Table 4.4, the basin mean 4-day rainfall is estimated at 629 mm, 575 mm, 413 mm, 168 mm and 385 mm at San Roque, Carmen, Wawa, Tibag and rivermouth of the Agno River respectively.

## (3) Outlow/inflow at Binga and Ambuklao dams

Reservoir operation record during typhoon Maring is available at both dams of the Binga and the Ambuklao. Hourly inflow and outflow of both reservoirs are estimated based on their operation record as shown in Fig. 4.13.

The Binga and Ambuklao dams are not equipped with a reservoir space for flood control because of their single purpose for power generation. As given in Fig. 4.12, therefore, outflow from reservoir shows almost same pattern of flood inflow to reservoir at both dams.

## (4) Inundation map

Flood mark survey was carried out by the Study Team to confirm the extent of inundation area as well as water depth of the flood caused by typhoon Maring. Thus, the inundation map is available for use in calibration of proposed model.

# 4.3.3 Basic conditions for simulation

# (1) Runoff coefficient

Runoff coefficient is derived from the relationship between the volume of direct flood runoff and the total rainfall amount during flood.

Along this line, six flood inflow hydrographs at the Ambuklao dam are examined to estimate runoff coefficient as illustrated in Fig. 4.14.

Shown in Fig. 4.15 is the examined relation for selected flood assuming that the base flow is equivalent to the initial runoff immediately before the rising limb of flood hydrographs.

The plotted data shows that the runoff coefficient of 0.5 is adequate until the rainfall amount reaches up to 300 mm, while it shifts to 1.0 beyond

the rainfall amount of 300 mm.

## (2) Base flow

The relationship between average base flow and drainage area is established as given in Fig. 4.16. From this relationship, the specific base flow is estimated to be  $0.055 \text{ m}^3/\text{sec/km}^2$ .

# (3) By-pass floodway channel to the Poponto swamp

Discharge rating curves at the inlet of the by-pass floodway channel to the Poponto Swamp are constructed based on the non-uniform flow calculation as prepared in Fig. 4.17. In this simulation, the diverted flood discharge to the by-pass channel is estimated by use of these rating curves.

In this connection, the flood from the Tarlac River basin directly flows into the Poponto Swamp.

# (4) Breached/overtopped flow to the Allied Rivers

As mentioned before, there still remains several breaches/gaps dowstream of San Roque along the existing dike on the right bank of the main Agno River.

Thus, it is reported that flood runoff of the Agno River was partly overflowed into the Allied Rivers.

The bankful flow capacity at the said breaches/gaps is estimated at about  $1,200~\text{m}^3/\text{sec}$  based on the non-uniform flow calculation along subjective river stretches. In this simulation, the flood discharge over  $1,200~\text{m}^3/\text{sec}$  is assumed to be overflowed into the Allied Rivers.

## 4.3.4 Calibration results

Calibration of model parameters is performed through try and error by assuming that parameter K of storage function for each sub-basin is adjustable for best combination and other remaining parameters of sub-basins and river channels are fixed as values initially set up.

After final calibration, parameters K for sub-basins are taken up by multiplying 1.6 times to initial K values set up by impirical formula mentioned before.

The simulated flood runofff is compared with the observed ones at 4 water level stations and the Binga and the Ambuklao dams as shown in Fig. 4.18. As seen in this figure, the applied model well simulated the recorded flood appropriately. Fig. 4.19 shows simulated water level and discharge hydrograph at the Poponto swamp during typhoon Maring. The retarded volume in the swamp is estimated at about 251 x  $10^6 \mathrm{m}^3$ . The results of final calibration are summarized in Table 4.5 and 4.6 for sub-basin and river channel respectively.

## 4.4 Design Rainfall

The available rainfall data is analyzed for design of the rainfall duration, the probable basin mean rainfall at base point and its hourly distribution. The results of this analysis are used to estimate the probable flood runoff.

## (1) Design rainfall duration

The design rainfall duration is determined from the duration of recorded major storms. Fig. 4.20 shows accumulated rainfall curves at San Roque, Wawa, Tibag and Sta. Barbara stations of AFFWS. Major storms recorded at the said stations show that rainfall duration is usually 4 days. The rainfall duration for runoff calculation is therefore, decided to be 4 days.

## (2) Probable basin mean rainfall

Annual basin mean rainfall with duration of 1, 2, 3 and 4 days are estimated at each base point by means of Thiessen polygon method and adjustment for basin mean elevation as mentioned before. The daily rainfall data at 16 stations is used for this estimation. Taking into account the data availability of selected stations, three types of Thiessen polygon are laid out as shown in Fig. 4.21. Applied Thiessen's weight and adjustment factor are tabulated in Tables 4.7 and 4.8 respectively. The annual maximum basin mean 4-day rainfall at rivermouth of the Agno River (BP-1), the Cayanga-Patalan River (BP-8) and the Pantol-Sinocalan River (BP-9) are thus estimated for the

period from 1970-1986 as summarized in Tables 4.9 to 4.11 respectively.

In case that rainfall data is not available as it is missing, the rainfall data is extraporated based on the highest correlated relation among selected stations.

The probable basin mean rainfall is computed from estimated annual maximum basin mean rainfall by means of Pearson Type III method. The estimated probable rainfall at 9 base points for duration of 1, 2, 3 and 4 days are summarized in Table 4.12. Frequency curves of annual maximum basin mean rainfall at each base point is given in Fig. 4.22.

## (3) Hourly rainfall distribution

3-hour rainfall records of 29 major storms at 5 stations of San Roque, Carmen, Wawa, Tibag and Sta. Barbara are adopted to design the hourly rainfall distribution.

The average 1-day accumulated curve is developed using the 1-day maximum rainfall which is derived from the recorded distribution with 4-day duration as shown in Fig. 4.23.

The average daily distribution of the total rainfall amount with 4-day duration is analyzed as follows:

Day	 la jak	Ratio (%)	
1st day	•	19	
2nd day		25	
3rd day		32	
4th day		24	4

Considering the above average distribution, the design rainfall distribution for 4-day duration is determined as follows:

1st day : Uniform distribution of R4-R3
2nd day : Uniform distribution of R2-R1

3rd day : Distribution of R1 by average rainfall pattern

4th day : Uniform distribution of R3-R2

Where, R1: probable 1-day basin mean rainfall

R2 : probable 2-day basin mean rainfall

R3 : probable 3-day basin mean rainfall

R4 : probable 4-day basin mean rainfall

Typical hourly distribution of design rainfall is illustrated in Fig. 4.23.

## 4.5 Evaluation of Probable Flood under Present River Condition

Before proceeding to the probable flood runoff estimation under the alternative flood control schemes to be discussed in succeeding Sub-section, the probable flood runoff estimated from rainfall is compared and evaluated with the one resulting from recorded flood runoff through frequency analysis.

Flood record at San Roque is selected for this evaluation. This is because San Roque is not so far affected by flooding whenever the existing dike system was breached/overtopped.

## (1) Probable flood runoff from recorded flood runoff

The probable flood at San Roque is estimated by the Pearson Type III method using the recorded annual maximum peak discharge as given in Table 4.1. Fig. 4.24 shows the frequency curve at San Roque.

## (2) Probable flood runoff from rainfall

The probable flood runoff at San Roque is estimated from probable basin mean rainfall at San Roque under the present river condition.

## (3) Comparison and evaluation

The estimated probable flood peak runoff is summarized below.

		Probable Flood R	unoff (m <sup>3</sup> /s)
Return	Period (year)	from Flood Record	from Rainfall
	100	6,440	6,260
	50	5,000	5,060
	25	3,900	3,960
	10	2,570	2,720
	5	1,810	1,710
	2	990	830
	1.05	370	320
e de la finale			

Fig. 4.25 shows the comparison results schematically. The estimated probable flood discharge calculated based on rainfall data and the one computed from recorded flood agree well with each other. This fact implies that the approach for estimation of flood runoff based on rainfall is appropriate and applicable to flood control planning.

## 4.6 Probable Flood Runoff under River Improvement Condition

## 4.6.1 Condition for calculation

The flood runoff calculation is carried out under the following conditions:

- (1) River channel : Confining dike system along the main Agno River and major tributaries
- (2) Dam/reservoir: As for the existing dams of Binga and Ambuklao there is no flood control space in the reservoir.

  Therefore, the outflow is assumed to be equal to the inflow. San Roque dam in which the detail design has been completed and Balog-Balog dam under construction are to be incorporated. The reservoir operation proposed in their report is applied.
- (3) Retarding area : Poponto swamp is not taken into account.

Tables 4.13 and 4.14 show parameters of storage function of river channel

under confining dike condition. Estimated storage function of sub-basin of the Allied Rivers is tabulated in Table 4.15.

# 4.6.2 Probable flood peak distribution

Based on the above conditions, the flood runoff calculation is made with different return period of 1.05, 2, 5, 10, 25, 50 and 100 years. The estimated flood peak distributions for the Agno River and the Allied Rivers basins are summarized in Figs. 4.2.6 and 4.2.7 respectively. The probable flood hydrographs at 9 base points having reccurrence interval of 10, 25, 50 and 100 years are shown in Fig. 4.28. The relationship between the basin area and the specific runoff estimated for 100-year peak flood is illustrated in Fig. 4.29. The specific runoff at locations having watershed of steep mountainous area such as the upstream basin of the Agno River and the Ambayoan River shows bigger values compared with the one in other mountainous area. This tendency becomes more remarkable in the Allied Rivers.

Shown in Fig. 4.30 is comparison of the probable flood peak discharge distribution under confining dike condition with and without San Roque dam.

# 4.7 Flood Water Level and Duration in Inundation Area

# (1) Inundation map during typhoon Maring

Flood mark survey was carried out by the Study Team to confirm the extent of inundation area as well as water depth of the flood caused by the typhoon Maring. Thus, the inundation map is available for use in calibration of proposed model.

## (2) Simulation by flood inundation model

The inundation analysis for typhoon Maring in 1984 are carried out by use of the flood inundation model.

The simulation results is compared with the actual inundation area and maximum depth based on flood mark survey as shown in Fig. 4.31. The inundated area and maximum inundation depth by the typhoon Maring is simulated fairly well.

# (3) Probable inundation area

The inundation area and maximum inundated area in the lowland of the Allied Rivers basin under the occurrence of the probable 100-year flood is estimated by the simulation model. Calculation result is illustrated in Fig. 4.3.2.

For the above simulation, the flood inflow to be overflowed from the dike of the Agno River is estimated based on the following hydrological condition:

- The river dike is to be breached when the flood water level rises to the level corresponding to the 50% of free board.
- The flood runoff corresponding to the above water level is assumed to be the breach-starting discharge.
- The flood runoff over the breach-starting discharge is assumed to be flowed into the Allied Rivers basin.
- The breach-starting discharge is determined for each river stretch based on the river cross section data as given below:

River stretch of the Agno River	Breach-starting discharge (m <sup>3</sup> /s)
San Roque - Confluence of the Ambayoan R.	1,200
Conf. of the Ambayoan R Conf. of the Banila R.	5,470
Conf. of the Banila R Poponto floodway	3,130
Poponto floodway - Conf. of the Tarlac R.	1,230
Conf. of the Tarlac R Conf. of the Olo R.	10,200
Conf. of the Olo R Rivermouth	6,890

#### LOW FLOW STUDY

#### 5.1 General

The objective of the low flow study is to obtain runoff data at selected locations for the Sediment Study in the Agno River basin on a daily basis for a continuous period of more than 20 years. These daily runoff data is to be used in the sediment balance study to assess the sediment transport capacity in the Agno River.

Taking into account the availability of discharge and rainfall records, the runoff characteristic at San Roque is initially examined by applying the tank model method using the daily discharge and rainfall records for the period of 1960-1971. Then the missing part and unreliable period of the daily discharge record at San Roque is supplemented with the generated runoff resulting from the applied simulation model for the period of 1960-1986 taking into account the data reliability.

Finally the daily runoff for the period of 1960-1986 at selected locations is estimated based on the ratio of the basin area and the annual basin mean rainfall thereof.

#### 5.2 Available Data

Along the main Agno River and the Tarlac River, nine water level gauging stations exist as given below:

Stati	on	Recorded Period
Agno River		
(1)	San Roque	1960 - 1971
(2)	Carmen	1960 - 1971
(3)	Poblacion	1960 - 1971
(4)	Wawa	1964 - 1972
(5)	Banaga	1965 - 1972
(6)	Baay West	1965 - 1972
		the state of the s

## Tarlac River

(7) Villa Aglipay 1962,1964 - 1972

(8) Palublub 1965 - 1972

(9) Sta. Lucia 1966,1968 - 1972

Among the above stations, San Roque is selected for the evaluation of runoff record taking into account the following hydrological conditions:

- (1) Runoff record of stations located in the main Agno River shows that the runoff at San Roque is not affected by flood overflow into the Allied River basins through the existing breached portion of the right bank dike system, while the one at stations located in the downstream of San Roque is influenced thereby.
- (2) In the evaluation of runoff record, the rainfall data and the runoff data during the corresponding period is necessary to examine the relation between basin mean rainfall amount and runoff depth. The rainfall data at four stations which cover in the upstream basin of San Roque are available for comparison with the record at the stations in the Tarlac River basin which are intermittent.

and the law of the first of the law of the l

(3) Runoff record at San Roque is more or less affected by the operation of the Binga and Ambuklao dams located in the upstream basin of the Agno River. Low flow is expected to be supplementarily increased by the outflow from the Binga dam. However, the influence is minimal from the viewpoint of Sediment Study, hence it is not taken into account in evaluation. The high flow is the main focus in this evaluation as it is not affected by the operation of both dams where no space for flood control is provided.

## 5.3 Procedure of Simulation

The basic procedure of simulation is explained below:

(1) The tank model is firstly constructed at San Roque for the upstream basin of the Agno River for 1960-1971 of available runoff record.

The concept of the model is described in the succeeding Section 5.4.

- (2) The calibration of the model parameters is mainly carried out in terms of the following aspects:
  - monthly mean runoff
  - duration curve of daily runoff, and
  - runoff coefficient

The best combination of model parameters is determined through try and error method.

- (3) The daily runoff at San Roque is generated on daily basis by using the calibrated model for continuous 27 years from 1960 to 1986.
- (4) In the preparation of natural daily runoff at San Roque, the simulated daily runoff is used instead of recorded runoff when they are judged to be unreliable or not available due to data collection interruption. Thus, the natural daily runoff at San Roque is supplemented by generated runoff for the period of 1960-1986. The estimated natural runoff is examined further by the double mass curve method to check its reliability and consistency.
- (5) Finally, the daily runoff for the period of 1960-1986 at an arbitrary location is estimated based on the ratio of the basin area and the annual basin mean rainfall thereof.

# 5.4 Simulation Model

# (1) Basic concept of tank model

Suppose a tank having two holes, one at the bottom and the other at the side as shown in Fig. 5.1. When the tank is filled with water, the water will be released from through two holes. In the low flow analysis, the water released through the side hole corresponds to the direct runoff to a stream and the water from the bottom hole goes into the ground water zone.

The depth of water released from a hole is given by the following relation:

 $I = C \cdot H$ 

where, I : Depth of water released (mm/day)

C : Hole coefficient

H : Water depth above hole (mm)

## (2) Applied tank model

For the low flow simulation, four tanks vertically combined are usually applied as shown in Fig. 5.1. Each tank represents each runoff mechanism in the watershed. The top tank corresponds to the surface runoff, the second one to the subsurface runoff and the third and fourth to base flow from the ground water zone.

In a process of simulation, the simulating process, daily rainfall depth is placed into the top tank and the depth of water released from a hole is calculated by the above equation. The water from the bottom hole is put into the second tank and the same process is repeated to the fourth tank.

The depth of stream runoff is given as the sum of the water released from the side holes of four tanks. Loss due to evapotranspiration is expressed by subtracting the depth of daily evapotranspiration from the storage of the top tank.

## 5.5 Calibration of Model

# 5.5.1 Input data

## (1) Basin mean rainfall

The daily basin mean rainfall in the upstream basin of San Roque is estimated by means of weighted average of the four rainfall stations in its watershed considering the basin mean elevation as described in previous Section 4.3. The Thiessen weight and adjustment factor of the selected four stations are as follows:

Station	Thiessen weight	Adjustment factor for
		basin mean elevation
Bugias	0.25	1.41
Ambuklao	0.28	<b>1.36</b>
Baguio	0.20	0.86
Bobok	0.27	1.18 · · · · · · · · · · · · · · · · · · ·
		<u>_</u>

The estimated monthly basin mean rainfall at San Roque is summarized in Table 5.1.

# (2) Evaporation ratio

The monthly evaporation data by class A-pan is available at Ambuklao and its average monthly mean evaporation for the period of 1954-1966 is given below.

Jan. Feb. Mar. Apr. May June Jul. Aug. Sept. Oct. Nov. Dec.

4.8 5.1 5.2 4.5 3.9 3.6 3.1 2.5 2.6 4.0 4.3 4.2

# (3) Observed runoff at San Roque

Recorded monthly runoff at San Roque for the period from 1960 to 1971 is summarized in Table 5.2.

# 5.5.2 Calibration results

The simulation model developed at San Roque is calibrated by examining the following three aspects of the calculated runoff:

- duration curve
- monthly mean runoff
- runoff coefficient

Calibration of runoff on daily basis is not valid because area distribution of a rainfall is usually not uniform in the basin and the basin mean rainfall does not coincide the peak in the observed runoff.

## (1) Monthly mean runoff

Monthly mean runoff simulated by the model is compared with the observed monthly mean runoff as shown in Fig. 4.2. The simulated runoff is satisfactorily similar to the recorded runoff for the period of 1960-1966, while the occurrence of flood do not coincide with observed one after 1967 except in 1968.

# (2) Duration curve

Tank parameters of the simulation model is firstly adjusted so as to fit the daily flow duration curve of the simulated runoff to that of the runoff observed in each year. Along this line, fitting of the curve is mainly made in high flow discharge to satisfy the requirement of the Sediment Study. Flow duration curves of simulated runoff is prepared in comparison with that of observed runoff for each year for the period from 1960 to 1971 as given in Fig. 5.3.

In calibration of duration curves, curves in 1967, 1970 and 1971 do not show similar patterns to the observed ones. This is mainly because the observed runoff data involves unreasonably high discharge in dry season. The calibration disregards these years.

## (3) Runoff coefficient

Table 5.3 shows runoff coefficients of observed and simulated runoff together with errors of simulation. The average runoff coefficients for the period of 1960-1971 are estimated to be 0.71 and 0.72 for observed and simulated respectively. The coefficient for each year varies from 0.60 to 0.88 which is within an acceptable range.

In addition, the errors range from 0% to 17%, which is considered to be acceptable for this calibration.

## (4) Tank parameters

Based on the above calibration, parameters of the applied tank model are determined as shown in Fig. 5.1

## 5.6 Long-term Runoff at San Roque

Fig. 5.4 shows simulated daily runoff at San Roque after the final calibration. Thus, daily discharge record at San Roque is supplemented with the generated runoff for the continuous 27 years from 1960 to 1986.

In this extrapolation by simulated runoff, the daily runoff for 1967-1986 is estimated by means of simulation model. The observed runoff for 1967-1971 is judged to be unreliable due to unreasonably high discharge period in the dry season. The estimated long-term runoff at San Roque is examined by introduction of the double mass curve to check its reliability and consistency based on the relation between runoff depth and basin mean rainfall. As shown in Fig. 5.5, the double mass curve shows reliable relation between runoff depth and basin mean rainfall with a satisfactory consistency.

Accordingly, annual runoff at San Roque is estimated to be 95.3 m<sup>3</sup>/sec. on an average in 1960-1986. Monthly mean runoff is summarized in Table 5.4.

## 5.7 Estimate of Runoff in Sub-basin

In order to estimate the daily runoff at an arbitrary location from estimated runoff at San Roque, the following equation is applied:

Q = C. Qs

 $C = A/As \cdot R/Rs$ 

where, C : Conversion ratio

Q : Daily runoff at the objective sub-basin

Qs : Daily runoff at San Roque

A : Catchment area of the objective sub-basin

As : Catchment area at San Roque

R : Annual basin mean rainfall of the objective sub-basin

Rs : Annual basin mean rainfall at San Roque

Flow duration curves of natural runoff for the period of 1960-1986 are constructed at Wawa and rivermouth of the Agno River based on the daily natural runoff at San Roque as shown in Fig. 5.6.

The dependable discharge for different percentage of time are derived from the above flow duration curves. The estimated dependable discharge is tabulated below:

			(U	nit: m	3/sec.)	
		Percent	of time	(%)		
Location	90	80	50	20	10	
San Roque	15	18	41	161	233	
Wawa	42	51	115	452	654	
Rivermouth	56	67	152	597	864	

## 6. METEOHYDROLOGICAL OBSERVATIONS

# 6.1 Establishment of Observation Stations

Four automatic raingauges and nine automatic water level gauges were installed by DPWH as shown in Fig. 6.1. Their detailed locations are given in Appendix.

These station were selected from the hydrological viewpoint taking into account the existing meteohydrological observation network in the Agno River and the Allied River basins. The observed meteohydrological data thereby together with the existing stations are to be used for the hydrological study in the Feasibility Study stage.

The selected stations are given below.

## Raingauges (4 sets)

- (1) Camp 4 : Near the Aropong-Camp 4 in the upper basin of the Bued River
- (2) Saytan : At the compound of Saytan Elem. School in the lower basin of the Bued River
- (3) Sto. Domingo: Near the Tacnien town in upper basin of the Tuboy
  River
- (4) Iba : Near the Iba town in the lower basin of the Bulsa River

## Water level gauges (9 sets)

## Agno River (3 sets)

- (1) Poponto Left Dike: Just upstream of the overflow spillway in the

  left side earth dike at the Poponto floodway,

  Agno River
- (2) Poponto Right Dike: End of the right side earth dike at the Poponto floodway, Agno River
- (3) Cojuangco Bridge: Road bridge connecting the towns of Camiling and Moncado, Tarlac River

# Rivers (6 sets)

(4)	Camp 1 :	Road bridge crossing Bued River between Baguio
		City and Brgy. Saytan, Tuba.
(5)	Aloragat	Road bridge at Aloragat River and connecting
		towns of Manaoag and Barangay Nalsian
(6)	Angalacan	: Road bridge at Angalacan River connecting
		Barangays Aloragat and Cabanbaran.
(7)	Tagamusing :	Road bridge at Tagamusing River connecting the
		tocons of Binalonan and San Manuel
(8)	Sinocalan	Road bridge at Sinocalan River connecting the
		town of Mapandan and Brgy. Pinmaludpud, Urdaneta
(9)	Ingalera :	Road bridge crossing Ingalera River at Brgy.
		Nansangaan, Malasiqui.

Installation of automatic gauges at the above stations was completed as given below:

	Station	Date of Completion	
Rainf	<u>all</u>		
(1)	Camp 4	Aug. 21, 1989	about 700
(2)	Saytan	Aug. 21	about 190
(3)	Sto. Domingo	Sept. 3	about 90
(4)	Iba	Sept. 3	about 100
	<u>level</u> Poponto Left Dike		18.325
(1)	Poponto Left Dike	- · · · · · · · · · · · · · · · · · · ·	18.325
(2)			12.669
(3)		Nov. 23	14.500
(4)	Camp 1	Dec. 4	178.600
(5)	Aloragat	Oct. 23	11.400
(6)	Angalacan	Oct. 17	10.300
(7)	Tagamusing	Oct. 25	31.800
(8)	Sinocalan	Oct. 20	9.200
(9)	Ingalera	Dec. 15	2.700

#### 6.2 Observations

The following observation works were carried out by DPWH under the supervision of the hydrological monitoring expert.

## (1) Rainfall

Hourly observation by the automatic rain gauge.

## (2) Water level

Hourly reading of the staff gauge installed at gauging station during flood before completion of the installation of automatic water level gauges.

## (3) Discharge measurement

Discharge measurement to construct discharge rating curves at respective stations. Measurement by float is applied during flood, while current meter during low flow.

#### (4) Sediment load

Sediment sampling at 10 sites and their laboratory test

# (5) Water quality

Electric conductivity test is scheduled to be conducted in coming dry season in 1990 to assess the sea water intrusion into the Agno, the Cayanga-Patalan and Pantol-Sinocalan Rivers.

## 6.3 Observation Record

## (1) Normal observation

Hourly observation by automatic rainfall and water level gauges was called out after completion of their installation.

# (2) Observation during typhoon Openg

In the period of September 10 to 14, 1989, the typhoon Openg attacked the Agno River basin. Hydrological observation records observed during the typhoon are summarized below:

## Rainfall

- Hourly rainfall were observed at four new stations.
- 3-hourly rainfall were observed at five stations of the Agno river FFWS.

## Water Level

- Hourly water level were observed by staff gauge reading at four new stations, at Cojuangco Bridge, Ingalera, Sinocalan and Tagamusing.

The observation records of hourly rainfall and water level are compiled in Fig. 6.2 and Fig. 6.3 respectively. The water level hydrograph observation was started almost at the time of flood peak because the typhoon hit the area during the weekend and, therefore, dispatch of observation crew was somehow delayed.

The basin mean 4-day rainfall is estimated at 431 mm. The rainfall isohyetal map shown in Fig. 6.4 indicates that a very heavy rainfall was experienced at Bued river basins. The basin mean rainfall in Allied River basin is estimated at 506 mm which corresponds to the 5-year probable rainfall. On the other hand, the basin mean rainfall in the Agno River basin is calculated at 253 mm, which is less than the probable rainfall with a 2-year return period.

## (3) Flood inundation due to typhoon Openg

Field investigation on flood conditions was carried out in two days, September 10 to 11 1989. In addition, aerial survey by helicopter was also conducted on September 13, 1989. The flood inundation area widely spread to the downstream of Sinocalan river, especially at Dagupan City, Calasiao and Santa Barbara. Two bridges were broken at Manaoag along Aloragat river due to the flood.

