

**APPENDIX A-2-2**

**Runoff Analysis**



## Runoff Analysis

### Rainfall Synthesis

The daily rainfall data for the six gauging stations, collected from the Meteorological Department, RID and NEA within and around the vicinity of the study area, contain many missing data. To generate such missing data, correlation study was done on the basis of monthly rainfall using the overlapping observation periods of the stations.

The coefficients of correlation and equations of linear regression employed to synthesize the missing rainfall data in the object stations were determined statistically by means of the method of least square on a monthly basis among stations.

The highest correlation was taken to complement the missing rainfall data and generation of daily rainfall was done following the procedures shown below;

a) Equation of linear regression obtained through the correlation study is expressed as:

$$Y = aX + b$$

where X: Monthly rainfall at the key station which keeps perfect daily record of rainfall during period under consideration

Y: Expected monthly rainfall at the object station which involves missing data

a,b: Coefficient and constant

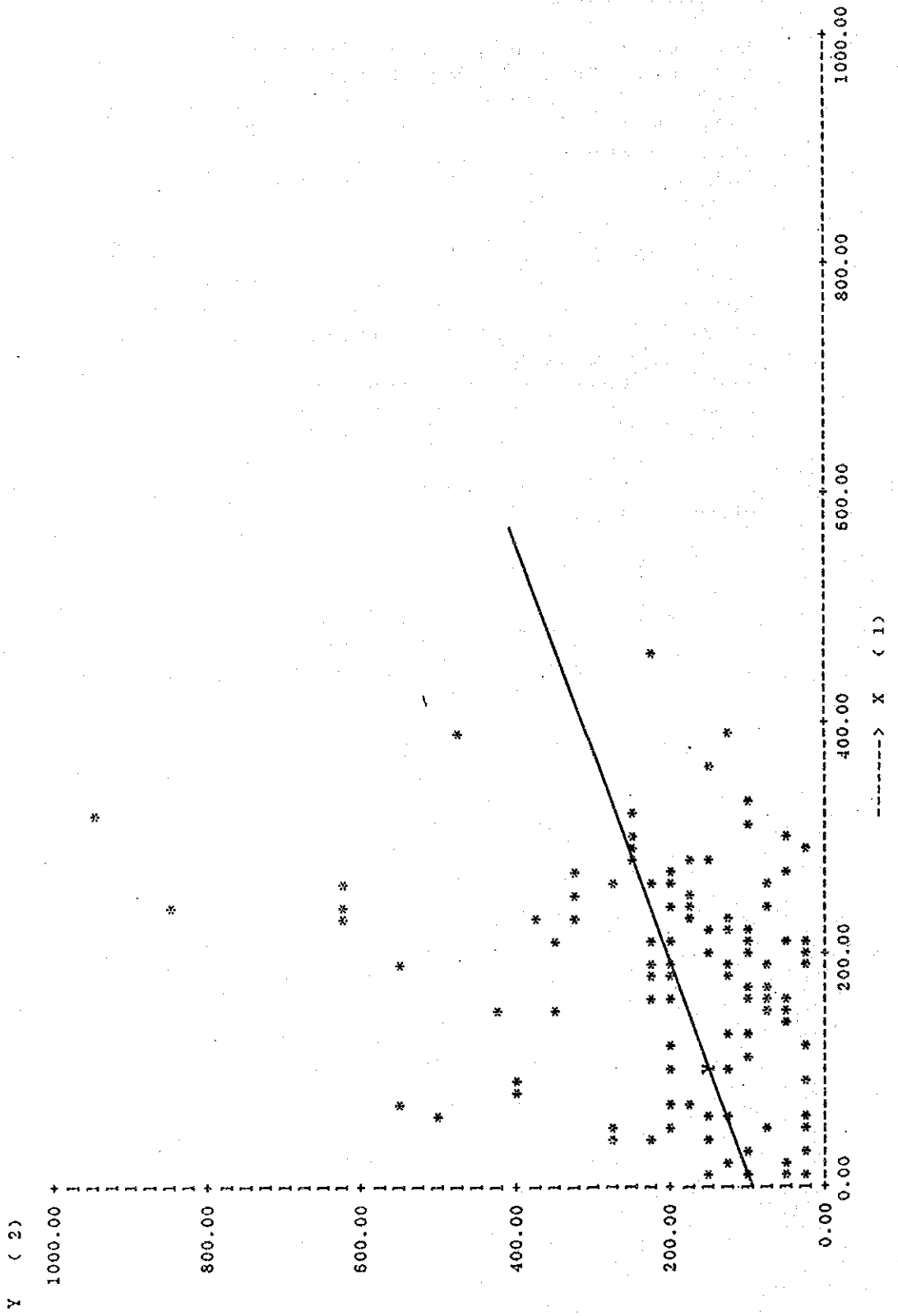
\*\*\*\*\* THE REGRESSION LINE OF CO-RELATION OF RAINFALL BETWEEN NAKORN SI THAMMARAT AND CHA\*\*\*\*\*

1973--1987

$$Y = 0.508 X + 92.061 \quad (MM)$$

$$X = 0.196 Y + 128.649 \quad (MM)$$

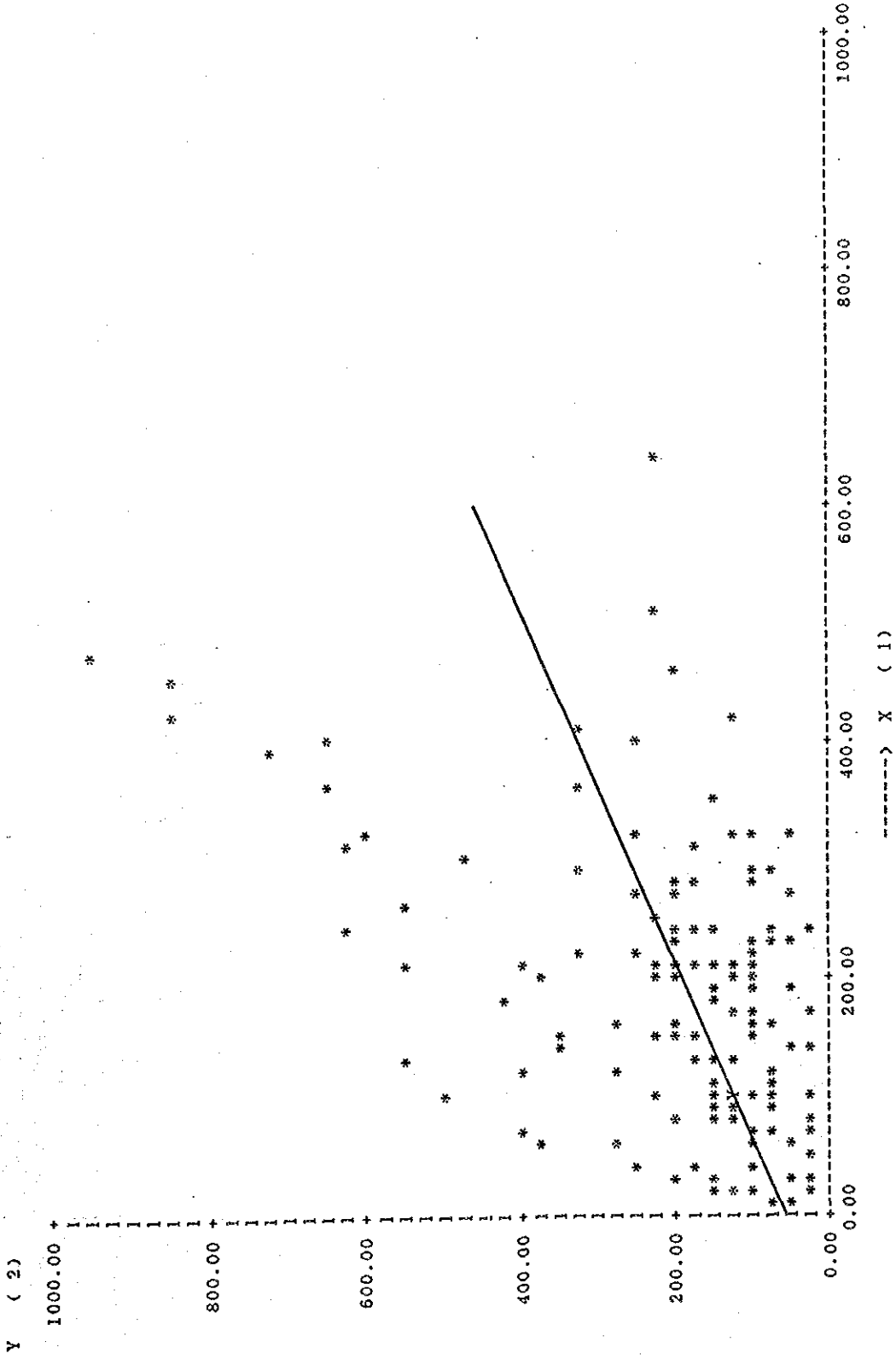
) R = 0.316



\*\*\*\*\* THE REGRESSION LINE OF CO-RELATION OF RAINFALL BETWEEN THUNG SONG AND NAKORN SI TH\*\*\*\*\*

1973--1987

Y = 0.753 X + 60.346 ( MM ) R = 0.498  
 X = 0.329 Y + 113.446 ( MM )

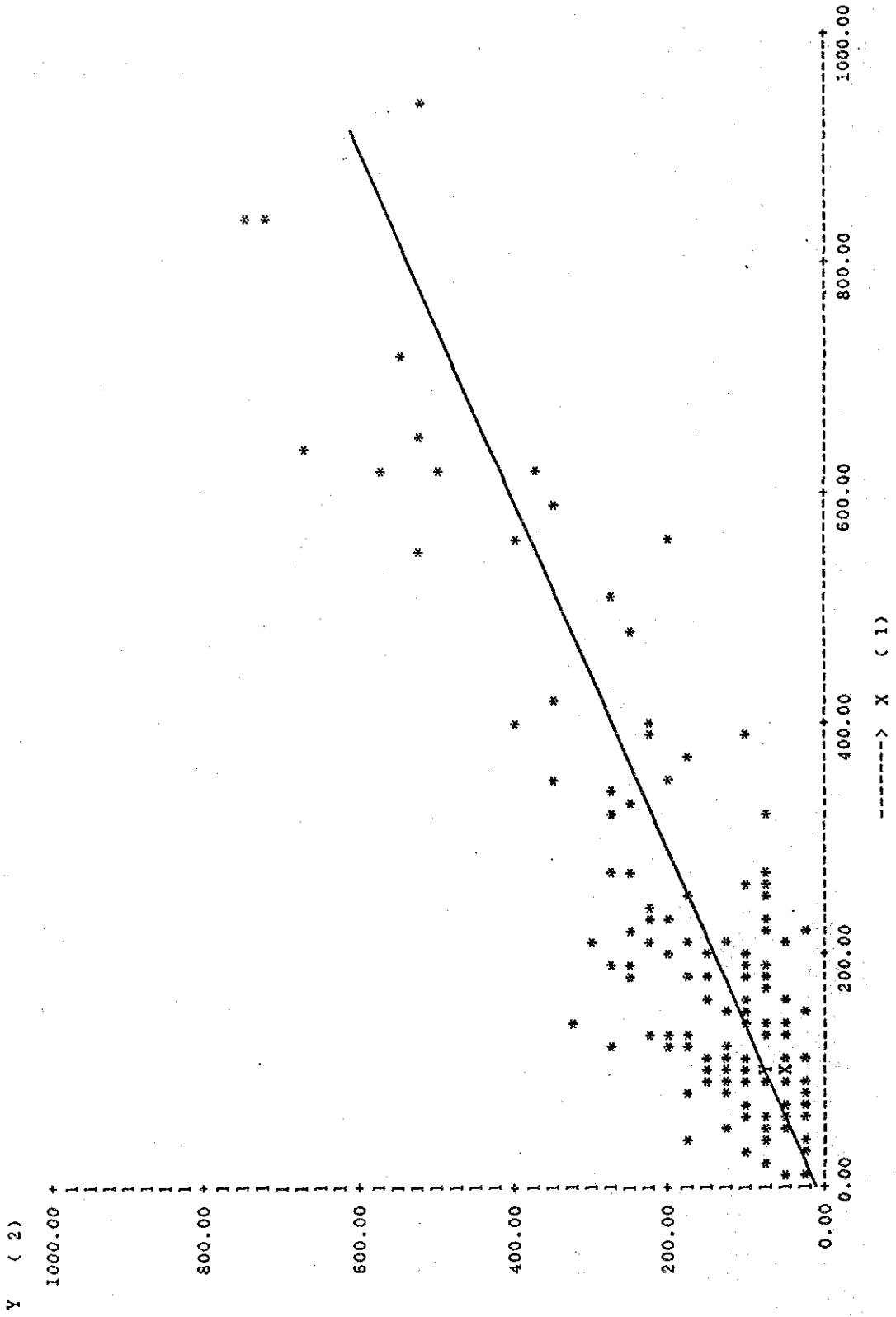


\*\*\*\*\* THE REGRESSION LINE OF CO-RELATION OF RAINFALL BETWEEN NAKORN SI THAMMARAT AND RON\*\*\*\*\*

1973--1987

$$Y = 0.702 X + 13.217 \quad ( \text{MM} ) \quad R = 0.858$$

$$X = 1.049 Y + 38.412 \quad ( \text{MM} )$$



\*\*\*\*\* THE REGRESSION LINE OF CO-RELATION OF RAINFALL BETWEEN CHAWANG AND LAN SAKA \*\*\*\*\*

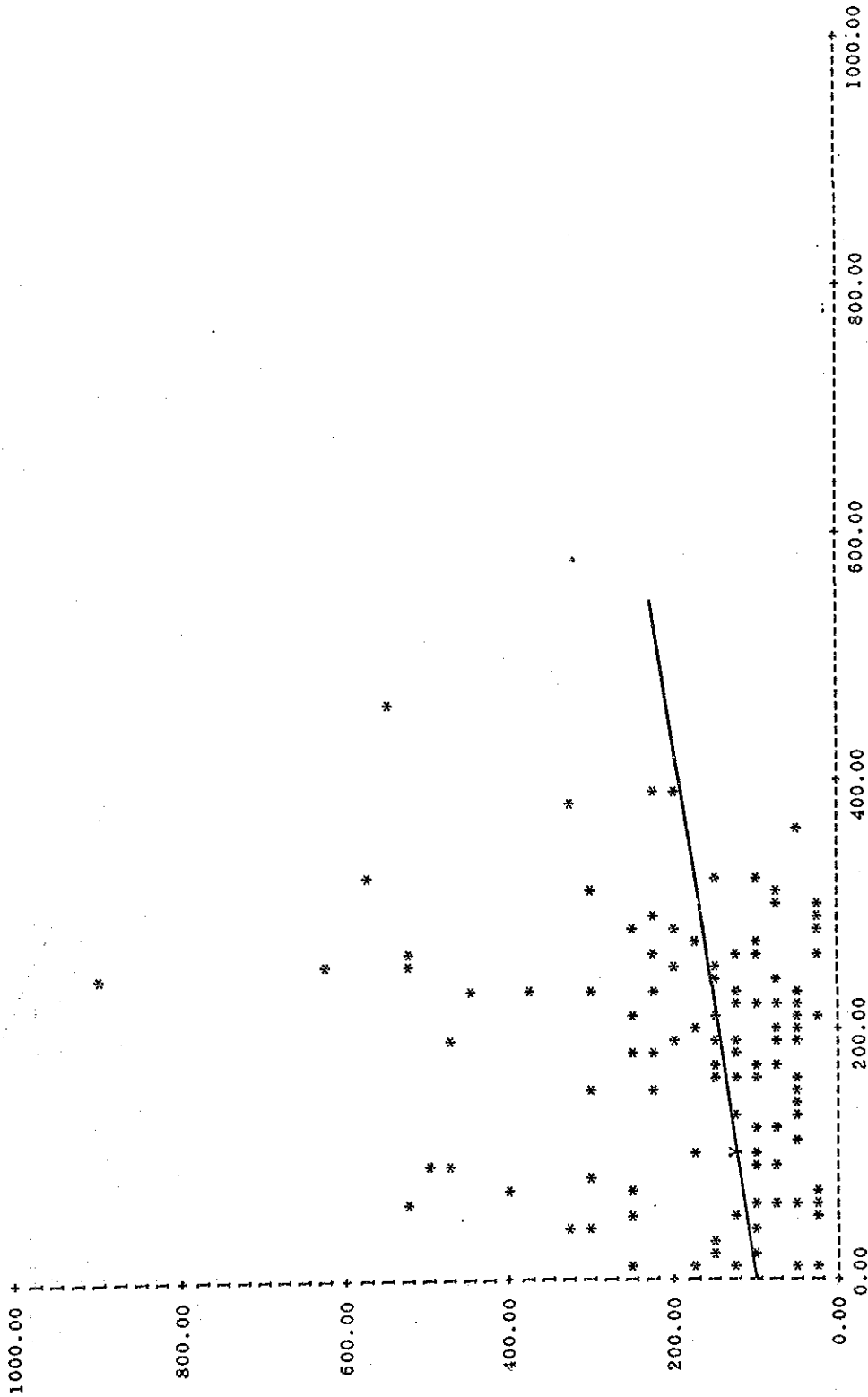
1973--1987

$$Y = 0.302 X + 106.708 \quad ( \text{MM} )$$

$$X = 0.139 Y + 147.301 \quad ( \text{MM} )$$

) R = 0.205

Y ( 2 )



\*\*\*\*\* THE REGRESSION LINE OF CO-RELATION OF RAINFALL BETWEEN THUNG SONG AND LAN SAKA \*\*\*\*\*

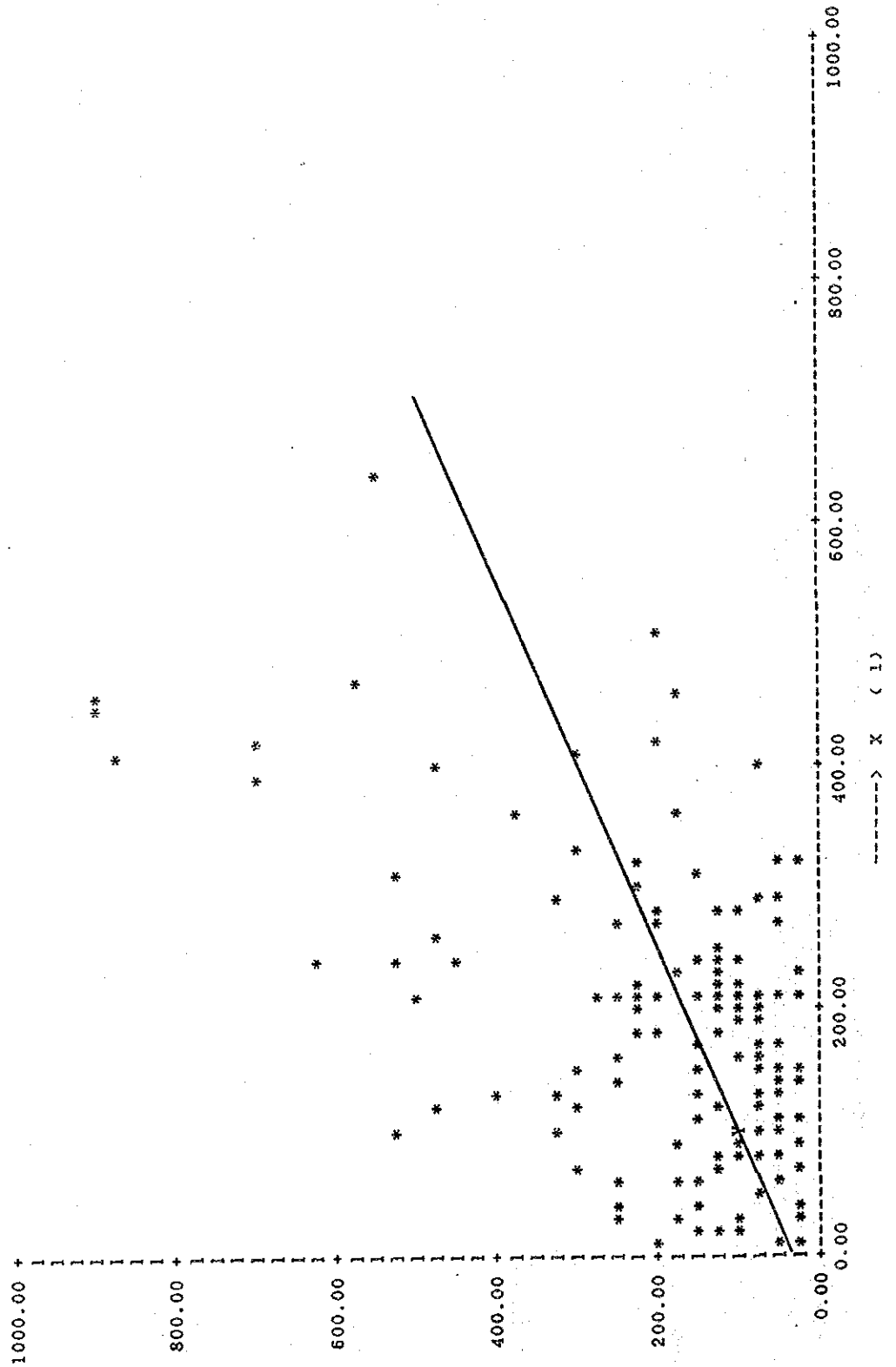
1973--1987

$$Y = 0.728 X + 38.245 \quad (MM)$$

$$X = 0.334 Y + 127.236 \quad (MM)$$

) R = 0.494  
)

Y ( 2 )





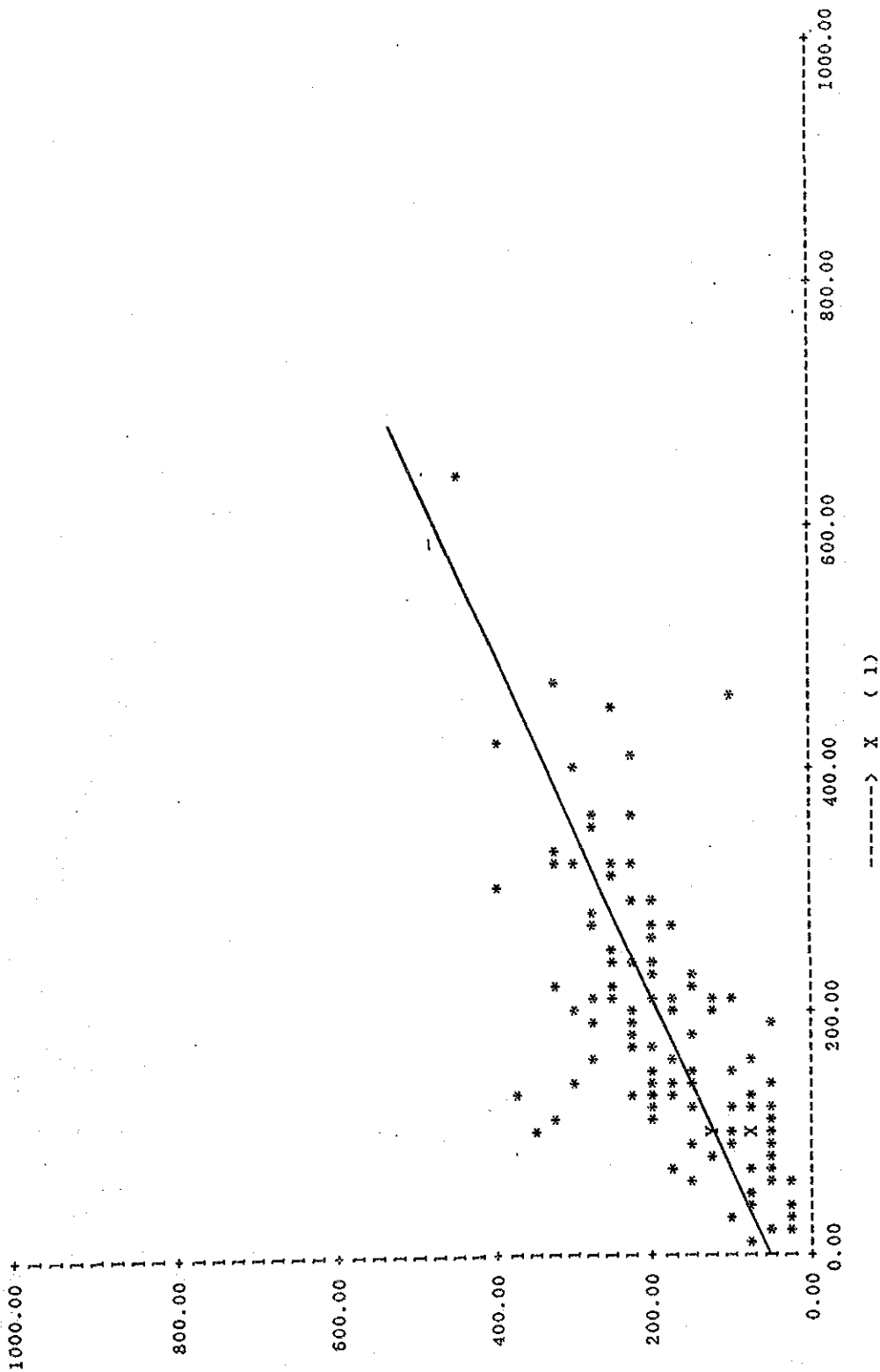
\*\*\*\*\*

THE REGRESSION LINE OF CO-RELATION OF RAINFALL BETWEEN THUNG SONG AND CHAWANG

1973--1987

$$Y = 0.649 X + 56.458 \quad ( \text{MM} ) \quad R = 0.732$$
$$X = 0.826 Y + 37.553 \quad ( \text{MM} )$$

Y ( 2 )

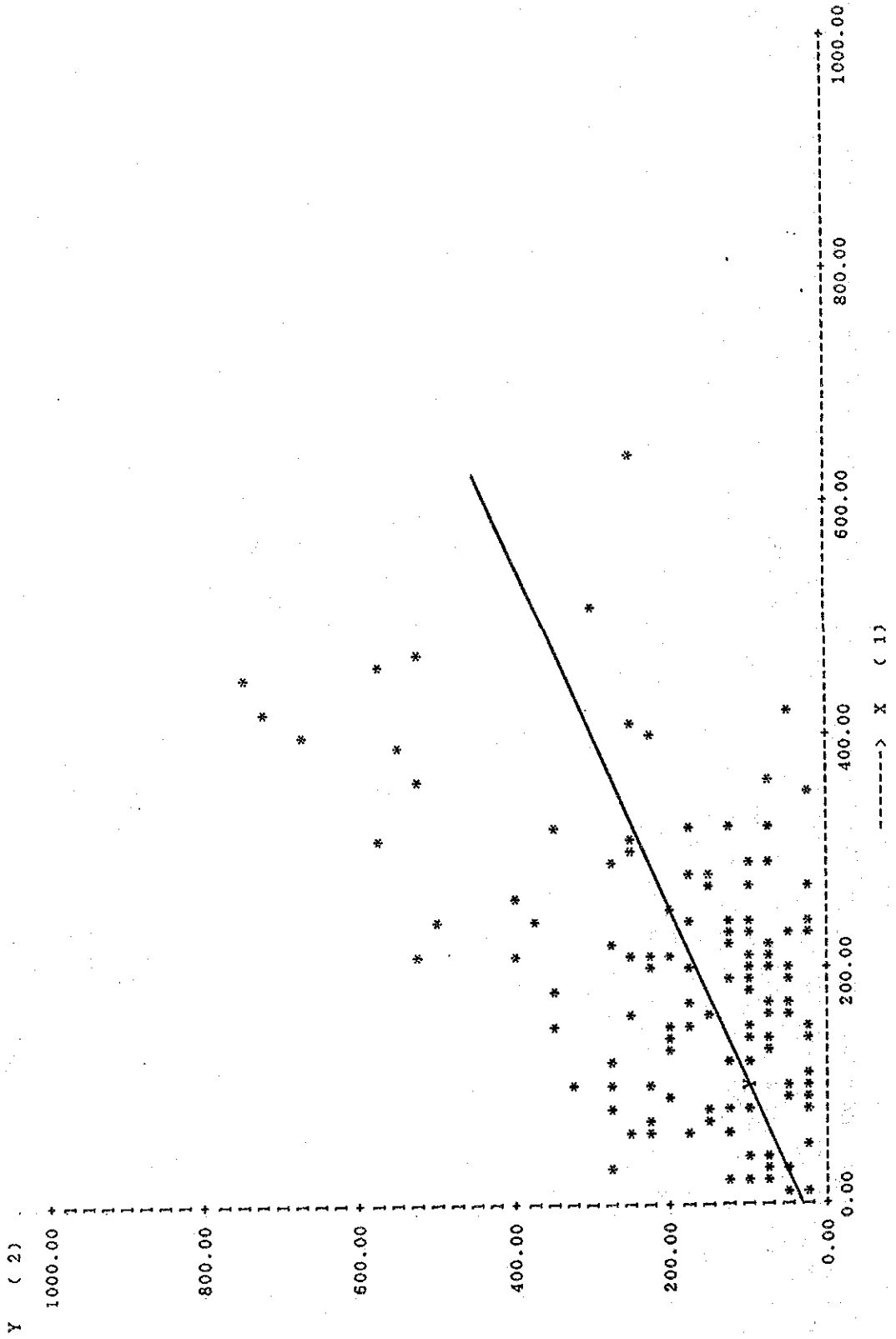


\*\*\*\*\* THE REGRESSION LINE OF CO-RELATION OF RAINFALL BETWEEN THUNG SONG AND RON PHIBUN \*\*\*\*\*

1973--1987

$$Y = 0.671 X + 34.597 \quad (MM) \quad R = 0.510$$

$$X = 0.387 Y + 125.210 \quad (MM)$$



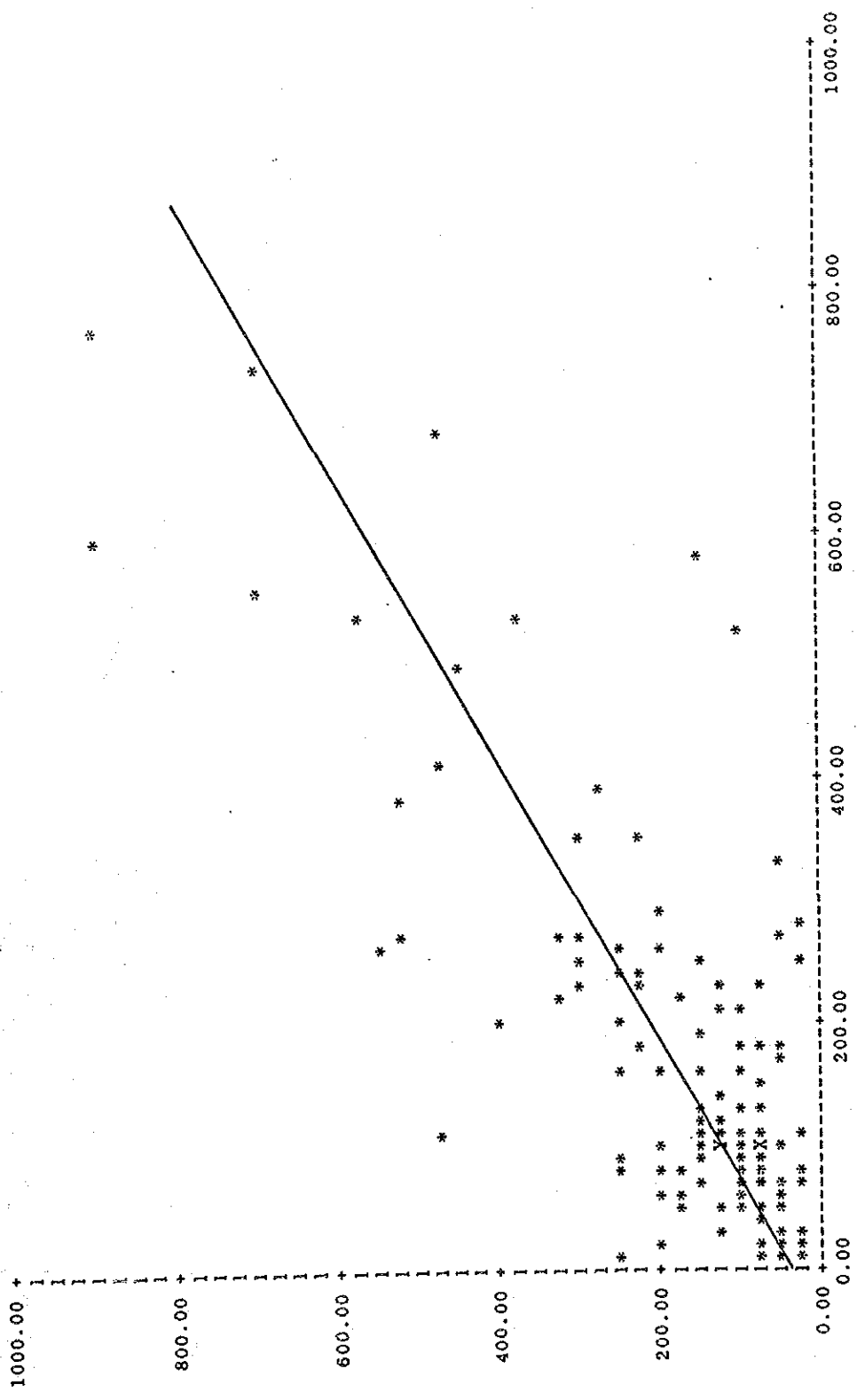
\*\*\*\*\*

\*\*\*\*\* THE REGRESSION LINE OF CO-RELATION OF RAINFALL BETWEEN RON PHIBUN AND LAN SAKA \*\*\*\*\*

1973--1987

$Y = 0.795 X + 37.098$  ( MM )  $R = 0.749$   
 $X = 0.705 Y + 44.645$  ( MM )

Y ( 2 )



-----> X ( 1 )

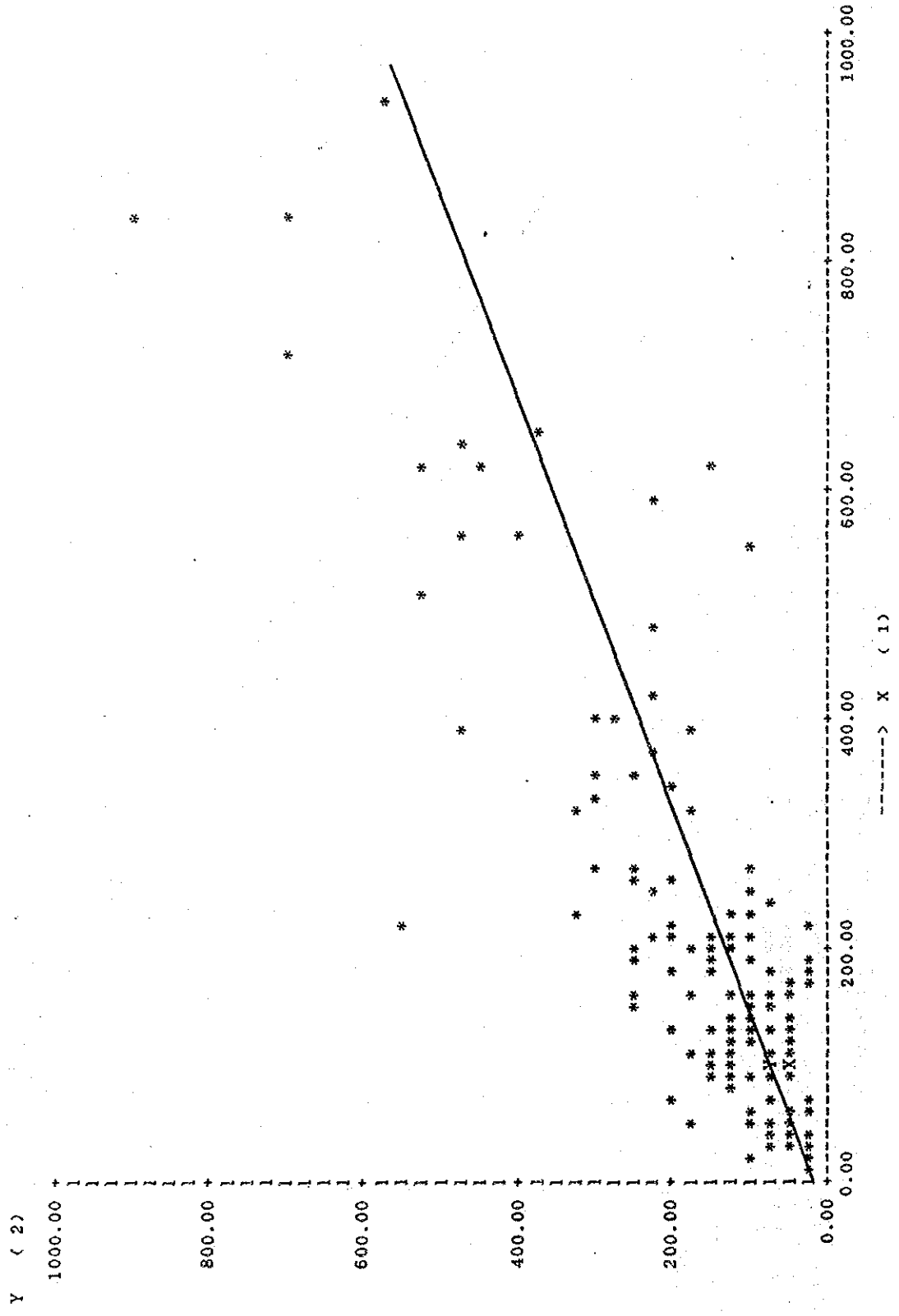
\*\*\*\*\* THE REGRESSION LINE OF CO-RELATION OF RAINFALL BETWEEN NAKORN SI THAMMARAT AND LAN\*\*\*\*\*

1973--1987

$$Y = 0.680 X + 18.829 \quad (MM)$$

$$X = 1.010 Y + 40.788 \quad (MM)$$

) R = 0.829



\*\*\*\*\* THE REGRESSION LINE OF CO-RELATION OF RAINFALL BETWEEN RON PHIBUN AND CHAWEANG \*\*\*\*\*

1973--1987

Y = 0.174 X + 146.806 ( MM ) R = 0.230  
 X = 0.304 Y + 91.949 ( MM )

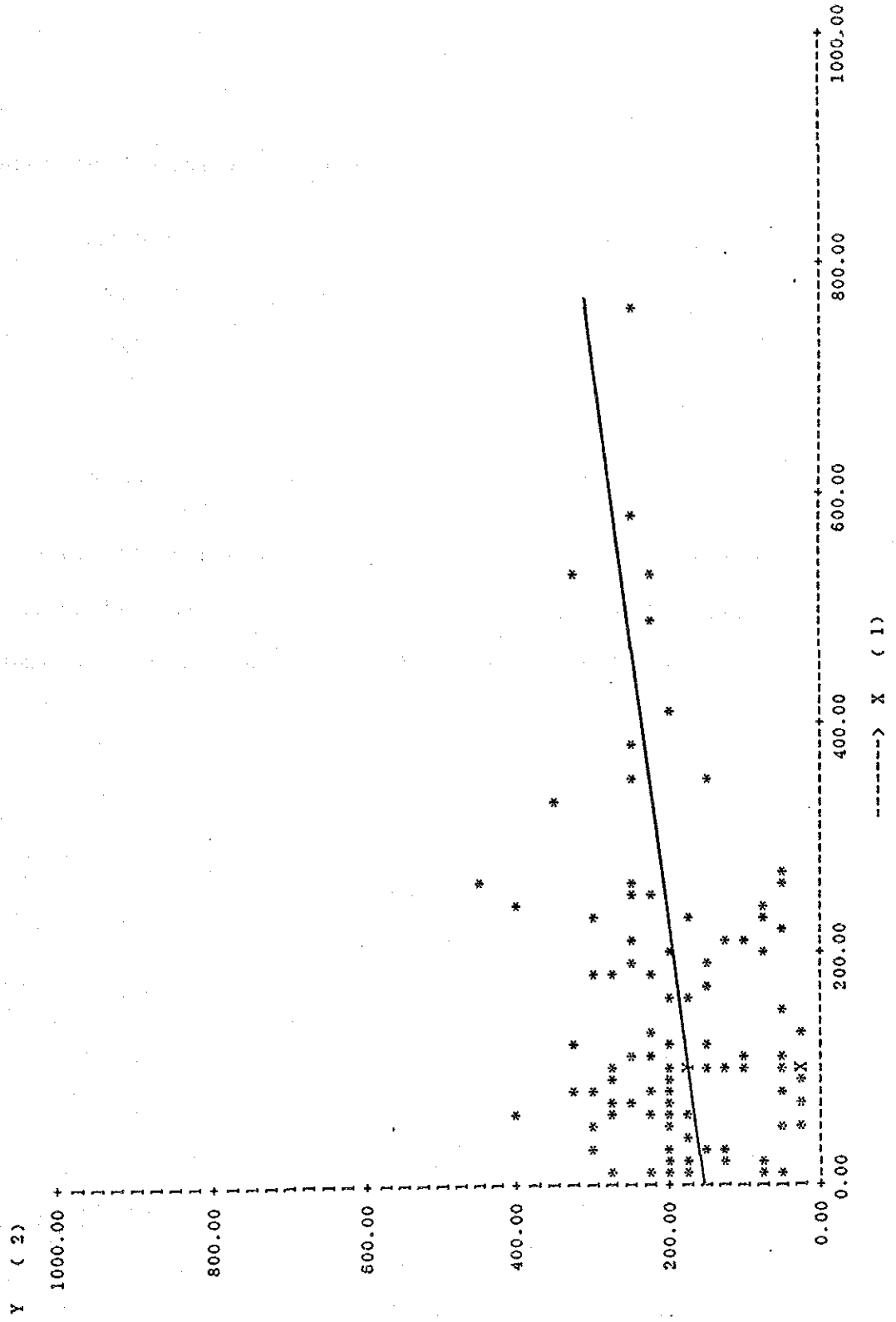


Table Ab-3-1 Co-relationship of Rainfall Stations

|         | THUNG | LAN   | RON   | OHAWENG | NAKON |
|---------|-------|-------|-------|---------|-------|
| THUGN   | -     | 0.510 | 0.494 | 0.732   | 0.498 |
| LAN     | 0.510 | -     | 0.749 | 0.230   | 0.829 |
| RON     | 0.494 | 0.749 | -     | 0.205   | 0.858 |
| CHAWENG | 0.732 | 0.230 | 0.205 | -       | 0.316 |
| NAKON   | 0.498 | 0.829 | 0.858 | 0.316   | -     |

Rainfall at Lan Saka =  $0.68 \times \text{Nakon} + 0.63$  (mm)

Rainfall at Ron Phiboon =  $0.702 \times \text{Nakon} + 0.44$  (mm)

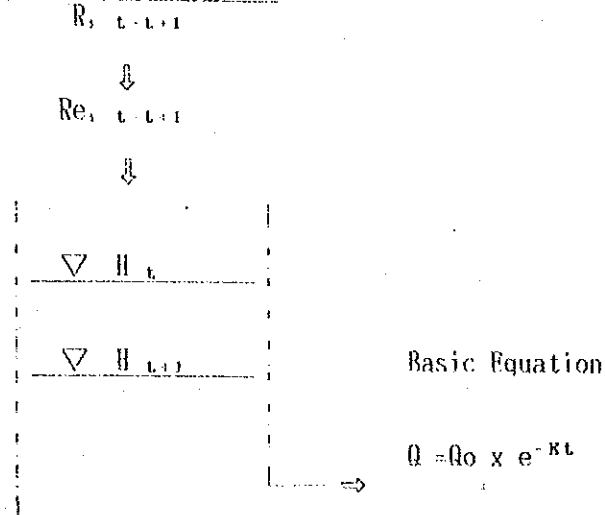
Rainfall at Thung Song =  $1.049 \times \text{Chawang} + 1.28$  (mm)

## 6-3-2 Runoff Model

### (I) Tank Model

#### (a) General

Water Balance in the Tank



The water balance in the tank is given by the following differential equation :

$$H_{t+1} = H_t + (Re_{t-t+1} - (Q_t + Q_{t+1})/2) dt$$

where:  $H_{t+1}$  = water stage in the tank at  $t = t+1$

$H_t$  = -do- at  $t = t$

$Re_{t-t+1}$  = effective rain poured into tank during time  $t$  and  $t+1$

$Q_t$  = outflow from tank at  $t = t$

$Q_{t+1}$  = -do- at  $t = t+1$

$dt$  = time interval for calculation

Giving that  $dt = 1.0$  day,  $Q_t = KH_t$  and  $Q_{t+1} = KH_{t+1}$ , then :

$$H_{t+1} = H_t + Re_{t-t+1} - KH_{t+1}/2$$

$$H_{t+1} = (1-K/2)/(1+K/2)H_t + 1/(1+K/2)Re_{t-t+1}$$

$$= aH_t + bRe_{t-t+1}$$

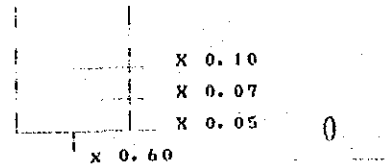
FIGURE A6-3-1 TANK MODEL AT X-70

Location X-70

Initial Water  
Depth (mm)

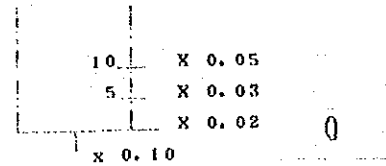
Catchment 39.0 km<sup>2</sup>

Top Tank



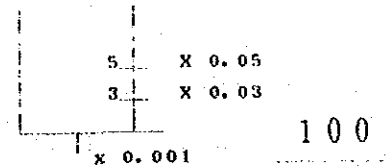
Study Period 1976 - 1979 (4 yrs)

Second Tank



Areal Rainfall 1723 mm/yr  
in Study Period

Third Tank

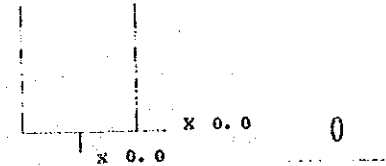


Rainfall Station (%) Adjusted

Lon Saka

100 X 1,047

Fourth Tank



Evapotranspiration (mm/day):

| Jan | Feb | Mar | Apr | May | Jun | Jul | Aug | Sep | Oct | Nov | Dec | Annual |
|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|--------|
| 2.2 | 2.9 | 3.0 | 3.2 | 2.8 | 3.1 | 3.0 | 3.2 | 2.6 | 2.4 | 1.9 | 2.1 |        |

Note: Evapotranspiration = Potential Evapotranspiration X 0.7

Operation 1 : Evapotranspiration Subtracted from top to thirt tanks,  
from top tank when water in top tank, from second tank  
when no water in top tank, so on.

