

### 8.2.3 Upper Kihansi Project

#### (1) Study on Dam Scale

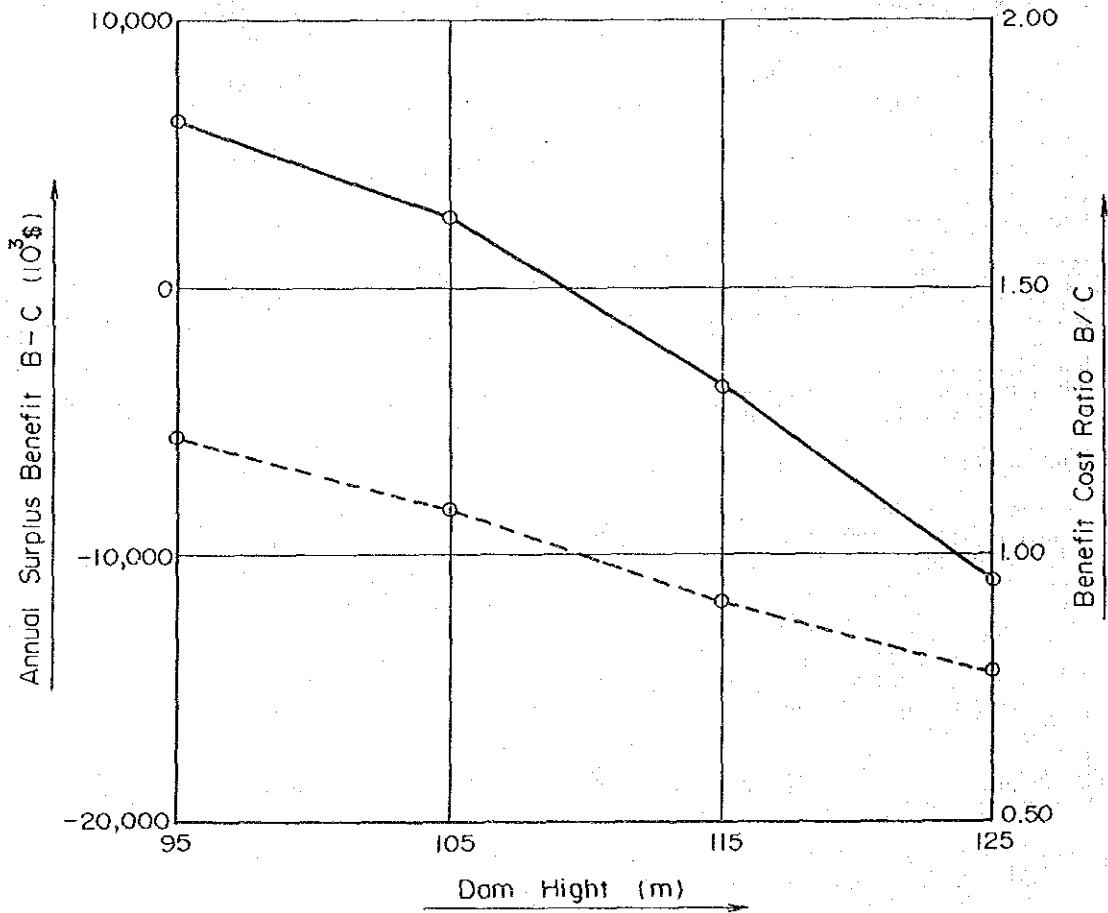
In "8.2.2 Study on Reservoir Scale", a comparison study is made based on the minimum dam scale for securing the storage capacity of each case. The economics when dam scales are increased with the optimum storage capacity fixed at  $75.1 \times 10^6 \text{ m}^3$  for the three cases of high water level EL. 1,370 m, 1,380 m and 1,390 m are studied, and the results are given in Table 8-8 and Fig. 8-10.

According to the results of the study, when the dam scale is made large, the head increases by the rise of intake water level through the increase in dam height and decrease in available drawdown, but the dam volume is also increased sharply, and the increase in cost due to this greatly exceeds the increase in benefit, and the economics of the Project is extremely impaired. Therefore, the dam scale with EL. 1,360 m as the high water level, which is the minimum scale of the dam required for securing the optimum storage capacity of  $75.1 \times 10^6 \text{ m}^3$ , is taken as the optimum dam scale.

Table 8-8 Study on Optimum Dam Height of Upper Kihansi Reservoir

Item	Unit	Case 1'	Case 2'	Case 3'	Case 4
		Upper Kihansi	UpperKihansi	Upper Kihansi	Upper Kihansi
High Water Level	m	1,390.00	1,380.00	1,370.00	1,360.00
Lower Water Level	m	1,380.50	1,368.00	1,351.00	1,330.00
Available Drawdown	m	9.50	12.00	19.00	30.00
Gross Storage Capacity	$10^6 m^3$	279.30	200.10	140.00	94.90
Effective Storage Capacity	$10^6 m^3$	75.10	75.10	75.10	75.10
Dam Type		Rockfill	Rockfill	Rockfill	Rockfill
Dam Height x Length	$10^3 m^3$	125 x 680	115 x 650	105 x 620	95 x 583
Dam Volume	$10^3 m^3$	11,500	9,200	7,600	5,300
Maximum Discharge	$m^3/s$	25.70	25.70	25.70	25.70
Standard Intake Water Level	m	1,390.00	1,380.00	1,370.00	1,360.00
Tail Water Level	m	1,138.50	1,138.50	1,138.50	1,138.50
Gross Head	m	251.50	241.50	231.50	221.50
Effective Head	m	244.50	234.50	224.50	214.50
Installed Capacity	MW	54	51	49	47
Firm Peak Power	MW	100.1	96.3	92.1	86.1
Annual Energy Production	$10^6 kWh$	330.9	317.1	298.3	275.1
Annual Firm Energy Production	$10^6 kWh$	377.1	366.8	352.9	335.7
Annual Benefit					
Peak Power Benefit	$10^3 US$$	26,237	25,241	24,140	22,568
Firm Energy Benefit	$10^3 US$$	12,959	12,605	12,127	11,537
Total Benefit (B)	$10^3 US$$	39,196	37,846	36,267	34,105
Investment Cost					
Civil Facilities Cost	$10^6 US$$	443.2	362.5	293.5	239.5
Electro-Mechanical Facilities Cost	$10^6 US$$	27.5	26.3	22.1	21.5
Total	$10^6 US$$	470.7	388.8	315.6	261.0
Annual Cost					
Civil Facilities Cost	$10^3 US$$	46,935	38,389	31,082	25,363
Electro-Mechanical Facilities Cost	$10^3 US$$	3,264	3,122	2,623	2,552
Total Cost (C)	$10^3 US$$	50,199	41,511	33,705	27,915
Annual Surplus Benefit (B - C)	$10^3 US$$	-11,003	-3,665	2,562	6,190
Benefit Cost Ratio (B/C)		0.781	0.912	1.076	1.221
Unit Annual Cost	US\$/kwh	0.133	0.113	0.096	0.083

Fig. 8-10 Study on Optimum Dam Height of Upper Kihansi Reservoir



(2) Study on Maximum Discharge and Installed Capacity

The maximum discharge and installed capacity of a hydroelectric power plant need to be selected to be the most economical considering the peak duration and site characteristics. In "8.1 Comparison Study on Development Scheme", and "8.2.2 Study on Reservoir Scale", it was decided that the peak duration time for a reservoir-type hydroelectric power plant in Tanzania is to be 13 hours as standard considering reserve capacity added to the annual load factor of the whole system, and in the Upper Kihansi Project, based on the peak duration time and firm discharge of 11.80 m<sup>3</sup>/s and considering the effect on the Lower Kihansi Project in case of decrease in intake capability due to lowering reservoir water level, the maximum discharge is selected to be 25.7 m<sup>3</sup>/s with installed capacity 47 MW.

The final decision on the maximum discharge and installed capacity of the Upper Kihansi Project is to be made at the time of the feasibility study for the Upper Kihansi Project to be carried out hereafter.

(3) Study on the Number of Turbine and Generator Units

The number of turbine and generator units for the Upper Kihansi Project is selected to be 1 unit considering economy of scale of the construction cost.

#### (4) Optimum Development Plan

The outline of the optimum development plan of the Upper Kihansi Project determined in the studies made up to this point are shown in Table 8-9. The inflows, discharges, spillover quantities when operating Upper Kihansi Reservoir for the 61-year period from 1927 to 1987 are shown in Table 8-10 and Fig. 8-11. The monthly energy production and firm energy production are shown in Tables 8-11 and 8-12, and in Fig. 8-12. The monthly peak power and peak power duration are given in Tables 8-13 and 8-14. The preliminary estimation of construction cost for the optimum development plan is shown in Table 8-15.

Table 8-9 Outline of Optimum Development Plan  
of Upper Kihansi Project

Reservoir

Catchment Area	583 km <sup>2</sup>
High Water Level	1,360.00 m
Low Water Level	1,330.00 m
Available Drawdown	30.00 m
Gross Storage Capacity	94.90 × 10 <sup>6</sup> m <sup>3</sup>
Effective Storage Capacity	75.10 × 10 <sup>6</sup> m <sup>3</sup>
Annual Average Runoff	15.68 m <sup>3</sup> /s
Firm Discharge	11.80 m <sup>3</sup> /s

Dam

Type	Rockfill
Height × Length	95 m × 583 m
Volume	5,300 × 10 <sup>3</sup> m <sup>3</sup>

Power Station

Standard Intake Water Level	1,360.00 m
Tail Water Level	1,138.50 m
Gross Head	221.50 m
Effective Head	214.50 m
Maximum Discharge	25.70 m <sup>3</sup> /s
Installed Capacity	47 MW
Unit Type × Number of Unit	Vertical Francisx1
Firm Peak Power	36.9 MW (86.1 MW)
Annual Total Energy Production	237.1 × 10 <sup>6</sup> kWh (275.1 × 10 <sup>6</sup> kWh)
Annual Firm Energy Production	175.7 × 10 <sup>6</sup> kWh (335.7 × 10 <sup>6</sup> kWh)

Note: Figures in ( ) show the values of cases including power generation increase in the Lower Kihansi Project due to regulating effect of the Upper Kihansi Project

Table 8-10 Summary of Operation Study on  
Upper Kihansi Reservoir

Unit:  $10^6 \text{ m}^3$

<u>Year</u>	<u>Inflow</u>	<u>Power Discharge</u>	<u>Spill</u>
1927	343.84	418.92	0.0
1928	367.62	362.46	0.0
1929	331.24	336.40	0.0
1930	398.91	385.88	0.0
1931	517.11	482.81	0.0
1932	535.32	535.59	0.0
1933	453.95	462.80	0.0
1934	430.24	420.24	0.0
1935	422.67	438.22	0.0
1936	591.59	554.66	21.38
1937	464.59	467.56	0.0
1938	282.86	328.10	0.0
1939	438.27	400.14	0.0
1940	429.74	436.79	0.0
1941	409.34	424.21	0.0
1942	506.86	474.87	0.0
1943	350.02	398.23	0.0
1944	388.25	348.31	0.0
1945	442.32	439.30	0.0
1946	362.09	396.48	0.0
1947	470.80	431.16	0.0
1948	425.00	469.62	0.0
1949	350.64	354.23	0.0
1950	380.81	365.44	0.0
1951	357.52	366.21	0.0
1952	535.32	489.06	5.01
1953	303.12	351.05	0.0
1954	280.17	280.17	0.0
1955	472.97	429.39	0.0
1956	483.50	488.18	0.0
1957	533.31	524.00	0.0
1958	531.89	531.89	0.0
1959	429.10	443.37	0.0
1960	532.18	512.63	14.85
1961	414.68	412.73	0.0
1962	720.01	620.53	91.86
1963	724.84	634.73	96.11
1964	707.91	658.32	49.59
1965	555.14	555.14	0.0
1966	547.97	560.33	0.0
1967	577.58	544.46	0.0
1968	888.16	716.93	191.99
1969	539.65	539.64	0.0
1970	543.61	543.61	0.0
1971	525.53	525.53	0.0
1972	656.89	638.13	18.76
1973	678.50	628.56	49.94
1974	636.01	613.86	22.15
1975	474.60	474.60	0.0
1976	513.02	513.06	0.0
1977	438.36	438.32	0.0
1978	476.85	476.85	0.0
1979	709.22	678.36	30.86
1980	449.57	449.57	0.0
1981	388.80	415.47	0.0
1982	412.09	385.42	0.0
1983	579.54	579.54	0.0
1984	531.98	531.98	0.0
1985	639.58	639.58	0.0
1986	755.81	704.54	51.27
1987	543.37	543.37	0.0
Average	494.79	484.78	10.46

Table 8-11 Total Energy Generation of Upper Kihansi Project

UNIT: 10<sup>6</sup> kWh

MONTH YEAR	< JAN >	< FEB >	< MAR >	< APR >	< MAY >	< JUN >	< JUL >	< AUG >	< SEP >	< OCT >	< NOV >	< DEC >	< TOTAL >
1927	34.78	29.37	14.48	14.23	14.88	14.35	14.67	14.41	13.42	9.70	8.83	13.21	196.33
1928	10.53	10.50	15.93	14.39	15.27	14.85	15.28	15.12	14.42	14.61	13.84	14.13	168.88
1929	13.11	8.85	13.93	14.32	15.40	14.85	15.19	14.93	14.10	13.50	7.89	8.80	154.85
1930	13.53	9.70	22.91	15.78	15.82	15.41	15.92	15.82	15.14	15.41	14.65	14.73	184.83
1931	14.37	13.64	31.90	32.38	22.94	19.66	20.72	17.98	16.25	15.99	15.32	15.66	236.80
1932	26.91	30.46	32.22	32.62	22.02	18.85	20.19	17.76	16.13	15.99	15.33	15.67	264.17
1933	27.62	29.25	27.21	14.72	15.88	15.57	16.09	16.18	15.56	15.94	15.24	15.48	226.76
1934	26.97	23.36	15.16	14.43	15.42	15.26	15.96	16.01	15.48	15.90	15.24	16.17	205.37
1935	26.55	26.07	26.59	14.18	14.81	14.37	14.76	14.56	13.80	13.05	10.57	14.61	203.93
1936	28.27	27.77	15.70	32.02	34.96	24.29	23.35	20.14	18.03	17.53	15.35	17.70	275.11
1937	25.23	21.28	31.69	14.75	18.85	17.89	19.45	17.13	16.23	16.42	15.33	15.65	229.90
1938	16.93	18.45	14.23	13.77	14.37	13.68	11.22	9.47	8.61	9.91	9.27	9.02	148.91
1939	13.96	11.05	13.93	27.83	15.95	15.90	18.02	16.09	15.55	15.92	15.21	15.46	194.89
1940	28.71	26.14	16.35	17.37	15.85	15.47	15.99	15.92	15.27	15.60	14.89	15.20	212.78
1941	15.08	29.02	22.96	14.21	15.16	14.95	15.44	15.35	14.68	14.90	14.24	14.65	200.65
1942	16.30	21.80	30.06	24.25	18.86	18.84	20.09	17.51	15.89	15.98	15.30	17.92	232.80
1943	19.52	21.96	15.49	14.24	15.34	15.22	15.66	15.50	14.80	15.00	14.13	13.31	190.18
1944	10.66	7.89	11.84	14.46	15.86	15.52	16.04	15.94	15.27	15.54	14.82	15.31	169.15
1945	25.40	23.81	16.77	14.69	21.94	16.73	18.46	16.16	15.56	15.92	15.20	15.52	216.14
1946	16.14	17.33	14.31	21.40	15.83	15.41	15.88	15.75	15.03	15.27	14.46	14.53	191.32
1947	14.53	19.43	23.09	14.55	15.69	15.51	16.10	16.10	15.55	15.93	15.21	28.81	210.50
1948	33.58	28.09	27.84	14.29	15.14	14.82	15.32	15.23	14.56	14.76	14.07	14.28	221.98
1949	13.40	16.63	14.45	14.40	15.27	14.79	15.17	14.96	14.16	14.19	8.34	7.51	163.28
1950	7.41	9.37	20.89	14.43	15.52	15.33	15.85	15.77	15.12	15.42	14.68	14.80	174.60
1951	14.35	12.70	13.94	14.01	15.08	14.64	14.99	14.74	13.91	11.83	13.67	14.27	168.13
1952	14.43	23.57	23.00	17.69	34.63	21.94	20.75	17.88	16.06	15.98	18.84	15.71	240.48
1953	18.69	17.35	14.44	14.02	14.77	14.43	14.71	14.38	12.12	8.46	7.53	11.08	161.98
1954	15.94	11.40	11.89	13.48	13.94	10.86	9.60	8.71	7.80	7.62	6.88	6.96	123.07
1955	8.38	12.79	16.91	30.56	20.84	19.99	20.57	17.78	15.94	15.98	15.31	15.62	210.66
1956	30.88	29.14	18.07	29.98	15.96	17.57	19.07	16.61	15.56	15.94	15.22	15.48	239.49
1957	28.11	29.22	20.23	26.18	28.98	17.91	19.64	18.24	17.17	17.42	15.91	19.02	258.03
1958	25.65	25.84	31.02	29.21	22.59	16.74	18.78	17.65	16.97	17.48	15.74	23.72	261.17
1959	26.03	26.12	24.68	14.51	15.47	15.11	15.62	15.59	15.02	15.41	14.80	15.23	213.58
1960	15.17	26.09	31.90	32.34	33.92	17.97	16.81	16.11	15.45	15.77	15.07	15.42	252.01
1961	18.60	25.62	17.98	14.44	15.57	15.31	15.70	15.62	14.98	15.27	14.63	15.26	198.97
1962	34.33	31.58	34.96	33.83	34.96	24.94	24.24	21.58	17.47	19.70	17.06	20.81	315.45
1963	34.02	30.98	34.81	33.83	34.96	23.35	25.12	21.68	19.74	19.45	25.98	17.37	321.28
1964	31.14	30.60	33.39	33.49	34.96	29.50	27.54	25.00	21.86	20.89	18.75	22.19	329.30
1965	29.72	29.28	31.84	32.28	20.14	17.56	20.05	18.83	17.53	18.23	16.82	20.76	273.04
1966	29.24	28.33	32.00	32.87	30.15	19.74	20.07	19.28	17.95	15.93	15.16	15.40	276.11
1967	21.51	28.21	23.57	15.62	27.91	21.63	21.27	19.45	17.71	17.96	19.50	34.77	269.11
1968	35.09	32.71	34.96	33.83	34.96	33.83	33.43	28.11	24.76	22.92	21.96	28.52	365.07
1969	33.57	29.44	29.94	22.06	22.98	17.93	19.91	19.52	17.39	17.08	16.79	19.08	265.69
1970	33.56	30.26	34.16	33.34	15.98	15.57	18.02	17.38	16.39	16.11	15.33	25.20	271.29
1971	27.19	29.30	26.14	27.99	17.72	15.97	20.71	18.09	17.22	21.92	16.76	19.53	258.55
1972	30.12	28.22	32.27	32.70	34.96	24.54	23.02	19.46	20.49	19.90	18.51	32.71	316.90
1973	34.39	31.20	34.56	33.84	34.96	26.62	23.62	20.54	19.56	19.68	18.51	22.55	318.03
1974	33.06	29.89	31.35	32.28	34.89	26.91	23.91	19.73	19.59	19.40	17.82	15.78	304.59
1975	27.56	22.66	15.90	15.67	24.79	20.97	20.54	18.47	18.10	17.04	15.34	17.69	234.73
1976	26.00	26.76	23.51	16.88	25.15	25.24	22.98	20.05	17.89	17.66	15.35	15.70	253.17
1977	24.99	20.50	16.05	14.65	17.05	17.54	18.76	16.68	15.57	15.96	15.42	23.23	216.39
1978	27.40	24.32	21.17	15.62	22.15	19.13	19.16	16.62	15.57	15.96	15.78	22.15	235.04
1979	33.51	29.28	31.89	32.25	34.69	33.83	32.00	26.80	21.18	19.69	18.76	23.90	335.80
1980	29.14	28.09	18.04	14.47	15.69	15.59	18.17	17.14	15.72	15.99	15.33	17.51	220.87
1981	23.09	22.94	17.76	14.46	15.51	15.25	15.76	15.69	15.04	15.36	14.64	14.89	200.40
1982	14.66	13.03	14.37	14.30	15.57	15.51	16.09	16.05	15.43	15.82	15.22	22.24	188.30
1983	33.86	29.79	26.20	21.14	33.14	28.25	25.77	20.39	18.02	17.54	15.58	17.41	287.09
1984	23.80	23.64	22.27	17.06	29.06	25.05	23.57	19.44	17.83	17.90	16.37	26.97	262.98
1985	33.82	29.87	32.02	30.10	30.98	26.18	25.58	20.96	18.86	18.10	19.81	30.13	316.41
1986	33.87	30.47	33.72	33.18	34.96	33.83	31.45	26.20	21.16	19.97	22.34	32.79	353.94
1987	33.80	30.06	32.68	14.83	21.66	21.71	22.21	19.16	16.93	17.54	16.95	22.04	269.56
T O T A L	1467.94	1442.48	1433.55	1322.67	1348.70	1164.15	1180.02	1073.42	994.53	989.21	936.83	1107.22	14440.71
A V E	24.06	23.65	23.50	21.68	22.11	19.08	19.34	17.60	16.30	16.22	15.36	18.15	237.06
M A X	35.09	32.71	34.96	33.84	34.96	33.83	33.43	28.11	24.76	22.92	25.98	34.77	365.07
M I N	7.41	7.89	11.84	13.48	13.94	10.86	9.60	8.71	7.80	7.62	6.88	6.96	123.07