# TABLES

Table 3.1 SUMMARY OF CLIMATIC CONDITIONS

	Jan.	Feb.	Har.	Apr	Hay	Jun,	July	Aug.	Sep.	Oct.	Hov.	Dec.	Annual
Hean Temperature (°c)													
f.	83	26.6		10.00 0.00		60 ( 60 (	28.1	27.5	67	28.0	27.2	50 60	e2 62
San Migue) (1951-1985)		18. 25.0	. 23 60 60 60	20.4 28.6	20 20	20°5	 	18.9 26.8	6. 6.	2 20 20 20 20 20	1.9.0 25.3	55 55 4. 4.	പ യെ ഡ
. <u> </u>							· ·						
Dagupan City (1951-1985)	30.9	31.8	33.55	34.9	6.3 At.	32.9	32.0	31.1	23 m	62 63	6.0 6.0	31.2	6.5 6.5 5.
Baguio (1951-1985) San Mionel (1969-1979)	31.0	23.6	2. 4. c.		22.5	80 en	23.0	22.0	22.9	63 m	23.23	80 60	10 m
.=									:			,	
12dinan (14 (1951-1995)	20.4	21.4	22	24.2	9 76	7.76	~	27.0	24.1	23.00	93.8	67	93.9
Baguio (1951-1985)	12.0	 	14.3	- KG	2.91	16.2	16.0	15.9		15.4	o ∞ ••••	0.	15.0
San Miguel (1968-1979)	18.8	19.0	20.3	21.3	23.1	23.2	8.22	23.1	22.6	22.3	21.6	20.2	21:6
Hean Relative Humidity (X)			;		•	a.	e e e e e e e e e e e e e e e e e e e	•					
Dagupan City (1951-1985)	5	e9 E-	202	70	£-	<del></del>	85	86 82	<del>3.</del>	98	<b>5</b>	5.	E
Baguio (1951-1985)	& &	e	<u>∞</u>	90	20 E	တ မ တ စ	ර ස ආ ර	83 E	ර ර	တ်ဆ	00 00 00 00	& &	ος ρ: 
- Rain	3	<b>?</b> .	<u> </u>		2	<b>3</b>		•	3	5	3	3	,
Dagunan City (1951-1985)	cva	~	era	LĘ⊅	13	E	63	6.7 6.7	20	13	ıcə	ત્ય	122
Baguio (1951-1985)	<b>-</b>	€3	*****	ఈ	19	22	26	6-3 5	<b>\$</b> 2	17	ග	ro,	166
Bvaporation (am)													
San Miguel (1968-1979) Ambuklao Dam (1954-1966)	146	152	194	204	170	138 108	128 96	113	127 80	131	131	133	1,768
		***************************************											

Table 4.1 RECORDED ANNUAL MAXIMUM DISCHARGE

Station : SAN ROQUE

Year		rrence ate	Gauge Height (m)	Discharge (m3/sec)
1950	Aug, 8	6:00 AM	5.06	1,040
1951	Jul. 31	6:00 AM	4.25	717
1952	Oct. 28	6:00 AM	3.95	473
1953	Aug. 21	0:00 PM	5,10	1,036
1954	Nov. 8	0:00 PM	5.80	1,404
1955	Sep. 24	6:00 AM	3.49	583
1956	Sep. 25	6:00 AM	3.87	314
1960	Aug. 26	6:00 PM	5.60	1,093
1961	Júl. 14	6:00 PM	4.99	758
1962	Jul. 22	-	•	900
1963	Sep. 12	6:00 AM	6.44	1,214
1964	Aug. 7	0:00 PM	6.96	2,046
1965	Jul. 15	7:00 AM	6.20	870
1966	May 20	5:00 PM	7.99	3,694
1967	Oct. 18	-	•	1,182
1968	Sep. 29	0:00 PM	8.40	4,350
1969	Jul. 29	6:00 AM	7.03	2,158
1970	Oct. 15	7:00 AM	5.90	550
1971	Aug. 14	•	6.99	862

Station : CARMEN

Year		rrence Pate	Gauge Height (m)	Discharge (m3/sec)
1950	Aug. 8	6:00 AM	25.53	1,720
1951	Jul. 31	0:00 PM	25.60	1,180
1952	Aug. 17	0:00 PM	24.30	725
1953	Jun. 5	0:00 PM	25.20	3,400
1954	Nov. 9	0:00 PH	25.48	3,075
1955	Sep. 24	6:00 AM	25.61	3,270
1956	Sep. 2	5:00 PM	24.32	1,283
1960	Aug. 23	8:00 PM	26.38	2,476
1961	Jul. 14	10:00 PM	24.88	1,326
1962	Jul. 23	6:00 AH	25.75	1,950
1963	Sep. 12	1:30 AM	25.92	2,114
1964	Aug. 8	3:00 PM	26.43	2,527
1965	Jul. 14	7:00 AM	26.66	2,743
1966	May 20	10:00 PM	26.60	2,404
1967	Oct. 17	11:00 SM	27.60	3,855
1968	Sep. 29	5:00 PM	26.68	2,764
1969	Jul 28	7:00 PM	25.83	1,658
1970	Sep. 12	6:00 PM	25.18	1,545
1971	Oct. 11		26.17	2,307

Source : Philippine Water Data - Surface Water Records, NWRC

# Table 4.2 MAJOR FLOOD RECORDS OBSERVED BY AFFWS

# (1) Rainfall (duration: 4-day)

(Unit: mm)

Typoon		Rainfall	gauging s	station	
rypoon	San Roque	Carmen	Wawa	Tibag	Sta. Barbara
Maring	475	277	250	105	334
Kuring		336	331	207	397
Daring	279	181	338	330	367
Gading	. =	401	345	241	548
Miding	457	202	187	165	360

# (2) Maximum discharge

(Unit: cu.m/sec)

Marin a am		Rainfall	gauging s	station	
Typoon	San Roque	Carmen	Wawa	Tibag	Sta. Barbara
Maring	2,816	2,220	3,061	610	265
Kuring	-	-	1,365	730	265
Daring	-	_ `	2,423	1,181	260
Gading	-	<del>-</del> ,	2,363	· <del>-</del>	-
Miding	-		2,705	_	262

Table 4.3 DISCHARGE RECORD OF TYPHOON MARING IN 1984

23:00

Table 4.4 BASIN MEAN RAINFALL AT TYPHOON MARING

Rai	nfall Station	Adjust-	Т	hiesen Wei	ght at Bas	se Point	
(4-d	ay Rainfall)	ment Factor	San Roque	Carmen	Wawa	Tibag	Rivermouth
1.	Baguio (826mm)	0.73	0.18	0.09	0.05	<b>-</b>	0.04
2.	Ambuklao (538 mm)	1.15	0.70	0.42	0.24	· · · · · · · · · · · · · · · · · · ·	0.18
3.	San Roque (475 mm)	1.52	0.12	0.12	0.07	<b>-</b> ; .	0.05
4.	San Nicolas (381 mm)	1.49		0.23	0.13	- :	0.09
5.	Binalonan (254 mm)	1.00	3	0.01	0.01	- -	0.01
6.	Balungao (293 mm)	1.08		0.12	0.12	-	0.09
7.	Carmen (279 mm)	1.00	$\frac{h_{i}}{h_{i}} = \frac{1}{2}$ $\frac{h_{i}}{h_{i}} = \frac{1}{2}$ $\frac{h_{i}}{h_{i}} = \frac{1}{2}$	0.01	0.03	<u>.</u>	0.02
8.	Wawa (254 mm)	1.00	- 1990 - 1990 - 1990 - <del>1</del> 990 - 1990 - 1990 - 1990	· · · · · · ·	0.06	<b>-</b> .	0.06
9.	Tibag (105 mm)	1.19		4. <u>-</u>	0.20	0.59	0.15
ΙΟ.	Mayantoc (179 mm)	1.28		- · · · · · · · · · · · · · · · · · · ·	0.09	0.41	0.17
11.	Mangatarem (273 mm)	1.37	- -		<b>-</b>	-	0.10
2.	Matalava (334 mm)	1.16	• • • • • • • • • • • • • • • • • • •		:	- ,	0.04
	Basin Mean 4-day Rainfal (mm)	en er	629	575	413	168	385

Table 4.5 STORAGE FUNCTION OF SUB-BASIN OF AGNO RIVER

Sub-basin		River	River	Coeff. of Funct		Lag-time
No.	Area (Km2)	Length (Km)	Gradient	K	р	(hr)
A01	514	58.5	1 / 40	62.9	0.666	5.0
AO2	103	22.5	1 / 10	95.3	0.481	2.0
AO3	243	27.5	1 / 20	77.4	0.566	2.0
A04	191	16.5	1 / 20	77.4	0.566	1.0
AO5	199	14.0	1 / 10	95.3	0.481	1.0
A06	_ 85	16.5	1 / 20	77.4	0.566	1.0
AO7	10	1.1	1 / 1480	21.3	0.990	0.0
AO8	151	25.5	1 / 20	77.6	0.565	2.0
A09	119	11.0	1 / 10	95.3	0.481	$\begin{array}{c} 1.0 \\ 1.0 \end{array}$
A10	40	7.0	1 / 10	95.3 95.1	$\begin{array}{c} \textbf{0.481} \\ \textbf{0.482} \end{array}$	1.0
A11	53 - 7	14.0	1 / 10 1 / 1510	21.2	0.990	0.0
A12	50	1.6 17.0	1 / 20	77.4	0.566	1.0
A13	47	12.5	1 / 240	36.7	0.990	2.0
A14 A15	11	8.0	1 / 190	39.4	0.961	1.0
A16	39	14.0	1 / 10	96.4	0.477	1.0
A17	26	8.0	1 / 10	95.3	0.481	1.0
A17	70	18.0	1 / 10	95.3	0.481	1.0
A19	4	0.5	1 / 1630	20.7	0.990	0.0
A20	54	2.2	1 / 1380	21.7	0.990	0.0
A21	119	23.0	1 / 240	36.7	0.990	3.0
A22	73	23.0	1 / 20	77.8	0.564	2.0
A23	4	0.8	1 / 1470	21.3	0.990	0.0
A24	93	27.5	1 / 20	77.4	0.566	2.0
A25	94	17.0	1 / 180	40.0	0.949	2.0
A26	31	17.0	1 / 850	25.1	0.990	2.0
A27	14	3.5	1 / 90	49.3	0.806	0.0
A28	20	1.1	1 / 1450	21.4	0.990	0.0
A29	24	2.2	1 / 1660	20.6	0.990	0.0
A30	119	23.5	1 / 20	77.4	0.566	2.0
А31	39	17.0	1 / 20	77.4	0.566	1.0
A32	120	13.5	1 / 30	68.5	0.623	1.0
A33	25	4.0	1 / 100	47.8	0.826	0.0
A34	283	37.5	1 / 190	39.4	0.961	3.0
A35	254	23.5	1 / 60	55.7	0.733 0.806	2.0
A36	21	3.5	1 / 90	49.3 42.3	0.909	2.0
A37	155	22.0	1 / 150 1 / 270	35.5	0.990	2.0
A38	102	13.5	1 / 1220	22.6	0.990	4.0
A39	778	32.7		77.2	0.567	2.0
A40 A41	221 20	$\begin{array}{c} 27.0 \\ 5.5 \end{array}$	1 / 20 1 / 10	95.3	0.481	0.0
A42	42	11.5	1 / 70	53.2	0.760	1.0
A43	26	8.5	1 / 430	30.8	0.990	1.0
A44	190	31.5	1 / 60	55.7	0.733	3.0
A45	105	29.0	1 / 30	68.5	0.623	2.0
A46	44	8.5	1 / 850	25.1	0.990	1.0
A47	51	2.2	1 / 1340	21.9	0.990	0.0
A48	157	25.5	1 / 20	77.4	0.566	2.0
A49	130	25.5	1 / 20	77.9	0.564	2.0
A50	10	1.5	1 / 1410	21.6	0.990	0.0
A51	78	15.0	1 / 30	68.5	0.623	1.0
A52	64	15.0	1 / 20	77.4	0.566	1.0
A53	8	1.1	1 / 1590	20.8	0.990	0.0
A54	54	11.0	1 / 20	77.4	0.566	1.0
A55	42	3.5	1 / 1660	20.6	0.990	0.0
A56	122	20.5	1 / 30	00.0	0.623	2.0
A57	79	8.5	1 / 10	95.3	0.481	1.0
A58	80	6.0	1 / 1330	22.0	0.990	1.0

Table 4.6 STORAGE FUNCTION OF RIVER CHANNEL UNDER PRESENT RIVER CONDITION OF AGNO RIVER

	River	River	Stora	ge Function	Lag Time		River	River	Stora	ge Function	Lag
nel No.	Length (km)	Slope	K	P	(kr)	nel No.	Length (km)	Slope	ĸ	P	fine (kr)
1	15.0	1/ 70	19264	0.659	1.0	19	11.5	1/ 350	29519	0.669 Q < 350	2.0
2	23.0	1/ 150	59433	0.608	2.0			·	3197	1.040 Q > 350	
3	22.5	1/ 110	84650	0.624	2.0	20	17.8	1/ 180	38147	0.662 Q < 750	2.0
4	12.0	1/ 190	62208	0.611	1.0			-	4000	1.000 Q > 750	
5	0.5	1/ 400	25920	0.611	1.0	21	9.5	1/ 290	24927	0.661 Q < 400	1.0
6	19.0	1/ 70	13006	0.829 Q < 1800	2.0			•	2766	1.026 Q > 400	
			49844	$-0.645  \tilde{Q} > 1800$		22	18.0	1/ 890	308909	0.596	2.0
7	5.5	1/ 90	6770	0.761 Q < 5500	0.0	23	16.5	1/1350	312500	0.602	2.0
		-,	19798	$0.645 \ Q > 5500$		24	5.0	1/ 80	10994	0.646 Q < 550	0.0
8	4.2	1/ 140	8243	0.753 Q < 3500	0.0			-,	1200	1.000 Q > 550	•
. •	•••	-,	19107	0.641 Q > 3500	. ***	25	11.0	1/ 130	27977	0.667 Q < 400	1.
9	8.0	1/ 200	16384	0.796 Q < 1000	1.0	•		-,	3258	1.022 0 > 400	•
•	***	-14	43896	0.653 Q > 1000	1.0	26	21.5	1/1390	95132	0.650 0 < 200	3.
10	7.2	1/ 190	14236	0.748 Q < 800	1.0		1110	1,1070	17486	0.968 Q > 200	
10		1) 170	39063	0.602 Q > 800	4.0	27	20.0	1/1650	162258	0.597 Q < 3500	3.
11	7.0	1/ 350	11525	0.854 Q < 140	1.0	21	10.0	11 2000	246	1.388 3500 < Q	
11	7.0	11 330	29519	0.669 Q > 140	1.0				240	< 8400	
12	20.5	1/ 840	6839	1.048	3.0				50516	0.801 Q > 840	
13	9.0	1/ 600	24927	0.661 Q < 150	1.0	28	10.2	1/ 600	22606	0.681 Q < 200	1.
13	3.0	1/ 000			1.0	20	19.2	1/ 000	3582		. 1.
14		3/ 000	6591	0.931 Q > 150	1.0	20		1/ 500			1
14	5.5	1/ 800	18434	0.637 Q < 300	1.0	29	6.2	1/ 700	14400	0.699	1.
10	10.0	1/ 000	2277	1.030 Q > 300	1.0	30	14.0	1/2320	242532	0.581 0 < 3400	2.
15	10.5	1/ 800	36868	0.637 <u>0</u> < 300	1.0				33	1.678 3400 < Q	-
16	15.0	1/1650	13374	0.954 Q < 2300	2.0					< 8200	
		. [2.00	106718	0.685 Q > 2300		··.		1 18400	141615	0.752 Q > 8200	
17	18.5	1/1650	23662	0.954 Q < 2300	2.0	31	19.2	1/7000	334925	0.581 Q < 3400	3.
	22.		188810	0.685 Q > 2300					45	1.678 3400 < Q	
18	15.3	1/ 190	29519	0.669 Q < 550	1.0	•				< 8200	
			6291	0.923 Q > 550					195563	0.752 Q > 8200	

Table 4.7 TIESEN WEIGHT BY BASE POINT FOR AGNO RIVER BASIN

(1) Type A (Period: 1970-1976, 1978)

Base					Rain	fall Gauging S	tation				
Point	Buguias	Adaoay	Sayangan	Bobok	Baguio	guio San Nicolas Binalo	Binalonan	Balungao	San Miguel	Surgui	Matalava
BP-1	0.04	0.04	0.02	0.05	0.04	0.12	10.0	0.14	0.12	0.34	0.08
BP-2	0.05	0.07	0.02	0.08	0.05	0.20	0.01	0.18	0.16	0.18	•
BP-3	80.0	0.12	0.05	0.18	0.09	0.32	0.03	0.12		0.01	•
BP-4	0.17	0.22	0.08	0.23	0.16	0.12	0.01	1			1
BP-5	ı,		i			ı.		i,		1.00	i
BP-6	4	•	1	E.		•	,	0.23	0.38	66,0	•
BP.7		,		0.48	,	0.52		:	•		

(2) Type B (Period: 1977, 1979 - 1980)

Base					Rainf	Rainfall Gauging Station	ation		- (		
oint T	Bobok	Baguio	Тареуо	တိ	Binalonan	Balungao		San Miguel		Mangatarem	Matalava
3P-1	0.10	0.03	0.10	0.12	0.01	60.0	0.08	0.10	0.21	0.12	0.04
3P-2	0.13	0.04	0.13	0.21	0.01	0.11		0.13			•
3P-3	0.28	90.0	0.21	0.31	0.01	0.11		t	•	•	•
3P-4	0.38	0:10	0.39	0.12	0.01	ı	• •	•	1	•	- 1
3P-5	•	•	•		•		•	1	0.99	0.01	•
BP-6		\$	•		•	0.13	0.22	0.32	0.33		
3P-7	0.48	,	•	0.52		•	•	: •	1	•	

(3) Type C (Period: 1981 - 1986)

Point         Bobok         Bagulo         Binatonan         San Nicolas         Balungao         Alcala         Tibaq         Mayantoc         Mangatarem           BP-1         0.16         0.05         0.01         0.12         0.09         0.07         0.15         0.20         0.11           BP-2         0.21         0.05         0.01         0.21         0.13         0.02         0.10           BP-4         0.67         0.19         0.01         0.13         0.02         0.09         0.01           BP-5         0.67         0.13         0.13         0.99         0.01           BP-6         0.22         0.34         0.13         0.22	Base	-				Rainfall Gau	ging Station					
0.05 0.01 0.12 0.09 0.07 0.15 0.05 0.05 0.01 0.21 0.13 0.09 0.20 0.10 0.01 0.30 0.10 0.02 0.02 0.19 0.13 0.13 0.13 0.34	Point	Bobok		Binalonan	San Nicolas	Balungao	Alcala	Tibag	-	Mangatarem	Matalava	
0.05 0.01 0.21 0.13 0.09 0.20 0.10 0.10 0.01 0.30 0.10 0.02 0.01 0.13 0.13 0.02 0.14 0.13 0.13 0.14 0.46	BP-1	0.16		0.01		0.09	0.07	0.15		0.11	0.04	
0.10 0.01 0.30 0.10 0.02 0.19 0.01 0.13 0.99 0.34 0.34 0.22	BP-2	0.21		0.01		0.13	0.09	0.20		•	•	
0.19 0.01 0.13 0.99 0.22 0.34 0.34	BP-3	0.47		0.01		0.10	0.02	•	•		1	
0.13 0.19 0.46 0.22	BP-4	0.67		0.01	0.13			•	•	•	•	•
0.34	BP.5		,		.1	•	•	•	0.99	0.01	`k	٠.
BP-7 0.66 - 0.34	BP-6	·			•	0.13	0.19	0.46	0.22	•	•	
	BP-7	0.66		1	0.34			•			•	: .

(1) Type A (Period: 1970-1976, 1978)

Base					Raint	fall Gauging St	tation				
Point		Adaoay	Sayangan	Bobok	Baguio	Baguio San Nicolas Binalonan Balungao	Binalonan	Balungao	San Miguel	Surgui	Matalava
۳. تو	1.19	1.39	09.0	1.15	0.55	1.55	1.00	1.13	1.29	1.16	1.25
P-2		1.39	09.0	1.15	0.55	1.55	1.00	1.13	1.28	1.27	ı
		1.39	09'0	1.15	0.55	1.55	1.00	1.16	s <sup>s</sup> .	1.00	•
P-4		1.39	0.60	1.15	0.55	1.50	1.00	•	•		
P-5		i.	•	· .: '				•	,	1.25	
BP-6	4	ı		r	•		,	1.13	1.28	1.27	ı
3P-7	•	·••	•	0.96	•	1.50	•			•	•

(2) Type B (Period: 1977, 1979 - 1980)

3986					Halfiie	Halfilail Gauging Station	lation	:			
oint	Bobok	Baguio	Тареуо	abeyo San Nicolas Binalonan Balungao	Binalonan	Balungao	Aicala	Alcala San Miguel Mayantoc Mangatarem Matalaya	Mayantoc	Mangatarem	Matalava
BP-1	1.08	89'0	96.0	1.54	1.00	1.14	1.00	1.26	1.17	1.20	1,25
3P-2	1.08	0.68	0.98	1.54	1.00	4.1	1.00	1.26	1.20		•
BP-3	1.08	0.68	0.98	1.54	1.00	1.18	1.00		•		•
3P-4	1.08	0.68	0.98	1.47	1.00		•	•	•	•	,
3P-5	•	•		; ·	•	,		••	1.21	1.10	,
3P-6	•	•	ı	:	, , ,	1.15	1.00	1.26	1.20	•	
3P-7	1.06		•	1.50	•			•	•	•	

(3) Type C (Period: 1981 - 1986)

Вазе					Rainfall Gauging Station	ing Station				
Point I	Bobok	Baguio	Binalonan	an Nicolas	Balungao	Alcala	Tibag	Mayantoc	Mayantoc Mangatarem Matalava	Matalava
BP-1	0.95	0.73	1:00	1.54	1.15	1.00		1.12	1,10	1.25
BP-2	0.95	0.73	1.00	1.54	1.15	1,00	1.23	1.24		
BP-3	0.95	0.73	1.00	1.54	1.24	1.00	•	•	ī	
8P-4	0.96	0.73	1.00	1.54	í		•		•	•
BP-5	,	•	ı	•	1	,	•	1.19	1,00	•
BP-6	,		ı		1.12	1.00	1.23	1.24	ı	
BP-7	0.95	•		1.50			•		-	

Table 4.9 (1/2) ANNUAL MAXIMUM BASIN MEAN 4-DAY RAINFALL AT RIVERMOUTH OF AGNO RIVER (BP-1)

(Unit:mm)

Year	Occurrence Date			-				Rinafa	11 Ga	uging	Stati	on		~~~~				Basin Mean
10.2		<b>,</b> 1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	
1970	Jun. 11	7.6	54.6	6.0	13.7	-	11.7	19.7	23.3	26.0	-	10.9	_	13.7	_	-	4.0	20.2
	Jun. 12	25.4	26.2	20.1	31.2	-	45.0	44.9	53.0	59.3	-	27.2	-	34.3	•	_	0.0	41.7
	Jun. 13			20.0		-	70.3	91.1	80.7	84.2	_	55.9	-	63.8	-	-	0.0	<b>80.</b> 8
	J.m. 14			22.0		_	52.5	41.3	48.8	54.6	-	18.1	-	22.8	` <u>~</u>	-	0.0	35.1
																		(177.8)
1971	Oct. 9	30.7	47.0	64.8	62.0	•	45.9	105.8	89.6	92.5	•	45.2	•	31.0	-	-	0.0	64.0
	Oct. 10	55.1	108.4	24.1	137.2	-	72.7	44.8	58.0	48.7	-	52.0	-	48.7	: 🗕	-	0.0	62.9
	Oct. 11	53.3	40.4	15.7	4.6	-				95.5		17.3	•.	24.4	-	-	0.0	54.0
	Oct. 12	61.0	3.0	<b>36.</b> 9	51.6	-	55.0	118.1	95.2	100.4	-	78.7	-	55.1	-	-	0.0	80.1
	1							: :		-								(251.1
1972	Jul. 17	69.4	100.2	53.8	243.6	-	479.6	190.3	177.5	150.9	-	115.3	-	140.5	-	-	83.3	175.0
	આ. 18	60.7	92.4	255.3	148.9	-	292.6	141.9	143.5	117.1	-	171.7	-	187.2	1 -	-	172.5	189.4
	ત્રા). 19	45.7	75.9	187.0	47.0	-	139.0	104.2	134.9	90.7		118.8	- ,	108.8	· -	-	132.1	123.6
	Jul. 20	0.0	0.0	78.3	50.5	-	144.6	102.0	70.6	89.2	-	70.3	-	119.6	-	-	142.6	112.2
									:	;					1.	. :		(601.1
973	Oct. 13	9.9	6.1	0.8	42.4	-				36.8	**	12.7	-	15.2	-	-	19.1	25.5
	Oct. 14	2.8		27.9		-		0.0			-	0.0	-	0.0	-		9.1	8.2
	Oct. 15	37.1		40.9				76.5		71.3		207.0	-	102.4	: =		46.7	114.8
	Oct. 16	21.1	22.4	15.0	41.4	-	74.5	36.7	7.6	39.9	-	20.9	-	33.8	<b>-</b>	-	14.0	37.5
																	<b>~</b>	(186.0
974	Aug. 14	_		30.4		-				31.7	-	40.9	-	40.2	- :	-	29,2	44.9
	Aug. 15			30.0		-				149.4	-	142.5	-	157.0	-	**	186.7	182.2 264.3
	Aug. 16			29.2		-				181.1	-	240.8	-	276.6	-	-	294.4	204.3 92.3
	Aug. 17	10.2	22.1	22.0	70.9	-	101.8	42.8	53.4	46.5	-	52.8	•	79.5	•	-	287.8	(583.6
												<b>56.</b> 5		70.7			63.6	71.7
1975	Aug. 10	67.0		76.2		-			50.3			26.0	-	78.7	-	-		21.0
	Aug. 11	76.5		79.8		-	39.4			63.2		0.3	-	5.9	-	-	5.3	6.7
*	Aug. 12	70.9		25.4		-		3.1		0.0	· : =	3.3	-	1.0	•	-	1.8 24.9	35.4
	Aug. 13	89.7	40.6	125.7	16.5	-	42.0	21.3	52.6	8.0	-	12.7	-	41.9		-	24.9	(134.7
	1									050.0		07.0		120.0	i		23.1	156.8
1976	Hay 22			59.7		-		105.7		250.2	-	97.0	-	179.9	•	-	دي. 103.9	139.8
	May 23			102.9		•		124.7		106.7	-	161.1	-	100.0	-	_	214.1	225.7
	May: 24			265.7		~		101.6		312.5	-	126.0	•	191.8	· <u></u>	-	150.1	164.5
	May 25	199.1	178.3	675.1	343.0	-	605.3	0.0	0.0	182.9	-	90.4	-	117.4	•	-	130.1	(686.9
977	હ્યા. 21	-	-	-		53.6		4 1		38.3	5.6	32.5	-	-	7.9	9.1		21.5
	Հմ. 22	-	-	-	22.9		14.0		30.5	6.3	9.4	6,9	-	-	6.6	7.6		13.1
	Jul. 23	-	-	-	82.6		216.0			74.4	3.6	8.9	-	-	19.8	22.8	11.7	61.2
	Jul. 24	-	-	-	38.4	62.8	42.8	26.9	.60,0	3.8	0.0	9.7		-	29.5	<i>5</i> 5.9	48.5	33,2
			_									<b>^</b>		10.0			2.0	(129.0)
978	Aug. 22			30.3	4.0	-		53.3		40.00	-	22.3	-	49.8	-	-	3.8	41.2
	Aug. 23			95.8		-	- 1		148.0		•	88.1	-	46.8	-	-	124.5	135.7
	Aug. 24			277.5		-	285.6	5.5			-	106.4	•	44.0	-	-	129.3	112.4 30.3
	Aug. 25	124.4	149.7	261.3	29.2	-	<b>33,</b> 0	13.0	1.0	8,6	-	13.5	-	4.6	-	. •	22.9	320.6)
				-														(320.0

