·					
.No.	Depth (m)	Rock Type	Classifi- cation	Coef.of Deformation D(kg/cm ²)	Coef.of Tangent Elasticity E(kg/cm²)
	31.00-31.50	f.Wt	CM	27,300	56,400
	34.70-35.20		CM	7,300	11,600
2	44.50-45.00	•	CM	14,000	36,700
:	62.50-63.00	Wt	СН	29,400	69,400
	68.50-69.00	#	CM	21,200	73,500
, . :	73.00-73.50	•	CM	13,400	24,500
	65.50-66.00	Wt	CL	3,500	4,200
3	77.00-77.50	n	CM	16,300	18,400
	87.50-88.00		CM	10,600	14,700
1	44.20-44.70	Wt	СН	30,600	45,900
	57.50-58.00	H	СН	16,600	19,600
5	13.50-14.00	f.Wt	CM	5,800	7,300
	25.50-26.00	Wt	CM	12,600	28,400
***************************************	16.70-17.20	f.Wt	CM	10,400	27,200
6	25.50-26.00	Wt	СН	153,100	490,000
	36.00-36.50	B	CM	-	26,200
	10.00-10.50	Ψt	CL	1,900	3,600
7	19.00-19.50	+	CL	3,900	4,900
	30.50-31.00	rt .	CM	22,800	27,200

Table E.1-4 Results of Physical Laboratory Test

BNo.	Depth	Elevation	Classif Specimen		•	Moisture ratio	Compressive strength
No. i	9. 1- 9.	2 EL 800	mortar		1. 72	17. 5	171.4
	24.0- 24.		mortar		1. 99	10.6	215. 4
	24. 5- 24.	6 784	rubble		2. 20	5. 2	180. 3
	28.0- 28.	1 781	mortar		1. 92	11.9	106.8
	39.0- 39.		₩t	CM	2.09		186. 2
	53.0- 53.				2. 25	6. 1	347. 9
	65.8- 65.				2. 28		507. 6
	74. 9- 75.				2. 39		766. 9
	88. 3- 88.	4 721	Wt	CM	2. 26	5. 5	161.8
No. 2	6. 7- 6.		mortar		1.62	23.0	70.6
	8.4- 8.		rubble		2. 19		354. 1
	23. 3- 23.		mortar		1.83	14.7	115.8
	25. 1- 25.		rubble		2. 26	3.8	642. 2
	27. 3- 27.		mortar		1. 73		93.0
	31. 3- 31.		Wt	CW	2. 12	8.5	299.9
	40. 1- 40.				1, 58		299. 9
	72. 9- 73.		711.		2. 31	48.0	-
	82. 5- 82.		Wt		2. 34	4.9 7.1	330. 4
	104.8-104.	9 704		÷	2. 17	1, 1	_
No. 3	8. 9- 9.	0 797	Ar	D	1.87	13.1	64.0
	10.7- 10.	8 795			1. 91	12.7	48.1
	43.0-43.	1 762	Tf	CM	1. 94	14.4	268.4
	54.1- 54.	2 751		CL	-	-	51.8
	61.0- 61.	1 745	Wŧ		1. 78	15. 2	36.0
	69.0- 69.				1.77		73. 1
	89. 9- 90.	0 716		CL	1.86	16. 1	63.4
No. 4	5.9 - 6.		Wt	CL	1.87	12.6	85. 4
	16.9 -17.	0 777		CH	2. 18	7.9	333. 7
	29.9 -30.	0 764		CM	2. 20	6. 5	297. 2
	37.4 -37.			CH	2. 23	6. 1	457.8
	46.8-46.				2. 23	6.0	468.0
	55.0 -55.	1 739			2. 26	5. 1	476. 2
No. 5	10.1 -10.		₩t	CM	2. 03	10.0	198.7
	28.0 -28.	1 763			2. 13	10.1	164.7
	31. 9 -32.				2. 23	5. 2	322. 7
	46.3 -46.	5 745		CH	2. 24	5. 3	427. 6
No. 6	12.8- 12.	9 745	₩t	CM	2. 20	7.1	316. 1
	18.0- 18.				2. 27	5.8	254. 7
	26. 7- 26.				2. 12	9. i	305. 1
	37. 2- 37.		Tf		2. 17	10. 4	
	54. 9- 55.	0 703	Wt		1.97	12. 4	82. 9
No. 7	8. 1- 8.	2 . 799	Az	D	1. 75	17. 5	33. 7
	13.8- 13.			D	1.79	15.7	-
	24.0- 24.			·CM	2.06	8. 9	112.7
	29.0- 29.	1 778			2.05	10.0	242.0
	34.4- 34.	5 773			2.09	9. 9	253.6

Table E.1-4 Results of Physical Laboratory Test

B-No. Depth	Elevation					Compressive strength
No. 8 19. 2- 19.	3 788	Wt.	CH	2. 38	2. 0	723. 9
34. 9~ 35.	0 773		D	1. 52	25.0	37. 4
47. 9- 48.	0 760		CM	1. 57	20. 3	152. 5
55. 9- 56.		· 	CM		17.8	119.6
			111			
Selguapa	(Cobble in	n Selguapa l	River B	ed)		
C-i	. • •		В	2. 11	5. 5	594.8
C-2		1	В	2. 67	2.0	371.5
C-3		. 1	В .	2. 31	2.4	546. 1

E.2 Present Condition of The Coyolar Dam

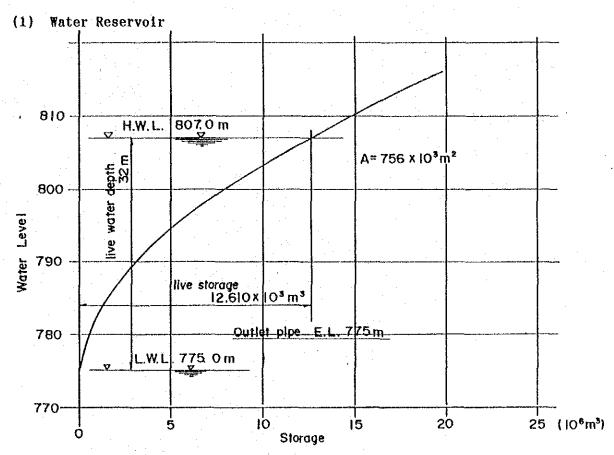


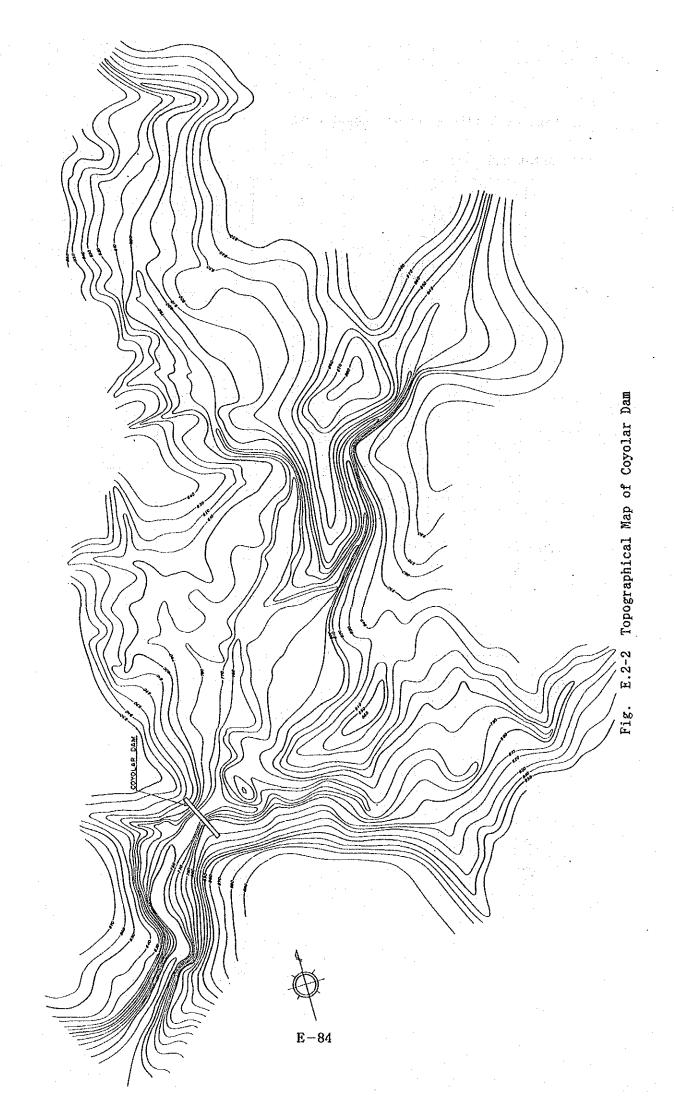
Fig. E.2-1 Water Level and Reservoir Volume Curve

Table E.2-1 Reservoir Level - Area - Volume

Table E.2-2 Reservoir Level - Volume

7,860

٠	Water	Surface	District	Cropp	wi	11	111 1	
ļ				Gross	W.L) V	W. L	V
	Level	Area	Capacity	Capacity				
ļ	₩. L	A	Y	V	i i			
-					816	20, 470		
I					815	19,450	800	7,860
l	815	956	4.46	19. 45	814	18, 558	799	7, 312
i	810	831	2. 38	14. 99	813	17, 666	798	6, 764
ŀ	807	756	4.75	12, 61	812	16,774	797	6, 216
Į	800	605	2. 73	7.86	811	15, 882	796	5, 668
l	795	490	2. 12	5. 12	810	14, 990	795	5, 120
l	790	360	1.50	3.01	809	14, 197	794	4, 698
l	785	245	0.96	1. 50	808	13, 403	793	4, 276
l	780	145	0.54	0.54	807	12, 610	792	3, 854
l	775	75	<u> i </u>	0.00	806	11, 931	791	3, 432
					805	11, 253	790	3, 010
					804	10, 574	785	1, 500
		*			803	9, 895	780	540
					802	9, 217	775	0
					801	8, 538		
					1		1 1	



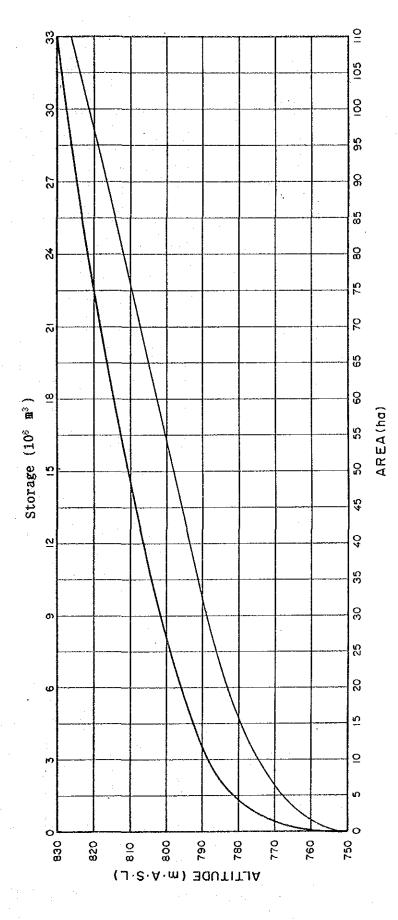


Fig. E.2-3 H-Q and H-A Curve

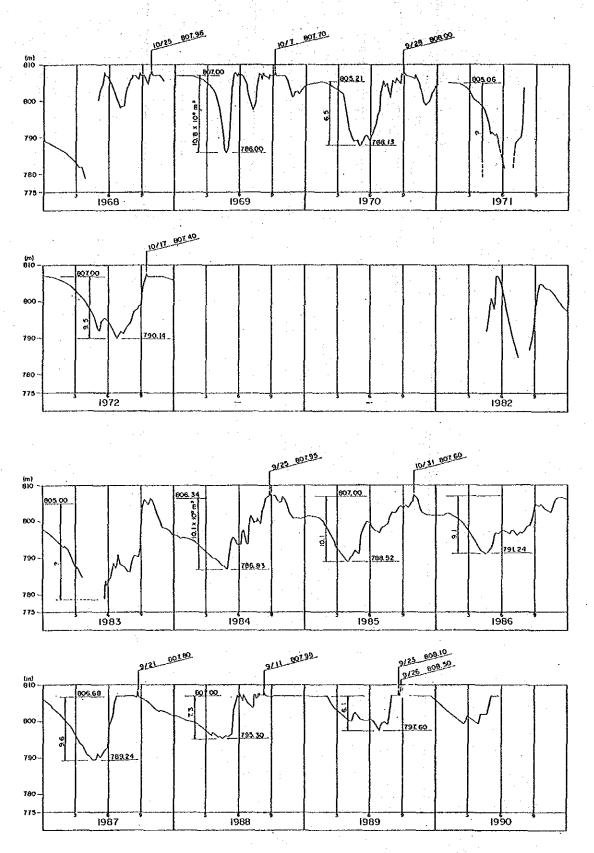


Fig. E.2-4 Recent Fluctuation of the Water Level at the Reservoir

Table E.2-3 Data of Reservoir Level (1/6)

·	1		7.		1											
Ŀ		1968	1969	1970	1971	1972	806. 94 806. 94 806. 94 806. 94	1982	1983	1984	1985	1986	1987	1988	1989	1990
1.	1	789, 21	807. 07	804.06	804.56	807, 02	806. 94		797, 58	796.96	801.16	801.96	805, 96	801.50	807.04	805.80
``	2		807, 08			807.02		~	797.70	796, 90	801.24	801.92	805.90	801.52	807.04	805. 16
	3		807. 08		804. 78	807. 02			797.76	796, 82	801.30	801.86	805.76	801.60		805.76 805.60
•	4		807.09			807. 02	50C 50		797.72	796.72	801.32	801.83	805.50	801.60	807.04	805.50
1.	- 5	789. 18	807.09	804.40		807. 01	900-92	. **.	797.60	196.68	001.40	801.91	805.74	801.54 801.54	807.01	
	6	1.7	007 D0			807.08			797.45	190.54	801.55	801.90 801.90	805.60	801.50		
	8		907.00			807 01		·	707 70	706 70	801.58	801.79	805.44	801.44	807.04	805.20
	9		807. 08		141	807 05			797 18	796 26	801.60	801.79		801.50	807.04	
1	10	789 DB	807. 07	804_62		807.01	806.96		797. 10	796, 16. 796, 03	801.62	801.87		801.56	807.04	805. OZ
ļ	îř		807. 07	.,7,1,55,1,55,	1 .	- WANTED	:	-	797.00	796.03	801.62	801.85	805, 28 805, 34	801.55		804.90
ļ l	12		807.07					7	796.90	795.91	801.72	801.89	805, 29	801.45		804.80
	13		807.06	804.90			;	-	796.86	795.80	801.72	801.85		801.35		804.70
	14		807.05		•		000 01	*	796. 78	795.72	801.70	801.83	805.06	801.32	807.04	804.60 804.48
	15	788. 80	807.06	804.74		805, 94	800.94	-	796.70	795.66	001.00	801.80 801.79	5 604 50	801.30	807.04	
	16	1000	897. Ub				:	-	700 00	795.58	801.62	801.13	804 K4	801.22	807.03	
	17 18		907 DE			•		_	706 54	786 40	801.60	801.71	804.66	801.15		
	19	2.5	807.06				1	-	796. 46	795 29	801.56	יתר וחמי	. OUY EQ.	- 001 10	• 807 03	. 30 1 05
1 1	20	788. 27	807.08	804, 85	:	806.92	806.94	-	796, 44	795.30	801.60	801.84	804.48	801.02	807.03	803.96
ļ	20 21		807.08						796.42	795.36	801.55	802.01	804.30	801.08	807.04	803.90
1	22	1.4	807. 10	4 1					796.30	795.48	801.50	802.17	804. 22	801.02	807.00	803.86
	23		807.08		:			-	796.30	795. 48	001.00	5 806 90	70 2 UB :	800.00	207 06	803. IU
	24	200 00	807. 05	nas ne		nne an	906 20	-	790.18	795: 62	: 001.07 : RN1 57	: 902.4V	803.34	900.10	807. 10	803.60
1	25 26	100.00	207 03	804.30		600-03	900.10	·	705 06	190.00	801.55	802.47	803.92	800.76	807.10	803.50
	27		RO7 03		:	:		_	795.82	795.66	801.63	802.52	803.80	800.74	807.12	803.28
	28		807. 02		:	:		-	795.70	795, 62	801.60	802.50	803.68	800.70	: 807. 10	803. 20
	29		807.03				:	-	795.58	795.72	801.57	802.49	803.56	800.68	807.09	803. 14
	30		807. 04		:			-	795. 58	795.74	801.52	802.50	803:44	800.52	907.08	803.10
 _	31	787. 82	807.05	805.04	; <u>-</u>	806.71	806. 94 806. 78 806. 54		795. 16	<u> 795. 64</u>	801.47	RD2 38	803.36	200.48	807.08	902.30 902.06
6.	1 2		807.V4	:	. 802. 01		•	-	105.01	190,64.	801.38	802.43	803, 26	900.55	807.10	802.30
	3		807. U3		i			-	795.06	795.30	801.44	802.43	803. 1G	800.50	807.10	802.86
	4		807. 02		:	:		-	794.96	795.38	801.38	802.44	803.06	: 800.50	: 807. 08	802.80
	5	787.51	807.06	805.15	904. 97	806. 42	806.44	٠ ٨.	794.80	795.40	801.32	802.43	802.96	800.55	807.08	802.70
Ì	6		807.04		:	:	•		794. 78	795. 34	801.26	802.30	000.00	800.44	607.09	802.60
	7		807.03					-	794. 64	795. 32	901.22	902 12	: 006.00 RN2 73	800.40	807.03	806.36
	8		807.02		i	:	806. 04	-	101 10	705.28	801.10	802.13	802.62	800.45	807.08	802.32
1	10	787. 27	807 OO	805 IR	ans on	806, 26	A06 04	_	794. 32	795 22	801, 17	802.10	006.06	. 800. 43	001.00	802, 22
	ïř	.1.7.13.51.	807.00					<u>-</u>	794. 22	795, 18	801.12	802.05	802. 12	: 800. 40	807.08	802.14
	12	- 1				:		-	121.00	133.66		801.99	802. 24	800.40	807.08	802.06
	13	l		:	:	:		- '	794.00	795.14	800.97	801.94	802. 14 802. 04			801.98
	4	200 00	000 07	oor n		00E 10	805. 72] -	793. 96		800.91	801.82				
	15 16	100. 85	BU6. 75	805. 21	805.06	900.10	003.72	-	793.86	795.01 795.06	800.71	801.84		800. 32		
	13							-		795.04	800.55	801.75		800.30		
	18					:			793.76	795.02		801.70				801.52
	19					. ,	:	-	793.71	795.02	800.20		801.60	800.18	807.05	
Ĺ	20	786.72	806.63	805.12	805.06	805.88	805.38	l	793.66	794, 96	800.00	801.51	801.46	799.98 799.90	807.05	
l	15			:	:			-	133.00		799.78	801.45	801.34	799. 90	807.02	
l	SS						:	j -		794.82	799.55 799.35	801.38 801.40		799.96 799.96		
	23				:			-		794.76 794.66	799, 15	NP 100 :	N 108:	799. 92	807.02	
	24 25	785 32	806. 40		: 804 GC	205 71	804.98	-	793.46		798.96			799. 90		
	26								1							000 00
	27						E .	-	793. 10	794.56	798.60	800.98	; 800. 58	799.70	806.98	800.76
	28	. 1	806.20	804.75	804.90	:	804. 76	-	793.18	794. 48	798. 42	800.90	: 800, 36	799.62	: 806. 98	800.68
	29	78G. 07														

Table E.2-3 Data of Reservoir Level (2/6)

100	7 11 1						1	jaka ja			. 1 5 21.	1.54	: <u></u>		
	1968	1969	1970	1971	1972	1974	1982	1983	1984	1985	1986	1987	1988	1989	1990
3. 1	ļ ,			 	L			793. 10	794.02		800.84	800.38	799.64	806.96	
l ž							-	792.94	794.14	798.04	800,82	800.24	799.60		800.52
3							-		794.06	797.82	800.75	800.08	799.58		800.48
. 4							-	792.58		797.60	800.68	799.92	799.54		800.38
5	785.60	806.08	804.68	804.74	805. 34	804.36	·	792.34	793.96	797.37	800.55		799.35		800.28
6									793.86	797.14	800.45		799. 24		800.22
1				λ_{ij}			*	792.42	793.80	796.94 796.72	800.33 800.20	799.54 799.52		806. 10	800.08
8						7 1	-		793.66	796. 55	800.12	799.42		805. 70	
9	405 19	00E 00	201 20	נס בסם	onr on	002 DO		791.94	793.58	796.38	800.02	799 28	799.12	805.50	
10.		909, 90	804.38	009.39.	oup. vv	602.60		791 60	793. 58	796.24	799. 91	799 12	799.06	805.20	799.82
112	***						- <u>-</u> -	791.30		796. 14	799. 81	799.02	798.90		799.76
13							-		793. 38	795.99	799.71	798.94	798.86	804.90	799.66
14									793.26	795. 78	799.60	798.68	798.90	804.75	799.54
15	784. 47	805.70	804.00	804.31	804.47	803.18	-	790.98	793.16	795.62	799.48	798.72	198.84	804.65	799. 42
16							_	790.80	793.06	795. 40	799, 28	798.60	798.80		799.30
17				•			-		792, 96	795. 24	799.14	798.44		804.36	
18		*				. "			792.96	795.04	799.01	798.28	798.70		799. 48
19						1.			792.84	794.86	798.88	798. 12	798.50		799.71
20 21	784.16	805.47	803.76	803.96	803.94	802.56		789.74		794.66	798.76	797.94	: 798. 38	803.98	(99.02
21							*:		792.56	794.64	798.66	797.78	798.42		799.97
22				•					792.44	794.56 794.38	798.35 798.27	797.80	798.32	803.70	800.12
23							-		792. 28	794. 20	798.17	797.66 797.50	798.36 798.32	803.64 803.60	800. 22 800. 30
24	202 52	nor an	000 20		003.40	001 00	-		792.18 792.36	793.99	798 04	797.20	798.26		800.48
25	783: 62	805.12	803.78	803.68	803.40	801.82	<u>.</u>		1792.26	793.80	797. 80	796.98	798. 10	803.50	
26 27			;	:			-	788.33	792. 18	793.60	797.71	796.72	797.98		800.80
28				:			Ī.,	788.06	792. 14	793. 30	797.66	796.50	798.02		801.20
29				:					792.04	792.98	797.60	796.52	197.78		801.54
30						11.0	_	787.40	791.94	792 60	797.51	796.52	797.65	803.02	801.46
31	283, 20	804.84	803. 20	802 94	803.00	สกก สล	- . -	787. 24		792.28	797.40	796:01	797.54	802.96	801.46
4. 1	144440		:	:	:			787. 13	791.86	792.06	797. 28	795.82	797.40	802.86	801.45
2			:	:			_	787. 16	791.72	791.98	797.02	795.50	797.28	602.70	801.39
3			:	:				787. 21	791.60	791.82	796.90	795.28	797.16	802.60	801.30
4	,						-	787.03		791.86	796.77	795.08	797.20	802.50	801.20
5	782, 35	804.77	802.61	802.50	803.70	800.02	-	786.81	791.21	791 88	796.60	794.98	797, 16	802.35	80L 14
6			:	:	:		-	786.56	791.06	791 82	796.48 796.38	: 794.78 : 794.56	797. 10	802.25	801.01
7		:		:			-	786.84	790.92 790.95	791.58	796.20	794.36	797.02 796.96	802.15 802.10	800 91
8								786.64	190.80	791.44	796.04	794.16		802.02	800.83
9	1.	804 22	002.02	. 000 CO	002 16	200 00		786. 24	790.70	791.26	795.88	793.96		801.95	800.70 800.60
10 11		804.34	802.02	800.69	011.500	799.00		786.01	790.56	791.08	795.70	793.72	796. 64	801.86	800.42
12							- '	785. 84		790.82	795.54	793.84		801.78	800.42
13							-		790.26	790.70	795.40	793.84	796.60		800.44
14			i	:	:			785.44	190.10	790.61	795. 26	793.64	796.54	801.50	800.38
15	782.30	803, 80	801.78	800, 42	801.56	798.64	-	785. 24	790.16	; 790, 50	- 795. 08	- 793, 58		801,40	800.22
16				:	•	:			790.08	: 790. 32	794.90	793.50			800.08
17			:		:		_	784.81	789.96	790.16	794.72	793.44		801.20	
18			:			:			789.96	790.06	794. 54	793.46		801.10	799.90
19			:	;		:	_		189.96	789.92	794.36	793.52			1,00.00
20 21		803.08	798.95	800.00	801.10	797.10	-		789.94 789.94	: 789, 80 : 789, 70	: 794.28 : 794.08	: 793.28 : 792.96		: 800. 90 : 800. 80	799.86
	780.48			:	:			-	789. 94	789. 10	793.88	: 792. 90 : 792. 70			
22		1	:		:	:	-		789. 76	789. 28	: 193. 00	792.41	796.60		. 133.00
23			:	:	:	:	-		789. 80		793.50	792.20			
24 25	779.00	901.00	795.66	799.51	t not :	796. 10	-		789.80		793. 20	791.96			
26	113.00	001.30	120.00	122.24	. 600, 44	150.10			789.80		793.04	792.02			
27	i	1					-		789.82			791.80			
28			:	:	:	:	1 -		789.72		792.83	791.54			
29		ĺ		:	:	:			789.70		792.66	791.16			\$00.02
30	l	799.87	792, 10	798.74	799.78	795.06	-		789.44	: 788.96	792.48	: 790.90	796.10	: 800.42	800. f.G.
									*						

Table E.2-3 Data of Reservoir Level (3/6)

			·													
		1968	1969	1970	1971	1972	1974	1982	1983	1984	1985	1986	1987	1988	1989	1990
	5. 1									789.50	789.74	792.32	790.85	795, 96	800.44	801.02
	S					(_		789. 40		792.15	790.60	795.99	800.40	801.46
	3							_		789. 30		791.96	790.64	795.94		801.78
	5		798. 10	790, 45	798. 27	798.80	704 00				790. 34 790. 40	791.96	130.00	795.84		801.98
ļ	6		130. 10	130. 23	1,30-61	130.00	194.00	-			790.30	791.88 791.85	790.50 790.34	795.72	800. JB ;	802.10
	. 7					:		-		789.06		791.81	790. 25		800.38 800.34	802.30 802.42
i	8							-		788.86	790. 30	791.75	790, 28		800.30	
	9		50. 50					-		788.56		791.70	790. 26	795, 86	800, 26	802 38
-	<u>10</u> 11		794, 98	789.58	797, 88	797, 90	793, 70			788.38		791.80	790, 23	: 795. 9D	800.22:	ี่ มกวาว ไ
-	12				:			. ~		788. 22	790.73	791.82	790. 20	795. 94	800.40	802. 36
	13							-		788.06 788.12		791, 74 791, 58	790.04		800.70	
	ÎÃ		1					·		787.90		791.40	789.70		801.10 801.50	
	15		791.52	788.83	796. 28	796, 70	793.10	-		787.82		791.24	789.60	195.00	801.90	RD2 24
	5. 16)					1)		787.17	791.34	791.25	789.55		802. 10	
	17									787. 67	791, 36	791. 27	789.50	795.60	802. 20	802.14
٠	18 19							_		787.73		791. 27	789.40	795.70	802. 25	802.08
	20		798 66	789. 10	704 94	706 OF	201 52			797.64	791.86 791.96	791.28	789. 24	795.86	802. 30	
••]	ži		100,00				174-76	792.32	***********	787.78 787.62		791.36 791.41	789.44 789.60	795.94	802.33 802.30	802.08
	22						796. 48	792.44		787. 47		791.66	789.70		802.30	
- 1	23							792. 82			791.62	791.78	789.70		802. 20	
	24		700 70	nnn • n				794.00	•	787.10		791.87	789.70	795.84	802.10	802.48
1	25 26	100	186. 13	789.16	791.58	794. 48	797.72	795.20 795.80		786.94		792.12	789, 50		801.98	
ı	27		786.00					796, 20		786.83 786.90		792.30 792.54	789. 70 789. 74	795.96	801.84	804.06
	28		102.00					797.86		787. 18		792.61	790.30	795 90	801.74 801.60	RD4 58
	- 29		787.60	* .	791.06			798.76			791. 19	792.68	790.52		801.50	
	30		000 00					799. 26		787.60	791. 23	792.74	790.66	795.74	801.30	804.95
	31 6. 1	800.55	787, 20	788. 13	791.5B	792.78	797.74	800. 40 800. 90				792.74	790. 90		801.20	
	2	090.33	101.20		:			800.90				792.75		795.96		
. [. 3		793. 12					800.76		790.96	794.04	792.76 792.68	790. 98 790. 80	796.10	800.88 800.80	
ĺ	4	ļ			,			800.76		791.56		79Z. 64	190.68		800.60	
ı	5	803. 17	795.48	788.50	791.48	791.94		800.40		792.50	796.38	793.40	790.50	795.90	800.50	806.76
	6		202 00					800.10			796.60	793.66	790. 34	795.90	800.40	806.77
	Я		797. 82			793. 80		799. 90 799. 58			796.80	794.94	790.45	796. 10	800. 20	806.77
	9							200 10		793. 12 794. 10	796.99	796. 02 796. 30	790. 24 790. 10	795.14	800.50	806.75
	10	804.28	802.30	788, 90	790.80	794,74		798.64		794.80	797. 40	796. 46	790. 10 790. 40	796.40	800.50 800.46	005 73
	11	804. 27	805.35					798. 20	779.60	794.80 795.10	797.76	796.62	791.16	797. 40	800.42	
1	12	807.15		: : :			1	798. 70	779.12	795. 20	198.02	796.68	791.46	798.20	800.60	
ı	13 14	807.70 807.50	806. 26					803. 80 807. 40		795.38	798. 24		791. 75	800.60		
j	15	807.36	807.50	790 53	791.34	795 38	Ì	807. 24		795.66 : 795.60 :	198.62 799.18	796.80		801.80	800. 52	
-	16	807.06	807.60			130.00		807. 20		795.78	799.46	796.82 796.88	791.85 791.76	802.85 803.40		807. 05 806. 90
ı	17	807.06	807.40				i	807. LO	779. 14	795.70	799 66	796.84	791.70	803.86		806.94
	18	807.06	807.60					807.03	779.96	795. 48	799.80	796.76	791.96	804.30		806.98
ĺ	19	807.07	807.30	200 00	200 24	E05 15			781.80	795.18	799. 96		792. 16	804.70	800.55	807.04
	20 21	807. 10 807. 48	807.30 807.18	790.60		195.41		807. 04 807. 10	782, 34 783, 48	795.08 794.90	800.07	796.60	792.23	804.90	800.50	807.14
ſ	22	807.18	807.10						783.78	794.58	800. 12 : 800. 06 :		792.36 792.60	805.20 805.60	800.44	806 98
- 1	23	807. 10	807.08		:			806. 94		:	800.00		792. 60 792. 70	806.70	BDD 32	806.76 806.58
١	24	807.04	807.00				1	806.70	782.64	793.90 :	799.93		792.75	806.40	800. 20	806.80 l
ı	25	807.00		789. 76		794.98			782.79	793.76	799.96	797.05	792.65	807.14	800.20	806.98
	26	מחב בר	807. 18					806.02			799. 96		792. 70	806.98	800. 20	
	27 28	806.65	807. 16 807. 18					805.72 805.40	783. 09 783. 24		799.84		795.40	80G. 75		1
	29		807. 26					805.08				797.47 797.66	797.60 :	806. 80 806. 60		!
	30	805.88		789.86		794.68		804.60		793.60	799.55	197.78	798.50	806.40	800.54	
													<u></u>		200.01	. 1

Table E.2-3 Data of Reservoir Level (4/6)

