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BASIC DESIGN STUDY REPORT ON THE PROJECT FOR BRIDGE CONSTRUCTION IN RURAL REGION IN GEOLOGICAL SURVEY

MAY 1989

JAPAN INTERNATIONAL COOPERATION AGENCY

国際協力事業団

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SUBSURFACE INVESTIGATION REPORT FOR THE BASIC DESIGN STUDY ON THE PROJECT FOR BRIDGE CONSTRUCTION IN RURAL REGION IN NORTHEAST THAILAND

1. INTRODUCTION

This report presents a preliminary subsurface investigation data for foundation design of ten (10) proposed bridges in rural region in Northeast of Thailand as listed in Table 1 under the Japan International Cooperation Agency (JICA). Locations of each bridgesite are shown in Fig.1. Test results in the field and in laboratory are shown in Boring Logs and Summary of Test Results in Appendix B and Appendix C respectively. Recommendations for foundation type of each bridge are given herein the report.

2. INVESTIGATION METHOD

2.1 Boring

Boring of 10 cm diameter were made by three rotary and one motorized drilling machines. The boreholes were drilled by power augering and percussion wash boring depending subsoil condition encountered. Three borings were made on each bridgesite down to hard stratum having SPT N-value of over 50 blows/30 cm.

2.2 Standard Penetration Test (SPT)

The standard penetration test was performed conforming to ASTM D 1586-67 at an interval of 1.00 m. The test was performed by driving a split spoon barrel of 5 cm. outside diameter into the soil by a 63.6 kg drop hammer free falling through a distance of 76 cm. Number of blows were recorded at

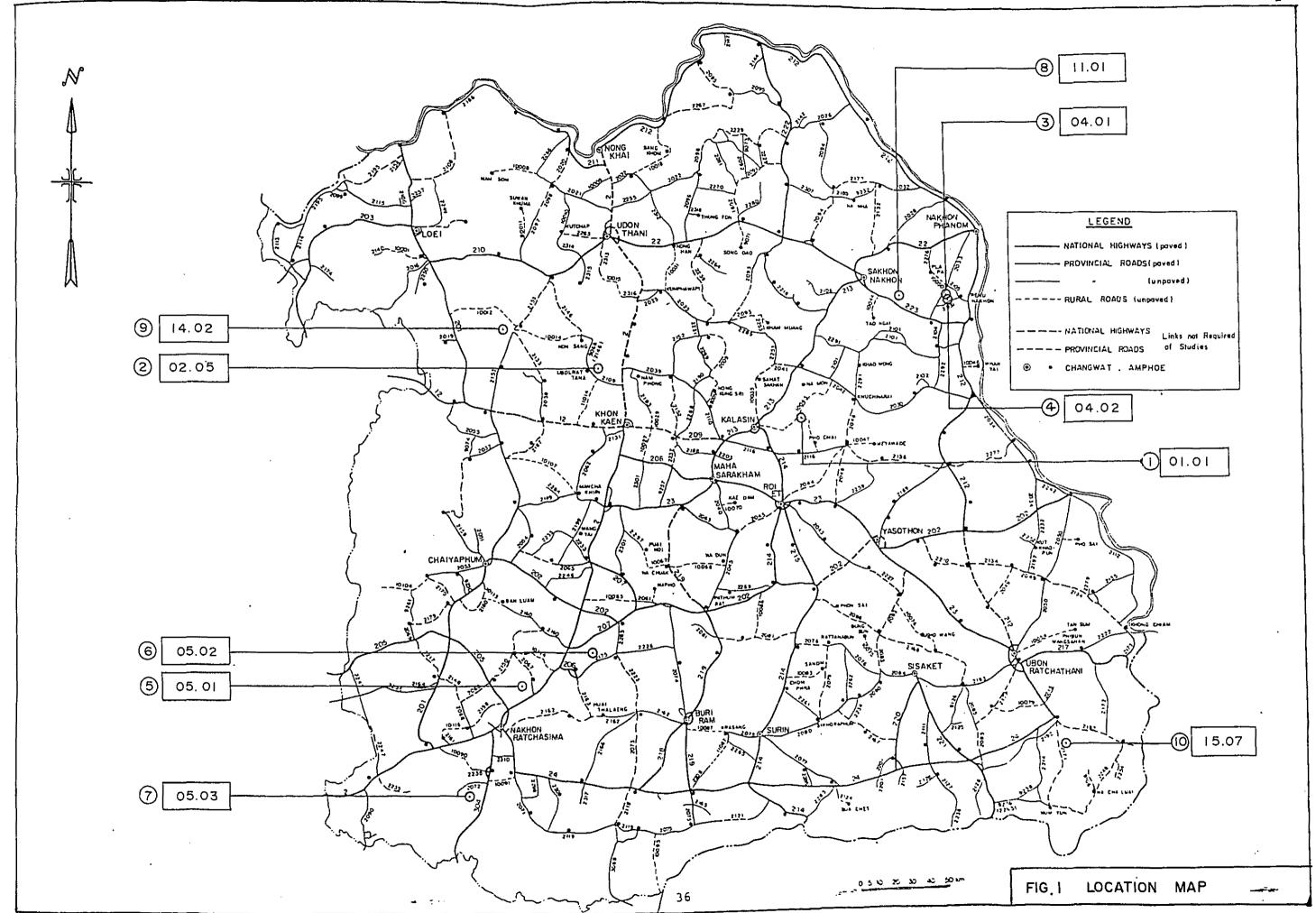


TABLE . I BORING QUANTITY LIST.

חמ	BRIDGE	BRIDGE NAME	LOCATION		BORING	G.D.M.	LABORATORY TESTS									
NO	NO.	DAIDOD MINI	(CHANGWAT)	NO	Depth (m.)	SPT.	Unit Weight	NMC.	LL.	PL.	Siev	GS.				
1.	01.01	HUAI KAE	Ban Kut Khlong- Ban Dan Tae Road	2	11.03 9.05	<u>11</u> 9	<u>3</u> 2	<u>5</u> 4	1_	_1_	3 4	<u>4</u> 2				
			(KALASIN)	3	10,40	10	5	5		_	5	4				
	00.05		Km.6+250	1	15.15	15	J	4			4	4				
2.	02.05	HUAI KHUM MUM	Ban Huai Sai-Ban Kut Chiang Mee Road	2	20,35	20		4		_	4	4				
			(KHON KAEN)	3	20.20	20	1	5	-	_	1	2				
3. 04			Km.0+750	1	10,05	10	_1	4	1	1	2	2				
	04.01	HUAI SOENG NO.1	Rt. No.2031-Ban Bo Dok Son Road	2	4.15	4	1_1_	2	L_	1		1 2				
			(NAKHON PHANOM)	3	10.03	10	2	3	2	2	1	2				
4.	04.02	NIAT COENC NO O	Km.1+150	1	9.07	9	3	3	1	1	2	2				
4.	04.02	HUAI SOENG NO.2	Rt.No.2031-Ban Bo Dok Son Road	2	2,12	2	1	2	_		2	1				
			(NAKHON PHANOM)	3	5.15	5	2	3	1	1	1	2				
5.	0.5		Ban Dan Khon Khob	1	15.15	15	4	15	4	4	3	4				
	05.01	LAM KLANG	(NAKHON RATCHASIMA)	2	13.13	13	6	13	3	3	1	3				
			(Williams Williams IIII)	3	15.18	15	5	15	3	3	4	4				
6.	05.00			1	20,45	20	9	9	1	1	5	5				
	05.02	LAM NAM MUN	Ban Kham Klang	2	27.45	27	11	11	4	4	5	7				
]		<u></u>	(NAKHON RATCHASIMA)	3	20.45	20	9	11	1	1	5	5				
7.	05.03	LAM PHRA PHLOENG	Ban Phla Bung	1	22.03	22	6	2	5_	8	6					
				2	18.05	18	8	9	<u> </u>	<u> </u>	6	4				
		, , , , , , , , , , , , , , , , , , ,	(NAKHON RATCHASIMA)	3	20.22	20	6	20	4	4	7	6				
8.	11 01	TAM NAM WAN	Km.3+200	1	14.05	14	5	5	<u> -</u>	<u> </u>	3	4				
٥.	11.01	LAM NAM KAM	Ban Khok Kong-Ban Phon Road	2	9.03	9	5	5		<u> </u>	3	3				
_			(SAKHON NAKHON)	3	19.05	19	6	8	<u> </u>		3	4				
9.	14.02	LAM NAM PHUAI	Km.5+650	1	11.08	11 :	2	4	3	3	3	3				
٠.	14.02	LAM NAM PHOAT	A.Sibun Ruang-Ban Pa Kha Road	2	6.05	6	1	4	 -	<u> -</u>	4	3				
_			(UDON THANI)	3	10.18	10	4	5	2	2	2	4_				
10	15.07	LAM SOM NO.1	Km.1+225 Ban Nakae(Rt.No.2171)-	1	8.27	8	3	4	<u> </u>		3	4				
			Ban Sao Lao Road	2	/ 1.45	1	1	1		-	1	1				
		<u> </u>	(UBON RATCHATHANI)	3	9.08	9	5	6	-	 -	2	3_				
		TOTAL		30	387.10	382	117	191	37	37	98	103				

REMARKS

SPT. : Standard Penetration Tests.

NMC. : Natural Moisture Contents.

LL. : Liquid Limit
PL. : Plastic Limit
GS. : Specific Gravity

TABLE. 2 WORK SCHEDULE

Bridge	Bridge Name	Location	Bor	ing	*	,		_					FEE	RU	ARY	·					***************************************		1			—	IAR	CH.			989	 3								-		
No.		(Chang Wat)	No.	Depth (m.)	1	6	7 8	9	10	11:\12	2 13	14	15	16 1	7 18	19 ;	20 2	1 22	23	24/2	5 25	27	20	Τ.	1_									<u> </u>				1		丁	丁	
(1)		Ban Kut Khlong-	1	11.03	a															2-12	2 20	151	28	1 2	1 3	4	5	5 7	8	9 1				<u>-</u>				-		-	+	+
01.01	HUAI KAE	Ban Dan Tae Road.	2	9.05	d	-	+	$\dagger \dagger$		_	1			\dashv	+	-		+-	+	-		╂{	-	- -	<u> </u>	╁┩	-	_			╬		+	+		-		- -	\vdash	-+	+	+
		(KALASIN)	3	10.40	a	+		╁╼╂	1	┪	╁	-		╁	+	╅	-	-		┝╼┼╸	-	╂╌╂	_	_			_				-		1	\perp				+	$\left\ \cdot \right\ $	-	+	+
(2)		KM.6+250 Ban Huai Sai-Ban	1	15.15	Ъ		_																	+			_				-					-					$\frac{1}{1}$	_
02.05	HUAI KHUM MUM	Kut Chiang Mee Road	2	20.35	p			1_1				ļ		_			- Annahili				L													T								
(2)		(KHON KAEN) KM.0+750	3	20.20	Ь	_					-							_												-	-			+				+			$\frac{1}{1}$	-
(3) 04.01	HUAI SOENG NO.1	Rt.No.2031-Ban Bo Dok Son Road.	1 2	10.03	a d									_					-											_				-		-						+
		(NAKHON PHANOM) KM.1+150	3	10.03	a			11		_				_	_ _							-																				I
(4)		Rt.No.2031-Ban Bo	1	9.07	a	-		-		+	-			_			-	_				-												_				_				_
04.02	HUAI SOENG NO.2	Dok Son Road.	2	2.12	a	1		-			 			_				_			_			1				_			_	1_		_		<u> </u>					\downarrow	
		(NAKHON PHANOM)	3	5.15	d	_		-	 	}_	_	-		-				_ _	<u> </u>			坩															<u> </u>				\dashv	
(5) 05,01	LAM KLANG	Ban Dan Khon Khob	1 2	15.15 13.13	Ъ					+	-			_			<u> </u>	-	-							-	-	\perp			\perp	-		-	-	-		_			\dashv	+
		(NAKHON RATCHASIMA)	3	15.18	b b														<u> </u>																						<u></u>	_
(6)		Ban Kham Klang	1	20.45	С												_		ļ		_					-								_							_	
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(7)			1	22.03	a					-	-	-					-				-																					
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(9)		KM.5+650 A.Si Bun Ruang-Ban	1	11.08	Ъ																							1														
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1		(UDONTHANI) KM.1+225	3	10.18						-	-	+		+	+		1	<u>-</u>	-							1			<u> </u>	11				_							П	1
(10)		Ban Na Kae(Rt.No.21) Ban Sao Lao Road.	1		С		\dashv	+	$\vdash \vdash$		+	+	\vdash	+	+-		-	+	+-	+	\dashv	+		-+	+	+		_	+	† †	\top		$\dagger \dagger$	+	1	\dagger	+	+	 		H	+
15.07	LAM SOM NO.1	(UBON RATCHATHANI)	2 3	2.00 ° 9.08	C			-		-		1		-	-			+	-		+				+	-		-														
·	TOTAL		30	387.63		* N	OTE		<u> L</u>	!_		.1	1		<u> </u>	<u>. </u> .		1	_,	<u>اليــــــــــــــــــــــــــــــــــــ</u>			· · · · · · ·																			
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APPENDIX A
SOIL PROFILE

- - TABLE 3-

DRILLING EQUIPMENT SPECIFICATIONS

1. Manufacturer's Designation : LD-7

No. of Units :

Make : ACKER DRILL CO., INC. USA.

Capacity : 150 M. with "AW" Rods and Standard Accesories.

Drilling Method : Rotary Drilling, Coring, Wash Boring

2. Manufacturer's Designation : LD-8

No. of Units : 1

Make : ACKER DRILL CO., INC. USA.

Capacity : 150 M. with "AW" Rods and Standard Accesories.

Drilling Method : Rotary Drilling, Coring, Wash Boring

3. Manufacturer's Designation : LD-9

No. of Units : 1

Make : ACKER DRILL CO., INC. USA.

Capacity : 200 M. with "AW" Rods and Standard Accesories.

Drilling Method : Rotary Drilling, Coring, Wash Boring

4. Manufacturer's Designation : M-1

No. of Units : 1

Make : ACKER DRILL CO., INC. USA.

Capacity : 30 M. with "AW" Rods.

Drilling Method : Wash Boring.

Note: :

- Drilling Rods Size : AW

- Sampler Used : 50.0 Cm. O.D. Split Spoon

- Weight of Hammer : 63.6 Kg.

- Casing Size : NW.

every 15 cm. of penetration until either 45 cm. have been penetrated or 50 blows have been applied. The first 15 cm. of penetration is considered to be a seating and the sum of blow required for the second and third 15 cm. of penetration is termed the standard penetration resistance (SPT N-value). Disturbed soil samples from the standard penetration test were kept closely in plastic bags and glass bottles to prevent a loss of moisture content. Soil samples in glass bottles were kept in wooden boxes for each boring and sent to Public Work Department (PWD).

2.3 Groundwater Level Observation

Groundwater level of each boring was observed after the boring was finished about 24 hours or more. The depth of groundwater is referred to the existing ground serface at each boring and given in Boring Logs and in Summary of Test Results. The minus sign indicates that groundwater level is lower than the existing ground surface and the plus sign indicates that the groundwater level is above the existing ground surface.

2.4 Laboratory Tests

Representative soil samples of each layer are selected to be tested as follows.

- Unit weight test
- Natural moisture content test
- Atterberg limits test (Liquid & Plastic Limit)
- Sieve analysis
- Specific gravity test

3. TOPOGRAPHY AND GEOLOGY IN NORTHEAST THAILAND

3.1 Topography

The northeast portion of Thailand is an elevated portion of the country, cover approximately 155,000 sq.km. It is bordered the west and south by marginal escarpments which rise as high on The interior of the region is 900 meters above sea level. structurally divided into two large basins, namely the Sakhon Nakhon and Khorat Basin, by Phu Phan uplifted mountain range. general surface of the region is slightly tilted from the western northern boundaries to the southeast and, except the Phu Phan range, is characterized by a monotonous undulating to nearly flat plain dotted with monadnock, cuesta and swamps. The average of the interior of the region is about 170 meters above level. The term "Plateau" is used for naming this region but technically the term has no meaning relevant to the structure of the region. It was apparently adopted because of the aforementioned western and southern escarpments that bordered the region which makes the region look resemble to plateau.

In general, the region is drained by three main rivers, one for Sakon Nakhon Basin in the north, and the other two for Khorat Basin in the south. For Sakon Nakhon Basin Mae Nam Songkhram and it's tributaries constitute a major drainage system whilst Mae Nam Chi and Mae Nam Mun are responsible for draining of the Khorat basin. Roughly most of the river flows across the region from the west marginal escarpment to the east and/or southeast and enters the Mae Khong River at the border of Thailand.

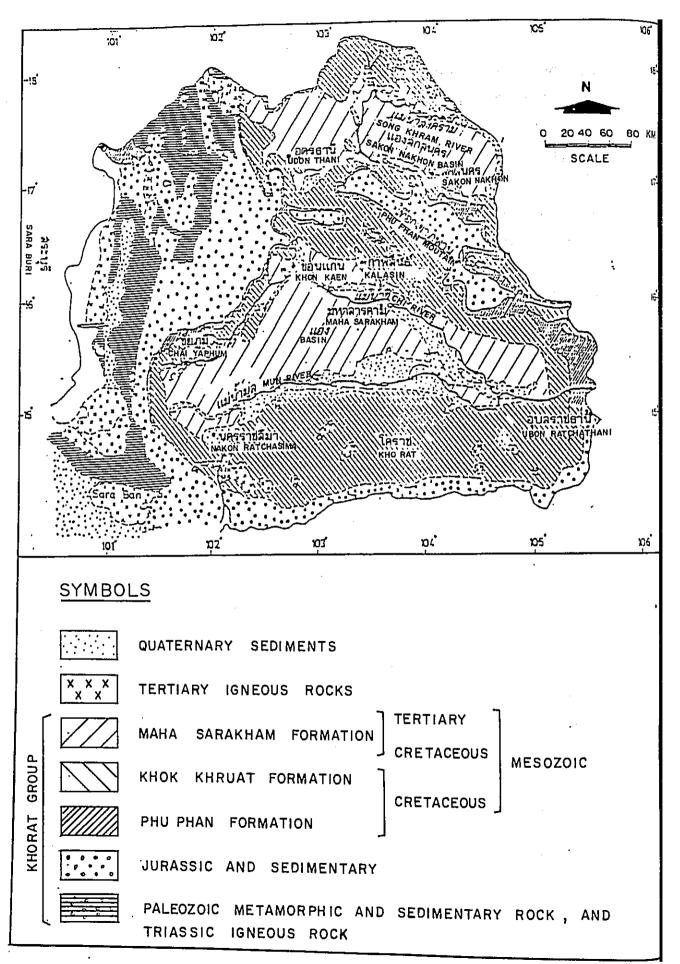


FIG. 2 GEOLOGICAL MAP OF THE NORTHEAST, THAILAND

3.2 Geology

Based on the geological map as shown in Figure 1, the Northeast Thailand lies on the continental Mesozoic sedimentary rocks, the Khorat Group, and the Quaternary deposits. The Khorat Group was uplifted and gently folded in late Tertiary to early Pleistodene time to form the broad syncline and a hill range on the south and the west.

The stratigraphy can be summarized from the older to the younger rock formations as follows:

- (1) <u>Huai Hin Lat Formation</u> This formation contains a basal polymictic conglomerate overlain by the sequence of gray to dark gray sandstone, siltstone, shale and limestone conglomerate.
- (2) Nam Phong Formation This formation consists of soft red to pale red siltstone and interbedded thick resistant beds of brownish red sandstone and conglomerate
- (3) Phu Kradung Formation The formation is characterized by predominantly soft, micaceous, reddish brown and grayish red siltstone; pale red, fine to very fine grained, well cemented calcareous sandstone; and interbedded and micaceous siltstone and sandstone.
- (4) Phra Wihan Formation This formation consists of massive, resistant, white to pink-coloured sandstone and some thin interbedded red siltstone and conglomerate.

- (5) Sao Khua Formation This formation is mainly the less resistant, reddish brown-coloured siltstone lying in between the more resistant, yellowish gray to brown or pale red sandstone.
- (6) Phu Phan Formation This formation is composed of massive beds of light-coloured, coarse to fine grained pebbly sandstone, and interbedded shale, siltstone and conglomerate.
- (7) Khok Kruat Formation This formation contains interbedded moderate consolidated red siltstone, moderately resistant white to red quartz sandstone and caliche conglomerate (buckshot conglomerate). In the upper part of the formation has thin layers and/or crystals of gypsum.
- (8) Maha Sarakham Formation This formation consists of distinguished three layers of rock salt: halite, carnellite and sylvite with subordinate anhydrite and gypsum, and two interbedded units of terrigenous red claystone, shale, siltstone, and fine-grained sandstone.
- (9) Phu Pok Formation This formation was believed to be eolian deposits and comprises very large-scaled cross bedding sandstone and small-scaled wavy bedding sandstone. Sandstone is red-coloured, fine grained, well sorted, and friable. The occurrence of the formation is only in the northern corner of the region.

- (10) Quaternary Deposits The Quaternary deposits are usually both fluviatile and eolian origins. The fluviatile deposit occurs in the vicinity of large rivers and of old river terraces and consists of gravel, sand, silt, and clay. The eolian deposit is generally yellow to red silty sand, loessial soil. Another Quaternary formation is laterite, loose form and continuous duricrust, which ofter occupy the topmost part of terraces and bedrocks.
- (11) <u>Volcalic Rocks</u> The volcanic rocks on the Khorat Plateau are the Tertiary basalts overlying the topmost part of the Khorat Group in the Southern part of the Plateau. The alkali basalt which is Hawaiite type extruded as lava flows and some places with minor eruptions throwing volcanic bomes which are found at Khao Kradung in Buri Ram province. The age of the basalt is in the range 0.92-3.8 million years.

4. SUBSOIL CONDITIONS AND FOUNDATION RECOMMENDATION

Subsoil conditions of each bridgesite are shown in Soil Profile (see Appendix A) and in Boring Logs (see Appendix B). Laboratory test results are summarized in tabular form in Appendix C. Explanation of subsoil conditions and foundation recommendation for preliminary design are described in the following pages.

BRIDGE NO.01.01

HUAI KAE BRIDGE

BAN KUTKLONG - BAN DAN TAE ROAD

A.MUANG, KALASIN

SUBSOIL CONDITIONS

The upper layers of soil are weak to medium strong which can be seen from SPT N-value varing from 3-30 blows/30 cm. These soil layers are loose to medium dense silty fine sand and very stiff fine sandy clay. Very strong layers of hard sandy clay and dense to very dense silty to clayey fine sand having SPT N-value of over 50 blows/ft. are encountered beneath the upper weak to medium strong soil starting from 8.00 m, 5.00 m. and 6.00 m. in BH-1, BH-2 and BH-3 repectively down to the bottom of boreholes.

FOUNDATION RECOMMENDATION

Pile foundation is recommended to be used at this site. Driven concrete with adequate steel reinforcement at tip is recommended to prevent damage of the tip during hard driving in very strong soil layer. Pile tip depth should be at 8.50 m., 5.00 m. and 6.00 m. depth from the existing ground serface in BH-1, BH-2 and BH-3 respectively.

BRIDGE NO. 02.05

HUAI KHUM MUN BRIDGE

KM.6+250 BAN HUAI SAI - BAN KUTCHIANG MEE ROAD

A. UBON RATTANA, KHON KAEN

SUBSOIL CONDITIONS

In BH-1, the subsoil is predominantly sand interbedded by soft fine sandy clay between 1.50-2.50 m. depth. From 0.00-8.00 m. depth the soil is weak and becoming to medium dense clayey fine sand between 8.00-10.00 m. depth. Strong layer of dense to very dense fine sand is encountered from 10.00 m. to the depth beyond the bottom of borehole of 15.15 m. depth.

In BH-2, the subsoil can be divided to 3 layers which are loose to medium dense silty fine sand in the uppermost from 0.00-6.00 m. depth, dense to very dense silty fine sand from 6.00-13.75 m. depth and hard clay from 13.75 m. depth to the depth beyond the bottom of borehole of 20.35 m. depth.

In BH-3, soft to medium and stiff sandy clay and medium dense to dense and very dense sand are encountered layers by layers. Weak soil is encountered between 2.00-4.00 m. depth and medium strong soil is encountered down to 12.00 m. depth. Beneath 12.00 m. depth, the soil is very strong except between 14.70-16.30 m. depth which is medium strong.

FOUNDATION RECOMMENDATION

Pile foundation is recommeded to be used at this site. Driven concrete pile with adequte steel reinforcement at tip is more preferable than steel pile because the major pile capacity is end bearing. The tip of pile is recommended to be at 10.00 m., 6.00 m. and 12.00 m. depth from the existing ground surface at BH-1, BH-2 and BH-3 respectively.

BRIDGE NO. 04.01

HUAI SOENG NO.1 BRIDGE

KM.0+750 RT. NO. 2031 - BAN BO DOK SON ROAD

A. NA KAE, NAKHON PHANOM

SUBSOIL CONDITIONS

Soft to medium clay layer having SPT N-value from 2-17 blows/30 cm. is encountered in the upper portion down to 5.00 m., 3.80 m. and 5.00 m. in BH-1, BH-2 and BH-3 respectively. Beneath this soft to medium clay layer, very strong soil of hard sandygravelly clay (laterite) having SPT N-value of over 50 blows/30 cm. is encountered in every borehole down to the depth beyond the bottom of borehole.

FOUNDATION RECOMMENDATION

Pile foundation is recommended to be used at this site. Driven concrete pile with proper tip reinforcement is recommended because it is end bearing pile. Pile tip depth at 5.00 m., 4.00 m. and 5.00 m. depth from the existing ground surface in BH-1, BH-2 and BH-3 respectively.

BRIDGE NO. 04.02

HUAI SOENG NO. 2 BRIDGE

KM.1+150 RT. NO. 2031-BAN BO DOK SON ROAD

A. NA KAE, NAKHON PHANOM

SUBSOIL CONDITION

Medium to stiff clay having SPT N-value from 5-16 blows/30 cm. is encountered in the upper portion down to 3.80 m., 1.50 m. and 4.50 m. depth in BH-1, BH-2 and BH-3 respectively. Beneath the medium to stiff clay, the soil is very strong strata of very dense laterite having SPT N-value of over 50 blows/ 30 cm. throughout the bottom of borehole.

FOUNDATION RECOMMENDATION

Spread footing is recommended to be used at this site. Depth of the spread footing is recommended at 4.00m., 2.00 m. and 5.00 m. depth from the existing ground surface at BH-1, BH-2 and BH-3 respectively. The allowable bearing capacity of spread footing of 50 t/sq.m. at the recommended depth can be used in design.

BRIDGE NO.05.01

LAM KLANG BRIDGE

BAN DON KHON KHOB

A. NON SOONG, NAKHON RATCHASIMA

SUBSOIL CONDITIONS

Loose to medium dense clayey and silty fine sand and sandy soil are encountered in the uppermost from 0.00-6.50 m. depth in BH-1 and BH-3. Very strong strata of clayey sand, sandy clay and clay with SPT N-value greater than 50 blows/30 cm. are found beneath 9.50 m. and 10.00 m. in BH-1 and BH-3 respectively. SPT N-value in BH-1 tends to increase with depth, but in BH-3 it varies considerably in the upper portion between 0.00-6.50 m. depth then it also increases with depth.

In BH-2, stiff to very stiff and hard fine sandy clay is encountered from 0.00-9.00 m. depth with SPT N-value varying from 13-56 blows/30 cm. Beneath 9 m. depth, the soil is hard clay of SPT N-value greater than 50 blows/30 cm.

FOUNDATION RECOMMENDATION

Spread footing is recommended to be used at this site. Depth of spread footing should be placed at 3.00 m., 2.00 m. and 4.00 m.depth at BH-1, BH-2 and BH-3 respectively. The allowable bearing capacity of 20 t/sq.m. is recommended at the recommended depth.

BRIDGE NO. 05.02

LAM NAM MUN BRIDGE

BAN KHAM KLANG

A. PHIMAI, NAKHON RATCHASIMA

SUBSOIL CONDITIONS

Loose to medium dense sand layers are encountered in the upper portion down to 13.50 m., 13.00 m. and 8.35 m. in BH-1, BH-2 and BH-3 respectively. In BH-1 and BH-2, stiff clay having SPT N-value between 7-12 blows/30 cm. lies beneath the loose to medium dense sand layers down to 17.25 m. in BH-1 and down to 17 m. in BH-2 but it is not encountered in BH-3. The very strong strata of dense to very dense sand and hard clay are encountered at 19.00 m., 17.00m. and 8.35 m.in BH-1, BH-2 and BH-3 down to the depth beyond the bottom of every borehole.

FOUNDATION RECOMMENDATION

Pile foundation is recommended to be used at this site. Either driven concrete or steel pile can be used because it acts as friction - end bearing pile. Pile tip depth is recommended at 8.50 m., 5.00 m.and 8.50 m. depth from the existing ground surface in BH-1, BH-2 and BH-3 respectively.

BRIDGE NO. 05.03

LAM PHRA PHLOENG BRIDGE

BAN PHLA BUNG

A. PAK THONG CHAI, NAKHON RATCHASIMA

SUBSOIL CONDITIONS

Weak soil of soft fine sandy clay and loose clayey fine sand are encountered between 4.00-7.00 m. in BH-1 and between 0.00-2.00 m. depth in BH-2. Generally, the subsoils at this site are sandy clay and clayey sand layers of medium to high and very high SPT N-value. SPT N-values in the most depths are quite constant with depth. Very strong strata of sandy clay, clayey sand and sandstone having SPT N-value greater than 50 blows/30 cm. are encountered at 20.00 m., 18.00 m. and 20.00 m. depth in BH-1, BH-2 and BH-3 respectively.

FOUNDATION RECOMMENDATION

Pile foundation is recommended to be used in this site. Either driven concrete or steel pile can be used because the pile is friction-end bearing pile. The recommended tip depth is at 8.00 m., 7.00 m. and 10.00 m. depth from the existing ground surface at BH-1, BH-2 and BH-3 respectively.

BRIDGE NO. 11.01

LAM NAM KAM BRIDGE

KM.3+200 BAN KHOK KONG - BAN PHON ROAD

A. MUNAG, SAKON NAKHON

SUBSOIL CONDITIONS

Weak to medium strong soil of silty to clayey fine sand and sandy clay are encountered from the existing ground surface down to 11.00 m.depth in BH-1, down to 6.00 m. in BH-2 and down to 8.00 m.in BH-3. Then the soil changes to hard clay having SPT N-value greater than 50 blows/30 cm. starting from 11.00 m., 6.00 m. and 15.50 m. depth down to the depth beyond the bottom of borehole. In BH-3, very stiff to hard sandy clay is encountered between the weak and very strong strata from 8.00-15.00 m. depth but it is not encountered in BH-1 and BH-2.