Remarks : 1: Buguias 2: Adaoay 3: Sayangan 4: Bobok 5: Tabeyo 6: Baguio 7: San Micolas 8: Binalonan 9: Balungao 10: Alcala 11: San Miguel 12: Tibag 13: Sungui 14: Mayantoc 15: Mangatarem 16: Matalava

Table 4.9 (2/2) ANNUAL MAXIMUM BASIN MEAN 4-DAY RAINFALL AT RIVERMOUTH OF AGNO RIVER (BP-1)

(Unit:em)

	Occurrence Rinefall Gauging Station  Date											Basin Mezn						
eer	varte -	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	
1979	Aug. 13	· •		-	15.0	23.1	96.1	44.2	39.4	5.1	5.1	26.6		_	16.8	18.5	3.1	25.8
	Aug. 14	•	-	-	16.6	62.5	285.4	134.1	50.3	49.0	25.4	28.8	•	-	116.1	110.5	62.9	97.9
	Aug. 15	-	-	-	68.6	44.3	75.8	65.3	86.9	79.8	102.1	173.2	•	-			160.3	154.2
	Aug. 16	-	_	-	8.9	13.7	81.3	18.8	42.5	21.6	29.0	26.0	7	-	161.1	149.1	102.1	81.8
	,																	(359.7
1980	Nov. 3	-	-	-	22.9	0.0	2.0	0.0	0.0	14.7	0.0	0.0	-	-	0.0			4.0
	Hoy. 4	-	-	-					41.7					-		25.9		69.7
	Nov. 5	-	•	-	495.6				102.6			141.2	•	-			85.3	225.1
	Nov. 6	- '	-	-	44.4	4.6	99.5	0.0	0.0	12.2	1.5	0.6	-	-	0.0	0.0	31.5	10.3
																		(309.1
1981	Jun. 10	-	v, 🕳	-	48.2	_	47.4	16.0	15.0	18.0	21.6	•	60.8	-			45.0	38.6
	Jun. 11	-	-	-	25.4	-	52.7	16.6	50.1	17.8	0.0	-	61.2	-	43.7	48.0	45.3	38.5
	Jun. 12	-	-	-	<b>59.</b> 7	-	126.0	55.6	50.5	48,3	34.3	-	96.3	-	93.8	91.4	84.6	91.0
	Jan. 13	-	-	-	58.4	-	73.8	52.6	65.5	64,0	50,6	-	63.0	-	83.6	82.6	45.7	73.7
											•							(241.8
1982	Jun. 30	_	-	_	0.0	- '	64.4	0.0	4.1	67.6	9.9	-	55.5	•	21.3	23.4	41.1	24.3
	Jul. 1	-		-	16.5	_	101.8	36.0	50,6	0.0	30.0		110.4	-	42.3	46.5	101.6	40,9
	હ્યા. 2	-	٠	-	60.9	_	164.4	35.6	11.4	2.5	44.5	-	181.0	_	90.3	88.4	186.7	73.1
Jul. 3			-	_	28.9	_	116.0	13.2	16.7	0.0	0.0	_	134.2	_	85.9	84.5	130.3	59.0
																		(197.2
1983	Aug. 12	-	٠	-	93.2		145.4	40.2	52,6	18.1	19.6	_	42.3	-	43.7	48.0	31.4	60.8
	Aug. 13	_			79.5	٠	103.9	29.8	24.4	22.8	27.7	_	59.8	_	35.6	39.1	44.3	50.6
	Aug. 14	-	-	-	114.2	_	208.8	32,8	99.8	103.6	78.5	_	114.0	-	130.9	123.2	105.9	104.8
	Aug. 15	_	•	_	72.7	-	83.6	42.4	60.8	44.9	59.7	-	103.4	-	73.4	73.9	93.1	76.0
	_																	(292.2
1984	t 77				43.4		35.3	20.2	11.4	102 1	3,6	-	81.3	_	E4 2	<b>57</b> 4	66.6	47.8
1904	Aug. 27	, -	-	_	171.4	-	,	_	158.8				123.9	_			117.9	189.4
	Aug. 28	-	•	-	136.7	-			76.7				104.5	_			94.5	95.2
	Aug. 29	• •	· -	-	88.7	-		71.2			14.5		71.6	_			54.9	67.5
	Aug. 30	-	-	-	00.7	•	131,3	/1.2		14.6	14.0	-	71.0	-	73.0	73.5	J1.5	(399.9
1000	1- 20				52.2		62 A	24.7	0.3	26.0	88 4		36.0	_	- 34 5	39.6	26.7	41.4
1 <b>98</b> 5	Jun. 20	-	-	-	134.4	. •			226.8			-	59.0	_			43.7	116.2
	Jun. 21	•	-	-	145.9	-			106.2				56.7				42.0	128.6
100	Jun. 22	-	· •	-	95.4				60.2				65.9	-			48.8	103.2
	Jun. 23		-	-	90.4	-	132.2	100.0	UJ.Z	90.2	4.6				100.0	3/ .0	40,0	(389.4
	. 1 .				175.0		204:0	100 7	104 4		101 2		15Ė 0		112 0	100 7	169.7	208.3
1986	Jul. 8	-	-		172.2		1		104.4				166.9	-			121.9	205.3 154.3
	9 ابد	-	-		218.8				59.7				127.2 96.7	_			85.1	100.7
	Jul. 10		-	-	60.5				20.9									
	Jul. 11	•	-	-	3.7	-	3.0	19.7	0.0	4.12	23.5	-	0.0	-	8.7	10.0	0.0	11.3 (484.5
Remerks	: 1: Bugu			Adaoay			Sayang	:	4: Bo									
	5: Tabe	n	6:	Baquio	)	7: 5	San Nie	xolas	8: 8	na lon	3.71							

15: Hangataren 16: Hatalava

14: Hayantoc

13: Surgui

Table 4.10 (1/2) ANNUAL MAXIMUM BASIN MEAN 4-DAY RAINFALL AT RIVERMOUTH OF CAYANGA-PATALAR RIVER (BP-8)

(Unit:ma)

,		Occurrence	Ri	nəfall	Gaugi	ng s	itation	Basin	١.		Heen
	Year	Date	1	2	3	4	5	6	7	8	11001
	1070	Jn. 11	19 7	5.5	23.3	_	25 A	24.9			25.6
	1970	Jan. 12		121.0		_		54.9	_		63.4
* *** * * * * * * * * * * * * * * * *				163.3	4		145.2				95.9
100		Jan. 13	1. 5	118.5	4 4 2 7	_	58.9		-11	_	58,7
18 6 6 6		Jm. 14	32,.3	110.3	ioin		د,دد	73.3	77		(243.7)
1.7	1000	3.1 12	49 B	69.1	28.4		109.9	4.1	_		47.3
	1971	ડેમી. 17 આ 19		134.2			14.9			_	56.9
		Jul. 18			42.0	_	150.4	1	47	_	149.3
and the second		Jul. 19		30.9	100	17		51.0	4	_	108.7
1		Jul. 20	303.7	30.9	17	.,=	707+7	25.0	-	<u>-</u> .	(362.3)
*****		1.3 19	420 C	310.6	177 E		320 A	147,8	1 4		286.3
	1972	ວນໄ. 17				-		170.8	-	_	216.7
		Jul. 18		258.8	4.1				_	-	161.2
Sylvania.	4.0	Jul. 19		245.7	5.4	• * ;	10.00	156.8	-	-	124.7
9.2		Jul. 20	144.5	147.8	/0.5	•	253.2	183.4	7:	-	(783,9)
14.		1					25.2	ae a	. <i>1</i>		• : :
	1973	0ct. 6		54.4		-		25.2	-	-	27.8
f		0ct. 7	2.00	29.6		-	5.44	99.9		-	126.3
		0ct. 8		108.6	45.5	:		37,5	7	***	80.7
ingen en e		0ct. 9	32.5	4.1	1.7	, <del>*</del> 1.	17.4	11.2	7	<del>-</del> .	12.1
			A.		:				: ' '		(246.9)
	1974	Aug. 14	38.4	49.3	20.3	-		25.5	-	-	39.8
		Aug. 15		200.4		**	100	194.5	7	₹.	143.3
		Aug. 16	188.5	328.9	189.5	4. <del>-</del> , 1	371.5	260.0	<b></b>	-	230.0
		Aug. 17	101.8	121.6	53,4	-	155.1	103.4	η=	•.	87.9
4.0		100			1.6		- 41.1				(501.0)
	1975	Aug. 10	163.6	115.9	50.3	-	131.3	<b>68.1</b>	-	<del>-</del> ,	97.4
		Aug. 11	39.4	4.9	2.0	-	25.7	20.1		-	15.5
		Aug. 12	15.2	4.4	1.8	-	9.3	6.4	-		6.6
	٠.	Aug. 13	42.0	120.4	52.6	-	28.3	32.3	-	-	53.8
	•	7.5						3			(173.3)
100	1976	Jun. 213	109.7	115.2	47.8	<b>⊸</b> , '	11.8	33.1	-	-	65.5
		Jun. 29	333.7	180.4	92.0	-	64,8	79.9			159.8
70		Jun. 30	395.4	342.0	198.1	_	182.9	140.4	_ `	-	258.3
1.0		Jul. 1	75.9	57.3	23.6	_	55.5	14.5	-	-	44.7
*							4 1		:		(529.3)
		200				٠.				-	149.5
	1977	Sep. 15		158.6		-		92.7	-	•	95.8
		Sep. 16		180.7		-		60.7	-	-	
	٠.	Sep. 17			12,0	- :		57.9	-		28.1
		Sep. 18	115.0	40.6	16.7	-	85.9	33.9		-	53.4
1									,		(326,8)
	1978	Aug. 21		103.3		, <del>-</del>		42.6	-	-	47.6
		Aug. 22	29.4			-		2.8		-	12.5
		Aug. 23			148.0	-	4.14	169.7	-	-	259,8
		Aug. 24	285.6	221.8	119.2	. =	189.C	153.5	-	· <del>-</del> ,	183.1
											(503.0)

ing ang ang

> Remarks : 1: Baguio 2: San Roque 3: Binstonan 4: Alcala 6: Sta-Barbara 6: Dagupan 7: Matalawa 8: Mangatarena

Table 4.10 (2/2) ANNUAL MAXIMUM BASIN MEAN 4-DAY RAINFALL AT RIVERMOUTH OF CAYANGA-PATALAR RIVER (BP-8)

(	Unit	:	mn
---	------	---	----

	Occurrence	Rin	Rimsfall Gauging Station Basin							. Mean	
Year	Date	1	2	3	4	5	6	7	8	1201	
1979	Aug. 13	96.1	95.7	39.4	_	37.4	7.7	-	_	58.9	
	Aug. 14	2.0		50.3		206.9	47.0	-	-	137.1	
	Aug. 15			86.9		361.2	162.5		<b>.</b>	130.4	
	Aug. 16				٠_				-	91.4	
13										(417.8	
1980	Nov. 3	2.0	0.0	0.0		0.0	0.0	-	_ :	0.	
	Nov. 4	64.8	101.3	41.7	_	52.3	24.2			55.0	
	liov. 5	698.7	196.5	102.6	-	176.3	103.0		•	274.4	
	Nov. 6	99.5	0.0	0.0	_	0.0	0.0			25.4	
										(355.4	
1981	Jun. 10	47.4	36.5	15.0		81.0	43.6		<b>-</b> 1.	34.8	
	Jm. 11		116.6	50.1	·	97.0	52.8	<b>.</b>	-	64.2	
	Jun. 12	126.0	132.4	60.5		173.5	126.6		-	101.6	
•	Jun. 13	73.8	140.2	65.6	_	158.1	59.9		-	87.	
1.5										(288.0	
1982	Jun. 30	64.4	10.0	4.1	_	47.3	23.9	_ :	-	25.	
	Jul. 1	101.8	117.3	50.6		93.9	91.0	<b></b> :		77.5	
	Jul. 2	164.4	27.7	11.4		168.2	88.88	_		74.	
	Jul. 3	116.0	40.6	16.7		161.6	96.8	<u>.</u> :	<b>-</b> , ·	65.4	
K)										(243.9	
1983	Aug. 12	145.4	120.4	52.6		97.0	70.6	_	_	90.0	
	Aug. 13					79.0		<b>-</b> .	-	56.4	
Ž2	Aug. 14					229.2	41.0	_	-	152.	
	Aug. 15			60.8		142.9	82.0	_	4	85.7	
										(384.2	
1984	Aug. 25	33 A	134.7	62.0	12	12.9	40 F			56.4	
1304	Aug. 27			11.4	-	114.0			- <u>-</u> -	32.0	
	Aug. 28			153.8						239.8	
	Aug. 29			76.7		95.3				140.0	
'	rug. 23	21011	701.11	70.7	-	30.0	111.13	-		(459.6	
1985	Jan. 20	A2 A	0.2	0.3	11	80.1	76 E		+ 1	23.1	
1300	Jun. 21			226.8	7	158.9		-	•	244	
	Jun. 22		5	106.2	1			•	-	177.0	
1:	4 24	2 * * * * *		60.2	- -	183.3		-	- <u> </u>	106.4	
:	Jun. 23	132,2	132.0	W.2		100.0	32.0	-	-	(551.	
1986	Jil. 8	. 22/10	100 3	104.6		103 3	376.8			206	
1300		525.0			Ţ	193.3		-	- 24	201.5	
	Jul. 10			20.9	Ū	4 4	62.4			65.4	
				0.0	-		0.0	-	-	3.:	
	Jul. 11	2.0	0.0	0.0	•	4U.3	V.U	-	-	(477.2	
										(4///	

5: Sta.Bartera 6: Degupan 7: Matalava 8: Mangatar

Table 4.11 (1/2) ANNUAL MAXIMUM BASIN MEAN 4-DAY RAINFALL AT RIVERMOUTH OF PANTOL-SINOCALAN RIVER

	Occurrence	R	imfali	Gauci	ina S	tation	Basin	1		
Year	Date			-				-		Hean
		1	2	3	4	5	6	7	8	ف کرد جام سوی
1970	Jan. 11	-	56.6	23.3	54.6	35.4	24.9	4.0	17.5	30.8
	Jan. 12	•	121.0	53.0	25.2	88.5	54.9	0.0	43.8	47.7
	Jan. 13		163.3							69.0
	Jun. 14	-	118.5	48.8	38.6	58.9	45.3	0.0	29.1	40.4
		•								(229.
1971	0ct. 8		162.6							61.8
	Oct. 9		176.8							68.
	Oct. 10		128.5						76.1	64.
	Oct. 11	-	180.0	91.8	40.4	88.4	2.5	0.0	43.8	64.2
										(298.9
972	Jul. 16	-	109.1	44.9	93.6	154.3	31.2	49.0	80.5	72.
	Jul. 17	7	310.5	177.5	100.2	320.0	147.8	83.3	175.1	148.
	Jul. 18		253.8							138.
	Jul. 19	-	245,7	134.9	75.9	231.8	155.8	132.1	124.7	123.
										(578.)
1973	Oct. 5						0.0			8.
	0ct. 6	-:	54.4							36.
	Oct. 7						99.9			41.
	0ct. 8	-	108.5	44.7	40.7	110.8	37.5	37.9	55.6	44.
										(178.
974	Aug. 14	-	49.3	20.3	<i>7</i> 3.9	112.7	25.5	29.2	55.7	45.
	Aug. 15								127.5	134.0
	Aug. 16		328.9							164.
	Aug. 1.7		121,6	53.4	22.1	155.1	108.4	287.8	80.9	76.
										(526.
1975	Aug. 12	-	4.4				6.4			4.0
	Aug. 13	-	120.4							45.0
	Aug. 14	-					51.9			35.0
	Aug. 15		11.9	4.9	17.9	61.6	20.4	50.8	30.5	15.
			* *	÷						(131.
L976	Hery 22	-	0.0						78.3	31.
	May 23	-	0.0				29.9			76.
	May 24	•					285.5			126.
	Mary 25	-	0.0	0.0	178.3	351.6	368.0	190.1	193.1	89.
					1 .					(436.
977	Sep. 15		158.6	77.7	50.1	0.0	92.7	62.0	0.0	60.
	Sep. 16	-	180.7	92.2	29.1	0.0	60.7			61.4
	Sep. 17	.=	29.2	12.0	37.0	0.0				27.3
	Sep. 18		40.6							23.6
										(187.
978	Aug. 21	-	103.3	42.5	33.7	28.9	42.6	44.2	14.3	40.0
-	Aug. 22	,	3.2	1.3	63.7	31.3	2.8	3.8	15.5	21.1
	Aug. 23		265.7	148.0	99.8	142.5	169.7	124.5	73.7	125.2
	Aug. 24		221.8							117.9
										(367.4

б: Оадирал

Remerks ; 1: Baguio

5: Sta.Barbara

3: Binaloren

7: Matalava

4: Alcala

8: Mangataren

Table 4.11 (2/2) ANNUAL MAXIMUM BASIN MEAN 4-DAY RAINFALL AT RIVERWOUTH OF PANTOL-SINOCALAN RIVER

(Unit:mm)

Year	Occurrence Date	H	linafal'	l egné	ng:	statio	J Rgz.	in		- Mean
icar	DATE:	1	. 2	3	4	5	6	7	8	
1979	Aug. 13	-	95.7	39.4	35.8	37.4	7.7	3.1	18.5	41.3
	Aug. 14	•	116.9	50.3	83.9	206.9	47.0	62.9	110.5	79.8
	Aug. 15	-	172.6	86.9	63.7	361.2	162.5	160.3	198.6	112.6
	Aug. 16	-	103.3	42.5	21.2	274.5	141.4	102.1	149.1	60.4
1		:	F							(418.0)
1980	<b>Հա</b> լ. 18	-	14.3	5.9	26.0	23.0	5.4	20.3	11.4	12.2
	Jul. 19	-	164.3	81.4	0.0	16.4	3.5	7.9	8.1	44.8
:	Jul. 20	-	187.1	96.4	85.1	43.6	65.0	46.5	21.6	. 76.6
	Jul. 21	-	120.0	52.3	98.4	62.0	117.7	116.1	30.7	68.2
										(221.9)
1981	Jun. 10	_	36.5	15.0	83.2	81.0	43.6	45.0	40.1	38.9
	Jan. 11	_	116.6	50.1	50.0	97.0	52.8	45.3	48.0	57.0
	Jun. 12	•	132.4	60.5	86.4	173.5	126.6	84.6	91.4	79.6
	Jun. 13	-	140.2	65.6	86.2	158.1	59.9	45.7	82.6	68.1
5							1.5			(306.0)
1982	Jun. 30	_	10.0	4.1	0.0	47.3	23.9	41.1	23.4	14.0
	Jul. : 1	-	117.3	50.6	32.5	93.9	91.0	101.6	45.5	61.3
•	Jul. 2		27.7	11.4	86.7	168.2	88.8	186.7	88.4	61.7
	Jul. 3	-	40.6	16.7	56.9	161.6	96.8	130.3	84.6	48.2
ar Sec										(247.2)
1983	Aug. 12	_	120.4	52.6	93.5	97.0	70.6	31.4	48.0	61.2
	Aug. 13	-	59.3	24.4	90.6	79.0	53.6	44.3	39.1	52.8
	Aug. 14	-	192.3	99.8	98.0	229.2	41.0	105.9	123.2	97.7
	Aug. 15	_	132.9	60.8	89.2	142.9	82.0	93,1	73.9	73.2
	•									(355.3)
1984	Aug. 26	-	134.7	62.0	78.7	12.9	49.6	19.1	6.4	58.0
1	Aug. 27	-	27.7							44.1
	Aug. 28	-							118.4	135.0
•	Aug. 29	-	157.1	76.7	102.7	95.3	127.4	94.5	47.2	83.8
										(390.8)
1986	Jun. 20	-	0.7	0.3	84.8	80.1	76.5	26.7	39.6	34.1
•	Jun. 21								83.1	151.2
٠.	Jun. 22	-	202.0	106.2	104.7	187.3	85.3	42.0	99.3	98.0
	Jun. 23	-	132.0	60.2	94.0	183.3	52.0	48.8	97.0	67.1
11.		٠				-			•	(421.1)
1986	<b>մել.</b> 7	٠ ـ	0.0	0.0	10.9	0.0	25.0	0.0	0.0	12.6
	<b>ա</b> լ. 8	-	199.3		110.3	193.3	376.8	169.7	102.7	126.8
	Jul. 9		131.2	59.7	120.1	152.7	173.8	121.9	79,5	91.2
	Jul. 10	_	50.8	20.9	90.8	163.9	62.4	85.1	85.9	49.5
	** * 1				٠.		: 1			(340.2)

Remarks ; 1: Baguio 2: San Roque 3: Binalonan 4: Alcala 5: Sta.Barbara 6: Dagupan 7: Matalava 8: Mangataren

Table 4.12 PROBABLE BASIN MEAN RAINFALL BY BASE POINT

(Unit: mm)

And the state of t	Return Period (Year)												
Base Point	1.05	2	5	10	25	50	100	200					
l-Day				-									
BP-1	71	142	202	242	295	334	375	410					
BP-2	71	148	214	260	319	354	411	451					
BP-3	74	159	236	291	364	421	479	54					
BP-4	68	158	251	323	425	510	603	70					
BP-5	99	147	203	249	316	378	445	52.					
BP-6	64	140	208	256	320	369	420	47					
BP-7	88	178	268	338	437	519	609	70					
BP-8	90	176	246	294	355	401	447	49					
BP-9	81	138	182	210	244	269	294	31:					
-Day		• •	•					÷					
	•			in the second			٤,						
BP-1	96	216	326	405	509	590	674	76.					
BP-2	98	227	: 346	431	546	635	728	82					
BP-3	112	251	376	465	583	675	770	86					
BP-4	106	252	389	488	622	727	837	95					
BP-5	130	221	325	410	537	648	774	91					
BP-6	98	207	316	399	517	613	718	83:					
BP-7	124	277	415	513	643	745	849	95					
BP-8	142	282	400	480	582	660	739	81					
BP-9	116	227	319	381	460	519	579	64					
3-Day						v v s							
	* 1												
BP-1	110	263	408	514	657	769	887	1,010					
BP-2	118	277	426	533	678	792	910	1,03					
BP-3	130	302	462	577	732	854	980	1,11					
BP-4	133	308	471	588	746	869	997	1,13					
BP-S	130	268	421	546	733	896	1,080	1,28					
BP-6	116	252	397	512	681	825	984	1,16					
BP-7	145	330	500	621	783	910	1,041	1,17					
BP-8	168	337	478	574	697	791	886	98					
BP-9	144	277	385	457	550	619	689	75:					
I-Day	* 4 •				:								
	111					A22							
Bb-1	126	301	466	586	747	875	1,008	1,14					
BP-2	138	319	486	606	766	891	1,022	1,15					
BP-3	157	344	511	629	784	904	1,028	1,15					
BP-4	154	342	512	632	791	914	1,042	1,17					
BP-5	147	305	482	629	849	1,041	1,259	1,50					
BP-6	130	287	454	586	780	944	1,125	-1,32					
BP-1	177	374	545	\$64	818	927	1,059	1,18					
8P-8	199	378	521	617	738	829	920	1,01					
BP-9	157	308	433	517	625	707	789	87					