			•					100	e de la Company		100		Alleria	196
	1968	1969	1970	1971	1972 794. 38 792. 88	1974	1982	1983	1984	1985	1986	1987	1988	1989
$\frac{7.1}{7.1}$	 	807.08	<u></u>		1		804, 14	783 70	797 56	799.42	707 84	798 80	106 15	800 46
1 2	1 4	807.06	:		794 38	· .	803, 76	784 00	793 56	799. 24	797 86		807.20	
1 3	1	807.03	:	:	134.00		803.30	784 40	193 62	799.02	797 86	799.30		
1 4	100	807. 22	1,745		:	l .			793.68	798 90	797 RO		807. 20	
5	804.87	807.14	791.56		:		802.36	784.76	793.72	798.72	797.62		807. 10	
6	****	807.07			:		801.98		793.66	798.60	797.50		807.02	
ž		807.00	:		:		801.40		793.84	798.50	797.57		806.88	
8					:		800.90	785, 50			197.42			800.44
9					792.88	l	800.40	786, 40	197.18	798. 28	797.34		807.30	
10	803, 87	806.74	792.30				799.84	786, 90	797.30 797.53	798.19	797.22	801.10	806. 10	800.20
10	1.41.11.11.11.11.11.11.11.11.11.11.11.11				:		799.24	788.00	797.53	798.02	797.10	801.80	806. 10	800.05
12			:			İ	798.80	788.34	797.40	797.92	796.98	: 802.30	806. 20	800.05
13	[:		ĺ • •	798.32	788.40	797. 12	797.88	796.88		806.80	800.05
14				:			797.82		796.84	797.76	796.94	804.10	807.30	
15	802.64	806. 10	793. 78			İ	797.52				796.94		807. 10	
16	1			:			797.20		796.06		796.87		806.96	
17		•	:	:					795.66		796.80	806.05	806.85	
18			:	:				787. 38	795.28	797.44	796.73	806.40		
19				:				787, 22	794.90	797.48	796.62		806.30	
20 21	800.92	804.51	796.10	.		,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,		787.30	794.58		796.58	806.95	805.90	
21		•					795. 16		794. 20		796.56	807.20		798. 30
22								787, 42			796.58	807.30	805.60	798. 10
23					790. 14					797.50			805.50	
24 25		000.00	000 11				793.70			797.44		807.10	805.36	
75	799.06	803.00	797. 44				793. 20		793.80	797.34	797.24	807.20	805.30	
26 27			:						793.80	197.60	797. 42 797. 58	001.00	805.20	797.00
1 61	798.25	:	799.40	:			792.44		793.80	797.02	707 74	: 007 10	805. 10 804. 90	207 90
28 29		:	133.40					790. L4 789. 74	793.98	797.55		907 05	804.80	707 ON
30			800.32		791.34	!		789.22				807.02	001 CD	708 90
31	700 20	800.34	803 NS		151.54	l i	191.10	788.66	705 40	798.14				
8 1	130. 60	000.01	803.91				790. 20		796.05	798.30	797.70	806.96	804 50	799:35
0. 2			805. 26				789.80		796.50	798.37	797.60	807.02	804.40	799. 50
3							789.34		796.50		797.36		804.44	
1 4	1		:	:			789. 12		796.50		797.24		804.50	
5	798.37	798.34	804.88		792.00		788.84		796.50	798.66	797.12	807.10	804.56	799. 84
Ě		:		-			788.50		796.46	798.72	795.98	807.25	801.70	799.90
1 7				788.22		1 1	788.06		196.24	798.78	796.82		804.50	
- 8		797.30					787.60	787.96	195.94	798.79	796.70		804.20	
9							787.20		795.60	798.82	796.56		804.10	
10	798.48	798. 23	804.10	789.00	791.72		786.70	788.12	795.30	798.82	796,40		803.80	
11						[[786. 10		795. 10	798. 78	796.26	807.02	803.75	
12	798.73		•	,			785. 50		794.98	798.82	796. 18	806.98	804.20	
13	800.34						785. 16		195.02	798.86	796.28	806.96	806, 80	
14		200 20	001 00	200 62				787.85	795 04		796.50		807. 20	
15	802.28	: 199. 10	801.88	109.51	792.40		784. 90	787, 62	795.06		796.68		807.30	
8.16	000 00							787.37	794.99	799.35 799.40	795.83 796.90	806.92 806.95	807 20	
17	803. 27	804.47						787.10	794.98	799.45	796.98	806.95	807. 10 806. 80	
18		•						786.83	795.02	799.46	797.02	: 806. 90		
19	904 27	205 23	ยกว วด	790 80	793, 30			786, 52 786, 25	795.06 795.10	799.52	797.04	806.82	806.50	799.60
20 21	1.4.A.Y. S.I.	.003.03						785.98	795.56	799.62	797.04	806.80		
22	1	806.67	:	:		i l	1	786.04	195.76	800.02	797.02		807.15	
23	1	807.04	•	790.44				786.04	795.68	800.60	796.90		807.04	
21	1	807.08	:		:		ļ	786.00	795.44	801.18	796.86	807. 02		802.10
25	805.85		801.24	792, 46	793.75			786. 16	795. 18	801.50	796.82	807.02		802.50
26	1	807. 22	801.06				[786. 32	794.80	801.76	795.84	807.02	807.60	
21]	807. 18		797.13		•	l		794.44			807 02	807 40	
1 28	1	807.16	803.00				l	785.90	794.10	802.20	797.01		807.70	807. 22
29	1	807. 18	:	799. 26	:			787.10	793.90	802.37	797.10	807.04	807.30	807. 16
30		807. LU	804.62		:			787.40				807.04		
31	806, 44	807.04	805, 46	: 803.48	794.40		l	787.50	794.40	802.58	797.02	: 807.02	1807.40	807.30

Table E.2-3 Data of Reservoir Level (5/6)

		<u> </u>	·	ر — نب سنم				<u> </u>		ı			
	1968	1989	1970	1971	1972	1974	1982	1983	1984 1985	1986	1987	1988	1989
9. 1	806.70	807.00				-		788, 20	795, 70 ; 802, 64	797.04	807.02	807.50	807. 20
2 3		806.86			794.75			788.90	798.90 802.70	797.18	807.03	807. 30	807. 12 807. 02
3		807.50 807.55						789.42 789.72	800. 10 802. 62 802. 50 802. 58	797.75 797.93	807.06 807.16	807. 22 807. 14	806.98
5		807. 26	805.32		795.96			789. 88	803. 28 : 802. 58	798. 10	807. 16	807.06	806.90
6	807.00	807.20				:		789.96	803.52 802.56	798.28	807.16	806.96	806.96
7	807.04	807. 24	805, 05		797.00		l	789.96 790.00	803, 80 802, 56	798. 38	807.04		806.98
8	807.25	807. 22						790.00	803.94 802.60	798. 45 798. 48	807. 02 806. 94	807.30 807.16	806. 98 806. 98
9	807. 18 807. 10	807.35 807.16	806. 28		797.74		1	789. 95 700 57	804. 12 : 802, 68 804. 58 : 802. 72	798.48	807.04	807.30	807.04
<u>10</u>	807.03	807. 13	806.50		: .l.v.l.r.f.r.	*************	ļ	790.72	805. 70 802. 79	798.38	807.04	807. 98	807. 10
12	000	807.08							806, 40 802, 84	798, 23	806.98	807.80	807.40
13	1 :	807. 04						790.70	806.66 802.94	798.44	806. 90		807. 30
14		200 20	00v 00		798. 22			790. 64 790. 60	806, 70 : 803, 06	798.60 798.66	806. 96 806. 96	807. 20 807. 10	807. 18 807. 25
15	806. 15	806.80	805. 82		190.26		787.00	700 50	806, 80 : 803, 18 807, 02 : 803, 30	798.75	806.98		807. 30.
16	805. 92						787. 20	790.41	807. 16 803. 56	798.96	806.98		807.30
18	J. 32	1. 1. 2. 2. 2. 3	804.82				787. 40		807.08 803.90	799. 24	: 806. 9Z	807. 20	807.40
19	806.90						788.00	790.40	807.02 804.06	799.45	806.92		807. 40
20 21	807. 03 807. 19		805.40		798.66	;	788, 70 789, 20	790.38	806, 90 : 804, 16	799.62	806.90 807.80		807, 45 807, 25
21	807. 19 807. 70	807. 28 807. 36	807.68 807.24			į	789. 20 789. 80	790. 34 790. 36	806. 84 : 804. 22 806. 50 : 804. 26	799. 80 800. 02	807. 30		807. 18
23	807. 46	807.30	807.12			1	790. 20	790.42	806. 26 804. 27	800.70	807.14		808.10
24	807. 32	807. 20	807.44				790.60	790.54	806.40 804.52	801.20	807.06		807.60
25	807, 20	807. 12	807. 18	1 1 1	799.01	•	791.20	791.37	807. 95 : 804. 44	801.56	807.02		807. 20
26	807:14	807.06	807.03			i	791.60	792.60	807. 34 : 804. 17	801.80	806.90		808.50 807.30
27	807.17	806.98	807.07 807.52	•	799. 17		792.40	793. 32 793. 56	807. 70 : 803. 98 807. 36 : 803. 75	802.90 803.85	806.80 806.70		807. 25
28 29	807. 09 807. 04	806.92	808.00				794. 30 795. 40	795. 94	807. 30 803. 57	804. 28	806.60		807.40
30	807.14			-	799.92	l	1796, 50	798.88	807.14 803.51	804, 50	806.56	805.88	
10. 1	807.09	807.01	807. 36		:	-	797. 40	800.98	807. 24 : 803. 59	804.62	806.60		807.80
2	807. 05	807. 02	807. 50 807. 28 807. 22 807. 10 807. 12 807. 12 807. 14 607. 04 807. 14				797.80	801.97		804.60	806.52 806.44		807.50 807.30
3	807. 06	807. 20 807. 16	807.28		802.85		799. 60 800. 10	802.43 804.00	807. 24 : 804. 30 807. 20 : 804. 56	804. 70 804. 58	806.40		807. 16
1 5	807. 08 807. 05	807.30	807. 10	5.0	804. 22	· .	801.30	804. 78	807. 13 804. 64	804. 40	806. 34		807. 14
š	807.00	807.50	807.12				803.00	805, 65	807. 15 804. 51	804.20	806.25		807. 20
7		807.70	807. 12				802.86	806.02	807. 30 : 804. 42	804. 10	806. 23		807. 16
8		807.54	807. 14				803. 30	806.20	807. 15 : 804. 30	804.05 804.02	806. 20 806. 17		807. 12 807. 06
9	one to	897. 36 807. 40	607.04	4 - 4 -	90F 47		803.70 804.00	806. 22 806. 16	807. 08 804. 38 807. 02 804. 39	804.02			806. 98
10 11	806.10	807.30	807. 10		. 000.30.		804. 30	806.06	806. 95 801. 25	801.30	805.12 806.08	807.30	807.04
12		807. 31	807.00				804.50	805.95	806.80 804.05	804.56	806.13		807. 04.
. 13	805. 21	807.30		,		1	804.60	805.72	806.60 803.91	804.58	805.10		807.04
14	100	807. 22	807. 14 807. 10 807. 00 806. 70 806. 80		807. 04		804.80	805.52	806. 38 803. 80 806. 10 803. 87	804.58 804.55	806.02		807. 04 807. 04
15	804.80	807 11	. 600. 10		: 001-UB	1	805.00	805.34 805.08	805. 84 : 803. 95	804.54	805.98		807.04
16 17	004.00	807.18	:	•	807.40		804. 98		805. 50 804. 25	804.60	: 805. 92	807. 20	807.04
18	806.40	807. 24	:	:	807. 20]	804.94	804.46	805. 46 804. 56	804.56	805.82		807.06
19	806. B5	807.84	i aan aa		807. 24		804.90	804. 14	805. 36 : 804. 77	804.38	805.76		807. 06 807. 06
20	807.34	807.30	806.80		807. 28	·····	804.82 804.96	804.54 804.71	805, 25 : 804, 90 805, 15 : 804, 99	804. 16 803. 94	: 805.65 : 805.50		807.06 807.10
21 22	807.15 807.06	807 28			: 807 3A		804.90		805.02 : 805.06	803.68	805.34		807. 10
23	807.00	807.17			807.22		804.74		804. 98 : 805. 12	803. 57	805.18	807. 30	807.10
24	807.07	807. 26		:	807.17		804.50		805. 14 805. 20	803.50	805.02		807:10
25	807.96	807.19	805.12		807. 14		804. 10		805. 30 : 805. 64		804.85		807. 10 807. 10
26	807. 34	807.16	:	:	: 807. 12 - 907. 11	1	803. 80 803. 74		805. 38 805. 70 805. 30 805. 70	803.43 803.43	804.75 804.60		807. 10
27 28	807. 20 807. 14	807 19			807 10		803.70		805, 18 805, 73	803.40	804. 48	807.40	807. 10
29	807.08	807.16			807.09		803 70		805.50 805.67	803.36	804.30	807. 35	807. 10
30	807.04	807.15	805. 12 805. 30	· .	807.09	١.	803.74	806. 12	806.50 807.20		804.34		807.10
31	807.15	807.12	: 805.30	<u>: </u>	: 807 . 0 8	<u> </u>	803, 70	805. 92	806, 90 807, 30	- 803. IS	· 804. 22	. 507. ZU	8U1. IU

Table E.2-3 Data of Reservoir Level (6/6)

		وسنينين		· · · · · · · · · · · · · · · · · · ·					4 1	74	2013 x 3	<u> </u>	<u> </u>		
	Na.	1968	1969	1970	1971	1972	1974	1982	1983	1984	1985	1986	1987	1988	1989
ſ	11. 1	807.20	807.08		807.12	807.12				807.00		803.05	804.02		807.10
١	2	807.06	807.04	807.06		807.09				807.00		803.05		807. 20	807.10
ı	- 3	807.36	807,00	807.04		807. 09 807. 09 807. 07				806.85		803, 08			807.10
1	4	807.23		807.00		807. 07		803, 60		806.60		803.12	803.75	807. 18	807.10
-	5	807. 26	806.80	806.89	807. 20			803.57		806.30		803.05	803.68	807. 20	
. [6	807. 16	***			807. 06		803. 47			806.90	803.01	803.62	807. 18	
	7	807. 12				807. 05 807. 08			804.10		806.70	802.90	803.52	807.17	2111 12
- [-: 8	807.08			50 0	807.08			803.74	805.50		802.76	803.55 803.45	807.16 807.16	807.10
1	9	807.04	one on	80C 20	007 11	807.06		803. 38 803. 40		805.20		802.72 802.68	803.38	807 18	` · -
1	10 11	807.03 807.00	.043.04.	003.13	3835	807. 06 807. 06		803.34	802.98	805.05 804.70	805.58	802 66	803.30	807.14	807.10
- 1	12	007.00				807. 07		803. 26	802.70	804.30	805. 15	802.86	803.24	807. 14	807. 08
1	13	806.89				807. 07		803. 21		803.94		803.10	803.18	807. 14	807.08
ŀ	14	807.08				807.06		803. 15		803.60		803. 22	803.02	807. 14	807.08
I	15	807. 10	804, 19	804.25	807.09	807.06		803.06		803.20		803.40	803.06	807.10	807.08
ì	11.16	807.12				807.06		802.97		802.70		803.80	802.98	807.10	807.08
	17	807.12				807. 12		802.88	801.20	802.60	803.58	804.20	802.90	807.10	807.08
	18	807.12				807. 10	:	802.75	800.86	802.50	803.23	804.40	802.85	807. 10	807.08
1	19	807.12				807.08	:	802.58	800.50	802. 18		804.60	802.80		807.08
	20	807.12	802.65	802.35	807.05	807.07		802.38		801.76	802.83	804.80	802.88	**********	807.08
`	21	807.12				807.05	:	802. 20		801.36		804.98	803.06		807.08
	22	807. 12		:		807.06			799.52		802.63	805. 24	803.16	807.10	
	23	806.80				807.06	:		799. 22	801.18	802.57	805.52	803.16	807.10	
	24	one so		200 00		807.05			799.06	800.96	802.51	805.70	: 803.12		807.08
- 1	25 26	806.00	801.07	800.27	807.06			801.50	798.88 798.67	800.74 800.74	802.44 802.38	: 805. 88 : 806. 02	803.04 802.98		807.08 807.08
ı	27		801.46		:	807. 05 807. 00		001. J4	798.48	800.70		806.10	802.98		807.08
Į	28	İ	001.40	· .		807.00	:		798.34	800.70	802.18	806.18	802.94		807.08
ı	29	\	1						798. 27	800.68	802.06	806. 20	802.92		807.08
	30	805.40	801.54	799, 09	807.04	806.95	: - :	800.86		800.80	801.98	806.30	802.86		807.08
- [12. 1	805, 40		799.02		:	:	800.75		800.92	801.88	\$96.34	802.80	807.10	807.06
	2	-				:		800.60		800.96	÷ 801. 79	806.40	802.74	807.10	807.06
	3	!		•	:		:		798.10	800.94		806.40	802.70	807.08	807.06
	4						:		798. 10	800.96		806.48	802.64	807.08	807.01
	5	}	802.67	799.49	807.06	806. 99	Ì		798.08	800.96	801.61 801.65	806.37	802.62 802.68		807.04 807.04
- 1	6					:	:		798.05 798.03	800.94 800.90	801.70	806.52 806.40	802.65		807.01
l	8	l	1		:	:			798.05	800.96	801.76	806.44	802.64		807.04
- 1	9		802 74			1 1 14	:	799.68		800.94	801.80	806.50	802.63	807.05	807.01
ı	10	İ		800.07	807.03	806.70	:	799.55	797.94	800.94	801.79	806.55	802.55	807.05	807.01
	11					•	:	799.43	797, 86	800.90	801.83	806.60	802, 47	807.04	807.01
j	12			:					797.79	800.91	801.84	806.60	802.40	807.04	807.04
	13	l	802, 24	:	:				797.70	800.90	801.70	806.60	802.41	807.01	
ı	14		000.00	000.00	002.01				797.62	800.88	801.70	806.65	802.38 802.30	807. 04	
	15 16] .	802.50	800.30	807.01	806. 47	:		797.57 797.64	800.84 800.90	: 801.75 : 801.71	806.68 806.60	802.16	807. 04 807. 04	
- 1	17	1	1		:	:	:		797.56	800.88	: 801.68	806.55	802.10	807.04	
Ì	18]]		:	:		798.64		800.86	801.64	805.54	802.02	807. 04	
	19		l		:	:	:	798.56	797.52	800.85	801.62	806.50	801.92	807. 04	
	20 21		803.00	802.42	807.01	806, 29	<u> </u>	798.44	797.41	800.84	801.60	806.60	801.95	807.04	
1	21			:	:			140.36	797.35	800.80	801.53	806.46	801.90	807.04	
1	22	1		:	:	:	:	798. 20		800.78	801.56	806.44	. 801.88	807.04	
į	23	į				:	:		797.16		801.56	805.40		807.04	
	24		on2	002 55		ane or	:	797. 93		800.88	801.41	806.30	\$801.74 \$801.70	807. 04 807. 04	
ŀ	25 26		803.44	803.58	807. 07	. 805. 25	:	797.93		800.81	801.42 801.36	806.25	801.61	807.04	
1	27	1	}	:	:		:	797. 88			801.40	806.14	801.68	807.01	
ı	28						:	797, 77			801.54	806. 18	801.62	807.04	
1	29	1	[:	:	:	:	797.63			801.78	806.10	801.60	807.04	
- 1	30	1]	:	:		:	797.50	796, 78	8' 74	801.86	806.04	801.56	807.04	805. 94
į	31	<u> </u>	803.92	804.43	807.02	806.06	<u>:</u>			860.94	: 801.94	805.94	801.56	807.04	805, 90

Table E.2-4 Reservoir-Rainfall (1/6)

										· · · · · · · · · · · · · · · · · · ·	-		
i			1968			1969		1970		1971	1972		1974
.			W.L. C	∮8 Qv	R .	W.L. Qs		R W.L. C	8 QV	R W.L.	R W.L.	Qs Qv	R W.L.
	1. 1		189, 21	-	0.5	801.01 807.08	. 2 - 2 -	U. 8 8U4. V6	0. L		807.02 807.02	0 0.0	805, 94
	;			Q. L	1.1	807.08	2 -		0.1			0 0.1	1,1
	1		444 14	0.2		801.09 807.09	3 -	804, 40	0. I		807.02		
٠.	5	1	789. 18	0. 1 0. 2		807. 08	1 -	004.40	0. 2		0. 2 807. 01 0. 3 807. 02		805.89
	i			0. 2		801.05	2 -		0. L	ł	807.01	0 0.1	
i				0.1		807. 08 807. 08	1 -		0. 2 0. 1		807.01 807.03		
	10		789.08	0. 1 0. j		. 007, 07	2 -	804, 52			807.03	0 0.2	898,96
	iii	ļ		0. l		807.07	2 -		-			V. I	
	18		•	0. I 0. 2		807.07	1 - -	804, 90	0. l 0. z)		0. 2 0. 2	1
٠.	13 14		7.	0. 2		807.06 807.06	i -	604, 30	0. 2	· 1	•	0. 2	
	į5		185.80	0. 2		801.08	1 -	804.74	0, 2		806, 94	0. 2	806,94
	16			0. 2		807.08 807.08 807.06	l/ -		0. 1 0. 2			0, 2	
	17 15			0. 2 0. 2		807.08	1 -		0.1			0. ž :	0.4
1	19			0.2		807.08	-		0.1			0. 2	
	10.	ļ	188, 27	9. 1.	. 2. 4.	. \$07, 08		804,85	0. 1 0. 1		806, 97.	0. 2	406, 94.
	21 22	1		0.1	6. U	807.08 807.10	; -		0. 2			0. 2 0. 2	
	23			0. 2		807.08	2		0. 2			-	
.	24			0.2		807.05	1 0.1		0. 2			0.1	
.	25 28		T88. 00	0, 2 0, 2		807. 04 807. 03	1 0.1		0. l 0. l		808, 89	0. l 9. ž	808, 78
	27			0.2		807.03	i 0. i		0. i			0. 1	
	28	ł		0.1		801.01	0 0.1		0.1			0.2	
	29 10	ļ.,		0. l		807. 03 807. 04	1 0.2		0. 2 0. 2			0.) 0. (i	
	31		181, 82	0.1 0.1		807.05	1 0.1	805.04	0. 1		806.71	0, 2	806, 54
	2. I			0, 1		807.04	1 0.1		0.1	805, 01		0. 2	
	2			0. L		897. 03 807. 02	1 0.1		0. 1 ! 0. 2			0. 2 0. 2	1
-	3	l		0. L	8. 2		0.1		t o			0.1	
1	Š	1.	8 787, 51	0.1		807.96	2 0.1			904, 97	806. 42	0, 2	808, 46
			.\$	0. l			1 0.1		0. 1 0. 1			- 6. 2	1
	1 8	[U.	. 4	0. l 0. l		807. 02	1 0.1		0.1	0. z 1		0. 2	
	. ,	1		0.1		807.01	I 0. i		0. L			0. 2	
l	10	ļ	187.27	9,].	l	807.00	9. J.	895, 18	0.2 0.1	805, 00.	805, 26 0. 2	0. 2	805,04
	11 12			0. 1 0. 1		807.00	0. <u>1</u> 0. 2		Λ 1		U. 6	0. 2 ± 0. 2	
	3	١.		0.1			0.1		0.1	0.2		-	
ļ	11			0.2		PAR 18	0. 2	. PAE 41	0.11	805.06	#A# 1A	0.2	805, 72
	15 16	Ì	785, 85	0. Z		806.15	0. 2		0.1	809.08	500.10	0. 2 0. 2	603.72
-	17]		0.1			0. l		0.1	j .		0. 2	
-	18			0.1			0. 2			20. 2	0.4	0. 2	
٠	19 20		786 77	0. 1 9. J		805, \$3	0. 2 0. 2	805, 12	0. 2 0. 2	805,06	0.4	0. 2 0. 2	805, 38
-	£7.	ļ		0. 1		. 1771 77	0.1		0. 2	,,,,,,,	71 /. 7771 77	0. 7	
Į	22	l		9. j			0.1		0. 2	}		0. 2	
. į	23 24			Q. 1 Q. 1		<i>.</i>	0. 1 0. 2		0. 2			0, 2 0, 2	·
i	24		786, 32	0. I		808. 10	0. 2		0. 2	804, 95	805.71		804. 98
İ	26			0.1			0. 2		0. 2			0. 2	
1	17			0. L		806, 20	0. 2 0. 2	804,75	0. 2 0. 2			- 0. 2	3. 0 804. 76
į	28 19		788.07	0. I 0. I		700.10	V. 5.	941, 17	V- E.J	· · · · · · · · · · · · · · · · · · ·	805, 60	0.1	***************************************
1			127.21		ſ							·	

Table E.2-4 Reservoir-Rainfall (2/6)

1	1968			1969	1.11.1	Γ	1970			i	971	197	2			1974
	R W.L.		R	W.L.	Qs Qv	R	W.L.	Qs	Qv	R	ዝ.ኒ.	R W.1	. Qs	Qv	R	W.L
1.1		0. I		-	0.2				0.1					0.2		
		0.1			0. 2				0. 1 0. 1			} .		0.2		7.5
3 4	i, 9	0, 1 0, 1	1		. 0.5	1			0. i			} :		0. 2		1.
	785, 60	0.1		805.08	0. I		804.68		0. 2		804.74	805.3		0.2		804.36
1 1		0. i 0. i			0.2				0. 2					0. 2		, i
8		0.1			0.1				0.1					0.2		
9		0, 1 0, J		ant 99	6 1		807.38		0.2		804 54	805,0)	0. Z		#64 fo
10.		······································	135.7.	997.77.					9.4					0.2	5. 4	- 5551 55
12	* .	0.1			0. 1	1			0.2	ļ.		4		0.1		
13	-:	0. l	Ì		0. I 0. I				0. ž 0. 2	1 .				0.2	l	
15	784, 47	0. I		805. 70	131 1-	Į	804.00		0.1	1	804.11		ŧ	0. 2		803, 18
16					-	•			0.2		13 T 3	[0.2	0.1	
[7 [8	10	0. ł 0. ł	1		0. i 0. i	!			0. 2			1		0. 2		
19	1. 0 	0.1			0. 1	:1:			0. 2		5 . 7			0. L		203 58
20.	784, 16	9. J.	ļ	503.47			593. 75.		0.1		9921 37.	\$93.9	L	0. 2		892,58
21	4	0. l 0. l	1		0.				0. 1	ı	2.	0.1		0. 2		
23		0, 1	ĺ		-	.1			0. 2 0. 2					0. ž 0. ž		
21 25	783, 62	Q. I		805, 12	0. 2 0. 2		803, 78		0. 2		803. 88	803.40)	0. 2		801.82
26	103.01	0.1			0. 7	:	,		0. 1			}		0. L	Ì	-
27	1	0. I	1		0. : 0. :				0. 1 0. 2			. `:		0.2		
28		0. l 0. l	1		,				0.1			1 .		0.2		
10		A 1	1		-	1		•	0. 2]	_	-	1	800. 88
31	783, 20		3.0	804.84	0. i		803. 20		0, 2 0, 2		802. 9 <u>4</u>	1		0. 2	<u> </u>	800. 68
4, 1	11 11 1	0. l 0. l			0. 1				0. 2			4.3		0. I 6. 1		
		0.1	1	•	-	1			0. 2			1		0.1	1.6	b.
!	1.0	0.1	ĺ	104. 17	~		802. 61		0.1	1. \$	80Z, 50	803.10) -	0, 2 0, 2		800.02
5	16, 0 782, 35 17, 5	0 I 0 I										, , ,		0.7	0. 1	
1	1.1	-	1		q.;				Q, Z 0, Z	0.2				0. 2 0. 2		
8 9		0, 1 0, 1	1	•	0. 0											i i
10		0. J	l	801.32	0.	<u>.</u>	\$02,02		0. 2		800, 69	802. J	.	0. Z	. 9, 5	199.00
11		0. J. 0. J.			0. : 0. :	}			0. 2 0. 1	1		0.3		0. 7		
12		0. i 0. i	i		. 	١.			0.1	1		[.		0. 2	İ	1
. 11		0.1			0.	2 25. 5			0. l		400.44	801.5		0. Z 0. Z	1	198. 64
15	782, 30	0, 1 0, 1		801.80	0. i	2 49.9 2 7 2	6 801. 78 9		0. I 0. 7		80V. 4Z	801.3	•	0.1		130.01
										1		1		0.3		
18		0. 2	i	*	0.	2			Į. 3		-	2.4		0, 3		
19		0.2	33.3	803 PA	0. a	3	198, 96		1. 3		800.00	2. 4 6. 9 801. 1	<u> </u>	0.3	l	797, 10
29. 21	780, 48		111.7.	. 777175.		\$		• • • • • •	į. į	1		1		0.3	1	
22		0. 7	1		v.	4			i. 8	1				0. 3 0. 1	-	
23		0. 1 Q. (7.1		0.				1. 2					0.3		
25	779.00	0.1] "	801.90	0. 1. 0.	3	795. 66		1. 3	:]	799. 5€	890. (4	0.3 0.3	0. 2	196, 10
Z6					0. 1.	3			1.1 			1		0. 3		
27		0. I 0. I							i. i					0. 1		: "
29		0. I	1		1.	3	102 10		1.1		700 10	799.	ı Á	0. 3 0. L		195.06
30	L	0, 1	J	197.87			192. [0		1.		110. /4	Li	м			177.40

Table E.2-4 Reservoir-Rainfall (3/6)

		1968			ſ	1969	<u> </u>		1970		I	1971	Γ	1972			1	1974
	, R		Qs	Qv	n	W.L.	na n	ם וי		Qs Qv			. p .	W.L.		Oυ	R '	
5, 1			43	0.1			40 4	<u>' -"</u>	д.Б.	1, i	- <u>``</u>	п.р.	1.1	и.Б.	ųo_	0. 2	 `` -	11.00
,	2.4	 .		0. 1			1.	0. 2		0.5			0.3		• •	0. 2		
3				0. 1			1.	2		0.2						0. 3	İ	
4	:			0, 6			Į.			, 0.1			١			0.3		
	14.0					798. 10	1. 1.		190, 45	0: 2 0: 3		798, 27	2.5			0.3	i	194.00
: 1	11.0				1		ί.			0.3			l . "· °				17. 7	1 .
è							i,		•	0. 3						0. \$		
9							Į.				3. :	!	1			0.3		204:10
19.]8.0 10.0			•••••		794, 98	<u>ļ</u> ,		189,58	0. 2 0. 2	ļ	197.08.	3.1	. 191.39		0.3	. 25.2.	793, 10
12	2.5						i.			0. 2	1	-	9 0			0.3		
13	1.7				ļ		l.	1 8.1		0.2	19.0)	0. 3			0.3		
11 [1.			. 0. 2	6. 1	195.28				0.3		193. 10
15 16	9. 4					191.32			788, 83	0.2) 140.28 		798.10		0.4	23. 8	143. 10
17	6.0						1.1				4.		38.4			0.3	58. 1	•
. 10	8.0				\		١.				12.		0.4			0.4		
19	111						I.	0	212.32	0. 2] I.:	1					29. 3	
20. 21	8.0					188,66			789, 10	0. i 0. i	}	. 194, 94		135.75		. y. s.	20.8	194,52
22	1.0				l		0.			0. 1	13.	2	1. 1			0.4	100. 7	196. 48
23	9.5				l		Q.			Q. 1	1] 0,3			0.4	0.7	-
21	1.5					*** **	0.			0.1	l	191,58		194. (8		0.4	10.8	197.72
25 26	1.0				•	186.13	C.		189, 16	0.1	}	(81'24	3 3	134.48		0.4		131.14
27	1.0					786.00	o.			0. [0.4		
28	5. 5						0.			0. \$			0.5			0.4		
29	20.0					787. 60	0. 0.			0. 5 0. 5		191.06	4.3	٠,		0.4	ļ	
30 31	15. 0 23. 0					186, 98	Ö.		788. 13			791.58		792, 78		0. 4		797, 14
		00.55			13.8	181, 20	O.	1.1		0. 1	4.8	3	1.1	110111		-		-
2							1.1	7		Q. 1			1.2			_	2. 4 15. 3	
3	10.0 5.0					193, 12	I. 1.			Q. L	4.4		1			-	13.3	
4 5		01. 17				193, 48	1.		188, 50	0.1	!	191.48	1	191.94		_	1	
6					93.0		1.	2		0.1	1	791, 48	16.8			-	l	
1						197. 82	1.	. !								-		
8 [21. 5				2.0		l.: l.	11		0. l 0. l			1.5	793. 80		_	1	
ا ۋر	5.5	04. 28				807, 30		۱ ' ' [788,90	0.1		790, 80				-	l	
11]	3.5 8	04, 27			6, 0	805.35	1.	Π.			28.	1	1.8					-
12	12.0 8							1 10.3 1 30.6		0. i 0. i	5.1					-	0.6	
13 24		07, 70 07, \$0	55 33		10.0	806. 25					9.					-	1.2	
is		07. 36				807, 50			790, 53			791.34				-	5. 3	
16		07.06	1			807.50	14 L			0.5	١.	_	0.3	1 -			10.6	
17		07.08	1		5.0	807.40	24 L				2.1)	١,٠			- 0 I	4.6 7.8	
18		07.08 07.03	1		1 3	807. 60 801. 30	44 I. 15 1.			0, 3 8, 3			["."			9.1		
20	14.3		3				. js . j.		790, 60		l	788.34	ļ	. 195, 47.		0.3		
21	59.0	07. 48	31		5. 5	807.18	1 L	1, 1		Q. S		-	12.9			0.3		
22		07. 18	7			807.10	1 1.			0. 5 0. 5			15. 8			0. 3 0. 3	18.5 17.4	
23) 24		07, 10 07, 04	j		a. 5	807.08 807.00	. 2 , I. L			0. 5 0. 5			, , , , ,			0. 1		
25		07.00	•		8. 3	896. 67	i.		789.15	0.5			0.4	194, 98		0. 1	0.7	
25				į	1.3	801.18	1 1.	(0, 5	}		}			0. 1	1	
27		08.65				807.46	29 1.			0.1						Q. I Q. j	18. 1 1. t	
28 29	9. 8 1. 5				21.1	807. [6 801. 18	1 1.			0. l 0. t	1					0.1	" '	
30		05, 88		i	7.0	501, 18 807, 14	5).		789.88_	0.1	[L	794, 68		0, 2	2,0	

Table E.2-4 Reservoir-Rainfall (4/6)

