The native structure of rock including bedded plane, joint plane and schistsity appears different characteristic between granite area and Paleozoic area. As mentioned above, the granite is generally recognized as a uniform rock mass with a few discontinuous plane. The zone of dense joint plane however develops sparsely at the margin of intrusive.

On the other hand, Paleozoic member is marked by distinct bedded plane with secondary schistcity. The bed commonly shows the ENE to WSW strike with high angle dip, and is noted by thin bed repeating in several centimeters. These directions are also refrected to the topography, depressions or cols on ridge arranging in similar direction to strike, and the structure also forms a linear weathering zone along softer facies example for slaty horizon. The schistcity of them commonly does not develop fully due to the low metamorphic grade.

The proposed dam axis situate on the hard sandstone horizon of Paleozoic member. The dam axis is in the same direction to the strike of them so that the most part of dam foundation are occupied by a similar rock facies as well as hard sandstone drilled by boring survey.

(4) Permeability and Bearing Capacity

Permeability and N value of site are summarized at Figures 5-4-8 and 5-4-9. The permeability test reveals low permeability condition less than 5 Lugeon in bedrock without near the saddle dam.

The CT-4 borehole was drilled in the slope stretching from the abutment of saddle dam. The permeability data of CT-4 shows a changeable value ranging 1 to 35 Lugeon with high permeable peak at 28 to 33 m depth. These permeable layer is also correlative with the upper horizon of bedrock which is observed as a slight sign of weathering such as an oxidation along cracks. The general tendency of permeability however is decreasing toward lower horizon below 2 Lugeon while the upper horizon of 15 m depth is in over 10 Lugeon.

Bearing capacity is obviously different between overburden and bedrock. The overburden usually shows very small bearing capacity which is indicated smaller than 20 blows as N value. The minimum value of 0 to 1 blow were observed at the center of dam axis, and is in the clayey layer where intercalates above the weathered bedrock. However, the N value abruptly increases toward the lower horizon made up of weathered bedrock to over 50 blows which is sufficient for the bearing capacity for dam foundation.

5.5 Khlong Katha

(1) Topography

The topography is characterized by two significant lineations which are expressed by two major valleys running through NW to SE and NE to SW. Furthermore, they are both noticeable for that converage at the dam axis. The bird's eye views of Figures 5-5-1 and 5-5-2 distinctly shows these characteristics and that the proposed dam site is situated on a position at the intersected two valleys. Accordingly, the low hill extended from mountain remains at the center of dam site.

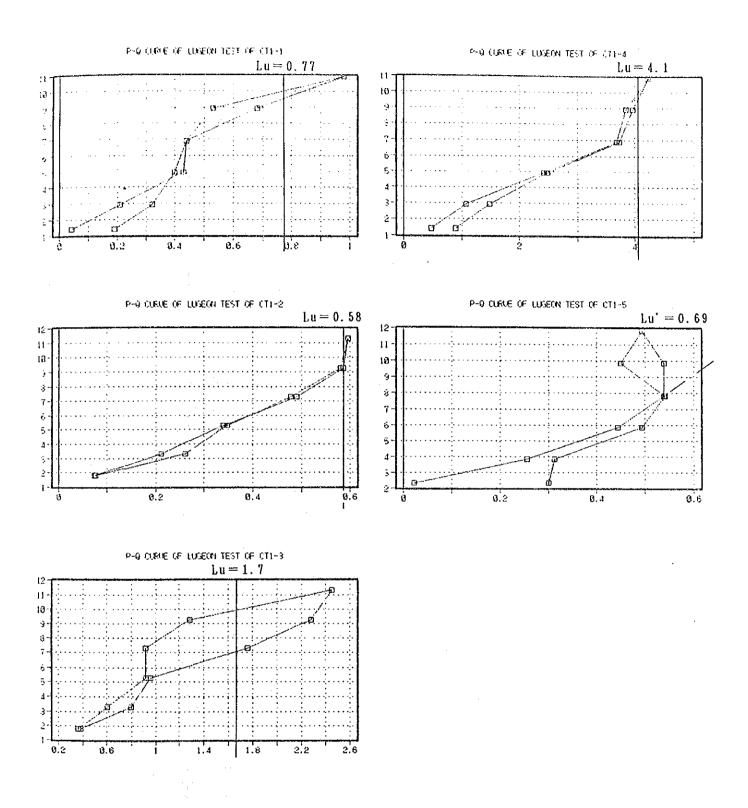
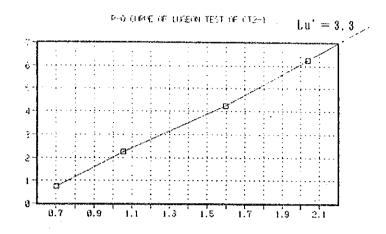
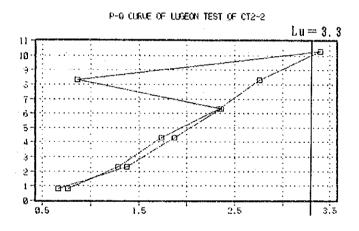