Table 8-12 Firm Energy Generation of Upper Kihansi Project

UNIT: 10<sup>6</sup> kWh

MONTH YEAR	< JAN >	< FEB >	< MAR >	< APR >	< MAY >	< JUN >	< JUL >	< AUG >	< SEP >	< OCT >	< NOV >	< DEC >	< TOTAL >
1927	15.88	13.26	13.77	13.63	14.33	13.80	14.04	13.67	12.77	9.70	8.83	13.21	156.89
1928	10.53	10.50	13.40	13.86	14.88	14.51	14.89	14.68	13.89	13.96	13.08	13.28	161.46
1929	13.11	8.85	13.00	13.76	15.06	14.50	14.77	14.40	13.45	13.28	7.69	8.80	150.85
1930	12.93	9.70	13.40	14.32	15.67	15.31	15.81	15.67	14.92	15.08	14.22	14.12	171.15
1931	13.61	12.27	14.01	14.53	15.93	15.57	16.09	16.09	15.54	15.91	15.18	15.44	180.15
1932	15.03	13.50	14.21	14.68	16.05	15.57	16.09	16.09	15.54	15.91	15.20	15.46	183.31
1933	15.02	12.93	13.85	14.32	15.76	15.54	16.09	16.09	15.52	15.84	15.06	15.18	181.19
1934	14.85	12.88	13.78	13.92	15.10	15.09	15.86	15.94	15.40	15.79	15.06	15.39	179.05
1935	15.04	12.88	13.78	13.55	14.24	13.83	14.17	13.88	13.03	13.05	10.57	13.95	161.98
1936	14.74	13.34	13.78	14.74	16.09	15.57	16.09	16.09	15.54	15.91	15.22	15.50	182.59
1937	15.04	12.88	13.87	14.36	15.86	15.57	16.09	16.09	15.54	15.91	15.20	15.42	181.81
1938	14.99	12.88	13.42	12.99	13.62	12.86	11.22	9.47	8.61	9.91	9.27	9.02	138.23
1939	13.04	11.05	13.00	14.06	15.86	15.57	16.09	16.09	15.50	15.81	15.02	15.16	176.24
1940	14.85	13.34	13.78	14.32	15.71	15.39	15.91	15.81	15.10	15.35	14.56	14.79	178.92
1941	14.61	12.78	13.79	13.60	14.73	14.65	15.13	15.00	14.27	14.36	13.65	14.01	170.58
1942	14.35	12.88	13.78	14.32	15.87	15.57	16.09	16.09	15.54	15.90	15.15	15.44	180.97
1943	15.04	12.88	13.78	13.64	14.98	15.03	15.44	15.22	14.44	14.51	13.48	13.31	171.75
1944	10.66	7.89	11.84	13.96	15.72	15.47	15.97	15.84	15.10	15.26	14.46	14.93	167.11
1945	14.89	12.88	13.78	14.28	15.83	15.57	16.09	16.09	15.51	15.81	15.00	15.23	180.96
1946	14.95	12.88	13.53	14.15	15.68	15.30	15.75	15.56	14.76	14.88	13.95	13.84	175.21
1947	13.83	12.60	13.78	14.08	15.48	15.45	16.09	16.09	15.51	15.82	15.02	15.35	179.08
1948	15.09	13.40	13.78	13.71	14.70	14.46	14.95	14.83	14.10	14.17	13.41	13.50	170.09
1949	13.05	12.05	13.74	13.88	14.88	14.42	14.75	14.44	13.53	13.36	8.34	7.51	153.95
1950	7.41	9.37	13.40	13.91	15.24	15.19	15.71	15.60	14.89	15.10	14.26	14.22	164.30
1951	13.58	11.91	13.03	13.33	14.62	14.21	14.49	14.14	13.18	11.83	12.84	13.48	160.63
1952	13.69	12.97	13.78	14.32	15.93	15.57	16.09	16.09	15.54	15.90	15.21	15.50	180.59
1953	15.04	12.88	13.71	13.34	14.18	13.91	14.09	13.63	12.12	8.46	7.53	11.08	149.97
1954	13.02	11.40	11.89	12.57	13.01	10.86	9.60	8.71	7.80	7.62	6.88	6.96	120.32
1955	8.38	12.04	13.77	14.32	15.87	15.57	16.09	16.09	15.54	15.89	15.16	15.37	174.09
1956	14.96	13.34	13.78	14.32	15.87	15.57	16.09	16.09	15.53	15.84	15.04	15.18	181.60
1957	14.87	12.91	13.83	14.32	15.87	15.57	16.09	16.09	15.54	15.91	15.22	15.51	181.71
1958	15.04	12.88	13.78	14.32	15.87	15.57	16.09	16.09	15.54	15.91	15.22	15.51	181.81
1959	15.04	12.88	13.78	14.02	15.17	14.87	15.38	15.34	14.74	15.08	14.44	14.82	175.56
1960	14.75	13.31	14.00	14.89	16.09	15.57	16.09	16.09	15.37	15.59	14.82	15.09	181.64
1961	14.87	12.88	13.78	13.92	15.30	15.16	15.49	15.38	14.70	14.88	14.20	14.86	175.41
1962	15.58	14.53	16.09	15.57	16.09	15.57	16.09	16.09	15.54	15.91	15.22	15.51	187.76
1963	15.38	14.06	16.02	15.57	16.09	15.57	16.09	16.09	15.54	15.91	15.22	15.51	187.02
1964	15.04	13.59	14.97	15.41	16.09	15.57	16.09	16.09	15.54	15.91	15.22	15.51	185.01
1965	15.04	12.95	13.97	14.46	15.93	15.57	16.09	16.09	15.54	15.91	15.22	15.51	182.27
1966	15.04	12.88	14.07	14.85	16.09	15.57	16.09	16.09	15.54	15.82	14.95	15.06	182.04
1967	14.81	12.88	13.78	14.32	15.87	15.57	16.09	16.09	15.54	15.91	15.22	15.87	181.94
1968	16.09	15.05	16.09	15.57	16.09	15.57	16.09	16.09	15.54	15.91	15.22	15.51	188.78
1969	15.09	13.06	13.94	14.32	15.87	15.57	16.09	16.09	15.54	15.91	15.22	15.51	182.19
1970	15.08	13.58	15.47	15.16	15.90	15.57	16.09	16.09	15.54	15.91	15.18	15.47	185.02
1971	15.04	12.96	13.88	14.32	15.87	15.57	16.09	16.09	15.54	15.91	15.22	15.51	181.99
1972	15.04	13.34	14.24	15.05	16.09	15.57	16.09	16.09	15.54	15.91	15.22	15.51	183.67
1973	15.62	14.20	15.73	15.57	16.09	15.57	16.09	16.09	15.54	15.91	15.22	15.51	187.12
1974	15.04	13.34	14.38	14.47	16.05	15.57	16.09	16.09	15.54	15.91	15.22	15.51	183.20
1975	15.04	12.88	13.78	14.32	15.87	15.57	16.09	16.09	15.54	15.91	15.21	15.49	181.77
1976	15.04	13.34	13.78	14.32	15.87	15.57	16.09	16.09	15.54	15.91	15.21	15.50	182.25
1977	15.05	12.88	13.78	14.23	15.79	15.57	16.09	16.09	15.53	15.87	15.19	15.51	181.55
1978	15.04	12.88	13.78	14.32	15.87	15.57	16.09	16.09	15.53	15.86	15.18	15.51	181.71
1979	15.05	12.95	14.00	14.45	15.96	15.57	16.09	16.09	15.54	15.91	15.22	15.51	182.32
1980	15.04	13.34	13.78	13.97	15.48	15.57	16.09	16.09	15.54	15.90	15.19	15.48	181.46
1981	15.04	12.88	13.78	13.96	15.22	15.07	15.57	15.47	14.77	15.01	14.21	14.35	175.35
1982	14.02	12.37	13.62	13.73	15.30	15.45	16.05	16.00	15.33	15.66	15.04	15.43	178.01
1983	15.27	13.28	13.98	14.32	15.87	15.57	16.09	16.09	15.54	15.91	15.22	15.51	182.65
1984	15.04	13.34	13.78	14.32	15.87	15.57	16.09	16.09	15.54	15.91	15.22	15.51	182.27
1985	15.25	13.33	14.08	14.32	15.87	15.57	16.09	16.09	15.54	15.91	15.22	15.51	182.77
1986	15.28	13.72	15.19	15.27	16.09	15.57	16.09	16.09	15.54	15.91	15.22	15.51	185.45
1987	15.23	13.45	14.51	14.48	15.85	15.57	16.09	16.09	15.54	15.91	15.22	15.51	183.44
T O T A L	879.13	776.27	849.86	870.90	948.00	926.27	952.38	945.98	906.61	915.76	861.78	887.19	10720.11
A V E	14.41	12.73	13.93	14.28	15.54	15.18	15.61	15.51	14.86	15.01	14.13	14.54	175.74
M A X	16.09	15.05	16.09	15.57	16.09	15.57	16.09	16.09	15.54	15.91	15.22	15.87	188.78
M I N	7.41	7.89	11.84	12.57	13.01	10.86	9.60	8.71	7.80	7.62	6.88	6.96	120.32

Table 8-13 Monthly Peak Power of Upper Kihansi Project

UNIT: MW

MONTH YEAR	< JAN >	< FEB >	< MAR >	< APR >	< MAY >	< JUN >	< JUL >	< AUG >	< SEP >	< OCT >	< NOV >	< DEC >	<TOTAL>
1927	46.4	42.9	40.2	41.1	41.9	41.7	41.0	39.9	38.6	28.3	26.6	38.8	467.4
1928	30.8	32.8	39.2	41.8	43.5	43.8	43.5	42.9	41.9	40.8	39.5	38.8	479.3
1929	38.3	32.6	38.0	41.6	44.0	43.8	43.1	42.1	40.6	38.8	23.8	25.7	448.4
1930	37.0	31.4	39.2	43.2	45.8	46.2	46.2	45.8	45.1	44.1	42.9	41.2	508.8
1931	39.8	39.7	40.9	43.9	46.5	47.0	47.0	47.0	46.9	46.5	45.8	45.1	536.1
1932	43.9	42.2	41.5	44.3	46.9	47.0	47.0	47.0	46.9	46.5	45.9	45.2	546.3
1933	43.9	41.8	40.5	43.2	46.0	46.9	47.0	47.0	46.9	46.3	45.5	44.4	539.4
1934	43.4	41.7	40.3	42.0	44.1	45.6	46.4	46.6	46.5	46.1	45.5	45.0	535.0
1935	44.0	41.7	40.3	40.9	41.6	41.8	41.4	40.6	39.3	38.1	31.9	40.8	482.3
1936	43.1	41.7	40.3	44.5	47.0	47.0	47.0	47.0	46.9	46.5	46.0	45.3	542.2
1937	44.0	41.7	40.5	43.4	46.3	47.0	47.0	47.0	46.9	46.5	45.9	45.1	541.2
1938	43.8	41.7	39.2	39.2	39.8	38.8	32.8	27.7	26.0	29.0	28.0	26.3	412.2
1939	38.1	35.8	38.0	42.5	46.3	47.0	47.0	47.0	46.8	46.2	45.3	44.3	524.3
1940	43.4	41.7	40.3	43.2	45.9	46.5	46.5	46.2	45.6	44.8	44.0	43.2	531.3
1941	42.7	41.3	40.3	41.1	43.0	44.2	44.2	43.8	43.1	42.0	41.2	40.9	507.9
1942	41.9	41.7	40.3	43.2	46.4	47.0	47.0	47.0	46.9	46.4	45.7	45.1	538.7
1943	44.0	41.7	40.3	41.2	43.8	45.4	45.1	44.5	43.6	42.4	40.7	38.9	511.4
1944	31.1	24.7	34.6	42.1	45.9	46.7	46.7	46.3	45.6	44.6	43.7	43.6	495.6
1945	43.5	41.7	40.3	43.1	46.3	47.0	47.0	47.0	46.8	46.2	45.3	44.5	538.7
1946	43.7	41.7	39.5	42.7	45.8	46.2	46.0	45.5	44.6	43.5	42.1	40.4	521.7
1947	40.4	40.7	40.3	42.5	45.2	46.6	47.0	47.0	46.8	46.2	45.3	44.9	535.1
1948	44.1	41.9	40.3	41.4	42.9	43.7	43.3	42.6	41.4	40.5	39.4	38.9	505.1
1949	38.1	39.0	40.1	41.9	43.5	43.5	43.1	42.2	40.9	39.0	25.2	21.9	458.5
1950	21.7	30.3	39.2	42.0	44.5	45.9	45.9	45.6	45.0	44.1	43.1	41.5	488.7
1951	39.7	38.5	38.1	40.2	42.7	42.9	42.3	41.3	39.8	36.6	38.8	39.4	478.3
1952	40.0	40.5	40.3	43.2	46.6	47.0	47.0	47.0	46.9	46.5	45.9	45.3	536.2
1953	44.0	41.7	40.1	40.3	41.4	42.0	41.2	39.8	36.6	24.7	22.7	32.4	446.8
1954	38.0	36.9	34.7	38.0	38.0	32.8	28.1	25.5	23.5	22.3	20.8	20.3	358.8
1955	24.5	38.9	40.2	43.2	46.4	47.0	47.0	47.0	46.9	46.4	45.8	44.9	518.4
1956	43.7	41.7	40.3	43.2	46.4	47.0	47.0	47.0	46.9	46.3	45.4	44.4	539.2
1957	43.4	41.8	40.4	43.2	46.4	47.0	47.0	47.0	46.9	46.5	46.0	45.3	540.9
1958	44.0	41.7	40.3	43.2	46.4	47.0	47.0	47.0	46.9	46.5	46.0	45.3	541.2
1959	44.0	41.7	40.3	42.3	44.3	44.9	44.9	44.8	44.5	44.1	43.6	43.3	522.7
1960	43.1	41.6	40.9	44.9	47.0	47.0	47.0	47.0	46.4	45.5	44.8	44.1	539.3
1961	43.4	41.7	40.3	42.0	44.7	45.8	45.3	44.9	44.4	43.5	42.9	43.4	522.2
1962	45.5	47.0	47.0	47.0	47.0	47.0	47.0	47.0	46.9	46.5	46.0	45.3	559.2
1963	44.9	45.5	46.8	47.0	47.0	47.0	47.0	47.0	46.9	46.5	46.0	45.3	556.9
1964	44.0	42.5	43.7	46.5	47.0	47.0	47.0	47.0	46.9	46.5	46.0	45.3	549.3
1965	44.0	41.9	40.8	43.7	46.6	47.0	47.0	47.0	46.9	46.5	46.0	45.3	542.6
1966	44.0	41.7	41.1	44.8	47.0	47.0	47.0	47.0	46.9	46.2	45.1	44.0	541.9
1967	43.3	41.7	40.3	43.2	46.4	47.0	47.0	47.0	46.9	46.5	46.0	46.4	541.6
1968	47.0	47.0	47.0	47.0	47.0	47.0	47.0	47.0	46.9	46.5	46.0	45.3	560.7
1969	44.1	42.2	40.7	43.2	46.4	47.0	47.0	47.0	46.9	46.5	46.0	45.3	542.3
1970	44.1	43.9	45.2	45.8	46.5	47.0	47.0	47.0	46.9	46.5	45.8	45.2	550.9
1971	44.0	41.9	40.6	43.2	46.4	47.0	47.0	47.0	46.9	46.5	46.0	45.3	541.7
1972	44.0	41.7	41.6	45.4	47.0	47.0	47.0	47.0	46.9	46.5	46.0	45.3	545.3
1973	45.7	45.9	46.0	47.0	47.0	47.0	47.0	47.0	46.9	46.5	46.0	45.3	557.2
1974	44.0	43.2	42.0	43.7	46.9	47.0	47.0	47.0	46.9	46.5	46.0	45.3	545.4
1975	44.0	41.7	40.3	43.2	46.4	47.0	47.0	47.0	46.9	46.5	45.9	45.3	541.1
1976	44.0	41.7	40.3	43.2	46.4	47.0	47.0	47.0	46.9	46.5	45.9	45.3	541.1
1977	44.0	41.7	40.3	43.0	46.1	47.0	47.0	47.0	46.9	46.4	45.9	45.3	540.4
1978	44.0	41.7	40.3	43.2	46.4	47.0	47.0	47.0	46.9	46.3	45.8	45.3	540.9
1979	44.0	41.9	40.9	43.6	46.6	47.0	47.0	47.0	46.9	46.5	46.0	45.3	542.7
1980	44.0	41.7	40.3	42.2	45.2	47.0	47.0	47.0	46.9	46.5	45.9	45.2	538.8
1981	44.0	41.7	40.3	42.1	44.5	45.5	45.5	45.2	44.6	43.9	42.9	41.9	522.0
1982	41.0	40.0	39.8	41.4	44.7	46.7	46.9	46.7	46.3	45.8	45.4	45.1	529.8
1983	44.6	43.0	40.9	43.2	46.4	47.0	47.0	47.0	46.9	46.5	46.0	45.3	543.7
1984	44.0	41.7	40.3	43.2	46.4	47.0	47.0	47.0	46.9	46.5	46.0	45.3	541.2
1985	44.6	43.1	41.2	43.2	46.4	47.0	47.0	47.0	46.9	46.5	46.0	45.3	544.1
1986	44.6	44.4	44.4	46.1	47.0	47.0	47.0	47.0	46.9	46.5	46.0	45.3	552.2
1987	44.5	43.5	42.4	43.7	46.3	47.0	47.0	47.0	46.9	46.5	46.0	45.3	546.1
TOTAL	2568.8	2489.7	2483.2	2629.5	2770.0	2796.7	2782.8	2764.1	2737.4	2675.8	2602.0	2592.3	31892.2
AVERAGE	42.1	40.8	40.7	43.1	45.4	45.8	45.6	45.3	44.9	43.9	42.7	42.5	522.8
MAXIMUM	47.0	47.0	47.0	47.0	47.0	47.0	47.0	47.0	46.9	46.5	46.0	46.4	560.7
MINIMUM	21.7	24.7	34.6	38.0	38.0	32.8	28.1	25.5	23.5	22.3	20.8	20.3	358.8







Fig. 8-11 Upper Kihansi Reservoir Operation

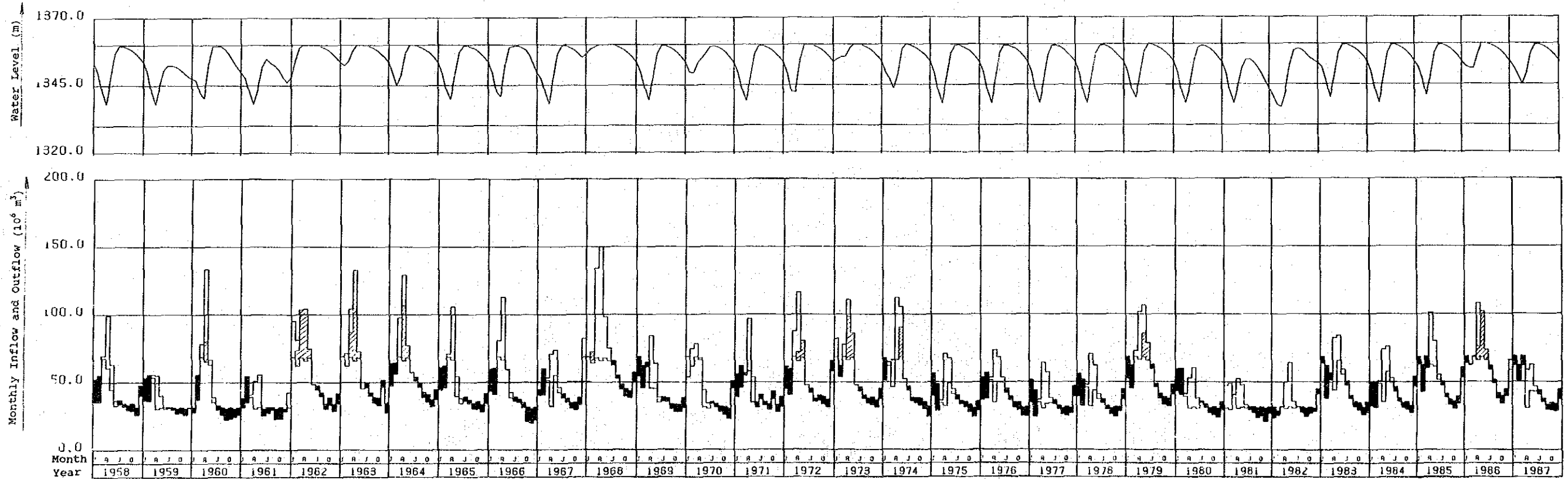
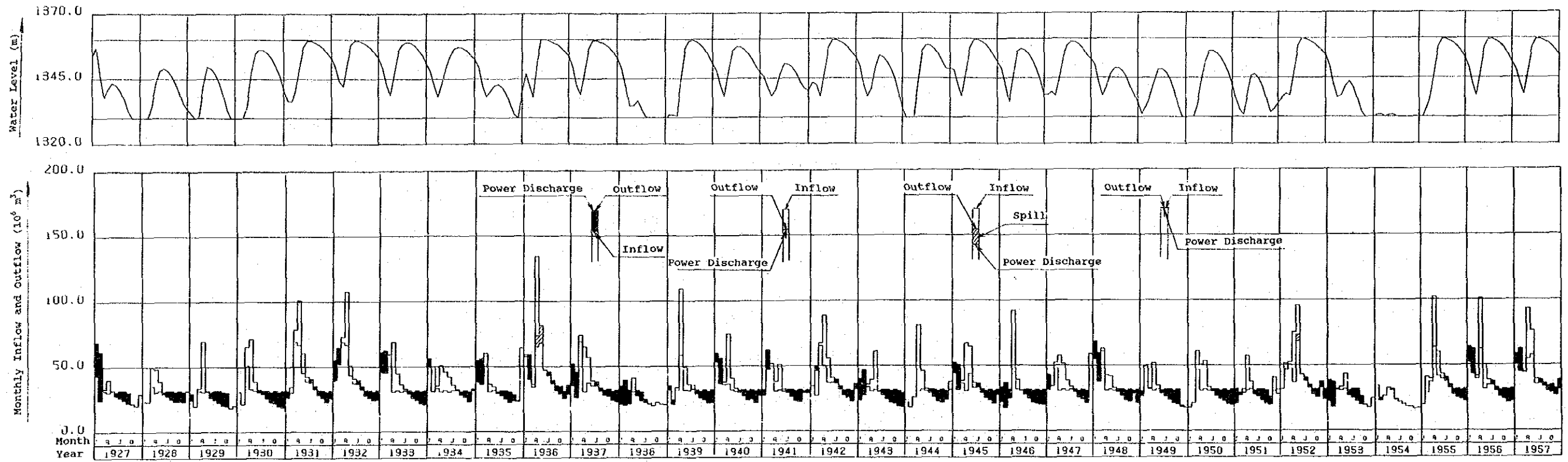




