

## 6.2 LONG TERM SIMULATION

### 6.2.1 CONDITIONS OF SIMULATION

Under the following conditions, the base flow simulation for a long-term period was carried out, using the model verified in Section 6.1:

- ① Discharge reference model;
  - Rowojedang Intake for Unit M, K. Mujur
  - K. Leprak No. 1 Check Dam for Unit R, K. Rejali
  - Planned Pronojiwo Dam for Unit G, K. Glidik
- ② Simulation period;  
30 years, from 1953 to 1982
- ③ Monthly rainfall data used;
  - Besuk Sat for Unit M, K. Mujur from 1952 to 1982
  - Curah Kobo'an for Unit R, K. Rejali from 1952 to 1982
  - Supit Urang for Unit G, K. Glidik from 1952 to 1982  
(Data from 1952 to 1969 is estimated by correlation to Curah Kobo'an)

### 6.2.2 SIMULATION RESULTS

The simulation results of long-term base flow are shown in the following figures and tables.

- ① Fig.-5.15 : Annual Mean Base Flow
- ② Fig.-5.16 : Annual Mean Monthly Base Flow Distribution
- ③ Fig.-5.17 : Annual Mean Monthly Base Flow and Rainfall Distribution
- ④ Fig.-5.18 : Monthly Distribution of Base Flow and Rainfall
- ⑤ Table-5.11 : Characteristics of Simulated Monthly Base Flow
- ⑥ Table-5.12 : Computer Output of Long-term Base Flow Simulation

From these figures and tables, the following characteristics of the base flow discharge are summarized:

- ① Among three points, the highest amounts of mean base flow and specific mean base flow are obtained at the planned Pronojiwo dam site of K. Glidik. The fluctuation coefficient is the smallest at the same site. This means that the area upstream of the point possesses a greater natural reservoir in the Mt. Semeru than the others;
- ② The periodicity of the monthly base flow is noted although the interval is not one but two or three years;
- ③ The fluctuation of the annual mean monthly base flow is rather leveled due to the reason stated above in ②;

- ④ The fluctuation of the annual mean base flow can be said to be small judging from its fluctuation coefficient (slightly lower than 20%),

Table-5.11 Characteristics of Simulated Monthly Base Flow

Reference Point	Items	$Q$ ( $m^3/s$ )	$\sigma_n$ ( $m^3/s$ )	$c_f$ (N.D.)	$q$ ( $m^3/s/km^2$ )
(M)	Intake Rowojedang of K. Mujur	0.898	0.258	0.287	0.013
(R)	Leprak No. 1 Check Dam of K. Rejali	0.992	0.309	0.312	0.036
(G)	Planned Pronojiwo Dam of K. Glidik	2.648	0.681	0.276	0.045

Notes:  $Q$  = Monthly mean base flow

$\sigma_n$  = Standard deviation

$c_f$  = Coefficient of fluctuation ( $\sigma_n/Q$ )

$q$  = Specific mean base flow ( $Q/area$ )

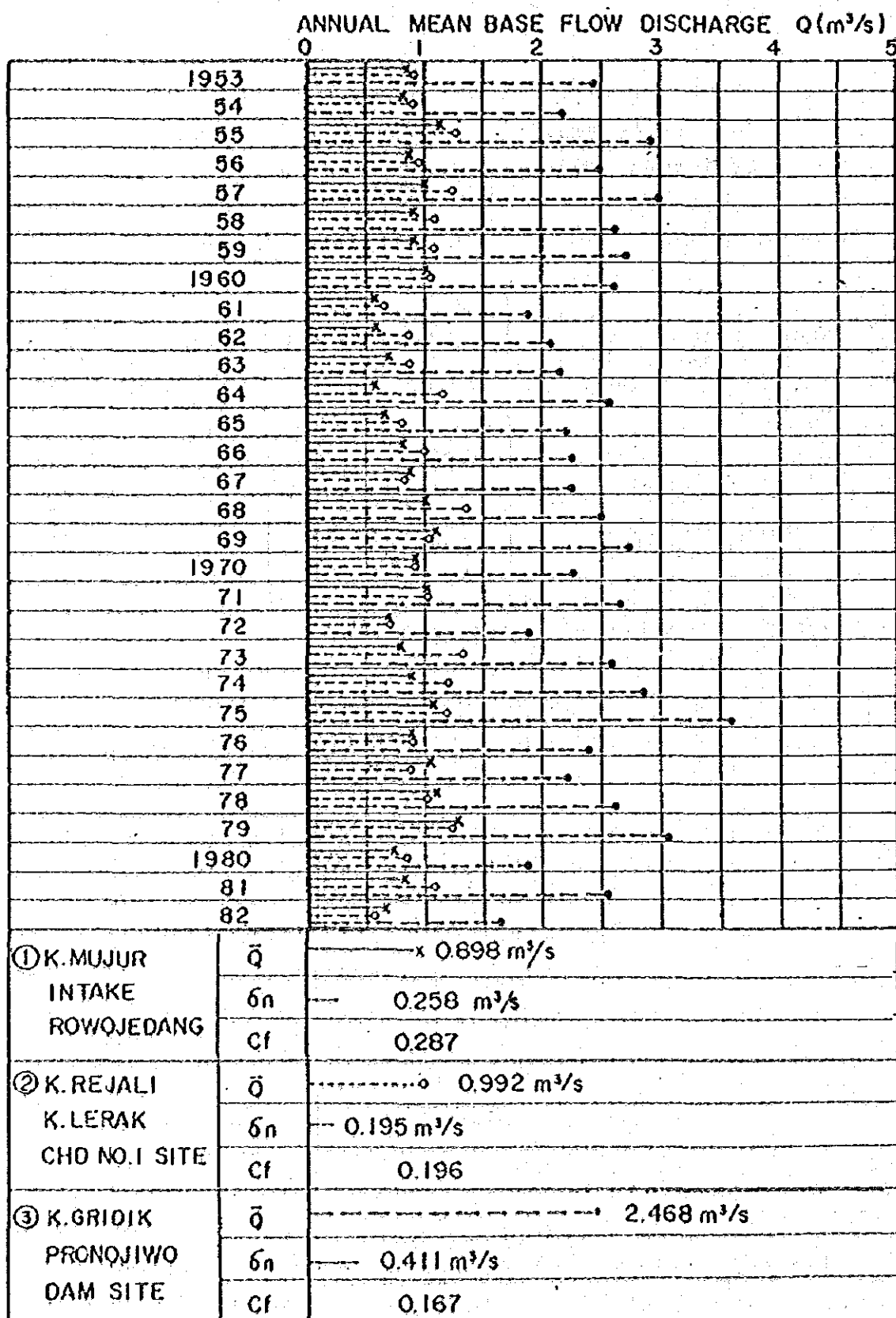


Fig.-5.15 Annual Mean Base Flow

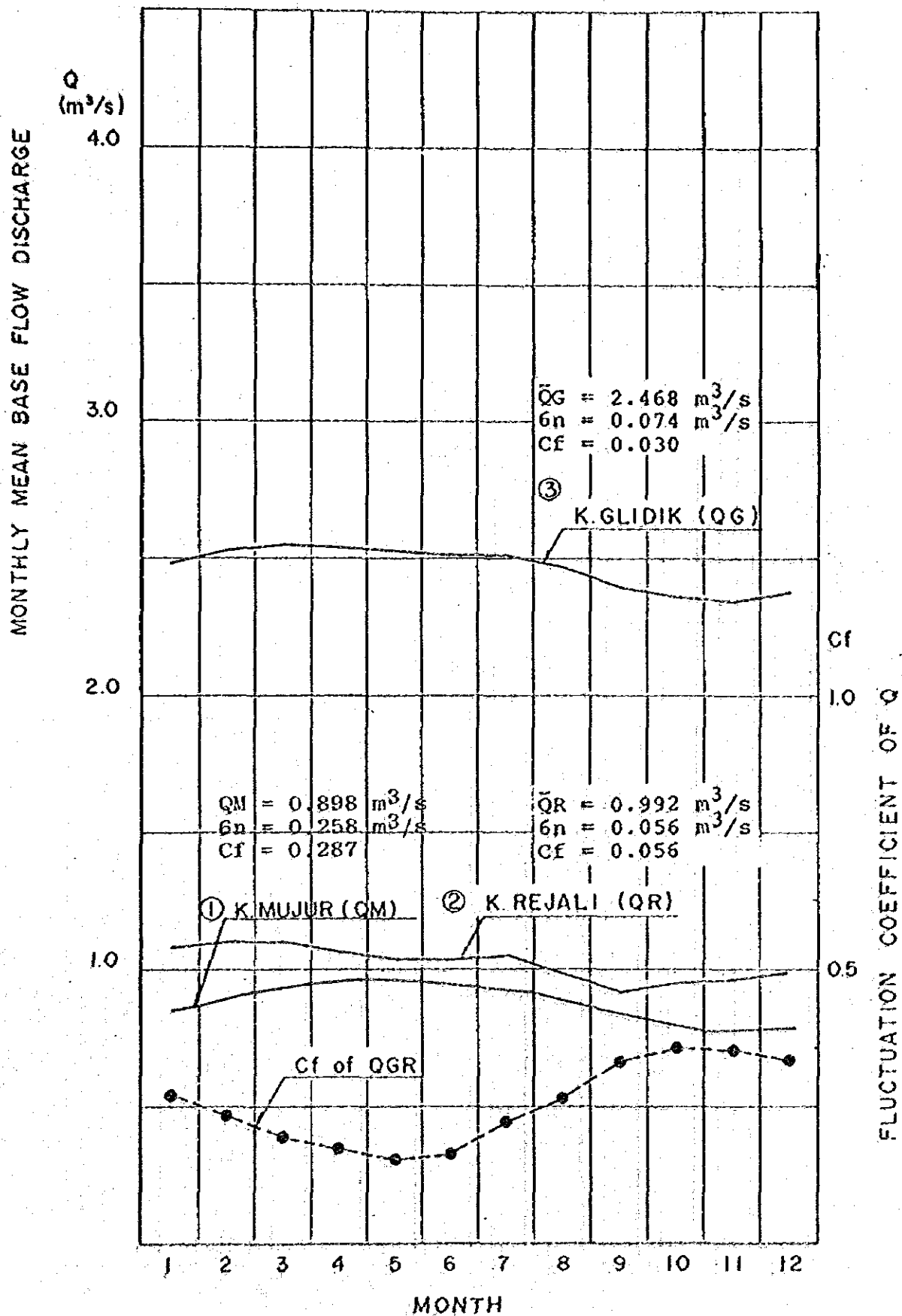


Fig.-5.16 Annual Mean Monthly Base Flow Distribution

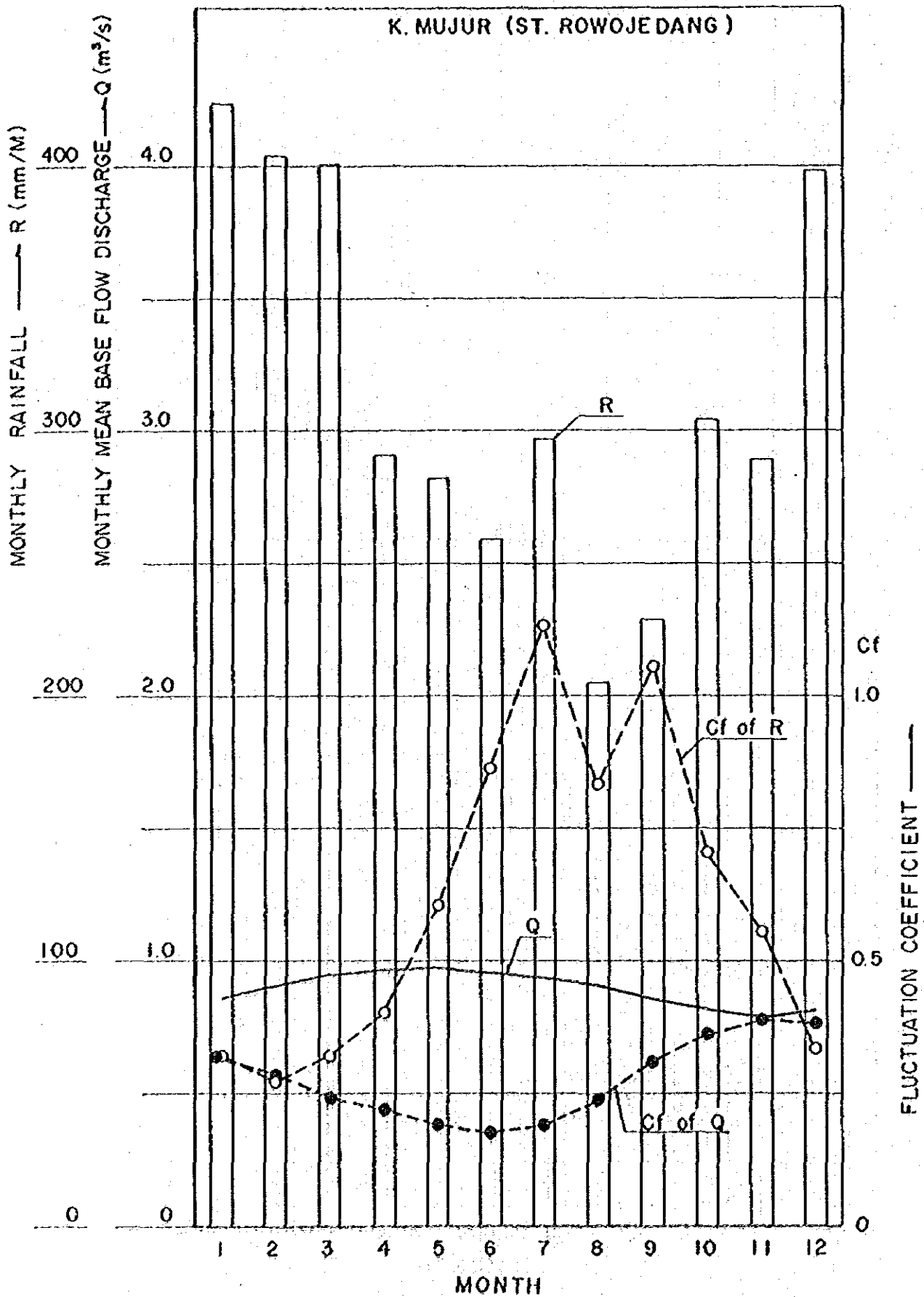


Fig.-5,17(1) Annual Mean Monthly Base Flow and Rainfall Distribution

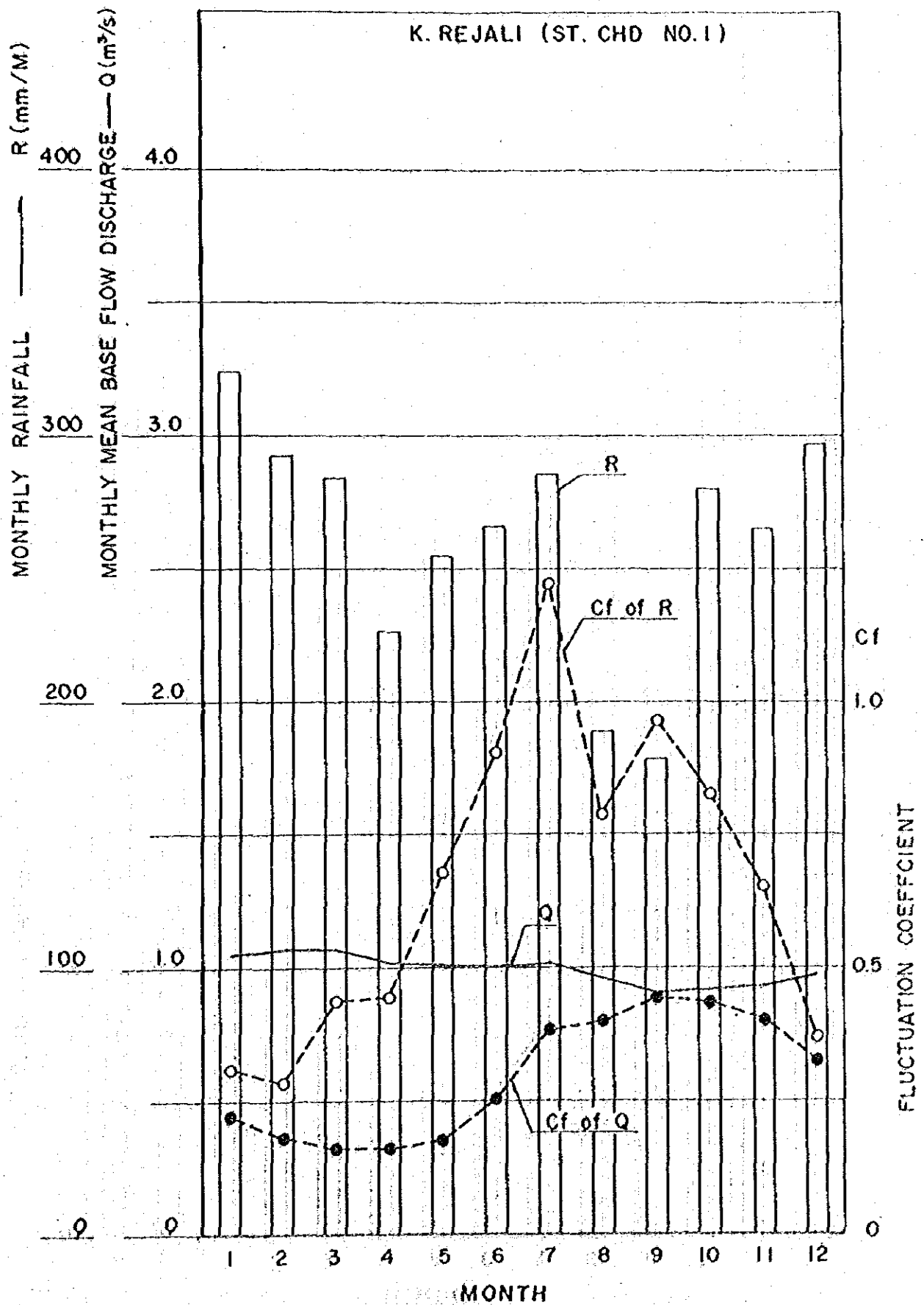


Fig.-5.17(2) Annual Mean Monthly Base Flow and Rainfall Distribution

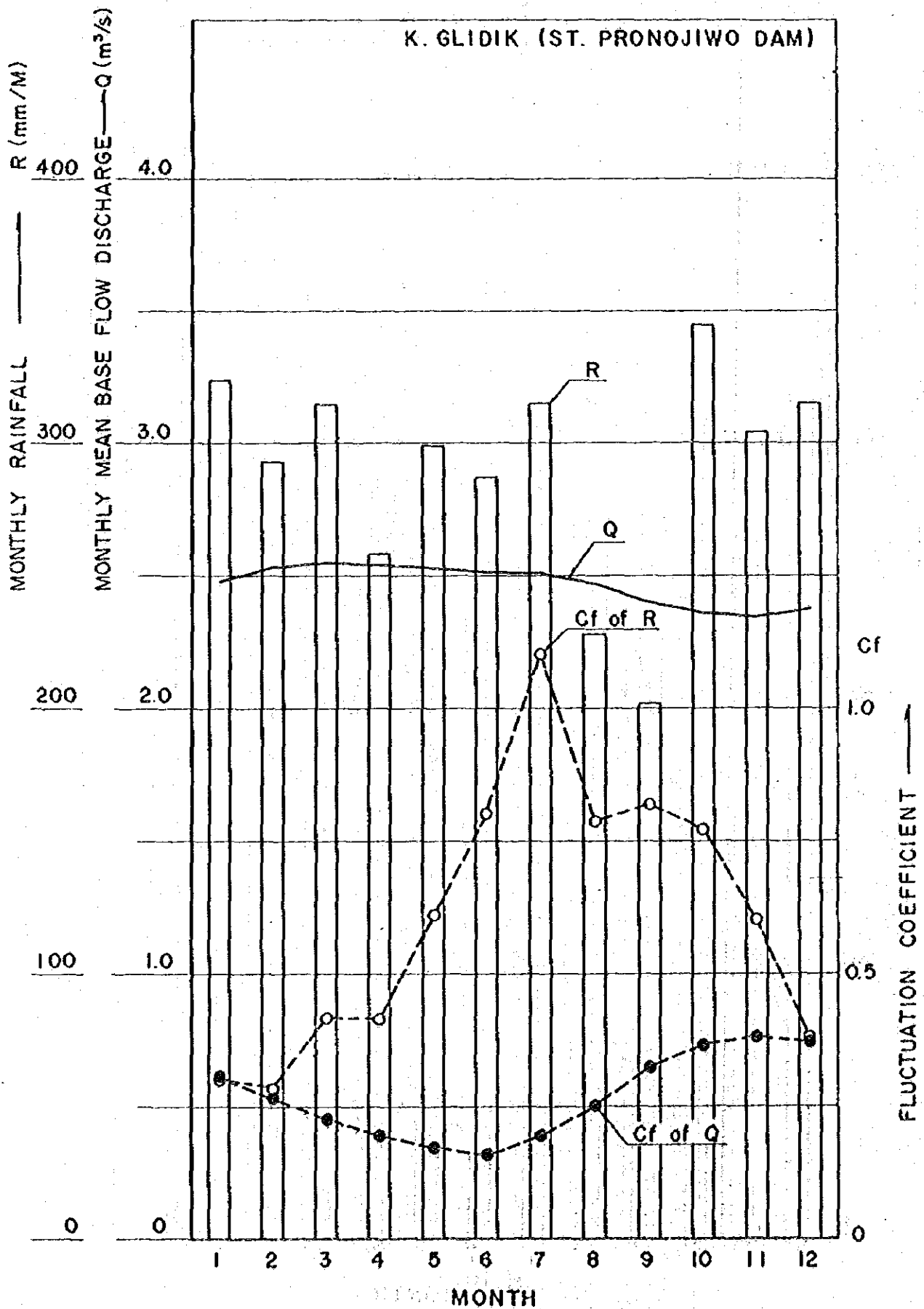


Fig.-5.17(3) Annual Mean Monthly Base Flow and Rainfall Distribution



Table-5.12 M (1) Computer Output of Long-term Base Flow Simulation

***** K. MUJUR (ST. KUMUDJANG) 1953-1982 ***** RAINFALL (mm)														
	1	2	3	4	5	6	7	8	9	10	11	12	TOTAL	MEAN
1953	282.0	383.0	442.0	396.0	346.0	12.0	99.0	119.0	10.0	101.0	205.0	468.0	2863.0	238.6
1954	457.0	372.0	317.0	483.0	251.0	487.0	235.0	348.0	28.0	216.0	384.0	368.0	3848.0	320.7
1955	563.0	344.0	353.0	185.0	195.0	688.0	1262.0	344.0	388.0	593.0	291.0	212.0	5418.0	451.5
1956	126.0	457.0	249.0	93.0	466.0	285.0	410.0	254.0	85.0	301.0	188.0	600.0	3514.0	292.8
1957	348.0	425.0	658.0	243.0	175.0	105.0	1268.0	140.0	59.0	25.0	12.0	478.0	3936.0	328.0
1958	473.0	335.0	382.0	350.0	224.0	655.0	212.0	491.0	112.0	341.0	351.0	466.0	4392.0	366.0
1959	376.0	433.0	168.0	239.0	421.0	317.0	293.0	39.0	334.0	185.0	228.0	636.0	3669.0	305.7
1960	393.0	458.0	430.0	452.0	638.0	531.0	74.0	214.0	284.0	282.0	285.0	232.0	4273.0	356.1
1961	319.0	225.0	183.0	432.0	297.0	42.0	174.0	6.0	2.0	2.0	102.0	213.0	1997.0	166.4
1962	580.0	483.0	311.0	43.0	15.0	163.0	531.0	210.0	12.0	276.0	260.0	435.0	3319.0	276.0
1963	575.0	318.0	518.0	356.0	20.0	79.0	16.0	5.0	0.0	53.0	192.0	278.0	2410.0	200.8
1964	212.0	354.0	464.0	212.0	264.0	154.0	80.0	217.0	293.0	624.0	399.0	149.0	3422.0	285.2
1965	375.0	204.0	490.0	163.0	159.0	60.0	98.0	12.0	101.0	124.0	388.0	347.0	2521.0	210.1
1966	427.0	412.0	477.0	263.0	409.0	66.0	36.0	261.0	385.0	426.0	529.0	412.0	4103.0	341.9
1967	577.0	638.0	291.0	186.0	38.0	116.0	253.0	90.0	54.0	136.0	62.0	639.0	3080.0	256.7
1968	238.0	302.0	360.0	500.0	469.0	399.0	1040.0	300.0	751.0	384.0	301.0	604.0	5678.0	473.2
1969	661.0	493.0	602.0	337.0	129.0	100.0	239.0	117.0	138.0	219.0	176.0	600.0	3811.0	317.6
1970	330.0	415.0	382.0	345.0	437.0	361.0	387.0	91.0	382.0	292.0	398.0	438.0	4258.0	354.8
1971	540.0	534.0	476.0	157.0	430.0	395.0	171.0	87.0	293.0	516.0	291.0	347.0	4237.0	353.1
1972	335.0	197.0	542.0	179.0	278.0	94.0	37.0	30.0	16.0	10.0	223.0	340.0	2281.0	190.1
1973	433.0	228.0	498.0	344.0	449.0	257.0	326.0	127.0	887.0	475.0	247.0	375.0	4646.0	387.2
1974	271.0	504.0	243.0	184.0	201.0	108.0	72.0	730.0	325.0	752.0	504.0	463.0	4357.0	363.1
1975	510.0	430.0	495.0	423.0	176.0	97.0	110.0	354.0	550.0	349.0	305.0	501.0	4300.0	358.3
1976	475.0	344.0	404.0	199.0	21.0	95.0	95.0	70.0	40.0	801.0	748.0	253.0	3635.0	302.9
1977	567.0	565.0	638.0	430.0	249.0	166.0	115.0	82.0	213.0	355.0	108.0	524.0	4012.0	334.3
1978	381.0	381.0	306.0	252.0	597.0	639.0	621.0	456.0	771.0	542.0	298.0	372.0	5616.0	468.0
1979	768.0	553.0	282.0	501.0	362.0	789.0	167.0	470.0	126.0	108.0	421.0	245.0	4792.0	399.3
1980	399.0	450.0	222.0	375.0	143.0	22.0	33.0	264.0	35.0	365.0	223.0	326.0	2857.0	238.1
1981	408.0	343.0	302.0	232.0	516.0	465.0	447.0	209.0	199.0	263.0	544.0	288.0	4214.0	351.2
1982	326.0	561.0	400.0	264.0	100.0	52.0	17.0	28.0	0.0	7.0	8.0	353.0	2146.0	176.8
TOTAL	12725.0	12141.0	12005.0	8744.0	8475.0	7797.0	8918.0	6165.0	6873.0	9125.0	8671.0	11962.0	113605.0	9467.2
MEAN	424.2	404.7	400.2	291.6	287.5	259.9	247.3	205.5	229.1	304.2	269.0	398.7	3786.8	315.6
S.D.	138.5	109.9	128.3	118.2	170.4	223.9	336.3	170.9	241.4	214.0	160.6	133.6	960.0	80.0
CF	0.326	0.272	0.321	0.405	0.603	0.862	1.131	0.832	1.054	0.704	0.556	0.335	0.254	0.254