Fig. 5-4-9-1 Result of Lugion Test of CT-1





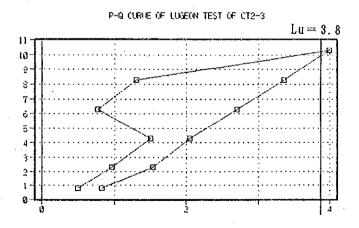


Fig. 5-4-9-2 Result of Lugion Test of CT-2

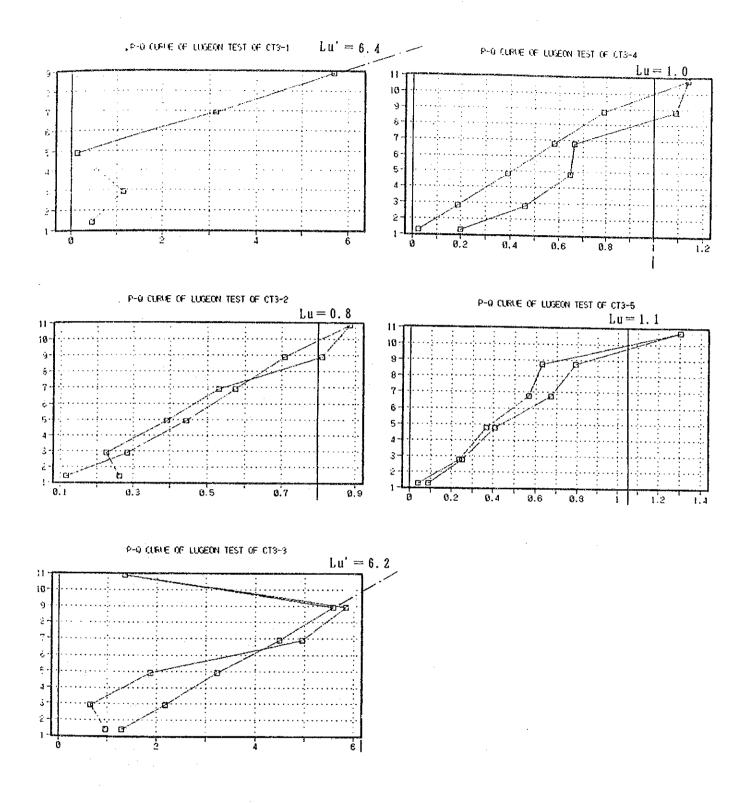
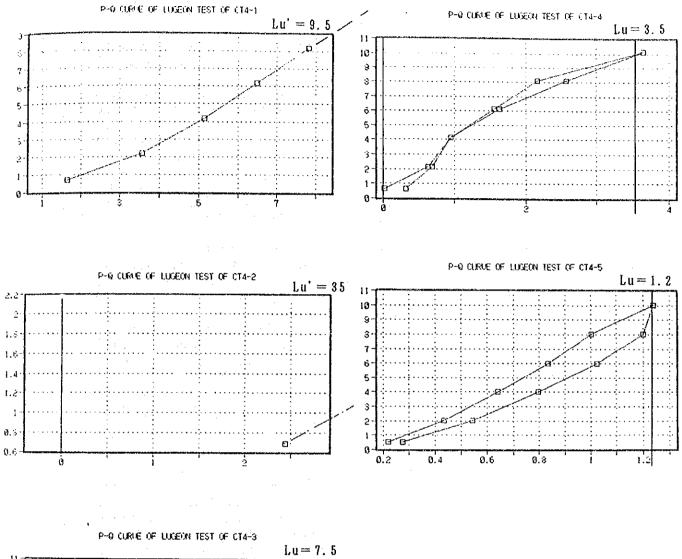


Fig. 5-4-9-3 Result of Lugion Test of CT-3



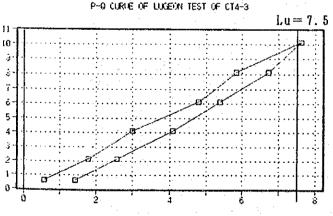


Fig. 5-4-9-4 Result of Lugion Test of CT-4

In accordance with above topographical feature, the lowest elevation at dam axis at about 24 m was seen at the both sides of river floor. The intermediate area of river floor is occupied by the low hilly mound with the relative height of about 5 m. As shown in Figure 5-5-5, the profile along dam axis also indicats the sharp boundary to sloping area from the river floor, so that the shape along dam axis is classified as a flat-floored to kastental valley.

The highest point in the watershed is shown at the northern summit of divide with the elevation of 400 m. On the other hand, the distance from dam axis to this summit is only 2.5 km. Therefore, the average gradient of slope is calculated to be 16/100. As shown in the longitudinal section of Figure 5-5-6, the detail profile along stream reveals the steeper slope than average gradient on the mountain area locally. The steepest slope is seen on the higher part above 100 m. The gradient is over 30/100 in contrast to lower part consisting of the flat river floor and terrace plane.

The terrace plane formed at several elevations are also observed in the watershed. The lowest terrace is situated beside the river bed and have a uniform plane flattened by sandy deposit at the elevation of 30 to 35 m. The higher terrace is on the side slope ranging the elevation of 50 to 75 m. Though the height of terrace position is variable individually, their topographical feature seems to be similar that the terrace deposit is not resting on plane and the eroded flat plane is only reserved on steep slopes. These terrace plane may be referred to as that the lower terrace and sandy deposit is corresponded to last transgression and that higher terrace is identical with an event of pleistocene eustatic changes.

(2) Overburden

The thickness of overburden is relatively thin in comparison with the other site as shown in Fig 5-5-8. The boring survey clarifies that its maximum depth is 13 m at the KK-2. The member of over burden however is same to the other site which is composed by top soil, sandy river deposit, sand and gravel terrace deposit and clayey deposit in order from the surface.

Top soil is marked by facies which is of the loose sand and gravel. It is underlain by a remarkable reddish layer. The layer mainly consist of lateritic clay ,furthermore, the under horizon of this layer is made up of the sandy terrace deposit. Terrace deposit correlating with lowest terrace is marked by the coarse sand with granule gravel and contains the tin minerals which has been dug for mining by several decades. The clayey facies was locally observed just on the bedrock. Its distribution shows an aspect as the filling up the relief of bedrock up to the 23 m in elevation. The facies are mainly of very soft greyish clay with high plasticity, but the thickness is less than 5 m resulting from KK-3 located at the center of its distribution.

(3) Bedrock

The geological members exposed on the site are shown in the Geological map of Khlong Katha Dam Site of Figure 5-5-7. The members without above mentioned overburden are grouped into two lithological types of granite which are of the coarse grained biotite porphyry or granite and the fine grained biotite-muscovite granite.

