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JARAN INTERMANDINAL COOPERATION AGENCY

FEDERATIVE REPUBLIC OF BRAZIL

THE STUDY

ON

THE DISASTER PREVENTION AND RESTORATION PROJECT

IN

SERRA DO MAR, CUBATÃO REGION, STATE OF SÃO PAULO

FINAL REPORT
DATA BOOK



22068

JANUARY 1991

JAPAN INTERNATIONAL COOPERATION AGENCY



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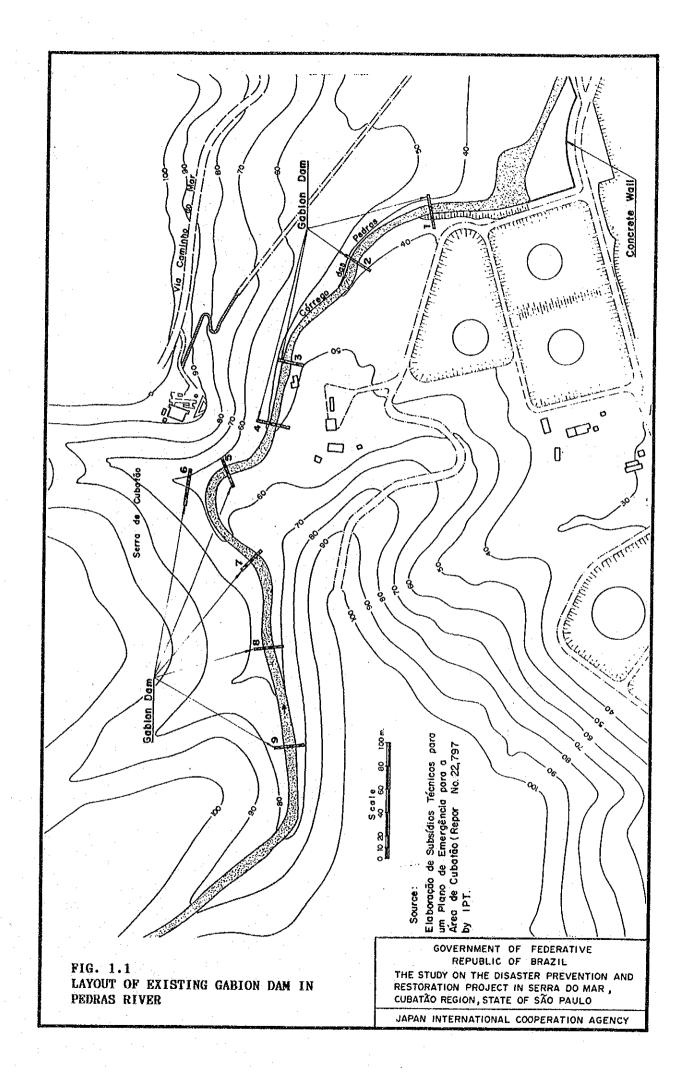
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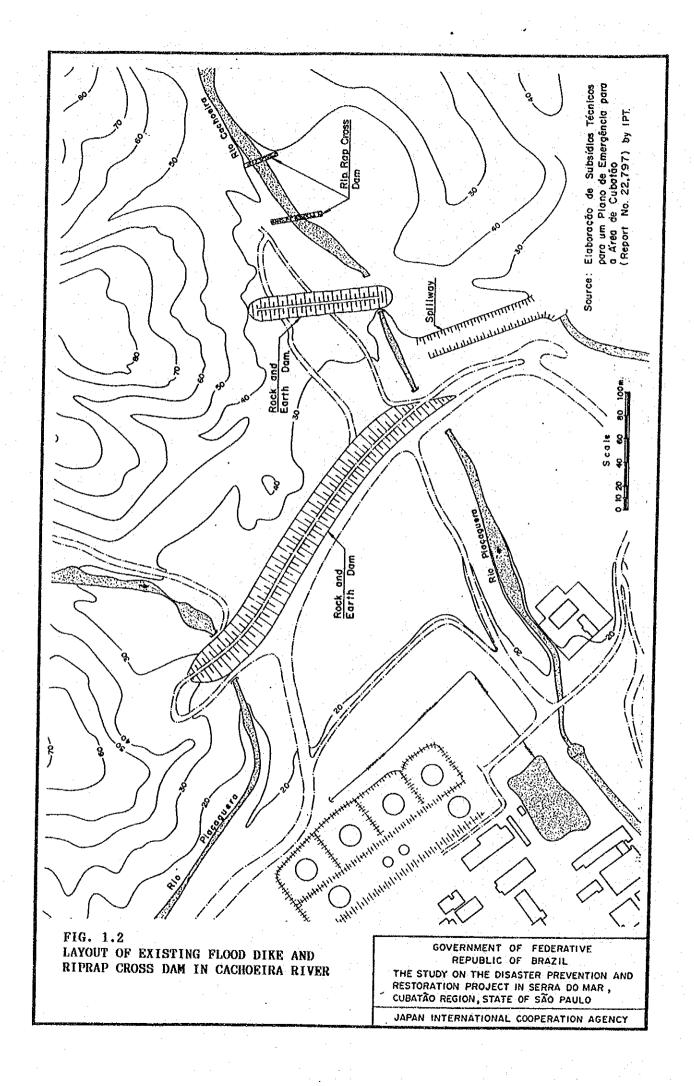
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TOPOGRAPHIC MAP FOR SABO DAM SITE





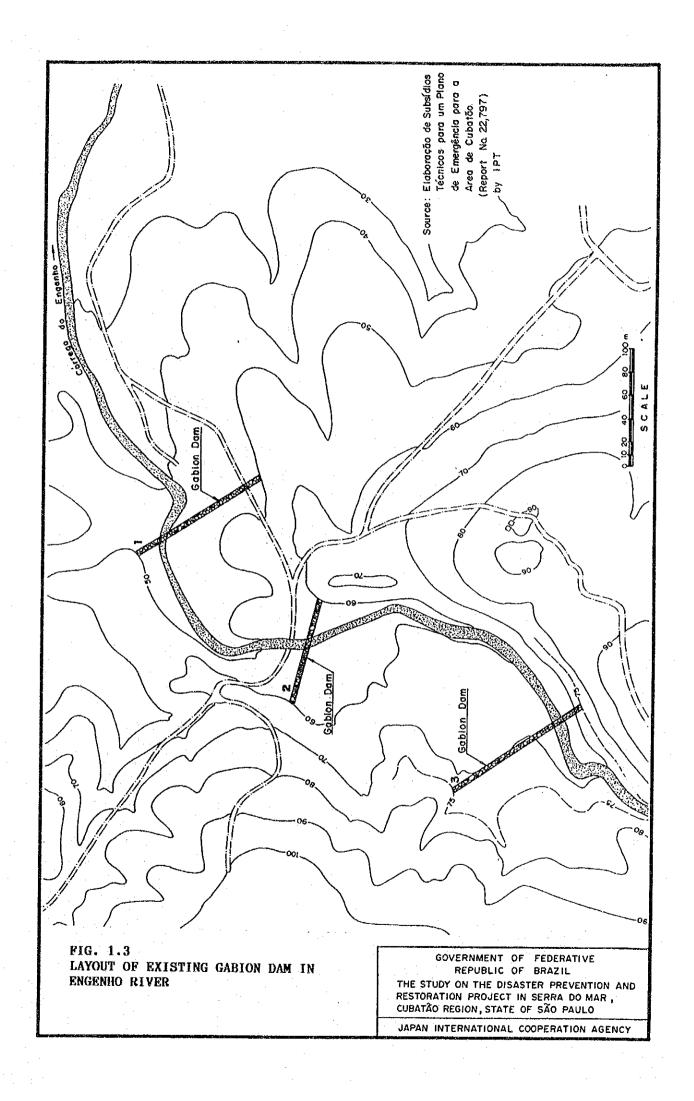


TABLE 2.1 HOURLY RAINFALL DATA OF MAJOR PAST FLOODS (1/3)

FEB	.24-25	1971 FL000) ·			JAN.20-23	.1976 FLOC	ย			
	DATE	TIME		IENRY BOR RI(mm)		DATE	TIME		- 153R RT(om)	STA.E3	-038R RT(mm)
	2.24	20	0.0			4 00	20	0.0	0.0	0.0	0.0
	2.24	21 22	7.0 2.0	7.0 9.0		1.20	21	C 0	0.0	0.0 0.0 17.6 9.9 0.5 0.7 2.1 0.7	0.0
	2.24					1.20	22	5/3 30 3	57.3 87 A	17.6	17.6
	2.24	24	0.0	9.0 9.0		1.20	24	0.7	6.88	0.5	28.0
	2.25	. 1	2.0	9.0 9.0 11.0 11.3 15.0 15.0		1.21	1	0.2	88.5	0.7	28.7
	2.25	2	0.3	11.3	*	1.21	. 2	0.2	88.7	2.1	30.8
	2.25	. 3	0.0	15.0		1.21	. J	2.4	87.1	0.7 7 k	31.5
	2,25	5	1.0	16.0		1.21	Ś	2.7	93.8	1.2	35.3
	2.25	4 5 6 7	1.0	15.0 16.0 17.0 46.0		1.21 1.21 1.21	6	1.9	95.7	0.7 2.6 1.2 3.2 1.2 3.3 2.5 4.4 1.4	38.5
	2.25	7	29.0 4.0	46.0		1.21	7	1.3	97.0	1.2	39.7
	2.25 2.25	9	40.2	90.2		1.21 1.21	. 0	21	99.1	3.3	43.0
	2.25	10	9.8	100.0		1.21	10	7.8	109.6	4,4	49.9
	2.25	11	28.0	128.0		1.21 1.21	11	0.9	110.5	1.4	51.3
	2.25	12 13	36.U	164.0 186.8	•	1.21	12	8.0	111.3	1.1	52.4
		14	9 7	194.0		1.21	14	0.0	111.3	0.0	54.4
	2.25	15	4.8	200.8		1.21	15	2.0	113.4	0.8	54.8
	2.25	16	6.2	200.8 207.0 213.0 216.0		1.21	16	10.2	123.6	1.1 0.0 1.5 0.8 2.4	57.2
	2.25 2.25	5 - 17 18	0.U 0.F	213.0		1.21	17	10.2	133.8	18.1	75.3
	2.25	19	3.0	217.0		1.21	15	49.8	213.3	2.4 18.1 16.0 46.2	137.5
	2.25	20	3.0 3.0 1.0	219.0 220.0 224.0 226.0		1.21					
	2.25	21	4.0	224.0		1.21	21	22.1	271.1	6.5 3.7 9.7	162.4
	2.25	22 23 24	2.0	228.0		1.21 1.21	22	10.3	287.4 705 A	3./	166.1
	2.25	24	0.5	228.5		1.21	24	33.9	339.7	13.9	189.7
	2.26	1	5.5	234.0		1.22	. 1	24.0	363.7	27.2	216.9
	2.26	2 3	4.U 6.D	244 0		1.22	2	6.1	349.8	11.3	228.2
	2.26	4	4.0	248.0	•	1.22	3	2.4	374.6	2.2	231.3
	2.24	5	1.0	249.0		1.22	5	2.5	377.1	2.8	234.3
	2.26	6	3.0	252.0 252.0		1.22	6	4.5	381.6	3.6	239.9
	2.20	20 21 22 23 24 1 2 3 4 5	U.U	252.0		1.22	7 8	2.9	384.5 384.7	3.3	243.2
Sou		TROPAULO	ال والوضوات ال		المنجية المستعدد	1.22	. 9 10	0.8	387.5 388.2	9.7 13.9 21.3 3.1 2.2 2.8 3.6 3.3 0.9 0.2 0.1	244.6
						1.22	11	1.3	389.5	0.1	244.9
				. •		1.22	12	1.2	390.7	0.1	245.0
JAL	N. 16-17	1973 FLOC	מו		6	1.22 1.22	14	1.9	393.0	3.1	247.1 250.2
			STA.E3	- 153R		1.22	15	2.5	395.5	<u>Z</u> .4	252.6
	DATE	TIME				1.22 1.22	16 17	1.1 4.6	. 396.6 401.2	0.1 2.1 3.1 2.4 3.6 7.0 2.4	256.2 263.2
	1.16		9.3	9.3		1.22 1.22	18 19	6.1	407.3	7.0 2.4 1.1 0.1	265.6
	1.16	9	25.2	34.5		1.22	20	0.6	407.9	0.1	266.7
	1.16	10 11 12 13	20.3	54.8 71.5 90.0		1.22	21	1.9	410.4	2.6	269.4
	1.16	12	18.5	90.0		1.22	22	2.0	412.4	2.6 1.6 0.8	271.0
			15.0	105.0		1.22 1.22	23 24	0.7	413.1	1.3	271.6 ° 273.1
	1.16	. 14	6.6	111.6		1.23	1	1.4	415.3	0.7.	273.8
	1.16 1.16	15 16	2.3 1.1	113.9 115.0		1.23	. 2	1.3	416.6	2.0	275.8
	1.16	17	0.6	115.6		1.23	. 3	1.9	418.5	0.8	276.6
	1.16	18	3.8	119.4		1.23 1.23	4 5	7.7 3.3	426.2 429.5	2.6 0.5	279.2 279.7
	1.16 1.16	19 20	0.5	119.9	* .	1.23	4		429 9	1.2-	280 9
	1.16		7.4 8.7	127.3 136.0		1.23	. 7	1.3	431.2	1.2	242.1
	1.14	22	1.9	137.9							
	1.16	23	6.2	144.1							
	1.16	24 1	2.3 0.0	146.4 146.4			C		11734777		
	1.17	2	1.0	147.4			2001	e;CTH	NUAFE	•	
	1.17	3	2.0	149.4							
	1.17 1.17	4 5	0.9 2,2	150.3 152.5							
	1.17	6	4.0	156.5							
	1.17	7	3.2	159.7							•

TABLE 2.1 HOURLY RAINFALL DATA OF MAJOR PAST FLOODS (2/3)

. MAL.	. 27-29 j)	1976 FL00						NOV.8-11.1	979 FL000				
	DATE	TIME	STA.E3- R(mm)	153R RT(mm)	STA.E3 R(mm)	-038R RT(mm)	-	DATE	TIME	STA.E3 R(mm)	REGI- RT(mm)	STA.E3 R(mm)	-038R RT(mm)
	1.27	12	14.7	14,7			ij.	11.08	20	0.0	0.0	0.0	0.0
	1.27	13	17,0	31.7			2	11.08	21	7.6	7.6	2.5	2.5
	1.27 ·	14	13.6	45.3		. :	1,	11.08	22	4.4	12.0	0.8	3.3
	1.27	15	0.0	45.3		•		11.08	23	1.0	13.0	1.4	4.7
	1.27	16	7.5	52.8				11.08 11.09	24 1	2.4 1.0	15.4	0.4	5.1
	1.27	17 18	8.8	61.6				11.09	2	1.5	16.4 17.9	2.0	7.1
	1.27	10	0.1	64. 4 64.5				11.07	3	2.4	20.3	2.9 0.5	10.0 10.5
	1.27	20	0.1	64.6				11.09	4	2.0	22.3	3.8	14.3
	1.27	21	0.0	64.6				11.09	5	3.8	26.1	5.1	19.4
	1.27	22	0.1	64.7				11.09	6	5.1	31.2	1.0	20.4
	1.27	23	0.1	64.8				11.09	7	6.6	37.8	6.6	27.C
	1.27	. 24	. 0.5	45.3				11.09	8	2.9	40.7	2.8	29.8
	1.28	1	0.1	65.4	-			11.09	9	2.6	43.3	10.5	40.3
	1.28	2	4.9	70.3				11.09	10	7.7	51.0		50.4
	1.28	3	0.0	70.3		•		11.09	11	6.9	57.9	8.0	58.4
	1.28	4 5	0,3	70.6				11.09	12	8.5	66.4	4.2	62.6
	1.28	6	2.9	73.5 74.0				11.09 11.09	13 14	9.8 8.1	76.2 84.3	5.2	67.8
	1.28	7	0.1	74.1				11.07	15	6.3	90.6	8 8 5 4	76.6 82.0
	1.28	á	1.9	76.0	0.7	0.7		11.09	16	5.8	96.4	3.4	85.4
	1.28	ç	10.2	86.2	1.6	2.3		11.09	17	8.3	104.7	3.0	88.4
	1.28	10		95.8	4.0	6.3		11.09	18	6.4	111.1	4.9	93.3
	1.28	11		102.5	13.0	19.3		11.09	19	6.5	117.6	3.3	96.6
	1.28	12	26.4	128.9	35.9	55.2		11.09	20	7.3	124.9	2.9	99.5
	1.28	. 13	27.2	156.1	17.4	72.6		11.09	21	8.3	133.2	2.1	101.6
	1.28	14 '		166.3	13.7	86.3		11.09	22	7.3	140.5	1.4	103.0
	1,28	15	18.9	185,2	24.9	111.2		11.09	23	9.2	149.7	1.5	104.5
	1.28	16	15.8	201.0	.19.3	130.5		11.09 11.10	24 1	7.5 9.9	157.2	4.1	3.801
	1.28	17	16.2	217.2	11.8	142.3		11.10	2	82.	167.1 · 175.3	2 & 2 0	111.2 113.2
	1.28	18	4.1	221.3	6.6	148.9 151.7		11.10	3.	6.0	181.3	3.1	116.3
	1.28	19 20	14.6 3.0	235.9 238.9	2.8 4.1			11.10	4	6.7		3.2	119.5
	1.28	21	2.7	241.6	14.5	170.3		11.10	5	5.4	193.4	4.2	123.7
	1.28	22	14.6	256.2	4.7	175.0		11.10	6	6.7	200.1	4.0	127.7
	1.28	23	16.6	272.8	5.6	180.6	•	11.10	7	5.8	205.9	1.6	129.5
	1.28	24	31.4	304.2	7.7	188.3		11.10	8	7.5	213.4	2.5	132.0
	1.29	1	7.1	311.3	6.9	195.2		11.10	9	6.2	219.6	3.3	135.3
	1.29	2	4.0	315.3		195.7		11.10	10	10.2	229.8	7.8	143.1
	1.29	3	47.8	363.1	15.3	211.0		11.10	11	10.7	240.5	7.3	150 4
	1.29	4	6.3	369.4	3.9	214.9		11.10 11.10	12 13	13.0 11.2	253.5 264.7	5.9	156.3
	1.29	5	7.0	376.4	31.3	24á.Z		11.10	14	9.3	274.0	ፊ.8 8.0	163.1 171.1
	1.29	6 7	13.7 10.8	390.1 400.9	2.5	248.7 250.9		11.10	15	9.3	283.3	9.7	180.8
	1.29	é	10.6	400.7	0.2	251.1		11.10	16	8.7	292.0	6.2	187.0
	1.27	9		400.9	6.1	257.2		11.10	17	7.3	299.3	10.0	197.0
	1.29	10		400.9	1.0	256.2		11.10	18	9.7	309.0	8.5	205.5
	1.29	11	:	400.9	0.5	258.7		11.10	19	6.9	315.9	4.8 0.3	210.3
	1.29	12	•	400.9	0.5			11.10	20	3.6	319.S		210.6
•	1.29	13		400.9	0.2	259.4		11.10	21	3.8	323.3	3.5	214.1
	1.29	14		400.9	0.7	260.1		11.10	22 23	4.4	327.7	2.2	216.3
	1.29	15		400.9	28.7	288.8		11.10 11.10	24	2.2 6.0	. 329 . 9 335 . 9	2.4	218.7
	1:29	16		400.9	3.7	292.5		11.11	1		339.8	3.2 2.1	221.9 224.0
	1.29	17		400.9	2.9	295.4		11.11	2	3.9	343.7	4.9	224.0
	1.29	18 19		400.9 400.9	2.3 0.0	297.7 297.7		11.11	3	2.9	346.6	0.7	229.6
	1.47	17		700,7	U.U	67/./		11.11	ភី	0.0	346.6	0.0	229.6
						. ,	-	. 11. 11	5	0.0	346.6	3.4	233.0
								11.11	. 6	0.5	347.1	2.3	235.3
								11.11	7	1.7	348.8	0.7	234.0
								11.11	8	4.3	353.1		
-		- *						11.11	· 9	0.9	354.0	•	
								11.11 11.11	10 11	0.9 0.3	354.9		
								11-11	t I	υ. ⊅	355.2		

Source; CTH/DAEE

TABLE 2.1 HOURLY RAINFALL DATA OF MAJOR PAST FLOODS (3/3)

FEB	1-2.1	983 FLOOD	STA.E3	10.30	**************************************	 3-038R	DEC.20-22,					*****
	DATE	TIME	R(mm)	RT(mm)	R(mm)		DATE	TIME	STA.E3- R(mm)		STA.E3- R(mm)	
	2.01 2.01 2.01 2.01 2.01 2.01 2.01 2.01	18 19 20 21 22 23 24	9.4 2.3 7.3 0.8 4.6 24.7 20.3 18.2 8.6 6.5 3.6	4.3 20.3 29.7 32.0 39.3 40.1 44.7 69.4 89.7 107.9			12.20 12.20 12.20 12.20 12.20 12.20 12.20 12.20 12.21 12.21 12.21 12.21 12.21 12.21 12.21 12.21 12.21 12.21 12.21	16 17 18 19 20 21 22 23 24 1 2 3 4 5 6 7	1.3 0.0 8.5 11.3 16.9 5.2 1.3 29.1	1.6 2.9 2.9 11.4 22.7 39.6 44.8 45.1 75.2 84.4	10.0 5.0 28.5 26.5 15.6 7.0 2.3 6.0	11.1 21.1 25.1 54.6 81.1 96.7 103.7 106.0
JAN S	15 54 ·	1985 FLOOI	.			٠,	12.21 12.21 12.21 12.21	10 11 12 13	4.0 8.8 6.8	137.8 141.8 150.6 157.4	0.8	152.1
	DATE	TIME	STA.E3- R(mm)	RI(mm)	5TA.E3- R(mm)	038R RI(mm)	12.21 12.21 12.21 12.21 12.21 12.21 12.21 12.21 12.21 12.21 12.21	15 16 17	2.2 4.0 5.6	161.5 165.5 171.1	•	
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A,B;Constants N ;Number of samples

;Correlation coefficients

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TABLE 2.2 CORRELATION COEFFICIENT OF 1-DAY RAINFALL	
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TABLE 2.2 CORRELATION COEFFICIENT OF 1-DAY RAINFALL BETWEEN STATIONS (2/2)

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:		E3-236R E3-153R	E3-037	F3-241	E3-149R	E3-143	E3-109	E3-144		E3-153R	E3-236F	E3-109	E3-038R	E3-149R	E3-101	E3-037	# - T - C 2		E3-236R	E3-241	E3-11-07	F3-143	E3-101	E3-037	E3-144	E3-038R		E3-037	E3-109	E3-1538	F3-241	E3-236R	E3-143	23-038R	1111	, , , , , , , , , , , , , , , , , , ,	E3-149R	E3-038R	53-133K	E3-241	E3-101	E3-109	E3-143	161161
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R ;Correlation coefficients
A,B;Constants
N ;Number of samples

TABLE 2.3 CORRELATION COEFFICIENT OF 2-DAY RAINFALL BETWEEN STATIONS (1/3)

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TABLE 2.3 CORRELATION COEFFICIENT OF 2-DAY RAINFALL BETWEEN STATIONS (2/3)

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TABLE 2.3 CORRELATION COEFFICIENT OF 2-DAY BAINFALL BETWEEN STATIONS (3/3)

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Z		76	60	63	80	72	61	81	000	25		26	154	121	174	117	, C	10	7.7	271) - -
m .		7.66	8.56	23.63	15.87	13.66	7.64	6.79	23.25	59.88		40.37	51.08	58.05	62.07	24.19	39.53	31.80	73.01	02.75	,
द		0.8629 X +	0.8237 X +	0.7276 X -	0.7191 X +	0.7365 X +	0.5465 X +	0.5710 X +	0.4828 X +	0.3952 X +	* * *	0.7222 X +	0.5265 X +	0.5838 X +	0.6025 X +	0.5574 X +	0.4712 X +	0.5130 X +	0.5620 X +	0.4321 X +	
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œ		0.789	0.652	0.652	0.647	0.615	0.534	0.527	0.527	0.250		0.789	0.533	0.523	0.518	0.512	0.489	0.472	997-0	0.385	1
×		E3-037	E3-101	E3-153R	E3~109	E3-038R	E3-236R	E3-143	E3-241	E3-144		E3-149R	E3-109	E3-101	E3-038R	E3-153R	E3-241	E3-236R	E3-144	E3-143	
		10	5	m	∞	v	41	ณ	۲,	4		0	ထ	ហ	40	m	7	₽4	4	۲۷	
	%≡ 81										N=184										
>-	E3-149R										E3-037	-									
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Source; CTM/DAEE

