%	60% DIAMETER (DIAMETRE60%)	язиз
NOT R	2.00~0.42****	%	30% DIAMETER (DIAMETRE 30%)	995
PROPO	0.42~0.074mm	%	10% DIAMETER (DIAMETRE 10%)	pin.
1 4	0.074~0.005****	%	COEFFICIENT OF UNIFORMITY (COEFFICIENT D'UNIFORMITÉ)	
	0.005mm>	%	COEFFICIENT OF CURVATURE (COEFFICIENT DE COURBURE)	

Citizes a demonstrativos de compromise describenções que de formación de participações de maior de compromise de monte de compromise de compro	GRADATION A		The American Contract		nazmandez e jelez de jez e ferefer et pr emja mbandja f kr	SMX (MPA)	FOR REPORTING (POUR LE RAPPORT)
(A	NALYSE GRANUL	UME I RIQU	ル丿				COOK EL TOUT ONLY
NAME OF SURVEY & LOCALITY (DÉNOMINATION DE L'ENQUÊTE ET LOCALITÉ)	Agno Flood	Control			DATE (DATE)		
SAMPLE NO. & DEPTH (N° DE L'ÉCHANTILLON ET PROFONDEUR)	DG - 5	(m ~	m)	TESTED BY (ESSAI PAR)		

> SPECIFIC GRAVITY (POIDS SPÉCIFIQUE) Gs

F (ge)	GRAIN SIZE (==) (GRANUROMÉTRIE)	50.8	38.1	25.4	19.1	9.52	4.76	2.00	0.84	0.42	0.25	0.105	0.074
SIEVE (CRIBLAGE	TOTAL PASSING(%) (TOTAL PASSANT)												
DROMETER ARÉOMÉTRIE)	GRAIN SIZE(==) (GRANULOMÉTRIE)				:								
HYDRON (ARÉON	TOTAL PASSING(%) (TOTAL PASSANT)				:								



★ COLLOÏDE)

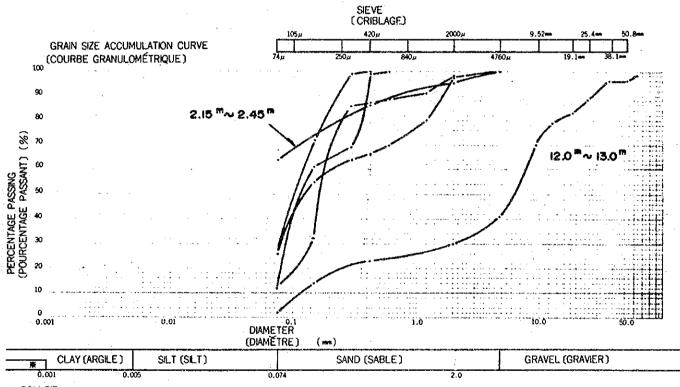
Fig. 7.13 GRADATION CURVE OF DG-5

	4.76mm<	%	MAXMUM DIAMETER (DIAMETRE MAXIMUM)	ग्रह्माः
z	4.76~2.00****	%	60% DIAMETER (DIAMÉTRE60%)	Mera
PROPORTION PROPORTION	2.00~0.42mm	%	30% DIAMETER (DIAMETRE 30%)	. <i>m</i> m
PROP(0.42~0.074mm	%	10% DIAMETER (DIAMETRE 10%)	प्राके
1	0.074~0.005mm	%	COEFFICIENT OF UNIFORMITY (COEFFICIENT D'UNIFORMITÉ)	
	0.005mm>	%	COEFFICIENT OF CURVATURE (COEFFICIENT DE COURBURE)	

(A)	GRADATION A NALYSE GRANUL	NALYSIS OMÉTRIQU	JE)			FOR REPORTING (POUR LE RAPPORT)
NAME OF SURVEY & LOCALITY (DÉNOMINATION DE L'ENQUÊTE ET LOCALITÉ)	Agno Flood	Control	ii-telepolulus Visanii j yyyy gyyyy gydyiyyyy cundy		DATE (DATE)	in a market embered a programme never a transfer de la reserva
SAMPLE NO. & DEPTH (N'DE L'ÉCHANTILLON ET PROFONDEUR)	MA - 2	(m ~	m)	TESTED BY (ESSAL PAR)	

> SPECIFIC GRAVITY (POIDS SPÉCIFIQUE) Gs

in S	GRAIN SIZE (==) (GRANUROMÉTRIE)	50.8	38.1	25.4	19.1	9.52	4.76	2.00	0.84	0.42	0.25	0.105	0.074
SIEVE	TOTAL PASSING(%) (TOTAL PASSANT)												
METER (ÉTRE)	GRAIN SIZE() (GRANULOMÉTRIE)												
	TOTAL PASSING(%) (TOTAL PASSANT)												



(COLLOIDE)

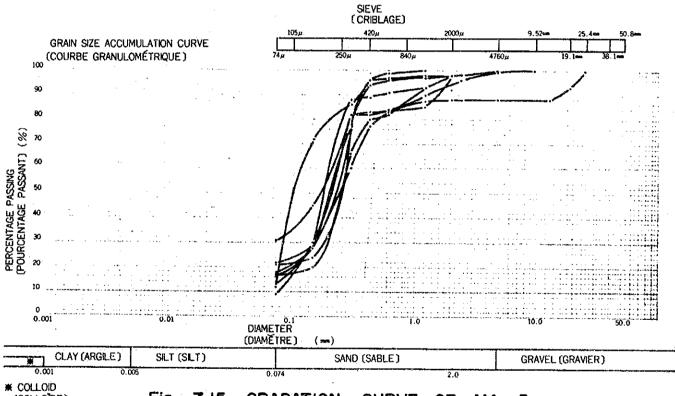
Fig. 7.14 GRADATION CURVE OF MA - 2

·	4.76mm<	%	MAXMUM DIAMETER (DIAMETRE MAXIMUM)	mm
z 2	4.76~2.00mm	%	60% DIAMETER (DIAMETRE60%)	ma
NATION NATION	2.00~0.42***	%	30% DIAMETER (DIAMETRE 30%)	, swin
PROP PROP	0.42~0.074555	%	10% DIAMETER (DIAMÉTRE 10%)	m-a.
a a	0.074~0.005㎜	%	COEFFICIENT OF UNIFORMITY (COEFFICIENT D'UNIFORMITÉ)	
	0.005mm>	%	COEFFICIENT OF CURVATURE (COEFFICIENT DE COURBURE)	

CETALATA PARAMETER AND	GRADATION ANALYSIS	3		FOR REPORTING
(A	(POUR LE RAPPORT)			
NAME OF SURVEY & LOCALITY (DÉNOMINATION DE L'ENQUÊTE ET LOCALITÉ)	Agno Flood Control		DATE (DATE)	
SAMPLE NO. & DEPTH (N° DE L'ÉCHANTILLON ET PROFONDEUR)	MA - 5 (m ~ m)	(ESSAL PAR)	

SPECIFIC GRAVITY (POIDS SPÉCIFIQUE) Gs

- July 1997	GRAIN SIZE (==) (GRANUROMÉTRIE)	50.8	38.1	25.4	19.1	9.52	4.76	2.00	0.84	0.42	0.25	0.105	0.`074
SIEVE (CRIBLAGE	TOTAL PASSING(%) (TOTAL PASSANT)												
METER (ÉTRE)	GRAIN SIZE(==) (GRANULOMÉTRIE)			:									
8 3	TOTAL PASSING(%) (TOTAL PASSANT)			:									



(COLLOIDE)