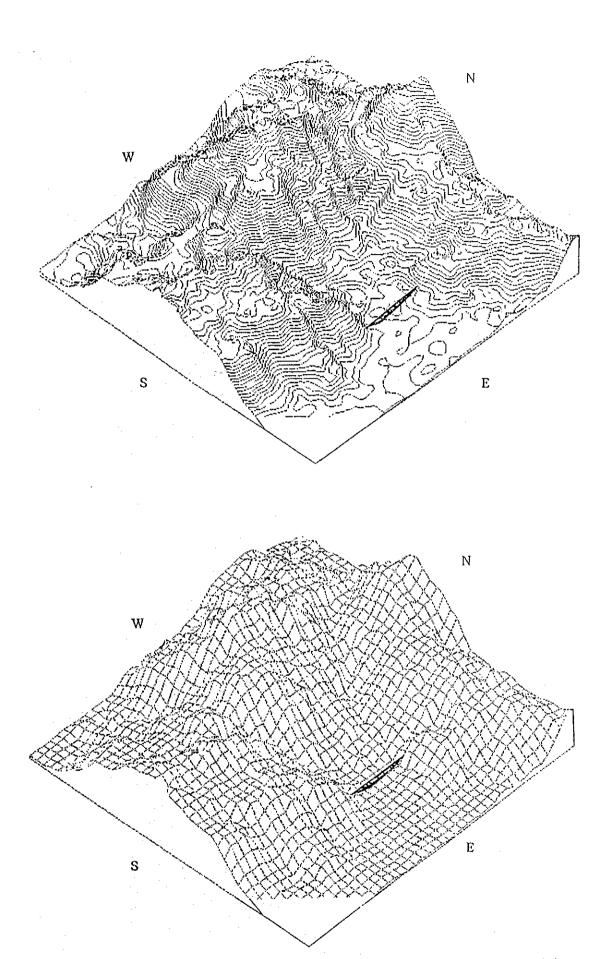
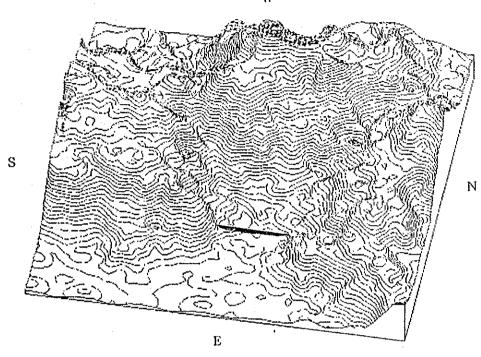


Fig. 5-5-1 Bird's Eye View of Khlong Katha Dam Site(1)