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10 £3-037	50.80	25.40	50.80	40.60	10.20	109.20	81.20	38.10	180.30	7.60		15.20	40.50	20.7	00.00	00.00	101 00	20.444	200	40.50	3	38.10	5.10	86.40	111.80	17.80	124,50	20.55	115 00	53.30		35.60	101.00	254.00	25.40	17.80	215.90	86.40	63.50	25.40	17.80	25.40	06.03	147.20	25.40	00 70	66.00	76.20	35.60	78.70
9 E3-149R			,1	ı	1	1			4	1	-		ı	1		۱ ۱	: 1	ı					ť	1	1	1	.	1 .	r !	• •		1				1	1	ı	1	ı		1	ı t	1			1	,	1	E .
8 E3-109	(63.59)	50.29	63.59)	(58.25)	(42.33)	(94.18)	(79.52)	56.94)	(131.42)	(40.97)		44.95)	36.43)	40.97	(61.071)	100.00	100.00	(00.000)	(80.08)	(88.25)	,	(56.94)	(39.66)	(82.24)	95.54)	46.31)	(102.19)	(17.50)	(21. 80)	(64.90)		55.63)	79.57)	(170.02)	50.29	(46.31)	(90.06)	154.70	38.00	.50	58.80	50.29)	7.50	200	32.00	124.00	15.40	20.50	213.50	63.80
7 E3-241	t	.1	ı	,	•	1	1		ı	t			•	1 1		: 1	1			•		1	ı	ı	i	İ				1		i I	i 1	1	ŧ	1	1	ı	1			1	•		į	1	ı	1	ŧ	l
5 E3-038R	203.20	139.70	114.30	86.40	101.60	101.60	198.10	43.10	152.40	35.60		02.01	00.00	114 30	20.41	137.20	137.20	20.40	121.90	10.20		210.80	58.40	223.50	134.60	.05.02	106.70		25.50	76.20		94.10	94.00	246.40	10.20	5.10	241.30	109.20	30.50	45.70	99.10	12.70	111.80	114.30	25.40	94.00	30.50	106.70	254.00	58.40
5 E3-101	•	1	•	,	t	1	1		ı	1		1 ;				i	1	1	ı	•		1	ı	•	ı	ŧ	1	· i		ı		} 1	•	1	•	•	ι		,	ł	ι	1	•	94.00	24.00	106.00	14.00	1	, ;	60.00
4 E3-144	ı	ı	1	1	:	1	1	ı		;		• 1			١	1	1	ı	1			ì	1		1		1 i			•		; I	1	1	•		•	1	ł		t	•	•		1	1	1	•		ı
3 E3-153R	(198.88)	(148.95)	(128.98)	(107.04)	(8.81)	118.99)	194.87)	72.99)	158.94)	(60.10	10.00	93 04)	100.001	128.98)	131.02)	146.98)	146.98)	55,14)	134.95)	47.12)		204.86)	85.02)	214.85)	144.94)	123.00	104 90)	103,033	89.03)	99.02)	i d	75.03)	113.01)	232.85)	47.12)	43.11)	228.84	(10.2CX	20.00	38.07)	81.98)	49.08)	44.23)	120.44)	60.68)	130.69)	52.15)	53.79)	195.85)	91.42)
2 E3-143	,	ı	1	1	.•	i	1	1		f		1 1	. 1	: 1		ı	ı	1	ŧ	ı			1	;		1	; (1		,		1 1		. 1	1	1	1	1	,		,	1	1	,	ı	1	,	1	1	
1 E3-236R	•	ł	•	ı	i	1	ı	i) ;	ŧ	į	1 1	i	. 1		1	3		1	1		•	ı	•				,	•	•		1 1	ı	1	1	1		i 1	ì	ı		1			1	r		1	ı	
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	10 E3-037	127.00	5.10	144,32)	218.40	38.10	88 90	50.80	00.	00.	71.10	172.70	00.	8	60.90	25.40	9.8	3	7.60	38	68.60	50.80	127.00	10.20	55.90	00	40.60	50.80	106.70	25.40	25.40	203.90	162.50	38.10		00.	45.70	20.30	20.10	127.00	12.70	55.90	2.50
	9 E3-149R	٠,١		1	•	1 1		ŧ	1	!	•) j	·	ı	1	ŧ			1	()	ı	1	ł			ı		1	ı	1 1	ı i	ı	ı			1	ŀ	1	ı i	i	•	t	1 1
(MM)	8 E3-109	77.30	125.60	207.60	120.90	06.19	22.80	40.20	90.00	9.30	00.	2	37.80	84.30	8	82.00	7.90		125 90	11.40	80.00	140.10	5	120.30	50.30	.10	8.30	40.60	134.82)	54.92	27.43)	149.68)	31.53)	21.26)		36.81)	142.70	55.00	18.48)	130.00	23.50	124.50	143.00
8)	7 E3-241	•		1	•	1 1	ı	1	ı	ì	1 . !	۱ ۱	1	ı	ı	٤.	1 1		1 1	ŧ	ı	1	ţ '		ı	•	ı	1	1	. 1	1	ı	ı		•	· ·		. 1	1	. 1	ı	1 1	1
IONS (2/8	6 E3~038R	152.40	127.00	200.70	299.70	101.60	132.10	35.60	90.	.00	88.90	25.40	00.	80.	61.00	132.10	139.70	6	101	00.	48.30	51.80	102.40	134.60	27.90	50.80	15.70	00.	127.00	127.00	7.60	127.00	38.10	45.70	6	50.80	7.60	127.00	50.80	228.60	25.40	203.20	12.70
DATA OF STATIONS	5 E3-101			1	1 1	: !	ŧ	1	ı	1		ı	,	1		1 1	ı		1 1	1	ı	ı	. 1	ı	1	•	•	ı	1 (1	ł			l i		ı	1 1	1	1	1	1	. 1	1
LL DATA	4 E3-144		ı ı				, t		l	•	1 1	1	ı	1			9.00	44 90	0 1	1	26.00	80.00	8.40	: 1	43.60	8	.50	22.40	3.00	8.1	47.00	7.00	160.00 0.00	23.00	i i	27.50	5.20	64.00	.60	90.	30.00	18.50	35.60
1-DAY RAINFA	3 E3-153R	95.60)	131.15)	191.51)	127.69)	100.90)	55.49)	68.29)	201	45.55)	42.02)	38.70)	66.53)	100,75)	86.96)	17.94	41.04)	25. 641	104.97)	21.60)	97.17)	146.44)	22.65)	145.11)	31.42)	62.03)	105.16)	133.17)	33.34)	80.90)	21.21)	219.24)	6.93)	37.30	6	32.00	5.60	62.90	2.40	116.33)	20.00	36.61)	29.78)
2.4 1-DA	2 E3-143	. 1 1	ı	<u> </u>	. 1	1	· · · · · · · · · · · · · · · · · · ·	, ,		i	1 1	· ·	1	,	01.87	6.40	30.40 (14.40 4	96.80			171.40						126.10 (33.00	00	110 00	10.50	51.80		108.60 (00.00	25.80 (18.70 (
	1 E3-236R	1 1	1	1		,	1	F 1		1	: 1	ı	1	ı	1 1		ı			1	1 (۱ ۱	1	1	ı			1 1	· •	j		1		ı	ı	, ,	ı	1	ı		: 1	ı	t
	DATE	1947 4.19								-	1949 2. 8	60	63 6		3 67	, 63	₹.	7	(J)	un (n o	1950 12, 4	2	7	122	2	1951 10.18													953 2 1.24			
	×	51 1									3 23											76 19					81 15								2**	•	~-	,; ·		97 19	' ,	-	-

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•					•												1.									.:	.*	٠								•	/;estima	corre				Source	
	10 E3-037	83.80	66,10	50.80	103.34)	. 05 . 05 . 05	45.70	58.40	2	104.10	22.30	33.00	86.40	73.70	33.00	60.20	10.20		210.80	38.10	22.90	58.40	12.70	182,90	61.00	172.70	25.40	.00	8	.00	25.40	86.40	12.70	152.40	121.00	76.20	25.40	2.50	25.40	66.00	25.40	76.20	99.10
	9 E3-149R	1	1 1	ŀ	;	1 1	1	1 (1		I	1		•)				•	, ı		ŧ	1	i i	: :	1		. •	1				•	1 1		. •	ı	1.1	. ,I	•	! !		ı
(WW)	8 E3-109	90.40	145.70	132.80	110.10	60.40	120.30	45.20		40.30	146.50	22.10	52.50	68.90	156.80	86.30	16.20	•	90.30	100.50	46.30	70.20	42.80	154.00	102.00	80.30	12.90	3.20	42.50	180.90	14.60	121.90	97.20	36.90		42.30	28.20	115.70	36.20	35.60	76.50	95.40	33.0
(3/8)	7 E3-241	F	F I	1		1 1	ŀ	† 1		t	l i	ı	1	1	! 1		ı		t (L - 1	1	i 1	1 i	· •	1		•		i .	1 1	1	i .	1	i i		1	1 :) 1	ı	, ,	ı		
STATIONS (6 E3-038R	165,10	111.80	38.10	134.60	73.60	55.90	65.50		114.30	221.00	27.90	81.30	104.20	203.20	27.50	30.50		142.30	40.70	17.80	94.00	52.10	175.30	152.40	104.10	15.30	32.07)	87.84)	63.50	15.30	86.40	53.30	144.80		109.20	12.70	78.70	12.70	28.40	17.70	66.00	· · · · · · · · · · · · · · · · · · ·
OF	5 E3-101	1	, ,	ı		1	•	40.00		8	197,40	15.90	107.20	96.90	101.50	91.20	10.00	;	7. 54 50 50	39.70	12.00	60.00	30.00	167.50	102.80	180.40	74.30	28.80	6	39.60	.20	35.80	i i	F F		97.30	29.80	3	6.30	21.80	45.20	90.60	,
FALL DATA	4 E3-144	72.80	44.60	11.80	15.10	83.40	1	1 1	;	3.00	•	•	;	1	1 1		5.10		72 00	101.00	24.00	78.80	135.50	52.50	200.00	28.20	22.60			10.20		•	233.50	36.50		•	14 20	73.17	64.60	53.10	1	100.40	
-DAY RAIN	3 E3-153R							98.40		(11.78)												105.80					27.50	(11.78)	135.20	224.20	19.20	203.90	220.30	150.20		124.50	29 20	193.70	131.20	137.70	131.30	133.10	† • • • •
2.4 1	2 E3-143	182.20	151.80	69.30	24.40	109.50	122.00	111.80	-	45.80	153.60	12.20	61,80	45.30	162.80	5.70	3.20		27.00	101.00	11.30	112.90	121.00	123.00	165.00	134.10	21.00	00-	112.00	177.50	16.60	161.20	00.00	126.70		24.00	51.30	108.90	105.50	101.50	ı	110.20	:
TABLE	1 E3-236R									1 1												1 1	٠							•													
	DATE	1953 12	1954 4	1954	1954 5	1929	1955	1955		1955 5.6	1956	1956 3	929	1956	1956 3	1956 3	1956 11	1056	1957	1957	1957	1957 12. 7	1957	1958	1958	200	1958 4.14	929	958	1958 12.15	80 60	20 00	1959 2.15	1959 2.16		3 =	2	2	_ =	1960 10.27	4m2 4m	~ ()	
	32	101	103	104	106	107	108	110		112	113	7 T		21.	118	119	120	191	122	123	124	125	127	128	129	2	131	132	134	135	136	138	139	140		141	143	\$ C	146	147	148	150	

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					d by ion AEE
					estimated correlati ce:CTH/DA
					();estimated b correlation Source:CTH/DAEE
		• •			<u> </u>
10 E3-037	88.30 7.60 121.30 205.70 .00 228.60 190.50 120.50	182.90 20.30 20.30 15.70 12.70 35.50 40.60 2.50 45.70	60.90 15.20 43.20 12.70 76.20 132.10 51.38) 27.76) 34.63)	50.80 63.50 139.70 152.40 43.20 91.40 91.40 254.00 61.00	15.20 43.20 26.21) 40.35) 127.00 22.90 243.80 109.30 200.70
9 E3-149R			20.00		40.50
8 83-109	113.20 32.30 69.60 333.20 4.20 105.20 136.80 33.40	136.90 33.20 93.20 98.50 175.20 112.60 1132.50 13.40 13.70	91.66 95.10 48.10 16.70 93.00 93.00 91.50 81.50 58.00 4.20	196.30 182.50 161.20 235.60 38.50 38.50 273.90 245.90 140.00 23.60	119.70 13.60 12.36 31.80 219.50 21.00 66.50 68.60 79.00 62.00
7 E3-241					
6 E3-038R	119.30 2.50 121.90 147.30 5.10 96.50 96.50 38.10	86.40 20.40 7.60 129.50 45.70 45.70 10.10	66.00 25.40 58.50 7.60 170.10 50.80 12.70	142.30 76.20 127.00 177.80 40.60 88.90 55.90 198.10 20.30 76.20	30.50 105.10 10.20 33.00 81.30 27.90 96.50 50.80 58.40
5 E3-101	79.80 6.80 6.80 29.60 12.80 10.20	90.50 90.50 51.60 9.90 13.60 11.70	31.30 10.50 27.00 5.20 100.50 70.20 34.40 17.30 46.80	135.80 37.30 136.40 185.20 19.70 46.90 169.60 57.20	64.50 85.50 148.10 2.50 69.40 14.10 37.00 38.10
4 E3-144	120.30 84.70 20.00 126.10 12.20 45.00	83.30 25.00 22.00 20.00 43.20 34.80 8.70 2.40 13.50	77.00 23.30 8.60 155.50 125.50 57.20 71.30	140.60 60.10 130.10 189.30 21.50 55.00 216.70 129.30 19.30	53.60 45.00 7.90 7.90 80.00 80.00 50.00 50.80
3 E3-153R	15.60 111.70 277.30 3.10 121.90 114.30 27.80 38.90 93.20	132.50 23.40 34.30 64.50 100.90 105.50 47.10 8.50	35.50 12.00 24.20 84.60 156.40 157.20 88.50 3.00	165.00 75.00 100.00 83.00 85.00 230.00 129.00 48.60 32.80	61.00 60.00 148.00 2.50 151.00 12.90 52.40 78.60 142.70
2 E3-143	153.20 15.90 143.70 94.30 31.70 24.90 83.40	108.50 24.50 60.50 3.00 51.00 44.50 19.60 8.50	35.50 12.00 24.20 84.60 150.00 140.00 70.00 46.00	150.00 72.00 51.00 210.00 23.00 64.00 61.00 22.60 81.00	61.00 60.00 10.00 23.00 54.00 13.00 45.00 63.00 62.00
1 E3-236R				1 7 1 1 1 1 1 1 1 1 1	
	22 23 23 23 24 25 25 25 25 25 25 25 25 25 25 25 25 25	22 24 24 24 25 24 25 24 25 24 25 25 25 25 25 25 25 25 25 25 25 25 25	22336533687	110 23 23 110 110 110	117 118 129 129 129 129 129
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Ď,	1961 1961 1961 1961 1961 1962 1962 1962	1962 1962 1963 1963 1963 1963 1963 1964 1964	1964 1964 1964 1965 1965 1965 1965 1965	1966 1966 1966 1966 1966 1966 1967 1967	1967 1967 1967 1968 1968 1968 1968 1968
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(WW)

TABLE 2.4 1-DAY RAINFALL DATA OF STATIONS (4/8)

(MM)

TABLE 2.4 1-DAY RAINFALL DATA OF STATIONS (5/8)

																																											υ	correlation						Source; CTH/DAEE
10 E3-037		111.80	01.10	200	33,00	81.30	66.00	17.80	147.30	195.60		9.6	83.80	200	20.20	20.01	5	20.00	15.30	45.70	•	15.30	23.70	21.30	83.50	82.80	90.	02.50	46.00	47.20		41.90	31.00	158.80	30.67	36	00.711	58.80	11.50	68.20		9.40	177.00	24.80	51.90	10.70	20.00	20.40	104.90	37.00
9 E3-149R	ç	32.30	200	17.00	34.30	56.10	ı. E	•	00.	90.20	4	05.00	10.50	20.00	00.00	22.20	21.50	80.30	09.6	30.30		44.50	10.40	104.70	02.50	0 20	2	54.30	38,30	89.00		7.60	65.10	139.40	00.00		79.00	9.30	6.50	78.90	1	5.50	09.78	02.21	1.00	26. 41	200	26.10	101.30	53.50
8 £3-109	72 60	150.30	47.20	31,40	28.70	248,60	124.30	29.50	55.70	58.40	200	00.00	121 40	17.40	220.70	9 4	58.70	58.30	70.60	14.40	:	42.40	1,40	02.	70.50	25.50	9	109.80	214.70	86.90		48.10	136.90	02.022	04.167	3.80	169.90	33.80	12.10	92.70		00.00	00.0	200.00	26.95	33.20	34.20	12.30	97.20	27.50
7 E3-241		1	ı	1	ı	i	ı	1	1			1		,		ı	•	1	;	1			ŧ		1 (66.00	204.40	73.20		15.50	206.40	96. 20	15.00	13,90	146.90	92.30	19.50	103.50		20.0	20. 70	2.7.	30.	61.80	92.80	88.60	125.80	93.90
6 E3-038R	58.40	38,10	12.70	88.90	30.50	111.80	66.00	5.10	124.40	192.40	2.50	2 20	61.00	47.50	167 951	111.00	80.00	18.50	68.00	50.80		139.70	200.007	41.50	127.70	78.50	4.00	18.00	27.20	47.30		35.70	112.42)	104.60	10.80	8	92.10	67.00	3.00	127.60		144 20	13.70	52.30	17.00	32,70	45.50	46.70	89.50	157.00
5 E3-101	4.50	49,30	14.30	21.60	59.70	65.10	51.20	15.00	83.60	00.00	6.20	145.40	19.80	67.50	186.50	48.20	64.40	60.20	7.50	9.90	6	26.20	2 20	23.50	35.30	88.60	8.40	19.50	35.60	27.30	;	9.10	136.20 (82.30	3,90	00.	138.00	50.50	1.40	218.30	ġ	120.10	20.5	60.70	31.10	54.90	78.10	99.70	156.70	121.30
4. E3-144	74.80	44.30	20.00	58 00	62.40	168,10	r	:	1 1	ı	1	1	1	1	ŧ	ŧ	•	ł	t	ı	:	; (. 1	1	. 1	1	1	ı	ŧ	1		ì	1 1		ŧ	1	ŀ	ŧ	1	•	1	٠ .	ı	1	ı	1	ŧ	,	1	1
3 E3-153R	117.40	55.70	26.10	78.60	73.50	263.20	118.50	26.50	24.90	02:017	19.10	204.60	88.70	58.30	292.30	65.20	55.30	116.70	12.70	17.10	40 10	10.30	62.40	48.30	89.80	97.20	5.20	83.10	148.70	94.30		28.90	157 70	142.80	14.80	2.70	180.30	128.60	24.10	203.30	14.00	98 90	5.60	86.70	44.00	88.60	107,50	39.40	184.30	134.60
2 E3-143	117.00	42.60	33.00	71.00	88.00	290.00	210.00	34.30	180.00		9.30	100.00	166.00	100.00	227.00	50.10	65.00	112.20	13.80	15.20	44 20	09.9	60.00	45.10	86.00	105.00	8.	102.00	166,10	100.60		08.81	181.70	139.30	14.00	1.50	160.30	80.00	40.00	184.50	14.80	80.00	3.30	80.60	50.70	91.40	117.60	51.60	241.30	141.80
1 £3-236R	ī	1	ı		ı	ı		ı			•	•	1	,		•			I	t	,		•			t	1	•	í	ı		06 161	230.30	124.70	12.30	4.20	155.80	142,50	13.60	137.30	10.80	57.60	3.30	55.20	31.90	72.50	104.10	180.70	160.70	166.00
ATE									2.23										8 26		10.11	11.19	11.20	1.21	1.22	5.19	2.20	5 5	52.5		٥ د	7	1.16	1.25	1.26	, s	٠ د د	. T	0 0	16.60	12.21	1.15	1.16	12. 3	12. 4	 	~ :	<u></u>	9.19	3
DA	_	Ξ.	_		Γ.		٦,	*	1970	•		_	Ξ.	***	-	Ξ.	,	r-4 1	1971	7	1971	1971	1971	1972	1972	1972	1972	1972	19/2	7)61	1972	1973	1973	1973	1973	50.00	101	1073	1073	0 - 1 -	1973	1974	1974	1974	1974	15/2	1975	1975	1975	
26	201	202	203	204	205	200	300	0 0	210		211	212	213	214	215	216	217	27.9	617	077	221	222	223	224	225	226	227	273	920	9	231	232	233	234	232	2 5	200	300	240	ì	241	242	243	7	243	2 0	200	243	250	
																																-												٠.						

(); estimated by correlation

	10 E3-037	3.50	23.10	19.50	12.60	14.50	21.30	207.30	37	36.20	279.20	18.50	72.10	8.20	5.30	32,30	175.00	53.40	27.80	88.00	33.60	29.00	177.50	59.20	12.40	77.60	23.20	103.70	08.58	2.30	100.50	18.20	186 40	84.70	101	35.80	72.90	.40	260.00	36.00	70.50	24.90 97.00
	9 E3-149R	2.70	22.80	20.30	7.60	11.70	98.70	100.00	74.80	20.00	311,00	7.60	23.30	22.70	5.80	1	220.90	21.80	20.40	124.30	10.70	22.30	138.70	58, 10	29.90	61.80	34.80	1	łı	ı	10.00	20.00	152.20	70.90	62.00	25.30	69.60	1.90	240.20	23.20	87.70	26.20 83.80
(MM)	8 E3-109	46.50	39.80	62.80	56.30	02.02	80.00	140.40	60.30	57.50	300.00	50.40	00.40	00 95	12.20	41.06)	79.45)	78.84)	19.35)	149.30	13.80	42.80	58.50	45.20	31.20	07.67	15.10	19.40	00.15	5.10	32.10	125 70	130.00	35.00	37.00	90.40	100,60	30	120 60	17.30	109.80	28.90 44.20
(8)	7 E3-241	6.90	62.50	86,70	68.60	130.50	43.00	116.90	56.50	115.70	442.00	103.20	154.50	171 60	17.60	· ·	<u> </u>	,	1	104.80	72.00	44.90	112.00	28.50	52.10	70.00	87.60	103.60	40	2.90	65.40	121 50	117.20	49.10	42.80	35.10	147.50	1.80	243.60 43.60	; '	123.00	70.80
STATIONS (6	5 E3-0388	2.70	18.50 28.80	10.20	9 9	121.50	39.90	203.90	38.90	28.10	251.10	34 80	33.60	61.70	2.30	30.40	146.20	104.00	24.50	38.00	23.30	10.80	129.90	31.80	38.80		53.90	128 90	91.00	00.	119.30	102.30	106.50	60.10	62.00	27.10	106.70	5.40	109.10	14.60	100,30	80.30
OF STAT	5 E3-101	6.30 28.40	26.60	23,50	26.50	125.00	126.50	267.60	36.50	54.50	184.70	52,10	35.50	107.40	3.20	52.50	114,40	115.10	17.70	22.40	33.80	16.20	184.50	29.20	102.90		64.80	26.70	8	3.10	42.90	130.30	106.50	37.10	55.70	13.40	141.60	50	77.30	1.10	148.10	64.60
ALL DATA	4 E3-144	1 1		3	1 1	•	:	•	1	ı				1	ì		ş	ı	t	1)	I ‡	1	ı	1	1 1		•	! !		ı		ŀ	ì	ı		ı	ı	ı		١.		l l .
AY RAINE	3 E3-153R	18.30	104,00	125.20	87.50	186.50	104.60	304.10	50.50	76.70	351.70	125.60	67.10	178.30	14.30	51.10	145.30	146.50	22.20	123.50	124.00	51.30	221.70	08.12	78.60		138.30	53.20	91.00	00.	43.00	144.70	164.50	25.30	78.30	24.70	159.50	3.10	110.20	3.10	139.00	61.10
2.4 1-D	E3-143	16.20	104.90	144.80	67.90	242.60	130.60	730.30	52.20	79.30	354.80	114.00	57.30	185.10	20.20	50.20	763.60	117.50	22.50	132.30	131.60	65.80	182.60	05.03	75.30		127.60	46.00	•	4.30	24.30	197.10	141.50	29.10	64.60	65.00	113.50	158 50	75.80	30.50	135,70	63.50
TABLE	1 E3-236R	62.10	76.00	130.20	70.00	240.70	94.50	7007	40.00	126.60	68 80	112.20	74.10	180.50	7.50	93.80	2	109.50	28.12	62.50	97.00	57.50	1 6	64 80			126.40	42.90		3.70	39.60	1	1	22.00	59.00	20.90	138.80	186.50	91.20	11.10	19.10	92.80
	DATE	1975 2.26 1975 10. 9	•						1976 1.22						976 9.28	2		977 1.18									1978 3, 6								979 12.16						80 10.13	
	*	251 1					, , ,	•	261 1								•	271 19	-	'	-	•			٠٠٠.		282 19	•						•	291 19	٦-			,,	~ -	٠	-