FOUNDATION RECOMMENDATION

Pile foundation is recommended to be used at this site. Driven concrete pile with proper steel reinforcement at the tip should be preferable than steel pile because it is end bearing pile. The recommended tip depth is at 11.00 m., 6.00 m. and 8.00 m. depth in BH-1, BH-2 and BH-3 respectively.

BRIDGE NO. 14.02

LAM NAM PHUAI BRIDGE

KM.5+650 A. SI BUN RUANG - BAN PA KHA ROAD

A. SI BUN RUANG, UDON THANI

SUBSOIL CONDITIONS

The upper portion soil is weak to medium strong soil of sandy caly and sand down to 8.25 m., 5.00 m. and 7.00 m. depth in BH-1, BH-2 and BH-3 respectively. Beneath these soil strata, hard clay of SPT N-value of over 50 blows/30 cm. is encountered through the bottom of borehole. The soil strata in BH-1 is vary considerably at about 5 m. depth where SPT N-value drops to 1 blows/30 cm. while the nearby depth has SPT N-value of 19-24 blows/30 cm.

FOUNDATION RECOMMENDATION

Pile foundation is recommendation to be used at this site. Driven concrete pile with proper steel reinforcement at the tip is recommended because it is end bearing pile. Pile tip depth at 8.50 m., 5.00 m. and 7.00 m. depth at BH-1, BH-2 and BH-3 is recommended.

BRIDGE NO. 15.07

LAM SOM NO.1 BRIDGE

KM.1+225 BAN NA KAE (RT.NO.2171) - BAN SAO LOA ROAD

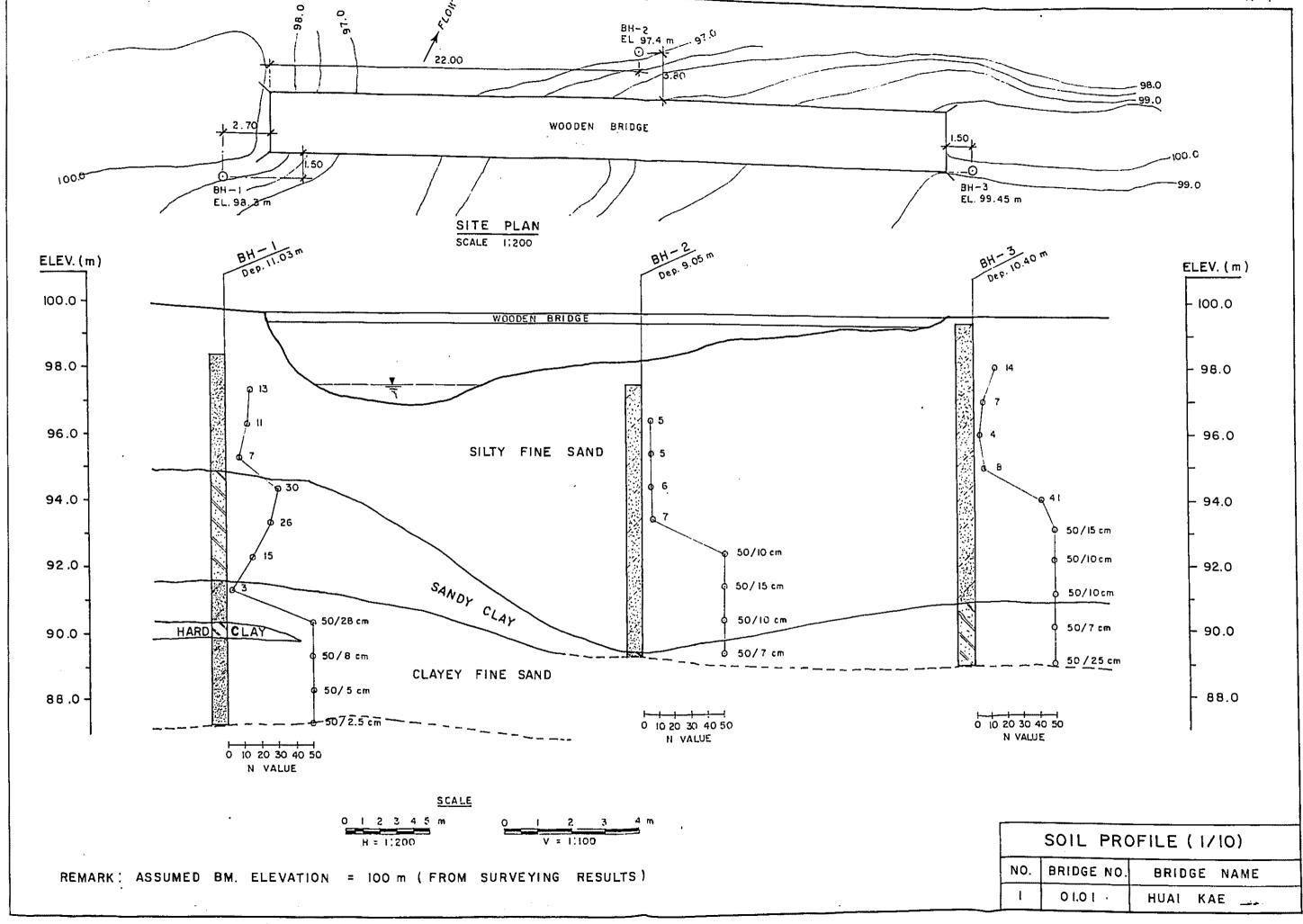
A. DET UDOM, UBON RATCHATHANI

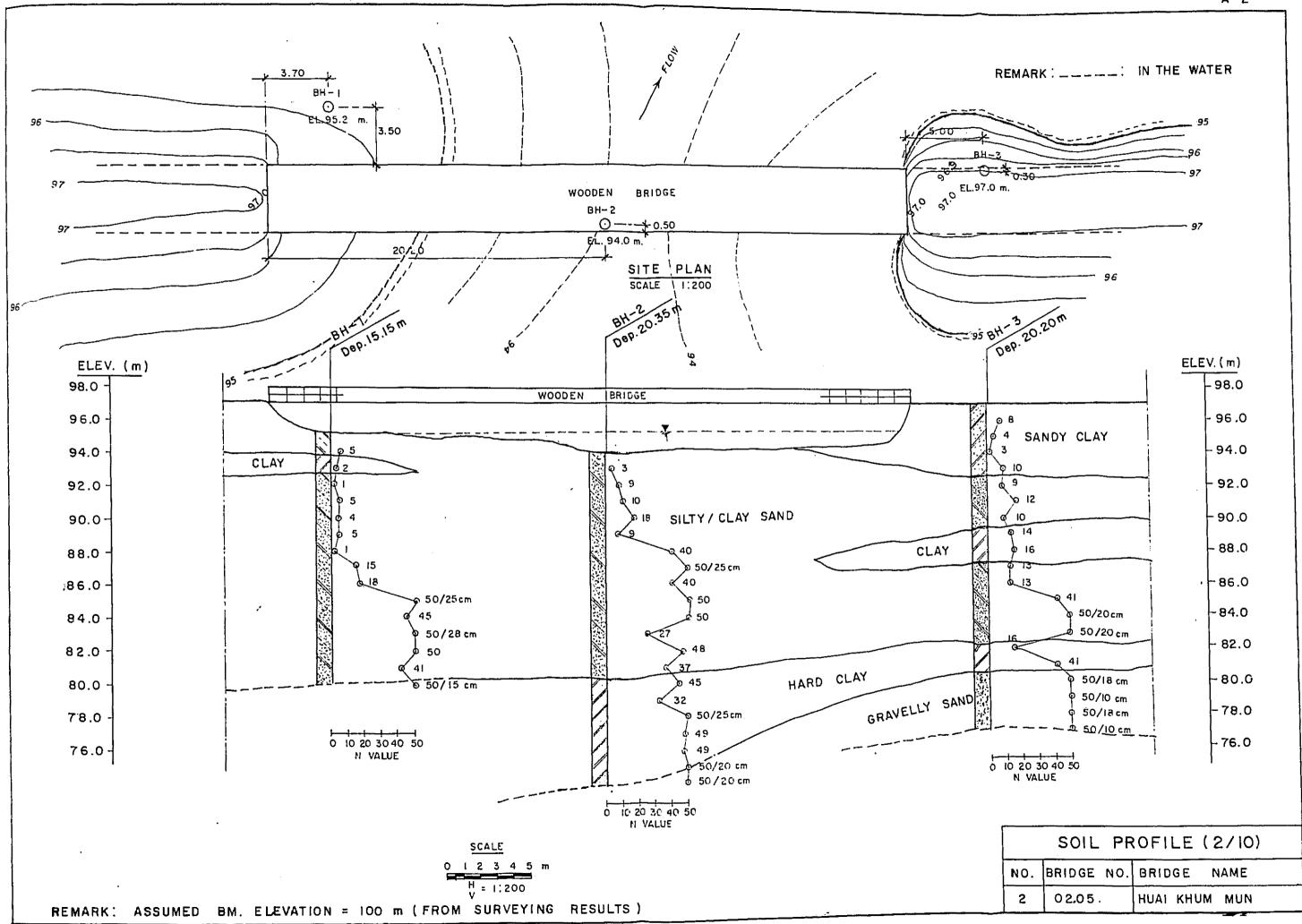
SUBSOIL CONDITIONS

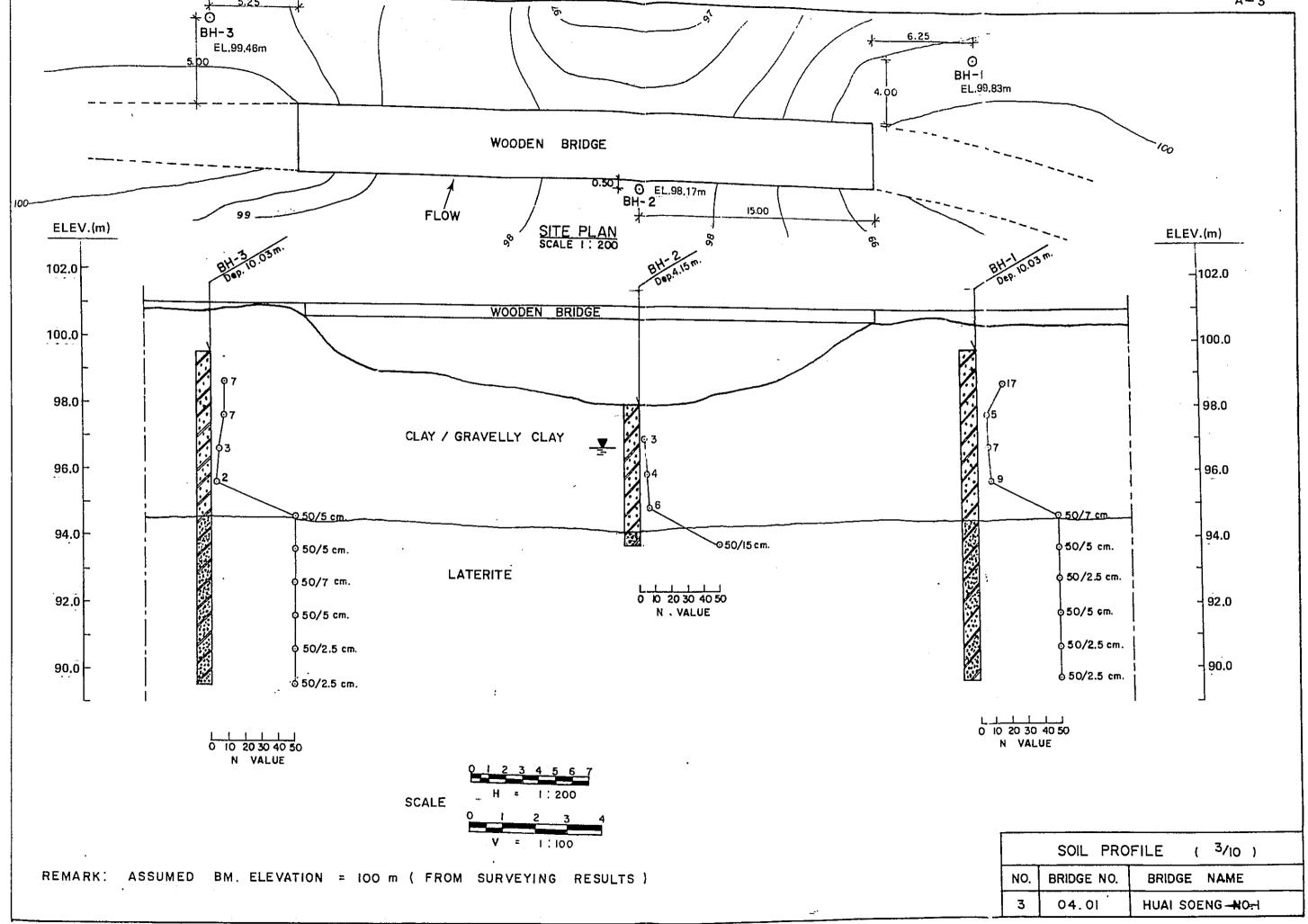
Laterite is encountered about 1 m. thick in BH-1 and BH-3 in the uppermost underlained by weak soil layers of sand and clay down to 7.50 m. and 8.20 m. depth in BH-1 and BH-3 respectively. Very dense siltstone of SPT N-value over 50 blows/30 cm. is encountered at 7.50 m., 1.35 m. and 8.20 m. depth in BH-1, BH-2 and BH-3 respectively.

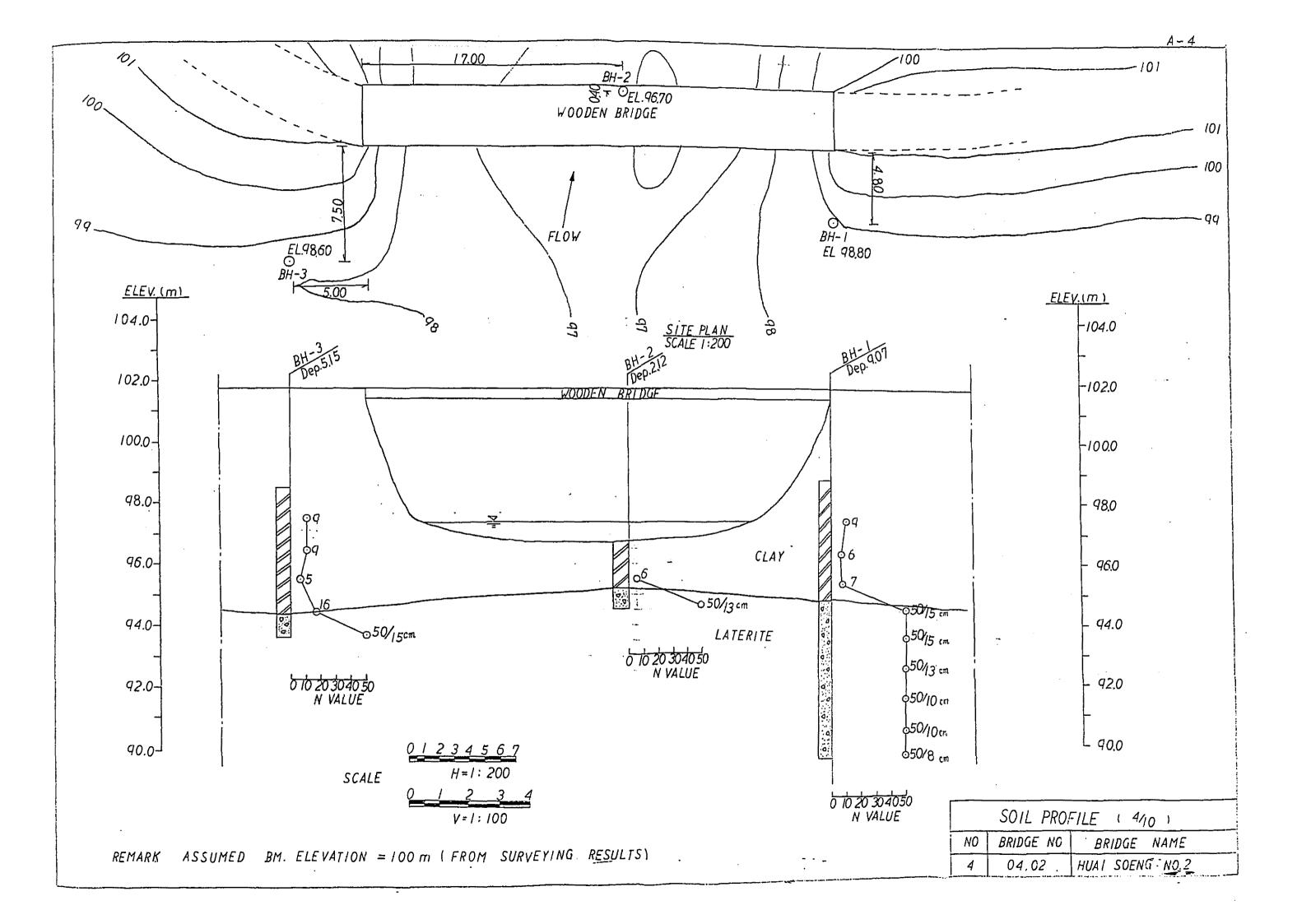
FOUNDATION RECOMMENDATION

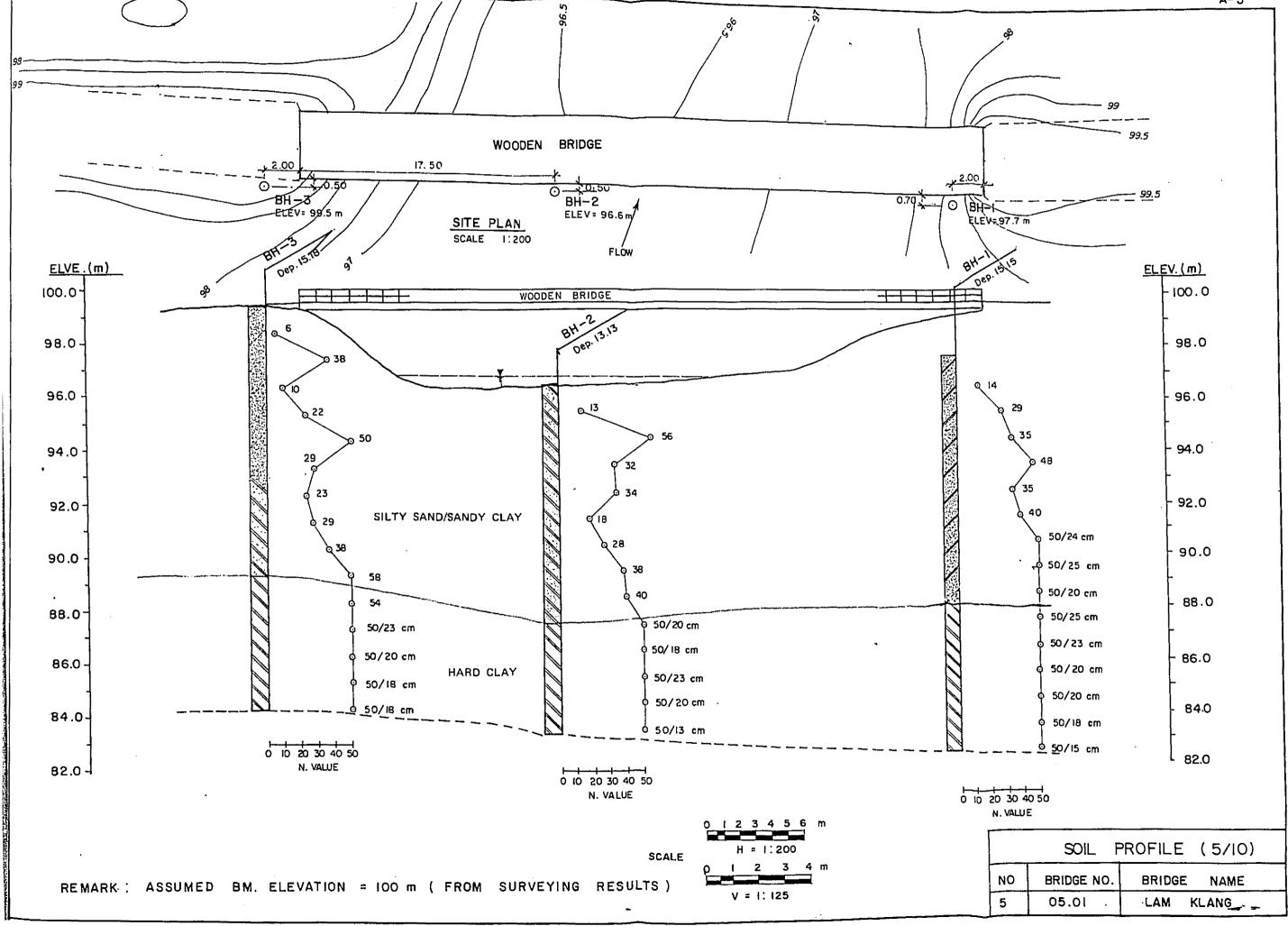
Both pile foundation and spread footing are recommended to be used at this site. For BH-1 and BH-3 pile foundation is to be used, but for BH-2 spread footing is to be used. Pile tip depth at 8.00 m. is recommended for both BH-1 and BH-3. At BH-2, depth of spread footing at 1.35 m. is recommended with the allowable bearing capacity of 50 t/sq.m.

