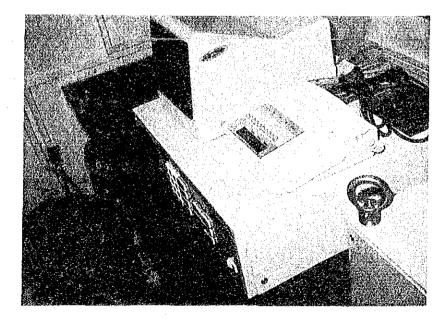
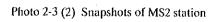


Two dimensional ultrasonic anemometer recording part

SO<sub>2</sub>, NO<sub>x</sub> and particulate measuring instruments



Data logging terminal



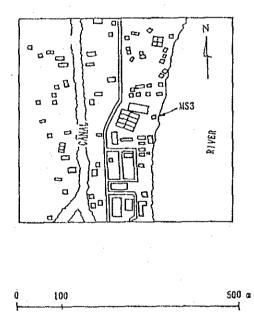
# (3) Mineral Department Office (MS3)

This office is located in Phra Pradaeng county, 4.6 km away from and to the northwest of South Bangkok Power. The eastern end of the office faces Chao Phraya river and the west side of the building commands a canal 120 m apart. The station, MS3 was placed in a corner of the park within Mineral Department site. The area has Bangkok Steel Industry on the other side of Chao Phraya river at a distance of 2.4 km to the west and Ajinomoto (Thailand) 600 m to the south.

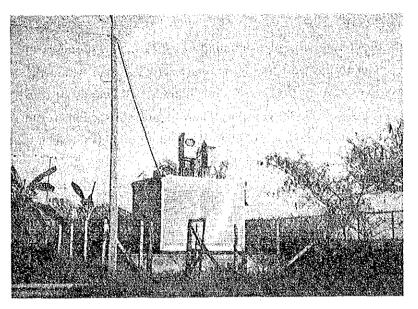
The traffic volume of the vicinity roads is small, but 700 m apart to the north-north-east of the station there are ferryboat terminals for shuttling service across Chao Phraya (in term of boats, 1,300 boats per day). Furthermore, Chao Phraya river itself has the traffic volume of 150 boats per day, in size ranging between several hundreds up to 10,000 or more in tonnage.

Suksawat road (Route 303) runs with daily traffic volume of 55,000 vehicles at 1 km apart from and to the west-south-west of the station MS3. The air quality was measured by instruments placed in MS3. Photo 2-4 are snapshots taken in the vicinity of MS3.

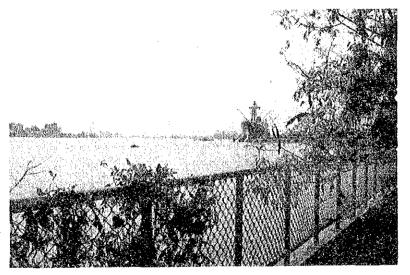




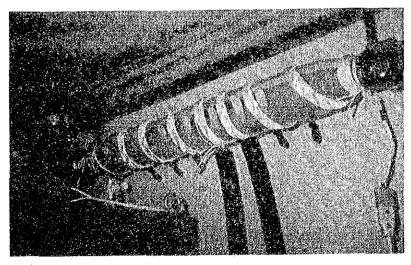




The external appearance of MS3

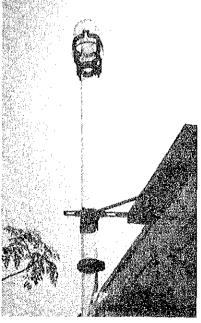


Chao Phraya river viewed from MS3



A manifold traced by the ribbon heater

Photo 2-4 Snapshot of MS3 station



Air intake

# (4) Provincial Office of Samut Prakarn (MS4)

The station MS4 was placed at the front gate side of Community Center in the premises of provincial office and has Chao Phraya river to the west and 30 m apart across a road within the premises. To the east of MS4, however, as shown in Figure 2-6, SuKhumvit road (Route 3) runs about 90 m apart from MS4 with daily traffic of 35,000 vehicles. There is an intersection to the north-north-east of MS4 and about 200 m apart, which has a daily traffic volume of 47,000 vehicles. There exists no factory in the neighborhood of MS4.

The air quality was measured by instruments placed in MS4. Photo 2-5 shows some of snapshots of the MS4 area.



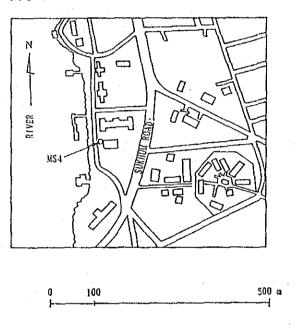
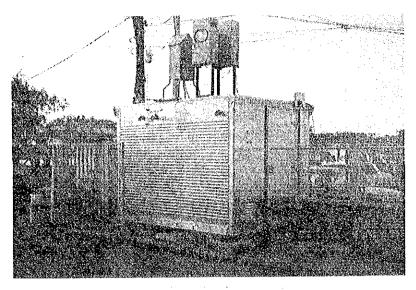
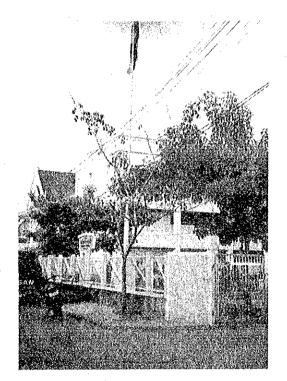


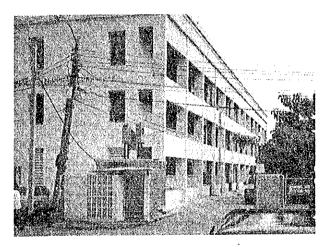
Figure 2-6 The area map of MS4 station



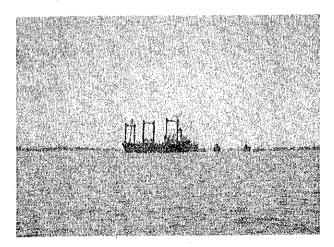
The external appearance of MS4



Samut Prakarn Provincial Office



MS4 viewed from the front gate of the community center



Chao Phraya river viewed from MS4

Photo 2-5 Snapshots taken from MS4 spot

(5) Housing and Industrial Estate office (MS5)

The station MS5 was placed within the premises of Housing and Industrial Estate office of Bang Plee county. The area is basicly a grassland and has scattered shops and houses to the south of MS5 and at a distance of 60 m as shown in Figure 2-7 or has a non-developed housing site to the further south.

There is the Industrial Estate office to the east of MS5 and 150 m apart across a lane leading to Thepharak road (Route 3268), which is non-paved. The spot where MS5 is placed has no factory in its neighborhood but has, to the south and 1.3 km apart, Bangna-Trat Highway (Route 34) with daily traffic of about 32,000 vehicles.

The air quality was measured by instruments placed in MS5 and the wind speed as well as direction was by an anemometer mounted on a pole 10 m high. Photo 2-6 shows the neighborhood views snapshotted.



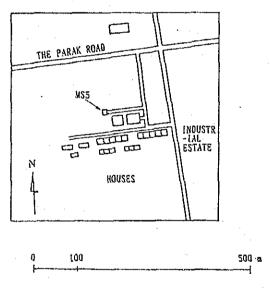
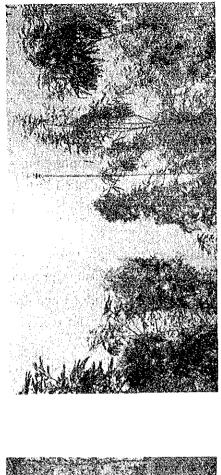
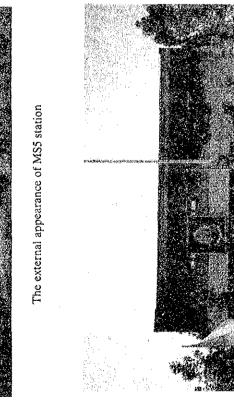


Figure 2-7 The area map of MS5



Housing and Industrial Estate office of Bang Plee county





Two dimensional ultrasonic anemometer fixed at a 10 m high pole top

Photo 2-6 Snapshots taken from MS5 spot

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# 3. Education and training relevant to handling of measuring instruments

The field survey, as aforementioned, is dependent on instruments of automatic and continuous type to complete a year round monitoring of such variables as  $SO_2$  and wind velocity. Thus the maintenance of those instruments was thought of utmost importance to assure the accuracy of measurements throughout such a long period. The job was basically arranged such that ONEB is responsible for the regular inspection and maintenance of instruments and the Japanese staff team for the periodical check and part replacement of them.

Under the circumstances, it was decided that ONEB staff engineers receive the training course with respect to basic theories involved, handling, maintenance and calibration of applied instruments. The training was also practiced from the viewpoint that those instruments can be operated by Thai staff members even after the completion of this project.

The technical transfer cooperation with respect to instruments handling was made three times in total each at the first, second and third field trip by Japanese staff. As for periodical inspection and maintenance of instruments, the transfer cooperation was made when 1st, 2nd, 3rd and 4th Japanese survey team practiced the scheduled checks on instruments. The persons who received such training and the content of transfer cooperations are listed as follows.

(1) Handling, maintenance and calibration of instruments

The first field survey period

Mr. Warawut Suadee	Environmental Officer
Mr. Kanok Suksomsunk	ditto
Mr. Khunchai Kriengkrai-udom	ditto
Mr. Santad Koompalum	ditto
The second field survey period	

Mr. Warawut Suadee

- Mr. Kanok Suksomsunk
- Mr. Khunchai Kriengkrai-udom
- Mr. Santad Koompalum
- Mr. Suphol Cheiwkijkachorn
- The third field survey period
- Mr. Warawut Suadee
- Mr. Kanok Suksomsunk
- Mr. Khunchai Kriengkrai-udom
- Mr. Santad Koompalum
- Mr. Suphol Cheiwkijkachorn
- (2) Scheduled inspection and maintenance of instruments
  - The first survey period
  - Mr. Warawut Suadee
  - Mr. Khunchai Kriengkrai-udom
  - Me. Santad Koompalum

The second field survey period

Mr. Warawut Suadee

Mr. Khunchai Kriengkrai-udom

Mr. Santad Koompalum

The third field survey period

Mr. Warawut Suadee

Mr. Khunchai Kriengkrai-udom

Mr. Santad Koompalum

The fourth field survey period

Mr. Warawut Suadee

Mr. Khunchai Kriengkrai-udom

Mr. Santad Koompalum

Mr. Phunsak Tiramongkol

Mr. Kanok Suksomsunk

The outline of technical transfer efforts such as handling of instruments, etc is as follows. It is described more in detail in the succeeding chapter with respect to each monitoring target.

# 3.1 The technical transfer related to instrument handling

The first effort of such technical transfer was made immediately after the monitoring station structure was built and the measuring instruments were brought in and placed in it.

The way of operation and handling of instruments were taught through practical drills and then by means of instruction manuals written in English and prepared in advance. After measurements started, Japanese staff checked together with ONEB staff the condition of instruments and readings once every hour according to the check manuals. As for Low volume samplers as well as Andersen samplers, all of them were temporarily assembled in an ONEB room and were subject to calibration while technical transfer relevant to such job being made. Then samplers were transported to each of stations where the result of training at ONEB was again reconfirmed.

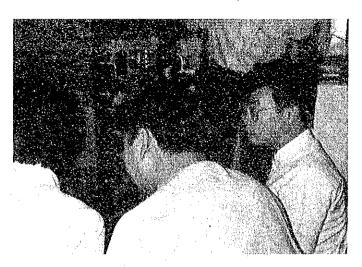
From the second field survey on, the technical transfers continued in such a way that both Thai and Japanese parties coworked in the adjustment and calibration of instruments. An activity snap is shown in Photo 3-1.

# 3.2 Technical transfer about scheduled inspection and maintenance

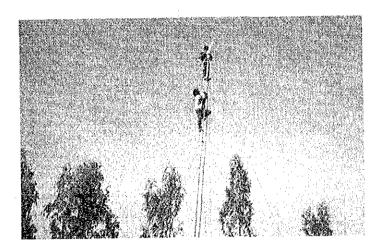
The transfer cooperation was made four times with respect to the scheduled inspection and maintenance of instruments.

(1)  $SO_2$  meter

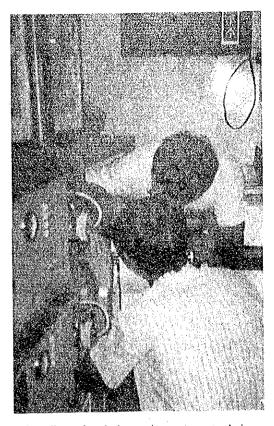
- 1) Replacement and adjustment of lamp unit
- 2) Cleaning of detector window
- 3) Cleaning of measuring cell
- 4) Replacement of detector window
- 5) Alignment of optical axis
- 6) The way of inspection of I/O and CPU board when sensitivity is dropped
- (2)  $NO_x$  meter
  - 1) Cleaning of cell window
  - 2) Replacement of photomultiplier
  - 3) Cleaning of detector interior
  - 4) Inspection method of dark current of detector
  - 5) Voltage measurement of O<sub>3</sub> generator power source
  - 6) The way of inspection of I/O and CPU board when sensitivity is dropped.
- (3)  $\beta$ -ray adsorption type dust meter
  - 1) Cleaning of cell
  - 2) Precaution relevant to  $\beta$ -ray source
  - 3) Adjustment of flow stabilization circuit
  - 4) Cleaning of dust trap
  - 5) The way of inspection of I/O and CPU board



 $SO_2$ ,  $NO_x$  and dust meter being explained



Two dimensional ultrasonic anemometer being adjusted



Two dimensional ultrasonic anemometer being explained



Three dimensional ultrasonic anemometer being explained

Photo 3-1 (1) Technical transfer interactions snapshotted

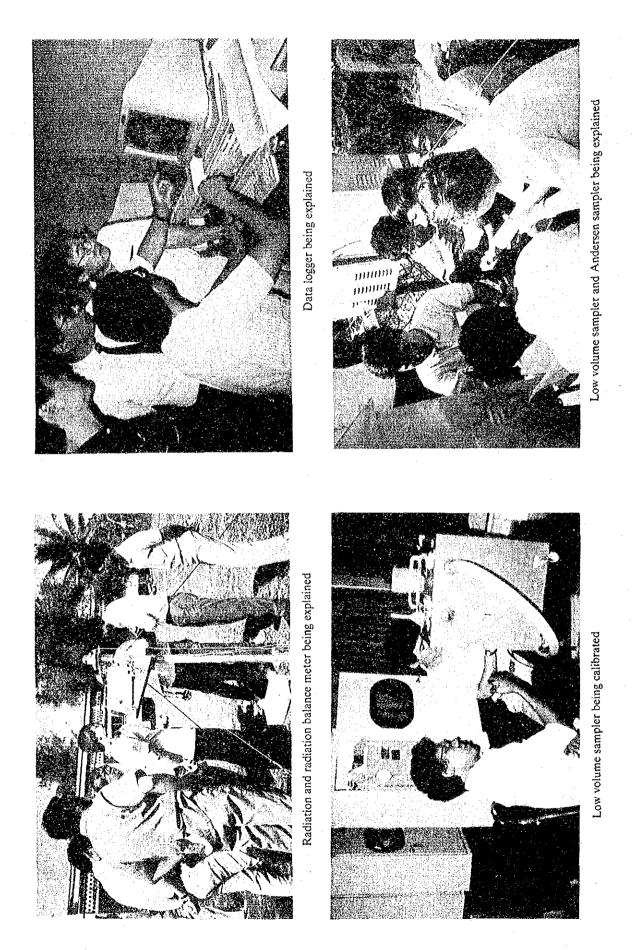


Photo 3-1 (2) Technical transfer interactions snapshotted

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# 4. Long term field survey (1 year survey)

A year long field survey continued for the period of January 17, 1988 through January 16, 1989 to measure an hour averages of  $SO_2$ , NO, NO<sub>2</sub>, SPM, wind speed and direction, air turburency, solar radiation and radiation balance by using respective instruments. The measurement data were typed out in hard copies and were simultaneously transmitted to a data logger and a telemetric printer installed at ONEB central supervisory and control room. (The data observed by MS1 station, however, were not transmitted to ONEB.)