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10 E3-037	41.90	5.40	21.10	2.60	58.90	78.90	15.10	2.30	10.30		154.70	22.50	22.10	00.000	00 75	04.00	200	25.60	17.30	٠.	101.70	92, 10	113.70	122.50	230.00	15.40	3.20	108.40	68.50		52.30	25.70	100 50	77.50	. 10	127.00	158.10	30.00		33.20	73.50	73.10	76.90	20.00	3.90	75.00	2.00	34.50
9 E3-149K	26.90	4.10	10.60	2.60	135.10	49.80	12.10	2.60	7.50	1 1	132.00	20.00	00 606	36.70	20.02	9	00.00	23.00	22.40	• •	93.70	53.70	65.40	24.00	06 031	41.30	1.70	65.90	50.20		58.50	34.45	91.30	56.20	00.	137.00	144.60	32.20	1	86.20	71.50	72.00	73.70	18.10	2.70	27.50	5.40	33.60
8 E3-109	69.40	46.40	65.70	13.50	20.85	62.90	1.10	2.10	72.60		98.50	?:	273 70	115 00	18.10	45.60	27.50	8.40	22.10	. ;	45.50	28.30	25.80	198 20	02.70	102.50	2.50	80.80	22.20	1	09.99	68 40	110.30	4.90	4.90	120.50	78.80	74 70		42.70	48.30	1.20	78.90	73.67	15.40	95.20	18.40	42.30
7 E3-241	84.60	3.60	179.80	08.6	132.10	96.10	11.80	2.60	91.80		107 60	200	212.50	7. 54	203.10	4 40	140.50	1	48.80			į		117.00	200	10.30	90	127.50	126.70		170 30	76.40	207.80	12.70	.50	180.00	t	ı ı		i	1	ŧ	1 1	. .	. 1	1	• •	I
6 E3-038R	33.60	23.30	93.15)	21.31)	1.4.10	115.30	6.60	1.20	80.60)		48 80	20.553	162 053	22 90	34.30	36.50	00.96	130.00	63.20	;	57.50	20.50	107 657	150.00	110.00	13.30	9,	76.50	55.40	;	35 00	21.70	138.70	90.20	33.80	158.40	22.00	35.80		25.40	47.20	34.80	43.40)	73.83)	13.78)	39.90	9 30	01 * 10
5 E3-101	53.40	23.70	57.80 (02.	20.00	46.30	8.50	1.50	40.10 (•	68.40	9.20	219.10	46.80	64.90	39.80	104.10	60.70	37.60		58.10	04.38	92.00	136.20	104.30	57.50	09.	13.10	78.50	ć	90.70	32.40	128.50	14.40	6.10	90.30	51 30	100.50		28.90	77.40	07.00	20.00	86.10	6.80	33.20	8.20	,
4 E3-144	1				, ,	ı	ľ	1	ı		. .	;	1	1		ı	;	1	1		68-10	20.00	199 70	95.10	85.50	96.80	3.20	63.70	83.90	,	96.40	54.50	93.00	5.30	8	200.20	00.00	124.60		26.00	79.00	07.70	43.40	133.00	12.00	67.60	10.40	,
3 E3-153R	87.30	109.70	122.50	3,00	18.00	86.00	18.00)	4.50	119.20	142 60	95.50	22,56)	227.50	71.50	112.10	44.50	123, 10	47.00	26.50		22.80	04.04	124 70	159.50	117.60	116.30	2.00	119.87)	115.40)	60	140.26)	85.13)	160.10	16.41)	4.20	142.12)	105.99)	122.85)	•	50.22)	117.80	166.40	59,34)	108.32)	11.67)	128.50	41.37)	
2 E3-143	102.60	121.50	130.90	4.90	16.30	87.10	9.50 (3.50	118.30	119 60	100.50	16.50 (102.10	51.80	84.70	37.90	119.50	50.20	19.70	5	33.00	36.00	122.40	151.50	120.50	134.00	3.50	101.70 (127.90 (6	153.50 (88.30 (148.60	5.50 (22.50	120.40	115.20 (146.20 (0	49,00	07.007	129.00	62.10 (54.00 (13.00 (128.50	119.70 (! !
1 E3-236R	83.90	63.30	137.90	200.40	07.00	68.20	7.50	09.	116.20	07.07.1	94.10	12.40	257.00	38.20	131.80	44.20	123.20	58.90	15.90	66	10.4	36.40	163.30	151.00	88,10	129.70	5.80	116,90	112.10	000	138.80	79.60	126.20	5.30	200	00.09	102.00	120.10		42.10	70.50 50.50	121.00	51.90	104.50	70	120.40	32.60 105.80	; ; ;
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TABLE 2.4 1-DAY RAINFALL DATA OF STATIONS (7/8)

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	4	();estimated by correlation
	10 E3-037	.50 133.40 121.50 42.53) 47.69) 24.80) 58.60) 110.93) 62.62)
	9 E3-149R	.50 103.50 166.10 31.00 (38.20 (6.30 (53.40 (59.00 (
(WW)	8 E3-109	.90 88.00 180.00 56.90 144.80 75.90 76.20 142.50 60.50
(8/	7 E3-241	
OF STATIONS (8/8)	6 E3-038R	71.50 152.30 106.00 33.20 188.30 52.14) 142.30 129.50
OF STA	5 E3-101	1.40 128.40 81.20 40.80 114.10 76.10 (125.10 90.80 76.80
ALL DATA	4 E3-144	.00 113.10 117.30 35.20 182.50 68.70 75.30 166.80 85.30
AY RAINF	3 E3-153R	12.69) 165.90 172.70 84.58) 180.11) 73.40) 84.11) 196.13) 99.94) 78.06)
TABLE 2.4 1-DAY RAINFALL	2 E3-143	.40 120.60 156.80 36.10 220.20 83.50 75.40 190.00 79.30
TABLE	1 E3-236R	1.80 123.60 190.20 79.00 181.60 67.00 78.50 198.80 95.50
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		10)	50.80	91,40	ć.	ď	37	v, i	. 1	•	•	7.7	n Ø	8.7	71.5	198.20) .		, k			79.4	7	6-67	43.2	4	~ 6	9 6	0 -	127.00		5.67	2.4.5	185.40	, c) e-		0,0	n	0,0		ó	> 0	* 1	77	40.6	7.16	32.1	157.50	3
		9 E3-1498	;- !	1 1	1	ı	1		ı	1 1	: 1	•		ı	1		I .	1 4			•		1	•				1		ı			ľ	ı	,			1	1						í		ı	·l	1		•
		8 E3-109	٥	84,323	19.9	5.1	92.0	7 0)	יט ע	8		137.82)	ġ	1	100	17.7 50.7	, v	62.52	77	7.		ξ.	96.8	7.2	59.3	^ ·	• 0	, 0		7		32	יי	144.00) () () ()	0	'n	**	2.0	5	,	7.00) e • 0	1 1	9	9 9	8	2.7	90.21)	
		17		٠	•	.	٠,	٠.	<i>,</i> .	, <u>.</u>			~ .	×	~ `	•	<i>-</i> ~	٠.	U		U		V	~		•	•																						J	<u>.</u>	J
٠	(WW)	7 E3-24					1	1 1	· •		1		1		1 (ı		1	.1			ž.	•		•				1,	. 1		•		t	1	,1	•	1	•	•	. 1	۱ ۱		1	1	. '	1			
:		6 E3-038R	6.50	139.70	00.7	03.5	7 0	2 0 0	9.90	N	37.2	1	00.701	10		S S S	27.0	65.1	39.7	11.8	0	ì	٥ ·	9 0	~ 0 ^ ^	124 50	, ,	24.5	7 90	12.4	52.4			000	167.70	0	o.	2	0	٠.	ω 	۲	0	00.1	2.6	62.5	6.5	15.7	80.2	154.60	4 1 1
	STATIONS (1/4	5 E3-101			ŧ	• (: 		1	ı	ŧ		1 t	ŀ	1			1	•	ţ	1			1 4		. 4	0	120.00		ı	į		1	ı	ŀ		f,		ļ	ŧ	ł			1	•	ı	•	1	F :	l †	
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:	FALL	3 E3-153R	150.61>	S	, ο α ο α	2 0	15.2	52.9	30.2	27.2	88	, in	6.5	63.7	69.7	20.02	۲.	75.7	8 .		7.40	d,	``	14	34.9	180.53)	67.5	82.6	11.8	64.7	45.6	77.6	95.2	84.3	12	58.7	79.61	, ,	0 1 0 3 k	7.5	•	د	32.66	5 7 6	98.45	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	90	70.70		1.47	
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1	ů.	2 E3-1	1	1	t i	'	1	1	•	•	,	1	i	•	1	•	1		ı	1	•	-1	•	,	,	•	1	•	ı	•	•	1		1	ı		\$ I	•	2	36.8) •	8-77	0.0	2 1	22.7	000	, v	212.90	81.6	32.2	
	TABLE 2	1. E3-236R	1	1	1 1	1		1.	1	•		ı	1	ŧ	ı		ı	1			ľ				ı			1			1	•	ì		1	. :) i		•	ì		!	1		1 1		ı ı	1	ł	ŀ	
		缸	4	Σ	• •			S, i	Ň	•	4	Ġ	2.5	₹.	٠,	:	٠, د .	4 F	3.0	1 -	•	22	∹	٠		6.19	7	ri C	it	, .	•	5.18	Ŋ	0 1	4.64	•		4	4	'n	٠.	+ +11	٠.	u	٠,	٠,	•	i er	٠.	r.	
		DAT	6.1	1936) IM	W	W.	e i	2	3 3	į	076	1941	76	7.	*	7 C	7 6	170	M (7	š	76	7	1945	, t	* ò	1. 2	7	ţ	1947	276	30 C	7 0,0 2,0 0,4	0 7 6	676	676	950	950		1950) C	200	1 026	120	1 11 10 10 10 10 10 10 10 10 10 10 10 10	952	256	325	
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	10 E3-037	•	3.0	6.0	0.99	0	ο. Ο (93.0	160.00	81.3	,	??	24.4	134 40	50.1	06.7	37.1	21.0	8	5.	v	7 2 2	8	0	8.77	11.8	5.1	79.4	101,60	4.0	7.	19.3	1.6	75.3	96,	9.0) r	78.8	3.2	. 4	7 (, v	4 1	, ,) I.	08.3	2 7	54.81)	٠.
	9 E3-1498		1	ı		ı			! !			• 1	. (: 1		1	1		•	•	•	ı	1	•	ı	1	1	1	ı	ı	1	1	ı	1	ı	ı	1 1	ŧ	ı		1	ı	. (1 1	1	1	1	20.00	ι
	8 E3-109	1.67	66.5	7,0	63.8	0.05	2 to 0	40	250.00	7.27	1			168.60	21.4	4.8	13.1	16.2		16.5	8	9	93.2	5.7	81.4	36.5	Ω.	25.5	70.50	?.	6.2	6.0	71.9	68-6	145.50	0.0	1 7 N C	67.8	70.1	1	4 ¢	0	4 t	7 7 7 8	64.8	08.9	9.5	29.80	8
· (1	7 E3-241				1		\$		1		ı	ı ı	,	•	ı	į	ı	ł	1	ł	ı	t	•	1	1		1	1	•	ı	1	١.	1	1	1	I 1		1	ı		1 4	t I		ı ı	1	1	1	ι	1
(2/4) (MM	6 E3-038R	2.7	96.5	2 60	77.8	 	, t		149.90	42.2	00	, ,	19.4	248.90	85.5	37.2	31.1	72.8	٠. ۱ د د	11.8	8.6	27.7	07.6	83.7	73.70	7.10	N.	27.0	78 70	0	2.7	7-7	83.7	51.0	121.80	, , ,	52.4	7.6	96.8		10	, v	1 C			δ.	3.5		v.
STATIONS (2	S E3-101	1	:	1	1	1 1		1	ı			6.4	2	13	04.1	1.2	92 7	01	N (2.0	6.7	270.30	54.7	1	06.87	0	ı			t	6.3	40.1	135,80	000	1 1	7 9	12.90	1.0		e C	ייינ	M	2	8	2	0.7	51.7	46.80	1
OF	4 E3-144	1.0	50.50	٧ ۲	1 C) (26.40	3	1		13.60	1		1	, '	4 2	20	מ כעיי	5.5	25	8	9.0	.0	۱ ٔ	554,80	. 1	. 1		64	7.7	ı `	0 F	104.70	1	M		ω	ر ب	0	ן ד	N.	80	31.9	9.0	3.2	72.60	
RAINFALL DATA	3 E3-153R	5.4	69	9 6) C	M (. 60	9.79	210.50	05.5	37.6	8	76.4	290.30	12.4	4.00	70	N 6	0 1	4	24.5	81.4	76.2	37.0	45.1	10	7 6) (223,50))	31.2	16.1	4.70	7 6	389.00	25.0	42.1	32.1	55.9	80	60.2	2.6	98.5	47.5	œ	13.6	26.5	3,00	
2.5 2-DAY	. 2 E3-143	8.0	61.7	יי מיי	1 4	35.4	44.5	73.2	221.10	99.2	31.5	3.5	45.8	165.80	80.9	4. 4.	^.00	1 0	200	•	37.8	88	55.70	25	> r > r		0 v	6 77	2	!	105.50	0	l i	140 10	• 1	47.6	126.00	08.3	33.0	5	95.50	1	8	47.5	108.80	90.0	١,	46.00	2
TABLE ?	1. E3-236R		2 1	ı ,	1	ı	ı	•	ı	ı	ı	ŧ							1		ı	ı			1 #			ŧ	ı		ı	1	ŀ	,			,		r ·	1			,	1	1	ı	ı		
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	10	92.1	4.6	0 7 7 0 7	0	7.8	74.3	6-67	223,60) 	6,1	50 .5	000 MM	40	. N	8.64	47.3	63.5	7.6	£	20.	6.3	54.6	-	, c	, o	. 0	2		0 0	62.6	54.5	8.7	201	, .	. c	17.70		80 4	Ď,	7 6	א פיני	0.0	W.	81.2	121.60	
	9 E3-149R	1	1 (ı ı	1	ı		t		•	110.00))	1	۲	130.50	2.4	96.8	4.8	6		15.1	6.7	5.2	2.	0 1	7 6		15.80		1 0	1.6	41.5	7.4	91		0 1	16.20		198.70	4.4	4 6 4 6 9 6	, C			42.2	135.00	^
	8 E3-109	8.8	17. 4. 0. 4. 0.	85.9	02.2	33.3	7.77	40.5	141.00	;	4 6 N 4	40	157.80	7 (03.7	9.9	38.1	75.3	eo O	80	4	3.1	71.2	24.5	ייני פייני	164.60	73.7	45.9) P7	4.	4.79	S	•) (93.00	:	4.0	200	7 4	200	66.2	0	96.8	163.10	4
(MM)	7 E3-241	1				1	1	1 1	i t		3 1			•	ţ	•	,		•	1	1		1	4,	. Y	101,20	60.8	11.8	4		88.4	54.6	14.4	200,42	0	5.0	ΙŌ	: {	129.90	100	57.7	39	89.2	;	1	176.80	, v
3/4)	6 E3-038R		6,44	54.0	96.5	5.6	43.2	7 2	73.6)	, ,	17	24.4	\$	57.5	98	91.0	v.	90.5	3.2	69.0		v k	182	115.40	5	0	0	158,00		78.2	2.	. 7 %	M	2	5.1		o v	7	39.8	55.4	64.0	9:9	28.5	126.50	٠ •
STATIONS (;	5 E3-101	321.60	9 4	63.1	50.5	50.1	500	1 C	3	· 0	, 0	8	66.20	3.6	27.0	65.2	9 (10	:	6.1	69-1	ໝູ ທ້າ	2.6	4 4		86	8 0	1.9	18.3	128.00	91,8	0.55	9 4	55.0	2.2	0	٥.	ó	* -	39.2	78.8	92.2	10.6	6.5	325	88.50	
DATA OF S	4 E3-144	319.40	7.7	6.0	3.8	8.6	10.0	2 0	ŧ	0	78.00	S	ı	1	1	ı	•	·	ı	i	1	ı	1 1		,	;	ì	;	•	ι	•	\$ 1	. 1		•			ı	ı	1	ı	1	•	1	1	1 1	
RAINFALL	3 E3-153R	183.00	26.0	77.6	78.0	0 i	7 6	31.0	7.2	73.1	04.7	36.7	145.00	6.76	0	5.4	2 6) o	*	6.2	72.7	יי ממ	7 V	23.4	30.0	157,60	83	52.7	17.3	104.50	30.7	9 6	. 0	68.5	85.5	77.6	74.0	7.80	54.6	28.4	90.3	92.7	95.6	٠,	000	72.3	
.5 2-DAY	2 E3-143	261.00	0.7	25.0	03.6	217	, v	90	41.0	59.6	04.0	78.0	144.50	50.0	8	96) r	1 6			99	70	7 4	20.7	7.97	3.3	61.8	20.0	6	83.30	N 6	9 0	8	M	07.2	60	30.5	67.5	89.1	44.1	62.5	7,1	05	175.80	2 6	7.76	
TABLE 2	1 E3~236R		,	1	ı	1 4	. 1	, 1	1		!	1	•	1	ı		i 1	,		,			. 1	1	01.5	137.00	2	70.1	8.7	60.90	26.10	41.40	33.30	4	35.00	07.76	10.7	55.2	00.70	14.8	31.00	86.3	ο (χ	154.20	72.1	54.5	
	DATE	996	966 12.2	966 12.2	796/ 7.1	467 111	968 3.1	968 3.2	968 12.	969 2.1	969 3.1	969 11.1	696	970 1.	2.2 076	07.1	971 3 2	971 8.2	}	971 10.10	7. I II. I	972 5.1	972 9.2	972 10.	973 1.1	973 1.2	7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	0 0 0	73 12.2		7 1 1	75	75 2.2	75 10.	5 10.1	7	2.21	76 1.2	76 1.2	76 1.2	76 67	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	A. Y . C	977 1.18	77. 4.1	77 10:1	;
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Source: CTH/DAEE

	10 -1498 E3-037	.80 236.7	.70 90.0	.601 00.8	197.5	- 2.3	7.811 7.00*	0.404	7 801	2.10 260.40	30 210 8	7 50 06	70. 138.9		.20 23.7	7.65 07.	.90 92.0	.10 13.2	.70 220.9	.00 257.4	2 62 07	90 147 3	80 19.6	.40. 193.8	.00 236.2	.30 379.4	.00 18.7	-10 176.9	5.90 78.00	**oc oc*	.50 178.0	_00 127.1	.80 188.1	2.2.	0.041 02	50	90 22	10 35.0	9.60 254.90	.20 (90.35	.50 (72,51	9.70 (170.15)	.70 (128.98
	8 E3-109. E3-	3.70 19	56.30	-20	0	5.10	7 7 7 Y	72 00 07	00.10	201.20 242	37.90	38.70	3.60 11	07-97	9.20 1	9.60 13	4.00	74.70	2.80 18	84.70 22	34.00 7	3.10	30.50	03.80 14	01.00	70.00 41	05.00 4	03.00	00	0 00.01	15.20 14	25.40 13	0.80	01 01 01	7.70	7 07.6	3.60	43.80 3	268.00 269	01.70	20.70 4	218.70 179	39,60 12
(MM)	7 E3-241	40.5	65.9	•	46.6	W .	. X	0	82.6	ω .	•	53.2	4	3.60	89.6	9	6".0	7.76	٠. د د	57.4	57:2	181.90	ł	ŧ	•	6.9	11.2	54.2	243.60		220.50	80.5	1	: 1	ıţ	1	1	ł	ı			1	ı
(4/4)	6 E3-038R	161.7	112.8	127.90	174.9	91.0	. « « « « « « « « « « « « « « « « « « «		133	113.3	123.7	109.8	113.9	23	8.06	174.6	121.9	81.0	165.7	195.0	δ.	33.4	93.2	41.0	2.0	60.0	13.3	4.9	83.10	•	228.90	192.2	109.5	, c	113.3	(111.8	49.2	108.6	258.3	221.5	170-2	239.40	163,1
OF STATIONS	5 44 E3-101	13.7	7.6	111.30	4 0	J. P.	1 0	0 0	0	41-4	8.4	53.0	8.0	23.70	0.8	8	8.	41-6	N F	9	11.7	3.9	98.3	150.5	0 143.3	0 240.5	58.1	91.6	155.50		142	3.100	170.7	140.00	95.59	0 92.9	0 41.4	7.29 0	0 209.6	0 154.9	190.2	10 215.90	0.0/1
RAINFALL DATA	4 153R E3-1	S	ω	06.	2.5	٠,	20	09	20.	7	M	٥.	4	- 02	٧.	4	٩	٠.	26	.040	Š	S	S	20 80.	30 161.	10 180.	30 66	200 147	101.2		.91) 98	.2. (40.	.021 (24.	.59) 130	.03) 155.	.90) 145.	.94) 78.	.96) 99.	.60 230.	.34) 217.	.03) 251.	.68) 242.	.002 (76.
2-DAY RAIN	3 -143 E3-	8.00 249	4.90 151	2.90 216	201 07.40	7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	8.60 309	4.30 103	8.50 184	9,80 223	6.40 11	3.70 15	6.10 14	1.50 109	5.80 13	6.80 .15	6 0 09.9	1.80	77 . 07 0	07) 09.0	6.50 18	7.40 16	2 06.6	9.20 17	9.20 16	2.00 27	7.50 12	9.60 (23	2°0		4,10 (147	OT	5.20 0 17	71) 00-0	1.10 (18	7.00 (12	2.50 (16	0.10 (12	7.40 33	52) 02.9	3.70 (24	272) 02.4	/I / 00-2
TABLE 2.5	1 E3-236R E3	8		1 6	7	106.40	M	1.00	5	7.80 1	02.30	1 07.82	76.70 1	'n	51.60 1	08.40	75.70	10.80	00.74	4	70.00	67.40 1	74.80	79.00 1	99.70	39.10 2	55,50	24.00	218.40 24) •	132.00 15	00 00	62.20	25.80	72.90 1	05.20	53.00 1	07.60	13.80 2	260.60 25	48.60	2	7 06.70
	DATE	978 1.1	978 2.	1978 2. 5	7/0 7/0	979	979 113	979 12.1	980 1.1	980 2.1	980 3.3	980 10.1	981 1.1	1981 2.10	981 3.	981 5.2	982 1.	V . V . V . V . V . V . V . V . V . V .	084 .74)	983 2.1	983 4.	983 12.1	984 1.2	984 3.2	985 1.2	7.7	4 4 4 7 9 6 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	1985 11. 3		1986 2. 2 1984 2.2	25. 4. 4. 4. 4. 4. 4. 4. 4. 4. 4. 4. 4. 4.	786	987 6.1	98#8 2.	988 2.2	988 3.	988 4.	988 12.2	1989 2. 4	989	· · · · · · · · · · · · · · · · · · ·	1
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	302 MOJI R.	138.38 53.40 111.94 52.86 124.86 67.09 67.09 61.96	102.71 10.79 186.25 28.24 78.71 93.25 38.47 166.60 42.33 24.33	138.64 29.39 49.38 22.51 83.44 11.52 70.56 174.19 126.64	17.13 21.48 63.48 6.81 95.67 17.35 90.31 143.90	93.69 17.36 6.34 84.52 18.38 37.27 62.59 71.91 67.24
	301 CUBATAO R.	122,40 122,40 135,37 96,04 145,83 81,85 67,37 140,12 71,37	26.87 36.93 207.08 18.80 61.96 61.96 63.99 174.72 47.872 15.57	24.21 28.35 100.41 29.50 86.96 35.22 91.13 161.01 106.94	19.77 7.24 86.14 9.16 201.28 160.77 160.50 90.94 176.96	80.99 27.68 28.16 152.42 80.92 55.75 96.73 113.15 86.33
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. (WW)						
(1/3)	303 WHOLE	99.33 23.99 128.83 197.33 159.40 59.73 96.61 56.63 74.76	19.81 32.69 44.39 18.55 39.22 70.88 44.13 19.44 11.68	62.73 94.26 12.36 79.90 105.31 95.11 15.68 129.67 40.18	45.08 66.41 152.94 38.76 84.59 21.74 172.98 38.59 35.38	35.52 123.08 6.20 70.03 142.04 29.15 97.04 73.42
RAINFALL (302 MOJI R.	137.45 26.95 130.59 189.66 259.70 33.87 109.09 109.02 39.40	1.19 73.80 107.56 19.47 4.82 10.75 53.20 103.14 39.54 93.34	119.76 17.33 1.45 56.64 62.85 127.69 10.54 123.11 36.68	20.02 15.92 123.70 120.08 13.89 146.16 63.57 94.71	38.27 95.02 9.87 100.74 40.23 194.54 22.47 69.45 155.55
1-DAY RA	301 CUBATAO R.	85.92 22.95 128.21 200.03 124.10 68.84 92.22 38.19 53.42 97.04	26.36 18.22 22.16 18.22 51.32 92.05 40.93 87.96 12.36	42.66 121.34 16.20 88.08 120.25 17.49 17.49 131.98	53.89 84.18 163.23 34.18 72.10 24.50 182.42 29.80 14.50 38.78	34.55 132.96 4.91 59.23 10.91 123.56 31.50 106.75 25.17 89.70
N MEAN	DATE	947 4.19 947 5.18 947 5.20 947 6.20 948 3.10 948 3.21 948 3.25	11.23 149 1.73 149 2.9 1949 2.9 1949 2.9 1949 3.10 1950 3.18 1950 3.13	950 4. 2 950 5. 5 950 5. 6 950 9.21 950 12. 4 950 12. 4 950 12. 3 950 12. 3 950 12. 3	1 10.18 2 1.11 2 2.20 2 2.20 2 2.20 2 2.20 2 3.16	2 9.18 2 10.12 2 10.13 2 12.13 3 2 1. 24 3 2 2. 2 3 3 7.31 3 8. 1
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TABLE 2.6						
	303 WHOLE	134.02 98.66 94.38 79.11 77.45 104.92 140.18 59.11 147.30	38.09 71.17 78.09 11.9.05 101.89 123.03 124.32 39.11 97.07	133.88 56.77 152.94 120.36 43.31 111.44 75.84 75.84 75.80	68.67 77.89 93.79 93.79 66.92 36.53 196.82 142.37 48.10 23.08	20.58 20.58 20.58 33.58 33.58 33.58 33.58 33.58 33.58 33.58
	302 MOJI R.	153.16 104.12 94.40 73.12 74.71 102.26 158.25 43.81 155.63	15.69 61.36 77.29 119.14 102.49 125.64 129.33 18.90 28.73	154.65 44.74 176.49 124.80 23.09 109.89 69.29 78.24 79.19	58.31 63.20 83.20 238.27 13.04 110.18 38.44 35.64	76.77 20.18 93.66 117.17 26.24 97.83 36.08 89.26 202.64 63.38
	301 CUBATAO E.	127.28 96.73 94.37 81.22 78.41 105.86 133.82 64.49 144.37	45, 97 74, 63 79, 54 119, 01 101, 68 122, 12 122, 12 122, 12 122, 12 16, 29 96, 49 53, 01	126.57 61.01 144.66 118.79 50.43 111.99 78.15 87.78 89.38 80.96	72.32 83.06 95.31 199.33 48.80 44.80 187.15 153.70 51.50	69.71 24.72 24.73 100.15 45.50 127.15 36.17 205.19 76.80
	표 [1.1.2.4.4.2.5.4.4.6.6.6.6.6.6.6.6.6.6.6.6.6.6.6.6.6	11221112223	4.22.22.22.11.12.21.12.12.12.12.12.12.12.	0012446664	6 0 0 0 0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
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Source: CTH/DAEE

