

H: LEAKAGE SURVEY

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C O N T E N T S

	Page
1. Objective of Survey	H- 1
2. Method of Leakage Estimation and Quantification	H- 1
3. Survey Works Conducted	H- 2
4. Survey Results	H- 3
5. Findings and Leakage Survey Data	H- 4

1. OBJECTIVE OF SURVEY

The primary purpose of this survey is to find the present statuses and characteristics of the distribution system leakage in the WASA water supply system in Trinidad and Tobago.

For this purpose, ten (10) small hydraulically isolated areas (receiving 24-hour water-service) of distribution system were selected and conducted a pilot leakage survey under the present study.

2. METHOD OF LEAKAGE ESTIMATION AND QUANTIFICATION

Leakage losses of the whole WASA system cannot be directly investigated and determined. Since, it is difficult to make a detailed survey for the entire water service area in the country under the present study. Therefore, a total 10 representative residential areas, of which distribution system could be hydraulically isolated to a small service block, were selected and carried out for a pilot leakage survey in the present study.

A master meter was installed on each water mains supplying water to each isolated block, and hourly meter readings were made for 24 hours and recorded to determine the daily demand patterns.

The night time minimum-flow in the respective selected service block was measured through 24 hours meter reading. The midnight-time minimum water flow, when the distribution system has a stable water pressure in higher level while no water usage, could be considered as a leakage loss amount in that service block.

Further, the system pressure in the service block was monitored for 24 hours in parallel with the flow metering and recording.

The total leakage loss amount a day is estimated from the total supplied water amount and system pressure variation in the respective service blocks/areas.

3. SURVEY WORKS CONDUCTED

3.1 Isolated Survey Blocks Selection

Following processes were taken for the survey blocks selection in the present study:

(1) Several candidate areas were listed for the potential survey area, according to the following criteria:

- Possibility to isolate the areas hydraulically from the system is confirmed; preferably each area should have a single dead-end supply main.
- Reasonably typical urban development is made and water supply conditions are sufficient.
- At least 50 and preferably 100 service connections are covered.

(2) The candidate or potential area were inspected, and primary choices were made.

(3) Investigations were made to ascertain whether the areas could practically be isolated from the distribution system.

(4) Final selection was made.

Out of a total 17 candidate areas/locations (ref. Table 3.1), the following eight areas were listed up under the reasonably typical urban development and water supply conditions:

(Trinidad): Port of Spain, St Joseph, ARIMA, Diego Martin, San Fernando, Trin city, Chagouras, and

(Tobago): Plymouth.

3.2 Survey/Study Activities

3.2.1 Water flow measurement

Following activities were conducted for the water flow measurement in the respective survey block:

- Control and close the distribution system valve to isolate hydraulically the survey block completely.
- Install a water flow meter at the inflow point and on the distribution main pipe of the isolated block.
- Measure and record the water flow amount continuously for 24 hours.

3.2.2 System water pressure record

During the water flow measuring time, the system water pressure was monitored and recorded at a water tap for 24 hours in the same survey block.

4. SURVEY RESULTS

A total 10 small blocks in the water service area were conducted the pilot leakage survey, all which were isolated hydraulically in the distribution system.

Of which, 8 blocks field survey works and leakage investigations were carried out by the mid January 1990, and the remaining 2 blocks survey were conducted by the end of March 1990.

Major findings from the distribution main flows and system pressure recordings are presented in the followings and Section 5. Findings and Leakage Survey Data, and its general analyses are made as presented in the followings.

The following items of data are obtained through the survey, and its

survey-results are analyzed for the above each survey/study area :

- (1) Daily supplied water amount,
- (2) Night time minimum water flow amount,
- (3) Night time system water pressures,
- (4) Estimated leakage amounts/losses,
- (5) Estimated unit water consumption, LPCD (litters per capita per day), and
- (6) Estimated unit leak amount (cubic meters per 1 km distribution pipeline : m³/km)

5. Findings and Leakage Survey Data

5.1 General of Findings

The estimated leakage losses/ amounts in the survey area are ranging from 30% to 80% of the total supplied amount. The average ratio of leakage losses to the total daily supplied water (or sometimes produced and distributed water) is estimated high at 45 to 50 % from the above results tentatively, since the investigation was conducted on the limited part of the existing system.

The rate of leakage losses are varying depending to the characteristics of the total system pipeline length, number of house connections, and the system facility aging conditions in the respective service area.

Generally, in the nighttime (during about 4 hours from midnight to 4 a.m.), the distribution system water pressure is stable in the higher level. While, the water flow amount decreases to the lower level and becomes in stable.

No. 001

Area : DIEGO MARTIN(JEDE st)

Date : Dec.13-14, 1989

$$Qx = Qo \times (Hx/Ho)^n$$

--(n = 0.5)-- --(n = 1.15)--
 --(orifice)-- --(crack)--

TIME hour min	METERED	METERED	Qtotal m3	Leak hole d(mm)	< TYPE - A >		< TYPE - B >	
	Q (m3/h)	PRESSURE (kg/cm2)			Leak QA1(m3)	Demand QA2(m3)	Leak QB1(m3)	Demand QB2(m3)
16 :40	3.84	2.1	---	14.55	---	---	---	---
16 :50	4.17	2.0	0.668	15.35	0.319	0.349	0.226	0.442
17 :00	4.62	2.1	0.733	15.96	0.327	0.406	0.239	0.494
17 :10	4.23	1.8	0.738	15.87	0.303	0.435	0.200	0.537
17 :20	4.32	1.9	0.713	15.82	0.311	0.402	0.213	0.500
17 :30	4.47	1.9	0.733	16.10	0.311	0.422	0.213	0.520
17 :40	3.50	1.9	0.664	14.24	0.311	0.353	0.213	0.451
17 :50	4.29	1.9	0.649	15.77	0.311	0.338	0.213	0.436
18 :00	4.59	1.8	0.740	16.53	0.303	0.437	0.200	0.540
18 :10	4.29	1.9	0.740	15.77	0.311	0.429	0.213	0.527
18 :20	5.26	1.9	0.796	17.46	0.311	0.485	0.213	0.583
18 :30	3.84	1.9	0.758	14.92	0.311	0.447	0.213	0.545
18 :40	4.65	1.7	0.708	16.88	0.294	0.413	0.187	0.520
18 :50	4.02	1.9	0.723	15.26	0.311	0.412	0.213	0.510
19 :00	4.35	1.8	0.698	16.09	0.303	0.395	0.200	0.497
19 :10	4.93	2.0	0.773	16.69	0.319	0.454	0.226	0.547
19 :20	5.08	1.8	0.834	17.39	0.303	0.532	0.200	0.634
19 :30	4.41	1.9	0.791	15.99	0.311	0.480	0.213	0.578
19 :40	3.75	2.1	0.680	14.38	0.327	0.353	0.239	0.441
19 :50	3.84	2.0	0.633	14.73	0.319	0.314	0.226	0.407
20 :00	4.38	2.1	0.685	15.54	0.327	0.358	0.239	0.446
20 :10	4.96	2.2	0.778	16.34	0.334	0.444	0.252	0.526
20 :20	4.02	2.2	0.748	14.71	0.334	0.414	0.252	0.496
20 :30	4.14	2.3	0.680	14.77	0.342	0.338	0.265	0.415
20 :40	4.11	2.3	0.688	14.71	0.342	0.345	0.265	0.422
20 :50	4.29	2.4	0.700	14.87	0.349	0.351	0.279	0.421
21 :00	3.90	2.3	0.683	14.33	0.342	0.340	0.265	0.417
21 :10	4.99	2.4	0.741	16.04	0.349	0.391	0.279	0.462
21 :20	3.96	2.3	0.746	14.44	0.342	0.404	0.265	0.481
21 :30	3.53	2.6	0.624	13.22	0.364	0.261	0.305	0.319
21 :40	3.17	2.5	0.558	12.66	0.357	0.202	0.292	0.266
21 :50	3.08	2.6	0.521	12.35	0.364	0.157	0.305	0.215
22 :00	2.87	2.5	0.496	12.04	0.357	0.139	0.292	0.204
22 :10	3.14	2.5	0.501	12.60	0.357	0.144	0.292	0.209
22 :20	3.96	2.6	0.592	14.01	0.364	0.228	0.305	0.286
22 :30	3.32	2.5	0.607	12.95	0.357	0.250	0.292	0.315
22 :40	3.23	2.7	0.546	12.53	0.371	0.175	0.319	0.227
22 :50	3.08	2.7	0.526	12.24	0.371	0.155	0.319	0.207
23 :00	2.78	2.8	0.488	11.52	0.377	0.111	0.333	0.156
23 :10	3.47	2.6	0.521	13.11	0.364	0.157	0.305	0.215
23 :20	3.32	2.8	0.566	12.59	0.377	0.188	0.333	0.233
23 :30	2.57	2.8	0.491	11.08	0.377	0.113	0.333	0.158
23 :40	2.75	3.2	0.443	11.08	0.403	0.040	0.388	0.056
23 :50	2.51	3.2	0.438	10.59	0.403	0.035	0.388	0.051
0 :00	2.57	3.2	0.423	10.71	0.403	0.020	0.388	0.036
0 :10	2.78	3.2	0.446	11.14	0.403	0.042	0.388	0.058
0 :20	2.87	3.2	0.471	11.32	0.403	0.067	0.388	0.083
0 :30	2.57	3.3	0.453	10.63	0.410	0.044	0.402	0.052
0 :40	2.96	3.2	0.461	11.50	0.403	0.057	0.388	0.073
0 :50	2.57	3.2	0.461	10.71	0.403	0.057	0.388	0.073
1 :00	2.54	3.2	0.426	10.65	0.403	0.022	0.388	0.038
1 :10	2.54	3.3	0.423	10.57	0.410	0.014	0.402	0.022
1 :20	2.60	3.3	0.428	10.69	0.410	0.019	0.402	0.027
1 :30	2.54	3.4	0.428	10.49	0.416	0.013	0.416	0.013
1 :40	2.48	3.4	0.418	10.37	0.416	0.003	0.416	0.003
1 :50	2.51	3.4	0.416	10.43	0.416	0.000	0.416	0.000

No. 001
 Area : DIEGO MARTIN(JEDE st)
 Date : Dec. 13-14. 1989

$$Q_x = Q_0 \times (H_x/H_0)^n$$

--(n = 0.5)-- --(n = 1.15)--
 --(orifice)-- --(crack)--

	TIME hour min	METERED	METERED	Qtotal m3	Leak hole d(mm)	< TYPE - A >		< TYPE - B >	
		Q (m3/h)	PRESSURE (kg/cm2)			Leak QA1(m3)	Demand QA2(m3)	Leak QB1(m3)	Demand QB2(m3)
2	2 :00	2.54	3.4	0.421	10.49	0.416	0.005	0.416	0.005
	2 :10	2.48	3.4	0.418	10.37	0.416	0.003	0.416	0.003
	2 :20	2.66	3.4	0.428	10.74	0.416	0.013	0.416	0.013
	2 :30	2.54	3.4	0.433	10.49	0.416	0.018	0.416	0.018
	2 :40	2.66	3.4	0.433	10.74	0.416	0.018	0.416	0.018
	2 :50	2.54	3.4	0.433	10.49	0.416	0.018	0.416	0.018
	3 :00	2.51	3.4	0.421	10.43	0.416	0.005	0.416	0.005
	3 :10	2.81	3.4	0.443	11.03	0.416	0.027	0.416	0.027
	3 :20	2.54	3.4	0.446	10.49	0.416	0.030	0.416	0.030
	3 :30	2.78	3.4	0.443	10.97	0.416	0.027	0.416	0.027
	3 :40	2.51	3.4	0.441	10.43	0.416	0.025	0.416	0.025
	3 :50	2.78	3.4	0.441	10.97	0.416	0.025	0.416	0.025
4	4 :00	2.72	3.3	0.458	10.94	0.410	0.049	0.402	0.057
	4 :10	2.90	3.3	0.468	11.29	0.410	0.059	0.402	0.067
	4 :20	2.60	3.2	0.458	10.78	0.403	0.055	0.388	0.071
	4 :30	2.66	3.2	0.438	10.90	0.403	0.035	0.388	0.051
	4 :40	2.66	3.3	0.443	10.82	0.410	0.034	0.402	0.042
	4 :50	3.35	3.2	0.501	12.23	0.403	0.097	0.388	0.113
	5 :00	2.66	3.1	0.501	10.99	0.397	0.104	0.374	0.127
	5 :10	3.08	3.0	0.478	11.92	0.391	0.088	0.360	0.118
	5 :20	2.90	3.0	0.498	11.57	0.391	0.108	0.360	0.138
	5 :30	2.99	2.9	0.491	11.84	0.384	0.107	0.346	0.145
	5 :40	3.17	2.7	0.513	12.41	0.371	0.143	0.319	0.194
	5 :50	3.47	2.5	0.553	13.24	0.357	0.197	0.292	0.261
6	6 :00	3.87	2.4	0.612	14.13	0.349	0.262	0.279	0.333
	6 :10	4.05	2.3	0.660	14.61	0.342	0.318	0.265	0.395
	6 :20	4.41	2.2	0.705	15.41	0.334	0.371	0.252	0.453
	6 :30	4.53	1.9	0.745	16.20	0.311	0.434	0.213	0.532
	6 :40	5.14	2.0	0.806	17.04	0.319	0.487	0.226	0.580
	6 :50	4.50	1.9	0.803	16.15	0.311	0.492	0.213	0.590
	7 :00	4.50	2.0	0.750	15.94	0.319	0.431	0.226	0.524
	7 :10	3.81	2.0	0.693	14.67	0.319	0.374	0.226	0.467
	7 :20	5.11	1.9	0.743	17.21	0.311	0.432	0.213	0.530
	7 :30	5.71	2.0	0.902	17.96	0.319	0.583	0.226	0.676
	7 :40	5.17	2.0	0.907	17.09	0.319	0.588	0.226	0.681
	7 :50	4.11	1.8	0.773	15.64	0.303	0.471	0.200	0.573
8	8 :00	5.05	2.0	0.763	16.89	0.319	0.444	0.226	0.537
	8 :10	5.65	1.9	0.892	18.10	0.311	0.581	0.213	0.679
	8 :20	4.26	1.9	0.826	15.71	0.311	0.515	0.213	0.613
	8 :30	5.62	1.8	0.823	18.29	0.303	0.521	0.200	0.623
	8 :40	4.56	2.0	0.848	16.05	0.319	0.529	0.226	0.622
	8 :50	4.08	1.9	0.720	15.38	0.311	0.409	0.213	0.507
	9 :00	5.50	2.0	0.798	17.63	0.319	0.479	0.226	0.572
	9 :10	5.29	1.9	0.899	17.51	0.311	0.588	0.213	0.686
	9 :20	4.20	2.0	0.791	15.40	0.319	0.472	0.226	0.565
	9 :30	4.87	2.0	0.756	16.59	0.319	0.437	0.226	0.530
	9 :40	4.84	2.0	0.809	16.54	0.319	0.490	0.226	0.583
	9 :50	5.86	2.0	0.892	18.19	0.319	0.573	0.226	0.666
10	10 :00	4.47	1.9	0.861	16.10	0.311	0.550	0.213	0.648
	10 :10	5.47	2.0	0.828	17.58	0.319	0.509	0.226	0.602
	10 :20	5.17	1.9	0.887	17.31	0.311	0.576	0.213	0.674
	10 :30	4.47	2.0	0.803	15.89	0.319	0.484	0.226	0.577
	10 :40	5.65	2.1	0.843	17.65	0.327	0.517	0.239	0.604
	10 :50	4.17	2.0	0.818	15.35	0.319	0.499	0.226	0.592
	11 :00	4.56	1.9	0.728	16.26	0.311	0.417	0.213	0.515
	11 :10	4.77	2.1	0.778	16.22	0.327	0.451	0.239	0.539

No. 001

Area : DIEGO MARTIN(JEDE st)

Date : Dec. 13-14. 1989

$$Q_x = Q_o \times (H_x/H_o)^n$$

--(n = 0.5)-- --(n = 1.15)--
 --(orifice)-- --(crack)--

TIME hour min	METERED	METERED	Qtotal m3	Leak hole d(mm)	< TYPE - A >		< TYPE - B >	
	Q (m3/h)	PRESSURE (kg/cm2)			Leak QA1(m3)	Demand QA2(m3)	Leak QB1(m3)	Demand QB2(m3)
11 :20	5.11	2.2	0.823	16.59	0.334	0.489	0.252	0.571
11 :30	4.93	2.2	0.837	16.30	0.334	0.502	0.252	0.585
11 :40	5.95	2.1	0.907	18.11	0.327	0.580	0.239	0.668
11 :50	5.92	2.2	0.989	17.86	0.334	0.655	0.252	0.737
12 :00	4.87	2.0	0.899	16.59	0.319	0.580	0.226	0.673
12 :10	5.80	2.1	0.889	17.88	0.327	0.562	0.239	0.650
12 :20	4.44	2.3	0.853	15.29	0.342	0.511	0.265	0.588
12 :30	4.99	2.2	0.786	16.39	0.334	0.451	0.252	0.534
12 :40	4.90	2.3	0.824	16.07	0.342	0.482	0.265	0.559
12 :50	4.41	2.4	0.776	15.08	0.349	0.426	0.279	0.497
13 :00	4.56	2.4	0.748	15.33	0.349	0.398	0.279	0.469
13 :10	3.75	2.4	0.693	13.91	0.349	0.343	0.279	0.414
13 :20	3.53	2.4	0.607	13.49	0.349	0.257	0.279	0.328
13 :30	4.26	2.3	0.649	14.98	0.342	0.307	0.265	0.384
13 :40	4.17	2.3	0.703	14.82	0.342	0.360	0.265	0.437
13 :50	4.08	2.3	0.688	14.66	0.342	0.345	0.265	0.422
14 :00	4.20	2.5	0.690	14.57	0.357	0.333	0.292	0.398
14 :10	4.77	2.0	0.748	16.42	0.319	0.429	0.226	0.522
14 :20	4.11	2.2	0.740	14.88	0.334	0.406	0.252	0.488
14 :30	4.65	2.2	0.730	15.83	0.334	0.396	0.252	0.478
14 :40	3.63	2.1	0.690	14.15	0.327	0.363	0.239	0.451
14 :50	2.81	2.1	0.537	12.45	0.327	0.210	0.239	0.298
15 :00	2.90	2.2	0.476	12.50	0.334	0.141	0.252	0.224
15 :10	2.08	2.1	0.415	10.71	0.327	0.088	0.239	0.176
15 :20	2.63	2.1	0.393	12.04	0.327	0.066	0.239	0.154
15 :30	2.51	2.0	0.428	11.91	0.319	0.109	0.226	0.202
15 :40	2.60	2.0	0.426	12.12	0.319	0.107	0.226	0.200
15 :50	3.20	2.1	0.483	13.28	0.327	0.157	0.239	0.244
16 :00	2.42	2.0	0.468	11.69	0.319	0.149	0.226	0.242
16 :10	2.60	1.9	0.418	12.28	0.311	0.107	0.213	0.205
16 :20	2.51	1.9	0.426	12.06	0.311	0.115	0.213	0.213
16 :30	3.11	2.0	0.468	13.25	0.319	0.149	0.226	0.242
16 :40	2.81	1.9	0.493	12.76	0.311	0.182	0.213	0.280
TOTAL	---	---	91.554	---	50.268	41.286	40.769	50.786
Average	3.81	2.42	0.636	14.029	54.91%	45.09%	44.53%	55.47%
MAX	5.95	3.40	0.989	18.293	0.416	0.655	0.416	0.737
MIN	2.08	1.70	0.393	10.366	0.294	0.000	0.187	0.000

kg/cm2 m3/10 min
 Leakage at Night: 3.40 0.416 10.428 : 1:50 a.m.
 Estimated night demand : 0.000

Nos. of house [A] 69 houses
 persons/house [B] 4.4 pesons/house
 A * B [C] 303.6 persons

< TYPE - A > < TYPE - B >
 Water Demand [D] 41.29 M3 50.79 M3
 l/day/capita D/C 135.99 l/d/c 167.28 l/d/c

No. 002
 Area : VICTORIA GARDEN-01
 Date : Dec. 7-8, 1989

$$Q_x = Q_0 \times (H_x/H_0)^n$$

--(n = 0.5)-- --(n = 1.15)--
 --(orifice)-- --(cracks)--

TIME hour min	METERED	METERED	Qtotal m3	Leak hole d(mm)	< TYPE - A >		< TYPE - B >	
	Q (m3/h)	PRESSURE (kg/cm2)			Leak QA1(m3)	Demand QA2(m3)	Leak QB1(m3)	Demand QB2(m3)
15 :35	24.98	1.1	---	43.62	---	---	---	---
15 :45	23.60	1.1	4.048	42.40	2.905	1.144	1.661	2.388
15 :55	24.92	1.0	4.043	44.62	2.770	1.274	1.488	2.555
16 :05	27.54	1.0	4.372	46.91	2.770	1.602	1.488	2.883
16 :15	24.71	1.0	4.354	44.43	2.770	1.585	1.488	2.866
16 :25	24.54	1.0	4.104	44.28	2.770	1.335	1.488	2.616
16 :35	25.61	1.0	4.179	45.23	2.770	1.410	1.488	2.691
16 :45	25.16	1.1	4.231	43.78	2.905	1.326	1.661	2.570
16 :55	24.40	1.1	4.130	43.11	2.905	1.225	1.661	2.469
17 :05	26.37	1.1	4.231	44.82	2.905	1.326	1.661	2.570
17 :15	25.30	1.1	4.306	43.90	2.905	1.401	1.661	2.645
17 :25	24.54	1.1	4.153	43.23	2.905	1.249	1.661	2.493
17 :35	22.74	1.0	3.940	42.62	2.770	1.170	1.488	2.452
17 :45	22.36	1.0	3.758	42.26	2.770	0.989	1.488	2.270
17 :55	23.09	1.0	3.788	42.95	2.770	1.018	1.488	2.299
18 :05	25.92	1.0	4.084	45.50	2.770	1.315	1.488	2.596
18 :15	24.67	1.0	4.216	44.39	2.770	1.446	1.488	2.728
18 :25	23.47	1.0	4.012	43.30	2.770	1.242	1.488	2.523
18 :35	24.23	1.0	3.975	44.00	2.770	1.205	1.488	2.487
18 :45	23.98	1.0	4.018	43.77	2.770	1.248	1.488	2.529
18 :55	25.88	1.0	4.155	45.47	2.770	1.385	1.488	2.667
19 :05	26.33	1.0	4.351	45.86	2.770	1.581	1.488	2.863
19 :15	25.12	1.0	4.288	44.80	2.770	1.518	1.488	2.799
19 :25	19.19	1.0	3.693	39.15	2.770	0.923	1.488	2.204
19 :35	26.54	1.2	3.811	43.99	3.034	0.777	1.835	1.975
19 :45	23.85	0.9	4.199	44.82	2.627	1.572	1.318	2.881
19 :55	27.02	1.2	4.239	44.39	3.034	1.205	1.835	2.404
20 :05	28.44	1.2	4.622	45.54	3.034	1.588	1.835	2.786
20 :15	28.37	1.3	4.734	44.58	3.158	1.576	2.012	2.722
20 :25	25.99	1.1	4.530	44.49	2.905	1.625	1.661	2.869
20 :35	26.43	1.1	4.368	44.87	2.905	1.464	1.661	2.708
20 :45	27.54	1.3	4.498	43.93	3.158	1.340	2.012	2.485
20 :55	29.33	1.3	4.739	45.33	3.158	1.581	2.012	2.727
21 :05	27.99	1.4	4.777	43.47	3.277	1.500	2.191	2.585
21 :15	28.75	1.4	4.728	44.06	3.277	1.451	2.191	2.537
21 :25	29.20	1.6	4.829	42.94	3.503	1.326	2.555	2.274
21 :35	27.12	1.6	4.693	41.39	3.503	1.190	2.555	2.138
21 :45	27.02	1.7	4.512	40.69	3.611	0.901	2.740	1.772
21 :55	27.37	1.7	4.533	40.95	3.611	0.921	2.740	1.793
22 :05	27.54	1.7	4.576	41.08	3.611	0.965	2.740	1.836
22 :15	27.88	1.8	4.618	40.74	3.716	0.903	2.926	1.693
22 :25	29.64	1.9	4.793	41.45	3.818	0.976	3.114	1.680
22 :35	29.26	2.1	4.908	40.16	4.014	0.895	3.493	1.415
22 :45	27.57	2.1	4.736	38.99	4.014	0.722	3.493	1.243
22 :55	29.61	2.2	4.765	39.93	4.108	0.657	3.685	1.080
23 :05	29.06	2.3	4.889	39.13	4.200	0.689	3.879	1.011
23 :15	28.85	2.3	4.826	38.98	4.200	0.626	3.879	0.947
23 :25	28.95	2.4	4.817	38.64	4.291	0.526	4.073	0.744
23 :35	28.33	2.4	4.773	38.22	4.291	0.483	4.073	0.700
23 :45	30.20	2.5	4.878	39.06	4.379	0.498	4.269	0.609
23 :55	28.71	2.5	4.909	38.09	4.379	0.530	4.269	0.640
0 :05	29.68	2.5	4.866	38.72	4.379	0.487	4.269	0.597
0 :15	28.64	2.4	4.860	38.43	4.291	0.569	4.073	0.787
0 :25	29.47	2.6	4.843	38.21	4.466	0.377	4.466	0.377
0 :35	28.71	2.6	4.848	37.71	4.466	0.383	4.466	0.383
0 :45	27.92	2.7	4.719	36.84	4.551	0.168	4.664	0.055