	1966 R W.L. 8.8 2.4 11.4 804.87 2.0 0.9.803,87. 5.5 802.64 890.97 198.25 1.1 196.28 2.0 198.37 1.5 2.0 1.9.804.37 2.3 21.1 805.85 0.5 2.0 22.0 406.44		1969			-ĭ970		ı · · i	571		1972		[***1574**	٦,
	R W.L.	Os Ov	1969 R W.L	Qs Qv	R	W.L	Qs Qv	R	W.L.	R	W.L.	Qs Qv	R W.	L
1. 1			807.08	2 1.1	37.2		0.1			·		0. 2		٦
1			16.8 801.08	1 1.1	1.5		, , -				794, 38	0. 2		
3	8,8		801.01	1 1.1	1.1		. · -	l	· \			0.2		
1 5	2. 4 11 4 404 67		2.4 607.14	5 3.4	0.4	791.56					-	0.2		-
- 4	11.1 000.0	1 1	3.0 807.07	i i.i	i.i		0. 1	4				0, 2		:
1		•	807.00	1.1			0.1	١.,				0. 2		. 1
6	7. 0		5 3	1.1			0.1	9.1			792.88	0.2		
10	0, 8, 803, 87		10.5 805.74		 	192.30	0.1	1.8				0.2		;
11		- 6 W		1. (١.,		1.0					0. 2	1.5	
12	5. 5		3.8	1.1	14.7		V, L	4.0				0. 2		
j∉		٠.	""	; i.i	7. 3		0.1	1.5				0.2		
15	802.61		806, 10	1.4	1. 1	793, 78	0.1	1.4				0. 2		
15			}	1.4	1 4.6 1 6 E		0.1	4 6				0. 2	1 .	
16		0. 9		i. i	0. 2		0. i	0, 1				0, 2		
19	1 11 111	0. 9		1.4	7. 9		9. 1	Ι΄.		١		0. 2		·
50	299,97		1.1.5 \$25.51.		13.9.	. 195. 10.	10			-7.		0.2		
22		0.9		1.1			0. i			0.1				
23	. :	0. 9	8.6	1.1	9.8		0.1			8.9	730.14	-		
24	120 05	0. 9	*02.00	1.4	1	101 44	0. L	1.0	·	9.9		0.2		
26	144.00	0.9	803,00	1. 3	0.6	177.11	0.1	3.2		111		0. 2	1.	
27	198. 25	0. 9	· .	1. 3	37. 5		0.1	2. 2		l		0. 2		
28		0. 3		1. 3	38, 6	799, 40	0.1			1.1		0. 2		
10	1. 1	0,1	1	1.1	١,,	200. 12	8.1	0.8		0.6	791, 34	0. 2		
31	198. 28	Q. 3	10.3 800.34	1.3	12. 2	803.05	0.1			0.4		0, ż		
8. 1	2. 0	0. 3	7. 1	1.1	1.4	803, 91	0.9	15. 9		1				
2		0.1	1.	1.3	1. 3	805. 26	1,4	.,				0. I		٠
ě		0. 3	8.5	1.1	1.0		i. i	3. 9	,			0. 2		٠.
5	798. 37	0. 3	198.34	1. 2	0.8	604.88	1.4	1		1	792,00	0. 1	0.4	
6		0. 3	19.0	1.2	0. 9		1.4	١,,,	788 22	ļ		0. 2		
		0. 3	797. 30	1. 2	12.1		1.1	1.6	100.64	2.2		0. 2	0.8	
9	1. 3	0, 3	\$2. \$	1. 2	4, 1		j. ₹			0.1		0.1		,
	2, 3, 798, 48	0, 1	30, 8, 198, 23,			804, 10	1.5		189, 99.	10.5	, 191, 17.	. 0.1	0, 1	
11	0. 6 10g 13	0 3 0.2	17.3	3. £,	25.0		1.4	1	•			0. 1		
13	11.0 800.16	0, 2	0.5	1. 3			1.4			1		4. A /T		
14		-	5.3	1. 3		101 42	1.4		750 17		702 10	0.	0.2	
15	802. 28	_	27. 1 199. 10	1.1	0.5	804.88	1.4		103. 31	'' '	172.49	0.1	V. 1	
17	2. 0 803. 27	_	0.1	1.4	1.9	•	i i			8.5		0.	1.5	
18		-	6.4 804.47	1. 4	2.1		1.4	1.0)			0. i		
19	3. 0 1. 0. 804 33	_	0.7	- 1.4		803 34	1.4	5. L	789 80	1.	783, 30	V. G.	1 0.5	
						. 777: 79.	` i. i	2. 2	;¥f2¥f. !	ļ	. 227138	0.	۱ ۲۰۰۰	
22	2. 3		21.0 805. 67	1.4			J. \$	l		1		0.	!	
23			8.5 807.01	1 1.4	l		1.3	11.1	790.44	100		0.		
25	21, 1 805, 85	9. I	18.5 807.1A	22 1.4	5.0	801. 24	1, 3	26.	792.46	'	193.75	0,	il .	
28	0, 5	0. 1	807. 22	10 1.4	11. 9	801.06	1.3	14. 6	3	.		0,	1 48.8	
27		0.1	1. 7 801. 18	7 1.4	1:5	403 PA	1.3	10.4	797.13	7.3	l	-	1.8	
19		0. 2	9.0 801.18	0 1.4 7 1.4	18. 2	80J. VQ	V. 9 0. 9	13.8	799.26	12.8	i . I	-	10. 3	
30	1.0	0, 2	601.10	1 1 (11.7	804. 62	0.9	39. 9)		: 			
31	22.0 808.44	0, 2	J 0.6 807,04	1 1.4	27.7	805.46	1. (41.4	803.48	19.	794, 40	!	0.8	_

Table E.2-4 Reservoir-Rainfall (5/6)

										· · · · · · · · · · · · · · · · · · ·				227						
		1968				1969				1970				971	_	1972	_			374
	R	W.L.	Qs	Q۷		W.L.	Qs	Qv		W.L.	Qs	Qv	R	W.L.	R	W.L.	аŞ	Qv	R	W.L
ī. T	7.3 80			0.1		807.00		1.4	0. 3			1.4						-	0.8	-
2	9. 3 2. 5			0.2		805.88		1.4	1.0			1.4				194. 15		-	2.4	
1	Z , 3			1		801. 50 8 01. 55	33 18	1.4	0,4			1.4			1.3				4. 4	
3		4	:			801.26	13	üä		805, 32		i.i				795, 98		-		
- i l	80	1,00	- 1		1.5	801. 20	8	1.4	1.2			1. €			13.1			-	ŀ	
7	7.0 50	7.04	. 1			807. 24	H		11.7	805.05		1.4	-			197.00		-	7. 9	
	11.7 80			i -		801.22	10	1.4				1.4						-	10.8	
	1. 3 80 40		- 1			801.35 807.38	6	I.t	in 7	\$05.25		1,4 .1,4.				.791,74		_	5. 9 1. 1	
. JQ	80	7, 19 1. 03	··ř·		14. 5	807. 13	∵{:-	17	14.7	808.30		117			·····	. 2711 75		- '	3. (
iż				- 1	ĺ	80 108	2	î. ŧ			,	1.4						-	25. 3	
13	3.1			_		807.04	1	1. ≰				1.4			ļ			0. 2	29.8	
ш				-				1.4		505, 52		1.4						0, ì	19.7	
15	05	6, 15	٠.			896, 80		1.4		805. 82		1.4				198. 22		-	ł	
15	14.6 8.0 80		÷) J. U			1.4	•			1.4			16.6			_	1	
18	17.0			_	6.6			1.4		804. 82		1,4			''''			~	8.0	
19	15,0 80	6. 90			16.6	1. 3.4		1. ₹	27. 3			1.4	l		0.1			0, 1	33. 2	
10	7, 0, 80	7, 93			23. 5.	505,08		1. ₹	1.5	805, 40	٠.	1.4			. 0, 9	190, 66			\$3, 1	
21	9. 4 80	I. 13	8,	-		101. 28	[9	1.4	45. 5			1, 1						0, 1 0, 1	24. 3	
22	12. 5 80			~	28. 6	891. 36				801. 24 801. 12	11	1.4			}			0. 1	0. i 23. 3	
23	13.0 80			_	14.3	601.30 601.20	21	1.4	21.4	807. 44	28	1.4	1)			_	0.3	
25	4, 6 80	7. 20	8			807. 12		1.4		807. 18	ĭ	1.4				799.01		0.1	1.5	
26	4,0 80	7 14	R.	-	l	891.06		1.4		807.03	i	1.4	1			:		0. i	14.7	
11	4, 5 80	7. 17	7	-		805.98				807.01	2	1.3			0.9			0. 1	25. 3	
28		7. 09	3							807.52	35	1.4				199. 17		0. Į	١.,	
29	1, 1 50		İ	- - ,-		806. 92				808.00	94 83	1. 4	_	_		199, 92		-	2. 1	_
30	5. 2 80 2. 5 80		5	0.1	10.3	807.01 807.04	<u> </u>	1.4		807, 92 807, 36	20	1.4				177:.26				
٠ ; ا	1, 0 80		i	0.1			Ö			807. 5D	33	ï. C			5.9			-	ĺ	
3 1	2, 2 80		i							807. 28	15	1.4	1		ì	802.86			1	
4	2. 8 80		2	0.1	1.2				15. 2	801. 2Z	9	1.4			5.9			-		
5	* 80		1	0. 1	7. 8	607.30	15	1.4		807. 10	3	1.4	ľ			804.22		-		
6	80	7. 00		0. 1		801.50				807. 12	4	1. {	ļ		0. 9 13. 8			_		
!				0. L 0. L	6. 1	807.70 807.51	55 37	1.4	J. (807. 12 807. 14	4	1.4	l		13.0			_	1	
8 9				0. L		897.36	20	1.4	15.3	807.01	ĭ	1.4	ŀ]			-		
10	50	8. 10					•	1.4		807, 14	5	1.4	l		l	806.42			l	
ii	11.0			0. 1	0.8	807.30				807.10	3	1.4	į .		l			0. I		
12				U. 1	1.1	601.31	16		0.6	101.60		1.4	ì		0.1			Q. L	1	
13	86	5. 21		0.1	1.1		15	1.4				1.4 1.4				807.04	1	_	1	
15	2.8			0.1			10 5		21	805, 10		1.1				807.08	ž	_	1	
18	2. 8 1. 0 80	4. 80		0.5			j	14				1.4				801. 20	8	-	l	
iil	2. 3			0.2	11.3		1	1,4				1.4	1			807.40	24	-	İ	
18	23.0 80	6. 10		0.7	1.1	807. 24	11	1.4	9. 3			1.4				807. 20	. 8	-		
19	10. 6 80					807.84		4.4	6. 1			1.4				807. 24	11	-		
20	51,4.40							44.	.54.	806.80		1.4		• • • • • • •		807.28	[3]]	Ţ.	}	
21 22		7, 15 7. 06	5	0. I 0. I		807. L9 807. 28		1.4	1.4			1.4	}			807.34	18	-	}	
23	80		1	0.1		801. LT	14	1.4	l "'			1.1	1		٠ · · · ا	807. 22	10	-	1	
26	11.5 80		2	0. 1		807. 25	12	1.4	1.0			1.4				807. 17	7	-	l	
25	53, 4 80		85	0. I		807.19	8	1. 4	,			1.4				807.14	5	-		
26	0.6 80		19	0. I		80T. L6	6	1.4				1.4	1		1	807.12	ţ	~		
21		1. 20	8	0. 1	1.8	891, 22	10	1.4	1.1			1.4	1			807.11 807.10	3	_	l	
28		7. [4	5	0. l 0. i	٠,,	807. 19 807. 16	8	1.4	3. 1 3. 7			1, (l		3.1	801.10 801.09	3	-		
29		7. 08 7. 04	, ,	0. i	V. 1	807. 15		- 1. 1 -]. 4	3. 1			1.4				801.09	3	-		
30 l					•	807.12	*	1.4	32.0						1	801.08				

Table E.2-4 Reservoir-Rainfall (6/6)

	1968				1969			1970				1971	1972			74
	R W.L.	Qs	Q٧	R	W.L.	Qs Q	v R	W.L.	Qs	Q٧	R	8.1	R W.L.	Qs Qv	R	W.
1. 1		•			807.08	2 1.4				1.1		807, 12	2.0 897.12	· - '	2. 1	_
2	807, 03 18, 3, 807, 36 2	l n	0.1		807.04 807.00	L 1.4		807.06 807.04	1		3.5	807, 12	3. 3 807. 09		0.4	. 1
1	807.23		-		50 r. 00	1.1		807.00	u t	1.4	15.5		807.09 807.07	, -		
5	16. 6 807. 26 1		0.7		808.80	1.3		805.89		i.i.	4	807 70	807.06	i -	ĺ	
8	**********		0.7			1 1	1			ii i			807.06	41 -		
-1	1. 3. 807. 12		0.1	4, §		1.4				1.1			801, 05	1 -		
8	807. Q8 807. Q4	2	0.7	0.4		1.4			٠.	1.4	:	+ 7 +	1.0 807.08 807.06	3 -]	1
. 10	3, 4, 607, 03		0.7		805,80			805, 19		1.4		107.11	807.08	1 -		
~iii]	807.00	f	0.7			1. (0.7			1.4	• • • • • •	_4711.64-	0.5 807.06	···{·····	ò. i	
12	2, 3		0.7			1.4	3. L						801,07	2 -	•	
13	806.89		0.1	٠,		1.4				1.4	0, 1		807.07		1.5	
Щ	807.08	2	-		804. 19			*** **				807, 09	801.06	! -		
15	807, 10	3			801.17	1.4		804.25		1.4		807, 09	807.08 801.08			
17	807.12 2.0 807.12	100		1		1. 4				ili.		i.	0.8 807.12			
ia l	807.12	ì i	-	2. 5		1.4				1.4		i	407 10	3 -	0, 7	
19	1. 0 407. 12	4	- 1	9.9		1.3				1. 3	1		807.08	2 -	1.0	٠
30.	107.12	<u> </u>		.0.4.	802,65			802, 35		1.3		.807.05	897.97			
81	2. 5 807, 12	∮ ::	. <u>.</u> .			1.3				1.3	8.1		807.05	1 -	9. 6	. 5
22	807, 12 806, 80	4 .	0.1			I. 3 I. 3		** *		1.3	3.4		807.06 807.06		0.8	
21	500.50		0. I				0.7			1.3	0.1		807.05		0.1	
25	808,00		0.7		801.07			800, 22		1.3		807.05		i -	5. 8	
28			0.7			0. 2	1.			1. 3			801.05	1 -	Ì	
27	1,479				801.46	0. 2				0, 6	ŀ		807.00	0. 2		
28			0. 1	0.7		0, 1		1.1		0.,6			807, 60			
29			0.2		*** **		5. 1	199.09		0.3		807.04	806. 95	0. 1 0. 2		
30	2, 2, 505, 10 - 805, 10		0. Z 0. Z	1.3	801.54	0. Z 0. Z		799.02		0.3	 	801.04	540.13	0. 2		
2			٠.١	j. 0		0, 2		*****		0. 2	1		·	0. 2		
3						0. 2	1			0.1	1.8			0. 1		
- 4			ı			0. 3				9. 2				0. 2	ł	
5					802.67	0, 3		799.49		0. 2	0.1	807.05	898, \$ 0	0. 2	İ	٠.
			٠			0.3	0.5			-				0, 2 0, 2		
			- [0.3				_	·			0. 2		
از					802.14	0.5				0. 2				0. 2	0.1	
ا ور					802.64			800.07		0. 2		807,03	0, 1, 806, 70	0.1		
11						0. 5	1.			0. 2	·			0. 2		
12	•		- 1			0. \$				0. 1	l			0. 2		
13					802. 24		11.1			0. l	1			0. 2 0. 2		
15			1		802,60	0. l 0. z		800.96		0.1		807.01	806, 47	0. 2		
;'			- 1		50,47 00	0. 2		500. 10		0. 1		VV VI		G. 2		
ii			- 1			n 2	1 10			0.1				0. 2		
18			1			9. 2	0.1			0. l				9. 1		
19			1			0.2	1			0.1				0. 2		
20					893,90			302, 42		0. I		807.91	806, 23	0. 2 0. 2	0, 4	
21						0. Z 0. ž	2			0. 1	1.5			0. 2 0. 2	3.3	
23			- 1			0. 2				0. 1	۳,			0.2	V V	
ii						0.1				0. 1	8.4			-		
25					803.44	0. t		803. 52		0. 1	1	807. 01	808.25	i		
26						0. 1				0. 1	ĺ			0. 2	1	
27						0. }								0. 2		
28			ĺ	•		0. 1 0. 1	1			0. 1 0. 1	l			0. 2 0. 2	ĺ	
29 30	•		- 1			V. 3 Q. 1				0. 1				0. 2 0. 2		
			- 1		803.92	0.1	,	604. 43		0. 1	1	807.02	808.05			

Table E.2-5 Record of Large Inflow/Rainfall (1/3)

		R	W. L	V					R	W. L	V	
68	6, 11	3.5	804. 27	10, 756		} {	72	6. 5		791. 94	3, 829	
	12				0.5*6*1.4H = 15			6	16.8		?	:
	13	42.6	807.70	13, 165	0.5(6+55)24H =2635	l: l:		7	65.6	?	?	
[.	7.7			,,				8		793, 80		
		88.1		2.409	+2, 650 =5, 059	H						1
									85.6		785	
69.	6. 1	13.6	787. 28	690)	ì		~~~~~	1-3333-			h
	2		789. 46	1, 348		ļ	72.	9. 30	4.9	799, 92	7,816	
	- 3		793.12	4, 327				10. 1	3.0		8, 118	
	4		794.00	4, 698		1		2		802.02	9, 231	
	5			5, 383		-		3	*.•	802.86	9, 801	ļ
	6		796. 96	6, 194	!			4	5 9	803.44		<u> </u>
	7		797.82	6, 665	1		-	5		804. 22		1
	8		798. 49	7, 033	!			6	0.9		11, 199	!
	9		798. 97		<u>į</u>	Ιİ		7	13.8		11, 133	į
		!				l I.		,	13.0	000.41	11, 512	
	10		802. 38	-	<u>.</u>				,,,		0 256	į
	11	0.0	805. 35	11,490					. 49. 1.		7, 190	
		1		10 000		1 1	00		۱ ۵	300 00	c 024	
		249.3		Tô' khố		1 1		6. 11. 06	7		6, 874	į
				40.600	1 · · · · · · · · · · · · · · · · · · ·			11. 18		798.00	n 446	
69.	6. 14			12, 108				6. 12	?	798.70	7, 148	i
	15				0.5*33*10.6 = 630				_	800. 20		i
	16	2.0	807.60	13, 086	0.5(33+44)24 =3326			6. 13	?	803.80	10, 439	
									ļ .	806.50		t
		22.0		978	+3, 956 =4, 934	1 1		8. 14	?	807.40	12, 927	0. 5*24*11. 6H = 501
				•								i I
70	4.14		(801.8)						l		6, 053	+501 =6,554
	15	49.9	801.78		,							i
	16		(801.2)			1	83	6. 17		779.14	447	
		ŀ				L		18	74.0	779.96	536	i L
		75.4		0				19	31.9	781.80	886	; 1
								20	7.5	782.34	989	; ;
70	9, 19	27. 3	(805.0)	11, 253				21	25.0	783.48	1, 208	•
	20			11, 524				22		783.78	1, 266	1 1 1
	21				0.5 + 53 + 8 = 763							
		1	,			ll			164. 2		819	
		74.3		1.896	+763 =2,659	<u> </u>						
		1						:				}
70	9. 27	16.6	807. 07	12, 666								
' "	28				0.5(2+35)24 = 1598							
	29	33 4	808 00	13 403	0.5(35+94)24 =5573							
	6.3	"""	000.00	10, 300	A. 0 (00.02) DZ 0010			į				
		74.6		737	+7, 171 =7, 908	\ \					ŀ	<u> </u> -
		17.0		101		, r			L			<u> </u>

Table E.2-5 Record of Large Inflow/Rainfall (2/3)

	<u></u>	155 1					<u>-</u> -	[·	···			
	R	W. L	V				1			. •	R	W. L	, V	
				 			1		1 :-			. :		
83. 9.28.06	9.5 7	193. 56	4, 512					85.	10. 29.	06		805. 67 805. 64	11,708	
28.18	30.7 7	794, 68	4, 985					1	29.	18		805. 64	11,687	
9. 29	7.1 7	195. 94	5, 635		;			1	10, 30		5. 2	807. 20	12, 769	
	14.2 7		6,063				1	j				807. 30		
9, 30	19.9 7	98.88	7, 246				1.	100	10.31		1000	807. 30	12, 848	
	9.0 7	199.92	7,816						*					1
10. 1	1,8 8	00.98	8, 525	 -						.:	6.8		1, 140	
	15.4 8	01.42	8,824					[1
10. 2	0.7 8	301. 97	9, 197					.87	6, 26,	06	7.1	792.70	4, 149	
		302.12	9, 299						26.			792, 90	4, 234	
10. 3	2.0 8	302.43	9, 509					ł	6. 27		54.1	795.40	5, 339	
ł	0.3 8		9,760			S. 1. 5	1					797.10	6, 271	
10. 4	3.7 8		10, 574				.		6, 28			797. 60	6, 545	land the second
	5.0 8		10, 995					1				797.90	6, 709	
10. 5	0.3 8		11, 104					ĺ	6. 29		2. 2	798. 10	6,819	
			·				1	į (ĺ	798, 28		
	119.6		6, 592		•		1		6.30		0.4	798. 50	7,038	<u>.</u>
	-22312						-	•						
84 7. 5	6.9 7	193, 72									67.8		2, 889	
6		193.66	4, 555					ļ						<u> </u>
7		93.84	4,630					87	9. 20		84.9	806, 90	12, 542	•
8	53.9 7		5, 339											0.5 * 67 * 21.7 = 2614
9		97. 18	6, 315					ł			***	(807. 3)		
10	4.5 7		6, 380								1.0		1.0	[
•			,,	·				100		1.2	119.4		703	+2,614 =3,317
	144.8		1, 825				ŀ	1		•••	, ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,			
	. 2001 0000						-	88	5. 10			(795.6)		
84. 9. 1.06	9.6 7	195, 70	5, 504					l.	5.15			795, 30		
1, 18		95. 80	5, 558		٠				5. 16	1		795. 40		:
9. 2	38. 6 7		7. 202				•							!
		199. 20	7, 422				1				85.0			
9. 3		100. 10	7, 928				1							
		01.70	9,014											:
9. 4	1.1 8		9, 556					-						!
-		302, 90	9, 828	!			1							!
9. 5		303. 28	10,086				1 -							!
				ļ. !										i !
	72.4		4, 582				}	1				•		
			.,	1			•	1			v .			!
			1				1							
			!				1.	1						1
		 					٦	L		1				i

Table E.2-5 Record of Large Inflow/Rainfall (3/3)

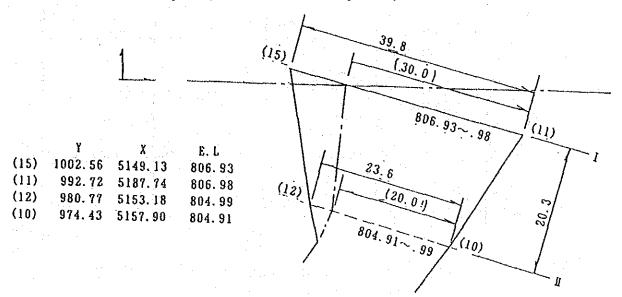
	:	R	W. L	V	
88	6. 9.06		796. 24	5, 800	
	9. 18	1.6		,,,,,,] !
	6. 10	11. 9	796. 40	5, 887	!
	***		796.80	6, 106	
	6. 11	17.8	797.40	6, 435	! !
	4, 11	2. 3	797.60	6, 545	
	6. 12	18. 3	798. 20	6,873	1
		2. 1	798.40	6, 983	
	6. 13	33. 6	800.60	8, 267	l !
		8.0	801.10	8,606	
	6. 14	0.5	801.80	9,081	
		1.0	802. 20	9, 353	1
	6. 15	10.1	802.85	9, 794	1
	*****		803. 20	10,031	
	6. 16		803, 40	10, 167	
		17.8	803, 70	10,371	
	6. 17	15.8	803.86	10, 479	[]
	18	2. 2	804.30	10,778	[
	19	11.8	804.70	11,049	} 1
	20	19. 9	804.90	11, 185	[]
	21	0.3	805.20	11, 389	† ! !
	22	11.4	805.60	11,660	{ 1 •
	23	12.5	806.70	12, 406]]]
					1 1
		199.1	· 	6,606	
88	7. 1	60. 2	806.15	12,033	 - -
• •	2	28. 7	807. 20		0.5*8*5.2 = 21
	3	6. 6	807.60		0.5(8+44)24 =2246
	4		(807. 2)		
		95.5		1,053	+2, 267 =3, 320
					;
88.	8. 11. 06	3. 9		10, 405	! }
	11. 18	1.9	803.80	10, 439	;
	8. 12		804. 20	10,710	•]
		1. 3	804.90	11, 185	i
	8. 13	0.4		12, 474	
		0. 2		12, 689	
	8. 14		807. 20		0. 5*8*16. 4H = 236
		2. 9	807. 20	12, 769	0.5/0/45\01.00/
	8. 15	0.1	807. 30	12,848	0.5(8+15)24 =994
		3. 1	807. 14		
	· ·	33. 1		2, 443	+1, 230 =3, 673

Table E.2-6 Rapid Fall of Water Level.

		W. L	V	Q	Qv	
		H. L		¥	4¥	
:				· 		
69.	4. 30	799.87	7,789	0.0	1.0	
	5. 5	798. 10	6, 819	2. 3	1.0	
	J. U		0,010	4.0	1. 2	
	5. 10	794. 98	5, 112			
	5. 15	791. 52	2 651	3.4	1.1	
	0. 10	131.02	9, 0,01	2. 4	1. 0	
	5. 20	788.66	2, 605			1 1 1
					-	1
4					•	!
70	4. 10	802.02	9, 231			
	4. 15	801. 78	. 0 000	0.4	0. 2	
	4. 10	801.78	9, 000	4.1	1. 1	1
	4. 20	798.96	7, 290		٠.	! ! [
	4.08	705 66	 E 100	4. 2	1. 2	1
	4. 25	795.66	5, 482	3. 7	1.1	i !
	4. 30	792. 10	3, 896			
	r r	700 45		1.6	0.5	<u>i</u>
	5. 5	790.45	3, 200	-		
82	6 OE	000 00	10 160			
02	6. 25	806.35	12, 109	2. 8	?	i !
	6. 30	804.60	10, 981	•		1 1 1
	n .	000 00	0.401	3. 5	?	t .
	7. 5	802. 36	9, 401	3. 9	?	į
	7. 10	799.84	7,772		. •	
	n 4°	000 50	A F04	2. 9	.?.	
	7. 15	797.52	6, 501	2. 4	?	
	7. 20	795. 62	5. 460		•	1

(2) Spillway

Outlet Capacity of the Present Spillway



The water flow has the critical depth at the section I shown in the figure, and becomes a supercritical flow from that point.

Since the plain of the spillway is reduced rapidly, the hydraulic calculations are conducted using the narrower section shown by the broken line in the figure.

The depth of the incoming section can be obtained as follows:

hr = hc =
$$\sqrt[3]{Q^2/gB^2}$$

g = 9.8, B = 30.0
hc = 0.0484 $Q^{2/3}$
Q = 93.91 hc^{3/2}

Table E.2-7 Outlet Capacity of the Spillway

ħ	Q	h	Q -	h	Q -
P	m3/s	m	m3/s	m	m3/s
0.01	0.1	0.25	11.7	1. 1	108.3
0.02	0. 3	0.30	15. 4	1. 2	123.5
0.03	0.5	0.35	19.4	1.3	139. 2
0, 04	0.8	0.40	23.8	1.4	155.6
0.05	1.1	0.45	28.4	1.5	172.5
0.06	1.4	0.50	33. 2	1.6	190.1
0.08	2. 1	0.60	43.6	1.7	208. 2
0.10	3.0	0.70	55.0	1.8	226.8
0.12	3.9	0.80	67. 2	1.9	246.0
0.14	4. 9	0.90	80. 2	2. 0	265.6
0.16	6.0	1.00	93. 9	2. 2	306.5
0.18	7.2				
0. 20	8.4				

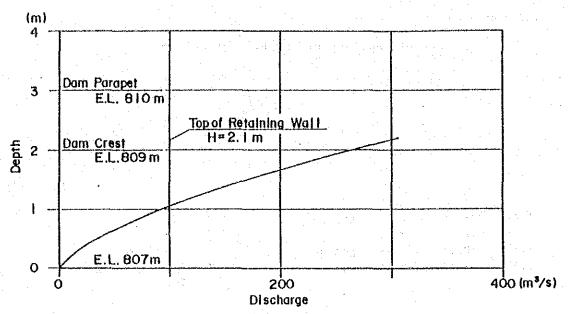


Fig. E.2-5 Discharge Capacity of the Spillway

The volume of flowing water does not flow over both the dam crest and the spillway is around 260 m3/s.

The following equation is built between section I and II.

 $4h + hI + VI^{2}/2g = hII + VII^{2}/2g + n^{2} \cdot L \cdot V^{2}/(R^{4/3} \cdot 2g)$

Table E.2-8 Flow Description of the Spillway

	up st	ream		4, 4	down	stream		
Q m3/s	lı m.	A m2	R	v m/s	lı m	A m2	R	v m/s
5	0. 142	4. 26	0. 141	1. 174	0.039	0.78	0.039	6.410
10	0. 225	6. 75	0. 222	i. 481	0.076	1. 52	0.075	6. 579
25	0.414	12.41	0. 403	2.015	0. 181	3. 62	0.178	6. 906
50	0.657	19.71	0. 629	2. 537	0. 348	6, 96	0. 336	7. 184
100	1.043	31. 28	0. 975	3. 197	0.663	13. 26	0.622	7. 541
200	1.655	49.66	1. 491	4. 027	1. 257	25, 14	1.117	7. 955
300	2. 169	65. 07	1.895	4. 610	1.830	36.60	1. 547	8. 197

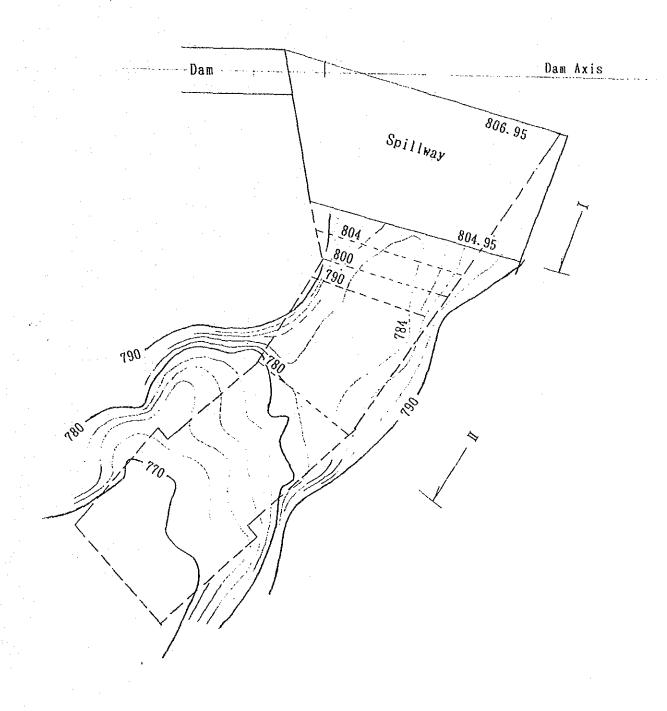


Fig. E.2-6 Washout of Spillway in First Phase of the Construction

Table E.2-9 Coordinates of Longitudinal Profile of the Dam

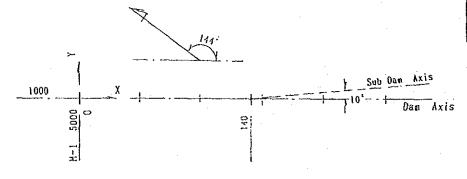
(Sub Dam Axis)

	Grou.		note		Grou.		note
X	G. L	E. L		j X	G. L	E. L	
n	10	m		m	11	10	
	000.0			-101.0		mm0 0	D 0
4789.0		•		5104.9	701 F	778.3	
4839.0		. :			781.5	778.0	D N-0
4859.0				5105.5	700	719.4	B. No2
4880.0				5110.0	799.0	795.0	in t
4902.0				5111.1	700 0	797.1	P-1
4926.0					799.0		
4941.0					800.0		
4974.0			:	5125.0		798.0	
5000.0			M~1		802.0		•
5005.0					804.0		4
	820.0				804.0		1 6. 11 1
	815.8				806.0	802.0	Left End
	812.4			5160.0			Spillway End
5023.5			Dam Right End				Masonry End
5030.0		802.0			808.0		
5035.0		799. 0		5194.0			
5040.0		793.0		5215.0			
5044.8		782. 2	P-4	5219.0			
5045.0		100.0		5235.0			
5050.0				5251.0		*	ROAD
5055.0				5257.0			ROAD
5058. 2			B. No1	5262.0			٠,
5060.0		771.0		5275.0			
5065.0		766.0		5282.0			
5070.0	765.0	761.5			882.0		H-2
5072.9			P-5;Y=990.4	5303.0			
5075.0		758.0	·	5325.0			ROAD
5080.0		753.5		5332.0	894.0		ROAD
5085.0	760.5						-
5090.3		748.4	P-2	1			
5095.0		755.0					•
5100.0	778.5	765.5		l			·

Point	Grou. G. L	Struct. E. L	note
5140.0	804.0		
5149.5	806.3	806.9	Dan End
5150.0		806.9	
5152.5		806.9	Spill. End
5160.0		806.9	
5170.0		807.0	
5176. 2		807.0	Mason. End
5177.2	807.0	7.4	
5184.7			
5188.0	810.6		
5190.0	810.0		
5193.7	812.0		
5199.3	816.0		
5207.0	820.0		
5217.5	825.0		
5232. 2	830.0		
5250.0	840.0		

Dam Cross Section

Pres	ent	lmpro	ved
Y	E. L	Y	E. L
-5. 40 -3. 00 -3. 00 3. 00 3. 00 3. 45 6. 25 20. 72 38. 72	749.00 797.00 809.00 809.00 803.30 800.10 794.10 774.00 749.00	-5. 40 -3. 00 -3. 00 3. 00 3. 00 5. 10 30. 75 52. 35 62. 40 60. 00 52. 35	749.00 797.00 811.50 811.50 804.83 802.50 774.00 750.00 747.00 747.00
5.00 10.00 15.00 20.00 25.00 30.00 35.00	796. 78 788. 89 781. 95 775. 00 768. 06 761. 11 754. 17	5. 00 10. 00 15. 00 20. 00 25. 00 30. 00 35. 00 40. 00 45. 00 50. 00	802. 61 797. 06 791. 50 785. 94 780. 39 774. 83 769. 28 763. 72 758. 17 752. 61



(3) Leakage

The leakage observed at the left side of the dam body is devided into two types.

- The leakage (1),(3) seems to be discharged from cracks and joints directly.
- The leakage (2) which shares most of the discharge has following characters.

Increase/decrease of the leakage volume delays about twelve hours against raising/fall of the water level of the reservoir.

The temperature of leakage water is one or two degrees lower than the one at the same elevation in the reservoir.

7 Feb. 1990 leakage water 21.5°C reservoir 23.5°C 10 Jul. 1990 leakage water 23.4°C reservoir 24.5°C

For the reasons mentioned above, it is concluded that the leakage is not discharged directly from the cracks, but discharged through some cracks with some depth in the rocks.

