

インドネシア
ボゴール農科大学大学院計画
モデルインフラ整備事業実施設計調査
報 告 書

付属資料C

技術資料

平成 2 年 4 月

国際協力事業団

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付属資料 C. 技術資料

1. 気象
2. 水文
3. 土質
4. 灌溉排水
5. 工事明細書
6. 勞務費及び材料単価
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8. 全体計画
9. 灌溉用水水収支測定プロット(ライシメーター)
10. チイヒドゥンポンプ場
11. ワークショップ・ワークステーション

付属資料 C 1 気象

1. General
2. Collected Data
3. Evaluation, Tabulation and Analysis

1. General

The project site is located at the outskirts of Bogor city which is about 60 km south of Jakarta.

It is laid on the alluvial fan developed from the northern slope of the Salak volcanic mountain (EL. 2,211 m).

Its geographical position is 6°34'S, 106°43' E and the elevation is about 200 m above sea level.

The climate belongs to the tropical monsoonal pattern. The Salak volcanic mountain, along with other mountains to the east, influences the rainfall distribution in the vicinity of Bogor city.

The Darmaga rainfall observation station was established in January, 1964 by the Meteorology and Geophysics Board of the Government (BMG) and in 1976 it is reorganized as the 1st class Climatological Station Darmaga Bogor (CSDB) with installation of additional climate measurement instrument. Since then, the climate observation is operating by the said BMO. The main office is located at Jalan Raya Darmaga 6.5 km, but its observation station is placed on the cleared land between the swamp (Rawadja) and the rubber forest in the north-east about 2.5 km of the project site. It can be accessed through Jalan Sindangbarang from Jalan Raya Sindang Barang or through village road from the Darmaga Campus IPB. Its geographic position is announced to be 6°30'S, 106°45'E, EL. 250 m, however, it can be read as 6°33'S, 106°45'E, EL. 190 m from the topographic map with scale of 1/50,000.

The area of the CSDB is 250 m² with 50 m length and 50 m width. The observing meteorological elements are air temperature, humidity, air pressure, sunshine, radiation, evaporation, wind speed and soil temperature.

2. Collected Data

The valuable observation records have been collected during the field survey period for the study as follows :

| Items | Calendar year | | | | | | | | | | | | | | | | | | | n | | | | | | |
|--------------------|---------------|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|
| | 64 | 65 | 66 | 67 | 68 | 69 | 70 | 71 | 72 | 73 | 74 | 75 | 76 | 77 | 78 | 79 | 80 | 81 | 82 | 83 | 84 | 85 | 86 | 87 | 88 | 89 |
| 1. Monthly Data | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1.1 Mean Tem. | | | | | | | | | | | | | | | | | | | | | | | | | | 19 |
| 1.2 Max Tem. | | | | | | | | | | | | | | | | | | | | | | | | | | 19 |
| 1.3 Min Tem. | | | | | | | | | | | | | | | | | | | | | | | | | | 19 |
| 1.4 Rainfall | | | | | | | | | | | | | | | | | | | | | | | | | | 26 |
| 1.5 Rainy day | | | | | | | | | | | | | | | | | | | | | | | | | | 26 |
| 1.6 Max. 24hr Rain | | | | | | | | | | | | | | | | | | | | | | | | | | 26 |
| 1.7 Re. Humidity | | | | | | | | | | | | | | | | | | | | | | | | | | 19 |
| 1.8 Sunshine % | | | | | | | | | | | | | | | | | | | | | | | | | | 19 |
| 2. Daily Data | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 2.1 Mean Tem. | | | | | | | | | | | | | | | | | | | | | | | | | | 13 |
| 2.2 Max Tem. | | | | | | | | | | | | | | | | | | | | | | | | | | 13 |
| 2.3 Min Tem. | | | | | | | | | | | | | | | | | | | | | | | | | | 13 |
| 2.4 Rainfall | | | | | | | | | | | | | | | | | | | | | | | | | | 13 |
| 2.5 Sunshine % | | | | | | | | | | | | | | | | | | | | | | | | | | 13 |
| 2.6 Re. Humidity | | | | | | | | | | | | | | | | | | | | | | | | | | 13 |
| 2.7 Pan Evap. | | | | | | | | | | | | | | | | | | | | | | | | | | 13 |
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| 3. Hourly Data | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 3.1 Rainfall | | | | | | | | | | | | | | | | | | | | | | | | | | 5 |

3. Evaluation, Tabulation and Analysis

All the collected data have been evaluated, tabulated and analyzed as shown in the following tables and a figure.

- Table C1-1 Monthly Mean temperature at the Climatological Station of Darmaga Bogor (CSDB)
- C1-2 Monthly Mean Maximum Temperature at the Climatological Station of Darmaga Bogor (CSDB)
- C1-3 Monthly Mean Minimum Temperature at the Climatological Station of Darmaga Bogor (CSDB)
- C1-4 Monthly Maximum Temperature at the Climatological Station of Darmaga Bogor (CSDB)
- C1-5 Monthly Minimum Temperature at the Climatological Station of Darmaga Bogor (CSDB)
- C1-6 Monthly Mean Relative Humidity (%) at the Climatological Station of Darmaga Bogor (CSDB)
- C1-7 Monthly Mean and Maximum of Pan Evaporation at the Climatological Station of Darmaga Bogor (CSDB)
- C1-8 Monthly Mean of Sunshine Percentage between 8:00 and 16:00 at the Climatological Station of Darmaga Bogor (CSDB)
- C1-9 Monthly Mean of Radiation Intensity (Kcal/cm²/day) at the Climatological Station of Darmaga Bogor (CSDB)
- C1-10 Monthly Total Rainfall at the Climatological Station of Darmaga Bogor (CSDB)
- C1-11 Number of Rainy Days at the CSDB
- C1-12 The Highest 24 hours Rainfall in the Month at the CSDB
- C1-13 Probability Calculation on the Highest Rainfall Data at the CSDB by Gumble Method, Data Period 26 years from 1964 to 1989
- | | | |
|--------------|---------------|---------------------|
| (1) January | (7) July | (13) Annual Maximum |
| (2) February | (8) August | |
| (3) March | (9) September | |
| (4) April | (10) October | |
| (5) May | (11) November | |
| (6) June | (12) December | |
- C1-14 The Highest Rainfall (mm) for the Short Duration in the Month and Annual at the CSDB
- | | |
|-------|------------|
| No. 1 | 1985, 1986 |
| No. 2 | 1987, 1988 |
| No. 3 | 1989 |
- C1-15 Calculation of Probability of Exceedance on the Data of the Short Duration Rainfall Intensity (mm/hr)
- | | |
|-------|---------------------------------------|
| No. 1 | 5 minutes, 10 minutes and 15 minutes |
| No. 2 | 30 minutes, 45 minutes and 60 minutes |
| No. 3 | 2 hours, 3 hours and 6 hours |
| No. 4 | 12 hours and 24 hours |
- C1-16 The Longest Dry Consecutive Days During one year at the CSDB

C1-17 Calculation of Probability of Exceedance on the Data of the Monthly Mean Pan Evaporation at the CSDB

- No. 1 January, February and March
- No. 2 April, May and June
- No. 3 July, August and September
- No. 4 October, November and December

C1-18 Estimated Possible Working Hours of Outdoor Works for Construction and Farming Practice

- No. 1 1985
- No. 2 1986
- No. 3 1987
- No. 4 1988
- No. 5 1989
- No. 6 Recapitulation of Estimated Possible Working hours and their percentage to the Scheduled Construction Working Hours

Fig.C1-1 Curves of Probable Rainfall Intensity in mm/hour

Table C1-1 Monthly Mean Temperature At The Climatological Station of Darmaga Bogor (CSDB)

| YEAR | Temperature in degree centigrade (°C) | | | | | | | | | | | |
|------|---------------------------------------|------|------|------|------|------|------|------|------|------|------|------|
| | Jan. | Feb. | Mar. | Apr. | May | Jun. | Jul. | Aug. | Sep. | Oct. | Nov. | Dec. |
| 1977 | 24.5 | 24.6 | 24.7 | 25.6 | 25.7 | 24.9 | 25.0 | 25.0 | 25.2 | 26.7 | 25.8 | 25.3 |
| 1978 | 24.7 | 25.1 | 25.3 | 25.3 | 25.7 | 25.2 | 24.8 | 25.1 | 25.3 | 25.1 | 25.6 | 24.9 |
| 1979 | 25.0 | 25.0 | 25.3 | 25.5 | 25.7 | 25.3 | 24.9 | 25.3 | 25.6 | 25.8 | 25.8 | 25.1 |
| 1980 | 24.7 | 24.8 | 24.8 | 25.6 | 26.0 | 26.2 | 25.3 | 24.8 | 25.8 | 25.4 | 25.5 | 24.9 |
| 1981 | 24.1 | 24.8 | 25.5 | 24.9 | 25.8 | 25.6 | 25.1 | 25.3 | 25.8 | 26.1 | 25.6 | 25.6 |
| 1982 | 24.1 | 24.8 | 25.1 | 25.3 | 25.9 | 25.4 | 25.0 | 24.9 | 25.6 | 26.0 | 26.1 | 25.8 |
| 1983 | 25.3 | 25.6 | 25.9 | 26.2 | 26.0 | 26.1 | 25.5 | 25.8 | 26.2 | 25.8 | 25.4 | 25.3 |
| 1984 | 24.7 | 24.6 | 24.9 | 25.3 | 24.9 | 25.3 | 25.0 | 25.0 | 24.7 | 25.8 | 25.5 | 24.9 |
| 1985 | 24.9 | 25.5 | 25.6 | 25.7 | 25.9 | 25.4 | 24.7 | 25.3 | 25.5 | 25.5 | 25.8 | 25.6 |
| 1986 | 24.7 | 24.6 | 24.8 | 25.7 | 26.2 | 25.7 | 25.1 | 25.0 | 25.1 | 25.8 | 25.0 | 25.7 |
| 1987 | 24.9 | 24.6 | 25.5 | 26.1 | 25.7 | 26.9 | 25.7 | 25.7 | 26.4 | 26.6 | 26.2 | 25.5 |
| 1988 | 25.7 | 25.4 | 25.5 | 26.3 | 26.1 | 25.4 | 25.7 | 25.6 | 26.1 | 26.0 | 25.8 | 24.7 |
| 1989 | 25.3 | 24.4 | 25.0 | 25.8 | 26.4 | 26.8 | 25.2 | 25.7 | 25.6 | 25.7 | 25.9 | 25.4 |
| Mean | 24.8 | 24.9 | 25.2 | 25.6 | 25.8 | 25.7 | 25.2 | 25.3 | 25.6 | 25.9 | 25.7 | 25.3 |

Table C1-2 Monthly Mean Maximum Temperature At The Climatological Station of Darmaga Bogor (CSDB)

| YEAR | Temperature in degree centigrade (°C) | | | | | | | | | | | |
|------|---------------------------------------|------|------|------|------|------|------|------|------|------|------|------|
| | Jan. | Feb. | Mar. | Apr. | May | Jun. | Jul. | Aug. | Sep. | Oct. | Nov. | Dec. |
| 1977 | 30.3 | 29.8 | 30.7 | 32.4 | 32.3 | 31.0 | 32.3 | 32.6 | 32.2 | 34.5 | 32.8 | 31.6 |
| 1978 | 30.3 | 31.1 | 31.5 | 32.3 | 32.2 | 31.7 | 30.7 | 30.0 | 30.8 | 31.2 | 31.6 | 29.6 |
| 1979 | 29.3 | 31.0 | 30.5 | 31.2 | 31.5 | 30.8 | 31.2 | 31.5 | 31.9 | 32.3 | 31.2 | 29.8 |
| 1980 | 28.5 | 29.7 | 31.3 | 31.6 | 31.6 | 31.7 | 31.4 | 31.0 | 31.7 | 31.6 | 31.4 | 29.8 |
| 1981 | 27.7 | 29.6 | 30.7 | 31.3 | 31.3 | 31.3 | 30.4 | 30.8 | 31.8 | 32.0 | 30.4 | 29.9 |
| 1982 | 27.8 | 29.6 | 30.7 | 30.6 | 31.4 | 30.9 | 31.1 | 31.8 | 33.5 | 33.2 | 32.9 | 31.3 |
| 1983 | 29.6 | 30.9 | 31.2 | 31.7 | 31.2 | 32.1 | 31.5 | 32.5 | 33.0 | 31.9 | 30.4 | 30.4 |
| 1984 | 28.7 | 28.9 | 29.9 | 30.5 | 30.7 | 31.0 | 30.7 | 30.9 | 30.4 | 31.5 | 31.1 | 29.4 |
| 1985 | 29.5 | 30.5 | 30.9 | 30.7 | 31.3 | 30.6 | 29.9 | 31.3 | 31.3 | 31.2 | 31.1 | 30.8 |
| 1986 | 28.2 | 29.7 | 30.0 | 31.2 | 31.8 | 31.3 | 30.9 | 30.8 | 30.7 | 31.2 | 30.6 | 30.9 |
| 1987 | 28.4 | 28.7 | 31.0 | 31.3 | 31.4 | 31.3 | 31.5 | 32.6 | 33.0 | 32.8 | 31.9 | 29.7 |
| 1988 | 30.2 | 30.3 | 30.6 | 31.6 | 31.3 | 30.9 | 31.6 | 31.5 | 32.8 | 31.6 | 30.8 | 29.0 |
| 1989 | 29.7 | 28.0 | 30.1 | 31.4 | 30.8 | 30.7 | 31.3 | 31.5 | 31.7 | 31.7 | 30.8 | 29.8 |
| Mean | 29.1 | 29.8 | 30.7 | 31.4 | 31.4 | 31.2 | 31.1 | 31.4 | 31.9 | 32.0 | 31.3 | 30.2 |

Table CI-3 Monthly Mean Minimum Temperature At The Climatological Station of Darmaga Bogor (CSDB)

| YEAR | Temperature in degree centigrade (°C) | | | | | | | | | | | |
|------|---------------------------------------|------|------|------|------|------|------|------|------|------|------|------|
| | Jan. | Feb. | Mar. | Apr. | May | Jun. | Jul. | Aug. | Sep. | Oct. | Nov. | Dec. |
| 1977 | 21.2 | 21.6 | 21.5 | 22.1 | 22.2 | 21.5 | 20.6 | 21.0 | 20.3 | 21.2 | 21.6 | 21.7 |
| 1978 | 21.8 | 21.8 | 21.8 | 21.7 | 22.1 | 21.8 | 21.1 | 21.1 | 21.2 | 21.2 | 21.2 | 21.9 |
| 1979 | 21.9 | 22.0 | 22.2 | 22.2 | 21.7 | 21.3 | 20.1 | 20.1 | 21.1 | 21.4 | 22.2 | 21.7 |
| 1980 | 22.2 | 21.7 | 21.1 | 22.1 | 22.1 | 21.4 | 21.2 | 20.6 | 21.7 | 21.2 | 21.6 | 21.7 |
| 1981 | 21.2 | 21.2 | 21.8 | 21.9 | 25.8 | 21.7 | 21.5 | 21.6 | 21.7 | 21.8 | 21.8 | 21.7 |
| 1982 | 21.5 | 21.5 | 21.7 | 22.2 | 21.8 | 21.4 | 20.4 | 19.5 | 19.8 | 20.8 | 21.6 | 22.2 |
| 1983 | 22.3 | 22.3 | 22.6 | 22.6 | 22.7 | 21.1 | 20.9 | 20.8 | 21.1 | 21.6 | 21.9 | 21.2 |
| 1984 | 21.7 | 21.7 | 21.7 | 21.9 | 21.6 | 20.9 | 25.0 | 21.0 | 21.1 | 21.7 | 21.8 | 21.3 |
| 1985 | 21.7 | 21.8 | 21.8 | 22.5 | 22.6 | 21.8 | 21.1 | 20.2 | 21.3 | 21.6 | 21.7 | 21.5 |
| 1986 | 22.1 | 21.5 | 22.0 | 22.6 | 22.4 | 22.1 | 20.9 | 20.8 | 21.5 | 22.1 | 22.0 | 22.3 |
| 1987 | 22.5 | 21.9 | 22.4 | 22.8 | 22.1 | 22.4 | 21.4 | 20.7 | 21.6 | 22.1 | 21.7 | 22.4 |
| 1988 | 22.7 | 22.2 | 22.7 | 22.3 | 22.8 | 21.6 | 21.4 | 21.5 | 21.4 | 22.2 | 21.4 | 21.4 |
| 1989 | 22.3 | 21.9 | 21.7 | 22.1 | 22.4 | 22.3 | 21.2 | 21.5 | 21.4 | 21.8 | 22.1 | 22.2 |
| Mean | 21.9 | 21.8 | 21.9 | 22.2 | 22.5 | 21.6 | 21.3 | 20.8 | 21.2 | 21.6 | 21.7 | 21.8 |

Table C1-4

Monthly Maximum Temperature At The Climatological Station of Darmaga Bogor (CSDB)

Latitude : 06°30'S Longitude : 106°45'E Altitude : 250m.

| YEAR | Temperature in degree centigrade (°C) | | | | | | | | | | | |
|------|---------------------------------------|------|------|------|------|------|------|------|------|------|------|------|
| | Jan. | Feb. | Mar. | Apr. | May | Jun. | Jul. | Aug. | Sep. | Oct. | Nov. | Dec. |
| 1977 | 33.8 | 31.8 | 33.2 | 33.8 | 33.3 | 32.7 | 33.9 | 34.0 | 34.8 | 35.9 | 34.4 | 33.4 |
| 1978 | 32.9 | 33.3 | 33.8 | 33.2 | 33.2 | 32.9 | 32.8 | 32.0 | 32.9 | 32.8 | 33.7 | 31.7 |
| 1979 | 33.0 | 31.8 | 33.2 | 33.2 | 32.8 | 33.5 | 33.8 | 32.6 | 33.6 | 33.8 | 32.6 | 32.5 |
| 1980 | 31.0 | 32.8 | 33.2 | 32.9 | 33.2 | 32.7 | 32.6 | 33.0 | 33.7 | 33.6 | 32.8 | 31.4 |
| 1981 | 31.3 | 32.0 | 33.6 | 32.5 | 32.4 | 32.2 | 32.0 | 32.3 | 33.0 | 33.8 | 32.9 | 33.8 |
| 1982 | 30.4 | 32.6 | 33.1 | 31.6 | 31.6 | 32.2 | 32.6 | 32.4 | 33.4 | 34.8 | 35.6 | 34.7 |
| 1983 | 33.2 | 33.0 | 32.9 | 33.4 | 32.3 | 33.4 | 33.4 | 34.3 | 34.4 | 33.2 | 32.3 | 32.5 |
| 1984 | 31.6 | 31.0 | 31.8 | 32.0 | 31.8 | 32.2 | 32.0 | 32.0 | 32.6 | 33.7 | 33.7 | 32.4 |
| 1985 | 32.0 | 32.3 | 33.0 | 32.8 | 32.9 | 32.0 | 32.3 | 32.6 | 32.6 | 33.0 | 32.9 | 33.9 |
| 1986 | 31.5 | 31.1 | 31.8 | 32.7 | 33.2 | 32.8 | 32.7 | 32.7 | 32.6 | 32.6 | 32.4 | 32.4 |
| 1987 | 30.9 | 31.8 | 32.5 | 32.5 | 33.0 | 32.7 | 32.8 | 33.7 | 35.2 | 34.4 | 34.4 | 32.8 |
| 1988 | 33.2 | 32.6 | 32.1 | 32.9 | 32.2 | 32.4 | 33.0 | 33.9 | 34.4 | 34.5 | 32.7 | 32.6 |
| 1989 | 31.0 | 30.3 | 32.7 | 33.6 | 32.5 | 31.9 | 32.4 | 33.0 | 33.6 | 33.6 | 32.9 | 32.5 |
| Mean | 32.0 | 32.0 | 32.8 | 32.9 | 32.7 | 32.6 | 32.8 | 33.0 | 33.7 | 33.9 | 33.2 | 32.7 |

Table C1-5 Monthly Minimum Temperature At The Climatological Station of Darmaga Bogor (CSDB)

| YEAR | Temperature in degree centigrade (°C) | | | | | | | | | | | |
|------|---------------------------------------|------|------|------|------|------|------|------|------|------|------|------|
| | Jan. | Feb. | Mar. | Apr. | May | Jun. | Jul. | Aug. | Sep. | Oct. | Nov. | Dec. |
| 1977 | 19.3 | 20.5 | 20.4 | 20.8 | 19.7 | 18.5 | 18.9 | 18.5 | 17.0 | 20.0 | 20.4 | 20.2 |
| 1978 | 20.5 | 20.8 | 20.2 | 20.2 | 21.0 | 20.2 | 19.6 | 20.2 | 20.1 | 20.1 | 16.5 | 20.5 |
| 1979 | 20.7 | 21.0 | 20.8 | 21.0 | 18.4 | 18.6 | 14.2 | 19.0 | 13.6 | 18.4 | 21.0 | 18.3 |
| 1980 | 21.0 | 19.4 | 17.6 | 20.6 | 21.0 | 19.7 | 19.1 | 18.4 | 19.0 | 19.9 | 20.4 | 20.2 |
| 1981 | 19.6 | 20.0 | 19.6 | 20.3 | 19.6 | 20.0 | 20.0 | 19.7 | 20.2 | 18.6 | 19.5 | 20.5 |
| 1982 | 20.0 | 20.0 | 19.6 | 21.1 | 19.6 | 19.8 | 18.2 | 17.7 | 16.3 | 18.2 | 19.9 | 21.0 |
| 1983 | 20.9 | 21.0 | 20.8 | 21.0 | 21.4 | 19.4 | 18.5 | 18.0 | 19.3 | 20.5 | 20.6 | 17.8 |
| 1984 | 20.7 | 20.2 | 20.4 | 20.8 | 20.2 | 17.6 | 19.5 | 18.2 | 19.4 | 20.2 | 19.2 | 19.0 |
| 1985 | 19.9 | 20.2 | 19.5 | 21.3 | 21.2 | 19.6 | 20.0 | 18.3 | 19.4 | 19.8 | 20.3 | 19.8 |
| 1986 | 21.2 | 20.0 | 20.6 | 20.9 | 20.7 | 20.5 | 17.2 | 17.8 | 20.0 | 20.7 | 20.4 | 20.9 |
| 1987 | 21.5 | 20.5 | 21.0 | 21.4 | 19.8 | 20.6 | 19.9 | 18.6 | 19.2 | 20.6 | 21.2 | 21.2 |
| 1988 | 20.0 | 19.1 | 21.4 | 20.6 | 21.8 | 18.7 | 19.4 | 20.3 | 19.9 | 20.1 | 21.4 | 19.6 |
| 1989 | 21.0 | 20.6 | 19.6 | 21.0 | 21.4 | 21.0 | 19.8 | 19.5 | 19.0 | 20.4 | 20.1 | 20.1 |
| Mean | 20.5 | 20.3 | 20.1 | 20.8 | 20.4 | 19.6 | 18.8 | 18.6 | 19.8 | 20.1 | 19.9 | 19.9 |

Table C1-6 Monthly Mean Relative Humidity(%) at the Climatological Station of
Darmaga Bogor (CSDB)

| YEAR | Latitude : 06°30'S | | | Longitude : 106°45'E | | | Altitude : 250m. | | | Oct. | Nov. | Dec. | Average |
|------|--------------------|------|------|----------------------|-----|------|------------------|------|------|------|------|------|---------|
| | Jan. | Feb. | Mar. | Apr. | May | Jun. | Jul. | Aug. | Sep. | | | | |
| 1971 | 90 | 92 | 90 | 88 | 88 | 87 | 84 | 82 | 82 | 86 | 86 | 89 | 87 |
| 1972 | 92 | 88 | 89 | 86 | 88 | 81 | 78 | - | 71 | 74 | - | - | 83 |
| 1973 | 91 | 91 | 90 | 90 | 92 | 88 | 86 | 87 | 87 | 87 | 86 | 89 | 87 |
| 1974 | 92 | 89 | 89 | 87 | 88 | 86 | 86 | 87 | 87 | 88 | 88 | 86 | 88 |
| 1975 | 88 | 88 | 84 | 87 | 85 | 82 | 85 | 82 | 89 | 85 | 85 | 84 | 85 |
| 1976 | 89 | 82 | 85 | 82 | 78 | 75 | 71 | 75 | 72 | 78 | 83 | 82 | 79 |
| 1977 | 90 | 86 | 90 | 87 | 86 | 88 | 79 | 81 | 77 | 75 | 84 | 86 | 84 |
| 1978 | 89 | 87 | 89 | 87 | 87 | 86 | 85 | 84 | 84 | 86 | 82 | 88 | 86 |
| 1979 | 88 | 88 | 88 | 87 | 84 | 83 | 81 | 85 | 82 | 82 | 85 | 88 | 85 |
| 1980 | 90 | 87 | 87 | 81 | 85 | 81 | 84 | 82 | 83 | 87 | 85 | 88 | 85 |
| 1981 | 90 | 88 | 87 | 86 | 86 | 85 | 85 | 82 | 83 | 81 | 84 | 85 | 85 |
| 1982 | 92 | 88 | 88 | 90 | 85 | 85 | 82 | 77 | 75 | 78 | 83 | 87 | 84 |
| 1983 | 90 | 88 | 88 | 87 | 88 | 84 | 81 | 79 | 92 | 86 | 88 | 86 | 86 |
| 1984 | 89 | 89 | 89 | 90 | 90 | 83 | 85 | 86 | 86 | 84 | 87 | 87 | 87 |
| 1985 | 89 | 86 | 85 | 88 | 86 | 86 | 86 | 82 | 83 | 85 | 85 | 85 | 86 |
| 1986 | 91 | 88 | 89 | 87 | 84 | 89 | 82 | 81 | 84 | 85 | 88 | 87 | 86 |
| 1987 | 90 | 91 | 88 | 87 | 87 | 85 | 82 | 77 | 77 | 81 | 84 | 87 | 85 |
| 1988 | 87 | 87 | 88 | 85 | 88 | 85 | 80 | 82 | 77 | 83 | 85 | 88 | 85 |
| 1989 | 88 | 88 | 87 | 83 | 88 | 84 | 83 | 81 | 82 | 83 | 85 | 89 | 85 |
| Mean | 90 | 88 | 88 | 87 | 86 | 84 | 82 | 82 | 82 | 83 | 85 | 85 | 87 |

Table C1-7 Monthly Mean and Maximum of Pan Evaporation (mm/day) at
the Climatological Station of Dramaga Bogor (CSDB)

Latitude : 06°30'S Longitude : 106°45'E Altitude : 250m.

| YEAR | Jan. | Feb. | Mar. | Apr. | May | Jun. | Jul. | Aug. | Sep. | Oct. | Nov. | Dec. | No. 1 | |
|------|----------|------|------|------|------|------|------|------|------|------|------|------|-------------|------|
| | | | | | | | | | | | | | Annual Mean | Max |
| 1977 | Mean | 2.22 | 1.94 | 1.69 | 2.75 | 3.06 | 2.24 | 3.20 | 3.63 | 3.68 | 4.23 | 3.33 | 2.81 | 2.90 |
| | σ | 1.08 | 0.89 | 0.99 | 1.00 | 0.85 | 0.80 | 0.44 | 0.55 | 1.29 | 0.78 | 0.99 | 0.90 | |
| | Max | 4.1 | 3.5 | 3.9 | 4.3 | 4.5 | 4.3 | 3.9 | 4.1 | 6.6 | 5.9 | 4.9 | 5.3 | 6.6 |
| 1978 | Mean | 2.34 | 3.20 | 2.76 | 3.26 | 2.92 | 2.49 | 2.76 | 2.86 | 3.30 | 3.70 | 4.45 | 3.30 | 2.86 |
| | σ | 1.40 | 1.30 | 1.18 | 1.32 | 0.86 | 0.87 | 0.84 | 1.26 | 0.85 | 1.21 | 1.60 | 1.65 | |
| | Max | 6.0 | 5.7 | 5.9 | 6.8 | 4.9 | 3.9 | 4.2 | 6.5 | 4.6 | 5.4 | 6.4 | 6.0 | 6.8 |
| 1979 | Mean | 2.92 | 3.12 | 2.97 | 3.08 | 3.02 | 2.66 | 3.06 | 3.03 | 3.24 | 3.57 | 2.53 | 2.32 | 2.96 |
| | σ | 1.22 | 0.99 | 1.13 | 0.90 | 0.73 | 0.89 | 0.76 | 0.94 | 0.87 | 0.88 | 0.63 | 0.97 | |
| | Max | 5.8 | 5.8 | 5.0 | 4.6 | 4.6 | 4.8 | 4.4 | 5.3 | 5.4 | 4.7 | 3.4 | 3.9 | 5.8 |
| 1980 | Mean | 1.75 | 2.34 | 2.87 | 2.25 | 2.62 | 2.91 | 2.98 | 2.92 | 3.20 | 3.13 | 3.06 | 2.31 | 2.70 |
| | σ | 1.00 | 1.23 | 1.26 | 0.59 | 0.89 | 1.09 | 0.64 | 1.16 | 0.94 | 0.97 | 0.92 | 1.02 | |
| | Max | 4.7 | 5.5 | 5.4 | 3.6 | 3.9 | 6.8 | 4.2 | 5.2 | 5.0 | 5.1 | 5.2 | 4.6 | 6.8 |
| 1981 | Mean | 1.69 | 2.71 | 2.99 | 3.02 | 2.75 | 2.72 | 2.79 | 2.68 | 2.84 | 3.16 | 2.87 | 2.86 | 2.76 |
| | σ | 0.70 | 1.03 | 0.88 | 0.87 | 0.89 | 0.79 | 0.85 | 0.78 | 0.89 | 1.12 | 0.84 | 1.14 | |
| | Max | 3.2 | 4.8 | 4.7 | 4.6 | 4.5 | 4.8 | 4.6 | 4.3 | 4.3 | 5.3 | 4.3 | 6.0 | 6.0 |
| 1982 | Mean | 1.67 | 2.76 | 2.87 | 2.63 | 2.73 | 2.40 | 2.70 | 3.09 | 3.85 | 3.74 | 3.21 | 2.63 | 2.86 |
| | σ | 0.77 | 1.01 | 0.82 | 0.80 | 0.73 | 0.63 | 0.49 | 0.88 | 0.56 | 0.87 | 0.80 | 0.97 | |
| | Max | 3.4 | 5.1 | 5.3 | 4.3 | 3.7 | 3.6 | 3.7 | 4.9 | 4.9 | 6.0 | 4.2 | 4.9 | 6.0 |
| 1983 | Mean | 2.49 | 2.94 | 3.12 | 3.26 | 3.00 | 3.40 | 3.40 | 4.05 | 4.67 | 3.64 | 3.09 | 3.67 | 3.39 |
| | σ | 0.93 | 0.86 | 1.28 | 0.89 | 0.83 | 0.69 | 0.98 | 0.55 | 0.60 | 1.07 | 0.87 | 1.09 | |
| | Max | 5.2 | 5.2 | 5.8 | 5.1 | 4.8 | 4.2 | 4.7 | 5.3 | 6.3 | 5.6 | 5.5 | 6.4 | 6.4 |

Table C1-7 Monthly Mean and Maximum of Pan Evaporation (mm/day) at
the Climatological Station of Dramaga Bogor (CSDB)

Latitude : 06°30'S Longitude : 106°45'E Altitude : 250m.

| YEAR | No. 2 | | | | | | | | | | | | |
|-----------|-------|------|------|------|------|------|------|------|------|------|------|------|------------------|
| | Jan. | Feb. | Mar. | Apr. | May | Jun. | Jul. | Aug. | Sep. | Oct. | Nov. | Dec. | Annual Mean, Max |
| 1984 Mean | 2.72 | 2.84 | 2.95 | 3.10 | 2.83 | 3.16 | 3.26 | 3.70 | 3.25 | 3.86 | 3.37 | 3.02 | 3.17 |
| σ | 1.12 | 0.88 | 1.03 | 0.73 | 0.82 | 0.63 | 0.76 | 0.82 | 0.77 | 0.87 | 0.99 | 1.24 | |
| Max | 5.1 | 4.3 | 4.7 | 5.6 | 5.6 | 4.1 | 4.8 | 5.4 | 4.9 | 5.4 | 5.2 | 5.9 | 5.9 |
| 1985 Mean | 3.01 | 3.44 | 3.72 | 3.25 | 3.19 | 2.81 | 2.70 | 3.79 | 4.11 | 3.60 | 3.78 | 3.86 | 3.43 |
| σ | 1.10 | 0.98 | 1.02 | 0.89 | 0.72 | 0.79 | 0.72 | 0.66 | 0.60 | 0.89 | 1.17 | 1.27 | |
| Max | 5.0 | 4.5 | 5.5 | 5.4 | 5.0 | 4.0 | 3.6 | 5.2 | 5.3 | 5.1 | 5.8 | 6.6 | 6.6 |
| 1986 Mean | 2.52 | 3.24 | 2.93 | 3.35 | 3.78 | 3.28 | 3.41 | 3.65 | 3.50 | 4.11 | 3.51 | 3.80 | 3.42 |
| σ | 0.72 | 1.05 | 0.87 | 0.75 | 0.50 | 0.65 | 0.57 | 0.93 | 1.12 | 0.99 | 1.17 | 0.94 | |
| Max | 4.2 | 4.6 | 4.4 | 4.4 | 4.7 | 4.3 | 4.4 | 6.1 | 5.7 | 5.9 | 5.4 | 5.5 | 6.1 |
| 1987 Mean | 2.28 | 2.78 | 3.63 | 3.47 | 4.10 | 3.69 | 4.02 | 4.99 | 5.37 | 5.10 | 4.65 | 3.39 | 3.96 |
| σ | 0.93 | 1.09 | 1.07 | 0.91 | 0.94 | 0.74 | 0.59 | 0.62 | 0.79 | 0.81 | 0.78 | 0.15 | |
| Max | 4.2 | 4.7 | 4.7 | 5.9 | 5.7 | 5.5 | 4.9 | 7.2 | 6.6 | 6.7 | 6.1 | 7.2 | |
| 1988 Mean | 3.45 | 4.27 | 3.75 | 4.34 | 3.77 | 3.40 | 3.96 | 4.12 | 4.89 | 4.49 | 3.87 | 3.36 | 3.97 |
| σ | 1.20 | 1.95 | 1.03 | 1.46 | 1.01 | 0.98 | 0.53 | 1.04 | 0.71 | 1.21 | 1.02 | 1.19 | |
| Max | 6.2 | 7.9 | 5.9 | 7.4 | 6.3 | 4.7 | 5.0 | 6.3 | 6.6 | 6.2 | 6.2 | 5.2 | 7.4 |
| 1989 Mean | 3.56 | 2.56 | 3.89 | 4.17 | 3.47 | 3.58 | 3.89 | 4.39 | 4.29 | 4.36 | 4.13 | 3.28 | 3.8 |
| σ | 1.25 | 1.03 | 1.35 | 1.17 | 0.84 | 0.85 | 0.88 | 0.80 | 0.81 | 1.18 | 1.24 | 1.28 | |
| Max | 5.5 | 4.6 | 7.3 | 6.8 | 5.2 | 6.5 | 6.8 | 5.9 | 6.1 | 6.4 | 6.3 | 5.8 | 7.3 |
| No. | 13 | 13 | 13 | 13 | 13 | 13 | 13 | 13 | 13 | 13 | 13 | 13 | |
| Mean | 2.51 | 2.93 | 3.09 | 3.23 | 3.17 | 2.98 | 3.24 | 3.61 | 3.86 | 3.90 | 3.53 | 3.12 | 3.26 |
| Std. Dev. | 0.59 | 0.54 | 0.55 | 0.54 | 0.45 | 0.45 | 0.46 | 0.65 | 0.73 | 0.53 | 0.60 | 0.50 | |

Table C1-8 Monthly Mean of Sunshine Percentage between 8:00 and 16:00 at
the Climatological Station of Dramaga Bogor (CSDB)

| YEAR | Latitude : 06°30'S Longitude : 106°45'E Altitude : 250m. | | | | | | | | | | | Average | |
|------|--|------|------|------|-----|------|------|------|------|------|------|---------|----|
| | Jan. | Feb. | Mar. | Apr. | May | Jun. | Jul. | Aug. | Sep. | Oct. | Nov. | Dec. | |
| 1971 | 29 | 23 | 33 | 76 | 73 | 72 | 81 | 90 | 73 | 43 | 38 | 40 | 56 |
| 1972 | 26 | 45 | 38 | 77 | 70 | 89 | 91 | - | 88 | 83 | - | - | 67 |
| 1973 | 29 | 48 | 39 | 64 | 61 | 67 | 73 | 80 | 60 | 63 | 48 | 37 | 56 |
| 1974 | 19 | 35 | 52 | 71 | 71 | 77 | 78 | 71 | 70 | 57 | 37 | 43 | 57 |
| 1975 | 47 | 30 | 41 | 62 | 75 | 77 | 76 | 83 | 67 | 50 | 57 | 34 | 58 |
| 1976 | 12 | 53 | 38 | 61 | 79 | 85 | 92 | 88 | 79 | 67 | 51 | 51 | 63 |
| 1977 | 34 | 18 | 39 | 68 | 81 | 60 | 87 | 89 | 81 | 83 | 66 | 48 | 63 |
| 1978 | 35 | 47 | 50 | 69 | 62 | 52 | 65 | 72 | 65 | 65 | 63 | 37 | 57 |
| 1979 | 30 | 42 | 38 | 60 | 63 | 70 | 79 | 83 | 72 | 75 | 51 | 43 | 59 |
| 1980 | 18 | 37 | 61 | 62 | 78 | 86 | 80 | 77 | 69 | 58 | 57 | 25 | 59 |
| 1981 | 15 | 42 | 65 | 70 | 69 | 74 | 67 | 76 | 62 | 66 | 36 | 37 | 57 |
| 1982 | 20 | 44 | 52 | 61 | 78 | 70 | 87 | 91 | 88 | 93 | 78 | 48 | 68 |
| 1983 | 42 | 56 | 57 | 62 | 61 | 86 | 89 | 87 | 85 | 63 | 42 | 55 | 65 |
| 1984 | 27 | 31 | 49 | 62 | 63 | 83 | 75 | 77 | 44 | 32 | 58 | 32 | 54 |
| 1985 | 50 | 48 | 56 | 51 | 70 | 67 | 69 | 87 | 80 | 62 | 60 | 52 | 63 |
| 1986 | 18 | 46 | 43 | 63 | 78 | 73 | 79 | 65 | 50 | 65 | 63 | 55 | 58 |
| 1987 | 19 | 34 | 67 | 67 | 80 | 71 | 90 | 79 | 80 | 61 | 28 | 64 | - |
| 1988 | 41 | 48 | 41 | 68 | 64 | 71 | 76 | 72 | 82 | 54 | 44 | 40 | 58 |
| 1989 | 47 | 18 | 53 | 67 | 65 | 66 | 76 | 77 | 77 | 59 | 55 | 55 | 60 |
| Mean | 29 | 39 | 48 | 65 | 71 | 73 | 79 | 81 | 72 | 65 | 53 | 40 | - |

Table C1-9 Monthly Mean of Radiation Intensity (Kcal/cm²/day) at
the Climatological Station of Dramaga Bogor (CSDB)

Latitude : 06°30'S Longitude : 106°45'E Altitude : 250m.

| YEAR | Jan. | Feb. | Mar. | Apr. | May | Jun. | Jul. | Aug. | Sep. | Oct. | Nov. | Dec. | Average | σ |
|----------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|---------|----------|
| 1977 | 199.1 | 174.6 | 199.6 | 276.6 | - | - | 295.2 | 319.4 | 294.3 | 299.8 | - | - | 257.3 | 52.9 |
| 1978 | 237.3 | 269.4 | 264.5 | 292.2 | 272.7 | 227.2 | 275.9 | 262.7 | 268.9 | 271.1 | 258.4 | 218.3 | 259.9 | 20.6 |
| 1979 | 225.7 | 269.2 | 247.4 | 244.7 | 258.4 | 264.7 | 278.6 | 292.6 | 264.6 | 271.9 | 245.5 | 204.9 | 255.7 | 22.9 |
| 1980 | 189.5 | 226.3 | 274.1 | 237.4 | 234.3 | 245.7 | 230.5 | 225.5 | 161.6 | 173.0 | 182.5 | 134.1 | 209.5 | 39.0 |
| 1981 | 102.3 | 168.3 | 179.5 | 196.6 | 188.7 | 199.5 | 192.4 | 206.7 | 203.1 | 220.2 | 190.8 | 173.2 | 185.1 | 28.5 |
| 1982 | 110.5 | 192.1 | 216.5 | 227.2 | 231.6 | 210.7 | 234.1 | 245.2 | 246.9 | 228.1 | 178.8 | 151.8 | 206.1 | 39.5 |
| 1983 | 139.3 | 155.9 | 147.3 | 162.3 | 134.4 | 194.3 | 195.5 | 233.0 | 231.6 | 188.8 | 150.5 | 166.3 | 174.9 | 32.2 |
| 1984 | 118.8 | 133.5 | 137.8 | 142.5 | 138.2 | 168.3 | 153.4 | 169.6 | 148.0 | 169.1 | 132.4 | 251.4 | 155.3 | 32.9 |
| 1985 | 299.4 | 304.3 | 309.1 | 323.8 | 294.0 | 283.0 | 286.9 | 351.1 | 347.9 | 333.5 | 277.7 | 289.6 | 308.4 | 24.1 |
| 1986 | 202.9 | 258.5 | 264.0 | 274.3 | 309.1 | 289.1 | 294.9 | 287.1 | 285.5 | 296.8 | 238.7 | 271.2 | 272.7 | 27.9 |
| 1987 | 200.2 | 256.7 | 289.8 | 244.8 | 290.4 | 273.6 | 311.6 | 340.9 | 286.0 | 269.4 | 302.5 | 206.5 | 272.7 | 39.3 |
| 1988 | 268.6 | 249.2 | 247.8 | 308.1 | 300.7 | 296.2 | 300.0 | 281.9 | 361.4 | 322.0 | 268.7 | 259.2 | 288.7 | 31.7 |
| 1989 | 276.2 | 218.1 | 310.6 | - | 295.4 | - | 396.7 | 298.3 | 313.6 | 324.9 | 280.0 | 263.7 | 297.8 | 43.9 |
| n | 13 | 13 | 13 | 12 | 12 | 11 | 13 | 13 | 13 | 13 | 12 | 12 | | |
| Mean | 197.7 | 221.2 | 237.5 | 244.2 | 245.7 | 241.1 | 265.1 | 270.3 | 262.6 | 259.1 | 225.5 | 215.9 | | |
| σ | 62.2 | 50.2 | 55.1 | 53.5 | 59.3 | 41.6 | 60.8 | 51.1 | 64.4 | 55.6 | 53.8 | 49.3 | | |
| Max. | 299.4 | 304.3 | 310.6 | 323.8 | 309.1 | 296.2 | 396.7 | 351.1 | 361.4 | 333.5 | 302.5 | 289.6 | | |

Table C1-10 Monthly Total Rainfall At The Climatological Station of Darmaga Bogor(CSDB)

| YEAR | Rainfall in millimeter (mm) | | | | | | | | | | | Annual | Jun. to Nov. |
|----------|-----------------------------|------|------|------|-----|------|------|------|------|------|------|--------|--------------|
| | Jan. | Feb. | Mar. | Apr. | May | Jun. | Jul. | Aug. | Sep. | Oct. | Nov. | | |
| 1964 | 457 | 305 | 321 | 417 | 202 | 143 | 86 | 257 | 348 | 286 | 208 | 343 | 3,373 |
| 1965 | 620 | 420 | 139 | 421 | 224 | 302 | 195 | 158 | 109 | 214 | 266 | 337 | 3,405 |
| 1966 | 211 | 301 | 270 | 389 | 118 | 61 | 80 | 39 | 37 | 353 | 135 | 181 | 2,175 |
| 1967 | 231 | 403 | 452 | 520 | 309 | 34 | 174 | 68 | 191 | 247 | 361 | 305 | 3,295 |
| 1968 | 259 | 272 | 482 | 214 | 103 | 295 | 225 | 183 | 449 | 263 | 255 | 245 | 3,245 |
| 1969 | 397 | 285 | 440 | 618 | 334 | 166 | 218 | 87 | 341 | 284 | 467 | 97 | 3,734 |
| 1970 | 328 | 445 | 303 | 343 | 281 | 185 | 238 | 279 | 376 | 159 | 272 | 187 | 3,396 |
| 1971 | 320 | 517 | 414 | 360 | 312 | 293 | 270 | 439 | 290 | 344 | 238 | 206 | 4,003 |
| 1972 | 527 | 293 | 344 | 272 | 330 | 48 | 69 | 129 | 20 | 172 | 392 | 313 | 2,909 |
| 1973 | 514 | 479 | 438 | 744 | 539 | 288 | 96 | 398 | 497 | 386 | 289 | 380 | 5,048 |
| 1974 | 402 | 306 | 413 | 336 | 337 | 250 | 368 | 327 | 552 | 493 | 169 | 257 | 4,210 |
| 1975 | 243 | 376 | 227 | 361 | 532 | 325 | 248 | 466 | 583 | 163 | 458 | 270 | 4,252 |
| 1976 | 781 | 181 | 242 | 202 | 345 | 113 | 73 | 244 | 160 | 241 | 382 | 305 | 3,269 |
| 1977 | 602 | 467 | 545 | 532 | 365 | 352 | 84 | 135 | 248 | 228 | 495 | 285 | 4,338 |
| 1978 | 384 | 229 | 628 | 332 | 303 | 320 | 309 | 414 | 412 | 553 | 474 | 313 | 4,671 |
| 1979 | 541 | 293 | 334 | 354 | 227 | 223 | 261 | 161 | 384 | 438 | 373 | 327 | 3,916 |
| 1980 | 386 | 368 | 308 | 476 | 338 | 272 | 223 | 226 | 348 | 413 | 518 | 454 | 4,330 |
| 1981 | 476 | 240 | 421 | 335 | 263 | 383 | 551 | 194 | 366 | 246 | 157 | 436 | 4,068 |
| 1982 | 477 | 240 | 214 | 580 | 396 | 164 | 247 | 71 | 90 | 241 | 501 | 430 | 3,651 |
| 1983 | 328 | 241 | 256 | 296 | 224 | 140 | 263 | 93 | 178 | 654 | 300 | 253 | 3,226 |
| 1984 | 382 | 235 | 551 | 508 | 420 | 190 | 259 | 455 | 317 | 328 | 252 | 185 | 4,082 |
| 1985 | 375 | 354 | 231 | 337 | 321 | 156 | 514 | 285 | 298 | 241 | 279 | 273 | 3,664 |
| 1986 | 311 | 436 | 526 | 233 | 241 | 281 | 232 | 264 | 387 | 252 | 543 | 528 | 4,234 |
| 1987 | 295 | 282 | 404 | 290 | 460 | 218 | 235 | 103 | 50 | 413 | 436 | 231 | 3,417 |
| 1988 | 434 | 380 | 344 | 445 | 371 | 148 | 89 | 200 | 80 | 240 | 151 | 307 | 3,189 |
| 1989 | 464 | 507 | 281 | 150 | 554 | 333 | 147 | 230 | 255 | 367 | 346 | 444 | 4,078 |
| Mean | 413 | 341 | 366 | 387 | 325 | 219 | 221 | 227 | 283 | 316 | 335 | 304 | 3,738 |
| σ | 131 | 93 | 119 | 135 | 112 | 96 | 120 | 125 | 156 | 120 | 122 | 97 | 598 |
| Max. | 781 | 517 | 628 | 744 | 554 | 383 | 551 | 455 | 497 | 654 | 543 | 528 | 5,048 |
| Min. | 211 | 181 | 139 | 150 | 103 | 61 | 69 | 39 | 20 | 159 | 135 | 97 | 2,175 |