Table 4.13 STORAGE FUNCTION OF RIVER CHANNEL UNDER CONFINING DIKE CONDITION OF AGNO RIVER

Channel	St	orage	Punctio	n	Lag	•	Channel	Storas	e Function	<del></del>	Lag
No.		UIGHU	t unouzo	· <b>41</b>	Tine		No.		.,		fine
101	. <u> </u>		Р		(hr)			K	P	***************************************	(hr)
<u> </u>	19,26	4	0.659	· · · · · · · · · · · · · · · · · · ·	1.0		17.	147,595	0.669	<del></del>	
2	59,43	3	0.608		2.0		18	29,519	0.669	Q<550	1.0
3	84,85	0	0.624	, ;; <del>}</del>	2.0	- /		6,291	0.923	Q>550	
4	43,89		0.653	Q<1700	1.0		19	29,519	0.669	Q<350	2.0
	8	1	1.523	1700(Q				3,197	1.040	Q>350	
				(3000			20	38,147	0.662	Q<750	2.0
	20,25	0	0.824	Q>3000			•	4,000	1.000	Q>750	
5	26,05	3:	0.628	Q<1200	1.0		21	24,927	0.661	Q<400	1.0
		8		1200(Q				2,766	1.026	Q>400	
				₹2100		* 4	22		0.613	Q<1200	2.0
	13,10	7	0.769		:			82	1.673	1200(Q	
6	13,00			Q<1800	2.0				4.	(1700	
	49,84			Q>1800			1.1	55,783	0.789	Q<1700	
7	6,77			Q<5500	0.0		23	•	0.561	Q<900	
	19,79			Q>5500,	•			23,840	0.888	Q>900	
. 8	8,24			Q<3500	0.0		24.7	148,698	0.561	Q<900	1.0
•	19,10			Q>3500			- A 3		0.888	Q>900	
9	16,38		0.796	Q<1000	1.0		25	10,994	0.646	Q<550	0.0
•	43,89		0.653	Q>1000				1,200	1.000	Q>550	
10	13,22		0.664	Q(250	1.0		26	27,977	0.667		1.0
	1,44		1.079	250(Q				3,258	1.022	Q>400	
	*, * .	ě.		<450		4.	27	117,188	0.602	Q<200	3.0
	20,50	3		Q>450			• • •	52,488	0.745	Q>200	• • •
11	24,35			Q(310	1.0		28	234,375	0.602	Q<2300	3.0
••	29			310(Q			<del></del>	29,282	0.959	2300(Q	
		10.5		<700				:		(6000	
	49,87		0.602	Q>700				177,799	0.716	9>6000	•
12	165,88		0.620		3.0		29		0.632	• • • • • • • • • • • • • • • • • • • •	1.0
10	2		1.845	1200 <q< td=""><td>310</td><td></td><td>30</td><td></td><td>0.524</td><td></td><td>1,0</td></q<>	310		30		0.524		1,0
		•	110.0	<2000			31	203,125	0.602	Q<2600	2.
	161,94	Ę.	0.717	Q>2000			••	9	1.879	2600(Q	
13	46,87		0.602	4. 2000	1.0			•		<6000	
14	25,45		0.624		1.0-	_		69,409	0.834	9(6000	
15	31,06		0.671		1.0		32	266,778	0.632	Q<2400	
16	156,25		0.602	Q<1200	2.0		411	49	1.727	2400(Q	3.0
LV	42		1.444	1200 <q< td=""><td>a i v</td><td></td><td></td><td></td><td></td><td>&lt;5000</td><td>***</td></q<>	a i v					<5000	***
	14	U	1:777	⟨2300				113,225	0.817	Q>5000	
	219,47	0	0.653	Q>2300				714,000	41411	4.6666	
	613,41	J	A+089	#1490n		•					

Table 4.14 STORAGE FUNCTION OF RIVER CHANNEL UNDER CONFINING DIKE CONDITION OF ALLIED RIVERS

Channel	River	River		Lag Time		
No.	Length (Rm)	Slope	K P	(hr)		
Panto River				<del></del>		
1.	4.9	1 / 80	8,059 0.646	0.0		
2.	6.0	1 / 130	14,655 0.660	. 1.0		
3.	6.5	1 / 350	27,984 0.638	1.0		
4.	6.0	1 / 900	18,662 0.677	1.0		
5.	17.5	1 / 580	18,662 0.677	2.0		
6.	6.8	1 / 900	31,668 0.607 Q < 500	1.0		
٠.		•	10,198 0.784 Q > 500			
7.	12.5	1 / 860	52,107 0.628 Q < 600	2.(		
		- • • • •	21,041 0.760 Q > 600			
8.	3.5	1 / 860	19,753 0.653	0.6		
9	5.4	1 / 1910	35,333 0.626	1.0		
10.	18.0	1 / 1050	59,038 0.669	2.1		
11.	24.5	1 / 1870	96,318 0.672	3.(		
12.	9.5	1 / 1910	62,248 0.632	1.4		
13.	8.0	1 / 1500	24,138 0.712	1.(		
14.	7.8	1 / 1500	27,364 0.685	1.0		
15.	7.1	1 / 1500	34,333 0.626	1.6		
16.	2.5	1 / 1910	12,463 0.661	0.0		
	•					
Cayanga River						
1.	11.3	1 / 420	35,138 0.658 Q < 400	1.0		
			23,427 0.733 Q > 400			
2.	12.5	1 / 1090	68,667 0.626	2.{		
3.	14.0	1 / 700	57,078 0.656	2.(		
4.	10.0	1 / 1270	45,756 0.636 Q < 250	1.0		
		**	38,896 0.678 Q > 250			
5.	18.0	1 / 220	106,209 0.616	2.(		
6.	6.0	1 / 1270	36,868 0.637	1.0		

Table 4.15 STORAGE FUNCTION OF SUB-BASIN OF ALLIED RIVERS

			Coeff. of		
Sub-basin	Catchment	River	Punct	ion	Lag-time
No.	Area (Km2)	Gradient	K	₽	(hr)
P01	75	1 / 20	48.38	0.354	1.0
PO2	15	1 / 40	39.30	0.416	1.0
203	21	1 / 20	48.38	0.354	0.0
204	16	1 / 40	39.30	0.416	1.0
205	40	1 / 150	26.43	0.568	1.0
PO6	15	1 / 1470	13.33	0.971	0.0
P07	33	1 / 40	39.30	0.416	1.0
809	30	1 / 600	17.44	0.787	2.0
P09	34	1 / 900	15.44	0.866	2.0
P10	24	1 / 740	16.38	0.827	2.0
P11	44	1 / 2750	11.04	0.990	1.0
P12	10	1 / 1320	13.77	0.947	0.0
P13	54	1 / 400	19.69	0.715	3.0
P14	29	1 / 520	18.20	0.761	2.(
P15	12	1 / 1630	12.92	0.995	0.0
P16	39	1 / 700	16.65	0.816	2.0
P17	98	1 / 100	29,85	0.516	0.0
P18	80	1 / 1370	13.61	0.955	0.0
P19	8	1 / 1420	13.47	0.963	0.0
P20	83	1 / 2800	10.99	0.990	2.1
P21	113	1 / 610	17.35	0.790	3.0
P22	19	1 / 1390	13.55	0.959	0.0
P23	53	1 / 3600	10.19	0.990	2.0
P24	57	1 / 1520	13.20	0.979	0.1
P25	20	1 / 1610	12.97	0.992	0.0
P26	4	1 / 1450	13.38	0.968	0.6
P27	76	1 / 1500	13.25	0.976	0.0
P28	31	1 / 1610	12.97	0.992	0.4
C01	66	1 / 20	48.38	0.354	1.(
CO2	30	1 / 330	20.86	0.584	2.0
C03	48	1 / 470	18.76	0.743	1.0
CO4	55	1 / 90	30.81	0.504	1.
C05	17	1 / 20	43.38	0.354	0.0
CO6	44	1 / 380	20.00	0.707	1.0
C07	-38	1 / 210	23.89	0.615	2.0
CO8	180	1 / 30	42.84	0.389	3.0
CO9	67	1 / 30	12.84	0.389	1.0
C10	39	1 / 140	26.99	0.559	0.0
C11	34	1 / 600	17.44	0.787	1.0

Table 5.1 MONTHLY BASIN MEAN RAINFALL AT SAN ROQUE

(Unit: sm)

									5				_
YBAR	Jan.	Peb.	Mar.	Apr.	Hay	Jane	July	Aug.	Sept.	Oct.	Nov.	Dec.	Potal
1960	50	113	64	204	232	408	335	1531	441	186	37	5	3606
1951	Õ	0	125	76	210	471	774	566	389	152	83	1	2847
1962	Ō	5	26	83	144	223	990	574	557	91	77	ì	2772
1983	8	2	35	28	120	781	302	362	788	29	27	64	2548
1964	ì	ī	27	71	227	452	292	1220	579	376	276	431	3952
1955	- \$	ĝ	85	144	336	346	634	224	431	191	49	0 -	2455
1966	16	18	45	66	872	248	316	503	609	87	279	70	3127
1967	18	5	9	209	190	1108	707	1095	621	1140	244	2	5347
1968	12	Ŏ	56	139	301	349	1028	1697	1254	64	33	. 0	4932
1969	20	Ž	11	82	375	375	1277	147	647	300	59	22	3919
1970	46	16	73	115	380	572		665	648	446	158	63	3757
1971	8	26	69	120	290	699	1231	670	440	569	157	127	4405
1972	24	4	· 52	187	301	846		773	371	60	86	25	5143
1973	12	10	63	60	427	336		628	287	495	108	42	2737
1974	63	8	76	169	238	482		985	233	1089	280	55	3992
1975	27	6	43		282	207	195	629	389	268	10	46	2182
1976	18	11	149	63		1207	403	357	571	161	32	6	3946
1977	3	0	3		164	242	503	535	541	61	163	0	2218
1978	1	0	24		212	484	470	1105	551	449	28	47	3492
1979	Ó	Ö	2		290	177	487	418	263	153	22	29	1944
1980	2	Ö	39	36	400	90	715	244	431	256	-519	3	2796
1981	Ğ	Ö	0		155	535	919	599	380	150	200	3	3017
1982	Õ	27	22	99		300	557	596	201	182	58	15	2158
1983	3	4	. 3	ž	128	212	692	768	413	.116	50	Đ	2393
1984	28	Ö	27	117	385	250	286	1079	213	279	10	0	2674
1985	0	14	23	167	174	1075	255	845	338	274	~ 76	10	3252
1986	10	Û	0	7	471	218		670	475	135	50	17	2893
Rean	14	10	39	94	314	410	659	746	484	287	121	40	3278

Table 5.2 RECORDED MONTHLY RUNOFF AT SAN ROQUE

												(Unit: n	Unit: n/3sec)	
	YBAR	Jan.	Peb.	Har.	Apr.	Kay	June	July	Aug.	Sept.	Oct.	Nov.	Dec.	Hean
7	1960	30.1		15.5	19.9	30.3	74.8	84.8	441.9	112.9	80.9	27.4	14.8	79.5
	1961	25.0	25.2	23.2	22.2	29.3	43.2	184.6	135.4	157.1	106.3	46.1	40.7	68.2
2.	1962	27.1	20.4	29.1	31.5	43.5	36.3	181.2	170.0	243.8	105.0	44.8	44.9	81.5
	1963	48.3	38.2	35.3	28.1	22.3	153.7	112.3	132.9	347.6	92.0	36.7	18.6	88.8
	1964	17.2	19.2	10.0	24.1	17.1	21.4	64.7	508.5	255.3	282.2	102.9	57.0	115.0
	1965	14.1	9.2	13.6	10.4		33.4	193.6	167.2	129.7	116.4	29.9	16.0	61.7
	1966	7.9		8 1	8.6	229.4	172.2	156.8	178.6	244.5	60.0	54.4	58.5	98.9
	1967	0.0	9.6	52,6	* .		132.8	117.0	257.6	211.9	191.9	208.4	83.2	144.8
	1968	27.1		•	14.9		15.7	108.0	561.1	645.2	275.0	60.1	24.9	148.3
-	1969	24.4	20.4	21.2			63.9	213.7	244.8	350.5	188.3	58.2	18.2	105.3
•	1970	9.1		6.6			108.5	161.8	184.3	201.5	244 2	158.4	121.9	103.3
	1971	72.2	70.5	54.9	41.3	(7.8	84.3		270.9	240.6	350.0	71.2	23.1	127.9
•	 Kean	25.2	21.9	23.4	49.7	50.2	78.4	146.6	271.1	261.7	174.4	74.9	43.5	101.9

TABLE 5.3 RUNOFF COEFFICEINTS OF OBSERVED AND SIMULATED RUN OFF

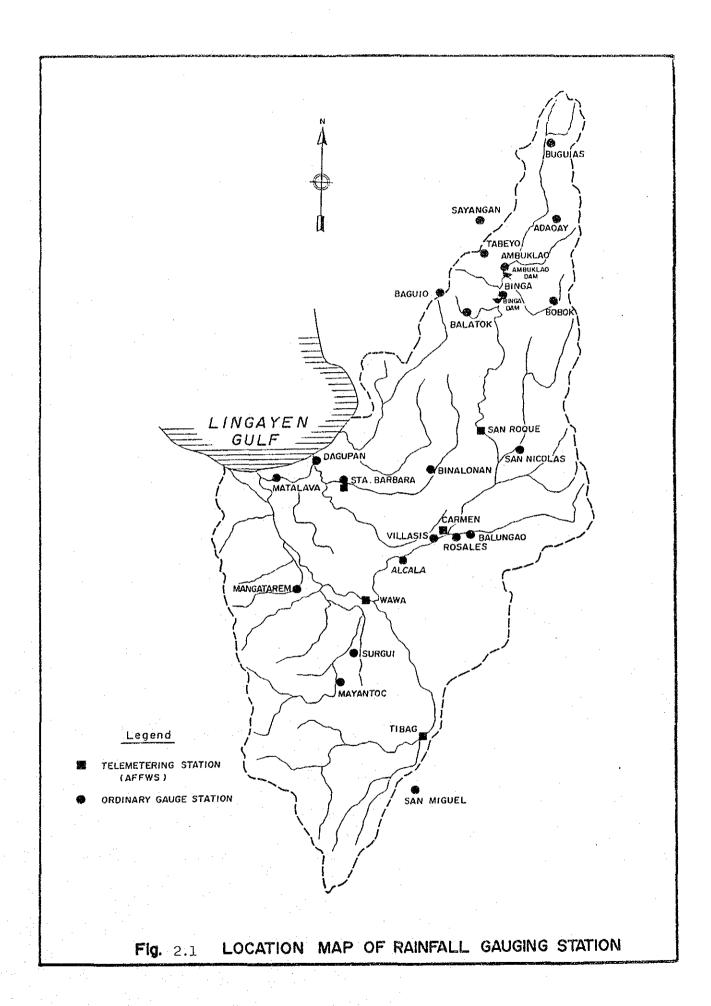
		Observ	ed	Simulate	Error	
YEAR	Basin Rainfall (mm)	Runoff (mm)	Coeff.	Runoff (mm)	Coeff.	(%)
1960	3,606	2,006	0.56	2,238	0.62	11
1961	2,847	1,721	0.60	1,993	0.70	16
1962	2,772	2,056	0.74	1,991	0.72	-3
1963	2,546	2,240	0.88	1,857	0.73	-17
1964	3,952	2,901	0.73	2,740	0.69	~6
1965	2,455	1,557	0.63	1,698	0.69	9
1966	3.127	2,495	0.80	2,124	0.68	15
1967	5,347	3,653	0.68	4,047	0.76	11
1968	4,932	3,742	0.76	3,787	0.77	1
1969	3,919	- 2,657	0.68	2,987	0.76	12
1970	3,757	2,606	0.69	2,730	0.73	5
1971	4,405	3,227	0.73	3,217	0.73	0
 lverage	3,639	2,572	0.71	2,617	0.72	5

Table 5.4 ESTIMATED MONTHLY RUNOFF AT SAN ROQUE

(Unit:m3/sec.	
---------------	--

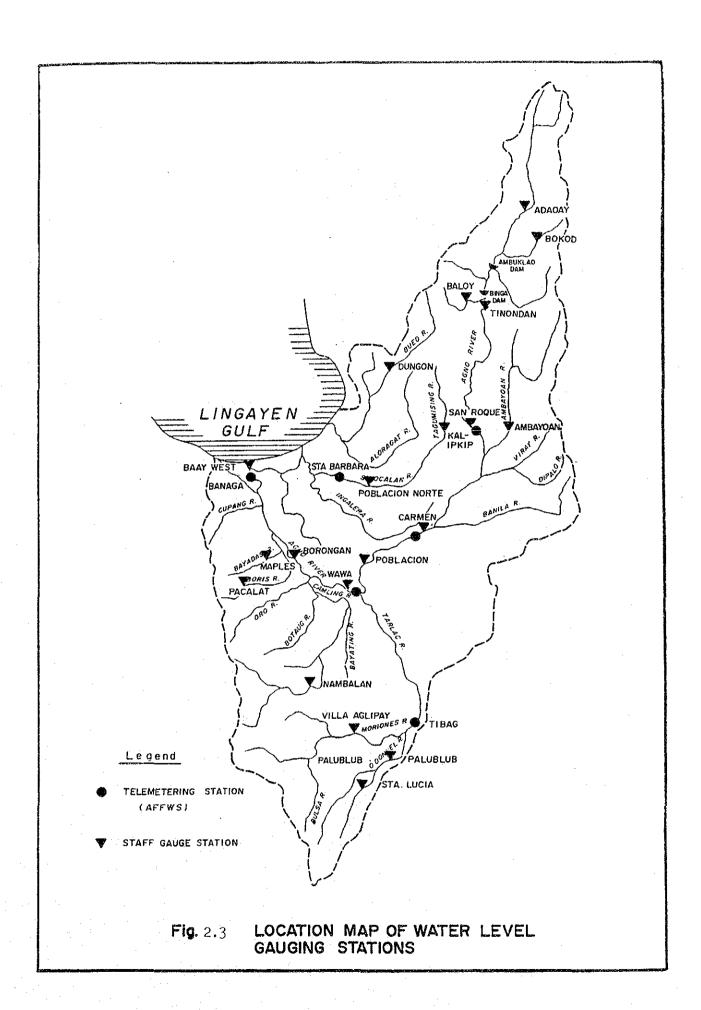
												1,,,,,,	,,,
YRAR	Jan.	Feb.	Mar.	Apr.	Kay	Jane	Jal.	Aug.	Sep.	Oct.	Rov.	Dec.	Kean
1980	30.1	21.1	15.5	19.9	30.3	74.8	84.8	441.9	112.9	80.9	27.4	14.8	79.5
1961	25.0	25.2	23.2	22.2	29.3	43.2	164.6	135.4	157.1	106.3	46.1	40.7	68.2
1962	27.1	20.4	29.1	31.5	43.5	36.3	181.2	170.0	243.8	105.0	44.8	44.9	81.5
1983	48.3	38.2	35.3	28.1	22.3	153.7	112.3	132.9	347.6	92.0	35.7	18.6	88.8
1964	17.2	19.2	10.0	24.1	17.1	21.4	54.7	508.5	255.3	282.2	102.9	57.0	115.0
1965	14.1	9.2	13.6	10.4	6.3	33.4	193.6	157.2	129.7	115.4	29.9	16.0	61.7
1966	7.9	8.0	8.1	8.6	229.4	172.2	156.8	178.6	244.5	60.0	54.4	58.5	98.9
1967	15.5	14.7	15.0	56.2	40.1	321.9	236.1	363.5	277.9	386.7	173.4	24.2	160.4
1968	18.4	18.1	18.5	25.2	66.1	94.5	259.6	476.4	550.4	217.4	36.1	20.9	150.1
1969	20.3	20.0	19.7	24.5	78.3	123.8	279.0	398.8	264.5	139.1	31.5	21.1	118.4
1970	22.5	20.4	23.0	25.2	86.3	191.6	163.7	216.8	274.8	175.0	70.9	27.8	108.2
1971	20.8	19.8	22.6	29.7	60.7	192.8	350.7	323.3	178.5	229.4	53.1	38.4	127.5
1972	27.4	21.1	20.8	39.7	63.7	227.4	673.7	192.6	203.4	72.2	29.6	23.5	157.9
1973	23.1	22.8	24.0	22.9	96.9	106.3	95.8	172.3	146.3	173.2	47.5	24.0	79.6
1974	23.0	21.4	24.3	36.3	40.1	155.8	101.9	274.8	159.9	232.2	189.0	44.5	114.5
1975	22.0	20.7	21.1	21.3	53.9	61.7	61.5	175.7	150.5	105.5	32.7	20.7	62.3
1976	19.9	19.5	19.3	20.8	216.2	333.9	313.9	166.0	191.8	100.2	25.4	20.7	120.6
1977	20.4	20.1	19.8	19.5	34.5	61.1	132.2	181.0	204.1	68.8	48.6	19.2	69.1
1978	18.9	18.6	18.4	21.4	34.8	143.7	136.9	323.1	273.2	162.2	58.8	22.3	102.7
1979	19.1	18.2	18.5	18.3	57.5	71.1	113.3	175.1	93.1	80.5	18.3	18.5	58.5
1980	17.6	17.3	17.4	19.7	83.3	50.3	166.4	122.9	140.8	86.9	212.4	25.3	80.0
1981	16.9	16.7	16.4	17.8	23.1	134.3	217.8	280.0	158.4	79.4	51.7	22.9	87.1
1982	16.8	16.6	16.3	22.1	22.6	55.5	154.3	195.1	117.7	62.9	19.2	16.0	\$9.8
1983	15.8	15.0	15.3	15.1	32.9	45.6	188.0	265.2	153.7	71.7	22.7	15.6	11.4
1984	17.2	15.1	15.9	20.1	88.8	73.1	82.8	247.1	198.3	87.8	33.2	15.4	74.6
1985	15.2	14.9	14.8	26.7	36.6	223.3	205.4	248.7	173.5	85.5	34.2	15.8	91.3
1986	15.5	15.3	15.1	14.9	90.5	99.6	253.5	182.6	238.7	73.1	20.2	15.1	85.3
Nean	20.6	18.8	18.9	23.8	62.4	122.9	190.9	259.8	209.3	133.1	57.4		95.3

## **FIGURES**



	Children of the Owner,	and the second second	double.	ة الإدام <sub>ال</sub> ي			-		-	****	*****			-		ya Dikar	Alaska PC		*****			******	-			**************************************
	Recorded Period	13	7-	8	6.	11	29	10	27	1.1	10	17	24	19	14 7	18	20	15	<b>o</b>	-£	10	14	7	7	7	7
	88 28 98 78		et me						+++					+++					<u> </u>							
	980 18 18 58							I						+++							Ī	1		1		L
Availability	67 87 87 87 87							+	+++		+			++++					Ŧ							
Data Av	99 17 27		++++									+		++-		<u>+</u>					<u>t</u>					
	89 29 99 99 79																					1				
	63 61 19 1360						1								, ,					7			, 	y ( .		, i i
-	Record	Dally	Daily	Dally	Daily	Dally	Dally	Dally	Dally	Dally	Daily	Daily	Dally	Daily	Daily Hourly	Dally	Daily	Daily	Daily	Dally	Daily	Dally	Hourly	Hourly	Hourly	Hourly
	Elevation (MSL)	1,316	816	2,286	735	1,723	1,483	588	1,367	950	•	•	5	•	•		,	-	,	•	-	•	•	•	•	
tion	Long.	120°50'00"	120°45'00"	120°40'00"	120°45'00"	121°00'00"	120°36'00"	120°43'46"	120°50'00"	120°39'00"	120°45'00"	120°35'00"	120°20'00"	120°14'00"	120°42'04"	120°42'14"	120°37'42"	120°21'00"	120*17'30"	120°25'00"	120°27'50"	120°38'00"	120.41.07"	120°35'34"	120°26'50"	120°34'09"
Location	Lat.	16.43.00"	16°38'00"	16°32'00"	16°29'00"	15°49'00"	16°24'00"	16"23"21"	16°27'00"	16°22'00"	16°01'00"	16.03.00.	16°03'00"	16.02.00"	15°59'47"	15°54'00"	15°53'36"	15°50'40"	15.47.30*	15°51'00"	15°36'20"	15°27'00"	16.02.37	15°53'24"	15°46'18"	15°29'14*
	Station	BUGUIAS	ADAOAY	SAYANGAN	AMBUKLAO	TABEYO	BAGUIO	BINGA	жовоя	BALATOK	SAN NICOLAS	BINALONAN	DAGUPAN	MATALAVA	STA. BARBARA	BALUNGAO	ROSALES	ALCALA	MANGATAREM	SURGUI	MAYANTOC	SANMIGUEL	SANFOCUE	CARMEN	WAWA	TIBAG
	<u> </u>	E	٥i	3	-	5.	9	~	83	6	6.	Ξ	12.	6.	4	15.	9	2	18	<u>6</u>	33	23	22.	23.	24.	25.

Fig. 2.2 DATA AVAILABILITY OF RAINFALL RECORD



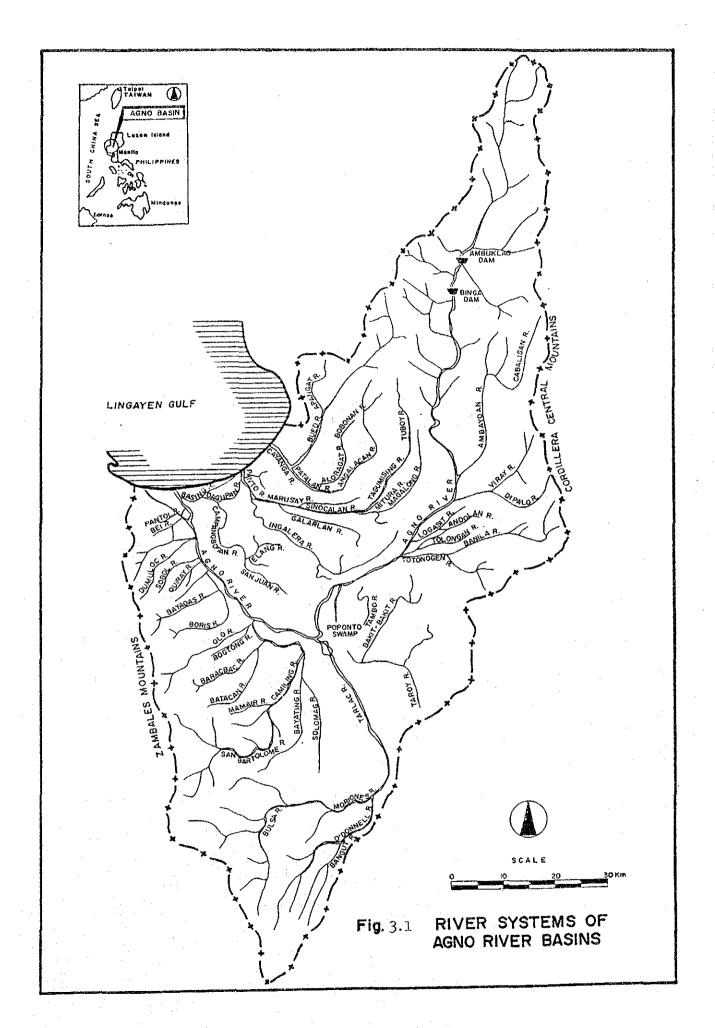
## .