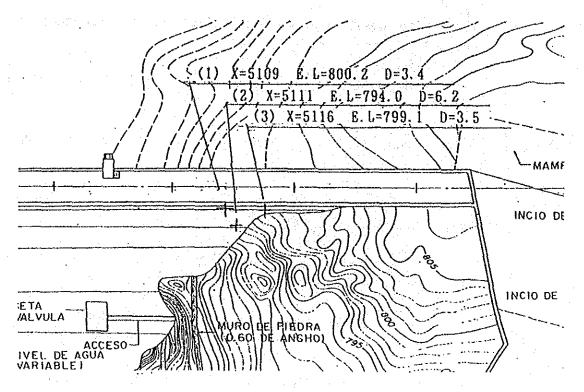


Fig. E.2-7 Location of Leakage Points

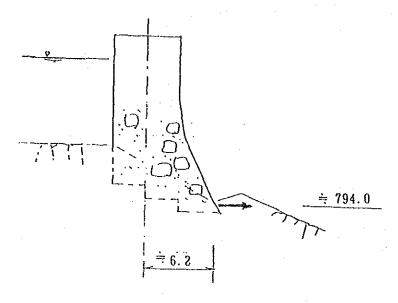
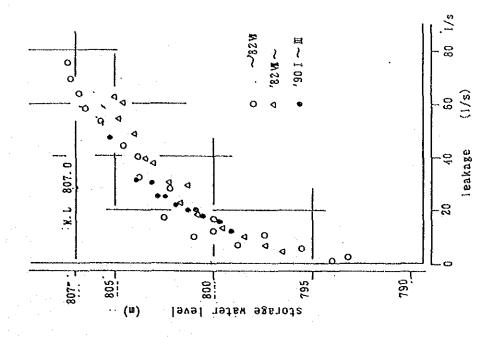
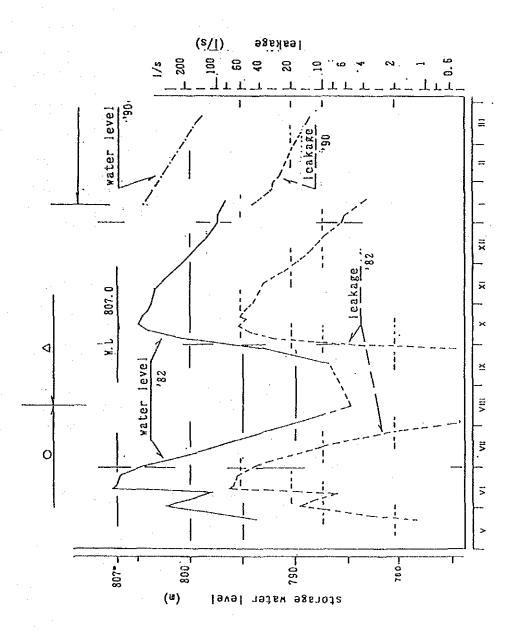


Fig. E.2-8 Section of Leakage Points





ig. E.2-9 Correlation of Water Level of Reservoir and Leakage

Table E.2-10 Observation Data of Leakage (1/2)

	Date	W. L	Leakage	log Q1
	1.		Ql	
		m	1/s	
	90. 1. 13	804.60	47.0	1.672
	1. 24	803.66	31.0	1.491
	1.29	803.13	30.0	1.477
	2. 3	802, 85	25.0	1.398
	2. 7	802.44	25.0	1, 398
	2. 14	801.90	22.0	1. 342
	2.16	801.61	22.0	1, 342
	2. 22	801.30	20. 3	1. 307
	2. 26	800.86	20.3	1, 307
	3. 3	800.47	17.7	1.248
	3. 12	799.73	15. 2	1.182
	3. 18	799.49	13. 1	1.117
	6. 23	806.54	54.0	1, 732
	7.10	806.94	54.0	1.732 1.732
	7.12	806. 97		1. 732
ĺ	8. 8	805.82	37.0	1. 568
	L	000.00	<u> </u>	2, 4,4,4
	82. 5. 22	793. 90	1. 2	0.079
	5. 25	796, 70	3. 4	0.531
	5. 28	798.80	7.0	0.845
	5. 30	801.00	10.0	1.000
	5. 31	801.90	12.0	1.079
	6. 1	802. 50	16.7	1. 223
	6. 5	800.40	12. 2	1.086
	6. 11	798.00	7, 0	0.845
ļ	6. 13	803.80	31.8	1. 502
	6. 13	806.50	58.0	1.763
ļ	6.14	807.40	74.9	1.874
	6. 14	807.35	74.9	1.874
	6. 15	807. 25	69.0	1.839
	6. 16	807.05	69.0	1.839
	6. 23	806.80	63.4	1.802
	6. 27	805.70	53.0	1.724
	6. 30	804.60	43.8	1.641
j	7. 2	803.80	40.0	1.602
	7. 5	802. 20	28.0	1.447
ļ	7. 10	799.80	16.5	1. 217
	7. 15	797.50	10.5	1.021
į	7. 20	795.60	5. 6	0.748
	7. 25	793. 20	2. 5	0.398
i	9 30	796 50	1 A	0 643

Date	W. L	Leakage Q1	log Q1
	ħ	1/s	
82. 10. 5	801.30	28.9	1.461
10, 10	804.00	48. 3	1.684
10.15	805.00	61.8	1.791
10. 20	804, 80	56.6	1.753
10. 20	804.80	54.3	1.735
10. 21	804.60	60. 2	1.780
10. 21	804.50	59.7	1.776
10. 25	804.10	55. 2	1.742
10.31	803.70	45.6	1.659
11. 5	803.60	42.5	1.628
11.10	803.40	38.7	1.587
11. 15	803.10	36.7	1.565
11. 20	802, 30	30.0	1.477
11. 25	801.70	22. 3	1.348
11.30	800.80	18.5	1.267
12. 5	800. 20	15.3	1.185
12.10	799.60	12.8	1.107
12.15	798.90	11.2	1.049
12. 20	798.40	9. 9	0.996
12. 31	797.40	6.7	0.826
83.1.5	797.40	6.4	0.806
1.16	796.60	4.0	0.602

Other Data

Date	W. L	Leakage Q1	log Q1
82. 7. 31	790.60	0.80	-0.097
8. 5	788.80	0. 22	-0.658
8. 9	787. 20	0.00	
8. 15	784.70	0, 00	-
9. 16	787.00	0.00	-
9. 27	793.00	0.00	

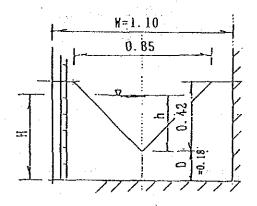
Table E.2-10 Observation Data of Leakage (2/2)

	Date	Water	Measured	Leakage		r Temp			Measured	Water	Coef.	Leakage
		Level	Depth		(2)	(3)	(3,)		Depth	Depth		
			H	Q					H	h	C	Q
٠,	90. 1. 13	804, 60	44.0	48.0		: : :			60	42	1.405	161.0
	1.24	803,66	40.0	31.0]	ì	Ì		58	40	1.400	142.0
	1, 29	803, 13	39. 5	29. 5				7	56	38	1.396	124.0
	2. 3	802.85	38.0	25.0			1		54	36	1.392	108.0
	2. 7	802.44	38.0	25.0	21.5	24.5	23. 5		52	34	1.389	94.0
	2.14	801.90	37.0	22.0			•		50	32	1, 386	80.0
	2.16	801.61	37.0	22.0	21.5	:	23.0		49	31	1. 384	74.0
	2. 22	801.30	36. 5	20.5	21.8				48	30	1.383	68.0
	2, 26	800.86	36.5	20.5					47	29	1. 382	63.0
٠,	3. 3	800.47	35. 5	17. 7					46	28	1.381	57.0
	3.12	799, 73	34.5	15.3	22.5	21.5			45	27_	1.380	52.0
	3. 18	799.49	33.5	13.1					44	26	1.379	48.0
									43	25	1.379	43.0
	90. 6. 23	806.54	45.5	54.0					42	24	1. 378	39.0
	7. 10	806. 94	45.5	54.0	23.4	23.4			41	23	1. 378	35.0
	7.12	806, 97	45.5	54.0			:		40	22	1.377	31.0
	8. 8	805. 82	41.5						39	21	1. 377	28. 0
	L			:					38	20	1.378	25.0
									37	19	1.378	22.0
									36	18	1. 378	18.9
									35	17	1.379	16.4
	40								34	16	1. 380	14. 1
						+ .		٠.	33	15	1. 381	12.0
									32	14	1. 383	10. 1
91	roula f	or Leak	age Cal	culation	on ·				31	13	1. 385	8.4
			to the feet of						30	12	1. 387	6. 9
			1.0						20	11	1 200	E C

$$Q = 1000 * c * h5/2$$

$$c = 1.355+0.61(0.0083h-0.09)2$$

$$Q : 1/s h : m$$



NUHATI, KUROKAWA and FUTIZAWA's formula - 90' Heasuring weir

29

28

27

26

Q≈Kh⁵/3 K=81. 2+h/0. 24+(8. 4+12/0) (h/W+0. 09) Q: discharge (n^3/n) h: head (n)

11 1.390

10 1.394

9 1.394

8 1.394

7 1.394

5. 6

4.4

3.4

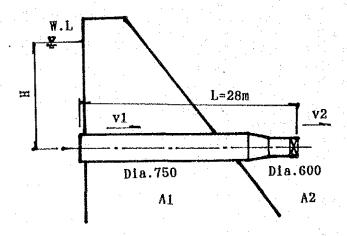
2. 5

1.8

(4) Outlet Work

1) Estimation of Discharge from the Valve (Nov. 1974 - Present)

A outlet pipe and a valve are installed in the Dam as shown below.



The discharge is estimated as follows.

$$Q = A \cdot v$$
 $Q = k * \sqrt{2gllo} * \Lambda_2$

where, lio: total head minus head loss

k: discharge efficiency of valve 0.8 - 0.9

assumed 0.8 in this case

The head loss is the total of inflow loss, friction loss and reducing loss.

$$\Sigma h = hI + hf + he$$

$$hi = 0.5 * v_1^2/2g = 0.0255 * v_1^2$$

$$hf = 124.6*n^2*L*v_1^2/(D_1^{4/3}*2*g)$$

where L: 28.0, $D_1 = 0.75$, n=0.015 (bending pipe)

he = $0.025*(1-(\Lambda_2/\Lambda_1)^2)*v_2^2/(8*sin(0/2)*2*g)$

 $= 0.0005 * V_2^2$

 $= 0.0011 * v_1^2$

Therefore the total head loss is:

h =
$$(0.0255+0.0588+0.0011)*v_1^2 = 0.0854*v_1^2$$

note : $A_1 = 1/4*\pi *D_1^2 = 1/4*\pi *0.75^2 = 0.442 m^2$
 $A_2 = 1/4*\pi *D_2^2 = 1/4*\pi *0.60^2 = 0.283 m^2$

 $Q = 0.8*\sqrt{2gllo} *A_2$

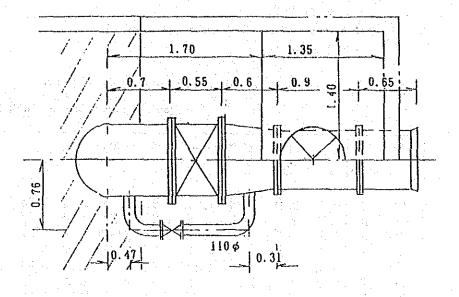
Q = 0.8* 19.6*(H-0.0854*v₁²) *0.283

 $Q = 0.835 * H^{1/2}$

Table E.2-11 Water Discharge from Valve

Howell-Bunger Valve 600ϕ

W. L.	h _e			Valve	0per	ated	Degre	Degree		,
	NL-775	1′	2	3	4	5	6	8	10	12'
n	: p)	n³/s								n³/s
807	32	0, 39	0.79	1.18	1.57	1.97	2.36	3. 15	3.94	4.723
806	31	0.39	0.77	1.16	1.55	1.94	2. 32	3. 10	3.87	4.649
805	30	0.38	0.76	1.14	1.52	1.91	2. 29	3.05	3.81:	4.573
804	29	0.37	0.75	1.12	1.50	1.87	2. 25	3.00	3.75	4.497
803		0.37	0.74	1.10	1.47	1.84	2. 21	2.95	3.68	
802	27	0.36	0.72	1.08	1.45	1.81	2.17	2.89	3.62	
801	26	0.35	0.71	1.06	1.42	1.77	2. 13	2.84	3.55	4. 258
800	25	0.35	0.70	1.04	1.39	1.74	2.09	2.78	3.48	
799	24	0.34	0.68	1.02	1.36	1.70	2.05	2.73	3.41	
798	23	0.33	0.67	1.00	1.33	1.67	2.00	2.67	3.34 :	
797	22	0.33	0.65	0.98	1. 31	1.63	1.96	2.61	3. 26 :	
796	21	0.32	0.64	0.96	1. 28	1.59	1.91	2.55	3. 19	3.826
795	: 20	0.31	0.62	0.93	1. 24	1.56	1.87	2.49	3.11:	3. 734
794	19	0.30	0.61	0. 91	1. 21	1.52	1.82	2.43	3.03;	
793	18	0.30	0.59	0.89	1.18	1.48	1.77	2. 36	2.95:	
792		0. 29	0.57	0.86	1. 15	1.43	1.72	. 2. 30	2.87	3. 443
791	16	0. 28	0.56	0.84	1.11	1.39	1.67	2. 23	2. 78 :	
790	15	0. 27	0.54	0.81	1.08	1.35	1.62	2. 16	2.69	
	10		0.44						-	
780	5	0.16	0.31	0.47	0.62	0.78	0. 93	1. 24	1.56	1.867
785	10	0. 22	0.44	0.66	0.88	1.10	1.32	1.76	2. 20	2.6



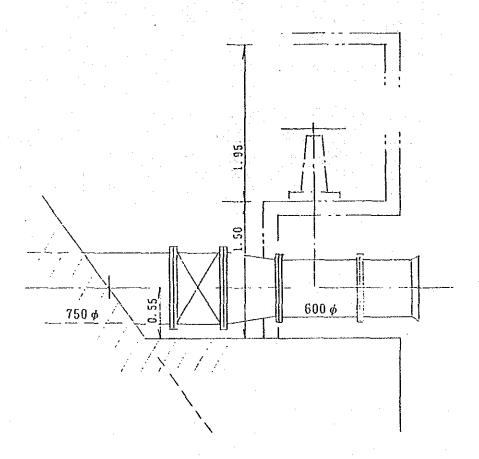


Fig. E.2-10 Details of Valve Location

The outlet discharge is computated by the following formula;

$$Q = C*\sqrt{2gllo} *A$$

where Qo : outlet discharge (m³/sec)

C: discharge coefficient at full-open stage

of valve

g : gravity acceleration

Ho: effective head

A : sectional area of valve (= $PI*D^2/4$) (m^2)

D : diameter of valve

In case of C=0.85

 $Q = 2.95*D^2* Ho (m^3/sec)$

 $D = (Qo/(2.95* Ho))^{1/2}*1000 (mm)$

This relation is shown in the following figure.

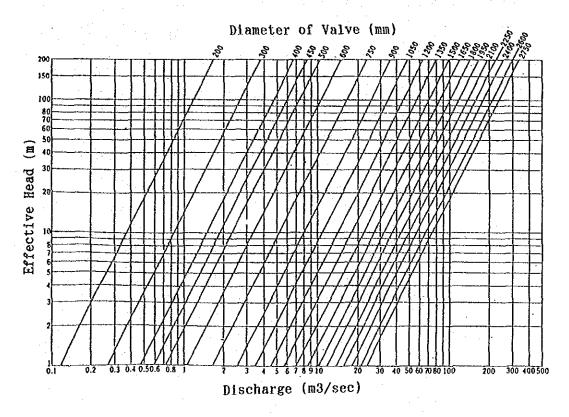


Fig. E.2-11 Correlation of Head, Discharge and Diameter of Valves

(5) Water Balance

Table E.2-12 Water Balance of the Reservoir in 1969

Month	Water	Storage	Outfall(+)	Infl	OW		Est -	Outfal	l	-
.	Level	Volume	Storage(-)	inflow	Extra	Evapo.	Leakage	e Valve	Other	Total
							*			
]]			1)	2)]				1)+2)
	m									
i l		(12,610)						•		
1 1		12, 610	0	2, 500	4, 150	110		90	1,980	2, 500
2	806. 20	12, 067	540	1, 250	860	110	320	350	1,010	1,790
3	804.84	11, 144	920	1, 250	· -	100		350	1, 420	2, 170
4	799.87	7, 789	3, 360	1, 250	-	100	270	860	3, 380	4, 610
5	786.98	2, 098	5, 690	1, 250		50	120	2, 680	4, 090	6, 940
6	807.00	12,610	-10, 510	14, 850	21, 430	100	280	3, 460	500	4, 340
7	800.34	8, 091	4, 520	2, 500	1,810	100	280	3, 720	2, 920	7,020
8	807.00	12,610	-4, 520	8, 930	5, 100	100	270	3, 540	500	4, 410
9	807.00	12,610	0	4,560	20,040	110	320	3,630	500	4,560
10	807.00	12,610	0	4,650	39, 480	110	320	3, 720	500	4,650
11	801, 54	8, 905	3, 700	2, 500	260	100	280	3, 110	2,710	6, 200
12	803. 92	10, 520	-1,610	3,090	-	-100	280	600	500	1, 480
Total			2, 090	48, 580	93, 130	1, 190	3, 360	26, 110	20, 010	50, 670
			·			0.04	0.11	0.83	0.64	1.61

Table E.2-13 Water Balance of the Reservoir in 1972

Month	Water	Storage	Outfall(+)	lnfl	OW.		. (Outfall	l	
	Level	Volume	Storage(-)	Inflow	Extra	Evapo.	Leakage	Valve	Other	Total
	m	100				1				
	(807.00)	(12, 610))						11 1	
1	806.71	12, 413	200	2, 500	0	110	320	420	1,850	2,700
2	805.60	11,660	750	2, 500	-	110	310	450	2, 380	3, 250
3	803.00	9,896	1, 760	1, 250	· -	100	300	460	2, 150	3,010
4	799.78	7, 739	2, 160	1, 250	-	90	250	580	2, 490	3, 410
5	792, 78	4, 183	3, 560	1, 250		70	170	910	3,660	4,810
6	794.68	4, 985	-800	2,500	_	70	150	190	1, 290	1,700
7	(791. 34)	3.575	1,410	2, 500		50	110	500	3, 250	3, 910
8	794.40	4,867	-1, 290	3, 750	-	60	130	250	2,020	2, 460
9	799. 92	7,816	-2, 950	5,000		80	200	100	1,670	2,050
10	807.00	12,610	-4,790	5,690	11,750	100	280	20	500	900
11	806.95	12, 576	30	2, 500	3,800	110	320	70	2,030	2, 530
12	806.06	11, 972	600	2, 500		100	310	470	2, 220	3, 100
[otal			640	33, 190	15, 550	1,050	2, 850	4, 420	25, 510	33, 830
					, , , , , , , , , , , , , , , , , , ,	0.03	0.09	0.14	0.81	1. 07

(6) Stability Analysis

Table E.2-14 Results of Stability Calculation on the Present Dam Present State m=0.72 K = 0.15 U = 0.50

		H.W.L = 807			H. W. L=797	HHWL =809
		·			٠	X =
	EL=749 B=44.12	EL=765 B=31.80	EL=780 B=20. 25	EL=795 B=8.86	EL=749 B=44.12	EL=749 B=44.12
V (t)	2, 054. 2	1, 096. 5	495. 6	156.8	2, 140. 5	2, 036. 9
H (t)	2, 422. 2	1, 314. 3	578.0	139. 5	1, 799. 4	1, 853. 9
M (t·m)	78, 312	31, 101	8, 973	1, 221	62, 866	66, 703
F. \$	3, 41	4. 30	5. 94	10. 43	4.63	4. 45
l (ក) e (ក)	38. 12 16. 06	28. 36 12. 46	18. 11 7. 98	7.79 3.36	29. 37 7. 31	32. 75 10. 69
p (t/m2) p1(t/m2) p2(t/m2)	46.6 148 -55	34. 5 116 - 47	24. 5 82 - 33	17. 7 58 -23	48. 5 97 0	46. 2 113 -21

Table E.2-15 Dam Stability Calculation (1/6)

Present m=0.72 H. W. L=807 U=0.50 K=0.15

E. L=749 L=44. 12

	Y	Н	У	х	М
W1	24.0		1. 20		29
2	57.6		0.80		46
D1	115. 2		1.60		184
2	178.8		5.40		966
3	19.5		9.48		185
	834.4		7.03		5, 866
4 5	1, 464. 4		22.47		32, 905
P	""	1,682.0		19.33	32, 513
E		53, 9		4.67	252
Ü	-639.7	:	14.71		-9, 410
KD1		17.3		16.00	277
2		26.8	;	52. 55	1, 408
3		2. 9		47.10	137
4		125. 2		22.55	2, 823
5		219, 7		15.03	3, 302
KW		294. 4		23. 20	6,830
1					
	2, 054. 2	2, 422. 2			78, 312

Table E.2-15 Dam Stability Calculation (2/6)

Present m=0.72 H.W.L=807

U=0.50 K=0.15

B. L=765 B=31.80

	V	H	y	χ	М
W1	16.0		0.80		13
2	25. 6		0.53		14
D1	51.2	4.	1.07		55
2	178.8	1.4 %	4.60		822
3	19.5		8,68		169
4	538.4		6. 23		3, 354
5	600. 9		17.83		10,714
P		924.5		14. 33	13, 248
E					-
U	-333.9		10.60		-3, 539
KD1		7.7		10.67	82
2		26. 8		36. 55	980
. 3		2. 9		31.10	90
4		80.8		14. 55	1, 176
5		90. 1		9.70	874
KW		181.5		16.80	3,049
	1,096,5 1	, 314. 3			31, 101

Table E.2-15 Dam Stability Calculation (3/6)

Present m=0.72 H.W.L=807

U=0.50 K=0.15

E. L=780 B=20. 25

	γ	Н	У	Х	Ж
W1	8.5		0.42	·	4
2	7.2		0.28		2
D1	14.4		0.57		. 8
2	178.8		3.85		688
3	19.5		7.93		155
	260.8		5, 48		1, 429
4 5	143.1		13.48	: :	1,929
P		392.0		9. 33	3,657
E		_		_	· -
U	-136.7		6.75		-923
KD1	-	2. 2		5. 67	12
2	i	26.8		21. 55	578
3	1	2. 9		16.10	47
4		39. 1		7.05	276
5	1	21. 5		4.70	101
KW		93. 5		10.80	1,010
· · · · · · · · · · · · · · · · · · ·					
	495.6	578.0			8,973

Table E.2-15 Dam Stability Calculation (4/6)

Present m=0.72 H. W. L=807 U=0.50 K=0.15

E. L=795 B=8.86

	Y	Н	У	х	М
W1	1, 0		0.05		0
. 2	0.1		0.03		0
D1	0, 2		0.07		0
2	168.0		3, 10		521
3	14.1		7.02		99
4 5					
P		84.5		4. 33	366
E				-	,-
U	-26.6		2. 92		-78
KD1		0.0		0.67	0
2		25. 2		7.00	176
3		2.1		1.70	4
4					
4 5					
KW		27. 7		4.80	133
	450.0	100 5			1 001
	156.8	139.5		:	1, 221

Table E.2-15 Dam Stability Calculation (5/6) m=0.72 H.W.L=798 U=0.50 K=0.15

E. L=749 L=44. 12

	Y	Ħ	y	Х	М
Wi	2. 4		1. 20		3
2	57. 8		0.80	i	46
Di	115. 2	*	1.60		184
2	178.8		5, 40	ļ	966
3	19.5		9.48		185
4	834. 4		7.03		5, 866
5	1, 464, 4		22. 47	-	32, 905
P	1	1, 200. 5	! :	16.33	19,604
Ē		53. 9		4.67	252
Ū	-540.5		14. 71		-7, 951
KD1		17. 3		16.00	277
2		26.8) !	52.55	1, 408
3		2. 9	! !	47, 10	137
4		125. 2	!	22. 55	2, 823
5		219. 7	! !	15.03	3, 302
KW		210. 1	!	19.60	4, 118
AN II	·	<u>~~~</u>	ļ		
	2. 131. 8	1, 856. 4	!		64, 125

Table E.2-15 Dam Stability Calculation (6/6)

m=0.72 H. W. L=797 U=0.50 K=0.15

E. L=749 B=44. 12

	V	Н	у	X	Ж
W1	 				_
2	. 57. 6		0.80		46
D1	115. 2	* *.	1.60		184
2	178.8	100	5.40		966
3	19.5		9.48		185
4	834.4		7.03		5, 866
5	1, 464. 4		22.47		32, 905
P		1, 152.0		16.00	18, 432
E		53.9		4.67	252
U	-529.4		14.71		-7.787
KD1		17.3		16.00	277
2		26.8		52. 55	1, 408
- 3		2. 9		47, 10	137
4		125. 2		22. 55	2, 823
5	1.7	219.7		15.03	3, 302
L KW	<u> </u>	201.6		19. 20	3, 871
	T				
	2, 140. 5	1, 799. 4			62,866

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Calculation basis

Fig. E.2-12 Schema of the Present Dam and Calculation Base

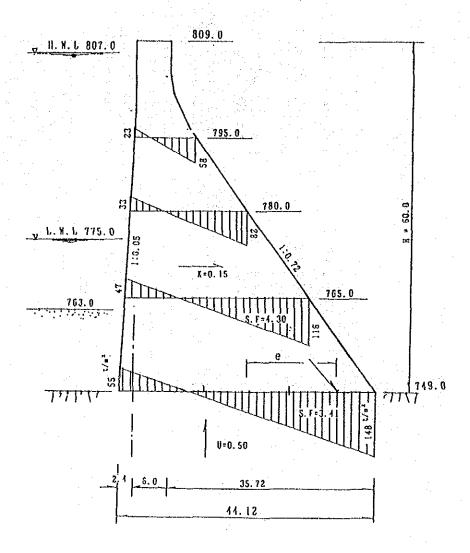


Fig. E.2-13 Calculation of the Present Dam Stability

E.3 The Coyolar Dam Rehabilitation Plan

(1) Design Flood Discharge

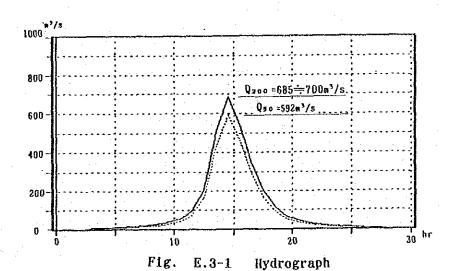
The design flood discharge of the Dam is Q = 700 m3/s (T = 1/200) as shown in the following table and figure.

Table E.3-1 llydrograph

T =1/200, 1/50

, ,	Rainfa	11		Dischar	ge
T	R200	R50	T	Q200	Qso
ħг	8.0	nn.	hŕ	# ³ /s	■ ³ /8
-1	0.3	0.3	2.5	3.9	1.2
2	0.4	0.4	3.5	6.7	3.9
2 3	0.5	0.4	4.5	9.1	6.3
4	0.6	0.4	5. 5	12.0	7.6
5	0.8	0.6	6.5	15.4	11.3
6	1.0	0.7	7.5	19.6	14.4
ž	1.3	1.0	8.5	26.0	19. 1
В	1.8	1.3	9.5	35.8	26.7
9	2.7	2.1	10.5	53.7	41.1
10	4.5	3.5	11.5	91.7	71.5
[11]	8.8	7.0	12.5	205. 3	165.0
12	25.6	21.0	13.5	502.0	427.1
13	60.0	53. 5	14.5	685.0	592. 1
14	14. 2	11.3	15.5	538.4	459.6
15	6.2	4.8	16.5	337.7	282.6
16	3.5	2.6	17.5	199. 2	161.3
17	2.2	1.7	18.5	112.9	91.4
18	1.6	1. 2	19.5	67.7	53. 2
19	1.1	0.8	20. 5	42.7	32.4
-20	0.8	0.7	21.5	28.6	20.3
21	0.7	0.5	22. 5	19.6	14.6
22	0.5	0.4	23. 5	14.9	11.4
23	0.5	0.4	24.5	12.2	9.8
24	0.4	0.4	25.5	8.9	7.5
25			26.5	4.9	
26	L	:	27.5	2.2	1.9

	74.
Init H	ydrograph
T· I	Rate
ħΓ	
0.0	0
0.5	0. 194
1.0	0. 287
1.5	0. 368
2.0	0. 329
2.5	0. 257
3.0	0.188
3.5	0. 130
4.0	0.089
4.5	0.059
5.0	0.038
5.5	0. 025
6.0 (0.016
6.5	0.010
7.0	0.006 [
7.5	0.004
8.0	0.003
8.5	0.002
9.0	0.001



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(2) Rehabilitation Plan

1) Dam Height

Height of Nonoverflow Section

The Dam height of nonoverflow section is to be studied in accordance with the conditions of the reservoir.

Determine the height of the non-overflow section of the dike, depending on whether the dam under consideration is equipped with flood discharge gate or not, by fixing it to a value greater than the maximum of those given in the Table 11-1 when the dam is of concrete type and fixing it to a value greater than the maximum added with 1 when the dam is of fill type.

Table E.3-2 Height of the Non-overflow Section of the Dike

Article	Category	Height of the non-overflow section of the dike (unit: m)				
	with flood	Hn + hw + he + 0.5 (in case hw + he < 1.5, Hn + 2)				
• • • • • • • • • • • • • • • • • • •	discharge gate	Hs + hw + $\frac{\text{he}}{2}$ + 0.5 (in case hw + $\frac{\text{he}}{2}$ < 1.5, Hs + 2) Hd + hw + 0.5 (in case hw < 0.5, Hd + 1)				
2	Dam not equipped flood	Hn + hw + he (in case hw + he < 2, Hn + 2) Hs + hw + $\frac{he}{2}$ (in case hw + $\frac{he}{2}$ < 2, Hs + 2)				
	charge gate	Hd + hw (in case hw < 1, Hd + 1)				

The symbols used in the above expressions indicate the following indication:

Hn: Normal water level (unit: m)

hw: Height of surge due to wind from the water level of the reservoir at the design flood level (unit: m)

he: Height of surge due to earthquake with design seismic coefficient, from the water level of the reservoir at normal water level (unit: m)

Hs: Surcharge water level (unit: m)

Hd: Design flood level (unit: m)

For a fill dam not equipped with flood gate where water flows down the spillway with depth of 2.5 m or less at the design flood run-off.

expressions "in case hw + he < 2, Hn + 2" and "in case hw + $\frac{he}{2}$ < 2, Hs +2" given in the Article 2 should be replaced by those "in case hw + he < 1, Hn + 1" and "in case Hw + $\frac{he}{2}$ < 1, He + 1" respectively.

Height of Surge by Wind

The height of surge due to wind should be calculated in the method S.M.B. When the upstream side of the dike is nearly vertical, this height must be calculated by the following expression as reflected waves change it into total height of wave.

 $hw = 0.00086*v^{1.1}*F^{8.45}$

where,

v: Average speed of wind for ten minutes (m/s)
v = 20 m/s

F: Maximum distance from the dike to the opposite bank at the design flood level (m), F = 1000 m

 $hw = 0.00086 * 20^{-1.1} * 1000^{-0.45} = 0.52$

Height of Wave by Earthquake

The height of wave due to earthquake is calculated by the expression of Seiichi Sato.

he = $K \cdot \tau \cdot \sqrt{gHo} / (2\pi)$

where,

K: Design seismic intensity at the normal water level, K=0.15

 τ : Cycle of earthquake, τ = 1 sec

Ho: Depth of reservoir at normal water level (m)

g: Gravity acceleration (9.8 m/s2)

he = $0.15*1*\sqrt{9.8*58.0}/(2*\pi) = 0.57$

Elevation of Nonoverflow Section

The elevation of nonflow section in this Dam is determined by "design flood water level" case as the overflow depth is large.

design flood water level

EL.810.4 m (=807.4+3.4)

extra height

1.0 m

elevation of the nonoverflow section EL.811.4 m

Shape of the Dam 2)

The shape of the rehabilitation dam are decided as follows;

- The elevation of vertex of the basic triangle is EL.811.5 m.
- The shape of downstream dam body is 1:m = 1:0.90
- The shape of upstream dam body is same as the existing one.

The elevation of the overflow section at the center of the dam body is EL.807.0m and used as a spillway.

The shape of the overflow crest at the upstream side of the dam was determined by the approximation of the result of "HARROLD Numbers". The crest shape of the lower stream side was determined by the approximation quadric line.

Upstream side of the dam (3m from dam-axis)

$x_1/Hd = 0.282$	Χį	=0.92		1.00	where	the	design
$x_2/lld = 0.175$	X2	=0.57	>	0.65	depth	(Hd)	=3.25m
$x_3/Hd = 0.107$	ХЗ	=0.35	->	0.35			
$r_1/IId = 0.5$	$\mathbf{r_i}$	=1.63		1.80			
$r_2/Hd = 0.2$	r2	=0.2	>	0.75			
y / Hd = 0.126	y	=0.41		0.40			

Downstream side of the dam

$$y^2 = 4m^2 hx$$
 $y^2 = 14.58x$ (m=0.90m h=4.5m)

 $x = 0.05 \quad 0.1$ 0.20.40.62 1.0 1.5 2.02.48 3.5 y= 0.85 1.21 1.71 2.41 3.00 3.82 4.68 5.40 6.00 7.14 8.10m

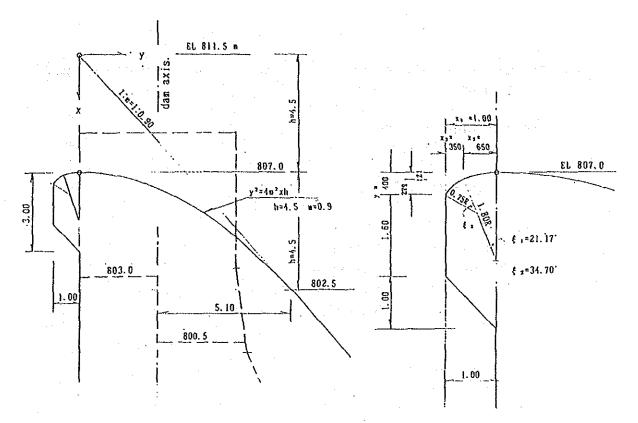


Fig. E.3-2 Shape of Dam Crest

(3) Calculation of Overflow Discharge

The design flood discharge of the Dam (return period of 200 years is assumed as $Q = 700 \text{ m}^3/\text{sec}$.