Operation 2 : Evapotranspiration reduced to 80% when rainy day.



Hydrological Water Balance (Average in study Period)

|             | Areal<br>Rainfall<br>(mm/yr) | Observed<br>Runoff<br>(mm/yr) | Computed<br>Runoff<br>(mm/yr) | Evapotrans-<br>piration<br>(mm/yr) | Ground Water<br>Recharge<br>(mm/yr) |
|-------------|------------------------------|-------------------------------|-------------------------------|------------------------------------|-------------------------------------|
| Water Depth | 1,723                        | 1,938                         | 1,448                         | 288                                | 0                                   |
| Ratio       |                              | 1,124                         | 0.840                         | 0.167                              | 0                                   |

(2) Multiple Regression Model

(a) General

Runoff (Q) is generally explained in the following formula as rainfall (R) Function ;

$$Q_i = f(R_{i1}, R_{i2}, R_{i3}, \dots, R_{in}) \quad \text{----- (1)}$$

- where
- $R_{i1}$  ; Today's Rainfall
  - $R_{i2}$  ; Previous day's Rainfall
  - $R_{i3}$  ; 2 days before Rainfall

Suppose that runoff is described as the linear combination of rainfall; formula (1) will be as follows,

$$Q_i = \beta_0 + \beta_1 R_{i1} + \beta_2 R_{i2} + \dots + \beta_n R_{in} + \delta_i \quad \text{---- (2)}$$

where,

- $\beta_0, \beta_1, \dots, \beta_n$  ; unknown constant
- $\delta_i$  ; Balance which can not be explained by  $R_{i1} \dots - R_{in}$ .

Multiple regression analysis is to obtain the most reliable im-  
partial estimate among these unknown parameters by

Now the balance square addition should be minimized in order to  
obtain the estimate of  $\beta_0, \beta_1, \dots, \beta_n, b_0, b_1, \dots, b_n$

$$E = \sum \left\{ Q_i - (b_0 + b_1 R_{i1} + \dots + b_n R_{in}) \right\}^2 \quad \text{---- (3)}$$

Namely

$$\begin{aligned}
 \frac{\alpha E}{\alpha b_0} &= -2 \sum \left\{ Q_i - (b_0 + b_1 R_{i1} + \dots + b_n R_{in}) \right\} = 0 \\
 \frac{\alpha E}{\alpha b_1} &= -2 \sum R_{i1} \left\{ Q_i - (b_0 + b_1 R_{i1} + \dots + b_n R_{in}) \right\} = 0 \\
 &\dots \dots \dots \\
 \frac{\alpha E}{\alpha b_n} &= -2 \sum R_{in} \left\{ Q_i - (b_0 + b_1 R_{i1} + \dots + b_n R_{in}) \right\} = 0
 \end{aligned} \tag{4}$$

By arranging the above equations, simultaneous equation can be obtained,

$$\begin{aligned}
 n b_0 + (\sum R_{i1}) b_1 + (\sum R_{i1}) b_2 + \dots + (\sum R_{in}) b_n &= \sum Q_i \\
 (\sum R_{i1}) b_0 + (\sum R_{i1}^2) b_1 + (\sum R_{i1} R_{i2}) b_2 + \dots + (\sum R_{i1} R_{in}) &= \sum R_{i1} Q_i \\
 &\dots \dots \dots \\
 (\sum R_{i1}) b_0 + (\sum R_{i1} R_{i1}) b_1 + (\sum R_{i2} R_{in}) b_2 + \dots + (\sum R_{in}^2) b_n &= \sum R_{in} Q_i
 \end{aligned} \tag{5}$$

The quadratic term describing non-linear runoff will be the following equation;

$$\begin{aligned}
 \ell_i &= Q_i - E Q_i \\
 \alpha_0 + \sum_{j=k}^{i+n} \sum_{k=j}^{i+n} \alpha_{jk} R_j R_k & E_i \tag{6}
 \end{aligned}$$

As the same way as linear equation,  $\alpha_0, \alpha_{i,j}$  can be obtained by minimizing the balance square addition (7)

$$E = \sum \left\{ \ell_i - \left( a_0 + \sum_{j=k}^{i+n} \sum_{k=j}^{i+n} a_{jk} R_j R_k \right) \right\}^2 \tag{7}$$

In order to minimize (7), the following formula must be formed.

$$\left. \begin{aligned} \frac{\alpha E}{\delta a_0} &= -2 \sum \left\{ e_i - \left( a_0 + \sum_{j=k}^{i+n} \sum_{k=j}^{i+n} a_{jk} R_j R_k \right) R_{i1} \right\} = 0 \\ \frac{\alpha E}{\delta a_{em}} &= -2 \sum R_i \cdot R_m + \left\{ e_i - \left( a_0 + \sum_{j=k}^{i+n} \sum_{k=j}^{i+n} a_{jk} R_j R_k \right) R_{i1} \right\} = 0 \end{aligned} \right\} (8)$$

Now,

$$a_0 + \sum_{j=k}^{i+n} \sum_{k=j}^{i+n} a_{jk} R_j R_k = \sum e_i$$

$$\left( \sum R_l R_m \right) a_0 + \sum \left\{ R_l R_m \sum_{j=k}^{i+n} \sum_{k=j}^{i+n} a_{jk} R_j R_k \right\} = \sum R_l R_m e_i$$

RUNOFF ANALYSIS BY TANK MODEL (DAILY BASE)

• LOCATION : THUNG SONG  
 • ANALYSED POINT : X-70  
 : LAN SAKA  
 • CA : 39.000 (kil)

DIMENSION OF TANK

|        |        | UPPER HOLE | MIDDLE HOLE | LOWER HOLE | PENETRATION | EVAPORATION RATE |
|--------|--------|------------|-------------|------------|-------------|------------------|
| TANK 1 | COEFF  | 0.100000   | 0.070000    | 0.050000   | 0.600000    | 1.000            |
|        | HEIGHT | 60.0       | 30.0        | 0.0        |             |                  |
| TANK 2 | COEFF  | 0.050000   | 0.030000    | 0.020000   | 0.400000    | 0.0              |
|        | HEIGHT | 10.0       | 5.0         | 0.0        |             |                  |
| TANK 3 | COEFF  | 0.050000   | 0.030000    | 0.025000   | 0.001000    | 0.0              |
|        | HEIGHT | 5.0        | 3.0         | 0.0        |             |                  |
| TANK 4 | COEFF  | 0.0        | 0.0         | 0.0        | 0.0         | 0.0              |
|        | HEIGHT | 0.0        | 0.0         | 0.0        |             |                  |

【 MONTHLY EVAPORATION 】

(mm/D)

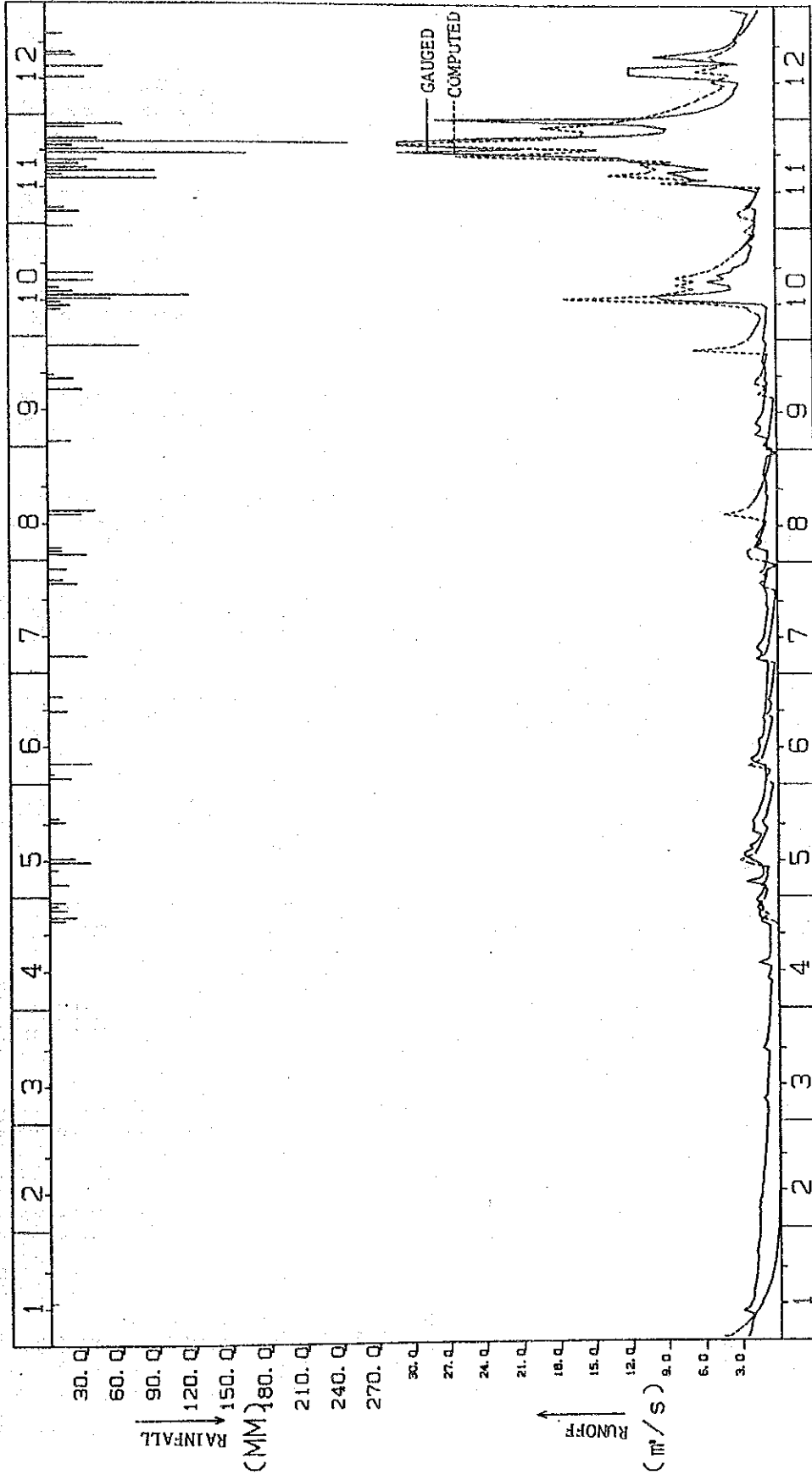
|      | 1    | 2    | 3    | 4    | 5    | 6    | 7    | 8    | 9    | 10   | 11   | 12   |
|------|------|------|------|------|------|------|------|------|------|------|------|------|
| RATE | 2.20 | 2.90 | 3.00 | 3.20 | 2.80 | 3.10 | 3.00 | 3.20 | 2.60 | 2.40 | 1.90 | 2.10 |

KUNOFF ANALYSIS BY TANK MODEL

(1976)

RAINFALL STATION: LAN SAKA

COEFFICIENT = 0.8132



GAUGING STATION : X-70 ( CA = 39.00 km )

< DAILY RAINFALL > THUNG SONG  
(1976 ) LAN SAKA

UNIT = (mm/D)

|             | 1 JAN   | 2 FEB   | 3 MAR   | 4 APR    | 5 MAY    | 6 JUN    | 7 JUL    | 8 AUG    | 9 SEP    | 10 OCT    | 11 NOV    | 12 DEC   |
|-------------|---------|---------|---------|----------|----------|----------|----------|----------|----------|-----------|-----------|----------|
| 1           | 0.0     | 0.0     | 0.0     | 0.0      | 0.0      | 0.0      | 0.0      | 0.0      | 0.0      | 0.0       | 0.0       | 0.0      |
| 2           | 0.0     | 0.0     | 0.0     | 0.0      | 0.0      | 17.8     | 0.0      | 31.4     | 18.8     | 0.0       | 0.0       | 0.0      |
| 3           | 0.0     | 0.0     | 0.0     | 0.0      | 0.0      | 4.2      | 0.0      | 10.5     | 0.0      | 0.0       | 0.0       | 0.0      |
| 4           | 0.0     | 0.0     | 0.0     | 0.0      | 15.2     | 0.0      | 0.0      | 10.5     | 0.0      | 0.0       | 26.2      | 0.0      |
| 5           | 0.0     | 0.0     | 0.0     | 0.0      | 0.0      | 0.0      | 31.4     | 0.0      | 0.0      | 0.0       | 13.6      | 0.0      |
|             | ( 0.0 ) | ( 0.0 ) | ( 0.0 ) | ( 0.0 )  | ( 15.2 ) | ( 22.0 ) | ( 31.4 ) | ( 52.3 ) | ( 18.8 ) | ( 0.0 )   | ( 39.8 )  | ( 0.0 )  |
| AVERAGE     | < 0.0 > | < 0.0 > | < 0.0 > | < 0.0 >  | < 3.0 >  | < 4.4 >  | < 6.3 >  | < 10.5 > | < 3.8 >  | < 0.0 >   | < 8.0 >   | < 0.0 >  |
| 6           | 0.0     | 0.0     | 0.0     | 0.0      | 0.0      | 34.6     | 0.0      | 0.0      | 0.0      | 0.0       | 0.0       | 0.0      |
| 7           | 0.0     | 0.0     | 0.0     | 0.0      | 0.0      | 0.0      | 0.0      | 0.0      | 0.0      | 0.0       | 0.0       | 0.0      |
| 8           | 0.0     | 0.0     | 0.0     | 0.0      | 6.3      | 0.0      | 0.0      | 0.0      | 0.0      | 10.5      | 0.0       | 0.0      |
| 9           | 0.0     | 0.0     | 0.0     | 0.0      | 0.0      | 0.0      | 0.0      | 0.0      | 0.0      | 18.8      | 0.0       | 0.0      |
| 10          | 0.0     | 0.0     | 0.0     | 0.0      | 33.5     | 0.0      | 0.0      | 0.0      | 0.0      | 10.5      | 0.0       | 0.0      |
|             | ( 0.0 ) | ( 0.0 ) | ( 0.0 ) | ( 0.0 )  | ( 39.8 ) | ( 34.6 ) | ( 0.0 )  | ( 0.0 )  | ( 0.0 )  | ( 39.8 )  | ( 0.0 )   | ( 0.0 )  |
| AVERAGE     | < 0.0 > | < 0.0 > | < 0.0 > | < 0.0 >  | < 8.0 >  | < 6.9 >  | < 0.0 >  | < 0.0 >  | < 0.0 >  | < 8.0 >   | < 0.0 >   | < 0.0 >  |
| 11          | 0.0     | 0.0     | 0.0     | 0.0      | 20.9     | 0.0      | 0.0      | 0.0      | 0.0      | 52.3      | 0.0       | 31.4     |
| 12          | 5.2     | 0.0     | 0.0     | 0.0      | 0.0      | 0.0      | 0.0      | 0.0      | 0.0      | 116.2     | 0.0       | 0.0      |
| 13          | 0.0     | 0.0     | 0.0     | 0.0      | 0.0      | 0.0      | 0.0      | 27.2     | 0.0      | 20.9      | 90.0      | 0.0      |
| 14          | 0.0     | 0.0     | 0.0     | 0.0      | 0.0      | 0.0      | 0.0      | 38.7     | 0.0      | 9.4       | 12.6      | 47.1     |
| 15          | 0.0     | 0.0     | 0.0     | 0.0      | 0.0      | 0.0      | 0.0      | 0.0      | 0.0      | 0.0       | 89.0      | 0.0      |
|             | ( 5.2 ) | ( 0.0 ) | ( 0.0 ) | ( 0.0 )  | ( 20.9 ) | ( 0.0 )  | ( 0.0 )  | ( 66.0 ) | ( 0.0 )  | ( 198.9 ) | ( 191.6 ) | ( 78.5 ) |
| AVERAGE     | < 1.0 > | < 0.0 > | < 0.0 > | < 0.0 >  | < 4.2 >  | < 0.0 >  | < 0.0 >  | < 13.2 > | < 0.0 >  | < 39.8 >  | < 38.3 >  | < 15.7 > |
| 16          | 0.0     | 0.0     | 0.0     | 0.0      | 0.0      | 0.0      | 0.0      | 0.0      | 28.3     | 37.7      | 33.5      | 0.0      |
| 17          | 0.0     | 0.0     | 0.0     | 0.0      | 0.0      | 0.0      | 0.0      | 0.0      | 0.0      | 0.0       | 26.2      | 24.1     |
| 18          | 0.0     | 0.0     | 0.0     | 0.0      | 0.0      | 0.0      | 0.0      | 0.0      | 0.0      | 37.7      | 41.9      | 20.9     |
| 19          | 0.0     | 0.0     | 0.0     | 0.0      | 0.0      | 0.0      | 0.0      | 0.0      | 20.9     | 0.0       | 0.0       | 0.0      |
| 20          | 0.0     | 0.0     | 0.0     | 0.0      | 0.0      | 14.7     | 0.0      | 0.0      | 5.2      | 0.0       | 163.3     | 0.0      |
|             | ( 0.0 ) | ( 0.0 ) | ( 0.0 ) | ( 0.0 )  | ( 0.0 )  | ( 14.7 ) | ( 0.0 )  | ( 0.0 )  | ( 54.4 ) | ( 75.4 )  | ( 264.9 ) | ( 45.0 ) |
| AVERAGE     | < 0.0 > | < 0.0 > | < 0.0 > | < 0.0 >  | < 0.0 >  | < 2.9 >  | < 0.0 >  | < 0.0 >  | < 10.9 > | < 15.1 >  | < 53.0 >  | < 9.0 >  |
| 21          | 0.0     | 0.0     | 0.0     | 0.0      | 12.6     | 0.0      | 0.0      | 0.0      | 0.0      | 0.0       | 47.1      | 0.0      |
| 22          | 0.0     | 0.0     | 0.0     | 0.0      | 7.3      | 0.0      | 0.0      | 0.0      | 0.0      | 0.0       | 20.9      | 0.0      |
| 23          | 0.0     | 0.0     | 0.0     | 0.0      | 0.0      | 0.0      | 0.0      | 0.0      | 0.0      | 0.0       | 246.0     | 13.6     |
| 24          | 0.0     | 0.0     | 0.0     | 12.6     | 0.0      | 10.5     | 0.0      | 0.0      | 0.0      | 0.0       | 41.9      | 0.0      |
| 25          | 0.0     | 0.0     | 0.0     | 22.0     | 0.0      | 0.0      | 23.0     | 0.0      | 0.0      | 0.0       | 0.0       | 0.0      |
|             | ( 0.0 ) | ( 0.0 ) | ( 0.0 ) | ( 34.6 ) | ( 19.9 ) | ( 10.5 ) | ( 23.0 ) | ( 0.0 )  | ( 0.0 )  | ( 0.0 )   | ( 356.0 ) | ( 13.6 ) |
| AVERAGE     | < 0.0 > | < 0.0 > | < 0.0 > | < 6.9 >  | < 4.0 >  | < 2.1 >  | < 4.6 >  | < 0.0 >  | < 0.0 >  | < 0.0 >   | < 71.2 >  | < 2.7 >  |
| 26          | 0.0     | 0.0     | 0.0     | 0.0      | 0.0      | 0.0      | 11.5     | 0.0      | 0.0      | 0.0       | 0.0       | 0.0      |
| 27          | 0.0     | 0.0     | 0.0     | 13.6     | 0.0      | 0.0      | 0.0      | 0.0      | 0.0      | 0.0       | 31.4      | 0.0      |
| 28          | 0.0     | 0.0     | 0.0     | 6.3      | 0.0      | 0.0      | 0.0      | 0.0      | 75.4     | 0.0       | 62.8      | 0.0      |
| 29          | 0.0     | 0.0     | 0.0     | 12.6     | 0.0      | 0.0      | 14.7     | 0.0      | 0.0      | 0.0       | 0.0       | 0.0      |
| 30          | 0.0     | 0.0     | 0.0     | 0.0      | 0.0      | 0.0      | 0.0      | 0.0      | 0.0      | 0.0       | 0.0       | 0.0      |
| 31          | 0.0     | 0.0     | 0.0     | 0.0      | 0.0      | 0.0      | 0.0      | 0.0      | 0.0      | 20.9      | 0.0       | 0.0      |
|             | ( 0.0 ) | ( 0.0 ) | ( 0.0 ) | ( 32.5 ) | ( 0.0 )  | ( 0.0 )  | ( 26.2 ) | ( 0.0 )  | ( 75.4 ) | ( 20.9 )  | ( 94.2 )  | ( 0.0 )  |
| AVERAGE     | < 0.0 > | < 0.0 > | < 0.0 > | < 6.5 >  | < 0.0 >  | < 0.0 >  | < 4.4 >  | < 0.0 >  | < 15.1 > | < 3.5 >   | < 18.8 >  | < 0.0 >  |
| GRAND TOTAL | 5.2     | 0.0     | 0.0     | 67.0     | 95.8     | 81.7     | 80.6     | 118.3    | 148.7    | 335.0     | 946.5     | 137.2    |
| AVERAGE     | 0.2     | 0.0     | 0.0     | 2.2      | 3.1      | 2.7      | 2.6      | 3.8      | 5.0      | 10.8      | 31.5      | 4.4      |
| MAX         | 5.2     | 0.0     | 0.0     | 22.0     | 33.5     | 34.6     | 31.4     | 38.7     | 75.4     | 116.2     | 246.0     | 47.1     |
| MIN         | 0.0     | 0.0     | 0.0     | 0.0      | 0.0      | 0.0      | 0.0      | 0.0      | 0.0      | 0.0       | 0.0       | 0.0      |

GAUGED  
DAILY RUNOFF, >  
(1976) >  
T H U N G S A K A  
L A N S A K A

UNIT = (mm/d)

1 1 NOV 1 2 DEC

10 OCT 1 1 NOV 1 2 DEC

9 SEP 10 OCT 1 1 NOV 1 2 DEC

8 AUG 9 SEP 10 OCT 1 1 NOV 1 2 DEC

7 JUL 8 AUG 9 SEP 10 OCT 1 1 NOV 1 2 DEC

6 JUN 7 JUL 8 AUG 9 SEP 10 OCT 1 1 NOV 1 2 DEC

5 MAY 6 JUN 7 JUL 8 AUG 9 SEP 10 OCT 1 1 NOV 1 2 DEC

4 APR 5 MAY 6 JUN 7 JUL 8 AUG 9 SEP 10 OCT 1 1 NOV 1 2 DEC

3 MAR 4 APR 5 MAY 6 JUN 7 JUL 8 AUG 9 SEP 10 OCT 1 1 NOV 1 2 DEC

2 FEB 3 MAR 4 APR 5 MAY 6 JUN 7 JUL 8 AUG 9 SEP 10 OCT 1 1 NOV 1 2 DEC

1 JAN 2 FEB 3 MAR 4 APR 5 MAY 6 JUN 7 JUL 8 AUG 9 SEP 10 OCT 1 1 NOV 1 2 DEC

|         |           |          |          |          |          |          |          |          |          |          |          |           |       |
|---------|-----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|-----------|-------|
| 1       | 2.650     | 1.650    | 1.030    | 0.770    | 1.500    | 1.070    | 0.850    | 0.850    | 0.850    | 1.070    | 1.700    | 11.000    |       |
| 2       | 2.590     | 1.650    | 1.030    | 0.730    | 1.300    | 1.030    | 0.810    | 0.810    | 0.810    | 0.980    | 1.650    | 8.010     |       |
| 3       | 2.470     | 1.650    | 0.980    | 0.730    | 1.210    | 0.980    | 0.810    | 0.810    | 0.810    | 0.940    | 1.700    | 6.170     |       |
| 4       | 2.410     | 1.700    | 0.980    | 0.690    | 1.070    | 0.980    | 0.810    | 0.810    | 0.810    | 0.890    | 1.650    | 5.250     |       |
| 5       | 2.350     | 1.600    | 1.030    | 0.650    | 2.590    | 1.070    | 1.750    | 1.750    | 1.750    | 1.750    | 1.600    | 4.500     |       |
| AVERAGE | ( 12.470) | ( 8.250) | ( 5.050) | ( 3.570) | ( 7.670) | ( 5.130) | ( 5.030) | ( 5.030) | ( 5.030) | ( 4.730) | ( 8.300) | ( 34.930) |       |
| <       | 2.494     | <        | 1.650    | <        | 1.534    | <        | 1.006    | <        | 1.006    | <        | 1.660    | <         | 6.986 |

|         |           |          |          |          |          |          |          |          |          |          |          |           |       |
|---------|-----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|-----------|-------|
| 6       | 2.290     | 1.700    | 1.030    | 0.650    | 1.450    | 1.030    | 1.350    | 1.350    | 1.350    | 0.810    | 1.550    | 4.000     |       |
| 7       | 2.180     | 1.600    | 1.300    | 0.610    | 1.210    | 1.960    | 1.300    | 1.300    | 1.300    | 0.810    | 2.350    | 3.580     |       |
| 8       | 2.130     | 1.650    | 1.030    | 0.570    | 1.250    | 2.240    | 1.700    | 1.700    | 1.700    | 0.770    | 1.910    | 3.300     |       |
| 9       | 3.020     | 1.500    | 1.030    | 0.890    | 1.250    | 1.700    | 1.500    | 1.500    | 1.500    | 0.770    | 1.700    | 3.300     |       |
| 10      | 2.470     | 1.450    | 0.980    | 0.690    | 1.550    | 1.550    | 1.300    | 1.300    | 1.300    | 0.730    | 1.550    | 3.020     |       |
| AVERAGE | ( 12.090) | ( 7.900) | ( 5.370) | ( 3.410) | ( 6.710) | ( 8.480) | ( 7.150) | ( 7.150) | ( 7.150) | ( 3.890) | ( 9.060) | ( 17.200) |       |
| <       | 2.418     | <        | 1.580    | <        | 1.342    | <        | 1.430    | <        | 1.430    | <        | 1.812    | <         | 3.440 |

|         |           |          |          |          |           |          |          |          |          |           |           |           |       |
|---------|-----------|----------|----------|----------|-----------|----------|----------|----------|----------|-----------|-----------|-----------|-------|
| 11      | 2.410     | 1.450    | 0.980    | 0.650    | 2.070     | 1.450    | 1.120    | 1.120    | 1.120    | 1.100     | 1.500     | 2.950     |       |
| 12      | 2.240     | 1.450    | 0.980    | 0.610    | 2.650     | 1.500    | 1.070    | 1.070    | 1.070    | 0.910     | 3.020     | 5.700     |       |
| 13      | 2.180     | 1.400    | 0.940    | 1.600    | 2.770     | 1.550    | 1.030    | 1.030    | 1.030    | 10.000    | 7.750     | 12.000    |       |
| 14      | 2.180     | 1.400    | 0.940    | 0.810    | 2.070     | 1.210    | 0.980    | 0.980    | 0.980    | 0.980     | 5.550     | 6.490     |       |
| 15      | 2.130     | 1.400    | 0.940    | 0.690    | 2.290     | 1.160    | 0.940    | 0.940    | 0.940    | 3.650     | 7.410     | 12.000    |       |
| AVERAGE | ( 11.140) | ( 7.100) | ( 4.780) | ( 4.360) | ( 11.850) | ( 6.870) | ( 5.140) | ( 5.140) | ( 5.140) | ( 29.460) | ( 26.170) | ( 44.650) |       |
| <       | 2.228     | <        | 1.420    | <        | 2.370     | <        | 1.028    | <        | 1.028    | <         | 5.892     | <         | 8.930 |

|         |          |          |          |          |          |          |          |          |          |           |           |           |       |
|---------|----------|----------|----------|----------|----------|----------|----------|----------|----------|-----------|-----------|-----------|-------|
| 16      | 2.070    | 1.350    | 0.890    | 0.650    | 1.800    | 1.120    | 0.890    | 0.890    | 0.890    | 3.790     | 8.600     | 3.020     |       |
| 17      | 2.020    | 1.300    | 0.890    | 0.650    | 1.550    | 1.120    | 0.850    | 0.850    | 0.850    | 5.620     | 5.530     | 5.470     |       |
| 18      | 1.960    | 1.250    | 0.850    | 0.650    | 1.400    | 1.070    | 0.810    | 0.810    | 0.810    | 4.280     | 8.260     | 9.970     |       |
| 19      | 1.910    | 1.250    | 0.850    | 0.730    | 2.070    | 1.210    | 0.770    | 0.770    | 0.770    | 4.800     | 12.000    | 7.070     |       |
| 20      | 1.910    | 1.210    | 0.850    | 0.690    | 2.020    | 1.070    | 0.940    | 0.940    | 0.940    | 3.580     | 13.000    | 4.720     |       |
| AVERAGE | ( 9.870) | ( 6.360) | ( 4.330) | ( 3.370) | ( 8.840) | ( 5.590) | ( 4.260) | ( 4.260) | ( 4.260) | ( 22.070) | ( 47.590) | ( 30.250) |       |
| <       | 1.974    | <        | 1.272    | <        | 1.768    | <        | 1.118    | <        | 1.118    | <         | 9.518     | <         | 6.050 |

|         |          |          |          |          |          |          |          |          |          |           |            |           |       |
|---------|----------|----------|----------|----------|----------|----------|----------|----------|----------|-----------|------------|-----------|-------|
| 21      | 1.850    | 1.210    | 1.350    | 0.650    | 2.020    | 1.030    | 0.850    | 0.850    | 0.850    | 3.440     | 38.000     | 3.930     |       |
| 22      | 1.850    | 1.160    | 1.070    | 0.650    | 2.070    | 0.980    | 0.850    | 0.850    | 0.850    | 2.650     | 21.000     | 3.440     |       |
| 23      | 1.800    | 1.160    | 1.030    | 0.650    | 1.850    | 0.980    | 0.850    | 0.850    | 0.850    | 2.290     | 45.000     | 3.160     |       |
| 24      | 1.800    | 1.120    | 0.980    | 1.400    | 1.700    | 0.940    | 0.980    | 0.980    | 0.980    | 2.180     | 71.000     | 3.020     |       |
| 25      | 1.910    | 1.120    | 0.940    | 1.350    | 1.550    | 0.940    | 1.120    | 1.120    | 1.120    | 2.130     | 24.000     | 2.830     |       |
| AVERAGE | ( 9.210) | ( 5.770) | ( 5.370) | ( 4.700) | ( 9.190) | ( 4.870) | ( 4.650) | ( 4.650) | ( 4.650) | ( 12.690) | ( 199.000) | ( 16.380) |       |
| <       | 1.842    | <        | 1.154    | <        | 1.838    | <        | 0.930    | <        | 0.930    | <         | 39.800     | <         | 3.276 |

|         |           |          |          |          |          |          |          |          |          |           |           |           |       |
|---------|-----------|----------|----------|----------|----------|----------|----------|----------|----------|-----------|-----------|-----------|-------|
| 26      | 1.800     | 1.120    | 0.890    | 1.600    | 1.450    | 0.890    | 1.030    | 1.030    | 1.030    | 2.020     | 12.000    | 2.650     |       |
| 27      | 1.800     | 1.070    | 0.850    | 1.450    | 1.350    | 0.890    | 0.980    | 0.980    | 0.980    | 1.910     | 9.160     | 2.470     |       |
| 28      | 1.750     | 1.070    | 0.810    | 1.700    | 1.250    | 0.890    | 0.890    | 0.890    | 0.890    | 2.350     | 8.890     | 2.470     |       |
| 29      | 1.700     | 1.030    | 0.810    | 1.350    | 1.160    | 0.850    | 0.850    | 0.850    | 0.850    | 1.850     | 11.000    | 2.290     |       |
| 30      | 1.700     | 1.030    | 0.770    | 1.800    | 1.120    | 0.850    | 0.810    | 0.810    | 0.810    | 1.700     | 28.000    | 2.130     |       |
| 31      | 1.650     | 1.030    | 0.770    | 1.800    | 1.120    | 0.850    | 0.810    | 0.810    | 0.810    | 1.800     | 28.000    | 3.510     |       |
| AVERAGE | ( 10.400) | ( 4.290) | ( 4.900) | ( 7.900) | ( 7.400) | ( 4.370) | ( 4.560) | ( 4.560) | ( 4.560) | ( 11.630) | ( 69.050) | ( 15.520) |       |
| <       | 1.733     | <        | 1.072    | <        | 1.233    | <        | 0.874    | <        | 0.874    | <         | 13.810    | <         | 2.587 |

|             |        |        |        |        |        |        |        |        |        |        |         |         |
|-------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|---------|---------|
| GRAND TOTAL | 65.180 | 39.670 | 29.800 | 27.310 | 51.660 | 35.310 | 30.790 | 30.790 | 30.790 | 86.470 | 359.170 | 158.930 |
| AVERAGE     | 144.   | 88.    | 66.    | 61.    | 114.   | 78.    | 68.    | 68.    | 68.    | 187.   | 796.    | 352.    |
| MAX         | 2.103  | 1.368  | 0.961  | 0.910  | 1.666  | 1.177  | 0.993  | 0.993  | 0.993  | 2.725  | 11.972  | 5.127   |
| MIN         | 3.020  | 1.700  | 1.350  | 1.800  | 2.770  | 2.240  | 1.750  | 1.750  | 1.750  | 10.000 | 71.000  | 12.000  |
|             | 1.650  | 1.030  | 0.770  | 0.570  | 1.070  | 0.850  | 0.0    | 0.0    | 0.0    | 0.770  | 1.500   | 2.130   |

COMPUTED

< DAILY RUNOFF (1976) > THUNG SONG LAN SAKA

UNIT = (mm/D)

|             | 1 JAN      | 2 FEB     | 3 MAR     | 4 APR     | 5 MAY      | 6 JUN     | 7 JUL     | 8 AUG      | 9 SEP     | 10 OCT     | 11 NOV      | 12 DEC     |
|-------------|------------|-----------|-----------|-----------|------------|-----------|-----------|------------|-----------|------------|-------------|------------|
| 1           | 4.586      | 0.151     | 0.027     | 0.012     | 1.072      | 0.413     | 0.336     | 0.859      | 0.397     | 2.272      | 2.079       | 11.103     |
| 2           | 4.100      | 0.135     | 0.026     | 0.012     | 0.996      | 1.000     | 0.301     | 2.358      | 1.058     | 2.045      | 1.789       | 9.879      |
| 3           | 3.665      | 0.121     | 0.026     | 0.011     | 0.912      | 0.270     | 0.270     | 2.555      | 0.790     | 1.864      | 1.639       | 8.860      |
| 4           | 3.276      | 0.108     | 0.025     | 0.011     | 1.360      | 0.716     | 0.241     | 2.414      | 0.673     | 1.694      | 2.739       | 7.956      |
| 5           | 2.929      | 0.096     | 0.024     | 0.011     | 1.060      | 0.680     | 1.656     | 1.834      | 0.636     | 1.531      | 3.067       | 7.132      |
| AVERAGE     | < 18.556 > | < 0.611 > | < 0.129 > | < 0.057 > | < 5.400 >  | < 3.726 > | < 2.804 > | < 9.719 >  | < 3.554 > | < 9.406 >  | < 11.313 >  | < 44.930 > |
|             | < 3.711 >  | < 0.122 > | < 0.026 > | < 0.011 > | < 1.080 >  | < 0.745 > | < 0.561 > | < 1.944 >  | < 0.711 > | < 1.881 >  | < 2.263 >   | < 8.986 >  |
| 6           | 2.618      | 0.086     | 0.024     | 0.011     | 0.954      | 2.364     | 1.200     | 1.620      | 0.588     | 1.378      | 2.487       | 6.388      |
| 7           | 2.341      | 0.080     | 0.023     | 0.010     | 0.880      | 1.754     | 0.893     | 1.484      | 0.537     | 1.237      | 2.062       | 5.718      |
| 8           | 2.092      | 0.075     | 0.023     | 0.010     | 0.939      | 1.326     | 0.828     | 1.355      | 0.487     | 1.427      | 1.871       | 5.115      |
| 9           | 1.870      | 0.071     | 0.022     | 0.010     | 0.795      | 1.210     | 0.774     | 1.227      | 0.439     | 2.142      | 1.708       | 4.575      |
| 10          | 1.672      | 0.067     | 0.021     | 0.009     | 2.367      | 1.120     | 0.711     | 1.107      | 0.395     | 2.321      | 1.548       | 4.091      |
| AVERAGE     | < 10.594 > | < 0.379 > | < 0.113 > | < 0.050 > | < 5.934 >  | < 7.774 > | < 4.406 > | < 6.792 >  | < 2.446 > | < 8.505 >  | < 9.677 >   | < 25.888 > |
|             | < 2.119 >  | < 0.076 > | < 0.023 > | < 0.010 > | < 1.187 >  | < 1.555 > | < 0.881 > | < 1.358 >  | < 0.489 > | < 1.701 >  | < 1.935 >   | < 5.178 >  |
| 11          | 1.495      | 0.063     | 0.021     | 0.009     | 3.085      | 1.024     | 0.647     | 0.995      | 0.354     | 5.806      | 1.396       | 5.156      |
| 12          | 1.456      | 0.060     | 0.020     | 0.009     | 2.401      | 0.929     | 0.585     | 0.892      | 0.317     | 17.468     | 1.255       | 4.380      |
| 13          | 1.255      | 0.056     | 0.020     | 0.009     | 1.853      | 0.838     | 0.527     | 1.977      | 0.284     | 10.109     | 9.329       | 3.727      |
| 14          | 1.130      | 0.053     | 0.019     | 0.009     | 1.681      | 0.753     | 0.473     | 4.295      | 0.254     | 8.202      | 5.612       | 6.464      |
| 15          | 1.015      | 0.050     | 0.019     | 0.008     | 1.540      | 0.676     | 0.424     | 2.968      | 0.227     | 6.767      | 13.767      | 4.953      |
| AVERAGE     | < 6.350 >  | < 0.282 > | < 0.099 > | < 0.044 > | < 10.560 > | < 4.220 > | < 2.657 > | < 11.127 > | < 1.435 > | < 48.351 > | < 31.360 >  | < 24.679 > |
|             | < 1.270 >  | < 0.056 > | < 0.020 > | < 0.008 > | < 2.112 >  | < 0.844 > | < 0.531 > | < 2.225 >  | < 0.287 > | < 9.670 >  | < 6.272 >   | < 4.936 >  |
| 16          | 0.910      | 0.047     | 0.018     | 0.008     | 1.403      | 0.606     | 0.380     | 2.278      | 1.476     | 8.188      | 10.488      | 4.124      |
| 17          | 0.815      | 0.045     | 0.018     | 0.008     | 1.270      | 0.542     | 0.340     | 1.982      | 1.074     | 6.668      | 9.795       | 4.924      |
| 18          | 0.730      | 0.042     | 0.017     | 0.008     | 1.144      | 0.485     | 0.304     | 1.802      | 0.814     | 8.200      | 11.072      | 5.412      |
| 19          | 0.653      | 0.040     | 0.017     | 0.007     | 1.028      | 0.434     | 0.272     | 1.645      | 1.725     | 6.645      | 8.534       | 4.524      |
| 20          | 0.584      | 0.037     | 0.016     | 0.007     | 0.922      | 0.365     | 0.243     | 1.490      | 1.612     | 5.605      | 26.299      | 3.780      |
| AVERAGE     | < 3.692 >  | < 0.211 > | < 0.087 > | < 0.038 > | < 5.767 >  | < 2.935 > | < 1.538 > | < 9.197 >  | < 6.700 > | < 35.307 > | < 66.188 >  | < 22.763 > |
|             | < 0.758 >  | < 0.042 > | < 0.015 > | < 0.008 > | < 1.153 >  | < 0.587 > | < 0.308 > | < 1.839 >  | < 1.340 > | < 7.061 >  | < 13.238 >  | < 4.553 >  |
| 21          | 0.522      | 0.035     | 0.016     | 0.007     | 1.223      | 0.612     | 0.217     | 1.343      | 1.242     | 4.929      | 18.794      | 3.390      |
| 22          | 0.467      | 0.034     | 0.016     | 0.007     | 1.289      | 0.565     | 0.194     | 1.207      | 1.126     | 4.434      | 14.711      | 3.067      |
| 23          | 0.417      | 0.033     | 0.015     | 0.007     | 1.017      | 0.527     | 0.173     | 1.083      | 1.043     | 4.000      | 43.182      | 3.274      |
| 24          | 0.373      | 0.032     | 0.015     | 0.007     | 0.947      | 0.477     | 0.155     | 0.970      | 0.953     | 3.596      | 26.711      | 2.809      |
| 25          | 0.333      | 0.031     | 0.014     | 0.007     | 0.869      | 0.434     | 0.137     | 0.869      | 0.864     | 3.227      | 18.891      | 2.507      |
| AVERAGE     | < 2.111 >  | < 0.164 > | < 0.076 > | < 0.031 > | < 5.346 >  | < 3.067 > | < 1.806 > | < 5.473 >  | < 5.227 > | < 20.185 > | < 122.289 > | < 15.048 > |
|             | < 0.422 >  | < 0.033 > | < 0.015 > | < 0.012 > | < 1.069 >  | < 0.613 > | < 0.361 > | < 1.095 >  | < 1.045 > | < 4.037 >  | < 24.458 >  | < 3.010 >  |
| 26          | 0.298      | 0.030     | 0.014     | 0.011     | 0.789      | 0.548     | 1.408     | 0.777      | 0.779     | 2.892      | 16.043      | 2.270      |
| 27          | 0.266      | 0.029     | 0.014     | 0.010     | 0.713      | 0.504     | 0.972     | 0.695      | 0.700     | 2.589      | 15.795      | 2.046      |
| 28          | 0.238      | 0.029     | 0.013     | 0.010     | 0.642      | 0.459     | 0.843     | 0.622      | 0.622     | 2.317      | 19.519      | 1.839      |
| 29          | 0.212      | 0.028     | 0.013     | 0.010     | 0.576      | 0.415     | 1.328     | 0.556      | 0.556     | 2.073      | 14.785      | 1.650      |
| 30          | 0.190      | 0.027     | 0.013     | 0.010     | 0.516      | 0.374     | 1.023     | 0.497      | 0.497     | 1.854      | 12.759      | 1.478      |
| 31          | 0.169      | 0.026     | 0.012     | 0.010     | 0.462      | 0.334     | 0.927     | 0.444      | 0.444     | 1.654      | 11.523      | 1.323      |
| AVERAGE     | < 1.372 >  | < 0.116 > | < 0.070 > | < 0.030 > | < 3.698 >  | < 2.301 > | < 6.502 > | < 3.590 >  | < 3.590 > | < 14.221 > | < 78.702 >  | < 10.606 > |
|             | < 0.229 >  | < 0.029 > | < 0.013 > | < 0.012 > | < 0.616 >  | < 0.460 > | < 1.084 > | < 0.598 >  | < 0.598 > | < 2.916 >  | < 15.740 >  | < 1.768 >  |
| GRAND TOTAL | 42.676     | 1.763     | 0.584     | 7.881     | 36.705     | 26.023    | 19.713    | 45.898     | 33.944    | 135.975    | 319.527     | 143.913    |
| AVERAGE     | 95.        | 4.        | 1.        | 17.       | 81.        | 53.       | 44.       | 102.       | 75.       | 301.       | 708.        | 319.       |
| MAX         | 1.377      | 0.061     | 0.019     | 0.263     | 1.184      | 0.801     | 0.636     | 1.481      | 1.131     | 4.386      | 10.651      | 4.642      |
| MIN         | 4.586      | 0.151     | 0.027     | 1.604     | 3.085      | 2.364     | 1.636     | 4.295      | 6.712     | 17.468     | 43.182      | 11.103     |
|             | 0.169      | 0.028     | 0.012     | 0.007     | 0.462      | 0.374     | 0.155     | 0.444      | 0.227     | 1.237      | 1.255       | 1.323      |