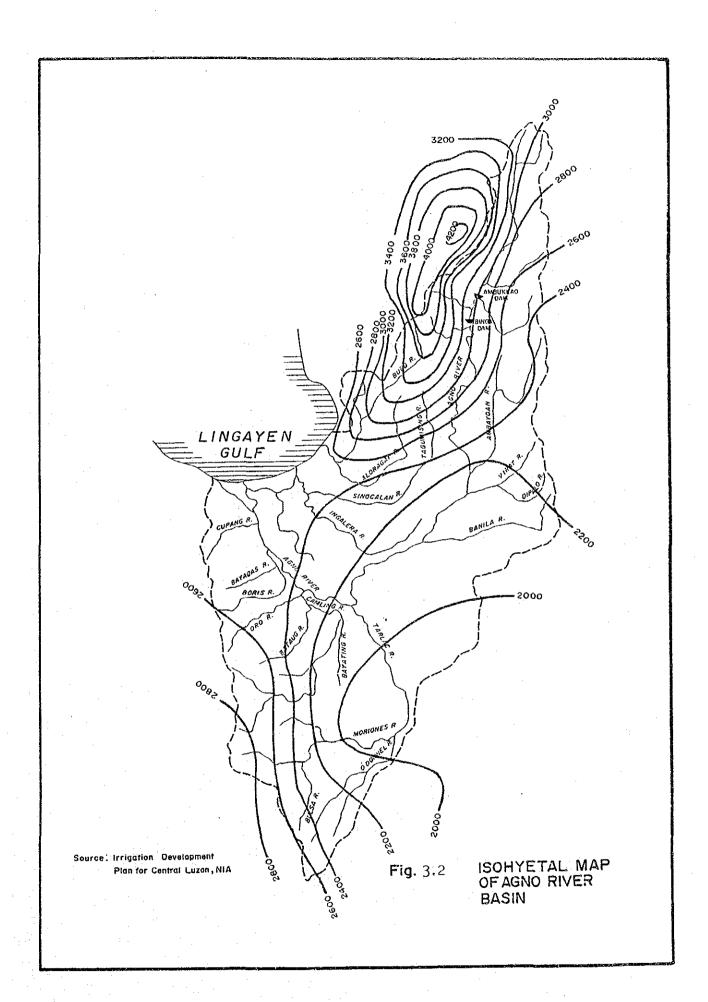
F								·	······			~~~									·				
		Recorded Period	11	13	ဖ	o	12	12	11	12	- 10	ത	ဟ	10	<b>*</b>	6	80	œ	12	12	6	ന	တ	6	
ŀ		88			_			-	-																
		7.8 8.8																				:		-	=
ł		98 98 78 83																							
İ		98													_										
-		78		VIII COMPANY			:				_		_					_		-		-		-:-	
ļ		ЕВ							:															٠	
		82			<u> </u>				:													:		-	
Į		1980														-							•		
1		1980																							
-		64	<u> </u>		_				·							-									
ĺ		87	-							-			_					_							
ı	<u>.</u>	77			-											-		_						-	
1	5	97	-	_				_									-			_					
١	d	12	ļ																		-				
1	Availability	27 23		_									Н	-	_	-	Н				-				
1		72	-	1	-			-	$\vdash$	$\vdash$	7		H	1	7	-			$\vdash$		-	<b>T</b>			$\dashv$
-1	Data	12-	1	-		H					1	-	-1-	$\top$	+	H	HH	-1-			1	1	_		
ı	Ω .	0261	1		H	+		-1-			1			-							Т				
1		69		1	Н																	П			
Ì		89				T	1	1			T			1											
١		۷9					П							1											
ı		99		П																					
ł		99																L	L	4		_	Ш	LL	
- 1		<b>79</b>				L	Ш		$\perp$		L					Ш			Ц.	Ш	Ш	Ш.,	Ш	Щ	
Į		£9					Ш		Щ	Ш		_		$\perp$	Щ	<u>L.</u>		_	1	4	LL,			4	_
į		62 61	Ш.	Ц.			Ш	4	1	Ц.	Ш			1	L		<u> </u>			<b>.</b>				1	
1		19		1			4	4	4	Щ			-			<u> </u>	H	_	4	-	<u> </u>		_		$\overline{}$
-		0961	Ļ	J.	Н	_	Щ	L	1	1		-	Н					-			-	_		-	$\dashv$
	Drainage	Area (km²)	246	48	87	958	1,225	281	2,209	2,284	405	240	06	141	180	74	5,646	5,564	6.4	5,134	117	4,196	142	872	
		River	Agno	Bokod	Twin	Agno	Agno	120°46'50" Ambayoan	Agno	Agno	Tariac	Tarlac	Tarłac	Bued	Sinocalan	120°38'18" Sinocalan	Agno	Agno	20°15'00" Bayaoas	Agno	20°15'29" Camiling	Agno	20°19'48" Camiling	Tariac	120°42'04" Sinocalan
Ì		7	5	5	5,	7:	2.	.0	6	2.	<u>ئ</u>	,	-	į.	.0	60	50	6	6	<b>*</b> 2	6	8	œ	ь	4
	Location	Long.	120°49'00" Agno	120°50'00" Bokad	120°32'22" TWin	120°43'17" Agno	120°41'45" Agno	120°46'5	120°35'30" Agno	120°27'22" Agno	120°26'56"	120°30'05"	120°29'11" Tarlac	120°30'50" Bued	120°28'20"	120°38'1	120°12'30" Agno	120°13'19" Agno	120°15'0	120°19'32" Agno	120°15'2	120°26'28" Agno	120°19'4	120°34'00" Tariac	120°42'0
	Loc	Lai.	26°35'00"	16°29'00"	16°23'08"	16°23'06"	16°08'07"	16°07'10"	15°53'30"	15°49'07"	15°28'06"	15°23'47"	15°22'10"	6°14'50"	16.00.00"	16°07'36"	16-00.39	15°59'42"	15°49'24"	15°49'23"	15°44'03"	15°45'50"	15°32'42"	15"29'55"	15°59'47"
		<u> </u>	<u> </u>	-		<b>V</b>	-			***	-		-			_		٦	-	-	-	***	一	<u> </u>	
	e e	Name	ADAOAY	BOKOD	BALOY	TINONGDAN	SANTOCIUE	AMBAYCAN	CARMEN	POBLACION	VILLA AGLIPAY	PALUBLUB	STA. LUCIA	DUNGON	POBLACION NORTE	KALIPKIP	BAAY WEST	BANAGA	MAPLES	BORONGAN	PACALAT	WAWA	NAMBALAN	TIBAG	STA, BARBARA
	<del></del>	2	-	c,	6,	4	5.	9	7	80	G	10	=	12	55	4.	15.	16,	17.	189	19	20.	21.	25.	23.

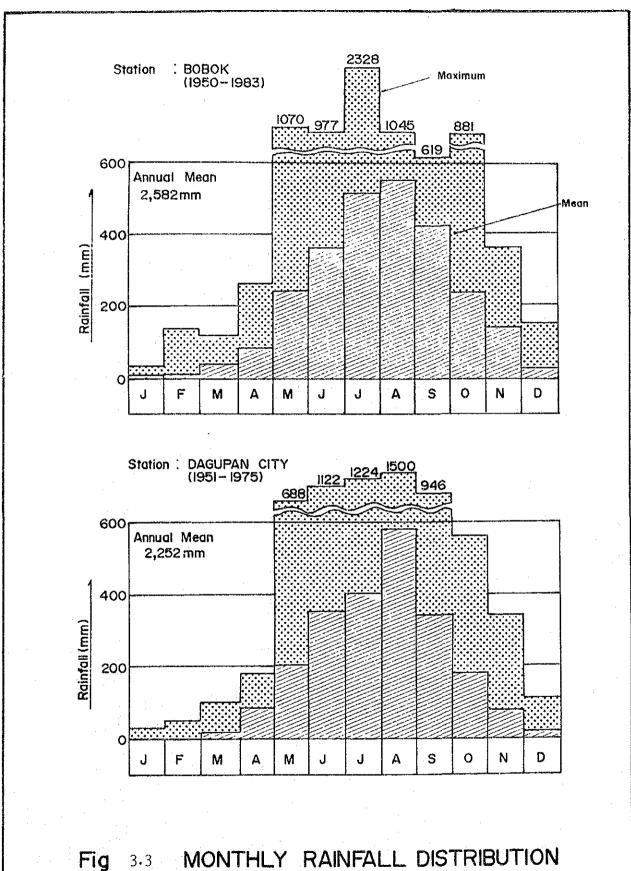
Remarks;

--: Daily Water Level ...... 3-hourly Water Level (AFFWS)

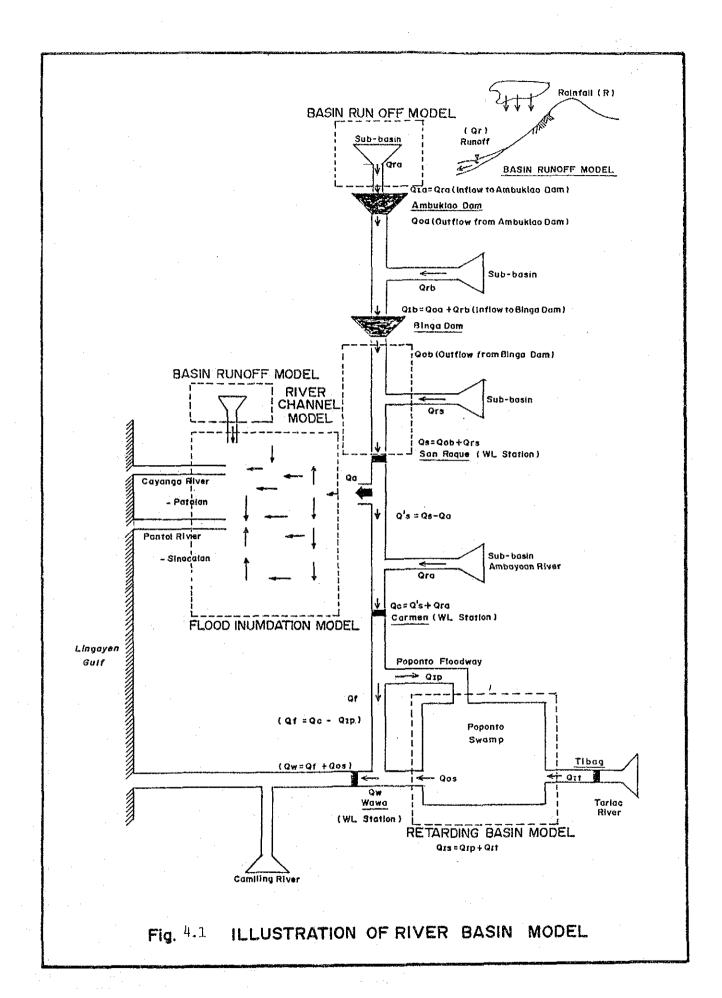
Fig. 2.4 DATA AVAILABILITY OF DISCHARGE RECORD

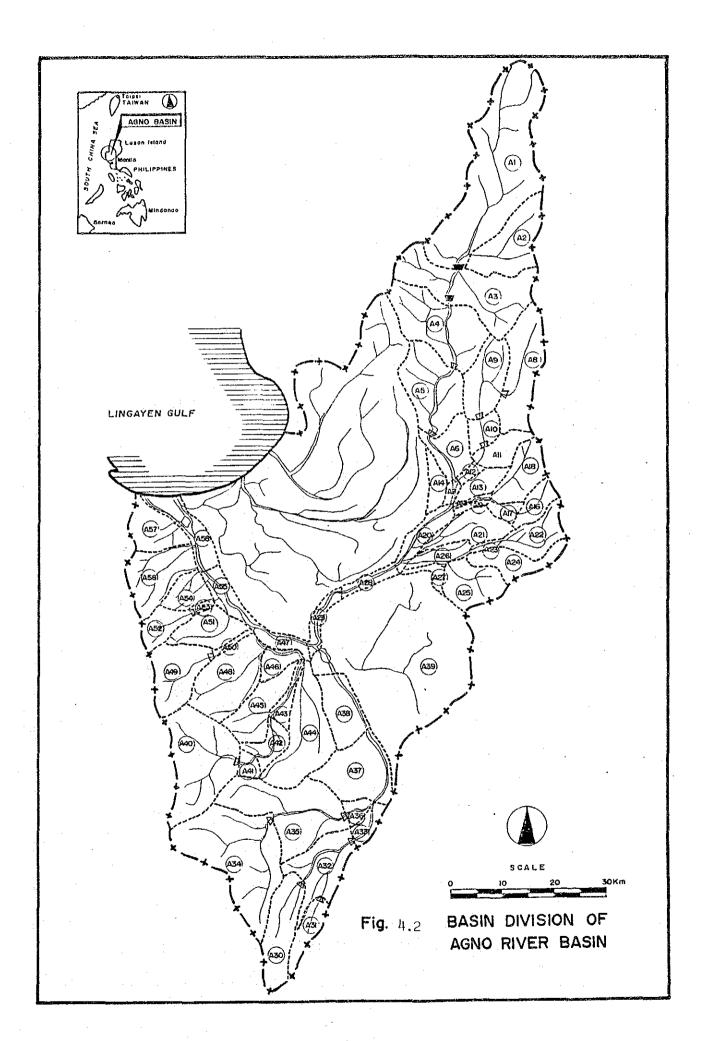


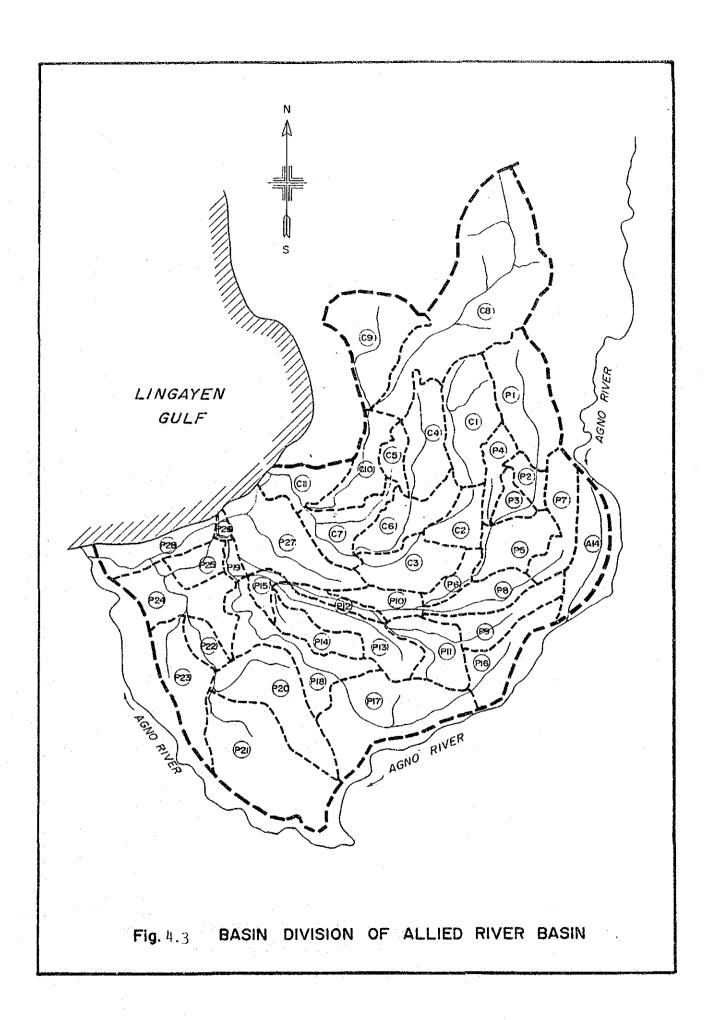


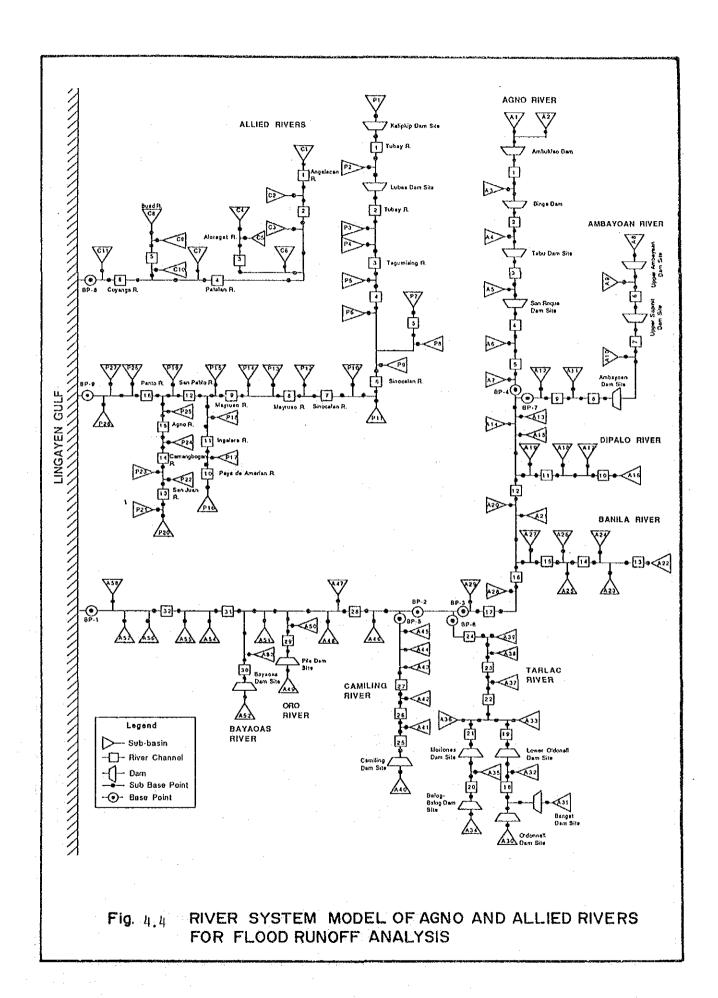


3.3









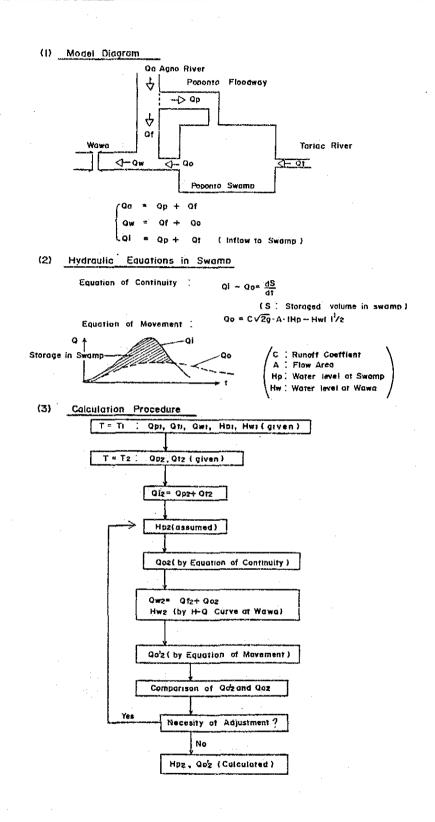


Fig. 4.5 ILLUSTRATION OF HYDRAULIC MODEL FOR POPONTO SWAMP

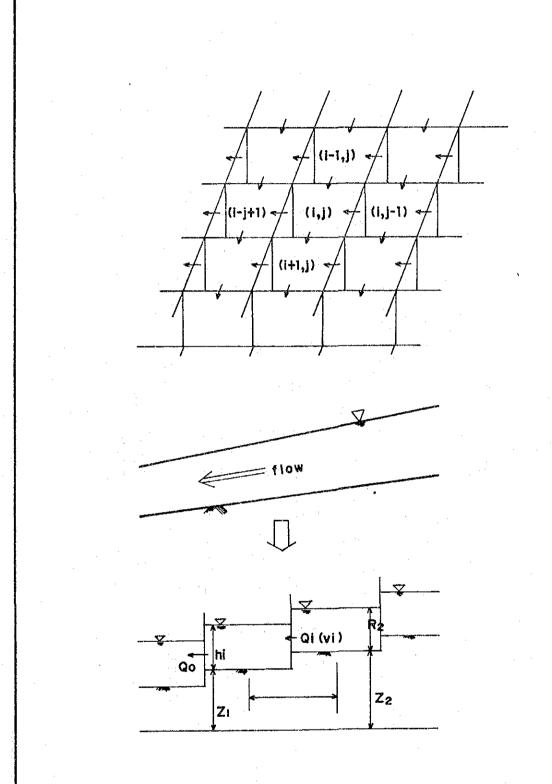
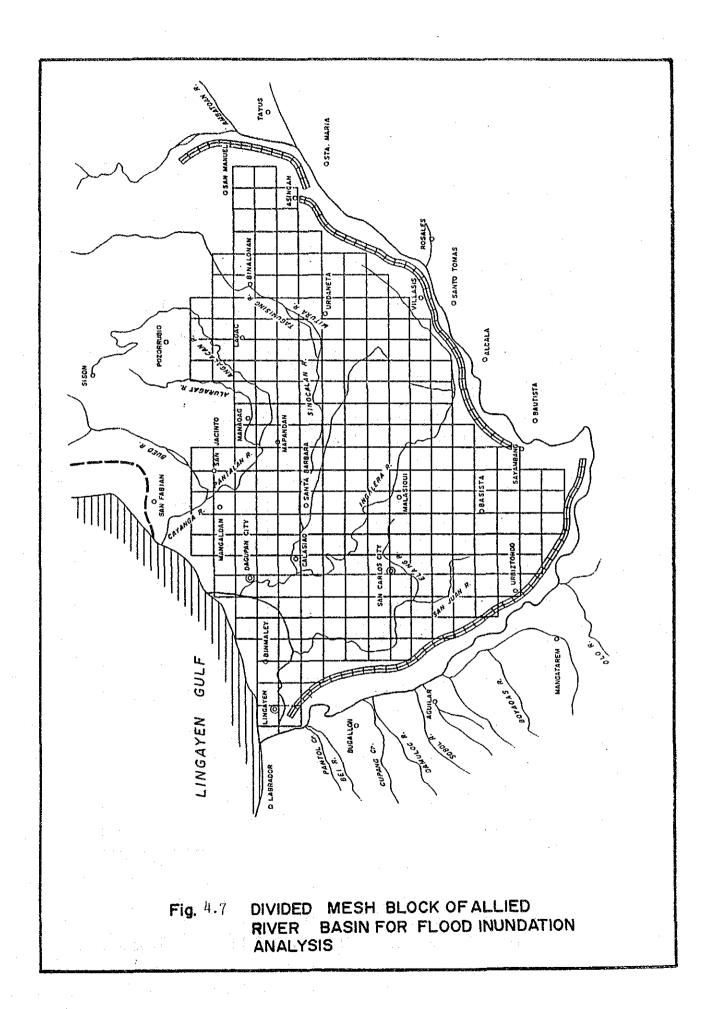
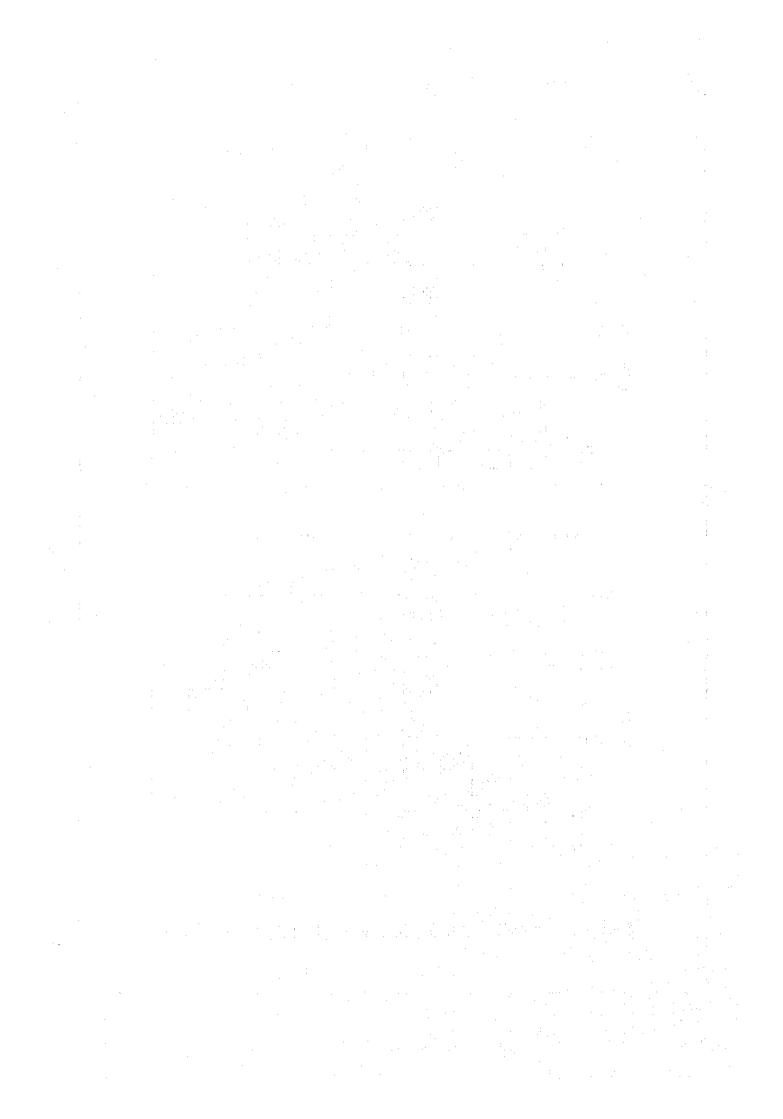
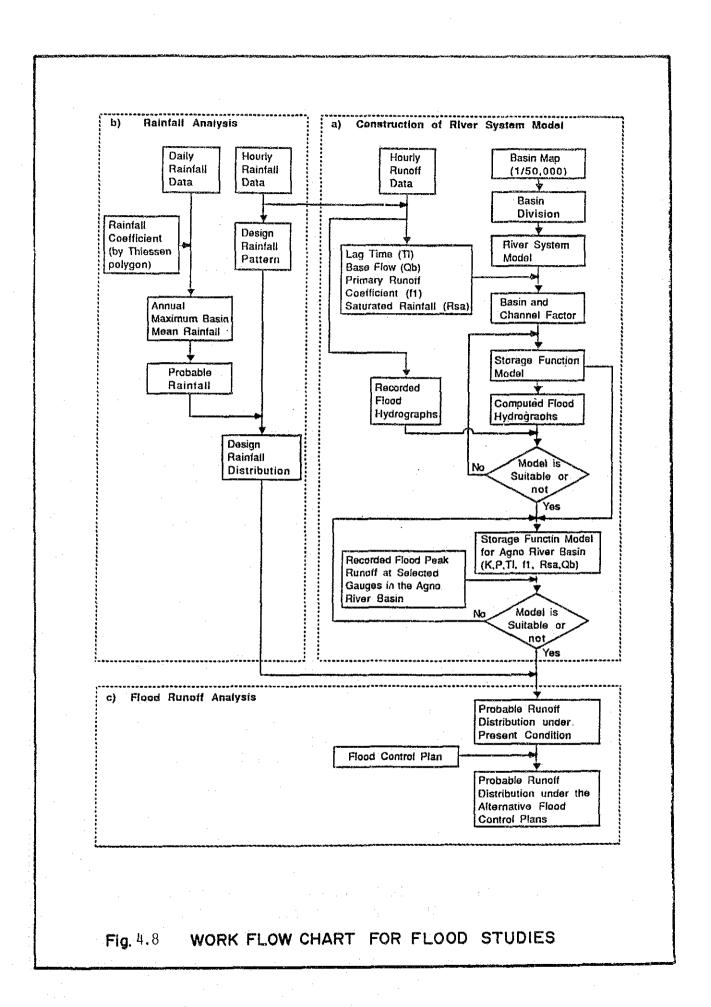