In addition to data collection above, total suspended particulate were monitored by low volume sampler at each station, where two samplers were installed, one with a polyfluorocarbon filter to improve the accuracy of elemental as well as ion analysis and the other with a quartz filter for carbon analysis of the dust.

The filters of sampler were replaced once every half a month and trapped particulate matters were subject to analyses throughout the survey period.

Table 4-1 summarizes the type of measurements practiced at every station.

	Observation	Measurements	Instruments						
MS1	ONEB Station	Sutphur dioxide (SO <sub>2</sub> )	Ultraviolet-spectrophotometry						
		Nitrogen oxides (NO, NO <sub>2</sub> )	Chemiluminescence NO <sub>x</sub> meter						
		Suspended particulate matter	$\beta$ -ray adsportion type meter						
		Total suspended particulate (TSP)	Low volume sampler						
		Wind velocity and direction	3-dimensional ultrasonic anemometer						
·		Air turbulency	ditto						
		Solar radiation	Eppley pyrheliometer						
	· · ·	Net radiation flux	Net radiation flux meter						
MS2	Power plant (EGAT)	SO <sub>2</sub>	Ultraviolet Spectro-photometry						
	-	$NO, NO_2$	Chemiluminescence NO <sub>x</sub> meter						
		SPM	$\beta$ -ray adsorption type meter						
		TSP	Low volume sampler						
	:	Wind velocity and direction	2-dimensional ultrasonic anemometer						
MS3	Mineral Department Office	SO <sub>2</sub>	Ultraviolet Spectrophotometry						
	* *	NO, NO <sub>2</sub>	Chemiluminescence NO <sub>x</sub> meter						
		SPM	$\beta$ -ray adsorption type meter						
		TSP	Low volume sampler						
MS4	Samut Prakarn Provincial	SO <sub>2</sub>	Ultraviolet Spectrophotometry						
1	Office	NO, NO <sub>2</sub>	Chemiluminescence NO <sub>x</sub> meter						
		SPM	$\beta$ -ray adsorption type meter						
		TSP	Low volume sampler						
MS5	Housing & Industrial Estate	SO <sub>2</sub>	Ultraviolet Spectrophotometry						
	Office	NO, NO <sub>2</sub>	Chemiluminescence NO <sub>x</sub> meter						
1		SPM	$\beta$ -ray adsorption type meter						
		TSP	Low volume sampler						
		Wind velocity and direction	2-dimensional ultrasonic anemometer						

Table 4-1	The type of measurements practiced at MS1 through MS5 for
	the longterm field survey period

# 4.1 Measurement of environmental pollutant concentrations

# 4.1.1. Measurement of SO<sub>2</sub> atmospheric concentration

In order to monitor the status quo of  $SO_2$  pollution in Samut Prakarn Industrial District, the  $SO_2$  measuring instruments of automatic and continuous type were placed at five stations and pollutant concentrations were measured once every hour continuously throughout one year survey period. The instruments were subject to the calibration once every week and also to the scheduled inspection, once every three months.

# (1) $SO_2$ environmental concentration measurement

There are several measurement methods proposed for the measurement of  $SO_2 + SO_3$  as shown in Table 4-2. Among these, methods of (1) through (4) are described in Japanese Industrial Standards (JIS) as continuous monitor of environmental  $SO_2$  concentration. In addition, the methods of (2) through (4) and (9) are described in Federal Register of EPA (U.S.A.) as continuous monitor and the method (9) as standard one for manual analysis. The method (1) is employed as one to judge whether the measured value meets the national control standards stipulated.

	Measuring methods	Pollutants	Applicable conc. range	Relative standard	Remarks
(1)	Solution conductmetry	so <sub>2</sub>	0 - 50 ppb, 0 - 1 ppm	JIS B7952	Continuous analyzer
(2)	Coulometry	so <sub>2</sub> .	0 - 100 ppb, 0 - 1 ppm	JIS B7952	- ditto -
(3)	Flame photometric	so <sub>2</sub>	0 - 100 ppb, 0 - 1 ppm	JIS B7952	- ditto -
(4)	Ultraviolet spectro-photometry	soz	0 - 100 ppb, 0 - 1 ppm	JIS B7952	- ditto -
(5)	Chronoamperometry	soz	0 - 100 ppb, 0 - 1 ppm	JIS B7952 Reference	- ditto -
(6)	Lead dioxide	so <sub>z</sub> + so <sub>3</sub>	Over 0.2 SO <sub>3</sub> mg/ d/100 cm2	B.S.1747 Part 15 ASTM D.2010	Relative conc. measurement
(7)	Alkali filter	so <sub>2</sub> + so <sub>3</sub>	Over 0.2 SO <sub>3</sub> mg/ d/100 cm2	-	- ditto -
(8)	Valium molybdate	so <sub>2</sub> + so <sub>3</sub>	-	-	Chemical analysis
(9)	Pararosaniline	so <sub>2</sub>	3 ppb - 5 ppb	ASTM C.2914	Continuous & Chemical analysis

Table 4-2 Measuring methods of ambient sulphur of	oxides
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(2) Methods used in this survey

The type of analyzer used in this survey is of Ultraviolet spectro-photometry type, which uses the fluorescence light emitted from the sulphur dioxide in the ambient air brought into the excited state,  $SO_2^*$ , by absorbing ultraviolet ray. The  $SO_2$  concentration is determined by measuring the fluorescence intensity. The reactions to show this principle are shown as follows,

$$SO_2 + h \nu 1 = SO_2^*$$
 .....(4-1)

$$SO_2 * = SO_2 + h v 2 \dots (4-2)$$

$$SO_2^* = SO + (O) \dots (4-3)$$

 $SO_2 * + M = SO_2 + M$  .....(4-4)

where the reaction (4-1) indicates that a SO<sub>2</sub> molecule absorbs the UV energy h  $\nu$  1 and goes into the excited state, SO<sub>2</sub><sup>\*</sup>, the reaction (4-2) the excited molecule emitting light energy h  $\nu$  2 when it returns to the ground state, the reaction (4-3) decomposition of the excited molecule by light and the reaction (4-4) the excited molecule losing its energy by colliding with other molecules (called quenching).

In general, when  $SO_2$  molecules are irradiated by a UV ray, absorption occurs in the following three wavelength bands as shown in Table 4-3 and Figure 4-1 in which band 1 and band 2 are weak in adsorption and show a large trend for quenching. Therefore, the band 3 with the largest absorption and the least quenching trend is selected as excitation light by means of a selection filter. The fluorescence light of excited  $SO_2$  is detected through the optical selection filter. Since the hydrocarbons in the air also emit fluorescence, they are normally removed by using an HC cutter (scrubber).

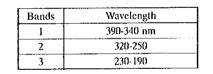


Table 4-3 Ultraviolet ray adsorption bands of SO<sub>2</sub>

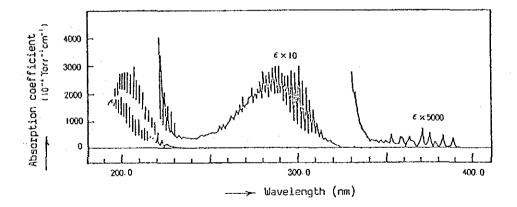


Figure 4-1 Adsorption spectrum of SO<sub>2</sub>

The SO<sub>2</sub> analyzer used in this survey is an ultraviolet-spectro-photometry one, manufactured by DKK Corporation, GFS-31 type. The analyzer is designed such that it can introduces the internally refined zero gas into the cell once every 20 minutes and stabilizes the zero point level by comparing the zero gas value with the sample value. The light source lamp is of pulse-driven type and thus reading is taken during the pulse lightening period of the lamp in order to minimize the effect of dark current of a photomultiplier tube. The mechanism is thought effective to prolong the service life of the lamp too.

The recording part of the system reads both instantaneous and hourly averages and has external I/O terminals and an external output connector to transmit hourly averages to the data logger as well as telemetric recorder.

As for hourly averages, the automatic range switcher is built in and changes the range from a smaller one to a next larger one when reading exceeds the scale range (0-0.05 ppm, 0-0.1 ppm, 0-0.2 ppm, 0-0.5 ppm, 0-1.0 ppm). When reading newly starts, the range gets automatically back to 0-0.05 ppm one.

Major specifications of this  $SO_2$  analyzer are shown in Table 4-4, the measurement system diagram in Figure 4-2 and the mechanical structure in Figure 4-3.

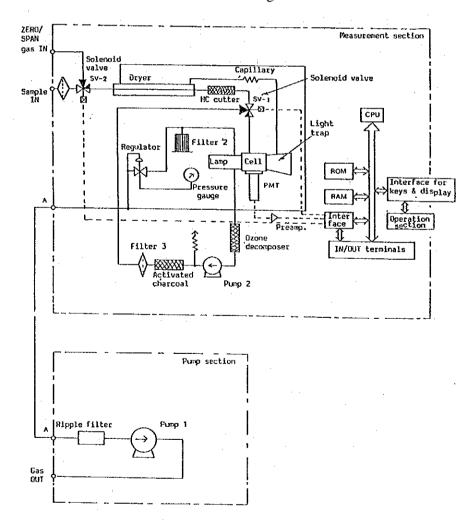


Figure 4-2 Measurement system diagram

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# Table 4-4 Major specifications of SO<sub>2</sub> analyzer

Name of product:	Atmospheric sulfur dioxide analyzer
Model:	GFS-31
Measurement object:	Atmospheric SO <sub>2</sub>
Measurement method:	Continuous measurement on the
	principle of ultraviolet fluores-
	cence
Measurement range:	Instantaneous value
	0-0.1, 0-0.2, 0-0.5, 0-1.0 ppm,
· · · · ·	manually switched 4 ranges
	Hourly average (Saw-tooth)
•	0-0.05, 0-0.1, 0-0.2, 0-0.5, 0-1.0
	ppm,
	automatically switched 5 ranges
Display:	Instantaneous value of SO <sub>2</sub>
Reproducibility:	Within $\pm 2\%$ FS
Stability: Zero drift	Within'± 1%FS/day
Span drift	Within $\pm 2\%$ FS/day
Response time:	Within 4 minutes for 90% response
Amblent temperature:	0-40°C
and the second	
Power requirements:	100VAC± 10%, 50/60Hz 150VA
Power consumption:	
Dimensions:	Neasurement section
	430(W)x596(D)x270(H) mm
	Pump section
	270(W)x285(D)x280(H) mm
Weight:	Measurement section 23kg
· · · · ·	Pump section 6kg
Color painting:	Munsell N4 and N7
Input/output signals;	<u>Transmission_output</u>
	0-1VDC (isolated input),
	instantaneous value and hourly
	average,
	(Max.internal resistance 500 $\Omega$ ,
	min. load resistance 100k $\Omega$ )
	<u>Contact output signals</u>
	o Instantaneous value measurement
	range switching signal
	o Hourly average value measurement
	range switching signal
	o Under-adjustment (TEST) signal
	o Blown-fuse signal
	o Under-calibration signal

o Calibration-impracticable signal

(Contact rating 50VDC 0.1A or less) Contact input signals

o External reset signal

o Observatory stop signal

o Auto-calibration start signa) (Contact rating 50VDC 0.1A or less) Data printer Analog recorder

# Related equipment:

Cubicle for outdoor installation

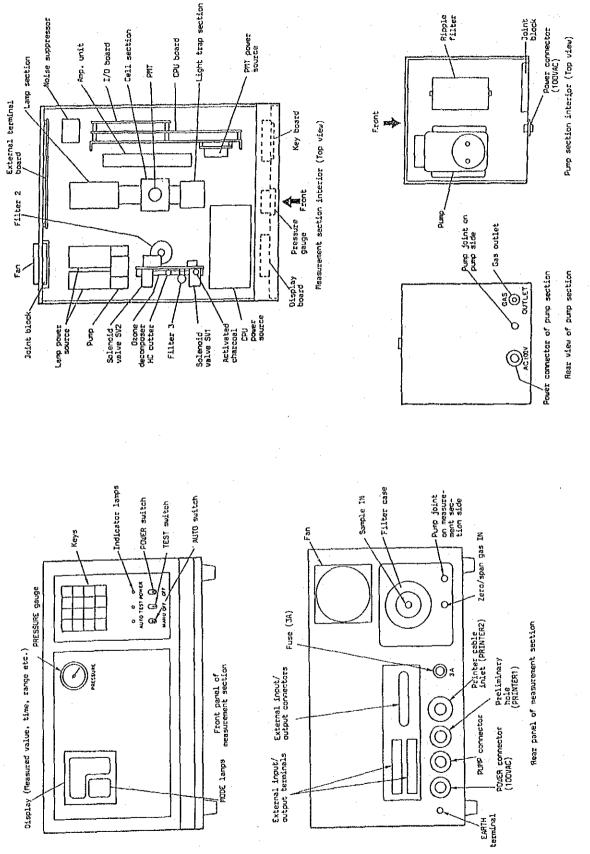


Figure 4-3 The mechanical structure of SO<sub>2</sub> analyzer

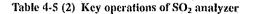
II - 28

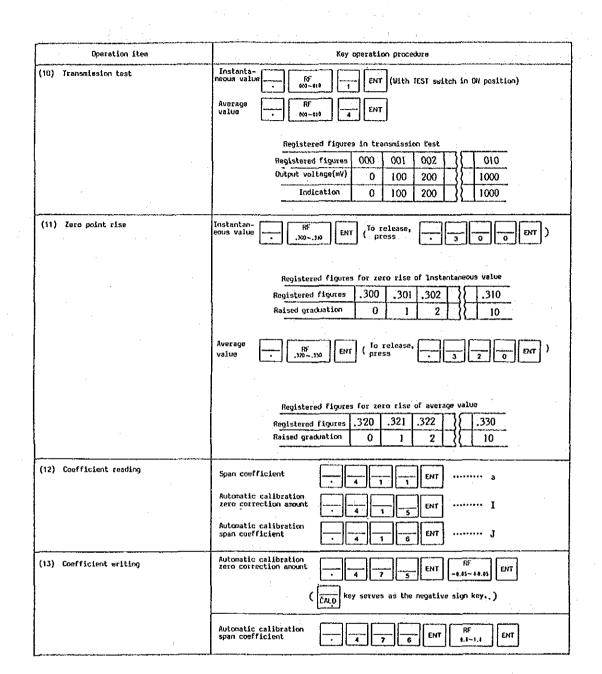
# (3) Operation

The analyzer is put into operations by actuating front panel keys (see Figure 4-3) in which the selection of operation mode leads the operator to various options like calibration, time setting, etc. The detail of key operations conforms to Japanese or English manuals.

Operation item		Key operation procedure
(1) Time	Setting	TIPE $\begin{bmatrix} RF \\ i:N-2i:H \end{bmatrix}$ ENT Press the entry key when the present time agrees with the registered figures.
	Reading	TIME ENT ( C depression for releasing. Display returns to concentration.)
(2) Zero gas introduction		ZER0     ENT     (C     depression for releasing.)
(3) Span gas introduction		SPAN ENT (C depression for releasing,)
(4) Span setting value	Vriting	SPAU BF BAT * Span gas concentration
	Reading	SPN.V ENT (C depression for releasing.)
(5) Automatic calibration time	Writing	Image: CAL.1     RF     Image: CAL.1     Image: CAL.
	Reading	[IAL_]     ENT     (     C     depression for releasing.)
(6) Automatic calibration period	Writing	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$
	Reading	PER     ENT     (C     depression for releasing.)
(?) Number of remaining days till next calib- ration	Writing	$\begin{bmatrix} CA, D \\ I \sim n \end{bmatrix} \begin{bmatrix} PF \\ I \sim n \end{bmatrix} \begin{bmatrix} ENT \end{bmatrix} $ (Returns to concentration indication after 7 second.)
	Reading	CAL.D ENT (C depression for releasing.)
<ul> <li>(8) Automatic calibration starting</li> </ul>		ENT (With AUTO switch in AUTO position.)
(9) Measurepent range	Switching (Writing)	Instantan- eous value HAMJ CONC AF ENT ( RF : 0.1, 0.2, 0.5, 1.0)
		Average RAMG AVG RF ENT ( RF : 0.05, 0.1, 0.2, 0.5, 1.0)
	Reading	RANG COXC ENT OI RAIT AUG ENT

# Table 4-5 (1) Key operations of SO<sub>2</sub> analyzer





# (4) Calibration

Though the GFS-31 SO<sub>2</sub> analyzer has a provision for automatic calibration capacity, the job was manually done in this survey. The procedures of calibration are the connection of calibration supply gas system with SO<sub>2</sub> meter, and then calibration of zero gas and span gas by means of the key panel on the front operation side of analyzer. The standard gas used was one cylindered with about 90 ppm in SO<sub>2</sub> content, pre-inspected by Chemicals Inspection & Testing Institute, Japan. Since the guarantee term of this standard gas is a half year period, it was replaced in the middle of survey period.