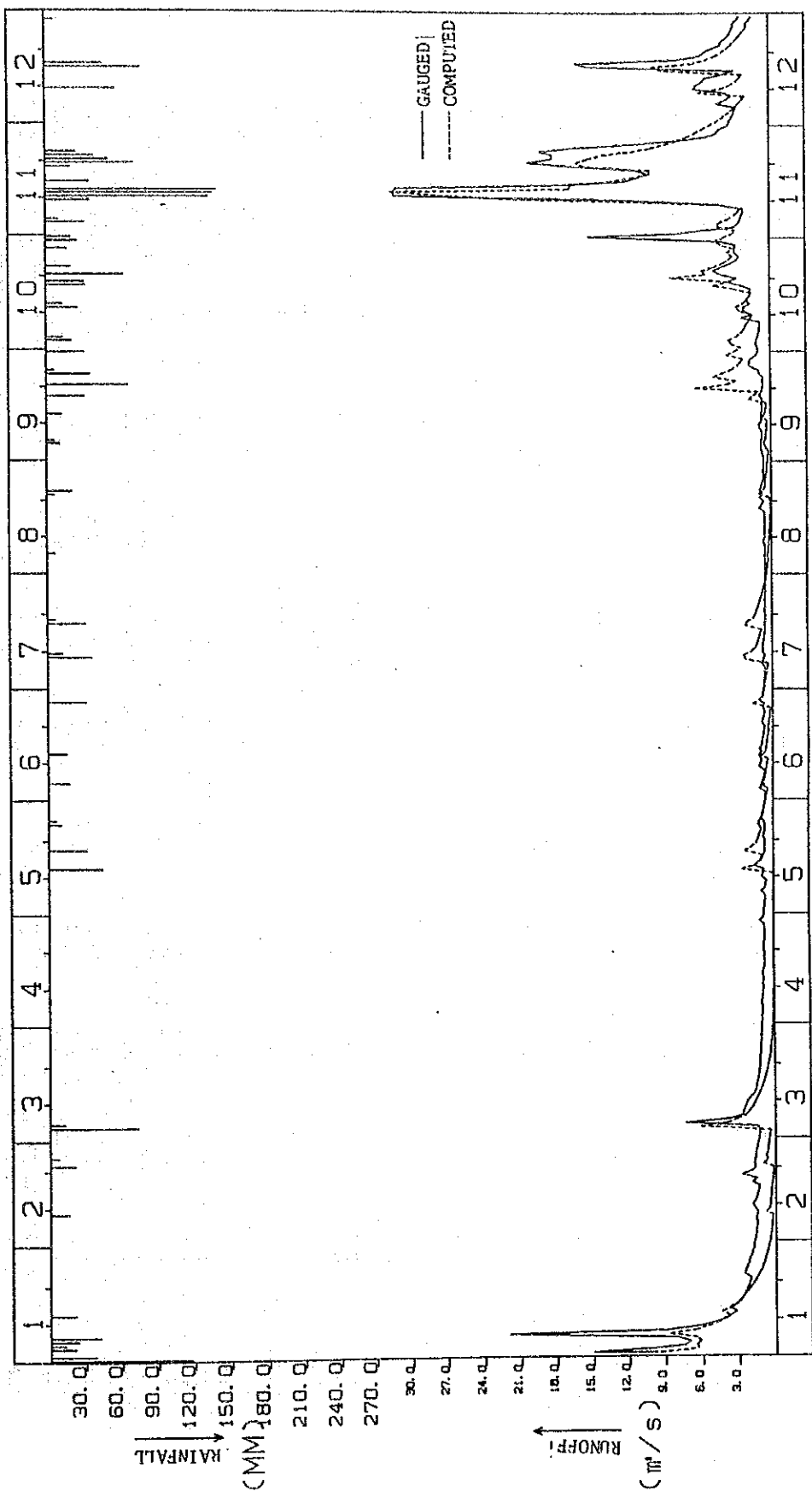


RUNOFF ANALYSIS BY TANK MODEL

(1977)

RAINFALL STATION: LAN SAKA

COEFFICIENT = 0.9027



GAUGING STATION: X-70 ( CA = 39.00km )

UNIT = (mm/D)

< DAILY RAINFALL > THUNG SONG  
(1977) > LAN SAKA

|             | 1 JAN    | 2 FEB    | 3 MAR    | 4 APR   | 5 MAY    | 6 JUN    | 7 JUL    | 8 AUG    | 9 SEP     | 10 OCT   | 11 NOV    | 12 DEC    |
|-------------|----------|----------|----------|---------|----------|----------|----------|----------|-----------|----------|-----------|-----------|
| 1           | 117.3    | 0.0      | 0.0      | 0.0     | 0.0      | 0.0      | 0.0      | 0.0      | 0.0       | 0.0      | 0.0       | 0.0       |
| 2           | 37.7     | 0.0      | 0.0      | 0.0     | 0.0      | 0.0      | 0.0      | 0.0      | 0.0       | 0.0      | 0.0       | 0.0       |
| 3           | 0.0      | 0.0      | 0.0      | 0.0     | 0.0      | 0.0      | 0.0      | 0.0      | 0.0       | 20.9     | 0.0       | 0.0       |
| 4           | 20.9     | 0.0      | 73.3     | 0.0     | 0.0      | 0.0      | 0.0      | 0.0      | 0.0       | 13.6     | 32.5      | 0.0       |
| 5           | 12.6     | 0.0      | 12.6     | 0.0     | 0.0      | 17.8     | 0.0      | 0.0      | 10.5      | 0.0      | 10.5      | 0.0       |
| AVERAGE     | < 37.7 > | < 0.0 >  | < 17.2 > | < 0.0 > | < 0.0 >  | < 3.6 >  | < 0.0 >  | < 0.0 >  | < 2.1 >   | < 6.9 >  | < 8.6 >   | < 0.0 >   |
| 6           | 23.0     | 0.0      | 0.0      | 0.0     | 0.0      | 0.0      | 0.0      | 6.3      | 6.3       | 0.0      | 0.0       | 0.0       |
| 7           | 41.9     | 0.0      | 0.0      | 0.0     | 0.0      | 0.0      | 0.0      | 0.0      | 0.0       | 0.0      | 0.0       | 0.0       |
| 8           | 0.0      | 0.0      | 0.0      | 0.0     | 0.0      | 0.0      | 0.0      | 0.0      | 0.0       | 0.0      | 0.0       | 0.0       |
| 9           | 0.0      | 15.7     | 0.0      | 0.0     | 0.0      | 0.0      | 36.6     | 0.0      | 0.0       | 0.0      | 0.0       | 0.0       |
| 10          | 0.0      | 0.0      | 0.0      | 0.0     | 0.0      | 0.0      | 12.6     | 0.0      | 0.0       | 0.0      | 36.6      | 58.6      |
| AVERAGE     | < 64.9 > | < 15.7 > | < 0.0 >  | < 0.0 > | < 0.0 >  | < 0.0 >  | < 49.2 > | < 6.3 >  | < 6.3 >   | < 0.0 >  | < 36.6 >  | < 58.6 >  |
| 11          | 0.0      | 0.0      | 0.0      | 0.0     | 0.0      | 0.0      | 0.0      | 0.0      | 0.0       | 0.0      | 135.1     | 0.0       |
| 12          | 0.0      | 0.0      | 0.0      | 0.0     | 0.0      | 0.0      | 0.0      | 0.0      | 0.0       | 26.2     | 138.2     | 0.0       |
| 13          | 20.9     | 0.0      | 0.0      | 0.0     | 45.0     | 15.7     | 0.0      | 0.0      | 12.6      | 13.6     | 141.3     | 0.0       |
| 14          | 0.0      | 0.0      | 0.0      | 0.0     | 0.0      | 0.0      | 0.0      | 0.0      | 0.0       | 0.0      | 0.0       | 0.0       |
| 15          | 0.0      | 0.0      | 0.0      | 0.0     | 0.0      | 0.0      | 0.0      | 0.0      | 0.0       | 0.0      | 36.6      | 0.0       |
| AVERAGE     | < 20.9 > | < 0.0 >  | < 0.0 >  | < 0.0 > | < 45.0 > | < 15.7 > | < 0.0 >  | < 0.0 >  | < 12.6 >  | < 39.8 > | < 451.3 > | < 0.0 >   |
| 16          | 0.0      | 0.0      | 0.0      | 0.0     | 0.0      | 0.0      | 0.0      | 0.0      | 0.0       | 0.0      | 0.0       | 79.6      |
| 17          | 0.0      | 0.0      | 0.0      | 0.0     | 0.0      | 0.0      | 0.0      | 0.0      | 0.0       | 0.0      | 0.0       | 48.2      |
| 18          | 0.0      | 0.0      | 0.0      | 0.0     | 31.4     | 0.0      | 31.4     | 0.0      | 31.4      | 32.5     | 0.0       | 0.0       |
| 19          | 0.0      | 0.0      | 0.0      | 0.0     | 0.0      | 0.0      | 6.3      | 0.0      | 0.0       | 31.4     | 20.9      | 0.0       |
| 20          | 0.0      | 0.0      | 0.0      | 0.0     | 0.0      | 0.0      | 0.0      | 0.0      | 0.0       | 0.0      | 73.3      | 0.0       |
| AVERAGE     | < 0.0 >  | < 0.0 >  | < 0.0 >  | < 0.0 > | < 31.4 > | < 0.0 >  | < 37.7 > | < 0.0 >  | < 31.4 >  | < 63.9 > | < 94.2 >  | < 127.7 > |
| 21          | 0.0      | 0.0      | 0.0      | 0.0     | 0.0      | 0.0      | 0.0      | 0.0      | 68.1      | 64.9     | 52.3      | 0.0       |
| 22          | 0.0      | 20.9     | 0.0      | 0.0     | 0.0      | 0.0      | 0.0      | 6.3      | 0.0       | 0.0      | 39.8      | 0.0       |
| 23          | 0.0      | 0.0      | 0.0      | 0.0     | 0.0      | 0.0      | 0.0      | 20.9     | 0.0       | 20.9     | 25.1      | 0.0       |
| 24          | 0.0      | 7.3      | 0.0      | 0.0     | 0.0      | 0.0      | 0.0      | 0.0      | 36.6      | 0.0      | 0.0       | 0.0       |
| 25          | 0.0      | 0.0      | 0.0      | 0.0     | 10.5     | 0.0      | 0.0      | 0.0      | 6.3       | 0.0      | 0.0       | 0.0       |
| AVERAGE     | < 0.0 >  | < 28.3 > | < 0.0 >  | < 0.0 > | < 10.5 > | < 0.0 >  | < 0.0 >  | < 27.2 > | < 111.0 > | < 85.9 > | < 117.3 > | < 0.0 >   |
| 26          | 0.0      | 0.0      | 0.0      | 0.0     | 6.3      | 0.0      | 0.0      | 0.0      | 0.0       | 0.0      | 0.0       | 0.0       |
| 27          | 0.0      | 0.0      | 0.0      | 0.0     | 0.0      | 31.4     | 0.0      | 0.0      | 0.0       | 0.0      | 0.0       | 0.0       |
| 28          | 0.0      | 0.0      | 0.0      | 0.0     | 0.0      | 0.0      | 0.0      | 0.0      | 0.0       | 17.8     | 0.0       | 0.0       |
| 29          | 0.0      | 0.0      | 0.0      | 0.0     | 0.0      | 0.0      | 0.0      | 0.0      | 0.0       | 0.0      | 0.0       | 7.3       |
| 30          | 0.0      | 0.0      | 0.0      | 0.0     | 0.0      | 0.0      | 0.0      | 0.0      | 31.4      | 26.2     | 0.0       | 0.0       |
| 31          | 0.0      | 0.0      | 0.0      | 0.0     | 0.0      | 0.0      | 0.0      | 0.0      | 0.0       | 0.0      | 0.0       | 0.0       |
| AVERAGE     | < 0.0 >  | < 0.0 >  | < 0.0 >  | < 0.0 > | < 6.3 >  | < 31.4 > | < 0.0 >  | < 0.0 >  | < 31.4 >  | < 64.9 > | < 0.0 >   | < 7.3 >   |
| GRAND TOTAL | 274.3    | 44.0     | 85.9     | 0.0     | 93.2     | 64.9     | 86.9     | 33.5     | 203.1     | 289.0    | 742.3     | 193.7     |
| AVERAGE     | 8.8      | 1.6      | 2.8      | 0.0     | 3.0      | 2.2      | 2.8      | 1.1      | 6.8       | 9.3      | 24.7      | 6.2       |
| MAX         | 117.3    | 20.9     | 73.3     | 0.0     | 45.0     | 31.4     | 36.6     | 20.9     | 68.1      | 64.9     | 141.3     | 79.6      |
| MIN         | 0.0      | 0.0      | 0.0      | 0.0     | 0.0      | 0.0      | 0.0      | 0.0      | 0.0       | 0.0      | 0.0       | 0.0       |

GAUGED  
DAILY RUNOFF  
(1977)

THUNG SONG  
LAN SAKA

UNIT = (mm/D)

1 JAN 2 FEB 3 MAR 4 APR 5 MAY 6 JUN 7 JUL 8 AUG 9 SEP 10 OCT 11 NOV 12 DEC

|             |            |           |            |           |           |           |           |           |           |            |             |            |          |
|-------------|------------|-----------|------------|-----------|-----------|-----------|-----------|-----------|-----------|------------|-------------|------------|----------|
| 1           | 9.970      | 1.750     | 1.350      | 1.070     | 0.810     | 0.650     | 0.730     | 0.530     | 0.610     | 1.030      | 15.000      | 3.440      |          |
| 2           | 15.000     | 1.700     | 1.300      | 1.030     | 0.850     | 0.650     | 0.690     | 0.530     | 0.610     | 1.070      | 7.670       | 3.300      |          |
| 3           | 10.000     | 1.600     | 1.300      | 1.030     | 0.770     | 0.610     | 0.650     | 0.530     | 0.730     | 1.210      | 5.470       | 3.160      |          |
| 4           | 7.410      | 1.600     | 1.450      | 0.980     | 0.770     | 1.120     | 0.650     | 0.530     | 0.810     | 1.120      | 2.950       | 2.950      |          |
| 5           | 7.070      | 1.550     | 7.330      | 0.980     | 0.730     | 0.770     | 0.610     | 0.530     | 0.810     | 1.030      | 2.590       | 2.830      |          |
|             | < 49.450 > | < 8.200 > | < 12.730 > | < 5.090 > | < 3.930 > | < 3.800 > | < 3.330 > | < 2.650 > | < 3.570 > | < 5.460 >  | < 33.680 >  | < 15.680 > |          |
| AVERAGE     | < 9.890 >  | < 1.640 > | < 2.546 >  | < 1.018 > | < 0.786 > | < 0.760 > | < 0.666 > | < 0.530 > | < 0.714 > | < 1.092 >  | < 6.736 >   | < 3.136 >  |          |
| 6           | 8.090      | 1.500     | 3.790      | 0.980     | 0.730     | 0.890     | 0.610     | 0.570     | 0.810     | 0.940      | 2.410       | 2.710      |          |
| 7           | 22.000     | 1.600     | 2.650      | 1.070     | 1.030     | 0.770     | 0.610     | 0.530     | 0.770     | 0.890      | 2.390       | 4.280      |          |
| 8           | 8.980      | 1.550     | 2.590      | 0.980     | 0.730     | 0.730     | 0.890     | 0.530     | 0.730     | 0.850      | 2.180       | 3.580      |          |
| 9           | 6.410      | 1.450     | 2.470      | 0.940     | 0.650     | 0.690     | 0.690     | 0.570     | 0.770     | 0.850      | 2.180       | 3.090      |          |
| 10          | 5.020      | 1.700     | 2.350      | 0.940     | 0.610     | 1.160     | 0.650     | 0.690     | 0.890     | 2.350      | 4.420       | 3.650      |          |
|             | < 50.500 > | < 7.800 > | < 13.850 > | < 4.910 > | < 3.750 > | < 4.240 > | < 3.450 > | < 2.890 > | < 3.970 > | < 5.880 >  | < 13.480 >  | < 17.310 > |          |
| AVERAGE     | < 10.100 > | < 1.560 > | < 2.770 >  | < 0.982 > | < 0.750 > | < 0.848 > | < 0.690 > | < 0.578 > | < 0.794 > | < 1.176 >  | < 2.696 >   | < 3.462 >  |          |
| 11          | 4.140      | 1.910     | 2.240      | 0.890     | 0.980     | 0.980     | 0.810     | 0.530     | 0.980     | 1.500      | 13.000      | 6.170      |          |
| 12          | 3.720      | 1.650     | 1.960      | 0.940     | 0.890     | 0.940     | 0.810     | 0.570     | 0.770     | 2.180      | 48.000      | 6.010      |          |
| 13          | 3.300      | 1.550     | 1.700      | 0.890     | 0.810     | 1.160     | 0.770     | 0.570     | 0.810     | 2.180      | 59.000      | 5.470      |          |
| 14          | 3.860      | 1.450     | 1.550      | 0.890     | 1.600     | 0.940     | 0.690     | 0.570     | 0.770     | 1.650      | 31.000      | 5.320      |          |
| 15          | 3.160      | 1.400     | 1.500      | 0.980     | 1.210     | 1.120     | 0.650     | 0.570     | 0.730     | 1.960      | 17.000      | 3.930      |          |
|             | < 18.180 > | < 7.960 > | < 8.950 >  | < 4.590 > | < 5.490 > | < 5.140 > | < 3.730 > | < 2.810 > | < 4.060 > | < 9.470 >  | < 168.000 > | < 26.900 > |          |
| AVERAGE     | < 5.636 >  | < 1.592 > | < 1.790 >  | < 0.918 > | < 1.098 > | < 1.028 > | < 0.746 > | < 0.562 > | < 0.812 > | < 1.894 >  | < 33.600 >  | < 5.380 >  |          |
| 16          | 2.890      | 1.350     | 1.450      | 0.850     | 0.980     | 0.890     | 0.610     | 0.570     | 0.730     | 1.650      | 12.000      | 2.890      |          |
| 17          | 2.690      | 1.910     | 1.400      | 0.810     | 0.810     | 0.890     | 0.570     | 0.570     | 0.810     | 1.650      | 11.000      | 15.000     |          |
| 18          | 2.530      | 1.550     | 1.350      | 0.770     | 0.730     | 0.810     | 0.610     | 0.570     | 0.730     | 1.600      | 10.000      | 16.000     |          |
| 19          | 2.410      | 2.770     | 1.300      | 0.850     | 0.770     | 0.770     | 0.570     | 1.030     | 0.940     | 2.240      | 11.000      | 7.670      |          |
| 20          | 2.240      | 1.910     | 1.250      | 0.810     | 0.730     | 0.730     | 0.570     | 0.810     | 0.770     | 3.510      | 16.000      | 5.700      |          |
|             | < 12.720 > | < 9.490 > | < 6.750 >  | < 4.090 > | < 4.020 > | < 4.090 > | < 2.930 > | < 3.550 > | < 3.980 > | < 10.650 > | < 60.000 >  | < 47.260 > |          |
| AVERAGE     | < 2.544 >  | < 1.898 > | < 1.350 >  | < 0.818 > | < 0.804 > | < 0.818 > | < 0.586 > | < 0.710 > | < 0.796 > | < 2.130 >  | < 42.000 >  | < 9.452 >  |          |
| 21          | 2.130      | 1.650     | 1.250      | 0.850     | 0.690     | 0.650     | 0.570     | 0.650     | 0.650     | 2.770      | 20.000      | 5.320      |          |
| 22          | 2.030      | 1.750     | 1.250      | 0.850     | 0.850     | 0.890     | 0.610     | 0.980     | 0.610     | 4.070      | 18.000      | 4.800      |          |
| 23          | 2.590      | 1.700     | 1.210      | 0.850     | 0.770     | 0.810     | 0.570     | 0.770     | 0.650     | 4.650      | 18.000      | 4.000      |          |
| 24          | 2.470      | 1.600     | 1.160      | 0.810     | 0.730     | 0.730     | 0.570     | 0.980     | 0.610     | 4.000      | 19.000      | 3.930      |          |
| 25          | 2.550      | 1.600     | 1.160      | 0.770     | 0.730     | 0.650     | 0.570     | 0.810     | 0.940     | 3.230      | 16.000      | 3.510      |          |
|             | < 11.570 > | < 8.300 > | < 6.030 >  | < 4.130 > | < 3.770 > | < 3.730 > | < 2.890 > | < 4.190 > | < 3.460 > | < 18.720 > | < 91.000 >  | < 21.560 > |          |
| AVERAGE     | < 2.514 >  | < 1.660 > | < 1.206 >  | < 0.826 > | < 0.754 > | < 0.746 > | < 0.578 > | < 0.838 > | < 0.692 > | < 3.744 >  | < 18.200 >  | < 4.512 >  |          |
| 26          | 2.240      | 1.500     | 1.160      | 0.810     | 0.770     | 0.810     | 0.570     | 0.770     | 0.980     | 2.710      | 11.000      | 3.230      |          |
| 27          | 2.180      | 1.450     | 1.120      | 0.810     | 1.030     | 0.690     | 0.530     | 0.650     | 1.750     | 2.530      | 7.580       | 3.090      |          |
| 28          | 2.020      | 1.400     | 1.120      | 0.810     | 0.850     | 1.120     | 0.530     | 0.610     | 1.750     | 2.950      | 5.320       | 2.950      |          |
| 29          | 1.960      | 1.800     | 1.120      | 0.810     | 0.810     | 0.810     | 0.530     | 0.650     | 2.890     | 4.350      | 2.950       | 2.950      |          |
| 30          | 1.800      | 1.800     | 1.070      | 0.890     | 0.770     | 0.770     | 0.530     | 0.610     | 1.160     | 2.830      | 4.140       | 2.650      |          |
| 31          | 1.800      | 1.800     | 1.070      | 0.890     | 0.690     | 0.690     | 0.530     | 0.610     | 4.070     | 4.070      | 4.070       | 2.410      |          |
|             | < 12.000 > | < 4.350 > | < 6.660 >  | < 4.530 > | < 4.920 > | < 4.200 > | < 3.220 > | < 3.900 > | < 7.290 > | < 17.980 > | < 32.590 >  | < 17.280 > |          |
| AVERAGE     | < 2.000 >  | < 1.450 > | < 1.110 >  | < 0.906 > | < 0.820 > | < 0.840 > | < 0.537 > | < 0.650 > | < 1.458 > | < 2.997 >  | < 6.478 >   | < 2.880 >  |          |
| GRAND TOTAL | 154.420    | 46.100    | 54.970     | 27.340    | 25.880    | 25.200    | 19.550    | 19.990    | 26.330    | 68.160     | 398.550     | 145.990    | 1012.478 |
| AVERAGE     | 342.       | 102.      | 122.       | 61.       | 57.       | 56.       | 43.       | 44.       | 58.       | 151.       | 883.        | 323.       | 2243.    |
| MAX         | 4.981      | 1.646     | 1.773      | 0.911     | 0.835     | 0.840     | 0.631     | 0.645     | 0.878     | 2.199      | 15.285      | 4.709      | 2.774    |
| MIN         | 22.000     | 2.770     | 7.330      | 1.210     | 1.600     | 1.600     | 0.890     | 1.030     | 1.750     | 4.650      | 59.000      | 16.000     | 16.000   |
|             | 1.800      | 1.350     | 1.070      | 0.770     | 0.610     | 0.610     | 0.530     | 0.530     | 0.610     | 0.850      | 2.180       | 2.410      |          |

COMPUTED

< DAILY RUNOFF > THUNG SONG  
( 1977 ) LAN SAKA

UNIT = (mm/D)

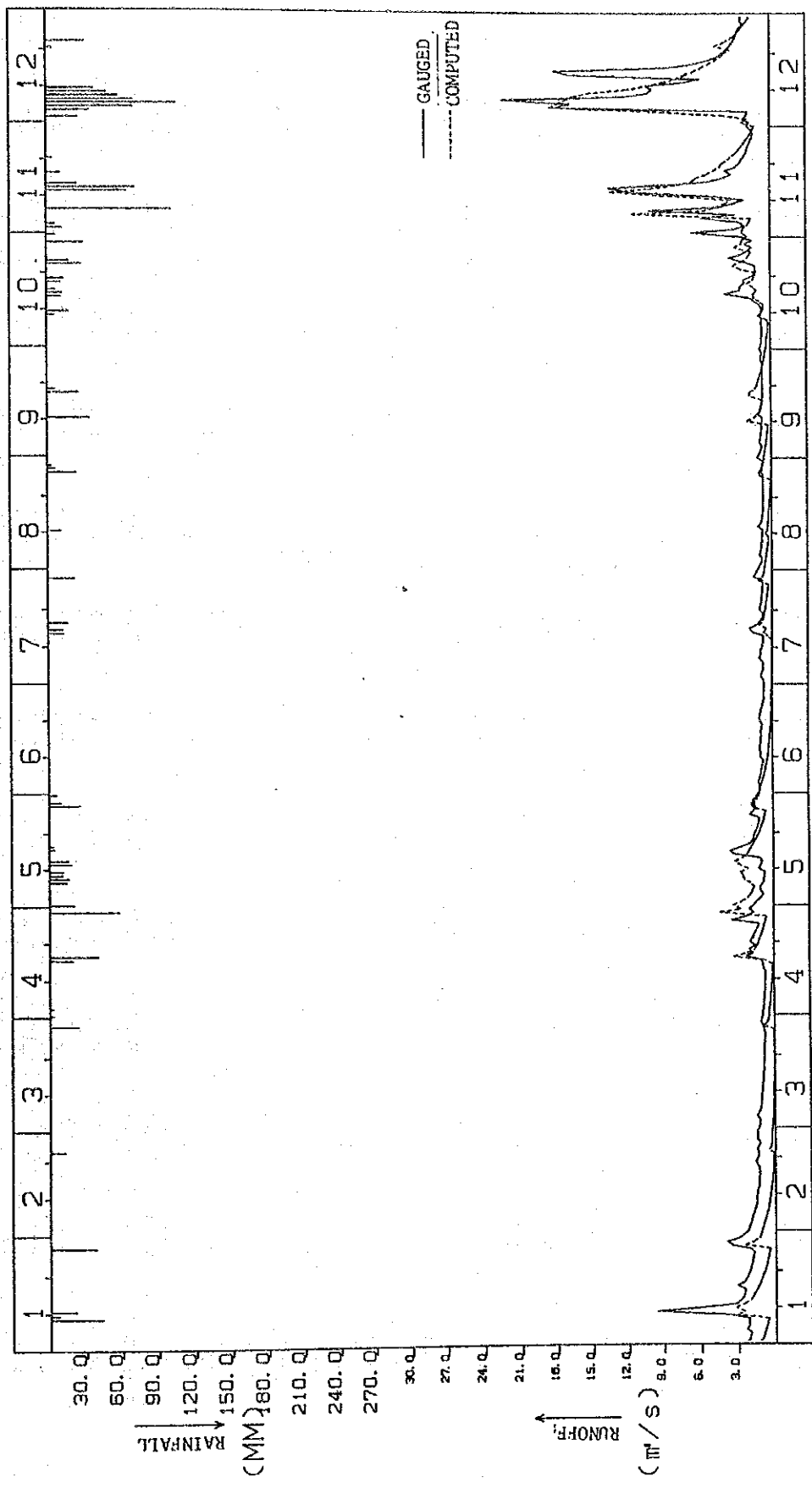
|             | 1 JAN      | 2 FEB     | 3 MAR      | 4 APR     | 5 MAY     | 6 JUN     | 7 JUL     | 8 AUG     | 9 SEP      | 10 OCT     | 11 NOV      | 12 DEC     |
|-------------|------------|-----------|------------|-----------|-----------|-----------|-----------|-----------|------------|------------|-------------|------------|
| 1           | 13.088     | 0.509     | 0.472      | 0.153     | 0.027     | 0.621     | 0.742     | 0.446     | 0.304      | 2.944      | 3.823       | 4.920      |
| 2           | 9.393      | 0.454     | 0.426      | 0.136     | 0.026     | 0.557     | 0.683     | 0.398     | 0.272      | 2.424      | 3.166       | 4.404      |
| 3           | 6.421      | 0.406     | 0.383      | 0.122     | 0.025     | 0.499     | 0.622     | 0.356     | 0.244      | 3.199      | 2.833       | 3.940      |
| 4           | 6.517      | 0.363     | 0.081      | 0.109     | 0.025     | 0.446     | 0.562     | 0.318     | 0.218      | 3.445      | 4.280       | 3.525      |
| 5           | 6.169      | 0.324     | 3.984      | 0.097     | 0.024     | 1.030     | 0.506     | 0.284     | 0.505      | 2.805      | 4.197       | 3.152      |
| AVERAGE     | ( 41.589 ) | ( 2.056 ) | ( 11.347 ) | ( 0.616 ) | ( 0.126 ) | ( 3.152 ) | ( 3.115 ) | ( 1.802 ) | ( 1.543 )  | ( 14.817 ) | ( 18.299 )  | ( 19.941 ) |
| 6           | 6.555      | 0.290     | 3.083      | 0.086     | 0.023     | 0.744     | 0.455     | 0.375     | 0.606      | 2.407      | 3.478       | 2.818      |
| 7           | 8.660      | 0.259     | 2.404      | 0.080     | 0.023     | 0.658     | 0.408     | 0.288     | 0.445      | 2.183      | 2.938       | 2.520      |
| 8           | 6.660      | 0.231     | 2.111      | 0.076     | 0.022     | 0.618     | 0.365     | 0.266     | 0.429      | 1.984      | 2.652       | 2.253      |
| 9           | 5.578      | 0.747     | 1.917      | 0.071     | 0.021     | 0.569     | 2.203     | 0.243     | 0.401      | 1.792      | 2.409       | 2.014      |
| 10          | 4.797      | 0.504     | 1.748      | 0.067     | 0.021     | 0.518     | 2.317     | 0.220     | 0.369      | 1.613      | 4.209       | 5.796      |
| AVERAGE     | ( 32.251 ) | ( 2.031 ) | ( 11.264 ) | ( 0.381 ) | ( 0.110 ) | ( 3.107 ) | ( 5.747 ) | ( 1.393 ) | ( 2.249 )  | ( 9.979 )  | ( 15.687 )  | ( 15.400 ) |
| 11          | 4.313      | 0.458     | 1.582      | 0.064     | 0.020     | 0.469     | 1.729     | 0.198     | 0.335      | 1.648      | 19.070      | 3.986      |
| 12          | 3.894      | 0.434     | 1.426      | 0.060     | 0.020     | 0.422     | 1.385     | 0.178     | 0.303      | 2.465      | 26.467      | 3.239      |
| 13          | 4.425      | 0.403     | 1.281      | 0.057     | 2.597     | 0.912     | 1.264     | 0.160     | 0.680      | 2.806      | 31.437      | 2.729      |
| 14          | 3.749      | 0.368     | 1.149      | 0.053     | 1.603     | 0.643     | 1.168     | 0.143     | 0.477      | 2.232      | 16.631      | 2.462      |
| 15          | 3.289      | 0.334     | 1.029      | 0.050     | 1.120     | 0.588     | 1.066     | 0.128     | 0.442      | 1.870      | 16.371      | 2.242      |
| AVERAGE     | ( 19.671 ) | ( 1.996 ) | ( 6.466 )  | ( 0.284 ) | ( 5.361 ) | ( 3.034 ) | ( 6.612 ) | ( 0.807 ) | ( 2.238 )  | ( 10.821 ) | ( 109.976 ) | ( 14.658 ) |
| 16          | 2.978      | 0.301     | 0.921      | 0.047     | 0.979     | 0.550     | 0.965     | 0.114     | 0.414      | 1.702      | 13.293      | 8.811      |
| 17          | 2.689      | 0.271     | 0.824      | 0.045     | 0.910     | 0.506     | 0.870     | 0.102     | 0.381      | 1.555      | 11.360      | 9.605      |
| 18          | 2.419      | 0.243     | 0.737      | 0.042     | 2.371     | 0.460     | 2.233     | 0.091     | 1.828      | 3.002      | 9.873       | 6.389      |
| 19          | 2.171      | 0.218     | 0.659      | 0.040     | 1.833     | 0.416     | 2.097     | 0.082     | 1.373      | 4.638      | 9.875       | 5.247      |
| 20          | 1.946      | 0.195     | 0.589      | 0.038     | 1.429     | 0.375     | 1.574     | 0.078     | 1.024      | 3.465      | 15.389      | 4.403      |
| AVERAGE     | ( 12.203 ) | ( 1.227 ) | ( 3.730 )  | ( 0.212 ) | ( 7.523 ) | ( 2.306 ) | ( 7.740 ) | ( 0.467 ) | ( 5.020 )  | ( 14.363 ) | ( 59.791 )  | ( 34.455 ) |
| 21          | 1.742      | 0.174     | 0.527      | 0.035     | 1.304     | 0.336     | 1.395     | 0.073     | 0.619      | 8.165      | 15.978      | 3.896      |
| 22          | 1.559      | 0.163     | 0.471      | 0.034     | 1.202     | 0.301     | 1.284     | 0.177     | 3.675      | 5.334      | 15.035      | 3.513      |
| 23          | 1.395      | 0.169     | 0.421      | 0.033     | 1.096     | 0.270     | 1.175     | 1.005     | 2.885      | 5.620      | 13.767      | 3.174      |
| 24          | 1.247      | 0.166     | 0.376      | 0.032     | 0.992     | 0.241     | 1.066     | 0.659     | 4.678      | 4.633      | 11.351      | 2.857      |
| 25          | 1.115      | 0.163     | 0.336      | 0.031     | 1.198     | 0.216     | 0.962     | 0.543     | 4.028      | 3.848      | 9.734       | 2.566      |
| AVERAGE     | ( 7.059 )  | ( 3.265 ) | ( 2.130 )  | ( 0.165 ) | ( 5.792 ) | ( 1.365 ) | ( 5.882 ) | ( 2.458 ) | ( 21.436 ) | ( 27.601 ) | ( 65.864 )  | ( 16.007 ) |
| 26          | 0.997      | 0.162     | 0.300      | 0.030     | 1.221     | 0.193     | 0.865     | 0.526     | 3.258      | 3.438      | 8.489       | 2.300      |
| 27          | 0.891      | 0.168     | 0.268      | 0.029     | 1.000     | 1.607     | 0.776     | 0.494     | 2.777      | 3.108      | 7.588       | 2.060      |
| 28          | 0.797      | 0.1520    | 0.240      | 0.028     | 0.925     | 1.150     | 0.696     | 0.455     | 2.508      | 3.531      | 6.818       | 1.844      |
| 29          | 0.712      | 0.148     | 0.214      | 0.028     | 0.845     | 0.833     | 0.623     | 0.415     | 2.280      | 2.987      | 6.124       | 1.855      |
| 30          | 0.637      | 0.144     | 0.191      | 0.027     | 0.766     | 0.792     | 0.557     | 0.375     | 3.582      | 4.024      | 5.492       | 1.580      |
| 31          | 0.569      | 0.140     | 0.171      | 0.026     | 0.690     | 0.690     | 0.498     | 0.338     | 4.606      | 4.606      | 4.606       | 1.427      |
| AVERAGE     | ( 4.603 )  | ( 1.700 ) | ( 1.384 )  | ( 0.144 ) | ( 5.447 ) | ( 4.595 ) | ( 4.016 ) | ( 2.604 ) | ( 14.405 ) | ( 21.693 ) | ( 34.511 )  | ( 11.067 ) |
| GRAND TOTAL | 117.375    | 12.276    | 36.322     | 1.801     | 24.359    | 17.560    | 33.111    | 9.532     | 46.891     | 99.274     | 304.127     | 111.528    |
| AVERAGE     | 260.       | 27.       | 80.        | 4.        | 54.       | 39.       | 73.       | 21.       | 104.       | 220.       | 674.        | 247.       |
| MAX         | 3.786      | 0.438     | 1.172      | 0.060     | 0.786     | 0.885     | 1.068     | 0.307     | 1.563      | 3.202      | 10.138      | 3.598      |
| MIN         | 15.088     | 0.943     | 6.081      | 0.153     | 2.597     | 1.807     | 2.317     | 1.005     | 6.169      | 8.165      | 31.437      | 9.605      |
|             | 0.569      | 0.174     | 0.171      | 0.027     | 0.020     | 0.193     | 0.365     | 0.073     | 0.218      | 1.448      | 2.409       | 1.427      |

RUNOFF ANALYSIS BY TANK MODEL

(1978)

RAINFALL STATION : LAN SAKA

COEFFICIENT = 0.8249



GAUGING STATION : X-70 ( CA = 39.00 km<sup>2</sup> )

UNIT = (mm/D)