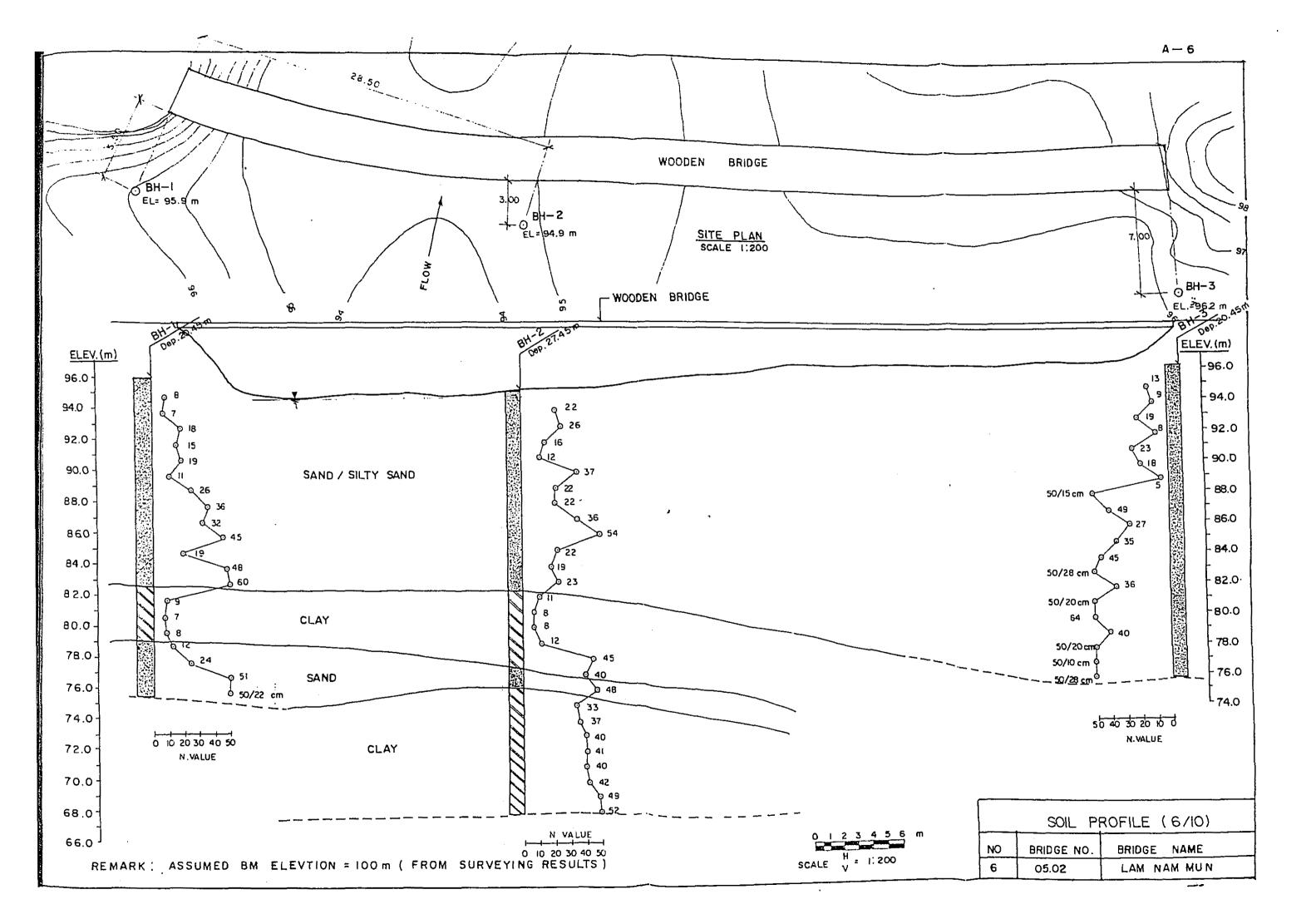


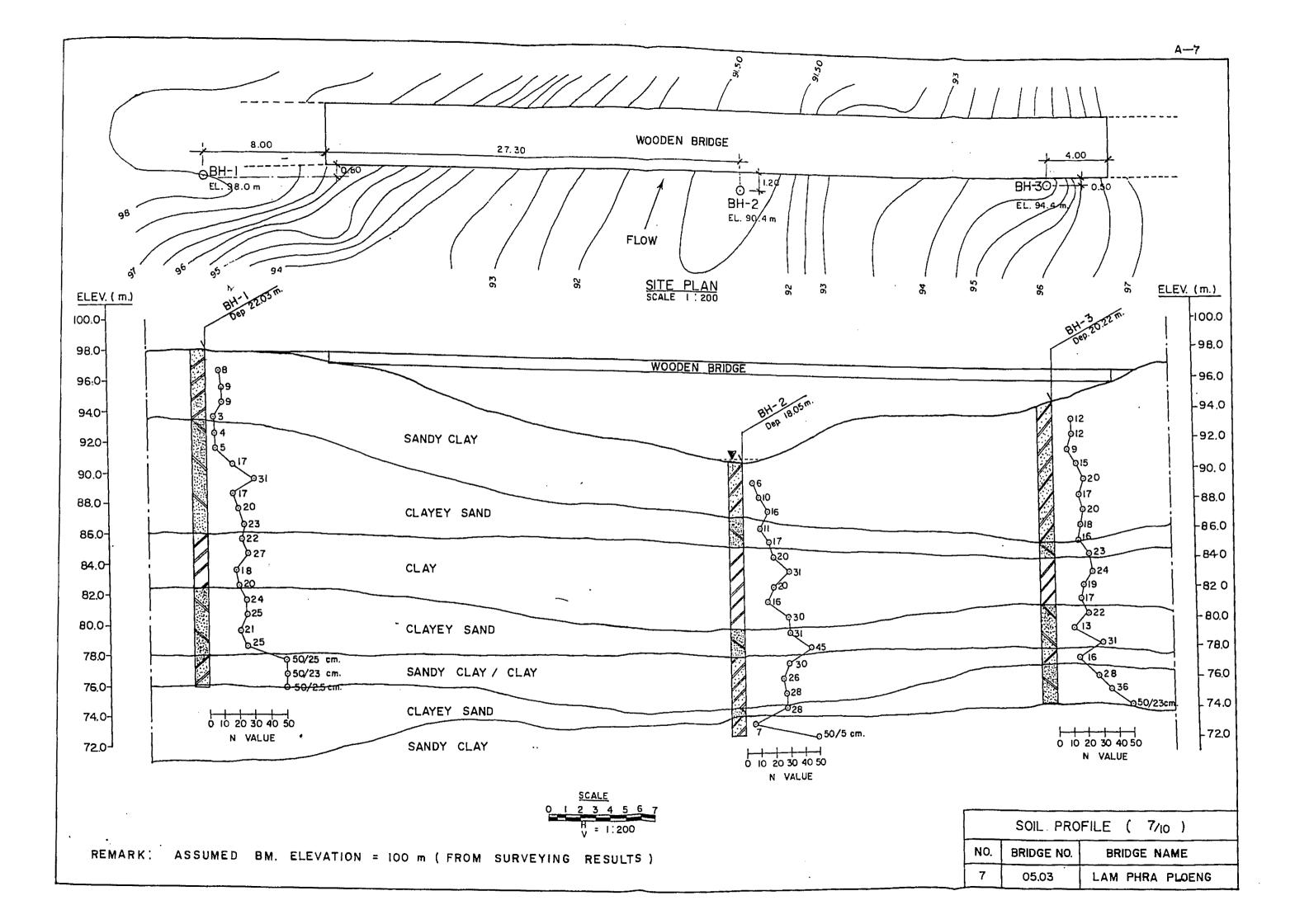


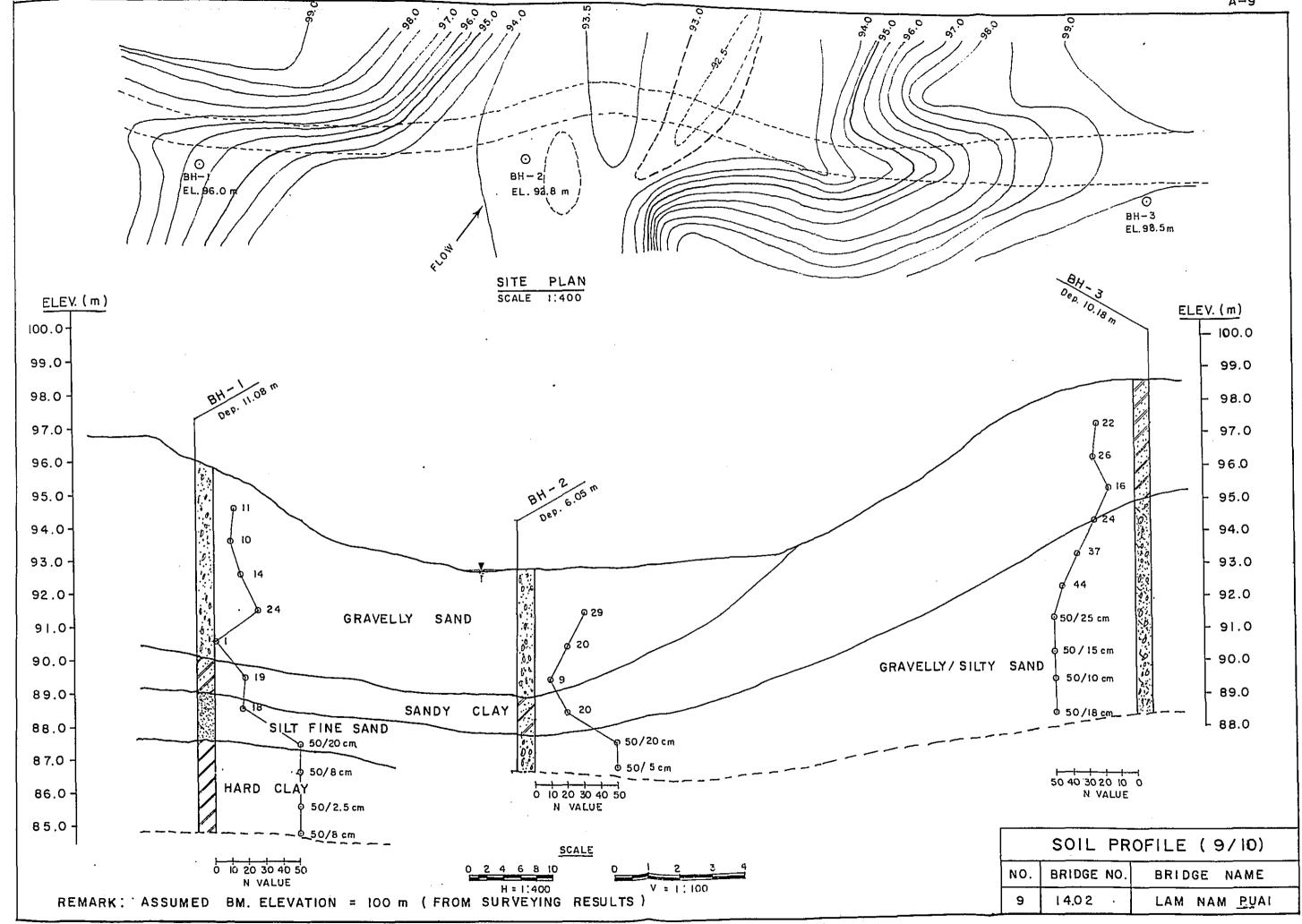


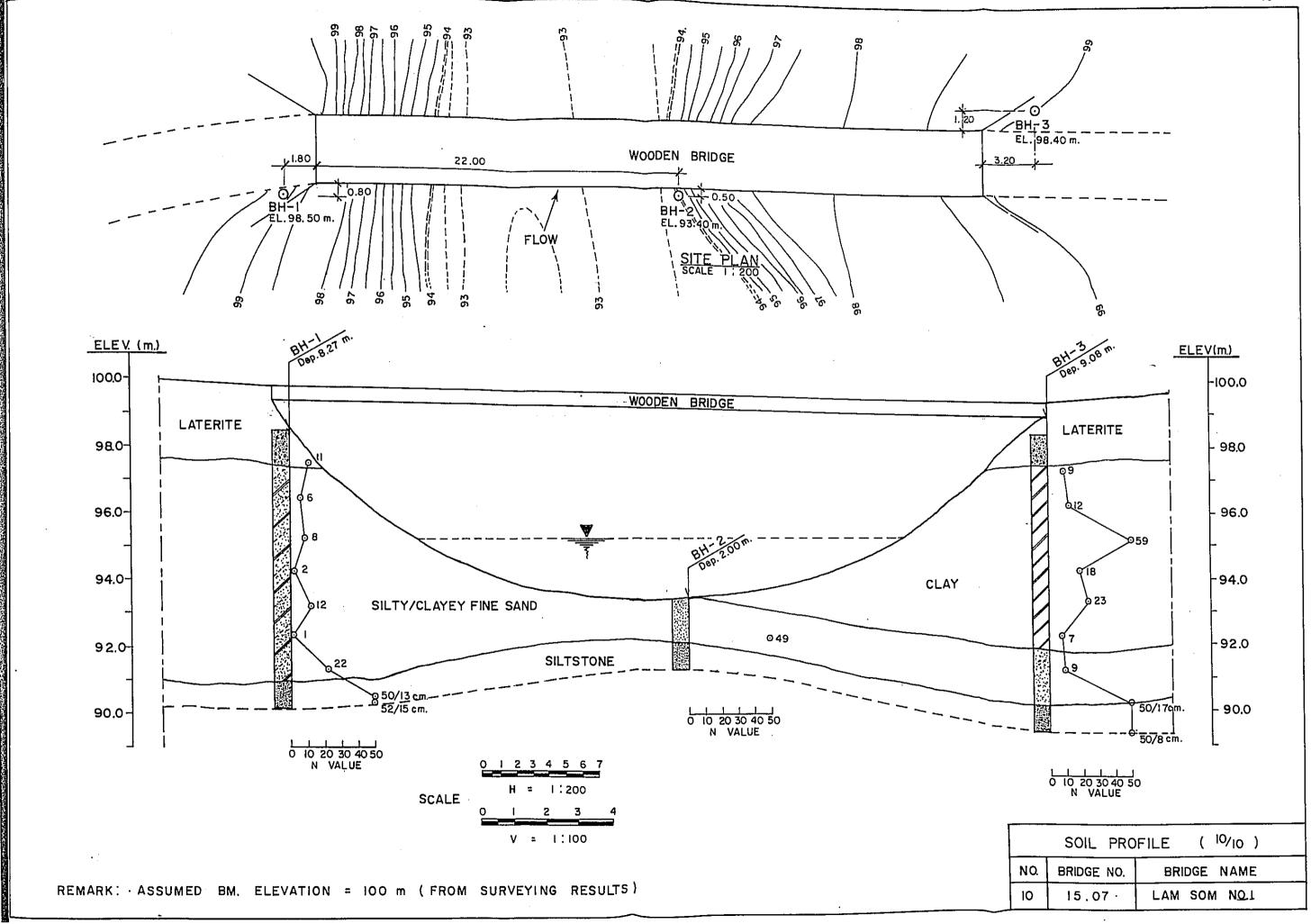












APPENDIX B

BORING LOGS

BORING LOC PROJECT 01.01 HUAI KAE LOCATION A. MUANG, KALASIN	<u>-</u>				O	ORING EPTH OORD.	(m.)	I	1.	03			_	OBS:	ERVI	ED V	VL (m.) 5/	3/8	98. 2.0 39	_	- - -
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SOIL DESCRIPTION	DEPTH (m.)	GRAPHIC LOG	метнор	SAMPLING		S P (blo O 2(T - ws/	N 11)		.	.(₩ _n	LL		0 t	Su (t JCT VT ID	/m². △	2 2 2 2 2 1 1 1 1 1		(1	ፕ _ተ t∕m 1.8	3
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(NO SALTY) 8,00 HAPD FINE SAND CLAY, PSIDDISH BROWN (CL) NO SALTY	8.	77	WO SS WO SS	8		50	78	C X	-		0											
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VERY STIFF SANDY CLAY, DARK GREY (NO SALTY) (CL) 16.30	14 - 15 -		WO SS WO	15		(; à	0,2	0 C 0/5 5 (7,	9)		0												
VERY DENSE CLAYEY- GRAVELLY SAND, GREY (SC,SM)	17 - 18 -		wo	17		5 (3	0/18 4,16	CM 2.5	CM)														
(NO SALTY) END OF BORING 20.20	B - 20-		wo ss. wo	19		50	39,	CN/2.	sav														

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VERY STIFF CLAY, DARK SHOWN AND GREY (NO SALTY) (CL) 1.50	1-		PA SS PA	ì		100	17	(8,	9)														_
MEDIUM CLAY, BROWN AND GREY (CL) (NO SALTY)	3-		SS PA SS PA SS	3		5 7 9	(3,4					19		***			- Constant della					0	
5.00 HARD SANDY-GRAVELLY CLAY, (LATERITE), REDDISH BROWN (CL) (NO SALTY)	5- 6- 7-		PA	8		50	75	CM S CI					Approximation of the state of t							Manual Control of the		The state of the s	
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SOFT TO MEDIUM CLAY, GREY AND BROWN (CL) (NO SALTY) 3.80	2-		WO SS WO SS	3	o o o	÷ 6/	2,2			 - -	1	*	:									0
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HARD SANDY-GRAVELLY CLAY (LATERITE), REDDISH BROWN (CL) (NO SALTY)	6 - 7 - 8 -		wo 33 Wo 52 Wo	5 7 7		50	0/5 0/5 0/5 0/5	CM CM	_							Annual Control of the					
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MEDIUM TO STIFF CLAY, BROWN AND GREY (CH) (NO SALTY) 3.80 VERY DENSE CLAYEY-GRAVELLY	2 ⁻ 3 ⁻ 4 ⁻		WO SS WO SS WO	3	6	6	(3)	4)		>		 - /							•		0	
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9 %	ATION A.NAKAE, NAKHON PHAN		, ,											- 0,	TE	-\N S	HED				_	_
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SOIL DESCRIPTION	0E P T H (m.)	GRAPHIC LOG	МЕТНОВ	SAMPLING		51 (bld IO 2	ows/			1-		(%)		{	,	Su () UC ! FV !	T .	⊡ ₹	P V		7 ₁ (†/1 6 1.8	m. ³)	•
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CLAY OR CLAYEY FINE SAND), LI-BROWN AND LI-GREY	. 6 -		PA		L	╀	<u> </u>	\perp			_				<u> </u>	_		Ĺ.					_
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BORING LOC PROJECT 05.01 LAM KLANG LOCATION A.NON SOONG, NAKHON 1		CHAS	IMA		BORIF DEPT COOR	H (m	.)	1:	3,1	.3					E S	/ED	WL TED	(m.)	±0 14/	2/	0(III B9
SOIL DESCRIPTION	DEPTH (m.)	GRAPHIC LOG	METHOD	SAMPLING B RECOVERY	(t	SPT	ft)		ļ		(%)		i	Œ X	Su (Γ	Δ P. □ T'	P .		7 ₁ (1/	
STIFF FINE SANDY CLAY, LI-GREY (CL)	1-		PA SS		0	13 (1	,8)			9						Í					0
(NO SALTY) 2.00	2-		wo ss wo			26,3		_	0	0		1						~			
VERY STIFF TO HARD FINE SANI CLAY, LI-BROWN AND LI-GREY (CL)	4- 5-		wo ss wo	4		, (B) 7,17)	-			0											
(NO SALTY)	6-		SS WO SS WO	6		Q18	28 (13			#							A TOTAL OF THE PARTY OF THE PAR				<i>G</i>
9.00	8-		SS WO SS WO	8		(15,20	\			© /	þ										
HARD CLAY, REDDISH BROWN (CL)	9- 10-		SS WO SS	9	50	50/2 33,1 7/80	7/5(M	-(†								•			
(NO SALTY)	11 -		WO SS WO SS		(a	50/	23CI /80	и . ⁽ :М))	9								-			
13.13 END OF BORING	13-		Wo SS	13		50/ 30,: 50/1	1			Ţ		-									
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BORING LOC	<u> </u>	********			ВС	RING	NC.)	вн-	-3				GRO	UND	ELI	EV.(n	1.)	9.	5	_
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					CC	ORD.				_				DAT	E S	TART	ED_	12	/2/	89	_
CATION A. NON SOONG, NAKHON	RAT	CHA	SIM	Α	<u> </u>									DAT	E F	NISH	ED _	13	/2/	89	_
SOIL DESCRIPTION	DEPTH (m.)	GRAPHIC LOG	METHOD	SAMPLING		S F (bla	ws /		1	-	(⊕ %}	LL -1	O X	UCT FVT	1 / m	Y PP	1	7. (1/ .6 1.	m ³)	1
COSE TO MEDIUM DENSE AND DENSE SILTY FINE SAND, PROWN AND LI-GREY (SC) (NO SALTY) 6.50 VERY STIFF TO HARD FINE SAND CLAY, LI-BROWN AND LI-GREY (CL) (NO SALTY) 10.00 HARD FINE SANDY CLAY, LI-GREY AND REDDISH BROWN (CL) (NO SALTY) 15.18 END OF BORING	3-		PA	1 3 4 5 6 7 7 8 9 10 11 12 13	0	(13 (15 (2 (2 (50) (32 (50) (40) (40 (50) (40) (40 (50) (40 (50) (40) (40 (50) (40) (40) (40 (50) (40) (40) (40) (40) (40) (40) (40) (4	25 (5, 2) (5, 2) (2) (2) (2) (2) (2) (2) (2) (3) (3) (3) (3) (3) (3) (3) (3) (3) (3	55) 55 (9) 56) 5 (9) 3(10, 29) 3(10,	38 (13) 38 38 38 (M)			7	9 40			15	20		.6 1.	8 2	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
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BORING LOC PROJECT 05.02 LAM NAM MUN LOCATION A. PHIMAI, NAKHON RAY		ASIM	A		DE	RING PTH ORD.	(m.)		3H- 20.	45			 GRO OB:	OUNI SER'	D E VED	LEV. WL	(m.) _ 9) _ 0 8/2).3 2/8	0 9	1 1 1 1
SOIL DESCRIPTION	DEPTH (m.)	GRAPHIC LOG	жЕТНОВ	SAMPLING B RECOVERY	 1	S F (blo () 2(ws /	ft)			- () 20	%	1) }	UC FV	T .	m ² } △ P □ T 5 2	P V			t m ³)	1 1
LOOSE SILTY FINE SAND, YELLOWISH BROWN (SP-SM) (NO SALTY) 3.00 MEDIUM DENSE SILTY FINE	1 - 2 - 3 -		PA SS PA SS	3		7 (4,3		<u>, </u>			0	-								9	
SAND, GREY (SM) (NO SALTY)	4- 5-		w0 ss w0 ss w0 ss	5		व्या		5,10 19 (9;1	0)			9										1
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(SM,SP-SM) (NO SALTY)	10-		wo wo ss wo	<u></u>	-		,23,	45	ام			9	7							0	/	
13.50 STIFF CLAY, LI-GREENISH	12- 13- 14-		SS WO SS WO	13			8,3	2)6	_													
GREY (CH) (NO SALTY) 17.25	15 -		WO SS WO SS	15 16	9	7	(3,4	_				7										_
LOOSE SAND, LI-GREENISH GREY (SM): 18.30 (NO SALTY) DENSE TO VERY DENSE SAND, LI-GREENISH GREY (SP-SM) (NO SALTY) END OF BORING 20.45	17 - 18 - 19 -		SS WO SS WO SS	(B)		(2	5,2	G 45, 6 5%	9 /5			6	•								/	7

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cocation A. PHIMAI, NAKHON RAT	CHA:	SIM	4			·····							ŧ			IED 📑				_
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MEDIUM DENSE TO DENSE AND VERY DENSE SAND GREENISH GREY (SP-SM) 13.00 STIFF CLAY, LI-GREENISH GREY (CL)	1 - 2 - 3 - 4 - 5 - 7 - 8 - 9 - 10 - 11 - 12 - 13 - 14 - 15 - 16 - 15 - 16 - 15 - 16 - 16 - 17 - 18 - 18 - 18 - 18 - 18 - 18 - 18		PA	2 3 4 5 6 7 8 9 10	8 B	02 02 02 02 02 02 02 02 02 02 02 02 02 0	20 7 6 7 6 2 2 7 7 6 6 7	[3] [3] [3] [3] [3] [3] [4] [4] [2] [2] [2] [3] [4] [2] [4] [2] [4] [4] [4] [4] [4] [4] [4] [4] [4] [4	>											
HARD CLAY, GREENISH GREY (CL) (NO SALTY 18.00 DENSE SILTY FINE SAND, GREENISH GREY AND DARK	17- 18-		WO SS WO SS WO	17	(19	26	45	\$ }			\$ -1	•								<u>}</u>
BROWN (SP-SM)(SALTY)19.50 HARD CLAY, REDDISH BROWN (CL) (SALTY)	20-		SS WO SS	 	(16,17	33		80											0	

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HARD CLAY, REDDISH BROWN (CL) (SALTY)	21 - 22 - 23 - 24 - 25 -	CHILIFFI CHAPT	wo ss wo ss wo ss wo ss wo ss	21 22 23 24 25		(1 (1 (20)	6,2 6,2 (18, 22)	0 4 1) 9 41 23) 42 6) 4	37 940 941		1	%		·	×		r	□ T	٧		(t/	m ³) 8 2.0	- 18
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BORING LOC PROJECT 05.03 LAM PHRA PHLO LOCATION A. PAK THONG CHAI,	ENG	HON	RAI		CC	PTH ORD	(m.)_	22	.03					OB5	E S	VED STAI	LEV WL RTEI	(m. 11) <u>-</u> ./2	5 . s /89	50	
SOIL DESCRIPTION	DEPTH (m.)	GRAPHIC LOG	METHOD	SAMPLING B RECOVERY	**************************************	S bid 10 2		ft)		۱		0 {%)	-L -i 40	X	UC FV	T T	m ² } △ P ⊡ T 5 2	P V	ı	7 (1/	m.)	-
SOFT TO STIFF FINE SANDY CLAY, DARK BROWN . (CL) (NO SALTY)	1		PA SS PA SS PA SS PA SS SS			9	(4	9)															
LOOSE CLAYEY FINE SAND, DARK BROWN (SC) (NO SALTY) 7.00 MEDIUM DENSE CLAYEY AND	5-		PA SS PA	5 6	9	4 (2,2) 3)		and the second s			A A A A A A A A A A A A A A A A A A A					Additional of the second secon					
SILTY SAND, DARK BROWN AND GREY (SC,SP-SM,SM) (NO SALTY)	9-		PA	9	-	3,18		o 3	O)		6	b							,			-0	
VERY STIFF CLAY, TRACE OF SAND, DARK BROWN (CL) (NO SALTY)	12-		PA SS PA SS PA	12		6		23 10,1 22 9,13 27 12,1) 5)				2										Dimensional Distriction of the Control of the Contr
DENSE CLAYEY FINE SAND (INTERMEDIATE SOIL), DARK BROWN (SC/CL) (NO SALTY)	16- 16-		PA SS PA SS PA SS	15 16 17	•		0 0	24 (II, 25 12, IO)	,11) 13)		0,0							The state of the s					
20.00 HARD SANDY CLAY (CL)	19 - 20-		PA	20	(50		25			0												

DATE FINISHED 13/2/59	BORING LOC 05.03 LAM PHRA PHLOEN POSITION A. PAK THONG CHAT. NA	G	ים ז	mc**		DEF	RING PTH DRO.	(m,)		<u>22.</u>	03				OBS DAT	ERV	EO Tar	WL TED	(m.)	9 -5	.50 /81	0 9	
HARD SANDY CLAY, LI-BROWN AND GREY (CL) (MO SALTY) VERY DENSE SANDSTONE, BROWNISH GREY (NO SALTY) (SM) 22 03 END OF BORING SS 20 50/35CM (130,26/05M) (130,26/05M) SS 21 50/25CM (130,26/05M) SS 22 50/35CM (130,26/05M) SS 2	SOIL DESCRIPTION		T				blo	H 2 /	ft)		ŀ		(%)		L L	o x	5 _u (UC1 FV1	1/n r 2	 n. ²) △ P! ⊡ T\	2	(7 ₁	m, ³)	
	HARD SANDY CLAY, LI-BROWN AND GREY (CL) (NO SALTY) 22.00 VERY DENSE SANDSTONE, BROWNISH GREY (NO SALTY) (SM) 22.03	21-		SS WO SS WO	20		50, 50, 50,	721 26	ft) 0 4 5 Ct /10 5 CN 0 / 8	о (M)	2		(%)	O 80		X	FVI	۲ (• T\	v]	(17	m,3)	

BORING LOC PROJECT 05.03 LAM PHRA PHLOEI LOCATION A. PAK THONG CHAI, N.	NG	ом в	OTAS	HAS	CO	RING PTH ORD	(m.	.)		18.	.05	<u> </u>			DB:	OUNC SERV E S	ÆD TAR	WL TEC	(m.) <u>+(</u> 3/2	2/8	0
SOIL DESCRIPTION	DEPTH (m.)	GRAPHIC LOG	METHOD	SAMPLING B RECOVERY		S I (Ыс	WE /	ft)		!	ļ	(%) 30 8	1	×	S _u (r .	Δ. P [] T	P V			m ³) 8 2.0
STIFF TO VERY STIFF SANDY CLAY, GREYISH BROWN AND DARK BROWN (CL) (NO SALTY) 3.50 MEDIUM DENSE CLAYEY AND SILTY SAND, DARK BROWN AND GREY (NO SALTY) (SC,SM) 5.50 VERY STIFF TO HARD CLAY, DARK BROWN (CL) (NO SALTY) (SC) 12.80 VERY STIFF CLAY, DARK BROWN (CL) (NO SALTY) (NO SALTY) 16.00 MEDIUM DENSE CLAYEY FINE SAND, DARK GREY (SC/CL) 16.79 MEDIUM SANDY CLAY, DARK GREY (NO SALTY) (CL) MEDIUM SANDY CLAY, DARK GREY (NO SALTY) VERY DENSE SANDSTONE, GREY (NO SALTY) (SM) 18.05 END OF BORING	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16		W0 SS W0 W0	1 2 3 4 4 5 7 7 8 8 9 10 11 11 11 11 11 11 11 11 11 11 11 11	(2)	6 0 0 0	3,3 (5 (5) (7) (7) (8) (7) (8) (7) (7) (7) (7) (7) (7) (7) (7) (7) (7) (6,1) (7,1) (7,1) (7,1) (7,1) (7,1) (7,1) (7,1) (7,1) (7,1)	0) 12												0	
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BORING LOC					BORING NO. B		GROUND ELEV.(m.)	
ROJECT 05.03 LAM PHRA PHLOP					COORD.		DATE STARTED 8	3/2/89
ocation A. PAK THONG CHAI. N	AKH		,	,	ļ		DATE FINISHED 10	1/2/89
SOIL DESCRIPTION	DEPTH (m.)	GRAPHIC LOG	METHOD	SAMPLING B RECOVERY	SPT - N (blows/ft) IO 2O 3O 40	PL Wn LL (%) JO 20 30 40	5u(1/m²) ⊙UCT △PP XFVT □TV 5 10 15 20	1/ _t (1/m ³) 1.6 1.8 2.0
La Contraction de la Contracti	1-		PA		© 13 (6,6)	Φ		
STIFF TO VERY STIFF FINE SANDY CLAY, DARK BROWN (CL)	2-		PA SS PA		0 12 (6,6)			. 9
(NO SALTY)	3-		PA	3 4	\$ 9 (4,5) \$ 15(6,9)			
	5-		PA	5	6 17(7,10)			
	7-		PA	7	6 17(7,10) 9 20 (9,11			
9.50	8- 9-		L	8	d 16(7,9)			
MEDIUM DENSE CLAYEY SAND, DARK BROWN (NO SALTY) (SC) 10.50	<u>-</u>		PA	10	(13,10)			
VERY STIFF SANDY CLAY, DARK BROWN (CL)	12-		PA	15	6 24 ((2,12) g 19(8)))	1 10		
(NO SALTY) 13.50]		PA SS PA	13	(17,8,9)			
MEDIUM DENSE TO DENSE CLAYEY FINE SAND, DARK BROWN AND GREY	14* 15-		РД	14	0 22 (8,14) (6,7)			
(SC) (NO SALTY) 16.50 VERY STIFF FINE SANDY CLAY	16-		PA SS PA	16	D 31	5		
DARK BROWN(CL) 17.50 (NO SALTY) MEDIUM DENSE TO DENSE AND VERY DENSE CLAYEY FINE			SS PA SS	17 18	0 16 (8,8			
SAND, DARK BROWN (3C)	- 19-		PA SS PA	Ð.	(17,19) & 30			
(NO SALTY END OF BORING 20.22	SO		SS.	2C	132.20/8CI			

SOIL DESCRIPTION	BORING LOG PROJECT 11.01 LAM NAM KAM LOCATION A.MUANG, SAKON NAKHON				3 NO			1		OBS DAT	UND E	LEV WL RTE	(m.)	0/2	3.20 2/89	,
FINE SAND, BROWN (SM) (NO SALTY) 3.00 SOFT TO MEDIUM FINE SANDY CLAY, (CL) (NO SALTY) To see the second of the	SOIL DESCRIPTION HEAD HEAD HEAD HEAD HEAD HEAD HEAD HEAD	СОС СОС МЕТНОВ	SAMPLING RECOVERY	S (bld 10 2	ows/fl)		 	(%)	1	×	UCT FVT	Δ p □ T	ዖ V		t/m ³)	. 11
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BORING LO PROJECT 11.01 LAM NAM KAM LOCATION A.MUANG, SAKON NAKH		BORING NO. BH. DEPTH (m.) 19 COORD.	.05	GROUND ELEV.(m. OBSERVED WL (m. DATE STARTED DATE FINISHED	.) <u>-3.00</u> 17/2/89
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MEDIUM DENSE GRAVELLY SAND BRONW (SP-SM) (NO SALTY) 2.50 LOOSE SAND, WITH GRAVEL, BROWN (SM)(NO SALTY) 3.80 VERY STIFF SANDY CLAY, GREY (SC/CL)(NO SALTY) 5.00 VERY DENSE GRAVELLY SAND, GREY (SM) (NO SALTY) 6.05 END OF BORING	2- 3-		PA SS PA SS PA SS WO	2 3		8 2	(4) (4) (2) (2) (4) (7)	2 (0) (1) (5) (6) (7) (5) (5) (5) (5) (7)	9 9 N N N N N N N N N N N N N N N N N N	6										.6		
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SOIL DESCRIPTION	DEPTH (m.)	GRAPHIC LOG	METHOD	SAMPLING B RECOVERY	10	S P blow 0 20	18/	ft)		1		(%)		1	(C	UC FV	T	m ² } △ P ⊡ T 5 2	ρ ∀		1, (1/ 6 l.	
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APPENDIX C SUMMARY OF TEST RESULTS

SUMMAR' PROJECT LOCATION		01.01 H	LTS Uai kae G, Kalas	iIN								HADE B DATE CHECKE DATE	Y : : D BY : :	NARONG P. 10/3/89 WITOON S 10/3/89	
SAMPLE No.	DEPTI	i (a)	USCS GROUP -		GRADATI PASSING	SIEVE)		NATURAL NATER CONTENT		AND 1	LIMITS NDICIES		SP.GR - G5	-	SPT-N
	FROM	10		84		#40	#200	(\$)		P	PL PI	i LI		(t/cu.m)	
55-1	1.00	1.45	SM	-		-	*		*				*******	-	13
55-2	2.00	2.45	SM	100	100	98	21	16	•				2.678	1.97	11
55-3	3.00	3.45	SM	•	-	-	-	-	-				-	-	7
55-4	4.00	4.45	CL	•	-	-	-	•	-		• .		-	-	30
55-5	5.00	5.45	CL	100	99	97	73	15	41	2	1 20	-0.3	2.698	2.05	26
SS-6	6.00	6.45	CL	*	-	-	_	-	•				-	•	15
SS-7	7.00	7.45	SC	100	100	95	42	24	-					•	3
55-8	B.00	8.40	ĈL	-	-	-	-	41	-			. -	2.705	2.07	50/28ca
55-9	9.00	9.07	SC		-	-	-	-	-					-	50/15cm
55-10	10.00	10.05	SC	•	-	-	~	8	-		•		2.676	-	50/10cm
SS-11	11.00	11.03	SC	•	-	-	-	•	•		•				50/8cm

FILE : 0101-1

SUMMARY PROJECT LOCATIO		01.01 H	LTS Wai kae G, kalas	Ih			GROUND	KO. : (m) : EL.(m): PTH (m):	97.4				DATE DATE	:	NARONG P. 10/3/89 WITCOM S. 10/3/89	
SAMPLE NO.	DEPTI	H (a)	USCS GROUP -	•	GRADAT: Passing	SIEVE)		NATURAL WATER CONTENT		TERBE AND	RG LIM INDIC		(%)	SP.GR Gs		SPT-N
	FROM	TO		14	#10	B 40	#200	(\$)		.1	PL	PI	LI		(t/cu.a)	
SS-1	1.00	1.45	SM		-			******		•	•	-	-	•	-	5
SS-2	2,00	2.45	SH	100	100	97	33	14		-	•	-	-	2.676	2.01	5
55-3	3.00	3.45	SM	•	-	-		•		-	•	-	-	•	-	6
SS-4	4.00	4,45	SM	100	100	98	17	16		-	•	-	-	-	•	7
SS-5	5.00	5.10	SM	-	-	-	-	-		-	-	-	-	*	-	50/10ca
55-6	6.00	6.15	SM	100	99	87	23	15	ı	-	-	-	-	2,666	1.86	50/15cm
SS-7	7.00	7.10	SH	-	-	-		•		-	-	-	-		-	50/10cm
SS-8	8.00	8.07	CL	100	100	99	63	15		-	-	-	-		•	50/8cs

FILE : 0101-2

SUMMAR PROJEC LOCATI		1.01 H	LTS UAI KAE G, XALAS	SIN			GROUND	NO. : (m) : EL.(m): PTH (m):	99.45			MADE BY DATE CHECKED DATE	:	NARONG P. 10/3/89 WITOON S. 10/3/89	
SAMPLE NO.	DEPTH From	(ø) TO	USCS Group	(% #4	GRADAT Passing			NATURAL WATER CONTENT	ATT	AND I	LIMITS NDICIES		SP.GR Gs	TOTAL UNIT WEIGHT (t/cu.m)	SPI-1
55-1 55-2 55-3 55-4	1.00 2.00 3.00 4.00	1.45 2.45 3.45 4.45	HZ HZ HZ	100 100	- 99 100	94 96		- 13 16			* *		2.685 2.678	1.92 2.12	14
SS-5 SS-6 SS-7 SS-8 SS-9	5.00 6.00 7.00 8.00 9.00	5.45 6.30 7.25 8.30 9.22	SH SH SH SH CL	100 - 100 - 100	100 - 100 - 93	99 - 99 - 78	28 24 -	20 - 18 -					2.695 - 2.686 -	1.9 - 1.89 - 1.67	8 41 50/15cs 50/10cs 50/10cs 50/8cs

FILE : 0101-3

SUMMAR	Y OF TE	ST RESU	LTS				BOAING	NO. :	8H-1				HADE BY	;	NARONG P	
	•						DEPTH .	(a) :	15.1	.5			DATE	:	5/3/89	
PROJEC	T :	02.05 H	UAI KHUN	MUN			GROUND	EL.(a):	95.2	2			CHECKED	BY:	S HOOTIW	•
LDCATI	ON :	A.UBON	RATTANA,	KHDN	KAEH		GWL DE	PTH (m):	-0.1	10			DATE	•	5/3/89	
SAMPLE NO.		H (m)	USCS GROUP -		GRADATION S	SIEVE)	*****	NATURAL WATER			INDIC	CIES	1)	SP.GR Gs	TOTAL UNIT WEIGHT	SPT-X
110.	FROM	TO	-11001	14		\$40	# 200				PL		LI	4,5	(t/cu.m)	
S5-1	1.00	1,45	SH	100	100	99	30	16		-	-			2.671		5
55-2	2.00	2,45	CL/SC	100		99	53			-	-	-	•	2.685	I.25	2
S5-3	3.00	3.45	SH	-	~	-	-	-		-	-	-	-	-	-	1
SS-4	4.00	4.45	SH	-		-	•	-		-	-	-	**	-	-	5
SS-5	5.00	5,45	SC	-	•	-	_	-		•	-	-			-	4
55-6	6.00	6.45	SC	-		-	-	-		-	-	-		-	-	5
SS-7	7.00	7.45	SM	100	100	99	34	26		-	-	-	•	2.688	-	1
SS-8	8.00	8.45	SC	-	•	-	-	-		•	-	-	н	-	-	15
SS-9	9.00	9.45	SC	-	•	-	-	-		-	•	-	-	-	-	18
SS-10	10.00	10.40	SP-SM	100	100	98	8	22	}	-	•	-	•	2.678		50/25cm
SS-11	11.00	11.45	SP-SM	-		-	-	-		-	-	-		•	-	45
SS-12	12.00	12.43	SP-SH	-	•	-	•	-		-	-	*	-	-	-	50/28cæ
SS-13	13.00	13.45	SP-SH	-	•	-	-	-	•	-	-	-	-	-	-	50
SS-14	14.00	14.45	SP-SM	-	-	-	•	-	•	-	-	-	•	•	-	41
55-15	15.00	15.15	SP-SM	-	•	-	•	-	· 110 1	RECOVER	Y	-	٠	•	-	50/15cm

FILE : 0205-1

 BORING NO. : BH-2
 MADE BY : MARONG P.