Overflow width: 60.0m

Pier : 1.2m x 4each

 $Q = C \times (B-NKH) \times H^{9/2}$

where.

C: Overflow coefficient (=Cd)

B: Overflow width = 60.0m

N: Numbers of contraction = 4x2 = 8

K : Contraction coefficient = 0.10

 $C = 1.6 \times \{(1+2a(H/Hd))/(1+a(H/Hd))\}$

 $Cd = 1.971 + 0.498\zeta + 6.63\zeta^{2}$

 ζ : x/Hd = 0.056 at y = 0.5Hd

 \therefore Cd = 2.02 = 2.0

against Hd = 3.4

 $Q = 2.0 \times (60.0-8 \times 0.1 \times 3.4) \times 3.4^{3/2} = 718m^3/sec > 700m^3/sec$

Therefore, the overflow depth is Hd = 3.4m.

- (4) Design Seismic intensity
- 1) Computation of Design Seismic Intensity from Data of Previous Earthquakes

For determination of design seismic intensity, the previous seismic acceleration at the Dam site are studied statistically from the collected data of past earthquakes.

The collected data covers the period 1898-1976 and is listed below.

It is estimated from the magnitude and focal distance of the earthquake by Okamoto's formula as follows:

 $\log (G/640) = ((x+40)/100) \times (-7.604 + 1.7244M - 0.1036M^2)$

where,

G: Maximum seismic acceleration (Gal)

x: Distance from the epicenter of earthquake (Km)

M: Magnitude (by Ritcher scale)

The maximum seismic acceleration estimated from the past earthquakes are rearranged in order and the probability calculation was performed based on the statistic data of the non-periodic seismic occurrence probability as follows:

Return period Te = (n/m)

n = Recorded year

m = Order of data

or

y = log Te

$$a = (x.y - xy) / (y^2 - y^2)$$

b = x - ay

x = ay + b

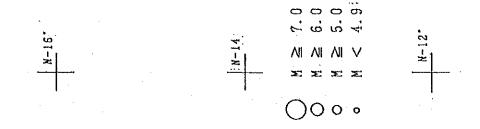
2) Others

The collected data of earthquakes covers the period until 1976, however the Comayagua and La Paz earthquakes have taken place lately.

According to the data of the El Cajon Dam, the maximum seismic acceleration of 0.15 was observed by the seismometer installed in October 1987.

Table E.3-3 Data of Earthquake

No.	Y.	H. D	Lat.	Dep.		lagn i tu	de g Dist.	a l
	٠	1.5	N.	₩.		Н.	l,	nax
3 .	eficili			14 57 14	Ka		Kn	ga
1	1898	4. 29	12.00	86.00	0	7. 90		18
2	1902	4. 19	14.00	91.00	0	8. 20	379	10
3	'07	12.30	12. 10	86.30	0	7. 20	279	- 11
4	'10	1. 1	16.50	84.00	60	7. 10	450	1
5	12	6.12	17.00	89.00	Õ	6.80	338	2
6	'15	9. 7	14.00	89.00	80		165	78
7	'16	11. 27	12.00	90.00	0	7.50	372	6
8	'19	6. 29	13.50	86.50	90	6.75	142	36
9	'21	3. 28	12.50	87.50	0	7. 30	202	-32
10	125	10. 5	12. 25	85. 25		6.75	335	2
11	'26	11. 5	12.30	85.80	135	7. 20	290	9
12	'28	10.25	12.30	85.80	Õ	6.50	290	2
13	'31		13.00	87.00	100	5. 75		4
14	'32		12.00	87.50	90	6. 90	258	8
15	'34	3. 7	13. 25	87.75		6. 25	122	25
16	'38	4.25		86.90	Ŏ	6. 50	244	4
17	'39	12. 26	13. 25	88. 25	7 5	6. 00	143	10
18	'40	2. 20	12.50	87.50	Ŏ	6. 50	202	9
19	'41	11.16	13. 25	88.50		5. 75		4
20	'42	8. 6	13. 90	90.93		8. 30	372	11
21		10. 2	14.50	89.75	160	6.50	243	4
22	45	10. 7	12. 25	89. 25	0	6. 75	297	· 3
23	'46	6. 24	14. 75	89.00	260	6.00	168	6
24	47	7.15	12.50	86.80	30	6.50	216	7
25	'48	6. 27	17.00	85.00	100	7.00	402	1
26	'51	5. 6	13.00	87.80	0	6.50	150	22
27	'52	11.20	12. 10	87.90	60	6. 25	250	-2
28	154	2. 19	12.50	87.50	0	6.63	204	11
•		1.13	14.00	86.42	100	5.75	124	10
29	'55	4. 4	13.00	87.00	0	6. 25	- 159	- 12
30	'56	1. 24	12.20	86.70	100	7.30	253	17
		10. 24	12.00	87.00	. 0	7. 23	266	13
31.		4. 5	12.61	87.80		5.60	195	1
32	'58	11.14	12.48	86. 44	72	6.50	237	5
		6. 27	13.00	88. 50	60	6.00	183	4
33	'59	2. 16	13.11	87. 34	0	5. 40	138	-3
34	'60	3. 24	13.50	87.00	0	5. 30	108	6
35	'61	5. 23	12.70	87. 30	138	6.50	183	12
36	'62	11.24	13.00	87.50	25	6.50	149	22
37	'63	12. 21	13. 40	87. 20	30	5. 60	110	12
38	64	2. 18	13.00	87. 50	30	5. 60	149	4
39	'65	5. 3	13.65	89. 15	23	6. 50	193	10
40	.66	12. 27	13. 30	88.80	78	5, 50	181	1
41	'67	11. 8	16.00	85. 90	28	5. 45	253	1
12	.68	6.11	13. 90	88.80	199	5. 28	148	2
43	'69	2. 25	15. 23	87. 47	15	5.00	99	4
44	'70	8. 12	12.02	86. 54	33	6.30	278	1
45	'71	6. 18	14.68	87. 57	7	4. 78	38	29
46	'72	12. 23	12. 36	86.12	5	6. 20	266	1
47	'73	7. 27	12.80	86.70	199	5. 28	192	1
48	174	3. 6	12. 30	86. 40	110	6. 10	256	1
49 En	'75	3. 13	16. 30	87.00	33	5. 11	224	20
50	'76	2. 4 9. 2	15. 32 13. 26	89. 10 89. 94	5 81	7. 50 6. 78	203 289	39 4



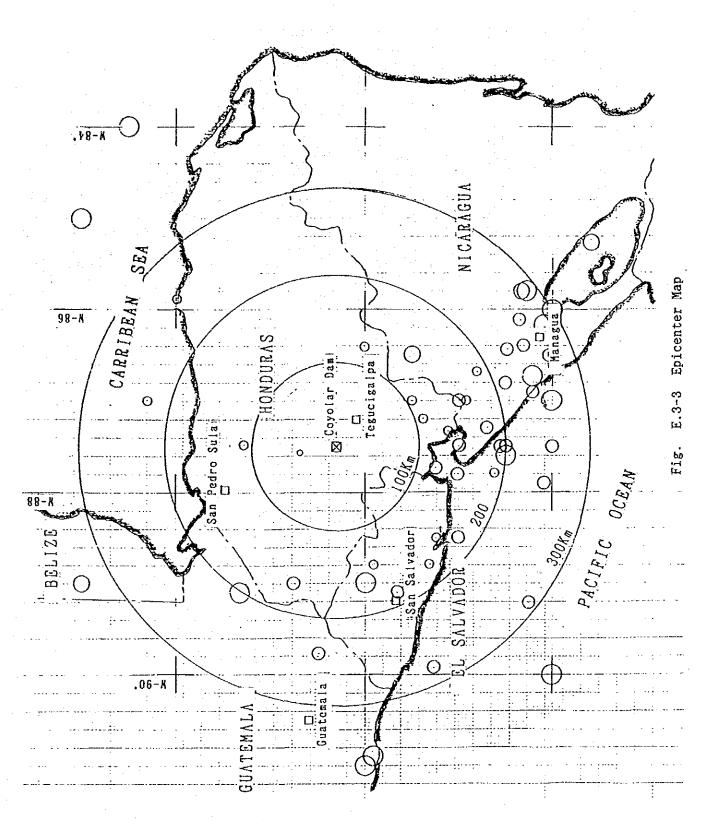


Table E.3-4 Expected Value of Earthquake Acceleration

No.	gal x	x 2	Te n/No.	y=logTe	y ²	ху	·		
	gal								
. 1	78	6084	44.000	1.6435	1.2820	128. 1893		•	
2	39	1521	22.000	1. 3424	1. 1586	52. 3545			
3	36	1296	14.667	1. 1663	1.0800	41.9879			
, š	32	1024		1,0414	1.0205	33. 3246			•
, ŝ	29	841	8. 800	0. 9445	0.9718	27. 3900			
ě	25	625	7. 333	0.8653	0. 9302	21.6325	đ.		
7	22	484	6. 286	0.7984	0.8935	17. 5638		* v	
8	22	484	5. 500	0.7404	NOAR O	16. 2880	je s	e de la companya de l	
9	18	324	4.889	0. 6892	0.8604 0.8302 0.8022	12. 4058			
10	17	289	4. 400	0.6435	n Rn22	10. 9387	15 E	San San San San San San	
11	13	169	4. 000	0.6021	0.7759	7. 8268	٠.		
12	12	144	3. 667	0.5643	0.7512	6. 7713		$a = (\overline{x} * \overline{y} - \overline{x} \overline{y}) / (\overline{y}$	$2-\overline{y^2}$) =12.2
13	12	144	3. 385	0. 5295	0.7277	6. 3541		$b = x - a * \overline{y} = 7.4$	
14	12	144	3. 143	0. 4973	0.7052	5. 9679		G = a * y + b = 12.2	v+7 A
15	11	121		0.4674				0 0.3.0 10.0.	, · • • •
16		121	2. 933		0.6836	5. 1410		Te=100 y=2.0 G	-22401-0 036
17	11		2.750	0.4393	0.6628	4. 8327	٠.		
	11	121	2. 588	0.4130	0.6427	4.5430		Te=200 y=2.3 G	=36 =0.048
18	10	100	2. 444	0.3882	0.6230	3. 8818	-		
19	10	100	2. 316	0.3647	0.6039	3.6470			
20	10	100	2. 200	0.3424	0. 5852	3. 4242			•
21		100	2. 095	0.3212	0.5668	3. 2123			
22	9	81	2.000	0.3010	0.5487	2. 7093		and the second second	
23	.9	18	1.913	0. 2817	O. 5308	2. 5355		•	
24	. 8	64	1.833	0. 2632	0.5131	2. 1059			
25	7	49	1.760	0. 2455	0.4955	1.7186		•	
26	6	36	1.692	0. 2285	0.4780	1. 3709			
27	6	36	1. 630	0. 2121	0.4605	1. 2725			
28	6	36	1.571	0. 1963	0.4431	1. 1778		*	
29	5	25	1.517	0. 1811	0. 4255	0. 9053			
30	4	16	1. 467	0.1663	0.4078	0.6653			
31	4	16	1.419	0. 1521	0.3900	0.6084		•	
32	4	16	1. 375	0. 1383	0.3719	0.5532			
33	4	16	1. 333	0. 1249	0. 3535	0. 4998			
34	4	16	1. 294	0.1120	0.3346	0.4479			
35	4	16	1. 257	0.0994	0.3153	0. 3975			
36	4	16	1. 222	0. 0872	0. 2952	0. 3486			
37	4	16	1. 189	0.0753	0.2743	0.3010	100		
38	3	9	1. 158	0.0637	0. 2523	0. 1910			
39	3	9	1. 128	0.0524	0. 2289	0. 1572			
40	2	4	1. 100	0.0414	0. 2035	0.0828			
41	2	4	1.073	0.0307	0. 1751	0.0613			
42	2	4	1.048	0.0202	0.1421	0.0404		•	
43	2	4	1.023	0.0100	0.0999	0.0200			
44	2	4	1,000	0.0000	0.0000	0.0000			
n=	<u>x</u> =	$\overline{\chi^2} =$	*	y = '	y 2 =	x y =			
44	12. 364	338. 86		0.4065	0. 5658	9. 9056		•	
-1-1	100 003	404.00		0. 1009	v. 0000	A* AAAA			•

(5) Uplift Force

Piezometric groundwater level in bore hole are observed. Those results are shown in the Table E.3-5.

The measuring level of bore hole No.2 is similar with the water level of the reservoir due to close to the leakeage point of large amount.

There is not plenty of data to decide uplift coefficient. In accordance with the grouting at dam construction stage and drilling data in 1984, it's reasonable to employ high value of coefficient. Therefore, 50 % of uplift coefficient is employed for design of the dam rehabilitation.

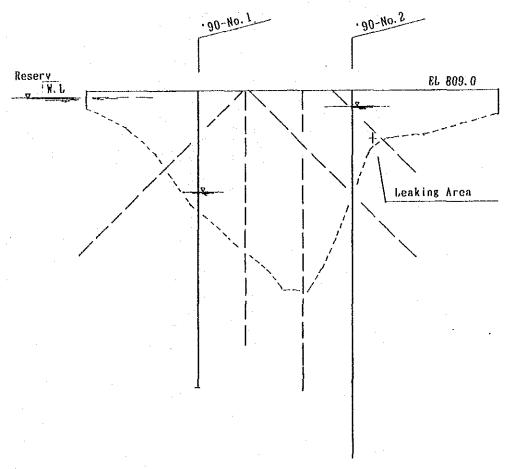
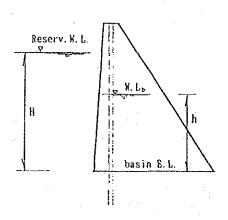


Fig. E.3-4 Groundwater Level along the Dam

Table E.3-5 Summary of Uplift Calculation

			'90 - No	o. 1	'90 - No	o. 2
1		Reserv.			•	
	Y. M. D	W.L.	W. L _b	U	W. Lb	V
	1974	m	n .	<u>, Baraj</u>	m	
٠	90. 3. 24	798.30	775.16	0. 140	797.12	0. 938
	28	799. 20	775.62	0. 152	797.85	0.932
	31	799.46	775.96	0.162	797.98	0.926
. 1	4.1	801.45	775.72	0.144	797.96	0.842
٠.	4 :	801. 20	775.54	0.139	797.50	0.830
	8	800.82	775.35	0.134	797.41	0.841
	12	800.42	775. 29	0.134	797.17	0.845
	16	800.08	774.80	0.119	796.89	0.846
ļ	20	799.86	774.44	0.107	796.80	0.850
-	24	799.70	774. 20	0.099	796.55	0.845
	28	799.90	774.60	0.112	796. 20	0.820
	30	800.66	775.00	0. 123	797.30	0.842
1	5. 2	801.46	775.48	0.136		0.823
	4	801.98	775.97	0.149		0.836
	6	802.30		0.151	798.85	0.849
	8	802.42	776.17	0. 154	799. 02	0.852
	12	802. 30	776.12	0.153	798.57	0.837
	16	802. 20	775.97	0.148	798.66	0.845
	20	802.08	775.88	0.146	798.60	0.847
1	22	802.04	775.83	0.145	798.46	0.842
	24	802.48	776.06	0.150	798.95	0.847
	25	803.54	776.70	0. 165	800, 08	0.857
	26	804.06	777.04	0.173	800.16	0.842
-	27	804.40	777. 22	0.176	800.70	0.852
1	28	804.58	777.40	0. 181	801.28	0.869
1	30	804.95	777.80	0.191	801.74	0.874
	31	805.85	778. 70	0. 212	803. 15	0.898
١	6.1	806.70	779. 15	0. 220	803.70	0.890
	2	807. 10	779.40	0. 224	804. 38	0.902
ļ	4	806.88	778. 55	0. 202	803.69	0.884
	8	806. 75	778. 26	0. 194	803. 28	0.873
	10	806.74	777.70	0.178	803. 42	0.879
	12	806. 94	778. 12	0.189	803. 21	0.865
ı	. 14	807. 10	778.78	0. 207	803. 91	0.885
	16	806.90	778.47	0. 199	803.66	0.882
	20	807.14	779.04	0. 214	803. 72	0.877
	22	806.76	777.85	0. 182	803. 26	0.872
	24	806.80	778. 58	0. 203	803. 25	0.870
		L :				



Uplift U (%) = h/HBasin E.L.

No. 1 =771. 4 No. 2 =779. 4

(6) Stability Calculation

The stability calculations of the dam are checked in cases of the water level WL= 807.0m, 810.5m (design flood water level after rehabilitation) and 809.0m (maximum water level at present) based on the following assumptions

Combination of Load

Case	Gravity Concrete Dam
Maximum water level	- Dead load
and surcharge water	- Water pressure
level	- Dynamic water pressure at
	seismic stage
	- Sediment pressure
	- Seismic inertia force
	- Uplift force
Design flood water	- Dead load
level	- Water pressure
	- Sediment pressure
	- Uplift force

- Dead load

The dead load of existing and proposed dam body is estimated based on the results of laboratory test as follows:

Existing dam body

Mortar specific gravity; 1.8

Stone - ditto - ; 2.2

Proportion of stone ; 50-60 %

Unit weight ; $\gamma = 2.0 \text{ ton/cm}^3$

New dam body

The unit weight is estimated γ = 2.3 ton/cm³ as safe value since no concrete test is executed.

- Water pressure

The water pressure caused by wave is neglected since its influence is quite small.

- Dynamic water pressure and inertias force at seismic stage

Seismic force is considered in case of the occurrence of earthquake with the intensity K=0.15. However, this force does not take into account at the design food water level.

- Sediment pressure

Sediment pressure is considered to operte lower than the actual ground level plus some height due to small sediment volume.

- Uplift force

Triangle load of 50 % of water pressure at upper stream side and 0% at lower stream side is estimated.

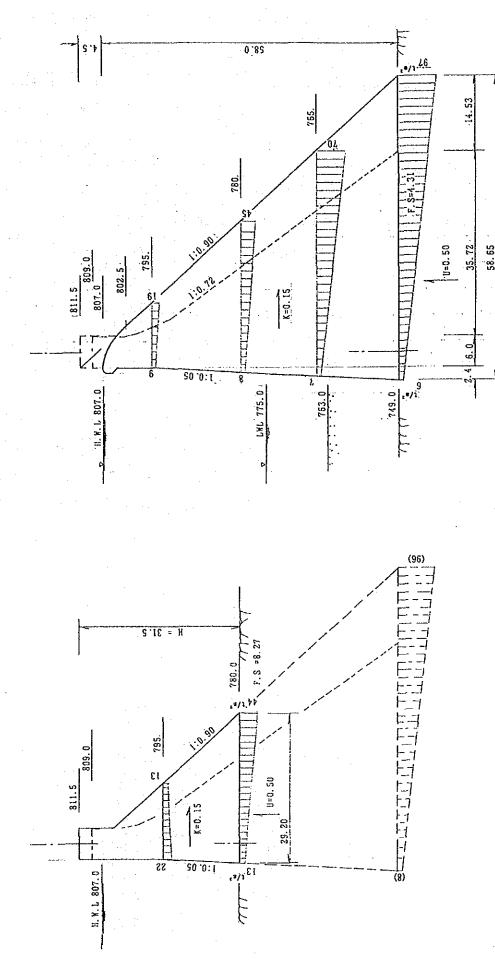


Fig. E.3-5 Results of the Stability Calculation after the Improvement

Table E.3-6 Results of Stability Analysis after Improvement m=0.90

 $K = 0.15 \quad U = 0.50$

		non ~ 0v	erflow Sect	ion			Overflow Se	ction	
		II. W. L = 807					H. W. L. =	807	
	EL=749 B=58.65	EL=765 B=43.45	EL=780 B=29.20	EL=795 B=14.95	EL=780 B=29, 20	EL=749 B=58.65	EL=765 B=43.45	EL=780 B=29. 20	EL=795 B=14, 95
V (t)	3, 073. 9	1, 731. 7	828. 6	263.8	806.1	3, 008. 0	1, 665. 8	762.7	204. 2
И (t)	2, 606. 8	1, 385. 5	609.6	145, 8	465. 1	2, 596. 9	1, 375. 6	599.7	136.9
M (t·m)	115, 394	46, 907	14, 337	1,806	12,798	114, 418	46, 142	13,770	1,717
F. S	4. 32	5. 70	8. 27	16. 83	10. 80	4. 31	5. 71	8. 32	17. 57
1 (m) e (m) p (t/m2) p1(t/m2) p2(t/m2)	98	27.09 5.36 39.9 69 10	17. 30 2. 70 28. 4 44 13	6.85 - 0.63 17.6 13 22	15. 88 1. 28 27. 6 35 20	38. 04 8. 71 51. 3 97 6	27. 70 5. 97 38. 3 70 7	18.05 3.45 26.1 45 8	8. 41 0. 93 13. 7 19 9

Table E.3-7 Stability Calculation at Non-overflow Section (1/5)

m≃0.90

U=0.50 K=0.15

H. W. L=807

E. L=749 B=58. 65

		1000			
	Y	H	У	X	М
WI	24.0		1. 20		29
2	57. 6		0.80		46
D1	115. 2		1.60		184
2	91.8		5. 15		473
3	19.5		9.48		185
4	834.4		7.02		5, 857
5	1, 464, 4		22. 47		32, 905
D11	134. 6		5. 59		752
12	96.8	'	12.12	7	1, 173
13	1,086.0		35.48		38, 531
P		1, 882.0	;	19, 33	32, 513
E		53. 9	, , f	4.67	252
U	-850.4		19.55		-16,625
KD1		17. 3		16.00	277
2	Ì	13.8	!	49.03	677
3	{	2. 9	; !	47. 10	137
4	j	125. 2	† 1 }	22, 55	2, 823
5	1	219, 7		15.03	3, 302
KD11		20. 2	, 1	57. 54	1, 162
12		14.5		49.04	711
13	}	162.9	! ! !	19.64	3, 199
KW		294. 4	! !	23. 20	6,830
			!		
	3, 073. 9	2,606.8			115, 394

Table E.3-7 Stability Calculation at Non-overflow Section (2/5) m=0.90 U=0.50 K=0.15

H. W. L=807 E. L=765 B=43. 45

	V ·	Н	У	X	M
W1	16.0	r g '	0.80		13
2	25. 6		0.53		14
D1	51. 2		1.07		55
2	91.8		4.35		399
3	19.5	*1	8.68		169
4	538. 4		6. 22	1	3, 349
5	609.6		17.83		10,869
D11	134.6		4.79		645
12	96.8		11. 32		1,096
13	604.4		26.98		16, 307
P	1,1-4	882.0		14.00	12, 348
B .		-		_	
U	-456.2		14:48		-6,606
KD1		7.7	} }	10.67	82
2		13.8		33.03	456
3		2.9	! !	31. 10	90
4		80.8	!	14. 55	1, 176
5		91.4	}	9. 70	887
KD11		20. 2	1	41. 54	839
12		14.5	1	33.04	479
13		90.7		13. 14	1, 192
KW		181.5	!	16.80	3, 049
			1	1	
	1, 731. 7	1. 385. 5	1		46, 907

Table E.3-7 Stability Calculation at Non-overflow Section (3/5) m=0.90 U=0.50 K=0.15

H. W. L=807 E. L=780 B=29. 20

	V	H	y	x	Я
WI	8.5		0.42		4
2	7. 2		0.28		2
DI	14.4		0.57		8
2	91.8		3.55		326
2	19.5		7.93		155
. 4	260.8		5. 48		1, 429
5	143.1		13.48	. 1	1, 929
D11	134.6		4.04		544
12	96, 8		10.57		1,023
13	249.0		19.33		4,813
P		364.5	: : :	9.00	3, 281
E		-	, ; ;		-
U	-197.1		9.73		-1,918
KD1		2. 2	: !	5. 67	12
2		13.8	1 F	18.03	249
3		2. 9	:	16. 10	47
4		39. 1	<u> </u>	7.05	276
5		21.5		4.70	101
KD11		20.2	: :	26.54	536
12		14.5	<u>'</u>	18.04	262
13		37.4		6.66	249
KW		93. 5	; ; }	10.80	1,010
	828.6	609.6		į	14, 337

H. W. L=807 E. L=795 B=14. 95

	V	Н	У	x	M
WI	1.0		0.05		. 0.
- 2	0.1		0.03	}	0
D1	0.2		0.07		- 0
2	81.0		2.82		
3	14.1		7.02		99
3 4	· · · · ·	The state	_		4
5	_			1	-
D11	134.6		3, 29		443
12	77.6		9.59		744
13		į	-		-
		72.0		4.00	288
P E		_	1	- !	_
U	-44.8		4. 98	!	-223
KD1		0.0		0.67	. 0
2		12. 2		3.49	43
3		2. 1		1.70	- 4
4					: . <u>.</u> _
5	-				_
KD11		20. 2		11.54	233
12		11.6	•	3.65	42
13	•			- 1	: -
K#		27. 7		4.80	133
				,	
	263.8	145.8			1,806

Table E.3-7 Stability Calculation at Non-overflow Section (5/5) m=0.90 U=0.50 K = -

H. H. W. L=810. 5 E. L=780 B=29. 20

	٧	Н	y	X	. М
W1	11.5		0.42		5
2	7. 2		0.28		2
10	14. 4		0.57		8
2	91.8		3.55		326
2 3	19.5		7. 93		155
4 5	260.8		5.48		1.429
5	143. 1		13.48		1, 929
D11	134.6		4.04		544
12	96.8		10.57	1	1,023
13	249.0		19.33		4,813
P		465.1		10.17	4, 730
3	,		:	-	-
U	-222. 6		9.73		-2, 166
KD1			, ! !		
. 2			; ; ;	. 1	
3				. !	
4				. 1	
5			1 } !		
KD11			:		
12		-	:		
13			; !		
KW					
		:			
	806.1	465. 1	•		12,798

(2/4)

at Overflow Se	U=0.50 K=0.15
y Calculation	1
-8 Stability	Overflow Section m=0.90
Table E.3-	5
on (1/4)	
ion at Overflow Section (1/4) Table E.3-8 Stability Calculation at Overflow Se	U=0. 50 K=0. 15
Calculation	n=0, 90
Stability Calculat	erflow Section
Table E.3-8	ŏ

E. L=749 B=58, 65

H. W. L=807

E. L=765 B-43.45

H. W. L=807

×

H

													-														
×	29	46	184	473	185	5,857	32, 905	듸	302	291	945		32, 513		-16, 625	277	677	137	2,823		45	437	266	527		6,830	114,418
×													19.33	4.67	- • -	ö	တ	~	4	'n		'n	જં	47.90	19.64	8	 -
>-	1.		1. 50						5.77		તાં				19, 55												
izzi													1, 682.0	53.9					125.2		8.0				162.9	9.	2, 596, 9
Λ		<u>.</u> .	115, 2	91.8	19.5	834. 4	1, 464. 4	ςς. Υ	52. 4		ကဲ	1,086.0			-850.4												3, 008. 0
	1,5	~	01	23	က	ব্য	ιņ	D21	22	23	24	D13	ሌ	(T)	5	10	7	m	*#	r.	(D21	22	23	24	m13	KW	

260 263 886 16, 307 12, 348

0,80 0,53 0,53 11,07 11,83 12,74 12,74 26,98

16. 0 25. 6 51. 2 51. 2 91. 8 538. 4 52. 4 34. 1 73. 6

14.00

10.67 33.03 31.10 14.55 9.70 40.66 39.30 36.15 31.90 13.14 16.80

13.7. 13.8. 2.9. 3.1. 3.1. 11.0. 11.0. 181.5.

1, 865.8 1, 375.6

Table E.3-8 Stability Calculation at Overflow Section (4/4) Table E.3-8 Stability Calculation at Overflow Section (3/4) m=0.90 Overflow Section

H W L=807

TT.

		•																										:		. •
							<u> </u>				<u></u>			 	<u></u>	:		-			· .				2	·				
U=0. 50 K=0. 15	B=14, 95	æ	0	0	Ċ	228	66	1	ı	2-	182	212	618	ı	288	ì	-223	0	43	₩.	1	1	O.	73	80	22	1	133		1,717
D=0. 50	E. L=795	×													4.00			0.67	3.49	1. 70	J	1	10.68	9.30	5.15	2.40		4.80		
		>	0.05	0.03	0.07	2.82	7.02	ı	1	-0.34	3.47	6.22	10.18	1.			4.98													
ш=0. 90	H. F. L=807	m .			-,							• • •		~ *-	72.0	1		0.0	12.2	2.1	1	1	8.0	7.9	ι. G	9. 1	1	27.7	(135, 9
Overflow Section	Ħ	٨	1.0	0.1	0.2	81.0	14.1	ľ	1	5.4	52.4	34.1	60.7	ŧ		: .	-44.8			·		:								204. 2 135. 9
Overflow			W1	~	I	2	673	* #	ശ	021	22	23	24	D13	ρ.	сщ	Þ	KD1	63	63	~#	u)	KD21	22	23	24	KD13	X.W.		
•			-											-					-											
	-																													
									٠.					٠				٠												
X=0.15	=780 B=29.20	×	4	63	∞	328	155	1, 429	1, 929	2	221	238	831	4.813	3, 281	1	-1.918	12	249	47	276	101	21	192	108	186	249	1,010		13, 770
=0. 20	=780 I	×							•						9.00	1		5.67	18.03	16, 10	7.05	4. 70	25.66	24.30	21.15	16.90	6.66	10.80		

0.42 0.53 0.53 0.54 113.48 111.29 111.29

> 14.4 91.8 19.5 260.8 143.1 5.4 5.4 34.1 73.6 249.0

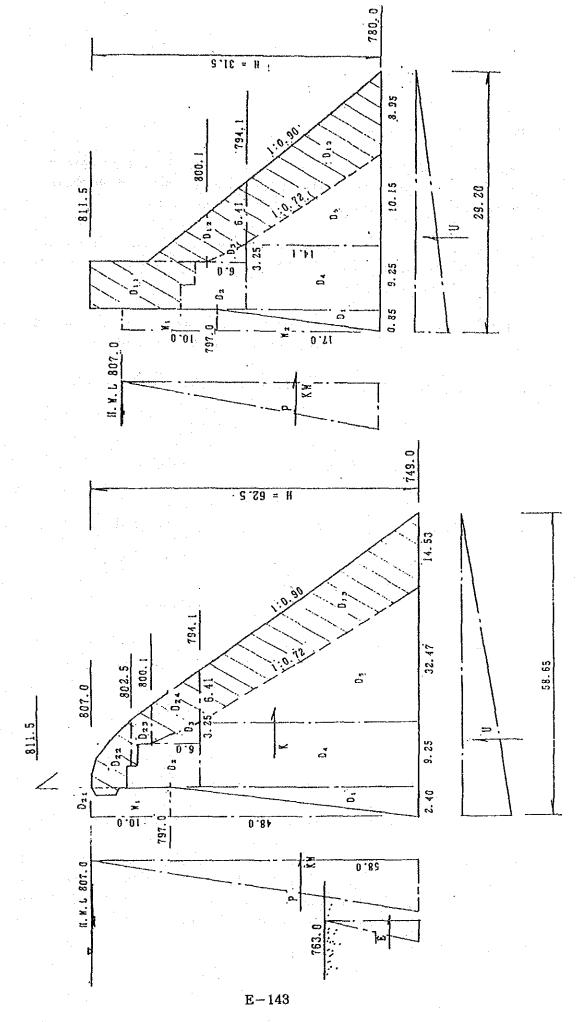


Fig. E.3-6 Dimension of Stability Calculation

(7) Essential Point for Construction

1) Concrete Pouring Season

It is essential to pour concrete in dry season (from November till April), especially at the bottom concrete section which is located at the riverbed side and has maximum width.

The outfall from the Dam reservoir takes place from the outlet pipe ($\phi750\text{mm}$) except when it is discharged from the spillway at the full water level stage.

Raising of the water level occurs due to rainfall in the rainy season on account of its insufficient discharge capacity.

Record of plenty of inflow in the rainy season is shown below.

Increase of storage volume:

	Increase	Discharge	Ħ	Total	Raising	of water
	storage	* * *	(<u> 10³m³)</u>	level	
Maximum (1st)	700 +	7200	ä	7900	775m →	800m
(2nd)	5800 +	500	=	6300	775± →	797m
Medium	3500		=	3500	775m →	791m
Minimum (3rd)	1100		=	1100	775m →	783m

Estimated value

The raising of the water level by rainfall possibly occurs although a decrease of the water level at the outlet pipe during the construction period.

According to the second record:

```
Primary water head = 26m (= 775m - 749m)
Water head after rainfall = 48m (= 797m - 749m)
```

The water head at the bottom of the Dam Increases from 4 kgf/cm² to 10 kgf/cm².

There is some possibility that the raising of the water level disturbs mainly stress transmission between the present and new Dam body and harms their tight connection. Then, it is better to avoid the rainy season for concrete pouring.

2) Construction Condition of Bottom Concrete

As plenty of concrete is poured, the construction period takes a few years.

The primary concrete will stop below the outlet pipe and the upper concrete will be poured after the installation of the outlet pipe.

The stability of the Dam body under this case is checked as follows.

3) Essential points for Grouting

Obvious leakage is observed at the left side of the Dam body and upper chute of the spillway.

The former leakage dissapears at the water level of m790m and similar characteristic is observed with the latter leakage.

Since the grouting point and leakage point are close especially in the former case, it is effective to lower the water level and to weaken the leakage force.