< DAILY RAINFALL > THUNG SONG  
( 1978 ) LAN SAKA

|             | 1 JAN    | 2 FEB    | 3 MAR    | 4 APR    | 5 MAY    | 6 JUN   | 7 JUL    | 8 AUG    | 9 SEP    | 10 OCT   | 11 NOV    | 12 DEC    |
|-------------|----------|----------|----------|----------|----------|---------|----------|----------|----------|----------|-----------|-----------|
| 1           | 0.0      | 0.0      | 0.0      | 3.1      | 19.9     | 0.0     | 0.0      | 0.0      | 0.0      | 0.0      | 0.0       | 0.0       |
| 2           | 0.0      | 0.0      | 0.0      | 0.0      | 0.0      | 0.0     | 0.0      | 0.0      | 0.0      | 0.0      | 12.6      | 26.2      |
| 3           | 0.0      | 0.0      | 0.0      | 3.1      | 0.0      | 0.0     | 0.0      | 0.0      | 0.0      | 0.0      | 7.3       | 0.0       |
| 4           | 0.0      | 0.0      | 0.0      | 0.0      | 0.0      | 0.0     | 0.0      | 0.0      | 0.0      | 0.0      | 0.0       | 35.6      |
| 5           | 0.0      | 0.0      | 0.0      | 0.0      | 0.0      | 0.0     | 0.0      | 0.0      | 0.0      | 0.0      | 0.0       | 72.2      |
| AVERAGE     | < 0.0 >  | < 0.0 >  | < 0.0 >  | < 6.3 >  | < 19.9 > | < 0.0 > | < 0.0 >  | < 0.0 >  | < 0.0 >  | < 0.0 >  | < 19.9 >  | < 134.0 > |
| 6           | 0.0      | 0.0      | 0.0      | 0.0      | 0.0      | 0.0     | 0.0      | 0.0      | 0.0      | 0.0      | 0.0       | 107.3     |
| 7           | 0.0      | 0.0      | 0.0      | 0.0      | 13.6     | 0.0     | 0.0      | 0.0      | 0.0      | 0.0      | 102.6     | 72.2      |
| 8           | 0.0      | 0.0      | 0.0      | 0.0      | 15.7     | 0.0     | 0.0      | 0.0      | 0.0      | 0.0      | 0.0       | 59.9      |
| 9           | 42.9     | 0.0      | 0.0      | 0.0      | 10.5     | 0.0     | 0.0      | 0.0      | 0.0      | 6.3      | 0.0       | 50.3      |
| 10          | 7.3      | 0.0      | 0.0      | 0.0      | 11.5     | 0.0     | 0.0      | 0.0      | 0.0      | 17.8     | 0.0       | 38.9      |
| AVERAGE     | < 50.3 > | < 0.0 >  | < 0.0 >  | < 0.0 >  | < 51.3 > | < 0.0 > | < 0.0 >  | < 0.0 >  | < 0.0 >  | < 24.1 > | < 102.6 > | < 328.7 > |
| 11          | 20.9     | 0.0      | 0.0      | 0.0      | 0.0      | 0.0     | 0.0      | 10.5     | 34.6     | 0.0      | 0.0       | 0.0       |
| 12          | 0.0      | 0.0      | 0.0      | 0.0      | 17.8     | 0.0     | 0.0      | 0.0      | 0.0      | 0.0      | 67.0      | 0.0       |
| 13          | 0.0      | 0.0      | 0.0      | 0.0      | 15.7     | 0.0     | 0.0      | 0.0      | 0.0      | 0.0      | 73.3      | 0.0       |
| 14          | 0.0      | 0.0      | 0.0      | 0.0      | 0.0      | 0.0     | 12.6     | 0.0      | 0.0      | 11.5     | 24.7      | 0.0       |
| 15          | 0.0      | 0.0      | 0.0      | 0.0      | 0.0      | 0.0     | 11.5     | 0.0      | 0.0      | 12.6     | 0.0       | 0.0       |
| AVERAGE     | < 20.9 > | < 0.0 >  | < 0.0 >  | < 0.0 >  | < 33.5 > | < 0.0 > | < 10.5 > | < 2.1 >  | < 34.6 > | < 24.1 > | < 165.0 > | < 0.0 >   |
| 16          | 0.0      | 0.0      | 0.0      | 18.8     | 4.2      | 0.0     | 0.0      | 0.0      | 0.0      | 7.3      | 0.0       | 0.0       |
| 17          | 0.0      | 0.0      | 0.0      | 39.8     | 3.1      | 0.0     | 15.7     | 0.0      | 0.0      | 0.0      | 11.1      | 0.0       |
| 18          | 0.0      | 0.0      | 0.0      | 0.0      | 0.0      | 0.0     | 0.0      | 0.0      | 25.1     | 11.5     | 0.0       | 0.0       |
| 19          | 0.0      | 0.0      | 0.0      | 0.0      | 0.0      | 0.0     | 0.0      | 0.0      | 6.3      | 13.6     | 0.0       | 0.0       |
| 20          | 0.0      | 0.0      | 0.0      | 0.0      | 0.0      | 0.0     | 0.0      | 0.0      | 0.0      | 0.0      | 0.0       | 0.0       |
| AVERAGE     | < 0.0 >  | < 0.0 >  | < 0.0 >  | < 58.6 > | < 7.3 >  | < 0.0 > | < 15.7 > | < 0.0 >  | < 31.4 > | < 32.5 > | < 11.1 >  | < 0.0 >   |
| 21          | 0.0      | 0.0      | 0.0      | 0.0      | 0.0      | 0.0     | 0.0      | 0.0      | 0.0      | 0.0      | 4.8       | 4.7       |
| 22          | 0.0      | 0.0      | 0.0      | 0.0      | 0.0      | 0.0     | 0.0      | 0.0      | 0.0      | 0.0      | 0.0       | 0.0       |
| 23          | 0.0      | 12.6     | 0.0      | 0.0      | 0.0      | 0.0     | 0.0      | 0.0      | 0.0      | 28.3     | 0.0       | 51.4      |
| 24          | 0.0      | 0.0      | 0.0      | 0.0      | 0.0      | 0.0     | 0.0      | 0.0      | 0.0      | 17.8     | 0.0       | 0.0       |
| 25          | 0.0      | 0.0      | 0.0      | 0.0      | 0.0      | 0.0     | 0.0      | 0.0      | 0.0      | 0.0      | 0.0       | 0.0       |
| AVERAGE     | < 0.0 >  | < 12.6 > | < 0.0 >  | < 0.0 >  | < 0.0 >  | < 0.0 > | < 0.0 >  | < 0.0 >  | < 0.0 >  | < 46.1 > | < 4.8 >   | < 36.1 >  |
| 26          | 0.0      | 0.0      | 0.0      | 0.0      | 0.0      | 0.0     | 0.0      | 0.0      | 0.0      | 9.2      | 1.0       | 7.2       |
| 27          | 0.0      | 0.0      | 0.0      | 0.0      | 0.0      | 0.0     | 0.0      | 0.0      | 0.0      | 0.0      | 0.0       | 0.0       |
| 28          | 37.7     | 0.0      | 0.0      | 0.0      | 0.0      | 0.0     | 0.0      | 23.0     | 0.0      | 0.0      | 0.0       | 0.0       |
| 29          | 0.0      | 0.0      | 23.0     | 57.6     | 9.4      | 0.0     | 22.0     | 6.3      | 0.0      | 30.4     | 0.0       | 0.0       |
| 30          | 0.0      | 0.0      | 0.0      | 0.0      | 0.0      | 0.0     | 0.0      | 3.1      | 0.0      | 0.0      | 0.0       | 0.0       |
| 31          | 0.0      | 0.0      | 0.0      | 0.0      | 6.3      | 0.0     | 0.0      | 0.0      | 0.0      | 7.3      | 0.0       | 0.0       |
| AVERAGE     | < 37.7 > | < 0.0 >  | < 23.0 > | < 57.6 > | < 40.8 > | < 0.0 > | < 22.0 > | < 32.5 > | < 0.0 >  | < 37.7 > | < 0.0 >   | < 0.0 >   |
| GRAND TOTAL | 108.9    | 12.6     | 23.0     | 122.5    | 152.9    | 0.0     | 61.8     | 42.9     | 66.0     | 164.4    | 303.4     | 498.8     |
| AVERAGE     | 3.5      | 0.4      | 0.7      | 4.1      | 4.9      | 0.0     | 2.0      | 1.4      | 2.2      | 5.3      | 10.1      | 16.1      |
| MAX         | 42.9     | 12.6     | 23.0     | 57.6     | 25.1     | 0.0     | 22.0     | 23.0     | 34.6     | 30.4     | 102.6     | 107.3     |
| MIN         | 0.0      | 0.0      | 0.0      | 0.0      | 0.0      | 0.0     | 0.0      | 0.0      | 0.0      | 0.0      | 0.0       | 0.0       |

THUNG SONG  
LAN SAKA

UNIT = (mm/D)

1 JAN 2 FEB 3 MAR 4 APR 5 MAY 6 JUN 7 JUL 8 AUG 9 SEP 10 OCT 11 NOV 12 DEC

|             |            |           |           |            |            |           |           |           |           |           |            |            |            |
|-------------|------------|-----------|-----------|------------|------------|-----------|-----------|-----------|-----------|-----------|------------|------------|------------|
| 1           | 2.290      | 2.240     | 1.300     | 0.990      | 1.650      | 1.120     | 0.650     | 1.160     | 1.160     | 1.160     | 0.940      | 2.350      | 1.850      |
| 2           | 2.130      | 2.150     | 1.250     | 0.940      | 1.400      | 1.070     | 0.690     | 1.030     | 1.030     | 1.030     | 0.820      | 6.410      | 1.700      |
| 3           | 2.070      | 2.020     | 1.210     | 0.890      | 1.030      | 1.120     | 0.940     | 0.850     | 0.850     | 0.850     | 0.770      | 2.890      | 2.180      |
| 4           | 2.020      | 1.910     | 1.450     | 0.850      | 0.850      | 1.160     | 0.850     | 0.770     | 0.770     | 0.770     | 0.770      | 2.070      | 1.910      |
| 5           | 2.350      | 1.850     | 1.350     | 0.850      | 1.070      | 1.070     | 0.770     | 0.990     | 0.990     | 0.990     | 0.730      | 2.470      | 1.800      |
| AVERAGE     | < 2.172 >  | < 2.030 > | < 1.312 > | < 0.904 >  | < 1.200 >  | < 1.108 > | < 0.780 > | < 0.800 > | < 0.800 > | < 0.800 > | < 0.806 >  | < 3.238 >  | < 1.888 >  |
| 6           | 2.180      | 1.750     | 1.160     | 0.810      | 1.120      | 0.990     | 0.770     | 0.940     | 0.940     | 0.940     | 0.730      | 5.620      | 18.080     |
| 7           | 2.240      | 1.650     | 1.120     | 0.810      | 0.850      | 0.990     | 0.770     | 0.850     | 0.850     | 0.850     | 0.730      | 2.890      | 16.650     |
| 8           | 2.130      | 1.550     | 1.120     | 0.770      | 0.810      | 0.890     | 1.070     | 0.850     | 0.850     | 0.850     | 0.810      | 9.880      | 22.370     |
| 9           | 3.720      | 1.500     | 1.070     | 0.770      | 0.770      | 0.810     | 0.940     | 0.730     | 0.730     | 0.730     | 0.730      | 4.350      | 12.200     |
| 10          | 9.610      | 1.550     | 1.070     | 0.770      | 0.730      | 0.770     | 0.990     | 0.810     | 0.810     | 0.810     | 0.890      | 3.020      | 10.060     |
| AVERAGE     | < 19.880 > | < 8.000 > | < 5.540 > | < 3.950 >  | < 4.280 >  | < 4.400 > | < 4.540 > | < 4.260 > | < 4.260 > | < 4.260 > | < 3.890 >  | < 25.760 > | < 79.360 > |
| 11          | 5.850      | 1.450     | 1.030     | 0.730      | 1.210      | 1.030     | 0.850     | 0.770     | 0.770     | 0.770     | 0.770      | 2.180      | 9.610      |
| 12          | 3.230      | 1.450     | 1.030     | 0.730      | 1.070      | 0.990     | 0.770     | 0.770     | 0.770     | 0.770     | 0.770      | 4.500      | 10.150     |
| 13          | 2.830      | 1.350     | 0.980     | 0.690      | 0.940      | 1.070     | 0.770     | 1.120     | 1.120     | 1.120     | 0.890      | 11.710     | 7.070      |
| 14          | 2.590      | 1.350     | 0.940     | 0.890      | 1.160      | 1.030     | 0.730     | 0.850     | 0.850     | 0.850     | 1.350      | 13.400     | 5.700      |
| 15          | 2.530      | 1.350     | 0.940     | 0.890      | 3.230      | 0.990     | 1.550     | 0.810     | 0.810     | 0.810     | 1.650      | 8.530      | 16.650     |
| AVERAGE     | < 17.030 > | < 6.950 > | < 4.920 > | < 3.950 >  | < 7.610 >  | < 5.110 > | < 4.670 > | < 4.320 > | < 4.320 > | < 4.320 > | < 5.430 >  | < 40.320 > | < 49.180 > |
| 16          | 2.470      | 1.300     | 0.940     | 0.890      | 3.510      | 0.990     | 1.850     | 0.770     | 0.770     | 0.770     | 3.720      | 5.100      | 17.970     |
| 17          | 3.090      | 1.300     | 0.890     | 2.240      | 2.650      | 0.940     | 1.250     | 0.690     | 0.690     | 0.690     | 2.470      | 3.860      | 8.710      |
| 18          | 2.530      | 1.300     | 0.890     | 1.700      | 1.850      | 0.990     | 0.990     | 0.730     | 0.730     | 0.730     | 2.470      | 3.160      | 6.410      |
| 19          | 2.350      | 1.500     | 0.890     | 2.020      | 1.650      | 0.890     | 0.810     | 0.730     | 0.730     | 0.730     | 2.130      | 3.650      | 5.170      |
| 20          | 2.240      | 1.550     | 0.850     | 1.500      | 1.600      | 0.850     | 0.730     | 0.690     | 0.690     | 0.690     | 2.180      | 2.830      | 4.280      |
| AVERAGE     | < 12.680 > | < 6.950 > | < 4.460 > | < 8.490 >  | < 11.260 > | < 4.660 > | < 5.630 > | < 3.610 > | < 3.610 > | < 3.610 > | < 12.970 > | < 18.600 > | < 42.540 > |
| 21          | 2.070      | 1.400     | 0.850     | 1.960      | 1.500      | 1.070     | 1.030     | 0.690     | 0.690     | 0.690     | 1.500      | 2.470      | 3.860      |
| 22          | 2.020      | 1.350     | 0.850     | 1.750      | 1.350      | 1.070     | 0.990     | 0.730     | 0.730     | 0.730     | 1.210      | 2.290      | 3.510      |
| 23          | 1.910      | 1.450     | 0.850     | 1.600      | 1.250      | 0.990     | 0.890     | 0.690     | 0.690     | 0.690     | 1.850      | 2.070      | 3.230      |
| 24          | 1.850      | 1.300     | 0.850     | 1.450      | 1.210      | 0.940     | 0.890     | 0.690     | 0.690     | 0.690     | 1.850      | 1.910      | 3.020      |
| 25          | 1.800      | 1.250     | 0.810     | 1.350      | 1.120      | 0.850     | 0.850     | 0.690     | 0.690     | 0.690     | 2.070      | 1.850      | 2.830      |
| AVERAGE     | < 9.650 >  | < 6.750 > | < 4.210 > | < 8.110 >  | < 6.430 >  | < 4.920 > | < 4.650 > | < 3.490 > | < 3.490 > | < 3.490 > | < 7.280 >  | < 10.590 > | < 16.450 > |
| 26          | 1.750      | 1.450     | 0.810     | 1.210      | 1.910      | 0.770     | 0.810     | 0.690     | 0.690     | 0.690     | 3.370      | 1.700      | 2.710      |
| 27          | 2.070      | 1.400     | 0.810     | 3.440      | 1.600      | 0.730     | 0.810     | 0.730     | 0.730     | 0.730     | 2.470      | 1.600      | 2.650      |
| 28          | 3.510      | 1.450     | 0.890     | 2.130      | 1.450      | 0.730     | 0.770     | 0.850     | 0.850     | 0.850     | 1.960      | 1.450      | 2.470      |
| 29          | 3.930      | *****     | 0.940     | 1.650      | 1.550      | 0.690     | 0.770     | 0.810     | 0.810     | 0.810     | 1.500      | 1.400      | 2.180      |
| 30          | 2.890      | *****     | 1.120     | 1.960      | 1.650      | 0.650     | 1.500     | 0.770     | 0.770     | 0.770     | 2.070      | 1.550      | 2.410      |
| 31          | 2.530      | *****     | 1.030     | *****      | 1.250      | *****     | 1.350     | 0.730     | 0.730     | 0.730     | 1.500      | *****      | 2.290      |
| AVERAGE     | < 16.680 > | < 4.300 > | < 5.600 > | < 10.390 > | < 9.410 >  | < 3.570 > | < 6.010 > | < 4.580 > | < 4.580 > | < 4.580 > | < 3.850 >  | < 12.870 > | < 14.710 > |
| GRAND TOTAL | 86.780     | 43.100    | 31.290    | 39.370     | 44.990     | 28.200    | 29.400    | 25.060    | 24.330    | 46.470    | 119.160    | 211.680    | 729.829    |
| AVERAGE     | 192.       | 95.       | 69.       | 87.        | 100.       | 62.       | 65.       | 56.       | 54.       | 103.      | 264.       | 469.       | 1617.      |
| MAX         | 2.799      | 1.539     | 1.009     | 1.312      | 1.451      | 0.940     | 0.948     | 0.808     | 0.811     | 1.499     | 3.972      | 6.828      | 2.000      |
| MIN         | 9.610      | 2.240     | 1.450     | 3.440      | 3.510      | 1.160     | 1.850     | 1.160     | 1.160     | 1.160     | 3.720      | 13.400     | 22.370     |
|             | 1.750      | 1.250     | 0.810     | 0.690      | 0.730      | 0.650     | 0.650     | 0.690     | 0.690     | 0.690     | 1.400      | 1.400      | 1.700      |

(mm/s) (mm) (mm/s) (mm/s) (mm/s) (mm/s) (mm/s) (mm/s) (mm/s) (mm/s) (mm/s) (mm/s) (mm/s) (mm/s)

COMPUTED

< DAILY RUNOFF (1978) > THUNG SONG  
LAN SAKA

UNIT = (mm/d)

1 JAN 2 FEB 3 MAR 4 APR 5 MAY 6 JUN 7 JUL 8 AUG 9 SEP 10 OCT 11 NOV 12 DEC

|         |           |           |           |           |            |           |           |           |           |           |            |            |
|---------|-----------|-----------|-----------|-----------|------------|-----------|-----------|-----------|-----------|-----------|------------|------------|
| 1       | 1.285     | 1.093     | 0.211     | 0.452     | 3.268      | 1.151     | 0.059     | 0.628     | 0.622     | 0.419     | 1.926      | 1.265      |
| 2       | 1.153     | 1.003     | 0.191     | 0.428     | 2.566      | 1.067     | 0.056     | 0.584     | 0.570     | 0.375     | 2.259      | 2.307      |
| 3       | 1.034     | 0.912     | 0.172     | 0.396     | 2.086      | 0.976     | 0.053     | 0.535     | 0.518     | 0.335     | 2.285      | 1.853      |
| 4       | 0.926     | 0.824     | 0.154     | 0.362     | 1.888      | 0.885     | 0.050     | 0.486     | 0.468     | 0.299     | 1.915      | 3.803      |
| 5       | 0.829     | 0.742     | 0.138     | 0.329     | 1.727      | 0.799     | 0.047     | 0.439     | 0.421     | 0.267     | 1.715      | 9.970      |
|         | ( 5.227 ) | ( 4.574 ) | ( 0.866 ) | ( 1.967 ) | ( 11.535 ) | ( 4.878 ) | ( 0.265 ) | ( 2.672 ) | ( 2.599 ) | ( 1.695 ) | ( 10.101 ) | ( 19.198 ) |
| AVERAGE | < 1.045 > | < 0.915 > | < 0.173 > | < 0.393 > | < 2.307 >  | < 0.976 > | < 0.053 > | < 0.534 > | < 0.520 > | < 0.339 > | < 2.020 >  | < 3.840 >  |

|         |           |           |           |           |            |           |           |           |           |           |            |            |
|---------|-----------|-----------|-----------|-----------|------------|-----------|-----------|-----------|-----------|-----------|------------|------------|
| 6       | 0.741     | 0.666     | 0.123     | 0.296     | 1.569      | 0.718     | 0.044     | 0.395     | 0.377     | 0.239     | 1.567      | 18.354     |
| 7       | 0.663     | 0.597     | 0.110     | 0.266     | 1.876      | 0.644     | 0.042     | 0.354     | 0.338     | 0.214     | 1.394      | 17.703     |
| 8       | 0.593     | 0.535     | 0.098     | 0.239     | 2.367      | 0.577     | 0.039     | 0.318     | 0.303     | 0.191     | 5.496      | 17.080     |
| 9       | 3.061     | 0.478     | 0.088     | 0.214     | 2.495      | 0.517     | 0.037     | 0.284     | 0.271     | 0.323     | 4.454      | 16.353     |
| 10      | 2.556     | 0.428     | 0.081     | 0.191     | 2.657      | 0.462     | 0.035     | 0.254     | 0.242     | 1.008     | 3.654      | 15.151     |
|         | ( 7.614 ) | ( 2.704 ) | ( 0.501 ) | ( 1.201 ) | ( 10.963 ) | ( 2.919 ) | ( 0.198 ) | ( 1.605 ) | ( 1.531 ) | ( 1.974 ) | ( 26.565 ) | ( 84.641 ) |
| AVERAGE | < 1.523 > | < 0.541 > | < 0.100 > | < 0.241 > | < 2.193 >  | < 0.584 > | < 0.040 > | < 0.321 > | < 0.306 > | < 0.395 > | < 5.313 >  | < 16.928 > |

|         |            |           |           |           |            |           |           |           |           |           |            |            |
|---------|------------|-----------|-----------|-----------|------------|-----------|-----------|-----------|-----------|-----------|------------|------------|
| 11      | 3.262      | 0.383     | 0.076     | 0.171     | 2.092      | 0.413     | 0.034     | 0.513     | 1.935     | 0.725     | 3.191      | 11.891     |
| 12      | 2.591      | 0.342     | 0.072     | 0.153     | 2.715      | 0.370     | 0.033     | 0.348     | 1.396     | 0.603     | 8.063      | 10.095     |
| 13      | 2.046      | 0.306     | 0.068     | 0.137     | 3.118      | 0.330     | 0.032     | 0.332     | 1.017     | 0.578     | 13.254     | 8.722      |
| 14      | 1.852      | 0.273     | 0.064     | 0.122     | 2.489      | 0.295     | 0.363     | 0.308     | 0.925     | 0.926     | 9.825      | 7.722      |
| 15      | 1.693      | 0.244     | 0.060     | 0.109     | 2.129      | 0.264     | 0.180     | 0.282     | 0.867     | 1.342     | 7.609      | 6.928      |
|         | ( 11.444 ) | ( 1.547 ) | ( 0.341 ) | ( 0.692 ) | ( 12.543 ) | ( 1.673 ) | ( 1.180 ) | ( 1.784 ) | ( 6.140 ) | ( 4.173 ) | ( 41.943 ) | ( 45.359 ) |
| AVERAGE | < 2.289 >  | < 0.309 > | < 0.068 > | < 0.138 > | < 2.509 >  | < 0.335 > | < 0.236 > | < 0.357 > | < 1.228 > | < 0.835 > | < 8.389 >  | < 9.072 >  |

|         |           |           |           |           |           |           |           |           |           |           |            |            |
|---------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|------------|------------|
| 16      | 1.540     | 0.218     | 0.057     | 0.773     | 1.990     | 0.236     | 0.475     | 0.256     | 0.797     | 1.427     | 6.360      | 6.232      |
| 17      | 1.392     | 0.195     | 0.054     | 3.241     | 1.822     | 0.211     | 1.077     | 0.231     | 0.726     | 1.105     | 6.065      | 5.593      |
| 18      | 1.254     | 0.174     | 0.051     | 2.117     | 1.639     | 0.188     | 0.767     | 0.208     | 1.758     | 1.436     | 5.174      | 5.013      |
| 19      | 1.126     | 0.155     | 0.048     | 1.534     | 1.480     | 0.168     | 0.683     | 0.187     | 1.716     | 1.905     | 4.599      | 4.489      |
| 20      | 1.009     | 0.139     | 0.045     | 1.345     | 1.332     | 0.150     | 0.645     | 0.167     | 1.305     | 1.479     | 4.147      | 4.017      |
|         | ( 6.321 ) | ( 0.881 ) | ( 0.255 ) | ( 9.009 ) | ( 8.263 ) | ( 0.953 ) | ( 3.648 ) | ( 1.050 ) | ( 6.303 ) | ( 7.352 ) | ( 26.345 ) | ( 25.345 ) |
| AVERAGE | < 1.264 > | < 0.176 > | < 0.051 > | < 1.802 > | < 1.653 > | < 0.191 > | < 0.730 > | < 0.210 > | < 1.261 > | < 1.470 > | < 5.269 >  | < 5.069 >  |

|         |           |           |           |           |           |           |           |           |           |            |            |            |
|---------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|------------|------------|------------|
| 21      | 0.904     | 0.124     | 0.043     | 1.234     | 1.196     | 0.134     | 0.597     | 0.150     | 1.160     | 1.292      | 3.851      | 3.697      |
| 22      | 0.809     | 0.111     | 0.040     | 1.135     | 1.072     | 0.120     | 0.545     | 0.134     | 1.077     | 1.194      | 3.415      | 3.266      |
| 23      | 0.724     | 0.490     | 0.038     | 1.033     | 0.960     | 0.107     | 0.494     | 0.119     | 0.987     | 2.442      | 3.070      | 4.445      |
| 24      | 0.647     | 0.299     | 0.036     | 0.934     | 0.859     | 0.095     | 0.445     | 0.107     | 0.896     | 3.020      | 2.755      | 3.740      |
| 25      | 0.579     | 0.287     | 0.034     | 0.841     | 0.768     | 0.085     | 0.400     | 0.095     | 0.809     | 2.394      | 2.469      | 3.149      |
|         | ( 3.662 ) | ( 1.310 ) | ( 0.190 ) | ( 5.176 ) | ( 4.856 ) | ( 0.541 ) | ( 2.480 ) | ( 0.605 ) | ( 4.928 ) | ( 10.343 ) | ( 15.560 ) | ( 18.297 ) |
| AVERAGE | < 0.732 > | < 0.262 > | < 0.038 > | < 1.035 > | < 0.971 > | < 0.108 > | < 0.496 > | < 0.121 > | < 0.986 > | < 2.069 >  | < 3.112 >  | < 3.659 >  |

|         |           |           |           |           |           |           |           |           |           |            |           |            |
|---------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|------------|-----------|------------|
| 26      | 0.517     | 0.273     | 0.033     | 0.755     | 0.687     | 0.080     | 0.359     | 0.085     | 0.737     | 1.917      | 2.211     | 2.824      |
| 27      | 0.462     | 0.254     | 0.032     | 0.677     | 0.614     | 0.075     | 0.321     | 0.993     | 0.653     | 1.737      | 1.978     | 2.564      |
| 28      | 2.459     | 0.233     | 0.031     | 0.606     | 1.619     | 0.071     | 0.288     | 1.011     | 0.585     | 1.593      | 1.770     | 2.315      |
| 29      | 1.761     | 0.211     | 0.030     | 0.580     | 1.477     | 0.067     | 1.123     | 0.839     | 0.524     | 2.922      | 1.582     | 2.082      |
| 30      | 1.320     | 0.190     | 0.029     | 0.560     | 1.332     | 0.063     | 0.792     | 0.704     | 0.469     | 2.307      | 1.415     | 1.869      |
| 31      | 1.180     | 0.170     | 0.028     | 0.540     | 1.196     | 0.059     | 0.658     | 0.669     | 0.469     | 2.307      | 1.415     | 1.675      |
|         | ( 7.700 ) | ( 0.761 ) | ( 0.240 ) | ( 9.073 ) | ( 7.365 ) | ( 0.355 ) | ( 3.541 ) | ( 4.301 ) | ( 2.958 ) | ( 12.832 ) | ( 8.956 ) | ( 13.329 ) |
| AVERAGE | < 1.283 > | < 0.254 > | < 0.034 > | < 1.815 > | < 1.228 > | < 0.071 > | < 0.590 > | < 0.717 > | < 0.592 > | < 2.139 >  | < 1.791 > | < 2.222 >  |

|             |        |        |       |        |        |        |        |        |        |        |         |         |         |
|-------------|--------|--------|-------|--------|--------|--------|--------|--------|--------|--------|---------|---------|---------|
| GRAND TOTAL | 41.968 | 11.778 | 4.191 | 27.125 | 55.525 | 11.318 | 11.311 | 12.017 | 24.458 | 38.370 | 129.469 | 206.169 | 573.699 |
| AVERAGE     | 93.    | 26.    | 9.    | 60.    | 123.   | 25.    | 25.    | 27.    | 54.    | 85.    | 287.    | 457.    | 1271.   |
| MAX         | 1.354  | 0.421  | 0.135 | 0.904  | 1.791  | 0.377  | 0.365  | 0.388  | 0.815  | 1.238  | 4.316   | 6.651   | 1.572   |
| MIN         | 3.262  | 1.093  | 0.903 | 4.340  | 3.268  | 1.151  | 1.123  | 1.011  | 1.935  | 3.020  | 13.254  | 18.354  | 84.641  |
|             | 0.462  | 0.111  | 0.031 | 0.109  | 0.614  | 0.063  | 0.032  | 0.085  | 0.242  | 0.191  | 1.415   | 1.265   |         |



**APPENDIX A-3-1**

**Study on Flow and Pressure Measurement  
in Distribution System**



Appendix      **STUDY ON FLOW AND PRESSURE MEASUREMENTS IN  
DISTRIBUTION SYSTEM**

(1)      Introduction

To evaluate the characteristics of the distribution system, pressure and flow measurements were made from 7 to 8 September, 1988.

(2)      Methods and Results

The flow measurements of 24-hours were conducted of the main distribution pipe in the treatment plant using the ultrasonic flow meter with pen recorder. The pressure measurements were made by installing pressure gage at 5 house connections in the distribution system of Thung Song.

Due to the lack of data for the existing distribution system, these tests for Na Bon were not conducted.

The results of flow measurement at the Thung Song waterworks, Location of Pressure measurement points and the results of pressure measurement are shown in Figures A3-1, A3-2 and A3-3 to A3-7, respectively.

The results of pressure measurements in the existing distribution system show similar pressure conditions with distribution network analysis (refer to section 3.1.3).

The results confirm the low pressure area identified by Thung Song PWA's official.

# FLOW RATE MEASUREMENT TEST

THUNG SONG

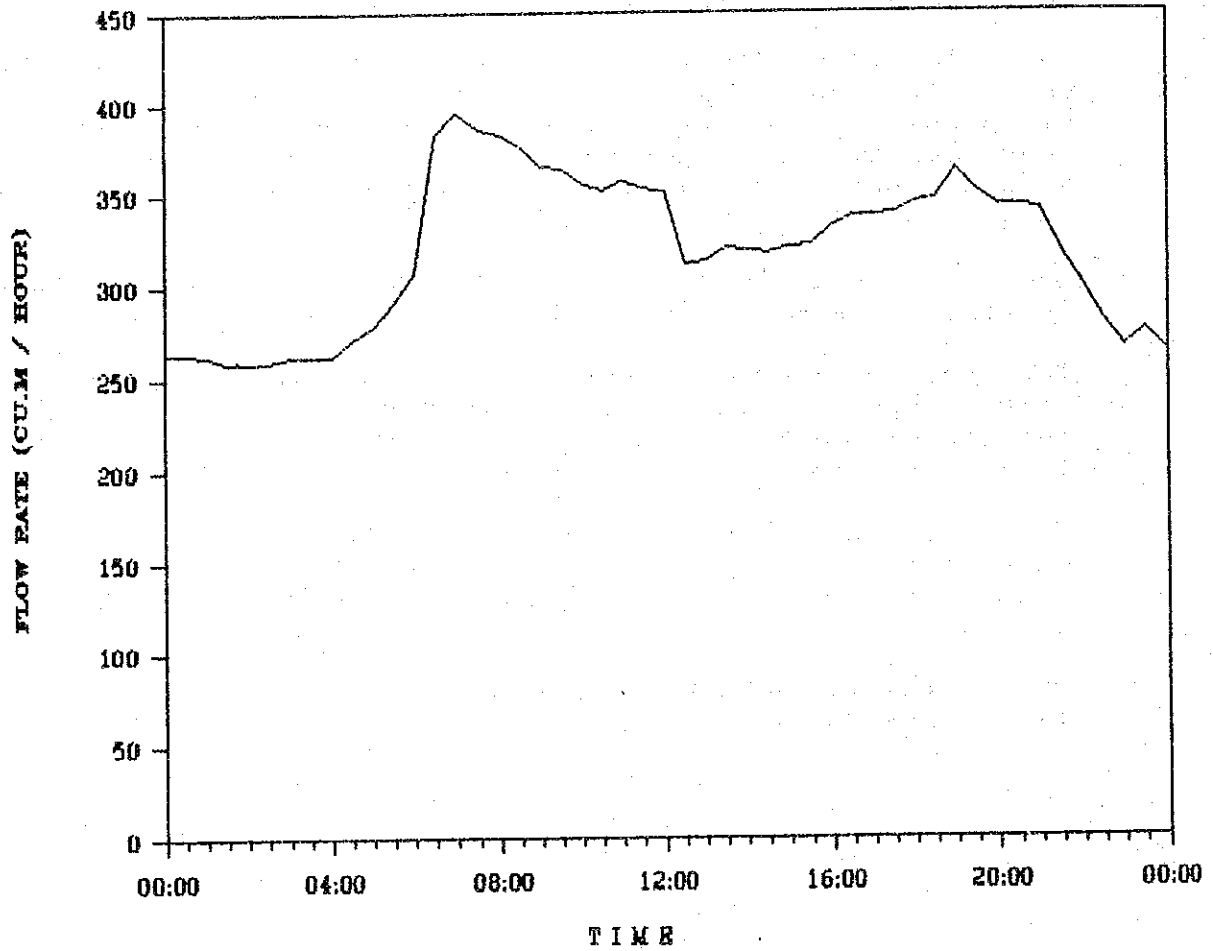


FIGURE A3-1  
FLOW RATE MEASUREMENT TEST

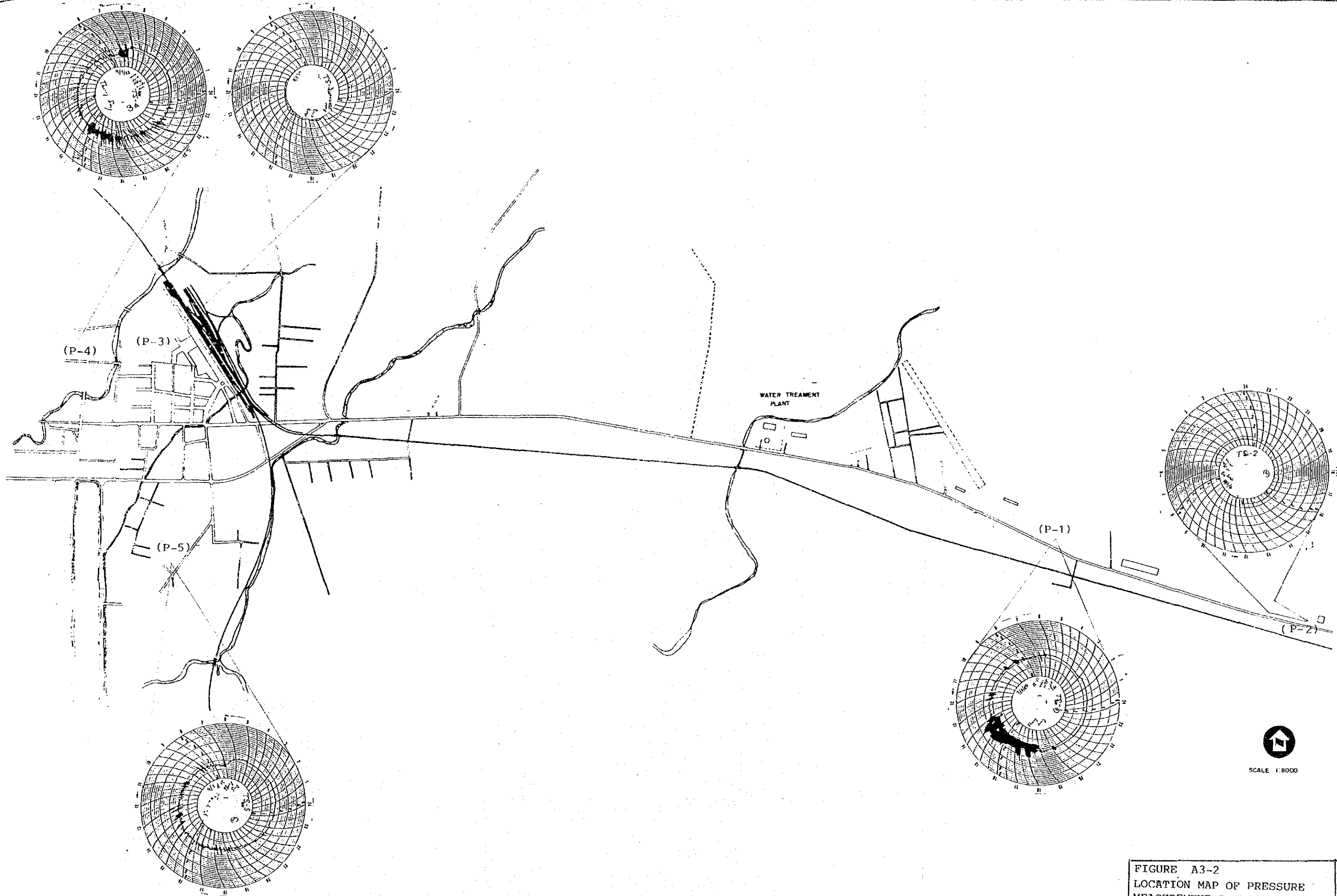


FIGURE A3-2  
 LOCATION MAP OF PRESSURE  
 MEASUREMENT POINTS



# PRESSURE MEASUREMENT TEST

THUNG SONG Point 1

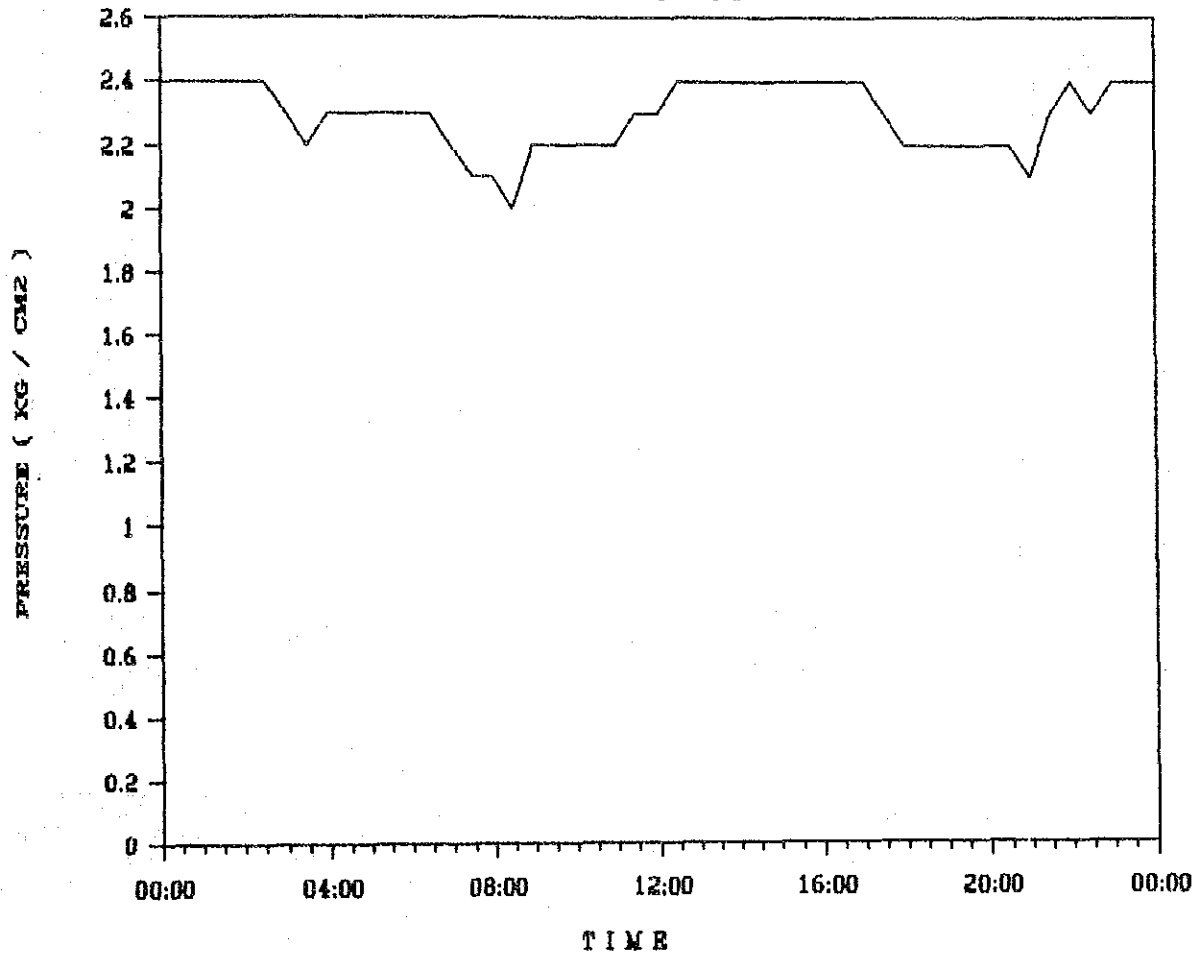


FIGURE A3-3  
PRESSURE MEASUREMENT TEST  
(Point 1)