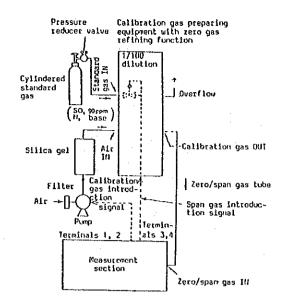


Figure 4-4 The supply system of calibration gas

# (5) Inspection and maintenance

In order to maintain the desirable performance of the SO<sub>2</sub> meter, the inspections were practiced as shown in Table 4-6, in which weekly and monthly periodical inspections and calibrations depended on ONEB and others were performed jointly by ONEB and Japanese staff.

		Co ja	cts of mainten	ance check	G	eck	bat:	leđ		Reference	
	00.34	ct	Itea	Contents	tdeck -	Month	3 months	6 wonths	Year	Section	
1	Flow pat	h tubinga	Direck	Fouling, buckling, discon- nection, leak	┢	0	-				
			Replacement	Each tube					σ		
		· · ·	Leak	Leak test	-		Ö				
2	Filter	Element(PF)	Replacement	Replacement by new one.	D						
	case	Case	Cleaning	Joints, filter case interior	-		Δ			7,2	
3	Glass el	ement of	Cleaning	Glass element			۵				
	Reasures	ent section	Replacement	Replacement with new one		-			D	7.3	
4	Suction		Check	Abnormal sound, vibration		0					
	pump sec	tion		Is pressure normal ?	0						
			Cleaning	Disphrage, valve, joint			Δ				
			Replacement	Replacement of disphragm and valve by new one.					0	7.4	
5	HC cutte ment	r replace-	Replacement	Replacement by new one.			0			7.5	
8	Activate replaces	d charcosl ent	Replacement	Replacement by new one.					o	7.5	
7	Ozone de replaçen	corposer ent	Replacement	Replacement by new one.					a	?.5	
8	Light so replaces	urce lamp ent	Replacement	Replacement by new one.					o'	7.6	
9	Cell		Cleaning	Cell wall		-		_	Δ	7,7	
10	Calibrat	100	Calibration	Manual zero/span	õ					5.1	
11	Clock		Check	Check for time deviation	ō					4.1 e.	
12	Capillar	γ	Cleaning -	Internal cleaning				Δ			
		-	Replacement	Replacment by OKK genuine parts					D		
13	External	tubings	Chack Fouling, buckling, dis- connection, leak							2.3	
			Replacement	Replacement by new one.					0		
14	Wiring w side	ith out-	Check	Loosening, breakdown	0		_			2.4	

Table 4-6 Scheduled inspection items of SO<sub>2</sub> analyzer

Check for abnormality. Perform the specified work. Adjust to specified values. Clean the specified place. Replace designated parts for maintaining the performance. â

# (6) Measurements

Table 4-7 summarizes the effective measuring hours except those spent for calibration as well as equipment troubles. The figures at all measuring points are thought longer than a guideline figure required for the effective monitoring station in Japan, i.e., 6,000 hours (cumulative).

Station	Effective measurement (hours)	Availability(%)
MS1	8,684	98.9
MS2	8,515	96.9
MS3	8,502	96.8
MS4	8,562	97.5
MS5	7,225	82.3

#### Table 4-7 Effective measuring hours of atmospheric SO2 concentration

(Remark: Total hours for Jan. 17, 1988 through Jan. 16, 1989 is 8,784 hrs.)

The causes of trouble that each monitoring station had were listed in Table 4-8 together with measured variables. Among them, the largest downtime in case of  $SO_2$  measurement, was caused by the dew drop formed inside the manifold and brought into the instrument. The troubles in photomultiplier and power failure follow as second and third largest single reason respectively.

Table 4-8 The causes of instrument downtime during the long term survey

	· · ·	· · ·				<u> </u>					<u>.</u>
	Missing cause	501	SPR	30	501	i	i dissing cause	201	Sra		301
	For calibration	-8	13	53	- 59		For calibration	- 35	14	- 68	68
	For maintenance	13	7	11	<u>u</u>		for azintenance	9	6	28	28
	Electric power out	- 38	35	41	49	i i	Electric power out	81	62	76	76
	Over-current					i	Over-current				ļ
	Dutlying value		L		1	1	Dotlying value		1		<u>i</u>
	Calibration error			49	19	1	Calibration error		1	303	303
75-1	Maintenance error					:6-4	Maintenance error		3.		1.1
	Poor indication				Ì		Poor indication	9			<u> </u>
	Temperature rise by air-conditioning				ł		Temperature rise by air-conditioning		· ·	10	to
	Kater condensation of manifold	<u> </u>			\	•	Water condensation of ashifold		109		<u> </u>
	Out of order of air-conditioning				1		Out of order of air-conditioning	67	67	718	718
	Nechanical trouble by water		23				Pechanical trouble by water				i i
	fechanical trouble	1	307	53	- 56	· ·	Techanical trouble		20	487	484
	Total	100	385	225	224	<u> </u>	Totai	222	230	1690	1687
	For calibration	57	23	- 56	56	Į	For calibration	: 32	12	- 60	60
	for mintenance	15	10	_15	<u>l 15</u>	)	For maintenance	8	7	_ 10	1_10
	Electric power out	164	134	140	140	Ì	Electric power out	159	185	192	192
	0/er-current		[		<u> </u>	[	Over-current	28	28	28	23
	Dutlying value		3		<u> </u>		Outlying value	399	3		L
	Galibration error	8		467	- 584		Calibration error	94		121	121
-S-2	Maintenance error			1.	<u> </u>	rs-s	Taiatesance error			211	211
	Poor indication		- 1		L	j	Poor indication			6	6
	Temperatury rise by air-cooditioning			21	21		Temerature rise by air-cooditioning				
	Hater condensation of manifold		125		Í	[	hater condensation of zanifold		6		<u> </u>
	Out of order of air-conditioning			49	49		Out of order of air-conditioning	143	149	149	149
	Sechanical Irouble by water				<u>į .</u>	Į ·	Nechanical trouble by water	495	70		
	Nechanical trouble	24	68	156	i 155	j –	Nechanical trouble	137	2	÷	1
	lotal	259	363	904	1021	<u> </u>	Total	1559	462	1143	1144
	For calibration	33	. 9	- 39	33		For callbration				
	For maintenance	12	17	· 31	31	]	For maintenance				
	Electric power out	56	31	31	35		Electric power out				
	Over-current			1		<b>)</b> .	Over-current				1
	Outlying value		5	117		} .	Outlying value				
	Calibration error			70	70		Calibration error	1.1			
NS-3	Malatenance error		23	44	44		l'aintenance error				
	Poor indication	· · ·					Poor indication			I	
	Tesperature rise by air-conditioning	·					Temperature rise by air-conditioning				
	Rater condensation of monifold					]	Hater condensation of manifold				<u> </u>
	Out of order of air-conditioning						Out of order of air-conditioning		.		
	Mechanical trouble by water						Nechanical trouble by water				
	Mechanical trouble	181	108	1772	1750		Nochanical trouble		[		
	fotal	282	205	2110	1979	l .	Total				

The hourly values of SO<sub>2</sub> concentration at each station are listed in the Data File chapter as shown by an example of Table 4-10. A summary of SO<sub>2</sub> measurement is shown in Table 4-9 which shows measurements of all stations satisfying the require ment set by Standards (daily average;  $0.3 \text{ mg/m}^3=0.117 \text{ ppm}$ , geometrical yearly mean;  $0.10 \text{ mg/m}^3=0.039 \text{ ppm}$ ). The detail discussion must resort to the separate part.

Station		MS1	MS2	MS3	MS4	MS5
Effective measuring time	(days)*	362	354	352	360	296
Yearly average	(ppb)	7	12	24	5	3
Geometrical yearly mean	(ppb)	. 4	8	16	- 3	2
Peak hourly value	(ppb)	109	112	199	79	- 48
Peak daily average	(ppb)	23	34	71	20	21
Daily average (98%) value	(ppb)	19	30	60	14	- 8

Table 4-9 A summary of SO<sub>2</sub> concentration measurements

(\*Effective measuring day means one in which hourly value is measured over 20 hours per day.)

# Table 4-10 SO<sub>2</sub> concentration measurement data (an example)

11

PAGE

										•				1011	11.1	(210)				•••									
	1	988Y8	BOYEAR.		10×1	н			Ŧ	LEN	(101)		50Z		ST. ( )) (MSL) OKEB							STATIO	STATION (PP8)						
HOUR Day	1	2	3	. 4	5	6	7	8	9	10	n	15	13	14	15	16	17	18	19	20	21	22	23	24	нін	мах	AVE	HOUR	TOTAL
1 2 3 4 5	4 3 9 6	3 3 3 9 6	3 3 3 5 6	3 3 5 8	3 3 4 7 11	4 3 3 7 6	3 3 3 7 15	8 .3 3	3 -2 9 10	3 3 4 7 8	5 3 5 5	1 3 4 5 11	2 3 6 8	2 2 1 6 10	2 2 8 8	2 3 2 9	2 3 4 9	7 6 8 7 7	8 7 8 9 8	9 7 8 7 10	8 8 9 11 10	4 6 9 10 7	3 4 8 13 10	43977	1 2 1 5 6	9 8 9 13 21	4 4 5 8 9	24 24 24 24 23	515
6 7 8 9 10	13 10 4 8 10	12 12 6 8 11	14 16 5 7 10	9 13 5 7 9	8 9 6 7 18	6 8 4 6	5 5 8 6	6 5 6 10 6	6 5 8 11 14	7 6 7 8	13 14 7 7 8	22 17 7 7 5	10 15 7 6 5	9 12 7 7 6	11 10 7 7 7	11 10 9 8 7	10 14 10 7 6	11 17 6 7 8	10 14 9 7 13	12 13 11 9 10	7 10 10 10 11	9 9 11 7 11	8 9 9 7	8 5 13 10 6	. 5 4 5 5	22 17 13 11 18	10 11 7 8 9	24 24 24 23	176 187 202
11 12 13 14 15	5 22 14 13 3	8 15 11 6 5	5 27 9 6 4	6 9 15 8 5	7 21 14 8	6 13 15 6 8	5 15 15 4 7	6 18 15 7 10	5 12 8 12 0	6 11 9 7 7	6 9 7 6	7 4 7 4 3	9 6 3 3	8 5 5 4 4	9 21 7 4 5	11 27 6 7	9 26 5 6	18 29 9 8 5	14 30 8 5 4	13 28 7 5 6	25 24 11 6 18	13 10 9 13	5 13 9 5 8	7 7 11 6 7	5	25 30 15 13 18	9 17 10 5 7	24 23 24 24 24	231 152 158
16 17 18 19 20	8 12 3 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	6 8 10 4 4	5 9 4 3	5 7 5 3	5 6 11 5 4	4 9 22 7 4	5 5 15 5 4	4 7 12 6 8	4 7 12 5 5	5 7 10 3 4	5 9 8 3 3	5 11 5 5	4 7 4 1 8	4 9 3 2 6	5 3 2 7	5 8 3 2 8	6 2 2 7	5 3 2 5	72544	7 3 8 7 7	8 5 10 8 8	9 7 10 5 9	11 10 7 2 7	14 15 2 4	4 2 1 2	14 14 22 8 9	- 6 7 8 4 5	24 23 24 23 24	196 89 129
21 22 23 24 25	2 7 11 11 5	4 6 7 5	45474	3 6 7 10	3 6 7 6 8	- 3 6 7 7 7	5 7 14 7 5	7 8 19 8 9	24 7 12	4 6 11 5 7	3 4 6 6 6	3 5 4	3 3 5 4 5	4 3 5 6	443777	44376	4 3 4 8 8	3 4 10 9 5	4 7 34 9	19 24 34 10 5	20 31 73 8 6	15 42 47 5 4	11 28 41 5 6	9 19 21 5 8	2 3 4 4	20 42 73 11 12	6 10 17 7 6	24 24 23 24	400 141 152
26 27 28 29	9 8 4 3	10 5 6 4	10 9 8 6	9 8 7 8	6 6 5 5	5 6 6	5 3 5 6	8 6 4 8	10 11 4 7	6 9 1 5	10 7 4 5	6 4 5	5 4 6	8 5 4 4	7 5 4 5	6 5 6 5	7 4 4 6	5 4 3 5	4 5 4 6	5 6 8	5 7 6 6	10 8 4 5	9 8 6 6	12 2 3 7	3 3 3	12 11 8 8	8 6 5 6	23 24 24 24	150
N1N	z	3	3	3	د	3	3	3	2	3	3	1	1 15	1 12	2 21	2 27	5 2	2 29	2 34	3 34	5 73	47	2 41	2 21	1	73			
MAX AVE	22	15. 7		15	21 7	22 7	15	21 8	24 B	31 6	11 5	22 6	5	5	د <b>،</b>	7	7	7	9	10	13	11	9	8			8		
HOUR	29	29	29	29	59	28	ż9	29	29	29	28	27	27	29	28	29	29	29	29	29	58	29	29	29				689	6286
101AL	ź17	200	204	195	215	193	500	241	237	185	178	172	145	158	173	198	193	217	253	305	379	317	275	230					5285

\*\*\*\*\*\*\*\*\*\* HONTHLY REPORT \*\*\*\*\*\*\*\*\*\*

### 4.1.2 Measurement of NO<sub>2</sub> atmospheric concentration

In order to investigate the status of pollution by  $NO_2$  concentration at Samut Prakarn Industrial District, five monitoring stations were placed within the territory where the hourly averages of both NO and  $NO_2$  were monitored for one year period by using instruments of automatic and continuously driven type. The instruments were subject to weekly calibration and to the scheduled maintenance once every three months.

## (1) Measuring instruments of atmospheric NO<sub>2</sub> concentration

The proposed methods for measurement of atmospheric nitrogen oxides (NO and NO<sub>2</sub>) can be mainly grouped into two types, Absorption spectrophotometric method which uses Salzman reagent (wet method) and Chemiluminescence method (dry method). The former is widely in use in countries like Japan, West Germany, South Africa and Italy, whereas the latter is employed by such countries as France, Netherlands, Taiwan, Korea, Singapore, Australia, Canada, United States and others.

# (2) The $NO_x$ analyzer used in this project

The type of analyzer used in this survey is one of Chemiluminescence type, which detects chemiluminescence as the result of NO and  $O_3$  reactions as shown below or continuously the NO concentration since the luminescence intensity is proportional to the concentration of NO.

 $NO + O_3 = NO_2 + O_2$  .....(4-5)

 $NO + O_3 = NO_2^* + O_2$  .....(4-6)

 $NO_2^* = NO_2 + h \nu$  .....(4-7)

Namely, NO in the air reacts rapidly with  $O_3$  to form  $NO_2$ , the part of which, say, about 10%, takes the excited state,  $NO_2^*$ . When this  $NO_2^*$  transforms into  $NO_2$ , the ground state, chemiluminescence is emitted with the wavelength between 600 and 2,500 nm (as shown in Figure 4-5). The spectra of ray is then detected by a photomultiplier tube. In other words, NO is measured indirectly in term of chemiluminescence intensity. Accordingly in order to measure the  $NO_2$  concentration, the system needs a converter to change  $NO_2$  into NO. The  $NO_2$  value is thus thought equivalent to difference of  $NO_x$  (NO+NO<sub>2</sub>) and NO. The converter works to convert the  $NO_2$  of sample air stream into NO and makes it possible to measure the total NO of both  $NO_2$  origin and originally existing portion.

