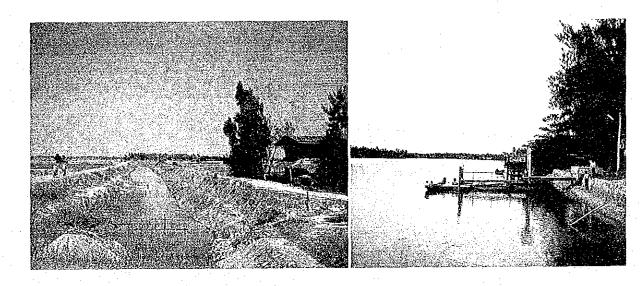
KINGDOM OF THAILAND ROYAL IRRIGATION DEPARTMENT MINISTRY OF AGRICULTURE AND COOPERATIVES

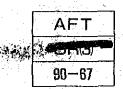
THE FEASIBILITY STUDY
ON
THE AGRICULTURAL WATER DEVELOPMENT PROJECT
OF
BANG PAKONG RIVER BASIN

Appendia (1)



OCTOBER 1990

JAPAN INTERNATIONAL COOPERATION AGENCY



No. 152



ROYAL IRRIGATION DEPARTMENT MINISTRY OF AGRICULTURE AND COOPERATIVES

THE FEASIBILITY STUDY ON THE AGRICULTURAL WATER DEVELOPMENT PROJECT OF BANG PAKONG RIVER BASIN

APPENDIX (1)

OCTOBER 1990

JAPAN INTERNATIONAL COOPERATION AGENCY



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APPENDIX-C: GEOLOGY, FILL MATERIALS AND SEISMICITY

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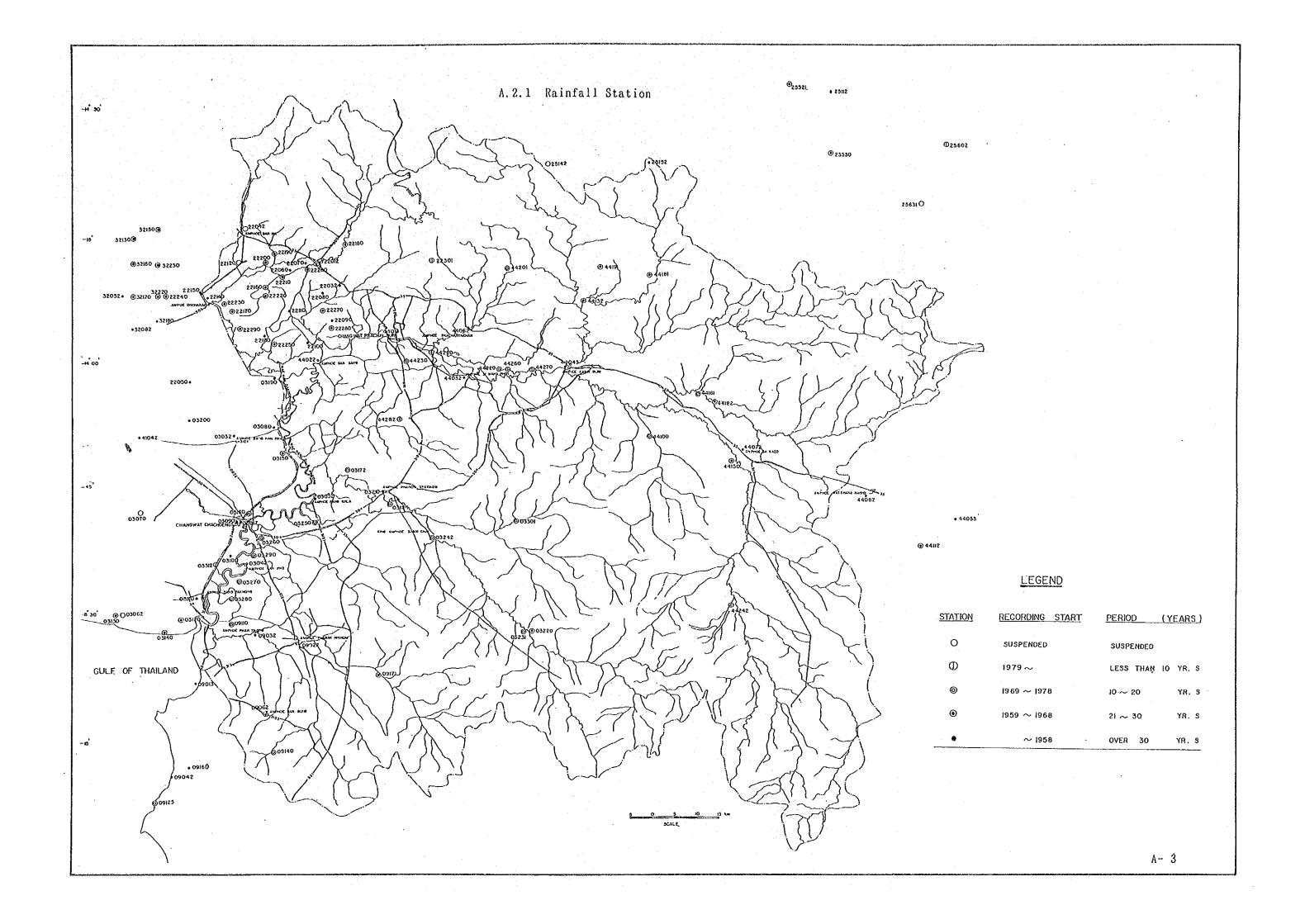
Appendix A- Meteorology and Hydrorology

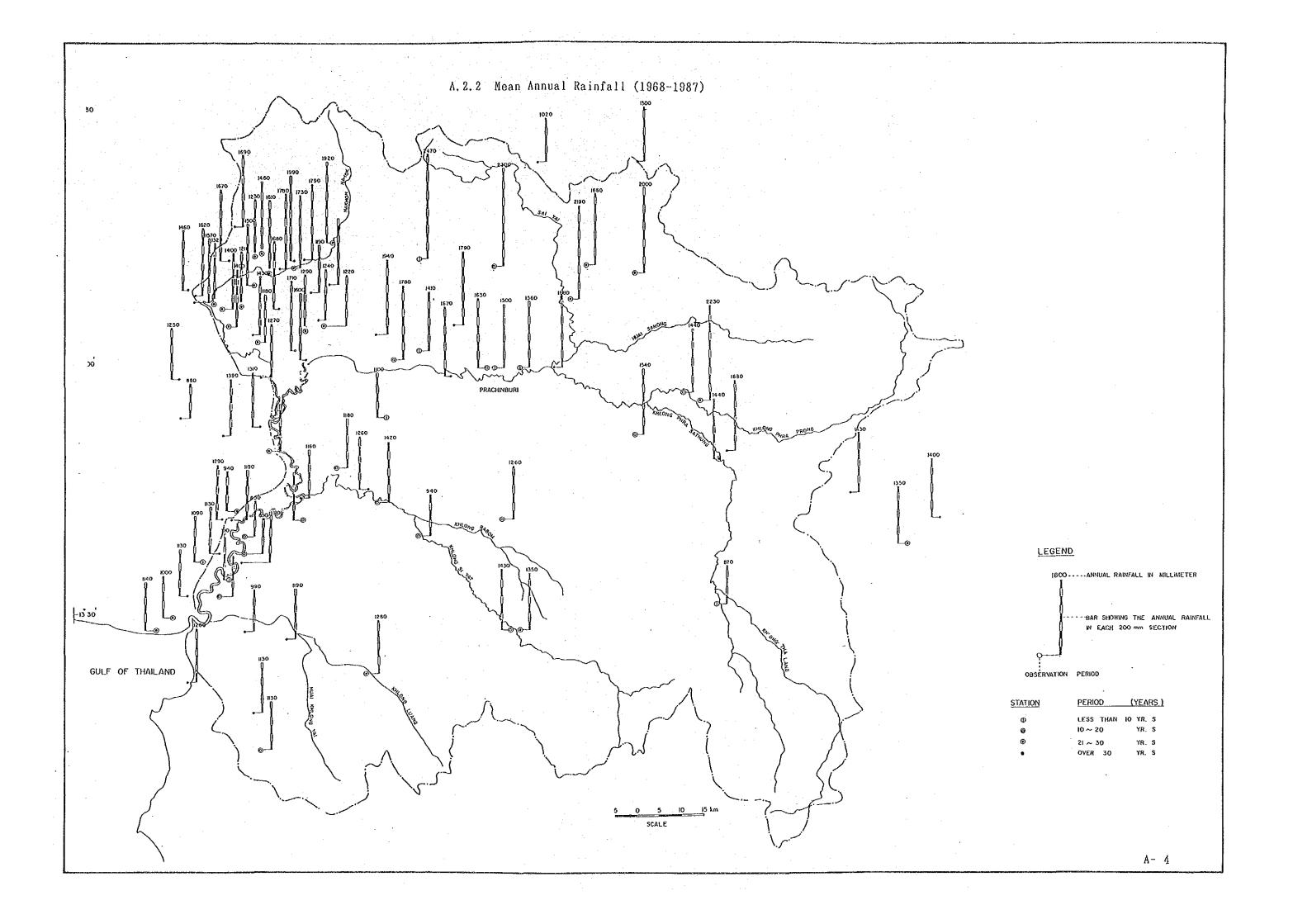
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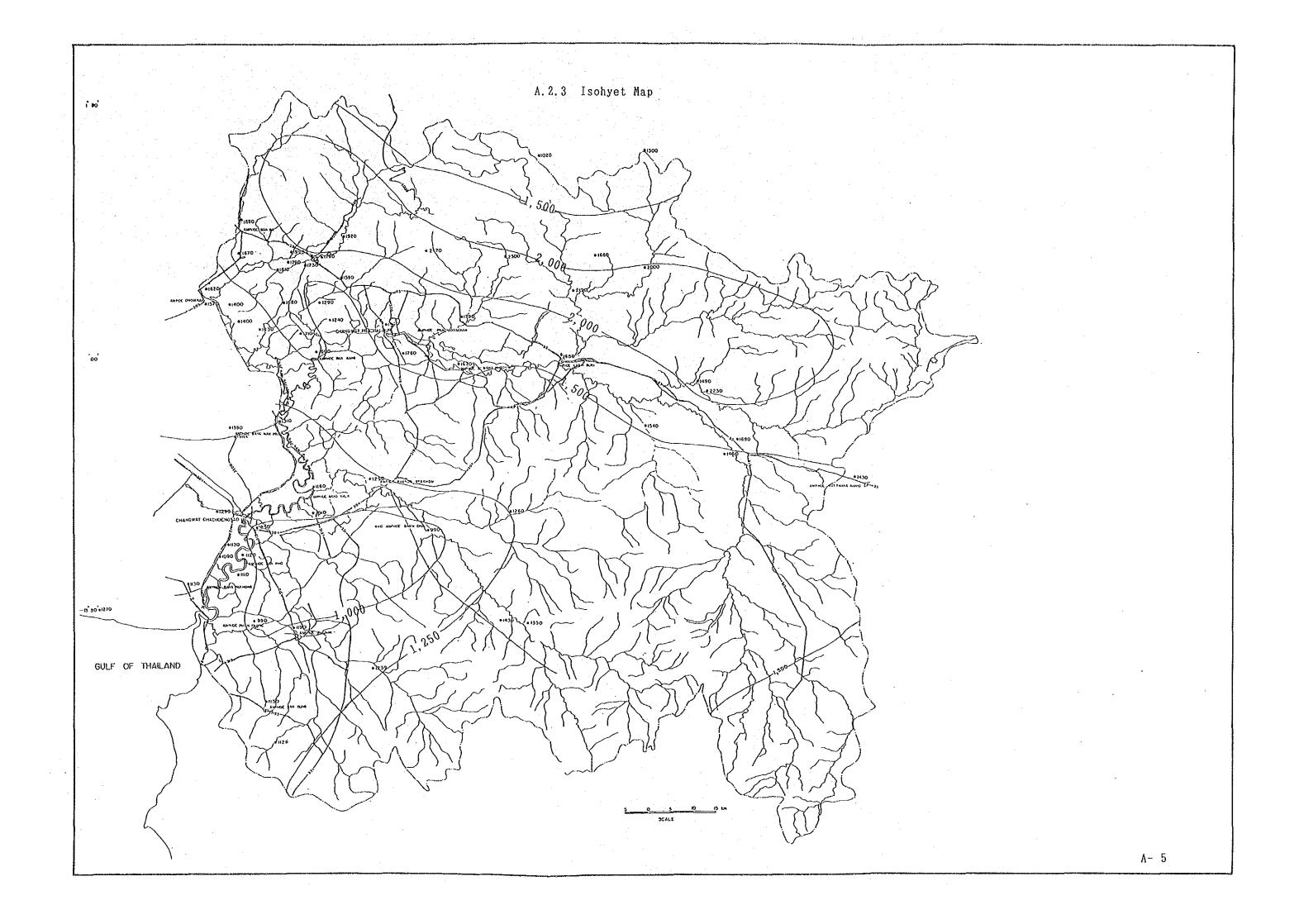
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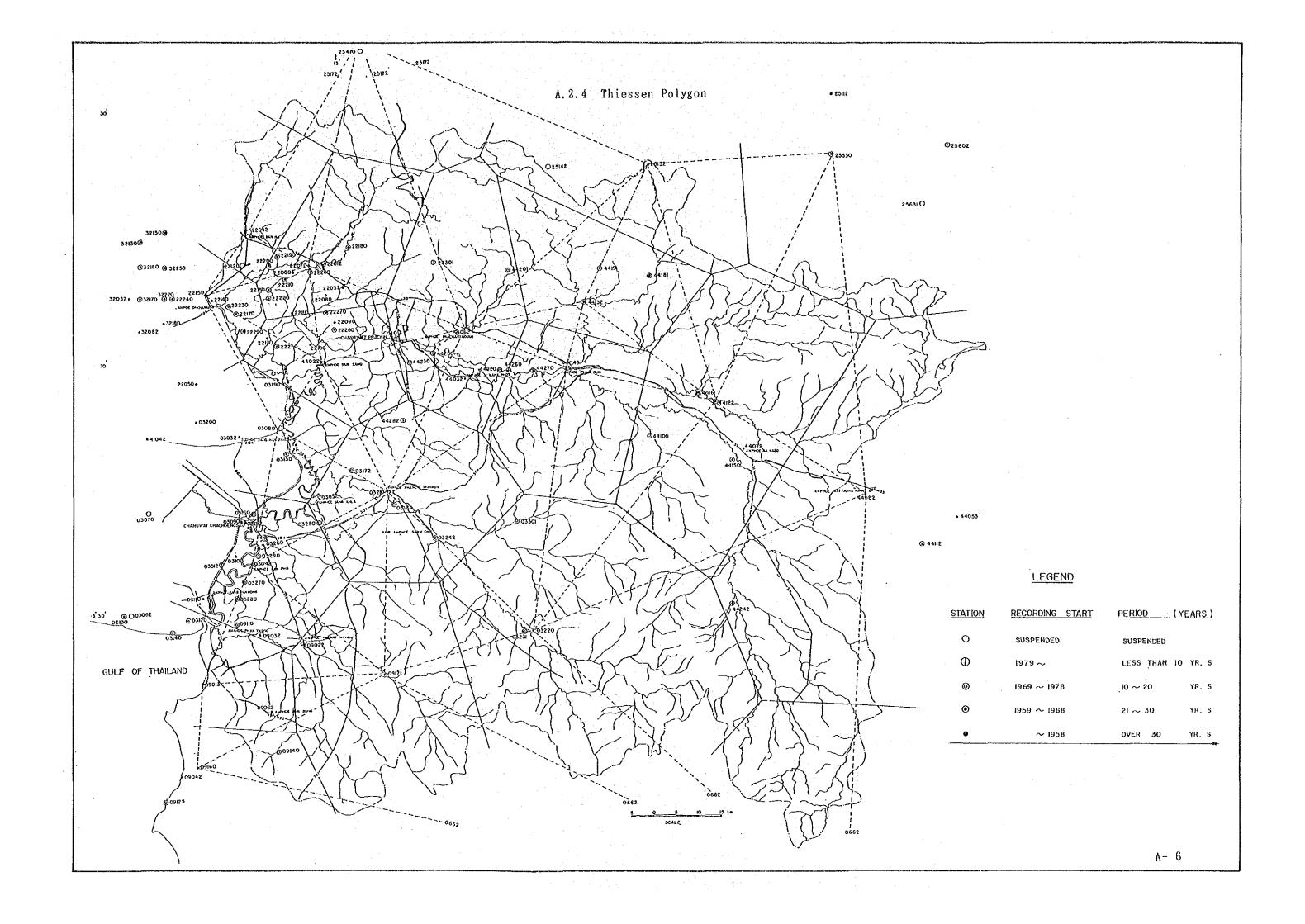
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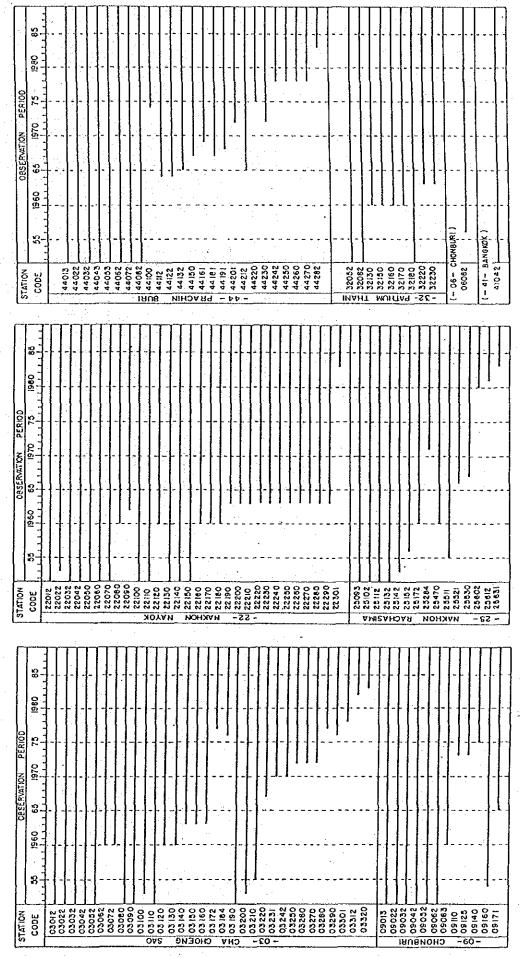








A.2.1 Observation Period of Rainfall Station



A.2.6 Thiessen Areal Ratio

Block	C. Area	Rainfall								Stat	tion C	nda (Thiess	on 1)			- 1			·	* 1 3	
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3	266	1,340	-	-	-	-	-	-	-	-	-	-	43	11	-	-	-	- '	46	-	-	-

A.2.7 Maximum One Day Rainfall

Maximum Two Days Rainfall

A. 2.8

29 Aug 25 Feb 21 Jun 23 Sep 31 Jul Date ST. 22070 126.7 191.0 155,7 167.0 191,7 104,7 109.3 177.5 193,7 162,8 123.7 119.0 114.4 113,5 121.2 193,2 149.6 87.2 Rain (m) 5 Sep Feb 16 Jun 20 Jun 18 Sep 4 Jul 8 Oct 10 Sep 20 Jul 19 Aug 14 Oct 30 Jun 19 Sep 17 Jun 23 Sep Date 44122 174.5 144.0 216,1 86.0 109.0 118,1 146.0 177.5 113.2 120.2 128,3 259.5 Rain 12 Jun 29 Sep 29 Jun 23 Aug 19 Aug 20 Jun 15 Sep 10 Jul ST. 44132 130.0 183.0 64.6 82.8 217.8 214.0 90.2 200.3 250.5 115.9 146.3 164.2 128.9 Rain (mm) Date 28 Aug 5 Sep 29 Jun 20 Sep 1 Sep 25 Sep 19 Jun 10 Jul 1 Jun Sep 27 Sep Мау ST. 44181 96.0 6.96 189,5 124.6 104.0 138,2 122.9 142.6 156,9 102,5 211.2 154.3 93.2 132.9 149.4 117,8 129.2 Rain (mm) 6 Aug 30 Sep 3 Jul 18 Sep Apr 22 Jun 25 Feb 17 Aug Jun 31 Jul 26 Aug Date 70,3 169.8 119.3 97.8 112.7 0.06 114.5 103.5 Rain (mm) 150.8 144,2 104.7 120.0 100,4 20 Aug 19 Sep 11 Oct 30 Aug 1 Feb 5 Jul 9 Oct 21 Jul 3 Jul 1 Jul Date ST. 44122 Rain (mm) 108.3 144.0 145.3 103,5 131.5 120.0 86.0 80.9 76.8 109.5 74.8 93.2 162.0 124.6 74.4 28 Aug 15 Jun 3 Sep 6 Sep 21 Jun 6 Sep 16 Sep 12 Jun 10 Jul 24 Aug 15 Apr 13 Sep 22 Sep 5 May 26 Oct 10 Oct 14 May Date ST. 44152 Rain (mm) 75.4 104.6 124.6 154.1 117,2 10 Aug 22 Oct 6 Sep 26 Sep 14 Oct 10 Jul 2 Jun 1 May 28 Sep 28 Sep 30 Jun 20 Sep 18 Jul Apr Date ST. 44181 Rain (mm) 0.99 74.2 114.0 71,5 148,0 102.5 72.3 115.6 132,5 80,2 94.8 84.8 78.7 111.4 71.7 119.9 123.6 88.1 128°0

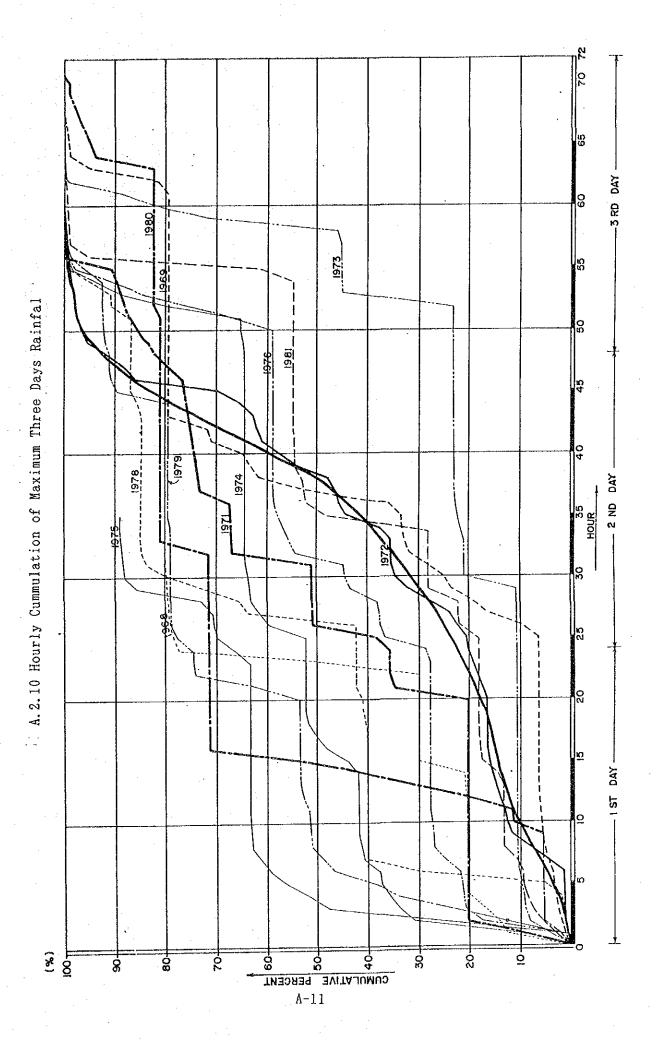
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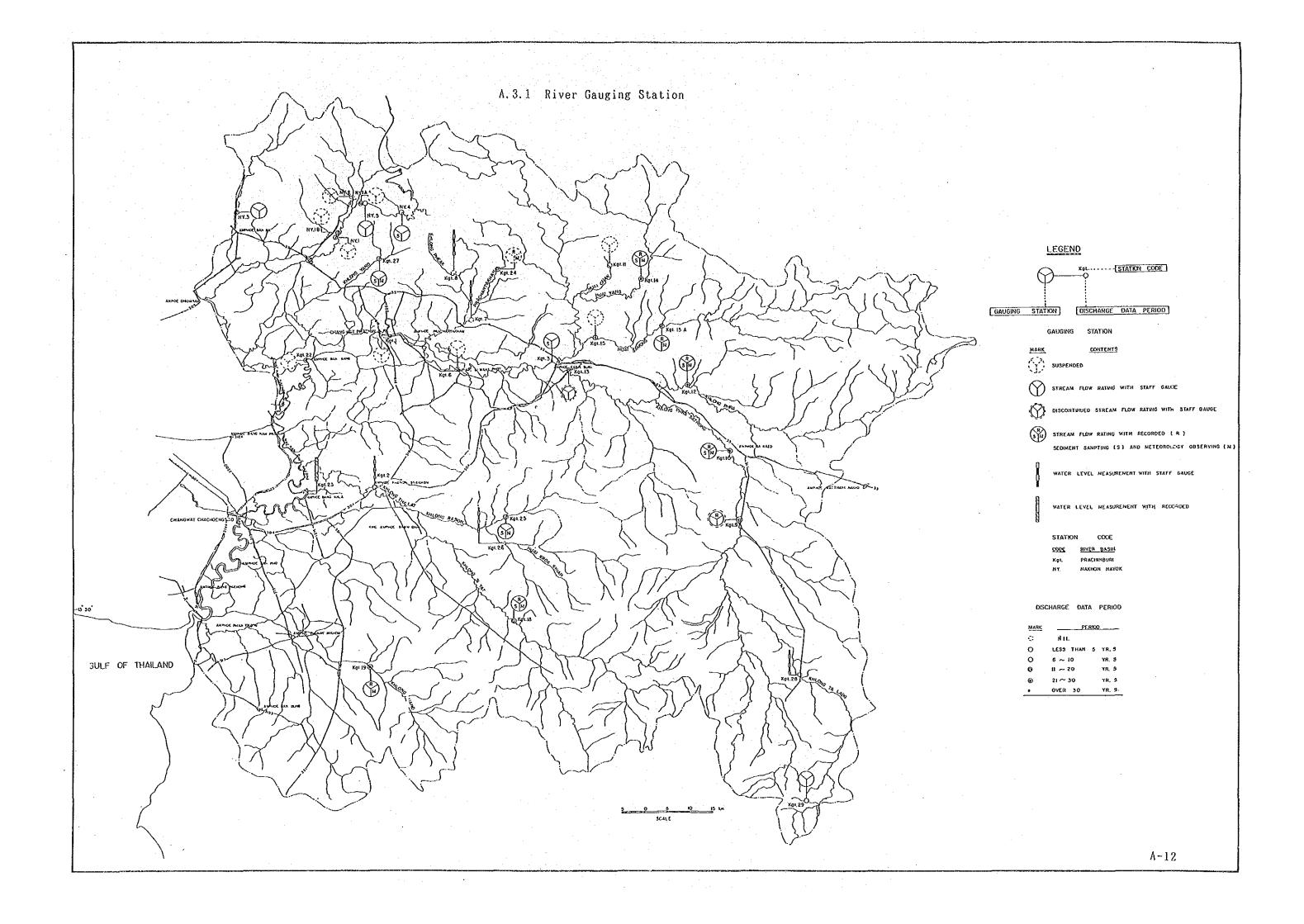
1970