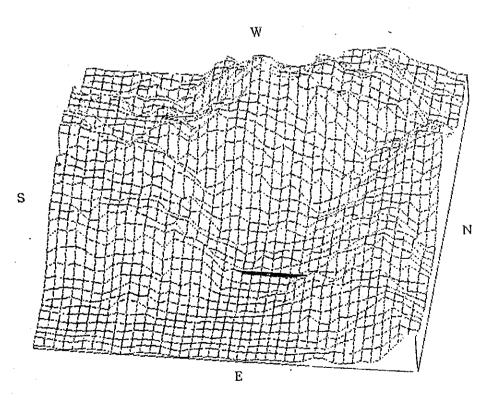


Fig. 5-5-2 Bird's Eye View of Khlong Katha Dam Site(2) 5-38

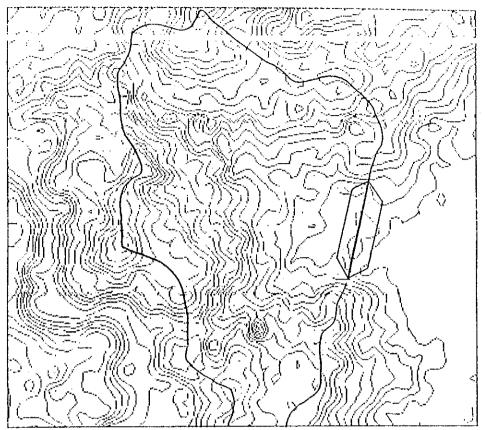


Fig. 5-5-3 Catchment Area of Khlong Katha Dam Site

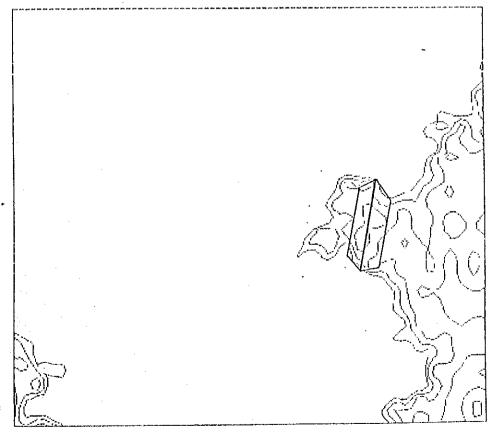


Fig. 5-5-4 Reservoir Area of Khlong Katha Dam Site 5-39

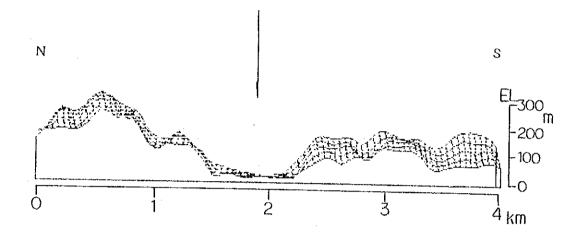


Fig. 5-5-5 Cross Section along Dam Axis of Khlong Katha Dam Site

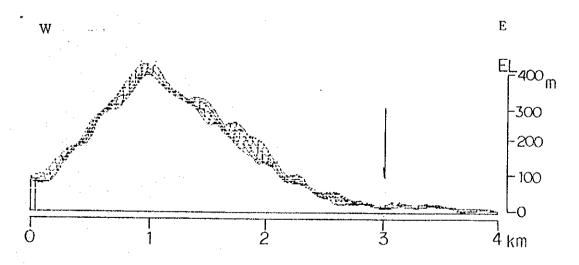
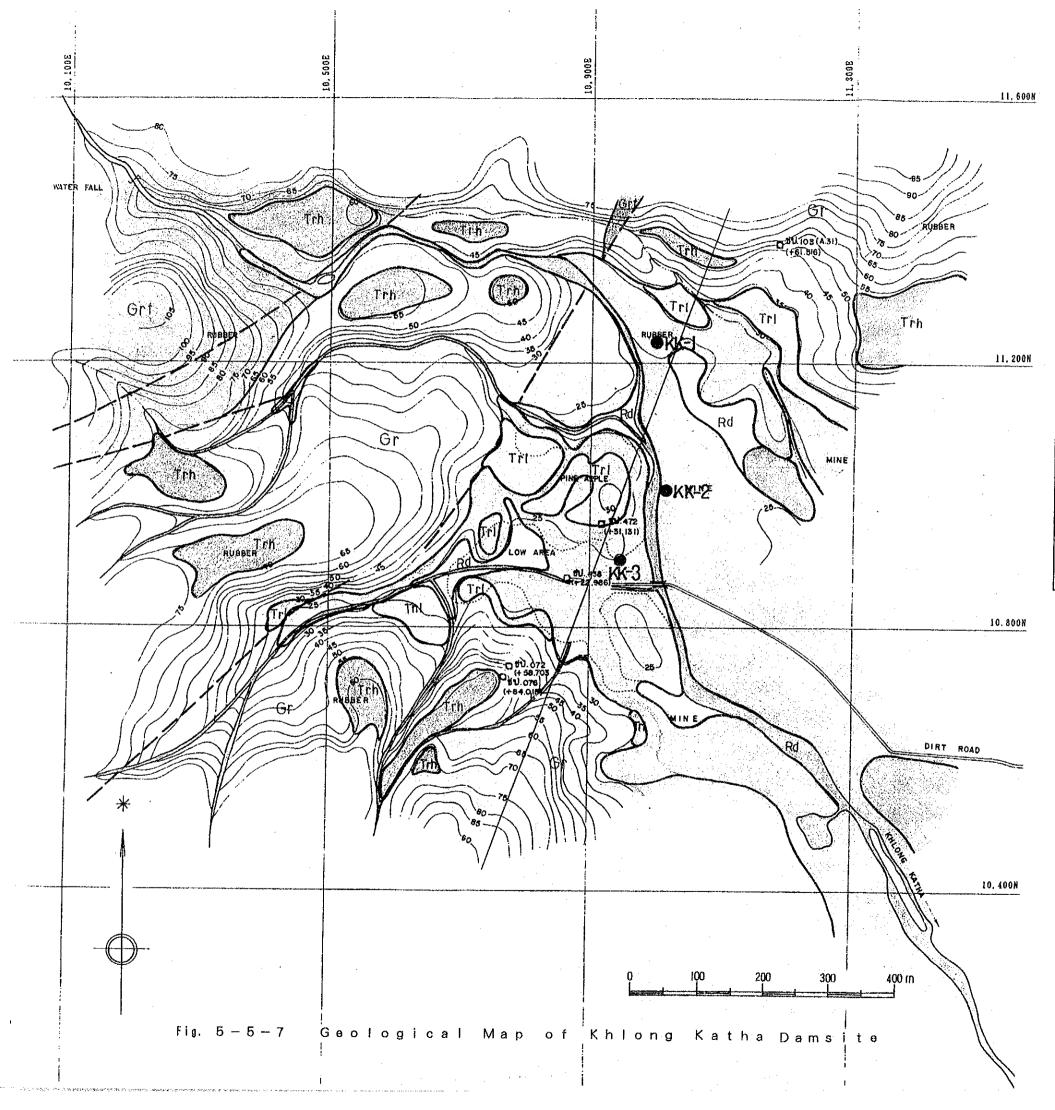


Fig. 5-5-6 Longidudinal Section along River Stream of Khlong Katha Dam Site



LEGEND Rd Alluvius Recent river deposite consisting of sand, gravel and silt. Swamp sediment of sand to clay Tre Erosional Terrace: Recent river terrace made up of gravel, sand and silt : Terrace deposit mainly composed of sand and gravel with thin clay layer Trl Lover Terrace Tra Middle Tarrace : Flat plain covering thin weathering material and sandy Layer locally Higher Terrace I : Erosional plain on the sideslope at the elevation of 100-150 m Trp Righer Terrace II : Highest erosional plain at the elevation of 200 m Ta Talus : Talus and colluvial deposite consisting of various size materials Ss Sandstone : Palaeozonic sandstone, beded metamorphosed sandstone with chert and slate layer S 1 Slate : Slate with metamorphosed sand and chert layer Gran Coarse Granite : Coarse grained biotite-porphyritic granite