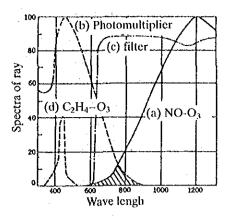


Figure 4-5 The chemiluminescence characteristics of NO-O<sub>3</sub>

The instrument applied in this survey is one of chemiluminescence types, GLN-31 manufactured by DKK Corporation, which is featured by a capacity of measuring both NO and  $NO_2$  by letting the sample air every 20 minutes through the converter and of giving the continuous output of both measured data.

The system also intakes the air intermittently every 4.5 minutes, thereby arrests chemiluminescence and detects the dark current of the photomultiplier as the major source of noise signal, which is stored in the system memory.

The stored information is then utilized to minimize the drift of zero point and to stabilize the measuring conditions. The recording part of the instrument stores both instantaneous and hourly average concentration values of NO and  $NO_2$  and has external I/O terminals and an external output connector, both of which serves to transmit hourly measured values to the data logger.

The instrument is also equipped with an automatic range switching mechanism as such is same case with GFS-31 type  $SO_2$  analyzer. Specifications of the analyzer are shown in Table 4-11, the measurement system diagram in Figure 4-6 and the mechanical structure of analyzer in Figure 4-7.

#### Table 4-11 Major specifications of NOx analyzer

Name of product:

Model: Object components: Measurement principle:

Measurement range:

#### Indication:

Repeatability: Zero drift: Span drift: Response time: Ambient temperature: Power requirements: Power consumption: Dimensions:

Weight:

Color painting: Input/output signals:

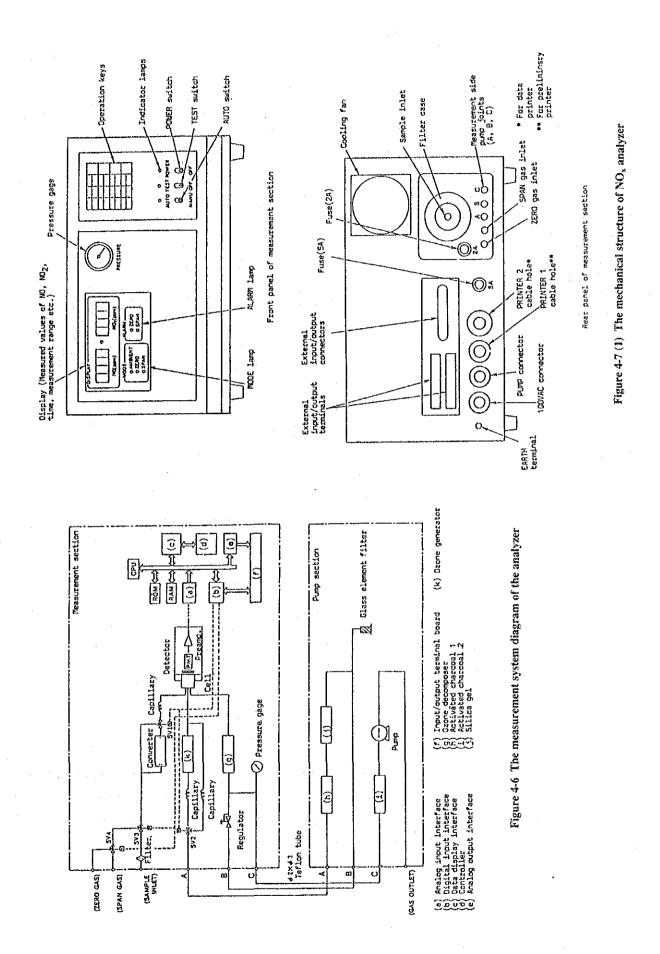
Atmospheric nitrogen oxides analyzer GLN-31 Atmospheric NO, NO2, NO<sub>X</sub> Chemiluminescence, continuous measurement Instantaneous value 0-0.1, 0-0.2, 0-0.5, 0-1, 0-2, 0-5 ppm. Manually switched 6 ranges. ranges for NO,  $NO_2$ ,  $NO_X$  can be set independently. Hourly average value (Saw-tooth record) 0-0.1, 0-0.2, 0-0.5, 0-1, 0-2, 0-5 ppm Automatically switched 6 ranges. Instantaneous values of NO and NO<sub>2</sub> (Simultaneous indication) Within  $\pm 2\%$ FS Within ± 2%FS/day Within ± 2%FS/day Within 3 minutes for 90% response 0-40℃ 100VAC 50 and 60Hz 25074 Measurement section 430(W)x595(D)x270(H) mm Pump section 240(W)x250(D)x280(H) mm Measurément section 32 kg Pump section 7.5 kg Munsell N4 and N7 Transmission output 0-iVDC (Isolated from input), instantaneous and hourly average values of NO,  $NO_2$ ,  $NO_3$ Contact output signals O Measurement range signal (Instantaneous and average values of NO, NO<sub>2</sub> and NO<sub>x</sub> independently) O TEST (under adjustment) signal O Blown-fuse signal O Under-calibration signal (optional) O Automatic-calibration-impracticable signal (optional)

<u>Contact input signal</u>

O External reset signal

O Observatory (station) stop signal

O External starting signal of automatic calibration (optional)



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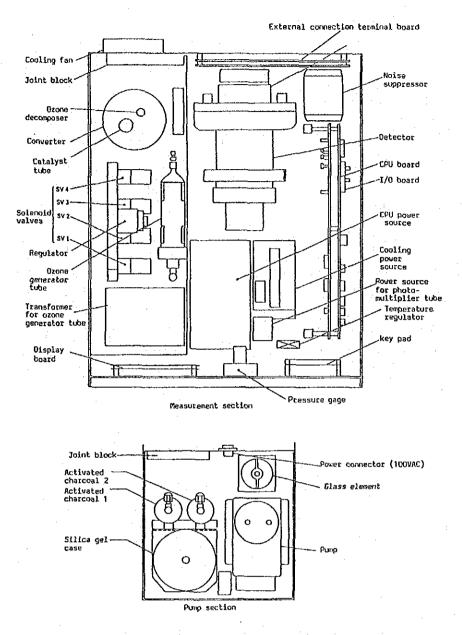


Figure 4-7 (2) The mechanical structure of NO<sub>x</sub> analyzer

# (3) Measurements

The instrument is designed such that operations like calibration, automatic calibration, time adjustment, etc., can be selected by actuating the key panel on its front. The detail description of key operations resorts to the brochures written both in English and Japanese but operation modes available are briefly shown in Table 4-12.

# Table 4-12 Operation modes of the NO<sub>x</sub> analyzer

Operation its	4	Xeying procedure	Reatiks
(I) 194	Juliling	IDE S.f. Det Press (Al her when the present them have been been ally the registered figures.	
	<b>N</b> octrig	IN East ( C Related by pressing C key, and singler )	
(2) Into po Setter- Action		U C Aland by perily ( by.)	
(3) tom per later- Artion		State of the second state	
[4] Sem witting return	trilling	SH. 2.7. Lo-to Drif (Wist about 1 mcous, display returno to their shulletter.)	
	Reality	Str. Day (C Balanad by providing C kty.)	
(5) Time of milamplic calibration	Walling	EA.1. A.f	
	Reacting	Mail (or) { C failment by perioding C tay.)	
(6) Period of min- solide collibration	Witsing	R.f.         Boff         Our By pressing to ber, slipping           i-s         Boff         our by constrained to second ration both           ct(or.)         tothory         tothory	
	feolSrg	The Lat ( C Malened by periods ( by))	
<li>(7) Somering runtur of Wys</li>	Hilling	Inter wood 1 second, stretter reported	Parface willing eft Auto-Calla-Parton willing procedure,
	<b>Dadirş</b>	ter or i a falmed by permity ( by.)	
(8) Arrant Marting of advention tailors- tion			kil silet eni b ja MR pullin.
(9) Anixement (args.		NO 2005 25 10 101	Bylsteins flyters 6,1, 9,2, 8,5, 1,6, 1,6, 3,4
		NO, ME DE M. DT	ning and Jogtunianicus estus Jogtunianicus estus Jogtunia hy tomós Jographi estilizón iti
		101 mt 10 1.7, per	In the cargo of 15 log of each starp tope, Mine they
		Average sclaw Average Add Hote S.T. Det	range is adouting by sellend.
		KO, MERINE V, DA	
		NOs Bec Hon Br #J. Dr	

uperation	fies	1 .	Keyin	e procedu	re .	Reuseks
(10) Provinsion Ing		Bigleten BADA vi Diwley	Igaret CO	05 500 500	10 1000 1000	itti adlek in Kli politin (D), politin (D),
(11) Coolfacture	Acading	Alla prà HOg men con della prà Span consetta rella csilient prioters 2) Zere consetta	(liciant, (typen) an Azes at0) (liciant, (typec) an Azes at0) an coefficient in an Son (typec) an at1s an coefficient is and low (typec) an at1s claray			
	W115-W	printer of	iciani (Systal en de 19) Ticiani (Systal en 18ciani (Systal en 14cianiz)			

# (4) Calibration

Prior to calibration, the zero gas generator and the cylindered standard gas (with about 4.5 ppm NO content) supply source are connected to the instrument and then front key panel is actuated to complete the zero point/span corrections. The cylindered standard gas in use is one inspected by Chemicals Inspection & Testing Institute, Japan and has a guarantee period of a half year for its concentration. Therefore the standard gas required the replacement every half a year during the survey period.

# (5) Inspection and maintenance

In order to maintain the desirable condition of the  $NO_x$  analyzer, it was subject to various inspections and maintenance jobs as listed in Table 4-13 in which weekly and monthly ones were dependent on ONEB and others were performed jointly by ONEB and Japanese staff.

$\left( \right)$		Maint	enance object i	itena		Int	etva	1		Reference section
		Item	Action	Osscription	heak	Month	3 months	6 aonths	Year	
1	Fice pa	h tubing	Check	Fouling, buckling, disconnection, leak		0				
		i a tr	Replacement	Each tube	Ŀ					
			Leak	Leak test			0			
2	Filter case	Element (PF )	Replacement	Replacement by a new one	a					7.2
		Filter case	Cleaning	Joint, case interior			Δ			· · ·
				· · · · ·						
3	Glass el	ement of pump	Cleaning	Glass element			Δ			7.3
			Replacement	Replacement by a new one						
۵.	Suction section	pump in pump	Check	Strange sound, strange vibration		0				
				Normal pressure	Ő					
			Cleaning	Diaphragm, valve, joint			Δ		•	7.4
			Replacement	Replace disphragm and value by new ones					o	
5	Solenoid	j valve	Check	Strange sound, strange chattering sound		0				7.5
	<u></u>		Replacement	Replacement by a new one			:		a	
6	Convert	T .	Replacement	Replace catalyst.					α	7.6
7	Ozona de	composer	Replacement	Replace catalyst.						7,7
8	Ozone gi	merating tube	Cleaning						Δ	2
9		el in pump	Check	Color change to pink	0					7.8
	section		Replacement	Replacement by a new or rejuvenated silica gel						
10		ed charcoal 1, 2 section	Replacement	Replacement by a new charcoal						7.9
11	Cell		Cleaning	Cell window, cell wall		·			Δ	7.10
12	Callbra	tion	Calibration	Zeto, span	0					4.5
13	Clock		Check	Check for time shift	ō					4.1(5)
14	Capilla	cy	Cleaning	Interior cleaning				Δ		
			Replacement	Replacement by genuine DKK parts					0	
15	External	l pipings	Check	Fouling, buckling, disconnection, leak		0	÷			2.3
			Replacement	Replacement by a new pipe					П	
16	External	connections	Check	Looseness, breakdown		0		_		2.4

Table 4-13 Inspections and maintenance jobs of NOx analyzer

O : Check for any abnormality. Take specified actions. Adjust to specified values.

 $\Delta$  : Clean specified places.

 $\Omega$  \* Replace specified parts for maintaining the performance of the analyzer.

# (6) Measurements

The effective measuring hours of both NO and  $NO_2$  contents at each station are shown in Table 4-14. All of them satisfy the minimum requirement hours stipulated for an effective monitoring station in Japan.

Station	Effective me	asuring hours	Availab	ility(%)
Station	NO	NO <sub>2</sub>	NO	NO <sub>2</sub>
MŞI	8,559	8.560	97.4	97.4
MS2	7,880	7,763	89.7	88.4
MS3	6,674	6,805	76.0	77.5
MS4	7,094	7,097	80.8	80.8
MS5	7,641	7,640	87.0	87.0

Table 4-14 Effective measuring hours of NO and NO <sub>2</sub> at each stat	and NO <sub>2</sub> at each station
---	-------------------------------------

Total hours for the period of Jan. 17, 1988 through Jan. 16, 1989 is 8,784 hrs.

As for causes of analyzer troubles, the breakdown is listed in Table 4-8, which indicates a single largest reason for analyzer downtime is the trouble of photomultiplier and the second and third

causes are found wrong calibration and power failure respectively. The hourly readings of NO<sub>2</sub> and NO<sub>x</sub>(NO + NO<sub>2</sub>) at each station are as exemplified in Table 4-16 or more thoroughly in Data File Chapter. The analytical study result is discussed in Part III as well. The summary of measurement results in Table 4-15 shows that the concentrations observed in all stations satisfy the value required by Standards (Hourly value;  $0.32 \text{ mg/m}^3=0.173 \text{ ppm}$ ).

Station		MS1	MS2	MS3	MS4	MS5
Effective measuring days	NO <sub>2</sub>	354	316	276	289	315
	NOx	354	316	270	289	315
Yearly average (ppb)	NO <sub>2</sub>	16	9	13	15	5
	NO <sub>x</sub>	38	18	24	34	9
Geometrical annual mean	NO <sub>2</sub>	12	6	10	10	3
(ppb)	NOx	23	14	18	22	6
Hourly peak value (ppb)	NO <sub>2</sub>	138	69	81	150	48
(ppb)	NOx	497	132	251	343	127
Day average peak value	NO <sub>2</sub>	49	32	41	69	16
(ppb)	NOx	176	56	75	180	36
Day average 98% value	NO <sub>2</sub>	33	20	30	46	14
(ppb)	NO <sub>x</sub>	112	4()	62	105	25

An effective measuring day is one which obtains more than 20 hourly values.