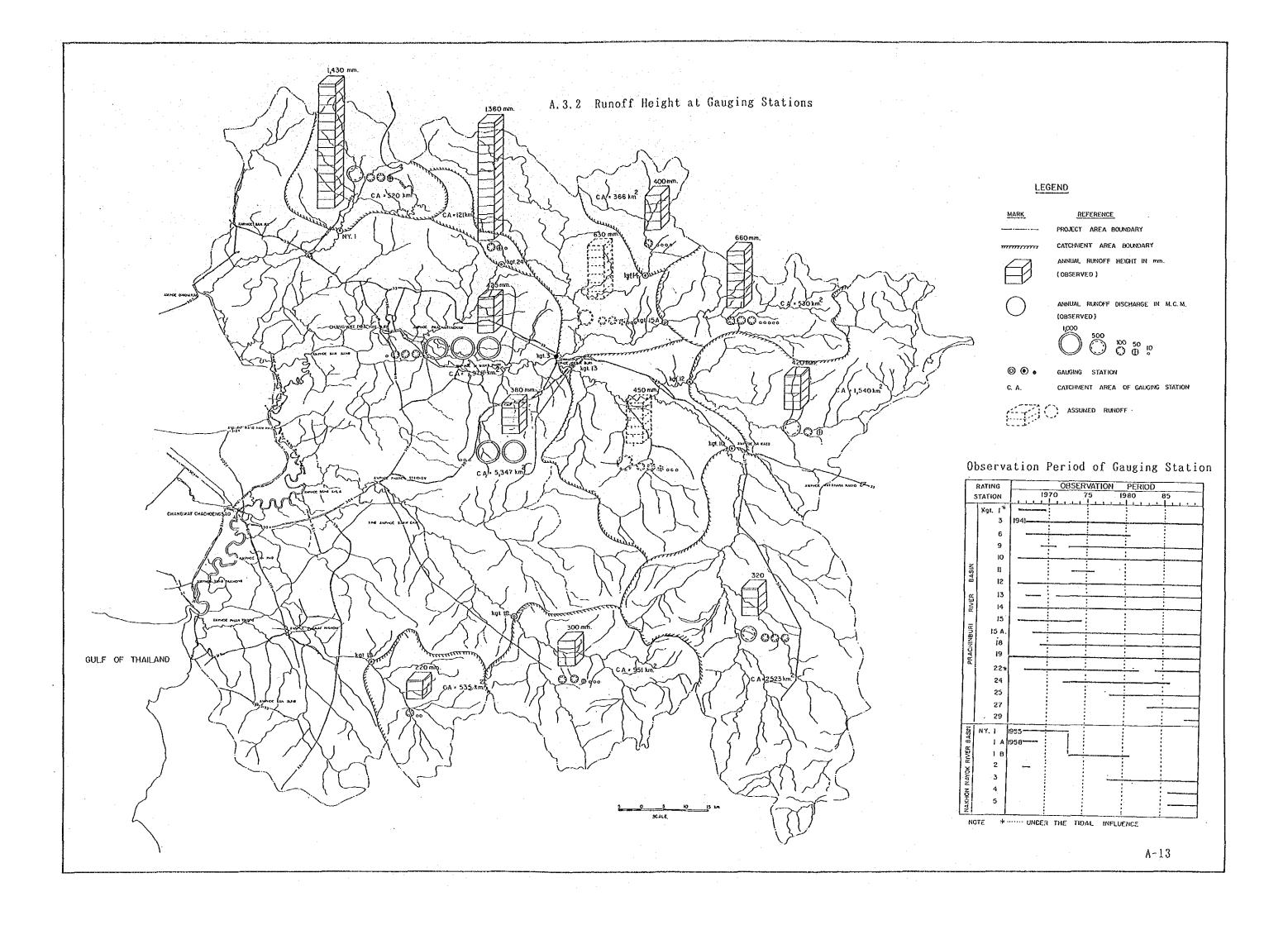
69

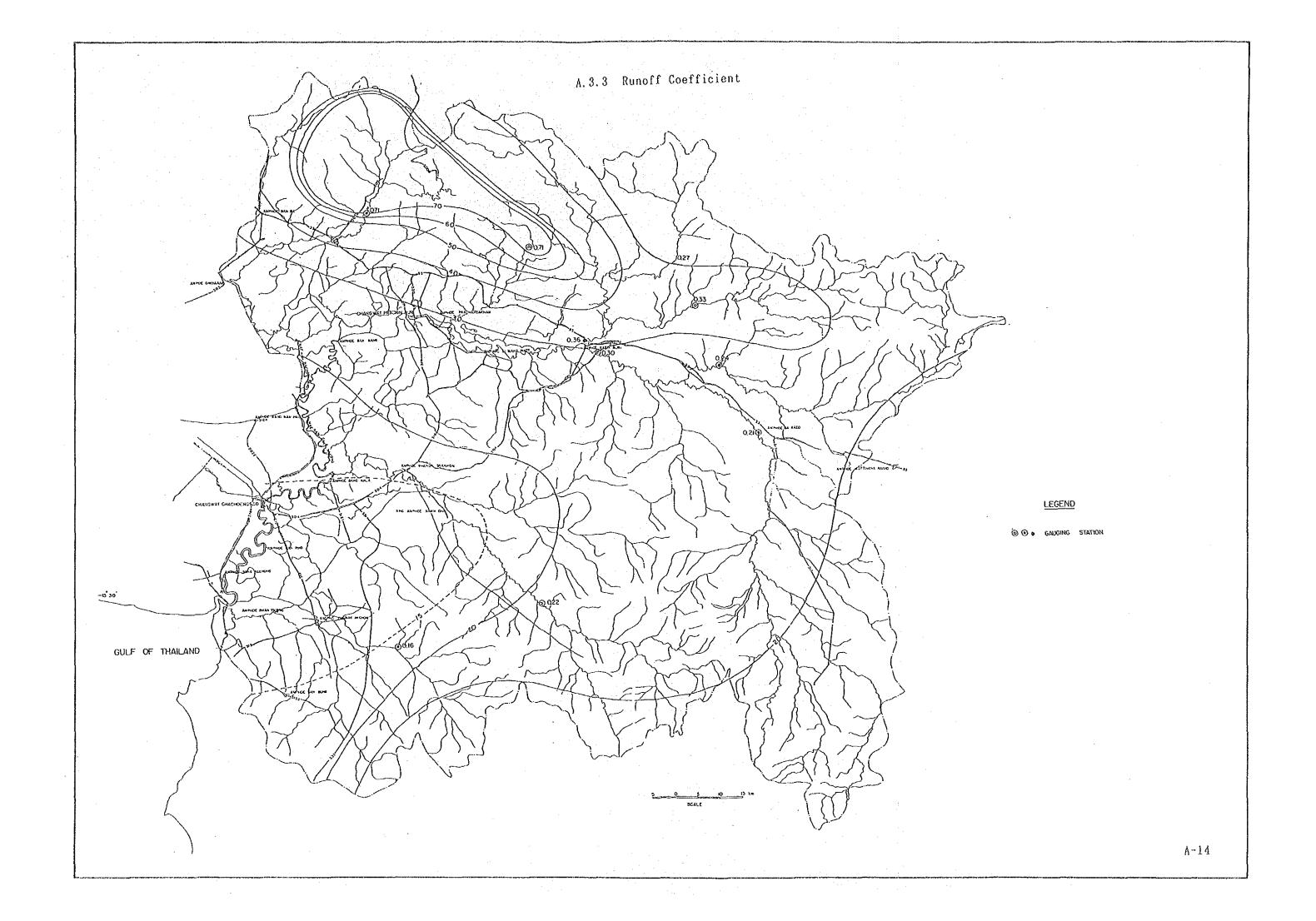
A. 2. 9 Maximum Three Days Rainfall

											-			1.7			٠
Your	ST. 44181	44181		44132		44122	S.L.	22070	Yanı	S.L.	03042	S.C.	03210	ST.	03220	ST.	44032
;	Rain (mm)	U/N	Rain (mm)	O/N	Rain (mm)	O/N	Rain (nun)	N/D		Rain (mm)	8] (1)	Rain (mm)	M/D	Rain (mm)	Q/N	Rain (mm)	Q/N
89	121,4	29 Jun	137,3	29 Jun	0.06	10 Aug	177,4	31 Jul	68	118.8	3' Aug	109.4	15 Agr	1	1	121.0	11 Sep
69	202.4	dos 61	185.7	2 Sep	195.2	16 Jun	207.2	28 Sep	69	147.6	28 May	99,1	20 Sep	1	1	150.2	3 Sep
1970	107.9	1 Sep	83.2	. 9 Jul	112.1	19 Jun	158.2	7 Jun	1970	114.8	20 Jun	188.5	19 Jun	119.0	24 Aug	175.8	15 Aug
7.1	120.5	27 Aug	90.4	26 Aug	146.8	17 Sep	192.6	3 Jul	71	122.7	13 Jun	244.8	15 Jun	189.3	28 Aug	198.5	14 Jun
72	251.7	4 Sep	306.1	S Sep	243.0	4 Sep	204.0	4 Sep	72	148.4	5 Sep	184,5	1 Jun	127.1	6 Sep	195.9	17 Sep
73	172.5	24 Sep	250.4	14 Sep	126.7	4 մաո	147.4	27 Sep	73	87.5	17 Sep	74.8	18 Sep	8.96	26 Sep	126.0	17 Sep
74	115.1	26 Aug	113.1	7 Jun	146.7	9 Oct	109.3	gnv 9	7.4	180.2	17 Oct	125,4	8 Oct	103.7	23 Jul	97.5	23 Apr
75	149.0	10 Jul	220.1	10 Jul	143.9	8 Oct	200.8	10 Jul	75	98.1	4 Sep	1.		•	•	109.7	1 Oct
92	206.6	31 May	263.0	23 Aug	324.0	30 Jun	239.6	28 Aug	92	109.6	12 Sep	119.2	11 Sep	160.7	22 Jul	1.93.1	27 Jul
77	129,1	9 Sep	143.8	19 Aug	186.5	dos 6	102.7	o Sep	11	109.7	19 Jun	112.5	19 Jun	200.7	20 Sep	171.7	das 6
78	146.6	27 Sep	210.2	28 Sep	180.4	20 Jul	159.6	9 Sep	7.8	95.5	28 Sep	ı			•	180.2	21 Jun
79	122.3	23 Sep	227.9	21 Sep	260.3	22 Sep	150.8	22 Sep	62	95.9	3 May		.	1	1	159.1	23 Sep
1980	155.5	28 Sep	152.5	26 Aug	227.7	16 Jun	147.7	24 Aug	1980	109.6	4 Aug	123.5	29 Sep	t ,	1	144.2	9 Sep
8	154.9	20 Sep	154.6	19. Sep	180.9	dos 6t	122.7	30 Aug	81	147,1	18 Sep	73.1	12 Sep	263.1	17 Sep	199.6	19 Sep
82	132.2	17 Jul	88.0	das s	159.7	19 Aug	156.0	23 Sep	82	92,4	13 Apr	90.0	16 Sep	85.0	24 Aug	130.7	3 Jun
83	200.9	8 Jun	168.7	3 Aug	233.2	27 Sep	206.0	9 Oct	83	138,5	17 Aug	226.3	3 Aug	142,6	3 Aug	139.7	13 Aug
2.2	116.5	22 Sep	•	.	205.1	9 Aug	138.0	10 Jul	80	150,4	unc 9	160.5	9 Aug	98.4	4 Jun	98.7	8 Aug
85	103,9	2 Jul	130.7	11 Jul	182.5	16 Apr	223.0	10 Jul	85	132,2	17 Sep	96.7	21 Oct	117.3	25 Jul	149.6	3 Sep
98	1.18.6	9 May	168.4	24 Aug	197.0	8 May	325.0	14 Aug	98	181.9	9 May	202.7	gny 6	179.4	guy 6	178 3	24 Aug
87	161.4	9 Sep	132.8	s Sep	117,1	7 Jun	164.3	5 Sep	87	105,4	Nov 1	14.5	31 Oct	114,6	26 Sep	161.0	3 Jul









A.3.4 Runoff Model

The model parameters such as the dimension of tank, effective rainfall and daily distribution factors were estimated using some selected data of actual observations of discharges on the river systems included in the Study.

Depletion Coefficient (k)

The k values used in the generation of daily runoff were determined using the equation described as under;

 $Q_1 = Q_0 \times e^{-kt}$

where: Q_1 = outflow from tank outlet at time t_1 in mm/day

 Q_0 = outflow at time t_0 in mm/day

e = natural number = 2.71828

k = depletion coefficient

 t_0 , t_1 = time in day

The equation connotes that during period of no rain, outflow from the tank would diminish continuously according to the magnitude of k, meaning that the value of k could be determined by the depletion curve as shown in Figure 4-7. The depletion coefficients for the river systems were determined from hydrographs drawn with the daily streamflow observations at gauging stations.

Height of Tank (HT)

Overflow from the tank occurs when the tank filled with rain water. The capacity of the tank to hold rain water, denoted in the runoff model as the specific height of tank, HT, is given in the following equation.

HT = Qmax/k

where: HT = finite height of tank in mm

Qmax = runoff discharge on the depletion curve where

overflow from the tank occurs, in mm

k = depletion coefficient

Tank Dimensions for Various Basins

For basins of proposed dams and irrigation blocks where no runoff data applicable in determinating a depletion coefficient, k, and a height of tank, HT, are available, their values were estimated on a log-log paper by plotting the already computed values against the topographic/geographic condition of drainage areas, as shown in Figure 4-8. The topographic or geographic condition was expressed in terms of the drainage areas, river density, form factor and compactness of the drainage areas.

- Drainage Area = measured on 1/50,000 scale maps, in sq.km.
- River Density = TL/A in km/sq.km

where TL = total length of stream inclusive of tributaries in km

A = drainage area in sq.km.

- Form Factor = A/L/L

where L = length of main stream in km

- Compactness = sq.rt(A)/LB

where LB = length of boundary of drainage area

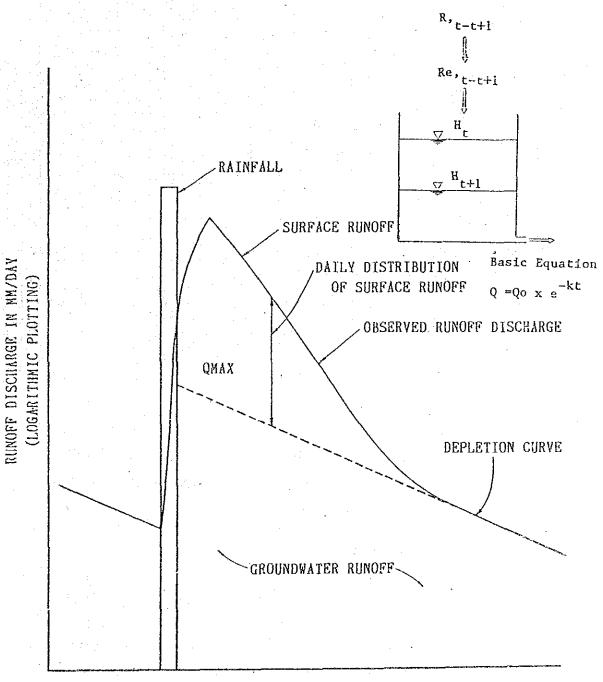
in km

 π = ration of circumference of a circle to its diameter

As is seen from Figure 4-8, the Form Factor, A/L/L, correlates well with both the k and HT, hence the following equations were used to determine tank dimension for the proposed storage damsite, where no measurement of streamflow is available.

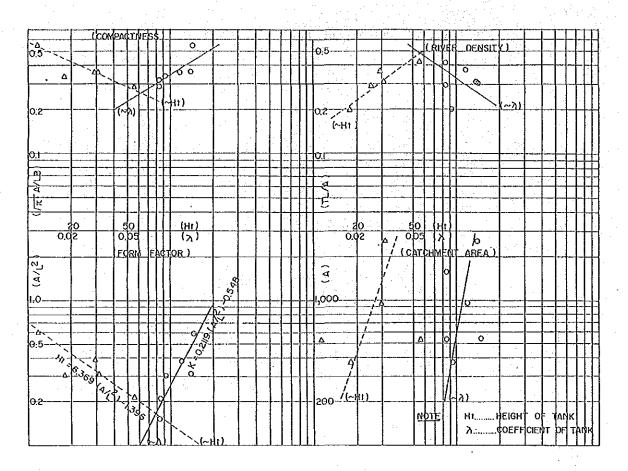
- Ht = 6.361 (A/L^2) 1.396, for estimation of tank height, and
- K = 0.2119 (A/L^2) 0.548, for depletion coefficient

A.3.5 Estimating Depletion Curve



TIME IN DAY (NORMAL PLOTTING)

A. 3.6 Tank Model Parameters and Geographic Conditions



<u>C</u>	ATCHMENT	TANK DI	MENSION	RIVRER	DENSITY	FORM	FACTOR	COMPAC	TNESS
STATION	AREA	<u> </u>	<u> </u>	<u>TL</u>	TL/A	<u>L A</u>	<u>/L/L</u>	<u>LB</u>	A/LB
	km			km		km	-		
Kgt.3	7,502	0.069	24.9	2.180	029	150	0.33	2.750	0.056
10	2,523	0.1407	31.2	780	0.31	90	0.31	250	0.36
12	1,540	0.0847		440	0.29	100	0.15	220	0.32
14	366	0.0937	18.1	75	0.20	35	0.30	100	0.34
15A	530	0.0847	55.8	220	0.42	50	0.21	140	0.29
18	951	0.120	29.5	350	0.37	50	0.38	150	0.36
19	535	0.146	11.6	160	0.30	30	0.59	75	0.55

A.3.7 Annual Sub-basin Runoff in 20 Years

en e						(UNIT:MCM/YEAR)				
SUB-									ENTIRE	
BASIN	UPP	KPS	MPP.	MHM	UBP	MNN	KTL	LBP	-BASIN	
(km ²)	(1,628)	(2,643) (970)	(2, 130)	(2,757)	(1,933)	(2,493)	(3, 106)	(17,660)	
	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1									
1968	558	782	413	1,117	1,404	1,278	598	700	6,850	
69	704	890	503	1,535	1,572	1,680	650	643	8,177	
70	693	927	533	1,295	1,752	1,864	1,013	746	8,823	
71	582	774	484	1,285	1,523	1,544	660	734	7,559	
72	687	950	503	1,428	1,554	1,736	565	624	8,047	
73	613	856	461	1,231	1,205	1,272	534	636	6,808	
74	616	849	494	1,421	1,424	1,432	498	779	7,513	
75	587	852	482	1,680	1,337	1,688	685	623	7,934	
76	806	958	673	1,527	1,494	1,732	694	673	8,557	
77	657	779	572	1,324	1,370	1,249	732	567	7,250	
78	654	700	600	1,596	1,381	1,363	758	627	7,679	
79	721	842	605	1,574	1,231	1,228	737	452	7,390	
1980	809	926	709	1,679	1,673	1,683	799	600	8,878	
81	727	1,006	628	1,639	1,773	1,662	1,107	677	9,219	
82	745	876	604	1,350	1,417	1,667	597	615	7,871	
83	859	1,070	715	1,524	1,804	2,015	894	848	9,729	
84	725	833	582	1,542	1,405	1,461	602	564	7,714	
85	752	925	581	1,390	1,445	1,581	615	510	7,799	
86	736	946	593	1,263	1,526	1,666	702	668	8,100	
87	579	801	460	1,242	1,337	1,076	<u>570</u>	666	6,731	
* *										
MEAN	690	877	560	1,431	1,481	1,544	700	648	7,931	
MAX.	859	1,070	715	1,679	1,804	2,015	1,107	848	9,729	
MIN.	558	700	413	1,117	1,205	1,076	498	452	6,731	
	: :									
1/10	586	766	455	1,221	1,276	1,238	541	542	6,971	
1/ 5	621	801	488	1,287	1, 339	1,338	577	571	7,257	

A.3.8 Monthly Runoff in Upper Phra Prong (UPP) basin

- •		A. 3.	8 Mo	nthly			Upper	Phra	Prong	(UPP) bas	in	
				# BAH	G PAKONG		ASIN DEV	ELOPHENT	STUOY=				
	. UPPER I	PHRA PRO	NG SUB-B	ASIN		(C.A.= 16	28.0 SQ.1	KH)	c u	NIT= RA	IN. OHD	RUNOFF(HCH)
		KAY	ومانت مانات مع	JUL	AUG.	SEP.		x :	£	JAN.	FEB.	HAR.	АИИА
1968	132.0 70.018 0.326	132.8 51.730	136.2 66.815 0.301	213.4 64.728 0.186	181.8 90.411 0.305	314,3 90.655 0.177	101.3 76.205 0.462	6.1 11.355 1.142	0.0 1.108 0.000	14.1 4.457 0.194	61.0 22.526 0.227	21.5 7.495 0.214	1314. 557.50 0.26
1969	44.9 13.730 0.188		278.4 94.396 0.208	342.7 121.961 0.219	265.7 122.657 0.284	491.7 174.614 0.218	139.1 85.568 0.378	16.8 22.827 0.836	0.0 1.769 0.000	9.6 3.020 0.194	23.1 7.997 0.212	35.2 6.903 0.121	1815. 703.53 0.23
1970	152.0 31.947 0.129	180.2 79.361 0.270	300.5	224.8	325.5	263.8 105.355	182.8 90.837	35.8 29.404	100	1.7 3.088 1.127	22.8 4.301 0.116	26.0 11.260 0.266	1761. 692.64 0.24
1971	90.4 30.466 0.207	140.8 42.078 0.184	274.0 102.218 0.229	202.3 76.400 0.232		314.1 112.684 0.220	158.3 77.675 0.301		0.7 2.055 1.806	0.0 0.277 0.000	52.9 18.069 0.210	56.5 12.227	1509. 581.67
1972	196.5 74.532 0.233	47.9 22.508 0.289	176.4 63.264 0.220			434.1 147.475 0.209	174.7 97.663 0.343	136.9 55.864 0.251	30.6 25.456 0.511	1.3 2.467 1.206	7.7 2.185 0.175	60.1 14.471 0.148	1752. 686.99 0.24
1973	55.6 18.256 0.202	104.3 39.547 0.233		341.1 103.921 0.187		111.627	177.4 110.521 0.383	29.863	5,184	21.2 2.323 0.067	24.8 11.721 0.291	148.0 42.788 0.178	1591. 612.57 0.23
1974	110.4 45.735 0.255	190.0 66.257 0.214	202.7 76.362 0.231	140.1 59.261 0.260	232.5 76.540 0.202	85.028	105.972	45.485	2.7 7.389 1.673	25.1 8.673 0.212	37.9 10.761 0.174	82.8 29.000 0.215	1551.
1975	12.611	201.7 53.853 0.164		93.940	295.7 110.230 0.229	82.454	86.618	27.796	3.9 4.808 0.752	0.0 0.402 0.000	25.3 8.005 0.194	112.0 24.898 0.136	1531. 586.75 0.23
1976	97.2 36.647 0.232			147.408	310.5 117.530 0.233	128.815	123.408	91.311	0.0 8.233 0.000	0.0 0.569 0.000	3.3 0.671 0.124	11.8 2.850 0.149	2016. 806.07 0.24
1977	97.9 24.989 0.157	201.8 57.293 0.174		294.1 90.925 0.190			87.519	43.633	0.0 8.110 0.000	3.5 1.093 0.194	21.8 6.419 0.181	62.5 18.759 0.184	1696. 656.81 0.23
1978	31.5 15.756 0.307	288.6 77.910 0.166	234.4 99.320 0.260		257.1 120.610 0.288		86.591		0.0 2.993 0.000	16.9 5.500 0.200	24.7 2.097 0.052	20.3 13.397 0.406	1659. 653.64 0.24
1979	98.1 26.628 0.167	266.8 77.230 0.178		335.5 151.292 0.277	97.982		104.841	27.542	0.0 3.322 0.000	0.0 0.235 0.000	45.0 5.329 0.073	48.5 21.675 0.275	1865. 721.91 0.23
1980	52.3 23.708 0.278	159.3 46.961 0.181			116.232		144.044		0.0 3.720 0.000	0.0 0.252 0.000	51.5 2.433 0.029	66.9 38.150 0.350	2061. 808.75 0.24
1981	69.8 18.167 0.160		303.1 111.589 0.226		124.756	348.2 112.769 0.199	92.946		0.0 13.047 0.000	0.0 0.838 0.000	74.0 22.094 0.183	58.6 12.011 0.126	1892. 727.45 0.23
1982	111.5 45.667 0.252	176.3 56.321 0.196	297.2 89.462 0.185	206.8 108.350 0.322	508.5 165.035 0.199	297.0 134.976 0.279	150.6 69.391 0.283	61.7 45.613 0.454	4.9 10.573 1.316	3.5 1.863 0.331	46.6 9.242 0.122		1864. 745.14 0.24
1983	36.6 5.469 0.092	104.7 25.440 0.149	317.2 105.674 0.205	121.949	162.209		209.492	47,1 52,678 0,687	7.7 6.271 0.501	11.0 5.318 0.297	20.8 5.779 0.171	104.2 21.119 0.124	2260. 859.06 0.23
1984	91.9 43.170 0.289	132.3 43.086 0,200	333.9 120.626 0.222		508.2 164.559 0.199	292.5 117.406 0.247	103.908	29.7 21.740 0.450	0.0 3.201 0.000	8.8 1.735 0.121	30.2 9.261 0.188	67.5 18.445 0.168	1827. 725.27 0.24
1985	241.4 55.596 0.141	268.6 120.898 0.277	273.0 98.853 0.222	272.4 118.689 0.268		378.2 129.896 0.211	77.805		0.0 8.204 0.000	0.0 0.527 0.000	47.7 3.943 0.051	61.5 24.513 0.245	1928. 751.79 0.23
1986	107.0 42.840 0.246	281.2 104.184 0.228	172.8 61.405 0.218	259.0 93.163 0.221	285.4 103.047 0.272	369.0 127.120 0.212	129.916	3.0 22.116 4.459	8.4 4.817 0.351	0.0 0.332 0.000	78.5 14.745 0.115	85.7 32.293 0.231	1891. 735.97 0.23
1987	92.0 41.090 0.274	168.2 48.492 0.177	327.3 107.755 0.202	163.8 90.760 0.340	0.316	347.3 119.388 0.211		80.0 39.459 0.303	0.0 5.220 0.000	0.0 0.333 0.000	41.5 8.091 0.120	30.9 17.887 0.355	1444. 579.08 0.24
VERAGE (HH) (HCH) (X)	96.3 33.851 0.216		255.5 90.011 0.216	259.4 101.205 0.240	284.5 109.357 0.236		190.9 100.793 0.324	45.0 37,410 0,510	5.2 7.742 0.911	5.8 2.165 0.228	37.1 8.783 0.146	58.0 18.940 0.201	1761.9 690.456 0.241

A.3.9 Monthly Runoff in Khlog Phra Sathung (KPS) basin

* BANG PAKONG RIVER BASIN DEVELOPHENT STUDY*

	* KHLONG	PHRA SA	THUNG SU	B-BASIN		(C.A.= 26	43.0 SQ.1	KH) .	(1	JNIT= RA	1R. (HR) ,	RUNOFF (HCH)
YEAR	APR.	HAY	JUN.	JUL.	AUG.	SEP.	001.	, VOK	OEC.	JAN.	FEB.	HAR,	ANNUAL
1968	158.1 98.876	123.4 76.880	157.9	205.9 103.539	249.7 157.284	268.8 120.871	104.9 92.161 0.332	4,8 14,293	0.0	4.5 1.795 0.152			1331.8 782.061 0.222
1969	44.2 15.594 0.133	140.7 61.301 0.165	213.1 108.858 0.193	130.286	154.752	426.9 227.153 0.201		40.727		8.1 3.957 0.185	34.5 17.026 0.187	55.0 19.113 0.131	1631.8 890.469 0:206
1970	148.3 59.730 0.152	123.1 83.884 0.258	269.8 125.157 0.176	253.3 149.438 0.223	304.7 156.445 0.194	241.4 130.996 0.205	149.6 107.628 0.272	44.2 26.883 0.230	77.6 62.264 0.303	0.0 3.393 0.000	22.5 5.704 0.096	21.6 15.286 0.268	1656.2 926.807 0.212
1971	71.3 31.795 0.169	156.6 68.903 0.166		164.4 92.740 0.213	101.744	133.867	114.051		6.239	0.0 7.618 0.000	34.9 18.252 0.198	47.0 13.409 0.108	774.386 0.207
1972	189.9 101.823 0.203	55.6 33.364 0.227	254.2 122.852 0.183	258.2 133.374 0.195	252.5 157.592 0.236	359.4 175.266 0.184	131.5 102.978 0.296	125.1 68.863 0.208	25.3 30.592 0.457	0.3 1.620 1.778	9.2 3.674 0.151	48.1 18.010 0.142	1709.4 950.006 0.210
1973	34.1 22.616 0.251	101.7 48.317 0.180	79.886	150.536	137.748	321.7 163.591 0.192	125.444	81.3 51.621 0.240	7.258	10.4 1.699 0.062	27.0 13.127 0.184	119.1 54.309 0.173	1561.4 856.151 0.207
1974	127.2 69.594 0.207	155.2 77.063 0.188	163.1 99.827 0.232	142.8 72.185 0.191	149.382	165.0 117.680 0.270	148.734	52.873		25.5 12.447 0.185	37.6 15.917 0.160	51.0 26.938 0.200	1513.0 849.031 0.212
1975	27.0 19.726 0.276	79.513	248.5 137.100 0.209	135.878	178.705	125.823	108.691	28.822	2.9 3.949 0.511	0.0 0.258 0.000	28.1 13.406 0.180	74.6 20.423 0.104	1564.9 852.293 0.206
1976	83.6 46.125 0.209	93.836	183.2 101.779 0.210	334.0 160.787 0.182	158.011	161.094	139.430	62.3 80.394 0.488	0.0 4.998 0.000	1.5 0.839 0.208	2.1 1.250 0.224	21.5 9.892 0.174	1692.7 958.434 0.214
1977	61.3 24.928 0.154	164.8 69.702 0.160					121.9 92.546 0.287	16.9 29.983 0.673	1.1 4.088 1.368	19.6 7.646 0.148	28.3 17.084 0.228	57.8 27.198 0.178	1413.8 778.931 0.208
1978	35.3 21.111 0.227	254.7 102.571 0.152	169.4 105.831 0.236	210.4 111.857 0.201	166.5 106.724 0.242	251.9 105.501 0.158	109.4 99.122 0.343	18.1 26.935 0.564	0.0 1.838 0.000	6.9 3.345 0.184	12.4 1.956 0.059	21.4 13.488 0.238	1256.4 700.278 0.211
1979	79.4 34.424 0.164		118.744	175.762	184.6 125.960 0.258	151.241	80.192	15.5 20.296 0.495	0.0 2.027 0.000	0.0 0.138 0.000	20.6 5.417 0.100	38.6 20.394 0.200	1527.8 841.580 0.208
1980	50.7 28.622 0.214	169.3 74.345 0.166	338.7 150.024 0.168	135,245	123.329	276.4 161.206 0.221	150.722	39.5 46.467 0.445	0.0 3.297 0.000	0.0 0.178 0.000	46.5 4.130 0.034	54.9 48.203 0.332	1664.9 925.767 0.210
1981	104.4 38.687 0.140			114.082		159.714	120.363	107.0 64.182 0.227	0.0 18.768 0.000	0.0 0.690 0.000	40.4 17.856	29.0 8.161 0.106	
1982	106.5 59.592 0.212	72.575	287.2 125.367 0.165	140.397		139.110	75.589		12.7 10.917 0.325		44.5 14.462 0.123	0.0 10.054 0.000	1560.2 876.358 0.213
1983	45.6 9.374 0.078	153.2 46.659 0.115	257.5 160.121 0.235	128.077	422.8 208.840 0.187	150.585	352.9 234.332 0.251	73.5 66.871 0.344		19.2 9.517 0.188	17.1 9.199 0.203	105.7 - 39.941 - 0.143	1980.6 1070.254 0.204
1984	67.0 46.316 0.262	140.3 63.521 0.171	279.9 145.195 0.196	105.2 84.313 0.303			136.2 109.496 0.304	16.2 16.219 0.379	0.0 1.915 0.000	16.7 4.733 0.107	29.1 16.167 0.210	49.3 20.470 0.157	1484.3 832.901 0.212
1985		218.3 129.498 0.224	145.211	293.0 170.469 0.220			147.8 94.743 0.242	44.6 41.154 0.349	0.6 6.943 4.518	0.0 0.337 0.000	28.2 5.451 0.073	23.9 16.283 0.258	1663.3 925.386 0.211
1986	42.553	158.196	154.2 90.743 0.223	106.760	290.6 145.961 0.190	362.0 179.654 0.188	197.8 149.988 0.287	8.8 23.129 0.991	15.0 9.712 0.245	0.0 0.391 0.000	42.8 12.912 0.114	69.6 26.074 0.142	1741.4 946.072 0.206
1987		133.8 66.370 0.188	304.7 144.090 0.179	137.7 103.185 0.283	196.1 95.326 0.184	291.5 165.357 0.215	90.8 63.076 0.263	93.9 56.609 0.228	0.0 10.294 0.000	0.0 0.389 0.000	56.7 24.512 0.163	0.302	1407.6 800.519 0.215
AVERAGE (HH) (HCH) (X)	89.3	82.084 1	234.3 21.513 1 0.196		46.613 1	285.3 51.043 1 0.200	15.956	46.4 42.242 0.345	8.3 10.047 0.459		29.8 11.794 0.150	46.4	1580.6 877.174 0.210

A.3.10 Monthly Runoff in Middle Phra Prong (MPP) basin

■ BANG PAKONG RIVER BASIN DEVELOPHENT STUDY=

_	* XIDOLE	PHRA PH	RONG SUB	-BASIN			C.A.≃ 9	70.0 SQ.)	(H)	((INIT= RA	IN. (MH).	RUNOFF (HCH)
YEA	R APR.	HAY	JUN.	JUL	AUG.	SEP.	OCI.	ROV.	DEC.	JAN.	FEB.	HAR.	ANNUAL
196	8 76.8 32.437 0.436	103.7 26.864 0.267	146.5 44.537 0.313	259.4 55.080 0.219	215.7 84.992 0.406	337.6 80.225 0.245	98.7 53.979 0.564	7.5 6.663 0.921	0.0 0.868 0.000	21.1 5.122 0.251	64.3 18.257 0.293	11.9 3.842 0.333	1343.1 412.865 0.317
196	9 34.0 6.361 0.193	37.297	72.442	397.1 109.549 0.284	93.998	375.8 108.153 0.297	52.250	12.0 13.105 1.122	0.0 0.797 0.000	0.248	10.0 2.470 0.254	34.4 5.790 0.173	1745.7 503.131 0.297
197	0 99.0 20.222 0.211	51,812	100.351	214.5 84.726 0.407	422.2 100.632 0.246	81.464	57.260	16.5 13.355 0.835	14.148	1.2 1.530 1.328	6.7 1.040 0.160	25.3 6.005 0.245	1826.7 532.544 0.301
197	1 142.5 29.577 0.214	148.5 39.337 0.273	307.0 87.457 0.294	259.6 72.274 0.287	248.4 67.212 0.279	280.4 80.515 0.296	192.5 63.176 0.338	7.5 23.068 3.157	0.7 1.355 1.984	0.0 0.193 0.000	33.6 8.694 0.267	60.0 10.891 0.187	1680.7 483.748 0.297
197	41.760 0.288	50.4 15.772 0.323	168.6 45.302 0.277	231.7 60.092 0.267	280.1 78.568 0.289	462.4 129.365 0.288	149.9 59.353 0.408	113.5 33.974 0.309	47.3 21.380 0.466	1.4 1.952 1.467	0.0 0.194 0.000	75.9 14.790 0.201	1730.4 502.501 0.299
197	3 51.0 12.437 0.251	169.6 45.160 0.274	154.7 47.579 0.317	309.0 82.567 0.275	266.7 69.079 0.267	306.1 84.044 0.283	140.7 66.909 0.490	45.6 16.604 0.375	0.0 2.871 0.000	17.9 1.605 0.093	26.7 8.497 0.328	95.7 23.629 0.254	1583.9 460.980 0.300
197	4 131.5 29.844 0.234	51.656	64.825	199.5 54.817 0.283	284.8 70.555 0.255	172.6 67.003 0.400	90,505	61.3 36.447 0.613	0.0 3.691 0.000	20.0 5.180 0.267	14.8 3.463 0.242	68.5 15.697 0.236	1693.2 493.682 0.301
197	36.5 10.559 0.298	41.054	268.8 68.216 0.262	248,2 86,247 0,358	87.330	62.043	72.782	37.3 22.719 0.627	1.3 2.899 2.259	0.0 0.143 0.000	46.1 11.817 0.264	92.4 16.484 0.184	1678.3 482.292 0.296
197	6 56.2 18.859 0.346	42.224	77.824	145.511	97.889		101.604	107.8 67.019 0.641		0.3 0.369 1.109	2.0 0.027 0.014	9.5 2.311 0.251	2285.5 673.088 0.304
197	7 94.6 19.055 0.208	43.418	59.589		342.3 96.268 0.290	439.0 134.093 0.315	64.645	27.0 34.838 1.330	0.0 6.620 0.000	12.9 3.249 0.260	17.0 2.830 0.172	51.3 12.819 0.257	1985.3 572.217 0.297
197	8 35.4 11.626 0.339	51.531	91.840	396.9 103.179 0.268	114.861	120.751	98.3 63.972 0.671	30.1 20.439 0.701	0.0 2.027 0.000	23.9 5.976 0.258	30.5 2.334 0.079	15.4 10.976 0.735	2053.2 599.511 0.301
197	9 148.9 27.950 0.194	80.002	78.062	132.775	219.7 78.468 0.368		62.075	23.3 18.618 0.823	0.0 1.809 0.000	0.0 0.087 0.000	35.7 2.155 0.062	51.1 16.855 0.340	2108.1 604.725 0.296
198	0 20.3 10.831 0.551	25.916				512.5 143.074 0.288	103.056	26.4 27.235 1.062	2.445	0.0 0.117 0.000	32.9 1.342 0.042	99.3 28.324 0.294	2469.3 709.160 0.296
198	1 107.2 21.126 0.203	63.657	87.816	335.5 94.392 0.290	401.5 120.919 0.311	374.9 103.786 0.285	112.9 55.358 0.506	153.1 42.496 0.286	0.0 13.641 0.000	0.654	65.3 15.765 0.249	63.0 8.241 0.135	2177.9 627.850 0.297
198	2 96.5 32.728 0.350	52.449	78.446	270.2 99.201 0.378			141.6 55.040 0.401	34.0 24.752 0.750	9.9 6.354 0.661	3.8 1.371 0.375	0.0 0.082 0.000	0.0 0.005 0.000	2039.1 604.105 0.305
198	3 5.3 0.264 0.051	21.937	368.4 93.806 0.263	371.6 105.841 0.294	168.307 0.280		140.959 0.370		0.202			79.5 13.752 0.178	
198	93.8 30.338 0.333		107.853	67.829	485.6 125.797 0.267	309.0 85.649 0.286	. 76.242	28.6 14.181 0.511	0.3 1.887 7.369	14.9 2.090 0.145	7.130	79.5 13.834 0.179	70,1.247
198	5 208.3 46.128 0.228	81.264	83.141	257.6 75.520 0.302		433.8 114.512 0.272		37.9 29.825 0.810	0.2 5.322 23.751	0.0 0.256 0.000	33.5 1.968 0.061	51.9 14.628 0.290	1990.7 581.185 0.301
198	33.387 0.311	75.169 0.275		253.4 72.511 0.295		421.3 117.035 0.286	240.7 91.544 0.392	0.4 15.540 35.760	5.5 2.332 0.441	0.0 0.145 0.000	7.468	44.7 14.278 0.329	2034.0 592.893 0.301
198	21.370 0.270	31.757	78.285 0.290	0.332	55.609	324.3 83.600 0.266	ብ ልንብ	0.355	0.0 4.772 0.000		0.092	22.2 24.246 1.124	1566.3 459.759 0.303
AYERA (HH) (HCH) (X)	89.0 22.843 0.265	197.3 46.439 0.243	0.277	0.299	339.3 97.438 1 0.296	366.6 101.978 0.287	194.1 72.117 0.383	44.6 25.985 0.600	5.8 5.142 0.914	0 288	31.4 5.520 0.181	51.6 12.870 0.257	1925/8 559, 678

A.3.11 Monthly Runoff in Maenum Hanuman (MHM) basin

. BANG PAKONG RIVER BASIN DEVELOPMENT STUDY.