Table-5.12 M (2) Computer Output of Long-term Base Flow Simulation

***** K. MUJUR (ST. KOWUJEDANG) 1953-1982 ***** HUNOFF ( m <sup>3</sup> /s )														
	1	2	3	4	5	6	7	8	9	10	11	12	TOTAL	MEAN
1953	1.007	1.040	1.042	1.117	1.137	1.074	0.973	0.834	0.676	0.559	0.490	0.500	10.494	0.874
1954	0.560	0.642	0.719	0.799	0.841	0.916	0.938	0.968	0.918	0.863	0.820	0.801	9.786	0.816
1955	0.856	0.903	0.949	0.943	0.912	0.955	1.159	1.278	1.403	1.473	1.430	1.364	13.625	1.135
1956	1.258	1.183	1.097	0.993	0.930	0.857	0.848	0.849	0.807	0.789	0.754	0.797	11.162	0.930
1957	0.831	0.897	1.005	1.040	1.036	0.984	1.119	1.123	1.136	1.051	0.889	0.803	11.917	0.993
1958	0.787	0.793	0.849	0.890	0.973	0.937	0.938	1.017	1.013	1.005	0.975	0.977	11.053	0.921
1959	0.983	1.021	0.999	0.968	0.952	0.925	0.922	0.867	0.838	0.773	0.730	0.777	10.756	0.896
1960	0.923	0.907	0.946	1.045	1.134	1.222	1.215	1.187	1.115	1.028	0.964	0.900	12.524	1.044
1961	0.861	0.816	0.765	0.761	0.760	0.734	0.715	0.632	0.535	0.438	0.359	0.323	7.701	0.642
1962	0.396	0.501	0.612	0.661	0.650	0.620	0.654	0.671	0.665	0.668	0.637	0.653	7.387	0.616
1963	0.736	0.809	0.928	1.001	0.973	0.911	0.797	0.666	0.541	0.423	0.346	0.325	6.456	0.705
1964	0.331	0.393	0.497	0.577	0.662	0.694	0.670	0.667	0.659	0.724	0.792	0.824	7.498	0.625
1965	0.864	0.846	0.677	0.872	0.855	0.793	0.710	0.590	0.495	0.419	0.425	0.404	8.210	0.684
1966	0.547	0.647	0.763	0.841	0.924	0.917	0.866	0.816	0.782	0.786	0.847	0.905	9.642	0.803
1967	0.907	1.107	1.158	1.170	1.102	0.996	0.895	0.776	0.662	0.569	0.467	0.496	10.396	0.866
1968	0.514	0.584	0.676	0.777	0.876	0.970	1.167	1.255	1.413	1.459	1.448	1.454	12.594	1.050
1969	1.479	1.480	1.320	1.491	1.389	1.249	1.099	0.950	0.828	0.735	0.648	0.664	13.531	1.128
1970	0.682	0.752	0.827	0.890	0.955	1.001	1.048	1.010	1.001	0.956	0.942	0.951	11.006	0.917
1971	1.003	1.068	1.136	1.132	1.142	1.131	1.082	1.007	0.937	0.907	0.880	0.886	12.309	1.020
1972	0.888	0.868	0.907	0.892	0.891	0.851	0.772	0.662	0.543	0.424	0.369	0.368	8.434	0.703
1973	0.428	0.490	0.603	0.694	0.804	0.873	0.928	0.916	1.023	1.077	1.115	1.145	10.097	0.841
1974	1.112	1.108	1.075	1.027	0.946	0.878	0.760	0.774	0.766	0.901	1.018	1.116	11.502	0.950
1975	1.204	1.259	1.304	1.334	1.295	1.197	1.060	0.943	0.909	0.894	0.905	0.946	13.250	1.104
1976	0.983	1.014	1.075	1.075	1.020	0.929	0.798	0.666	0.551	0.595	0.702	0.799	10.207	0.851
1977	0.948	1.062	1.145	1.287	1.322	1.281	1.185	1.033	0.893	0.801	0.712	0.727	12.436	1.036
1978	0.734	0.775	0.819	0.848	0.924	1.030	1.154	1.253	1.383	1.453	1.469	1.452	13.292	1.108
1979	1.479	1.487	1.468	1.454	1.384	1.403	1.340	1.327	1.234	1.122	1.042	0.950	15.691	1.308
1980	0.914	0.927	0.909	0.911	0.873	0.792	0.705	0.644	0.556	0.550	0.533	0.557	8.871	0.739
1981	0.613	0.673	0.732	0.775	0.650	0.919	0.997	1.019	1.006	0.963	0.968	0.951	10.465	0.872
1982	0.961	1.009	1.032	1.041	0.997	0.908	0.788	0.662	0.525	0.403	0.296	0.274	8.896	0.741
TOTAL	25.777	27.060	28.552	29.305	29.431	28.947	28.302	27.063	25.811	24.808	23.973	24.152	323.188	26.933
MEAN	0.859	0.902	0.952	0.977	0.981	0.965	0.943	0.902	0.860	0.827	0.799	0.805	10.773	0.898
S.D.	0.279	0.260	0.236	0.216	0.186	0.173	0.182	0.216	0.269	0.299	0.313	0.309	2.046	0.171
CI	0.325	0.288	0.248	0.220	0.190	0.180	0.193	0.239	0.313	0.361	0.392	0.383	0.190	0.190

Table-5.12 M (3) Computer Output of Long-term Base Flow Simulation

***** K. MUJUR (ST. KOWOJEDANG) 1953-1982 *****				RUNOFF (10 <sup>3</sup> m <sup>3</sup> /day)								TOTAL	MEAN
1	2	3	4	5	6	7	8	9	10	11	12		
1953	87.0	93.5	96.5	95.2	92.8	84.1	72.1	58.4	48.3	42.3	43.2	906.7	75.6
1954	48.4	62.1	69.0	72.7	79.2	81.0	83.6	79.5	74.6	70.8	69.2	845.5	70.5
1955	74.0	82.0	81.5	78.8	82.5	100.1	110.4	121.2	127.3	123.6	117.9	1177.2	98.1
1956	108.7	94.8	85.8	80.4	74.0	73.2	73.3	69.8	68.1	65.2	68.9	964.4	80.4
1957	71.8	86.8	89.9	89.5	85.1	96.7	97.1	98.2	90.8	76.8	69.4	1029.6	85.8
1958	68.0	73.2	76.9	75.5	80.9	81.0	87.9	87.5	86.8	84.3	84.4	955.0	79.6
1959	85.0	86.3	83.6	82.3	80.0	79.7	74.9	72.4	66.8	63.1	67.1	929.4	77.4
1960	71.1	85.2	90.3	98.0	105.6	105.0	102.5	96.2	88.8	83.3	77.8	1082.1	90.2
1961	74.4	66.1	65.8	65.7	63.4	61.8	54.0	46.2	37.9	31.0	27.9	665.4	55.4
1962	34.2	52.8	57.1	56.2	53.9	56.5	58.0	57.5	57.7	55.0	56.4	638.3	53.2
1963	63.6	60.9	80.1	84.1	78.7	68.8	57.6	46.7	36.5	29.9	28.1	730.6	60.9
1964	28.6	33.9	42.9	49.9	59.9	58.7	57.6	56.9	62.6	66.4	71.2	647.8	54.0
1965	74.6	73.1	75.8	73.8	68.5	61.3	51.0	42.8	36.2	36.7	40.1	709.3	59.1
1966	47.2	55.0	65.9	70.8	70.2	74.8	70.5	67.5	67.9	73.2	78.2	933.0	69.4
1967	86.1	95.0	101.1	95.3	86.1	77.3	67.0	57.2	49.2	40.4	42.9	898.2	74.8
1968	44.4	58.4	67.1	75.7	83.8	100.9	108.5	122.1	126.1	125.1	125.6	1088.1	90.7
1969	127.8	127.9	131.4	120.0	107.9	94.9	82.0	71.5	63.5	56.0	57.4	1169.1	97.4
1970	58.9	65.0	71.5	82.5	86.5	89.6	87.2	86.5	82.6	81.4	82.2	950.9	79.2
1971	86.7	92.3	98.2	98.6	97.7	93.4	87.0	80.9	78.4	76.0	76.5	1063.5	88.6
1972	76.8	75.0	78.4	77.0	73.5	66.7	57.2	46.9	36.6	31.9	31.8	728.7	60.7
1973	37.0	42.3	52.1	60.5	75.4	80.2	79.2	88.4	93.1	96.3	99.0	872.4	72.7
1974	96.1	95.7	92.0	88.8	75.6	65.7	66.9	66.2	77.8	88.0	96.4	993.8	82.8
1975	104.0	108.7	112.6	111.9	103.5	91.6	81.5	78.5	77.2	78.2	81.8	1144.8	95.4
1976	84.9	87.6	92.9	88.1	80.3	69.0	57.5	47.6	51.4	60.7	69.0	881.9	73.5
1977	81.9	91.8	102.4	114.2	110.7	102.3	89.3	77.1	69.2	61.5	62.8	1074.5	89.5
1978	63.4	66.9	73.2	79.9	89.0	99.7	108.2	119.5	125.5	126.9	125.4	1148.5	95.7
1979	127.7	128.5	125.6	119.6	121.2	115.8	114.7	106.7	97.0	90.1	82.1	1355.7	113.0
1980	78.9	80.1	78.6	75.4	68.4	60.9	55.6	48.1	47.5	46.1	48.1	766.5	63.9
1981	53.0	56.2	63.3	73.5	79.4	86.1	88.0	86.9	83.2	83.6	82.2	904.2	75.4
1982	83.0	87.2	89.2	86.1	78.4	68.1	57.2	45.4	34.8	25.5	23.7	768.6	64.3
TOTAL	2227.2	2534.5	2466.9	2532.0	2542.8	2445.3	2355.2	2230.1	2143.4	2071.3	2086.8	27923.7	2327.0
MEAN	74.2	78.0	82.2	84.4	84.8	81.5	77.9	74.3	71.4	69.0	69.6	930.8	77.6
S.D.	24.1	22.5	20.4	18.6	16.1	15.0	18.6	23.2	25.8	27.0	26.7	176.8	14.7
Cv	0.325	0.288	0.248	0.221	0.190	0.180	0.239	0.313	0.361	0.392	0.383	0.190	0.150

Table-5.12 R (1) Computer Output of Long-term Base Flow Simulation

***** K. REJALI (ST. (MD NO.1) 1953-1982) RAINFALL ( mm ) *****														
	1	2	3	4	5	6	7	8	9	10	11	12	TOTAL	MEAN
1953	205.0	219.0	331.0	227.0	310.0	79.0	57.0	207.0	26.0	129.0	226.0	317.0	2333.0	194.4
1954	389.0	250.0	58.0	346.0	227.0	335.0	237.0	290.0	67.0	80.0	417.0	540.0	3236.0	269.7
1955	279.0	169.0	207.0	72.0	160.0	750.0	888.0	318.0	318.0	453.0	243.0	269.0	4126.0	343.8
1956	148.0	320.0	126.0	64.0	243.0	208.0	418.0	321.0	93.0	242.0	244.0	472.0	2901.0	241.7
1957	189.0	274.0	616.0	251.0	103.0	187.0	1537.0	155.0	111.0	61.0	42.0	399.0	3925.0	327.1
1958	216.0	301.0	337.0	178.0	168.0	603.0	362.0	401.0	96.0	351.0	204.0	313.0	3530.0	294.2
1959	377.0	444.0	194.0	251.0	457.0	254.0	379.0	41.0	224.0	141.0	278.0	310.0	3350.0	279.2
1960	421.0	261.0	508.0	179.0	172.0	664.0	155.0	220.0	83.0	216.0	219.0	121.0	3219.0	268.2
1961	464.0	279.0	201.0	135.0	215.0	13.0	176.0	5.0	44.0	21.0	58.0	216.0	1830.0	152.5
1962	298.0	294.0	241.0	251.0	229.0	292.0	610.0	176.0	35.0	264.0	120.0	410.0	3220.0	268.3
1963	516.0	169.0	454.0	375.0	8.0	69.0	9.0	0.0	24.0	240.0	240.0	376.0	2500.0	208.3
1964	292.0	288.0	452.0	292.0	632.0	139.0	107.0	162.0	445.0	712.0	313.0	163.0	3997.0	333.1
1965	365.0	201.0	275.0	214.0	81.0	173.0	57.0	34.0	66.0	97.0	339.0	178.0	2100.0	175.0
1966	345.0	337.0	302.0	262.0	377.0	165.0	17.0	194.0	161.0	652.0	544.0	377.0	3823.0	318.6
1967	336.0	424.0	141.0	74.0	74.0	38.0	163.0	83.0	107.0	99.0	75.0	463.0	2082.0	173.5
1968	276.0	219.0	342.0	388.0	656.0	242.0	1148.0	346.0	417.0	234.0	140.0	364.0	4752.0	396.0
1969	378.0	385.0	298.0	454.0	77.0	195.0	151.0	142.0	95.0	253.0	156.0	388.0	2972.0	247.7
1970	246.0	215.0	156.0	239.0	372.0	353.0	230.0	75.0	209.0	183.0	458.0	382.0	3118.0	259.8
1971	402.0	304.0	240.0	62.0	448.0	372.0	60.0	72.0	317.0	388.0	311.0	186.0	3162.0	263.5
1972	342.0	235.0	303.0	126.0	206.0	90.0	21.0	17.0	16.0	32.0	261.0	239.0	1888.0	157.3
1973	532.0	333.0	420.0	336.0	489.0	433.0	532.0	135.0	728.0	391.0	228.0	212.0	4769.0	397.4
1974	301.0	426.0	216.0	164.0	148.0	121.0	78.0	616.0	501.0	874.0	353.0	411.0	4209.0	350.7
1975	445.0	251.0	339.0	276.0	204.0	120.0	75.0	313.0	385.0	420.0	244.0	295.0	3367.0	280.6
1976	235.0	302.0	307.0	155.0	44.0	48.0	96.0	65.0	46.0	716.0	904.0	176.0	3094.0	257.8
1977	413.0	257.0	359.0	329.0	65.0	57.0	113.0	34.0	111.0	108.0	90.0	337.0	2273.0	189.4
1978	351.0	351.0	231.0	313.0	467.0	347.0	235.0	203.0	333.0	251.0	193.0	182.0	3457.0	288.1
1979	312.0	499.0	204.0	286.0	337.0	1055.0	171.0	422.0	100.0	58.0	426.0	265.0	4135.0	344.6
1980	324.0	153.0	118.0	220.0	161.0	18.0	32.0	414.0	49.0	641.0	262.0	273.0	2665.0	222.1
1981	208.0	360.0	136.0	127.0	488.0	498.0	469.0	207.0	179.0	109.0	362.0	181.0	3324.0	277.0
1982	117.0	274.0	319.0	173.0	66.0	54.0	17.0	28.0	3.0	9.0	1.0	105.0	1166.0	97.2
TOTAL	9742.0	8794.0	8523.0	6822.0	7669.0	7992.0	8600.0	5696.0	5389.0	8425.0	7951.0	8920.0	94523.0	7876.8
MEAN	324.7	293.1	284.1	227.4	255.6	266.4	286.7	189.9	179.6	280.8	265.0	297.3	3150.8	262.6
S.D.	100.8	83.1	124.8	100.5	173.5	241.2	350.4	149.9	172.8	231.2	172.5	109.8	858.0	71.5
Cv	0.311	0.283	0.439	0.442	0.679	0.905	1.222	0.789	0.962	0.823	0.651	0.369	0.272	0.272

Table-5.12 R (2) Computer Output of Long-term Base Flow Simulation

***** K. NEJALI (ST. CHO NO.1) 1953-1982 *****														RUNOFF ( m <sup>3</sup> /s )	
	1	2	3	4	5	6	7	8	9	10	11	12	TOTAL	MEAN	
1953	1.251	1.158	1.176	1.119	1.141	0.974	0.801	0.766	0.596	0.547	0.595	0.715	10.838	0.903	
1954	0.876	0.898	0.761	0.865	0.865	0.957	0.959	0.996	0.847	0.721	0.880	1.118	10.742	0.895	
1955	1.126	1.040	0.980	0.817	0.756	1.178	1.657	1.615	1.554	1.576	1.425	1.335	15.060	1.255	
1956	1.178	1.182	1.035	0.853	0.831	0.786	0.934	0.994	0.862	0.864	0.866	1.054	11.439	0.953	
1957	0.999	1.014	1.293	1.235	1.066	0.979	1.966	1.741	1.497	1.229	0.961	1.045	15.025	1.252	
1958	0.991	1.024	1.075	0.985	0.890	1.140	1.188	1.280	1.111	1.150	1.066	1.080	12.981	1.082	
1959	1.155	1.267	1.167	1.116	1.227	1.166	1.221	1.006	0.961	0.898	0.881	0.935	12.960	1.080	
1960	1.067	1.059	1.237	1.125	1.020	1.323	1.186	1.123	0.953	0.905	0.874	0.774	12.646	1.054	
1961	0.967	0.960	0.940	0.848	0.821	0.651	0.643	0.511	0.427	0.341	0.297	0.388	7.820	0.652	
1962	0.533	0.661	0.725	0.779	0.804	0.874	1.184	1.109	0.924	0.933	0.821	0.961	10.306	0.859	
1963	1.172	1.079	1.214	1.256	1.000	0.845	0.657	0.506	0.404	0.490	0.566	0.735	9.923	0.827	
1964	0.814	0.872	1.047	1.075	1.367	1.226	1.049	0.971	1.102	1.436	1.408	1.257	13.643	1.137	
1965	1.285	1.158	1.118	1.047	0.890	0.834	0.690	0.547	0.454	0.412	0.580	0.600	9.617	0.801	
1966	0.746	0.862	0.999	1.014	0.890	1.025	0.832	0.805	0.756	1.103	1.319	1.363	11.935	0.995	
1967	1.353	1.398	1.217	1.015	0.856	0.699	0.667	0.577	0.516	0.460	0.400	0.662	9.821	0.818	
1968	0.745	0.776	0.896	1.025	1.328	1.273	1.928	1.652	1.821	1.640	1.391	1.372	16.048	1.337	
1969	1.376	1.395	1.336	1.398	1.152	1.030	0.907	0.612	0.709	0.748	0.707	0.850	12.420	1.035	
1970	0.865	0.850	0.792	0.808	0.934	1.027	1.011	0.667	0.840	0.797	0.982	1.088	10.858	0.905	
1971	1.192	1.197	1.136	0.940	1.078	1.151	0.974	0.627	0.883	0.988	1.025	0.962	12.353	1.029	
1972	1.026	0.995	1.024	0.909	0.873	0.761	0.610	0.479	0.367	0.295	0.421	0.517	8.278	0.690	
1973	0.829	0.936	1.047	1.143	1.302	1.397	1.550	1.365	1.657	1.636	1.481	1.333	15.716	1.310	
1974	1.270	1.327	1.215	1.083	0.954	0.824	0.691	1.003	1.194	1.653	1.627	1.624	14.466	1.206	
1975	1.637	1.493	1.454	1.377	1.255	1.080	0.846	0.908	0.994	1.110	1.076	1.078	14.351	1.196	
1976	1.031	1.046	1.070	0.976	0.810	0.667	0.561	0.489	0.404	0.866	1.414	1.303	10.656	0.888	
1977	1.374	1.291	1.300	1.301	1.099	0.920	0.803	0.639	0.559	0.492	0.440	0.598	10.816	0.901	
1978	0.745	0.871	0.883	0.953	1.132	1.189	1.147	1.079	1.116	1.082	1.006	0.931	12.132	1.011	
1979	0.970	1.154	1.041	1.074	1.112	1.706	1.527	1.556	1.319	1.071	1.164	1.123	14.860	1.238	
1980	1.146	1.024	0.891	0.849	0.767	0.605	0.492	0.699	0.597	0.969	0.989	1.005	10.038	0.836	
1981	0.967	1.044	0.943	0.844	1.057	1.240	1.367	1.261	1.132	0.964	1.029	0.957	12.808	1.067	
1982	0.850	0.884	0.941	0.873	0.728	0.599	0.499	0.378	0.289	0.221	0.161	0.196	6.588	0.549	
TOTAL	31.535	31.944	32.034	30.710	30.227	30.125	30.597	28.761	26.844	27.558	27.853	28.960	357.147	29.761	
MEAN	1.051	1.069	1.068	1.024	1.008	1.004	1.020	0.959	0.895	0.919	0.928	0.965	11.905	0.992	
S.D.	0.235	0.194	0.173	0.167	0.179	0.254	0.394	0.384	0.398	0.401	0.374	0.316	2.338	0.195	
CF	0.223	0.182	0.162	0.163	0.178	0.253	0.386	0.400	0.445	0.437	0.403	0.327	0.196	0.196	