(MM)	
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TABLE	

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303 WHOLE	26.78 58.73 49.73 70.56 73.09 43.88 54.36 113.54 78.43	52.71 57.95 308.44 59.54 80.95 46.90 98.68 10.85 119.33	105.32 21.70 109.09 65.94 48.86 38.07 134.16 37.61 46.10 55.03	65.12 39.45 59.29 47.34 2.29 2.29 54.67 10.39 133.50 141.07	59.23 53.63 120.63 117.98 117.98 116.17 116.17 21.41 59.20
302 MOJI R.	8.45 27.28 22.19 31.96 118.87 113.81 49.25 41.08	253.28 253.28 66.39 66.39 58.74 59.39 4.20 4.20 163.78	90.09 24.54 62.77 62.77 20.95 130.86 39.30 32.25 68.53	42.46 54.81 109.07 60.15 1.14 104.20 6.89 115.21 126.40 62.10	67.17 37.01 38.77 3.69 151.93 19.47 19.47 15.23
301 CUBATAO R.	33.23 69.85 59.43 84.15 92.17 54.46 56.11 122.09 91.58	55.69 66.54 324.34 57.13 88.76 60.27 112.51 13.19 15.78	110.69 20.69 125.39 55.44 58.69 46.80 135.32 37.01 50.97	73.09 34.04 41.77 42.84 2.70 37.23 11.63 139.94 146.24	56.44 59.47 128.33 1.62 210.03 115.70 10.62 123.54 22.58 52.16
	2.26 10.10 10.10 11.11 11.2 12.28 12.29 1.20 1.20	22.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2	1.13 10.12 10.12 10.12 11.15 1.15 2.3	23.6 3.6 3.7 6.1 11.1 11.1 11.1 13.1 13.1 13.1 13.1	21.1.1.2.2.2.1.1.1.2.2.2.1.1.1.2.2.1.1.1.2.2.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1
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303 MHOLE	88.30 93.87 32.44 56.56 44.84 220.93 109.04 23.61 152.21	9.33 96.54 37.54 230.55 52.35 57.95 57.95 23.33	59.98 37.83 23.86 47.00 91.60 91.60 78.94 4.16 82.25 150.17	38.94 139.18 184.52 141.90 7.10 2.60 157.22 73.90 14.70	8.19 8.14 70.11 43.85 51.68 61.68 28.29 126.63 87.60
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302 MOJI R	71.62 59.44 18.71 18.71 18.71 30.80 122.73 73.43 10.90 1120.61 120.61	2.33 102.8776 69.76 69.76 163.86 88.91 60.36 41.68 41.68 41.68 41.68	100.98 129.45 7.90 50.51 112.07 72.02 3.14 39.67 55.09	38.359 98.322 159.21 106.87 7.16 6.04 6.04	3.86 142.44 15.04 15.04 20.08 30.08 37.47 115.10
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301 CUBATAO R.	94.16 105.98 37.27 53.62 49.79 255.47 121.57 28.09 74.68	11.80 106.01 36.65 36.65 39.48 39.48 85.79 85.79 15.67	45.55 29.48 45.76 84.40 81.37 4.51 97.23 90.38	39.06 153.56 193.43 154.23 7.07 7.07 7.07 78.42 78.42 78.42 78.42 78.42 78.42 78.42 78.42 78.42 78.42 78.42 78.43	9.71 86.51 5.71 76.54 51.89 59.28 68.70 68.70 138.20 77.91
	22.20 23.11 23.11 23.11 23.23	22. 22. 22. 23. 24. 24. 25. 25. 25. 25. 25. 25. 25. 25. 25. 25	10.11 11.20 11.22 11.22 1.22 5.19 5.20 9.22 9.22	11.25 11.25 11.25 11.25 11.25 12.26 13.46 13.20	2111221112 21112211112 2112211122
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303 WHOE!	132.37 20.00 96.14 274.73 3.74 87.12 127.09 35.56 35.41	129.21 26.88 51.56 74.67 61.15 92.79 96.98 30.73 3.72	65.97 49.77 41.30 38.56 113.01 98.03 76.82 52.20 52.20 3.94	168.10 120.23 132.82 167.94 48.56 131.80 164.00 124.45 28.29 28.29	78.16 57.45 59.95 22.28 166.78 19.47 71.26 104.34
2 8	112.09 7.38 115.23 183.36 3.91 13.42 129.58 78.97 32.26	13.25 22.01 16.53 97.55 42.48 42.48 52.14 6.31 18.15	68.19 32.13 32.13 53.94 9.84 85.08 85.08 21.66 4.82 10.59	129.83 87.07 134.05 179.80 40.88 87.52 87.64 202.51 29.33	38.64 120.00 13.85 34.40 108.59 125.96 123.83 65.44 91.12 22.80
302 MOJI R.	22 22 23 25 26 26 26 26 26 26 26 26 26 26 26 26 26	11. 22.52.99.16.23.53.43.91.	866 88 462 41	123 173 173 173 87 202 22 22 23	25 120 108 108 123 123 123 123 123 123 123 123 123 123
<u>~</u>	24.44 89.42 306.89 3.68 113.06 1126.21 20.28 36.52 114.48	134.83 28.59 63.89 66.62 67.72 107.09 1139.32 4.95 49.62	65,19 55,98 36,85 48,66 48,66 62,84 62,94 13,55	57.39 51.26 51.26 51.26 51.26 51.26 51.26 51.38 51.38 51.39 51.93	92.07 35.44 76.18 18.01 17.19 17.19 59.86 73.31 67.88
301 CUBATAO	245 306 306 113 126 126 144	134 288 668 107 107 44 49	65 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	181 132 132 163 163 147 190 96 96 27 27	92 35 35 76 18 18 17 17 108 67
1 1	2. 9 2.27 2.27 2.30 12.13 1.26 3.13 3.13	22.23 22.23 22.23 22.23 22.23 24.23 25.23 25.23	7 33 118 118 119 115 116 123 24	22.22.23.23.23.23.23.23.23.23.23.23.23.2	3.17 111. 2 111. 3 3.18 3.27 3.27 12. 2
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Source; CTH/DAEE

(2/2)	303 WHOLE	17.13	161.50	61.67	159.23	58.13	50.00 101.00	86.22	70.19			DAEE	. * !					÷																								•	
	302 MOJI R.	47.48	119.72	38.19	153.01	48.33	11.010	106.56	46.25			rce;CTH/DAEE	•																														
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	303 WHOLE	67.96	87.74	12.64	123.77	7.34	80.73	, ,	86.77	6	120.83	17.20	236.29	78.48	54.54	43.85	102.03	30.44		61.21	42.03	140.15	170.33	106.45	87.17	2.38	95.18 62.91	63.92	20.03	131.99	27.58	9.36	134.91	78.55	22.80	41.82	30.72	110.03	36.96	86.04	13.19	23.93	64.64
	302 MOJI R.	39.92	74.41	16.35	140.03	.64	100.50	5.7	64.71		177.08	19.40	191.78	31.53	32.34	40.52	07.70	48.25		65.32	57.84	118.64	166.81	119.72	25.14	1.00	53,94	50.69	0 tr 0 c	127.00	75.64	22.99	146.93	97.00	41.44	29.26	38.90	81.44	35.24	69.83	74 38	0.92	37.29
	301 CUBATAO R.	77.83	92.44	11.33	118.05	9.70	7.00	3 6	94.54		120.21		251.95	95.00	62.35	45.08	25. 50	24.17	;	59.76	36.47	147.72	171.57	101.77	109.00	3.68	56.07	68.57	76.28	133.74	10.32	4.57	130.68	78.10	97.36	46.24	27.95	120.09	37.57	91.74	110.04	29.21	74.26
	DATE a	981 1.15								. •								983 12.11									1985 4.12	1985 11. 2								37 3.16						 	4
	×	301 19	,,	_	_		- ·			•	~ *	٠	۰~	_	,		-	320 19					_		Ξ.		330 19	331 191								341 1987	, ,-			7	-		~
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	303 WHOLE	0	8	129.28	84.0	4 8 4 1	50.		0.0) 	87.0	8	80.9	22.9	66.2	57.2	9.	76.0	15.7	13	`	4 t 4 t 1 t	40,) u	7.0	0 C	,,	0 (4.0	109.29		4.6	38.7	85.0	83.7	152,37	70.8	90.8	62.6	45.6	56.0		9.4	0 0 0 0 0 0		10.0	Q O	11.0		18	8.3	-
	302 MOJI R.	7,5	79.2	104.88	39.6	24.0	14	7.00		9 4	•	29.0	09.2	113.50	14.4	71.9	31.7	9.80	63.0	78.7	ζ.		9 0) r	, ,	,		,,	7 4 4 6	,,,	60.114	•	ε. 10.	8.	98.7	39.1	119.47	98.5	17.3	28.5	30.4	35.2	•) · c	0 4	00	M	63.7	7	86.1	15.39	5.9	
(MM)	301 CUBATAO R.	8	8	137.87	64.5		יי פיני) O	71.	. 4	•	۲.	50.8	7.69	5.8	64.2	66.8	22.5	45.4	28.7	16.4	7.70	2 4 6	 M	2 88	70.0	77.2	. 6	,) X	190.58		80.9	52.4	15.4	7.66	163.95	5.00	16-7	10,4	27	63.4	30.5	27.	59.1	54.5	21.1	85.5	05.2	7.5	17.18	3,4	
(3	च्य	7	6	10.12		4	٠,	•	7	'n		1.14	~			=1		3	2	2.5	N		2	7	0.3	2 1	~	2			12. 4		1.24	10.26	1-25	1.26	2.0	v	77.77	2 4 4	٠. ١٠	/7.51	٦,	•	N	2		n	~*	۲.	2.23	۲,	
L (1/2	DAT	D N	8	1952	ν o	, 6	v	10	10	Š		1955	9	9	Š	8	S.	in I	<u>ا (۱</u>	S	D.	9	8	9	8	S	9	9	5	10	1959		1960	9	0 1	٥ ·	200		100	2 4	D .	0	O.	o	596	796	o	œ	ø	6	1965 1	o	
RAINFALL	, ¥	5.1	25	S	4 t		200	S	59	9		61	62	63	79	92	99		χ,	69	0	71	72	73	7.4	75	76	77	78	29	80		8 c	1 0	o c	# t	0 0	α 0 α	à œ	0 00	6	> .	91	92	6	76	φ.	96	26	80 C	6.0	001	
MEAN 2-DAY R	303 WHOLE	31.8	09.5	149.62	0.0	. 00	7	95.8	9.60	54.9		157.01	16.7	47.4	9. 9.	9-52	59.7	2.6	7.7/	24.8	26.7	43.5	21.3	8.7	7.66	46.7	0	53.0	70.1	66.69	116.75		154.14	40.7	77.1	E (, r	•	10	9 M) u	^ ^	08.5		85.0	10.4	70.2	76.2	8.60	61.9	108.65	94.5	
2.7 BASIN	302 MOJI R.	57.5	7.80	167.29	· α	200	76.7	81.5	21.6			148.06	03.1	77.1	6.0	21.5	27	, , , , , , , , , , , , , , , , , , ,) i	21.5	9	56.9	37.4	48.6	12.4	23.3	143.42	33.9	89.2	0.9	37.4		157.54	200	, ,	4 · · · · · · · · · · · · · · · · · · ·	9 0	, ,	, r	, M) () () ()) ,	13.1	8.7	19.4	38.2	59.7	53.6	35.9	66.9	133.78	02.2	
TABLE	301 CUBATAD R.	22.7	8	145.41		92.4	25.3	00.8	05.3	62.1		160.17	71.7	٠. ١	4,0		,,,	1 4	•	0.0	20.00	38.8	5.6	05.9	6.76	55.0	139.26	29.7	63.4	1.3	7.60	;	152.94	9.0	9 6		0 Q		45.7	2	1 4	•	71.7	0.4	208.0	00.6	73.9	84.1	5.8	60.0	99.80		
	DATE	36 1	56 3	77 7.5	38.	38 6.	39 1.2	39 2.2	40 1.	40 3.1		60.16.62			, r			1 1 1 1	1	2 **	1	44 2.27	3.1	M		5 6.3	5 1.1	3.1	3.5	7.12	7 4.1	,	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2		אנ	,	1	5	9.3	0 3.1	M 0		7 0	0	2 6	122	27.	H 01 1	130-1	 	, , , ,	2	
	Π	0.1	э c	* O	0.00	19	13	13	19	19	. •	701	, C	N C	1 0		, ,	. a	0			21, 194	O :	& . •	4	2 19	9 19	7 19	8 19	9 19	0 19	•	32 194	4.	10		9	7 19	8 19	9 19	0 19		1 19	2 79	5 19) i	ν (γ (7 4) (i	9 6	50 195	` `	

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	303 WHOLE	171.77	101.13	120-15	98.73	49.63	65.06	274.57	97.91	174.26	197.06	0	440.44	40.70	45.64	12.20	40.40	10.0		000	260.88		133.01	145.95	72.87	•7	180.37	~	90.15	156.68	153.66	153.47	. (149.61	V . V	76.7	9.0	0.00	10.70	4 N	40	200		w	r:	238.38		. '	I / DAMM		•		
-	302 MOJI R.	170.17	100.77	110.98	105.88	61.28	711.09	79.172	129.27	155.79	155.62	r) C	. 0	٠.	1 U	16	0	11		218.37	 	63.87	136.30	135.73	147.42	169.49	286.53	26.14	137.73	90.14	69.02		0.00	104.41	1007	60.00	10.10 04.00	97.73	63.70	20.70	258.82))))	91.2	155.99	22.1		•	urce;CT				
(MM)	301 CUBATAO R.	172.33	101.25	123,38	0	70.07	00.04	000	00.00	20.	411.65	126.32	147.13	129.98	76.20	103.77	127.75	30.74	97.77	214.55	275.85	1		\$0. At 1	100.04	700	184.20	10.07	112.67	105.55	176.02	183,20	130 40	130.00	164.00	163.07	0.4.7.	137.55	107.70	138.24	76 28	301.23	!	228.36	N)	4.			Ŋ				
2)	斑		N (, ,	- - - -	;	,	- - -	•	•	3.31	10.12	1.14	2.10	ω ω	5.20	1. 4	2.25	12. 2	1.31		21.	, ,	7	100	, ,	7.00	7	* *	15	-			12-18	3.15	6-14	7	2.20		M	12,20		2. 4				•					
L (2/2)	DATE	1978	17.0	1978	0 4 0	1070	1070	1070	1080	9 6	00	1980	1980	1981	1981	1981	1981	1982	1982	1982	1983	1001	3 0	000	780	1001	1000	1000	000	000	1400	1402	1986	1986	1986	1987	1981	1987	1988	1988	1988	1988		1989	φ.	ထ	-						
RAINFALL	¥	100	7 P		i i i	1 10	157	α 1 τ	0 0		2	161	162	163	164	165	166	167	168	169	170	171	172	171	174	47.5	176	17.0	87.	7 7 0	λ C	001	181	185	183	184	185	186	187	188	189	190		191	7 Y	ያ አ ዝ							
MEAN 2-DAY	303 WHOLE	7	n.	62.262	•	i A	ĎΑ	ò٤	'n٧	٠.	4	182,16	89.00	265.78	132.65	86.64	161.54	260.16	267.18	110.30	121.26		60.01	07.10	100.00	70.00	27.252	25.41	510.54	249.00	159.83	88.60	77	į	, ,	ľ	2	٧,	80	20	4	167.89		290.44	64.7	366.39	7.07	27.8	2.60	51,3	7.92	25	
2.7 BASIN	302 MOJI R.	313.85	128.40	77.77	0.00	7 × × × × × × × × × × × × × × × × × × ×	000	74, 75	200.00	/ V - K = T	74.011	0	ø	153.59	W	Ó	O.	ø	M	N	98.87		00.044		97.301	94.70	0,44	24.04	0.00	1 0 0	107.40	/0-/0	7	127.42	. 1	71.81	'n	123.56	6	54.15	32.69	138.61		237.60	240.77	296.84	125.13	67.66	63.58	175.87	114.45	130,13	٠,٠
TABLE	301 CUBATAO R.	296.18	1,40.04	287.83	200.00	127.51	94.18	77 -702	133-17	176.17	0	200.15	68.06	305.26	149.66	24.68	163.15	290.97	291.06	96.58	129.14	61 22	45.07	7 6 6	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0) &	120 75	` `	9 7	4 0	9 7	11.0	154.47	92.22	128.42	127.98	163.26	111.14	129.28	143.58	146.64	178.20	1	309.04	275.14	390.87	145.89	149.03	125.70	126.21	150.64	22.07.4	0 / 40/
	DATE	1966 3.6	4 -	1 e	,	77)	6-4	l lu	M	5	,	69 2.19	w.	9.11.3	9 12.		2.2	m .	2.2	3,2	2.8	1.10			72. 5.19		, 6				, 40		12.2	ed ed	12	-	g-t	2	5 10. 9	10.1	-1 1-1	72.2	•	1.20	. r	N .	4	7.0	V	•		,	
	¥	101	•	. , .	•	-	•	-	4-4	•	•	111 196	**	• •	-	•	-	~	4	-	7				124 197							•	131 1973	٠,	7	•	•	4-3		ę, i	~	-		142 1976		1				. ~	1 .	٠,٠	٠

TABLE 2.8 PROBABLE BASIN MEAN RAINFALL BY VARIOUS METHODS

CUBATAG R	IVER BASIN		1	unitimm	CUBATAD RIV	VER BASIN			unit;mm
			Method	 			, —, i i i i	Method	! ! ! !
Return Period(yr.	WAI KADOY		2		eturn eriod(yr	IWAI -KADOYA	l ULL	! !	
	149	150	150	151	N		: M	18	Lin
,	ייי	207	402	202	ហ		m	96.	
i i	240	244	241	24	10		ın	<u>4</u>	ä
Ϋ́ì	787	300.	286	287	25		•	5	٠,
100	322.4	338.2 376.7	320.7 354.7	321	100	414.9 451.5	498 0 560.9	470.4 525.7	441.3
MOJI RIVER	NISHE				MOJI RIVER.	BASIN	† 1 1 1 1 1	1 1 1 1 1 1	
† † † † † † † † † † † † † † † † † † †	; ; ; ; ; ; ; ;		Method	 				Method	
Return Period(yr)	IWAI	1 =	į <u>z</u> .	ı <u>iii</u>	Return Period(yr)	IWAI -KADOYA	WEIBULL	HAZEN	GUMBEL
2	136		135.	134.B	2		I N	1 2 1	12
<i>a,</i>	172	ហ	173.	¥	ហ		ണ	4	
16	C.	202.0		201.8	10	282.9	292.3	284.3	4
Ĭ,	221.	₹.	226.	ID	25		_	34.	₹~4
ល័	239	Κ.	247	5-4	50		m	72.	m
10(257.	o !	268.	9 1	100		C	. 60	- + I
WHOLE		. !			WHOLE				
٠			Method			 		Method	! ! ! ! !
Return	INTERPED	1 1 1 1 1 1	1 1 1 1 1 1 1 1 1 1	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	4 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1461	1 1 1 1	1 1 1 1 1 1 1	
eriod(yr	-KADO	IBUL		ш	9.5	KADOYA	WEIBULL	HAZEN	GUMBEL
N	139.	140	140,		N		1 44	1 1 6	i m
	186.	190	187.		LC.		0	ı,	LI.
1(218.	224	217.		10		4	7	m
22	257.	266	255.		25		m	76.	'n
Ň	286		283.8	296.2	្ត ពិភ	1960 1990 1990 1990	4 1 4 1 10	, 4 , w	1 4
101	712	20 E			00/		ì	} {	,

TABLE 2.9 N-HOUR MAXIMUM RAINFALLS AT RIO DAS PEDRAS STATION

	Date and Rainfall (mm)	Date and Rainfall (mm)	
Year	r 3 hr 4 hr 6	Year 1 hr 2 hr 3 hr 4 hr 6 hr 9 hr 12 hr 18	hr 24 hr
7-38	20-02 09-02 03-03 E3-03 03-04 05-05 05-05		
ļ	43.2 76.1 94.3 126.2 168.1 175.5 218.0 243.2	011-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00 01-00	10 00 0
38-39	08-03 08-03 08-03 08-03 24-12 24-12 24-12 24-12	25-01 28-02 28-02 28-02 28-02	02 27-02 08 27-08
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Ċ	, IPT (RELATORIO No. 23, 395, Vol. 5)	24.7 77.8 103.0 118.4 13P 8 134 F 140 0	ខ្លួច
NOTE;	B (Year) means Oct. 37 - So	02-12 02-12 02-12 02-12 01-02 01-02	02 01-08
		62.0 66.4 99.8 114.4 132.0 175.8 216.1	ί.
		5 60-08 60-08 60-08 90-08 90-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-08 80-0	ស្ង
		23-01 23-01 23-03 7 48-0 140 0 15K-K-1	0.202.0
		54.8 64.1 78.1 104.0 141.5 190.5 226.8 2	'n

40 84-85 25-03 23-01 54.8 64.1

Source, IPT (RELATORIO No. 23,394, Vol.5) Note, 59-60 (Year) means Oct. 59 - Sep. 60 (); Maximum

TABLE 2.10 HOURLY RAINFALL AND WATER LEVEL OF THE FEB.1988 FLOODS SUBJECT TO CALIBRATION

Ultraf	ertil S	tation		Para	mapiacat	a Station		Feb . 7	- B	
Date	Time	Hourly Rainfall (mm)	Total (mm)	Date	Time.	Hourly Rainfal: (mm)		Date	Time	Water Level (n
8	9 10 11 12 13 14 15 16 17 18 19 20 21 22 23		0.9 6.9 33.5 35.1 50.4 62.4 63.7 64.1 66.5 67.2 67.3 68.4 69.1 70.4		8	8 9 0 0 1 2 2 3 4 4 5 7 12 1 2 4 9 0 1 2 4 9 2 2 2 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3	0.3 3.6 15.7 36.1 36.2 39.6 64.5 66.6 68.9 71.7 73.8 75.5 77.3 77.6 78.1		7	0 0.20 0 0.20 0 0.20 2 0.20 2 0.20 3 0.20 5 0.16 6 0.16 7 0.27 9 0.27 9 0.39 9 0.39 9 0.29 9 0.29
								· .	11 12 13 14 15 16 17 18 19 20 21 22 23 24	0 23 0 23 0 23 0 23 0 24 0 26 0 33 0 35 0 35 0 30 0 29
trafert	il Stat	ion		Paranag	viacaba 9	Station		Feb.20) - 51	
te Ti	Ra	urly To infall (mm)	tal (mm)	Date		dourly To Mainfall (mm)	otal (mm)	Date		Water Level (m
20	21 22 23 24	0.3 0.0 0.0 0.0 0.0 0.0 1.1 8.2 11.0 6.3 2.2 0.7 1.1 0.2 0.2	0.3 0.3 0.3 0.3 0.3 0.3 0.3 43.8 54.8 60.1 65.3 667.1 67.3 67.5 67.8	21	8 9 10 11 13 14 15 16 17 18 19 20 21 23 4 5	0.1 0.0 0.0 2.7 32.7 4.4 8.5 7.2 2.1 0.3 0.8 0.6	0.1 0.1 0.1 2.8 35.5 39.9 48.4 53.6 57.7 58.5 59.6 60.2 60.5 60.6	2.	10 11 13 14 15 16 17 16 17 18 18 18 18 18 18 18 18 18 18 18 18 18	0.22 0.20 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.1