Fig. 8-12 Energy Generation of Upper Kihansi Project

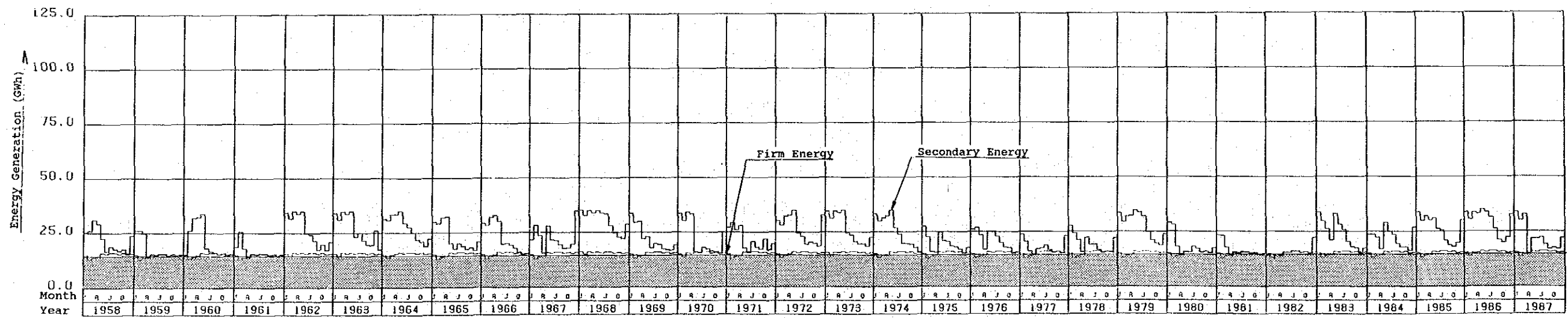
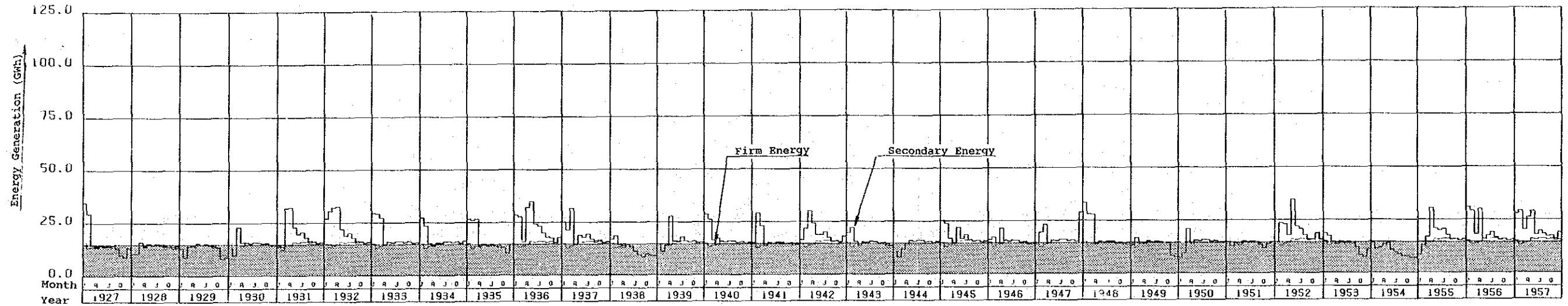






Table 8-15 Preliminary Estimation of Construction Cost of Upper Kihansi Project

Unit: 10<sup>3</sup>S

	Upper Kihansi		
	F.C.	F.C.	Total
1. Preparatory Work			
1-1 Access Road	0	0	0
1-2 Camp Facility & Others	3,600	1,000	4,600
Sub Total	3,600	1,000	4,600
2. Compensation	0	5	5
3. Civil Works			
3-1 Diversion & Cofferdam	2,059	641	2,700
3-2 Dam & Spillway	107,801	33,599	141,400
3-3 Intake	3,621	1,079	4,700
3-4 Headrace Tunnel	1,733	567	2,300
3-5 Penstock	1,698	502	2,200
3-6 Powerhouse & Switchyard	4,436	1,264	5,700
3-7 Tailrace Tunnel	1,878	622	2,500
3-8 Tailrace Outlet	610	190	800
Sub Total	123,836	38,464	162,300
4. Hydraulic Equipment	2,000	500	2,500
5. Electro-mechanical Equipment	10,700	3,400	14,100
6. Transmission Line	100	100	200
7. Total Cost (1+2+3+4+5+6)	40,236	43,469	183,705
8. Engineering & Administration 7 x 7.5%	11,034	2,760	13,794
9. Physical Contingency (1+2+3) x 15% + (4+5+6) x 10%	20,395	6,320	26,715
10. Interest during Construction	28,163	8,623	36,786
11. Grand Total (7+8+9+10)	199,828	61,172	261,000

## 8.2.4 Lower Kihansi Project

### (1) Study on Regulating Reservoir Scale

#### (a) Study on Storage Capacity

The scale of the regulating reservoir is decided to have effective capacity so that the discharge of Lower Kihansi Power Station is able to be completely regulated regardless of what the inflow condition may be. So,  $0.48 \times 10^6 \text{ m}^3$  is to be the storage capacity of the regulating reservoir corresponding to the maximum discharge of  $22.2 \text{ m}^3/\text{s}$ .

#### (b) Study on Dam Scale

The annual sedimentation at Lower Kihansi Dam, when considering the sediment trapping rate depending on the regulating reservoir capacity is to be  $2,500 \text{ m}^3/\text{yr}$ . It is scheduled for Upper Kihansi Dam to be completed 3 years after completion of Lower Kihansi Dam and it is sufficient for the sedimentation capacity of Lower Kihansi Dam to consider only this period, but in planning, the sedimentation capacity of Lower Kihansi Dam is set for  $0.1 \times 10^6 \text{ m}^3$  of sedimentation during a 50-year period assuming that Upper Kihansi Dam does not exist. As a consequence, the sedimentation level is to be EL. 1,125 m. A dam of minimum scale with the effective capacity of  $0.48 \times 10^6 \text{ m}^3$  needed for maximum discharge of  $22.2 \text{ m}^3/\text{s}$  is the high water level of 1,135 m in view of the dead storage capacity and the structure of the intake. Further, since the discharge water level of the

Upper Kihansi Project is EL. 1,140 m, the maximum dam scale is to the high water level of EL. 1,140 m.

The results of study for the cases of minimum and maximum dam scales are given in Table 8-16.

As a result of study, the incremental benefit due to head increase because of increase in dam scale is to exceed the incremental cost of increase in dam volume, and the optimum dam scale is determined as to be the dam of high water level of 1,140 m.

Table 8-16 Study on Optimum Dam Height of Lower Kihansi Reservoir

Item	Unit	Case 4	Case 4'
		Lower Kihansi	Lower Kihansi
High Water Level	m	1,140.00	1,135.00
Lower Water Level	m	1,137.00	1,129.00
Available Drawdown	m	3.00	6.00
Gross Storage Capacity	10 <sup>6</sup> m <sup>3</sup>	1.39	0.68
Effective Storage Capacity	10 <sup>6</sup> m <sup>3</sup>	0.48	0.48
Dam Type		Concrete gravity	Concrete gravity
Dam Height x Length		35 x 177	30 x 165
Dam Volume	10 <sup>3</sup> m <sup>3</sup>	54	47
Maximum Discharge	m <sup>3</sup> /s	22.20	22.20
Standard Intake Water Level	m	1,140.00	1,135.00
Tail Water Level	m	296.50	296.50
Gross Head	m	843.50	838.50
Effective Head	m	813.00	808.00
Installed Capacity	MW	153	152
Firm Peak Power	MW	101.8	101.0
Annual Energy Production	10 <sup>6</sup> kWh	868.9	861.9
Annual Firm Energy Production	10 <sup>6</sup> kWh	551.0	546.6
Annual Benefit			
Peak Power Benefit	10 <sup>3</sup> US\$	26,683	26,469
Firm Energy Benefit	10 <sup>3</sup> US\$	18,936	18,784
Total Benefit (B)	10 <sup>3</sup> US\$	45,619	45,253
Investment Cost			
Civil Facilities Cost	10 <sup>6</sup> US\$	119.9	117.9
Electro-Mechanical Facilities Cost	10 <sup>6</sup> US\$	86.4	85.9
Total	10 <sup>6</sup> US\$	206.3	203.6
Annual Cost			
Civil Facilities Cost	10 <sup>3</sup> US\$	12,697	12,486
Electro-Mechanical Facilities Cost	10 <sup>3</sup> US\$	10,256	10,196
Total Cost (C)	10 <sup>3</sup> US\$	22,953	22,682
Annual Surplus Benefit (B - C)	10 <sup>3</sup> US\$	22,666	22,571
Benefit Cost Ratio (B/C)		1.987	1.995
Unit Annual Cost	US\$/kWh	0.042	0.041

(2) Study on Maximum Discharge and Installed Capacity

In "8.2.2 Study on Reservoir Scale", the peak duration time for the Lower Kihansi Project is taken as 13 hours, with the firm discharge  $11.9 \text{ m}^3/\text{s}$  adding the firm discharge  $0.1 \text{ m}^3/\text{s}$  of the remaining catchment area to the firm discharge of the Upper Kihansi Project of  $11.8 \text{ m}^3/\text{s}$ , and the maximum discharge is selected to be  $22.2 \text{ m}^3/\text{s}$  with installed capacity 153 MW.

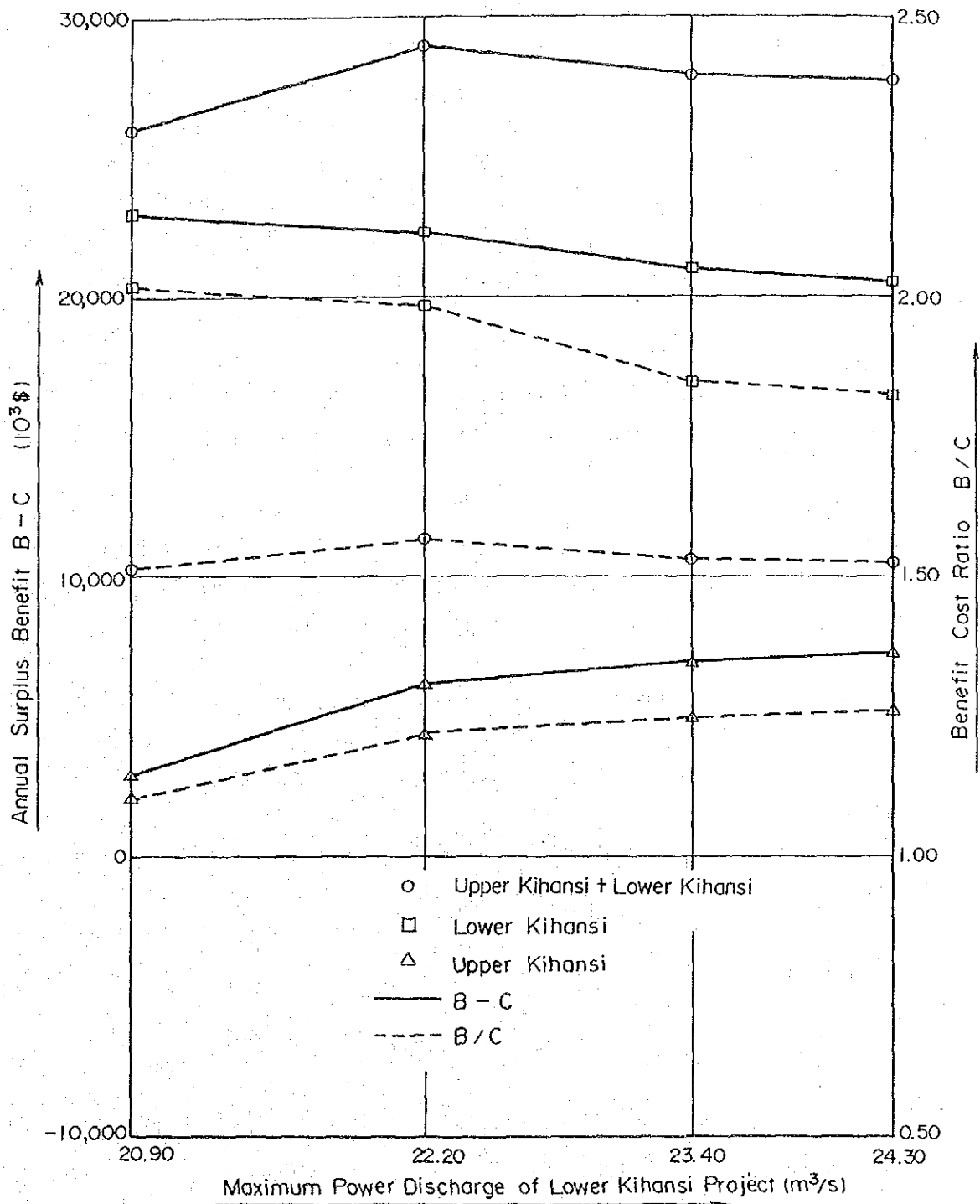
If the maximum discharge is to be increased over  $22.2 \text{ m}^3/\text{s}$ , it will result in a slight increase in firm energy in spite of increase in firm peak power because the maximum discharge of the Upper Kihansi Project is set larger than the project. A comparison study is made in the cases that maximum discharge is increased to  $24.3 \text{ m}^3/\text{s}$  and  $23.4 \text{ m}^3/\text{s}$  and is decreased to  $20.9 \text{ m}^3/\text{s}$ . The result is shown in Table 8-17 and Fig. 8-13.

As a result of the study if the maximum discharge is increased the incremental cost due to increase in maximum discharge is to exceed the incremental benefit and if the maximum discharge is decreased the reduction benefit due to decrease in maximum discharge is to exceed the reduction cost. Thus the maximum discharge is determined to be  $22.2 \text{ m}^3/\text{s}$  with installed capacity 153MW.

Table 8-17 Study on Optimum Discharge of Lower Kihansi Project

Item	Unit	Case 2'			Case 3'			Case 4			Case 5'		
		Upper Kihansi	Lower Kihansi	Total	Upper Kihansi	Lower Kihansi	Total	Upper Kihansi	Lower Kihansi	Total	Upper Kihansi	Lower Kihansi	Total
High Water Level	m	1,360.00	1,140.00		1,360.00	1,140.00		1,360.00	1,140.00		1,360.00	1,140.00	
Lower Water Level	m	1,330.00	1,113.00		1,330.00	1,113.00		1,330.00	1,113.00		1,330.00	1,113.00	
Available Drawdown	m	30.00	27.00		30.00	27.00		30.00	27.00		30.00	27.00	
Gross Storage Capacity	10 <sup>6</sup> m <sup>3</sup>	94.90	1.39		94.90	1.39		94.90	1.39		94.90	1.39	
Effective Storage Capacity	10 <sup>6</sup> m <sup>3</sup>	75.10	0.48		75.10	0.48		75.10	0.48		75.10	0.48	
Dam Type		Rockfill	Concrete		Rockfill	Concrete		Rockfill	Concrete		Rockfill	Concrete	
Dam Height x Length	10 <sup>3</sup> m <sup>3</sup>	95x583	95x177		95x583	95x177		95x583	95x177		95x583	95x177	
Dam Volume	10 <sup>6</sup> m <sup>3</sup>	5,300	54		5,300	54		5,300	54		5,300	54	
Maximum Discharge	m <sup>3</sup> /s	25.70	24.30		25.70	23.40		25.70	22.20		25.70	20.90	
Standard Intake Water Level	m	1,360.00	1,140.00		1,360.00	1,140.00		1,360.00	1,140.00		1,360.00	1,140.00	
Tail Water Level	m	1,138.50	296.50		1,138.50	296.50		1,138.50	296.50		1,138.50	296.50	
Gross Head	m	221.50	843.50		221.50	843.50		221.50	843.50		221.50	843.50	
Effective Head	m	214.50	813.00		214.50	813.00		214.50	813.00		214.50	813.00	
Installed Capacity	MW	47	167		47	161		47	153		47	144	
Firm Peak Power	MW	86.1	101.8	187.9	86.1	101.8	187.9	86.1	101.8	187.9	86.1	101.8	180.7
Annual Energy Production	10 <sup>6</sup> kWh	275.4	886.6	1,162.0	275.4	880.1	1,155.5	275.4	880.1	1,144.0	274.9	854.8	1,129.7
Annual Firm Energy Production	10 <sup>6</sup> kWh	366.5	551.0	917.5	366.5	551.0	908.8	366.5	551.0	886.7	366.5	551.0	848.5
Annual Benefit	10 <sup>3</sup> US\$	22,568	26,683	49,251	22,568	26,683	49,251	22,568	26,683	49,251	22,568	26,683	47,364
Peak Power Benefit	10 <sup>3</sup> US\$	12,595	18,936	31,531	12,595	18,936	31,531	12,595	18,936	31,531	12,595	18,936	29,160
Firm Energy Benefit	10 <sup>3</sup> US\$	35,163	45,619	80,782	35,163	45,619	80,782	35,163	45,619	80,782	35,163	45,619	76,524
Total Benefit (B)													
Investment Cost	10 <sup>6</sup> US\$	239.5	126.8	366.3	239.5	125.0	364.5	239.5	119.9	359.4	239.5	118.3	357.8
Civil Facilities Cost	10 <sup>6</sup> US\$	21.5	97.9	119.4	21.5	96.3	117.8	21.5	86.4	107.9	21.5	85.3	106.8
Electro-Mechanical Facilities Cost	10 <sup>6</sup> US\$	261.0	224.7	485.7	261.0	221.3	482.3	261.0	206.3	467.3	261.0	203.6	464.6
Total Cost (C)													
Annual Cost	10 <sup>3</sup> US\$	25,363	13,428	38,781	25,363	13,238	38,060	25,363	12,697	38,060	25,363	12,528	37,891
Civil Facilities Cost	10 <sup>3</sup> US\$	2,552	11,621	14,173	2,552	11,431	12,808	2,552	10,256	12,808	2,552	10,125	12,677
Electro-Mechanical Facilities Cost	10 <sup>3</sup> US\$	27,915	25,049	52,964	27,915	24,669	52,584	27,915	22,953	52,584	27,915	22,653	50,568
Total Cost (C)													
Annual Surplus Benefit (B - C)	10 <sup>3</sup> US\$	7,248	20,570	27,818	6,950	20,950	27,900	6,190	22,665	28,856	2,990	22,966	25,956
Benefit Cost Ratio (B/C)	US\$/kWh	1.360	1.821	1.525	1.248	1.849	1.531	1.221	1.887	1.557	1.107	1.814	1.513
Unit Annual Cost		0.076	0.045	0.088	0.078	0.045	0.088	0.078	0.042	0.083	0.094	0.041	0.060

Fig. 8-13 Study on Optimum Discharge of Lower Kihansi Project





(3) Study of Number of Turbine and Generator Units

For an installed capacity of 153 MW, the four alternatives of 1 unit, 2 units, 3 units and 4 units are conceivable when considering the number of turbine and generator units, and the following can be said about the four alternatives.

- In case of the 1-unit alternative, economy of scale in the construction cost can be expected, but the capacity of the single unit is too large compared with the capacity of the power system and the frequency drops in the system of a tripping accident are great.
- With the 2-unit alternative, the capacity of one unit is 76.5 MW and still large, and in case of a tripping accident the frequency drop in the system exceed the limit.
- With the 3-unit alternative the degree of freedom in operation is considered to be adequate. There is also no problem in system operation.
- With the 4-unit alternative, there is also no problem in system operation, but the construction cost is to be comparatively high.

Therefore, 3 units of unit capacity 51 MW which is the most reasonable from the standpoints of development scale and the economics is to be selected.

(4) Installed Capacity of Lower Kihansi Project Prior to Start-up of Upper Kihansi Project

The Lower Kihansi Project has headrace, penstock, and tailrace in a single line, so that in independent operation of the Lower Kihansi Project prior to start-up of the Upper Kihansi Project, the dam and waterways are all to be completed at the time of starting independent operation, but it is possible for turbines and generators to be partially commissioned at the time of independent operation. The number of turbine and generator units for the Lower Kihansi Project is decided as 3. If 2 units are to be commissioned at the time of independent start-up, the maximum available discharge is  $14.8 \text{ m}^3/\text{s}$  and the installed capacity 102 MW. Since the firm output at the time of independent start-up of the Lower Kihansi Project is to be 101.8 MW, there is no shortage in firm output even with commissioning of 2 units. The plant factor of firm energy of  $551 \times 10^6 \text{ kWh}$  is to be 61.7 per cent and lower than the annual load factor of the system of 64 per cent, so that all of the firm energy can be consumed within the system. Therefore, at the time of independent start-up of the Lower Kihansi Project, it is thought that partial commissioning with 102 MW of initial capacity makes it possible to avoid unnecessary advance investment. This may be suitable in its way, from a view point focussing on the advance investment.

However, independent start up with a full capacity of 153 MW is recommended due to the following reasons.

At the time of independent start-up of the Lower Kihansi Project, there are thermal power stations amounting to 110 MW included in the power system, and in case the energy production of hydroelectric power stations is considered in terms of firm energy,  $226 \times 10^6$  kWh in 1997 and  $375 \times 10^6$  kWh in 1998 are to be generated at these thermal power stations. Since it is desirable for power generation by these thermal power stations to be continuous operation for base load, the operating capacity is to be 26 MW in 1997 and 43 MW in 1998. When the inflow of hydro power stations has become 17 per cent over firm discharge, there is no necessity for thermal power generation in both 1997 and 1998. The results of study in case of making the installed capacity of the Lower Kihansi Project at the time of independent start-up partial commissioning with 102 MW are shown in Table 8-18.

