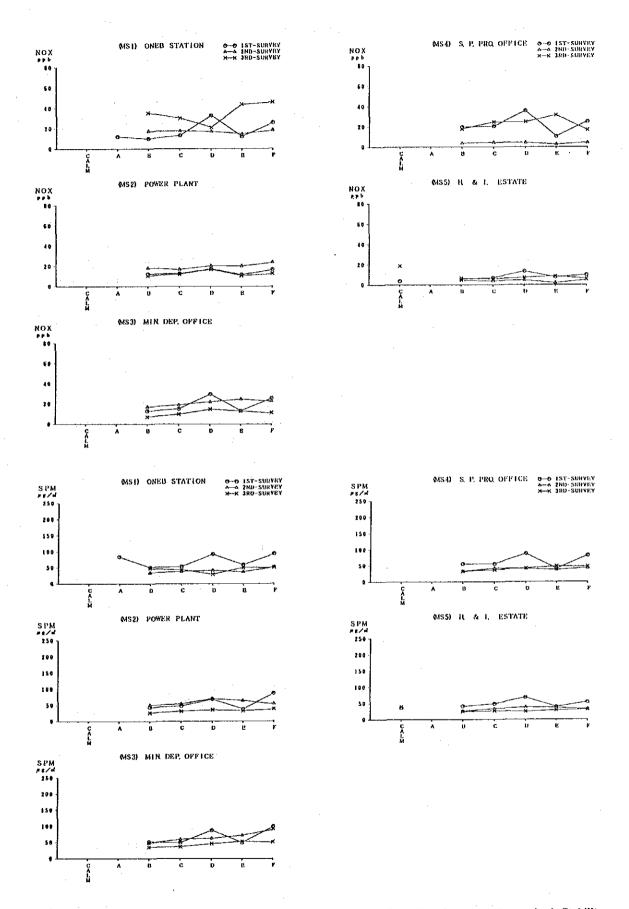


Fig. 2-8(1) Dependence of Air Pollutant Concentration during the Short Term Field Survey on Atmospheric Stability





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3. Data Analysis of Chemical Components Contained in Particulate Matter

Another analytical study was done on the chemical components in particulate matter collected on filter papers by Low-volume and Andersen samplers. In case of the data analysis above where concentrations of chemical components are found less than the detection confidence level, 1/2 of such detection limit values are used in calculation.

3.1 Average Concentration of Chemical Components

Table 3-1 shows the average concentration of chemical components in each short term field survey. In this table, the figures marked "*" are those in which the number of nondetectable data is 50% or more. The data on Ag, Ba, Cs, La, Lu, Ni, and W are mostly less than the detection confidence level. Table 3-2 shows the names of top 10 chemical components which rank in high average concentration. The concentration of soil particle (Si, Ca, Al), sea-salt particle (Na, Cl), secondary particle (SO₄²⁻ and NH₄⁺) and carbon are found relatively high.

Table 3-1(1) Average Concentrations of Chemical Components in Particulate Matter-

.

| (unit;ng/#³) | 3 seasons | Geometric mean | 2.5% | 3.945+ 161.889 161.889 2166.465 2781.190 2781.190 | 1250.322 532.623 | 522.212 119.722* | 428.701 | 1121.127 873.972 4106.012 | | |
|--------------------------------|------------|--------------------|--|--|----------------------|--|----------------|---|---|---|
| (unit; | Average of | Average | 26.0 26.0 26.0 26.0 27.0 27.0 27.0 27.0 27.0 27.0 27.0 27 | 3.967± 345.667 2221.333 3116.667 | 1314.000 610.000 | 262.000 262.000 | 559.333 | 1212.667 977.333 4525.000 | | |
| | survey | Geometric mean | 200 200 200 200 200 200 200 200 | 188-534 188-534 2272-735 | 1003.551 314.961 | 419.823 100.001 | 240.206 | 878.735 429.667 2751.701 | 8 | |
| : | Third : | Average | 989,988,989,989,989,989,989,989,989,989 | 200-000 200-000 2740-000 2740-000 | 1016.000 | 442.000 100.000 | 310.000 | 882.00 7284.00 7884.00 | e are over 50% try | |
| | Survey | Geometric mean | 28.0000 28.000000 28.000000 28.0000 28.0000 28.0 | 3.50 88.538 2081.648 2081.648 2081.648 | 1700.241 535.544 | 109-111 231-312 | 533.877 | 1566.855 1307.234 5110.184 | en trace date / On spectrometr | spectrophotometry Ion chromatography |
| | Second : | Average | | 3.500 101.000 2206.000 2370.000 | 1758.000 562.000 | 574.000 190.000 | 744.000 | 1740.000 1308.000 5842.000 | is marked when Flame photometry Atomic absorption | chromotogeus |
| Coarse) | survey | Geometric mean | 1417.086 1417.086 27.1612 27.1612 20.1 | 4.085= 364.684 2218.145 3945.622 | 1145.553 | 630.540 100.000 | 614.384 | 962.053 1188.521 1282.522 | Note: # | |
| Andersen Sampler (Fine+Coarse) | First : | Average | | 4.100 624.000 2250.000 4240.000 | 1168.000 908.000 | 570.000 100.000≈ | 624.000 | 1016.000 1194.000 5082.000 | | |
| Sample | | nents | ⋦⋖⋦ ଷ ℙ ⋳ ౸⋳⋳⋳⋦≝≈⋥⋽ <u></u> ⋽⋬ ĕ ≋≅⋭⋎⋎⋎⋭⋢⋿⋗⋑⋬ | 3205 | Na* K* | Ga ² * Mg ² * | Ē | ខន្លន | | |
| Andersen | Mathod | neurou analysis | Instrument activation analysis | X-ray fluore- scence | с, ц | AAS | SP | I C | | |
| g/æ ³) | 3 seasons | Geometric mean | ៹ ^ឝ ៳ਗ਼ਜ਼ਗ਼ ਖ਼ੑਞਲ਼ਜ਼ੵੑਸ਼ਲ਼ਲ਼ਖ਼ਖ਼ਲ਼ਲ਼ਲ਼ਫ਼ਫ਼ਲ਼ਲ਼ਖ਼ੑੑਫ਼ਲ਼ਲ਼ਲ਼ੑੑਫ਼ਲ਼ਲ਼ਖ਼ੑੑਲ਼ਗ਼ਫ਼ਲ਼ਖ਼ੑੑੑਲ਼ਲ਼ ਫ਼ੑਫ਼ਲ਼ਜ਼ੵੑਸ਼ਲ਼ਲ਼ਖ਼ਫ਼ਲ਼ਲ਼ਫ਼ਫ਼ਲ਼ਲ਼ੑਫ਼ਲ਼ਲ਼ਖ਼ਫ਼ਲ਼ਲ਼ਫ਼ੑੑਲ਼ਲ਼ਲ਼ਫ਼ਲ਼ਲ਼ਫ਼ੑਲ਼ਲ਼ | 1.084 139.286 1104.078 3472.580 | 1305.024 708.313 | 269.121 73.428* | £9.718≠ | 624.961 640.453 750.554 | 14144.613 9468.120 4600.461 | |
| (unit;ng/m³) | Average of | Average | 8.6.00 8.6.00 8.6.00 8.6.00 8.6.00 8.6.00 8.6.00 8.6.00 8.6.00 | 328.333 328.333 328.000 3280.000 3280.000 | 1358.667 800.667 | 395.333 82.667* | 140.667= | 846.000 794.000 5003.303 | 15380.000 10200.000 5186.667 | |
| | survey | Geometric mean | ੑੵੵਫ਼ੵਸ਼ਗ਼ਫ਼ੑਸ਼ੑੑੑਫ਼ੑਫ਼ੑੑਫ਼ੑਫ਼ੑੑਫ਼ੑਫ਼ੑਫ਼ੑਫ਼ੑਫ਼ੑਫ਼ੑਫ਼ੑਫ਼ੑਫ਼ੑਫ਼ੑਫ਼ੑ | 0.822 138.961 778.579 2672.505 | 1109.829 441.523 | 224.463 59.568* | 67.846* | 811.537 298.473 3805.674 | 9801.129 7121.914 2579.948 | 25 |
| | Thirds | Average | 0.0.5 8.30.0 | 1.100+ 345.000 842.000 2880.000 | 1142.000 476.000 | 308.000 64.000# | 86.00 ≄ | 946.000 3380.000 3360.000 | 10320.000 7580.000 2780.000 | is marked when trace date are over 50% |
| | survey | Georgetric mean | 9.0.25% 2.2 | 0.871+ 39.404 963.152 2652.205 | 1365.362 682.021 | 134.183 74.206= | 135.871 | 355.148 961.180 4206.121 | 13245.635 8566.070 4647.324 | in trace date |
| | Second s | Average | 6.0.20 | 1.100+ 101.000 1080.000 2750.000 | 1416.000 716.000 | 176.000 84.000# | 200.000 | 822.000 980.000 9820.000 | 13540.000 8840.000 4700.000 | s narked whe |
| | survey | Geometric Dean | 0.334 17.572 17.572 17.572 17.572 17.572 17.572 17.572 11.252 11. | 1.783 344.544 1794.742 5907.875 | 1477.559 | 647.146 89.600 | 107.565 | 823.724 945.199 8254.551 | 21798.293 13913.012 7817.617 | Note; * is ED : Frame |
| npler | First s | Average | 282,000 283,000 283 | 2.000 528.000 1882.000 6120.000 | 1518.000 1210.000 | 702.000 100.000 | 136.000 | <i>s</i> 70.000 1014.000 6520.000 | 22230.000 14150.000 8080.000 | |
| ne San | | nents | ⋦⋍⋦ ॺ ₽⋴⋴⋴⋴⋴⋴⋴⋴∊⋍∊⋴⋴∊∊∊∊∊∊∊∊⋴⋴⋴⋴⋴⋴⋴⋴⋴⋴⋴⋴⋴⋴⋴⋴⋴ | აწაუგ | ма+ К• | Ga ² • Mg ² • | NH. | ວຂຶ້ສ | TotalC Elem-C Orga-C | |
| Low-volume Sampler | | analysis | Instrument activation analysis | X-ray fluore- scence | FР | AAS | SР | 1 C | Carbon analysis | |
| | | | | | | | | | | |

FP : Flame photometry AMS : Atomic absorption spectrometry SP : Spectrophotometry IC : Ion chromotography

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Table 3-1(2) Average Concentrations of Chemical Components in Particulate Matter

| | Method C of r analysis | Tistication and set and set of the set of t | X-ray fluore- Pb scence Si Si | FР K• | AAS M | SP | 0 | |
|------------------|------------------------------|--|---|-------------------------------|--|--------------|--|--|
| | Compo- nents Average | | | | Ga ² Mg ² · 50 | NH. 574 | 200 200 200 200 200 200 200 200 200 200 | |
| First survey | | 80.0%140.0140.0404040404040404040404040404040 | 2.000+ 388.000 1234.000 1234.000 180.000+ 173 | 380.000 367 728.000 718 | 50.000* 50 50.000* 50 | 574.000 563 | 113 220.000 3625 3700.000 3625 | Note PP SP |
| | Geometric Average Bean | ౸ఴౣ౺౼ౙఀౙ౸ౘ౸౸౸౸ౙఀ౸ఴఀ౸౸ౙఀఀఀఀఀఴఀఴఀఀౢౚ౸౸౸ౢఀౚఀ౸ౘ ౢఴౢఀౙౢఴౢౙౙౙౙ౾ౚౚఄఀౢఴౢౚ౿౿౽౿ఴౢఀౙఴౣఀౢౚ౸౸౸ౢౚౚ౸ౘ ౢఴఀఴౢఀఴౢౙఴౙఴౢఀౙ౾ౚౚఄౢౢఴౢౚ౿౿౽౿ఴౢఴౢ౾ౚౚౢ౾ఴఀౢౚౢౚఀ ౸౸ఀ౻ౢౚఀౘ౸౸ౚఀ౸ఴౚౣౙౢౚ౸౸౸౸ఴఀౢఀౢఴఀౚఀ౺౸ౚఀౚఀౚౚఀౚఀౚ | 2.000* 223.485 1212.282 178.280* 178.280* 150. | 367.236 338. 718.661 414. | 50.000 50. 50.000 50. | 583.516 694. | 113.847 180.000 200.215 188.000 3625.336 4160.000 | * is Flame Atomic Specture |
| Second survey | age Geometric mean | ౸౸ఀ౻ౢ౽౸౸౸ఀ౸ౢౚఀ౸౸ౙఀ౸౸ౙఀఀ౸ౢౘఀఀఀఀఀౢ౼౸ఀఀఀ౸౸ౘఀఀఀఀ౸౸౾ఀఀ౺౸ౙ ౙ౾ఄౙఴౢౢఴఴౢౢౢౢౢౢౢౢౢౢౢౢౢౢౢౢౢౢౢౢౢౢౢౢౢౢౢౢౢౢౢ | 1.500 59.000 1002.000 150.000 150.000 | 338.000 414.000 336. | 50.000± 50. | 694.000 438 | .000 142.154 .000 186.068 .000 3608.637 | is marked when trace date are over 50% Flame photometry Atomic absorption spectrometry Spectrophotometry |
| | 4. 1 | ୦୦୫୦୦୦୦୦୦୦୦୦୦୦୦୦୦୦୦୦୦୦୦୦୦୦୦୦୦୦୦୦୦୦୦୦୦ | 1.500* 35.577* 352.417 150.000* 150.000* 20 | 383.670 35 388.167 25 | 50.000+ 7 50.000+ 5 | 438.535 25 | | e date are trometry |
| Third survey | Average Ge | ౸ૡ૽ૼૡ૱ૡૹૺ૱ૹ૿૱ૡ૱ૡૹ૿૱ૹ૿૱ઌૼૡૡૼ૾૾૱૾૾૱૱ૡૹૺ ૹૢૢૢૺૹૹૢૢૢૢૢૢૢૢૢૢૢૢૢૢૢૢૢૢૢૢૢૢૢૢૢૢૢૢૢ | 20.000+ 200.000+ 200.000+ | 320.000 258.000 | 76.000# 50.000# | 280.000 | 128.000 142.000 2012.000 | over 50% . |
| | Geometric A | ៹ស៊ីលុកកុពី១.ឪភូនេសន៍លន័លនិត០និត្សស្ទីអាកុ០០០០.កីក០នី ខ្លួនខ្លួនខ្លួនខ្លួនខ្លួនខ្លួនខ្លួនខ្លួន | 2.000+ 113.959 1060.578 200.000+ | 324.879 212.964 | 64.600 4 50.000 4 | 168.257 | 115.053 141.487 1844.911 | |
| Average of 3 | Average G | ౸ౙౚౚ౮ౢౢౢౢౢౢౢౢఴౢౢౢౢౢౢౢౢౢౢౢౢౢౢౢౢౢౢౢౢౢౢౢౢౢౢౢ | 1.833* 217.667 1102.000 176.667* | 376.000 456.567 | 58.667# 50.000# | 509.333 | 157.333 183.333 3290.667 | |
| 3 seasons | Georetric Bean | 9.09.00.00.00.00.00.00.00.00.00.00.00.00 | 1.817* 96.766 1069.845 174.874* | 351.332 336.331 338.331 | 54.457 * 50.000* | 346.552 | 123.025 174.896 2880.957 | |
| | Method of analysis | Instrument activation analysis analysis | X-ray fluore- scence | લ | AAS | ЗЪ | U M | |
| | Compo- nents | ⋦ ⋍ ⋦ॺ₽₢⋧⋳⋳⋧⋼⋥⋇⋶⋧⋍⋞⋎%%⋭⋳⋍⋗⋺৶ | <u> ৪</u> ৬% | Na⁺ K• | Ca ²⁺ Mg ²⁺ | . " B | 58 8 2 | |
| First | Average | ៹ ^Ŋ Ⴣ෪Ⴡ෪ඁඁ෪෪෫ඁ෫෧෫෪෪෪෪෪෪෪෪෪෪෪෪෪෪෪෪෪෪෪෪෪෪෪෪෪෪෪෪ | 2.100± 236.000 1016.000 4060.000 | 788.000 180.000 | 620.000 50.000# | 50.00 | 852.000 974.000 1382.000 | |
| survey | Gecmetric mean | 50.00 50 | 2.031± 137.118 974.625 3754.766 | 772.232 173.470 | 577.188 50.000 | 50.00+ | 806.287 971.560 1235.928 | Note; * is FP : Flam AAS : Atom |
| Second survey | Average | 8.9.9.9.9.9.9.9.9.9.9.9.9.9.9.9.9.9.9.9 | 22204.000 22204.000 | 1380.000 148.000 | 524.000 140.000 | 50.000 | 1580.000 1120.000 1682.000 | is marked when Flame photometry Atomic absorption Spectrophotometry |
| survey | Geometric Bean | ౸ఴౢౢఀౚ౺౺ౘ౼౷౸౺౸౸ఴఄ౺ఄ౸ఴౢఀౚౚౙఀౙౙఀ౺౸౸౸౸౸౸ఴఴౚ ౢౢ౽ఄఄ౾ఴౢఴఴౢఴఴఀౢౢౢౢౢఴఴౢౢఀౚఴౢౢఀఴౚౢౢౙౢఴౢౢౢౢౢౙౢౚౢఴఴఴఴౢఴౢఴౢౢౢఴౢౢౢౢౢఴౢౚౢౢౢఴౢఴౢఴౢఴ | 2.000 22.4550 1086.457 2042.156 | 1329.233 130.615 | 484.725 113.123 | 50.000 | 1493.644 1119.309 1412.273 | marked when trace date are over photometry coshotometry cophotometry |
| Third s | Average | -0% 41% 42% 42% 42% 42% 42% 42% 42% 42% 42% 42 | 2.30 100.000 2540.000 | 886.000 102.000 | 38.00 50.00 | 50.00 | 754.000 2000 2000 2000 2000 2000 2000 2000 | are over 50% |
| SULVEY | Geometric mean | ៹ ⁸⁸ -1-467-98 48885-99-9-95889-98 48885-99-9-95889-98 48885-99-9-99-99-99-99-99-99-99-99-99-99-99- | 2.287# 47.330# 1118.754 208.331 | | 36.68 50.00 | 50,000 | 249.164 277.173 287.151 | 12 |
| Average of 3 sea | | 9.9.1.1.1.9.99.9.8.9.9.9.9.9.9.9.9.9.9.9 | 2.13 2.0000 2.00000 2.0000 2.0000 2.00000 2.00000 2.00000 2.00000 2.00000000 | 538.000 143.333 | 50.333 80.00# | 50.00 | 1055.233 794.000 1325.333 | · · |
| 3 seasons | Geometric mean | 989-94-489-989-989-989-989-989-989-989-9 | 2.123 59.107 1058.107 2583.322 | 635-121 025-613 | 458.104 65.632 | 50.00 | 966.284 678.925 1156.491 | |

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Table 3-2 Top Ten Average Concentrations of Chemical Components

| | r | n sample | nderser | A | 1 | | • | CD01 |
|------|------|---------------|---------|-------|--------------|------------------|------|------|
| 1 | Tota | rse 2.1μm) | (> 2 | .1µn) | Fine (< 2 | voluge ampler | | SEQ) |
| 4626 | S04 | 2940 | Si | 3291 | \$04 | 15380 | С | 1) |
| 3117 | SI | 1960 | Cl | 1102 | S | 5033 | S0 | 2) |
| 2347 | CI | 1621 | Ca | 637 | K | 3920 | Si | 3) |
| 2221 | S | 1335 | \$0₄ | 509 | NH4 * · | 1719 | Cl | 4) |
| 1708 | Ca | 1119 | S | 467 | K٠ | 1421 | Na | 5) |
| 1457 | Na | 1055 | C1 - | 460 | Zn | 1412 | Ca . | 6) |
| 1314 | Na⁺ | 1042 | Na | 415 | Na | 1359 | Na* | 7) |
| 1213 | C1 - | 951 | Al | 387 | CI | 1294 | Fe | 8) |
| 1201 | Fe | 938 | Na * | 376 | Na• | 1268 | S | 9) |
| 1120 | К | 913 | Fe | 288 | Fe | 975 | К | 10) |

Note) Larbon is measured by low volume sampler, but not measured by andersen sampler.

3.2 Spatial Distribution of Chemical Components

Fig. 3-1 shows the spatial distribution of the concentration of representative chemical components. These components are considered to be marker elements of the main emission sources. The marker elements are as follows: All results are shown in the APPENDIX.

| Sc, Al, Ti | Soil |
|--------------------------------------|--|
| Na, Cl, Na ⁺ | Sea-salt particle |
| Pb, Br | Gasoline automobile |
| v | Petroleum combustion |
| Mn, Cr, Fe | Steel mill |
| Zn, K | Wastes incineration and Glass industry |
| Ca, Si | Road dust |
| SO4 ²⁻ , NO3 ⁻ | Secondary particle |
| Organic C | Diesel automobile |

The spatial distribution of these components classified by main emission sources are as follows:

(1) Soil

The highest concentration of Sc, Al and Ti are measured at MS5 compared with other monitoring stations as the location of MS5 is surrounded by fields. The concentration of those at MS1 and MS4 also are relatively high, which may be due to the dust blown up from roads.

(2) Sea-salt particle

The concentration of Cl, Na and Na⁺ are relatively high at MS2, MS3 and MS4 located near Chao Phraya river, but their concentrations are low at MS1 and MS5 located in inland sites.

(3) Gasoline automobile

The concentration of Br is relatively high at MS1 and MS4 located near roads. It seems due to the influence of the exhaust gas from gasoline automobiles. But, the concentration of Pb at those monitoring stations are low contrary to our expectation in spite of Pb as well as Br being contained in the exhaust gas of gasoline automobiles. We cannot figure out the cause of the phenomenon. At MS5, the concentration of Pb is found to be extremely low.

(4) Petroleum combustion

V (Vanadium) is the marker element of petroleum combustion. The concentration of V is relatively high at MS2 and highest at MS3. The amount of V in fine particles is found always higher than that of coarse particles.

(5) Steel mill

The concentrations of Mn, Cr and Fe at MS3 are extremely higher than the concentration of those at other monitoring stations. This seems due to the influence of the electric arc furnace plant located near MS3.

(6) Wastes incineration and Glass industry

Zn and K are marker elements of incineration of the wastes and Glass industry. The concentration of Zn at MS3 is extremely high, but the concentrations of K maintains almost the same level in all monitoring stations.

(7) Road dust

Ca and Si arc originated from road dust picked up by car transportation or from soil blown up by wind. The little differences of the concentration of those elements between the monitoring stations are found.

(8) Secondary particle

Generally, SO_4^{2-} and NO_3^{-} have their origin in secondary particles, and the regional difference of the concentration of SO_4^{2-} and NO_3^{-} are found not so clear because the reaction speed of " $SO_2 \rightarrow SO_4^{2-}$ " and " $NO \rightarrow NO_3^{-}$ " is slow. Therefore, the regional difference of NO_3^{-} is found not clearly in this study. But significant differences of SO_4^{2-} concentration between the stations were found. This is probably due to the reason that SO_4^{2-} also originates from sea-salt.

(9) Diesel automobile

The concentration of organic carbon is relatively high at MS1, MS3 and MS4. Diesel car and vessels are thought contributing to concentration at these monitoring stations.

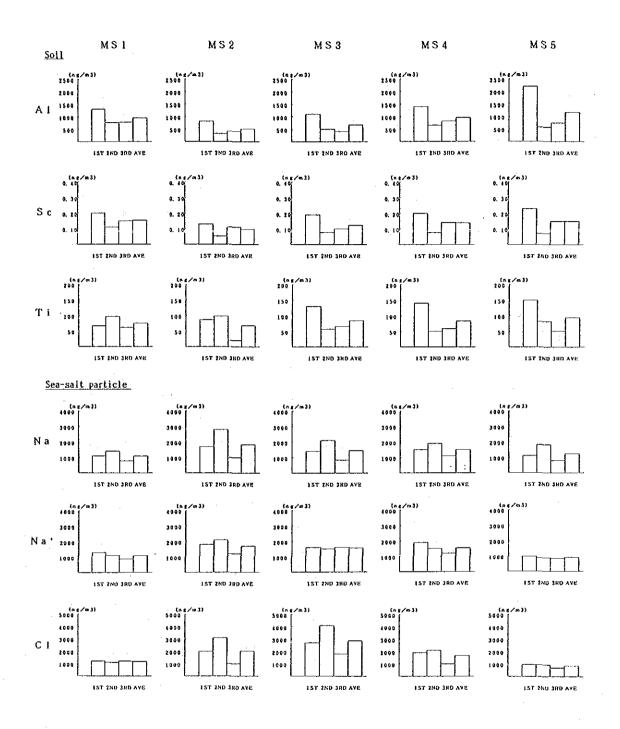


Fig. 3-1(1) Spatial Distribution of Chemical Components (Low-Volume Sampler)

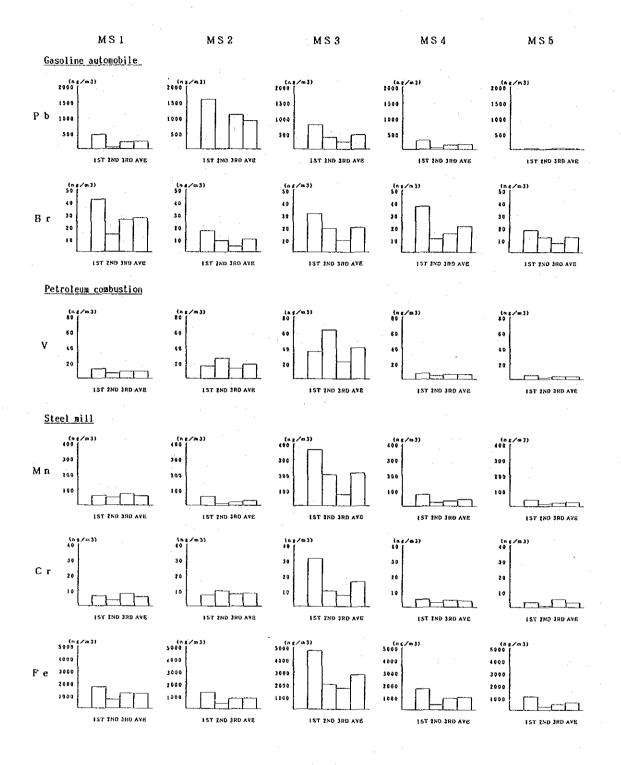


Fig. 3-1(2) Spatial Distribution of Chemical Components (Low-Volume Sampler)

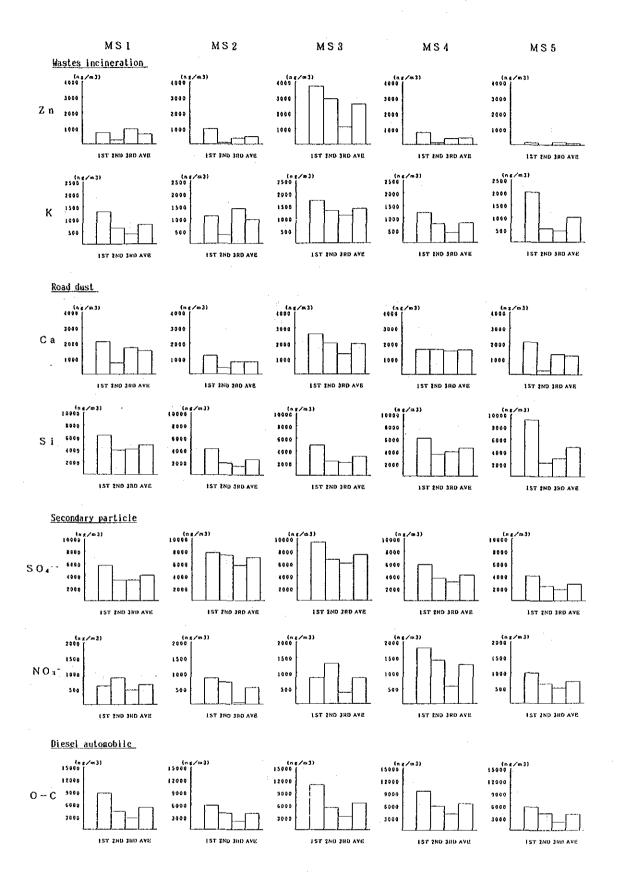


Fig. 3-1(3) Spatial Distribution of Chemical Components (Low-Volume Sampler)

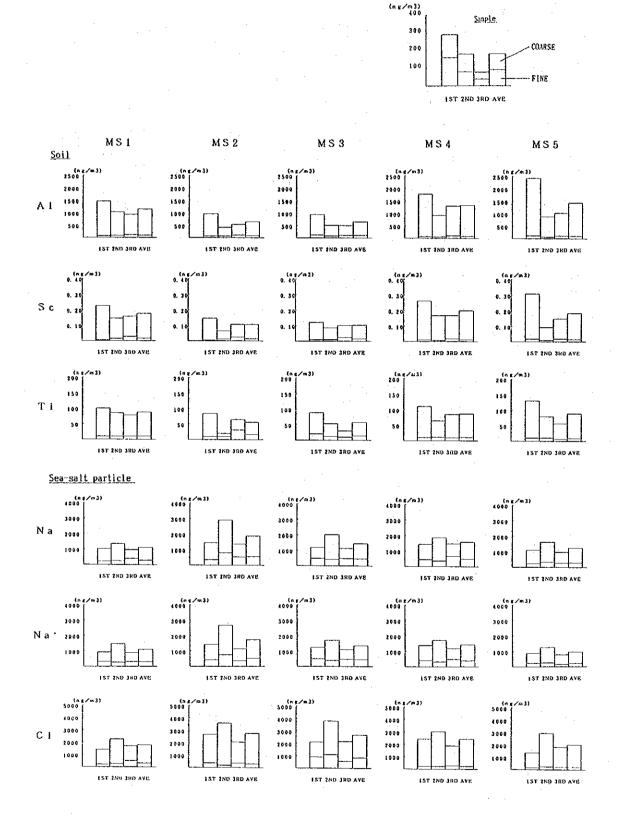


Fig. 3-1(4) Spatial Distribution of Chemical Components (Andersen Sampler)

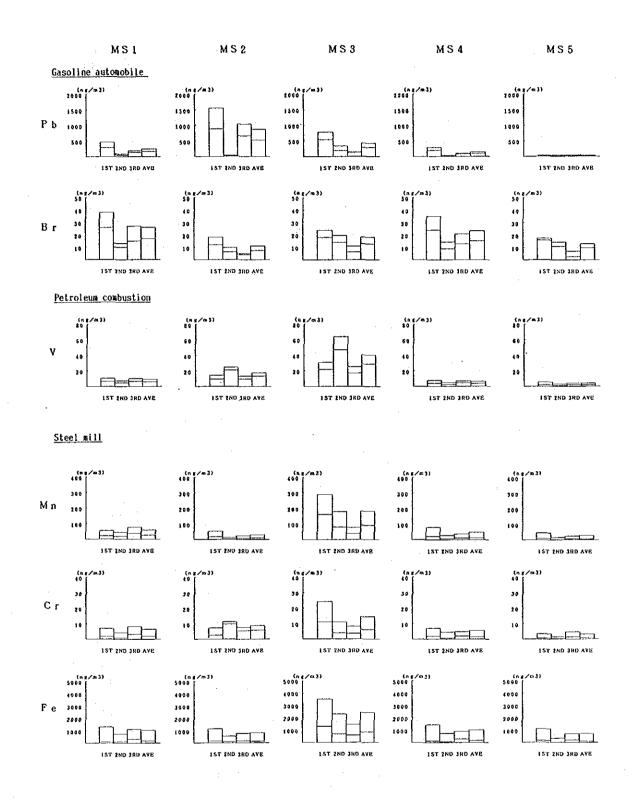


Fig. 3-1(5) Spatial Distribution of Chemical Components (Andersen Sampler)

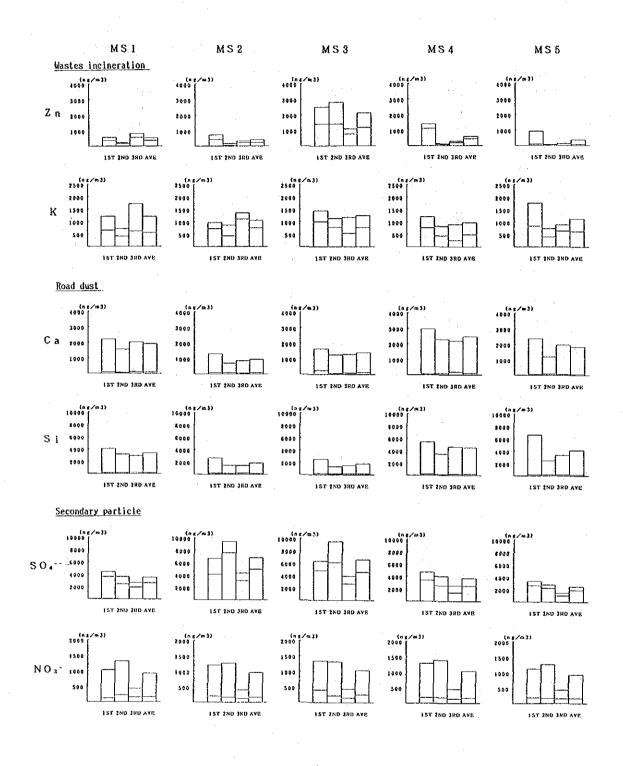


Fig. 3-1(6) Spatial Distribution of Chemical Components (Andersen Sampler)

3.3 Comparison of the Concentrations of Chemical Components between Monitoring Stations

This section discusses the comparison of the concentration of chemical components between MS5 having the lowest concentration of TSP and other monitoring stations.

Fig. 3-2 shows the results of the comparisons, and the X and Y axes are shown logarithmically because the chemical component concentrations vary in the broad range of $10^{-2} \sim 10^4$ ng/m³. These concentrations positioned above the 45° diagonal line, correspond to concentrations higher than those of MS5. The data smaller than the detection confidence level are excluded because of unreliable figures. The element concentration analyzed by fluorescence X-ray method has the symbol (*) attached to elemental ones.

Observed points through this comparative study are:

(1) MS1

The difference of concentration of each chemical component between MS1 and MS5 is relatively large, above all with respect to Pb, Zn, Sb, V, Mn. This trend is probably due to the effects of petroleum combustion, automobiles, steel mills, wastes incineration and the glass industry.

(2) MS2 and MS3

Since MS2 and MS3 locate in an industrial area, the concentrations of chemical components, are high except for the marker components of soil and secondary particles. It is thought that the high concentration of V is due to burning of petroleum, those of high Mn, Cr and Fe to steel mills, Na, Cl and Cl⁻ to sea-salt particles, and Zn and Sb to wastes incineration and glass industry, respectively.

(3) MS4

The concentrations of Pb, Zn, V, Sb and Cl^- are relatively high. But the concentrations of other components showed the same levels as those at MS5.

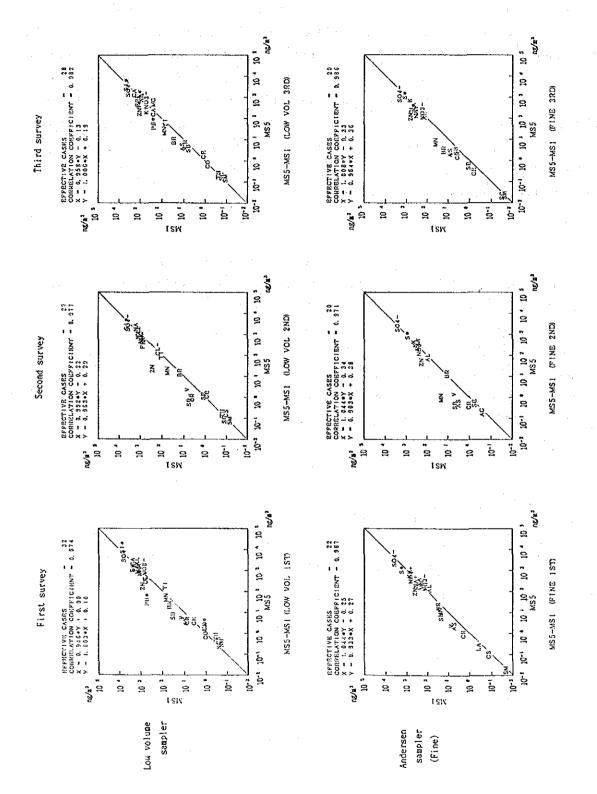
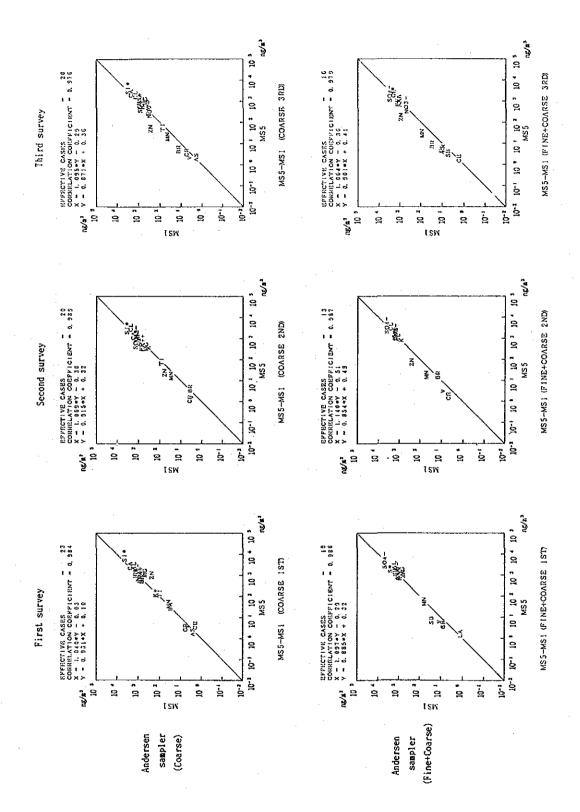
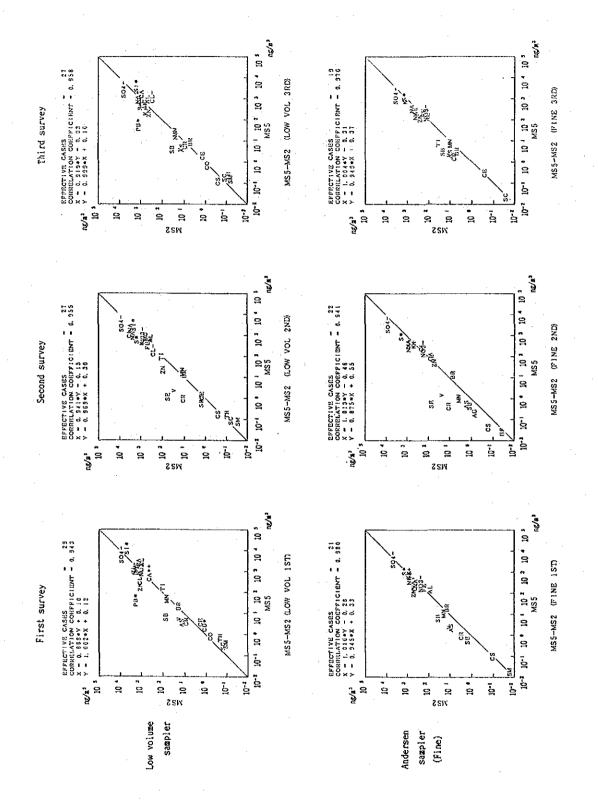


Fig. 3-2(1) Concentration of Chemical Components in MSS and MS1

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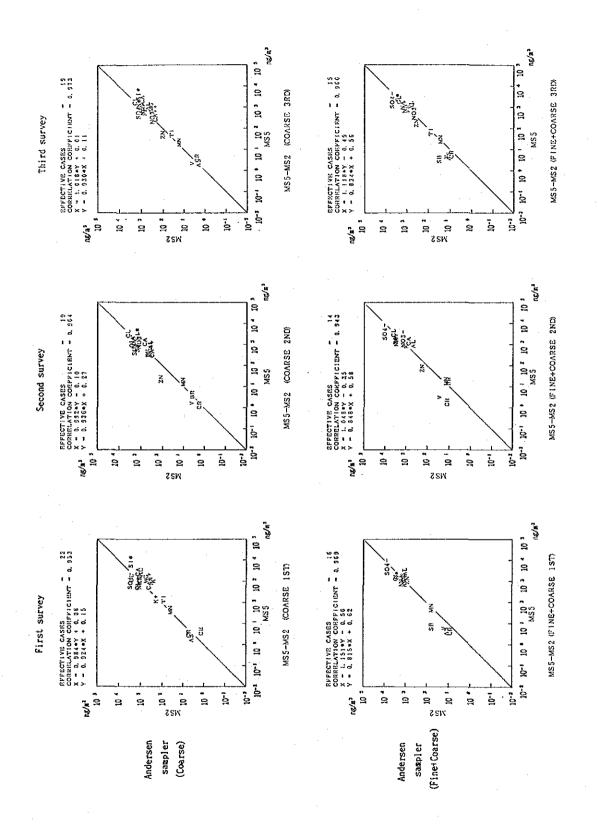