Fig. 4.6 ILLUSTRATION OF SEQUENTIAL MODEL POND







-HY.71-

· The Company of the Compa

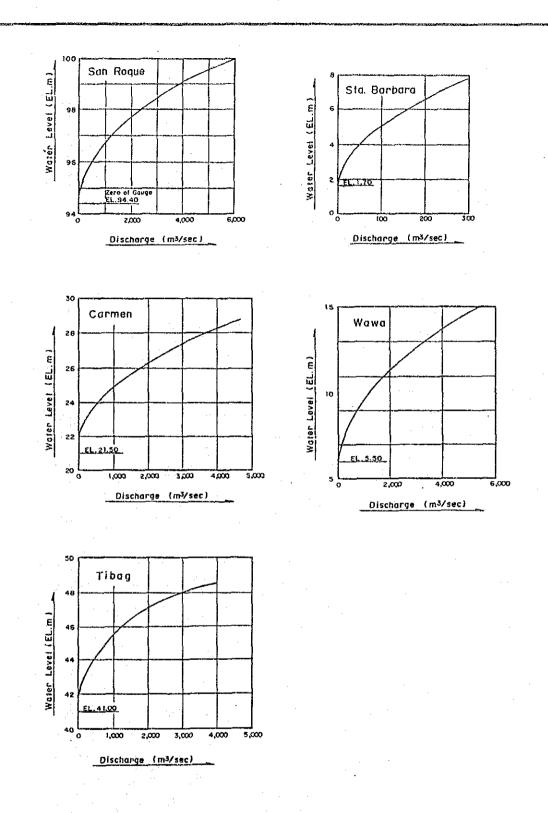
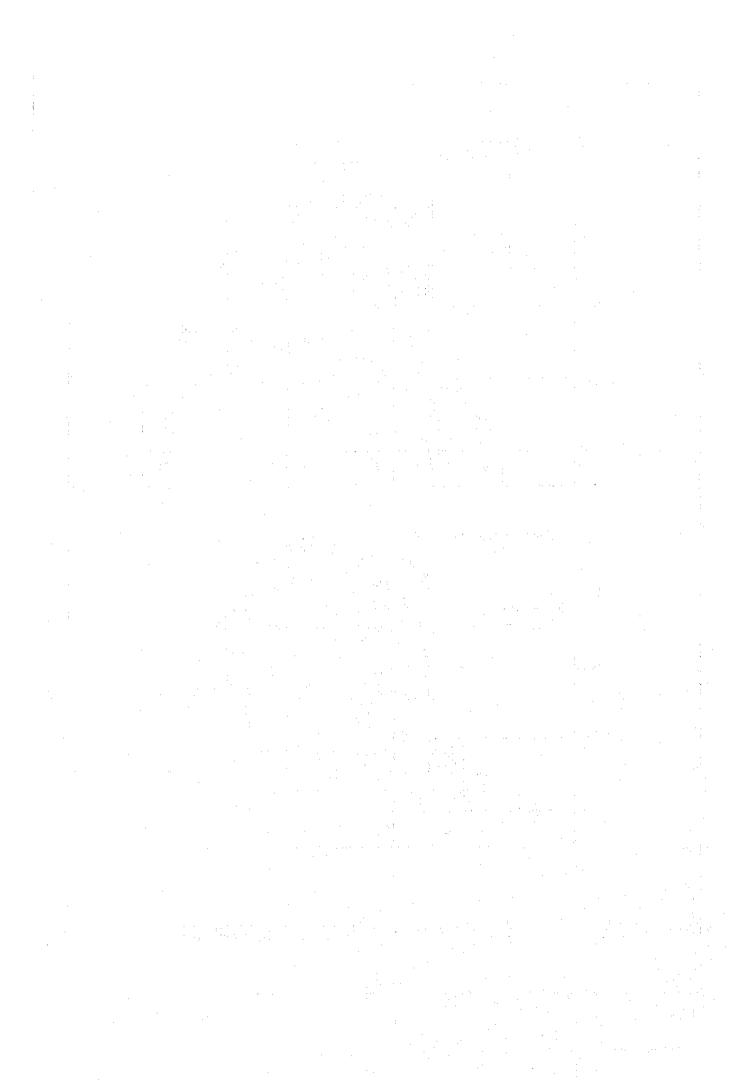


Fig. 4.9 DISCHARGE RATING CURVES AT TELEMETERING STATION



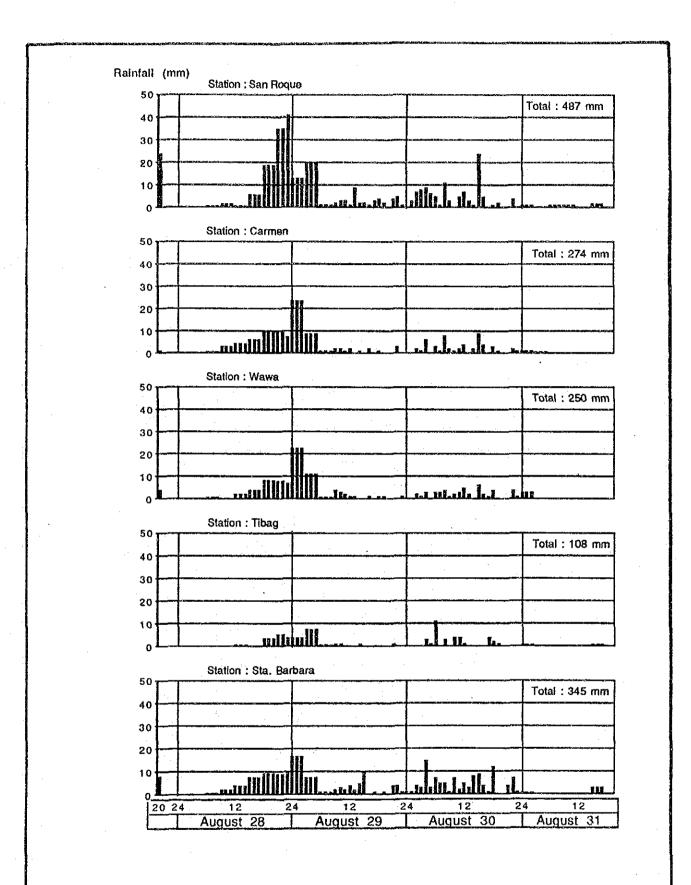
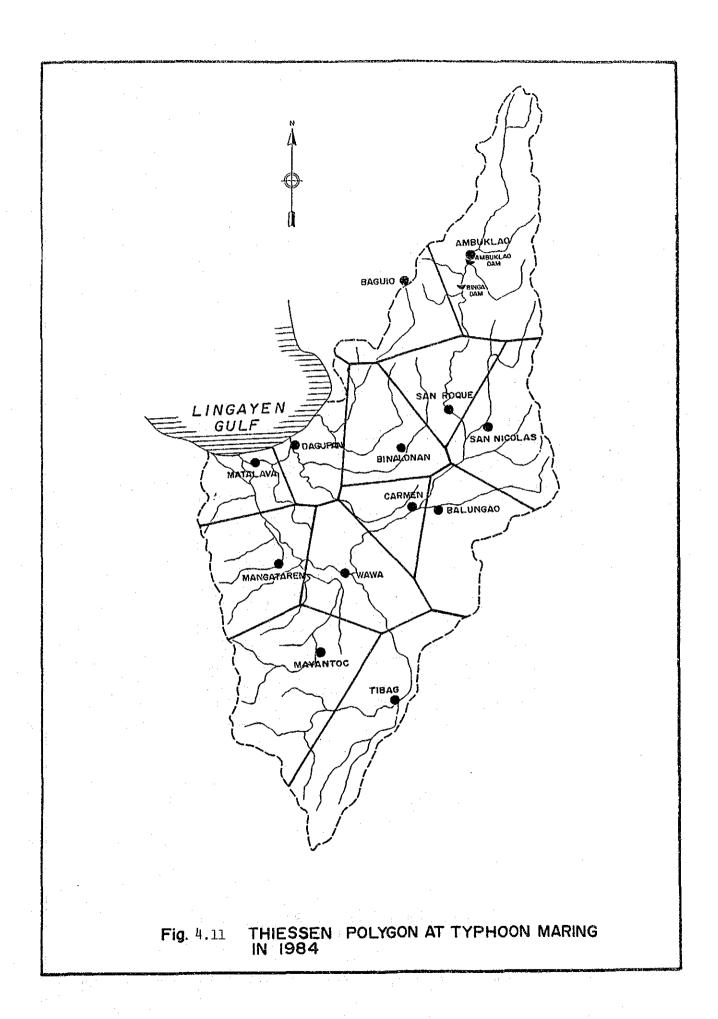
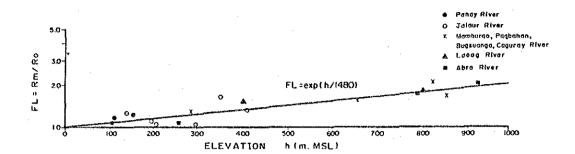


Fig. 4.10 RECORDED RAINFALL HYETOGRAPHS
DURING THYPOON MARING IN 1984

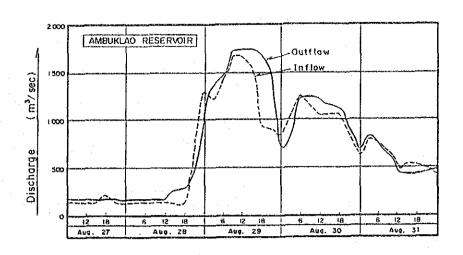




RIVER NAME	STREAM GAGING STATION	DRAINAGE AREA (A:Km²)	Q ann/A (mm/yr)	RUNOFF RATE	Rm (Qana/fi A} (mm/yr)	۴L (Rm/Ro)	AVERAGE BASIN ELEVATION (m,MSL)	Ro (mm/yr)
> 02	STA. RITA CUARTERO	880	1780	0.7	2540	1.20	158	2120
PANAY	PALAGUIAN MAAYON	265	1480	0.6	2470	1.16	120	2 120
9.52	TUMALALUD MAMBUSAO	307	1350	0.6	2250	1,06	111	2120
0.	ALIBUNAN CALINOG	120	1990	0.8	2490	1.28	418	1940
RIVER	SIMSIMAN CALINOG	169	2490	0.8	3110	1.60	359	1940
) E	POBLACION, PASSI	534	1450	0.6	2420	1.25	180	1940
=	PADER, DUENAS	247	1390	0.7	1990	1.02	295	1940
ALAUR	SAN MATTAS DINGLE	1065	1240	0.6	2070	1.07	193	1940
N P	MINA, POTOTAN	186	1170	0.6	1950	10.1	213	1940
	CALYAN POTOTAN	1499	1420	0.6	2370	1.22	156	1940
RAO R.	CABACO ABBA DE LLOG	189	3251	0.8	4064	1,59	8 33	2555
PAGBA- HAN R.	TALABIAN, MAMBURAO	263	3560	0.8	4450	2.00	844	2229
BUGSU-	BATASAN SAN JOSE	434	2723	0.7	3890	1.50	662	2590
CAGU-	OTOYAN SAN JOSE	136	2688	0.8	3360	1.25	270	2698
ERG	POBLACION L A O A G	1355	2214	0.7	3163	1.49	401	2117
LAOAG RIVER	MANALAC SOLSONA	73	2723	0.8	3404	1.77	804	1928
1	BANADANG BANTAY	4813	2512	0.6	4 187	1.67	779	2513
ABRA RIVER	PANG - OT LAGAYON	664	3619	0.7	5 170	1.97	952	2620
4 ₹	LINGSAU PENERUBIA	120	2295	0:8	2869	1.03	267	2780

Source: Nationwide Flood Control Plan

Fig. 4.12 ADJUSTMENT FACTOR FOR BASIN MEAN ELEVATION



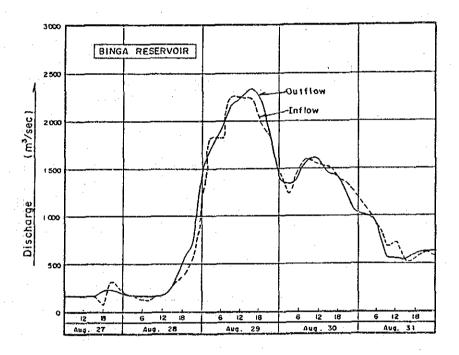
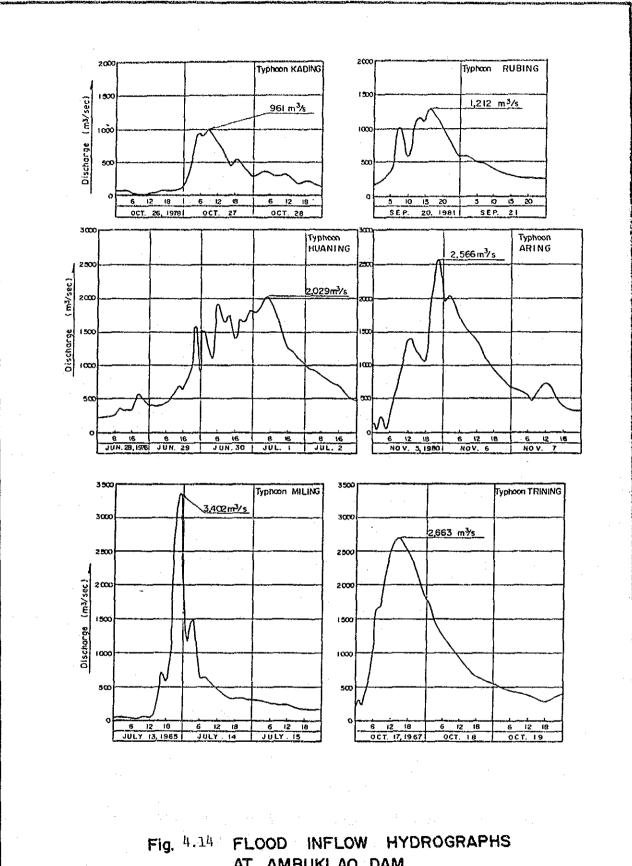


Fig. 4.13 RESERVOIR OPERATION AT BINGA AND AMBUKLAO DAMS DURING TYPHOON MARING IN 1984



AT AMBUKLAO DAM

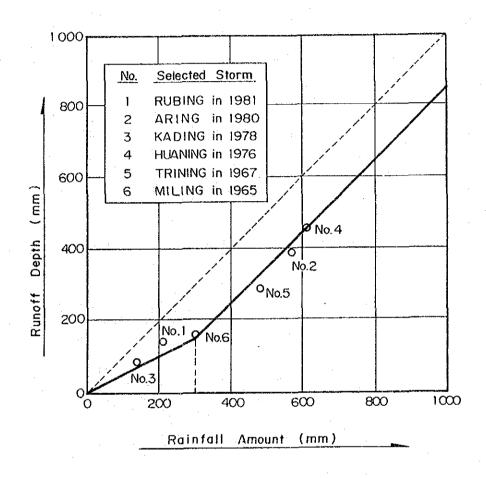
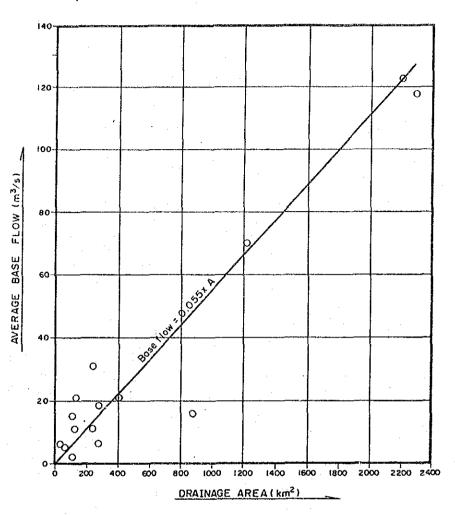


Fig. 4.15 RELATION BETWEEN RAINFALL AMOUNT AND RUNOFF DEPTH AT AMBUKLAO DAM



STATION NAME	DRAINAGE AREA(km²)	AVERAGE BASE FLOW (m <sup>3</sup> /s)
San Roque , San Manuel	. 1,225	70.5
Carmen , Rosales	2,209	122.8
Sta.Maria, San Nicolas	. 581	18. 5
Pacalat , Mangatorem	126	11.1
Poblacion, Bayambang	2,284	118.9
Maples, Aguilar	64	5. I
Adaoag , Kabayan	246	31.0
Bokod , Bengue!	48	6.8
Balangao - Compatling	112	2.6
Villa Agilpay	405	21.1
Tibae , Tarlas	872	15.9
Poblacion , Mayantoc	280	. 6, 8 .
Nambalan, Moyantoc	142	21.4
Palublub, Capas	240	11:5
Pacalat , Mangalarem	117	15.5

Fig. 4.16 BASE FLOW CURVE

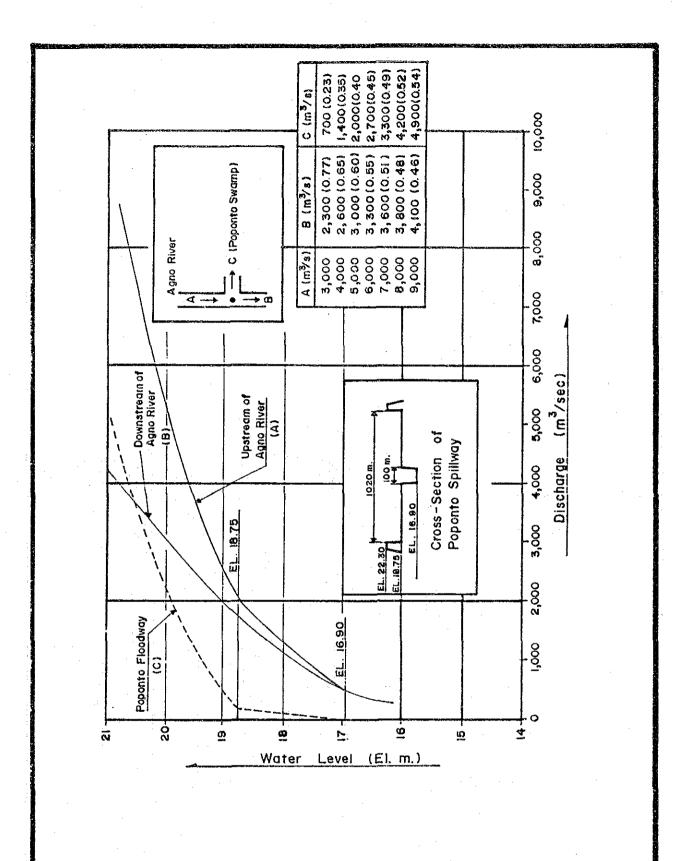


Fig. 4.17 DISCHARGE RATING CURVES AT POPONTO FLOODWAY

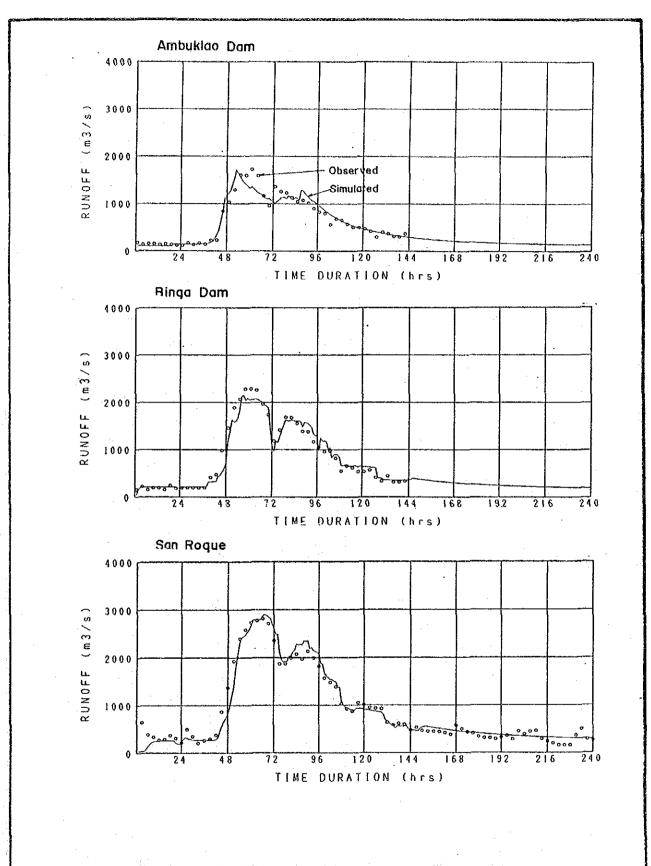


Fig. 4.18 OBSERVED AND SIMULATED FLOOD HYDROGRAPHS DURING TYPHOON MARING IN 1984 (1/2)

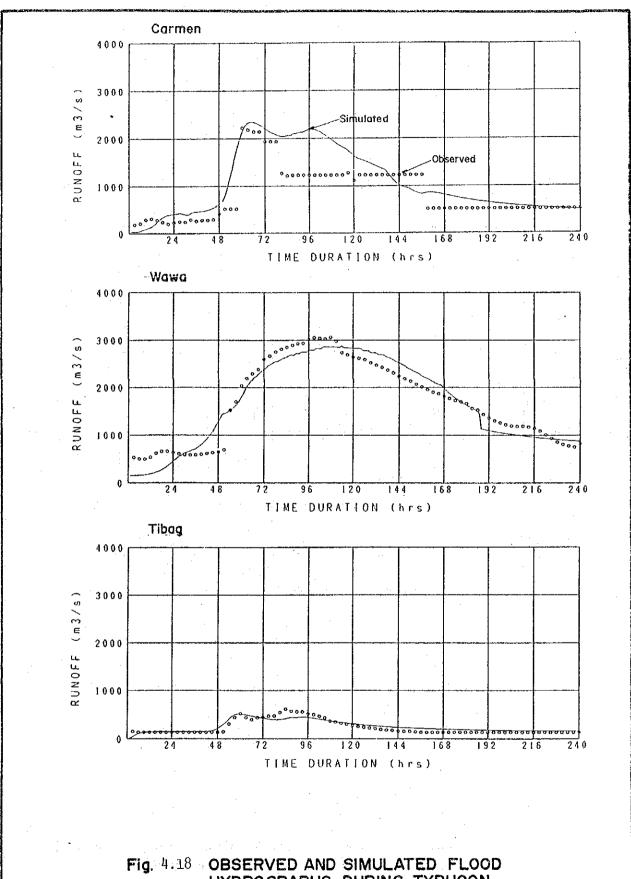


Fig. 4.18 OBSERVED AND SIMULATED FLOOD HYDROGRAPHS DURING TYPHOON MARING IN 1984(2/2)

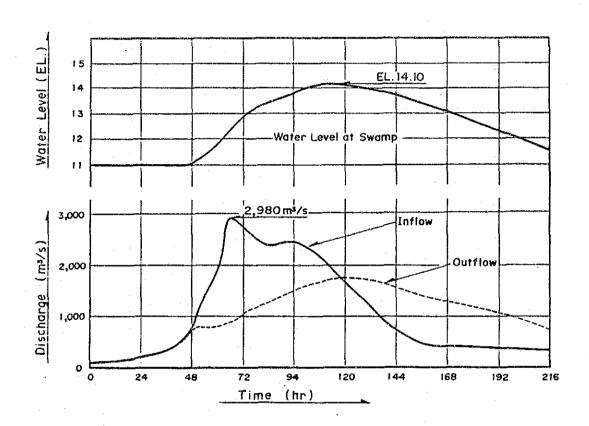


Fig. 4.19 SIMULATED WATER LEVEL AND DISCHARGE HYDROGRAPHS AT POPONT SWAMP DURING TYPHOON MARING IN 1984

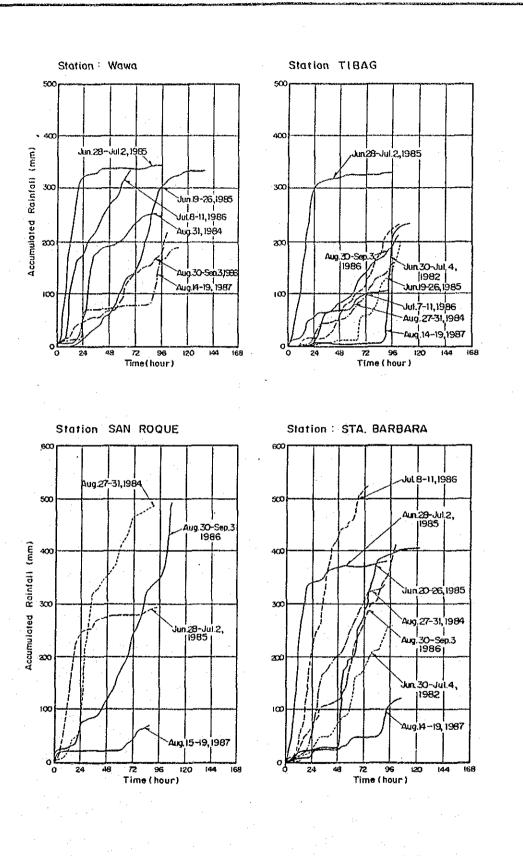
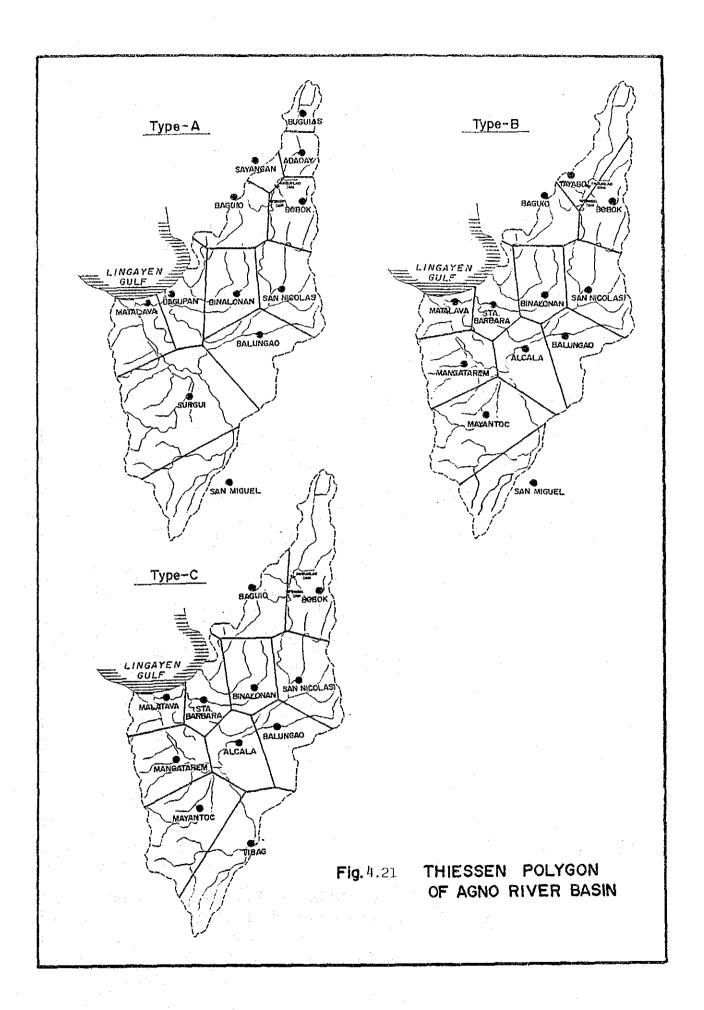