 DEPTH (m) : 20.35
 DATE : 5/3/89

 GROUND EL.(m): 94.0
 CHECKED BY : WITOON S.

 GHL DEPTH (m):+1.00
 DATE : 5/3/89

 SUMMARY OF TEST RESULTS

PROJECT : 02.05 HUAI KHUM MUN LOCATION : A.UBON RATTANA, KHON KAEN

SAMPLE NO.	DEPT	H (a)	USCS GROUP	(২	GRADATIO PASSING S			ATURAL KATER ONTENT -		BERG LI ID INDI	HITS (%) CIES		SP.GR Gs	TOTAL UNIT WEIGHT	SPT-H
	FROM	TO		#4	#10	#40	#200	(*)	LL	PL	Id	LI		(t/cu.m)	
SS-1	1.00	1.45	SH	100	100	99	37	22	-	-	-	-	2.692	-	}
SS-2	2.00	2.45	SM	-	•	-	-	-	-	-	-	•	-	-	9
SS-3	3.00	3.45	SH	-	-	-	-	-	-	-	-	•		•	10
SS-4	4.00	4.45	SM	•	-	-	-	-	-	-	-	•			18
SS-5	5.00	5.45	SH	100	100	91	15	20	-	-	-	•	2.67	•	9
SS-6	6.00	6.45	SH	-	-	-	-	-	-	-	-	-	-	•	40
SS-7	7.00	7.40	SM	-	-	-	-	-	-	-	-	-	-	-	50/25cm
SS-8	8.00	8.45	SH	100	100	99	28	-	-	-	-	-	•,	-	40
SS-9	9.00	9.45	SM	-	-	-	-	-	-	-	-	-	-	-	50
SS-10	10.00	10.45	SM	-	-	-	-	-	-	_	-	-	-	•	50
55-11	11.00	11.45	SP-SM	100	100	68	11	21	-	-	-	-	2.677	•	27
SS-12	12.00	12.45	SP-SM	-	•	-	-	-	-	-	-	-	-	-	48
SS-13	13.00	13.45	SP-SM	-	-	-	-	-	-	-	-	-	-	•	37
55-14	14.00	14.45	CŁ	-	-	-	-	-	-	-	-	•	-	•	45
SS-15	15.00	15.45	CŁ	-	•	-	-	32	-		•	•	2.708	1.88	32
SS-16	16.00	16.40	CL	-	•	-	-	-	-	-	•	-	-	•	50/25ca
SS-17	17.00	17.45	CL	-	-	-	-	-	-	-	-	-	-	-	49
55-18	18.00	18.45	CL	-	-	-	•	-	-	-	-	-	-	-	49
SS-19	19.00	19.35	CL	-	-	-	-	-	-	-	-	•	-	-	50/20cm
SS-20	20.00	20.35	CL	-	•	-	•	-	•	-	-	-	-	-	50/20cm

FILE: 0205-2

		 										*			
SUMMARY	OF TE	ST RESU	LTS				BORING		BH-3			HADE BY	· :	NARONG P.	
							DEPTH (20.20			DATE	:	5/3/89	
PROJEC			HUHN IAU					EL.(n):				CHECKED	BY:	WITOON S.	
LOCATIO	OH :	A.UBDX	RATTANA,	KHON	XAEN		GWL DEA	'(m) HT	0.00			DATE	:	5/3/89	
SAMPLE	DEPT	H (m)	USCS	(\$	GRADATIO PASSING S			HATURAL HATER		ERBERG I		(%)	SP.GR		SPT-N
NO.	FRON	TO	GROUP -	14	#10	#40	1200	CONTENT (%)		PL	ΡI	LI	G5	HEIGHT (t/cu.m)	
55-1	1.00	1.45	CL	100	99	99	85	18	-	-	-		2.689	-	8
SS-2	2.00	2.45	CL	-	-	-	-	-	-	•	-		-	-	4
\$5-3	3.00	3.45	ÇL	-	-	-	-	33	-	-	-	. <u>-</u>	2.713	-	2
55-4	4.00	4.45	ÇL	-	•	-	-	-	-	-	-	. -	-	-	10
SS-5	5.00	5.45	SH	-	-	-	-	-	-	-	-	. -	-	-	9
55-6	6.00	6.45	SH	-	-	-	-	-	-	•	-		-	-	18
SS-7	7.00	7.45	SH	-	-	-	-	-	-	-	-		-	-	10
\$\$-8	8.00	8.45	CL	-	•	-	-	27	-	• •	-	-	-	1.97	14
SS-9	9.00	9.45	CL	-	•	-	-	-	-	-	-	· -	-	•	16
\$\$-10	10.00	10.45	SH	-	-	-	-	-	-	-	•	• •	-	-	13
SS-11	11.00	11.45	SH	-	-	-	-	-	-	•	•		-	-	13
\$5-12	12.00	12.45	SH	-	-	-	-	-		•	-	-	-	•	41
SS-13	13.00	13.20	SM	-	-	-	-	21	-		•		-	•	50/20ca
55-14	14.00	14.35	SM	-	•	-	•	•	-	• •	•	•		· -	50/20cm
SS-15	15.00	15.45	CL	-	-	-	•	25	, -	•	•	•	2.74	-	16
55-16	16.00	16.45	CL	-	-	-	-	-	•	•	•		-	•	41
SS-17	17.00	17.33	SC	-	-	-	-	•	•	•	•	• •	-	• -	50/18cm
55-18	18.00	18.10	SM	•	•	-	-	•	•	•	•		=	•	50/10cm
55-19	19.00	19.18	. SM	•	-	-	-	•	•	•	•		-	• •	50/18ca
SS-20	20.00	20.10	SH	-	•	•	•	-		•		- •	•	•	50/10cm

FILE : 0205-3

PROJECT LOCATIO		4.01 H	UAI SOENG E, NAXHON								DATE CHECKED DATE	:) BY : :	NARONG P. 4/3/89 HITOON S. 4/3/89	
SAMPLE NO.	DEPTH	(n)	USCS GROUP	(1	GRADATI PASSING			NATURAL HATER CONTENT		G LIHITS INDICIES		SP.GR Gs		SPI-)
	FROH	10		14	#10	#40			LL	PL P	I LI		(t/cu.a)	
\$S-1	1.00	1.45	CL	-		*	-		-	 -	-		*	1
SS-2	2.00	2,45	CL	-	-	•	-	26	44	22 2	2 0.18	2.741	1.88	į
SS-3	3.00	3.45	CL	-	•	**	-	-	-	•		-	. •	•
SS-4	4.00	4.45	CL	-	-	•	-	-	-	-		-	-	4
SS-5	5.00	5.07	CL	100	99	79	67	10	-	•		2.722	-	50/8c
SS-6	6.00	6.05	CL	-	-	**	-	-	-	-	-	-	•	50/5c
SS-7	7.00	7.03	CL	-	-	-	-	-	-	•		•	-	50/3c
SS-B	8.00	8.05	CL	100	97	79	86	11	-	-		•	-	50/50
SS-9	9.00	9.03	CL	-	-	*	-	-	-	-		•	•	50/30
SS-10	10.00	10.03	CL	_	_	***	-	13	-	-		_		50/30

FILE: 0401-1

SUMMARY PROJECT LOCATIO	: 0	4.01 H	LTS UAI SOENG E, NAKHON								HADE DATE CHEC DATE	XED	: BY :	NARONG P. 4/3/89 Witoon S. 4/3/89	
SAMPLE NO.	DEPTH FROM	(a) TO	USCS GROUP	(\$	GRADAT: PASSING	SIEVE)	*****	NATURAL WATER -CONTENT (%)	 AND 1	LIMITS		LI	SP.GR Gs	TOTAL UNIT NEIGHT (t/cu.m)	SPT-N
SS-1 SS-2 SS-3 SS-4	1.00 2.00 3.00 4.00	1.45 2.45 3.45 4.15	CL CL SC	- - 74	51	- - 38	- - 34	-		19	13 0,	- .77 -	2.738 - -	2.05	3 4 6 50/15c⊪

FILE : 0401-2

PRDJEC	T : (LTS UAI SOEN E, NAKHO				BORING NO DEPTH (m GROUND EI GNL DEPTI) : L.(m):	98.44				MADE BY DATE CHECKED DATE	:	MARONG P. 4/3/89 WITOOM S. 4/3/89	
SAMPLE NO.		H (m) TO		-		SIEVE)	C	ONTENT		AND	IHDI			SP.GR Gs		SPT-N
55-1 55-2	1.00	1.45 2.45	CL	-	-	-	-	- 20	29	· ·)	- 15	- 14	0.36	2.710	2.04	7 7
55-3 55-4	3.00 4.00	3.45 4.45	CF	•	-	-	•	- 18	- 20)	- 11	- 9	- 0.78		2.10	3 2
SS-5 SS-6	5.00 6.00	5.05 6.05	CT	100	98 -	79 -	68 -	9	-	•	-	-	•	2.695 -	•	50/5cm 50/5cm
55-7 55-8	7.00 8.00	7.07 8.05	CF	•	-	-	-	-	-	•	-	-	-	-	***	50/8cm 50/5cm
SS-9 SS-10	9.00 10.00	9.03 10.03	CF	•	•	-	-	-	-	•	-	•	-	-	-	50/3cm 50/3cm

FILE : 0401-3

SUMMARY PROJECT LOCATIO	: 0)4.02 H	JLTS JUAI SOEK AE, HAKHO						96.08				HADE BY DATE CHECKED DATE	:	NARONG P. 5/3/89 WITOON S. 5/3/89	
SAMPLE NO.	DEPTH	ł (as) TO	USCS - GROUP -	(1	GRADATI PASSING	SIEVE)	1 200	NATURAL HATER -CONTENT (1)		OKA	G LIHI Indici PL	ES		SP.GI		SPI-A
		I V						(1/						*****	(0)00.01	******
SS-1	1.00	1.45	CH	-	-	•	-	-	-		-	-	*			ç
SS-2	2.0D	2.45	CH	-	-	•	-	34	62		26	36	0.22	2.73	6 1.91	5
55-3	3.00	3.45	CH	•	•	-	-	-	•		•	*	~	•		1
SS-4	4.00	4.15	SC/CL	-	•	•	-	-	•		•	-	-			50/15cm
\$5-5	5.00	5.15	SC/CL	99	90	62	48	19	-		-	-	•	2,71	1 1.78	50/15cm
55-6	6.00	6.12	SC/CL	-	•	•	-	-	-		-	-			•	50/13cm
SS-7	7.00	7.10	SC/CL	-	•	•	-	•	-		-	-	•			50/10ca
SS-8	8.00	8.10	SC/CL	100	90	64	49	15	-		-	-	•		- 1.64	50/10cm
\$5-9	9.00	9.07	SC/CL	-	•	-	•	-	•		-	-	•			50/8cm

FILE : 0402-1

SUHHARY	OF TES	ST RESU	LTS				BORING		8H-2			-	IADE BY	:	NARONG P.	
PROJECT LOCATIO			UAI SOEN E, NAXHO				GROUND	n) : EL.(a): TH (a):	92.4			C	ATE HECKED ATE	8Y :	5/3/89 Hitoon S. 5/3/89	
SAMPLE NO.	DEPTH	i (n)	USCS GROUP -	-	GRADAT PASSING	SIEVE)		NATURAL NATER CONTENT		AND	INDIC		;)	SP.G		SPT-N
	FROM	TO	ango;	#4				(\$)			PL	ΡĮ	LI	G,	(t/cu.m)	
\$\$-1 \$\$-2	1.00 2.00	1.45 2.12	CL CL	100 94		95 64	89 59	23 10			-	-		2.68 2.70		6 50/13cm

FILE : 0402-2

SUMMARY PROJECT	: 0	4.02 X	UAI SOENG					(a) : EL.(a):			****		MADE BY DATE CHECKED	BY:	NARONG P 5/3/89 WITOON S	
LOCATIO	# : A	. HAKA	E, NAKHON	**************************************	UN		GHL DE	PTH (m):	-1.3]			DATE	:	5/3/89	
SAMPLE NO.	DEPTH	(m)	USCS GROUP	(\$	GRADATI PASSING			HATURAL RATER TKATROO-	!	TERBER AND			*)	SP.GR		SPT-N
110.	FROM	TO	4NOV	#4	#10	#40				ı	PL	ΡĬ	LI	03	(t/cu.a)	
\$\$-1 \$\$-2	1.00	I.45 2.45	CL CL	-		·	 - -	- 26		- 30	- 19	- 11	0.64	2.746	1.89	9
SS-3	3.00	3.45	ÇL	-	•	-	-	-	•	-	-	-	•	-	-	5
\$\$-4 \$\$-5	4.00 5.00	4.45 5.15	CL SC	- 97	- 69	- 50	44	26 13			:	-		2.723	2.02	16 50/15cm

FILE: 0402-3

SUMMARY PROJECT LOCATIO)5.01 l	.AM KLANO		RATCHASIMA							MADE BY DATE CHECKED DATE	:	NARONG P. 23/2/89 HITOON S. 23/2/89	
SAMPLE NO.	DEPTH FROM	l (m) TO	USCS GROUP		GRADATID PASSING S	IEVE)				ERBERG LI AND INDI PL	CIES		SP.GR Gs	TOTAL UNIT WEIGHT (t/cu.m)	SPT-N
	1 1/1/11								,						
SS-1	1.00	1.45	SC	-	•	-	•	15	-	-	•	•	-	-	14
SS-2	2.00	2.45	SC	91	90	85	21	13	33	13	20	0	2.715	2.14	29
SS-3	3.00	3.45	SC	-	-	-	-	14	-	-	-	-	-	•	35
55-4	4.00	4.45	SC	-	-	-	-	12	-	-	-	-	-	•	48
SS-5	5.00	5.45	CL/SC	100	100	98	50	13	38	16	22	-0.13	2.711	2.18	35
SS-6	6.00	6.45	CL/SC	-	~	-	•	11	-	-	-	-	-		40
SS-7	7.00	7.39	SC	-	-	-	-	15	-	-	-	-	-	-	50/24 ci
SS-8	8.00	8.41	SC	100	100	85	32	13	22	10	12	0.25	2.693	•	50/25 ct
SS-9	9.00	9.36	SC	-	-	-	-	14	-	•	-	-	-	-	50/20 ca
SS-10	10.00	10.25	CL	-	•	•		17	-	-	-	-	-	-	50/25 c
SS-11	11.00	11.38	CL	•	-	-	-	16	30	12	18	0.22	2.706	2.09	50/23 c
SS-12	12.00	12.20	ÇL	-	-	-	-	15	-	-	-	-	-	-	50/20 c
SS-13	13.00	13.20	CL	-	-	-	-	15	-	-	-	-	•	-	50/20 c
SS-14	14.00	14.18	CL	-	•	-	-	15	-	-	-	-	-	-	50/18 c
SS-15	15.00	15.15	CL	-	-	-	-	17	-	-	-		-	2.10	50/15 c

FILE : 0501-1

SUMMAR' PROJECT		05.01 L	LTS AM KLANG DONG, NA		CHASIMA		BORING NO DEPTH (m GROUND E GNL DEPT) :1 L.(m):9	3,13 6.6			MADE BY DATE CHECKED DATE	: : By : :	NARONG P 23/2/89 WITOON S 23/2/89	
SAMPLE KO.		10 H (m)	USCS GROUP -	(* P/	RADATIO ASSING S	IEVE)	₩ C #200	ATURAL WATER ONTENT - (*)	A	BERG LIN ND INDIC	CIES	·	SP.GR Gs	TOTAL UNIT MEIGHT (t/cu.m)	SPT-H
00.1															
\$\$-1	1.00	1.45	CL	•	-	•	-	17			•	• • •		1.99	13
55-2	2.00	2.45	CL	-	-	-	-	12	31	13	18	0.06	2.718	2.19	56
55-3	3.00	3.45	CL	-	-	-	-	12	-	•	•	-	-	-	32
SS-4	4.00	4.45	CL	-	-	-	•	14	-	•	-	-	•	2.15	34
\$S-5	5.00	5.45	CL	-	-	-	-	20	-	-	-	-	-	-	18
55-6	6.00	6.45	CL	100	99	92	64	15	37	16	21	-0.05	2.696	2.08	28
SS-7	7.00	7.45	CL	_	-	-		13	-	-		_	-	•	38
55-8	8.00	8.45	CL	-	•		-	21	-	-	•	-	-	1.96	40
55-9	9.00	9,36	CL	-	-	-		16	_				_	•	50/20 cm
SS-10	10.00	10.33	CL	-	_	_		16	30	13	17	0.18	2.681	1.84	50/18 cm
\$5-11	11.00	11.23	CL	_	_		_	14	JV -	10	11	0.10			•
					•	-	-		-	•	•	•	•	-	50/23 cm
SS-12	12.00	12.20	CL	•	-	-	-	17	•	•	•	-	-	-	50/20 cm
55-13	13.00	13.13	CL	-	•	•	-	14	-	-	•	-	-	-	50/13 cm

FILE : 0501-2

SUMMARY OF TEST RESULTS

BORING NO. : 8H-3

DEPTH (m) : 15.18

PROJECT : 05.01 LAM KLANG

GROUND EL.(m): 99.5

LDCATION : A.NON SOONG, NAKHON RATCHASIMA

GWL DEPTH (m): -1.60

DATE : 23/2/89

SAMPLE No.	DEPT	H (m)	USCS Group -	(1	GRADATI Passing			NATURAL HATER CONTENT		BERG LI ND INDI	-	1)	SP.GR G5	TOTAL UNIT Weight	SPT-H
1104	FROM	TO		34	F 10	140	4200	(\$)	LL	PL	PI	LI		(t/cu.m)	
\$5-1	1.00	1.45	SH	-	-	-	•	7	-	-	-	-	-	-	6
55-2	2.00	2.45	SM	99	96	76	16	11	-	-	•	-	2.691	1.81	38
55-3	3.00	3.45	SM	-	-	-	-	13	-	-	•	-	-	•	10
55-4	4.00	4.45	SC	100	100	98	41	14	31	12	19	0.11	-	2.13	22
\$\$-5	5.00	5.45	SC	-	-	•	•	13	•	-	*	-	-		50
55-6	6.00	6.45	SC	100	100	97	32	14	-	-	•	-	2.696	2.11	29
\$5-7	7.00	7.45	CF	-	•	•	-	19	-	-	•	-	-	•	23
\$\$-B	8.00	8.45	CL	-	-	-	•	14	35	14	21	0	-	2.13	29
55-9	9.00	9.45	CL	-	. •	•	•	16	-	-	-	-	-	•	38
55-10	10.00	10.30	SC	100	100	98	32	13	-	-	•	+	2.712	*	58
\$5-11	11.00	11.45	CL	-	•	•	-	18	-	-	-	•	-	-	54
SS-12	12.00	12.38	CL	•	-	-	•	17	•	•	-	-	-	•	50/23 cm
55-13	13.00	13.36	CF	-	-	-	•	15	27	12	15	0.2	2.717	2.14	50/20 c ≘
SS-14	14.00	14.33	CL	•	-	•	-	13	-	•	-	•	-	•	50/18 cm
\$\$-15	15.00	15.18	CL	•	*	•		17	-	-	-		-	•	50/18 cm

FILE: 0501-3

SUMMAR' PROJEC		5.02 :	LAH NAI		CHASIMA		BORING H DEPTH (m GROUND E GHL DEPT) : L.(m):				HADE BY DATE CHECKED DATE	:	NARONG P. 20/2/89 WITOON S. 20/2/89	
SAMPLE NO.	DEPTI	l (a)	USCS Group -	-	GRADATI PASSING	SIEVE)		ATURAL WATER DNTENT	f	R8ERG LI AND INDI	CIES		SP.GR Gs	TOTAL UNIT WEIGHT	SPI-N
	FROM	TO	-11-2	#4	#10	#40	#200	(1)	LL	PL	PΙ	LI		(t/cu.m)	
SS-I	1.00	1.45	SP-SH	100	100	98	9	23	-	-	-	-	2.691	1.87	
SS-2	2.00	2.45	SP-SM	-	-	-	-	-	-	-	-	-		. •	1
SS-3	3.00	3.45	SM	-	-	•	~	20	-	-	-	-	• •	1.75	18
SS-4	4.00	4.45	SH	•	•	•	-	-	-	-	-	-	•	-	15
SS-5	5.00	5.45	SM	-	-	-	-	-	-	-	-	-	-	-	19
SS-6	6.00	6.45	SM	100	95	77	43	21	-	-	-	•	2.683	2.08	11
SS-7	7.00	7.45	SH	-	-	-	-	•	-	-	-	-	-	-	26
SS-8	8.00	8.45	SM	. •	-	-	•	18	-	-	-	-	-	2.06	36
SS-9	9.00	9.45	SM	-	-	-	-	-	-	-	-	-	-	-	32
SS-10	10.00	10.45	SP-SH	100	100	99	8	22	· -	-	~		2.692	1,75	45
SS-11	11.00	11.45	SM	-	-	•	-	-	-	-	-	-	-	•	19
SS-12	12.00	12.45	SH	-	-	•	-	•	-	-	-	-	-	:	48
SS-13	13.00	13.45	SM	99	96	72	41	78	-	-	-	-	-	1.92	60
SS-14	14.00	14.45	CH	-	-	•	-	•	-	-	-	-	-	-	9
SS-15	15.00	15.45	CH	-	-	-	-	33	62	27	35	0.17	2.722	1.88	1
SS-16	16.00	16.45	CH	-	-	•	-	-	-	-	•	-	-	•	â
SS-17	17.00	17.45	CH,SM	-	•	-	-	26	•	-	-	-	-	2.04	12
SS-18	18.00	18.45	SP-SH	-	-	-	-	-	-	-	-	-	•	*	24
SS-19	19.00	19.45	SP-SM	100	100	95	9	22	-	-	-	-	2.699	1.83	. 51
SS-20	20.00	20.45	SP-SM	-	-	-	-	-	-	•	-	•	-	•	50/2202

FILE : 0502-1

 SUMMARY OF TEST RESULTS
 BORING NO. : 8N-2
 HADE BY : NARONG P.

 DEPTH (m) : 27.45
 DATE : 20/2/89

 PROJECT : 05.02 : LAM NAH HUN
 GROUND EL.(m): 94.9
 CHECKED BY : HITOOH S.

 LOCATIOH : A.PHIMAI, HAKHON RATCHASIMA
 GWL DEPTH (m): -0.30
 DATE : 20/2/89
 GRADATION NATURAL ATTERBERG LIMITS (%) TOTAL SAMPLE DEPTH (m) USCS (% PASSING SIEVE) WATER AND INDICIES SP.GR UNIT SPT-N FROM TO #4 #10 #40 #200 (%) LL PL PI LI (t/cu.m) SS-1 1.00 1.45 SP-SH SS-2 2.00 2.45 SP-SH 100 5 - - - - 2,697 99 19 1.65 22 ----26 \$\$-3 3.00 3.45 \$P-\$M 15 1.94 16 . SS-4 4.00 4.45 SP-SH --12 SS-5 5.00 5.45 SP-SM 100 100 97 10 22 - 2.689 37 SS-6 6.00 6.45 SP-SM • , • -22 • SS-7 7.00 7.45 SP-SM 22 - 1.92 99 \$\$-8 8.00 8.45 \$P-\$M 99 60 4 21 36 SS-9 9.00 9.45 SP-SM ----54 SS-10 10.00 10.45 SP-SM 22 SS-11 11.00 11.45 SM - 2.698 99 79 33 16 16 2.05 19 SM SS-12 12.00 12.45 23 SS-13 13.00 13.45 CL 33 1.89 11 \$\$-14 14.00 14.45 CL • 8 SS-15 15.00 15.45 CL 48 21 27 0.44 2.712 1.89 33 SS-16 16.00 16.45 CL 12 - 23 SS-17 17.00 17.45 CL 27 11 16 0.75 2.717 2.11 14 SS-18 18.00 18.45 SP-SM 40 -SS-19 19.00 19.45 SP-SM 100 100 94 22 2.697 1.84 48 \$\$-20 20.00 20.45 ÇL 33 ÇL \$5-21 21.00 21.45 37 20 0.3 28 47 \$\$~22 22.00 22.45 ÇL 27 1.88 40 SS-23 23.00 23.45 CL 41 SS-24 24.00 24.45 CL 40 SS-25 25.00 25.45 CH 27 53 23 30 0.13 2.730 2,02 42 \$\$-26 26,00 26,45 CH 49 SS-27 27.00 27.45 CH 52

FILE: 0502-2

SUMMARY PROJECT LOCATION	т:		LAM NAM		CHASIHA		BORING DEPTH (GROUND GWL DEP	m) : EL.(m):			••••		MADE BY DATE CHECKED DATE		NARONG P 20/2/89 WITOON 5 20/2/89	
SAMPLE NO.	DEPT	H (m)	USCS GROUP -	(}	GRADAT PASSING			NATURAL WATER CONTENT		AN	ERG LII D INDI	CIES	\$)	SP.G G		SPT-N
110.	FROM	TO	GRUUP	#4	#10	#40	#200	(\$)			PL	ÞI	LI	u	(t/cu.m)	
SS-1	1.00	1.45	SH	-		-	-	20		-	_	-	-		- 1.84	13
SS-2	2.00	2.45	SM	-	-	-	-	-		-	-	-	•			9
SS-3	3.00	3.45	SH	100	100	61	29	21		-	-	_	- '	2.69	6 1.78	19
SS-4	4.00	4,45	-	-	-	•	-	-	NO RE	COVE	RY.	-	-			8
SS-5	5.00	5,45	SM	-	-	•	-	21		-	•	•	-		- 1.84	23
SS-6	6.00	6,45	SC	-	-	-	-	-		-	-	-	-			18
SS-7	7.00	7.45	SM-SC	91	71	27	17	15	1	7	11	6	0.67	2,69	8 2.02	5
SS-8	8.00	8,45	PT	-	-	•	-	22		-	-	-	-		- , -	50/15ca
SS-9	9.00	9.45	SP-SM	-	-	-	-	-		-	-	-	-			49
SS-10	10.00	10.45	SP-SM	100	100	94	8	25		-	-	-	-	2.69	2 1.94	27
SS-11	11.00	11.45	SP-SM	-	-	•	-	-		-	•	-	-			35
SS-12	12.00	12.45	SP-SH	-	-	-	-	-		-	•	-	-			45
SS-13	13.00	13,45	SP-SM	-	-	•	-	23		-	-	-	-		- 1.71	50/28ca
SS-14	14.00	14.45	SP-SH	-	_	-	•	-	NO RE	COVE	RY	-	-			36
SS-15	15.00	15.45	SP-SH	100	98	62	7	20		-	-	-	-	2.70	8 1.81	50/20
SS-16	16.00	16.45	SP-SM	-	-	-	-	-		-	-	-	-		-	64
SS-17	17.00	17.45	SC	-	-	-	_	-		-	-	-	-			40
SS-18	18.00	18.45	SM	100	99	38	24	16		-	-	-	-	2.69	5 2.09	50/20ca
55-19	19.00	19.45	79	-	-	-	-	30		-	-	-	-			50/10cm
55-20	20.00	20.45	SM	-	-	-	•	17		-	-	-	-		- 2.12	50/28cm

FILE : 0502-3

SUMMARY PROJECT LOCATIO	:	05.03	: LAM		PHLOEN HAKHO		CHASIMA		(m) : EL.(m): PTH (m):	-5.50		~		MADE BY DATE CHECKED DATE	:	HARONG P. 20/2/89 HITOON S. 20/2/89	****
SAMPLE	DED.	TH (a)	uso	ı\$		RADAT SSING	ION SIEVE)		NATURAL WATER			AG LI Indi	HITS (CTES	3)	SP.GR	TOTAL	SPT-N
NO.	-++^*		GRO						-CONTENT						Gs	WEIGHT	5 , , , ,
	FROM	Ţ)		#4	#10	#40		(\$)		•	PL	PI	LÏ	-	(t/cu.m)	
SS-1	1.00	1.4	5	CL	_			*	12			-	-	*		*	8
\$\$-2	2.00	2.4	5	CL	100	100	100	62	12	-	•	-	-	•	-	-	9
SS-3	3,00	3.4	5	CL	100	100	100	67	15	25	,	11	14	0.29	2.721	2.07	9
SS-4	4.00	4.4	5	CL	-	-	**	•	19		•	-	-	**	-	•	3
SS-5	5.00	5.4	5	SÇ	-	-		•	18		•	-	-	*	-	-	4
55-6	6.00	6.4	5	SC.	100	100	96	40			5	10	15	0.53	2.711	2.04	5
55-7	7.00	7.4	5	SM	-	-	•	-	19		-	•	•	•	-	•	17
SS-8	8.00			SC	-	•		-			•	-	-	*	-	-	31
55-9	9.00	9.4	5 SP-		96	62	17	3	_		•	-	•	•	2.687	1.85	17
SS-10	10.00			SÇ	-	•			1.		-	-	•	***	-	•	20
SS-11	11.00	11.4	5	SH	100	98	1 82	24			-	•	•	**	-	•	23
SS-12	12.00	12.4	5	CL	-	•			٠.	?	-	-	•	*	-	-	22
	13.00		5	CL	100	100	99	94		-	7	15	22	0.23	2.731	2.05	27
55-14	14.00			CL	-	•	. "	•	••		-	•	-	•	-	-	18
SS-15	15.00			CL	-	•	• •	• •	17		-	•	•	-	-	-	20
55-16	16.00			/CL	-	•			16		-	-	•	*	-	•	24
SS-17	17.00		-	/CL	-	•		•			-	-	**	-	-	•	25
SS-18	18.00			/CL	99	98	3 90) 46			5	15	10	0.1	2.696	2.04	21
\$5-19	19.00			/CL	-	•	•		•-		<u>-</u>						25
SS-20	20.00			CL	96	89	9 8	1 62			0	17	23	-0.17	2.701	2.21	50/25ca
55-21	21.00			CL	•	•	•		. 14	•	<u>.</u>	•	-	•	-	•	50/23cm
\$\$-22	22.00	22.0	3	SH	-	•	•		•	- NO RE	COVER	(Y	**	-	-	•	50/3cm