Table C1-11 Number of Rainy Days at the CSDB

| YEAR | The number of rainy days | | | | | | | | | | | TOTAL | |
|----------|--------------------------|------|------|------|------|------|------|------|------|------|------|-------|-------|
| | Jan. | Feb. | Mar. | Apr. | May | Jun. | Jul. | Aug. | Sep. | Oct. | Nov. | Dec. | |
| 1964 | 19 | 20 | 21 | 24 | 18 | 12 | 20 | 17 | 17 | 20 | 21 | 22 | 221 |
| 1965 | 30 | 26 | 20 | 18 | 16 | 19 | 10 | 6 | 9 | 9 | 17 | 24 | 204 |
| 1966 | 21 | 25 | 23 | 18 | 18 | 9 | 7 | 9 | 12 | 26 | 22 | 22 | 212 |
| 1967 | 23 | 24 | 22 | 24 | 12 | 3 | 11 | 5 | 8 | 16 | 24 | 25 | 197 |
| 1968 | 25 | 22 | 23 | 24 | 17 | 19 | 16 | 16 | 21 | 23 | 19 | 19 | 244 |
| 1969 | 17 | 21 | 17 | 28 | 11 | 12 | 11 | 7 | 19 | 12 | 22 | 14 | 191 |
| 1970 | 26 | 23 | 25 | 18 | 20 | 17 | 9 | 10 | 16 | 12 | 24 | 21 | 221 |
| 1971 | 18 | 23 | 23 | 8 | 18 | 19 | 12 | 11 | 14 | 23 | 18 | 17 | 214 |
| 1972 | 24 | 21 | 29 | 18 | 21 | 3 | 3 | 11 | 2 | 10 | 25 | 25 | 192 |
| 1973 | 26 | 25 | 28 | 22 | 25 | 15 | 14 | 20 | 17 | 18 | 17 | 23 | 250 |
| 1974 | 25 | 24 | 22 | 22 | 19 | 15 | 13 | 22 | 19 | 25 | 17 | 22 | 245 |
| 1975 | 26 | 25 | 27 | 26 | 24 | 9 | 16 | 19 | 23 | 22 | 20 | 20 | 257 |
| 1976 | 30 | 20 | 24 | 20 | 13 | 9 | 6 | 12 | 11 | 21 | 23 | 22 | 181 |
| 1977 | 29 | 25 | 29 | 23 | 23 | 18 | 9 | 11 | 12 | 9 | 23 | 24 | 235 |
| 1978 | 26 | 22 | 26 | 19 | 21 | 20 | 15 | 22 | 20 | 22 | 17 | 22 | 252 |
| 1979 | 20 | 20 | 24 | 20 | 22 | 11 | 7 | 16 | 16 | 18 | 26 | 21 | 221 |
| 1980 | 28 | 21 | 23 | 21 | 14 | 12 | 16 | 14 | 22 | 23 | 28 | 25 | 247 |
| 1981 | 29 | 21 | 25 | 22 | 20 | 16 | 19 | 20 | 19 | 18 | 21 | 20 | 259 |
| 1982 | 29 | 21 | 22 | 23 | 18 | 16 | 12 | 5 | 10 | 13 | 21 | 24 | 214 |
| 1983 | 21 | 22 | 18 | 20 | 22 | 11 | 12 | 7 | 14 | 24 | 21 | 216 | |
| 1984 | 26 | 26 | 24 | 25 | 22 | 12 | 17 | 19 | 24 | 23 | 23 | 22 | 263 |
| 1985 | 25 | 24 | 24 | 23 | 22 | 21 | 16 | 14 | 19 | 17 | 18 | 15 | 238 |
| 1986 | 30 | 24 | 26 | 21 | 13 | 17 | 14 | 14 | 24 | 23 | 26 | 26 | 258 |
| 1987 | 31 | 26 | 24 | 19 | 22 | 16 | 12 | 4 | 9 | 16 | 21 | 23 | 223 |
| 1988 | 28 | 24 | 25 | 15 | 24 | 14 | 4 | 14 | 15 | 19 | 20 | 19 | 221 |
| 1989 | 25 | 24 | 19 | 16 | 24 | 14 | 14 | 9 | 11 | 19 | 16 | 25 | 216 |
| Mean | 25.3 | 23.0 | 23.6 | 20.7 | 19.2 | 13.8 | 11.8 | 13.0 | 15.5 | 18.4 | 21.2 | 21.6 | 226.6 |
| σ | 3.9 | 2.0 | 3.0 | 4.0 | 4.0 | 4.6 | 4.0 | 5.5 | 5.4 | 5.0 | 3.2 | 3.0 | 22.8 |
| Max | 31 | 26 | 29 | 25 | 21 | 17 | 22 | 24 | 26 | 26 | 26 | 26 | 259 |
| Min | 17 | 20 | 17 | 8 | 11 | 3 | 6 | 4 | 2 | 9 | 17 | 14 | 181 |

Table C1-12 The Highest 24 hours Rainfall in the Month at the CSDB

(unit : mm)

| YEAR | Jan. | Feb. | Mar. | Apr. | May | Jun. | Jul. | Aug. | Sep. | Oct. | Nov. | Dec. |
|------|------|------|------|------|-----|------|------|------|------|------|------|------|
| 1964 | 100 | 92 | 49 | 71 | 42 | 44 | 19 | 44 | 87 | 50 | 41 | 49 |
| 1965 | 80 | 58 | 32 | 70 | 105 | 43 | 47 | 75 | 70 | 62 | 51 | 112 |
| 1966 | 63 | 81 | 40 | 99 | 39 | 37 | 26 | 26 | 15 | 46 | 27 | 23 |
| 1967 | 29 | 51 | 59 | 80 | 91 | 33 | 60 | 6 | 74 | 65 | 94 | 52 |
| 1968 | 78 | 52 | 103 | 59 | 21 | 47 | 54 | 101 | 77 | 85 | 58 | 37 |
| 1969 | 66 | 18 | 71 | 98 | 99 | 87 | 70 | 38 | 91 | 57 | 77 | 25 |
| 1970 | 52 | 59 | 39 | 59 | 55 | 57 | 58 | 117 | 116 | 33 | 38 | 30 |
| 1971 | 92 | 98 | 86 | 98 | 98 | 61 | 103 | 132 | 89 | 68 | 39 | 35 |
| 1972 | 85 | 88 | 57 | 70 | 59 | 28 | 11 | 22 | 20 | 72 | 17 | 44 |
| 1973 | 113 | 69 | 51 | 104 | 70 | 63 | 54 | 71 | 96 | 64 | 79 | 87 |
| 1974 | 68 | 41 | 85 | 71 | 69 | 59 | 148 | 81 | 61 | 80 | 25 | 38 |
| 1975 | 36 | 54 | 33 | 88 | 78 | 177 | 44 | 84 | 86 | 30 | 67 | 48 |
| 1976 | 84 | 43 | 50 | 36 | 181 | 72 | 41 | 96 | 29 | 35 | 63 | 58 |
| 1977 | 80 | 77 | 60 | 84 | 60 | 80 | 28 | 36 | 69 | 74 | 49 | 80 |
| 1978 | 47 | 41 | 80 | 70 | 27 | 69 | 149 | 53 | 108 | 109 | 65 | 53 |
| 1979 | 106 | 63 | 79 | 71 | 60 | 110 | 137 | 26 | 119 | 77 | 82 | 40 |
| 1980 | 41 | 115 | 50 | 66 | 70 | 76 | 61 | 45 | 119 | 129 | 77 | 144 |
| 1981 | 52 | 58 | 111 | 70 | 44 | 83 | 146 | 72 | 57 | 47 | 31 | 128 |
| 1982 | 56 | 68 | 55 | 97 | 89 | 78 | 82 | 31 | 48 | 63 | 85 | 111 |
| 1983 | 74 | 43 | 69 | 82 | 44 | 57 | 81 | 34 | 55 | 90 | 64 | 56 |
| 1984 | 73 | 32 | 106 | 93 | 79 | 88 | 57 | 114 | 88 | 83 | 59 | 33 |
| 1985 | 73 | 105 | 64 | 74 | 63 | 36 | 103 | 88 | 59 | 84 | 76 | 60 |
| 1986 | 40 | 105 | 104 | 53 | 72 | 110 | 105 | 71 | 87 | 48 | 80 | 82 |
| 1987 | 42 | 33 | 66 | 76 | 88 | 63 | 69 | 50 | 11 | 81 | 83 | 31 |
| 1988 | 89 | 67 | 61 | 83 | 77 | 64 | 73 | 63 | 17 | 53 | 34 | 59 |
| 1989 | 75 | 240 | 54 | 41 | 122 | 92 | 51 | 64 | 70 | 83 | 50 | 104 |

Table C1-13

Probability Calculation of the Highest Daily Rainfall Data at the CSDB
by Gumble Method (Data period 26 years 1964-1989)

- (1) January
- (2) February
- (3) March
- (4) April
- (5) May
- (6) June
- (7) July
- (8) August
- (9) September
- (10) October
- (11) November
- (12) December
- (13) Annual Maximum

(1) Probability Calculation of Maximum Daily Rainfall in January at the Climatological Station of Darmaga Bogor (CSDB). by Gumble Method (Data period : 1964 - 1989)

GUMBLE MAX. DISTRIBUTION

DATA N=26.

| | | |
|--------|-------|---|
| D(1)= | 100.0 | CALCULATION |
| D(2)= | 80.0 | SUM X= 1794. |
| D(3)= | 63.0 | SUM X^2= 136198. |
| D(4)= | 29.0 | SUM X^3= 11118768. |
| D(5)= | 78.0 | MEAN X= 69. |
| D(6)= | 66.0 | MEAN X^2= 5258.384615 |
| D(7)= | 52.0 | MEAN X^3= 427644.9231 |
| D(8)= | 92.0 | SUM DEV SQU. S=12412. |
| D(9)= | 85.0 | VARIANCE S/N=477.38 |
| D(10)= | 113.0 | UNBIASED VARI. =S/(N-1)= |
| D(11)= | 62.0 | 496.48 |
| D(12)= | 36.0 | VARIATION COEF.=SX/MEAN |
| D(13)= | 84.0 | X=0.32 |
| D(14)= | 80.0 | STANDARD DEV. SX=√(S/N)= |
| D(15)= | 47.0 | 21.85 |
| D(16)= | 106.0 | STA. DEV. EST. USX=√(S/(N-1))=22.28 |
| D(17)= | 41.0 | SKEWNESS COEF. CS1=0.03 |
| D(18)= | 52.0 | UNBIASED S.C. CS1=0.03 |
| D(19)= | 56.0 | PROBABLE EXTREAM VALUE(XT), RETURN PERIOD(T), |
| D(20)= | 74.0 | FREQUENCY FUNCTION: |
| D(21)= | 73.0 | XT=XM+K*SX, K=(YT-YM)/SY |
| D(22)= | 73.0 | , XM=MEAN X, YT=-LN(LN(T)/(T-1)) |
| D(23)= | 40.0 | SO THAT XT=XM-(YM*SX/SY)+ (SX/SY)*YT |
| D(24)= | 42.0 | CAL. VALUE: |
| D(25)= | 89.0 | XM=69. SX=22.28 YM=0.5 |
| D(26)= | 75.0 | T=50. |

RANKING

| | | |
|-------------|--|---------------------|
| I=1. X=113. | ESTIMATE EQUATION: | C.L.=95% LMT=+-38.7 |
| I=2. X=106. | XT=58.18+20.33YT | C.L.=90% LMT=+-32.5 |
| I=3. X=100. | T=200. | C.L.=80% LMT=+-25.3 |
| I=4. X=92. | T=100. | C.L.=68% LMT=+-19.7 |
| I=5. X=89. | XT=65.6 | T=200. |
| I=6. X=85. | T=4. XT=83.5 | C.L.=95% LMT=+-57.3 |
| I=7. X=84. | T=5. XT=88.7 | C.L.=90% LMT=+-48.1 |
| I=8. X=80. | T=10. XT=103.9 | C.L.=80% LMT=+-37.5 |
| I=9. X=80. | T=20. XT=118.6 | C.L.=68% LMT=+-29.3 |
| I=10. X=78. | T=25. XT=123.2 | |
| I=11. X=75. | T=50. XT=137.5 | |
| I=12. X=74. | T=100. XT=151.7 | |
| I=13. X=73. | T=200. XT=165.9 | |
| I=14. X=73. | T=1000. XT=198.5 | |
| I=15. X=68. | NOTE 1. XT : Magnitude of the event reached or exceeded on an average once in T years | |
| I=16. X=66. | 2. T : Return period | |
| I=17. X=63. | 3. C. L. : Confidence level | |
| I=18. X=56. | 4. LMT : Conficence limit | |
| I=19. X=52. | | |
| I=20. X=52. | | |
| I=21. X=47. | | |
| I=22. X=42. | | |
| I=23. X=41. | | |
| I=24. X=40. | | |
| I=25. X=36. | | |
| I=26. X=29. | | |

(2) Probability Calculation of Maximum Daily Rainfall in February at the Climatological Station of Darmaga Bogor (CSDB).by Gumble Method (Data period : 1964 - 1989)

GUMBLE MAX. DISTRIBUTION

| DATA N=26. | CALCULATION | CONFIDENCE INTERVAL |
|--------------|---|----------------------|
| D(1)= 92.0 | SUM X= 1851. | T=5. |
| D(2)= 58.3 | SUM X^2= 176947. | C.L.=95% LMT=+-27.7 |
| D(3)= 81.0 | SUM X^3= 23640921. | C.L.=90% LMT=+-23.2 |
| D(4)= 51.0 | MEAN X= 71.19230769 | C.L.=80% LMT=+-18.1 |
| D(5)= 52.0 | MEAN X^2= 6805.653846 | C.L.=68% LMT=+-14.1 |
| D(6)= 18.0 | MEAN X^3= 909266.1923 | T=10. |
| D(7)= 59.0 | SUM DEV SQU. S=45170.038 | C.L.=95% LMT=+-38.3 |
| D(8)= 98.0 | 46 | C.L.=90% LMT=+-32.1 |
| D(9)= 88.0 | VARIANCE S^2/N=1737.31 | C.L.=80% LMT=+-25. |
| D(10)= 69.0 | UNBIASED VARI. =S/(N-1)= | C.L.=68% LMT=+-19.5 |
| D(11)= 41.0 | 1806.8 | T=20. |
| D(12)= 54.0 | VARIATION COEF.=SX/MEAN | C.L.=95% LMT=+-49. |
| D(13)= 45.0 | X=0.59 | C.L.=90% LMT=+-41.1 |
| D(14)= 77.0 | STANDARD DEV. SX=SQRT(S/N)= | C.L.=80% LMT=+-32. |
| D(15)= 41.0 | 41.68 | C.L.=68% LMT=+-25. |
| D(16)= 63.0 | STA. DEV. EST. USX=SQRT(S/(N-1))=42.51 | T=25. |
| D(17)= 115.0 | SKEWNESS COEF. CS1=2.45 | C.L.=95% LMT=+-52.4 |
| D(18)= 58.0 | UNBIASED S.C. CS1=2.402 | C.L.=90% LMT=+-44. |
| D(19)= 68.0 | PROBABLE EXTREME VALUE(XT), RETURN PERIOD(T), | C.L.=80% LMT=+-34.3 |
| D(20)= 43.0 | FREQUENCY FUNCTION: | C.L.=68% LMT=+-26.7 |
| D(21)= 32.0 | XT=XM+K*SX, K=(YT-YM)/SY | T=50. |
| D(22)= 105.0 | , XM=MEAN X, YT=-LN(LN(T/(T-1))) | C.L.=95% LMT=+-63.1 |
| D(23)= 105.0 | SO THAT XT=XM-(YM*SX/SY)+(SX/SY)*YT | C.L.=90% LMT=+-52.9 |
| D(24)= 33.0 | CAL. VALUE: | C.L.=80% LMT=+-41.3 |
| D(25)= 67.0 | XM=71.19230769 SX=42.51 | C.L.=68% LMT=+-32.2 |
| D(26)= 240.0 | YM=0.5321 SY=1.0961 | T=100. |
| RANKING | ESTIMATE EQUATION: | C.L.=95% LMT=+-73.8 |
| I=1. X=240. | XT=50.56+38.78YT | C.L.=90% LMT=+-61.9 |
| I=2. X=115. | T=200. | C.L.=80% LMT=+-48.3 |
| I=3. X=105. | C.L.=68% LMT=+-37.6 | |
| I=4. X=105. | T=200. | C.L.=95% LMT=+-84.5 |
| I=5. X=98. | C.L.=90% LMT=+-70.9 | |
| I=6. X=92. | C.L.=80% LMT=+-55.3 | |
| I=7. X=88. | C.L.=68% LMT=+-43.1 | |
| I=8. X=81. | T=1000. | C.L.=95% LMT=+-109.4 |
| I=9. X=77. | C.L.=90% LMT=+-91.8 | |
| I=10. X=69. | C.L.=80% LMT=+-71.6 | |
| I=11. X=68. | C.L.=68% LMT=+-55.8 | |
| I=12. X=67. | T=2. XT=64.8 | |
| I=13. X=63. | T=4. XT=98.9 | |
| I=14. X=59. | T=5. XT=108.7 | |
| I=15. X=58. | T=10. XT=137.8 | |
| I=16. X=58. | T=20. XT=165.7 | |
| I=17. X=54. | T=25. XT=174.6 | |
| I=18. X=52. | T=50. XT=211.9 | |
| I=19. X=51. | T=100. XT=229. | |
| I=20. X=43. | T=200. XT=255.9 | |
| I=21. X=43. | T=1000. XT=318.4 | |
| I=22. X=41. | NOTE 1. XT : Magnitude of the event reached or exceeded on an average once in T years | |
| I=23. X=41. | 2. T : Return period | |
| I=24. X=33. | 3. C. L. : Confidence level | |
| I=25. X=32. | 4. LMT : Confidence limit | |
| I=26. X=16. | | |

(3) Probability Calculation of Maximum Daily Rainfall in March at the Climatological Station of Darmaga Bogor (CSDB), by Gumble Method (Data period : 1964 - 1989)

GUMBLE

| DATA N= | 26.0 | CALCULATION | CONFIDENCE INTERVAL |
|---------|--------|--|---------------------|
| D(1)= | 49.0 | SUM X= 1714. | T=5. |
| D(2)= | 32.0 | SUM X^2= 125726. | C.L.=95% LMT=+-14.7 |
| D(3)= | 40.0 | SUM X^3= 10117234. | C.L.=90% LMT=+-12.3 |
| D(4)= | 59.0 | MEAN X= 65.92307692 | C.L.=80% LMT=+-9.6 |
| D(5)= | 103.0 | MEAN X^2= 4835.615385 | C.L.=68% LMT=+-7.5 |
| D(6)= | 71.0 | MEAN X^3= 389124.3846 | T=10. |
| D(7)= | 39.0 | SUM DEV SQU. S=12733.846 | C.L.=95% LMT=+-20.3 |
| D(8)= | 86.0 | 15 | C.L.=90% LMT=+-17.1 |
| D(9)= | 57.0 | VARIANCE S/N=489.76 | C.L.=80% LMT=+-13.3 |
| D(10)= | 51.0 | UNBIASED VARI. =S/(N-1)= | C.L.=68% LMT=+-10.4 |
| D(11)= | 85.0 | 509.35 | T=20. |
| D(12)= | 33.0 | VARIATION COEF.=SX/MEAN | C.L.=95% LMT=+-26. |
| D(13)= | 50.0 | X=0.34 | C.L.=90% LMT=+-21.8 |
| D(14)= | 60.0 | STANDARD DEV. SX=f(S/N)= | C.L.=80% LMT=+-17. |
| D(15)= | 80.0 | 22.13 | C.L.=68% LMT=+-13.3 |
| D(16)= | 79.0 | STA. DEV. EST. USX=f(S/(N-1))=22.57 | T=25. |
| D(17)= | 50.0 | SKEWNESS COEF. CS!=0.533 | C.L.=95% LMT=+-27.8 |
| D(18)= | 111.0 | UNBIASED S.C. CS1=0.522 | C.L.=90% LMT=+-23.3 |
| D(19)= | 55.0 | | C.L.=80% LMT=+-18.2 |
| D(20)= | 69.0 | | C.L.=68% LMT=+-14.2 |
| D(21)= | 106.0 | | T=50. |
| D(22)= | 64.0 | PROBABLE EXTREAM VALUE< XT>, RETURN PERIOD(T), | C.L.=95% LMT=+-33.5 |
| D(23)= | 104.0 | FREQUENCY FUNCTION: | C.L.=90% LMT=+-28.1 |
| D(24)= | 66.0 | | C.L.=80% LMT=+-21.9 |
| D(25)= | 61.0 | | C.L.=68% LMT=+-17.1 |
| D(26)= | 54.0 | XT=XM+K*SX, K=(YT-YM)/SY | T=100. |
| | | , XM=MEAN X, YT=-LN(LN(T)/(T-1))) | C.L.=95% LMT=+-39.2 |
| | | SO THAT XT=XM-(YM*SX/SY)+ (SX/SY)*YT | C.L.=90% LMT=+-32.9 |
| | | CAL. VALUE: | C.L.=80% LMT=+-25.6 |
| | | XM=65.92307692 SY=22.57 | C.L.=68% LMT=+-20. |
| | | YM=0.5321 SY=1.0961 | T=200. |
| | | ESTIMATE EQUATION: | C.L.=95% LMT=+-44.9 |
| | | XT=54.97+20.59YT | C.L.=90% LMT=+-37.6 |
| I=1. | X=111. | T=2. XT=62.5 | C.L.=80% LMT=+-29.3 |
| I=2. | X=106. | T=4. XT=80.6 | C.L.=68% LMT=+-22.9 |
| I=3. | X=104. | T=5. XT=85.9 | T=1000. |
| I=4. | X=103. | T=10. XT=101.3 | C.L.=95% LMT=+-58.1 |
| I=5. | X=86. | T=20. XT=116.1 | C.L.=90% LMT=+-48.8 |
| I=6. | X=85. | T=25. XT=120.8 | C.L.=80% LMT=+-38. |
| I=7. | X=80. | T=50. XT=135.3 | C.L.=68% LMT=+-29.6 |
| I=8. | X=79. | T=100. XT=149.7 | |
| I=9. | X=71. | T=200. XT=164. | |
| I=10. | X=69. | T=1000. XT=197.2 | |
| I=11. | X=66. | | |
| I=12. | X=64. | | |
| I=13. | X=61. | | |
| I=14. | X=60. | | |
| I=15. | X=59. | | |
| I=16. | X=57. | | |
| I=17. | X=55. | | |
| I=18. | X=54. | | |
| I=19. | X=51. | | |
| I=20. | X=50. | | |
| I=21. | X=50. | | |
| I=22. | X=49. | | |
| I=23. | X=40. | | |
| I=24. | X=39. | | |
| I=25. | X=33. | | |
| I=26. | X=32. | | |
| | | NOTE 1. XT : Magnitude of the event reached or exceeded on an average once in T years | |
| | | 2. T : Return period | |
| | | 3. C. L. : Confidence level | |
| | | 4. LMT : Confidence limit | |

(4) Probability Calculation of Maximum Daily Rainfall in April at the Climatological Station of Darmaga Bogor (CSDB) by Gumble Method (Data period: 1964 - 1989)

GUMBLE MAX. DISTRIBUTION

DATA N=26.

D(1)= 71.0
D(2)= 70.0
D(3)= 99.0
D(4)= 88.0
D(5)= 59.0
D(6)= 98.0
D(7)= 59.0
D(8)= 98.0
D(9)= 70.0
D(10)= 104.0
D(11)= 71.0
D(12)= 88.0
D(13)= 36.0
D(14)= 84.0
D(15)= 70.0
D(16)= 71.0
D(17)= 66.0
D(18)= 70.0
D(19)= 70.0
D(20)= 82.0
D(21)= 93.0
D(22)= 74.0
D(23)= 53.0
D(24)= 76.0
D(25)= 83.0
D(26)= 41.0

RANKING

I=1. X=104.
I=2. X=99.
I=3. X=98.
I=4. X=98.
I=5. X=93.
I=6. X=88.
I=7. X=84.
I=8. X=83.
I=9. X=82.
I=10. X=80.
I=11. X=76.
I=12. X=74.
I=13. X=71.
I=14. X=71.
I=15. X=71.
I=16. X=70.
I=17. X=70.
I=18. X=70.
I=19. X=70.
I=20. X=70.
I=21. X=66.
I=22. X=59.
I=23. X=59.
I=24. X=53.
I=25. X=41.
I=26. X=36.

CALCULATION

SUM X= 1936.
SUM X²= 151266.
SUM X³= 12286876.
MEAN X= 74.46153846
MEAN X²= 5817.923077
MEAN X³= 472572.1538
SUM DEV SQU. S=7108.4615
39
VARIANCE S/N=273.4
UNBIASED VARI. =S/(N-1)=
284.34
VARIATION COEF.=SX/MEAN
X=0.22
STANDARD DEV. SX=f(S/N)=
16.53
STA. DEV. EST. USX=f(S/(
N-1))=16.86
SKEWNESS COEF. CS!= -0.3
UNBIASED S.C. CS1= -0.294

PROBABLE EXTREME VALUE(XT), RETURN PERIOD(T),
FREQUENCY FUNCTION:

XT=X_M+K*SX, K=(YT-YM)/SY
, XM=MEAN X, YT=-LN(LN(T
(T-1)))
SO THAT XT=X_M-(YM*SX/SY)
+(SX/SY)*YT
CAL. VALUE:
XM=74.46153846 SX=16.86
YM=0.5321 SY=1.0961

ESTIMATE EQUATION:
XT=66.28+15.39YT

T=2. XT=71.9
T=4. XT=85.4
T=5. XT=99.3
T=10. XT=100.9
T=20. XT=112.
T=25. XT=115.5
T=50. XT=126.3
T=100. XT=137.
T=200. XT=147.7
T=1000. XT=172.5

NOTE 1. XT : Magnitude of the event reached or exceeded
on an average once in T years
2. T : Return period
3. C. L. : Confidence level
4. LMT : Confidence limit

CONFIDENCE INTERVAL

| | |
|---------|---------------------|
| T=5. | C.L.=95% LMT=+-11. |
| | C.L.=90% LMT=+-9.2 |
| | C.L.=80% LMT=+-7.2 |
| | C.L.=68% LMT=+-5.6 |
| T=10. | C.L.=95% LMT=+-15.2 |
| | C.L.=90% LMT=+-12.7 |
| | C.L.=80% LMT=+-9.9 |
| | C.L.=68% LMT=+-7.7 |
| T=20. | C.L.=95% LMT=+-19.4 |
| | C.L.=90% LMT=+-16.3 |
| | C.L.=80% LMT=+-12.7 |
| | C.L.=68% LMT=+-9.9 |
| T=25. | C.L.=95% LMT=+-20.8 |
| | C.L.=90% LMT=+-17.4 |
| | C.L.=80% LMT=+-13.6 |
| | C.L.=68% LMT=+-10.6 |
| T=50. | C.L.=95% LMT=+-25. |
| | C.L.=90% LMT=+-21. |
| | C.L.=80% LMT=+-16.4 |
| | C.L.=68% LMT=+-12.8 |
| T=100. | C.L.=95% LMT=+-29.3 |
| | C.L.=90% LMT=+-24.6 |
| | C.L.=80% LMT=+-19.1 |
| | C.L.=68% LMT=+-14.9 |
| T=200. | C.L.=95% LMT=+-33.5 |
| | C.L.=90% LMT=+-28.1 |
| | C.L.=80% LMT=+-21.9 |
| | C.L.=68% LMT=+-17.1 |
| T=1000. | C.L.=95% LMT=+-43.4 |
| | C.L.=90% LMT=+-36.4 |
| | C.L.=80% LMT=+-28.4 |
| | C.L.=68% LMT=+-22.1 |

(5) Probability Calculation of Maximum Daily Rainfall in May at the Climatological Station of Darmaga Bogor (CSDB).by Gumble Method (Data period : 1964 - 1989)

GUMBLE MAX. DISTRIBUTION

| DATA N=26. | CALCULATION | CONFIDENCE INTERVAL |
|--------------|---|--------------------------------|
| D(1)= 42.0 | SUM X= 1902. | T=5. C.L.=95% LMT=+-21.3 |
| D(2)= 105.0 | SUM X^2= 166022. | C.L.=90% LMT=+-17.9 |
| D(3)= 39.0 | SUM X^3= 17153118. | C.L.=80% LMT=+-14. |
| D(4)= 91.0 | | C.L.=68% LMT=+-10.9 |
| D(5)= 21.0 | MEAN X= 73.15384615 | T=10. C.L.=95% LMT=+-29.5 |
| D(6)= 99.0 | MEAN X^2= 6385.461538 | C.L.=90% LMT=+-24.8 |
| D(7)= 55.0 | MEAN X^3= 659735.3077 | C.L.=80% LMT=+-19.3 |
| D(8)= 98.0 | SUM DEV SQU. S=26883.384 | C.L.=68% LMT=+-15.1 |
| D(9)= 59.0 | 62 | T=20. C.L.=95% LMT=+-37.8 |
| D(10)= 79.0 | VARIANCE S/N=1033.98 | C.L.=90% LMT=+-31.7 |
| D(11)= 69.0 | UNBIASED VARI. =S/(N-1)= | C.L.=80% LMT=+-24.7 |
| D(12)= 78.0 | 1075.34 | C.L.=68% LMT=+-19.3 |
| D(13)= 81.0 | VARIATION COEF.=SX/MEAN | T=25. C.L.=95% LMT=+-40.4 |
| D(14)= 60.0 | X=0.44 | C.L.=90% LMT=+-33.9 |
| D(15)= 27.0 | STANDARD DEV. SX=SQRT(S/N)= | C.L.=80% LMT=+-26.4 |
| D(16)= 60.0 | 32.16 | C.L.=68% LMT=+-20.6 |
| D(17)= 79.0 | STA. DEV. EST. USX=SQRT(S/(N-1))=32.79 | T=50. C.L.=95% LMT=+-48.7 |
| D(18)= 44.0 | SKEWNESS COEF. CS!=1.243 | C.L.=90% LMT=+-40.8 |
| D(19)= 89.0 | UNBIASED S.C. CS1=1.219 | C.L.=80% LMT=+-31.8 |
| D(20)= 44.0 | | C.L.=68% LMT=+-24.8 |
| D(21)= 79.0 | | T=100. C.L.=95% LMT=+-56.9 |
| D(22)= 63.0 | | C.L.=90% LMT=+-47.8 |
| D(23)= 72.0 | | C.L.=80% LMT=+-37.2 |
| D(24)= 88.0 | | C.L.=68% LMT=+-29. |
| D(25)= 77.0 | CONFIDENCE INTERVAL | T=200. C.L.=95% LMT=+-65.2 |
| D(26)= 122.0 | PROBABLE EXTREME VALUE(XT), RETURN PERIOD(T), FREQUENCY FUNCTION: | C.L.=90% LMT=+-54.7 |
| | XT=XM+K*SY, K=(YT-YM)/SY | C.L.=80% LMT=+-42.6 |
| RANKING | , XM=MEAN X, YT=-LN(LN(T)/(T-1))) | C.L.=68% LMT=+-33.2 |
| I=1. X=181. | SO THAT XT=XM-(YM*SY/SY) | T=1000. C.L.=95% LMT=+-84.4 |
| I=2. X=122. | +(SX/SY)*YT | C.L.=90% LMT=+-79.8 |
| I=3. X=105. | CAL. VALUE: | C.L.=80% LMT=+-55.2 |
| I=4. X=99. | XM=73.15384615 SY=32.79 | C.L.=68% LMT=+-43.1 |
| I=5. X=98. | YM=0.5321 SY=1.0961 | T=2. XT=68.2 |
| I=6. X=91. | ESTIMATE EQUATION: | T=4. XT=94.5 |
| I=7. X=89. | XT=57.24+29.92YT | T=5. XT=102.1 |
| I=8. X=88. | | T=10. XT=124.6 |
| I=9. X=79. | | T=20. XT=146.1 |
| I=10. X=78. | | T=25. XT=152.9 |
| I=11. X=77. | | T=50. XT=174. |
| I=12. X=72. | | T=100. XT=194.9 |
| I=13. X=70. | | T=200. XT=215.7 |
| I=14. X=70. | | T=1000. XT=263.9 |
| I=15. X=69. | | |
| I=16. X=65. | | |
| I=17. X=60. | | |
| I=18. X=60. | | |
| I=19. X=59. | | |
| I=20. X=55. | | |
| I=21. X=44. | | |
| I=22. X=44. | | |
| I=23. X=42. | | |
| I=24. X=39. | | |
| I=25. X=27. | NOTE 1. XT : Magnitude of the event reached or exceeded on an average once in T years | |
| I=26. X=21. | 2. T : Return period | |
| | 3. C. L. : Confidence Level | |
| | 4. LMT : Confidence Limit | |

(6) Probability Calculation of Maximum Daily Rainfall in June at the Climatological Station of Darmaga Bogor (CSDB). by Gumble Method (Data period : 1964 - 1989)

GUMBLE MAX. DISTRIBUTION

DATA N=26.

D(1)= 44.0
D(2)= 43.0
D(3)= 37.0
D(4)= 33.0
D(5)= 47.0
D(6)= 87.0
D(7)= 57.0
D(8)= 61.0
D(9)= 28.0
D(10)= 63.0
D(11)= 59.0
D(12)= 177.0
D(13)= 72.0
D(14)= 80.0
D(15)= 69.0
D(16)= 110.0
D(17)= 76.0
D(18)= 83.0
D(19)= 78.0
D(20)= 57.0
D(21)= 88.0
D(22)= 36.0
D(23)= 110.0
D(24)= 63.0
D(25)= 64.0
D(26)= 92.0

RANKING

I=1. X=177.
I=2. X=110.
I=3. X=110.
I=4. X=92.
I=5. X=88.
I=6. X=87.
I=7. X=83.
I=8. X=80.
I=9. X=78.
I=10. X=76.
I=11. X=72.
I=12. X=69.
I=13. X=64.
I=14. X=63.
I=15. X=63.
I=16. X=61.
I=17. X=59.
I=18. X=57.
I=19. X=57.
I=20. X=47.
I=21. X=44.
I=22. X=43.
I=23. X=37.
I=24. X=36.
I=25. X=33.
I=26. X=28.

CALCULATION

SUM X= 1814.
SUM X^2= 150666.
SUM X^3= 15013664.
MEAN X= 69.76923077
MEAN X^2= 5794.846154
MEAN X^3= 577448.6154
SUM DEV SQU. S=24104.615
39
VARIANCE S/N=927.1
UNBIASED VARI. =S/(N-1)=
964.18
VARIATION COEF.=SX/MEAN
X=0.44
STANDARD DEV. SX=J(S/N)=
30.45
STA. DEV. EST. USX=J(S/(
N-1))=31.05
SKEWNESS COEF. CS!=1.551
UNBIASED S.C. CS1=1.521
PROBABLE EXTREME VALUE(
XT), RETURN PERIOD(T),
FREQUENCY FUNCTION:

XT=XM+K*SX, K=(YT-YM)/SY
, XM=MEAN X, YT=-LN(LN(T
(T-1)))
SO THAT XT=XM-(YM*SX/SY)
+(SX/SY)*YT
CAL. VALUE:
XM=69.76923077 SX=31.05
YM=0.5321 SY=1.0961
ESTIMATE EQUATION:
XT=54.7+28.33YT
T=2. XT=65.1
T=4. XT=90.
T=5. XT=97.2
T=10. XT=118.5
T=20. XT=138.8
T=25. XT=145.3
T=50. XT=165.2
T=100. XT=185.
T=200. XT=204.7
T=1000. XT=250.4

NOTE

1. XT : Magnitude of the event reached or exceeded on an average once in T years
2. T : Return period
3. C. L. : Confidence level
4. LMT : Confidence limit

CONFIDENCE INTERVAL

| | |
|---------|---------------------|
| T=5. | C.L.=95% LMT=+-20.2 |
| | C.L.=90% LMT=+-17. |
| | C.L.=80% LMT=+-13.2 |
| | C.L.=68% LMT=+-10.3 |
| T=10. | C.L.=95% LMT=+-28. |
| | C.L.=90% LMT=+-23.5 |
| | C.L.=80% LMT=+-18.3 |
| | C.L.=68% LMT=+-14.3 |
| T=20. | C.L.=95% LMT=+-35.8 |
| | C.L.=90% LMT=+-30. |
| | C.L.=80% LMT=+-23.4 |
| | C.L.=68% LMT=+-18.2 |
| T=25. | C.L.=95% LMT=+-38.3 |
| | C.L.=90% LMT=+-32.1 |
| | C.L.=80% LMT=+-25. |
| | C.L.=68% LMT=+-19.5 |
| T=50. | C.L.=95% LMT=+-46.1 |
| | C.L.=90% LMT=+-38.7 |
| | C.L.=80% LMT=+-30.1 |
| | C.L.=68% LMT=+-23.5 |
| T=100. | C.L.=95% LMT=+-53.9 |
| | C.L.=90% LMT=+-45.2 |
| | C.L.=80% LMT=+-35.2 |
| | C.L.=68% LMT=+-27.5 |
| T=200. | C.L.=95% LMT=+-61.7 |
| | C.L.=90% LMT=+-51.8 |
| | C.L.=80% LMT=+-40.4 |
| | C.L.=68% LMT=+-31.5 |
| T=1000. | C.L.=95% LMT=+-79.9 |
| | C.L.=90% LMT=+-67.1 |
| | C.L.=80% LMT=+-52.3 |
| | C.L.=68% LMT=+-40.8 |

(7) Probability Calculation of Maximum Daily Rainfall in July at the Climatological Station of Darmaga Bogor (CSDB).by Gumble Method (Data period : 1964 - 1989)

GUMBLE MAX. DISTRIBUTION

DATA N=26.

D(1)= 19.2
D(2)= 47.0
D(3)= 26.0
D(4)= 60.0
D(5)= 54.0
D(6)= 70.0
D(7)= 58.0
D(8)= 103.0
D(9)= 11.0
D(10)= 54.0
D(11)= 148.0
D(12)= 44.0
D(13)= 41.0
D(14)= 28.0
D(15)= 149.0
D(16)= 137.0
D(17)= 61.0
D(18)= 146.0
D(19)= 82.0
D(20)= 81.0
D(21)= 57.0
D(22)= 103.0
D(23)= 105.0
D(24)= 69.0
D(25)= 73.0
D(26)= 51.0

RANKING

I=1. X=149.
I=2. X=148.
I=3. X=146.
I=4. X=137.
I=5. X=105.
I=6. X=103.
I=7. X=103.
I=8. X=82.
I=9. X=81.
I=10. X=73.
I=11. X=70.
I=12. X=69.
I=13. X=61.
I=14. X=60.
I=15. X=58.
I=16. X=57.
I=17. X=54.
I=18. X=54.
I=19. X=51.
I=20. X=47.
I=21. X=44.
I=22. X=41.
I=23. X=28.
I=24. X=26.
I=25. X=19.
I=26. X=11.

CALCULATION

SUM X= 1877.
SUM X^2= 174843.
SUM X^3= 19296155.
MEAN X= 72.19230769
MEAN X^2= 6724.730769
MEAN X^3= 742159.8077
SUM DEV SQU. S=39338.038
46
VARIANCE S/N=1513.
UNBIASED VARI. =S/(N-1)=
1573.52
VARIATION COEF.=SX/MEAN
X=0.54
STANDARD DEV. SX=√(S/N)=
38.9
STA. DEV. EST. USX=√(S/(
N-1))=39.67
SKEWNESS COEF. CS1=0.65
UNBIASED S.C. CS1=0.637

PROBABLE EXTREAM VALUE(
XT), RETURN PERIOD(T),
FREQUENCY FUNCTION:
XT=XM+K*SX, K=(YT-YM)/SY
, XM=MEAN X, YM=-LN(LN(T
SO THAT XT=XM-(YM+SX/SY)
+(SX/SY)*YT

CAL. VALUE:
XM=72.19230769 SX=39.67
YM=0.5321 SY=1.0961

ESTIMATE EQUATION:
XT=52.93+36.19YT

T=2. XT=66.2
T=4. XT=98.
T=5. XT=107.2
T=10. XT=134.4
T=20. XT=160.4
T=25. XT=168.7
T=50. XT=194.1
T=100. XT=219.4
T=200. XT=244.6
T=1000. XT=302.9

NOTE

1. XT : Magnitude of the event reached or exceeded on an average once in T years
2. T : Return period
3. C. L. : Confidence level
4. LMT : Conficence limit

CONFIDENCE INTERVAL

| | | |
|---------|----------|-------------|
| T=5. | C.L.=95% | LMT=+-25.8 |
| | C.L.=90% | LMT=+-21.7 |
| | C.L.=80% | LMT=+-16.9 |
| | C.L.=68% | LMT=+-13.2 |
| T=10. | C.L.=95% | LMT=+-35.7 |
| | C.L.=90% | LMT=+-30. |
| | C.L.=80% | LMT=+-23.4 |
| | C.L.=68% | LMT=+-18.2 |
| T=20. | C.L.=95% | LMT=+-45.7 |
| | C.L.=90% | LMT=+-38.3 |
| | C.L.=80% | LMT=+-29.9 |
| | C.L.=68% | LMT=+-23.3 |
| T=25. | C.L.=95% | LMT=+-48.9 |
| | C.L.=90% | LMT=+-41. |
| | C.L.=80% | LMT=+-32. |
| | C.L.=68% | LMT=+-24.9 |
| T=50. | C.L.=95% | LMT=+-58.9 |
| | C.L.=90% | LMT=+-49.4 |
| | C.L.=80% | LMT=+-38.5 |
| | C.L.=68% | LMT=+-30. |
| T=100. | C.L.=95% | LMT=+-68.8 |
| | C.L.=90% | LMT=+-57.8 |
| | C.L.=80% | LMT=+-45. |
| | C.L.=68% | LMT=+-35.1 |
| T=200. | C.L.=95% | LMT=+-78.8 |
| | C.L.=90% | LMT=+-66.2 |
| | C.L.=80% | LMT=+-51.6 |
| | C.L.=68% | LMT=+-40.2 |
| T=1000. | C.L.=95% | LMT=+-102.1 |
| | C.L.=90% | LMT=+-85.7 |
| | C.L.=80% | LMT=+-66.8 |
| | C.L.=68% | LMT=+-52.1 |

(8) Probability Calculation of Maximum Daily Rainfall in August at the Climatological Station of Darmaga Bogor (CSDB).by Gumble Method (Data period : 1964 - 1989)

GUMBLE MAX. DISTRIBUTION

DATA N=26.

D(1)= 44.0
D(2)= 75.0
D(3)= 26.0
D(4)= 6.0
D(5)= 101.0
D(6)= 58.0
D(7)= 117.0
D(8)= 132.0
D(9)= 22.0
D(10)= 71.0
D(11)= 81.0
D(12)= 84.0
D(13)= 96.0
D(14)= 36.0
D(15)= 53.0
D(16)= 26.0
D(17)= 45.0
D(18)= 72.0
D(19)= 31.0
D(20)= 34.0
D(21)= 114.0
D(22)= 88.0
D(23)= 71.0
D(24)= 50.0
D(25)= 63.0
D(26)= 64.0

RANKING

I=1. X=132.
I=2. X=117.
I=3. X=114.
I=4. X=101.
I=5. X=96.
I=6. X=88.
I=7. X=84.
I=8. X=81.
I=9. X=75.
I=10. X=72.
I=11. X=71.
I=12. X=71.
I=13. X=64.
I=14. X=63.
I=15. X=53.
I=16. X=50.
I=17. X=45.
I=18. X=44.
I=19. X=38.
I=20. X=36.
I=21. X=34.
I=22. X=31.
I=23. X=26.
I=24. X=26.
I=25. X=22.
I=26. X=6.

CALCULATION

SUM X= 1640.
SUM X^2= 129842.
SUM X^3= 11793740.
MEAN X= 63.07692308
MEAN X^2= 4993.923077
MEAN X^3= 453605.3846
SUM DEV SQU. S=26395.846
15
VARIANCE S/N=1015.22
UNBIASED VARI. S/(N-1)=
1055.83
VARIATION COEF.=SX/MEAN
X=0.51
STANDARD DEV. SX=T(S/N)=
31.86
STA. DEV. EST. USX=T(S/(
N-1))=32.49
SKEWNESS COEF. CS1=0.326
UNBIASED S.C. CS1=0.319

PROBABLE EXTREME VALUE(
XT), RETURN PERIOD(T),
FREQUENCY FUNCTION:
XT=XM+K*SX, K=(YT-YM)/SY
, XM=MEAN X, YT=-LN(LN(T
(T-1)))
SO THAT XT=XM-(YM*SX/SY)
+(SX/SY)*YT
CAL. VALUE:
XM=63.07692308 SX=32.49
YM=0.5321 SY=1.0961
ESTIMATE EQUATION:
XT=47.3+29.64YT
XT=47.3+29.64YT
T=2. XT=58.2
T=4. XT=84.2
T=5. XT=91.8
T=10. XT=114.
T=20. XT=135.3
T=25. XT=142.1
T=50. XT=163.
T=100. XT=183.6
T=200. XT=204.3
T=1000. XT=252.

CONFIDENCE INTERVAL

| | T=5. | T=10. | T=20. | T=50. | T=100. |
|----------|------------|---------|-------|-------|--------|
| C.L.=95% | LMT=+-21.1 | | | | |
| C.L.=90% | LMT=+-17.7 | | | | |
| C.L.=80% | LMT=+-13.8 | | | | |
| C.L.=68% | LMT=+-10.8 | | | | |
| | | T=10. | | | |
| C.L.=95% | LMT=+-29.3 | | | | |
| C.L.=90% | LMT=+-24.6 | | | | |
| C.L.=80% | LMT=+-19.1 | | | | |
| C.L.=68% | LMT=+-14.9 | | | | |
| | | T=20. | | | |
| C.L.=95% | LMT=+-37.4 | | | | |
| C.L.=90% | LMT=+-31.4 | | | | |
| C.L.=80% | LMT=+-24.5 | | | | |
| C.L.=68% | LMT=+-19.1 | | | | |
| | | T=25. | | | |
| C.L.=95% | LMT=+-40. | | | | |
| C.L.=90% | LMT=+-33.6 | | | | |
| C.L.=80% | LMT=+-26.2 | | | | |
| C.L.=68% | LMT=+-20.4 | | | | |
| | | T=50. | | | |
| C.L.=95% | LMT=+-48.2 | | | | |
| C.L.=90% | LMT=+-40.5 | | | | |
| C.L.=80% | LMT=+-31.5 | | | | |
| C.L.=68% | LMT=+-24.6 | | | | |
| | | T=100. | | | |
| C.L.=95% | LMT=+-56.4 | | | | |
| C.L.=90% | LMT=+-47.3 | | | | |
| C.L.=80% | LMT=+-36.9 | | | | |
| C.L.=68% | LMT=+-28.8 | | | | |
| | | T=200. | | | |
| C.L.=95% | LMT=+-64.6 | | | | |
| C.L.=90% | LMT=+-54.2 | | | | |
| C.L.=80% | LMT=+-42.2 | | | | |
| C.L.=68% | LMT=+-32.9 | | | | |
| | | T=1000. | | | |
| C.L.=95% | LMT=+-83.6 | | | | |
| C.L.=90% | LMT=+-70.2 | | | | |
| C.L.=80% | LMT=+-54.7 | | | | |
| C.L.=68% | LMT=+-42.7 | | | | |

NOTE 1. XT : Magnitude of the event reached or exceeded on an average once in T years
 2. T : Return period
 3. C. L. : Confidence level
 4. LMT : Confidence limit

(9) Probability Calculation of Maximum Daily Rainfall in September at the Climatological Station of Darmaga Bogor (CSDB). by Gumble Method (Data period : 1964 - 1989)

9th GUMBLE MAX. DISTRIBUTION

DATA N=26.

| | |
|--------|-------|
| D(1)= | 87.0 |
| D(2)= | 70.0 |
| D(3)= | 15.0 |
| D(4)= | 74.0 |
| D(5)= | 77.0 |
| D(6)= | 91.0 |
| D(7)= | 116.0 |
| D(8)= | 89.0 |
| D(9)= | 20.0 |
| D(10)= | 96.0 |
| D(11)= | 61.0 |
| D(12)= | 86.0 |
| D(13)= | 29.0 |
| D(14)= | 69.0 |
| D(15)= | 108.0 |
| D(16)= | 119.0 |
| D(17)= | 119.0 |
| D(18)= | 57.0 |
| D(19)= | 48.0 |
| D(20)= | 55.0 |
| D(21)= | 88.0 |
| D(22)= | 59.0 |
| D(23)= | 87.0 |
| D(24)= | 11.0 |
| D(25)= | 17.0 |
| D(26)= | 70.0 |

RANKING

| | |
|-------|--------|
| I=1. | X=119. |
| I=2. | X=119. |
| I=3. | X=116. |
| I=4. | X=108. |
| I=5. | X=96. |
| I=6. | X=91. |
| I=7. | X=89. |
| I=8. | X=88. |
| I=9. | X=87. |
| I=10. | X=87. |
| I=11. | X=86. |
| I=12. | X=77. |
| I=13. | X=74. |
| I=14. | X=70. |
| I=15. | X=70. |
| I=16. | X=69. |
| I=17. | X=61. |
| I=18. | X=59. |
| I=19. | X=57. |
| I=20. | X=55. |
| I=21. | X=48. |
| I=22. | X=29. |
| I=23. | X=20. |
| I=24. | X=17. |
| I=25. | X=15. |
| I=26. | X=11. |

CALCULATION

| | |
|-----------------------------|-------------|
| SUM X= | 1818. |
| SUM X^2= | 152760. |
| SUM X^3= | 13981530. |
| MEAN X= | 69.92307692 |
| MEAN X^2= | 5875.384615 |
| MEAN X^3= | 537751.1538 |
| SUM DEV SQU. S= | 25639.846 |
| 15 | |
| VARIANCE S/N= | 986.15 |
| UNBIASED VARI. =S/(N-1)= | |
| 1025.59 | |
| VARIATION COEF.=SX/MEAN | |
| X=0.45 | |
| STANDARD DEV. SX=SQRT(S/N)= | |
| 31.4 | |
| STA. DEV. EST. USX=S/(N-1) | |
| N-1)=32.02 | |
| SKEWNESS COEF. CS1=-0.35 | |
| 5 | |
| UNBIASED S.C. CS1=-0.348 | |

PROBABLE EXTREME VALUE(XT), RETURN PERIOD(T), FREQUENCY FUNCTION:

XT=X_M+K*SX, K=(YT-YM)/SY
, X_M=MEAN X, YT=-LN(LN(T/(T-1)))
SO THAT XT=X_M-(YM*SX/SY)+
(SX/SY)*YT

CAL. VALUE:
XM=69.92307692 SX=32.02
YM=0.5321 SY=1.0961

ESTIMATE EQUATION:

XT=54.38+29.21YT

T=2. XT=65.1

T=4. XT=90.8

T=5. XT=98.2

T=10. XT=120.1

T=20. XT=141.1

T=25. XT=147.8

T=50. XT=168.4

T=100. XT=188.8

T=200. XT=209.1

T=1000. XT=256.1

CONFIDENCE INTERVAL

| | |
|---------|---------------------|
| T=5. | C.L.=95% LMT=+-20.8 |
| T=10. | C.L.=90% LMT=+-17.5 |
| T=20. | C.L.=80% LMT=+-13.6 |
| T=25. | C.L.=68% LMT=+-10.6 |
| T=50. | C.L.=95% LMT=+-28.8 |
| T=50. | C.L.=90% LMT=+-24.2 |
| T=50. | C.L.=80% LMT=+-18.9 |
| T=50. | C.L.=68% LMT=+-14.7 |
| T=100. | C.L.=95% LMT=+-31. |
| T=100. | C.L.=90% LMT=+-24.1 |
| T=100. | C.L.=80% LMT=+-18.8 |
| T=100. | C.L.=68% LMT=+-14.7 |
| T=200. | C.L.=95% LMT=+-39.5 |
| T=200. | C.L.=90% LMT=+-35.1 |
| T=200. | C.L.=80% LMT=+-25.8 |
| T=200. | C.L.=68% LMT=+-20.1 |
| T=500. | C.L.=95% LMT=+-47.5 |
| T=500. | C.L.=90% LMT=+-43.9 |
| T=500. | C.L.=80% LMT=+-31.1 |
| T=500. | C.L.=68% LMT=+-24.2 |
| T=1000. | C.L.=95% LMT=+-55.6 |
| T=1000. | C.L.=90% LMT=+-46.6 |
| T=1000. | C.L.=80% LMT=+-36.3 |
| T=1000. | C.L.=68% LMT=+-28.4 |
| T=2000. | C.L.=95% LMT=+-63.6 |
| T=2000. | C.L.=90% LMT=+-53.4 |
| T=2000. | C.L.=80% LMT=+-41.6 |
| T=2000. | C.L.=68% LMT=+-32.5 |
| T=4000. | C.L.=95% LMT=+-82.4 |
| T=4000. | C.L.=90% LMT=+-69.2 |
| T=4000. | C.L.=80% LMT=+-53.9 |
| T=4000. | C.L.=68% LMT=+-42.1 |

NOTE

1. XT : Magnitude of the event reached or exceeded on an average once in T years
2. T : Return period
3. C. L. : Confidence level
4. LMT : Confidence limit

(10) Probability Calculation of Maximum Daily Rainfall in October at the Climatological Station of Darmaga Bogor (CSDB).by Gumble Method (Data period : 1964 - 1989)

GUMBLE MAX. DIS. RUTION

DATA N=26.