# Table 4-16 NO<sub>2</sub> concentration measurement results (example)

										1		****	•	нон	INLY	8690	១១ វ											PAGE	- 13
	1	988Y	EAR	2	40×1	н			i	ĨĒĦ	(103		ж02						5	it. (	t	1) (	HS1)	<b>ONE</b> 8	STATIO	N	G	>60)	
DAY DAY	3 1	2	. 1	4	5			76	9	10	• •	15	12	5 14	15	12	17	18	19	20	2	55	23	24	MIN	нах	344	HOUR	TOTAL
1 2 3 4 5	1 3 2 6 2	2	2 3 4	3	3	. 4	ť	9 9 1 12	7 9 7 5 6	5 7 2	2	2	10		11 10 5	17 9 7	22	22	19 11 5	10	10	10 7	10 9	4 9 7 2 5	1 2 1 2 1	11 22 11 12 21	6 9 5 7	23 24 24 24 24 23	133 224 133 120 168
6 7 8 9 10	5 10 5 4 8	8	20	19	14 5 5	.12 S 8	1	2 10 0 13	13 8 9 15	75	15 5 3	19 8	14 5 4	12	8	9	12	16	14 5 5	16 6 6	10	16 5 11	8 10 5 9 15	8 5 4 9 13	5 5 4 3	19 20 13 17 18	10 13 6 7 10	24 24 24 24 15	239 302 150 157 145
11 12 13 14 15	18 7 22 10 5	24		10 21 7	21 27 7	25 29 7	20	31 29 29	13 27 21 26 12	10 18 12 7	12	۰۰۰۰ ۵ ه	**** 8 8	19 7 6	39 8 8	4 44 7 9 12	49 B 10	55 11 8	(9 16	(0 13 9	28 17 15	17 16 15	4 18 11 7 15	4 9 12 6 28	3 7 6 5	18 55 29 29 28	9 27 16 10 10	24 22 24 24	208 595 381 247 231
16 17 18 19 20	28 8 29 17 11	24 7 28 19 9	20 8 24 18 11	6 24 19	4	11 8 24 27 15	23 23 22	19 28 24	15 20 24 16 17	19 17 27 7 11	15 19 7	10	5 9 7 7 25	5	6	5 58 6 28	8 5 6	6 10 7 7 11	8 10 29 40 18	10 42	17 39 55	28 32 37	10 30 27 15 32	9 28 20 11 12	5 5 5 9	28 30 42 58 60	12 14 21 20 24	24 23 24 23 24	285 321 507 456 566
21 22 23 24 25	15 39 44 20 6	18 29 24 11 7	15 28 18 10 7	28 30 9	13 33 20 8 7	20 25 20 9 8		40 36 14	16 36 46 9 18	9 16 34 7 10	7 9 14 5 8	5 11 6 8	6 6 7 8 10	6	8	7 7 6 10 12	8 9	8 1D 39 15 6	26 32 71 19 8	70 69 75 14 7		85 66	54 79 52 7 6	46 63 25 6 7	5 6 5 5	70 85 75 20 18	23 33 32 11 9	24 24 24 24	557 780 748 254 218
26 27 28 29	11 3 4 2	11 4 6 8	14 4 8 7	 	13 11 5 4	10 11 5 7	12 9 13	14 11 8 16	15 16 8 7	7 9 5 3	17 7 5 6	9 6 3 6	4 6 9	17 4 5 3	12 6 6 4	9 5 5 5	5	5 5 5 5	5 6 5 10	5 7 6 9	6 7 5 7		5 4 7	5447	5 3 2	17 16 8 16	10 7 5 7	23 24 24 24	226 159 129 161
M1N	1	1	1	1	1	4	7	8	5	ş	, s	2	1	2	3	. 4	4	3	5	6	5	4	4	z	۱				
MAX	44	29	26		33	29	36		46	34	53	30	25			44	49	55	71	75	83	85	79	61		85			
AVE Hour	12	11 29	11 29	10 29	12 29	12 28	16 28	19 28	16 28	10 28	9 27	9 25	8 26	8 28	9 28	· 10 29	10 29	11 29	16 29	21 29	21 29	20 29	16 29	13			13	680	
TOTAL	3(3	324	47 312	303	335	332	434	535		281	241	222	200	533		297	294	315	470	612	614	575	408	370				000	8818

# 4.1.3 Atmospheric concentration measurement of suspended particulate matter

In order to grasp the pollution status quo by the suspended particulate matter, five monitoring stations were installed across the Samut Prakarn Industrial District and hourly SPM average concerations were measured. The calibration and scheduled inspection are practiced once every month and once every three months respectively.

# (1) SPM measuring method

There are basicly six groups of method proposed for the measurement of atmospheric particulate matter concentrations as shown in Table 4-17. Among them, types of analyzer that allow the automatic measurement of hourly values are Digital particulate meter,  $\beta$ -ray absorption method, Piezoelectric balance method. Each of these six methods has good and bad points and varies in measured diameter of particulate matter. Accordingly which method to be employed depends largely on various conditions of the country. In Japan, the total suspended particulates (TSP) is defined as dust suspended in the atmospheric air and the portion of such dust in diameter less than 10  $\mu$ m is called Suspended Particulate Matter (SPM). The implication of this definition is that such SPM can deposit inside the human lung and influence his respiratory organs. Thus the control standards was set for the SPM concentration in the air and simultaneously the Low volume air sampler with a sorting device for 10  $\mu$ m size particles is employed as standard method. But this method is not suitable for a short term measurement. To cover this weakness of Low volume sampler, Piezoelectric balance meter and  $\beta$ -ray absorption type dust meter are added as standard methods to make hourly measurement possible.

## (2) Dust meters applied to this survey

The type of dust meter used in this survey is a  $\beta$ -ray absorption meter suitable for the measurement of hourly SPM concentration. The beta-ray analyzer is an instrument based on the principle that absorption rate of beta-ray increases in proportion to the mass of the substance when its quality remains constant and the ray at a low energy level irradiates the substance. Thus the beta ray irradiation on the particulate matter collected on the filtration paper gives informations about its quantity.

The relationship between intensity of beta-ray transmitted and dust quantity is expressed by the following equation

$$I = I_0 \exp(-\mu m \cdot Xm) \qquad (4-8)$$

where;

I : Beta ray intensity transmitted through filter and particulate matter

 $I_o$ : Beta ray intensity transmitted only through filter

 $\mu$ m : Mass absorption coefficient (cm<sup>2</sup>/g)

Xm : Mass of particulate matter  $(g/cm^2)$ 

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### Table 4-17 Classification of measuring method of atmosphere particulate matter concentration

Monitoring method	Monitoring Instrument	Principle	Size range	Remarks
Filter contami- nation method	Smoke sampler (OECD method)	o Suck air through white filter. Uaually 24 hours. Contamina- tion of littler is measured by reflection index matter. Value is converted to international smoke unit (ug/ng). Simple mechanism and filted to continuous monitoring	0 to 20-30 µm	o Widely used in European countries. Method recommended by OECD. Afr auching speed is low and ascuple is limited to inhalable particles. The results of monitoring is influenced by black color substances, and not indicating real weight. Limited range of chemical analysis is possible even by small quantity of sample
	Tape sampler (ASTM method)	o Sams with OECD method. Sample collected on filter automatic- ally forwarding with 2-6 hours interval. Contamination is evaluated by transprancy index and expressed by hase unit (COH) usually, but some cases, by tellection index (RUDS)	0 to 40 µm	o Flow rate is larger than OECD mathod. Ellective sampling of inhalable particles is possible by method employed in USA. Fitted for continuous monitoring.
Filtration sampling method	High volume asmpler	<ul> <li>Air is sucked through glass fibre filter usually by turbine blower. Collected stample is weighed under constant tempera- ture and humidity. Most widely used and in West Germany membrane filter and rotary pump are employed.</li> </ul>	0.1 to 80-100 yes	o Widely used in USA. Particu- late larger than inhalable particle is apt to be collected, and not fitted for monitoring in dirty places. Sampfing is usually for 6 days with 24 hours cycle. Obtain- able enough sample for chemical analysis.
	Low volume samplet	o Principle is same with high volume sampler, but flow rate is far samiler and designed to be fitted for long term air sucking.	0 to 20-30 µm	o Flow rate is smaller than high volume sampler and possible to sample inhiable particles effectively. In Japan, used with cyclon type separator to multi-stage separator to cut the particles larger than 10 microns.
Light scattering method	Digital dust analyser	o By light scattering, directly measure particulate as aerosol. Individual particles are counted and measure particles size or integrate the scattered light from a certain volume of air.	0,5 to 10 µm	o Used as monitor of SPM in Japan In some extent. But catibration is alwaya necessary and evaluation impossible to compare with direct weight method.
Beta ray absorption method	Beta ray absorption mass monitor	o Particulate matter is collected on filter for a certain time (usually 30 min.) continuously. Beta ray icrediated and a part of energy is absorbed, Weight conc, is determined by Beta ray intensity transmitted,	0 to 20 µm (filter system)	o Instrument cost is usually expensive. In West Germany, used for monitoring. Important instrument to study short time variation of particulate.
Piero balance method	Piezo balance mass monitor	o Based on piezo oscillator method. The weight of particles accumulated on oscillator proportionally change by vitration number, and weight conc. is determined by this relation.	0.01 to 10 pm (electrostatic system) 0.3 to 20 pm (impactor system)	o This method is high sensitive, but defects in electrostatic collection index and impacts of humblity to sample. Detection of weight without removing substances accumu- lated on quartz is limited.
Particle separating method	Cascade impactor	o Particulates are classified into several stages by impac- tion. Weight of each substance is directly weighed.	0.5 to 20 μm	o Conc. in certain range of particle size is evaluated. Used in USA but not widely used.
	Dichotomos sampler	o Known as vertical impactor. Particulate is separated to 2 size range and each particle is collected on filter and weighed.	0 to 30 µm	o Used in USA for monitor of sulfate. Under consideration to be used for monitoring particulate matter in USA.

From the equation (4-8), the mass of particulate matter is calculated as

 $Xm = 1/\mu m \ln(I_o/I) \dots$ 

(4-9)

Also the concentration of particulate matter is expressed as

$$C = S/V \cdot Xm \times 10^{3} = (S/V) \cdot (1/\mu m) \cdot \ln(I_{o}/I) \times 10^{3} \dots (4-10)$$

where;

C: concentration of particulate matter (mg/m<sup>3</sup>)

S: collection area (cm<sup>2</sup>)

V: air aspiration volume  $(m^3)$ 

The type of dust meter used in this survey is a beta-ray absorption one, DUB-12 type manufactured by DKK Corporation. This dust analyzer aspirates the sample air at a fixed rate of 18 liter/ min through a cyclone sieve and traps the airborne SPM by a glass fiber made filter which is then irradiated by the beta-ray to measure the transmitted intensity. The mass concentration (mg/m<sup>3</sup>) is calculated through an internal data treatment based on above mentioned principle. The measured hourly average values are simultaneously recorded at each station and are transmitted to a data logger in the central observation center.

The detection part of the instrument is designed as shown in Figure 4-8 such that beta-ray channel and air aspiration channel intersect each other at an acute angle where the filter is placed horizontally. The detection part is thus divided into two parts, above and under the filter level. The beta-ray emitting source (Promethium 147, <sup>147</sup> Pm) is installed in the upper part and the semiconductor detector (silicon valence electron detector) in the lower part. The mechanical design permits blank monitoring, dust collection and its detection at a same spot and the detection error due to the misplacement of filter is minimized. The arrangement is also recommendable for monitoring of low concentration of dust in a high sensitivity and makes it possible to measure instantaneous values of varying concentrations.

The procedures of measurement conforms to a programme time chart shown in Figure 4-9 which covers such operations as filter forwarding, blank monitoring, air flow measurement and completes a series of automatic and continuous operations.

Major specifications of beta-ray dust meter and the flow chart of monitoring processes are shown in Table 4-18 and in Figure 4-10 respectively.

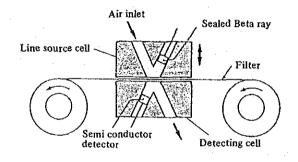


Figure 4-8 The mechanical design of detection part

	····			·			<u> </u>				<u> </u>		
Time - 0.00							1.0	20					
Program step		0		2	3	4~13	14			1	D	1	2
Program item	Source cell swent Filier paper fouding Source cell descent	Actalion Biank rivasuroment		Мезия	rement with (55°32'')	ecration .		Filter paper feeding	Source cell accont	Source cell descant	Avtation Blank firésuccment	Merurement with seration	Meautement with areation
Time	30"	3.28	3'58"	3'58''	3.28.	3.28	3.28.		30.,		3:58"	3'58"	3'58''
Radiation source driving metor													
Filter paper feeding motor motor													
Sampling pump													
Measurement value output				Measusement result of (1) is given as a pulse train output.	Measurement result of (2) is given us a pulse train output output,	Mezsuremanı result of (3)-(12) is given es a pulsa train oulput	Measurement result of (13) Is given as a puise train output.		-	Management result of (14)	is given as a pulse train output.	Copversion value based on measurement result of (1)-(14) is given as output.	

Figure 4-9 The programme time chart

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of
Specifications
Table 4-18

Input/output signals:

Atmospheric nitrogen oxides
·
Atmospheric NO, NO <sub>2</sub> , NO <sub>X</sub>
Chemiluminescence, continuous
measurement
Instantaneous value
0-0.1, 0-0.2, 0-0.5, 0-1, 0-2, 0-5
Manually switched 5 ranges
for NO, NO2, NO <sub>X</sub> can be set
independently.
Hourly average value
(Saw-tooth record)
0-0.2, 0-0.5, 0-1, 0-2, 0-5
· · · · ·
Automatically switched 6 ranges.
Instantaneous values of NO and NO $_2$
(Simultaneous indication)
2 X F S
2%FS/day
2×FS/day
minutes for 90% response
0-40°C
50 and 60Hz
Measurement section
430(#)×595(D)×270(H) mm
Pump section
240(W)X250(D)X280(H) mm
Measurement section 32 kg
section 7.5 kg
Wiinselj N/ sad Ni
lon

Iransmission output O-IVDC (Isolated from input), instantaneous and hourly average values of NO, NO2, NOx Contact output signals

- O Measurement range signal
- (Instantaneous and average values of NO, NO<sub>2</sub> and NO<sub>X</sub> independently) O TEST (under adjustment) signal
  - O Blown-fuse signal
- O Under-calibration signal (optional)
- O Automatic-calibration-impracticable
  signal (optional)
- Contact input signal
- O External reset signal
- O Observatory (station) stop signal
- CExternal starting signal of automatic calibration (optional)

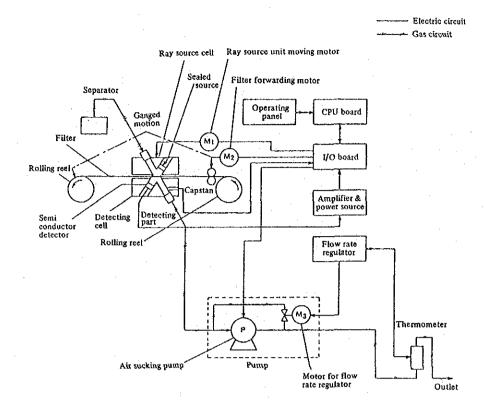


Figure 4-10 The system diagram of beta-ray absorption analyzer

Beta-ray source is Promethium 147 of about 100 microcurie and is designed such that the leakage or permeatation of the radioactive isotope from source container will not cause the environmental pollution problem. It is strictly forbidden to take out the sealed ray source for any reason. In Japan, the qualification, permit and registration are not required for handling such an radioactive substance. Though the half life of Promethium 147 being about 2.6 years, the drift of zero point by time elaspe is small as shown in Figure 4-11 and thus the source can be used longer than 7 years.

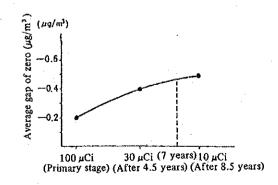


Figure 4-11 The drift of zero point by source intensity

(3) Operations

Operations of the instrument are by the key pannel installed in the front part of the analyzer (as shown in Figure 4-12) and comply with operation modes listed in Table 4-19 which cover automatic monitoring, calibration, time setting, etc. The key operations are described more in detail in brochures Japanese and English.

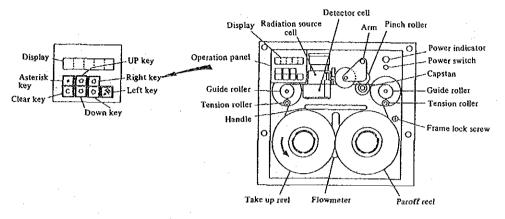


Figure 4-12 Operation board of front part

		· ·
Indicater	Mode	Objective
00-00	Automatic monitor	Normally indicating time (flash 1 sec) alarm signal indicating at abnormal
	of time mode at a second I	
	Manual handling	Moving ray source, filter forwarding, ON/OFF of pump, flow rate regulation
	Equivalent membrane value	Recording and indicating of membrane value
0	Calibration	Blank monitoring, membrane monitor, calibration
GIII	Span coefficient	Recording and indicating of span coefficient
Ø	Time	Time correction and indication
	Month and Day	Correction of month and day
	Year	Correction of year
8: 11	Station number	Recording of station number
<u>e::::</u>	Judgement	Confirmation of ROM, recording of corrected number, printing data, confirmation of installed watch
	Corrected Value A	Recording and indicating of numerical values for zero point adjustment, without changing membrane
<u> [] []</u>	Corrected Value B	Recording and indicating of numerical values for adjustment of sensibility without changing membrane
CIII)	Transmittance test	Output selecting 10 divided sensibility of 0-1000 pulse/hour

 Table 4-19 Operation modes of the dust meter

# (4) Calibration

The calibration of beta-ray analyzer is done as follows;

- (a) Place an equivalent membrane film made of polyamide resin with a premeasured and known blank value on the filter of detecter
- (b) Irradiate and get the membrane absorb the beta-ray and read the output of weight concentration corresponding to the thickness of the film.
- (c) Confirm the equivalent membrane value or correct, if required, such equivalent value by operating the key pannel.