	* NAEHUHAH HUHAK	N SUB-BASIN		(C.4	.= 2130	0.0 SQ.¥	(H)	()	INIT= RAI	и. око 🕠	RUNOFF (NCN)
YEAR	APR. HAY	JUN. JUL.	AUG.	SEP.	OCT.	NOV.	DEC.	JAR.	FEO.	KAR.	JAUNHA
1968	94.4 139.9 67.182 109.657 0.334 0.368	178.6 253.0 115.201 172.695 0.303 0.320	243.5 221.741 0.428	265.3 181.863 11 0.322	104.3 8.874 0.535	12.2 18.312 0.702	0.0 2.875 0.000	61.7 40.135 0.305	41.1 37.237 0.426	58.3 31.817 0.256	1452.3 1117.587 0.361
1969		335.5 373.6 234.914 289.521	306.2 234.946	541.0 372.960 17	211.8			1.0 0.761 0.366	8.8	42.2	2081.3 1535.006 0.346
1970	131.2 198.9 62.353 148.241 0.223 0.350	293.9 220.7 194.784 175.975 0.311 0.374	302.9 211.242 0.327	252.0 194.936 17 0.363	233.9 74.232 0.350	16.5 54.406 1.545	46.4 38.418 0.389	7.0 7.443 0.497	13.404	25.2 19.803 0.369	1752.2 1295.235 0.347
1971	99.5 151.0 59.913 93.209 0.283 0.290	358.1 283.6 250.197 224.390 0.328 0.371	203.301		11.307	. 22.042	0.3 2.574 3.582	0.0 0.251 0.000		43.9 21.202 0.227	1703.6 1257.929 0.347
1972	64.948 40.427	254.6 269.7 156.583 198.826 0.289 0.346	216.648	408.735 17	75.924			0.6 2.449 1.810	1.176	53.4 26.898 0.236	1918.6 1427.666 0.349
1973	37.1 121.7 27.427 82.829 0.347 0.319	127.004 160.823	150.234	360.857 18		38.8 34.173 0.414	0.0 5.277 0.000	10.6 2.558 0.113		97.9 71.520 0.343	1648.3 1230.718 0.351
1974	152.5 273.8 89.233 185.840 0.275 0.319	245.995 173.715	229.650	142.766 21	276.2 13.249 0.362	64.4 71.097 0.518	0.1 7.933 55.350	20.4 13.309 0.307	15.2 10.194 0.314	75.0 37.853 0.237	1898.9 1420.832 0.351
1975	46.4 163.0 44.529 84.341 0.451 0.243	275.657 260.969	319.395	272.548 27		58.7 64.708 0.518	4.8 8.800 0.869	0.0 0.461 0.000	36.8 16.681 0.213	99.7 60.260 0.284	2257.7 1679.794 0.349
1976	39.6 164.4 39.648 96.319 0.470 0.275	268.6 361.0 175.860 274.650 0:307 0.357	291.238	266.287 20		114.6 136.229 0.558	8.7 10.421 0.560	0.0 4.151 0.000	4.5 0.164 0.017	38.1 25.178 0.310	2042.6 1526.963 0.351
1977	99.3 200.0 67.531 113.842 0.319 0.267	142.841 216.916	243.219	266,258 16			0.2 17.388 39.808	13.4 1.474 0.052	10.7 14.662 0.641	42.6 15.757 0.174	1785.5 1323.740 0.348
1978	72.9 279.0 65.493 153.128 0.422 0.258	221.453 251.799	309.021	356.336 16	139.0 3.494 0.552	32.9 41.458 0.592	0.0 7.516 0.000	19.6 13.469 0.322	12.7 2.774 0.103	5.6 10.404 0.866	2135.7 1596.344 0.351
1979		401.8 382.5 272.004 296.978 0.318 0.365	221.147	345,459 9	61.4 18.439 0.752	9.7 28.873 1.395	0.0 1.798 0.000	0.0 0.067 0.000	48.6 22.194 0.214	40.1 34,384 0.402	2173.9 1574.307 0.340
1980	42.3 127.4 32.773 72.598 0.364 0.267	253.642 280.400	340.872	344.131 22	252.1 23.837 0.417	7.6 39.817 2.473	0.0 2.559 0.000	0.0 0.111 0.000	33.0 11.690 0.166	113.2 76.725 0.318	2292.2 1679.155 0.344
1981	143.5 271.4 85.580 211.478 0.280 0.366	258.793 235.281	273.846	239.736 14	150.8 19.528 0.466	145.5 116.404 0.376	5.8 23.404 1.895	0.0 1.007 0.000	36.2 22.844 0.296	56.8 20.712 0.171	2195.8 1638.611 0.350
1982	64.1 153.7 58.804 92.975 0.430 0.284	155.433 188.825	307.366	282,519 15		78.3 63.306 0.380	5.1 41.197 3.778	3.2 3.806 0.565	0.0 0.296 3.377	0.0 0.027 0.000	1783.6 1349.650 0.355
1983	8.7 112.2 1.806 54.937 0.097 0.230	243.3 271.5 166.109 203.057 0.321 0.351	528.0 365.609 0.325	383.6 260.889 35 0.319	420.5 7.960 0.400	23.1 41.300 0.848	10.7 4.454 0.196	14.1 14.067 0.469	31.9 16.151 0.238	94.9 38.005 0.188	
1984		368.7 195.4 282.338 164.911 0.359 0.396	351,329	240.784 20		39.271	0.0 4.726 107.370	2.4 1.116 0.219	19.0 11.220 0.277	74,3 37.574 0.237	2041.1 1541.727 0.355
1985	188.6 297.5 99.838 229.598 0.248 0.362	246.6 237.4 194.351 177.452 0.370 0.351	151.893			42.7 68.417 0.752	0.0 18.725 0.000	0.0 0.662 0.000		44.8 33.745 0.354	1853.5 1390.178 0.352
1986	154.0 241.5 99.902 175.132 0.305 0.340	158.6 201.4 119.426 147.189 0.354 0.343	200.618	233.862 20 0.339	0.400	1.2 28.542 11.229	10.8 9.084 0.396	0.0 0.437 0.000	37.5 12.310 0.154	46.9 32.567 0.326	1719.2 1263.061 0.345
1987	103,4 158.5 63.137 115.716 0.287 0.343	0.327 0.393	175.349 0.322	308.040 12	6.430 0.523	0.365	0.0 10.243 0.000	0.437	31.857	0.720	1647.1 1242.457 0.354
AVERAGE (HH) (HCH) (X)	92.3 189.5 61.123 123.469 2	284.1 278.7 200.273 212.170 0.331 0.357	341.5 251.236 0.345	387.1 2 275.501 183 0.334 0	10.1 178 5	48.3 9.138 0.575	1.021	7.7 5.417 0.329	27.6 14.392 0.245	53.4 32.087 0.282	1926.3 1430.764 0.349

A. 3. 12 Monthly Runoff in Bang Pakong (UBP) basin

* BANG PAKONG RIVER BASIN DEVELOPMENT STUDY*

	UPPER 1	BANG PAK	ONG SUB-E	BASIN		()	C.A.= 27	57.0 SQ.1	(H)	,	INTT RAT	н. снн) 👉	RUNOFF (NCN)
YEAR	APR.		JUN	JUL.	AUG.	SEP.	OCY.	NOV	DEC.	JAN.	FEB.	MAR.	ANNUAL
1968	145.3 115.116 0.287	103.4 117.241 0.411	153.7 123.520 0.292	340.1 291.630 0.311	290.5 308.880 0.386	244.3 219.353 0.326	124.1 139.707 0.408	22.0 25.053 0.414	0.0 2.713 0.000	35.9 24.889 0.251	9.0 19.382 0.778	20.9 16.711 0.290	1489.3 1404.193 0.342
1969	63.2 48.991 0.281	178.0 133.965 0.273	227.6 222.085 0.354	350.2 333.617 0.346	242.3 222.175 0.333	391.7 364.998 0.338	130.5 129.938 0.361	18.8 37.952 0.732	0.0 1.344 0.000	8.0 4.672 0.211	26.7 22.608 0.308	71.4 49.673 0.252	1708.5 1572.017 0.334
1970	129.0 101.708 0.286	157.8 150.949 0.347	339.4 271.830 0.291	247.3 231.195	518.1 483.846	281.6 251.436 0.324	130.0	10.7	61.8 57.645	0.4	7.4 3.955	21.7 18.235	1905.3 1752.359 0.334
1971	105.1 63.593 0.220	119.716	343.047 0.313	0.321	265.364 0.296	260.2 242.901 0.339	163.220 0.330	58.800 1.356	1.809 0.493	0.000	0.322	0.165	1734.2 1522.948 0.319
1972	110.7 105.982 0.347		269.9 213.525 0.287	159.5 169.800 0.386	267.3 229.782 0.312	371.1 328.576 0.321	227.3 237.874 0.380	123.2 109.025 0.321	55.8 76.062 0.495	0.0 2.636 0.000	0.0 0.064 0.000	43.7 26.484 0.220	1690.4 1553.839 0.333
1973	54.0 47.043 0.316	167.2 132.782 0.288	151.666		233.677	218.348	83.4 121.121 0.527	35.0 32.847 0.341	3,499	0.790	16.654	51.682	1204.800
1974	126.6 81.998 0.235	169.1 138.944 0.298	164.3 180.010 0.397	194.114	295.9 276.204 0.339	164.7 165.154 0.364	241.464	87.9 93.973 0.388	0.9 4.220 1.728	27.5 17.569 0.232	14.8 12.207 0.300	0.310 25.7 18.478 0.261	1583.5 1424.333 0.326
1975	31.0 25.151 0.294	128.4 87.531 0.247		282.6 268.641 0.345		247.8 223.604 0.327	126.709		1.9 3.879 0.755	0.0 0.161 0.000	27.4	31.8 14.880 0.170	1508.4
1976	83.8 52.677 0.228	125.0 101.145 0.293	133.5 91.391 0.248			318.4 292.895 0.334		19.5 58.808 1.092	1.9 2.456 0.466	1.2 0.867 0.256	1.2 0.665 0.198	25.3 22.450 0.322	1680.5 1494.273 0.323
1977	81.1 66.767 0.299	159.2 107.730 0.246	187.272		256.810	303.974			0.0 4.067 0.000	13.3 7.432 0.202	44.2 22.659 0.186	49.1 44.718 0.330	1529.3 1369.948 0.325
1978	43.1 44.305 0.373		256.3 235.915 0.334	298.0 267.368 0.325	218.376	356.8 277.593 0.282	106.560	39.5 36.203 0.332	0.0 7.976 0.000	5.3 4.048	5.9	26.4	1527.3
1979	94.1 72.679 0.280		168.4 154.929 0.334	242.4 224.200 0.336	214.2 211.733 0.359	207.431	75.400	6.773	0.0 0.213 0.000	0.0 0.005 0.000	3.5 2.884 0.300	29.1 14.296 0.178	1368.7 1231.423 0.326
1980	41.9 - 38.287 - 0.331	118.5 87.277 0.267		322.215	338.7 315.676 0.338	385.2 337.066 0.317	186.483	14.8 35.492 0.872	0.0 1.056 0.000	0.0 0.022 0.000	19.6 8.528 0.158	53.3 43.148 0.294	1866.6 1672.560 0.325
1981	131.8 88.476 0.244			355.5 346.980 0.354	388.402	233.4 191.517 0.298	104.647		0.3 17.882 20.782	0.0 0.335 0.000		18.901	1925.7 1773.432 0.334
1982	77.5 61.196 0.287	127.9 87.159 0.247				280.0 254.126 0.329		31.650	32.8 34.819 0.385	0.1 0.832 2.573	0.0 0.023 3.742	3.5 2.105 0.215	1557.7 1417.383 0.330
1983	4.5 2.321 0.186	116.373	233,600	314.1 284.628 0.329	506.7 421.393 0.302	322.7 261.472 0.294	313.251	31.7 . 38.937 0.446	10.792	18.0 36.639 0.738	62.2 40.539 0.236	45.1 43.861 0.352	2085.9 1803.804 0.314
1984		119.156		177.220	315.581	257.8 212.536 0.299	238.678	20.468	2.173		13,755	43.0 22.809 0.192	1573.8 1405.046 0.324
1985	156.4 103.033 0.239	176.347	160.416	245.4 214.674 0.317	208.788	438.2 372.080 0.308	132.451	43.5 64.288 0.537		0.0 0.136 0.000	2.6 1.077 0.147	4.8 3.845 0.289	1576.3 1444.663 0.332
1986	133.1 90.234 0.246	219.825	188.5 162.177 0.312	238.8 204.015 0.310	366.484	329.4 288.218 0.317	153.330	2.1 22.647 3.851	8.9 8.377 0.343	0.0 0.284 0.000	0.008	18.6 10.030 0.196	1724.2 1525.627 0.321
1987	78.9 58.445 0.269	124.394	175.911	0.339	167.297	374.8 336.769 0.326	98.590 0.477	87.642	0.0 8.450 0.000	0.000	45.723		1448.9 1337.174 0.335
AVERAGE (HK) (HCH) (X)	87.9 66.439 1 0.274	168.9 136.667 0.293	233.8 207.671 2 0.322	266.1 243.846 :	323.8 295.469 2	305,4 267,502 1	146.1 158.440 0.393	38.2 47.491 0.451	10.0 12.848 0.465	7.5 6.535 0.318	18.1 12.722 0.256	35.1 25.743 0.266	1640.9 1481.372 0.327

A.3.13 Monthly Runoff in Maenum Nakhon Nayok (MNN) basin

* BANG PAKONG RIVER BASIN DEVELOPHENT STUDY*

en e	* MAENUK						C.A.= 19			(1	INIT= RAI	IN. CHH) ,	RUNOFF (HCH))
YEAR	APR.	HAY	JUN.	JUL.	AUG.	SEP.	OCŤ.	NOV.	DEC.	JAN.	FEB:	HAR.	ANNUAL
	162.6 113.043	122.6 128.291		291.8 235.369	274.0 269.374	238.5 209.394		39.5 35.079	0.0 4.789	-		93.1 60.382 0.335	1438.3 1278.038 0.460
1969		128.096	336.5 285.300 0.439	346.138	162.948	414.202		33.796	1.992	2.3 2.925 0.668		49.3 34.237 0.360	
1970	157.9 120.168 0.394	228.5 200.357 0.454	371.2 320.911 0.447	293.9 248.061 0.437	353.1 322.386 0.472	437.0 372.501 0.441	147.7 148.065 0.519	11.0 19.305 0.909	47.6 48.136 0.523	0.0 3.086 0.000	42.0 23.079 0.285	31.9 37.648 0.611	2121.6 1863.701 0.454
1971	99.2 70.604 0.368	123,200	270.812	297.1 276.300 0.481	294.534	315.1 289.428 0.475	157.0 145.017 0.478	37.130	1.152	0.0 0.144 0.000	1.3 1.580 0.614	60.4 34.177 0.293	1754.4 1544.076 0.455
1972	143.2 123.301 0.446	71.3 64.667 0.469	240.057	230.689	309.1 255.534 0.428	415.508		143.2 117.841 0.426	75.031	0.0 3.129 0.000	2.7 1.996 0.377	47.6 29.486 0.320	1950.1 1736.485 0.461
1973	67.112	167.768	226.2 206.649 0.473	230.437	208.804	196.261		31.654	2.677	1.9 0.691 0.188	7.701	50.9 37.421 0.381	1415.0 1271.988 0.465
1974	101.6 76.131 0.388	124.518	190.7 180.336 0.489	225.4 191.536 0.440		189.209		92.051	4.766	50.3 38.114 0.392	12.0 14.011 0.604	40.9 30.029 0.380	1635.5 1432.367 0.453
1975		141.204	343.902	366.7 330.942 0.467	302,141		151.9 148.991 0.508	54.286	35.097	0.0 1.085 0.000	18.7 15.769 0.435	31.3 16.050 0.266	
1976	51,400	164.7 142.367 0.447	118.492	440.2 380.220 0.447	474.766	300.166	183.2 166.686 0.471	\$2.8 82.167 0.805	2,505	0.0 0.782 0.000		15.5 11.526 0.385	1732.052
1977	50.018	119.459	151.1 141.529 0.484	179.831	216.509			40.524	8.738	5.6 4.773 0.439	86.9 48.870 0.291	11.1 30.566 1.420	1420.6 1249.412 0.455
1978	39.0 30.767 0.409	168.566	236.7 214.116 0.468	305,296	213.997	312.909		15.7 18.479 0.610	1.386	10.1 9.449 0.486			1524.1 1363.012 0.463
1979	105.889	198.2 177.787 0.464	142.708	215.6 197.540 0.474	226.140	291.4 241.271 0.428	87.900	0.0 18.807 254.492	0.0 0.573 0.000	0.0 0.018 0.000	2.5 2.382 0.491	36.9 27.120 0.381	1371.5 1228.134 0,463
1980			320.9 255.905 0.413			292.087	214.893		0.0 1.869 0.000	0.0 0.057 0.000	32.9 17.320 0.272	17.8 24.965 0.726	1682,710
1981	151.7 128.242 0.437	205.9 178.582 0.449	250.7 210.175 0.434	327.5 298.029 0.471	343.1 297.628 0.449	344.3 306.561 0.461	109.9 128.469 0.605	92.7 76.891 0.429	14.866	0.0 0.379 0.000	1.3 1.023 0.410	44.5 21.060 0.245	1871.7 1661.904 0.459
1982		165.1 138.635 0.434	228.905	261.461	301.187	465.7 404.658 0.450	102.595		58.101	3.4 4.854 0.745	0.7 0.908 0.645	13.4 12.439 0.481	1667.186
1983		217.254	210.846	200,340	546.020		432.0 412.924 0.495	65.982		3.2 6.337 1.030	49.6 31.290 0.326	53.7 40.407 0.390	2307.8 2015.056 0.452
1984	107.6 96.412 0.464	146.991	108.2 119.957 0.574	295.796	355.646	200.122	143.3 160.251 0.579	16.169	0.0 1.248 0.000	5.552	4.5 6.222 0.720	78.2 57.032 0.377	1594.1 1461.396 0.474
1985	125.4 115.543 0.477	188.675	171.6 163.834 0.494	246.099	238.385	532.2 450.704 0.438	107.855	50.6 58.796 0.601	0.0 10.620 0.000		0.0 800.0 0.000	0.0 0.000 0.000	1759.1 1580.766 0.465
1986			132.576		394.247		207.938		19.1 18.657 0.504	0.0 0.828 0.000	7.5 1.826 0.126		1878.9 1666.219 0.459
1987	66.1 55.859 0.437	91.023 0.433	172.168 0.431	128.4 135.145 0.544	97.223 0.575	360.2 326.197 0.469	85.721 0.595	52.6 53.364 0.525	0.0 6.600 0.000	0.389	48.1 37.255 0.401	8.7 14.270 0.851	1143.1 1076.003 0.487
AVERAGE (HH) (HCH) (X)	99.2 79.782	175.4 148.809 0.439	229.7 203.808 2 0.459	287.8 256.438 3 0.461	328.6 291.283 0.459	349.0 300.666 0.446	151.0 155.161 0.532	41.9 48.997 0.605	11.1 15.349 0.717	5.3 4.721 0.465	16.9 11.502 0.351	36.2 27.429 0.392	1732.0 1543.943 0.461

A. 3.14 Monthly Runoff in Khlong Tha Lat (KTL) basin

* BANG PAKONG RIVER BASIN DEVELOPMENT STUDY*

	* KHLONG	THA LAT	SUB-BAS	l H			C.A.= 24	93.0 SQ.1	(H)	(U	INIT= RA	н. (нн)	RUNOFF (MCH)
YEAR	APR.	HAY	JUN.	JUL.	AUG.	SEP.	OCT.	NOV.	DEC.	JAN.	FEO.	HAR.	ANNUAL
•	182.2	138.3	123.4	73.7	146.6	287.7	105.3	0.5	0.0	2.0	2.6	2.3	1064.4
1969	34.3 13.617 0.159	153.7 50.111 0.131	76.7 63.905 0.334	101.0 51.120 0.203	252.2 94.787 0.151	281.1 164.430 0.235	204.4 112.493 0.221	22.9 33.741 0.591	0.0 1.503 0.000	5.0 1.829 0.148	31.8 14.182 0.179	130.8 48.273 0.148	0.225 1293.7 649.990 0.202
1970	149.1 79.503 0.214	204.9 95.807 0.188	438.0 204.614 0.187	171.0 131.281 0.308	368.8 153.807 0.167	232,4 107.080 0.185	189.0 144.139 0.306	4.7 20.424 1.747	116.6 60.569 0.208	0.1 3.761 17.085	17.8 1.730 0.039	7.4 10.490 0.570	1899.8 1013.204 0.214
1971		167.7 90.281 0.216	186.1 98.752 0.213	145.6 84.297 0.232	286.0 91.706 0.129	139.9 111.632 0.320	218.0 93.824 0.173	0.7 46.576 26.049	0.2 1.726 3.852	0.0 0.153 0.000	1.7 0.761 0.178	41.2 11.557 0.112	1292.7 659.964 0.205
1972	207.4 88.569 0.171	36.8 29.975 0.327	229.4	10.9	67.3 31.951	341,3 142,724	86.7 74.180	53.5 28.675	15.2	0.0	0.2	39.7 13.008	1088.4 565.368
1973	6.8 9.162 0.539	151.9 60.130	109.5 69.635 0.255	140.7 68.039 0.194	217.7 94.987 0.175	217.2 98.708 0.182	83.9 83.993 0.402	34.7 22.103 0.256	0.0 2.966 0.000	0.3 0.183 0.213	20.1 3.908 0.078	39.6 20.729 0.210	1022.4 534.542 0.210
1974	160.3 68.286 0.171	55.2 40.379 0.293	19.370	178.8 64.458 0.145	151.4 80.446 0.213	51.293	225.1 105.143 0.187	57.615	0.0 3.644 61.994	8.0 3.030 0.151	3.1 1.811 0.232	2.230	958.9 497.704 0.208
1975	22.9 11.043 0.193		62.340	254.5 121.976 0.192		149.424	209.0 136.154 0.261			0.0 0.070 0.000	46.1 21.723 0.189	60.0 19.493 0.130	1338.2 684.567 0.205
1976	84.8 33.231 0.157	51.486	23.885	298.8 109.468 0.147	150.7 102.657 0.273	144.777	268.4 122.992 0.184	79.935	0.8 4.783 2.433	4.6 2.459	0.9 0.418 0.196	33.6 17.514 0.209	1314.5 693.604 0.212
1977	61.7 29.088 0.189	48.344	93.284		106.187	268.3 137.499 0.206	55.8 67.459 0.485	28.3 15.940 0.226	0.0 3.838 0.000	60.2 30.367 0.202	51.2 25.921 0.203	74.6 29.483 0.159	1423.4 732.117 0.206
1978	29.4 22.432 0.306	157.9 60.970 0.155	55.073		111.460	179.684	196.3 131.217 0.268		0.0 1.248 0.000	12.6 6.073 0.193	26.3 3.893 0.059	20.2 16.984 0.338	1439.1 757.523 0.211
1979	85.2 29.620 0.139	283.2 147.714 0.209	203.6 102.071 0.201	260.9 114.189 0.176	176.0 112.839 0.257	352.7 175.702 0.200	1.2 32.410 11.019	23.8 12.104 0.204	0.0	0.0	1.0 0.312	20.2 8.193 0.163	1407.7 736.897 0.210
1980	30.0 14.306 0.191		135.533		• 90.877	156.155	158.7 116.905 0.296	128.1 87.781 0.275	0.0 5.139 0.000	0.0 0.197 0.000	28.5 3.996 0.056		1540.3 799.483 0.208
1981		431.8 224.340 0.208	134.401	167.9 87.278 0.209	243.8 146.882 0.242	258.524	105.286	55.612	0.0 33.332 0.000	0.0 0.990 0.000	2.2 0.716 0.128	14.2 2.735 0.077	2125.0 1107.208 0.209
1982	117.4 56.974 0.195		272.3 111.601 0.164	96.1 93.909 0.392	211.3 92.110 0.175	74.635	59.437	20.5 19.992 0.391	60.7 32.554 0.215	0.0 1.163 0.000	0.6 0.309 0.211	2.2 0.898 0.161	1133.2 596.804 0.211
1983	60.5 4.468 0.030	47.375	120.809	127.8 59.358 0.186	544.8 269.459 0.198	266.9 110.231 0.166	287.0 192.596 0.269	60.0 48.747 0.326	0.9 3.843 1.705	33.9 10.385 0.123	22.5 15.976 0.285	37.5 10.934 0.117	1756.9 894.180 0.204
1984	63.5 35.791 0.226	03.000	89.919	94.3	160.9	221.3 101.528	161.4 100.350 0.249	19.1 16.994	0.0 1.925	32.6 7.240	63.2	29.8 15.475 0.208	1157.9 602.009 0.209
1985		233.4 126.532 0.217	40.112	199,2 70,299 0,142	96.1 75.258 0.314	66.366	210.7 95.524 0.182	75.7 65.075 0.345	2.7 7.524 1.101	0.0 0.300 0.000	10.6 4.400 0.166	2.7 2.011 0.295	614.905
1986	165.6 57.163 0.139	134.3 89.113 0.266	62.150	114,9 57,972 0,202	308.7 152.678 0.198	238.3 97.450 0.164	159.259	6.7 23.874 1.420	1.1 2.009 0.714	0.0 0.104 0.000	0.0 0.012 0.000	73.4 0.366 0.002	1426.2 702.149 0.197
1987	57.9 52.053 0.361	17.4 20.233 0.467	56.220	112.0 59.920 0.215	197.1 92.363 0.188	0.155	94.191	0.197	0.0 12.878 0.000	0.0 0.412 0.000	105.9 45.696 0.173	16.1 15.628 0.390	1026.4 569.631 0.223
AVERAGE (HH) (HCH) (X)	98.5 42.714 0.174	75.696 -0.199	84.600 0.208	85.226 ° 0.202	213.9 106.371 0.199	263.8 126.125 0.192	162.9 105.887 0.261	44.1 37.116 0.337	9.904 0.401	3.524 0.177	21.8 9.101 0.167	35.7 14.204 0.159	1343.6 700.467 0.209