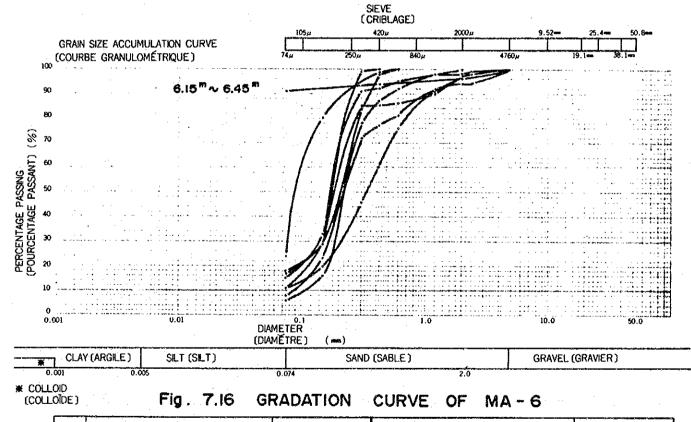
Fig. 7.15 **GRADATION** CURVE OF MA - 5

	4.76mm<	%	MAXMUM DIAMETER (DIAMÉTRE MAXIMUM)	sia.
ZZ	4.76~2.00mm	%	60% DIAMETER (DIAMÉTRE60%)	, in
ORTION	2.00~0.42mm	%	30% DIAMETER (DIAMÉTRE 30%)	Sign.
909	0.42~0.0747	%	10% DIAMETER (DIAMETRE 10%)	. mm
-5	0.074~0.005	%	COEFFICIENT OF UNIFORMITY (COEFFICIENT D'UNIFORMITÉ)	
	0.005mm>	%	COEFFICIENT OF CURVATURE (COEFFICIENT DE COURBURE)	

(A	GRADATION ANALYSIS NALYSE GRANULOMÉTRIQ		ngang Digwig Salaman Propinsi Pagas Camari Prigas Re	FOR REPORTING (POUR LE RAPPORT)
NAME OF SURVEY & LOCALITY (DÉNOMINATION DE L'ENQUÊTE ET LOCALITÉ)	Agno Flood Control	Control control field of the Security S	DATE (DATE)	A THE STATE OF THE PROPERTY OF
SAMPLE NO. & DEPTH (N' DE L'ÉCHANTILLON ET PROFONDEUR)	MA - 6 (m ~ m)	TESTED BY (ESSAI PAR)	

SPECIFIC GRAVITY (POIDS SPÉCIFIQUE) Gs

/F.	GRAIN SIZE (+++) (GRANUROMÉTRIE)	50.8	38.1	25.4	19.1	9.52	4.76	2.00	0.84	0.42	0.25	0.105	0.074
SIEVE	TOTAL PASSING(%) (TOTAL PASSANT)												
METER MÉTRE)	GRAIN SIZE(=) (GRANULOMÉTRIE)		·										
8 8	TOTAL PASSING(%) (TOTAL PASSANT)												

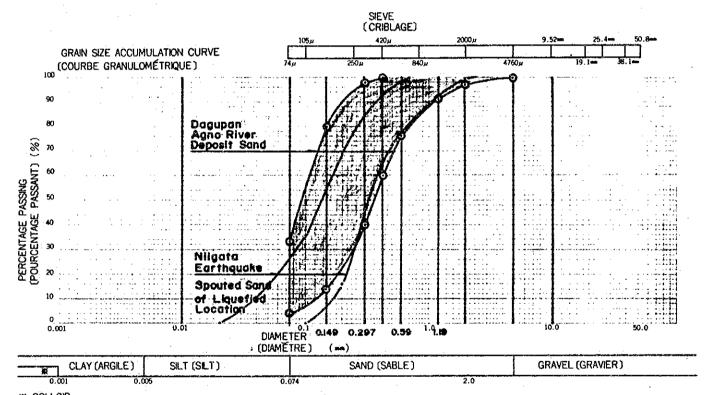


	4.76mm<	%	MAXMUM DIAMETER (DIAMÈTRE MAXIMUM)	ento.
22	4.76~2.00mm	%	60% DIAMETER (DIAMÉTRE60%)	me
SRTIO DRTIO	2.00~0.42***	%	30% DIAMETER (DIAMETRE 30%)	945
PROP(0.42~0.074mm	%	10% DIAMETER (DIAMÉTRE 10%)	SHIP.
	0.074~0.005mm	%	COEFFICIENT OF UNIFORMITY (COEFFICIENT D'UNIFORMITÉ)	,
	0.005mm>	%	COEFFICIENT OF CURVATURE (COEFFICIENT DE COURBURE)	

(Physical Sandras Cyristy Carlos Sandras Assess Carlos Car	GRADATION	ANALYSIS	Market Street,	ric Patrix and All Co	<u>ne i negoti dini ne ne permina depoti pri di</u> edunic	FOR REPORTING
(A	NALYSE GRANL	ILOMÉTRIQU	JE)			(POUR LE RAPPORT)
NAME OF SURVEY & LOCALITY (DÉNOMINATION DE L'ENQUÊTE ET LOCALITÉ)	Agno Flood	Control			DATE (DATE)	
SAMPLE NO. & DEPTH (N'DE L ÉCHANTILLON ET PROFONDEUR)		(m ~	m)	TESTED BY (ESSAL PAR)	

SPECIFIC GRAVITY (POIDS SPÉCIFIQUE) Gs

VE AGE J	GRAIN SIZE () (GRANUROMÉTRIE)	50.8	38.1	25.4	19.1	9.52	4.76	2.00	0.84	0.42	0.25	0.105	0.074
SIEV (CRIBL)	TOTAL PASSING(%) (TOTAL PASSANT)												
DROMETER REOMETRIE)	GRAIN SIZE(➡) (GRANULOMÉTRIE)												
8.2	TOTAL PASSING(%) (TOTAL PASSANT)												·



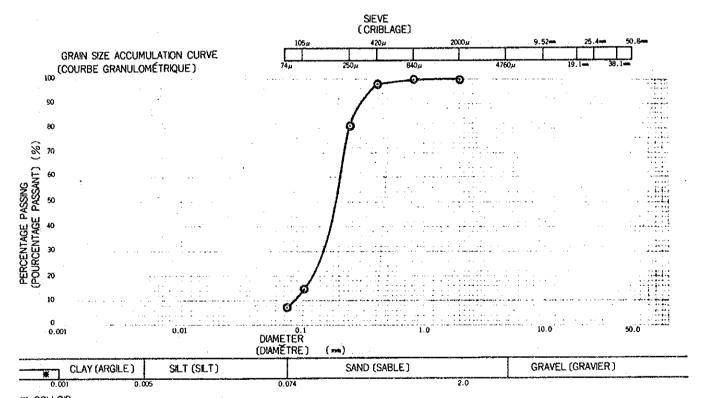
(COLLOIDE) Fig. 7.17 COMPARISON BETWEEN SANDS IN STUDY AREA AND NIGATA SAND

	4.76mm <	%	MAXMUM DIAMETER (DIAMETRE MAXIMUM)	relates.
	4.76~2.00mm	%	60% DIAMETER (DIAMÉTRE60%)	nom.
RTION)	2.00~0.42mm	%	30% DIAMETER (DIAMETRE 30%)	sum.
ROPC	0.42~0.074mm	%	10% DIAMETER (DIAMETRE 10%)	जन्म
1	0.074~0.005mm	%	COEFFICIENT OF UNIFORMITY (COEFFICIENT D'UNIFORMITÉ)	
	0.005mm>	%	COEFFICIENT OF CURVATURE (COEFFICIENT DE COURBURE)	

(A	GRADATION NALYSE GRANU	ANALYSIS LOMÉTRIQI				FOR REPORTING (POUR LE RAPPORT)
NAME OF SURVEY & LOCALITY (DÉNOMINATION DE L'ENQUÊTE ET LOCALITÉ)	Agno Floor	l Control			DATE (DATE)	
SAMPLE NO. & DEPTH (n'de l'échantillon et profondeur)		(m ~	m)	(ESSAI PAR)	