Table E.3-9 Stability Calculation Placing Concrete up to EL 773m

m = 0.90 (E. $L \le 773.0$) m = 0.72 (E. L > 773.0)

			H. W. L = 807 K=0.15				H.W.L = 807 K = -		
		EL=749 B=58.65	EL=773 B=25.64		EL=795 B=8. 86	EL=749 B=58.65		EL=780 B=20. 25	
γ	t	2, 526. 3	746. 6	495. 6	156.8	2, 526. 3	746. 6	495. 6	156.8
H	ŧ	2, 524. 6	850.8	578. 0	139. 5	1.735.9	578. 0	392. 0	84. 5
М	tn	101, 089	16, 498	8,973	1, 221	85, 155	12, 879	6, 949	908
F. S		4. 29	5. 22	. 5. 94	10. 43	6. 23	7.69	8.76	17. 21
l e p p ₁ p ₂	頁 t/g ² t/g ² t/g ²	40. 01 10. 69 43. 1 90 - 4	22. 10 9. 28 29. 1 92 - 34	•	7. 79 3. 36 17. 7 58 -23	33. 71 4. 38 43. 1 62 24		•	

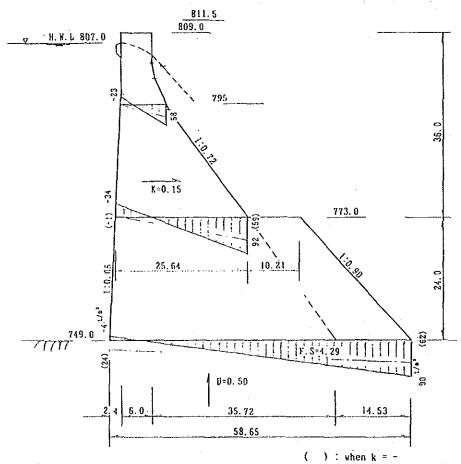


Fig. E.3-7 Stability Calculation Placing Concrete up to EL 773m E-146

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F.1 Irrigation Plan

- (1) Irrigation Water Requirement
- 1) Evapo-transpiration for Crops (Et crop)

Et crop is obtained in the following equation.

Et crop = Kc x ETo

where; Kc : Crop Coefficient

ETo: Evapo-transpiration

The monthly crop coefficient of each crop proposed is tabulated in Table F.1-1 below and detailed analysis of each crop's Kc are in Table F.1-2 (1/3-3/3).

Table F.1-1 Monthly Crop Coefficient

Month	May	Jun	July	Aug	Sept	0ct	Nov.	Dec	Jan	Feb	Mar	Apr
Crops	0.48	0. 68	0.87	0.04	0.84	0. 67	0.00	0.00	0.00	0.00	0.00	0.00
Maize (I)												
Maize (II)	0,00	0.00	0.00	0.00		0.53	0.72		0.94	0.83	0.66	0.00
Maize (III)	0.00	0.00	0.00	0.00	0.00	0.52	0.58	0.78	0.94	0. 91	0,77	0.63
Rice (I)	1.07	1.14	1, 19	1.16	1.10	1.00	0.00	0.00	0.00	0.00	0.94	0. 98
Rice (II)	0.00	0.00	0.00	0.00	0.94	0.98	1.07	1.14	1.19	1.16	1.10	1.00
Tobacco	0.00	0.00	0.00	0.00	0.56	0.79	1.06	1.10	1.03	0.91	0.00	0.00
Soy Bean	0.50	0.63	0.79	0.81	0.85	0.65	0.00	0.00	0.00	0.00	0.00	0.00
Vegeta(A)-1	0.00	0.00	0.00	0.00	0.00	0.56	0.78	0.83	0.91	0.87	0.70	0.00
Vegeta(A)-2	0.00	0.00	0.00	0.00	0.54	0.76	0.82	0.91	0.87	0.70	0.00	0.00
Vegeta(A)-3	0.46	0.66	0.80	0.85	0.92	0.75	0.00	0.00	0.00	0.00	0.00	0.00
Vegeta(A)~4	0.93	0.79	0.00	0.00	0.00	0.00	0.00	0.00	0.52	0.61	0.81	0.83
Vegeta(B)-1	0.00	0.00	0.00	0.00	0.52	0.67	0.78	0.86	0.89	0.80	0.00	0.00
Vegeta(B)-2	0.88	0.78	0.00	0.00	0.00	0.00	0.00	0.00	0.55	0.69	0.79	0.86
Vegeta(B)−3	0.00	0.00	0.00	0.00	0.52	0.63	0.77	0.83	0.89	0.84	0.73	0.00
Fruits	0.85	0.85	0.85	0.85	0.85	0.85	0.85	0.85	0.85	0.85	0.85	0.85
Coffee	1.05	1.05	1.05	1.05	1.05	1.05	1.05	1.05	1.05	1.05	1.05	1.05
Pasture	0.55	0.55	0. 55	0.55	0. 55	0.55	0.50	0.50	0.50	0.50	0, 50	0.50

Table F.1-2 Crop Coefficient (Kc) (1/3)

Maize (I)

	May			June			July			Augu	st		Sep	tembe	r	()c tobi	r .
1	2	3	ī	2	3	1	2	3	1	2	3	1		2	3	1	2	3
0.46					1.05							-,",			, .			
	0,46	0.46	0.60	0.88	1.05	1.05	1,05	1.05	0. 93	0, 77	0. 63	} ``	1.10	1.5		100	111	1.11
					0.88								3	1 4				
			0.46	0,46	0.60	0.88	1.05	1.05	1.05	1.05	0. 93	0.7	7 0.	63		·		
				0.46	0.46	0.60	0.88	1.05	1.05	1.05	1. 05	0.9	3 0.	77.0	63	3.79	Sec. 2. 2	٠.
					0.46	0.46	0.60	0,88	1.05	1.05	1.05	1.0	5 0.	93 0	77	0.63	1.	
						0.46	0.46	0.60	0.88	1.05	1. 03	1.0	5 1.	05 0	93	0. 77	0.63	
0.46	0.46	0.51	0.80	0.69	0 75	0 79	0.88	0 94	N 97	0 93	0.91	n a	g ń	85 f	78	0 70	0.63	

Maize (II)

																	,
	Octobe	r	K	ovenb	er	<u> </u>	Decem	ber		Janu	ary	F	ebrus	гy		March	h .
1	2	3	1	2	3	1	2	3	1.	2	3	1	2	3	1	2	3
0.52	0, 52	0. 65	0. 90	1.05	1.05	1.05	1.05	0.93	0.75	0.63	10.				-		
	0.52	0. 52	0.65	0.90	1.05	1.05	1.05	1.05	0.93	0.75	0.63	100	: 11				
	ē.	0, 52	0.52	0.65	0.90	1.05	1.05	1.05	1.05	0.93	0, 75	0.63			5.1		
		٠	0.52	0.52	0, 65	0.90	1.05	1.05	1.05	1.05	0.93	0, 75	0. 63).	Bre.	1	
				0.52	0.52	0.65	0.90	1.05	1,05	1.05	1.05	0.93	0.75	0.63	40	÷	
					0.52	0.52	0.65	0.90	1.05	1.05	1.05	1, 05	0.93	0.75	0.63	91.	4.0
				1		0.52	0. 52	0.65	0.90	1.05	1.05	1, 05	1, 05	0, 93	0.75	0.63	
0. 52	0. 52	0. 56	0.65	0.73	0.78	0.82	0.90	0. 95	0.97	0.93	0. 91	0.88	0.84	0.77	0.69	0.63	

Maize (111)

(ctob	er		Мо	vem	ber			Decem	ber		Janua	ary	F	ebrua	ry		March			April	
1	. 2	3		i	2		3	1	2	3	1	2	3	1	2	3	1	2	3	i	2	3
		0. 52	0. :	52	0. 6	5 0	. 90	1.05	1.05	1.05	1.05	0.93	0.75	0.63								
			0. 5	52	0.5	2 0	. 65	0.90	1.05	1.05	1.05	1.05	0. 93	0.75	0.63							
					0.5	2 0	. 52	0.65	0.90	1.05	1.05	1.05	1.05	0.93	0.75	0.63				1.		
-2						0	. 52	0.52	0, 65	0.90	1.05	1.05	1.05	1.05	0.93	0.75	0.63	41.57				
								0. 52	0, 52	0.65	0.90	1.05	1.05	1.05	1.05	0.93	0.75	0.63		4.		
									0. 52	0. 52	0.65	0.90	1.05	1.05	1.05	1.05	0.93	0.75	0. 63	. '		
					-1					0.52	0.52	0. 65	0.90	1.05	1.05	1.05	1.05	0.93	0.75	0. 63		
		0.52	0. 9	52	0.5	6 0	65	0.73	0.78	0.82	0.90	0.95	0.97	0.93	0, 91	0.88	0.84	0.77	0. 69	0. 63		

Rice (1)

			<u> </u>		<u> </u>								<u> </u>							
March	April	ļ.		Bay			June			July			Augus	st	S€	ptem	ær		Octob	er
3	2	3	1	2	3	1	2	3	- 1	2	3	. 1	2	3	1	2	3	1	2	3
0. 94 0. 9	34 1. 10	1. 10	1.10	1. 25	1. 25	1. 25	1, 25	1. 25	1. 25	1.00	1.00	1.00	:							
0. 9	14 0. 94	1.10	1.10	1. 10	1. 25	1.25	1. 25	1.25	1.25	1.25	1.00	1.00	1.00	4.7	÷ '	**		-		
	0. 94	0.94	1.10	1.10	1, 10	1. 25	1. 25	1. 25	1. 25	1.25	1.25	1.00	1.00	1.00	100	1				
		0.94	0.94	1. 10	1. 10	1.10	1.25	1. 25	1. 25	1.25	1.25	1. 25	1.00	1.00	1.00					
			0. 94	0. 94	1. 10	1, 10	1, 10	1. 25	1. 25	1.25	1.25	1.25	1. 25	1.00	1.00	1.00	1.1		4.1	
				0. 94	0.94	1. 10	1.10	1.10	1.25	1.25	1.25	1.25	1.25	1. 25	1.00	1.00	1.00		:	
					0.94	0.94	1.10	1. 10	1.10	1. 25	1. 25	1, 25	1, 25	1. 25	1.25	1.00	1.00	1.00	. 5	
						0, 94	0.94	1. 10	1.10	1.10	1. 25	1. 25	1.25	1. 25	1. 25	1.25	1,00	1.00	1.00	
							0.94	0.94	1.10	1.10	1, 10	1. 25	1. 25	1.25	1.25	1. 25	1. 25	1.00	1.00	1.00
0. 94 0. 9	4 0.99	1.02	1.04	1.07	1, 10	1, 12	1.13	1, 17	1, 20	1. 19	1.18	1.17	1.16	1.14	1.13	1.10	1.06	1.00	1,00	1.00

Rice (11)

September	0ctol	ber.		Nov	enb	er		Dece	aber		Janua	ary	Fe	ebrua	У		Harch	1		Аргі	1
3 1	2	3	1	2)	3	ī	Ż	3	. 1	2	3	1	. 2	3	1	2	3	1	2	3
0. 94 0. 94	1.10	1.10	1.10	1. 2	5 1	. 25	1. 25	1. 25	1. 25	1. 25	1.00	1.00	1.00	. ,.							
0. 94	0.94	1.10	1.10	1.1	0 1	. 25	1.25	1, 25	1.25	1. 25	1. 25	1,00	1.00	1.00							-
	0. 94	0.94	1.10	1.1	0 1	. 10	1. 25	1. 25	1. 25	1. 25	1. 25	1. 25	1.00	1.00	1.00						
		0.94	0.94	1.1	0 1	. 10	1. 10	1. 25	1. 25	1.25	1. 25	1.25	1. 25	1.00	1.00	1.00					
			0.94	0. 9	34 1	. 10	1.10	1, 10	1. 25	1. 25	1. 25	1. 25	1. 25	1. 25	1.00	1.00	1.00				
				0. 9													1.00				
					0.												1.00				
							0. 94										1.25				
																	1. 25				
0. 94 0. 94	0. 99	1.02	1.04	1. (7 1	. 10	1. 12	1. 13	1. 17	1. 20	1.19	1.18	1. 17	1.16	1.14	1.13	1. 10	1.06	1.00	1.00	1.00

Table F.1-2 Crop Coefficient (Kc) (2/3)

Septe	aber	Oct	ber			Nove	abe	r		Dece	ber		Janu	ary	Fe	brusi	гу		March	1		April	
3	1	2	3		1	. 2		3	1	. 2	3	1	2	3	1	2	3	1	2	3	1	2	3
0.94	0. 94	1, 1	0 1. 1	0 :	1. 10	1, 25	1,	25	1.25	1. 25	1, 25	1, 25	1.00	1.00	1,00								
	0.94	0.9	4 1.1	0 3	1. 10	1.10	1.	25	1.25	1. 25	1.25	1.25	1.25	1.00	1.00	1.00		100					
		0. 9	4 0.9	4	1. 10	1.10	1.	10	1.25	1.25	1.25	1.25	1. 25	1, 25	1.00	1.00	1.00						
			0.9	4 (). 94	1, 10	1.	10	1.10	1. 25	1.25	1.25	1, 25	1. 25	1, 25	1.00	1.00	1.00					
				(). 94	0.94	1.	10	1.10	1.10	1. 25	1.25	1. 25	1. 25	1, 25	1.25	1,00	1,00	1,00				
						0.94	0.	94	1, 10	1, 10	1.10	1.25	1, 25	1.25	1. 25	1, 25	1, 25	1.00	1.00	1.00			
							0.	94	0.94	1.10	1.10	1. 10	1. 25	1. 25	1. 25	1. 25	1, 25	1.25	1.00	1.00	1,00		
					٠.		٠.		0, 94	0.94	1.10	1, 10	1.10	1, 25	1. 25	1.25	1. 25	1. 25	1.25	1,00	1.00	1.00	
										0.94	0.94	1.10	1, 10	1.10	1. 25	1, 25	1.25	1.25	1.25	1. 25	1.00	1.00	1,00
0.94	0. 94	0. 9	9 1.0	2	1.04	1.07	i,	10	1. 12	1, 13	1.17	1. 20	1. 19	1.18	1, 17	1.16	1.14	1, 13	1, 10	1.06	1.00	1.00	1.00

Tobacco

				100						- :							
S	eptent	er	- 1	octobe	er	N	ovemb	er		Decem	per		Janua	ry	Fe	bruar	у
1	2	3	1	2	3	1	2	3	1	2	3	1	2	3	1	2	3
0. 51	0.60	0.75	0. 95	1.10	1.10	1. 10	1, 10	1, 10	1.10	1, 10	1. 10	0. 95	0.85				
	0.51	0. 60	0.75	0.95	1.10	1. 10	1, 10	1.10	1.10	1, 10	1. 10	1.10	0.95	0.85			
		0.51	0.60	0.75	0.95	1.10	1, 10	1. 10	1. 19	1.10	1.10	1.10	1. 10	0.95	0, 85		
															0.95		
															1.10		
0. 51	0.56	0. 62	0.70	0.78	0. 90	1.00	1. 07	1. 10	1. 10	1. 10	1. 10	1. 07	1.02	1,00	0. 97	D. 90	0. 85

Soy Beans (2 years rotation)

	Ma	rct	i .			A	pri	<u> </u>			May			June			July			Augus	t
1	1	2	3		1		2	3		1	2	3	1	2	3	1	2	3	1	2	3
	0, 1	50	0.5	0	0, 73	Ĩ.	.00	1,00	1,1	00	0.85	0.58		,							
			0.5	Ð	0.50	0	. 73	1,00	1.1	œ	1.00	0.85	0.58								
					0. 50	0	. 50	0.73	1.	00	1.00	1.00	0.85	0.58		٠					
						0	. 50	0.50	0.	73	1.00	1.00	1,00	0.85	0. 58	:					
								0, 50	0.	50	0.73	1.00	1.00	1.00	0. 85	0.58					
									0.	50	0.50	0.73	1.00	1,00	1.00	0.85	0.58				
											0.50	0.50	0.73	1.00	1.00	1.00	0. 85	0. 58	i		
												0.50	0.50	0.73	1.00	1.00	1, 00	0, 85	0.58		
											4	2.00	0.50	0.50	0.73	1,00	1,00	1,00	0.85	0.58	
	0.	50	0. 5	n	0. 58	0	. 55	0.75	0.	79	0.80	0.77	0, 77	0.81	0.86	0.89	0.86	0.81	0.72	0.58	

Vegetables (A)-1

	Cctob	er	N	ovesb	61.		Dece∎	ber		Janu	ary	F	ebrua	ry		March	
1	2	3	1	2	3	1	2	3	1	2	3	1	2	3	1	2	3
	0. 52	0. 52	0.77	1.05	1.05	1, 05	0. 90	0.70									
		0.52	0. 52	0.77	1.05	1, 05	1.05	0.90	0.70								
			0. 52	0.52	0.77	1.05	1.05	1.05	0.90	0.70							
				0.52	0.52	0.77	1.05	1.05	1.05	0.90	0.70						
					0.52	0.52	0.77	1.05	1.05	1.05	0.90	0.70					
						0.52	0.52	0.77	1.05	1.05	1.05	0.90	0.70		-		
							0.52	0.52	0.77	1.05	1.05	1.05	0.90	0.70			
							. 17	0.52	0.52	0.77	1.05	1.05	1.05	0.90	0.70		
								**	0.52	0.52	0.77	1.05	1.05	1.05	0. 90	0.70	
_	0.52	0.52	0.60	0. 72	0.78	0.83	0.84	0.82	0.82	0.86	0.92	0.95	0. 93	0.88	0.80	0.70	

Vegetables (A)-2

S	epte	ibe	r		(ctol	er		N	ove#b	er		Deces	ber		Jar	nuai	ry	Fe	bruar,	у
1	2		3 -		1	2		3	1	2	3	1	2	3	1	1	2	3	1	2	3
0. 51	0.5	1 0	. 74	1.	05	1. 05	1.	05	0. 90	0.70											
	0. 5	1 0	. 51	0.	74	1.03	1.	05	1.05	0.90	0.70			1							
		0	. 51	0.	51	0.74	1.	05	1.05	1.05	0.90	0.70	1 1								
				0.	51	0.51	0.	74	1.05	1.05	1.05	0. 90	0.70)*					•		
						0.51	0.	51	0.74	1.05	1.05	1, 05	0.90	0.7)						
							0.	51	0.51	0.74	1.05	1.05	1.05	0. 9	0.70) .					
									0.51						5 (), 9(3.00			
										0.51					5 1.09						
					٠						0.51	0. 51	0.74	1.0	5 1. OS	i 1. ()5 (). 9 0	0. 70		
51	0.5	1 0	50	n	20	0 22	n	22	0 03	0. 81	n #1	0.00	0.02	0 0	ፍ በ Qʻ	t n s	RR (1 20	0.70 (กกก	

Table F.1-2 Crop Coefficient (Kc) (3/3)

May	June		July		Augus		Septe	mber .	October
1 2	3 1 2	3 1	2 3	1	2	3	1 2	3	1 2 3
0.46 0.4	16 0.73 1.05	1.05 1.05	0. 90 0. 70)					
	16 0.46 0.73						J. 1		
	0.46 0.46	0.73 1.05	1.05 1.0	5 0. 90	0.70	1		4.14	A 1.
		0.46 0.73					25.44	1.742	No. of the second
		0.46 0.48	0.73 1.0	5 1.05	1.05	. 90 0	. 70	ويمرفن	Action to the second
			0.46 0.73						
		184							
			0.40						
	1					7			
0.45 0.4	16 0.55 0.68								

Vegetables (A)-4

	Janu	ary		F	ebrua	iry		Marc	h		Apri	1		May			June	
1	2	3		1	2	3	1	. 2	3	1	2	3	į	2	3	1	2	3
		0. 52	0.	52	0.77	1.05	1.05	1.05	0, 90	0.70	1. 30			٠.			. :	
			0.	52	0.52	0.77	1.05	1.05	1.05	0, 90	0.70	30.0	- 1					
					0.52	0.52	0.77	1.05	1.05	1, 05	0, 90	0.70	7.6	100		:		
						0.52	0. 52	0.77	1.05	1.05	1.05	0.90	0.70	+ E .	1.			
•											1.05				- 6	eti.,	. :	
								0.52	0.52	0.77	1.05	1.05	1, 05	0.90	0.70	Arriva.		-
									0.52	0.52	0.77	1.05	1.05	1.05	0.90	0.70		
									1	0, 52	0. 52	0.77	1.05	1.05	1.05	0. 90	0. 70	43
															1.05			0. 7
		0.52	fi	52	0.60	0.71	0.78	0.82	0.83	0 82					0.92			n

Vegetables (B)-1

September	October	November	December	January	February
1 2 3	1 2 3	1 2 3	1 2 3	1 2 3	1 2 3
0. 51 0. 51 0. 60	0. 83 0. 95 0. 95	0. 95 0. 95 0. 88	0. 73		
0.51 0.51	0,60 0,83 0,95	i 0.95 0.95 0.95	0, 88 0, 73		
0. 51	0. 51 0. 60 0. 83	0. 95 0. 95 0. 95	0. 95 0. 88 0. 73	artagin .	1. A. A.
	0.51 0.51 0.60	0, 83 0, 95 0, 95	0.95 0.95 0.88 (3.73	1.0
	0.51 0.51	0.60 0.83 0.95	0. 95 0. 95 0. 95 (3. 88 0. 73	200
	0. 51	0, 51 0, 60 0, 83	0. 95 0. 95 0. 95 (1, 95 0, 88 0, 73	1
		0.51 0.51 0.60	0.83 0.95 0.95 (. 95 0. 95 0. 88	0.73
	4.04		0, 60 0, 83 0, 95 (
	1.0		0.51 0.60 0.83 (
0. 51 0. 51 0. 54	0. 61 0. 68 0. 73		0. 82 0. 86 0. 89 (

Vegetables (B)-2

																			_				7								
	Jan	uar	y		F	ebi	นล	У				Marc	h				A	ri.	1			Ma	y					June	:		-
1	2		3		1		2	-	3		1	2		3		1		2	3		1		2	-	3		1	2		3	7
0. 54	0.5	4 0.	65	0.	85	Õ.	95	0.	95	0.	95	0. 95	0,	87	Ō.	72			-,		5	_									-
	0.5	4 0.	54	0.	65	0.	85	0.	95	0.	95	0.95	0.	95	0.	87	0.	72			:		2.1							•	
		0.	54	0.	54	0.	65	O.	85	0.	95	0.95	0.	95	0.	95	O.	87	0. 7	2											
				0.	54	0.	54	0.	65	0.	85	0.95	0.	95	0.	95	0.	95	0.8	7 (1.72	×,	1.	:	:						
						0.	54	0.	54	0.	65	0.85	0.	95	0.	95	0.	95	0. 9	5 (). 87	0.	72	٠,							
								0.	54	0.	54	0.65	0.	85	O.	95	0.	95	0. 9	5 (). 95	0.	87	0.	72						
										0.	54	0.54	0.	65	0.	85	0.	95	0. 9	5 1). 95	0.	95	0.	87	0.	72				
												0.54	0.	54	0.	65	Ö,	85	0.9	5 (). 95	0.	95	O.	95	Û.	87	0. 72			
													0.	54	0.	54	0.	65	0.8	5 (). <u>9</u> 5	Ð.	95	0.	95	0.	95	0.87	0	. 72	
0.54	0.5	4 0	57	ñ	64	n	70	n	74	Û	77	N 70	n	รัก	n	82	ñ	88	n a	0 1	1 80	ī	RR	fì	87	n	24	0 70	Ñ	72	-

Vegetables (B)-3

												:						
Se	ptember			Octob	er	М	ove≊b	er		Decem	ber		Janu	ary	Fel	ruary		March
1	2	}	1	2	3	1	2	3	1	2	3	1	2	3	1	2	3	1
	0.52 0.5	2 (. 63	0.84	0. 95	0. 95	0, 95	0.95	0.87	0.73		81,						
	0. 9	2 0	. 52	0.63	0.84	0, 95	0, 95	0.95	0.95	0.87	0.73	- 1	1.0					
										0.95			es,					
				0.52	0.52	0.63	0, 84	0.95	0.95	0.95	0.95	0.87	0.73		110			
					0. 52	0.52	0.63	0.84	0. 95	0.95	0.95	0.95	0. 87	0.73	Lagar Teach			
										0.95								
															0.87 0	73		
															0. 95 0		3. 73	
								•							0.95 0			
	0. 52 0. 9	2 0	. 56	0.63	0. 69	0.74	0.77	0.79										

In accordance with the proposed cropping pattern, monthly ETcrop of each proposed crop are obtained and summarized in Table F.1-3 by equation stated above based on 10 days ETcrop tabulated in Table F.1-4 (1/3-3/3).

Table F.1-3 Monthly Evapotranspiration by Crops

													(Unit: mm)
Month	May	Jun	July	Aug	Sept	0ct	Nov	Dec	Jan	Feb	Mar	Apr	Total
Crops									· · · · · · · · · · · · · · · · · · ·				
Maize (I)	68. 9	87. 7	116.7	124.6	99. 3	51.9	0.0	0.0	0.0	0.0	0.0	0.0	
Maize (II)	0.0	0.0	- 0.0	0.0	0.0	61.3	66. 9	88. 2	103.8	ୀ04. 4	61.1	0.0	485.7
Maize (III)	0.0	0.0	0.0	0.0	0.0	19. 2	53.6	76.9	104.6	114. 2	111.8	33. 4	513.7
Rice (I)	154.9	147. 1	159.5	153.9	129. 5	115.0	0.0	0.0	0.0	0.0	50.8	154.3	1,064.9
Rice (11)	0.0	0.0	0.0	0.0	35.7	113.0	98.7	112.9	132.0	145.7	160.8	157.0	955. 9
Tobacco	0.0	0.0	0.0	0.0	66.3	91.0	97.8	108.9	114. 1	114. 1	0.0	0.0	592. 2
Soy Bean	47.0	80.8	105.4	108.1	100.8	50.7	0.0	0.0	0.0	0.0	0.0	0.0	492. 9
Vegeta(A)-1	0.0	0.0	0.0	0.0	0.0	42. 5	72.0	81.8	101.3	109.4	29.4	0.0	436. 5
Vegeta(A)-2	0.0	0.0	0.0	0.0	63. 2	87.7	75.0	90. 1	96. 1	28. 7	0.0	0.0	440.8
Vegeta(A)-3	43. 2	85.1	107.7	113.4	108.7	58.5	0.0	0.0	0.0	·· 0.0	0.0	0.0	516.6
Vegeta(A)-4	134.9	102.3	0.0	0.0	0.0	0.0	0.0	0.0	21. 3	77. 2	119.4	130.8	585. 9
Vegeta(B)-1	0.0	0.0	0.0	0.0	61.3	77. 3	71.6	84.8	98. 7	100. 2	0.0	0.0	494.0
Vegeta(B)-2	127.7	101.1	0.0	0.0	0.0	0.0	0.0	0.0	61. 2	87. 5	115.8	134.5	627.7
Vegeta(B)-3	0.0	0.0	0.0	0.0	40.0	71.9	70.8	81.9	99. 1	106. 1	30.7	0.0	500.6
Fruits	123.3	109.6	113.9	113.1	100.3	97.8	78. 2	84.1	94. 4	107.1	125.0	133.5	1, 280. 1
Coffee	152.3	135.5	140.7	139.7	123.9	120.8	96.6	104.0	116.6	132. 3	154. 4	164.9	1, 581. 3
Pasture	79.8	71.0	73.7	73. 2	64.9	63, 3	46.0	49.5	55. <u>5</u>	63.0	73. 5	78.5	791.7
Total	931.9	920. 2	817.5	825. 9	994.0	1, 121.8	827.3	963. 2	1, 198.6	1, 289.8	1,032.6	986.8	11, 909. 5
Average	103. 5	102. 2	116.8	118.0	82. 8	74.8	75. 2	87.6	92. 2	99. 2	93. 9	123.4	1, 169. 6

May 2 5 0 0 6 2 35															
Month days ETO Maize (I) Maize (III) Maize (III) Rice (I) Rice (II) Tob									e stiller Vijite (a.)						
Month days ETO		12 1	a.	Evinno	tunnen	irati	on (Et	eron)	hv Cr	rops	(1/3)		227	·	•
Month Image	# F	L.T	-4	Evapo	rt ansp	11 061	On (EC	CLOP	<i>0</i> , 01	ОРО	,,,,,	3	(u	nit: 1	m/day)
May	1	10	1.2	Ma	ize (I)	Maiz	ze (II)	Maize	(III)	Ric	ce (I)	Rice	e (II)	Tol	bacco
May	da	lays	ETo	Kc	ETcrop	Ke	ETcrop	Kc ·	ETcrop			Kc	ETcrop	Kc	ETcrop
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Table Tabl								÷	£1			*.			÷
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34 5.3 0.63 3.34 0.94 4.98 1.00 5.30															A
Apr 35 5.2 0.99 5.15 1.00 5.20															
36 5.2 1.02 5.30 1.00 5.20										1.02	5.30	1.00	5. 20		

Table F.1-4 Evapotranspiration (Etcrop) by Crops (2/3)

10010	1 4		u upo v											m/day)
	10		Soy	Bean	Vege	ta(A)-1	Vege	ta(A)-2	Vege	ta(A)-3	Vege	ta(A)-4	Veget	ta(B)-1
Month	days	ETo	Kc	ETcrop	Kc	ETcrop	Kc	ETcrop	Kc	ETcrop	Kc	ETcrop	Kc	ETcrop
	1	5. 1			÷					and the second	0.92	4.69		
May	2	5.0	0.50	2.50	٠				0.46	2.30	0.95	4.75		
	3	4.4	0.50	2.20	_				0.46	2.02	0.92	4.05		
	4	4.3	0.58	2.49					0.55	2.37	0.88	3.78		
Jun	5	4.3	0.55	2.37				4	0.68	2.92	0.80	3, 44		
	6	4.3	0.75	3.23					0.75	3.23	0.70	3.01		
	7	4.4	0.79	3.48				:	0.80	3.52				<u> </u>
July	8	4.5	0.80	3.60		1.			0.81	3.65			*	
	9	4.5	0.77	3.47					0.80	3.60		•		
	10	4.5	0.77	3,47				· -	0.80	3.60			· · · · · · · · · · · · · · · · · · ·	
Aug	11	4.4	0.81	3,56					0.85	3.74				
	12	4.4	0.86	3.78	11	i t			0.91	4.00		٠		
	13	4.1	0.89	3.65		· # · · · · · · · · · · · · · · · · · ·	0.51	2.09	0.95	3.90			0.51	2.09
Sept	14	3.9		3.35			0.51	1.99	0.93	3.63			0.51	1.99
· ·	15	3.8	0.81	3.08			0.59	2.24	0.88	3.34			0.54	2.05
	16	3.9	0.72	· · · · · · · · · · · · · · · · · ·			0.70	2.73	0.80	3.12	_	,	0.61	2.38
0ct	17	3.9		2, 26	0.52	2.03	0.77	3.00	0.70	2,73			0.68	2.65
	18	3.7			0.60	2, 22	0.82	3.03					0.73	2.70
**************************************	19	2.4			0.72	1.73	0.83	1.99				•	0.76	1.82
Nov	20	3.4			0.78	2.65	0.81	2.75					0.78	2.65
	21	3.4			0.83	2.82	0.81	2.75					0.79	2.69
	22	3.3	, i ·		0.84	2,77	0.86	2, 84					0.82	2.71
Dec	23	3.2	٠		0.82	2.62	0.92	2.94					0.86	2.75
		3.4	: -		0.82	2,79	0.95	3, 23				•	0.89	3.03
	25	3.4			0.86	2.92	0.93	3.16					0.9	3.06
Jan	26	3.6			0.92	3.31	0.88	3.17					0.89	3.20
	27	4.1	v		0.95	3.90	0.80	3.28			0.52	2,13	0.88	3,61
	28	4.1			0.93	3.81	0.70	2.87			0.52	2.13	0.85	3.49
Feb	29	4.1	1		0.88	3.61		• .			0.60	2.46	0.81	3.32
	30	4.4			0.80	3, 52					0.71	3.12	0.73	3.21
	31	4.2				2.94					0.78	3, 28		
Mar		5.1		1.5		•					0.82	4.18		
		5.4	11								0.83	4.48		
		5.3	•								0.82	4.35		
Apr		5. 2		1							0.82	4.26		
~-F-		5.2								4	0.86	4.47		
	···													

Table F.1-4 Evapotranspiration (Etcrop) by Crops (3/3)

	10		Vosc	- (g) - o	Monat	-0(B)-0	17.	mita		offee	Dog	m/day)
	10	TATI	vege	RT	vege	la(D)-3	n~ L1	Ducasa Ducasa	V.	OTIES	ra: Vo	LLODOL Sente
month					NC NC	dorora				ETcrop		
u	1	5.1	0.89	4, 54			0.85	4, 34		5.36		2, 81
May	2	5.0		The second second			0.85	4. 25	1.05	5 (4) A		2.75
		4.4		3,83			0.85					2.42
	4	4, 3		3, 61			0.85		1.05	1.00		2.37
Jun	5	4.3		3.40	-		0.85	3.66	1.05			
	6	4.3	0.72	3.10		· .	0.85	3,66	1,05			
. · .	7	4.4		, P			0.85	3.74	1.05	4 474		
July	8	4.5		٠.,	.*	•	0.85	3, 83	1.05			2.48
	9	4.5					0.85		1,05			2.48
	10	4.5				•	0.85	3.83				2.48
Aug	11	4.4					0.85	3, 74				2.42
 -	12	4.4					0.85	3.74				2,42
	13	4.1			۰. ۲۵	0.00	0.85		1.05		1 to 10 to 1	2.26
Sept	14	3.9			0.52			3.32	1.05			2.15
<u>.:</u>	15	3.8			0.52			3, 23	1.05			2.09
	16	3.9			0.56			3.32	1.05			2. 15
0ct	17				1	2,46			1.05			
	18	3.7			0.69	· · · · · · · · · · · · · · · · · · ·		3.15				2.04
	19	2.4				1.78	4.1		1.05		0.50	
Nov	20	3.4			0.77	2.62	0.85	2, 89		3.57	0.50	1.70
	21	3.4			0.79			2,89		3.57	0.50	1.70
D	22	3.3			0.80		0.85		1,05		0.50	1.65
Dec	23	3.2			0.82			2, 72		3.36	0.50	1.60
· · · · · · · · · · · · · · · · · · ·	24	3.4	0.54	1 04	0.86		0.85			3.57	0.50	1,70
7	25	3.4	0.54	1.84	0.89					3.57	0.50	1.70
Jan	26	3.6	0.54	1, 94	0.90	3, 24	0.85			3.78	0.50	1.80
	27	4.1		2.34	0.89		0.85			4, 31	0.50	2.05
11. 1	28	4.1	0.64	2.62	0.88					4.31	0.50	2.05
Feb	29		0.70	2.87	0.85					4.31	0.50	2.05 2.20
	30		0.74		0.80					4.62		
W	31		0.77	3, 23	0.73	3, 07	0.85	3.57	1.05	4.41	0.50	2.10
Mar	32		0.79	4.03			0.85	4.34	1.05	5.36	0.50	2.55
	33		0.80	4.32			0.85	4, 59	1.05	5, 67	0.50	2,70
	34		0.82	4.35			0.85	4.51	1.05	5. 57	0.50	2.65
Apr	35	5.2	0.86				0.85	4.42	1.05	5.46	0.50	2.60
	36	5.2	0.89	4.63			0.85	4.42	1.05	5.46	0.50	2,60

2) Irrigation Method

Intake Rate test was carried out at five points of representative soil series in the Study Area. The results of the field intake rate tests are tabulated in the following Table F.1-5.