A.3.15 Monthly Runoff in Lower Bang Pakong (LBP) basin

* BANG PAKONG RIVER BASIN DEVELOPMENT STUDY*

		* LOVER E	ANG PAK						ELOPMENT 06.0 SQ.1		٠			
				JUX.									878. 14. (88) 18. (88)	RUNOFF(HCH) ARNUAL
3 -	YEAR	APR.		وموسا المساملات والمساعدة		*	=	I	*					
	1968	107.0 81.735 0.246	148.6 76.565		115.5 58.720 0.164	86.923	123.038	133.0 90.269 0.219	21.5 17.744 0.265	0.1 0.971 3.209	58.0 29.214 0.162			1259.3 699.801 0.179
	1969	89.4 44.107 0.159	186.3 74.615 0.129	63.736	56.351	91.128	164.494	71.187	28.502	0.0 0.969 0.000	14.3 6.814 0.153	19.8 9.130 0.148	73.4 31.607 0.139	1241.3 642.639 0.167
٠.	1970	86.1 46.630 0.174	190.8 85.226 0.144	150.040	90.001	87.055	93.320	91,191	14.147		0.9 2.710 0.989	50.4 15.022 0.096	34.3 27.326 0.256	1418.7 746.423 0.169
	1971	93.1 42.422 0.147	175.8 68.374 0.125	201.8 113.617 0.181		143.768		108.834	28.719	3.4 2.019 0.190	0.0 1.020 0.000	18.3 9.296 0.163	55.2 15.143 0.088	1440.4 734.024 0.164
	1972	118.0 67.281 0.184	18.927	221.8 101.584 0.147	35.9 37.332 0.335	29.416	380.7 173.678 0.147		57.040	18.6 15.850 0.274	1.5 1.392 0.303		60.8	
	1973	66.6 31.473 0.152	167.5 81.433 0.157	58.067		229.5 122.041 0.171	117.767	66.860	25.309	0.7 2,538 1,113	0.9 0.244 0.085	37.1 13.871 0.120	88.4 40.919 0.149	
	1974	146.0 68.142 0.150	144.2 77.480 0.173		168.2 82.752 0.158	184.0 97.555 0.171	172.4 94.143 0.176	195,997	68.883	0.2 3.541 7.429	49.1 22.851 0.150	29.2 16.143 0.178	30.5 12.751 0.135	1490.7 778.758 0.168
	1975	24.6 17.771 0.232	158.1 66.202 0.135	49.737	190.8 97.724 0.165	73,643	135.405	105.007	26.594	0.7 1.361 0.617	0.0 0.045 0.000	48.0 23.311 0.156	91.6 26.681 0.094	1219.1 623.479 0.165
	1976	95.9 49.878 0.167	143.8 83.375 0.187		203.8 89.598 0.142			102.891	36.7 53.273 0.467	0.9 1.693 0.599	1.6 0.782 0.156	15.1 6.482 0.138	33.6 19.172 0.184	1253.3 673.486 0.173
	1977	91.1 41.893 0.148	185.4 82.596 0.143		150.1 78.287 0.168		82.389	64.215		0.1 6.407 36.483	34.8 15.101 0.140	37.8 17.486 0.149	73.0 31.675 0.140	1112.5 567.470 0.164
	1978	54.3 33.293 0.197	241.1 119.932 0.160		201.3 88.720 0.142		147.895		17.562	0.0 0.918 0.000	8.2 4.299 0.170	16.8 2.693 0.052	12.5 11.866 0.305	1184.8 626.630 0.170
	1979	72.3 27.073 0.121	120.4 62.725 0.168	99,7 52,176 0,168	96.9 48.798 0.162		113.232	37.938	7,403	0.1 0.450 1.602	0.0 0.018 0.000	14.5 6.319 0.140	88.6 41.019 0.149	876.2 452.498 0.166
	1980	65.8 38.664 0.189	74.2 33.436 0.145	110.043		90.993	109.327	94.253	35.7 29.658 0.268	0.0 1.289 0.000	0.5 0.298 0.190	25.8 10.700 0.133	37.2 14.856 0.128	1153.1 600.474 0.168
٠.	1981	158.1 73.435 0.150	207.7 105.898 0.164		149.6 71.265 0.153	100.1 65.338 0.210		84.476	74.5 46.320 0.200	0.0 .8.601 0.000	0.0 0.272 0.000	9.6 1.939 0.065	54.6 15.648 0.092	1316.9 676.542 0.165
	1982	143.6 79.680 0.179	88.3 46.342 0.169	236.6 106.678 0.145	77.953	59.013		120.4 74.446 0,199	61.0 40.757 0.215	49.0 30.043 0.197	0.0 0.750 13.264	14.3 7.427 0.168	9.5 5.530 0.187	1155.8 614.910 0.171
	1983	51.0 16.082 0.101	125.2 54.032 0.139	140.9 79.979 0.183	165.5 76.057 0.148	221,749	107.351		54.6 50.119 0.296	5.3 3.266 0.199	20.4 9.545 0.151	73.0 34.986 0.154	26.8 14.816 0.178	1656.1 847.721 0.165
	1984	86.3 42.963 0.160	98.8 48.967 0.160	185.9 89.932 0.156	165.0 92.810 0.181	149.2 70.763 0.153	162.6 79.371 0.157	149.1 91.836 0.198	15.7 12.849 0.264	0.0 1,173 0.000	19.9 6.104 0.099	22.0 12.550 0.184	30.7 14.195 0.149	1085.2 563.511 0.167
	1985	90.4 40.197 0.143	195.4 95.366 0.157	12.7 26.627 0.675	111.7 43.444 0.125	79.8 48.452 0.196	238.3 102.385 0.138	160.6 91.865 0.184	69.1 46.156 0.215	0.1 7.436 30,525	0.0 0.184 0.000	10.3 2.637 0.082	6.3 5.481 0.280	974.7 510.229 0.169
	1986	130.2 56.305 0.139	172.6 93.997 0.175	139.0 66.437 0.154	155.8 72.991 0.151	250.2 133.404 0.172	149.5 71.870 0.155	262,2 140,271 0,172	12.9 21.094 0.525	3.1 3.105 0.327	0.0 0.110 0.000	1.8 0.896 0.159	27.1 7.187 0.085	1304.3 667.665 0.165
	1987	63.6 28.873 0.146	139.5 69.383 0.160	119.4 70.838 0.191	130.0 50.194 0.124	122.0 79.113 0.209	238.8 104.259 0.141	185.4 102.854 0.179	97.8 67.319 0.222	0.0 6.877 0.000	0.0 0.172 0.000	108.3 50.827 0.151	54.0 35.474 0.211	1258.7 666.181 0.170
•	AVERAGE (HH) (HCH) (X)	91.7 46.395 0.163	149.6 72.243 0.155	143.5 75.248 0.169	137.6 70.294 0.165	176.8 87.934 0.160	240.5 16.799 0.156	163.1 98.451 0,194	44.1 34.060 0.249	7.1 7.113 0.323	10.5 5.096 0.156	29.0	47.1 20.994 0.144	1240.4 647.601 0.168

A.3.16 Monthly Runoff in Entire Bang Pakong Basin

* BANG PAKONG RIVER BASIN DEVELOPHENT STUDY*

	* ENTIRE	BASIN		- 0		The second second		50.0 SQ.)	the second part	.	INIT= RA	(ки) ,	RUNOFF(HCH))
YEAR	APR	HAY	JUN.	JUL.	AUG.	SEP.	OCT.	NOV.	DEC.	JAN.	FEB.	HAR.	ANNUAL
 1968	136.5 680.053 0.282	128.5 689.244 0.304	156.2 696.7071 0.252	211.0 030.2111 0.276	218.4 291.5811 0.335	268.1 138.586 0.241	108.7 752,992 0,392	14.8 146.398 0.561	0.0 14.827 49.006	28.1 117.858 0.237	25.1 135.105 0.305	35.7 155.976 0.248	1331.1 6849.512 0.291
1969	64.5 289.903 0.254	161.9 624.840 0.219	211.5 1145.6301 0.307	264.0 438.5391 0.309	244.1 177.3851 0.273	410.0 990.999 0.275	153.7 899.629 0.332	24.1 264.111 0.620	0.2 14.120 3.966	7.1 24.898 0.197	22.8 92.879 0.231	66.4 214.102 0.183	1630.2 8177.016 0.284
1970	131.1 522.257 0.226	182.1 895.631 0.279	339.8 1460.0311 0.243	210.9 217.1781 0.327	341.7 624.2821 0.269	262.5 337.083 0.288	163.2 961.903 0.334	21.7 199.495 0.520	65.2 354.292 0.308	1.3 36.445 1.581	25.8 68.235 0.150	24.0 146.053 0.345	1769.3 8822.871 0.282
1971													1547.4 7558.707 0.277
1972	0.230	0.010	0,240	0.324	V	V. L. U.	0.301	0.203	0.504	1, 505	0,1,,	0.102	
1973			144.9 785.2021 0.307										
1974	134.0 528.958 0.223	162.9 762.132 0.265	157.0 905.242 0.327	192.1 892.8331 0.263	255.1 237.746 0.275	156.8 912.2711 0.329	285.1 335.305 0.265	78.1 518.420 0.376	1.0 41.576 2.431				1515.3 7513.125 0.281
1975	31.2 192.601 0.349	619.392	1240.9881		292.4 449.4391 0.281	298.7301	056.393	286.782		0.0 2.625 0.000	34.8 129.386 0.211	71.6 199.169 0.158	1587.7 7934.055 0.283
1976	81.4 328.462 0.229	147.6 672.911 0.258	154.6 721.1901 0.264	341.1 616.1211 0.268	305.7 667.4171 0.309	284.8 542.2861 0.307	279.7 188.097 0.241	64.0 649.131 0.575	1.7 39.967 1.332	1.4 10.318 0.425	4.6 11.153 0.138	25.7 110.893 0.244	1692.3 8557.930 0.286
1977	79.3 324.266 0.232	173.7 642.380 0.209	162.8 835.3441 0.290	254.3 136.3351 0.253	235.9 223.6581 0.294	299.5 523.452 0.288	134.8 789.780 0.332	26.3 278.116 0.599	0.3 59.256 13.036	22.9 71.135 0.176	38.8 155.931 0.228	54.6 210.975 0.219	1483.2 7250.609 0.277
1978	43.6 244.783 0.318	234.2 901.551 0.218	197.4 1086.1571 0.312	288.0 372.1021 0.270	216.8 252.8401 0.327	378.0 593.178 0.239	105.4 815.053 0.438	22.4 222.637 0.564	0.0 25.902 0.000	11.4 52.159 0.259	14.9 18.449 0.070	16.1 92.955 0.327	1528.2 7677.742 0.284
1979	94.6 370.858 0.222	1119.687	1018.6411			357.0 448.085 0.230	39.6 579.189 0.829	11.7 140.416 0.679	11.883	0.0 0.621 0.000	0.143	44.9 183.936 0.232	7391.430 0.280
1980	47.2 229.045 0.275	510.569	1462.0541		581.5761		203.1 234.187 0.344		0.0 21.374 0.000		32.7 60.139 0.104	59.0 311.534 0.299	1771.9 8878.023
1981			1313.0491				341.068			0.0 5.165 0.000	92.143	41.0 107.469 0.148	9218.766
1982	105.6 494.059 0.265	143.4 599.674 0.237	268.5 1130.4271 0.238	198.2 206.2691 0.345	337.0 644.07314 0.276	272.9 471.860 0.305	586.540	47.6 326.038 0.388	224.558	1.4 15.556 0.612	13.6 32.749 0.136	4.0 39.712 0.560	0.290
1983	29.8 40.206 0.076	153.5 584.003 0.216	234.6 1170.9391 0.283	235.6 179.3022 0.283	512.3 363.58114 0.261	317.6 431.51220 0.255	352.9 041.249 0.328	49.3 391.558 0.450	10.8 46.300 0.242	17.5 96.605 0.312	42.1 161.706 0.218	64.2 222.835 0.197	2020.1 9729.773 0.273
1984			1160.5091		350.9 648.6001 0.266		089.441		18.248	19.6 45.764 0.132		51.8 199.834 0.218	1520.5 7713.758 0.287
1985	160.7 589.573 0.208	1148.172	159.9 912.5401 0.323	227.9 116.639 0,277	163.3 966.06510 0.335	332.5 635.611 8 0.279		52.3 409.628 0.443	0.5 72.303 8.183		18.1 27.310 0.085	0.288	1533.9 7799.055 0.288
1986	131.5 530.493 0.229	1120.891	758.53110		596.29613	390.4531		5.7 183.371 1.836	8.8 58.093 0.374		22.0 50.177 0.129		1659.6 8099.617 0.276
1987		567.363	968.149 8	341.296 i 0.313		525.079 (0.274	576.265 0.342	445.201 0.288	0.0 65.334 0.000		77.5 252.448 0.184		1346.1 6730.770 0.283
AVERAGE (HH) (HCH) (X)	397.829 0.243	0.249		229,4 35,347138 0,293	274.3 85.696144 0.286	306.6 60.138 98 0.270	169.7 39.977 3 0.330	43.9 32.436 0.429	0.561	32.354 0.248	86.790 1 0.191	0.222	1590.7 7931.410 0.282

A.3.17 Annual Runoff at Proposed Dam Sites

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<u>.</u>		<u>ဖ</u>				32																		45				26
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A.4 Probable Flood Hydrograph at Proposed Dam Sites A.4.1 Probable Storm Rainfall

1) Storm Records

The storm rainfall is estimated in high rainfall area over 2,000 mm/yr., on basis of the isohyet map. The maximum one day, two days, and three days rainfall in 20 years from 1968 to 1987 are examined as to four stations being operated by RID in the said area.

Consequently, following items are made clear from the storm records.

- The consecutive storm rainfall could be expressed on three days maximum.
- Three days rainfall less than 200 mm, relatively small rainfall, has an areal difference among four stations.
- The big storm over 200 mm of three days maximum in 1972 and 1979 shows the same span of occurrence on examined four stations.
- The three days maximum in 1972 is recorded at the same period in whole basin and assumed to arise the biggest damage.
- The linear interpolation between three days maximum and the mean annual rainfall at stations could be adopted.

The correlation between the probable storm and the mean annual rainfall at the station (code 4412), which has the highest annual rain among four stations, is selected as the basis to estimate the storm rainfall of proposed dam sites.

2) Hourly Rainfall

The hourly record of three days maximum rainfall is available at the station (code 44181) which is equipped with an automatic recorder and it shows the following characteristics.

- Total rainfall amount reaches 100 % in 60 hours from the biginning.
- Three days rainfall on 4 6 September, 1972 is recorded as the maximum of 20 years in the entire basin and its hourly cumulation shows the typical pattern.

3) Effective Storm Rainfall

In consideration of runoff loss, the effective rainfall for the direct runoff is determined from the consecutive three days rainfall. The runoff record and storm rainfall are reviewed and resulted in Appendics D.

5) Dimensionless Unit Hydrograph

Dimensionless unit hydro-graphs are given in A.4.5 - 10 and those watershed parameters are also listed in A.4.3.

A.4.2 Design Storm Rainfall

Time (Hour)	Runoff Ratio(%)		Proba 1/20	ble Ra 1/100	ainfall	(mm/ 1/100	hr.) 0 1/10000
123456789011234567890112345678901234567890123445678901234567890 at 1234567890 at 123567890 at 12356780 at 123567800 at 123567800 at 12	0.4 0.7 1.3 1.3 1.3 1.3 1.3 1.3 1.3 1.3	1	1.4.07917.631.044.343.3.3.4.9.04.23.3.3.4.3.3.3.4.3.3.3.4.3.3.3.4.3.3.3.4.3.3.3.4.3.3.3.4.3.3.3.4.3.3.3.4.3.3.3.4.3.3.3.4.3.3.3.4.3.3.3.4.3.3.3.4.3.3.3.4.3.3.3.4.3.3.3.4.3.3.3.4.3.3.3.3.4.3.3.3.4.3.3.3.4.3.3.3.4.3.3.3.4.3.3.3.4.3.3.3.4.3.3.3.4.3.3.3.4.3.3.3.4.3.3.3.4.3.3.3.3.4.3.3.3.3.4.3.3.3.3.3.4.3	4.54 4.54 1.77 1.82 4.85 1.84 1.77 1.82 1.82 1.84 1.77 1.82 1.82 1.83 1.84 1.82 1.83 1.84 1.85	4.535.993.862.68002.92.1.7593.1.97 4.523.31.2.2.34.34.54.4.5667.7	4.37 6.91 1.60 9.11 6.09 1.10 6.11 6.09 1.11 1.10 1.11 1.10 1.11 1.10 1.11 1.10 1.11 1.10	8.2 6.1 6.1 6.6 3.6 4.6
							•

A.4.3 Parameters of Dimensionless Unit Hydro-graph

						1. 1. 1. 1.	,								
8.11	UPP-3	266	30	1.5	000	0000 0000 0000 0000	1339	5.22	MNN-4	114	αO	4	300 70	46 6 ••• 6 •• 6 • 6	1602
8.10	UPP-2	1,040	.80 80	40	600 400 600	10.7 11.68 24.20	1547	8.21	MNN-6	13 13 13	œ ₩	0	4.6 4.6 0.0	4.14 7.14 7.14 7.20 7.20 7.20	1851
တ ဟ	KPS-4	614	48	25	00 00 00	99.38 39629 17.01	1566	\$.20	UBP-5	107	H	O T	5.20 4.00	88.004 0048 48.00	1855
တ္ခ	KPS-4	1,452	ထ	40	0000	10.8 113038 33.37	1538	8.19	MHM-3	273	37	22	700 580	9.0 9.20 36120 7.80	1571
8.7	КРS4 1-3	2,253	හ හ	45	300 400	111 125 1635.75 48.3522	1513	S. 18	MHM-2	1 8 9	28	14	700 40	0000 0. 88.70 884	2109
8.6	KTL-5	798	4 0	2	00 11 11	255 255 334 110 2034 110 2034	1369	8.17	MHM-3	80 40	ω	4	12 10 00	7	1342
လ လ	KTL-9	വ യ വ	က လ	ო ო	н 60	18 68 68 20 20 80 80 80 80	1334	5.16	MHM-6	<u>ဖ</u> ၈	7	4	41 00 00	40 to	1342
8.4	KTL-9	976	ဆ က	20	1 84 5	775 775 775 775 775 775 775 775 775 775	1334	8.15		6 4.8 4.8	26	H C	4 70 7	7.00 0.00 11.000 0.000	1417
8	001 11 11 12 14	1,371	7.1	4 3	14 00 00	175.00 1701.00 1701.00 1800.00	1331	8.14	MHM-8	64	10	φ	260 120	9100 9100 9000 9000	1748
8.2	LBP-12	344	EI EV	10	004	7 2 2 3 3 2 3 2 3 3 3 3 3 3 3 3 3 3 3 3	1268	5.13	MHM-9	147	20	13	170 0	0000 .00. 00770 00111	1836
8.1	LBP-11	528	25	n H	900	88.41 15.89.21 5.992	Annual mm)1266	8.12		443	48	20	14 00 00	8.8 4.84 12.04 40.04	Annual (mm)2030
Item	1.Block	2.C.Area	. H	4. Lo.	5. H12	TWHO THU THU	6.Mean A	Item	1.Block	2.0.8 2.0.8 2.0.8	∄ •	4. Lc.	E E E E	TAKH QHM DB DB DB DB	6.Mean Rain.(n

A. 4.4 Peak Flood Discharge

(unit:cu.m/s)

Dam	C.Area			Probab	ility		
Site	(sq.km)	1/10	1/20	1/100	1/500	1/1000	1/10000
			1				
No.1	528	579	665	844	1,007	1,073	1,294
2	344	407	466	593	709	756	911
3	1,371	1,357	1,547	1,954	2,332	2,488	3,001
4	976	1,110	1,270	1,605	1,912	2,040	2,452
5	585	663	760	961	1,146	1,221	1 471
6	798	904	1,028	1,291	1,539	1,640	1,976
7	2,253	2,597	2,950	3,694	4,384	4,665	5,608
8	1,452	1,791	2,028	2,532	3,000	3,190	3,831
9	614	851	964	1,203	1,424	1,514	1,816
10	1,040	1,300	1,472	1,836	2,170	2,313	2,777
11	226	338	386	488	582	620	746
12	443	822	921	1,134	1,334	1,417	1,693
13	147	289	325	400	471	500	598
14	64	130	147	182	213	227	271
15	338	462	527	662	787	837	1,006
16	96	148	169	212	252	269	322
17	68	102	116	147	174	185	223
18	159	359	402	494	580	615	735
19	273	390	442	551	652	694	832
20	107	226	253	312	366	388	464
21	151	286	322	397	467	497	594
22	114	217	245	304	358	380	454

A. 4.5 Design Flood Hydrograph (1/10)

(DAM NO.) CATCHMENT HOUR	(NO. 1) A= 528	(NO. 2) A= 344	(NO. 3) A=1371	(NO. 4) A= 976	(NO. 5) A= 585	(NO. 6) A= 798	(NO. 7) A=2253	(NO. 8) A=1452	(NO, 9) A= 614	(NO.10) A=1040	(NO.11) A= 226
2 4	0.2	0.3	0.3	0.4	0.2	0.2	0.5	0.4	0.2	0.3	0.2
6	1.9 9.0	10.3	1.9 7.3	3.3 14.7	1.8 8.0	2.1 9.0	3.6 14.0 43.3	2.9 11.8	2.2 9.7	2.2 8.8	8.4
. 8	24.6	25.5	22.7	41 1	8.0 22.5	26.1		35.8 80.0	27.6 56.6	26.7 59.5 103.8 152.4 192.8 220.0 231.2 231.0 229.5 235.3 250.1	20.8
10 12	47.4 72.0	43.8 60.6	52.1 95.6	82.2 128.3 168.8	46.2 73.5 98.2	55,5 90,6	180.7 275.1 361.3 425.8 459.5	140.5	90.0	103.8	35.7 49.5
14	93.0	73,4	146.2	168.8	98.2	125.0 151.3 164.5 167.2 164.2	275.1	207.5	120.3	152.4	59.9 64.2
16	106.6	78.8	193.0	197.1	116.4 124.0	151.3	361.3	263.5	142.2	220.0	63.4
18	110.9 108.4	77.8 74.2	228.4 247.4	205.5	123.7	167.2	459.5	318.3	151.4	231.2	60.5
20 22	105.0	74.2 71.9	253.1	200.1	120.8	164.2	469.0	318.8	147.9	231.0	58.6
24	105.8	74.7 82.0	253.1	200.2	120.3	162.6	. 468.6 . 476.0	324.5	154.7	235.3	63.4 60.5 58.6 60.9 66.8
26 28	112.7 124.2	90.6	253.1 253.1 256.9 269.8 293.1 322.7 359.3	197.1 208.0 205.5 200.1 200.2 211.4 232.2 256.6	126.4 138.4 152.6	162.6 169.5 183.9 202.5 202.5 225.2 252.1 282.2 313.8 348.4 397.4 470.4	468.6 476.0 500.5	140.5 207.5 263.5 302.0 318.3 318.8 317.0 324.5 344.4 377.8 417.4	120.3 142.5 151.8 151.4 147.9 147.3 154.7 169.4 186.9 207.8	250.1	13.9
30	137.5	90.6 100.3 112.5	293.1	256.6	152.6	202.5	544.4	377.8	186.9 207.8	274.6 303.6	81.8 91.8
32	153.1	112.5	322.7	207.4	190.7	252.1	544.4 599.7 667.9 745.4 831.9	465.4	233.2	338.5	407
34 36	172.2 192.5	126.8 140.4	400.9	358.8	213.3	282.2	745.4	520.7	261.1	378.9	114.5
38	212.6	154.1	447.4	397.1	236.4	313.8	831.9 928.8	580.8 646.9	261.1 289.4 321.6	422.3	141.8
40 42	212.6 236.4 273.2	154.1 173.9 206.9	561.7	507.3	300.8	397.4	1047.4	733.0	371.2	533.5	168.9
44	720 1	253,1 307,2	646.7	609.3	190.5 190.5 213.3 236.4 262.4 300.8 359.2 437.4	470.4	1217.7 1468.4	860.5	452.4	627.6	207.9
46 48	399.2	307.2	767.8	358.8 397.1 441.0 507.3 609.3 743.9 900.4	530.2	573.0 697.9 814.8	1794.4	1293.8	452.4 569.0 699.5 802.1	947.2	306.3
50	399.2 477.2 545.7	403.2	1095.0	1030*0	614.4	814.8	2148.3	1539.2	802.1	1125.1	103.4 114.5 125.7 141.8 168.9 207.9 256.6 306.3 336.9
- 52	579.0	407.0	447.4 499.5 561.7 646.7 767.8 920.7 1095.0 1247.5	1110.3 1099.8	663.1 663.4	891.3	2438.9 2597.3	1/1/.9	851.7 843.4	274.6 303.6 338.5 378.9 422.5 470.5 533.5 627.6 770.6 947.2 1125.1 1252.2 1300.9	315.3
54 56	568.4 522.9	335.4	1357 /	1021.9	621.9	860.5	2597.2	465.4 520.7 580.8 646.9 733.0 860.5 1053.8 1293.8 1539.2 1717.9 1791.0 1756.2 1633.7	851.9 843.4 787.2 701.3	1271.8	277.2
. 58	458.4 394.3	363.6 403.2 407.0 381.1 335.4 283.6 241.3	1295.7 1185.0 1057.2	905.1 782.7	\$55.1	904.4 860.5 778.2 683.2 595.4 522.1	2461.4	1633.7 1467.8	701.3	1180.0	315.3 277.2 234.3 199.4
60	394.3 341.5	241.3	1185.0	782.7 679.1	482.4	595.4	2243.0 1996.4	1293.6	609.2 529.6 463.5 408.5	1058.0 931.7	171.1
62 64	298.2 261.3	207.1 179.0	936.8	593.9	366.9 323.2	522.1	1767.9	1141.4	463.5	821.6	171.1 147.9
66	261.3	155.0	832.6	521.9	323.2	461.3 408.5 363.0	1570.6 1403.4	1011.8 901.7	408.5 361.2	728.3 648.7	128.1 110.3
68 70	229.6 202.1	133,5 115.4	744.0 666.9	460.3 406.6	285.5	363.0	1257.9	0.309	319,9	648.7 579.6 520.1	110.3 95.4
66 68 70 72 74	178.7	100.4	599.7	360.8	224.9	374.1	1131.3	723.3 653.1 592.8 539.8 492.6	284.6	520.1	83.0
74 76	158.7	87.6 76.7	542.3 493.1	321.8	201.1 180.4	290.9 262.0	1023.5 930.7	022.1 592.8	254.6 228.3 205.0	469,4 425,9 387,6	63.4
78 78 ,	141.2 125.9	67.3	450.8	287.7 257.5 231.0	162.0	221 6	850.7	\$39.8	205.0	387.6	55.6
- 80	112.5	59.1	413.3	231.0	145.7	213.6	779.6	492.6 449.8	184,4 166,2	353.4 322.5	48.9 43.0
82 84	100.7 90.3	51.9 45.6	379.5 348.8	207.6 186.9	131.2 118.4	213.6 193.3 175.1 158.9 144.5	779.6 715.4 656.9 603.4 554.6	449.8 411.0	150.0	294.4	72.4 63.4 55.6 48.9 43.0 37.7 33.0 28.9 25.4
86	81.1	40.0	320.7	168.6	107.1	158.9	603.4	375.8 344.2	135.7 122.9	269.1 246.3	33.0
88	72.8	35.0 30.7	294.9 271.5	152.2 137.4	97.0 87.9	144.5 131.5	510.4	315.7	111.4	225.8	25.4
90 92 ·	65.3 58.4	27.0	250.3	123.8	79.6	119.8	470.3	289.9	100.9	207.3	22.3
94	52.2	23.7 20.8 18.2	250.3 231.0	123.8 111.4	72.0	109.2	470.3 434.0	266.7	91,2 82,3 74,1	190.5 175.3	22.3 19.6 17.2
96 98	46.6	20.8	213.5 197.6	100.0 89.7	65.0 58.6	99.4 90.3	401.0 370.9	245.5 226.1	74,1	161.4	15.1
100	37.3	15.9	183.0	80.6	52.7 47.5	81.9	343.4	208.3 191.8	8,66	148.5	13.2
100 102	33.4	13.7 11.8	169.5 157.1	72.5 65.3	47.5 42.9	74.1 67.1	318.0 294.4	171.8	60.2 54.3	136.5 125.3	11.4 9.7 8.2
104 106 108	30.0 26.9	9.9	145.5	58.9	38.7	60.8	272.4	161.7	49.1	114.8	8.2
108	24.1	8.2	145.5 134.6	53.2	35.1	55.2	251.7	148.2	44.5	105.1	6.8 5.5 4.3 3.3 2.3
110	21.5 19.1	6.7 5.2	124.4 114.7	47.9 43.1	31.8 28.7	50.2 45.6	232.2 213.9	135.8 124.5	36.5	88.2	4,3
112 114	16.8	3.9	105.8 97.5	38.6 34.3	0.65	41.6	213.9 197.0	114.2	33.0.	80.8	3.3
116	14.6	2.8	97.5	34.3	23.3 20.9	37.8 34.3	181.6	104.8	29.0 26.5	74.1 68.0	-1.5
118 120	12.6	1.9 1.2	89.9 83.1	30.2 26.4	18.5	31.1	154.7	114.2 104.8 96.2 88.5	23.5	62.5	0.9
122	8.9	0.7	76.8	22.8	16.3	27.9	167.6 154.7 142.9 132.0 122.0	81.4 74.8 68.8 63.1 57.7 52.4 47.4	49.1 44.5 40.3 36.5 33.0 29.6 26.5 23.5 20.7 18.0 15.5 13.1	57.5 52.8	0.5
124	7.2 5.7	0.4	71.0 65.6	19.4 16.3	14.2 12.2	24.9 22.1	122.0	68.8	15.5	48.5	0.3
126 128	4.3	0.1	60.7	13.3 10.5	10.4	19.4	112.8	63.1	13.1	44.4	0.1
130	3.1	0.1	56.1	10.5	8.6 6.9	19.4 16.9 14.5	104.2	57.7 52.4	10.9 8.8	40.4 36.4	0.0 0.0
132 134	2.1 1.3	0.0	51.9 47.8	8.0 5.8	5,4	12.2	112.8 104.2 96.3 88.7	47.4	6.8	33.0	0.0
136	0.8	0.0	44.0	3.9	4.0	10.1	81.4	0	5.0	29.6	0.0 0.0
138 140	0.4 0.2	0.0 0.0	40.3 36.7	2.5 1.5	2.8 1.9	8.1 6.2	74.3 67.5	38.0 33.ა	3.5 2.3	114.8 105.1 96.3 88.2 80.8 74.1 68.0 62.5 57.5 52.8 48.5 44.4 40.4 33.0 29.6 26.3 23.1	0.0
140	٧٠،٤					<u></u>					

A. 4. 5 Design Flood Hydrograph (1/10)

(UNIT: A=50, KM, AUNOFF=CU.M/S)

(UNIT: A=50, KM, AUNOFF=CU.M/S)

(DAM NO.) CATCHMENT HOUR	(NO.12) A= 443	(NO.13) A= 147	(NO.14) A= 64	(NO.15) A= 338	(NO.16) A= 96	(NO.17) A= 68	(NO.18) A= 159	(NO.19) A= 273	(NO. 20) A= 107	(NO.21) A= 151	(HO. 22) A= 114
CATCHMENT HOUR 2 4 6 8 10 12 14 16 18 20 22 24 26 28 30 32 34 36 38 40 42 44 46	0,2 1.9 8,4 24,1 50.1 80.5 108.9 130.0 137.6 140.3 137.4 136.4 142.9 171.9 191.2 214.4 240.0 267.6 302.9 363.4 458.6 578.0	0.2 2.1 8.4 19.4 31.3 42.0 49.3 51.4 49.8 49.8 45.8 65.7 74.1 83.7 50.7 74.1 83.7 51.7 52.0 100.9 117.3 151.7 201.5	A= 64 0.2 1.9 6.4 12.3 17.6 22.0 23.9 23.4 20.6 22.8 25.2 27.8 35.4 39.4 43.0 47.3 77.6 102.3	A= 338 0.3 2.5 10.9 27.2 47.1 65.7 79.9 86.3 85.5 85.7 79.1 89.7 99.2 109.8 123.1 138.8 168.9 190.3 226.5 281.8	A= 96 0.4 3.9 10.8 17.8 24.3 28.5 22.7 24.9 227.5 30.9 33.6 38.3 43.7 48.2 52.1 58.6 71.3 90.7 112.8 138.5	A= 68 0,2 2.0 6.3 11.2 15.5 19.0 20.0 19.2 17.7 16.5 17.0 19.0 21.0 22.1 25.1 26.0 29.7 32.9 35.8 39.7 47.7 59.8 74.8	A= 159 0, 2 2, 2 9, 1 21, 9 36, 5 49, 7 56, 6 61, 2 56, 4 59, 2 65, 3 72, 1 79, 8 89, 8 101, 2 111, 9 124, 8 150, 7 196, 1 252, 8 305, 8	A= 273 0.1 1.0 4.6 13.0 26.5 41.9 55.7 65.7 69.7 69.2 67.6 67.4 70.9 77.8 85.8 95.4 107.1 119.9 132.8 147.7 170.7 208.7 22.9	A= 107 0.3 2.5 9.0 18.6 27.9 36.0 40.5 38.3 35.6 38.7 42.9 47.5 52.6 57.9 73.5 80.7 97.1 130.5 171.8	A= 151 0.1 1.3 5.9 15.0 26.4 37.4 46.0 50.2 50.2 48.1 46.5 47.9 52.2 57.8 60.7 89.6 98.6 112.4 139.9 183.7 230.5	A= 114 0.5 4.9 14.1 24.1 33.0 39.3 40.8 38.7 35.3 32.9 34.8 38.5 43.0 47.0 53.3 60.9 67.2 72.8 81.4 99.3 134.8
48 50 52 54 56 58 60 62 64 66 68 70 72 74 76 80 82 84 86 88 90	378.0 694.8 780.8 821.9 812.6 760.3 680.0 593.4 516.6 453.0 400.1 354.3 314.4 280.3 251.1 225.6 203.1 183.0 165.2 149.4 135.4 122.9 111.6	240. y 277. 9 289. 1 278. 9 253. 9 217. 7 154. 5 131. 2 96. 8 82. 5 70. 7 60. 9 52. 7 45. 7 39. 7 39. 4 29. 8 22. 4 19. 5	120.4 128.8 118.8 102.9 83.4 68.8 57.0 47.5 39.7 32.7 27.0 22.5 18.8 15.8 15.8 15.8 15.2 11.0	231.9 461.7 461.7 432.2 381.0 323.1 274.9 236.4 204.6 177.4 153.1 132.7 115.6 101.0 88.6 77.8 68.5 60.3 53.0 46.6 40.9	148.3 141.5 127.1 103.7 81.0 65.7 52.7 43.1 34.3 27.0 21.5 17.2 13.7 11.0 8.7 6.9 5.3 4.0 2.8 1.9	72.1 101.6 99.6 91.0 77.0 61.1 40.9 33.8 27.7 22.3 18.2 14.9 12.2 10.0 8.2 6.7 5.5 4.4 3.5 2.7 2.0	363.8 359.6 369.7 220.7 278.2 234.0 199.0 170.4 146.9 126.5 108.4 93.5 81.0 70.4 61.4 53.6 40.8 35.6 31.1 27.1	202.1 369.4 390.9 385.7 353.9 276.4 240.2 210.1 185.0 144.7 128.7 128.7 128.7 67.4 60.9 55.2	204.2 224.1 225.9 211.8 187.6 155.7 128.8 108.2 91.0 77.0 64.4 54.0 45.6 32.9 27.9 23.7 20.2 17.1 14.6 12.4	266.8 286.0 284.8 266.5 236.1 201.3 171.7 148.1 128.5 111.7 96.8 84.2 73.6 56.8 50.1 44.2 39.1 30.4 26.8 23.6	208.0 217.2 207.2 186.5 154.4 121.5 99.0 80.0 85.7 53.1 42.2 33.9 27.4 22.2 17.9 14.5 11.6 9.2 7.2 5.3 3.8 2.5 1.6
92 94 96 98 100 102 104 106 108 110 112 114 118 120 122 124 128 130 132 134 136 138 140	101.3 91.9 83.2 75.2 67.9 61.3 55.4 50.2 45.5 41.4 37.6 34.1 30.8 27.7 24.8 22.0 19.4 16.9 12.3 10.2 6.3 4.5 10.2 6.3 10.2 6.3 10.2 6.3 10.3 10.8	14.7 12.7 10.9 9.2 7.7 6.3 5.0 3.9 2.8 1.9 1.3 0.4 0.2 0.1 0.0 0.0 0.0 0.0	2.6 1.9 1.3 0.8 0.5 0.1 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	31.6 27.8 24.5 21.6 18.4 14.1 10.1 8.3 6.6 5.1 3.7 2.5 1.6 0.5 0.2 0.1 0.0 0.0	0.4 0.2 0.1 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.9 0.6 0.3 0.2 0.1 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	20.8 18.1 15.8 13.6 11.7 9.9 8.2 6.6 5.2 3.9 1.9 1.2 0.7 0.2 0.1 0.0 0.0 0.0 0.0	45.1 40.7 33.0 29.7 26.8 24.1 21.8 19.7 17.9 16.1 14.6 13.0 10.2 9.0 7.8 6.6 5.5 4.5 2.7 1.9 1.9	7.3 5.9 4.6 3.5 2.5 1.7 1.0 0.3 0.2 0.1 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	20.8 18.4 16.3 14.4 12.7 11.2 9.7 8.4 7.1 6.0 4.9 3.9 3.0 2.2 1.5 0.6 0.2 0.1 0.0 0.0 0.0	0.9 0.5 0.3 0.1 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0