D(1)= 50.0
D(2)= 62.0
D(3)= 46.0
D(4)= 65.0
D(5)= 85.0
D(6)= 57.0
D(7)= 33.0
D(8)= 68.0
D(9)= 72.0
D(10)= 64.0
D(11)= 80.0
D(12)= 50.0
D(13)= 35.0
D(14)= 74.0
D(15)= 109.0
D(16)= 77.0
D(17)= 129.0
D(18)= 47.0
D(19)= 63.0
D(20)= 58.0
D(21)= 33.0
D(22)= 84.0
D(23)= 48.0
D(24)= 81.0
D(25)= 53.0
D(26)= 93.0

RANKING

I=1. X=129.
I=2. X=109.
I=3. X=90.
I=4. X=85.
I=5. X=84.
I=6. X=83.
I=7. X=83.
I=8. X=81.
I=9. X=80.
I=10. X=77.
I=11. X=74.
I=12. X=72.
I=13. X=68.
I=14. X=65.
I=15. X=64.
I=16. X=63.
I=17. X=62.
I=18. X=57.
I=19. X=53.
I=20. X=50.
I=21. X=48.
I=22. X=47.
I=23. X=46.
I=24. X=35.
I=25. X=33.
I=26. X=30.

CALCULATION
SUM X= 1768.
SUM X^2= 133390.
SUM X^3= 11015776.

MEAN X= 68.
MEAN X^2= 5130.384615
MEAN X^3= 423683.6923
SUM DEV SQU. S=13166.
VARIANCE S/N=506.38
UNBIASED VARI. S/(N-1)=
526.64
VARIATION COEF.=SX/MEAN
X=0.33
STANDARD DEV. SX=S/(S/N)=
22.5
STA. DEV. EST. USX=S/(N-1))=22.95
SKEWNESS COEF. CS!=0.522
UNBIASED S.C. CS1=0.512

PROBABLE EXTREAM VALUE(XT), RETURN PERIOD(T),
FREQUENCY FUNCTION:

XT=XM+K*SX, K=(YT-YM)/SY
, XM=MEAN X, YT=-LN(LN(T
/(T-1)))

SO THAT XT=XM-(YMM*SX/SY)
+(SX/SY)*YT

CAL. VALUE:

XH=68. SX=22.95 YM=0.5
321 SY=1.0961

ESTIMATE EQUATION:

XT=56.86+20.94YT

T=2. XT=64.5

T=4. XT=82.9

T=5. XT=88.3

T=10. XT=104.

T=20. XT=119.1

T=25. XT=123.8

T=50. XT=138.6

T=100. XT=153.2

T=200. XT=167.8

T=1000. XT=201.5

CONFIDENCE INTERVAL

T=5.
C.L.=95% LMT=+-14.9
C.L.=90% LMT=+-12.5
C.L.=80% LMT=+-9.8
C.L.=68% LMT=+-7.6

T=10.
C.L.=95% LMT=+-20.7
C.L.=90% LMT=+-17.3
C.L.=80% LMT=+-15.5
C.L.=68% LMT=+-10.5

T=20.
C.L.=95% LMT=+-26.4
C.L.=90% LMT=+-22.2
C.L.=80% LMT=+-17.3
C.L.=68% LMT=+-13.5

T=25.
C.L.=95% LMT=+-28.3
C.L.=90% LMT=+-23.7
C.L.=80% LMT=+-18.5
C.L.=68% LMT=+-14.4

T=50.
C.L.=95% LMT=+-34.1
C.L.=90% LMT=+-28.6
C.L.=80% LMT=+-22.3
C.L.=68% LMT=+-17.4

T=100.
C.L.=95% LMT=+-39.8
C.L.=90% LMT=+-33.4
C.L.=80% LMT=+-26.1
C.L.=68% LMT=+-20.3

T=200.
C.L.=95% LMT=+-45.6
C.L.=90% LMT=+-38.3
C.L.=80% LMT=+-29.8
C.L.=68% LMT=+-23.3

T=1000.
C.L.=95% LMT=+-59.1
C.L.=90% LMT=+-49.6
C.L.=80% LMT=+-38.6
C.L.=68% LMT=+-30.1

- NOTE 1. XT : Magnitude of the event reached or exceeded on an average once in T years
2. T : Return period
3. C. L. : Confidence level
4. LMT : Confidence limit

(11) Probability Calculation of Maximum Daily Rainfall in November at the Climatological Station of Darmaga Bogor (CSDB).by Gumble Method (Data period : 1964 - 1989)

GUMBLE MAX. DISTRIBUTION

DATA N=26.

D(1)= 41.0
D(2)= 51.0
D(3)= 27.0
D(4)= 94.0
D(5)= 58.0
D(6)= 77.0
D(7)= 58.0
D(8)= 39.0
D(9)= 17.0
D(10)= 79.0
D(11)= 25.0
D(12)= 67.0
D(13)= 63.0
D(14)= 49.0
D(15)= 65.0
D(16)= 82.0
D(17)= 77.0
D(18)= 31.0
D(19)= 85.0
D(20)= 64.0
D(21)= 59.0
D(22)= 76.0
D(23)= 80.0
D(24)= 83.0
D(25)= 34.0
D(26)= 50.0

RANKING

I=1. X=94.
I=2. X=85.
I=3. X=83.
I=4. X=82.
I=5. X=80.
I=6. X=79.
I=7. X=77.
I=8. X=77.
I=9. X=76.
I=10. X=67.
I=11. X=65.
I=12. X=64.
I=13. X=63.
I=14. X=59.
I=15. X=58.
I=16. X=51.
I=17. X=50.
I=18. X=49.
I=19. X=41.
I=20. X=39.
I=21. X=38.
I=22. X=34.
I=23. X=31.
I=24. X=27.
I=25. X=25.
I=26. X=17.

CALCULATION

SUM X= 1511.
SUM X^2= 99481.
SUM X^3= 7080743.
MEAN X= 58.11538462
MEAN X^2= 3826.192308
MEAN X^3= 272336.2692
SUM DEV SQU. S=11668.653
85
VARIANCE S/N=448.79
UNBIASED VARI. =S/(N-1)=
466.75
VARIATION COEF.=SX/MEAN
X=0.36
STANDARD DEV. SX=f(S/N)=
21.18
STA. DEV. EST. USX=f(S/(
N-1))=21.6
SKEWNESS COEF. CS!= -0.23
UNBIASED S.C. CS1=-0.226
PROBABLE EXTREME VALUE(
XT), RETURN PERIOD(T),
FREQUENCY FUNCTION:

XT=XM+K*SX, K=(YT-YM)/SY
, XM=MEAN X, YT=-LN(LN(T
/(T-1)))
SO THAT XT=XM-(YM*SX/SY)
+(SX/SY)*YT

CAL. VALUE:
XM=58.11538462 SX=21.6
YM=0.5321 SY=1.0961
ESTIMATE EQUATION:
XT=47.63+19.71YT
T=2. XT=54.9
T=4. XT=72.2
T=5. XT=77.2
T=10. XT=92.
T=20. XT=106.2
T=25. XT=110.7
T=50. XT=124.5
T=100. XT=138.3
T=200. XT=152.
T=1000. XT=183.8

NOTE

1. XT : Magnitude of the event reached or exceeded on an average once in T years
2. T : Return period
3. C. L. : Confidence level
4. LMT : Confidence limit

CONFIDENCE INTERVAL

| | |
|---------|---------------------|
| T=5. | C.L.=95% LMT=+-14.1 |
| | C.L.=90% LMT=+-11.8 |
| | C.L.=80% LMT=+-9.2 |
| | C.L.=68% LMT=+-7.2 |
| T=10. | C.L.=95% LMT=+-19.5 |
| | C.L.=90% LMT=+-16.3 |
| | C.L.=80% LMT=+-12.7 |
| | C.L.=68% LMT=+-9.9 |
| T=20. | C.L.=95% LMT=+-24.9 |
| | C.L.=90% LMT=+-20.9 |
| | C.L.=80% LMT=+-16.3 |
| | C.L.=68% LMT=+-12.7 |
| T=25. | C.L.=95% LMT=+-26.6 |
| | C.L.=90% LMT=+-22.3 |
| | C.L.=80% LMT=+-17.4 |
| | C.L.=68% LMT=+-13.6 |
| T=50. | C.L.=95% LMT=+-32.1 |
| | C.L.=90% LMT=+-26.9 |
| | C.L.=80% LMT=+-21. |
| | C.L.=68% LMT=+-16.4 |
| T=100. | C.L.=95% LMT=+-37.5 |
| | C.L.=90% LMT=+-31.5 |
| | C.L.=80% LMT=+-24.5 |
| | C.L.=68% LMT=+-19.1 |
| T=200. | C.L.=95% LMT=+-42.9 |
| | C.L.=90% LMT=+-36. |
| | C.L.=80% LMT=+-28.1 |
| | C.L.=68% LMT=+-21.9 |
| T=1000. | C.L.=95% LMT=+-55.6 |
| | C.L.=90% LMT=+-46.7 |
| | C.L.=80% LMT=+-36.4 |
| | C.L.=68% LMT=+-28.4 |

(12) Probability Calculation of Maximum Daily Rainfall in December at the Climatological Station of Darmaga Bogor (CSDB).by Gumble Method (Data period : 1964 - 1989)

GUMBLE MAX. DISTRIBUTION

DATA N=26.

D(1)= 49.0
D(2)= 112.0
D(3)= 23.0
D(4)= 52.0
D(5)= 37.0
D(6)= 25.0
D(7)= 30.0
D(8)= 35.0
D(9)= 44.0
D(10)= 87.0
D(11)= 38.0
D(12)= 48.0
D(13)= 58.0
D(14)= 80.0
D(15)= 53.0
D(16)= 40.0
D(17)= 144.0
D(18)= 128.0
D(19)= 111.0
D(20)= 51.0
D(21)= 33.0
D(22)= 60.0
D(23)= 82.0
D(24)= 51.0
D(25)= 59.0
D(26)= 104.0

RANKING

I=1. X=144.
I=2. X=128.
I=3. X=112.
I=4. X=111.
I=5. X=104.
I=6. X=87.
I=7. X=82.
I=8. X=80.
I=9. X=60.
I=10. X=59.
I=11. X=58.
I=12. X=56.
I=13. X=53.
I=14. X=52.
I=15. X=49.
I=16. X=48.
I=17. X=44.
I=18. X=40.
I=19. X=38.
I=20. X=37.
I=21. X=35.
I=22. X=33.
I=23. X=31.
I=24. X=30.
I=25. X=25.
I=26. X=23.

CALCULATION

SUM X= 1619.
SUM X^2= 128971.
SUM X^3= 12430367.
MEAN X= 62.26923077
MEAN X^2= 4960.423077
MEAN X^3= 478091.0385
SUM DEV SQU. S=28157.115
39
VARIANCE S/N=1082.97
UNBIASED VARI. =S/(N-1)=
1126.28
VARIATION COEF.=SX/MEAN
X=0.53
STANDARD DEV. SX=J(S/N)=
32.91
STA. DEV. EST. USK=J(S/(
N-1))=33.56
SKEWNESS COEF. CS1=0.964
UNBIASED S.C. CS1=0.945

PROBABLE EXTREME VALUE(
XT), RETURN PERIOD(T),
FREQUENCY FUNCTION:
XT=XM+K*SX, K=(YT-YM)/SY
, XM=MEAN X, YT=-LN(LN(T
SO THAT XT=XM-(YM*SX/SY)
+(SX/SY)*YT

CAL. VALUE:
XM=62.26923077 SX=33.56
YM=0.5321 SY=1.0961

ESTIMATE EQUATION:

XT=45.98+30.62YT

T=2. XT=57.2
T=4. XT=84.1
T=5. XT=91.9
T=10. XT=114.9
T=20. XT=136.9
T=25. XT=143.9
T=50. XT=165.5
T=100. XT=186.8
T=200. XT=208.1
T=1000. XT=257.5

NOTE

1. XT : Magnitude of the event reached or exceeded on an average once in T years
2. T : Return period
3. C. L. : Confidence level
4. LMT : Confidence limit

CONFIDENCE INTERVAL

| | |
|---------|---------------------|
| T=5. | C.L.=95% LMT=+-21.8 |
| | C.L.=90% LMT=+-18.3 |
| | C.L.=80% LMT=+-14.3 |
| | C.L.=68% LMT=+-11.1 |
| T=10. | C.L.=95% LMT=+-30.2 |
| | C.L.=90% LMT=+-25.4 |
| | C.L.=80% LMT=+-19.0 |
| | C.L.=68% LMT=+-15.4 |
| T=20. | C.L.=95% LMT=+-38.7 |
| | C.L.=90% LMT=+-32.4 |
| | C.L.=80% LMT=+-25.3 |
| | C.L.=68% LMT=+-19.7 |
| T=25. | C.L.=95% LMT=+-41.4 |
| | C.L.=90% LMT=+-34.7 |
| | C.L.=80% LMT=+-27.1 |
| | C.L.=68% LMT=+-21.1 |
| T=50. | C.L.=95% LMT=+-49.8 |
| | C.L.=90% LMT=+-41.8 |
| | C.L.=80% LMT=+-32.6 |
| | C.L.=68% LMT=+-25.4 |
| T=100. | C.L.=95% LMT=+-58.2 |
| | C.L.=90% LMT=+-48.9 |
| | C.L.=80% LMT=+-38.1 |
| | C.L.=68% LMT=+-29.7 |
| T=200. | C.L.=95% LMT=+-66.7 |
| | C.L.=90% LMT=+-56. |
| | C.L.=80% LMT=+-43.6 |
| | C.L.=68% LMT=+-34. |
| T=1000. | C.L.=95% LMT=+-86.4 |
| | C.L.=90% LMT=+-72.5 |
| | C.L.=80% LMT=+-56.5 |
| | C.L.=68% LMT=+-44.1 |

(13) Probability Calculation of Annual Maximum Daily Rainfall at the Climatological Station of Darmaga Bogor (CSDB).by Gumble Method (Data period : 1964 - 1989)

GUMBLE MAX. DISTRIBUTION

DATA N=26.

D(1)= 100.0
D(2)= 112.0
D(3)= 99.0
D(4)= 94.0
D(5)= 103.0
D(6)= 99.0
D(7)= 117.0
D(8)= 132.0
D(9)= 88.0
D(10)= 113.0
D(11)= 148.0
D(12)= 177.0
D(13)= 181.0
D(14)= 84.0
D(15)= 149.0
D(16)= 137.0
D(17)= 144.0
D(18)= 146.0
D(19)= 111.0
D(20)= 90.0
D(21)= 114.0
D(22)= 105.0
D(23)= 110.0
D(24)= 88.0
D(25)= 89.0
D(26)= 240.0

RANKING

I=1. X=240.
I=2. X=181.
I=3. X=177.
I=4. X=149.
I=5. X=148.
I=6. X=146.
I=7. X=144.
I=8. X=137.
I=9. X=132.
I=10. X=117.
I=11. X=114.
I=12. X=113.
I=13. X=112.
I=14. X=111.
I=15. X=110.
I=16. X=105.
I=17. X=105.
I=18. X=100.
I=19. X=99.
I=20. X=99.
I=21. X=94.
I=22. X=90.
I=23. X=89.
I=24. X=88.
I=25. X=88.
I=26. X=84.

CALCULATION

SUM X= 3170.
SUM X^2= 419096.
SUM X^3= 60858920.
MEAN X= 121.9230769
MEAN X^2= 16119.07692
MEAN X^3= 2340727.692
SUM DEV SQU. S=32599.846
15
VARIANCE S/N=1253.84
UNBIASED VARI. =S/(N-1)=
1303.99

VARIATION COEF.=SX/MEAN

X=0.29
STANDARD DEV. SX=SQRT(S/N)=
35.41
STA. DEV. EST. USX=SQRT(S/(N-1))=36.11
SKEWNESS COEF. CS1=1.57
UNBIASED S.C. CS1=1.539

PROBABLE EXTREME VALUE(XT), RETURN PERIOD(T),
FREQUENCY FUNCTION:

XT=XM+K*SX, K=(YT-YM)/SY
, XM=MEAN X, YT=-LN(LN(T)/(T-1)))
SO THAT XT=XM-(YM*SX/SY)+
(SX/SY)*YT

CAL. VALUE:

XM=121.9230769 SX=36.11
YM=0.5321 SY=1.9961

ESTIMATE EQUATIONS:
XT=104.39+32.94YT

T=2. XT=116.5
T=4. XT=145.4
T=5. XT=153.8
T=10. XT=178.5
T=20. XT=202.2
T=25. XT=209.7
T=50. XT=232.9
T=100. XT=255.9
T=200. XT=278.8
T=1000. XT=331.9

- NOTE 1. XT : Magnitude of the event reached or exceeded on an average once in T years
2. T : Return period
3. C. L. : Confidence level
4. LMT : Confidence limit

CONFIDENCE INTERVAL

T=5. C.L.=95% LMT=+-23.5
C.L.=90% LMT=+-19.7
C.L.=80% LMT=+-15.4
C.L.=68% LMT=+-12.
T=10. C.L.=95% LMT=+-32.5
C.L.=90% LMT=+-27.3
C.L.=80% LMT=+-21.3
C.L.=68% LMT=+-16.6
T=20. C.L.=95% LMT=+-41.6
C.L.=90% LMT=+-34.9
C.L.=80% LMT=+-27.2
C.L.=68% LMT=+-21.2
T=25. C.L.=95% LMT=+-44.5
C.L.=90% LMT=+-37.4
C.L.=80% LMT=+-29.1
C.L.=68% LMT=+-22.7
T=50. C.L.=95% LMT=+-55.5
C.L.=90% LMT=+-45.
C.L.=80% LMT=+-35.
C.L.=68% LMT=+-27.3
T=100. C.L.=95% LMT=+-62.7
C.L.=90% LMT=+-52.6
C.L.=80% LMT=+-41.
C.L.=68% LMT=+-32.
T=200. C.L.=95% LMT=+-71.8
C.L.=90% LMT=+-60.2
C.L.=80% LMT=+-46.9
C.L.=68% LMT=+-36.6
T=1000. C.L.=95% LMT=+-92.9
C.L.=90% LMT=+-78.
C.L.=80% LMT=+-60.8
C.L.=68% LMT=+-47.4

Table C1-14

**The Highest Rainfall (mm) for the Short Duration
in the Month and Annual at the CSDB**

No. 1 1985, 1986

No. 2 1987, 1988

No. 3 1989

The Highest Rainfall for the Short Duration in the Month and Annual at the CSDB.

No. 1

| Month | Minutes | | | | | | Hours | | | | |
|-------------------|---------|-------|-------|-------|-------|------|-------|-------|-------|-------|-------|
| | 5 | 10 | 15 | 30 | 45 | 60 | 2 | 3 | 6 | 12 | 24 |
| A. Records | | | | | | | | | | | |
| 1985 | | | | | | | | | | | |
| Jan. | 14.7 | 29.4 | 39.2 | 58.8 | 62.0 | 73.1 | 73.1 | 73.4 | 73.4 | 73.4 | 73.4 |
| Feb. | 10.2 | 20.4 | 25.5 | 39.9 | 55.7 | 63.6 | 74.8 | 83.2 | 101.5 | 105.0 | 105.0 |
| Mar. | 10.0 | 18.0 | 20.0 | 36.0 | 47.0 | 50.0 | 60.5 | 63.5 | 64.0 | 64.0 | 64.0 |
| Apr. | 9.9 | 19.9 | 29.8 | 49.7 | 62.4 | 62.8 | 63.8 | 63.9 | 64.0 | 64.0 | 64.0 |
| May | 9.9 | 19.8 | 29.7 | 44.6 | 55.6 | 60.4 | 62.1 | 62.5 | 62.9 | 62.9 | 62.9 |
| Jun. | 9.0 | 10.0 | 16.0 | 27.8 | 28.7 | 30.0 | 33.5 | 34.1 | 34.4 | 35.9 | 35.9 |
| Jul. | 20.0 | 30.0 | 45.0 | 60.0 | 72.0 | 85.0 | 90.0 | 94.0 | 102.7 | 102.7 | 102.7 |
| Aug. | 20.2 | 25.3 | 35.4 | 60.6 | 75.8 | 84.3 | 87.7 | 87.7 | 87.7 | 87.7 | 86.8 |
| Sep. | 10.4 | 13.0 | 17.0 | 28.0 | 35.3 | 42.5 | 43.2 | 43.7 | 58.5 | 58.7 | 58.7 |
| Oct. | 10.0 | 16.0 | 20.0 | 40.0 | 54.0 | 60.0 | 78.9 | 83.5 | 84.0 | 84.0 | 84.0 |
| Nov. | 10.0 | 15.0 | 20.0 | 36.0 | 45.5 | 48.4 | 48.4 | 48.4 | 76.7 | 76.7 | 76.7 |
| Dec. | 10.0 | 19.0 | 23.0 | 34.0 | 38.0 | 40.0 | 60.5 | 60.5 | 60.5 | 60.5 | 60.5 |
| Annual Max | | | | | | | | | | | |
| mm | 20.2 | 30.0 | 45.0 | 60.6 | 75.8 | 85.0 | 90.0 | 94.0 | 102.7 | 105.0 | 105.0 |
| mm/hr | 242.4 | 180.0 | 180.0 | 121.2 | 101.1 | 85.0 | 45.0 | 31.3 | 17.1 | 8.8 | 4.4 |
| 1986 | | | | | | | | | | | |
| Jan. | 7.5 | 13.0 | 20.0 | 34.0 | 38.0 | 39.9 | 39.9 | 39.9 | 40.5 | 41.0 | |
| Feb. | 20.0 | 30.0 | 40.0 | 60.0 | 68.0 | 82.5 | 98.0 | 102.5 | 104.7 | 104.7 | 104.7 |
| Mar. | 10.0 | 20.0 | 24.0 | 38.0 | 54.0 | 64.0 | 80.0 | 96.0 | 104.2 | 104.2 | 104.2 |
| Apr. | 10.0 | 20.0 | 23.0 | 40.0 | 54.0 | 54.9 | 55.3 | 55.4 | 55.4 | 55.4 | 55.4 |
| May | 20.0 | 30.0 | 40.0 | 50.0 | 66.0 | 71.4 | 71.4 | 71.4 | 71.4 | 71.4 | 71.4 |
| Jun. | 10.0 | 20.0 | 30.0 | 60.0 | 65.0 | 68.8 | 80.0 | 90.0 | 112.5 | 113.8 | 113.8 |
| Jul. | 10.0 | 20.0 | 30.0 | 50.0 | 55.0 | 70.0 | 104.5 | 104.8 | 104.8 | 104.8 | 104.8 |
| Aug. | 20.0 | 30.0 | 35.0 | 50.0 | 58.0 | 62.0 | 66.4 | 66.4 | 67.0 | 70.4 | 70.4 |
| Sep. | 20.0 | 30.0 | 37.0 | 49.0 | 52.0 | 70.0 | 72.5 | 72.5 | 80.6 | 88.8 | 88.8 |
| Oct. | 10.0 | 18.0 | 26.0 | 35.9 | 36.3 | 40.0 | 44.8 | 46.4 | 47.4 | 47.4 | 47.4 |
| Nov. | 15.0 | 20.0 | 30.0 | 40.0 | 58.0 | 62.5 | 74.5 | 78.0 | 78.4 | 78.4 | 78.4 |
| Dec. | 15.0 | 25.0 | 35.0 | 60.0 | 62.0 | 76.0 | 80.5 | 80.5 | 80.5 | 80.5 | 80.5 |
| Annual Max | | | | | | | | | | | |
| mm | 20.0 | 30.0 | 40.0 | 60.0 | 68.0 | 82.5 | 104.5 | 104.8 | 112.5 | 113.8 | 113.8 |
| mm/hr | 240.0 | 180.0 | 160.0 | 120.0 | 90.7 | 82.5 | 52.3 | 34.9 | 18.8 | 9.5 | 4.7 |

The Highest Rainfall for the Short Duration in the Month and Annual at the CSDB.

No. 2

| Month | Minutes | | | | | | Hours | | | | |
|-------------------|---------|-------|-------|-------|------|------|-------|------|------|------|------|
| | 5 | 10 | 15 | 30 | 45 | 60 | 2 | 3 | 6 | 12 | 24 |
| 1987 | | | | | | | | | | | |
| Jan. | 10.0 | 17.0 | 20.0 | 32.0 | 39.0 | 37.0 | 40.0 | 42.5 | 43.4 | 43.4 | 43.4 |
| Feb. | 7.0 | 9.8 | 10.0 | 20.0 | 30.5 | 30.0 | 30.9 | 32.5 | 32.5 | 32.5 | 67.4 |
| Mar. | 10.0 | 18.7 | 18.9 | 25.0 | 33.0 | 37.0 | 60.0 | 64.5 | 67.4 | 67.4 | 67.4 |
| Apr. | 17.0 | 20.0 | 25.0 | 33.0 | 36.0 | 50.0 | 61.0 | 72.5 | 76.8 | 76.8 | 76.8 |
| May | 15.0 | 25.0 | 39.0 | 43.0 | 64.0 | 67.0 | 85.0 | 87.9 | 87.9 | 87.9 | 87.9 |
| Jun. | 14.0 | 20.0 | 25.0 | 34.0 | 46.0 | 52.0 | 59.0 | 59.0 | 64.0 | 64.0 | 64.0 |
| Jul. | 10.0 | 20.0 | 27.0 | 40.0 | 60.0 | 63.5 | 68.5 | 69.5 | 70.2 | 70.2 | 70.2 |
| Aug. | 10.0 | 20.0 | 30.0 | 40.0 | 48.0 | 50.0 | 50.3 | 50.3 | 50.3 | 50.3 | 50.3 |
| Sep. | 5.5 | 9.5 | 10.0 | 10.1 | 10.2 | 10.3 | 11.3 | 11.3 | 11.3 | 11.3 | 11.3 |
| Oct. | 10.0 | 20.0 | 23.0 | 42.0 | 54.0 | 60.0 | 72.3 | 72.3 | 83.0 | 83.0 | 83.0 |
| Nov. | 16.0 | 20.0 | 26.0 | 37.0 | 45.5 | 55.0 | 75.5 | 77.0 | 77.0 | 82.5 | 82.5 |
| Dec. | 7.3 | 9.5 | 12.7 | 15.5 | 17.5 | 27.1 | 29.2 | 29.2 | 29.2 | 29.8 | 29.8 |
| Annual Max | | | | | | | | | | | |
| mm | 17.0 | 25.0 | 39.0 | 43.0 | 64.0 | 67.0 | 85.0 | 87.9 | 87.9 | 87.9 | 87.9 |
| mm/hr | 204.0 | 150.0 | 156.0 | 86.0 | 85.3 | 67.0 | 42.5 | 29.3 | 14.7 | 7.3 | 3.7 |
| 1988 | | | | | | | | | | | |
| Jan. | 10.0 | 20.0 | 26.0 | 40.0 | 56.0 | 71.0 | 74.0 | 74.0 | 74.0 | 90.0 | 90.0 |
| Feb. | 10.0 | 20.0 | 27.0 | 40.0 | 50.0 | 66.0 | 67.0 | 67.0 | 67.0 | 67.0 | 67.0 |
| Mar. | 10.0 | 15.0 | 20.0 | 31.0 | 33.5 | 34.0 | 50.0 | 53.0 | 58.8 | 59.0 | 59.0 |
| Apr. | 15.0 | 20.0 | 30.0 | 50.0 | 65.6 | 70.5 | 75.0 | 75.6 | 86.7 | 86.7 | 86.7 |
| May | 9.6 | 16.8 | 19.8 | 34.8 | 39.1 | 40.3 | 52.4 | 55.6 | 80.2 | 80.2 | 80.2 |
| Jun. | 9.5 | 16.5 | 21.0 | 28.6 | 30.0 | 33.8 | 34.0 | 34.4 | 64.3 | 64.3 | 64.3 |
| Jul. | 9.8 | 19.6 | 31.5 | 41.3 | 46.1 | 48.7 | 52.5 | 61.8 | 69.8 | 70.0 | 70.0 |
| Aug. | 8.5 | 10.2 | 20.1 | 35.5 | 36.6 | 36.9 | 37.0 | 37.0 | 60.5 | 63.1 | 63.1 |
| Sep. | 6.5 | 8.7 | 9.6 | 13.0 | 14.9 | 15.8 | 15.9 | 15.9 | 16.7 | 16.7 | 16.7 |
| Oct. | 8.0 | 10.2 | 12.2 | 20.4 | 25.4 | 26.5 | 43.8 | 47.3 | 51.3 | 52.1 | 52.1 |
| Nov. | 6.0 | 10.0 | 14.7 | 20.2 | 30.2 | 31.7 | 33.5 | 33.9 | 33.9 | 33.9 | 33.9 |
| Dec. | 10.0 | 20.0 | 20.4 | 33.2 | 38.0 | 40.6 | 40.6 | 40.6 | 46.5 | 49.0 | 49.0 |
| Annual Max | | | | | | | | | | | |
| mm | 15.0 | 20.0 | 31.5 | 50.0 | 56.0 | 71.0 | 74.0 | 74.0 | 86.7 | 86.7 | 86.7 |
| mm/hr | 180.0 | 120.0 | 126.0 | 100.0 | 74.7 | 71.0 | 37.0 | 24.7 | 14.5 | 7.2 | 3.6 |

The Highest Rainfall for the Short Duration in the Month and Annual at the CSDB.

No. 3

| Month | Minutes | | | | | | Hours | | | | |
|-------------------|---------|-------|-------|-------|-------|------|-------|------|-------|-------|-------|
| | 5 | 10 | 15 | 30 | 45 | 60 | 2 | 3 | 6 | 12 | 24 |
| 1989 | | | | | | | | | | | |
| Jan. | 8.0 | 10.2 | 19.4 | 31.4 | 48.6 | 58.9 | 69.0 | 75.0 | 75.2 | 75.2 | 75.2 |
| Feb. | 10.1 | 17.1 | 22.9 | 36.7 | 40.2 | 43.9 | 67.5 | 87.4 | 127.4 | 226.3 | 233.1 |
| Mar. | 10.2 | 20.1 | 23.9 | 32.3 | 33.8 | 35.4 | 52.4 | 54.7 | 54.7 | 54.7 | 54.8 |
| Apr. | 18.6 | 21.8 | 22.8 | 29.3 | 32.1 | 33.9 | 38.3 | 40.1 | 40.7 | 40.8 | 40.8 |
| May | 10.0 | 20.0 | 25.5 | 47.3 | 60.0 | 71.7 | 78.2 | 82.8 | 122.6 | 123.6 | 133.6 |
| Jun. | 9.0 | 12.3 | 18.0 | 28.0 | 41.0 | 63.0 | 77.0 | 91.1 | 92.7 | 92.7 | 92.7 |
| Jul. | 11.0 | 19.0 | 25.0 | 42.0 | 48.3 | 50.2 | 50.6 | 50.7 | 50.7 | 50.7 | 50.7 |
| Aug. | 10.0 | 15.0 | 24.8 | 41.0 | 49.7 | 52.1 | 53.7 | 56.3 | 60.0 | 62.7 | 62.7 |
| Sep. | 14.0 | 24.0 | 34.0 | 53.0 | 54.1 | 54.1 | 70.3 | 70.3 | 70.3 | 70.3 | 70.3 |
| Oct. | 16.0 | 30.0 | 40.0 | 44.5 | 54.0 | 57.0 | 59.0 | 61.5 | 61.5 | 61.7 | 61.7 |
| Nov. | 11.2 | 21.2 | 25.0 | 31.3 | 40.0 | 41.3 | 61.0 | 73.5 | 83.4 | 83.4 | 83.4 |
| Dec. | 20.0 | 26.0 | 31.0 | 54.0 | 75.0 | 82.0 | 91.1 | 94.1 | 103.5 | 103.5 | 103.5 |
| Annual Max | | | | | | | | | | | |
| mm | 18.6 | 30.0 | 40.0 | 54.0 | 75.0 | 82.0 | 91.1 | 94.1 | 127.4 | 226.3 | 233.1 |
| mm/hr | 223.2 | 180.0 | 160.0 | 108.0 | 100.0 | 82.0 | 45.6 | 31.4 | 21.2 | 18.9 | 9.7 |

B. Maximum of Records (1985 - 1988)

| | | | | | | | | | | | |
|-------|-------|-------|-------|-------|-------|------|-------|-------|-------|-------|-------|
| mm | 20.2 | 30.0 | 40.0 | 60.0 | 75.0 | 82.5 | 104.5 | 104.8 | 127.4 | 226.3 | 233.1 |
| mm/hr | 242.2 | 180.0 | 160.0 | 120.0 | 100.0 | 82.5 | 52.3 | 34.9 | 21.2 | 18.9 | 9.7 |

Table C1-15

Calculation of Probability of Exceedance on the Data
of the Short Duration Rainfall Intensity (mm/hr)
Data Period 5 years

- No. 1 5 minutes, 10 minutes, 15 minutes
- No. 2 30 minutes, 45 minutes, 60 minutes
- No. 3 2 hours, 3 hours, 6 hours
- No. 4 12 hours, 24 hours

Probability Calculation of Rainfall Intensity for the short duration
at the CSDB (unit: mm/hr) : No. 1

IWAI METHOD 5 min.

DATA N=5.
D(1)=242.4
D(2)=240.
D(3)=204.
D(4)=180.
D(5)=223.2.
RANKING & PLOTTING POSITION

P. OF EXCEEDANCE

RANK DATA WEIBULL PLOT%
(J) (X) J/(N+1) F=1-P
1. 242.4 16.7 83.3
2. 240. 33.3 66.7
3. 223.2 50. 50.
4. 204. 66.7 33.3
5. 180. 83.3 16.7

CALCULATION

SUM X= 1089.6
MEAN X= 217.92
SUM OF DEVIATION SQUARE
S=2746.368
VARIANCE S/N=549.27
S/(N-1)=686.592
SD/(MEAN X)=0.108
SD=J(S/N)=23.437
USD=J(S/(N-1))=26.203
SKEWNESS CFT. CS1=-0.491
6
UNBIASED S.C. CS1=-0.439
7

MEAN LOG(XI)=2.335668144
XG=216.6

CAL. OF B-VALUE

1. T=242.4. S=180.
B(1.)=-304.0333333

MEAN B=-304.03

USED B=0.

X0=216.6
LOG(X0+B)=2.33567
1/A=0.07643 SX=0.04825

IWAI FORMULA

LOG(Y+(0.))=2.33567
+0.07643*KSI(YR)

PROBABILITY IWAI

| | |
|--------|-------|
| Y(2) | 216.6 |
| Y(3) | 228.5 |
| Y(4) | 235.6 |
| Y(5) | 240.5 |
| Y(10) | 254.1 |
| Y(20) | 265.8 |
| Y(25) | 269.3 |
| Y(50) | 279.7 |
| Y(100) | 289.3 |

IWAI METHOD

10 min.

DATA N=5.
D(1)=180.
D(2)=180.
D(3)=150.
D(4)=120.
D(5)=180.
RANKING & PLOTTING POSITION

P. OF EXCEEDANCE

RANK DATA WEIBULL PLOT%
(J) (X) J/(N+1) F=1-P
1. 180. 16.7 83.3
2. 180. 33.3 66.7
3. 180. 50. 50.
4. 150. 66.7 33.3
5. 120. 83.3 16.7

CALCULATION

SUM X= 810.
MEAN X= 162.
SUM OF DEVIATION SQUARE
S=2880.
VARIANCE S/N=576.
S/(N-1)=720.
SD/(MEAN X)=0.148
SD=J(S/N)=24.
USD=J(S/(N-1))=26.833
SKEWNESS CFT. CS1=-0.843
8
UNBIASED S.C. CS1=-0.754
7

MEAN LOG(XI)=2.204218004
XG=160.04

CAL. OF B-VALUE

1. T=180. S=120.
B(1.)=-199.8407171

MEAN B=-199.84

USED B=0.
X0=160.04
LOG(X0+B)=2.20422
1/A=0.1101 SX=0.06957

IWAI FORMULA

LOG(Y+(0.))=2.20422
+0.1101*KSI(YR)

PROBABILITY IWAI

| | |
|--------|-------|
| Y(2) | 160. |
| Y(3) | 172.9 |
| Y(4) | 180.6 |
| Y(5) | 186.1 |
| Y(10) | 201.4 |
| Y(20) | 214.9 |
| Y(25) | 219. |
| Y(50) | 231.3 |
| Y(100) | 242.8 |

IWAI METHOD 15 min.

DATA N=5.
D(1)=180.
D(2)=160.
D(3)=156.
D(4)=126.
D(5)=160.
RANKING & PLOTTING POSITION

P. OF EXCEEDANCE

RANK DATA WEIBULL PLOT%
(J) (X) J/(N+1) F=1-P
1. 180. 16.7 83.3
2. 160. 33.3 66.7
3. 160. 50. 50.
4. 156. 66.7 33.3
5. 126. 83.3 16.7

CALCULATION

SUM X= 782.
MEAN X= 156.4
SUM OF DEVIATION SQUARE
S=1507.2
VARIANCE S/N=301.44
S/(N-1)=376.8
SD/(MEAN X)=0.111
SD=J(S/N)=17.362
USD=J(S/(N-1))=19.411
SKEWNESS CFT. CS1=-0.567
8
UNBIASED S.C. CS1=-0.507
8

MEAN LOG(XI)=2.191401522
XG=155.38

CAL. OF B-VALUE

1. T=180. S=126.
B(1.)=-307.3412605

MEAN B=-307.34

USED B=0.
X0=155.38
LOG(X0+B)=2.1914
1/A=0.07966 SX=0.05045

IWAI FORMULA

LOG(Y+(0.))=2.1914
+0.07966*KSI(YR)

PROBABILITY IWAI

| | |
|--------|-------|
| Y(2) | 155.4 |
| Y(3) | 164.3 |
| Y(4) | 169.6 |
| Y(5) | 173.3 |
| Y(10) | 183.5 |
| Y(20) | 192.3 |
| Y(25) | 195. |
| Y(50) | 202.8 |
| Y(100) | 210.1 |

Probability Calculation of Rainfall Intensity for the short duration
at the CSDB (unit: mm/hr) : No. 2

IWAI METHOD 30 min.

DATA N=5.
D(1)=121.2
D(2)=120.
D(3)=86.
D(4)=100.
D(5)=108.
RANKING & PLOTTING POSITION

P. OF EXCEEDANCE
RANK DATA WEIBULL PLOT%
(J) (X) J/(N+1) F=1-P
1. 121.2 16.7 83.3
2. 120. 33.3 66.7
3. 108. 50. 50.
4. 100. 66.7 33.3
5. 86. 83.3 16.7

CALCULATION
SUM X= 535.2
MEAN X= 107.04
SUM OF DEVIATION SQUARE
S=861.632
VARIANCE S/N=172.33
S/(N-1)=215.408
SD/(MEAN X)=0.123
SD=√(S/N)=13.127
USD=√(S/(N-1))=14.677
SKEWNESS CFT. CS1=-0.410
8
UNBIASED S.C. CS1=-0.367
4

MEAN LOG(XI)=2.026121214
XG=106.2

CAL. OF B-VALUE
1. T=121.2 S=86.
B(1.)=-164.4692308

MEAN B=-164.47

USED B=0.
X0=106.2
LOG(X0+B)=2.02612
1/A=0.08729 SX=0.05525

IWAI FORMULA
LOG(Y+(0.))=2.02612
+0.08729*KSI(YR)

PROBABILITY IWAI

| | |
|--------|-------|
| Y(2) | 106.2 |
| Y(3) | 112.9 |
| Y(4) | 116.9 |
| Y(5) | 119.7 |
| Y(10) | 127.4 |
| Y(20) | 134.2 |
| Y(25) | 136.2 |
| Y(50) | 142.2 |
| Y(100) | 147.8 |

IWAI METHOD 45 min.

DATA N=5.
D(1)=101.1
D(2)=90.7
D(3)=85.3
D(4)=74.7
D(5)=100.
RANKING & PLOTTING POSITION

P. OF EXCEEDANCE
RANK DATA WEIBULL PLOT%
(J) (X) J/(N+1) F=1-P
1. 101.1 16.7 83.3
2. 100. 33.3 66.7
3. 90.7 50. 50.
4. 85.3 66.7 33.3
5. 74.7 83.3 16.7

CALCULATION
SUM X= 451.8
MEAN X= 90.36
SUM OF DEVIATION SQUARE
S=479.232
VARIANCE S/N=95.85
S/(N-1)=119.808
SD/(MEAN X)=0.108
SD=√(S/N)=9.79
USD=√(S/(N-1))=10.946
SKEWNESS CFT. CS1=-0.391
2
UNBIASED S.C. CS1=-0.349
9

MEAN LOG(XI)=1.953325615
XG=89.81

CAL. OF B-VALUE
1. T=101.1 S=74.7
B(1.)=-134.4675654

MEAN B=-134.47

USED B=0.
X0=89.81
LOG(X0+B)=1.95333
1/A=0.07663 SX=0.04829

IWAI FORMULA
LOG(Y+(0.))=1.95333
+0.07663*KSI(YR)

PROBABILITY IWAI

| | |
|--------|-------|
| Y(2) | 89.8 |
| Y(3) | 94.8 |
| Y(4) | 97.7 |
| Y(5) | 99.8 |
| Y(10) | 105.4 |
| Y(20) | 110.3 |
| Y(25) | 111.7 |
| Y(50) | 116. |
| Y(100) | 120.1 |

IWAI METHOD 60 min.

DATA N=5.
D(1)=85.
D(2)=82.5
D(3)=67.
D(4)=71.
D(5)=82.
RANKING & PLOTTING POSITION

P. OF EXCEEDANCE
RANK DATA WEIBULL PLOT%
(J) (X) J/(N+1) F=1-P
1. 85. 16.7 83.3
2. 82.5 33.3 66.7
3. 82. 50. 50.
4. 71. 66.7 33.3
5. 67. 83.3 16.7

CALCULATION
SUM X= 387.5
MEAN X= 77.5
SUM OF DEVIATION SQUARE
S=254.
VARIANCE S/N=50.8
S/(N-1)=63.5
SD/(MEAN X)=0.092
SD=√(S/N)=7.127
USD=√(S/(N-1))=7.969
SKEWNESS CFT. CS1=-0.438
8
UNBIASED S.C. CS1=-0.392
5

MEAN LOG(XI)=1.887403976
XG=77.16

CAL. OF B-VALUE
1. T=85. S=67.
B(1.)=-111.4937931

MEAN B=-111.49

USED B=0.
X0=77.16
LOG(X0+B)=1.8874
1/A=0.06471 SX=0.04111

IWAI FORMULA
LOG(Y+(0.))=1.8874
+0.06471*KSI(YR)

PROBABILITY IWAI

| | |
|--------|------|
| Y(2) | 77.2 |
| Y(3) | 80.7 |
| Y(4) | 82.8 |
| Y(5) | 84.3 |
| Y(10) | 88.3 |
| Y(20) | 91.8 |
| Y(25) | 92.8 |
| Y(50) | 95.8 |
| Y(100) | 98.6 |

Probability Calculation of Rainfall Intensity for the short duration
at the CSDB (unit: mm/hr.) : No. 3

IWAI METHOD 2 hours

DATA N=5.
D(1)=45.
D(2)=52.3
D(3)=42.5
D(4)=37.
D(5)=45.6
RANKING & PLOTTING POSITION

P. OF EXCEEDANCE
RANK DATA WEIBULL PLOT%
(J) (X) J/(N+1) F=1-P
1. 52.3 16.7 83.3
2. 45.6 33.3 66.7
3. 45. 50. 50.
4. 42.5 66.7 33.3
5. 37. 83.3 16.7

CALCULATION

SUM X= 222.4
MEAN X= 44.48
SUM OF DEVIATION SQUARE
S=122.548
VARIANCE S/N=24.51
S/(N-1)=30.637
SD/(MEAN X)=0.111
SD=√(S/N)=4.951
USD=√(S/(N-1))=5.535
SKEWNESS CFT. CS!=0.0881
UNBIASED S.C. CS1=0.0788

MEAN LOG(XI)=1.64545394
XG=44.2

CAL. OF B-VALUE

1. T=52.3 S=37.
B(1.)=20.6

MEAN B=20.6

USED B=20.6
X0=44.29
LOG(X0+B)=1.81219
1/A=0.05234 SX=0.03301

IWAI FORMULA
LOG(Y+(20.6))=1.81219
+0.05234*KSI(YR)

PROBABILITY IWAI

| | |
|--------|------|
| Y(2) | 44.3 |
| Y(3) | 46.7 |
| Y(4) | 48.1 |
| Y(5) | 49.1 |
| Y(10) | 51.8 |
| Y(20) | 54.1 |
| Y(25) | 54.7 |
| Y(50) | 56.7 |
| Y(100) | 58.5 |

IWAI METHOD 3 hours

DATA N=5.
D(1)=31.3
D(2)=34.9
D(3)=29.3
D(4)=24.7
D(5)=31.4
RANKING & PLOTTING POSITION

P. OF EXCEEDANCE
RANK DATA WEIBULL PLOT%
(J) (X) J/(N+1) F=1-P
1. 34.9 16.7 83.3
2. 31.4 33.3 66.7
3. 31.3 50. 50.
4. 29.3 66.7 33.3
5. 24.7 83.3 16.7

CALCULATION

SUM X= 151.6
MEAN X= 30.32
SUM OF DEVIATION SQUARE
S=55.728
VARIANCE S/N=11.15
S/(N-1)=13.932
SD/(MEAN X)=0.11
SD=√(S/N)=3.339
USD=√(S/(N-1))=3.733
SKEWNESS CFT. CS!=0.431
4
UNBIASED S.C. CS1=-0.385
8

MEAN LOG(XI)=1.478972797
XG=30.13

CAL. OF B-VALUE

1. T=34.9 S=24.7
B(1.)=-69.37409091

MEAN B=-69.37

USED B=0.
X0=30.13
LOG(X0+B)=1.47897
1/A=0.07831 SX=0.04961

IWAI FORMULA
LOG(Y+(0.))=1.47897
+0.07831*KSI(YR)

PROBABILITY IWAI

| | |
|--------|------|
| Y(2) | 30.1 |
| Y(3) | 31.8 |
| Y(4) | 32.8 |
| Y(5) | 33.5 |
| Y(10) | 35.5 |
| Y(20) | 37.2 |
| Y(25) | 37.7 |
| Y(50) | 39.1 |
| Y(100) | 40.5 |

IWAI METHOD 6 hours

DATA N=5.
D(1)=14.7
D(2)=14.5
D(3)=17.1
D(4)=18.8
D(5)=21.6
RANKING & PLOTTING POSITION

P. OF EXCEEDANCE
RANK DATA WEIBULL PLOT%
(J) (X) J/(N+1) F=1-P
1. 21.6 16.7 83.3
2. 18.8 33.3 66.7
3. 17.1 50. 50.
4. 14.7 66.7 33.3
5. 14.5 83.3 16.7

CALCULATION

SUM X= 86.7
MEAN X= 17.34
SUM OF DEVIATION SQUARE
S=35.372
VARIANCE S/N=7.07
S/(N-1)=8.843
SD/(MEAN X)=0.153
SD=√(S/N)=2.66
USD=√(S/(N-1))=2.974
SKEWNESS CFT. CS1=0.4155
UNBIASED S.C. CS1=0.3716
MEAN LOG(XI)=1.234058609
XG=17.14

CAL. OF B-VALUE

1. T=21.6 S=14.5
B(1.)=-10.67054945

MEAN B=-10.67

USED B=0.