Table-5.12 R (3) Computer Output of Long-term Base Flow Simulation

***** K. REJALI (ST. CHD NO.1) 1953-1982 ***** RUNOFF ( 10 <sup>3</sup> m <sup>3</sup> /day )														
	1	2	3	4	5	6	7	8	9	10	11	12	TOTAL	MEAN
1953	108.1	100.0	101.6	96.7	98.6	84.1	69.2	66.1	51.5	47.3	51.4	61.7	936.4	78.0
1954	75.7	77.6	65.7	74.7	74.7	82.7	82.9	86.0	73.2	62.3	76.0	96.6	928.1	77.3
1955	97.3	69.8	84.7	70.6	65.3	101.8	143.2	139.5	134.2	136.2	123.1	115.4	1301.2	108.4
1956	101.8	102.1	89.4	73.7	71.8	67.9	80.7	85.9	74.5	74.6	74.9	91.1	988.3	82.4
1957	86.3	87.6	111.7	106.7	92.1	84.9	169.8	150.4	129.4	106.2	83.0	90.3	1298.1	108.2
1958	85.0	84.5	92.9	85.1	76.9	98.5	102.6	110.6	96.0	99.4	92.1	93.4	1121.6	93.5
1959	99.8	109.4	100.8	96.4	106.0	100.7	105.5	86.9	83.0	74.2	76.1	80.8	1119.7	93.3
1960	92.2	91.5	106.8	97.2	88.1	114.3	102.5	97.0	82.4	78.2	75.5	66.9	1092.6	91.1
1961	83.6	85.2	81.2	73.3	71.0	56.2	55.0	44.1	36.9	29.5	25.7	33.5	675.7	56.3
1962	46.1	57.1	62.6	67.3	69.5	75.5	102.3	95.8	79.8	80.6	70.9	83.0	890.6	74.2
1963	101.2	93.2	104.9	108.0	86.4	73.0	56.8	43.8	34.9	42.3	48.9	63.5	857.4	71.4
1964	70.3	75.3	90.4	92.8	118.1	105.9	92.3	83.9	95.3	124.1	121.6	108.6	1178.7	98.2
1965	111.0	100.1	96.0	90.5	78.9	72.1	59.0	47.3	39.3	35.6	50.1	51.8	830.9	69.2
1966	64.4	74.5	86.3	87.6	95.9	88.6	71.9	69.6	65.3	95.3	114.0	117.8	1031.2	85.9
1967	116.9	120.7	105.1	87.7	74.1	60.4	57.6	49.8	44.6	39.7	34.6	57.2	848.6	70.7
1968	64.4	67.0	77.4	84.5	114.8	110.0	166.6	160.0	157.3	141.7	120.2	118.5	1386.6	115.5
1969	118.8	120.5	115.5	120.8	99.5	89.0	78.3	70.2	61.2	64.6	61.1	73.5	1073.1	89.4
1970	74.7	73.5	68.4	69.8	80.7	88.7	87.3	74.9	72.6	68.8	84.8	94.0	938.2	78.2
1971	103.0	103.4	98.1	81.2	93.2	99.4	84.1	71.5	76.3	85.4	88.6	83.1	1067.3	88.9
1972	88.7	86.0	88.4	78.6	75.5	65.7	52.7	41.4	31.7	25.5	36.4	44.7	715.2	59.6
1973	71.6	80.9	93.9	98.7	112.5	120.7	134.0	117.9	143.2	141.4	127.9	115.2	1357.9	113.2
1974	109.7	114.6	105.0	93.5	82.4	71.2	59.7	86.8	103.2	142.8	140.6	140.3	1249.9	104.2
1975	141.4	120.0	125.8	119.0	108.5	93.3	76.5	78.5	85.9	95.9	93.0	93.2	1239.9	103.3
1976	89.1	90.4	92.4	84.3	70.0	57.6	50.2	42.2	34.9	74.9	122.1	112.6	920.7	76.7
1977	118.7	111.6	112.3	112.4	94.9	79.5	69.4	55.2	48.3	42.5	38.0	51.7	934.5	77.9
1978	84.3	75.3	76.3	82.3	97.8	102.7	99.1	93.2	96.4	93.5	86.9	80.5	1048.3	87.4
1979	83.8	99.7	93.4	93.1	96.1	147.4	131.9	134.4	114.0	92.5	100.6	97.0	1263.9	107.0
1980	99.0	88.9	77.0	73.4	66.3	52.3	42.5	60.4	51.6	83.7	85.4	86.8	867.3	72.3
1981	83.6	90.2	81.5	73.3	91.3	107.1	118.1	108.9	97.8	83.2	88.9	92.7	1106.6	92.2
1982	73.5	76.3	81.3	75.4	62.9	51.8	40.5	32.7	24.9	19.1	13.9	16.9	569.2	47.4
TOTAL	2724.6	2759.9	2767.7	2653.4	2611.6	2602.8	2643.6	2485.0	2319.3	2381.0	2406.5	2502.1	30857.7	2571.3
MEAN	90.8	92.0	92.3	88.4	87.1	86.8	88.1	82.8	77.3	79.4	80.2	83.4	1028.6	85.7
S.D.	20.3	16.7	14.9	14.5	15.5	22.0	34.0	33.1	34.4	34.7	32.3	27.3	202.0	16.8
CF	0.223	0.182	0.162	0.163	0.178	0.253	0.386	0.400	0.445	0.437	0.403	0.327	0.196	0.196

Table-5.12 G (1) Computer Output of Long-term Base Flow Simulation

*****KGLIDIK (ST. PRONGJIWO DAM) 1953-1962 *****														RAINFALL (mm)	
	1	2	3	4	5	6	7	8	9	10	11	12	TOTAL	MEAN	
1953	237.0	250.0	357.0	258.0	337.0	117.0	97.0	259.0	67.0	165.0	257.0	343.0	2724.0	227.0	
1954	412.0	280.0	98.0	371.0	258.0	360.0	267.0	318.0	106.0	118.0	438.0	555.0	3581.0	298.4	
1955	307.0	203.0	239.0	111.0	194.0	754.0	886.0	344.0	344.0	473.0	273.0	298.0	4426.0	368.8	
1956	183.0	346.0	164.0	103.0	273.0	240.0	439.0	347.0	131.0	272.0	274.0	491.0	3263.0	271.9	
1957	222.0	303.0	627.0	281.0	140.0	220.0	1502.0	190.0	148.0	100.0	82.0	421.0	4236.0	353.0	
1958	248.0	328.0	362.0	211.0	202.0	615.0	386.0	423.0	134.0	376.0	236.0	340.0	3861.0	321.7	
1959	400.0	464.0	227.0	281.0	476.0	284.0	402.0	81.0	255.0	176.0	306.0	337.0	3689.0	307.4	
1960	442.0	290.0	525.0	212.0	206.0	673.0	190.0	251.0	121.0	248.0	250.0	157.0	3565.0	297.1	
1961	483.0	307.0	233.0	173.0	247.0	55.0	210.0	47.0	84.0	62.0	98.0	248.0	2247.0	187.2	
1962	325.0	322.0	271.0	281.0	260.0	320.0	622.0	210.0	76.0	293.0	156.0	432.0	3568.0	297.3	
1963	532.0	203.0	473.0	398.0	50.0	127.0	51.0	42.0	65.0	270.0	270.0	399.0	2880.0	240.0	
1964	320.0	316.0	472.0	320.0	642.0	174.0	144.0	196.0	465.0	718.0	340.0	197.0	4304.0	358.7	
1965	408.0	233.0	304.0	246.0	119.0	207.0	97.0	75.0	105.0	135.0	364.0	211.0	2504.0	208.7	
1966	370.0	362.0	415.0	291.0	400.0	199.0	59.0	227.0	195.0	661.0	559.0	400.0	4138.0	344.8	
1967	361.0	445.0	176.0	113.0	117.0	79.0	197.0	121.0	144.0	136.0	114.0	482.0	2485.0	207.1	
1968	304.0	250.0	367.0	411.0	646.0	272.0	1132.0	371.0	438.0	265.0	175.0	388.0	5019.0	418.2	
1969	401.0	408.0	325.0	473.0	116.0	228.0	186.0	177.0	133.0	283.0	191.0	411.0	3332.0	277.7	
1970	276.0	247.0	191.0	269.0	396.0	376.0	261.0	114.0	241.0	216.0	477.0	405.0	3471.0	289.2	
1971	376.0	279.0	363.0	70.0	710.0	404.0	80.0	55.0	341.0	456.0	326.0	281.0	3741.0	311.7	
1972	251.0	184.0	436.0	119.0	296.0	88.0	17.0	19.0	13.0	0.0	268.0	251.0	1942.0	161.8	
1973	505.0	436.0	508.0	261.0	423.0	400.0	389.0	216.0	216.0	793.0	462.0	243.0	4852.0	404.3	
1974	328.0	348.0	171.0	157.0	211.0	45.0	34.0	934.0	425.0	1131.0	416.0	520.0	4720.0	393.3	
1975	353.0	334.0	425.0	442.0	460.0	66.0	121.0	277.0	674.0	692.0	383.0	313.0	4540.0	378.3	
1976	263.0	300.0	325.0	200.0	12.0	57.0	68.0	133.0	79.0	692.0	976.0	118.0	3223.0	268.6	
1977	336.0	110.0	337.0	338.0	142.0	94.0	139.0	49.0	160.0	121.0	53.0	53.0	1932.0	161.0	
1978	274.0	237.0	338.0	298.0	523.0	682.0	614.0	452.0	591.0	551.0	226.0	215.0	5001.0	416.7	
1979	278.0	382.0	215.0	422.0	404.0	698.0	177.0	269.0	76.0	92.0	482.0	258.0	3753.0	312.7	
1980	237.0	198.0	124.0	295.0	179.0	19.0	29.0	376.0	95.0	444.0	335.0	209.0	2542.0	211.8	
1981	231.0	231.0	98.0	143.0	471.0	717.0	667.0	295.0	159.0	415.0	381.0	239.0	4047.0	337.2	
1982	84.0	197.0	306.0	198.0	61.0	43.0	0.0	17.0	0.0	0.0	0.0	241.0	1147.0	95.6	
TOTAL	9747.0	8793.0	9472.0	7746.0	8971.0	8613.0	9463.0	8867.0	6081.0	10354.0	9168.0	9456.0	104733.0	8727.2	
MEAN	324.9	293.1	313.7	258.2	299.0	287.2	315.4	228.9	202.7	345.1	305.6	315.2	3491.1	290.9	
S.D.	97.1	82.8	131.2	106.8	182.5	229.7	347.3	180.4	166.1	266.3	183.2	119.8	967.7	80.6	
CE	0.299	0.283	0.416	0.414	0.610	0.800	1.101	0.788	0.820	0.772	0.600	0.380	0.277	0.277	

Table-5.12 G (2) Computer Output of Long-term Base Flow Simulation

*****GLIDIK (ST. PRONGJWU DAM) 1953-1982 *****														
*****														
	1	2	3	4	5	6	7	8	9	10	11	12	TOTAL	MEAN
1953	2.959	2.941	2.941	2.940	2.923	2.774	2.537	2.279	1.962	1.746	1.644	1.666	29.413	2.451
1954	1.818	1.972	2.006	2.104	2.131	2.249	2.331	2.415	2.353	2.224	2.176	2.291	26.071	2.173
1955	2.447	2.559	2.557	2.395	2.251	2.400	2.627	3.219	3.523	3.631	3.554	3.487	34.849	2.904
1956	3.317	3.177	2.955	2.666	2.365	2.145	2.130	2.202	2.207	2.222	2.207	2.319	29.934	2.494
1957	2.383	2.482	2.697	2.799	2.804	2.718	3.248	2.468	3.742	3.570	3.173	2.906	35.993	2.900
1958	2.705	2.592	2.581	2.527	2.372	2.433	2.500	2.773	2.841	2.883	2.785	2.748	31.741	2.645
1959	2.747	2.842	2.853	2.845	2.853	2.809	2.884	2.775	2.680	2.479	2.365	2.295	32.427	2.702
1960	2.375	2.436	2.635	2.670	2.668	2.841	2.846	2.694	2.761	2.589	2.406	2.246	31.372	2.614
1961	2.241	2.262	2.304	2.264	2.200	2.021	1.943	1.750	1.578	1.375	1.191	1.114	22.244	1.854
1962	1.174	1.347	1.551	1.748	1.892	2.046	2.351	2.522	2.575	2.549	2.374	2.357	24.487	2.041
1963	2.480	2.537	2.717	2.618	2.719	2.575	2.293	1.982	1.695	1.515	1.423	1.528	26.283	2.190
1964	1.672	1.859	2.118	2.337	2.723	2.878	2.928	2.808	2.753	2.900	3.053	3.115	31.143	2.595
1965	3.134	3.002	2.900	2.789	2.607	2.457	2.212	1.914	1.639	1.428	1.412	1.436	26.930	2.244
1966	1.504	1.785	2.041	2.244	2.476	2.549	2.493	2.390	2.219	2.332	2.549	2.816	27.488	2.291
1967	3.008	3.153	3.103	2.977	2.737	2.430	2.176	1.896	1.661	1.459	1.307	1.387	27.295	2.275
1968	1.517	1.716	1.952	2.181	2.545	2.786	3.421	3.751	4.104	4.117	3.916	3.689	35.695	2.975
1969	3.535	3.416	3.314	3.286	3.053	2.871	2.604	2.402	2.197	2.085	1.946	1.973	32.683	2.724
1970	1.998	2.051	2.061	2.078	2.163	2.298	2.406	2.390	2.333	2.209	2.257	2.360	26.605	2.217
1971	2.537	2.642	2.722	2.595	2.755	2.852	2.884	2.748	2.575	2.478	2.492	2.536	31.817	2.651
1972	2.528	2.454	2.453	2.334	2.314	2.199	2.005	1.709	1.381	1.063	0.958	0.952	22.350	1.862
1973	1.199	1.534	1.965	2.278	2.591	2.811	3.010	3.068	3.021	3.172	3.267	3.342	31.258	2.605
1974	3.333	3.244	3.059	2.864	2.619	2.313	2.007	2.136	2.255	2.969	3.454	3.931	34.184	2.849
1975	4.094	4.126	4.084	4.039	4.002	3.743	3.375	2.936	2.830	2.969	3.205	3.355	42.738	3.562
1976	3.333	3.218	3.008	2.954	2.705	2.397	1.994	1.633	1.335	1.464	1.983	2.355	28.470	2.372
1977	2.737	2.740	2.732	2.734	2.681	2.521	2.318	1.980	1.683	1.427	1.231	1.102	25.885	2.157
1978	1.069	1.089	1.258	1.467	1.818	2.296	2.826	3.274	3.686	3.979	4.044	3.945	30.751	2.563
1979	3.705	3.485	3.229	3.090	2.967	3.102	3.090	3.095	2.873	2.606	2.504	2.404	36.148	3.012
1980	2.369	2.297	2.134	2.010	1.901	1.743	1.582	1.547	1.439	1.580	1.708	1.851	22.161	1.847
1981	1.961	2.008	1.941	1.879	1.957	2.251	2.709	3.036	3.154	3.177	3.150	3.105	30.329	2.527
1982	2.950	2.746	2.563	2.326	2.062	1.784	1.484	1.204	0.929	0.685	0.498	0.485	19.695	1.641
TOTAL	74.922	75.766	76.532	76.240	75.873	75.294	75.414	74.203	71.985	70.881	70.233	71.094	888.439	74.036
MEAN	2.497	2.526	2.551	2.541	2.529	2.510	2.514	2.473	2.399	2.363	2.341	2.370	29.615	2.468
S.D.	0.763	0.677	0.573	0.501	0.434	0.402	0.484	0.614	0.774	0.861	0.889	0.891	4.933	0.411
CE	0.305	0.268	0.225	0.197	0.172	0.160	0.193	0.248	0.323	0.364	0.380	0.376	0.167	0.167



Table-5.12 G (3) Computer Output of Long-term Base Flow Simulation

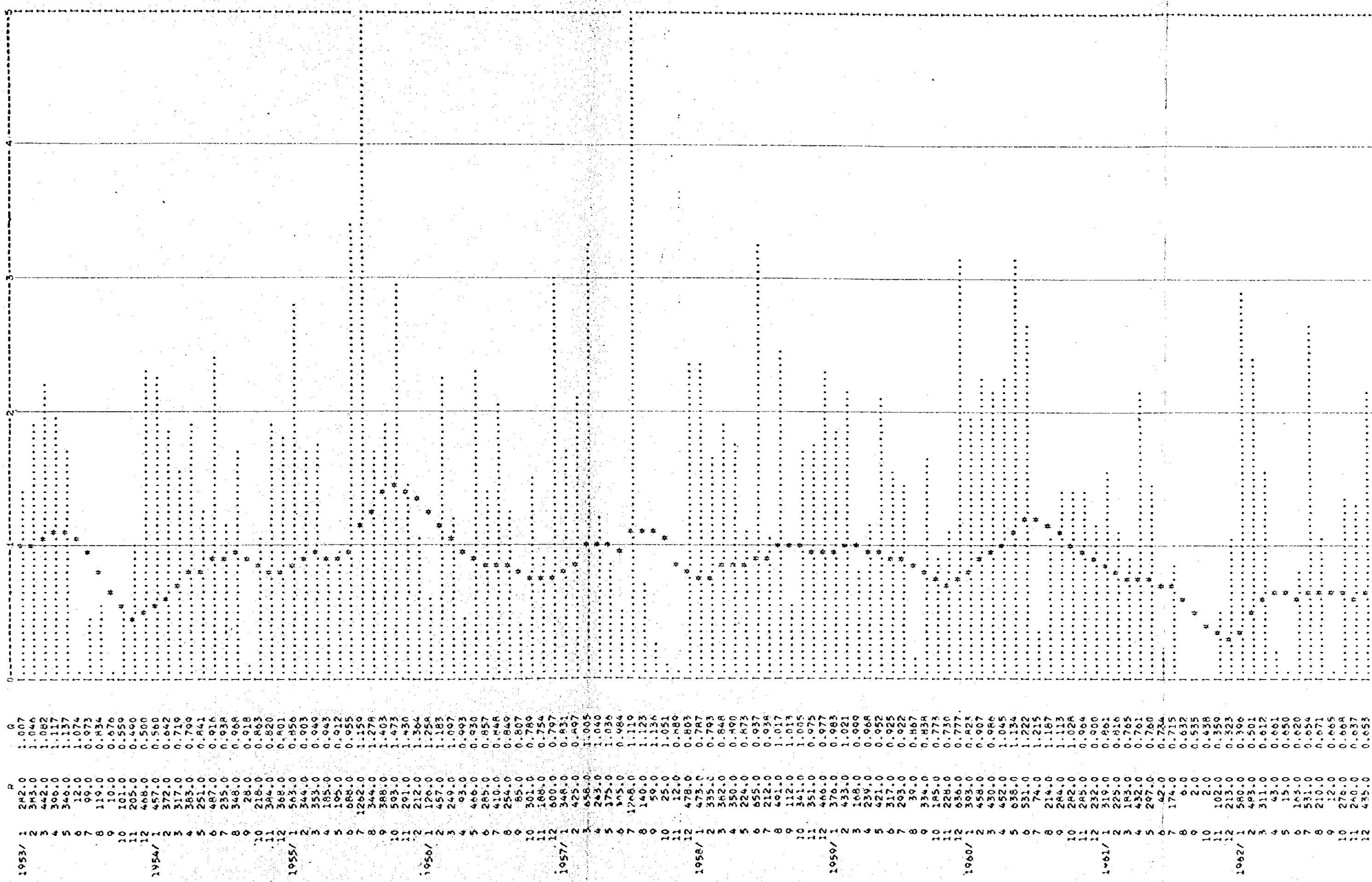
*****K.G.LIOIK (ST. PHUNOJLWO DAM) 1953-1982 长期基流模拟结果*****												
RUNOFF ( $10^3 m^3/day$ )												MEAN
1	2	3	4	5	6	7	8	9	10	11	12	TOTAL
1953	255.7	258.4	254.0	252.6	239.7	219.2	196.9	169.5	150.9	142.0	144.0	2541.3
1954	157.1	170.4	181.8	184.1	194.3	201.4	208.7	203.3	192.1	188.0	198.0	2252.5
1955	211.4	221.1	206.9	194.5	207.4	244.3	278.1	304.4	313.7	307.0	301.3	3010.9
1956	286.6	274.5	255.3	206.0	185.3	184.0	190.2	190.7	192.0	190.7	200.3	2586.3
1957	205.9	214.7	233.0	242.3	234.9	280.6	299.7	323.3	308.4	274.1	251.0	3109.8
1958	233.7	223.9	223.0	205.0	210.2	216.0	239.6	245.5	249.1	240.6	237.5	2742.4
1959	237.3	245.5	246.5	246.5	242.7	249.2	239.7	231.5	214.2	204.3	198.3	2801.7
1960	205.2	210.5	227.7	230.7	245.5	245.9	250.4	236.6	223.7	207.9	194.1	2710.5
1961	193.7	195.4	199.0	190.1	174.6	167.9	151.2	136.4	118.8	102.9	96.2	1921.9
1962	214.4	216.4	234.0	163.5	176.9	203.1	217.9	222.3	220.2	205.1	203.7	2115.7
1963	214.3	210.2	243.5	234.0	222.5	198.1	171.2	146.5	130.9	123.0	132.0	2270.9
1964	144.5	160.5	183.0	235.2	248.6	253.0	242.7	237.9	250.6	263.8	269.2	2690.8
1965	270.8	259.4	250.5	225.3	212.3	191.1	165.3	141.6	123.4	122.0	124.1	2326.8
1966	137.7	154.2	176.3	213.9	220.2	215.4	206.5	191.8	201.5	220.2	243.3	2375.0
1967	259.9	272.4	268.1	236.5	209.7	188.0	163.8	143.5	126.1	112.9	119.8	2358.3
1968	131.1	148.2	168.7	219.9	240.7	295.6	324.1	354.6	355.7	338.3	318.7	3084.0
1969	305.4	295.3	246.4	263.8	248.1	224.9	207.6	189.6	180.1	168.1	170.5	2823.8
1970	172.6	177.2	178.1	186.9	198.5	207.9	206.5	201.6	190.8	195.0	203.9	2298.7
1971	219.2	228.3	235.2	238.1	246.4	249.2	257.4	222.5	214.1	215.3	219.1	2748.9
1972	218.4	212.0	211.9	199.9	190.0	173.2	147.7	119.4	91.9	82.8	82.3	1931.0
1973	103.6	132.5	169.7	223.8	242.9	260.1	265.1	261.0	274.1	282.3	288.8	2700.7
1974	287.9	280.2	244.3	226.3	199.9	173.4	184.5	194.8	256.5	298.5	339.6	2953.5
1975	353.7	356.5	351.1	345.8	323.4	291.6	253.7	244.5	256.5	276.9	289.8	3692.6
1976	288.0	278.1	267.7	233.7	207.1	172.3	141.1	115.3	126.5	171.3	203.5	2459.8
1977	236.5	236.7	236.0	231.7	217.8	200.3	171.1	145.4	123.3	106.3	95.2	2236.5
1978	92.4	94.1	108.7	157.1	198.4	244.1	282.9	318.5	243.8	349.4	340.9	2656.9
1979	320.1	301.1	279.0	256.3	268.0	266.9	267.4	248.2	225.1	216.3	207.7	3123.2
1980	204.7	198.5	144.3	164.2	150.6	136.7	133.7	124.3	136.5	147.6	159.9	1914.7
1981	169.5	173.5	167.7	169.1	194.5	254.1	262.3	272.5	274.5	272.2	268.3	2620.4
1982	254.9	237.3	219.7	173.1	154.2	128.2	104.0	80.2	59.2	43.1	41.9	1701.7
TOTAL	6473.5	6546.2	6612.4	6555.4	6505.4	6515.8	6411.2	6219.5	6124.1	6068.1	6142.5	76761.2
MEAN	215.0	218.2	220.4	218.5	216.8	217.2	213.7	207.5	204.1	202.3	204.8	2558.7
S.D.	65.9	58.5	49.5	43.3	37.5	34.7	53.0	56.9	74.4	76.8	77.0	426.2
CF	0.305	0.268	0.225	0.197	0.172	0.160	0.193	0.323	0.364	0.380	0.376	0.167