Fig. 4.20 ACCUMULATED RAINFALL CURVES AT TELEMETERING STATION



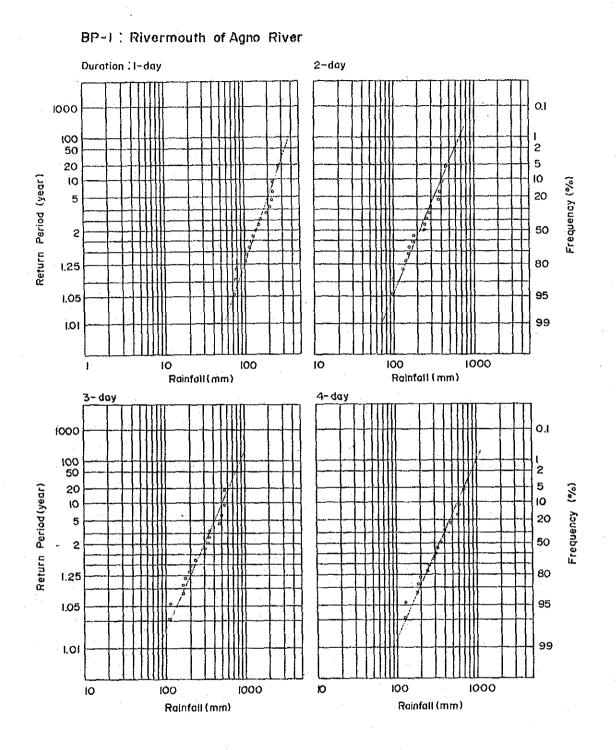
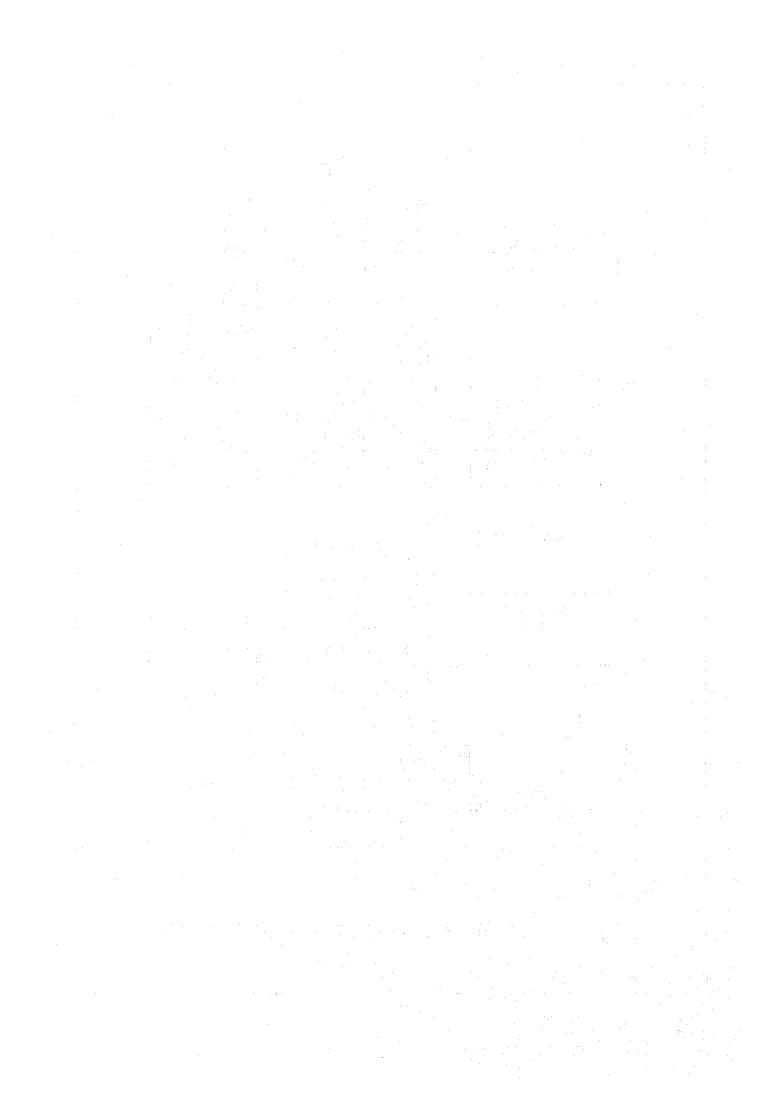


Fig. 4.22 FREQUENCY CURVE OF ANNUAL MAXIMUM BASIN MEAN RAINFALL AT BASE POINT (1/9)



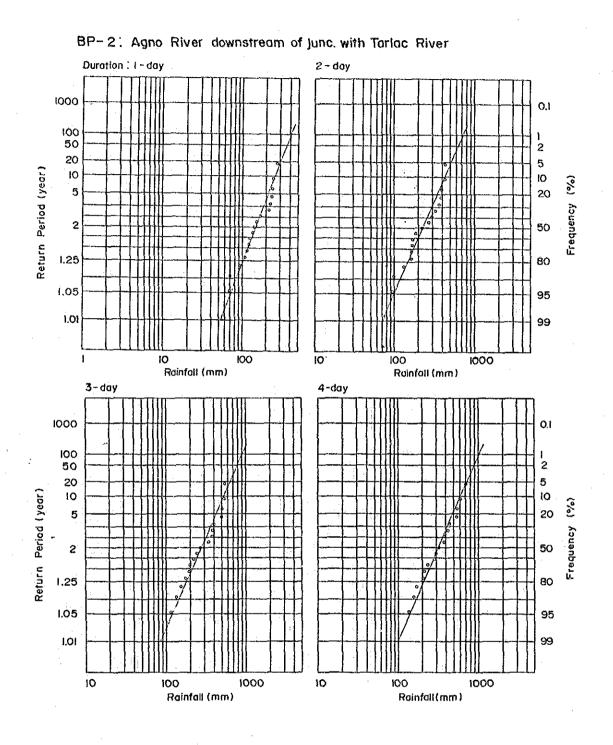
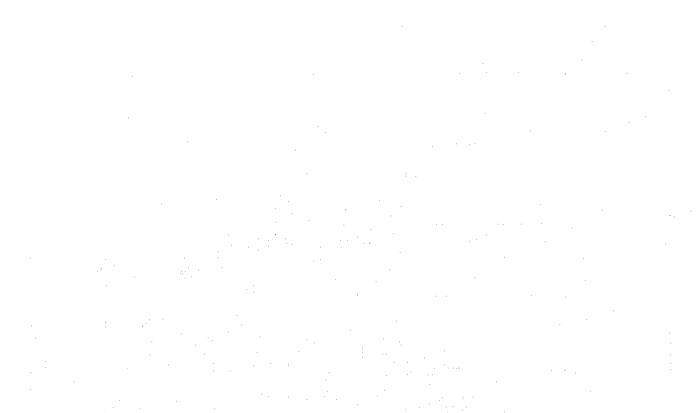


Fig. 4.22 FREQUENCY CURVE OF ANUAL MAXIMUN BASIN MEAN RAINFALL AT BASE POINT (2/9)



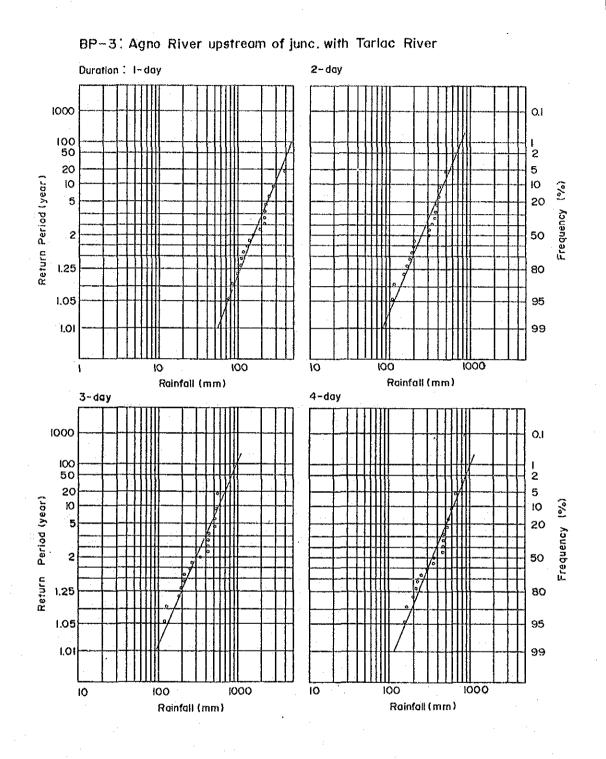
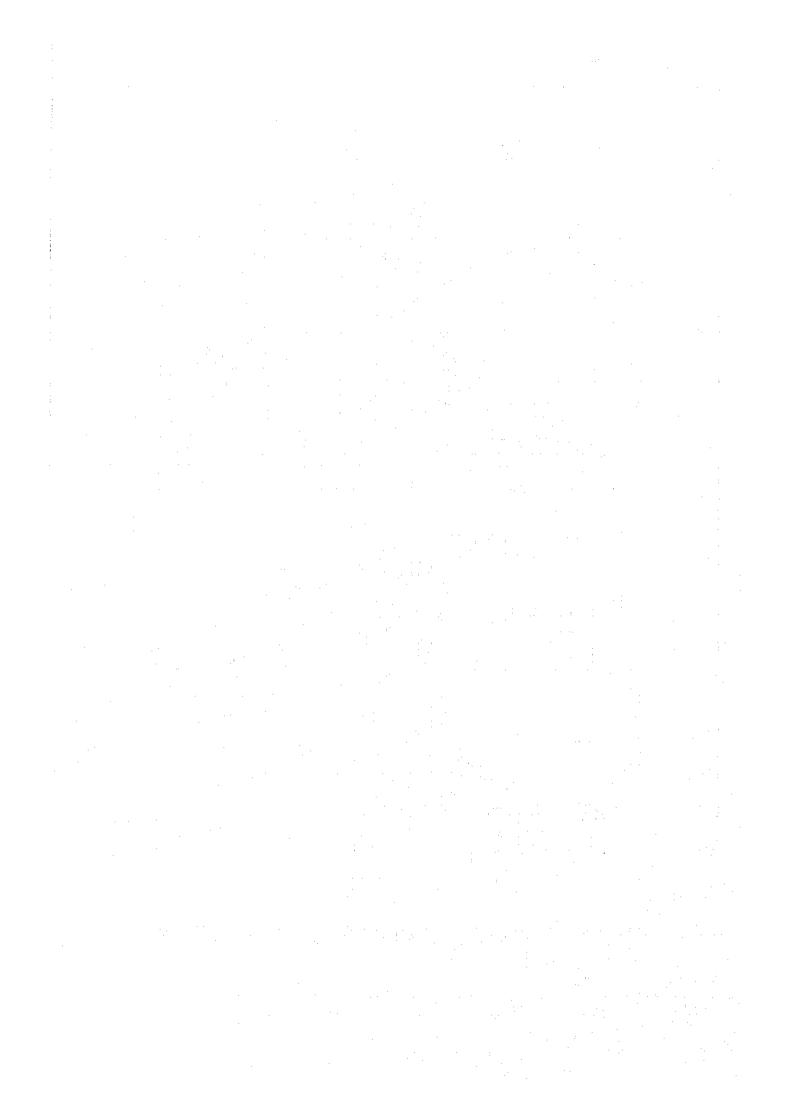


Fig. 4.22 FREQUENCY CURVE OF ANNUAL MAXIMUM BASIN MEAN RAINFALL AT BASE POINT (3/9)



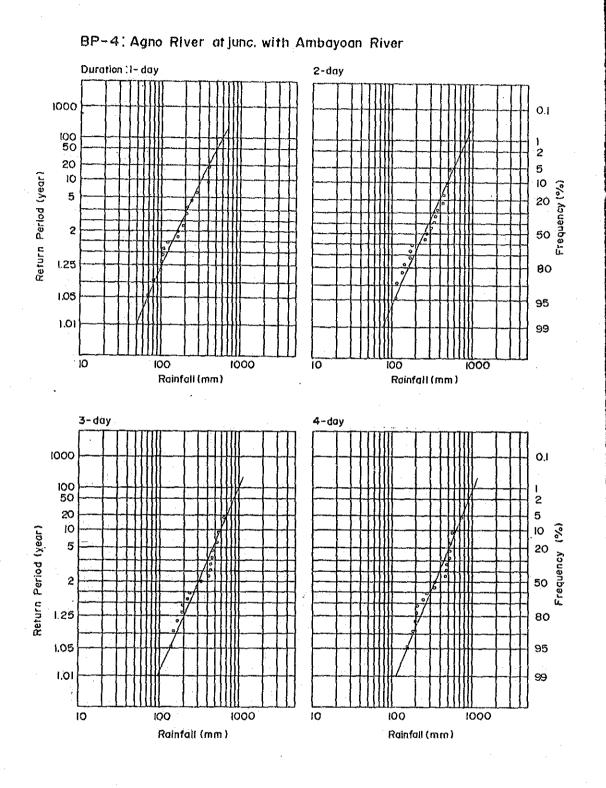


Fig. 4.22 FREQUENCY CURVE OF ANNUAL MAXIMUM BASIN MEAN RAINFALL AT BASE POINT (4/9)

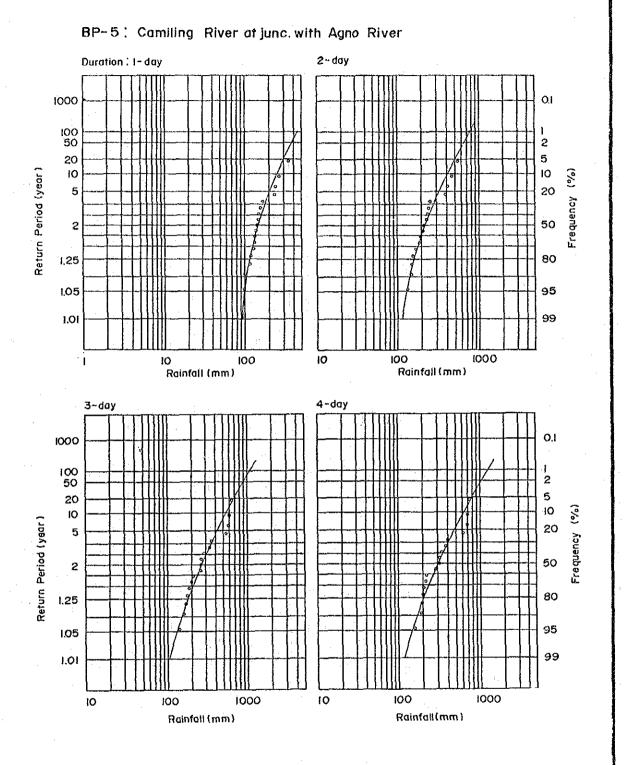


Fig. 4.22 FREQUENCY CURVE OF ANNUAL MAXIMUM BASIN MEAN RAINFALL AT BASE POINT (5/9)

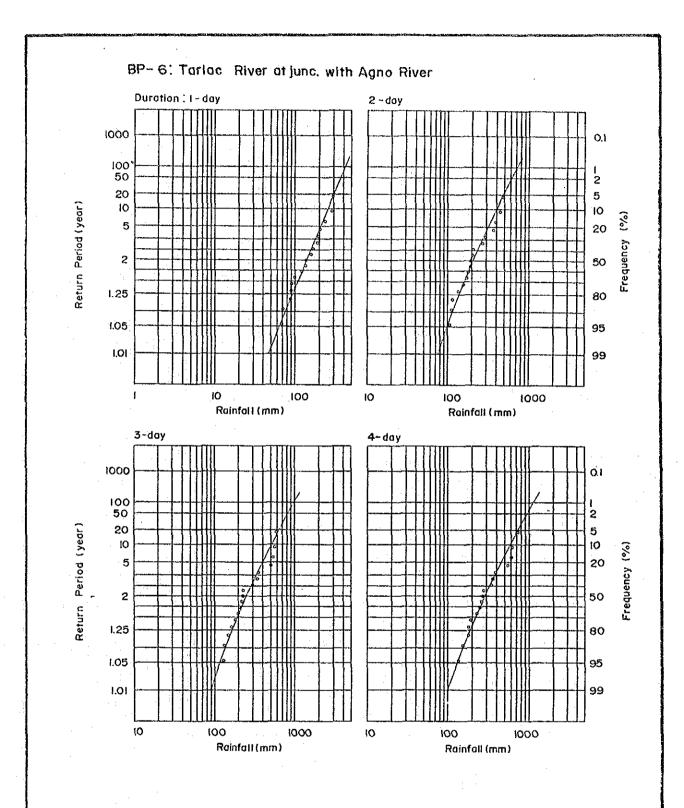


Fig. 4.22 FREQUENCY CURVE OF ANNUAL MAXIMUM BASIN MEAN RAINFALL AT BASE POINT (6/9)

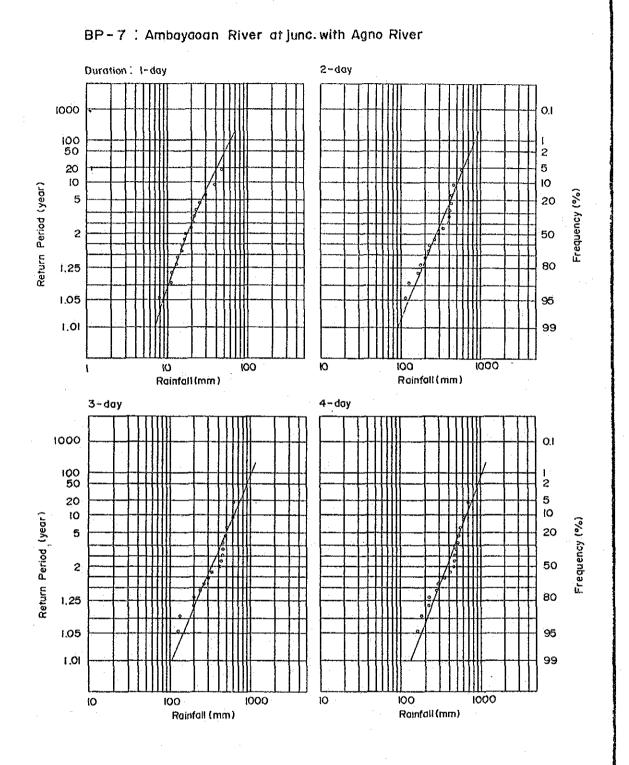


Fig. 4.22 FREQUENCY CURVE OF ANUAL MAXIMUN BASIN MEAN RAINFALL AT BASE POINT (7/9)

. .

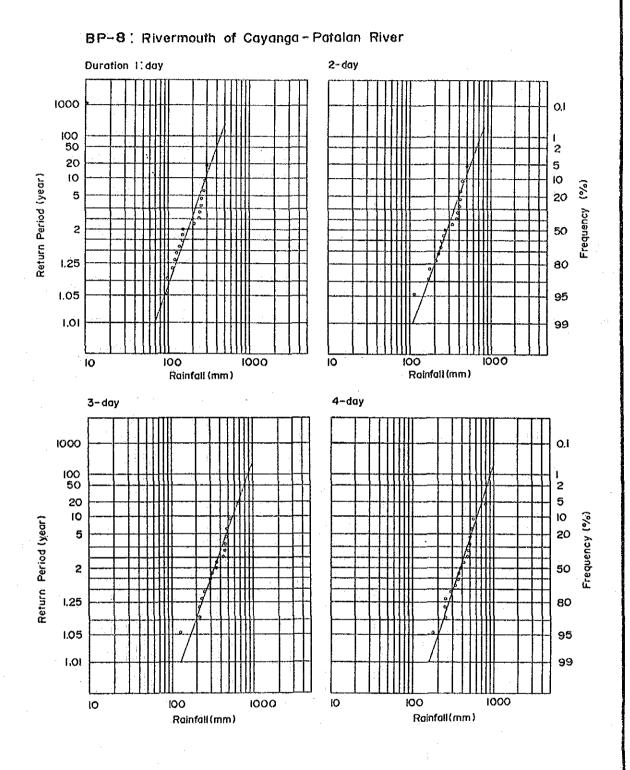


Fig. 4.22 FREQUENCY CURVE OF ANNUAL MAXIMUM BASIN MEAN RAINFALL AT BASE POINT (8/9)

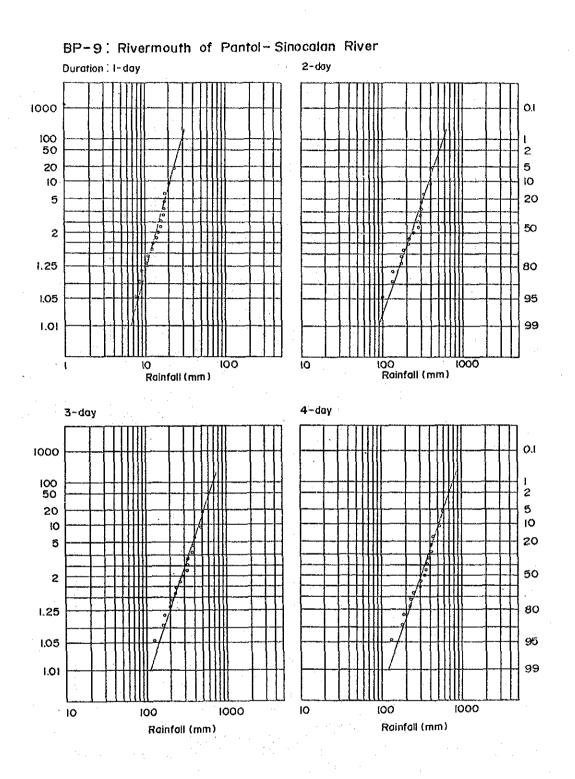
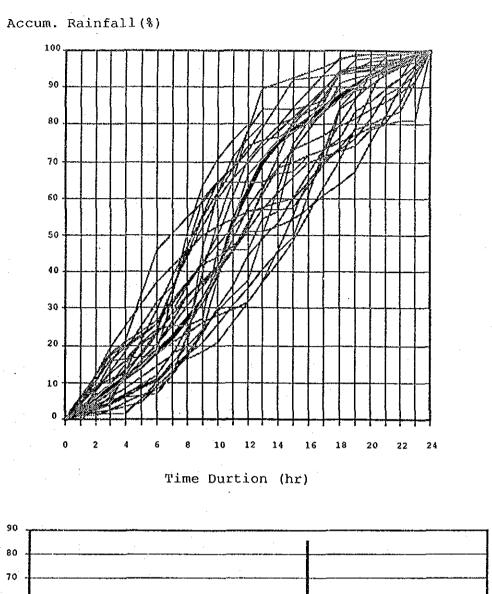


Fig. 4.22 FREQUENCY CURVE OF ANNUAL MAXIMUM BASIN MEAN RAINFALL AT BASE POINT (9/9)



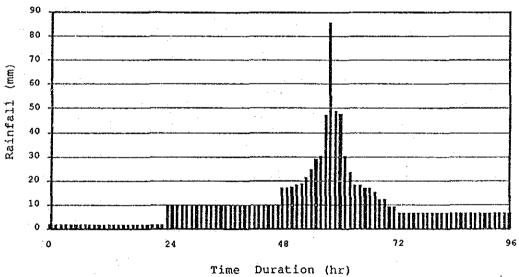


Fig. 4.23 HOURLY DESIGN RAINFALL DISTRIBUTION

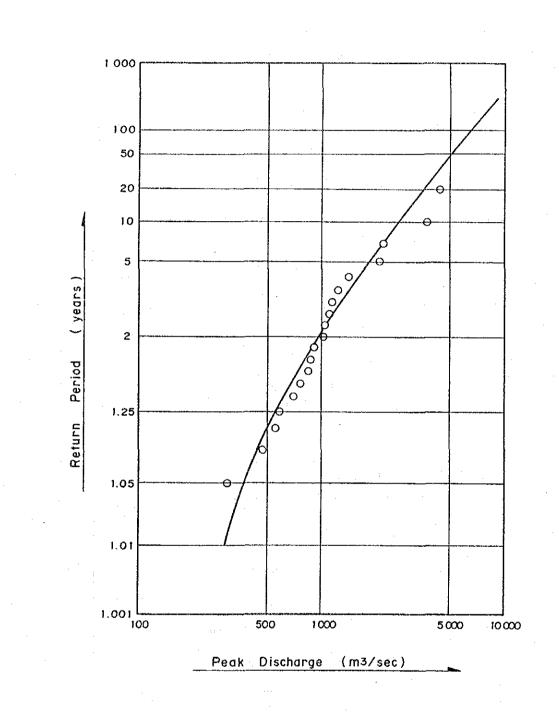
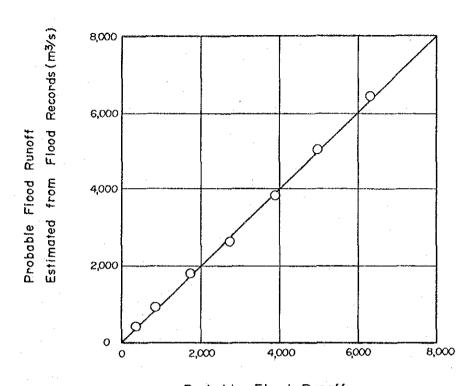