X0=17.14
LOG(X0+B)=1.23406
1/A=0.10351 SX=0.06544

IWAI FORMULA
LOG(Y+(0.))=1.23406
+0.10351*KSI(YR)

PROBABILITY IWAI

| | |
|--------|------|
| Y(2) | 17.1 |
| Y(3) | 19.4 |
| Y(4) | 19.2 |
| Y(5) | 19.8 |
| Y(10) | 21.3 |
| Y(20) | 22.6 |
| Y(25) | 23. |
| Y(50) | 24.2 |
| Y(100) | 25.4 |

Probability Calculation of Rainfall Intensity for the short duration
at the CSDB (unit: mm/hr) : No. 4

IWAI METHOD 12 hours

```
DATA N=5.
D(1)=7.3
D(2)=7.2
D(3)=8.8
D(4)=9.5
D(5)=18.9
RANKING & PLOTTING POSITION
```

P. OF EXCEEDANCE
RANK DATA WEIBULL PLOT%
(J) (X) J/(N+1) F=1-P
1. 18.9 16.7 83.3
2. 9.5 33.3 66.7
3. 8.8 50. 50.
4. 7.3 66.7 33.3
5. 7.2 83.3 16.7

CALCULATION
SUM X= 51.7
MEAN X= 10.34
SUM OF DEVIATION SQUARE
S=95.452
VARIANCE S/N=19.09
S/(N-1)=23.863
SD/(MEAN X)=0.423
SD=J(S/N)=4.369
USD=J(S/(N-1))=4.885
SKEWNESS CFT. CS!=1.3524
UNBIASED S.C. CS1=1.2096

MEAN LOG(XI)=9.838646874
E-01
XG=9.64

CAL. OF B-VALUE
1. T=18.9 S=7.2
B(1.)=-6.327038123

MEAN B=-6.33

USED B=0.
X0=9.64
LOG(X0+B)=0.98386
1/A=0.24263 SX=0.15349

IWAI FORMULA
LOG(Y+(0.))=0.98386
+0.24263*KSI(YR)

PROBABILITY IWAI

| | |
|--------|------|
| Y(2) | 9.6 |
| Y(3) | 11.4 |
| Y(4) | 12.6 |
| Y(5) | 13.4 |
| Y(10) | 16. |
| Y(20) | 18.5 |
| Y(25) | 19.2 |
| Y(50) | 21.7 |
| Y(100) | 24.2 |

IWAI METHOD

24 hours

```
DATA N=5.
D(1)=3.7
D(2)=3.6
D(3)=4.4
D(4)=4.7
D(5)=9.7
RANKING & PLOTTING POSITION
```

P. OF EXCEEDANCE
RANK DATA WEIBULL PLOT%
(J) (X) J/(N+1) F=1-P
1. 9.7 16.7 83.3
2. 4.7 33.3 66.7
3. 4.4 50. 50.
4. 3.7 66.7 33.3
5. 3.6 83.3 16.7

CALCULATION
SUM X= 26.1
MEAN X= 5.22
SUM OF DEVIATION SQUARE
S=25.948
VARIANCE S/N=5.19
S/(N-1)=6.487
SD/(MEAN X)=0.436
SD=J(S/N)=2.278
USD=J(S/(N-1))=2.547
SKEWNESS CFT. CS!=1.3782
UNBIASED S.C. CS1=1.2327

MEAN LOG(XI)=6.853652986
E-01
XG=4.85

CAL. OF B-VALUE
1. T=9.7 S=3.6
B(1.)=-3.165972222

MEAN B=-3.17

USED B=0.
X0=4.85
LOG(X0+B)=0.68537
1/A=0.24816 SX=0.15693

IWAI FORMULA
LOG(Y+(0.))=0.68537
+0.24816*KSI(YR)

PROBABILITY IWAI

| | |
|--------|------|
| Y(2) | 4.8 |
| Y(3) | 5.8 |
| Y(4) | 6.4 |
| Y(5) | 6.8 |
| Y(10) | 8.1 |
| Y(20) | 9.4 |
| Y(25) | 9.8 |
| Y(50) | 11.1 |
| Y(100) | 12.4 |

Table C1 - 16 The Longest Dry Consecutive Days During One Year
at The CSDB

GUMBEL MAX. DISTRIBUTION

DATA N=13.

| | | |
|--------|------|------|
| D(1)= | 23.0 | 1977 |
| D(2)= | 10.0 | 1978 |
| D(3)= | 19.0 | 1979 |
| D(4)= | 15.0 | 1980 |
| D(5)= | 15.0 | 1981 |
| D(6)= | 34.0 | 1982 |
| D(7)= | 20.0 | 1983 |
| D(8)= | 18.0 | 1984 |
| D(9)= | 9.0 | 1985 |
| D(10)= | 10.0 | 1986 |
| D(11)= | 25.0 | 1987 |
| D(12)= | 17.0 | 1989 |
| D(13)= | 21.0 | 1988 |

PROBABLE EXTREME VALUE(
XT), RETURN PERIOD(T),
FREQUENCY FUNCTION:

XT=X_M+K*S_X, X_M=MEAN X,
K=(Y_T-Y_N)/S_Y, Y_T=-LN(LNC
T/(T-1)))
Y_T=REDUCED VARIATE, Y_N=R
EDUCED MEAN
XT=X_M-(Y_N*S_X/S_Y)+(S_X/S_Y)
*Y_T

CAL. VALUE:

X_M=18.15384615 S_X=6.9
Y_N=0.507 S_Y=0.9971

ESTIMATE EQUATION:
XT=14.65+6.92Y_T

RANKING

I=1. X=34.
I=2. X=25.
I=3. X=23.
I=4. X=21.
I=5. X=20.
I=6. X=19.
I=7. X=18.
I=8. X=17.
I=9. X=15.
I=10. X=15.
I=11. X=10.
I=12. X=10.
I=13. X=9.

T=2. XT=17.2
T=4. XT=23.3
T=5. XT=25.
T=10. XT=30.2
T=20. XT=35.2
T=25. XT=36.8
T=50. XT=41.7
T=100. XT=46.5
T=200. XT=51.3
T=1000. XT=62.4

CALCULATION

SUM X= 236.
SUM X^2= 4856.
SUM X^3= 111440.

T=11. XT=30.9
T=12. XT=31.5
T=13. XT=32.1

MEAN X= 18.15384615
MEAN X^2= 373.5384615
MEAN X^3= 8572.307692
SUM DEV SQU. S=571.69230

T=14. XT=32.7
T=15. XT=33.2
T=16. XT=33.6
T=17. XT=34.

77
VARIANCE S/N=43.98
UNBIASED VARI. =S/(N-1)=

T=18. XT=34.5
T=19. XT=34.8
T=20. XT=35.2

47.64
VARIATION COEF.=S/X_M

X=0.37

STANDARD DEV. S_X= $\sqrt{S/N}$ =
6.63

STA. DEV. EST. USX= $\sqrt{S/(N-1)}$ =6.9

SKEWNESS COEF. CS1=0.667
UNBIASED S.C. CS1=0.641

Table C-17

**Calculation of Probability of Exceedance
on the Data of Monthly Mean Pan Evaporation
at the C S D B.**

- No.1 January, February and March
- No.2 April, May and June
- No.3 July, August and September
- No.4 October, November and December

Calculation of Probability of Exceedance

Monthly Mean Pan Evaporation : No. 1 January, February and March

IWAI METHOD

```

DATA N=13.
D(1)=2.22
D(2)=2.34
D(3)=2.92
D(4)=1.75
D(5)=1.69
D(6)=1.67
D(7)=2.49
D(8)=2.72
D(9)=3.01
D(10)=2.52
D(11)=2.28
D(12)=3.45
D(13)=3.56

```

P. OF EXCEEDANCE

RANK DATA WEIBULL PLOT%
(J) (X) J/(N+1) F=1-P
1. 3.56 7.1 92.9
2. 3.45 14.3 85.7
3. 3.01 21.4 78.6
4. 2.92 28.6 71.4
5. 2.72 35.7 64.3
6. 2.52 42.9 57.1
7. 2.49 50. 50.
8. 2.34 57.1 42.9
9. 2.28 64.3 35.7
10. 2.22 71.4 28.6
11. 1.75 78.6 21.4
12. 1.69 85.7 14.3
13. 1.67 92.9 7.1

CALCULATION

SUM X= 32.62
MEAN X= 2.509230769
SUM OF DEVIATION SQUARE
S=4.570292308
VARIANCE S/N=0.35
S/(N-1)=3.88576923E-01
SD/(MEAN X)=0.236
SD=J(S/N)=0.593
USD=J(S/(N-1))=0.617
SKEWNESS CFT. CS1=0.213
UNBIASED S.C. CS1=0.2046
MEAN LOG(XI)=3.871178565
E-01
XG=2.44

CAL. OF B-VALUE

1. T=3.56 S=1.67
B(1.)=0.024

MEAN B=0.02

USED B=0.02

X0=2.44
LOG(X0+B)=0.39077
1/A=0.15293 SX=0.10389

IWAI FORMULA
LOG(Y+(0.02))=0.39077
+0.15293*KSI(YR)

PROBABILITY IWAI

| | |
|--------|-----|
| Y(2) | 2.4 |
| Y(3) | 2.7 |
| Y(4) | 2.9 |
| Y(5) | 3. |
| Y(10) | 3.4 |
| Y(20) | 3.7 |
| Y(25) | 3.8 |
| Y(50) | 4.1 |
| Y(100) | 4.4 |

IWAI METHOD

```

DATA N=13.
D(1)=1.94
D(2)=3.2
D(3)=3.12
D(4)=2.34
D(5)=2.71
D(6)=2.76
D(7)=2.94
D(8)=2.84
D(9)=3.44
D(10)=3.24
D(11)=2.78
D(12)=4.27
D(13)=2.56

```

RANKING & PLOTTING POSITION

P. OF EXCEEDANCE
RANK DATA WEIBULL PLOT%
(J) (X) J/(N+1) F=1-P
1. 4.27 7.1 92.9
2. 3.44 14.3 85.7
3. 3.24 21.4 78.6
4. 3.2 28.6 71.4
5. 3.12 35.7 64.3
6. 2.94 42.9 57.1
7. 2.84 50. 50.
8. 2.78 57.1 42.9
9. 2.76 64.3 35.7
10. 2.71 71.4 28.6
11. 2.56 78.6 21.4
12. 2.34 85.7 14.3
13. 1.94 92.9 7.1

CALCULATION

SUM X= 38.14
MEAN X= 2.933846154
SUM OF DEVIATION SQUARE
S=3.833707693
VARIANCE S/N=0.29
S/(N-1)=3.194756411E-01
SD/(MEAN X)=0.185
SD=J(S/N)=0.543
USD=J(S/(N-1))=0.565
SKEWNESS CFT. CS1=0.6269
UNBIASED S.C. CS1=0.6023

MEAN LOG(XI)=0.460129407
XG=2.88

CAL. OF B-VALUE

1. T=4.27 S=1.94
B(1.)=2.355555556E-02

MEAN B=0.02

USED B=0.02
X0=2.89
LOG(X0+B)=0.46318
1/A=0.11658 SX=0.0792

IWAI FORMULA
LOG(Y+(0.02))=0.46318
+0.11658*KSI(YR)

PROBABILITY IWAI

| | |
|--------|-----|
| Y(2) | 2.9 |
| Y(3) | 3.1 |
| Y(4) | 3.3 |
| Y(5) | 3.4 |
| Y(10) | 3.7 |
| Y(20) | 3.9 |
| Y(25) | 4. |
| Y(50) | 4.3 |
| Y(100) | 4.5 |

IWAI METHOD

```

DATA N=13.
D(1)=1.69
D(2)=2.76
D(3)=2.97
D(4)=2.87
D(5)=2.99
D(6)=2.87
D(7)=3.12
D(8)=2.95
D(9)=3.72
D(10)=2.93
D(11)=3.63
D(12)=3.75
D(13)=3.89

```

RANKING & PLOTTING POSITION

P. OF EXCEEDANCE
RANK DATA WEIBULL PLOT%
(J) (X) J/(N+1) F=1-P
1. 3.89 7.1 92.9
2. 3.75 14.3 85.7
3. 3.72 21.4 78.6
4. 3.63 28.6 71.4
5. 3.12 35.7 64.3
6. 2.99 42.9 57.1
7. 2.97 50. 50.
8. 2.95 57.1 42.9
9. 2.93 64.3 35.7
10. 2.87 71.4 28.6
11. 2.87 78.6 21.4
12. 2.76 85.7 14.3
13. 1.69 92.9 7.1

CALCULATION

SUM X= 40.14
MEAN X= 3.087692308
SUM OF DEVIATION SQUARE
S=4.00023077
VARIANCE S/N=0.31
S/(N-1)=3.333525642E-01
SD/(MEAN X)=0.18
SD=J(S/N)=0.555
USD=J(S/(N-1))=0.577
SKEWNESS CFT. CS1=-0.709
2
UNBIASED S.C. CS1=-0.681
4

MEAN LOG(XI)=4.814047602
E-01
XG=3.03

CAL. OF B-VALUE

1. T=3.89 S=1.69
B(1.)=-5.430833335

MEAN B=-5.43

USED B=0.
X0=3.03
LOG(X0+B)=0.4814
1/A=0.13045 SX=0.08865

IWAI FORMULA
LOG(Y+(0.02))=0.4814
+0.13045*KSI(YR)

PROBABILITY IWAI

| | |
|--------|-----|
| Y(2) | 3. |
| Y(3) | 3.3 |
| Y(4) | 3.4 |
| Y(5) | 3.7 |
| Y(10) | 3.9 |
| Y(20) | 4. |
| Y(25) | 4.3 |
| Y(50) | 4.4 |
| Y(100) | 5. |

Calculation of Probability of Exceedance
Monthly Mean Pan Evaporation : No.2 April, May and June

| IWAI METHOD | APR | MAY |
|-----------------------------|-----------------------------|-----------------------------|
| DATA N=13. | DATA N=13. | DATA N=13. |
| D(1)=2.75 | D(1)=3.06 | D(1)=2.24 |
| D(2)=3.26 | D(2)=2.92 | D(2)=2.49 |
| D(3)=3.08 | D(3)=3.02 | D(3)=2.66 |
| D(4)=2.25 | D(4)=2.62 | D(4)=2.91 |
| D(5)=3.02 | D(5)=2.75 | D(5)=2.72 |
| D(6)=2.63 | D(6)=2.73 | D(6)=2.4 |
| D(7)=3.26 | D(7)=3. | D(7)=3.4 |
| D(8)=3.1 | D(8)=2.83 | D(8)=3.16 |
| D(9)=3.25 | D(9)=3.19 | D(9)=2.81 |
| D(10)=3.35 | D(10)=3.78 | D(10)=3.28 |
| D(11)=3.47 | D(11)=4.1 | D(11)=3.69 |
| D(12)=4.34 | D(12)=3.77 | D(12)=3.4 |
| D(13)=4.17 | D(13)=3.47 | D(13)=3.58 |
| RANKING & PLOTTING POSITION | RANKING & PLOTTING POSITION | RANKING & PLOTTING POSITION |
| P. OF EXCEEDANCE | P. OF EXCEEDANCE | P. OF EXCEEDANCE |
| RANK DATA WEIBULL PLOT% | RANK DATA WEIBULL PLOT% | RANK DATA WEIBULL PLOT% |
| (J) (X) J/(N+1) F=1-P | (J) (X) J/(N+1) F=1-P | (J) (X) J/(N+1) F=1-P |
| 1. 4.34 7.1 92.9 | 1. 4.1 7.1 92.9 | 1. 3.69 7.1 92.9 |
| 2. 4.17 14.3 85.7 | 2. 3.78 14.3 85.7 | 2. 3.58 14.3 85.7 |
| 3. 3.47 21.4 78.6 | 3. 3.77 21.4 78.6 | 3. 3.4 21.4 78.6 |
| 4. 3.35 28.6 71.4 | 4. 3.47 28.6 71.4 | 4. 3.4 28.6 71.4 |
| 5. 3.26 35.7 64.3 | 5. 3.19 35.7 64.3 | 5. 3.28 35.7 64.3 |
| 6. 3.26 42.9 57.1 | 6. 3.06 42.9 57.1 | 6. 3.16 42.9 57.1 |
| 7. 3.25 50. 50. | 7. 3.02 50. 50. | 7. 2.91 50. 50. |
| 8. 3.1 57.1 42.9 | 8. 3. 57.1 42.9 | 8. 2.81 57.1 42.9 |
| 9. 3.08 64.3 35.7 | 9. 2.92 64.3 35.7 | 9. 2.72 64.3 35.7 |
| 10. 3.02 71.4 28.6 | 10. 2.83 71.4 28.6 | 10. 2.66 71.4 28.6 |
| 11. 2.75 78.6 21.4 | 11. 2.75 78.6 21.4 | 11. 2.49 78.6 21.4 |
| 12. 2.63 85.7 14.3 | 12. 2.73 85.7 14.3 | 12. 2.4 85.7 14.3 |
| 13. 2.25 92.9 7.1 | 13. 2.62 92.9 7.1 | 13. 2.24 92.9 7.1 |
| CALCULATION | | |
| SUM X= 41.93 | SUM X= 41.24 | SUM X= 38.74 |
| MEAN X= 3.225384615 | MEAN X= 3.172307692 | MEAN X= 2.98 |
| SUM OF DEVIATION SQUARE | SUM OF DEVIATION SQUARE | SUM OF DEVIATION SQUARE |
| S=3.823923077 | S=2.60143077 | S=2.6672 |
| VARIANCE S/N=0.29 | VARIANCE S/N=0.2 | VARIANCE S/N=0.21 |
| S/(N-1)=3.1866025564E-01 | S/(N-1)=2.167858975E-01 | S/(N-1)=2.222666667E-01 |
| SD/(MEAN X)=0.168 | SD/(MEAN X)=0.141 | SD/(MEAN X)=0.152 |
| SD=f(S/N)=0.542 | SD=f(S/N)=0.447 | SD=f(S/N)=0.453 |
| USD=f(S/(N-1))=0.565 | USD=f(S/(N-1))=0.466 | USD=f(S/(N-1))=0.471 |
| SKEWNESS CFT. CS!=0.4755 | SKEWNESS CFT. CS!=0.746 | SKEWNESS CFT. CS!=0.015 |
| UNBIASED S.C. CS1=0.4568 | UNBIASED S.C. CS1=0.7167 | 4 |
| MEAN LOG(XI)=5.025160724 | MEAN LOG(XI)=4.972732852 | UNBIASED S.C. CS1=-0.014 |
| E-01 | E-01 | 8 |
| XG=5.18 | XG=3.14 | MEAN LOG(XI)=4.690874316 |
| CAL. OF B-VALUE | CAL. OF B-VALUE | E-01 |
| 1. T=4.34 S=2.25 | 1. T=4.1 S=2.62 | XG=2.95 |
| B(1.)=1.510434783 | B(1.)=-2.005454545 | CAL. OF B-VALUE |
| MEAN B=1.51 | MEAN B=-2.01 | 1. T=3.69 S=2.24 |
| USED B=1.51 | USED B=-2.01 | B(1.)=14.563333333 |
| X0=3.19 | X0=3.09 | MEAN B=14.56 |
| LOG(X0+B)=0.67256 | LOG(X0+B)=0.03506 | USED B=14.56 |
| 1/A=0.07238 SX=0.04911 | 1/A=0.23579 SX=0.16019 | X0=2.97 |
| IWAI FORMULA | IWAI FORMULA | LOG(X0+B)=1.24388 |
| LOG(Y+(1.51))=0.67256 | LOG(Y+(-2.01))=0.03506 | 1/A=0.01652 SX=0.01173 |
| +0.07238*KSI(YR) | +0.23579*KSI(YR) | IWAI FORMULA |
| PROBABILITY IWAI | PROBABILITY IWAI | LOG(Y+(14.56))=1.24388 |
| Y(2) 3.2 | Y(2) 3.1 | +0.01652*KSI(YR) |
| Y(3) 3.4 | Y(3) 3.3 | PROBABILITY IWAI |
| Y(4) 3.6 | Y(4) 3.4 | Y(2) 3. |
| Y(5) 3.7 | Y(5) 3.5 | Y(3) 3.2 |
| Y(10) 4. | Y(10) 3.8 | Y(4) 3.3 |
| Y(20) 4.2 | Y(20) 4. | Y(5) 3.4 |
| Y(25) 4.3 | Y(25) 4.1 | Y(10) 3.6 |
| Y(50) 4.5 | Y(50) 4.4 | Y(20) 3.8 |
| Y(100) 4.7 | Y(100) 4.7 | Y(25) 3.8 |
| | | Y(50) 4. |
| | | Y(100) 4.1 |

Calculation of Probability of Exceedance
Monthly Mean Pan Evaporation : No. 3 July, August and September

IWAI METHOD

```

DATA N=13.
D(1)=3.2
D(2)=2.76
D(3)=3.06
D(4)=2.98
D(5)=2.79
D(6)=2.7
D(7)=3.4
D(8)=3.26
D(9)=2.7
D(10)=3.41
D(11)=4.02
D(12)=3.96
D(13)=3.89
RANKING & PLOTTING POSITION

```

P. OF EXCEEDANCE

| RANK DATA WEIBULL PLOT% | | |
|-------------------------|------|---------------|
| (J) | (X) | J/(N+1) F=1-P |
| 1. | 4.02 | 7.1 92.9 |
| 2. | 3.96 | 14.3 85.7 |
| 3. | 3.89 | 21.4 78.6 |
| 4. | 3.41 | 28.6 71.4 |
| 5. | 3.4 | 35.7 64.3 |
| 6. | 3.26 | 42.9 57.1 |
| 7. | 3.2 | 50. 50. |
| 8. | 3.06 | 57.1 42.9 |
| 9. | 2.98 | 64.3 35.7 |
| 10. | 2.79 | 71.4 28.6 |
| 11. | 2.76 | 78.6 21.4 |
| 12. | 2.7 | 85.7 14.3 |
| 13. | 2.7 | 92.9 7.1 |

CALCULATION

```

SUM X= 42.13
MEAN X= 3.240769231
SUM OF DEVIATION SQUARE
S=2.721892308
VARIANCE S/N=0.21
S/(N-1)=0.226824359
SD/(MEAN X)=0.141
SD=f(S/N)=0.458
USD=f(S/(N-1))=0.476
SKEWNESS CFT. CS!=0.4684
UNBIASED S.C. CS1=0.4501

```

```

MEAN LOG(XI)=5.064346321
E-01
XG=3.21

```

```

CAL. OF B-VALUE
1. T=4.02 S=2.7
B(1.)=-1.833

```

MEAN B=-1.83

```

USED B=0.
X0=3.21
LOG(X0+B)=0.50643
1/A=0.08847 SX=0.06015

```

```

IWAI FORMULA
LOG(Y+(-0.))=0.50643
+0.08847*KSI(YR)

```

| PROBABILITY IWAI | |
|------------------|-----|
| Y(2) | 3.5 |
| Y(3) | 3.2 |
| Y(4) | 3.4 |
| Y(5) | 3.5 |
| Y(6) | 3.6 |
| Y(10) | 3.9 |
| Y(20) | 4.1 |
| Y(25) | 4.1 |
| Y(50) | 4.3 |
| Y(100) | 4.5 |

IWAI METHOD

```

DATA N=13.
D(1)=3.63
D(2)=2.86
D(3)=3.03
D(4)=2.92
D(5)=2.68
D(6)=3.09
D(7)=4.05
D(8)=3.7
D(9)=3.79
D(10)=3.65
D(11)=4.99
D(12)=4.12
D(13)=4.39
RANKING & PLOTTING POSITION

```

P. OF EXCEEDANCE

| RANK DATA WEIBULL PLOT% | | |
|-------------------------|------|---------------|
| (J) | (X) | J/(N+1) F=1-P |
| 1. | 4.99 | 7.1 92.9 |
| 2. | 4.39 | 14.3 85.7 |
| 3. | 4.12 | 21.4 78.6 |
| 4. | 4.05 | 28.6 71.4 |
| 5. | 3.79 | 35.7 64.3 |
| 6. | 3.7 | 42.9 57.1 |
| 7. | 3.65 | 50. 50. |
| 8. | 3.63 | 57.1 42.9 |
| 9. | 3.09 | 64.3 35.7 |
| 10. | 3.03 | 71.4 28.6 |
| 11. | 2.92 | 78.6 21.4 |
| 12. | 2.86 | 85.7 14.3 |
| 13. | 2.68 | 92.9 7.1 |

CALCULATION

```

SUM X= 46.9
MEAN X= 3.607692308
SUM OF DEVIATION SQUARE
S=5.51923077
VARIANCE S/N=0.42
S/(N-1)=4.599358975E-01
SD/(MEAN X)=0.181
SD=f(S/N)=0.652
USD=f(S/(N-1))=0.678
SKEWNESS CFT. CS!=0.4093
UNBIASED S.C. CS1=0.3933

```

```

MEAN LOG(XI)=5.502494242
E-01
XG=3.55

```

CAL. OF B-VALUE

```

1. T=4.99 S=2.68
B(1.)=-1.352105263

```

MEAN B=-1.35

```

USED B=-1.35
X0=3.51
LOG(X0+B)=0.33543
1/A=0.18634 SX=0.12658

```

IWAI FORMULA

```

LOG(Y+(-1.35))=0.33543
+0.18634*KSI(YR)

```

PROBABILITY IWAI

| Y(2) | 3.5 |
|--------|-----|
| Y(3) | 3.8 |
| Y(4) | 4. |
| Y(5) | 4.1 |
| Y(10) | 4.5 |
| Y(20) | 4.9 |
| Y(25) | 5. |
| Y(50) | 5.4 |
| Y(100) | 5.7 |

IWAI METHOD

```

DATA N=13.
D(1)=3.68
D(2)=3.3
D(3)=3.24
D(4)=3.2
D(5)=2.84
D(6)=3.85
D(7)=4.67
D(8)=3.25
D(9)=4.11
D(10)=3.5
D(11)=5.37
D(12)=4.89
D(13)=4.29
RANKING & PLOTTING POSITION

```

P. OF EXCEEDANCE

| RANK DATA WEIBULL PLOT% | | |
|-------------------------|------|---------------|
| (J) | (X) | J/(N+1) F=1-P |
| 1. | 5.37 | 7.1 92.9 |
| 2. | 4.89 | 14.3 85.7 |
| 3. | 4.67 | 21.4 78.6 |
| 4. | 4.29 | 28.6 71.4 |
| 5. | 4.11 | 35.7 64.3 |
| 6. | 3.85 | 42.9 57.1 |
| 7. | 3.68 | 50. 50. |
| 8. | 3.5 | 57.1 42.9 |
| 9. | 3.3 | 64.3 35.7 |
| 10. | 3.25 | 71.4 28.6 |
| 11. | 3.24 | 78.6 21.4 |
| 12. | 3.2 | 85.7 14.3 |
| 13. | 2.84 | 92.9 7.1 |

CALCULATION

```

SUM X= 50.19
MEAN X= 3.860769231
SUM OF DEVIATION SQUARE
S=6.952692308
VARIANCE S/N=0.53
S/(N-1)=5.793910257E-01
SD/(MEAN X)=0.189
SD=f(S/N)=0.731
USD=f(S/(N-1))=0.761
SKEWNESS CFT. CS!=0.6113
UNBIASED S.C. CS1=0.5873

```

```

MEAN LOG(XI)=5.792066432
E-01
XG=3.79

```

CAL. OF B-VALUE

```

1. T=5.37 S=2.84
B(1.)=-1.407460317

```

MEAN B=-1.41

```

USED B=-1.41
X0=3.76
LOG(X0+B)=0.37067
1/A=0.18606 SX=0.12641

```

IWAI FORMULA

```

LOG(Y+(-1.41))=0.37067
+0.18606*KSI(YR)

```

PROBABILITY IWAI

| Y(2) | 3.8 |
|--------|-----|
| Y(3) | 4.1 |
| Y(4) | 4.3 |
| Y(5) | 4.4 |
| Y(10) | 4.9 |
| Y(20) | 5.3 |
| Y(25) | 5.4 |
| Y(50) | 5.8 |
| Y(100) | 6.2 |

Calculation of Probability of Exceedance
Monthly Mean Pan Evaporation : No.4 October, November and December

IWAI METHOD $\alpha_i \cdot 10^3$

| | | | | | | | | | | | | | |
|-----------------------------|-----------|----------|-----------|-----------|-----------|-----------|-----------|-----------|----------|------------|-----------|------------|------------|
| DATA N=13. | D(1)=4.23 | D(2)=3.7 | D(3)=3.57 | D(4)=3.13 | D(5)=3.16 | D(6)=3.74 | D(7)=3.64 | D(8)=3.86 | D(9)=3.6 | D(10)=4.11 | D(11)=5.1 | D(12)=4.49 | D(13)=4.36 |
| RANKING & PLOTTING POSITION | | | | | | | | | | | | | |

P. OF EXCEEDANCE

| RANK DATA WEIBULL PLOT% | | |
|-------------------------|------|---------------|
| (J) | (X) | J/(N+1) F=1-P |
| 1. | 5.1 | 7.1 92.9 |
| 2. | 4.49 | 14.3 85.7 |
| 3. | 4.36 | 21.4 78.6 |
| 4. | 4.23 | 28.6 71.4 |
| 5. | 4.11 | 35.7 64.3 |
| 6. | 3.86 | 42.9 57.1 |
| 7. | 3.74 | 50. 50. |
| 8. | 3.7 | 57.1 42.9 |
| 9. | 3.64 | 64.3 35.7 |
| 10. | 3.6 | 71.4 28.6 |
| 11. | 3.57 | 78.6 21.4 |
| 12. | 3.16 | 85.7 14.3 |
| 13. | 3.13 | 92.9 7.1 |

CALCULATION

SUM X= 50.69
 MEAN X= 3.899230769
 SUM OF DEVIATION SQUARE
 $S=3.626892308$
 VARIANCE S/N=0.28
 $S/(N-1)=3.022410257E-01$
 $SD/\langle MEAN X\rangle=0.135$
 $SD=\sqrt{S/N}=0.528$
 $USD=\sqrt{S/(N-1)}=0.55$
 SKEWNESS CFT. CS!=0.5904
 UNBIASED S.C. CS1=0.5673

MEAN LOG(XI)=5.871114883
 E-01
 XG=3.86

CAL. OF B-VALUE
 1. T=5.1 S=5.13
 $B(1.)=-2.085098039$

MEAN B=-2.09

USED B=-2.09
 X0=3.82
 $LOG(X0+B)=0.23914$
 $1/A=0.18676$ SX=0.12688

IWAI FORMULA
 $LOG(Y+(-2.09))=0.23914$
 $+0.18676*KSI(YR)$

PROBABILITY IWAI
 $Y(2)$ 3.8
 $Y(3)$ 4.1
 $Y(4)$ 4.2
 $Y(5)$ 4.3
 $Y(10)$ 4.7
 $Y(20)$ 4.9
 $Y(25)$ 5.
 $Y(50)$ 5.5
 $Y(100)$ 5.6

IWAI METHOD $\alpha_i \cdot 10^3$

| | | | | | | | | | | | | | |
|-----------------------------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|------------|------------|------------|------------|
| DATA N=13. | D(1)=3.33 | D(2)=4.45 | D(3)=2.53 | D(4)=3.06 | D(5)=2.87 | D(6)=3.21 | D(7)=3.09 | D(8)=3.37 | D(9)=3.78 | D(10)=3.51 | D(11)=4.65 | D(12)=3.87 | D(13)=4.13 |
| RANKING & PLOTTING POSITION | | | | | | | | | | | | | |

P. OF EXCEEDANCE

| RANK DATA WEIBULL PLOT% | | |
|-------------------------|------|---------------|
| (J) | (X) | J/(N+1) F=1-P |
| 1. | 4.65 | 7.1 92.9 |
| 2. | 4.45 | 14.3 85.7 |
| 3. | 4.13 | 21.4 78.6 |
| 4. | 3.87 | 28.6 71.4 |
| 5. | 3.78 | 35.7 64.3 |
| 6. | 3.51 | 42.9 57.1 |
| 7. | 3.37 | 50. 50. |
| 8. | 3.33 | 57.1 42.9 |
| 9. | 3.21 | 64.3 35.7 |
| 10. | 3.09 | 71.4 28.6 |
| 11. | 3.06 | 78.6 21.4 |
| 12. | 2.87 | 85.7 14.3 |
| 13. | 2.53 | 92.9 7.1 |

CALCULATION

SUM X= 45.05
 MEAN X= 3.526923077
 SUM OF DEVIATION SQUARE
 $S=4.657276924$
 VARIANCE S/N=0.36
 $S/(N-1)=3.881064103E-01$
 $SD/\langle MEAN X\rangle=0.17$
 $SD=\sqrt{S/N}=0.599$
 $USD=\sqrt{S/(N-1)}=0.623$
 SKEWNESS CFT. CS!=0.3494
 UNBIASED S.C. CS1=0.3357

MEAN LOG(XI)=5.411949528
 E-01
 XG=3.48

CAL. OF B-VALUE
 1. T=4.65 S=2.53
 $B(1.)=1.572272727$

MEAN B=1.57

USED B=1.57
 X0=3.49
 $LOG(X0+B)=0.70435$
 $1/A=0.07442$ SX=0.05057

IWAI FORMULA
 $LOG(Y+(1.57))=0.70435$
 $+0.07442*KSI(YR)$

PROBABILITY IWAI
 $Y(2)$ 3.5
 $Y(3)$ 3.8
 $Y(4)$ 3.9
 $Y(5)$ 4.
 $Y(10)$ 4.3
 $Y(20)$ 4.6
 $Y(25)$ 4.7
 $Y(50)$ 4.9
 $Y(100)$ 5.1

IWAI METHOD $\alpha_i \cdot 10^3$

| | | | | | | | | | | | | | |
|-----------------------------|-----------|----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|------------|------------|------------|
| DATA N=13. | D(1)=2.81 | D(2)=3.3 | D(3)=2.32 | D(4)=2.31 | D(5)=2.86 | D(6)=2.63 | D(7)=3.67 | D(8)=3.02 | D(9)=3.86 | D(10)=3.8 | D(11)=3.39 | D(12)=3.36 | D(13)=3.28 |
| RANKING & PLOTTING POSITION | | | | | | | | | | | | | |

P. OF EXCEEDANCE

| RANK DATA WEIBULL PLOT% | | |
|-------------------------|------|---------------|
| (J) | (X) | J/(N+1) F=1-P |
| 1. | 3.86 | 7.1 92.9 |
| 2. | 3.8 | 14.3 85.7 |
| 3. | 3.67 | 21.4 78.6 |
| 4. | 3.39 | 28.6 71.4 |
| 5. | 3.36 | 35.7 64.3 |
| 6. | 3.3 | 42.9 57.1 |
| 7. | 3.28 | 50. 50. |
| 8. | 3.02 | 57.1 42.9 |
| 9. | 2.86 | 64.3 35.7 |
| 10. | 2.81 | 71.4 28.6 |
| 11. | 2.63 | 78.6 21.4 |
| 12. | 2.32 | 85.7 14.3 |
| 13. | 2.31 | 92.9 7.1 |

CALCULATION

SUM X= 40.61
 MEAN X= 3.123846154
 SUM OF DEVIATION SQUARE
 $S=3.210707693$
 VARIANCE S/N=0.25
 $S/(N-1)=2.675589744E-01$
 $SD/\langle MEAN X\rangle=0.159$
 $SD=\sqrt{S/N}=0.497$
 $USD=\sqrt{S/(N-1)}=0.517$
 SKEWNESS CFT. CS!=0.198
 UNBIASED S.C. CS1=-0.198

MEAN LOG(XI)=4.889306718
 E-01
 XG=3.08

CAL. OF B-VALUE
 1. T=3.86 S=2.31
 $B(1.)=56.98$

MEAN B=56.98

USED B=56.98
 X0=3.12
 $LOG(X0+B)=1.77989$
 $1/A=0.00529$ SX=0.00192

IWAI FORMULA
 $LOG(Y+56.98)=1.77989$
 $+0.00529*KSI(YR)$

PROBABILITY IWAI
 $Y(2)$ 3.1
 $Y(3)$ 3.3
 $Y(4)$ 3.5
 $Y(5)$ 4.
 $Y(10)$ 4.3
 $Y(20)$ 4.6
 $Y(25)$ 4.7
 $Y(50)$ 4.9
 $Y(100)$ 5.1

Table C1-18

**Estimated Possible Working Hours of Outdoor Works for
Construction and Farming Practice**

No. 1 1985

No. 2 1986

No. 3 1987

No. 4 1988

No. 5 1989

No. 6 Recapitulation of Estimated Possible
Working Hours and their Percentage to the
Scheduled Construction Working Hours

No. 1 Estimated Possible Working Hours

Scheduled Daily Construction Working Hours : 10 hrs from 7:00 up to 17:00
 If rainfall is equal to or in excess of 0.25 mm per hour, outdoor works will be deferred.

Year : 1985

| Month Date | Jan. | Feb. | Mar. | Apr. | May | Jun. | Jul. | Aug. | Sep. | Oct. | Nov. | Dec. | Remarks |
|-------------|------|------|------|------|-----|------|------|------|------|------|------|------|---------|
| 1 | 10 | 10 | 9 | 8 | 10 | 10 | 10 | 10 | 7 | 10 | 10 | 10 | |
| 2 | 10 | 10 | 8 | 10 | 9 | 10 | 8 | 8 | 10 | 9 | 10 | 10 | |
| 3 | 9 | 10 | 9 | 9 | 10 | 9 | 8 | 10 | 10 | 10 | 7 | 10 | |
| 4 | 10 | 10 | 8 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 8 | 9 | |
| 5 | 9 | 10 | 8 | 10 | 9 | 9 | 10 | 10 | 10 | 10 | 7 | 7 | |
| Sub-Total | 48 | 50 | 42 | 47 | 48 | 48 | 46 | 48 | 47 | 49 | 42 | 46 | |
| 6 | 9 | 9 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 8 | |
| 7 | 7 | 9 | 9 | 10 | 10 | 9 | 10 | 7 | 10 | 10 | 9 | 10 | |
| 8 | 8 | 8 | 9 | 10 | 9 | 9 | 10 | 10 | 9 | 10 | 10 | 10 | |
| 9 | 8 | 7 | 9 | 8 | 9 | 10 | 9 | 10 | 6 | 10 | 10 | 10 | |
| 10 | 10 | 9 | 10 | 7 | 10 | 9 | 10 | 10 | 10 | 8 | 9 | 10 | |
| Sub-Total | 42 | 42 | 47 | 45 | 48 | 47 | 49 | 47 | 45 | 48 | 48 | 48 | |
| 11 | 9 | 8 | 10 | 10 | 10 | 10 | 8 | 10 | 10 | 10 | 9 | 10 | |
| 12 | 5 | 8 | 10 | 10 | 7 | 9 | 10 | 10 | 10 | 10 | 10 | 10 | |
| 13 | 10 | 10 | 9 | 10 | 8 | 10 | 10 | 10 | 9 | 10 | 10 | 10 | |
| 14 | 10 | 10 | 10 | 8 | 8 | 10 | 7 | 10 | 10 | 7 | 10 | 10 | |
| 15 | 5 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | |
| Sub-Total | 39 | 46 | 49 | 48 | 43 | 49 | 45 | 50 | 49 | 47 | 49 | 50 | |
| 16 | 9 | 9 | 10 | 9 | 10 | 10 | 10 | 10 | 10 | 9 | 10 | 8 | |
| 17 | 10 | 10 | 8 | 9 | 10 | 10 | 9 | 10 | 9 | 7 | 10 | 10 | |
| 18 | 10 | 8 | 10 | 9 | 10 | 10 | 10 | 9 | 10 | 10 | 10 | 10 | |
| 19 | 8 | 10 | 10 | 9 | 10 | 10 | 10 | 10 | 10 | 7 | 7 | 10 | |
| 20 | 10 | 9 | 8 | 10 | 10 | 9 | 8 | 10 | 10 | 10 | 10 | 9 | |
| Sub-Total | 47 | 46 | 46 | 46 | 50 | 49 | 47 | 49 | 49 | 43 | 47 | 47 | |
| 21 | 8 | 10 | 10 | 10 | 10 | 10 | 7 | 10 | 10 | 10 | 10 | 8 | |
| 22 | 8 | 6 | 10 | 7 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | |
| 23 | 10 | 8 | 10 | 10 | 9 | 10 | 10 | 10 | 10 | 10 | 10 | 7 | |
| 24 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 9 | 9 | 10 | 9 | 10 | |
| 25 | 10 | 10 | 8 | 9 | 10 | 8 | 9 | 8 | 10 | 10 | 10 | 10 | |
| Sub-Total | 46 | 44 | 48 | 46 | 49 | 48 | 46 | 47 | 49 | 50 | 49 | 45 | |
| 26 | 9 | 10 | 8 | 7 | 7 | 10 | 10 | 10 | 7 | 8 | 7 | 10 | |
| 27 | 10 | 6 | 10 | 9 | 9 | 10 | 8 | 10 | 10 | 10 | 10 | 9 | |
| 28 | 10 | 7 | 10 | 10 | 5 | 9 | 8 | 10 | 8 | 4 | 8 | 7 | |
| 29 | 10 | - | 10 | 10 | 10 | 9 | 10 | 10 | 10 | 10 | 10 | 10 | |
| 30 | 9 | - | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 7 | 9 | 10 | |
| 31 | 10 | - | 7 | - | 10 | - | 10 | 10 | - | 10 | - | 10 | |
| Sub-Total | 58 | 23 | 55 | 46 | 51 | 48 | 56 | 60 | 45 | 49 | 44 | 56 | |
| Grand Total | 280 | 251 | 287 | 278 | 289 | 289 | 289 | 301 | 284 | 286 | 279 | 292 | |

No. 2 Estimated Possible Working Hours

Scheduled Daily Construction Working Hours : 10 hrs from 7:00 up to 17:00
 If rainfall is equal to or in excess of 0.25 mm per hour, outdoor works will be deferred.

Year : 1986

| Month Date | Jan. | Feb. | Mar. | Apr. | May | Jun. | Jul. | Aug. | Sep. | Oct. | Nov. | Dec. | Remarks |
|-------------|------|------|------|------|-----|------|------|------|------|------|------|------|---------|
| 1 | 10 | 8 | 7 | 5 | 10 | 9 | 10 | 10 | 10 | 10 | 9 | 10 | |
| 2 | 8 | 10 | 8 | 10 | 10 | 10 | 10 | 9 | 10 | 10 | 9 | 10 | |
| 3 | 10 | 10 | 8 | 10 | 10 | 10 | 10 | 10 | 9 | 8 | 9 | 10 | |
| 4 | 8 | 10 | 9 | 9 | 10 | 10 | 10 | 7 | 9 | 10 | 10 | 10 | |
| 5 | 10 | 8 | 9 | 9 | 10 | 8 | 10 | 10 | 10 | 7 | 6 | 10 | |
| Sub-Total | 46 | 46 | 41 | 43 | 50 | 47 | 50 | 46 | 48 | 45 | 43 | 50 | |
| 6 | 7 | 9 | 7 | 7 | 10 | 10 | 10 | 8 | 10 | 10 | 6 | 10 | |
| 7 | 7 | 10 | 6 | 10 | 10 | 10 | 10 | 10 | 9 | 10 | 9 | 10 | |
| 8 | 5 | 9 | 10 | 10 | 10 | 9 | 9 | 9 | 10 | 10 | 6 | 10 | |
| 9 | 10 | 10 | 10 | 8 | 9 | 10 | 10 | 10 | 9 | 10 | 9 | 10 | |
| 10 | 10 | 7 | 9 | 9 | 10 | 8 | 10 | 10 | 10 | 9 | 8 | 8 | |
| Sub-Total | 39 | 45 | 42 | 44 | 49 | 47 | 49 | 47 | 48 | 49 | 38 | 48 | |
| 11 | 9 | 8 | 8 | 7 | 10 | 8 | 10 | 10 | 9 | 10 | 8 | 10 | |
| 12 | 7 | 7 | 10 | 8 | 8 | 10 | 10 | 10 | 10 | 8 | 7 | 8 | |
| 13 | 6 | 10 | 10 | 9 | 10 | 10 | 10 | 9 | 10 | 9 | 10 | 10 | |
| 14 | 10 | 9 | 8 | 9 | 9 | 10 | 10 | 10 | 10 | 10 | 8 | 10 | |
| 15 | 8 | 10 | 6 | 9 | 9 | 7 | 10 | 10 | 9 | 10 | 10 | 8 | |
| Sub-Total | 40 | 44 | 42 | 42 | 46 | 45 | 50 | 49 | 48 | 47 | 43 | 46 | |
| 16 | 10 | 7 | 10 | 10 | 10 | 9 | 10 | 10 | 6 | 10 | 10 | 8 | |
| 17 | 8 | 10 | 7 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 9 | 5 | |
| 18 | 8 | 10 | 10 | 10 | 10 | 8 | 10 | 10 | 10 | 10 | 10 | 10 | |
| 19 | 7 | 10 | 9 | 8 | 10 | 10 | 10 | 10 | 10 | 10 | 9 | 8 | |
| 20 | 7 | 10 | 9 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 7 | 10 | |
| Sub-Total | 40 | 47 | 45 | 48 | 50 | 47 | 50 | 50 | 46 | 50 | 45 | 41 | |
| 21 | 7 | 10 | 8 | 8 | 10 | 10 | 10 | 10 | 10 | 10 | 8 | 9 | |
| 22 | 6 | 10 | 7 | 10 | 10 | 10 | 8 | 10 | 10 | 10 | 10 | 10 | |
| 23 | 8 | 10 | 7 | 10 | 10 | 10 | 10 | 10 | 7 | 10 | 9 | 10 | |
| 24 | 7 | NA | 10 | 10 | 10 | 10 | 10 | 9 | 10 | 10 | 10 | 10 | |
| 25 | 9 | NA | 10 | 10 | 10 | 10 | 10 | 9 | 9 | 10 | 10 | 8 | |
| Sub-Total | 37 | - | 42 | 48 | 50 | 50 | 48 | 48 | 46 | 50 | 47 | 47 | |
| 26 | 6 | NA | 10 | 10 | 10 | 10 | 10 | 10 | 8 | 6 | 10 | 8 | |
| 27 | 9 | NA | 10 | 10 | 10 | 10 | 8 | 10 | 10 | 4 | 7 | 10 | |
| 28 | 10 | NA | 8 | 10 | 10 | 10 | 10 | 10 | 10 | 6 | 8 | 7 | |
| 29 | 10 | - | 10 | 9 | 10 | 10 | 8 | 10 | 10 | 8 | 7 | 8 | |
| 30 | 10 | - | 8 | 10 | 9 | 10 | 10 | 10 | 10 | 8 | 10 | 7 | |
| 31 | 8 | - | 10 | - | 9 | - | 10 | 10 | - | 10 | - | 9 | |
| Sub-Total | 53 | - | 56 | 49 | 58 | 50 | 56 | 60 | 48 | 42 | 42 | 42 | |
| Grand Total | 255 | - | 268 | 274 | 303 | 286 | 303 | 300 | 284 | 283 | 258 | 274 | |

No. 3 Estimated Possible Working Hours

Scheduled Daily Construction Working Hours : 10 hrs from 7:00 up to 17:00

If rainfall is equal to or in excess of 0.25 mm per hour, outdoor works will be deferred.