# PRESSURE MEASUREMENT TEST

THUNG SONG Point 2

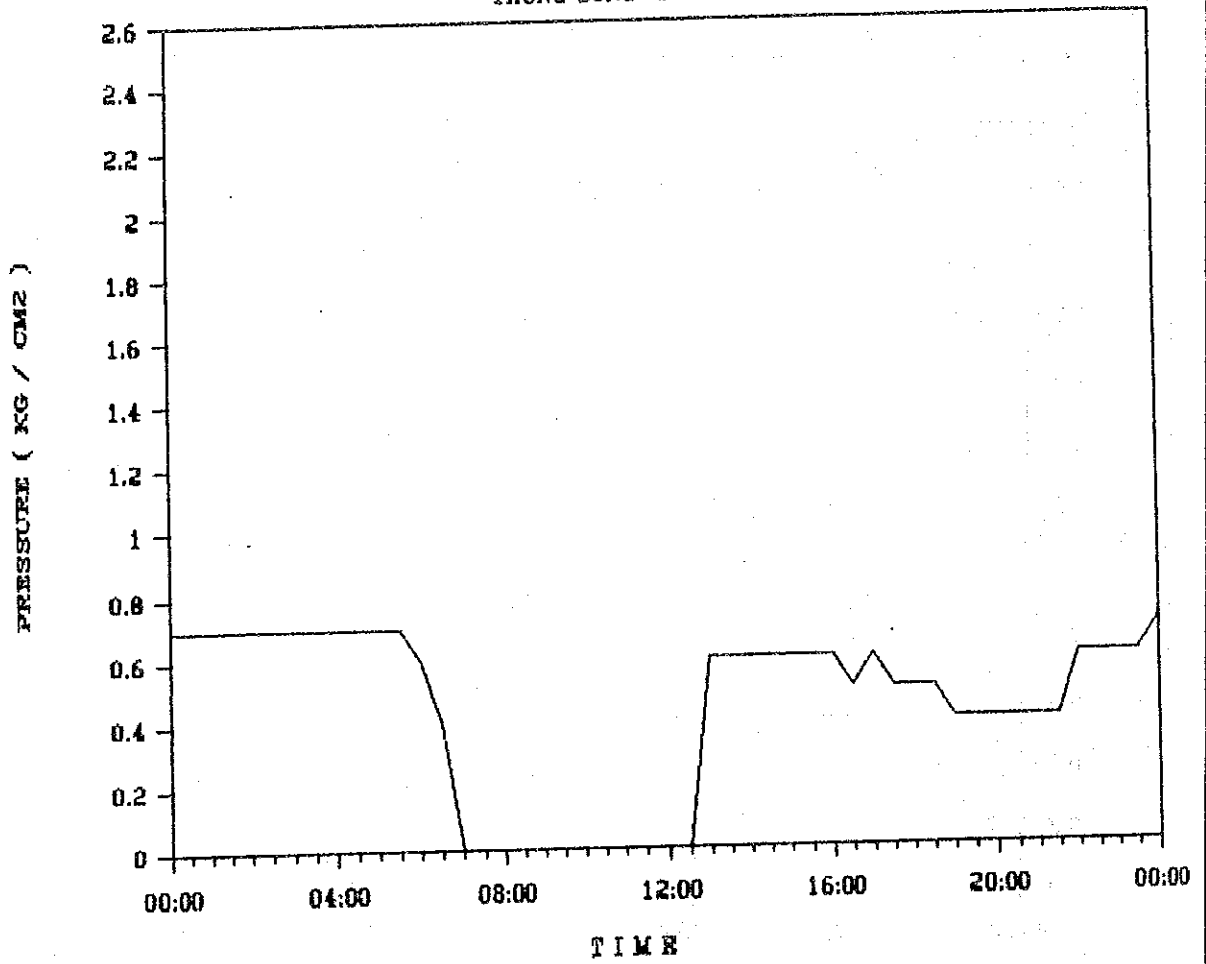


FIGURE A3-4

PRESSURE MEASUREMENT TEST  
(Point 2)



# PRESSURE MEASUREMENT TEST

THUNG SONG Point 3

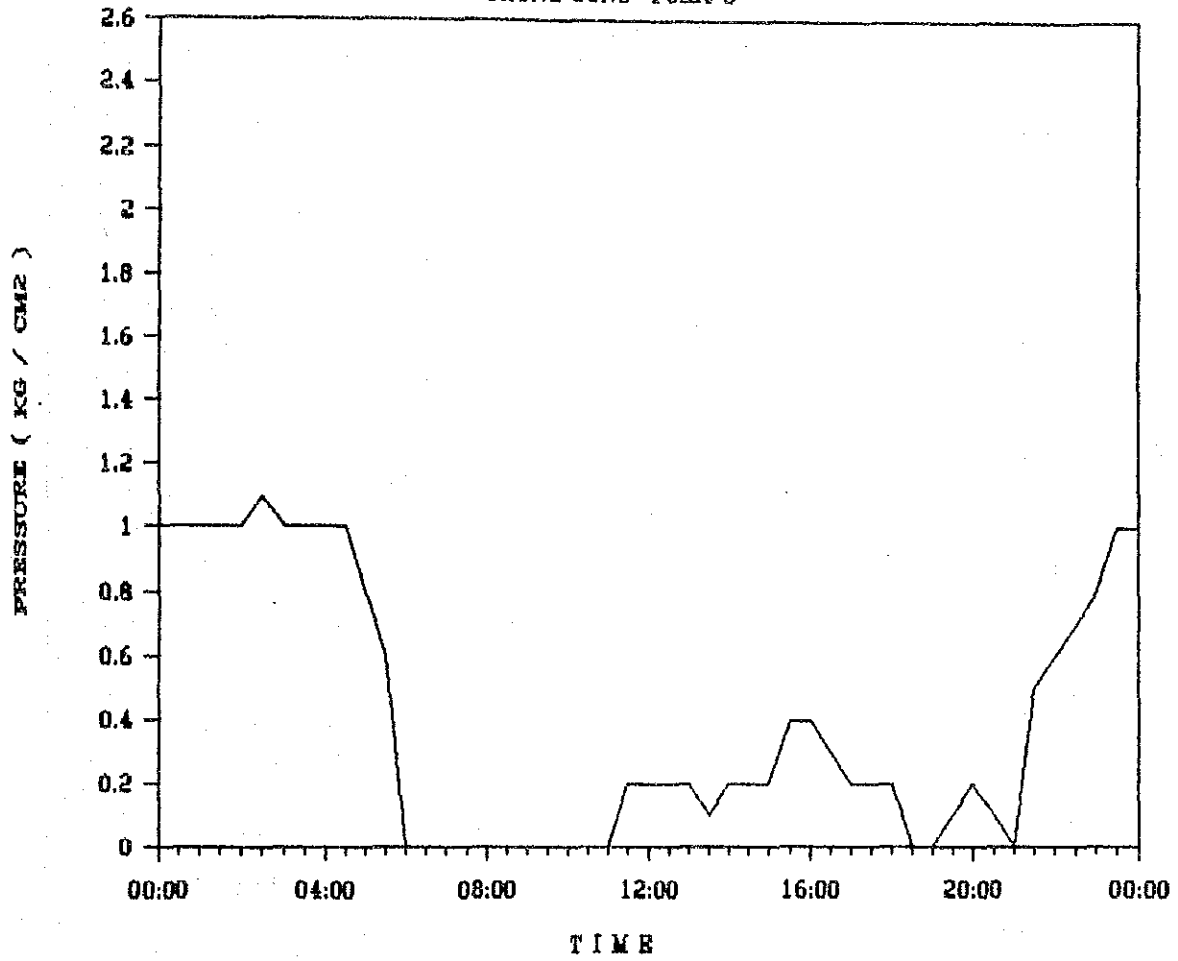


FIGURE A3-5  
PRESSURE MEASUREMENT TEST  
(Point 3)

# PRESSURE MEASUREMENT TEST

THUNG SONG Point 4

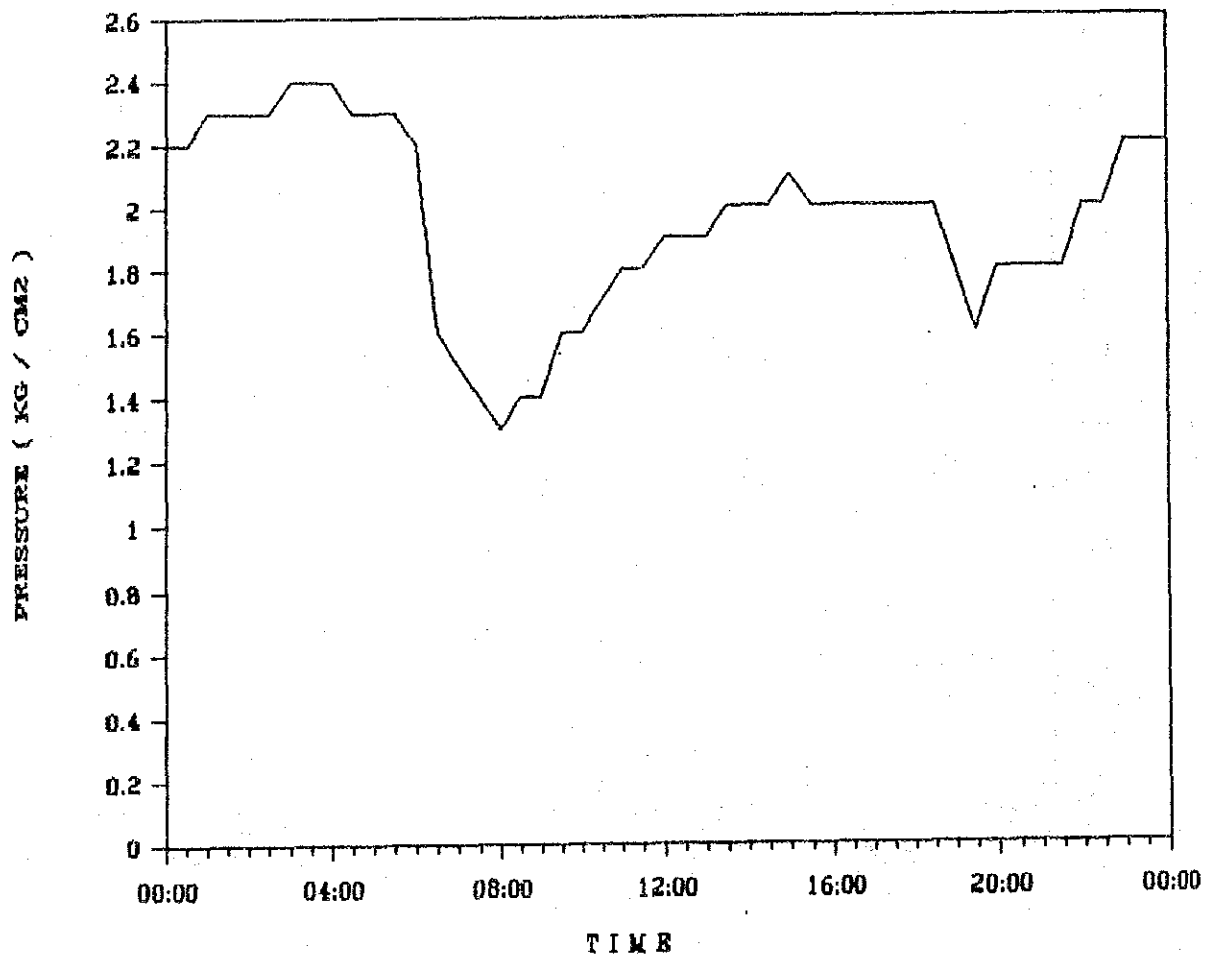


FIGURE A3-6  
PRESSURE MEASUREMENT TEST  
(Point 4)

# PRESSURE MEASUREMENT TEST

THUNG SONG Point 5

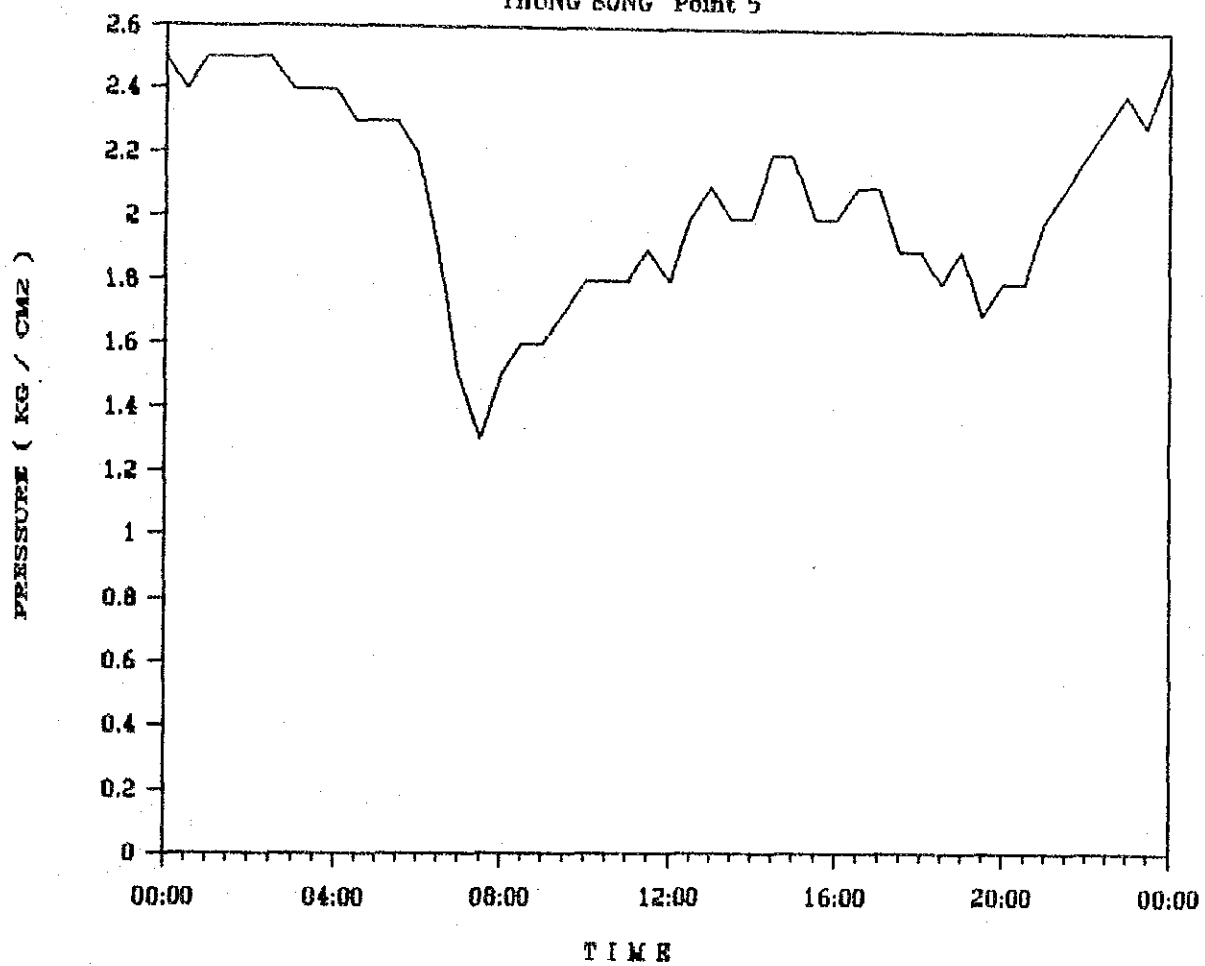


FIGURE A3-7  
PRESSURE MEASUREMENT TEST  
(Point 5)



**APPENDIX A-3-2**

**Study on Water Quality on Distribution Network**



APPENDIX WATER QUALITY ON DISTRIBUTION NETWORK

(1) General

Water quality analysis was conducted along the existing distribution mains by use of a portable water quality analyzer. Parameters of the analysis are pH, temperature and conductivity.

The results of the analysis are shown in Table A4-1. Sampling points are indicated in Figure A4-1.

(2) Causes of high pH

Results shown that only one sampling point No. 3 is pH 9.3. Other points show relatively low pH within the water quality standard. Based on the field investigation, the following causes may result in calcium dissolution from the inner wall of asbestos cement pipes.

- a) Pipe are newly installed ( less than two years ago).
- b) Water is retained long inside of pipe due to low water flow.

(3) Countermeasure

Drain-off from hydrants or blow-off pipes should be periodically carried out in this area.

Table A 4-1 Results of Water Quality Analysis

| Items                                 | Sampling Point |      |      |      |      |      |      |      |      |      | #1 |
|---------------------------------------|----------------|------|------|------|------|------|------|------|------|------|----|
|                                       | 1              | 2    | 3    | 4    | 5    | 6    | 7    | 8    | 9    | 10   |    |
| pH                                    | 7.18           | 7.67 | 9.30 | 7.13 | 6.97 | 7.50 | 7.20 | 7.20 | 6.85 | 7.20 |    |
| Temp. (°C)                            | 28.5           | 30.7 | 29.5 | 31.6 | 31.2 | 29.5 | 30.2 | 30.1 | 30.2 | 27.2 |    |
| Conductivity<br>(5x10 <sup>3</sup> μ) | 5.0            | 5.8  | 6.7  | 4.6  | 5.9  | 5.8  | 5.6  | 5.3  | 5.5  | 5.5  |    |

Note: #1 Treated Water at Water Treatment Plant



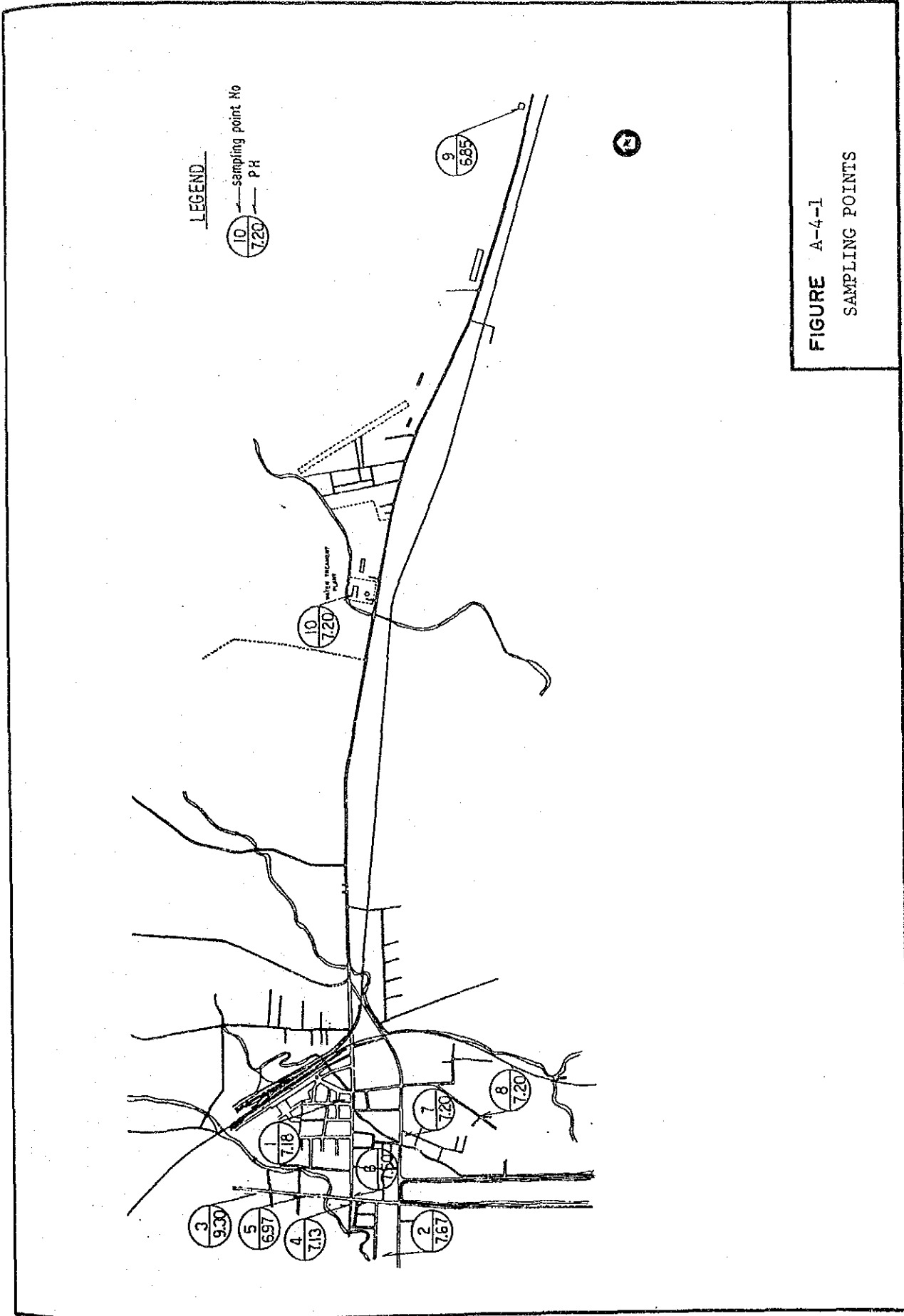


FIGURE A-4-1  
SAMPLING POINTS



**APPENDIX A-3-3**

**Jar Test on Raw Water of the Water Treatment Plant**



## APPENDIX JAR TEST

## 1 General

Jar Test was conducted to evaluate the present dosage rate of coagulant and to verify the appropriate dosage rate. The test was conducted on September 1988 for the raw water presently used by the waterworks.

## 2 Coagulant Used

Aluminum sulfate is being used as coagulant at Thung Song Waterworks as well as the other waterworks. The chemical is a solid type in a package of 25 kg bag, which is dissolved in the coagulant solution tank with an effective volume of about 1.0 cu.m.

According to the operator, they are consuming 50 kg (two bags) of aluminum sulfate a day. From this amount of consumption, dosage rate is calculated as below:

Dosage rate (R) for daily average flow rate:

$$R = 50,000 \text{ g} / 4,700 \text{ cu.m/day} = 10.6 \text{ mg/l}$$

Concentration of the coagulant in the solution tank is calculated from the amount of chemical dissolved and the volume of the tank as follows:

Concentration of coagulant solution (C)

$$C = 50,000 \text{ g} / 1.0 \text{ cu m} = 50,000 \text{ mg/l}$$

This solution was diluted 10 times for use of Jar Test; therefore, solution had the concentration of:

$$50,000 \times (1/10) = 5,000 \text{ mg/l}$$

## 3 Test Procedure

Test procedure followed the PWA's regulation for Jar Test. Sequence and time are shown as follows:

- a) Coagulant dosed
- b) Rapid Mixing, 60 rpm - 7.5 min
- c) Flocculation, 40 rpm - 7.5 min
- d) Flocculation, 25 rpm - 5.0 min
- e) Sedimentation, about 5 min

## 4 Condition and Results

Jar Test was conducted with a series of six different dosage rates. The condition and results are as shown in Table A5-1.

Table A5-1 Jar Test Condition and Result

|                                | 1       | 2                | 3       | 4       | 5       | 6       |
|--------------------------------|---------|------------------|---------|---------|---------|---------|
| 1. Coagulant Solution (ml)     | 0.5     | 1.0              | 2.0     | 3.0     | 4.0     | 5.0     |
| 2. Dosage Rate (mg/l)          | 2.5     | 5.0              | 10      | 15      | 20      | 25      |
| 3. Turbidity after setting     | 2.3     | <1.0             | 2.3     | 2.3     | 2.3     | 2.3     |
| 4. pH                          | 6.81    | 6.50             | 6.10    | 5.80    | 5.12    | 4.85    |
| 5. Conductivity (micro ohm/cm) | 4.9     | 5.0              | 5.1     | 5.3     | 5.8     | 6.6     |
| 6. Characteristics of floc     | No floc | floc size 1-2 mm | No floc | No floc | No floc | No floc |

From the results above, it is observed that dosage rate of 5.0 mg/l shows the most effective removal of turbidity. Considering this, present dosage rate (10.6 mg/l) may be reduced although the dosage should be made evenly through the operation with a proper mixing and flocculation process.

**APPENDIX A-4-1**

**Study on Water Consumption**





APPENDIX      STUDY ON WATER CONSUMPTION

1    Data Collection

Present water consumption data was collected from the waterworks' meter reading records for the study of water demand and distribution network analysis. Meter reading records at the waterworks office consist of volumes of cards in PWA's format for each connection. Monthly consumptions from September 1987 to August 1988 of each connection are recorded on this card.

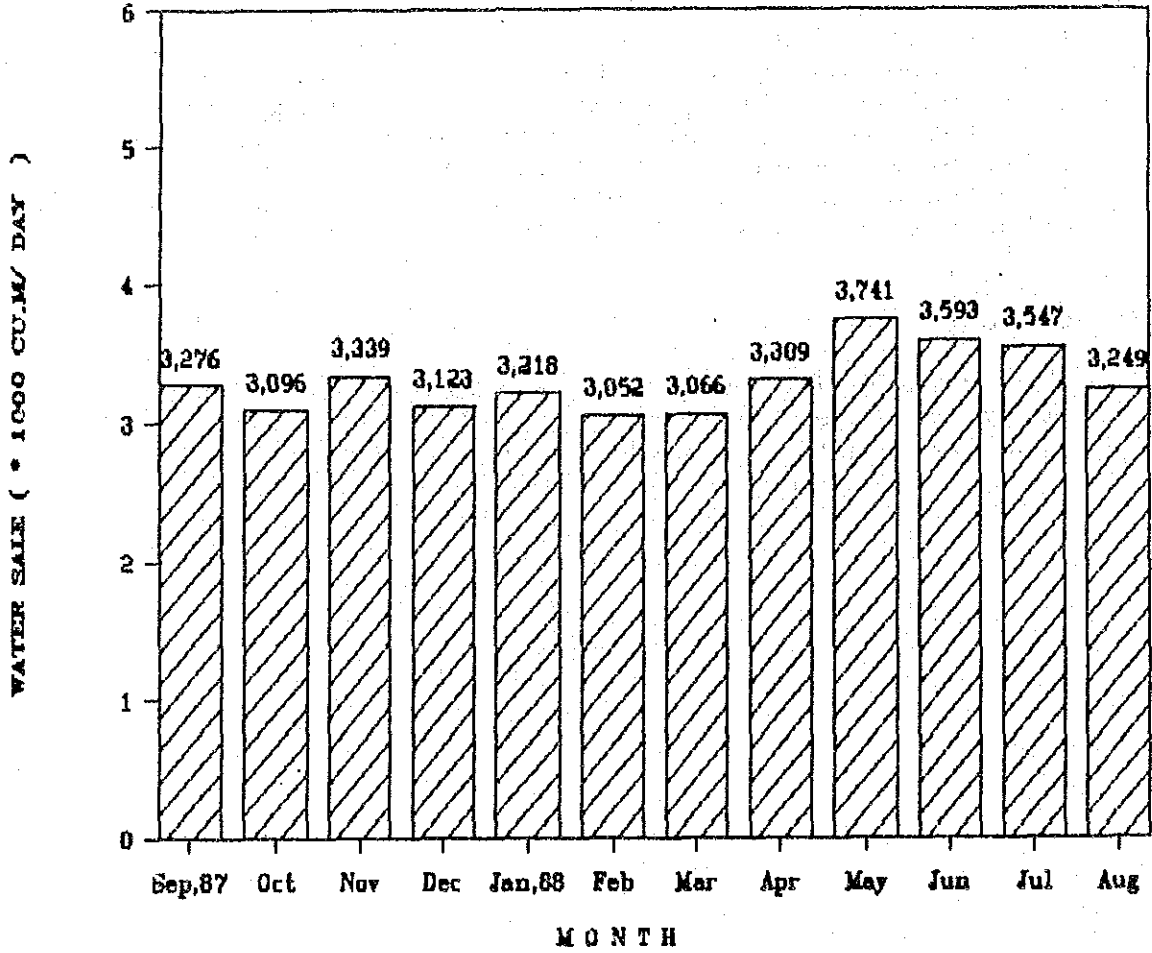
Data collection was made in a manner of copying figures water consumption of each consumer for every month. For distribution network analysis, each consumer was located on the map by interviewing meter readers of the waterworks. When the exact locations were not identified, they were located in some extent of the pipeline. Big consumers were also identified for further analysis.

2    Collected Data

Raw data copied from meter reading books was then summed up by month and by area. The attached sheets hereafter show the summary of water consumption.

# WATER SALE OF THUNG SONG W.W.

## DAILY AVE. BY MONTH (MUNICIPALITY)

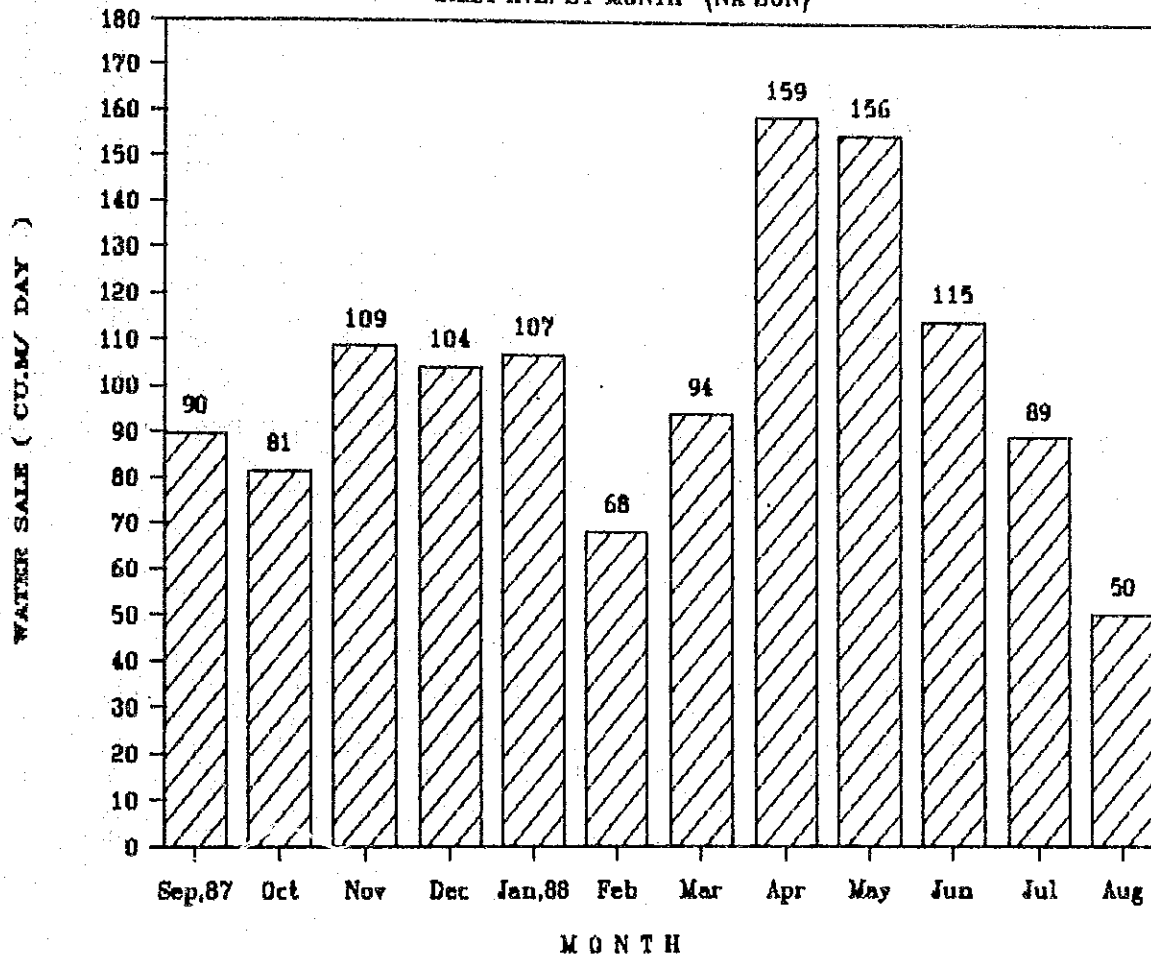


FIGURE

A2 - 2 - 1

# WATER SALE OF THUNG SONG W.W.

DAILY AVE. BY MONTH (NA BON)



FIGURE

A2 - 2 - 2

Table A2 - 2 - 1  
Grand Summary of Thung Song Waterworks

| Thung Song Municipality |        |        |         |        |        |        |        |        |         |         |         |         |           |          |
|-------------------------|--------|--------|---------|--------|--------|--------|--------|--------|---------|---------|---------|---------|-----------|----------|
| File No.                | Sep,87 | Oct    | Nov     | Dec    | Jan,88 | Feb    | Mar    | Apr    | May     | Jun     | Jul     | Aug     | Total     | Day Ave. |
| 0                       | 34,924 | 31,630 | 33,432  | 33,984 | 31,872 | 27,060 | 27,869 | 24,626 | 36,456  | 34,682  | 34,500  | 33,519  | 384,554   | 1098.66  |
| 1-1                     | 3,757  | 6,074  | 6,818   | 6,726  | 7,078  | 5,947  | 6,250  | 6,627  | 7,826   | 7,112   | 7,273   | 7,290   | 80,778    | 224.38   |
| 1-2                     | 4,329  | 4,556  | 4,409   | 4,220  | 4,660  | 3,987  | 4,254  | 5,144  | 6,021   | 4,510   | 4,847   | 4,363   | 55,300    | 151.51   |
| 1-3                     | 2,364  | 2,537  | 2,441   | 2,283  | 2,653  | 2,516  | 2,867  | 3,002  | 3,597   | 3,377   | 3,470   | 3,002   | 34,109    | 94.75    |
| 2-1                     | 3,580  | 3,552  | 3,561   | 3,486  | 3,584  | 3,202  | 3,489  | 3,553  | 3,938   | 3,596   | 4,119   | 3,279   | 51,812    | 119.92   |
| 2-2                     | 3,057  | 3,143  | 3,190   | 2,969  | 3,176  | 2,924  | 3,103  | 3,528  | 3,582   | 3,396   | 3,475   | 3,004   | 41,734    | 109.81   |
| 3-1                     | 5,665  | 5,635  | 6,190   | 5,117  | 6,024  | 4,992  | 5,587  | 6,385  | 6,650   | 6,056   | 5,900   | 5,847   | 70,048    | 194.58   |
| 3-2                     | 4,578  | 4,941  | 4,361   | 4,285  | 4,434  | 4,249  | 4,408  | 5,358  | 5,344   | 5,149   | 5,299   | 4,997   | 57,403    | 157.85   |
| 4-1                     | 2,712  | 2,594  | 2,470   | 2,494  | 2,690  | 2,159  | 2,229  | 2,666  | 2,982   | 2,934   | 2,802   | 2,735   | 32,177    | 88.16    |
| 4-2                     | 3,312  | 3,238  | 3,783   | 3,095  | 4,069  | 3,413  | 3,205  | 3,902  | 4,485   | 4,244   | 4,064   | 3,880   | 44,690    | 122.44   |
| 5-1                     | 5,604  | 5,160  | 6,201   | 5,567  | 5,888  | 5,181  | 5,932  | 6,285  | 7,125   | 6,061   | 6,305   | 5,999   | 71,308    | 195.36   |
| 5-2                     | 3,080  | 3,176  | 4,041   | 3,037  | 3,261  | 2,974  | 3,421  | 3,530  | 4,128   | 3,449   | 3,500   | 3,165   | 40,762    | 115.07   |
| 5-3                     | 2,181  | 2,358  | 2,261   | 2,279  | 2,324  | 2,354  | 2,882  | 2,487  | 2,939   | 2,486   | 2,811   | 1,956   | 29,318    | 80.32    |
| 5-4                     | 1,943  | 2,150  | 1,991   | 1,974  | 2,138  | 1,838  | 2,300  | 2,066  | 2,521   | 2,213   | 2,565   | 2,055   | 25,754    | 75.38    |
| 6-1                     | 1,815  | 2,011  | 1,915   | 2,019  | 1,884  | 1,697  | 1,929  | 2,595  | 2,039   | 2,141   | 1,914   | 1,489   | 23,448    | 64.24    |
| 6-2                     | 1,946  | 2,310  | 2,193   | 2,301  | 2,162  | 1,933  | 2,285  | 2,298  | 2,473   | 2,396   | 2,378   | 1,947   | 26,622    | 72.94    |
| 6-3                     | 2,750  | 2,706  | 2,138   | 2,462  | 2,290  | 2,590  | 2,709  | 2,472  | 2,538   | 2,413   | 2,624   | 2,271   | 29,963    | 82.09    |
| 6-4                     | 1,024  | 987    | 1,096   | 1,258  | 1,297  | 1,207  | 1,235  | 1,296  | 1,348   | 1,206   | 1,217   | 1,012   | 14,183    | 40.94    |
| 7-1                     | 4,161  | 3,859  | 3,757   | 3,605  | 4,098  | 3,517  | 4,179  | 5,615  | 4,215   | 4,297   | 4,681   | 3,785   | 49,769    | 136.35   |
| 7-2                     | 3,509  | 3,354  | 3,915   | 3,637  | 4,188  | 4,776  | 4,907  | 5,868  | 5,764   | 6,057   | 6,227   | 5,135   | 57,317    | 180.71   |
| Total (ca. n/so)        | 98,291 | 95,971 | 100,163 | 96,798 | 99,770 | 88,516 | 95,040 | 99,283 | 115,971 | 107,775 | 109,971 | 100,730 | 1,221,049 | 3,405    |
| Total (ca. n/d)         | 3,276  | 3,096  | 3,339   | 3,123  | 3,218  | 3,052  | 3,066  | 3,309  | 3,741   | 3,593   | 3,547   | 3,249   |           |          |

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| File No.         | Sep,87 | Oct   | Nov   | Dec   | Jan,88 | Feb   | Mar   | Apr   | May   | Jun   | Jul   | Aug   | Total  | Day Ave. |
|------------------|--------|-------|-------|-------|--------|-------|-------|-------|-------|-------|-------|-------|--------|----------|
| W1               | 1,317  | 1,209 | 1,672 | 1,716 | 1,809  | 891   | 1,169 | 2,343 | 2,409 | 1,699 | 1,435 | 599   | 19,854 | 53.35    |
| W2               | 1,381  | 1,316 | 1,587 | 1,519 | 1,514  | 1,091 | 1,752 | 2,431 | 2,413 | 1,742 | 1,334 | 966   | 19,046 | 52.18    |
| Total (ca. n/so) | 2,698  | 2,525 | 3,259 | 3,235 | 3,323  | 1,982 | 2,921 | 4,774 | 4,822 | 3,441 | 2,769 | 1,565 | 38,900 | 108      |
| Total (ca. n/d)  | 90     | 81    | 109   | 104   | 107    | 68    | 94    | 159   | 156   | 115   | 89    | 50    |        |          |

**APPENDIX A-4-2**

**Questionnaire Survey for Residents**



### 1 Objective

The door-to-door questionnaire survey was conducted to obtain the basic information on the resident's living conditions, water use patterns, responses to the municipal system and/or their own water sources and willingness for house-connection supply, and covered the area served or unserved by the municipal water supply system.

### 2 Survey Area

The survey area was divided into 5 blocks taking into account the boundary of the municipality, railway and roads as shown in Figure A1-2-1. All blocks were fully or partially served by the municipal system.

### 3 Survey Item

The form used for the questionnaire survey was originally written by Thai and included the following items.

1. General
  - 1.1 Address
  - 1.2 Type of House
  - 1.3 No. of Persons in Family
  - 1.4 No. of Employees
  - 1.5 Average Monthly Income
  - 1.6 Average Monthly Medical Expense
2. Type of Water Supply
3. Conditions in case of Municipal System
  - 3.1 Pressure
  - 3.2 Quantity
4. Other Sources than Municipal System
  - 4.1 Type of Source
  - 4.2 Conditions in case of Groundwater
5. Potability
6. Water Quality in case of Municipal System
  - 6.1 Color
  - 6.2 Smell
  - 6.3 Turbidity
7. Average Monthly Water Consumption

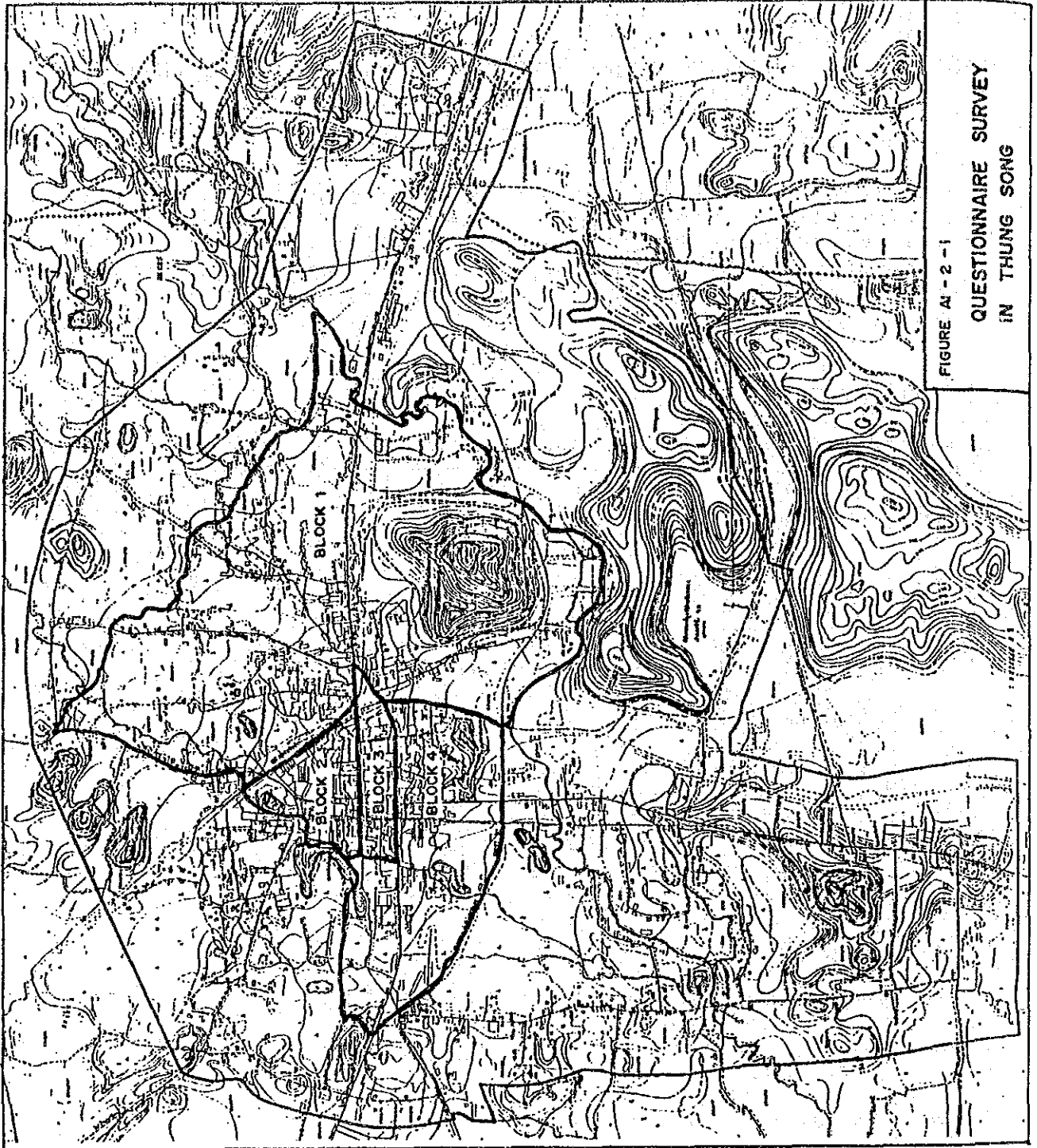
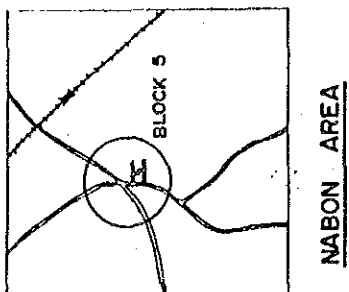


FIGURE A1-2-1  
QUESTIONNAIRE SURVEY  
IN THUNG SONG





8. Average Monthly Water Charge
9. Willingness to Pay for Water Charge
10. Water Quality in case of Other Source
  - 10.1 Color
  - 10.2 Smell
  - 10.3 Turbidity
11. Willingness to Connect to the Municipal System
12. Willingness to Pay for Connection Fee
13. Willingness to Pay for Water Charge

#### 4 Survey Method

College students were employed as interviewers and were engaged in the questionnaire survey with the guidance of the PWA Head Office staff. The survey was conducted to 183 residents on September 8, 1988.