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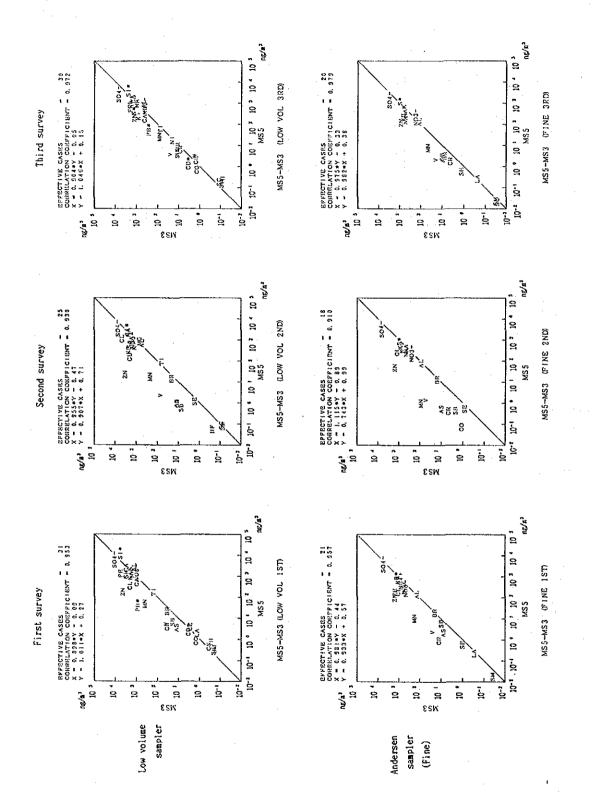


Fig. 3-2(5) Concentration of Chemical Components in MS5 and MS3

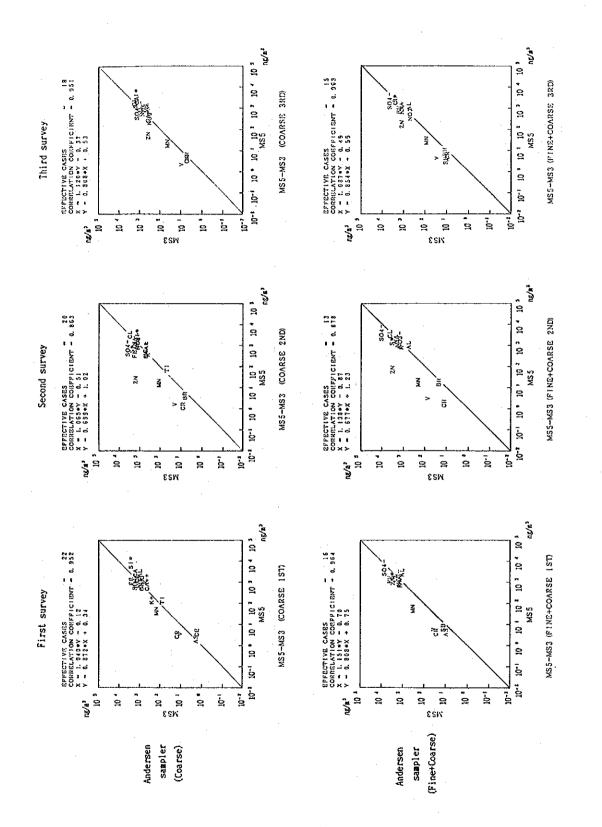


Fig. 3-2(6) Concentration of Chemical Components in MS5 and MS3

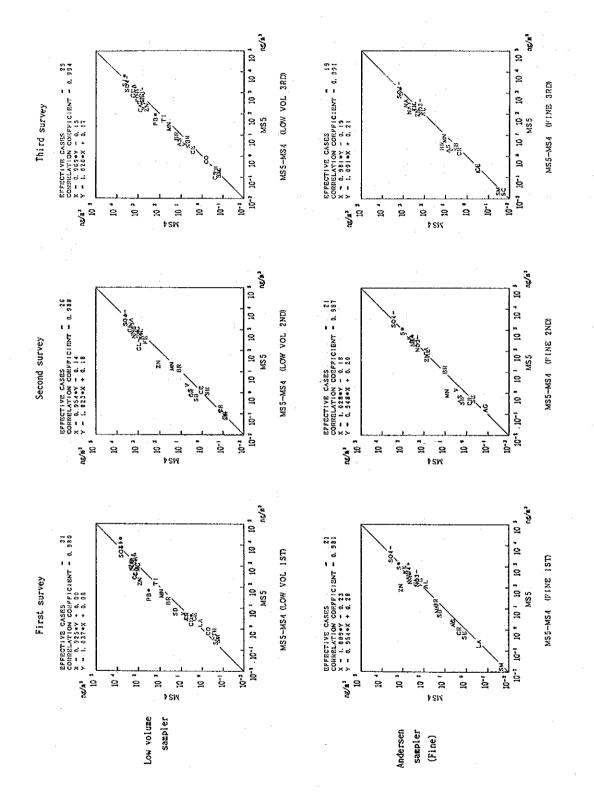
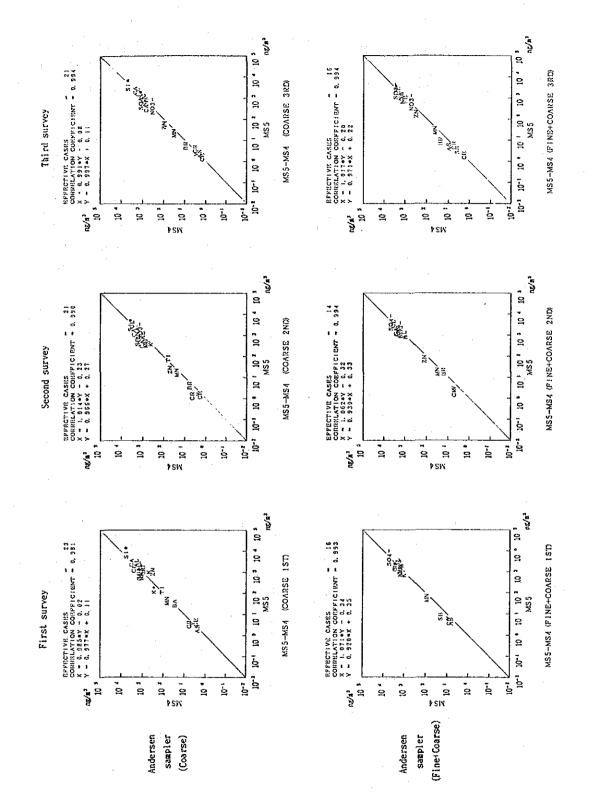


Fig. 3-2(7) Concentration of Chemical Components in MS5 and MS4

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3.4 Resemblance among the Monitoring Stations by Cluster Analysis Based on Correlation Coefficients of Chemical Components Concentration

The cluster analysis is sometimes instrumental for us to elucidate the regional resemblance among monitoring stations. Taken as a measure to represent the degree of regional resemblance in this study is the correlation coefficient calculated with respect to concentration of chemical components contained in total suspended particulate collected by Low-volume sampler and Andersen samplers among monitoring stations. As for TSP collected by Andersen sampler, the sample was divided into two parts, coarse and fine particle fractions and cluster analysis was done. The group averaging method were used as the solution methods for cluster analysis in this study. In order to avoid the effect by absolute value of each chemical component influencing the correlation coefficients, the data were normalized according to the equation (3-1). For the data which have values less than the detection minimum, a half value of such detection limit was assigned to them. Also, the chemical components having the value less than the detection minimum by more than 50% were excluded from the calculation.

$$Z_{\alpha i} = \frac{X_{\alpha i} - \overline{X}_{\alpha}}{S_{\alpha}}$$
(3-1)

where

 $Z_{\alpha i}$; normalized concentration value of component α at point i

 $X_{\alpha i}$; absolute value of component α at point i

 \overline{X}_{α} ; means of 5 points with respect to component α

 S_{α} ; standard deviation of 5 points with respect to component α

The correlation coefficient of chemical components concentration among regions and the results of cluster analysis are shown in Table 3-3 and Fig. 3-3 respectively. While admitting some difference coming from seasonal changes and types of dust meters, one can notice the following three clusterings to represent the regional difference.

(1) the region adjoining industrial areas represented by MS2 and MS3 stations

(2) the region apart from industrial areas represented by MS4 and MS5 stations

(3) the region neighboring the urban area represented by MS1 position

Table 3-3 Correlation Coefficient of Chemical Components Concentration among Monitoring Stations

ist survey

lst survey

| | IS1 | MS2 | MS3 | MS4 | MS5 | |
|---------------------------------------|-------|--------------|------------------------|-----------|-----|----------|
| MS1) ONEB STATION | / | | | | | |
| MS2) POWER PLANT | -0.33 | \backslash | | | | |
| MS3) MIN. DEP. DFFICE -0.23 0.08 | -0.23 | 0.08 | | | | |
| MS4) S.P.PR0.0FFICE -0.24 -0.16 -0.26 | -0.24 | -0.16 | -0.26 | \square | | |
| MS5) H.S. I. ESTATE | 0.07 | -0.62 | 0.07 -0.62 -0.51 -0.21 | -0.21 | Ζ | <u> </u> |
| 2nd survey | | | | | | |

| | | NS 1 | MS2 | X 53 | MS4 | MS5 |
|-------|-----------------------|-------------|------------------|------------------------|-------|--------------|
| ŝ | MSI) ONEB STATION | Z | | | | |
| NS2) | MS2) POWER PLANT | -0.56 | | | | |
| (ESI) | MS3) MIN. DEP. OFFICE | -0.38 -0.24 | -0.24 | \langle | | |
| VS4) | MS4) S.P. PRO. OFFICE | 0.03 | 0.03 -0.45 -0.23 | -0.23 | / | |
| NS5) | MSS) H.S I. ESTATE | 0.45 | -0.11 | 0.45 -0.11 -0.69 -0.03 | -0.03 | \mathbb{Z} |
| | | | | | | |

| 3rd survey | | | | | |
|-----------------------|------------|-------------------|------------------------|------|-----|
| | NS1 | NS2 | MS2 MS3 | WS4 | MS5 |
| MSI) DNEB STATION | Δ | | | | |
| MS2) POWER PLANT | -0.59 | | | | |
| MS3) MIN. DEP. OFFICE | -0.11 0.17 | 0.17 | | | |
| MS4) S.P.PRO.OFFICE | -0.06 | -0.06 -0.51 -0.58 | -0.58 | Λ | |
| MS5) H.& I. ESTATE | -0.06 | -0.37 | -0.06 -0.37 -0.67 0.35 | 0.35 | / |
| All seasons | | | | | |
| | ۲ ۲۷۶ | 459 | 553 | NCA | ビンス |

| All seasons | | | | | |
|-----------------------|-------|-------------------|------------------------|-------|-----|
| | NS I | HS2 | WS3 | MS4 | MS5 |
| MSI) ONES STATION | / | | | | |
| POWER PLANT | -0.49 | / | | | |
| MS3) MIN. DEP. OFFICE | -0.28 | 0.00 | / | | |
| MS4) S.P.PRO.OFFICE | -0.03 | -0.03 -0.37 -0.39 | -0.39 | / | |
| MS5) H.& I. ESTATE | 0.03 | -0.41 | 0.08 -0.41 -0.52 -0.01 | -0.01 | / |
| | | | | | |

| | I SH | MS2 | MS3 | MS4 | MS5 |
|-----------------------|-------------|------------------------|-----------|-------|--------------|
| MSI) QNE8 STATION | | | - | | |
| MS2) POWER PLANT | -0.20 | | | | |
| MS3) MIN. DEP. OFFICE | -0.65 -0.31 | -0.31 | \langle | | |
| MS4) S.P.PRO.OFFICE | 0.06 | 0.06 -0.26 -0.24 | -0.24 | | |
| MSS) H.& I. ESTATE | -0:13 | -0.13 -0.43 0.03 -0.30 | 0.03 | -0.30 | \mathbb{Z} |
| 2nd survey | | | | | |

| i | | | | | | | |
|------------|-------------|-------------------|------------------|---------------------|---------------------|--------------------|--|
| | NS5 | | | | | \mathbb{Z} | |
| • | MS4 | | | | / | 0.51 | |
| | KS X | | | | -0.38 | -0.41 | |
| | NS2 | | \langle | -0.54 | -0.21 -0.21 -0.38 | -0.23 -0.16 -0.41 | |
| | I SM | / | -0.48 | -0.02 -0.54 | -0.21 | -0.23 | |
| 2nd survey | | MSI) ONEB STATION | MS2) POWER PLANT | MS3) MIN.DEP.OFFICE | MS4) S.P.PRO.OFFICE | MSS) H.& I. ESTATE | |
| 2nd | | (1 SM) | (S2) | MS3) | MS4) | NS5) | |

3rd

| | | NS1 | HS2 | 8SM | XS4 | 8SF. |
|-------|---------------------|-------------|------------------------|-------------|---------|--------------|
| (1SN | MS1) ONEB STATION | Ľ | | | | |
| MS2) | MS2) POWER PLANT | ې 8.9 | V | | | |
| MS3) | MS3) MIN.DEP.OFFICE | -0.14 -0.25 | -0.25 | \langle | | |
| AS4) | MS4) S.P.PRO.OFFICE | ଷ ୧ | -0.29 -0.37 -0.29 | -0.23 | | |
| (SSI) | MS5) H.& I. ESIATE | 0.10 | 0.10 -0.36 -0.38 -0.33 | 8 8 9 | -0 8 | \mathbb{Z} |
| ALL | All seasons | ľ | | | | |

| 2 X23 X24 X25 | | | 21 | 31 -0.28 | -0.09 -0.29 -0.23 -0.03 |
|---------------|-------------------|------------------|-----------------------|---------------------|-------------------------|
| MS1 MS2 | Ζ | -0.35 | -0.32 -0.37 | -0.11 -0.31 -0.28 | 0-00-0- |
| | #SI) ONEB STATION | MS2) POWER PLANT | MS3) MIN. DEP. OFFICE | MS4) S.P.PRO.OFFICE | MS5) H.S. I. ESTATE |

| | %S5 | | | | | 7 | |
|------------|--------|-------------------|------------------|-----------------------|----------------------|-----------------|--|
| | MS4 WS | | | | | 0.05 | |
| | | | | 7 | 2 | 53 0. | |
| | 2 MS3 | | - | 8 | 12 -0. | 65 -0. | |
| | 1 MS2 | 7 | 4 | 27 0.03 | -0.05 -0.12 -0.54 | 014 -0.65 -0.53 | |
| | 15% | 4 | -0.41 | E -0.27 | | | |
| | | NOLTH | LANT | 05510 | OFFIC. | ESTATE | |
| lst survey | | NE8 ST | OWER P | I.N. DEP | .P.PRO | | |
| ist s | | MS1) DNES STATION | MS2) POWER PLANT | MS3) MIN. DEP. OFFICE | MS4) S.P.PRO. OFFICE | MS5) H.& I. | |

| 255 | | | | | / | | MS5 | | | | | / | | MSS | | | | | ſ |
|-----|-----------------|----------------|------------------|----------------|---------------|--------|-----|--------------|-------------|----------------|-------------------|---------------|--------|------------|--------------|-------------|-----------------------|----------------|---|
| 2 | | | | / | 0.05 | | NS4 | | <u>`</u> | | / | 0.30 | | XS4 | | | | /_ | |
| 2 | | | \mathcal{V} | -0.54 | -0.53 | | NS3 | | | | -0.64 | -0.62 | | HS3 | | | / | -0.67 | |
| 22 | | $\overline{/}$ | 0.03 | -0.12 | -0,65 | 1 | YS2 | | V | 0.8 | -0.43 | -0.47 | ÷. | 725 7 | | | 0.13 | -0.20 | |
| ē | 7 | -0.41 | -0.21 | -0.05 | 0_I4 | | is: | Z | -0.74 | -0.40 | 0.23 | 0.52 | | NS1 | Ľ | F0.8 | F-0.13 | -0.13 | |
| | NOITATE SEATION | POWER PLANT | MIN. DEP. OFFICE | S.P.PRO.OFFICE | H.& I. ESTATE | survey | | ONEB STATION | POWER PLANT | MIN.DEP.OFFICE | S. P. PRO. OFFICE | H.& I. ESTATE | survey | | ONEB STATION | POWER PLANT | AS3) MIN. DEP. OFFICE | S.P.PRO.OFFICE | |
| | MS 1) | NS2) | HS3) | MS4) | MS5) | 2nd | | (1S); | (25) | MS3) | (S4) | MS5) | 3rd | | 11 SH | NS2) | NS3) | (JSK) | |

| ord survey | vey | | | | | |
|-------------|---------------------|-------------------|----------------|-------|---------|------------|
| | | NS I | XS2 | MS3 | %S4 MS5 | XS5 |
| S1) ONE | MS1) ONEB STATION | / | | | | |
| S2) P0W | MS2) POWER PLANT | -0.64 | $\overline{/}$ | | | |
| S3) MIN | MS3) MIN.DEP.OFFICE | -0.13 0.13 | 0.13 | / | | |
| S4) S.P | MS4) S.P.PRO.OFFICE | -0.13 -0.20 -0.67 | -0-20 | -0.67 | / | |
| S5) H.& | MS5) H.& I. ESTATE | -0.18 -0.36 -0.55 | -0.36 | -0.53 | 0.26 | / |
| All seasons | sons | | | | | |
| | | | 1 | - | | |

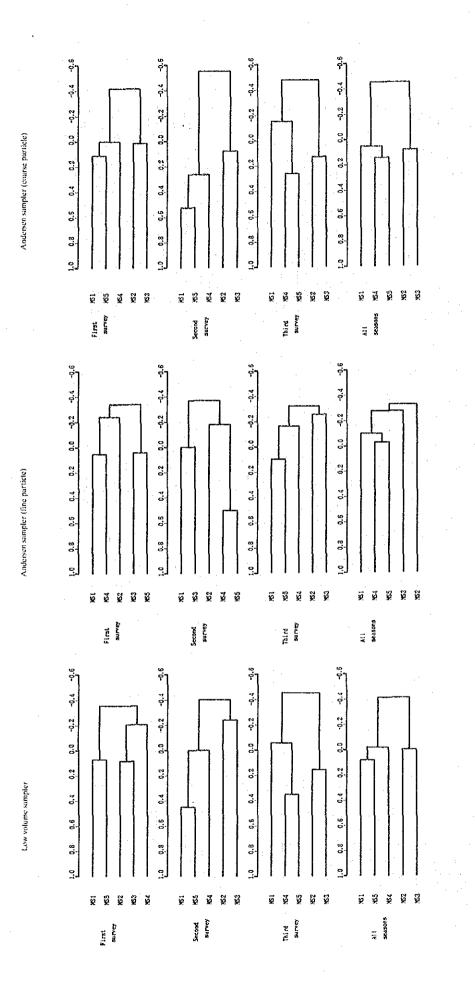


Fig. 3-3 Hierarchical Structure of Monitoring Station by the Cluster Analysis

3.5 The Relationships between Chemical Components

The relationships between chemical components were analyzed in this section. As it is difficult to analyze the relationship of all combinations of chemical components because of the number of combinations involved, the analytical study was limited to seven emission sources and the pairs of chemical components of each emission source are selected as shown in Table 3-4.

| Soil | Sea-salt | Secondary particle | Petroleum combustion | Steel mill | Automobile | Others |
|--|--|---|--|---|--|--|
| AI-Sc AI-Ti AI-Si AI-Fc Sc-Ti Sc-Si Sc-Fc Si-Ti Si-Fc Fc-Ti AI-Ca Si-Ca Sc-Ca Ti-Ca | ClNa Cl ⁻ -Na SO ₄ ²⁻ -Cl SO ₄ ²⁻ -Na BrCl BrNa BrSO ₄ ²⁻ BrCl | NH4 ⁺ -SO4 ²⁻ NH4 ⁺ -NO3 ⁻ Na-NO3 ⁻ SO4 ²⁻ -NO3 ⁻ | $S-SO_4^{2-}$ $V-SO_4^{2-}$ $V-S$ $V-clemental carbon (V-E-C) V-organic carbon(V-O-C)$ | Cr-Mn Fe-Mn Fe-Cr Ca-Mn Ca-Cr | Pb-Br Pb-E-C Pb-O-C Br-E-C Br-O-C Br-SO ₄ ²⁻ Br-NO ₃ ⁻ Br-K E-C-SO ₄ ²⁻ O-C-SO ₄ ²⁻ | E-C-Zn O-C-Zn E-C-K O-C-K Pb-As Zn-K Zn-K Zn-As Pb-Sb Zn-Sb |

Table 3-4 Pair of Components for the Relationship Among Chemical Components

The result of regression analysis among various chemical components concentration is summarized in Table 3-5, in which data are treated in two ways, one excluding those less than the detection limit and the other applying a half value of the detection limit value for such data smaller than the detection limit. The correlation coefficients diagram among chemical components concentration is exemplified in Fig. 3-4 and the rest is filed in Data Sheets.

Reviewing those analytical data, one can notice a significant correlation coefficient ($r \ge 0.8$) between two components listed below.

• Low-volume sampler case

Al-Sc, Al-Si, Sc-Si, S-SO42, Br-E-C, Br-O-C, Cr-Mn, Fe-Mn, Fe-Cr, Pb-Sb

Andersen sampler case (with respect to TSP)

Al-Sc, Al-Ti, Al-Si, Sc-Ti, Sc-Si, Si-Ca, Sc-Ca, Cl-Na, Cl^- -Na, NH_4^+ -SO $_4^{2-}$, Cr-Mn, Fe-Mn, Fe-Cr, Pb-Sb

- Andersen sampler case (fine particles only)
 Al-Sc, NH₄⁺-SO₄²⁻, Fe-Mn, Ca-Mn, Pb-Sb
- Andersen sampler case (coarse particles only)
 Al-Sc, Al-Ti, Al-Si, Sc-Ti, Sc-Si, Si-Ti, Si-Ca, Sc-Ca, Cl-Na, Cl⁻-Na, V-S, Cr-Mn, Fe-Mn, Fc-Cr, Pb-Sb

Above all, noteworthy is a significant correlation ($r \ge 0.9$) among those chemical component combinations of coarse particles in the Andersen sampler. The chemistry of such components is thought identical to those of soil and thus components like Al, Sc, Ti, Si or coarse particles have

their origin in soil of the ground.

The combination of Cl-Na or Cl^--Na of coarse particles are found the same in a significant correlationship and it is thought most likely that they exist in NaCl form as sea salt and in the coarse particle range.

Another high correlation tound in combinations of Cr-Mn, Fe-Mn, Fe-Cr of coarse particles may be traced back to steel plant dust or it is thought contributory to the coarser size range of trapped dust.

The combination of Pb and Sb also shows a significant correlation and is thought attributable to the glass industry as an element source.

As for fine particle size, a significant correlation seen in $NH_4^+ - SO_4^{--}$ suggests the existence of $(NH_4)_2SO_4$ salt as a secondary particle. But the NH_4NO_3 salt is less likely to exist since the regression coefficient is found to be 0.152. The reason to support this conclusion is that the NO_3^- ion generally exists as a nitric acid fume and reacts with NaCl of sea salt to form the NaNO₃ coarse particle. But in a cold climate, the nitric acid particle formed by heterogenous nucleus reaction neutralizes the NH_4^+ ion to form NH_4NO_3 fine particles¹¹. Accordingly, it is thought that in the warm climate of Thailand, the correlation coefficient of NH_4^+ and NO_3^- remains small (r=0.152) and that of Na and NO_3^- remain comparatively larger (r=0.680) in the coarse particle size range.

| Ш | - | 129 |
|---|---|-----|

| ٢ | | я, | កម្មស្មិតម្មស្មិតម្មស្មិត | លីសីសីលីសីសីសី | សិសិសិសិស | សងរស | សតេសតេសតេស | សិសិសិសិសិ | ស៊ីស៊ីស៊ីស៊ីស៊ីស៊ីស៊ីស៊ីស៊ីស៊ីស៊ីស៊ីស៊ីស |
|-----------------|--------------|----|--|---|--|--|--|--|---|
| value for trace | | s. | 0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0. | 55555555555555555555555555555555555555 | 0.5%1 0.5%3 0.5%3 0.2%3 0.2%3 0.215 | 0.157 0.157 0.167 0.140 | 00000000000000000000000000000000000000 | 0.892 0.947 0.658 0.658 0.468 | 0.555 0.557 0.557 0.552 0.5550 0.5550 0.5550 0.15555 0.15555 0.15555 0.15555 0.15555 0.15555 0.15555 0.1555 |
| | Value | q | 0.0 88.5 89.5 89.5 89.5 89.5 89.5 89.5 89.5 | 711.91 1484.41 1884.41 1884.41 1884.41 1884.43 1851.43 1553.28 3891.07 521.88 | 1423.70 3842.46 3865.27 3865.27 4645.38 | 3619. 16 714. 45 220. 35 651. 83 | 17.21 9170.30 9170.30 4781.57 4781.57 1718.31 1719.31 5331.07 5331.47 5531.68 1677.38 2533.68 2533.68 | -13.05 28.19 29.15 29.15 29.15 20.15 21.05 | |
| | Adopted nati | ß | 9. 77±10-1 9. 77±10-1 9. 550 9. 550 9. 550 9. 550 9. 140 9. 140 140 140 140 140 140 140 140 140 140 | 0.0.0.9 0.0.0 0.0 0.0 0.0 0.0 0.0 0 0.0 0 0.0 0 0.0 | 2882828 888788 8887888 | 0.000 88.00 88.00 88.00 88.00 | 0.403 2.874 2.874 1.130 1.91.073 191.073 191.073 162.046 16.036 1 | 11.640 0.079 0.079 0.005 0.005 | |
| - | 1 | a | ដងសូមិនសូមិនសូមិនដែល | ងសម្ភងក្មស្ត | សិសិសិសិសិ | r-133 | 44488884888 | ភាពភាជា | <u> </u> |
| le sampler | 3 | - | 22222222222222222222222222222222222222 | 50000000000000000000000000000000000000 | 0.286 | 0.212 | 0.0.00000000000000000000000000000000000 | 00000 8.989 8.888 1.8888 1.8888 1.8888 1.8888 1.8888 1.8888 1.8888 1.8888 1.8888 1.8 | 0.555 0.410 0.410 0.459 0.458 0.563 0.563 0.563 0.563 0.563 |
| 3 | t for trace | Ą | ୦.୫.୫.୫. ୫.୪.୫.୫.୫.୫.୫.୫.୮.୮୦୦ ୫.୪.୫.୫.୫.୫.୫.୫.୫.୫.୫.୫.୫.୫.୫.୫.୫.୫.୫.୫ | 711.91 1484.41 1581.65 550.33 550.33 1551.43 1551.43 1551.43 1551.43 1551.43 1551.43 1551.43 | 285.27 885.27 885.27 885.27 885.27 885.38 | 888558 88788 88788 | 17.85 3555.75 3555.75 4778.87 4778.87 4778.87 3591.03 3591.07 5591.55 5591.65 5591.750 | -13.49 -28.19 0.15 -4.26 | -722,55 574,41 891,64 891,64 81,04 81,01 81,04 81,01 81,04 81,01 81,04 81,01 81,04 81,0100,0000000000 |
| ical Except | EXCet | а | 9. 77*10 ⁻⁵ 9. 77*10 ⁻⁵ 9. 74*10 ⁻⁵ 9. 0.044 9. 108 907. 1085 907. 1085 9 | 0.412 0.303 0.303 0.216 0.303 | 22.28 23.28 2.28 2 | 3.149 0.282 0.082 | 0.000 101.073 100.073 | 11.640 0.073 0.073 0.118 0.118 0.118 | 0.000.000 0.000.000 0.000.000 0.000.000 |
| | Uleates[| XX | AAAAXXXXXXXAXXX " | ល ខ្លះ 2 ខ្លះ 2 ខេន្តនេះ ខេន្តនេះ ខេន្តនេះ ខេន្ត ខេត ខេត្ ខេត្ ខេត្ | | NH4 • 504 ^z - NH4 • 1003 ⁻ NH4 = 1003 - S04 ^z - 1003 - | Pb B Pb B Pb B Pb B Pc S Pc S Pc S | ກ ສອງ ສອງ ເຊິ່ງ ເຊິ່ງ | 6090 0100 88888 88888 8888 8888 8888 8888 |
| - | ย 5 | i | 1105 | 1162-692 | สปราการใ กราวราช | particle Secondary | ari lozzi af irlozotus | l9912 ∐i∎ | olliers |

Table 3-5(1) Results of Regression Analysis between Chemical Components

ល្អប្មស្មាល ដេដេដ លីលីសីសី លី២លីសី សិកិតតិសិក សិសិរថិសិសិលីល Adopted half value for trace data đ 0.514 888.88 888.88 0.745 0.782 0.673 (Andersen sampler , Fine+Coarse) ្តូនទទួនទទួនទទួនទទួនទទួន ខ្លួនទទួនទទួនទទួនទទួន ខ្លួនទទួនទទួនទទួនទទួន ទទួនទទួនទទួន ងគខ 5226 8458 នក្ខន្មន្លន 1158.1 513.1 523.1 523.5 2757 2757 2003 1.628.88 م ผลื่อวิธีอ 8.51 8.52 8.51 0.001 8888 90009 90009 8823388688 in regression line. Y = a X + b, a : regression coefficient b : intercept r : correlation coefficient n : number of data ဝဝဝဝ႙ဒ္ဒလဲရှိ w ក្មាភិភាពក្ ក្មសិតក្ម ក្ដីស្ដីភ្ន ដដាកាត សីសិកសិកសិក d 0.523 0.541 0.544 0.581 0.581 0.581 0.581 0.581 0.581 0.581 0.785 0.785 0.679 256423338969.0.0.0 25642338969.0.0.0 25642338969 0.955 0.457 0.457 558 9.0.0 88888 88888 0.881 0.882 0.856 0.856 0.856 0.856 0.856 data ы trace 50.25 20.25 ងនុទ្ធ១៩១ នទេនទេន 8=e88488a4222e3 288888846 សតុខ 39P5 o, 8883 8883 8883 85.23.23.23.38 8898 Except for 3.825 20.857 20.857 0.0000 8233800 823800 82800 1.21±10-1 21±10-1 21557-505 -2.0300 -2.03000 -2.03000 -2.03000 -2.03000 -2.0300 -2.0300 -2.0300 -2.0 Note) ð S = 50,2+ V = 50,2+ V = 5 Pb = Br Br = S0, 2 Br = N03, NH, • SO, • NH, • NO, NA = NO, SO, • • NO, 255233 ***** \$£2223 Chemical components X Y particle Secondary eni losel Stidozofine Retroleum Rotiendari 19912 11 ia ຮາວທານ 3162-692 Hos

Table 3-5(2) Results of Regression Analysis between Chemical Components

| | | | · . | | | | | |
|----------------------------------|-------------------|--|---|---|---|---|---|--|
| data | a | លីសីសីសីសីសីសីសីសីសីសីសី | លកកកកកកក | សកត | ងដសដ | លីសីសីស | កតកកកក | ដដដដ |
| trace | ч | 0.233 0.022 0.0200 0.0200 0.0200 0.0200 0.02000 0.02000 0.02000 0.02000 0.0200000000 | 00000000000000000000000000000000000000 | 0.485 0.741 0.036 | 0.267 | 0.103 0.116 0.242 0.173 | 0.983 | 0.617 0.482 0.582 0.585 0.585 0.151 |
|) If value for | ٩ | 24.25 8.25 8.25 8.25 8.25 8.25 8.25 8.25 8 | 2201.13 2302.13 2302.28 2302.12 2307.05 2307.05 117.30 | -36.23 2134.71 1038.02 | 948.58 157.78 141.92.90 | 11.94 2207.05 152.75 152.85 | -4-73 15.86 0.61 0.61 | 3.38 3.19 2.07 2.07 |
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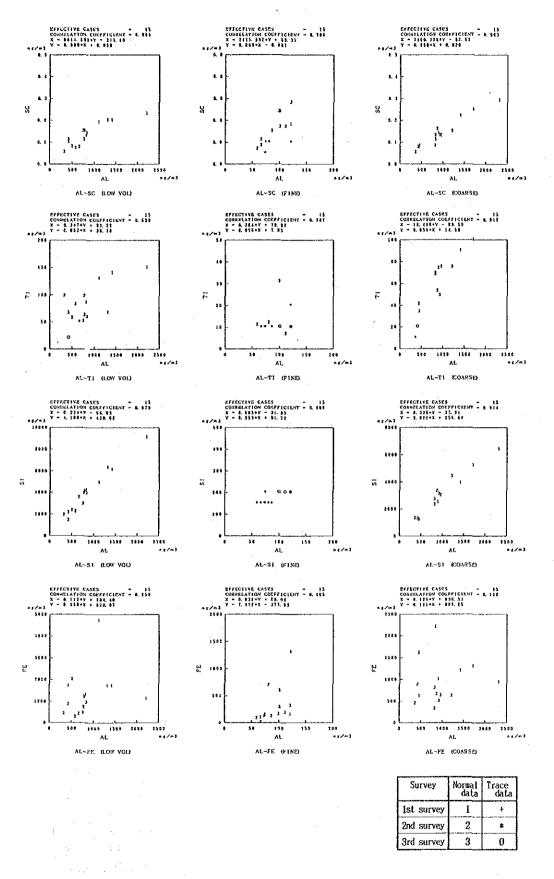


Fig. 3-4(1) An Example of Scatter Grams of Chemical Components for Variation of Seasons

III - 131

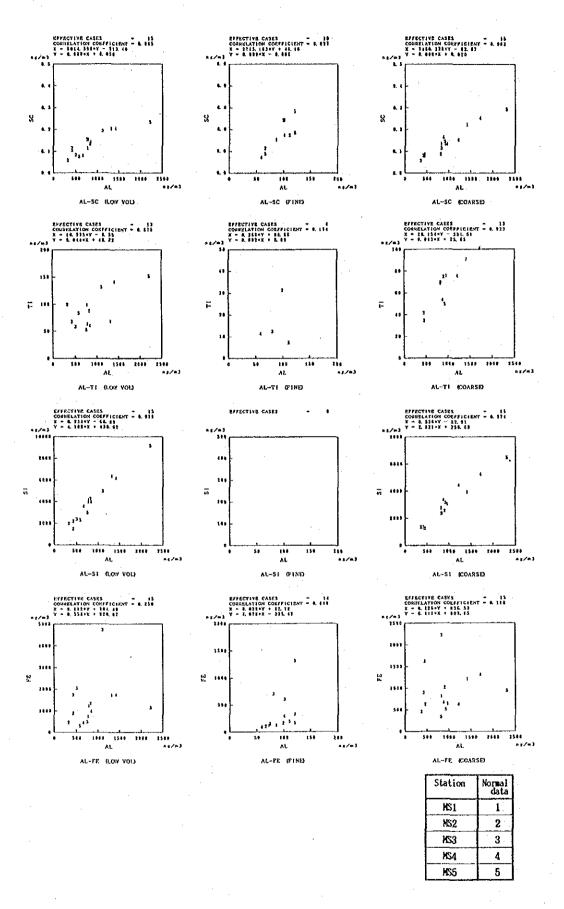


Fig. 3-4(2) An Example of Scatter Grams of Chemical Components for Variation of Stations

III - 132

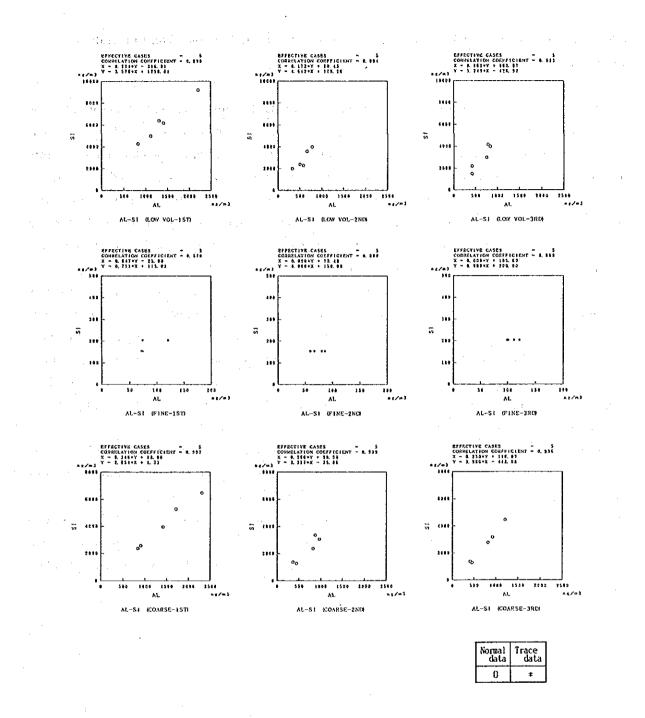


Fig. 3-4(3) An Example of Scatter Grams of Chemical Components for Comparison with Seasons

3.6 Resemblance among the Chemical Components by Cluster Analysis Based on Correlation Coefficients of Chemical Components Concentration

In order to check the similarity among chemical components, cluster analysis was done on their data obtained with respect to dust samples trapped by Low-volume sampler as well as Andersen sampler. As a measure to quantify the degree of similarity among variables, correlation coefficients among such chemical components concentration were calculated while setting the linkage distance approximated by the group average method. Data smaller than the detection limit value were thought to be equal to 1/2 of that detection limit. As for those chemical components in which more than 50 pct of the data drop below the detection minimum, they were excluded from analytical study. The result of cluster analysis is shown in Fig. 3-5.

As for clustering analysis of all seasonal data by Low volume sampler, the chemical components are found classifiable into five groups. The first group of Al, Si, Th, Sm and Sc has a high value of similarity of 0.9 and with their origin in soil. The second of Sb and Pb is supposedly related to glass and nonferrous industries. The third of T-C, E-C, O-C neighboring with the Br, S group with a similarity of 0.8 to cover chemical components coming from Diesel and gasoline cars. The fourth of Ni and V having their origin in fuel oil combustion. And the fifth of Mn, Zn, Fe and Cr cluster having similarity of 0.8–0.9 originated in the industrial park with steel mills in it.

Thus the clustering analysis of chemical components found in dust sample trapped by Lowvolume sampler gave the information on dust origins, namely ground soil, glass and nonferrous industries, automobiles, combustion fuel oil and steel plants. This information coupled with cluster analysis done on dust in two particle size ranges, fine and coarse, made it clear that the cluster of Na, Na⁺, Cl and Cl⁻ having similarity of over 0.9 indicates the existence of sea salt in a coarser range whereas that of NH_4^+ and SO_4^{--} found in fine particles shows the existence of secondary particles. First survey

Second survey

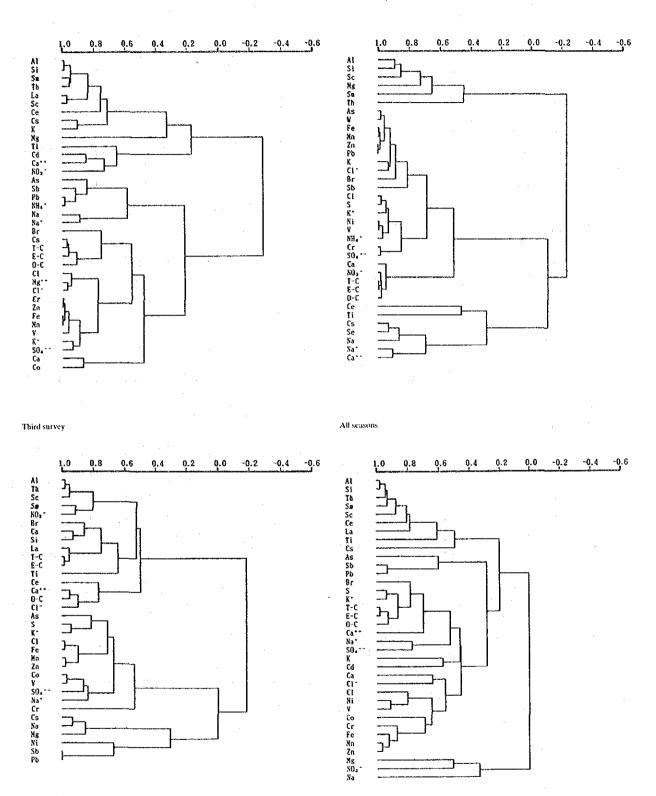


Fig. 3-5(1) Hierarchical Structure of Chemical Components by Cluster Analysis (Low Volume Sampler)

First survey

Second survey

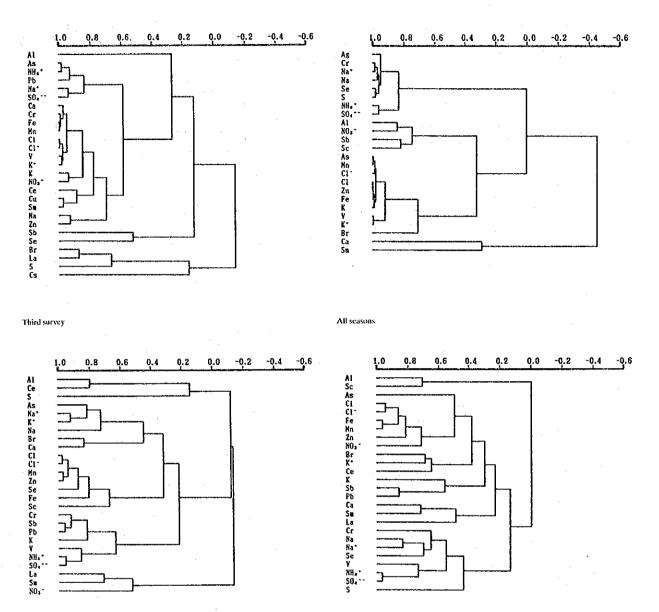


Fig. 3-5(2) Hierarchical Structure of Chemical Components by Cluster Analysis (Andersen Sampler, Fine Particle) First survey

Second survey

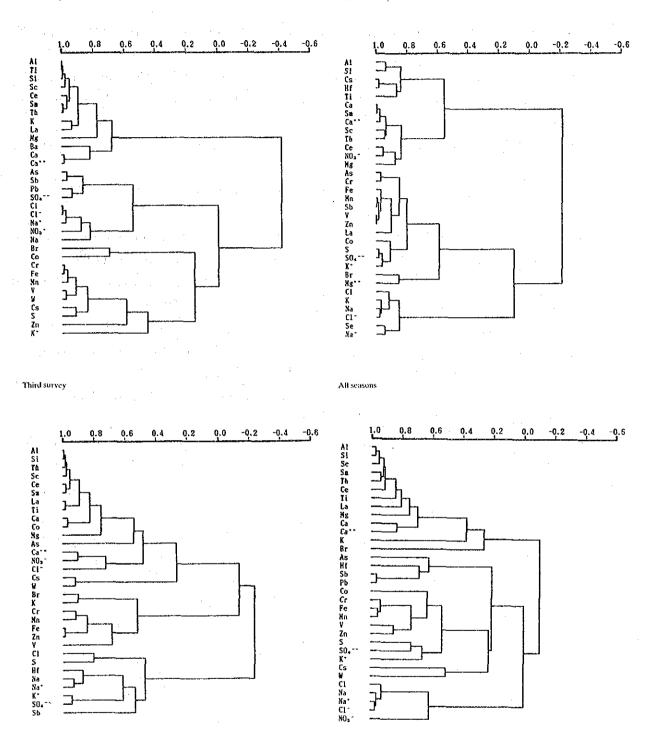


Fig. 3-5(3) Hierarchical Structure of Chemical Components by Cluster Analysis (Andersen Sampler, Coarse Particle)

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PART IV ANALYTICAL STUDY ON CURRENT EMISSION VOLUME OF ATMOSPHERIC POLLUTANTS (SO₂ and NO_x)

1. Sources investigated

Among a number of jobs leading to a successful development of the environmental control management plan, of utmost importance is not only the estimation of pollutant emission volumes but the accuracy with which such emission volumes from sources in the specified district are monitored. The management plan requires a total simulation map to cover the whole specified area or pollutant sources within the area. Such environmental pollution maps developed were initially checked at several points such that the calculated values come in a good agreement with observed ones. Once insignificant differences confirmed, the proposed diffusion model, diffusion factors as well as emission volumes from sources were assumed practically applicable and were used to project the probable points where the pollutant concentrations are likely to reach the maximum or to such levels to exceed the national control standards. When highly polluted points are made known, say, in topoghraphic maps developed, the next step is to evaluate the degree of contribution by each source to the situation and thereby to prepare the reduction plan against each pollution source. Same stepwise approaches were thought effective against sources expected in future as well.