Year : 1987

| Month Date | Jan. | Feb. | Mar. | Apr. | May | Jun. | Jul. | Aug. | Sep. | Oct. | Nov. | Dec. | Remarks |
|---------------|------|------|------|------|-----|------|------|------|------|------|------|------|---------|
| 1 | 9 | 10 | 10 | 10 | 8 | 9 | 10 | 10 | 10 | 9 | 10 | 10 | |
| 2 | 9 | 7 | 9 | 7 | 10 | 10 | 10 | 9 | 10 | 9 | 9 | 9 | |
| 3 | 5 | 10 | 6 | 10 | 10 | 10 | 10 | 10 | 9 | 10 | 8 | 8 | |
| 4 | 7 | 8 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 9 | 9 | |
| 5 | 7 | 9 | 9 | 10 | 8 | 8 | 10 | 10 | 9 | 10 | 10 | 9 | |
| Sub-Total | 37 | 44 | 44 | 47 | 46 | 47 | 50 | 49 | 48 | 48 | 46 | 45 | |
| 6 | 10 | 9 | 9 | 9 | 8 | 7 | 10 | 10 | 10 | 10 | 10 | 5 | |
| 7 | 9 | 7 | 10 | 10 | 10 | 8 | 10 | 10 | 10 | 10 | 8 | 6 | |
| 8 | 9 | 8 | 10 | 8 | 10 | 9 | 10 | 10 | 10 | 10 | 8 | 7 | |
| 9 | 9 | 4 | 10 | 7 | 10 | 10 | 8 | 10 | 10 | 10 | 8 | 8 | |
| 10 | 10 | 6 | 9 | 9 | 8 | 10 | 10 | 10 | 10 | 10 | 10 | 8 | |
| Sub-Total | 47 | 34 | 48 | 43 | 46 | 44 | 48 | 50 | 50 | 50 | 44 | 34 | |
| 11 | 10 | 7 | 10 | 10 | 7 | 10 | 10 | 10 | 10 | 10 | 10 | 6 | |
| 12 | 10 | 9 | 10 | 6 | 10 | 10 | 10 | 10 | 10 | 8 | 10 | 10 | |
| 13 | 10 | 10 | 10 | 9 | 9 | 10 | 10 | 10 | 10 | 10 | 9 | 10 | |
| 14 | 4 | 9 | 10 | 9 | 9 | 10 | 10 | 10 | 10 | 10 | 7 | 10 | |
| 15 | 7 | 10 | 9 | 8 | 8 | 10 | 10 | 10 | 10 | 10 | 7 | 8 | |
| Sub-Total | 41 | 45 | 49 | 42 | 43 | 50 | 50 | 50 | 50 | 48 | 43 | 44 | |
| 16 | 8 | 8 | 10 | 8 | 10 | 10 | 10 | 9 | 10 | 8 | 10 | | |
| 17 | 10 | 8 | 9 | 10 | 8 | 10 | 10 | 10 | 10 | 9 | 9 | 10 | |
| 18 | 7 | 6 | 7 | 10 | 8 | 10 | 10 | 10 | 10 | 10 | 10 | 8 | |
| 19 | 8 | 10 | 9 | 10 | 10 | 10 | 10 | 10 | 10 | 9 | 9 | 9 | |
| 20 | 9 | 9 | 8 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 8 | |
| Sub-Total | 42 | 43 | 43 | 48 | 46 | 50 | 50 | 49 | 48 | 46 | 45 | | |
| 21 | 10 | 10 | 8 | 10 | 10 | 10 | 10 | 9 | 10 | 9 | 10 | 10 | |
| 22 | 7 | 7 | 9 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 8 | 10 | |
| 23 | 10 | 7 | 9 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 9 | |
| 24 | 7 | 8 | 8 | 9 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 4 | |
| 25 | 9 | 10 | 10 | 10 | 10 | 9 | 10 | 10 | 10 | 10 | 10 | 10 | |
| Sub-Total | 43 | 42 | 44 | 49 | 50 | 49 | 50 | 49 | 50 | 49 | 48 | 43 | |
| 26 | 9 | 7 | 10 | 10 | 9 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | |
| 27 | 5 | 7 | 9 | 10 | 10 | 10 | 10 | 10 | 8 | 10 | 10 | 10 | |
| 28 | 10 | 10 | 6 | 10 | 9 | 8 | 10 | 9 | 10 | 9 | 10 | 10 | |
| 29 | 10 | - | 7 | 10 | 10 | 9 | 10 | 10 | 10 | 10 | 10 | 8 | |
| 30 | 8 | - | 8 | 10 | 8 | 10 | 10 | 10 | 9 | 9 | 8 | 10 | |
| 31 | 9 | - | 10 | - | 10 | - | 10 | 10 | - | 10 | - | 10 | |
| Sub-Total | 51 | 24 | 50 | 50 | 56 | 47 | 60 | 59 | 47 | 58 | 48 | 58 | |
| Grand Total | 261 | 232 | 278 | 279 | 287 | 287 | 308 | 307 | 294 | 301 | 275 | 269 | |

No. 4 Estimated Possible Working Hours

Scheduled Daily Construction Working Hours : 10 hrs from 7:00 up to 17:00

If rainfall is equal to or in excess of 0.25 mm per hour, outdoor works will be deferred.

Year : 1988

| Month Date | Jan. | Feb. | Mar. | Apr. | May | Jun. | Jul. | Aug. | Sep. | Oct. | Nov. | Dec. | Remarks |
|-------------|------|------|------|------|-----|------|------|------|------|------|------|------|---------|
| 1 | 10 | 10 | 9 | 8 | 10 | 10 | 10 | 10 | 9 | 10 | 7 | 9 | |
| 2 | 10 | 6 | 10 | 7 | 10 | 10 | 10 | 10 | 10 | 9 | 8 | 10 | |
| 3 | 9 | 10 | 10 | 8 | 7 | 9 | 10 | 10 | 10 | 10 | 10 | 7 | |
| 4 | 10 | 9 | 8 | 10 | 8 | 10 | 8 | 10 | 10 | 9 | 8 | 9 | |
| 5 | 10 | 6 | 8 | 10 | 10 | 10 | 10 | 8 | 10 | 10 | 9 | 10 | |
| Sub-Total | 49 | 41 | 45 | 43 | 45 | 49 | 48 | 48 | 49 | 48 | 42 | 45 | |
| 6 | 10 | 3 | 9 | 10 | 10 | 10 | 10 | 9 | 10 | 10 | 10 | 10 | |
| 7 | 7 | 10 | 10 | 8 | 10 | 10 | 10 | 10 | 10 | 10 | 8 | 9 | |
| 8 | 10 | 10 | 10 | 10 | 10 | 7 | 10 | 10 | 9 | 10 | 9 | 9 | |
| 9 | 9 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 9 | 10 | 6 | |
| 10 | 10 | 10 | 7 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | |
| Sub-Total | 46 | 43 | 46 | 48 | 50 | 47 | 50 | 49 | 49 | 49 | 47 | 44 | |
| 11 | 10 | 10 | 10 | 10 | 10 | 9 | 10 | 10 | 10 | 7 | 8 | 8 | |
| 12 | 10 | 8 | 9 | 8 | 10 | 10 | 10 | 10 | 9 | 10 | 9 | 8 | |
| 13 | 10 | 7 | 10 | 10 | 6 | 10 | 10 | 10 | 10 | 10 | 7 | 6 | |
| 14 | 9 | 9 | 10 | 10 | 8 | 10 | 10 | 10 | 9 | 10 | 9 | 8 | |
| 15 | 6 | 8 | 8 | 10 | 6 | 10 | 10 | 9 | 10 | 9 | 10 | 7 | |
| Sub-Total | 45 | 42 | 47 | 48 | 40 | 49 | 50 | 49 | 48 | 46 | 43 | 37 | |
| 16 | 10 | 7 | 9 | 10 | 10 | 10 | 6 | 10 | 10 | 10 | 10 | 9 | |
| 17 | 8 | 8 | 10 | 10 | 8 | 10 | 10 | 10 | 9 | 8 | 10 | 4 | |
| 18 | 8 | 10 | 9 | 10 | 10 | 10 | 10 | 10 | 10 | 8 | 10 | 4 | |
| 19 | 8 | 8 | 10 | 10 | 8 | 8 | 10 | 10 | 10 | 8 | 10 | 4 | |
| 20 | 9 | 9 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 9 | 10 | 4 | |
| Sub-Total | 43 | 42 | 48 | 50 | 46 | 48 | 46 | 50 | 49 | 43 | 50 | 25 | |
| 21 | 9 | 10 | 6 | 9 | 10 | 10 | 10 | 9 | 10 | 10 | 10 | 6 | |
| 22 | 10 | 10 | 7 | 10 | 10 | 10 | 10 | 10 | 9 | 10 | 10 | 10 | |
| 23 | 9 | 10 | 7 | 10 | 10 | 10 | 9 | 10 | 10 | 5 | 9 | 10 | |
| 24 | 10 | 8 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 9 | 10 | |
| 25 | 7 | 10 | 8 | 10 | 10 | 10 | 10 | 10 | 9 | 10 | 10 | 10 | |
| Sub-Total | 45 | 48 | 38 | 49 | 50 | 50 | 49 | 49 | 48 | 45 | 48 | 46 | |
| 26 | 8 | 9 | 6 | 10 | 9 | 10 | 10 | 10 | 9 | 10 | 6 | 10 | |
| 27 | 7 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 8 | 10 | 9 | 8 | |
| 28 | 10 | 10 | 8 | 10 | 10 | 10 | 10 | 10 | 9 | 10 | 9 | 10 | |
| 29 | 10 | 10 | 6 | 7 | 9 | 10 | 10 | 10 | 9 | 6 | 9 | 10 | |
| 30 | 9 | - | 4 | 8 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 8 | |
| 31 | 10 | - | 10 | - | 10 | - | 10 | 10 | - | 10 | - | 10 | |
| Sub-Total | 54 | 39 | 44 | 45 | 58 | 50 | 60 | 60 | 45 | 56 | 43 | 56 | |
| Grand Total | 282 | 255 | 268 | 283 | 289 | 293 | 303 | 305 | 288 | 287 | 273 | 253 | |

No. 5 Estimated Possible Working Hours

Scheduled Daily Construction Working Hours : 10 hrs from 7:00 up to 17:00

If rainfall is equal to or in excess of 0.25 mm per hour, outdoor works will be deferred.

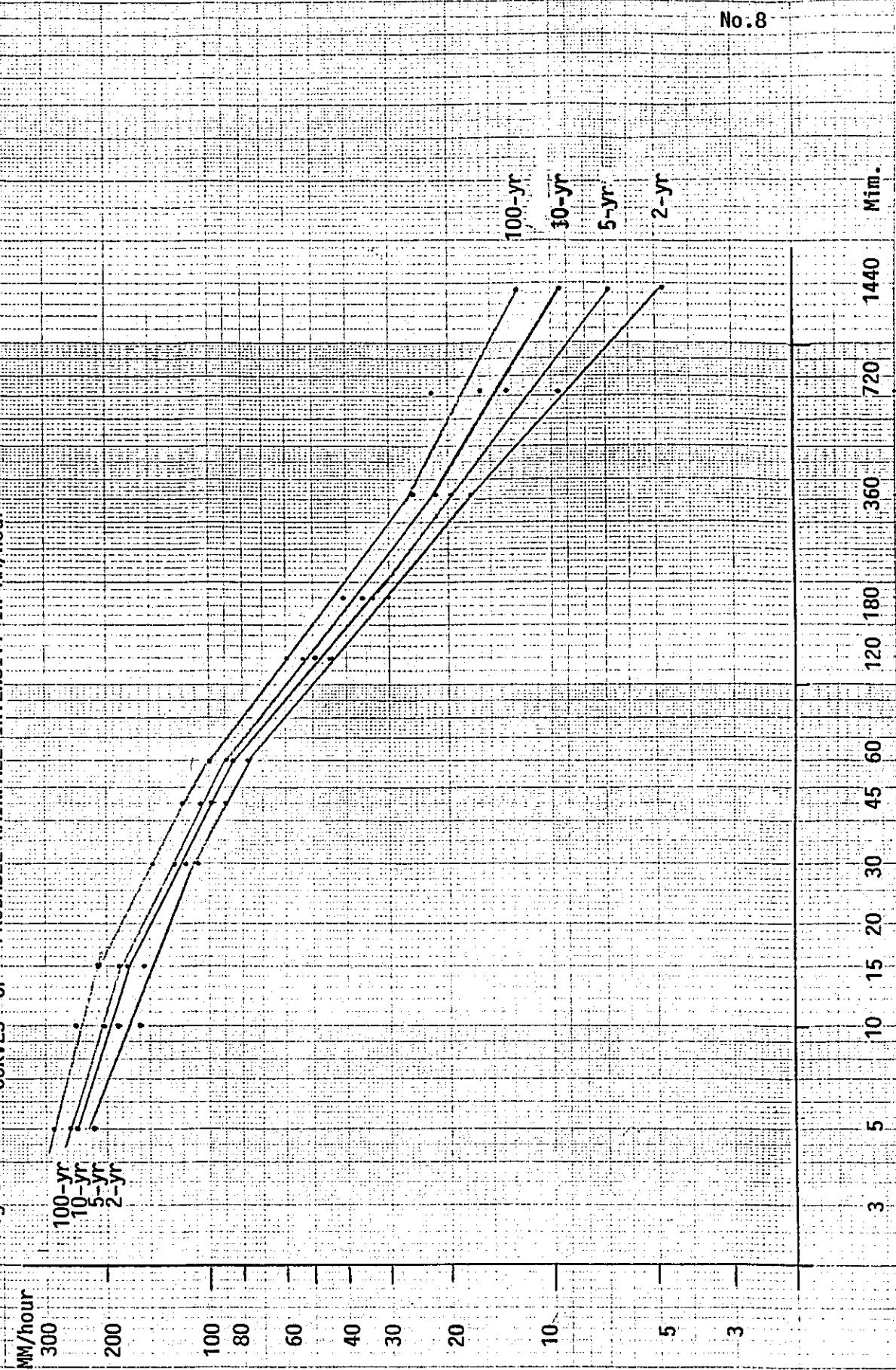
Year : 1989

| Month Date | Jan. | Feb. | Mar. | Apr. | May | Jun. | Jul. | Aug. | Sep. | Oct. | Nov. | Dec. | Remarks |
|---------------|------|------|------|------|-----|------|------|------|------|------|------|------|---------|
| 1 | 9 | 10 | 10 | 7 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 6 | 10 |
| 2 | 10 | 8 | 8 | 10 | 10 | 9 | 10 | 10 | 9 | 10 | 8 | 7 | |
| 3 | 10 | 9 | 10 | 10 | 9 | 10 | 10 | 10 | 10 | 10 | 6 | 9 | |
| 4 | 10 | 3 | 10 | 9 | 8 | 8 | 10 | 10 | 10 | 10 | 8 | 8 | 10 |
| 5 | 10 | 6 | 10 | 8 | 9 | 10 | 8 | 10 | 10 | 10 | 10 | 10 | |
| Sub-Total | 49 | 36 | 48 | 44 | 46 | 47 | 48 | 50 | 49 | 48 | 38 | 46 | |
| 6 | 10 | 6 | 9 | 9 | 9 | 10 | 10 | 10 | 9 | 10 | 10 | 7 | |
| 7 | 10 | 5 | 10 | 6 | 10 | 10 | 10 | 9 | 10 | 10 | 10 | 10 | |
| 8 | 9 | 8 | 10 | 10 | 8 | 10 | 10 | 10 | 10 | 9 | 6 | 9 | |
| 9 | 10 | 10 | 8 | 7 | 10 | 10 | 7 | 10 | 10 | 9 | 9 | 7 | |
| 10 | 8 | 10 | 5 | 10 | 8 | 10 | 10 | 10 | 10 | 10 | 8 | 8 | |
| Sub-Total | 47 | 39 | 42 | 42 | 45 | 50 | 47 | 49 | 49 | 48 | 43 | 41 | |
| 11 | 8 | 9 | 7 | 9 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | |
| 12 | 10 | 8 | 10 | 8 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 5 | |
| 13 | 9 | 4 | 10 | 10 | 8 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | |
| 14 | 8 | 10 | 10 | 9 | 10 | 10 | 10 | 10 | 9 | 10 | 10 | 9 | |
| 15 | 9 | 10 | 10 | 9 | 9 | 10 | 10 | 10 | 10 | 10 | 9 | 8 | |
| Sub-Total | 44 | 41 | 47 | 45 | 47 | 50 | 50 | 50 | 49 | 50 | 49 | 42 | |
| 16 | 10 | 5 | 9 | 10 | 9 | 10 | 10 | 10 | 10 | 5 | 9 | 9 | |
| 17 | 8 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 9 | 10 | 10 | 10 | |
| 18 | 7 | 10 | 9 | 9 | 10 | 10 | 10 | 10 | 10 | 10 | 9 | 9 | |
| 19 | 8 | 7 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 9 | 10 | 10 | |
| 20 | 7 | 5 | 10 | 10 | 9 | 10 | 10 | 10 | 10 | 10 | 8 | 10 | |
| Sub-Total | 40 | 37 | 48 | 49 | 48 | 50 | 50 | 50 | 49 | 42 | 48 | 48 | |
| 21 | 8 | 10 | 8 | 10 | 8 | 10 | 10 | 10 | 9 | 9 | 10 | 10 | |
| 22 | 8 | 10 | 9 | 10 | 8 | 10 | 10 | 10 | 8 | 8 | 6 | 10 | |
| 23 | 9 | 9 | 8 | 10 | 10 | 10 | 10 | 10 | 9 | 9 | 10 | 10 | |
| 24 | 10 | 10 | 9 | 10 | 10 | 9 | 9 | 10 | 9 | 10 | 10 | 9 | |
| 25 | 8 | 10 | 10 | 9 | 10 | 8 | 10 | 9 | 10 | 7 | 10 | 10 | |
| Sub-Total | 43 | 49 | 44 | 49 | 46 | 47 | 49 | 49 | 45 | 43 | 46 | 49 | |
| 26 | 9 | 9 | 10 | 10 | 10 | 10 | 9 | 7 | 10 | 10 | 9 | 10 | |
| 27 | 10 | 10 | 10 | 9 | 10 | 10 | 10 | 10 | 10 | 10 | 9 | 8 | |
| 28 | 7 | 10 | 10 | 10 | 10 | 10 | 9 | 10 | 10 | 10 | 10 | 8 | |
| 29 | 9 | - | 9 | 9 | 10 | 10 | 10 | 10 | 10 | 10 | 8 | 9 | |
| 30 | 10 | - | 8 | 10 | 10 | 10 | 10 | 7 | 9 | 10 | 10 | 8 | |
| 31 | 10 | - | 10 | - | 8 | - | 10 | 10 | - | 9 | - | 9 | |
| Sub-Total | 55 | 29 | 57 | 48 | 58 | 50 | 58 | 54 | 49 | 57 | 47 | 52 | |
| Grand Total | 278 | 231 | 286 | 277 | 290 | 294 | 302 | 302 | 290 | 288 | 271 | 278 | |

**No. 6 Recapitulation of Estimated Possible Working Hours
and their Percentage to the Scheduled Construction Working Hours**

| Year | Month Decade | Jan. | Feb. | Mar. | Apr. | May | Jun. | Jul. | Aug. | Sep. | Oct. | Nov. | Dec. | Remarks |
|------|---------------|------|------|------|------|-----|------|------|------|------|------|------|------|---------|
| 1985 | 1 Hrs % ditto | 90 | 92 | 89 | 92 | 96 | 95 | 95 | 95 | 92 | 97 | 90 | 94 | |
| | 2 Hrs % ditto | 86 | 92 | 95 | 94 | 93 | 98 | 92 | 99 | 98 | 90 | 96 | 97 | |
| | 3 Hrs % | 104 | 67 | 103 | 92 | 100 | 96 | 102 | 107 | 94 | 99 | 93 | 101 | |
| | T Hrs % | 280 | 251 | 287 | 278 | 289 | 289 | 289 | 301 | 284 | 286 | 279 | 292 | |
| | | 90 | 90 | 93 | 93 | 93 | 96 | 93 | 97 | 95 | 92 | 93 | 94 | |
| 1986 | 1 Hrs % ditto | 85 | 91 | 83 | 87 | 99 | 94 | 99 | 93 | 96 | 94 | 81 | 98 | |
| | 2 Hrs % ditto | 80 | 91 | 87 | 90 | 96 | 92 | 100 | 99 | 94 | 97 | 88 | 87 | |
| | 3 Hrs % | 90 | NA | 98 | 97 | 108 | 100 | 104 | 108 | 94 | 92 | 89 | 89 | |
| | T Hrs % | 255 | - | 268 | 274 | 303 | 286 | 303 | 300 | 284 | 283 | 258 | 274 | |
| | | 82 | | 86 | 91 | 98 | 95 | 98 | 97 | 95 | 91 | 86 | 88 | |
| 1987 | 1 Hrs % ditto | 84 | 78 | 92 | 90 | 92 | 91 | 98 | 99 | 98 | 98 | 90 | 89 | |
| | 2 Hrs % ditto | 83 | 88 | 92 | 90 | 89 | 100 | 100 | 100 | 99 | 96 | 89 | 89 | |
| | 3 Hrs % | 94 | 66 | 94 | 99 | 106 | 96 | 110 | 108 | 97 | 107 | 96 | 101 | |
| | T Hrs % | 261 | 232 | 278 | 279 | 287 | 287 | 308 | 307 | 294 | 301 | 275 | 269 | |
| | | 84 | 83 | 90 | 90 | 93 | 96 | 99 | 99 | 98 | 97 | 92 | 87 | |
| 1988 | 1 Hrs % ditto | 95 | 84 | 91 | 91 | 95 | 96 | 98 | 97 | 98 | 97 | 99 | 99 | |
| | 2 Hrs % ditto | 88 | 86 | 95 | 98 | 86 | 97 | 96 | 99 | 97 | 89 | 93 | 62 | |
| | 3 Hrs % | 99 | 87 | 82 | 94 | 108 | 100 | 99 | 109 | 93 | 101 | 91 | 102 | |
| | T Hrs % | 282 | 255 | 268 | 283 | 289 | 293 | 303 | 305 | 288 | 287 | 273 | 253 | |
| | | 91 | 88 | 86 | 94 | 93 | 98 | 98 | 98 | 96 | 93 | 91 | 82 | |
| 1989 | 1 Hrs % ditto | 96 | 75 | 90 | 86 | 91 | 97 | 95 | 99 | 98 | 96 | 81 | 87 | |
| | 2 Hrs % ditto | 84 | 78 | 95 | 94 | 95 | 100 | 100 | 100 | 98 | 92 | 97 | 90 | |
| | 3 Hrs % | 98 | 78 | 101 | 97 | 104 | 97 | 107 | 103 | 94 | 100 | 93 | 101 | |
| | T Hrs % | 278 | 231 | 286 | 277 | 290 | 294 | 302 | 302 | 290 | 288 | 271 | 278 | |
| | | 90 | 83 | 92 | 92 | 94 | 98 | 97 | 97 | 97 | 93 | 90 | 90 | |

Fig C1 - 1 CURVES OF PROBABLE RAINFALL INTENSITY IN MM/hour



No.8

No. A1-31465

付属資料 C 2 水文

1. General
2. River System of the Cihideung River
3. River Surveying Results of the Cihideung River at the Project Site
4. Recapitulation of Records for Irrigation Intake Water at the Cihideung River
5. Available River Water at the Project Site
6. Estimate of Flood Discharge of the Cihideung River
7. Design flood and Design Floor Elevation of the Pump Station under Consideration

| | |
|---------------|---|
| Fig. C2-1 | Catchment Area of the Cihideung River |
| Fig. C2-2 | River System of the Cihideung River |
| Fig. C2-3 | River Profile in the Catchment Area |
| Fig. C2-4 | Discharge Curve of the Cihideung River at Pump Station Site under Consideration |
| Fig. C2-5 | Curve of the Relationship between R_n and Q_N |
| Table C2-1 | Calculated Flood Q_N by Der Weduwen Formula |
| Table C2-2 | Calculated Probable Flood Discharge |
| Drawings C2-1 | Plan, Profile, Typical Cross Section and Flood Discharge Curve of the Cihideung River |
| Drawings C2-2 | Cross Section of the Cihideung River (1/2) |
| Drawings C2-3 | - do - (2/2) |

1. General

The water source of the Cihideung River is available at the Project site. It, therefore, is necessary to study on availability of drought discharge in the dry season and on recurrence of flood, river capacity of flood passing in relations to flood water level and discharge of the Cihideung River.

During the field survey, efforts have been made for collection of hydrological data of the Cihideung River at the water source section of Bogor Branch Office, West Java Provincial Public Works. Irrigation intake water records at the Cihideung weir were collected for only 1988 and 1989. Also, river surveying for plan, profile and cross section of about 400 m distance of the Cihideung River at the Project site was

carried out by the survey team. The results were studied subsequently for flood discharge estimate as well as location of future pump station.

2. River System of the Cihideung River

The color topographic maps with scale of 1/50,000 (old print) and the black and white copies of topographic maps with the same scale have been used for study of the catchment area.

The Cihideung River Originates the Salak mountains, accurately in the Peak (EL. 2,180 m) which locates on the connected ridge between the Salak mountain (EL. 2,211 m) and the Sumbu mountain (EL. 1,916 m). It flows down toward north in collecting drained water from its tributaries developed on the northern slope of the Salak mountains and reaches to the Project site after run about 18 km. The catchment area is 35 km^2 showing nearly a long elliptic shape on the map.

The Project site and catchment area of the Cihideung River is attached as Fig. C2-1 and the river system is illustrated in Fig. C2-2. As seen from Fig. C2-2, there are nine (9) tributaries, and the catchment areas are estimated at 35 km^2 , 16 km^2 , 15 km^2 and 13 km^2 at the sites of the pump station, the Cihideung weir, the Cianyar weir and the Cisunar weir, respectively.

River profile in the Catchment area has been prepared as shown in Fig. C2-3.

3. River Surveying Results of the Cihideung River at the Project Site

During the field survey period, the river route surveying for plan, profile and cross section was carried out for about 400 m distance of the Cihideung River.

The plan, profile and typical cross sections are given in Drawing C2-1 to -3.

The typical flow section is estimated as follows :

| | | |
|--|---|----------|
| 1. Bottom width at EL. 209.0 m | : | 5.8 m |
| 2. Width at EL. 211.6 m of the crest of Cihideung Supply Weir | : | 22 m |
| 3. Width at EL. 213.6 m | : | 34 m |
| 4. Side Slope | : | 3 to 1 |
| 5. River bed slope (average) | : | -0.00725 |
| 6. Damming up height at the Cihideung Supply Weir (EL. 211.6 m - EL. 209 m) | : | 2.6 m |
| 7. Distance between Cihideung Supply Weir and pump station | : | 255 m |
| 8. Roughness coefficient of Manning Formula | : | 0.020 |

Utilizing the above survey results, river capacity on flood passing in relation to water level and discharge has been calculated and shown in a curve as given in Fig. C2-4.

4. Recapitulation of Records for Irrigation Intake Water at the Cihideung River

The Water Resource Division, Bogor Branch Office of the West Java Provincial Public Works (SBDPUJB) is the responsible agency for water use of the Cihideung River.

Irrigation intake water and spilled water at the Cihideung Weir site is being record by the gate master at every morning and evening.

In order to know the status of river discharge, daily records from February, 1988 to December, 1989 have been collected with kind cooperation of the above SPBPU.

All the data were evaluated and arranged in a form of mean flow during pentad period as attached in Table C2-1.

Table C 2-1 Pentad Mean Irrigation Intake Flow and Spilled Flow
at the Cihideung Irrigation Weir (Catchment Area = 16 km²)

(Unit : lit/sec)

| 1988 | | | | | | 1989 | | | | | | 1988 | | | | | | 1989 | | | | | |
|------|--------|-------------------|-------|-------|--------|-------|-------|------|---|--------|-------------------|-------|-------|--------|--------|--------|------|------|--|--|--|--|--|
| | Intake | Spill | Total | Note | Intake | Spill | Total | Note | | Intake | Spill | Total | Note | Intake | Spill | Total | Note | | | | | | |
| J | 1 | | | | 440 | 528 | 968 | | J | 1 | 189 | 0 | 189 | 296 | 384 | 680 | | | | | | | |
| | 2 | No Data Available | | | 428 | 152 | 580 | | | 2 | 195 | 634 | 829 | 305 | 393 | 698 | | | | | | | |
| | 3 | | | | 423 | 472 | 895 | | | 3 | 179 | 0 | 179 | 300 | 275 | 575 | | | | | | | |
| | 4 | | | | 432 | 104 | 536 | | | 4 | 176 | 0 | 176 | 294 | 90 | 384 | | | | | | | |
| | 5 | | | | 452 | 546 | 998 | | | 5 | 163 | 0 | 163 | 305 | 435 | 740 | | | | | | | |
| | 6 | | | | 485 | 0 | 485 | | | 6 | 198 | 0 | 198 | 302 | 0 | 302 | | | | | | | |
| M | | | | | 443 | 300 | 743 | | M | 183 | 106 | 183 | | 300 | 263 | 563 | | | | | | | |
| F | 1 | 315 | 378 | 693 | 322 | 191 | 513 | | A | 1 | | | | 251 | 0 | 251 | | | | | | | |
| | 2 | 329 | 178 | 507 | 324 | 262 | 586 | | | 2 | No Data Available | | | 275 | 0 | 275 | | | | | | | |
| | 3 | 319 | 214 | 533 | 311 | 369 | 680 | | | 3 | | | | 252 | 0 | 252 | | | | | | | |
| | 4 | 317 | 0 | 317 | 308 | 202 | 510 | | | 4 | | | | 270 | 0 | 270 | | | | | | | |
| | 5 | 355 | 116 | 471 | 274 | 0 | 274 | | | 5 | | | | 252 | 202 | 457 | | | | | | | |
| | 6 | 354 | 985 | 1,339 | 214 | 205 | 419 | | | 6 | | | | 260 | 164 | 424 | | | | | | | |
| M | | 332 | 312 | 644 | 292 | 205 | 497 | | M | | | | | 260 | 61 | 321 | | | | | | | |
| M | 1 | 223 | 1,024 | 1,247 | 306 | 0 | 306 | | S | 1 | 239 | 0 | 239 | 249 | 0 | 249 | | | | | | | |
| | 2 | 276 | 3,034 | 3,310 | 313 | 0 | 313 | | | 2 | 240 | 0 | 240 | 263 | 0 | 263 | | | | | | | |
| | 3 | 270 | 2,596 | 2,866 | 318 | 0 | 318 | | | 3 | 232 | 0 | 232 | 247 | 0 | 247 | | | | | | | |
| | 4 | 255 | 1,402 | 1,657 | 314 | 0 | 314 | | | 4 | 239 | 0 | 239 | 251 | 0 | 251 | | | | | | | |
| | 5 | 264 | 920 | 1,184 | 319 | 104 | 423 | | | 5 | 243 | 0 | 243 | 241 | 0 | 241 | | | | | | | |
| | 6 | 271 | 1,587 | 1,858 | 319 | 1,434 | 1,753 | | | 6 | 266 | 0 | 266 | 264 | 0 | 264 | | | | | | | |
| M | | 260 | 1,761 | 2,021 | 315 | 256 | 571 | | M | 243 | 0 | 243 | | 253 | 0 | 253 | | | | | | | |
| A | 1 | 266 | 325 | 591 | 313 | 943 | 1,256 | | O | 1 | 265 | 1,165 | 1,430 | 230 | 366 | 596 | | | | | | | |
| | 2 | 265 | 960 | 1,225 | 313 | 281 | 594 | | | 2 | 261 | 1,328 | 1,589 | 233 | 188 | 421 | | | | | | | |
| | 3 | 267 | 1,044 | 1,311 | 301 | 0 | 301 | | | 3 | 257 | 2,611 | 2,868 | 244 | 1,548 | 1,792 | | | | | | | |
| | 4 | 259 | 342 | 601 | 307 | 864 | 1,171 | | | 4 | 273 | 1,178 | 1,451 | 240 | 3,860 | 4,100 | | | | | | | |
| | 5 | 257 | 274 | 531 | 300 | 90 | 390 | | | 5 | 279 | 1,370 | 1,649 | 240 | 2,732 | 2,972 | | | | | | | |
| | 6 | 254 | 0 | 254 | 289 | 0 | 289 | | | 6 | 247 | 563 | 810 | 242 | 3,140 | 3,382 | | | | | | | |
| M | | 261 | 491 | 752 | 304 | 363 | 667 | | M | 264 | 1,369 | 1,633 | | 238 | 1,972 | 2,210 | | | | | | | |
| M | 1 | 263 | 576 | 839 | 300 | 779 | 1,079 | | N | 1 | 284 | 435 | 719 | 375 | 8,080 | 8,455 | | | | | | | |
| | 2 | 241 | 474 | 715 | 309 | 868 | 1,177 | | | 2 | 245 | 0 | 245 | 298 | 388 | 686 | | | | | | | |
| | 3 | 236 | 461 | 697 | 295 | 866 | 1,161 | | | 3 | 245 | 0 | 245 | 361 | 3,336 | 3,697 | | | | | | | |
| | 4 | 269 | 435 | 704 | 317 | 967 | 1,284 | | | 4 | 287 | 594 | 881 | 363 | 6,256 | 6,619 | | | | | | | |
| | 5 | 264 | 90 | 354 | 306 | 860 | 1,166 | | | 5 | 287 | 563 | 850 | 305 | 224 | 529 | | | | | | | |
| | 6 | 261 | 128 | 389 | 321 | 1,357 | 1,678 | | | 6 | 258 | 0 | 258 | 304 | 0 | 304 | | | | | | | |
| M | | 256 | 361 | 617 | 308 | 950 | 1,258 | | M | 268 | 265 | 533 | | 334 | 3,047 | 3,381 | | | | | | | |
| J | 1 | 251 | 0 | 251 | 329 | 1,051 | 1,380 | | D | 1 | 267 | 176 | 443 | 359 | 11,447 | 11,806 | | | | | | | |
| | 2 | 260 | 628 | 888 | 324 | 638 | 962 | | | 2 | 259 | 90 | 349 | 442 | 1,728 | 2,170 | | | | | | | |
| | 3 | 253 | 156 | 409 | 336 | 0 | 336 | | | 3 | 288 | 269 | 557 | 414 | 0 | 414 | | | | | | | |
| | 4 | 230 | 0 | 230 | 270 | 0 | 270 | | | 4 | 291 | 370 | 661 | 347 | 1,249 | 1,596 | | | | | | | |
| | 5 | 207 | 0 | 207 | 282 | 0 | 282 | | | 5 | 253 | 0 | 253 | 401 | 458 | 859 | | | | | | | |
| | 6 | 198 | 0 | 198 | 288 | 0 | 288 | | | 6 | 258 | 0 | 258 | 360 | 6,244 | 6,604 | | | | | | | |
| M | | 233 | 131 | 364 | 305 | 281 | 586 | | M | 269 | 151 | 420 | | 387 | 3,521 | 3,908 | | | | | | | |

Note

1. Source : Seksi BOGOR DPU. Java Barat. (SBDPUJB)
2. Flow is estimated on the basis of overflow depth read at morning and evening.
3. M means the average in the month.

5. Available River Water at the Project Site

As seen from Table C2-1, the spilled flow at the Cihideung weir is high in the rainy season but very small or zero in both dry season and in no rain pentad in rainy season.

While the water shortage of the irrigation experimental farm, IPB concentrates in the dry season, much water release from the Cihideung Weir can be unexpected.

So, run-off from the tributaries : Cimboran, Cirandi, Cibeurem, Cikiruk, Cipakar and Cisawah becomes to the reliable water source for the Project. Such remaining part of the catchment area in downstream of the Cihideung Weir is 19 km^2 in total at the pump station site under consideration.

The run-off in the drought period available for the Project is estimated as follows :

1. The lowest run-off at the Cihideung Weir, : 163 lit/sec
5th pentad July, 1988 ($CA = 16 \text{ km}^2$)
2. Specific run-off of the above : 10 lit/sec/ km^2
3. Estimated lowest run-off from the remaining catchment : 133 lit/sec
($CA = 19 \text{ km}^2$, safety factor 0.7)
4. Irrigation water requirements for the Cihideung irrigation system from the Cihideung Supply Weir : 115 lit/sec
($IA = 64 \text{ ha}$, Unit W. R. = 1.8 lit/sec/ha)
5. Available water source at the Pump Station Site : 18 lit/sec
(Item 3 - Item 4)

From the above, it is concluded that river discharge available for the Project is 18 lit/sec during the drought period.

6. Estimate of Flood Discharge of the Cihideung River

The catchment area of the Cihideung River is estimated at 35 km^2 at pump station site under consideration read on the Topographic Map with the scale of 1:50,000.

Also, the following features of the catchment area are found :

- the highest elevation EL 2,000 m
- the lowest elevation EL 190 m
- the longest river length L 17.8 km
- the average river slope I $910/16,000 = 0.0569$

The Chilideung River system and profile have been illustrated as shown in Fig and Fig .

The Der Weduwen flood formula has been applied for this area as follows :

$$Q_n = \alpha \cdot \beta \cdot q_u \cdot A$$

in which,

$$\alpha = 1 - \frac{4.1}{\beta \cdot q_u + 7}$$

$$\beta = \frac{120 + \left(\frac{t+1}{t+9}\right) A}{120 + A}$$

$$q_u = \frac{R_n}{240} \cdot \frac{67.65}{t+1.45}$$

$$t = 0.25 \cdot L \cdot Q^{-0.125} \cdot I^{-0.25}$$

and where,

Q_n or Q = N - Yr flood discharge in m^3/sec

R_n = N - Yr design rainfall in mm/day

α or F = run-off coefficient

β or B = areal reduction coefficient for the catchment rainfall

q_u or Qu = heavy rainfall given in m^3/sec per km^2

A = catchment area in km^2 upto $100 km^2$

t = duration of heavy rainfall in hours

L = river length in km

I = average gradient of river or terrain, for determination the upstream 10 % of the length is excluded. Height difference and length are taken from a point 0.1 L from the upstream catchment boundary.

Using the above figures of the Catchment, the relationship between R_n and Q_n have been calculated with the try and error method by assuming Q_n as follows.

Calculated Flood Qn by Der Weduwen Formula

| RN = 5 | RN = 10 | RN = 20 | RN = 30 | RN = 50 |
|------------|-------------|-------------|------------|------------|
| T = 8.406 | T = 7.606 | T = 6.859 | T = 6.441 | T = 5.932 |
| F = 0.425 | F = 0.437 | F = 0.461 | F = 0.484 | F = 0.528 |
| B = 0.896 | B = 0.891 | B = 0.886 | B = 0.883 | B = 0.879 |
| QU = 0.143 | QU = 0.311 | QU = 0.678 | QU = 1.072 | QU = 1.909 |
| QN = 1.9 | QN = 4.2 | QN = 9.7 | QN = 16 | QN = 31 |
| | | | | |
| RN = 60 | RN = 70 | RN = 80 | RN = 90 | RN = 100 |
| T = 5.755 | T = 5.608 | T = 5.483 | T = 5.374 | T = 5.278 |
| F = 0.547 | F = 0.566 | F = 0.583 | F = 0.6 | F = 0.615 |
| B = 0.878 | B = 0.876 | B = 0.875 | B = 0.874 | B = 0.873 |
| QU = 2.347 | QU = 2.796 | QU = 3.253 | QU = 3.717 | QU = 4.189 |
| QN = 39.5 | QN = 48.5 | QN = 58.2 | QN = 68.3 | QN = 78.8 |
| | | | | |
| RN = 200 | RN = 300 | RN = 400 | | |
| T = 4.691 | T = 4.386 | T = 4.188 | | |
| F = 0.726 | F = 0.79 | F = 0.831 | | |
| B = 0.868 | B = 0.865 | B = 0.863 | | |
| QU = 9.18 | QU = 14.489 | QU = 19.999 | | |
| QN = 202.5 | QN = 346.6 | QN = 502 | | |

Based on the above calculation, curve of the relationship between Rn and QN for flood discharge of the Cihideung River has been shown in Fig. C2-5.

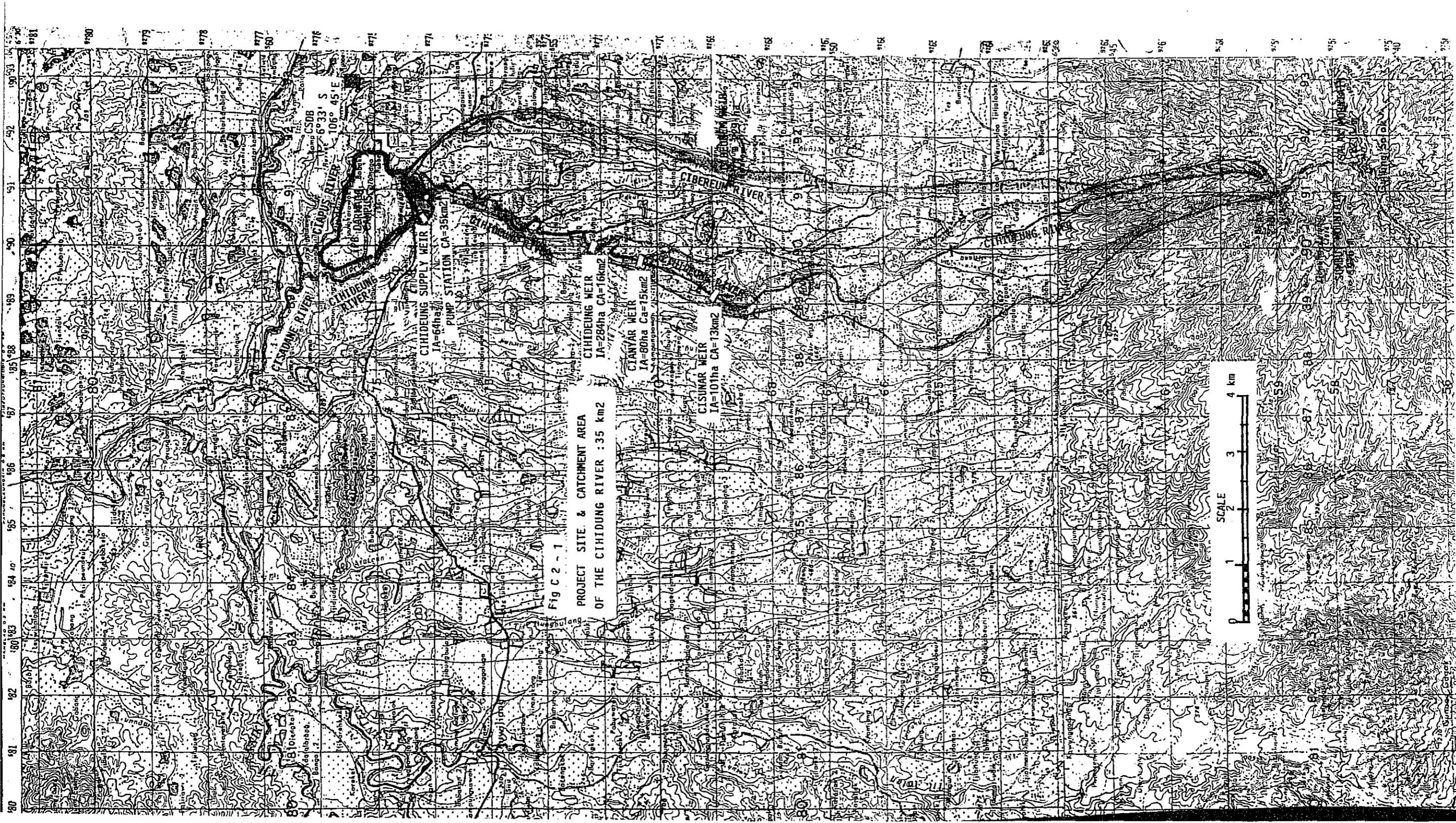
By applying the Der Weduwen flood formula with parameters of probable daily rainfall (mm/day) for annual and every monthly maximum rainfall, flood discharges of the Cihideung River have been estimated as shown in Table C2-2.

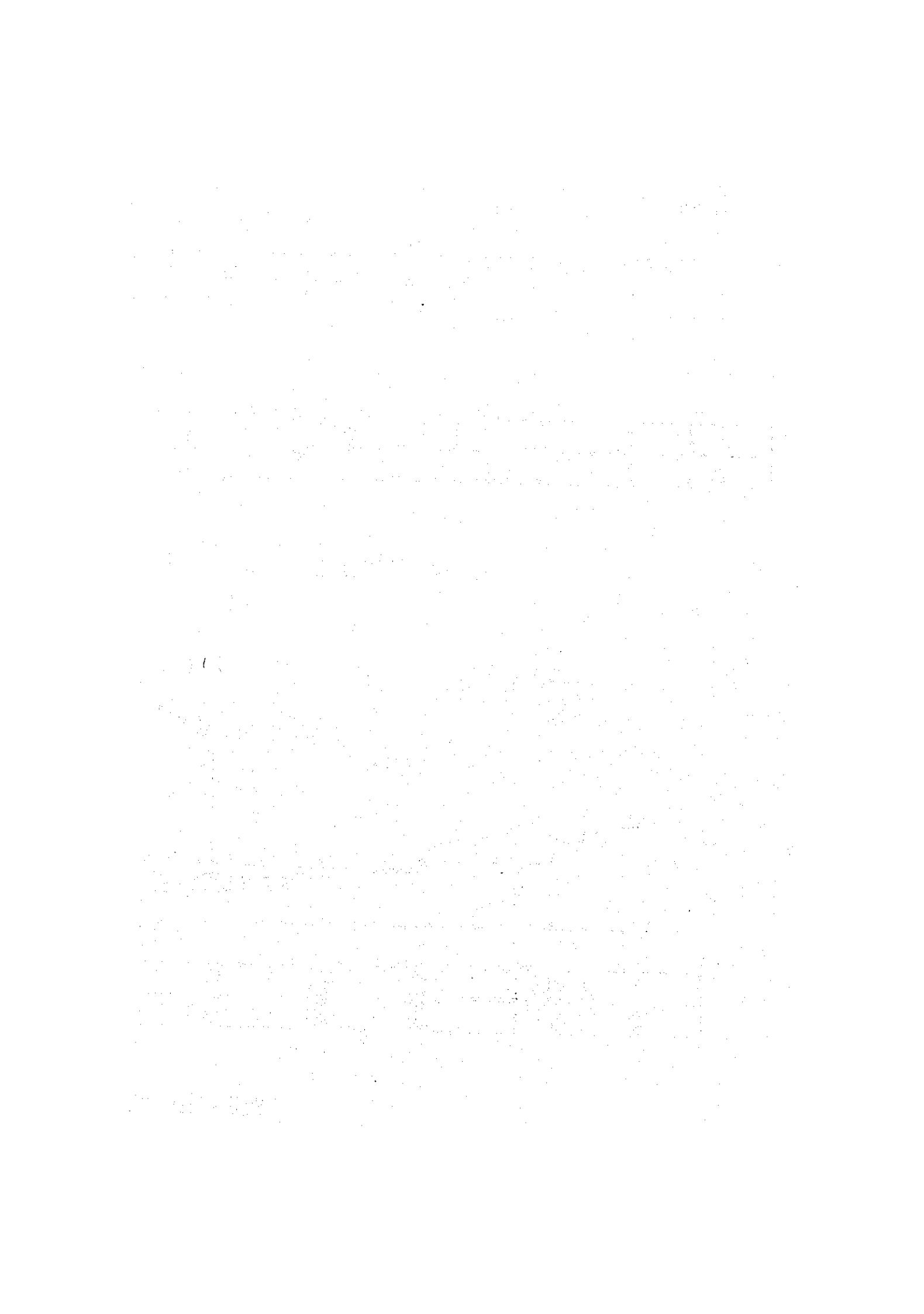
Table C2-2 Calculated Probable Flood Discharge

| Return Period | Items | Unit | Annual | Jan. | Feb. | Mar. | Apr. | May | Jun. | Jul. | Aug. | Sep. | Oct. | Nov. | Dec. |
|---------------|-------|-------------------|--------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 2-Yr | Rn | mm/day | 116.5 | 65.6 | 64.8 | 62.5 | 71.9 | 68.2 | 65.1 | 66.2 | 58.2 | 65.1 | 64.5 | 54.9 | 57.2 |
| | Qn | m ³ /s | 97.1 | 44.5 | 48.3 | 41.7 | 50.3 | 46.9 | 44.0 | 45.0 | 37.9 | 44.0 | 43.5 | 35.1 | 37.0 |
| 4-Yr | Rn | mm/day | 145.4 | 83.5 | 98.9 | 80.6 | 85.4 | 94.5 | 90.0 | 98.0 | 84.2 | 90.8 | 82.9 | 72.2 | 84.1 |
| | Qn | m ³ /s | 131.5 | 61.6 | 77.6 | 58.7 | 63.6 | 73.0 | 68.3 | 76.7 | 62.3 | 69.1 | 61.0 | 50.6 | 62.2 |
| 5-Yr | Rn | mm/day | 153.8 | 88.7 | 108.7 | 85.9 | 89.3 | 102.1 | 97.2 | 107.2 | 91.8 | 98.2 | 88.3 | 77.2 | 91.9 |
| | Qn | m ³ /s | 141.9 | 66.9 | 88.3 | 64.1 | 67.5 | 81.1 | 75.8 | 86.7 | 70.1 | 76.9 | 66.5 | 55.4 | 70.2 |
| 10-Yr | Rn | mm/day | 178.5 | 103.9 | 137.8 | 101.3 | 100.9 | 124.6 | 118.5 | 134.4 | 114.0 | 120.1 | 104.0 | 92.0 | 114.9 |
| | Qn | m ³ /s | 173.7 | 83.0 | 122.2 | 80.2 | 79.8 | 106.5 | 99.4 | 118.1 | 94.3 | 101.2 | 83.2 | 70.3 | 95.3 |
| 20-Yr | Rn | mm/day | 202.2 | 118.6 | 165.7 | 116.1 | 112.0 | 146.1 | 138.8 | 160.4 | 135.3 | 141.1 | 119.1 | 106.2 | 136.9 |
| | Qn | m ³ /s | 205.5 | 99.5 | 157.0 | 96.7 | 92.0 | 132.3 | 123.4 | 150.3 | 119.2 | 126.2 | 100.1 | 85.6 | 121.1 |
| 50-Yr | Rn | mm/day | 232.9 | 137.5 | 201.9 | 135.3 | 126.3 | 174.0 | 165.2 | 194.1 | 163.0 | 168.4 | 138.6 | 124.5 | 165.5 |
| | Qn | m ³ /s | 248.3 | 121.8 | 205.1 | 119.2 | 108.5 | 167.8 | 156.4 | 194.5 | 153.6 | 160.5 | 123.1 | 106.3 | 156.8 |
| 100-Yr | Rn | mm/day | 255.9 | 151.7 | 229.0 | 149.7 | 137.0 | 194.9 | 185.0 | 219.4 | 183.6 | 188.8 | 153.2 | 138.3 | 186.8 |
| | Qn | m ³ /s | 281.3 | 139.3 | 242.8 | 136.8 | 121.2 | 195.6 | 182.3 | 229.3 | 180.5 | 187.4 | 141.2 | 122.8 | 184.7 |

7. Design Flood and Design Floor Elevation of the Pump Station under Consideration

As seen from Table C2-2, 100-Yr flood is 255.9 m³/sec and 229.0 m³/sec for annual data and February data, respectively. Thus, the design flood for the pump station is decided to be 260 m³/sec. Accordingly, design high water level is found to be EL 214.6 m so that the design floor elevation of the pump station is determined to be EL. 215.0 m in adding 0.4 m allowance to the designed high water level.