: Fine grained biotite-muscovite granite

Get. Pine Granite

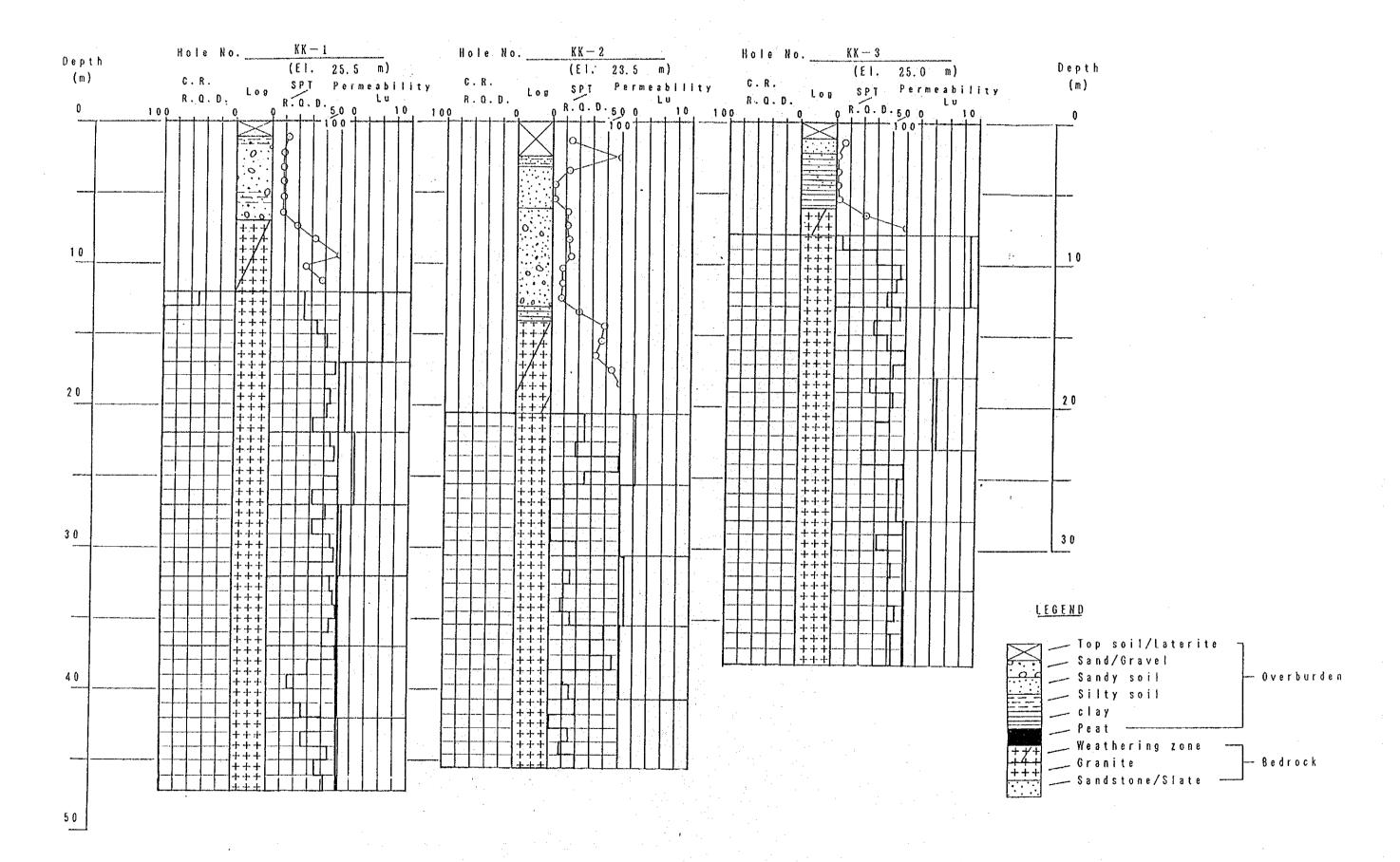


Fig. 5-5-8 Result of Boring Survey

The coarse granite forms the most part of the reservoir and south-eastern area of watershed. The rock mass is pronounced by the massive facies with minor intrusion of the granite-phophyry and quartz vein. According to the progress of boring survey, quartz vein is enable to readily distinguished from others since these facies are fairly harder for drilling than other layers. The facies' change occurs at the several meters in boreholes repeatedly.

The fine granite is marked by not only fine grained phonocryst but also high frequency of intrusive vein and remaining the bedded plane and joint plane. At the many outcrop these discontinuous planes well develop; consequently, the scarp or free face is formed in direction of these planes.

The weathering zone is also observed at both of boring core and outcrop. The weathering zone is less than 10 m and is of the light brown gravely facies with much content of clay. From the result of KK-2 which is located on the center of dam axis and have the thickest weathering zone, the sign of weathering was found out up to 24 m depth.

(4) Geological Structure

Two zones of faults are recognized in the field reconnaissance, one of which is running through the upstream of reservoir area and another is along the dam axis. Both roughly show the same trend of NE-SW to NNE-SSW and can be trace out in the watershed from the right slope to the left slope which does not across to the dam axis. Along these fault zone, the scarp or differential weathering is observed, Slight alterative layer is also interbedded along the contacted plane.

From the view point of general topographical property, two large lineations across the dam axis and may be inferred as a structural valley as previously stated. However, neither boring investigation nor field reconnaissance survey revealed any evidence of a fracture zone. The quantity of investigation however has not been enough until the present for leading a conclusion that these lineations are not derived from a fault structure.

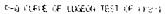
The primary structure such as the bedding or joint plane is not so many in the boring core while the watershed area locally presents a high frequency of discontinuous plane as already stated. Accordingly, it may be concluded that the bedrock making up of dam foundation does not involve any fracture and is built up of the massive rock facies.

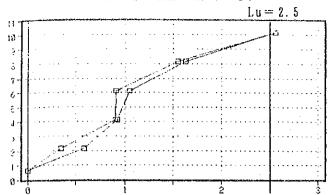
(5) Permeability and Bearing Capacity

Permeability observed in borehole was very low and less than 9 Lugeon. Especially below the 18 m depth, the permeability was further lower around 1 Lugeon. The bearing capacity in overburden deposit normally indicates small value which is less than 1 converting into N value.

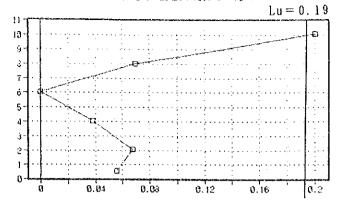
The result of permeability test is shown in Figure 5-5-9, the permeability of bedrock varies from 10 to 0.1 Lugeon which is differed in degree between the upper horizon and the lower one. The upper horizon, generally above 20 m depth, finding out a sign of weathering is

Fig. 5-5-9-1 Result of Lugion Test of KK-1

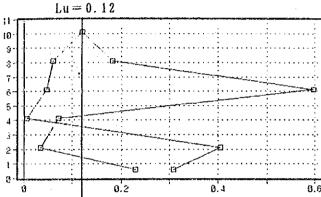




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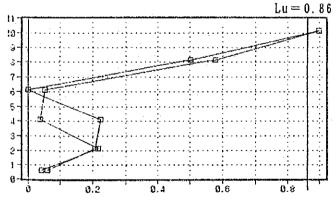
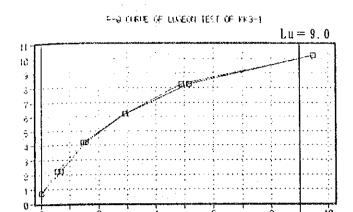
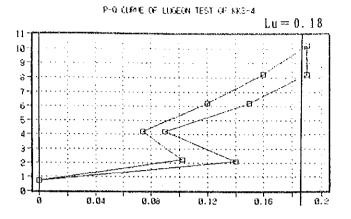
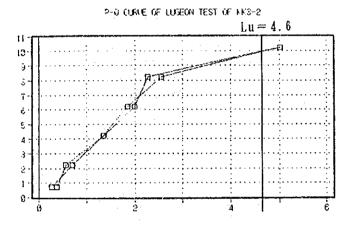


Fig. 5-5-9-2 Result of Lugion Test of KK-2







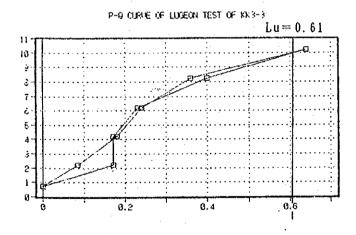


Fig. 5-5-9-3 Result of Lugion Test of KK-3

correlative with high permeability zone over the 5 Lugeon. In contrast to these, the lower horizon shows very low value indicating smaller than 1 Lugeon. Especially below the 25 m depth where any oxidative pollution by weathering was not found out in the boring core, the layer looks like a impervious rock mass.