This investigation covered the present and future SO_2 and NO_x emissions from all stationary sources, vehicles, ships and ferryboats in Samut Prakarn District. This part, however, discussed the analytical study result only about the present status (as of 1988) and left same analytical study for the future sources in the part VI.

2. SO₂ and NO_x emission volume from factories

2.1 Summary of survey

The estimation of SO_2 and NO_x emission volume from factories is mainly dependent on the survey by questionnaire. Small plants, however, not quite suitable for such data survey method were treated such that fuel consumption and emission volume are proportional to the number of employees and they can be calculated by multiplying the unit fuel consumption per person by the number of workforce. The items listed in the questionnaire are supposed to cover all informations required for calculation of atmospheric pollutant concentrations but there were quite a few questionnaire retreieved partially filled, which required additional make-up efforts through hearing and those described in the succeeding chapter. As for NO_x emission, measurement data were not available from the factories and so they were calculated by knowing such factors as fuel consumption and type, equipment, production amount, etc, based on a method applied in Japan.

2.2 Questionnaire survey

As stated above, variables to influence the pollutants from each stationary source is the amount and type of fuels used and thus upon consultation with ONEB the JICA contractor sent questionnaire to 577 factories of 2,456 in total which have smoke stacks in Samut Prakarn area. The list of

factories who reported back the information is shown in Table 2-1 and counts 208 in total. The plants listed in Table 2-2, with facility number zero (0) are those without any smoke stack and counts 11 in total.

| Name of county | Registered in master list | Questionnaire mail | Questionnaire return |
|-----------------|------------------------------|-----------------------|-------------------------|
| 1 Muang | 974 | 185 | - 63 |
| 2 Bang Plee | 286 | 94 | 28 |
| 3 Phra Pradaeng | 1196 | 298 | 117 |
| TOTAL | 2456 | 577 | 208 |

 Table 2-1 The number of factories from which questionnaire were retrieved

About a few of selected plants, the joint survey team of ONEB and Japanese staff visited them and confirmed the specifications and status data and for those in which some discrepancy be found followup actions were taken to make data consistency. The number of factories and facilities by county listed in Table 2-3 shows 59% of facilities in Phra Pradaeng. Table 2-4 summarizes the facilities by equipment type and shows 58% of facilities having the boiler in them.

The fuel type and consumption by facility type are shown in Table 2-5. It shows the type of fuel in use in Samut Prakarn area is mainly of fossil one, above all, fuel oil but others are also used such as firewood and rice chaff in boiler and drier furnace. Table 2-6 shows the type and consumption of fuel by business type, from which one can notice South Bangkok Power Plant being the largest consumer.

Table 2-2 (1) List of factory

| | THAL TEXT | THAT TRI | N & H MA | INTON GL | HITACHT (| NATIONAL | THON BUR | THE TRAI | TEPHSATA | LUND THI | ASTAN CH | SIAM ALT | KLONG SU | PHATHANA | RHANNON DEPENDING | RATA SHO | THAT ACR | NICCO FI | SAHA PAI | STAY DAT | STANDARD | THAJ-YAN | MANG TH | I LIAL VIN | CHILA M | SRISIAM | KLONG BA | BANGKOK | SLAM YAN | DANCKOK | KLID FII | THAT AR | THAL ST | THANAKU | | | STAY ST | GENERAL | ERAMAN 7 | KAO INDI | Salpan' | THAL CHI | CHAO PH | THAT UN TALTAN |
|--|------------------------------|-----------|----------------------|---------------------|--------------------|------------------------|--------------|----------|----------|-------------------------|------------------------------|--|---------------------------|------------------------|------------------------------------|---------------------|-------------------------|-------------|------------|------------|--|----------|--------------------------|------------|-----------------------------|---------|-----------|---------|---------------------|-------------|---|--|------------------------------|--------------------------|--|------------------------|------------|-----------|-------------------------------------|---------------------------------------|--------------------------------|-------------|---------------------|---|
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| 094 | L | | | | | | | | | · | | | | | | | | | | | | | | | | | | | | | | i | I | | | | | | | | | | | |
| Fuel Coasu. | Q. | 215 | \$ | 8 | | | 12000 | 2 | 8 | 200 | 320 | 1 2 2 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 | <u> </u> | 8434 | 2004 | | × | 8 | 2 | 1202 | 52 | 88 | 22 | 144 | 38 | 311 | ജ | | 727 | <u>}</u> | 1 | 316 | 407 | Still Still | <u>्</u> र्म | 38 | 860 | 181 | 8 | 8 | 102 | 0 | 6 | 1433 |
| Faci. | | 40 | | ~ | | | | | | | ~~~ | ×~> | 2 | ~~· | 4 | | | | | 5 | | | | | - - - - | , | - | 4 | ~ | -0 | 4 | 2 | с. П | 4 | .76 | 2 | , c. | 8 | | ~~~ | | 0 | | 202 |
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| | 5 9 | | 16000 | | | 8 | | 88 | 888 888 | 33 | 220 | 38 | 8 | 8 | 6400 | <u>s</u> s | 88 | | 8400 2010 2010 | 1000 | 886 | | 88 1 1 | | 212000 | 38 88 | 40000 | 17200 | 0006 | <u>868</u> 8 | | 1983 | 3200 | 382 | |
| . • | Gegistered Number | 82 | 5 12 12 | 34(3)-2/15 | 2(1)-1/75 | 13(2) -5/20 | 22(2)-1/77 | 20-15/17 | 22(2)-7/16 | 22(4)-1/15 | 13(2)-5/28 | 202-21/13 | 46-2/13 | 22(2)-40/15 | 200-1/21 | 13(2)-2/12 | 5 | 64(5)-2/13 | 2(5) -2/12 3/5 -1/07 | 177-764 88 | 7(U)-1/18 | 23-2/14 | 8(1)-1/13 | <u>32(8)-2/16</u> 53(8)-2/16 | 55-2/15 | 48(3)-2/19 | 27(1)-3/19 | 2(0)-34/15 | 59-8/15 | 74(2)-3/15 | 78(1)-2/15 | 78(1)-4/15 | 22(1)-3/15 | 59-1/17 | |
| Table 2-2 (2) List of factory | 6 | 1 69 1 THAI INDUSTRIES PROMOTION CO., L.T. 1 70 1 SIAN BROTHER CO., LTD. | 71 LUCKYTEX (TEATLAND) LTD.MILL#1 72 ADDATENC AND DWEING CO. 15D | 11 | 74 UNRECH TEAL STEEL CO., LTD. | | 71 I CHARGEN APPEN HATTANA HEAVING 78 I LIAN CHAI HEAVING | | 80 YONG LEE HEAVING LTD. PART 81 THAI DETPRCENT CO. LTD | | ., LTD. | 85 ADVICE SANG TEXTILE LTD., PART | | 8 I RUAN PHATEANA TEXTILE CO. LTD. | | | 9 3 WATTANA INDUSTRIES FACTORY LTD., PART | 8 | 96 BANGKOK DRYING & SILO (00., LTD. 47 NANAPAN GAMEDODICE (00. 1 TD. | - E | | 101 YEAUITT INDUSTRY LTD. PART | 102 S. TAAISERI INNUSTRY CO., LTD. | TT CONTRACTOR | 105 THAT-ASAHI GLASS CO., LTD. | 107 STAN FINE CHEMICAL CO., LTD. | 108 SONGCHAI SPINNING CO., LTD. | 110 METRO SPINING CO., LTD. | 111 BANGKOK STEEL INDUSTRY CO., LTD. | 112 BANGKOK ELECTRIC WIRE AND CABLE | 114 THAT BICYCLE INDUSTRY (D. LTD. | THAT | 116 SRISUKSAMAD SPINNING CO. LID. | INDIA STEEL W., LTD. | |
| | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| able 2 | Fuel Cocsu (H/Y) | 3316 1749 | 817 27 | 88 | | 1814 | <u>7</u> 8 | 8 | <u>8</u> 4 | 1881 | 144 | 216 | 321 | 2479 | 835 835 | 8 | 10 | , Б | 520 185 | 534 | 336 | 1084 | 240 | 14 | 5870 1850 | | 00 | 324 | 22/14 | 2056 | 22 | 147 | - SK | <u>8</u> 29 | 230 230 |
| Table 2 | Num, Fuel Faci Cocsu lity (L4/Y) | 4 316 2 1749 | 4 817 9 37 | 209 | | 7 1814 | - en | 5 300 300 300 300 300 300 300 300 300 30 | 2 2 | 14 1997 | 2 144 | 2 216 | 321 | 2 2479 | 83 83 1 | 3 182 | 2 104 | 6 | 2 520 1 186 | 2 534 | 2 5 335 | <u>4</u> 7084 | 3 240 | 3 144 | 4 5870 9 1850 | 2000 2000 2000 | 4 3430 | 1 324 | 3 2374 | 4 2056 | 1 72 | 1 147 5 505 | 2 32 33 32 32 | 3 150 | 4 1165 |
| Table 2 | 283 | 40 | - - - | 100 1 200 | | | | 300 2 300 | 192 1 250 192 1 144 | 555 14 1997 | | 100 2 216 | 42 3 200 1 | <u>58</u> 2 24 | 538 253 253 | 45 3 182 | 76 2 104 | 5 1 59 | 1100 2 520 10 1 185 | 511 2 534 | 37 2 162 43 6 336 | + | AG1 3 240 | + | | 73 1 | 415 4 | 180 1 | 131 3 2 | E00 4 | 1 01 | 40 | 20 20 20 20 20 20 20 20 20 20 20 20 20 2 | 544 3 | 4.44 |
| Table 2 | Raci Fr Faci Fr Lity C. | 561 4 20 2 | - - - | 2000 100 1 209 | | | | 11200 300 2 300 | 72X0 250 2 2X3 5 5640 192 1 144 | 35388 555 14 1397 | | <u>800 10 2 216</u> | 42 3 200 1 | <u>58</u> 2 24 | 1400 536 1 559 | <u>500 45 3 182</u> | 10540 100 2 104 | 800 5 1 5 5 | 38200 1100 2 520 5670 10 1 185 | ÷. | | + | | 2000 201 3 144 | | 73 1 | 4- | 180 1 | 3 | E00 4 | | 40 | 20 20 20 20 20 20 20 20 20 20 20 20 20 2 | iπ, | 4.44 |
| Table 2 | area Num. Num. Fu (m) Empi Faci Co (m) ovee lity (k | 51-3/13 107200 651 4 8(1)-2/22 10400 80 2 | 5(3)-1/14 52800 250 4 71/5 3/16 1463 40 5 | <u>52(1)-1/17 2000 100 1 1</u> | <u>13(2)-2/26 32(0)</u> 34(1)-2/23 1600 | <u>60-1/13 500 257 7 1</u> | <u>7((1)-6/15 11000 820 5 2</u> (3)-3/13 8000 111 3 | 22 20 - 5/18 11200 | 22(2)-4/21 72(0) 51-4/15 5640 | 64(1)-1/12 35588 | 22 (4) - 3/14 11200 | 20.9/2 | 44-1/21 56660 42 3 3 | <u>15(2)-3/15 8000 35 2 24</u> | 6(1)-1/15 | 52(1)-2/15 | 20-4/13 | 600-1/20 | 20 -9/14 20 -1/75 | 7(1)-1/19 8000 | 20(2)-1/21 4800 | 800 | 14 2800 16 55600 | 88 | 24400 | 9120 73 1 | 44000 415 4 1 1300 415 4 1 | 180 1 | 19344 131 3 3 2 | 1770 E00 4 | 2400 70 1 | 100 J | 4800 93 2 2 | 87380 544 3 | 4.44 |
| Table 2 | Num. Num. Fu Empl Faci Co ovee lity (A | 1 SIAN TYZE CO., LTD. 1 TAAI CASTRE OIL INDUSTRY CO., LTD. 1 8(1)-2/22 1 104201 801 2 1 | 5(3)-1/14 52800 250 4 71/5 3/16 1463 40 5 | UNION CONCERCIAL DEVELOPMENT 52(1)-1/17 2000 100 1 | 1600 | <u>60-1/13 500 257 7 1</u> | 1 [SUZU MOTORS (THAILAND) 20. LUU 77(1)-6/15 1 [1000] 201 5 1 MARBOON BLEAGTING & DYEING FACTORY 22 (3)-3/13 2000 1 111 3 1 | ALPHATEXE INDUSTRY CO., LTD. 22/20-5/18 11200 | PERAPRADARIC HEAVING CO., LTD. 22 (2) -4/21 72(2) NONYANG TIPE CO. 1.TD. 51-4/15 5640 | METAL BOX (THAILAND) CD., LTD. 64 (1)-1/12 35588 | SARONTIAL (1979) CO., LTD. 22(4)-3/14 11200 | I CHAIYARPORN HEAVING LTD., PART 22 (2) -9/23 | PRCIFIC PLASTICS (THAILARD) 44-1/21 56660 42 3 3 | LATATIANS UNSTRUCTION W. LIV. 200-1/10 2000 38 2 20 | PEACE CANNING (1958) 00., LTD. 6(1)-1/15 | 52(1)-2/15 | CHER SEIN REANS TEXTILE 22(2)-4/13 | SIN LEE FUAD | 20 -9/14 20 -1/75 | NIMITRI INTERNATIONAL CO. LTD. 7(1)-1/19 8000 | T.S. FOOD CENESARTE DD 17D 2000 1002 1102 1120 113000 113000 113000 113000 113000 113000 113000 113000 113000 113000 113000 113000 113000 113000 | THAI PLASTIC AND CHEMICAL CO., LTD. 44-1/14 80000 | MIANG TEAI STEEL O., LTD. 59-1/14 23300 | 1241 110 120 12 10 12 10 12 12 12 12 12 12 12 12 12 12 12 12 12 | THE BANGKOK IRON AND STEEL HORKS 1 59-2723 54400 | 9120 73 1 | THAI CAUROS CO., LTD. 2.1.000 415 4 | SAHAROU MERVING, FACTORY 22.00-11/26 2400 180 1 | THAT EDIBLE OIL CO., LTD. , 8(1) -4/15 19344 131 3 2 | I SURSAMAD VERETRELE OIL CLOSEED 8(U)-1/18 1400 50 1 | PATTANAKIT INDUSTRY LTD., PART | TIENG NGUAN HUAD HEAVING CO., LTD. 22(2)-2/19 | SURSAMAD ACRUCULTURAL PRODUCT 1 2 (2) - 2/24 1 15UU 301 3 7 that herr pettrana cd 1, 170 153 (7) - 1/14 4200 92 2 | TOYOTA NOTOR THAILLAND CO., LID. TT(1)-1/18 87350 544 3 | 14200 85 4 11200 100 4 |

| Name of county | Number of factories | Number of facilities |
|-----------------|---------------------|-------------------------|
| I Muang | 63 | 145 |
| 2 Bang Plee | 28 | 47 |
| 3 Phra Pradaeng | 117 | 278 |
| TOTAL | 208 | 470 |

Table 2-3 Number of factories and facilities by county

Table 2-4 Number of facilities by equipment

| Code | Name of facility type | Number of faci- lities |
|------|--|---|
| 101 | Boiler (for electric power) | 5 |
| 103 | (other) | 267 |
| 502 | Metal fusion furnace (for aluminum smelting) | 6 |
| 503 | " " (for other smelting) | 2 16 |
| 601 | Netal rolling furnace (steel/continuous) | 16 |
| 602 | " " (steel/batch) | 42533512652181 |
| 603 | " " (aluminum/continuous) | 1 2 |
| 607 | Metal heat treatment furnace (steel/continuous) | 5 |
| 608 | " " (steel/batch) | 3 |
| 611 | // // (other/continuous) | 3 |
| 612 | // // (other/batch) | 5 |
| 613 | Metal forging furnace (steel/continuous) | ļ <u>1</u> |
| 702 | Oil heating furnace (updraft) | 2 |
| 703 | // // (other) | 6 |
| 915 | Glass melting furnace (tank furnace) | 5 |
| 918 | Other melting furnace | 2 |
| 1001 | Reaction furnace (for inorganic chemicals) | 1 |
| 1004 | Direct heating furnace (for foodstuffs) | 8 |
| 1105 | Detergent drying furnace | |
| 1106 | Other drying furnace | 67 |
| 1201 | Electric furnace (arc furnace for iron manufacture) | 8 |
| 1202 | " " (three-phase resistance for iron) | 1 |
| 1205 | " " (three-phase resistance for iron) | 1 |
| 1209 | <pre>" " (low frequency induction furnace)</pre> | 1 |
| 1302 | Waste incinerator (for domestic urban wastes/batch) | 2 |
| 1303 | " " (for industrial wastes/continuous) | 1 |
| 1304 | " " (for industrial wastes/batch) |] 3 |
| 1416 | Fusion furnace (crucible furnace for lead) | 2 |
| 1419 | <pre>// // (crucible furnace for zinc)</pre> | 1 1 2 1 3 2 1 3 3 |
| 1421 | " " (other for zinc) | 3 |
| 1423 | Drying furnace (for lead) | 3 |
| 1802 | Activated carbon manufacturing reactor (other) | Ĩ |
| 2501 | Fusion furnace (for manufac.of lead storage battery) | 10 |
| 2603 | Reactor (for manufacture of lead pigment) | $1 \\ 3$ |
| 1 | Diesel generator |] 3 |
| 8 | Other | 18 |
| | TOTAL | 470 |

Table 2-5 Fuel type and consumption by facility type

Ficity (MH) 20 320 320 320 320 2827 451534 451534 (30) ige Ege 43560 £ 0(1) 51600 8 fuel consumption (number of facilities) Domes. Indus. E Wastes Wastes r (ton) (ton) 83 調 g ۳e 180 34500 0 ther Raw (ton) 588880°C 11/1/04 ଞ୍ଚ Nonfer Raw ro.Ore Coke (ton) (ton) 888 ଞ୍ଚିତ୍ର 0000 30(2) Sulfi-de Ore (ton) ដ្ដទ 217(1) 84 (7) | 11306 | 345610 (65) | (8) Iron (ton) 334610 53 88 11 330 (2) 1650 00) 255(4) 28 LNG LPG (ton) 769 (2) 20) 2 (8 (3) 86 (ton) 1285201 1285200 ଞ୍ଚୁର ଅନୁ Other solid (ton) 888 ж К Paddy & Husk (ton) 1048 C 681 8 Lumber 2001 (19) (ton) (14) (14) 2(0) 807 800 800 (ton) ଞ୍ଚିତ୍ର ie S Other Liquid (*kl*) පුල жe kero-sene (kel) යිම ଞ୍ଚି Light 011 838 808 808 808 808 12 25 12 iä⊝ 480 151716 (224) 2261(5) 23(2) 1685 1885 1885 86588 205(8) 560972 (309) Heavy 0i1 (kt):
 0613
 Meral forming f. (steel/cont.)
 128(1)

 0702
 011 heating furnace (updraft)
 844(2)

 0703
 011
 #
 #

 0703
 011
 #
 #
 844(2)

 0703
 011
 #
 #
 #
 844(2)

 0703
 011
 #
 #
 #
 844(2)

 0703
 011
 #
 #
 #
 844(2)

 0703
 01
 #
 #
 #
 844(2)

 0703
 015
 Glass melting furnace (tank)
 3010
 (steel/batch) 2810(4) 82760 32760 (1)076 (c) Se 9 " " " (low frequ.) 2 Meste inciner. (domest./batch) 3 ** " " (indust./batch) 4 * " (indust./batch) 5 Fusion furnace (crucible/sine) 2 1 * " (crucible/sine) 2 3 Drying furnace (for lead) 3 | Drving furnace (for lead) 2 | Activated carbon manu. reactor 1 | Fusion f. (lead shor, battery) 3 | Reactor (lead pigment) 1 | Diecel generator other/smelt.) 0601 | Metal rolling f. (steel/cont.) (alumi/smelt.) (other/batch) Electric furnace (arc furnace) (three-phase) (three-phase) Boiler (for electric power) Name of facility type TOTAL generator 0502 Metal fusion f. (other) ۲ ۲ * ž * \$ Ł 1010 1201 0103 1202 1205 0612 Sode

Table 2-6 Consumption of fuel by business catogory

| | | | | | | | | | | | | | | fuel | consumpt | ion (nusbe | r of fac | ilities) | |
|-------|------------------------------|---------------|----------------------|-----------------------|--------------------------|---------------|-----------------|--------------------------|-------------------------|--------------|--------------|---------------|---------------------------|---------------------------|----------------------|-----------------------|---------------------------|---------------------------|--------------------------|
| Coda | Name of business category | Heavy (41) | Lieh} 011 (ki) | Kero- sene (ki) | Other 1 (quid (ka) | Coal (ton) | lusber (ton) | Paddy a Husk (ton) | Other solid (tor) | LNG (ton) | LPG (ton) | Iron (ton) | Sulfl- de Ora (ton) | Nonfer ro.Ore (ton) | Raw Coke (ton) | Otber Rан (ton) | Pomes. Hastes (ton) | lndus. Kastes (ton) | Elect- ricity USAD |
| 1~21 | Food industry | 52233(76) | 18(5) | 613(4) | | 900(1) | 4851(5) | 8817(6) | 1 8100(1) 1 | | 56(6) | | | 1 | i | | | 66(1) | ; |
| 22~33 | Textile industry | 34777 (95) | 25(1) | | | 1405(1) | 2719(5) | | 480(1) | | 608(7) | | | | | | | | 0(1) |
| 34~37 | Wood industry | - 134C D | 1 | | | 1 | 14400(2) | 1048(1) | | | | | : | | | | | | 100 |
| 38~41 | Pulp and Paper | 23991(7) | | 1 | | 4730(1) | | | . | | | | | 1 | | | | | 1 |
| 42~53 | Chemical Industry | 23613(53) | 76102 | | 35(1) | ł | 31 (4) | | 1 1 | | 267(4) | | 217(1) | 1 | | | 18(1) | 92 (3) | |
| 54~58 | Ceranic industry | 50100(4) | 1400(1) | | · . | 1 | | | 1 | | 2350(2) | | | | | | | | 1 |
| - 59 | Iron and Steel | 22127(30) | 51(1) | | | 1 | | | | | 1.1.1.1 | 345610(8) | | | 1800(2) | 177780/61 | | | 42331619 |
| 60 | Non-ferrous metal | 2178(7) | | | | : 1 | | | | | 70(4) | | | 930 (3) | | | | | 9278(3) |
| 61~83 | Netal and Nachine | 7381 (34) | 282313 | 152(4) | 71(4) | . 1 | | | 1 | | 7955 (42) | | | : | | 7800(3) | | | 1293919 |
| 84~99 | Other assuractory | 324438(2) | | | _ | 1 | | | ; 1 | 1285200(5) | 1 | 1 | | | | | | | 1 |
| | TOTAL | 560972 | 5078 | 765 | 106 | 7035 | 22001 | 3865 | · 8590 j | 1285200 | 11306 | 345610 | 217 | 930 | 1900 | 185580 | 13 | 158 | 451534 |
| [| IUIAL | (309) | (33) | (8) | (5) | ധി | (16) | (T) | യ | (5) | (65) | ങ | (D) | (3) | (2) | (8) | (D) | (4) | യ |

2.3 Calculation of SO₂ and NO_x emission volume and exhaust gas volume based on the questionnaire survey data

2.3.1 Exhaust gas volume

The volume of exhaust gas from each plant was reported in the questionnaire. But for those not reported by questionnaire they were calculated by using the equation (2-1). If the calculated value is found exceeding 30 m/s in term of the stack exit velocity, it was thought erroneous. Taken as corrective actions are reexamination of reported data such as fuel consumption, stack geometry through additional hearing of the factory involved. The emission volume was calculated based on confirmed data. The residual oxygen content and wet exhaust gas factor are shown in Table 2-7 and Table 2-8 respectively. They are average figures in use in Japan.

The exhaust gas volume by each factory and each facility type is shown in Table 2-9 where the pattern (1) deals with consolidated data about each facility and the pattern (2), about the stack. Also included are SO_2 , NO_x emission volume data calculated by the formula which will be mentioned later.

Table 2-7Residual O2 in flue gas by facility type(mean value in Japan)

0, (J) ი 1 ب 1- ت 60 000 <u>ہ</u>ہ 14 60° r--9 ω~-ŝ 01 61 ---Rossting furnace (for copper, lead, zinc) Blast furnace (for copper, lead, zinc) Husion furnace (for copper lead, zinc) Prying furnace (for copper, lead, zinc) Aggregate drying furnace Coment row malerial drying furnace Bride raw mulerial drying furnace Gast drying furnace Other drying furnace 0901~0905 Coment calcination furnace 0906~0907 Brick calcination furnace 0909 Line calcination furnace 0912~0913 Pottery calcination furnace 0916~0917 Glass melting furnace Name of facility type 0601~0606 Metal rolling furnace 0607~0612 Metal Neat treatmont furnace 0613~0618 Metal forging furnace Boiler (for electric power) Boiler (for heating) Boiler (other) 0301~0305 Roasting furnace 0306~0308 Sintering furnace 0312~0314 Pellet calcination furnace 1001~1002 Reaction furnace 1003~1004 Direct heating furnace 0501~0506 Metal fusion furnace 0701~0703 0il heating furnace Combustion furnace [301~1304 Haste incinerator average [201~12]2 Electric furnace Gas generator Gas heater 0401~0402 Blast furnace 0403~0404 Converter Coke furnace 1401~1403 1407~1403 1413~1421 1422~1424 0821 1022223 102223 10223 10223 10233 10033 10033 10033 10033 100 Code 0102 0102 0102 1020 1082

[Source] Ministry of International Trade and Industry (MITI). "Manual of Mabient SOx and NOx Prediction Method in Comprehensive Environmental Assessment", 357p, 1PCAJ (in Japanese), (1385).

Table 2-8 Fuel properties by fuel type (mean value in Japan)

| SEQ) | | | | | | | | | | | | | | |
|------------|--|----------------|-------------|------|--------------|--------------------------|--------------|--------------------------------|-------------------|----------------------------|--------------------|------------|----------------|--------------|
| | | EGORY | | | | TIME ZONE START-END | | KANE | | (X) | (KCAL/) | (/H) | NORMAL (/H) | (/Y) |
| 1) | 1 1 1 | 12(7) | 103 | 65 | 4428 | 21:00-15:00 | 1-12 | 11 A HEAVY OI | u z. | 160 0.9612 | 10461 | 111 | 96 | 425 |
| 2) 3) | 1 2 1 1 2 2 | 42 42 | 103 | | 1675 | 0:00-24:00 | | 13 C HEAVY OF 35 LPG | | 500 0.9529 | | -1 -1 | 240 | 402 |
| 4) 5) | 1 2 3 | | 103 103 | | 8040 1675 | | | | | 002=-1.0000 | | -1 -1 | 19 | 150 |
| 6) 7) | 1 6 1 | 4(3) | | | 3000 | | | 11 A HEAVY OF 11 A HEAVY OF | IL 1. | 280 0.946 | 10000 | -1 | 52 105 | 156 756 |
| 8) | 1 7 1 | | 1304 | | 1680 | | | 14 LIGHT OIL | ۱. | 200 0.8660 | 10950. | 38 | 25 | 47 |
| 9) | 1 8 1 | 59 | 601 | 84 | 7200 | 0:00-24:00 | 1-12 | 54 INDUSTRI.W | | 000 -1.0000 500 0.9325 | | 90 -1 | 50 5 | 92 |
| 103 | | 59 | 1201 | | 7200 | | | 14 LIGHT OIL | 1. 0. | 800 0.8660 | 0 10950* | -1 -1 | 7 12445 | 51 89604 |
| 145 | ********* | | | | * 3 6 6 | | 1-13 | 61 ELECTRICIT | | 000+-1.0000 | | -1 | 8320 | 59904 |
| 11) | 1 9 1 | 6U | 1504 | 8404 | 1200 | 0:00-24:00 | 1-12 | 43 NONFERROUS 61 ELECTRICIT | | 000 -1.000 | | -1 -1 | 125 | 900 5160 |
| 12) 13) | 1 12 1 1 12 2 | 22(3) 22(3) | 103 | 76 | 4800 | 8:20- 0:20 | 1-12 | 13 C HEAVY OI 13 C HEAVY OI | IL 2. | 500 0.9529 500 0.9529 | 10340 | -1 -1 | 1250 1250 | 6000 6000 |
| 14) | 1 12 3 | 22(3) | 103 103 | | | 0:20- 8:20 | 1 | 13 C HEAVY OI | | 300 0.9529 | | -1 | 0 | 0 |
| 152 | $ \begin{array}{ccccccccccccccccccccccccccccccccc$ | | | | | 5 A. A. | | 14 LIGHT DIL 11 A HEAVY DI | | 280 0.9462 | | -1 | 13 69 | · 25 |
| 17) | 1 15 1 | | | | 100 | | | 13 C HEAVY OF | | 500 0.9529 | | -1 | 84 | 737 |
| 18) | 1 15 2 | 64(1) 64(1) | | | 8760 8760 | 0:00-24:00 | | 13 C HEAVY 01 | IL 2. | 500 0.952 | 10340 | -1 -1 | 84 88 | 737 767 |
| 50) | 1 15 4 | 64(1) | 612 | 88 | 8760 | 0:00-24:00 | 1-12 | 61 ELECTRICIT | tv o. | 000#-1.0000 |). 86Q× | -1 | 450 | 3942 |
| 21) 22) | 1 15 5 | 64(1) 64(1) | | | 8760 8760 | | | 61 ELECTRICIT 61 ELECTRICIT | | 000+-1.0000 | | -1 -1 | 450 120 | 3942 1051 |
| 233 | 1 16 1 | 70 | 1106 | 77 | 2400 | 8:00-17:00 | 1-12 | 35 LPG | 0. | 002+-1.0000 | 12145= | -1 | 8 | 20 |
| 24) | 1 17 1 | | | | | | | 13 C HEAVY OI | | 950 0.9400 | | 590 | 300 | 2200 |
| 25) 26) | | | 103 1304 | | 0 1500 | | 1-12 1-12 | 13 C HEAVY OI 54 INDUSTRI. | IL 1. WASTE 0. | 950 0.9400 |) 10295) 4000* | -1 -1 | 44 | 0 66 |
| 27) 28) | 1 18 1 1 18 2 | | | | 4800 800 | | | 11 A HEAVY OI 35 LPG | | 000 0.9408 002±-1.0000 | | 75 -1 | 70 70 | 336 56 |
| 29) 30) | | | | | 6240 4368 | | 1-12 1-12 | 11 A HEAVY DI 11 A HEAVY DI | | 160 0.961 160 0.961 | | 100 100 | 63 63 | 390 273 |
| 31) | 1 20 1 | 22(1) | 103 | 76 | 6912 | | | 13 C HEAVY OF | | 500 0.9529 | | -1 | 1128 | 7800 |
| 32) 33) | | | | | 0 | 0:00-24:00 | 1-12 | 13 C HEAVY 01 13 C HEAVY 01 | | 500 0.9529 500 0.9529 | | -1 -1 | 0 | 0 |
| 343 | 1 20 4 | 22(1) | 103 | 74 | 0 | 0:00-24:00 | 1-12 | 13 C HEAVY OF | IL 2. | 500 0.9529 | 10340 | -1 | ō | Ó |
| 35) 36) | | | | | 6912 | 0:00-24:00 0:00-24:00 | 1-12 | 35 LPG 35 LPG | | 0021.0000 0021.0000 | | -1 -1 | 38 10 | 264 |
| 37) | 1 20 7 | | | | 6912 | 0:00-24:00 | 1-12 | 35 LPG | 0. | 002*~1.0000 | 12145. | -1 | 29 | 198 |
| 38) 39) | 1 21 1 | | | | 1048 3930 | | 1-12 | 15 KEROSENE 15 KEROSEHE | | 033* 0.7951 033* 0.7951 | | -1 -1 | 6 6 | 6 24 |
| 402 | | 77(2) | 502 | 88 | 3000 | 8:00-21:00 | 1-12 | 14 LIGHT OIL | 0. | 600 0.8450 002*-1.0000 | 10950* | -1 | . 7 | 20 52 |
| 42> | | 77(2) | | | | | | 11 A HEAVY OI | | 160 0.9612 | | 500 | · 18 480 | 1728 |
| 43) | 1 23 1 | 52(2) | 103 | -1 | 0 | | | 23 LUMBER | | 100 -1.0000 | 3500 | -1 | 0 | 0 |
| 44) | | 22(2) | 103 | 88 | 2080 | 8:00-17:00 | 1-12 | 13 C HEAVY 01 | 1L 2. | 920 0.9510 | 10513 | -1 | 17 | 35 |
| 45) | 1 25 1 | 22(2) | 103 | 83 | 2400 | 8:00-16:00 | 1-12 | .11 A HEAVY OF | IL 2. | 000 0.9408 | 10430 | - 1 | 11 | 26 |
| 46) | 1 27 1 | 60 | 603 | 83 | 3840 | 8:00-24:00 | 1-12 | 35 LPG | 0. | 002*-1.0000 | 12145* | -1 | 1 | 2 |
| 47) | | 74(5) | 103 | 70 | | 0:00-24:00 | 1-12 | 11 A HEAVY OF | IL 1. | 280 0.9462 | | - 44 | 38 | 315 |
| 48) 49) | 1 29 3 | 74(5) | 103 | 84 | 5760 5760 | 0:00-24:00 | 1-12 | 11 A REAVY OF | rL 1. | 280 0.9462 280 0.9462 | 10000 | 44 44 | 38 38 | 315 315 |
| 50) 51) | 1 29 4 | 74(5) | 1423 | 70 | 84Q0 84Q0 | 0:00-24:00 | 1-12 | 35 LPG | 0. | 002*-1.0000 002*-1.0000 | 12145* | -1 -1 | 13 13 | 107 |
| 52) | 1 30 1 | | 103 | | 4160 | | | 11 A REAVY OF | | 980+ 0.9300 | | -1 | 13 | 52 |
| 53) | | 22(2) | 103 | 87 | 7200 | 0:00-24:00 | 1-12 | 23 LUMBER | ٥. | 1001.0000 | 3820 | -1 | 120 | 865 |
| 54) | 1 33 1 | 98 | 103 | 88 | 5110 | 10:00-24:00 | 1-12 | 11 A HEAVY OI | 1L Z. | 000 0.9405 | 10430 | 114 | 86 | 438 |
| 55) | 1 34 1 | | | | | | | 11 A REAVY DI | | 160 0.961 | | -1 | 53 | 144 |
| 56) 57) | | 13(2) 13(2) | | | 1480 1470 | 7:00-17:00 7:00-17:00 | 1-12 | 11 A HEAVY OF 11 A HEAVY OF | 11. 2. IL 2. | 920 0.9500 920 0.9500 | 10518 10518 | 280 280 | 220 220 | 350 |
| 58) 59) | 1 36 2 | | | | 2400 | 7:30-16:00 7:30-16:00 | 1-12 1-12 | 11 A HEAVY OF 11 A HEAVY OF | IL 1. IL 1. | 280 0.9462 280 0.9462 | | -1 -1 | 75 75 | 180 180 |
| 60) | | 38(2) | 103 | 83 | 8760 | 1 | | 21 GENERAL CO | | 000 -1.0000 | 6399* | -1 | 540 | 4730 |
| 61) | 1 40 1 | 52(1) | 103 | 80 | 2360 | 8:00-17:00 | 1-12 | 13 C HEAVY O | 11. 2. | 500 0.9525 | 10340 | 30 | 25 | 59 |
| 62) | 1 41 1 | | | | | | | 13 C HEAVY OF | | 660 0.9764 | | -1 | 125 | 684 |
| 63) 54) | 1 41 3 | 44 | 103 103 | -1 | 5460 | 0:00-24:00 | 1-8 | 13 C HEAVY OI 13 C HEAVY OI | IL 2. | 660 0.9764 660 0.9764 | 10400 | -1 -1 | 125 | 684 684 |
| 65) | 1414 | 44 | 103 | 8808 | 3300 | 0:00-24:00 | 8-12 | 13 C REAVY OI | IL 2. | 660 0.9768 | | -1 | 738 | 2436 |

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| | A.P. | | | |
|------|------|----------|-------------|-------|
| P121 | Ur | LACTELLI | (PATTERN 1) | 1 e - |