Cihideung Supply weir -0.255 km

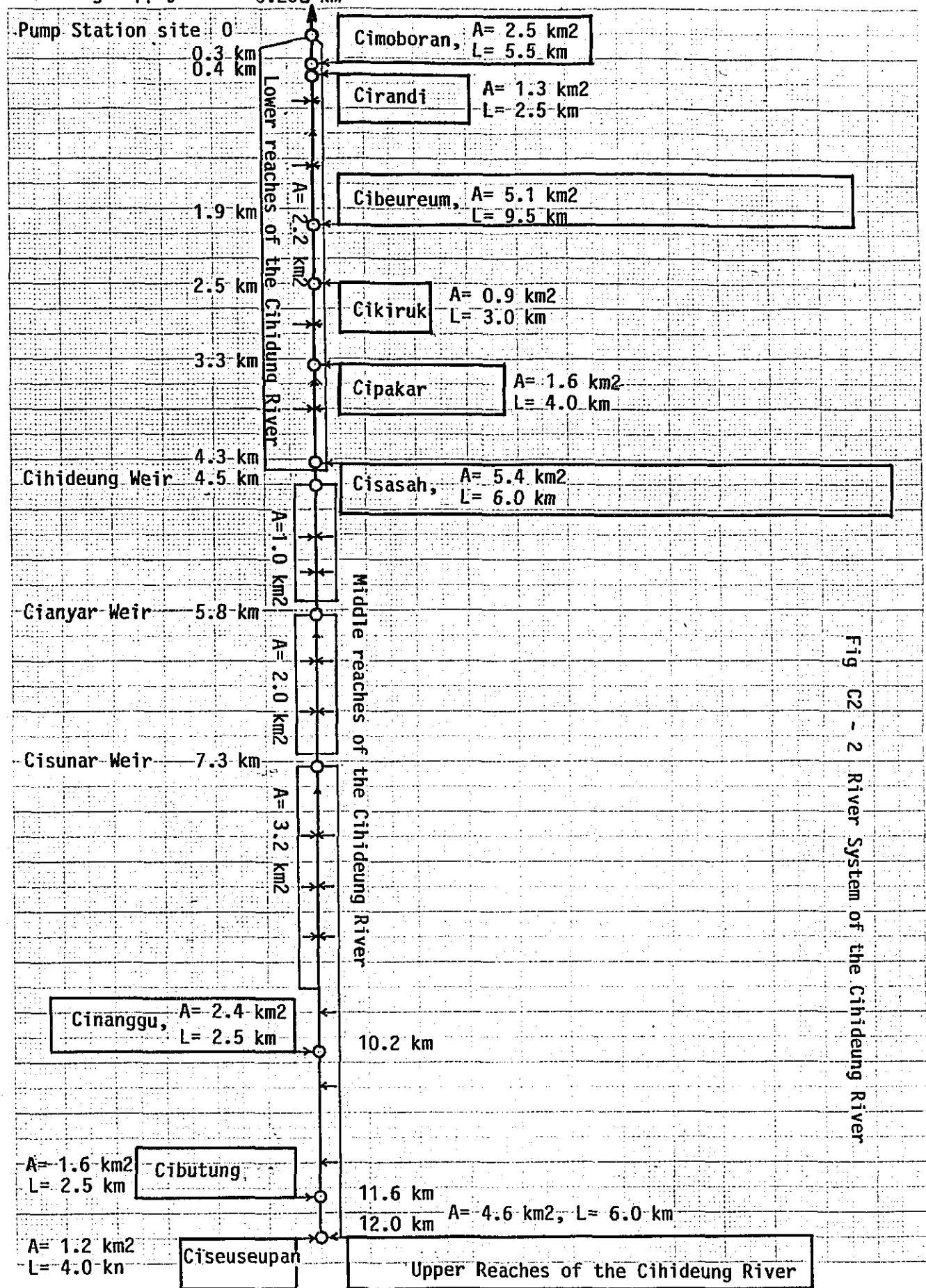
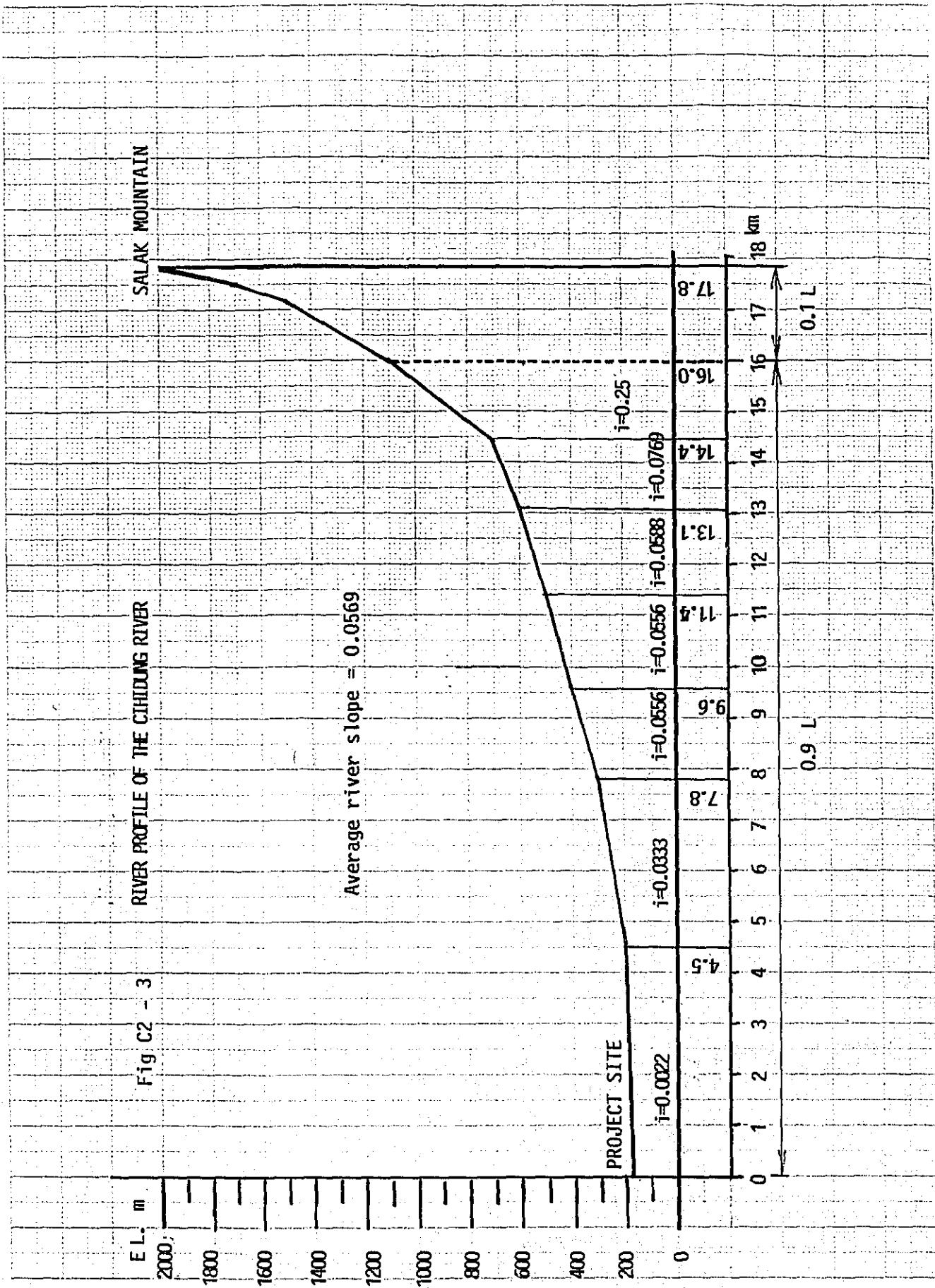


Fig C2 - 3 RIVER PROFILE OF THE CHIONG RIVER

SALAK MOUNTAIN

Average river slope = 0.0569



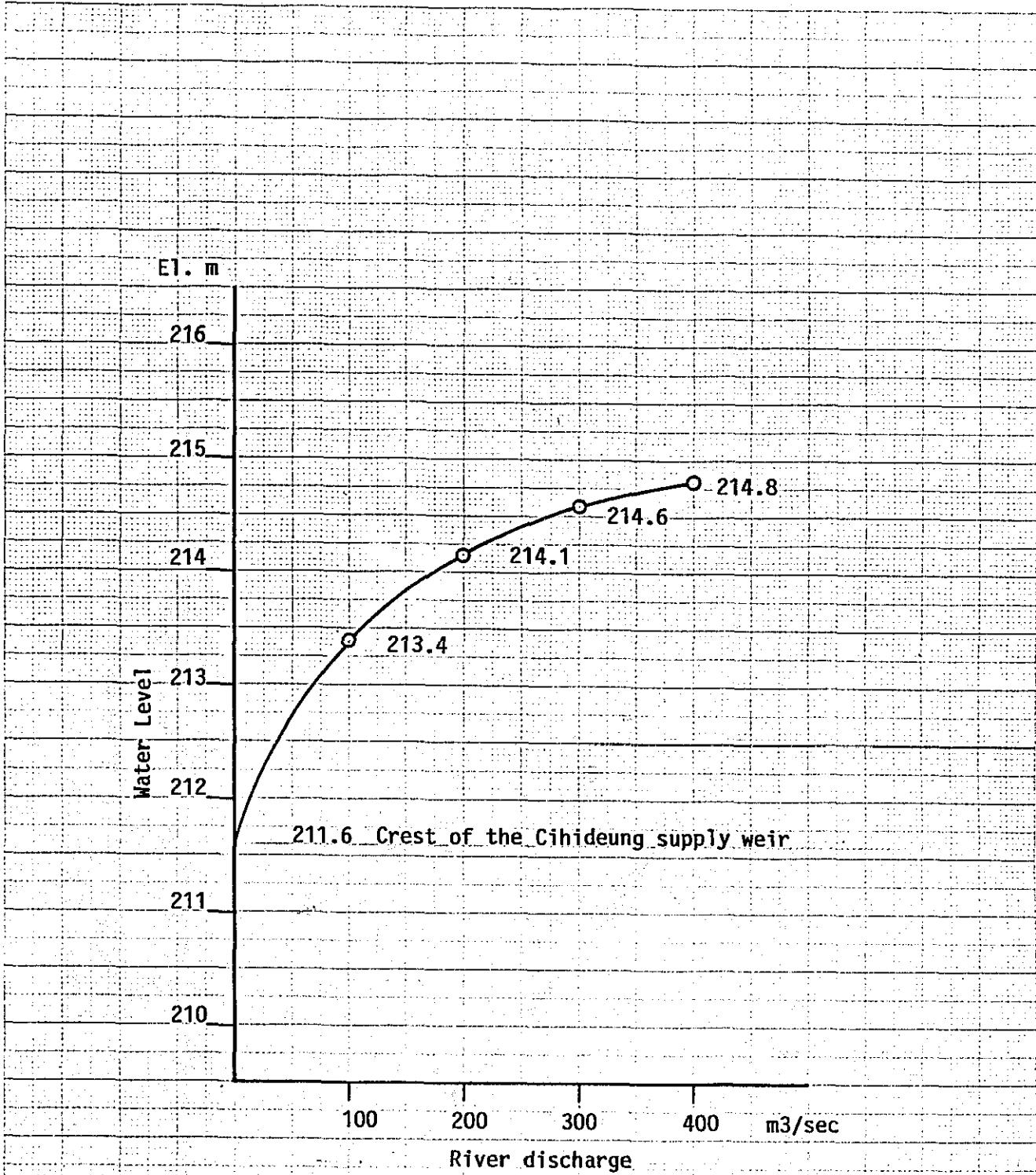


Fig C2 - 4 Discharge Curve of the Cihideung River at Pump Station Site under consideration

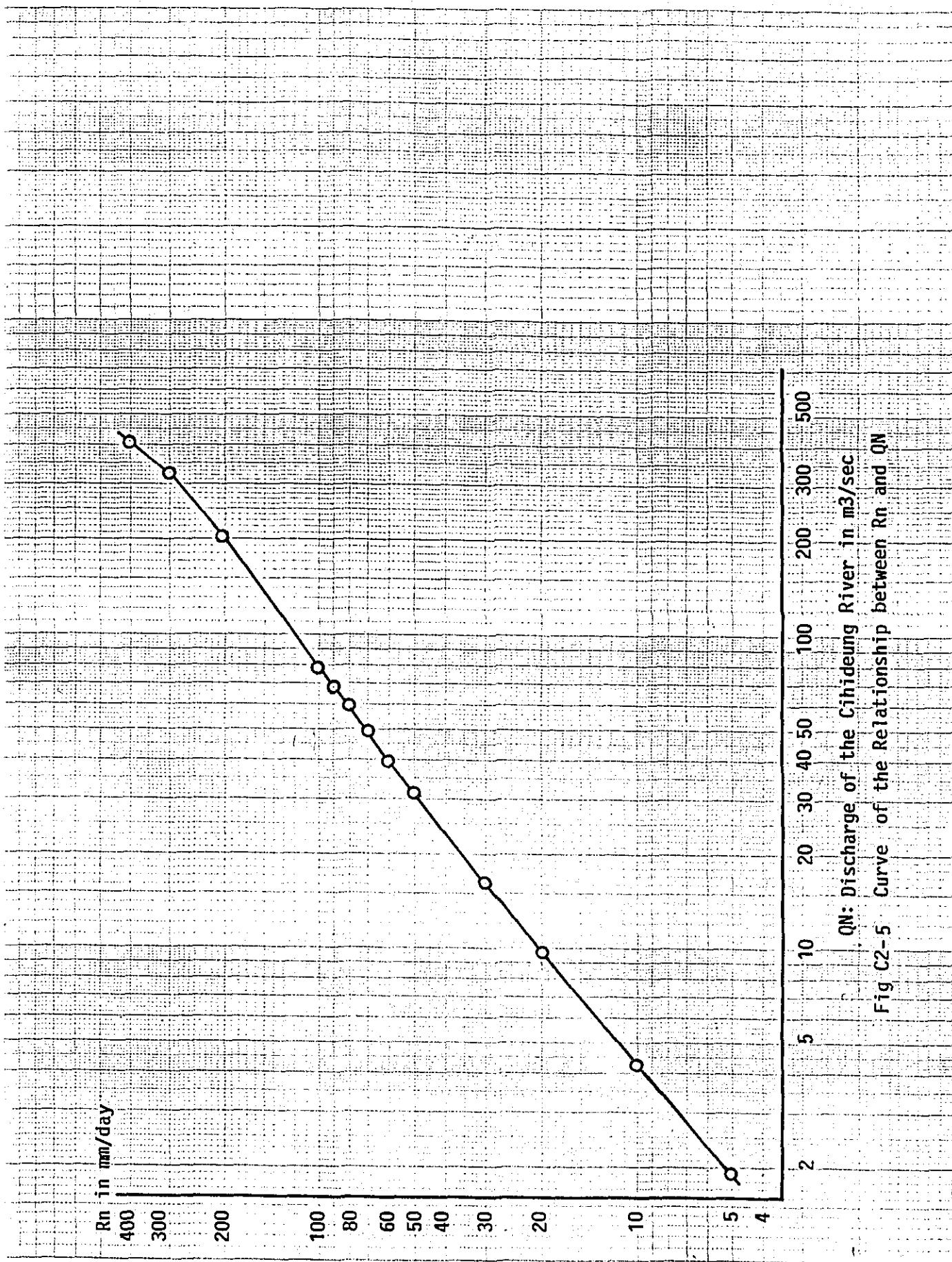
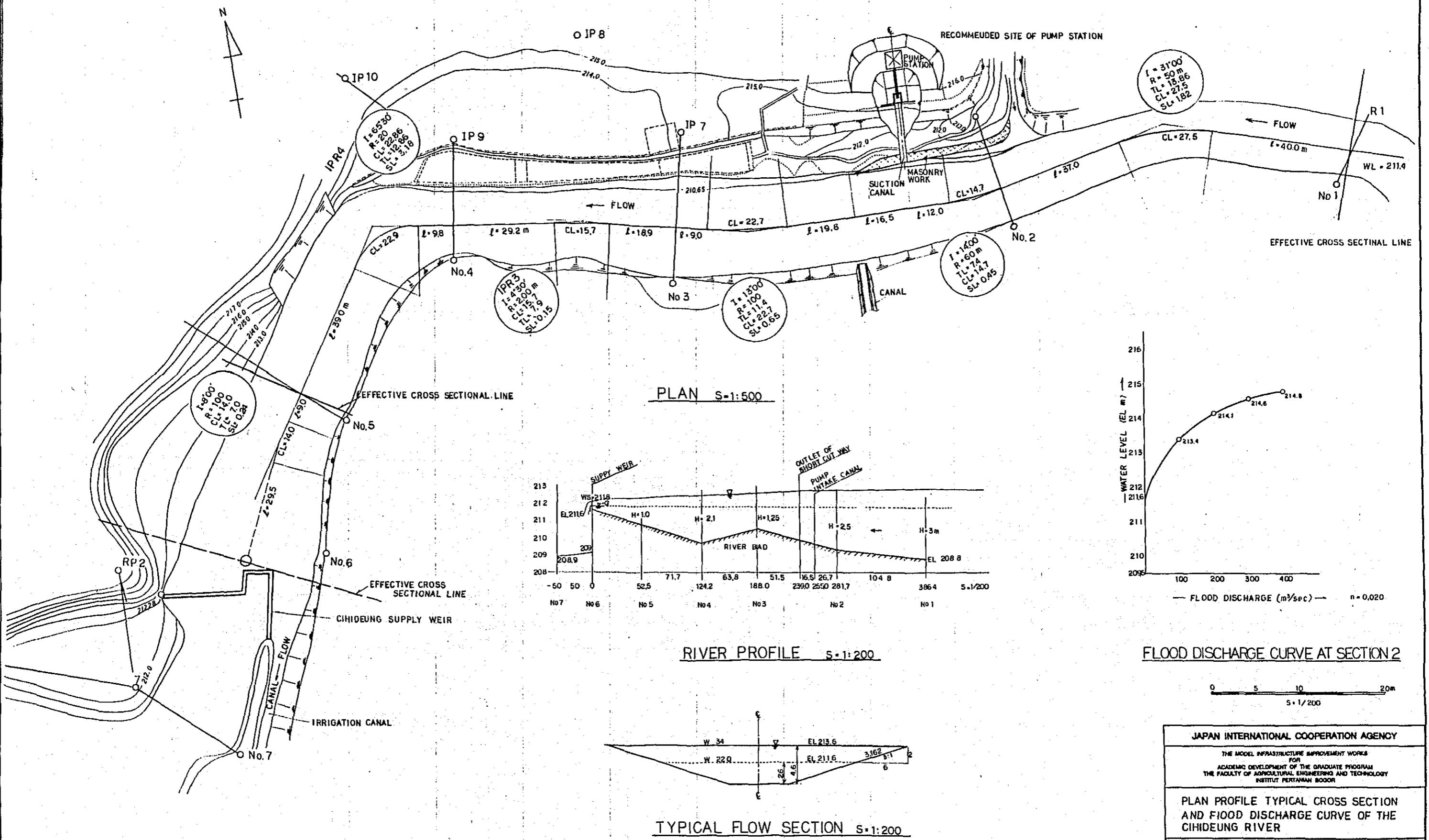
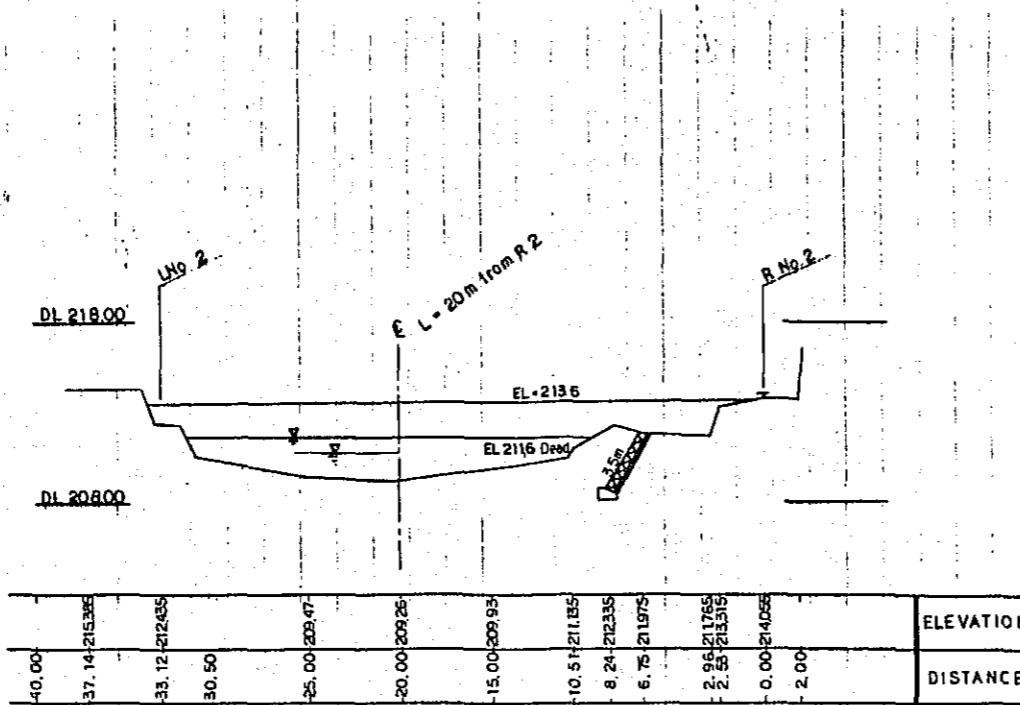


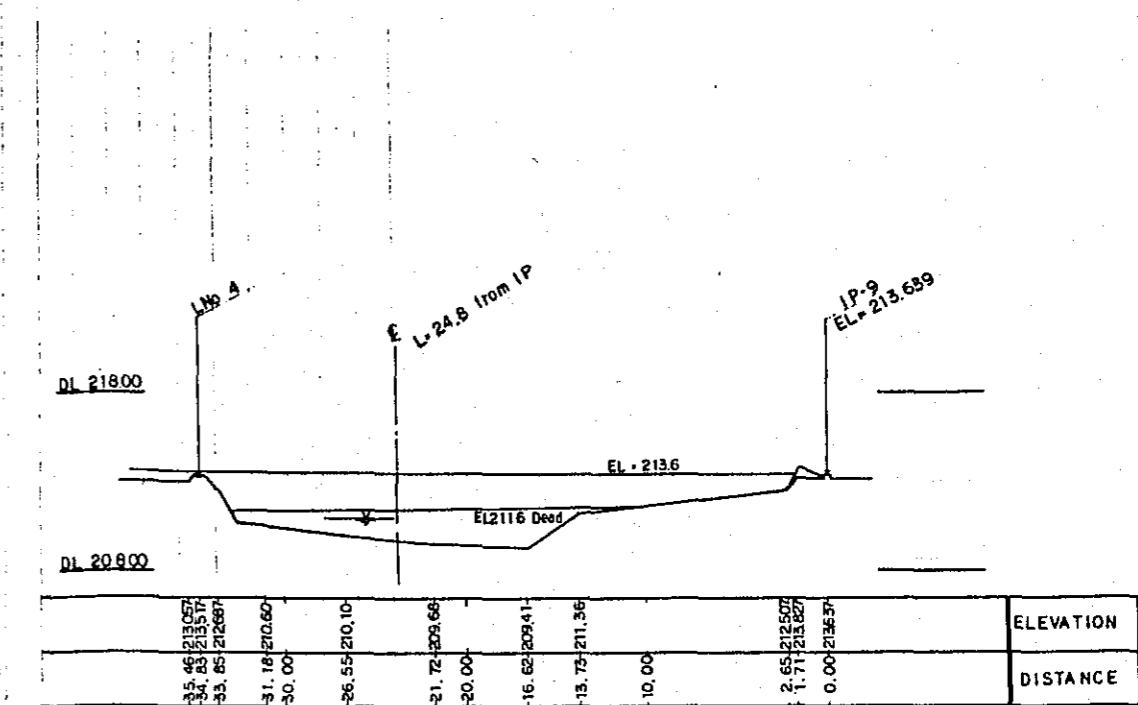
Fig C2-5. Curve of the Relationship between RN and QN



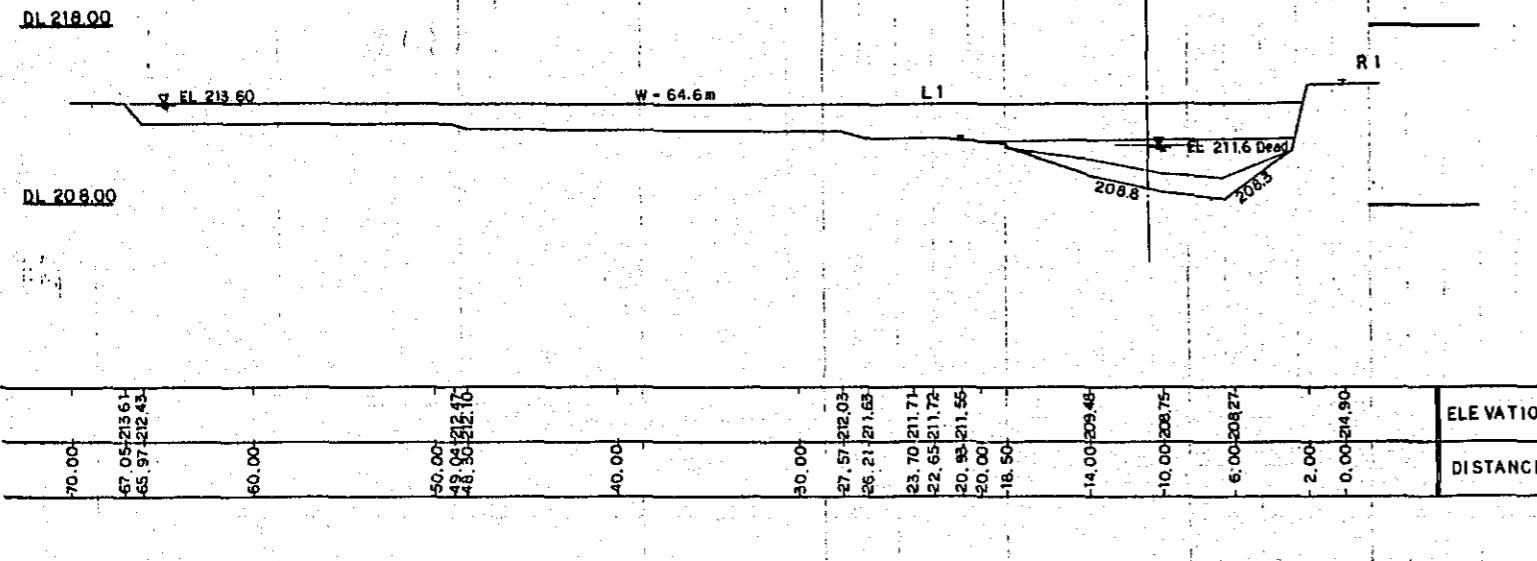
—69—



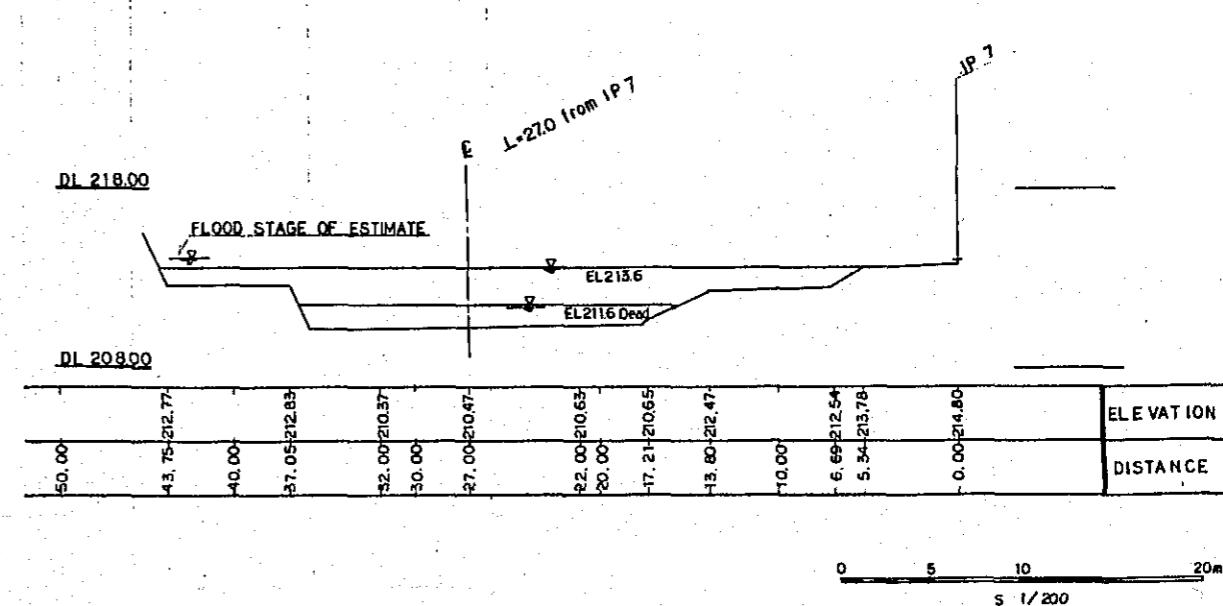
No.2 SECTION S-1:200



No.4 SECTION S-1:200



No.1 SECTION S-1:200



No.3 SECTION S-1:200

| | |
|---|-------------|
| JAPAN INTERNATIONAL COOPERATION AGENCY | |
| THE MODEL INFRASTRUCTURE IMPROVEMENT WORKS FOR ACADEMIC DEVELOPMENT OF THE GRADUATE PROGRAM THE FACULTY OF AGRICULTURAL ENGINEERING AND TECHNOLOGY INSTITUT PERTANIAN BOGOR | |
| CROSS SECTION OF THE CIHIDEUNG RIVER (1/2) | |
| PREPARED BY | DRAWING NO. |
| CHECKED BY | C2-2 |

DL 218.00

DL 208.00

| |
|---------------|
| 70.00 |
| -67.14-22.94 |
| -61.33-212.97 |
| -60.46-215.14 |

| |
|---------------|
| 53.06-212.44 |
| -50.00 |
| -48.41-212.82 |

CANAL
TOP OF WEIR

EFFECTIVE WIDTH 32m
UPSTREAM SIDE
DOWNSTREAM SIDE

L-16.8m from R6

R No.6

DL 218.00

R No.7

L-20m from R7

R No.7

DL 208.00

WL-210.7m

| |
|-------|
| 70.00 |
|-------|

| |
|----------------|
| -65.98-217.747 |
| -65.54-217.857 |
| -62.94-216.257 |

| |
|---------------|
| 53.06-212.44 |
| -50.00 |
| -48.41-212.82 |

| |
|---------------|
| -210.69 |
| -40.00-210.71 |
| -210.98 |

| |
|---------------|
| 30.00-209.72 |
| -20.00-210.04 |
| -10.00-209.75 |

| |
|-------------|
| -209.70 |
| 0.00-212.27 |
| 50.00 |

| |
|-----------|
| ELEVATION |
| DISTANCE |

| |
|-------|
| 50.00 |
|-------|

| |
|---------------|
| 40.23-210.91 |
| -39.10-212.91 |
| 35.41-212.88 |

| |
|---------------|
| 30.05-212.93 |
| -32.88-209.24 |
| 30.00-209.10 |

| |
|-------------|
| 20.00-208.9 |
|-------------|

| |
|-----------|
| ELEVATION |
| DISTANCE |

No.6 SECTION S-1:200

EL 212.771

R No.5

W=49m

210.95

Down El 211.6

R No.5

37m from R No.5

0 5 10 20m
S 1:200

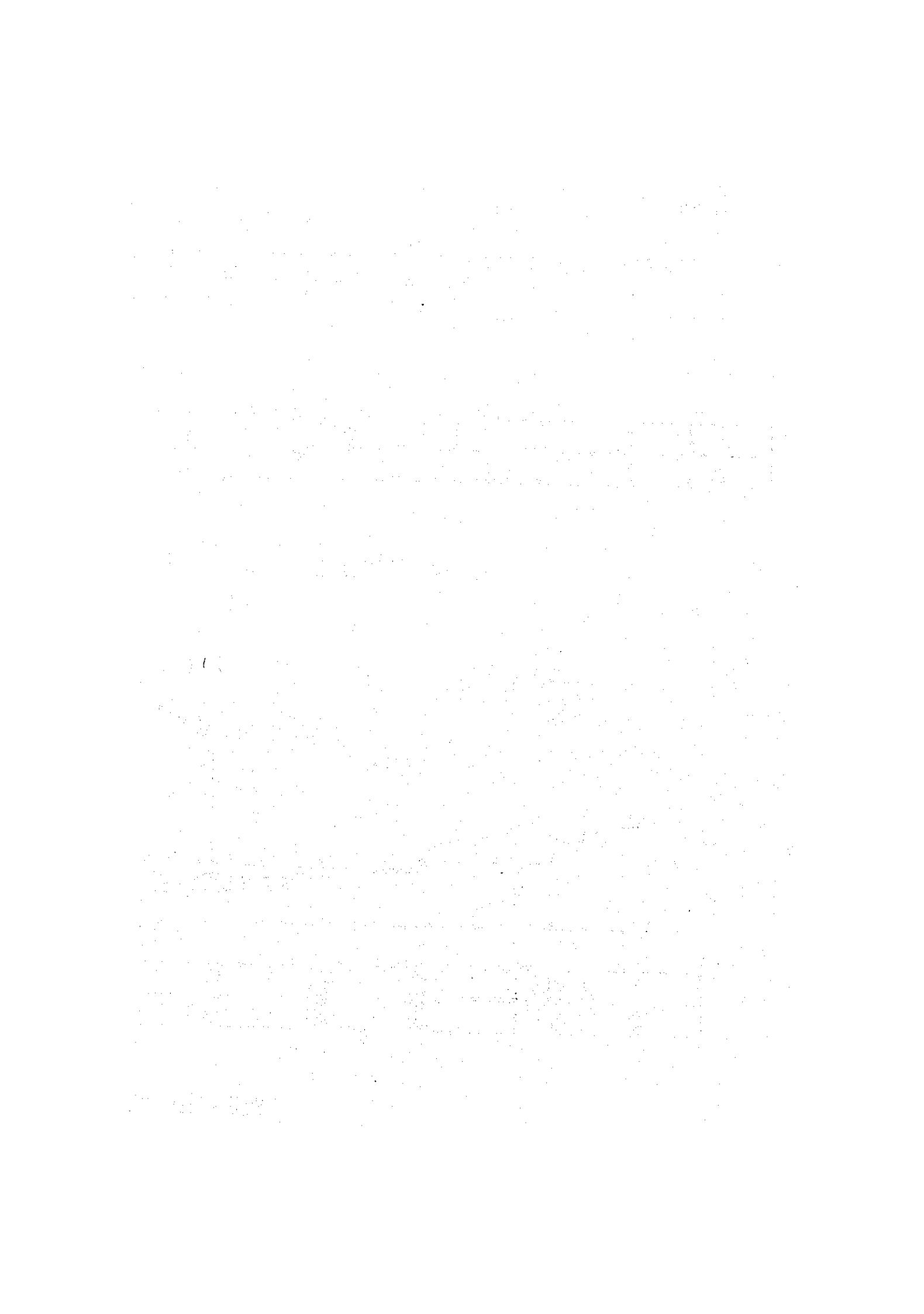
JAPAN INTERNATIONAL COOPERATION AGENCY

THE MODEL INFRASTRUCTURE IMPROVEMENT WORKS
FOR
ACADEMIC DEVELOPMENT OF THE GRADUATE PROGRAM
THE FACULTY OF AGRICULTURAL ENGINEERING AND TECHNOLOGY
INSTITUT PERTANIAN BOGOR

CROSS SECTION OF THE CIHIDEUNG
RIVER (2/2)

PREPARED BY
CHECKED BY

DRAWING NO.
C2-3



付属資料 C 3 土質

1. General
2. Result

Fig. C3-1 Grain Size Accumulation Curve
Fig. C3-2 Plasticity Chart

Table C3-1 Results of Soil Physical Characteristics Determination

1. General

During the field survey, one test pit with dimensions of 1.5 m width, 1.5 m length and 1.0 m depth was digged at the south west part of the coconut trees growing area.

Two soil samples were taken from 0.5 m (No. 1) and 1.0 m (No. 2) depth and tested the soil mechanic characteristics at the Soil Laboratory of Soil Physics and Mechanics, Faculty of Agricultural Technology, IPB Darmaga Campus.

The tested items were :

- (1) mechanical analysis including measurement of soil moisture ratio, hydrometer test and grading by sieve
- (2) plastic limit and liquid limit

The test was carried out by Messers M. Azron D., Asep. S., Erizal who are counterparts of JICA Expert Dr. Seiji Sudo.

2. Result

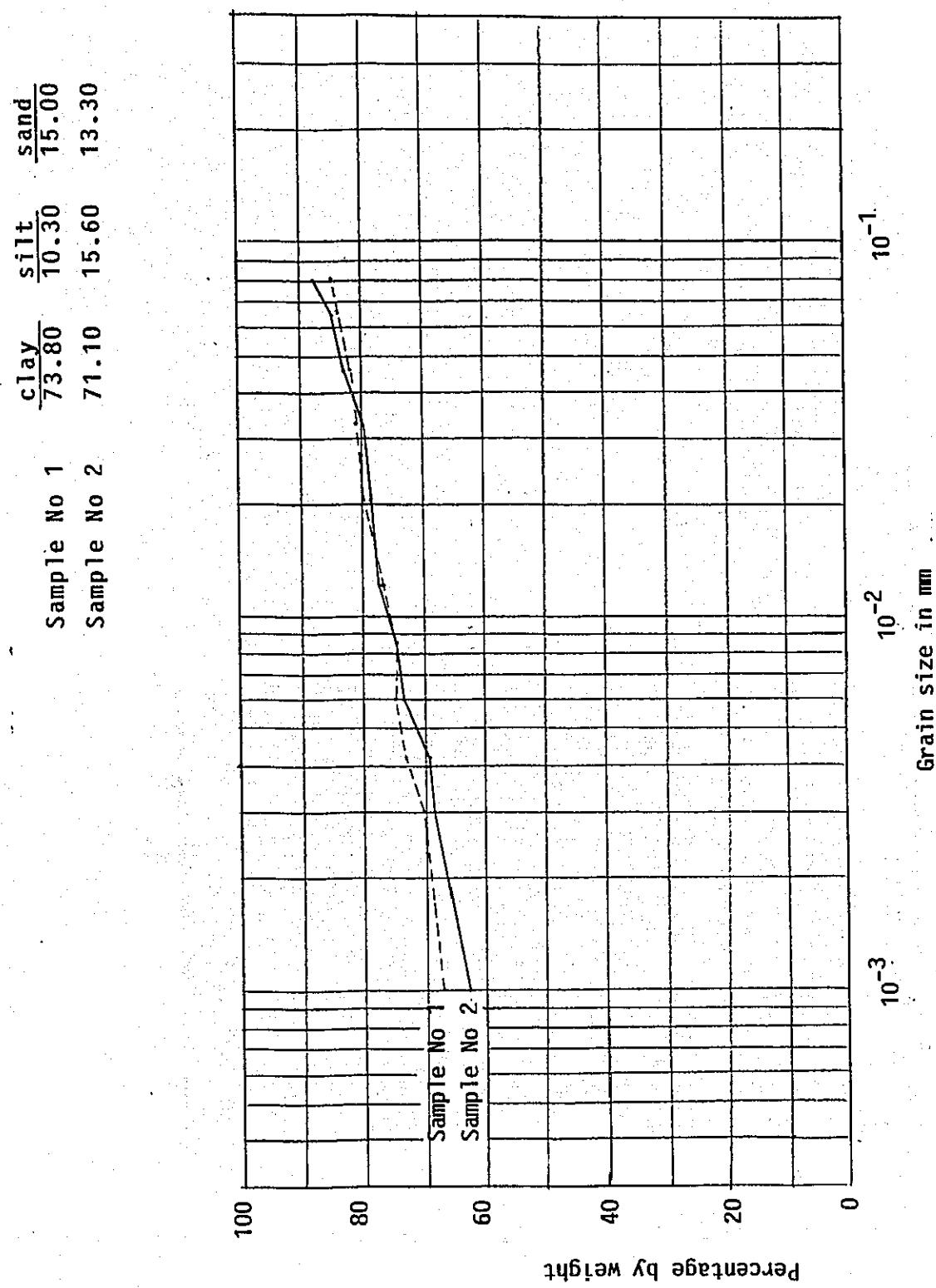
The test results have been arranged in Table C3-1 and Fig. C3-1 and Fig. C3-2.

As seen from the data, the soil has been classified as volcanic cohesive soil with high liquid limit (VH2).

Table C3-1 Results of soil Physical Characteristics Determinations

| Location : | Leuwikopo, IPB Darmaga Campus Bogor | |
|---|-------------------------------------|-------|
| Characteristics | Sample No. | |
| | 1 | 2 |
| 1. Natural water content, W_n (by weight, %) | 59.70 | 62.34 |
| 2. Atterberg limit : | | |
| Air dried soil : | | |
| - Plastic limit, W_p (%) | 60.92 | 63.54 |
| - Liquid limit, W_l (%) | 84.10 | 85.80 |
| - Plasticity index, IP (%) | 23.18 | 22.26 |
| Fresh soil : | | |
| - Plastic limit, W_p (%) | 59.67 | 63.52 |
| - Liquid limit, W_l (%) | 85.70 | 91.00 |
| - Plasticity index, IP (%) | 26.03 | 27.48 |
| Plasticity Chart : Volcanic cohesive soil (VH2) | | |
| 3. Specific gravity, G_s | 2.64 | 2.70 |
| 4. Texture (JSF Grading) : | | |
| - Plastic limit, W_p (%) | 73.80 | 71.10 |
| - Liquid limit, W_l (%) | 10.30 | 15.60 |
| - Plasticity index, IP (%) | 15.90 | 13.30 |
| Triangle coordinates : fine soil, F | | |
| 5. Data sheets : enclosed | | |

Fig C3 - 1 Grain size accumulation curve



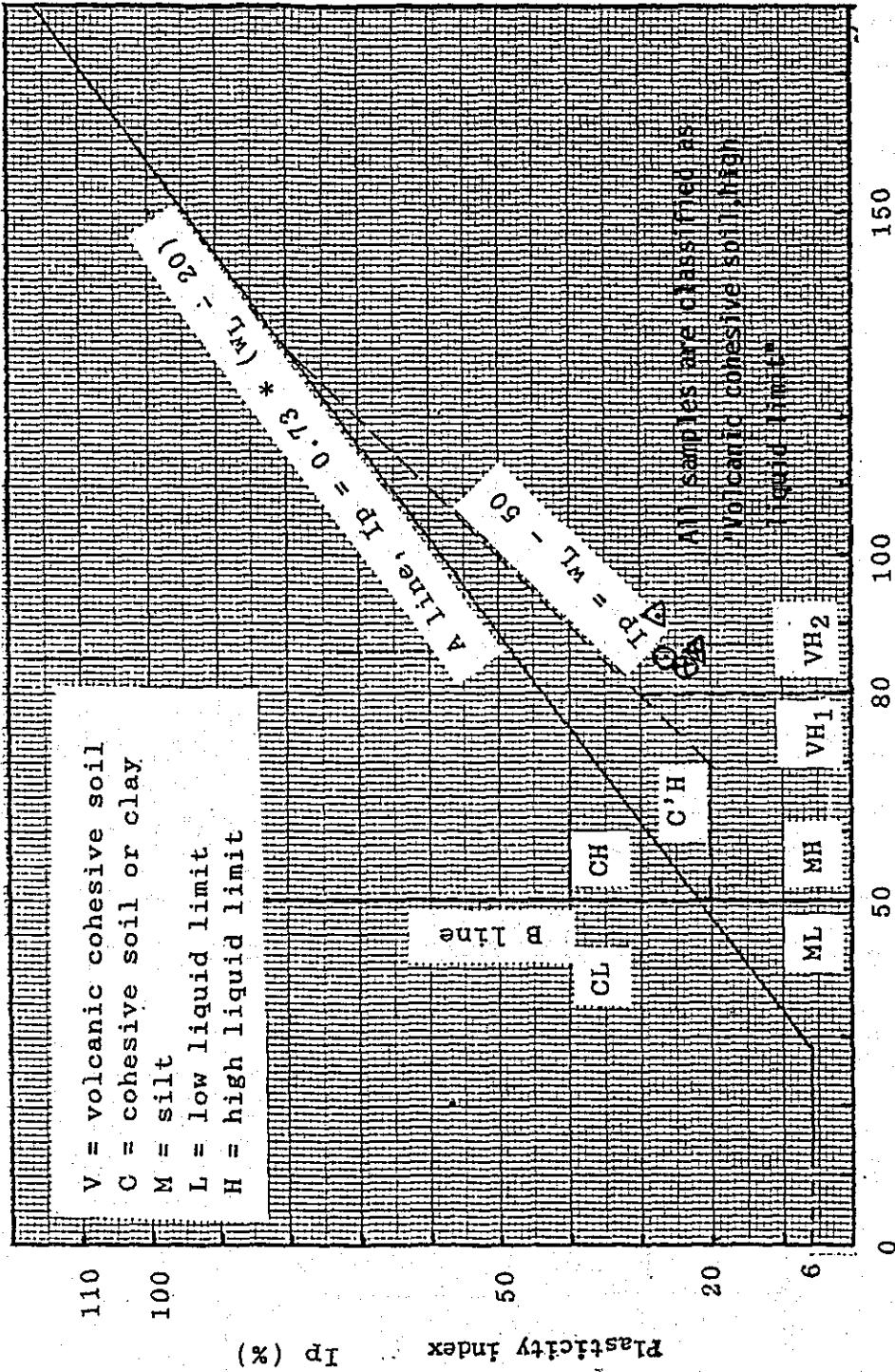


Fig C3 - 2 plasticity chart

付属資料 C 4 滞溉排水

1. Determination of the basic years for planning and design of irrigation facilities
2. Calculation of crop water requirements
 - 2.1 Reference crop evaporation
 - 2.2 Cropping plan on irrigation experiment fields
 - 2.3 Crop Coefficients (K_c)
 - 2.4 Crop Water requirements
3. Calculation of Water Balance
4. Drainage plan

Table C4-1 Calculation of Probability of Non Exceedance on Dry Season Rainfall at the CSDB : 4 months, July, August, September, October

C4-2 Calculation of Probability of Non Exceedance on Annual Rainfall at the CSDB

C4-3 Calculation of Probability of Exceedance on Annual Rainfall at the CSDB

C4-4 Estimated Reference Evapotranspiration : ETo by applying FAO : Pan Evaporation Method

C4-5 Estimated Crop Water Requirements of the Experimental Farm by applying FAO : Pan Evaporation Method (Case A)

C4-6 Estimated Crop Water Requirements of the Experimental Farm by applying FAO : Pan Evaporation Method (Case B)

C4-7 Calculation of Water Balance in the Wet year of 1977 which is corresponding to 5 years Return Period in the Probability of Exceedance for Data of Annual Rainfall at the CSDB (Case A)

C4-8 Calculation of Water Balance in the Dry year of 1988 which is corresponding to 5 years Return Period in the Probability of Non Exceedance for Data of Annual Rainfall at the CSDB (Case A)

C4-9 Calculation of Water Balance in the Wet year of 1977 which is corresponding to 5 years Return Period in the Probability of Exceedance for Data of Annual Rainfall at the CSDB (Case B)

C4-10 Calculation of Water Balance in the Dry year of 1988 which is corresponding to 5 years return Period in the Probability of Non Exceedance for Data of Annual Rainfall at the CSDB (Case B)

1. Determination of the basic years for planning and design of irrigation facilities

Probability analyses have been made on the dry season rainfall of 4 months : July, August, September, October and annual rainfall obtained data at the Climatological Station Darmaga Bogor (CSDB), by the Iwai method as shown in Tables C4-1 to 3, respectively. As the results, the years of 1988 and 1977 have been decided as the basic years for irrigation planning and design.