#### 5 Survey Results

The results of the questionnaire survey are summarized in Table A1-5-1.

##### 1) General

55.2% of the respondents lived in residential houses while 43.7% in commercial buildings and the remaining 1.1% was unknown due to the omission of confirmation by the interviewers.

The total numbers of persons in families and employees were 918 and 434, respectively. Accordingly, one household is composed of 5.02 family members and 2.37 employees on an average with a total of 7.39 persons.

Regarding the average monthly income, 82.0% of the respondents were in the up-to-6,000 Baht bracket, or 14.2% in the up-to-2,000 Baht, 33.9% in the 2,001-3,000 Baht, 15.9% in the 3,001-4,500 Baht and 18.0% in the 4,501-6,000 Baht brackets, respectively. The average in respondents weighted by the number of persons and the median in each income bracket was approximately 4,700 Baht, but the number of persons was biggest in the 2,001-3,000 Baht bracket.

As to the average monthly medical expense, 39.9% was in the up-to-50 Baht bracket and 14.7%, 11.5% and 20.8% were in the 51-100, 101-200 and 201-500 Baht brackets, respectively. The average in respondents calculated by the same method as the above is 300 Baht, but the number of persons was biggest in the the up-to-50 Baht bracket.

2) Type of Water Supply

60.1% of the respondents used the municipal system only, 23.0% the other source than the municipal system and 16.9% the combined system of the municipal system and other source(s).

87.7% or 64 out of 73 other sources was groundwater as shown below.

| Block No.             | 1         | 2         | 3         | 4         | 5         | Total      |
|-----------------------|-----------|-----------|-----------|-----------|-----------|------------|
| Municipal System Only | 14        | 30        | 25        | 28        | 13        | 110        |
| plus Rain/River       | 1         | -         | 4         | -         | -         | 5          |
| plus Pond/Reservoir   | -         | 1         | -         | -         | -         | 1          |
| plus Water Vendor     | -         | -         | -         | 1         | -         | 1          |
| plus Well             | 7         | -         | 2         | 5         | 10        | 24         |
| Well Only             | 18        | -         | -         | 15        | 6         | 39         |
| plus Water Vendor     | -         | -         | -         | 1         | -         | 1          |
| Rain/River Only       | -         | -         | -         | -         | 2         | 2          |
| <b>Total</b>          | <b>40</b> | <b>31</b> | <b>31</b> | <b>50</b> | <b>31</b> | <b>183</b> |

3) Response to Municipal System

The reputation of the PWA waterworks among 141 respondents using the municipal system was not so good, that is to say, 47.5% complained of low pressure, 24.8% of insufficient water, 36.2% of color, 47.5% of smell and 50.4% of turbidity. However, there were big gaps in response by the block. Though the low pressure took place in all blocks, especially in Block 5 (Nabon), the respondents except for Block 5 have insufficient water. The complaint of color was conspicuous in Blocks 2 and 3, while smell was mostly detected in Blocks 1, 2 and 3 and turbidity was found in Blocks 1, 2, 3 and 5.

4) Potability

This question was originally intended to know the potability of tap water, but the answer seemed to be made not only for the tap water but also for other source water, since the question followed that on other sources.

Accordingly, the evaluation was made extracting the data from respondents using tap water or well water only.

|              | Tap Water         | Well Water       |
|--------------|-------------------|------------------|
| Drinking     | 54 (49.1%)        | 28 (71.8%)       |
| Not Drinking | 6 ( 5.4%)         | 8 (20.5%)        |
| Both         | 50 (45.5%)        | - (-)            |
| Unknown      | - (-)             | 3 (7.7%)         |
| <b>Total</b> | <b>110 (100%)</b> | <b>39 (100%)</b> |

49.1% used well water for drinking and 45.5% for drinking and not-drinking in spite of their complaints of its water quality, while 71.8% used well water for drinking.

The doubt as to the kind of water the respondents (who answered that they didn't use only one source for drinking) used for drinking is remained. They may use the water vendor, although this is not expressed clearly in the survey.

5) Water Quality of Other Sources

As mentioned above, the main water source was the groundwater. 23.3% complained of color, 19.2% of smell and 24.6% of turbidity. Scrutinizing the data block by block, such complaints mostly took place in Block 4, while Blocks 1 and 5 were comparatively blessed with water quality. Compared with those in tap water, the complaint of water quality was rather less in well water.

6) Conditions of Wells

The well depth distribution is shown below. Between 2.4 and 30 m and 79.7% wells had depths of not more than 10 m. The almost wells with depths of more than 10 m were located in Block 5.

| Block No.                        | <5m          | >5m<br><10m | >10m<br><15m | >15m<br><20m | >20m<br><30m | Un-<br>known | Total |
|----------------------------------|--------------|-------------|--------------|--------------|--------------|--------------|-------|
| 1                                | 13           | 11          | 1            | -            | -            | -            | 25    |
| 2                                | -            | -           | -            | -            | -            | -            | -     |
| 3                                | -            | 2           | -            | -            | -            | -            | 2     |
| 4                                | 10           | 10          | 1            | -            | -            | -            | 21    |
| 5                                | 1            | 4           | 5            | 5            | 1            | -            | 16    |
| Total                            | 24           | 27          | 7            | 5            | 1            | -            |       |
| Well Dep.<br>(m)                 | 4.4<br>(24)  | 7.5<br>(27) | 14.0<br>(7)  | 19.2<br>(5)  | 30.0<br>(1)  |              |       |
| Water Dep.<br>(m)                | 2.6<br>(24)  | 4.5<br>(26) | 8.6<br>(7)   | 13.2<br>(5)  | 27.0<br>(1)  |              |       |
| Operation<br>Time (h/d)          | 1.9<br>(10)  | 1.6<br>(15) | 1.8<br>(6)   | 9.3<br>(4)   | 2.0<br>(1)   |              |       |
| No. of<br>Fetching<br>Time (1/d) | 13.3<br>(14) | 6.1<br>(10) | 10.2<br>(2)  | 2.0<br>(1)   | -<br>(-)     |              |       |

The figures in parentheses show the number of wells used for the average calculation.

7) Average Monthly Water Consumption, Water Charge and Willingness-to-Pay.

Regarding the average monthly water consumption, 44.7% belonged to the up-to-15 cu m bracket and 31.2% to the 16-30 cu m bracket.

27.7% of the respondents paid for the water charge in the up-to-50 Baht bracket and 37.6% in the 51-100 Baht brackets, while, according to the result on the willingness-to-pay for water charge, 41.1% wanted that the water charge would be in the up-to-50 Baht bracket and 39.7% in the 51-100 Baht bracket. The expectant amount was rather less than the actual payment.

8) Willingness-to-Connect

Out of 183 respondents, 42 didn't use the municipal system at present. However, 49.6% was willing to connect to the municipal system. Such people mainly lived in Blocks 1, 4 and 5. They wanted that the connection fee would be less than 2,500 Baht (65%) and the water charge less than 100 Baht (85.0%), which a little bit more than that of existing consumers as mentioned above.

Reasons for unwillingness-to-connect were summarized below.

| Block No.                              | 1         | 2        | 3        | 4        | 5        | Total     |
|--|-----------|----------|----------|----------|----------|-----------|
| There is a well                        | 2         | -        | -        | 2        | -        | 4         |
| Well water is enough                   | -         | -        | -        | 5        | -        | 4         |
| Don't use much water                   | 2         | -        | -        | -        | -        | 2         |
| Not necessary                          | 1         | -        | -        | -        | -        | 1         |
| Lack of money                          | -         | -        | -        | -        | 1        | 1         |
| Tap water is expensive in installation | 1         | -        | -        | 2        | -        | 3         |
| Tap water is expensive                 | 3         | -        | -        | -        | -        | 3         |
| Others                                 | 1         | -        | -        | -        | 1        | 2         |
| Unknown                                | 1         | -        | -        | -        | -        | 1         |
| <b>Total</b>                           | <b>11</b> | <b>-</b> | <b>-</b> | <b>9</b> | <b>2</b> | <b>22</b> |

Contents of others were as follows:

- o It will take time to connect the municipal system and the connection work will be difficult.
- o Although having already paid for the connection fee, I give up it due to no work.

Most people who were unwilling to connect to the municipal system thought that they already had wells and those were enough or clean. Wells were very close and indispensable to their living.

Table A1-5-1 SUMMARY OF QUESTIONNAIR SURVEY IN THUNG SONG

| Block No.                        | 1   | 2   | 3   | 4   | 5   | Total | Rate (%) |
|----------------------------------|-----|-----|-----|-----|-----|-------|----------|
| No. of Samples                   | 40  | 31  | 31  | 50  | 31  | 183   |          |
| 1. General                       |     |     |     |     |     |       |          |
| 1.1 Address                      |     |     |     |     |     |       |          |
| 1.2 Type of House                |     |     |     |     |     |       |          |
| Residential                      | 26  | 4   | 14  | 37  | 20  | 101   | 55.2     |
| Commercial                       | 14  | 26  | 17  | 12  | 11  | 80    | 43.7     |
| Residential/Commercial           | -   | 1   | -   | 1   | -   | 2     | 1.1      |
| Unknown                          | -   | -   | -   | -   | -   | -     | -        |
| 1.3 No. of Persons in Family     | 178 | 142 | 165 | 249 | 184 | 918   |          |
| Unknown (No. of Samples)         | -   | -   | -   | -   | -   | -     | -        |
| 1.4 No. of Employees             | 66  | 69  | 93  | 102 | 104 | 434   |          |
| Unknown (No. of Samples)         | -   | -   | -   | -   | -   | -     | -        |
| 1.5 Ave. Monthly Income          |     |     |     |     |     |       |          |
| Baht                             |     |     |     |     |     |       |          |
| up to 2,000                      | 5   | 4   | 6   | 8   | 3   | 26    | 14.2     |
| 2,001-3,000                      | 17  | 10  | 4   | 27  | 4   | 62    | 33.9     |
| 3,001-4,500                      | 9   | 6   | 4   | 5   | 5   | 29    | 15.9     |
| 4,501-6,000                      | 5   | 4   | 9   | 6   | 9   | 33    | 18.0     |
| 6,001-7,500                      | 3   | -   | 3   | 1   | 2   | 9     | 4.9      |
| 7,501-10,000                     | 1   | 3   | 4   | 1   | 2   | 11    | 6.0      |
| 10,001-15,000                    | -   | 2   | 1   | 2   | 5   | 10    | 5.5      |
| 15,001-50,000                    | -   | 2   | -   | -   | -   | 2     | 1.1      |
| Over 50,000                      | -   | -   | -   | -   | 1   | 1     | 0.5      |
| Unknown                          | -   | -   | -   | -   | -   | -     | -        |
| 1.6 Ave. Monthly Medical Expense |     |     |     |     |     |       |          |
| Baht                             |     |     |     |     |     |       |          |
| up to 50                         | 4   | 20  | 18  | 13  | 18  | 73    | 39.9     |
| 51-100                           | 16  | 1   | 2   | 2   | 6   | 27    | 14.7     |
| 101-200                          | 7   | -   | 1   | 11  | 2   | 21    | 11.5     |
| 201-500                          | 9   | 4   | 4   | 16  | 5   | 38    | 20.8     |
| 501-1,000                        | 2   | -   | 5   | 6   | -   | 13    | 7.1      |
| 1,001-2,000                      | -   | 3   | -   | 2   | -   | 5     | 2.7      |
| 2,001-5,000                      | -   | 1   | 1   | -   | -   | 2     | 1.1      |
| Over 5,000                       | -   | 2   | -   | -   | -   | 2     | 1.1      |
| Unknown                          | 2   | -   | -   | -   | -   | -     | 1.1      |
| 2. Type of Water Supply          |     |     |     |     |     |       |          |
| Municipal System                 | 14  | 30  | 25  | 28  | 13  | 110   | 60.1     |
| Combined                         | 8   | 1   | 6   | 6   | 10  | 31    | 16.9     |
| Other Sources                    | 18  | -   | -   | 16  | 8   | 42    | 23.0     |
| Unknown                          | -   | -   | -   | -   | -   | -     | -        |
| 3. Municipal System              |     |     |     |     |     |       |          |
| 3.1 Pressure                     |     |     |     |     |     |       |          |
| Low                              | 12  | 16  | 12  | 8   | 19  | 67    | 47.5     |
| High                             | 10  | 14  | 18  | 26  | 4   | 72    | 51.1     |
| Unknown                          | -   | 1   | 1   | -   | -   | 2     | 1.4      |
| 3.2 Quantity                     |     |     |     |     |     |       |          |
| Sufficient                       | 15  | 31  | 30  | 28  | 1   | 105   | 74.5     |
| Not Sufficient                   | 7   | -   | -   | 6   | 22  | 35    | 24.8     |
| Unknown                          | -   | -   | 1   | -   | -   | 1     | 0.7      |

Table A1-5-1 SUMMARY OF QUESTIONNAIR SURVEY IN THUNG SONG (CONT'D)

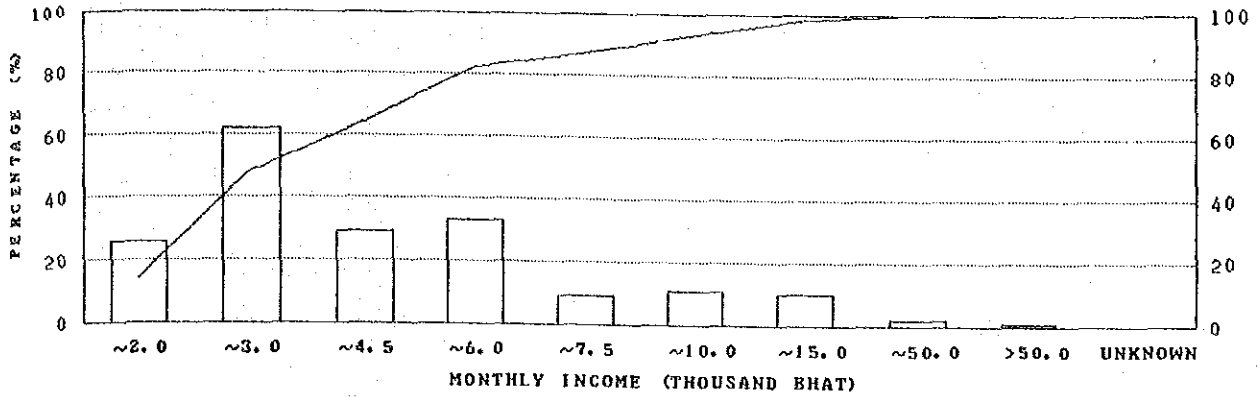
| Block No.                           | 1  | 2  | 3  | 4  | 5  | Total | Rate (%) |
|-------------------------------------|----|----|----|----|----|-------|----------|
| 4. Other Sources                    |    |    |    |    |    |       |          |
| Rain/River                          | 1  | -  | 4  | -  | 2  | 7     |          |
| Pond/Reservoir                      | -  | 1  | -  | -  | -  | 1     |          |
| Water Vendor                        | -  | -  | -  | 2  | -  | 2     |          |
| Groundwater-Shallow Well            | 25 | -  | 2  | 21 | 16 | 64    |          |
| -Deep Well                          | -  | -  | -  | -  | -  | -     |          |
| Unknown                             | -  | -  | -  | -  | -  | -     |          |
| 5. Potability                       |    |    |    |    |    |       |          |
| Drinking                            | 35 | 1  | 2  | 40 | 25 | 103   | 56.3     |
| Not Drinking                        | 5  | -  | 2  | 10 | -  | 17    | 9.3      |
| Both                                | -  | 30 | 27 | -  | -  | 57    | 31.1     |
| Unknown                             | -  | -  | -  | -  | 6  | 6     | 3.3      |
| 6. Water Quality (Municipal System) |    |    |    |    |    |       |          |
| 6.1 Color                           |    |    |    |    |    |       |          |
| Yes                                 | 9  | 15 | 19 | 5  | 3  | 51    | 36.2     |
| No                                  | 11 | 16 | 12 | 29 | 19 | 87    | 61.7     |
| Unknown                             | 2  | -  | -  | -  | 1  | 3     | 2.1      |
| 6.2 Smell                           |    |    |    |    |    |       |          |
| Yes                                 | 14 | 16 | 23 | 9  | 5  | 67    | 47.5     |
| No                                  | 8  | 15 | 8  | 25 | 17 | 73    | 51.8     |
| Unknown                             | -  | -  | -  | -  | 1  | 1     | 0.7      |
| 6.3 Turbidity                       |    |    |    |    |    |       |          |
| Yes                                 | 12 | 15 | 21 | 6  | 17 | 71    | 50.4     |
| No                                  | 9  | 16 | 10 | 28 | 5  | 68    | 48.2     |
| Unknown                             | 1  | -  | -  | -  | 1  | 2     | 1.4      |
| 7. Ave. Monthly Water Consumption   |    |    |    |    |    |       |          |
| Up to 15 cu m                       | 8  | 20 | 12 | 11 | 12 | 63    | 44.7     |
| 16-30 cu m                          | 9  | 7  | 7  | 14 | 7  | 44    | 31.2     |
| 31-50 cu m                          | 1  | 2  | 3  | 1  | -  | 7     | 5.0      |
| 51-75 cu m                          | 1  | 1  | 1  | -  | -  | 3     | 2.1      |
| 76-100 cu m                         | 2  | 1  | 6  | -  | -  | 9     | 6.4      |
| 101-150 cu m                        | -  | -  | 2  | 1  | -  | 3     | 2.1      |
| 151-200 cu m                        | -  | -  | -  | -  | -  | -     | -        |
| 201-300 cu m                        | -  | -  | -  | -  | -  | -     | -        |
| Over 300 cu m                       | -  | -  | -  | -  | -  | -     | -        |
| Unknown                             | 1  | -  | -  | 7  | 4  | 12    | 8.5      |
| 8. Ave. Monthly Water Charge        |    |    |    |    |    |       |          |
| Baht                                |    |    |    |    |    |       |          |
| Up to 50                            | 8  | 8  | 7  | 5  | 11 | 39    | 27.7     |
| 51-100                              | 8  | 13 | 8  | 19 | 5  | 53    | 37.6     |
| 101-150                             | 2  | 8  | 5  | 5  | 4  | 24    | 17.0     |
| 151-200                             | 1  | -  | 1  | 4  | 2  | 8     | 5.7      |
| 201-300                             | 1  | 1  | 6  | -  | -  | 8     | 5.7      |
| 301-500                             | 1  | 1  | 1  | -  | -  | 3     | 2.1      |
| 501-1,000                           | -  | -  | 2  | 1  | 1  | 4     | 2.8      |
| Over 1,000                          | -  | -  | 1  | -  | -  | 1     | 0.7      |
| Unknown                             | 1  | -  | -  | -  | -  | 1     | 0.7      |

Table A1-5-1 SUMMARY OF QUESTIONNAIR SURVEY IN THUNG SONG (CONT'D)

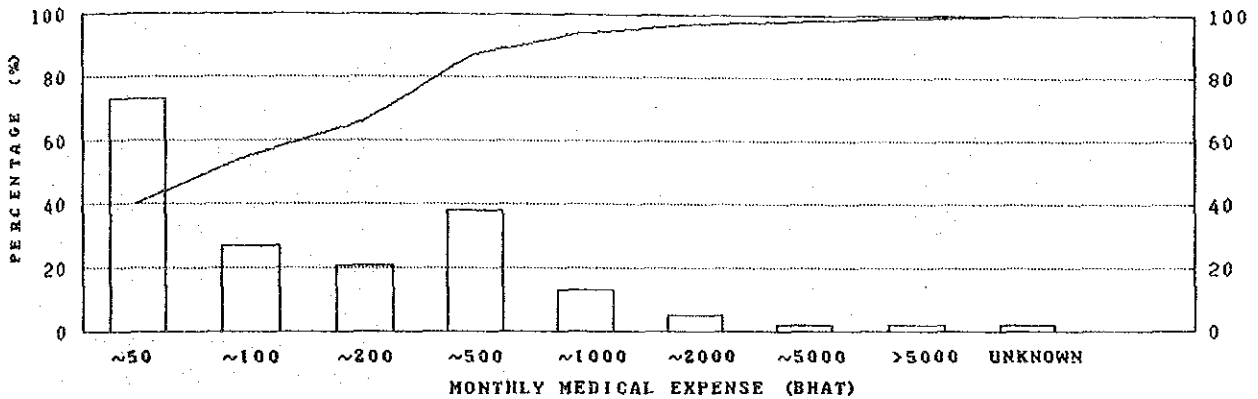
| Block No.                                 | 1  | 2  | 3  | 4  | 5  | Total | Rate (%) |
|---|----|----|----|----|----|-------|----------|
| 9. Willingness to Pay                     |    |    |    |    |    |       |          |
| Baht                                      |    |    |    |    |    |       |          |
| Up to 50                                  | 15 | 8  | 14 | 12 | 9  | 58    | 41.1     |
| 51-100                                    | 5  | 13 | 11 | 20 | 7  | 56    | 39.7     |
| 101-200                                   | 2  | 8  | 4  | 1  | 4  | 19    | 13.5     |
| 201-500                                   | -  | 2  | 2  | -  | 2  | 6     | 4.3      |
| 501-1,000                                 | -  | -  | -  | 1  | -  | 1     | 0.7      |
| Over 1,000                                | -  | -  | -  | -  | 1  | 1     | 0.7      |
| Unknown                                   | -  | -  | -  | -  | -  | -     | -        |
| 10. Water Quality (Other Source)          |    |    |    |    |    |       |          |
| 10.1 Color                                |    |    |    |    |    |       |          |
| Yes                                       | 2  | -  | 1  | 11 | 3  | 17    | 23.3     |
| No  | 23 | 1  | 3  | 10 | 14 | 51    | 69.9     |
| Unknown                                   | 1  | -  | 2  | 1  | 1  | 5     | 6.8      |
| 10.2 Smell                                |    |    |    |    |    |       |          |
| Yes                                       | 5  | 1  | -  | 6  | 2  | 14    | 19.2     |
| No  | 21 | -  | 4  | 15 | 15 | 55    | 75.3     |
| Unknown                                   | -  | -  | 2  | 1  | 1  | 4     | 5.5      |
| 10.3 Turbidity                            |    |    |    |    |    |       |          |
| Yes                                       | 5  | -  | -  | 11 | 2  | 18    | 24.6     |
| No  | 21 | 1  | 4  | 10 | 15 | 51    | 69.9     |
| Unknown                                   | -  | -  | 2  | 1  | 1  | 4     | 5.5      |
| 11. Willingness to Connect                |    |    |    |    |    |       |          |
| Yes                                       | 7  | -  | -  | 7  | 6  | 20    | 47.6     |
| No  | 11 | -  | -  | 9  | 2  | 22    | 52.4     |
| Unknown                                   | -  | -  | -  | -  | -  | -     | -        |
| 12. Willingness to Pay for Connection Fee |    |    |    |    |    |       |          |
| Baht                                      |    |    |    |    |    |       |          |
| Up to 1,000                               | 3  | -  | -  | -  | -  | 3     | 15.0     |
| 1,001-2,000                               | 3  | -  | -  | 1  | 6  | 10    | 50.0     |
| 2,001-2,500                               | -  | -  | -  | 1  | -  | 1     | 5.0      |
| 2,501-3,000                               | 1  | -  | -  | 4  | -  | 5     | 25.0     |
| 3,001-4,000                               | -  | -  | -  | 1  | -  | 1     | 5.0      |
| 4,001-5,000                               | -  | -  | -  | -  | -  | -     | -        |
| 5,001-6,000                               | -  | -  | -  | -  | -  | -     | -        |
| Over 6,000                                | -  | -  | -  | -  | -  | -     | -        |
| Unknown                                   | -  | -  | -  | -  | -  | -     | -        |
| 13. Willingness to Pay for Water Charge   |    |    |    |    |    |       |          |
| Baht                                      |    |    |    |    |    |       |          |
| Up to 50                                  | 4  | -  | -  | 1  | -  | 5     | 25.0     |
| 51-100                                    | 3  | -  | -  | 3  | 6  | 12    | 60.0     |
| 101-200                                   | -  | -  | -  | 3  | -  | 3     | 15.0     |
| 201-500                                   | -  | -  | -  | -  | -  | -     | -        |
| 501-1,000                                 | -  | -  | -  | -  | -  | -     | -        |
| Over 1,000                                | -  | -  | -  | -  | -  | -     | -        |
| Unknown                                   | -  | -  | -  | -  | -  | -     | -        |



MONTHLY INCOME DISTRIBUTION



MONTHLY MEDICAL EXPENSE DISTRIBUTION



TYPE OF WATER SOURCE & WILLINGNESS-TO-CONNECT

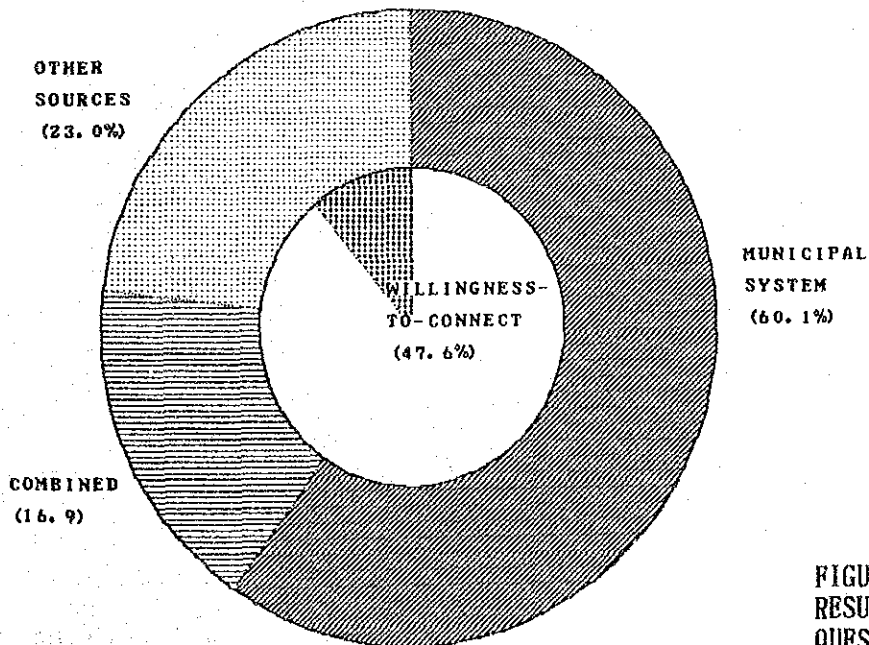
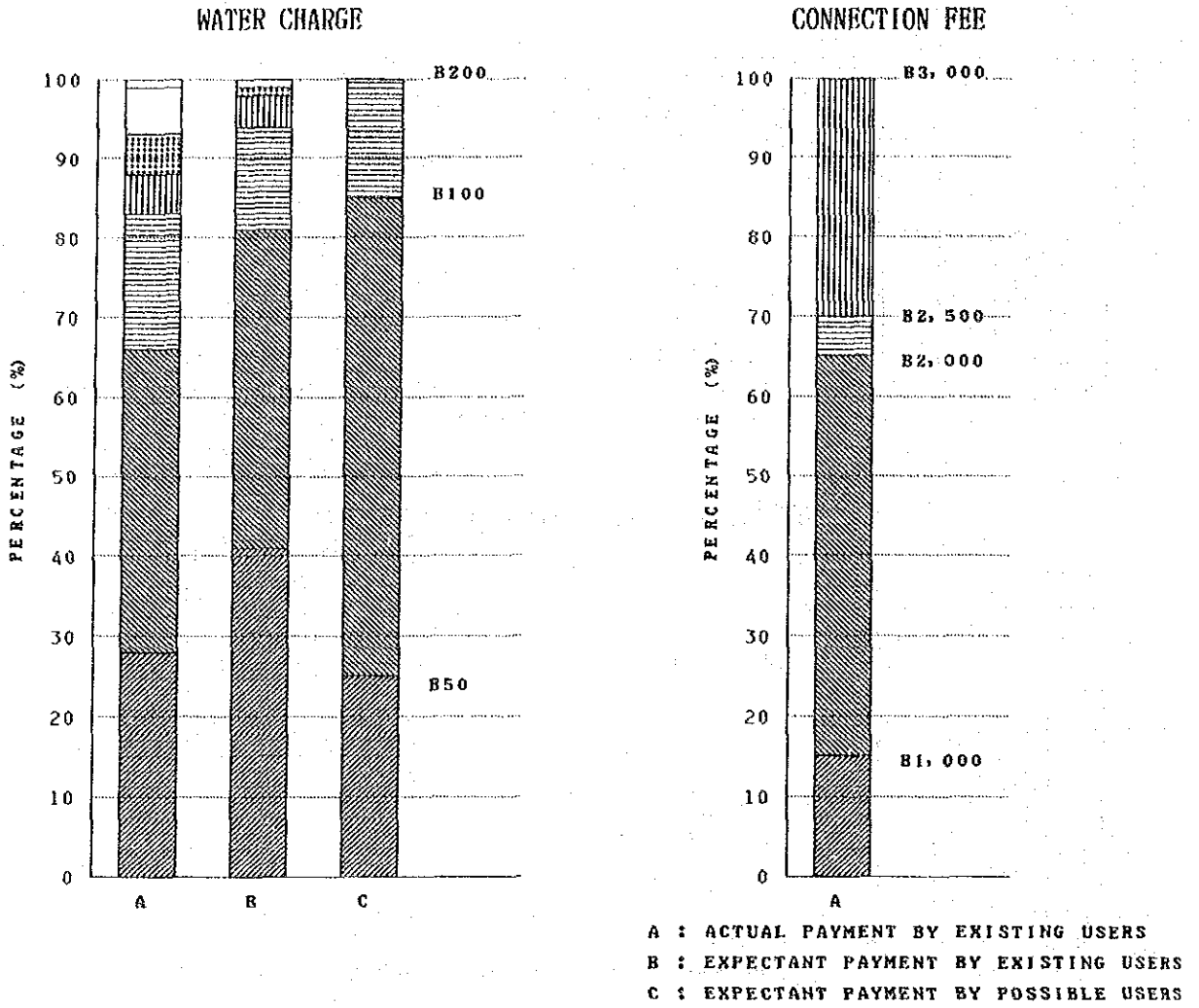


FIGURE A1-5-2  
RESULTS OF  
QUESTIONNAIRE SURVEY (1)  
(THUNG SONG)

WILLINGNESS-TO-PAY



COMPLAINTS OF RESPONDENTS

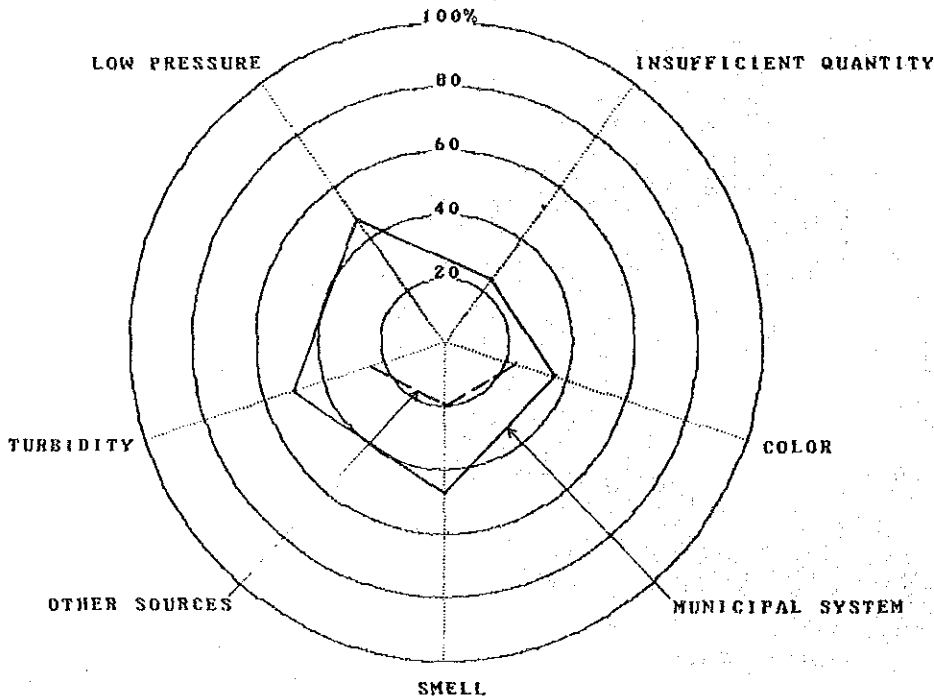


FIGURE A1-5-2  
RESULTS OF  
QUESTIONNAIRE SURVEY (2)  
(THUNG SONG)

**APPENDIX A-6-1**

**Construction Unit Cost**



Unit Cost

| Item                      | Material | Fitting | Labor                     | SubTotal | Transprt<br>( $<800kw$ ) | Profit<br>etc.(21%<br>(w/10%cont) | Total 1 | Pavement | Total 2 |
|---------------------------|----------|---------|---------------------------|----------|--------------------------|-----------------------------------|---------|----------|---------|
| Pipeline                  |          |         |                           |          |                          |                                   |         |          |         |
|                           | <*****>  |         | P W A 's Unit Rate (1987) |          |                          | *****>                            |         |          |         |
| a. A/C Pipe(Normal Tytpe) | (25%)    |         |                           |          |                          |                                   |         |          |         |
| 100 mm                    | 85       | 21      | 56                        | 162      | 6                        | 35                                | 224     | 140      | 364     |
| 150 mm                    | 142      | 36      | 77                        | 255      | 11                       | 56                                | 353     | 154      | 507     |
| 200 mm                    | 255      | 64      | 90                        | 409      | 19                       | 90                                | 569     | 166      | 735     |
| 250 mm                    | 352      | 88      | 126                       | 566      | 29                       | 125                               | 792     | 179      | 971     |
| 300 mm                    | 507      | 127     | 167                       | 801      | 40                       | 177                               | 1119    | 223      | 1342    |
| 400 mm                    | 970      | 243     | 248                       | 1461     | 80                       | 324                               | 2050    | 248      | 2298    |
| 500 mm                    | 1362     | 341     | 278                       | 1981     | 132                      | 444                               | 2812    | 283      | 3095    |
| 600 mm                    | 1761     | 440     | 354                       | 2555     | 161                      | 570                               | 3615    | 319      | 3934    |
| b. Steel Pipe             | (35%)    |         |                           |          |                          |                                   |         |          |         |
| 150 mm                    | 545      | 191     | 99                        | 835      | 12                       | 178                               | 1127    | 140      | 1267    |
| 200 mm                    | 720      | 252     | 111                       | 1083     | 22                       | 232                               | 1471    | 154      | 1625    |
| 250 mm                    | 1080     | 378     | 153                       | 1611     | 38                       | 346                               | 2195    | 166      | 2361    |
| 300 mm                    | 1330     | 465     | 202                       | 1998     | 58                       | 432                               | 2736    | 179      | 2915    |
| 400 mm                    | 1420     | 497     | 250                       | 2167     | 80                       | 472                               | 2991    | 223      | 3214    |
| 500 mm                    | 1785     | 625     | 361                       | 2771     | 160                      | 615                               | 3901    | 248      | 4149    |
| 600 mm                    | 2140     | 749     | 468                       | 3357     | 264                      | 760                               | 4820    | 283      | 5103    |
| 700 mm                    | 2495     | 873     | 582                       | 3950     | 322                      | 897                               | 5686    | 319      | 6005    |

Unit Cost

For Transmission Pipeline (Transportation < 800 km)

| Item   | Material | Fitting<br>(10%) | Labor | SubTotal | Transprt<br>(<800km) | Profit<br>etc.(21%) | Total 1<br>(w/10%cont) | Pavement | Total 2                | Adopted<br>(1988) |      |        |  |
|--|----------|------------------|-------|----------|----------------------|---------------------|------------------------|----------|------------------------|-------------------|------|--------|--|
| <***** Unit Rate Based on Pipe Material Cost as of December, 1988 *****> |          |                  |       |          |                      |                     |                        |          |                        |                   |      |        |  |
| a. A/C Pipe (Class 20 Normal type)                                       |          |                  |       |          |                      |                     |                        |          |                        |                   |      |        |  |
|  | (10 %)   |                  |       |          |                      |                     |                        |          | PWA<br>Price<br>(1987) | Ratio             |      |        |  |
| 100 mm   | 115      | 12               | 63    | 190      | 7                    | 41                  | 261                    | 153      | 414                    | 364               | 1.14 | 410    |  |
| 150 mm   | 189      | 19               | 87    | 295      | 12                   | 64                  | 408                    | 168      | 577                    | 507               | 1.14 | 580    |  |
| 200 mm   | 328      | 33               | 101   | 462      | 21                   | 101                 | 643                    | 181      | 824                    | 735               | 1.12 | 820    |  |
| 250 mm   | 454      | 45               | 142   | 641      | 32                   | 141                 | 895                    | 196      | 1091                   | 971               | 1.12 | 1,090  |  |
| 300 mm   | 643      | 64               | 188   | 895      | 44                   | 197                 | 1249                   | 244      | 1493                   | 1342              | 1.11 | 1,490  |  |
| 400 mm   | 1217     | 122              | 279   | 1618     | 87                   | 358                 | 2270                   | 271      | 2541                   | 2298              | 1.11 | 2,540  |  |
| 500 mm   | 1699     | 170              | 313   | 2182     | 144                  | 488                 | 3096                   | 309      | 3405                   | 3095              | 1.10 | 3,410  |  |
| 600 mm   | 2187     | 219              | 398   | 2804     | 176                  | 626                 | 3967                   | 349      | 4315                   | 3934              | 1.10 | 4,320  |  |
| b. Steel Pipe  |          |                  |       |          |                      |                     |                        |          |                        |                   |      |        |  |
|  | (15 %)   |                  |       |          |                      |                     |                        |          |                        |                   |      |        |  |
| 150 mm   | 550      | 83               | 111   | 744      | 13                   | 159                 | 1008                   | 168      | 1176                   | 1267              | 0.93 | 1,270  |  |
| 200 mm   | 908      | 136              | 125   | 1168     | 24                   | 250                 | 1587                   | 181      | 1769                   | 1625              | 1.09 | 1,770  |  |
| 250 mm   | 1210     | 182              | 172   | 1564     | 42                   | 337                 | 2136                   | 196      | 2332                   | 2361              | 0.99 | 2,360  |  |
| 300 mm   | 1507     | 226              | 227   | 1960     | 63                   | 425                 | 2693                   | 244      | 2937                   | 2915              | 1.01 | 2,940  |  |
| 400 mm   | 1887     | 283              | 281   | 2451     | 87                   | 533                 | 3378                   | 271      | 3649                   | 3214              | 1.14 | 3,650  |  |
| 500 mm   | 2261     | 339              | 406   | 3006     | 175                  | 668                 | 4233                   | 309      | 4542                   | 4149              | 1.09 | 4,540  |  |
| 600 mm   | 2723     | 408              | 526   | 3657     | 288                  | 829                 | 5252                   | 349      | 5600                   | 5103              | 1.10 | 5,600  |  |
| 700 mm   | 3179     | 477              | 655   | 4311     | 352                  | 979                 | 6206                   | 407      | 6612                   | 6005              | 1.10 | 6,610  |  |
| 800 mm   | 4527     | 679              | 932   | 6138     | 460                  | 1385                | 8781                   | 465      | 9246                   |                   |      | 9,250  |  |
| 900 mm   | 5104     | 766              | 1051  | 6921     | 582                  | 1575                | 9986                   | 523      | 10508                  |                   |      | 10,510 |  |
| 1000 mm  | 6804     | 1021             | 1401  | 9225     | 718                  | 2088                | 13234                  | 581      | 13815                  |                   |      | 13,820 |  |
| 1100 mm  | 7926     | 1189             | 1632  | 10746    | 869                  | 2439                | 15460                  | 639      | 16099                  |                   |      | 16,100 |  |
| 1200 mm  | 9048     | 1357             | 1863  | 12268    | 1034                 | 2793                | 17705                  | 697      | 18402                  |                   |      | 18,400 |  |
| 1350 mm  | 11000    | 1650             | 2265  | 14915    | 1309                 | 3407                | 21594                  | 784      | 22378                  |                   |      | 22,380 |  |
| 1500 mm  | 12953    | 1943             | 2667  | 17563    | 1616                 | 4027                | 25526                  | 871      | 26398                  |                   |      | 26,400 |  |

\*\*\* Note: Pipe material prices are estimated from the contractor's purchasing price as of Dec. 1988