FILE: 0503-1

28

28

1.99

1.99

SUMMARY PROJECT LOCATIO)5.03 :	JLTS : Lan Phr Inong Cha			CHASINA		(m) ; EL.(m);				MADE BY DATE CHECKED DATE	:	NARONG P. 20/2/89 WITCON S. 20/2/89	
SAMPLE NO.	DEPTH	(a)	USCS GROUP -	(%	GRADATI Passing	SIEVE)		NATURAL WATER CONTENT		ERBERG LI AND INDI	CIES		SP.GR Gs		SPI-N
	FROM	TO		\$4	910	#40	¥200	(\$)	LL	PL	PI	LI		(t/cu.m)	
SS-1	1.00	1.45	CL	100	99	97	61	30	-	-	-	-	-	_	 6
SS-2	2.00	2.45	CL	100	99	78	63	25	-	•	-	•	2.712	2.05	10
SS-3	3.00	3.45	CL	-	-	-	•	•	-	-	-	-	٠.	-	16
SS-4	4.00	4.45	SC	100	100	86	40	20	-	•	-	-	2.705	2.15	11
SS-5	5.00	5.45	SM	-		-	•	-	•	•	-	-	•	-	17
SS-6	6.00	6.45	CL	100	100	99	86	23	-	•	-	- '	•	2.02	20
SS-7	7.00	7.45	CL	-	-	-	_	-	-	-	-	-	-	-	31
SS-8	8.00	8.45	CL	-	-	•	-	-	-	•	-	-	-	-	20
SS-9	9.00	9.45	CL	-	-	-	-	21	-	•	-	-	2.722	2.11	16
55-10	10.00	10.45	CL	-	-	-	-	-	-	-	-	-	-	-	30
\$S-11	11.00	11.45	SC	-	-	•	-	-	-	•	-	-	-	•	31
SS-12	12.00	12.45	SC	100	99	92	43	17	-	•	-	•	-	2.09	45
SS-13	13.00	13.45	CL	-	-	-	-	-	-	-	-	-	-		30
SS-14	14.00	14.45	CL	-	-	-	-	19	-	-	-	-	2.699	2.08	26

22

28

FILE : 0503-2

SS-15 15.00 15.45

SS-16 16.00 16.45 SC/CL SS-17 17.00 17.45 CL SS-18 18.00 18.05 SM

CL

99

98

SUNMARY OF TEST RESULTS

BORING NO. : BH-3

DEPTH (m) : 20.22

DATE : 20/2/89

PROJECT : 05.03 : LAM PHRA PHLOENG GROUND EL.(m): 94.4

LOCATIOH : A.PAK THONG CHAI, NAKHON RATCHASIMA GWL DEPTH (m): -5.50

DATE : 20/2/89

SAMPLE NO.	DEPTI	i (a)	USCS GROUP -	(\$	GRADATI PASSIHG			NATURAL WATER CONTENT		BERG LI ND IHDI		\$)	SP.GR Gs	TOTAL UNIT WEIGHT	SPT-N
1104	FROM	10	4,00	24	110	#40	1200	(4)	LL	PL	PΙ	LI		(t/cu.p)	
55-1	1.00	1.45	CL	•	•		-	17	-	•	•	•	-		8
SS-2	2.00	2.45	CL	100	99	98	87	17	44	21	23	-0.17	2.712	1.69	9
SS-3	3.00	3.45	CL	100	100	92	59	15	-	-	•	-	-	-	9
SS-4	4.00	4.45	CT	-	-	-	-	26	-	-	-	-	-	*	3
\$\$-5	5.00	5.45	CL	-	-	-	-	19	49	21	28	-0.07	2.694	2.02	4
55-6	6.00	6.45	ÇL	•	-	-	•	18	-	-	-	-	-	***	5
SS-7	7.00	7.45	CL	-	-	-	-	22	-	-	•	•	-	•	17
SS-8	8.00	8.45	CL	100	97	77	62	23	49	20	29	0.1	2.696	1.92	31
SS-9	9.00	9.45	CL	•	· -	*	-	28	-	-	-	-	-	•	17
SS-10	10.00	10.45	SC	99	92	48	23	13	-	-	•	-	2.686	•	20
SS-11	11.00	11.45	CL	-	-	•	-	20	-	•	-	-	•	•	23
SS-12	12.00	12.45	CL	•	-	-	-	19	26	14	12	0.42	-	2.14	22
SS-13	13.00	13.45	£L	-	-	•	•	20	•	-	-	•	-	•	27
SS-14	14.00	14.45	SC	-	-	•	-	15	•	-	-	•	-	•	18
SS-15	15.00	15.45	SC	100	99	92	13	16	-	-	-	-	2.71	2.11	20
SS-16	16.00	16.45	SC	-	-	-	-	19	-	-	-	-	-	**	24
\$\$-17	17.00	17.45	CL	100	100	99	59	19	•	•	•	•	-	2.01	25
SS-18	18.00	18.45	5C	-	-	•	-	16	-	-	-	-	-	•	21
SS-19	19.00	19.45	SC	100	100	97	41	16	-	-	-	•	2.721	-	25
SS-20	20.00	20.22	SC	•		•	•	17	*	•	-	-	_		50/23cm

FILE: 0503-3

		ST RESU 11.01 L A. MUAN		I NAKHO	N		BORING (DEPTX (GROUND GNL DEP	m) : EL.(m): TH (m):	14.05			MADE BY DATE CHECKED DATE	8Y :	NARONG P. 23/2/89 WITOON S. 23/2/89	
			USCS GROUP -			IEVE)				ERBERG LII AND INDIO	CIES			HEIGHT	SPT-j
	FAOM	TO.		14	#10	#40	1200	(\$)	LL	PL	PI	LI		(t/cu.a)	
SS-1	1.00	1.45	SH	*		•	*	-		**	•	•	•	•	li
SS-2	2.00	2.45	SH	100	100	99	46	14	-	-	-	-	2.672	1.86	H
SS-3	3.00	3.45	CL	•	-	-	•	-	•		•	•	•	-	1
SS-4	4,00	4.45	CL	100	100	98	55	19	**	•	-	•	2.683	2.17	2
SS-5	5.00	5.45	CL	-	•	-	•	•	***		-	•			ţ
55-6	6.00	6.45	CL	•	•	•	٠.	23	•		•	•	•	2.03	1
55-7	7.00	7.45	SH	•	•	-	•	-		•	•	•	-	-	5
8-22	8.00	8,45	SH	•	•	-	•	-		•	•	•	-	-	13
SS-9	9.00	9.45	SM	99	96	87	29	18	***	•	•	•	2.694	2.05	1
SS-10	10.00		SC	•	-	•	•	-	*	•	-	•	-	•	2(
55-11	11.00	11.37	CL	•	-	-	•	•		•	•	•	-	-	50/230
SS-12	12.00	12.15	C£	•	•	•	-	17	-	•	•	•	2.710	1.75	50/150
SS-13	13.00	13,10	CL	•	*	*	-	-		•	•	*	•	-	50/10a
													_	_	50/50
SS-14			CL	- 				-						_	20, 20,
SS-14 FILE : SUMMARY	1101-:	EST RESU	JLTS LAM HAM		- -		GROUND	(a) : EL.(a):	95.0		-	MADE BY DATE CHECKED DATE	:	NAROHG P. 23/2/89 WITOON S. 23/2/89	
SS-14 FILE : SUMMARY PROJECT LOCATIO	1101-	EST RESU	JLTS LAM NAM AG, SAKD USCS	H NAKHI	ON GRADATIO PASSING	 JN	DEPTH GROUND GHL DEI	(a) : EL.(a): PTH (a): HATURAL WATER	9.03 95.0 0.00 AT			DATE CHECKED DATE	: BY : 	23/2/89 NITODN S. 23/2/89 TOTAL UNIT	
SS-14 FILE : SUMMARY PROJECT	1101-	EST RESU 11.01 I A. HUAH TH (m)	JLTS AM HAM AG, SAXD	H NAKHI	GRADATIO PASSING :	 JN	DEPTH (GROUND GNL DE	(a) : EL.(a): PTH (a): HATURAL NATER CONTENT	9.03 95.0 0.00 AT	TERBERG LI AND INDI	CIES	DATE CHECKED DATE (%)	: BY : 	23/2/89 WITODN S. 23/2/89 TOTAL UNIT	
SS-14 FILE : SUMMARY PROJECT LOCATIO	OF TOP	EST RESU 11.01 1 A. MUAN TH (m)	JLTS LAM HAM AG, SAKO USCS - GROUP	HAAN H	GRADATIO PASSING :	JH SIEVE)	DEPTH (GROUND GNL DE	(a) : EL.(a): PTH (a): HATURAL WATER	9.03 95.0 0.00 AT	TERBERG LI AND INDI		DATE CHECKED DATE (%)	: BY : 	23/2/89 NITODN S. 23/2/89 TOTAL UNIT	SPI
SS-14 FILE : SUMMARY PROJECT LOCATIO SAMPLE NO.	1101-	EST RESU 11.01 1 A. MUAN TH (m) TO	JLTS AM HAM AG, SAKO USCS - GROUP	1 NAKHI	GRADATIO	ON SIEVE)	DEPTH GROUND GWL DE	(a) : EL.(a): PTH (a): HATURAL WATER CONTENT (1)	9.03 95.0 0.00 AT	TERBERG LI AND INDI	CIES	DATE CHECKED DATE (%)	SP.GR	23/2/89 HITODN S. 23/2/89 TOTAL UNIT HEIGHT (t/cu.m)	SPI
SS-14 FILE : SUMMARY PROJECT LOCATIO SAMPLE NO. SS-1 SS-2	0F TO TO TO THE TOTAL TO THE TO	11.01 1 A. HUAN TH (m) 10.45 2.45	JLTS AM HAM HAG, SAXD USCS - GROUP SC SP-SM	14 44 98	GRADATIO PASSING : 110	140 67	DEPTH GROUND GWL DEI	(a) : EL.(a): PTH (a): NATURAL NATER -CONTENT (1)	9.03 95.0 0.00 AT	TERBERG LI AND INDI	CIES	DATE CHECKED DATE (%)	SP.GR	23/2/89 HITODN S. 23/2/89 TOTAL UNIT HEIGHT (t/cu.m)	SPI
SS-14 FILE: SUMMARY PROJECT LOCATIO SAMPLE NO. SS-1 SS-2 SS-3	0F TON : OEP FROM 1.00 2.00 3.00	11.01 I A. HUAH TH (m) TO 1.45 2.45 3.45	JLTS AM HAM HAG, SAXD USCS - GROUP SC SP-SH SC	1 NAKHI (3 44 98 95	GRADATIO PASSING : 110 95	940 440 67	DEPTH (GROUND GWL DE) #200 -7 33	(a) : EL.(a): PTH (a): NATURAL NATER -CONTENT (1)	9.03 95.0 0.00 AT	TERBERG LI AND INDI	CIES	DATE CHECKED DATE (%)	SP.GR G5	23/2/89 HITODN S. 23/2/89 TOTAL UNIT HEIGHT (t/cu.m) 1.83 2.05	SPI
SS-14 FILE: SUMMARY PROJECT LOCATIO SAMPLE NO. S5-1 SS-2 SS-3 SS-4	0F TON : 0EP FROM 1.00 2.00 3.00 4.00	1 EST RESU 11.01 I A. HUAH TH (m) 1.45 2.45 3.45 4.45	USCS - GROUP SC SP-SM SC SC SC	14 44 98	GRADATIO PASSING : 110	140 67	DEPTH (GROUND GWL DE) #200 -7 33	(a) : EL.(a): PTH (a): NATURAL NATER -CONTENT (1)	9.03 95.0 0.00 AT	TERBERG LI AND INDI	CIES	DATE CHECKED DATE	SP.GR	23/2/89 HITODN S. 23/2/89 TOTAL UNIT HEIGHT (t/cu.m) 1.83 2.05	SPI
SS-14 FILE: SUMMARY PROJECT LOCATIO SAMPLE NO. SS-1 SS-2 SS-3 SS-4 SS-5	0F TON : 0EP FRON 1.00 2.00 3.00 4.00 5.00	1 EST RESU 11.01 I A. HUAH TH (m) 1.45 2.45 3.45 4.45 5.45	USCS - GROUP SC SP-SM SC SC SC CL	1 NAKHI (3 44 98 95	GRADATIO PASSING : 110 95	940 440 67	DEPTH (GROUND GWL DE) #200 -7 33	(a) : EL.(a): PTH (a): NATURAL NATER -CONTENT (1) 21 24	9.03 95.0 0.00	TERBERG LI AND INDI	CIES	DATE CHECKED DATE	SP.GR G5	23/2/89 HITODN S. 23/2/89 TOTAL UNIT HEIGHT (t/cu.m) 1.83 2.05 2.05	SPT
SS-14 FILE: SUMMARY PROJECT LOCATIO SAMPLE NO. SS-1 SS-2 SS-3 SS-4 SS-5 SS-6	0F TON : 0EP FROM 1.00 2.00 3.00 4.00	1 EST RESU 11.01 I A. HUAH TH (m) 1.45 2.45 3.45 4.45	USCS - GROUP SC SP-SM SC SC SC	44 44 98 95	GRADATIC PASSING : #10 95 90 58	940 440 67	DEPTH (GROUND GHL DE) #200 7 33 33	(a) : EL.(a): PTH (a): NATURAL NATER -CONTENT (1)	9.03 95.0 0.00	TERBERG LI AND INDI	CIES	DATE CHECKED DATE	SP.GR GS 2.691 2.694 2.679	23/2/89 MITODN S. 23/2/89 TOTAL UNIT HEIGHT (t/cu.m) 1.83 2.05 2.05	SPT
SS-14 FILE: SUMMARY PROJECT LOCATIO SAMPLE NO. SS-1 SS-2 SS-3 SS-4 SS-5	0F TON : 0EP FRON 1.00 2.00 3.00 4.00 5.00	1 EST RESU 11.01 1 A. HUAN TH (m) 1.45 2.45 3.45 4.45 5.45 6.30	USCS - GROUP SC SP-SM SC SC SC CL	44 44 98 95	GRADATIC PASSING : #10 95 90 58	940 440 67	DEPTH (GROUND GHL DE) #200 7 33 33	(a) : EL.(a): PTH (a): NATURAL NATER -CONTENT (1) 21 24	9.03 95.0 0.00 AT	TERBERG LI AND INDI	CIES	DATE CHECKED DATE	SP.GR GS 2.691 2.694 2.679	23/2/89 HITODN S. 23/2/89 TOTAL UNIT HEIGHT (t/cu.m) 1.83 2.05 2.05	SPI
SS-14 FILE: SUMMARY PROJECT LOCATIO SAMPLE NO. SS-1 SS-2 SS-3 SS-4 SS-5 SS-6	0F TOP TOP TOP TOP TOP TOP TOP TOP TOP TOP	TH (m) 1.45 2.45 3.45 4.45 5.30 7.25	USCS - GROUP SC SP-SM SC CL CL	44 44 98 95	GRADATIC PASSING S #10 95 90 58	940 440 67	DEPTH GROUND GWL DEI	(a) :: EL.(a): PTH (a): NATURAL NATER -CONTENT (%) 21 24 22	9.03 95.0 0.00 AT	TERBERG LI AND INDI	CIES	DATE CHECKED DATE	SP.GR GS 2.691 2.694 2.679	23/2/89 HITODN S. 23/2/89 TOTAL UNIT HEIGHT (t/cu.m) 1.83 2.05 2.05	SPT-

FILE : 1101-2

SUHMARY	OF TES	ST. RESU	LTS		*****		BORING		BH-3		*****	MADE BY	;	NARONG P.	40
							DEPTH (19.05			DATE	:	23/2/89	
PROJEC1			AM NAM K					EL.(n):				CHECKED	BY:	WITOON S.	
LOCATIO)N : /	A. NUAN	G, SAKON	NAKNI	DN.		GWL DE	TH (a):	-3.00			DATE	:	23/2/89	
					GRADAT	 10N	*	HATURAL	 114	ERBERG L	IHITS	(<u>+</u>)		TOTAL	
SAMPLE	DEDTI	H (m)	USCS	12	PASSING			WATER		AND INC		(*)	SP.GR	UNIT	SPT-H
NO.		, (4) 	GROUP -					CONTENT					Gs	WEIGHT	4 1. 11
110.	FROM	TO	3.1.001		#1A	* 40				01	nt	1.7	u5		
	rkun			14	#10	#40	1200	(1)	11	PL	PI	LI	******	(t/cu.m)	
SS-1	1.00	1.45	SH	100	99	98	44	15	-	-	•	-	2.663	1.74	2
SS-2	2.00	2.45	SM	-	-	-	-	•	-	-	*	-	•	•	18
55-3	3.00	3.45	SM	-	-	•	-	19	-	-	-	-	•	**	1
SS-4	4.00	4.45	SH	-	-	~	-	•	-	-	-	-	-	**	12
SS-5	5.00	5.45	SC	99	98	90	36	18	-	-	-	-	2.681	2.14	4
55-6	6.00	6.45	SC	-	-	-	-	•	-	-	-	-	-	•	8
SS-7	7.00	7.45	SC	100	100	97	32	18	-	٠.	-	-	2.669	2.07	10
SS-8	B.00	8.45	CL	-	-	-	-	•	-	-	-	-	-	**	35
55-9	9.00	9.45	ÇL	•		-	-	-	-	-	-	-	-	***	41
SS-10	10.00	10.45	CL	•	-	-	-	30	-	-	•	-	-	1.99	27
SS-11	11.00	11.45	CL	•	-	-	-	-	-		•	-	-	*	34
SS-12	12.00	12.45	CL	-	-	-	-	-	-	-	•	-	-	*	29
55-13	13.00	13.45	CL	•	-	-	-	30	-	. •	-	-	2.692	1.95	18
SS-14	14.00	14.45	CL	_	-	-	•	-	-		•		•	-	20
SS-15	15.00	15.45	CL	-	-	-	•	•	-	•		. -	-		27
SS-16	16.00	16.32	CL	-	-	-	-	21	-		•	· -	-	1.71	50/29cm
\$\$-17	17.00	17.07	CL	-	-	-	-	•	-		•	-	-	•	50/9c⊞
SS-18	18.00	18.10	CL	-	-		· -	16	, .		•	•	-	-	50/10cm
55-19	19.00	19.05	CL	-	-	-	-	-	-			· -	-	-	50/5cm

FILE : 1101-3

SUMMARY PROJECT LOCATIO		14.02 L	ILTS AM HAM PH BUN RUANG,		I THANT		DEPTH (GROUND	NO. : (a) : EL.(a): TX (a):	11.08 96.0			MADE BY DATE CHECKED DATE) BY: ; ; ;	NARONG P 23/2/89 WITOON S 23/2/89	
SAMPLE NO.	DEPTH FROM	i (a) TO	USCS GROUP	(%	GRADATIO PASSING S			NATURAL HATER CONTENT		AND II				UNIT	SPT-X
SS-1	1.00		SC/CL	-	-	-	•	•	-	•	• ·				11
SS-2	2.00	2.45	SC/CL	100	100	99	49	17	23	1	4	9 0.33	2.967	2.06	10
SS-3	3.00	3.45	SM	•	-	-	-	-	-	•	-			•	14
SS-4	4.00	4.45	SM	-	-	-	-	•	-		•		-	•	24
SS-5	5.00	5.45	SM	96	88	70	18	20	-		-	• •	2.681	•	. 1
SS-6	6.00	6.45	CL	-	-	-	-	~	-		-		-	•	19
SS-7	7.00	7.45	SM	100	100	97	18	19	-	, ,	-		2.682		18
SS-8	8.00	8.35	SM	-	•	-	-		-		-		-	-	50/20 cm
SS-9	9.00	9.08	CL	-	-	-	-	13		. ,	-		-	1.95	50/8 ca
SS-10	10.00	10.03	CL	-	-	-	-	-	-		_		_	-	50/3 cm
SS-11	11.00	11.08	CL	-	-	•	-	_			-		·-	. -	50/8 cm

FILE: 1402-1

YRAHHUZ	OF TES	T RESU	LTS			٠	BORING DEPTH		BH-2 6.05				ADE BY ATE		HARONG P. 23/2/89	
PROJECT	: 1	4.02 L	AN NAM P	HUAI			GROUND	EL.(a):	92.85			· Cł	RECKED	8Y :	WITOOH S.	
LOCATIO	N : A	. SI 8	UN RUANG	, UDOI	IKAHT I			PTH (m):				DA	ATE	:	23/2/89	
SAMPLE NO.	DEPTH	(a)	USCS Group -	٤)	GRADAT PASSING			NATURAL WATER			RG LII INDI(HITS (%) CIES)	SP.GR	JATOT TIKU	SPT-H
nu.	FROM	ŢO	GRUUP -	#4	#10	#40		-cohteht (*)	Ll		PL	ΡΙ	LI	G5	WEIGHT (t/cu.m)	
55-1	1.00	1.45	SP-SM	66	42	20	8	10	-		-	-		2.671	-	29
SS-2	2.00	2.45	SP-SH	-	•	-	-	-	-		-	-	-	-	-	20
SS-3	3.00	3.45	SH	82	66	39	12	15		•	•	-	-	2,679	-	9
SS-4	4.00	4,45	SC/CL	100	100	99	48	17	-		-	-	-	2.707	2.09	20
SS-5	5.00	5,20	SH	63	48	26	14	12			-	-	•	-	-	50/20cm
SS-6	6.00	6.05	SM	-	-	-	-	_	HO REC	OVER	Y	_	-	-	•	50/5ca

FILE : 1402-2

PROJEC		4.02 L	LTS AM NAM P UN RUANG									MADE DATE CHEC DATE	: KED BY		NARONG P. 23/2/89 WITDON S. 23/2/89		
SAMPLE NO.		(g)		(\$	GRADATI Passing	SIEVE)		NATURAL WATER CONTENT			LIMITS		SP	.GR Gs	TOTAL UNIT WEIGHT	SPI	'-N
	FROM	10		#4	#10	#40	#200	(\$)	LL	ρ	L P	I	LI		(t/cu.m)		
SS-1	1.00	1.45	CL	100	100	99	70	11	25	1	6	9 -0.	56 2.	709	2.08		22
55-2	2.00	2.45	CL	-	•	•	-	-	-		•	•	-	-	•		26
SS-3	3.00	3.45	ÇL	100	100	99	80	17	•		•	-	- 2.	692	2.05		16
SS-4	4.00	4,45	SH		-	-	•	-	-		-	-	-	-			24
SS-5	5.00	5.45	SM-SC	95	80	52	32	8	19	1	2	7 -0.	57 2.	662	1.85		37
SS-6	6.00	6,45	SM-SC	٠.	-	-	-	-	-		•	-	-	-	•		44
SS-7	7.00	7.40	SM	68	54	34	15	11	-		-	-	-	-	•	50/25	CM
SS-8	8.00	8,45	SM		•	-	-	-	-		-	•	-	•	•	50/15	CIB
SS-9	9.00	9.10	SM	•		-	-	12	-		-	•	- 2,	686	1.9	50/10	CA
SS-10	10.00	10.18	SM		_	-	-	-	-		-	-	-	-	•	50/18	CR

F1LE: 1402-3

SUMMARY PROJECT LOCATIO		5.07 L	.AN SOM	TAR KOBL	CHATHANI		GROUND	NO. : (m) : EL.(m): PTH (m):	98.5	, I			MADE BY DATE CHECKED DATE	:	NARONG P. 25/2/89 NITOON S. 25/2/89	
SAHPLE NO.	DEPTH	(p)	USCS - GROUP	,	GRADATI PASSING	SIEVE)		NATURAL WATER -CONTENT		TTERB!	RG LI INDI		(‡)	SP.GR Gs		SPT-#
114.	FROM	10	unuvi	24	#10	140	1200			LL	PL	PI	LI		(t/cu.m)	
SS-1	1.00	1.45	SH	100	100	99	28	9		-	*	-	*	2.687	1.64	11
SS-2	2,00	2.45	SM	-	-	-	-	-		-	•	-	-	•	-	6
SS-3	3.00	3.45	SH	100	99	96	41	13		-	•	-	-	2.696	1.79	8
SS-4	4.00	4.45	SIL	-	-	-	-	-	HO 1	RECOVE	RY	-	-	-	•	7
SS-5	5.00	5.45	SM	•	-	-	_	-	NO A	LECOVE	RY	•	-	-	-	17
SS-6	6.00	6.45	SC/CL	100	100	99	49	23		-	-	-	-	2.708	2.07	1
SS-7	7.00	7.45	-		-	-	-	+		-	. •	-	-	-		2
SS-8	8.00	8.12		•	-	-	-	14		-	•	-	-	2.723	; -	50/130
55-9	8.12	8.27	SH	-	-	-	-			-	•	-	-	-		50/150

FILE : 1507-1

SUMMARY OF TEST RESULTS PROJECT : 15.07 LAM SON LOCATION : A. DET UDON, UBON RATCHATHANI							GROUND	NO. : (m) : EL.(m): PTH (m):	93.4			***	MADE BY DATE CHECKED E DATE			NARONGÉP. 25/2/89 HITOON S. 25/2/89	
SAMPLE NO.	DEPTH FROM	(m) TO	USCS GROUP		GRADATI PASSING	SIEVE)			••••	AND	RG LIME INDICE	ES	(\$) LI	_	P.GR Gs	TOTAL UNIT HEIGHT (t/cu.m)	SPT-N
58-1	1.00	1,45	SM	98	95	66	21	22		_	-	•	•	2	.697	1.80	49

FILE : 1507-2

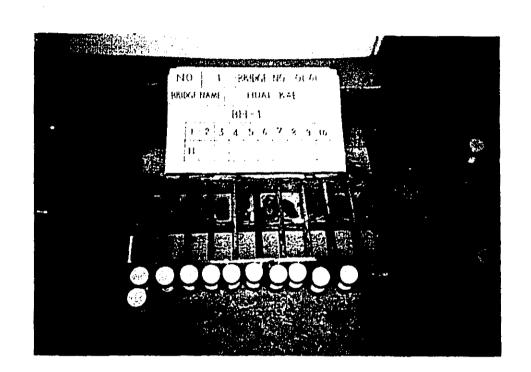
SUMMARY PROJECT LOCATION	: 1	5.07 l	ULTS AM SOH UDOM, UBON	i Ra'	ICHATHANI		GAOUNO	ND. : (m) : EL.(m): PTH (m):	98.4				MADE BY DATE CHECKED DATE	:	NARONG P. 25/2/89 WITOON S. 25/2/89	
SAMPLE NO.	DEPTH Froh	(ø) 70	USCS - Grdup	(%	GRADATIO PASSING S			NATURAL WATER CONTENT			RG LIMI INDICI		(\$) LI	SP.GR Gs	TDTAL UNIT HEIGHT (t/cu.m)	SPT-N
								··	**							
55-1	1.00	1.45	CL	•	-	-	-	15		•	•	-	-	2.736	2.00	9
55-2	2.00	2.45	CL	-	_	-	-	-		•	•	-	-	-	-	12
SS-3	3.00	3.45	CL	•	-	-	-	19		•	•	•	-	-	1.94	59
SS-4	4.00	4.45	CL	•	-	-	-	-		•	•	-	-	-	-	18
SS-5	5.00	5.45	CL	•	-	-	-	13	,	•	-	-	-	2.712	2.12	23
SS-6	6.00	6.45	CL	-	-	-	-	-		•	•	-	-	-	-	7
SS-7	7.00	7,45	SP-SH	100	98	98	9	22	!	-	•	-	_	2.693	1.75	9
55-8	8.00		SP-SH	100	100	97	10	19)	-	-	-	-	_	1.63	50/17cm
55-9	9.00	9.08	SH			-	-	16	•	•	•	-	-	-	*	50/8cm

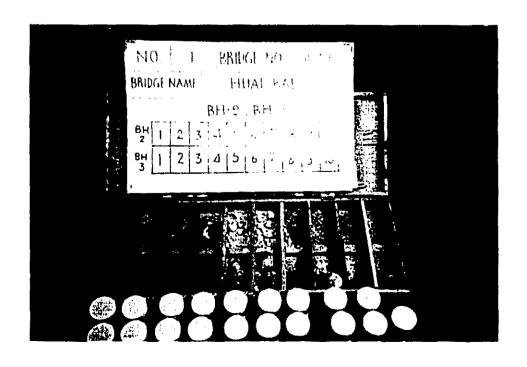
FILE: 1507-3

APPENDIX D

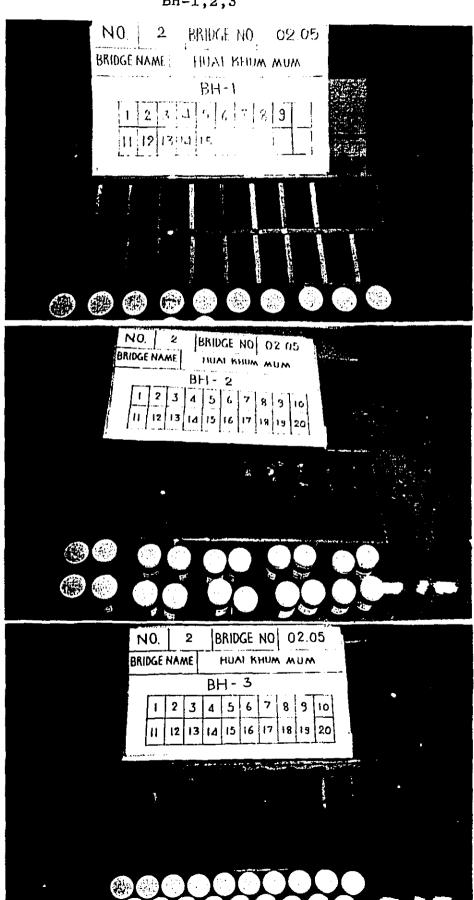
PHOTOGRAPHS OF COREBOX SAMPLES

(1) Bridge No.01.01
Bridge Name HUAI KAE
BH-1,2,3



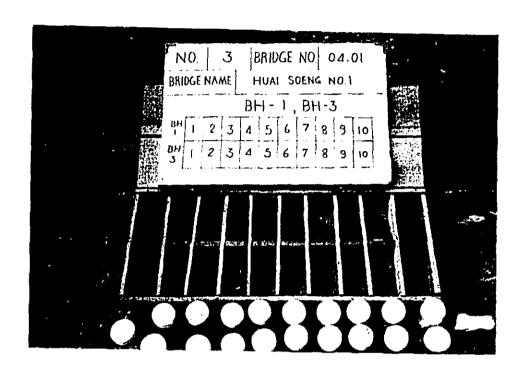


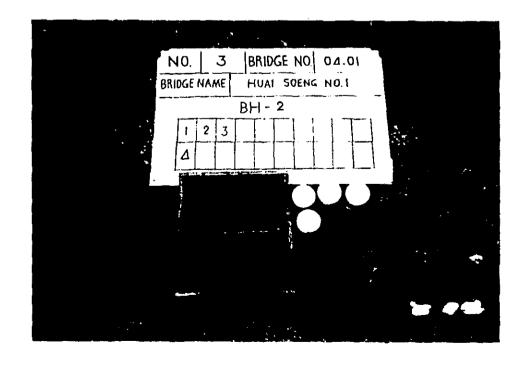
(2) Bridge No.02.05 Bridge Name HUAI KHUM MUM BH-1,2,3