6396.9

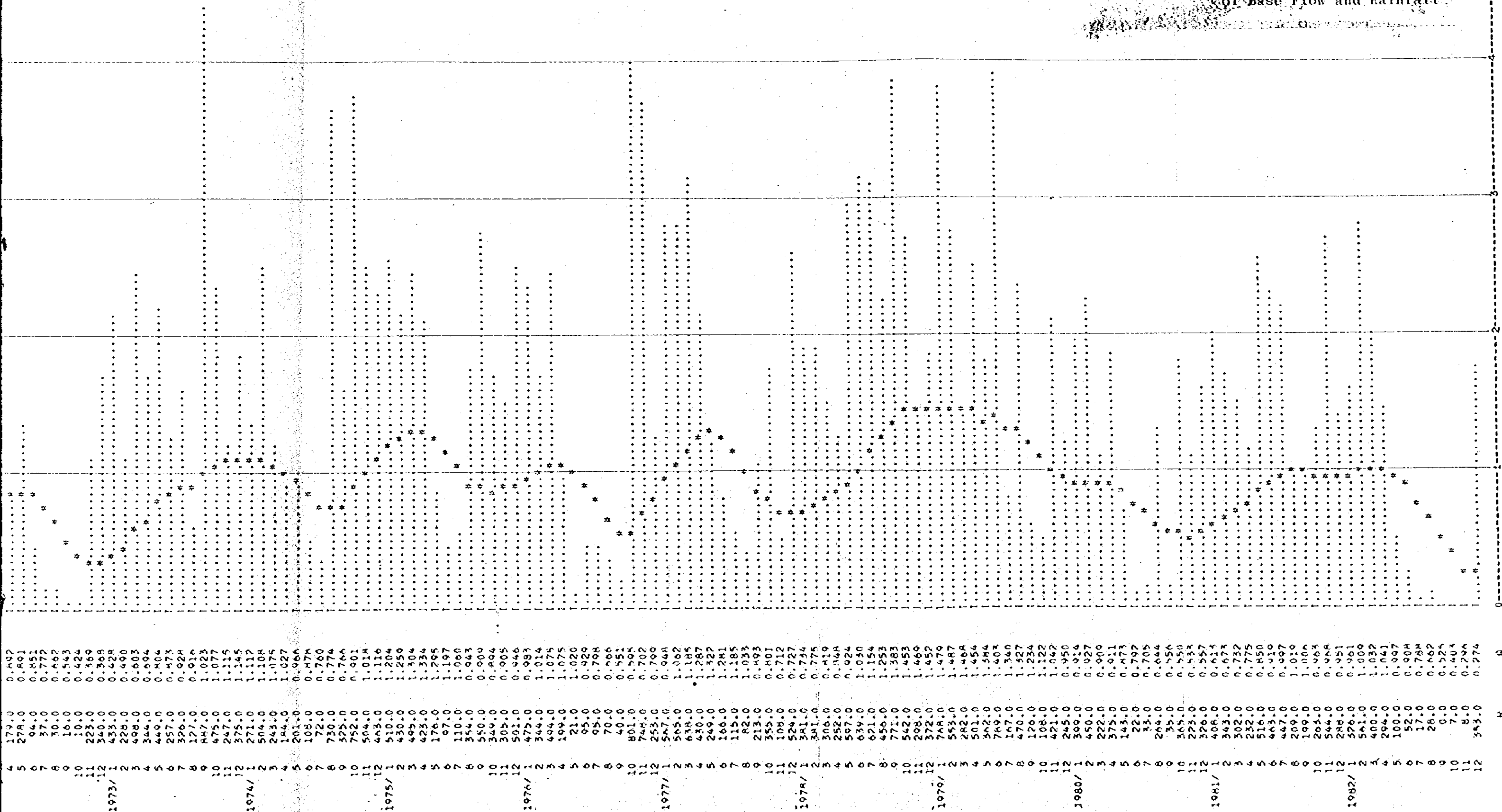
213.2

35.5

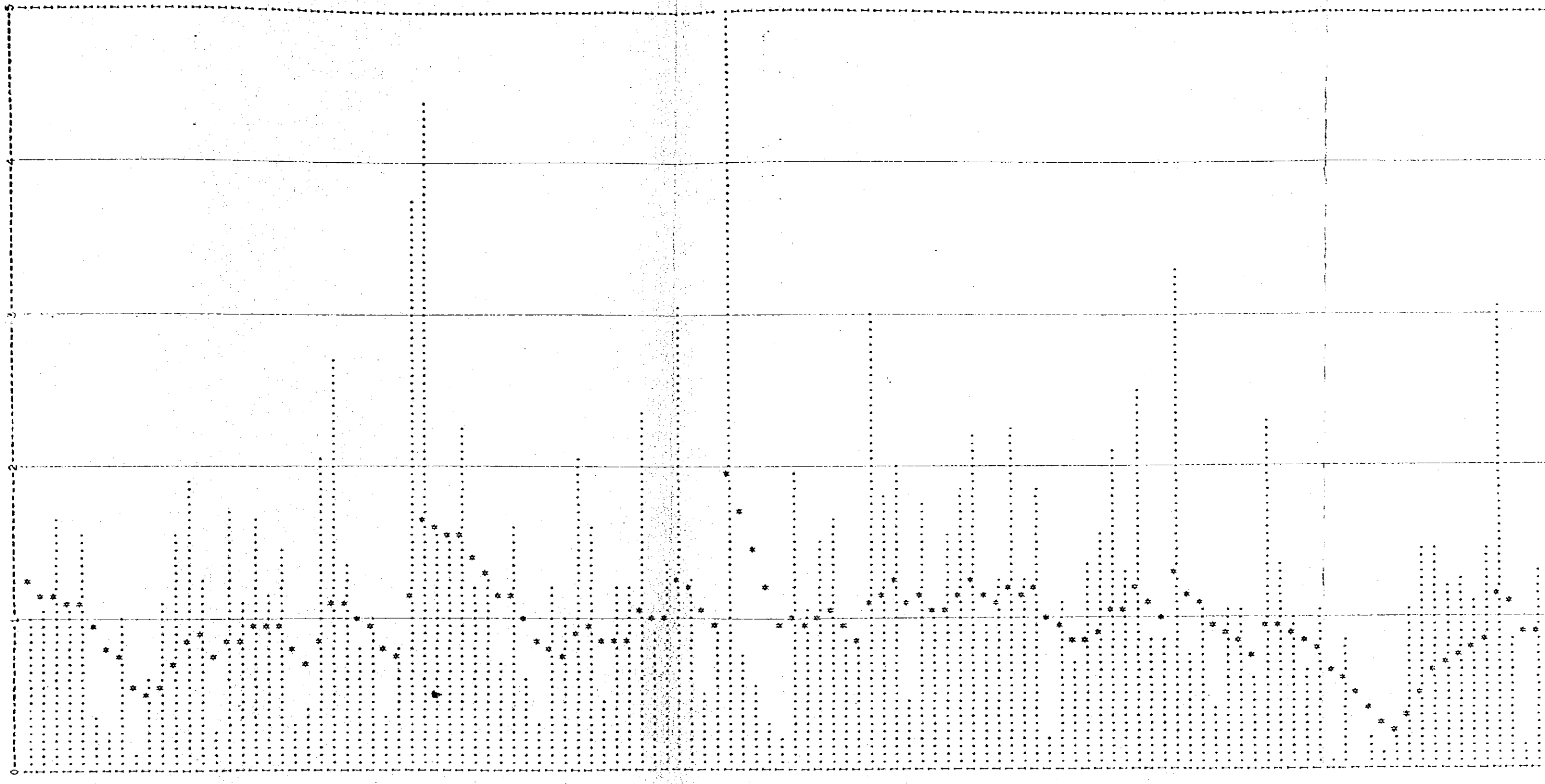
0.167



Year	1	2	3	4	5	6	7	8	9	10	11	12
1963/	0.501	0.612	0.650	0.620	0.654	0.671	0.665	0.668	0.637	0.653	0.736	0.800
1964/	0.829	1.001	0.973	0.911	0.797	0.666	0.541	0.423	0.340	0.325	0.331	0.393
1965/	0.497	0.577	0.662	0.694	0.679	0.667	0.650	0.724	0.702	0.824	0.804	0.877
1966/	0.572	0.455	0.793	0.710	0.590	0.495	0.370	0.250	0.130	0.025	0.064	0.047
1967/	0.763	0.841	0.924	0.917	0.866	0.816	0.782	0.766	0.847	0.905	1.107	1.158
1968/	0.997	1.170	1.102	0.996	0.776	0.569	0.467	0.436	0.514	0.584	0.576	0.777
1969/	0.970	1.167	1.255	1.413	1.450	1.468	1.454	1.470	1.480	1.520	1.491	1.589
1970/	0.682	0.752	0.827	0.955	1.001	1.034	1.010	1.001	0.954	0.942	0.951	1.003
1971/	0.664	0.682	0.752	0.827	0.955	1.001	1.034	1.010	1.001	0.954	0.942	0.951
1972/	0.664	0.682	0.752	0.827	0.955	1.001	1.034	1.010	1.001	0.954	0.942	0.951
1973/	0.664	0.682	0.752	0.827	0.955	1.001	1.034	1.010	1.001	0.954	0.942	0.951

Fig. 5.18(1) Monthly Distribution  
of Base Flow and Rainfall

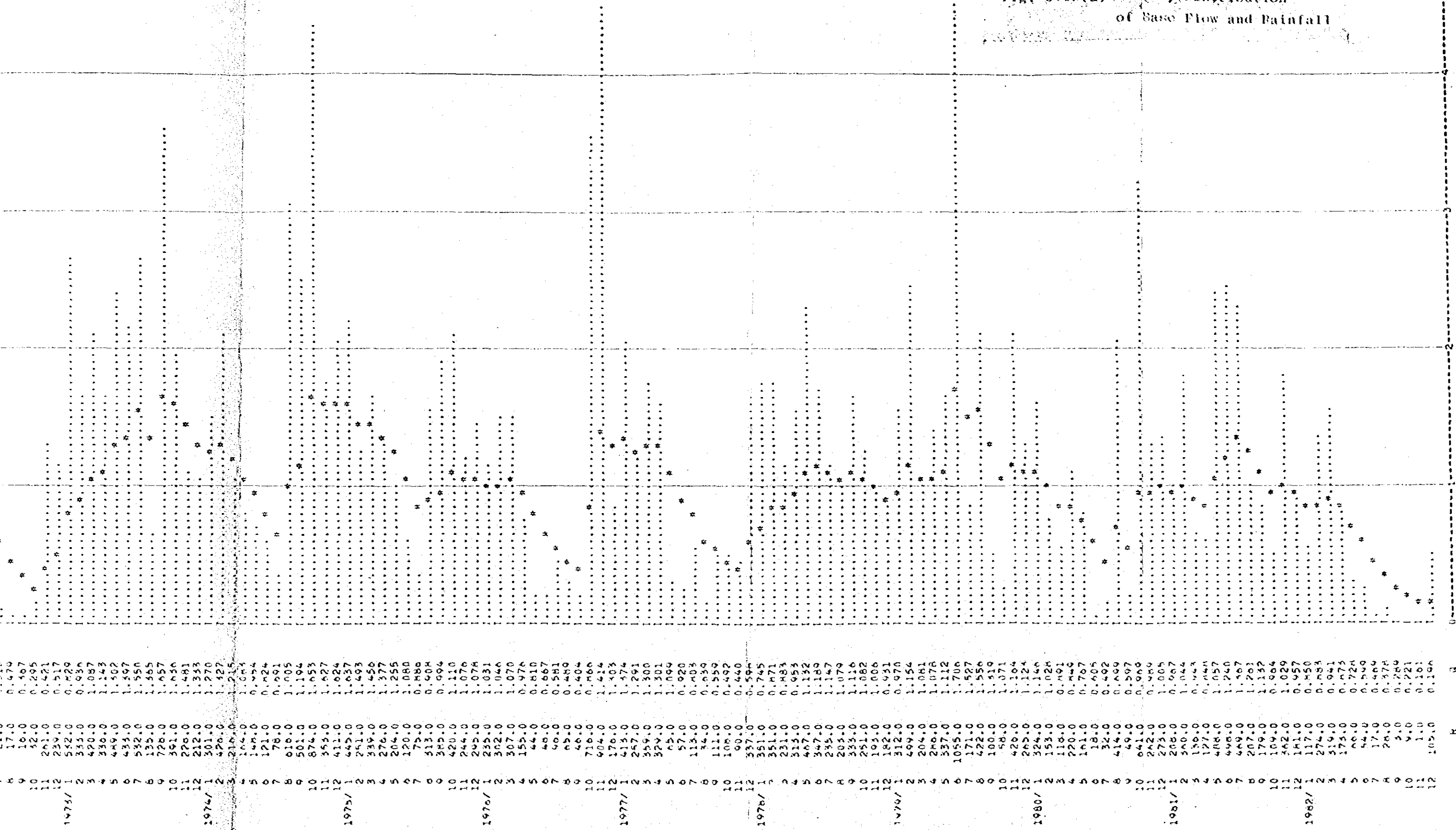
1953/ 1 205.0 1.251  
2 219.0 1.158  
3 331.0 1.170  
4 227.0 1.119  
5 310.0 1.141  
6 79.0 0.974  
7 57.0 0.401  
8 207.0 0.766  
9 20.0 0.596  
10 129.0 0.547  
11 226.0 0.595  
12 317.0 0.715  
1954/ 1 349.0 0.876  
2 250.0 0.698  
3 58.0 0.761  
4 346.0 0.905  
5 227.0 0.865  
6 335.0 0.957  
7 237.0 0.959  
8 200.0 0.996  
9 67.0 0.447  
10 40.0 0.721  
11 417.0 0.480  
12 540.0 1.118  
1955/ 1 279.0 1.124  
2 149.0 1.040  
3 207.0 0.980  
4 72.0 0.817  
5 160.0 0.756  
6 750.0 1.174  
7 888.0 1.657  
8 318.0 1.615  
9 318.0 1.554  
10 453.0 1.576  
11 243.0 1.425  
12 269.0 1.335  
1956/ 1 148.0 1.178  
2 320.0 1.182  
3 126.0 1.035  
4 64.0 0.853  
5 243.0 0.831  
6 208.0 0.786  
7 416.0 0.934  
8 321.0 0.904  
9 93.0 0.862  
10 242.0 0.864  
11 244.0 0.866  
12 472.0 1.054  
1957/ 1 149.0 0.990  
2 274.0 1.014  
3 610.0 1.293  
4 251.0 1.235  
5 103.0 1.060  
6 187.0 0.970  
7 1537.0 1.966  
8 155.0 1.741  
9 111.0 1.497  
10 61.0 1.220  
11 42.0 0.961  
12 399.0 1.045  
1958/ 1 216.0 0.991  
2 301.0 1.024  
3 337.0 1.075  
4 178.0 0.985  
5 168.0 0.890  
6 603.0 1.140  
7 362.0 1.188  
8 401.0 1.240  
9 90.0 1.111  
10 351.0 1.150  
11 204.0 1.066  
12 313.0 1.080  
1959/ 1 377.0 1.155  
2 444.0 1.267  
3 104.0 1.167  
4 251.0 1.116  
5 457.0 1.227  
6 254.0 1.166  
7 379.0 1.221  
8 41.0 1.006  
9 224.0 0.961  
10 141.0 0.858  
11 278.0 0.881  
12 310.0 0.935  
1960/ 1 421.0 1.067  
2 261.0 1.059  
3 508.0 1.237  
4 179.0 1.125  
5 172.0 1.020  
6 664.0 1.323  
7 155.0 1.186  
8 220.0 1.123  
9 83.0 0.953  
10 216.0 0.905  
11 219.0 0.874  
12 121.0 0.774  
1961/ 1 464.0 0.967  
2 274.0 0.986  
3 201.0 0.940  
4 136.0 0.848  
5 215.0 0.821  
6 13.0 0.651  
7 176.0 0.843  
8 5.0 0.511  
9 44.0 0.427  
10 21.0 0.341  
11 50.0 0.297  
12 216.0 0.366  
1962/ 1 264.0 0.661  
2 241.0 0.725  
3 251.0 0.770  
4 229.0 0.604  
5 202.0 0.474  
6 610.0 1.184  
7 176.0 1.106  
8 35.0 0.224  
9 244.0 0.933



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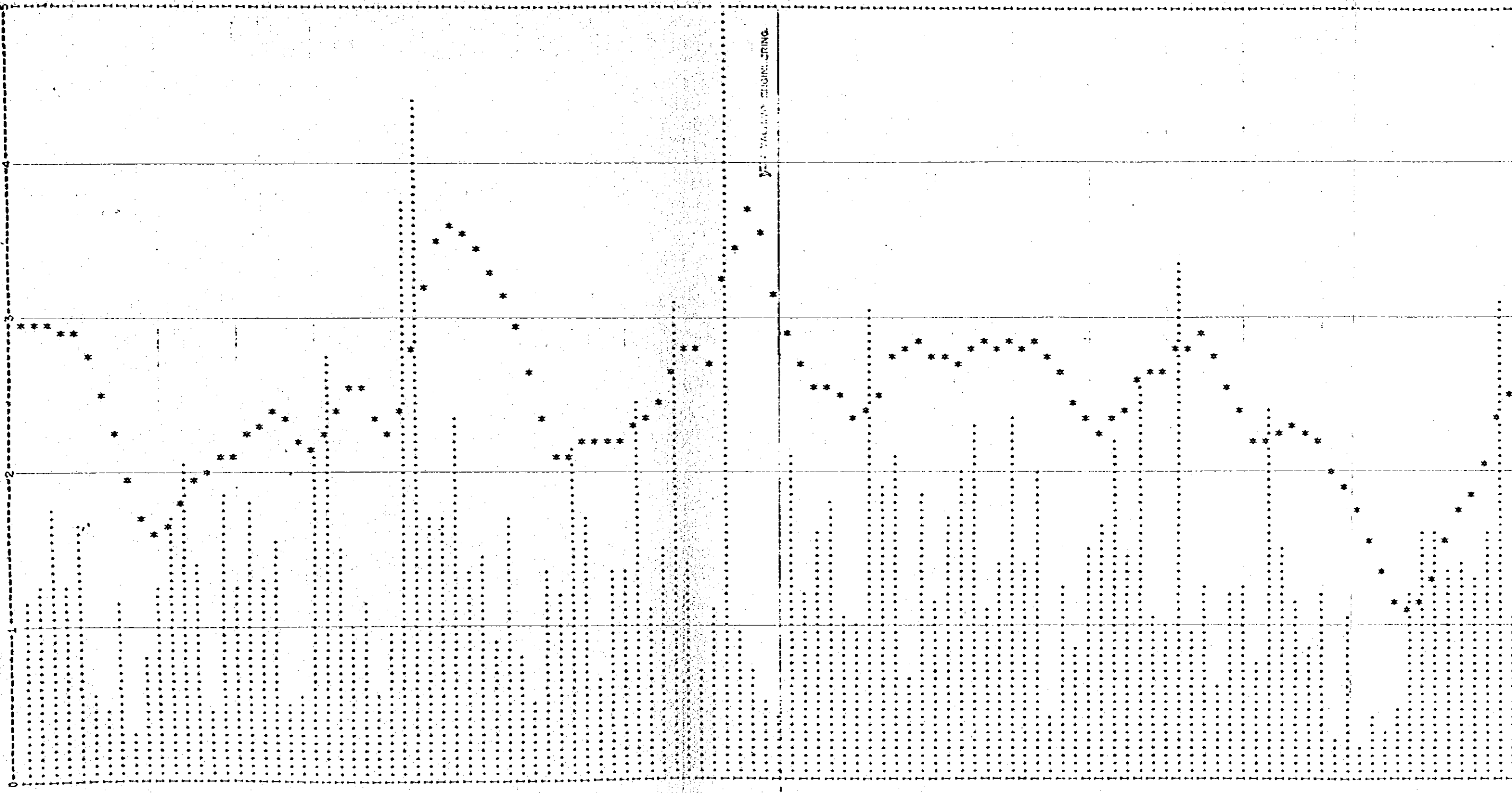
Fig. 5.18(2) Monthly Distr  
of Base Flow

Fig. -5.18(2) Monthly Distribution  
of Base Flow and Rainfall





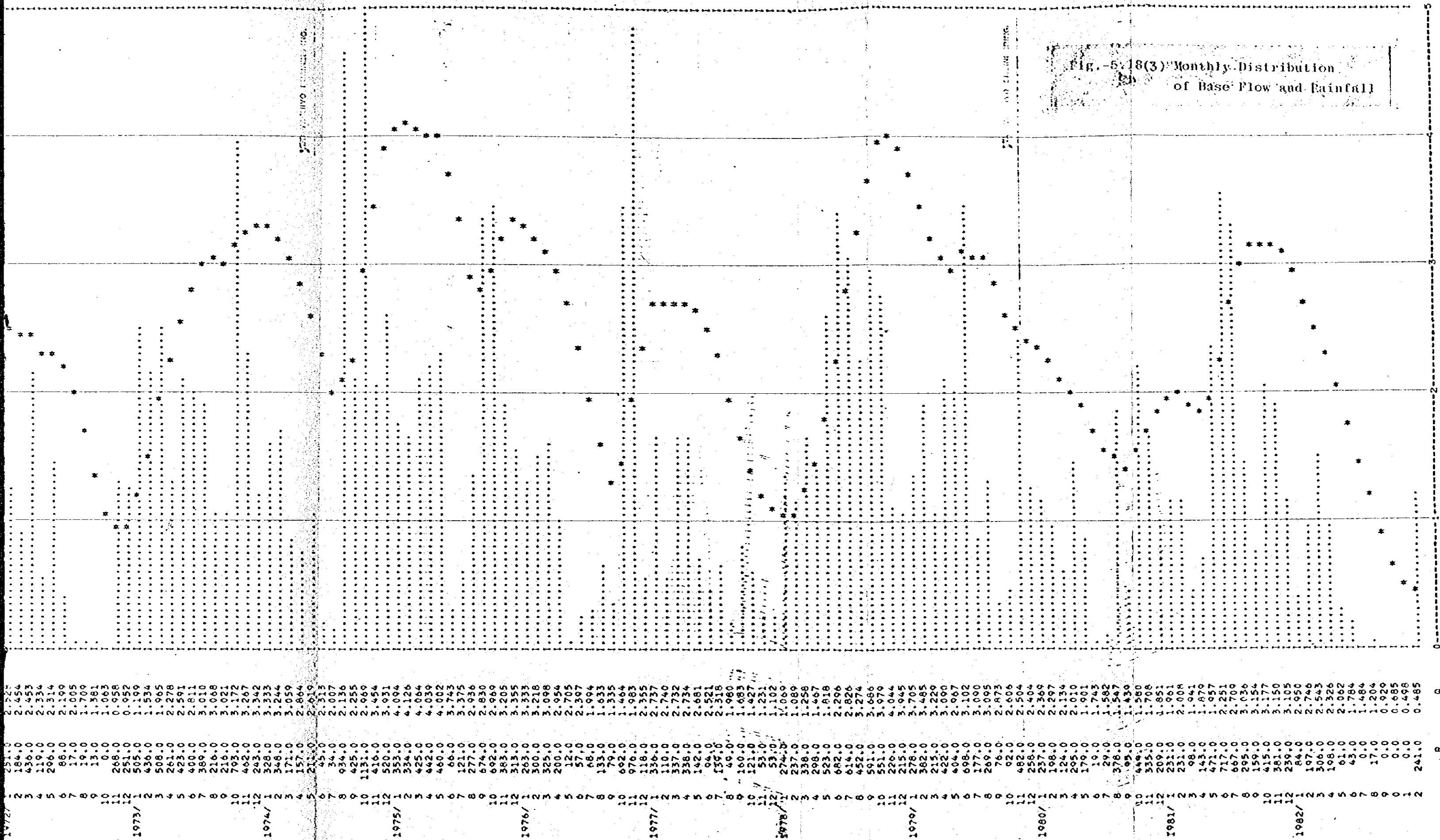
1953/ 1 237.0  
2 250.0  
3 357.0  
4 258.0  
5 357.0  
6 117.0  
7 197.0  
8 239.0  
9 67.0  
10 165.0  
11 257.0  
12 343.0  
1954/ 1 412.0  
2 280.0  
3 88.0  
4 371.0  
5 258.0  
6 267.0  
7 318.0  
8 118.0  
9 555.0  
10 307.0  
11 203.0  
12 111.0  
1955/ 1 194.0  
2 754.0  
3 886.0  
4 344.0  
5 473.0  
6 273.0  
7 183.0  
8 346.0  
9 164.0  
10 273.0  
11 298.0  
12 183.0  
1956/ 1 183.0  
2 346.0  
3 164.0  
4 273.0  
5 273.0  
6 439.0  
7 347.0  
8 131.0  
9 272.0  
10 274.0  
11 491.0  
12 222.0  
1957/ 1 222.0  
2 303.0  
3 281.0  
4 140.0  
5 220.0  
6 1502.0  
7 190.0  
8 148.0  
9 100.0  
10 82.0  
11 421.0  
12 328.0  
1958/ 1 328.0  
2 362.0  
3 211.0  
4 202.0  
5 615.0  
6 386.0  
7 423.0  
8 134.0  
9 376.0  
10 336.0  
11 340.0  
12 400.0  
1959/ 1 400.0  
2 404.0  
3 227.0  
4 281.0  
5 284.0  
6 402.0  
7 81.0  
8 255.0  
9 176.0  
10 337.0  
11 442.0  
12 200.0  
1960/ 1 200.0  
2 325.0  
3 212.0  
4 206.0  
5 673.0  
6 251.0  
7 121.0  
8 248.0  
9 250.0  
10 157.0  
11 483.0  
12 307.0  
1961/ 1 173.0  
2 226.0  
3 230.0  
4 173.0  
5 247.0  
6 55.0  
7 210.0  
8 47.0  
9 64.0  
10 92.0  
11 348.0  
12 325.0  
1962/ 1 325.0  
2 271.0  
3 281.0  
4 260.0  
5 320.0  
6 210.0



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Fig. -5-18(3) Monthly Distribution  
of Base Flow and Rainfall





APPENDIX

Observed Rainfall  
& Discharge Data



Table - Observed Rainfall and Discharge Data at Mujur Bridge Station

Month/Year : Feb./'83  
 Catchment Area : 125.70 Km<sup>2</sup>

Rainfall (mm)										Discharge		Remarks
002400	000000	000000	000000	000000	000000	000000	000000	000000	000000	R	Qp Observed (m <sup>3</sup> /s)	
1	0.07	0.05	0.01	0.04	0.06	0.04	0.02	0.01	0.01	0.01	0.01	
2	0.07	0.05	0.01	0.04	0.06	0.04	0.02	0.01	0.01	0.01	0.01	
3	0.07	0.05	0.01	0.04	0.06	0.04	0.02	0.01	0.01	0.01	0.01	
4	0.07	0.05	0.01	0.04	0.06	0.04	0.02	0.01	0.01	0.01	0.01	
5	0.07	0.05	0.01	0.04	0.06	0.04	0.02	0.01	0.01	0.01	0.01	
6	0.07	0.05	0.01	0.04	0.06	0.04	0.02	0.01	0.01	0.01	0.01	
7	0.07	0.05	0.01	0.04	0.06	0.04	0.02	0.01	0.01	0.01	0.01	
8	0.07	0.05	0.01	0.04	0.06	0.04	0.02	0.01	0.01	0.01	0.01	
9	0.07	0.05	0.01	0.04	0.06	0.04	0.02	0.01	0.01	0.01	0.01	
10	0.07	0.05	0.01	0.04	0.06	0.04	0.02	0.01	0.01	0.01	0.01	
11	0.07	0.05	0.01	0.04	0.06	0.04	0.02	0.01	0.01	0.01	0.01	
12	0.07	0.05	0.01	0.04	0.06	0.04	0.02	0.01	0.01	0.01	0.01	
13	0.07	0.05	0.01	0.04	0.06	0.04	0.02	0.01	0.01	0.01	0.01	
14	0.07	0.05	0.01	0.04	0.06	0.04	0.02	0.01	0.01	0.01	0.01	
15	0.07	0.05	0.01	0.04	0.06	0.04	0.02	0.01	0.01	0.01	0.01	
16	0.07	0.05	0.01	0.04	0.06	0.04	0.02	0.01	0.01	0.01	0.01	
17	0.07	0.05	0.01	0.04	0.06	0.04	0.02	0.01	0.01	0.01	0.01	
18	0.07	0.05	0.01	0.04	0.06	0.04	0.02	0.01	0.01	0.01	0.01	
19	0.07	0.05	0.01	0.04	0.06	0.04	0.02	0.01	0.01	0.01	0.01	
20	0.07	0.05	0.01	0.04	0.06	0.04	0.02	0.01	0.01	0.01	0.01	
21	0.07	0.05	0.01	0.04	0.06	0.04	0.02	0.01	0.01	0.01	0.01	
22	0.07	0.05	0.01	0.04	0.06	0.04	0.02	0.01	0.01	0.01	0.01	
23	0.07	0.05	0.01	0.04	0.06	0.04	0.02	0.01	0.01	0.01	0.01	
24	0.07	0.05	0.01	0.04	0.06	0.04	0.02	0.01	0.01	0.01	0.01	
25	0.07	0.05	0.01	0.04	0.06	0.04	0.02	0.01	0.01	0.01	0.01	
26	0.07	0.05	0.01	0.04	0.06	0.04	0.02	0.01	0.01	0.01	0.01	
27	0.07	0.05	0.01	0.04	0.06	0.04	0.02	0.01	0.01	0.01	0.01	
28	0.07	0.05	0.01	0.04	0.06	0.04	0.02	0.01	0.01	0.01	0.01	
29	0.07	0.05	0.01	0.04	0.06	0.04	0.02	0.01	0.01	0.01	0.01	
30	0.07	0.05	0.01	0.04	0.06	0.04	0.02	0.01	0.01	0.01	0.01	
31	0.07	0.05	0.01	0.04	0.06	0.04	0.02	0.01	0.01	0.01	0.01	

- Notes : 1. Space @ expresses rainfall observation station name. 4. R means average depth of rainfall over area.  
 2. Space @ shows rainfall observation station number. 5. Qp means peak flood.  
 3. Space @ shows Thiessen Coefficient.