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| SEQ) | UN | TOR | 1.1 | BUSINE SS CAT Egory | LITY | TING | ROAK | OPERATING TIME ZONE START-END | TING | | FU N A M E | EL AND Sulfur (%) | RAV HATE GRAVITY | RIAL TO CALORY (KCAL/) | BE USED- Rating (/H) | NORMAL (/H) | ANNUAL (7Y) | |
|-------------------|--------|----------|----------|---------------------------|-------------|--------------|--------------------|--|------------------|----------|---|-------------------------|------------------------------|------------------------------|-----------------------------|-----------------|----------------|---|
| 66) 67) | 1 | | 1 2 | 26 26 | 103 103 | | 4640 0 | 7:00-23:00 7:00-23:00 | | | A HEAVY OIL A HEAVY OIL | | | 10000 | 60 +1 | 50 0 | 232 0 | |
| 68) | 1 | 44 | 1 | 48(9) | 103 | 71 | 800 | 8:00-16:00 | 8-12 | 11 | A HEAVY OIL | 2.160 | 0.9612 | 10461 | 15 | 12 | 10 | |
| 69) 70) | 1 | | 1 2 | 74 (5) 74 (5) | | | 7200 | 0:00-24:00 | | | C HEAVY OIL C HEAVY OIL | | 0.9529 | 10340 10340 | -1 | 36 | 258 D | |
| 71) | 1 | 45 | 3 | 74 (5) | 2501 | -1 | 7200 7200 | 0:00-24:00 | 1-12 | 19 | OTHER LIQUID | 1.236 | 0.8866 | 10600 | -1 -1 | 2 | 16 16 | • |
| 73) | 1 | 45 | 5 | 74 (5) 74 (5) | 2501 | -1 | 7200 | 0:00-24:00 | 1-12 | 19 | OTHER LIQUID | 1.236 | 0.8866 | 10600 | -1 | 2 | 16 | |
| 75) 76) | 1 | 45 | 7 8 | 74(5) | 2501 | -1 | 7200 | 0:00-24:00 | 1-12 | 19 | Des frances a second a | 1.236 | 0.8866 | 12145= 10600 10950= | -1 -1 -1 | 8 3 3 | 56 23 11 | |
| 77) | 1 | | . 1 | 64 (2) | 103 | | 3600 | 0:00-24:00 | | | A HEAVY OIL | | 0.9408 | 10430 | -1 | 15 | 54 | |
| 78) 79) 80) | 1 1 | 46 | 234 | 64(2) | | 81 | 3800 4500 56 | 0:00-24:00 6:30-21:30 8:30-17:00 | 1-12 | 35 | A HEAVY OIL LPG LPG | 0.002* | 0.9408 ~1.0000 -1.0000 | 10430 11158 11158 | -1 -1 -1 | 19 | 68 18 0 | |
| 81) | - | 46 | | 22(2) | 103 | | 1320 | | | | | ÷. | 0.9462 | 10000 | -1 | 120 | 158 | |
| 82) | 1 | | 2 | | 103 | | 1320 | 7:00-16:00 | 1 A A | | A HEAVY OIL | 14 C _ | 0.9462 | 10000 | -1 | 120 | 158 | |
| 83) 84) | 1 | 49 | 1 | 22(2) | 103 | 65 | 2482 | 5:30-22:00 | 1-12 | 11 | A HEAVY OIL A HEAVY OIL | 1.280 | 0.9462 | 10000 | -1 | 88 29 | 218 | |
| 85) 86) | 1 | | 3 | 9(2) 9(2) | 103 | | 2482 8472 | 5:30-22:00 | · · | | A HEAVY OIL | 2.000 | 0.9462 | 10000 | -1 34 | 48 25 | 118 | |
| 87) 88) | 1 | 51 | 23 | 9(2) | 1106 | 80 | 8472 8472 | 0:00-24:00 | 1-12 | 11 | A HEAVY OIL | 2.000 | 0.9408 | 10430 | -1 | 35 | 292 | |
| 89) | i | | | | 1106 | | 8472 | 0:00-24:00 | 1-12 | 11 | A HEAVY OIL | 2.000 | 0.9408 | 10430 | -1 | 35 | 292 | |
| 90) 91) | 1 | | 1 2 | 42 42 | 103 703 | | 4480 750 | 8:00-24:00 8:30-14:00 | | | C HEAVY OIL Light oil | 2.500 | 0.9529 0.8660 | 10340 10950* | 50 -1 | 30 4 | 134 3 | |
| 92) 93) | 1 1 | 53 53 | 1 | | 103 103 | | 4752 832 | 7:00-23:00 |) 1-12) 1-12 | | A HEAVY OIL A HEAVY OIL | 2.160 | 0.9612 0.9612 | 10461 10461 | -1 -1 | 69 46 | 328 38 | |
| 94) | 1 | 54 | 1 | 74(2) | 103 | -1 | 7200 | 0:00-24:00 | 1-12 | 14 | LIGHT OIL | 0.560. | 0.8300 | 10950+ | -1 | 145 | 1043 | |
| 95) 96) | 1 | | 1 2 | | | 8303 8402 | 8400 8400 | 0:00-24:00 | | | C HEAVY OIL C HEAVY OIL | 3.500 3.500 | 0.9900 | 10336 10336 | -1 -1 | 571 571 | 4800 4800 | |
| 97) 98) | 1 | | . 1 | | 103 | | 0 6000 | 7:00- 3:00 | | | A HEAVY OIL A HEAVY OIL | 1.280 | 0.9462 | 10000 | -1 -1 | 0 200 | 0 1200 | |
| 993 | 1 | 56 | 3 | \$(3) | | -1 | 1240 | 8:00-17:00 | 1-12 | 35 | LPG LIGHT DIL | 0.002 | | 12145# | -1 | 0 | 0 1 | |
| 101) | 1 | 56 | Š | 5(3) | 8 | 65 65 | 7200 | 7:00- 3:00 7:00- 3:00 | 1-12 | 35 | | 0.002. | -1.0000 | | -1 -1 | ô | 0 | |
| 103) | i | | 7 | | | 65 | 7200 | 7:00- 3:00 | 1-12 | | LPG | | -1.0000 | 12145 | -1 | ŏ | ŏ | |
| 104) | 1 | | 8 | | | 65 | | 7:00- 3:00 | | 35 | LPG | 0.002* | -1.0000 | 12145* | -1 | 0 | · 0 | |
| 105) | 1 | | <u>1</u> | | 103 | | 1960 | 8:00-16:00 | | | A HEAVY OIL | | 0.9612 | | 63 | 50 | 98 | |
| 107) | 1 | | 2 | | 103 103 | | 1800 1800 | 8:00-20:00 8:00-20:00 | | | A HEAVY OIL A HEAVY OIL | 2.000 | 0.9408 | 10430 | -1 | 25 25 | 45 45 | |
| 108) | 1 | 61 | 1 | 15(2) | 103 | 86 | 3600 | 0:00-24:00 | | | PADDY & HUSK | 0.000+ | -1.0000 | 2600 | -1 | 750 | 2700 | |
| 109) | - | 63 | 1 | | 103 | | 96 | | | | LIGHT OIL | 0.460 | 0.8300 | 10950* | -1 | 94 | 9 | |
| 110) | 1 | 64 | 1 2 | 47(2) | 103 | 74 | 7200 | 0:00-24:00 | 1-12 | -11 | C HEAVY OIL | 2.160 | 0.9764 0.9809 | 10400 10461 | 217 42 | 180 31 | 1296 203 | |
| 112) 113) | 1 | | 1 | | 103 1416 | | 0 270 | 0:00-24:00 | 1.1 | | C HEAVY OIL | | 0.9764 | 10400 | -1 | 0 | 0 | |
| | | 65 | 2 | | 1416 | | 270 | 0:00-24:00 | | 35 | NONFERROUS ORE LPG Nonferrous ore | 0.002+ | -1.0000 | 0* 12145± | -1 -1 | 56 | 15 | |
| ••• | - | | | ••• | | | 270 | | | | LPG | | -1.0000 | 0* 12145* | -1 -1 | 56 3 | 15 1 | |
| 115) 116) | 1 | 66 66 | 1 2 | 22(2) 22(2) | 103 103 | | 3600 3600 | 0:00-24:00 | | | A HEAVY OIL A HEAVY OIL | 2.800 | 0.9383 0.9383 | 10394 10394 | 337 524 | 250 300 | 900 1080 | |
| 117) 118) | | 67 57 | 1 2 | | | | 3600 3600 | 0:00-24:00 | 1-12 1-12 | 11 11 | A HEAVY OIL A HEAVY OIL | 3.000 | 0.9850 0.9850 | 10000 | 54 54 | 50 50 | 180 180 | |
| 119) 120) | 1 | 68 68 | 1 2 | | 103 103 | | | 0:00-24:00 | 1-12 | 13 | C HEAVY OIL | 3.000 | 0.9561 | 10296 10296 | -1 | 251 302 | 1810 2172 | |
| 121) 122) | 1 | | 3 | 22(3) | 103 103 | 69 | 7200 | 0:00-24:00 | 1-12 | 13 | C HEAVY DIL C HEAVY DIL | 3.000 | 0.9561 | 10296 | -1 | -302 | 2172 | |
| 123) 124) | 1 | 68 | 5 | 22(3) | 103 | 69 | 7200 | 0:00~24:00 | 1-12 | 13 | C HEAVY OIL C HEAVY OIL | 3.000 | 0.9561 | 10296 | -1 -1 | 302 302 | 2172 2172 | |
| 125) | 1 | 68 68 | 7 | 55(3) | 103 | 69 | 0 | 0:00-24:00 | 1-12 | 13 | C HEAVY OIL C HEAVY OIL | 3.000 | 0.9561 | | -1 -1 -1 | 0 0 0 | 0 | |
| 127) | | 69 | 1 | 46 | 103 | 60 . | 1000 | 9:00-13:00 | 1-12 | 11 | A HEAVY OIL | 3.000 | 0.9850 | | 78 | 65 | 0 65 | |
| 128) | • | 69 70 | 2 1 | | 1302 915 | | | 14:00-16:00 | | | INDUSTRI .WASTE | 0.127* | -1.0000 | 4000* | -1 | 0 | 0 | |
| 130) | 1 | 70 | 2 | 55 | 915 | | 8400 | | 1-12 | 13 | C HEAVY OIL | 3.300 | 0.9900 0.9900 0.9200 | 9900 9900 | -1 -1 | 333 | 2800 3500 | |
| 132) | | 70 | | | 1106 | | | 0:00-24:00 | | | | 0.002* | -1.0000 | 10950× 12145* | -1 -1 | 167 83 | 1400 | |
| 133) | 1 | 71 | . 1 | 64(1) | 1106 | 60 | 4800 | 6:00-22:00 |) 1-12 | | ELECTRICITY OTHER RAW | | -1.0000 | 860+ €0 | -1 | . Z | 9 0 | |
| 134) | 1 | 71 | | 64(1) | 1106 | 60 | 4800 | 6:00-22:00 | 1-12 | 61 | ELECTRICITY OTHER RAW | 0.000* | -1.0000 | 860+ Q# | -1 -1 | 20 | 9 | |
| 135) 136) | | 72 72 | | 71 71 | | | | 8:00-16:00 8:00-16:00 | | | | 0.002= | -1.0000 -1.0000 | 11158 11158 | -1 -1 | 141 141 | 282 282 | |

| | | | | | LIST | T OF F | ACILITY (P | ATTERN | 1) | | | | | | | |
|--|-----------|-------------------|--|------------------------------|----------------------------|----------------------|--|------------------------------|----------------------|---|---------------------------|---|-------------------------|----------------------------------|----------------------------|---------------------------------------|
| SEQ) | 016 1 | OK TET | 33 (AI | L111 | 1186 | NUUR | OPERATING TIME ZONE START-END | TING | | N A N E | FUEL AND Sulfur (%) | RAW MAT Gravity | CALORY | BE USED- RATING (/H) | NORMAL (/H) | ANNUAL (/Y) |
| 137) | | | | 2501 | | 6048 | | | | | 0,002 | | 11900 | -1 | 3 | 15 |
| 138) | | 73 2 73 3 | 72 | 2501 | ÷ . | 6048 | 0:00-24:00 | | 15 | KEROSENE | 0.033 | -1.0000 | 11056 | -1 -1 | 27 | · 163 61 |
| 140) | 1 | 73 4 | 72 | 2501 1423 103 | 84 | 4032 6336 2304 | 7:00-24:00 0:00-24:00 8:00-17:00 | 1-12 | 35 | LPG | 0.002 | 0.9900 | 11900 | -1 | 10 10 | 61 64 |
| 142) | | | 72 | 103 | | | 8:00-17:00 | | | | | 0.9200 | | 11 60 | 11 60 | 26 127 |
| 143) 144) 145) | 1 | | 77(1) | 1106 | 79 | 4048 4048 4048 | 6:00-20:00 6:00-20:00 6:00-20:00 | 1-12 | 14 | LIGNY OIL | 1.200 | 0.8660 0.8660 0.8660 | 10950* | -1 -1 -1 | 14 14 14 | 56 56 56 |
| 146) | | 3 1 | 2(1) | 103 | | 8760 | 010-24:00 | 1-12 | 11 | A HEAVY OIL | 1.280 | 0.9462 | 10000 | 38 | 28 | 245 |
| 1473 | | 4 1 | 42 | 103 | | 3000 | | | | A HEAVY OIL | | 0.9408 | | 140 | 138 | 414 |
| 148) 149) 150) 151) 152) 153) | 2 2 2 2 2 | | 77(1) 77(1) 77(1) 77(1) 77(1) 77(1) | 1106 1106 1106 1106 | 77 77 77 77 77 | 4224 | 8:00-24:00 8:00-24:00 8:00-16:00 8:00-16:00 | 1-12 1-12 1-12 1-12 | 35 35 35 35 | 1 <i>PG</i> 1PG 1PG | 0.002 0.002 0.002 | -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 0.9750 | 11158 11158 11158 | -1 -1 -1 -1 -1 -1 | 27 27 18 70 82 | 112 112 112 37 149 216 |
| 154) | 2 | 6 1 | 9(1) | 103 | 85 | 960 | 8:00-16:00 | 1-12 | 25 | PADDY & HUSK | 0.0004 | -1.0000 | 3440 | -1 | 542 | 520 |
| 155) 156) | | 7 <u>1</u> 7 2 | 22(4) | 103 103 | | 0 1600 | 8:00-17:00 8:00-17:00 | 11- 4 11- 4 | 11 11 | A REAVY OIL A REAVY OIL | | 0.9408 | | -1 31 | 26 0 | 0 41 |
| 157) | | 8 1 | 26 | 103 | -1 | | | | | A HEAVY OIL | | 0.9462 | | - 65 | 50 | 120 |
| 158) 159) | | 9 1 9 2 | 42 | 103 103 | | 2440 | 7:00~ 8:00 | 1-12 | 11 | A REAVY DIL A HEAVY DIL | | 0.9462 | | -1 | 0 | 0 |
| 160) | 2 | 9 3 9 4 | 42 42 | 103 | 84 87 | 2840 2840 | 7:00-15:00 7:00-15:00 | 1-12 1-12 | 11 11 | A HEAVY OIL A HEAVY OIL | 1.280 | D.9462 0.9462 0.9462 | 10000 | -1 -1 -1 | 93 186 278 | 245 490 735 |
| 162) 163) | | | | 103 103 | | 3400 | 7:30-22:45 | 1-12 | 11 | A HEAVY OIL A HEAVY OIL | | 0.9462 | | -1 -1 | 57 57 | 204 204 |
| 164) 165) | 2 | 11 2 | 22(1) | 103 103 | 75 | 4200 4200 | 7:00-21:00 | 1-12 | 13 | C HEAVY OIL C REAVY OIL | 2.500 | 0.9529 0.9529 | 10340 | -1 -1 | 143 143 | 600 600 |
| 166) 167) | | | 55 | 915 | | 7854 2400 | 0:00-24:00 | | | · . | | -1.0000 | | 221 | 208 | 1650 |
| 168) | | | 70 | 103 | | 2080 | 8:00-16:00 | | | PADDY & HUSK | | 0.9200 | 3440 | -1 | 1000 | 2400 |
| 169) | | | 4(4) | 103 | | 1500 | | • | | A HEAVY OIL | | 0.9358 | | 15 -1 | 11 120 | 23 150 |
| 170) | 2 | 16 1 | 47(3) | 103 | -1 | 1500 | 9:00-14:05 | | | | | 0.8596 | | 1 | 1 | 1 |
| 171) 172) 173) | s s | 17 2 | 60 | 103 502 8 | | 7200 4320 4500 | 0:00-24:00 0:00-24:00 8:00-23:00 |) 1-12 | 13 | C HEAVY OIL C HEAVY OIL LPG | 3.500 | 0.9950 | 9900 | 27 54 -1 | 25 42 15 | 183 181 66 |
| 1743 | 2 | 18 1 | 9(1) | 1 | -1 | 960 | | | | LIGHT OIL | 0.560 | 0.8413 | | -1 | 13 | 12 |
| 1751 | | | 4(1) | | | 0 7680 | 0:00-24:00 0:00-24:00 | 1-12 | 11 11 | A HEAVY DIL A BEAVY DIL | | 0.9358 0.9358 | | -1 -1 | 0 70 | 0 538 |
| 177) | 2 | 20 1 | 64 (9) | 503 | 87 | 870 | 10:30-13:30 | 1-12 | 12 | B HEAVY OIL | 1.500 | 0.9750 | 10000 | -1 | 22 | 20 |
| 1783 | - | | | 103 | 85 | 1080 | 7:30-16:30 | 1-12 | 25 | PADDY & HUSK | 0.000 | -1.0000 | 3440 | -1 | 250 | 270 |
| 179) | | | | | | | 8:00-11:00 | | | | 1.500 | 0.9200 | 10950= | -1 | 3 | 2 |
| 1803 | 2 | 23 1 23 2 | 15(1) | 103 | 82 | 1600 | 8:00-16:00 |) 1-12 | 13 | GENERAL COAL C HEAVY OIL | 2.500 | -1.0000 | 9900 | 167 100 | 125 75 | 900 120 |
| 182) 183) 184) | 2 (| 23 4 | 15(1) 15(1) 15(1) | 1106 | 82 | 0 1600 1600 | | 1~12 | 13 | C HEAVY OIL A HEAVY OIL A HEAVY OIL | 2.000 | 0.9529 0.9408 0.9408 | 10000 | -1 -1 -1 | 0 78 76 | 0 125 |
| | 2 | | 78(1) | | | 4368 | 6:00-22:00 | | | | | -1.0000 | | -1 -1 | 233 | 125 1018 |
| 186) | e e | | 78(1) | | | 4368 | 6:00-22:00 | | 14 35 | LIGHT OIL LPG | 0.560 | 0.8300 | * 10950* 11158 | -1 -1 | 102 233 | 445 1018 |
| 187) | 2 | 24 3 | 78(1) | 1106 | 77 | 4368 | 6:00-22:00 | 1-12 | 35 | LIGHT OIL LPG | 0.560-0 | 0.8300 | + 10950+ 11158 | -1 -1 | 102 | 445 1018 |
| 1883 |) 2 | 24 4 | 78(1) | 8 | 77 | 4368 | 9:00-55:00 | . 1-12 | | LIGHT OIL Light oil | | | 10950* 10950* | -1 -1 | 102 16 | 445 70 |
| 189) | | 25 1 | 77(2) | | | | 8:00-16:00 | | | | 0.002 | -1.0000 | 11158 | -1 | 72 | 173 |
| 190) 191) 192) | | 26 2 | | 1106 | 81 | 810 | 8:00-13:00 | 1-12 | - 35 | A HEAVY OIL LPG Electricity | 0.002 | 0.9850 -1.0000 -1.0000 | 11158 | -1 -1 -1 | 25 5 0 | 180 4 0 |
| 193) | | | 59 | | | | 0:00-24:00 | | | OTHER RAW ELECTRICITY | | -1.0000 | | 13461 8297 | 11538 7111 | 57600 35500 |
| 194) | | 1 5 | | | | | 0:00-24:00 | | 46 61 | OTHER RAW ELECTRICITY | 0.000 | -1.0000 | ≎0 ≉068 | 13461 8297 | 11538 7111 | \$7600 35500 |
| 195) 196) | - | 1 3 | | | 7202 | 0 4864 | | | 61 | OTHER RAW ELECTRICITY | 0.000 | -1.0000 | 860= | -1 -1 | 0 | 0 |
| 1967 | | 2 1 | | | 6803 7706 | | | | | C HEAVY OIL | | 0.9900 | | 673 600 | 576 400 | 2880 2880 |
| 198) | 3 | 2 Z | 8(1) | 103 | 7706 | 7200 | 0:00-24:00 | 1-12 | 13 | C HEAVY OIL | | 0.9529 | | 400 | 400 | 2880 |
| 199) | | | 22(2) | | | | | | | C HEAVY OIL | | 0.9529 | | 315 | 113 | 951 |
| 200) | 3 | 4 1 | 38(2) | 103 | 8801 | 8520 | 0:00-24:00 | 1-12 | 13 | C HEAVY OIL | 2.660 | 0.9765 | 10400 | 271 | 250 | 2130 |

| SEQ) | CO FAC FAC | | | | | OPERATING | OPERA | | N A N | E | | RAW NATE GRAVITY | | | HORMAL | |
|--------------|------------------|--------------|--------------|----------|--------------|--------------------------|--------------|------|--------------------|---------|--------|---------------------|----------------|------------|------------|--------------|
| | TY Y TY | | | | | START-END P | | | | c | (1) | GANDIT | (KCAL/) | (/H) | (/8) | (/ Y) |
| | | | | ÷., | | | | | | | - A. | | | | | |
| 201) 202) | 3 5 1 3 5 2 | 13(2) | 103 | | | 0:00-24:00 | | | A HEAVY | | | 0.9408 | 10430 10430 | 3270 | 0005 0 | 20904 0 |
| 203) | 3 5 3 | 13(2) | 103 | 64 | : 0 | 0:00-24:00 | 1-12 | 11 | A HEAVY | DIL | 2.000 | 0.9408 | 10430 | -1 | 0 | 0 |
| 204) | 3 5 4 | 13(2) | 1802 | 7502 | 8040 | 0:00-24:00 | 1-12 | 15 | KEROSEN | E | 0.0331 | 0.7951 | 11000 | 72 | 36 | 289 |
| 205) | 3 6 1 | 59 | 601 | 6812 | 2352 | 8:00-17:00 | 1-12 | | C HEAVY IRON | 011 | | 0.9764 | 10400 | 200 | 175 | 412 2800 |
| 206) | 3 6 2 | 59 | 601 | 6812 | 2352 | 8:00-17:00 | 1-12 | 13 | C REAVY | OIL | 2.660 | 0.9764 | 10400 | 220 | 190 | 447 |
| 2075 | 3 6 3 | 59 | 601 | 6812 | 2352 | 8100-17:00 | 1-12 | - 41 | IRON C REAVY | 011 | | -1.0000 | 03 10400 | -1 | 1275 | 3000 784 |
| | | | | | | | | | IRON | | | -1.0000 | 0+ | -1 | 2210 | 5200 |
| 208) | 371 | 59 | | | 2400 | 7:30-16:00 | 1~12 | | C HEAVY | | 2.660 | 0,9764 | 10400 | -1 | 220 | 528 |
| 2093 | 3 7 2 | 59 | 601 | 8707 | 2400 | 7:30-16:00 | 1-12 | 13 | C HEAVY | 01L | 2.660 | 0.9764 | 10400 | -1 | 110 | 264 |
| 210) | 3 8 1 | 55(5) | 103 | 8801 | 8448 | 0:00-24:00 | 1-12 | 13 | C HEAVY | 01L | 3.500 | 0.9900 | 10495. | 372 | 73 | 616 |
| 211) | 3 9 1 | 47(1) | | | 7896 | 0:00-24:00 | 1-12 | | SULFIDE | | | -1.0000 | 1500+ | -1 | 28 | 217 |
| 212) 213) | 3 9 2 | | 103 103 | | 7896 1440 | 0:00-24:00 | 1-12 1-12 | | A HEAVY A HEAVY | | 1.280 | 0.9462 | 10000 10000 | . 21 21 | 17 | 132 |
| 214) | 3 9 4 | 47(1) | 1105 | 68 | 6000 | 0:00-24:00 | 1-12 | 14 | LIGHT O | 11 | 0.600 | 0.8450 | 10950* | 83 | 75 | 450 |
| 215) | 3 10 1 | - 59 | 601 | 7801 | 2368 | 8:00-17:00 | 1-12 | 13 | C HEAVY | 01L | 2.160 | 0.9612 | 10461 | 338 | 230 | 545 |
| 216) | 3 11 1 | 52(2) | 103 | | 4800 | 8:00-24:00 | | | A HEAVY | | 1.280 | 0.9462 | 10000 | -1 | 38 | 180 |
| 217) | 3 11 2 | 52(2) | 103 | 87 | 4800 | 8:00-24:00 | 1-12 | 11 | A HEAVY | 011 | 1.280 | 0.9662 | 10000 | -1 | 45 | 216 |
| 218) 219) | 3 12 1 3 12 2 | | | | 8400 2160 | 0:00-24:00 7:15-19:15 | 1-12 | | PADDY & A HEAVY | | | -1.0000 | 3500+ | 208 | 125 | 1048 |
| | * | | | | | | | | | | | 0.9462 | 10000 | 110 | 62 | 134 |
| 220) 221) | 3 13 1 3 13 2 | 9(6) 9(6) | 103 | | 0000 0000 | 0:00-24100 | | | C HEAVY C HEAVY | | | 0.9306 | 10495 | 250 250 | 190 190 | 1140 1140 |
| 222) | 3 14 1 | 38(2) | 103 | 6412 | 2020 | 0:00-24:00 | 1-12 | | C HEAVY | | 2.500 | 0.9529 | 10340 | 558 | | |
| 223) | 3 14 2 | 38(2) | 103 | 72 | 7920 | 0:00-24:00 | 1-12 | 13 | CHEAVY | 01L | 2,500 | 0.9529 | 10340 | 558 | 516 516 | 4087 |
| 224) 225) | 3 14 3 3 14 4 | | 103 | | 7920 | 0:00-24:00 | 1-12 1-12 | 13 | C HEAVY C HEAVY | 011 | 2.500 | 0.9529 | 10340 | 558 -1 | 516 0 | 40.87 |
| 226) | 3 15 1 | 6(1) | 103 | -1 | 1800 | 8:00-14:00 | 1-12 | | LUMBER | | 0 100 | -1.0000 | 3500= | -1 | - | |
| | | 3(1) | 105 | -1 | 1000 | 0.00-14100 | 1-12 | | A HEAVY | OIL | | 0.9612 | 10461 | 10 | 133 | 240 3 |
| 227) | 3 16 1 | 51 | 103 | | 4200 | 0:00-24:00 | 1-12 | 13 | C HEAVY | OIL | 3.500 | 0.9950 | 9900 | 233 | 225 | 945 |
| 228) 229) | 3 16 2 3 16 3 | | 103 103 | | 4200 2112 | 0:00-24:00 | 1-12 1-12 | 13 | C HEAVY | 011 | 3.500 | 0.9950 | 9900 | 233 311 | 225 | 945 634 |
| 230) | 3 16 4 | | 103 | | 2112 | 0:00-24:00 | 1-12 | | C HEAVY | | | 0.9950 | 9900 | 389 | 375 | 792 |
| 231) | 3 17 1 | 8(1) | | | 900 | 0:00-24:00 | 1-12 | 13 | C HEAVY | OIL | 3.500 | 0.9900 | 9900 | 300 | 215 | 194 |
| 232) | 3 17 2 | 8(1) | 103 | 85 | 7200 | 0:00-24:00 | 1-12 | 13 | C HEAVY | 011 | 3.500 | 0.9900 | 8900 | 300 | 216 | 1555 |
| 233) | | | 103 | | 3200 | 9:00-55:00 | 1-12 | | A HEAVY | | | 0.9462 | 10000 | 103 | 62 | 197 |
| 234) 235) | 3 18 2 | 5(3) | 103 | | 7200 3200 | 0:00-24:00 6:00-22:00 | 1-12 1-12 | 11 | A HEAVY A HEAVY | 01L | 1.280 | 0.9462 | 10000 | 105 85 | 43 51 | 456 164 |
| 236) | 3 18 4 | 5(3) | 103 | 89 | 0 | 0:00-24:00 | 1-12 | 11 | A HEAVY | ŌĨĹ | 1.230 | | 10000 | -1 | õ | Ö |
| 237) 238) | 3 19 1 | 74 (5) | | | | 0:00-24:00 | 1-12 | | LPG | | | -1.0000 | 11805 | 8 | 5 | 31 |
| | 3 19 2 | | | | | 0:00-24:00 | | | ELECTRI | | 0.000* | -1.0000 | 860= | 15 | 7 | 26 |
| 239) | 3 20 1 | 52(1) | 103 | 73 | 7200 | 0:00-24:00 | 1-12 | 13 | C HEAVY | OIL | 2.500 | 0.9529 | 10340 | -1 | 29 | 508 |
| 240) | 3 21 1 | 13(2) | 103 | 84 | 60 | 8:00-17:00 | 1-12 | 14 | LIGHT O | IL. | 0.400 | 0.8450 | 10950* | -1 | 7 | 1 |
| 241) | 3 22 1 | 34(1) | 8 | -1 | 2496 | 8:00-17:00 | 1-12 | 61 | ELECTRI | C 1 T Y | 0.000 | -1.0000 | 860× | · -1 | ٥ | 1 |
| 242) | 3 23 1 | | 611 | | 7200 | 0:00-24:00 | 1-12 | 11 | A HEAVY | OIL | 2.000 | 0.9408 | 10430 | 100 | 80 | 576 |
| 243) 244) | 3 23 2 3 23 3 | | 611 | | 7200 7200 | 0:00-24:00 0:00-24:00 | 1-12 1-12 | 11 | A HEAVY A HEAVY | 01L | 2.000 | 0.9408 | 10430 | 100 | 80 | 576 |
| 245) | 3 Z3 4 | 60 | 612 | 83 | 4800 | 0:00-24:00 | 1-12 | 61 | ELECTRI | C1TY - | 0.000 | -1.0000 | 860+ | -1 | 80 429 | 576 2059 |
| 246) 247) | 3 23 6 | | 612 1421 | | 4800 540 | 0:00-24:00 8:00-15:00 | 1-12 1-12 | | ELECTRI A HEAVY | | | -1.0000 | 860* 10430 | -1 | 429 80 | 2059 |
| 248} | 3 23 7 | 60 | 1421 | 84 | 540 | 8:00-15:00 | 1-12 | 11 | A HEAVY | 01L | | 0.9408 | 10430 | 100 | 80 | 43 |
| 2493 2503 | 3 24 1 3 24 2 | 77(1) | | | 2096 2096 | 7:00-16:00 7:00-16:00 | | 13 | C HEAVY | 01L | | 0.9900 | 9900 | 75 | 63 | 131 |
| 251) | 3 24 3 | 77(1) | 1106 | 62 | 2096 | 7:00-18:00 | 1-12 | 35 | LPG LPG | | | -1.0000 | 11158 | 41 41 | 37 37 | 77 77 |
| 252) 253) | 3 24 4 | | 1106 | 72 72 | 2096 2096 | 7:00-16:00 7:00-16:00 | 1-12 | | LPG LPG | | 0.002+ | -1.0000 | 11158 11158 | 41 | 37 37 | 77 |
| 254) | 3 25 1 | | | | | 8:00-24:00 | | | | | | | | | | |
| 255) | 3 25 Z | 22(3) | 103 | 64 | 960 | 8:00-24:00 | - 1-12 | 11 | A HEAVY A HEAVY | 011 | 1.280 | 0.9462 | 10000 | -1 -1 | 10 | 10 15 |
| 256) | 3 25 3 | 55(3) | 103 | -1 | 2880, | 8:00-24:00 | 1-12 | 53 | LUNBER | | 0.100= | -1.0000 | 3820 | -1 | 250 | 720 |
| 257) 258) | 3 26 1 | 22(2) | | | 0 000a | 0:00-24:00 0:00-24:00 | 1-12 | 11 | A HEAVY | 011 | | 0.9300. | | -1 | 0 | 0 |
| | | | | | | | | | | 011 | | 0.9529 | 10340 | 63 | 50 | 300 |
| 259) 260) | 3 27 1 3 27 2 | | 103 103 | | 1500 300 | 8:00-16:00 | | | | 01L | | -1.0000 | 3820 10461 | 480 -1 | 400 80 | 600 24 |
| 261) | 3 28 1 | 51 | 103 | 64 | Z400 | 7:00-17:00 | | | A HEAVY | | | 0.9850 | 10000 | | | |
| 262) | | | | | | | | | | | | | | -1 | 60 | 144 |
| 263) | 3 29 2 | 64(1) | 1106 | 72 | 6336 | 0:00-24:00 | 1-12 | 35 | LPG LPG | | 0.002+ | -1.0000 | 11158 11158 | -1 -1 | 33 33 | 208 208 |
| 264) 265) | 3 29 4 | 64(1) | 1106 1106 | | 6336 6336 | 0:00-24:00 | 1-12 1-12 | | LPG LPG | | | -1.0000 | 11158 11158 | -1 -1 | 33 33 | 208 208 |
| 266) 267) | | 64(1) | 1106 | 72 | 6336 | 0:00-24:00 0:00-24:00 | 1-12 | 35 | L PG L PG | | 0.002+ | -1.0000 | 11158 | -1 | 33 | 208 |
| 268) | 3 29 7 | 64 (1) | 1106 | 72 | 6336 | 0:00-24:00 | 1-12 | 35 | LFG | | 0.002= | -1.0000 | 11158 11158 | -1 -1 | 33 33 | 208 208 |
| 269) 270) | 3 29 9 | 64(1) | | 72 | 6336 6336 | 0:00-24:00 | 1-12 1-12 | | LPG ELECTRI | C I T Y | | -1.0000 | 11158 860+ | -1 -1 | 33 | 208 |
| 271) 272) | 3 29 10 | | 1106 | 72 | 6336 | | 1-12 1-12 | 61 | ELECTRI ELECTRI | CI f Y | 0.000= | -1.0000 | 860* | -1 | 0 | 0 |
| ~~~, | , 11 | | * * * * 0 | | 0000 | | 1-15 | 01 | | | 0.000 | -1.0000 | 860= | -1 | 0 | ¢ |

| | 274) | 3 29 3 29 3 29 3 29 | | | | | 41 21 | AKI-ENU | TING PERIOD | | | | | | (#) | | (KÇAL/) | | (78) | CM |
|---|--------------------------------------|------------------------------|-------------|----------------------------------|------------------------------------|-----------------------------------|----------------------------------|--|--------------------------------------|----------------------------|---------------------|--|------------------|----|------------------------------------|---|---|-----------------------------------|---|--|
| | 277) 278) | 3 30 | | 64(1) | 1106 7 | 2 63 | 36 Q: | 00-24:00 00-24:00 00-24:00 | 1-12 | 61 | ÊĻI | ECTRI | CITY | · | 0,000* | -1.0000 -1.0000 -1.0000 | 860* 860* 860* | -1 -1 -1 | 0 0 0 | 0 0 0 |
| | | | | | 103 - 103 - | | | 00-17:00 00-17:00 | | | | | | | | 0.9462 0.9462 | | 90 -1 | 60 Q | 144 |
| | | | | | 103 - 103 - | | | 00-10:00 00-10:00 | | | | | | | | | 10495= 10495= | -1 -1 | 32 32 | 18 18 |
| | 280) 281) | 3 32 3 32 | 1 2 | | 103 B 103 B | | | 00-21:00 00-21:00 | | | | | | | | 0.9358 | 10495+ 10495+ | -1 -1 | 40 40 | 108 108 |
| | 282) 283) 284) | | 1 2 3 | | 703 71 1 71 1302 71 | B | 12 1: | 00-24:00 00- 1:30 00-16:00 | 1-12 | 14 | 1.1 | GHT C | IL | TE | 1.200 | 0.9408 | | 50 1 -1 | 38 1 37 | 319 2 18 |
| | 285) 286) 287) 287) 288) | 3 34 | 1 2 3 4 | 2(1) 2(1) | 103 7 103 7 1106 7 1106 7 | 7 52 3 14 | 00 8: 40 8: | 30- 7:30 30- 7:30 30-24:00 30-24:00 | 1-12 8-12 | 11 11 | A A | KEAVY Keavy | 01L 01L | | 3.000 3.000 | 0.9850 0.9850 0.9850 0.9850 | 10000 | 60 90 110 160 | 56 84 103 155 | 291 437 149 223 |
| | | 3 35 | | | 103 8 103 8 | | | 00- 2:00 00- 2:00 | | 25 23 | PĂ LŲ | DDY I Mber | RUSK | | 0.000. 0.100: | ~1.0000 ~1.0000 ~1.0000 ~1.0000 | | -1 -1 -1 -1 | 0 833 542 | 0 0 4498 2927 |
| | | 3 36 | | - A | 103 8 | | | 00-16:00 00-15:00 | | | | | | | | 0.9509 | 10495+ | -1 | 140 | 369 287 |
| | 293) 2943 2953 | 3 38 3 38 | 1 2 | 52(1) 52(1) | 103 6 103 6 103 6 | 5 24 5 | 00 8: 0 8: | 00-16:00 90-16:00 00-16:00 | 1-12 | 14 14 | | GHT (GHT (|)IL 816 | | 0.460 | 0.8596 0.8596 | 10950+ 10950+ 10950+ | 400 400 400 | 80 0 0 | 192 0 |
| | 296) 297) | | 12 | 22(2) 22(2) | 103 7. 103 8 | | | 00-16:00 | | | | | | | | 0.9612 | | 30 38 | 19 32 | 39 65 |
| | 298) | 3 40 | 1 | 52(1) | 103 7 | 8 25 | 60 8: | 00-16:30 | 1-12 | 13 | C | REAVI | 01L | | 2.500 | 0.9529 | 10340 | -1 | 56 | 144 |
| | 3003 | · | 1 | | 103 7 | | | 00-13:00 00-24:00 | | | | | TOIL | | | -1.0000 | 3820 10400 | -1 45 | 20 | 590 53 |
| | 301) | 3 42 | 2 | 55(5) | 103 7 | 1 65 | 00 0: | 00-24:00 | 1-12 | 11 | | HEAVI | 1 01L | | 2.660 | 0.9764 | 10400 | 45 | 40 70 | 260 |
| | 303) | 3 44 | 1 | 7(1) | 103 7 | 6 9 | 36 7: | 00-10:00 | 1-12 | 11 | A | HEAV1 | 01L | | 5.000 | 0.9408 | 10430 | 120 | 100 | 94 |
| | 304) 305) | 3 44 | | | 103 8 103 8 | | | 00-19:00 00-17:00 | | | | | | | 1 | 0.9408 | | 125 56 | 125 51 | 162 |
| • | 308) 307) | 3 45 | 2 | | 103 - 103 7 | • | | 00-17:00 | | | | | | | | 0.9408 | | -1 | 0 | 0 |
| | 308) 309) 310) 311) 312) | 3 46 3 46 3 46 3 46 | 2 3 4 5 | 22(2) 22(2) 22(2) 22(2) | 103 7 | 907 18 907 9 907 9 907 9 | 50 8: 30 8: 30 8: 30 8: | 00-21:00 00-21:00 00-17:00 00-17:00 00-17:00 |) 1-12) 1-12) 1-12) 1-12 | 13 35 35 35 | С ЦР ЦР | HEAVY G G G | 01L | | 0.005* 0.005* 5.200 | -1.0000 -1.0000 | | -1 -1 -1 -1 -1 -1 | 65 65 21 21 21 21 | 120 120 20 20 20 |
| | 313) 314) 315) 316) | 3 47 3 47 | | 44 44 44 44 | 103 8 103 8 103 - 103 - | 586 1 | 40 0: 0 0: | 00-24:00 00-24:00 00-24:00 00-24:00 |) 1-12) 1-12 | 13 13 | c | HEAVY HEAVY | 01L | | 2.660 | 0.9764 0.9764 0.9764 0.9764 | 10400 10400 | 450 450 450 | 410 410 0 0 | 3542 3542 0 0 |
| | 318) | 3 48 3 48 3 48 | Ş | 59 59 59 | 601 7 601 7 601 8 | 1 | 0 8: | 00-17:00 00-17:00 00-17:00 | 1-12 | . 11 | - A - I | HEAVY | DIL | | 2.160 | 0.9612 0.9612 0.9612 | 10461 | 160 -1 -1 | 100 0 0 | 240 0 0 |
| | 320) 321) | | 2 | 64 64 | 103 7 103 7 | | 60 0: 60 0: | 00-24:00 00-24:00 | 1-12 | 11 11 | A A | HEAVY | 01L 01L | | | 0.9462 0.9462 | | 250 250 | 210 210 | 832 332 |
| | 322) 323) 324) | 3 50 | 1 2 3 | 52(1) 52(1) 52(1) | | 4 Z4 | 00 8: | 00-16:00 00-16:00 00-16:00 | 1-12 | 13 | ¢ | HEAVY HEAVY HEAVY | OIL | | 2.500 | 0.9529 0.9529 0.9529 | 10340 | 40 40 -1 | . 30 . 0 | 72 72 0 |
| | | 3 51 3 51 | | 59 59 | 1201 7 | | | 00-24:00 00-24:00 | | 61 12 45 41 61 | 6 RA IR EL | ECTRI HEAVY V COX ON ECTRI | 01L E CITY | | 0.000* 1.950 0.570* 0.000 | -1.0000 -1.0000 0.9370 -1.0000 -1.0000 -1.0000 | 0* 860= 9900 7000* 0* 860= | -1 -1 167 -1 -1 -1 | 7800 12760 83 156 7800 12760 | 65006 73500 478 900 45000 73500 |
| | 327) 328) | | 3 4 | 59 59 | 601 6 601 8 | | | 00-24:00 00-26:00 | | 45 12 | RA B | HEAVY HEAVY HEAVY | OIL | | 0.570* | 0.9370 -1.0000 0.9370 0.9370 | 9900 7000= 9900 9900 | 167 -1 700 700 | 83 156 585 585 | 478 900 2808 2106 |
| | 329) 330) | 3 52 3 52 | | | 103 7 103 8 | | | 0-24:00 | | | | | | | 1.280 | 0.9462 | | -1 400 | 0 257 | 0 1850 |
| | 331) | 3 53 | 1 | 46 | 103 7 | Z 16 | | 00-16:00 | | | | | | | | | 10950= | -1 | 5 | 8 |
| | 332) 333) 334) 335) | 3 54 | 1 2 3 4 | 13(2) 13(2) 13(2) 13(2) | 103 7 | 1 28 1 28 | 80 0:0 80 0:0 | 00-24:00 00-24:00 00-24:00 00-24:00 | 1-12 | 13 13 | ¢ i | HEAVY HEAVY | 0IL 0IL | | 3.500 | 0.9900 0.9900 0.9900 0.9900 0.9900 | 9900 9900 9900 9900 | 400 400 400 | 300 300 300 300 | 864 864 864 864 |
| | 336) | 3 55 | 1 | 48(2) | | | | 0-17:00 | | | | | | | | 0.9300 | | -1 | 0 | 0 |
| | 337) 338) | 3 56 3 57 | 1 | | 103 8 103 7 | | | 00-21:00 | | | | | | | | 0.9612 | | -1 29 | 77 29 | 324 188 |