		1.1.9.									
(DAM NO.)	(NO. 1) A= 528	(NO. 2) A= 344	(NO. 3) A≃1371	(HO, 4) A= 976	(NO. 5) A= 585	(NO. 6) A= 798	. (NO. 7) A=2253	.(NO. 8) A=1452	(NO. 9) A= 614	(NO.10) A=1040	(NO.11) A= 226
HOUR	A- 360	H- 344	4-1311	K- 710	A- 202	A- 170	N-2673		11		<u> </u>
, ,	0.2	0.3	0.3	0.4	0.2	0.3	0.6	0.4	0.3	0.3	0.2
2	2.2	0.3 2.7	0.3 2.1	3.6	2.0	2.4	4.0	3.3	2.5	2.4	2.2 9.3
. 6 8	27.2	11.4 28.3	8.1 25.2	16.3 45.5	8.8 25.0	10.0 28.9	15.5 48.0		10.8 30.6	9.8 29.6	23.0
10	52.5	48.5	57.7	91.1 142.2	51.3 81.5	61.5	109.6	88.7	62.8	65.9	39.6
12 14	79.8 103.1	67.2 81.4	106.0 162.1	187.1	108.9	100.5 138.5	200.3 305.0	155.8 230.0	99.8 133.3	115.1 168.9	54.8 66.4
. 16	118.1	87.3	214.0	218.5	129.0	167.7	400.5	292.1	157.9	213.7	71.2
18 20	122.9 120.1	86.2 82.2	253.2 274.2	230.6	137.5 137.1	182.4 185.3	472.1 509.4	334.8 352.9	168.3 167.8	243.8 256.2	70.3 87.1
5.5	116.4	79.7	280.6	221.8	134.0	182.0	519.9	353.4	164.0	256.1 254.4	65.0
24 26	117.3 124.9	82.8 90.9	280.6 284.8	232.0	133.4 140.1	180.3 187.9	519.5 527.6	351.4 359.7	163.3 171.5	8,065	67.5 74.1
28	137.7	100.4	299.1 324.9	257.4	153.4	203.8	554.8	381.7	187.8 207.1	277.3 304.4	81.9
30 32	152.4 169.7	111.1 124.7	357.7	284.4 316.3	169.2 188.2	224.5 249.7	603.4 664.7	418.8 462.7	230.4	336.6 336.6 375.3 420.0 468.4 522.5 596.8 711.0	90.6 101.7
34	190.9	140.6	398.3 444.4	355.4	211.2	279 4	740.4	515.9 577.2	258.5 289.4	375.3	114.7 127.0
36 38	213.4	155.7 170.8	495.9	397.8	236.4 262.0	312.9 347.9	826.3 922.2	643.8	320.8	468.4	139.3
40	262.0	192.8	553.8	489.1	291.0	386.4	1031.1	718.3	357.6 417.7	522.5	157.3
42 44	303.4 369.3	230.1 286.2	623.9 722.9	564.5 686.8	334.6 404.3	442.4 529.8	1168.5 1371.5	819.4 973.7 1212.0	520.2	711.0	188.7 238.0
46	458.3	357.8	867.0 1055.9	857.5	502.8	658.4	1680,0	1212.0 1494.6	660.8 807.4	887.3 1094.6	300.7 356.8
48 50	556.7 634.7	426.9 466.0	1264.3	1048.6 1201.8	616.5 711.7	809. <i>9</i> 943.0	2068.4 2476.0	1769.8	915.2	1292.8	386.3
52 54	865.4	433.3	1264.3 1440.5 1540.7	1270.0	760.1 754.6	1021.1	2789.2 2950.5	1958.6 2028.4	964.3 951.4	1426.6	384.0 357.3
54 56	648.0 594.3	380.6	1547.0	1250.3 1158.5 1024.8	705.2	1028.2 975.1	2936.7	1982.8	886:4	1472.3 1435.4	313.6
58	520.4 447.5	321.7	1470.8 1343.3	1024.8	628.7 546.2	880.5 772.7	2778.0 2529.4	1841.9	789.3 685.7 596.2	1330.1 1191.8	265.1 225.6
65 28	387.5	273.7 235.0	1197.7	886.0 768.8	6/4./	673.4	2250.5	1653.6 1457.4	596.2	1049.4	193.7
64	338.5 296.8	203.2 176.0	1061.1 943.1	672.4 591.2	415.4 366.1	590.5 521.9	1993.0 1770.9	1286.1 1140.3	521.9 460.2	1049.4 925.5 820.6	167.5 145.1
. 66 . 86	260.9	151.6	842.7	521.6	323.6	462.4	1582.6	1016.3	407.0	731.1	125.0
70 72	229.6 203.0	131.1 114.0	755.6 679.6	460.9 409.0	286.5 255.0	411.0 367.0	1418.8 1276.6	908.9 816.0	360.5 320.9	653.6 586.6	108.1 94.0
74	180.3	99.5	614.8	364.9	. 228.0	329.5 296.8	1155.3	736.9	286.9	529.5	82.1
.76 78	160.4 143.1	87.1 76.5	559.3	326.1 291.9	204.5	296.8 267.8	1050.8	668.9	257.3 231.1	480.5 437.3	71.9 63.1
80	127.8	67.2	511.4 468.8	261.9	183.6 165.2	241.9	880.2	\$55.8	207.9	398.7	55.4
82 84	114.5	59.0 51.8	430.5 395.7	235.4 211.9	148.8 134.3	218.9 198.3	807.7 741.6	507.5 463.7	187,3 169,1	363.8 332.2	48.7 42.7
86 .	102.7	45.4	363.7	. 191.2	121.5	180.0	681.3	424.1	153.0	303.6	37.5
88 ° 90	82.8 74.2	39.8 34.9	334.5 307.9	172.7 155.9	110.0 99.7	163.7 149.0	626.2 576.3	388.4 356.3	138.6 125.6	303.6 277.9 254.8 233.9	32.8 28.8
95	66.4	- 30.7	283.9	140.4	90.3	135.8	531.1	327.2	113.8	233.9	25.3 22.3
94 96	59.3 53.0	27.0 23.7	262.0 242.2	126.3 113.4	81.7 73.7	123.7 112.6	490.1 452.8	301.0 277.1	102.8 92.8	215.1 197.9	22.3 19.6
98	47.3	20.8	224.1	101.8	66.4	102.3	419.0	255.3	83.6	182.1	17.2
100 102	38.0	18.1 15.7	207.6 192.4	.91.4 82.2	59.8 53.9	92.7 84.0	387.9 359.2	235.2 216.4	83.6 75.4 67.9	215.1 197.9 182.1 167.6 154.1	14.9 12.9
104	34.2	13.4	178.3	74.1	48.6	76.1	332.6	198.9 182.5	61.3	161.6	11.1
106 108	- 30.7 27.5	11.3 9.4	165.1 152.7	66.8 60.4	44.0 39.8	69.0 62.6	307.7 284.2	182.5	55.4 50.2	129.6 118.6	9.3 7.7
110	24.5	7.6	141.0	54.4	36.1	56.9	262.1	153.2	50.2 45.5	108.6	6.3
112 114	21.7 19.1	6.0 4.5	130.1 119.9	49.0 43.8	32.7 29.5	51.8 47.2	241.5 222.5	140.5 128.9	41.2 37.2	99.5 91.2	4.9 3.7
116	16.6	3.1	110.6 102.1	38.9	26.5	42.9	205.2 189.3	118.3	37.2 33.5	83.7.	2.6
118 120	14.3 12.2	2.1 1.3	102.1 94.3	34.3 30.0	23.7 21.0	39.0 35.2	189.3 174.8	108.7 99.9	29.9 26.5	76.8 70.6	1.7 1.0
122	10.1	0.7	87.1	25.9	18.5	31.7	161.4	92.0	23.3. 20.3	64.9 59.7	0.6
124 126	8 2 6 5	0 4 0 2	80.5 74.5	22.1 18.5	16.1 13.9	28.3 25.1	149.1 137.9	84.6 77.8	20.3 17.5	54.8	0.3 0.2
128	4.9	0.1	68.9	15.1	11.8	22.0	127.5	71.4	. 14.8	50.2	0.1
130 132	3.5 2.3	0.1 0.0	63.7 58.9	11.9	9.8 7.9	19.2 16.4	117.9 108.9	85.2 59.2	12.2	45.7	0.0 0.0
134	1.4	0.0	54.4	6.4	6.1	13.9	100.3	53.5	7.6	37.3	0.0
136 138	0.8	0.0	50.0 45.8	4.3 2.7	4.5 3.2	11.4 9.1	92.0 84.1	48.1 43.0	5.6 3.9	33.4 29.7	0.0 0.0
140	0.2	ŏ.ŏ	41.7	1.6	2,1	7.0	76.4	38.0	2.6	26.1	0.0

A. 4.6 Design Flood Hydrograph (1/20)

CUNIT: A=SQ.KM.RUNOFF=CH.M/S

(DAM NO.)	(NO.12) A= 443	(NO.13) A= 147	(NO.14) A= 64	(NO. 15) A= 338	(NO.16) A= 96	(NO.17) A= 68	(NO.18) A= 159	(NO.19) A= 273	(NO.20) A= 107	(NO.21) A= 151	(HO.22) A= 114
CDAM NO.) CATCHNENT HOUR 2 4 6 8 10 12 14 18 20 22 24 28 30 32 34 358 40 24 46 48 50 52 54 68 60 67 72 74 78 80 82 84 88 89 92 94 96 100 110 111 116 118 120 122 126 130 132 136 136 136 136 137 136 136 136 136 136 136 136 136 136 136	(NO. 12) A= 443 0.2 26.7 26.7 589.2 120.1 155.8 155.8 155.8 155.8 155.8 155.8 155.8 156.8 157.9 150.6 150.9 237.7 236.8 237.9 237.8 237.9 247.9 24	(NO.13) A= 147 0.3 2.3 21.5 24.6 54.7 55.8 53.9 55.8 72.9 65.8 72.9 72.1 13.6 179.1 232.6 2813.1 324.5 284.2 243.8 204.1 173.7 126.9 92.4 38.6 33.9 59.1 232.6 281.8 204.1 173.7 126.9 92.4 38.6 38.6 38.6 7.8 7.8 7.8 7.8 7.8 7.8 7.8 7.8 7.8 7.8	(NO. 14) A= 64 0.2 2.1 7.1 13.6 24.4 26.5 24.2 26.5 24.2 26.6 22.9 24.2 26.6 22.9 24.2 26.7 26.6 22.9 26.6 27.7 53.6 27.7 53.3 43.7 53.3 44.6 144.6 115.3 93.3 44.7 67.2 92.0 117.7 144.8 144.8 133.1 115.3 93.3 25.3 117.7 14.8 3.8 2.9 2.1 1.4 0.9 0.5 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	(NO.15) A= 338 0.3 2.8 12.0 30.1 52.2 72.8 88.6 94.8 99.6 87.7 90.5 120.7 136.5 153.8 121.7 136.5 153.8 121.7 136.5 153.8 120.7 136.7 121.7 136.5 153.8 121.7 136.5 153.8 121.7 136.5 153.8 121.7 136.5 153.8 121.7 136.5 153.8 121.7 136.5 153.8 121.7 136.5 153.8 121.7 136.5 153.8 150.5 173.0 150.7 160	(NO. 16) A= 96 0.5 4.3 12.0 19.7 31.5 32.4 30.5 27.6 30.5 27.6 30.5 27.7 64.9 104.1 135.7 104.1 135.7 104.1 135.7 104.1 135.7 107.1 109.2 109.9 7.8 6.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0		(NO. 18) A= 159 0.3 2.5 10.1 24.3 455.1 69.4 67.8 662.5 75.4 80.0 88.5 99.5 1125.9 145.4 178.3 227.0 287.0 287.0 2364.3 385.4 402.2 390.7 358.2 27.0 287.0				
138 140	7.0 5.2 3.6	0.0 0.0 0. 0	0.0 0.0 0.0	0.0 0.0 0.0	0.0 0.0 0.0	0.0 0.0 0.0	0.0 0.0 0.0	2.2 1.5 0.9	0.0 0.0 0.0	0.0 0.0 0.0	0.0 0.0 0.0

A. 4.7 Design Flood Hydrograph (1/100) (UNIT: A=SO.KM.RUNOFF=CU.H/S)

(DAM NO.)	(NO. 1) A= 528	(NO. 2) A= 344	(NO.:3) A=1371	(NO. 4) A= 976	(NO. 5) A= 585	(NO. 6) A= 798	V=5522 (NO' 1)	(NO. 8) A=1452	(NO. 9) A= 614	(NO.10) A=1040	(NO.11) A= 226
HOUR 2 4	0.3 2.6	0.3 3.3	0.4	0.5	0.3	0.3	0.7 4.8	0.5 4.0 15.9	0,3 3.0 13.1	0.4 2.9 11.9	0.3 2.7 11.3
8 10	12.1 33.0 63.7	13.8 34.3 58.9	9.8 30.5 70.0	19.8 55.2 110.5	2.4 10.7 30.3 62.2 98.9	12.1 35.1 74.6	18.8 58.2 133.0	48.1 107.6	37.1 76.2	35.9 80.0	28.0 48.0
12 14	96.9 125.0	81.6	128.6	172.6 227.0	98.9 132.1	121.9	243.0 370.0	189.0	121.1 161.8	139.6 205.0 259.3	66.5 80.6
16 18	143.3 149.2 145.8	105.9 104.6	259.6 307.2 332.7	265.2 279.8 276.4	132.1 156.5 166.8 166.3	168.1 203.5 221.3 224.8	485.9 572.7 618.0	279.0 354.4 406.2 428.1	191.6 204.2 203.6	295.8 310.9	86.4 85.3 81.4
20 22 24	141.2	105.9 104.6 99.8 96.7 100.4	340.5 340.5	269.1 269.3 284.3	161.9	220.8 218.7		428.8 426.4	199.0 198.2	310.7 308.7	78.8 81.9
24 26 28	142.3 151.6 167.1	110.2 121.9	345.5 362.8	312.3	170.0 186.1	228.0 247.3	640.2 673.1	436.4 463.1 508.2	208.1 227.8 251.3	316.4 336.4 369.4	89.9 99.4 110.0
30 32 34 36 38 40	167.1 184.9 205.9 231.6	110.2 121.9 134.8 151.3 170.6	394.2 434.0 483.2	345.1 383.8 431.2	205.3 228.3 256.2	272.4 302.9 339.0	630.8 630.3 640.2 673.1 732.1 806.5 898.3 1002.9 1122.1 1266.4 1463.5	561.4 625.9	279.5 313.7	408.4 455.3	123.4 139.1
36 38	258.9 285.9	188.9 207.3	\$39.2 802.0	482.6 534.4	286.8	379.6	1002.9	700.7 784.4	351.5 392.4 447.4	509.9 570.8 645.1	154.0 169.2 193.3
40 42 44	319.0 376.2	235.2 289.6 379.1	\$39.2 602.0 674.1 767.4 906.7 1117.6	597.4 705.6 892.4	318.1 355.3 417.1 523.0	472.1 551.3 683.6 866.9	1266.4 1463.5 1764.7	885.9 1036.3 1266.8	543.3 689.9	756.5 927.0	242.0 318.9
46 48	477.1 608.7 733.6	479.7 556.1	1117.6	705.6 892.6 1136.4 1373.5 1539.4 1604.6	664.9 808.8	1060.5	2192.4	1588.8 1937.3	864.1 1030.6	1163.5 1416.9	399.4 459.4
50 52	817.3 843.5	593.2 585.9	1646.1 1849.3	1539,4 1604.6	913.7 961.0 947.3	1211.0 1291.3 1290.2	3172.1 3524.6 3694.4	2252.9 2461.4 2531.5	1150.2 1202.6 1181.7	1643.4 1790.8 1836.4	488.4 481.5 446.2
- 54 56 - 58	745.5 652.1	543.4 476.5 402.9	1945.9 1843.7	1568.4 1448.7 1280.2	882.2 785.5	1219.1 1099.0	3660.8 3455.1	2287.0	1098.9 978.0 849.8	1786 6	391.2 330.9 281.8
60 62	608.7 733.6 817.3 843.5 815.6 745.5 652.1 560.9 485.9 424.7	343.0 294.7 254.9 220.7	117.6 1378.2 1646.1 1849.3 1954.0 1945.9 1843.7 1681.2 1498.1 1327.3 1180.0	1107.0 960.8	682.4 593.3 519.5	964,3 840,6 737,4	3142.7 2796.1 2476.8	2052.2	849.8 739.3 647.7 571.3	1650.8 1478.6 1302.2 1148.9	2/.2 1
66 68	372.6 327.6 288.5	220.7 190.1	1367.3 1180.0 1054.8	841.0 739.9 653.1	458.1 405.2	652.2 578.2	2201.6	1809.0 1596.9 1416.5 1263.3	505.4	908.6	209.4 181.3 156.2
70 72	288.5 255.1 226.6	164.6	1054.8 946.1 851.6	577.2 512.4	358.9	514.2 459.3	1968.3 1765.7 1589.7 1439.3	1015.4	447.8 398.6 356.5	812.7 729.7 658.9	135.2 117.7 102.7
74 76 78	226.6 201.6 179.8 160.7	125.0 109.5 96.1	771.0 701.6 641.6	457.0 408.6 365.8	285.7 256.2 230.1 207.0 186.6 168.4 152.4 138.1	412,3 371,4 335,2	1309.4 1197.1	917.1 832.6 758.3	319.8 287.2	597.9 544.2	90.0 79.0
80 82	144.0	84.5 74.2	588.2 540.1	328.2	207.0 186.6	335.2 302.8 274.0	1096.9 1006.5	691.8 631.7	258.4 233.0	496.1 452.7	69.4 61.0
84 86	129.3 116.1	65.1 57.1	496.3 456.2 419.6	295.1 265.8 239.9	168,4 152,4	248.4 225.5 205.1	924.1 849.0 780.4	577.2 528.0 483.7	210.4 190.4 172.5	413.4 377.9 346.0	53.5 46.9 41.1
88 90 = 92	104.2 93.3 83.5	50.0 43.9 38.6	386.3 356.2	216.6 195.4 176.0		205.1 186.7 170.2	718.3 662.1 611.0	443.7	156.2 141.4	317.3 291.3	36.1 31.7
94 96	74.6 86.6	34,0 29.9	328.8 303.9	158.3 142.2	102.4 92.4 83.2 75.0	155.0	611.0 564.7 522.5	407.7 375.1 345.3 318.1	127.8 115.4 104.0	267.9 246.5 226.9	27.9 24.6 21.5
98 100 102	59.6 53.4 47.9	26,2 22.8 19.7	281.4 260.6 241.5	127.7 114.7 103.2	75.0 67.6	128.0 116.1 105.2	483.8 448.0	293.0 269.5	93.7 84.5	208.7 191.8	18.8 16.2
104 106	43.1 38.7	16.9 14.2	223.8 207.2	93.0 84.0	67.6 61.0 55.2 50.0	95.3 86.4	414.7 383.5	247.6	76.3 69.0	176.0 161.2 147.7	13.9 11.7 9.7
108 110 112	34.7 30.9 27.4	11.8 9.5 7.4	191.6 176.9 163.2	75.9 68.5 61.6	45.4 41.1	78.5 71.3 85.0	354.2 326.6 300.9	208.2 190.9 175.0	62.5 56.7 51.3	135.3 123.9	7.8 6.1
114 116	24.1 21.0	5.5 3.8	176.7 163.2 150.4 138.8 128.1 118.4	55.0 48.9	37.1 33.3	59.2 53.9 49.0	277.4 255.8	160.5 147.5	46.4 41.7 37.2	113.6 104.3 95.8	4.5 3.1
118 120	18.1 15.3 12.7	2.5 1.6 0.9	128.1 118.4 109,4	43.1 37.6 32.5	29,8 26.4 23.2	49.0 44.2 39.8	236.0 218.0 201.4	135.5 124.7 114.8	33.0 29.0	88.1 81.0	2.1 1.3 0.7
122 124 126	10.3	0.5	101.1 93.6	27.7 23.1	20.2 17.4	35.5 31.4	186.2 172.3	105.5 97.1	25.2 21.7	74.5 68.4	0.4 0.2
128 130	6.0 4.2	0.1 0.1 0.0	86.6 80.1 74.1	18.8 14.7 11.1	14.7 12.2 9.8	27.6 24.0 20.6	159.2 147.2 136.0	89.0 81.3 73.9	18.3 15.1 12.1	62.5 57.0 51.6	0.1 0.1 0.0
132 134 136	2.8 1.7 1.0	0.0	68.4 62.9	7.9 5.3	7.5 5.6	17.3 14.2	125.2 114.9	66.8 60.0	9.3 6.8	46.5 41.6	0.0 0.0
138 140	0.6 0.3	0.0 0.0	57.6 52.5	3.3 2.0	3.9 2.5	11,3 8.6	104.9 95.4	53.5 47.3	4.7 3.1	36.9 32.5	0.0

A. 4.7 Design Flood Hydrograph (1/100)

(DAM NO.) CATCHMENT HOUR	(NO.12) 6= 443	(NO.13) A= 147	(NO.14) A= 64	(NO.15) A= 338	(NO.16) A= 96	(NO.17) A≃ 68	(NO.18) A= 159	(NO.19) A= 273	(KO, 20) A= 107	(NO.21) A≃ 151	(NO.22) A= 114
CATCHMENT HOUR 2 4 6 10 12 14 16 18 20 22 24 26 28 30 32 34 36 38 40 42 44 48 50 52 54 56 60 62 64 68 70 72 74 76		A= 147 0.3 2.8 11.3 26.1 56.5 66.4 69.1 66.9 63.2 61.6 65.4 72.2 78.9 13.0 129.1 151.8 129.1 151.8 234.3 294.6 349.5 387.5 400.2 384.5 349.5 387.5 13.9 97.7 133.5 113.9 97.7 84.2 72.8 63.1		A= 338 0, 4 14.6 36.3 88.4 107.5 116.0 115.0 115.0 115.0 116.6 116.7 120.7 133.5 147.7 165.6 186.7 206.9 227.8 232.5 437.1 543.0 622.6 628.4 608.2 654.4 608.5 332.5 247.9 249.8 215.7 185.7 185.5 125.1	A= 96 0.6 0.6 2.2 14.6 24.0 32.7 38.3 37.0 33.5 37.0 33.5 37.0 41.5 45.2 51.5 58.8 64.8 70.0 78.9 101.8 145.6 180.7 205.5 212.7 145.8 92.2 74.0 60.5 48.1 37.9 30.2 24.2 115.3	A= 68 0.3 8.4 15.1 20.9 25.5 26.8 23.8 23.8 23.8 23.9 26.9 26.5 26.3 31.1 26.9 26.5 26.3 31.1 26.9 27.1 28.3 31.1 26.0 26.0 26.1 27.1 28.2 28.3 31.1 28.2 28.3 31.1 28.2 28.3 31.1 28.2 28.3 31.1 28.2 28.3 31.1 28.2 28.3 31.1 29.7 29.7 20.1 20.7 20.7 20.7 20.7 20.7 20.7 20.7 20.7	0.3 3.0 12.3 29.5 49.0 66.9 79.7 84.2 82.3 76.1 75.9 79.7 87.8 97.0 107.4 122.0 143.4 169.9 197.5 287.9 358.3 428.8 474.3 478.9 380.6 320.4 201.3 173.4 148.7 128.2 111.1 96.6 84.2	A= 273 0.2 1.4 6.2 17.5 35.6 56.4 74.9 88.3 93.1 90.7 95.3 104.6 128.3 144.1 161.5 180.2 205.9 250.6 319.1 399.1 475.0 528.8 551.3 540.1 550.7 244.5 355.2 293.7 228.8 202.5 180.1 160.9	A= 107 0.4 3.3 12.1 25.0 37.5 48.4 57.5 48.1 47.8 63.8 63.8 63.8 60.6 91.4 105.8 125.5 198.0 247.0 286.6 310.9 311.6 291.4 257.8 214.0 177.1 188.8 125.2 106.7 74.3 62.8 53.2 45.3 38.5	A= 151 0.2 1.8 7.9 20.2 35.6 50.4 61.8 67.5 67.5 64.7 62.5 64.4 70.2 77.7 62.5 109.1 124.4 145.1 174.4 216.8 272.2 277.5 236.9 204.3 177.3 154.3 153.7 116.3 101.8 89.3 78.5	A= 114 0.7 6.6 19.0 32.4 44.4 52.9 54.8 52.1 47.5 46.8 51.8 57.9 63.2 7.8 119.7 81.8 90.4 98.8 119.7 81.6 258.1 213.4 259.4 259.4 259.4 269.6 275.5 168.1 137.0 110.7 91.0 73.5 58.4 47.0 38.8 24.9 20.1
78 80 82 84 85 88 90 92 94 96 100 102 104 108 110 114 115 120 124 126 130 132 138 140	280.0 252.4 208.2 186.2 186.6 153.9 139.7 114.7 103.7 73.7 76.6 69.4 62.9 57.2 47.1 42.6 38.2 34.2 36.6 13.8 11.0 8.5 4.4	54.8 47.5 41.2 35.8 31.0 26.9 23.4 20.3 17.5 15.7 10.6 8.8 5.2 3.8 2.6 1.7 0.6 0.3 0.2 0.1 0.0 0.0 0.0 0.0 0.0 0.0	15.3 12.7 10.6 8.8 7.3 5.9 4.6 3.5 1.7 1.1 0.7 0.2 0.1 0.0 0.0 0.0 0.0 0.0 0.0 0.0	110.0 96.8 85.1 74.8 65.8 67.7 50.8 44.7 39.4 34.7 30.6 26.7 20.0 11.6 9.2 7.0 5.1 3.4 2.2 1.3 0.7 0.4 0.0 0.0 0.0 0.0	9.7 7.4 5.5 3.8 2.5 0.9 0.5 0.1 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	9.5 7.7 6.2 4.9 3.8 2.8 1.9 1.2 0.1 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	73.5 64.2 56.1 48.9 42.7 37.3 32.6 28.5 24.9 21.6 15.9 11.1 9.0 7.3 3.8 2.5 1.6 0.9 0.5 0.1 0.1 0.0 0.0 0.0	129. Z 116. 3 104. 8 94. 5 85. 5 77. 4 70. 0 63. 3 57. 1 51. 4 46. 3 41. 7 33. 9 30. 7 25. 1 18. 3 16. 4 10. 8 9. 2 7. 7 6. 2 4. 7 6. 2 4. 7 6. 3 1. 4 1. 6 1. 6 1. 6 1. 6 1. 6 1. 6 1. 6 1. 7 1. 6 1. 6 1. 7 1. 7 1. 8 1. 6 1. 7 1. 6 1. 7 1. 6 1. 7 1. 6 1. 7 1. 8 1. 6 1. 7 1. 7 1. 8 1.	32.7 27.8 27.7 20.1 17.1 14.4 12.0 9.9 8.0 6.2 4.6 3.3 2.2 1.4 0.8 0.1 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	69.3 61.2 54.0 47.7 42.1 37.1 32.7 28.9 25.5 22.0 17.6 13.4 11.8 8.2 6.7 5.3 4.0 9 2.0 1.3 0.8 0.1 0.1 0.0 0.0 0.0	16.1 12.7 9.8 7.2 5.1 2.1 1.2 0.7 0.3 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0