Fig. 4.24 FREQUENCY CURVE OF ANNUAL MAXIMUM PEAK DISCHARGE AT SAN ROQUE



Probable	Flood	Runoff	
Estimated	from	Rainfall	$(m^3/s)$

Davis Desired (Marsh)	Probable Flood Runoff(m³/s)					
Return Period (year)	from Flood Record	from Rainfall				
100	6,440	6, 260				
50	5,000	5,060				
25	3,900	3,960				
10	2,570	2,720				
5	1,810	1,710				
2	990	830				
1.05	370	320				

Fig. 4.25 COMPARISON OF PROBABLE FLOOD PEAK RUNOFF AT SAN ROQUE

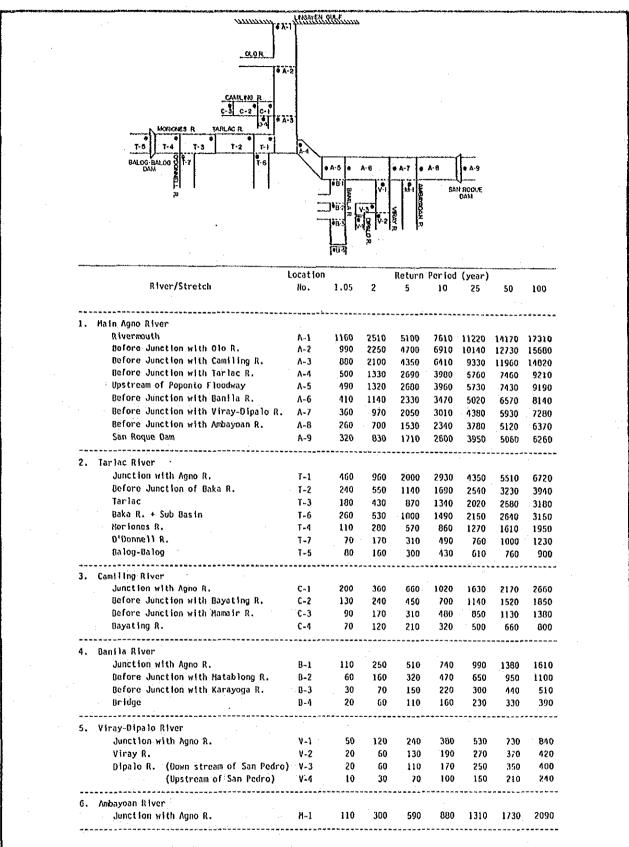
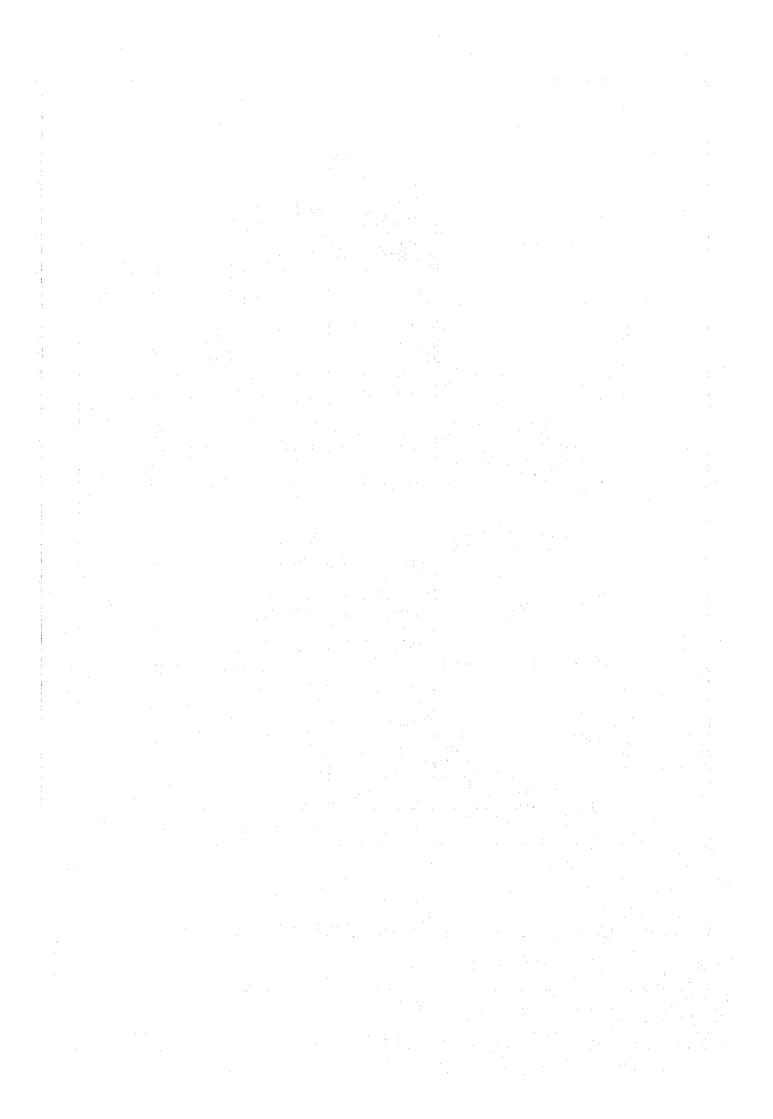
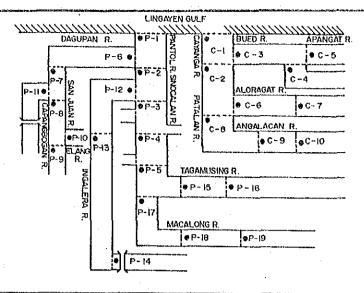


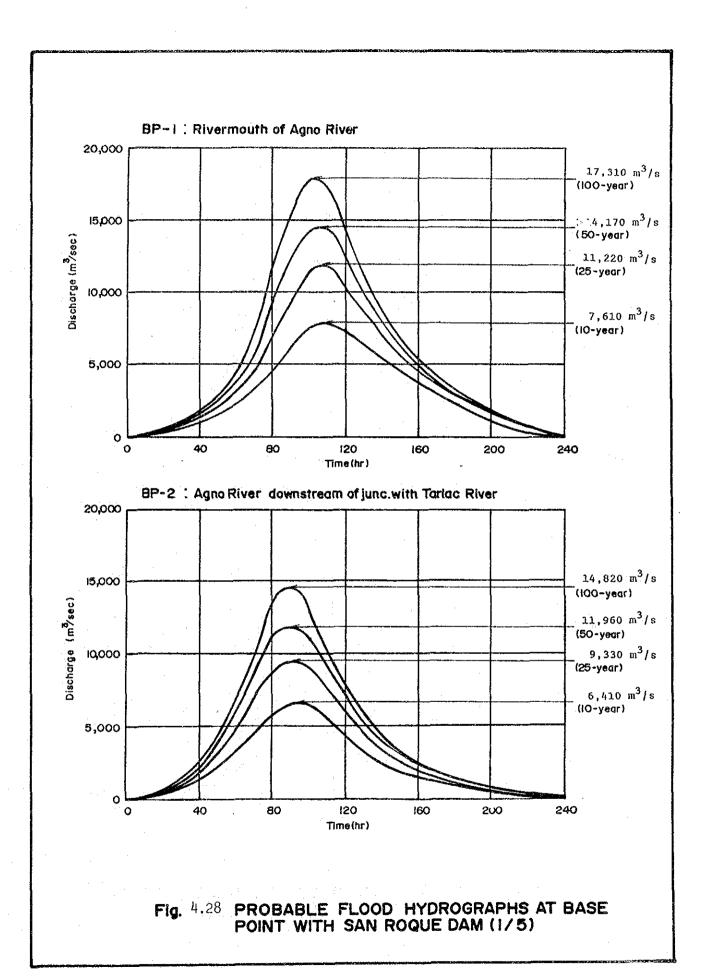
Fig. 4.26 PROBABLE FLOOD PEAK DISCHARGE DISTRIBUTION OF AGNO RIVER UNDER CONFINING DIKE CONDITION (WITH SAN ROQUE DAM)

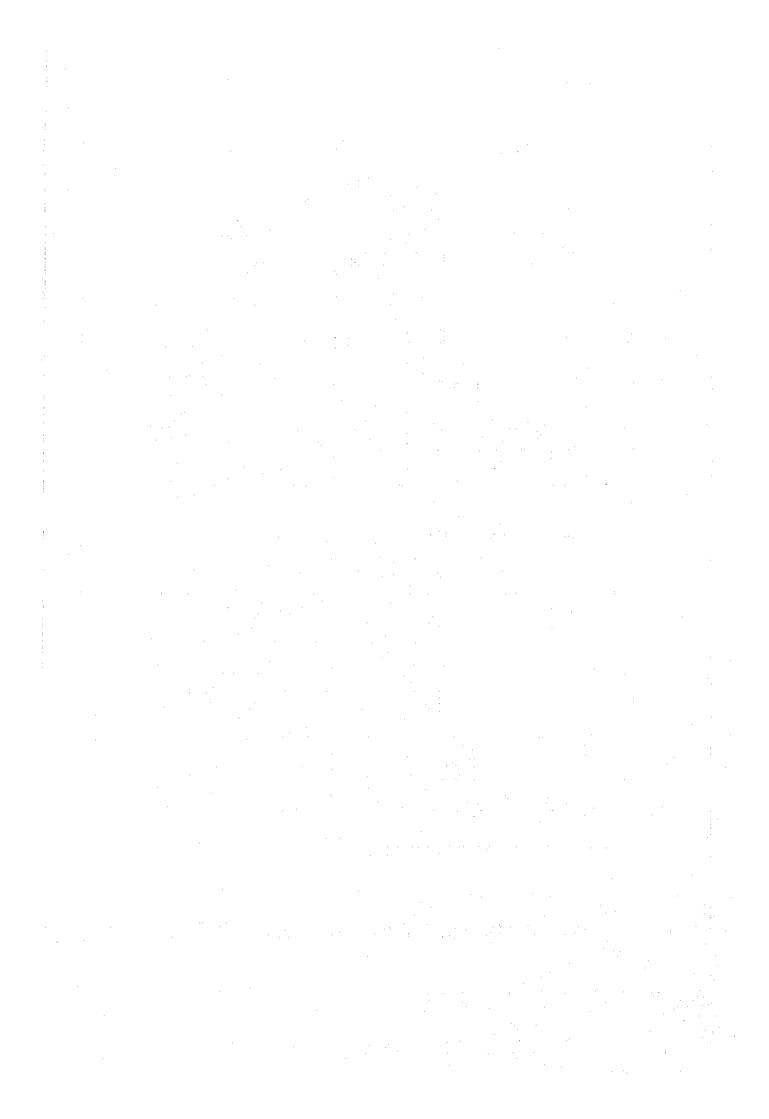


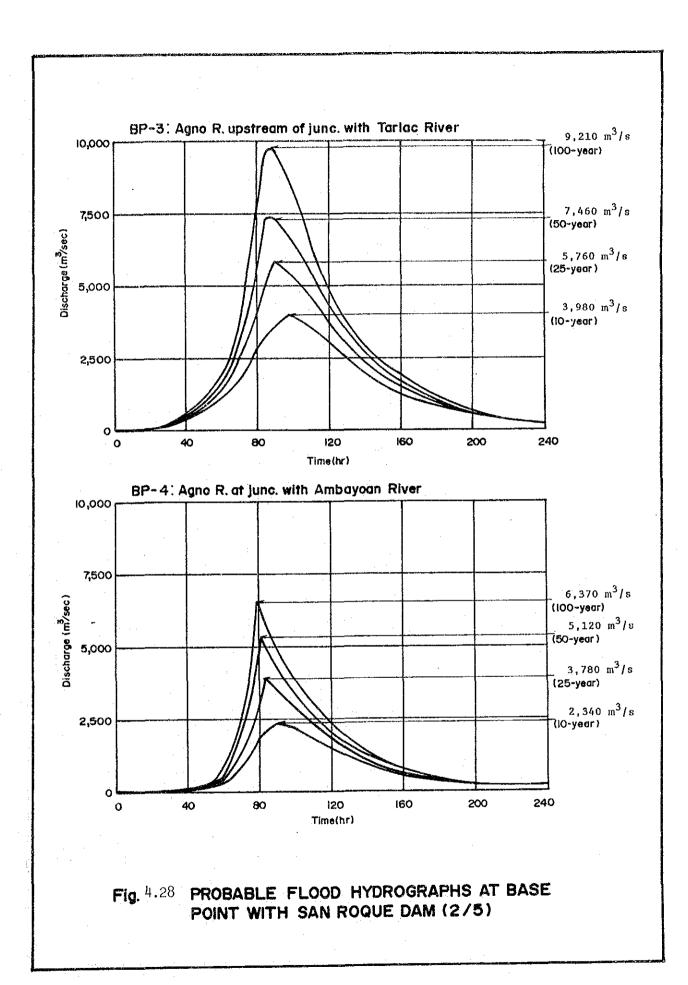


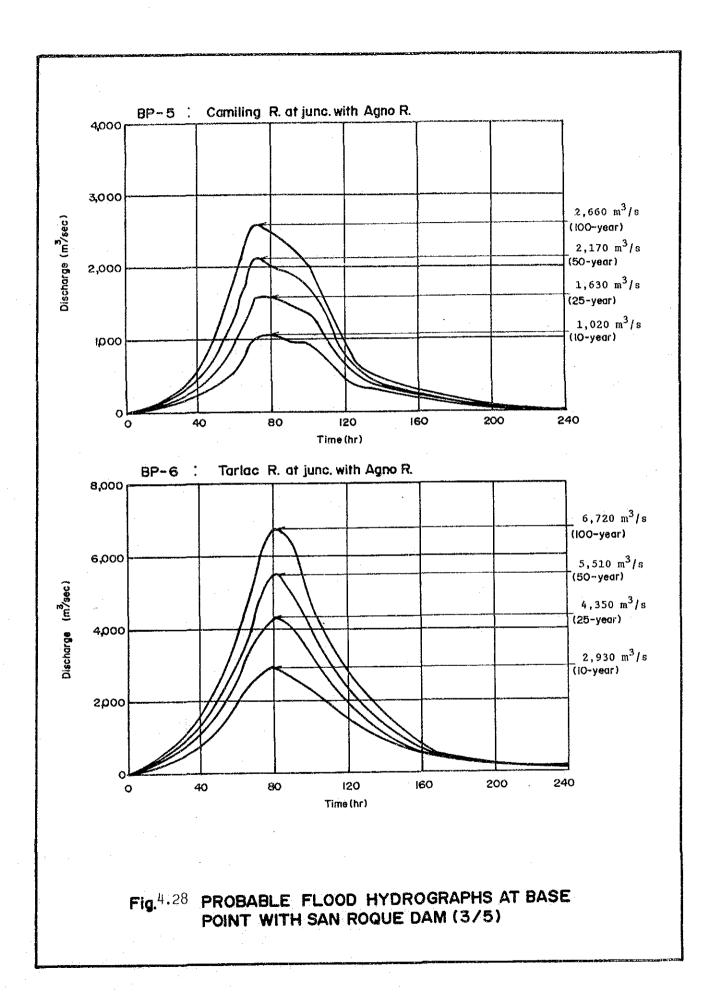
	Location								
	River/Stretch	No.	1.05	2	5	10	25	50	100
 1.1	Cayanga/Patalan Rivers				·				• • • • • • • • • • • • • • • • • • • •
	Rivermouth	C-1	270	580	1070	1490	2080	2560	3030
	Before Junction with Bued R.	€-5	140	300	550	770	1060	1310	1550
1.2	Bued River								
	Junction with Cayanga R.	C-3	130	290	520	730	1040	1290	1550
	Before Junction with Apangat R.	C-4	90 -	200	340	500	750	950	1170
	Apangat R.	C-5	30	60	120	160	220	260	300
1.3	Aloragat River								
	Junction with Patalan R.	C-6	50	110	210	280	380	470	550
	Amagbagan	C-7	30	60	100	140	200	240	290
1.4	Angalacan River							2	
	Junction with Patalan R.	C-8	70	150	200	400	670	710	840
	Maraboc	C-9 ·	50	110	190	270	400	510	620
٠.	Killo	C-10	30	80	130	190	290	370	460
 2.1	Panto/Sinocalan River		+						
	Rivermouth	P-1	430	810	1340	1900	2710	3260	1000
	Before Junction with Dagupan R.	P-2	280	540	850	1220	1740	2220	2670
	Before Junction with Ingalera R.	P-3 .	190	380	600	860	1260	1640	2000
	Hefore Junction with Quinabolotan R.	P-4	140	280	430	620	950	1250	1530
	Catablan	P-5	120	250	370	540	850	1120	1380
2.2	Dagupan City								
	Junction with Panto R.	P-6	170	300	480	690	950	1110	1260
	Before Junction with Dasing R.	P-7	130	240	380	540	740	870	990
	Lower San Juan R.	P-8	100	170	270	390	540	630	720
	Upper San Juan R.	P-9	50	90	150	200	280	330	380
	Elang R.	P-10	50	80	120	190	260	310	350
	Campangbogan R.	P-11	30	50	90	120	170	190	220
2.3	Ingalera River								
1	Junction with Sinocalan R.	P-12	80	150	250	360	500	600	670
	Ta lospa tang	P-13	60	120	180	260	370	450	540
	San Kicolas	P-14	20	40	50	00	120	150	100
2.4	Tagumising/Tuboy River			٠.					
	Junction with Sinocalan R.	P-15	98	170	250	350	580	790	990
	Yatyat	P-16.	70	150	230	330	540	730	910
2.5	Hacalong River								
	Junction with Sinocalan R.	P-17	10	90	1 30	190	270	330	390
	Urdaneta	P-18	30	60	80	120	190	210	280
	San Hanuel	P-19	20	30	50	70	100	140	160

Fig. 4.27 PROBABLE FLOOD PEAK DISCHARGE DISTRIBUTION OF ALLIED RIVERS UNDER CONFINING DIKE CONDITION









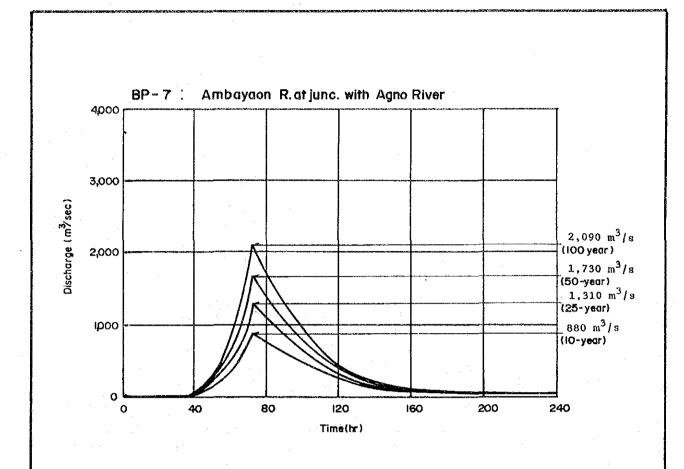
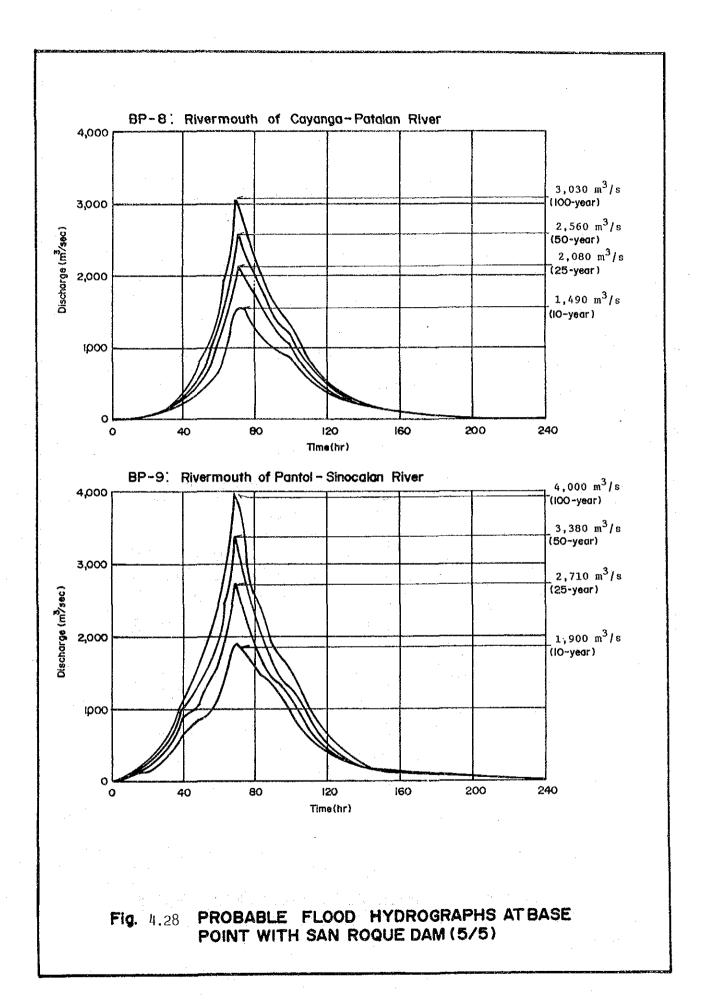
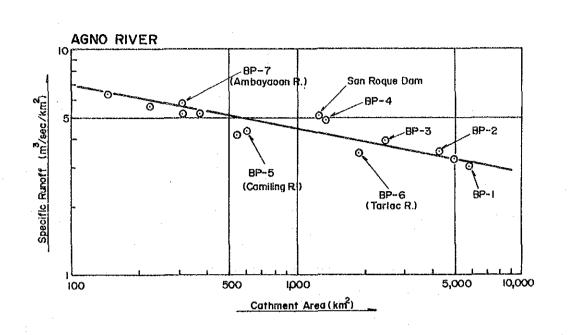


FIG. 4.28 PROBABLE FLOOD HYDROGRAPHS AT BASE POINT WITH SAN ROQUE DAM (4/5)





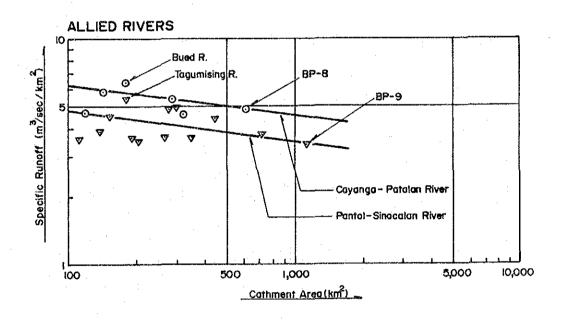
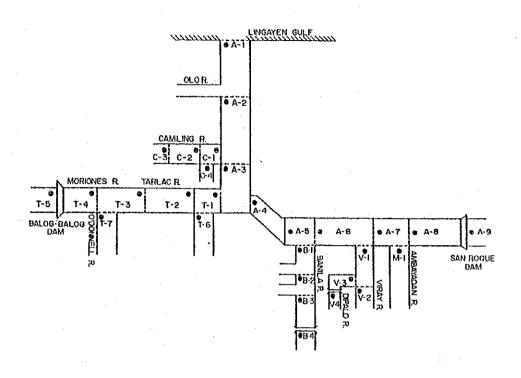


Fig. 4.29 RELATIONSHIP BETWEEN SPECIFIC RUNOFF OF 100 - YEAR FLOOD AND CATCHMENT AREA



	Location	Location			Return Period (year)				
River/Stretch	No.	1.05	2	5	10	25	50	100	
. With San Roque Dam									
Rivermouth	Λ-i	1160	2510	5100	7610	11220	14170	1731	
Before Junction with Olo R.	۸-2	990	2250	4700	6910	10140	12730	1560	
Defore Junction with Camiling R.	Λ-3	880	2100	4350	6410	9330	11960	1482	
Before Junction with Tarlac R.	Λ-4	500	1330	2690	3980	5760	7460	921	
Upstream of Poponto Floodway	A-5	490	1320	2680	3960	5730	7430	919	
Before Junction with Banila R.	A-6	410	1140	2330	3470	5020	6570	814	
Before Junction with Viray-Dipalo R.	A-7	360	970	2050	3010	4380	5930	728	
Before Junction with Ambayoan R.	A-8	260	700	1530	2340	3780	5120	63	
San Roque Dam	Λ-9	320	830	1710	2600	3950	5060	62	
. Without San Rogue Dam									
Rivermouth	۸-1	1240	2760	5520	8270	12020	15000	179	
Before Junction with Olo R.	Λ-2	1090	2610	5120	7510	10850	13530	162	
Before Junction with Camiling R.	Λ-3	. 1010	2430	4840	7070	10270	12790	154	
Before Junction with Tarlac R.	Λ-4	660	1570	3060	4470	6450	8040	97	
Upstream of Poponto Floodway	Λ-5	650	1560	3030	4430	6420	7990	96	
Defore Junction with Danila R.	Λ-6	570	1370	2650	3890	5670	7060	85	
Before Junction with Viray-Dipale R.	A-7	500	1220	2300	3120	5020	6230	75	
Before Junction with Ambayoan R.	Λ-8	340	890	1820	2740	4190	5370	66	
San Roque Dam	Λ-9	320	830	1710	2600	3950	5060	62	

Fig. 4.30 PROBABLE FLOOD PEAK DISCHARGE UNDER CONFINING DIKE CONDITION WITH AND WITH-OUT SAN ROQUE DAM