Although the bearing capacity in overburden is very low, the layer showing low N value is so thin as usually presenting about 10 to 15 m. The minimum value observed in the site is obtained from the clayey horizon situated between weathering granite and sandy terrace deposit. Only 0 to 1 blow was observed there. It is increasing to both directions of the upper and lower horizon. Toward the lower facies of weathering granite, the bearing capacity becomes increasingly a large value more than 50 blows while it only increases up to 15 blows even in maximum value toward the upper facies of the terrace deposit and top soil.

5-6 Bang Tho Sung

(1) Topography

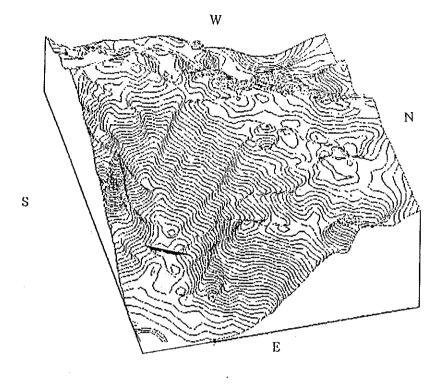
The Bang Tho Sung site is situated beside the Bangwad Reservoir. Its topographical aspect pronounced by the narrower river bed than the other proposed sites. As visualized from the bird's eye view of Figure 5-6-1, the site represents a trough shaped valley which involves the flat riverbed having longer axis along the stream and contrastively narrow width of riverbed. The planned dam length is less than 600 m which is the shortest among all sites in this study. However the short dam length, the reservoir occupies an area stretching out over 800 m to the upstream.

The lowest elevation is seen near the center of dam axis and is represented with the elevation about 30 m. The wide flat spreads out with similar elevation of dam axis to the down area and also the flat extends to 500 m to the upstream. The abutment slope have considerably steep gradient in contrast with these of low flat and continues to the the ridges forming the divide of watershed. The highest summit making the divide is presented with the elevation over the 450 m. As illustrated longitudinal and cross profile in Figures 5-6-5 and 5-6-6, the slope forming the ridge to low flat shows a peculiar form of the convex in the upper and contrastively concave in the lower slope ,and is marked by a modification of the several terrace plane resting on it. The average gradient of slope is estimated about 30/100. The terrace planes can be classified into three groups depending on their elevation respectively.

The lower terrace is at the elevation below 45 m and is located at the surroundings of the river bed. The middle terrace is at the elevation of about 50 m; the higher terrace is at 75 m. The deposit making the terrace surface is only shown on the lower one. The others are formed with an erosional plane as well as that of other dam site. Their origin is same to other site. Therefore, they are resulted from the Pleistocene sea level changes.

(2) Overburden

Since the boring survey was not conducted until the present, the overburden in the site only observed at the surface by the field



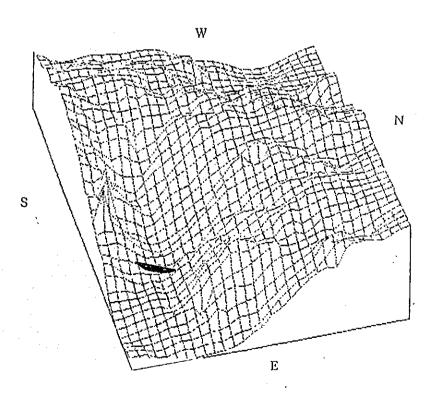
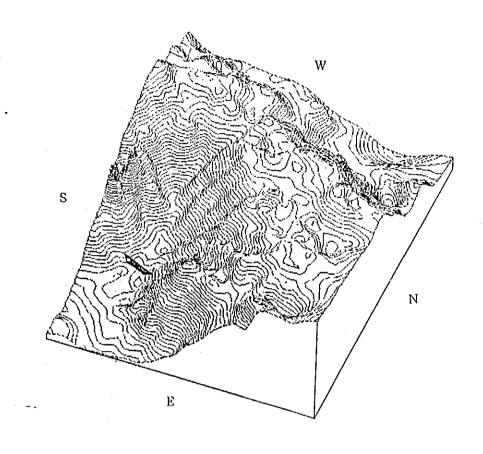


Fig. 5-6-1 Bird's Eye View of Bang The Sung Dam Site(1)



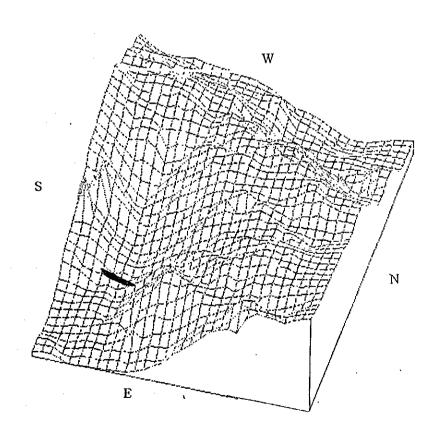
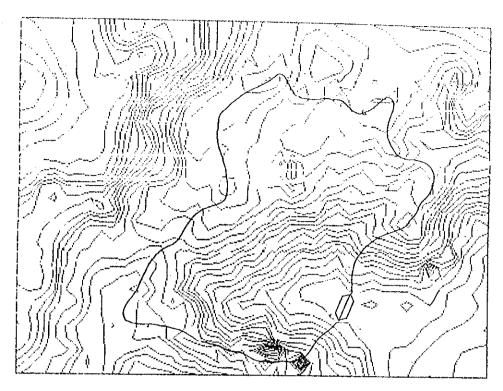


Fig. 5-6-2 Bird's Eye View of Bang The Sung Dam Site(2)