Unit Cost

For Distribution Pipeline (Transportation < 800 km)

| Item | Material | Fitting | Labor | SubTotal | Transprt<br>(<800km) | Profit<br>etc. (21%)(w/10%cont) | Total 1 | Pavement |  | Total 2 | Adopted<br>(1988) |
|------|----------|---------|-------|----------|----------------------|---------------------------------|---------|----------|--|---------|-------------------|
|------|----------|---------|-------|----------|----------------------|---------------------------------|---------|----------|--|---------|-------------------|

| ***** Unit Rate Based on Pipe Material Cost as of December, 1988 |       |      |      |       |      |      |       | ***** |       | PWA<br>Price<br>(1987) | Ratio |        |
|--|-------|------|------|-------|------|------|-------|-------|-------|------------------------|-------|--------|
| a. A/C Pipe (Class 20 Normal type)                               |       |      |      |       |      |      |       |       |       |                        |       |        |
| (25 X)   |       |      |      |       |      |      |       |       |       |                        |       |        |
| 100 mm   | 115   | 29   | 63   | 207   | 7    | 45   | 284   | 153   | 437   | 364                    | 1.20  | 440    |
| 150 mm   | 189   | 47   | 87   | 323   | 12   | 70   | 446   | 168   | 614   | 507                    | 1.21  | 610    |
| 200 mm   | 328   | 82   | 101  | 511   | 21   | 112  | 708   | 181   | 890   | 735                    | 1.21  | 890    |
| 250 mm   | 454   | 113  | 142  | 709   | 32   | 155  | 986   | 196   | 1181  | 971                    | 1.22  | 1,180  |
| 300 mm   | 643   | 161  | 188  | 991   | 44   | 217  | 1378  | 244   | 1621  | 1342                   | 1.21  | 1,620  |
| 400 mm   | 1217  | 304  | 279  | 1801  | 87   | 397  | 2513  | 271   | 2784  | 2298                   | 1.21  | 2,780  |
| 500 mm   | 1699  | 425  | 313  | 2437  | 144  | 542  | 3435  | 309   | 3744  | 3095                   | 1.21  | 3,740  |
| 600 mm   | 2187  | 547  | 398  | 3132  | 176  | 695  | 4403  | 349   | 4752  | 3934                   | 1.21  | 4,750  |
| b. Steel Pipe  |       |      |      |       |      |      |       |       |       |                        |       |        |
| (35 X)   |       |      |      |       |      |      |       |       |       |                        |       |        |
| 150 mm   | 550   | 193  | 111  | 854   | 13   | 182  | 1154  | 168   | 1322  | 1267                   | 1.04  | 1,320  |
| 200 mm   | 908   | 318  | 125  | 1350  | 24   | 289  | 1829  | 181   | 2010  | 1625                   | 1.24  | 2,010  |
| 250 mm   | 1210  | 424  | 172  | 1806  | 42   | 388  | 2459  | 196   | 2654  | 2361                   | 1.12  | 2,650  |
| 300 mm   | 1507  | 527  | 227  | 2262  | 63   | 488  | 3095  | 244   | 3338  | 2915                   | 1.15  | 3,340  |
| 400 mm   | 1887  | 660  | 281  | 2828  | 87   | 612  | 3880  | 271   | 4151  | 3214                   | 1.29  | 4,150  |
| 500 mm   | 2261  | 791  | 406  | 3458  | 175  | 763  | 4835  | 309   | 5144  | 4149                   | 1.24  | 5,140  |
| 600 mm   | 2723  | 953  | 526  | 4202  | 288  | 943  | 5977  | 349   | 6325  | 5103                   | 1.24  | 6,330  |
| 700 mm   | 3179  | 1113 | 655  | 4946  | 352  | 1113 | 7052  | 407   | 7459  | 6005                   | 1.24  | 7,460  |
| 800 mm   | 4527  | 1584 | 932  | 7043  | 460  | 1576 | 9986  | 465   | 10451 |                        |       | 10,450 |
| 900 mm   | 5104  | 1786 | 1051 | 7941  | 582  | 1790 | 11344 | 523   | 11867 |                        |       | 11,870 |
| 1000 mm  | 6804  | 2381 | 1401 | 10586 | 718  | 2374 | 15045 | 581   | 15626 |                        |       | 15,630 |
| 1100 mm  | 7926  | 2774 | 1632 | 12332 | 869  | 2772 | 17570 | 639   | 18209 |                        |       | 18,210 |
| 1200 mm  | 9048  | 3167 | 1863 | 14077 | 1034 | 3173 | 20113 | 697   | 20810 |                        |       | 20,810 |
| 1350 mm  | 11000 | 3850 | 2265 | 17115 | 1309 | 3869 | 24522 | 784   | 25307 |                        |       | 25,310 |
| 1500 mm  | 12953 | 4533 | 2667 | 20153 | 1616 | 4571 | 28974 | 871   | 29846 |                        |       | 29,850 |

\*\*\* Note: Pipe material prices are estimated from the contractor's purchasing price as of Dec. 1988

Unit Cost

For Transmission Pipeline (Transportation >= 800 km)

| Item | Material | Fitting<br>(10%) | Labor | SubTotal | Transprt<br>(>=800km)etc.<br>(21%)(w/10%cont) | Profit | Total 1 | Pavement | Total 2 | Adopted<br>(1988) |
|------|----------|------------------|-------|----------|---|--------|---------|----------|---------|-------------------|
|------|----------|------------------|-------|----------|---|--------|---------|----------|---------|-------------------|

<\*\*\*\*\* Unit Rate Based on Pipe Material Cost as of December, 1988 \*\*\*\*\*>

a. A/C Pipe (Class 20 Normal type)  
(10 %)

|        |      |     |     |      |     |     |      |     |      |      |      |       |
|--------|------|-----|-----|------|-----|-----|------|-----|------|------|------|-------|
| 100 mm | 115  | 12  | 63  | 190  | 13  | 43  | 270  | 153 | 423  | 364  | 1.16 | 420   |
| 150 mm | 189  | 19  | 87  | 295  | 24  | 67  | 424  | 168 | 593  | 507  | 1.17 | 590   |
| 200 mm | 328  | 33  | 101 | 462  | 42  | 106 | 670  | 181 | 852  | 735  | 1.16 | 850   |
| 250 mm | 454  | 45  | 142 | 641  | 63  | 148 | 937  | 196 | 1133 | 971  | 1.17 | 1,130 |
| 300 mm | 643  | 64  | 188 | 895  | 87  | 206 | 1308 | 244 | 1551 | 1342 | 1.16 | 1,550 |
| 400 mm | 1217 | 122 | 279 | 1618 | 175 | 377 | 2387 | 271 | 2658 | 2298 | 1.16 | 2,660 |
| 500 mm | 1699 | 170 | 313 | 2182 | 288 | 519 | 3288 | 309 | 3597 | 3095 | 1.16 | 3,600 |
| 600 mm | 2187 | 219 | 398 | 2804 | 352 | 663 | 4201 | 349 | 4549 | 3934 | 1.16 | 4,550 |

b. Steel Pipe (15 %)

|         |       |      |      |       |      |      |       |     |       |      |      |        |
|---------|-------|------|------|-------|------|------|-------|-----|-------|------|------|--------|
| 150 mm  | 550   | 83   | 111  | 744   | 26   | 162  | 1025  | 168 | 1193  | 1267 | 0.94 | 1,270  |
| 200 mm  | 908   | 136  | 125  | 1168  | 48   | 255  | 1619  | 181 | 1801  | 1625 | 1.11 | 1,800  |
| 250 mm  | 1210  | 182  | 172  | 1564  | 83   | 346  | 2192  | 196 | 2387  | 2361 | 1.01 | 2,390  |
| 300 mm  | 1507  | 226  | 227  | 1960  | 127  | 438  | 2778  | 244 | 3022  | 2915 | 1.04 | 3,020  |
| 400 mm  | 1887  | 283  | 281  | 2451  | 175  | 551  | 3495  | 271 | 3766  | 3214 | 1.17 | 3,770  |
| 500 mm  | 2261  | 339  | 406  | 3006  | 350  | 705  | 4466  | 309 | 4775  | 4149 | 1.15 | 4,780  |
| 600 mm  | 2723  | 408  | 526  | 3657  | 577  | 889  | 5636  | 349 | 5984  | 5103 | 1.17 | 5,980  |
| 700 mm  | 3179  | 477  | 655  | 4311  | 704  | 1053 | 6674  | 407 | 7081  | 6005 | 1.18 | 7,080  |
| 800 mm  | 4527  | 679  | 932  | 6138  | 919  | 1482 | 9393  | 465 | 9857  |      |      | 9,860  |
| 900 mm  | 5104  | 766  | 1051 | 6921  | 1163 | 1698 | 10760 | 523 | 11283 |      |      | 11,280 |
| 1000 mm | 6804  | 1021 | 1401 | 9225  | 1436 | 2239 | 14190 | 581 | 14771 |      |      | 14,770 |
| 1100 mm | 7926  | 1189 | 1632 | 10746 | 1738 | 2622 | 16616 | 639 | 17256 |      |      | 17,260 |
| 1200 mm | 9048  | 1357 | 1863 | 12268 | 2068 | 3011 | 19081 | 697 | 19778 |      |      | 19,780 |
| 1350 mm | 11000 | 1650 | 2265 | 14915 | 2617 | 3682 | 23336 | 784 | 24120 |      |      | 24,120 |
| 1500 mm | 12953 | 1943 | 2667 | 17563 | 3231 | 4367 | 27677 | 871 | 28548 |      |      | 28,550 |

\*\*\* Note: Pipe material prices are estimated from the contractor's purchasing price as of Dec. 1988



Unit Cost

For Distribution Pipeline (Transportation >= 800 km)

| Item   | Material | Fitting | Labor | SubTotal | Transprt<br>(>=800km)etc.(21%) | Profit<br>(w/10%cont) | Total 1 | Pavement | Total 2 | Adopted<br>(1988) |      |        |
|--|----------|---------|-------|----------|--------------------------------|-----------------------|---------|----------|---------|-------------------|------|--------|
| <***** Unit Rate Based on Pipe Material Cost as of December, 1988 *****> |          |         |       |          |                                |                       |         |          |         |                   |      |        |
| a. A/C Pipe (Class 20 Normal type)                                       |          |         |       |          |                                |                       |         |          |         |                   |      |        |
|  | (25 x)   |         |       |          |                                |                       |         |          |         |                   |      |        |
| 100 mm   | 115      | 29      | 63    | 207      | 13                             | 46                    | 293     | 153      | 446     | 364               | 1.23 | 450    |
| 150 mm   | 189      | 47      | 87    | 323      | 24                             | 73                    | 462     | 168      | 630     | 507               | 1.24 | 630    |
| 200 mm   | 328      | 82      | 101   | 511      | 42                             | 116                   | 736     | 181      | 917     | 735               | 1.25 | 920    |
| 250 mm   | 454      | 113     | 142   | 709      | 63                             | 162                   | 1028    | 196      | 1223    | 971               | 1.26 | 1,220  |
| 300 mm   | 643      | 161     | 188   | 991      | 87                             | 227                   | 1436    | 244      | 1680    | 1342              | 1.25 | 1,680  |
| 400 mm   | 1217     | 304     | 279   | 1801     | 175                            | 415                   | 2630    | 271      | 2901    | 2298              | 1.26 | 2,900  |
| 500 mm   | 1699     | 425     | 313   | 2437     | 288                            | 572                   | 3627    | 309      | 3936    | 3095              | 1.27 | 3,940  |
| 600 mm   | 2187     | 547     | 398   | 3132     | 352                            | 732                   | 4637    | 349      | 4986    | 3934              | 1.27 | 4,990  |
| b. Steel Pipe  |          |         |       |          |                                |                       |         |          |         |                   |      |        |
|  | (35 x)   |         |       |          |                                |                       |         |          |         |                   |      |        |
| 150 mm   | 550      | 193     | 111   | 854      | 26                             | 185                   | 1171    | 168      | 1340    | 1267              | 1.06 | 1,340  |
| 200 mm   | 908      | 318     | 125   | 1350     | 48                             | 294                   | 1861    | 181      | 2042    | 1625              | 1.26 | 2,040  |
| 250 mm   | 1210     | 424     | 172   | 1806     | 83                             | 397                   | 2514    | 196      | 2709    | 2361              | 1.15 | 2,710  |
| 300 mm   | 1507     | 527     | 227   | 2262     | 127                            | 502                   | 3179    | 244      | 3423    | 2915              | 1.17 | 3,420  |
| 400 mm   | 1887     | 660     | 281   | 2828     | 175                            | 631                   | 3997    | 271      | 4268    | 3214              | 1.33 | 4,270  |
| 500 mm   | 2261     | 791     | 406   | 3458     | 350                            | 800                   | 5068    | 309      | 5377    | 4149              | 1.30 | 5,380  |
| 600 mm   | 2723     | 953     | 526   | 4202     | 577                            | 1004                  | 6361    | 349      | 6709    | 5103              | 1.31 | 6,710  |
| 700 mm   | 3179     | 1113    | 655   | 4946     | 704                            | 1187                  | 7520    | 407      | 7927    | 6005              | 1.32 | 7,930  |
| 800 mm   | 4527     | 1584    | 932   | 7043     | 919                            | 1672                  | 10598   | 465      | 11062   |                   |      | 11,060 |
| 900 mm   | 5104     | 1786    | 1051  | 7941     | 1163                           | 1912                  | 12118   | 523      | 12641   |                   |      | 12,640 |
| 1000 mm  | 6804     | 2381    | 1401  | 10586    | 1436                           | 2525                  | 16001   | 581      | 16582   |                   |      | 16,580 |
| 1100 mm  | 7926     | 2774    | 1632  | 12332    | 1738                           | 2955                  | 18726   | 639      | 19365   |                   |      | 19,370 |
| 1200 mm  | 9048     | 3167    | 1863  | 14077    | 2068                           | 3391                  | 21490   | 697      | 22187   |                   |      | 22,190 |
| 1350 mm  | 11000    | 3850    | 2265  | 17115    | 2617                           | 4144                  | 26264   | 784      | 27049   |                   |      | 27,050 |
| 1500 mm  | 12953    | 4533    | 2667  | 20153    | 3231                           | 4911                  | 31125   | 871      | 31996   |                   |      | 32,000 |

\*\*\* Note: Pipe material prices are estimated from the contractor's purchasing price as of Dec. 1988

Unit Cost

| Construction Works   | Price in 3 Lowest Tenders (1988)<br>(A) | Estimated Cost (A)*1.35 | PWA's Unit Cost (for 1987) | Adopted Cost (1988)    |
|--|---|-------------------------|----------------------------|------------------------|
| Concrete Work<br>(incl. Form Work, Scaffolding)                                    | Baht 2,200 /cu m                        | Baht 2,970 /cu m        | -                          |                        |
| Re-Bar   | Baht 18 /kg                             | Baht 24 /kg             | -                          |                        |
| Unit Concrete Cost<br>(incl. Form Work, Scaffolding, Re-Bar(100kg/cu m concrete))) |   | Baht 5,370 /cu m        | -                          | 5,400                  |
| Earth Work   |   |                         |                            |                        |
| Excavation (with Backfill)   | 55 /cu m                                | 79 /cu m                | -                          | 80                     |
| Soil Fill  | 53 /cu m                                | 76                      |                            | 120<br>(From PWA Cost) |
| Architectural Works  |   |                         |                            |                        |
| Administration Bldg.   | 4,516 /sq m                             | 6,451 /sq m             |                            |                        |
| Head Quarter Bldg.   | 3,612                                   | 5,160                   |                            | 5,000                  |
| Chlorination House   | Baht 2,830 /sq m                        | Baht 4,043 /sq m        | 3610 - 4300                | 3,800                  |
| Pump House<br>(excl. pump pit)   | Baht 1,860 /sq m                        | Baht 2,657 /sq m        | 3540 - 4200                | 3,600                  |

Unit Cost

| Construction Works           | PWA's Cost<br>(for 1987)<br>(Baht 1000) | Unit Cost<br>(Baht/cu m/h)<br>(A) | Estimated Cost<br>(for 1989)<br>(A)*1.30 | Adopted<br>Cost<br>(1988)  |
|------------------------------|---|-----------------------------------|--|----------------------------|
| <b>Treatment Facilities</b>  |   |                                   |  |                            |
|                              |   |                                   | Unit Cost<br>(Baht/cu m/h)               | Unit Cost<br>(Baht/cu m/h) |
| <b>Sedimentation Basin</b>   |   |                                   |  |                            |
| 50 cu m/hr                   | 1,310                                   | 26,200                            | 34,100                                   | 34,000                     |
| 100 cu m/hr                  | 1,633                                   | 16,330                            | 21,200                                   | 21,000                     |
| 200 cu m/hr                  | 3,136                                   | 15,680                            | 20,400                                   | 20,000                     |
| 250 cu m/hr                  | 5,133                                   | 20,532                            | 26,700                                   | 27,000                     |
| 500 cu m/hr                  | 7,708                                   | 15,416                            | 20,000                                   | 20,000                     |
| 1000 cu m/hr                 | 17,723                                  | 17,723                            | 23,000                                   | 23,000                     |
| <b>Filters</b>               |   |                                   |  |                            |
| 50 cu m/hr                   | 588                                     | 11,760                            | 15,300                                   | 15,000                     |
| 100 cu m/hr                  | 1,044                                   | 10,440                            | 13,600                                   | 14,000                     |
| 200 cu m/hr                  | 2,227                                   | 11,135                            | 14,500                                   | 15,000                     |
| 250 cu m/hr                  | 2,337                                   | 9,348                             | 12,200                                   | 12,000                     |
| 500 cu m/hr                  | 4,674                                   | 9,348                             | 12,200                                   | 12,000                     |
| 1000 cu m/hr                 | 11,356                                  | 11,356                            | 14,800                                   | 15,000                     |
| <b>Clear Water Reservoir</b> |   |                                   |  |                            |
|                              |   |                                   | Unit Cost<br>(Baht/cu m)                 | Unit Cost<br>(Baht/cu m)   |
| 500 cu m                     | 887                                     | 1,774                             | 2,300                                    | 2,300                      |
| 1000 cu m                    | 1,628                                   | 1,628                             | 2,100                                    | 2,100                      |
| 1500 cu m                    | 2,699                                   | 1,799                             | 2,300                                    | 2,300                      |
| 2000 cu m                    | 2,803                                   | 1,402                             | 1,800                                    | 1,800                      |
| 2250 cu m                    | 3,282                                   | 1,459                             | 1,900                                    | 1,900                      |
| 3000 cu m                    | 6,633                                   | 2,211                             | 2,900                                    | 2,900                      |
| 3300 cu m                    | 6,603                                   | 2,001                             | 2,600                                    | 2,600                      |
| 4000 cu m                    | 7,730                                   | 1,933                             | 2,500                                    | 2,500                      |
| 5800 cu m                    | 10,809                                  | 1,864                             | 2,400                                    | 2,400                      |
| <b>Elevated Tank</b>         |   |                                   |  |                            |
|                              |   |                                   | Cost<br>(Baht 1000)                      | Cost<br>(Baht 1000)        |
| 50 cu m                      | 722                                     |                                   | 940                                      | 900                        |
| 120 cu m                     | 1,146                                   |                                   | 1,490                                    | 1,500                      |
| 250 cu m                     | 1,394                                   |                                   | 1,810                                    | 1,800                      |



**APPENDIX A-8-1**

**Capacity Calculation of the Water Treatment Plant**



## Capacity Calculation for Treatment Plant

| Item                  | Total System ( for 2011 ) |                        |
|-----------------------|---------------------------|------------------------|
| Planned Flow          | Q=                        | 8,400 cu m/d           |
| (Daily Max)           | =                         | 350 cu m/hr            |
|                       | =                         | 5.8 cu m/min           |
|                       | =                         | 0.097 cu m/sec         |
| No. of Treatment Line |                           |                        |
|                       |                           | 2 Lines                |
|                       |                           | 4,200 cu m/d x 2 lines |
| (1)                   |                           |                        |
| Receiving Well        |                           |                        |
| Criteria              | T=                        | 1.5 min                |
|                       | d=                        | 2.8 m                  |
| No.                   |                           | 1 unit                 |
| Dimension             | Circular                  |                        |
|                       | Dia                       | 2.0 m                  |
|                       | v=                        | 9 cu m                 |
|                       | t=                        | 1.5 min                |
| (2)                   |                           |                        |
| Mixing Tank           |                           |                        |
| Criteria              | T=                        | 1.0 min                |
| Dimension             | Square x 3 units          |                        |
|                       | L m x                     | W m x D m x units      |
|                       | 1.2                       | 1.2 1.5 3              |
|                       | v =                       | 6.48 cu m              |
|                       | t =                       | 1.1 min                |
| Mixer                 | Mechanical Flush Mixer    |                        |

Capacity Calculation for Treatment Plant

| Item                 | Total System ( for 2011 )  |
|----------------------|--|
| (3) Coagulant Mixing |  |
| Coagulant            | Solid Aluminum Sulphate (Al <sub>2</sub> (SO <sub>4</sub> ) <sub>3</sub> )<br>containing 15 % Al <sub>2</sub> O <sub>3</sub> |
|                      | Dosage Rate : 10-25 mg-solid alum/l<br>Average 10 mg/l   |
|                      | Coagulant Solution : 5 % solution  |
|                      | Dosage Amount :<br>84 kg-Alum/day  |
|                      | Coagulant Solution ( 5 % solution)   |
|                      | = 2 cu m/day   |
| No. of Mixer         | 2 units  |
| Type                 | Batch Type Mixing  |
| Capacity             | 0.8 cu m/unit  |
| Dimension            | Square x 3 units (1 stand by):<br>L m x W m x D m x units<br>1.0 1.0 1.0 2   |
|                      | v = 1.0 cu m/unit  |
|                      | Total V = 2.0 cu m   |



## Capacity Calculation for Treatment Plant

| Item        | Total System ( for 2011 )                   |
|-------------|---|
| (4)         |   |
| Flocculator |   |
| Type        | Hydraulic Flocculation                      |
| No.         | N = 2 lines x 2 units<br>= 4 units          |
| Unit Flow   | q = 1.46 cu m/min/unit                      |
| Criteria    | T = 30 min                                  |
| Dimension   | W m x L m x D m x n units<br>1.2 15.0 2.5 4 |
|             | v = 45 cu m/unit                            |
|             | t = 30.9 min                                |

## Capacity Calculation for Treatment Plant

| Item                             | Total System ( for 2011 )   |
|----------------------------------|---|
| (5)                              |   |
| Sedimentation Basin              |   |
| Type                             | Rectanglar, Horizontal Flow   |
| No.                              | N = 2 line x 1 basins<br>= 2 basins   |
| Unit Flow                        | q = 175.0 cu m/hr/basin   |
| Criteria                         | Retention Time<br>T = 4 hours   |
| Dimension                        | W m x L m x D m x N<br>6 30 4.0 2<br>v = 720 cu m/basin<br>t = 4.1 hours  |
| Flow velocity                    | v = 12.2 cm/min   |
| Surface Load                     | a = 23.3 m <sup>3</sup> /m <sup>2</sup> /day  |
| Sludge Removal                   | Mechanical Scraper  |
| Sludge Amount                    |   |
| Solid Amount (ton-DS)            | $So = Q(K(T1-T2)+0.16xB) \times 10^{-6}$ where So: Sludge dry weight (ton)<br>Q : Treated water amount (m <sup>3</sup> /d)<br>K : Coefficient converting turbidity to SS (0.8-1.5 ->> 1.2)<br>T1 : Turbidity in raw water (ave = 12)<br>T2 : Turbidity after Sedimentation (ave = 7)<br>B : Alum dosage rate (ave. = 10 mg/l) |
|                                  | So = 0.06 ton-DS/day  |
| Water Contents of Drained Sludge |   |
|                                  | w = 99.5 %  |
| Sludge Volume                    |   |
|                                  | v = 13 cu m/d   |

## Capacity Calculation for Treatment Plant

| Item                  | Total System ( for 2011 )  |
|-----------------------|--|
| (6)                   |  |
| Rapid Sand Filter     |  |
| Type                  | Down Flow, Single Media  |
| No.                   | N = 2 lines x 4 units<br>= 8 units   |
| Unit Flow             | q = 1,050 cu m/day/unit  |
| Criteria              | Surface Load<br>120 - 150 m <sup>3</sup> /m <sup>2</sup> /day  |
| Dimension             | W m x L m x N units<br>2.5 3.0 8   |
|                       | a = 8 sq m/unit  |
| Surface Load          | La = 140.0 m <sup>3</sup> /m <sup>2</sup> /day   |
| Filter Washing        |  |
| Frequency             | Once a day for each filter   |
| Rate                  | Surface Washing<br>0.2 m <sup>3</sup> /m <sup>2</sup> /min x 5 min<br>Backwashing<br>0.6 m <sup>3</sup> /m <sup>2</sup> /min x 10 min  |
| Water Amount required | Surface Washing<br>v = 8 sq m/unit x 8 units<br>x 0.2 m <sup>3</sup> /m <sup>2</sup> /min x 5 min<br>= 60 cu m/day<br>Backwashing<br>v = 8 sq m/unit x 8 units<br>x 0.6 m <sup>3</sup> /m <sup>2</sup> /min x 10 min<br>= 360 cu m/day |
|                       | Total q= 420 cu m/day  |

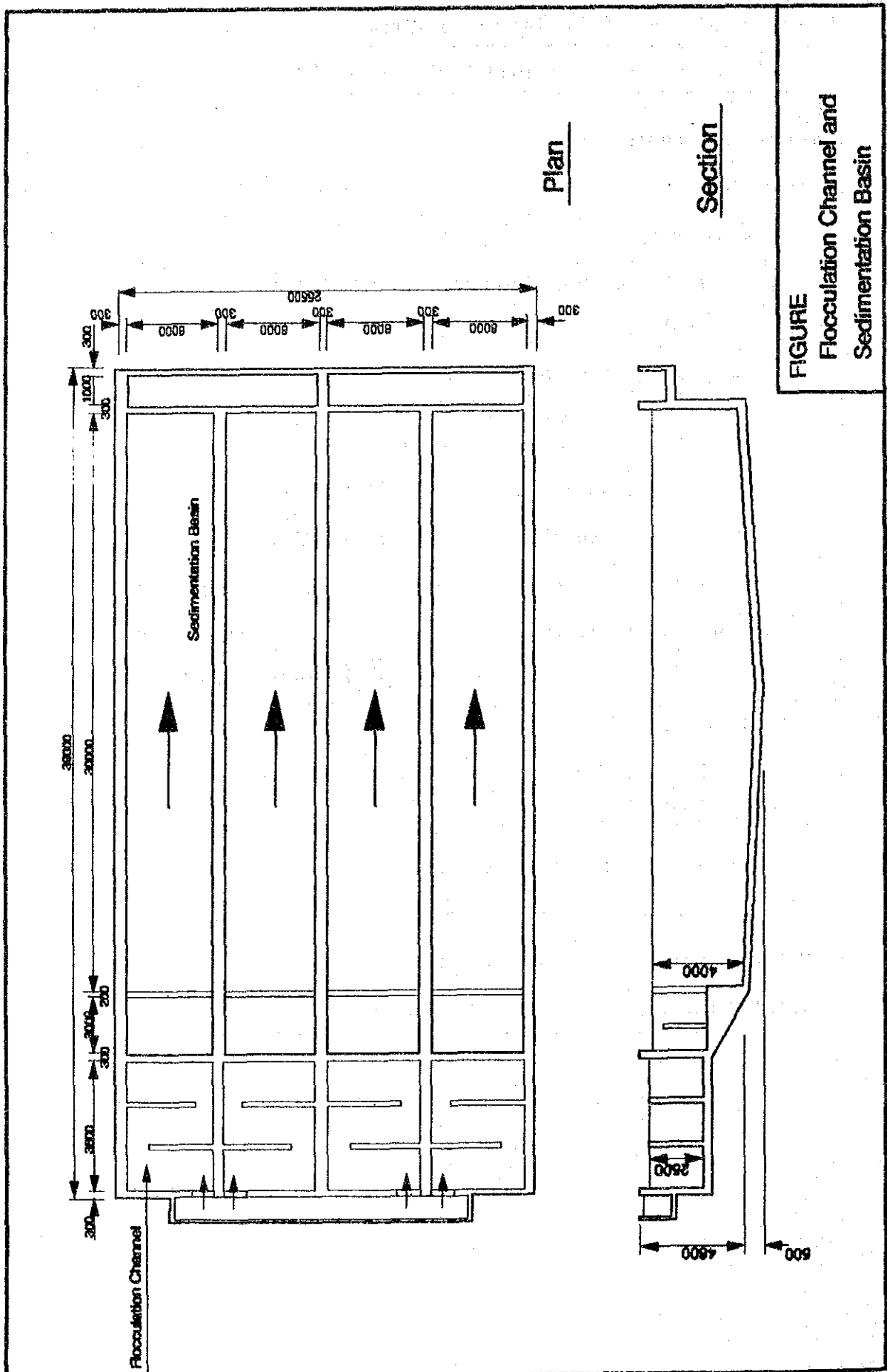
## Capacity Calculation for Treatment Plant

| Item                          | Total System ( for 2011 )  |
|-------------------------------|--|
| Solid Amount<br>in Wastewater |  |
| Solid Amount<br>(ton-DS)      | $S_o = Q * K * (T_1 - T_2) * 10^{-6}$ <p>where <math>S_o</math>: Sludge dry weight (ton)<br/> <math>Q</math>: Treated water amount (m<sup>3</sup>/d)<br/> <math>K</math>: Coefficient converting turbidity<br/> to SS (0.8-1.5 -&gt; 1.2)<br/> <math>T_1</math>: Turbidity before filter (ave = 7)<br/> <math>T_2</math>: Turbidity after filter (ave = 0)</p> |
|                               | $S_o = 0.07$ ton-DS/day  |
| SS Contents                   | $s = 168$ mg/l   |

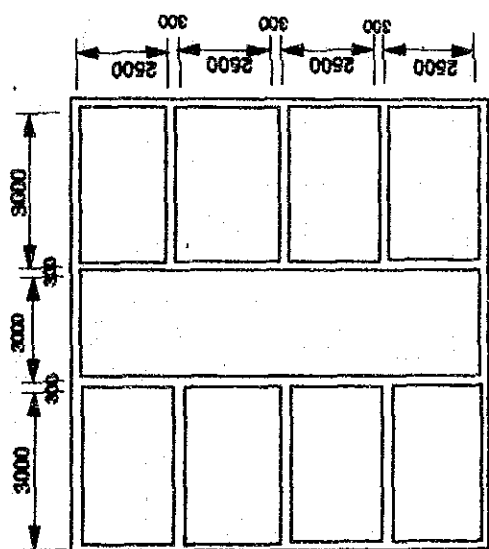
|                       |                           |
|-----------------------|---------------------------|
| (7)                   |                           |
| Clear Water Reservoir |                           |
| No.                   | $N = 1$ units             |
| Criteria              | Retention Time            |
|                       | $T = 8$ hours             |
| Required Volume       | $V = 2,800$ cu m          |
| Dimension             | L m x W m x D m x N units |
|                       | 20 x 30 x 5 x 1           |
|                       | Total Volume              |
|                       | $v = 3,000$ cu m          |
| Retention Time        | $t = 8.6$ hours           |

## Capacity Calculation for Treatment Plant

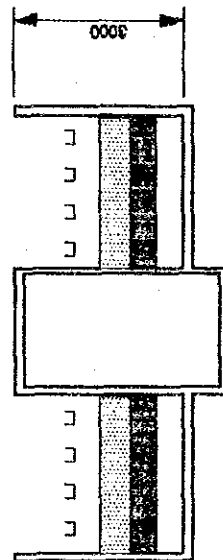
| Item                    | Total System ( for 2011 )                                      |
|-------------------------|--|
| :(8)                    |  |
| :Chlorination Equipment |  |
| : Injection Point       | : at the Inlet of Clear Water Reservoir                        |
| : Dosage Rate           | : 2.0 ppm  |
| : Type                  | : Liquid Chlorine (1-ton cylinder)                             |
| : Amount                | : 17 kg- Cl gas/day  |
| : Injector              | : Vacuum Type Injector   |
|                         | : No. of unit            2 units                               |
|                         | :                            (excl. 1 units stand-by)          |
|                         | : Rate                    0.35 kg/h/unit                       |
|                         | : Capacity                10 kg/h/unit                         |
| : Storage               | : 1 month  |
| : Storage Amount        | : 17 kg /day x 30 day =    504 kg                              |
|                         | :                            =            11 cylinders (50 kg) |
| :(9) Clear Water Pump   |  |
| : No.                   | : N =            3 units + 1 stand-by                          |
| : Flow per unit         | : q =            2.7 cu m/min/unit                             |
| : Diameter              | : D =            200 mm  |
| : Head                  | : H =            30 m  |
| : Motor output          | : P =            30 KW   |
| : Total Capacity        | : Q =            11,760 cu m/day                               |



**FIGURE**  
**Flocculation Channel and**  
**Sedimentation Basin**



Plan



Section

FIGURE  
Rapid Sand Filter

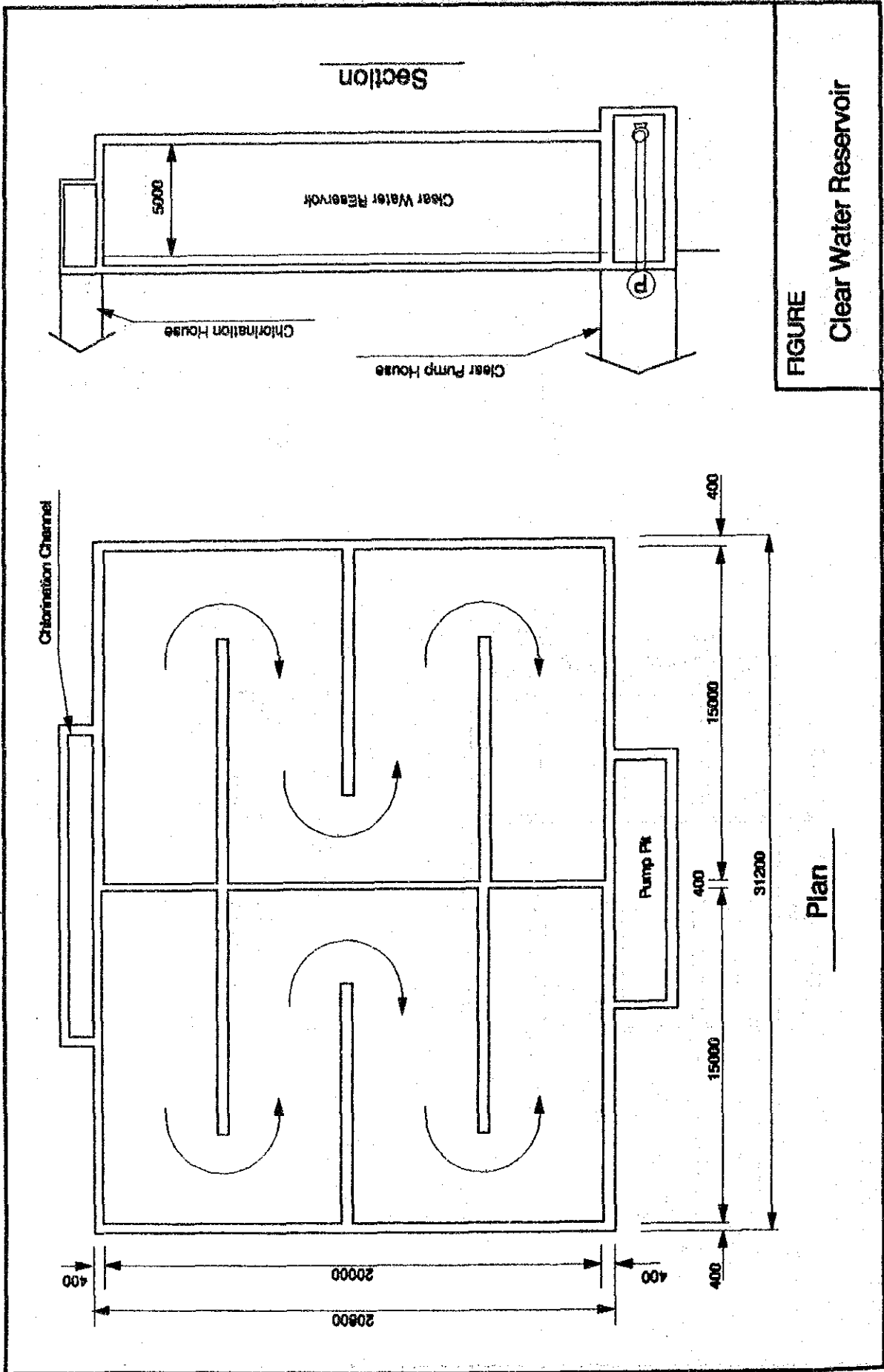


FIGURE  
Clear Water Reservoir

Plan



**APPENDIX A-8-2**

**Distribution Network Analysis**



Table 6-3-1 Results of Distribution Network Analysis

T I T L E : Thung Song (Proposed)  
 NO. OF PIPES : 141  
 NO. OF NODES : 124  
 PEAK FACTOR : 1.25  
 MAX HEADLOSS/Km : 100  
 MAX UNBAL(LPS) : .007

| PIPE NO. | FROM Node | TO Node | LENGTH ( M ) | DIA (MM) | HWC | FLOW (LPS) | VELOCITY (MPS) | HEADLOSS (M/KM) | HEADLOSS ( M ) |
|----------|-----------|---------|--------------|----------|-----|------------|----------------|-----------------|----------------|
| 1        | 200       | 1       | 110.00       | 400      | 110 | 126.94     | 1.01           | 3.39            | 0.37           |
| 2        | 1         | 2       | 423.00       | 250      | 110 | 31.20      | 0.64           | 2.49            | 1.05           |
| 3        | 2         | 3       | 920.00       | 200      | 110 | 24.34      | 0.77           | 4.67            | 4.30           |
| 4        | 3         | 4       | 680.00       | 200      | 110 | 7.18       | 0.23LO         | 0.49            | 0.33           |
| 5        | 4         | 5       | 1120.00      | 150      | 100 | 5.01       | 0.28LO         | 1.21            | 1.36           |
| 6        | 1         | 6       | 462.00       | 400      | 110 | 95.74      | 0.76           | 2.01            | 0.93           |
| 7        | 6         | 7       | 1152.00      | 400      | 110 | 92.97      | 0.74           | 1.91            | 2.19           |
| 8        | 7         | 8       | 240.00       | 300      | 100 | 91.44      | 1.29           | 8.95            | 2.15           |
| 9        | 8         | 9       | 436.00       | 300      | 100 | 89.25      | 1.26           | 8.55            | 3.73           |
| 10       | 9         | 10      | 258.00       | 300      | 100 | 7.29       | 0.10LO         | 0.08            | 0.02           |
| 12       | 10        | 12      | 256.00       | 100      | 100 | 4.36       | 0.55           | 6.76            | 1.73           |
| 13       | 12        | 13      | 292.00       | 100      | 110 | 3.11       | 0.40           | 3.03            | 0.89           |
| 14       | 9         | 14      | 296.00       | 300      | 100 | 79.54      | 1.13           | 6.91            | 2.05           |
| 15       | 14        | 15      | 70.00        | 150      | 100 | 2.18       | 0.12LO         | 0.26            | 0.02           |
| 16       | 15        | 16      | 394.00       | 100      | 100 | 0.92       | 0.12LO         | 0.38            | 0.15           |
| 17       | 15        | 17      | 410.00       | 100      | 100 | 0.60       | 0.08LO         | 0.17            | 0.07           |
| 18       | 14        | 18      | 106.00       | 300      | 100 | 77.36      | 1.09           | 6.57            | 0.70           |
| 19       | 18        | 19      | 186.00       | 200      | 100 | 21.52      | 0.69           | 4.44            | 0.82           |
| 20       | 19        | 20      | 28.00        | 200      | 100 | 16.23      | 0.52           | 2.63            | 0.07           |
| 21       | 19        | 23      | 328.00       | 150      | 100 | 5.08       | 0.29LO         | 1.24            | 0.41           |
| 22       | 20        | 21      | 106.00       | 200      | 110 | 16.23      | 0.52           | 2.21            | 0.23           |
| 23       | 21        | 22      | 126.00       | 200      | 110 | 9.64       | 0.31           | 0.84            | 0.11           |
| 24       | 23        | 22      | 28.00        | 150      | 100 | 1.87       | 0.11LO         | 0.20            | 0.01           |
| 25       | 23        | 24      | 375.00       | 100      | 110 | 1.44       | 0.18LO         | 0.73            | 0.27           |
| 26       | 24        | 25      | 200.00       | 100      | 110 | 0.83       | 0.11LO         | 0.26            | 0.05           |
| 27       | 21        | 26      | 176.00       | 150      | 100 | 6.16       | 0.35           | 1.78            | 0.31           |
| 28       | 22        | 26      | 175.00       | 100      | 110 | 1.87       | 0.24LO         | 1.18            | 0.21           |
| 29       | 26        | 27      | 454.00       | 150      | 100 | 6.87       | 0.39           | 2.18            | 0.99           |
| 30       | 27        | 28      | 110.00       | 100      | 110 | 1.20       | 0.15LO         | 0.52            | 0.06           |
| 31       | 29        | 28      | 116.00       | 100      | 110 | 2.01       | 0.26LO         | 1.35            | 0.16           |
| 32       | 18        | 30      | 226.00       | 300      | 100 | 54.83      | 0.78           | 3.47            | 0.79           |
| 33       | 22        | 37      | 20.00        | 200      | 110 | 9.05       | 0.29LO         | 0.75            | 0.01           |
| 34       | 30        | 31      | 44.00        | 200      | 100 | 17.65      | 0.56           | 3.07            | 0.14           |
| 35       | 31        | 32      | 284.00       | 150      | 100 | 3.81       | 0.22LO         | 0.73            | 0.21           |
| 36       | 32        | 33      | 18.00        | 100      | 100 | 1.46       | 0.19LO         | 0.89            | 0.02           |
| 37       | 33        | 34      | 270.00       | 100      | 100 | 0.88       | 0.11LO         | 0.35            | 0.09           |
| 38       | 31        | 35      | 164.00       | 200      | 100 | 11.62      | 0.37           | 1.42            | 0.23           |
| 39       | 35        | 36      | 80.00        | 200      | 100 | 10.05      | 0.32           | 1.08            | 0.09           |
| 40       | 36        | 50      | 90.00        | 150      | 100 | 0.32       | 0.02LO         | 0.01            | 0.00           |
| 41       | 36        | 37      | 20.00        | 200      | 100 | 8.11       | 0.26LO         | 0.73            | 0.01           |
| 42       | 37        | 38      | 62.00        | 150      | 110 | 4.20       | 0.24LO         | 0.73            | 0.05           |