Table 8-18 Actual Reserved Margin in 1997 and 1998

Year	System Demand			System Availability															
	GWh	MW	MW with 15% Reserve	Hydro Firm Base						Hydro 17% Incremental Base									
				Hydro		Thermal		Total		Hydro		Thermal		Total					
				GWh	MW	GWh	MW	GWh	MW	GWh	MW	GWh	MW	GWh	MW	GWh	MW	%	
1997	2,449	437	502	2,226	475	223	26	2,449	501	64	14.6	2,501	475	0	0	2,601	475	38	8.7
1998	2,601	463	534	2,226	475	375	43	2,601	581	55	11.9	2,601	475	0	0	2,601	475	12	2.6

According to the results of study, in order to secure reserve capacity of 15 per cent within the system, in case of considering inflow at hydro power plants on the basis of firm discharge, it is to be necessary for standby operation of thermal power stations of 1 MW and 16 MW, respectively, for 1997 and 1998, and in case of considering 17 per cent extra over firm discharge, 28 MW and 59 MW, respectively.

If the Lower Kihansi Project at the time of independent start-up is to be started up with all 153 MW of installed capacity, it becomes unnecessary for such standby operation of thermal power plants, while it is also unnecessary for back-up by thermal power stations in case of faulting of power sources so that probability of faulting within the system is resulted to be lowered, and it is extremely effective for improving the reliability of the system. Therefore, the Lower Kihansi Project is to be started up independently with its fully installed capacity of 153 MW.

(5) Optimum Development Plan

The outline of the optimum development plan of the Lower Kihansi Project determined as a result of the studies made up to this point are shown in Table 8-19. The monthly energy productions and firm energies with independent start-up of the Lower Kihansi Project for the 61-year period from 1927 to 1987 are shown in Tables 8-20 and 8-21, and in Fig. 8-19. The monthly peak power and peak power durations are shown in Tables 8-22 and 8-23. The monthly energy productions and firm energy production of the Lower Kihansi Project after commissioning of the Upper Kihansi Project are shown

in Tables 8-24 and 8-25, and in Fig. 8-15. The monthly peak power and peak power duration are given in Tables 8-26 and 8-27. The preliminary estimation of construction cost of the optimum development plan is given in Table 8-28.

Table 8-19 Outline of Optimum Development Plan  
of Lower Kihansi Project

Reservoir

Catchment Area	590 km <sup>2</sup>
High Water Level	1,140.00 m
Low Water Level	1,137.00 m
Available Drawdown	3.00 m
Gross Storage Capacity	1.39 × 10 <sup>6</sup> m <sup>3</sup>
Effective Storage Capacity	0.48 × 10 <sup>6</sup> m <sup>3</sup>
Annual Average Runoff	15.87 m <sup>3</sup> /s
Firm Discharge	9.40 m <sup>3</sup> /s

Dam

Type	Concrete Gravity
Height × Length	35 m × 177 m
Volume	54 × 10 <sup>3</sup> m <sup>3</sup>

Power Station

Standard Intake Water Level	1,140.00 m
Tail Water Level	296.50 m
Gross Head	843.50 m
Effective Head	813.00 m
Maximum Discharge	22.20 m <sup>3</sup> /s
Installed Capacity	153 MW
Unit Type × Number of Unit	Vertical Pelton×3
Firm Peak Power	151.0 MW (101.8 MW)
Annual Total Energy Production	906.9 × 10 <sup>6</sup> kWh (868.9 × 10 <sup>6</sup> kWh)
Annual Firm Energy Production	710.9 × 10 <sup>6</sup> kWh (511.0 × 10 <sup>6</sup> kWh)

Note: Figures in ( ) show the values of cases without the  
Upper Kihansi Project.

Table 8-20 Total Energy Generation of Lower Kihansi Project without Upper Kihansi Project

UNIT: 10<sup>6</sup> kWh

MONTH YEAR	< JAN >	< FEB >	< MAR >	< APR >	< MAY >	< JUN >	< JUL >	< AUG >	< SEP >	< OCT >	< NOV >	< DEC >	<TOTAL>
1927	83.60	66.80	64.00	77.50	61.30	53.60	50.60	47.00	43.10	42.20	38.80	56.20	664.70
1928	45.40	44.90	96.20	93.10	74.90	56.80	53.40	48.60	45.40	46.10	45.30	60.70	710.80
1929	47.20	38.50	64.80	110.00	60.30	51.40	47.80	43.80	39.70	38.50	35.60	39.00	616.60
1930	59.60	41.70	113.60	110.00	74.40	62.50	56.50	50.20	44.50	42.80	38.50	36.80	731.10
1931	51.10	66.80	113.60	110.00	113.60	81.90	73.00	63.60	54.50	50.50	44.50	50.50	873.60
1932	76.50	100.70	113.60	110.00	98.50	78.90	71.00	62.80	54.10	50.40	46.70	47.70	910.90
1933	87.80	87.40	113.60	110.00	86.00	70.00	63.50	56.90	49.80	47.00	42.20	40.70	854.90
1934	95.20	59.20	67.80	97.80	88.40	81.20	69.10	62.20	54.60	51.10	44.70	60.80	832.10
1935	73.20	70.40	113.60	70.50	66.50	57.40	53.70	48.90	44.00	47.00	45.30	113.60	804.10
1936	111.70	77.40	70.10	110.00	113.60	91.40	83.00	71.80	61.30	56.50	49.10	55.20	951.10
1937	68.00	50.70	113.60	110.00	110.30	75.20	68.10	60.40	54.40	52.20	46.40	44.30	853.60
1938	40.90	39.00	41.50	79.50	53.10	46.40	44.00	41.40	38.00	43.10	40.50	39.80	547.20
1939	67.40	40.30	64.90	110.00	95.30	69.40	62.70	55.60	49.30	46.40	42.30	42.50	746.10
1940	102.30	70.70	72.80	110.00	78.90	63.50	57.70	52.20	46.10	47.70	41.70	53.10	796.70
1941	53.60	91.90	100.30	73.90	99.20	62.30	57.00	51.00	44.90	43.60	57.10	56.80	791.60
1942	96.50	52.80	113.60	110.00	108.10	78.80	70.60	61.80	53.20	49.30	44.00	62.60	901.30
1943	45.30	53.50	69.20	76.40	113.60	58.00	52.90	47.40	42.40	40.90	36.90	55.90	672.40
1944	45.90	35.30	50.20	110.00	88.70	62.20	56.60	50.30	43.90	41.70	46.50	72.80	704.10
1945	85.40	61.10	74.60	110.00	113.60	70.80	64.40	56.70	49.00	45.60	40.60	53.80	825.60
1946	42.30	34.30	48.50	110.00	75.40	59.30	53.90	48.00	42.10	40.60	39.40	38.90	632.70
1947	83.20	66.60	101.30	110.00	99.20	74.40	65.50	57.60	49.70	46.60	41.10	113.60	908.80
1948	105.90	73.30	113.60	82.00	80.30	63.20	57.70	52.00	45.60	43.50	55.30	41.70	814.10
1949	51.70	95.60	62.20	100.10	66.90	55.10	50.70	45.70	40.70	39.30	35.50	34.60	678.10
1950	34.20	40.50	113.60	97.30	102.80	64.20	58.20	51.70	47.30	44.30	39.80	38.60	732.50
1951	40.40	51.80	55.50	110.00	72.30	53.50	50.70	45.10	40.20	38.60	78.80	54.40	691.30
1952	81.20	89.90	100.90	110.00	113.60	82.60	73.10	63.20	53.80	49.60	63.70	46.70	928.30
1953	42.60	34.40	60.40	64.40	83.30	51.60	47.80	43.30	38.80	37.80	34.30	47.40	586.10
1954	65.80	43.40	50.40	62.40	57.10	45.10	41.90	38.70	35.20	34.90	32.10	32.70	541.70
1955	37.50	78.30	76.00	110.00	113.60	83.20	72.40	62.80	53.30	48.80	46.50	42.90	825.30
1956	99.90	83.00	80.10	110.00	94.60	74.40	66.70	58.40	50.20	46.60	41.10	43.20	850.20
1957	98.40	86.00	86.10	110.00	113.60	75.30	68.90	64.60	58.00	56.10	51.40	60.10	928.50
1958	68.80	69.60	113.60	110.00	113.60	70.80	65.60	62.40	57.30	56.30	50.80	78.40	917.00
1959	71.20	70.60	107.90	106.80	77.90	61.20	60.20	57.70	52.60	52.80	50.50	60.50	829.90
1960	54.40	72.70	113.60	110.00	113.60	75.50	58.10	50.20	43.10	45.00	47.70	50.90	834.80
1961	60.80	68.50	79.70	98.10	107.60	49.10	53.40	57.40	44.40	44.90	55.80	82.20	801.90
1962	113.60	102.60	113.60	110.00	113.60	93.90	86.30	77.30	59.20	64.80	55.90	67.10	1057.90
1963	113.60	102.60	113.60	110.00	113.60	87.90	89.70	77.70	67.80	63.80	90.20	53.70	1084.20
1964	91.50	106.30	113.60	110.00	113.60	110.00	98.90	90.30	75.80	69.30	52.40	72.50	1114.20
1965	85.80	89.10	113.60	110.00	105.30	74.00	70.40	66.90	59.40	59.10	54.90	66.90	955.40
1966	83.90	79.70	113.60	110.00	113.60	82.30	70.50	68.50	61.00	40.90	38.80	43.40	906.20
1967	78.10	79.20	103.30	110.00	113.60	89.40	75.10	69.20	60.10	58.10	65.20	113.60	1014.90
1968	113.60	106.30	113.60	110.00	113.60	110.00	113.60	102.10	86.80	77.10	74.70	97.10	1218.50
1969	105.60	88.90	113.60	110.00	113.60	75.40	69.90	69.50	58.90	54.80	54.80	60.40	975.40
1970	104.40	102.60	113.60	110.00	85.60	67.00	66.10	61.30	55.00	51.00	45.00	88.60	950.20
1971	75.80	69.90	106.80	110.00	103.80	67.90	72.90	64.00	58.20	73.20	54.70	62.10	939.30
1972	87.40	79.20	113.60	110.00	113.60	92.40	81.70	69.20	70.60	65.50	61.40	113.60	1058.00
1973	113.60	102.60	113.60	110.00	113.60	92.70	84.00	73.30	67.10	64.70	61.50	73.90	1070.60
1974	99.10	102.60	89.90	110.00	113.60	101.30	85.10	70.20	67.20	63.60	58.80	47.50	1008.90
1975	77.20	56.30	70.90	110.00	113.60	86.90	72.30	65.50	61.50	54.60	47.50	56.90	873.20
1976	71.00	73.20	103.00	110.00	113.60	103.20	81.60	71.50	60.80	57.00	48.40	48.00	941.30
1977	67.10	47.40	71.50	110.00	110.80	73.90	65.50	58.70	50.70	48.70	52.80	76.50	833.60
1978	76.60	63.20	93.20	110.00	113.60	79.90	67.00	58.50	50.90	47.30	55.40	72.30	887.90
1979	101.60	87.70	113.60	110.00	113.60	110.00	113.60	89.50	73.30	64.70	62.40	79.10	1119.10
1980	83.50	78.70	79.90	102.30	113.60	73.70	67.10	60.40	52.50	50.00	46.90	57.40	866.00
1981	59.50	57.50	78.80	101.30	92.60	63.90	57.40	53.30	46.10	48.30	40.50	52.60	751.80
1982	45.50	49.30	61.80	96.70	113.60	68.60	61.40	53.90	47.80	52.50	55.00	80.30	786.60
1983	113.60	73.90	99.70	110.00	113.60	110.00	92.20	72.80	61.30	56.50	50.10	53.90	1007.60
1984	62.30	60.40	97.80	110.00	113.60	102.50	83.80	69.20	60.50	57.90	53.20	91.10	962.30
1985	113.60	83.00	113.60	110.00	113.60	106.80	91.50	74.90	64.40	58.70	66.40	103.30	1099.80
1986	113.60	102.60	113.60	110.00	113.60	110.00	113.60	94.80	73.20	65.80	76.20	113.60	1200.60
1987	113.60	98.80	113.60	110.00	113.60	89.70	78.60	68.10	57.10	56.50	55.40	71.90	1026.90
TOTAL	4739.60	4351.00	5642.00	6320.10	6071.40	4633.70	4210.20	3742.00	3271.70	3132.70	3079.00	3804.70	53000.10
AVERAGE	77.70	71.33	92.49	103.61	99.53	75.96	69.02	61.34	53.63	51.36	50.48	62.40	868.85
MAXIMUM	113.60	106.30	113.60	110.00	113.60	110.00	113.60	102.10	86.80	77.10	90.20	113.60	1218.50
MINIMUM	34.20	34.30	41.50	62.40	53.10	45.10	41.90	38.70	35.20	34.90	32.10	32.70	541.70



Table 8-21 Firm Energy Generation of Lower Kihansi Project without Upper Kihansi Project

UNIT: 10<sup>6</sup> kWh

MONTH YEAR	< JAN >	< FEB >	< MAR >	< APR >	< MAY >	< JUN >	< JUL >	< AUG >	< SEP >	< OCT >	< NOV >	< DEC >	< TOTAL >
1927	47.60	43.00	47.60	46.00	47.60	46.00	47.60	47.00	43.10	42.20	38.80	47.60	544.10
1928	45.30	44.50	47.60	46.00	47.60	46.00	47.60	47.60	45.30	46.10	45.30	47.60	556.50
1929	47.20	38.40	47.60	46.00	47.60	46.00	47.60	43.70	39.70	38.50	35.50	38.90	516.70
1930	47.60	41.70	47.60	46.00	47.60	46.00	47.60	47.60	44.40	42.70	38.50	36.80	534.10
1931	47.60	43.00	47.60	46.00	47.60	46.00	47.60	47.60	46.00	47.60	44.40	47.60	558.60
1932	47.60	44.50	47.60	46.00	47.60	46.00	47.60	47.60	46.00	47.60	42.20	40.60	548.80
1933	47.60	43.00	47.60	46.00	47.60	46.00	47.60	47.60	46.00	47.60	44.70	47.60	558.90
1934	47.60	43.00	47.60	46.00	47.60	46.00	47.60	47.60	46.00	47.60	42.20	47.60	556.90
1935	47.60	43.00	47.60	46.00	47.60	46.00	47.60	47.60	44.00	47.60	45.30	47.60	556.90
1936	47.60	44.50	47.60	46.00	47.60	46.00	47.60	47.60	46.00	47.60	46.00	47.60	561.70
1937	47.60	43.00	47.60	46.00	47.60	46.00	47.60	47.60	46.00	47.60	42.20	40.60	548.80
1938	40.90	38.90	41.40	46.00	47.60	46.00	44.00	41.30	38.00	43.00	40.40	39.70	507.20
1939	47.60	40.30	47.60	46.00	47.60	46.00	47.60	47.60	46.00	46.30	42.30	42.40	547.30
1940	47.60	46.50	47.60	46.00	47.60	46.00	47.60	47.60	46.00	47.60	41.70	47.60	557.40
1941	47.60	43.00	47.60	46.00	47.60	46.00	47.60	47.60	44.80	43.50	46.00	47.60	554.90
1942	47.60	43.00	47.60	46.00	47.60	46.00	47.60	47.60	46.00	47.60	44.00	47.60	558.20
1943	45.20	43.00	47.60	46.00	47.60	46.00	48.00	41.60	47.30	42.30	40.90	36.90	526.20
1944	45.80	35.30	47.60	46.00	47.60	46.00	47.60	47.60	43.90	41.70	46.00	47.60	542.70
1945	47.60	43.00	47.60	46.00	47.60	46.00	47.60	47.60	46.00	45.60	40.50	47.60	552.70
1946	42.30	34.30	47.60	46.00	47.60	46.00	47.60	47.60	42.00	40.60	39.30	38.90	519.80
1947	47.60	43.00	47.60	46.00	47.60	46.00	47.60	47.60	46.00	46.50	41.00	47.60	554.20
1948	47.60	44.50	47.60	46.00	47.60	46.00	47.60	47.60	45.50	43.40	46.00	41.70	551.10
1949	47.60	43.00	47.60	46.00	47.60	46.00	47.60	45.70	40.70	39.30	35.50	34.50	521.10
1950	34.20	40.40	47.60	46.00	47.60	46.00	47.60	47.60	46.00	44.30	39.80	38.50	525.60
1951	40.30	43.00	47.60	46.00	47.60	46.00	47.60	45.00	40.10	38.60	46.00	47.60	535.40
1952	47.60	44.50	47.60	46.00	47.60	46.00	47.60	47.60	46.00	47.60	46.00	46.70	560.80
1953	42.50	34.40	47.60	46.00	47.60	46.00	47.60	43.30	38.80	37.80	34.30	47.40	513.30
1954	47.60	43.00	47.60	46.00	47.60	45.10	41.90	38.70	35.20	34.90	32.10	32.70	492.40
1955	37.50	43.00	47.60	46.00	47.60	46.00	47.60	47.60	46.00	47.60	46.00	42.80	545.30
1956	47.60	44.50	47.60	46.00	47.60	46.00	47.60	47.60	46.00	46.60	41.00	43.20	551.30
1957	47.60	43.00	47.60	46.00	47.60	46.00	47.60	47.60	46.00	47.60	46.00	47.60	560.20
1958	47.60	43.00	47.60	46.00	47.60	46.00	47.60	47.60	46.00	47.60	46.00	47.60	560.20
1959	47.60	43.00	47.60	46.00	47.60	46.00	47.60	47.60	46.00	47.60	46.00	47.60	560.20
1960	47.60	44.50	47.60	46.00	47.60	46.00	47.60	47.60	43.10	45.00	46.00	47.60	556.20
1961	47.60	43.00	47.60	46.00	47.60	46.00	47.60	47.60	44.30	44.80	46.00	47.60	555.70
1962	47.60	43.00	47.60	46.00	47.60	46.00	47.60	47.60	46.00	47.60	46.00	47.60	560.20
1963	47.60	43.00	47.60	46.00	47.60	46.00	47.60	47.60	46.00	47.60	46.00	47.60	560.20
1964	47.60	46.50	47.60	46.00	47.60	46.00	47.60	47.60	46.00	47.60	46.00	47.60	561.70
1965	47.60	43.00	47.60	46.00	47.60	46.00	47.60	47.60	46.00	47.60	46.00	47.60	560.20
1966	47.60	43.00	47.60	46.00	47.60	46.00	47.60	47.60	46.00	40.90	38.80	43.40	542.10
1967	47.60	43.00	47.60	46.00	47.60	46.00	47.60	47.60	46.00	47.60	46.00	47.60	560.20
1968	47.60	44.50	47.60	46.00	47.60	46.00	47.60	47.60	46.00	47.60	46.00	47.60	561.70
1969	47.60	43.00	47.60	46.00	47.60	46.00	47.60	47.60	46.00	47.60	46.00	47.60	560.20
1970	47.60	43.00	47.60	46.00	47.60	46.00	47.60	47.60	46.00	47.60	44.90	47.60	559.10
1971	47.60	43.00	47.60	46.00	47.60	46.00	47.60	47.60	46.00	47.60	46.00	47.60	560.20
1972	47.60	44.50	47.60	46.00	47.60	46.00	47.60	47.60	46.00	47.60	46.00	47.60	561.70
1973	47.60	43.00	47.60	46.00	47.60	46.00	47.60	47.60	46.00	47.60	46.00	47.60	560.20
1974	47.60	43.00	47.60	46.00	47.60	46.00	47.60	47.60	46.00	47.60	46.00	47.50	560.10
1975	47.60	43.00	47.60	46.00	47.60	46.00	47.60	47.60	46.00	47.60	46.00	47.60	560.20
1976	47.60	44.50	47.60	46.00	47.60	46.00	47.60	47.60	46.00	47.60	46.00	47.60	561.70
1977	47.60	43.00	47.60	46.00	47.60	46.00	47.60	47.60	46.00	47.60	46.00	47.60	560.20
1978	47.60	43.00	47.60	46.00	47.60	46.00	47.60	47.60	46.00	47.30	46.00	47.60	559.90
1979	47.60	43.00	47.60	46.00	47.60	46.00	47.60	47.60	46.00	47.60	46.00	47.60	560.20
1980	47.60	44.50	47.60	46.00	47.60	46.00	47.60	47.60	46.00	47.60	46.00	47.60	561.70
1981	47.60	43.00	47.60	46.00	47.60	46.00	47.60	47.60	46.00	47.60	40.50	47.60	554.70
1982	45.50	43.00	47.60	46.00	47.60	46.00	47.60	47.60	46.00	47.60	46.00	47.60	558.10
1983	47.60	43.00	47.60	46.00	47.60	46.00	47.60	47.60	46.00	47.60	46.00	47.60	560.20
1984	47.60	44.50	47.60	46.00	47.60	46.00	47.60	47.60	46.00	47.60	46.00	47.60	561.70
1985	47.60	43.00	47.60	46.00	47.60	46.00	47.60	47.60	46.00	47.60	46.00	47.60	560.20
1986	47.60	43.00	47.60	46.00	47.60	46.00	47.60	47.60	46.00	47.60	46.00	47.60	560.20
1987	47.60	43.00	47.60	46.00	47.60	46.00	47.60	47.60	46.00	47.60	46.00	47.60	560.20
TOTAL	2846.70	2603.70	2897.40	2806.00	2903.60	2805.10	2894.30	2874.80	2739.20	2788.20	2669.70	2782.60	33611.30
AVERAGE	46.67	42.68	47.50	46.00	47.60	45.99	47.45	47.13	44.90	45.71	43.77	45.62	551.00
MAXIMUM	47.60	44.50	47.60	46.00	47.60	46.00	47.60	47.60	46.00	47.60	46.00	47.60	561.70
MINIMUM	34.20	34.30	41.40	46.00	47.60	45.10	41.90	38.70	35.20	34.90	32.10	32.70	492.40

Table 8-22 Monthly Peak Power of Lower Kihansi Project without Upper Kihansi Project