| SEQ) | CO FAC FAC | BUSINE | FACI | STAR | OPE. | OPERATING | OPERA | | FI | UEL AND F | AW HATE | RIAL TO | BE USED- | | |
|------------------------------|--------------------------------------|----------------------------------|------------------------------|----------|------------------------------|--|----------------|----------|---|----------------------------------|--------------------------------------|----------------------------------|--------------------------|--------------------------|------------------------------|
| | זי ייז | SS CAT Egory | TYPE | YEN | KOUR (H) | TIME ZONE START-END | TING PERIOD | | NAHE | SULFUR ((X) | | CALORY (KCAL/) | RATING | NORHAL (74) | ARNUAL (/Y) |
| 340) | 3 57 2 3 57 3 | 8(1) 8(1) | 103 103 | 77 83 | | | | | A HEAVY OIL Other solid | 1.280 0.100+- | 0.9462 | 10000 3440 | -1 1458 | 1250 | 8100 |
| 341) | 3 58 1 | 8(1) | 103 | | • | | | | C HEAVY OIL | | | 10495* | -1 | | C |
| 342) 343) 344) 345) | 3 59 1 3 59 2 3 59 3 3 59 4 | 22(2) 22(2) 22(2) 22(2) | | 84 82 | 8448 | 0:00-24:00 0:00-24:00 | 1-12 1-12 | 13 13 | C HEAVY OIL C HEAVY OIL C HEAVY OIL C HEAVY OIL | 2,500 2,500 2,500 2,500 | 0.9529 0.9529 | 10340 10340 10340 10340 | -1 -1 -1 -1 | 0 250 50 50 | 2112 422 422 |
| 346) | 3 60 1 | 22(2) | 103 | 78 | 2700 | 8:00-17:00 | 1-12 | 11 | A HEAVY OIL | 2,160 | 0.9600 | 10481 | -1 | 27 | 72 |
| 347) | 3 61 1 | 22(2) | 103 | 88 | 2400 | 7:30-15:00 | 1-12 | 23 | LUMBER | 0.100+- | 1.0000 | 3500* | -1 | 175 | 420 |
| 348) 349) 350) | 3 62 1 3 62 2 3 62 3 | 2(2) | 1004 1004 1004 | 80 | 4500 4500 4500 | 8:00-23:00 8:00-23:00 8:00-23:00 | 1-12 | 15 | KEROSENE | 0.0331 | 0.7951* | 11100* 11100* 11100* | 27 27 27 | 24 24 24 | 108 108 108 |
| 351) 352) | 3 63 1 3 63 2 | 53(7) 53(7) | | | 2320 0 | 8:00-16:00 8:00-16:00 | | 19 35 | OTHER LIQUID LPG | | 0.8569 | | -1 | -15 0 | 35 |
| 353) 354) 355} | 3 64 1 3 64 2 3 64 3 | 77(1) 77(1) 77(1) | 103 103 103 | 74 | 2750 2750 2750 | 7:30-20:00 | 1-12 | 11 | A HEAVY OIL A HEAVY OIL A HEAVY OIL | 1.290 | | 10542 10542 10542 | -1 -1 -1 | 18 18 18 | 50 50 50 |
| 356) | 3 65 1 | 52(1) | 103 | 85 | 2400 | 7:00-17:00 | 1-12 | 11 | A HEAVY OIL | | 0.9358 | | -1 | 35 | 84 |
| 357) | 3 66 1 | 22(4) | 103 | 8401 | 4080 | 5:00-17:00 | 1-12 | 26 | OTHER SOLID | 0.000 - | 1.0000 | 3440 | -1 | 200 | 480 |
| 358) 359) 360) 361) | 3 67 1 3 67 2 3 67 3 3 67 4 | 50(4) 50(4) 50(4) 50(4) | 703 8 | 86 86 | 0 | 7:30-16:30 7:30-16:30 | 1-12 1-12 | 13 13 | C HEÁVY OIL C HEAVY OIL C HEAVY OIL Industri.Waste | 2.500 | | 10340 10340 10340 4000+ | 98 -1 -1 -1 | 86 0 0 0 | 210 |
| 362) | 3 68 1 | 22(2) | 103 | | 7200 | | | | A HEAVY OIL | | 0.9358 | | 50 | 38 | 270 |
| 363) 364) 365) | 3 68 2 3 69 1 3 69 2 | 22(2) 22(1) 22(1) | | 80 | 7200 | | 1-12 | 13 | A HEAVY DIL | | 0.9529 | | 50 ~1 | 38 100 | 270 |
| 366) 367) | 3 69 2 3 70 1 3 70 2 | 26 | 103 103 | 83 | 7200 4800 2400 | 8:00-24:00 0:00- 8:00 | 1-12 | 11 | C HEAVY OIL A HEAVY OIL A HEAVY OIL | | 0.9612 | 10340 10461 10461 | -1 -1 -1 | 100 83 83 | 400 |
| 358) 369) | 3 71 1 3 71 2 | 22(2) | 103 103 | 76 | | 0:00-24:00 | 1-12 | 13 | | · . | 0.9529 | 5 · · | -1 -1 | 208 208 | 200 874 874 |
| 370) | 3.72 1 | 22(3) | 103 | | 4800 | 7:00-24:00 | 1 | | 1. A. | 2.500 | | 10340 | 17 | 14 | 68 |
| 371) 372) | 3 73 1 3 73 2 | 34 (3) 34 (3) | | | 7200 7200 | 0:00-24:00 0:00-24:00 | | | | 0.100- | 1.0000 | 3820 3820 | -1 -1 | 750 1250 | 5400 9000 |
| 373) 374) | 3 74 1 3 74 2 | 59 59 | 602 602 | | 2208 2208 | 8:00-15:00 8:00-16:00 | 1-12 1-12 | 13 13 | C HEAVY OIL C HEAVY OIL | | 0.9529 | | 94 94 | 63 63 | 139 139 |
| 375) 376) 377) 378) | 3 75 1 3 75 2 3 75 3 3 75 4 | 2(1) 2(1) | 1106 1106 1106 1106 | 80 84 | 2400 2400 2400 2400 | 0:00-24:00 0:00-24:00 0:00-24:00 0:00-24:00 0:00-24:00 | 1-12 1-12 | 11 11 | A REAVY OIL A REAVY OIL A REAVY OIL A REAVY OIL | 2.000 | 0.9408 0.9408 0.9408 0.9408 | 10430 10430 | 600 600 600 600 | 500 500 500 500 | 1200 1200 1200 1200 |
| 379) 380) | 3 76 1 | 13(2) 13(2) | 103 103 | 82 | 1095 | 8:00-11:00 | 1-12 | 11 | A HEAVY OIL A HEAVY OIL | 1.280 | 0.9462 | 10000 | 45 -1 | 34 | 37 |
| 381) | | 22(2) | 103 | 74 | | 1.1 | | | A REAVY OIL | | 0.9612 | | 17 | 13 | 109 |
| 382) 383) | 5 78 1 3 78 2 | | | | 6000 3000 | 8:00- 4:00 8:00-17:00 | 1-12 1-12 | 11 11 | A HEAVY OIL A HEAVY OIL | | 0.9612 | | 35 30 | 35 30 | 210 |
| 384) 385) | 3 79 1 3 79 2 | 22(2) 22(2) | 103 103 | | \$400 | 8:00- 2:00 | 1-12 | 11 | A HEAVY DIL A HEAVY DIL | 2.000 | 0.9408 | 10430 | -1 | 133 | 720 |
| 386) | 3 80 1 | 22(2) | 103 | 83 | 7200 | 0:00-24:00 | 1-12 | 23 | LUMBER | 0.000 - | 1.0000 | 3820 | ~1 | 16 | 114 |
| 387) | 3 81 1 | 47(1) | 103 | 78 | 4800 | 8:00-24:00 | 1~12 | 14 | LIGHT OIL | 0.460 | 0.8596 | 10950* | -1 | 5 | - 24 |
| 388) 389) | 3 82 1 3 82 2 | 22(4) 22(4) | 103 103 | | 3600 3600 | | | | A HEAVY OIL A HEAVY OIL | 2.160 2.160 | 0.9612 | 10461 10461 | 300 300 | 200 150 | 720 540 |
| 390) | 3 83 1 | 13(2) | 103 | 85 | 3000 | 7:00-17:00 | 1-12 | 11 | A HEAVY OIL | 2.760 | 0.9358 | 10495= | - i | 48 | 144 |
| 391) | ··· | 22(2) | | | · · · . | | | , | A HEAVY OIL | | 0.9612 | | -1 | .44 | 120 |
| 392) 393) | 3 85 1 3 85 2 | 22(2) 22(2) | 103 103 | | 2700 0 | 8:00-17:00 8:00-17:00 | 1-12 1-12 | 11 11 | A HEAVY OIL A HEAVY OIL | | 0.9462 | | -1 -1 | 27 G | 72 |
| 394) | 3 86 1 | | 103 | 84 | 1800 | 8:00-14:00 | 1-12 | 11 | A HEAVY OIL | 2.000 | 0.9408 | 10430 | -1 | 40 | 72 |
| 395) 396) | 5 87 1 3 87 2 | 26 | 103 | | | | | | C HEAVY OIL C HEAVY OIL | 2.920 | 0.9509 0.9509 | 10495× 10495× | -1 -1 | 39 45 | 296 345 |
| 397) | 3 89 1 | 22(2) | 103 | 85 | 3000 | 8:00-18;00 | 1-12 | 11 | A HEAVY OIL | 2.160 | 0.9612 | 10461 | -1 | 14 | 41 |
| 398) | | | | | | | | | C HEAVY OIL | | 0.9764 | | 200 | 190 | 441 |
| 399) 400) | | 13(2) | | | | 7:00-15:00 | | | A HEAVY OIL | | 0.9462 | | 65 | 50 | 80 |
| | 3 94 1 | | 1104 | | 480 | | 10+ Q | 14 | LIGH) VIL | V.660 | 0.8413 | 107208 | -1 | : 7 | 2 |

IV - 14

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| | | UN TOR | - ILI | SS CA1 | F 1.11 | Y TINC | i HÖUR | TINE ZONE | TING | N A H E | SULFUR (%) | GRAVITY | CALORY (KCAL/) | RATING (/H) | NORMAL (/H) | ARNUAL (7Y) |
|----------|---------------------------------|-------------------------|----------|----------------------------------|----------------------------------|----------------------------|--|--|----------------------|--|----------------------------------|---|----------------------------------|----------------------------------|--|--|
| 4(| 043 | 3 95 | 22 | 64(5) | 141 | 9 72 | 7200 | 0:00-24:00 | 1-12 | 13 C HEAVY DIL | 2.500 | 0.9529 | 10340 | -1 | 33 | 240 |
| 40 | D5) D6) D7) | 3 96 3 96 3 96 | 2 | 2(5) | 110 110 110 | 5 78 | 270 | 8:00-17:00 | 8-11 | 11 A HEAVY DIL 11 A HEAVY DIL 11 A HEAVY DIL 11 A HEAVY DIL | 1.280 1.280 1.280 | 0.9462 0.9462 0.9462 | 10000 | 139 139 240 | 139 139 260 | 37 37 211 |
| 4 | 08) 09) 10) 11) | | 23 | 2(5) |) 100) 100) 100) 100 | 483 484 | 3590 3590 3590 3590 | 0:00-24:00 | 7-11 | 13 C HEAVY DIL 13 C HEAVY DIL 13 C HEAVY DIL 13 C HEAVY DIL 13 C HEAVY DIL | 2,500 | 0.9529 0.9529 0.9529 0.9529 | 10340 10340 | -1 -1 -1 -1 | გ გ კ | 22 22 22 22 |
| 4. 4. | 12) 13) 14) 15) 16) | 3 98 3 98 3 98 | 2 | 88 88 | 10 10 10 | i 7111 1 7401 1 7508 | 8400 8400 8400 8400 8400 8400 | 0:00-24:00 0:00-24:00 0:00-24:00 0:00-24:00 0:00-24:00 | 1-12 1-12 1-12 | 34 LNG 34 LNG 34 LNG | 0.000 0.000 0.000 0.000 | -1.0000 -1.0000 -1.0000 -1.0000 -1.0000 0.9000 | 13286 13286 13286 13286 | -1 -1 -1 -1 -1 -1 | 24500 24500 45500 45500 45500 54000 | 205800 205800 382200 382200 109200 324000 |
| 4 | 18) | 3 99 3 99 3 99 | 2 | 7(1) | 10 10 10 | | | 6:00-24:00 | 1-12 | 13 C HEAVY OIL 13 C HEAVY DIL 13 C HEAVY DIL | 2.920 | 0.9900 0.9900 0.9900 | 10513 | -1 -1 -1 | 50 50 50 | 240 240 240 |
| | 20) 21) | | | 24 | 10 | 3 80 | | 9:00-15:00 | 1-12 | 11 A REAVY OIL 61 ELECTRICITY | 5.000 | 0.9408 | 10430 | 134 | 100 | 110 |
| | 22> | 3 101 | | 1997 - M | | 680 3-1 | 7920 | | | 11 A REAVY OIL | | •-1.0000 • 0.9300 | 860* 10495* | -1 -1 | 50 | 396 |
| 4 | 23) 24) 25) | 3 102 3 102 3 102 | 1 | 8(1) | 10 | 383 380 883 | 720 720 720 | 8:00-16:00 8:00-16:00 8:00-16:00 | 1-12 | 11 A NEAVY DIL 23 Lumber 11 A Heavy dil | 0.100 | 0.9358 | 3820 | -1 -1 -1 | 313 125 13 | 225 90 |
| 4 | 26) | 3 103 | 1 | 52(2) | 10 | 3 82 | 1400 | 9:00-16:30 | 1-12 | 11 & REAVY OIL | 1.280 | 0.9850 | 10000 | 21 | 14 | 20 |
| 4 | 27) 28) 29) | 3 104 3 104 3 104 | 2 | 53(B) | 91 | 8 87 | | 8:00-12:00 0:00-24:00 0:00-24:00 | 1-12 | 23 LUMBER | 0.100 | -1.0000 -1.0000 -1.0000 | 3820 3820 3820 | -1 -1 -1 | 8 2 2 | 9 11 11 |
| | 30) 31) | 3 105 3 105 | | | | 5 71 | 8760 8760 | | | 11 & REAVY OIL 11 & REAVY OIL | | 0.9462 | | 2063 | 1667 3333 | 14600 29200 |
| 43 | 32) | 3 106 | | 64 (8) | o so | 3 8712 | 2400 | 8:00-17:00 | 1-12 | 11 A HEAVY OIL | 2.760 | 0.9558 | 10495. | -1 | 1 | 3 |
| 4 | 33) | | | 48(3) |) 10 | 3-1 | 1055 | 8:00-17:00 | 1-12 | 11 A HEAVY OIL | 2.160 | 0.9612 | 10461 | . 76 | 61 | 64 |
| | 34) | | | | | | 2920 | | | 14 LIGHT OIL | 1.200 | 0.8660 | 10950* | · -1 | 9 | 25 |
| | 35) 36) | 3 109 | 2 | 55(1 | | | | | | 13 C REAVY DIL 13 C REAVY DIL | 3.500 | 0.9950 0.9950 | | -1 -1 | 167 125 | 600 450 |
| | 37) | 3 110 | 1 | 55(5 | | 3 73 | 0 | | | 13 C HEAVY OIL | | 0.9529 | | 1 | • 0 | |
| | 38) 39) | 3 110 | | 55(5) | | | 1440 8744 | 0:00-24:00 | 1-12 1-12 | 13 C HEAVY OIL 21 General Coal | 2.500 | 0.9529 | 10340 4409 | -1 -1 | 75 208 | 108 1405 |
| ٤. | 40) | 3 111 | 1 | 59 | 120 | 1 71 | 7200 | | | 61 ELECTRICITY 41 IRON | | -1.0000 | +068 · | -1 -1 | 10000 | 72000 123850 |
| | ÷., | 3 111 | | | - | 1 74 | 1296 | | | 61 ELECTRICITY 41 IRON | 0.000 | -1.0000 | 860× | -1 -1 | 5000 8600 | 6480 11150 |
| • | 42) | 3 111 | | 59 | . 60 | 1 77 | 6000 | 0:00-24:00 | 1-12 | 13 C HEAVY OIL 13 C HEAVY OIL 13 C HEAVY OIL | 3.500 | 0.9529 0.9900 0.9900 | 10340 9900 10495* | -1 -1 -1 | 236 236 236 | 1417 1417 1417 |
| 4. | 43} | 3 111 | . 4 | 59 | 10 | 3 85 | 7200 | 0:00-24:00 | 1-12 | 13 C HEAVY OIL 13 C HEAVY OIL | 2.500 | 0.9529 | 10340 9900 | -1 -1 | 38 38 | 333 333 |
| 4. | 44) | 3 111 | 5 | 59 | | 8 85 | 7200 | 0:00-24:00 | 1-12 | 13 C HEAVY OIL 13 C HEAVY OIL 13 C HEAVY OIL 13 C HEAVY OIL 13 C HEAVY OIL | 2.500 | 0.9900 0.9529 0.9900 0.9900 | 10340 9900 | -1 -1 -1 -1 | 38 38 38 38 | 333 333 333 333 |
| | 45) 46) | | | 74(2) 74(2) | | 2 73 8 83 | 2568 7200 | 0:00-24:00 0:00-24:00 | 1-12 1-12 | 11 & HEAVY OIL 46 OTHER RAW 61 ELECTRICITY | 0.000 | 0.9300 -1.0000 -1.0000 | ■ 10495= 0= 860= | -1 -1 -1 | 166 1083 550 | 426 7800 3960 |
| 4. | 48) | 3 113 | 2 | | 60 60 | 7.63 | 2120 2120 | 8:00-17:00 8:00-17:00 | 1-12 1-12 | 11 A HEAVY OIL 11 A HEAVY OIL | | 0.9612 | | -1 -1 | 160 150 | 339 319 |
| 4 | 50) | 3 113 | - 4 | 77(2) | 60 | 7 63 | 2120 2120 | 8:00-17:00 | 1-12 | 11 A HEAVY OIL 11 A HEAVY OIL | 2.160 2.160 | 0.9612 | 10461 10461 | -1 -1 | 40 40 | 85 85 |
| | | 3 113 | | 77(2) | | 778 878 | 2120 | 8:00-17:00 | | 11 A HEAVY OIL 61 ELECTRICITY 11 A HEAVY OIL | 0.000 | 0.9612 -1.0000 0.9612 | 840= | -1 -1 -1 | 50 0 40 | 127 0 84 |
| 4 | 53) 54) | 3 113 3 113 3 113 | 7 | 77(2) | | 8 78 3 78 3 78 | 2120 2120 | 8:00-17:00 8:00-17:00 | 1-12 1-12 | 11 A HEAVY OIL 11 A HEAVY OIL 11 A HEAVY OIL 11 A HEAVY OIL | 2.160 2.160 | 0.9612 0.9612 0.9612 | 10461 10461 | -1 -1 -1 | 60 40 40 | 127 85 85 |
| 4 | 57) | 3 114 3 114 | 2 | 78(1) | 60 | 387 | 1896 | 6:00~14:00 | 1-12 | 13 C HEAVY OIL 13 C HEAVY OIL | 2.500 | 0.9529 0.9529 | 10340 | -1 -1 | 19 19 | 36 36 |
| 4 | 58) 57) 60) | 3 114 | . 4 5 | 78(1) 78(1) 78(1) | 110 | 5 87 | 1896 | 6:00-14:00 8:00-16:00 8:00-16:00 | 1-12 | | 0.002 | 0.9529 -1.0000 -1.0000 | 11158 | -1 -1 -1 | 13 11 11 | 24 21 21 |
| 4. | 61) 62) 63) 64) | 3 119 3 119 3 119 | 23 | 78(1) 78(1) 78(1) 78(1) | 110 | 678 688 | 4160 4160 | 6:55-23:00 6:55-23:00 6:55-23:00 6:55-23:00 | 1-12 1-12 | 35 LPG 35 LPG | 0.002 | -1.0000 -1.0000 -1.0000 | 11158 11158 | -1 -1 -1 -1 | 14 14 14 14 | 56 56 56 56 |
| 4 | 65) | 3 117 | | 59 | 120 | 5 85 | | · · · · | | 46 OTHER RAW | 0.000 | -1.0000 | Ű≢ | -1 | 4400 | 34500 |
| | 66) 67) | 3 117 3 117 | 3 | | | 2 70 | | | | 61 ELECTRICITY 13 C HEAVY OIL 13 C HEAVY OIL | 2.860 | -1.0000 0.9764 0.9764 | | 7000 500 600 | 5500 450 500 | 43560 1782 750 |
| 4. | 68) | 3 118 | | 59 | 120 | 2 76 | 6480 | 0:00-24:00 | 1-12 | 46 OTHER RAW 61 ELECTRICITY | | -1.0000 | 0= 860= | -1 -1 | 4333 4533 | 28080 29372 |
| | | 3 118 3 118 | | 59 59 | | 1 72 1 72 | | | | 13 C HEAVY OIL 13 C HEAVY OIL | 2.460 | 0.9300 | | -1 | 500 500 | 540 540 |
| | | | | | | | | | | | | | | | | |
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| | CO FAC FAC UN TOR ILI TY Y TY | HOUR | PRODUC. | ENITT RATING (RM3/H) | ED GAS NORMAL (NH3/K) | ANNUAL Sox (NM3/Y) | ANNUAL NOX (RH3/Y) | SHA NO PE | HEI | DIA | ACK TEM (*C) | NX | МΥ | DX (N) | |
|-------------------|-------------------------------------|--------------|------------|----------------------------|-----------------------------|--------------------------|--------------------------|--------------|------------|----------|----------------------|-------------|------------|------------|------------|
| 1) | 1 1 1 | 4428 | -1 | -1 | 1526+ | 6177 | 927 | 18 | 15 | 0.5 | 215 | 22 | 23 | 120 | , 9 |
| 2) ⁻ | | 1675 | -1 | ~1 | 3816= | 6704 | 860 | . 1 B | | <u>م</u> | 200 | 26 | 10 | 460 | |
| 3) | | 8040 | -1 | -1 | 272+ | 2 | 194 | 2 8 | 12 | 0.4 | 200 | 26 | 10 | 460 | 3 |
| 4) 5) | 1 2 3 | 8040 1675 | -1 | -1 | 369= 78+ | 2 | 264 | 38 | 12 | 0.4 | 200 | 26 26 | 10 | 460 | 3 |
| | | | | • | 100 | ų | 12 | 4 B | 12 | 0.0 | 200 | - 60 | 10 | 460 | 3 |
| 6) 7) | 1 6 1 | 3000 | -1 -1 | ~1 -1 | 827+ 1670+ | 1323 | 320 | 1 B | 12 | 0.3 | 200 | 26 | | 600 | |
| | | 1200 | -4 | -1 | 10/04 | 6404 | 1553 | 28 | 12 | 0.3 | 200 | 26 | 11 | 600 | • |
| 8) | 2 7 1 | 1680 | -1 | -1 | 1078+ | 342 | 55 | 1 8 | 26 | 0.7 | 150 | 28 | 11 | 20 | 1 |
| 9) | | 7200 | -1 | -1 | 216* | 1177 | 188 | 18 | | 1.5 | 100 | 21 | 14 | 40 | |
| 10) | 1 8 2 | 7200 | 72000 | -1 | 42000+ | 0 | 12503 | 18 | | | 100 | 21 | 14 | 40 | |
| 11) | 1 9 1 | 7200 | 8600 | -1 | 5017= | 0 | 1493 | | | 9.9 | _1 | 22 | | 4.00 | |
| | | | | | · · · · · | | 1473 | 18 | 2 | ¥.Y | -1 | 22 | 23 | 650 | 1 |
| 12) 13) | 1 12 1 | 4800 4800 | -1 -1 | -1 -1 | 19875+ 19875+ | 100054 | 12831 | 18 | | 0.8 | | 27 | 9 | 220 | 1 |
| 14) | 1 12 3 | 0 | -i | -1 | 1701.50 | 100035 | 12831 | 2 B 3 B | | 0.8 | | 27 27 | | 220 | |
| 15) | 1 : 13 1 | | | | | | - | | | | - | | | -10 | 1 |
| 1.57 . | | 2000 | -1 | -1 | 196* | 89 | 33 | 1 A | 20 | 0.3 | -1 | 55 | 21 | 540 | 8 |
| 16) | 1.14 1 | 1450 | -1 | -1 | 1097* | 848 | 205 | 1 B | 25 | 0.4 | -1 | 22 | 12 | 240 | Í S |
| 17) | 1 15 8 1 | 8760 | -1 | -1 | 2671= | 12290 | | | | | | | | | |
| 18) | | 8760 | -1 | -1 | 2671= | 12290 | 2452 2452 | 1 B 2 B | | 1.6 | 80 80 | 34 34 | | 500 | |
| 19) | 1 15 .3 | 8760 | -1 | -1 | 1996* | .: 11 | 915 | 3 B | 12 | 0.6 | 80 | 34 | 8 | 500 | 2 |
| 20) 21) | 1 15 4 | 8760 8760 | -1 -1 | -1 | 0* | . 0 | 0 | 4 B. | | 0.8 | -1 | 34 | 8 | 500 | 2 |
| 22) | | 8760 | -1 | -i | 0. | .ŭ | . 0 | 5 B 6 B | | 0.6 | -1 -1 | 34 | 8 | 500 500 | 2 |
| 23) | 1 16 1 | 2400 | - • | - • | | _ | | | | 1 | | | | | |
| 237 | | 2600 | -1 | -1 | 363= | 0 | 42 | 1 B | . 5 | 9.9 | -1 | 28 | 19 | 120 | 1 |
| 24) | | 7200 | -1 | -1 | 4770= | 28228 | 4621 | 1 A | | 0.9 | | 23 | | 240 | |
| 25) 26) | 1 17. 2 | 1500 | -1 | -1 | 0 387* | 0 | 0 | 1 A 2 A | | | 250 | 23 | 21 | 240 | 8 |
| | | 1000 | • | | 561+ | v | | ZA | Ş | 0.6 | -1. | 23 | 21 | 160 | 7 |
| 27) 28) | | 4800 | -1 | -1 | 1113: | 4426 | 716 | 1 B | | 0.5 | -1 | 24 | | 500 | |
| 207 | 1 18 2 | 800 | -1 | -1 | 3175= | 1 | 116 | 28 | 5 | 9.9 | ~1 | 24 | 21 | 500 | 3 |
| 29) | | 6240 | -1 | -1 | 1005= | 5668 | 851 | 1 B | 18 | 0.5 | -1 | 22 | 32 | 280 | 8 |
| 30) | 1 19 2 | 4368 | -1 | -1 | 1002* | 3968 | 596 | 2 A | 16 | 0.6 | ~1 | 25 | 12 | 280 | 8 |
| 31) | | 6912 | · -1 | -1 | 17935∓ | 130071 | 16680 | 18 | 15 | 1.0 | 250 | 30 | 8 | 380 | ٦ |
| 32) | 1 20 2 | 0 | -1 | -1 | · 0 | 0 | 0 | 1 B | | 1.0 | | 30 | | 380 | |
| 33) 34) | 1 20 3 | . 0 | : -1 -1 | -1 | 0 | 0 | 0 | 28 | | 1.0 | | 30 | . 8 | 380 | 3 |
| 35) | | 6912 | -1 | 1 | 739. | 0 | 0 483 | 2 B 3 B | | 1.0 | 250 | 30 | 8 | 380 380 | 3 |
| 39) | 1 20 6 | 6912 | -1 | -1 | 194 . | 1 | 121 | 4 B | | 0.5 | -1 | 30 | | 380 | |
| 37) | 1 20 7 | 6912 | -1 | -1 | 1315+ | 3 | 411 | 58 | | 0.4 | -1 | 30 | | 380 | |
| 38) | 1 21 1 | 1048 | -1 | -1 | 87* | 1 | 5 | 1 . | 7 | 0.3 | -1 | 24 | 21 | 480 | , |
| 39) | | | -1 | -1 | 87* | 4 | 21 | 2 A | 7 | 0.3 | -1 | 24 | 21 | 480 | 2 |
| 40) 41) | 1 21 3 | 3000 3000 | -1 -1 | -1 | 211* 816= | 71 | 34 108 | 3 A 4 A | 7 | 0.3 | -1 -1 | 24 24 | | 480 | |
| , | | 3660 | • | | 010- | • | 100 | - 1 | . 1 | 0.4 | -1 | 24 | 4 t | 480 | ~ |
| 42) | 1 55 1 | 3966 | -1 | -1 | 7632* | 25114 | 3771 | 18 | 20 | 0.5 | -1 | 22 | 13 | 860 | 6 |
| 43) | 1 23 1 | 0 | -1 | -1 | . 0 | 0 | 0 | 1 . | 18 | 0.4 | -1 | 25 | 20 | 260 | 2 |
| 5 | | | | | | | | | | | | | | | |
| 443 | 1 24 1 | 2080 | -1 | -1 | 270= | 680 | 76 | 1 A | 17 | 0.3 | 115 | 22 | 13 | 80 | 9 |
| 45) | 1 25 1 | 2400 | -1 | -1 | 175= | 342 | . 55 | 18 | 6 | 0.5 | -1 | 23 | 13 | 500 | 5 |
| 463 | 1 27 1 | 3840 | -1 | -1 | 17. | ~ | | | | | | | | | |
| | * ** * | | -1 | -1 | 52* | 0 | 3 | 1 8 | 5 | 0.3 | -1 | 34 | . 8 | \$00 | 2 |
| 47) | | \$760 | -1 | -1 | 604 × | 2671 | 647 | 18 | | 0.4 | | 28 | 8 | \$00 | 8 |
| 48) 49) | | 5760 5760 | -1 -1 | -1 -1 | 604 = 604 = | 2671 2671 | 647 | 2 B | | 0.4 | | 85 90 | 8 | \$00 | 8 |
| 50) | | 8400 | -1 | -1 | 197* | 25/1 | 372 | 38 48 | 15 | 0.4 | 270 | 28 28 | 8 8 | 500 500 | 8 |
| 51) | 1 29 5 | 8400 | -1 | -1 | 197• | -1 | 372 | 48 | | Q.8 | ÷ī | 28 | 8 | 500 | 8 |
| 523 | 1 30 1 | 4160 | -1 | -1 | 207= | 670 | 110 | 18 | 9 | 0.3 | ·- 1 | 22 | 14 | 140 | , |
| | | | - | - | | | | | | | | | | | ' |
| \$3) | 1 32 1 | 7200 | -1 | -1 | 749= | 605 | 214 | 1 A | 12 | 0.5 | ` →1 | 23 | 12 | 20 | 1 |
| \$43 | | 5110 | -1 | -1 | 1347 * | 5769 | 933 | 1 A | 12 | 0.3 | -1 | 23 | 23 | \$40 | 7 |
| 553 | | | | | | | | | | | | · | | | |
| 151 | 1 34 1 | 2700 | -1 | -1 | 843* | 2093 | 314 | 18 | 20 | 0.5 | -1 | 22 | 14 | 880 | 4 |
| 56) | | 1480 | -1 | -1 | 3498= | 6796 | 759 | 1 A | | | 210 | 21 | | 400 | |
| 57) | 1 35 2 | 1470 | -1 | -1 | 3498* | 6796 | 759 | 2 A | 15 | 0.7 | 210 | 21 | | 600 | |
| 58) | | 2400 | · -1 | -1 | 1193= | 1526 | 370 | 18 | 12 | 0.8 | '-1 | 22 | 13 | 120 | 7 |
| 593 | 1,36 Z | 2400 | -1 | - 1 | 1193= | 1526 | 370 | 28 | | 0.8 | | 22 | | 120 | |
| 60) | 1 39 1 | 8760 | -1 | -1 | 6310* | 99330 | 13417 | 18 | 15 | 0.5 | -1 | 23 | 21 | 580 | |
| | | | | | | | | | | + | 1 | | | | |
| 61) | 1 40 1 | 2340 | -1 | -1 | 398 * | 984 | 126 | 1 A | 14 | 0.4 | -1 | 55 | 21 | 180 | 9 |
| 623 | 1 41 1 | 5460 | -1 | - 1 | 1988= | 12435 | 1507 | 1 3 | 21 | 0.5 | -1 | 26 | . 11 | 440 | ់រ |
| 63) | 1 41 2 | 5480 | -1 | -1 | 1988* | 12435 | 1507 | 2 B | 21 | 0.7 | -1 | 50 | 11 | 640 | 1 |
| 64) 65) | | 5460 3300 | -1 -1 | -1 | 1988 | 12435 44288 | 1507 5369 | 3 B 4 B | | 0.7 | -1 -1 | 26 | | 640 | |
| | | | | | | | 3304 | • 5 | <i>c</i> 1 | 0.0 | -1 | 26 | ** | 640 | 1 |
| | -1 42 1 | 4640 | -1 | -1 | 795+ | 1967 | 476 | 18 | | 0.3 | | 22 | | 200 | |
| 66) | 1 23 - | | -1 | -1 | 0 | 0 | 0 | 28 | - 25 | 0.3 | 80 | 22 | 16 | 200 | 4 |
| 66) 67) 68) | 1 42 2 | v | | | | | | | | | | | | | |

| | | | | | | LIST OF | FACILITY | , CPATTERI | K 2) | | | | | | | |
|--|-----------------------|--|------------------|--|----------------------------------|--|--|---|---|---|---|----------------------------|--|--|--|--|
| SEQ) | TY | FAC TOR Y | FAC ILI TY | 0PE. HOUR (H) | ARRUAL PRODUC, (TOW/Y) | EMIT RATING (NM3/H) | TED GAS HORMAL (NM3/H) | ANNUAL SOX (NH3/Y) | ANNUAL NOX (RH3/Y) | SHA | HE1 DIA (M) (M) | TEM | | ΗY | | ÐY |
| 69) 70) 71) 72) 73) 74) 75) 76) | | 45 45 45 45 45 45 | 234567 | 7200 7200 7200 7200 7200 7200 3300 | -1 -1 -1 -1 -1 | -1 -1 -1 -1 -1 -1 -1 | 572* 0 26* 26* 26* 167* 39* 49* | 4302 0 123 123 123 123 1 176 80 | 552 0 48 48 48 155 69 22 | 1 B 2 B 3 B 5 B 6 B 7 B 6 | 11 0.4 8 0.4 8 0.2 12 0.3 8 0.3 12 0.3 5 0.2 6 0.2 | -1 -1 -1 -1 -1 | 24 24 24 24 24 24 24 | 12 12 12 12 12 12 12 | 420 420 420 420 420 420 420 420 | 880 880 880 880 880 880 |
| 77) 78) 79) 80) | 1 1 1 | 46 46 46 46 | 1 | 3600 3600 4500 | -1 | -1 -1 -1 -1 | 239* 302* 109* 363* | 711 896 0 0 | 115 145 32 0 | 1 B 2 B 3 8 4 8 | 15 0.9 15 0.4 5 9.9 10 0.4 | 170 170 -1 | 26 26 26 | 9 9 9 | 480 480 480 480 | 280 280 280 |
| 81) 82) | 1 | | 5 | 1320 1320 | -1 -1 | -1 -1 | 1908. 1908: | 1340 1340 | 324 324 | 18 28 | 15 0.5 15 0.5 | | | | | |
| 83) 84) 85) | 1 1 1 | | 1 | 2482 2482 2482 | -1 -1 -1 | -1 -1 -1 | 1399± 461± 763± | 1848 602 1000 | 448 146 242 | 1 B 2 B 3 B | 20 0.3 20 0.3 20 0.3 | -1 | 23 | 14 | | 620 |
| 86) 87) 88) 89) | 1. | 51 51 51 51 | 2 3 | 8472 8472 8472 8472 | -1 -1 -1 -1 | -1 -1 -1 -1 | 398+ 1299+ 631+ 1299+ | 3846 1936 | 456 692 348 692 | 1 B 2 B 2 B 2 B | $\begin{array}{c} 15 & 0.6 \\ 10 & 0.5 \\ 10 & 0.5 \\ 10 & 0.5 \\ 10 & 0.5 \end{array}$ | ~1 -1 | 38 38 38 38 | 6 | 480 480 480 480 | 720 720 |
| 90) 91) | 1 | 52 52 | 1 | 4480 | -1 -1 | -1 -1 | 4775 | 2235 | 287 | 1 B | 25 0.3 15 0.2 | -1 | 22 | 14 | 60 | 320 |
| 925 | 1 | 53 | 1 | 4752 | -1 | -1 | 1097: | 4767 | 716 | 2 B 1 B | 21 0.7 | ~1 | 21 | 23 | 920 | 720 |
| 93) 94) | 1 | 53 54 | | 832 7200 | -1 -1 | -1 -1 | 731• 2182= | 552 3394 | 83 1370 | 2 B 1 B | 21 0.7 9 0.3 | | | | | |
| 95) 96) | | 55 55 | | 8400 8400 | -1 -1 | -1 -1 | 9079* 9079* | 116424 116424 | 10660 10660 | 1 B 2 B | 30 0.6 30 0.6 | | | | | |
| 97) 98) 99) 100) | 1 | 56 56 56 | 3 | 0 6000 1240 1240 | -1 -1 -1 -1 | -1 -1 -1 -1 | 0 3180* 0* 26* | 10174 | 0 2464 0 0 | 1 B 2 B 3 B 4 B | 6 0.6 6 0.6 6 0.6 6 0.3 | 175 · -1 | | 19 19 | 480 480 480 640 | 920 920 |
| 101) 102) 103) 104) | 1 1 1 | 56 56 | 56.7 | 7200 7200 7200 7200 | -1 -1 | -1 -1 -1 -1 | 0= 0= 0= 0= | 00000 | 0 0 0 | 5 B 6 B 7 B 7 B | 4 0.3 4 0.3 5 0.3 5 0.3 | -1 -1 -1 | 21 21 | 19 19 19 | 540 640 840 640 | 980 980 960 |
| 105) | 1 | 58 | 1 | 1960 | -1 | -1 | 795= | 1424 | 214 | 1 B | 15 0.5 | -1 | 22 | 23 | 160 | 940 |
| 106) 107) | | 59 59 | | 1800 1800 | -1 -1 | -1 | 398+ 398+ | 593 593 | 96 | 1 B 2 Ə | 21 0.6 21 0.6 | | | | | |
| 108> | 1 | 61 | 1 | 3600 | | -1 | 4680* | | 454 | 1 A | 18 0.5 | | | | | |
| 109) | | 63 | 1 | 96 | -1 | -1 | 1414+ | 35 | 12 | 1 8 | 15 0.5 | -1 | 22 | 13 | 840 | 720 |
| 110) 111) 112) | 1 | | | 7200 6480 0 | -1 | -1 | 2862= 493= 0 | | 2856 443 0 | 18 28 38 | 10 0.5 6 0.3 15 0.8 | -1 | 23 | 21 | 600 600 600 | 940 |
| 113) 114) | | 65 65 | 1 2 | 270 | | -1 -1 | 272* 272* | | | 18 19 | 11 0.2 11 0.2 | | | | | |
| 115) 116) | | 66 66 | 2 | 3600 3600 | | -1 -1 | 3975* 4770* | | 1905 2286 | 19 28 | 10 0.4 14 0.6 | | | | 400 400 | |
| 117) 118) | | | | 3600 3600 | | -1 -1 | 795× 795× | | 385 385 | 18 29 | 21 0.4 21 0.4 | | | | | |
| 119) 120) 121) 122) 123) 124) 125) 126) | 1 1 | 68 68 68 68 68 68 68 68 | 2 | 7200 7200 7200 7200 7200 0 0 0 | -1 -1 -1 -1 -1 -1 | -1 -1 -1 -1 -1 -1 | 3991* 4802* 4802* 4802* 4802* 0 0 0 | 43610 43610 43610 | 4640 4640 4640 4640 | 1 A 2 A 2 A 3 A 3 A 4 A | 15 1.2 20 1.5 20 1.5 20 1.5 20 1.5 20 1.5 20 1.5 20 1.5 15 1.3 | -1 -1 -1 -1 -1 | 25 25 25 25 25 25 25 25 25 | 9 9 9 9 9 9 9 | 720 720 720 720 720 720 720 720 | 760 760 760 760 760 760 |
| 127) 128) | | 69 69 | | 1000 192 | | | 1034= 0= | 1345 0 | 139 0 | 18 28 | 10 0.4 15 0.4 | -1 -1 | | | 520 520 | |
| 129) 130) 131) 132) | . 1 1 - | 70 70 70 70 70 | 3 | 8400 8400 8400 8400 | -1 | -1 -1 | 9266* 11603* 3518* 3765* | 84892 13524 | 34280 42850 2039 1453 | 1 A 2 A 3 B 4 8 | 18 0.6 18 0.6 6 1.7 9 1.0 | 1 1 | 25 | 15 | | 760 900 |
| 133) 134) | 1 | 71 71 71 | 1 | 4800 | -1 | -1 -1 | 0* 0* | 0 | 0 | * 8 1 8 2 8 | 12 0.3 16 0.5 | -1 | 22 | 24 | 520 440 440 | 440 |
| 135) | 1 | | • 1 | 2000 | -1 | -1 -1 -1 | 2741± 2741≠ | 4 | - 496 496 | 2 D 1 B 2 8 | 13 0.6 15 0.6 | -1 | 21 | 21 | | 720 |
| 137) 138) 139) 140) 141) | 1 1 1 1 1 | 73 73 73 73 73 73 | 1 2 3 4 5 | 6048 6048 4632 6336 2304 | -1 -1 -1 -1 -1 | -1 -1 -1 -1 -1 | 63= 721= 156= 151= 165= | 0 16 14 1 218 | 41 545 102 218 37 | 1 C Z B 3 B 4 C 5 C | 10 0.5 10 0.2 10 0.2 10 0.2 10 0.2 | 90 70 70 60 -1 | 21 21 21 21 21 21 | 21 21 21 21 21 21 | 560 560 580 580 480 | 680 680 660 660 480 |
| 142) | 1 | 73 74 | | 2112 | | - L - 1 | 903+ | 1063 407 | 180 84 | 6 A 1 B | 15 0.3 8 0.4 | -1 | 21 | 21 | 560 | 560 |
| | | | | | | | | | | | | - | | | | |