| PIPE NO. | FROM Node | TO Node | LENGTH ( M ) | DIA (MM) | HWC | FLOW (LPS) | VELOCITY (MPS) | HEADLOSS (M/KM) | HEADLOSS ( M ) |
|----------|-----------|---------|--------------|----------|-----|------------|----------------|-----------------|----------------|
| 43       | 37        | 41      | 44.00        | 200      | 100 | 12.88      | 0.41           | 1.71            | 0.08           |
| 44       | 38        | 39      | 62.00        | 150      | 110 | 3.53       | 0.20LO         | 0.53            | 0.03           |
| 45       | 39        | 40      | 18.00        | 150      | 100 | 3.01       | 0.17LO         | 0.47            | 0.01           |
| 46       | 39        | 43      | 70.00        | 100      | 100 | 0.26       | 0.03LO         | 0.04            | 0.00           |
| 47       | 40        | 44      | 80.00        | 100      | 110 | 1.71       | 0.22LO         | 1.01            | 0.08           |
| 48       | 40        | 45      | 182.00       | 100      | 100 | 1.07       | 0.14LO         | 0.50            | 0.09           |
| 49       | 44        | 46      | 16.00        | 100      | 110 | 1.71       | 0.22LO         | 1.01            | 0.02           |
| 50       | 45        | 46      | 66.00        | 100      | 100 | 0.38       | 0.05LO         | 0.07            | 0.00           |
| 51       | 41        | 42      | 70.00        | 100      | 110 | 0.45       | 0.06LO         | 0.08            | 0.01           |
| 52       | 43        | 42      | 46.00        | 100      | 110 | 0.00       | 0.00LO         | 0.00            | 0.00           |
| 53       | 46        | 47      | 18.00        | 100      | 100 | 0.02       | 0.00LO         | 0.00            | 0.00           |
| 54       | 48        | 47      | 50.00        | 100      | 110 | 0.91       | 0.12LO         | 0.31            | 0.02           |
| 55       | 49        | 48      | 70.00        | 100      | 110 | 1.59       | 0.20LO         | 0.88            | 0.06           |
| 56       | 41        | 49      | 20.00        | 200      | 100 | 12.33      | 0.39           | 1.58            | 0.03           |
| 57       | 46        | 61      | 92.00        | 100      | 110 | 1.59       | 0.20LO         | 0.87            | 0.08           |
| 58       | 47        | 57      | 70.00        | 100      | 110 | 0.39       | 0.05LO         | 0.06            | 0.00           |
| 59       | 49        | 54      | 34.00        | 200      | 110 | 10.65      | 0.34           | 1.01            | 0.03           |
| 60       | 30        | 51      | 114.00       | 300      | 100 | 35.25      | 0.50           | 1.53            | 0.17           |
| 61       | 51        | 52      | 120.00       | 100      | 110 | 2.53       | 0.32           | 2.07            | 0.25           |
| 62       | 51        | 80      | 104.00       | 300      | 100 | 32.57      | 0.46           | 1.32            | 0.14           |
| 63       | 52        | 53      | 100.00       | 100      | 110 | 2.40       | 0.31           | 1.88            | 0.19           |
| 64       | 53        | 58      | 104.00       | 150      | 110 | 0.51       | 0.03LO         | 0.01            | 0.00           |
| 65       | 53        | 54      | 24.00        | 150      | 100 | 1.11       | 0.06LO         | 0.08            | 0.00           |
| 66       | 54        | 55      | 34.00        | 200      | 110 | 11.69      | 0.37           | 1.20            | 0.04           |
| 67       | 55        | 56      | 70.00        | 100      | 110 | 0.45       | 0.06LO         | 0.08            | 0.01           |
| 68       | 56        | 57      | 60.00        | 100      | 110 | 0.11       | 0.01LO         | 0.01            | 0.00           |
| 69       | 55        | 59      | 26.00        | 200      | 110 | 10.75      | 0.34           | 1.03            | 0.03           |
| 70       | 59        | 60      | 136.00       | 150      | 110 | 2.88       | 0.16LO         | 0.37            | 0.05           |
| 71       | 60        | 61      | 18.00        | 150      | 100 | 2.47       | 0.14LO         | 0.33            | 0.01           |
| 72       | 80        | 81      | 20.00        | 100      | 110 | 2.80       | 0.36           | 2.50            | 0.05           |
| 73       | 81        | 82      | 255.00       | 100      | 110 | 1.01       | 0.13LO         | 0.38            | 0.10           |
| 74       | 80        | 83      | 90.00        | 300      | 100 | 27.92      | 0.39           | 1.00            | 0.09           |
| 75       | 61        | 62      | 122.00       | 100      | 110 | 1.89       | 0.24LO         | 1.20            | 0.15           |
| 76       | 62        | 63      | 106.00       | 100      | 100 | 1.25       | 0.16LO         | 0.67            | 0.07           |
| 77       | 63        | 64      | 76.00        | 100      | 100 | 0.43       | 0.05LO         | 0.09            | 0.01           |
| 78       | 65        | 64      | 44.00        | 100      | 100 | 2.48       | 0.32           | 2.37            | 0.10           |
| 79       | 61        | 65      | 104.00       | 100      | 100 | 1.68       | 0.21LO         | 1.15            | 0.12           |
| 80       | 59        | 67      | 64.00        | 200      | 110 | 7.74       | 0.25LO         | 0.56            | 0.04           |
| 81       | 67        | 66      | 36.00        | 200      | 110 | 12.88      | 0.41           | 1.44            | 0.05           |
| 82       | 66        | 65      | 166.00       | 150      | 100 | 3.20       | 0.18LO         | 0.53            | 0.09           |
| 83       | 64        | 69      | 160.00       | 100      | 100 | 0.54       | 0.07LO         | 0.14            | 0.02           |
| 84       | 70        | 69      | 210.00       | 150      | 110 | 3.50       | 0.20LO         | 0.52            | 0.11           |
| 85       | 66        | 70      | 176.00       | 200      | 110 | 8.03       | 0.26LO         | 0.60            | 0.11           |
| 86       | 70        | 71      | 160.00       | 200      | 110 | 3.73       | 0.12LO         | 0.15            | 0.02           |
| 87       | 71        | 72      | 190.00       | 150      | 110 | 6.26       | 0.35           | 1.54            | 0.29           |
| 88       | 72        | 73      | 130.00       | 150      | 110 | 3.03       | 0.17LO         | 0.40            | 0.05           |
| 89       | 73        | 74      | 150.00       | 150      | 110 | 1.52       | 0.09LO         | 0.11            | 0.02           |
| 90       | 74        | 75      | 450.00       | 150      | 110 | 0.61       | 0.03LO         | 0.02            | 0.01           |

| PIPE NO. | FROM Node | TO Node | LENGTH ( M ) | DIA (MM) | HWC | FLOW (LPS) | VELOCITY (MPS) | HEADLOSS (M/KM) | HEADLOSS ( M ) |
|----------|-----------|---------|--------------|----------|-----|------------|----------------|-----------------|----------------|
| 91       | 68        | 67      | 25.00        | 200      | 100 | 5.22       | 0.17LO         | 0.32            | 0.01           |
| 92       | 83        | 68      | 310.00       | 200      | 100 | 9.56       | 0.30           | 0.99            | 0.31           |
| 93       | 68        | 77      | 204.00       | 150      | 110 | 3.57       | 0.20LO         | 0.54            | 0.11           |
| 94       | 77        | 76      | 170.00       | 150      | 110 | 3.13       | 0.18LO         | 0.43            | 0.07           |
| 95       | 76        | 71      | 26.00        | 200      | 110 | 4.55       | 0.14LO         | 0.21            | 0.01           |
| 96       | 83        | 84      | 6.00         | 300      | 100 | 17.56      | 0.25LO         | 0.42            | 0.00           |
| 97       | 84        | 85      | 20.00        | 150      | 100 | 4.22       | 0.24LO         | 0.88            | 0.02           |
| 98       | 85        | 86      | 236.00       | 150      | 100 | 4.22       | 0.24LO         | 0.88            | 0.21           |
| 99       | 86        | 87      | 20.00        | 100      | 100 | 3.92       | 0.50           | 5.57            | 0.11           |
| 100      | 86        | 90      | 96.00        | 100      | 100 | 0.29       | 0.04LO         | 0.05            | 0.00           |
| 101      | 87        | 88      | 60.00        | 100      | 100 | 0.06       | 0.01LO         | 0.00            | 0.00           |
| 102      | 87        | 89      | 96.00        | 100      | 100 | 3.79       | 0.48           | 5.22            | 0.50           |
| 103      | 84        | 91      | 146.00       | 200      | 100 | 13.13      | 0.42           | 1.78            | 0.26           |
| 104      | 91        | 92      | 90.00        | 100      | 100 | 1.89       | 0.24LO         | 1.44            | 0.13           |
| 105      | 91        | 94      | 182.00       | 200      | 110 | 10.44      | 0.33           | 0.98            | 0.18           |
| 106      | 92        | 93      | 160.00       | 100      | 100 | 0.12       | 0.02LO         | 0.01            | 0.00           |
| 107      | 92        | 77      | 172.00       | 100      | 100 | 0.57       | 0.07LO         | 0.16            | 0.03           |
| 108      | 78        | 76      | 170.00       | 150      | 110 | 1.89       | 0.11LO         | 0.17            | 0.03           |
| 109      | 78        | 79      | 194.00       | 100      | 100 | 0.39       | 0.05LO         | 0.08            | 0.01           |
| 110      | 101       | 78      | 50.00        | 200      | 110 | 2.68       | 0.09LO         | 0.08            | 0.00           |
| 111      | 101       | 102     | 100.00       | 200      | 100 | 0.18       | 0.01LO         | 0.00            | 0.00           |
| 112      | 103       | 101     | 3.00         | 200      | 110 | 3.35       | 0.11LO         | 0.12            | 0.00           |
| 113      | 94        | 103     | 117.00       | 200      | 110 | 3.89       | 0.12LO         | 0.16            | 0.02           |
| 114      | 94        | 95      | 40.00        | 200      | 100 | 6.08       | 0.19LO         | 0.43            | 0.02           |
| 115      | 95        | 97      | 310.00       | 100      | 100 | 0.25       | 0.03LO         | 0.03            | 0.01           |
| 116      | 95        | 96      | 22.00        | 100      | 100 | 5.36       | 0.68           | 9.91            | 0.22           |
| 117      | 96        | 98      | 285.00       | 100      | 100 | 4.14       | 0.53           | 6.13            | 1.75           |
| 118      | 98        | 99      | 212.00       | 100      | 110 | 3.80       | 0.48           | 4.40            | 0.93           |
| 119      | 99        | 100     | 380.00       | 100      | 110 | 2.60       | 0.33           | 2.17            | 0.83           |
| 201      | 6         | 201     | 700.00       | 100      | 110 | 0.86       | 0.11LO         | 0.28            | 0.20           |
| 202      | 201       | 202     | 470.00       | 100      | 110 | 0.31       | 0.04LO         | 0.04            | 0.02           |
| 203      | 201       | 203     | 580.00       | 100      | 110 | 0.35       | 0.04LO         | 0.05            | 0.03           |
| 204      | 7         | 204     | 1250.00      | 100      | 110 | 0.21       | 0.03LO         | 0.02            | 0.02           |
| 205      | 9         | 226     | 880.00       | 100      | 110 | 0.15       | 0.02LO         | 0.01            | 0.01           |
| 206      | 226       | 205     | 800.00       | 100      | 110 | 0.15       | 0.02LO         | 0.01            | 0.01           |
| 207      | 205       | 206     | 670.00       | 100      | 110 | 0.15       | 0.02LO         | 0.01            | 0.01           |
| 209      | 13        | 208     | 240.00       | 100      | 110 | 2.44       | 0.31           | 1.94            | 0.46           |
| 212      | 208       | 211     | 670.00       | 100      | 110 | 2.44       | 0.31           | 1.94            | 1.30           |
| 213      | 211       | 29      | 350.00       | 100      | 110 | 2.44       | 0.31           | 1.94            | 0.68           |
| 215      | 75        | 213     | 650.00       | 100      | 110 | 0.49       | 0.06LO         | 0.10            | 0.07           |
| 216      | 74        | 214     | 700.00       | 100      | 110 | 0.43       | 0.05LO         | 0.08            | 0.05           |
| 218      | 100       | 216     | 720.00       | 100      | 110 | 0.60       | 0.08LO         | 0.14            | 0.10           |
| 219      | 216       | 217     | 900.00       | 100      | 110 | 0.18       | 0.02LO         | 0.02            | 0.01           |
| 220      | 216       | 218     | 150.00       | 100      | 110 | 0.00       | 0.00LO         | 0.00            | 0.00           |
| 221      | 218       | 219     | 800.00       | 100      | 110 | 0.31       | 0.04LO         | 0.04            | 0.03           |
| 224      | 222       | 218     | 1130.00      | 100      | 110 | 0.97       | 0.12LO         | 0.35            | 0.40           |
| 225      | 223       | 222     | 900.00       | 100      | 110 | 1.70       | 0.22LO         | 0.99            | 0.89           |
| 226      | 89        | 223     | 620.00       | 100      | 110 | 3.34       | 0.43           | 3.47            | 2.15           |

| PIPE NO. | FROM Node | TO Node | LENGTH ( M ) | DIA (MM) | HWC | FLOW (LPS) | VELOCITY (MPS) | HEADLOSS (M/KM) | HEADLOSS ( M ) |
|----------|-----------|---------|--------------|----------|-----|------------|----------------|-----------------|----------------|
| 227      | 223       | 224     | 870.00       | 100      | 110 | 0.65       | 0.08LO         | 0.17            | 0.14           |
| 228      | 17        | 207     | 730.00       | 100      | 110 | 0.00       | 0.00LO         | 0.00            | 0.00           |
| 229      | 5         | 225     | 440.00       | 100      | 110 | 0.24       | 0.03LO         | 0.03            | 0.01           |
| 230      | 5         | 227     | 450.00       | 100      | 110 | 0.22       | 0.03LO         | 0.02            | 0.01           |

| NODE NO. | FLOW (LPS) | ELEVATION ( M ) | H G L ( M ) | PRESSURE ( M ) |
|----------|------------|-----------------|-------------|----------------|
| 1        | 0.000      | 61.10           | 85.83       | 24.73          |
| 2        | -6.858     | 61.44           | 84.77       | 23.33          |
| 3        | -17.158    | 60.79           | 80.48       | 19.69          |
| 4        | -2.173     | 62.53           | 80.14       | 17.61          |
| 5        | -4.549     | 73.53           | 78.78       | 5.25           |
| 6        | -1.913     | 60.07           | 84.90       | 24.83          |
| 7        | -1.326     | 55.92           | 82.70       | 26.78          |
| 8        | -2.190     | 55.48           | 80.56       | 25.08          |
| 9        | -2.271     | 54.08           | 76.83       | 22.75          |
| 10       | -2.927     | 53.66           | 76.81       | 23.15          |
| 12       | -1.250     | 53.30           | 75.08       | 21.78          |
| 13       | -0.670     | 53.70           | 74.19       | 20.49          |
| 14       | 0.000      | 52.71           | 74.78       | 22.07          |
| 15       | -0.657     | 52.02           | 74.76       | 22.74          |
| 16       | -0.924     | 53.48           | 74.61       | 21.13          |
| 17       | -0.599     | 52.00           | 74.69       | 22.69          |
| 18       | -1.007     | 51.70           | 74.08       | 22.38          |
| 19       | -0.218     | 53.46           | 73.26       | 19.80          |
| 20       | 0.000      | 53.46           | 73.19       | 19.73          |
| 21       | -0.434     | 52.58           | 72.95       | 20.37          |
| 22       | -0.587     | 51.79           | 72.85       | 21.06          |
| 23       | -1.766     | 51.79           | 72.85       | 21.06          |
| 24       | -0.610     | 50.72           | 72.58       | 21.86          |
| 25       | -0.829     | 50.62           | 72.53       | 21.91          |
| 26       | -1.154     | 53.00           | 72.64       | 19.64          |
| 27       | -5.669     | 53.30           | 71.65       | 18.35          |
| 28       | -3.209     | 53.38           | 71.59       | 18.21          |
| 29       | -0.429     | 53.30           | 71.75       | 18.45          |
| 30       | -1.931     | 51.44           | 73.30       | 21.86          |
| 31       | -2.218     | 51.44           | 73.16       | 21.72          |
| 32       | -2.355     | 50.59           | 72.96       | 22.37          |
| 33       | -0.579     | 50.58           | 72.94       | 22.36          |
| 34       | -0.879     | 50.21           | 72.85       | 22.64          |
| 35       | -1.571     | 51.60           | 72.93       | 21.33          |
| 36       | -1.619     | 51.79           | 72.85       | 21.06          |
| 37       | -0.094     | 51.79           | 72.83       | 21.04          |
| 38       | -0.664     | 51.70           | 72.79       | 21.09          |
| 39       | -0.267     | 51.60           | 72.75       | 21.15          |
| 40       | -0.223     | 51.70           | 72.74       | 21.04          |

| NODE<br>NO. | FLOW<br>(LPS) | ELEVATION<br>( M ) | H G L<br>( M ) | PRESSURE<br>( M ) |
|-------------|---------------|--------------------|----------------|-------------------|
| 41          | -0.105        | 51.60              | 72.76          | 21.16             |
| 42          | -0.447        | 51.58              | 72.75          | 21.17             |
| 43          | -0.259        | 51.57              | 72.75          | 21.18             |
| 44          | 0.000         | 51.57              | 72.66          | 21.09             |
| 45          | -0.692        | 51.60              | 72.65          | 21.05             |
| 46          | -0.484        | 51.57              | 72.65          | 21.08             |
| 47          | -0.540        | 51.57              | 72.65          | 21.08             |
| 48          | -0.687        | 51.58              | 72.66          | 21.08             |
| 49          | -0.078        | 51.61              | 72.72          | 21.11             |
| 50          | -0.320        | 51.61              | 72.84          | 21.23             |
| 51          | -0.148        | 51.55              | 73.13          | 21.58             |
| 52          | -0.134        | 51.56              | 72.88          | 21.32             |
| 53          | -0.778        | 51.50              | 72.69          | 21.19             |
| 54          | -0.079        | 51.50              | 72.69          | 21.19             |
| 55          | -0.494        | 51.48              | 72.65          | 21.17             |
| 56          | -0.343        | 51.50              | 72.64          | 21.14             |
| 57          | -0.491        | 51.52              | 72.64          | 21.12             |
| 58          | -0.506        | 51.35              | 72.69          | 21.34             |
| 59          | -0.125        | 51.48              | 72.62          | 21.14             |
| 60          | -0.407        | 51.50              | 72.57          | 21.07             |
| 61          | -0.496        | 51.50              | 72.56          | 21.06             |
| 62          | -0.640        | 51.40              | 72.42          | 21.02             |
| 63          | -0.817        | 52.20              | 72.35          | 20.15             |
| 64          | -2.360        | 51.85              | 72.34          | 20.49             |
| 65          | -2.407        | 51.60              | 72.44          | 20.84             |
| 66          | -1.640        | 51.30              | 72.53          | 21.23             |
| 67          | -0.090        | 51.35              | 72.58          | 21.23             |
| 68          | -0.764        | 51.35              | 72.59          | 21.24             |
| 69          | -4.045        | 52.13              | 72.32          | 20.19             |
| 70          | -0.803        | 51.25              | 72.43          | 21.18             |
| 71          | -2.023        | 51.53              | 72.40          | 20.87             |
| 72          | -3.225        | 51.90              | 72.11          | 20.21             |
| 73          | -1.517        | 52.23              | 72.06          | 19.83             |
| 74          | -0.477        | 52.68              | 72.04          | 19.36             |
| 75          | -0.115        | 52.70              | 72.03          | 19.33             |
| 76          | -0.466        | 51.53              | 72.41          | 20.88             |
| 77          | -1.011        | 51.25              | 72.48          | 21.23             |
| 78          | -0.407        | 51.30              | 72.44          | 21.14             |
| 79          | -0.388        | 50.94              | 72.42          | 21.48             |
| 80          | -1.846        | 51.52              | 72.99          | 21.47             |
| 81          | -1.796        | 50.40              | 72.94          | 22.54             |
| 82          | -1.006        | 47.88              | 72.84          | 24.96             |
| 83          | -0.804        | 51.53              | 72.90          | 21.37             |
| 84          | -0.207        | 51.53              | 72.90          | 21.37             |
| 85          | 0.000         | 51.53              | 72.88          | 21.35             |
| 86          | 0.000         | 51.05              | 72.67          | 21.62             |
| 87          | -0.076        | 51.05              | 72.56          | 21.51             |
| 88          | -0.057        | 50.95              | 72.56          | 21.61             |

| NODE<br>NO. | FLOW<br>(LPS) | ELEVATION<br>( M ) | H G L<br>( M ) | PRESSURE<br>( M ) |
|-------------|---------------|--------------------|----------------|-------------------|
| 89          | -0.449        | 50.90              | 72.06          | 21.16             |
| 90          | -0.295        | 50.90              | 72.66          | 21.76             |
| 91          | -0.801        | 51.47              | 72.64          | 21.17             |
| 92          | -1.200        | 51.27              | 72.51          | 21.24             |
| 93          | -0.119        | 50.94              | 72.51          | 21.57             |
| 94          | -0.473        | 50.90              | 72.46          | 21.56             |
| 95          | -0.472        | 50.86              | 72.44          | 21.58             |
| 96          | -1.224        | 50.89              | 72.22          | 21.33             |
| 97          | -0.250        | 50.38              | 72.43          | 22.05             |
| 98          | -0.336        | 50.96              | 70.48          | 19.52             |
| 99          | -1.204        | 50.05              | 69.54          | 19.49             |
| 100         | -1.995        | 49.59              | 68.72          | 19.13             |
| 101         | -0.489        | 50.99              | 72.44          | 21.45             |
| 102         | -0.182        | 50.85              | 72.44          | 21.59             |
| 103         | -0.532        | 50.94              | 72.44          | 21.50             |
| 200 R       | 126.939       | 61.20              | 86.20          | 25.00             |
| 201         | -0.205        | 62.00              | 84.70          | 22.70             |
| 202         | -0.306        | 64.10              | 84.68          | 20.58             |
| 203         | -0.348        | 63.00              | 84.67          | 21.67             |
| 204         | -0.205        | 59.30              | 82.68          | 23.38             |
| 205         | 0.000         | 58.50              | 76.81          | 18.31             |
| 206         | -0.149        | 60.10              | 76.80          | 16.70             |
| 207         | 0.000         | 52.00              | 74.69          | 22.69             |
| 208         | 0.000         | 54.50              | 73.73          | 19.23             |
| 211         | 0.000         | 54.50              | 72.43          | 17.93             |
| 213         | -0.494        | 52.60              | 71.97          | 19.37             |
| 214         | -0.429        | 50.80              | 71.99          | 21.19             |
| 216         | -0.420        | 50.00              | 68.61          | 18.61             |
| 217         | -0.180        | 53.10              | 68.60          | 15.50             |
| 218         | -0.667        | 49.50              | 68.61          | 19.11             |
| 219         | -0.307        | 51.00              | 68.58          | 17.58             |
| 222         | -0.727        | 48.00              | 69.01          | 21.01             |
| 223         | -0.997        | 48.00              | 69.91          | 21.91             |
| 224         | -0.647        | 48.00              | 69.76          | 21.76             |
| 225         | -0.243        | 73.53              | 78.77          | 5.24              |
| 226         | 0.000         | 56.20              | 76.82          | 20.62             |
| 227         | -0.218        | 73.53              | 78.77          | 5.24              |



Table 6-4-1 Results of Distribution Network Analysis

T I T L E : NA 8on (Proposed)  
 NO. OF PIPES : 27  
 NO. OF NODES : 24  
 PEAK FACTOR : 1.25  
 MAX HEADLOSS/Km : 100  
 MAX UNBAL(LPS) : .005

| PIPE NO. | FROM Node | TO Node | LENGTH ( M ) | DIA (MM) | HWC | FLOW (LPS) | VELOCITY (MPS) | HEADLOSS (M/KM) | ( M ) |
|----------|-----------|---------|--------------|----------|-----|------------|----------------|-----------------|-------|
| 1        | 400       | 13      | 30.00        | 150      | 100 | 15.32      | 0.87           | 9.59            | 0.29  |
| 2        | 2         | 1       | 115.00       | 150      | 100 | 0.64       | 0.04L0         | 0.03            | 0.00  |
| 3        | 3         | 2       | 30.00        | 150      | 100 | 0.69       | 0.04L0         | 0.03            | 0.00  |
| 4        | 4         | 3       | 115.00       | 150      | 100 | 0.97       | 0.05L0         | 0.06            | 0.01  |
| 5        | 5         | 4       | 140.00       | 150      | 100 | 2.72       | 0.15L0         | 0.39            | 0.05  |
| 6        | 6         | 5       | 25.00        | 150      | 100 | 3.46       | 0.20L0         | 0.61            | 0.02  |
| 7        | 7         | 6       | 75.00        | 150      | 100 | 4.36       | 0.25L0         | 0.94            | 0.07  |
| 8        | 7         | 8       | 67.00        | 100      | 100 | 0.10       | 0.01L0         | 0.01            | 0.00  |
| 9        | 4         | 9       | 88.00        | 100      | 100 | 0.27       | 0.03L0         | 0.04            | 0.00  |
| 10       | 7         | 9       | 213.00       | 100      | 100 | 1.26       | 0.16L0         | 0.68            | 0.14  |
| 11       | 10        | 7       | 25.00        | 150      | 100 | 5.91       | 0.33           | 1.65            | 0.04  |
| 12       | 11        | 10      | 85.00        | 150      | 100 | 5.91       | 0.33           | 1.65            | 0.14  |
| 13       | 12        | 11      | 260.00       | 150      | 100 | 7.25       | 0.41           | 2.41            | 0.63  |
| 14       | 15        | 11      | 123.00       | 150      | 100 | 0.30       | 0.02L0         | 0.01            | 0.00  |
| 15       | 13        | 12      | 75.00        | 150      | 100 | 7.25       | 0.41           | 2.41            | 0.18  |
| 16       | 13        | 14      | 208.00       | 150      | 100 | 8.06       | 0.46           | 2.93            | 0.61  |
| 17       | 14        | 15      | 188.00       | 100      | 100 | 1.59       | 0.20L0         | 1.04            | 0.20  |
| 18       | 16        | 15      | 60.00        | 150      | 100 | 1.50       | 0.09L0         | 0.13            | 0.01  |
| 19       | 14        | 17      | 87.00        | 150      | 100 | 5.53       | 0.31           | 1.46            | 0.13  |
| 20       | 17        | 16      | 110.00       | 150      | 100 | 3.29       | 0.19L0         | 0.56            | 0.06  |
| 21       | 15        | 22      | 47.00        | 150      | 100 | 1.16       | 0.07L0         | 0.08            | 0.00  |
| 22       | 22        | 23      | 23.00        | 150      | 100 | 0.56       | 0.02L0         | 0.01            | 0.00  |
| 23       | 22        | 21      | 53.00        | 100      | 100 | 0.62       | 0.08L0         | 0.18            | 0.01  |
| 24       | 17        | 18      | 63.00        | 100      | 100 | 1.56       | 0.20L0         | 1.01            | 0.06  |
| 25       | 18        | 19      | 130.00       | 100      | 100 | 0.58       | 0.07L0         | 0.16            | 0.02  |
| 26       | 21        | 19      | 20.00        | 100      | 100 | 0.43       | 0.05L0         | 0.09            | 0.00  |
| 27       | 19        | 20      | 92.00        | 100      | 100 | 0.31       | 0.04L0         | 0.05            | 0.00  |

| NODE NO. | FLOW (LPS) | ELEVATION ( M ) | H G L ( M ) | PRESSURE ( M ) |
|----------|------------|-----------------|-------------|----------------|
| 400 R    | 15.315     | 55.46           | 70.46       | 15.00          |
| 1        | -0.637     | 52.11           | 69.03       | 16.92          |
| 2        | -0.050     | 49.34           | 69.04       | 19.70          |
| 3        | -0.280     | 50.01           | 69.04       | 19.03          |
| 4        | -1.487     | 51.54           | 69.04       | 17.50          |
| 5        | -0.734     | 51.22           | 69.10       | 17.86          |
| 6        | -0.902     | 54.40           | 69.11       | 14.71          |
| 7        | -0.195     | 54.13           | 69.18       | 15.05          |
| 8        | -0.097     | 54.71           | 69.18       | 14.47          |

| NODE<br>NO. | FLOW<br>(LPS) | ELEVATION<br>( M ) | H G L<br>( M ) | PRESSURE<br>( M ) |
|-------------|---------------|--------------------|----------------|-------------------|
| 9           | -1.523        | 52.28              | 69.04          | 16.76             |
| 10          | 0.000         | 53.12              | 69.23          | 16.11             |
| 11          | -1.644        | 52.43              | 69.37          | 16.94             |
| 12          | 0.000         | 56.15              | 69.99          | 13.84             |
| 13          | 0.000         | 57.46              | 70.17          | 12.71             |
| 14          | -0.949        | 57.71              | 69.56          | 11.85             |
| 15          | -1.636        | 54.38              | 69.37          | 14.99             |
| 16          | -1.788        | 54.72              | 69.38          | 14.66             |
| 17          | -0.676        | 53.57              | 69.44          | 15.87             |
| 18          | -0.980        | 54.86              | 69.37          | 14.51             |
| 19          | -0.697        | 54.21              | 69.35          | 15.14             |
| 20          | -0.313        | 53.92              | 69.35          | 15.43             |
| 21          | -0.190        | 54.21              | 69.35          | 15.14             |
| 23          | -0.358        | 53.24              | 69.36          | 16.12             |
| 22          | -0.178        | 54.20              | 69.36          | 15.16             |

**APPENDIX A-11-1**

**Details of Operation Cost**



WATER TRANSMISSION AND DISTRIBUTION COST STUDY (Thung Song)

| Year | E    |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|
|      | 1990 | 1991 | 1992 | 1993 | 1994 | 1995 | 1996 | 1997 | 1998 | 1999 |

1. Planned Daily Average Water Demand (cu m/d)

|            | E     |       |       |       |       |       |       |       |       |       |
|------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
|            | 1990  | 1991  | 1992  | 1993  | 1994  | 1995  | 1996  | 1997  | 1998  | 1999  |
| Thung Song | 4,394 | 4,512 | 4,594 | 4,677 | 4,763 | 4,849 | 4,938 | 5,034 | 5,132 | 5,232 |
| Ba Bon     | 558   | 577   | 597   | 616   | 637   | 657   | 678   | 699   | 721   | 743   |
| Total      | 4,952 | 5,089 | 5,191 | 5,293 | 5,400 | 5,506 | 5,616 | 5,733 | 5,853 | 5,975 |

2. Planned Daily Maximum Water Demand: QDM (cu m/d)

|               | E     |       |       |       |       |       |       |       |       |       |
|---------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
|               | 1990  | 1991  | 1992  | 1993  | 1994  | 1995  | 1996  | 1997  | 1998  | 1999  |
| Peak Factor = | 1.30  |       |       |       |       |       |       |       |       |       |
| Thung Song    | 5,712 | 5,866 | 5,972 | 6,080 | 6,192 | 6,304 | 6,419 | 6,544 | 6,672 | 6,802 |
| Ba Bon        | 725   | 750   | 776   | 801   | 828   | 854   | 881   | 909   | 937   | 966   |
| Total         | 6,438 | 6,616 | 6,748 | 6,881 | 7,020 | 7,158 | 7,301 | 7,453 | 7,609 | 7,768 |

3. Treatment Plant

| Existing Plant     | 1990  | 1991  | 1992  | 1993  | 1994  | 1995  | 1996  | 1997  | 1998  | 1999  | 2000  | 2001  | 2002  | 2003  | 2004  | 2005  | 2006  | 2007  | 2008  | 2009  | 2010  | 2011  |
|--------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Net Treatment Capa | 5,333 | 5,333 | 5,333 | 5,333 | 5,333 | 5,333 | 5,333 | 5,333 | 5,333 | 5,333 | 5,333 | 5,333 | 5,333 | 5,333 | 5,333 | 5,333 | 5,333 | 5,333 | 5,333 | 5,333 | 5,333 | 5,333 |
| Max. Capacity      | 8,400 | 8,400 | 8,400 | 8,400 | 8,400 | 8,400 | 8,400 | 8,400 | 8,400 | 8,400 | 8,400 | 8,400 | 8,400 | 8,400 | 8,400 | 8,400 | 8,400 | 8,400 | 8,400 | 8,400 | 8,400 | 8,400 |

4. Water Amount for Intake Design : (cu m/d)

| Raw water for Treatment Plant (Daily Max)/51.0841.1 | 1990  | 1991  | 1992  | 1993  | 1994  | 1995  | 1996  | 1997  | 1998  | 1999  | 2000  | 2001  | 2002  | 2003   | 2004   | 2005   | 2006   | 2007   | 2008   | 2009   | 2010   | 2011   |
|---|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| Raw water for Treatment Plant                       | 7,648 | 7,859 | 8,017 | 8,175 | 8,340 | 8,503 | 8,673 | 8,854 | 9,039 | 9,228 | 9,419 | 9,615 | 9,870 | 10,131 | 10,397 | 10,657 | 10,944 | 11,236 | 11,534 | 11,835 | 12,145 | 12,460 |

5. Daily Average Intake Amount

| Raw water for Treatment Plant | 1990  | 1991  | 1992  | 1993  | 1994  | 1995  | 1996  | 1997  | 1998  | 1999  | 2000  | 2001  | 2002  | 2003  | 2004  | 2005  | 2006  | 2007  | 2008  | 2009  | 2010  | 2011  |
|-------------------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Raw water for Treatment Plant | 4,952 | 5,089 | 5,191 | 5,293 | 5,400 | 5,506 | 5,616 | 5,733 | 5,853 | 5,975 | 6,099 | 6,226 | 6,391 | 6,560 | 6,732 | 6,907 | 7,086 | 7,275 | 7,468 | 7,664 | 7,864 | 8,068 |

6. Pump Characteristics

| Raw Water Pump              | 1990   | 1991   | 1992   | 1993   | 1994   | 1995   | 1996   | 1997   | 1998   | 1999   | 2000   | 2001   | 2002   | 2003   | 2004   | 2005   | 2006   | 2007   | 2008   | 2009   | 2010   | 2011   |
|-----------------------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| Raw Water Pump              | 200 mm | 200 mm | 200 mm | 200 mm | 200 mm | 200 mm | 200 mm | 200 mm | 200 mm | 200 mm | 200 mm | 200 mm | 200 mm | 200 mm | 200 mm | 200 mm | 200 mm | 200 mm | 200 mm | 200 mm | 200 mm | 200 mm |
| Clear Water Pump at New RTP | 200 mm | 200 mm | 200 mm | 200 mm | 200 mm | 200 mm | 200 mm | 200 mm | 200 mm | 200 mm | 200 mm | 200 mm | 200 mm | 200 mm | 200 mm | 200 mm | 200 mm | 200 mm | 200 mm | 200 mm | 200 mm | 200 mm |
| at Exis. RTP                | 200 mm | 200 mm | 200 mm | 200 mm | 200 mm | 200 mm | 200 mm | 200 mm | 200 mm | 200 mm | 200 mm | 200 mm | 200 mm | 200 mm | 200 mm | 200 mm | 200 mm | 200 mm | 200 mm | 200 mm | 200 mm | 200 mm |

WATER TRANSMISSION AND DISTRIBUTION COST STUDY (Thung Song)

| Item                   | Y     |       |       |       |       | A     |       |       |       |       | B      |        |        |        |        |        |        |        |        |        |        |        |
|------------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
|                        | 1990  | 1991  | 1992  | 1993  | 1994  | 1995  | 1996  | 1997  | 1998  | 1999  | 2000   | 2001   | 2002   | 2003   | 2004   | 2005   | 2006   | 2007   | 2008   | 2009   | 2010   | 2011   |
| No. of Operating Pumps | 1     | 1     | 1     | 1     | 1     | 1     | 1     | 1     | 1     | 1     | 2      | 2      | 2      | 2      | 2      | 2      | 2      | 2      | 2      | 2      | 2      | 2      |
| Raw Water Pump         | 6,230 | 6,230 | 6,230 | 6,230 | 6,230 | 6,230 | 6,230 | 6,230 | 6,230 | 6,230 | 12,460 | 12,460 | 12,460 | 12,460 | 12,460 | 12,460 | 12,460 | 12,460 | 12,460 | 12,460 | 12,460 | 12,460 |
| Max. Capa. of Pump     | 6,230 | 6,230 | 6,230 | 6,230 | 6,230 | 6,230 | 6,230 | 6,230 | 6,230 | 6,230 | 12,460 | 12,460 | 12,460 | 12,460 | 12,460 | 12,460 | 12,460 | 12,460 | 12,460 | 12,460 | 12,460 | 12,460 |

8. No. of Operating Pumps

| Item                  | Y      |        |        |        |        | A      |        |        |        |        | B      |        |        |        |        |        |        |        |        |        |        |        |
|-----------------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
|                       | 1990   | 1991   | 1992   | 1993   | 1994   | 1995   | 1996   | 1997   | 1998   | 1999   | 2000   | 2001   | 2002   | 2003   | 2004   | 2005   | 2006   | 2007   | 2008   | 2009   | 2010   | 2011   |
| Raw Water Pump        | 1      | 1      | 1      | 1      | 1      | 1      | 1      | 1      | 1      | 1      | 2      | 2      | 2      | 2      | 2      | 2      | 2      | 2      | 2      | 2      | 2      | 2      |
| Max. Capa. of Pump    | 6,230  | 6,230  | 6,230  | 6,230  | 6,230  | 6,230  | 6,230  | 6,230  | 6,230  | 6,230  | 12,460 | 12,460 | 12,460 | 12,460 | 12,460 | 12,460 | 12,460 | 12,460 | 12,460 | 12,460 | 12,460 | 12,460 |
| at Exis. PTP          | 2      | 2      | 2      | 2      | 2      | 2      | 2      | 2      | 2      | 2      | 2      | 2      | 2      | 2      | 2      | 2      | 2      | 2      | 2      | 2      | 2      | 2      |
| Max. Capa. of Pump    | 10,560 | 10,560 | 10,560 | 10,560 | 10,560 | 10,560 | 10,560 | 10,560 | 10,560 | 10,560 | 21,120 | 21,120 | 21,120 | 21,120 | 21,120 | 21,120 | 21,120 | 21,120 | 21,120 | 21,120 | 21,120 | 21,120 |
| Total Capacity (cu m) | 10,560 | 10,560 | 10,560 | 10,560 | 10,560 | 10,560 | 10,560 | 10,560 | 10,560 | 10,560 | 21,120 | 21,120 | 21,120 | 21,120 | 21,120 | 21,120 | 21,120 | 21,120 | 21,120 | 21,120 | 21,120 | 21,120 |

9. Motor Output (Kv)

| Item             | 20  | 80  | 80  | 80  | 80  | 20  | 20  | 20  | 20  | 20  | 40  | 40  | 40  | 40  | 40  | 40  | 40  | 40  | 40  | 40  | 40  | 40  |
|------------------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| Raw Water Pump   | 589 | 606 | 619 | 630 | 643 | 655 | 668 | 682 | 696 | 711 | 726 | 741 | 756 | 771 | 786 | 801 | 816 | 831 | 846 | 861 | 876 | 891 |
| Clear Water Pump | 80  | 80  | 80  | 80  | 80  | 80  | 80  | 80  | 80  | 80  | 80  | 80  | 80  | 80  | 80  | 80  | 80  | 80  | 80  | 80  | 80  | 80  |

10. Energy Consumption (Kwh/day)

| Item             | 589 | 606 | 619 | 630 | 643 | 655 | 668 | 682 | 696 | 711 | 726 | 741 | 756 | 771 | 786 | 801 | 816 | 831 | 846 | 861 | 876 | 891 |
|------------------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| Raw Water Pump   | 589 | 606 | 619 | 630 | 643 | 655 | 668 | 682 | 696 | 711 | 726 | 741 | 756 | 771 | 786 | 801 | 816 | 831 | 846 | 861 | 876 | 891 |
| Clear Water Pump | 970 | 970 | 970 | 970 | 970 | 970 | 970 | 970 | 970 | 970 | 970 | 970 | 970 | 970 | 970 | 970 | 970 | 970 | 970 | 970 | 970 | 970 |

11. Pump Operation Cost (Baht 11,000/year)

| Item             | 275 | 275 | 275 | 275 | 275 | 275   | 275   | 275   | 275   | 275   | 275   | 275   | 275   | 275   | 275   | 275   | 275   | 275   | 275   | 275   | 275   | 275   |
|------------------|-----|-----|-----|-----|-----|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Raw Water Pump   | 275 | 275 | 275 | 275 | 275 | 275   | 275   | 275   | 275   | 275   | 275   | 275   | 275   | 275   | 275   | 275   | 275   | 275   | 275   | 275   | 275   | 275   |
| Clear Water Pump | 709 | 707 | 713 | 718 | 724 | 730   | 736   | 742   | 748   | 754   | 760   | 766   | 772   | 778   | 784   | 790   | 796   | 802   | 808   | 814   | 820   | 826   |
| Total Cost       | 975 | 982 | 987 | 993 | 999 | 1,000 | 1,014 | 1,028 | 1,042 | 1,057 | 1,071 | 1,085 | 1,099 | 1,113 | 1,127 | 1,141 | 1,155 | 1,169 | 1,183 | 1,197 | 1,211 | 1,225 |

Chemical Cost

| Item                    | 16,038 | 16,469 | 16,768 | 17,071 | 17,385 | 17,699 | 18,024 | 18,374 | 18,732 | 19,097 | 19,465 | 19,845 | 20,360 | 20,889 | 21,422 | 21,977 | 22,539 | 23,134 | 23,743 | 24,364 | 24,995 | 25,635 |
|-------------------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| Alum (ave 10.0 mg/l)    | 16,038 | 16,469 | 16,768 | 17,071 | 17,385 | 17,699 | 18,024 | 18,374 | 18,732 | 19,097 | 19,465 | 19,845 | 20,360 | 20,889 | 21,422 | 21,977 | 22,539 | 23,134 | 23,743 | 24,364 | 24,995 | 25,635 |
| Chemical (kg/y)         | 65.0   | 66.7   | 67.9   | 69.1   | 70.4   | 71.7   | 73.0   | 74.4   | 75.8   | 77.3   | 78.8   | 80.4   | 82.5   | 84.6   | 86.8   | 89.0   | 91.3   | 93.7   | 96.2   | 98.7   | 101.2  | 103.8  |
| Cost (Baht 1000)        | 16.0   | 16.5   | 16.8   | 17.1   | 17.4   | 17.7   | 18.0   | 18.4   | 18.7   | 19.1   | 19.5   | 19.8   | 20.4   | 20.9   | 21.4   | 22.0   | 22.5   | 23.1   | 23.7   | 24.3   | 24.9   | 25.6   |
| Chlorine (ave 2.0 mg/l) | 3,294  | 3,294  | 3,294  | 3,294  | 3,294  | 3,294  | 3,294  | 3,294  | 3,294  | 3,294  | 3,294  | 3,294  | 3,294  | 3,294  | 3,294  | 3,294  | 3,294  | 3,294  | 3,294  | 3,294  | 3,294  | 3,294  |
| Chemical (kg/y)         | 3,294  | 3,294  | 3,294  | 3,294  | 3,294  | 3,294  | 3,294  | 3,294  | 3,294  | 3,294  | 3,294  | 3,294  | 3,294  | 3,294  | 3,294  | 3,294  | 3,294  | 3,294  | 3,294  | 3,294  | 3,294  | 3,294  |
| Cost (Baht 1000)        | 50.0   | 51.4   | 52.3   | 53.3   | 54.2   | 55.2   | 56.2   | 57.3   | 58.4   | 59.5   | 60.7   | 61.9   | 63.5   | 65.2   | 66.9   | 68.6   | 70.3   | 72.2   | 74.1   | 76.0   | 78.0   | 80.0   |
| Total cost (Baht 1000)  | 131.0  | 137.0  | 139.5  | 142.0  | 144.6  | 147.3  | 150.1  | 153.0  | 156.0  | 159.0  | 162.1  | 166.3  | 170.7  | 175.1  | 179.5  | 184.1  | 189.0  | 194.0  | 199.1  | 204.2  | 209.5  | 215.0  |
| Total                   | 1,100  | 1,118  | 1,137  | 1,157  | 1,177  | 1,197  | 1,218  | 1,239  | 1,260  | 1,281  | 1,302  | 1,323  | 1,344  | 1,365  | 1,386  | 1,407  | 1,428  | 1,449  | 1,470  | 1,491  | 1,512  | 1,533  |









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