Table F.1-5 Result of Intake Rate Test

No. Test		Soil Series	Accumulated Infiltration (mm)	Intake Rate (mm/hr)	Basic Intake Rate (mm/hr)
1.		PM	D=9.9T0.58	I=345T-0.4	² 34
2.		COM	D=4.4T ^{0.59}	I=156T-0.4	16
3.	3°	CAN	D=7.4T0.58	I=258T-0 4	² 67
4.		LEP	D=3.6T0.66	I=143T-0.3	4 23
5.		MOC	D=9.0T0.60	I=270T-0.5	⁶ 16
	9 (1 1			Average	31.2

3) Effective Rainfall

Evapotranspiration and precipitation ratio method by USDA stated in the FAO report described previously is employed in this report.

The result of the calculation is shown in Table F.1-6 below.

Table F.1-6 Effective Rainfall

	1.1	3 31	Yang in		<u> </u>						•	(Unit:	mm)
Month	May	Jun.	July	Aug.	Sept.	Oct.	Nov.	Dec.	Jan.	Feb.	Mar.	Apr.	Total
Rainfall													
(1945-88)	129.3	170.3	104.3	125.8	171.8	106.9	25. 2	6. 2	1.8	6. 2	7. 2	33.4	888. 4
Average													
ETcrop	103.5	102. 2	116.8	118.0	82.8	74.8	75. 2	87.6	92. 2	<u>9</u> 9. 2	93. 9	123.4	1, 169. 6
*Effective	84. 9	101.3	73.3	86. 4	82.8	67.3	17.6	4.4	1. 2	6.2	5. 1	25.0	
Rainfall													
(Corrected) **	81.8	97. 6	70.6	83. 2	79.7	64.8	16.9	4. 2	1. 2	6.0	4. 9	24. 1	
Effective			_										
Rainfall	80	95	70	80	75	60	15	0	0	5	0	20	500
(Employed)													

Note *: Evapotranspiration/precipitation ratio method (by USDA)

^{**} The correction factor for effective storage is 0.963. (soil water storage 60 mm)

4) Irrigation Efficiency

Taking into account the topographical feature, canal structure, distribution system, irrigation method, irrigation system and so on, irrigation efficiency is estimated in accordance with FAO guideline as below:

Ea: Field Application Efficiency ratio between water directly available to the crop and that received at the field inlet

Eb: Field Canal Efficiency ratio between water received at the field inlet and that received at the field inlet

Ec: Conveyance Efficiency ratio between water received at inlet to a block of fields and that released at the project headworks.

Ep: Project Efficiency ratio between water made directly available to the crop and that released at the headworks, or Ep=Ea x Eb x Ec

Factors affecting conveyance (Ec) are, amongst others, size of the irrigated acreage, size of rotational unit, number and types of crops requiring adjustments in the supply, (Eb) is affected primarily by the method and control of operation, the type of soils in respect of the seepage losses, length of field canals, size of the irrigation block and the fields. As can be expected the distribution efficiency (Ed) has been shown to be particular sensitive to quality of technical as well as organizational operation of procedures (Ed = Ec·Eb). Farm efficiency (Ef) is much dictated by the operation of the main supply system in meeting the field supply requirements as well as by the irrigation skill of the farmers.

Table F.1-7 Conveyance (Ec), Field Canal (Eb), Distribution (Ed) and Field Application Efficiency (Ea)

Conveyance Efficiency (Ec)		
Continuous supply with no su	ubstantial change in flow	0.9
Rotational supply in project	ts of 3,000 - 7,000 ha and	
rotational areas of 70 -	300 ha, with effective management	0.8
Rotational supply in large	schemes (>10,000 ha) and small	
schemes (<1,000 ha) with	respective problematic communicati	lon
and less effective manage	ement:	
	based on predetermined schedule	0.7
	based on advance request	0.65
atata kana		
Field Canal Efficiency (Eb)		
Blocks larger than 20 ha:	unlined	0.8
	lined or piped	0.9
Blocks up to 20 ha:	unlined	0.7
	lined or piped	0.8
	en en en en en en en en en en en en en e	
Distribution Efficiency (Ed =	Ec·Eb)	
Average for rotational suppl	y with management and	
	communication adequate	0.65
Francis Cognitive Constitution	sufficient	0.55
Million Committee Committee	insufficient	0.40
	poor	0.30
Field Application Efficiency ((Ea) USDA US(SCS)	
Surface methods		
	light soils 0.55	
	medium soils 0.70	
	heavy soils 0.60	
	graded border 0.60-0.75	0.53
·	basin and level border 0.60-0.80	0.58
•	contour ditch 0.50-0.55	
	furrow 0.55-0.70	0.57
	corrugation 0.50-0.70	
Subsurface	up to 0.80	
Sprinkler, hot dry climate	0.60	
moderate climate	0.70	0.67
humid and cool	0.80	
Rice		0.32

Source: ICID/ILRI

	Ea	Eb	Ec	Ep
Furrow Irrigation	0.60	0.90	0.85	0.46

5) Irrigation Water Requirement

The monthly, seasonal, and yearly irrigation water requirements for Sector I and Sector II can be determined for each proposed crop based on the crop requirement, effective rainfall, cropping area for each crop shown in Table F.1-8, 9 and irrigation efficiency by using following equation.

 $W.R = (A \times Net Et crop)/(1 - Lr) \times 10/Ep$

where;

A : Irrigation area (ha)

Net Et crop : Eto-Pe

ETo : Crop Water Requirement (mm)

Pe : Effective Rainfall (mm)
Ep : Irrigation Efficiency

that I have a

Lr : Leaching Water Requirement

However, no leaching water requirement is considered in this Project in accordance with results of soil and water quality test.

The result of the 10 days, monthly, seasonal and yearly water requirement calculation for Sector I and Sector II are summarized in Table F.1-10 and irrigation requirement by crops for Sector I and Sector II are shown in Table F.1-11 and 12 respectively. Water Requirement for each crop in Sector I and Sector II are shown in Table F.1-13 to 46.

Table F.1-8 Irrigation Area by Crops in Sector I

	10				er ger			Na	мė	(of		ro	o s				•	_TOTA
Month	day		В	C	D_	E	F	G	H	<u>I</u> _	J	K	L	M	N	0	P	Q	(ha)
	1	13			185							77		77		34		34	43
May	2	40			226			7			7	63		63		34	19	34	49
	3	67			267			21			21	49		49		34	19	34	56
	4	94		٠	308			35	-	٠	35	35	-	35		34	19	34	62
Jun	5	120			329		•	49			49	21		21		34	19	34	67
	6	147			329			63			63	7		7		34	19	- 34	70
:	7	161			329			77	_		17					34	19	34	73
July	8	161			329			91			91					34	19	34	75
1.0	9	161			329			105			105					34	. 19	34	78
	10	161			329			105			105					34	19	34	78
Aug	11	161			308			91			91					34	19	34	73
	12	147	\$ ·		267			77		* •. •	77		1.1.3			34	19	34	65
:	13	120			226		4	63		7	63		7			34	19	34	57
Sept	14	94			185		.11	49		21	49		20		7	34	19	34	52
	15	67			144	10	19	35		35	35		34		21	34	19	34	48
	16	40	7		103	31	26	21		49	21		47		35	34	19	34	46
0ct	17	13	19		62	52	30	: 7	7	63	7		61		49	34	19	.34	45
	18		33	7	21	72	30	-	20	77		•	74		63	34	19	34	48
	19		46	21	• •	82	30		34	91			88		77	34	19	34	55
Nov	20		59	34	1	82	30		47	105			102		91	34	19	34	63
	21		72	48		82	30	-	61	105	÷		108		105	34	. 19	34	69
	22		79	62		82	30		74	91			108		112	34	19	34	72
Dec	23		79	76		82	30		88	77	٠		102		112	34	19	34	73
	24		79	82		82	30		102	63			88		105	34	19	34	71
	25		79	82		82	30		102	49			74	7	91	34	19	34	68
Jan	26		79	82		82	30		88	35			61	21	77	34	19	34	64
,	27		72	82		82	26		74	21		.7	47	35	63	34	19	34	59
	28		59	82		82	19		61	7		21	34	49	49	34	19	34	54
Feb	29		46	76		72	11		47			35	20	63	35	34	19	34	49
ŧ	30		33	62		52	4		34			49	7	77	21	34	19	34	42
	31		19	48		31			20			63		91	7	34	19	34	36
Mar	32		7	34		10			7			77		105		34	19	34	32'
	33			21	21							91		112		34	19	34	33
	34			7								105		112		34	19	34	37
Apr	35			4 J. J	103							105		105		34	19	34	399
•	36				144							91		91		34	19	34	413
A:	Maiz	e (1	[)	B:	Maiz	e (I	I)	C:	Maiz	e (1	(II)	D:	Rice	· (I))	E:	Rice	(II)	
F;	Toba				Soy				Vege				Vege				Vege		
K:	Vege	**	1)-4		Vege				Vege				Vege				Frui		
D.	Coff		,		Dact								_	-					

P:

Coffee Q: Pasture

Table F.1-9 Irrigation Area by Crops in Sector II

	10	·				+ -		No	мe		of	<i>.</i> .	c o	n 0				(0111	t: ha) TOTAI
Month		- A		C	D	E	F	G	Н		J	K	L	P S M	N	0	P	Q	-
11011011	1	23		<u> </u>	310				**			129		129		56	31	56	734
May		68			379		1.	12			12	106		106		56	31	56	820
******		112			448			35			35	82		82		56	31	56	93
		157			517	-		59		100	- 59	59		59		56	31	56	1,05
Jun		202		•	551			82			82	35	٠	35		56	31	56	1, 13
		247			551			106			106	12		12		56	31	56	1,17
		269			551			129			129					56	31	56	1, 22
July		269			551			153			153					56	31	56	
		269			551			176		:	176					56	31	-56	1,31
		269			551			176			176		٠.			56	31	56	1,31
Aug		269			517			153			153					56	31	56	1, 23
		247	.*		448		*	129			129					56	31	56	1,09
		202			379		6	106		12			11			56	31	56	96
Sept	14	157			310		19	82		35	82		34		12	56	31	56	87
		112			241	18	31	59		59	59	7	57		35	56	31	56	81
 -	16	68	11		172	51	44	35		82	35	· · · · · · · · · · · · · · · · · · ·	80		59	56	31	56	78.
0ct	17	23	33		103	86	50	12	11	106	12		102		82	56	31	56	76
	18		55	11	34	120	50		34	129			125		106	56	31	56	80
Attitude to the second termination in	19		76	34	-	138	50		57	153		:	148		129	56	31	56	92
Nov	20		99	58		138	50		80	176	٠.		170		153	56	31	56	1,06
-	21		120	80		138	50		102	176			182		176	56	31	56	1, 16
^	22		131	103		138	50		125	153			182		188	56	31	56	1, 21
Dec	23	-	131	126		138	50		148	129			170		188	56	31	56	1, 22
	24		131	138		138	50		170	106		٠.	148	3 -	176	56	31	56	1, 20
	25		131	138		138	50		170	82			125	12	153	56	31	56	1, 14
Jan	26		131	138		138	50		148	59			102	35	129	56	31	56	1,07
	27		120	138	·	138	44		125	35		12	80		106	56	31	56	999
	28		99	138		138	31		102	12		35	57	82	82	56	31	56	920
Feb	29			126		120	19		80			59		106	59	56	31	56	82
·	30		55	103		86	6		57			82	11	129	35	56	31	56	70
	31		33	80		51			34			106		153	12	56	31	-56	61
Mar	32		11	58		18			11			129		176	-	56	31	56	54
	_33				. 34							153		188	<u>.</u>	56	31	_56_	55
	34			11	103							176		188		56	31	56	62
Apr	35				172							176		176		56	31	56	66
	36				241				·			153		153		56	31	56	69
A:		ze (ze (1						D:						(11	•
p •	Toba	2000		G.	Sov	Rear	}	H:	Veg	eta(/	A)-1	T:	Veg	eta(/	1)-2	J:	Vege	ata (A)-3

F: Tobacco G: Soy Bean H: Vegeta(A)-1 I: Vegeta(A)-2 J: Vegeta(A)-3

K: Vegeta(A)-4 L: Vegeta(B)-1 M: Vegeta(B)-2 N: Vegeta(B)-3 O: Fruits

Table F.1-10 Summary of Water Requirements by Sector

		Secto	r I	Sector	11	TOT	Αl
	10	Water Requ	irement	Water Requ		Water Requ	iremeni
Month	days	(NCM)	(m3/s)	(MCM)	(m3/s)	(m3/s) ((1/s/ha)
	1	0.193	0,446	0.323	0.747	1, 192	0. 55
Жаў	. 2	0.204	0.472	0.342	0.791	1. 263	0. 590
	3	0.167	0.386	0. 279	0.646	1.032	0.48
	4	0.126	0.291	0. 211	0.488	0.779	0.36
Jun	5	0.130	0, 302	0.218	0.506	0.807	0.37
100	δ	0.144	0.333	0, 241	0.557	0.890	0.41
	7	0.305	0.707	0.511	1, 183	1, 890	0.88
July	8	0.341	0.788	0.570	1.320	2, 109	0.98
	9	0, 350	0.811	9. 587	1. 358	2. 169	1, 91
	10	0.297	0.688	0.498	1, 152	1.839	0.85
Aug	11	0.264	0.611	0.442	1.024	1.635	0.76
100	12	0.233	0.539	0.390	0.902	1. 441	0.67
	13	0. 182	0.420	0.304	0.704	1. 125.	0.52
Sept	14	0. 120	0.279	0. 202	0.467	0.745	0.34
	15	0.078	0.181	0.131	0.303	0.483	0. 22
	16	0.104	0.240	0.174	0.402	0. 642	0.30
0ct	. 17	0.101	0.234	0.169	0.392	0. 626	0. 29
1.5	18	0.098	0. 223	0.162	0.374	0. 597	0. 27
	19	0.169	0.392	0. 284	0.657	1.049	0, 49
Nov	20	0.310	0.717	0.519	1. 201	i. 918	0.89
	21	0.347	0.804	0.582	1. 347	2. 152	1.00
	22	0. 437	1.013	0.733	1,696	2, 709	1.26
Dec	23	0.441	1.020	0.738	1.708	2. 728	1. 27
	24	0.472	1.093	0.791	1.830	2. 923	1. 36
	25	0.459	1.063	0.769	1. 781	2.844	1. 32
Jan	26	0.456	1.055	0.764	1.768	2. 823	1. 31
	27	0.476	1.103	0. 798	1.847	2. 949	1. 37
	28	0.405	0.938	0.679	1, 571	2. 508	1. 17:
Feb	29	0.350	0.810	0. 586	1. 357	2.168	1.01
	30	0.312	0.723	0. 523	1. 210	1. 933	0.90
- ;	31	0. 263	0.608	0.440	1.019	1. 627	0.76
Жаг	32	0. 277	8.641	0.464	1.073	1. 714	0. 80
	33	0.305	0.707	0.511	1. 184	1.890	0.88
	34	0.294	0.679	0. 492	1.138	1. 817	0.84
Apr	35	0. 325	0.753	0.545	1.261	2.014	0.94
-	36	0.355	0.821	0.594	1. 376	2. 197	1.02
TOT	A L	9.888		16, 562			
Maximu			1.103		1. 847	2. 949	1. 37

Table		F.1-11	l Summary	ary of	ĭ	rrigation		Requirement	nt by	crops	in	Sector	H			i		Ē	Unit: MCA)
	ន									Kame	of C r	s d 0							
Month	D.	S .A	നാ	ပ	۵	ρυ	Œ	e e	ᄧ	•		¥		Œ	×	0	Д.	0	OTAL
V.	w4 #4				0, 105 0, 130		_					0.033 0.028		0.031		0.012	0. 011 0. 010	0.001	0.193
}	***				0.124							0,014		0.012		0.008	0.008		0.167
	-				0, 109							0.005		0.003		0.004	0.005		0.125
ij	us 1		•		0.119			•			6	0.001		0.001		3.004	0.005	::	0.130
.	اٍٰ	9. 002			5 S			100			3					500			0.144
	t	0.038			0. 208			0.019		-	0.020					0.010	000	0.001	0, 305
July					0.213			0.025			0.028					0.011	0.013	0.001	0.341
	5	- 1			0, 210			0, 025			0.028					0.011	0.010	0.001	0.350
	10				0.183			0.018	 		0.021					0.008	0.008		0. 297
Aug	≓	0.049			0. 161		-	0.018			0.021				· .	0.008	0.008		0.264
	7				0.134			0.018			0.022					9.008	0.008		0. 233
	11	1			0, 103			0.015			0.019					0.007	0.007		0.182
Sept					0.071		÷	0,009		. :	0.012	:				900.0	0.00		0.120
		ď			0.047	0.002		0.004			0.006					0.005	0.006		0.078
	15	Ì	0.000		0.042	0.011	0.004	0.004		0.008	0.005		0.004	1	0, 001	0,003	0,008	0.001	0.104
Oct	H	Ö	0.000		0.025	0.021	0.001	0.000	0.000	0.014	0.001		0.003		0.005	0.003	0.008	0.001	0.101
	82		0.001		9.00 <u>1</u>	0.027	0.003		0.001	9.017			0.011		0.001	0,008	5.003	0.000	0.036
	5		0.010	0.003		0.035	0.012		0.00	0.029			0.025		0.021	0.011	0.008	0.002	0, 163
Nov	20		0.025	0.010		0 055	0.020		0.022	0.051			0.047	.,1	0.041	0.017	0.012	0.003	0.310
ĺ	22		0 033	0.018		0.057	0.021		0.030	0.02			0.051		5.043	0.01	2 I n n	0,003	0.347
٠	23		0.045	0.032		0.065	0.023		0.044	0.055			0.063		a. 063	0.020	0.014	0.012	0 437
Ž	2 2	:	0.048	0.040	ż	0 064	0.023		0, 050	0.043			0.060		0.063	0.020	0.013	0.012	0.441
	3 4		900	0.043		0.00	0.029		0 064	200			070	0.00	000	2000	200	270.0	7 7 6
į	2 6		200	500		, r	0.00		# C C			-	0.0	900	20.00	170	910	7 6	737
	2 6		0.057	0.00		0 0	0.023		0.062	0.015		0.003	0.037	0.018	0.049	0.025	0.017	0.015	0.476
	183		0.044	0.064		0.082	0.015		0.048	0,004		0,003	0.024	0.026	0.036	0.024	0.017	0.014	0,405
Peb	23		0.032	0.058		0.071	0.008		0, 035			0.017	0.014	0.037	0.025	0.024	0.017	0.014	0.350
	S	:	0.023	0.049		0.054	0.063		0.024			0.031	0.005	0.051	0.015	0.026	0.018	0.015	0.312
	31		0.012	0.036		0.031			0.013			0.044		0.063	0.005	0.026	0.018	0.015	0.253
Mar	8		0.005	0.029		0.013						0.069		0.031	·	0.037	0.021	0.018	0.277
	55			0.016	이							0.088		0.104		0.033	0.023	0.019	0.305
	35			0.004	0.057						-	0.083	٠.	0.088		0.028	0.020	0.014	0. 294
Apr	35		-		0.099							0.081		0.086		0.027	0.013	0.014	0.325
	36				0.143							0.074		0.077		0.027	0.019	0.014	0.355
T 0 T	. T	0.372			63	444 0.839	٠,	137	0.525		0.182	0, 581	0.496	0.722	0.560	0.562	0.433	0.241	9. 888
A: Maize	Maize (1	9 ;	8: Maize (11		C: Marze	(111)	U: Kice (1)	៊	K. Vegeta(A)-A		r: locacco) (2)			:				
; ;	Vegeta(B)	(H)-7	N: Vegeta(R	2 (B) = 3		4		3	Q: Pasture			•							
, K	,	•		•		?													

.

Unit: MCM) 0, 001 0, 002 0, 002 0.002 Tobacco Vegeta(B)-1 0.020 0.020 0.013 0.006 0.006 0.017 0.018 0.014 0.013 0.013 0.012 0.010 ដដ 0.002 0.008 0.035 0.035 0.082 0.106 0.106 0.093 0.083 0.083 0.083 0.083 0.938 Rice (11) Vegeta(A)-4 Pasture 0.005 0.015 0.029 0.043 0.085 0.152 0.154 0.148 1.210 0.052 0.039 0.020 0.006 0.002 0.042 0.085 0.085 0.105 0.106 0.082 0.070 0.040 0.023 0.006 0.014 0.013 治罪な of Irrigation Requirement by crops in Sector 0.005 0.056 0.047 0.024 0.008 0.002 Crops Rice (I) Vegeta(A)-3 Coffee 0.033 0.035 0.035 0.035 0.037 0.037 0.008 0.008 0, 304 ö 0.013 0.023 0.029 0.085 0.088 0.093 0.093 0.056 0.007 0.262 0.879 0.657 2 11 6 0.000 0.002 0.015 0.037 0.037 0.051 0.107 0.108 0.088 0.088 0.088 0.088 0.088 0.088 Maize (III) Vegeta(A)-2 Fruits 0.001 0.032 0.041 0.023 0.023 0.025 0.015 0.015 0.005 0.005 0.399 0.007 0.011 0.020 0.020 0.035 0.039 0.038 0.040 0.039 0.038 0.038 0.038 1.490 0, 109 0, 120 0, 120 0, 126 0, 143 0, 137 0, 052 0, 021 0.004 0.034 0.034 0.059 0.059 Maize (11) Vegeta(A)-1 Vegeta(B)-3 0.037 0.095 0.165 4.093 0.175 0.218 0.208 0.200 0.200 0.348 0.348 0.226 0.227 0.173 0.0179 0.013 0,006 0,017 0,023 0,053 0,053 0,117 0,1108 0,097 0,061 0,061 0,061 0,061 0.993 F.1-12 Summary 品品岩 0.840 0.000 0.000 0.000 0.001 0.001 0.001 0.001 0.002 0.008 æ : Maize (1) : Soy Bean : Vegeta(B)-2 0.624 0.005 0.005 0.005 0.005 0.007 0.007 0.007 0.007 0.007 0.007 0.007 10 Month days -1 -4 1--4 G # Je 2 Apr 0

Table F.1-13	Irrigation	Requirement	for Maze	(I) in Sector I
			and the second second	

* :							(Unit: MCM)
	10		ETcrop	Pe		Irrigation	Water
Month	days	(mm/day)	(mm/10day) (i	nm/10day)	(mm/10day)	Area (ha)	Requirement
974	1	2. 35	23. 5	26.7		13	
May	2	2.30	23.0	26. 7		40	
- 14 A	3	2. 24	22. 4	26.7		67	
	4	2. 58	25. 8	31. 7		94	
Jun	5	2.97	29.7	31. 7		120	
	6	3. 23	32. 3	31.7	0, 6	147	0.002
	7	3. 48	34.8	23, 3	11. 4	161	0.039
July	- 8	3.96	39.6	23, 3	16. 3	161	0.056
	9	4. 23	42.3	23. 3	19.0	161	0.065
	-10	4. 37	43.7	26, 7	17. 0	161	0.058
Aug	11	4.09	40.9	26.7	14. 3	161	0.049
	12	4.00	40.0	26. 7	13.4	147	0.042
	13	3.65	36.5	25.0	11.5	120	0.030
Sept	14	3. 32	33. 2	25.0	8. 1	94	0.016
	15	2, 96	29.6	25.0	4.6	67	0.007
	16	2. 73	27. 3	20. 0	7. 3	40	0.006
0ct	17	2. 46	24. 6	20.0	4. 6	13	0.001
	18		· · · · · · · · · · · · · · · · · · ·	20.0			
	19			5. 0			* *
Nov	20		• •	5.0			
	21			5.0			
	22	1		and the first		•	1
Dec	23						
····	24						
	25					•	
Jan	26						
	27					<u>.</u>	
	28			1.7			
Feb	29			1.7	100		
	30			1.7			
	31						
Mar	32						•
	33						T
	34			6.7			
Арг	35			6. 7			
	36			6. 7			

Table F.1-14 Irrigation Requirement for Maze (II) in Sector I

	10	RTCFOD	ETerop	Pe	Net ETcrop	Irrigation	(Unit: MCM) Water
						Area (ha)	
	1		<u></u>	26.7			
May				26. 7			
	3			26.7			
	4			31.7			
Jun	5			31.7			
	6			31.7			
	7			23. 3			
July	8			23. 3	1.		
	9			23. 3			
	10			26.7			
Aug	11			26. 7			٠
	12			26.7			
	13			25. 0			
Sept	-14			25.0	•		•
	15			25.0	<u> </u>		
	16	2.03	20.3	20.0	0.3	7	0.000
0ct	17	2.03	20. 3	20.0	0.3	19	0.000
	18	2.07	20. 7	20.0	0.7	33	0.001
	19	1.56	15.6	5.0	10.6	46	0.010
Nov		2. 48	24. 8	5. 0	19.8	59	0.025
	21	2.65	26, 5	5.0	21. 5	72	0.033
_	22	2. 71	27. 1		27. 1	79	0.045
Dec	23	2. 88	28. 8		28.8	79	0.048
	24	3. 23	32. 3		32.3	79	0.054
	. 25	3. 30	33.0		33.0	79	0.055
Jan	26	3. 35	33. 5		33. 5	79	0.056
	27	3, 73	37.3	4 8	37.3	72	0.057
.	- 28	3. 61	36. 1	1.7	34. 4	59	0.044
Feb	29	3. 44	34. 4	1. 7	32.8	46	0. 032
	30	3. 39	33.9	1. 7	32. 2	33	0. 023
	31	2. 90	29.0		29.0	19	0.012
Mar	32	3. 21	32. 1		32. 1	7	0.005
	33			· A 7		 	
	34			6. 7			
Арг	35			6. 7			
	36			6. 7		· · · · · · · · · · · · · · · · · · ·	

Table F.1-15 Irrigation Requirement for Maze (III) in Sector I

						<u> </u>	(Unit: MCM)
			ETcrop				Water
Month	days	(mm/day)	(mm/10day) (mm		(mm/10day)	Area (ha)	Requirement
	1			26. 7		•	
May	2			26. 7	÷ .		
	3			26. 7	<u> </u>		
	4			31. 7			
Jun	5			31. 7			
	6			31.7		·	· · · · · · · · · · · · · · · · · · ·
	7			23. 3			
July	8			23. 3			• •
	9_			23. 3			<u> </u>
	10			26.7			
Aug	. 11			26. 7			
	12			26. 7	- , :		
C4	13			25.0			*.
Sept	14			25.0		•	
	15 16			25. 0 20. 0			<u> </u>
0ct	17			20.0			
OCT	18	1. 92	19. 2	20.0		7	
	13	1. 25	12. 5	5.0	7. 5	<u></u>	0.003
Nov	20	1. 90	19. 0	5. 0	14.0	34	0.010
1101	21	2. 21	22. 1	5.0	17.1	48	0.018
	22	2. 41	24. 1	<u>~</u>	24. 1		0.032
Dec	23	2. 50	25. 0	÷	25.0	76	0.040
000	24	2. 79	27. 9		27. 9	82	0.049
	25	3.06	30.6		30.6	82	0.054
Jan	26	3. 42	34. 2		34. 2	82	0.060
	27	3, 98	39. 8		39.8	82	0,070
	28	3.81	38. 1	1. 7	36. 5		0.064
Feb	29	3.73	37.3	1. 7	35.6		
	30	3. 87	38. 7	1.7	37. 1	62	0.049
	31	3. 53	35. 3		35. 3	48	0.036
Mar	32	3. 93	39. 3		39. 3	34	0.029
	33	3, 73	37. 3		37. 3	21	0.016
	34	3. 34	33. 4	6. 7	26. 7	7	0.004
Apr	35			6. 7			· ·
-	36			6. 7			

Table F.1-16 Irrigation Requirement for Rice (I) in Sector I (Unit: MCM) ETcrop-Рe Net ETcrop Irrigation Water ETcrop Month days (mm/day) (mm/10day) (mm/10day) (mm/10day) Area (ha) Requirement 185 0.105 5.30 26.7 26. 4 53.0 1 0.130 2 26.7 26.8 226 5, 35 53. 5 May 4.84 26.7 21.7 267 0.124 48.4 0.109 31.7 308 48. 2 16.5 4 4.82 329 0.119 31.7 16.9 Jun 5 4,86 48.6 329 0.131 31.7 18.6 5.03 50.3 0.208 329 7 5. 28 52.8 23. 3 29.5 5, 35 329 0.213 8 53.6 23.3 30.2 July 0.210 23. 3 29.8 329 9 5. <u>31</u> 53. <u>1</u> 26.7 26.0 329 0.183 10 5. 27 52. 7 308 0.161 11 5.10 51.0 26.7 24. 4 Aug 267 0.134 12 5, 02 50.2 26.7 23.5 46.3 25. 0 21.3 226 0.103 13 4.63 17.9 185 0.071 14 4, 29 42.9 25.0 Sept 0.047 25.0 15.3 144 15 4.03 40.3 19.0 20.0 103 0.042 16 3, 90 39.0 20.0 19.0 62 0.025 0ct 17 3.90 39.0 21 3.70 20.0 17.0 0.007 37.0 18 19 5.0 5.0 20 Nov 5.0 21 22 23 Dec 24 25 Jan 26 27 1.7 28 1.7 Feb 29 1.7 30 31 32 Маг <u>50.8</u> 21 0.022 33 5.08 50.8 6.7 43. 2 62 0.057 4.98 49.8 34

6.7

6.7

44.8

46.4

0.099

0.143

103

144

35

36

Apr

5.15

5.30

51.5

53.0

Table F.1-17 Irrigation Requirement for Rice (II) in Sector I

	10	ETcrop	ETerop	Pe	Net ETcrop	Irrigation	Water
Month	days	(mm/day)	(mm/10day)		(mm/10day)	Area (ha)	Requirement
10	1			26. 7		**	
May	2	11.5		26.7	er jage		*
*****	3			26.7			
	4			31.7			
Jun	5		i	31. 7	•		
	6			31.7	<u> </u>		
1.5	7			23. 3	.,		
July	8	145		23. 3	the first		•
1 /	9_	:		23. 3		· .	
	10			26. 7			
Aug	11		•	26. 7			
	12	1 4		26. 7			
	13			25.0			
Sept	-14			25.0	ALC: UNITED STATE	200	4
	15	3. 57	35.7	25.0	10.7	10	0.002
	16	3.67	36.7	20.0	16. 7	31	0.011
Oct:	17	3.86	38.6	20.0	18.6	52	0.021
	18	3. 77	37.7	20.0	17.7	72	0. 027
	19	2. 50	25.0	5. 0	20.0	82	0.035
Nov	20	3.64	36.4	5. 0	31. 4	82	0.055
	21	3.74	37.4	5, 0	32. 4	82	0.057
	22	3. 70	37.0		37.0	82	0.065
Dec	23	3.62	36. 2		36. 2	82	0.064
	24	3. 98	39.8		39.8	82	0.070
	25	4.08	40.8		40.8	82	0.072
Jan	26	4. 28	42.8		42.8	82	0.075
	27	4.84	48.4		48, 4	82	0.085
	28	4.80	48.0	1. 7	46. 3	82	0.082
Feb	29	4. 76	47.6	1.7	45. 9	72	0. 071
	30	5.02	50. 2	1.7	48. 5	52	0.054
	31	4.75	47. 5		47. 5	31	0. 031
Mar	32	5.61	56. 1		56. 1	10	0.013
	33	5. 72	57. 2		57. 2		
	34	5. 30	53.0	6.7	46.3		
Apr	35	5. 20	52. 0	6. 7	45. 3		
•	36	5. 20	52.0	6. 7	45. 3		

Table F.1-18 Irrigation Requirement for Tobacco in Sector I

	10	ЕТсгор	BTcrop	Pe	Net ETcrop	Irrigation	Water
Month					(mm/10day)		
	<u> </u>			26. 7	:		
May	2			26.7			
-	3			26. 7			
	4			31. 7			
Jun	- 5	V		31. 7			
	6	1. 1. 1.	· · · · · · · · · · · · · · · · · · ·	31.7			
74 [4	7			23. 3			
July	8		•	23, 3			
	9_		-	23. 3			<u> </u>
	10	* -	- 1	26.7			
Aug	11			26. 7			
	12			26. 7			· · · · · · · · · · · · · · · · · · ·
1.11	13	2.09	20.9	25.0		4	
Sept	14	2. 18	21.8	25.0		11	
	15	2.36	23. 6	25. 0	·	19	
100	16	2. 73	27.3	20.0	7. 3	26	0.004
0ct	17	3.04	30. 4	20.0	10. 4	30	0.007
	18_	3, 33	33. 3	20.0	13.3	30	0,009
	19	2.40	24. 0	5.0	19.0	30	0.012
Nov	20	3.64	36.4	5.0	31.4	30	0, 020
<u></u>	21	3.74	37.4	5.0	32. 4	30_	0. 021
	22	3. 63	36. 3		36. 3	30	0. 023
Dec	23	3. 52	35. 2		35. 2	30	0. 023
	24	3.74	37. 4	······	37.4	30	0.024
	25	3, 64	36. 4		36. 4	30	0.023
Jan	26	3. 67	36. 7		36. 7	30	0. 024
	27	4. 10	41.0	·	41.0	26	0. 023
	28	3. 98	39. 8	1. 7	38.1	19	0. 01
Feb	29	3, 69	36 . 9	1.7	35. 2	11	0.008
	30	3.74	37.4	1.7	35. 7	4	0. 003
	31						
Mar	32						
	33						
	34			6.7			
Apr	35			6. 7			
	36			6. 7			