Source: CTH/DAEE

TABLE 2.11 HOURLY RAINFALL OF DEC.1989 FLOOD SUBJECT TO CALIBRATION

Portao	40				Саіка	10		
Date	Time	Hourly Rainfall (mm)	Total		Date	Time	Hourly Rainfall	Total
		~~~~~	********				(mm)	(mm)
14	8	0.0	0.0		14	8	0.0	0.0
	9		0.0			9	0.0	0.0
	10	0.0	0.0			10	2.0	6.0
	-11	0.0	0.0			11	6.0	8.0
	12 13	0.0	0.0			75	0.0	8.0
	14	0.0	0.0			13	,-	
	15	16.0	0.0 16.0			14	8.0	16.0
	16	7.0	23:0			15 16	32.0 12.0	. 48.0
	17	0.0	6.69			17	8.0	60.0 68.0
	18		23.0			18	15.0	
	19	0.0.	23.0			19	15.0	98.0
	50	29.0	52.0			20	46.0	144.0
	51	9.0	61.0			21	7.0	
	55	0.0	61.0			22		152.0
	53	0.0	61.0			53	0.0	152.0
15	24	2.0	63.0			24	0.0	152.0
. 13	1 2	0.0	63.0		15		0.0	152.0
	3	0.0	63.0 63.0		1	5	0.0	152.0
	4	0.0	63:0			3 4	0.0	152.0
	5	7.0	70.0			5	0.0 5.0	152.0
	6	2,0	72.0			6	2.0	157.0 157.0
	7	6.0	78.0			7	0.0	159.0
	- 8	3.0	81.0		15	8	3.0	132.0
	9	11.0	92.0			9	7.0	169.0
	10	0.0	92.0			10	0.0	169.0
	ii	3.0	95.0			11	1.0	170.0
	18	4.Q	99.0			12	0.0	. 170.0
	13 14	3.0	102.0			13	0.0	170.0
	15	0.0	102.0	-		14	0.0	170.0
	16	0.0	102.0			15	0.0	170.0
	17	0.0	102.0			16 17	0.0	170.0
	18	6.0	108.0			18	4.0 3.0	174.0 177.0
	19	3.0	111.0			19		177.0
	. 50	0.0	111.0			20	0.0	177.0
	. 81	0.0	111.0			21	0.0	177.0
	55	0.0	111.0			55	0.0	177.0
	23	0.0	111.0			53	0.0	177.0
	24	0.0	111.0			24	0.0	177:0
	1		111.0			í		177.0
	. 3		111.0			2		177.0
	4		111.0			3		177.0
			111.0 111.0			4 5		177.0
	5 6		111.0			ອ 6		177.0
	7		111.0			7		177.0 177.0

Source; CTH/DAEE

## TABLE 2.12 ESTIMATED PROBABLE DISCHARGE OF CUBATÃO RIVER (EXISTING CONDITION)

-										1:											
47-40-10 47-40-10 47-40-10	2 240 27 PLT 25.24.00 36.09	25.18.00	384.14	24.12.00 29.12.00	0 11 0 11 0 12 0 12 0 13 0 13 0 13	30.11.60	5 N. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1.	25.12.00	25.12.00	25.12.00 25.12.00 25.12.00 25.12.00	GMAX-DATA G-MAX	END OF PLT 25.13.00	25.15.00	3 EF	25.12.00 25.12.00	25.12.00	25.13.00 96.14	25.15.00	25.12.00	#11.015 R. APT P1.0E\$ 25.12.00 25.12.00 454.72 1319.52	10 10 25.12.00 1319.52
# # # # # # # # # # # # # # # # # # #	11 25.13.00 504.67	25.22.00	20 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	14. IMGATS BRG 23.13.00 2 25.13.00	15 25,13.00 552,17	16 21.12.00 57.73	17 18 ANCHET 08Q HWRY BRDEN 23.15.00 25.12.00 586.29 [96.02	12 100.02	25.13.00 747.60	20 8FR PERODE 25,15,00 723,07	ATAC-CATAC	11 25_12_00 1170_69	12 25, 9.00 126.76	15 15 25 25 25 25 25 25 25 25 25 25 25 25 25	25,12,00 128,12,00	12 52.13.00	16 25. 9.00 130.80	15 ARCHET DNG NBBY SRDEN 25.13.00 25. 9.00 1329.49 312.20		25.13.00 25.13.00	77.6877 00.51.62 75.50.60 648
4 × 4 × 4 × 4 × 4 × 4 × 4 × 4 × 4 × 4 ×	25.13.09	25.15.00	23.22.00	33384 :188 33384 :188	25.23.23.200.25.23.200.23.23.23.23.23.23.23.23.23.23.23.23.23.	25.12.00		27 28 EREGUE 4. AFT PERSUE 29.12.00 25.12.00 212.30 014.02	29 2 AIVE POUTH 0 25.13.00 2 916.20		ATAN-OATA	25,12,00	22 23.53.60 103.52	23 Bi	24.12.00 25.12.00 350.70	28.13.00	26 PE 25-12-69	27 28 28 EXUR MOUSH PERSONE R. AFT PERSONE RIVE MOUSH 25.12.00 25.13.00 440.00 1276.00 1876.15	28 RI PEROUE RI 25.13.00 1276.66	24 1VR #OUTH 25.13.00 1876.35	
	10 #5153d	SCHARGE(CUB	ATAG MIVER	DESIGN DISCHARGE(CUBATAD GIVER FEB.24.7] FLOOD TYPE,WW1/ 5 .EXISTING CONDITION)	12000 TPB5	1897 S /184	STING COND.	11043	•	:	;	SIO METSIG	CHAPGECEURA	TAD RIVER	DESICH DISCHAPGECCURATAG RIVER FEB.24.7% FLOOD TYPE,W=1/ 30.EXISIIMG CONDITIONS	00 TYPE, W=1.	/ 50.EXESTE	ING CONDITIO	2		
2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	25.14.00 78.18.78.38	25.17.00	3 8F 25.12.00 560.14	8FR 914085 28.12.00 586.62	25.15.00	25.13.00	7 0 25.15.00 3 106.12	8 - 25.12.00 194.54		25.12.00 25.12.00 25.12.00	AT40-X4H-0	25.13.00 25.13.00	95'081 25'77'52	7 25. 9.00.	erP PILDES 25. 9.00 1017.70	71.401 00.51.85	25.12.00 234.00	25.13.90	25. 9.00 327.55	9 10 PILDES R. AFT PILDES 25.12.00 25.12.00 532.13 1521.46	77 PILDES 23.12.00 1921.46
# # # # # # # # # # # # # # # # # # #	11 25,12,00 755,16	12 23.120	13 25, 25 25, 25 25, 5 25, 5	120210 120210 12012100 12012100	50 10 10 10 10 10 10 10 10 10 10 10 10 10	25.12.00	21 57 0 00.115.00 7 25.15.00	3ACHET SRG HRRY BRDEN 25.15.00 25.12.00 878.29 255.00	18 18,13,09 1055,97	20 Brs >codus 23.13.00 1032.50	4 X 4 X 4 X 4 X 4 X 4 X 4 X 4 X 4 X 4 X	11 25.12.00 1576.58	12 25. 9.00	25.12.00 24.12.00	14 146875 986 25.12.00 1498.62	15 25.23.00 1474.13	16 AH 25, 9.00 154.87	17 ARCRET BAG HRRT BRDEK 25.13.00 25.70.00 1534.30 352.93	16 MRY BRDEK 25, 9,00 352,93	25.23.00	20 8FB PEABUE 25.13.60 1490.27
# T # O - X 4 # 4 # T # O - X 4 # 4 X 4 # 1 - 0	21. 25.13.90 56.18	22.25.40	25 22 25 25 25 25 25 25 25 25 25 25 25 2	24.17 PROUE	25.12.00	28,200	27 PERFOUE 8. 0 25,12.00 3 320.57	28 25,12,00 25,13,00 320,57 1301,95	25 13 00 17 H 25 13 00 13 13 13 10 10 10 10 10 10 10 10 10 10 10 10 10		4740-8 4740-9	21 25,12,60 123,50	25.13.00	25. 25. 3	24 9AIX PROUE 25,12,00	25,13,00	26 PR 25, 9,00	29 28 28 0214 PERGUE R. AFT PERGUE RIVA MOUTH 25.12.00 25.13.00 25.13.00 518.70 2127.52 2121.04	28 FT PEKQUE R 25:13.00 2127.52	29 IVA MOUTH 25.15.00 2121.04	
	DESIGN DIS	SCHAPGECGUS	ATAG RIVER	BESIGN DISCHAPGEKKUBAKAO RIVER FEB.22.71 FLOOD TVPE,V4.7/ 10.EXISTIMG (G401110M)	173an 0007.	147/ 10, EXI	10x92 9x1.5	71017			,	\$651G* DI.	SCHARGECCUBI	ITAG RIVER I	DÉSICW DISCHARGECCUBATAG RIVEM FEB.24:7; FLOOD TYPE,W-1/100.EXISTING COWDITION)	000 TPE,V=:	1/100/EXIST	IXOMOD DKI		٠	
6 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	END OF PLT 25.13.00 112.65	28.15.00	25.12.00	25.12.00 25.12.00 706.00	25.15.00	28.14.00	25.13.00	25.12.00		10 PILOES B, AFT DILOES 25:12:00 25:12:00 355:73 1061:79	OMAX-DATA	25.13.00 25.13.00 262.54	25.14,00 256.50	\$6.4811 00.4 .25 2	6## PILDES 25. 9.00 1171.62	5 25,12,00 129.36	25.12.00	25.15.00	8 25, 9.00 380.0?	9 10 PILOES 9, AFT JILDES 25,22,20 609,42 ;722,93	10 25.12.20 25.12.20
A	11 25,12,00	25. 9.00	25.12.00	14 1MGRTS BRG 25.12.00 1022.33	25.13.00 1021.77	25. 9.00 98.15	17 ANCHET ORG HARY DROPE 25.13.00 25.12.0 1070.41 265.7	18 NWAY BRDEN 25.12.00 265.78	25,25,00	20 BFR PERGUE 25.13.00 1250.57	CHAX-DATA	25.12.00 25.12.00	12 . 25, 9.00 169,57	25.12.00 2706.44	16 IMGRTS BRG 25.12.00 1705.44	25.13.00 25.13.00 3674.53	16 A: 25. 9.00	17 18 AXCMET GRG MMRY BRDEM 25.13.00 25. 9.00 1739.04 359.75	18 18 50 50 25, 9,00 359,75	25.13.00	20 BFR PRRGUE 25.13.00 1690.29
SHAN-DATA G-HAN	25,13,00	25.13.00		23 8AIX PROUE BAIX PROUE 25, 9.00 25,12,00 226,84 283,00	25.22.00	26.12.00	27 28 PEREGUE R. AFT PERGUE 25.12.00 25.12.00	25 1FT PERQUE 25.13.00 1551.82	25 25 200 25 25 200		40-740-47-40-47-40-47-40-47-40-47-40-47-40-47-40-47-40-47-40-47-40-47-40-47-40-47-40-47-40-47-40-47-40-47-40-4	25.12.00	22 25.13.00	25. 9.50	24 3007 XINB 3007 XIX. 25,12,25	25,13,00	26 PEREGUE 9. 25, 0.00 25,12.00 220,44 SE1.01	20 20 RIVE MOUTH PERSONE RIVE MOUTH 25.12.00 25.13.00 25.13.00 551.01 2575.24	26 LFT PERQUE R 25,13,00	29 IVR HQUIM 25.13.20 2366.19	
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### TABLE 2.13 ESTIMATED PROBABLE DISCHARGE OF MOJI RIVER (EXISTING CONDITION)

KOZUZ-MON 1 TYPE-MON 1	G= 1 TYPE-#G= 1 1965, 1,22 = 1985, 1,24	1985. 1.	1985. 1,22 - 1985. 1,24	1.34						:03	KOZUI-NO- 1 T	OFFICE DISCHARGECENDI REVER JAKEZA'85 FLOOD TIPE/MELJ 25/EKESTIKG COMDITION) [0= 1 TYPE-HG= 1 1985, 1.22 - 1985, 1.22 - 1	JE MEVER JA: 1985.	1945, 1.22 - 1985, 1.24	1.26	25, EXESTING	COMPITION			
OF STATE OF		25	2	75	88	8	'n	*	ñ	CHITER	***************************************	ŗ	Ş	;	;		. '			
; `							•				ULTRAFERTL			BIRE INOID	*	Š.	ř	SY 25 26 INDIO R. APTR 2NDIO	36 FTR 24010	Ř
DON' ONCE THE TOTAL	28.05	243.42 213.07		27.58	72. B1. 55	23. 9.00	25. 8.00 10.36	25. 9.00 23	23.10.00	GFAX-0A7A G-MAX	788.23	25. 7.00	790.10	566.47	23. 7.00	23. 8.00	22. 7.00	23. 8.00	25. 9.00	23.10.00
07	5		. 3	;	\$	97		40	9	CHITEN-RYURYD	:	:			٠	• .				
						7	PIACACUERA AFT	AFTR PICCR			3	BARE PICGR	S.	ij	3	\$	3	PLACAGUERA AFTE POSCOR	TR PICCE	67
GRAX-DATA 23, 7, 0	23, 7,50, 25,10,00 50,90, 225,20	55. 25. 25	23, 7,00 2	23- 7-50	25. 8.00	25. 7.00	23. 8.00 2 51.56	25.10.00 23	23.11.00	OMAN-DATA	23. 7.00	23.10.00	23. 7.40	23. 7.00	23. 7.00	25. 8.00	23. 7.00	23. 7.00	23.10.00	23.11.00
のとなりとボールがたいまり										CHITEM-RYURYS	T A				01.77	136.489	\$9.45		646.80	547.11
	S1 RIVE HOUTH					٠					8	16	٠							
BMAK-DATA 23, 7.0 G-MAK 25.7	23, 7,00 23,31,00 25,595 240,10	·						a.		SHAK-DATA D-MAK	23. 7.00	23.11.00			•			÷		
N91830	OSSIGM DIZCHABGEKMDJI RIVER JAM.22'85 FLOOD TYPE,W=1/ 5 JEXISTEMG COMDITION>	RIVER JAN.22	785 PLOOD T	YPE/8-1/ 5	JERISTERG 4	COMBITIONS					DESIGN 013	SCHARGE (MOJ 1	RIVER JAN	DESIEW DISCHARGE(MOJI MIYER JAN,22-05 PLODG TYPE,4m1/ KO.RYICTIME FOMDITIONS	25 / L=8,8417	Outstatute o	1000			
1 -DE-THAL I WOM-INZOX	1 - DR-16.4	1985. 1.	1985. 1.22 - 1985, 1.24	1.24		•				KOZU CHITCK-RI	KOZUL-KO* 1 TYPE-KO* 1 CHITER-RYDRYD	PE-RO# 1	1985.	1985. 1.22 - 1985, 1,24	1,24			,		
SOUTRAFEST	1. 31	32 8:3	53 Brite EWDED	75	ĸ	å	37 INDIO K. APT	38 AFT# IN010	\$		30 ULTAAFERTL	ž	ñ	33	35	ĸ	ğ	37 348 18910 8: 4819 34810	10 G	ŝ
GMAK-DATA 23. 8.00 G-MAK 620.84	23. 7.00	23, 8.00 2	23, 9,00 2	25. 7.00 2	23. 5.00	23. 7.00	25. 8.00 2	350,16	326.55	0MAX-DATA 0-84X	945.02	23. 7.05	23. B.00 965.90	23. 9.00	23. 7.00 2	25. 8.00 2	5. 7.00	23. 7.00		23, 9,00
CHITEM-RYDRYO										CHITEN-RTURYO						:				
9	41 BFRE FICGR	<b>;</b>	5,	;	ş	97	A7 PIRCAGUERE AFT	48 AFTR PICGR	5		ç	41 BFRE FICGR	;	3	77	\$	97	CA CACACUCA ATTE PINCE	63.5	\$
QHAN-ONTA 23. 7.(	23, 7,00 23,10,00 50,12 348,91	25. 7.00 23. 7.00 23. 7.00 90.11 37.65 127.76	37.65		23. 8.00 77.77	23. 7.00	23, 8,00 2 51,39	23,10,00 23	25.11.00	OMAX-DATA O-MAX	23, 7.00	23. 4.00	23. 7.00	25. 7.00	23. 7.00 %	25. 5.00 2	23. 7.00	173. 7.00		23.11.00
CHITEN-DYGAYO	÷									CH17EH-RTURYO	ruero		-							
0\$	S1 BIVE HOUTH					•					8	SI RIVE HOUTH					.•			:
QMAX-DATA 23, 7,00 Q-MAX 42,23	23 361.63									CHAX-DATA C-BAX	23. 7.00	633,76								. **
											10 H21540	165HANGE CHD.	NAL RAVE 5	DESION DISCHARGE(MDJI RIVER JAM.22°8) FCOOD TYPE.Wellions	TTPECUELLES	OOVEXISTING	COMPETIONS			
DESIGNATION DISCUSSION OF TAXABLE	DESIGN DISCHARGEGNDIR RIVER JAM.22'05 PLODO TYBE-U-1/ 10.5%15 INC LUMPLIAURS HOW I TYPE-MO- 1 1988. 1.22 - 1985. 1.24	1 RIVER JAN. 2 1985. 2	# 34#.22" 65 FLOOD (TPE, 1985. 1.22 - 1985. 1.24	1.24	2011210101	dept ideas				KOZ. CH3TER-L	KOZU(-MO+ 1 TY CHITEK-RYURYO	1 TYPE-MON 1	1985.	1985, 1.22 - 1985, 1.24	1.1.24					
	31	ž.	33	7.	ĸ	*	SY SALE	SB STR INDIO.	20		NLTRAFERTL	X.	28	53 BFRE 1MD10	*	ñ	**	37 38 IMDIO R. AFTR 18010	38 FTR 18910	*
CHAK-DATA ZX. 6. 0-MAX S70.	23. 6.00 23. 7.00 23. 8.00 23. 9.00 \$70.04 \$7.17 \$73.54 630.88	37. 5.00		23. 7.00	25, B.50 35,95	25. 7.00	23. 6.00		23,10,60	DARK-DATA 23	1039.67	73. 7.00	1040.51	723.20.	23. 7.00	23. 0.00	7,00	23. 7.00	730.16	23.10.00
CMETEN-RYCHYO	40. 43.	<b>27</b>	. 4	;	. 7	;	L7 PIACAGUÉRA AP	87 ED316 ELAY	\$		9	41 BFRK PICGR	3	<b>7</b>	3	\$ .	3	47 PIACAGUERA AFTR PICGR	CR PICGR	\$
25. 7 2-68% 64. 7	25. 7.00 23.10.00 656.11	23, 7,00 116,90	25, 7,00 25, 7,00 49,34 168,24	23, 7,00	23. 8.00	25. 7.90 23. 8.00 54.78 105.A			25,11,00	GMAX-DATA 23 Q-MAX CHITEM-RYURYO	23. 7.00 315.78 RYURYO	702.87	23, 7.00	23.7.00	292,23	170,77	53. 7.00	188.44	25.10.00	688.05
CH1754-8745710	200					•					2	S1 RIVD MOUTH								
CHAX-DATA 43. 7.00	.00 23.11.00					:	<b>,</b> .		ŕ	GHAN-DATA G-MAX	23. 7.00 98.12	23.11,00								
				:																

# TABLE 2.14 ESTIMATED PROBABLE DISCHARGE OF CUBATAO RIVER (IMPROVED CONDITION)

GESIGN DISCHARGE (CUBATAG RIVER, PES.24 1971 FLOOD TYPE, WW1/ ? )

DESIGN DISCHARGE (CUBATAD RIVER, FEB.24 1971 FLOOD TYPE, Wall 25)

1.   1.   1.   1.   1.   1.   1.   1.									1 1		· ·	٠.										
11   12   13   14   15   15   15   15   15   15   15	4 + 4 0 + 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4			25.12.00 384.40		25.15.00 23.15.00			8 3,12,00 129.01	11.088 R. AFT 25.12.00 R	71000 5.12.00 570.10	4744-2474 4744-4	25.13.00 167.59	25.15.00	34.00 34.00 34.28						PILDES R. AFT PILDES 25:12:00 25:12:00 454.72 1319:52	48 4
	A TACTOR ACTIONS TO THE STATE OF THE STATE O			13 25.13.00 534.79	34 INGRTS BRG ZS.15.00 536.79		•	17 NCHET BRG WW 25.13.00 389.38		19 878 85.13.00 750.69	20 20 5.13.00 724.17	4740-X489 4740-X489	25.12.00	12 25. 9.00 126.74	13 1 25.12.00 1279.33				17 HCHET BRG MR 25.15.00 1356.00	18 187 58DEK 25, 9.00 512,20	19 25.15.00 1556.36	20 20 20 00 25,13,00
1,1,1,2,   1,1,1,1,   1,1,1,1,   1,1,1,1,   1,1,1,1,		25	22		24 141% PRQUE	: 		27. EREGUE 4. AF	ZB T PERGUE RI	29 VR MOUTH			12	22		2.5 2.5 2.5 3.5 3.5 3.5 3.5 3.5 3.5 3.5 3.5 3.5 3	ĸ		27	28	52 5	2
10   10   10   10   10   10   10   10	ATAU-XARD MAN-Q			25.12.00			25.12.00			25.13.00	•	GMAX-DATA G-MAX	25.12.00	25,13,00	35. 9.00			25.12.00	25.12.00	25.13.00	25.13.	8.5
1	. •	DESIGN DI	ISCHARGE COUR	ATAG BIVER,	FE 24 1971	I PLOOD TYPE	2 12 12 23	. •			, <b>t</b>	;	O KOTSTO	. 908890		168 34 1074		Š				
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	SHAK-DATA S-18A	38.18.00							83	1345.52		DRAX-DATA R-BAX	25.12.00	25.13.00				25. 9.00-	⋖	E.	25.15.0	E 9 E
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	ATAU-XAND X44-0			25. 9.00	25.12.00	25,12,00	25.12.00	25.12.00	1559.25	25.13.00		ATAOLKAND NAS-0	25.12.00	25.13.00	25. 9.00		25.12.00	25. 9.00	25.12.00	25.13.00	25.15.00	x 0