UNIT: MW

MONTH YEAR	< JAN >	< FEB >	< MAR >	< APR >	< MAY >	< JUN >	< JUL >	< AUG >	< SEP >	< OCT >	< NOV >	< DEC >	<TOTAL>
1927	118.00	118.00	118.00	118.00	118.00	118.00	118.00	116.57	110.43	104.73	99.49	118.00	1375.21
1928	112.52	118.00	118.00	118.00	118.00	118.00	118.00	116.26	114.28	116.07	118.00	118.00	1403.13
1929	117.10	105.62	118.00	118.00	118.00	118.00	118.00	108.54	101.81	95.53	91.08	96.63	1306.30
1930	118.00	114.45	118.00	118.00	118.00	118.00	118.00	113.96	106.08	98.63	91.20	1350.30	1350.30
1931	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	113.93	118.00	1411.93
1932	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	1416.00
1933	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	116.61	108.22	100.78	1387.61
1934	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	114.57	118.00	1412.57
1935	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	112.79	116.58	116.13	118.00	1407.50
1936	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	1416.00
1937	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	109.93	1407.93
1938	101.42	106.94	102.79	118.00	118.00	118.00	109.11	102.59	97.44	106.75	103.64	98.56	1283.26
1939	118.00	110.59	118.00	118.00	118.00	118.00	118.00	118.00	118.00	114.95	108.35	105.26	1383.15
1940	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	106.94	118.00	1404.94
1941	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	114.94	108.06	118.00	118.00	1402.99
1942	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	112.72	118.00	1410.72
1943	112.27	118.00	118.00	118.00	118.00	118.00	118.00	117.43	108.56	101.49	94.58	88.91	1331.25
1944	113.68	93.54	118.00	118.00	118.00	118.00	118.00	118.00	112.45	103.44	118.00	118.00	1367.11
1945	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	113.04	103.90	118.00	1396.94
1946	104.95	94.24	118.00	118.00	118.00	118.00	118.00	118.00	107.77	100.63	100.80	96.49	1312.87
1947	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	115.63	105.23	118.00	1400.86
1948	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	116.72	107.77	118.00	103.39	1389.88
1949	118.00	118.00	118.00	118.00	118.00	118.00	118.00	113.34	104.28	97.52	90.93	85.65	1317.73
1950	84.84	111.11	118.00	118.00	118.00	118.00	118.00	118.00	118.00	109.81	101.94	95.62	1329.32
1951	100.09	118.00	118.00	118.00	118.00	118.00	118.00	111.73	102.95	95.70	118.00	118.00	1354.47
1952	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	115.78	1413.78
1953	105.49	96.51	118.00	118.00	118.00	118.00	118.00	107.34	99.40	93.71	87.89	117.60	1295.94
1954	118.00	118.00	118.00	118.00	118.00	115.59	103.85	95.92	90.27	86.56	82.30	81.04	1245.54
1955	93.06	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	106.26	1379.31
1956	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	115.56	105.19	107.20	1389.95
1957	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	1416.00
1958	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	1416.00
1959	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	1416.00
1960	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	110.53	111.57	118.00	118.00	1402.10
1961	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	113.67	111.24	118.00	118.00	1404.91
1962	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	1416.00
1963	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	1416.00
1964	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	1416.00
1965	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	1416.00
1966	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	101.51	99.46	107.71	1370.68
1967	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	1416.00
1968	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	1416.00
1969	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	1416.00
1970	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	115.25	118.00	1413.25
1971	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	1416.00
1972	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	1416.00
1973	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	1416.00
1974	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	117.83	1415.83
1975	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	1416.00
1976	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	1416.00
1977	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	1416.00
1978	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	116.00	117.31	118.00	118.00	1415.31
1979	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	1416.00
1980	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	1416.00
1981	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	103.73	118.00	1401.73
1982	112.86	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	1410.86
1983	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	1416.00
1984	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	1416.00
1985	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	1416.00
1986	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	1416.00
1987	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	1416.00
TOTAL	7058.27	7084.98	7182.79	7198.00	7198.00	7195.59	7174.96	7127.48	7026.25	6914.06	6846.98	6899.82	84907.18
AVERAGE	115.71	116.15	117.75	118.00	118.00	117.96	117.62	116.84	115.18	113.35	112.25	113.11	1391.92
MAXIMUM	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	118.00	1416.00
MINIMUM	84.84	93.54	102.79	118.00	118.00	115.59	103.85	95.92	90.27	86.56	82.30	81.04	1245.54







Table 8-24 Total Energy Production of Lower Kihansi Project with Upper Kihansi Project

UNIT: 10<sup>6</sup> kWh

MONTH YEAR	< JAN >	< FEB >	< MAR >	< APR >	< MAY >	< JUN >	< JUL >	< AUG >	< SEP >	< OCT >	< NOV >	< DEC >	< TOTAL >
1927	113.60	102.60	61.20	59.40	61.10	59.10	61.00	61.00	58.10	62.20	38.80	56.20	774.30
1928	45.40	44.90	68.80	59.50	61.30	59.10	61.00	61.00	59.00	60.90	59.00	61.10	701.00
1929	57.10	38.50	61.20	60.00	61.10	59.10	61.00	60.90	58.90	58.20	35.60	39.00	650.60
1930	59.60	41.70	98.80	64.30	61.30	59.20	61.10	61.00	59.00	60.90	58.90	60.80	746.60
1931	61.00	58.20	113.60	110.00	80.00	74.80	78.70	68.20	61.60	61.00	59.00	61.00	895.10
1932	106.60	106.30	113.60	110.00	83.80	71.80	76.70	67.40	61.20	61.00	59.00	61.00	978.40
1933	113.60	102.60	113.60	60.00	61.40	59.30	61.10	61.40	59.00	61.00	59.00	60.90	872.80
1934	107.90	95.90	64.00	59.60	61.40	59.40	61.20	61.10	59.10	61.00	59.00	63.20	812.80
1935	105.10	102.60	112.20	59.30	61.20	59.10	61.00	61.00	59.00	55.00	45.30	61.90	842.70
1936	113.60	106.30	66.30	110.00	113.60	91.40	88.80	76.40	68.40	66.90	59.00	68.70	1029.40
1937	99.90	87.30	113.60	59.00	72.70	68.10	73.90	65.00	61.50	62.60	59.00	60.90	884.40
1938	67.10	75.60	60.90	59.40	61.00	59.00	47.70	41.40	38.00	43.10	40.50	39.80	633.50
1939	61.20	46.50	61.20	110.00	61.50	60.60	68.50	41.10	59.00	60.90	58.90	60.90	770.30
1940	113.60	106.30	69.00	70.70	61.30	59.20	61.10	61.00	59.00	61.00	58.90	61.00	842.10
1941	61.00	102.60	96.90	59.30	61.60	59.20	61.10	61.00	59.00	60.90	59.10	61.10	802.80
1942	67.20	89.40	113.60	98.30	72.70	71.70	76.30	66.40	60.30	61.00	59.00	69.80	905.70
1943	77.20	90.10	65.40	59.40	61.80	59.10	61.00	61.00	58.90	60.90	58.90	55.40	769.10
1944	45.90	35.30	50.20	60.30	61.40	59.20	61.10	61.00	59.00	60.90	59.00	61.30	674.60
1945	101.40	97.70	70.80	60.00	84.60	63.70	70.20	61.30	59.00	60.90	58.90	61.00	849.50
1946	64.20	71.00	61.30	87.80	61.30	59.10	61.00	61.00	58.90	60.90	58.90	60.90	766.00
1947	61.40	81.10	97.50	59.80	61.60	59.30	61.20	61.10	59.00	60.90	58.90	112.90	834.70
1948	113.60	106.30	113.60	59.40	61.30	59.20	61.10	61.00	59.00	60.90	59.10	60.90	875.40
1949	58.50	72.00	61.10	59.60	61.20	59.10	61.00	60.90	58.90	60.90	37.10	34.60	684.90
1950	34.20	40.50	90.10	59.40	61.60	59.20	61.10	61.00	59.00	60.90	58.90	60.90	707.00
1951	60.90	55.20	61.00	59.80	61.30	59.10	61.00	60.90	58.90	49.60	59.40	61.00	708.10
1952	61.40	98.90	97.10	71.90	113.60	82.60	78.90	67.80	60.90	61.00	72.50	60.90	927.50
1953	73.90	71.10	61.10	59.20	61.40	59.10	61.00	60.90	50.60	37.80	34.30	47.40	677.80
1954	61.20	48.00	50.40	59.20	61.10	46.30	41.90	38.70	35.20	34.90	32.10	32.70	541.70
1955	37.50	55.50	71.40	110.00	80.20	74.10	78.20	67.50	60.40	61.00	59.00	60.90	817.70
1956	113.60	106.30	76.30	110.00	61.50	66.90	72.50	63.00	59.00	60.90	58.90	60.90	909.80
1957	112.40	102.60	85.20	106.10	111.40	68.20	74.60	69.20	65.10	66.50	61.20	73.80	996.30
1958	100.70	102.60	113.60	110.00	86.90	63.70	71.40	67.00	64.40	66.70	60.50	92.10	999.60
1959	103.00	102.60	104.10	59.70	61.30	59.20	61.10	61.10	59.10	61.00	59.00	61.10	852.30
1960	61.00	106.30	113.60	110.00	113.60	68.40	63.90	61.00	59.00	60.90	59.00	61.00	937.70
1961	74.30	102.60	75.90	59.60	61.70	59.00	61.00	61.10	59.00	60.90	59.10	61.40	795.60
1962	113.60	102.60	113.60	110.00	113.60	93.90	92.10	81.90	66.30	75.20	65.60	80.80	1109.20
1963	113.60	102.60	113.60	110.00	113.60	87.90	95.50	82.30	74.90	74.20	100.00	67.40	1135.60
1964	113.60	106.30	113.60	110.00	113.60	110.00	104.70	94.90	82.90	79.70	72.10	86.20	1187.60
1965	113.60	102.60	113.60	110.00	77.20	66.90	76.20	71.50	66.50	69.50	64.70	80.60	1012.90
1966	113.60	102.60	113.60	110.00	113.60	75.20	76.30	73.20	68.10	60.90	58.90	60.90	1026.90
1967	86.30	102.60	99.50	63.60	107.30	82.30	80.90	73.80	67.20	68.50	75.90	113.60	1020.60
1968	113.60	106.30	113.60	110.00	113.60	110.00	113.60	106.70	93.90	87.50	84.50	110.80	1264.10
1969	113.60	102.60	113.60	89.50	88.40	68.30	75.70	74.10	66.00	65.20	64.50	74.10	995.60
1970	113.60	102.60	113.60	110.00	61.40	59.20	68.50	66.00	62.10	61.40	59.00	98.10	975.50
1971	107.70	102.60	109.70	110.00	68.30	60.80	78.70	68.70	65.30	83.60	64.50	75.80	995.70
1972	113.60	106.30	113.60	110.00	113.60	92.40	87.50	73.90	77.70	75.90	71.20	113.60	1149.30
1973	113.60	102.60	113.60	110.00	113.60	92.70	89.80	78.00	74.20	75.10	71.20	87.60	1122.00
1974	113.60	102.60	113.60	110.00	113.60	101.30	90.90	74.90	74.30	74.00	68.50	61.20	1098.50
1975	109.10	93.00	67.10	63.80	95.30	79.80	78.10	70.10	68.60	65.00	59.00	68.80	917.70
1976	102.90	106.30	99.20	68.70	96.70	96.10	87.40	76.10	67.90	67.40	59.00	61.00	988.70
1977	98.90	84.10	67.70	59.90	66.10	66.80	71.30	63.30	59.00	61.00	59.40	90.20	847.70
1978	108.50	99.80	89.40	63.60	85.20	72.80	72.80	63.10	59.00	61.00	60.80	86.00	922.00
1979	113.60	102.60	113.60	110.00	113.60	110.00	113.60	94.10	80.40	75.10	72.20	92.80	1191.60
1980	113.60	106.30	76.10	59.70	61.80	59.30	69.10	65.00	59.60	61.00	59.00	68.10	856.60
1981	91.40	94.10	75.00	59.60	61.50	59.20	61.10	61.00	59.00	61.00	58.90	61.00	802.80
1982	60.90	55.10	61.10	59.60	61.90	59.30	61.10	61.00	59.00	61.00	59.10	86.70	745.80
1983	113.60	102.60	109.30	85.80	113.60	107.50	97.90	77.40	68.40	66.90	59.90	67.60	1070.50
1984	94.20	97.00	94.00	69.40	111.70	95.40	89.60	73.80	67.60	68.30	62.90	104.80	1028.70
1985	113.60	102.60	113.60	110.00	113.60	99.70	97.20	79.50	71.50	69.10	76.20	113.60	1160.20
1986	113.60	102.60	113.60	110.00	113.60	110.00	113.60	99.50	80.30	76.20	85.90	113.60	1232.50
1987	113.60	102.60	113.60	59.80	83.40	82.60	84.40	72.70	64.20	66.90	65.20	85.60	994.60
TOTAL	5560.90	5446.60	5560.00	4974.10	4983.20	4416.00	4511.00	4138.30	3847.30	3856.60	3689.80	4338.90	55322.70
AVERAGE	91.16	89.29	91.15	81.54	81.69	72.39	73.95	67.84	63.07	63.22	60.49	71.13	906.93
MAXIMUM	113.60	106.30	113.60	110.00	113.60	110.00	113.60	106.70	93.90	87.50	100.00	113.60	1264.10
MINIMUM	34.20	35.30	50.20	59.20	61.00	46.30	41.90	38.70	35.20	34.90	32.10	32.70	541.70

Table 8-25 Firm Energy Production of Lower Kihansi Project with Upper Kihansi Project

UNIT: 10<sup>6</sup> kWh

MONTH YEAR	< JAN >	< FEB >	< MAR >	< APR >	< MAY >	< JUN >	< JUL >	< AUG >	< SEP >	< OCT >	< NOV >	< DEC >	< TOTAL >
1927	61.50	55.60	61.20	59.40	61.10	59.10	61.00	61.00	58.10	42.20	38.80	56.20	675.20
1928	45.40	44.90	61.50	59.50	61.30	59.10	61.00	61.00	59.00	60.90	59.00	61.10	693.70
1929	57.10	38.50	61.20	59.60	61.10	59.10	61.00	60.90	58.90	58.20	35.60	39.00	650.20
1930	59.60	41.70	61.50	59.60	61.30	59.20	61.10	61.00	59.00	60.90	58.90	60.80	704.60
1931	61.00	55.60	61.50	59.60	61.50	59.60	61.50	61.50	59.60	61.00	59.00	61.00	722.40
1932	61.50	57.60	61.50	59.60	61.50	59.60	61.50	61.50	59.60	61.00	59.00	61.00	724.90
1933	61.50	55.60	61.50	59.60	61.40	59.30	61.10	61.40	59.00	61.00	58.90	60.90	721.20
1934	61.50	55.60	61.50	59.60	61.40	59.40	61.20	61.10	59.10	61.00	59.00	61.50	721.90
1935	61.50	55.60	61.50	59.30	61.20	59.10	61.00	61.00	59.00	55.00	45.30	61.50	701.00
1936	61.50	57.60	61.50	59.60	61.50	59.60	61.50	61.50	59.60	61.50	59.00	61.50	725.90
1937	61.50	55.60	61.50	59.40	61.50	59.60	61.50	61.50	59.60	61.50	59.00	60.90	723.30
1938	61.50	55.60	60.90	59.40	61.00	59.00	47.70	41.40	38.00	43.10	40.50	39.80	607.90
1939	61.20	46.50	61.20	59.60	61.50	59.60	61.50	61.10	59.00	60.90	58.90	60.90	711.90
1940	61.50	57.60	61.50	59.60	61.30	59.20	61.10	61.00	59.00	61.00	58.90	61.00	722.70
1941	61.00	55.60	61.50	59.30	61.50	59.20	61.10	61.00	59.00	60.90	59.10	61.10	720.30
1942	61.50	55.60	61.50	59.60	61.50	59.60	61.50	61.50	59.60	61.00	59.00	61.50	723.40
1943	61.50	55.60	61.50	59.40	61.50	59.10	61.00	61.00	58.90	60.90	58.90	55.40	714.70
1944	45.90	35.30	50.20	59.60	61.40	59.20	61.10	61.00	59.00	60.90	59.00	61.30	673.90
1945	61.50	55.60	61.50	59.60	61.50	59.60	61.50	61.30	59.00	60.90	58.90	61.00	721.90
1946	61.50	55.60	61.00	59.60	61.30	59.10	61.00	61.00	58.90	60.90	58.90	60.90	719.70
1947	61.40	55.60	61.50	59.60	61.50	59.30	61.20	61.10	59.00	60.90	58.90	61.50	721.50
1948	61.50	57.60	61.50	59.40	61.30	59.20	61.10	61.00	59.00	60.90	59.10	60.90	722.50
1949	58.50	55.60	61.10	59.60	61.20	59.10	61.00	60.90	58.90	60.90	37.10	34.60	668.50
1950	34.20	40.50	61.50	59.60	61.50	59.20	61.10	61.00	59.00	60.90	58.90	60.90	678.30
1951	60.90	55.20	61.00	59.60	61.30	59.10	61.00	60.90	58.90	49.60	59.40	61.00	707.90
1952	61.40	57.60	61.50	59.60	61.50	59.60	61.50	61.50	59.60	61.00	59.60	60.90	725.30
1953	61.50	55.60	61.10	59.20	61.40	59.10	61.00	60.90	50.60	37.80	34.30	47.40	649.90
1954	61.50	48.00	50.40	59.20	61.10	46.30	41.90	38.70	35.20	34.90	32.10	32.70	541.70
1955	37.50	55.50	61.50	59.60	61.50	59.60	61.50	61.50	59.60	61.00	59.00	60.90	698.70
1956	61.50	57.60	61.50	59.60	61.50	59.60	61.50	61.50	59.00	60.90	58.90	60.90	724.00
1957	61.50	55.60	61.50	59.60	61.50	59.60	61.50	61.50	59.60	61.50	59.60	61.50	724.50
1958	61.50	55.60	61.50	59.60	61.50	59.60	61.50	61.50	59.60	61.50	59.60	61.50	724.50
1959	61.50	55.60	61.50	59.60	61.30	59.20	61.10	61.10	59.10	61.00	59.00	61.10	721.10
1960	61.00	57.60	61.50	59.60	61.50	59.60	61.50	61.00	59.00	60.90	59.00	61.00	723.20
1961	61.50	55.60	61.50	59.60	61.50	59.00	61.00	61.10	59.00	60.90	59.10	61.40	721.20
1962	61.50	55.60	61.50	59.60	61.50	59.60	61.50	61.50	59.60	61.50	59.60	61.50	724.50
1963	61.50	55.60	61.50	59.60	61.50	59.60	61.50	61.50	59.60	61.50	59.60	61.50	724.50
1964	61.50	57.60	61.50	59.60	61.50	59.60	61.50	61.50	59.60	61.50	59.60	61.50	724.50
1965	61.50	55.60	61.50	59.60	61.50	59.60	61.50	61.50	59.60	61.50	59.60	61.50	724.50
1966	61.50	55.60	61.50	59.60	61.50	59.60	61.50	61.50	59.60	60.90	58.90	60.90	722.60
1967	61.50	55.60	61.50	59.60	61.50	59.60	61.50	61.50	59.60	61.50	59.60	61.50	724.50
1968	61.50	57.60	61.50	59.60	61.50	59.60	61.50	61.50	59.60	61.50	59.60	61.50	724.50
1969	61.50	55.60	61.50	59.60	61.50	59.60	61.50	61.50	59.60	61.50	59.60	61.50	724.50
1970	61.50	55.60	61.50	59.60	61.40	59.20	61.50	61.50	59.60	61.40	59.00	61.50	723.30
1971	61.50	55.60	61.50	59.60	61.50	59.60	61.50	61.50	59.60	61.50	59.60	61.50	724.50
1972	61.50	57.60	61.50	59.60	61.50	59.60	61.50	61.50	59.60	61.50	59.60	61.50	724.50
1973	61.50	55.60	61.50	59.60	61.50	59.60	61.50	61.50	59.60	61.50	59.60	61.50	724.50
1974	61.50	55.60	61.50	59.60	61.50	59.60	61.50	61.50	59.60	61.50	59.60	61.20	724.20
1975	61.50	55.60	61.50	59.60	61.50	59.60	61.50	61.50	59.60	61.50	59.00	61.50	723.90
1976	61.50	57.60	61.50	59.60	61.50	59.60	61.50	61.50	59.60	61.50	59.00	61.00	725.40
1977	61.50	55.60	61.50	59.60	61.50	59.60	61.50	61.50	59.00	61.00	59.40	61.50	723.20
1978	61.50	55.60	61.50	59.60	61.50	59.60	61.50	61.50	59.00	61.00	59.60	61.50	723.40
1979	61.50	55.60	61.50	59.60	61.50	59.60	61.50	61.50	59.60	61.50	59.60	61.50	724.50
1980	61.50	57.60	61.50	59.60	61.50	59.30	61.50	61.50	59.60	61.00	59.00	61.50	725.10
1981	61.50	55.60	61.50	59.60	61.50	59.20	61.10	61.00	59.00	61.00	58.90	61.00	720.90
1982	60.90	55.10	61.10	59.60	61.50	59.30	61.10	61.00	59.00	61.00	59.10	61.50	720.20
1983	61.50	55.60	61.50	59.60	61.50	59.60	61.50	61.50	59.60	61.50	59.60	61.50	724.50
1984	61.50	57.60	61.50	59.60	61.50	59.60	61.50	61.50	59.60	61.50	59.60	61.50	726.50
1985	61.50	55.60	61.50	59.60	61.50	59.60	61.50	61.50	59.60	61.50	59.60	61.50	724.50
1986	61.50	55.60	61.50	59.60	61.50	59.60	61.50	61.50	59.60	61.50	59.60	61.50	724.50
1987	61.50	55.60	61.50	59.60	61.50	59.60	61.50	61.50	59.60	61.50	59.60	61.50	724.50
TOTAL	3655.70	3322.80	3725.40	3633.30	3747.30	3611.60	3708.50	3696.90	3563.20	3625.10	3462.30	3613.60	43365.70
AVERAGE	59.93	54.47	61.07	59.56	61.43	59.21	60.80	60.60	58.41	59.43	56.76	59.24	710.91
MAXIMUM	61.50	57.60	61.50	59.60	61.50	59.60	61.50	61.50	59.60	61.50	59.60	61.50	726.50
MINIMUM	34.20	35.30	50.20	59.20	61.00	46.30	41.90	38.70	35.20	34.90	32.10	32.70	541.70