No. 002

Area : VICTORIA GARDEN-01

Date : Dec. 7-8, 1989

$$Q_x = Q_o \times (H_x/H_o)^n$$

---(n = 0.5)--- ---(n = 1.15)---
 ---(orifice)--- ---(cracks)---

TIME	hour	min	METERED	METERED	Qtotal	Leak	< TYPE - A >		< TYPE - B >	
			Q	PRESSURE			Leak	Demand	Leak	Demand
			(m3/h)	(kg/cm2)	m3	d(mm)	QA1(m3)	QA2(m3)	QB1(m3)	QB2(m3)
	0	:55	27.85	2.6	4.648	37.15	4.466	0.182	4.466	0.182
	1	:05	26.43	2.5	4.523	36.54	4.379	0.144	4.269	0.254
	1	:15	26.71	2.4	4.428	37.11	4.291	0.138	4.073	0.355
	1	:25	27.44	2.5	4.513	37.23	4.379	0.133	4.269	0.244
	1	:35	28.92	2.6	4.697	37.85	4.466	0.231	4.466	0.231
	1	:45	26.47	2.6	4.616	36.21	4.466	0.150	4.466	0.150
	1	:55	27.12	2.6	4.466	36.66	4.466	0.000	4.466	0.000
2	2	:05	27.68	2.6	4.567	37.03	4.466	0.101	4.466	0.101
	2	:15	27.64	2.6	4.610	37.01	4.466	0.144	4.466	0.144
	2	:25	27.57	2.5	4.601	37.32	4.379	0.222	4.269	0.332
	2	:35	26.68	2.5	4.521	36.72	4.379	0.142	4.269	0.252
	2	:45	26.68	2.6	4.447	36.36	4.466	-0.019	4.466	-0.019
	2	:55	26.95	2.6	4.469	36.54	4.466	0.003	4.466	0.003
	3	:05	27.47	2.6	4.535	36.89	4.466	0.069	4.466	0.069
	3	:15	26.81	2.6	4.523	36.45	4.466	0.058	4.466	0.058
	3	:25	26.95	2.6	4.480	36.54	4.466	0.014	4.466	0.014
	3	:35	27.33	2.7	4.523	36.45	4.551	-0.028	4.664	-0.141
	3	:45	27.26	2.6	4.549	36.75	4.466	0.083	4.466	0.083
	3	:55	26.81	2.6	4.506	36.45	4.466	0.040	4.466	0.040
4	4	:05	26.16	2.6	4.414	36.00	4.466	-0.052	4.466	-0.052
	4	:15	26.05	2.6	4.351	35.93	4.466	-0.115	4.466	-0.115
	4	:25	25.74	2.5	4.316	36.06	4.379	-0.063	4.269	0.047
	4	:35	25.99	2.4	4.311	36.61	4.291	0.020	4.073	0.238
	4	:45	27.09	2.4	4.423	37.38	4.291	0.133	4.073	0.350
	4	:55	27.12	2.4	4.518	37.40	4.291	0.227	4.073	0.444
	5	:05	27.06	2.6	4.515	36.62	4.466	0.049	4.466	0.049
	5	:15	26.81	2.6	4.489	36.45	4.466	0.023	4.466	0.023
	5	:25	27.02	2.6	4.486	36.59	4.466	0.020	4.466	0.020
	5	:35	27.88	2.6	4.575	37.17	4.466	0.109	4.466	0.109
	5	:45	27.40	2.5	4.607	37.21	4.379	0.228	4.269	0.338
	5	:55	28.71	2.5	4.676	38.09	4.379	0.297	4.269	0.407
6	6	:05	29.54	2.3	4.854	39.45	4.200	0.654	3.879	0.976
	6	:15	27.02	2.2	4.713	38.15	4.108	0.605	3.685	1.028
	6	:25	26.78	2.0	4.483	38.89	3.917	0.567	3.303	1.181
	6	:35	27.61	1.4	4.533	43.18	3.277	1.255	2.191	2.341
	6	:45	25.74	1.3	4.446	42.47	3.158	1.288	2.012	2.433
	6	:55	26.64	1.0	4.365	46.13	2.770	1.595	1.488	2.877
	7	:05	23.16	0.9	4.150	44.16	2.627	1.523	1.318	2.832
	7	:15	24.33	0.8	3.958	46.62	2.477	1.480	1.151	2.806
	7	:25	21.12	0.4	3.788	51.65	1.752	2.036	0.519	3.269
	7	:35	20.74	0.4	3.488	51.18	1.752	1.737	0.519	2.969
	7	:45	19.05	0.4	3.316	49.05	1.752	1.564	0.519	2.797
	7	:55	19.01	0.5	3.172	46.34	1.958	1.213	0.671	2.501
8	8	:05	18.84	0.5	3.154	46.14	1.958	1.196	0.671	2.484
	8	:15	21.39	0.5	3.353	49.16	1.958	1.394	0.671	2.682
	8	:25	21.91	0.5	3.608	49.75	1.958	1.650	0.671	2.938
	8	:35	24.12	0.5	3.836	52.20	1.958	1.877	0.671	3.165
	8	:45	23.43	0.5	3.963	51.45	1.958	2.004	0.671	3.292
	8	:55	25.16	0.5	4.049	53.32	1.958	2.091	0.671	3.379
	9	:05	24.60	0.5	4.147	52.72	1.958	2.188	0.671	3.476
	9	:15	24.60	0.4	4.100	55.74	1.752	2.348	0.519	3.581
	9	:25	25.61	0.4	4.184	56.88	1.752	2.433	0.519	3.665
	9	:35	24.78	0.5	4.199	52.91	1.958	2.241	0.671	3.529
	9	:45	25.26	0.6	4.170	51.04	2.145	2.025	0.827	3.343
	9	:55	25.26	0.6	4.210	51.04	2.145	2.065	0.827	3.383
10	10	:05	25.16	0.6	4.202	50.94	2.145	2.056	0.827	3.375

No. 002

Area : VICTORIA GARDEN-01

Date : Dec. 7-8. 1989

$$Q_x = Q_o \times (H_x/H_o)^n$$

--(n = 0.5)-- --(n = 1.15)--

--(orifice)-- --(cracks)--

TIME hour min	METERED	METERED	Qtotal m3	Leak hole d(mm)	< TYPE - A >		< TYPE - B >	
	Q (m3/h)	PRESSURE (kg/cm2)			Leak QA1(m3)	Demand QA2(m3)	Leak QB1(m3)	Demand QB2(m3)
10 :15	24.23	0.6	4.116	49.99	2.145	1.971	0.827	3.289
10 :25	24.50	0.6	4.061	50.27	2.145	1.916	0.827	3.234
10 :35	22.46	0.6	3.913	48.13	2.145	1.768	0.827	3.086
10 :45	20.67	0.5	3.594	48.32	1.958	1.636	0.671	2.924
10 :55	19.81	0.5	3.373	47.31	1.958	1.415	0.671	2.703
11 :05	20.50	0.4	3.359	50.89	1.752	1.608	0.519	2.840
11 :15	19.67	0.3	3.348	53.56	1.517	1.831	0.373	2.975
11 :25	19.46	0.3	3.261	53.28	1.517	1.744	0.373	2.888
11 :35	17.98	0.3	3.120	51.21	1.517	1.603	0.373	2.747
11 :45	18.56	0.4	3.045	48.42	1.752	1.293	0.519	2.526
11 :55	18.56	0.4	3.093	48.42	1.752	1.342	0.519	2.574
12 :05	19.70	0.3	3.188	53.60	1.517	1.671	0.373	2.816
12 :15	20.67	0.3	3.364	54.91	1.517	1.847	0.373	2.991
12 :25	21.74	0.5	3.534	49.56	1.958	1.576	0.671	2.864
12 :35	22.33	0.6	3.673	47.99	2.145	1.527	0.827	2.845
12 :45	23.02	0.7	3.779	46.88	2.317	1.462	0.988	2.792
12 :55	21.12	0.8	3.678	43.43	2.477	1.201	1.151	2.527
13 :05	22.53	0.8	3.638	44.86	2.477	1.160	1.151	2.486
13 :15	21.08	0.8	3.634	43.39	2.477	1.157	1.151	2.483
13 :25	21.22	0.8	3.525	43.54	2.477	1.048	1.151	2.374
13 :35	23.12	0.8	3.695	45.44	2.477	1.218	1.151	2.544
13 :45	20.50	0.8	3.635	42.79	2.477	1.158	1.151	2.484
13 :55	23.91	0.7	3.701	47.78	2.317	1.384	0.988	2.713
14 :05	23.67	0.8	3.965	45.98	2.477	1.488	1.151	2.814
14 :15	24.60	0.9	4.023	45.51	2.627	1.395	1.318	2.704
14 :25	24.33	0.9	4.078	45.26	2.627	1.450	1.318	2.759
14 :35	24.23	0.6	4.047	49.99	2.145	1.901	0.827	3.220
14 :45	24.05	1.0	4.023	43.83	2.770	1.254	1.488	2.535
14 :55	23.64	1.0	3.974	43.46	2.770	1.205	1.488	2.486
15 :05	22.67	1.0	3.859	42.56	2.770	1.090	1.488	2.371
15 :15	23.57	0.8	3.853	45.88	2.477	1.376	1.151	2.702
15 :25	23.53	1.0	3.925	43.36	2.770	1.155	1.488	2.437
15 :35	22.78	1.2	3.859	40.76	3.034	0.825	1.835	2.024
TOTAL	---	---	605.137	---	453.311	151.825	329.259	275.878
Average	25.20	1.41	4.202	43.351	74.91%	25.09%	54.41%	45.59%
MAX	30.20	2.70	4.909	56.876	4.551	2.433	4.664	3.665
MIN	17.98	0.30	3.045	35.925	1.517	-0.115	0.373	-0.141

Leakage at Night: $\frac{\text{kg/cm}^2}{2.60}$ $\frac{\text{m}^3/10 \text{ min}}{4.466}$ 36.656 : 1:55 a.m.
 Estimated night demand : 0.000

Nos. of house [A] 91 houses
 persons/house [B] 4.4 pesons/house
 A * B [C] 400.4 persons

< TYPE - A > < TYPE - B >
 Water Demand [D] 151.83 M3 275.88 M3
 l/day/capita D/C 379.18 1/d/c 689.00 1/d/c

No. 003

Area : VICTORIA GARDEN-02

Date : Dec. 12-13. 1989

$$Qx = Qo \times (Hx/Ho)^n$$

---(n = 0.5)--- ---(n = 1.15)---

---(orifice)--- ---(crack)---

TIME hour min	METERED		Qtotal m3	Leak hole d(mm)	< TYPE - A >		< TYPE - B >	
	Q (m3/h)	PRESSURE (kg/cm2)			Leak QA1(m3)	Demand QA2(m3)	Leak QB1(m3)	Demand QB2(m3)
13 40	12.11	1.8	---	26.85	---	---	---	---
13 50	8.76	1.5	1.739	23.90	0.948	0.791	0.527	1.212
14 0	8.70	1.5	1.455	23.82	0.948	0.507	0.527	0.928
14 10	12.87	1.4	1.798	29.48	0.916	0.881	0.487	1.310
14 20	11.89	1.5	2.063	27.85	0.948	1.115	0.527	1.536
14 30	11.51	1.5	1.950	27.40	0.948	1.002	0.527	1.423
14 40	11.58	1.7	1.924	26.64	1.009	0.915	0.609	1.315
14 50	10.34	1.6	1.827	25.55	0.979	0.847	0.568	1.259
15 0	10.88	1.7	1.768	25.82	1.009	0.759	0.609	1.159
15 10	10.37	1.6	1.771	25.59	0.979	0.792	0.568	1.203
15 20	9.68	1.7	1.671	24.35	1.009	0.661	0.609	1.062
15 30	10.12	1.8	1.650	24.55	1.039	0.611	0.650	1.000
15 40	9.27	1.7	1.616	23.83	1.009	0.606	0.609	1.007
15 50	10.22	1.7	1.624	25.02	1.009	0.615	0.609	1.015
16 0	6.93	1.7	1.429	20.61	1.009	0.420	0.609	0.820
16 10	9.39	1.7	1.360	23.99	1.009	0.351	0.609	0.751
16 20	10.63	1.8	1.668	25.16	1.039	0.630	0.650	1.018
16 30	7.78	1.8	1.534	21.52	1.039	0.495	0.650	0.884
16 40	10.56	1.7	1.528	25.44	1.009	0.519	0.609	0.919
16 50	9.17	1.6	1.644	24.07	0.979	0.665	0.568	1.076
17 0	10.66	1.7	1.653	25.56	1.009	0.643	0.609	1.044
17 10	9.65	1.7	1.693	24.32	1.009	0.683	0.609	1.084
17 20	11.73	1.7	1.782	26.81	1.009	0.772	0.609	1.173
17 30	11.23	1.6	1.913	26.63	0.979	0.934	0.568	1.345
17 40	12.46	1.6	1.974	28.05	0.979	0.995	0.568	1.406
17 50	11.55	1.8	2.001	26.22	1.039	0.962	0.650	1.351
18 0	7.72	1.8	1.606	21.44	1.039	0.567	0.650	0.956
18 10	8.82	1.5	1.378	23.99	0.948	0.430	0.527	0.851
18 20	11.77	1.6	1.716	27.26	0.979	0.737	0.568	1.148
18 30	10.98	1.6	1.896	26.33	0.979	0.917	0.568	1.328
18 40	11.01	1.6	1.833	26.37	0.979	0.853	0.568	1.265
18 50	9.93	1.8	1.745	24.32	1.039	0.706	0.650	1.095
19 0	9.30	1.8	1.603	23.53	1.039	0.564	0.650	0.952
19 10	10.88	1.8	1.682	25.45	1.039	0.643	0.650	1.031
19 20	9.33	1.8	1.684	23.57	1.039	0.645	0.650	1.034
19 30	12.53	1.7	1.822	27.71	1.009	0.812	0.609	1.213
19 40	12.43	1.8	2.080	27.21	1.039	1.041	0.650	1.430
19 50	14.01	1.7	2.203	29.30	1.009	1.194	0.609	1.594
20 0	13.89	1.8	2.325	28.76	1.039	1.286	0.650	1.675
20 10	13.54	2.0	2.286	27.66	1.095	1.191	0.734	1.552
20 20	11.86	2.0	2.117	25.88	1.095	1.022	0.734	1.383
20 30	12.15	2.1	2.001	25.88	1.122	0.879	0.776	1.224
20 40	10.44	2.3	1.883	23.45	1.174	0.708	0.862	1.021
20 50	11.61	2.1	1.838	25.30	1.122	0.716	0.776	1.061
21 0	14.11	2.1	2.143	27.89	1.122	1.021	0.776	1.367
21 10	11.55	2.3	2.138	24.67	1.174	0.964	0.862	1.276
21 20	11.39	2.4	1.912	24.24	1.199	0.712	0.905	1.006
21 30	11.80	2.5	1.933	24.42	1.224	0.708	0.949	0.984
21 40	11.86	2.6	1.972	24.24	1.248	0.723	0.993	0.979
21 50	11.32	2.7	1.932	23.46	1.272	0.660	1.037	0.895
22 0	11.61	2.8	1.911	23.54	1.295	0.615	1.081	0.830
22 10	8.98	3.0	1.716	20.35	1.341	0.375	1.170	0.546
22 20	8.16	3.0	1.428	19.40	1.341	0.087	1.170	0.258
22 30	9.01	3.1	1.431	20.22	1.363	0.068	1.215	0.216
22 40	9.46	3.1	1.539	20.72	1.363	0.176	1.215	0.324
22 50	7.84	3.0	1.442	19.02	1.341	0.101	1.170	0.272

No. 003
 Area : VICTORIA GARDEN-02
 Date : Dec. 12-13. 1989

$$Q_x = Q_0 \times (H_x/H_0)^n$$

--(n = 0.5)-- --(n = 1.15)--
 --(orifice)-- --(crack)--

TIME	METERED		METERED	Qtotal	Leak	< TYPE - A >		< TYPE - B >		
	hour	min	Q			Leak	Leak	Demand	Leak	Demand
			Q	m3	d(mm)	QA1(m3)	QA2(m3)	QB1(m3)	QB2(m3)	
0	23	0	8.79	3.2	1.386	19.81	1.385	0.001	1.260	0.126
	23	10	8.89	3.3	1.473	19.77	1.406	0.067	1.306	0.168
	23	20	9.49	3.6	1.532	19.99	1.469	0.063	1.443	0.089
	23	30	8.35	3.7	1.487	18.62	1.489	-0.002	1.489	-0.002
	23	40	9.01	3.7	1.447	19.34	1.489	-0.042	1.489	-0.042
	23	50	8.00	3.6	1.418	18.35	1.469	-0.051	1.443	-0.025
	0	0	8.51	3.8	1.376	18.67	1.509	-0.133	1.536	-0.160
	0	10	9.68	3.4	1.516	20.48	1.428	0.088	1.351	0.165
	0	20	9.52	3.7	1.600	19.88	1.489	0.111	1.489	0.111
	0	30	9.52	3.9	1.587	19.62	1.529	0.058	1.582	0.005
	0	40	9.74	3.8	1.605	19.98	1.509	0.096	1.536	0.069
	0	50	9.39	3.9	1.594	19.49	1.529	0.065	1.582	0.012
	1	0	9.80	3.7	1.599	20.17	1.489	0.110	1.489	0.110
	1	10	8.87	3.6	1.556	19.33	1.469	0.087	1.443	0.113
	1	20	9.24	3.6	1.509	19.72	1.469	0.040	1.443	0.066
	1	30	9.20	3.6	1.537	19.68	1.469	0.068	1.443	0.094
	1	40	9.99	3.6	1.599	20.51	1.469	0.130	1.443	0.156
	1	50	9.99	3.6	1.665	20.51	1.469	0.196	1.443	0.222
2	2	0	9.01	3.6	1.583	19.48	1.469	0.114	1.443	0.140
	2	10	9.55	3.6	1.547	20.05	1.469	0.078	1.443	0.104
	2	20	9.36	3.6	1.576	19.85	1.469	0.107	1.443	0.133
	2	30	9.27	3.6	1.553	19.76	1.469	0.084	1.443	0.110
	2	40	9.20	3.7	1.539	19.55	1.489	0.050	1.489	0.050
	2	50	9.52	3.7	1.560	19.88	1.489	0.071	1.489	0.071
	3	0	8.95	3.7	1.539	19.28	1.489	0.050	1.489	0.050
	3	10	8.92	3.7	1.489	19.25	1.489	0.000	1.489	0.000
	3	20	10.50	3.7	1.618	20.88	1.489	0.129	1.489	0.129
	3	30	9.99	3.7	1.708	20.37	1.489	0.218	1.489	0.218
	3	40	9.55	3.7	1.628	19.92	1.489	0.139	1.489	0.139
	3	50	9.11	3.6	1.555	19.58	1.469	0.086	1.443	0.112
4	4	0	9.11	3.4	1.518	19.87	1.428	0.091	1.351	0.167
	4	10	8.32	3.4	1.453	18.99	1.428	0.025	1.351	0.101
	4	20	8.70	3.1	1.418	19.87	1.363	0.055	1.215	0.203
	4	30	8.60	3.2	1.442	19.60	1.385	0.057	1.260	0.181
	4	40	9.27	3.2	1.489	20.35	1.385	0.104	1.260	0.229
	4	50	9.17	3.3	1.537	20.08	1.406	0.130	1.306	0.231
	5	0	7.40	3.3	1.381	18.04	1.406	-0.026	1.306	0.075
	5	10	7.65	2.6	1.254	19.47	1.248	0.006	0.993	0.262
	5	20	7.81	3.0	1.288	18.98	1.341	-0.053	1.170	0.118
	5	30	7.65	2.9	1.288	18.94	1.318	-0.030	1.125	0.163
	5	40	9.61	2.7	1.438	21.62	1.272	0.166	1.037	0.402
	5	50	8.41	2.7	1.502	20.22	1.272	0.230	1.037	0.465
6	6	0	7.30	2.4	1.309	19.40	1.199	0.110	0.905	0.404
	6	10	11.48	2.2	1.565	24.87	1.148	0.417	0.819	0.746
	6	20	13.89	1.7	2.114	29.17	1.009	1.105	0.609	1.505
	6	30	14.46	1.5	2.363	30.71	0.948	1.414	0.527	1.835
	6	40	15.25	1.0	2.476	34.90	0.774	1.702	0.331	2.145
	6	50	13.16	1.4	2.368	29.81	0.916	1.451	0.487	1.880
	7	0	18.03	1.4	2.599	34.89	0.916	1.683	0.487	2.112
	7	10	15.88	1.3	2.826	33.36	0.883	1.943	0.447	2.379
	7	20	14.80	1.3	2.557	32.20	0.883	1.674	0.447	2.109
	7	30	14.01	1.3	2.401	31.33	0.883	1.518	0.447	1.954
	7	40	13.29	1.3	2.275	30.52	0.883	1.392	0.447	1.828
	7	50	11.70	1.2	2.083	29.21	0.848	1.234	0.408	1.675
8	8	0	12.87	1.2	2.048	30.64	0.848	1.199	0.408	1.640
	8	10	13.25	1.2	2.177	31.09	0.848	1.329	0.408	1.769

No. 003

Area : VICTORIA GARDEN-02

Date : Dec. 12-13, 1989

$$Q_x = Q_o \times (H_x/H_o)^n$$

--(n = 0.5)-- --(n = 1.15)--
 --(orifice)-- --(crack)--

TIME hour min	METERED	METERED	Qtotal m3	Leak hole d(mm)	< TYPE - A >		< TYPE - B >	
	Q (m3/h)	PRESSURE (kg/cm2)			Leak	Demand	Leak	Demand
					QA1(m3)	QA2(m3)	QB1(m3)	QB2(m3)
8 20	10.91	1.2	2.013	28.21	0.848	1.165	0.408	1.605
8 30	14.08	1.0	2.083	33.54	0.774	1.308	0.331	1.752
8 40	15.09	0.9	2.431	35.65	0.734	1.696	0.293	2.138
8 50	12.27	0.8	2.280	33.10	0.692	1.588	0.256	2.024
9 0	14.36	1.2	2.219	32.36	0.848	1.371	0.408	1.811
9 10	11.92	1.0	2.190	30.86	0.774	1.416	0.331	1.859
9 20	14.84	1.1	2.230	33.62	0.812	1.418	0.369	1.861
9 30	13.92	1.2	2.397	31.86	0.848	1.549	0.408	1.989
9 40	12.15	1.0	2.173	31.16	0.774	1.398	0.331	1.842
9 50	12.94	1.3	2.091	30.11	0.883	1.208	0.447	1.644
10 0	12.62	0.8	2.130	33.57	0.692	1.438	0.256	1.874
10 10	12.49	1.4	2.093	29.04	0.916	1.176	0.487	1.605
10 20	7.43	1.4	1.660	22.40	0.916	0.744	0.487	1.173
10 30	9.11	1.4	1.378	24.80	0.916	0.462	0.487	0.891
10 40	8.73	1.4	1.487	24.28	0.916	0.571	0.487	1.000
10 50	9.84	1.3	1.548	26.26	0.883	0.665	0.447	1.100
11 0	10.63	1.2	1.706	27.84	0.848	0.858	0.408	1.298
11 10	12.15	1.3	1.898	29.18	0.883	1.016	0.447	1.451
11 20	9.49	1.4	1.803	25.31	0.916	0.887	0.487	1.316
11 30	11.36	1.2	1.738	28.78	0.848	0.889	0.408	1.330
11 40	9.61	1.4	1.748	25.47	0.916	0.831	0.487	1.260
11 50	11.45	1.4	1.755	27.80	0.916	0.839	0.487	1.268
12 0	12.18	1.4	1.969	28.68	0.916	1.053	0.487	1.482
12 10	9.24	1.6	1.785	24.16	0.979	0.806	0.568	1.217
12 20	10.88	1.6	1.677	26.21	0.979	0.697	0.568	1.109
12 30	9.08	1.6	1.663	23.95	0.979	0.684	0.568	1.095
12 40	8.89	1.7	1.498	23.34	1.009	0.488	0.609	0.889
12 50	11.80	1.6	1.724	27.30	0.979	0.745	0.568	1.156
13 0	8.41	1.6	1.684	23.05	0.979	0.705	0.568	1.116
13 10	7.75	1.5	1.347	22.48	0.948	0.398	0.527	0.819
13 20	12.34	1.5	1.674	28.37	0.948	0.726	0.527	1.147
13 30	10.56	1.7	1.908	25.44	1.009	0.899	0.609	1.299
13 40	8.92	1.7	1.623	23.38	1.009	0.614	0.609	1.014
TOTAL	---	---	254.373	---	161.764	92.609	119.760	134.613
Average	10.60	2.20	1.766	24.578	63.59%	36.41%	47.08%	52.92%
MAX	18.03	3.90	2.826	35.647	1.529	1.943	1.582	2.379
MIN	6.93	0.80	1.254	18.040	0.692	-0.133	0.256	-0.160

Leakage at Night: $\frac{\text{kg/cm}^2}{\text{m}^3/10 \text{ min}}$ 3.70 1.489 19.247 : 3:10 a.m.
 Estimated night demand : 0.000

Nos. of house [A] 91 houses
 persons/house [B] 4.4 pesons/house
 A * B [C] 400.4 persons

< TYPE - A > < TYPE - B >
 Water Demand [D] 92.61 M3 134.61 M3
 l/day/capita D/C 231.29 l/d/c 336.20 l/d/c

No. 004

Area : DIEGO MARTIN(PAREL PARK)