### TABLE 2.15 ESTIMATED PROBABLE DISCHARGE OF MOJI RIVER

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13-70   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-10   13-1	41-40-12 41-40-13	j ^s		25. 6.00	20 24 C 21 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2			23 24 1.43	13010 A. A. 25. 11.00	38 878 14910 25, 9.00 231.04	29. 23. 20. 60 23. 20. 60		30 ULTRAFERT 23. 8.00 788.23	-					25. 7.00	37 SE 1 MD10 R. AFTR 18010 25. 8.03 25. 9.00 48.78 037.15	38 FTR INDIG 23, 9,00	. A
13, 700   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150.00   23,150	47.40-KAMB 47.40-KAMB			23, 7,00	23.700	23. 7.00	25. 8.00	23. 7.00	47 11ACAGUERA A 25. 0.00 51.50	AB PTP PICGN 23.10.00 273.41	23.12.00	0MAX-DA74 G-MAX	-		42 23. 7.00				23. 7.90	######################################	778 FICGS 23. 9.00 759.16	2
DESIGN DISCAMREE (NO.1 RIVER, JAM.722-23,1983 FLOOD TYPE, WHY \$ 3)  ULTAMACLE	4740-1480 4740-14	23. 7.00 23. 7.00	51 41VR MQUIN 25.12.00 217.15			•						STAC-XATO STAC-XATO		23.20.00 377.52				•				
ULTRACENT 33 31 32 OFFE IND C		DESTER DE	SCHARGE (HOJ)	r santa t	AN.22-23.198	15 FL000 TYP	( \$ 21 m 2)	÷					BESICK DIS	(FOW) BEARD)	RIVER, 38	K.22-23.1985	5 floop TYPE	(05 /149 /3				
23-7-00 21-0-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-00 23-7-0	4 7 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	Ď	33. 7.00	32 23. 8.00 626.99				23. 7.05			25. 9.00 351.29	4 - 4 - 4 - 4 - 4 - 4 - 4 - 4 - 4 - 4 -							36 25. 7.46	38 1MOID R. APTR INDIO 23, 7.00 23, 9.00 57.08 730,50	38 23. 9.00 739.30	X
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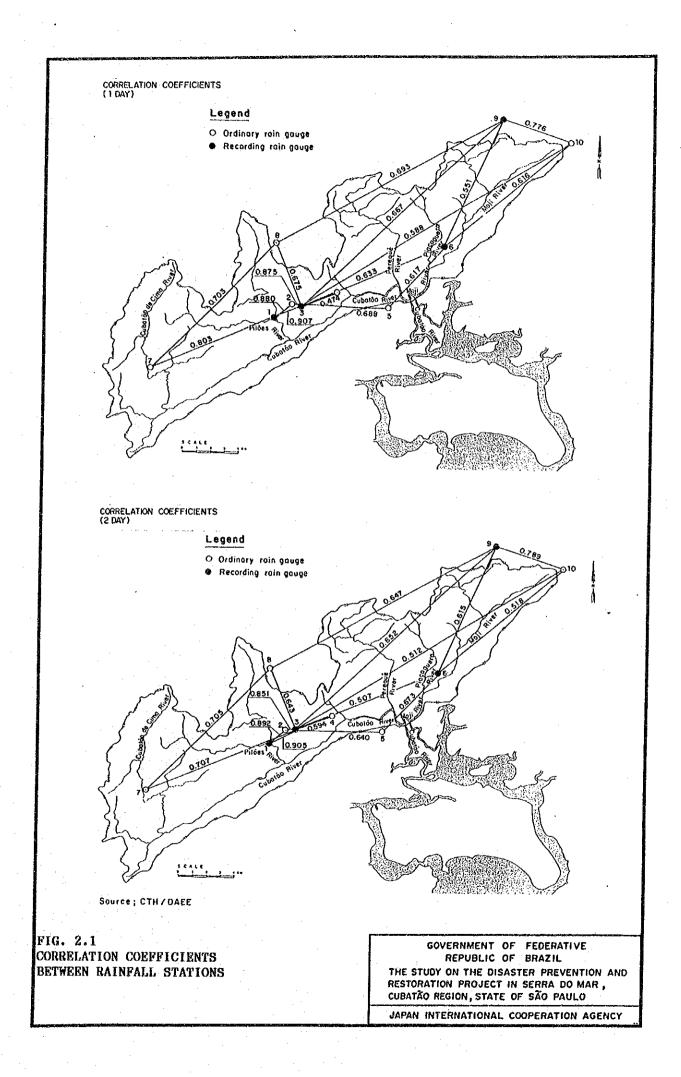
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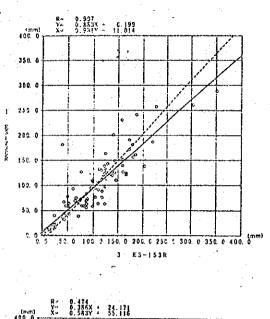
TABLE 2.16 FLOOD TO BE OVERFLOWED FROM RIVERS (CUBATÃO RIVER)

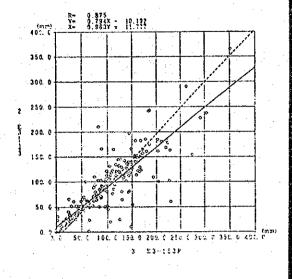
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		eriod	25	2 4 7	3,0	200	1020	126.6	310.1	237.5	806	0.0	0	0.0	00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	90
	h No.36)	Return Perio	10	c	2 6	5 Y	7.85	72.3	232.0	171.3	46.9	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
.!	Peregue River (Mesh No.36)		5	0	8 6	48.0	15.0	33.1	170.6	119.4	9.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0:0	0.0	0.0	0.0	0.0	0.0
i	ereque Ri		2	0	3 6	9 0	9 6	00	62.1	40.9	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	000	0.0
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	m3/sec		100	0	200	30.0	3000	300.0	300.0	300.0	300.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	Umit:		95	00	3 2	204.8	220.5	300.0	300.0	300.0	300.0	0.0	0.0	0.0	0.0	00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	00	000	0.0
		eriod	25	00	000	126.2	27.8	169.8	300.0	300.0	183.6	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	200	0.0
80	n No.30)	Return I	10	00	00	00	0.0	0.0	256.8	300.0	14.5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0:0	0.0	0.0	0.0	0.0	0.0	0.0	00
ć	IVET (MES		5	0.0	0	000	0.0	0.0	69.7	156.0	0:0	0.0	0:0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	200	0:0
, ,	Cubatao Kivet (Mesn No.30		2	0.0	0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		0.0
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	Unit: m3/sec		8	0.0	0.0	156.8	58.1	135.7	551.7	7.56.1	145.9	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	000	0.0
	Unit		8	0.0	00	0:0	0.0	3.5	373.4	543.1	24.00	0	0.0	0.0	00	0.0	0.0	O (	0.0	0.0	0.0	0.0	00	000	9 0 0 0	000	0.0
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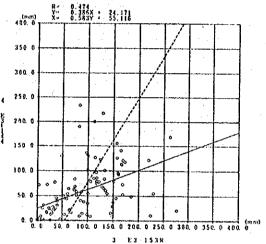
TABLE 2.17 FLOOD TO BE OVERFLOWED FROM RIVERS (MOJI RIVER)

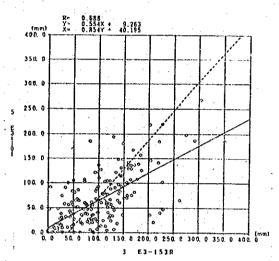
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	Doring	25	6	20.10	35.78	8	17.63	1.89	00.0	000	000	000	8	000	000	000	000	000	000	000	00.0	0.00	00.0	0.00	00.0	0.0	00.0	0.00
	Denim	10	17.60	17.02	23.18	0.13	12.23	0.24	80.0	000	000	00.0	000	000	000	000	000	000	000	800	800	000	90.0	0.00	000	8	000	0.00
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		ςς Θ	905 21	160.62	20705	20.4.00	00007	9	800	0.00	0.00	0.00	000	000	000	0.00	0.0	0.0	0.0	800	0.00	800	0.00	000	000	800	000	0.00
	n Period	25	714.08	145.40	210.40	10070	47.77	3	000	0.0	0.00	0.00	90.0	8	900	000	0.0	000	0.00	0.00	0.0	8	0.0	0.00	800	9.8	0.00	0.00
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ಕ	-	3	314.59	60.43	16.20	12421	154.31	3	00.00	8	000	0.00	000	0.0	0.0	90.0	0.0	900	8	000	8	8	000	900	8	9	800	0.00
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	Rerum Period	22	121.41	117.23	8	7. 17	77.78	100	5.5	3	8	8	8	8	0.0	0.00	00.0	000	8	000	8	8	9.6	38	38	3 8	8	9 9
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Piasaguera River		5	55.55	6139	44.08	20.04	22.04	100	767	33	00 5	000	8	8	900	200	8	8	8	200	20.0	33	200	38	200	3 6	3 6	3
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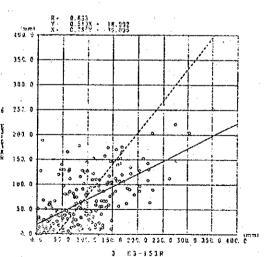


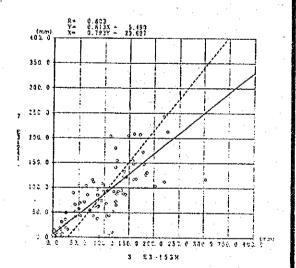










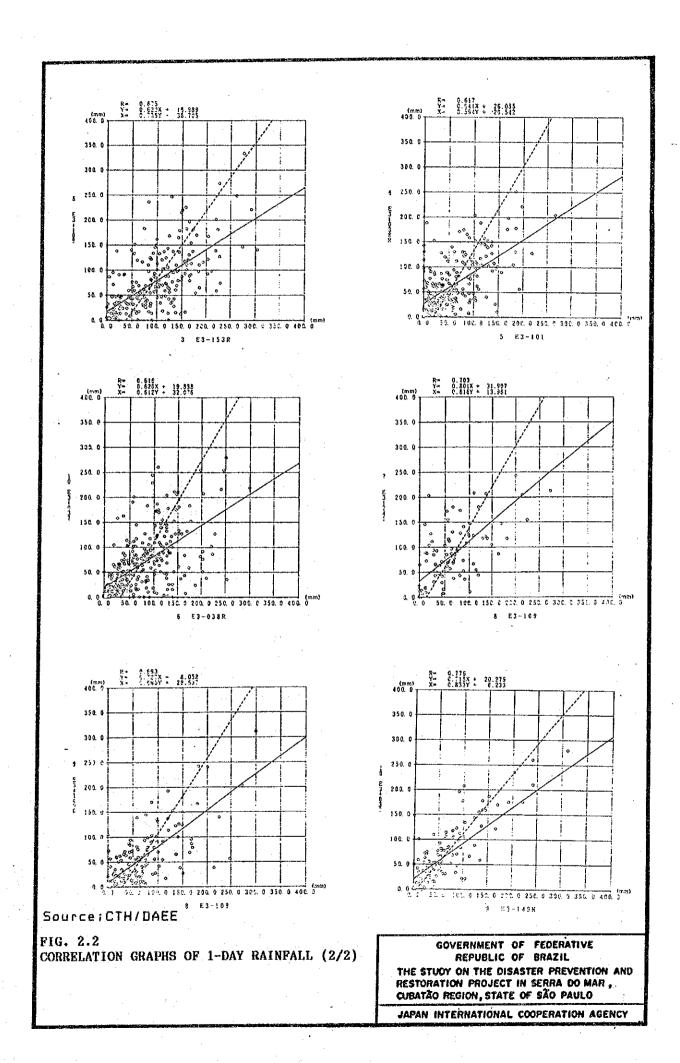


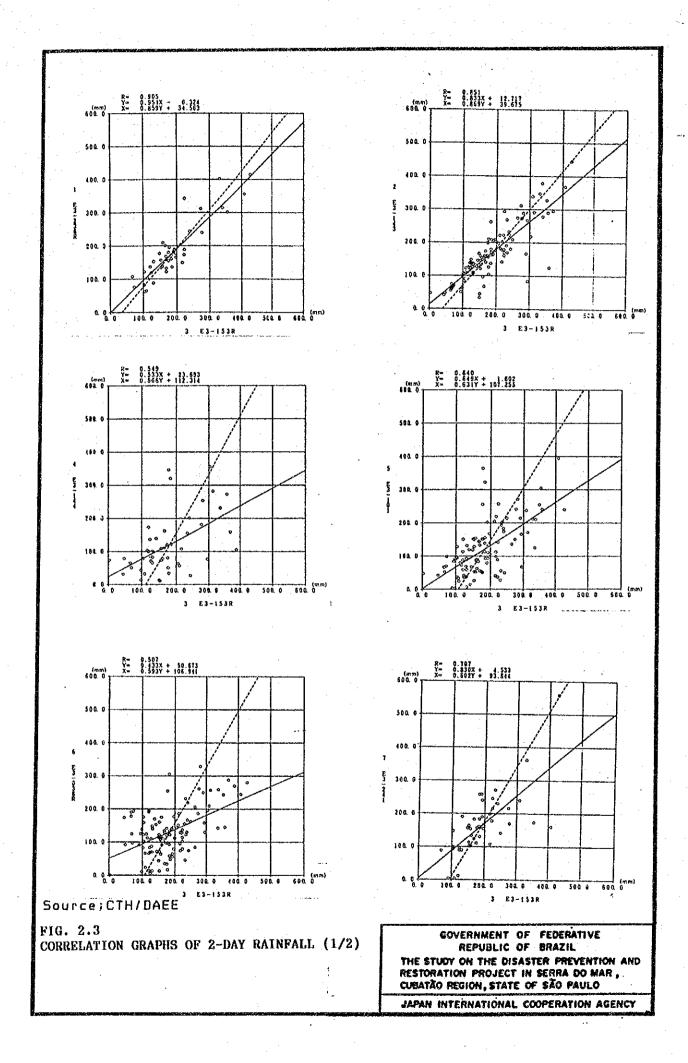
Source; CTH/DAEE

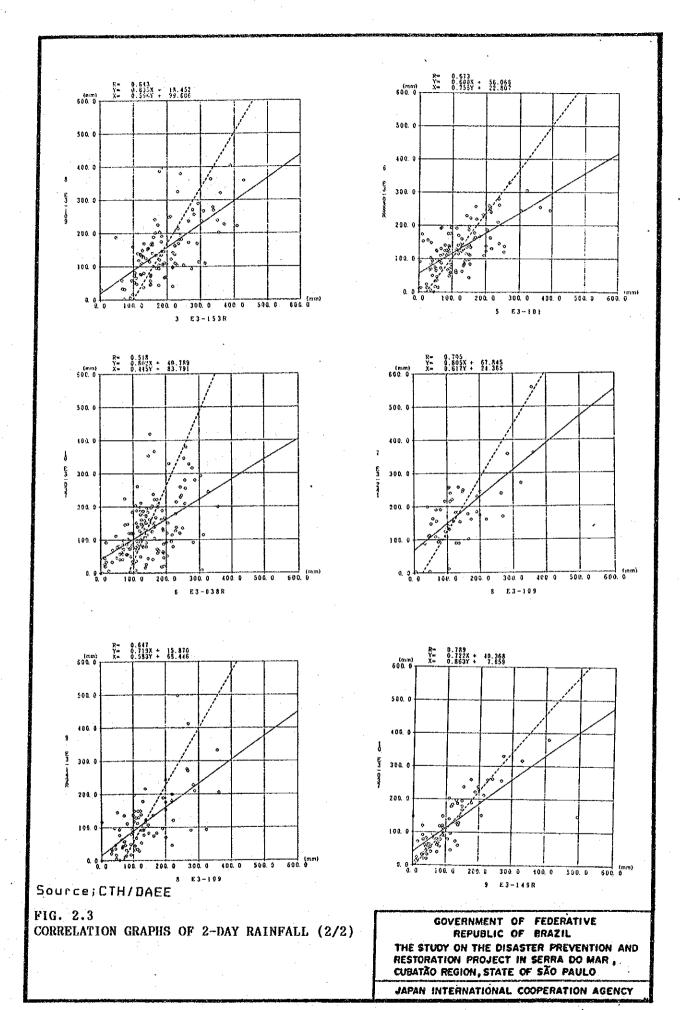
FIG. 2.2 CORRELATION GRAPHS OF 1-DAY RAINFALL (1/2)

GOVERNMENT OF FEDERATIVE REPUBLIC OF BRAZIL THE STUDY ON THE DISASTER PREVENTION AND RESTORATION PROJECT IN SERRA DO MAR, CUBATÃO REGION, STATE OF SÃO PAULO

JAPAN INTERNATIONAL COOPERATION AGENCY







17:17

AVAILABILITY OF RAINFALL RECORDS

	Marc.72	Jan.50	Sep. 52	Nov. 49 Jun.69 Jan. 84	Aug.44 Jan.48 Mar.55	Jan.36 Nov.71	Jun.72 Aug.86	Jan.44	And the state of t	Jan.36	
Station Year	E3 - 236 R	E3 - 143	E3 - 153 R	E3 - 144	E3 - 101	E3 - 038 R	E3 - 241	E3 - 109	E3 - 149 R	E3 - 037	
g.	F-12.	N	<u>(10)</u>	4	Ŋ	<b>@</b>	~	@	თ	(2)	

Source: CTH/DAEE

FIG. 2.4
RAINFALL STATION USED FOR
CALCULATION OF BASIN MEAN RAINFALL

GOVERNMENT OF FEDERATIVE
REPUBLIC OF BRAZIL
E STUDY ON THE DISASTER PREVENTION

Complement of Shortage of Observation

Recording Rain Gauge

Adopted Stations

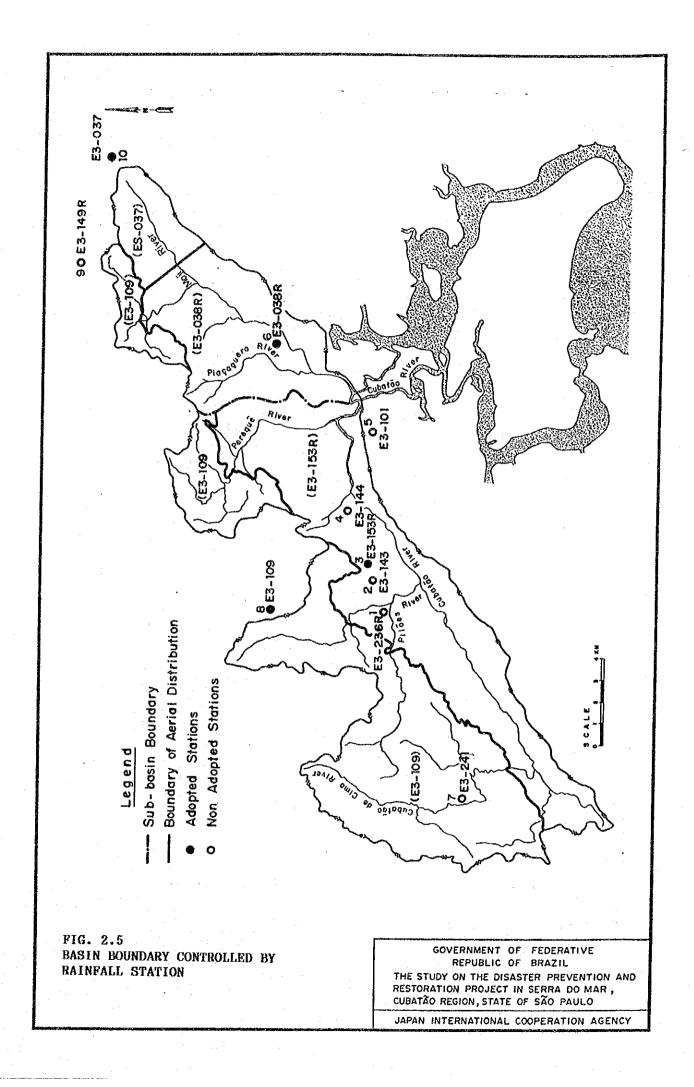
Ordinary Rain Gauge

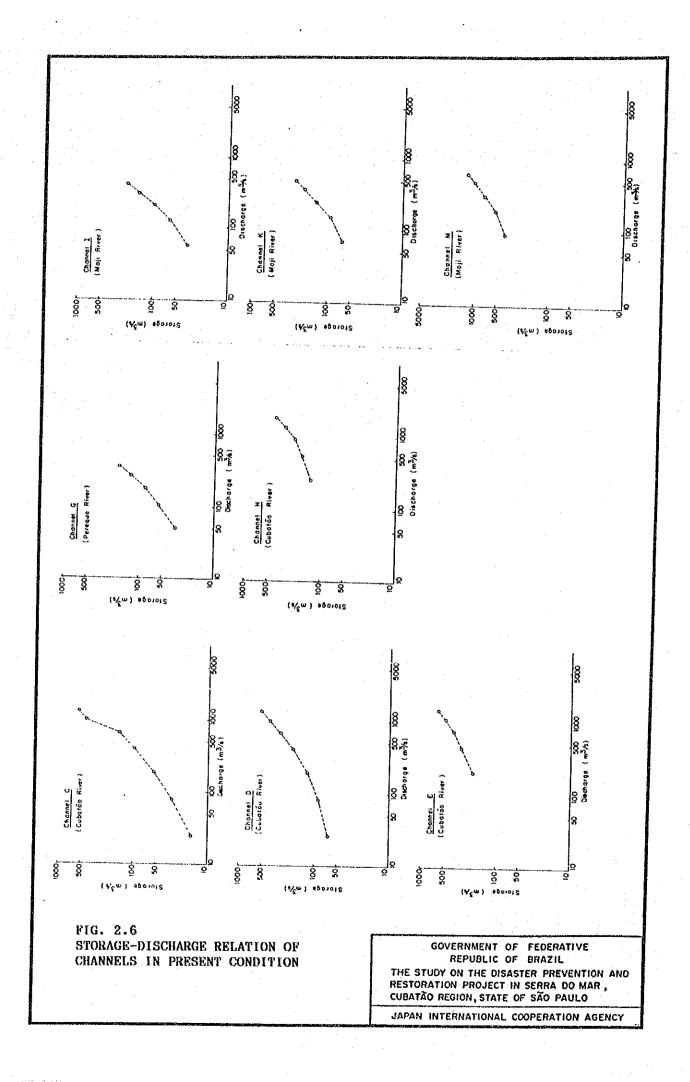
THE STUDY ON THE DISASTER PREVENTION AND RESTORATION PROJECT IN SERRA DO MAR, CUBATÃO REGION, STATE OF SÃO PAULO

JAPAN INTERNATIONAL COOPERATION AGENCY

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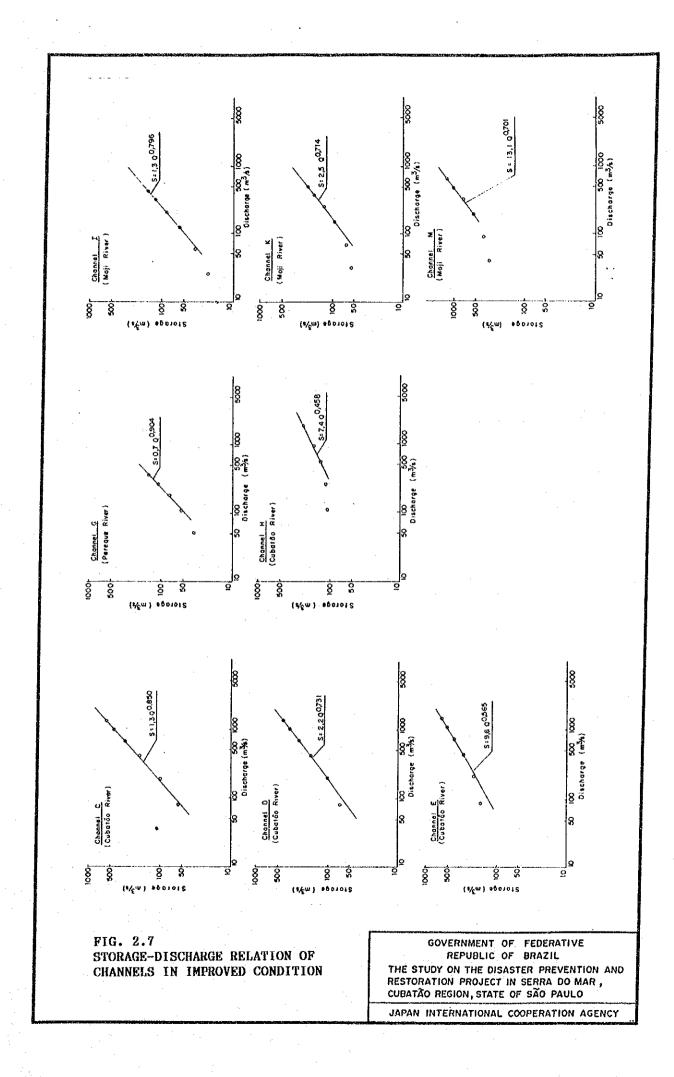


TABLE 3.1 LONGITUDINAL PROFILE OF EXISTING CUBATÃO RIVER

Sact	 H				Deepest -Riverbed		و جربی جنگ عبید دیگی میشد بیرین چین کار جاد در مقت کارک چین خین میشد آمید کردن کارک کار	Eleva	tion	⟨EL.	m )		
	Lq .	140	Single	Accum.	(EL. m)	(m)	Left Bank					Right	Dike
	C.	0	0	0		80	0.47		0.73				
		1	350	350		78	1.05	100	0.66		٠.		
		2		500	-4.70	82	0.91		1.95				
		3	530	730	-5.30	127	1.38		1.21				
	C.	4	140	870			2,72		1.38		**		2.41
		5	180	1050		85	2.52		1.54				1.93
		6	510	1590		. 93	3.200		2.30				3.22
		7	190	1450		703	3.100		2.50				2.95
		8	530	1680	-5.10	90	2.237		2.50				2.91
		9		1880		97	2.86		2.44				2.49
		10	500	2080	-4.60	97 99	2.79		2.40				2.98
•		77	190	2270	-3.80	77	3.31 2.91		2.70	·			3.53
		13	780 500	2470 2650	-3.80 -4.30	93 90	2.97		2.65 5.43				3.54° 3.57
		14	240	2890	-4.60	95	6.10		3.94	4.			3.93 3.93
		15	200	3090			and the second s		3.14				3.10
		16	190	3280	-3.10		4.03		3.05				3.86
		17	270	3550	-3.40				3.44			3	J. UU
		18	200	3750	-2 70	88	6.22		5.20				
		17	190	3940	-5.70		3.83		3.00				
-		50	200	4140	-4.30	70	6.62		7.17				
		51	550	4360	~2.20	80	6.09		6.12				
	Ĉ.		225	4585	-3.60		·		6.82				
	C:		240	4825		74	7.08	1	6.76			•	
		24	170	4995	-1.40		7.22		7.17				
		25	510	5205	0.00	240	6.784		7.04			•	
	С.		220	5425	-0.40	530	14,20		6.59				
	C.		140	5585		63	23.00		6.13				
	С.	28	170	5755	0.20	45	8.58		4.36	-			
	С.		190	5945	1.80	58	6.70	•	5.25				
		30	170	6115	1.20	118	18.32		6.09				3.19
		31	210	6325		1.10	9.27		6.45				7.97
	C:		210	<b>653</b> 5	0.50	58	14.23		5.31			. 6	.30
	<b>C</b> '.		170	6705	0.20	75	5,41		5.67				
	<b>C</b> .:		240	6945	1.80		6.35		5.20				
	<u>C</u> .:		500	7145	2.20	63	7.57		6.16				
	<u>c</u> .:		450	7595	1.60	85	7.77		3.06				
	<b>C</b> .:		400	7995	2.10	85	9.90		. 337			-	
	C.:		400	8395	3.10	80	6.74		4.79	•	* .		
	<u>C</u> .:		390	8785	3,20	89			8.74			•	
	C.		410	9195	5.36	120	10.45		1.91				
	<u>C</u> .		440	9635	7.22	105			0.39	•			
	U,	42	. 310	9945	8.88	150	26.500		9.45				

(m, IGGSP)

(m, IGGSP)

TABLE 3.2 LONGITUDINAL PROFILE OF EXISTING PEREQUE RIVER

Sprit	2	Uistanc	(B)	Deepest	River			Elevation	on (EL.	ê		
		Single	Accum.	(EL.m)	(E)	Left	Bank	Right B	ank Left	t Dike	Right D	1 ' 77   00
	0	0	0				į.		,0	1		1 6
	₩	220	000		) (M		•	) (i	- 0 	4	л . (	u i
	ณ	150	370	i q				u c	0 2	งับ บั	วัง ขัง	უ .
	ທ	040	6.40	i		. •	•	ម (	, 0	•	m i	<b>.</b>
	4	020	000	iç	1 C		•	IJ <	บี่	•	ന	
	V.	i u	4	òç			•	4 (	ม สำเ	٠.	4.6	_
	40	100	240	•				m ·	ਜ਼ ਲ਼			ω
	1	7 6	7 1				٠.	4	.15		۲.	٥
	٠ (	1 (	14 to 1			•	•	ব	<u>-</u>	•	7.	0
	ומ	n n	1645	•		-	•	IJ	66.		4	
	0~	190	1832	•		•	•	7	47		1	4 0
	40	150	1985	•	10.		٠.	. 4	(1	•		
	돢	D D D	2235		70	-	-	) 4	1 7 C	٠		
	<u>ជ</u>	310	25.45	•	40		•	0 4	0 0 7 5	•	_	
0- 미	೮	170	2715	4.40	- I	-	•	. 0 4	u 0			
	14	120	2835		O I			o Ç	7 6			
	T C	220	3055			<del></del>	•	) C	<b>,</b>			
	16	175	3830		6.6							
	17	180	3410			i û	) (	H C	 			
	გქ დ	250	3660	l)		ים ימ	. 4	200	3 (			

(m,IGGSP)

TABLE 3.3 LONGITUDINAL PROFILE OF EXISTING MOJI RIVER

j	1								
Sec	n t N	Distance (m	) Deepest	7 2	İ	Elevat	ion (E	El. m)	
i	· [	Single Accum	(EL.	≩ j ~	Left Bank	Right	Bank	eft Dike	Right Dike
			(O)	0	0-0-			-	
		009	ពុ	0	) <del>-</del>		) C		
>		1090	ี (1	0	ια		1 1.		
		2 069 5	•	0	10	ĺ	· ď		
	•	190	ល់	0	2. 3	<b>)</b>	5		
		160 27	რ				·		
		240 P.0	1	0	ณ		•	-	
		170 3£	10 –P. 4	0	เ				
		26 062	1	o	o o				
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	٠.	330	ດ  -	0	4		į u		
	ㅋ '	000	7	0	7	•	, U		
	~.	180 43	7	<b>41</b>	4.9	,	, w		
٠	~;	200 45	<b>.</b>	9	ด				:
	٠.	210 47	<b>→</b>	0	ω 4			:	
	Σ:	180 45	730 -1.3	35	 	,	ה ה ה		
٠,	44	260 51	-1	0	0				
	T .	190 50	1	0	3.6	•	! C		
	٠, i	250 56		4	4.0	(**	. U.		
	u i	165 57	SO	ຸດ	4 4	7			
	U (	210 55	şi I	0	5.0	7	4.29		
	U (	5005	+ + -	ው	9.0	*	7		
	u I	500 63	7.1.		4.9		4		
	(U I	100 6T	P		4		į.		
	เบ	230 68		,	7.42	) <b>/</b>			
٠.	O.	130 65	ເນ		(C)	. •	. α		
	ณ.	230 71	໙	<b>~</b>	4.5	3 4	! 4		
	N	260 74	໙		6	, <del>-</del>	. 4		
	U	320 77	4		6 7 9	1 (1) 1 •••			
	ന	400 81			0				
1						i	)		

(m, IGGSP

TABLE 3.4 LONGITUDINAL PROFILE OF EXISTING PIAÇAGUERA RIVER

1 1	1 Q	: 1									٠										
[ ] [ ]	1 4																				
1 1	1 02	1																		•	
		1																			
	1 (4) 1 (4) 1 (4)	1																			
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 vati	ht 33	1	<b>⊣</b> (	<b>η</b> ΄ ()	<b>1</b> £	ν,	4	4	Į,	יו נ	n •	4.	0	,,		0 (	N	27	Q	1 4	
Н	Rig	1 .																			
 	Bank	1 0	) (C	, Q	, c	, ,	<b>1</b> 1	æÖ.	(	ប	) a	0 1	7.91	S	, r		9	0	4.76	4 05	
1	 Left	! ! !												6-4	ς-	<b>₹</b> ₹		N	ΙŅ	ı in	
River	dth (m)		i 4	20.	) t-	, 7	† f	າງ <b>⊣</b>	10	10	C C	` (	⊃ -†	22	C.C.	) (		40	37	0.9	
1 1 4 1 5	3 0	101	.20			,	,		ບຸ	۲,	C	, £	٧.	Ö	4	Ç	1 (	`	o	ល	
1 0	Kiver (EL.	, T	i ( <del>1</del>	    	0 -	c	י כ	•	e⊣	ç-4	4	. L	` ;	10	ç~(	7,	,	0	(7	4 7	
(E)	ארנים. הטטטשי	0	300	570	QQ:	TU TU	0	` (	30 30	₹~i	4	Û	1 {	Y	Š	m	ľ	ו מ	N	8	: i   #
	- C	0	300	270	417	367	440	1 0	)     	230	490	787	1 ,	7 4 7	173	237	101	, (C	7.40		
   0   .2		0 .	_	Ν.	m	4.	m	7	0 !		<b>40</b>	0	,	) t	<del>,</del>	12	رب س	, ,	<b>†</b> 1		111
ر د خ	) i	Ω	Ω_	Δ.	ο.	<u>α</u>	Ω.	Ω	Ĺ	Ļ	a.	α.	0	. (	Ļ	α.	Q.	. 0	. 1	ı.	

TABLE 3.5 LONGITUDINAL PROFILE OF EXISTING INDIO RIVER

	Left Bank Right Bank Left Dike Right Dike	2.46 2.91 9.35 9.04 22.79 23.89 27.00 33.20
1 1. 0	(E)	3 H 4 S 3 4 4 S
(m) Despest River	(EL. m)	0 -0.19 25 1397 5.47 14 2297 22.37 14 2567 31.73 28
	CE I	
Distanc =t. No	7 T	0 1397 900 270
Sert. No.	Sing	M1.0 0 M1.1 1397 M1.2 900 M1.3 270

### TABLE 3.6 ESTIMATED BANKFUL CARRYING CAPACITY OF CHANNEL (PRESENT CONDITION)

	CUBATAD	RIVER					HOJI RIVI	ER			•
	Section		nce(m)		ity			Distan	ce(m)		
		Sing.	Accn.	H(m,1885P)	(a/Em)()		22211011	Sing.	Acem.	H(m,IGGSP)	O(m3/s)
10 111 123 134 15 16 17 18 19 20 21 22 23 24 25 27 28 29 31	C2	0 160 150 240 120 205 190 185 260 190 270 205 170 270 270 270 270 270 240 145 216 216 216 216 216 216 216 216 216 216	0 160 310 550 670 870 1,075 1,265 1,450 1,710 2,090 2,280 2,785 2,785 2,785 3,130 3,605 3,775 3,800 3,605 3,775 3,800 4,670 4,670 4,835 5,057 5,475 5,610 5,770 5,760 5,770 5,780	0.64 1.37 1.84 2.95 2.02 2.75 1.84 2.92 2.95 2.95 2.95 3.54 3.93 3.10 3.75 4.66 5.93 5.35 6.78 6.78 6.78 6.78 7.56 4.29 4.39	177 1794 1,220 1,032 2,019 333 1,215 1,649 1,302 1,045 946 836 826 1,061 1,101 750 942 1,177 2,171 1,753 1,740 1,432 1,095 1,104 1,428 1,292 1,308 1,926 1,849 516 281	3 4 5 6 7 8 9 10 11 12 13 14 15 16 17	M1 H2 M4 H6 H7 H8 H10 H10 BRG: H12 H13 H14 H15 H14 H18 H22 H23 H23 H24 H25 H26 H27 H27 H28 H28 H28 H28 H28 H28 H28 H28	0 0 0 0 0 0 0 0 0 0 0 10 15 16 16 245 160 245 160 245 120 130 200 200 205 180 275 190 205 190 205 190 205 205 205 205 205 205 205 20	0 810 1,435 2,750 3,420	0.72 0.72 1.46 0.98 0.94 1.41 12.20 1.55 1.98 2.41 4.14 4.14 4.14 2.46 3.04 2.56 2.69 3.14 2.55 1.90 4.30 4.36 4.63 5.69 4.17 4.17	90 80 280 118 66 67 124 105 132 190 249 807 520 186 243 186 243 177 183 198 231 248 255 273 388 255 273 389 256 273 389 256 273 273 273 273 273 273 273 273 273 273