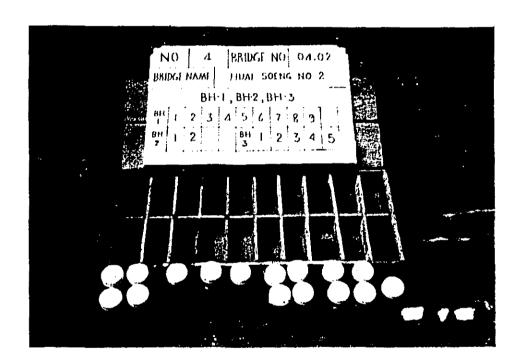
÷

(3) Bridge No.04.01
Bridge Name HUAI SOENG NO.1
BH-1,2,3

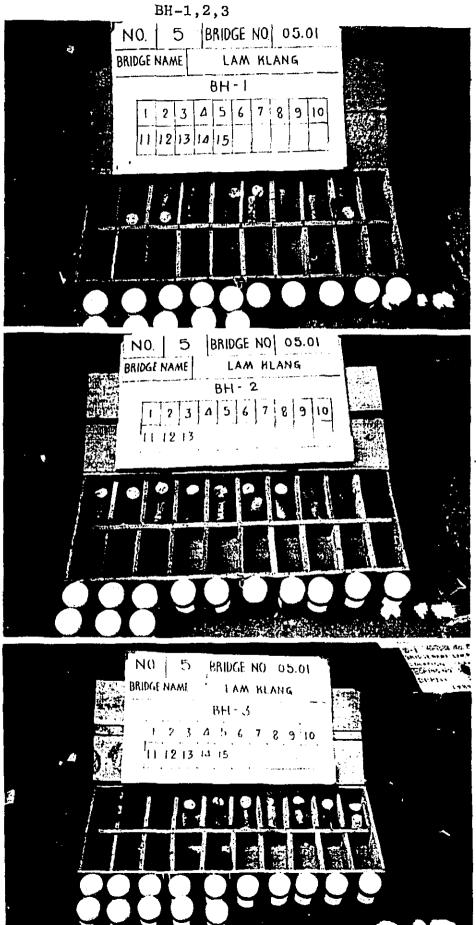




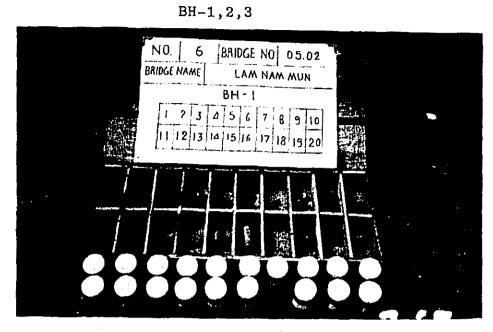
(4) Bridge No.04.02
Bridge Name HUAI SOENG NO.2
BH-1,2,3

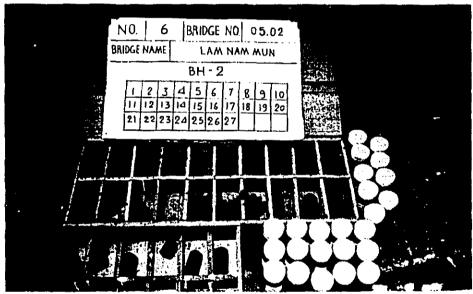


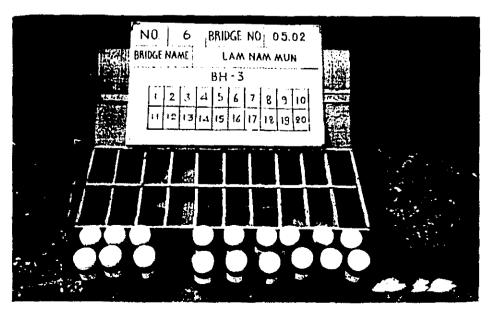
(5) Bridge No.05.01 Bridge Name LAM KLANG



(6) Bridge No.05.02
Bridge Name LAM NAM MUN



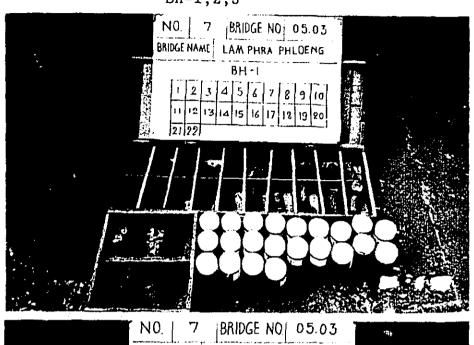




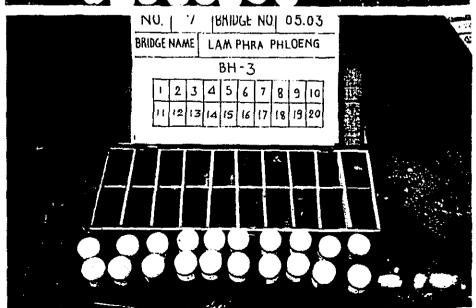
(7) Bridge No.05.03

Bridge Name LAM PHRA PHLOENG

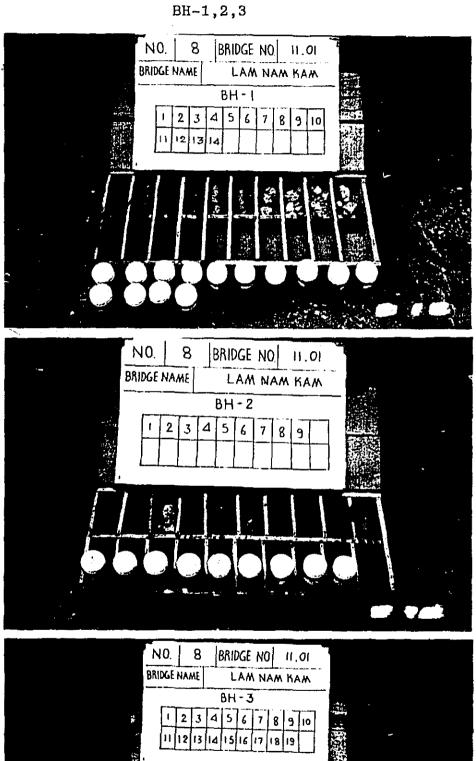
BH-1,2,3



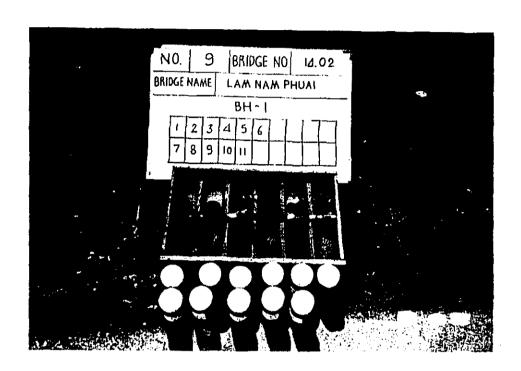


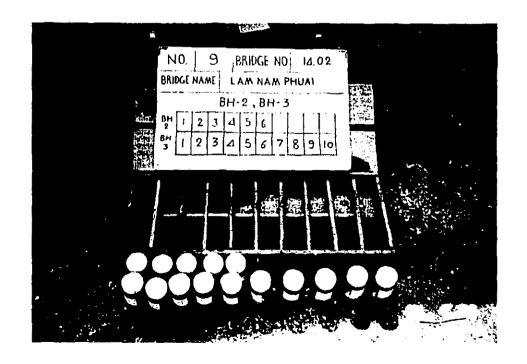


(8) Bridge No.11.01
Bridge Name LAM NAM KAM



(9) Bridge No.14.02
Bridge Name LAM NAM PHUAI
BH-1,2,3

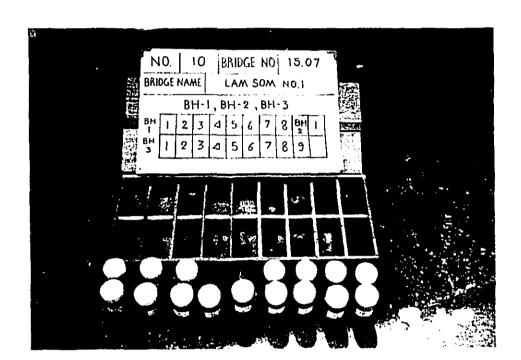




(10) Bridge No.15.07

Bridge Name LAM SOM NO.1

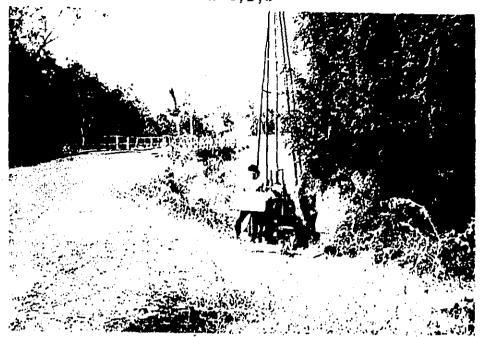
BH-1,2,3





PHOTOGRAPHS OF DRILLING OPERATIONS

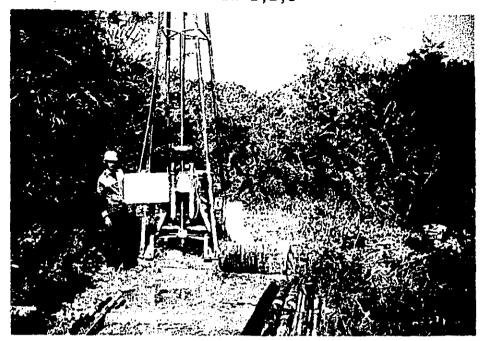
(1) Bridge No.01.01
Bridge Name HUAI KAE
BH-1,2,3

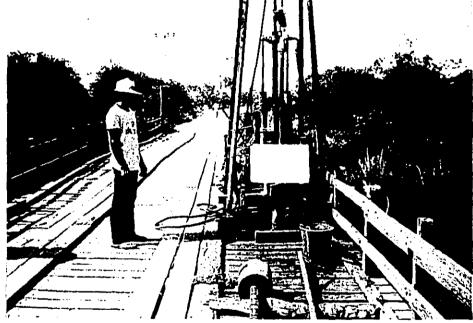


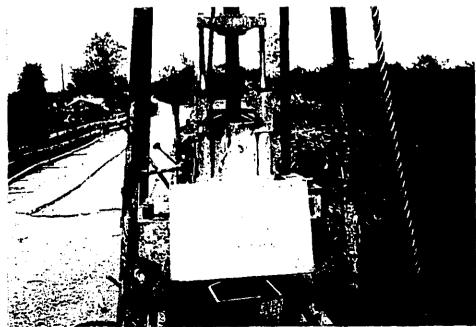




(2) Bridge No.02.05
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(3) Bridge No.04.01
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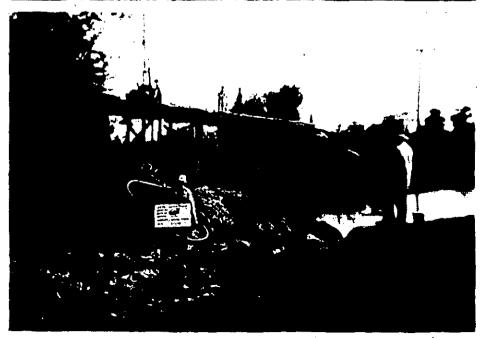




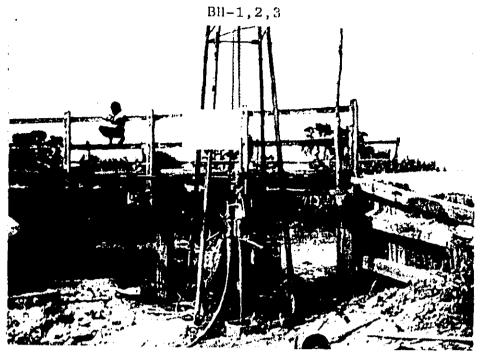
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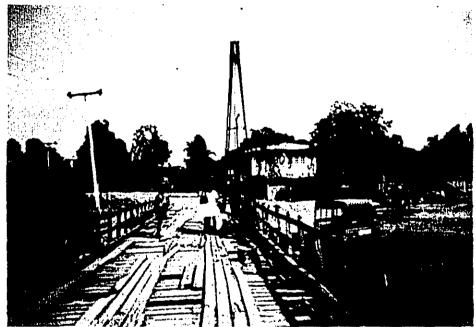


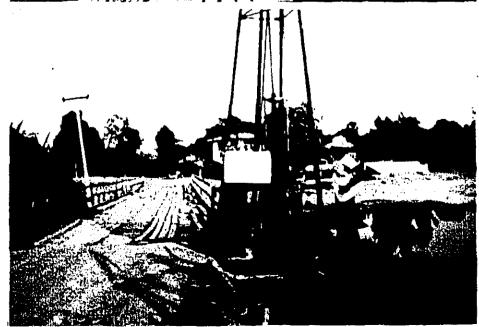




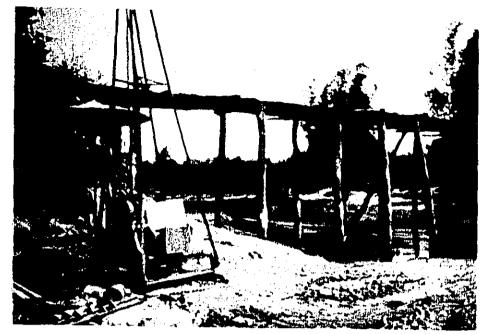
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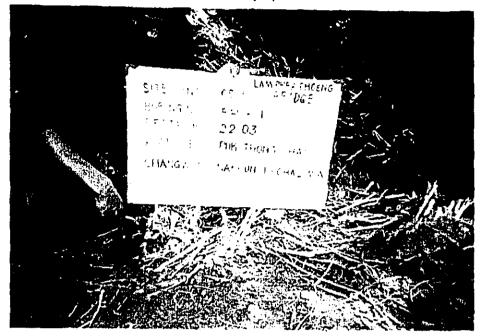
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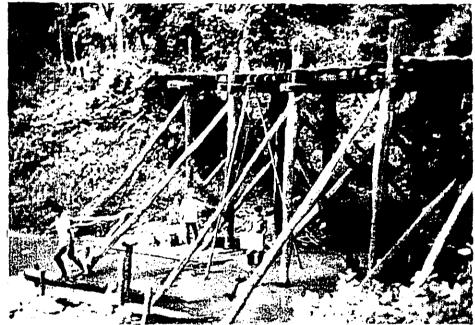


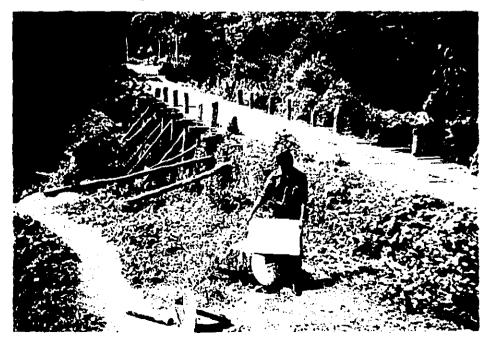




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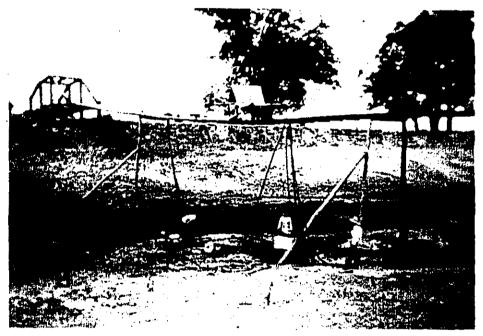


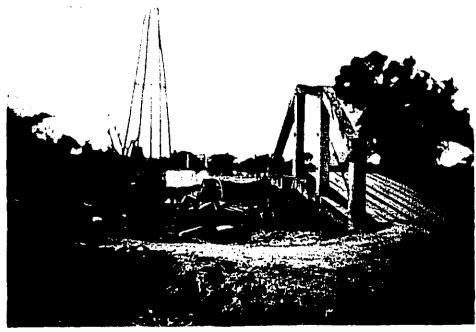




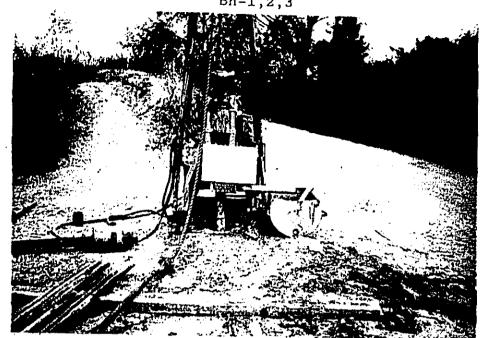
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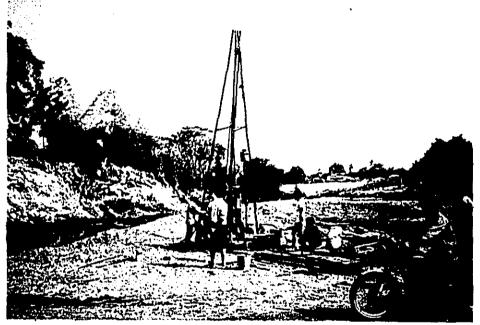






(9) Bridge No.14.02
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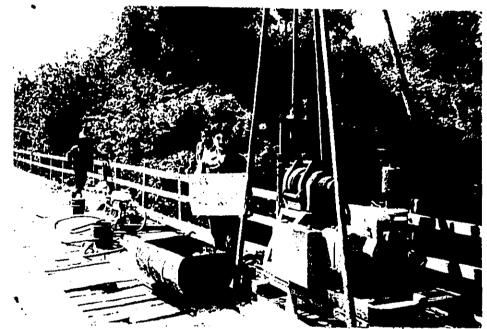






(10) Bridge No.15.07 Bridge Name LAM SOM NO.1







APPENDIX F

REVIEW OF THE CONTINENTAL MESOZOIC STRATIGRAPHY OF THAILAND

WORKSHOP ON STRATIGRAPHIC CORRELATION OF THAILAND AND MALAYSIA

Haad Yai, Thailand 8-10 September, 1983

REVIEW OF THE CONTINENTAL MESOZOIC STRATIGRAPHY OF THAILAND

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INTRODUCTION

The continental Mesozoic redbeds are widely distributed throughout the buntry, especially in the Khorat Plateau, from which the group's name was btained. The rocks are predominantly red clastic, i.e., sandstone, silttone, claystone, shale and conglomerate. The Khorat Group rests unconformably on older rocks, generally of Paleozoic age, but occasionally it verlies the Permo-Triassic igneous rocks and/or Lower to Middle Triassic edimentary rocks.

The Khorat Group was previously reviewed in Thai by Nakornsri (1975) and in English by Kulasing (1975) and Ramingwong (1978). This paper is an attempt to update the knowledge so far reported about the Khorat rocks and their equivalents.

REVIEW OF PREVIOUS WORKS

Lee (1923) was the first geologist who noted the non-marine Mesozoic tocks in the Khorat Plateau and divided them into Upper and Lower Group, the Triassic age was given.

Brown et al. (1953) named the Khorat Series to represent the continental redbeds and the marine Triassic limestone of northern Thailand. The sequence consists of interbedded sandstone, conglomerate, shale and early limestone. No fossil was found except some petrified wood.

La Moreaux et al. (1956) divided the Khorat Series, following Chalithan and Bunnag (1954), into three members and assigned the age of this sequence to the Triassic period. Their subdivision are as follows:

Phu Kradung Member is the oldest member it lies unconformably on Faleozoic rocks. The lowest part began with the basal conglomerate and was subsequently overlain by massive purple shale with minor sandstone.

From the Phu Kradung Formation: the lower jaw of the new crocodile species, Sunosuchus thailandicus (Buffetaut and Ingavat, 1980).

From the Huai Hin Lat Formation: Cyclotosaurus of posthwmus Frass (Ingavat and Janvier, 1981), Ceratodus of szechuanensis (Dipnoi) (Martin and Ingavat, 1982), aquatic chelonian gen. et sp. indet. (Broin et al.), Phytosaur (Buffetaut and Ingavat, 1982).

SUMMARY

The continental Mesozoic rocks in Thailand can be divided provincially into the Khorat-Phayao basin and other small separated basins (Bunopas, 1978, Pitakpaivan and Chonglukmani, 1978). The Khorat-Phayao basin is part of the huge basin, so-called "Indochina basin". It is believed that this basin covered the areas of the eastern part of northern Thailand, the eastern Thailand, the northern part of Campuchea, the northeastern Thailand and can be traced across the border to Laos and probably to southern China. The basin is roughly trending NW-SE direction. Thus, the source rocks are the Chieng Saen massif, the Khun Tan granite, the concealed igneous rocks in the central plain, the Chon Buri massif, the Pailin massif in Campuchea, the Kontum, Rao Co and Song Ma massif in Viet Nam. The basin is probably connected to the Lampang sea by the NW end and/or probably to another sea in Campuchea. The thickness variation of the Nam Phong and Phu Kradung Formation shows that the basin center is more or less parallel to the line between Khon Kaen and Maha Sarakham. Lower to Middle Triassic Sediments.

Lower to Middle Triassic Sediments

The Indosinian orogeny uplifted the Permian basin. Compressional forces caused the Permian series to be folded and faulted. The continental Mesozoic sediments started to accumulate since the Scythian in some area in the north, contemporaneously with the beginning of the Marine Triassic Lampang Group (Hahn and Sieberhuner, 1982).

From the field observation in the northeastern and north-central Thailand, e.g. at Phu Hin Kong, Chum Phae, just west of the Huai Hin Lat type locality, the redbeds start with basal conglomerate containing pebbles of limestone. Overlying the redbeds is the interbedded sequence of reddish brown conglomerate and sandstone with an intercalation of volcanic rocks at the upper part. Subsequently, conglomerate beds with pebbles of volcanic rocks are encountered again. The sequence is followed by the black shale of the Huai Hin Lat Formation.

The section along the Pitsanulok-Lom Sak Highway and its vicinity starts with the basal conglomerate that rests unconformably on the Permain limestone. The sequence is followed by predominant gray beds, but redbeds wer observed locally. After that the pyroclastic rocks appear. Redbeds are found again in the upper part showing an intercalation with the volcanic rocks. The true redbeds belonging to the Khorat Group overlies this sequence with an inferred contact. The correlation between these two strata above both conglomerate beds is inferred, but, possibly they are equivalent.

The difference in natures of folding was found in these two sequences, together with the presence of igneous dikes in the lower unit, and, in addition, the Permian limestone was found as a thrusted sheet above the volcanic rocks. The latter two criteria are not seen in the nearby Khorat Group. The data suggest possibly an unconformity. The environment of deposition is considered to be a fluvio-lacustrine type. Unidentified bone fragments and fossil plants are found. The age of the unit is Middle Triassic (Maranate, in print) and probably a continuation from the Lower Triassic. These continental sediments occurred in the north-central and northeastern part of the country while in the western and northern part marine deposits were found. By the reasons already mentioned, the new rock unit is suggested.

The Huai Hin Lat Formation

After the late stage of the Indonisian orogeny, probably in Carnian, the Huai Hin Lat sediments were deposited in the separated paleo-basins. The contacts with the older Triassic rocks were more or less unconformable. The depositional environment was considered to be a fluvio-lacustrine type. Restricted basins were typical, and the limestone is believed to be a lacustrine deposit (Broin et al. 1982). According to the paleogeography it can be noted that, in some areas, the Huai Hin Lat Formation comprises only redbeds, while in other areas it may contain a minor gray beds. Since the positions of the Norian beds are located in the middle part of the sequence, the base of the Huai Hin Lat Formation are considered to be Carnian (Chonglakmani and Sattayrak, 1978).

The Nam Phong Formation

Just before or when all small-separated basins were filled with the Huai Hin Lat sediments, the Nam Phong Formation started its accumulation. The deposits were transitionally changed into redbeds from the gray beds below. As the matter of fact, the Nam Phong Formation is the lowest formation of the Khorat Group where the Huai Hin Lat is absent, e.g. in the high lands and the basin flanks. It is predominantly reddish brown and resistant sandstone, siltstone and conglomerate. No fossil was found but the age is considered to be between those of the Huai Hin Lat and of the Phu Kradung Formation, i.e., Rhaetian. The fluvio-lacustrine environment was its depositional environment.

The Phu Kradung Formation

Deposition of the Phu Kradung Formation took place when the Indochina basin was a huge basin. This unit rests unconformably on the Pre-Khorat rocks at the basin flanks. Ward and Bunnag (1964) noted the contact between the Nam Phong and Phu Kradung Formation at the limestone alternating zone. The formation is characterized by predominantly claystone in the lower part, and with some massive sandstone intercalation in the middle part, while the upper part consists of massive sandstone interbedded with claystone. The interpreted marine ingression based on the presence of a Plesiosaur tooth at Nong Bua Lam Phu (Ward and Bunnag, 1964) was doubtful due to a recent discovery of the fresh water crocodile bones (Buffetaut and

Ingavat, 1980) probably at the same locality. The fluvio-lacustrine depositional environment is again assigned to the Phu Kradung sediments (Hahn, 1982 a). The claystone represented the flood plain deposits, while sandstone was the channal sand of the meandering streams. The upper sequence characterized a gradually change to the Phra Wihan rocks's environment. The age of this formation is Lower Jurassic (Hayami, 1968, Hahn, 1982 a).

The Phra Wihan Pormation

The formation comprises massive, resistant, light-coloured sandstone with some interbedded siltstone and comglomerate. Pebbly sandstone usually are encountered in the upper part of the section. The sequence reveals a deposition of braided streams. In some areas, it resembles the fluvio-lacustrine deposits (Hahn, 1982 a). The fossils indicated the Upper Triassic to Lower Jurassic age. The age of the formation is considered to be the Middle Jurassic.

The Sao Khua Pormation

This formation is known as the less-resistant, reddish brown-coloured siltstone lying in between the more resistant sandstone. Aside from the marine pelecypods (Ward and Bunnag, 1964, Huhn, 1982 a), Plesiosaur tooth (Hahn, 1982 a) and Icthyosaur tooth (Takai, 1963), other types of fossils and the rock characteristics suggest the continental depositional environment. The age of the Sao Khua Formation is Upper Jurassic.

The Phu Phan Pormation

This formation is characterized by massive beds of light-coloured, pebbly sandstone and conglomerate. The average thickness is about 80 meters, but at Nam Phung Dam site, it is about 400 meters thick. The middle part of the Nam Phung section comprises the redbeds containing Lower Cretaceous pelecypods (Kobayashi, 1968). Paleocurrent measurements in the northern part of the Khorat Plateau was studied by the author. The result suggests the S-SW and/or W current direction which is similar to that of the Phra Wihan Formation. Hahn (1982 a) considered the Phu Phan Formation as a typical fluviatile sediments.

The Khok Kruat Pormation

The redbeds overlying the Phu Phan Formation represent the Khok Kruat Formation. It consists predominantly of sandstone with some siltstone and claystone. The fluviatile environment is suggested and the deposition took place in an arid climate. Gypsum nodules and lenses were observed. The fossil found in its equivalent beds, the Ban Na Yo Formation, points to the Upper Cretaceous age (Kobayashi, 1968).

The Maha Sarakham Formation

This formation is thought to rest unconformably on the underlying Knorat strata (Japakasetr and Workman, in print) thus, raising the problem about its status. This rock unit consists of the Lower, Middle and Upper

Rook Salt with 2 units of claystone in between. The unconformity does not show a strong discordance, thus a disconformity is suggested (Japakasetr and Workman, in print). The depositional basin, is quite similar in shape to that of the older Khorat sediments. The Khorat and Sakon Nakorn basins were the same basin at that time. The age of this formation is inferred as the Upper most Cretaceous.

The Phu Tok Pormation

This informal formation was mapped by Sattayarak and Suthectorn (1979). It consists of two sandstone types, one with very large-scaled crossbedding and the other with small wavy structures. The sandstone was described as a red-coloured, fine-grained, well sorted and friable rock. The gross characteristics of this formation resembled an eclian deposits. The strata are found above the Khok Kruat Formation, but, correlation with the Maha Sarakham Formation is not conclusive. It was probably deposited contemporaneously, but in different environment, with the rock salt. This formation, on the other hand, is possibly younger than the Maha Sarakham Formation as it lies unconformably on the latter.

The Upper Claystone

The sequence consists typically of brick red-coloured olaystone, silt-stone and sandstone with gypsum and anhydrite lenses and/or nodules. This unit rests unconformably on the Maha Sarakham Formation (Japakasetr and Workman, in print). Its age is likely to be Tertiary more than Mesozoic. Furthermore, the sandstone resembled that of the Phu Tok Formation. If this is true, the two units would be of the same age but with a slightly different environment of deposition. This unit cropped out in the central part of the Plateau. It was probably accumulated in two separated basins, the Khorat and Sakon Nakorn basins, alter the Himalayan orogeny built up the Phu Phan anticlinorium.

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REFERENCES

- Asama, K. (1973). Some younger Mesozoic plant from the Lom Sak Formation, Thailand: Geol. Paleont. Southeast Asia, v. 13, p. 39-46.
- Southeast Asia, v. 23, p. 51-64.