Figure 4-14 shows results of measuring the equivalent membrane value with respect to several types of material. Reviewing the figures, a linearity is found as seen in Figure 4-14 for materials varying in density.

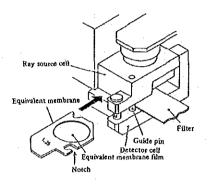


Figure 4-13 Placement of a equivalent membrane

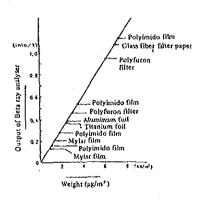


Figure 4-14 The corelation between the output of beta-ray absorption analyzer and the density of equivalent embrane made of various materials.

(5) Inspection and maintenance

The appropriate inspection and maintenance jobs are paramountly important in order to maintain the desirable performance and operation of the analyzer and were practiced as shown in Table 4-20. The monthly replacement of filter, monthly calibration by means of an equivalent membranc and daily inspection were done by ONEB and other inspections jointly by ONEB and Japanese staff.

			liems to be main	tenanced	I	nte	cva	1
No		Item	Action	Description	1 month		6 months	1 year
1	Filter	r paper	Replacement	Replace by a new roll				
2	Cyclor	ne sieve section	Cleaning	Oust trap cleaning		Δ		
		· · ·	Cleaning	Cyclone sieve cleaning			Δ	
2		Olaphragm	Replacement	Replace diaphragm by a new one.				
	dwn u	Sampling pump	Replacement	Replace or overhaul the pump.	-			
	pling p section			· · · · · · · · · · · · · · · · · · ·				ŀ
	Sampling sectio							
		Øraid-hose	Replacement	Replace the hose by a new one.				O,
4		nal tubing conne-	Cleaning	Internally deposited dust removal		Δ		н. Т
	tions		Replacement	Replace tubes by new ones.			D	
5	Beta 1	ray source cell	Cleaning	Internally deposited dust removal			Δ	
8	Sampli	ing tube	Cleaning	Inner wall cleaning		Δ		
-			Replacement	Replace by new ones.				
7	Caliba	ration	Calibration	With equivalent (calibration) film	0			
8	Flow 1	rate regulator	Adjustment	Balancing adjustment			0	
9	Flowne	ater	Cleaning	Cleaning of inner wall and float				$\Delta$
10	Flow	ate adjust valve	Cleaning	Cleaning of needle and inner wall				Δ

## Table 4-20 Inspection items of beta-ray absorption dust meter

## (6) Measurement

The effective measuring hours and SPM instrument availability at each station are shown in Table 4-21. The figures show that all of stations satisfy the minimum requirement as effective monitoring station in Japan.

Station	Effective measurement (hours)	Availability (%)
MSI	8,399	95.6
MS2	8,419	95.8
MS3	8,579	97.7
MS4	8,504	96.8
MS5	8,322	94.7

Table 4-21	Effective measuring hours of atmospheric SPM concentration
	at each station

Total hours for Jan. 17, 1988 through Jan. 16, 1989 is 8,784 hrs.

The breakdown of instrument downtime is shown in Table 4-8. The cause for troubles varies from one station to the other, but the mechanical trouble comes first, then comes power failure next.

The summary of hourly SPM values is shown in Table 4-23 and data recorded by each station are presented in Data File Chapter. A summary of SPM measurement is shown in Table 4-22. The analytical study of them resorts to Part III.

Station	MSI	MS2	MS3	MS4	* MS5
Effective measuring hours	348	344	355	350	343
Yearly average $(\mu g/m^3)$	60	56	63	68	43
Geometrical yearly average (µg/m <sup>3</sup> )	46	42	50	49	32
Hourly peak value ( $\mu$ g/m <sup>3</sup> )	477	870	702	605	661
Daily peak average $(\mu g/m^3)$	156	169	157	201	119
Daily average 98% value ( $\mu$ g/m <sup>3</sup> )	130	125	132	162	103

Table 4-22 A summary of SPM concentration measured

An effective measuring day is one when measurements is possible more than 20 hours.

## Table 4-23 An example of SPM concentration measured

										٠	****		• 1	HONT	ILY	REPO	RT	***	* * * *	***						· · ·		PAGE	- 15	
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NOU Day		2	3	4	5	6	7	6	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	H1N	нах	ÂVE	HOUR	TOTAL	
1 2 3 4 5	32 52 38	41 46 48 30 48	40 37	75 84 35	36 26 35	64 23 31	94 35 48		118 41 40	111 30 -51	52 40 86	57 30 70	54 33 52	52 14 50	52	72 40 60	- 93 - 25 - 71	108 40 50	120 58 70	118 75 59	132	85 51 64	96 51 62	117 51 52	21 32 14 25 30	119 132 84 86 94	57 81 42 52 51	24 24	1018 1248	
6 7 8 9 10	61 48 59	45 74 31 40 61	80 52 40	- 91 51 49	71 55 54	100 70 72	118 75 96	128 101 115 140 69	110 67 101	80 41 58	61 33 60	110 48 50	102 40 50	94 25 25	60 40 46	77 45 54	76 57 56	95 49 80	125 54 51	133 57 53	96 48 89	90 51 83	54 41 80		50 25 25	193 133 115 140 110	75 88 52 63 57	24 24 24 24 24	1246	
11 12 13 14 15	60 58 68		179 50		133 98 48	140 120 56	144 103 80	87 101 172 120 144	163 141 118	109 70 50	115 60 47	68 61 56	35 60 51 46 46	78		152 52 52	153 65 63	188 72 59	213 88 63	168 64	90 83	80 72 72	75 71 57		50 45	92 213 172 120 144	62 127 78 64 61	24 24	1488 3037 1861 1525 1466	
16 17 18 19 20	24 83 41	80 30 79 46 60	129	41 131 42	35 91	47 93 76	61 122 69	105 115 150 80 90	110	86 167 40	71+ 138 32	01 31	73 61 51	41		40	31 40 46	38 42	31 52 72	38 94 114	48 110 161	45 76 96 130 187	89 118 55	89 60	24 38 31	105 115 167 161 187	63 61 94 61 84	24 23 24 24 24	1515 1393 2253 1461 2014	
21 22 23 24 25	217 212 222	130	81 110 159	104 93 143	111 86 96	80 99 108	98 170 89	97 115 190 128 140	112 196 73	60 173 61	41 76 47:	68 48	53 53	53 57	83	70 52	71 66 37	84 72 52	115 168	162 303 50	266 392 40	219 296 270 20 33	313 232 -32	285 200 21	46 20		87 129 146 77 50	24 24 24 23 24	2078 3087 3507 1778 1211	
28 27 28 29	39 22	34 26		30 39	43 33	.55 25		81 88 55 113	86 84	40	36 40	18 18	44 35 25 34	34 29	41	31 41	26 33		41 43	43 55	31 45	41	36 24	26	31 16 18 18	81 88 84 113	47 40 38 39	24 24 24 24	1124 962 900 925	
нік	51	59	25	30	26	23	35	55	40	55	51	18	25	14	16	30	25	25	29	37	\$2	50	24	21	14	•				
HAX								, 190 112																		392	70			
NOUR		29						29																			10	693		
TOTAL	1969	1832		1843		1898		5239 Z		1913			406			506 1	1	711	084	2694	856	2618 2	365	216					48368	

## 4.1.4 Measurement of atmospheric concentration of TSP

In order to analyze the pollution status of Samut Prakarn Industrial District area by TSP (Total Suspended Particulate), Low volume Samplers installed in five stations continued the monitoring for one year survey period. The filter placement, its exchange (once every half month) and instrument inspection were done jointly by Japanese and ONEB staff during 1st through 3rd field trips which lasted 15 days each. The same jobs were carried out by ONEB staff for the remaining ten and a half month period. Each monitoring station had two Low volume samplers, one with a polyfluorocarbon filter to assure elemental and ion analyses and the other with a quartz filter for carbon analysis.

### (1) Summary of the investigation

The Low volume samplers were calibrated prior to monitoring service and were brought in each station. Staffs in five groups loaded the filters onto the instruments at 11:00 AM of the measurement starting day and let meters aspirating the atmospheric air at the rate of 10 liters per minute. After the instruments started measurement, staff visited each station twice a day in the morning and in the afternoon and completed recording of data as shown in Table 4-24 as well as flow rate adjustment.

As for weighing of the filters loaded with TSP trapped, they were sent back to Ishikawajima Inspection & Instrumentation Co., Ltd. in Japan and were kept in a constant temp.-moisture bath (thermo-hygrostat) prior to measurement by a chemical balance. The data sheet used is as shown in Table 4-25. The atmospheric concentration of TSP was calculated by knowing both the aspirated air volume and weight of dust trapped by the filter in compliance with the method to be discussed in the succeeding chapter.

Vanilocíne !	SLILION		lastruneat X	•		Filter ¥0.		Tr	ye ol		folyleone Quirks	-  F	erson in thirse			
Kasiloris <b>e</b> F	eriod		. Vorning, Aftern . Vorning, Aftern		ala aia	Tatal Sempti kau	ار ``	·		e Flo	= ALEE ed Voluat		(Q /el=	[ մեի-անյ	lors odjus Ler adjust	la ca
Dile Vaslk Rour Day Via	Flue Veter Scale	Pressure · (unkg)	Counter Votue	Dite		Floe Veier Scate	Pressure (aalg)	مدلع	ater Y	- يەھىلېن	Dute Voath II Dry V	our	Flow Weter Scale	Pressure (maty)	Counter	********
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	6) 1) 6)			É				·			Runchs		N		l	

## Table 4-24 Data recording chart of Low volume sampler

## Table 4-25 TSP recording chart of Low volume sampler

lio:	itering Station		Instrum	ent No.				÷		Cycla		
filter No.	Sampling Period Bonth, Cay, Hour, Hin.	Incubating time before sampling		Total flow rate (m <sup>3</sup> )	Veight before	Weight after sampling	Sampled Volume	Par con	ticala centr. s/m)	e Lit Ien.	ora- Hual. (\$1)	Remark
	frea:											
	To:		 									
	Fron:											
	To:				I	<u> </u>						
	fres:											
	ta:						[	4_				
	Fron:		 		1			_		L		
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	From:	I	 			L		_		L.		
	Ta:											
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	To:									L		
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	1a:							_	····.			
	Fron:					L						
	To:	1	 l		<u> </u>	ļ		4				
	From:	1		_	<u> </u>							
	Jo:		 !			<u> </u>						Ĺ

(2) Instrument

1) Low volume sampler

The instrument is designed such that it can aspirate the ambient air at the rate of 3-25 liter per minute and continuously for the period of a half month in order to trap the total suspended particulate on the filter. The instrument used in this survey (manufactured by Shibata Scientific Technology Co., Ltd. type LT-20) has also a provision to keep the filter holder in a shelter that excludes any influence of rain drops and fallout large size dust particles.

The air aspiration volume is determined by a float type flow meter and a dry-type integrating flow meter attached to the instrument.

Though this Low volume sampler is equipped with a sieve to eliminate the suspended particulate of over 10 micron size before their reaching the filter, the sieve part was removed from the sampler because the objective is not measurement of suspended particulate matter less than 10 micron size, but that of total suspended particulate. The sieve is essentially a multiple horizontal plates arranged in parallel with a small gap between them. When the air passes in laminar flow through this horizontal elutriator, large size airborne particles deposit on the plates as they pass through the clearances while fine dust particles go through with air stream. The penetration rate of the elutriator is calculated by the following Equation (4-11)

$$P(\%) = 1 - \frac{LW \ \varrho g \ d^2}{18 \ \eta \ v}$$
(4-11)

where L =length of plates (cm)

W = width of plates (cm)

N = number of plates

 $\rho$  = density of aerosol particles (g/cm<sup>3</sup>)

g = acceleration of gravity (m/s<sup>2</sup>)

d = effective diameter of aerosol particles (cm)

 $\eta$  = viscosity coefficient of air (poise)

v =flow rate (cm<sup>3</sup>/s)

Figure 4-15 shows the typical example of penetration characteristics of a horizontal elutriator. Particles of 10 micron or over can be eliminated when the sampler LT-20 is used at the flow rate of 20 liter per minute.

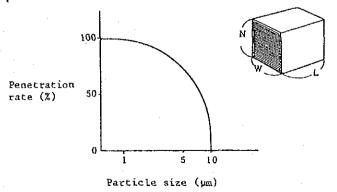


Figure 4-15 The efficiency curve of a multiple plates horizontal elutriator

Specifications of the Low volume sampler used in this study are listed in Table 4-26 and its external appearance in Figure 4-16.

Multistage separator (Elutriator)	: Standard 20L/min
Filter holder	: Holder, for 55¢mm Clip , for 55¢mm 44¢mm (Effective)
Flowneter	: Glass, float type 3 to 32L/min
Integrating gas meter	: Dry type, capacity 0.05 to 59L/min
Vacuum gauge	: 0 to 1000mm H <sub>2</sub> 0
Suction pump	: AC 100V, 50/60Hz, 35W 1.5/1.1 (A) Flow rate 1 to 25L/min
Power cable	: Smm, 7A, with ground terminal
Fuse	: 5A, 6.6 x 30
Dimensions	: 600(W) x 480(D) x 1570(H) mm
Accessories	: Glass fiber filter, ø55 100pcs Milipore AP-200
	Fuse (SA) 1 pc

Table 4-26 Specifications of Low volume sampler

# Driver 1 pc Soft cover 1 pc

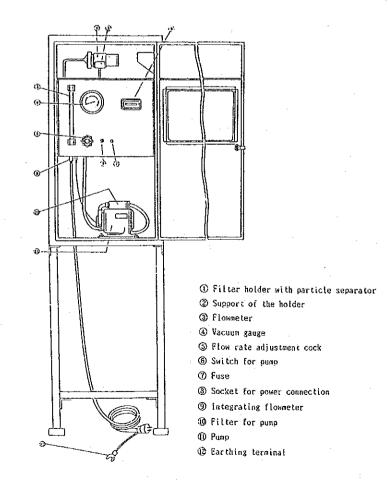


Figure 4-16 The Low volume sampler

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The operation procedures of the sampler are as follows:

- \* The filter is weighed prior to mounting, then placed between the filter holder and adapter and is fixed as illustrated by Figure 4-17.
- \* Prior to the start of monitoring, time and reading of the integrated flow meter are exactly recorded.
- \* At three minutes after the power is on, the flow meter is adjusted at a preset point.
- \* At the end of monitoring, readings of the integrated flow meter, rotameter and pressure gauge are recorded before the power being switched off.

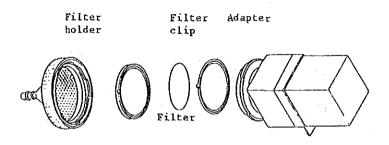


Figure 4-17 Placement of the filter

# 2) Wet-type gas meter

A wet-type gas meter was employed for calibration of the flow rate of the rotameter installed in Andersen sampler and Low volume sampler and also the integrated flow meter installed in the latter. The type of meter employed is one manufactured by SHINAGAWA KEIKI Co., Ltd. model W-NK-10.

As shown in Figure 4-18, the incoming air through the inlet is led to the front chamber and then to a round shaped drum through suction tube. The interior of the drum is sectioned into 4 chambers water sealed. The air flow is admitted to and goes out from each of these chambers and gives the rotational thrust to the drum (shown by an arrow sign). The air exhaust volume per rotation is constant and thus the integrated flow rate can be calculated by knowing the number of rotations. Specifications of this gas meter and its external appearance are respectively shown in Table 4-27 and Figure 4-19.