· Fig. 5-6-3 Catchment Area of Bang The Sung Dam Site

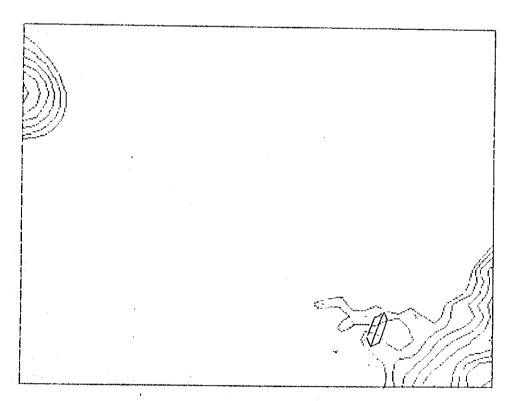


Fig. 5-6-4 Reservoir Area of Bang The Sung Dam Site

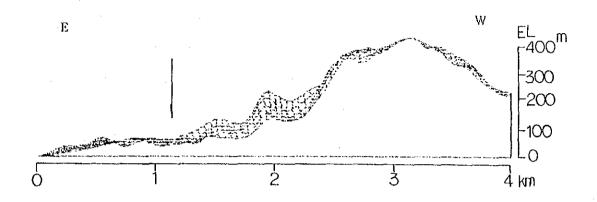


Fig. 5-6-5 Longitudinal Section along River Stream of Bang The Sung Dam Site

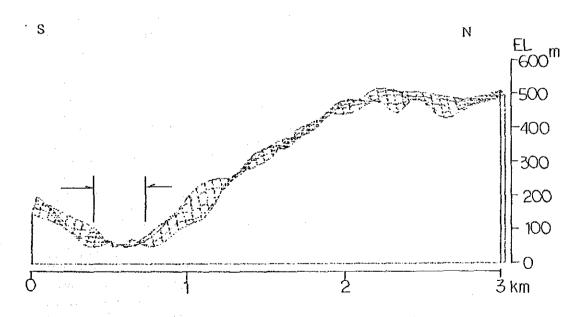


Fig. 5-6-6 Cross Section along Dam Axis of Bang The Sung Dam Site

reconnaissance. The member recognized in the surface is describable as three layers inclusive of Recent river deposit, lower terrace deposit and talus deposit in the order from the upper horizon.

Recent river deposit and lower deposit mainly consist of the loose sand and gravel facies, and spreads widely out the down of dam axis. The talus deposit is tractable to the foot slopes, especially between the constant slope and waning slope. It covers thickly on the surface. And the component of tulus deposit is mostly formed of the lateritic clay with gravel. Although the stratigraphical order for the overburden is still unknown, the layer of tulus facies plunges beneath the overlaying terrace deposit at the center of valley.

When the whole geological condition is supposed to be similar to Bangwad reservoir or Bang Nieo Dam site, the facies of overburden can be classified into above stated three members a total thickness of which may be inferred to be reached up to 20 m locally ranging from top soil to weathering granite.

(3) Bedrock

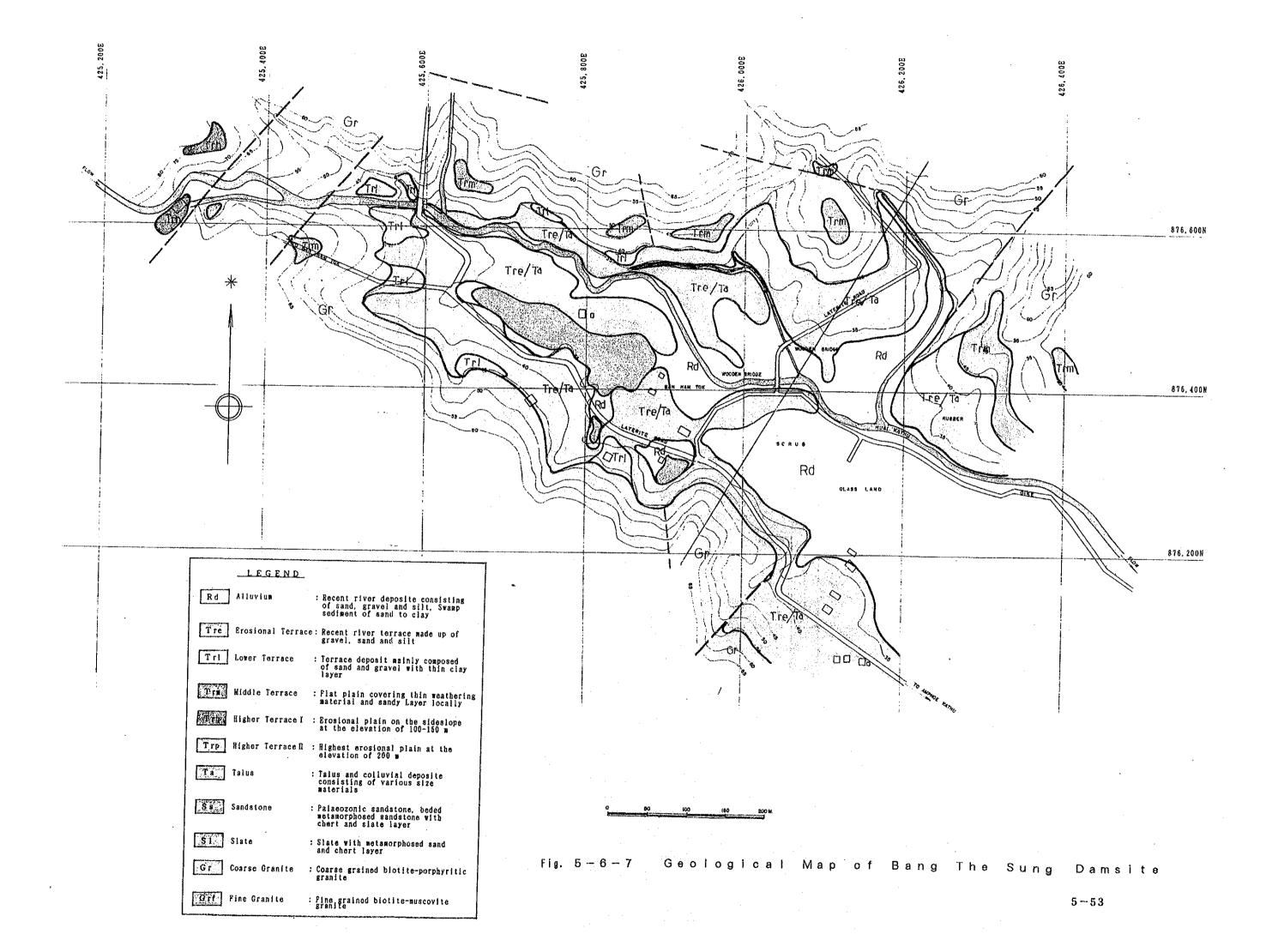
The bedrock of site is of granite which is classified as coarse grained biotite-phophyritic granite. Whole watershed area is formed of same type of granite; the rock is noted by uniformed mass with a few joint plane. The joint well develops locally for example, along a distributary at north of watershed. The distinct joints arranging in direction of ENE with 0.5 to 1 m interval is observed along a stream. The huge exposures are scattered on slope and fresh rock was observed there. The frequent quartz veins run through these outcrops on the southern slope of the reservoir.