Table F.1-19 Irrigation Requirement for Soy Beans in Sector I

<u> 711.</u>								: MCM)
	10	ETerop	ETcrop	Pe	Net ETcrop	Irrigation	W	ater
Month:	days	(mm/day)	(mm/10day) (mm		(mm/10day)	Area (ha)	Requ	irement
	. 1							
May	2	2, 50		26.7	٠.	7		47
	3	2. 20	22.0	26.7		21		
	4	2.49	24. 9	31. 7		. 35	•	
Jun	- 5		23. 7	31.7		49		
	6	3, 23	32. 3	31.7		63		0.001
	7	3.48	34.8	23. 3	11.4	77		0.019
July	8	3, 60	36.0	23.3	12. 7	91	-	0. 025
	9	3.47	34. 7	23. 3	11.3	105		0.025
	10	3. 47	34. 7	26. 7	8.0	105		0.018
Aug	11	3. 56	35. 6	26. 7	9.0	91	2 1	0.018
	12	3. 78	37.8	26.7	11. 2	77		0.018
	13	3.65	36. 5	25.0	11.5	63		0.016
Sept	14	3. 35	33. 5	25.0	8. 5	49	-	0.009
·	15	3.08	30.8	25.0	5. 8	35		0.004
	16	2. 81	28. 1	20.0	8.1	21		0.004
0ct	17	2. 26	22.6	20.0	2.6	7		0.000
	18			20.0				
4 1	19			5.0	6.5			
Nov	20			5. 0	S	14	100	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
	21		.8.	5.0				
	22		:				7.	
Dec	23							
	24							
	25							
Jan	26					v -		
	27							
	28			1.7				
Feb	29			1.7				4 .C.
	30			1. 7	100			
	31							
Mar	32							
	33							
	34			6. 7				
Apr	35			6. 7				٠.
uhr	36			6. 7				
	00		·····	<u> </u>				

Table F.1-20 Irrigation Requirement for Vegetable (A)-1 in Sector I

	- 10	ETcrop	FTaran	Pe	Not Elaron	Irrigation	(Unit: MCM) Water
						Area (ha)	
MOILEIL	1	(min) Cost	Valley A Octoby /	26. 7	(may xoday)	ποα τιας	RoquiTomon
May	2			26. 7			8. P.
111.04	3	•		26. 7	. •		
	4		****	31. 7	<u></u>		
Jun	5			31. 7			
0 0.11	6			31. 7	٠.		
<i></i>	7			23. 3			
July	. 8			23. 3			and the
0413	9			23. 3			
	10			26.7			
Aug	11			26. 7			
1146	12			26. 7			
·	13		· · · · · · · · · · · · · · · · · · ·	25. 0		· ····································	
Sept	14			25. 0	١.		a * .
oopt	15			25. 0		. · ·	
	16			20.0			
Oct	17	2.03	20. 3	20.0	0.3	7	0.000
	18	2. 22	22. 2		2. 2	20	0.00
	19	1.73	17. 3		12. 3	34	0.00
Nov	20	2. 65	26. 5	5. 0	21. 5	47	0. 02
	21	2. 82	28. 2		23. 2	61	0.03
	22	2.77	27. 7		27.7	74	0.04
Dec	23	2. 62	26. 2		26. 2	88	0. 050
300	24	2.79	27. 9		27. 9	102	0.06
 	25	2. 92	29. 2		29. 2	102	0.06
Jan	26	3. 31	33. 1		33. 1	88	0.06
	27	3.89	38. 9		38. 9	74	0.06
Service Service	28	3, 81	38.1	1.7	36, 5	61	0.04
Feb	29	3. 61	36. 1	1.7	34. 4	47	0.03
	30	3. 52	35. 2	1.7	33. 5	34	0.02
	31	2. 94	29. 4		29. 4	20	0. 01
Mar	32	5 1	***			7	
III.	33			•		,	
	34			6. 7			
Apr	35			6. 7			
uhi	36			6.7			

Table F.1-21 Irrigation Requirement for Vegetable (A)-2 in Sector I

- 1					<u> </u>		(Unit	: MCM)
1 1		ETcrop				Irrigation		ater
Month	days	(mm/day) (m	m/10day) (r		(mm/10day)	Area (ha)	Requ	irement
	1			26. 7				
May	2			26.7				* * *
	3			26.7	·			
	4			31.7				
Jun	5			31.7			٠.	
	<u>6</u>			31.7	·			
71				23.3				
July	8			23. 3				
	9	·		23. 3	 			
A	10	the second		26.7				
Aug	11 12			26. 7 26. 7	· v			****
	13	2 00	20. 9		 	7		
Cont		2. 09 1. 99	20. s 19. 9	25. 0 25. 0		21		
Sept	14 15	2. 24	22.4	25. 0 25. 0		35		
	16	2. 73	27. 3	20.0	7. 3	49		0.008
0ct	17	3. 00	30. 0	20.0	10.0	63		0.014
UCU	18	3. 03	30. 3	20.0	10. 3	77		0.017
	19	1. 99	19. 9	5.0	14. 9	91		0.029
Nov	20	2. 75	27. 5	5. 0	22. 5	105		0.051
	21	2. 75	27. 5	5. 0	22. 5	105		0.051
	22	2. 84	28. 4		28. 4	91		0.055
Dec	23	2. 94	29. 4		29. 4	77		0.049
	24	3. 23	32. 3		32. 3	63		0.044
 	25	3. 16	31.6		31. 6	: 49		0.033
Jan	26	3. 17	31.7		31.7	35		0.024
	27	3. 28	32.8		32.8	21		0.015
	28	2.87	28. 7	1.7	27. 0	7		0.004
Feb	29			1. 7				
	30			1. 7		<u> </u>		
	31					,		
Mar	32							
	33					.,		
	34			6. 7				
Apr	35			6. 7				
	36			6. 7				

Table F.1-22 Irrigation Requirement for Vegetable (A)-3 in Sector I

	10	ETerop	RTeron	Pe	Net ETcron	Irrigation	(Unit: MCM) Water
						Area (ha)	
montan	1	(may Gay)	(may x u duy)	26. 7	Chany To Gray y	11.00 (11.0)	110 44 2 3 0 110 11
May	2	2. 30	23.0	26. 7		7	* * * * * * * * * * * * * * * * * * * *
111020	3	2. 02	20. 2	26.7		21	2
·	4	2. 37	23. 7	31. 7		35	
Jun	5	2. 92	29. 2	31. 7		49	147
	- 6	3. 23	32. 3	31.7	0.6	63	0.001
	7	3, 52	35. 2	23. 3	11. 9	77	0. 020
July	8	3.65	36. 5	23. 3	13. 1	91	0.026
	9	3, 60	36.0	23. 3	12, 7	105	0. 028
	10	3, 60	36.0	26. 7	9. 3	105	0. 021
Aug	11	3.74	37.4	26. 7	10.7	91	0. 021
	12	4.00	40.0	26. 7	13.4	77	0. 022
	13	3.89	38. 9	25. 0	13. 9	63	0.019
Sept	14	3, 63	36. 3	25.0	11. 3	49	0.012
-	15	3. 34	33. 4	25.0	8.4	35	0.006
	16	3.12	31. 2	20.0	11.2	21	0.005
0ct	17	2, 73	27. 3	20.0	7. 3	7	0.001
	18			20.0			
	19			5. 0			
Nov	20			5.0			
	21			5.0			
	22						
Dec	23						
	24						
	25						
Jan	26						
	27						
4	28			1.7			
Feb	29			1. 7			
	30			1.7			
	31				_		
Mar	32					:	
	33						
	34		: .	6. 7			
Apr	35			6.7			
	36			6. 7		<u> </u>	

Table F.1-23 Irrigation Requirement for Vegetable (A)-4 in Sector I

8.1	1.4940						(Unit	MCM)
11.	10	ETcrop	ETcrop	Pe Net	ETcrop I	rrigation	¥	ater
Month				m/10day) (mm			Requ	irement
	1	4. 69	46. 9	26. 7	20.3	77		0.033
May	2	4.75	47.5	26. 7	20. 8	63		0.028
	3	4.05	40.5	26. 7	13.8	49	,	0.014
	4	3.78	37.8	31. 7	6. 2	35		0.005
Jun	5	3.44	34. 4	31. 7	2. 7	21		0.001
	6	3, 01	30.1	31.7		7		
	7			23. 3				
July				23. 3				
	. 9			23. 3	1 .5"			
	10			26.7				
Aug	11			26. 7				
	12			26.7				
	13			25.0		1 1 1	/	
Sept	-14			25.0				v *.
	15			25. 0	4 4			
of all to	16			20.0			:	
0ct	17			20.0				
	18		•	20.0				•
	19			5. 0				
Nov	20	•		5. 0	•			1.
	21			5.0			13	
	22							
Dec	23			•			27.1	
	24							
	25							
Jan	26							tist.
	27	2. 13	21. 3		21. 3	7		0.003
	28	2. 13	21. 3	1. 7	19.7	21		0.009
Feb	29	2.46	24. 6	1.7	22. 9	35		0.017
	30	3. <u>12</u>	31, 2	1.7	29.6	49		0.031
	31	3. 28	32. 8		32.8	63	-	0.044
Mar	32	4.18	41.8		41.8	77		0.069
	33	4. 48	44.8		44.8	91		0.088
	34	4. 35	43, 5	6. 7	36.8	105		0.083
Apr	35	4. 26	42.6	6.7	36.0	105		0.081
-	36	4.47	44. 7	6. 7	38. 1	91		0.074

Table F.1-24 Irrigation Requirement for Vegetable (B)-1 in Sector I

							(Unit	: MCM)
	10	Efcrop	ETerop	Pe	Net ETcrop	Irrigation		ater
Month	days	(mm/day)	(mm/10day) (r	mm/10day)	(mm/10day)	Area (ha)	Requ	irement
: .	. 1			26.7				
May	2	X ,		26. 7				
4.15	- 3			26. 7			3'	
	4			31.7				
Jun	5			31.7				:
	6			31.7	41			
	7	· · · · · · · · · · · · · · · · · · ·		23, 3				
July	8			23. 3				
	9			23. 3				
	10		··	26.7				
Aug	11			26.7			-	
	12			26.7				
	13	2. 09	20, 9	25.0		7		
Sept	14	1. 99	19. 9	25.0		20		
	15	2. 05	20. 5	25.0		34		
	16	2. 38	23. 8	20.0		47	-	0.004
0ct	17	2. 65	26. 5	20.0		61		0.009
000	18	2. 70	27.0	20.0	7. 0	74		0.011
	19	1. 82	18. 2	5. 0		88		0. 025
Nov	20	2. 65	26. 5	5.0	21. 5	102		0.047
1101	21	2. 69	26. 9	5.0	21. 9	108		0.051
	22	2. 71	27. 1		27.1	108		0.063
Dec	23	2. 75	27. 5		27. 5	102		0.060
DOC	24	3. 03	30. 3		30. 3	88		0.057
	25	3.06	30. 6.		30.6	74		0.049
Jan	26	3. 20	32. 0		32.0	61		0.042
Van	27	3. 61	36.1		36. 1	47		0.037
	28	3. 48	34. 8	1.7	33. 2	34		0.024
Feb	29	3. 32	33. 2	1. 7	31.5	20		0.014
τÓυ	30	3. 21	32. 1	1.7	30. 5	7		0.005
	31	V. 61	Va. z	** !	77.0	<u>'</u>		
Маг	32		•					
maı	33	at a second						
·	34			6. 7				
Ann	35		*	6.7				
Apr				6. 7				
	36			0. /				····

Table F.1-25 Irrigation Requirement for Vegetable (B)-2 in Sector I (Unit: MCM)

	14.43						(Unit:	MCM)
1,11	10 I	3Terop	ETcrop	Pe Net	ETcrop	Irrigation	Wa	ter
				1/10day) (mm/			Requi	rement
	1	4. 54	45. 4	26. 7	18.7	77		0.031
May	2	4.40	44.0	26. 7	17. 3	63	:	0.023
	3	3.83	38. 3	26. 7	11.6	49		0.012
	4	3.61	36. 1	31. 7	4.5	35		0.003
Jun	. 5	3.40	34.0	31. 7	2. 3	21		0.001
÷	6	3. 10	31.0	31.7		7		
	7			23. 3				
July	8			23. 3			*	
	9			23. 3				
	10			26. 7				
Aug	11			26. 7				
	12			26. 7				
	13			25.0		and the	* * *	
Sept	14			25. 0				100
	15			25. 0				·
e des les	16			20. 0	No. 1	* * *	- 1	
0ct	17		.*	20. 0				.*
	18	:		20. 0	·		·	·
14 L	19			5. 0		į.		
Nov	20	1.19	: .	5. 0				
	21			5.0	1 1 1	• : :		
1.0	22	14.	100		7.7			
Dec	23	11 -	1.0	•	1.7			
	24					· · · · · · · · · · · · · · · · · · ·		
	25	1.84	18.4		18.4	. 1		0.003
Jan	26	1. 94	19. 4		19.4	21		0.009
	27	2. 34	23.4		23.4	35	*******	0.018
	28	2, 62	26. 2	1. 7	24.6	49		0.026
Feb	29	2.87	28. 7	1.7	27.0	63		0.037
	30	3. 26	32.6	1.7	30. 9	77		0.051
	31	3. 23	32. 3		32. 3	91		0.063
Маг	32	4.03	40. 3		40.3	105	* .	0.091
	33	4. 32	43, 2		43.2	112		0.104
	34	4. 35	43.5	6. 7	36.8	112		0.088
Apr	35	4.47	44.7	6. 7	38. 1	105		0.086
•	36	4.63	46.3	6. 7	39.6	91		0.077

Table F.1-26 Irrigation Requirement for Vegetable (B)-3 in Sector I

						Irrigation	
MONTH		(mm/day)	(mm/luday)			Area (ha)	Kequirement
11	1		•	26.7			
May	2			26.7	*	•	
· .	3			26.7	· ·		
	4			31.7			
Jun	. 5			31.7			
	6			31.7			
	7		÷	23. 3			
July	. 8			23. 3			
	9			23. 3	<u> </u>		
: . . •	10			26.7			•
Aug	11			26.7			
4.5	12			26.7			
	13		00.0	25.0			
Sept	14	2.03	20. 3	25.0		7	
· · · · ·	15	1. 98	19.8	25.0		21	0.004
	16	2. 18	21.8	20.0		35	0.001
0ct	17	2. 46		20.0	4.6	49	0.005
· · · · · -	18	2. 55	25. 5		5.5	63	0.007
	19	1.78	17.8			77	0. 021
Nov	20	2. 62	26. 2		21. 2	91	0.041
<u> 1 </u>	21	2. 69	26. 9	5.0	21. 9	105	0.049
	22	2.64	26.4		26.4	112	0.063
Dec	23	2.62	26. 2		26. 2	112	0.063
<u></u>	24	2. 92	29. 2		29. 2	105	0.066
in Territoria Po r enta	25	3.03	30. 3		30. 3		0.059
Jan	26	3. 24	32. 4		32. 4	77 63	0.053
<u> </u>	27	3.65	36.5	4 17	36.5		0.049
n.L	28	3.61	36. 1	1.7		49	0. 036
Feb	29	3. 48	34.8	1.7	33. 2	35	0. 025
1	30	3. 52	35. 2	1.7	33.5	21	0.015
	31	3.07	30.7		30. 7	7	0.005
Mar	32						
	33						
	34	į.		6. 7			
Apr	35			6. 7			
	36			6.7			

Table	F.1-27	Irrigation	Requirement	for	Fruits	in.	Sector I	
		-				٠.	Minte MON	

1,7 31	1						(Unit:	
						Irrigation		
Month	days					Area (ha)	Requi	rement
	1	4.34	43, 4	26.7		34		0.012
May	2	4. 25	42.5	26. 7	15.8	34		0.011
	3	3.74	37.4	26.7	10.7	34		0.008
	4	3.66	36.6	31. 7	4. 9	34		0.004
Jun	5	3.66	36.6	31.7	4. 9	34	• :	0.004
	6	3.66	36.6	31. 7	4.9	34	<u> </u>	0.004
	7	3.74	37. 4	23. 3	14. 1	34	-	0.010
July	8	3.82	38. 3	23. 3	. 14. 9	34	-	0.011
-	9	3.82	38. 3	23. 3	14. 9	34		0.011
	10	3.82	38.3	26. 7	11.6	34		0.008
Aug	11	3.74	37.4	26.7	10. 7	34	*:	0.008
	12	3.74	37. 4	26. 7	10.7	34		0.008
· · · · · · · · · · · · · · · · · · ·	13	3.48	34. 8	25. 0	9.8	34		0.007
Sept	14	3. 32	33. 2	25.0	8. 1	34	1	0.006
· · ·	15	3.23	32. 3	25.0	7.3			0.005
111	16	3. 32	33. 2	20.0	13.1	34		0.009
· Oct	17	3.32	33. 2	20.0	13.1	34		0.009
	18	3.15	31. 5	20.0		34	: :	0.008
(1.5)	19	2.04	20. 4	5. 0		34		0.011
Nov	20	2.89	28.9	5.0	23. 9		1,41	0.017
New Year	21	2.89	28. 9	5.0	23. 9	34		0.017
17, 31	22	2.80	28. 0		28. 0	34		0.020
Dec	23	2.72	27. 2		27. 2	34		0.020
4.1.1	24	2.89	28. 9		28. 9	34		0.021
7° '	25	2.89	28. 9	··	28. 9	34		0. 021
Jan	26	3.06	30. 6		30.6		3.5	0.022
	27	3.48	34.8		34.8	34		0.025
	28	3. 48	34. 8	1. 7	33. 2	34		0.024
Feb	29	3. 48	34. 8	1.7	33. 2	34		0.024
	30	3.74	37. 4	1.7	35. 7	34		0.026
	31	3. 57	35. 7		35. 7	34		0.026
Mar	32	4. 34	43. 4		43.4	34		0.031
	33	4. 59	45. 9		45, 9	34		0.033
	34	4. 51	45. 1	6. 7	38. 4	34		0.028
Apr	35	4. 42	44. 2	6. 7	37. 5	34	1	0. 027
	36	4. 42	44. 2	6. 7	37. 5	34		0.027

Table F.1-28 Irrigation Requirement for Coffee in Sector I

	* • 1	20 111	1 Eacton	Kedarren	iene ror	corree in	
<u> </u>	10	Drawa	DY	n.	Mak Drama	p Irrigation	(Unit: MCM)
N .1	10	BICTOP	PicLob	P0	Net Bicro	p irrigation	Water
Month	days	(mm/day)	mm/roday)	(mm/luday)	(mm/luday) Area (ha)	Requirement
	1	5. 35	53.6	6411	26.		
May	2	5. 25	52. 5	26. 7	25.		
	3_	4.62	46.2	26. 7			
	4	4, 52	45. 2	31. 7	13.		
Jun	5	4. 52	45. 2	31.7	13.		
	6.	4, 52	45. 2	31.7	13.		
	7	4.62	46. 2	23. 3	22.		
July	8	4. 73	47.3	23. 3	23.		
	9	4. 73	47.3	23. 3	23.		
	10	4.73	47. 3	26. 7	20.		
Aug	11	4. 62	46. 2	26. 7	19.		and the second s
	12	4. 62	46. 2	26. 7	19.	· · · · · · · · · · · · · · · · · · ·	~
	13	4. 31	43. 1	25.0	18.		
Sept	14	4.10	40.9	25.0	15.		
	15	3.99	39. 9	25.0			
Est.	16	4. 10	40.9	20.0	20.	2. 4	
0ct	17	4. 10	40.9	20.0	20.		
· ·	18	3.89	38, 9	20. 0		9 19	
1.0	19	2.52	25. 2		20.		
Nov	20	3.57	35. 7	5. 0	30.		
<u></u>	21	3.57	35.7		30.		
	22	3.47	34. 7	.*	34.		
Dec	23	3. 36	33. 6		33.		
	24	3, 57	35.7		35.	7 19	0.014
	25	3.57	35. 7		35.	7 19	0.014
Jan	26	3: 78	37.8		37.	8 19	0.015
11.	27	4.31	43.1		43.	1 19	0.017
٠	28	4.31	43.1	1. 7	41.	4 19	0.017
Feb	29	4. 31	43.1	1.7	41.		0.017
	30	4. 62	46. 2	1.7			
	31	4. 41	44.1		44.	1 19	0.018
Mar	32	5. 35	53.6		53.		
7.4	33	5. 67	56.7		56.		
1, 1	34	5. 57	55. 7	6. 7	49.		
Apr	35	5. 46	54. 6	6. 7	47.		
	36	5. 46	54.6	6. 7	47.		

Table F.1-29 Irrigation Requirement for Pasture in Sector I

							(Unit:	
					Net ETcrop			iter
Month					(mm/10day)		Requi	
	1	2.81			1.4			0.001
May	2	2, 75	27. 5	26.7	0.8	34		0.001
	3	2. 42	24. 2	26.7		34		
	4	2. 37	23. 7	31.7		34		
Jun	5	2. 37	23.7	31.7		34		
<u> </u>	6_	2. 37	23. 7	31.7		34		
	7	2.42	24. 2	23. 3	0. 9	34		0.001
July	8	2. 48	24.8	23.3	1.4	34		0.001
<u> 4 û</u> .	9	2. 48	24.8	23. 3	1.4	: 34	- 1	0.001
	10	2, 48	24.8	26.7		34		
Aug	11	2, 42	24, 2	26.7	18 B	34		
71.	12	2. 42	24. 2	26.7	<u> </u>	34	- 7	
	13	2. 26	22. 6	25.0		34	1.1	
Sept	14	2. 15	21. 5	25.0		34	•	
	15	2.09	20. 9	25.0		34		
	16	2. 15	21. 5	20.0	1.4	34		0.001
Oct	17	2. 15	21.5	20.0	1.4	34		0.001
	18	2.04	20. 4	20.0	0.4	34		0.000
	19	1. 20	12. 0	5.0	7.0	34		0.005
Nov	20	1.70	17. 0	5.0	12.0	34		0.009
	21	1.70	17.0	5.0	12.0	34		0.009
	22	1.65	16. 5		16.5	34		0.012
Dec	23	1.60	16.0		16.0	34		0.012
	24	1.70	17.0		17. 0	34		0.012
	25	1. 70	17.0		17. 0			0.012
Jan	26	1.80	18. 0		18.0	34		0.013
	27	2.05	20. 5		20. 5	34		0.015
	28	2.05	20. 5	1.7	18.8	34		0.014
Feb	29	2.05	20.5	1.7	18.8	- 34		0.014
	30	2. 20	22. 0	1.7	20. 3	34		0.015
	31	2. 10	21.0		21.0	34		0.015
Mar	32	2. 55	25. 5		25. 5		*	0.018
	33	2.70	27. 0		27.0	34		0.019
	34	2. 65	26. 5	6.7	19.8			0.014
Apr	35	2. 60	26. 0	6. 7		34		0.014
****	36					V-1		~, ~ ~ ~

Table F.1-30 Irrigation Requirement for Maze (I) in Sector II

	10	ETcrop	ETcrop	Pe	Net ETcrop	Irrigation	Water
						Area (ha)	Requiremen
	1	2. 35	23. 5	26. 7		23	
May	2	2.30	23.0	26. 7	. *	68	
•	3	2. 24	22. 4	26. 7		112	
	4	2. 58	25. 8	31.7		157	
Jun	5	2. 97	29. 7	31.7		202	
	6	3. 23	32. 3	31. 7	0.6	247	0.003
	7	3. 48	34. 8	23. 3	11.4	269	0.060
July	. 8	3. 96	39. 6	23. 3	16. 3	269	0.094
	9	4. 23	42. 3	23. 3	19.0	269	0.109
	10	4. 37	43.7	26. 7	17.0	269	0.098
Aug	11	4.09	40.9	26. 7	14. 3	269	0.082
	12	4.00	40.0	26.7	13. 4	247	0.071
	13	3.65	36. 5	25.0	11.5	202	0.050
Sept	14	3. 32	33. 2	25.0	8. 1	157	0. 021
•	15	2. 96	29. 6	25. 0	4.6	112	0, 011
	16	2. 73	27. 3	20.0	7. 3	68	0.011
0ct	17	2.46	24. 6	20.0	4. 6	23	0.002
	18			20.0	·		
	19			5. 0	•		•
Nov	20	<i>(1)</i>		5. 0		V.	
	21	12 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		5.0		<u> </u>	
	22						
Dec	23						
. Nan	24	· · · · · · · · · · · · · · · · · · ·		<u> </u>			
	25						
Jan	26	1.					
	27	:					
	28			1. 7		•	
Feb	29			1. 7			
60,00	30			1.7	<u> </u>		
	31						
Mar	32	* *					
	33	· .					
	34			6. 7			
Apr	35			6. 7			
	36			6. 7			

Table F.1-31 Irrigation Requirement for Maze (II) in Sector II

					 		(Unit: MCM)	
		ETcrop	ЕТсгор		Net ETcrop		Water	
<u>Month</u>	days	(mm/day)	(mm/luday)(m		(mm/10day)	Area (na)	<u>kequirement</u>	
	Ţ	•		26.7				
May	2	# T		26.7	tale to the		, * · ·	
	3			26. 7		· · · · · · · · · · · · · · · · · · ·		
T	4		•	31. 7 31. 7		***		
Jun	5	- *		31. 7				
	$-\frac{6}{7}$			23. 3				
				23. 3				
July	8			23. 3				
	10		· · · · · · · · · · · · · · · · · · ·	26.7				
Aug	11			26. 7		•	4	
Aug	12			26. 7		: l		
	13			25. 0	· · · · · · · · · · · · · · · · · · ·			
Sept	14			25. 0				
oopt	15			25. 0				
	16	2. 03	20. 3	20.0	0. 3	11	0.000	
0ct	17	2.03	20. 3	20. 0	0. 3	33	0.000	
	18	2.07	20. 7	20.0	0. 7	55	0.001	
	19	1.56	15. 6	5. 0	10. 6	76	0.017	
Nov	20	2.48	24. 8	5.0	19.8	99	0.042	
	21	2.65	26. 5	5. 0	21.5	120	0.055	
	22	2.71	27. 1		27. 1	131	0.076	
Dec	23	2. 88	28. 8		28.8	131	0.081	
	24	3, 23	32. 3		32. 3	131	0.091	
	25	3. 30	33.0		33.0	131	0.093	
Jan	26	3. 35	33. 5		33. 5	. 131	0.094	
	27	3, 73	37. 3		37. 3	120	0.096	
	28	3.61	36. 1	1. 7	34.4	99	0.073	
Feb	29	3.44	34. 4	1.7	32.8	76	0.054	
	30	3. 39	33. 9	1.7	32. 2	55	0.038	
	31	2. 90	29. 0		29.0	33	0. 020	
Mar	32	3. 21	32. 1		32. 1	- 11	0.008	
	33							
	34			6. 7				
Apr	35			6. 7			1.5	
	36			6. 7			1. 1	

Table F.1-32 Irrigation Requirement for Maze (III) in Sector II

	10	Drama	PT	D.	Nat Dragge	Inninati	(Unit: MCM)
					Net ETcrop		Water Requirement
INJECTI	1	Visiny GGZY	CHILD TOUGHT	26.7	(mily 10000)	m va may	1.0.40.1.0.1.011
May	2			26. 7			
111.00	3			26.7	1		
	4	· · · · · · · · · · · · · · · · · · ·		31. 7	·		
Jun	5			31.7			
	6			31. 7			
	7			23. 3			
July	8			23. 3			
	9 .		100	23. 3		4 2	
	10			26.7			
Aug	11		*	26.7			
1 2	12	. 1.		26.7		: .	•
	13	:		25.0			
Sept	14			25.0			
	15			25.0			
. :	16			20.0			
0ct	17	· .		20.0	1		٠.,
	18	1. 92	19. 2	20.0	*	- 11	
	19	1. 25	12. 5	5. 0	7. 5	34	0.000
Nov	20	1.90	19.0	5.0	14.0	:58	0.017
	21	2. 21	22. 1	5.0	17.1	80	0.029
	22	2.41	24. 1		24. 1	103	0.053
Dec	23	2.50	25.0		25. 0	126	0.068
	24	2.79	27. 9		27. 9	138	0.082
	25	3.06	30.6		30. 6	138	0.090
Jan	26	3.42	34. 2		34. 2	138	0.101
a .	27	3.98	39.8		39 <u>.</u> 8	138	0.117
	28	3.81	38.1	1.7	36. 5	138	0. 108
Feb	29	3.73	37.3	1.7	35. 6	126	0.097
	30	3.87	38.7	1,7	37 <u>.</u> 1	103	0.083
	31	3. 53	35. 3		35. 3	. 80	0.061
Mar	32	3. 93	39. 3		39. 3	58	0.048
	33	3.73	37. 3		37. 3	34	0.027
	34	3. 34	33. 4	6. 7	26. 7	11	0.006
Apr	35		•	6. 7			
	36	,	-	6. 7			

B:

Table F.1-33	Irrigation	Requirement for	Rice (I)	in	Sector	II

21275	3 2 4		nm.				(Unit	: MCM)
					t ETcrop li			
Month					m/10day) Ar		Kequ	
	1	5. 30	53.0	26.7	26. 4	310	1	0.175
May	2	5. 35	53. 5	26.7	26. 8	379		0. 218
	3	4.84	48.4	26.7	21.7	448		0. 208
	4	4.82	48. 2	31. 7	16.5	517		0. 182
Jun	5	4.86	48.6	31. 7	16. 9	551	. •	0. 200
,	6_	5, 03	50.3	31.7	18.6	551		0. 220
	- 7	5. 28	52. 8	23. 3	29. 5	551		0.348
July	8	5. 35	53. 6	23. 3	30. 2	551		0.35
	9	<u>5. 31</u>	53. 1	23. 3	29. 8	551		0, 351
	- 10	5. 27	52. 7	26. 7	26. 0	551		0.307
Aug	11	5. 10	51.0	26.7	24. 4	517		0. 270
	12	5.02	50.2	26. 7	23. 5	448	1	0. 22
	13	4. 63	46. 3	25. 0	21. 3	379		0.17
Sept	14	4. 29	42.9	25. 0	17. 9	310	;	0.119
- • •	15	4. 03	40. 3	25. 0	15. 3	241		0.079
	16	3. 90	39.0	20.0	19.0	172	1.	0.070
0ct	17	3. 90	39. 0	20.0	19. 0	103		0.04
	18	3. 70	37. 0	20.0	17. 0	34		0.013
	19	<u> </u>		5. 0				5, 51,
Nov	20			5. 0	e de la companya de la companya de la companya de la companya de la companya de la companya de la companya de La companya de la companya de la companya de la companya de la companya de la companya de la companya de la co			
1101	21			5. 0				
	22			0.0				
Dec	23							
Dec	24				•	•	1.4	
	25							
Jan	26							
Jan	27	•					** .	
				1.7				·····
P.L	28		* .					
Feb	29			1. 7		* *		
	30			1.7		· · · · · · · · · · · · · · · · · · ·		
14.	31				-	e. 1		•
Mar	32	F 44	.		FA A			
	33	5.08	50.8		50.8	34		0.03
	34	4. 98	49. 8	6. 7	43. 2	103		0.09
Apr	35	5. 15	51. 5	6. 7	44. 8	172		0.16
	36	5. 30	53.0	6. 7	46. 4	241		0. 239

Table F.1-34 Irrigation Requirement for Rice (II) in Sector II

	10	ETerop	ETcrop	Pe	Net BTcrop	Irrigation	Water	
						Area (ha)	Requirement	
	1			26. 7				
May	2			26. 7				
	3			26. 7				
	4			31. 7				
Jun	5			31. 7				
	6			31.7				
	7			23. 3				
July	8	•		23. 3				
	9			23.3				
	10			26. 7	•			
Aug	11			26.7	•			
	12			26. 7	:			
	13			25.0		-		
Sept	14	-		25. 0			1.0	
-	15	3. 57	35. 7	25.0	10.7	.18_	0.004	
12 - 2	16	3. 67	36. 7	20.0	16. 7	51	0.018	
0ct	17	3.86	38.6	20.0	18.6	86	0.034	
	18	3.77	37.7	20.0	17.7	120_	0.046	
ł -	19	2. 50	25. 0	5.0	20.0	138	0.059	
Nov	20	3.64	36. 4	5. 0	31.4	138	0.093	
a. B	21	3.74	37.4	5.0	32, 4	138	0.096	
	22	3. 70	37.0		37. 0	138	0.109	
Dec	23	3.62	36. 2		36. 2	138	0. 107	
1 .	24	3. 98_	39. <u>8</u>		39.8	138_	0. 117	
	25	4.08	40.8		40.8	138	0.120	
Jan	26	4. 28	42.8		42.8	138	0.126	
4.1	27	4.84	48. 4		48.4	138	0. 143	
	28	4. 80	48.0	1. 7	46. 3	138	0. 137	
Feb	29	4. 76	47.6	1.7	45. 9	120	0.118	
	30	5.02	50.2	1.7	48.5	86_	<u>0.090</u>	
	31	4.75	47.5		47.5	51	0.052	
Мат	32	5. 61	56.1		56.1	18	0. 021	
	33	5. 72	57. 2		57. 2			
	34	5. 30	53.0	6.7	46. 3			
Apr	35	5. 20	52.0	6. 7	45. 3		•	
	36	5. 20_	52. <u>0</u>	6. 7	45. 3			