- Younger Mesozoic Plants from Trang, Southern Thailand: Geol. Paleont. Southeast Asia, v. 22, p. 35-47.
- Baum, F., Von Braun, E., Hahn, L., Hess, A., Kock, K.E., Kruse, G., Quarch, H. and Siebenhuner, M., et al., 1970. On the geology of northern Thailand: Beih. Geol. Jahrb., Heft 102, p. 1-24.
- Borax, E. and Stewart R.D., 1965. Notes on the Khorat Series of Northeastern Thailand: Rep. Third Symp. Dev. Petrol, Res. Asia, Far East, ECAFE committee, p. 1-25.
- Broin, F.D., Ingavat, R., Janvier, P. and Sattayarak, N., 1982, Triassic turtle remains from Northeastern Thailand: Jour. of Vertebrate Paleontology, V. 2 (1): p. 41-46.
- Brown, G.F., Buravas, S., Charaljavanaphet, J., Jalichandra, N., Johnston, W.D., Sresthaputra, V., and Taylor, G.C., 1951, Geological reconnaissance of mineral deposits of Thailand: U.S. Geol. Surv. Bull. 984; Geol. Surv. Mem. 1, Roy. Dept. Mines, Bangkok, Thailand, (1953), 183 p.
- Buffetaut, E. and Ingavat, R., (1980), A new crocodilian from the Jurassic of Thailand and the paleogeographical position of Southeast Asia in the Mesozoic, 3 p.
- Bunopas, S., 1971, On the geology and stratigraphy of the Nam Phrom Dam and its vicinities: Geological Society of Thailand, Newsletter 4 (1-3), p. 17-40.
- , 1976, Geology of Amphoe Bo Phloi, North Kancharaburi with Special Notes on the "Kanchanaburi Series": Jour. Geol. Soc. Thailand. Vol. 1, no. 1-2, p. 51-67.
- , Nakanat, A., and Bunjitradul, S., 1970, Stratigraphy and structure of the Khorat rocks along Phitsanulok-Lom Sak Highway: Min. Res. Gazette, v. 15, no. 7, p. 9-20.
- Chonglakmani, C., and Sattayarak, N., 1978, Stratigraphy of the Huai Hin Lat Formation (Upper Triassic) in northern Thailand: Praceedings of the third Regional Conference on the Geology and Mineral Resources of Southeast Asia, Nutalaya, P. (ed.), Bangkok, p. 739-762, 35 figs.
- Endo, S., and Fujiyama, I., 1965, Some late Mesozoic and late Tertiary plant and a fossil insect from Thailand: Geol. and Palaeont. Southeast Asia, Tokyo Univ. Press, v. 2, p. 301-307.
- Gardner, L.S., Howarth, H.F., and Na Chaingmai, P., 1967, Salt resources of Thailand: Thai Dept. Mineral Resources, Rept. Invest. 11, 100 p.
- Garson, M.S., Young, B., Mitchell, A.H.G. and Tait, B.A.R., 1975, The geology of the tin belt in peninsular Thailand around Phuket, Phangnga and Takua Pa: Inst. Geol. Overseas Memoir no. 1, 112 p.

- Hahn, L., 1976, The stratigraphy and palaeogeography of the non-marine Mesozoic deposits in northern Thailand: Geol. Jahr., Reihe B., Heft 21 p. 155-169.
- , 1982. Stratigraphy and marine ingressions of the Mesozoic Khorat Group in Northeastern Thailand: Geol. Jb., B 43, p. 1-28.
- , 1982, The Triassic in Thailand: Sonderdruck aus der Geologischen Rundschau, B. 71, Heft 3, p. 1041-1056.
- of Northern and Western Thailand: Bundesant. Geowies. Rohst.. p.
- Haile, N.S., 1973, Note on Triassic fossil pollen from the Nam Pha Formation, Chulaporn (Nam Phrom), Thailand. Geol. Soc. Thailand Newsl., v. 6, no. 1, p. 15-16.
- Haworth, H.F., Na Chiangmai, P. and Phiancharoen, C., 1966, Ground water resources development of northeastern Thailand: Thai Dept. of Mineral Resources, Ground water Bulletin No. 2, 1252 p.
- Hayami, I., 1960, Two Jurassic pelecypods from west Thailand: Trans Proc. Palaeont. Soc. Japan, n. ser., no 38, p. 284.
- , 1968, Some non-marine bivalves from teh Mesozoic Khorat Group of Thailand: Geol. and Palaeont. Southeast Asia, Tokyo Univ. Press, v. 4, p. 100-108.
- Hinthong, C., 1974, Notes on the geology of the Khao Yai national park and its vicinity: Geol. Soc. Thailand Newsl., v. 7, no. 1. p. 3-10.
- Hite, R.J., Potential for potash and related mineral resources, Khorat Plateau, Northeast Thailand and Central Laos, translated to Thai by Suwanayon, P., 1975, Mineral Resources Gazette, v. 20, p. 10-44.
- Ingavat, R. and Taquet, P., 1978, First discovery of dinosaur remain in Thailand: Geology and mineral resources of Thailand, v. 3, no. 1, p. SP1, 1-6.
- Ingavat, R. and Janvier, P. 1981, Cyclotosaurus of. post-humus Fraas (Capitosauridae, Stereospondyli) from the Huai Hin Lat Formation (Norian, Upper Triassic) of northeastern Thailand, with a note on capitosaurid phylogeny and biogeography: Geobios 14(6): p. 711-723.
- Inthuputi, B. and Suwanasing, A., 1978, Sandstone-type uranium deposits Khorat Plateau, Northeastern Thailand: Geology and mineral resources of Thailand, v. 3, no. 1, p. E2, 1-16.
- Iwai, J., 1968, The sedimentary structures observed in rocks of the Khorat Group and Overlying formation: Geol. and Palaeont. Southeast Asia, Tokyo Univ. Press, v. 5, p. 166-172.

- , 1972, Pelletal limestone of the Phu Kadung formation, Mesozoic Khorat Group, Thailand: Geol. and Palaeont. Southeast Asia, Tokyo Univ. Press, v. 10, p. 257-263.
- , 1973, Dolomitic limestone of the Phu Kadung formation, Mesozoic Khorat Group, Thailand: Geol. and Palaeont. Southeast Asia, Tokyo Univ. Press, v. 12, p. 173-178.
- Iwai, J., Asama, K., Veeraburus, M. and Hongnusonthi, A., 1966, Stratigraphy of the so-called Khorat Series and a note on the fossil plant-bearing Palaeozoic strata in Thailand: Geol. and Palaeont. Southeast Asia, Tokyo Unvi. Press, v. 2, p. 179-196.
- , Sakagami, S., Nakornsri, N. and Yuyen, W., 1968, Mesozoic Stratigraphy of the north-west part of the Khorat Plateau, Thailand: Geol. and Palaeont. Southeast Asia, Tokyo Univ. Press, v. 5, p. 151-165.
- , Hongnusonthi, A., Asama K., Kobayashi, T., Konno, E., Nakornsri, N., Veeraburus, M. and Yuyen, W., 1975, Non-marine Mesozoic formation and fossils in Thailand and Malaysia: Geol. and Palaeont. Southeast Asia, Tokyo Univ. Press, v. 15, p. 191-218.
- Kobayashi, T., 1964 a, Geology of Thailand: Geol. Palaeont. Southeast Asia, v. 1, p. 1-15.
- p. 17-29.
- , 1968, The Cretaceous non-marine pelecypods from the Nam Phung dam site in the northeastern part of the Khorat Plateau, Thailand, with a note on the Trigonioididae: Geol. and Palaeont. Southeast Asia, Tokyo Univ. Press, v. 4, p. 109-138.
- , 1973, The early and middle Paleozoic history of the Burmese-Malayan geosyncline: Geol. and Palaeont. Southeast Asia, Tokyo, Univ. Press, v. 11, p. 93-108.
- Kobayashi, T., 1975, Upper Triassic Estherids in Thailand and the Conchostracan development in Asia in the Mesozoic era: Geol. and Palaeont. Southeast Asia, Tokyo Univ. Press, v. 16, p. 57-90.
- , 1976, Pratya Samutopatham toward Thailand's Palaeontology, four ages of her geological history: Journ. Geol. Soc. Thailand, v. 2, no. 1-2, p. 67-74.
- , 1978, The Jurassic Palaeogeography of Japan and Southeast Asia: Proceedings of the Japan Academy, v. 54, Ser. B, no. 10, p. 583-588.
- , Takai, F. and Hayami, I., 1964, On some Mesozoic fossil from the Khorat Series of east Thailand and note on the Khorat series: Geol. Palaeont, Southeast Asia, v. 1, p. 119-133.

- Kon'no, E. and Asama, K., 1973, Mesozoic plants from Khorat, Thailand: Geoland Palaeont. Southeast Asia, Tokyo Univ. Press, v. 12, p. 149-172.
- Lamoreaux, P.E., Charal-Javanaphet, J.C., Jalichan N., Na Chiangmai P., Bunnag, D., Thavisri, A. and Rakprathum, C., 1959, Reconnaissance of the geology and groundwater of the Khorat Plateau, Thailand: U.S. Geol. Surv., Water supply paper 1429, 62 p.
- Lee, W.M. 1923, Reconnaissance Geological Report of the Khorat Region, Province of Nakhon Rajasima, Udon, Rot Et and Ubon, Siam. Mimeogr. Copy Reproduction.
- Pitakpaivan, K. and Chonglakmani, C., 1978, Thailand continental Mesozoic basins fo Thailand: Stratigraphic correlation between sedimentary basins of the ESCAP region, v. 4, p. 45-49.
- Piyasin, S., 1972, Geology of Changwat Lampang Sheet, scale 1:250,000: Department of Mineral Resources, Rep. Invest., v. 14, 98 p.
- , 1975, Stratigraphy and sedimentology of the Kaeng Krachan Group (Carboniferous): Dept. Geol. Sci. Chiang Mai, Spec. Pub., no. 1, v. 2, p. 25-36.
- , 1982, The new Relation of Lampang Group (Triassic) and Khorat Group (Upper Triassic to Cretaceous): Geol. and Palaeont. Southeast Asia, v. 23, p.
- Ramingwong, T., 1978, A review of the Khorat Group of Thailand: Third regional conference on geology and mineral resources of Southeast Asia, Bangkok, Thailand, p. 763-774.
- Von Braun, E., and Jordan, R., 1976, The stratigraphy and palaeontology of the Mesozoic sequence in the Mae Sot area in western Thailand: Geol. Jahr., Reihe B., Heft 21, p. 5-25.
- Ward, D.E. and Bunnag, D., 1964, Stratigraphy of the Mesozoic Khorat Group in northeastern Thailand: Thai Dept. Mineral Resources, Rept. Invest., 95 p.
- Workman, D.R., 1981, Study of strata in southern Laos equivalent to the Khorat Group of Thailand using satellite imagery: Natural Resources Division, ESCAP, United Naitons, Bangkok, Thailand, p. 1-4.

APPENDIX G

STANDARD PENETRATION TEST
UNIFIED SOIL CLASSIFICATION SYSTEM
LIST OF TERMS USED AND SYMBOLS
REFERENCES

Standard Method for PENETRATION TEST AND SPLIT-BARREL SAMPLING OF SOILS¹

This Standard is issued under the fixed designation D 1386; the number immediately following the designation indicates the year of original adoption or, in the case of revision, the year of last revision. A number in parentheses indicates the year of last reapproval.

This method has been approved for use by agencies of the Department of Defense and for listing in the DoD Index of Specifications and Standards.

1. Scope

1.1 This method describes a procedure for using a split-barrel sampler to obtain representative samples of soil for identification purposes and other laboratory tests, and to obtain a measure of the resistance of the soil to penetration of the sampler.

2. Apparatus

2.1 Drilling Equipment - Any drilling equipment shall be acceptable that provides a reasonably clean hold before insertion of the sampler to ensure-that the penetration test is performed on undisturbed soil, and that will permit the driving of the sampler to obtain the sample and penetration record in accordance with the procedure described in Section 3. To avoid "whips" under the blows of the hammer. it is recommended that the drill rod have a stiffness equal to or greater than the A-rod. An "A" rod is a hollow drill rod or "steel" having an outside diameter of 1% in. (41.2 mm) and an inside diameter of 11 in (28.5 mm), through which the rotary motion of drilling is transferred from the drilling motor to the cutting bit. A stiffer drill rod is suggested for holes deeper than 50 ft (15 m). The hole shall be limited in diameter to between 2% and 6 in. (57.2 and 152 mm),¹

2.2 Split-Barrel Sampler—The sampler shall be constructed with the dimensions indicated in Fig. 1. The drive shoe shall be of hardened steel and shall be replaced or repaired when it becomes dented or distorted. The coupling head shall have four 12-in, (12.7-

mm) (minimum diameter) vent ports and shall contain a ball check valve. If sizes other than the 2-in. (50.8-mm) sampler are permitted, the size shall be conspicuously noted on all penetration records.

2.3 Drive Weight Assembly—The assembly shall consist of a 140-lb (63.5-kg) weight, a driving head, and a guide permitting a free fall of 30 in. (0.76 m). Special precautions shall be taken to ensure that the energy of the falling weight is not reduced by friction between the drive weight and the guides.

2.4 Accessory Equipment—Labels, data sheets, sample jars, paraffin, and other necessary supplies should accompany the sampling equipment.

3. Procedure

3.1 Clear out the hole to sampling elevation using equipment that will ensure that the material to be sampled is not disturbed by the operation. In saturated sands and silts withdraw the drill bit slowly to prevent toosening of the soil around the hole. Maintain the water level in the hole at or above ground water level.

3.2 In no case shall a bottom-discharge bit be permitted. (Side-discharge bits are permissible.) The process of jetting through an opentube sampler and then sampling when the

⁴ This method is under the jurisdiction of ASTM Committee D-18 nn Suil and Rock for Engineering Purposes. Current edition approved Oct, 20, 1967, Originally issued 1958, Replaces D 1586 64 T.

³ Worshey, M. J., Surface Exploration and Sumpling of Soils for Civil Engineering Purposes, The Ingineering Foundation, 345 East 47th St. New York, N. Y. 10017.

D 1586

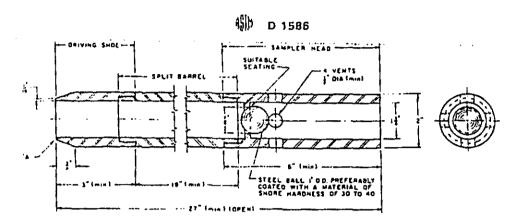
desired depth is reached shall not be permitted. Where easing is used, it may not he driven below sampling elevation. Record any loss of circulation or excess pressure in drilling fluid during advancing of boles.

- 3.3 With the sampler resting on the hottom of the hole, drive the sampler with blows from the 140-th (63.5-kg) hammer falling 30 in. (0.76 m) until either 18 in. (0.45 m) have been penetrated or 100 blows have been applied.
- 3.4 Repeat this operation at intervals not longer than 5 ft (1.5 m) in homogeneous stratu and at every change of stratu.
- 3.5 Record the number of blows required to effect each 6 in. (0.15 m) of penetration or fractions thereof. The first 6 in. (0.15 m) is considered to be a seating drive. The number of blows required for the second and third 6 in. (0.15 m) of penetration added is termed the penetration resistance, N. If the sampler is driven less than 18 in. (0.45 m), the penetration resistance is that for the last 1 ft (0.30 m) of penetrated, the logs shall state the number of blows and the fraction of 1 ft (0.30 m) penetrated).
- 3.6 Bring the sampler to the surface and open. Describe carefully typical samples df soils recovered as to composition, structure, consistency, color, and condition; then put into jars without ramming. Seal them with wax or

hermetically seal to prevent evaporation of the soil moisture. Affix lubels to the jar or make notations on the covers (or both) bearing job designation, boring number, sample number, depth penetration record, and length of recovery. Protect samples against extreme temperature changes.

4. Report

- 4.1 Data obtained in borings shall be recorded in the field and shall include the following:
 - 4.1.1 Name and location of job.
 - 4.1.2 Date of boring-start, finish,
- 4.1.3 Boring number and coordinate, if available,
 - 4.1.4 Surface elevation, if available,
 - 4.1.5 Sample number and depth.
- 4.1.6 Method of advancing sampler, penetration and recovery lengths.
- 4.1.7 Type and size of sampler,
- 4.1.8 Description of soil,
- 4.1.9 Thickness of layer.
- 4.1.10 Depth to water surface; to loss of water; to artesian head; time at which reading was made.
 - 4.1.11 Type and make of machine.
 - 4.1.12 Size of casing, depth of cased hole,
 - 4.1.13 Number of blows per 6 in. (0.15 m),
 - 4.1.14 Names of crewmen, and
 - 4.1.15 Weather, remarks.



Nitts 1-Split burrel may be 152 in, inside diameter provided it contains a liner of 16-gage wall thickness.

Nort. 2—Core retainers in the driving shoe to prevent loss of sample are permitted.

Nort. 3—The corners at A may be slightly rounded.

Metric Equivalents

in.	nin)	in.	mm
%. (16 gage)	1.5-	2	50.8
4	12.7	3	76.2
r.	19.0	6	152.4
%	22.2	18	457.7
X	34.9	27	685.8
18	38.1		

FIG. 1 Standard Split Burrel Sampler Assembly.

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This standard is subject to revision at any time by the responsible technical committee and must be reviewed every five years and if not revised, either reapproved or withdrawn. Your comments are invited either for revision of this standard or for additional standards and should be addressed to ASTM Headquarters. Your comments will receive earful consideration at a meeting of the responsible technical committee, which you may attend. If you feel that your comments have not received o fair hearing you should make your views known to the ASTM Committee an Standards, 1916 Race St., Philadelphia, Pa. 19103, which will schedule a further hearing regarding your comments. Falling satisfaction there, you may appeal to the ASTM Board of Directors.

Standard Test Method for CLASSIFICATION OF SOILS FOR ENGINEERING PURPOSES¹

Description of the designation indicates the year of the fixed designation D 2487; the number immediately following the designation indicates the year of report adoption or, in the case of revision, the year of last revision. A number in parentheses indicates the year of last reapproval, a uperscript epsilon (1) indicates an editorial change since the last revision or reapproval.

1. Scope

1.1 This test method describes a system for dassifying mineral and organo-mineral soils for ingineering purposes based on laboratory determination of particle-size characteristics, liquid amit, and plasticity index and shall be used when precise classification is required.

NOTE 1-Use of this standard will result in a single classification group symbol and group name except when a soil contains 5 to 12 % fines or when the plot of the liquid limit and plasticity index values falls into the crosshatched area of the plasticity chart. In these to cases, a dual symbol is used, for example, GP-GM, CL-ML. When the laboratory test results indicate that the soil is close to another soil classification group, the borderline condition can be indicated with two symbols reparated by a slash. The first symbol should be the one based on this standard, for example, CL/CH, GM/SM. SC/CL. Borderline symbols are particularly useful when the liquid limit value of clayey soils is close to 59. These soils can have expansive characteristics and the use of a borderline symbol (CL/CH, CH/CL) will alert the user of the assigned classifications of expansive potential.

- 1.2 The group symbol portion of this sytem is based on laboratory tests performed on the portion of a soil sample passing the 3-in. (75-mm) sieve (see Specification E 11).
- 1.3 As a classification system, this test method is limited to naturally occurring soils.

NOTE 2-The group names and symbols used in this test method may be used as a descriptive system applied to such materials as shale, claystone, shells, trushed rock, etc. See Appendix X2.

1.4 This test method is for qualitative application only.

NOTE 3-When quantitative information is required for detailed designs of important structures, this test method must be supplemented by laboratory tests or other quantitative data to determine performance characteristics under expected field conditions,

- 1.5 The system is based on the widely recognized Unified Soil Classification System which was adopted by several U.S. Government agencies in 1952 as an outgrowth of the Airfield Classification System developed by A. Casagrande.2
- 1.6 This standard may involve hazardous materials, operations, and equipment. This standard does not purport to address all of the safety problems associated with its use. It is the responsibility of whoever uses this standard to consult and establish appropriate sofety and health proctices and determine the opplicability of regulatory limitations prior to use.

2. Applicable Documents

- 2.1 ASTM Standords:
- C 117 Test Method for Material Finer Than 75-µm (No. 200) Sieve in Mineral Aggregates by Washing
- C 136 Method for Sieve Analysis of Fine and Coarse Aggregates³
- C 702 Methods for Reducing Field Samples of Aggregate to Testing Size3
- D420 Recommended Practice for Investigation and Sampling Soil and Rock for Engineering Purposes*
- D421 Method for Dry Preparation of Soil

¹ This test method is under the jurisdiction of ASTM Committee D-18 on Soil and Rock and is the direct responsibility of Subcommittee D18.07 on Identification and Classification of

Current edition approved Aug. 17, 1983. Published October 1983. Originally published as D 2487 - 66 T. Last previous edition D 2487 - 69 (1975).

Casagrande, A., "Classification and Identification of Soils."

Transactions, ASCE, 1948, p. 901.

Annual Book of ASTIA Standards, Vol 04.02.

Annual Brack of ASTM Standards, Vol 04.08.

Samples for Particle-Size Analysis and Determination of Soil Constants*

- D422 Method of Particle-Size Analysis of Soils⁴
- D423 Test Method for Liquid Limit of Soils*
- D 424 Test Method for Plastic Limit and Plasticity Index of Soils*
- D653 Terms and Symbols Relating to Soil and Rock⁴
- D 1140 Test Method for Amount of Material in Soils Finer than the No. 200 (75-µm) Sieve⁴
- D2216 Method for Laboratory Determination of Water (Moisture) Content of Soil, Rock, and Soil-Aggregate Mixtures⁴
- D 2217 Method for Wet Preparation of Soil Samples for Particle-Size Analysis and Determination of Soil Constants⁴
- D 2488 Recommended Practice for Description of Soils (Visual-Manual Procedures)⁴
- E 11 Specification for Wire-Cloth Sieves for Testing Purposes³

3. Summary of Method

- J.1 As illustrated in Table 1, this classification system identifies three major soil divisions: coarse-grained soils, fine-grained soils, and highly organic soils. These three divisions are further subdivided into a total of 15 basic soil groups.
- 3.2 Based on the results of visual observations and prescribed laboratory tests, a soil is catalogued according to the basic soil groups, assigned a group symbol(s) and name, and thereby classified. The flow charts, Fig. 1 for fine-grained soils, and Fig. 2 for coarse-grained soils, can be used to assign the appropriate group symbol(s) and name.

4. Significance and Use

- 4.1 This test method classifies soils from any geographic location into categories representing the results of prescribed laboratory tests to determine the particle-size characteristics, the liquid limit, and the plasticity index.
- 4.2 The assigning of a group name and symbol(s) along with the descriptive information required in Recommended Practice D 2488 can be used to describe a soil to aid in the evaluation of its significant properties for engineering use.
- 4.1 The various groupings of this classification system have been devised to correlate in a general way with the engineering behavior of soils. This test method provides a useful first step in any

field or laboratory investigation for geotechnical engineering purposes.

4.4 This test method may also be used as an aid in training personnel in the use of Recommended Practice D 2488.

5. Terminology

5.1 Definitions—Except as listed below, all definitions are in accordance with Definitions D 653:

NOTE 4—For particles retained on a 3-in. (75-mm) U.S. standard sieve, the following definitions are suggested:

Cobbles—particles of rock that will pass a 12-in. (300-mm) square opening and be retained on a 3-in. (75-mm) U.S. standard sieve, and

Boulders—particles of rock that will not pass a 12, in. (300-mm) square opening

5.1.1 gravel—particles of rock that will pass a 3-in. (75-mm) sieve and be retained on a No. 4 (4.75-mm) U.S. standard sieve with the following subdivisions:

Coarse—passes 3-in. (75-mm) sieve and retained on %-in. (19-mm) sieve, and

Fine—passes ¼-in. (19-mm) sieve and retained on No. 4 (4.75-mm) sieve.

5.1.2 sand—particles of rock that will pass a No. 4 (4.75-mm) sieve and be retained on a No. 200 (75-µm) U.S. standard sieve with the following subdivisions:

Coarse—passes No. 4 (4.75-mm) sieve and retained on No. 10 (2.00-mm) sieve,

Medium—passes No. 10 (2.00-mm) sieve and retained on No. 40 (425-µm) sieve, and

Fine—passes No. 40 (425-µm) sieve and retained on No. 200 (75-µm) sieve.

- 5.1.3 clay—soil passing a No. 200 (75-µm) U.S. standard sieve that can be made to exhibit plasticity (putty-like properties) within a range of water contents and that exhibits considerable strength when air dry. For classification, a clay is a fine-grained soil, or the fine-grained portion of a soil, with a plasticity index equal to or greater than 4, and the plot of plasticity index versus liquid limit falls on or above the "A" line.
- 5.1.4 silt—soil passing a No. 200 (75-µm) U.S. standard sieve that is nonplastic or very slightly plastic and that exhibits little or no strength when air dry. For classification, a silt is a fine-grained soil, or the fine-grained portion of a soil, with a plasticity index less than 4 or if the plot of plasticity index versus liquid limit falls below the "A" line,
- 5.1.5 organic clay-a clay with sufficient or-

Anic content to influence the soil properties. For classification, an organic clay is a soil that would be classified as a clay except that its liquid limit value after oven drying is less than 75% of its liquid limit value before oven drying.

- 5.1.6 arganic silt—a silt with sufficient organic content to influence the soil properties. For classification, an organic silt is a soil that would be classified as a silt except that its liquid limit value after oven drying is less than 75 % of its liquid limit value before oven drying.
- 5.1.7 peat—a soil composed of vegetable tissue in various stages of decomposition usually with an organic odor, a dark-brown to black color, a spongy consistency, and a texture ranging from fibrous to amorphous.
- 5.2 Descriptions of Terms Specific to This Standard:
- 5.2.1 coefficient of curvature, Cc—the ratio $(D_{10})^2/(D_{10}\times D_{60})$, where D_{60} , D_{30} , and D_{10} are the particle diameters corresponding to 60, 30, and 10% finer on the cumulative particle-size distribution curve, respectively.
- 5.2.2 coefficient of uniformity, Cu—the ratio D_{10}/D_{10} , where D_{10} and D_{10} are the particle diameters corresponding to 60 and 10 % finer on the cumulative particle-size distribution curve, respectively.

6. Apparatus

6.1 In addition to the apparatus that may be required for obtaining and preparing the samples and conducting the prescribed laboratory tests, a planticity chart, similar to Fig. 5, and a cumulative particle-size distribution curve, similar to Fig. 4, are required.

NOTE 5.—The "U" line shown on Fig. 3 has been empirically determined to be the approximate "upper limit" for natural soils. It is a good check against erroneous data, and any test results that plot above or to the left of it should be verified.

7. Sampling

- 7.1 Samples shall be obtained and identified in accordance with a method or methods, recommended in Recommended Practice D 420 or by other accepted procedures.
- 7.2 For accurate identification, the minimum amount of test sample required for this test method will depend on which of the laboratory tests need to be performed. Where only the particle-size analysis of the sample is required, specimens having the following minimum dry weights are required:

Maximum Particle Size. Sieve Opening	Minimum Specimen Size, Dry Weight
4,75 mm (No. 4)	100 g (0.25 lb)
9.5 mm (½ in.)	200 g (0.5 lb)
19.0 mm (% in.)	1.0 kg (2.2 lb)
38.1 mm (1½ in.)	8.0 kg (18 lb)
75.0 mm (3 in.)	60.0 kg (132 lb)

Whenever possible, the field samples should have weights two to four times larger than shown.

- 7.3 When the liquid and plastic limit tests must also be performed, additional material will be required sufficient to provide 150 g to 200 g of soil finer than the No. 40 (425-µm) sieve.
- 7.4 If the field sample or test specimen is smaller than the minimum recommended amount, the report shall include an appropriate remark.

8. Classification of Peat

8.1 A sample composed primarily of vegetable tissue in various stages of decomposition and has a fibrous to amorphous texture, a dark-brown to black color, and an organic odor should be designated as a highly organic soil and shall be classified as peat, PT, and not subjected to the classification procedures described hereafter.

9. Preparation for Classification

- 9.1 Before a soil can be classified according to this test method, generally the particle-size distribution and the plasticity characteristics of the minus 3-in. (75-mm) material must be determined. See 9.8 for the specific required tests.
- 9.2 The preparation of the soil specimen(s) and the testing for particle-size distribution and liquid limit and plasticity index shall be in accordance with accepted standard procedures. Two procedures for preparation of the soil specimens for testing for soil classification purposes are given in Appendixes X3 and X4. Appendix X3 describes the wet preparation method and is the preferred method for cohesive soils that have never dried out and for organic soils.
- 9.3 When reporting soil classifications determined by this test method, the preparation and test procedures used shall be reported or referenced.
- 9.4 Although the test procedure used in determining the particle-size distribution or other considerations may require a hydrometer analysis of the material, a hydrometer analysis is not necessary for soil classification.
- 9.5 The percentage (by dry weight) of any plus 3-in. (75-mm) material must be determined and

reported as auxiliary information.

- 9.6 The maximum particle size shall be determined (measured or estimated) and reported as auxiliary information.
- 9.7 When the cumulative particle-size distribution is required, a set of sieves shall be used which include the following sizes (with the largest size commensurate with the maximum particle size) with other sieve sizes as needed or required to define the particle-size distribution:

3-in. (75-mm) %-in.(19.0-mm) No. 4 (4.75-mm) No. 10 (2.00-mm) No. 40 (425-μm) No. 200 (75-μm)

- 9.8 The tests required to be performed in preparation for classification are as follows:
- 9.8.1 For soils estimated to contain less than 5 % fines, a plot of the cumulative particle-size distribution curve of the fraction coarser than the No. 200 (75-µm) sieve is required. The cumulative particle-size distribution curve may be plotted on a graph similar to that shown in Fig. 4.
- 9.8.2 For soils estimated to contain 5 to 15 % fines, a cumulative particle-size distribution curve, as described in 9.8.1, is required, and the liquid limit and plasticity index are required.
- 9.8.2.1 If sufficient material is not available to determine the liquid limit and plasticity index, the fines should be estimated to be either silty or clayey using the procedures described in Recommended Practice D 2488 and so noted in the report.
- 9.8.3 For soils estimated to contain 15% or more fines, a determination of the percent fines, percent sand, and percent gravel is required, and the liquid limit and plasticity index are required. For soils estimated to contain 90% fines or more, the percent fines, percent sand, and percent gravel may be estimated using the procedures described in Recommended Practice D 2488 and so noted in the report.

10. Preliminary Classification Procedure

- 10.1 Class the soil as fine-grained if 50 % or more by dry weight of the test specimen passes the No. 200 (75-μm) sieve and follow Section 11.
- 10.2 Class the soil as coarse-grained if more than 50 % by dry weight of the test specimen is retained on the No. 200 (75- μ m) sieve and follow Section 12.