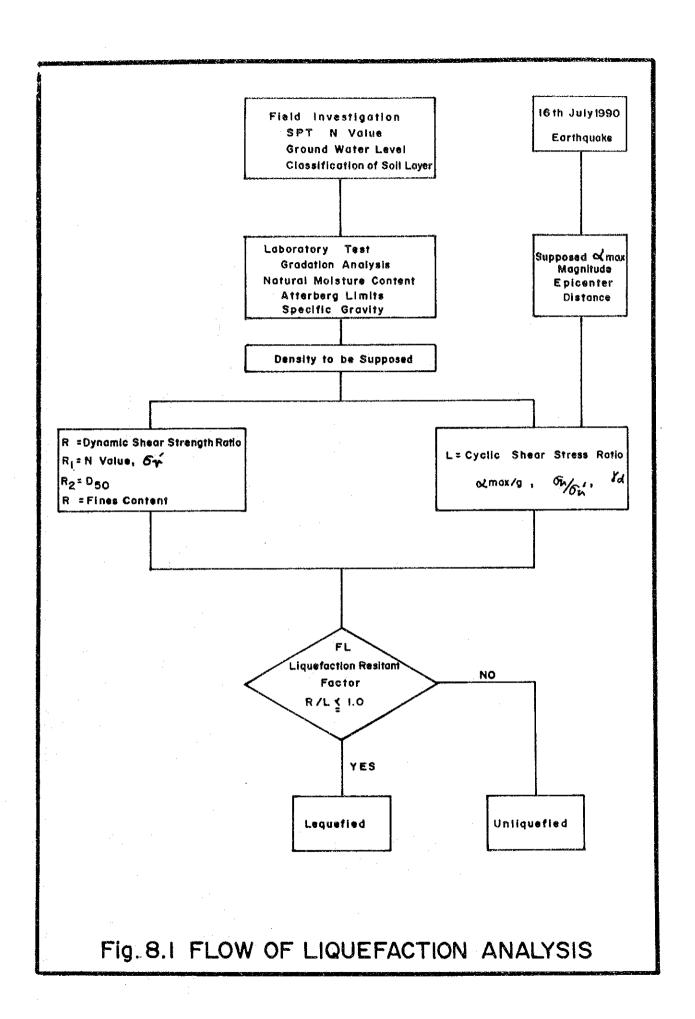
> SPECFIC GRAVITY (POIDS SPÉCFIQUE) Gs

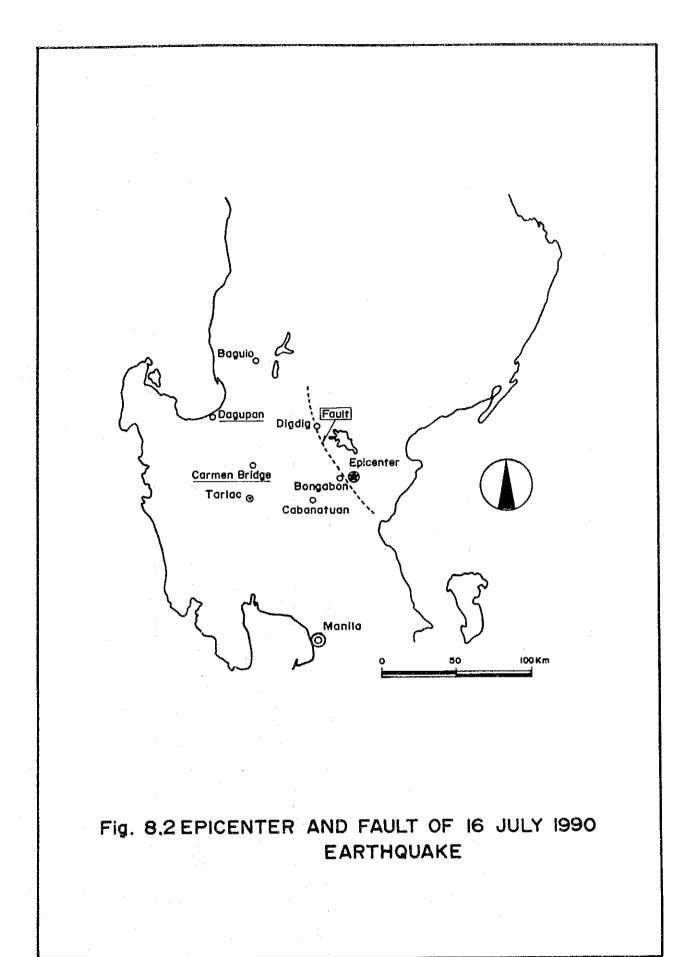
/E AGEJ	GRAIN SIZE (∞) (GRANUROMÊTRIE)	50.8	38.1	25.4	19.1	9.52	4.76	2.00	0.84	0.42	0.25	0.105	0.074
SIEVE (CRIBLAGE	TOTAL PASSING(%) (TOTAL PASSANT)					-		100	99.9	98.2	80.8	14.6	7.4
YDROMETER AREOMETRE)	GRAIN SIZE(**) (GRANULOMÉTRIE)												
HYDRON	TOTAL PASSING(%) (TOTAL PASSANT)												·