It has been found that the year of 1988 is regarded as the dry year having the probability of non-exceedance with 5 years return period for annual rainfall but with 10 years return period for dry season rainfall, while the year of 1977 as the wet year having the probability of exceedance with 5 years return period for annual rainfall but having the probability of non-exceedance with 6 years return period for dry season rainfall.

Moreover, the longest dry consecutive days during one year have been calculated with the negligence of a light rain less than 5 mm/day based on the daily rainfall data of 13 years from 1977 through 1989 obtained at the CSDB and arranged as follows :

The Longest Dry Consecutive Days during One Year at the CSDB

| Year | Days | Period | Remarks |
|----------|------|---------------------------|------------|
| 1977 | 23 | 3 to 25 July | Basic year |
| 1978 | 10 | 15 to 24 July | |
| 1979 | 19 | 6 to 25 May | |
| 1980 | 15 | 19 August to 2 September | |
| 1981 | 15 | 5 to 19 August | |
| 1982 | 34 | 15 August to 17 September | Maximum |
| 1983 | 20 | 23 July to 11 August | |
| 1984 | 18 | 16 June to 3 July | |
| 1985 | 9 | 8 to 20 December | Minimum |
| 1986 | 10 | 15 to 24 August | |
| 1987 | 25 | 3 to 27 August | |
| 1988 | 21 | 22 August to 11 September | Basic year |
| 1989 | 17 | 15 April to 1 May | |
| Mean | 18.1 | | |
| σ | 6.6 | | |

The probability of non-exceedance for the above data is also analyzed with the Gamble method. It was found that the years of 1977 and 1988 correspond to the return period of 4 years and 3 years, respectively.

From the above, it was concluded that the decided basic years are adequate to use for irrigation planning and design of this project.

2. Calculation of crop water requirements

Crop water requirements of upland crops and paddy were estimated by applying FAO : Pan Evaporation Method : Irrigation & Drainage paper No.24 to the evaluated data of the observation records at the CSDB. Most of the data are shown in Appendix C1 Climate.

2.1 Reference crop evapotranspiration

Probability of non-exceedance on the data of monthly mean pan evaporation has been analyzed with the application of the Iwai method. The results are as follows :

| Reference crop evapotranspiration (unit : mm/day) | | | | | |
|---|---------------|-------|-----------|---------------|-------|
| | Return Period | | | Return Period | |
| | 5-yr | 10-yr | | 5-yr | 10-yr |
| January | 3.0 | 3.4 | July | 3.6 | 3.9 |
| February | 3.4 | 3.7 | August | 4.1 | 4.5 |
| March | 3.6 | 4.0 | September | 4.4 | 4.9 |
| April | 3.7 | 4.0 | October | 4.3 | 4.7 |
| May | 3.5 | 3.8 | November | 4.0 | 4.3 |
| June | 3.4 | 3.6 | December | 3.6 | 3.8 |

Reference crop evapotranspiration ETo has been estimated using the data of monthly mean temperature, wind velocity, relative humidity and the pan evaporation with 10 years return period.

The Class A evaporation pan has been placed in the dry surface area at the windward side distance of about 25 m at the CSDB, therefore the pan factor (K_p) to be used in the calculation was decided to be 0.79 throughout one year.

The estimated reference crop evaporation ETo are shown on Table C4-4.

2.2 Cropping plan on irrigation experiment fields

With consideration to the natural climate of Bogor area, cropping plans were studied for upland experiment fields of 5,500 m² and paddy experiment fields of 3,150 m², respectively.

Two kinds of cropping have been chosen for this study. The former consists of 3 times upland cropping on upland fields and 3 times paddy cropping on paddy fields in one year as Case A, and the later is comprised of 3 times upland cropping on upland fields and 2 times paddy cropping in the rainy season and 1 time upland cropping in the dry season on paddy field as Case B.

From the tendency of rainfall distribution, it was found that the start of paddy cropping will be at the beginning of November, so, this has been taken into the both cases.

Paddy variety is assumed to be the improved varieties such as Cisadane, Knung Aceh, of which the growing periods are 130 - 140 days.

Corn of 133 days, fruit vegetable of 133 days (such as cucumber, eggplant, melons, tomatoes and peppers) and soybeans of 92 days are chosen for upland cropping on upland fields.

Also, soybeans of 92 days are selected as the dry season crop on the paddy field.

2.3 Crop coefficients (K_c)

The crop growing season has been divided into four stages, those are, (1) initial stage, (2) crop development stage, (3) mid-season stage and (4) late season stage. In referring Fig. 7, Table 21 & 22 in the said FAO : I & D Papers

No.24, the following crop coefficients have been applied to the calculation of crop water requirements :

| | Corn (133) | Fruit, Vegetable (133) | Soybeans (92) | Paddy (102) |
|----------------------------|--------------|---------------------------|---------------|-------------|
| (1) Initial stage | 0.5 (20) | 0.5 (31) | 0.5 (15) | 1.1 (25) |
| (2) Crop development stage | 0.75 (41) | 0.78 (41) | 0.75 (16) | 1.1 (26) |
| (3) Mid-season stage | 1.05 (41) | 1.05 (40) | 1.0 (30) | 1.05 (25) |
| (4) Late-season stage | 1.0-0.55(31) | 0.93-0.6(21) | 0.9-0.45(31) | 0.95 (26) |

Note : 1. Parentheses () show the growing days for each stage of crops.
 2. Paddy is given the figures after transplanting.

2.4 Crop water requirements

The calculation of crop water requirements has been tabulated for the above two Cases as shown in Table C4-5 and C4-6.

In the calculation, percolation of the paddy field is assumed to be 2 mm/day throughout one year. Also, the necessary water for land preparation and paddling practice before transplanting of seedling is assumed to be 250 mm during 10 days or 5 days. Seedling age may be 20 to 25 days olds.

3. Calculation of water balance

In order to check the status of water balance after construction of irrigation and drainage facilities and to find the adequacy of the designed farm pond capacity (1,000 m³) and the necessity of supplemental pumping irrigation water supply from the Cihidung river, the calculation of water balance has been made for every pentad period throughout one year by dividing two cases : Case A & B and two basic years : 1988 & 1977, as shown in Table C4-7 to 10.

After deduction of effective rainfall, crop requirements of upland and paddy crops : Column (5) & (6) in the Tables have been calculated for every pentad period throughout one year of 1988 & 1977 with the following assumptions :

- (1) If daily rainfall is less than 5 mm, the effective rainfall for crops is regarded as zero.
- (2) If daily rainfall is more than 5 mm and less than the estimated crop water requirements, the difference is to be irrigated.
- (3) If daily rainfall is equal to or more than the estimated crop water requirements, irrigation is not required.

Irrigation requirements of upland field : Column (9) in the Tables were calculated for 5,500 m² including the tractor test field by multiplying the above crop requirements and by dividing 60 % of irrigation efficiency and 95 % of conveyance efficiency.

Irrigation requirements of paddy field : Column (10) in the Tables were calculated for 3,150 m² of paddy field including lysimeter are by multiplying the above crop requirements and by dividing 95 % of conveyance efficiency.

The catchment area of the farmpond has been designed to be 24,100 m² in total on the topographic survey drawing, which includes 5,400 m² of the tractor test road, 5,700 m² of the tractor test field, 7,700 m² of the irrigation experiment field (paddy), the lysimeter area and the farm pond, and 5,300 m² of the irrigation experiment field (upland crops). However the effective catchment area of the farm pond has been estimated to be 21,000 m² nearly equal to 90 % of the designed area, with the safety side consideration.

Rainfall on the catchment area will be drained to the designed drainage canal and led to the farm pond.

The run-off to the pond in each pentad period is estimated from the daily rainfall records in 1988 and 1977 with the following assumptions :

1. Total rainfall in the pentad (5-day as normal, 6-day is the last pentad of the month having 31 days, 3-or 4-day is the last pentad of February) is considered as the source of run-off to the farm pond.
2. If the pentad rainfall is less than the Product of 3 mm/day multiplying the number of the days in the pentad, the run-off to the pond is regarded as zero.
3. If the pentad rainfall is more than the above Product, the run-off to the pond is calculated as 60 % to the amount over the Product.

The calculation of water balance have been made in the following manner :

1. Calculate the Water Volume : the carried over pond volume (Column 12) from the previous pentad plus the run-off (Column 8) minus the irrigation requirements (Column 11) in the pentad,
2. If Water Volume is less than 1,000 m³ of the pond capacity, the Water Volume will be stored in the farm pond,
3. If Water Volume is more than 1,000 m³, the exceed water volume will be spilled out, and
4. If Water Volume becomes minus, the water shortage will be filled by the Cihidung pump.

The maximum water shortage was found to be 486 m³ in the 1st pentad July, 1988 (Case B, Table C4-8). Based on this figure, the required pump capacity at the Cihidung river may be with the assumption of 9 hr pump operation in one day :

$$\text{Req. Capacity} = \frac{486 \text{ m}^3}{5 \text{ day} \times 9 \text{ hr}} = 10.8 \text{ m}^3/\text{hr} = 0.18 \text{ m}^3/\text{min.} = 3 \text{ lit/sec.}$$

The following table is the recapitulation of water balance calculation.

| | | Case A | | Case B | |
|-----------------------------------|----------------|--------|--------|--------|--------|
| | | 1977 | 1988 | 1977 | 1988 |
| 1. Rainfall | mm | 4,338 | 3,189 | 4,338 | 3,189 |
| 2. Crop Water Requirements. | | | | | |
| upland | mm | 664 | 707 | 664 | 707 |
| paddy | mm | 1,456 | 1,853 | 950 | 1,275 |
| 3. Run-off to Pond | | | | | |
| mm | | 2,065 | 1,390 | 2,065 | 1,390 |
| m ³ | | 43,365 | 29,190 | 43,365 | 29,190 |
| 4. Irrigation Water Requirements. | | | | | |
| upland | m ³ | 6,412 | 6,831 | 6,412 | 6,831 |
| paddy | m ³ | 4,820 | 6,133 | 3,147 | 4,222 |
| Total | | 11,232 | 12,964 | 9,559 | 11,053 |
| 5. Water Shortage | m ³ | 1,421 | 2,395 | 415 | 1,187 |
| 6. Spillout Water | m ³ | 32,686 | 18,080 | 33,353 | 18,783 |
| 7. Pump Operation | hr | 133 | 224 | 38 | 112 |
| 8. Number of Full Storage of Pond | | 10 | 10 | 11 | 9 |
| 9. Full storage of Pond | | | | | |
| No. of pentad | | 36 | 31 | 39 | 34 |
| Percentage in the year | | 50 | 43 | 54 | 47 |

Table C4 - 1 Calculation of Probability of Non Exceedance on Dry Season Rainfall
at the CSDB , for 4 months period : July,August,September,October

IWAI METHOD

DATA N=26.

D(1)=977. 1964
D(2)=676. 1965
D(3)=509. 1966
D(4)=680. 1967
D(5)=1120. 1968
D(6)=930. 1969
D(7)=1052. 1970
D(8)=1343. 1971
D(9)=390. 1972
D(10)=1377. 1973
D(11)=1740. 1974
D(12)=1460. 1975
D(13)=718. 1976
D(14)=695. 1977
D(15)=1688. 1978
D(16)=1244. 1979
D(17)=1210. 1980
D(18)=1357. 1981
D(19)=649. 1982
D(20)=1188. 1983
D(21)=1359. 1984
D(22)=1338. 1985
D(23)=1135. 1986
D(24)=801. 1987
D(25)=609. 1988
D(26)=999. 1989

RANKING & PLOTTING POSITION

P. OF NON-EXCEEDANCE
RANK DATA WEIBULL PLOT%

(I) (X) $I/(N+1)$ P=1-F
1. 390. 3.7 96.3
2. 509. 7.4 92.6
3. 609. 11.1 88.9
4. 649. 14.8 85.2
5. 676. 18.5 81.5
6. 680. 22.2 77.8
7. 695. 25.9 74.1
8. 718. 29.6 70.4
9. 801. 33.3 66.7
10. 930. 37. 63.
11. 977. 40.7 59.3
12. 999. 44.4 55.6
13. 1052. 48.1 51.9
14. 1120. 51.9 48.1
15. 1135. 55.6 44.4
16. 1188. 59.3 40.7
17. 1210. 63. 37.
18. 1244. 66.7 33.3
19. 1338. 70.4 29.6
20. 1343. 74.1 25.9
21. 1357. 77.8 22.2
22. 1359. 81.5 18.5
23. 1377. 85.2 14.8
24. 1460. 88.9 11.1
25. 1688. 92.6 7.4
26. 1740. 96.3 3.7

CALCULATION

SUM X= 27244.
MEAN X= 1047.846154
SUM OF DEVIATION SQUARE
S=3291903.385
VARIANCE S/N=126611.67
 $S/(N-1)=131676.1354$
 $SD=\sqrt{S/(N-1)}=355.825$
 $USD=\sqrt{S/(N-1)}=562.872$
SKEWNESS CFT. CS1=0.0322
UNBIASED S.C. CS1=0.0316

MEAN LOG(XI)=2.991806788
XG=981.31

CAL. OF B-VALUE

1. T=1740. S=390.
B(1.)=1698.944415
2. T=1688. S=509.
B(2.)=442.7737695
3. T=1460. S=609.
B(3.)=694.0150038

MEAN B=945.24

USED B=945.24

X0=1015.38

LOG(X0+B)=3.29239

$1/A=0.11456$ SX=0.07957

IWAI FORMULA

$$\text{LOG}(Y+(945.24))=3.29239$$

$$-0.11456*KSI$$

PROBABILITY IWAI

| | | | |
|-------|--------|--------|-------------------------|
| Y(2) | 1015.4 | Y(25) | 469.1 |
| Y(3) | 964. | Y(50) | 391.5 |
| Y(4) | 783.6 | Y(100) | 325.2 |
| Y(5) | 730.5 | Y(200) | 267.4 |
| Y(6) | 690.9 | Y(300) | 236.8 |
| Y(7) | 661.4 | Y(400) | 216.2 |
| Y(8) | 636.8 | Y(500) | 201. |
| Y(9) | 616. | | |
| Y(10) | 598.5 | | |
| Y(11) | 583.1 | | |
| Y(12) | 569.5 | | |
| Y(13) | 557.4 | | |
| Y(15) | 536.6 | | 1977 Return period T= 6 |
| Y(16) | 527.5 | | |
| Y(17) | 519.1 | | 1988 Return period T=10 |
| Y(18) | 511.4 | | |
| Y(19) | 504.1 | | |
| Y(20) | 497.4 | | |
| Y(22) | 485.1 | | |
| Y(24) | 474.1 | | |
| Y(26) | 464.4 | | |
| Y(28) | 455.4 | | |
| Y(30) | 447.4 | | |

**Table C4 - 2 Calculation of Probability of Non-Exceedance
on Annual Rainfall at the CSDB**

IWAI METHOD

DATA N=26.
 D(1)=3573. 1964
 D(2)=3405.
 D(3)=2175.
 D(4)=3295.
 D(5)=3245.
 D(6)=3734.
 D(7)=3396.
 D(8)=4003.
 D(9)=2909.
 D(10)=5048.
 D(11)=4210.
 D(12)=4252.
 D(13)=3269.
 D(14)=4338.
 D(15)=4671.
 D(16)=3916.
 D(17)=4330.
 D(18)=4068.
 D(19)=3651.
 D(20)=3226.
 D(21)=4082.
 D(22)=3664.
 D(23)=4234.
 D(24)=5417.
 D(25)=3189.
 D(26)=4078. 1989
 RANKING & PLOTTING POSITION

P. OF NON-EXCEEDANCE
 RANK DATA WEIBULL PLOT%
 (I) (X) 1/(N+1) P=1-F
 1. 2175. 3.7 96.3
 2. 2909. 7.4 92.6
 3. 3189. 11.1 88.9
 4. 3226. 14.8 85.2
 5. 3245. 18.5 81.5
 6. 3269. 22.2 77.8
 7. 3295. 25.9 74.1
 8. 3573. 29.6 70.4
 9. 3396. 33.3 66.7
 10. 3405. 37. 63.
 11. 3417. 40.7 59.3
 12. 3651. 44.4 55.6
 13. 3664. 48.1 51.9
 14. 3734. 51.9 48.1
 15. 3916. 55.6 44.4
 16. 4003. 59.3 40.7
 17. 4082. 63. 37.
 18. 4078. 66.7 33.3
 19. 4082. 70.4 29.6
 20. 4210. 74.1 25.9
 21. 4234. 77.8 22.2
 22. 4252. 81.5 18.5
 23. 4330. 85.2 14.8
 24. 4338. 88.9 11.1
 25. 4571. 92.6 7.4
 26. 5048. 96.3 3.7

CALCULATION
 SUM X= 97178.
 MEAN X= 3737.615385
 SUM OF DEVIATION SQUARE
 S=9304984.154
 VARIANCE S/N=357884.01
 S/(N-1)=372199.3662
 SD/(MEAN X)=0.16
 SD=√(S/N)=598.234
 USD=√(S/(N-1))=610.081
 SKEWNESS CFT. CSI=-0.208
 3
 UNBIASED S.C. CSI=-0.204
 3

MEAN LOG(XI)=3.56662142
 XG=3686.56

CAL. OF B-VALUE
 1. T=5048. S=2175.
 B(1.)=-17394.91496
 2. T=4671. S=2909.
 B(2.)=13.46497293
 3. T=4338. S=3189.
 B(3.)=-1580.175243

MEAN B=-6320.54

USED B=0.
 X0=3686.56
 LOG(X0+B)=3.56662
 1/A=0.10629 SX=0.07377

IWAI FORMULA
 $\log(Y+(0.))=3.56662$
 $-0.10629*KSI$

PROBABILITY IWAI
 Y(2) 3686.5
 Y(3) 3421.7
 Y(4) 3280.4
 Y(5) 3186.9
 Y(10) 2953.2
 Y(20) 2773.4
 Y(25) 2722.9
 Y(50) 2584.
 Y(100) 2464.8

Table C4 - 3 Calculation of Probability of Exceedance
on Annual Rainfall at the CSDB

RANKING & PLOTTING POSITION

| P. OF EXCEEDANCE | | |
|------------------|-------|-----------------------|
| RANK | DATA | WEIBULL PLOT% |
| (J) | (X) | $J/(N+1) \quad F=1-P$ |
| 1. | 5048. | 3.7 96.3 |
| 2. | 4671. | 7.4 92.6 |
| 3. | 4338. | 11.1 88.9 |
| 4. | 4330. | 14.8 85.2 |
| 5. | 4252. | 18.5 81.5 |
| 6. | 4234. | 22.2 77.8 |
| 7. | 4210. | 25.9 74.1 |
| 8. | 4082. | 29.6 70.4 |
| 9. | 4078. | 33.3 66.7 |
| 10. | 4068. | 37. 63. |
| 11. | 4003. | 40.7 59.3 |
| 12. | 3916. | 44.4 55.6 |
| 13. | 3734. | 48.1 51.9 |
| 14. | 3664. | 51.9 48.1 |
| 15. | 3651. | 55.6 44.4 |
| 16. | 3417. | 59.3 40.7 |
| 17. | 3405. | 63. 37. |
| 18. | 3396. | 66.7 33.3 |
| 19. | 3373. | 70.4 29.6 |
| 20. | 3295. | 74.1 25.9 |
| 21. | 3269. | 77.8 22.2 |
| 22. | 3245. | 81.5 18.5 |
| 23. | 3226. | 85.2 14.8 |
| 24. | 3189. | 88.9 11.1 |
| 25. | 2909. | 92.6 7.4 |
| 26. | 2175. | 96.3 3.7 |

PROBABILITY IWAI

| | |
|--------|--------|
| Y(2) | 3686.5 |
| Y(3) | 3971.9 |
| Y(4) | 4143. |
| Y(5) | 4264.5 |
| Y(10) | 4601.9 |
| Y(20) | 4900.4 |
| Y(25) | 4991.2 |
| Y(50) | 5259.6 |
| Y(100) | 5514. |

CALCULATION

SUM X= 97178.

MEAN X= 3737.615385

SUM OF DEVIATION SQUARE

S=9304984.154

VARIANCE S/N=357884.01

S/(N-1)=372199.3662

SD/(MEAN X)=0.16

SD=√(S/N)=598.234

USD=√(S/(N-1))=610.081

SKEWNESS CFT. CS1=-0.208

3

UNBIASED S.C. CS1=-0.204

3

MEAN LOG(XI)=3.56662142

XG=3686.56

CAL. OF B-VALUE

1. T=5048. S=2175.

B(1.)=-17394.91496

2. T=4671. S=2909.

B(2.)=13.46497293

3. T=4338. S=3189.

B(3.)=-1580.175243

MEAN B=-6320.54

Table C4-4 Estimated Reference Crop Evapotranspiration : ETo by applying FAO:
Pan Evaporation Method

| | Jan. | Feb. | Mar. | Apr. | May | Jun. | Jul. | Aug. | Sep. | Oct. | Nov. | Dec. | Remarks |
|--|------|------|------|------|------|------|------|------|------|------|------|------|---|
| 1. Monthly Mean Temp. (°C) | 24.8 | 24.9 | 25.2 | 25.6 | 25.8 | 25.7 | 25.2 | 25.3 | 25.6 | 25.9 | 25.7 | 25.3 | 1977-1989 |
| 2. Wind Velocity | | | | | | | | | | | | | |
| a. 0.5 m height (km/day) | 1.71 | 2.09 | 2.15 | 1.75 | 1.67 | 1.55 | 1.85 | 1.79 | 1.93 | 1.93 | 1.96 | 2.10 | 1972-1989 |
| b. Corrected at 2 m height (km/day) | 55 | 68 | 70 | 57 | 54 | 50 | 60 | 58 | 63 | 63 | 64 | 68 | Factor 1.35 |
| 3. R. H. mean (%) | 90 | 88 | 88 | 87 | 86 | 84 | 82 | 82 | 83 | 83 | 85 | 87 | 1971-1989 |
| 4. Pan Factor (Kp) | 0.79 | 0.79 | 0.79 | 0.79 | 0.79 | 0.79 | 0.79 | 0.79 | 0.79 | 0.79 | 0.79 | 0.79 | FAO Case B-D=25 m RH > 70 % Kp = 0.79 |
| 5. Pan Evaporation (mm/day) | 3.4 | 3.7 | 4.0 | 4.0 | 3.8 | 3.6 | 3.9 | 4.5 | 4.9 | 4.7 | 4.3 | 3.8 | T = 10 Yr n = 13 |
| 6. ETo (mm/day) | 2.7 | 2.9 | 3.2 | 3.2 | 3.0 | 2.8 | 3.1 | 3.6 | 3.9 | 3.7 | 3.4 | 3.0 | |

Table C4-5 Estimated Crop Water Requirements of the Experimental Farm by applying FAO:
 Pan Evaporation Method (Case A)

| Upland Field : 3 cropping, Paddy Field : 3 cropping No. 1 | | | | | | | | | | | | | | | | | | | | |
|--|--------|---------------------------|----------------|----------------|---------------|----------------|----------------|---------------|-------------|--------------|--------|---------------------------|----------------|--------------------|---------------|----------------|----------------|---------------|-------------|-----------------|
| Month | Pentad | Upland Field | | | | Paddy Field | | | | Upland Field | | | | Paddy Field | | | | | | |
| | | ET ₀ mm/day | Growing day | K _c | CWR mm/day | Growing day | K _c | CWR mm/day | P mm/day | Month | Pentad | ET ₀ mm/day | Growing day | K _c | CWR mm/day | Growing day | K _c | CWR mm/day | P mm/day | Total mm/day |
| Nov. | 1 | 3.4 | 5 | 0.5 | 1.7 | - | - | - | - | Feb. | 1 | 2.9 | 97 | 1.05 | 3.0 | 87 | 0.95 | 2.8 | 2 | 4.8 |
| | 2 | 3.4 | 10 | 0.5 | 1.7 | - | - | - | - | | 2 | 2.9 | 102 | 1.05 | 3.0 | 92 | 0.95 | 2.8 | 2 | 4.8 |
| | 3 | 3.4 | 15 | 0.5 | 1.7 | 5 | 1.1 | 3.7 | 2 | | 3 | 2.9 | 105 | 1.00 | 2.9 | 97 | 0.95 | 2.8 | 2 | 4.8 |
| | 4 | 3.4 | 20 | 0.5 | 1.7 | 10 | 1.1 | 3.7 | 2 | | 4 | 2.9 | 110 | 1.00 | 2.9 | 102 | 0.95 | 2.8 | 2 | 4.8 |
| | 5 | 3.4 | 25 | 0.75 | 2.6 | 15 | 1.1 | 3.7 | 2 | | 5 | 2.9 | 115 | 0.9 | 2.6 | 107 | - | - | 0 | 0 |
| | 6 | 3.4 | 30 | 0.75 | 2.6 | 20 | 1.1 | 3.7 | 2 | | 6 | 2.9 | 118 | 0.8 | 2.3 | 110 | - | - | 0 | 0 |
| Dec. | 1 | 3.0 | 35 | 0.75 | 2.3 | 25 | 1.1 | 3.3 | 2 | Mar. | 1 | 3.2 | 123 | 0.7 | 2.2 | 115 | - | - | - | 0 |
| | 2 | 3.0 | 40 | 0.75 | 2.3 | 30 | 1.1 | 3.3 | 2 | | 2 | 3.2 | 128 | 0.6 | 1.9 | - | 2nd paddy | - | 50 | 5.5 |
| | 3 | 3.0 | 45 | 0.75 | 2.3 | 35 | 1.1 | 3.3 | 2 | | 3 | 3.2 | 133 | 0.55 | 1.8 | 5 | 1.1 | 3.5 | 2 | 5.5 |
| | 4 | 3.0 | 50 | 0.75 | 2.3 | 40 | 1.1 | 3.3 | 2 | | 4 | 3.2 | 140 | Fruit Vegetable | 10 | 1.1 | 3.5 | 2 | 5.5 | |
| | 5 | 3.0 | 55 | 0.75 | 2.3 | 45 | 1.1 | 3.3 | 2 | | 5 | 3.2 | 145 | 0.5 | 1.6 | 15 | 1.1 | 3.5 | 2 | 5.5 |
| | 6 | 3.0 | 61 | 0.75 | 2.3 | 51 | 1.1 | 3.3 | 2 | | 6 | 3.2 | 151 | 0.5 | 1.6 | 21 | 1.1 | 3.5 | 2 | 5.5 |
| Jan. | 1 | 2.7 | 66 | 1.05 | 2.8 | 56 | 1.05 | 2.8 | 2 | Apr. | 1 | 3.2 | 16 | 0.5 | 1.6 | 26 | 1.1 | 3.5 | 2 | 5.5 |
| | 2 | 2.7 | 71 | 1.05 | 2.8 | 61 | 1.05 | 2.8 | 2 | | 2 | 3.2 | 21 | 0.5 | 1.6 | 31 | 1.1 | 3.5 | 2 | 5.5 |
| | 3 | 2.7 | 76 | 1.05 | 2.8 | 66 | 1.05 | 2.8 | 2 | | 3 | 3.2 | 26 | 0.5 | 1.6 | 36 | 1.1 | 3.5 | 2 | 5.5 |
| | 4 | 2.7 | 81 | 1.05 | 2.8 | 71 | 1.05 | 2.8 | 2 | | 4 | 3.2 | 31 | 0.5 | 1.6 | 41 | 1.1 | 3.5 | 2 | 5.5 |
| | 5 | 2.7 | 86 | 1.05 | 2.8 | 76 | 1.05 | 2.8 | 2 | | 5 | 3.2 | 36 | 0.78 | 2.5 | 46 | 1.1 | 3.5 | 2 | 5.5 |
| | 6 | 2.7 | 92 | 1.05 | 2.8 | 82 | 0.95 | 2.6 | 2 | | 6 | 3.2 | 41 | 0.78 | 2.5 | 51 | 1.1 | 3.5 | 2 | 5.5 |

Table C4-5 Estimated Crop Water Requirements of the Experimental Farm by applying FAO:
Pan Evaporation Method (Case A)

Upland Field : 3 cropping, Paddy Field : 3 cropping
No. 2

| Month | Pentad | Upland Field | | | | Paddy Field | | | | Upland Field | | | | Paddy Field | | | | Month | Pentad | ET _o mm/day | Growing day | K _c | CWR | P mm/day |
|-------|--------|---------------------------|----------------|----------------|-----|----------------|----------------|-----|-------------|--------------|--------|---------------------------|----------------|----------------|------|-------------|-------|--------|---------------------------|---------------------------|----------------|----------------|-------------|-------------|
| | | ET _o mm/day | Growing day | K _c | CWR | Growing day | K _c | CWR | P mm/day | Month | Pentad | ET _o mm/day | Growing day | K _c | CWR | P mm/day | Month | Pentad | ET _o mm/day | Growing day | K _c | CWR | P mm/day | |
| May | 1 | 3.0 | 46 | 0.78 | 2.3 | 56 | 1.05 | 3.2 | 2 | 5.2 | Aug. | 1 | 3.6 | 5 | 0.5 | 1.8 | 31 | 1.1 | 4.0 | 2 | 6.0 | 2 | 6.0 | |
| | 2 | 3.0 | 51 | 0.78 | 2.3 | 61 | 1.05 | 3.2 | 2 | 5.2 | | 2 | 3.6 | 10 | 0.5 | 1.8 | 36 | 1.1 | 4.0 | 2 | 6.0 | 2 | 6.0 | |
| | 3 | 3.0 | 56 | 0.78 | 2.3 | 66 | 1.05 | 3.2 | 2 | 5.2 | | 3 | 3.6 | 15 | 0.5 | 1.8 | 41 | 1.1 | 4.0 | 2 | 6.0 | 2 | 6.0 | |
| | 4 | 3.0 | 61 | 0.78 | 2.3 | 71 | 1.05 | 3.2 | 2 | 5.2 | | 4 | 3.6 | 20 | 0.75 | 2.7 | 46 | 1.1 | 4.0 | 2 | 6.0 | 2 | 6.0 | |
| | 5 | 3.0 | 66 | 0.78 | 2.3 | 76 | 1.05 | 3.2 | 2 | 5.2 | | 5 | 3.6 | 25 | 0.75 | 2.7 | 51 | 1.1 | 4.0 | 2 | 6.0 | 2 | 6.0 | |
| | 6 | 3.0 | 72 | 0.78 | 2.3 | 82 | 0.95 | 3.2 | 2 | 5.2 | | 6 | 3.6 | 31 | 0.75 | 2.7 | 57 | 1.05 | 4.0 | 2 | 6.0 | 2 | 6.0 | |
| Jun. | 1 | 2.8 | 77 | 1.05 | 2.9 | 87 | 0.95 | 2.7 | 2 | 4.7 | Sep. | 1 | 3.9 | 36 | 1.0 | 3.9 | 62 | 1.05 | 4.1 | 2 | 6.1 | 2 | 6.1 | |
| | 2 | 2.8 | 82 | 1.05 | 2.9 | 92 | 0.95 | 2.7 | 2 | 4.7 | | 2 | 3.9 | 41 | 1.0 | 3.9 | 67 | 1.05 | 4.1 | 2 | 6.1 | 2 | 6.1 | |
| | 3 | 2.8 | 87 | 1.05 | 2.9 | 97 | 0.95 | 2.7 | 2 | 4.7 | | 3 | 3.9 | 46 | 1.0 | 3.9 | 72 | 1.05 | 4.1 | 2 | 6.1 | 2 | 6.1 | |
| | 4 | 2.8 | 92 | 1.05 | 2.9 | 102 | - | - | - | 0 | | 4 | 3.9 | 51 | 1.0 | 3.9 | 77 | 1.05 | 4.1 | 2 | 6.1 | 2 | 6.1 | |
| | 5 | 2.8 | 97 | 1.05 | 2.9 | 107 | - | - | - | 0 | | 5 | 3.9 | 56 | 1.0 | 3.9 | 82 | 0.95 | 3.7 | 2 | 5.7 | 2 | 5.7 | |
| | 6 | 2.8 | 102 | 1.05 | 2.9 | 112 | - | - | - | 0 | | 6 | 3.9 | 61 | 1.0 | 3.9 | 87 | 0.95 | 3.7 | 2 | 5.7 | 2 | 5.7 | |
| Jul. | 1 | 3.1 | 107 | 1.05 | 3.3 | - | 3rd paddy | | | | Oct. | 1 | 3.7 | 66 | 0.9 | 3.3 | 92 | 0.95 | 3.5 | 2 | 5.5 | 2 | 5.5 | |
| | 2 | 3.1 | 112 | 1.05 | 3.3 | 5 | 1.1 | 3.4 | 2 | 5.4 | | 2 | 3.7 | 71 | 0.8 | 3.0 | 97 | 0.95 | 3.5 | 2 | 5.5 | 2 | 5.5 | |
| | 3 | 3.1 | 117 | 0.93 | 2.9 | 10 | 1.1 | 3.4 | 2 | 5.4 | | 3 | 3.7 | 76 | 0.7 | 2.6 | 102 | - | - | - | 0 | - | 0 | |
| | 4 | 3.1 | 122 | 0.82 | 2.5 | 15 | 1.1 | 3.4 | 2 | 5.4 | | 4 | 3.7 | 81 | 0.6 | 2.2 | 107 | - | - | - | 0 | - | 0 | |
| | 5 | 3.1 | 127 | 0.7 | 2.2 | 20 | 1.1 | 3.4 | 2 | 5.4 | | 5 | 3.7 | 86 | 0.5 | 1.9 | 112 | - | - | - | 0 | - | 0 | |
| | 6 | 3.1 | 133 | 0.6 | 1.9 | 26 | 1.1 | 3.4 | 2 | 5.4 | | 6 | 3.7 | 92 | 0.45 | 1.7 | - | - | - | - | - | - | - | |

1. ET_o : Estimated reference crop evapotranspiration by Pan Evaporation Method with Return Period of 10 years.
2. Growing day : Days after planted at the end of the Pentad, as for Paddy the day after transplanting (Seedling 25 days old).

3. K_c : Assumed value in reference to FAO Irrigation and Drainage Paper No.24.
4. CWR : Crop water requirements = ET_o times K_c.

5. Fruit Vegetable : Total growing days of vegetable are as follows : Cucumber 130 days, Egg plant 130 days, Melons 120 days, Tomato 135 days, Peppers 125 days

Table C4-6 Estimated Crop Water Requirements of the Experimental Farm by applying FAO:
Pan Evaporation Method (Case B)

No.1

| Month | Pentad | Upland Field | | | Paddy Field | | | Upland Field | | | Paddy Field | | |
|-------|--------|---------------------------|----------------|------|---------------|----------------|------|---------------|---------------------------|----------------|-------------|---------------|---------------------------|
| | | ET _o mm/day | Growing day | Kc | CWR mm/day | Growing day | Kc | CWR mm/day | ET _o mm/day | Growing day | Kc | CWR mm/day | ET _o mm/day |
| | | | | | | | | | | | | | |
| Nov. | 1 | 3.4 | 5 | 0.5 | 1.7 | - | - | 25 | Feb. | 1 | 2.9 | 97 | 1.05 |
| | 2 | 3.4 | 10 | 0.5 | 1.7 | - | - | 25 | | 2 | 2.9 | 102 | 1.05 |
| | 3 | 3.4 | 15 | 0.5 | 1.7 | 5 | 1.1 | 5.7 | | 3 | 2.9 | 105 | 1.00 |
| | 4 | 3.4 | 20 | 0.5 | 1.7 | 10 | 1.1 | 5.7 | | 4 | 2.9 | 110 | 1.00 |
| | 5 | 3.4 | 25 | 0.75 | 2.6 | 15 | 1.1 | 5.7 | | 5 | 2.9 | 115 | 0.9 |
| | 6 | 3.4 | 30 | 0.75 | 2.6 | 20 | 1.1 | 5.7 | | 6 | 2.9 | 118 | 0.8 |
| Dec. | 1 | 3.0 | 35 | 0.75 | 2.3 | 25 | 1.1 | 3.3 | Mar. | 1 | 3.2 | 123 | 0.7 |
| | 2 | 3.0 | 40 | 0.75 | 2.3 | 30 | 1.1 | 3.3 | | 2 | 3.2 | 128 | 0.6 |
| | 3 | 3.0 | 45 | 0.75 | 2.3 | 35 | 1.1 | 3.3 | | 3 | 3.2 | 133 | 0.55 |
| | 4 | 3.0 | 50 | 0.75 | 2.3 | 40 | 1.1 | 3.3 | | 4 | 3.2 | Fruit | - |
| | 5 | 3.0 | 55 | 0.75 | 2.3 | 45 | 1.1 | 3.3 | | 5 | 3.2 | Vegetable | - |
| | 6 | 3.0 | 61 | 0.75 | 2.3 | 51 | 1.1 | 3.3 | | 6 | 3.2 | 5 | 1.6 |
| Jan. | 1 | 2.7 | 66 | 1.05 | 2.8 | 56 | 1.05 | 2.8 | Apr. | 1 | 3.2 | 16 | 0.5 |
| | 2 | 2.7 | 71 | 1.05 | 2.8 | 61 | 1.05 | 2.8 | | 2 | 3.2 | 21 | 0.5 |
| | 3 | 2.7 | 76 | 1.05 | 2.8 | 66 | 1.05 | 2.8 | | 3 | 3.2 | 26 | 0.5 |
| | 4 | 2.7 | 81 | 1.05 | 2.8 | 71 | 1.05 | 2.8 | | 4 | 3.2 | 31 | 0.5 |
| | 5 | 2.7 | 86 | 1.05 | 2.8 | 76 | 1.05 | 2.8 | | 5 | 3.2 | 36 | 0.78 |
| | 6 | 2.7 | 92 | 1.05 | 2.8 | 82 | 0.95 | 2.6 | | 6 | 3.2 | 41 | 0.78 |

Table C4-6 Estimated Crop Water Requirements of the Experimental Farm by applying FAO :
Pan Evaporation Method (Case B)

No. 2

| Month | Pentad | Upland Field | | | | Paddy Field | | | | Upland Field | | | | Paddy Field | | | |
|-------|--------|---------------------------|----------------|------|---------------|----------------|------|---------------|-------------|--------------|--------|---------------------------|----------------|-------------|---------------|-------------|-----------------|
| | | ET _o mm/day | Growing day | Kc | CWR mm/day | Growing day | Kc | CWR mm/day | P mm/day | Month | Pentad | ET _o mm/day | Growing day | Kc | CWR mm/day | P mm/day | Total mm/day |
| May | 1 | 3.0 | 46 | 0.78 | 2.3 | 46 | 1.1 | 3.3 | 2 | 5.3 | Aug. | 1 | 3.6 | 5 | 0.5 | 1.8 | - |
| | 2 | 3.0 | 51 | 0.78 | 2.3 | 51 | 1.1 | 3.3 | 2 | 5.3 | | 2 | 3.6 | 10 | 0.5 | 1.8 | 1.8 |
| | 3 | 3.0 | 56 | 0.78 | 2.3 | 56 | 1.05 | 3.2 | 2 | 5.2 | | 3 | 3.6 | 15 | 0.5 | 1.8 | 1.8 |
| | 4 | 3.0 | 61 | 0.78 | 2.3 | 61 | 1.05 | 3.2 | 2 | 5.2 | | 4 | 3.6 | 20 | 0.75 | 2.7 | 2.7 |
| | 5 | 3.0 | 66 | 0.78 | 2.3 | 66 | 1.05 | 3.2 | 2 | 5.2 | | 5 | 3.6 | 25 | 0.75 | 2.7 | 2.7 |
| | 6 | 3.0 | 72 | 0.78 | 2.3 | 72 | 1.05 | 3.2 | 2 | 5.2 | | 6 | 3.6 | 31 | 0.75 | 2.7 | 2.7 |
| Jun. | 1 | 2.8 | 77 | 1.05 | 2.9 | 77 | 1.05 | 2.9 | 2 | 4.9 | Sep. | 1 | 3.9 | 36 | 1.0 | 3.9 | 3.9 |
| | 2 | 2.8 | 82 | 1.05 | 2.9 | 82 | 0.95 | 2.7 | 2 | 4.7 | | 2 | 3.9 | 41 | 1.0 | 3.9 | 3.9 |
| | 3 | 2.8 | 87 | 1.05 | 2.9 | 87 | 0.95 | 2.7 | 2 | 4.7 | | 3 | 3.9 | 46 | 1.0 | 3.9 | 3.9 |
| | 4 | 2.8 | 92 | 1.05 | 2.9 | 92 | 0.95 | 2.7 | 2 | 4.7 | | 4 | 3.9 | 51 | 1.0 | 3.9 | 3.9 |
| | 5 | 2.8 | 97 | 1.05 | 2.9 | 97 | 0.95 | 2.7 | 2 | 4.7 | | 5 | 3.9 | 56 | 1.0 | 3.9 | 3.9 |
| | 6 | 2.8 | 102 | 1.05 | 2.9 | 102 | 0.95 | 2.7 | 2 | 4.7 | | 6 | 3.9 | 61 | 1.0 | 3.9 | 3.9 |
| Jul. | 1 | 3.1 | 107 | 1.05 | 3.3 | 107 | - | - | - | - | Oct. | 1 | 3.7 | 66 | 0.9 | 3.3 | 3.3 |
| | 2 | 3.1 | 112 | 1.05 | 3.3 | 110 | - | - | - | - | | 2 | 3.7 | 71 | 0.8 | 3.0 | 3.0 |
| | 3 | 3.1 | 117 | 0.93 | 2.9 | 115 | - | - | - | - | | 3 | 3.7 | 76 | 0.7 | 2.6 | 2.6 |
| | 4 | 3.1 | 122 | 0.82 | 2.5 | - | - | - | - | - | | 4 | 3.7 | 81 | 0.6 | 2.2 | 2.2 |
| | 5 | 3.1 | 127 | 0.7 | 2.2 | - | - | - | - | - | | 5 | 3.7 | 86 | 0.5 | 1.9 | 1.9 |
| | 6 | 3.1 | 133 | 0.6 | 1.9 | - | - | - | - | - | | 6 | 3.7 | 92 | 0.45 | 1.7 | 1.7 |

1. ET_o : Estimated reference crop evapotranspiration by Pan Evaporation Method with Return Period of 10 years.

2. Growing day : Days after planted at the end of the Pentad, as for Paddy the day after transplanting (Seedling 25 days old).