4.8	100		9 1								
(DAM NO.)	(110, 1)	(NO. 2)	(RO. 3)	(NO. 4)	(NO. 5)	(NO. 6)	(NO. 7)	(NO. 8)	(NO. 9)	(NO.10)	(NO.11)
CATCHMENT	(NO. 1) A= 528	A= 344	A=1371	A= 976	A= 585	A= 798	A=2253	A=1452	A= 614	A=1040	852 =A
HOUR	1.0	to the second	1.13	2000				•			
2	0.3	0.4	0.4	0,6	0.3	0.4 3.3 14.2	0.8	0.6	0.4	0.5	0.3
4	3.1	3.8	2,9	5.1	2.8	3.3	5.6	4.6	3.5 15.3	3.4	3.1
6 8	14.1 38.6	16.1 40.0	11.5 35.6	23.1 64.5	12.5 35.4	// 0	22.0 67.9	18.5 56.2	43.3	13.9 41.9	13 . 2 32 . 6
10	71 1	68.7	81.7	129.0	72.6	87.1	155.4	125.6	88.9	93.4	56.0
12	113.1	95.2	150.1	201.4	115.4	142.3	403.0	220.6 325.7	141.3	162.9	77.6
14	145.9	115.3 123.7	229.5 303.0	265.0 309.5	154.2 182.6	196.2 237.5	431.8	413.6	188.8 223.6	239.2 302.6	94.0 100.9
16 18	113.1 145.9 167.3 174.1 170.1	122.1	358.5	326.5	194.6	87.1 142.3 196.2 237.5 258.3	567.1 668.5 721.4	474.1 499.7	238.3	345.3	99.6
20	170.1	116.5	388.3 397.4	322.6	194.1	262.4 257.7 255.3	721.4	499.7	237.7	362.9	95.0
55	164.8	112.8	397.4 397.4	314.1 314.3	189.7 188.9	257.7	736.3 735.6	500.5 497.6	232.2	362.6	92.0 95.6
22 24 26 28 30	176.9	117.2 128.7 142.2	403.3	331.8	198.4	266.1	747.2	509.4	242.9	360.3 369.3 392.6	104.9
28	195.0	142.2	423.5 460.1	331.8 364.5	217.2	266.1 288.6 317.9	785.6	509.4 540.6	265.9	365.9	116.0
30	215.8 240.3	157.4 176.6	460,1	402.7	239.6	317.9	854.5	593.1 655.3 731.4	293.3	431.1	128.4 144,1
32 34	270.3	199.1	564.0	503.3	266.5 299.0 335.0 373.8	395.7	1049.4	731.4	367.0	532.2	162.4
36	302.2	199.1 220.5	629.7	563.8	335.0	443.6	1176.2	823.6	415.9	599.7	162.4 180.0
38	335.1 380.7	243.7	704.8	447.9 503.3 563.8 628.3 718.0	373.8	497.3	1329.9	935,2	4//.2	431.1 476.6 532.2 599.7 681.7 790.6	200,4 238.8
40	465 2	365 9	923.7	877.1	516.5	682.7	1806.4	1289.9	683.3	943.2	308.2
44	599.9	478.3	1115.6	877.1 1120.9 1402.9	656.0	855.5	2192.5	1575.5	849.7	1152.6	398.1
46	755.1	588.2	1384.2	1402.9	822.3	1071.5	2698.9	1945.3	1043.5	1422.7	485.5 550.8
48 50	981.7	708 8	460.1 506.6 564.0 629.7 704.8 797.3 923.7 1115.6 1384.2 1695.8 1998.5	1843.8	1095.6	1451.7	3803.1	731.4 823.6 935.2 1082.8 1289.9 1575.5 1945.3 2336.1 2690.2 2924.2 2998.9	231.3 242.9 265.9 293.3 326.3 367.0 415.9 477.2 560.8 683.3 849.7 1043.5 1230.8 1365.6 1423.3 1396.2	943.2 1152.6 1422.7 1706.5 1960.9 2126.6 2174.7	581.7
52	1006.8	697.2	2221.9	1911.7	1145.7	1538.9	4197.2	2924.2	1423.3	2126.6	581.7 571.6 528.9
54	970.5	645.4	2332.9	1863.2	1125.9	1532.7	4383.8	2998.9	1396.2	2174.7	-528.9 -463.6
48 50 52 54 56 58	380.7 465.2 599.9 755.1 891.7 9106.8 970.5 885.9 774.8 666.7 577.9 505.3 443.5	243.7 285.2 365.9 478.3 588.2 669.8 708.8 697.2 645.7 478.6	2221.9 2332.9 2316.2 2191.0 1996.5 1779.0 1576.6 1402.1 1253.7 1125.1 1013.3 917.6 835.1	1402.9 1663.1 1843.8 1911.7 1863.2 1718.8 1518.5 1313.5 1140.7 998.9 879.1 776.2 686.0	425.7 516.5 656.0 822.3 981.4 1095.6 1145.7 1125.9 1047.0 931.8 809.7 704.4 617.1 544.4 481.5 426.7 379.8	353.6 395.7 443.6 497.3 566.8 682.7 855.5 1071.5 1286.8 1451.7 1445.9 1532.7 1445.9 1302.9 1143.3 997.0 875.1	785.6 854.5 941.3 1049.4 1176.2 1329.9 1530.9 1806.4 2192.5 2698.9 3262.3 3803.1 4197.2 4383.8 4335.1 4087.5 3717.0 3307.5 2930.6	2916.8 2703.2 2425.6	1156 4	2110.0 1950.9	392.3
60	666.7	407.7	1996.5	1313.5	809.7	1143.3	3717.0	2425.6	1003.7	1950.9 1747.3	334.2
.62	577.9	478.6 407.7 350.3 303.0 262.4 226.1 195.8 170.4 148.8 130.4	1779.0	1140.7	704.4	997.0	3307.5	2138.6 1888.6	1003.7 873.6 765.5 675.4	1539.2 1358.6	287.2 248.4
64 66	505.3 7.7.5	262.6	12/6.6	879.1	544.4	774.3	2605.9	1676.0	675.4	1205.6	215.1
68	303.7 393.4 303.7 269.8 240.2 214.2 191.5	226.1	1253.7	776.2	481.5	774.3 686.7 610.8	2330.8	1495.3	597.6	1205.6 1075.2 962.0 864.0 780.2 708.0 644.4 587.5 536.1 489.7 447.7 449.9 376.0	185.4
70	343.4	195.8	1125.1	686.0 609.0 543.3 485.8	426.7	610.8	2091.8	1338.5	529.5 471.4 421.7 378.3 339.8 305.8 275.7 249.0 225.3 204.1 184.9	962.0	160.5 139.7
70 72 74 76 78	303.7 269.8	1/0.4	1013.3 917 K	543.3	379.6	545.7 489.9	1883.8 1705.9 1552.2	1202.4	421.7	780.2	122.1
76	240.2	130.4	835.1	485.8	304.7	441.3	1552.2	986.2 898.1	378.3	708.0	107.0
78	214.2	114.5 100.6	763.7 700.2 642.9 590.8	435.0 390.4	273.6	441.3 398.3 359.9	1419.0 1300.3 1193.1	898.1	339.8	644.4	93.9 82.5 72.4 63.5 55.7 48.9 42.9
80 82	191.5 171 A	88.3	700.2	351.0	240.2		1193.1	819.5 748.4 683.9	275.7	536.1	72.4
84	154.1	77.5	590.8	316.3	200.4	295.2 268.1	1095.5	683.9	249.0	489.7	63.5
86	154.1 138.3	67.9 59.6	543.0 499.5 460.0	245 5	181.4	268.1	1006.5	625.7	225.3	447.7	55.7
88 90	124.1 111.2	59.6 52.3	449.5	237.7	164.3	243.8	973.4 851.8	573.2 525.9	184.9	376.0	42.9
92 :	99.4	46.0	424.1	209.3	134.7	202.3	785.2	483.2 444.6	167.3 151.2	345.2	
94	88.9	40.5 35.6	391.6	188.3	339.6 304.7 273.6 246.2 221.9 200.4 181.4 164.3 148.9 134.7 121.8	184.3	1193.1 1095.5 1006.5 925.4 851.8 785.2 724.7 669.9	444.6	151.2	345.2 317.5 292.1	33.2 29.2 25.6
96	79.4 71.0	35.6 31.2	362.0	169.1	00 1	167.6	669.9 410 0	409.3 377.0	136.5 123.1	292.1 268.8	29.2 25.6
98 100	63.7	27.2	391.6 362.0 335.2 310.5 287.7 266.6 246.8 228.1 210.6 194.2	267.7 232.5 209.3 188.3 169.1 151.9 136.5 122.8 110.8	89.3 80.5 72.7	222.1 202.3 184.3 167.6 152.2 138.0 125.0	619.9 573.9 531.3 491.8 454.7	347.1 319.3 293.4	110.9 100.0	268.8 247.2 227.1 208.5 191.0	22.3
102	63.7 57.2	27.2 23.5 20.1 16.9 14.0 11.2 8.7	287.7	122.8	80.5	125.0	531.3	319.3	100.0	227.1	19.3
104	51.4 46.2	20.1	6.365 8 456	110.8	72.7 . AS R	123.0 113.3 102.8 93.4 84.9 77.3 70.5 64.1 58.2	491.8 454.7	249.4	90.4 81.8	208.>	16.5 13.8
106 108	41.4	14.0	228.1	90.5	65.8 59.6 54.1	93.4	417.7	269.2 246.7	74.1	175.0	11.4
108 110 112	36.9	11.2	210.6	81.5	54.1	84,9	387.3 356.9	226.2	67.2 60.8	175.0 160.3 146.9	9.2
112	32.7 28.7	8.7 6,4	194.2 179.1	73.3 65.5	48.9	77.3	356.9 329.0	207.5	56.8	146.9 134.7	7.1 5.2
114 116	25.0	4.5	165.3	58.2	44.2 39.7 35.5	64.1	303.4	174.9	54.9 49.3 44.0	123.7	3.7
118	21.5	. 2.9	152.6	51.3	35.5	\$8.2	303.4 279.9	160.8	44.0	113.6	2.4
120	18.2 15.1	1.8 1.0	141.0 130.4	44.7 38.6	31.4 27.6	52.6 47.3	238.6	147.9	39.0 34.2	104.5 96.1	1.5 0.8
122 124	12.2	0.6	120.6	32.8	24.0	52.6 47.3 42.2	258.6 239.0 221.0 204.5 189.1 174.8	226.2 227.5 190.3 174.9 160.8 147.9 136.2	29.8	88.3	0.5
126	9.5	0.3 0.2	111.6 103.3	27.3	20.6	37.4	204.5	112.1	25.5	81.1	0.2
128	7.0 4.9	0.2	103.3	22.1 17.3	17.4 14.4	32.8 28.5	189.1 176 8	105.5	21.5 17.7	74.1 67.5	0.1 0.1
130 132	3.3	0.1	95.5 88.4	12.9	11.5	24.4	161.4	96.3 87.6	14.1	61.2	0.0
134	2.0	0.0	81.5	9.2	8.9	20.5	148.6	79.1 71.0	10,8	55.0	0.0
136	1.2 0.7	0.0	75.0 68.7	. 6.2 3.9	6.5	16.7 13.2	136.3 124.5	/1.0 .63.4	8.0 5.5	49.2 43.7	0.0
138 140	0.7	0.0 0.0	62.6	2.3	3.0	10.1	113.1	63,4 56.0	3.6	43.7 38.4	0.0

A.4.8 Design Flood Hydrograph (1/500)

(UNIT: A=SQ.KM.RUNOFF=CU.M/S)

(DAM NO.) CATCHMENT HOUR	(69.12) (NO.13 A= 443 A= 14) (NO.14) 7 A= 64	(NO.15) A= 338	(NO.16) A= 96	(NO.17) A= 68	(NQ.18) A= 159	(NO.19) A= 273	(NO.20) A= 107	(NO.21) A= 151	(NO. 22) A= 114
2 4	0.3 0.4 3.0 3.3 13.2 13.2	0.3 3.0 10.0	0.4 4.0 17.1	0.6 6.1 17.0	0.3 3.2 9.9	0.4 3.5 14.4	0.2 1.6 7.2	0.4 3.9 14.1	0.2 2.1 9.2	0.8 7.7 22.2
8 10	37.8 30.5 78.7 49.1	19.3 27.6	42.6 73.9	28.0 38.2 44.7	17.6 24.4	34.4 57.2	20.4 41.6	29.2 43.8	23.5 41.5	37.8 51.8
12 14	126.3 66.0 170.9 77.4	34.6 37.5	103.2 125.5	45.8	29.8 31.3	78.0 93.0	65.8 87.4	56.5 63.4	58.8 72.2 78.8	61.7
16 18	204.1 80.6 219.2 78.1	36.7 34.2	135.4 134.2	43.2 39.1	30.1 27.8	98.2 96.0	103.1 109.4 108.7	63.6 60.1	78.7	60.8 55.4
20 22	220.2 73.7 215.6 71.9	32.0 32.4	128.3 124.2	36.5 39.1	25.8 26.8	91.1 88.5	106.1	56.2 55.8	75.5 73.0	51.7 54.6
24 26	214.2 76.4 224.4 84.3 244.9 93.2	35.8 39.6	128.6 140.9 155.8	43.1 48.4	29.8 33.0	88.5 93.0 102.5	105.8	60.8 67.4	75.2 82.0	60.4 67.5
28 30 32	244.9 93.2 271.0 103.3 306.6 118.1 358.3 140.3	43.6 48.7	172.3 193.3	52.7 60.1	36.2 40.8 46.7	113.4 127.7 152.0	122.1 134.7 149.8	74.5 82.8 96.6	90.7 100.5 113.8	83.6
34 36	358.3 140.3 424.1 166.5	48.7 56.3 66.7 79.1	217.9	68.6 75.6 82.1	51.6 56.3 65.9	184.1	168.6 191.3	116.5 137.1	133.4 158.3	95.6 109.1 129.6
38 40	495.6 192.2 571.3 227.4	91.5 112.6 143.2	274.0 330.4	99.3 134.6	65.9 88.2	184.1 213.8 241.8 280.9 343.0	219.7	154 7	184.3 215.4	155.7 197.4
42	671.6 281.6 811.5 350.4	1/5.9	422.6	181.1 218.2 245.2	117.8 145.7	343.0 423.8	219.7 258.6 315.2 392.4	236.6	261.9 325.0	256.4 308.3
46 48	982.5 413.2 1151.8 456.8	200.6 213.7	655.5 743.7	252.4	165.5 174.1	423.8 501.7 557.7 579.8	481.5 566.9	188.2 236.6 292.7 338.1 365.9 366.2	390.1 441.3 467.6	345.7 357.9
55 50	1277.0 470.9 1334.1 452.1	209.5 192.4	786.6 775.2	236.9 211.2	167.5 151.6	579.8 562.1	627.6	366.2 342.2	462.8	338.7 303.5
54 56	1313.9 410.8 1227.3 352.4 1097.7 295.1 958.7 250.4	166.6 135.1 111.4	719.4 632.7	171.9 134.5	127.9 101.7	562.1 514.9 446.6 375.9	638.0 591.1	342.2 302.7 251.4	431.9 382.4	251.0 197.7
58 60	1227.3 352.4 1097.7 295.1 958.7 250.4	111.4 92.4 77.0	537.0 457.7 393.9	109.0 87.4 71.4	83.4 68.0	3/5.9 319.8	455.2	208.1 174.8 147.1	326.4 278.6	161.1 130.2
62 64 66	835.4 213.7 733.0 183.6 647.9 157.1	64.4 53.0	3/1 0	56.9 44.8	68.0 56.3 46.2 37.2 30.3	373.9 319.8 274.0 236.3 203.6 174.6	481.5 566.9 627.6 652.2 638.0 591.1 524.7 455.2 346.9 305.8	124.6	240,4	107.0 86.4
68 70	573.9 133.9 509.5 114.9	43.9 36.6	295.8 255.5 221.6	35.7 28.6	30.3 24.8	174.6 150.6	270.4 239.4	124.6 104.2 87.3 73.8	181.5 157.4 137.0	68.7 55.3 44.7
72 74	454.4 99.0 407.3 85.7	30.6	193.2 169.0	22.9	20.4 16.7	130.4 113.5	213.0 190.3	62.6 53.2 45.3	119.8 105.1	36.2 29.3
76 78	366.1 74.3 329.6 64.5	21.4 17.9	148.3 130.4	18.3 14.5 11.4	13.7 11.2	98.9 86.4	170.6 153.1	45.3 38.5	92.5 81.6	23.5 18.8
80 82	297.2 56.0 268.4 48.6	15.0 12.5	114.8 100.9	8.7 6.4	9.1 7.4	75.4	137.6 124.0	32.7 27.8	72.0 63.6	14.8 11.4
84 86	242.7 42.1 219.9 36.5	10.4 8.5	88.8 78.0	4.5 3.0	5.8 4.4	65.9 57.5 50.2	111.9 101.2	23.6	56.2 49.5	8.4 5.9
88 90	199.5 31.7 181.2 27.5	5.4	68.5 60.2	1.8 1.1	3.2	43.8 38.3	91.5 82.8	16.9 14.1	43.7 38.5	4.0 2.5
92 94	164.5 23.9 149.1 20.6	4.1 2.9	53.0 46.8	0.6 0.3	1.5 0.9	33.4 29.2	82.8 74.8 67.5	11.6 9.3	34.0 30.1	1.4 0.8
96 98	135.0 17.6 122.1 14.9 110.4 12.3	2.0 1.3	. 41.2 36.3	0.2 0.1	0.5 0.3 0.1	25.3 21.8	60.9 54.8 49.3	7.2 5.4	26.6 23.5 20.7	0.4
100 102 104	110.4 12.3 99.8 10.1 90.2 8.0	0.8 0.4 0.2	31.7 27.6 23.7	0.0 0.0 0.0	0.1 0.0	18.6 15.6 12.9	44.5 40.1	3.9 2.6 1.6	18.1 15.8	0.1 0.1 0.0
106 108	81.7 6.1 74.1 4.4	0.1 0.1	20.1	0.0 0.0	0.0	10.5	36.3 32.9	1.0	13.6 11.5	0.0
110 112	67.3 3.0 61.1 2.0	0.0	13.7	0.0	0.0	6.2 4.4	29.8 26.9	0.3 0.1	9.6 7.8	0.0
114 116	55.4 1.2 50.1 0.7	0.0	8.2 5.9	0.0	0.0	3.0 1.9	24.2 21.7	0.1	6.2	0.0 0.0
118 120	45.0 0.4 40.2 0.2	0.0	2.6	0.0 0.0	0.0	1.1	19.3 17.0	0.0	3.4 2.3	0.0
122	35.6 0.1 31.2 0.1	0.0	1.5	0.0	0.0	0.3	14.8 12.8	0.0	0.9	0.0
124 126 128	27.1 0.0 23.2 0.0	0.0	0.5 0.2	0.0	0.0	0.1 0.0	10.8 9.0	0.0	0.5	0.0
130 132	19.5 0.0 16.1 0.0	0.0	0.1 0.1	0.0	0.0	0.0	7.3 5.7	0.0	0.1	0.0
134 136 138	12.9 0.0 9.9 0.0 7.3 0.0	0.0 0.0 0.0	0.0 0.0 0.0	0.0 0.0 0.0	0.0 0.0 0.0	0.0 0.0 0.0	4.3 3.1 2.1	0.0 0.0 0.0	0.0 0.0 0.0	0.0 0.0 0.0
140	5,1 0.0	0.0	0.0	0.0	0.0	0.0	1.3	0.0	0.0	0.0

A. 4.9 Design Flood Hydrograph (1/1,000) CUNIT: A=SQ.KM.RUNOFF=CU.M/S)

	Table 1		*********	********	********	*******	*******	****** (UNIT: A≈SO	.KM,RUNOFF	≃CU.M/S)
	18.5										
CDAM NO	.) (NO. 1)	(NO, 2)	(NO. 3)	(NO. 4)	(NO. 5)	(NO. 6)	(110. 7)	(NO. 8)	(NQ. 9)	(#0.10)	(NO.11)
CATCHME	NT A= 528	A= 344	A=1371	A= 976	A= 585	A= 798	A=5523	A=1452	A= 614	A=1040	A= 226
HOUR											
: 2 4	0.3 3.2	4.0	0.5	0.6 5.4	0.3 3.0	0.4 3.5	0.9 5.9	0.7 4.9	0.4 3.7	0.5 3.6	0,3 3.3
6	14.9	17.1	3.1 12.2	24.5	13.2	15.0	23.3	19.6	16.2	14.7	13.9
8	40.8 78.8	42.4 72.8	37.8 86.6	68.3	37.5 76.9	43.4 92.2	72.0 164.4	59.5 133.0	45.9 94.2	44.4 98.9	34.6 59.3
10 12	119.8	100.8	159.0	213.4	122.3	150.7	300.4	233.7	149.7	172.6	82.2
14 16	154.6 177.2	122.1	243.2 320.9	280.7 327.8	163.3 193.5	207.8 251.5	457.4	345.0 438.1	200.0 236.9	253.4 320.5	99.6
: 18	184.4	129.3 123.4	379.8	345.9	206.2	273.6 277.9	600.7 708.1	502.2	252.4	365.8	105.5
20 20	180.2 174.6	119.5	411.3 420.9	341.7 332.7	205.6	277.9 273.0	764.1 779.9	529.3 530.1	251.8 246.0	384.4 384.1	100.6 97.5
24	176.0	124.1	420.9	333.0	200.1	270.4 281.9	779.2	527.1 539.6	245.0	381.6	97.5 101.3
26 28	176.0 187.4 206.6	124.1 136.3 150.6	427.2 448.6	351.4 386.1	210.1 230.1	305.7	791.5 832.2	539.6 572.6	257.2 281.7	391.2 415.9	111.2 122.9
. 30	228.6	166.7	487.3	4.86.6	253.8	336.7	832.2 905.2	628.3	310.7	456.6 505.1	136.0 152.6
32 34	254.5 286.3 320.4	187.1 210.9	536.6 597.5	474.5 533.2	282.2 316.8	374.5 419.3	997.4 1113.1	694.4 776.4	345.9 390.7	565.0	172.0
36	320.4	233.8	667.7	598.3	355.5	471.1	1253.0	878.8	447.2 519.7	640.2 735.5	191.5 216.4
38 40	356.9 410.6	260.5 310.7	749.8 853.0	671.7 778.7	399.3 460.9	531.7 613.8	1427.1 1657.6	1008.0 1175.9 1402.4	612.5	859.0 1025.3	261.9
. 42		401.0	997.7	778.7 956.9	562.9	743.4	1657.6 1961.7	1402.4 1701.1	739.5 912.3	1025.3 1243.9	335.9 428.6
44	813.4	517.5 630.9 715.6	1209.2 1497.9	1507.9	711.6 884.6	927.6 1152.8 1376.8	2372.7 2902.3 3490.8 4057.8	2087.1 2495.8	1115.1	1525.6	519.5
. 48	954.7	715.6 755.7	1824.2 2140.0	1778.6	884.6 1050.0	1376.8 1549.2	3490.8	2495.8 2867.8	1311.9 1453.5	1822.7 2089.9	587.6 619.6
50 52	507.1 652.1 813.4 954.7 1047.6 1073.3 1033.8 943.4	742.6	2372.4	1214.9 1507.9 1778.6 1967.0 2036.7	1169.1 1220.8 1198.8 1114.5	1639.8	4471.2 4665.6	3113.1	1513.6	2263.6	608.4
54	1033.8	687.1 602.3	2487.4	1983.7 1329.4	1198.8	1631.8 1538.8	4665.6	3190.2 3101.7	1484.2	2313.2	562.8 493.3
56 58	042.1	509.6	2333.1	1616.2	331'0	1386.5	4611.4 4346.9	2874.1	1378.9 1227.3	2074.1	417.5
60	710.1	434.2 373.1	2372.4 2487.4 2467.5 2333.1 2125.8 1894.3	1398.2	862.0 750.0	1216.7 1061.2	3952.8 3517.5	2579.0 2274.1	1067.0 928.7	1857.6 1636.7	355.7 305.7
62 64	615.6 538.4	322.7 279.5	10/0.7	1214.5 1063.6	657.1	931.7	3117.0	2008.6	813.9	1636.7 1444.8	264.3
. 66 68	472.6 415.6	279.5 240.9	1493.2 1335.5	936.2 826.6	579.7 512.8	824.3 731.2	2772.2 2479.8	1782.6 1590.6	718.2 635.4	1282.3 1143.7	229.0 197.4
70 72	365.9	208.6	1198.7 1079.6 977.8 889.9 813.9	730.6	454.4	650.4	2225.7 2004.6 1815.4 1651.8	1423.9	563.1 501.3	1023.4	170.9
72 74	323.7 287.6	181.5 158.6	1079.6 977.8	648.6 578.7	404.5 361.8	581.1 521.7	2004.6 1815.4	1279.3 1155.7	301.3 448.5	919.2 830.0	148.8 130.0
76	256.0 228.4	139.0	889.9	578.7 517.4	324.5	521.7 470.0	1651.8	1049.2	402.4	753.3	113.9
78 80	228.4 204.2	122.0	813.9 746.2	463.4 415.9	291.5 262.3	424.2 383.3	1510.1 1383.8 1269.7	955.6 871.9	361.5 325.3	885.6 825.1	100.0 87.8
82	183.0	94.1	685.1	374.0 337.0	236.5	383,3 346.9 314,5	1269.7	796.3	293.3 264.9	570.5 521.0	77.1 67.6
84 86	164.2 147.5 132.3	82.5 72.4	629.6 578.7	304.1	213.6 193.2	285.6	1166.0 1071.3	727.7 665.8	239.7	476.4	59.4
88 1	132.3	63.5	532.3 490.2	274.5	175.1 158.6	285.6 259.8 236.6	985.0 906.7	610.0 559.7	217.1 196.6	436.2 400.1	52.0 45.7
90 92	118.5 106.0	55.8 49.0	452.1	247.6 223.0	143.5	215.5	835.9	514.3	178.0	367.4	40.2
94	94.7	43.2	417.4	200.6	129.7 117.1	196.3 178.4	771.5 713.1	473.2 435.6	160.9 145.2	337.8 310.8	35.4 31.1
96 98	84.7 75.7 67.9	38.0 33.3	385.9 357.3	180.2 161.8	105.5	162.1	450. Ø	401.2	130.9	286.0	27.3
100 102	67.9 61.0	29.0 25.0	330.9	145.4 130.9	95.1	147.0 133.2	610.8 565.5 523.4	369.4 339.7	118.0 106.4	263.1 241.7	23.7
104	54.9 49.3	21.4	306.7 284.1 263.0 243.1	118.1	85.8 77.5	120.7 109.5	523.4	312.2	96.1	221.8	20.5 17.5
106 108	49.3 44.1	18.0 14.8	263.0	106.6 96.4	70.1 63.5	109.5 99.5	483.9 446.9	286.5 262.6	87.0 78.8	203.3 186.2	14.7 12.1
110	39.3	11.9	224.5	86.9	57.6	90.5	412.2	240.8	71.5	170.6	9.7
112 114	34.8 30.6	9.2 6.8	224.5 207.0 190.9	78.1 69.8	52.1 47.1	82.4 75.1	379.9 350.2	220.8 202.6	64.7 58.4	156.3 143.4	7.5 5.5
116	26.6	4.8	176.2	62.0	42.3	75.1 68.3	323.0	186.2	52.4	131.7 120.9	3.9
118 120	22.9 19.4	3.1 1.9	162.6 150.3	54.6 47.6	37.8 33.5	62.1 56.1	298.0 275.4	171.1 157.5	46.8 41.5	111.2	1.6
122	16.0	1.1	139.0	41.1	29.4	50.4	254.5	144.9	36.4	102.3 94.0	0.9 0.5
124 126	12.9 10.0	0.6 0.3	128.5 119.0	34.9 29.0	25.6 21.9	45.0 39.8	235.3 217.8	133.2 122.5	31.6 27.0	86.3 78.9	0.3
128	7.4	0.2	110.1	23.5	18.5	34.9	201.3	112.3 102.5	22.8 18.7	78.9 71.8	0.1 0.1
130 132	5.2 3.5	0.1	101.9	18.3 13.7	15.3 12.2	30.3 25.9 21.7	186.1 171.8	93.2	14.9	65.1 58.5	0.0
134	2.2	0.0	86.9 79.9	9.7 8.5	9.4 6.9	21.7 17.7	158.2 145.1	84.2 75.6	11.5 8.4	58.5 52.4	0.0 0.0
136 138	0.7	0.0	73.2	4.1	4.8	14.0	132.5	67.4	5.9	46.5	0.0
140	0.4	0.0	66.7	2.4	3.1	10.7	120.4	59.5	3.8	40.8	0.0

A. 4. 9 Design Flood Hydrograph (1/1,000) (UNIT: A=SQ.KM.RUNOFF=CU.H/S)

(DAM NO.)	(NO.12) A= 443	(NO.13) A= 147	(NO.14) A= 64	(NO. 15) A= 338	(NO. 16) A= 96	(NO.17) A= 68	(NO.18) A= 159	(NO.19) A= 273	(NO. 20) A= 107	(NO.21) A= 151	(NO.22) A= 114
CATCHMENT HOUR 2 4 6 8 10 12 14 16 18 20 22 24 28 30 32 34 38 40 42 44 46 48 50 52 54 66 67 70 76 76 76 80 82 84 86 88 89 90 92 94 96 98 100 102 104 110 1112 114 116 118 120	A= 443 0.4 3.2 14.0 40.0 83.4 133.8 181.0 216.2 232.2 238.4 226.9 237.7 259.6 288.7 350.1 389.9 462.0 536.0 536.0 613.7 718.3 865.4 1045.6 1224.3 1356.5 1394.7 1302.7 1165.2 1017.7 886.9 778.2 687.9 669.3 541.0 482.6 432.5 388.8 233.5 248.0 257.8 233.5 248.0 315.6 285.0 257.8 233.5 248.0 315.6 285.0 257.8 233.5 247.7 158.4 143.4 143.4 129.7 117.2 106.0 886.8 78.7 54.8 853.1 47.7 64.6	0.4 3.5 14.0 32.3 52.0 69.9 82.0 85.4 82.7 76.2 80.9 88.7 109.9 127.9 134.5 181.7 207.3 243.7 300.6 373.0 485.2 500.0 436.0 374.0 374.0 373.0 485.2 265.8 226.9 195.0 166.8 142.2 122.0 105.2 91.0 78.9 68.5 59.4 51.6 44.7 38.8 33.7 29.2 25.3 21.8 18.6 15.7 11.3 0.7 0.4 0.2	A= 64 0.3 3.2 10.6 20.4 20.2 36.6 39.7 38.9 36.3 98.7 152.7 161.1 74.0 98.7 120.5 113.2 227.0 202.2 176.8 143.4 118.3 98.0 152.7 168.4 176.6 176.8 176.6 176.8 176	A= 338 0.4 4.2 18.1 45.2 78.3 109.3 132.9 143.4 142.2 145.2 146.3	A= 96 0.7 6.5 18.0 29.6 47.3 48.6 47.3 48.6 41.4 45.7 80.1 144.5 231.1 268.5 224.4 182.7 115.9 92.9 60.5 47.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	A= 68 0.4 10.47 25.8 31.5 31.9 27.4 28.35 31.9 27.4 28.35 31.7 28.35 31.7 28.35 31.7 28.35 31.7 28.35 31.7 28.35 31.7 28.35 31.7 28.35 31.7 28.35 31.7 28.35 31.7 28.35 31.7 28.35 31.7 28.35 31.7 28.35 31.7 28.35 31.7 28.35 31.7 28.35 31.7 28.35 31.7 31.7 31.7 31.7 31.7 31.7 31.7 31.7	0.4 3.7 15.2 36.5 60.6 82.7 98.6 104.0 101.7 93.8 98.5 108.6 120.7 259.2 300.0 365.3 450.7 596.4 546.8 200.7 259.2 300.0 365.3 450.7 596.4 546.8 200.8 259.2 300.8 300.9	0.2 1.7 7.7 21.6 44.1 69.7 109.2 115.9 115.9 115.9 124.3 112.4 112.4 112.4 112.4 112.4 112.6 113.8 129.6 239.4 239.4 239.4 239.4 239.4 241.1 514.4 664.2 667.9 667.8 2693.6 678.2 557.7 483.8 1287.5 226.5 226.5 226.5 227.7 483.8 1287.5 226.5 227.7 483.8 1287.5 2087.5 20	A= 107 0.4 4.1 14.9 31.0 4.59.8 67.1 63.6 59.5 9.1 71.4 78.9 168.6 201.4 71.4 78.9 168.6 201.6 202.2 311.4 3388.5 388.7 363.2 321.2 266.7 220.8 185.5 48.1 132.2 110.6 92.7 78.3 66.6 56.5 48.1 132.2 110.6 92.7 78.3 66.6 1132.2 110.6 92.7 78.3 66.1 132.2 110.6 92.7 78.3 66.1 132.2 110.6 92.7 78.3 66.1 132.2 110.6 92.7 78.3 66.1 132.2 110.6 92.7 78.3 66.1 132.2 110.6 92.7 78.3 66.1 132.2 110.6 92.7 78.3 66.1 132.2 110.6 92.7 78.3 66.1 132.2 110.6 93.7 93.7 93.7 93.7 93.7 93.7 93.7 93.7	A= 151 0.2 2.2 9.8 24.9 62.2 76.5 83.4 83.4 83.4 83.4 977.3 796.8 96.1 106.7 122.2 145.9 246.3 279.9 346.5 295.8 279.9 346.5 295.8 271.5 192.6 192.6 193.6 193.7 194.6 195.7 196.7	0.9 8.1 23.5 40.0 65.4 67.8 64.4 58.7 57.8 64.4 58.7 75.7 88.1 121.1 148.6 211.7 273.6 328.1 357.4 380.1 359.6 322.2 266.4 209.9 171.0 138.2 113.5 91.7 7 73.0 25.0 25.0 25.0 25.0 25.0 25.0 25.0 25
118	47.7	0.4	0.0	4.2	0.0	0.0	1.2	20.5	0.0	3.6	0.0