- Procedure for Classification of Fine-Grained Soils (50 % or more by dry weight passing the No. 200 (75-µm) sieve)
- 11.1 The soil is an inorganic clay if the position of the plasticity index versus liquid limit plot, Fig. 3, falls on or above the "A" line, the plasticity index is greater than 4, and the presence of organic matter does not influence the liquid limit as determined in 11.3.2.
- 11.1.1 Classify the soil as a lean clay, CL, if the liquid limit is less than 50. See area identified as CL on Fig. 3.
- 11.1.2 Classify the soil as a fat clay, CH, if the liquid limit is 50 or greater, See area identified as CH on Fig. 3.
- Note 6.—In cases where the liquid limit exceeds 110 or the plasticity index exceeds 60, the plasticity chan may be expanded by maintaining the same scale on both axes and extending the "A" line at the indicated slope,
- 11.1.3 Classify the soil as a silty clay, CL-ML if the position of the plasticity index versus liquid limit plot falls on or above the "A" line and the plasticity index is in the range of 4 to 7. See area identified as CL-ML on Fig. 3.
- 11.2 The soil is an inorganic silt if the position of the plasticity index versus liquid limit plot. Fig. 3, falls below the "A" line or the plasticity index is less than 4, and presence of organic matter does not influence the liquid limit at determined in 11.3.2.
- 11.2.1 Classify the soil as a silt, ML, if the liquid limit is less than 50. See area identified as ML on Fig. 3.
- 11.2.2 Classify the soil as an elastic sill, MH, if the liquid limit is 50 or greater. See area identified as MH on Fig. 3.
- 11.3 The soil is an organic silt or clay if organic matter is present in sufficient amounts to influence the liquid limit as determined in 11.3.2
- 11.3.1 If the soil has a dark color and an organic odor when moist and warm, a second liquid limit test shall be performed on a test specimen which has been oven dried at 110 ±5°C to a constant weight, typically over night.
- 11.3.2 The soil is an organic silt or organic clay if the liquid limit after oven drying is less than 75% of the liquid limit of the original specimen determined before oven drying (see Procedure B of Method D 2217).
- 11.3.3 Classify the soil as an organic silt or organic clay, OL, if the liquid limit (not orce dried) is less than 50 %. Classify the soil as as

Again silt, OL, if the plasticity index is less than 4. or the position of the plasticity index versus bauid limit plot falls below the "A" line. Classify the soil as an organic clay, OL, if the plasticity andex is 4 or greater and the position of the plasticity index versus liquid limit plot falls on or above the "A" line. See area identified as OL for CL-ML) on Fig. 3.

11.3.4 Classify the soil as an organic clay or organic silt, OH, if the liquid limit (not oven dried) is 50 or greater. Classify the soil as an organic silt, OH, if the position of the plasticity index-versus liquid limit plot falls below the "A" line. Classify the soil as an organic clay, OH, if the position of the plasticity index versus liquid-limit plot falls on or above the "A" line. See area identified as OH on Fig. 3.

11.4 If less than 30% but 15% or more of the test specimen is retained on the No. 200 (75-µm) sieve, the words "with sand and/or gravel" shall be added to the group name. For example, lean clay with sand, CL; silt with sand and gravel, ML.

11.5 If 30% or more of the test specimen is tetained on the No. 200 (75-µm) sieve, the words "sandy" or "gravelly" shall be added to the group name. Add the word "sandy" if 30% or more of the test specimen is retained on the No. 200 (75-µm) sieve and the coarse-grained portion is predominantly sand. Add the word "gravelly" if 30% or more of the test specimen is retained on the No. 200 (75-µm) sieve and the coarse-grained portion is predominantly gravel. For example, sandy lean clay, CL; gravelly fat clay, CH; sandy silt, ML.

 Procedure for Classification of Coarse-Grained Soils (more than 50 % retained on the No. 200 (75-µm) sieve)

12.1 Class the soil as gravel if more than 50 % of the coarse fraction (plus No. 200 (75-µm) sieve) is retained on the No. 4 (4.75-mm) sieve.

12.2 Class the soil as sand if 50 % or more of the coarse fraction (plus No. 200 (75-μm) sieve] passes the No. 4 (4.75-mm) sieve.

12.3 If 12 % or less of the test specimen passes the No. 200 (75-μm) sieve, plot the cumulative particle-size distribution, Fig. 4, and compute the coefficient of uniformity, Cu, and coefficient of curvature, Cc, as given in Eqs. 1 and 2.

$$Cu = D_{e0}/D_{t0} \tag{1}$$

$$Cc = (D_{10})^2/(D_{10} \times D_{10})$$
 (2)

where:

 D_{10} , D_{30} , and D_{60} = the particle-size diameters corresponding to 10, 30, and 60 %, respectively, passing on the eumulative particle-size distribution curve, Fig. 4.

Note 7—It may be necessary to extrapolate the curve to obtain the D_{10} diameter.

12.3.1 If less than 5% of the test specimen passes the No. 200 (75-µm) sieve, classify the soil as a well-graded gravel, GW, or well-graded sand. SW, if Cu is greater than 4.0 for gravel or greater than 6.0 for sand, and Cc is at least 1.0 but not more than 3.0.

12.3.2 If less than 5 % of the test specimen passes the No. 200 (75-µm) sieve, classify the soil as poorly graded gravel, GP, or poorly graded sand, SP, if either the Cu or the Cc criteria for well-graded soils are not satisfied.

12.4 If more than 12 % of the test specimen passes the No. 200 (75-µm) sieve, the soil shall be considered a coarse-grained soil with fines. The fines are determined to be either clayey or silty based on the plasticity index versus liquid limit plot on Fig. 3. (See 9.8.2.1 if insufficient material available for testing).

12.4.1 Classify the soil as a clayey gravel, GC. or clayey sand, SC, if the fines are clayey, that is, the position of the plasticity index versus liquid limit plot, Fig. 3, falls on or above the "A" line and the plasticity index is greater than 7.

12.4.2 Classify the soil as a silty gravel, GM. or silty sand, SM, if the lines are silty, that is, the position of the plasticity index versus liquid limit plot, Fig. 3, falls below the "A" line or the plasticity index is less than 4.

12.4.3 If the fines plot as a silty clay, CL-ML, classify the soil as a silty, clayey gravel, GC-GM, if it is a gravel or a silty, clayey sand, SC-SM, if it is a sand.

12.5 If 5 to 12 % of the test specimen passes the No. 200 (75-µm) sieve, give the soil a dual classification using two group symbols.

12.5.1 The first group symbol shall correspond to that for a gravel or sand having less than 5 % fines (GW, GP, SW, SP), and the second symbol shall correspond to a gravel or sand having more than 12 % fines (GC, GM, SC, SM).

12.5.2 The group name shall correspond to the first group symbol plus "with clay" or "with silt" to indicate the plasticity characteristics of the fines. For example, well-graded gravel with clay, GW-GC; poorly graded sand with silt, SP-SM (See 9.8.2.1 if insufficient material available for testing).

Note 8—If the fines plot as a silty clay, CL-ML, the second group symbol should be either GC or SC. For example, a poorly graded sand with 10 % fines, a liquid limit of 20, and a plasticity index of 6 would be classified as a poorly graded sand with silty clay, SP-SC.

12.6 If the specimen is predominantly sand or gravel but contains 15% or more of the other coarse-grained constituent, the words "with gravel" or "with sand" shall be added to the group name. For example, poorly graded gravel with sand, clayey sand with gravel.

12.7 If the field sample contained any cobbles or boulders or both, the words "with cobbles," or "with cobbles and boulders" shall be added to the group name. For example, silty gravel with cobbles, GM.

13. Report

13.1 The report should include the group name, group symbol, and the results of the laboratory tests. The particle-size distribution shall be given in terms of percent of gravel, sand, and fines. The plot of the cumulative particle-size distribution curve shall be reported if used in classifying the soil. Report appropriate descriptive information according to the procedures in Recommended Practice D 2488. A local or commercial name or geologic interpretation for the material may be added at the end of the descriptive information if identified as such. The test procedures used shall be referenced.

NOTE 9—Example: Clayey Gravel with Sand and Cobbles (GC)—46 % fine to coarse, hard, subrounded sand, 24 % clayey fines, LL = 38, Pl = 19; weak reaction with HCl; original field sample had 4 % hard, subrounded cobbles; maximum size 150 mm.

In-Place Conditions—firm, homogeneous, do

Geologic Interpretation—alluvial fan.
NOTE 10—Other examples of soil descriptions are given in Appendix X1.

14. Precision and Bias

14.1 This test method provides qualitative data only; therefore, a precision and bias state, ment is nonapplicable.

					7	Soil Classification
Ċ.	Criteria for Assigning Group Symbols and Group Names Using Laboratory Tests ⁴	and Group Names Using Labor	'sisy Tests'	1 - 0,	Group Symbol	Group Name
Coarse-Grained Soils	Gravels	Clean Gravels	Cu'z 4 and 1 s Cc s 34		<u>₹</u>	Well-graded gravel*
More than 30 % retained on No. 200 sieve	tion retained on No. 4 sieve	Less than 5 % lines.	Cu < 4 and/or I > Cc > 34	34	å	Poorly graded gravel
	-	Gavets with Fines	Fines classify as ML or MH	¥	₩S	Silty gravel ^{7.6.8}
	*	More than 1.2 % lines	Fines classify as CL or CH	F	૪	Clayey gravel (E.M.
	Sands	Clean Sands	Co≥6 and 1 ≤ Cc ≤ 34		ΑS	Well-graded sand'
	passes No. 4 sieve	Less than 5 % (Ind.)	Cu < 6 and/or 1 > Cc > 3	3€	gs.	Poorly graded sand'
		Sands with Fines	Fines classify as ML or MH	431	ΣM	Silty sand GAV
		More than 12.35 fines	Fines classify as CL or CH	=	ន	Clayey sand G.K.)
Fine-Grained Soils	Silts and Clays	inorganic	PI > 7 and plots on or above "A" line	bove "A" line	7	Lean clay East
sicke	Laguid timit iess inan 30		PI < 4 or plots below "A" line	- line/	ML	Silvator
		organic	Liquid limit - oven dried Liquid limit - not dried	2 < 0.75	o L	Organic claytana Organic silletana
	Silts and Clays	inorganic	Pf plats on or above "A" fine	line	푼	Fat clay Fire
	Liquid limit 30 or more		Pt plots below "A" line		MH	Elastic sill ****
		urpanic	Liquid fimit - oven dried < 0.75 Liquid fimit - not dried	4 < 0.75	Æ	Organic clay 64.00
Highly organic soils	Prima	Primarily organic matter, dark in color, and organic odor	lor, and organic odor		F	Peat
Hased on the material passing the 3-in, [75-mm] sieve. If field sample contained cobbles or boulders, or both, add "with cobbles us boulders, or both" to group name. **Gravels with \$10.12 % fines require dual symbols: **GW-GW well-graded gravel with site **GW-GW well-graded gravel with the **GW-GW well-graded gravel with site GW-GW pandly graded gravel with site GW-GW pandly graded gravel with site Sands with \$10.12 % fines require dual symbols: \$W-SM well-graded sand with site \$W-SM well-graded sand with site \$W-SM pandly graded sand with site site \$W-SM pandly graded sand with site site \$W-SM pandly graded sand with site site \$W-SM pandly graded sand with site site site \$W-SM pandly graded sand with site site site site site site site site	And And And And And And And And And And	² Cu = Dω/Dio Cc = \frac{(Du)^2}{D_{10} \times D_{20}}\$ f If suit contains ≥ 15 % sand, add "with sand" to group more. "If fines are organic, add "with organic fines" to group mit. "If fines are organic, add "with organic fines" to group mit. "It said contains ≥ 15 % gravel, add "with gravel" to group mit. "It said contains ≥ 15 % gravel, add "with gravel" to group mit. "It said contains ≥ 15 % gravel, add "with gravel" to group mit. "It said contains plut to hatched area, will is a ClMit. Its clay.	5	* If soil contains 15 to 29 % plus No. 200 or "with gravel," whichever is predominant. * If soil contains ≥ 30 % plus No. 200, pre add "sand" to group name. * If soil contains ≥ 30 % plus No. 200 gravel, add "gravell," to group name. * Pl ≥ 4 and pluts below "A" line. * Pl of 4 or pluts below "A" line. * Pl plots on or above "A" line. * Pl plots halow "A" line.	29% plus cr is pred e plus No ne. 0% plus r above " "A" line.	* If soil contains 15 to 29 % plus No. 300, add "with sand" "with gravel," whichever is predominant. * If soil contains ≥ 30 % plus No. 200, predominantly sand, ld "sandy" to group name. * If soil contains ≥ 30 % plus No. 200, predominantly stel, add "gravelly" to group name. * Pl ≥ 4 and plots on or above "A" line. * Pl ≥ 4 or plus below "A" line. * Pl plots on or above "A" line. * Pl plots below "A" line.

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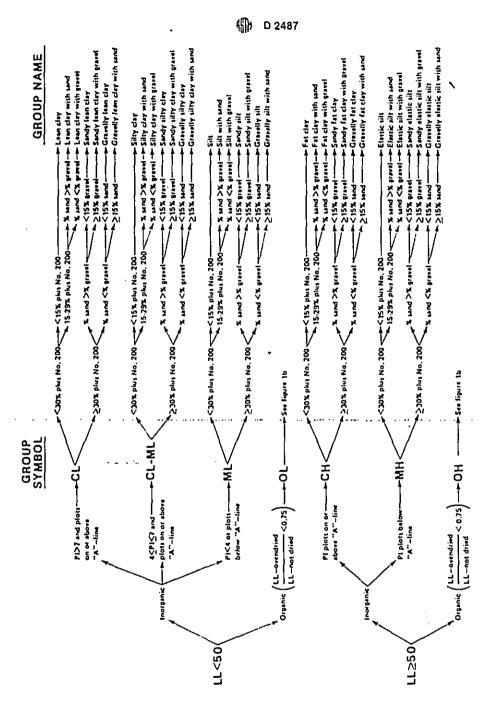


FIG. 1s Flow Chart for Classifying Fine-Grained Soil (50 % or More Passes No. 200 Siere)

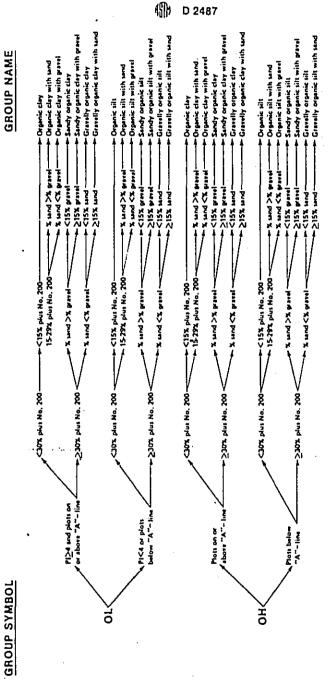


FIG. 1b Flum Chart for Classifying Organic Fine-Grained Soil (50 % or More Passes No. 200 Siere)

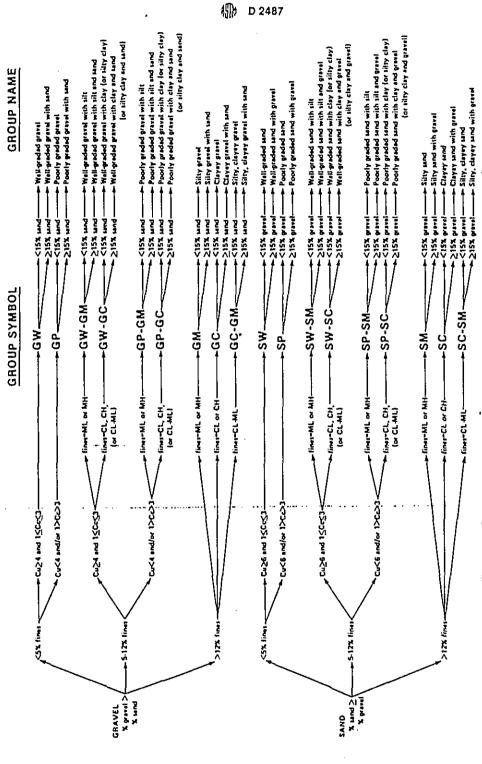
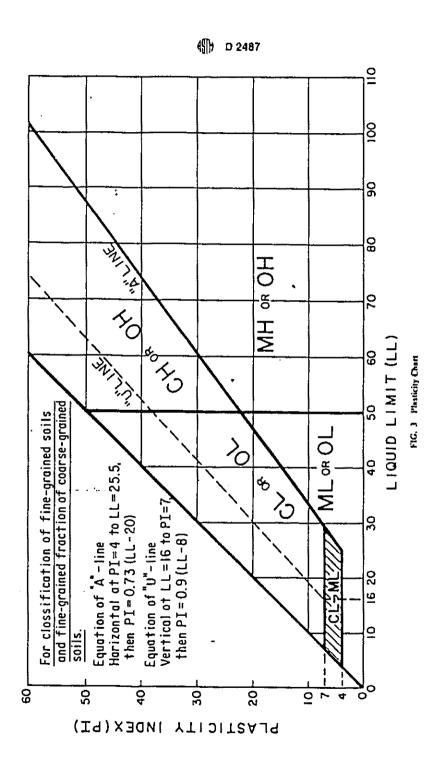


FIG. 2 Flow Chart for Chassifying Course-Crained Solis (Nine Than 50 % Retained on No. 200 Sieve)





SIEVE ANALYSIS

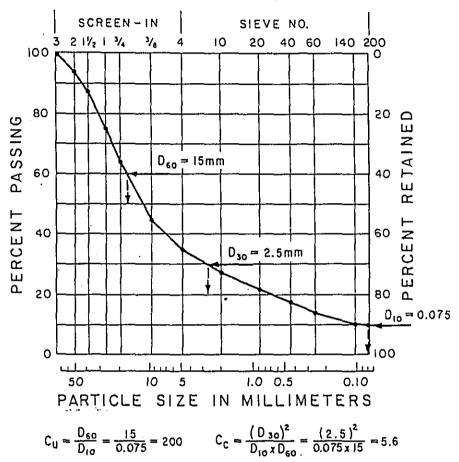


FIG. 4 Cumulative Particle-Size Plot

APPENDIXES

(Nonmandatory Information)

XI. EXAMPLES OF DESCRIPTIONS USING SOIL CLASSIFICATION

X1.1 The following examples show how the information required in 13.1 can be reported. The appropriate descriptive information from Recommended Practice D 2488 is included for illustrative purposes. The additional descriptive terms that would accompany the soil classification should be based on the intended use of the classification and the individual circum-

X1.1.1 Well-Graded Gravel with Sand (GW)-73 % fine to coarse, hard, subangular gravel; 23 % fine to coarse, hard, subangular sand; 4 % fines; Cc = 2.7, Cu

= 12.4.

X1.1.2 Silty Sand with Gravel (SM)—61 % predominantly fine sand; 23 % silty fines, LL = 33, PI = 6; 16 % fine, hard, subrounded gravel; no reaction with HCI; (field sample smaller than recommended), In-Place Conditions—Firm, stratified and contains lenses of silt 1 to 2 in, thick, moist, brown to gray, in-place density = 106 lb/ft3 and in-place moisture = 9 %.

X1.1.3 Organic Clay (OL)-100 % fines, LL (not

rial, take extreme care in obtaining a representative portion of the No. 40 (425-µm) fraction. Typically, a larger portion than normal has to be selected, such as the minimum weights required in 7.2.

X3.7.1.2 To obtain a representative specimen of a basically cohesive soil, it may be advantageous to pass the soil through a %-in. (19-mm) sieve or other convenient size so the material can be more easily mixed and then quartered or split to obtain the representative specimen.

X3.7.2 Process the representative specimen in accordance with Procedure B of Method D 2217.

X3.7.3 Perform the liquid-limit test in accordance with Method D 423, except the soil shall not be air dried prior to the test.

X3.7.4 Perform the plastic-limit test in accordance with Test Method D 424, except the soil shall not be air dried prior to the test, and calculate the plasticity index.

X3.8 Determine the particle-size distribution as follows:

X3.8.1 If the water content of the fraction passing the 3-in. (75-mm) sieve was required (X3.6.3), use the water-content specimen for determining the particle-size distribution. Otherwise, select a representative spec-

imen in accordance with Methods C 702 with a minimum dry weight as required in 7.2.

X3.8.2 If the cumulative particle-size distribution including a hydrometer analysis is required, determine the particle-size distribution in accordance with Method D 422. See 9.7 for the set of required sieves.

X3.8.3 If the cumulative particle-size distribution without a hydrometer analysis is required, determine the particle-size distribution in accordance with Method C 136. See 9.7 for the set of required sieves. The specimen should be soaked until all clayey aggregations have softened and then washed in accordance with Test Method C 117 prior to performing the particle-size distribution.

X3.8.4 If the cumulative particle-size distribution is not required, determine the percent fines, percent sand, and percent gravel in the specimen in accordance with Test Method C 117, being sure to soak the specimen long enough to soften all clayey aggregations, followed by Method C 136 using a nest of sieves which shall include a No. 4 (4.75-mm) sieve and a No. 200 (75-µm) sieve.

X3.8.5 Calculate the percent fines, percent sand, and percent gravel in the minus 3-in, (75-mm) fraction for classification purposes.

X4. AIR-DRIED METHOD OF PREPARATION OF SOILS FOR TESTING FOR CLASSIFICATION PURPOSES

X4.1 This appendix describes the steps in preparing a soil sample for testing for purposes of soil classification when air-drying the soil before testing is specified or desired or when the natural moisture content is near that of an air-dried state.

X4.2 If the soil contains organic matter or mineral colloids that are irreversibly affected by air drying, the wet-preparation method as described in Appendix X3 should be used.

X4.3 Since this classification system is limited to the portion of a sample passing the 3-in. (75-mm) sieve, the plus 3-in. (75-mm) material shall be removed prior to the determination of the particle-size characteristics and the liquid limit and plasticity index.

X4.4 The portion of the field sample finer than the 3-in. (75-mm) sieve shall be obtained as follows: X4.4.1 Air dry and weigh the field sample.

X4.4.2 Separate the field sample into two fractions on a 3-in. (75-mm) sieve.

X4.4.3 Weigh the two fractions and compute the percentage of the plus 3-in. (75-mm) material in the field sample.

X4.5 Determine the particle-size distribution and

liquid limit and plasticity index as follows (see 9.8 for when these tests are required):

X4.5.1 Thoroughly mix the fraction passing the 3in, (75-mm) sieve.

X4.5.2 If the cumulative particle-size distribution including a hydrometer analysis is required, determine the particle-size distribution in accordance with Method D 422. See 9.7 for the set of sieves that is required.

X4.5.3 If the cumulative particle-size distribution without a hydrometer analysis is required, determine the particle-size distribution in accordance with Test Method D 1140 followed by Method C 136. See 9.7 for the set of sieves that is required.

X4.5.4 If the cumulative particle-size distribution is not required, determine the percent fines, percent sand, and percent gravel in the specimen in accordance with Test Method D 1140 followed by Method C 136 using a nest of sieves which shall include a No. 4 (4.75-mm) sieve and a No. 200 (75-µm) sieve.

X4.5.5 If required, determine the liquid limit and the plasticity index of the test specimen in accordance with Test Methods D 423 and D 424.

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dried) = 32, LL (oven dried) = 21, PI (not dried) = 10;

wet, dark brown, organic odor, weak reaction with HCl. X1.1.4 Silty Sand with Organic Fines (SM)—74 % he to coarse, hard, subangular reddish sand; 26 % organic and silty dark-brown fines, LL (not dried) = 37, LL (oven dried) = 26, PI (not dried) = 6, wet, weak teaction with HCI.

X1.1.5 Poorly Graded Gravel with Silt, Sand, Cob-

bles and Boulders (GP-GM)-78 % fine to coarse, hard. subrounded to subangular gravel; 16 % fine to coarse. hard, subrounded to subangular sand; 6 % silty (estimated) fines; moist, brown; no reaction with HCl; original field sample had 7 % hard, subrounded cobbles and 2 % hard, subrounded boulders with a maximum size of 18 in.

X2. USING SOIL CLASSIFICATION AS A DESCRIPTIVE SYSTEM FOR SHALE, CLAYSTONE, SHELLS, SLAG, CRUSHED ROCK, ETC.

X2.1 The group names and symbols used in this test method may be used as a descriptive system applied to materials that exist in situ as shale, claystone, sandstone. silistone, mudstone, etc., but convert to soils after field or laboratory processing (crushing, slaking, etc.).

X2.2 Materials such as shells, crushed rock, slag, etc., should be identified as such. However, the procedures used in this method for describing the particle size and plasticity characteristics may be used in the description of the material. If desired, a classification in accordance with this test method may be assigned to aid in describing the material.

X2.3 If a classification is used, the group symbol(s) and group names should be placed in quotation marks or noted with some type of distinguishing symbol. See examples.

X2.4 Examples of how soil classifications could be incorporated into a description system for materials that are not naturally occurring soils are as follows:

X2.4.1 Shale Chunks-Retrieved as 2 to 4-in. pieces

of shale from power auger hole, dry, brown, no reaction with HCl. After laboratory processing by slaking in water for 24 h, material classified as "Sandy Lean Clay (CL)"—61 % clayey fines, LL = 37, PI = 16; 33 % fine to medium sand; 6 % gravel-size pieces of shale.

X2.4.2 Crushed Sandstone—Product of commercial crushing operation; "Poorly Graded Sand with Silt (SP-SM)"-91 % fine to medium sand; 9 % silty (estimated) fines; dry, reddish-brown, strong reaction with

X2.4.3 Broken Shells—62 % gravel-size broken shells; 31 % sand and sand-size shell pieces; 7 % lines: would be classified as "Poorly Graded Gravel with Sand (GP)".

X2.4.4 Crushed Rock—Processed gravel and cob-bles from Pit No. 7; "Poorly Graded Gravel (GP)"— 89 % fine, hard, angular gravel-size particles: 11 % coarse, hard, angular sand-size particles, dry, tan; no reaction with HCl; Cc = 2.4, Cu = 0.9.

X3. PREPARATION AND TESTING FOR CLASSIFICATION PURPOSES BY THE WET METHOD

X3.1 This appendix describes the steps in preparing a soil sample for testing for purposes of soil classifica-tion using a wet-preparation procedure.

X3.2 Samples prepared in accordance with this procedure should contain as much of their natural water content as possible and every effort should be made during obtaining, preparing, and transportating the samples to maintain the natural moisture.

X3.3 The procedures to be followed in this test method assume that the field sample contains fines, sand, gravel, and plus 3-in. (75-mm) particles and the cumulative particle-size distribution plus the liquid limit and plasticity index values are required (see 9.8). Some of the following steps may be omitted when they

are not applicable to the soil being tested.

X3.4 If the soil contains plus No. 200 (75-µm) particles that would degrade during dry sieving, use a test procedure for determining the particle-size character-istics that prevents this degradation. X3.5 Since this classification system is limited to

the portion of a sample passing the 3-in. (75-mm) sieve, the plus 3-in, (75-mm) material shall be removed prior to the determination of the particle-size characteristics and the liquid limit and plasticity index.

X3.6 The portion of the field sample finer than the 3-in. (75-mm) sieve shall be obtained as follows:

X3.6.1 Separate the field sample into two fractions

on a 3-in. (75-mm) sieve, being careful to maintain the natural water content in the minus 3-in. (75-mm) fraction. Any particles adhering to the plus 3-in. (75-mm) particles shall be brushed or wiped off and placed in the fraction passing the 3-in. (75-mm) sieve.

X3.6.2 Determine the air-dry or oven-dry weight of the fraction retained on the J-in. (75-mm) sieve, Determine the total (wet) weight of the fraction passing the 3-in, (75-mm) sieve.

X3.6.3 Thoroughly mix the fraction passing the 3in. (75-mm) sieve. Determine the water content, in accordance with Method D 2216, of a representative specimen with a minimum dry weight as required in .2. Save the water-content specimen for determination of the particle-size analysis in accordance with X3.8.

X3.6.4 Compute the dry weight of the fraction passing the 3-in. (75-mm) sieve based on the water content and total (wet) weight. Compute the total dry weight of the sample and calculate the percentage of material retained on the 3-in. (75-mm) sieve.

X3.7 Determine the liquid limit and plasticity index as follows:

X3.7.1 If the soil disaggregates readily, mix on a clean, hard surface and select a representative sample by quartering in accordance with Method C 702.

X3.7.1.1 If the soil contains coarse-grained particles coated with and bound together by tough clayey mate-

LIST OF TERMS USED AND SYMBOLS

1) DRILLING & SAMPLING

AD = BCR = BS = CA = CR = FVT =	After Casing Removed After Drilling Before Casing Removed Bentonite Slurry Casing Advanced Casing Removed Field Vanc Shear Test Ground Water Level	PA =	Hand Augering Power Augering Pocket Penetrometer Standard Penetration Test Split - Spoon Shelby Tube Thin-Walled Bit Wash Out
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2) SOIL PROPERTIES

Wn 1.1. PL PI 1.1	 Natural Water Content Liquid Limit Plastic Limit Plasticity Index Liquidity Index 	G _S = Specific Gravity Yt = Total Unit Weight Su = Undrained Shear Strength St = Sensitivity SPT-N= Standard Penetration Resistance
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3) SOIL CONSISTENCY AND COMPACTNESS

	COHESIVE SOILS		COI	HESIONLESS SOILS	
Consistency	SPT-N (Blows/Et.)	Unconfined Shear Strength (t/m ²)	Compactness	SPT - N (Blows/Ft.)	Relative Density
Very Soft Soft Medium Stiff Very Stiff Hard	0 - 2 2 - 4 4 - 8 8 - 15 15 - 30 > 30	< 1.25 1.25 - 2.50 2.50 - 5.00 5.00 - 10.00 10.00 - 20.00 > 20.00	Very Loose Loose Medium Dense Very Dense	0 - 4 4 - 10 10 - 30 30 - 50 > 50	0 - 15 15 - 35 35 - 65 65 - 85 85 - 100

4) TERMS USED FOR IDENTIFYING MINOR COMPONENT OF SOIL

Term	% of Sample
Truce	< 10
Trace to some	10 - 20
Some	20 - 35
And	35 - 50

REFERENCES

- 1. ASTM STANDARDS (1980), "Soil and Rock, Building Stones", Part 19, American Society for Testing and Materials.
- LAMBE, T.W. (1951), "Soil Testing for Engineers", John Wiley
 Sons Inc. New York, 1951.
- 3. LAMBE, T.W. and WHITMAN, R.V., "Soil Mechanics", John Wiley & Sons Inc. New York, 1969.
- 4. PECK, R.B., HANSON, W.E. and THORNBURN, T.H., "Foundation Engineering", John Wiley & Sons Inc. New York, 1974.
- 5. POULOS, H.G. and DAVIS, E.H., "Pile Foundation Analysis and Design", Taiwan, Copyright 1980.
- 6. SIMON, N.E. and MENZIES, B.K. (1975), "A Short Course in Foundation Engineering", The English Language Books Society and Newes-Butterworth, London, 1975.
- 7. TERZAGHI, K. and PECK, R.B. (1948), "Soil Mechanics in Engineering Practice", John Wiley & Sons Inc. New York, 1967.
- 8. TOMLINSON, M.J., "Pile Design and Construction Practice", First published 1979, Taiwan.
- 9. SATTAYARAK, N., "Review of The Mesozoic Stratigraphy of Thailand", Workshop on Stratigraphic Correlation of Thailand and Malaysia, Haad Yai, Thailand, 8-10 September 1983., V.1, p127-148.