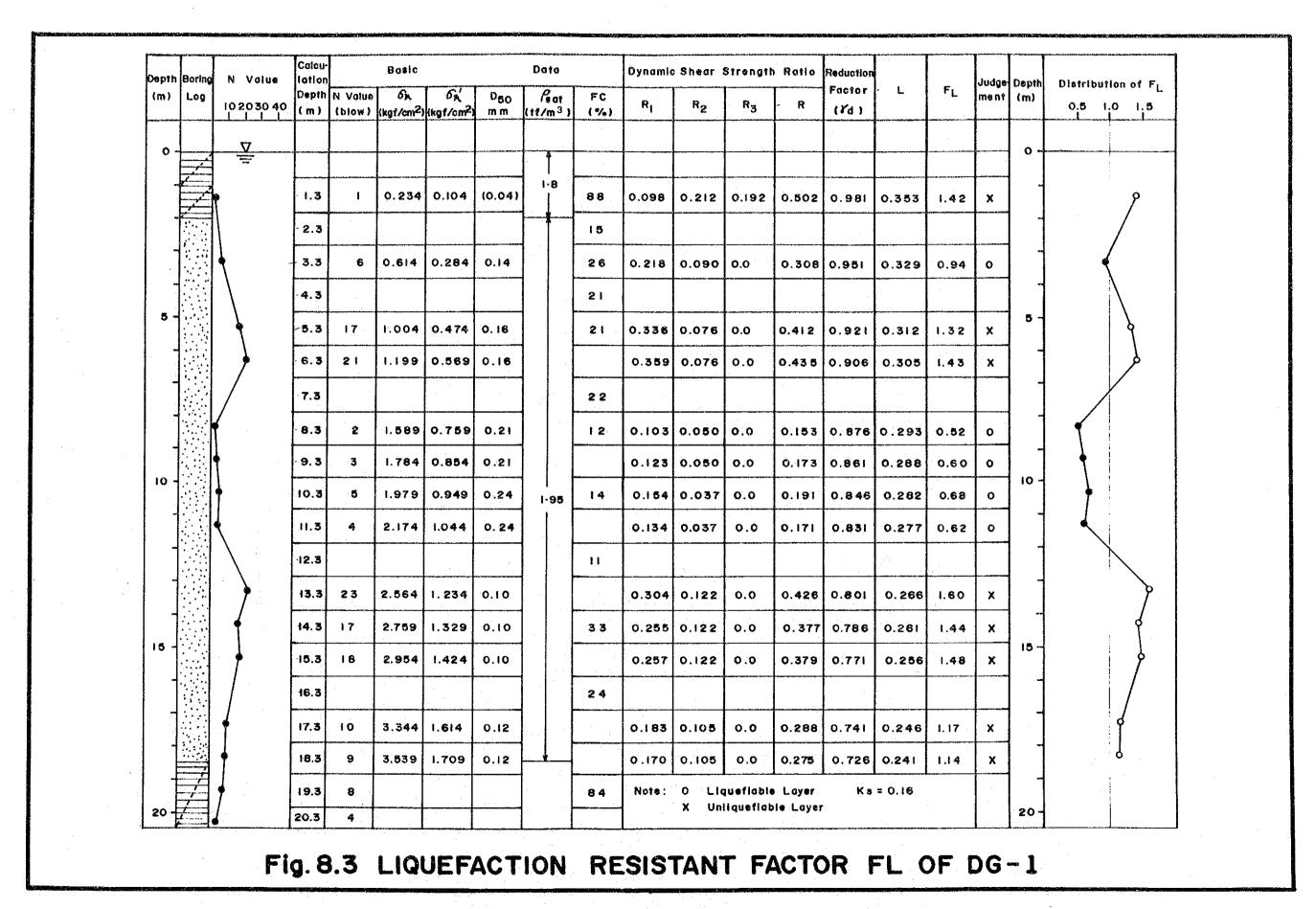


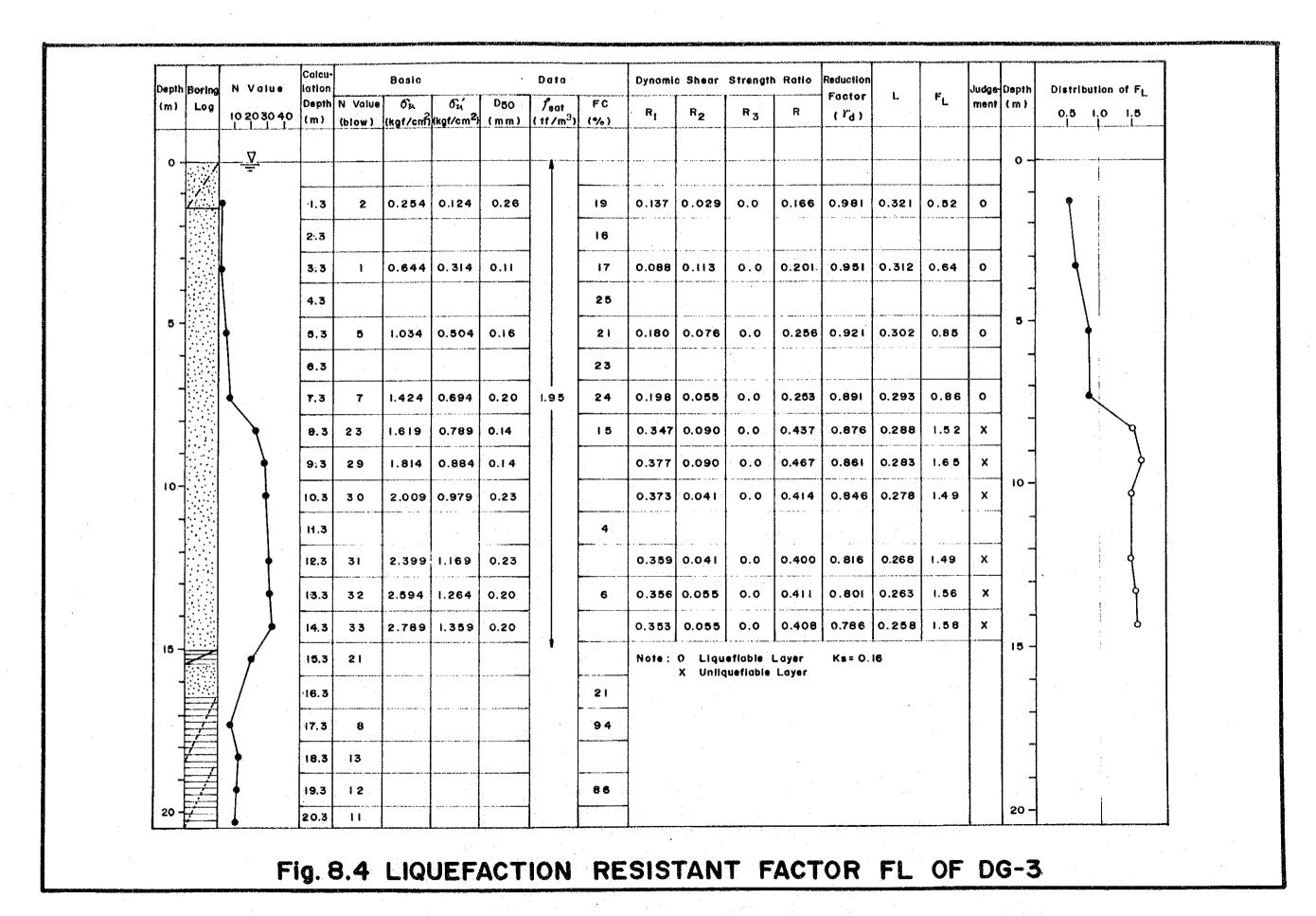
* COLLOID Fig. 7.18 GRADATION CURVE OF MIDDLE AGNO RIVER SAND

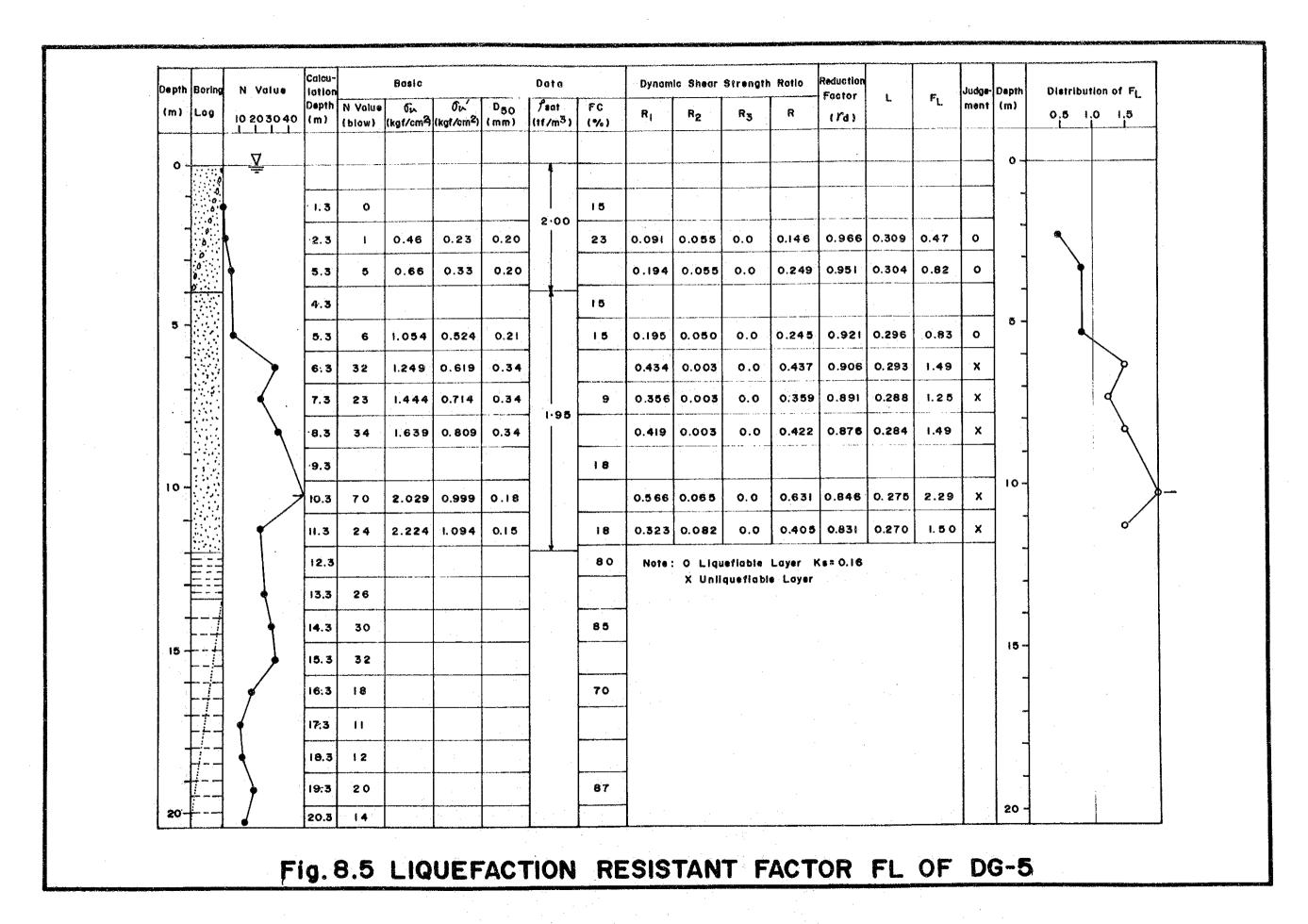
	4.76mm<	0	%	MAXMUM DIAMETER (DIAMETRE MAXIMUM)	2.0	7945)
1.0	4.76~2.00mm	0	%	60% DIAMETER (DIAMÉTRE60%)	0.20	99/5
PROPORTION (PROPORTION)	2.00~0.42mm	2	%	30% DIAMETER (DIAMETRE 30%)	0.15	пил
8 8	0.42~0.074mm	91	%	10% DIAMETER (DIAMETRE 10%)	0.085	1965
1	0.074~0.005mm	7	%	COEFFICIENT OF UNIFORMITY (COEFFICIENT D'UNIFORMITÉ)	2.4	
	0.005mm>		%	COEFFICIENT OF CURVATURE (COEFFICIENT DE COURBURE)	1.3	