A. 4.10 Design Flood Hydrograph (1/10,000)

(UNIT: A=SQ.KM,RUNOFF=CU.M/S)

	to the total contract of	English Control		. "		4.			•		
(DAM NO.)	(NO. 1)	(NO. 2)	(NO. 3)	(NO. 4)	(NO. 5)	(NO. 6)	(NO. 7)	(NO. 8)	(NO. 9)	(NO.10)	(NO.11)
CATCHMENT		A= 364	A=1371	A= 976	A= 585	(NO. 6) A= 798	A=2253	A=1452	A= 614	A=1040	A= 226
HOUR											
						0.5		0.8	0.5	0.6	0.4
: 2	0.4	0.5	0.6 3.7	0.7 6.5	0.4	4.2	1.1 7.0	5.8	. 4,4	4.3	3.9
. 6	3.8 17.7	4.8 20.3	14.5	29.1	3.6 15.7	17.8	27.7	23.4	19.3	17.5	16.6
. 8	48.6	50 4	14 9	81.2	44.5	51.5	27.7 85.6	70.8	54.5	52.8	/1 1
10	93.7	86.5	102.9	162.4	91.4	51.5 109.7	195.5	158.1	111.9 178.0	117.6	70.5
12	142.4	119.9	102.9 189.1 289.1	253.7	145.3 194.2	179.1 247.0	357.1 543.8	277.8	178.0	205.2	97.8
14	93.7 142.4 183.8	145.2	289.1	333.7	194.2	247.0	543.8	410.1 520.8	237.8	117.6 205.2 301.3 381.1 434.8 456.9 456.7 453.7 465.1 494.4	70.5 97.8 118.4 127.0 125.4 119.6
16	210.7	155.7 153.7	381.5	389.7	230.0	299.0 325.2	714.2	260.8	281.6 300.1 299.3 292.4 291.2 305.8	361.1	127.0
18 20	219.2 214.2	155.7	451.5	411.2	245.1	323.2	841.8 908.4 927.2	597.0 629.2 630.2	200.1	454.0	119 4
55		142.1	500 4	395.5	238.9	330.4 324.5	927.2	630.2	292.4	456.7	· 113.A
24	209.2	147.6	500.4	395.5 395.8 417.8	237.9	321.5	926.3	626.7	291.2	453.7	120.4
26	8.555	1.62.0	507.8	417.8	249.8	335.1	940.9	641.4	305.8	465.1	132.1
28 30	245.6	179.1 198.2 222.5	489.0 500.4 500.4 507.8 533.3 579.3 638.5	459.1 507.2 564.8	237.9 249.8 273.5	363.5	926.3 940.9 989.3 1077.2 1192.4 1347.4 1551.3 1810.4	680.7	334.9 370.3 417.5 486.0	494.4	146.1
30	271.8	198.2	579.3	507.2	301.7	400.3	10//.2	748.0	3/0.3	343.7 405.8	161.6 181.8
32	3/1.0	222.5	717.5	. 204.0	333.9	443.9 503.8	13/7 4	965.0	788.0	\$43.7 605.8 689.5	208.5
34 36	389.4	288 9	804.1	640.1 736.7 858.8	636.3	579.7	1551.3	1101.1	575.1	804.4	242.8
38	450.9	338.3	924.3	858.8	508.0	676.1	1810.4	1290.5	673.4	943.4	285.4 340.4
40	534.3	408.2	1078.5	1012.8	598.3	794.1	2122.2	1508.2	778.5	1101.4	
42	207.5 209.2 222.8 245.6 271.8 302.7 341.8 389.4 450.9 534.3	252.6 288.9 338.3 408.2 509.8	638.5 713.5 806.1 924.3 1078.5 1275.7	1223.4	721.0	950.4	2490.0	1769.3	918.7	1291.6	421.2
44	816.6	0.39 70	1535.1	1517.3	888.1	1158.0	2958.2	2106.3	1116.0	1537.9 1861.6 2207.8	526.1 630.8
46 48	1160 8	769.2 866.3	22/0 /	2158 3	1275 /	1414.0	3202.1 1213.3	3026 8	1581.8	2207.8	709.4
50	816.6 998.9 1160.8 1266.9 1294.2 1244.8 1135.4 .993.2 855.3 741.7	911 4	1535, 1 1867, 6 2240, 4 2603, 2 2871, 2 3001, 2 2972, 2 2808, 2 2558, 2 2280, 0 2021, 5 1798, 7 1609, 3 1445, 0 1301, 8	858.8 1012.8 1223.4 1512.3 1845.7 2158.3 2375.3 2452.8 2385.7 2199.0 1943.1 1681.8 1461.3 1280.1	301.7 335.9 380.0 436.3 508.0 598.3 721.0 888.1 1084.6 1275.4 1412.6 1470.9 1442.1 1339.9 1192.5 1036.8	321.5 335.1 363.5 400.3 445.9 503.8 579.2 676.1 794.1 1950.4 1158.0 1414.0 1472.7 1872.0 1975.5 1962.7 1849.5 1462.7 1276.3 1462.7	1810.4 2122.2 2490.0 2958.2 3562.7 4243.3 4904.5 5385.4 5608.1 5537.1 5217.1 4743.8	626.7 641.4 680.7 748.0 832.2 945.9 1101.1 1290.5 1508.2 1769.3 2106.3 2549.1 3024.8 3458.9 3744.2	486.0 575.1 673.4 778.5 918.7 1116.0 1351.9 1581.8 1747.1 1816.2	2519.7	745.8
SS	1294.2	911.4 893.9 826.5 724.4	2871.2	2452.8	1470.9	1975.5	5385.4	3744.2	1816.2	2721.7 2777.1	731.2
54	1244.8	826.5	3001.2	2385.7	1442.1	1962.7	5608.1	3830.7	111111	2777.1	676.0
56	1135.4	724.4	2972.2	2199.0	1339.9	1849.5	5537.1	3721.4 3447.5 3093.8	1652.7	2691.4 2487.5 2228.3	592.4
58	993.2	613.2 522.5 449.1 388.4 336.5 290.1 251.3 218.8 191.1	2808.2	1943.1	1192.5	1666.3	5217.1	3447.5	1471.1 1279.3	2487.3	501.5 427.4
60	8>>.3	522.5	2228.2	1681.8	1036.8	1402.7	4743.0	2729.1	1113 8	1984 0	367.4
62 64	6/8 7	398 /	2021 5	1280 1	902.5 790.9	1120 9		2/11 /	976.3	1734.3	317.7
66	648.7 569.5 500.9 441.2	336.5	1798.7	1126.8	697.9	992.0	3743.3 3330.3 2979.9 2675.2 2410.0 2182.7 1986.2 1815.9 1664.1 1527.1 1402.4	2140.7 1910.5 1710.6 1537.0 1388.7 1260.9	1113.8 976.3 861.6	1964.0 1734.3 1539.6 1373.6	275.3
68	500.9	290.1	1609.3	995.0	617.5	992.0 880.1	2979.9	1910.5	762.4 675.8 601.8	1373.6	237.4
70	441.2	251.3	1445.0	879.7	547.2 487.2	782,9	2675.2	1710.6	675.8	1229.2	205.6
72	390.3 346.9	218.8	1301.8	781.2	487.2	499.6	2410.0	1537.0	538.4	1104.2 997.2	179.0 156.4
74 78	346.9 308.8	191.1	11/9.2	697.0 623.4	435.8	628.2	1004.7	1260.7	483.1	905.1	137.0
78	275 5	1/4 0	981 7	558 4	351.3	510.9	1815 9		434.1	823.9	120.2
80	246.4	167.5 146.9 129.1	900.1	558.4 501.2 450.8 406.1	316.2	566.0 510.9 461.8 418.0 379.0	1664.1	1048.0 957.2 874.9	390.7	751.3	105.7
82	220.8	113.4 99.5 87.3 76.6 67.3	826.4	450.8	285.0	418.0	1527.1	957.2	352.2	685.6	92.8
84	198.1	99.5	759.5	406.1	257.4	379.0	1402.4	874.9	318.1	626.3	81.4
86	177.9	87.3	698.2	366.4	232.9	344.1 313.0	1288.6 1185.0	800.6 733.5 673.1	287.8 260.6	572.8 524.5	71.5 62.7
88 90	124.0	/0.0 47 3	- 042.3 - 501 X	298.3	101 1	285.0	1090.9	673.1	236.1	481.1	55.1
92	308.8 275.5 246.4 220.8 198.1 177.9 159.6 143.0	59.1	5/5/4	268.7	435.8 391.0 351.3 316.2 285.0 257.4 232.9 211.0 191.1 173.0 156.3 141.1	250 6	1005.8	618.5	213.7	441.7	48.4
94	114.3	52.1	503.8	241 7	156.3	236.4	928.4	568.9	193.2	406.1	42.6
96	114.3 102.2	45.8	465.9	217.2	141.1	215.0	858.2	523.7 482.2	174.4 157.3	373.6	37.4
98	91.5 82.0	45.8 40.1	431.3	195.1	127.2 114.7	259.6 236.4 215.0 195.3 177.1	794.0	482.2	157.3	343.7 316.2	32.8 28.5
100	82.0	34.9 30.1 25.7 21.5	399.5	175.4	114.7	1//.1	734.9 680.3	444.0 408.5	141.8	- 290.5	24.6
102 104	73.7 66.2	20.1	3/U.1	1/2 5	103.3	160.5 145.6	629.6	375.3	127.9 115.6 104.6	266.6	21.0
106	59.5	21.5	317.3	128.6	93.4 84.6	132.0	582 2	375.3 344.4	104.6	244.4	17.6
108	53.2	17.7 14.2 11.0	1301.8 1179.2 1073.4 981.7 980.1 826.4 759.5 698.2 642.3 591.6 545	217.2 195.1 175.4 157.9 142.5 128.6 116.2	76.6	132.0 120.0	537.7 495.9 457.1 421.4	315.7	94.7	223.9	14.4
110	47.4	14.2	270.9	104.7	69.5	109.1	495.9	289.6	85.9 77.7	205.2	11.6
112	42.0	11.0	249.8	94.1	62.9	99.4	457.1	289.6 265.6 243.8	77.7 70.1	188.0 172.5	8.9 6.6
114	36.9	8.1	250.4	84.1 74.6	56.7	90.6 82.3	388.7	224.1	62.9	158.4	4.6
116 118	32.0 27.5	5.6 3.7	104 3	45.7	45.5	74.8	358.8	205.9	56.1	145.5	3.0
120	23.2	2.3	181.5	65.7 57.2 49.2 41.7	51.0 45.5 40.3 35.3 30.7 26.3	74.8 67.5 60.7	358.8 331.6	205.9 189.4	49.7	133.8	1.9
122	19.2	1.3	167.9	49.2	35.3	60.7	306.4	174.3	43.5 37.7	123.0	1.1
124	15.4	0.7	155.3	41.7	30.7	54.1	283.4	160.3 147.3	37.7	113.0	0.6
126	11.9	0.4	143.8	34.6 27.9	26.3	47.8	262.2 242.3	147.3 135.0	32.2 27.1	103.7 94.8	0.3
128 130	8.8 6.2	0.2	133.1 123.0	27.9	22.1	41.9	223.9	123.2	22.3	86.3	1.1 0.6 0.3 0.2 0.1
132	4.1	0.1	113.8	16.3	18.2 14.5	36.3 31.0	206.8	112.0	17.8	78.1	0.0
134	3.6	0.0	113.8 105.0	11.6	11.1	25.9	190.3	101.0	13.6	70.2	0.0
136	1.5	0.0	96.5	7.8	8.2 5.7	21.1	174.5	90.6	10.0	8.56	0.0
138	0.8	0.0	88.3	4.9	5.7	16.7	159.3	80.7 71.2	7.0 4.6	55.6 48.8	0.0 0.0
140	0.4	0.0	80.5	2.9	3.7	12.7	144.6	(1.6	4.0	40.0	

A. 4. 10 Design Flood Hydrograph (1/10,000)

CUNIT: A=SQ.KM.RUNOFF=CU.H/S)

(DAM NO.) CATCHMENT HOUR	(NO.12) A= 443	(NO.13) A= 147	(HO.14) A= 64	(NO.15) A= 338	(NO.16) A= 96	(NO.17) A= 68	(NO.18) A= 159	(NO.19) A= 273	(NO.20) A= 107	(NO.21) A= 151	(NO.22) A= 114
2	0,4 3,8	0.4 4.1	0.4 3.8	0.5 5.0	0.8 7.7	0.4	0.5	0.2	0.5 4.9 17.7	0.3	1.0 9.7
6 8	16.6 47.6 99.1	16.6 38.3 61.8	12.6 24.2 34.7	21.5 53.7 93.1	21.4 35.2 48.1	12.4 22.2 30.7	18.1 43.4 72.1	9.1 25.7 52.4	36.8 55.2	11.6 29.6 52.3	28.0 47.6
10 12	159.1	83.1	43.6 47.2	129.9	56.3	37.5	98.3	82.9	71.1	74.0 90.9	65.3 77.7
14 16	215.2 257.0	97.5 101.5	46.2	158.0 170.5	57.7 54.4	39.4 37.9	117.2 123.7	110.0 129.8 137.8	79.8 80.1	99.2	80.6 76.5
18 20	276.0 277.3	98.4 92.8	43.1 40.3	169.0 161.5	49.2 45.9	34.9 32.5 33.7	120.9 114.7	136.9	75.6 70.8	99.1	69.8 65.1
22 24	271.5 269.8	90.5 96.2	40.8 45.0	156.4	49,2 54,3 61,0	37.5	111.5 117.4	133.6 133.2	70.3 76.6	91.9 94.7	68.7 76.1
26 28	283.7 314.5 360.9	106.2 118.9	45.0 49.9 55.5 65.9 82.3	162.0 177.4 196.2 217.1	61.0 66.4	41.6 45.6	131.7 153.6	140.1 153.7 170.1	70.3 76.8 85.0 96.0 114.6 141.1 165.1 185.5 206.9	94.7 103.3 115.3	76.7 76.1 85.0 93.0 109.1 137.2 162.2 182.3 208.8 258.0 330.2
30 32	360.9 424.8 502.4	138.7 169.0	85.9 82.3	245.1	66. 4 75. 7 87. 2 103. 7 122. 3 144. 9 182. 6 237. 7 241. 7 314. 2 322. 1 301. 7 268. 6 218. 7 171. 2	51.4 59.2	153.6 182.2 216.0	191.9	114.6 141.1	132.7 159.2 190.6 219.8	109.1 137.2
34 36	502.4 584.1 664.7	201.1 228.8	96.4 108.3 121.5	285.2 336.8	103.7 122.3	69.4	251.7	223.9 265.3	165.1 185.5	190.6 219.8	162.2 182.3
38 40	664.7 751.6	228.8 256.0 297.3 363.5	144.6	393.8 464.0	144.9 182.6	96.7 120.9	284.0 316.1 363.2	310.2 358.4	244,0	247.5	208.8 258.0
1.5 4.4	751.6 872.5 1044.5	448.6	184.2 224.7	568.8 707.6	237.2 281.7	155.3 188.6	439.8 540.5	423.1 514.8	304.0 373.7	339.5 417.3	330.2 394.0 440.0
46 48	1256.7 1467.5	526.7 580.6	255.3 271.3	847.9 955.0	314.2 322.1	96.7 120.9 155.3 188.6 212.5 222.6 213.6 193.1 162.9	637.7 707.4	253.3 310.2 358.4 423.1 514.8 623.3 728.3	430.1 464.4	498.2 561.8	440.0 454.4
50 52	1623.2 1693.5	597.7 573.4	265.6 243.8	1006.3	301.7 268.6	213.6	734.5 711.6		464.2 433.6	594.1	429.6 384.7
54 56	1666.7 1556.5	520.8 446.7	211.1 171.2	989.8 917.8 807.2	218.7	162.9 129.5	851.7 565.3	832.1 812.9 752.9	383.4	587.5 547.9 485.0	318.1 250 A
58 60	1392.2	374.2	141.2	807.2 685.3 584.2	138.7 111.2	106.2	476.0 405.0	668.5 580.1	318.4 263.6 221.5	414.1 353.5	204.2 165.0 135.6
62 64	1060.0	271.1 233.0	117.1 97.7 81.7	502.9	የሰ የ	86.7 71.7 58.9	347.0	504.8 442.3	186.4 157.9 132.1	305.1 264.8	135.6 109.6
66	822.3	199.3	67.2	502.9 435.4 377.8 326.5 283.2 247.0	72.4 57.1 45.5	47,4 38.7	299.3 257.9	390.0	132.1	230.5	87.2
68 70	728.5 647.0	170.0 145.8	67.2 55.7 46.4	283.2	36.4	31.7	221.2 190.7	345.0 305.5	110.7 93.6	199.9 174.0 152.2	56.7
72 74	647.0 577.1 517.3 465.1 418.7	145.8 125.7 108.8	38.8 32.5 27.2 22.7 19.0	247.0 216.0 189.6	29.1 23.2	26.0 21.3	165.3 143.8	271.8 243.0 217.8 195.5 175.8 158.4	93.6 79.4 67.5 57.4	133.5 117.5	56.7 45.8 37.0 29.7 23.7 18.7
76 78	465.1 418.7	94.3 81.9	27.2	166.7	18.4 14.4	21.3 17.5 14.3	125.3 109.5	217.8 195.5	48,8	103.6	29.7 23.7
80 82	240.7	71.1 61.7	19.0 15.8	146.7 129.1	11.0 8.1	11.6 9.3	95.6 83.5	175.8 158.4	41.5 35.2	91.5 80.9	14.4
84 86	308.4 279.4	53.5 46.4	10.7	113.5 99.8	5.6 3.7	7.3 5.6	72.9 63.6	129.2	29.9 25.3	71.4 63.0	10.6 7.5
88 90	253.5 230.2	40.2 34.9	8.6 6.7	87.7 77.1	2.3 1.3	4.1 2.8	55.5 48.4	116.9 105.7	25.3 21.3 17.7	55.5 49.0	5.0 3.1
92 94	209.0 189.5	30.2 26.0	5.1 3.7	67.9 59.9	0.7 0.4	1.8 1.1	42.3 36.9	95.6 86.2	14.6 11.7	43.2 38.2	1.8 1.0
96 98	189.5 171.6 155.2	22.2 18.7	2.5	52.7 46.4	0.2	0.6 0.3	32.0 27.5	77.7 70.0	9.1 6.8	33.8	1.0 0.5 0.3 0.1
100 102	155.2 140.3 126.8	15.6 12.7	1.0 0.5	40.5 35.1	0.0	0.2	23.4 19.7	63.1 56.8	4.9 3.3	29.8 26.3 23.0	0.1
104 106	114.7 103.9	10.0 7.7	0.3	30.1 25.5	0.0	0.0	16.3	51.3 46.4	2.1 1.2	19.9 17.1	0.0 0.0 0.0 0.0
108 110	94.2 85.5	5.6 3.8	0.1 0.0	21.2 17.2	0.0	0.0	13.2 10.3 7.7	42.0 38.0	0.7 0.4	14.5 12.1	0.0
112	77.6 70.3	2.5	0.0	13.6 10.3	0.0	0.0	7.7 5.5 3.7	34.3	0.2 0.1	9.8 7.8	0.0
116	63.5	8.0	0.0	7.4 5.0	0.0	0.0	2.3	27.6	0.0	5.9 4.3	0.0
118 120	57.0 50.8	0.5	0.0	3.2	0.0 0.0	0.0	0.8	34.3 30.9 27.6 24.5 21.6 18.8 16.2 13.7	0.0	2.9	0.0
122 124	44.9 39.4	0.1 0.1	0.0	1.9	0.0	0.0 0.0	0.2	16.2	0.0	1.1	0.0
126 128	34.1 29.2	0.0	0.0	0.6 0.3	0.0	0.0	0.1 0.1	11.4	0.0	0.3	0.0
130 132	24.6 20.2	0.0	0.0	0.2 0.1	0.0	0.0 0.0	0.0	9.2 7.2	0.0	0.2	0.0
134 136	16.2 12.5	0.0 0.0	0.0	0.0 0.0	0.0	0.0	0.0	5.4 3.9	0.0 0.0	0.0	0.0
138 140	9.2 6.4	0.0 0.0	0.0	0.0 0.0	0.0 0.0	0.0 0.0	0.0 0.0	2.6 1.6	0.0	0.0 0.0	0.0

APPENDIX-B. LAND USE AND SOIL

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B.1 LAND USE

1) INTRODUCTION

Land use information in the area is very important for development of crop diversification planning which is in turn needed for estimation of irrigation water demand and also the designation of irrigation system. This is because different land use type such as paddy, upland crop orchard require different irrigation method.

2) STUDY METHODOLOGY

A) Data Collection and Review

Information on land use was collected from, various government agencies concerned both in Bangkok and other provinces in the study area as follows

- 1) Land use Planning Division. Department of Land Development
 - Land Use Maps at scale 1:100,000 of Chon Buri, Chachoengsao Prachin Buri and Nakhon Nayok
- 2) Provincial Agricultural Extension Offices of Chon Buri, Chachoengsao Prachin Buri and Nakhon Nayok
 - Agricultural data of each province
- 3) Provincial Commercial Offices of Chon Buri, Chachoengsao, Prachin Bun and Nakhon Nayok
 - Annual Reports

These mentioned maps and reports are reviewed and extracted to obtain specific information required for study.

B) Field Survey

The field survey carried out during study period was done in parallel with the soil every in order to:

- make supplementary land use survey with particular emphases on changes of land use patterns.
- collect land use data from provincial agencies and interview with government officers, private sectors and farmers to obtain information necessary for study.

3) RESULT OF STUDY

A) General Land Use Feature

General land use of Bang Pakong river besin is clearly defined by its topography. The low flat land in the western is entirely devoted to paddy cultivation with some orchards along the river banks. The upland and mountainous areas in the eastern are mostly under several upland crops, orchard plantation and forest. In total study area of approximately 1,766,000 ha, the agricultural land comprises 993,760 ha or about 56 percent. Amount this, paddy, upland crop, orchard and vegetables with others share 467,290 ha (27 percent), 391,060 ha (22 percent), 102,000 ha (6 percent) and 24,410 ha (1 percent) respectively. The other 772,240 ha (44 percent) is devoted to forest, mountainous and miscellaneous areas. The agriculture is mostly still under rainfed.

Paddy cultivation in the area is largely limited only in wet season. Dry season cropping after rice is rare. Prachin Buri occupies the largest area whereas Chon Buri has smallest.

Total upland crop area of the basin is 391,060 ha or about 22 percent with the largest in Prachin Buri and smallest in Nakhon Nayok. Dominant crop is cassava grown widespreadly in every province. Maize is another economic crop largely cultivated in Amphoe Wang Nam Yen and Sa Kaew of Prachin Buri province.

Orchard plantations totalling about 102,000 ha or approximately 6 percent include mainly mango, coconut and other mixed orchards. Prachin Buri and Nakhon Nayok have the largest and smallest planted arear respectively. Chachoengsao is now popular in mango plantation while Prachin Buri is well known in sweet bamboo and durian.

For vegetables which are grown in very small area of about only one percent can be recognized only where there is adequate water available.

Land use maps of Chan Buri, Chachoengsao, Prachin Buri and Nakhon Nayok were shown in Figures B1 to B4.

B) Land Use Area by Amphoc-wise

Area coverages of main land use categories by Amphoc-wise of the four provinces were presented in Tables B-1. The main categories are agricultural land and other land use. The agricultural land comprises paddy, upland crop, orchard and vegetables.

C) Land Use Area by Sub-basin

The study area was analyized and divided into 8 sub-basins as follows:

- a) Lower Bang Pakong (LBP)
- b) Khlong Thalat (KTL)
- c) Upper Bang Pakong (UBP)
- d) Mac Nam Nakhon Nayok (MNN)
- e) Middle Phra Prong (MPP)
- f) Mac Nam Hanuman (MNH)
- g) Khlong Phra Sathung (KPS)
- h) Upper Phra Prong (UPP)

The area coverages of land use by each sub-basin were summarized in Table B-2 to 6.

D) Preliminary Land Use Patterns Under Project Implementation

Generally, factors to be considered when making land use planning namely soil suitability, topography, water source, market, farmers traditions, etc. In this study area major crops are paddy in lowland and cassava with maize on upland. Cassava is facing with marketing problem. At the same time soybean, mungbean and fruit orchards are extensively promoted by government due to market demand is high. Thus cassava area should considered to be reduced or freezed and replaced by other promissing crops as mentioned above. Under project implementation the dry season cropping area in the service area especially in paddy land will be certainly considerable increased. Suitable crops recommended for dry season should be soybean, mungbean and groundnut better than second rice due to water is limited. Preliminary land use planning with project is thus designated as follows:

paddy land wet season: paddy

dry season: soybean, mungbean, ground and some

second rice

upland area wet season: maize

dry season: soybean, mungbean, groundnut

orchard: mainly mango, palmelo and durian

vegetables: grown in both wet and dry seasons

orchard extension: some paddy land should be changed to mango

plantation.

TABLE B-1 LAND USE OF PROJECT AREA BY AMPHOE

			Agaila	ultural La	e de la companya de		: ha
Province / Amphoe	Project		Agile		Other		
	nrea	Paddy	Upland	orchard	Vegetable and other	sub-tota	land
		11111					
CHON BURT	206,520	48,310	84,160	25,700	19,450	177,620	28,900
Λ. Muang	10,400	3,340	1,570	1,550	340	6,800	3,600
A. Phanat Nikhon	72,710	24,280	18,410	5,440	14,030	62,160	10,500
A. Ban Bung	58,320	7,160	34,670	7,630	2,070	51,530	6,790
A. Phan Thong	17,590	11,290	1,580	1,090	1,550	15,510	2,080
King A. Bo Thong	42,380	2,190	24,090	8,760	1,460	36,500	5,880
A. Nong Yai	5,120	50	3,840	1,230	-	\$,120	i
CHACHOENGSAO	444,490	91,210	75,030	19,500	750	186,490	258,000
A. Muang	6,760	5,110		780	120	6,010	750
A. Bang Khla	25,650	16,460	500	7,730	250	24,940	710
A. Ban Pho	14,770	12,550	-	950		13,500	1,270
A. Bang Pakong	\$,450	2,680	-	440	30	3,150	2,300
A. Phanom Sarakham	112,200	21,850	22,880	1,740	120	46,590	65,610
A. Sanam Chai Khet	236,290	6,050	41,350	3,030	- "	50,430	185,860
King A. Plaeng Yoo	23,560	8,470	10,300	3,880	230	22,880	680
King A. Ratchasan	19,810	18,040	7	950		18,990	820
			-				
PRACHIN BURI	846,200	254,570	219,060	38,770	2,920	515,320	330,880
A. Huang	42,860	21,700	650	9,700	940	32,990	9,870
A. Ban Sang	29,440	25,710	_	840	30	26,580	2,860
A. Khok Pip	13,140	9,130	1,610	360	90	11,190	1,950
A. Si Maha Phot	31,820	16,580	6,320	3,050	170	26,120	5,700
A. Prachanta Kham	77,280	18,090	150	3,050	80	21,370	55,910
A. Kabin Buri	119,500	43,490	18,890	2,800	80	65,260	54,240
A. Nadi	111,180	15,010	17,330	9,700	30	42,070	69,110
A. Sa Kaew	206,550	67,070	66,310	4,830	400	138,610	67,940
A. Wang Nam Yen	. 69,200	4,620	56,100	1,450	80	62,250	6,950
A. Natthana Nakhon	104,050	30,960	15,480	2,500	1,000	49,940	54,110
King A. Khlong Hat	41,180	2,210	36,220	490	20	38,940	2,240
						 	
NAKHON NAYOK	149,590	80,400	1,210	7,590	1,290	90,490	59,100
A. Maung	66,030	33,490	140	3,280	290	37,200	28,830
A. Ban Na	22,270	14,890	750	2,050	930	18,620	3,650
A. Ongkharak	15,550	13,810	300		10	15,180	370
A. Pak Phli .	45,470	18,120	20	1,200	60	19,490	26,250
			<u> </u>	<u> </u>			
OTHER PROVINCES	119,200	1,800.	11,600	10,440		23,840	95,360
TOTAL,	1,766,000	476,290	391,060	•	24,410	993,760	772,240
	i	l	i '		i	I .	