Date : Dec. 18-19, 1989

$$Q_x = Q_o \times (H_x/H_o)^n$$

--(n = 0.5)-- --(n = 1.15)--

--(orifice)-- --(crack)--

TIME	METERED		METERED	Qtotal	Leak	< TYPE - A >		< TYPE - B >		
	hour	min	Q			Leak	Demand	Leak	Demand	
			PRESSURE	m3	hole	QA1(m3)	QA2(m3)	QB1(m3)	QB2(m3)	
		(m3/h)	(kg/cm2)		d(mm)					
	10	20	5.53	1.1	---	20.52	---	---	---	
	10	30	6.08	1.2	0.968	21.06	0.479	0.488	0.305	0.662
	10	40	6.29	1.3	1.031	20.99	0.499	0.532	0.335	0.696
	10	50	6.89	1.3	1.098	21.97	0.499	0.600	0.335	0.764
	11	0	6.41	1.3	1.108	21.19	0.499	0.610	0.335	0.774
	11	10	6.38	1.4	1.066	20.75	0.517	0.548	0.365	0.701
	11	20	6.89	1.4	1.106	21.57	0.517	0.588	0.365	0.741
	11	30	6.80	1.3	1.141	21.83	0.499	0.642	0.335	0.806
	11	40	7.56	1.3	1.197	23.02	0.499	0.698	0.335	0.862
	11	50	6.98	1.2	1.212	22.56	0.479	0.733	0.305	0.906
12	12	0	6.20	1.2	1.098	21.26	0.479	0.619	0.305	0.793
	12	10	6.62	1.3	1.068	21.54	0.499	0.570	0.335	0.734
	12	20	6.23	1.4	1.071	20.51	0.517	0.553	0.365	0.706
	12	30	6.65	1.5	1.073	20.83	0.536	0.538	0.395	0.679
	12	40	6.20	1.5	1.071	20.11	0.536	0.535	0.395	0.676
	12	50	7.04	1.5	1.103	21.43	0.536	0.568	0.395	0.709
	13	0	6.80	1.5	1.153	21.06	0.536	0.618	0.395	0.759
	13	10	6.29	1.5	1.091	20.26	0.536	0.555	0.395	0.696
	13	20	6.83	1.5	1.093	21.11	0.536	0.558	0.395	0.699
	13	30	6.80	1.5	1.136	21.06	0.536	0.600	0.395	0.741
	13	40	5.92	1.5	1.060	19.65	0.536	0.524	0.395	0.665
	13	50	6.77	1.6	1.058	20.68	0.553	0.504	0.425	0.632
14	14	0	5.77	1.6	1.045	19.09	0.553	0.492	0.425	0.620
	14	10	6.47	1.4	1.020	20.90	0.517	0.503	0.365	0.655
	14	20	6.89	1.4	1.113	21.57	0.517	0.596	0.365	0.749
	14	30	5.83	1.4	1.060	19.84	0.517	0.543	0.365	0.695
	14	40	7.50	1.4	1.111	22.50	0.517	0.593	0.365	0.746
	14	50	5.89	1.5	1.116	19.60	0.536	0.580	0.395	0.721
	15	0	6.01	1.4	0.992	20.14	0.517	0.474	0.365	0.627
	15	10	5.95	1.4	0.997	20.04	0.517	0.479	0.365	0.632
	15	20	7.10	1.3	1.088	22.30	0.499	0.589	0.335	0.753
	15	30	4.65	1.3	0.979	18.05	0.499	0.481	0.335	0.644
	15	40	4.44	1.3	0.758	17.64	0.499	0.259	0.335	0.423
16	15	50	6.08	1.4	0.877	20.26	0.517	0.359	0.365	0.512
	16	0	5.95	1.3	1.003	20.42	0.499	0.504	0.335	0.668
	16	10	5.26	1.4	0.934	18.85	0.517	0.417	0.365	0.570
	16	20	6.41	1.2	0.973	21.62	0.479	0.493	0.305	0.667
	16	30	6.11	1.2	1.043	21.11	0.479	0.564	0.305	0.738
	16	40	5.95	1.3	1.005	20.42	0.499	0.506	0.335	0.670
	16	50	5.50	1.4	0.954	19.27	0.517	0.437	0.365	0.590
	17	0	7.01	1.3	1.043	22.16	0.499	0.544	0.335	0.708
	17	10	7.50	1.3	1.209	22.92	0.499	0.711	0.335	0.874
	17	20	7.04	1.3	1.212	22.21	0.499	0.713	0.335	0.877
	17	30	6.17	1.3	1.101	20.79	0.499	0.602	0.335	0.766
	17	40	7.59	1.3	1.147	23.06	0.499	0.648	0.335	0.812
	17	50	6.68	1.2	1.189	22.07	0.479	0.710	0.305	0.884
18	18	0	7.38	1.2	1.172	23.20	0.479	0.693	0.305	0.866
	18	10	5.98	1.2	1.113	20.88	0.479	0.634	0.305	0.808
	18	20	6.65	1.0	1.053	23.05	0.437	0.615	0.248	0.805
	18	30	7.01	0.8	1.138	25.02	0.391	0.747	0.192	0.947
	18	40	6.98	1.1	1.166	23.06	0.459	0.707	0.276	0.890
	18	50	7.32	1.3	1.192	22.65	0.499	0.693	0.335	0.857
	19	0	8.62	1.3	1.328	24.58	0.499	0.830	0.335	0.994
	19	10	6.50	1.4	1.260	20.95	0.517	0.743	0.365	0.895
	19	20	6.98	1.3	1.123	22.11	0.499	0.625	0.335	0.789
	19	30	6.01	1.4	1.083	20.14	0.517	0.565	0.365	0.718

No. 004

Area : DIEGO MARTIN(PAREL PARK)

Date : Dec. 18-19. 1989

$$Qx = Qo \times (Hx/Ho)^n$$

--(n = 0.5)-- --(n = 1.15)--

--(orifice)-- --(crack)--

TIME	METERED		METERED	Qtotal	Leak hole	< TYPE - A >		< TYPE - B >		
	hour	min	Q			Leak	Demand	Leak	Demand	
			PRESSURE	m3	d(mm)	QA1(m3)	QA2(m3)	QB1(m3)	QB2(m3)	
			(kg/cm2)							
	19	40	7.10	1.4	1.093	21.89	0.517	0.575	0.365	0.728
	19	50	7.13	1.4	1.186	21.94	0.517	0.668	0.365	0.821
20	20	0	6.38	1.4	1.126	20.75	0.517	0.608	0.365	0.761
	20	10	6.83	1.5	1.101	21.11	0.536	0.565	0.395	0.706
	20	20	6.77	1.5	1.133	21.01	0.536	0.598	0.395	0.739
	20	30	8.74	1.6	1.293	23.49	0.553	0.739	0.425	0.867
	20	40	6.62	1.7	1.280	20.14	0.570	0.710	0.456	0.824
	20	50	8.19	1.7	1.234	22.40	0.570	0.664	0.456	0.778
	21	0	7.13	1.6	1.277	21.22	0.553	0.723	0.425	0.852
	21	10	6.86	1.6	1.166	20.81	0.553	0.613	0.425	0.741
	21	20	7.19	1.8	1.171	20.69	0.587	0.584	0.487	0.684
	21	30	6.38	1.8	1.131	19.49	0.587	0.544	0.487	0.644
	21	40	7.80	1.8	1.182	21.55	0.587	0.595	0.487	0.695
	21	50	7.04	2.0	1.237	19.94	0.618	0.618	0.549	0.687
22	22	0	8.07	1.9	1.259	21.63	0.603	0.656	0.518	0.741
	22	10	7.74	1.9	1.318	21.18	0.603	0.715	0.518	0.800
	22	20	7.13	1.9	1.239	20.33	0.603	0.636	0.518	0.721
	22	30	6.59	1.9	1.143	19.54	0.603	0.541	0.518	0.625
	22	40	5.11	1.9	0.975	17.21	0.603	0.372	0.518	0.457
	22	50	6.44	2.0	0.963	19.07	0.618	0.344	0.549	0.413
	23	0	6.41	2.0	1.071	19.03	0.618	0.452	0.549	0.521
	23	10	5.14	2.1	0.963	16.83	0.634	0.329	0.581	0.381
	23	20	4.96	2.0	0.842	16.74	0.618	0.223	0.549	0.292
	23	30	5.11	2.0	0.839	16.99	0.618	0.221	0.549	0.290
	23	40	4.68	2.2	0.816	15.88	0.649	0.167	0.613	0.203
	23	50	5.50	2.1	0.848	17.41	0.634	0.215	0.581	0.267
0	0	0	6.11	2.2	0.968	18.14	0.649	0.319	0.613	0.355
	0	10	5.83	2.2	0.995	17.72	0.649	0.346	0.613	0.382
	0	20	5.35	2.2	0.932	16.98	0.649	0.283	0.613	0.319
	0	30	4.93	2.2	0.857	16.30	0.649	0.208	0.613	0.244
	0	40	5.11	2.2	0.837	16.59	0.649	0.188	0.613	0.224
	0	50	4.26	2.2	0.781	15.15	0.649	0.132	0.613	0.168
	1	0	4.77	2.2	0.753	16.03	0.649	0.104	0.613	0.140
	1	10	5.62	2.2	0.866	17.40	0.649	0.217	0.613	0.253
	1	20	4.20	2.3	0.818	14.87	0.663	0.155	0.645	0.173
	1	30	4.68	2.3	0.740	15.70	0.663	0.077	0.645	0.095
	1	40	4.05	2.4	0.728	14.45	0.678	0.050	0.678	0.050
	1	50	4.26	2.4	0.693	14.82	0.678	0.015	0.678	0.015
2	2	0	4.41	2.4	0.723	15.08	0.678	0.045	0.678	0.045
	2	10	4.99	2.4	0.783	16.04	0.678	0.106	0.678	0.106
	2	20	3.81	2.4	0.733	14.02	0.678	0.056	0.678	0.056
	2	30	3.99	2.4	0.650	14.34	0.678	0.027	0.678	0.027
	2	40	4.17	2.4	0.680	14.66	0.678	0.003	0.678	0.003
	2	50	3.96	2.4	0.678	14.29	0.678	0.000	0.678	0.000
	3	0	4.32	2.4	0.690	14.93	0.678	0.013	0.678	0.013
	3	10	4.44	2.4	0.730	15.13	0.678	0.053	0.678	0.053
	3	20	4.77	2.4	0.768	15.68	0.678	0.090	0.678	0.090
	3	30	4.50	2.4	0.773	15.23	0.678	0.095	0.678	0.095
	3	40	4.44	2.4	0.745	15.13	0.678	0.068	0.678	0.068
	3	50	3.96	2.4	0.700	14.29	0.678	0.023	0.678	0.023
4	4	0	4.84	2.4	0.733	15.80	0.678	0.056	0.678	0.056
	4	10	3.93	2.4	0.731	14.24	0.678	0.053	0.678	0.053
	4	20	4.47	2.3	0.700	15.34	0.663	0.037	0.645	0.055
	4	30	5.53	2.3	0.833	17.07	0.663	0.170	0.645	0.188
	4	40	4.41	2.3	0.828	15.24	0.663	0.165	0.645	0.183
	4	50	4.32	2.2	0.728	15.25	0.649	0.079	0.613	0.115

No. 004
 Area : DIEGO MARTIN(PAREL PARK)
 Date : Dec. 18-19. 1989

$$Q_x = Q_o \times (H_x/H_o)^n$$

--(n = 0.5)-- --(n = 1.15)--
 --(orifice)-- --(crack)--

TIME hour min	METERED	METERED	Qtotal m3	Leak hole d(mm)	< TYPE - A >		< TYPE - B >	
	Q (m3/h)	PRESSURE (kg/cm2)			Leak QA1(m3)	Demand QA2(m3)	Leak QB1(m3)	Demand QB2(m3)
5 0	4.47	2.2	0.733	15.52	0.649	0.084	0.613	0.120
5 10	5.14	2.1	0.801	16.83	0.634	0.167	0.581	0.220
5 20	4.53	2.1	0.806	15.80	0.634	0.172	0.581	0.225
5 30	5.38	2.0	0.826	17.43	0.618	0.207	0.549	0.276
5 40	4.59	1.9	0.831	16.31	0.603	0.228	0.518	0.313
5 50	4.62	1.8	0.768	16.59	0.587	0.181	0.487	0.281
6 0	6.44	1.7	0.922	19.86	0.570	0.351	0.456	0.466
6 10	6.62	1.6	1.088	20.45	0.553	0.535	0.425	0.663
6 20	6.77	1.3	1.116	21.78	0.499	0.617	0.335	0.781
6 30	6.68	1.2	1.121	22.07	0.479	0.642	0.305	0.816
6 40	6.95	1.2	1.136	22.51	0.479	0.657	0.305	0.831
6 50	5.26	1.2	1.018	19.59	0.479	0.538	0.305	0.712
7 0	4.71	1.2	0.831	18.53	0.479	0.352	0.305	0.526
7 10	6.44	1.2	0.929	21.67	0.479	0.450	0.305	0.624
7 20	7.68	1.0	1.177	24.77	0.437	0.739	0.248	0.929
7 30	7.22	1.1	1.242	23.45	0.459	0.783	0.276	0.965
7 40	7.16	1.1	1.198	23.35	0.459	0.740	0.276	0.922
7 50	6.98	1.1	1.178	23.06	0.459	0.720	0.276	0.902
8 0	6.71	1.1	1.141	22.61	0.459	0.682	0.276	0.865
8 10	6.08	1.2	1.066	21.06	0.479	0.587	0.305	0.761
8 20	5.77	1.2	0.988	20.51	0.479	0.508	0.305	0.682
8 30	6.98	1.1	1.063	23.06	0.459	0.604	0.276	0.786
8 40	5.44	1.0	1.035	20.85	0.437	0.598	0.248	0.787
8 50	4.99	1.2	0.869	19.08	0.479	0.390	0.305	0.564
9 0	6.26	1.2	0.938	21.37	0.479	0.458	0.305	0.632
9 10	6.14	1.1	1.033	21.63	0.459	0.575	0.276	0.757
9 20	6.14	1.1	1.023	21.63	0.459	0.565	0.276	0.747
9 30	5.62	1.1	0.980	20.69	0.459	0.521	0.276	0.704
9 40	4.62	1.1	0.853	18.76	0.459	0.395	0.276	0.577
9 50	6.53	1.2	0.929	21.82	0.479	0.450	0.305	0.624
10 0	6.35	1.0	1.073	22.52	0.437	0.636	0.248	0.826
10 10	5.65	1.0	1.000	21.25	0.437	0.563	0.248	0.752
10 20	7.47	1.1	1.093	23.85	0.459	0.635	0.276	0.817
TOTAL	---	---	144.450	---	79.438	65.067	62.595	81.855
Average	6.02	1.62	1.003	19.662	54.99%	45.04%	43.33%	56.67%
MAX	8.74	2.40	1.328	25.022	0.678	0.830	0.678	0.994
MIN	3.81	0.80	0.650	14.017	0.391	0.000	0.192	-0.027

kg/cm2. m3/10 min
 Leakage at Night: 2.40 0.678 14.290 : 2:50 a.m.
 Estimated night demand : 0.000

Nos. of house [A] 58 houses
 persons/house [B] 4.4 pesons/house
 A * B [C] 255.2 persons

< TYPE - A > < TYPE - B >
 Water Demand [D] 65.07 M3 81.85 M3
 l/day/capita D/C 254.96 l/d/c 320.75 l/d/c

No. 005

Area : TRAIN CITY(9th WEST Ave)

Date : Dec. 18-19, 1989

$$Q_x = Q_o \times (H_x/H_o)^n$$

---(n = 0.5)--- ---(n = 1.15)---

---(orifice)--- ---(crack)---

	TIME hour min	METERED	METERED	Qtotal m3	Leak hole d(mm)	< TYPE - A >		< TYPE - B >	
		Q (m3/h)	PRESSURE (kg/cm2)			Leak QA1(m3)	Demand QA2(m3)	Leak QB1(m3)	Demand QB2(m3)
	15 0	6.80	1.4	---	21.43	---	---	---	---
	15 10	4.28	1.3	0.923	17.32	0.149	0.774	0.095	0.828
	15 20	4.28	1.3	0.713	17.32	0.149	0.564	0.095	0.618
	15 30	5.09	1.3	0.781	18.88	0.149	0.632	0.095	0.686
	15 40	4.91	1.3	0.833	18.55	0.149	0.684	0.095	0.738
	15 50	3.63	1.2	0.712	16.27	0.143	0.568	0.087	0.625
16	16 0	3.84	1.1	0.623	17.10	0.137	0.485	0.078	0.544
	16 10	4.20	1.1	0.670	17.89	0.137	0.533	0.078	0.592
	16 20	4.78	1.1	0.748	19.08	0.137	0.611	0.078	0.670
	16 30	3.90	1.1	0.723	17.24	0.137	0.586	0.078	0.645
	16 40	3.39	1.1	0.608	16.07	0.137	0.470	0.078	0.529
	16 50	3.16	1.1	0.546	15.51	0.137	0.409	0.078	0.467
	17 0	3.23	1.1	0.533	15.69	0.137	0.395	0.078	0.454
	17 10	3.88	1.1	0.593	17.19	0.137	0.455	0.078	0.514
	17 20	4.06	1.2	0.662	17.21	0.143	0.518	0.087	0.575
	17 30	3.77	1.2	0.653	16.58	0.143	0.509	0.087	0.566
	17 40	3.27	1.2	0.587	15.44	0.143	0.443	0.087	0.500
	17 50	4.31	1.2	0.632	17.73	0.143	0.488	0.087	0.545
18	18 0	3.61	1.2	0.660	16.23	0.143	0.517	0.087	0.573
	18 10	4.71	1.2	0.693	18.53	0.143	0.550	0.087	0.607
	18 20	3.59	1.2	0.692	16.18	0.143	0.548	0.087	0.605
	18 30	3.43	1.1	0.585	16.16	0.137	0.448	0.078	0.507
	18 40	4.82	1.1	0.688	19.16	0.137	0.550	0.078	0.609
	18 50	3.97	1.3	0.733	16.68	0.149	0.583	0.095	0.637
	19 0	5.34	1.4	0.776	18.99	0.155	0.621	0.103	0.672
	19 10	4.28	1.4	0.802	17.00	0.155	0.647	0.103	0.698
	19 20	3.48	1.6	0.647	14.83	0.165	0.481	0.121	0.526
	19 30	5.36	1.7	0.737	18.12	0.170	0.566	0.129	0.607
	19 40	4.44	1.7	0.817	16.49	0.170	0.646	0.129	0.687
	19 50	4.80	1.7	0.770	17.15	0.170	0.600	0.129	0.641
20	20 0	3.41	1.7	0.684	14.45	0.170	0.514	0.129	0.555
	20 10	2.74	1.8	0.513	12.77	0.175	0.337	0.138	0.374
	20 20	2.76	2.0	0.458	12.49	0.185	0.273	0.156	0.302
	20 30	2.60	2.0	0.447	12.12	0.185	0.262	0.156	0.291
	20 40	1.86	2.0	0.372	10.25	0.185	0.187	0.156	0.216
	20 50	2.58	2.0	0.370	12.07	0.185	0.185	0.156	0.214
	21 0	2.80	2.0	0.448	12.58	0.185	0.263	0.156	0.292
	21 10	1.21	1.9	0.334	8.37	0.180	0.154	0.147	0.187
	21 20	2.42	2.0	0.303	11.69	0.185	0.118	0.156	0.147
	21 30	2.26	2.2	0.390	11.03	0.194	0.196	0.174	0.216
	21 40	3.39	2.2	0.471	13.51	0.194	0.277	0.174	0.297
	21 50	2.60	2.1	0.499	11.97	0.189	0.310	0.165	0.334
22	22 0	2.11	2.0	0.393	10.92	0.185	0.208	0.156	0.237
	22 10	2.67	2.0	0.398	12.28	0.185	0.213	0.156	0.242
	22 20	3.32	1.9	0.499	13.87	0.180	0.319	0.147	0.352
	22 30	3.57	1.9	0.574	14.38	0.180	0.394	0.147	0.427
	22 40	2.20	1.8	0.481	11.45	0.175	0.305	0.138	0.343
	22 50	2.69	2.3	0.408	11.90	0.198	0.209	0.183	0.224
	23 0	3.72	2.4	0.534	13.85	0.203	0.332	0.192	0.342
	23 10	2.08	2.8	0.483	9.97	0.219	0.265	0.230	0.254
	23 20	1.25	1.8	0.278	8.63	0.175	0.102	0.138	0.139
	23 30	2.26	1.8	0.293	11.60	0.175	0.117	0.138	0.154
	23 40	1.52	1.8	0.315	9.51	0.175	0.140	0.138	0.177
	23 50	1.81	2.1	0.278	9.99	0.189	0.088	0.165	0.113
0	0 0	1.75	2.2	0.297	9.71	0.194	0.103	0.174	0.123
	0 10	1.63	2.2	0.282	9.37	0.194	0.088	0.174	0.108

No. 005

Area : TRAIN CITY(9th WEST Ave)

Date : Dec. 18-19, 1989

$$Q_x = Q_o \times (H_x/H_o)^n$$

--(n = 0.5)-- --(n = 1.15)--

--(orifice)-- --(crack)--

TIME hour min	METERED Q (m3/h)	METERED PRESSURE (kg/cm2)	Qtotal m3	Leak hole d(mm)	< TYPE - A >		< TYPE - B >	
					Leak QA1(m3)	Demand QA2(m3)	Leak QB1(m3)	Demand QB2(m3)
0 20	1.66	2.7	0.274	8.98	0.215	0.059	0.220	0.054
0 30	1.61	2.2	0.273	9.31	0.194	0.079	0.174	0.099
0 40	1.34	2.3	0.246	8.40	0.198	0.048	0.183	0.063
0 50	1.37	2.3	0.226	8.50	0.198	0.028	0.183	0.043
1 0	1.21	2.3	0.215	7.98	0.198	0.017	0.183	0.032
1 10	1.75	2.3	0.247	9.60	0.198	0.048	0.183	0.064
1 20	1.32	2.4	0.256	8.25	0.203	0.053	0.192	0.064
1 30	1.28	2.6	0.217	7.96	0.211	0.006	0.211	0.006
1 40	1.50	2.6	0.232	8.62	0.211	0.021	0.211	0.021
1 50	2.08	2.6	0.298	10.15	0.211	0.088	0.211	0.088
2 2 0	1.32	2.5	0.283	8.17	0.207	0.077	0.202	0.082
2 2 10	2.06	2.6	0.282	10.10	0.211	0.071	0.211	0.071
2 2 20	1.25	2.6	0.276	7.87	0.211	0.065	0.211	0.065
2 2 30	1.28	2.6	0.211	7.96	0.211	0.000	0.211	0.000
2 2 40	1.25	2.6	0.211	7.87	0.211	0.000	0.211	0.000
2 2 50	1.30	2.6	0.213	8.03	0.211	0.002	0.211	0.002
3 3 0	1.34	2.8	0.220	8.00	0.219	0.001	0.230	-0.010
3 3 10	1.34	2.6	0.223	8.15	0.211	0.013	0.211	0.013
3 3 20	1.32	2.6	0.222	8.09	0.211	0.011	0.211	0.011
3 3 30	1.34	2.6	0.222	8.15	0.211	0.011	0.211	0.011
3 3 40	1.39	2.6	0.228	8.30	0.211	0.017	0.211	0.017
3 3 50	1.34	2.5	0.228	8.23	0.207	0.021	0.202	0.026
4 4 0	1.34	2.6	0.223	8.15	0.211	0.013	0.211	0.013
4 4 10	1.34	2.5	0.223	8.23	0.207	0.017	0.202	0.022
4 4 20	1.32	2.4	0.222	8.25	0.203	0.019	0.192	0.029
4 4 30	1.75	2.3	0.256	9.60	0.198	0.058	0.183	0.073
4 4 40	1.72	2.2	0.289	9.62	0.194	0.095	0.174	0.115
4 4 50	1.99	2.1	0.309	10.47	0.189	0.120	0.165	0.144
5 5 0	1.61	1.8	0.300	9.79	0.175	0.125	0.138	0.162
5 5 10	1.41	2.2	0.252	8.71	0.194	0.058	0.174	0.078
5 5 20	3.00	1.6	0.368	13.76	0.165	0.202	0.121	0.247
5 5 30	2.24	1.5	0.437	12.09	0.160	0.277	0.112	0.325
5 5 40	2.15	1.2	0.366	12.52	0.143	0.223	0.087	0.279
5 5 50	1.63	1.7	0.315	9.99	0.170	0.145	0.129	0.186
6 6 0	1.75	1.4	0.282	10.87	0.155	0.127	0.103	0.178
6 6 10	1.86	1.3	0.301	11.42	0.149	0.152	0.095	0.206
6 6 20	2.49	1.4	0.363	12.97	0.155	0.208	0.103	0.259
6 6 30	5.72	1.0	0.684	21.38	0.131	0.553	0.070	0.614
6 6 40	3.36	1.5	0.757	14.80	0.160	0.597	0.112	0.645
6 6 50	4.13	1.3	0.624	17.01	0.149	0.475	0.095	0.529
7 7 0	3.21	1.2	0.612	15.30	0.143	0.468	0.087	0.525
7 7 10	3.95	1.2	0.597	16.97	0.143	0.453	0.087	0.510
7 7 20	4.60	1.0	0.713	19.17	0.131	0.582	0.070	0.642
7 7 30	3.95	0.8	0.713	18.78	0.117	0.596	0.054	0.658
7 7 40	3.99	1.0	0.662	17.85	0.131	0.531	0.070	0.591
7 7 50	3.52	0.9	0.626	17.22	0.124	0.502	0.062	0.564
8 8 0	4.40	0.8	0.660	19.82	0.117	0.543	0.054	0.606
8 8 10	4.46	0.7	0.738	20.64	0.109	0.629	0.047	0.692
8 8 20	4.55	0.7	0.751	20.84	0.109	0.641	0.047	0.704
8 8 30	5.00	0.7	0.796	21.85	0.109	0.686	0.047	0.749
8 8 40	4.85	0.7	0.821	21.52	0.109	0.711	0.047	0.774
8 8 50	3.45	0.6	0.692	18.86	0.101	0.590	0.039	0.653
9 9 0	3.81	1.0	0.605	17.45	0.131	0.474	0.070	0.535
9 9 10	3.70	0.9	0.626	17.65	0.124	0.502	0.062	0.564
9 9 20	4.02	1.1	0.643	17.50	0.137	0.506	0.078	0.565
9 9 30	3.34	0.9	0.613	16.77	0.124	0.489	0.062	0.551

No. 005

Area : TRAIN CITY(9th WEST Ave)