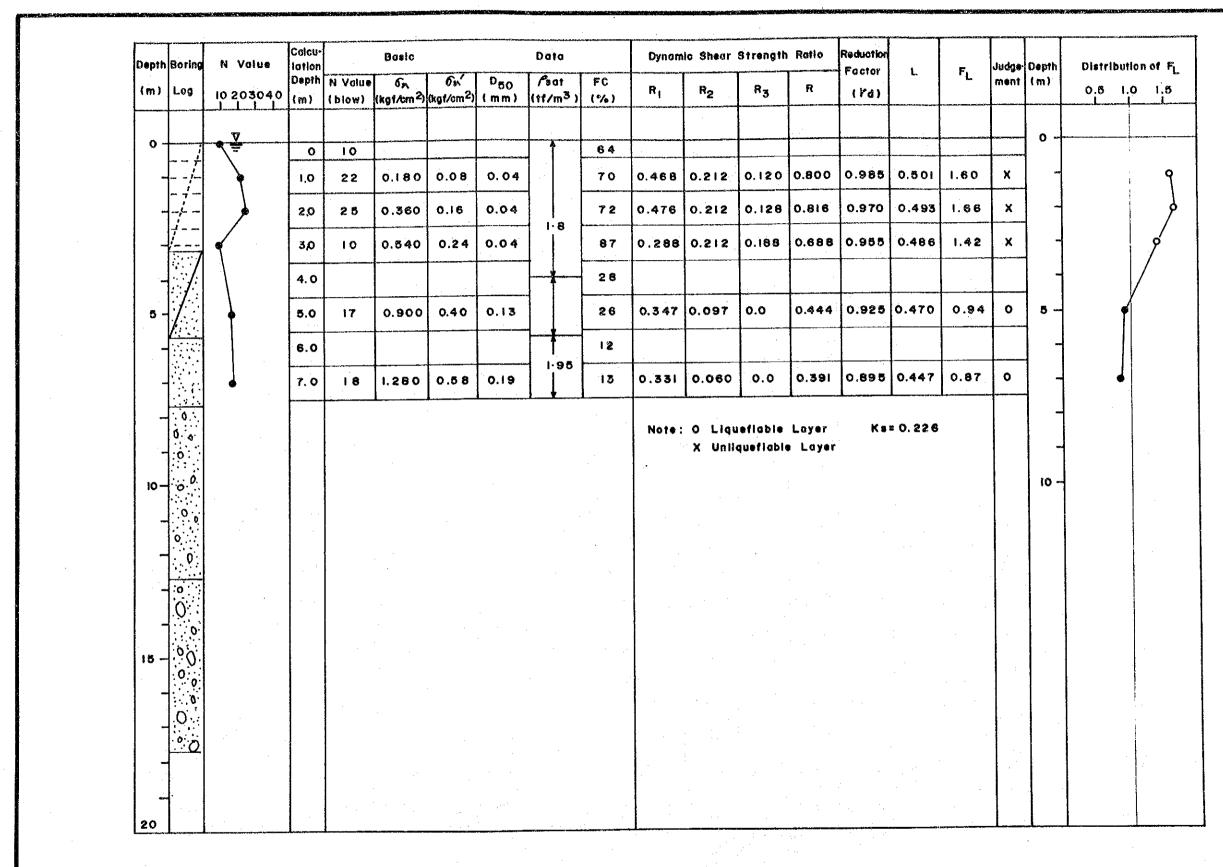
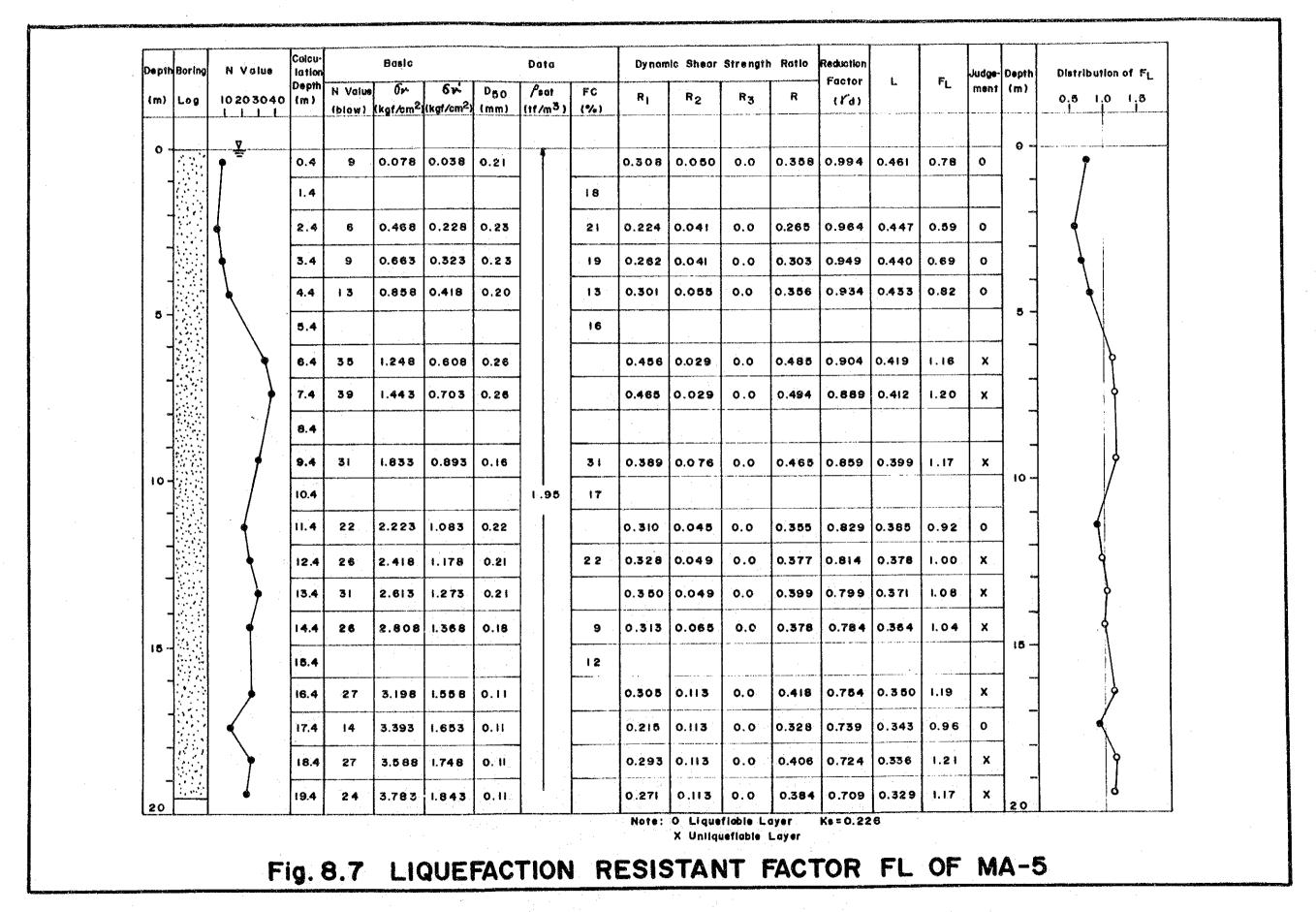
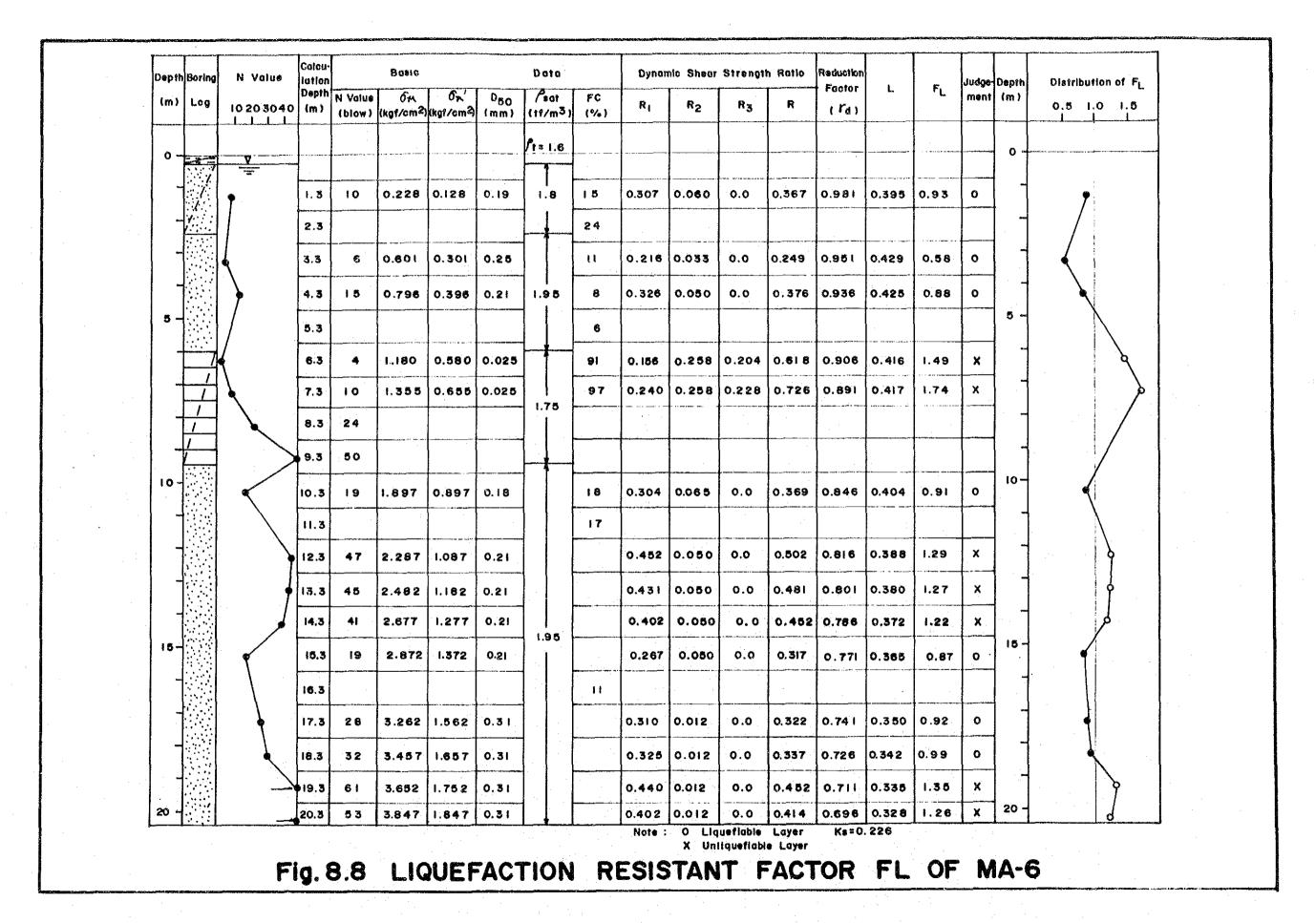
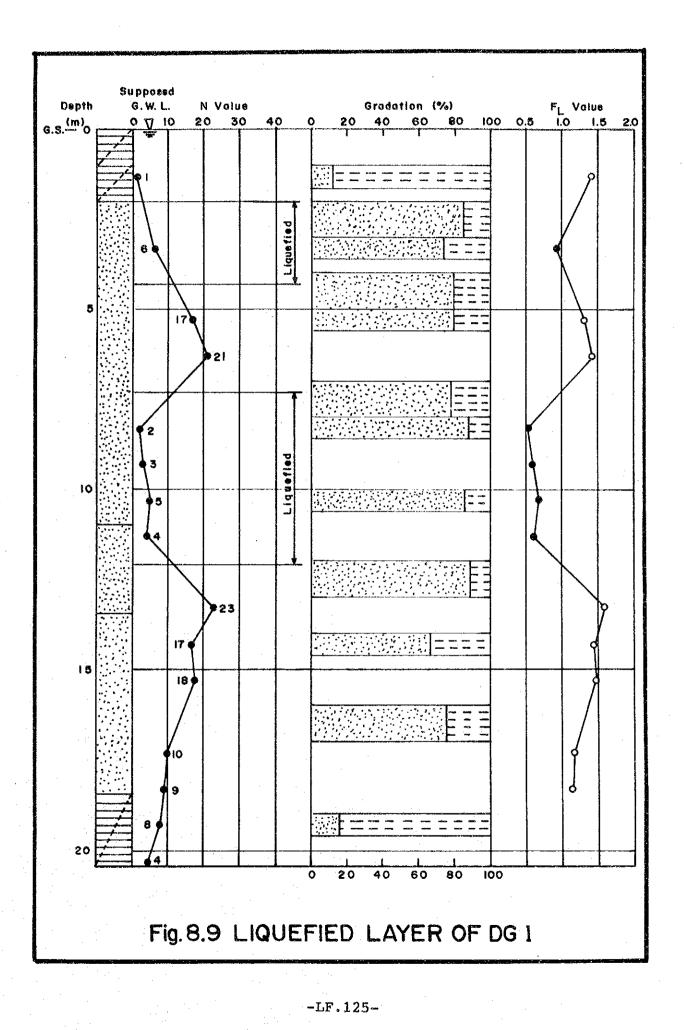
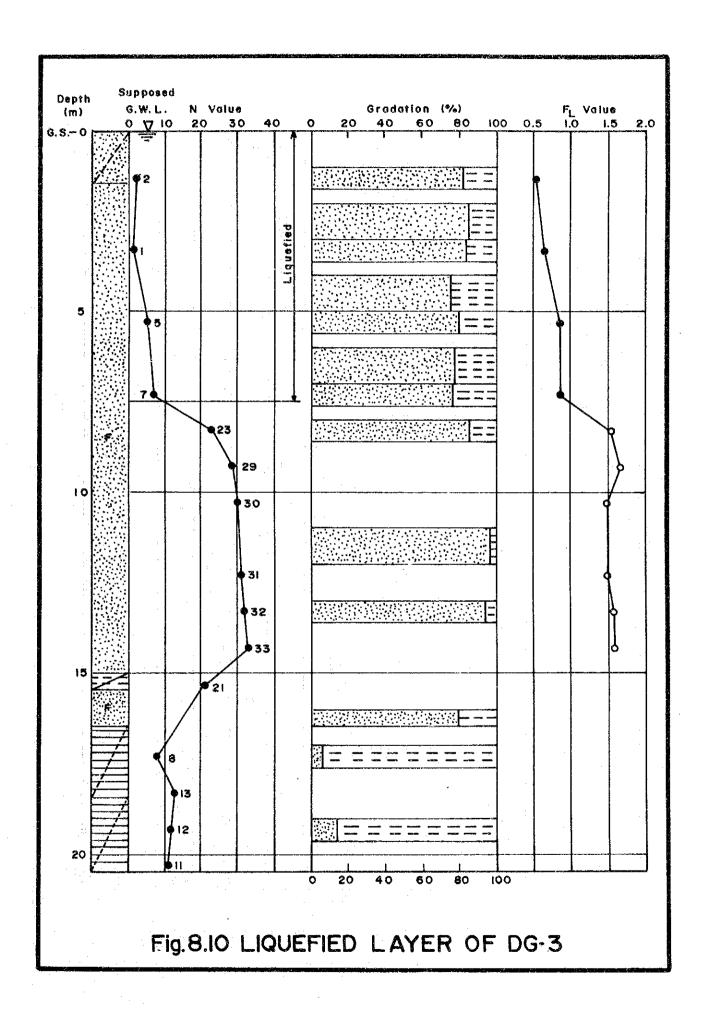