Table 8-26 Monthly Peak Power of Lower Kihansi Project with Upper Kihansi Project

UNIT: 10<sup>6</sup> kWh

MONTH YEAR	< JAN >	< FEB >	< MAR >	< APR >	< MAY >	< JUN >	< JUL >	< AUG >	< SEP >	< OCT >	< NOV >	< DEC >	< TOTAL >
1927	152.72	152.72	151.74	152.22	151.66	151.49	151.35	151.24	149.07	104.83	99.59	139.47	1708.08
1928	112.63	119.04	152.72	152.69	152.06	151.59	151.43	151.29	151.24	151.22	151.24	151.65	1748.78
1929	141.68	105.73	151.77	152.72	151.63	151.42	151.26	151.15	151.07	144.31	91.17	96.72	1640.62
1930	147.87	114.56	152.72	152.72	152.05	151.76	151.52	151.34	151.21	151.12	151.03	150.94	1778.83
1931	151.36	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	151.34	151.21	151.34	1826.99
1932	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	151.34	151.28	151.26	1828.33
1933	152.72	152.72	152.72	152.72	152.39	151.99	151.73	152.39	151.37	151.24	151.14	151.06	1824.17
1934	152.72	152.72	152.72	152.72	152.46	152.33	151.89	151.69	151.52	151.36	151.22	152.72	1826.05
1935	152.72	152.72	152.72	152.00	151.82	151.60	151.44	151.30	151.20	136.41	116.24	152.72	1772.88
1936	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	151.35	152.72	1831.22
1937	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	151.27	151.16	1829.59
1938	152.72	152.72	151.08	152.28	151.42	151.27	118.45	102.69	97.56	106.85	103.74	98.65	1539.42
1939	151.84	127.68	151.77	152.72	152.66	152.72	152.72	151.50	151.36	151.22	151.15	151.11	1798.43
1940	152.72	152.72	152.72	152.72	152.18	151.79	151.56	151.40	151.26	151.26	151.13	151.42	1822.86
1941	151.44	152.72	152.72	152.11	152.72	151.75	151.54	151.36	151.22	151.14	151.60	151.53	1831.83
1942	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	151.31	151.20	152.72	1829.66
1943	152.72	152.72	152.72	152.18	152.72	151.62	151.42	151.25	151.15	151.06	150.98	137.41	1807.94
1944	113.79	93.63	124.66	152.72	152.47	151.75	151.52	151.34	151.19	151.09	151.27	152.00	1497.43
1945	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.13	151.35	151.20	151.09	151.44	1826.22
1946	152.72	152.72	151.29	152.72	152.08	151.66	151.44	151.27	151.14	151.05	151.06	151.00	1820.14
1947	152.31	152.72	152.72	152.72	152.72	152.12	151.79	151.55	151.37	151.23	151.11	152.72	1825.06
1948	152.72	152.72	152.72	152.35	152.22	151.78	151.56	151.39	151.24	151.14	151.54	151.09	1822.46
1949	145.23	152.72	151.69	152.72	151.83	151.54	151.35	151.20	151.10	151.02	95.05	85.73	1691.17
1950	84.92	111.21	152.72	152.72	152.72	151.81	151.57	151.38	151.30	151.16	151.07	150.99	1713.57
1951	151.05	151.55	151.35	152.72	151.99	151.49	151.35	151.19	151.08	123.11	152.26	151.46	1790.57
1952	152.25	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	151.32	152.72	151.23	1829.24
1953	152.72	152.72	151.64	151.82	152.31	151.43	151.27	151.13	129.81	93.80	87.97	117.71	1644.32
1954	151.80	131.95	125.14	151.76	151.60	118.77	103.95	96.02	90.35	86.65	82.38	81.12	1371.47
1955	93.15	152.41	152.72	152.72	152.72	152.72	152.72	152.72	152.72	151.29	151.27	151.12	1768.25
1956	152.72	152.72	152.72	152.72	152.70	152.72	152.72	152.72	151.38	151.23	151.11	151.13	1826.57
1957	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	1832.59
1958	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	1832.59
1959	152.72	152.72	152.72	152.72	152.15	151.72	151.63	151.56	151.46	151.41	151.40	151.64	1823.82
1960	151.46	152.72	152.72	152.72	152.72	152.72	152.72	151.34	151.17	151.18	151.31	151.36	1824.11
1961	152.72	152.72	152.72	152.72	152.72	151.35	151.43	151.55	151.21	151.18	151.56	152.28	1824.13
1962	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	1832.59
1963	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	1832.59
1964	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	1832.59
1965	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	1832.59
1966	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	151.06	151.04	151.14	1827.68
1967	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	1832.59
1968	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	1832.59
1969	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	1832.59
1970	152.72	152.72	152.72	152.72	152.38	151.90	152.72	152.72	152.72	152.47	151.23	152.72	1829.70
1971	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	1832.59
1972	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	1832.59
1973	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	1832.59
1974	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	151.95	1831.82
1975	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	151.30	152.72	1831.17
1976	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	151.33	151.27	1829.76
1977	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	151.40	151.29	152.30	152.72	1829.43
1978	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	151.41	151.25	152.72	152.72	1829.82
1979	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	1832.59
1980	152.72	152.72	152.72	152.72	152.72	152.10	152.72	152.72	152.72	151.33	151.28	152.72	1829.15
1981	152.72	152.72	152.72	152.72	152.58	151.80	151.55	151.43	151.26	151.28	151.09	151.41	1823.26
1982	151.20	151.47	151.68	152.72	152.72	151.95	151.67	151.44	151.31	151.40	151.53	152.72	1821.80
1983	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	1832.59
1984	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	1832.59
1985	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	1832.59
1986	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	1832.59
1987	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	1832.59
TOTAL	9076.18	9047.71	9249.58	9310.62	9303.28	9256.84	9206.14	9176.84	9133.94	8997.64	8876.11	8969.54	109604.42
AVERAGE	148.79	148.32	151.63	152.63	152.51	151.75	150.92	150.44	149.74	147.50	145.51	147.04	1796.79
MAXIMUM	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	152.72	1832.59
MINIMUM	84.92	93.63	124.66	151.76	151.42	118.77	103.95	96.02	90.35	86.65	82.38	81.12	1371.47









Fig. 8-14 Energy Generation of Lower Kihansi Project without Upper Kihansi Project

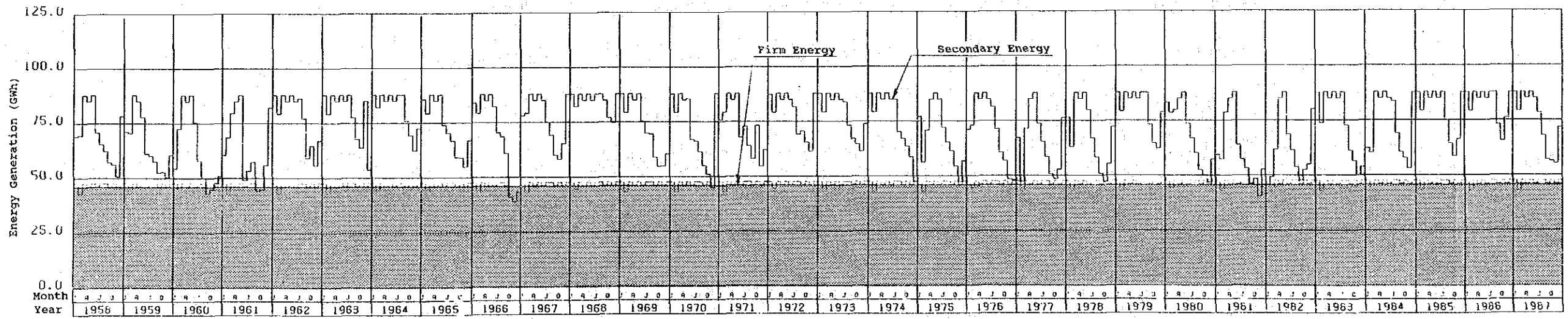
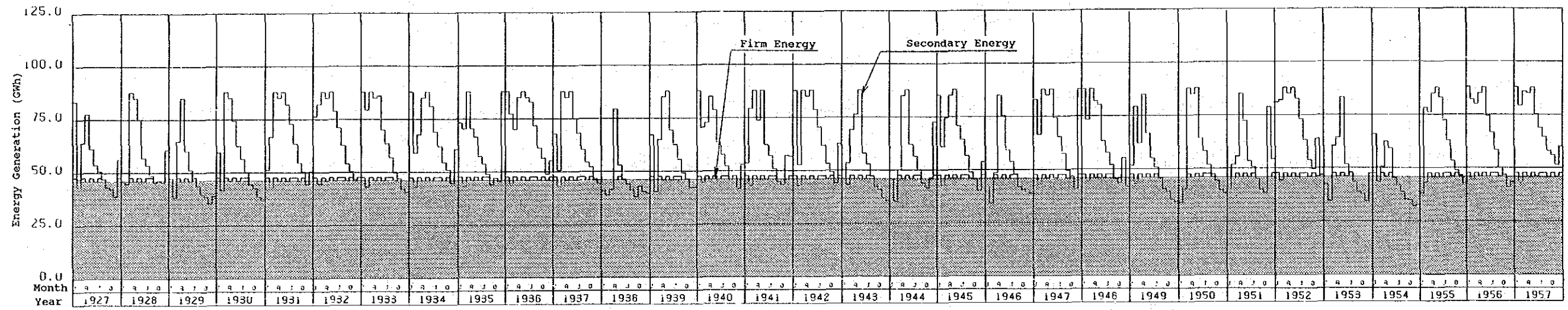
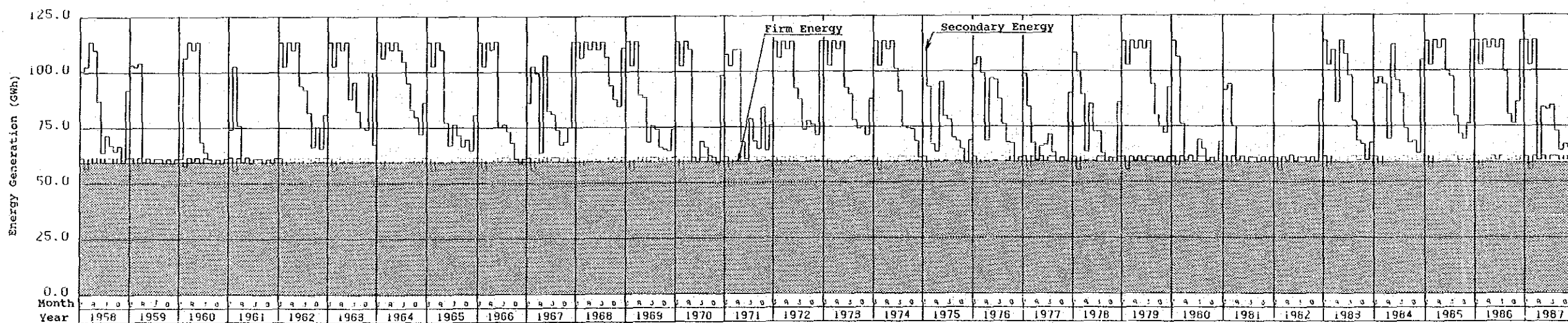
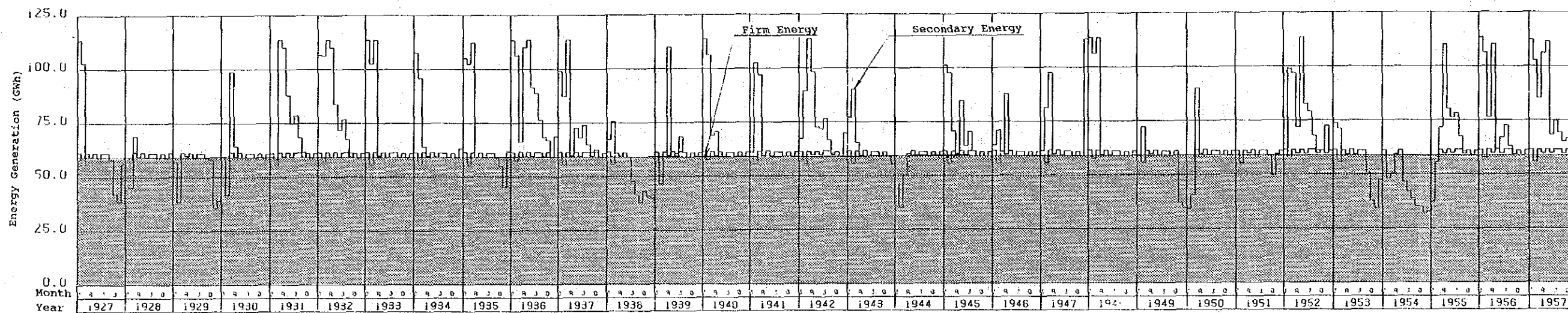




Fig. 8-15 Energy Generation of Lower Kihansi Project with Upper Kihansi Project





**Table 8-28 Preliminary Estimation of Construction Cost of  
Lower Kihansi Project**

Unit ; 10<sup>3</sup>\$

	Lower Kihansi		
	F.C.	L.C.	Total
1. Preparatory Work			
1-1 Access Road	0	19,100	19,100
1-2 Camp Facility & Others	7,700	5,600	13,300
Sub total	7,700	24,700	32,400
2. Compensation	0	2	2
3. Civil Works			
3-1 Diversion & Cofferdam	160	40	200
3-2 Dam & Spillway	7,631	2,169	9,800
3-3 Intake	1,087	313	1,400
3-4 Headrace Tunnel	2,253	747	3,000
3-5 Penstock Tunnel	7,364	2,836	10,200
3-6 Powerhouse & Switchyard	9,880	2,720	12,600
3-7 Tailrace Tunnel	1,203	397	1,600
3-8 Tailrace Outlet	390	110	500
Sub Total	29,968	9,332	39,300
4. Hydraulic Equipment	5,760	1,440	7,200
5. Electro-mechanical Equipment	27,700	8,700	36,400
6. Transmission Line	11,000	7,900	18,900
7. Total Cost (1+2+3+4+5+6)	82,128	52,074	134,202
8. Engineering & Administration 7 x 7.5%	8,042	2,011	10,053
9. Physical Contingency (1+2+3)x15% + (4+5+6)x10%	10,096	6,909	17,005
10. Interest during Construction	24,680	20,360	45,040
11. Grand Total (7+8+9+10)	124,946	81,354	206,300





**Chapter 9 POWER SYSTEM EXPANSION PLAN AND  
POWER SYSTEM ANALYSIS**



Chapter 9

POWER SYSTEM EXPANSION PLAN AND  
POWER SYSTEM ANALYSIS

Contents

	<u>Page</u>
9.1 Power System Expansion Plan . . . . .	9 - 1
9.2 Transmission Line Plan . . . . .	9 - 1
9.2.1 General . . . . .	9 - 1
9.2.2 Receiving Substation . . . . .	9 - 4
9.2.3 Transmission Line Route . . . . .	9 - 4
9.2.4 Transmission Voltage and Number of Transmission Line Circuits . . . . .	9 - 8
9.2.5 Electric Power for Construction Work . . . . .	9 - 11
9.3 Power System Analysis . . . . .	9 - 11
9.3.1 Conditions and Main Results of Power System Analysis . . . . .	9 - 11
9.3.2 Power Flow Calculation . . . . .	9 - 15
9.3.3 Short Circuit Capacity Calculation . . . . .	9 - 17
9.3.4 Stability Calculation . . . . .	9 - 17



### List of Tables

Table 9-1	Transmission System Development Plan
Table 9-2	Economic comparison of Transmission Plans
Table 9-3	Load Forecast by Load Centers
Table 9-4	Short Circuit Capacity

### List of figures

Fig. 9-1	Power Transmission Line Route
Fig. 9-2	Diagram of Power Transmission Lines
Fig. 9-3	1999 Impedance Map
Fig. 9-4	1997 Peak Power Flow (Loop Operation Case)
Fig. 9-5	1997 Peak Power Flow (Separate Operation Case)
Fig. 9-6	1997 Night Power Flow
Fig. 9-7	1999 Peak Power Flow (Double Circuit Case)
Fig. 9-8	1999 Peak Power Flow (Single Circuit Case)
Fig. 9-9	1997 Peak, Kihansi 3LG-0 (Loop Operation Case)
Fig. 9-10	1997 Peak, Kihansi 3LG-0 (Separate Operation Case)
Fig. 9-11	1999 Peak, Kihansi 3LG-0 (Double Circuit Case)
Fig. 9-12	1999 Peak, Kidatu 3LG-0 (Single Circuit Case)
Fig. 9-13	1999 Iringa Bus Voltage at the Fig. 9-11 Case



## Chapter 9. POWER SYSTEM EXPANSION PLAN AND POWER SYSTEM ANALYSIS

### 9.1 Power System Expansion Plan

The power system expansion plan of the ACRES Report is presented in Table 9-1. The construction of an additional 220 kV transmission line from Kidatu Power Station to Ubungo Substation is planned to deal with the increased power flow in this section and to improve the supply reliability to Dar Es Salaam. The construction of a new 220 kV line from Singida to Arusha is designed to deal with the voltage drop and increased power flow of the eastern power system and to improve the supply reliability in this area. It is expected that the Grid System will have sufficient reliability in supplying the power of Kihansi Power Stations to the load centers with high stability.

### 9.2 Transmission Line Plan

#### 9.2.1 General

Kihansi Site is located approximately 480 km to the west of Dar Es Salaam, and the generating capacity is 200 MW composed of the 153 MW power generated by Lower Kihansi Power Station and the 47 MW power generated by Upper Kihansi Power Station. It is not expected that this amount of power is consumed in the vicinity of the power station site, and most of the power will be consumed at Dar Es Salaam and in the Eastern 132 kV power system. In our study, only the transmission line connecting the power station site to Iringa Substation has been examined, and it was assumed that the power from Iringa Substation will be transmitted to the load centers by the Grid System.



The outline of the transmission line plan is as follows.

- a) Receiving Substation: Iringa Substation
- b) Transmission Voltage: 220 kV
- c) Conductor Size : 380 mm<sup>2</sup> ACSR (Bison) single conductor
- d) Number of Transmission Line Circuits: 220 kV double circuit (with Upper Power Station connected to one circuit by a  $\pi$ -branch)
- e) Transmission Line Lengths:
  - From Lower Power Station to Upper Power Station : 8 km
  - From Upper Power Station to Iringa Substation : 105 km

Table 9-1 Transmission System Development Plan

<u>Year</u>	<u>System Additions</u>
1992	Kidatu-Morogoro-Dar Es Salaam (new substation) - 300 km, 220 kV, conductor Tern Dar Es Salaam (new substation)-Ubungo - 10 km, 220 kV, conductor Bluejay (Transformer addition) D.E.S. (new substation) 220/132/33 kV, 90/90/40 MVA
1993	Pangani Falls-Hale - 16 km, 132 kV, conductor Wolf
1995	Singida-Arusha - 300 km, 220 kV, conductor Bison
1996	Lower Kihansi-Iringa* - 113 km, 220 kV, conductor Bison
1999	Upper Kihansi connection* - 0.4 km, 220 kV, conductor Bison
2002	Masigira-Mufindi - 145 km, 220 kV, conductor Bison
2005	Hale-Tanga - 60 km, 132 kV, conductor Wolf Rumakali-Mbeya - 85 km, 220 kV, conductor Bison Mufindi-Iringa-Kidatu - 290 km, 220 kV, conductor Bison Kidatu-Morogoro-D.E.S. (new substation) - 300 km, 220 kV, conductor Bluejay

Note: \* Based on JICA plan

Source: 1) Power Sector Development Plan 1985 to 2010,  
TANESCO/ACRES, 1985  
2) Review of 1985 Power Sector Development Plan,  
TANESCO/ACRES, 1989

### 9.2.2 Receiving Substation

The nearest substation is Iringa Substation which is located in Iringa, about 100 km from Kihansi Site. Iringa Substation is a main substation of the Grid System and it has three entrances of 220 kV transmission lines which come from Kidatu Power Station, Mtera Power Station and western part of Tanzania. It is possible to send the electric power of Kihansi Power Stations stably to the load centers from Iringa Substation by the Grid System.

There is a space in Iringa Substation to construct two entrances from Kihansi Power Stations. As the transmission lines from Kihansi Power Stations will cross over the existing 220 kV transmission line from the western part of Tanzania, just before Iringa Substation, it will be necessary to move the existing switching equipment of Iringa Substation.

### 9.2.3 Transmission Line Route

The following two alternative routes can be considered for the transmission line from Upper Power Station to Iringa Substation (see Fig. 9-1).

Route A: The transmission line runs from Upper Kihansi Power Station to the north along the existing road, and directly goes to Iringa Substation. (The line length from Upper Kihansi Power Station to Iringa Substation is 105 km.)

Route B: The transmission line runs to the west from Upper Kihansi Power Station and is connected to the existing 220 kV transmission line near Mafinga, to deliver power to Iringa Substation.

(The line length from Upper Kihansi Power Station to Mafinga is 80 km.)

Based on the following analyses, we decided to select Route A.

- a) While the transmission line can be constructed along the existing road for Route A, almost one half of the line has to be built along a region far away from existing road if Route B is adopted. In constructing a transmission line, the presence of existing road for transmission of materials and equipment influences the construction cost a great deal. Line maintenance is also easy when there is an existing road along the line.
- b) There are some potential hydroelectric sites to the southwest of Iringa. When these sites are developed, a large amount of power will be transmitted through the transmission line between Iringa and Mufindi. It is desirable to transmit the power of Kihansi Power Stations directly to Iringa Substation belonging to the main power grid in order to avoid concentration of power flow and maintain high reliability of power supply.