TABLE B-2 LAND USE BY IRRIGATION BLOCK

T			n:1 - 1 - 1				
Irrigation Block		Paddy (ha)	Upland (ha)	Orchard (ha)	Vegetable & BTC (ha)	Sub-total (ha)	Other Land Area (ha)
l Lower Bang Pakor	<u>18</u>						
- LBP 1	3,500	•	-	160	_	160	3,340
- LBP 2	11,900	4,840		1,020	240	6,100	5,800
- LDP 3	52,600	43,890	1,440	5,390	1,390	52,110	490
- LBP (14,200	8,390	•	1,280	2,880	12,550	1,650
- LBP 5	27,900	10,480	11,870	1,490	3,860	27,700	200
- LBP 6	8,000	5,960	470	830	1	7,260	740
- LBP 7	50,100	3,970	36,440	5,110	~	45,520	4,580
- LBP 8	18,200	9,950	6,620	1,160	-	17,730	470
- LBP 9	8,800	2,620	5,460	-	-	8,080	720
- LBP 10	8,500	2,530	5,250	140	-	7,920	580
- GBP 11	18,400	640	12,770	1,020	-	14,430	3,970
- 1.8P 12	34,400	140	24,770	230	-	25,140	9,260
- LBP 13	5,600	2,780	1,270	-	-	4,050	1,550
- LBP 14	20,100	1,250	17,130	<u>.</u>	•	18,380	1,720
- LBP 15	6,500	1,850	4,180	<u>-</u>	-	6,030	470
- LBP 16	19,900	2,200	16,080		· -	18,280	1,620
- CBP 17	2,000	1,190	360	_		1,550	450
Sub-total	310,600	102,680	144,110	17,830	8,370	272,990	37,610

		TABL	. <u>Б</u> В-3	LAND	USE	BY INKIGAT	LION BE	<u>ock</u>
	Tueldakian mlaak			1	lgricultui	ral Land		Other ha
	Irrigation Block	Project Area	Paddy (ha)	Upland (ha)	Orchard (ha)	Vegetable & RTC (ha)	Sub-total (ha)	
	2 Khlong Tha bat							
-	- RTL 1	3,200	1,370	1,380	60	80	2,890	310
	- KTL 2	8,600	130	7,510	140	80	7,860	740
	- KT6 3	6,900		6,270	-	_ 12 12 1	6,270	630
	- RTL 4	13,700	190	10,080		•	10,870	2,830
	- KTL 5	61,700	760	11,620	500	_	12,880	48,820
	- KTL 6	18,100	180	8,230	-	-	8,410	9,690
	- RTG 7	39,500	250	9,870	_	<u>_</u>	10,120	29,380
	- KTL 8	39,100	380	3,640	_	-	4,020	35,080
	- KTL 9	58,500	130	2,450	-	-	2,580	55,920
	Sub-total	249,300	3,990	61,050	700	160	65,900	183,400
	3 Upper Bang Pakong							
	- UBP 1	108,000	91,940	4,670	4,910	3,900	105,420	580
	- UBP 2	44,600	17,720	330	25,330	620	44,000	600
	- UBP 3	75,000	31,690	31,750	3,480	2,220	72,140	2,860
	- UBP 4	39,400	23,030	380	8,160	1,820	33,390	6,010
	- UBP 5	10,700	_	-	-	-	-	10,700
	Sub-total	275,700	167,380	37,130	41,880	8,560	254,950	20,750

TABLE B-4 LAND USE BY IRRIGATION BLOCK

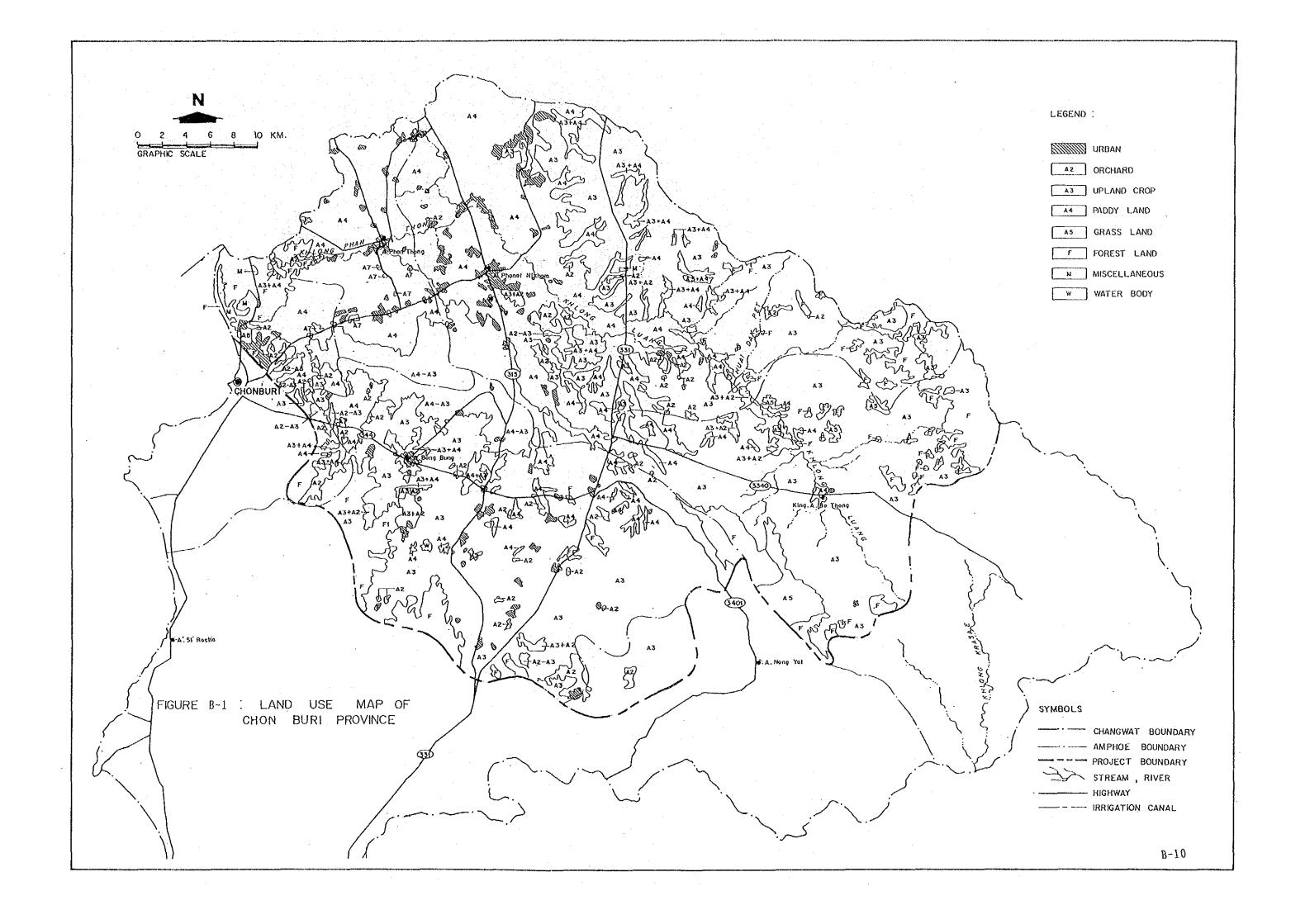
Irrigation Block	Project Area		1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	Agricult	ıral Land		Other Land
fittering proce	(ha)	Paddy (ha)	Upland (ba)	Orchard (ha)	Vegetable & RTC (ha)	Sub-total (ha)	Area (ha)
4 Hae Naw Hakhon Way	rok						
- NKK 1	49,800	34,280	•	800	.	35,080	14,720
- BNN 2	36,900	26,030	-	2,540	2,080	30,650	5,250
- 8ии 3	34,500	17,940	1,450	1,660	1,300	22,350	12,150
- BRH 4	11,400	<u>-</u>	· -	-		-	11,400
- KNN 5	45,600	3,430	1,100	7,110	-	11,640	33,960
- RXX 6	15,100	-	-	,	-	-	15,100
Sub-total	193,300	81,680	2,550	12,110	3,380	99,720	93,580
5 Middle Phra Prong		·					
- Kbb 1	97,000	19,520	21,820	-	-	41,340	55,660
Sub-total	97,000	19,520	21,820	- '	· •	41,340	55,660

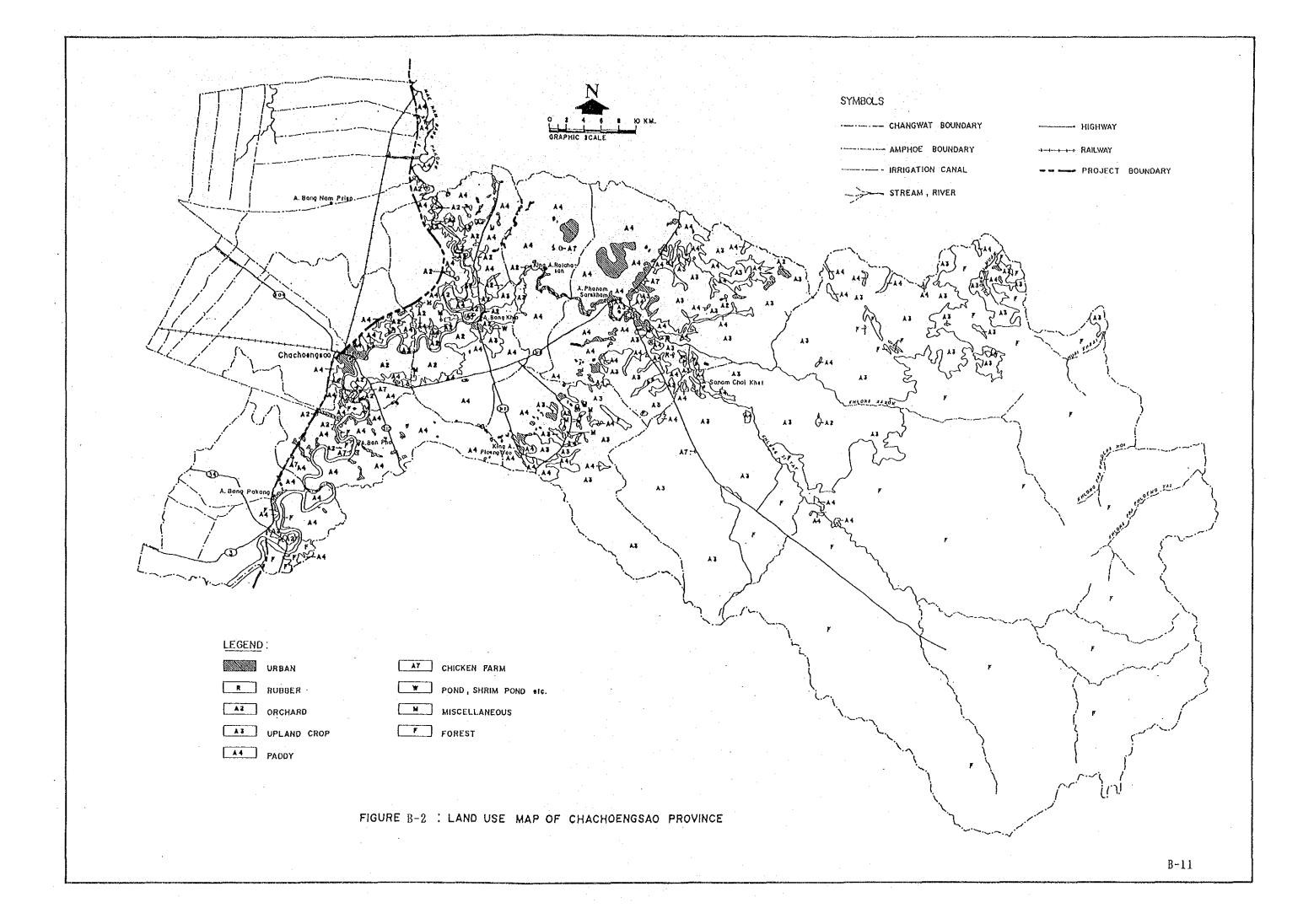
TABLE B-5 LAND USE BY IRRIGATION BLOCK

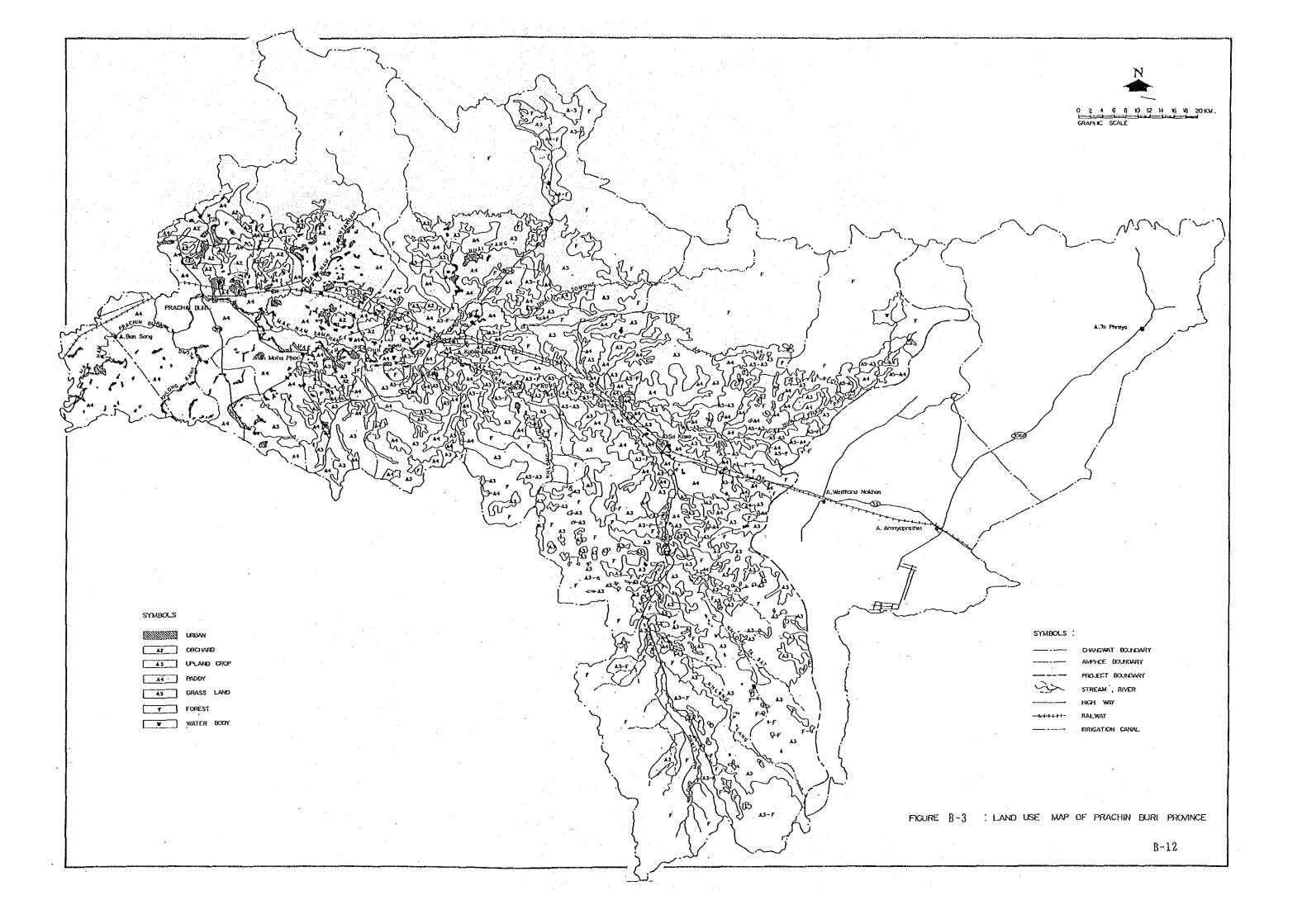
		Agricultural Land					
Irrigation Block Pro	Project Area	Paddy (ha)	Upland (ha)	Orchard (ha)	Vegetable & RTC (ha)	Sub-total (ha)	Other Land Area (ba)
6 Nae Nam Hanuman					,		
- NAN 1	91,700	20,640	18,510	15,470	80	51,700	37,000
- KHK 2	15,900	•	-	•		•	15,900
- AHX 3	27,300	•	-	••	• 1. 181	· · ·	27,300
- NHN 4	17,400	3,880	390	-	<u>-</u>	4,270	13,130
- XHX 2	5,800	-	•	-	-	-	6,800
- NAN 6	9,600	-	5,650	-	• • • • • • • • • • • • • • • • • • •	5,650	3,950
- HBH 7	23,200	<u>-</u>	•	-	-	-	23,200
- NHN 8	6,400	-	•	-	-	•	6,400
- KBR 3	14,700	_	-	•	-	- -	14,700
Sub-total	213,000	24,520	24,550	15,470	80	64,620	148,380

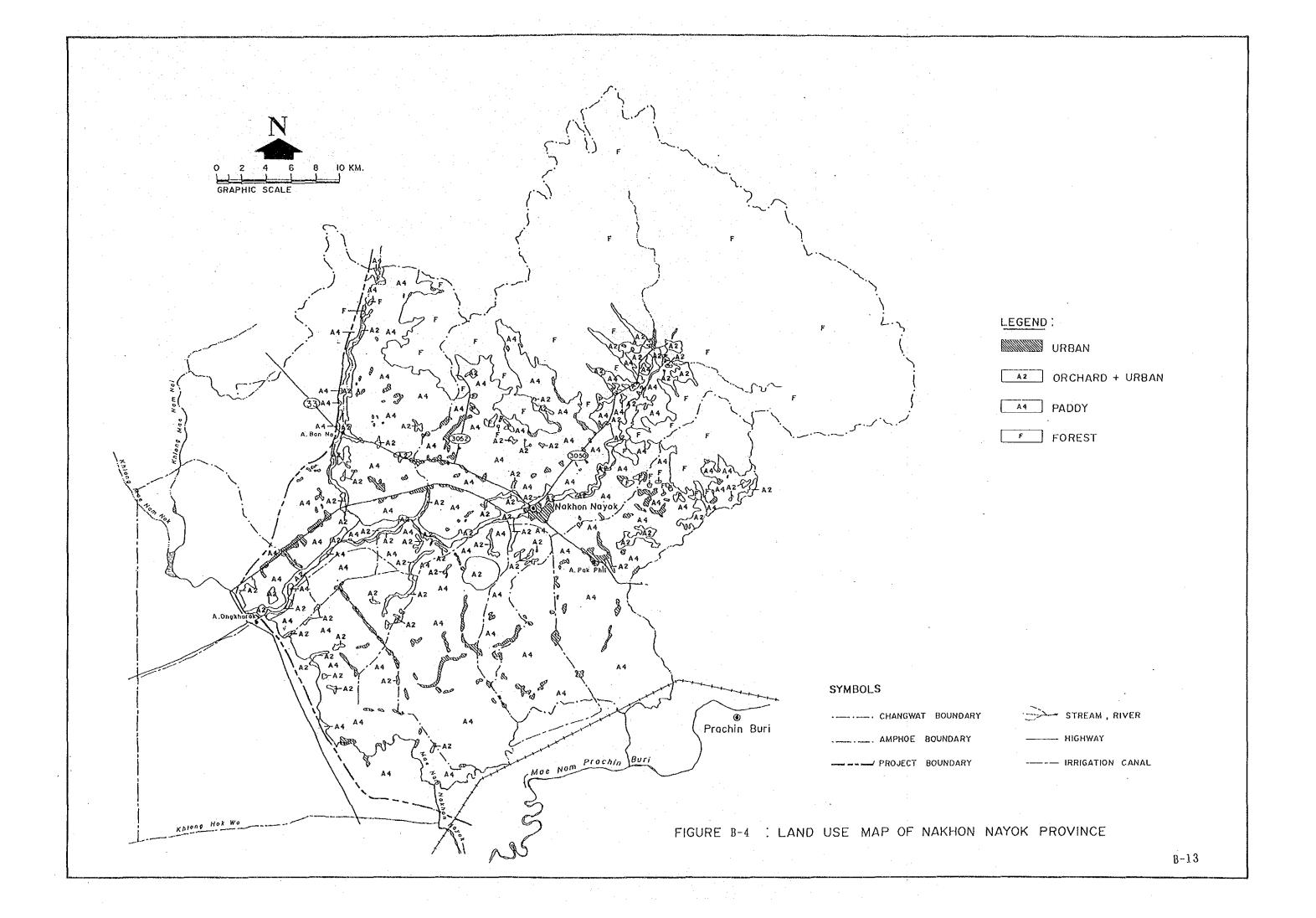
TOTAL B-6 LAND USE BY IRRIGATION BLOCK

Irrigation Block	Project Area	Agricultural Land					Other tool
		Paddy (ha)	Upland (ba)	Orchard (ha)	Vegetable & BTC (ha)	Sub-total (ha)	Other Land Area (ha)
7 Khlong Phra Sathu	ng					-	
- KPS 1	39,000	16,130	11,930	3,860	530	32,450	6,550
- KPS 2	80,100	9,240	7,040	1,990	1,300	19,570	60,530
- RPS 3	83,800	2,620	29,150	1,160	110	33,040	50,760
- KPS 4	61,400	1,970	21,850	1,160	110	25,090	36,310
Sub-total	264,300	29,960	69,970	8,170	2,050	110,150	154,150
8 Upper Phra Prong							
- UPP 1	58,800	25,040	22,840	3,850	520	52,250	6,550
- UPP 2	77,400	21,520	7,040	1,990	1,290	31,840	45,560
- UPP 3	26,600		-	-	<u>.</u>		26,600
Sub-total	162,800	46,560	29,880	5,840	1,810	84,090	78,710









B.2. SOIL (ALLOVER BASIN STUDY)

1. INTRODUCTION

Information on soils is very necessary for agricultural water resources development project. Soil characteristics and their suitability are certainly a guidance for land use planning, irrigation water demand estimation, irrigation system designing. The study on soils for this project is thus to provide such data for crop-diversification planning and for irrigation development as well. These data will be obtained through soil survey, soil analysis and soil suitability interpretation.

2. STUDY METHODOLOGY

A. Data Collection and Review

Soils in this area have been studied by the Department of Land Development and other agencies. As the results, following maps and references were collected and reviewed to obtain specific information required.

- A) Soil Survey Division, Department of Land Development (DLD)
 - Detailed Reconnaissance Soil Maps at scale 1:100,000 of Chon Buri, Chachaengsao, Prachin Buri and Nakhon Nayok.
 - Soil Survey Reports of the four mentioned provinces
 - Land Use Planning Reports of Chon Buri, Chachoengsao and Prachin Buri
- B) Nakhon Nayok Agricultural Extension Office (DOAE)
 - Report on Acid Sulfate Soil Improvement
- C) Prachin Buri Rice Research Center (DOA)
 - Reports on Rice Fertilizer Trials on Acid Sulfate Soils
- D) Geotechnical Division, Royal Irrigation Department (RID)
 - Land Classification Map (some part of project area)
 - Soil analysis data

B. Field Survey

Field survey was carried out in order to:

A) check the validity of the above mentioned soil maps for use in agricultural planning.

- B) make the supplementary soil survey with particular emphasis on: a) soil texture, b) problem soils
- C) determine suitability for cropping and irrigation of various soil series.
- D) interview with government officers of the provincial agencies concerned, private sectors and farmers.

Additional soil survey was made by an examination of soils from auger borings, road cuts and in excavations. Observations were made to a depth of 150 cm. A short description of each soil horizon was recorded in the field sheets. Descriptions contained information about depth, texture, colour, pH, occurrence of mottles and others. Soil classification at soil series level currently used in DLD was adopted. Soil sample collection was done and analyzed in laboratory.

3. RESULT OF STUDY

A. Parent Material and Landform

Soils in study area are derived from four main parent materials namely marine sediments, brackish water sediments riverine sediments and residuum and colluvium. The flat lowlands in the western of the study area occupying approximately 30 percent are mainly formed from sediments of marine, brackish water, recent and semi-recent riverine alluvium. The highlands in the eastern are originated from old alluvial deposits and residual materials from mostly elastic rocks with some granite and limestone. Old alluvium found about 28 percent occurs on terrace landform little higher than paddy land whereas residuum and colluvium are dominated on piedmont and foothill areas. Extent is about equal to old alluvial terrain, that is about 28 percent. The rest of 19 percent is devoted to mountainous and slope complex areas.

Major landforms of this area can be identified into seven groups including tidal flat, former tidal flat, floodplain, low terrace, higher terrace, foothill and mountainous areas. Soils and their distribution patterns are highly correlated with the landforms on which they occur.

B. Soil Mapping Unit

Based on detailed reconnaissance soil maps of Chon Buri, Chachoengsao, Prachin Buri and Nakhon Nayok as presented in Figures B1, 2, 3 and 4. These are distributed in the mentioned four provinces in the numbers of 28, 36, 37 and 15 units as shown in Tables B-7 to B13 respectively. Mapping units are soil series, association and complex. These subgroups and families are also shown in the mentioned tables. Their extents by Amphoe-wise in each province from Chon Buri to Nakhon Nayok were tabulated in Tables B14 to B17 respectively.

C. Soil Types and Their Characteristics

Major characteristics of all soils are tabulated in Table <u>B-18 to B-32</u>. Their fertility levels are shown in Table B-33 to B-39. Soil types and

characteristics can be summarized based on parent materials and landforms as follows:

A) Soils on Lowland

a) Soils Divided from Marine Sediment

These marine sediment soil types are formed on tidal flat and former tidal flat.

a) Soils on Tidal Flat

The tidal flat areas are found around the river mouth. They are still under the influences of sea water. The soils are very deep, poorly drained very dark gray unripen marine clay. Soil reaction is neutral to mildly alkaline with pH ranging from 7 to 8. Soil fertility is rather high. Theses soils are potential acid sulfate containing high content of pyrite in subsoils. Under present reduction condition, they do not show acid reaction. However, they are rapidly transformed into acid sulfate soils when they are drained due to the pyrite will be oxidized and becoming acid condition.

Soils of this group comprise The Chin and Bung Pakong series making up 6,140 ha or about 0.4 percent of study area.

Due to these soils are flooded by sea water during high tide and still being under mangrove forest, they are not suited for crop cultivation and should strict their use for existing mangrove forest and some shrimp ponds,

b) Soils on Former Tidal Flat

Former tidal flats occupy the flat areas away from the reach of sea water flooding. Soils are very deep, poorly drained, slow permeability. They are characterized by gray or brownish gray clay with brownish and greenish mottles overlying gray, olive gray or greenish gray clay with brownish and greenish mottles. Bluish unriper marine clay clay occur in deep horizon. Soil reaction is slightly acid to neutral (pH6.5 7.0) subsoil increasing to alkaline (pH8.0) with depth. They are fertile soils with high nutrient status.

Soil units grouped into this category include Smert Prakarn, Bangkok, Phan Thong, Bang Nam Pries and Chachoengsao constituing the area coverage of about 40,200 ha or 2.5 percent of study area. Chachoengsao series is the biggist unit covering about 24,000 ha or around 1 percent.

These soils are now under paddy, they are best suited for paddy cultivation and worthy for irrigation development. Many upland crops such as soybean, mungbean and vegetables can be grown in dry season under irrigation scheme.

b) Soils Derived from Brackish Water Sediment

They occur on former tidal flat area developing from brackish water deposits. Most soils are actual acid sulfate having clayey texture throughout the profile. Horizon of dark gray clay occurs in the deep subsoils normally below 150 cm. The profile contains straw yellow jarosite mottles at some depths causing very strongly acid to extremely acid reaction. Such a low pH will reduce availability of phosphorus and make alluminum and iron toxic. Activity of soil microbs becomes very low and physical property of soils are poor resulting in low productivity.

Soils included are Cha-am, Maha Phot, Rangst, Rangsit-very acid, Onkharak, Don Muang and undifferentiated ridged acid soils. The extents are approximately 204,800 ha or 12 percent of study area. Rangsit series is the biggest unit covering some 96,500 ha or 6 percent of study area.

Due to acidity, these soils are modurately to poorly suited for paddy. However, with lime application at favorable rate and under irrigated water, acidity will be reduced resulting in increasing of rice yield. Some paddy areas have been changed to many kinds of fruit orchards such as mango, coconut, tangerine and palmelo. In dry season, many upland crops and vegetables can be grown. To leach soil acidity dry season rice crop is most favorable.

c) Soils Derived from Riverine Sediment

Riverine alluvial sediments are transported by riverine flesh water. On lowlands of the project area, they are formed on floodplain and low terrace which can be discussed as following.

i) Soils on Floodplain

Floodplain formations include river levees and flat areas or back swamps away from river.

Soils on levees: They are very deep, moderately well drained, stratified, fine-loamy with some mottles in subsoils. Soil reaction varies from strongly acid to slightly acid with pH of 5.0 to 6.5. Nutrient status is relatively low.

There are two soil series including Chiang Mai and Pran Bri. They are recognized only small extent of about 900 ha or 0.5 percent of study area.

They are well suited for orchard and for irrigation purpose.

Soils on back swamps: They are very deep, poorly drained with grayish brown or yellowish brown clay loam to clay. They are flooded by impounded rain and river water during the rainy season. Soil reaction is from medium to slightly acid with pH of 5.5 to 6.5.

Two soils are mapped namely Ratchaburi and Bang Pa-in covering about 12,000 ha or 0.7 percent of study area.

They are now used for paddy cultivation which is well suitable for irrigation.

ii) Soils on Low Terrace: They are move matured than those of floodplains. Clay illuviation has brought about the formation of an argillic horizon in most soils. They consist of either fine loamy or clayey with a wide range of colours from gray to brown. Distinct and prominent red and yellowish brown mottles occur throughout the profile. Soil reaction is between slightly to strongly and with pH of 5.0 to 6.5. Nutrient status is relatively low.

Soil units in this group are Alluvial Complex-poorly drained and well drained, Chon Buri, Klang, La-ngu, Hin Kong, Roi Er, Makham and Phen. They cover about 228,400 ha or 14 percent of study area.

The are considered moderately suited for paddy and well suited for irrigation development.

B) Soils on Highland

On highlands, soils are developed from the materials namely old alluvium on middle terrace, residuum and colluvium from elastic rocks, granite and limestone on high terrains.

a) Soils Derived from Old Aluvium

These soils occur on middle terraces which are found in positions above nearly flat low terraces. Topography is undulating dissected by many small tributaries. Soils derived from this parent material an either sandy, loamy or gravelly textures.

i) The sandy soils are very deep, excessively drained having sand or loamy sand texture throughout. Sandy clay loam may occur in the deep subsoil below 80-100 cm. Water holding capacity is very low and

permeability is high. Fertility is low. Only one soil unit is recognized in the area of about 8,250 ha or 0.5 percent of study area. These soils are generally not suited for paddy and poorly suited for upland crops due to sandy texture. Irrigation water cannot be irrigated by normal method because of the soil is too permeable and topography is uneven and high. They should be under rainfed upland crop cultivation.

- ii) The loamy soils are very deep, moderately well drained to well drained. Colours vary from brown, strong brown to yellowish red. Water holding capacity is medium and permeability is moderate. Fertility is low. They are generally well suited for orchard and moderately suited for upland crops. Irrigation development is possible by particular method depending on topography. Soil units are Ko Khanun, Don Rai, Khor Satuk, Warin and Yosothon covering the area about 293,660 ha or about 18 percent of study area. Khorat series occupies the most extent about 80,000 ha or 5 percent.
- iii) The gravelly soils are those having lateritic concretions at shallow depth making them poorly suited for upland crops and not favorable for irrigation. Soils classified in this type are Phon Phi Bang Khla, Pang Rai, Nong Khok and Mae Rim making up 165,700 ha or about 10 percent. Bang Khla series are the biggest covering about 85,200 ha or 5 percent of study area. These soils should be cultivated to upland crop, tree crop or reforest.

b) Soils Derived from Residuum and Colluvium

The residual and colloquial soils occur on highlands, foothill slopes and mountainous areas comprising those formed from elastic rock, granite and limestic.

- i) Soils developed from elastic rocks are mostly gravelly soils poorly suited for upland crops, and not suited for irrigation. Those are Kabin Buri, Chiang Khan, Wang Shaphung. O Lum Chiak, Husi Yot, Muak Lat Ya and Tha Yang, totalling 214,850 ha or about 13 percent of study area. Kabin Buri series cover the largest area of about 93,200 ha or 6 percent of study area. They are suited for upland crops, tree crops or reforestation. Thap Phrik and Thap Kwang series are only two soils that are very deep, medium-textured suitable for orchard and upland crops. However, irrigation suitability is based on topography.
- ii) Soils derived from granitic rocks are very deep sand y and coarse loamy-textured poorly suited for upland crops and not suited for irrigation. Soil units include Ban Bung, Hup Kapong, Sattahip, Map Bon and Mong Mot series. They occupy 111,600 ha or about 7 percent

of study area. Ban Bung series having 41,300 ha or 2.5 percent are the biggest soils. They should be under upland crop or tree crop.

iii) Soils derived from limestone are found very small area of about 9,200 ha, or 0.5 percent. Mast are clayey soils having relatively high fertility. Lop Buri, Takhli and Bung Chanang are included, Lop Buri series are very deep, black or very dark grayish brown clay. Tha Khli series are similar to Lop Buri but containing lime concretions. Bung Chanang series are shallow to moderately deep, yellowish red clay. Lop Buri soils should be used for orchard or upland crop while Tha Khli and Bung Chanang are for upland crop or tree crop plantation.

Soils on mountainous areas are generally very shallow. Due to many severe limitations such as very high and steep topgraphy, severe erosion, they are not suited for any kind of crop cultivation and should be under forest. The extents are approximately 287,350 ha or about 17 percent of study area.

D. Soil Suitability Classification

For effective land use planning, soil suitability for specific use is essential. In this section, the suitability of soils is identified for paddy (P), non-flooded annual crop (N) and fruit tree plantation (F).

(1) Soil Suitability Class: Principally, there are five classes as follows:

Class I (P-I, N-I, F-I): Soils very well suited having no significant limitations

Class II (P-II, N-II, F-II): Soils well suited having slight limitations

Class III (P-III, N-III, F-III): Soils moderately suited having moderate limitations that require special management

Class IV (P-IV, N-IV, F-IV): Soils poorly suited having severe limitations that require very careful management

Class V (P-V, N-V, F-V): Soils not suited having very severe limitations that preclude their use for crop production with ordinary method.

(2) <u>Soil Suitability Subclass</u>: At the lower level, the suitability classes are further identified into subclasses based on kinds and degree of hazard of limitations.

The followings are the main limitations used in identifying suitability classes into subclasses.

- f: flooding susceptibility to flash floods or prolonged dup flooding or both, which damage the crops or limit choice of crops.
 - x: salinity excessive salts which affect crop growth
 - s: unfavorable surface soil texture
 - j: jarosite
 - n: low nutrient status or low fertility
 - g: gravels in soil profile
 - w: risk of water shortage water stress in growing season
 - d: impeded drainage
 - t: topography of slope
 - c: consolidated layer.

Suitability subclass for paddy, non-flooded annual crop and fruit tree of each soil unit are given in Table B-40 to B-42.

E. Land Plan Analysis and Management

This section will cover general view of land use planning emphazing on analysis of land use suitability zonings for crop cultivation and other land use types. These are made based on information on soil suitability discussed in 3.5 and existing land use conditions.

In all, eightzones of suitable land use of study area were distinguished listed as follows:

- Zone 1: Soils suited for paddy, well suited for irrigation
- Zone 2: Soils suited for upland crop, not suited for irrigation
- Zone 3: Soils suited for upland crop, tree crop or reforestation, not suited for irrigation
- Zone 4: Soils suited for upland crop on tree crop, not suited for irrigation.