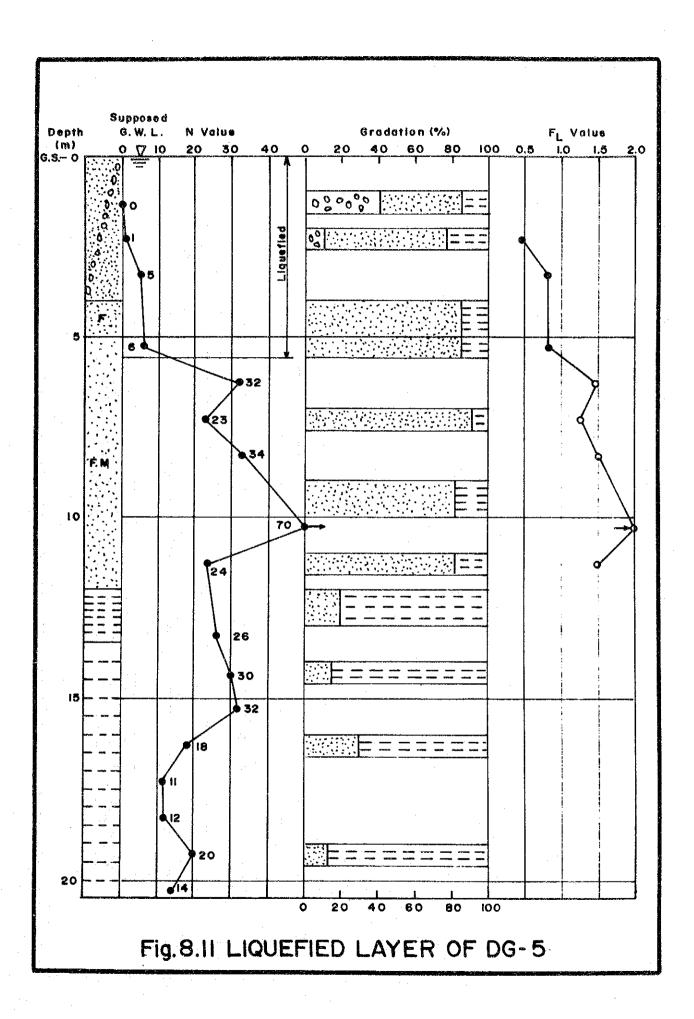
Fig. 8.6 LIQUEFACTION RESISTANT FACTOR FL OF MA-2