Date : Dec. 18-19. 1989

$$Q_x = Q_o \times (H_x/H_o)^n$$

---(n = 0.5)--- ---(n = 1.15)---
 ---(orifice)--- ---(crack)---

TIME	METERED		Qtotal	Leak	< TYPE - A >		< TYPE - B >			
	hour	min			Q (m3/h)	PRESSURE (kg/cm2)	Leak	Demand	Leak	Demand
			m3	d(mm)	QA1(m3)	QA2(m3)	QB1(m3)	QB2(m3)		
10	9	40	3.39	0.9	0.561	16.90	0.124	0.437	0.062	0.499
	9	50	4.22	0.8	0.634	19.41	0.117	0.517	0.054	0.580
	10	0	3.81	0.8	0.669	18.45	0.117	0.552	0.054	0.615
	10	10	4.15	0.7	0.663	19.91	0.109	0.554	0.047	0.617
	10	20	2.98	0.7	0.594	16.87	0.109	0.485	0.047	0.548
	10	30	4.44	1.0	0.618	18.83	0.131	0.488	0.070	0.548
	10	40	5.14	1.5	0.798	18.31	0.160	0.638	0.112	0.686
	10	50	4.33	1.2	0.789	17.77	0.143	0.646	0.087	0.703
	11	0	3.93	1.0	0.688	17.72	0.131	0.558	0.070	0.618
	11	10	4.94	0.9	0.739	20.40	0.124	0.615	0.062	0.677
	11	20	6.78	0.8	0.977	24.61	0.117	0.860	0.054	0.922
	11	30	4.67	1.2	0.954	18.45	0.143	0.811	0.087	0.868
	11	40	4.91	1.0	0.798	19.81	0.131	0.668	0.070	0.728
	11	50	3.81	0.8	0.727	18.45	0.117	0.610	0.054	0.672
12	12	0	4.15	1.2	0.663	17.40	0.143	0.520	0.087	0.577
	12	10	2.02	1.3	0.514	11.90	0.149	0.365	0.095	0.419
	12	20	4.49	1.2	0.543	18.10	0.143	0.399	0.087	0.456
	12	30	3.27	1.3	0.647	15.14	0.149	0.498	0.095	0.552
	12	40	3.75	1.4	0.585	15.91	0.155	0.430	0.103	0.482
	12	50	1.43	1.4	0.432	9.83	0.155	0.277	0.103	0.328
	13	0	2.62	1.6	0.338	12.86	0.165	0.172	0.121	0.217
	13	10	1.72	1.4	0.362	10.78	0.155	0.207	0.103	0.258
	13	20	3.52	1.3	0.437	15.70	0.149	0.288	0.095	0.342
	13	30	4.11	1.8	0.636	15.64	0.175	0.460	0.138	0.498
	13	40	3.57	1.6	0.640	15.02	0.165	0.475	0.121	0.519
	13	50	2.74	1.8	0.526	12.77	0.175	0.350	0.138	0.388
14	14	0	3.88	1.2	0.552	16.82	0.143	0.408	0.087	0.465
	14	10	2.35	1.4	0.519	12.60	0.155	0.364	0.103	0.416
	14	20	4.06	1.1	0.534	17.59	0.137	0.397	0.078	0.456
	14	30	3.79	1.3	0.654	16.30	0.149	0.505	0.095	0.559
	14	40	3.99	1.0	0.648	17.85	0.131	0.518	0.070	0.578
	14	50	1.43	1.4	0.452	9.83	0.155	0.297	0.103	0.348
	15	0	2.76	1.6	0.349	13.20	0.165	0.184	0.121	0.229
TOTAL			---	---	73.908	---	23.415	50.493	17.614	56.294
Average			3.09	1.60	0.513	14.118	31.68%	68.32%	23.83%	76.17%
MAX			6.80	2.80	0.977	24.608	0.219	0.860	0.230	0.922
MIN			1.21	0.60	0.211	7.870	0.101	0.000	0.039	-0.010

kg/cm2 m3/10 min
 Leakage at Night: 2.60 0.211 7.870 : 2:40 a.m.
 Estimated night demand : 0.000

Nos. of house [A] 43 houses
 persons/house [B] 4.3 pesons/house
 A * B [C] 184.9 persons

< TYPE - A > < TYPE - B >
 Water Demand [D] 50.49 M3 56.29 M3
 l/day/capita D/C 273.08 l/d/c 304.46 l/d/c

No. 006
 Area : VALSAYEN
 Date : Dec. 28-29. 1989

$$Q_x = Q_o \times (H_x/H_o)^n$$

--(n = 0.5)-- --(n = 1.15)--
 --(orifice)-- --(crack)--

TIME	METERED		METERED	Qtotal	Leak hole d(mm)	< TYPE - A >		< TYPE - B >		
	hour	min	Q (m3/h)			PRESSURE (kg/cm2)	Leak	Demand	Leak	Demand
				m3		QA1(m3)	QA2(m3)	QB1(m3)	QB2(m3)	
	14	40	13.80	0.6	---	---	---	---	---	
	14	50	13.20	0.6	2.250	36.90	2.440	-0.190	3.175	-0.925
	15	0	14.70	0.6	2.325	38.94	2.440	-0.115	3.175	-0.850
	15	10	14.40	0.6	2.425	38.54	2.440	-0.015	3.175	-0.750
	15	20	14.10	0.6	2.375	38.13	2.440	-0.065	3.175	-0.800
	15	30	14.90	0.3	2.417	46.62	1.725	0.692	1.431	0.986
	15	40	14.00	0.3	2.408	45.19	1.725	0.683	1.431	0.977
16	15	50	14.10	0.3	2.342	45.35	1.725	0.617	1.431	0.911
	16	0	14.40	0.3	2.375	45.83	1.725	0.650	1.431	0.944
	16	10	14.00	0.3	2.367	45.19	1.725	0.642	1.431	0.936
	16	20	14.90	0.3	2.408	46.62	1.725	0.683	1.431	0.977
	16	30	14.90	0.3	2.483	46.62	1.725	0.758	1.431	1.052
	16	40	14.70	0.3	2.467	46.30	1.725	0.742	1.431	1.036
	16	50	14.20	0.3	2.408	45.51	1.725	0.683	1.431	0.977
	17	0	14.20	0.3	2.367	45.51	1.725	0.642	1.431	0.936
	17	10	15.10	0.3	2.442	46.93	1.725	0.717	1.431	1.011
	17	20	14.20	0.3	2.442	45.51	1.725	0.717	1.431	1.011
	17	30	14.00	0.3	2.350	45.19	1.725	0.625	1.431	0.919
	17	40	13.60	0.3	2.300	44.54	1.725	0.575	1.431	0.869
18	17	50	13.70	0.3	2.275	44.70	1.725	0.550	1.431	0.844
	18	0	13.00	0.3	2.225	43.54	1.725	0.500	1.431	0.794
	18	10	13.40	0.3	2.200	44.21	1.725	0.475	1.431	0.769
	18	20	13.00	0.3	2.200	43.54	1.725	0.475	1.431	0.769
	18	30	12.80	0.3	2.150	43.21	1.725	0.425	1.431	0.719
	18	40	12.60	0.3	2.117	42.87	1.725	0.392	1.431	0.686
	18	50	13.70	0.3	2.192	44.70	1.725	0.467	1.431	0.761
	19	0	13.50	0.3	2.267	44.37	1.725	0.542	1.431	0.836
	19	10	13.80	0.3	2.275	44.86	1.725	0.550	1.431	0.844
	19	20	14.70	0.3	2.375	46.30	1.725	0.650	1.431	0.944
	19	30	15.30	0.3	2.500	47.24	1.725	0.775	1.431	1.069
	19	40	15.40	0.3	2.558	47.39	1.725	0.833	1.431	1.127
20	19	50	14.20	0.3	2.467	45.51	1.725	0.742	1.431	1.036
	20	0	15.00	0.3	2.433	46.77	1.725	0.708	1.431	1.002
	20	10	14.50	0.4	2.458	42.80	1.992	0.466	1.992	0.466
	20	20	14.70	0.4	2.433	43.09	1.992	0.441	1.992	0.441
	20	30	14.90	0.4	2.467	43.38	1.992	0.475	1.992	0.475
	20	40	15.20	0.4	2.508	43.82	1.992	0.516	1.992	0.516
	20	50	15.30	0.4	2.542	43.96	1.992	0.550	1.992	0.550
	21	0	15.00	0.4	2.525	43.53	1.992	0.533	1.992	0.533
	21	10	12.20	0.4	2.267	39.26	1.992	0.275	1.992	0.275
	21	20	11.30	0.4	1.958	37.78	1.992	-0.034	1.992	-0.034
	21	30	11.70	0.4	1.917	38.44	1.992	-0.075	1.992	-0.075
	21	40	11.60	0.4	1.942	38.28	1.992	-0.050	1.992	-0.050
	21	50	12.40	0.4	2.000	39.58	1.992	0.008	1.992	0.008
22	22	0	12.50	0.4	2.075	39.74	1.992	0.083	1.992	0.083
	22	10	12.20	0.4	2.058	39.26	1.992	0.066	1.992	0.066
	22	20	13.10	0.3	2.108	43.71	1.725	0.383	1.431	0.677
	22	30	12.60	0.3	2.142	42.87	1.725	0.417	1.431	0.711
	22	40	12.10	0.3	2.058	42.01	1.725	0.333	1.431	0.627
	22	50	12.70	0.3	2.067	43.04	1.725	0.342	1.431	0.636
	23	0	12.40	0.3	2.092	42.53	1.725	0.367	1.431	0.661
	23	10	13.10	0.3	2.125	43.71	1.725	0.400	1.431	0.694
	23	20	13.50	0.3	2.217	44.37	1.725	0.492	1.431	0.786
	23	30	12.50	0.3	2.167	42.70	1.725	0.442	1.431	0.736
	23	40	12.20	0.3	2.058	42.18	1.725	0.333	1.431	0.627
	23	50	12.20	0.3	2.033	42.18	1.725	0.308	1.431	0.602

No. 006
 Area : VALSAYEN
 Date : Dec. 28-29. 1989

$$Qx = Qo \times (Hx/Ho)^n$$

---(n = 0.5)--- ---(n = 1.15)---
 ---(orifice)--- ---(crack)---

TIME	METERED		Qtotal	Leak	< TYPE - A >		< TYPE - B >			
	hour	min			Q (m3/h)	PRESSURE (kg/cm2)	Leak	Demand	Leak	Demand
			m3	d(mm)	QA1(m3)	QA2(m3)	QB1(m3)	QB2(m3)		
0	0	0	12.10	0.3	2.025	42.01	1.725	0.300	1.431	0.594
	0	10	12.00	0.3	2.008	41.84	1.725	0.283	1.431	0.577
	0	20	12.60	0.3	2.050	42.87	1.725	0.325	1.431	0.619
	0	30	13.00	0.3	2.133	43.54	1.725	0.408	1.431	0.702
	0	40	14.00	0.3	2.250	45.19	1.725	0.525	1.431	0.819
	0	50	14.00	0.3	2.333	45.19	1.725	0.608	1.431	0.902
	1	0	13.80	0.3	2.317	44.86	1.725	0.592	1.431	0.886
	1	10	13.30	0.3	2.258	44.04	1.725	0.533	1.431	0.827
	1	20	14.20	0.3	2.292	45.51	1.725	0.567	1.431	0.861
	1	30	13.50	0.3	2.308	44.37	1.725	0.583	1.431	0.877
	1	40	13.60	0.4	2.258	41.45	1.992	0.266	1.992	0.266
	1	50	13.10	0.4	2.225	40.68	1.992	0.233	1.992	0.233
2	2	0	13.30	0.4	2.200	40.99	1.992	0.208	1.992	0.208
	2	10	12.70	0.4	2.167	40.05	1.992	0.175	1.992	0.175
	2	20	13.10	0.4	2.150	40.68	1.992	0.158	1.992	0.158
	2	30	12.50	0.4	2.133	39.74	1.992	0.141	1.992	0.141
	2	40	12.40	0.4	2.075	39.58	1.992	0.083	1.992	0.083
	2	50	12.30	0.4	2.058	39.42	1.992	0.066	1.992	0.066
	3	0	12.40	0.4	2.058	39.58	1.992	0.066	1.992	0.066
	3	10	12.20	0.4	2.050	39.26	1.992	0.058	1.992	0.058
	3	20	12.20	0.4	2.033	39.26	1.992	0.041	1.992	0.041
	3	30	12.30	0.4	2.042	39.42	1.992	0.050	1.992	0.050
	3	40	12.20	0.4	2.042	39.26	1.992	0.050	1.992	0.050
	3	50	12.60	0.4	2.067	39.89	1.992	0.075	1.992	0.075
4	4	0	12.00	0.4	2.050	38.93	1.992	0.058	1.992	0.058
	4	10	11.80	0.4	1.983	38.61	1.992	-0.009	1.992	-0.009
	4	20	12.20	0.4	2.000	39.26	1.992	0.008	1.992	0.008
	4	30	12.20	0.4	2.033	39.26	1.992	0.041	1.992	0.041
	4	40	11.70	0.4	1.992	38.44	1.992	-0.000	1.992	-0.000
	4	50	12.30	0.4	2.000	39.42	1.992	0.008	1.992	0.008
	5	0	16.50	0.4	2.400	45.65	1.992	0.408	1.992	0.408
	5	10	16.60	0.4	2.758	45.79	1.992	0.766	1.992	0.766
	5	20	16.90	0.4	2.792	46.20	1.992	0.800	1.992	0.800
	5	30	16.90	0.4	2.817	46.20	1.992	0.825	1.992	0.825
	5	40	17.60	0.4	2.875	47.15	1.992	0.883	1.992	0.883
	5	50	16.60	0.4	2.850	45.79	1.992	0.858	1.992	0.858
6	6	0	17.40	0.5	2.833	44.34	2.227	0.606	2.575	0.259
	6	10	15.90	0.5	2.775	42.38	2.227	0.548	2.575	0.200
	6	20	16.30	0.5	2.683	42.91	2.227	0.456	2.575	0.109
	6	30	14.90	0.5	2.600	41.03	2.227	0.373	2.575	0.025
	6	40	16.20	0.5	2.592	42.78	2.227	0.365	2.575	0.017
	6	50	15.10	0.5	2.608	41.30	2.227	0.381	2.575	0.034
	7	0	16.10	0.5	2.600	42.65	2.227	0.373	2.575	0.025
	7	10	16.30	0.5	2.700	42.91	2.227	0.473	2.575	0.125
	7	20	15.60	0.5	2.658	41.98	2.227	0.431	2.575	0.084
	7	30	14.70	0.5	2.525	40.75	2.227	0.298	2.575	-0.050
	7	40	14.50	0.5	2.433	40.47	2.227	0.206	2.575	-0.141
	7	50	14.30	0.4	2.400	42.50	1.992	0.408	1.992	0.408
8	8	0	14.00	0.4	2.358	42.05	1.992	0.366	1.992	0.366
	8	10	13.80	0.4	2.317	41.75	1.992	0.325	1.992	0.325
	8	20	14.80	0.4	2.383	43.24	1.992	0.391	1.992	0.391
	8	30	15.10	0.4	2.492	43.67	1.992	0.500	1.992	0.500
	8	40	13.80	0.4	2.408	41.75	1.992	0.416	1.992	0.416
	8	50	13.10	0.4	2.242	40.68	1.992	0.250	1.992	0.250
	9	0	14.20	0.4	2.275	42.35	1.992	0.283	1.992	0.283
	9	10	14.20	0.4	2.367	42.35	1.992	0.375	1.992	0.375

No. 006

Area : VALSAYEN

Date : Dec. 28-29, 1989

$$Q_x = Q_o \times (H_x/H_o)^n$$

--(n = 0.5)-- --(n = 1.15)--

--(orifice)-- --(crack)--

TIME hour min	METERED	METERED	Qtotal m3	Leak hole d(mm)	< TYPE - A >		< TYPE - B >	
	Q (m3/h)	PRESSURE (kg/cm2)			Leak QA1(m3)	Demand QA2(m3)	Leak QB1(m3)	Demand QB2(m3)
9 20	13.50	0.3	2.308	44.37	1.725	0.583	1.431	0.877
9 30	14.00	0.3	2.292	45.19	1.725	0.567	1.431	0.861
9 40	14.80	0.3	2.400	46.46	1.725	0.675	1.431	0.969
9 50	13.70	0.4	2.375	41.60	1.992	0.383	1.992	0.383
10 0	14.00	0.4	2.308	42.05	1.992	0.316	1.992	0.316
10 10	14.10	0.4	2.342	42.20	1.992	0.350	1.992	0.350
10 20	14.40	0.4	2.375	42.65	1.992	0.383	1.992	0.383
10 30	13.90	0.4	2.358	41.90	1.992	0.366	1.992	0.366
10 40	14.10	0.4	2.333	42.20	1.992	0.341	1.992	0.341
10 50	13.30	0.4	2.283	40.99	1.992	0.291	1.992	0.291
11 0	13.60	0.4	2.242	41.45	1.992	0.250	1.992	0.250
11 10	14.40	0.4	2.333	42.65	1.992	0.341	1.992	0.341
11 20	13.90	0.4	2.358	41.90	1.992	0.366	1.992	0.366
11 30	13.90	0.4	2.317	41.90	1.992	0.325	1.992	0.325
11 40	14.20	0.4	2.342	42.35	1.992	0.350	1.992	0.350
11 50	14.80	0.4	2.417	43.24	1.992	0.425	1.992	0.425
12 0	14.80	0.4	2.467	43.24	1.992	0.475	1.992	0.475
12 10	14.30	0.4	2.425	42.50	1.992	0.433	1.992	0.433
12 20	14.60	0.4	2.408	42.94	1.992	0.416	1.992	0.416
12 30	14.20	0.4	2.400	42.35	1.992	0.408	1.992	0.408
12 40	14.10	0.4	2.358	42.20	1.992	0.366	1.992	0.366
12 50	14.00	0.4	2.342	42.05	1.992	0.350	1.992	0.350
13 0	13.50	0.4	2.292	41.29	1.992	0.300	1.992	0.300
13 10	13.60	0.4	2.258	41.45	1.992	0.266	1.992	0.266
13 20	14.40	0.4	2.333	42.65	1.992	0.341	1.992	0.341
13 30	13.80	0.5	2.350	39.49	2.227	0.123	2.575	-0.225
14 0	13.10	0.5	2.242	38.47	2.227	0.015	2.575	-0.333
13 50	14.20	0.5	2.275	40.05	2.227	0.048	2.575	-0.300
14 0	14.10	0.5	2.358	39.91	2.227	0.131	2.575	-0.216
14 10	14.40	0.6	2.375	38.54	2.440	-0.065	3.175	-0.800
14 20	14.70	0.6	2.425	38.94	2.440	-0.015	3.175	-0.750
14 30	14.00	0.6	2.392	38.00	2.440	-0.048	3.175	-0.784
14 40	13.70	0.6	2.308	37.59	2.440	-0.131	3.175	-0.867
TOTAL	---	---	333.125	---	280.346	52.779	276.440	56.685
Average	13.88	0.39	2.313	42.450	84.16%	15.84%	82.98%	17.02%
MAX	17.60	0.60	2.875	47.394	2.440	0.883	3.175	1.127
MIN	11.30	0.30	1.917	36.897	1.725	-0.190	1.431	-0.925

Leakage at Night: 0.40 kg/cm2 1.992 m3/10 min 38.440 : 4:40 a.m.
 Estimated night demand : 0.000

Nos. of house [A] 80 houses
 persons/house [B] 4.3 persons/house
 A * B [C] 344 persons

Water Demand [D] 52.78 M3 56.68 M3
 l/day/capita D/C 153.43 l/d/c 164.78 l/d/c

No. 007

Area : Plymouth

Date : Jan. 3-4, 1990

$$Q_x = Q_o \times (H_x/H_o)^n$$

---(n = 0.5)--- ---(n = 1.15)---
 ---(orifice)--- ---(crack)---

TIME hour min	METERED	METERED	Qtotal m3	Leak hole d(mm)	< TYPE - A >		< TYPE - B >	
	Q (m3/h)	PRESSURE (kg/cm2)			Leak QA1(m3)	Demand QA2(m3)	Leak QB1(m3)	Demand QB2(m3)
15 :05	15.01	2.0	---	29.1	---	---	---	---
15 :15	15.97	2.0	2.582	30.0	1.069	1.513	0.622	1.960
15 :25	16.10	2.1	2.673	29.8	1.096	1.577	0.658	2.014
15 :35	15.81	1.8	2.659	30.7	1.014	1.645	0.551	2.108
15 :45	16.07	1.9	2.657	30.5	1.042	1.614	0.587	2.070
15 :55	16.60	1.8	2.723	31.4	1.014	1.708	0.551	2.171
16 :05	16.34	1.8	2.745	31.2	1.014	1.731	0.551	2.194
16 :15	17.00	1.6	2.778	32.8	0.956	1.822	0.481	2.297
16 :25	17.21	1.8	2.851	32.0	1.014	1.836	0.551	2.300
16 :35	18.08	1.9	2.941	32.4	1.042	1.899	0.587	2.354
16 :45	19.61	1.8	3.141	34.2	1.014	2.126	0.551	2.590
16 :55	17.71	1.7	3.110	32.9	0.986	2.124	0.516	2.594
17 :05	16.55	1.8	2.855	31.4	1.014	1.841	0.551	2.304
17 :15	17.84	2.1	2.866	31.4	1.096	1.770	0.658	2.208
17 :25	19.96	2.5	3.150	31.8	1.196	1.954	0.804	2.346
17 :35	21.41	2.6	3.448	32.6	1.219	2.228	0.841	2.606
17 :45	18.85	3.1	3.355	29.2	1.331	2.024	1.030	2.325
17 :55	19.32	2.8	3.181	30.4	1.265	1.916	0.916	2.265
18 :05	18.27	2.1	3.133	31.7	1.096	2.037	0.658	2.474
18 :15	17.21	2.0	2.957	31.2	1.069	1.887	0.622	2.334
18 :25	17.55	2.4	2.897	30.1	1.171	1.725	0.767	2.129
18 :35	20.38	2.4	3.161	32.4	1.171	1.989	0.767	2.393
18 :45	18.08	2.8	3.205	29.4	1.265	1.940	0.916	2.289
18 :55	18.80	3.2	3.073	29.0	1.353	1.721	1.068	2.005
19 :05	17.47	3.2	3.023	27.9	1.353	1.670	1.068	1.954
19 :15	17.37	3.0	2.903	28.3	1.310	1.594	0.992	1.911
19 :25	17.00	3.0	2.864	28.0	1.310	1.555	0.992	1.872
19 :35	16.15	3.4	2.763	26.5	1.394	1.368	1.145	1.617
19 :45	15.30	3.6	2.621	25.4	1.435	1.186	1.223	1.398
19 :55	15.17	3.9	2.539	24.8	1.493	1.046	1.341	1.198
20 :05	13.96	4.1	2.428	23.5	1.531	0.897	1.421	1.007
20 :15	14.04	3.7	2.333	24.1	1.454	0.879	1.262	1.071
20 :25	14.27	4.5	2.359	23.2	1.604	0.755	1.581	0.778
20 :35	13.24	4.5	2.293	22.3	1.604	0.689	1.581	0.711
20 :45	14.59	4.6	2.319	23.3	1.622	0.698	1.622	0.698
20 :55	14.25	4.5	2.403	23.2	1.604	0.799	1.581	0.822
21 :05	13.40	4.6	2.304	22.3	1.622	0.682	1.622	0.682
21 :15	13.27	4.7	2.223	22.1	1.639	0.583	1.662	0.560
21 :25	12.45	4.0	2.143	22.3	1.512	0.631	1.381	0.762
21 :35	13.80	3.4	2.188	24.5	1.394	0.793	1.145	1.042
21 :45	13.45	4.0	2.271	23.2	1.512	0.759	1.381	0.890
21 :55	13.80	4.2	2.271	23.2	1.550	0.721	1.461	0.810
22 :05	11.02	4.4	2.068	20.5	1.586	0.482	1.541	0.527
22 :15	12.21	4.5	1.936	21.4	1.604	0.332	1.581	0.355
22 :25	12.90	4.6	2.093	21.9	1.622	0.471	1.622	0.471
22 :35	11.55	4.7	2.038	20.6	1.639	0.398	1.662	0.375
22 :45	12.71	4.6	2.022	21.8	1.622	0.400	1.622	0.400
22 :55	11.50	4.7	2.018	20.6	1.639	0.378	1.662	0.355
23 :05	11.02	4.4	1.877	20.5	1.586	0.291	1.541	0.336
23 :15	10.65	4.5	1.806	20.0	1.604	0.202	1.581	0.225
23 :25	11.02	4.7	1.806	20.2	1.639	0.167	1.662	0.144
23 :35	11.18	4.7	1.850	20.3	1.639	0.211	1.662	0.188
23 :45	10.55	4.6	1.811	19.8	1.622	0.189	1.622	0.189
23 :55	10.81	4.6	1.780	20.1	1.622	0.158	1.622	0.158
0 :05	10.07	4.5	1.740	19.5	1.604	0.136	1.581	0.159
0 :15	10.18	4.6	1.688	19.5	1.622	0.066	1.622	0.066