The transmission line route from Lower Power Station to Upper Power Station first runs on the left bank of Kihansi River, crosses the river near Upper Power Station to reach Upper Power Station. The connection to Upper Power Station will be a single circuit  $\pi$ -branch, which will be connected on the crossarm of the transmission tower just before Upper Power Station. After Lower Power Station is commissioned and before Upper Power Station is operated, this  $\pi$ -branch will be short-circuited on the transmission tower. The diagram of the transmission line from

Lower Power Station to Iringa Substation is illustrated in Fig. 9-2.

Fig. 9-1 Power Transmission Line Route

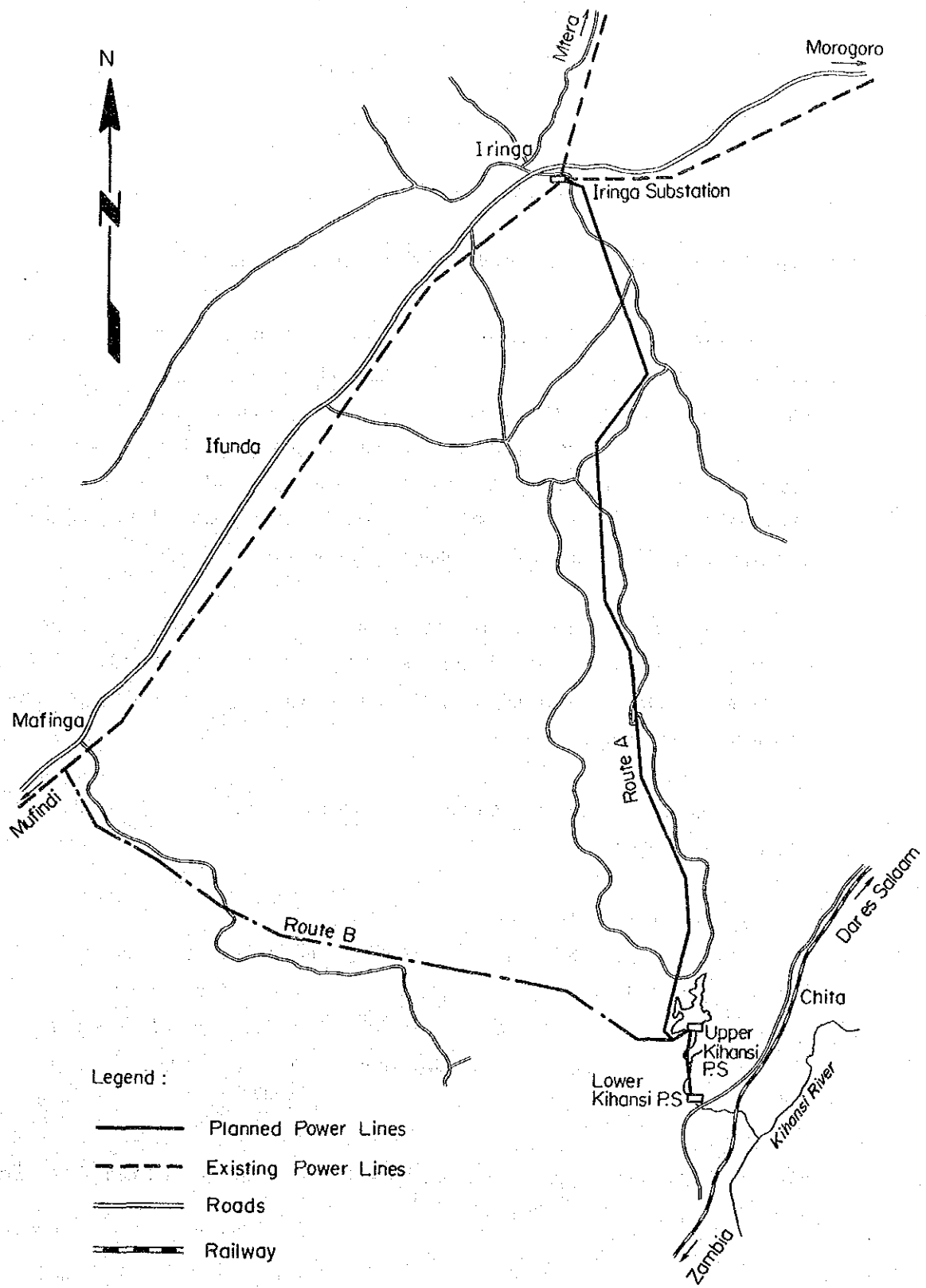
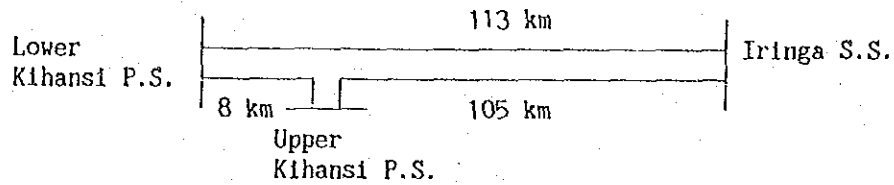


Fig. 9-2 Diagram of Power Transmission Lines



#### 9.2.4 Transmission Voltage and Number of Transmission Line Circuits

It is more economical, and the operation of the system is easier, to select the transmission voltage from the existing voltage classes. In this transmission plan, 132 kV line does not have sufficient capacity, considering the transmission power of 200 MW and the transmission distance of 113 km to Iringa Substation, therefore, the 220 kV voltage class was selected.

For the number of transmission line circuits, single circuit and double circuits can be considered. The economic comparison of single and double circuits cases is given in Table 9-2.

Annual power transmission loss was calculated with the following equation.

$$P_{\text{lossh}} = P_{\text{loss}} \cdot P \cdot H$$

$P_{\text{lossh}}$ : Annual power transmission loss

$P_{\text{loss}}$ : Peak power transmission loss

$P$ : Loss factor,  $P = A \cdot f^2 + (1 - A) \cdot f$

$f$ : Load factor,  $0.2 \leq A \leq 0.3$

$H$ : 24 x 365

The following value was adopted for the calculation in Table 9-2.

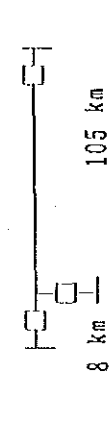
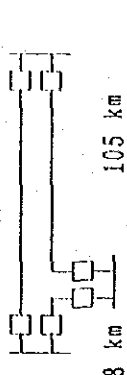
$$f = 0.66$$

$$A = 0.3$$

From Table 9-2, the construction cost of the single circuit transmission line is cheaper than that of the double circuits transmission line. However, as Kihansi Power Stations are going to be the major power source of Tanzania, outage of this transmission line may cause an extensive blackout in the Grid System. Therefore, the double circuit transmission line has been adopted to assure high reliability.



Table 9-2 Economic comparison of Transmission Plans

Transmission Pattern	Case1		Case2	
	Lower Kihansi P. S.	Iringa S. S.	Lower Kihansi P. S.	Iringa S. S.
				
Transmission Line				
Voltage (kV)	220	220	220	220
Length to be constructed (km)	113	105	113	113
Conductor	Bison	Bison	Bison	Bison
Construction Cost (Millions of \$)	10.8	10.8	16.8	16.8
Annual Cost (Millions of \$)	1.23	1.23	1.92	1.92
Station Equipment				
Switch Gear sets				
Lower Kihansi P.S.	1	1	2	2
Upper Kihansi P.S.	1	1	2	2
Iringa S.S.		1		2
Construction Cost (Millions of \$)	2.5	2.5	4.9	4.9
Annual Cost (Millions of \$)	0.29	0.29	0.56	0.56
Transmission Losses				
Peak Power Loss (MW)	5.8	5.8	2.9	2.9
Annual Energy Loss (GWh)	30.0	30.0	15.0	15.0
Annual Cost (Millions of \$)	1.05	1.05	0.53	0.53
Total Annual Cost (Millions of \$)	2.57	2.57	3.01	3.01

Note: 1) Annual Factor: 11.4 %  
 2) Cost for Power Loss and Energy Loss: €3.5/kWh

### 9.2.5 Electric Power for Construction Work

There is not a distribution power line near the proposed site of Kihansi Power Stations. A power line supplying the electric power for the construction work will have to be constructed all the way from Iringa Substation. Excessively advanced investment is necessary to substitute this power line by advancing the construction of the main transmission line, and also, it would not be possible to construct the transmission line in time for the power plant construction. Therefore, it has been decided not to build a power line for construction work, but rather install diesel generator plants to supply the electric power.

## 9.3 Power System Analysis

### 9.3.1 Conditions and Main Results of Power System Analysis

Power system analysis has been done for the Grid System of 1997, the commissioning year of Lower Power Station, and 1999, the commissioning year of Upper Power Station.

It was assumed that the Grid System will be developed based on the plan of the ACRES Report given in Table 9-1 and all the power of the Grid System is supplied by the hydraulic power stations based on the plan of TANESCO. The estimated load of the each substation, based on the demand forecast and the energy consumption by region of the ACRES Report, is given in Table 9-3. The power factor of the load of the each substation was assumed as 0.85.

The following transformers were assumed to be added in accordance with the growth of the demand.

<u>Substations</u>	<u>Voltage (kV)</u>	<u>Capacity (MVA)</u>
Kiyungi	132/33	20
Tanga	132/33	20

The impedance map which was used for the calculation is given in Fig. 9-3.

The main results of the power system analysis are as follows.

- a) The voltage of the Grid System becomes low in the eastern area and high in the western area at peak time. The voltage of the western area becomes higher at off-peak time compared with that of peak time. Therefore, it is necessary to arrange reactive power suppliers suitably. The arrangement of reactive power suppliers should be studied in detail according to the development of the Grid System.
- b) In the case of the fault which causes the trip of the transmission line between Iringa Substation and Kidatu Power Station, Kihansi and Mtera Power Stations cannot keep synchronism with Kidatu Power Station. So it is desirable to make the transmission line between Iringa Substation and Kidatu Power Station double circuits. It is also desirable to make the transmission line between Iringa Substation and Mtera Power Station double circuits for the reliability of power supply of the Grid system.

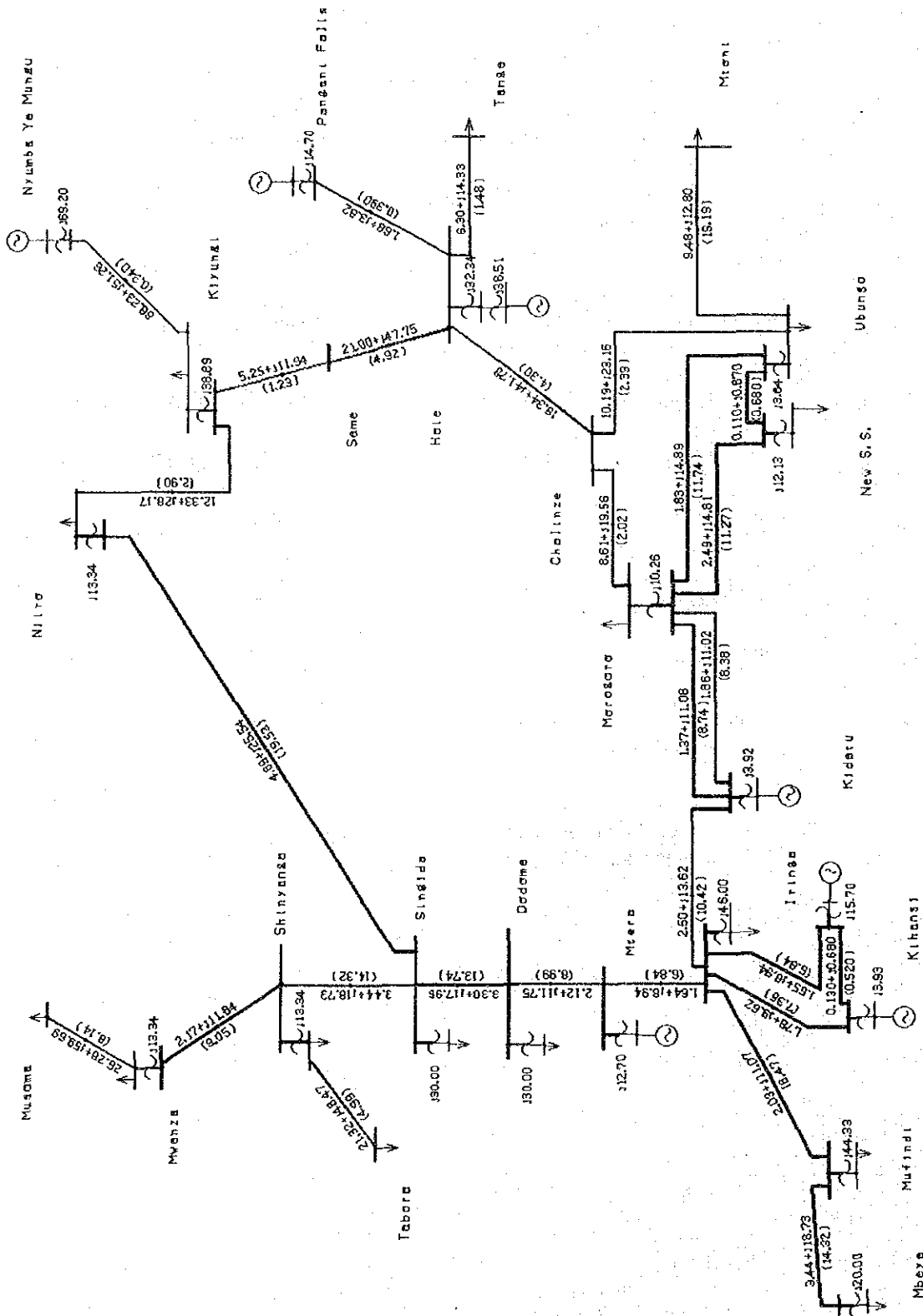
Table 9-3 Load Forecast by Load Centers

<u>Load Centers</u>	<u>Peak Load (MW)</u>	
	<u>1997</u>	<u>1999</u>
Arusha (Njiro)	32.9	37.1
Dar es Salaam (Ubungo+New Substation)	193.1	217.8
Morogoro	28.8	32.5
Moshi (Kiyungi)	25.0	28.3
Tanga	31.2	35.2
Dodoma	8.2	9.2
Iringa	23.1	26.0
Mbeya	17.8	20.1
Musoma	5.5	6.2
Mwanza	24.6	27.8
Shinyanga	20.6	23.2
Singida	1.5	1.7
Tabora	6.1	6.9
Mtoni	18.7	21.1
<u>Total</u>	<u>437.0</u>	<u>493.0</u>
Mufindi	25.0	25.0

Note: Mufindi boiler contractually only uses secondary energy off peak.

Fig. 9-3 1999 Impedance Map

R+X(Y/2) % at 100 MVA Base



### 9.3.2 Power Flow Calculation

The power flow of peak time in 1997, on condition that the Grid System is operated in loop, is given in Fig. 9-4. From Fig. 9-4, it is known that the voltage of the Grid System becomes low in the eastern area and high in the western area. The reason is that the heavy power flow from the power stations located in the central area of Tanzania to the eastern area causes the large voltage drop in the eastern area and, on the contrary, the voltage of the western area is high because of the light power flow of the western power system.

As the measure of this voltage unbalance, it is necessary to connect condensers to the Grid System of the eastern area and reactors to that of the western area. The voltage of the generators of Kihansi Power Stations is needed to be kept high because of the high voltage of the Grid System of the eastern area.

It is desirable for the security of the Grid System to operate the Grid System in loop but loop operation has some difficulty. Therefore, the power flow of the case that the loop of the Grid System is separated between Njiro and Kiyungi, where the power flow of peak time is the lightest in the loop, is studied. The power flow is given in Fig. 9-5. The voltage of the western area of Fig. 9-5 is higher than that of Fig. 9-4.

The power flow of night in 1997, when the voltage of the western area is supposed to become the highest because of light loads, is given in Fig. 9-6.

In addition to the reactive power suppliers in Table 4-2, the following reactive power suppliers are used in calculation to keep the voltage of the Grid System approximately within  $\pm 10\%$  of the rated voltage.

<u>Case</u>	<u>Substations</u>	<u>Reactors</u> (MVA)	<u>Condensers</u> (MVA)
1997 Peak	Ubungo		30
	New S.S.		30
	Mtoni		10
	Kiyungi		5
	Mufindi	10	
1997 Night	Ubungo	40	
	Dodoma	10	
	Singida	20	
	Njiro	10	
1999 Peak	Ubungo		20
	New S.S.		10

Note: The facilities which are duplicated with that of former years are omitted.

From the result of the power flow calculation, the voltage of some buses exceeds  $\pm 10\%$  of the rated voltage. As the voltage which is over  $\pm 10\%$  of the rated voltage exceeds the range of normal operation, the above mentioned reactive power suppliers are not enough for the desirable operation of the Grid System. It is necessary to study the voltage of the Grid System with detailed load distribution in accordance with the development of the Grid System. It is also necessary for voltage regulation to consider the operation of thermal generators located near the main load centers such as Dar Es Salaam.

The power flow of peak time in 1999 was also calculated. The result for the case that the transmission line between Kihansi Power Stations and Iringa Substation is double circuits is given in Fig. 9-7 and the case that this line is single circuit is given in Fig. 9-8.

The voltage drop between Lower Power Station and Iringa Substation becomes 1% larger and the transmission loss of this section becomes double for the single circuit case compared with the double circuits case.

### 9.3.3 Short Circuit Capacity Calculation

The short circuit capacities of each year are given in Table 9-4. The short circuit current is not so large as to exceed the breaking capacity of breakers.

### 9.3.4 Stability Calculation

The stability of the Grid System was studied on condition of the power flow at peak time in 1997. The swing curves of the main generators are given in Fig. 9-9 for the case that the Grid System is in loop operation and in Fig. 9-10 for the case that it is in separated operation. The fault that one circuit of the transmission line between Lower Power Station and Iringa Substation was tripped after a three phase short circuit fault at the point near Lower Power Station was assumed for the calculation. This fault is supposed to have the heaviest influence for the stability of Lower Power Station.

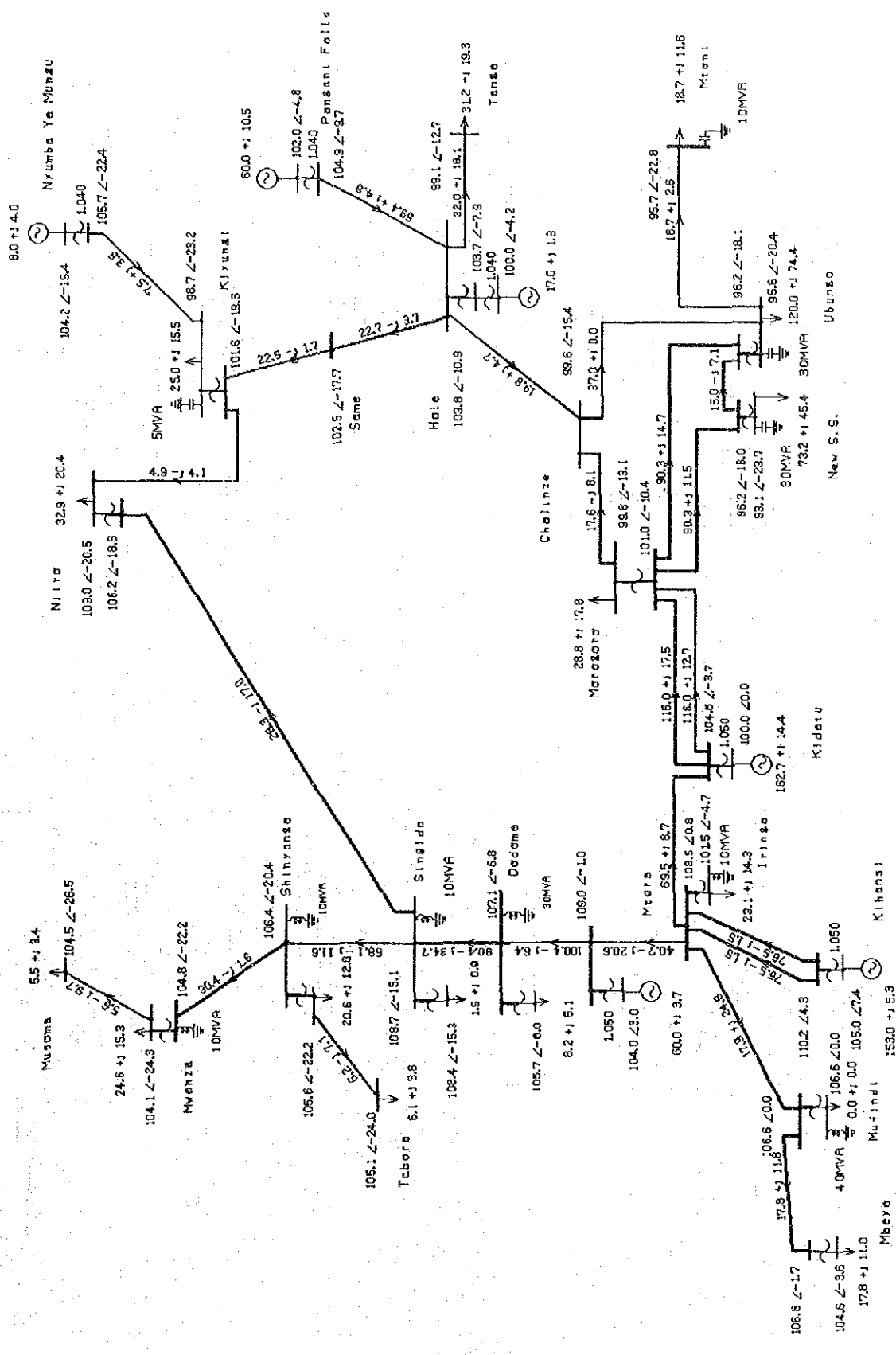
The stability on condition of the power flow at peak time in 1999 was also studied. The swing curves are given in Fig. 9-11 for the case that the transmission line between Kihansi Power Stations and Iringa Substation is double circuits and in Fig. 9-12 for the case that the line is single circuit. The same fault with 1997 case was assumed for the double circuit case and the fault that one circuit of the transmission line between Kidatu Power Station and Morogoro Substation was tripped after a three phase short circuit fault at the point near Kidatu Power



Station was assumed for the calculation of the single circuit case. The bus voltage of Iringa substation at the Fig. 9-11 case is given in Fig. 9-13. Judging from the figures, the power swing of the generators in the Grid System becomes stable within several cycles of the power swing after the fault. However, if the transmission line between Iringa Substation and Kidatu Power Station is tripped with a fault, Kihansi and Mtera Power Stations cannot keep synchronism with Kidatu Power Station. Considering the role of Kihansi and Mtera Power Stations for the power supply of the eastern area, it is desirable to make the transmission line between Iringa Substation and Kidatu Power Station double circuits. It is also desirable to make the transmission line between Iringa Substation and Mtera Power Station double circuits for the improvement of the reliability of power supply of the Grid system.