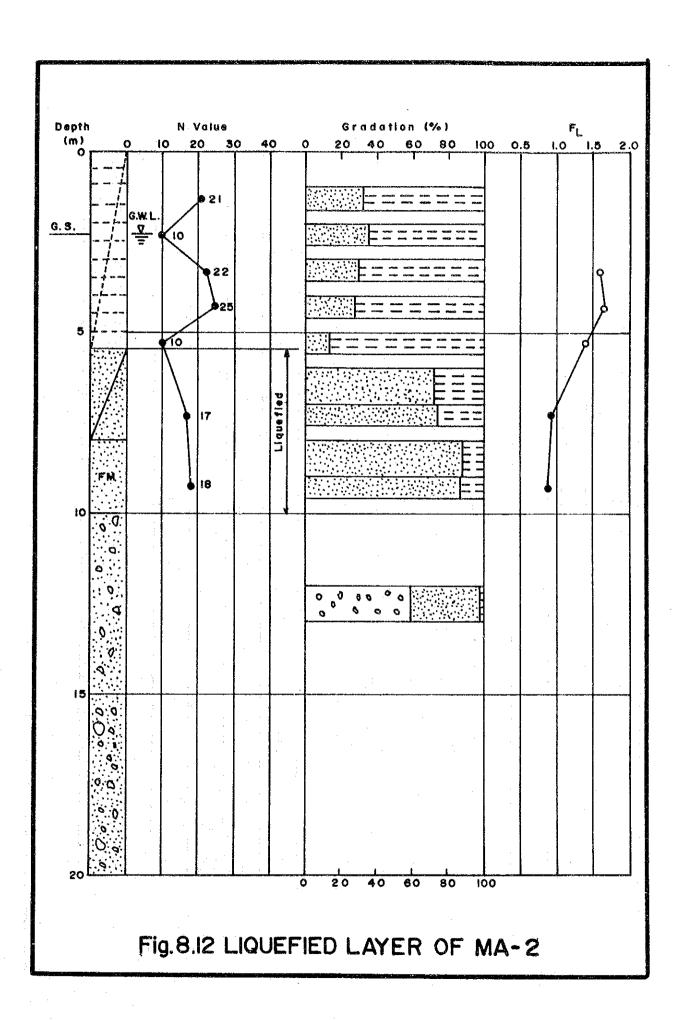




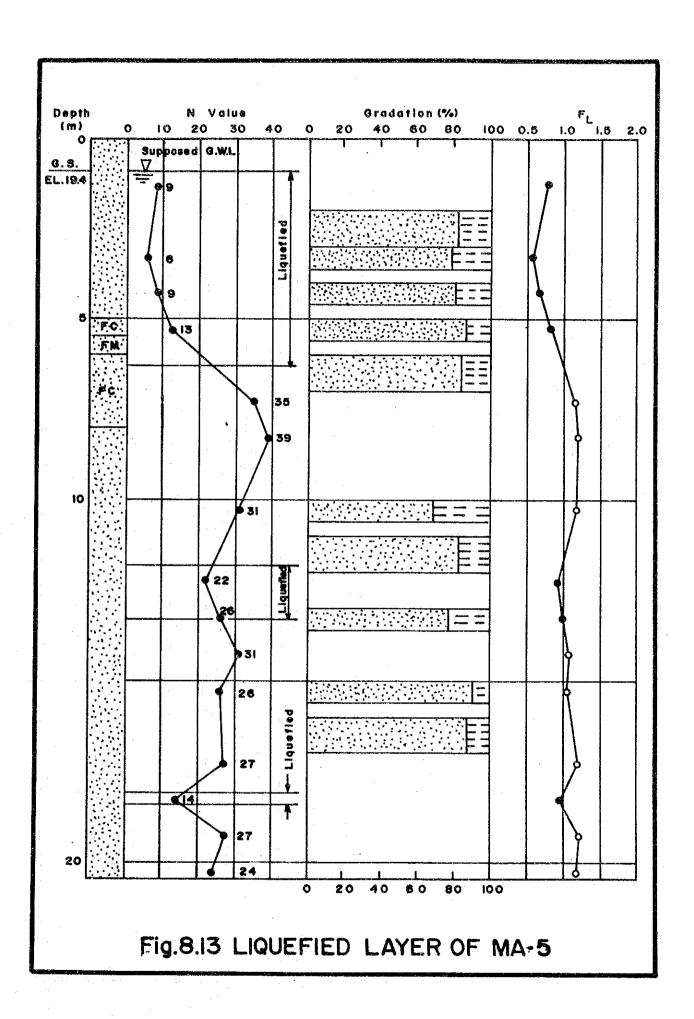


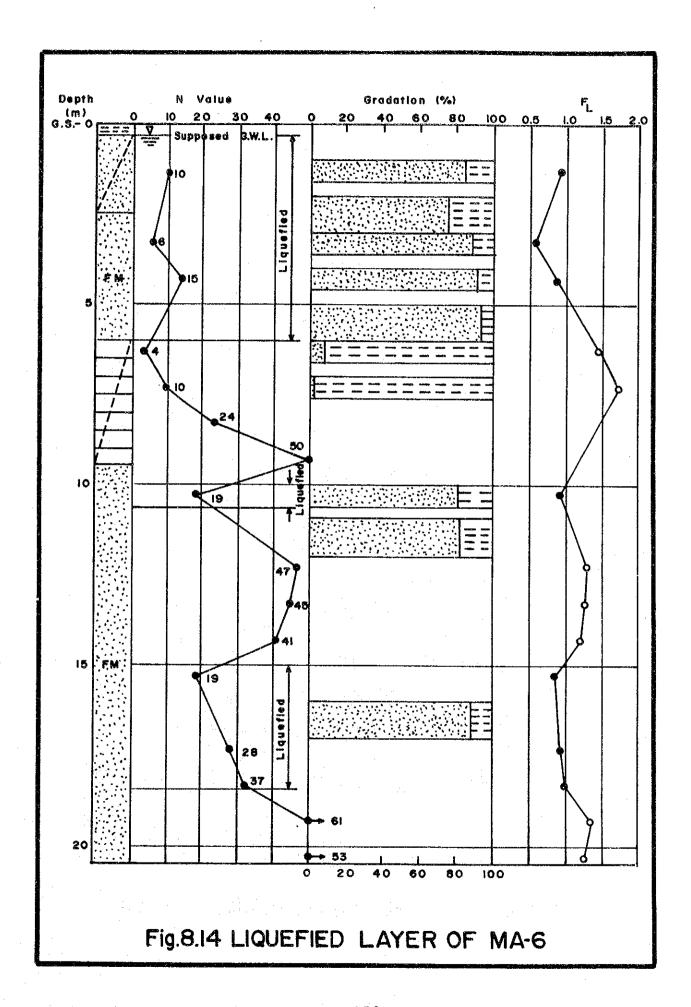






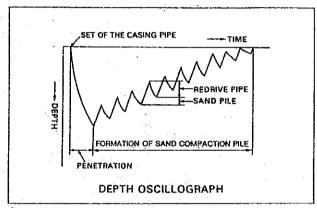
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Process