No. 007

Area : Plymouth

Date : Jan. 3-4, 1990

$$Q_x = Q_o \times (H_x/H_o)^n$$

--(n = 0.5)-- --(n = 1.15)--

--(orifice)-- --(crack)--

TIME hour min	METERED	METERED	Qtotal m3	Leak hole d(mm)	< TYPE - A >		< TYPE - B >	
	Q (m3/h)	PRESSURE (kg/cm2)			Leak QA1(m3)	Demand QA2(m3)	Leak QB1(m3)	Demand QB2(m3)
0 :25	9.51	4.6	1.641	18.8	1.622	0.019	1.622	0.019
0 :35	9.88	4.6	1.616	19.2	1.622	-0.006	1.622	-0.006
0 :45	9.83	4.7	1.643	19.0	1.639	0.003	1.662	-0.020
0 :55	9.75	4.7	1.632	19.0	1.639	-0.008	1.662	-0.031
1 :05	9.80	4.8	1.629	18.9	1.657	-0.027	1.703	-0.074
1 :15	10.20	4.7	1.667	19.4	1.639	0.027	1.662	0.004
1 :25	9.73	4.7	1.661	18.9	1.639	0.022	1.662	-0.001
1 :35	9.73	4.6	1.622	19.0	1.622	0.000	1.622	0.000
1 :45	9.99	4.6	1.643	19.3	1.622	0.022	1.622	0.022
1 :55	9.86	4.5	1.654	19.3	1.604	0.050	1.581	0.073
2 :05	10.10	4.6	1.663	19.4	1.622	0.042	1.622	0.042
2 :15	10.28	4.8	1.698	19.4	1.657	0.042	1.703	-0.005
2 :25	10.04	4.6	1.693	19.3	1.622	0.072	1.622	0.072
2 :35	9.67	4.6	1.643	19.0	1.622	0.021	1.622	0.021
2 :45	9.59	4.5	1.605	19.0	1.604	0.001	1.581	0.024
2 :55	9.96	4.5	1.629	19.4	1.604	0.025	1.581	0.048
3 :05	9.57	4.7	1.628	18.8	1.639	-0.012	1.662	-0.035
3 :15	10.20	4.6	1.648	19.5	1.622	0.026	1.622	0.026
3 :25	9.91	4.6	1.676	19.2	1.622	0.054	1.622	0.054
3 :35	10.47	4.5	1.698	19.9	1.604	0.094	1.581	0.117
3 :45	9.94	4.7	1.701	19.1	1.639	0.062	1.662	0.039
3 :55	9.78	4.7	1.643	19.0	1.639	0.004	1.662	-0.019
4 :05	10.41	4.6	1.683	19.7	1.622	0.061	1.622	0.061
4 :15	9.83	4.6	1.687	19.1	1.622	0.065	1.622	0.065
4 :25	10.25	4.0	1.673	20.2	1.512	0.161	1.381	0.292
4 :35	9.65	3.8	1.658	19.9	1.474	0.184	1.302	0.357
4 :45	10.02	3.6	1.639	20.5	1.435	0.205	1.223	0.416
4 :55	8.24	3.6	1.522	18.6	1.435	0.087	1.223	0.298
5 :05	7.82	3.9	1.338	17.8	1.493	-0.155	1.341	-0.003
5 :15	7.80	3.7	1.302	18.0	1.454	-0.153	1.262	0.039
5 :25	8.14	3.9	1.328	18.1	1.493	-0.165	1.341	-0.013
5 :35	9.80	3.9	1.495	19.9	1.493	0.002	1.341	0.154
5 :45	9.17	3.6	1.581	19.6	1.435	0.146	1.223	0.358
5 :55	10.73	3.0	1.658	22.2	1.310	0.349	0.992	0.666
6 :05	11.15	2.5	1.823	23.7	1.196	0.628	0.804	1.019
6 :15	13.64	1.6	2.066	29.4	0.956	1.109	0.481	1.584
6 :25	16.15	1.5	2.483	32.5	0.926	1.556	0.447	2.036
6 :35	15.91	1.3	2.672	33.4	0.862	1.810	0.379	2.293
6 :45	15.94	1.1	2.654	34.8	0.793	1.861	0.313	2.341
6 :55	18.00	1.1	2.828	37.0	0.793	2.035	0.313	2.515
7 :05	16.63	1.0	2.886	36.4	0.756	2.130	0.280	2.605
7 :15	16.73	0.8	2.780	38.7	0.676	2.104	0.217	2.563
7 :25	17.16	0.8	2.824	39.1	0.676	2.148	0.217	2.607
7 :35	16.42	0.8	2.798	38.3	0.676	2.122	0.217	2.581
7 :45	16.26	1.0	2.723	36.0	0.756	1.967	0.280	2.443
7 :55	16.86	1.1	2.760	35.8	0.793	1.967	0.313	2.447
8 :05	17.50	1.1	2.863	36.5	0.793	2.070	0.313	2.550
8 :15	16.31	1.2	2.818	34.5	0.828	1.989	0.346	2.472
8 :25	15.28	1.2	2.633	33.4	0.828	1.804	0.346	2.287
8 :35	17.13	1.2	2.701	35.3	0.828	1.873	0.346	2.355
8 :45	16.42	1.0	2.796	36.2	0.756	2.040	0.280	2.515
8 :55	18.05	1.0	2.873	38.0	0.756	2.116	0.280	2.592
9 :05	17.31	1.1	2.947	36.3	0.793	2.154	0.313	2.634
9 :15	16.12	1.0	2.786	35.9	0.756	2.030	0.280	2.505
9 :25	16.55	1.0	2.723	36.4	0.756	1.966	0.280	2.442
9 :35	16.44	1.2	2.749	34.6	0.828	1.921	0.346	2.403

No. 007

Area : Plymouth

Date : Jan. 3-4. 1990

$$Q_x = Q_o \times (H_x/H_o)^n$$

--(n = 0.5)-- --(n = 1.15)--

--(orifice)-- --(crack)--

< TYPE - A > < TYPE - B >

TIME hour min	METERED	METERED	Qtotal m3	Leak hole d(mm)	< TYPE - A >		< TYPE - B >	
	Q (m3/h)	PRESSURE (kg/cm2)			Leak QA1(m3)	Demand QA2(m3)	Leak QB1(m3)	Demand QB2(m3)
9 :45	17.42	1.2	2.822	35.6	0.828	1.993	0.346	2.476
9 :55	15.99	1.2	2.784	34.1	0.828	1.956	0.346	2.438
10 :05	18.13	1.3	2.843	35.6	0.862	1.981	0.379	2.464
10 :15	16.10	1.3	2.853	33.6	0.862	1.990	0.379	2.473
10 :25	19.32	1.0	2.952	39.3	0.756	2.196	0.280	2.671
10 :35	19.38	1.0	3.225	39.3	0.756	2.469	0.280	2.945
10 :45	18.05	1.2	3.119	36.3	0.828	2.291	0.346	2.773
10 :55	16.42	1.1	2.873	35.4	0.793	2.079	0.313	2.560
11 :05	15.30	1.0	2.643	35.0	0.756	1.887	0.280	2.363
11 :15	14.96	1.0	2.522	34.6	0.756	1.766	0.280	2.241
11 :25	14.99	1.1	2.496	33.8	0.793	1.703	0.313	2.183
11 :35	16.34	1.1	2.611	35.3	0.793	1.818	0.313	2.298
11 :45	15.20	1.2	2.628	33.3	0.828	1.800	0.346	2.283
11 :55	15.46	1.2	2.555	33.6	0.828	1.727	0.346	2.209
12 :05	16.71	1.2	2.681	34.9	0.828	1.853	0.346	2.335
12 :15	19.01	1.3	2.977	36.5	0.862	2.115	0.379	2.598
12 :25	16.42	1.6	2.953	32.2	0.956	1.996	0.481	2.471
12 :35	16.49	1.9	2.743	30.9	1.042	1.700	0.587	2.156
12 :45	16.34	2.1	2.736	30.0	1.096	1.640	0.658	2.078
12 :55	15.52	2.0	2.655	29.6	1.069	1.586	0.622	2.033
13 :05	16.26	2.0	2.648	30.3	1.069	1.579	0.622	2.026
13 :15	15.60	2.2	2.655	29.0	1.121	1.534	0.694	1.961
13 :25	16.07	2.5	2.639	28.5	1.196	1.444	0.804	1.835
13 :35	15.70	2.3	2.648	28.8	1.147	1.501	0.731	1.917
13 :45	15.52	2.5	2.602	28.0	1.196	1.406	0.804	1.797
13 :55	16.84	2.7	2.697	28.6	1.242	1.454	0.879	1.818
14 :05	15.04	2.4	2.657	27.8	1.171	1.485	0.767	1.889
14 :15	15.52	2.0	2.547	29.6	1.069	1.477	0.622	1.924
14 :25	15.41	2.1	2.578	29.1	1.096	1.482	0.658	1.919
14 :35	16.68	2.1	2.674	30.3	1.096	1.578	0.658	2.016
14 :45	15.12	2.4	2.650	27.9	1.171	1.479	0.767	1.883
14 :55	15.46	2.7	2.548	27.4	1.242	1.306	0.879	1.670
15 :05	17.18	2.4	2.720	29.8	1.171	1.549	0.767	1.953
TOTAL	---	---	342.924	---	178.571	164.353	139.358	203.566
Average	14.30	2.88	2.381	27.3	52.07%	47.93%	40.64%	59.36%
MAX	21.41	4.80	3.448	39.3	1.657	2.469	1.703	2.945
MIN	7.80	0.80	1.302	17.8	0.676	-0.165	0.217	-0.074

kg/cm2 m3/10 min
 Leakage at Night: 4.60 1.622 19.037 : 1:35 a.m.
 Estimated night demand : 0.000

Nos. of house [A] 280 houses
 persons/house [B] 4.7 pesons/house
 A * B [C] 1316 persons

< TYPE - A > < TYPE - B >
 Water Demand [D] 164.35 M3 203.57 M3
 l/day/capita D/C 124.89 l/d/c 154.69 l/d/c

No. 008

Area : ARIMA (NETTOVILE)

Date : Jan. 9-10. 1990

$$Q_x = Q_0 \times (H_x/H_0)^n$$

--(n = 0.5)-- --(n = 1.15)--

--(orifice)-- --(crack)--

TIME	METERED		METERED	Qtotal	Leak	< TYPE - A >		< TYPE - B >		
	hour	min	Q			hole	Leak	Demand	Leak	Demand
			Q	m3	d(mm)	QA1(m3)	QA2(m3)	QB1(m3)	QB2(m3)	
			(m3/h)							
			(kg/cm2)							
	11	20	6.00	2.1	---	18.19	---	---	---	
	11	30	5.15	1.9	0.929	17.28	0.517	0.412	0.411	0.518
	11	40	4.23	1.9	0.782	15.66	0.517	0.265	0.411	0.370
	11	50	6.95	1.8	0.932	20.34	0.503	0.429	0.386	0.545
12	12	0	5.83	2.0	1.065	18.15	0.530	0.535	0.436	0.629
	12	10	3.66	2.2	0.791	14.04	0.556	0.235	0.487	0.304
	12	20	4.06	2.1	0.643	14.96	0.543	0.100	0.461	0.182
	12	30	3.28	2.2	0.612	13.29	0.556	0.056	0.487	0.125
	12	40	5.35	2.2	0.719	16.98	0.556	0.163	0.487	0.232
	12	50	4.57	2.3	0.827	15.52	0.569	0.258	0.512	0.314
	13	0	3.52	2.1	0.674	13.93	0.543	0.131	0.461	0.213
	13	10	4.54	2.2	0.672	15.64	0.556	0.116	0.487	0.185
	13	20	4.81	2.2	0.779	16.10	0.556	0.223	0.487	0.292
	13	30	5.18	2.3	0.833	16.52	0.569	0.264	0.512	0.320
	13	40	5.69	2.2	0.906	17.51	0.556	0.350	0.487	0.419
	13	50	5.35	2.1	0.920	17.17	0.543	0.377	0.461	0.459
14	14	0	6.68	2.1	1.003	19.19	0.543	0.459	0.461	0.541
	14	10	5.35	2.1	1.003	17.17	0.543	0.459	0.461	0.541
	14	20	6.17	2.0	0.960	18.67	0.530	0.430	0.436	0.524
	14	30	5.35	2.2	0.960	16.98	0.556	0.404	0.487	0.473
	14	40	6.00	2.2	0.946	17.98	0.556	0.390	0.487	0.459
	14	50	6.57	2.3	1.048	18.60	0.569	0.479	0.512	0.535
	15	0	5.66	2.4	1.019	17.03	0.584	0.435	0.546	0.473
	15	10	5.76	2.3	0.952	17.42	0.569	0.383	0.512	0.439
	15	20	4.27	2.3	0.836	15.00	0.569	0.267	0.512	0.324
	15	30	4.88	2.4	0.763	15.86	0.581	0.182	0.538	0.225
	15	40	4.44	2.3	0.777	15.29	0.569	0.208	0.512	0.264
	15	50	6.03	2.3	0.873	17.82	0.569	0.304	0.512	0.360
16	16	0	6.00	2.3	1.003	17.78	0.569	0.434	0.512	0.490
	16	10	6.61	2.3	1.051	18.66	0.569	0.482	0.512	0.539
	16	20	5.32	2.2	0.994	16.93	0.556	0.438	0.487	0.507
	16	30	6.64	2.1	0.997	19.13	0.543	0.453	0.461	0.535
	16	40	5.42	2.1	1.005	17.29	0.543	0.462	0.461	0.544
	16	50	6.44	2.0	0.988	19.07	0.530	0.458	0.436	0.552
	17	0	4.37	2.1	0.901	15.52	0.543	0.358	0.461	0.439
	17	10	5.08	2.3	0.788	16.36	0.569	0.219	0.512	0.275
	17	20	4.20	2.2	0.773	15.04	0.556	0.217	0.487	0.287
	17	30	4.44	2.3	0.720	15.29	0.569	0.151	0.512	0.208
	17	40	4.61	2.2	0.754	15.76	0.556	0.198	0.487	0.267
	17	50	4.61	2.4	0.768	15.42	0.581	0.188	0.538	0.230
18	18	0	7.46	2.2	1.006	20.04	0.556	0.450	0.487	0.519
	18	10	5.05	2.4	1.043	16.14	0.581	0.462	0.538	0.505
	18	20	4.98	2.2	0.836	16.38	0.556	0.280	0.487	0.349
	18	30	3.59	2.3	0.714	13.75	0.569	0.146	0.512	0.202
	18	40	6.61	2.5	0.850	18.27	0.593	0.257	0.564	0.286
	18	50	5.73	2.7	1.028	16.69	0.616	0.412	0.616	0.412
	19	0	5.64	2.8	0.948	16.41	0.627	0.320	0.642	0.305
	19	10	7.63	3.0	1.106	18.76	0.649	0.457	0.695	0.410
	19	20	9.49	2.9	1.427	21.10	0.638	0.788	0.669	0.758
	19	30	10.85	2.9	1.695	22.56	0.638	1.057	0.669	1.026
	19	40	10.10	3.2	1.746	21.24	0.671	1.075	0.749	0.997
	19	50	9.66	3.1	1.647	20.94	0.660	0.987	0.722	0.925
20	20	0	7.46	2.6	1.427	19.22	0.604	0.822	0.590	0.837
	20	10	10.17	2.1	1.469	23.68	0.543	0.926	0.461	1.008
	20	20	4.78	2.1	1.246	16.23	0.543	0.703	0.461	0.784
	20	30	8.13	2.3	1.076	20.69	0.569	0.507	0.512	0.564

No. 008

Area : ARIMA (NETTOVILE)

Date : Jan. 9-10. 1990

$$Q_x = Q_o \times (H_x/H_o)^n$$

--(n = 0.5)-- --(n = 1.15)--
 --(orifice)-- --(crack)--

TIME	METERED		Qtotal	Leak	< TYPE - A >		< TYPE - B >			
	hour	min			Q (m3/h)	PRESSURE (kg/cm2)	Leak QA1(m3)	Demand QA2(m3)	Leak QB1(m3)	Demand QB2(m3)
	20	40	6.78	2.3	1.243	18.90	0.569	0.674	0.512	0.730
	20	50	8.30	2.4	1.257	20.69	0.581	0.676	0.538	0.719
	21	0	7.97	2.4	1.356	20.27	0.581	0.775	0.538	0.818
	21	10	8.03	2.5	1.333	20.14	0.593	0.741	0.564	0.770
	21	20	8.37	2.5	1.367	20.56	0.593	0.774	0.564	0.803
	21	30	8.85	2.8	1.435	20.56	0.627	0.808	0.642	0.793
	21	40	8.30	2.8	1.429	19.91	0.627	0.802	0.642	0.787
	21	50	7.66	2.8	1.330	19.12	0.627	0.703	0.642	0.688
22	22	0	8.03	2.8	1.308	19.58	0.627	0.680	0.642	0.665
	22	10	8.68	2.8	1.393	20.36	0.627	0.765	0.642	0.750
	22	20	9.29	3.0	1.498	20.70	0.649	0.848	0.695	0.802
	22	30	7.66	2.9	1.413	18.96	0.638	0.774	0.669	0.744
	22	40	8.17	2.9	1.319	19.58	0.638	0.681	0.669	0.650
	22	50	8.47	2.8	1.387	20.11	0.627	0.759	0.642	0.744
	23	0	8.75	2.7	1.435	20.63	0.616	0.819	0.616	0.819
	23	10	5.83	2.7	1.215	16.84	0.616	0.599	0.616	0.599
	23	20	5.12	2.7	0.913	15.78	0.616	0.297	0.616	0.297
	23	30	4.47	2.7	0.799	14.74	0.616	0.183	0.616	0.183
	23	40	3.90	2.7	0.698	13.77	0.616	0.082	0.616	0.082
	23	50	3.49	2.7	0.616	13.03	0.616	-0.000	0.616	-0.000
0	0	0	4.13	2.7	0.635	14.17	0.616	0.019	0.616	0.019
	0	10	4.47	2.8	0.717	14.61	0.627	0.089	0.642	0.074
	0	20	4.30	2.8	0.731	14.33	0.627	0.104	0.642	0.089
	0	30	3.93	2.8	0.686	13.70	0.627	0.059	0.642	0.044
	0	40	4.00	2.8	0.661	13.82	0.627	0.034	0.642	0.019
	0	50	3.93	2.8	0.661	13.70	0.627	0.034	0.642	0.019
	1	0	4.37	2.8	0.692	14.44	0.627	0.064	0.642	0.049
	1	10	4.13	2.8	0.708	14.04	0.627	0.081	0.642	0.066
	1	20	4.13	2.8	0.688	14.04	0.627	0.061	0.642	0.046
	1	30	3.86	2.8	0.666	13.58	0.627	0.039	0.642	0.024
	1	40	4.34	2.8	0.683	14.39	0.627	0.056	0.642	0.041
	1	50	4.17	3.0	0.709	13.87	0.649	0.060	0.695	0.014
2	2	0	4.03	2.9	0.683	13.75	0.638	0.045	0.669	0.015
	2	10	4.34	2.8	0.698	14.39	0.627	0.070	0.642	0.055
	2	20	3.79	2.8	0.678	13.45	0.627	0.050	0.642	0.035
	2	30	4.17	2.8	0.663	14.11	0.627	0.036	0.642	0.021
	2	40	4.13	2.8	0.692	14.04	0.627	0.064	0.642	0.049
	2	50	4.54	2.8	0.723	14.72	0.627	0.095	0.642	0.080
	3	0	4.74	2.8	0.773	15.04	0.627	0.146	0.642	0.131
	3	10	4.54	2.8	0.773	14.72	0.627	0.146	0.642	0.131
	3	20	4.61	2.8	0.763	14.84	0.627	0.135	0.642	0.120
	3	30	4.37	2.8	0.748	14.44	0.627	0.121	0.642	0.106
	3	40	4.30	2.8	0.723	14.33	0.627	0.095	0.642	0.080
	3	50	4.27	2.8	0.714	14.28	0.627	0.087	0.642	0.072
4	4	0	4.13	2.8	0.700	14.04	0.627	0.073	0.642	0.058
	4	10	4.17	3.0	0.692	13.87	0.649	0.042	0.695	-0.004
	4	20	4.03	3.0	0.683	13.63	0.649	0.034	0.695	-0.012
	4	30	4.81	3.0	0.737	14.89	0.649	0.087	0.695	0.041
	4	40	6.03	2.8	0.903	16.97	0.627	0.276	0.642	0.261
	4	50	4.71	2.9	0.895	14.86	0.638	0.257	0.669	0.226
	5	0	4.64	2.9	0.779	14.75	0.638	0.141	0.669	0.110
	5	10	5.42	2.8	0.838	16.09	0.627	0.211	0.642	0.196
	5	20	2.10	2.8	0.627	10.01	0.627	-0.001	0.642	-0.016
	5	30	4.54	2.7	0.553	14.86	0.616	-0.063	0.616	-0.063
	5	40	1.52	2.6	0.505	8.68	0.604	-0.099	0.590	-0.085
	5	50	2.67	2.3	0.349	11.86	0.569	-0.219	0.512	-0.163

No. 008
 Area : ARIMA (NETTOVILE)
 Date : Jan. 9-10. 1990

$$Q_x = Q_0 \times (H_x/H_0)^n$$

--(n = 0.5)-- --(n = 1.15)--
 --(orifice)-- --(crack)--

TIME	METERED		METERED	Qtotal	Leak hole	< TYPE - A >		< TYPE - B >		
	hour	min	Q			PRESSURE	Leak	Demand	Leak	Demand
			(m3/h)	(kg/cm2)	m3	d(mm)	QA1(m3)	QA2(m3)	QB1(m3)	QB2(m3)
6	6	0	2.00	2.2	0.389	10.38	0.556	-0.167	0.487	-0.098
	6	10	3.08	2.0	0.423	13.19	0.530	-0.107	0.436	-0.013
	6	20	3.01	1.9	0.508	13.21	0.517	-0.009	0.411	0.096
	6	30	5.73	1.8	0.728	18.47	0.503	0.225	0.386	0.342
	6	40	7.29	1.7	1.085	21.13	0.489	0.596	0.362	0.723
	6	50	6.74	1.6	1.169	20.63	0.474	0.695	0.337	0.832
	7	0	5.35	1.6	1.008	18.38	0.474	0.533	0.337	0.670
	7	10	6.78	1.7	1.011	20.38	0.489	0.522	0.362	0.649
	7	20	7.93	1.6	1.226	22.38	0.474	0.752	0.337	0.888
	7	30	6.00	1.7	1.161	19.17	0.489	0.672	0.362	0.799
	7	40	7.32	1.7	1.110	21.18	0.489	0.621	0.362	0.748
	7	50	6.07	1.7	1.116	19.29	0.489	0.627	0.362	0.754
8	8	0	6.40	1.7	1.039	19.80	0.489	0.550	0.362	0.677
	8	10	4.71	1.8	0.926	16.75	0.503	0.423	0.386	0.539
	8	20	5.15	1.9	0.822	17.28	0.517	0.305	0.411	0.410
	8	30	5.49	1.9	0.887	17.84	0.517	0.370	0.411	0.475
	8	40	3.83	1.8	0.777	15.14	0.500	0.277	0.382	0.395
	8	50	6.88	1.8	0.893	20.24	0.503	0.390	0.386	0.506
	9	0	5.66	2.0	1.045	17.88	0.530	0.515	0.436	0.609
	9	10	6.51	1.9	1.014	19.42	0.517	0.497	0.411	0.603
	9	20	6.07	1.9	1.048	18.76	0.517	0.532	0.411	0.637
	9	30	7.42	1.9	1.124	20.74	0.517	0.607	0.411	0.713
	9	40	7.02	1.3	1.203	22.18	0.427	0.776	0.266	0.938
	9	50	8.51	1.9	1.294	22.21	0.517	0.777	0.411	0.883
10	10	0	16.07	2.0	2.048	30.13	0.530	1.518	0.436	1.612
	10	10	8.37	2.0	2.037	21.74	0.530	1.506	0.436	1.600
	10	20	7.63	2.1	1.333	20.51	0.543	0.790	0.461	0.872
	10	30	6.03	2.2	1.138	18.02	0.556	0.582	0.487	0.652
	10	40	8.13	1.5	1.180	23.03	0.459	0.721	0.313	0.867
	10	50	6.07	2.1	1.183	18.29	0.543	0.640	0.461	0.722
	11	0	17.46	3.0	1.961	28.38	0.649	1.312	0.695	1.265
	11	10	7.02	2.1	2.040	19.67	0.543	1.497	0.461	1.579
	11	20	7.08	2.1	1.175	19.76	0.543	0.632	0.461	0.714
TOTAL			---	---	140.192	---	83.028	57.163	77.113	63.078
Average			5.85	2.38	0.974	17.219	59.22%	40.78%	55.01%	44.99%
MAX			17.46	3.20	2.048	30.129	0.671	1.518	0.749	1.612
MIN			1.52	1.30	0.349	8.678	0.427	-0.219	0.266	-0.163

kg/cm2 m3/10 min
 Leakage at Night: 2.70 0.616 13.030 : 23:50 a.m.
 Estimated night demand : 0.000

Nos. of house [A] 91 houses
 persons/house [B] 4.4 pesons/house
 A * B [C] 400.4 persons

< TYPE - A > < TYPE - B >
 Water Demand [D] 57.16 M3 63.08 M3
 l/day/capita D/C 142.77 l/d/c 157.54 l/d/c

No. 009

Area : ARIMA (TUMPUNA)