38 39 40	C32 C33 SUEIR	200 165 120	6,365 6,530 6,650	5.36 6.30 6.08 5.20	569 373 499 405 76		PEREQUE	RIVER			
41	C34 C35	125	4 776	P 0.4	76 158 104 939				ice(m)	Сарас	
43	C36 C37	450 405	7,425 7,830	5.67 8.79 10.07 6.36	939 1,359		Section	Sing.		H(m,IGG5P)	
45 46 47 48 49	C38 C39 C40 C41 C42	425 405 420 450 315	8,255 8,660 9,080 9,530 9,845	6.36 11.58 12.02 10.89 12.60	175 1,606 1,639 369 729	12 33 44 55 66 77 8 9 10 11 11 12 13 14 15 16 17 18 19 20 21 22	C8 PEO PE1	0 150 220 150 240 135 80 55 155 205 170 235 140 255 315 145 125 210 175 250	0 150 370 520 595 975 1,030 1,185 1,390 1,560 2,120 2,455 2,690 2,455 2,690 3,190 3,365 3,550 3,800	2.47 2.43 2.08 2.47 1.84 1.84 4.15	1,045 160 128 163 105 104 303 301 461 473 444 483 609 886 793 471 673 862 400 379

TABLE 3.7 PROPOSED LONGITUDINAL PROFILE OF CUBATÃO RIVER (1/2)

Longitudinal Data of CUBATAO River (Case C-1)

	Section	Distan	ice (m)	Gradient of	Design Discharge	Design E		(m.IGGSP)
	No.	Single	Accum.	River bed		River Bed		
٠.	. C.3	0	. 0	1/2560	2,300	-3.90	4.10	5.30
	l. Raitway	110	110	1/2560	2,300	-3.86	4.14	5.34
. 1	C.4	30	140	1/2560	2,300	-3.85	4.15	5.35
1	l 6.5	180	320	1/2560	2,300	-3.78	4.22	5.42
1	C.6	210	530	1/2560	2,300	-3.70	4.30	5.50
- 1	C.7	190	720	1/2540	2,300	-3.63	4.37	5.57
	C.8	230	950	1/2560	2,300	-3.54	4.46	5.66
-	Af. Conf.Pereque	100	1,050	1/2560	2,300	-3.51	4.49	5.69
	Bf. Conf.Pereque	0	1,050	1/2560	1,800	-3.51	4.49	
1	C.9	100	1,150	1/2560	1,800	-3.47	4.53	5.69
1	€.10	200	1,350	1/2560	1,800	-3.39	4.61	5.69
:	C. 11	190	1,540	1/2560	1,800	-3.32	4.68	5.69
	C. 12	200	1,740	1/2560	1,800	-3.25	4.75	5.75
2		180	1,920	1/2560	1,800	-3.18	4.82	5.82
1	C. 14	240	2,160	1/2560	1,800	-3.10	4.91	5.91
i	C. 15	200	2,360	1/2560	1,800	-3.01	4.99	
i	C. 16	190	2,550	1/2540	1,800	-2.94		5.99
•	C. 17	270	2.820	1/2560	1,800		5.06	6.06
į	C. 18	200	3,020	1/2560	1,800	-2.84	5.16	6.16
•	Weir Bn.	170	3,190	1/2560		-2.76	5.24	6.24
_	Weir Up.	170	3,170	1/1530	1,800 1,800	-2.70	5.30	6.30
•	C. 19	20	3,210	1/1530	1,800	-1.70	5.30	6.30
ij	C 20	200	3,410	1/1530		-1.69	5.31	6.31
•	C.21	220	3,410		1,800	-1.56	5.44	6.44
,	C.22	225	3,855	1/1530 1/1530	1,800	-1.41	5.59	4.59
3		240	4,095		1,800	-1.27	5.73	6.73
١	C.24	240 170		1/1530	1,800	-1.11	5.89	6.89
:	C.25	210	4,265	1/1530	1,800	~1.00	6.00	7.00
:	C.25		4,475	1/1530	1,600	-0.86	6.14	7.14
,	€.27	220	4,695	1/1530	1,800	-0.72	6.28	7.28
:	C.27	160	4,855	1/1530	1,800	-0.61	6.39	7.39
٠		170	5,025	1/1530	1,800	-0.50	4.50	7.50
-	Bridge	130	5,155	1/1530	1,800	-0.41	6.59	7.59
-	Bridge	. 0	5,155	1/1530	1,600	-0.41	6.59	7.59
•	U.E.	60	5,215	1/1530	1,600	-0.38	6.62	7.62
į	0.00	170	5,385	1/1530	1,600	-0.26	6.74	7,74
4	×	210	5.595	1/1530	1,600	-0.13	4.87	
	V. V.	210	5,805	1/1530	1,600	0.01	7.01	8.01
;	C.33	170	5,975	1/1530	1,600	0.12	7.12	8.12
-	Weir	120	6,095	1/1530	1,600	0.20	7.20	8.20
	Weir	0	6,095			0.20	7.20	8.20
	€.34	120	6,215					
	C.35	200	6,415					

TABLE 3.7 PROPOSED LONGITUDINAL PROFILE OF CUBATÃO RIVER (2/2)

Longitudinal Data of CUBATAO River (Case C-2(1))

Section	Distan	sca (m)	Gradient	Design Discharge	Design E	levation	(m.1665P)
No.	Single	Accum.	River bed	(m3/s)	River Bed	H.W.L.	Dike Crown
C.3	0	0	1/2560	1,300	-3.90	2.60	3.60
Railway	110	110	1/2560	1,300	-3.86	2.64	3.64
C.4	30	140	1/2560	1,300	-3.85	2.65	3.65
C.5	180	320	1/2560	1,300	-3.78	2.72	3.72
C.4	210	530		1.300	-3.70	2.80	3.80
C.7	190	720	1/2560	1.300	-3,63	2.87	3.87
C.8	230	950		1,300	-3,54	2.96	3.96
Af. Conf. Pereque	100		1/2560	1,300	-3.51	2.99	3.79
Bf. Conf.Pereque	0	1,050	1/2560	650	-3.51	2.99	3.99
C. 9	100	1,150	1/2560	850	-3.47	3.03	4.03
C. 10	200	1,350	1/2560	850	~3.39	3.11	4.11
C. 11	190	1,540	1/2560	850	-3.32		
C. 12	200	1,740	1/2560	850	-3.32		4.18
C. 13	180	1,920	1/2560	850		3 25	4.25
C. 14	240	2,160			-3.18	3.32	4.32
C. 15		2,360	1/2560	850	-3,09	3.41	4.41
C. 15	200		1/2560	850	-3.01	3.49	4.49
	190	2,550	1/2560	850	-2.94	3.56	4.56
C.17	270	2,820	1/2560	. 850	-2.84	3.66	4.66
C.18	200	3.020	1/2560	850	-2.76	3.74	4.74
Weir Dn.	170	3,190	1/2560	850	-2.70	3.80	4.80
₩eir Up.	0	3,190	1/1120	850	-1.00	3.80	4.80
C. 19	20	3,210	1/1120	850	-1.02	- 3,78	4.78
C.20	200	3,410	1/1120	850	-1.18	3.62	4.62
C.21	220	3.630	1/1120	850	-1.36	3,44	4.44
C.22	225	3,855	1/1120	850	-1.54	3.26	4.26
C.23	240	4.095	1/1120	850	-1.74	3.06	4.06
C.24	170	4,265	1/1120	850	-1.68	2.92	3.92
C.25	210	4,475	1/1120	850	-2.05	2.75	3.75
C.26	220	4,695	1/1120	850	-2,23	2.57	3.57
C.27	160	4,855	1/1120	850	-2.36	2.44	3.44
C.28	170	5,025	1/1120	850	-2.50	2.30	3.30
Bridge	130	5,155	1/1120	850	-2.60	2.20	3.20
Bridge	Õ	5,155	1/1120	500	-2.60	2.20	3.20
C. 29	60	5,215	1/1120	500	-2.65	2.15	3.15
C.30	170	5,385	1/1120	500 500	-2.79	2.13	3.13
C.31	210	5,595	1/1120	500 500	-2.74	1.84	
€.32	210	5,405	1/1120	500 500	-2.70 -3.13		2.84
C.33	170	5,975	1/1120	500 500	-3.13 -3.27	1.67	2.67
Veir	170	6,095				1.53	2.53
		01010	1/1120	500	-3.37	1.43	2.43
					1.60	6.40	7.40
Weir C.34 C.35		0 120	0 120	0 120	0 120	0 120	0 120 120

Longitudinal Data of CUBATAO River (Case C-2(2))

	Section	Distan	ce (m)	Gradient of	Design Discharge	Design E	levation	(m.1885P)
	No.	Single	Accum.	River bed	(m3/s)	River Bed	H.V.L.	Dike Crown
-	С.3	0	0	1/2560	1,600	-3.90	3.30	4.30
	Railway	110	110	1/2560	1,600	-3.86	3.34	4.34
1	C.4	30	140	1/2560	1,600	-3.85	3.35	4.35
3	€.5	180	320	1/2540	1,600	-3.78	3.42	4.42
•	€.6	210	530	1/2540	1.400	-3.70	3.50	4.50
-	C.7	190	720	1/2560	1,600	-3.63	3.57	4.57
i	8.3	230	. 950	1/2560	1,600	-3.54	3.66	
	Af. Conf.Pereque	100	1,050	1/2560	1,600	-3.51	3.69	4.69
-	Bf. Conf.Pereque	0	1,050	1/2560	1,100	-3.51	3.69	4.69
- !	C.9	100	1,150	1/2560	1,100	-3,47	3.73	4.73
	C.10	200	1,350	1/2560	1,100	-3.39	3.81	4.81
·	C.11	190	1,540	1/2560	1,100	-3.32	3.88	4.88
:	C. 12	200	1,740	1/2560	1,100	-3.25	3.95	
Z	C. 13	180	1,920	1/2560	1,100	-3.18	4.02	
	C. 14	240	2,160	1/2560	1,100	-3.09		5.11
į	C.15	200	2,360	1/2540	1,100	~3.01	4.19	5.19
i	C. 16	190	2,550	1/2560	1,100	-2.94	4.26	5.26
	C. 17	. 270	2,820	1/2540	1,100	-2.84	4.36	5.36
1	C.18	200	3,020	1/2560	1,100	-2.76	4,44	5.44
-	Weir Dn.	170	3,190	1/2560	1,100	-2.70	4.50	5.50
-	Veir Up.	0	3,190	1/1160	1,100	-1.00		5.50
1	C. 19	20	3,210	1/1160	1,100	-0.98	4.52	5.52
į	C.20	200	3,410	1/1160	1,100	-0.61	4.69	5.49
	C.21	220	3,630	1/1160	1,100	-0.62	4.58	5.88
1	C.22	225	3,855	1/1160	1,100	-0.43	5.07	6.07
3	C.23	240	4,095	1/1160	1,100	-0.22	5.28	6.28
1	C.24	170	4,265	1/1160	1,100	-0.07		6.43
•	C.25	210	4,475	1/1160	1,100	0.11	5.61	6.61
•	C.26	220	4,695	1/1160	1,100	0.30	5.80	6.80
	C.27	160	4,855	1/1160	1,100	0.43	5.93	6.93
1	C.28	170	5,025	1/1160	1,100	0.58	6.08	7.08
-	Bridge	130	5,155	1/1160	1,100	0.69	6.19	7.19
-	Bridge	0	5, 155	1/1160	750	0.49	6.19	7 19
•	C.29	60	5,215	1/1160	750	0.74	6.24	7.24
i	C.30	170	5,385	1/1160	750	0.89	6.39	7.39
4	C.31	210	5,595	1/1160	750		6.57	7.57
!	C.32	210	5,805	1/1160	750	1.25	6.75	7.75
. 3	C.33	170	5,975	1/1160	750	1.40		7.90
*	Welr	120	6,095	1/1160	750	1.50	7.00	8.00
	Aeir	. 0	6,095			1.50	7.00	8.00
	C.34	120	6,215					
	C.35	200	6,415	*				

TABLE 3.8 PROPOSED LONGITUDINAL PROFILE OF PEREQUE RIVER

### Longitudinal Data of PEREQUE River (for Case C-1)

	Section	Distan		Gradient	Design Discharge	Design E	levation	(m.IGGSP)
	No.	Single	Accum.	River bed	(m3/s)	River Bed	H.W.L.	Dike Crawn
	Pe.O	0	0	1/1200	500	-2.00	4.50	\$.70
i	Pe. 1	220	220	1/1200	500	-1.80	4.50	5.70
1	Pe.2	150	370	1/1200	500	-1.70	4.50	5.70
	Pe.3	240	610	1/1200	500	-1.50	4.50	5.70
-	Railway Br.	135	745	1/1200	500	-1.40	4.50	5.70

### Longitudinal Data of PEREQUE River (for Case C-2(1))

	Section	Distan	ice (m)	Gradient of	Design Discharge	Design E	levation	(m,IGGSP)
	No.	Single	Accum.	River bed	(m3/s)	River Bed	H.W.L.	Dike Crown
	Pe.O	0	0	1/1200	500	-2.00	3.00	4.00
t	Pe.1	220	220	1/1200	500	-1.80	3.00	4.00
1	Pe.2	150	. 370	1/1200	500	~1.70	3.00	4.00
	Pe.3	240	610	1/1200	500	-1.50	3.00	4,00
-	Railway Br.	135	745	1/1200	500	-1.40	3.00	4.00

### Longitudinal Data of PEREQUE River (for Case C-2(2))

	Section		ce (m)	Gradient	Design Discharge			(m,IGGSP)
	No.	Single	Accum.	River bed	(m3/s)	River Bed	H.W.L.	Dike Crown
-	Pe.0	0	0	1/1200	500	-2.00	3.70	4.70
1	Pe.1	220	220	1/1200	500	-1.80	3.70	4.70
1	Pe.2	150	370	1/1200	500	-1.70	3.70	4.70
ŧ	Pe.3	240	610	1/1200	500	-1.50	3.70	4.70
	Railway Br.	135	745	1/1200	500	-1.40	3.70	4.70

TABLE 3.9 PROPOSED LONGITUDINAL PROFILE OF MOJI RIVER

Longitudinal Data of MOJI River (Case M-1)

Section	Distar	nce (m)	Gradient	Design Discharge	Design E	levation	(m, IGG5P)
No.	Single	Accum.	River bed		River Bed	H.W.L.	Dike Crow
н.з	0	0	1/2460	1,000			
H.4	670	690	1/2460	1,000	-2,20	4.00	5.0
M.5	190	880	1/2460	1,000	-2.12	4.08	5.0
M.6	160	1,040	1/2460	1,000	-2.06	4.14	5.1
H.7	240	1,280	1/2460	1,000	-1.96	4.24	5.2
H.8	170	1,450	1/2460	- 1,000	-1.89	4.31	5,3
M.9	290	1,740	1/2460	1,000	-1.77	4.43	5.4
M. 10	170	1,910	1/2460	1,000	~1.71	4.49	5.4
H.11	330	2,240	1/2460	1,000	-1.57	4.63	5.6
M. 12	230	2,470	1/2460	1,000	-1.48	4.72	5.7
M. 13	180	2,650	1/2460	1,000	-1.41	4.79	5.7
M. 14	200	2,050	1/2460	1,000	-1.32	4.88	5.8
H. 15	210	040.E	1/2460	1,000	-1.24	4.96	5.9
H 16	180	3,240	1/2460	1,000	-1.17	5.03	6.0
M. 37	260	3,500	1/2460	1,000	-1.06	5.14	6.1
Figover Dn.	150	3,650	1/2460	1,000	-1.00	5.20	6.2
Flyover Up	0	3,650	1/1850	1,000	-1.00	5.20	6.2
H. 18	40	3,690	1/1650	1,000	-0.98	5,22	6.2
M. 19	220	3,910	1/1850	1,000	-0.86	5.34	6.3
N. 20	165	4,075	1/1850	1,000	-0.77	5.43	6.4
M.21	210	4,285	1/1850	1,000	-0.66	5.54	6.5
H. 22	· 200	4,485	1/1850	1,000	-0.55	5.65	6.6
H.23	200	4,685	1/1850	1,000	-0.44	5.76	6.7
H.24	220	4,905	1/1850	1,000	-0.32	5.88	6.8
H.25 Weir Do.	230	5, 135	1/1850	1,000	-0.20	6.00	7.0
M.25 Wair Up	0	5, 135	1/1850	1,000	-0.20	6.00	7.0

Longitudinat Data of MOJI River (Case H-2)

	Section	Distan	ice (m) .	Gradient of	Design Discharge	Design Elevation (m,IGGSP)						
	No.	Single	Accum.	River bed	(m3/r)	River Bed	H.W.L.	Dike Crown				
	Е.Н	0	0	1/2340	1,000							
1	P .0	690	: 690	1/2340	1,000	-2.20	4.00	5.00				
į	Railway	250	940	1/2340	1,000	-2.09	4.11	5.11				
1	Confituence	130	1,070	1/2340	1,000	-2.04	4.16	5.16				
1	Bifurcate	1,125	2,175	1/2340	1,000	-1.56	4.64	5.64				
Į	H. 12	125	2,320	1/2340	1,000	-1.50	4.70					
ŧ	M. 13	180	2,500	1/2340	1,000	-1.43	4.77	5.77				
ŧ	M. 14	200	2,700	1/2340	1,000	-1.34	4.86	5.86				
1	H. 15	210	2,510	1/2340	1,000	-1.25	4.95	5.95				
ţ	H. 16	180	3,090	1/2340	1,000	-1.18	5.02	6.02				
ł	N. 17	260	3,350	1/2340	1,000	-1.06	5.14	6.14				
-	Flyover Do.	150	3,500	1/2340	1,000	-1.00	5.20	6.20				
-	Flyover Up	0	3,500	1/1850	1,000	-1.00	5.20	6.20				
!	H.18	40	3,540	1/1850	1,000	-0.98	5.22	6.22				
ı	H. 19	220	3,740	1/1850	1,000	-0.84	5.34	6.34				
1	М.20	165	3,925	1/1850	1,000	-0.77	5.43	6.43				
ŧ	H.21	210	4,135	1/1850	1,000	-0.66	5.54	6.54				
1	M. 22	200	4,335	1/1850	1,000	-0.55	5.65	6.65				
ï	H.23	200	4,535	1/1850	1,000	-0.44	5.76	6.76				
ŧ	H.24	220	4,755	1/1850	1,000	-0.32		6.88				
-	M.25 Weir Dn.	230	4,985	1/1850	1,000	-0.20	6.00	7.00				
_	M.25 Wair Up	O	4,985	1/1850	1,000	-0.20	6.00	7.00				

TABLE 3.10 PROPOSED LONGITUDINAL PROFILE OF PIACAGUERA AND INDIO RIVER

### Longitudinal Data of PIACAGUERA River (Case M-2)

	Posti sa	Distan	ce (m)	Gradient	Design	Design Elevation (m, IGGSP)						
	Section No.	Single Accum.		of River bed	Discharge (m ³ /s)	River Bed	H.W.L.	Dike Crown				
-	P.1+130(Confl.)	0	0	1/2000	250	-2.00	4.20	5.20				
1	P.2	190	190	1/2000	250	-1.90	4.20	5,20				
1	P.3	420	610	1/2000	250	-1.70	4.20	5.20				
-	P.4	370	980	1/2000	250	-1.50	4.20	5.20				
2	Railway Br.	610	1,590	1/2000	250	~1,20	4.30	5.20				
-	Railway Br.	0.	1,590	1/ 400	250	-0.20	4.30	5.20				
3	3.0k	1030	2,620	1/ 400	250	2.40	6.90	7.50				
-	3.0k	. 0	2,620	1/ 100	250	4.10	8.60	9.20				
4	P. 10	297	2,917	1/ 100	250	7.10	11.60	12.20				
-	P.10	. 0	2,917	1/ 100	250	9.10	13.60	14.20				
5	P.12	380	3,297	1/ 100	250	12.90	17.40	18.00				

### Longitudinal Data of PIACAGUERA River (Case M-1)

		Distan	ce (m)	Gradient	Design	Design Elevation (m, IGGSP)						
	Section No.	Single	Accum.	of River bed	Discharge (m³/s)	River Bed	H.W.L.	Dike Crown				
_	P.0	0	0	1/2000	250	-2.20	4.00	5.00				
Ė	P.1(Railway Br.)	250	250	1/2000	250	-2.10	4.00	5.00				
1	P.2	320	570	1/2000	250	~1.90	4.00	5.00				
	P. 3	420	990	1/2000	250	-1.70	4.00	5.00				
-	P.4	370	1,360	1/2000	250	-1.50	4.00	5.00				
2	Railway Br.	610	1,970	1/2000	250	-1.20	4.30	5.00				
_	Railway Br.	0	1.970	1/ 400	250	-0.20	4.30	5.00				
3	3.0k	1030	3.000	1/ 400	250	2.40	6.90	7.50				
_	3.0k	0	3,000	1/ 100	250	4.10	8.60	9.20				
4	P. 10	297	3.297	1/ 100	250	7.10	11.60	12.20				
_	P. 10	0	3,297	1/ 100	250	9.10	13.60	14.20				
5	P. 12	380	3,677	1/ 100	250	12.90	17.40	18.00				

### Longitudinal Data of INDIO River (for Case-H-1 and H-2)

	Section		ce (m)	Gradient of	Design Discharge	Design E	levation	(m,1665P)
	No.	Single	Accum.	River bed	(m3/s)	River Bed	H.W.L.	Dike Crown
-	Confluence	0	0		100	-1.20	5.00	6.00
ı	M1.0	180	180	-	100	-0.20	5.00	6.00
1	M1+370	370	550	-	100	1.60	5.00	6.00