Table - Observed Rainfall and Discharge Data at Mujur Bridge Station

Month/Year : Mar./'83  
 Catchment Area : 125.77 km<sup>2</sup>

Rainfall (mm)										Discharge		Remarks					
RAZDO	KWOTZK	REDDOF	4-SAMUR	SUSWEND	MUNZGAIK	TEMPER	4-LAKKER	4-PAK-S	WZORONZAK	KUSTOVAKA	D. P. AT		GAND-PAKS	KAZDANZ	R	Qp	Observed Time
3	5	7	10	12	20	24	30	31	33	36	37	39	41	0.1	3.0	13:00 ~ 17:00	
1	1	1	1	1	1	10	1	0.30	0.5	0.3	2.1	0.03	0.07	0.1	11.1	3.0	
5	37	5	3	36	22	2	2	17.1	38.1	8.1	38.1	6.1	30.1	30.1	3.0	4	
4	7	1	1	29	1	1	1	3.1	3.1	1	6.1	1	1	1.1	4.1	7	
5	1	1	1	1	1	1	1	16.1	16.1	1	11.3	0.1	1	7.1	3.1	4	
6	1	1	1	6	13	1	1	13.1	13.1	4.1	15.1	24.1	7.1	11.1	4.1	4	
7	33	1	1	19	1	1	1	7.1	7.1	0.1	7.1	10.1	10.1	7.1	3.0	4	
8	22	1	1	10	1	7	7	7.1	7.1	3.1	30.1	9.1	12.1	13.1	3.0	4	
9	47	5	23	20	24	4	4	16.1	15.1	15.1	26.1	38.1	23.1	38.1	12.1	4	
10	3	1	1	1	1	1	1	4.1	4.1	2.1	1.1	5.1	1.1	2.1	9.1	14:30 ~ 17:35	
11	16	1	1	3	16	1	1	7.1	7.1	1	33.1	1	1	9.1	3.0	14:30 ~ 17:35	
12	1	17	1	1	1	1	1	0.1	0.1	3.1	2.1	3.1	1	2.1	4.0	14:30 ~ 17:35	
13	25	17	31	41	14	10	10	40.1	40.1	9.1	27.1	9.1	2.1	26.1	22.1	4	
14	5	5	1	67	1	2	2	11.1	11.1	3.1	8.1	6.1	0.1	9.1	7.1	4	
15	2	5	15	9	34	22	22	26.1	26.1	5.1	12.1	1.1	1	15.1	7.1	4	
16	32	3	3	3	1	1	1	2.1	2.1	5.1	16.1	42.1	1.1	9.1	13.1	9:15 ~ 17:00	
17	9	1	1	19	10	1	1	7.1	7.1	1	20.1	0.1	1	7.1	4.1	13:00 ~ 17:00	
18	11	12	4	2	1	1	1	14.1	14.1	1	5.1	1	14.1	7.1	4.1	4	
19	12	1	1	1	2	2	2	8.1	8.1	1	5.1	1	2.1	2.1	7.1	4	
20	1	4	1	1	1	3	3	0.1	0.1	0.1	0.1	4.1	31.1	15.1	4.1	4	
21	8	1	1	42	1	1	1	1.1	1.1	1.1	30.1	5.1	9.1	10.1	7.1	4	
22	13	37	17	7	35	2	2	13.1	13.1	1	13.1	4.1	9.1	13.1	9.1	4	
23	1	1	1	4	9	2	2	13.1	13.1	13.1	2.1	1.1	11.1	2.1	19.1	4	
24	1	1	1	1	1	1	1	1	1	1	1	1	1	1	4.1	4	
25	25	1	1	2	2	1	1	6.1	6.1	6.1	5.1	1.1	1	7.1	3.1	4	
26	1	1	3	1	1	1	1	1.1	1.1	1.1	0.1	1.1	1.1	1.1	2.1	4	
27	1	1	1	1	1	1	1	1	1	1	1	1	27.1	13.1	2.1	4	
28	1	39	19	6	9	7	7	51.1	0.1	18.1	0.1	18.1	1.1	9.1	1.1	4	
29	1	1	1	1	1	1	1	0.1	0.1	0.1	1	3.1	1	0.1	2.1	13:00 ~ 17:00	
30	1	35	20	1	1	4	4	13.1	13.1	13.1	3.1	1	2.1	2.1	2.1	13:00 ~ 17:00	
31	2	1	1	9	1	1	1	0.1	0.1	0.1	1.1	1	1.1	5.1	3.1	4	
32	320	176	149	334	192	192	192	(279)	152	45.1	185.1	176.1	316	316	316	4	

Notes : 1. Space @ expresses rainfall observation station name. 4. R means average depth of rainfall over area.  
 2. Space @ shows rainfall observation station number. 5. Qp means peak flood.  
 3. Space @ shows Thiessen Coefficient.



Table - Observed Rainfall and Discharge Data at Mujur Bridge Station

Month/Year : Apr. / '83  
 Catchment Area : 125.00 Km<sup>2</sup>

Rainfall (mm)										Discharge		Remarks
DATE	TIME	30-40	40-50	50-60	60-70	70-80	80-90	90-100	100-110	R	Qp	Observed Time
1	1	1	1	1	1	1	1	1	1	1	1	13:00 ~ 17:00
2	1	1	1	1	1	1	1	1	1	1	1	1
3	1	1	1	1	1	1	1	1	1	1	1	1
4	1	1	1	1	1	1	1	1	1	1	1	1
5	1	1	1	1	1	1	1	1	1	1	1	1
6	1	1	1	1	1	1	1	1	1	1	1	1
7	1	1	1	1	1	1	1	1	1	1	1	1
8	1	1	1	1	1	1	1	1	1	1	1	1
9	1	1	1	1	1	1	1	1	1	1	1	1
10	1	1	1	1	1	1	1	1	1	1	1	1
11	1	1	1	1	1	1	1	1	1	1	1	1
12	1	1	1	1	1	1	1	1	1	1	1	1
13	1	1	1	1	1	1	1	1	1	1	1	1
14	1	1	1	1	1	1	1	1	1	1	1	1
15	1	1	1	1	1	1	1	1	1	1	1	1
16	1	1	1	1	1	1	1	1	1	1	1	1
17	1	1	1	1	1	1	1	1	1	1	1	1
18	1	1	1	1	1	1	1	1	1	1	1	1
19	1	1	1	1	1	1	1	1	1	1	1	1
20	1	1	1	1	1	1	1	1	1	1	1	1
21	1	1	1	1	1	1	1	1	1	1	1	1
22	1	1	1	1	1	1	1	1	1	1	1	1
23	1	1	1	1	1	1	1	1	1	1	1	1
24	1	1	1	1	1	1	1	1	1	1	1	1
25	1	1	1	1	1	1	1	1	1	1	1	1
26	1	1	1	1	1	1	1	1	1	1	1	1
27	1	1	1	1	1	1	1	1	1	1	1	1
28	1	1	1	1	1	1	1	1	1	1	1	1
29	1	1	1	1	1	1	1	1	1	1	1	1
30	1	1	1	1	1	1	1	1	1	1	1	1
31	1	1	1	1	1	1	1	1	1	1	1	1
32	1	1	1	1	1	1	1	1	1	1	1	1
33	1	1	1	1	1	1	1	1	1	1	1	1
34	1	1	1	1	1	1	1	1	1	1	1	1
35	1	1	1	1	1	1	1	1	1	1	1	1
36	1	1	1	1	1	1	1	1	1	1	1	1
37	1	1	1	1	1	1	1	1	1	1	1	1
38	1	1	1	1	1	1	1	1	1	1	1	1
39	1	1	1	1	1	1	1	1	1	1	1	1
40	1	1	1	1	1	1	1	1	1	1	1	1
41	1	1	1	1	1	1	1	1	1	1	1	1
42	1	1	1	1	1	1	1	1	1	1	1	1
43	1	1	1	1	1	1	1	1	1	1	1	1
44	1	1	1	1	1	1	1	1	1	1	1	1
45	1	1	1	1	1	1	1	1	1	1	1	1
46	1	1	1	1	1	1	1	1	1	1	1	1
47	1	1	1	1	1	1	1	1	1	1	1	1
48	1	1	1	1	1	1	1	1	1	1	1	1
49	1	1	1	1	1	1	1	1	1	1	1	1
50	1	1	1	1	1	1	1	1	1	1	1	1
51	1	1	1	1	1	1	1	1	1	1	1	1
52	1	1	1	1	1	1	1	1	1	1	1	1
53	1	1	1	1	1	1	1	1	1	1	1	1
54	1	1	1	1	1	1	1	1	1	1	1	1
55	1	1	1	1	1	1	1	1	1	1	1	1
56	1	1	1	1	1	1	1	1	1	1	1	1
57	1	1	1	1	1	1	1	1	1	1	1	1
58	1	1	1	1	1	1	1	1	1	1	1	1
59	1	1	1	1	1	1	1	1	1	1	1	1
60	1	1	1	1	1	1	1	1	1	1	1	1
61	1	1	1	1	1	1	1	1	1	1	1	1
62	1	1	1	1	1	1	1	1	1	1	1	1
63	1	1	1	1	1	1	1	1	1	1	1	1
64	1	1	1	1	1	1	1	1	1	1	1	1
65	1	1	1	1	1	1	1	1	1	1	1	1
66	1	1	1	1	1	1	1	1	1	1	1	1
67	1	1	1	1	1	1	1	1	1	1	1	1
68	1	1	1	1	1	1	1	1	1	1	1	1
69	1	1	1	1	1	1	1	1	1	1	1	1
70	1	1	1	1	1	1	1	1	1	1	1	1
71	1	1	1	1	1	1	1	1	1	1	1	1
72	1	1	1	1	1	1	1	1	1	1	1	1
73	1	1	1	1	1	1	1	1	1	1	1	1
74	1	1	1	1	1	1	1	1	1	1	1	1
75	1	1	1	1	1	1	1	1	1	1	1	1
76	1	1	1	1	1	1	1	1	1	1	1	1
77	1	1	1	1	1	1	1	1	1	1	1	1
78	1	1	1	1	1	1	1	1	1	1	1	1
79	1	1	1	1	1	1	1	1	1	1	1	1
80	1	1	1	1	1	1	1	1	1	1	1	1
81	1	1	1	1	1	1	1	1	1	1	1	1
82	1	1	1	1	1	1	1	1	1	1	1	1
83	1	1	1	1	1	1	1	1	1	1	1	1
84	1	1	1	1	1	1	1	1	1	1	1	1
85	1	1	1	1	1	1	1	1	1	1	1	1
86	1	1	1	1	1	1	1	1	1	1	1	1
87	1	1	1	1	1	1	1	1	1	1	1	1
88	1	1	1	1	1	1	1	1	1	1	1	1
89	1	1	1	1	1	1	1	1	1	1	1	1
90	1	1	1	1	1	1	1	1	1	1	1	1
91	1	1	1	1	1	1	1	1	1	1	1	1
92	1	1	1	1	1	1	1	1	1	1	1	1
93	1	1	1	1	1	1	1	1	1	1	1	1
94	1	1	1	1	1	1	1	1	1	1	1	1
95	1	1	1	1	1	1	1	1	1	1	1	1
96	1	1	1	1	1	1	1	1	1	1	1	1
97	1	1	1	1	1	1	1	1	1	1	1	1
98	1	1	1	1	1	1	1	1	1	1	1	1
99	1	1	1	1	1	1	1	1	1	1	1	1
100	1	1	1	1	1	1	1	1	1	1	1	1

Notes : 1. Space @ expresses rainfall observation station name. 4. R means average depth of rainfall over area.  
 2. Space @ shows rainfall observation station number. 5. Qp means peak flood.  
 3. Space @ shows Thiessen Coefficient.

Table - Observed Rainfall and Discharge Data at Mujur Bridge Station

Month/Year : May / '83  
 Catchment Area : 125.70 km<sup>2</sup>

Rainfall (mm)										Discharge		Remarks
Station	1	2	3	4	5	6	7	8	9	R	Qp	
1	18	40	44	50	32	33	33	31	31	31	31	13:00 ~ 18:00
2	18	40	44	50	32	33	33	31	31	31	31	13:00 ~ 18:00
3	22	24	20	43	38	30	30	30	30	30	30	13:00 ~ 18:00
4	5	23	25	3	13	14	14	14	14	14	14	13:00 ~ 18:00
5	4	2	11	-	-	4	4	4	4	4	4	13:00 ~ 18:00
6	12	4	-	25	7	28	28	28	28	28	28	13:00 ~ 18:00
7	18	24	17	14	6	21	21	21	21	21	21	13:00 ~ 18:00
8	-	-	1	-	-	1	1	1	1	1	1	13:00 ~ 18:00
9	-	-	-	13	-	1	1	1	1	1	1	13:00 ~ 18:00
10	-	-	-	-	-	-	-	-	-	-	-	13:00 ~ 18:00
11	5	2	6	2	-	5	5	5	5	5	5	13:00 ~ 18:00
12	23	3	15	15	-	10	10	10	10	10	10	13:00 ~ 18:00
13	77	3	-	49	-	2	2	2	2	2	2	13:00 ~ 18:00
14	-	-	-	-	-	-	-	-	-	-	-	13:00 ~ 18:00
15	17	10	-	14	-	2	2	2	2	2	2	13:00 ~ 18:00
16	-	31	-	53	13	17	17	17	17	17	17	13:00 ~ 18:00
17	11	34	30	5	28	12	12	12	12	12	12	13:00 ~ 18:00
18	32	-	1	23	19	9	9	9	9	9	9	13:00 ~ 18:00
19	25	3	5	20	-	1	1	1	1	1	1	13:00 ~ 18:00
20	9	6	-	29	-	2	2	2	2	2	2	13:00 ~ 18:00
21	-	-	-	-	-	-	-	-	-	-	-	13:00 ~ 18:00
22	2	-	28	1	-	-	-	-	-	-	-	13:00 ~ 18:00
23	11	51	51	32	37	21	21	21	21	21	21	13:00 ~ 18:00
24	18	-	-	13	32	30	30	30	30	30	30	13:00 ~ 18:00
25	202	5	134	44	44	2	2	2	2	2	2	13:00 ~ 18:00
26	10	-	37	13	-	-	-	-	-	-	-	13:00 ~ 18:00
27	65	36	79	9	45	46	46	46	46	46	46	13:00 ~ 18:00
28	17	57	15	45	-	12	12	12	12	12	12	13:00 ~ 18:00
29	-	-	15	-	-	-	-	-	-	-	-	13:00 ~ 18:00
30	30	-	5	5	-	1	1	1	1	1	1	13:00 ~ 18:00
31	2	-	-	7	-	-	-	-	-	-	-	13:00 ~ 18:00
T.C	650	343	771	536	370	370	370	370	370	370	370	UNRECORDED

Notes : 1. Space @ expresses rainfall observation station name. 4. R means average depth of rainfall over area.  
 2. Space @ shows rainfall observation station number. 5. Qp means peak flood.  
 3. Space @ shows Thiessen Coefficient.

Table - Observed Rainfall and Discharge Data at Mujur Bridge Station

Month/Year : Jun. / 1983  
 Catchment Area : 125.70 km<sup>2</sup>

Date	Rainfall (mm)										Discharge		Remarks
	02mm	2K-26-2	00004	4-11-23K	5-12-20	7-24-20	9-24-20	11-24-20	13-24-20	15-24-20	R	Qp Observed (m <sup>3</sup> /s)	
1	007	008	008	008	008	008	008	008	008	008	008	008	
2	007	008	008	008	008	008	008	008	008	008	008	008	
3	007	008	008	008	008	008	008	008	008	008	008	008	
4	007	008	008	008	008	008	008	008	008	008	008	008	
5	007	008	008	008	008	008	008	008	008	008	008	008	
6	007	008	008	008	008	008	008	008	008	008	008	008	
7	007	008	008	008	008	008	008	008	008	008	008	008	
8	007	008	008	008	008	008	008	008	008	008	008	008	
9	007	008	008	008	008	008	008	008	008	008	008	008	
10	007	008	008	008	008	008	008	008	008	008	008	008	
11	007	008	008	008	008	008	008	008	008	008	008	008	
12	007	008	008	008	008	008	008	008	008	008	008	008	
13	007	008	008	008	008	008	008	008	008	008	008	008	
14	007	008	008	008	008	008	008	008	008	008	008	008	
15	007	008	008	008	008	008	008	008	008	008	008	008	
16	007	008	008	008	008	008	008	008	008	008	008	008	
17	007	008	008	008	008	008	008	008	008	008	008	008	
18	007	008	008	008	008	008	008	008	008	008	008	008	
19	007	008	008	008	008	008	008	008	008	008	008	008	
20	007	008	008	008	008	008	008	008	008	008	008	008	
21	007	008	008	008	008	008	008	008	008	008	008	008	
22	007	008	008	008	008	008	008	008	008	008	008	008	
23	007	008	008	008	008	008	008	008	008	008	008	008	
24	007	008	008	008	008	008	008	008	008	008	008	008	
25	007	008	008	008	008	008	008	008	008	008	008	008	
26	007	008	008	008	008	008	008	008	008	008	008	008	
27	007	008	008	008	008	008	008	008	008	008	008	008	
28	007	008	008	008	008	008	008	008	008	008	008	008	
29	007	008	008	008	008	008	008	008	008	008	008	008	
30	007	008	008	008	008	008	008	008	008	008	008	008	
31	007	008	008	008	008	008	008	008	008	008	008	008	

- Notes : 1. Space @ expresses rainfall observation station name. 4. R means average depth of rainfall over area.  
 2. Space @ shows rainfall observation station number. 5. Qp means peak flood.  
 3. Space @ shows Thiessen Coefficient.

Table - Observed Rainfall and Discharge Data at Klopaswit Bridge Station

Month/Year : Feb / '83  
Catchment Area : 82.20 Km<sup>2</sup>

Rainfall (mm)					Discharge		Remarks
00200	20200	30200	40200	50200	R	Qp Observed Time	
1	0.07	0.06	0.04	0.05	0.19	3.2	
2	0.07	0.06	0.04	0.05	0.19	3.2	
3	0.07	0.06	0.04	0.05	0.19	3.2	
4	0.07	0.06	0.04	0.05	0.19	3.2	
5	0.07	0.06	0.04	0.05	0.19	3.2	
6	0.07	0.06	0.04	0.05	0.19	3.2	
7	0.07	0.06	0.04	0.05	0.19	3.2	
8	0.07	0.06	0.04	0.05	0.19	3.2	
9	0.07	0.06	0.04	0.05	0.19	3.2	
10	0.07	0.06	0.04	0.05	0.19	3.2	
11	0.07	0.06	0.04	0.05	0.19	3.2	
12	0.07	0.06	0.04	0.05	0.19	3.2	
13	0.07	0.06	0.04	0.05	0.19	3.2	
14	0.07	0.06	0.04	0.05	0.19	3.2	
15	0.07	0.06	0.04	0.05	0.19	3.2	
16	0.07	0.06	0.04	0.05	0.19	3.2	
17	0.07	0.06	0.04	0.05	0.19	3.2	
18	0.07	0.06	0.04	0.05	0.19	3.2	
19	0.07	0.06	0.04	0.05	0.19	3.2	
20	0.07	0.06	0.04	0.05	0.19	3.2	
21	0.07	0.06	0.04	0.05	0.19	3.2	
22	0.07	0.06	0.04	0.05	0.19	3.2	
23	0.07	0.06	0.04	0.05	0.19	3.2	
24	0.07	0.06	0.04	0.05	0.19	3.2	
25	0.07	0.06	0.04	0.05	0.19	3.2	
26	0.07	0.06	0.04	0.05	0.19	3.2	
27	0.07	0.06	0.04	0.05	0.19	3.2	
28	0.07	0.06	0.04	0.05	0.19	3.2	
29	0.07	0.06	0.04	0.05	0.19	3.2	
30	0.07	0.06	0.04	0.05	0.19	3.2	
31	0.07	0.06	0.04	0.05	0.19	3.2	
32	0.07	0.06	0.04	0.05	0.19	3.2	
33	0.07	0.06	0.04	0.05	0.19	3.2	
34	0.07	0.06	0.04	0.05	0.19	3.2	
35	0.07	0.06	0.04	0.05	0.19	3.2	
36	0.07	0.06	0.04	0.05	0.19	3.2	
37	0.07	0.06	0.04	0.05	0.19	3.2	
38	0.07	0.06	0.04	0.05	0.19	3.2	
39	0.07	0.06	0.04	0.05	0.19	3.2	
40	0.07	0.06	0.04	0.05	0.19	3.2	
41	0.07	0.06	0.04	0.05	0.19	3.2	
42	0.07	0.06	0.04	0.05	0.19	3.2	
43	0.07	0.06	0.04	0.05	0.19	3.2	
44	0.07	0.06	0.04	0.05	0.19	3.2	
45	0.07	0.06	0.04	0.05	0.19	3.2	
46	0.07	0.06	0.04	0.05	0.19	3.2	
47	0.07	0.06	0.04	0.05	0.19	3.2	
48	0.07	0.06	0.04	0.05	0.19	3.2	
49	0.07	0.06	0.04	0.05	0.19	3.2	
50	0.07	0.06	0.04	0.05	0.19	3.2	
51	0.07	0.06	0.04	0.05	0.19	3.2	
52	0.07	0.06	0.04	0.05	0.19	3.2	
53	0.07	0.06	0.04	0.05	0.19	3.2	
54	0.07	0.06	0.04	0.05	0.19	3.2	
55	0.07	0.06	0.04	0.05	0.19	3.2	
56	0.07	0.06	0.04	0.05	0.19	3.2	
57	0.07	0.06	0.04	0.05	0.19	3.2	
58	0.07	0.06	0.04	0.05	0.19	3.2	
59	0.07	0.06	0.04	0.05	0.19	3.2	
60	0.07	0.06	0.04	0.05	0.19	3.2	
61	0.07	0.06	0.04	0.05	0.19	3.2	
62	0.07	0.06	0.04	0.05	0.19	3.2	
63	0.07	0.06	0.04	0.05	0.19	3.2	
64	0.07	0.06	0.04	0.05	0.19	3.2	
65	0.07	0.06	0.04	0.05	0.19	3.2	
66	0.07	0.06	0.04	0.05	0.19	3.2	
67	0.07	0.06	0.04	0.05	0.19	3.2	
68	0.07	0.06	0.04	0.05	0.19	3.2	
69	0.07	0.06	0.04	0.05	0.19	3.2	
70	0.07	0.06	0.04	0.05	0.19	3.2	
71	0.07	0.06	0.04	0.05	0.19	3.2	
72	0.07	0.06	0.04	0.05	0.19	3.2	
73	0.07	0.06	0.04	0.05	0.19	3.2	
74	0.07	0.06	0.04	0.05	0.19	3.2	
75	0.07	0.06	0.04	0.05	0.19	3.2	
76	0.07	0.06	0.04	0.05	0.19	3.2	
77	0.07	0.06	0.04	0.05	0.19	3.2	
78	0.07	0.06	0.04	0.05	0.19	3.2	
79	0.07	0.06	0.04	0.05	0.19	3.2	
80	0.07	0.06	0.04	0.05	0.19	3.2	
81	0.07	0.06	0.04	0.05	0.19	3.2	
82	0.07	0.06	0.04	0.05	0.19	3.2	
83	0.07	0.06	0.04	0.05	0.19	3.2	
84	0.07	0.06	0.04	0.05	0.19	3.2	
85	0.07	0.06	0.04	0.05	0.19	3.2	
86	0.07	0.06	0.04	0.05	0.19	3.2	
87	0.07	0.06	0.04	0.05	0.19	3.2	
88	0.07	0.06	0.04	0.05	0.19	3.2	
89	0.07	0.06	0.04	0.05	0.19	3.2	
90	0.07	0.06	0.04	0.05	0.19	3.2	
91	0.07	0.06	0.04	0.05	0.19	3.2	
92	0.07	0.06	0.04	0.05	0.19	3.2	
93	0.07	0.06	0.04	0.05	0.19	3.2	
94	0.07	0.06	0.04	0.05	0.19	3.2	
95	0.07	0.06	0.04	0.05	0.19	3.2	
96	0.07	0.06	0.04	0.05	0.19	3.2	
97	0.07	0.06	0.04	0.05	0.19	3.2	
98	0.07	0.06	0.04	0.05	0.19	3.2	
99	0.07	0.06	0.04	0.05	0.19	3.2	
100	0.07	0.06	0.04	0.05	0.19	3.2	

Notes : 1. Space ( ) expresses rainfall observation station name. 4. R means average depth of rainfall over area.  
2. Space ( ) shows rainfall observation station number. 5. Qp means peak flood.  
3. Space ( ) shows Thiessen Coefficient.