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|--------------|----------------|----------|------------------|--------------|------------------------------|----------|-----------------------------|---------------|--------------------------|------------|-------|-----|-----------------|----------|----------|------------|------------|---|-----|
| SEQ) | CD UN Ty | | FAC ILI TY | HOUR | ARKUAL PRODUC. (TON/Y) | RATING | ED GAS NORMAL (NM3/N) | | ANNUAL NOX (NM3/Y) | 51 | A HEI | DIA | TEN | | | DX | | | |
| 144) | 1 | 74 | 2 | 4046 | -1 -1 | -1 | 491. | 407 | 84 | 26 | . 8 | 0.4 | -1 | | | 50Ó | 840 | | |
| 145) | 2 | | | 8760 | -1 | -1 -1 | 491* | 407 | 84 503 | 38 | | | | 21 | | 500 | | | |
| 147) | 2 | | | 3000 | -1 | -1 | 2194. | 5453 | 862 | 1 / | | | 270 | 45 30 | | 280 500 | | | |
| 148) | 2 | È- 5 | | 4224 | -1 | -1 | 1225+ | 2 | 214 | 10 | | 0.5 | | 42 | | 520 | | | |
| 149) | 5 | 5 | - 2 | 4224 | -1 | -1 | 1225+ | 2 | 214 | 28 | 10 | 0.5 | 1 | 42 | 18 | 850 | 720 | | |
| 150) 151) | 5 | 5 | | 4224 2112 | -1 -1 | -1 | 1225* | 2 | 214 71 | 3 H 4 B | | 0.5 | | 42 42 | | 880 880 | | | |
| 152> | 2 | 5 | 5 | 5775 | -1 | -1 | 31751 | 2 | 284 | 5 8 | | 0.5 | | 12 | | 800 | | | |
| 153) | 2 | 5 | 6 | 2640 | -1 | -1 | 1304 • | 3685 | 457 | 68 | 5 10 | Q.5 | -1 | 42 | 18 | 800 | 800 | | |
| 154) | 2 | | | 960 | - 1 | -1 | 3382* | ٥ | 116 | 1 4 | | 1-1 | | 43 | 24 | 640 | 620 | | |
| 155) | 2 | 7 | | 0 1600 | -1 -1 | -1 -1 | 0 413= | 0 540 | 0 87 | 1 E 2 9 | | 0.4 | | 34 34 | | 600 600 | | | |
| 157) | 2 | 8 | 1 | 2400 | -1 | -1 | 795+ | 1017 | 246 | 1 8 | 12 | 0.5 | -1 | 42 | 18 | 900 | 160 | | |
| 15B) | 2 | 9 | 1 | | -1 | -1 | 0 | ó | 0 | 18 | 18 | 0.5 | -1 | 44 | 18 | 520 | 120 | | |
| 159) 160) | 2 | 9 | | 2640 | -1 -1 | -1 | 1479* 2957* | 2077 | 503 1006 | 2 8 | | 0.5 | | 44 | | 520 | | | |
| 161) | ź | 9 | | 2640 | -1 | -1 | 4420# | 6231 | | 3 B 4 B | | 0.5 | | 44 44 | | 440 | | | |
| 162) | 2 | 10 | | 3600 | -1 | -1 | 906* | 1730 | 419 | 1 B | | 0.2 | | ~ < | | | | | |
| 163) | 2 | 10 | | 3600 | | -1 | 906* | 1730 | 419 | 2 8 | | 0.4 | | 36 36 | | 920 920 | 420 | | |
| 164) | 2 | 11 | 1 | 4200 | -1 | -1 | 2274+ | 10005 | 1283 | 1 4 | 25 | 8.0 | [:] -1 | 38 | 19 | 660 | | | |
| 165) | -,- | 11 | | 4200 | -1 | -1 | 2274= | 10005 | 1283 | 2 \$ | | 0.8 | | 38 | | | | | |
| 166) | | 12 | | 7854 | -1 | -1 | 7076* | 23 | 13089 | 18 | | 0,5 | | 35 | 25 | 80 | 20 | | |
| 167) | | 13 | | 2400 | -1 | -1 | 6240+ | 0 | 534 | 1 4 | | 0.6 | | 45 | 15 | | 920 | | |
| 168) 169) | | 14 | | 2080 | -1 | -1 | 165= | 222 | 33 | 18 | | 0.5 | | 42 | | 660 | | • | |
| 170) | | 16 | | 1500 1300 | -1 -1 | -1 -1 | 1908= 13= | 3184 | 366 | 18 | | 0.4 | | 29 | | 320 | | | |
| | | | | | | | - | | 1 | 1 8 | | | 175 | 30 | 24 | | 40 | | |
| 171) | | 17 | | 7200 | -1 -1 | -1 -1 | 398× 1336× | 4461 4412 | 391 602 - | 1 B 2 A | | 0.4 | | 41 41 | | 540 540 | | | |
| 173) | 2 | 17 | 3 | 4500 | ·~î | -1 | 408* | 1 | 116 | 3 B | | 9.9 | | 41 | | \$40 | | | |
| 174) | | 18 | | 960 | -1 | -1 | 304= | 47 | 221 | 18 | 5 | 9.9 | -1 | 49 | 18 | 460 | 320 | | |
| 175) | 2 | 19 | 1 | | -1 | -1 | 0 | 0 | 0 | 1 B | | | 250 | | | 460 | | | |
| 176) | | 19 | | 7680 | -1 | -1 | 1113+ | 9727 | | 28 | | | 250 | | | 460 | | | ÷., |
| 1773 | | 20 | | 570 | -1 | -1 | 700× | 205 | 59 | 1 4 | | 0.5 | -1 | | | 260 | 20 | | |
| 178) | . - - | | | 1080 | -1 | ~1 | 1540* | 0 | 60 | 1 A | | 0.9 | -1 | 55 | | 500 | | | |
| 179) | | 22 | | 720 | -1 | ~1 | 70* | 19 | - 40 | 1 0 | | 0.1 | | 45 | | 220 | | | |
| 180) 181) | 2 | 23 23 | | 7200 | -1 -1 | -1 -1 | 1461 1193* | 25200 2001 | 1516 246 | 1 A 2 B | | | 200 200 | | | 500 500 | | | |
| 182) | · 2 | 23 | 3 | | | -1 | ò | · • • • • | õ | 38 | | 0.8 | | 42 | | 300 | | | |
| 183) 184) | | 23 23 | | 1600 1600 | -1 -1 | -1 | 2894= 2894= | 1646 | 284 284 | 4 B 4 B | | 9.9 | | 42 42 | | 500 500 | | | |
| <i>e</i> | • • | | | | | | | | | | | | | | | | | | |
| 185) 186) | 2 | 24 24 | | 4348 4348 | | -1 | 14150+ 14150= | 1462 | 2579 | 18 | 5 | 9.9 | -1 | | | 280 280 | | | |
| 187) | 5 | 24 | ં 3 | 4368 | ~1 | -1 | 14150= | 1462 | 2579 | 1 8 | 5 | 9.9 | -1. | 43 | 18 | 280 | \$00 | | |
| 188) | 2 | 24 | 4 | 4368 | -1 | -1 | 337* | 509 | 96 | 2 C | 2 | 0.2 | -1 | 43 | 18 | 280 | 500 | | |
| 159) | 2 | 25 | 1 | 2400 | -1 | -1 | 3266* | 2 | 330 | 18 | 5 | 9.9 | 1 | 37 | 20 | 860 | 60 | | |
| . 190) | | 50 | | 7200 | | -1 | 795* | 3723 | 599 | 1 4 | | | -1 | | | .40 | 40 | | |
| 191) 192) | | 26 26 | | 810 7200 | -1 | -1 -1 | 227= | ŏ | 8 0 | 2 A 3 B | | 9.9 | -1 -1 | 34 34 | | 40 | 40 | | |
| 193) | 3 | | | 4864 | 23567 | -1 | 21000 | ٥ | 4092 | 1 4 | 21 | 00 | 40 | 17 | 22 | 880 | 920 | | |
| 194) | 3 | 1 | 2 | 4864 | 23567 | - 1 | 21000 | 0 | 4092 | 1 A | 21 | 9.9 | 40 | 17 | 22 | 880 | 920 | | |
| 195) 196) | 3 | 1 | 3 | 0 4864 | | | 0 10685* | 0 63867 | 6736 | 1 A 2 A | | | 40 -1 | 17 | | 880 880 | | | |
| 197) | 3 | | | | | | 6360= | 48025 | | | ÷ | ÷ . | 250 | 20 | | 140 | | | |
| 198) | 3 | S | 2 | 7200 | -1 | -1 -1 | 6360* | 48026 | 6159 | 1 A 1 A | 31 | 1.4 | 250 | 20 | | 140 | | | |
| 199) | 3 | | 1 | 8448 | -1 | -1 | 1797* | 15859 | 2034 | 18 | 20 | ò.5 | 180 | 18 | 22 | 500 | 480 | | |
| 200) | 3 | | | 8550 | -1 | -1 | 3975+ | 38729 | 4695 | 18 | 20 | 0.0 | 1 | 17 | 23 | 140 | 600 | | |
| 201) 202) | 3 | 5 | 1 2 | 8040 0 | | -1 | 41340* 0 | 275331 0 | 44519 0 | 1 4 | | | 250 | | | 380 380 | | | |
| 2031 | 3 | 5 | 3 | . o | -1 | -1 | . 0 | ٥ | 0 | 2 4 | 24 | 1.4 | 250 250 | . 14 | 22 | 380 | 420 | | |
| 2043 | 3 | <u></u> | | 8040 | -1 | -1 | 663= | 53 | 15 | 4 / | 25 | 1.4 | 240 | 14 | | 420 | 540 | | |
| 205) | 3 | \$ | | 2352 | | | 3246* | 7490 | 988 | 18 | | | 250 | 18 | | 20 | | | |
| 208) 207) | | | 3 | 2352 | | | 3525• 6029* | 8127 13890 | 1072 1832 | 28 | | | 250 250 | 18 18 | 17 17 | 20 20 | 360 360 | | |
| 208) | 3 | | | | | -1 | 4081= | 9599 | 1266 | 1 8 | | | -1 | 16 | | | | | |
| 209) | 3 | | 5 | 2400 | | | 2041+ | 4800 | | ž e | | | -1 | 16 | | | | | |
| 210) | 3 | | | 8448 | -1 | - 1 | 1161* | 14941 | 1389 | 16 | 5 15 | 0.6 | 180 | 18 | 22 | 640 | 820 | | |
| 211) | | | 1 | 7896 | -1 | -1 | 0• | 0 | 0 | . 1 E | 3 5 | 9.9 | -1 | 19 | 22 | 520 | 840 | | |
| | | | | | | | | | | | | | | | | | | | |

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| | | | | | LIST OF | FACILITY | CPATTER | H 2) | | | | | | | |
|-----|--|--|--|------------------------------|----------------------------|---|--|-------------------|--------------------------------------|--|----------------------|----------------------------|----------------------------|---------------------------------|--|
| | SEQ) | CD FAC FAC UN TOR ILL TY Y TY | HDUR | ANNUAL PRODUC. (TON/Y) | RATING | (ED GAS Normal (HM3/R) | SOX | NDX | SKA | | TEM | HX | MY | DX (H) | or |
| | | 3 9 3 | 7896 1440 | -1 -1 | -3 | 270* 270* 2633* | 1119 203 1597 | 271 49 | 2 B 3 A | 13 0.2 21 0.1 16 0.4 | 30 50 | 19 19 | 22 | 520 | 840 |
| | 214) 215) | | | -1 -1 | -1 | 62671 | 7921 | | 4 A 1 8 | 16 0.4 | | | | | |
| | 216) 217) | | 4800 | -1 -1 | -1 -1 | 604± 716= | 1528 1831 | | 1 B 2 B | 15 0.5 | -1 -1 | 21 21 | 23 23 | 20 20 | 700 |
| | | 3 12 1 3 12 2 | 2160 | -1 -1 | -1 -1 | 1820* 2300* | 0 1136 | | 1 B 2 A | 12 0.4 | | | | | |
| | 220) 221) | 3 13 2 | 6000 | -1 -1 | -1 -1 | 3021+ 3021+ | 13352 13352 | | 1 A 2 A | 15 0.5 15 0.5 | | | | | |
| | 222) 223) 224) 225) | 3 14 2 | 7920 7920 7920 7920 0 | | -1 -1 -1 -1 | 6204* 8204* 8204* 0 | 68154 68154 68154 0 | 8740 8740 | 1 A 2 A 3 A 1 A | 20 0.8 20 0.8 20 0.8 | 5 210 5 210 | 18 18 | 23 23 | 260 260 280 260 | 380 320 |
| | Z26) | 3 15 1 | | -1 | -1 | 989= | 212 | 61 | 1 B | 15 0.3 | 5 -1 | 14 | 22 | 780 | 600 |
| | | 3 16 2 3 16 3 | 4200 4200 2112 2112 | ~ 1 | -1 -1 | 3578* 3578* 4770* 5963* | 23037 23037 15455 19307 | 2020 | 1 B 2 B 3 B 4 B | 15 0.4 15 0.4 15 0.4 15 0.4 | 5 200 5 200 | 19 19 | 23 | 60 60 | |
| | | | 900 7200 | | | 3434* 3434* | 4705 37716 | | | 21 0.9 20 0.9 | | | | | |
| • . | 234) 235) | 3 18 2 | 3200 7200 3200 0 | -1 | -1 -1 | 986* 1002* 811* 0 | 1670 3866 1390 0 | 936 337 | 18 28 38 48 | 15 0.5 18 0.5 15 0.5 19 0.5 | 3 210 5 210 | 19 19 | 22 22 | 940 940 | 180 180 |
| | 237) 238) | 3 19 2 | | | | 105# 0* | 0 | | 1 A 1 A | 11 0.0 11 0.0 | | | | | |
| | 239) | | 7200 | | -1 | 461= | 3485 | 447 | 1 B | 21 0.9 | 5 150 | 21 | 55 | 320 | 560 |
| | 240) 241) | | | | | 105* | | | 1 B 1 B | 10 0.3 5 9.4 | | | | | |
| | 242) | 3 23 1 | 7200 | -1 | -1 | 1619= | 7587 | 1542 | 1 A | 12 0.4 | 5 -1 | 20 | 23 | 420 | 280 |
| | 2443 | 3 23 3 | 7200 7200 4800 | - 2 | -1 | | 7587 | 2542 | | 12 0.0 | 5 - 1 | 20 | - 23 | 420 | 280 |
| | 246) 247) | 3 23 5 3 23 6 | 4800 540 540 | -1 -1 | -1 -1 | 0= 5936= | 0 566 566 | 0 | 4 B | 14 0.4 5 9.9 5 9.9 | 5 -1 9 -1 | - 20 | 23 23 | 420 | 280 280 |
| | 249) 250) 251) 252) 253) | 3 24 2 3 24 3 | 2096 2096 2096 2096 2096 | -1 -1 -1 | -1 | 1002* 1678* 1678* 1678* 1678* | 3177 1 1 1 1 | 147 147 147 | 1 A 2 A 3 A 4 A 5 A | 7 0.4 11 0.7 11 0.4 11 1.5 11 0.7 | -1 -1 -1 | 19 19 | 22 22 22 | | 840 840 840 |
| | 254) 255) 256) | .3 25 2 | 960 960 2880 | -1 -1 -1 | | 159* 239* 1560* | 85 218 504 | | 18 28 33 | 18 0.5 18 1.0 15 0.8 | -1 | 20 | 23 | 560 | 560 |
| | 257) 258) | 3 26 1 3 26 2 | 6000 | -1 -1 | -1 -1 | 0 795× | 0 5003 | 0 642 | 18 28 | 25 0 8 25 0 8 | | | | | |
| | 259) 260) | 3 27 1 3 27 2 | 300 | | | 2496* 1272* | 420 349 | 148 52 | 1 Å 2 Å | ₹5 0.5 75 0.5 | | | | | |
| | 261) | 3 28 1 | 2400 | -1 | -1 | 954* | 2979 | 308 | 18 | 10 0.4 | | 14 | | 400 | |
| · | 262) 263) 264) 265) 265) 265) 267) 268) | 3 29 2 3 29 3 3 29 4 3 29 5 3 29 6 | 6336 6336 6336 6336 6336 6336 | -1 -1 -1 -1 -1 | -1 -1 -1 -1 -1 | 1497= 1497= 1497= 1497= 1697= 1697= 1697= | 2 2 2 2 2 2 2 2 2 2 | 397 | 48 59 68 | 16 0.5 18 0.7 18 0.7 18 0.7 18 0.7 18 0.7 | 40 45 45 45 | 19 19 19 19 19 | 22 22 22 22 22 | 860 860 860 860 | 240 240 240 240 240 240 |
| | 269) 270) | 3 29 8 3 29 9 | 6336 6336 6336 | -1 -1 | -1 -1 | 1497* | 3 | 397 0 | 78 88 98 | 18 0.7 18 0.7 18 0.7 | 45 -1 | 19 19 | 22 22 | 860 860 880 | 240 260 |
| · . | 271) 272) 273) 274) 275) | 3 29 11 | 6336 6336 | -1 -1 -1 | -1 -1 -1 | 0 = 0 = 0 = 0 = | 0 0 0 0 | 0 | 10 8 11 8 12 8 13 8 14 8 | 19 0.7 18 0.7 18 0.7 18 0.7 18 0.7 | -1 -1 -1 | 19 | 22 22 22 | 980 880 880 880 880 | 240 260 260 |
| | 276) 277) | 3 30 1 3 30 2 | | -1 -1 | -1 -1 | 954* Q | 1721 0 | 296 0 | 1 Å 2 Å | 24 1.0 15 1.0 | | | | 460 460 | |
| | 278) 279) | 3 31 1 3 31 2 | 560 560 | -i -1 | -1 -1 | 509= 509= | 325 325 | 38 38 | 1 B 2 B | 8 0.3 8 0.3 | -1 -1 | 14 14 | | 740 740 | |
| | 280) 281) | | 2700 | -1 -1 | -1 -1 | 636= 636= | 1953 1953 | 230 230 | 1 A 2 B | 18 0.8 12 1.1 | | | | | |
| | 282) 283) 284) | 3 33 2 | 8400 12 490 | -1 -1 -1 | -1 -1 -1 | 604 × 23 × 325 × | 4202 15 | 708 38 16 | 18 28 38 | 15 0.5 6 0.6 13 0.5 | -1 | - 18 | 18 | 880 | 660 |
| | | | 410 | -1 | - 1 | 22.74 | • | 10 | | | -1 | 10 | 10 | 490 | |

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| J. | L15T | OF | FACILITY | (PATTERN | 2) |
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| | SEQ) | CO FAC FAC UN TOR 1L TY Y TY | C OPE. HOUR (N) | ANNUAL PRODUC. (TON/Y) | RATING (NH3/H) | IED GAS NORHAL (NM37H) | ANNUAL SOX (RH3/Y) | ANNUAL NDX : (NM3/Y) | SHA NO PE | HE I | DIA | ACK DA Tem (*c) | та Их | ЯΥ | DX (N) | DY |
|---|----------------------|------------------------------------|----------------------------------|------------------------------|-------------------|------------------------------|--------------------------|----------------------------|-------------------|-------------|-------------------|-----------------------|----------------|----------------|-------------------|-------------------|
| | 287) 288) | | 3 3440 4 3440 | | -1 -1 | 3821= 5751= | 3082 4613 | 354 531 | 28 28 | | | ~1 -1 | | | 420 420 | |
| | 289) 290) | | 1 0 2 5400 | -1 -1 | -1 -1 | 0 8580= | 0 3149 | 0 1603 | 1 A 2 A | | | | 20 20 | | 320 320 | |
| | 291) | 3 36 | 3900 | 1 | -1 | 2226* | 11059 | 1232 | 1 B | 15 | 0.7 | 175 | 14 | 22 | 780 | 880 |
| | 292) | 3 37 | - | -1 | 1 | 1749= | 4786 | 614 | 1 B | 25 | 0.8 | -1 | 20 | 22 | 500 | 680 |
| | 293) 294) 295) | 3 38 2 | 1 2400 2 .0 5 .0 | -1 -1 -1 | -1 -1 -1 | 1204 • 0 0 | 531 0 0 | 261 0 0 | 1 B 2 B 3 B | 12 | 0.3 0.3 0.3 | -1 -1 -1 | 19 | 22 | 860 860 860 | 40 |
| | 296) 297) | | 1 2080 2 2080 | -1 -1 | -1 -1 | 302. 509. | 567 945 | 85 142 | 1 B 2 B | | 0.5 0.5 | | | | 620 620 | |
| | 298) | 3 40 5 | | -i | -1 | 890+ | 2401 | 308 | 1 A | 15 | D.6 | -1 | 21 | 22 | 140 | 600 |
| | 299) | | 1140 | -1 | -1 | 125* | 16 | 6 | 1 A | 10 | 0.3 | -1 | 14 | 22 | 80 | 660 |
| | 300) 301) | | 1 6500 2 6500 | -1 | -1 -1 | 636× 636× | 4727 4727 | 573 573 | 1 B 2 B | | 0.3 0.3 | | | | 300 300 | |
| | 302) | | 2655 | -1 | -1 | 1113* | 2450 | 396 | 1 A. | 8 | 0.3 | -1 | 20 | 22 | 220 | 820 |
| | 303) 304) | | 936 2 3520 | -1 -1 | -1 -1 | 1590* 1988* | 1238 5795 | 200 937 | 1 B 2 B | | 0.5 | -1 -1 | 19 19 | | 540 540 | |
| | 305) 306) | | 3168 0 | -1 -1 | -1 -1 | 811* 0 | 2134 | 345 0 | 1 B 2 B | 14 14 | 0.5 | -1 -1 | 19 19 | | 840 840 | |
| • | 307) 308) | | 1860 | -1 | -1 -1 | 1034= 1034= | 2001 2001 | 257 257 | 1 B 2 B | 15 | 0.5 | 150 150 | 17 | | 180 180 | |
| | 309) 310) | 3 46 1 | 930 | -i -1 | -1 -1 | 953× 953× | 0 | 42 | -3:8 4 8 | 15 | 0.5 | 100 | 17 | 18 | 180 180 180 | 680 |
| | 311) 312) | 3 46 5 | 930 930 | -1 -1 | -1 -1 | 953* 953* | 0 | 42 | 58 68 | 15 | 0.3 | 100 | | 18 | 180 180 | 680 |
| | 313) 314) | | 1 8640 2 8640 | -1 -1 | -1 -1 | 6519× | 64396 64396 | 7506 7806 | 1 A 2 A | 25 | 0.7 | 225 | | | 800 800 | |
| | 315) 316) | 3 47 3 3 47 4 | 5 O | -1 -1 | -1 -1 | 0 | 0 | 0 | 3849 | 12 | 0.7 | 225 | 15 | 22 | 800 800 800 | 480 |
| | 317) 318) 319) | 3 48 1 | 2400 | -1 -1 -1 | -1 -1 -1 | 1855* 0 0 | 3488 0 0 | 570 0 0 | 18 28 38 | 10 | 0.4 | -1 -1 -1 | 18 | 17 17 17 | | 940 940 940 |
| | 320) 321) | | 3960 3960 | -1 -1 | -1 -1 | 3339= 3339= | 7054 | 1709 | | 12 | 0.6 | 180 | 19 | 24 | 480 480 | 40 |
| | 322) 323) 324) | 3 50 | - 1 2400 2 2400 3 0 | -1 | -2 -1 -1 | 477* 477* 0 | 1201 1201 0 | | 1828 | 10 | 1.3 | -1 -1 | 16 | 19 | 200 200 | 840 |
| | 325) | 3 51 | 1 5760 | 30000 | -1 | 21294* | 9705 | . 0 5209 | 38 1 A | | - | - T- | 16 15 | | 200 300 | |
| | 326) 327) 328) | 3 51 | 2 \$740 3 4800 4 3600 - | -1 | -1 -1 -1 | 21294* 10852* 10852* | 9705 35914 26936 | 5209 6151 4613 | 1 A 2 S 3 B | 28 | 1.0 | 300 | 15 15 15 | 21 | 300 260 260 | 480 |
| | 329) 330) | | 1 0 2 7200 | | -1 -1 | 0 4086* | 0 15684 | 0 3799 | 18 25 | | | 155 215 | 16 16 | | 360 360 | |
| | 3312 | 3 53 | - | | -1 | 75+ | 28 | 11 | 18 | 10 | 0.2 | 150 | 19 | 23 | 560 | 140 |
| | 332) 333) | 3 54 | 1 2880 2 2880 | -1 | -1 -1 | 4770= 4770= | 20956 20956 | 1838 1838 | 18 25 | 18 | 0.9 | 175 | 15 | | 40 | 40 40 |
| | 334) 335) | 3 54 3 | 3 2880 4 4320 | -1 | -1 -1 | 4770= 4770= | 20956 20956 | 1838 1838 | 38 48 | 18 | 0.9 | 200 . | 15 15 | 52 | 40 | 40 40 |
| | 336) | 3 55 | 1 0 | -1 | -1 | ° 0 | Q | o | 1 Å | 10 | 0.5 | -1 | 20 | 55 | 720 | 60 |
| | 337) | 2 29 | 1 4200 | -1 | -1 | 1224# | 4709 | 707 | 1 A | 50 | 0.3 | -1 | 15 | 20 | 140 | 680 |
| | 338) 339) | 3 57 . | 1 4480 | -1 | -1 -1 | 461+ 0 | 1596 | 386 0 | 18 26 | 6 | 0.0 | -1 -1 | 19 | | 560 560 | |
| | 340) 341) | ******* | 3 480 - 1 0 | | -1 -1 | 13125× 0 | 5670 | 1802 0 | 38 14 | | | -1 -1 | | 53 | 560 500 | 740 |
| | 342) | | 1 0 | - | -1 | 0 | 0 | 0 | 18 | 10 | 0.5 | 230 | 14 | 22 | 420 | |
| | 343) 344) | 3 59 | 2 8448 3 8448 | -1 | -1 -1 | 3975= 795+ | 35219 7037 | 4516 880 | 2 9 3 8 | 10 10 | 0.7 | 170 | 14 14 | 22 | 420 420 | 500 |
| | 345) 346) | ··· | 6 8648 | | -1 | 795. | 7037 | 880 | 48 | 10 | 0.6 | 270 | 14 | 22 | 420 | 500 |
| | 348) | 3 60 | - ` | - | -1 -1 | 429* 1092* | 1045 294 | 157 95 | 1,8 1 A | | | -1 -1 | | | 240 | |
| | 348) | 3 62 | 1 4500 | -1 | -1 | 243= | 20 | 106 | 18 | | | -1 -1 : | | | 00 660 | |
| | 349) 350) | 3 62 3 62 | 2 4500 3 4500 - | -1 -1 | -1 -1 | 243= 243• | 20 | 105 105 | 18 18 | 5 | 9.9 9.9 | -1 | 15 | 20 | 660 | 120 |
| | 352) | 3 63 | - | -1 | -1 -1 | 182- | 21 0 | 71 0 | 18 | 5 | 0.5 9.9 | 100 A. | | | 140 140 | |
| | 353) 354) 355) | 3 64 3 | 1 2750 2 2750 3 2750 | -1 | -1 | 286= 286= 284= | 414 | 105 105 | 18 29 | 12 | 0.3 | -1 | 20 20 | 21 | 980 980 | 720 |
| | | | 3 2750 - L 2400 | | -1 -1 | 286* 557* | 1354 | 105 180 | 38 18 | | 0.3 | | 20 | 21 | 980 | 720 |
| | | | | • | - | | | 100 | | ** | ··· | -1 | ** | ~~ | 600 | 700 |

| | SEQ) | UN | TOR | ILI | HOUR | PRODUC. | EN177 RATING (NM3/H) | ED GAS NORHAL (NM3/H) | ANNUAL SOX (NH37Y) | ROX | SHA NO PE | HEI | DIA | тен | HX | нт | ФX | DY (M) |
|-------|----------------------|----------|----------------|--------|----------------------|----------------|----------------------------|-----------------------------|---------------------------|----------------------|----------------|------|------------|------------|----------------|----|------------|-------------------|
| | 357) | | 66 | | 4080 | -1 | -1 | 5100* | o | 107 | 1.8 | 18 | 0.5 | -1 | 19 | 53 | 120 | 160 |
| | 358) 359) | | 67 67 | 1 2 | 2440 | | -1 -1 | 1367+ 0 | 3502 0 | 468 | 18 26 | | 1.2 | | 14 14 | | | 300 300 |
| | 360) 361) | 3 | 67 | 3 | 0 90 | -1 -1 | -1 | ů 0* | ő | 0 | 38 48 | 20 | 0.8 | 1 | 14 | 25 | 940 | 300 300 |
| | 362) | 3 | 68 | | 7200 | -1 | -1 | 604 = | 4882 | \$76 | 1 # | 14 | 0.5 | -1 | 14 | 19 | 740 | 260 |
| | 363) | | 68 | | 7200 | -1 | -1 | 404* | 4882 | \$76 | 2 B | | | -1 | | | | 260 |
| | 364) 365) | | 69 | | 7200 7200 | -1 -1 | -1 -1 | 1590 1590 | 12007 12007 | 1540 | 1 B 1 B | | 0.9 | | 17 | | | |
| | 366) 367) | | 70 70 | | 4800 2400 | -1 -1 | -1 -1 | 1320+ 1320+ | 5813 2907 | 873 436 | 1 A 2 A | | 0.5 | -1 -1 | 14 14 | | | 520 520 |
| | 368) 369) | | 71 71 | | 4200 4200 | -1 -1 | -1 -1 | 3307= 3307= | 14575 14575 | 1869 1869 | 1 B 2 B | | 0.6 | | 13 13 | | | 60 60 |
| | 370) | | | | 4800 | -1 | -1 | 223+ | 1134 | 145 | 1 A | | 0.8 | | 18 | | | 160 |
| | 371) | | 73 | 1 | 7200 | -1 | -1 | 4680= | 3780 | 1334 | 1 A | | 1.0 | | | | | 540 |
| | 372) 373) | | 73 | | 7200 | -1 -1 | -1 -1 | 7800. 1169. | 6300 2318 | 2223 383 | 2 A 1 B | | 0.8 | | 18 | | | 540 880 |
| | 374) | 3 | 74 | 2 | 2508 | -1 | -1 | 1169. | 2318 | 383 | 28 | 23 | 0.4 | -1 | 15 | | | |
| | 375) 376) 377) | 3 | 75 75 75 | 2 | 2400 2400 2400 | -1 -1 -1 | -1 -1 | 18550* 18550* 18556* | 15805 - 15805 15805 | 2844 2844 2844 | 1 B 3 B | 5 | 9.9 | 40 | | 23 | 500 | 840 840 840 |
| · · · | 378) | 3 | 75 | | 2400 | -1 | -1 | 18550= | 15805 | 2844 | 1 B 1 B | | 9.9 | | 16 | | | 840 |
| | 379) 380) | | 76 | 1 2 | 1095 0 | -1 -1 | -1 -1 | 541* 0 | 314 | 76 0 | 1 A 2 B | | 0.5 0.5 | | 13 13 | | | 640 640 |
| | 381) | | 77 | | 8448 | -1 | -1 | 207+ | 1584 | 538 | 18 | 9 | 0.5 | -1 | 14 | 50 | 60 | 160 |
| | 3B2) 383) | 3 | 78 78 | ì | 6000 3000 | | +1 -1 | 557 477 • | 3052 1308 | 458 196 | 1 A 2 A | | 0.3 | | 14 14 | | | 80 80 |
| | 384) | 3 | 79 | 1 | 5400 | -1 | -1 | 2115+ | 9483 | 1533 | 1 B | 18 | 0.6 | -1 | 15 | 20 | 60 | 580 |
| | 385) | <u> </u> | 79 | 2 | 0 7200 | -1 -1 | -1 -1 | 0 100= | 0 0 | 0 28 | 2 B 1 B | | 0.5 | | 15 16 | | | 580 |
| | 387) | | | | 4800 | -1 | -1 | 75* | 66 | 33 | 18 | | 0.2 | -1 | 16 | | | 840 |
| | 388) | | 82 | | 3600 | -1 | -1 | 3180. | 10464 | 1571 | 1 B | 15 | 0.5 | | | 23 | 480 | 140 |
| | 389) | | 82 | | 3600 | -1 | -1 | 2385* | 7848 | 1178 | 2 B | | 0.5 | | | | | 140 |
| | 390) | | 83 84 | | 3000 2700 | | -1 | 763* 700* | 2603 | 307 262 | 1 B 1 8 | | | | 14 15 | | | 800 440 |
| | 392) | 3 | 85 | t | 2700 | -1 | - 1 | 429* | 610 | 148 | 1 A | -15 | 0.5 | -1 | 14 | 22 | 320 | 700 |
| | 393) | - | 85 | 2 | | -1 | -1 | 0 | • 948 | 0 | 2 . | | 0.5 | | 14 | | | 700 |
| | 394) 395) | | 84 | | 1800 7680 | -1 | -1 -1 | 636× 620× | 5753 | 153 641 | 1 A | | 0.8 | | 20 14 | | | 620 |
| | 396) | 3 | 87 | 2 | 7680 | -1 | -1 | 716# | 6706 | 747 | 2 A | 12 | 0.6 | 90 | 14 | 22 | 480 | 620 |
| | 397) 398) | | 89 90 | | 3000 | | -1 | 223= 3021= | 596 8018 | 89 972 | 1 A 1 8 | | 0-4 | 1 | 13 14 | | | |
| | 3993 | | 91 | | 2320 | _ | -1 | 7954 | 678 | | 18 | | | | 19 | | | 720 |
| | 4003 | | 93 | ī | | | -1 | 74 • | 8 | 2 | 1 A | 2 | 0.2 | -1 | 15 | 20 | 320 | 440 |
| | 401) 402) | | 94 94 | | | | -1 -1 | 4638= 4638= | 790 790 | 143 143 | 1 C 2 C | | | | 16 16 | | | |
| | 403) | 3 | 93 | | 7200 | -1 | -1 | 473= | 2001 | 279 | 18 | | | | 15 | | | |
| | 404) 405) | | 95 96 | • | 7200 | | -1 | 2449× 5157× | 4002 314 | | 28 18 | | | | 15 16 | | | |
| | 406) 407) | 3 | 96 96 | ź | 270 | -1 | ~1 | 5157= 9646+ | 314 | 85 | 18 | 5 | 9.9 | -1 | 16 16 | 19 | 480 | 960 |
| | 408) | 3 | 97 | 1 | 3590 | -1 | -1 | 67* 67* | 367 | 47 | 18 | 5 | 9.9 | 45 | 17 | 27 | 500 | 240 |
| | 409) 410) 411) | 3 | 97 97 97 | 3 | 3590 3590 3590 | -1 | | 67× 67× | 367 | 47 | 18 18 18 | \$ | 9.9 | | 17 17 17 | 27 | 600 | 240 |
| | 412) | 3 | 98 | 1 | 8400 | -1 | ~1 | 5 50193* | 0 | 310364 | 1 A | 76 | 3.4 | 140 | 17 | 19 | 840 | 740 |
| | 413) 414) | 3 | 98 | 3 | 8400 | -1 | -1 | 550193* 1021788* | . 0 | 310364 | 2 A 3 A | 84 | .5.0 | 135 | | 19 | 880 | 786 |
| | 415) 416) | | 98 98 | 5 | 8400 8400 | -1 -1 | | 1021788* 828564* | | 574391 1050318 | 4 A 5 A | 110 | 5.0 | 135 150 | 17 | 19 | 920 | |
| | 417) 418) | - 3 | 99 97 | 1 | 4800 4800 | | | 795= 795= | 4857 | 542 | 18 28 | - 30 | 0.5 | -1 | 19 19 | 15 | 940 | 600 |
| | 419) | 3 | 99 | 3 | 4800 | -1 | -1 | 795* | | | 38 | | | | 19 | | | |
| | 420) 421) | | 100 | | 1098 1098 | | | 1590 <i>*</i> 0* | | | 1 A 2 B | | | | 16 16 | | | |
| | 422) | 3 | 101 | 1 | 7920 | -1 | -1 | 795. | 5104 | 839 | 18 | 10 | 0.4 | -1 | 16 | 18 | 900 | 960 |

.

| | | | | | · . | | | | | | | | | | | | |
|--------------|-----|------------|------|--------------|-------|---------|-----------------|--------------|--------------|----------------|----------|-----|----------|----------|----------|------------|-----|
| SEQ | 60 | 640 | \$40 | 195 | | | ED GAS | ARRUAL | ANNUAL | | | 57 | ACK I | DATA- | · | | |
| | | | | | | RATING | NORMAL | SOX | NOX | SHA | | | | | | | |
| | | Ŷ | ŤŸ | | | (NH37H) | (14374) | | (NH3/Y) | | | | | | | (N) | (8) |
| | | • | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | |
| 423) | | 102 | | | -1 | | 4977. | 4068 | 480 | 18 | | 0.5 | -1 | 17 | | 340 | |
| 424) | | 102 | | 720 | -1 | | 760. | - 63 | 22 | 2 A | | 0.5 | | 17 | | 340 | |
| 425) | 3 | 102 | - 3 | 720 | ~1 | -1 | 289. | 163 | - 19 | 38 | . 12 | 0.2 | -1 | 17 | 17 | 340 | 940 |
| 426) | | 101 | | 1400 | -1 | ~1 | 223+ | 177 | 43 | 18 | | | -1 | | | 500 | |
| \$207 | | | | 1400 | 1 | | 41.34 | 111 | 43 | 10 | 13 | 0.3 | -1 | 16 | 17 | 200 | 040 |
| 427) | 3 | 104 | | 1200 | -1 | -1 | 50+ | 6 | 2 | 1 A | 12 | 1.0 | : | 17 | 1.0 | 180 | 290 |
| 428) | | 104 | | 7200 | -1 | | 22+ | š | 3 | 2 Å | | 1.0 | | 17 | | 180 | |
| 429) | | 104 | | 7200 | -1 | -1 | 22+ | 8 | 3 | 3 Å | | 1.0 | | 17 | | 180 | |
| | | | | | - | - | | | | 2 11 | | ••• | • | • • | | 100 | 100 |
| 430) | 3 | 105 | . 1 | 8760 | -1 | -1 | 46384* | 123778 | 172563 | 1 A | 50 | 3.4 | 300 | 18 | 18 | . 60 | 880 |
| 431) | 3 | 105 | - 2 | 8760 | -1 | -1 | 92741= | 247556 | 345125 | 2 A | | | 300 | | | 140 | |
| | - | | | | | | | | | | | | | | | | |
| 432) | 3 | 106 | 1 | 2400 | -1 | -1 | 32* | 55 | . 9 | 1 8 | 15 | 0.4 | -1 | 17 | 18 | 550 | 340 |
| | | | | | | | | | | | | | | | | | |
| 433) | | 107 | | 1055 | -1 | -1 | 970+ | 930 | 140 | 1 B | 10 | 0.5 | -1 | 17 | 18 | 340 | 740 |
| | | | | | | | 1 | | | | | | | | | | |
| 434) | | 108 | | 2920 | -1 | -1 | 135= | 182 | 34 | 18 | 8 | 0.3 | -1 | 16 | 18 | 700 | 380 |
| | | | | * | | · . | | | | | | | | | | | |
| 435) 436) | | 109 | | 3600 | -1 | -1 | 2655+ | 14626 | 1283 | 1 B | | 0.5 | | 16 | | 360 | |
| 4301 | 2 | 109 | | 3600 | -1 | -1 | 1986⊧ | 10970 | 962 | 2 B | 15 | 0.4 | -1 | 16 | 20 | 360 | 120 |
| 437) | - | 110 | 1 | :0 | -1 | 1 | 0 | 0 | 0 | 1 B | <u> </u> | | | | | ~ · | |
| 438) | | 110 | | 1440 | -1 | | 1193+ | | 231 | 2 A | | 0.5 | -1 | 16 | | 900 | |
| 439) | | 110 | | 6744 | -1 | -1 | 2430. | 29505 | 2740 | 3 Å | | 1.0 | | 16 16 | | 900 | |
| | - | | | • | - | - | 21300 | 21505 | 2140 | | | 1.0 | -1 | 10 | | 700 | 200 |
| 440) | 3 | 111 | 1 | 7200 | 66800 | -1 | 40133* | . 0 | 11947 | 1 A | 30 | 1.5 | -1 | 17 | 23 | 480 | 20 |
| 441) | 3 | 111 | . 2 | 1296 | 6200 | -1 | 20093. | ŏ | 1077 | 1 . | | 1.5 | | 17 | | 480 | žõ |
| 442> | 3 | 111 | 3 | 6000 | -1 | -1 | 13133+ | 92368 | 10052 | 2 A | | 1.2 | | 17 | | 440 | 60 |
| 443) | 3 | 111 | . 4 | 7200 | -1 | -1 | 1813* | 21707 | 2171 | 3 A | 50 | 0.6 | -1 | 17 | | 360 | |
| 444) | 3 | 111 | 5 | 7200 | 1 | -1 | 2538+ | 21707 | 2171 | 4 A | 30 | 0.9 | -1 | 17 | Z2 | 420 | 900 |
| | • | | | | | | | | | | | | : | | · . | | |
| 445) | | 112 | | 256B | -1 | -1 | 5279= | 5491 | | 1 B | | 0.5 | -1 | 17 | 18 | 200 | 40 |
| 446) | | 112 | | 7200 | -1 | -1 | 0* | 0 | 0 | . 2 8 | 5 | 9.9 | -1- | 17 | 18 | 240 | 40 |
| | | | | | | | | | | | · | | | | | | |
| 447) 448) | | 113 | | 2120 | -1 | -1 | 3238* | 4927 | 930 | . 1 B | | 0.8 | | - 21 | | 100 | |
| 449) | | 113 | | 2120 | -1 | -1 | 3035* 809* | 4636 | 875 | 2 B 3 B | | 0.8 | | 21 | | 100 | |
| 450) | | 113 | | 2120 | -1 | -1 | 809* | 1235 | 233 233 | - 3 B - 4 B | | 0.6 | | 21 | | 100 | |
| 451) | | 113 | | 2120 | -1 | | 1214* | 1235 | 348 | S B | | 0.6 | -1 | 21 | | 100 | |
| | | 113 | | 2120 | -1 | | 809+ | 1221 | 230 | 6 B | | 0.6 | -1 | 21 21 | 21 21 | - 60 | 560 |
| 453) | | 113 | | 2120 | -1 | | 1336= | 1846 | 277 | 7 8 | | 0.4 | -1 | 51 | | 100 | |
| 454) | | 113 | | 2120 | -1 | -î | 870+ | 1235 | 185 | 8 8 | | 0.4 | -1 | 21 | | 100 | |
| 455) | | 113 | | 2120 | -1 | | 890* | 1235 | 185 | 9 B | | 0.4 | -1 | 21 | 21 | | 600 |
| | - | | | | | | | | | | | | | | | | |
| 456) | | 114 | | 1896 | -1 | -1 | 384 e | 600 | 97 | 1 8 | 11 | 0.2 | +1 | 19 | 23 | 500 | 260 |
| 457) | | 114 | | 1896 | -1 | -1 | 384 * | 600 | 97 | 2 B | | 0.2 | -1 | 19 | | 500 | |
| 458) | | 114 | | 1896 | -1 | -1 | 207* | 400 | 51 | 3 B | - 11 | 0.4 | -1 | 19. | 23 | 300 | 260 |
| 459) | 3 | 114 | 4 | 1896 | -1 | -1 | 499= | 0 | 40 | 48 | 5 | 9.9 | -1 | 19 | 23 | 500 | 260 |
| 440) | 3 | 114 | 5 | 1896 | -1 | -1 | 499: | 0 | 40 | 48 | | 9.9 | -1 | 19 | 23 | 500 | 260 |
| | - | | | | - | • | | • | | | | | - | | | | |
| 4613 | - 3 | 115 | 1 | 4160 | -1 | -1 | 272= | 1 | . 99 | 18 | 5 | 0.3 | -1 | 20 | 21 | 960 | 440 |
| 462) | | 115 | | 4160 | -1 | | 635× | 1 | 107 | 2 B | | 0.6 | | 20 | | 960 | |
| 463) | | 115 | | 4160 | -1 | | 635* | 1 | 107 | 38 | | 0.6 | 80 | 20 | | 960 | |
| 484) | 3 | 5 115 | 4 | 4160 | -1 | -1 | 635= | 1 | 107 | 4 B | 15 | 0.6 | 80 | 20 | 21 | 960 | 440 |
| | | | | | | | | | | | | | | | | | |
| 465) | | 117 | | 7920 | | | 6364* | 0 | 2084 | 1 4 | | 1.5 | -1 | 19 | | 440 | |
| 466) | | 117 | | 3960 | | | 8348* | 32398 | 5058 | 28 | | 0.8 | -1 | 19 | | 300 | |
| 467) | 3 | 5 117 | . 3 | 1500 | -1 | -1 | 9275* | 13435 | 2129 | 38 | 20 | 0.6 | -1 | 19 | 21 | 360 | 740 |
| 1200 | | | | | 76740 | | 3768. | - | (17- | | - | | | | | | |
| 468) 469) | | 118 118 | | 6480 1080 | | | 22886* 4638* | 0 | 6132 | 1 A | | 1.0 | -1 | 16 | | 160 | 60 |
| 4703 | | 118 | | 1080 | | | 4038* | 8648 8648 | 1245 1245 | 28 28 | | 0.6 | -1 -1 | 16 16 | | 180 180 | |
| | | , 110 | | 1000 | -1 | -1 | -010+ | 0040 | 1543 | . 4 8 | د.» | 0+0 | -1 | 10 | 24 | 190 | 140 |
| | | | | | | | | | | | | | | | | | |

2.3.2 Calculation of SO₂ emission volume

The emission volume of SO_2 from each factory was calculated by the equation (2-2) shown below. The sulphur content of the heavy fuel oil and kerosene, if not specified by retrieved questionnaire, was thought equal to that of sample fuels in use in Thailand analyzed which is shown in Table 2-10. Likewise, the sulphur content of other fuel as well as its specific gravity was thought similar to the Japanese average shown in Table 2-8.

| Solid fuel $Qs = A$ | Annual fuel consump. \times S | Surphur content $	imes$ 0.007 |) |
|-----------------------|---------------------------------|---|-------|
| (Nm ³ /yr) | (kg/yr) | (%) | |
| Liquid fuel $Qs = A$ | Annual fuel consump. \times S | .G. \times Surphur content \times 0.007 | (2-2) |
| (Nm³/yr) | (liter/yr) | (%) | |
| | | | |

Gaseous fuel Qs = Annual fuel consump. × Surphur content × 0.01 (Nm^3/yr) (Nm^3/yr)

 Table 2-10 Surphur content of heavy fuel oil and diesel oil in use in Thailand

| Fuel type | Surphur content (%) |
|------------------------------|---|
| Heavy fuel oil No. 1, 2 *(A) | 1.98 (value of No.1 class) |
| Heavy fuel oil No. 3, 4 *(B) | 2.58 (value of No.4 class) |
| Heavy fuel oil No. 5, 6 *(C) | 2.46 (Mean of No.5 (3.04%) and No.6 (1.88%)) |
| Diesel oil | 0.56 (mean of Shell (0.65%) and ESSO (0.46%)) |

Note : The *(A) to (C) is the symbol used in questionnaire.