Date : Jan. 9-10. 1990

$$Q_x = Q_o \times (H_x/H_o)^n$$

--(n = 0.5)-- --(n = 1.15)--
 --(orifice)-- --(crack)--

	TIME		METERED Q	METERED PRESSURE	Qtotal m3	Leak hole d(mm)	< TYPE - A >		< TYPE - B >		
	hour	min	(m3/h)	(kg/cm2)			Leak QA1(m3)	Demand QA2(m3)	Leak QB1(m3)	Demand QB2(m3)	
14	14	0	30.25	3.4	---	36.20	---	---	---	---	
	14	10	26.48	3.3	4.728	34.12	0.564	4.164	0.482	4.246	
	14	20	23.36	3.2	4.153	32.30	0.555	3.598	0.465	3.688	
	14	30	25.26	3.1	4.052	33.85	0.546	3.505	0.448	3.603	
	14	40	20.58	3.1	3.820	30.56	0.546	3.274	0.448	3.372	
	14	50	24.69	3.2	3.773	33.21	0.555	3.217	0.465	3.307	
	15	0	26.48	3.3	4.264	34.12	0.564	3.701	0.482	3.782	
	15	10	21.73	3.3	4.018	30.91	0.564	3.454	0.482	3.536	
	15	20	22.96	3.4	3.724	31.54	0.572	3.152	0.499	3.226	
	15	30	24.75	3.5	3.976	32.51	0.580	3.395	0.516	3.460	
	15	40	21.73	3.2	3.873	31.15	0.555	3.318	0.465	3.408	
	15	50	16.51	3.5	3.187	26.55	0.580	2.606	0.516	2.671	
	16	16	0	21.56	3.7	3.173	29.92	0.597	2.576	0.550	2.623
		16	10	18.31	3.2	3.323	28.60	0.555	2.767	0.465	2.857
		16	20	14.92	3.5	2.769	25.24	0.580	2.189	0.516	2.254
16		30	14.75	3.0	2.473	26.08	0.537	1.935	0.432	2.041	
16		40	16.04	2.8	2.566	27.67	0.519	2.047	0.399	2.167	
16		50	14.71	2.6	2.563	27.00	0.500	2.062	0.366	2.196	
17		0	14.99	1.2	2.475	33.06	0.340	2.135	0.151	2.324	
17		10	15.43	1.0	2.535	35.11	0.310	2.225	0.122	2.413	
17		20	16.78	0.8	2.684	38.71	0.278	2.407	0.094	2.590	
17		30	15.09	1.3	2.656	32.52	0.354	2.302	0.165	2.491	
18	17	40	16.78	1.1	2.656	35.75	0.325	2.330	0.136	2.520	
	17	50	10.37	1.0	2.263	28.78	0.310	1.952	0.122	2.140	
	18	0	8.20	1.2	1.548	24.45	0.340	1.208	0.151	1.397	
	18	10	11.02	2.0	1.602	24.95	0.439	1.163	0.271	1.331	
	18	20	9.08	1.3	1.675	25.22	0.354	1.321	0.165	1.510	
	18	30	13.12	1.9	1.850	27.58	0.428	1.422	0.255	1.595	
	18	40	11.56	2.1	2.057	25.24	0.450	1.607	0.287	1.770	
	18	50	9.93	2.1	1.791	23.40	0.450	1.341	0.287	1.504	
	19	0	9.46	2.1	1.616	22.84	0.450	1.166	0.287	1.329	
	19	10	8.81	2.1	1.523	22.04	0.450	1.073	0.287	1.236	
20	19	20	10.14	2.2	1.579	23.37	0.460	1.119	0.302	1.277	
	19	30	14.21	2.4	2.029	27.07	0.481	1.549	0.334	1.695	
	19	40	13.36	2.1	2.298	27.14	0.450	1.848	0.287	2.011	
	19	50	9.66	2.3	1.918	22.56	0.471	1.448	0.318	1.600	
	20	0	11.36	2.4	1.752	24.20	0.481	1.271	0.334	1.418	
	20	10	8.00	2.3	1.613	20.53	0.471	1.143	0.318	1.295	
	20	20	6.20	2.5	1.183	17.70	0.491	0.693	0.350	0.833	
	20	30	8.34	2.7	1.212	20.14	0.510	0.702	0.383	0.829	
	20	40	12.07	2.8	1.701	24.01	0.519	1.182	0.399	1.302	
	20	50	8.85	2.7	1.743	20.74	0.510	1.234	0.383	1.361	
22	21	0	10.68	1.8	1.628	25.22	0.416	1.211	0.240	1.388	
	21	10	7.46	2.4	1.512	19.61	0.481	1.031	0.334	1.178	
	21	20	5.18	2.8	1.053	15.73	0.519	0.534	0.399	0.654	
	21	30	6.61	3.3	0.983	17.05	0.564	0.419	0.482	0.501	
	21	40	6.40	2.4	1.084	18.17	0.481	0.604	0.334	0.750	
	21	50	6.57	2.4	1.081	18.41	0.481	0.600	0.334	0.747	
	22	0	7.22	2.3	1.149	19.50	0.471	0.679	0.318	0.831	
	22	10	6.03	3.7	1.104	15.83	0.597	0.507	0.550	0.555	
	22	20	7.29	3.8	1.110	17.28	0.605	0.505	0.567	0.543	
	22	30	5.18	3.8	1.039	14.57	0.605	0.434	0.567	0.472	
23	22	40	4.68	3.8	0.822	13.85	0.605	0.217	0.567	0.255	
	22	50	4.23	3.9	0.743	13.08	0.613	0.130	0.584	0.159	
	23	0	4.44	4.0	0.723	13.32	0.621	0.102	0.601	0.121	
	23	10	3.90	4.0	0.695	12.48	0.621	0.074	0.601	0.094	

No. 009
 Area : ARIMA (TUMPUNA)
 Date : Jan. 9-10, 1990

$$Q_x = Q_o \times (H_x/H_o)^n$$

---(n = 0.5)--- ---(n = 1.15)---
 ---(orifice)--- ---(crack)---

TIME	METERED		Qtotal	Leak	< TYPE - A >		< TYPE - B >			
	hour	min			Q	PRESSURE	Leak	Demand	Leak	Demand
			m3	d(mm)	QA1(m3)	QA2(m3)	QB1(m3)	QB2(m3)		
0	23	20	3.86	4.0	0.647	12.42	0.621	0.026	0.601	0.046
	23	30	4.61	4.0	0.706	13.57	0.621	0.085	0.601	0.105
	23	40	4.06	4.0	0.723	12.73	0.621	0.102	0.601	0.121
	23	50	5.83	4.3	0.824	14.99	0.643	0.181	0.653	0.171
	0	0	4.71	4.0	0.878	13.72	0.621	0.258	0.601	0.277
	0	10	4.03	4.1	0.728	12.61	0.628	0.100	0.618	0.110
	0	20	4.20	4.2	0.686	12.80	0.636	0.050	0.636	0.050
	0	30	4.98	4.2	0.765	13.93	0.636	0.129	0.636	0.129
	0	40	4.51	4.2	0.791	13.26	0.636	0.155	0.636	0.155
	0	50	4.00	4.2	0.709	12.49	0.636	0.073	0.636	0.073
	1	0	4.20	4.2	0.683	12.80	0.636	0.047	0.636	0.047
	1	10	4.10	4.2	0.692	12.64	0.636	0.056	0.636	0.056
	1	20	4.03	4.3	0.678	12.46	0.643	0.034	0.653	0.024
	1	30	3.76	4.2	0.649	12.11	0.636	0.013	0.636	0.013
	1	40	4.06	4.2	0.652	12.58	0.636	0.016	0.636	0.016
	1	50	4.03	4.2	0.674	12.53	0.636	0.038	0.636	0.038
2	2	0	3.90	4.2	0.661	12.33	0.636	0.025	0.636	0.025
	2	10	3.73	4.2	0.636	12.06	0.636	0.000	0.636	0.000
	2	20	4.27	4.3	0.667	12.83	0.643	0.023	0.653	0.013
	2	30	4.44	4.2	0.726	13.16	0.636	0.090	0.636	0.090
	2	40	4.00	4.2	0.703	12.49	0.636	0.068	0.636	0.068
	2	50	4.03	4.4	0.669	12.39	0.651	0.018	0.671	-0.002
	3	0	4.13	4.3	0.680	12.61	0.643	0.037	0.653	0.027
	3	10	4.10	4.3	0.686	12.57	0.643	0.042	0.653	0.033
	3	20	4.98	4.2	0.757	13.93	0.636	0.121	0.636	0.121
	3	30	4.03	4.2	0.751	12.53	0.636	0.115	0.636	0.115
	3	40	4.27	4.2	0.692	12.90	0.636	0.056	0.636	0.056
	3	50	4.06	4.2	0.694	12.58	0.636	0.058	0.636	0.058
4	4	0	4.13	4.2	0.683	12.69	0.636	0.047	0.636	0.047
	4	10	4.13	4.2	0.688	12.69	0.636	0.052	0.636	0.052
	4	20	4.20	4.2	0.694	12.80	0.636	0.058	0.636	0.058
	4	30	3.45	4.2	0.638	11.60	0.636	0.002	0.636	0.002
	4	40	4.64	4.2	0.674	13.45	0.636	0.038	0.636	0.038
	4	50	3.86	3.4	0.708	12.93	0.572	0.136	0.499	0.210
	5	0	4.00	3.8	0.655	12.80	0.605	0.050	0.567	0.088
	5	10	6.07	3.7	0.839	15.88	0.597	0.242	0.550	0.290
	5	20	7.46	3.2	1.128	18.25	0.555	0.572	0.465	0.662
	5	30	7.32	3.0	1.232	18.37	0.537	0.694	0.432	0.800
	5	40	5.73	3.0	1.088	16.26	0.537	0.550	0.432	0.656
	5	50	8.30	3.0	1.169	19.57	0.537	0.632	0.432	0.737
6	6	0	5.25	3.0	1.129	15.56	0.537	0.592	0.432	0.697
	6	10	7.39	2.4	1.053	19.52	0.481	0.573	0.334	0.719
	6	20	10.37	2.7	1.480	22.45	0.510	0.970	0.383	1.097
	6	30	13.46	2.7	1.986	25.58	0.510	1.476	0.383	1.603
	6	40	13.97	2.1	2.286	27.75	0.450	1.836	0.287	1.999
	6	50	10.61	2.1	2.048	24.18	0.450	1.599	0.287	1.762
	7	0	12.71	2.2	1.943	26.16	0.460	1.483	0.302	1.641
	7	10	12.54	2.1	2.104	26.29	0.450	1.655	0.287	1.818
	7	20	14.27	1.9	2.234	28.76	0.428	1.807	0.255	1.979
	7	30	11.80	1.8	2.173	26.51	0.416	1.756	0.240	1.933
	7	40	14.27	1.6	2.173	30.02	0.392	1.780	0.210	1.963
	7	50	13.39	1.7	2.305	28.64	0.405	1.900	0.225	2.080
8	8	0	13.80	1.7	2.266	29.08	0.405	1.861	0.225	2.041
	8	10	13.59	1.7	2.283	28.86	0.405	1.878	0.225	2.058
	8	20	15.46	1.7	2.421	30.78	0.405	2.016	0.225	2.196
	8	30	17.87	1.7	2.778	33.09	0.405	2.373	0.225	2.553

No. 009

Area : ARIMA (TUMPUNA)

Date : Jan. 9-10. 1990

$$Q_x = Q_o \times (H_x/H_o)^n$$

--(n = 0.5)-- --(n = 1.15)--
 --(orifice)-- --(crack)--

TIME	METERED		Qtotal	Leak	< TYPE - A >		< TYPE - B >			
	hour	min			Q (m3/h)	PRESSURE (kg/cm2)	Leak	Demand	Leak	Demand
			m3	d(mm)	QA1(m3)	QA2(m3)	QB1(m3)	QB2(m3)		
8	40	13.66	1.0	2.628	33.03	0.310	2.317	0.122	2.505	
8	50	12.17	1.5	2.153	28.17	0.380	1.773	0.195	1.958	
9	0	12.54	1.4	2.059	29.10	0.367	1.692	0.180	1.879	
9	10	11.36	1.7	1.992	26.38	0.405	1.587	0.225	1.767	
9	20	9.39	1.9	1.729	23.33	0.428	1.302	0.255	1.474	
9	30	9.86	2.2	1.604	23.04	0.460	1.144	0.302	1.302	
9	40	10.75	2.6	1.718	23.08	0.500	1.217	0.366	1.351	
9	50	12.07	2.6	1.902	24.45	0.500	1.401	0.366	1.535	
10	10	0	11.76	2.5	1.986	24.38	0.491	1.495	0.350	1.636
10	10	10	6.98	2.7	1.562	18.42	0.510	1.052	0.383	1.179
10	20	10.14	2.6	1.427	22.41	0.500	0.926	0.366	1.060	
10	30	7.56	2.7	1.475	19.17	0.510	0.965	0.383	1.092	
10	40	5.69	2.7	1.104	16.63	0.510	0.594	0.383	0.722	
10	50	6.51	2.6	1.017	17.96	0.500	0.516	0.366	0.650	
11	0	8.41	2.7	1.243	20.22	0.510	0.734	0.383	0.861	
11	10	7.32	2.2	1.311	19.86	0.460	0.851	0.302	1.009	
11	20	8.34	2.8	1.305	19.95	0.519	0.786	0.399	0.906	
11	30	8.44	2.8	1.398	20.07	0.519	0.879	0.399	0.999	
11	40	10.37	2.9	1.568	22.06	0.528	1.039	0.415	1.152	
11	50	5.42	2.9	1.316	15.95	0.528	0.787	0.415	0.901	
12	12	0	5.25	2.8	0.889	15.83	0.519	0.370	0.399	0.490
12	10	6.78	2.9	1.003	17.83	0.528	0.474	0.415	0.587	
12	20	6.37	3.0	1.096	17.14	0.537	0.558	0.432	0.664	
12	30	6.17	3.0	1.045	16.87	0.537	0.508	0.432	0.613	
12	40	7.18	3.1	1.113	18.05	0.546	0.566	0.448	0.664	
12	50	5.05	3.3	1.019	14.90	0.564	0.456	0.482	0.537	
13	0	8.17	3.4	1.102	18.81	0.572	0.530	0.499	0.603	
13	10	9.22	3.5	1.449	19.84	0.580	0.869	0.516	0.934	
13	20	5.86	3.5	1.257	15.82	0.580	0.676	0.516	0.741	
13	30	5.08	3.2	0.912	15.06	0.555	0.357	0.465	0.447	
13	40	6.30	3.3	0.948	16.64	0.564	0.385	0.482	0.466	
13	50	5.96	3.3	1.022	16.19	0.564	0.458	0.482	0.540	
14	14	0	7.66	3.4	1.135	18.22	0.572	0.563	0.499	0.636
TOTAL		---	---	230.256	---	75.931	154.325	62.122	168.133	
Average		9.66	2.98	1.599	20.875	32.98%	67.02%	26.98%	73.02%	
MAX		30.25	4.40	4.728	38.714	0.651	4.164	0.671	4.246	
MIN		3.45	0.80	0.636	11.597	0.278	0.000	0.094	-0.002	

Leakage at Night: $\frac{\text{kg/cm}^2}{4.20}$ $\frac{\text{m}^3/10 \text{ min}}{0.636}$ 12.06 : 2:10 a.m.
 Estimated night demand : 0.000

Nos. of house [A] 102 houses
 persons/house [B] 4.4 pesons/house
 A * B [C] 448.8 persons

< TYPE - A > < TYPE - B >
 Water Demand [D] 154.32 M3 168.13 M3
 l/day/capita D/C 343.86 l/d/c 374.63 l/d/c

No. 011
 Area : RANGE PARK. CHAGUANAS
 Date : Jan. 24-25. 1990

$$Q_x = Q_o \times (H_x/H_o)^n$$

--(n = 0.5)-- --(n = 1.15)--
 --(orifice)-- --(crack)--

TIME hour min	METERED		Qtotal m3	Leak hole d(mm)	< TYPE - A >		< TYPE - B >	
	Q (m3/h)	PRESSURE (kg/cm2)			Leak QA1(m3)	Demand QA2(m3)	Leak QB1(m3)	Demand QB2(m3)
10 :30	7.66	1.6	---	22.00	---	---	---	---
10 :40	7.76	1.6	1.285	22.14	0.683	0.602	0.498	0.787
10 :50	7.86	1.6	1.302	22.28	0.683	0.619	0.498	0.803
11 :00	7.86	0.8	1.310	26.50	0.483	0.827	0.225	1.085
11 :10	7.49	1.5	1.279	22.10	0.661	0.618	0.463	0.817
11 :20	7.29	2.4	1.232	19.39	0.837	0.395	0.794	0.437
11 :30	4.57	1.7	0.988	16.73	0.704	0.284	0.534	0.454
11 :40	5.32	1.7	0.824	18.05	0.704	0.120	0.534	0.290
11 :50	5.49	1.2	0.901	20.01	0.592	0.309	0.358	0.543
12 :00	5.66	1.2	0.929	20.32	0.592	0.338	0.358	0.571
12 :10	5.79	2.1	0.954	17.87	0.783	0.172	0.681	0.273
12 :20	4.84	1.8	0.886	16.98	0.725	0.161	0.571	0.315
12 :30	4.44	1.6	0.773	16.75	0.683	0.090	0.498	0.275
12 :40	5.46	1.8	0.825	18.03	0.725	0.100	0.571	0.254
12 :50	6.88	1.5	1.028	21.18	0.661	0.367	0.463	0.566
13 :00	5.93	1.3	1.068	20.38	0.616	0.452	0.392	0.675
13 :10	4.51	1.4	0.870	17.45	0.639	0.231	0.427	0.443
13 :20	3.45	2.0	0.663	13.96	0.764	-0.100	0.644	0.019
13 :30	3.12	1.9	0.548	13.45	0.744	-0.197	0.607	-0.060
13 :40	3.90	2.0	0.585	14.84	0.764	-0.179	0.644	-0.059
13 :50	4.40	1.9	0.692	15.97	0.744	-0.053	0.607	0.085
14 :00	4.20	1.7	0.717	16.04	0.704	0.013	0.534	0.182
14 :10	3.69	1.9	0.658	14.62	0.744	-0.087	0.607	0.050
14 :20	4.71	1.8	0.700	16.75	0.725	-0.025	0.571	0.129
14 :30	3.69	1.6	0.700	15.27	0.683	0.017	0.498	0.202
14 :40	3.66	1.8	0.613	14.76	0.725	-0.112	0.571	0.042
14 :50	3.18	1.8	0.570	13.76	0.725	-0.155	0.571	-0.001
15 :00	3.45	1.8	0.553	14.33	0.725	-0.172	0.571	-0.018
15 :10	4.03	1.8	0.623	15.49	0.725	-0.101	0.571	0.053
15 :20	4.95	1.8	0.748	17.17	0.725	0.024	0.571	0.178
15 :30	3.25	1.8	0.683	13.91	0.725	-0.041	0.571	0.113
15 :40	4.88	2.0	0.678	16.60	0.764	-0.086	0.644	0.033
15 :50	4.98	2.1	0.822	16.57	0.783	0.039	0.681	0.140
16 :00	4.91	1.5	0.824	17.90	0.661	0.163	0.463	0.362
16 :10	3.01	1.4	0.660	14.26	0.639	0.021	0.427	0.233
16 :20	3.66	1.2	0.556	16.34	0.592	-0.036	0.358	0.198
16 :30	4.68	1.5	0.695	17.47	0.661	0.034	0.463	0.232
16 :40	3.32	1.7	0.667	14.26	0.704	-0.037	0.534	0.132
16 :50	4.40	3.0	0.643	14.25	0.935	-0.292	1.027	-0.383
17 :00	2.71	1.2	0.593	14.06	0.592	0.001	0.358	0.235
17 :10	3.25	1.2	0.497	15.40	0.592	-0.095	0.358	0.139
17 :20	2.17	1.4	0.452	12.10	0.639	-0.187	0.427	0.024
17 :30	5.15	1.4	0.610	18.65	0.639	-0.029	0.427	0.183
17 :40	6.44	1.3	0.966	21.24	0.616	0.350	0.392	0.573
17 :50	4.20	1.3	0.887	17.15	0.616	0.271	0.392	0.494
18 :00	4.78	1.4	0.748	17.96	0.639	0.109	0.427	0.321
18 :10	7.05	1.4	0.986	21.82	0.639	0.347	0.427	0.559
18 :20	4.78	1.2	0.986	18.67	0.592	0.394	0.358	0.628
18 :30	5.05	1.4	0.819	18.47	0.639	0.180	0.427	0.392
18 :40	6.03	1.2	0.923	20.97	0.592	0.332	0.358	0.565
18 :50	4.91	1.0	0.912	19.81	0.540	0.372	0.290	0.621
19 :00	5.62	1.3	0.878	19.84	0.616	0.262	0.392	0.485
19 :10	6.13	1.1	0.979	21.61	0.566	0.413	0.324	0.655
19 :20	6.10	1.0	1.019	22.08	0.540	0.479	0.290	0.729
19 :30	6.20	1.4	1.025	20.46	0.639	0.386	0.427	0.598
19 :40	7.22	1.3	1.118	22.49	0.616	0.503	0.392	0.726

No. 011
 Area : RANGE PARK. CHAGUANAS
 Date : Jan. 24-25. 1990

$$Q_x = Q_o \times (H_x/H_o)^n$$

--(n = 0.5)-- --(n = 1.15)--
 --(orifice)-- --(crack)--

TIME	METERED		Qtotal	Leak hole	< TYPE - A >		< TYPE - B >		
	hour min	Q (m3/h)			PRESSURE (kg/cm2)	d(mm)	Leak QA1(m3)	Demand QA2(m3)	Leak QB1(m3)
20	19 :50	6.88	1.5	1.175	21.18	0.661	0.514	0.463	0.712
	20 :00	6.74	1.5	1.135	20.97	0.661	0.474	0.463	0.672
	20 :10	6.47	1.4	1.101	20.90	0.639	0.462	0.427	0.674
	20 :20	6.40	1.6	1.073	20.10	0.683	0.389	0.498	0.574
	20 :30	5.08	1.8	0.957	17.39	0.725	0.232	0.571	0.386
	20 :40	4.27	1.6	0.779	16.42	0.683	0.096	0.498	0.281
	20 :50	5.01	1.8	0.773	17.27	0.725	0.049	0.571	0.203
	21 :00	4.78	1.6	0.816	17.37	0.683	0.133	0.498	0.318
	21 :10	4.54	1.8	0.777	16.44	0.725	0.052	0.571	0.206
	21 :20	5.56	2.0	0.842	17.72	0.764	0.078	0.644	0.198
	21 :30	5.56	2.4	0.927	16.93	0.837	0.090	0.794	0.132
	21 :40	5.42	2.0	0.915	17.50	0.764	0.151	0.644	0.271
	21 :50	5.39	2.1	0.901	17.24	0.783	0.118	0.681	0.220
22	22 :00	5.83	2.2	0.935	17.72	0.801	0.134	0.719	0.216
	22 :10	4.91	2.2	0.895	16.26	0.801	0.094	0.719	0.176
	22 :20	4.84	1.4	0.813	18.08	0.639	0.173	0.427	0.385
	22 :30	4.40	2.0	0.770	15.77	0.764	0.006	0.644	0.126
	22 :40	6.07	2.3	0.873	17.88	0.819	0.053	0.756	0.116
	22 :50	5.79	2.3	0.988	17.46	0.819	0.169	0.756	0.232
	23 :00	6.57	2.3	1.030	18.60	0.819	0.211	0.756	0.274
	23 :10	6.10	2.3	1.056	17.93	0.819	0.237	0.756	0.300
	23 :20	5.79	2.3	0.991	17.46	0.819	0.172	0.756	0.235
	23 :30	6.17	2.3	0.997	18.03	0.819	0.178	0.756	0.240
	23 :40	5.83	2.3	1.000	17.52	0.819	0.181	0.756	0.244
	23 :50	5.39	2.4	0.935	16.67	0.837	0.098	0.794	0.141
0	0 :00	5.59	2.4	0.915	16.98	0.837	0.078	0.794	0.121
	0 :10	5.25	2.5	0.903	16.29	0.854	0.049	0.832	0.071
	0 :20	5.56	2.5	0.901	16.76	0.854	0.047	0.832	0.068
	0 :30	5.29	2.5	0.904	16.35	0.854	0.050	0.832	0.072
	0 :40	5.62	2.5	0.909	16.85	0.854	0.055	0.832	0.077
	0 :50	5.52	2.5	0.928	16.70	0.854	0.074	0.832	0.096
	1 :00	5.66	2.5	0.932	16.91	0.854	0.078	0.832	0.099
	1 :10	5.69	2.5	0.946	16.96	0.854	0.092	0.832	0.113
	1 :20	5.59	2.6	0.940	16.64	0.871	0.069	0.871	0.069
	1 :30	5.25	2.6	0.903	16.13	0.871	0.033	0.871	0.033
	1 :40	5.76	2.6	0.918	16.89	0.871	0.047	0.871	0.047
	1 :50	6.00	2.7	0.980	17.08	0.887	0.093	0.909	0.071
2	2 :00	5.39	2.7	0.949	16.19	0.887	0.062	0.909	0.040
	2 :10	5.59	2.7	0.915	16.49	0.887	0.028	0.909	0.006
	2 :20	5.62	2.7	0.934	16.53	0.887	0.047	0.909	0.025
	2 :30	5.56	2.7	0.932	16.44	0.887	0.044	0.909	0.022
	2 :40	5.49	2.6	0.921	16.49	0.871	0.050	0.871	0.050
	2 :50	5.32	2.6	0.901	16.24	0.871	0.030	0.871	0.030
	3 :00	5.59	2.7	0.909	16.49	0.887	0.022	0.909	-0.000
	3 :10	5.42	2.7	0.918	16.23	0.887	0.030	0.909	0.008
	3 :20	5.79	2.6	0.934	16.94	0.871	0.063	0.871	0.063
	3 :30	5.12	2.6	0.909	15.93	0.871	0.038	0.871	0.038
	3 :40	6.24	2.7	0.947	17.42	0.887	0.059	0.909	0.037
	3 :50	6.07	2.7	1.026	17.18	0.887	0.138	0.909	0.116
4	4 :00	5.35	2.6	0.952	16.28	0.871	0.081	0.871	0.081
	4 :10	5.10	2.6	0.871	15.90	0.871	0.000	0.871	0.000
	4 :20	5.59	2.6	0.891	16.64	0.871	0.020	0.871	0.020
	4 :30	5.86	2.6	0.954	17.04	0.871	0.083	0.871	0.083
	4 :40	5.32	2.6	0.932	16.24	0.871	0.061	0.871	0.061
	4 :50	5.18	2.7	0.875	15.87	0.887	-0.012	0.909	-0.034
	5 :00	5.08	2.7	0.855	15.72	0.887	-0.032	0.909	-0.054

No. 011
 Area : RANGE PARK, CHAGUANAS
 Date : Jan. 24-25, 1990

$$Q_x = Q_o \times (H_x/H_o)^n$$

--(n = 0.5)-- --(n = 1.15)--
 --(orifice)-- --(crack)--
 < TYPE - A > < TYPE - B >