Table - Observed Rainfall and Discharge Data at Klopasawit Bridge Station

Month/Year : Mar./'83  
 Catchment Area : 82.20 Km<sup>2</sup>

Rainfall (mm)										Discharge		Remarks
BEZDO	NOZG&K	G. JUYERK	G. DAK-S	SOZOKUZ&O	NOZG&K	G. DAK-S	G. JUYERK	BEZDO	R	Qp (m <sup>3</sup> /s)	Observed Time	
3	20	30	31	36	37	41						
1	0.07	0.06	0.04	0.65	0.07	0.13	0.14					
2	1			0.3	0.3	2.0			0.7	4.0	13:00 ~ 13:00	
3	38			12.0		21.0			16.0	13.0		
4	2			8.0		30.0			57.0	7.0	13:00 ~ 13:30	
5				16.0		4.0			9.0	4.0		
6	1			16.0		11.0			13.0	6.0	13:00 ~ 13:00	
7	33			7.0		10.0			9.0	4.0		
8	22			7.0		50.0			14.0	6.0		
9	48			62.0		16.0			40.0	13.0	13:00 ~ 21:00	
10	3			4.0		1.0			3.0	9.0	13:00 ~ 19:00	
11	16			7.0		33.0			10.0	4.0	13:00 ~ 20:00	
12				0.0		22.0			0.0	5.0	13:00 ~ 13:00	
13	25			4.0		9.0			5.0	13.0	13:00 ~ 13:00	
14	5			11.0		8.0			8.0	4.0	13:00 ~ 13:00	
15	2			28.0		12.0			11.0	13.0	13:00 ~ 13:00	
16	52			2.0		26.0			9.0	13.0	13:00 ~ 13:00	
17	9			9.0		20.0			9.0	13.0	13:00 ~ 13:00	
18	11			12.0		5.0			11.0	13.0	13:00 ~ 13:00	
19	12			2.0		5.0			5.0	13.0	13:00 ~ 13:00	
20				0.0		0.0			2.0	13.0	13:00 ~ 13:00	
21	8			1.0		9.0			11.0	13.0	13:00 ~ 13:00	
22	12					13.0			10.0	13.0	13:00 ~ 13:00	
23	6			13.0		11.0			9.0	13.0	13:00 ~ 13:00	
24										13.0	13:00 ~ 13:00	
25	25			6.0		35.0				13.0	13:00 ~ 13:00	
26				1.0		0.0			8.0	13.0	13:00 ~ 13:00	
27						29.0			20.0	6.0		
28				5.0		0.0			2.0	4.0		
29						0.0			0.0	8.0		
30	1			13.0		37.0			8.0	8.0		
31	2					6.0			5.0	4.0		
32	320			16.0		46.0			31.0	4.0		

- Notes : 1. Space @ expresses rainfall observation station name. 4. R means average depth of rainfall over area.  
 2. Space @ shows rainfall observation station number. 5. Qp means peak flood.  
 3. Space @ shows Thiessen Coefficient.

Table - Observed Rainfall and Discharge Data at Klopaswit Bridge Station

Month/Year: Apr. / '83  
 Catchment Area: 72.20 Km<sup>2</sup>

Rainfall (mm)						Discharge		Remarks
						R	Qp Observed (m <sup>3</sup> /s)	
1	5	20	31	33	37	41		
2	0.09	0.06	0.45	0.07	0.13	0.14		
3	1							
4	11							
5	6							
6	27							
7	22							
8	4							
9	1							
10								
11	24							
12	54							
13	12							
14								
15								
16								
17								
18								
19								
20								
21								
22								
23								
24								
25								
26								
27								
28								
29								
30								
31								
Σ	338							
Σ R	338							

- Notes:
1. Space ① expresses rainfall observation station name.
  2. Space ② shows rainfall observation station number.
  3. Space ③ shows Thiessen Coefficient.
  4. R means average depth of rainfall over area.
  5. Qp means peak flood.

Table - Observed Rainfall and Discharge Data at Klopasawit Bridge Station

Month/Year : May / '83  
 Catchment Area : 72.20 km<sup>2</sup>

Rainfall (mm)					Discharge		Remarks
Station	Time	mm	mm	mm	R	Qp	
1	18	38.2	14.2	12.1	35.1	20.5	13:00 ~ 14:05
2	-	1.1	-	-	0.2	9.7	13:10 ~ 13:50
3	22	2.2	32.5	17.2	12.1	9.7	"
4	5	-	3.5	-	0.5	-	"
5	4	32.2	1.2	3.2	23.1	11.7	"
6	18	2.2	7.2	11.2	12.2	11.7	13:00 ~ 14:00
7	14	15.2	6.2	26.2	24.2	13.2	13:00 ~ 14:00
8	-	2.2	1.2	4.2	2.2	11.2	"
9	-	24.2	-	6.2	19.2	-	"
10	-	-	-	-	-	-	"
11	3	0.2	2.2	9.2	2.2	-	"
12	23	32.2	1.2	32.2	31.2	-	"
13	77	57.2	14.2	52.2	56.2	27.2	"
14	-	2.2	-	-	1.2	-	"
15	17	4.2	2.2	26.2	1.2	-	"
16	-	40.2	33.2	66.2	40.2	20.2	13:10 ~ 14:00
17	11	3.2	1.2	10.2	5.2	11.2	13:00 ~ 14:00
18	32	65.2	3.2	24.2	36.2	-	"
19	25	1.2	12.2	5.2	9.2	9.7	"
20	9	12.2	-	15.2	13.2	-	"
21	-	12.2	0.2	15.2	1.2	-	"
22	2	2.2	2.2	-	1.2	-	"
23	11	16.2	31.2	2.2	15.2	12.2	13:00 ~ 14:00
24	12	14.2	13.2	15.2	14.2	-	"
25	202	7.2	12.2	14.2	44.2	8.2	"
26	10	24.2	112.2	112.2	125.2	11.2	"
27	65	16.2	12.2	23.2	74.2	-	"
28	19	11.2	13.2	20.2	18.2	-	"
29	-	28.2	1.2	11.2	26.2	-	"
30	30	7.2	12.2	20.2	10.2	-	"
31	2	2.2	-	2.2	2.2	-	"
7.1	650	152.2	772.2	544.2	770.2	-	"

Notes :

1. Space @ expresses rainfall observation station name.
2. Space @ shows rainfall observation station number.
3. Space @ shows Thiessen Coefficient.
4. R means average depth of rainfall over area.
5. Qp means peak flood.

Table - Observed Rainfall and Discharge Data at Klopsewit Bridge Station

Month/Year: Jan./'83  
Catchment Area: 82.20 km<sup>2</sup>

Rainfall (mm)										Discharge		Remarks
DATE	STATION	TIME	Q. LEKKE	Q. PAK - 5	3020202020	XKX-ONE	P. SAT	R. 2302020	R	Qp	Observed Time	
1	3	007	0.06	0.05	0.07	0.04	0.13	0.14			1200 ~ 1200	
2	3	20	0.04	0.05	0.07	0.04	0.13	0.14				
3	3	30	0.04	0.05	0.07	0.04	0.13	0.14				
4	3	40	0.04	0.05	0.07	0.04	0.13	0.14				
5	3	50	0.04	0.05	0.07	0.04	0.13	0.14				
6	3	00	0.04	0.05	0.07	0.04	0.13	0.14				
7	3	10	0.04	0.05	0.07	0.04	0.13	0.14				
8	3	20	0.04	0.05	0.07	0.04	0.13	0.14				
9	3	30	0.04	0.05	0.07	0.04	0.13	0.14				
10	3	40	0.04	0.05	0.07	0.04	0.13	0.14				
11	3	50	0.04	0.05	0.07	0.04	0.13	0.14				
12	3	00	0.04	0.05	0.07	0.04	0.13	0.14				
13	3	10	0.04	0.05	0.07	0.04	0.13	0.14				
14	3	20	0.04	0.05	0.07	0.04	0.13	0.14				
15	3	30	0.04	0.05	0.07	0.04	0.13	0.14				
16	3	40	0.04	0.05	0.07	0.04	0.13	0.14				
17	3	50	0.04	0.05	0.07	0.04	0.13	0.14				
18	3	00	0.04	0.05	0.07	0.04	0.13	0.14				
19	3	10	0.04	0.05	0.07	0.04	0.13	0.14				
20	3	20	0.04	0.05	0.07	0.04	0.13	0.14				
21	3	30	0.04	0.05	0.07	0.04	0.13	0.14				
22	3	40	0.04	0.05	0.07	0.04	0.13	0.14				
23	3	50	0.04	0.05	0.07	0.04	0.13	0.14				
24	3	00	0.04	0.05	0.07	0.04	0.13	0.14				
25	3	10	0.04	0.05	0.07	0.04	0.13	0.14				
26	3	20	0.04	0.05	0.07	0.04	0.13	0.14				
27	3	30	0.04	0.05	0.07	0.04	0.13	0.14				
28	3	40	0.04	0.05	0.07	0.04	0.13	0.14				
29	3	50	0.04	0.05	0.07	0.04	0.13	0.14				
30	3	00	0.04	0.05	0.07	0.04	0.13	0.14				
31	3	10	0.04	0.05	0.07	0.04	0.13	0.14				

- Notes:
1. Space @ expresses rainfall observation station name.
  2. Space @ shows rainfall observation station number.
  3. Space @ shows Thiessen Coefficient.
  4. R means average depth of rainfall over area.
  5. Qp means peak flood.



Table - Observed Rainfall and Discharge Data at Check Dam Leprak No.1 Station

Month/Year : Feb. / '83  
 Catchment Area : 27.50 Km<sup>2</sup>

Rainfall (mm)					Discharge		Remarks
Sl. No.	Time	Q <sub>p</sub>	R	Q <sub>p</sub>	Observed	Time	
1	32	31	32	35	38	7.2	
2	31	25	25	25	25	2.6	
3	31	25	25	25	25	14.2	
4	31	31	31	31	31	6.1	
5	25	66	66	66	66	6.1	
6	31	31	31	31	31	25.2	
7	31	31	31	31	31	1.9	
8	31	31	31	31	31	42.5	
9	12	31	31	31	31	19.9	START
10	23	21	21	21	21	21.2	
11	11	61	61	61	61	5.7	
12	11	13	13	13	13	5.7	
13	14	10	10	10	10	4.1	
14	11	11	11	11	11	4.1	
15	11	11	11	11	11	4.1	
16	11	11	11	11	11	4.1	
17	11	11	11	11	11	4.1	
18	11	11	11	11	11	4.1	
19	11	11	11	11	11	4.1	
20	11	11	11	11	11	4.1	
21	11	11	11	11	11	4.1	
22	11	11	11	11	11	4.1	
23	11	11	11	11	11	4.1	
24	11	11	11	11	11	4.1	
25	11	11	11	11	11	4.1	
26	11	11	11	11	11	4.1	
27	11	11	11	11	11	4.1	
28	11	11	11	11	11	4.1	
29	11	11	11	11	11	4.1	
30	11	11	11	11	11	4.1	
31	11	11	11	11	11	4.1	
32	11	11	11	11	11	4.1	
33	11	11	11	11	11	4.1	
34	11	11	11	11	11	4.1	
35	11	11	11	11	11	4.1	
36	11	11	11	11	11	4.1	
37	11	11	11	11	11	4.1	
38	11	11	11	11	11	4.1	
39	11	11	11	11	11	4.1	
40	11	11	11	11	11	4.1	
41	11	11	11	11	11	4.1	
42	11	11	11	11	11	4.1	
43	11	11	11	11	11	4.1	
44	11	11	11	11	11	4.1	
45	11	11	11	11	11	4.1	
46	11	11	11	11	11	4.1	
47	11	11	11	11	11	4.1	
48	11	11	11	11	11	4.1	
49	11	11	11	11	11	4.1	
50	11	11	11	11	11	4.1	
51	11	11	11	11	11	4.1	
52	11	11	11	11	11	4.1	
53	11	11	11	11	11	4.1	
54	11	11	11	11	11	4.1	
55	11	11	11	11	11	4.1	
56	11	11	11	11	11	4.1	
57	11	11	11	11	11	4.1	
58	11	11	11	11	11	4.1	
59	11	11	11	11	11	4.1	
60	11	11	11	11	11	4.1	
61	11	11	11	11	11	4.1	
62	11	11	11	11	11	4.1	
63	11	11	11	11	11	4.1	
64	11	11	11	11	11	4.1	
65	11	11	11	11	11	4.1	
66	11	11	11	11	11	4.1	
67	11	11	11	11	11	4.1	
68	11	11	11	11	11	4.1	
69	11	11	11	11	11	4.1	
70	11	11	11	11	11	4.1	
71	11	11	11	11	11	4.1	
72	11	11	11	11	11	4.1	
73	11	11	11	11	11	4.1	
74	11	11	11	11	11	4.1	
75	11	11	11	11	11	4.1	
76	11	11	11	11	11	4.1	
77	11	11	11	11	11	4.1	
78	11	11	11	11	11	4.1	
79	11	11	11	11	11	4.1	
80	11	11	11	11	11	4.1	
81	11	11	11	11	11	4.1	
82	11	11	11	11	11	4.1	
83	11	11	11	11	11	4.1	
84	11	11	11	11	11	4.1	
85	11	11	11	11	11	4.1	
86	11	11	11	11	11	4.1	
87	11	11	11	11	11	4.1	
88	11	11	11	11	11	4.1	
89	11	11	11	11	11	4.1	
90	11	11	11	11	11	4.1	
91	11	11	11	11	11	4.1	
92	11	11	11	11	11	4.1	
93	11	11	11	11	11	4.1	
94	11	11	11	11	11	4.1	
95	11	11	11	11	11	4.1	
96	11	11	11	11	11	4.1	
97	11	11	11	11	11	4.1	
98	11	11	11	11	11	4.1	
99	11	11	11	11	11	4.1	
100	11	11	11	11	11	4.1	

- Notes : 1. Space (A) expresses rainfall observation station name. 4. R means average depth of rainfall over area.  
 2. Space (B) shows rainfall observation station number. 5. Q<sub>p</sub> means peak flood.  
 3. Space (C) shows Thiessen Coefficient.

Table - Observed Rainfall and Discharge Data at Check Dam Leprek No.1 Station

Month/Year : Mar./'83  
 Catchment Area : 27.60 km<sup>2</sup>

Rainfall (mm)					Discharge		Remarks
G. S							

- Notes : 1. Space @ expresses rainfall observation station name.  
 2. Space @ shows rainfall observation station number.  
 3. Space @ shows Thiessen Coefficient.  
 4. R means average depth of rainfall over area.  
 5. Qp means peak flood.

Table - Observed Rainfall and Discharge Data at Check Dam Leprak No.1 Station

Month/Year : Apr. / '83  
Catchment Area : 27.60 km<sup>2</sup>

Rainfall (mm)										Discharge		Remarks
										R	Qp Observed (m <sup>3</sup> /s) : Time	
3020												

- Notes :
1. Space ① expresses rainfall observation station name.
  2. Space ② shows rainfall observation station number.
  3. Space ③ shows Thiessen Coefficient.
  4. R means average depth of rainfall over area.
  5. Q<sub>p</sub> means peak flood.

Table - Observed Rainfall and Discharge Data at Check Dam Leprak No.1 Station

Month/Year : May / '83

Catchment Area : 27.40 Km<sup>2</sup>

Rainfall (mm)										Discharge		Remarks
										R	Qp Observed (m <sup>3</sup> /s)	
Sl. No.	10	20	30	40	50	60	70	80	90	100	110	Time
1	10	20	30	40	50	60	70	80	90	100	110	13:00 ~ 14:00
2	10	20	30	40	50	60	70	80	90	100	110	14:00 ~ 15:00
3	10	20	30	40	50	60	70	80	90	100	110	15:00 ~ 16:00
4	10	20	30	40	50	60	70	80	90	100	110	16:00 ~ 17:00
5	10	20	30	40	50	60	70	80	90	100	110	17:00 ~ 18:00
6	10	20	30	40	50	60	70	80	90	100	110	18:00 ~ 19:00
7	10	20	30	40	50	60	70	80	90	100	110	19:00 ~ 20:00
8	10	20	30	40	50	60	70	80	90	100	110	20:00 ~ 21:00
9	10	20	30	40	50	60	70	80	90	100	110	21:00 ~ 22:00
10	10	20	30	40	50	60	70	80	90	100	110	22:00 ~ 23:00
11	10	20	30	40	50	60	70	80	90	100	110	23:00 ~ 24:00
12	10	20	30	40	50	60	70	80	90	100	110	24:00 ~ 25:00
13	10	20	30	40	50	60	70	80	90	100	110	25:00 ~ 26:00
14	10	20	30	40	50	60	70	80	90	100	110	26:00 ~ 27:00
15	10	20	30	40	50	60	70	80	90	100	110	27:00 ~ 28:00
16	10	20	30	40	50	60	70	80	90	100	110	28:00 ~ 29:00
17	10	20	30	40	50	60	70	80	90	100	110	29:00 ~ 30:00
18	10	20	30	40	50	60	70	80	90	100	110	30:00 ~ 31:00
19	10	20	30	40	50	60	70	80	90	100	110	31:00 ~ 32:00
20	10	20	30	40	50	60	70	80	90	100	110	32:00 ~ 33:00
21	10	20	30	40	50	60	70	80	90	100	110	33:00 ~ 34:00
22	10	20	30	40	50	60	70	80	90	100	110	34:00 ~ 35:00
23	10	20	30	40	50	60	70	80	90	100	110	35:00 ~ 36:00
24	10	20	30	40	50	60	70	80	90	100	110	36:00 ~ 37:00
25	10	20	30	40	50	60	70	80	90	100	110	37:00 ~ 38:00
26	10	20	30	40	50	60	70	80	90	100	110	38:00 ~ 39:00
27	10	20	30	40	50	60	70	80	90	100	110	39:00 ~ 40:00
28	10	20	30	40	50	60	70	80	90	100	110	40:00 ~ 41:00
29	10	20	30	40	50	60	70	80	90	100	110	41:00 ~ 42:00
30	10	20	30	40	50	60	70	80	90	100	110	42:00 ~ 43:00
31	10	20	30	40	50	60	70	80	90	100	110	43:00 ~ 44:00
32	10	20	30	40	50	60	70	80	90	100	110	44:00 ~ 45:00
33	10	20	30	40	50	60	70	80	90	100	110	45:00 ~ 46:00
34	10	20	30	40	50	60	70	80	90	100	110	46:00 ~ 47:00
35	10	20	30	40	50	60	70	80	90	100	110	47:00 ~ 48:00
36	10	20	30	40	50	60	70	80	90	100	110	48:00 ~ 49:00
37	10	20	30	40	50	60	70	80	90	100	110	49:00 ~ 50:00
38	10	20	30	40	50	60	70	80	90	100	110	50:00 ~ 51:00
39	10	20	30	40	50	60	70	80	90	100	110	51:00 ~ 52:00
40	10	20	30	40	50	60	70	80	90	100	110	52:00 ~ 53:00
41	10	20	30	40	50	60	70	80	90	100	110	53:00 ~ 54:00
42	10	20	30	40	50	60	70	80	90	100	110	54:00 ~ 55:00
43	10	20	30	40	50	60	70	80	90	100	110	55:00 ~ 56:00
44	10	20	30	40	50	60	70	80	90	100	110	56:00 ~ 57:00
45	10	20	30	40	50	60	70	80	90	100	110	57:00 ~ 58:00
46	10	20	30	40	50	60	70	80	90	100	110	58:00 ~ 59:00
47	10	20	30	40	50	60	70	80	90	100	110	59:00 ~ 60:00
48	10	20	30	40	50	60	70	80	90	100	110	60:00 ~ 61:00
49	10	20	30	40	50	60	70	80	90	100	110	61:00 ~ 62:00
50	10	20	30	40	50	60	70	80	90	100	110	62:00 ~ 63:00
51	10	20	30	40	50	60	70	80	90	100	110	63:00 ~ 64:00
52	10	20	30	40	50	60	70	80	90	100	110	64:00 ~ 65:00
53	10	20	30	40	50	60	70	80	90	100	110	65:00 ~ 66:00
54	10	20	30	40	50	60	70	80	90	100	110	66:00 ~ 67:00
55	10	20	30	40	50	60	70	80	90	100	110	67:00 ~ 68:00
56	10	20	30	40	50	60	70	80	90	100	110	68:00 ~ 69:00
57	10	20	30	40	50	60	70	80	90	100	110	69:00 ~ 70:00
58	10	20	30	40	50	60	70	80	90	100	110	70:00 ~ 71:00
59	10	20	30	40	50	60	70	80	90	100	110	71:00 ~ 72:00
60	10	20	30	40	50	60	70	80	90	100	110	72:00 ~ 73:00
61	10	20	30	40	50	60	70	80	90	100	110	73:00 ~ 74:00
62	10	20	30	40	50	60	70	80	90	100	110	74:00 ~ 75:00
63	10	20	30	40	50	60	70	80	90	100	110	75:00 ~ 76:00
64	10	20	30	40	50	60	70	80	90	100	110	76:00 ~ 77:00
65	10	20	30	40	50	60	70	80	90	100	110	77:00 ~ 78:00
66	10	20	30	40	50	60	70	80	90	100	110	78:00 ~ 79:00
67	10	20	30	40	50	60	70	80	90	100	110	79:00 ~ 80:00
68	10	20	30	40	50	60	70	80	90	100	110	80:00 ~ 81:00
69	10	20	30	40	50	60	70	80	90	100	110	81:00 ~ 82:00
70	10	20	30	40	50	60	70	80	90	100	110	82:00 ~ 83:00
71	10	20	30	40	50	60	70	80	90	100	110	83:00 ~ 84:00
72	10	20	30	40	50	60	70	80	90	100	110	84:00 ~ 85:00
73	10	20	30	40	50	60	70	80	90	100	110	85:00 ~ 86:00
74	10	20	30	40	50	60	70	80	90	100	110	86:00 ~ 87:00
75	10	20	30	40	50	60	70	80	90	100	110	87:00 ~ 88:00
76	10	20	30	40	50	60	70	80	90	100	110	88:00 ~ 89:00
77	10	20	30	40	50	60	70	80	90	100	110	89:00 ~ 90:00
78	10	20	30	40	50	60	70	80	90	100	110	90:00 ~ 91:00
79	10	20	30	40	50	60	70	80	90	100	110	91:00 ~ 92:00
80	10	20	30	40	50	60	70	80	90	100	110	92:00 ~ 93:00
81	10	20	30	40	50	60	70	80	90	100	110	93:00 ~ 94:00
82	10	20	30	40	50	60	70	80	90	100	110	94:00 ~ 95:00
83	10	20	30	40	50	60	70	80	90	100	110	95:00 ~ 96:00
84	10	20	30	40	50	60	70	80	90	100	110	96:00 ~ 97:00
85	10	20	30	40	50	60	70	80	90	100	110	97:00 ~ 98:00
86	10	20	30	40	50	60	70	80	90	100	110	98:00 ~ 99:00
87	10	20	30	40	50	60	70	80	90	100	110	99:00 ~ 100:00
88	10	20	30	40	50	60	70	80	90	100	110	100:00 ~ 101:00
89	10	20	30	40	50	60	70	80	90	100	110	101:00 ~ 102:00
90	10	20	30	40	50	60	70	80	90	100	110	102:00 ~ 103:00
91	10	20	30	40	50	60	70	80	90	100	110	103:00 ~ 104:00
92	10	20	30	40	50	60	70	80	90	100	110	104:00 ~ 105:00
93	10	20	30	40	50	60	70	80	90	100	110	105:00 ~ 106:00
94	10	20	30	40	50	60	70	80	90	100	110	106:00 ~ 107:00
95	10	20	30	40	50	60	70	80	90	100	110	107:00 ~ 108:00
96	10	20	30	40	50	60	70	80	90	100	110	108:00 ~ 109:00
97	10	20	30	40	50	60	70	80	90	100	110	109:00 ~ 110:00
98	10	20	30	40	50	60	70	80	90	100	110	110:00 ~ 111:00
99	10	20	30	40	50	60	70	80	90	100	110	111:00 ~ 112:00
100	10	20	30	40	50	60	70	80	90	100	110	112:00 ~ 113:00

Notes : 1. Space ( ) expresses rainfall observation station name. 4. R means average depth of rainfall over area.  
 2. Space ( ) shows rainfall observation station number. 5. Qp means peak flood.  
 3. Space ( ) shows Thiessen Coefficient.