The yearly SO₂ emission volume by each factory and by each facility was shown in Table 2-9, and that by county was shown in Table 2-11, which indicates characteristically that the emission volume of SO₂ from Phra Pradaeng area have much volume. The source distribution figure of SO₂ emission volume from stationary sources with the recovered questionnaire is shown in Fig. 2-1. And that by facility type in Table 2-12 indicates that the emission volume from boiler being significant. That by business category in Table 2-13 indicates that textile industry comes first and next is South Bangkok Thermal Plant. SO₂ emission volume by stack height in Table 2-14 indicates that the emission volume from the stacks in the range of the height from 10 to 40 m and those over 110 m being significant. When the top 20 largest of them are reviewed in Table 2-15, they mostly center around Phra Pradaeng area that has many factories.

| Name of county | Number of factories | Number of facilities | SO ₂ entission volume (ton/year) | NO _x emission volume (ton/year) |
|-----------------|---------------------|----------------------|---|--|
| 1 Muang | 63 | 145 | 3992.28 | 523.84 |
| 2 Bang Pice | 28 | 47 | 314.66 | 76.94 |
| 3 Phra Pradaeng | 117 | 278 | 9341.63 | 7507.25 |
| TOTAL | 208 | 470 | 13648.57 | 8108.03 |

Table 2-11 Emission volume by county

Table 2-12 Emission volume by facility type

.

| | | | ····· | |
|----------|--------------------------------|-------------|------------|---------------|
| [| | Number | SO₂ | NOx |
| Code | Name of facility type | of | emission | emission |
|) | · · · · · | faci- | voluze | volume |
| | | lities | (ton/year) | (ton/year) |
| 101 | Boiler (for electric power) | 5 | 2624.40 | 5798.93 |
| 103 | // (other) | 267 | 7787.58 | 730.20 |
| 502 | Metal fusion f. (alumi/smelt.) | 6 | 109.36 | 15.49 |
| 503 | " (other/smelt.) | Ž | 0.74 | 0.14 |
| 601 | Metal rolling f. (steel/cont.) | 16 | 836.78 | 77.80 |
| 602 | " " (steel/batch) | 4 | 144.77 | 16.33 |
| 603 | " " (alumi/cont.) | 2 | 0.03 | 1.88 |
| 607 | Metal heat tre.f.(steel/cont.) | | 39.66 | 5.38 |
| 608 | " " (steel/hatch) | 5 3 3 | 6.92 | 0.87 |
| 611 | " " (other/cont.) | : 3 | 65.03 | 9.50 |
| 612 | " " (other/batch) | 5 | 0.00 | 0.00 |
| 613 | Metal forging f. (steel/cont.) | 1 | 5.72 | 0.57 |
| 702 | Oil heating furnace (updraft) | 2 | 40.21 | 3.61 |
| 703 | " " (other) | 6 | 22.09 | 3.66 |
| 915 | Glass melting furnace (tank) | 5 | 1497.61 | 1248.38 |
| 918 | Other melting furnace | 2 | 0.04 | 0.01 |
| 1001 | Reaction furnace (chemicals) | . 1 | 0.00 | 0.00 |
| 1004 | Direct heating furnace (food) | 8 | 4.38 | 1.04 |
| 1105 | Detergent drying furnace | 1 | 4.56 | 1.06 |
| 1106 | Other drying furnace | 67 | 270.38 | 65.39 |
| 1201 | Electric furnace (arc furnace) | 8 | 55.45 | 90.62 |
| 1202 | " " (three-phase) | 1 | 0.00 | 12.59 |
| 1205 | // // (three-phase) | 1 | 0.00 | 4.28 |
| 1209 | " " (low frequ.) | 1 | 0.00 | 3.07 |
| 1302 | Waste inciner. (domest./batch) | . 2 | 0.01 | 0.03 |
| 1303 | " " (indust./cont.) | - 1 | 0.00 | 0.00 |
| 1304 | " " (indust./batch) | 3 2 1 | 0.99 | 0.11 |
| 1416 | Fusion furnace (crucible/lead) | 2 | 0.00 | 0.01 |
| 1419 | " " (crucible/zinc) | | 11.43 | 1.13 |
| 1421 | " " (other/zinc) | 3 | 3.24 | 0.40 |
| 1423 | Drying furnace (for lead) | 3 | 0.01 | 1.97 |
| 1802 | Activated carbon manu, reactor | | 0.15 | 0.03 |
| 2501 | Fusion f. (lead stor. battery) | 10 | 1.88 | 2.39 |
| 2603 | Reactor (lead pigment) | 1 | 0.00 | |
| | Diesel generator | - 3 - 18 | 0.23 | 0.61 10.52 |
| 8 | Other | 18 | 114.92 | 10.02 |
| | TOTAL | 470 | 13648.57 | 8108.03 |

Table 2-13 Emission volume by business category

| NOx emission volume (ton/year) | 20.83 20.83 20.85 20.93 20 | 8108.03 |
|--|--|----------|
| S O _z emission volume (ton/year) | 267.36 58.93 58.93 58.93 58.93 58.93 59.94 55.93 50.73 50.73 55.75 55.73 55.75 | 13648.57 |
| Number of faci- lities | -oull%80000%2%o-u-lonwert-longuatelenee | 470 |
| Number of facto- ries | ๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛ | 208 |
| Name of business category | Agricultural products Meat products Meat products Dairy industry Vegetable or fruits products Fish products made from flour Grain, seed or root processing Flavoring Confined livestock feeding Textile industry Clothing materials processing Rope, net or bag-net Shees Mood industry Clothing materials for cessing Rope, net or bag-net Shees Hulp and paper industry Chemical industry Pulp and paper industry Chemical industry Plastic materials & synthetics Plastic materials & synthetics Plastic materials & synthetics Plastic materials & synthetics Plastic products Plastic products Rubber Plastic products Soap, cosmetic Chemical products fiass products findustry Methines (not use electricity) Machines (use electric parts) Machines (electric parts) Machines | TOTAL |
| Code | %58837757588888888888899999999999999999988888888 | |

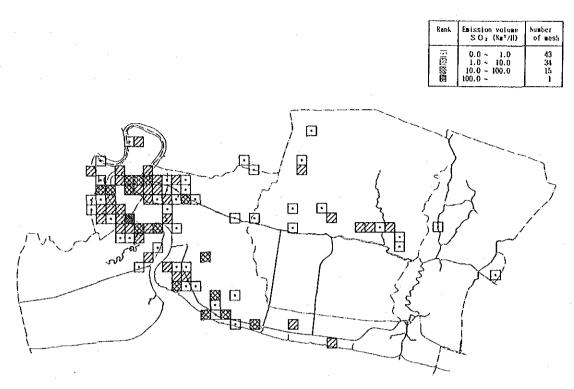
NOx emission volume (ton/year) 5800.85 250.49 8.46 107.98 1255.55 78.73 134.82 210.54 15.26 8108.03 245.35 SO2 emission volume (ton/year) 2774.97 1151.50 1536.28 1161.04 93.62 311.49 2640.88 32.05 1643.91 13648.57 2302.84 Number Number of of facto- faci-ries lities 102 107 ပ 470 111 ഗ ∞ 28 32 14 .---49 40 ഹ প্ন က 208 60 က -4 d. Π 61~83 | Metal and Machine Name of business category 42~53 Chemical industry Non-ferrous metal 84~99 | Other manufactory 22~33 Textile industry 54~58 Ceramic industry Iron and Steel 38~41 | Pulp and Paper 1~21 Rood industry 34~37 | Wood industry TOTAL Code ់ ស្រួ 8

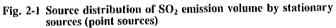
| Actual stack height (m) | Number of stacks | SO2 emission volume (ton/year) | NOx emission volume (ton/year) |
|----------------------------------|------------------------|---|---|
| 0~9 | 56 | 424.57 | 77.48 |
| 10 ~ 19 | 214 | 3646.49 | 524.09 |
| 20 ~ 29 | 75 | 3751.89 | 424,60 |
| 30 ~ 39 | 16 | 2140.27 | 219.82 |
| 40 ~ 49 | 0 | 0.0 | 0.0 |
| $50 \sim 59$ | 1 | 353.65 | 354.37 |
| 60 ~ 69 | 0 | 0.0 | 0.0 |
| 70 ~ 79 | 2 | 0.0 | 1274.71 |
| 80 ~ 89 | 1 | 0.0 | 1183.66 |
| 90 ~ 99 | 1 | 707.30 | 708.74 |
| 100 ~109 | 0 | 0.0 | 0.0 |
| 110 ~119 | 2 | 2624.40 | 3340.56 |
| TOTAL | 368 | 13648.57 | 8108.03 |

Table 2-14 Emission volume by stack height

| Table 2-15 | The top 20 largest of emission vo | lume for each |
|-------------------|---|---------------|
| | factory (in order of SO ₂ emission | volume) |

| SEQ) | Cou- nty Code | Fac- tory No. | Name of factory | Num. of faci lity | SOz emission volume (ton/year) | NOx emission volume (ton/year) |
|---|--|--|---|----------------------------|--|---|
| 1) 2) 3) 4) 5) 6) 7) 8) 9) 10) 11) 12) | 3 3 1 1 3 1 3 1 3 1 3 1 | 98 105 55 68 14 12 70 111 20 47 39 | SOUTH BANGKOK THERMAL PLANT THAI-ASAHI GLASS AJINOMOTO (THAILAND) THAI DEVELOPMENT PAPER THAI TRICOT THAI UNION PAPER THAI TEXTILE PRINTING UNION GLASS BANGKOK STEEL INDUSTRY LUCKYTEX (THAI) THAI PLASTIC AND CHEMICAL YIP YIN TUM | 5222532454212 | $\begin{array}{c} 2624.40\\ 1060.95\\ 786.81\\ 665.28\\ 602.23\\ 584.17\\ 571.74\\ 475.26\\ 387.95\\ 371.65\\ 367.97\\ 283.80 \end{array}$ | $5798.93 \\1063.11 \\91.45 \\43.78 \\46.06 \\53.84 \\52.70 \\165.56 \\56.31 \\36.34 \\32.06 \\27.55 \\$ |
| 13) 14) 15) 16) 17) 18) 19) 20) | | 2 54 51 41 16 1 75 59 | THANAKORN VEGETABLE OIL THAI CHUROS THE BANGKOK IRON AND STEEL ASIA FIBER SIAM TYRE THAI STEEL BAR UNITED GRAIN CENTURIES TEXTILE | 2 4 4 3 4 3 | 274.43 239.50 235.03 233.13 230.96 182.48 180.63 140.84 | 25.29 15.10 43.50 20.31 14.56 30.64 23.36 12.89 |





2.3.3 Calculation of NO_x emission volume

The NO_x emission volume of each facility except electric furnace and incinerator of non-and industrial wastes was calculated by the equation (2-3).

| NO_x emission vol. = | Annual fuel consump. > | < Thermal value |
|------------------------|------------------------|----------------------|
| (kg/yr) | (liter/yr) | (kcal/liter) |
| | kg/yr | kcal/kg |
| | Nm ³ /yr | kcal/Nm ³ |

× Emission factor × 10^{-8} (2-3) (kg/10⁸ kcal)

Where

 No_x emission factor per carolific value is shown in Table 2-16. The table was prepared by referring to following sources.

- Ministry of International Trade and Industry, "Manual of Ambient SO_x and NO_x Prediction Method in Comprehensive Environmental Assessment" (1982)
- (2) Japan Environment Agency, "Report of Atmospheric Emission Survey by Exhausted Gas Factories" (1981)

When these two sources disagree in the value of emission factor by facility type and by fuel type, the whichever larger was selected (Please note star * marked ones).

As for NO_x emission volume for electric furnace and incinerator of wastes, the value was estimated by following formula (2-4) (2-5) respectively.

(1) Electric furnace

NO_x emission vol. = Annual production × NO_x emission factor (2-4) (kg/yr) (ton/yr) (kg/t-product)

where

 NO_x emission factor per ton of product is 0.3566 (from the source (2))

(2) Incinerator for industrial wastes

| NO _x emission vol. | = Annual production × | NO _x emission factor | ••••• | (2-5) |
|-------------------------------|-----------------------|---------------------------------|-------|-------|
| (kg/yr) | (ton/yr) | (kg/t-waste) | | |

where

 NO_x emission factor per ton of waste is 1.859 (non-industrial waste)

1.226 (industrial waste)

The values. were also taken from the source (2)

The NO_x emission volumes by factory and by facility type was shown in Table 2-9, and NO_x emission volumes by county was shown in Table 2-11, those by facility in Table 2-12, those by business type in Table 2-13, those by stack height in Table 2-14 and those in increasing order in Table 2-17. The source distribution figure of NO_x emission volume from stationary sources with the recovered questionnaire is shown in Fig. 2-2.

| Rank | Emission volume NOx (Nm³/H) | Number of mesh |
|------|--|-------------------|
| | 0.0 ~ 1.0 1.0 ~ 10.0 10.0 ~ 100.0 100.0 ~ | 74 19 1 |

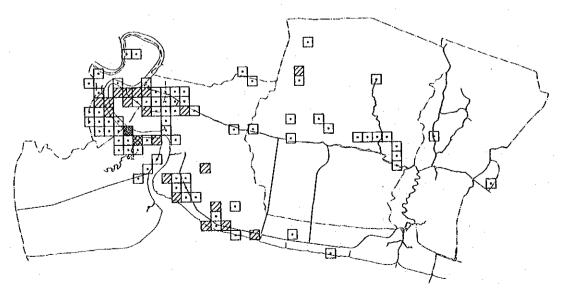


Fig. 2-2 Source distribution of NO_x emission volume by stationary sources (point sources)

Table 2-16 NO_x emission factor per carolific value

| | | | | | | | | | | | | | | | _,_ | | | . | | _ | | | | | | | | | | | | | | | | | | - | | , | <u> </u> | | | | | 1 | | |
|----|--------------------------------------|------------|-----------------------------|----------------|-----------|------------|----------------------|------------------|-------------|-------------|------------------|-----------------------------------|--|------------------|----------------------------------|-----------|--------------------------------|--|-----------|--|--|--------------------------------|-------------------------------|-----------|--------------|---------|------------------------------|-----------------------|-----------|--|-------------------------|--------|----------------------|-------------|---------------|-----------------|----------------|---------------------------|---------------------------------|-------|--------------------------------|--------------|-------------------|---------|---------|---|--------------------|--|
| | Rework | | | | | | 10 IO | | Kinten 11 | | | | 27 - L - L - L - L - L - L - L - L - L - | Note 37 | | | | | ļ | | | | | (2 37 ov | 000 | 0 H 0 | | 16 3) | | | Nota 4) | | | N 000 | | | | | | | | | | 30 | | | | |
| | factor (cal) | (Conros) | 898 | N SIX | 28 83 X | R R | 2/2/ M | 5 3 5 5 | 13,202 | | 32 40% | S0.88 | 61 X | 1 10 10 | 12.2 | 29 - L | X XX | 28 | 88 | *2 5 | in the second se | 8 | 40.41% | 46.46% | **** | Å8 R | ¥00.9¥ | 12.63% | 3488 | 20.15 | 223 | 10.60% | 2.5% | N IN X | 1 | -11.61 <u>×</u> | *5 C | 5 in | \square | -1 | 17. U | 84 83 | C 1 | N 2/ X | - F - 3 | | . "Hanual | e) (1922) |
| 20 | vox emission fact (ke/10"kcal) | o rer 0 | **** **** | - 30 Q | 10.02 | | 19 19 19 19 | | | . | 8.8 | 69°.3% | | 11 | 2 Q Q | 14 | 24.2 | 144 | 2 2 | | 1 | 18,49% | 3.6 | 31.25 | 18.8 | 26.52 | | | 4.61% | 20 20 20 20 20 20 20 20 20 20 20 20 20 2 | 20.03× | 50 | 5.53 | × 31 | *8.C | 5.62 | 99 19 19 | | 0.90 | 3.8 | 28 | 8.83 8.63 | 110, 18% | - 26.02 | 28 | | stry (1171). "Ham | d in Jannere). (in Jannere) |
| | of fuel | | lieny 01 | - Items 011-1- | Light 0il | kerosone - | | | Durth I had | Other solid | L b c l | lion was | | IN WAR | | | | | linuu 011 | | | | Harry Oil | Henvy 0il | - Light 01-+ | υĒ | î | Linther | Neavy 011 | Light Oil | Light Off | | Licht 01 | je | | Heavy Oil | | γc | Kerosche | ا بعم | 20.00 | L P G | 5 | 10 And | | | Trade and Industry | aux and mux rrediction (reliced a) Arconomic 200m (RCA) (|
| | K | | 11 2 | 12 | <u> </u> | 1 | 2 e | 38 | Ť | ٦ 38 | | 11-13 | - | 2 | | 2 | 2 N | , e | | 17 | 12 | | 12 | | - | 87 | 2 | 8 | 112.03 | 1 | | 512 | 5 |) 38 | | | | 389 | 15 | | <u>7</u> 9 | 288 | Σ. | | 588 | | functional - | |
| | Nome of facility type | | Boiler (for electric power) | | <i>l</i> | | | | <u>.</u> | | | Mathal Gration ((aliani / serie) | | (ollocr/seel t.) | Netal rolling f. (steel/cont.) } | | <pre>* * (stoet/batch) {</pre> | and the second s | E | a (atract there is a construction of the state of the sta | x (other/cont.) | Petal forrine f. (storl/cont.) | 011 heating fermoon (updraft) | i. | r r (other) | | Glass weiting furnace (tank) | Other welling furnace | | Direct heating furnace (food) | Deterent drying furnace | | Other drying furnace | | fusion furned | | ۰. ۲ | Bruise furners (for fead) | Activated carbon wante, reactor | | Fusion f. (lead stor. bathery) | | Diese?, generator | | Uther . | | | or regulate and and musi- Professional Argenterments |
| | | | 1010 | - | | | | | | | - | 8 | | g | ī | | 2020 | NSN 1 | | | | 100 | | | gg | | 0915 | 8160 | | <u>8</u> | 1105 | į | 901 | | | 6IV | 12 | | 8 | | ន៍ | | 100 | - | 3 | | | |

Sources Japan Env. Agency. "Munort of aucospheric emittion survey by exhibited gass from factorics", 620, (in Japanese), (1381).

Table 2-17 The top 20 largest of emission volume for each factory (in order of NO_x emission volume)

| | ners a sur vedility datas metter avail 60 a danata ataba taning binang ata a ang ang ang ang ang ang ak Dataih Santas ang Ab |
|---|--|
| N Ox emission volume (ton/year) | 27 80 80 80 80 80 80 80 80 80 80 80 80 80 |
| S O z emission volume (ton/year) | 2624.40 1060.95 765.25 |
| Num. of faci lity | 0040000004400000440 |
| Name of factory | SOUTH BANGKOK THERMAL PLANT THAL-ASAHL GLASS UNION GLASS AJINOMOTO (THALLAND) BANGKOK STEEL INDUSTRY THAI UNION PAPER THAI UNION PAPER THAI DEVELOPMENT PAPER THAI STEEL BAR YIP YIN TUM MICRO FIBER INDUSTRY SIAM STEEL SYNDICATE THAINAKORN VEGETABLE OIL UNITED GRAIN ASIA FIBER |
| Fac- tory No. | 8655232855558525585555555555555555555555 |
| Cou- nty Code | |
| SEQ) | ଌୢୄଢ଼ୢଌୢୣ୷ୄୢୢୄୢୢୄୄୄଢ଼ୄଌୄ୷ୢୄଌୄଢ଼ୢୄୡୄଢ଼୷ୠ୶ଢ଼୶ |

2.3.4 Exhaust gas Temperature

In order to calculate the effective height of the stack, the temperature of exhaust gas from each source has to be determined. Thus the temperature data reported in the questionnaire was referenced. But for those facilities missing them, the mean of reported data was employed. Table 2-18 summarizes the temperature data of various facilities.

| | | Number of | Ope | rating | facil | ities |
|----------------|--|------------------------|----------|--------------------|----------------------|-------------------------|
| Code | Name of facility type | all faci- lities | all | Tem, bla- nk | Tem. wri- tten | Ave.of temp. (°C) |
| 101 103 | Boiler (for electric power) " (other) | 5 267 | 5 228 | 0 149 | 5 79 | 140 189 |
| 502~ 503 | | 8 | 8 | 6 | 2 | 80 |
| $601 \sim 603$ | Metal rolling furnace | 22 | 20 | 12 | Ĩ | 223 |
| 607~ 612 | | 16 | 16 | 16 | Ō | - |
| 613 | Metal forging furnace | 1 | 1 | 1 | 0 | |
| 702~ 703 | Oil heating furnace | - 8 | 7 | 5 | 2 | 320 |
| 915 | Glass melting furnace (tank) | 8 5 2 | 5 | - 3 | 2 | 300 |
| 918 | Other melting furnace | 2 | 2 | 2 | 0 | · · |
| 1001 | Reaction furnace (chemicals) | 1. | -1 | - 1. 1 | 0 | · — |
| 1004 | Direct heating furnace (food) | 8 | 8 | 4 | 4 | 45 |
| 1105 | Detergent drying furnace | 1 | l | 0 | | 350 |
| 1106 | Other drying furnace | 67 | 66 | 45 | - 21 | 17 |
| 1201~1209 | Electric furnace | 11 | 10 | 5 | 5 | 84 |
| 1302~1304 | Waste incinerator | 6 | 6 | 5 | | 150 |
| 1416~1421 | Fusion furnace | 6 | 6 | 6 | 0 | |
| 1423 | Drying furnace (for lead) | . 3 | 3 | 2 | ļ | 60 |
| 1802 | Activated carbon manu. reactor | | 1 | 0 | L L | 240 |
| 2501 | Fusion f. (lead stor. battery) | 10 | 10 | 7 | 3 | 90 |
| 2603 | Reactor (lead pigment) | -1 | 1 | 3 | 0 | |
| | Diesel generator | 3 18 | 3 | 17 | 0 | |
| 8 | Other | 10 | 1 f | . 11 | U | |
| | TOTAL | 470 | 425 | 290 | 135 | 164 |

Table 2-18 Temperature data by facility type

2.4 Emission volume of SO₂ and NO_X from factories without the questionnaire

2.4.1 Procedure of estimation for emission volume

However, there are 2,456 factories registered in Samut Prakarn prefecture, the questionnaire have been recovered only for 208 factories. Emission volume from factories without the questionnaire were estimated as a area source of $2 \text{ km} \times 2 \text{ km}$, based on fuel consumption per employee for each category of industry, which were calculated from the master list of exhaust gas data and data of factories with the recovered questionnaire.

There are three methods for estimation of emission volume from factories without the questionnaire. These methods are based on the following indices.

- (1) Fuel consumption per employee
- (2) Fuel consumption per area of factory
- (3) Fuel consumption per production amount

We reviewed these methods and adopted the first one finally, because there were no data about area of factory in the master list and production amount were not on the equal basis. To be concrete, fuel consumption per employee by business category were calculated from annual fuel consumption volume (heavy oil equivalent) and number of employee in each factory with the recovered questionnaire. Moreover, the figures of fuel consumption per employee (the unit consumption figures) were widely dispersed, we didn't adopt average value but medium value.

We estimated fuel consumption volume of each mesh for factories without the questionnaire as follows;

(Unit consumption figure)×(Number of employee in the master list)

Emission volume of SO₂ and NO_x of each mesh were calculated as follows;

(Fuel consumption volume of each mesh)×(Emission factor)

Procedure of estimation for emission volume in factories without the questionnaire are shown in Fig. 2-3.

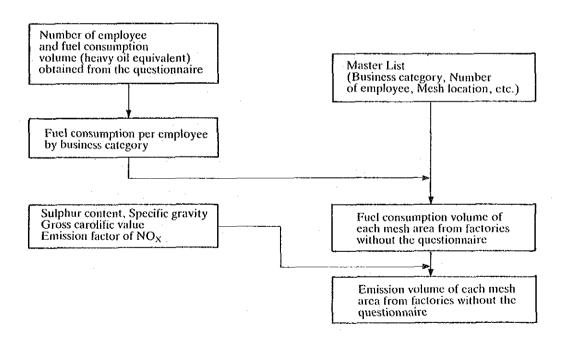


Fig. 2-3 Procedure of estimation for SO₂ and NO_x emission volume from factories without the questionnaire

2.4.2 Selection of factories to be investigated

Master List is rearranged to each category of industry in each district, the result is shown in Table 2-19. Table 2-20 shows relationship among the Table 2-19, questionnaire to have been sent (ONEB selected 577 factories) and questionnaire to have been recovered (208 factories). These

results are rearranged to major categories of industry in each district, finally and shown in Table 2-21. Thus, number of factories, whose questionnaire were not recovered, is 369 (recovered ratio is 36%) and calculation result of pollutant emission volume should be uncertain, unless some estimation method was introduced. However, all the questionnaires for factories with exhaust gas source and whose employee are over 500 persons are confirmed to be recovered, resurvey for factories with less than 500 employees should be necessary.

Therefore, ONEB extracted the factories with less than 500 employees from the Master List again and reconfirmed whether pollutant emission facilities are existing or not, by telephone calling or visiting to the factories. These results are shown in Table 2-22 and Table 2-23.

As a result, the followings are clarified;

- (1) Among the factories without recovered questionnaire (369 factories), 167 factories were confirmed to have pollutant emission facilities.
- (2) Among the factories without recovered questionnaire (369 factories), 130 factories were found that it is uncertain whether they had pollutant emission facilities.
- ③ Among the factories with questionnaire not to have been sent, 275 factories were discovered to have pollutant emission facilities.

Thus, 572 factories without recovered questionnaire should be subject to estimate emission volume. Other discovered items as a result of resurvey and concept of estimation are shown in Table 2-24.

| | | · | | | | | |
|----------------------|--|---|--|---|--|----------------------|----------------|
| Name of | 6 | | Cou | nty | | Kase of business | C |
| business category | de | 1 | 2 | 3 | Tot, | calegory | d |
| | 234567 | 1 2 3 1 12 | 3 | 27 | 30 1 7 8 | Ceranic Industry | CA CH CH CH CH |
| Foot | - 8 9 | 2 | | 15 25 19 | 19 17 | fron Steel | 5 |
| industry | 10 | 8 | 43 2 | 10 | 28 | Non-ferro, | Ģ |
| | 11 12 13 14 15 20 21 | 3 4 19 9 11 | 2 2 4 2 | 3 21 5 10 1 | 3 7 42 16 25 3 1 | | 66666666 |
| Textile Industry | ~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~ | 66 4 7 1 1 3 19 135 12 9 | 6] 3 2 7 1 1 3 2 2 | 157 8 15 10 4 11 1 2 3 5 | 229 13 22 14 9 37 13 2 2 18 15 | Ketal and Nachine | 88666677777788 |
| Wood industry | 28885 | 44 17 10 17 | 17 2 4 4 | 40 10 8 16 | 101 29 22 37 | Other | 80880 |
| Pulp and Paper | 33 33 43 41 | 4 2 8 14 | 1 | 4 10 5 14 | 8 13 13 29 | sanulac- tory | |
| Chemical industry | 434444485383 | 13 1 2 8 6 6 11 6 14 31 | 3 1 2 6 2 4 2 6 | 927888237233 | 875 m 288 | TOTAL | |

| Table 2- | -19 | Number | of | factories | by | business | category | by | master list |
|----------|-----|--------|----|-----------|----|----------|----------|----|-------------|
| | | | | | | | | | |

County

Table 2-20 Number of factories by business category by each data

| list | é ŝ | € – | = | 5 | ~ | ~~~ | 2 I | ດຕ | *** | • | - | 88 | · · · |
|---------|------------------------|---------------------|------------|------------|------------------|----------------------|---------------------|--------------------|------------------|-------------------------|------|----------------|-----------|
| mas tor | liew | യതന ന | ফ | 8 | 154 | m | - 80 | 0 2 2 | - | ෆ | - | 571 | |
| # م | al l data | అచట⊸ట | 12 | 8 | <u> </u> | 55°82 | 27\$8 | 38 ⁸ &~ | ~~go- | 400 <u>0</u> 006 | გოდ | 2456 | |
| | පළ | និតានានាន | \$ | 8 | 8888888 | 388857 | 2625 | 않ਙ쪽귀의 | 888888 | 888888 | 858 | | |
| Name of | calegory | Ceramic industry | iron Stoel | Non farro. | | Netal and Machine | | | | wanufac kory tory | | TOTA | |
| L | | L | <u>.</u> | | | | | | | | | | |
| list | 5 E | r თთთი | SUDO | n CV | -102 103 | 8 0 | ₹ | | n | | 4-4 | , - c | |
| kestor | mo i l | თ ადია | 2≌8 | 3œ- | °7 8 | 9 | e | 1 | 8 ~8 | 90 (N | 1-m- | 4 4 | പയളന |
| ų. | a i l da ta | 8-1-1-00 | 254 | °8' | ٥٣-٤٣ <u>8</u> - | 828- | zo£ | 2002 | 5885 | ಹಿದವಳು | 87 | °88 | 372~288 |
| | 38 | 004001 | - 00 0 | າຊ= | 2867298 | នទេននេ | នគនន | នេងខ្លួន | **** | 8864 | 52 | 氧枪卷 | 8668338 |
| Name of | ours measo category | | | industry | | | Textile industry | | Head industry | Pulp and Paper | | Territori 1 | indus try |

Table 2-21 Number of factories by each data for each major business category

| all data aail 1 2 3 Tot. 257 26 134 282 154 257 26 134 282 154 28 55 217 500 72 28 27 74 139 100 28 27 74 139 100 28 27 74 139 100 28 27 74 139 100 17 28 146 277 56 21 13 3 57 73 54 32 13 3 57 73 54 32 14 4 17 35 34 43 303 106 434 343 43 43 374 286 136 265 577 56 | | | a yd | laster | list | by master list for each county | ch coui | nty |
|---|---------------|-------------------|------|--------|----------|--------------------------------|---------|------|
| category 1 2 3 Tot. Tot. Food industry 83 65 134 282 154 Food industry 83 65 134 282 154 Pulp and Paper 257 26 217 500 72 Pulp and Paper 28 27 74 139 100 Pulp and Paper 28 27 74 139 100 Pulp and Paper 28 27 74 139 100 Chemical industry 101 12 24 21 56 21 Iron and Steel 13 3 57 73 54 Non-ferrous metal 13 3 57 73 54 Metal and Machine 303 106 43 343 34 Metal and Machine 303 106 43 343 34 Of AL 365 107 257 37 557 37 557 <t< td=""><td>ode</td><td>Name of Dusiness</td><td></td><td>alle</td><td>lata</td><td></td><td>mail</td><td>re-</td></t<> | ode | Name of Dusiness | | alle | lata | | mail | re- |
| Food industry 83 65 134 282 11 500 12 Textile industry 257 26 217 500 1 10 | | calegory | | 8 | es es | Tot. | Tot. | Tot. |
| Textile industry 257 26 217 500 * Wood industry 237 26 217 500 * Wood industry 38 27 74 183 10 Cheucal Paper 28 27 74 183 10 Cheucal Paper 28 27 73 75 75 75 Cheucal Industry 17 12 27 26 73 75 Iron and Steel 13 3 57 73 73 75 73 75 73 75 73 75 76 76 73 75 73 75 73 75 73 75 73 75 73 75 73 75 73 73 73 73 73 73 73 73 75 73 73 73 73 73 73 73 73 73 73 73 73 74 73 73 | ~21 | Food industry | 8 | 53 | 134 | 282 | 154 | 49 |
| Wood industry 28 71 14 139 10 Pulp and Paper 28 2 33 63 5 | 88~ ~ | Textile industry | -257 | 8 | 217 | 200 | 22 | 8 |
| Pulp and Paper 28 2 33 63 Chemical industry 101 25 146 273 3 Ceramic industry 171 12 27 55 35 57 35 Icon and Steel 13 3 57 73 35 35 73 35 Iron and Steel 13 3 57 73 35 36 | ~31 | Į | 88 | 22 | 74 | 189 | 100 | 3 |
| Chemical industry 101 26 146 273 Ceramic industry 17 12 27 56 Iron and Steel 13 3 57 73 Mon-ferrous metal 14 4 17 25 Mon-ferrous metal 14 4 17 25 Metal and Machine 303 106 434 35 Otheral and Machine 305 155 57 137 Otheral and Machine 305 155 57 137 Otheral and Machine 307 25 157 57 | 3~41 | and | 83 | 2 | R | ន | 10 | 4 |
| Ceramic industry 17 12 27 56 Iron and Steel 13 3 57 73 Non-ferrous metal 14 4 17 35 Montferrous metal 14 4 17 35 Other manufactory 55 156 57 137 Other manufactory 55 15 57 137 TOTAL 974 285 156 557 575 | ~23 ~ | Chemical industry | 101 | 8 | 146 | 273 | 81 | 40 |
| Iron and Steel 13 57 73 Non-ferrous metal 14 4 17 35 Metal and Machine 305 106 424 345 Other manufactory 955 155 57 137 TOTAL 974 286 156 2456 5 | ~58 | Ceramic industry | 11 | 12 | 12 | 33 | 12 | 4 |
| Non-ferrous metal 14 17 35 Metal and Machine 308 106 434 848 Other manufactory 65 15 57 137 TOTAL 974 286 1196 2456 5 | 53 | Iron and Steel | 13 | en | 57 | 73 | 3 | II |
| Metal and Machine 303 106 434 848 0ther manufactory 65 15 57 137 TOTAL 374 286 1196 2456 5 | ദ്ദ | Non-ferrous metal | Ы | 4 | 11 | R | ន | 5 |
| Other wanufactory 65 15 57 137 TOTAL 974 286 1196 2456 57 | 2 2 2 | | 308 | 901 | | 848 | 9 9 | 8 |
| 974 286 1196 2456 | ₹ 80 80 | Other manufactory | 8 | 15 | 5 | 137 | с С | 3 |
| | | TOTAL | 974 | 286 | 1196 | | 57 | 208 |

Table 2-22 Number of factories which may have facilities but no questionnaire for each county (employee less than 500)

| | | | 0 | (question | enaire ¤ | ailed bu | (questionnaire mailed but not return) | (mu) | | Θ |
|---|------------------|--------|---------------|------------|------------------|---------------|---------------------------------------|-------------------------|--------|------------------|
| | Name of country | (1) | <u>8</u> 2 | ខេត្ត | (72 | (5) cannot | (6) facil. | (T) facil. | | Bailed |
| | | ciosed | faci- lity | answer | infor- mation | con- tact | | excist fuel known | total | facil. excist |
| 1 | Muang | 9 | 29 | 4 | 2 | 40 | 40 19 | 2.0 | 20 125 | 69 |
| ~ | Rang Bo | 1 | 1 | | | 2.3 | 3 | | 28 | 3 |
| 2 | Bang Plee | | 6 | | 2 | 12 | ¢0 - | 5 | 34 | * |
| ŝ | Phra Produeng | 91 | ٧ | 2 | . 4 | 28 | 43 | 44 | 141 | 134 |
| ო | Phra Samut Jedee | 2 | ł | 2 | 1 | 4 | 19 | 6 | 41 | 27 |
| | TOTAL | 25 | 47 | с л | 14 | 107 | 25 | 75 | 363 | 275 |

| | | (questionnaire mailed but not return) | | | | | | | | ,0 |
|--------|----------------------|---------------------------------------|----------------------------|----------------------|-------------------------------|-------------------------------|--|--|-------|---|
| Name o | of business category | (1) closed | (2) no faci- lity | (3) not answer | (4) no infor- mation | (5) cannot con- tact | (6) facil. oxcist fuol unknown | (7) facit. excist fuel known | total | (ques, not Mailed facil, excist |
| 1~21 | Food industry | 13 | 13 | 1 | 1 | 31 | 22 | 14 | 95 | 29 |
| 22~33 | Textile industry | | | | 2 | | 6 | 5 | 13 | 73 |
| 34~37 | Hood industry | 4 | 30 | | 2 | 42 | 17 | 2 | 97 | 1 |
| 38~41 | Pulp and Paper | 1 | | | 2 | 1 | 1 | 1 | 6 | 3 |
| 42~-53 | Chemical industry | 2 | 2 | 1 | 2 | 7 | 16 | 12 | 42 | .47 |
| 54~58 | Ceranic industry | 1 | 2 | · 1 | 1 | 4 | 4 | 5 | 18 | 3 |
| 59 | Iron and Steel | 2 | | 4 | | 13 | 7 | 2.1 | 47 | 14 |
| 60 | Non ferrous metal | | ******** | 2 | 2 | 7 | .9 | 8 | 28 | t |
| 61~83 | Netal and Nachine | 2 | | | 2 | 2 | .8 | -7 | 21 | 9,6 |
| 84~99 | Other manufactory | | | | | | 2 | | 2 | 8 |
| | TOTAL | 25 | 47 | 9 | 14 | 107 | 92 | 75 | 369 | 275 |

 Table 2-23 Number of factories which may have facilities but no questionnaire for each major business category (employee less than 500)

Table 2-24 Methods for the estimation of emission volume

| Mailed but not recovered Q. | (1) closed (2) no-facility | Not subjected to estimate | | | |
|-----------------------------|---|--|--|--|--|
| | (3) no-answer(4) no-information(5) cannot contact | Fuel consumption (Heavy Oil base) was estimated based on number of employce | | | |
| | (6) facility exist and fuel type known but consumption unknown | Fuel consumption (Heavy Oil base) was estimated by using fuel consumption rate. After that these were converted to reported fuel type. | | | |
| | (7) facility exist and fuel type and consumption known | Adopted reported data (fuel type and consumption) | | | |
| not mailed but f | acility exist | Fuel consumption (Heavy Oil base) was estimated based on number of employee | | | |

2.4.3 To set up the fuel consumption rate by business category

As the indices of factory scale, it is used generally number of employee, area of factory, production amount and etc. To estimate the emission volume from factories without the questionnaire, we adopted the number of employee because that there were no data about area of factory in the master list and production amount were not on the equal basis.