In order to calibrate the performance of rotameter and integrated flow meter, the wet-type gas meter, pressure gauge, integrated flow meter, rotameter and the pump were all connected in series as shown in Figure 4-23. Calibrations were done on rotameter readings and count values of the integrated flow meter.

(Please refer the detail discussion to " Calculation of TPM Concentration" by Low volume sampler and Andersen one.)

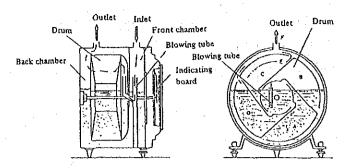


Figure 4-18 The mechanical structure of wet-type gas meter

Table 4-27 Specifications of the wet-type meter

Measuring range:	20 - 6.000 l/h
Drum capacity:	10 liter
Pressure loss:	Under 15 mm H <sub>2</sub> O
Indicator board:	l rotation 10 liter, minimum readint 0.02 l maximum intergrating volume 9.999 m <sup>3</sup>
Maximum pressure:	1,000 am H <sub>2</sub> O
Pressure resistance:	1,500 mma H <sub>2</sub> O
Tolerable temperature:	Under 50°C
Weight:	Weight 35 kg, weight at operation 62 kg

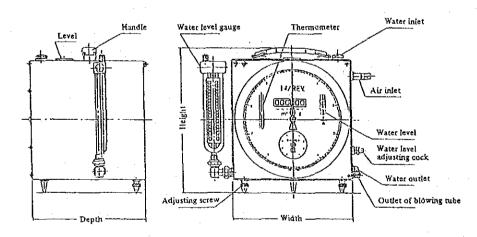


Figure 4-19 The external appearance of wet-type gas meter

The operation procedures of the wet-type gas meter are as follows.

(i) Installation

The wet-type gas meter should be mounted on a flat and stable (vibration-free) table and is positioned at an exact horizontal level.

A level gauge and adjusting screw are to be used.

- (ii) Adjustment of the water level
  - (a) Open a plug of water inlet of blow pipe located in the right side of the meter and pour in the water until the meniscus comes to the level 2 cm above the water level indicator.
  - (b) Confirmation of water in blow pipe

Open the plug of outlet of blow pipe on the right side of the meter, and check the water. When water is present inside the pipe, the meter will not rotate. Thus drain the water completely and close the plug.

(c) Idle operation

Close the water inlet plug, connect the inlet pipe, and make the meter idly run about 20 to 30 rotations. After idle run, return the inner pressure of meter to the atmospheric one and drain water gradually by means of a level adjusting cock at the right side of meter and keep the water level indicator in the midpoint of meniscus as shown in Figure 4-20.



Figure 4-20 Adjustment of the water level

(iii)Leak test

Tightly connect the inlet and outlet tubes to the meter not to cause any leakage and then close the outlet. Apply the pressure from the inlet side and close the inlet. Observe the water level and confirm that no leakage exists.

(iv)Measurement

Connect the inlet and outlet tubes, set the meter in operation the mode and start measurement after about 20 idle rotations of the longer pointer. When a significant difference being observed between water temperature and air temperature, keep idle operations until the former comes to an reasonable agreement with the latter.

(v) Drainage of water

After measurements are completed, the remaining water in the instrument is to be drained completely, by opening the water discharge plug located right and back side of the meter. Confirm the discharge including the inside of drum by tilting the instrument backwardly.

3) Chemical balance

The precision chemical balance is employed for weighing the filters of Low volume samplers

and Andersen samplers. Both samplers require a sensitivity of 1/100 mg for weighing the filters and thus selected is Mettler H54AR type semi-micro balance, specifications of which are shown in Table 4-28.

Table 4-28 Specifications of the chemical balance used

Weighing range	up to 170 g
Minimum weighing value	0.01 mg
Standard deviation	plus/minus 0.01 mg

## 4) Aging box

For storage of filters desiccated before and after sampling of particulate matter, the aging boxes are normally in use. In most cases,  $Ca(NO_3)_2$  is placed inside the aging boxes to maintain the filter humidity constant.

However, throughout this survey project, the door of aging boxes were kept open and accordingly the humidity in them were thought same as that of air-conditioned room, 55-65%. (The arrangement is mainly due to the fact that the humidity of aging boxes is often disturbed by door opening and closing when filters were taken in or out.)

### 5) Filters

Two types of filters were used for Low volume samplers to measure TSP concentration, one made of polyfluorocarbon and the other of quartz fiber.

The former was thought instrumental in improving the elemental and ion analyses, and the latter for analysis of total carbon and non-volatile carbon (inorganic carbon) of the particulate matter.

Table 4-29 Specifications of filters

Specifications of the filters used in this study are listed in Table 4-29.

Quartz-fiber file (TOYO-ROSHI QR-1)		Polyfrone filter (TOYO-ROSHI PF040)
Thickness (mm)	0.35	0.95
Weight (g/m <sup>2</sup> )	75	560
Percentage of vacant space (Vol. %)	_	73
Pressure loss (mmAq/5 cm/sec)	25	-
Collection efficiency (0.3 µm DOP %)	99	95.0

Sampling characteristics of various filters has long been studied by Industrial Pollution Control Association of Japan (IPCAJ). According to a comparative study made by IPCAJ, four filters made of quartz, glass, membrane and polyfluorocarbon are selected and are subject to experiments at same time/place conditions. The result of such an comparative study is shown in Table 4-30.

### Table 4-30 Sampling characteristics of filters

Material	Relative weight
Quartz Glass	0.99
Glass	1.06
Polyfluorocarbon	0.94
Membrane	1.00

The relative weight=each filter weight against the average weight of tested filters.

As shown in the table, the difference of relative weight or particulate trapping characteristics between them is found comparatively small. One can see, however, a slightly higher value in a glass made filter. When such an difference is assumed significant, a possible reason that we can think of might be that the acid gas in the air (mainly  $SO_2$ ) is adsorbed to the surface of alkaline glass filter and causes an increase in the apparent weight.

The relative weight of polyfluorocarbon filter is found a little smaller than the average, which may suggest a better passing characteristics of the filter. In evaluation of particulate concentration by weighing the filter, the humidity of environment where weighing is performed is a most influential single factor. Accordingly IPCAJ has conducted a study with respect to (a) hygroscopicity of new filters and (b) hygroscopicity of particulate matter. Eight filters made of four different materials, two each of a same material, were weighed in the atmosphere of varying humidity. The effect of humidity on filters were investigated together with the influence coming from type of material. The study result is as shown in Figure 4-21.

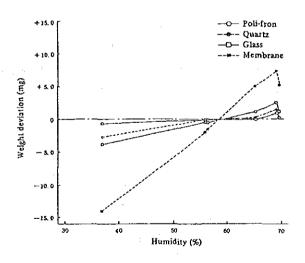


Figure 4-21 Weight change of filters by humidity

As for hygroscopicity of the particulate matter, an investigation was done by using two sets of Low volume samplers, which were continuously operated for two days period while changing the filters (made of quartz and polyfluorocarbon) every 8 hours. The filters loaded with particulate matter were desiccated and weighed in various humidity atmospheres. The study result is as shown in Figure 4-22.

To avoid the hydroscopicity effect of filters, non-used filters were simultaneously weighed

and weight increment of them due to varying humidity was subtracted from the measured weight of filters loaded with dust.

From Figure 4-21 one can see the weight increase in all tested filters by increasing humidity, a most significant increase about the membrane filter, glass one coming next and then poly-fluorocarbon filter following. From Figure 4-22, one can see the contribution of humidity change to weight increase being larger in particulate matter than in types of filter.

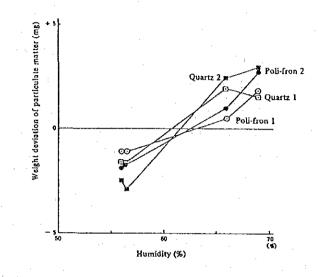


Figure 4-22 Weight change of particulate matter by humidity

(3) Calculation of Total Suspended Particulate

1) Calibration of Low volume samplers

The rotameter and integrated flow meter to be mounted on Low volume samplers were subject to calibration jobs which used a wet-type gas meter as shown in Figure 4-23. The wet-type gas meter, pressure gauge, integrated flow meter, rotameter and a suction pump were all connected in series as illustrated.

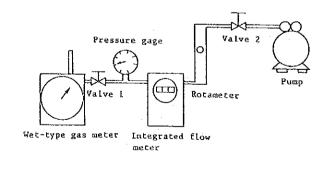


Figure 4-23 Calibration of the rotameter and integrated flow meter for Low volume samplers

 (i) The initial readings of the pressure gauge were recorded when new filters (polyfluorocarbon and quartz fiber made) were mounted on the Low volume sampler and the flow rate of rotameter was set at 10 liter per minute.
 The readings taken are as shown in Table 4-31.

Table 4-31 Initial pressure values

Type of filters	Initial head loss
Polyfluorocarbon filter	81 mm Aq
Quartz fiber filter	110 mm Aq

- (ii) To study the relationship between pressure gauge readings and the rotameter of Low volume sampler, the mounted filters were removed from samplers and then the flow rate of rotameter was again fixed at 10 liter per minute and the water head loss was adjusted to the initial pressure values shown in Table 4-31 by controlling Valve 1.
- (iii)While keeping the condition above stated, measured were time and count value of the integrated gas meter required to complete 10 liter air flow through the wet-type gas meter.
- (iv) The readings of the pressure gauge were recorded when the flow rate of rotameter were set at 5, 15, 20 and 25 liter/min respectively. Also measured were time requirement and the count value of integrated gas meter to complete the air flow of 5, 10, 15, 20 and 25 liter per minute respectively. Table 4-32 shows an example of measurement and the complete set of data file in Appendix.
- (v) The flow rate calculable from the time requirement to complete aspiration of a predetermined amount of air was subject to the temperature correction since the rotameter is designed at 20°C. The equation used for such correction is:

 $Qg_0 = ((273 + T_0)/(273 + Temp.)) \times V \times 60/t$  ..... (4-12) where

Qg<sub>0</sub>; the flow rate through the wet-type gas meter at 20°C (liter/min)

Temp.; the wet-type gas meter temperature during calibration (°C)

 $T_0$ ; the designed temperature of rotameter (20°C)

V; the measured air volume of wet-type gas meter (liter)

t; time required to aspirate the amount of air (s)

(vi) The flow rate Qr at the designed conditions of rotameter is expressed as a function of Qr, reading value of rotameter, as shown by Equation 4-13. An example of such caliculation results is also shown in Table 4-32.

 $Qr_0 = Qr ((273 + T_0)/(273 + Temp.))^{1/2} \times ((760 - \Delta P)/P_0)^{1/2}$  ..... (4-13) where

Qr<sub>0</sub>; the flow rate of rotameter at designed conditions (liter/min)

Qr; the reading value of rotameter (liter/min)

 $P_0$ ; the designed pressure of rotameter (737 mm Hg)

 $\Delta P$ ; the reading value of pressure gauge (mmHg)

 $T_0$ ; the designed temperature of rotameter (20°C)

Temp.; the temperature during calibration (°C)

(vii) The relation between  $Qg_0$  (the flow rate of wet-type gas meter calculated by Equation 4-12) and  $Qr_0$  (the flow rate of rotameter calculated by Equation 4-13) is expressed by the following equation.

 $Qg_0 = a(Qr_0)+b$  ..... (4-14) where a and b are regression coefficients.

Figure 4-24 shows an example of such calculations and the whole set of data file is enclosed in Appendix.

(viii)  $Qrs_0$  (the flow rate when  $Qg_0$  is 10 liter/min) was calculated and then Qr values by Equation 4-15 while keeping the water head loss at 0, 250, 500, 750, and 1000 mmAq respectively. Figure 4-25 shows an example of such calculations and the whole set is enclosed in Appendix.

Reference figures obtained were also posted on the inside face of shelter door of Low volume samplers at each station.

 $Qr = Qrs_0/((273 + T_0)/(273 + Temp.))^{1/2} \times (760 - \Delta P)/P_0)^{1/2}$  (4-15) where

Qr; the reading value of rotameter (liter/min)

Qrs<sub>0</sub>; the flow rate of rotameter calculated by Equation 4-14 while keeping Qg<sub>0</sub> at

10 liter per minute (liter/min)

P<sub>0</sub>; the designed pressure of rotameter (737 mmHg)

 $\Delta P$ ; the reading value of pressure gauge (mmHg)

 $T_0$ ; the designed temperature of rotameter (20°C)

Temp.; average temperatures expected at survey spots

Jan. to Feb.	27.0°C
Mar. to Apr.	29.8
May to June	29.4
July to Aug.	28.6
Sept. to Oct.	28.1
Nov. to Dec.	26.6

#### Table 4-32 Calibration result of the rotameter for Low volume samplers

No1070236	HS1-0
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									1	
Pressure	Flow	Count	er Val	ue	Total	Sampling	Vel Gas	Flow	Ave.	Flow
ΔP	heter			Total	Sampling	Time	Neter	Val.0g0	0g0	Val.Qr0
<mmåq></mmåq>	Scale	Refore	After	Count	Volume<1.>	<sec></sec>	Temp< C>	<l min=""></l>		<t. min=""></t.>
40	5	257.2	262.6	5.1	5	61.23	24.2	4.9303	4.83	5.0;
40	5	264.6	269.6	5.0	5	01.35	24.2	4.8209		
110	10	44.9	55.3	10.4	10	61.04	24.2	9.2367	9.24	10.03
110	10	59.5	70.3	10.8	10	61.00	24.2	9.2425		· · · · · · · · · · · · · · · · · · ·
217	15	78.8	89.5	10.7	10	42.48	24.2	13.9247	13.89	14.00
247	15	<u> </u>	109.8	10.8	10	42.67	24.2	13.8827		
462	20	132.0	154.0	22.0	20	63.16	24.2	18.7309	18.72	19.70
462	20	160.4	182.3	21.9	20	63.23	24.2	18.7101		
732	25	197.7	220.0	22.3	20	51.19	24.2	23.1108	23.15	24.27
732	25	225.3	247.5	22.2	20	51.02	24.2	23.1878		

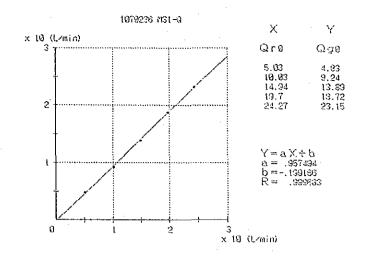
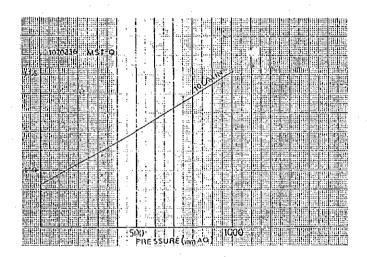
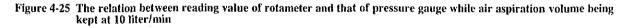


Figure 4-24 The relationship between the flow rate of Wet-type gas meter and that of rotameter





- 2) Air aspiration volume of Low volume samplers
  - (i) Estimation of aspirated air volume from reading value of rotameter and that of pressure gauge

The total air volume aspirated through Low volume samplers was calculated by summing up incremental aspirations ( $R_i$ ) between (i-1) and (i) patrol which were subject to temperature correction.

(a) Firstly, the flow rates of rotameter before and after it was adjusted by patrol members were corrected according to both Equation 4-16 and Equation 4-17 to meet the design conditions of 20°C and 737 mmHg.

$$Qra_{0i-1} = ((760 - \Delta Pa_{i-1})/P_0)^{1/2} \times ((273 + T_0)/(273 + Temp.))^{1/2} \times Qra_{i-1} \dots (4-16)$$

$Qrb_{0i} = ((760 -$	$(\Delta Pb_i)/P_0)^{1/2} \times ((273 + T_0)/(273 + Temp.))^{1/2}$	
$\times$ Qrb <sub>i</sub>		17)

where

- $Qra_{0i-1}$ ; the flow rate after adjustment at (i-1) patrol to meet the designed conditions (liter/min)
- Qrb<sub>0i</sub>; the flow rate before adjustment at (i) patrol to meet the design conditions (liter/min)

 $Qra_{i-1}$ ; rotameter reading value after adjustment at (i-1) patrol (liter/min)

Qrb<sub>i</sub>; rotameter reading value before adjustment at (i) patrol (liter/min)

 $T_0$ ; the design temperature of rotameter (20°C)

Temp.; average temperature expected during measurement (°C)

P<sub>0</sub>; the design pressure of rotameter (737 mmHg)

 $\Delta Pa_{i-1}$ ; the reading value of pressure gauge after adjustment at (i-1) patrol (mmHg)

 $\Delta Pb_i$ ; the reading value of pressure gauge before adjustment at (i) patrol

(mmHg)

(b) Secondly, the flow rate  $Qr_0$  at design condition of rotameter was corrected into the flow rate of wet-type gas meter,  $Qg_0$  at 20°C by Equation 4-18.