Table - Observed Rainfall and Discharge Data at Check Dam Leprak No1 Station

Month/Year : Jun. / '83  
Catchment Area : 27.10 km<sup>2</sup>

Rainfall (mm)					Discharge		Remarks
Sl. No.	Time	Station	Amount	Intensity	R	Qp Observed (m <sup>3</sup> /s)	
1	1						
2	2						
3	3						
4	4						
5	5						
6	6						
7	7						
8	8						
9	9						
10	10						
11	11						
12	12						
13	13						
14	14						
15	15						
16	16						
17	17						
18	18						
19	19						
20	20						
21	21						
22	22						
23	23						
24	24						
25	25						
26	26						
27	27						
28	28						
29	29						
30	30						
31	31						
32	32						

- Notes :
1. Space ( ) expresses rainfall observation station name.
  2. Space ( ) shows rainfall observation station number.
  3. Space ( ) shows Thiessen Coefficient.
  4. R means average depth of rainfall over area.
  5. Qp means peak flood.

Table - Observed Rainfall and Discharge Data at Planned Pronojiwo Dam Station

Month/Year : Feb. / '83  
 Catchment Area : 54.30 Km<sup>2</sup>

Date	Rainfall (mm)						Discharge		Remarks
	0.10000	0.10000	0.10000	0.10000	0.10000	0.10000	R	Qp Observed (m <sup>3</sup> /s)	Time
1	30	31	32	33	34	35	16.7		
2	36	37	38	39	40	41	16.7		
3	42	43	44	45	46	47	16.7		
4	48	49	50	51	52	53	16.7		
5	54	55	56	57	58	59	16.7		
6	60	61	62	63	64	65	16.7		
7	66	67	68	69	70	71	16.7		
8	72	73	74	75	76	77	16.7		
9	78	79	80	81	82	83	16.7		
10	84	85	86	87	88	89	16.7		
11	90	91	92	93	94	95	16.7		
12	96	97	98	99	100	101	16.7		
13	102	103	104	105	106	107	16.7		
14	108	109	110	111	112	113	16.7		
15	114	115	116	117	118	119	16.7		
16	120	121	122	123	124	125	16.7		
17	126	127	128	129	130	131	16.7		
18	132	133	134	135	136	137	16.7		
19	138	139	140	141	142	143	16.7		
20	144	145	146	147	148	149	16.7		
21	150	151	152	153	154	155	16.7		
22	156	157	158	159	160	161	16.7		
23	162	163	164	165	166	167	16.7		
24	168	169	170	171	172	173	16.7		
25	174	175	176	177	178	179	16.7		
26	180	181	182	183	184	185	16.7		
27	186	187	188	189	190	191	16.7		
28	192	193	194	195	196	197	16.7		
29	198	199	200	201	202	203	16.7		
30	204	205	206	207	208	209	16.7		
31	210	211	212	213	214	215	16.7		
32	216	217	218	219	220	221	16.7		
33	222	223	224	225	226	227	16.7		
34	228	229	230	231	232	233	16.7		
35	234	235	236	237	238	239	16.7		
36	240	241	242	243	244	245	16.7		
37	246	247	248	249	250	251	16.7		
38	252	253	254	255	256	257	16.7		
39	258	259	260	261	262	263	16.7		
40	264	265	266	267	268	269	16.7		
41	270	271	272	273	274	275	16.7		
42	276	277	278	279	280	281	16.7		
43	282	283	284	285	286	287	16.7		
44	288	289	290	291	292	293	16.7		
45	294	295	296	297	298	299	16.7		
46	300	301	302	303	304	305	16.7		
47	306	307	308	309	310	311	16.7		
48	312	313	314	315	316	317	16.7		
49	318	319	320	321	322	323	16.7		
50	324	325	326	327	328	329	16.7		
51	330	331	332	333	334	335	16.7		
52	336	337	338	339	340	341	16.7		
53	342	343	344	345	346	347	16.7		
54	348	349	350	351	352	353	16.7		
55	354	355	356	357	358	359	16.7		
56	360	361	362	363	364	365	16.7		
57	366	367	368	369	370	371	16.7		
58	372	373	374	375	376	377	16.7		
59	378	379	380	381	382	383	16.7		
60	384	385	386	387	388	389	16.7		
61	390	391	392	393	394	395	16.7		
62	396	397	398	399	400	401	16.7		
63	402	403	404	405	406	407	16.7		
64	408	409	410	411	412	413	16.7		
65	414	415	416	417	418	419	16.7		
66	420	421	422	423	424	425	16.7		
67	426	427	428	429	430	431	16.7		
68	432	433	434	435	436	437	16.7		
69	438	439	440	441	442	443	16.7		
70	444	445	446	447	448	449	16.7		
71	450	451	452	453	454	455	16.7		
72	456	457	458	459	460	461	16.7		
73	462	463	464	465	466	467	16.7		
74	468	469	470	471	472	473	16.7		
75	474	475	476	477	478	479	16.7		
76	480	481	482	483	484	485	16.7		
77	486	487	488	489	490	491	16.7		
78	492	493	494	495	496	497	16.7		
79	498	499	500	501	502	503	16.7		
80	504	505	506	507	508	509	16.7		
81	510	511	512	513	514	515	16.7		
82	516	517	518	519	520	521	16.7		
83	522	523	524	525	526	527	16.7		
84	528	529	530	531	532	533	16.7		
85	534	535	536	537	538	539	16.7		
86	540	541	542	543	544	545	16.7		
87	546	547	548	549	550	551	16.7		
88	552	553	554	555	556	557	16.7		
89	558	559	560	561	562	563	16.7		
90	564	565	566	567	568	569	16.7		
91	570	571	572	573	574	575	16.7		
92	576	577	578	579	580	581	16.7		
93	582	583	584	585	586	587	16.7		
94	588	589	590	591	592	593	16.7		
95	594	595	596	597	598	599	16.7		
96	600	601	602	603	604	605	16.7		
97	606	607	608	609	610	611	16.7		
98	612	613	614	615	616	617	16.7		
99	618	619	620	621	622	623	16.7		
100	624	625	626	627	628	629	16.7		
101	630	631	632	633	634	635	16.7		
102	636	637	638	639	640	641	16.7		
103	642	643	644	645	646	647	16.7		
104	648	649	650	651	652	653	16.7		
105	654	655	656	657	658	659	16.7		
106	660	661	662	663	664	665	16.7		
107	666	667	668	669	670	671	16.7		
108	672	673	674	675	676	677	16.7		
109	678	679	680	681	682	683	16.7		
110	684	685	686	687	688	689	16.7		
111	690	691	692	693	694	695	16.7		
112	696	697	698	699	700	701	16.7		
113	702	703	704	705	706	707	16.7		
114	708	709	710	711	712	713	16.7		
115	714	715	716	717	718	719	16.7		
116	720	721	722	723	724	725	16.7		
117	726	727	728	729	730	731	16.7		
118	732	733	734	735	736	737	16.7		
119	738	739	740	741	742	743	16.7		
120	744	745	746	747	748	749	16.7		
121	750	751	752	753	754	755	16.7		
122	756	757	758	759	760	761	16.7		
123	762	763	764	765	766	767	16.7		
124	768	769	770	771	772	773	16.7		
125	774	775	776	777	778	779	16.7		
126	780	781	782	783	784	785	16.7		
127	786	787	788	789	790	791	16.7		
128	792	793	794	795	796	797	16.7		
129	798	799	800	801	802	803	16.7		
130	804	805	806	807	808	809	16.7		
131	810	811	812	813	814	815	16.7		
132	816	817	818	819	820	821	16.7		
133	822	823	824	825	826	827	16.7		
134	828	829	830	831	832	833	16.7		
135	834	835	836	837	838	839	16.7		
136	840	841	842	843	844	845	16.7		
137	846	847	848	849	850	851	16.7		
138	852	853	854	855	856	857	16.7		
139	858	859	860	861	862	863	16.7		
140	864	865	866	867	868	869	16.7		
141	870	871	872	873	874	875	16.7		
142	876	877	878	879	880	881	16.7		
143	882	883	884	885	886	887	16.7		
144	888	889	890	891	892	893	16.7		
145	894	895	896	897	898	899	16.7		
146	900	901	902	903	904	905	16.7		
147	906	907	908	909	910	911	16.7		
148	912	913	914	915	916	917	16.7		
149	918	919	920	921	922	923	16.7		
150	924	925	926	927	928	929	16.7		
151	930	931	932	933	934	935	16.7		
152	936	937	938	939	940	941	16.7		
153	942	943	944	945	946	947	16.7		
154	948	949	950	951	952	953	16.7		
155	954	955	956	957	958	959	16.7		
156	960	961	962	963	964	965			

Month/Year : Mar. / '73  
Catchment Area: 54.30 Km<sup>2</sup>.

[illegible]

Notes :

1. Space ① expresses rainfall observation station name.
2. Space ② shows rainfall observation station number.
3. Space ③ shows Thiessen Coefficient.
4. R means average depth of rainfall over area.
5. Qp means peak flood.

Table - Observed Rainfall and Discharge Data at Planned Pronojiwo Dam Station

Month/Year : Apr./'83  
 Catchment Area : 54.30 Km<sup>2</sup>

Rainfall (mm)					Discharge		Remarks
					R	Qp Observed (m <sup>3</sup> /s) Time	
1	0.1	0.1	0.1	0.1	0.1	12.00 - 12.00	
2	0.1	0.1	0.1	0.1	0.1	12.00 - 12.00	
3	0.1	0.1	0.1	0.1	0.1	12.00 - 12.00	
4	0.1	0.1	0.1	0.1	0.1	12.00 - 12.00	
5	0.1	0.1	0.1	0.1	0.1	12.00 - 12.00	
6	0.1	0.1	0.1	0.1	0.1	12.00 - 12.00	
7	0.1	0.1	0.1	0.1	0.1	12.00 - 12.00	
8	0.1	0.1	0.1	0.1	0.1	12.00 - 12.00	
9	0.1	0.1	0.1	0.1	0.1	12.00 - 12.00	
10	0.1	0.1	0.1	0.1	0.1	12.00 - 12.00	
11	0.1	0.1	0.1	0.1	0.1	12.00 - 12.00	
12	0.1	0.1	0.1	0.1	0.1	12.00 - 12.00	
13	0.1	0.1	0.1	0.1	0.1	12.00 - 12.00	
14	0.1	0.1	0.1	0.1	0.1	12.00 - 12.00	
15	0.1	0.1	0.1	0.1	0.1	12.00 - 12.00	
16	0.1	0.1	0.1	0.1	0.1	12.00 - 12.00	
17	0.1	0.1	0.1	0.1	0.1	12.00 - 12.00	
18	0.1	0.1	0.1	0.1	0.1	12.00 - 12.00	
19	0.1	0.1	0.1	0.1	0.1	12.00 - 12.00	
20	0.1	0.1	0.1	0.1	0.1	12.00 - 12.00	
21	0.1	0.1	0.1	0.1	0.1	12.00 - 12.00	
22	0.1	0.1	0.1	0.1	0.1	12.00 - 12.00	
23	0.1	0.1	0.1	0.1	0.1	12.00 - 12.00	
24	0.1	0.1	0.1	0.1	0.1	12.00 - 12.00	
25	0.1	0.1	0.1	0.1	0.1	12.00 - 12.00	
26	0.1	0.1	0.1	0.1	0.1	12.00 - 12.00	
27	0.1	0.1	0.1	0.1	0.1	12.00 - 12.00	
28	0.1	0.1	0.1	0.1	0.1	12.00 - 12.00	
29	0.1	0.1	0.1	0.1	0.1	12.00 - 12.00	
30	0.1	0.1	0.1	0.1	0.1	12.00 - 12.00	
31	0.1	0.1	0.1	0.1	0.1	12.00 - 12.00	

- Notes:
1. Space @ expresses rainfall observation station name.
  2. Space @ shows rainfall observation station number.
  3. Space @ shows Thiessen Coefficient.
  4. R means average depth of rainfall over area.
  5. Qp means peak flood.



Table - Observed Rainfall and Discharge Data at Planned Pronojiwo Dam Station

Month/Year : May / '83

Catchment Area : 54.3<sup>km</sup>2

Rainfall (mm)										Discharge		Remarks
										R	Qp Observed (m <sup>3</sup> /s)	
Date	6. JUNE	7. JUNE	8. JUNE	9. JUNE	10. JUNE	11. JUNE	12. JUNE	13. JUNE	14. JUNE	15. JUNE	16. JUNE	17. JUNE
1	11	11	11	11	11	11	11	11	11	11	11	11
2	11	11	11	11	11	11	11	11	11	11	11	11
3	11	11	11	11	11	11	11	11	11	11	11	11
4	11	11	11	11	11	11	11	11	11	11	11	11
5	11	11	11	11	11	11	11	11	11	11	11	11
6	11	11	11	11	11	11	11	11	11	11	11	11
7	11	11	11	11	11	11	11	11	11	11	11	11
8	11	11	11	11	11	11	11	11	11	11	11	11
9	11	11	11	11	11	11	11	11	11	11	11	11
10	11	11	11	11	11	11	11	11	11	11	11	11
11	11	11	11	11	11	11	11	11	11	11	11	11
12	11	11	11	11	11	11	11	11	11	11	11	11
13	11	11	11	11	11	11	11	11	11	11	11	11
14	11	11	11	11	11	11	11	11	11	11	11	11
15	11	11	11	11	11	11	11	11	11	11	11	11
16	11	11	11	11	11	11	11	11	11	11	11	11
17	11	11	11	11	11	11	11	11	11	11	11	11
18	11	11	11	11	11	11	11	11	11	11	11	11
19	11	11	11	11	11	11	11	11	11	11	11	11
20	11	11	11	11	11	11	11	11	11	11	11	11
21	11	11	11	11	11	11	11	11	11	11	11	11
22	11	11	11	11	11	11	11	11	11	11	11	11
23	11	11	11	11	11	11	11	11	11	11	11	11
24	11	11	11	11	11	11	11	11	11	11	11	11
25	11	11	11	11	11	11	11	11	11	11	11	11
26	11	11	11	11	11	11	11	11	11	11	11	11
27	11	11	11	11	11	11	11	11	11	11	11	11
28	11	11	11	11	11	11	11	11	11	11	11	11
29	11	11	11	11	11	11	11	11	11	11	11	11
30	11	11	11	11	11	11	11	11	11	11	11	11
31	11	11	11	11	11	11	11	11	11	11	11	11
TOTAL	11	11	11	11	11	11	11	11	11	11	11	11

- Notes : 1. Space ① expresses rainfall observation station name. 4. R means average depth of rainfall over area.  
 2. Space ② shows rainfall observation station number. 5. Qp means peak flood.  
 3. Space ③ shows Thiessen Coefficient.

Table - Observed Rainfall and Discharge Data at Planned Pronojiwo Dam Station

Month/Year : Jan./'83  
Catchment Area : 54.30 km<sup>2</sup>

Rainfall (mm)										Discharge		Remarks
R										Qp	Observed Time	
Station	Station	Station	Station	Station	Station	Station	Station	Station	Station			
1	2	3	4	5	6	7	8	9	10	11	12	13
15	16	17	18	19	20	21	22	23	24	25	26	27
29	30	31	32	33	34	35	36	37	38	39	40	41
43	44	45	46	47	48	49	50	51	52	53	54	55
57	58	59	60	61	62	63	64	65	66	67	68	69
71	72	73	74	75	76	77	78	79	80	81	82	83
85	86	87	88	89	90	91	92	93	94	95	96	97
99	100	101	102	103	104	105	106	107	108	109	110	111
113	114	115	116	117	118	119	120	121	122	123	124	125
127	128	129	130	131	132	133	134	135	136	137	138	139
141	142	143	144	145	146	147	148	149	150	151	152	153
155	156	157	158	159	160	161	162	163	164	165	166	167
169	170	171	172	173	174	175	176	177	178	179	180	181
183	184	185	186	187	188	189	190	191	192	193	194	195
197	198	199	200	201	202	203	204	205	206	207	208	209
211	212	213	214	215	216	217	218	219	220	221	222	223
225	226	227	228	229	230	231	232	233	234	235	236	237
239	240	241	242	243	244	245	246	247	248	249	250	251
253	254	255	256	257	258	259	260	261	262	263	264	265
267	268	269	270	271	272	273	274	275	276	277	278	279
281	282	283	284	285	286	287	288	289	290	291	292	293
295	296	297	298	299	300	301	302	303	304	305	306	307
309	310	311	312	313	314	315	316	317	318	319	320	321
323	324	325	326	327	328	329	330	331	332	333	334	335
337	338	339	340	341	342	343	344	345	346	347	348	349
351	352	353	354	355	356	357	358	359	360	361	362	363
365	366	367	368	369	370	371	372	373	374	375	376	377
379	380	381	382	383	384	385	386	387	388	389	390	391
393	394	395	396	397	398	399	400	401	402	403	404	405
407	408	409	410	411	412	413	414	415	416	417	418	419
421	422	423	424	425	426	427	428	429	430	431	432	433
435	436	437	438	439	440	441	442	443	444	445	446	447
449	450	451	452	453	454	455	456	457	458	459	460	461
463	464	465	466	467	468	469	470	471	472	473	474	475
477	478	479	480	481	482	483	484	485	486	487	488	489
491	492	493	494	495	496	497	498	499	500	501	502	503
505	506	507	508	509	510	511	512	513	514	515	516	517
519	520	521	522	523	524	525	526	527	528	529	530	531
533	534	535	536	537	538	539	540	541	542	543	544	545
547	548	549	550	551	552	553	554	555	556	557	558	559
561	562	563	564	565	566	567	568	569	570	571	572	573
575	576	577	578	579	580	581	582	583	584	585	586	587
589	590	591	592	593	594	595	596	597	598	599	600	601
603	604	605	606	607	608	609	610	611	612	613	614	615
617	618	619	620	621	622	623	624	625	626	627	628	629
631	632	633	634	635	636	637	638	639	640	641	642	643
645	646	647	648	649	650	651	652	653	654	655	656	657
659	660	661	662	663	664	665	666	667	668	669	670	671
673	674	675	676	677	678	679	680	681	682	683	684	685
687	688	689	690	691	692	693	694	695	696	697	698	699
701	702	703	704	705	706	707	708	709	710	711	712	713
715	716	717	718	719	720	721	722	723	724	725	726	727
729	730	731	732	733	734	735	736	737	738	739	740	741
743	744	745	746	747	748	749	750	751	752	753	754	755

- Notes : 1. Space ( ) expresses rainfall observation station name. 4. R means average depth of rainfall over area.  
2. Space ( ) shows rainfall observation station number. 5. Qp means peak flood.  
3. Space ( ) shows Thiessen Coefficient.

THE REPUBLIC OF INDONESIA

THE FEASIBILITY STUDY ON THE VOLCANIC DEBRIS  
CONTROL AND WATER CONSERVATION PROJECT  
IN THE SOUTHEASTERN SLOPE OF MT. SEMERU

SUPPORTING REPORT (5)

PART - C  
GROUND WATER

FEBRUARY, 1984

JAPAN INTERNATIONAL COOPERATION AGENCY



## C. GROUNDWATER

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## 1. INTRODUCTION

### 1.1 OBJECTIVE

The principal objective of this hydrogeological study is to delineate the groundwater system in the study area. This study results will be contributed to the evaluation of groundwater development potential at the prospective sites, closely related to the project feature of sediment control work.

### 1.2 BACKGROUND

The study area located in the southeastern slope of Mt. Semeru has abundant rainfall amount in rainy season, but the shortage of irrigation water appears more or less in the certain area during dry season.

Groundwater is recognized as the stable water resource in comparison with surface water, and is expected to be one of solutions to resolve this shortage of irrigation water.

It is necessary that the prospective site will have an adequate groundwater basin structure to store enough capacity of groundwater.

From the viewpoints of topographical and geological conditions, the K. Lengkong basin located in the south of Mt. Semeru will be recognized as the main target of groundwater development potential.

Moreover, the K. Lengkong basin will be included into the first priority project area of K. Rejati.

### 1.3 STUDY ITEMS

Hydrogeological study consists mainly of geology, groundwater, water quality and these integral interpretations, and also depends on hydrology, water and land use, and so on.

Taking into consideration the above-mentioned study results, this report will be dealt with the following study items;

- ① Groundwater Level
  - Well inventory
  - Observation of groundwater level
  - Interpretation and consideration
- ② Water Quality
  - Simplified water quality test; pH, T, DO, EC, Turb.
  - Chemical analysis; Na, K, Mg, Ca, Cl, SO<sub>4</sub>, HCO<sub>3</sub>, etc.
  - Hydro-geochemical interpretation
  - Water quality evaluation for use
- ③ Hydrogeology of K. Lengkong Basin
  - Hydraulic properties; Groundwater table, Permeability, etc.
  - Delineation of groundwater system; Aquifer, Basin structure, Groundwater movement, etc.
  - Panorama for groundwater development

Flow chart of these field works and studies are as shown in Fig.-1.1.

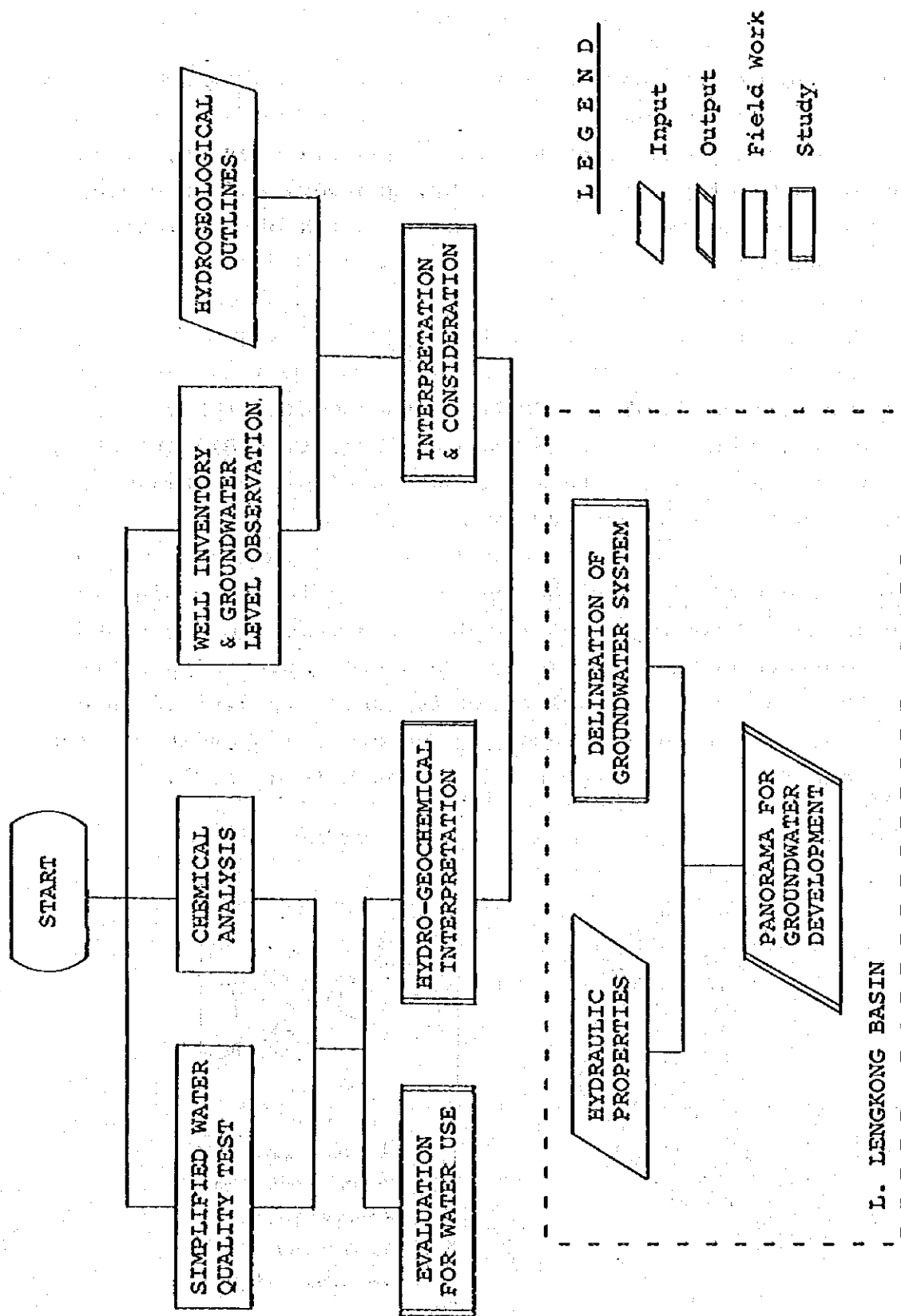


Fig.-1.1 Flow Chart of Groundwater Study

#### 1.4 OUTLINES OF THE STUDY AREA

Before enter the groundwater and water quality studies, we will mention briefly about topography, geology, and land use, because these studies are closely related with our hydrogeological studies.