;	M1+520	150	700		100	2.20	5.20	6.00
ţ	, H1+620	100	800	1/500	100	2.40	5.40	6.00
	Railway Br.	370	1,170	1/500	100	2.90	5.90	6.50

TABLE 3.11 PROPOSED LONGITUDINAL PROFILE OF PRIORITY PROJECT (MOJI RIVER)

Single Accum. River bed (m3/s)  9 0 0 1/2340 6 690 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 1/1850 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6 690 1/2340 6		Section	Distance	ice (m)	Gradient	Design	Design El	Elevation (m, 1665P	(m, IGGSP)
M.3 690 690 1/2340 600 -2.20 4.  ailway 250 690 1/2340 600 -2.09 4.  fluence 130 1,070 1/2340 600 -2.09 4.  furcate 1,125 2,195 1/2340 600 -1.56 4.  M.12 125 2,320 1/2340 600 -1.56 4.  M.13 200 2,700 1/2340 600 -1.43 4.  M.14 200 2,700 1/2340 600 -1.25 4.  M.15 200 2,700 1/2340 600 -1.25 4.  M.15 200 1/2340 600 -1.00 5.  M.16 3,090 1/2340 600 -1.00 5.  M.17 260 3,350 1/3340 600 -1.00 5.  M.18 40 3,500 1/1850 600 -0.98 5.  M.20 220 4,335 1/1850 600 -0.66 5.  M.21 220 4,335 1/1850 600 -0.25 5.  Meir Dn. 230 4,985 1/1850 600 -0.20 6.  Meir Dn. 230 4,985 1/1850 600 -0.20 6.	1		Single	Accum.	River bed	(m3/s)	1	H.E.L.	Dike Crown
Pe.O 690 1/2340 600 -2.20 4. fluence 130 1,070 1/2340 600 -2.09 4. fluence 130 1,070 1/2340 600 -2.09 4. fluence 1,125 2,195 1/2340 600 -1.56 4. furcate 1,125 2,320 1/2340 600 -1.56 4. furcate 1,125 2,320 1/2340 600 -1.50 4. furcate 2,910 1/2340 600 -1.34 4. furcate 1,125 2,910 1/2340 600 -1.34 4. furcate 1,125 2,910 1/2340 600 -1.06 5. furcate 1,135 2,00 1/2340 600 -1.00 5. furcate 1,135 2,00 1/1350 600 -1.00 5. furcate 1,135 1/1350 600 -0.66 5. furcate 1,135 1/1350 600 -0.66 5. furcate 1,135 1/1350 600 -0.66 5. furcate 1,135 1/1350 600 -0.65 5. furcate 1,135 1/1350 600 -0.65 5. furcate 1,135 1/1350 600 -0.65 5. furcate 1,135 1/1350 600 -0.65 5. furcate 1,135 1/1350 600 -0.65 5. furcate 1,135 1/1350 600 -0.65 5. furcate 1,135 1/1350 600 -0.65 5. furcate 1,135 1/1350 600 -0.65 5. furcate 1,135 1/1350 600 -0.65 5. furcate 1,135 1/1350 600 -0.65 5. furcate 1,135 1/1350 600 -0.65 5. furcate 1,135 1/1350 600 -0.65 5. furcate 1,135 1/1350 600 -0.65 6. furcate 1,1350 600 600 600 600 600 600 600 600 600 6	à	Σ	0	0	1/2340	009	;; ; ; ; ; ; ;	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	
Alluence 130 1,070 1/2340 600 -2.09 4. Fluence 130 1,070 1/2340 600 -2.04 4. Furcate 1,125 2,195 1/2340 600 -1.56 4. Furcate 1,125 2,320 1/2340 600 -1.50 4. Fu.13 180 2,500 1/2340 600 -1.34 4. Fu.14 200 2,700 1/2340 600 -1.34 4. Fu.15 2,910 1/2340 600 -1.34 4. Fu.15 260 3,350 1/2340 600 -1.06 5. Fu.16 2,910 1/2340 600 -1.00 5. Fu.18 40 3,540 1/1850 600 -1.00 5. Fu.18 40 3,540 1/1850 600 -0.98 5. Fu.18 40 3,540 1/1850 600 -0.98 5. Fu.18 220 4,335 1/1850 600 -0.66 5. Fu.23 200 4,335 1/1850 600 -0.35 5. Fu.23 200 4,985 1/1850 600 -0.32 5. Fu.18 600 -0.20 6. Fu.18 600 -0.20 6. Fu.18 600 -0.20 6. Fu.19 600 -0.20 6.		Pe.0	069	069	1/2340	909		4.00	2,00
fluence 130 1,070 1/2340 600 -2.04 4. furcate 1,125 2,195 1/2340 600 -1.56 4. furcate 1,125 2,320 1/2340 600 -1.50 4. furcate 1,125 2,320 1/2340 600 -1.50 4. fur.13 200 2,700 1/2340 600 -1.34 4. fur.15 2,910 1/2340 600 -1.34 4. fur.15 260 3,350 1/2340 600 -1.05 5. fur.17 260 3,350 1/2340 600 -1.06 5. fur.18 40 3,540 1/1350 600 -1.00 5. fur.18 40 3,540 1/1350 600 -0.96 5. fur.18 40 3,540 1/1350 600 -0.96 5. fur.18 22 220 4,335 1/1350 600 -0.66 5. fur.23 220 4,335 1/1350 600 -0.35 5. fur.23 220 4,355 1/1350 600 -0.35 5. fur.23 220 4,985 1/1350 600 -0.32 5. fur.19 0 4,985 1/1350 600 -0.20 6.			250	940	1/2340	909		4.11	m T
furcate 1,125 2,195 1/2340 600 -1.56 4.  M.12 125 2,320 1/2340 600 -1.50 4.  M.13 180 2,500 1/2340 600 -1.34 4.  M.14 200 2,700 1/2340 600 -1.34 4.  M.15 210 2,910 1/2340 600 -1.25 4.  M.15 26 3,350 1/2340 600 -1.06 5.  M.17 260 3,350 1/2340 600 -1.00 5.  M.18 40 3,500 1/1850 600 -1.00 5.  M.20 220 3,760 1/1850 600 -0.98 5.  M.21 220 4,335 1/1850 600 -0.55 5.  Meir Dn. 230 4,985 1/1850 600 -0.32 5.  Weir Up 0 4,985 1/1850 600 -0.32 6.  Meir Up 0 4,985 1/1850 600 -0.20 6.			130	1,070	1/2340	909	-2.04	4, 16	5.16
M.12 125 2,320 1/2340 600 -1.50 4.134 1.13 180 2,500 1/2340 600 -1.34 4.14 200 2,700 1/2340 600 -1.34 4.15 2.10 2,910 1/2340 600 -1.25 4.1.25 4.15 2.00 3,350 1/2340 600 -1.06 5.1.25 4.1.25 1.12 2.00 3,350 1/2340 600 -1.00 5.1.25 1.18 2.20 3,500 1/1850 600 -1.00 5.1.20 2.20 3,760 1/1850 600 -0.98 5.1.22 2.20 4,135 1/1850 600 -0.96 5.1.22 2.20 4,335 1/1850 600 -0.55 5.1.22 2.20 4,755 1/1850 600 -0.32 5.1.22 2.20 4,985 1/1850 600 -0.32 5.1.22 2.20 4,985 1/1850 600 -0.32 5.1.23 1/1850 600 -0.32 5.1.23 1/1850 600 -0.20 6.20 6.20			1,125	2,195	1/2340	009	- 1.56	4.64	. v.
M.13 180 2,500 1/2340 600 -1.43 4. M.14 200 2,700 1/2340 600 -1.34 4. M.15 210 2,910 1/2340 600 -1.25 4. M.15 260 3,090 1/2340 600 -1.05 5. M.17 260 3,500 1/2340 600 -1.06 5. M.18 40 3,500 1/1850 600 -0.98 5. M.19 220 3,760 1/1850 600 -0.98 5. M.20 165 3,925 1/1850 600 -0.66 5. M.21 210 4,135 1/1850 600 -0.65 5. M.22 200 4,335 1/1850 600 -0.44 5. Meir Dn. 230 4,985 1/1850 600 -0.20 6. Meir Dn. 230 4,985 1/1850 600 -0.20 6.	•-	M. 12	125	2,320	1/2340	009	-1.50	4.70	
M.14 200 2,700 1/2340 600 -1.34 4. M.15 210 2,910 1/2340 600 -1.25 4. M.15 280 3,090 1/2340 600 -1.25 4. M.17 260 3,350 1/2340 600 -1.06 5.  Dover Dn. 150 3,500 1/1850 600 -1.00 5. M.18 40 3,540 1/1850 600 -0.98 5. M.19 220 3,760 1/1850 600 -0.96 5. M.20 165 3,925 1/1850 600 -0.77 5. M.21 20 4,335 1/1850 600 -0.55 5. Meir Dn. 230 4,985 1/1850 600 -0.32 5. Meir Dn. 230 4,985 1/1850 600 -0.20 6.		m E	180	2,500	1/2340	009	-1.43	4.77	
M.15		M. 14	200	2,700	1/2340	009	-1.34	4.86	
M.16 180 3,090 1/2340 600 -1.18 5. 260 3,350 1/2340 600 -1.06 5. 260 2,350 1/2340 600 -1.06 5. 260 2,500 1/1850 600 -1.00 5. 220 3,760 1/1850 600 -0.98 5. 4.22 220 3,760 1/1850 600 -0.96 5. 4.22 220 4,755 1/1850 600 -0.66 5. 220 4,755 1/1850 600 -0.65 5. 220 4,755 1/1850 600 -0.55 6. 220 4,755 1/1850 600 -0.35 6. 220 4,985 1/1850 600 -0.20 6. 8. Weir Dn. 230 4,985 1/1850 600 -0.20 6.		χ. 13	210	2,910	1/2340	009	-1.25	4.95	n. 95
M.17 260 3,350 1/2340 600 -1.06 5.    bver Dn. 150 3,500 1/2340 600 -1.00 5.    over Up		M. 16	180	3,090	1/2340	009	-1.18	5.02	6.02
Daver Dn.         150         3,500         1/2340         600         -1.00         5.50           Aver Up         0         3,500         1/1850         600         -0.98         5.50           Av. 18         40         3,540         1/1850         600         -0.98         5.50           Av. 20         165         3,760         1/1850         600         -0.96         5.50           Av. 21         210         4,135         1/1850         600         -0.65         5.50           Av. 23         200         4,535         1/1850         600         -0.45         5.50           Av. 24         220         4,755         1/1850         600         -0.32         5.74           Weir Dn.         230         4,985         1/1850         600         -0.20         6.50           Weir Up.         0         4,985         1/1850         600         -0.20         6.20	<del>-</del> -	M. 17	260	3,350	1/2340	909	-1.06	5.14	6.14
over Up       0       3,500       1/1850       600       -1.00       5.         4.18       40       3,540       1/1850       600       -0.98       5.         4.19       220       3,740       1/1850       600       -0.96       5.         4.20       165       3,925       1/1850       600       -0.77       5.         4.21       210       4,135       1/1850       600       -0.66       5.         4.23       200       4,535       1/1850       600       -0.55       5.         4.24       220       4,755       1/1850       600       -0.32       5.         Weir Dn.       230       4,985       1/1850       600       -0.20       6.         Weir Up       0       4,985       1/1850       600       -0.20       6.	1.		150		1/2340	009	-1.00	5.20	6.20
7.18 40 3,540 1/1850 600 -0.98 5. 7.20 3,760 1/1850 600 -0.96 5. 7.20 165 3,925 1/1850 600 -0.77 5. 7.21 210 4,135 1/1850 600 -0.66 5. 7.22 200 4,535 1/1850 600 -0.55 5. 7.23 200 4,535 1/1850 600 -0.35 5. 7.24 220 4,755 1/1850 600 -0.32 5. 8.10 0 4,985 1/1850 600 -0.20 6.	1	100	a		1/1850	009	-1.00	5.20	6.20
7.19 220 3,760 1/1850 600 -0.66 5. 7.20 165 3,925 1/1850 600 -0.77 5. 7.21 210 4,135 1/1850 600 -0.66 5. 7.22 200 4,335 1/1850 600 -0.55 5. 7.23 200 4,535 1/1850 600 -0.55 5. Weir Dn. 230 4,985 1/1850 600 -0.20 6. Weir Up 0 4,985 1/1850 600 -0.20 6.	<b>G</b> 10.	¥. 18	40		1/1850	009		5.22	6 22
7.20 165 3,925 1/1850 600 -0.77 5. 7.21 210 4,135 1/1850 600 -0.66 5. 7.22 200 4,335 1/1850 600 -0.55 5. 7.23 200 4,536 1/1850 600 -0.44 5. 7.24 220 4,755 1/1850 600 -0.32 5. Weir Dn. 230 4,985 1/1850 600 -0.20 6.		δ. Σ.	220		1/1850	900		5.34	6.34
7.21 210 4,135 1/1850 600 -0.66 5. 7.22 200 4,335 1/1850 600 -0.55 5. 7.23 200 4,535 1/1850 600 -0.44 5. 7.24 220 4,755 1/1850 600 -0.32 5. Weir Dn. 230 4,985 1/1850 600 -0.20 6. Weir Up 0 4,985 1/1850 600 -0.20 6.		M.20	165		1/1850	900	-0.77		6.43
7.22 200 4,335 1/1850 600 -0.55 5. 7.23 200 4,535 1/1850 600 -0.44 5. 4.24 220 4,755 1/1850 600 -0.32 5. Weir Dn. 230 4,985 1/1850 600 -0.20 6. Weir Up 0 4,985 1/1850 600 -0.20 6.		M.21	210		1/1850	009			
7.23 200 4,535 1/1850 600 -0.44 5. 4.24 220 4,755 1/1850 600 -0.32 5. Weir Dn. 230 4,985 1/1850 600 -0.20 6. Weir Up 0 4,985 1/1850 600 -0.20 6.		Σ. Σ.	200		1/1850	009		•	
4.24 220 4,755 1/1850 600 -0.32 5. Weir Dn. 230 4,985 1/1850 600 -0.20 6. Weir Up 0 4,985 1/1850 600 -0.20 6.		<b>A</b> . 23	200	4,535	1/1850	009			6.76
Weir Dn. 230 4,985 1/1850 600 -0.20 6. Weir Up 0 4,985 1/1850 600 -0.20 6.			220	4,755	1/1850	009			
Weir Up 0 4,985 1/1850 600 -0.20 6.	•	Weir	230	4,985	1/1850	900			7 00
	ι .	Weir	0	4,985	1/1850	909		6.00	7.00

# TABLE 3.12 NON-UNIFORM FLOW CALCULATION (CASE:M-2)

									:										
۵	1.078	1.083	1.083	1.083	1.085	1.085	1.086	1.087	1.087	1.087	1.087	1.079	1.078	1.077	1.077	1.077	1.077	1.077	1.078
œ	5.035	5.121	5.156	5,165	5.270	5.272	5.285	5.296	5.310	5.323	5.337	5.278	5.269	5.262	5.258	5.249	5.240	5.231	5.226
∢*	455.0	466.1	470.6	471.8	485.1	485.4	487.0	488.4	490.2	491.9	493.7	449.0	447.7	446.8	446.2	445.0	443.8	442.7	442.1
<b>&gt;</b>	2.198	2.145	2.125	2,119	2.061	2.060	2.053	2.048	2.040	2.033	2.025	2.227	2.233	2.238	2.241	2.247	2.253	2.259	2.262
Œ	1000.0	1000.0	1000.0	1000.0	1000.0	1000.0	1000.0	1000.0	1000.0	1000.0	1000.0	1000.0	1000.0	1000.0	1000.0	1000.0	1000.0	1000.0	1000.0
X	o.	690.0	250.0	130.0	1125.0	125.0	180.0	200.0	210.0	180.0	260.0	190.0	220.0	165.0	210.0	200.0	200.0	220.0	230.0
12	-2.200	-1.960	-1.880	-1.830	-1.450	-1.400	-1.340	-1.270	-1.200	-1.140	-1.050	980	860	770	660	550	-,440	320	200
×	3.700	4.050	4.172	4.233	4.740	4.793	4.870	4.954	5.042	5.117	5.223	5.262	5.369	5.449	5.553	5.652	5.751	5.861	5.977
2 2	? .	e i i i	5	3 2	2	,	77. 7	10°	. X	7 7		) on	M. 20	2 6	2 6		27.	Ko z cz.	9

### DEFINITION OF CODE

H : Calculated water level (m).Z : The deepest river bed (m).

DX: Distance between sections (m).

Q : Discharge (m3/s).

V : Average velocity (m/s).

R : Hydraulic mean depth (m).
D : Correction coefficient.

$$D = \alpha \frac{A_1^{1/8} \frac{h^2}{n^3} d\xi}{\left(\left(\frac{k}{n} \frac{h}{n} \frac{\kappa^2 d}{n} \right)^3\right)}$$

d : Energy correction coefficient (X ≡ 1.0) B : Width of river (m).

h : Water level (m). n : Coefficient of roughness. m

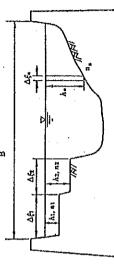


TABLE 3.13 NON-UNIFORM FLOW CALCULATION (CASE:M-2, PRIORITY PROJECT w=1/10)

																,									
a	3.022	2.682	2.319	1.761	1.449	1.410	1.444	1.480	1.518	1.527	1.532	1.776	1.923	1.653	1.586	1.696	1.740	1.607	1.445	1.344	1.401	1.442	1.423	1.128	1.265
œ	2.490	2.699	3.014	3.516	3.596	3.692	3,787	3.835	3.853	3.916	3.941	3.882	3.741	4.050	3.988	4.043	4.119	4.113	4.009	4.170	4.251	4.222	4.242	4.258	4.246
∢	677.4	526.9	410.4	304.3	257.1	255.3	271.3	282.9	292.0	300.8	304.5	450.5	413.0	343.2	316.7	336.4	359.0	332.8	284.7	325.9	291.0	300.7	296.8	379.3	253.7
۸	.886	1.139	1.462	1.972	2.333	2.350	2.212	2.121	2.055	1.994	1.970	1.332	1.453	1.748	1.894	1.783	1.671	1.803	2.107	1.841	2.062	1.986	2.022	1.582	2.365
СУ	600.0	0.008	0.009	0.009	200.0	0.009	600.0	0.009	0.009	0.009	0.009	0.009	800.0	600.0	600.0	0.009	0.009	600.0	0.009	600.0	600.0	0.009	600.0	600.0	0.009
χ	6.	200.0	200.0	290.0	250.0	130.0	250.0	250.0	250.0	250.0	125.0	125.0	180.0	200.0	210.0	180.0	260.0	190.0	220.0	165.0	210.0	200.0	200.0	220.0	230.0
1-7	-2.560	-2.456	-2.351	-2.200	-2.090	-2.040	-1.933	-1.827	-1.720	-1.613	-1.560	-1.540	-1.600	-1.760	-1.480	-1.380	-1.220	-1.180	-1.320	-1.280	-1.980	-1.380	-1.440	420	200
æ	2.780	2.823	2.872	3.007	3.192	3.325	3.587	3.810	4.010	4.202	4.292	4.501	4.534	4.587	4.677	4.799	4.967	5.051	5.130	5.325	5.371	5.502	5.617	5.874	5.785
, So.	? C	20 6	2 6	٦ <u></u>	118	ino di		2 6	2 5	2	n :	7 :	3 3	e 14	CT -	0 1		9 9	<u> </u>	3 :	, ç	3 6	3 6		3

### DEFINITION OF CODE

H : Calculated water level (m).

Z : The deepest river bed (m).

DX: Distance between sections (m).

Q : Discharge (m³/s).

V : Average velocity (m/s).
R : Hydraulic mean depth (m).
D : Correction coefficient.

A3 (" " dE

d : Energy correction coefficient (d≅1.0) B : Width of river (m).

h : Water leyel (m).

n : Coefficient of roughness.