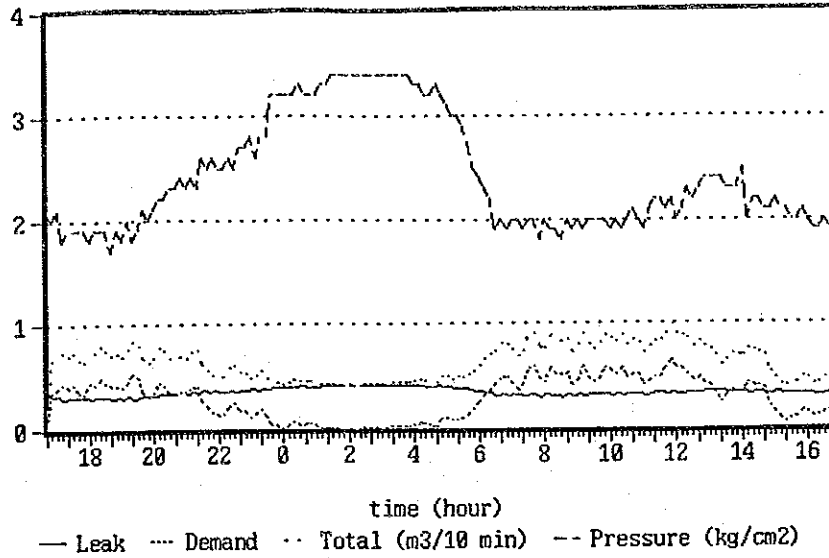
TIME hour min	METERED	METERED	Qtotal m3	Leak hole d(mm)	Leak		Leak	
	Q (m3/h)	PRESSURE (kg/cm2)			QA1(m3)	Demand QA2(m3)	QB1(m3)	Demand QB2(m3)
5 :10	5.12	1.9	0.850	17.23	0.744	0.106	0.607	0.243
5 :20	4.95	2.0	0.839	16.72	0.764	0.075	0.644	0.195
5 :30	5.05	2.2	0.833	16.49	0.801	0.032	0.719	0.115
5 :40	4.78	2.2	0.819	16.05	0.801	0.018	0.719	0.101
5 :50	5.93	2.3	0.893	17.67	0.819	0.073	0.756	0.136
6 :00	5.12	2.3	0.921	16.42	0.819	0.102	0.756	0.165
6 :10	6.61	2.2	0.978	18.87	0.801	0.176	0.719	0.259
6 :20	6.44	1.9	1.088	19.32	0.744	0.343	0.607	0.480
6 :30	5.83	1.8	1.023	18.63	0.725	0.298	0.571	0.452
6 :40	5.16	2.4	0.916	16.31	0.837	0.079	0.794	0.122
6 :50	6.20	1.6	0.947	19.79	0.683	0.264	0.498	0.448
7 :00	4.91	1.4	0.926	18.21	0.639	0.287	0.427	0.499
7 :10	6.61	1.2	0.960	21.96	0.592	0.368	0.358	0.602
7 :20	4.40	1.6	0.918	16.67	0.683	0.234	0.498	0.419
7 :30	4.95	1.4	0.779	18.28	0.639	0.140	0.427	0.352
7 :40	4.27	1.3	0.768	17.30	0.616	0.153	0.392	0.376
7 :50	4.88	1.6	0.763	17.56	0.683	0.079	0.498	0.264
8 :00	3.66	1.4	0.712	15.72	0.639	0.073	0.427	0.284
8 :10	3.12	1.6	0.565	14.04	0.683	-0.118	0.498	0.067
8 :20	3.59	1.6	0.559	15.06	0.683	-0.124	0.498	0.061
8 :30	3.86	1.5	0.621	15.87	0.661	-0.041	0.463	0.158
8 :40	4.37	1.4	0.686	17.18	0.639	0.047	0.427	0.259
8 :50	6.57	1.4	0.912	21.06	0.639	0.273	0.427	0.484
9 :00	3.76	1.4	0.861	15.93	0.639	0.222	0.427	0.434
9 :10	4.91	1.3	0.723	18.55	0.616	0.107	0.392	0.330
9 :20	5.76	1.2	0.889	20.50	0.592	0.298	0.358	0.531
9 :30	4.84	1.4	0.883	18.08	0.639	0.244	0.427	0.456
9 :40	4.17	1.6	0.751	16.23	0.683	0.068	0.498	0.253
9 :50	5.05	1.5	0.768	18.15	0.661	0.107	0.463	0.306
10 :00	5.56	1.5	0.884	19.04	0.661	0.223	0.463	0.422
10 :10	4.95	1.5	0.876	17.97	0.661	0.214	0.463	0.413
10 :20	2.91	1.5	0.655	13.78	0.661	-0.006	0.463	0.192
10 :30	4.84	1.5	0.646	17.77	0.661	-0.016	0.463	0.183
TOTAL			124.708	---	105.783	18.925	87.210	37.498
Average	5.20	1.88	0.866	17.464	84.82%	15.18%	69.93%	30.07%
MAX	7.86	3.00	1.310	26.496	0.935	0.827	1.027	1.085
MIN	2.17	0.80	0.452	12.104	0.483	-0.292	0.225	-0.383

kg/cm2 m3/10 min
 Leakage at Night: 2.60 0.871 15.90 : 4:10 a.m.
 Estimated night demand : 0.000

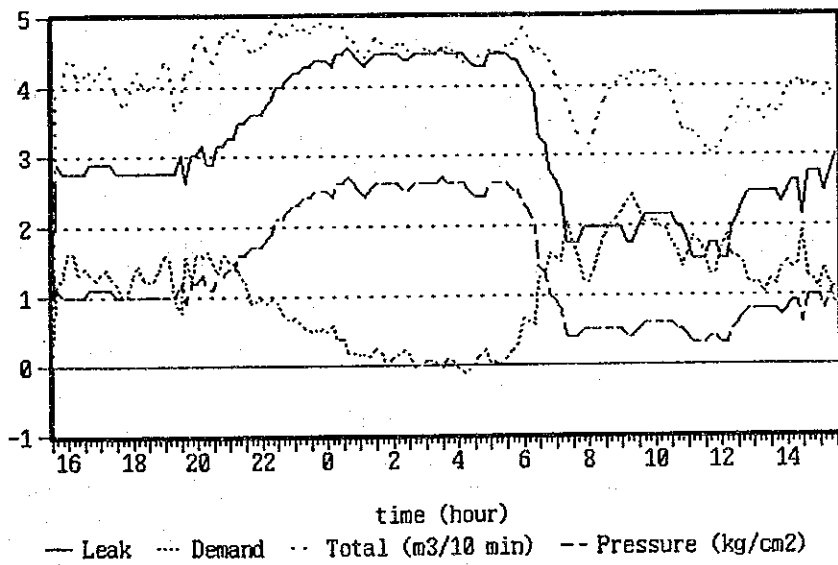
Nos. of house [A] 79 houses
 persons/house [B] 3.8 pesons/house
 A * B [C] 300.2 persons

< TYPE - A > < TYPE - B >
 Water Demand [D] 18.93 M3 37.50 M3
 l/day/capita D/C 63.04 l/d/c 124.91 l/d/c

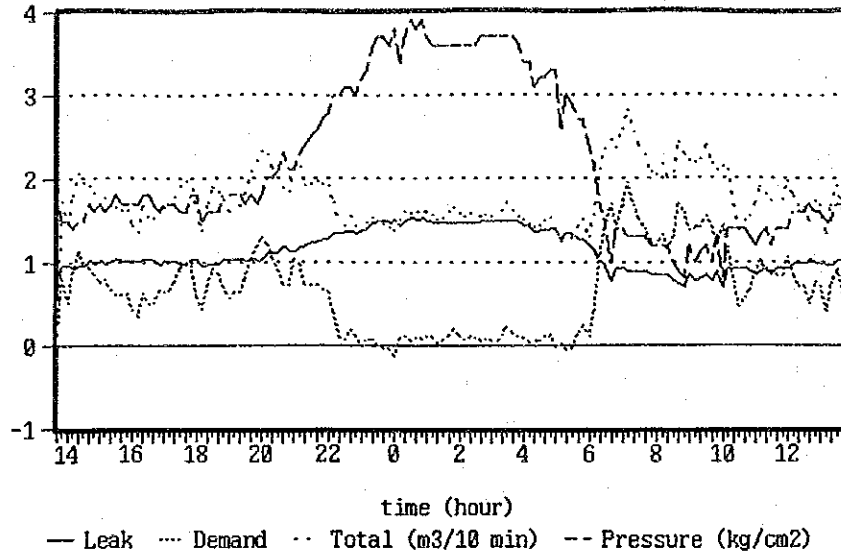
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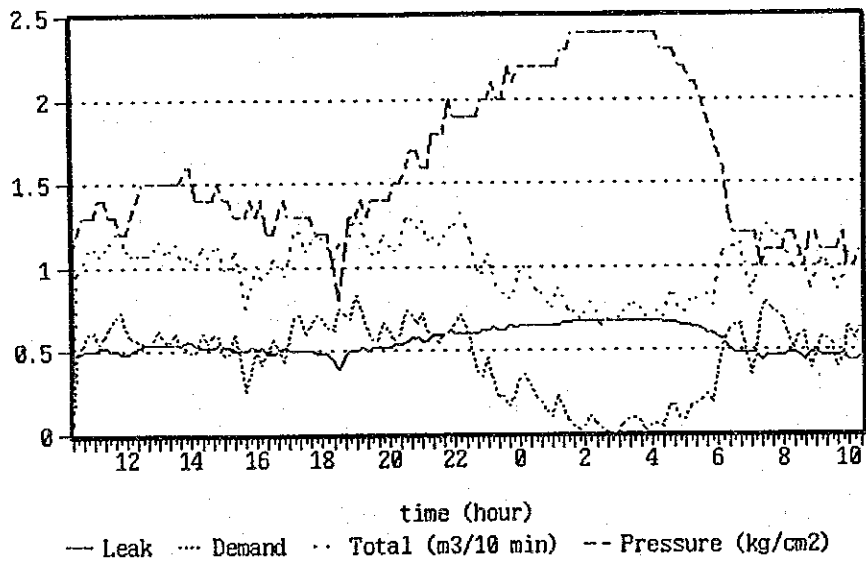
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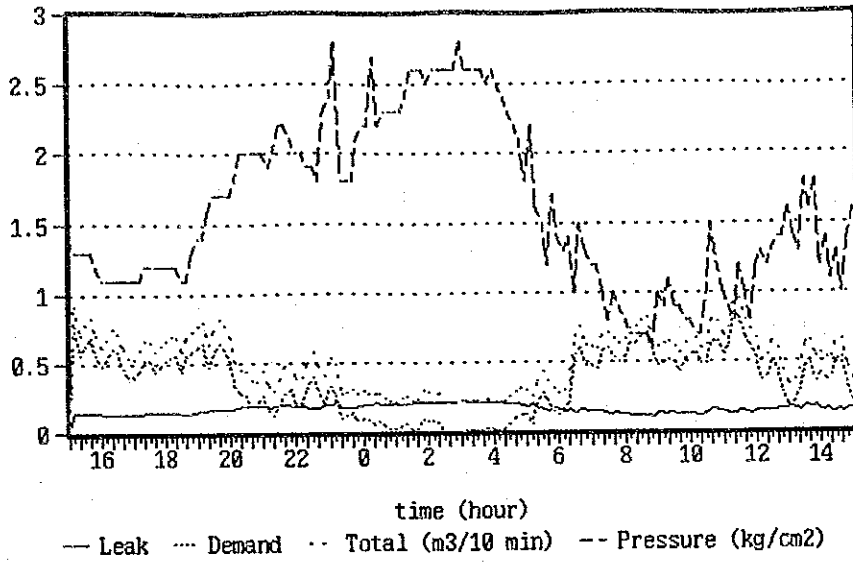
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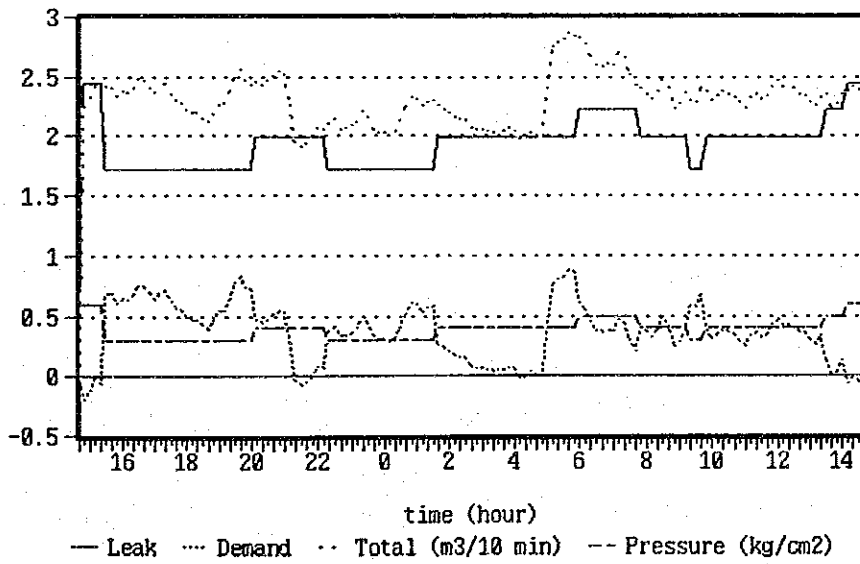
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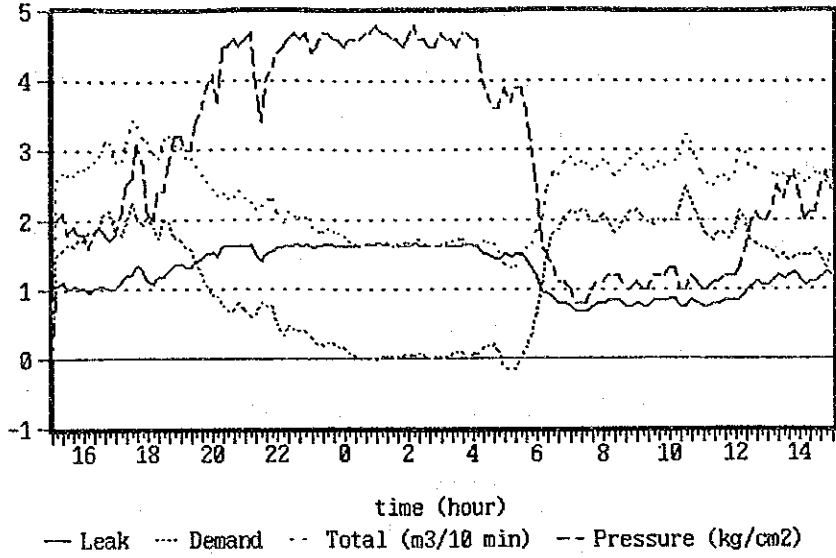
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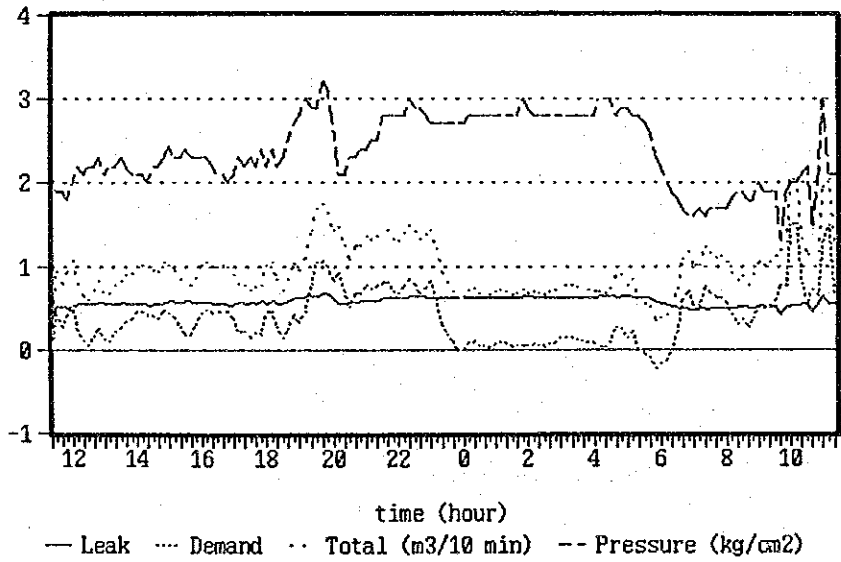
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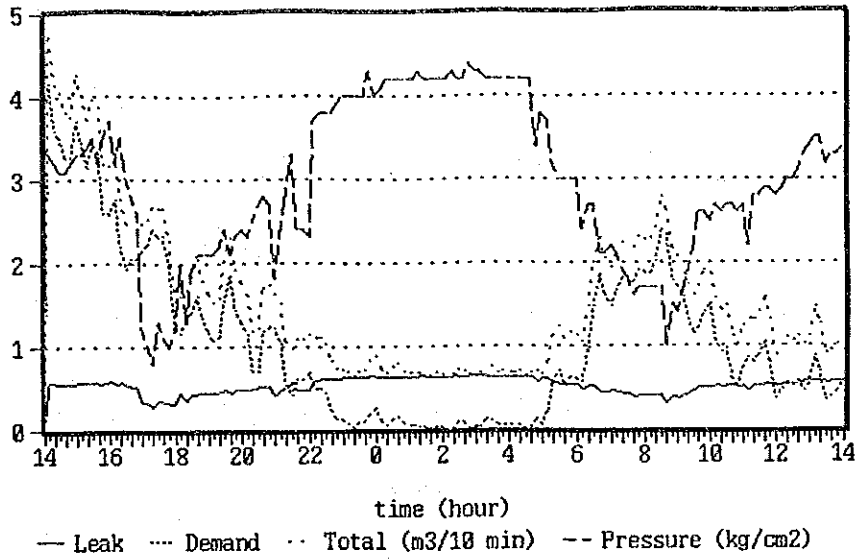
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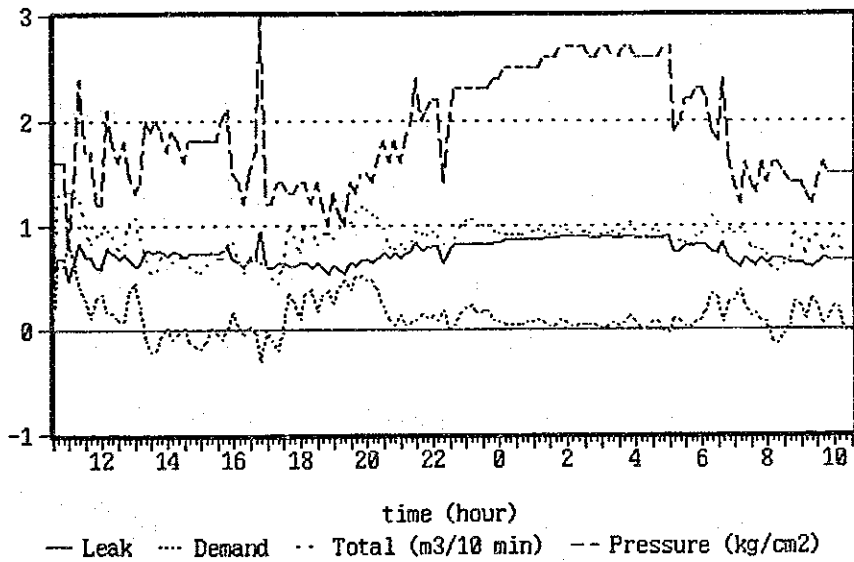
No. 008



No. 009



No. 011



I: EXISTING WATER SUPPLY FACILITIES

Table 3.3.1 WATER SUPPLY FACILITIES IN THE DISTRICT OF NORTH CENTRAL

WASA CODE	NO. REGION FACI	NAMES OF FACILITIES	PRODUCT. CAPACITY RAINY (m3/day)	PRODUCT. CAPACITY DRY (m3/day)	STORAGE CAPACITY (m3)	(I.G.)	H.W.L (m)	(TGL f)	(MSL f)	(m)	(TGL f)	(MSL f)	L.W.L (m)	(TGL f)	(MSL f)	** COORDINATES *** to EAST to NORTH
[A] PRODUCTION FACILITIES																
1	N/Cent WELL	Arouca (Well)	553	653												683.000 75.000
2	N/Cent W.W	Caroni	272,760	272,760												681.165 70.920
3	N/Cent W.W	Caura	11,360	9,310												678.090 78.755
4	N/Cent W.W	Las Lomas (Well)	11,360	11,360												686.065 67.950
5	N/Cent W.W	Loango/Naranjo	3,180	2,500												672.975 84.300
6	N/Cent W.W	Tacarigua (Well)	14,550	14,550												679.100 76.785
		Tacarigua Well # 2														
		Tacarigua Well # 3														
		Tacarigua Well # 4														
		Tacarigua Well # 5														
		Tacarigua Well # 6														
		Tacarigua Well # 8														
		Tacarigua Well # 9														
		Tacarigua Well #10														
		Tacarigua Well #11														
		Tacarigua Well #13														
		Tacarigua Well #14														
7	N/Cent W.W	Valsayn (Well)	27,280	27,280												673.310 77.013
8	N/Cent INT	Loango	59	59												682.825 85.500
9	N/Cent INT	Lepinot	35	35												671.500 79.500
10	N/Cent INT	Mt. D'or	88	88												686.200 79.800
11	N/Cent INT	St John's Road	454	454												681.560 79.600
12	N/Cent INT	Surrey Village	18	18												
13	N/Cent INT	Waterfall Rd-Intake	59	59												
TOTAL			341,856	339,126												
[B] TRANSMISSION/DISTRIBUTION FACILITIES																
1	N/Cent STO	Caura Hospital			164	36,000	143.82	471.86	471.86	141.51	464.26	464.26				677.875 78.500
2	N/Cent STO	Las Lomas			246	54,000	85.61	280.87	280.87	82.09	269.34	269.34				685.460 65.196
3	N/Cent STO	Mt. Hope			22,750	5,000,000	91.52			82.91						671.526 78.411
4	N/Cent STO	Santa Margarita			91	20,000	159.17	522.20	522.20	156.67	514.00	514.00				674.695 78.525
5	N/Cent STO	St Augustine			16,835	3,700,000	140.21	460.00	460.00	134.11	440.00	440.00				674.165 78.630
6	N/Cent STO	St Johns			91	20,000	145.50	477.35	477.35	143.05	469.31	469.31				675.700 79.085
7	N/Cent STO	St Joseph			13,650	3,000,000	108.20	355.00	355.00	103.63	340.00	340.00				673.053 78.477
8	N/Cent STO	Valley View			1,024	225,000	***	***	***	***	***	***				673.400 81.250
TOTAL					54,851	12,055,000										
1	N/Cent BPS	Caura Royal Road														678.270 77.755
2	N/Cent BPS	Gordon Street														674.800 77.800
3	N/Cent BPS	Irving Street														670.450 77.715
4	N/Cent BPS	Mendes Drive														672.230 77.570
5	N/Cent BPS	Tunapuna														675.500 76.750

Table 3.3.2 WATER SUPPLY FACILITIES IN THE DISTRICT OF NORTH EAST (1)

NO.	WASA REGION FACI CODE	NAMES OF FACILITIES	PRODUCT. CAPACITY		STORAGE CAPACITY (m ³)	H.W.L.		L.W.L.		** COORDINATES to EAST to NORTH	
			RAINY (m ³ /day)	DRY (m ³ /day)		(m) (TGL f)	(MSL f)	(m) (TGL f)	(MSL f)		
[A] PRODUCTION FACILITIES											
1	N/E	W.W Aripo (New)	9,030	8,490						693.600 78.715	
2	N/E	W.W Guanapo	6,880	6,880						690.920 78.635	
3	N/E	W.W Hollis	31,826	31,826						697.725 82.725	
4	N/E	W.W North Oropuche	49,125	44,825						702.963 79.850	
5	N/E	W.W Toco	2,400	1,740						723.250 92.600	
6	N/E	WELL Arima #6	644	644						687.050 76.600	
7	N/E	INT Aripo	35	35						692.000 86.450	
8	N/E	INT Brasso Seco Paria	27	27						720.450 83.450	
9	N/E	INT Cumaca	45	45						710.155 57.500	
10	N/E	INT Four Roads Tamana	70	70						713.925 97.500	
11	N/E	INT Grande Riviere	35	35						701.100 62.300	
12	N/E	INT Los Armadillos	105	105						707.200 96.400	
13	N/E	INT Matelot	35	35						710.500 80.650	
14	N/E	INT Matura	35	35						715.475 97.000	
15	N/E	INT Montevideo	35	35						687.053 86.100	
16	N/E	INT Morne La Croix	27	27						697.240 79.650 *	
17	N/E	INT Quare (Rd.) (Valencia	2,935	2,935						714.450 83.120	
18	N/E	INT Salibea	35	35						722.100 97.300	
19	N/E	INT Sans Souci	493	493							
TOTAL			103,817	98,317							
[B] TRANSMISSION/DISTRIBUTION FACILITIES											
1	N/E	STO Arima New			2,275	500,000	133.86	439.25	133.84	439.10	687.362 77.175
2	N/E	STO Arima Old			819	180,000	130.15	427.00	127.10	417.00	687.643 77.265
3	N/E	STO Calvary Hill		(not in use)	455	100,000	198.27	650.50	193.82	635.90	687.280 77.510
4	N/E	STO Cleaver Road			1,024	225,000	127.71	419.00	118.57	389.00	688.150 76.750
5	N/E	STO Comparo			159	35,000	***	***	***	***	710.764 65.252
6	N/E	STO Cumana			91	20,000	82.07	269.27	79.26	260.03	724.252 93.641
7	N/E	STO Fort Read			7,599	1,670,000	147.52	484.00	124.55	408.63	693.692 77.812
8	N/E	STO Guaico			2,275	500,000	76.60	251.31	65.93	216.31	701.900 70.400
9	N/E	STO Malabar			1,820	400,000	91.59	300.50	86.61	284.14	688.141 79.949
10	N/E	STO Nestor		(not in use)	23	5,000	87.64	287.52	85.93	281.93	703.928 65.872
11	N/E	STO North Oropuche			45,500	0	***	***	126.49	***	702.963 79.500
12	N/E	STO O'Meara		(not in use)	27	6,000	79.46	260.70	78.09	256.20	687.224 75.508
13	N/E	STO Sangre Grande			382	84,000	61.83	202.85	58.93	193.35	705.900 69.383
14	N/E	STO Talparo			182	40,000	76.20	250.00	73.15	240.00	689.430 62.212
15	N/E	STO Tamana Hill Road		(not in use)	91	20,000	***	***	***	***	698.864 62.226
16	N/E	STO Toco		(not in use)	455	100,000	132.22	433.80	129.33	424.30	724.800 96.300
TOTAL					63,177	3,885,000					
1	N/E	BPS Arima									687.990 75.450
2	N/E	BPS Aripo									694.100 76.950
3	N/E	BPS C&Igal									707.753 68.100