##### 1.4.1 TOPOGRAPHY

Mt. Semeru is located about 100 km southeast of Surabaya and about 30 km west of Lumajang (long. 113°E, lat. 8°S); the study area covers the southern and southeastern slopes of this mountain with an area of about 730 km<sup>2</sup>.

Mt. Semeru, one of the most active volcanoes in Indonesia, is a very young stratovolcano of the Quaternary period and stands at the southern end of a series of volcanoes stretching north and south. This range of volcanoes is generally divided into three topographical units; Tengger mountains, Jambangan complex volcano and Mt. Semeru, from north to south (Fig.-1.2).

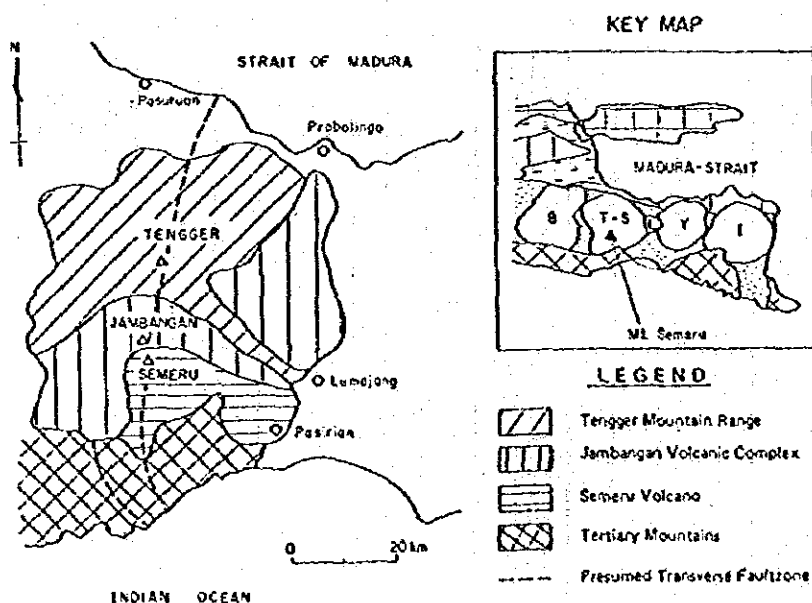


Fig. 1.2 Schematic Geomorphological Unit Map of Tengger - Semeru Volcanic Row.

Mt. Semeru is the youngest of these volcanoes and is being formed on the southern slope of the Jambangan complex volcano, which is the oldest.

On the south of Mt. Semeru, a range of mountains is found, consisting of Tertiary rocks with an elevation of 200 m to 1,000 m. The piedmont of Mt. Semeru develops extensively from east to southeast and reaches as far as Lumajang; however, its development towards the south is interrupted by the Tertiary mountains. The slopes of Mt. Semeru extending towards the north are formed covering a length of 2,600 m over the Jambangan volcano.

(1) Southeastern Slope of Mt. Semeru

The southeastern part of Semeru Volcano, a subject area of the current study, can be divided into the following 3 geomorphological units.

i) Main Part of the Volcanic Cone

Main part of the volcanic cone is over EL. 1,500 m, where volcanic activity of Semeru Volcano directly affects. Pyroclastic flow, ash fall, lapilli, volcanic bomb and lava etc. spewed directly from the crater, are distributed over this area and its inclination is very steep at 27 degree.

ii) Volcanic Fan

The volcanic fan is the slope between EL. 150 and 1,500 m, where Lahar and Ladu disasters mostly concentrate. The volcanic fan is classified, as shown in Table-1.1.

Tablo-1.1 Geomorphological Subunits of Volcanic Fan

Geomorphological Subunits		Deposits	Elevation // Slope
Ladu Fan		lava flow pyroclastic flow Lahar	EL. 800 to 1,500 m
Lahar Fan	Lahar Fan A	Lahar	EL. 250 to 800 m steep sloped fan
	Lahar Fan B	Lahar	EL. 150 to 250 m slow sloped fan

## iii) Volcanic Piedmont Periphery

Volcanic piedmont periphery is a very slow sloped flat ground formed outside of the volcanic fan. In this area, exists an overflow deposit comprising sand, subangular pebbles, silt and clay. Further outside of this terrain, the alluvial plain and the coastal plain are formed.

## (2) Tertiary Mountains and Hills

In the southwestern part of the study area lie steep mountains of Mature stage of max. EL. 1,000 m consisting of Tertiary volcanic rocks. In the north of these mountains near the boundary between Semeru Volcano and the mountains, a mountain range extends east to west in arcs, which blocks the extension of the foot of Semeru Volcano to the south. The slope of the mountains is very steep and dissected with many small valleys. To the south of Pasirian, two isolated hills consisting of the Tertiary Volcanic breccia stand out in the Volcanic fan.



### (3) River Systems

A great number of valleys is conspicuously developed on the southern and southeastern slopes of Mt. Semeru. These valleys can be classified into three river systems flowing into the Indonesian ocean; i.e., K. Mufur, K. Rejali and K. Glidik, as shown in Fig.-1.3.

#### i) K. Mufur

The main channel of K. Mufur is formed by B. Sat, B. Tunggeng and K. Mufur, in that order. The average incline of the main stream from the mountain top to the river mouth is  $1/11$ , which represents the most moderate gradient of the three rivers.

#### ii) K. Rejali

The main channel of K. Rejali is formed by B. Kobo'an, K. Leprak, K. Regoyo and K. Rejali, in that order. The main stream from the mountain top to the river mouth runs swiftly at the average inclination of  $1/9.2$ . The river deeply erodes the Tertiary mountains (Kobo'an valley) from EL. 500 m to 600 m, and forms an alluvial fan at its lower reaches once again.

#### iii) K. Glidik

The main channel of K. Glidik is formed by B. Bang, K. Lengkong and K. Glidik in that order. The average inclination from the mountain top to the river mouth is of  $1/9.0$ , which represents the steepest slope among the three rivers. K. Glidik collects water from valleys on the southern slope of Mt. Semeru and flows down through a valley deeply eroded in the Tertiary mountains.

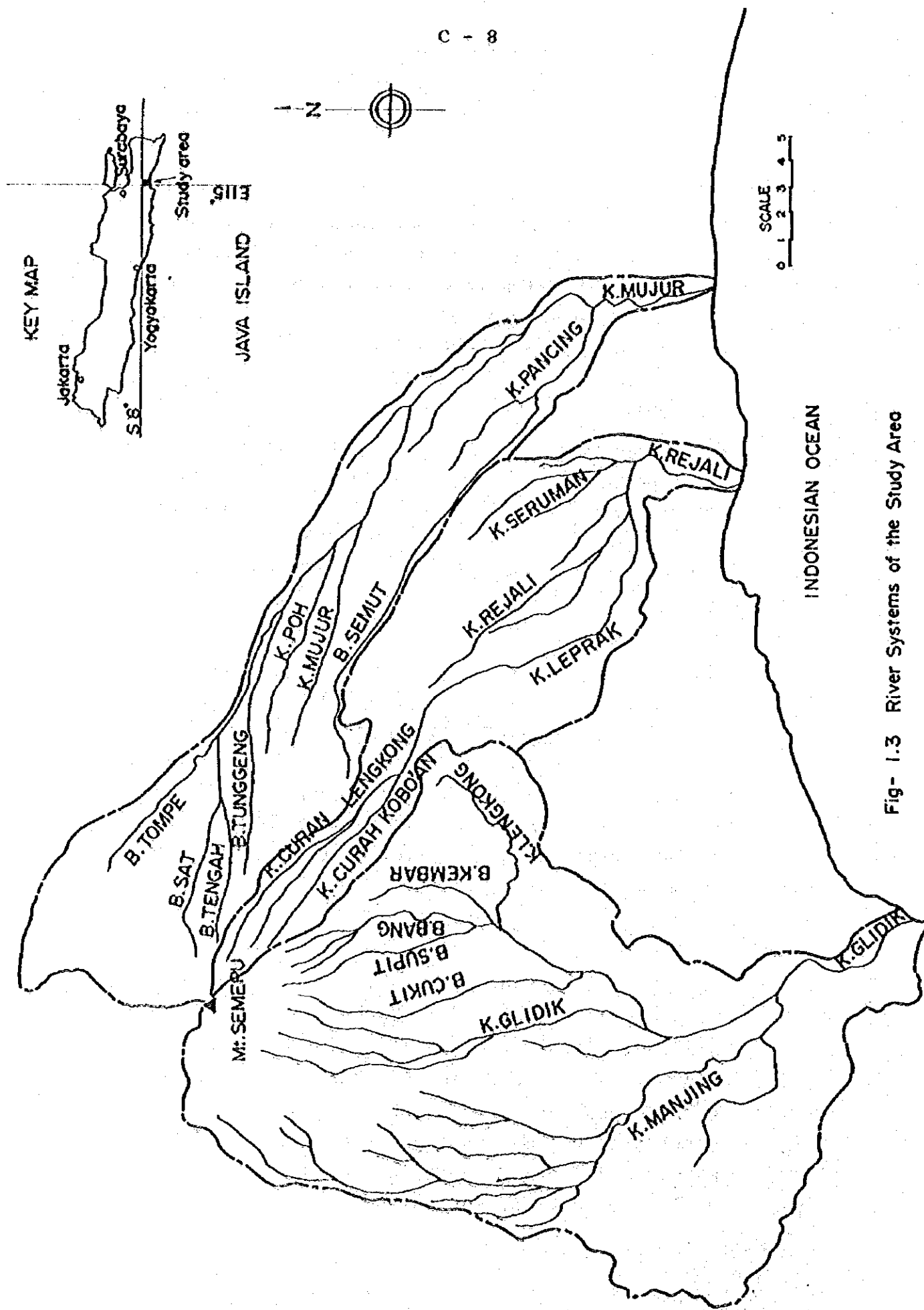


Fig- 1.3 River Systems of the Study Area

#### 1.4.2 GEOLOGY

##### (1) Lithology and Stratigraphy

The study area covers both Tertiary volcanic rocks and Tertiary limestone distribution area and Quaternary volcanic products distribution area. Geology of the study area is largely divided into Tertiary system of south and Quaternary system of north. Tertiary system and Quaternary system are respectively divided into several layers as shown in Table-1.2 and schematically represented in Fig.-1.4.

##### i) Tertiary System




Tertiary system of the study area is mostly composed of such volcanic rocks as andesite and tuff breccia distributed in the south of the study area. Mountains consisting of Tertiary system show very steep topography of the mature stage, making a sharp contrast with the smooth slope of Semeru Volcano consisting of Quaternary system.

Tertiary system of the study area is divided into following 5 layers from lower to upper.

- Green Tuff
- Limestone Layer
- Alternation of Andesite/Tuff Breccia
- Tuff
- Volcanic Breccia

As sedimentary rocks, only limestone is distributed in a very narrow sphere near the estuary of K. Glidik.

Table-1.2 Sequence of Strata of the Study Area

Age	Layer	Facies	
Holocene 	Alluvial Deposits	Sand, round-subangular gravels, silt, clay stratified.	
	Younger Volcanic Products (From Semeru Volcano)	Primary Volcanic Products	Andesite to basaltic lava, pyroclastic deposits, ash, bomb, lapilli, etc. very loose.
		Younger Lahar Deposits	Loose sand and angular gravels.
		Older Lahar Deposits	Compact sand and angular gravels.
	Pleistocene 	Older Volcanic Products (From Jambangan Volcanic Complex and Tengger Mountain Range)	Andesitic to basaltic lava, Pyroclastic deposits, ash, bomb, lapilli, Lahar deposits, etc., weathered.
Volcanic Breccia		Volcanic breccia partly intercalated sandy tuff and andesite lava.	
Tuff		Tuff partly intercalated tuff breccia, tuffaceous mudstone, tuffaceous sand, andesite lava and pumice layer.	
Alternation of andesite Lava and Volcanic Breccia		Alternation of andesite lava and volcanic breccia.	
Limestone		Chalky limestone, partly calcarenite.	
Miocene 	Green Tuff	Green tuff, green volcanic breccia, green tuff breccia, propylite, acidic welded tuff, liparite, etc.	

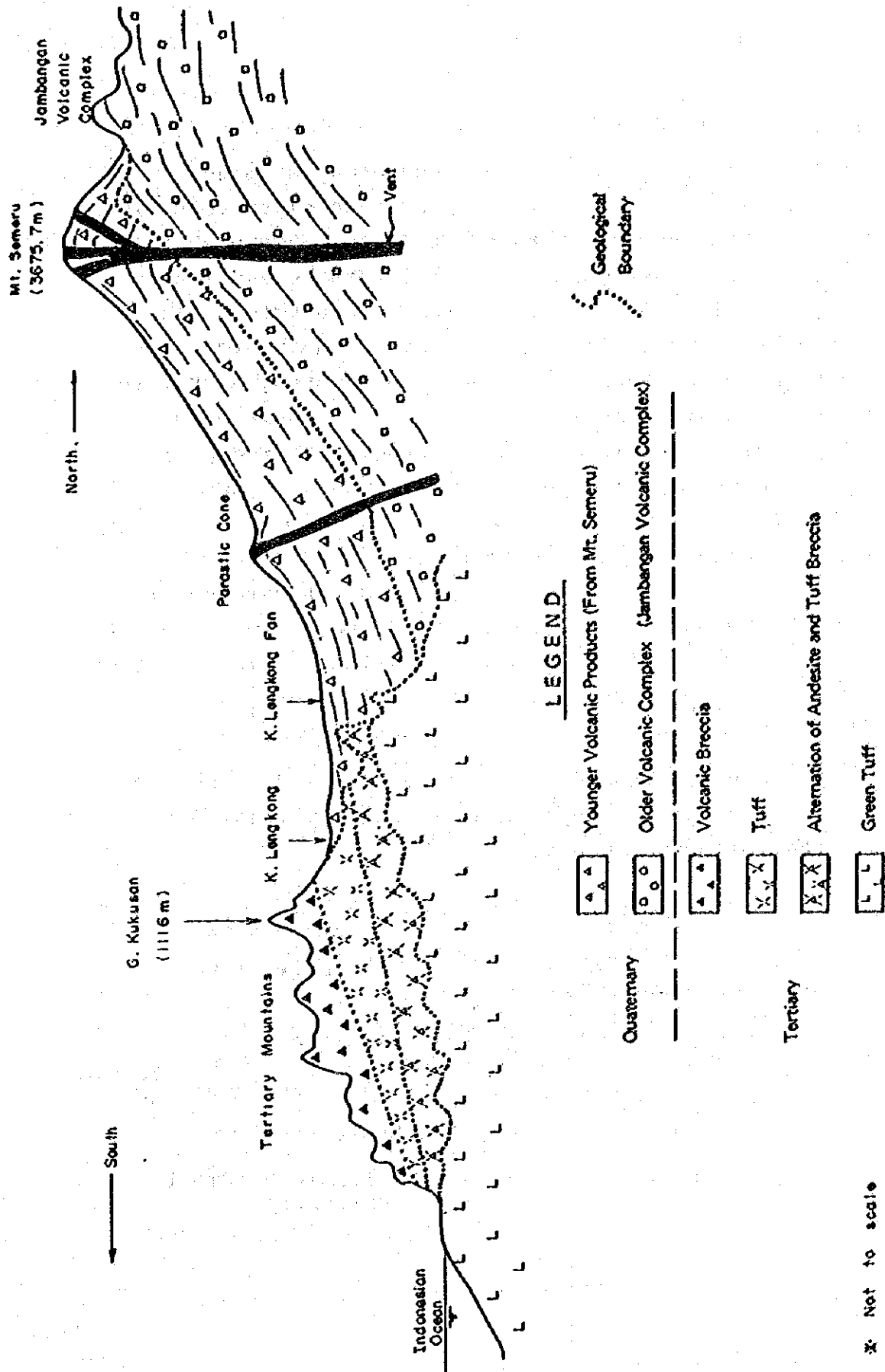


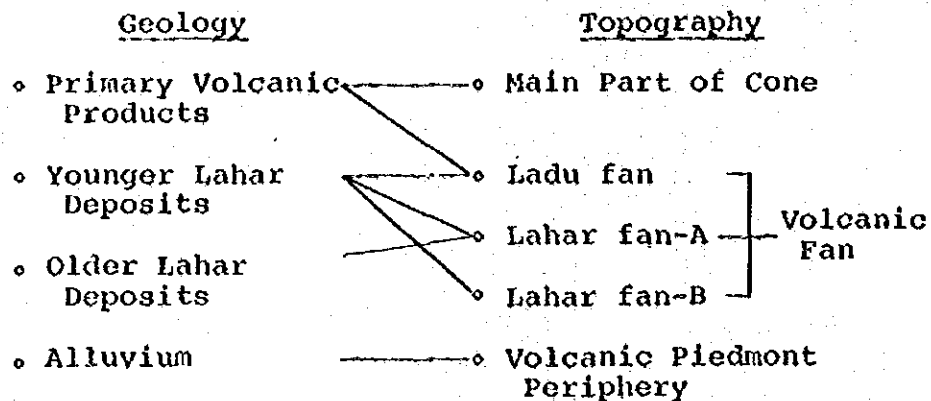
Fig- 1.4 Schematic Geological Profile of the Study Area

## ii) Quaternary System

Quaternary system of the study area is largely classified from lower to upper into older volcanic products of Tengger Mountain Range, Jambangan volcanic complex, younger volcanic products which is presently being supplied from Semeru Volcano and alluvium which is being deposited in the volcanic piedmont periphery. Volcanic products from Semeru Volcano are classified according to their origin, primary volcanic products, younger Lahar deposits and older Lahar deposits.

- Older Volcanic Products
- Younger Volcanic Products
  - Older Lahar deposits
  - Younger Lahar deposits
  - Primary volcanic ejecta
- Alluvium

The distribution of volcanic products from Semeru Volcano and its topography is closely related in the following manner.



## (2) Geological Structure

### i) Geological Structure of Tertiary System

Green tuff, layers at the bottom of Tertiary system in the study area repeat foldings and are dissected by faults at many places, showing a very complicated geological structure due to the intrusion of granite batholith in the middle Miocene period.

Limestone is only distributed in a very narrow sphere near the estuary of K. Glidik and its bedding plane is generally horizontal with caves developing along the bedding plane.

Alternation of andesite/volcanic breccia, tuff layer and tuff breccia layer, are presumed to be continuously superposed without long hiatus covering discordantly green tuff layer of underneath. Small folds are observed in these layers and they gently slope towards south (toward Indonesian Ocean). Faults are rarely observed in these layers.

### ii) Geological Structure of Quaternary System

Older and younger volcanic products of Quaternary period are thickly distributed on a series of large depression zones called Solo Zone. In those volcanic products, folds and faults by crustal movements are not observed, but small folds and faults due to compaction settlement are partially observed.

Although the internal structure of stratovolcano is not generally well known, a schematic profile of Semeru volcano will be presumed as shown in Fig.-1.5. Its bedding plane of volcanic products is considered to be roughly parallel with the present slope of volcano.

On the ring at EL. 1,500 m around Semeru volcano, several parasitic volcanoes are lined up where a circular fault is presumed to exist.

From the macroscopic viewpoint of a series of Tengger - Semeru volcanoes, it is presumed that a large transverse fault zone runs cutting across Java Island along Tengger - Semeru volcanic row extending in N-S direction.

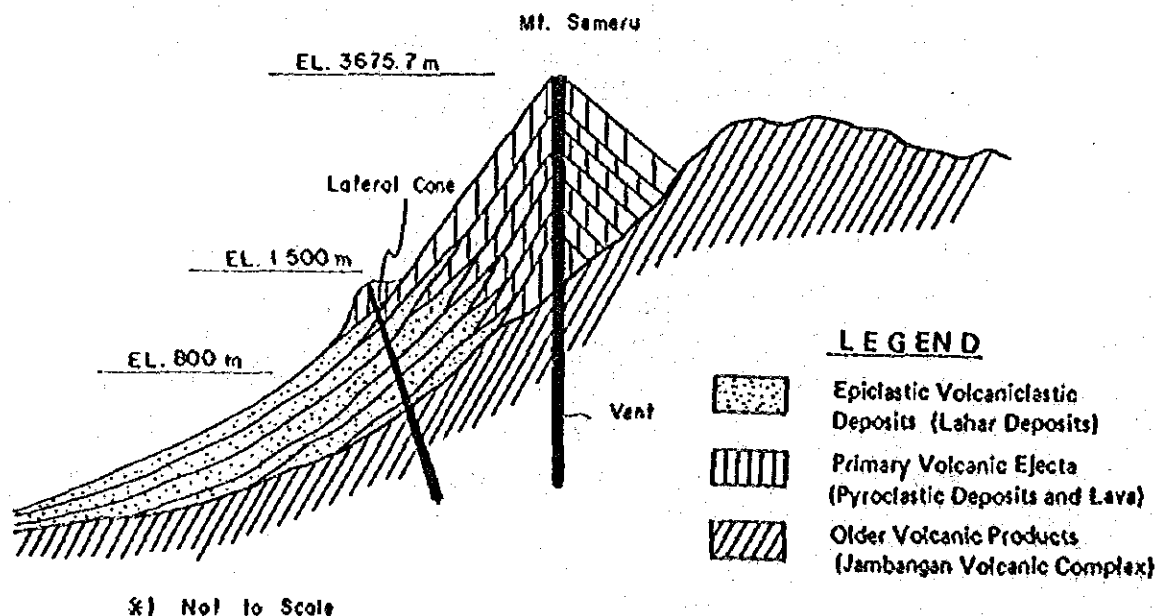


Fig.- 1.5 Schematic Structural Profile of Mt. Semeru



## 1.4.3 LAND USE

The present conditions of land use inside the study area as agricultural purpose are noticeably compatible with its topographical conditions. Conceptual relationships between topography and land use are given in Table-1.3.

Table - 1.3 Conceptual Relationships of Topography and Land use

Topography			Land use
Main part of volcanic cone	2500m and over		Bare soil
	2500m and under		Forest (natural)
Ladu Fan			Forest (natural/artificial), Dry field (mainly sugarcane), Cloves, Coffee.
Lahar Fan	Steep Slope	B. Sat Fan	Rice paddy (single- and double-harvesting), Dry field
		B. Semut fan	Wasteland, Artificial forest, Rice paddy (single- and double-harvesting) Dry field, Cloves
		K. Rejali fan	Rice paddy (double-harvesting), Wasteland
		K. Lengkong fan	Wasteland
		K. Poh fan (old fan)	Stable rice paddy (double-harvesting), Tobacco, Corn
	Gentle-slope		Rice paddy (double-harvesting); half of B. sat fan, dry field.
Volcanic Periphery			Dry field (considerable area of land where planting during dry season is not possible)
Alluvial plain			Rice paddy (double-harvesting)
Tertiary mountains			Forest (natural/artificial), Coffee, Cloves, Cassava
Old volcanic piedmont	Pronojiwo		Coffee, Dry field
	Left bank of B. Sat and K. Lateng		Coffee, Dry field, Rice paddy (single-harvesting)

## 2. GROUNDWATER INVESTIGATION

### 2.1 GENERAL

The in-situ investigation of groundwater level consists of;

- Field reconnaissance
- Continuous observation of groundwater level in long period at 17 wells with installation of automatic water level gauge.
- Regular measurement of water level in borehole in K. Lengkong fan, using potable water level gauge.
- Quasi-simultaneous measurement of groundwater level in K. Lengkong basin, using potable water level gauge.

In this Chapter, the study will be carried out, based on the results of continuous groundwater level observation at 17 wells. This study intends to clarify some characteristics as general hydrogeology of the study area from the interpretation of data, taking account of topography, geology, land use and so on.

The work allocation of groundwater level observation for the Indonesian Government and JICA Team is as follows;

- i) Indonesian Government
  - Groundwater level observation
  - Data arrangement
- ii) JICA
  - Technical guidance relating to observation method and data arrangement
  - Data analysis and its interpretation

Detail study of groundwater will be dealt with in the chapter of "Hydrogeology of K. Lengkong Basin" (§4).