Meanwhile, it became clear based on the returned questionnaire data that various kind of fuels was used in each factory. So, to calculate the fuel consumption per employee, it was multiplied various kind of fuel's consumption by the conversion coefficient (equivalent to heavy oil).

We adopted the conversion coefficients which is used generally in Japan and shown in Table 2-25. According to this table, $1 \text{ k}\ell$ kerosene is equivalent to 0.9 k ℓ heavy oil, and 1 ton lumber (gross carolific value 3500 kcal/kg) is equivalent to 0.35 k ℓ heavy oil.

Based on the fuel consumption volume converted into heavy oil which was calculated from questionnaire data and the number of employee, we calculated the fuel consumption rate (per number of employee) by business category. But because of widely dispersive data, we didn't adopted average value but medium value. Fuel consumption rate per employee is shown in Table 2-26. Reviewing the result, the figures largely differ from ones available in Japan. This may be due to the small number of sample data. Thus the comsumption data shown in Table 2-27 are applied in place of those in Table 2-26 as consolidated figures.

| Fuel type | Conversion coefficient | | | |
|--------------------------------|---|--|--|--|
| Heavy Oil | 1.0 ((1() | | | |
| Light Oil | 0.95 ((1)) | | | |
| Kerosene | 0.9 (7/7) | | | |
| General coal | 0.7 (<i>l</i> /kg) | | | |
| Coke | 0.8 (f/kg) | | | |
| Lumber | 0.35 (C/kg) Carolific Value=3,500 kcal/kg | | | |
| LNG | 1.3 (<i>C</i> /kg) | | | |
| LPG | 1.2 ((/kg) | | | |
| Other fuel | Convert into Heavy Oil (Carolific Value=10,000 kcal/c) | | | |
| Material, Waste Electricity | Exclude from conversion | | | |

Table 2-25 The conversion coefficients equivalent to Heavy Oil

 Table 2-26
 Fuel consumption rate (heavy oil equivalent) per number of employee by business category

| Code | Name of business | Number of facto- | Generator of fuel consumption per number of employee (unit : 0.01k1/year/person) | | | |
|-------|-------------------|------------------------|---|--|--|--|
| | category | | Kedian | Each value | | |
| 1~21 | Food industry | 45 | 438 | 13333,8200,7033,5639,3510,2833,2505, 2441,2270,2185,1329,1638,1002,995,973 383,833,600,385,854,550,500,433,400,383 357,352,353,357,354,776,252,218,206 203,180,140,106,106,100,67,80,54,25,1 | | |
| 22~33 | Textile industry | 56 | 137 | 3000,2540,2469,2003,1850,1500,1148,1016 810,781,735,577,433,491,462,411,358,330 270,240,240,220,216,183,182,180,160,150 123,120,116,111,107,104,103,101,100,99 82,81,77,77,69,67,58,55,47,45,44,31,30 30,28,21,17,4 | | |
| 34~31 | Wood industry | 2 | 1065 | 1834,296 | | |
| 38~41 | Pulp and Paper | 4 | 2058 | 2759, 2637, 1479, 722 | | |
| 42~53 | Chemical industry | 31 | - 210 | 1840, 1828, 764, 656, 561, 552, 502, 492, 464 458, 404, 366, 360, 351, 300, 250, 249, 240 210, 209, 195, 194, 189, 180, 163, 144, 115 92, 80, 75, 70, 57, 36, 35, 33, 11, 4 | | |
| 54~58 | Ceramic industry | 2 | 2387 | 3388,1385 | | |
| 59 | Fron and Steel | 11 | 587 | 1963, 1246, 1042, 879, 748, 587, 556, 535, 486 300, 28 | | |
| 60 | Non-ferrous metal | 4 | 128 | 706,226,29,11 | | |
| 61~83 | Metal and Machine | 27 | 72 | 1633, 509, 407, 404, 370, 350, 339, 334, 231, 214 105, 59, 76, 72, 63, 49, 44, 44, 33, 30, 23, 26, 26 24, 18, 18, 6 | | |
| 84~99 | Other manufactory | 1 | 292 | 292 | | |

| Name of business category | Generator of fuel consumption per number of employee (0,01 kg/year/person) |
|---|---|
| Food industry | 438 |
| Textile industry Wood industry | 155 |
| Pulp and Paper Chemical industry Ceramic industry | 250 |
| lron and Steel Non-fe <u>rrous metal</u> | 556 |
| Metal and Machine | 72 |
| Other manufactory | 292 |

Table 2-27 Fuel consumption rate per number of employee used for estimation of fuel consumption

2.4.4 Estimation for the fuel consumption volume of each mesh area

We estimated the fuel consumption volume of each mesh area for factories registered in the master list and not reported by questionnaire but had emitting facility.

2.4.5 To set up the emission factor

To calculate the emission volume from factories without the questionnaire, we used as general rule the general value which was used in Japan as a data of sulphuric content, specific gravity, gross calorific value and emission factor of NO_X . However, we adopted the analytic result of fuel used in Thailand as the sulphur content of heavy oil and light oil.

2.4.6 Estimation for emission volume of SO₂ and NO_X

By multiplying the fuel consumption of each mesh area by emission factor, we presumed the emission volume of SO_2 and NO_x for each mesh area from factories without the questionnaire. Emission volume of SO_2 and NO_x is shown in Table 2-28, Table 2-29, respectively. The source distribution figure of SO_2 and NO_x emission volume from stationary sources without the questionnaire is shown in Fig. 2-4 and Fig. 2-5.

| [| N | S O 2 | emission | volume (t | on/year) |
|--------------|------------------------------|--------|--------------|------------------|----------|
| Code | Name of business category | Muang | Bang Plee | Phra Pradaeng | TOTAL |
| 1~21 | Food industry | 358.0 | 152.2 | 282.0 | 792.2 |
| 22~33 | Textile industry | 169.7 | 49.7 | 250.1 | 469.5 |
| 34~37 | Wood industry | 25.9 | 8.5 | 21.2 | 55.6 |
| $38 \sim 41$ | Pulp and Paper | 3.1 | 19.5 | 2.4 | 25.0 |
| $42 \sim 53$ | Chemical industry | 193.1 | 113.7 | 191.3 | 498.1 |
| $54 \sim 58$ | Ceramic industry | 48.4 | 4.5 | 622.9 | 675.8 |
| 59 | Iron and Steel | 171.4 | 164.9 | 991.3 | 1327.6 |
| 60 | Non-ferrous metal | 91.9 | 3.4 | 201.1 | 296.4 |
| 61~83 | Metal and Machine | 100.5 | 79.2 | 324.7 | 504.4 |
| 84~99 | Other manufactory | 8.8 | 20.9 | 6.8 | 36.5 |
| | TOTAL | 1170.8 | 616.5 | 2893.8 | 4681.1 |

 Table 2-28 SO₂ emission volume from factories without the questionnaire by business category in each county

IV - 36

| [| Nous of Lustress | NOx | emission | volume (t | on/year) |
|-------|------------------------------|-------|--------------|-------------------|----------|
| Code | Name of business category | Nuang | Bang Plee | Plira Pradaeng | TOTAL |
| 1~21 | Food industry | 33.9 | 14.4 | 27.0 | 75.3 |
| 22~33 | Textile industry | 16.3 | 4.6 | 23.4 | 44.3_ |
| 34~37 | Wood industry | 2.4 | 0.8 | 3.1 | 6.3 |
| 38~41 | Pulp and Paper | 0.3 | 1.8 | 0.4 | 2.5 |
| 42~53 | Chemical industry | 18.3 | 10.6 | 17.4 | 46.3 |
| 54~58 | Ceramic industry | 5.1 | 0.5 | 343.9 | 349.5 |
| 59 | Iron and Steel | 14.3 | 15.4 | 77.2 | 106.9 |
| 60 | Non-ferrous metal | 8.4 | 0.3 | 17.4 | 26.1 |
| 61~83 | Metal and Machine | 10.0 | 7.4_ | 34.3 | 51.7 |
| 84~99 | Other manufactory | 0.8 | 2.0 | 0.6 | 3.4 |
| | TOTAL | 109.8 | 57.8 | 544.7 | 712.3 |

Table 2-29 NO_X emission volume from factories without the questionnaire by business category in each county

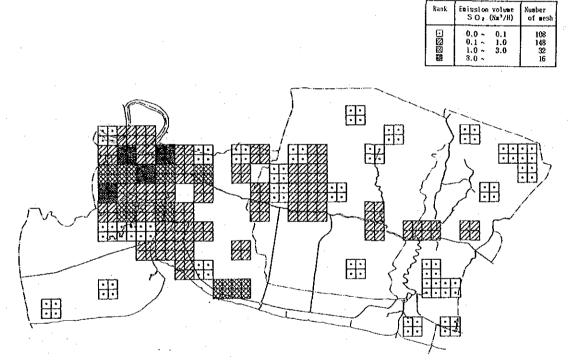


Fig. 2-4 Source distribution of SO₂ emission volume by stationary sources (area sources)

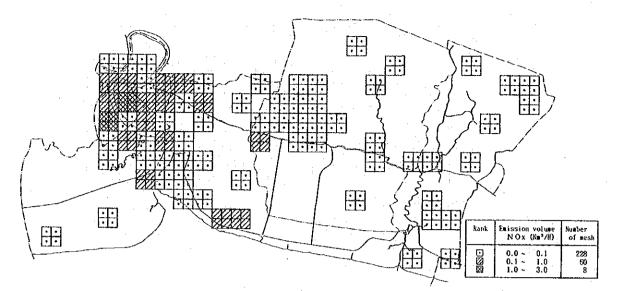


Fig. 2-5 Source distribution of NO_X emission volume by stationary sources (area sources)

2-5 Total emission volume of SO₂ and NO_X from stationary sources (point sources and area sources)

Total emission volume of SO_2 and NO_X from stationary sources located in Samut Prakarn prefecture was calculated by summing up those from factories with the recovered questionnaire (point sources) and without the questionnaire (area sources). The result is shown in Table 2-30 and the source distribution figure of SO_2 and NO_X emission volume from stationary sources is shown in Fig. 2-6 and Fig. 2-7.

From these table and figures it results in that emission volume of SO_2 from factories located in Samut Prakarn prefecture is 18,329.7 T/Y and those of NO_X is 8,820.5 T/Y, and emission volume of SO₂ and NO_X from Pra-Pradaeng in which many factories were located was conspicuous. And the number of factories with the recovered questionnaire was not so many (recovered rate; 27%), but emission volume of SO₂ and NO_X from these factories were 13,648.6 T/Y (74% of total SO_X) and 8,108 T/Y (92% of total NO_X) respectively.

As a result, it was clear that emission volume from large and middle class emission sources were ocupied considerably large part of them from stationary sources.

| Source | Number of factories | SO2 emission volume (ton/year) | NOx emission volume (ton/year) |
|--------------------------|------------------------|---|---|
| Questionnaire return | 208 | 13649 | 8108 |
| (point source) | (27%) | (74%) | (92%) |
| Questionnaire | 572 | 4681 | 712 |
| nothing (area source) | (73%) | (26%) | (8%) |
| TOTAL | 780 | 18330 | 8820 |
| TOTAL | (100%) | (100%) | (100%) |

Table 2-30 Emission volume of SO2 and NOX from factories located in Samut Prakarn prefecture

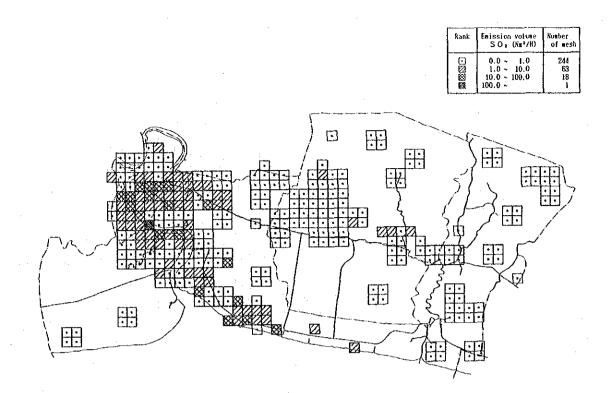


Fig. 2-6 Source distribution of SO₂ emission volume by stationary sources (total)

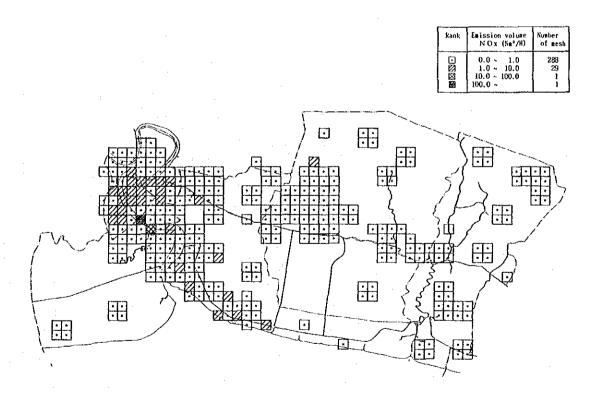


Fig. 2-7 Source distribution of NO_X emission volume by stationary sources (total)

3. Estimation of SO₂ and NO₈ emission volume from roadways

3.1 Outline of the study

The SO₂ and NO_x emission factors separately set for varying types of vehicle and motorway were combined with actual traffic volumes investigated in this report, which then led to the estimation of emission volume of SO₂ as well as NO_x by daytime period and by type of motorways in Samut Prakarn district. In evaluation of exhaust emission volume, the trunk motorways as many as 31 and 243 km long in total were thought as line sources and other minor roadways as negligible sources. The NO_x emission factors of the car were not obtainable in Thailand and thus those of non regulated cars specified by Ministry of Construction, Japan were applied. As for SO₂ emission, the sulphur content of sample fuel was analyzed and the result obtained was referenced.

The following shows the work flow chosen for evaluation of emission volume exhausted from automobiles.

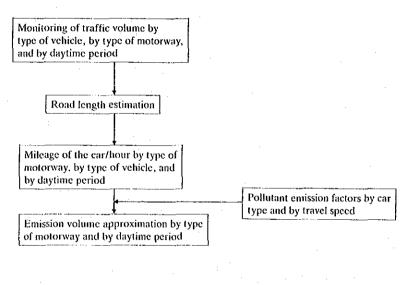


Fig. 3-1 Flow chart for estimation of SO₂ and NO_x emission volume from road way

3.2 Investigation of the traffic volume and drive speed

The traffic volume of Samut Prakarn district was monitored at nine points shown in Fig. 3-2 for 24 hours period. The types of vehicle subject to above survey are shown in Fig. 3-3 and consist of four groups (1) Diesel light vehicle (small truck equivalent), (2) Diesel heavy vehicle (regular size truck, passenger bus, special vehicle), (3) Gasoline car (regular car) and (4) Others (LPG driven car as well as motorcycle equivalent).

The traffic volume survey took place on January 13, 1988 at 4 points (during the first field survey period) and on July 13, 1988 at 5 points (during the third survey period). At MS-1 point, the additional survey was done for both periods in order to estimate the seasonal fluctuation.

The result of this effort is graphed in Fig. 3-4 which indicates the seasonal change of traffic volume is not significant. The traffic volume recorded during the survey periods is summarized in Table 3-1 and actual data at each survey point by type of vehicle and by daytime period in Table 3-2.

The Table 3-3 shows the drive speed of vehicles recorded during same survey period.

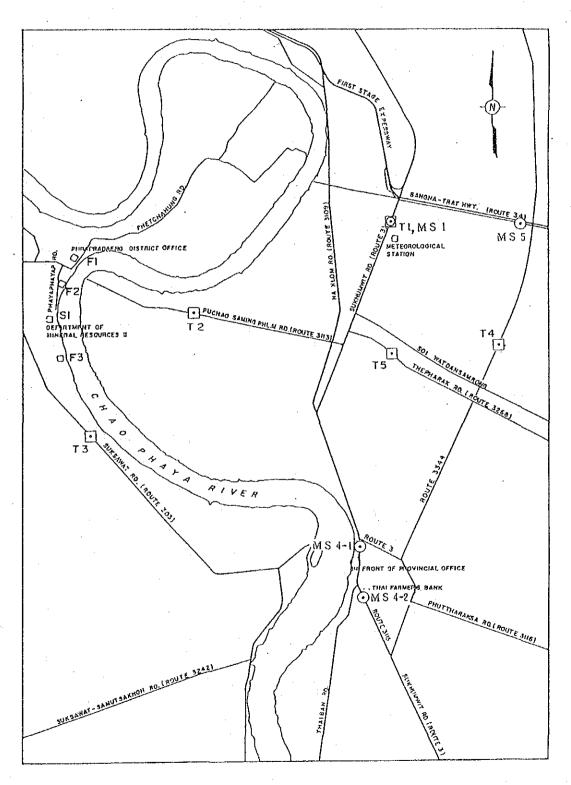
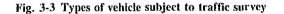
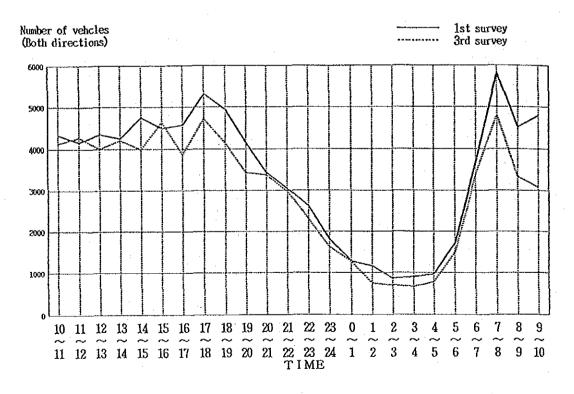
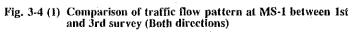


Fig. 3-2 Traffic survey points

| GASOLINE | LPG | GASOLINE | DIESEL LIG | T VEHICLES | . pr | ESCL HEAVY VEHICI | ES . |
|--------------------|--------------|----------------|---------------|------------|-----------|-------------------|-----------------|
| HOTOR-CYCLE | TANI | PASSENGER CARS | PECK UP TRUCK | AEDIUN OUS | HEAVY BUS | 6 WIEELS TRUCK | LO HHEELS TRUCK |
| SPO Lalonground | id id | | | | | | |







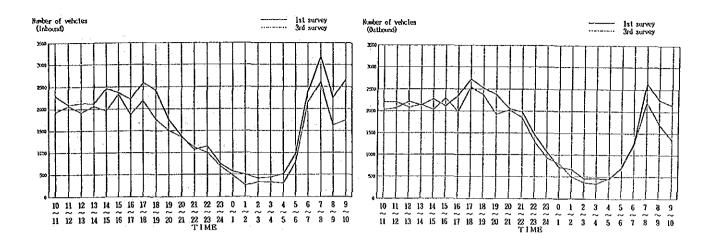


Fig. 3-4 (2) Comparison of traffic flow pattern at MS-1 between 1st and 3rd survey

| ion Diess LV 1 17,44 (21.3 4-1 10,33 (29.5 4-2 4,99 | HV 87 13,9 3) (17.0 58 6,5 | 1ine 01 24,653 0) (30.1) | 3 25,881 | Total 81,922 (100%) | speed (km/h) 47 |
|---|---|---|---|---|---|
| (21.3 4-1 10,3 (29. | 3) (17.) 58 6,5 | 0) (30.1) | | | 47 |
| (29, | | 93 6 59 | | L | |
| 4-2 4.0 | | | | 34,849 (100%) | 45 |
| 4-2 4,9 | | | | 17,054 (100%) | 56 |
| 5 9,6 (30,4 | | | | 31,867 (100%) | 65 |
| i 15,2 (21. | | | | 71,949 (100%) | 47 |
| 2 9,1 (28. | | | | 32,137 (100%) | 30 |
| | | | | 55,719 (100%) | 34 |
| | | | | 34,660 (100%) | 40 |
| | | | | 24,267 (100%) | 30 |
| | (23. 4 10.1 (29.4 5 7.7 (31.5 | $\begin{array}{c ccccccccccccccccccccccccccccccccccc$ | $\begin{array}{c ccccccccccccccccccccccccccccccccccc$ | $\begin{array}{c ccccccccccccccccccccccccccccccccccc$ | $\begin{array}{c ccccccccccccccccccccccccccccccccccc$ |

Table 3-1 Summary of traffic survey

Table 3-2 (1) Results of the traffic survey

| Station3Sl | 0a1 | | /1/13-14 | Û | rection. | |
|-------------|----------|----------|----------|----------|----------|--------|
| | Diesel | | | Gaso- | | |
| list | LV | . 88 | LY+89 | lice | Others | Total |
| 10:00~11:00 | 879 | 1.077 | 1.958 | 1.190 | 1.182 | 4.328 |
| 11:00-12:00 | 974 | 1,070 | 2.044 | 1.091 | 1.041 | 4.155 |
| 12:00~13:00 | 1.029 | . 940 | 1.969 | 1.190 | 1.191 | 4.350 |
| 13:00~14:00 | 1.138 | 765 | 1.903 | 1.165 | 1.176 | 4.245 |
| 14:00~15:00 | 1.150 | 953 | 2.123 | 1.310 | 1.311 | 4.744 |
| 15:00~16:00 | 1.141 | 952 | 2.103 | 1.295 | 1.095 | 4,493 |
| 16:00~17:00 | 1.053 | 717 | 1.770 | 1, (93 | 1,310 | 4.573 |
| 17:00~18:00 | 924 | 592 | 1.516 | 2.195 | 1.508 | 5.319 |
| 18:00~19:00 | 906 | 581 | 1.587 | 1.708 | 1.540 | 4,935 |
| 19:00-20:00 | 843 | 623 | 1.472 | 1.324 | 1.353 | 4.149 |
| 20:00-21:00 | 721 | 124 | 1.145 | 1.124 | 1.156 | 3.425 |
| 21:00-22:00 | 645 | 318 | 964 | 919 | 1,107 | 3.050 |
| 22:00~23:00 | 525 | 229 | 754 | 826 | 1.031 | 2,611 |
| 23:00~24:00 | 351 | 159 | 520 | 467 | 823 | 1.816 |
| 0:001:00 | 264 | \$8 | 352 | 318 | 609 | 1,239 |
| 1:00~ 2:00 | 243 | . 111 | 354 | 233 | 568 | 1.175 |
| 2:00~ 3:00 | 238 | 101 | 339 | 153 | 385 | 817 |
| 3:00~ 4:00 | 255 | 144 | 399 | 130 | 378 | 907 |
| 4:00~5:00 | 255 | 223 | 484 | 120 | 369 | 973 |
| 5:00~ 6:00 | 433 | 533 | 971 | 259 | 483 | 1.712 |
| \$:00~7:00 | 620 | 780 | 1.400 | 1.052 | 1.215 | 3.\$67 |
| 7:00~ 8:00 | 331 | 667 | 1.493 | 2,353 | 1.851 | 5.812 |
| 8:00~ 9:00 | 391 | 572 | 1.453 | 1.583 | 1.459 | 4.510 |
| 9:00~10:00 | 1.157 | 1,135 | 2.292 | 1,039 | 1.415 | 4.795 |
| Total | 17.487 | 13,901 | 31,358 | 24, \$53 | 25,831 | 81.522 |
| Notes : | LY . Lig | hł Vehic | ia X | V = Zeav | y Venicl | e i |

| Station554- | · · · · · · · · · · · · · · · · · · · | Diesel | | Gaso- | | |
|-------------|---------------------------------------|--------|--------|-------------|--------|-------|
| tinè | 1.5 | | LY÷EV | line | Olhers | Tota |
| 10:00~11:00 | 6S0 | 317 | 997 | 399 | 601 | 1,99 |
| 11:00~12:00 | 612 | 350 | \$62 | 403 | 552 | 2.01 |
| 12:00-13:00 | 523 | 366 | 889 | 4{3 | 635 | 1.958 |
| 13:00~14:00 | 591 | 336 | 927 | 358 | 5\$0 | 1.87 |
| 14:00~15:00 | 428 | 656 | 1.084 | 405 | 611 | 2.18 |
| 15:00~16:00 | 440 | 644 | 1.084 | 421 | 670 | 2,17 |
| 16:00~17:00 | 417 | 633 | 1.100 | 477 | 697 | 2,27 |
| 17:00~18:00 | 589 | 382 | 1.071 | 483 | 367 | 2, 42 |
| 18:00~19:00 | 605 | 374 | 580 | 434 | 742 | 2.15 |
| 19:00~20:00 | 511 | 210 | 781 | 310 | 561 | 1,75 |
| 20:00~21:00 | 447 | 250 | 697 | 288 | 532 | 1.51 |
| 21:00~22:00 | 315 | 179 | 495 | 220 | 352 | 1.07 |
| 22:00~23:00 | 195 | 65 | 261 | 133 | 314 | 71 |
| 23:00~24:00 | 149 | 55 | 204 | 69 | 273 | 55 |
| 0:00~1:00 | 172 | 30 | 202 | 58 | 221 | - 18 |
| 1:00~ 2:00 | 165 | 18 | 184 | 63 | 144 | 39 |
| 2:00~3:00 | 187 | 19 | 206 | 13 | 143 | 35 |
| 3:00~ 4:00 | 214 | 15 | 230 | 15 | 123 | 35 |
| 4:00 5:00 | 234 | - 37 | 271 | 52 | 169 | 47 |
| 5:00- 5:00 | 323 | 181 | 510 | 62 | 241 | 81 |
| 6:00~7:00 | 428 | 333 | 751 | 133 | 238 | 1.13 |
| 7:00~ 8:00 | 780 | 304 | 1,084 | 4 45 | 715 | 2,24 |
| 8:00~9:00 | 618 | 372 | 990 | 455 | 662 | 2,10 |
| 9:00~10:00 | 626 | 355 | 981 | 374 | 440 | 1.79 |
| Total | 10.358 | 5.593 | 16.951 | 5,527 | 11.371 | 34,84 |

| Station, | Qa t | e1983 | /1/13-14 | Di | rection. | Both | | |
|---|--------|--------|----------|--------|----------|--------|--|--|
| Tine | Diesel | | | Gaso- | Others | Total | | |
| | LŸ | - XV | LY÷XY | tine | others | 10111 | | |
| 10:00-11:00 | 630 | 722 | 1.352 | 633 | 142 | 2.132 | | |
| 11:00~12:00 | 725 | 898 | 1,622 | 517 | 126 | 2.325 | | |
| 12:00~13:00 | 553 | 721 | 1.284 | 550 | . 93 | 1.927 | | |
| 13:00~14:00 | 542 | 749 | 1.291 | 575 | 93 | 1.960 | | |
| 14:00-15:00 | 643 | 610 | 1,253 | 576 | 99 | 1,923 | | |
| 15:00~16:00 | 652 | 755 | 1.409 | 638 | 132 | 2.178 | | |
| 16:00~17:00 | 825 | 690 | 1.315 | \$54 | 139 | 2,108 | | |
| 17:00-18:00 | 585 | 614 | 1,229 | .840 | 202 | 2.271 | | |
| 18:00~19:00 | 561 | (17 | 978 | 530 | 139 | 1,697 | | |
| 19:00~20:00 | 514 | 419 | 933 | 392 | 100 | 1.425 | | |
| 20:00~21:00 | 425 | 412 | 837 | 291 | 81 | 1,205 | | |
| 21:00~22:00 | 288 | 288 | 575 | 233 | 71 | \$35 | | |
| 22:00~23:00 | 245 | 289 | 534 | 227 | 52 | 823 | | |
| 23:00~24:00 | 203 | 252 | 470 | 140 | 52 | \$52 | | |
| 0:00~1:00 | 149 | 244 | 393 | 92 | 40 | 525 | | |
| 1:00~2:00 | 138 | 197 | 335 | 65 | 35 | 437 | | |
| 2:00~3:00 | 107 | 183 | 255 | 45 | 17 | 357 | | |
| 3:00~ 4:00 | 102 | 201 | 303 | 53 | 10 | 355 | | |
| 4:00~ 5:00 | 109 | 257 | 375 | 43 | 20 | 633 | | |
| 5:00~ 5:00 | 148 | 334 | 482 | 53 | 28 | 353 | | |
| ô:00~7:00 | 232 | 446 | 723 | 173 | 63 | 981 | | |
| 1:00~ 8:00 | 312 | 437 | 803 | 364 | 205 | 1.373 | | |
| 8:00~9:00 | (40 | (38 | 873 | 428 | 115 | 1.421 | | |
| 9:00~10:00 | 638 | 531 | 1,1\$9 | 579 | 137 | 1.585 | | |
| ĵota l | 9.692 | 11,153 | 20,850 | 8, 314 | 2,203 | 31.857 | | |
| Notes : LV + Light Vehicle - NV + Reavy Vehicle | | | | | | | | |

| Station854- | 2 Date | 1533 | /1/13-14 | 01 | rection. | 3 015 |
|-----------------|------------|-------|----------|-------|----------|------------------|
| | Diesel | | | Gaso- | Others | |
| Ti=e | LY | 84 | LV ÷ SV | lice | Uthers | lsioi |
| 10:00~11:00 | 350 | 113 | 4\$3 | 191 | 503 | 1,157 |
| 11:00~12:00 | 315 | 71 | 337 | 574 | 402 | 1.363 |
| 12:00~13:00 | 282 | 83 | 370 | 181 | 139 | 590 |
| 13:00~14:00 | 279 | 94 | 373 | 155 | 391 | 922 |
| 14:00-15:00 | 319 | 102 | 421 | 1\$2 | 413 | 1.601 |
| 15:00~15:00 | 253 | \$9 | 378 | 155 | 392 | 925 |
| 16 : 00~17 : 00 | 322 | 82 | 404 | 157 | 423 | \$50 |
| 17:00~18:00 | 324 | 87 | 411 | 165 | 555 | 1.132 |
| 18:00~19:00 | 330 | 95 | 425 | 185 | 504 | 1.036 |
| 19:00~20:00 | 208 | 79 | 287 | 129 | -122 | 837 |
| 20:00~21:00 | 208 | 30 | 283 | 95 | 371 | 760 |
| 21:00~22:00 | 105 | 46 | 152 | 75 | 267 | 493 |
| 22:00-23:00 | 73 | 24 | 102 | 43 | 262 | 412 |
| 23:00~24:00 | 54 | 23 | 77 | 27 | 101 | 205 |
| 0:00~1:00 | 69 | 9 | 78 | 18 | 115 | 312 |
| 1:00~2:00 | 3 3 | 2 | 53 | 18 | 75 | - 151 |
| 2:00~3:00 | 47 | 3 | ડગ | 6 | 48 | 10- |
| 3:00~4:00 | \$5 | ; | 59 | 5 | 35 | 130 |
| 4:00~ 5:00 | 99 | 15 | 114 | 3 | 13 | 157 |
| 5:00~ 6:00 | 115 | 46 | 151 | 19 | 121 | 301 |
| 5:00-7:00 | 155 | 101 | 255 | 65 | 257 | 578 |
| 7:00~8:00 | 235 | 91 | 333 | 153 | 111 | 1,018 |
| 8:00~ S:00 | 305 | 100 | 405 | 185 | 1:0 | 1,632 |
| 9:00~10:00 | 322 | 81 | 403 | 160 | 132 | 1.025 |
| Total | 4.985 | 1,532 | 5.517 | 2,955 | 7,531 | 17.054 |

•

Notes : EV + Light Vehicle 3V - Heavy Vehicle

, .

Table 3-2 (2) Results of the traffic survey

| StationIl | Dat | a1938 | /7/13-14 | 01 | rection. | Bath |
|-------------|--------|-------------|----------|--------|----------|--------------|
| | Olesel | | | Gaso- | | |
| Tice | L٧ | ۸V | L¥ + XY | line | 012373 | Totel |
| 10:00~11:00 | 952 | \$33 | 1.950 | 1.007 | 1.170 | 4.127 |
| 11:00~12:00 | 850 | 1.051 | 1,501 | 1,101 | 1.271 | 4,273 |
| 12:00~13:00 | \$83 | 952 | 1.935 | 26S | 1.102 | 3,999 |
| 13:00~14:00 | 1.058 | 893 | 1,951 | 1.037 | 1.155 | 4,203 |
| 14:00~15:00 | 898 | 875 | 1.773 | 1.119 | 1.103 | 3,995 |
| 15:00~16:00 | 1.209 | 977 | 2.186 | 1.233 | 1.214 | 4,533 |
| 16:00~17:00 | 897 | 625 | 1,513 | 1,320 | 1,023 | 3,856 |
| 17:00~18:00 | 831 | 398 | 1,423 | 1.755 | 1.534 | 4.718 |
| 13:00~19:00 | 811 | 591 | 1.402 | 1.414 | 1,322 | 4,133 |
| 19:00~20:00 | 737 | 607 | 1.344 | 925 | 1.157 | 3.425 |
| 20:00~21:00 | 635 | 407 | 1.042 | 1.050 | 1.270 | 3,372 |
| 21:00~22:00 | 551 | 314 | 853 | 930 | 1.114 | 2,972 |
| 22:01~23:00 | - 131 | 231 | 712 | 643 | \$55 | 2.316 |
| 23:00~24:00 | 295 | 152 | 448 | 446 | 137 | 1,531 |
| 0:00~1:00 | 242 | 91 | 333 | 345 | 603 | 1.231 |
| l:CO~ 2:00 | 205 | 82 | 287 | 203 | 259 | 759 |
| ?:00~ 3:00 | 180 | \$ 6 | 285 | \$2 | 345 | 703 |
| 3:00~ 1:00 | ារ | 106 | 233 | 35 | 75 | 458 |
| 4:00~ 5:00 | 235 | .175 | 410 | 59 | 259 | 773 |
| 5:00~ 5:00 | 353 | £93 | 845 | 195 | | |
| 5:00~7:00 | 395 | 715 | 1.231 | 1,258 | 833 | |
| 1:00~ 8:00 | 710 | 509 | 1.219 | 1.901 | 1.697 | {.817 |
| 3:00~ 9:00 | 672 | 415 | 1.023 | | 1,002 | 3, 329 |
| 9:00~10:00 | 753 | 781 | 1.544 | 822 | 716 | 3.032 |
| [ota1 | 15.2S4 | 12,727 | 23,011 | 21.323 | 22.510 | 71,949 |

Notes : LV . Light Vehicle HV - Heavy Yehicle

| Station12 | 001 | | /7/13-14 | | rection. | Both |
|---|----------------|-------|--------------|--------------|--------------|--------|
| tize | Diesal | | | Gaso. | Others | Total |
| 11-6 | ٤V | EV . | $LV \div SY$ | liae | 011.014 | 10141 |
| 10:00~11:00 | 625 | 636 | 1,261 | 344 | 5 { ? | 2.147 |
| 11:00~12:00 | 452 | 654 | 1,116 | 303 | : 554 | 1.983 |
| 12:00~13:00 | 561 | 583 | 1.14 | 292 | 493 | 1.929 |
| 13:00~14:00 | 532 | 554 | 1.055 | 325 | 517 | 1.929 |
| 14:0015:00 | 535 | 607 | 1.192 | 332 | : 417 | 1.571 |
| 15:00~16:00 | 665 | 898 | 1.363 | 343 | 607 | 2,313 |
| 16:00-17:00 | 6?2 | 545 | 1,168 | 373 | 201 | 2,102 |
| 17:0018:00 | 600 | 383 | \$68 | 260 | 535 | 1,833 |
| 18:00~19:00 | 510 | 330 | 840 | 374 | 421 | 1,635 |
| 19:00~20:00 | 376 | 235 | 611 | 205 | 854 | 1.660 |
| 20:00~21:00 | 395 | 170 | 565 | 140 | 538 | 1,243 |
| 21:00~22:00 | 158 | 126 | 324 | 138 | 273 | 135 |
| 22:00-23:00 | 122 | 135 | 257 | 167 | 289 | 713 |
| 23:00~24:00 | 83 | 92 | 175 | 123 | 293 | 591 |
| 0:00~1:00 | 50 | 28 | 78 | 147 | 150 | 375 |
| 1:00~ 2:00 | 37 | 44 | 81 | 54 | 72 | 207 |
| 2:00~ 3:00 | 28 | 21 | 52 | 37 | 73 | 152 |
| 3:00~ 1:00 | \overline{n} | 57 | 128 | 15 | 5 | 185 |
| 4:00~ 5:00 | 119 | \$2 | 211 | 15 | 51 | 217 |
| 5:00~ 5:00 | 183 | 160 | 348 | 50 | 105 | 483 |
| 5:00~7:00 | 523 | 415 | 914 | 144 | 355 | 1.443 |
| 7:00~8:00 | 586 | 353 | 949 | \$ 55 | 934 | 2.333 |
| 8:00~ 9:00 | 603 | 370 | 973 | 417 | 513 | 1.958 |
| 9:00~10:00 | 582 | 541 | 1.123 | 257 | :::\$ | 1.836 |
| Total | 9,129 | 7.848 | 16,977 | 5.307 | 9.353 | 32.137 |
| Notes : LY + Light Vehicle NY + Heavy Vehicle | | | | | | |

| Station13 | Da é | . 1093 | /7/\3-14 | Di | rection. | |
|-------------------|----------|--------|----------|---------------|---------------------------------------|--------|
| 313110413 | 02.4 | Diasel | | Geso- | | |
| îi=z | - L¥ - 1 | | LV ÷ 87 | line | Others | ĩot≟l |
| 10:00~11:00 | | 1.010 | 1,565 | | 934 | 3.513 |
| 11:00~12:00 | | 545 | 1.630 | | | 3.091 |
| 12:00~13:00 | 870 | 1.070 | 1.940 | | | 3.558 |
| 12:00~13:00 | 850 | 874 | 1.734 | | 910 | 3.315 |
| 14:00~15:00 | 300 | 564 | 1.562 | | | |
| 14:00~15:00 | 998 | 915 | 1.913 | | | 3,724 |
| 15:00~18:00 | 853 | 631 | 1.559 | | | 3,403 |
| | 842 | 491 | 1.333 | | | 3.591 |
| 17:00-18:00 | 635 | 41 | 1.127 | | | 2.873 |
| 18:00~19:00 | | | 1.118 | | | 2.534 |
| 19:00~20:00 | 671 | 447 | 832 | 520 | | 2.125 |
| 20:00~21:00 | 497 | 335 | | | | 1.957 |
| 21:00~22:00 | 131 | 314 | | | | 1.563 |
| 22:00~23:00 | 323 | | | | | 1.051 |
| 23 : 60 - 24 : 60 | 171 | 190 | 351 | 202 | | 1.001 |
| 0:00~1:00 | 125 | 140 | 265 | <u> </u> | | |
| 1:00~2:00 | \$5 | | | | <u></u> | |
| 2:00~ 3:00 | 97 | 120 | 217 | · · · · · · · | | |
| 3:00~ 4:00 | | | | | <u> </u> | 551 |
| 4:01~ 5:00 | | 2?3 | 378 | | | |
| 5:07~ 5:00 | | 405 | 617 | | | |
| 5:00~1:00 | 401 | 510 | 911 | 592 | · · · · · · · · · · · · · · · · · · · | 2.030 |
| 7:00~ 8:00 | 559 | 337 | | | | |
| 8:00~9:00 | 543 | 479 | 1,124 | 111 | 853 | 2,799 |
| 9:00~10:00 | 795 | 867 | 1.662 | 629 | 509 | 2,900 |
| lsto] | 13.185 | 12.280 | 25,455 | 12, 939 | 17.414 | 55,713 |

Notes : LV - Light Vehicle 2V - Heavy Vehicle

Date...1583/7/13-14 Station...74 Direction....Zoth Cara-Others Total Diesel | 27 | LV÷27 1i=e . 1 V tine 677 374 2.193 10:00~11:00 724 413 1.137 11:00~12:00 647 317 1.024 500 272 1.796 12:00~13:00 633 607 351 2.123 477 1.165 13:00~14:00 650 337 1,037 617 395 2,049 711 -ian 1.152 655 14:00~15:00 437 2.245 15 : 00 - 16 : 00 452 1.211 759 753 418 2.357 15:00~17:00 317 781 1.093 \$25 453 2.477 17:00~18:00 814 191 1.005 1.217 679 2,501 18:00~19:00 658 148 805 851 529 2.155 19:00-20:00 454 191 \$45 552 368 1,565 20:00-21:00 359 121 480 332 282 1.141 21:00~22:00 222 107 329 329 248 906 22:00~23:00 160 69 229 203 182 519 23:00-24:00 94 45 139 124 119 392 0:00~1:00 1:00~2:00 50 210 28 78 İ 83 19 61 39 103 45 32 180 2:00-3:00 ŧ\$ | 37 83 43 20 145 3:60~ 4:60 (3 38 87 35 27 150 4:00~5:00 48 :2 90 33 39 162 5:00~5:60 91 211 120 103 127 441 6:00~7:00 236 222 518 631 359 1.559 817 2.795 7:09-8:09 572 147 719 1.250 8:00~9:00 - 555 159 847 453 2,015 715 583 439 1,122 312 2.044 610 9:00~10:00 10.178 5.007 15.183 12.135 7.342 34.650 lotal Notes : EV . Light Vehicle EV . Neavy Vehicle

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