Table 3.3.2 WATER SUPPLY FACILITIES IN THE DISTRICT OF NORTH EAST (2)

NO.	REGION	FACI	NAMES OF FACILITIES	PRODUCT. CAPACITY RAINY DRY	STORAGE CAPACITY (m ³) (I.G)	H.W.L. (m) (TGL f) (MSL f)	L.W.L. (m) (TGL f) (MSL f)	** COORDINATES **** to EAST to NORTH
4	N/E	BPS	Calvary Hill	(not in use)				687.750 78.700 *
5	N/E	BPS	Caparo					681.412 58.696
6	N/E	BPS	Guaico					702.454 70.525
7	N/E	BPS	Quare					597.800 79.260

Table 3.3.3 WATER SUPPLY FACILITIES IN THE DISTRICT OF NORTH WEST (1)

WASA NO. REGION FACI	CODE FACI	NAMES OF FACILITIES	PRODUCT. CAPACITY RAINY (m3/day)	CAPACITY DRY (m3/day)	STORAGE CAPACITY (m3)	H.W.L (m) (TGL f)	L.W.L (m) (TGL f)	(MSL f)	(MSL f)	** COORDINATES *** to EAST to NORTH
[A] PRODUCTION FACILITIES										
1 N/W	W.W	Acono	2,100	1,560				674.950	83.545	
2 N/W	W.W	Dorington Gardens	5,400	5,400				658.320	84.435	
3 N/W	W.W	El Socorro (Well)	24,126	24,126				669.250	75.200 ?	
4 N/W	W.W	Four Roads (Well)	28,900	28,900				575.750	81.750 *	
		Four Roads D/M # 9								
		Four Roads D/M #11								
		Four Roads D/M #12								
		Four Roads D/M #10								
		Four Roads D/M #14								
		Four Roads D/M #15								
5 N/W	W.W	River Estate (Well)	6,820	6,820				657.814	83.820	
		River Estate Well #2						657.860	84.990	
		River Estate Well #3						657.370	86.390	
		River Estate Well #4								
		River Estate Well #5								
		River Estate Well #6								
		River Estate Well #7								
		River Estate Well #8								
6 N/W	WELL	La Pastora Wells	2,900	2,900				667.333	84.863 ?	
		La Pastora Well #1						666.917	86.045 ?	
		La Pastora Well #2								
		La Pastora Well #3								
		La Pastora Well #4								
7 N/W	WELL	Tucker Valley Wells	13,640	13,640				651.816	82.502	
		Tucker Valley # 4						652.074	83.122	
		Tucker Valley # 6A						651.539	83.014	
		Tucker Valley # 7						651.201	85.673	
		Tucker Valley #10						651.475	86.061	
		Tucker Valley #13								
		Tucker Valley #15								
		Tucker Valley #16A								
		Tucker Valley #17								
		Tucker Valley #25								
		Chaguaramas #30								
		Chaguaramas #32								
8 N/W	INT	Blanchisseuse	44	44				684.500	93.350	
9 N/W	INT	Covigne	358	358				655.500	85.750	
10 N/W	INT	Damier	200	200				680.600	93.900	
11 N/W	INT	La Canoa	94	94				670.600	85.250	
12 N/W	INT	La Pastora Res. Road	88	88				667.750	87.250	
13 N/W	INT	La Pastora/Capriata	266	266				667.000	87.600	
14 N/W	INT	Las Cuevas	45	45				675.150	91.000	
15 N/W	INT	Mon Repos	90	90				666.750	79.750	
16 N/W	INT	Pipiol	305	305				665.850	83.550	
17 N/W	INT	Tyrico	305	305				671.750	89.100	

Table 3.3.3 WATER SUPPLY FACILITIES IN THE DISTRICT OF NORTH WEST (2)

WASA CODE	NO. REGION FACI	NAMES OF FACILITIES	PRODUCT. CAPACITY RAINY DRY	STORAGE CAPACITY (m3)	(I.G)	(m) (TGL f) (MSL f)	(m) (TGL f) (MSL f)	(m) (TGL f) (MSL f)	L.W.L (TGL f) (MSL f)	** COORDINATES ** to EAST to NORTH			
		TOTAL	85,376	84,836									
[B]		TRANSMISSION/DISTRIBUTION FACILITIES											
1 N/W	STO	Alcoea	(not in use)	500	109,890	90.22	296.00	296.00	85.65	281.00	281.00	653.125	81.380
2 N/W	STO	Carenage	(not in use)	910	200,000	90.22	296.00	296.00	85.65	281.00	281.00	653.325	81.500 ?
3 N/W	STO	Chagnaramas (U)		1,138	250,000	***	***	***	***	***	***	651.548	86.740
4 N/W	STO	Covigne		9,109	2,000,000	125.58	412.00	412.00	118.87	390.00	390.00	656.100	85.860
5 N/W	STO	Dundonald Hill		182	40,000	154.84	507.99	507.99	151.63	497.49	497.49	660.130	81.250
6 N/W	STO	La Pastora	(not in use)	910	200,000	158.80	521.00	521.00	***	***	***	668.400	85.600 ?
7 N/W	STO	Mallick		22,700	5,000,000	54.41	-	-	47.24	-	-	668.339	78.475
8 N/W	STO	Morvant		1,820	400,000	108.20	355.00	355.00	103.63	340.00	340.00	666.562	79.208
9 N/W	STO	Point Cumena	(not in use)	2,275	500,000	116.43	382.00	382.00	111.86	367.00	367.00	656.335	81.250
10 N/W	STO	Richplain	(not in use)	27	6,000	154.68	507.48	507.48	152.96	501.84	501.84	656.140	84.540
11 N/W	STO	River Estate	(not in use)	700	0	***	***	***	***	***	***	658.100	87.700
12 N/W	STO	Tyrice	(not in use)	37	8,100	***	***	***	***	***	***	671.250	89.250
		TOTAL		40,299	8,713,990								
[C]		PRODUCT. CAPACITY RAINY DRY											
1 N/W	HLPS	Morvant										666.562	79.208
2 N/W	HLPS	Tucker Valley										652.200	82.650
3 N/W	BPS	83 Rd										647.000	80.900
4 N/W	BPS	Carenage										654.250	81.250
5 N/W	BPS	Covigne										656.560	85.250
6 N/W	BPS	Harts Cut										649.750	80.925
7 N/W	BPS	Hutton Road No.1										662.920	81.075 *
8 N/W	BPS	La Canoa Road										669.220	80.470
9 N/W	BPS	Lady Young										666.550	79.140
10 N/W	BPS	Pichplain										656.800	84.525
11 N/W	BPS	Quarry Road										669.770	78.315
12 N/W	BPS	Ross Lands										659.655	80.780
13 N/W	BPS	Simeon Road										658.315	82.805

Table 3.3.4 WATER SUPPLY FACILITIES IN THE DISTRICT OF PORT OF SPAIN (1)

NO. REGION FACI	WASA CODE	NAMES OF FACILITIES	PRODUCT. CAPACITY		STORAGE CAPACITY (m3)	H.W.L.		L.W.L.		** COORDINATES to EAST to NORTH
			RAINY (m3/day)	DRY (m3/day)		(m) (TGL f)	(MSL f)	(m) (TGL f)	(MSL f)	
[A] PRODUCTION FACILITIES										
1	P.O.S. W.W	Maraval	5,910	4,770						662.375 83.000
2	P.O.S. W.W	Paramin	390	390						662.450 84.400
3	P.O.S. W.W	St. Anns	840	840						663.425 81.175
4	P.O.S. WELL	KingGeorgev Park #2 KingGeorgev Park #3 KingGeorgev Park #4	10,340	10,340						661.247 79.653 661.874 79.533 ? 660.872 79.635
5	P.O.S. WELL	Moka Wells	1,590	1,590						663.349 84.629 663.687 84.902
6	P.O.S. WELL	Savannah Wells	12,270	12,270						662.528 79.092 662.521 79.596 661.874 79.521 662.136 79.341 662.141 79.116 662.338 79.079
7	P.O.S. WELL	St Clair	1,820	1,820						
8	P.O.S. INT	Ariapita	138	138						
9	P.O.S. INT	Cascade	207	207						
10	P.O.S. INT	Dibe	145	145						
TOTAL			33,650	32,510						660.200 83.425
[B] TRANSMISSION/DISTRIBUTION FACILITIES										
1	P.O.S. STO	Ariapita	91	91	20,000	268.25	880.09	264.72	868.50	665.030 81.860
2	P.O.S. STO	Cascade	341	341	75,000	114.30	375.00	111.25	365.00	664.475 80.800
3	P.O.S. STO	Gonzales	46	46	10,000	***	***	***	***	664.330 78.690
4	P.O.S. STO	Hololo	1,138	1,138	250,000	199.26	653.75	193.17	633.75	664.075 81.100
5	P.O.S. STO	Knaggs Hill	27,300	27,300	3,090,000	99.46	326.32	92.96	305.00	661.905 80.450
6	P.O.S. STO	Laventille	5,915	5,915	1,900,000	87.01	285.45	83.35	273.45	663.830 77.650
7	P.O.S. STO	Maraval	3,346	3,346	735,366	81.43	267.16	78.08	256.16	661.600 83.250
8	P.O.S. STO	Mc Shine	546	546	120,000	127.86	419.49	124.71	409.14	663.909 78.195
9	P.O.S. STO	Paramin	?	?	?	***	***	***	***	662.300 86.900
10	P.O.S. STO	Picton No.1	13,650	13,650	3,000,000	137.77	452.00	131.06	430.00	664.253 77.900
11	P.O.S. STO	Picton No.2	22,750	22,750	5,000,000	99.36	326.00	90.53	297.00	664.100 77.500
12	P.O.S. STO	Picton No.3	45,500	45,500	10,000,000	124.03	406.92	113.36	371.90	664.383 77.733
13	P.O.S. STO	Red Hill	900	900	900	152.73	406.92	149.38	406.92	665.580 78.955
14	P.O.S. STO	St Barbs	1,024	1,024	235,000	235.38	739.43	222.64	730.43	664.871 78.800
TOTAL			122,547	122,547	23,825,366					657.675 80.870
1	P.O.S. HLPS	Farrell	(not in use)	(not in use)						

Table 3.3.4 WATER SUPPLY FACILITIES IN THE DISTRICT OF PORT OF SPAIN (2)

NO.	REGION	FACI	NAMES OF FACILITIES	PRODUCT. CAPACITY RAINY	DRY	STORAGE CAPACITY (m3)	(I.G)	H.W.L (m) (TGL f)	(MSL f)	L.W.L (m) (TGL f)	(MSL f)	** COORDINATES ***** to EAST to NORTH
2	P.O.S.	HLPS	Paramin No.2									662.100 84.800
3	P.O.S.	HLPS	Paramin No.3									661.800 85.250
4	P.O.S.	HLPS	Paramin No.4									661.950 86.100
5	P.O.S.	BPS	Brievess Road									660.915 81.020
6	P.O.S.	BPS	Foncette Road									663.990 80.725
7	P.O.S.	BPS	Gonzales									663.885 78.700
8	P.O.S.	BPS	Hutton Road No.2									662.595 81.075
9	P.O.S.	BPS	Knages Hill									661.930 80.435 ?
10	P.O.S.	BPS	Second Avenue									663.430 80.315

Table 3.3.5 WATER SUPPLY FACILITIES IN THE DISTRICT OF SAN FERNAND/SOUTH CENTRAL

WASA CODE	REGION FACI NAMES OF FACILITIES	PRODUCT. CAPACITY RAINY DRY	STORAGE CAPACITY (m3)	(I.G)	(m)	(TGL f)	(MSL f)	(m)	(TGL f)	(MSL f)	COORDINATES ***
		(m3/day)									to EAST to NORTH
[A]	PRODUCTION FACILITIES										
1	S/C W.W Carlsen Field	11,175									575.240 59.740 *
2	S/C W.W Carlsen Field Well #5	11,175									677.783 60.800
3	S/C W.W Freeport	6,165	6,165								672.636 53.780
	TOTAL	11,175	11,175								
[B]	TRANSMISSION/DISTRIBUTION FACILITIES										
1	S/C STO Basta Hall		3,413	750,000	122.22	401.00	401.00	117.65	386.00	386.00	670.950 49.320
2	S/C STO California		22,750	5,000,000	59.84	-	-	49.38	-	-	670.985 48.105
3	S/C STO Chacon Street		7,280	1,600,000	77.72	255.00	255.00	73.15	240.00	240.00	688.355 36.900
4	S/C STO Freeport		4,550	1,000,000	115.82	380.00	380.00	111.25	365.00	365.00	678.784 56.372
5	S/C STO Marryat Street	(not in use)	13,423	2,950,000	108.81	357.00	357.00	104.39	342.50	342.50	668.840 36.555
6	S/C STO Naparima		9,100	2,000,000	103.63	340.00	340.00	99.06	325.00	325.00	668.850 36.550
7	S/C STO Pepper Village		1,820	400,000	229.97	754.50	754.50	***	-	-	678.992 49.604
8	S/C STO San Fernando		22,750	5,000,000	51.97	-	-	44.20	-	-	669.209 48.105
9	S/C STO Springlands	(not in use)	?	?	***	-	-	***	-	-	672.570 41.700
	TOTAL		85,086	18,700,000							
1	S/C BPS California										668.270 50.240
2	S/C BPS Marryat Street										668.900 36.525
3	S/C BPS San Fernando										669.247 36.855
4	S/C BPS Gran Couva										
5	S/C BPS Springland										

Table 3.3.6 WATER SUPPLY FACILITIES IN DISTRICT OF SOUTH EAST

WASA REGION	CODE	NAMES OF FACILITIES	PRODUCT. CAPACITY RAINY (m3/day)	PRODUCT. CAPACITY DRY (m3/day)	STORAGE CAPACITY (m3)	(I.G)	H.W.L (m)	(TGL f)	(MSL f)	(m)	(TGL f)	(MSL f)	COORDINATES to EAST to NORTH
[A] PRODUCTION FACILITIES													
1	S/E	W.W Biche	259	259									703.000 53.450
2	S/E	W.W Navet	77,280	77,280									691.235 50.189
3	S/E	WELL Guayaguayare #1	897	897									717.800 31.700
4	S/E	WELL Maloney	1,358	1,358									
5	S/E	WELL Mayaro	792	792									
6	S/E	WELL Tournebride Wells	1,194	1,194									
		Tournebride #1											
		Tournebride #2											
7	S/E	SPR Guaracara	1,136	1,136									718.000 30.280
8	S/E	SPR Mayo	630	630									717.700 30.250
9	S/E	SPR Morichal	718	718									680.750 46.700
		TOTAL	84,264	84,264									680.000 45.250
[B] TRANSMISSION/DISTRIBUTION FACILITIES													
1	S/E	STO Devenish Hill			228	50,000	183.18	601.00	601.00	***			683.628 49.080
2	S/E	STO Dunmore Hill			2,275	500,000	154.23	506.00	506.00	143.26	470.00	470.00	682.628 35.644
3	S/E	STO Guaracara			1,392	306,000	136.70	448.50	448.50	133.58	438.25	438.25	680.700 46.032
4	S/E	STO Guayaguayare			82	18,000	***	***	***	***	***	***	713.550 21.250
5	S/E	STO Kelly Village			1,138	250,000	199.26	653.75	653.75	***	***	***	679.080 42.300
6	S/E	STO La Lune			91	20,000	59.34	194.67	194.67	56.54	185.51	185.51	682.636 14.500
7	S/E	STO Maloney			1,024	225,000	66.90	219.50	219.50	59.59	195.50	195.50	718.122 33.012
8	S/E	STO Marac		(not in use)	82	18,000	58.56	192.13	192.13	56.45	185.19	185.19	680.708 14.492
9	S/E	STO Mayaro		(not in use)	364	80,000	66.75	219.00	219.00	62.79	206.00	206.00	717.525 38.500
10	S/E	STO Mayo			91	20,000	132.10	433.40	433.40	128.90	422.90	422.90	677.720 45.360
11	S/E	STO Morichal			159	35,000	113.39	372.00	372.00	110.34	362.00	362.00	679.316 45.284
12	S/E	STO Ortoire Hill Road			91	20,000	49.80	163.39	163.39	47.34	155.33	155.33	719.200 41.850
		TOTAL			7,017	1,542,000							
[C] TRANSMISSION/DISTRIBUTION FACILITIES													
1	S/E	BPS Guayaguayare											718.750 25.050
2	S/E	BPS Malgretoute											676.900 36.650
3	S/E	BPS Maloney											718.352 32.950
4	S/E	BPS St Julien (Post Office Trace)											682.584 36.560
5	S/E	BPS St Marys											684.680 26.780
6	S/E	BPS Tebaquite											688.000 47.000
7	S/E	BPS T.C.O.											
8	S/E	BPS Biche											687.300 45.700
9	S/E	BPS Whiteland											
10	S/E	BPS Bermont											

Table 3.3.7 WATER SUPPLY FACILITIES IN DISTRICT OF SOUTH WEST

ORG. NO.	WASA CODE	REGION FACI NAMES OF FACILITIES	PRODUCT. CAPACITY RAINY (m3/day)	PRODUCT. CAPACITY DRY (m3/day)	STORAGE CAPACITY (m3)	(I.G)	(m)	H.W.L (TGL f) (MSL f)	(m)	L.W.L (TGL f) (MSL f)	** COORDINATES ** to EAST to NORTH
[A] PRODUCTION FACILITIES											
260	1 S/W	buy Trintoc to Pt. Fortin	69	69							
260	2 S/W	buy Trintoc to Techier	155	155							
239	3 S/W	buy Texaco to Guayaguayare	180	180							
241	4 S/W	W.W Cap De Ville (Well)	1,006	1,006							642.975 19.525
242	5 S/W	W.W Carepal (Well)	1,400	1,400							648.676 14.964
246	6 S/W	W.W Chatham (Well)	4,385	4,385							640.250 20.000
246	7 S/W	W.W Fyzabad (Well)	1,500	1,500							659.000 25.750
248	8 S/W	W.W Granville (Well) to Cap De Ville to Cedros to Granville Tank	2,800	2,800							631.450 19.800
256	9 S/W	W.W Penal (Well)	3,500	3,500							656.685 22.500
260	10 S/W	W.W Point Fortin (Well)	980	980							647.600 25.392
243	11 S/W	W.W Siparia (Coora) (Well)	3,033	3,033							663.975 20.000
243	12 S/W	WELL Clarke Road #4 & #5	623	623							
TOTAL 19,631 19,631											
[B] TRANSMISSION/DISTRIBUTION FACILITIES											
236	1 S/W	STO Bennett Village	(not in use)		296	?	?	?	?	?	?
238	2 S/W	STO Buenos Ayres	(not in use)		910						
240	3 S/W	STO Cap De Ville			1,820						
243	4 S/W	STO Clarke Road			1,820						
247	5 S/W	STO Gonzales Street	(not in use)		455						
249	6 S/W	STO Granville	(not in use)		2,730						
252	7 S/W	STO K.T.O.			91						
253	8 S/W	STO Los Gallos	(not in use)		23						
254	9 S/W	STO New Village	(not in use)		319						
257	10 S/W	STO Penal	(not in use)		91						
258	11 S/W	STO Penal Rock Road No.1	(not in use)		910						
259	12 S/W	STO Penal Rock Road No.2	(not in use)		432						
261	13 S/W	STO Siparia No.1	(not in use)		9,897						
TOTAL 2,175,000											
237	1 S/W	BPS Boodoosingh									653.490 30.620
255	2 S/W	BPS Oropouche									650.000 30.700
262	3 S/W	BPS **Benett Village									
263	4 S/W	BPS **Clark Road									

Table 3.3.8 WATER SUPPLY FACILITIES IN DISTRICT OF TOBAGO

WASA NO. REGION FACI	CODE NAMES OF FACILITIES	PRODUCT. CAPACITY		STORAGE CAPACITY (m3)	H.W.L.		L.W.L.		COORDINATES to EAST to NORTH	
		RAINY (m3/day)	DRY (m3/day)		(m)	(TGL f)	(m)	(TGL f)		(MSL f)
(A) PRODUCTION FACILITIES										
1	TOBAGO INT Parlaturier	70	70						743.350	40.250
2	TOBAGO W.W Courland	7,368	7,368						753.950	41.450
3	TOBAGO W.W Hillsborough	8,582	8,582						767.400	48.900
4	TOBAGO W.W Kings Bay	2,994	2,994						760.900	41.700
5	TOBAGO W.W Richmond	2,467	2,467						745.550	36.600
6	TOBAGO WEL Government Farm #3	335	335						760.600	48.250
7	TOBAGO INT Bloody Bay	24	24						752.300	47.800
8	TOBAGO INT Castara	80	80						766.600	51.700
9	TOBAGO INT Charlotteville	388	388						748.800	42.200
10	TOBAGO INT Craig Hall	2,461	2,461						754.000	40.200
11	TOBAGO INT Green Hill	3,360	3,360						762.650	51.400
12	TOBAGO INT L'Anse Fourmi	34	34						767.850	49.200
13	TOBAGO INT Speyside	86	86							
14	TOBAGO INT Hillsborough West River	3,150	3,150							
	TOTAL	31,399	31,399							
(B) TRANSMISSION/DISTRIBUTION FACILITIES										
1	TOBAGO STO Bad Hill			1,024	225,000	****	****	****	744.600	40.250
2	TOBAGO STO Castara			23	5,000	****	****	****	752.000	47.550
3	TOBAGO STO Charlotteville			168	37,000	****	****	****	765.250	50.950
4	TOBAGO STO Fort George			1,456	320,000	149.96	492.00	482.00	748.150	36.850
5	TOBAGO STO Green Hill			2,275	500,000	****	****	****	753.850	40.250
6	TOBAGO STO Hospital			202	44,500	****	****	****	748.050	36.350
7	TOBAGO STO Les Coteaux			9	1,875	124.97	410.00	405.00	746.350	42.300
8	TOBAGO STO Mason Hall			228	50,000	227.99	748.00	194.79	749.150	41.000
9	TOBAGO STO Moriah			455	100,000	361.19	1185.00	327.99	750.250	44.750
10	TOBAGO STO Parlaturier			?	?	?	?	?	757.000	49.250
11	TOBAGO STO Patience Hill			46	10,000	190.27	624.25	187.83	743.850	37.950
12	TOBAGO STO Toco Hill			?	?	?	?	?	761.300	43.625
13	TOBAGO STO Whim Hill			159	35,000	179.22	588.00	146.63	746.150	39.550
14	TOBAGO STO Zion Hill			1,138	250,000	****	****	****	761.100	42.950
15	TOBAGO STO Signal Hill			2,275	500,000	115.88	380.00	103.63		
	TOTAL			9,458	2,078,375					
(C) BPS FACILITIES										
1	TOBAGO BPS Highlands Road								748.850	42.900
2	TOBAGO BPS Zion Hill								761.800	43.000
3	TOBAGO BPS Mt. Gomery									
4	TOBAGO BPS King Peter									

J: FIELD FLOW MEASUREMETN OF TRANSMISSION/DISTRIBUTION MAINS

J: FIELD FLOW MEASUREMENT OF TRANSMISSION/DISTRIBUTION MAINS

C O N T E N T S

	Page
1. General	J- 1
2. Survey Method	J- 1
3. Selection of Survey Points	J- 1
4. Outline of Survey Results	J- 2

J FIELD FLOW MEASUREMENT ON TRANSMISSION/DISTRIBUTION MAINS

1. General

Continuous 24-hour flow measurement was carried out to examine flow conditions in the transmission/distribution mains including water flow rate, water pressure, leakage and conveyance capability of the mains.

In the course of the flow measurement, the measurement team organized for this purpose has faced numerous difficulties. The results obtained from this measurement are not necessarily desirable one. Some are not accurate. All results as presented herein, however, may suggest some facets of the existing water supply conditions.

2. Survey Method

In due consideration of the survey objectives and accuracy of the survey equipment, survey method was formulated as follows:

Flow measurement is at 10 minute intervals for continuous 24 hours and a method of simultaneous two-point measurement at a distance of minimum 1 km on the same main installing ultra-sonic flow meters. Pressure measurement is continuous 24 hours at the same points. The measurement team is organized from WASA's engineers and staff to conduct the survey under supervision of the Study Team.

On the other hand, level survey is conducted under responsibility of WASA to obtain distance and differentials of ground level between two points.

3. Selection of Survey Points

Prior to the measurement survey, the Study Team conducted a preliminary survey to select 8 survey points. Selection was made from the following view-points:

- 1) Transmission/distribution mains principally from the four large scale waterworks, i.e., Caroni, North Oropouche, Navet and Hollis in order to obtain flow capability of mains severally which might be installed under different projects and methods.
- 2) Mains installed on the ground where measurement can be easily conducted and pipe excavation is not required, to save time as much as possible.
- 3) Mains which have less offtakes due to a limited number of the flow meters.
- 4) Straight pipelines where any valves, bends and branches are not installed principally for a distance of 15 times the diameter, a minimum span length required for flow measurement (10 times diameter upper and 5 times diameter downward from the meter installation point).