$Qg_{0i-1} = a[Qr_{0i-1}] + b$	(4.18)
$Qg_{0i} = a[Qr_{0i}] + b$	

where

- $Qg_{0i-1}$ ; the corrected flow rate to meet the design conditions after adjustment at (i-1) patrol (liter/min)
- Qg<sub>0i</sub>; the corrected flow rate to meet the design conditions before adjustment at (i) patrol (liter/min)
- (c) The air volume aspirated  $R_i$  during (i-1) partol and (i) patrol was obtained as a product of lapse time and the mean of flow rate after adjustment at (i-1) patrol and that before adjustment at (i) patrol.

 $R_i = (Qg_{0i-1} + Qg_{0i})/2 \times t \times 1/1000 \quad ..... (4-19)$  where

 $R_i$ ; the air volume aspirated during (i-1) and (i) patrol (m<sup>3</sup>)

t; lapse time during (i-1) and (i) patrol (min)

(d) The total air volume aspirated to meet the design conditions is calculated by summing up all of incremental air volumes aspirated during each patrol time. The total air volume aspirated at field conditions is thus estimated by Equation 4-20.

$$V_1 = \sum_{i=1}^{n} R_i \times ((273 + \text{Temp.})/(273 + T_0)) \qquad (4-20)$$

where

 $V_1$ ; total air volume aspirated at the temperature of monitoring (m<sup>3</sup>) n; number of patrols (excluding the initial startup and including the last patrol when the monitoring job was terminated.)

 $T_0$ ; the design temperature of rotameter (20°C)

Temp.; the average temperature expected (°C)

Table 4-33 shows an example of such calculations and the data as a whole is enclosed in Appendix.

The estimation of aspirated air volume by the above-mentioned method is incorrect in case the power failures occur. Thus they were monitored by both recording charts (of automatic and continuous monitors) and the count values of the integrated flow meter. The frequency of power failure observed is listed in Table 4-34.

Table 4-33	An example calculation to estimate the air volume to be
	aspirated by Low volume sampler

MSI-Q         ROTOR NJ.1070236         TENP(°C)         27.0           LAPSE         STOP         ROTOR         PRESSURE         CORRECTED         CALIBRATED           DATE         TIME         TIME         TIME         BETER         DIFFERENCE         FLOV         RATE           1/17         11<:0         0         11.0         110.0         11.5         10.8	FLOV VOL (m3)
DATE TIME TIME TIME METER DIFFERENCE FLOW RATE FLOW RATE (MIN) (MIN) (L/min) (mmAg) (L/min) (L/min)	VOL
(MIN) (MIN) (L/min) (makq) (L/min) (L/min)	
(MIN) (MIN) (L/min) (mmAq) (L/min) (L/min)	(m3)
1/1711:0 0 11.0 110.0 11.5 10.8	
1 /17 15 :43 8 283 0 10.5 105.0 11.0 10.3	3.0
<u>1 /17 15 :43 £ 0 11.0 105.0 11.5 10.8</u>	
1 /18 9 :55 B 1092 0 10.9 110.0 11.4 10.7	11.7
1 /18 9 :55 F 0 11.0 110.0 11.5 10.8	
I /18 14 :46 B 291 0 10.7 110.0 11.2 10.5	3.1
<u>1/18 14 :46 E 0 10.9 110.0 11.4 10.7</u>	
1 /19 9 .53 8 1147 0 11.0 110.0 11.5 10.8	12.3
1 /19 9 :53 F 0 10.9 110.0 11.4 10.7	
1 /10 15 20 8 327 0 10.9 110.0 11.4 10.7	3.5
<u>1 /19 15 :20 F 0 10.9 110.0 11.4 10.7</u>	1
1 /20 10 :57 8 1177 0 11.0 118.0 11.5 10.8	12.7
<u>1 /20 10 :57 F 0 10,9 118,0 11,4 10.7</u>	
1/20 15 :53 8 302 0 10.7 116.0 11.2 10.5	3.2
<u>1 /20 15 :59 £ 0 11.0 120.0 11.5 10.8</u>	
1 /21 10 .10 8 1091 0 11.2 120.0 11.7 11.0	11.9
<u>1 /21 10 :10 F 0 11.0 120.0 11.5 10.8</u>	
1 /22 10 : 3 8 1433 0 11.0 120.0 11.5 10.8	15.5
<u>1 /22 10 : 3 £ 0 11.0 120.0 11.5 10.8</u>	
1 /23 10 :25 8 1462 0 11.0 125.0 11.5 10.8	15.8
1 /23 10 125 F 0 11.0 125.0 11.5 10.8	
1 /24 8 :50 8 1345 0 11.0 125.0 11.5 10.8	14.5
1/24 8 50 F 0 11.0 125.0 11.5 10.8	
1 /25 10 :42 8 1552 0 11.0 125.0 11.5 10.8	16.7
_1 /25 10 :42 F 0 11.0 125.0 11.5 10.8	
1 /26 10 :36 8 1434 0 11.0 137.0 11.5 10.8	15.5
1 /26 10 136 F 0 11.0 137.0 11.5 10.8	
1 /27 15 :36 B 1740 0 10.8 140.0 11.3 10.6	18.6
_1 /27 15 :36 F 0 11.0 140.0 11.5 10.8	
1 /28 14 :12 8 1356 0 11.1 145.0 11.6 10.9	14.7
_1 /28 14 :12 F 0 11.1 145.0 11.6 10.9	
1 /29 10 :57 8 1245 0 11.1 145.0 11.6 10.9	13.5
1 /29 10 :57 £ 011.1 145.0 11.6 10.9	
1/30 11 : 0 8 1443 0 11.3 155.0 11.8 11.1	15.8
TOTAL 18720 (min) TOTAL	206.9 (m3

Regression coefficients; a = 0.957b = -0.199Qg0 = a(Qr0) + b

- (ii) A method to estimate the air aspiration volume by using count values of the integrated flow meter
  - a) The flow rate, Y, per one rotation of the integrated flow meter was calculated by knowing the time SE required for X rotations of the meter by Equation 4-21. An example of such calculations is shown in Table 4-35 and other data file is enclosed in Appendix.

 $Y = SE(s)/X(rotations) \times Qg_0(\ell/min)/60(S/min) = SE \cdot Qr/60 \cdot X \quad \dots \quad (4-21)$ 

where

Y;The flow rate per one rotation of the integrated flow meter (liter/count) SE; time required for X rotations of the meter (s)

Qg<sub>0</sub>; the flow rate of wet-type gas meter (liter/min)b) A regressional equation shown by Equation (4-22) was developed to show the relationship between readings of rotameter and the flow rate of integrated flow meter

with respect to one rotation. Equation (4-22) is a third order equation.

Y = g(Qr) .....(4-22)

An example of such calculations is shown in Figure 4-26 and other data file is enclosed in Appendix.

Date/time	Station	Power failure (minutes)	Troubles		Date/time	Station	Power failure (minutcs)	Troubles
11:50–15:40 17/Jan. 1988	MS3	230	Short circuiting of Andersen sampler		8:00-11:00 10/Sep. 1988	MS2	180	Power failure
16:40-16:50 20/Jan. 1988	MS2	10	Power failure	•	17:10 7/Sep.	MS5	2490	Power failure
15:40–15:50 21/Jan. 1988	MS5	10	Power failure		10:20 9/Sep. 1988 0:00-2:00	MS3	120	Power failure
4:00-7:00 10/Feb. 1988	MS5	180	Power failure		17/Sep. 1988 1:00-11:45	MS4	645	Power failure
10:20-10:40 1/Mar. 1988	MS2	20	Power failure		28/Sep. 1988 12:40 28/Sep.	MS4	1535	Power failure
21:00-23:00 1/Apr. 1988	MS4	120	Power failure		14:15 29/Sept. 1988			
9:30-10:00 10/Apr. 1988	MS2	30	Power failure		14:10-15:20 15/Oct. 1988	MS2	70	Power failure
3:20-3:40 13/Apr. 1988	MS5	20	Power failure		12:00-15:30 7/Oct. 1988	MS5	210	Power failure
3:30-4:50 13/Apr. 1988	MS3	80	Power failure		9:30-16:40 30/Oct. 1988	MS1	430	Power failure
3:40-9:40 13/Apr. 1988	MS2	360	Power failure		16:10 29/Oct. 	MS2	2640	Power failure
4:20-8:20 13/Apr. 1988	MS1	240	Power failure		4:10-6:10 17/Nov. 1988	MS1	120	Power failure
1:00-3:00 15/Apr. 1988	MS2	120	Power failure		12:10-12:40 24/Nov. 1988	MS2	30	Power failure
5:10-6:20 7/July 1988	MS3	70	Power failure		9:20-9:50 29/Nov. 1988	MS2	30	Power failure
16:50–17:30 8/July 1988	MS3	40	Power failure		17:10-19:30 1/Dec. 1988	MS2	140	Power failure
10:00-12:00 3/July 1988	MS5	120	Power failure		11:50–20:20 5/Dec. 1988	MS2	510	Power failure
22:10 8/Aug.   4:00 9/Aug. 1988	MS5	350	Power failure		20:00 9/Dec.20:	MS4	3975	Power failure
3:00-6:00 21/Aug. 1988	MSI	180	Power failure		14:15 12/Dec. 1988 6:40-7:20 10/Dec. 1988	MS5	. 40	Power failure
15:10-15:40 20/Aug. 1988	MS2	30	Power failure		9:40–15:10 25/Dec. 1988	MSI	330	Power failure
3:15–12:15 7/Sep. 1988	MS2	540	Power failure		18:5019:50 30/Dec. 1988	MS4	60	Power failure

# Table 4-34 Power failure time

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Flow	ilet.	уо	1070236	MS1-0

Flow Meter	Integrated	Sampling	Wet Gas Met.	Integrated	Average
Scale	Gas Meter	Time	Flow Val;	Meter Flow	Y T
Qr	count X	SE <sec></sec>	f <qr><l min=""></l></qr>	Y <l count=""></l>	<l count=""></l>
5	5.4	61.23	4.5883	0.8671	0.90
5	5.0	61.35	4.5883	0.9383	
10	10.4	64.04	9.3758	0.9622	0.94
10	10.8	64.00	9.3758	0.9260	
15	10.7	42.48	14.1632	0.9372	0.93
15	10.8	42.67	14.1632	0.9326	
20	22.0	63.16	18.9507	0.9068	0.91
20	21.9	63.23	18.9507	0.9119	
25	22.3	51.19	23.7382	0.9082	0.91
25	22.2	51.02	23,7382	0.9093	

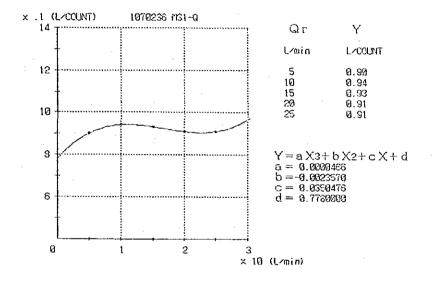


Figure 4-26 The relationship between reading values of rotameter and the flow rate of integrated flow meter per one rotation.

c) The total air volume aspirated by Low volume sampler is obtained by summing up sampling volume R<sub>i</sub> for a period of from a patrol to another. The value R<sub>i</sub> is calculated by Equation (4-23).

 $R_{i} = g[(Qra_{i-1} + Qrb_{i})/2] \times (IC_{i} - IC_{i-1}) \times 1/1000 \quad ..... (4-23)$  where

 $R_i$ ; the air volume aspirated during (i-1) and (i) patrol (m<sup>3</sup>)

Qra<sub>i-1</sub>; the reading value of rotameter after adjustment at (i-1) patrol (liter/min)

Qrb<sub>i</sub>; the reading value of rotameter before adjustment at (i) patrol (liter/min)

- $IC_{i-1}$ ; the count number of integrated flow meter after adjustment at (i-1) patrol (count number)
- IC<sub>i</sub>; the count number of integrated flow meter before adjustment (i) patrol (count number)
- d) The total air volume aspirated is obtained by summing up sampling volume R<sub>i</sub> dur-

ing (i-1) and (i) patrol according to Equation (4-24).

 $V_2$ ; the total air volume aspirated (m<sup>3</sup>)

n; the number of patrols (excluding the startup one and including the last patrol to complete the monitoring)

An example of such calculations is shown in Table 4-36 and other data file is enclosed in Appendix.

Table 4-36 An example of aspirated air volume calculations for Low volume sampler

151-0		80r	UR NO.	1070236			
			INTEGRATE		RUTUR	CALIBRATED	FLOV
DATE	TIME		VALUE	TOTAL	HETER	FLOV RATE	Vot.
			(COUNT)	(COURT)	(L/min)	(L/cont)	(m3)
1/11	11:0		430	0	11.0	· · · · · · · ·	
1 717	15 :43	8	3410	2080	10.5	0.040	2.8
1/17	[5:43	F	3410		11.0		
1 /18	9:55 0:55	B F	15158	11746	10.9	0.940	11.0
			15158		11.0		
1 /18	14 .48	B	18316	3160	10.7	0.940	3.0
1 718 1 719	<u>14 48</u> 0 153	- <u>F</u>	18316		10.9		
1 /19	0 53	F	30635	12319	11.0	0.040	11.6
	<u> </u>	1 8	30835	3566	10.9		
	15 .20	0 F	34201	1300	10.9	0.940	3.4
1 /20		- <u>r</u> -B	34201		10.9		·
1 /20		- U F	46802	12601	11.0	0.940	11.8
	10 :57 15 :59		46802		10.9		
1 /20		B	50147	3345	10.7	0.940	3.1
1 /20		<u> </u>	50147				
1 /21	10 :10	8	62032	11885	11 2	0.940	11.2
1/21	10 :10	<u> </u>	62032		11.0		
1 /22	10 : 3	B	-77441	15409	11.0	0.940	14.5
1 /22	10:3	F	77441		<u> </u>		
	10 :25	ß	93164	15723	11.0	0.940	14.8
1 /23	10 :25	F	93164		11.0		
1 /24	8:50	8	107591	14427	11.0	0.940	13.6
1 /24	8 :50	F	107591		11.0	· · · · · · · · · · · · · · · · · · ·	
	10 42	8	124340	16749	11.0	0.940	15.7
	10 42	F	124340		11.0		
1 /26	10 :36	8	139696	15356	11.0	0.940	14.4
	10 :36	F_	139696		11-0		
	15 :35	8	158455	18759	10.8	0.940	17.6
	15:36	<u> </u>	158455				
1 728	14 112	8	173468	15013	11.1	0.040	14.1
1 /28	14 :12	F_	173468		<u>_1 . </u>	·	
	10 :57	B	187118	13650	11.1	0.940	12.8
<u>1 /29</u> 1 /30	10 :57	F	187118		<u> </u>		
	11:0	8	203047	15929	11.3	0.940	15.0

TOTAL 190.5

Regression coefficients a = 4.66E-5 b = -0.002357 c = 0.0350476 d = 0.778 Y = g(qr0)

3) Calculation of TSP concentration measured by Low volume sampler

TSP concentration was measured by weighing filters before and after samplings. The ambient concentration of TSP is calculated by Equation (4-25).

$$C = (We - Ws)/V \times 10^3$$
 ..... (4-25)

where

C; the concentration of TSP ( $\mu$ g/m<sup>3</sup>)

We; the weight of filter after sampling (mg)

Ws; the weight of filter before sampling (mg)

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