- Set the pipe at the specified position on the ground.
 Actuate the vibrator to penetrate the pipe into the ground. When there is a hard layer which makes it difficult to penetrate the pipe, water or air jet is used to force penetration.
 Penetration reaches a design depth.
 A quantity of sand is placed in the pipe from the upper hopper and whille drawing up the pipe to the specified level, sand in the pipe is discharged into the bored hole by compressed air.
 The pipe is redriven into the hole and sand is compacted by vibration. Sand is compressed into the surrounding subsoil layer.
 Again feed sand into the pipe and draw up the pipe to the specified height.
 By repeating the above process, complete the compozer pile up to the ground level.



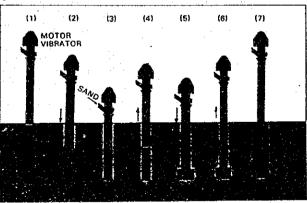


Fig. 9.1 SAND COMPACTION PILE **METHOD**

Vibro Rod Method

This is a method of compacting toose sandy soil by pressing under vibration, various types of special rods with characteristic projections provided at their ends and sides.

Advantages

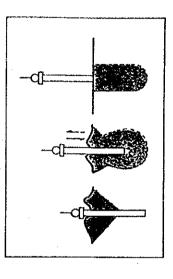
1) Vibration compaction effect is enhanced by spe-

cial rod processing.

2) Compaction force is transmitted to adjacent ground, owing to special rod processing; as interval between positions to be treated can be widened, work is economical.

widened, work is economical.

3) Working machinery is light and easy to move; work efficiency becomes higher and cost can be lowered.



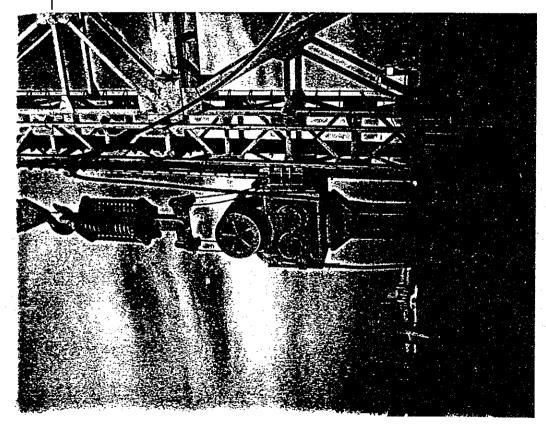


Fig. 9.2 ROD COMPACTION METHOD

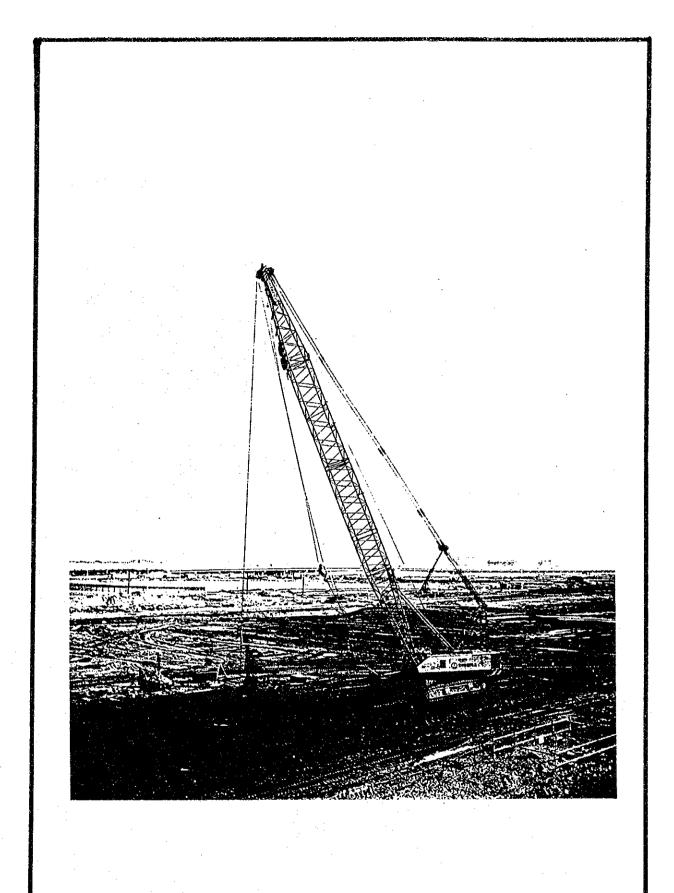
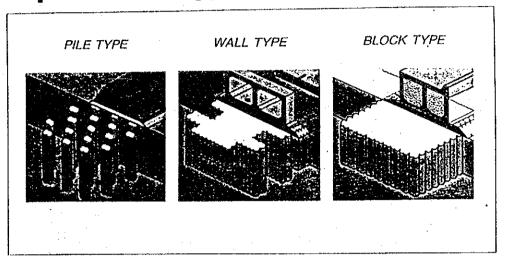


Fig. 9.3 DYNAMIC CONSOLIDATION METHOD

Improvement Type



Construction System

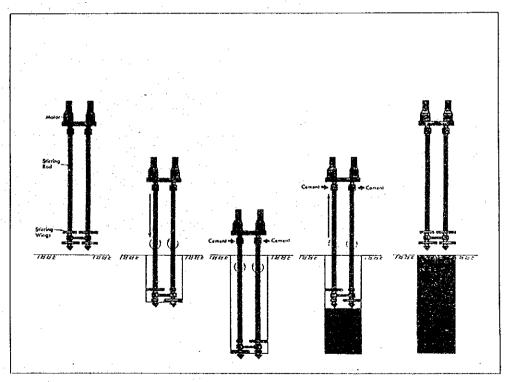
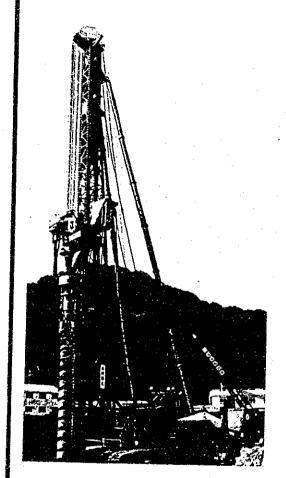


Fig. 9.4 DEEP MIXING METHOD



Gravel Drain Method

This is a different type of method in principle from the conventional compaction method, and involves forming gravel drain piles in loose sandy ground in order to prevent liquefaction of sand during earthquakes. This is effected by immeadiate dissipation of the excess pore water pressure.

Advantrages

1) Construction can be carried out without adverse effect on the adjacent ground.

2) There is no vibration effect on exisiting structures and vicinity.

3) Accordingly construction can be achieved in urban area.

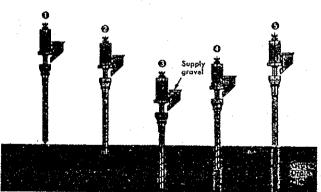


Fig. 9.5 GRAVEL PILE METHOD

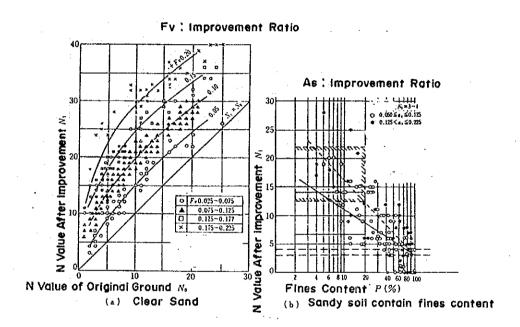


Fig. 9.6 DESIGN CHART OF SCP FOR SANDY SOILS