Fig. 9-4 1997 Peak Power Flow (Loop Operation Case)

P+Q [MW, MVAR] V/B [%/deg]

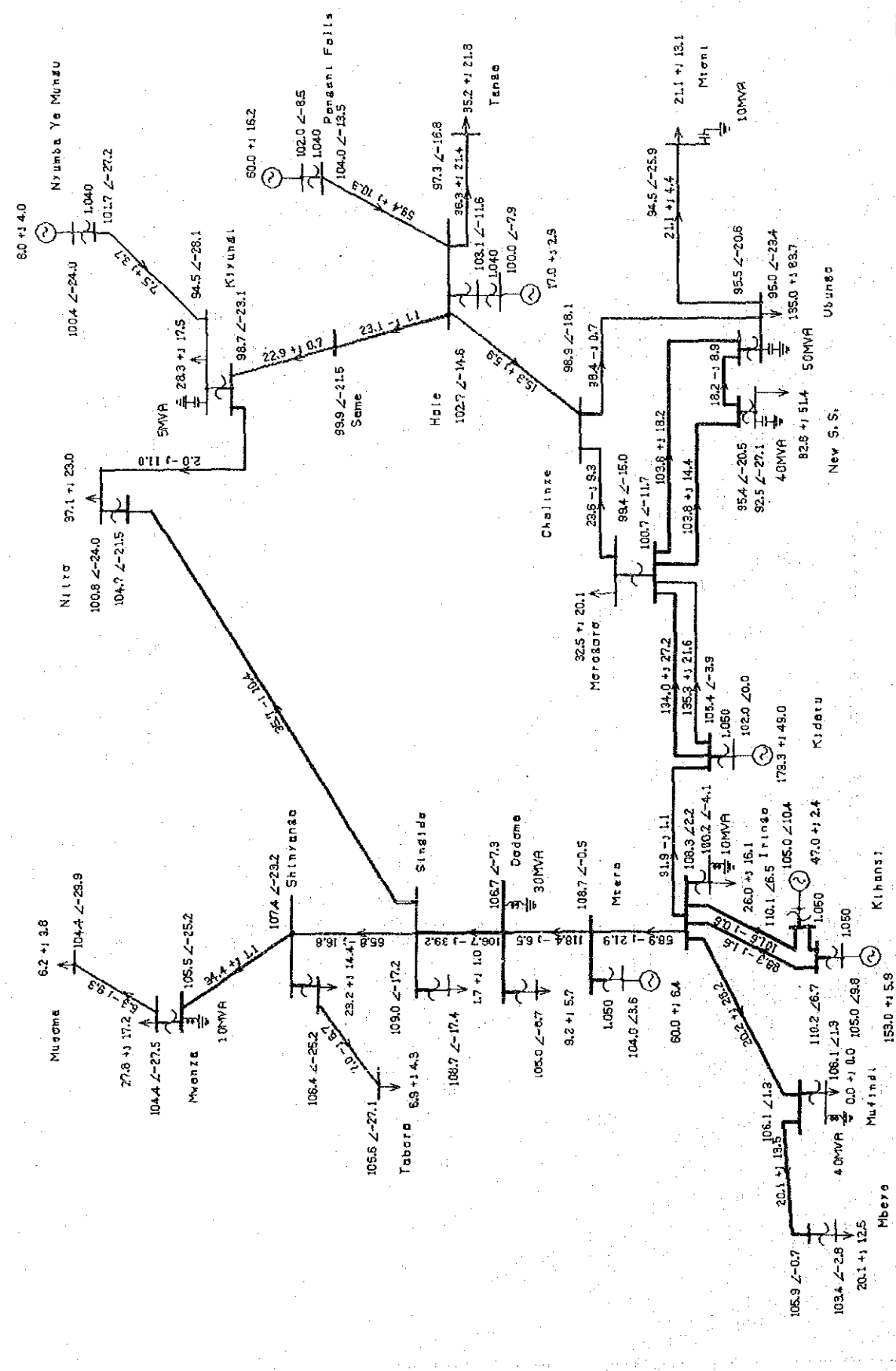






P+JQ [MW, MVar] VZB [%∠deg]

Fig. 9-7 1999 Peak Power Flow (Double Circuit Case)



P+JQ [MW, MVAr] V/Z [%/de8]

Fig. 9-8 1999 Peak Power Flow (Single Circuit Case)

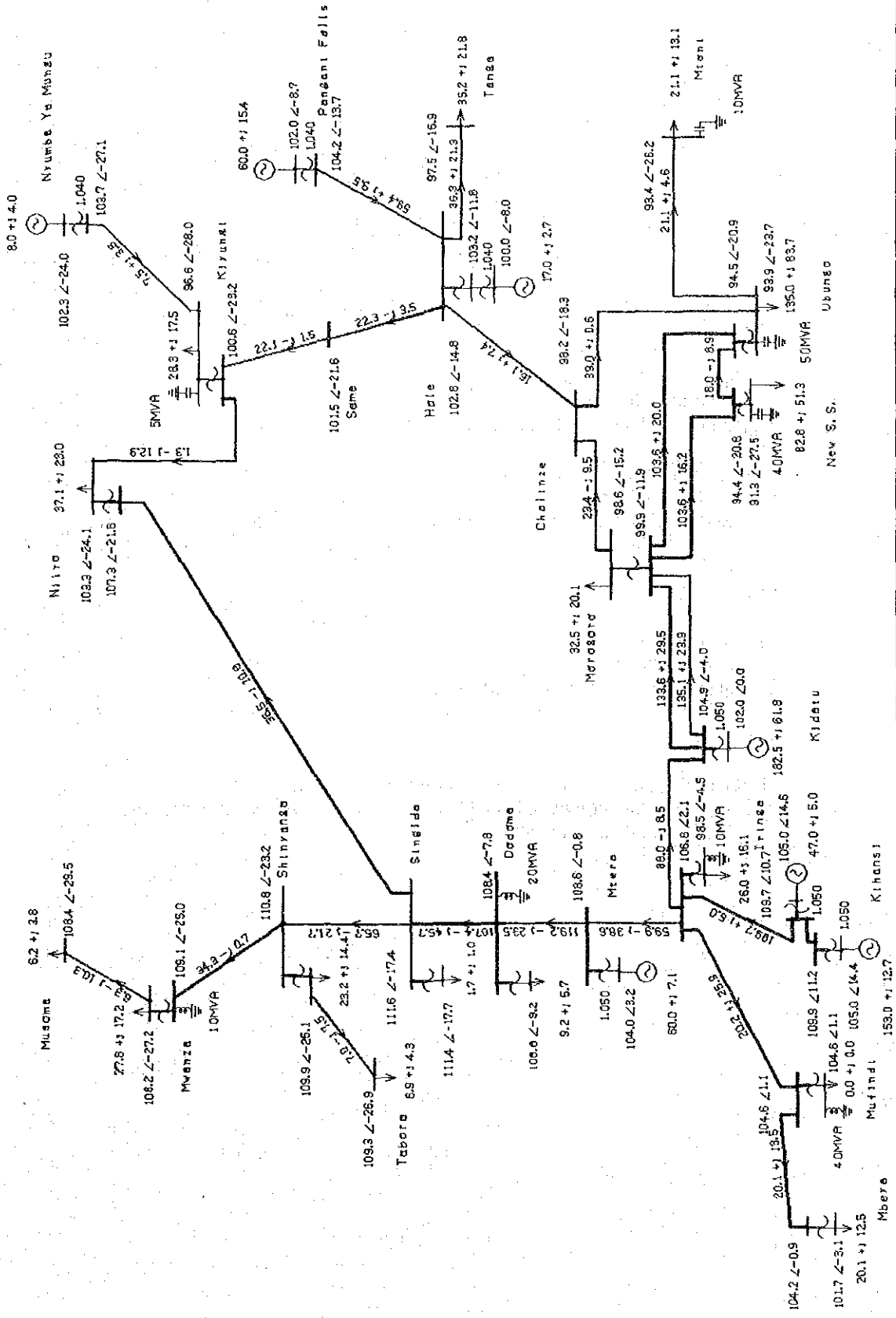


Table 9-4 Short Circuit Capacity

	<u>Short circuit capacity (MVA)</u>	<u>Short circuit current (kA)</u>
<u>1997</u>		
Loop Operation Case		
Iringa Substation	608	1.6
Lower Kihansi Power Station	643	1.7
Separate Operation Case		
Iringa Substation	510	1.4
Lower Kihansi Power Station	563	1.5
<u>1999</u>		
Loop Operation Case		
Iringa Substation	694	1.9
Lower Kihansi Power Station	765	2.1
Upper Kihansi Power Station	751	2.0

Note: 1)  $X_d'$  is used for the calculation  
 2) The short circuit current is the value at the 220 kV buses.

Fig. 9-9 1997 Peak, Kihansi 3LG-0 (Loop Operation Case)

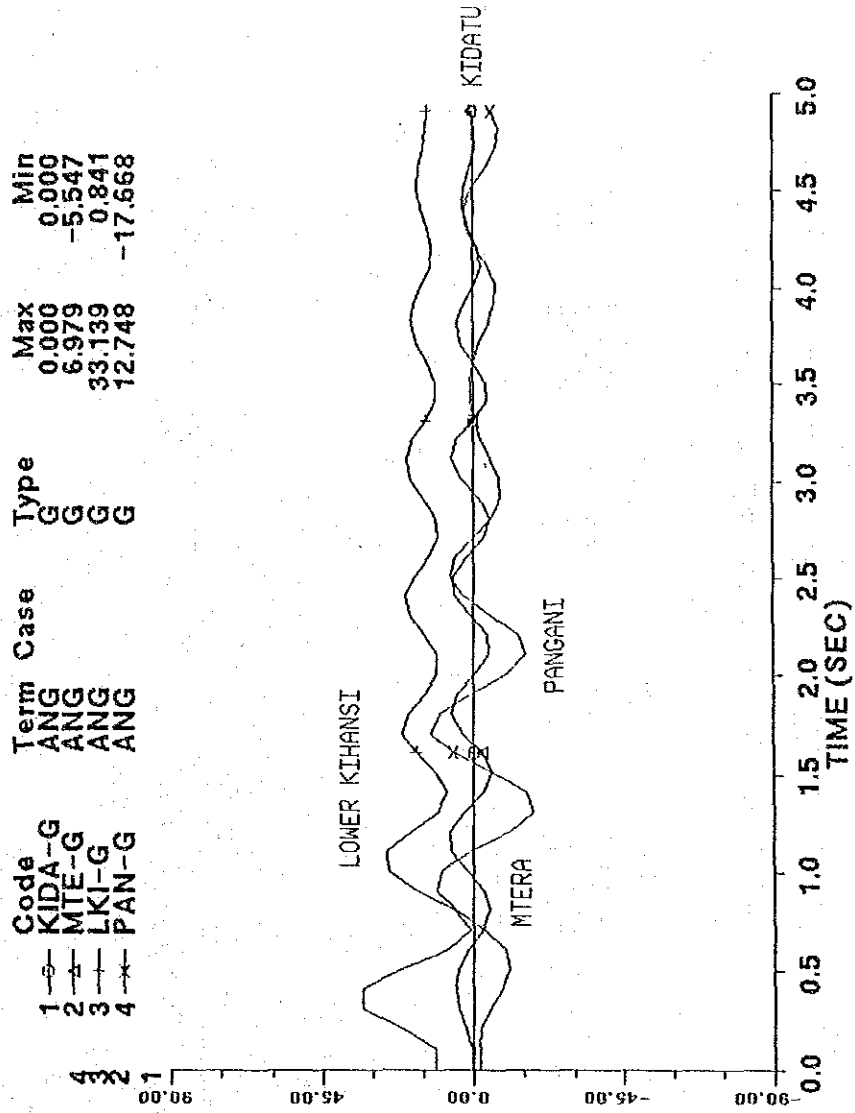




Fig. 9-10 1997 Peak, Kihansi 3LG-0 (Separate Operation Case)

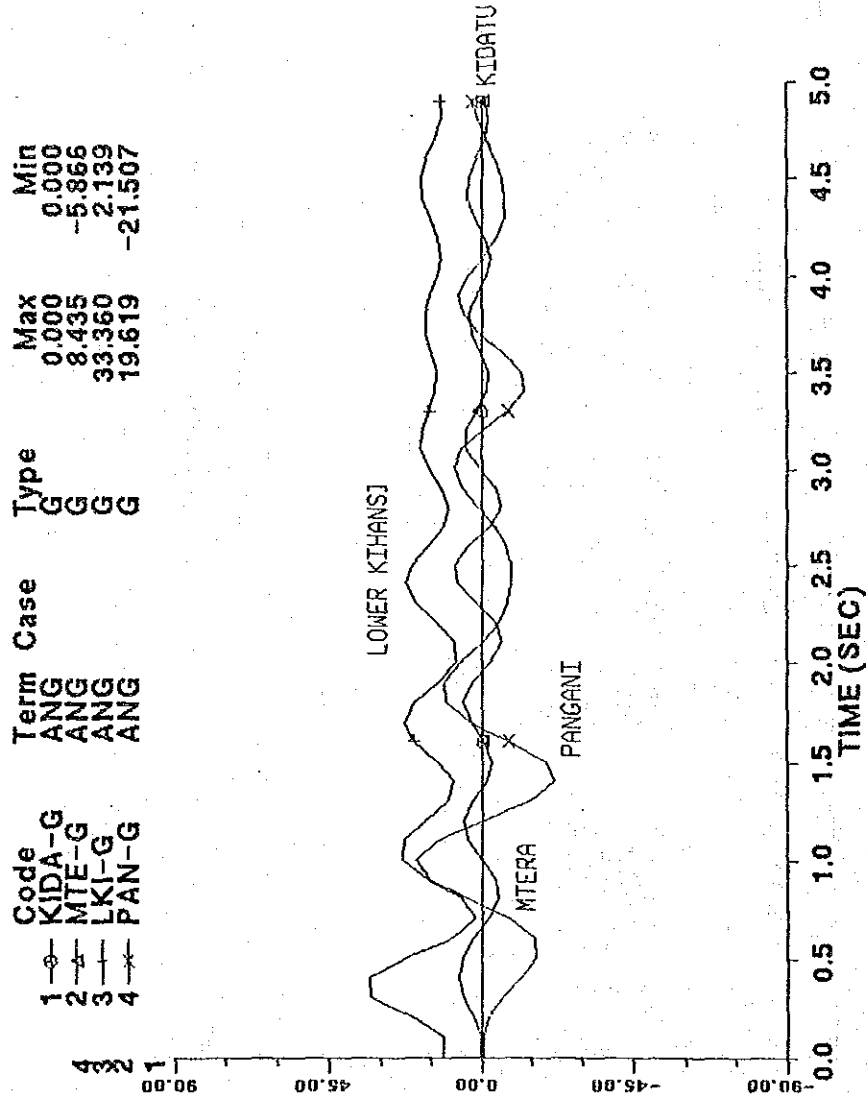


Fig. 9-11 1999 Peak, Kihansi 3LG-0 (Double Circuit Case)

Code	Term	Case	Type	Max	Min
1-○	ANG	ANG	G	0.000	0.000
2-△	ANG	ANG	G	8.243	-4.258
3-+	ANG	ANG	G	38.666	5.058
4-x	ANG	ANG	G	11.725	-25.600

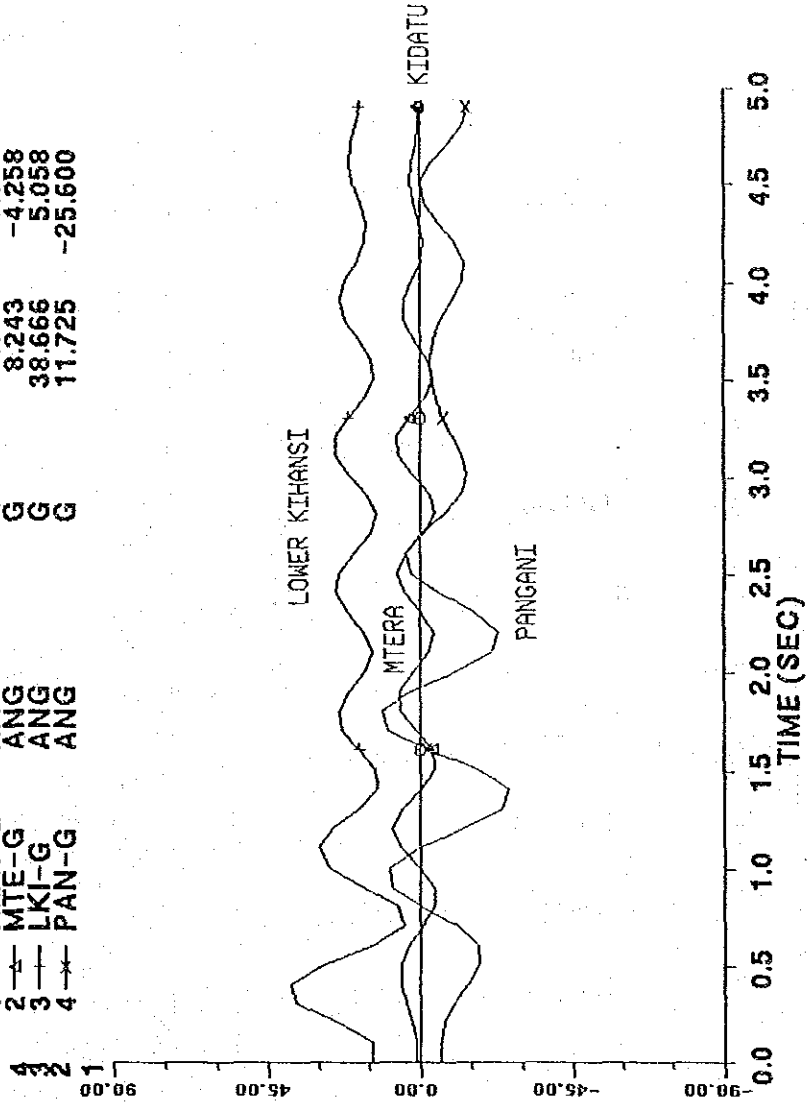


Fig. 9-12 1999 Peak, Kidatu 3LG-0 (Single Circuit Case)

Code	Term	Case	Type	Max	Min
1	KIDA-G	ANG	G	0.000	0.000
2	MTE-G	ANG	G	6.703	-9.797
3	LKI-G	ANG	G	23.470	9.582
4	PAN-G	ANG	G	-2.484	-27.018

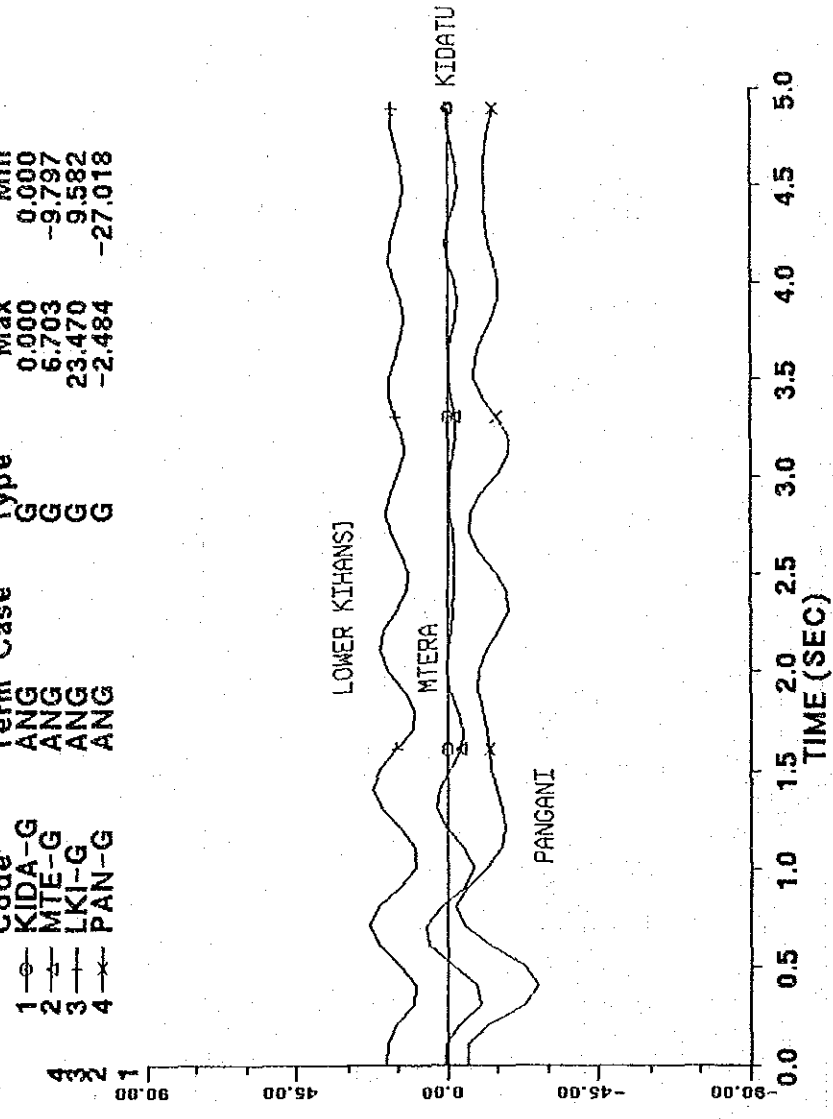


Fig. 9-13 1999 Iringa Bus Voltage at the Fig. 9-11 Case