However, the weathered zone in which the rock completely alter to sapolite is also found out at many places. Its thickness can hardly be grasped obviously since there is no boring survey. In case that the weathering condition seems to be equivalent to the Bang Nieo Dam site, the weathering zone is inferred to be at least 5 m on fresh granite facies.

(4) Geological Structure

The fault trending to the NE-SW is expressed as the main structure in the site which is the same faulting system as the regional lineation. In consequence of practical survey within the watershed, two faults in accordance with NE-SW trend are traceable downstream and the upstream respectively. Both faults are also supported by topographical characteristics such as cols on ridge, linear valley and fault scarp. They are correlative with next lineations recognized in the surrounding area at the site.

The secondary structure is shown along the direction of WNW-ESE and N-S which are interrupted by the main structure above. From the result of field reconnaissance, the lineations along them are dominant on the northern slope of reservoir and are topographically marked by a continuous fault scarp in many places, while most of these lineations are intercepted by the main structure. In view of geological structure, it may be assumed that a part of them passes the dam foundation, nevertheless the secondary faults are not continuously crossing by a main fault.



(5) Permeability and Bearing Capacity

Neither permeability nor bearing capacity was grasped through the insitu data not for carrying out the boring survey in this site. In order to be in these circumstance, the permeability and bearing capacity for this site have to be presumed on the basis of the data in other site. From the view point of surface condition of geology, the Ban Nieo Dam site appears to be similar to this site, so that it is expected that the permeability is probably low in the bed rock and that the bearing capacity is also low in the overburden.

GEOLOGICAL ASSESSMENT

The engineering geological assessment for dam construction is described in the following chapter with respect to the geological members of overburden and bedrock respectively.

6.1 Overburden

At the thought of dam construction, the most severe problem in all dam sites are very deep Recent river bed and terrace deposit.

The overburden, in general, can be classified into three facies as shown in the following Table 6-1-1 from the engineering properties inclusive of typographical situation, lithological change, permeability and bearing capacity.

	4 1	
:	Table 6-1-1	Classification of Overburden

Practical	Generalized	Average of	Maximum	Thickne	ess (m)
Classification	Lithology	N-value	BN	CT	KK
Top soil/River bed	Lateritic soil, Sand and gravel with clay	10	2	2	2
Terrace Deposit	Sand and gravel	15	10	7	10
Clay/Peat	Clayey deposit with sandy inter-calations.	1	7	7	3
Weathering zone of Bedrock	Lateritization, sapolite	50	17	15	6

BN : Bang Nieo Dam CT : Khao Che Tra KK : Khlong Katha

Based on the engineering geological characteristics, at least overburden including the lowest member of clayey deposit shall be excavated off throughout the dam foundation, because it is too loose to be used for dam foundation. Even if the dam scale is smaller than 30 m high, the bearing capacity of clayey deposit is so weak that all of overburden members have to be taken away. When the higher dam is planned, the excavation line shall be put on the deeper horizon which is correlative with the weathering zone of bedrock. For both abutment of all site and the low terrace hill seeing at Che tra site, the overburden are so thin that the stripping off can be reduced to only for top soil.

While at an impervious core trench, the overburden should be excavated completely, because it has high permeability in contrast to the bedrock especially at sandy and gravel layer. Moreover there is a doubt for a toughness as a foundation of dam, even small scale dam, in a part of loose clayey deposit.

6.2 Bedrock

The bed rock in the site consists of granite and sandstone. Among five proposed dam site, four sites of Khlong Lo Young, The Bang Nieo Dam, Khlong

Katha and Bang Tho Sung are observed granite. Only Che Tra site is formed of sandstone. Although they are lithologically quite different, the engineering characteristic is similar in parts; for example, the bearing capacity and permeability is indicated as severally strong and low for both rock facies. Consequently, there is no problem with a bearing capacity as a foundation of fill type dam if the overburden and highly weathered rock have been excavated. In the case of a large scaled dam more than 50 m in height such as Khlong Katha, Bang Tho Sung and Khlong Lo Young, the main part of foundation should be based on the fresh bedrock.

Permeability of foundation is generally low; however, the value shows the slightly higher than 2 Lugeon which is a target value for grouting work. Accordingly, the grouting work shall be required up to impervious zone of bedrock. The depth reaching out the impervious horizon is supposed to be 10 to 15 m from the surface of foundation so that the grouting curtain shall be provided to this level. The high permeability of grouting zone is mainly due to the crack and/or joints opened under the influence of weathering. A cement grouting is recommened for an impervious curtain treatment.

At any rate, grouting work is required to all of proposed sites even though the quantity of work is not so much.

6.3 Embankment Materials

There is no information for embankment materials except for that of field reconnaissance and existing study at Khlong Katha.

All of sites are composed of hard rock which is locally crop out on the side slope in the vicinity of dam site. In view of these geological condition, the riprap and rock zone materials are available to be readily obtained from the surrounding area.

The weathering zone is thick especially in the Paleozoic layer which is spread out in the Che Tra site, the down stream of Khlong Lo Young, Bang Nieo Dam and Bang Tho Sung sites. These weathering facies show favorable properties for core zone or random materials. The quantities of materials are also enough for embankment volume of proposed dam at above mentioned four sites but Khlong Katha. Since the bedrock of site is formed of granite at all, furthermore, the adjacent area of site is not also underlain by Paleozoic facies, the Khlong Katha site may be pointed out a difficulty in procurement of the core zone materials. However, it would be expected that a coming study for a wider area than this time or a careful consideration for dam types will solve the problem in the detailed design.

APPENDIX A-1

Boring Log

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