3. K_c : Assumed value in reference to FAO Irrigation and Drainage Paper No.24.

4. CWR : Crop water requirements = ET_o times K_c.

5. Fruit Vegetable : Total growing days of vegetable are as follows : Cucumber 130 days, Egg plant 130 days, Melons 120 days, Tomato 135 days, Peppers 125 days

Table C4-7

Calculation of Water Balance in the Wet year of 1977

which is corresponding to 5 years Return Period

in the Probability of Exceedance for Data of Annual Rainfall at the CSDB. (Case A)

| (1) | (2) | (3) | (4) | (5) | (6) | (7) | (8) | (9) | (10) | (11) | (12) | (13) | (14) | (15) | No. 1 (16) | |
|------|------|-----------|-----|-----|-----|-----|-------|-----|------|------|-------|------|------|-------|---------------|--|
| | | | | | | | | | | | | | | | | |
| 1977 | Jan. | 5 | 42 | 6 | 10 | 16 | 336 | 58 | 33 | 91 | 245 | | | 0 | | |
| | | 5 | 89 | 6 | 10 | 44 | 924 | 58 | 33 | 91 | 1,000 | | | 78 | | |
| | | 5 | 18 | 12 | 20 | 2 | 42 | 116 | 66 | 182 | 860 | | | 0 | | |
| | | 5 | 182 | 0 | 0 | 100 | 2,100 | 0 | 0 | 0 | 1,000 | | | 1,960 | | |
| | | 5 | 102 | 6 | 10 | 52 | 1,092 | 58 | 33 | 91 | 1,000 | | | 1,001 | | |
| | | 6 | 169 | 6 | 10 | 91 | 1,911 | 58 | 33 | 91 | 1,000 | | | 1,820 | | |
| | | Sub-total | 602 | 36 | 60 | 305 | 6,405 | 348 | 198 | 546 | | | | 4,859 | | |
| Feb. | | 5 | 133 | 6 | 10 | 71 | 1,491 | 58 | 33 | 91 | 1,000 | | | 1,400 | | |
| | | 5 | 133 | 3 | 5 | 71 | 1,491 | 29 | 17 | 46 | 1,000 | | | 1,445 | | |
| | | 5 | 128 | 6 | 10 | 68 | 1,428 | 58 | 33 | 91 | 1,000 | | | 1,337 | | |
| | | 5 | 12 | 12 | 20 | 0 | 0 | 116 | 66 | 182 | 818 | | | 0 | | |
| | | 5 | 46 | 6 | 0 | 19 | 399 | 58 | 0 | 58 | 1,000 | | | 159 | | |
| | | 3 | 15 | 3 | 0 | 0 | 0 | 29 | 0 | 29 | 971 | | | 0 | | |
| | | Sub-total | 467 | 36 | 45 | 229 | 4,809 | 348 | 149 | 497 | | | | 4,341 | | |
| Mar. | | 5 | 63 | 6 | 0 | 29 | 609 | 58 | 0 | 58 | 1,000 | | | 522 | | |
| | | 5 | 78 | 4 | 176 | 38 | 798 | 39 | 583 | 622 | 1,000 | | | 176 | | |
| | | 5 | 99 | 0 | 0 | 50 | 1,050 | 0 | 0 | 0 | 1,000 | | | 1,050 | | |
| | | 5 | 64 | 0 | 0 | 29 | 609 | 0 | 0 | 0 | 1,000 | | | 609 | | |
| | | 5 | 105 | 2 | 6 | 54 | 1,134 | 19 | 20 | 39 | 1,000 | | | 1,095 | | |
| | | 6 | 136 | 2 | 6 | 71 | 1,491 | 19 | 20 | 39 | 1,000 | | | 1,452 | | |
| | | Sub-total | 545 | 14 | 188 | 271 | 5,691 | 135 | 623 | 758 | | | | 4,904 | | |

Table C4.7

Calculation of Water Balance in the Wet year of 1977

which is corresponding to 5 years Return Period

in the Probability of Exceedance for Data of Annual Rainfall at the CSDB. (Case A)

| Year | Month | Rainfall | Crop Req. | | | Run-off to Pond | | | Irrigation Req. | | | Balance | | | Remarks Rmax(mm/day) | No. 2 (16) |
|------|-----------|----------|-----------|----|-------|-----------------|----------------|-----------------|-----------------|----------------|----------------|----------------|----------------|----------------|-------------------------|---------------|
| | | | Upland | | Paddy | R _o | V _o | Volume | Upland | Paddy | Total | Pond volume | Shortage | Spill out | Pump Ope. hr | |
| | | | mm | mm | min | mm | mm | mm ³ | m ³ | m ³ | m ³ | m ³ | m ³ | m ³ | | |
| 1977 | Apr. | 44 | 8 | 24 | 17 | 357 | 77 | 79 | 156 | 1,000 | 1,000 | 201 | 201 | 37 | 37 | |
| | 5 | 77 | 4 | 12 | 37 | 777 | 39 | 40 | 79 | 1,000 | 1,000 | 698 | 698 | 33 | 33 | |
| | 5 | 74 | 2 | 6 | 35 | 735 | 19 | 20 | 39 | 1,000 | 1,000 | 696 | 696 | 29 | 29 | |
| | 5 | 162 | 6 | 18 | 88 | 1,848 | 58 | 60 | 118 | 1,000 | 1,000 | 1,730 | 1,730 | 84 | 84 | |
| | 5 | 93 | 6 | 12 | 47 | 987 | 58 | 40 | 98 | 1,000 | 1,000 | 889 | 889 | 37 | 37 | |
| | 5 | 82 | 9 | 18 | 40 | 840 | 87 | 60 | 147 | 1,000 | 1,000 | 693 | 693 | 39 | 39 | |
| | Sub-total | 532 | 35 | 90 | 264 | 5,544 | 338 | 299 | 637 | | | 4,907 | 4,907 | | | |
| | May | 50 | 6 | 12 | 21 | 441 | 58 | 40 | 98 | 1,000 | 1,000 | 343 | 343 | 24 | 24 | |
| | 5 | 117 | 3 | 6 | 61 | 1,281 | 29 | 20 | 49 | 1,000 | 1,000 | 1,232 | 1,232 | 48 | 48 | |
| | 5 | 87 | 3 | 6 | 43 | 903 | 29 | 20 | 49 | 1,000 | 1,000 | 854 | 854 | 36 | 36 | |
| | 5 | 22 | 9 | 18 | 4 | 84 | 87 | 60 | 147 | 937 | 937 | 0 | 0 | | | |
| | 5 | 77 | 9 | 18 | 37 | 777 | 87 | 60 | 147 | 1,000 | 1,000 | 567 | 567 | 60 | 60 | |
| | 6 | 12 | 18 | 24 | 0 | 0 | 174 | 79 | 253 | 747 | 747 | 0 | 0 | | | |
| | Sub-total | 365 | 48 | 84 | 166 | 3,486 | 464 | 279 | 743 | | | 2,996 | 2,996 | | | |
| | Jun. | 91 | 6 | 10 | 46 | 966 | 58 | 33 | 91 | 1,000 | 1,000 | 622 | 622 | 56 | 56 | |
| | 5 | 153 | 6 | 10 | 83 | 1,743 | 58 | 33 | 91 | 1,000 | 1,000 | 1,652 | 1,652 | 73 | 73 | |
| | 5 | 94 | 9 | 15 | 47 | 987 | 87 | 50 | 137 | 1,000 | 1,000 | 850 | 850 | 80 | 80 | |
| | 5 | 9 | 15 | 0 | 0 | 0 | 145 | 0 | 145 | 855 | 855 | 0 | 0 | | | |
| | 5 | 5 | 15 | 0 | 0 | 0 | 145 | 0 | 145 | 710 | 710 | 0 | 0 | | | |
| | 5 | 0 | 15 | 0 | 0 | 0 | 145 | 0 | 145 | 565 | 565 | 0 | 0 | | | |
| | Sub-total | 352 | 66 | 35 | 176 | 3,696 | 638 | 116 | 754 | | | 3,124 | 3,124 | | | |

Table C4-7

Calculation of Water Balance in the Wet year of 1977

which is corresponding to 5 years Return Period

in the Probability of Exceedance for Data of Annual Rainfall at the CSDB. (Case A)

| (1) Year | (2) Month | (3) Pentad | (4) Rainfall mm | (5) Crop Req. mm | (6) Run-off to Pond mm | (7) Crop Req. mm | (8) Run-off to Pond mm | (9) Irrigation Req. mm | Balance | | | (14) Pump Ope. hr | (15) Rmax(mm/day) | (16) No. 3 |
|-------------|--------------|---------------|-----------------------|------------------------|------------------------------|------------------------|------------------------------|------------------------------|--------------|-------------|--------------------------|-------------------------|----------------------|---------------|
| | | | | | | | | | Upland mm | Paddy mm | Total mm ³ | | | |
| 1977 | Jul. | 5 | 6 | 16 | 244 | 0 | 0 | 154 | 808 | 962 | 0 | 397 | 37 | |
| | | 5 | 0 | 20 | 30 | 0 | 0 | 193 | 99 | 292 | 0 | 292 | 27 | |
| | | 5 | 0 | 15 | 30 | 0 | 0 | 145 | 99 | 244 | 0 | 244 | 23 | |
| | | 5 | 7 | 15 | 30 | 0 | 0 | 145 | 99 | 244 | 0 | 244 | 23 | |
| | | 5 | 0 | 15 | 30 | 0 | 0 | 145 | 99 | 244 | 0 | 244 | 23 | |
| | | 6 | 71 | 6 | 18 | 32 | 672 | 58 | 60 | 118 | 54 | | | |
| | | Sub-total | 84 | 87 | 382 | 32 | 672 | 840 | 1,264 | 2,104 | 1,421 | 133 | | |
| | | Aug. | 5 | 3 | 10 | 30 | 0 | 0 | 97 | 99 | 196 | 358 | | |
| | | | 5 | 36 | 8 | 24 | 13 | 273 | 77 | 79 | 156 | 475 | | |
| | | | 5 | 41 | 6 | 18 | 16 | 336 | 58 | 60 | 118 | 693 | | |
| | | | 5 | 1 | 15 | 30 | 0 | 0 | 145 | 99 | 244 | 449 | | |
| | | | 5 | 9 | 12 | 24 | 0 | 0 | 116 | 79 | 195 | 254 | | |
| | | | 6 | 45 | 12 | 24 | 18 | 378 | 116 | 79 | 195 | 437 | | |
| | | Sub-total | 135 | 63 | 150 | 47 | 987 | 609 | 495 | 1,104 | | | | |
| | | Sep. | 5 | 53 | 16 | 28 | 23 | 483 | 154 | 93 | 247 | 673 | 49 | |
| | | | 5 | 0 | 20 | 35 | 0 | 193 | 116 | 309 | 364 | | | |
| | | | 5 | 66 | 12 | 21 | 31 | 651 | 116 | 70 | 186 | 829 | 35 | |
| | | | 5 | 128 | 8 | 14 | 68 | 1,428 | 77 | 46 | 123 | 1,000 | 1,134 | |
| | | | 5 | 1 | 20 | 30 | 0 | 0 | 193 | 99 | 292 | 708 | | |
| | | | 5 | 0 | 20 | 30 | 0 | 0 | 193 | 99 | 292 | 416 | | |
| | | Sub-total | 248 | 96 | 158 | 122 | 2,562 | 920 | 523 | 1,449 | | 1,134 | | |

Table C4-7

Calculation of Water Balance in the Wet year of 1977 which is corresponding to 5 years Return Period in the Probability of Exceedance for Data of Annual Rainfall at the CS

Table C4:8

Calculation of Water Balance in the Dry year of 1988
which is corresponding to 5 years Return Period

in the Probability of Non Exceedance for Data of Annual Rainfall at the CSDB. (Case A)

| (1) | (2) | (3) | (4) | (5) | (6) | (7) | (8) | (9) | (10) | (11) | (12) | (13) | (14) | (15) | No. 1 (16) | |
|------|-------|-----------|----------|-----------|-----------------|-----|-----------------|-----------|-----------------------|----------------------|----------------------|----------------------------|-------------------------|--------------------------|---------------|--------------|
| Year | Month | Pentad | Rainfall | Crop Req. | Run-off to Pond | | Irrigation Req. | | | | | | | | | Remarks |
| | | | mm | mm | mm | mm | Upland Paddy | Ro Volume | Upland m ³ | Paddy m ³ | Total m ³ | Pond volume m ³ | Shortage m ³ | Spill out m ³ | Pump Ope. hr | Rmax(mm/day) |
| 1988 | Jan. | 5 | 95 | 9 | 15 | 48 | 1,008 | 87 | 50 | 137 | 871 | 0 | 0 | 0 | 73 | |
| | | 5 | 10 | 15 | 20 | 0 | 0 | 145 | 66 | 211 | 660 | 0 | 0 | 0 | 45 | |
| | | 5 | 55 | 9 | 15 | 24 | 504 | 87 | 50 | 137 | 1,000 | 27 | 27 | 27 | 89 | |
| | | 5 | 158 | 3 | 5 | 86 | 1,806 | 29 | 17 | 46 | 1,000 | 1,760 | 1,760 | 1,760 | 23 | |
| | | 5 | 47 | 6 | 10 | 19 | 399 | 58 | 33 | 91 | 1,000 | 308 | 308 | 308 | 37 | |
| | | 6 | 69 | 6 | 10 | 32 | 672 | 58 | 33 | 91 | 1,000 | 581 | 581 | 581 | 37 | |
| | | Sub-total | 434 | 48 | 75 | 209 | 4,389 | 464 | 249 | 713 | | 2,676 | | | | |
| | Feb. | 5 | 43 | 9 | 15 | 17 | 357 | 87 | 50 | 137 | 1,000 | 220 | 220 | 220 | 29 | |
| | | 5 | 31 | 9 | 15 | 10 | 210 | 87 | 50 | 137 | 1,000 | 73 | 73 | 73 | 15 | |
| | | 5 | 22 | 12 | 20 | 4 | 84 | 116 | 66 | 182 | 902 | 0 | 0 | 0 | 28 | |
| | | 5 | 68 | 6 | 10 | 32 | 672 | 58 | 33 | 91 | 1,000 | 483 | 483 | 483 | 43 | |
| | | 5 | 65 | 9 | 0 | 30 | 630 | 87 | 0 | 87 | 1,000 | 543 | 543 | 543 | 43 | |
| | | 4 | 151 | 3 | 0 | 83 | 1,743 | 29 | 0 | 29 | 1,000 | 1,714 | 1,714 | 1,714 | 67 | |
| | | Sub-total | 380 | 48 | 60 | 176 | 3,696 | 464 | 199 | 663 | | 3,033 | | | | |
| | Mar. | 5 | 63 | 9 | 0 | 29 | 609 | 87 | 0 | 87 | 1,000 | 522 | 522 | 522 | 45 | |
| | | 5 | 69 | 6 | 250 | 32 | 672 | 58 | 828 | 886 | 786 | 0 | 0 | 0 | 41 | |
| | | 5 | 89 | 4 | 12 | 44 | 924 | 39 | 40 | 79 | 1,000 | 631 | 631 | 631 | 61 | |
| | | 5 | 15 | 0 | 24 | 0 | 0 | 0 | 79 | 79 | 921 | 0 | 0 | 0 | 32 | |
| | | 5 | 62 | 4 | 12 | 28 | 588 | 39 | 40 | 79 | 1,000 | 430 | 430 | 430 | 18 | |
| | | 6 | 46 | 6 | 18 | 17 | 357 | 58 | 60 | 118 | 1,000 | 239 | 239 | 239 | 18 | |
| | | Sub-total | 344 | 29 | 316 | 150 | 3,150 | 281 | 1,047 | 1,328 | | 1,822 | | | | |

Table C4-8

Calculation of Water Balance in the Dry year of 1988
which is corresponding to 5 years Return Period
in the Probability of Non Exceedance for Data of Annual Rainfall at the CSDB. (Case A)

| (1) | (2) | (3) | (4) | (5) | (6) | (7) | (8) | (9) | (10) | (11) | (12) | (13) | (14) | (15) | No. 2 (16) | |
|------|------|-----------|-----|--------|-------|-----|-----------------|--------|-------|-----------------|----------------|----------------|----------------|----------------|---------------|----|
| | | | | | | | | | | | | | | | | |
| | | | | Upland | Paddy | Ro | Volume | Upland | Paddy | Total | m ³ | m ³ | m ³ | m ³ | Rmax(mm/day) | |
| | | | | mm | mm | mm | mm ³ | mm | mm | mm ³ | | | | | | |
| 1988 | Apr. | 5 | 30 | 6 | 18 | 9 | 189 | 58 | 60 | 118 | 1,000 | | 71 | | 17 | |
| | | 5 | 73 | 4 | 12 | 35 | 735 | 39 | 40 | 79 | 1,000 | | 656 | | 37 | |
| | | 5 | 123 | 6 | 18 | 65 | 1,365 | 58 | 60 | 118 | 1,000 | | 1,247 | | 78 | |
| | | 5 | 92 | 6 | 18 | 46 | 966 | 58 | 60 | 118 | 1,000 | | 848 | | 75 | |
| | | 5 | 35 | 12 | 24 | 12 | 252 | 116 | 79 | 195 | 1,000 | | 57 | | 35 | |
| | | 5 | 92 | 9 | 18 | 46 | 966 | 87 | 60 | 147 | 1,000 | | 819 | | 83 | |
| | | Sub-total | 445 | 43 | 108 | 213 | 4,473 | 416 | 359 | 775 | | | 3,698 | | | |
| | | May | 5 | 77 | 6 | 12 | 37 | 777 | 58 | 40 | 98 | 1,000 | | 679 | | 37 |
| | | | 5 | 66 | 9 | 18 | 31 | 651 | 87 | 60 | 147 | 1,000 | | 504 | | 55 |
| | | | 5 | 124 | 3 | 6 | 65 | 1,365 | 29 | 20 | 49 | 1,000 | | 1,316 | | 77 |
| | | | 5 | 47 | 6 | 12 | 19 | 399 | 58 | 40 | 98 | 1,000 | | 301 | | 33 |
| | | | 5 | 21 | 12 | 24 | 4 | 84 | 116 | 79 | 195 | 889 | 0 | 0 | | |
| | | | 6 | 36 | 12 | 24 | 11 | 231 | 116 | 79 | 195 | 925 | 0 | 0 | | |
| | | Sub-total | 371 | 48 | 96 | 167 | 3,507 | 464 | 318 | 782 | | | 2,800 | | | |
| | | Jun. | 5 | 66 | 12 | 20 | 31 | 651 | 116 | 66 | 182 | 1,000 | | 394 | | 64 |
| | | | 5 | 51 | 6 | 10 | 22 | 462 | 58 | 33 | 91 | 1,000 | | 371 | | 27 |
| | | | 5 | 21 | 12 | 20 | 4 | 84 | 116 | 66 | 182 | 902 | 0 | 0 | | |
| | | | 5 | 3 | 15 | 0 | 0 | 0 | 145 | 0 | 145 | 757 | 0 | 0 | | |
| | | | 5 | 7 | 12 | 0 | 0 | 0 | 116 | 0 | 116 | 641 | 0 | 0 | | |
| | | | 5 | 0 | 15 | 0 | 0 | 0 | 145 | 0 | 145 | 496 | 0 | 0 | | |
| | | Sub-total | 148 | 72 | 50 | 57 | 1,197 | 696 | 165 | 861 | | | 765 | | | |

Table C4-8

Calculation of Water Balance in the Dry year of 1988

which is corresponding to 5 years Return Period

in the Probability of Non Exceedance for Data of Annual Rainfall at the CSDB. (Case A)

| (1) | (2) | (3) | (4) | (5) | (6) | (7) | (8) | (9) | (10) | (11) | (12) | (13) | (14) | (15) | No. 3 (16) | |
|------|------|-----------|-----------|----------|-----------|-----------------|-----|-------|-------|-------|-------|-------|------|------|---------------|--|
| | | | | | | | | | | | | | | | | |
| | Year | Month | Pentad | Rainfall | Crop Req. | Run-off to Pond | | | | | | | | | | |
| | | | | mm | mm | mm | mm | mm | mm | mm | mm | mm | mm | mm | mm | |
| 1988 | Jul. | 5 | 6 | 16 | 250 | 0 | 0 | 154 | 828 | 982 | 0 | 486 | 45 | | | |
| | | 5 | 7 | 16 | 30 | 0 | 0 | 154 | 99 | 253 | 0 | 253 | 24 | | | |
| | | 5 | 0 | 15 | 30 | 0 | 0 | 145 | 99 | 244 | 0 | 244 | 23 | | | |
| | | 5 | 73 | 12 | 30 | 35 | 735 | 116 | 99 | 215 | 520 | | | | | |
| | | 5 | 3 | 15 | 30 | 0 | 0 | 145 | 99 | 244 | 276 | | | | | |
| | | 6 | 0 | 12 | 36 | 0 | 0 | 116 | 119 | 235 | 41 | | | | | |
| | | Sub-total | 89 | 86 | 406 | 35 | 735 | 830 | 1,343 | 2,173 | 983 | 92 | | | | |
| | | Aug. | 5 | 42 | 6 | 18 | 16 | 336 | 58 | 60 | 118 | 259 | | | | |
| | | | 5 | 64 | 8 | 24 | 29 | 609 | 77 | 79 | 156 | 712 | | | | |
| | | | 5 | 69 | 6 | 18 | 32 | 672 | 58 | 60 | 118 | 1,000 | 41 | | | |
| | | | 5 | 0 | 15 | 30 | 0 | 0 | 145 | 99 | 244 | 756 | | | | |
| | | | 5 | 25 | 12 | 24 | 6 | 126 | 116 | 79 | 195 | 687 | | | | |
| | | | 6 | 0 | 18 | 36 | 0 | 0 | 174 | 119 | 293 | 394 | | | | |
| | | | Sub-total | 200 | 65 | 150 | 83 | 1,743 | 628 | 496 | 1,124 | 266 | | | | |
| | | | Sep. | 5 | 3 | 20 | 35 | 0 | 0 | 193 | 116 | 309 | 85 | 0 | | |
| | | | | 5 | 1 | 20 | 35 | 0 | 0 | 193 | 116 | 309 | 0 | 224 | 21 | |
| | | | | 5 | 26 | 12 | 22 | 7 | 147 | 116 | 73 | 189 | 0 | 42 | 4 | |
| | | | | 5 | 15 | 16 | 28 | 0 | 0 | 154 | 93 | 247 | 0 | 247 | 23 | |
| | | | | 5 | 17 | 16 | 24 | 1 | 21 | 154 | 79 | 233 | 0 | 212 | 20 | |
| | | | | 5 | 18 | 16 | 24 | 2 | 42 | 154 | 79 | 233 | 0 | 191 | 18 | |
| | | | Sub-total | 80 | 100 | 168 | 10 | 210 | 964 | 556 | 1,520 | 916 | 86 | | | |

Table C4-8

**Calculation of Water Balance in the Dry year of 1988
which is corresponding to 5 years Return Period
in the Probability of Non Exceedance for Data of Annual Rainfall at the**

| Annual Rainfall & Irrigation Requirements | | | | | | | | | | | | Remarks | | | |
|---|-----------|--------|----------|--------------|-----------------|----------|--------------------------|--------------------------|-------------------------|-------------------------|-------------------------------|----------------------------|-----------------------------|-----------------|---------|
| (1) | (2) | (3) | (4) | (5) | (6) | (7) | (8) | (9) | (10) | (11) | (12) | (13) | (14) | (15) | |
| Year | Month | Pentad | Rainfall | Crop Req. | Run-off to Pond | | | Irrigation Req. | | | | Balance | | | |
| | | | mm | Upland mm | Paddy mm | Ro mm | Volume m ³ | Upland m ³ | Paddy m ³ | Total m ³ | Pond volume m ³ | Shortage m ³ | Spill out m ³ | Pump Ope. hr | Remarks |
| | | | mm | mm | mm | mm | m ³ | m ³ | m ³ | m ³ | m ³ | m ³ | m ³ | Rmax(mm/day) | |
| 1988 | Oct. | 5 | 4 | 20 | 24 | 0 | 0 | 193 | 79 | 272 | 0 | 272 | 0 | 25 | |
| | 5 | 5 | 15 | 24 | 0 | 0 | 145 | 79 | 224 | 0 | 224 | 0 | 21 | | |
| | 5 | 73 | 6 | 0 | 35 | 735 | 58 | 0 | 58 | 677 | | | | 53 | |
| | 5 | 83 | 6 | 0 | 41 | 861 | 58 | 0 | 58 | 1,000 | | | | | |
| | 5 | 9 | 8 | 0 | 0 | 0 | 0 | 77 | 0 | 77 | 923 | | | 480 | |
| | 6 | 66 | 8 | 0 | 29 | 609 | 77 | 0 | 77 | 1,000 | | | | 36 | |
| | Sub-total | | 240 | 63 | 48 | 105 | 2,205 | 608 | 158 | 766 | | 496 | 935 | 46 | |
| | Nov. | 5 | 51 | 4 | 75 | 22 | 462 | 39 | 248 | 287 | 1,000 | | 175 | 21 | |
| | 5 | 43 | 6 | 91 | 17 | 357 | 58 | 301 | 359 | 998 | | 0 | | | |
| | 5 | 21 | 4 | 12 | 4 | 84 | 39 | 40 | 79 | 1,000 | | | | 3 | |
| | 5 | 1 | 10 | 30 | 0 | 0 | 97 | 99 | 196 | 804 | | | | | |
| | 5 | 18 | 12 | 24 | 2 | 42 | 116 | 79 | 195 | 651 | | | | | |
| | 5 | 17 | 12 | 24 | 1 | 21 | 116 | 79 | 195 | 477 | | | | | |
| | Sub-total | | 151 | 48 | 256 | 46 | 966 | 465 | 846 | 1,311 | | | 178 | | |
| | Dec. | 5 | 41 | 9 | 18 | 16 | 336 | 87 | 60 | 147 | 666 | | | | |
| | 5 | 44 | 12 | 24 | 17 | 357 | 116 | 79 | 195 | 828 | | | | 45 | |
| | 5 | 99 | 3 | 6 | 50 | 1,050 | 29 | 20 | 49 | 1,000 | | | | 59 | |
| | 5 | 109 | 6 | 12 | 56 | 1,176 | 58 | 40 | 98 | 1,000 | | | | 829 | |
| | 5 | 5 | 12 | 30 | 0 | 0 | 116 | 99 | 215 | 785 | | | | 1,078 | |
| | 6 | 9 | 15 | 30 | 0 | 0 | 145 | 99 | 244 | 541 | | | | | |
| | Sub-total | | 307 | 57 | 120 | 139 | 2,919 | 551 | 397 | 948 | | | 1,907 | | |
| Total | | | 3,189 | 707 | 1,853 | 1,390 | 29,190 | 6,831 | 6,133 | 12,964 | 2,395 | 18,080 | 224 | | |

Table C4-9

Calculation of Water Balance in the Wet Year of 1977
which is corresponding to 5 years Return Period

in the Probability of Exceedance for Data of Annual Rainfall at the CSDB. (Case B)

| (1) | (2) | (3) | (4) | (5) | (6) | (7) | (8) | (9) | (10) | (11) | (12) | (13) | (14) | (15) | No. 1 (16) | |
|------|-----------|-----|-----|-----|-----|-----|-------|--------------|-----------------------|--------------|-------|----------------------------|-------------------------|--------------------------|---------------|----------------------|
| | | | | | | | | | | | | | | | | |
| | | | | | | | | Upland Paddy | Volume m ³ | Upland Paddy | Total | Pond volume m ³ | Shortage m ³ | Spill out m ³ | Pump Ope. hr | Remarks Rmax(mm/day) |
| | | | mm | mm | mm | mm | mm | | | | | | | | | |
| 1977 | Jan. | 5 | 42 | 6 | 10 | 16 | 336 | 58 | 33 | 91 | 245 | 0 | 0 | 0 | 0 | 0 |
| | | 5 | 89 | 6 | 10 | 44 | 924 | 58 | 33 | 91 | 1,000 | 78 | 78 | 0 | 0 | 0 |
| | | 5 | 18 | 12 | 20 | 2 | 42 | 116 | 66 | 182 | 860 | 0 | 0 | 0 | 0 | 0 |
| | | 5 | 182 | 0 | 0 | 100 | 2,100 | 0 | 0 | 0 | 1,000 | 1,960 | 1,960 | 54 | 54 | 54 |
| | | 5 | 102 | 6 | 10 | 52 | 1,092 | 58 | 33 | 91 | 1,000 | 1,001 | 1,001 | 60 | 60 | 60 |
| | | 6 | 169 | 6 | 10 | 91 | 1,911 | 58 | 33 | 91 | 1,000 | 1,820 | 1,820 | 80 | 80 | 80 |
| | Sub-total | | 602 | 36 | 60 | 305 | 6,405 | 348 | 198 | 546 | | | | | | |
| | Feb. | 5 | 133 | 6 | 10 | 71 | 1,491 | 58 | 33 | 91 | 1,000 | 1,400 | 1,400 | 55 | 55 | 55 |
| | | 5 | 133 | 3 | 5 | 71 | 1,491 | 29 | 17 | 46 | 1,000 | 1,445 | 1,445 | 65 | 65 | 65 |
| | | 5 | 128 | 6 | 10 | 68 | 1,428 | 58 | 33 | 91 | 1,000 | 1,337 | 1,337 | 77 | 77 | 77 |
| | | 5 | 12 | 12 | 20 | 0 | 0 | 116 | 66 | 182 | 818 | 0 | 0 | 0 | 0 | 0 |
| | | 5 | 46 | 6 | 0 | 19 | 399 | 58 | 0 | 58 | 1,000 | 159 | 159 | 19 | 19 | 19 |
| | | 3 | 15 | 3 | 0 | 0 | 0 | 29 | 0 | 29 | 971 | 0 | 0 | 0 | 0 | 0 |
| | Sub-total | | 467 | 36 | 45 | 229 | 4,809 | 348 | 149 | 497 | | | | | | |
| | Mar. | 5 | 63 | 6 | 0 | 29 | 609 | 58 | 0 | 58 | 1,000 | 522 | 522 | 44 | 44 | 44 |
| | | 5 | 78 | 4 | 0 | 38 | 798 | 39 | 0 | 39 | 1,000 | 759 | 759 | 54 | 54 | 54 |
| | | 5 | 99 | 0 | 36 | 50 | 1,050 | 0 | 119 | 119 | 1,000 | 931 | 931 | 35 | 35 | 35 |
| | | 5 | 64 | 0 | 61 | 29 | 609 | 0 | 202 | 202 | 1,000 | 407 | 407 | 22 | 22 | 22 |
| | | 5 | 105 | 2 | 6 | 54 | 1,134 | 19 | 20 | 39 | 1,000 | 1,095 | 1,095 | 53 | 53 | 53 |
| | | 6 | 136 | 2 | 6 | 71 | 1,491 | 19 | 20 | 39 | 1,000 | 1,452 | 1,452 | 60 | 60 | 60 |
| | Sub-total | | 545 | 14 | 109 | 271 | 5,691 | 135 | 361 | 496 | | | | | | |
| | | | | | | | | | | | | | | | | 5,166 |

Table C4-9

Calculation of Water Balance in the Wet year of 1977

which is corresponding to 5 years Return Period

in the Probability of Exceedance for Data of Annual Rainfall at the CSDB. (Case B)

| Year | Month | Pentad | Rainfall | Crop Req. | Run-off to Pond | | | Irrigation Req. | | | Balance | | | No. 2 (16) | | |
|------|-------|-----------|----------|-----------|-----------------|-----|-------|-----------------|----------------|----------------|----------------|----------------|----------------|----------------|----|--|
| | | | | | Upland | | Paddy | Ro Volume | Upland | Paddy | Total | Pond volume | Shortage | Spill out | | |
| | | | | | mm | mm | mm | m ³ | m ³ | m ³ | m ³ | m ³ | m ³ | m ³ | | |
| 1977 | Apr. | 5 | 44 | 8 | 24 | 17 | 357 | 77 | 79 | 156 | 1,000 | 201 | 698 | 37 | | |
| | | 5 | 77 | 4 | 12 | 37 | 777 | 39 | 40 | 79 | 1,000 | 696 | 696 | 33 | | |
| | | 5 | 74 | 2 | 6 | 35 | 735 | 19 | 20 | 39 | 1,000 | 1,730 | 1,730 | 29 | | |
| | | 5 | 162 | 6 | 18 | 88 | 1,848 | 58 | 60 | 118 | 1,000 | 889 | 889 | 84 | | |
| | | 5 | 93 | 6 | 12 | 47 | 987 | 58 | 40 | 98 | 1,000 | 693 | 693 | 37 | | |
| | | 5 | 82 | 9 | 18 | 40 | 840 | 87 | 60 | 147 | 1,000 | 693 | 693 | 39 | | |
| | | Sub-total | | 35 | 90 | 264 | 5,544 | 338 | 299 | 637 | | 4,907 | | | | |
| | | May | | 50 | 6 | 12 | 21 | 441 | 58 | 40 | 98 | 1,000 | 343 | 343 | 24 | |
| | | 5 | 117 | 3 | 6 | 61 | 1,281 | 29 | 20 | 49 | 1,000 | 1,232 | 1,232 | 48 | | |
| | | 5 | 87 | 3 | 6 | 43 | 903 | 29 | 20 | 49 | 1,000 | 854 | 854 | 36 | | |
| | | 5 | 22 | 9 | 18 | 4 | 84 | 87 | 60 | 147 | 937 | 0 | 0 | | | |
| | | 5 | 77 | 9 | 18 | 37 | 777 | 87 | 60 | 147 | 1,000 | 567 | 567 | 60 | | |
| | | 6 | 12 | 18 | 24 | 0 | 0 | 174 | 79 | 253 | 747 | 0 | 0 | | | |
| | | Sub-total | | 365 | 48 | 84 | 166 | 3,486 | 464 | 279 | 743 | 2,996 | | | | |
| | | Jun. | | 91 | 6 | 10 | 46 | 966 | 58 | 33 | 91 | 1,000 | 622 | 622 | 56 | |
| | | 5 | 153 | 6 | 10 | 83 | 1,743 | 58 | 33 | 91 | 1,000 | 1,652 | 1,652 | 73 | | |
| | | 5 | 94 | 9 | 15 | 47 | 987 | 87 | 50 | 137 | 1,000 | 850 | 850 | 80 | | |
| | | 5 | 9 | 15 | 20 | 0 | 0 | 145 | 66 | 211 | 789 | 0 | 0 | | | |
| | | 5 | 5 | 15 | 20 | 0 | 0 | 145 | 66 | 211 | 578 | 0 | 0 | | | |
| | | 5 | 0 | 15 | 20 | 0 | 0 | 145 | 66 | 211 | 367 | 0 | 0 | | | |
| | | Sub-total | | 352 | 66 | 95 | 176 | 3,696 | 638 | 314 | 952 | 3,124 | | | | |

Table C4-9

Calculation of Water Balance in the Wet year of 1977
which is corresponding to 5 years Return Period
in the Probability of Exceedance for Data of Annual Rainfall at the CSDB. (Case B)

| (1) | (2) | (3) | (4) | (5) | (6) | (7) | (8) | (9) | (10) | (11) | (12) | (13) | (14) | (15) | No. 3 (16) |
|------|-------|-----------|----------|--------------|-----------------|-----------------|--------|-------|----------------|----------------|----------------|----------------|-----------|--------------|---------------|
| Year | Month | Pentad | Rainfall | Crop Req. | Run-off to Pond | Irrigation Req. | | | Pond volume | Total | | Spill out | Pump Ope. | Remarks | |
| | | | mm | Upland Paddy | Ro Volume | | Upland | Paddy | m ³ | m ³ | m ³ | m ³ | hr | Rmax(mm/day) | |
| 1977 | Jul. | 5 | 6 | 16 | 0 | 0 | 0 | 154 | 0 | 154 | 213 | | | | |
| | | 5 | 0 | 20 | 0 | 0 | 0 | 193 | 0 | 193 | 20 | | | | |
| | | 5 | 0 | 15 | 0 | 0 | 0 | 145 | 0 | 145 | 0 | 125 | | 12 | |
| | | 5 | 7 | 15 | 0 | 0 | 0 | 145 | 0 | 145 | 0 | 145 | | 13 | |
| | | 5 | 0 | 15 | 0 | 0 | 0 | 145 | 0 | 145 | 0 | 145 | | 13 | |
| | | 6 | 71 | 6 | 0 | 32 | 672 | 58 | 0 | 58 | 614 | | | | |
| | | Sub-total | 84 | 87 | 0 | 32 | 672 | 840 | 0 | 840 | 415 | | 38 | | |
| | Aug. | 5 | 3 | 10 | 10 | 0 | 0 | 97 | 33 | 130 | 484 | | | | |
| | | 5 | 36 | 8 | 8 | 13 | 273 | 77 | 26 | 103 | 654 | | | | |
| | | 5 | 41 | 6 | 6 | 16 | 336 | 58 | 20 | 78 | 912 | | | | |
| | | 5 | 1 | 15 | 15 | 0 | 0 | 145 | 50 | 195 | 717 | | | | |
| | | 5 | 9 | 12 | 12 | 0 | 0 | 116 | 40 | 156 | 561 | | | | |
| | | 6 | 45 | 12 | 12 | 18 | 378 | 116 | 40 | 156 | 783 | | | | |
| | | Sub-total | 135 | 63 | 47 | 987 | 609 | 209 | 818 | | | | | | |
| | Sep. | 5 | 53 | 16 | 16 | 23 | 483 | 154 | 53 | 207 | 1,000 | 59 | | | |
| | | 5 | 0 | 20 | 20 | 0 | 0 | 193 | 66 | 259 | 741 | 0 | | | |
| | | 5 | 66 | 12 | 12 | 31 | 651 | 116 | 40 | 156 | 1,000 | 236 | | 35 | |
| | | 5 | 128 | 8 | 8 | 68 | 1,428 | 77 | 26 | 103 | 1,000 | 1,325 | | 69 | |
| | | 5 | 1 | 20 | 20 | 0 | 0 | 193 | 66 | 259 | 741 | 0 | | | |
| | | 5 | 0 | 20 | 20 | 0 | 0 | 193 | 66 | 259 | 482 | 0 | | | |
| | | Sub-total | 248 | 96 | 96 | 122 | 2,562 | 920 | 317 | 1,243 | 1,620 | | | | |

Table C4:9

Calculation of Water Balance in the Wet year of 1977
which is corresponding to 5 years Return Period
in the Probability of Exceedance for Data of Annual Rainfall at the CSDB. (Case B)

| (1) | (2) | (3) | (4) | (5) | (6) | (7) | (8) | (9) | (10) | (11) | (12) | (13) | (14) | (15) | No. 4 (16) |
|------|-------|-----------|--------------|-------------|-----------------|--------------------------|--------------------------|-------------------------|-------------------------|-------------------------------|----------------------------|-----------------------------|-----------------|---------|---------------|
| Year | Month | Pentad | Rainfall | Crop Req. | Run-off to Pond | | | | | | | | | | |
| | | | Upland mm | Paddy mm | Ro mm | Volume m ³ | Upland m ³ | Paddy m ³ | Total m ³ | Pond volume m ³ | Shortage m ³ | Spill out m ³ | Pump Ope. hr | Remarks | |
| 1977 | Oct. | 5 | 11 | 16 | 12 | 0 | 0 | 154 | 40 | 194 | 288 | | | | |
| | | 5 | 45 | 16 | 16 | 18 | 378 | 154 | 53 | 207 | 459 | | | | |
| | | 5 | 3 | 20 | 20 | 0 | 0 | 193 | 66 | 259 | 200 | | | | |
| | | 5 | 8 | 12 | 12 | 0 | 0 | 116 | 40 | 156 | 44 | | | | |
| | | 5 | 74 | 16 | 16 | 35 | 735 | 154 | 53 | 207 | 572 | | | | |
| | | 6 | 87 | 16 | 16 | 41 | 861 | 154 | 53 | 207 | 1,000 | | | | |
| | | | | | | | | | | | | 226 | | | 45 |
| | | Sub-total | 228 | 92 | 92 | 94 | 1,974 | 925 | 305 | 1,230 | | | 226 | | |
| | | Nov. | 5 | 140 | 2 | 30 | 75 | 1,575 | 19 | 99 | 118 | 1,000 | 1,457 | | 82 |
| | | | 5 | 214 | 0 | 0 | 119 | 2,499 | 0 | 0 | 0 | 1,000 | 2,499 | | 48 |
| | | | 5 | 26 | 4 | 18 | 7 | 147 | 39 | 60 | 99 | 1,000 | 48 | | 15 |
| | | | 5 | 13 | 6 | 18 | 0 | 0 | 58 | 60 | 118 | 882 | 0 | | |
| | | | 5 | 35 | 12 | 24 | 12 | 252 | 116 | 79 | 195 | 939 | 0 | | |
| | | | 5 | 67 | 6 | 12 | 31 | 651 | 58 | 40 | 98 | 1,000 | 492 | | 47 |
| | | | Sub-total | 495 | 30 | 102 | 244 | 5,124 | 290 | 338 | 628 | | 4,496 | | |
| | | Dec. | 5 | 20 | 12 | 24 | 3 | 63 | 116 | 79 | 195 | 868 | 0 | | |
| | | | 5 | 99 | 9 | 18 | 50 | 1,050 | 87 | 60 | 147 | 1,000 | 771 | | 80 |
| | | | 5 | 42 | 9 | 18 | 16 | 336 | 87 | 60 | 147 | 1,000 | 189 | | 25 |
| | | | 5 | 46 | 6 | 12 | 19 | 399 | 58 | 40 | 98 | 1,000 | 301 | | 30 |
| | | | 5 | 55 | 9 | 18 | 24 | 504 | 87 | 60 | 147 | 1,000 | 357 | | 40 |
| | | | 6 | 23 | 12 | 24 | 3 | 63 | 116 | 79 | 195 | 868 | 0 | | |
| | | | Sub-total | 285 | 57 | 114 | 115 | 2,415 | 551 | 378 | 929 | | 1,618 | | |
| | | Total | 4,338 | 664 | 950 | 2,065 | 43,365 | 6,412 | 3,147 | 9,559 | 415 | 33,353 | 38 | | |

Table C4-10

Calculation of Water Balance in the Dry year of 1988

which is corresponding to 5 years Return Period

in the Probability of Non Exceedance for Data of Annual Rainfall at the CSDB. (Case B)

| Year | Month | Pentad | Rainfall | Crop Req. | | | Run-off to Pond | | | Irrigation Req. | | | Balance | | | Remarks | Rmax(mm/day) | No. 1 (16) | |
|------|-------|-----------|----------|-----------|-----|-------|-----------------|--------|----------------|-----------------|----------------|----------------|----------------|----------------|----------------|-----------|--------------|---------------|--|
| | | | | Upland | | Paddy | R _o | Volume | m ³ | Upland | Paddy | Total | Pond volume | Shortage | Spill out | Pump Ope. | | | |
| | | | | mm | mm | mm | mm | mm | m ³ | m ³ | m ³ | m ³ | m ³ | m ³ | m ³ | hr | | | |
| 1988 | Jan. | 5 | 95 | 9 | 15 | 48 | 1,008 | 87 | 50 | 137 | 871 | 871 | 0 | 0 | 0 | 73 | | | |
| | | 5 | 10 | 15 | 20 | 0 | 0 | 145 | 66 | 211 | 660 | 660 | 0 | 0 | 0 | | | | |
| | | 5 | 55 | 9 | 15 | 24 | 504 | 87 | 50 | 137 | 1,000 | 1,000 | 27 | 27 | 45 | | | | |
| | | 5 | 158 | 3 | 5 | 86 | 1,806 | 29 | 17 | 46 | 1,000 | 1,000 | 1,760 | 1,760 | 89 | | | | |
| | | 5 | 47 | 6 | 10 | 19 | 399 | 58 | 33 | 91 | 1,000 | 1,000 | 308 | 308 | 23 | | | | |
| | | 6 | 69 | 6 | 10 | 32 | 672 | 58 | 33 | 91 | 1,000 | 1,000 | 581 | 581 | 37 | | | | |
| | | Sub-total | | | 48 | 75 | 209 | 4,389 | 464 | 249 | 713 | 2,676 | 2,676 | | | | | | |
| | | Feb. | | | 43 | 9 | 15 | 17 | 357 | 87 | 50 | 137 | 1,000 | 1,000 | 220 | 220 | 29 | | |
| | | 5 | 31 | 9 | 15 | 10 | 210 | 87 | 50 | 137 | 1,000 | 1,000 | 73 | 73 | 15 | | | | |
| | | 5 | 22 | 12 | 20 | 4 | 84 | 116 | 66 | 182 | 902 | 902 | 0 | 0 | | | | | |
| | | 5 | 68 | 6 | 10 | 32 | 672 | 58 | 33 | 91 | 1,000 | 1,000 | 483 | 483 | 28 | | | | |
| | | 5 | 65 | 9 | 0 | 30 | 630 | 87 | 0 | 87 | 1,000 | 1,000 | 543 | 543 | 43 | | | | |
| | | 4 | 151 | 3 | 0 | 83 | 1,743 | 29 | 0 | 29 | 1,000 | 1,000 | 1,714 | 1,714 | 67 | | | | |
| | | Sub-total | | | 380 | 48 | 60 | 176 | 3,696 | 464 | 199 | 663 | 3,033 | 3,033 | | | | | |
| | | Mar. | | | 63 | 9 | 0 | 29 | 609 | 87 | 0 | 87 | 1,000 | 1,000 | 522 | 522 | 45 | | |
| | | 5 | 69 | 6 | 0 | 32 | 672 | 58 | 0 | 58 | 1,000 | 1,000 | 614 | 614 | 41 | | | | |
| | | 5 | 89 | 4 | 72 | 44 | 924 | 39 | 238 | 277 | 1,000 | 1,000 | 647 | 647 | 61 | | | | |
| | | 5 | 15 | 0 | 110 | 0 | 0 | 0 | 364 | 364 | 636 | 636 | 0 | 0 | | | | | |
| | | 5 | 62 | 4 | 12 | 28 | 588 | 39 | 40 | 79 | 1,000 | 1,000 | 145 | 145 | 32 | | | | |
| | | 6 | 46 | 6 | 18 | 17 | 357 | 58 | 60 | 118 | 1,000 | 1,000 | 239 | 239 | 18 | | | | |
| | | Sub-total | | | 344 | 29 | 212 | 150 | 3,150 | 281 | 702 | 983 | 2,167 | 2,167 | | | | | |

Table C4-10

Calculation of Water Balance in the Dry year of 1988
which is corresponding to 5 years Return Period
in the Probability of Non Exceedance for Data of Annual Rainfall at the CSDB. (Case B)

| (1) Year | Month | Pentad | Rainfall mm | Crop Req. mm | Run-off to Pond mm | Irrigation Req. mm | Balance | | | No. 2 (16) Rmax(mm/day) | | | | |
|-------------|-------|-----------|----------------|-----------------|-----------------------|-----------------------|--------------------------|-------------------------|-------------------------|-------------------------------|-------|-------|-------|----|
| | | | | | | | | | | | | | | |
| | | | | | | | Upland m ³ | Paddy m ³ | Total m ³ | | | | | |
| 1988 | Apr. | 5 | 30 | 6 | 18 | 9 | 189 | 58 | 60 | 1,118 | 1,000 | 71 | 17 | |
| | | 5 | 73 | 4 | 12 | 35 | 735 | 39 | 40 | 79 | 1,000 | 656 | 37 | |
| | | 5 | 123 | 6 | 18 | 65 | 1,365 | 58 | 60 | 118 | 1,000 | 1,247 | 78 | |
| | | 5 | 92 | 6 | 18 | 46 | 966 | 58 | 60 | 118 | 1,000 | 848 | 75 | |
| | | 5 | 35 | 12 | 24 | 12 | 252 | 116 | 79 | 195 | 1,000 | 57 | 35 | |
| | | 5 | 92 | 9 | 18 | 46 | 966 | 87 | 60 | 147 | 1,000 | 819 | 83 | |
| | | Sub-total | 445 | 43 | 108 | 213 | 4,473 | 416 | 359 | 775 | | 3,698 | | |
| | | May | 5 | 77 | 6 | 12 | 37 | 777 | 58 | 40 | 98 | 1,000 | 679 | 37 |
| | | | 5 | 66 | 9 | 18 | 31 | 651 | 87 | 60 | 147 | 1,000 | 504 | 55 |
| | | | 5 | 124 | 3 | 6 | 65 | 1,365 | 29 | 20 | 49 | 1,000 | 1,316 | 77 |
| | | | 5 | 47 | 6 | 12 | 19 | 399 | 58 | 40 | 98 | 1,000 | 301 | 33 |
| | | | 5 | 21 | 12 | 24 | 4 | 84 | 116 | 79 | 195 | 889 | 0 | 0 |
| | | | 6 | 36 | 12 | 24 | 11 | 231 | 116 | 79 | 195 | 925 | 0 | 0 |
| | | Sub-total | 371 | 48 | 96 | 167 | 3,507 | 464 | 318 | 782 | | 2,800 | | |
| | | Jun. | 5 | 66 | 12 | 20 | 31 | 651 | 116 | 66 | 182 | 1,000 | 394 | 64 |
| | | | 5 | 51 | 6 | 10 | 22 | 462 | 58 | 33 | 91 | 1,000 | 371 | 27 |
| | | | 5 | 21 | 12 | 20 | 4 | 84 | 116 | 66 | 182 | 902 | 0 | 0 |
| | | | 5 | 3 | 15 | 25 | 0 | 0 | 145 | 83 | 228 | 674 | 0 | 0 |
| | | | 5 | 7 | 12 | 20 | 0 | 0 | 116 | 66 | 182 | 492 | 0 | 0 |
| | | | 5 | 0 | 15 | 25 | 0 | 0 | 145 | 83 | 228 | 264 | 0 | 0 |
| | | Sub-total | 148 | 72 | 120 | 57 | 1,197 | 696 | 397 | 1,093 | | 765 | | |

Table C4-10

Calculation of Water Balance in the Dry year of 1988
which is corresponding to 5 years Return Period

in the Probability of Non Exceedance for Data of Annual Rainfall at the CSDB (Case B)

| Year | Month | Pentad | Rainfall | Crop Req. | | | Run-off to Pond | | | Irrigation Req. | | | Balance | | | Remarks Rmax(mm/day) | |
|------|------------------|--------|----------|------------|------------|------------|-----------------|------------|------------|-----------------|----------------|----------------|----------------|----------------|----------------|-------------------------|--|
| | | | | Upland | | Paddy | Ro | Volume | mm | m ³ | Upland | Paddy | Total | m ³ | m ³ | Pump Ope. | |
| | | | | mm | mm | mm | mm | mm | mm | m ³ | m ³ | m ³ | m ³ | m ³ | m ³ | hr | |
| 1988 | Jul. | 5 | 6 | 16 | 0 | 0 | 0 | 0 | 0 | 154 | 0 | 154 | 110 | 0 | 44 | 4 | |
| | 5 | 7 | 16 | 0 | 0 | 0 | 0 | 0 | 0 | 154 | 0 | 154 | 0 | 0 | 145 | 14 | |
| | 5 | 0 | 15 | 0 | 0 | 0 | 0 | 0 | 0 | 145 | 0 | 145 | 0 | 0 | 619 | | |
| | 5 | 73 | 12 | 0 | 0 | 0 | 35 | 735 | 116 | 0 | 116 | 0 | 116 | 0 | 474 | | |
| | 5 | 3 | 15 | 0 | 0 | 0 | 0 | 0 | 0 | 145 | 0 | 145 | 0 | 0 | 358 | | |
| | 6 | 0 | 12 | 0 | 0 | 0 | 0 | 0 | 0 | 116 | 0 | 116 | 0 | 0 | 0 | | |
| | Sub-total | | | 89 | 86 | 0 | 35 | 735 | 830 | 0 | 830 | 0 | 830 | 189 | 0 | 18 | |
| | Aug. | 5 | 42 | 6 | 6 | 16 | 16 | 336 | 58 | 20 | 78 | 616 | 616 | 0 | 122 | 63 | |
| | 5 | 64 | 8 | 8 | 29 | 609 | 77 | 26 | 103 | 1,000 | 1,000 | 1,000 | 1,000 | 0 | 594 | 41 | |
| | 5 | 69 | 6 | 6 | 32 | 672 | 58 | 20 | 78 | 1,000 | 1,000 | 1,000 | 1,000 | 0 | 805 | | |
| | 5 | 0 | 15 | 15 | 0 | 0 | 0 | 145 | 50 | 195 | 195 | 195 | 195 | 0 | 775 | | |
| | 5 | 25 | 12 | 12 | 6 | 126 | 116 | 40 | 156 | 0 | 0 | 0 | 0 | 0 | 541 | | |
| | 6 | 0 | 18 | 18 | 0 | 0 | 0 | 174 | 60 | 234 | 234 | 234 | 234 | 0 | 0 | | |
| | Sub-total | | | 200 | 65 | 83 | 1,743 | 628 | 216 | 844 | 716 | 0 | 0 | 0 | 0 | 0 | |
| | Sep. | 5 | 3 | 20 | 0 | 0 | 0 | 193 | 66 | 259 | 282 | 282 | 282 | 282 | 0 | 0 | |
| | 5 | 1 | 20 | 20 | 0 | 0 | 0 | 193 | 66 | 259 | 23 | 23 | 23 | 23 | 0 | | |
| | 5 | 26 | 12 | 12 | 7 | 147 | 116 | 40 | 156 | 0 | 0 | 0 | 0 | 0 | 14 | | |
| | 5 | 15 | 16 | 16 | 0 | 0 | 0 | 154 | 53 | 207 | 0 | 0 | 0 | 0 | 0 | 193 | |
| | 5 | 17 | 16 | 16 | 1 | 21 | 154 | 53 | 207 | 0 | 0 | 0 | 0 | 0 | 186 | 18 | |
| | 5 | 18 | 16 | 16 | 2 | 42 | 154 | 53 | 207 | 0 | 0 | 0 | 0 | 0 | 165 | 16 | |
| | Sub-total | | | 80 | 100 | 100 | 10 | 210 | 964 | 331 | 1,295 | 544 | 544 | 544 | 544 | 52 | |

Table C4-10

Calculation of Water Balance in the Dry year of 1988
which is corresponding to 5 years Return Period
in the Probability of Non Exceedance for Data of Annual Rainfall at the CSDB. (Case B)

| (1) | (2) | (3) | (4) | (5) | (6) | (7) | (8) | (9) | (10) | (11) | (12) | (13) | (14) | (15) | No. 4 (16) |
|------|-------|-----------|----------|--------------|-----------------|----------|--------------------------|--------------------------|-------------------------|-------------------------|----------------|----------------|----------------|----------------|---------------|
| Year | Month | Pentad | Rainfall | Crop Req. | Run-off to Pond | | Irrigation Req. | | | | Pond volume | Shortage | Spill out | Pump Ope. | Remarks |
| | | | mm | Upland mm | Paddy mm | Ro mm | Volume m ³ | Upland m ³ | Paddy m ³ | Total m ³ | m ³ | m ³ | m ³ | m ³ | |
| 1988 | Oct. | 5 | 4 | 20 | 20 | 0 | 0 | 193 | 66 | 259 | 0 | 259 | 24 | | |
| | | 5 | 5 | 15 | 15 | 0 | 0 | 145 | 50 | 195 | 0 | 195 | 18 | | |
| | | 5 | 73 | 6 | 6 | 35 | 735 | 58 | 20 | 78 | 657 | | | | |
| | | 5 | 83 | 6 | 6 | 41 | 861 | 58 | 20 | 78 | 1,000 | | | | |
| | | 5 | 9 | 8 | 8 | 0 | 0 | 77 | 26 | 103 | 897 | 440 | 53 | | |
| | | 6 | 66 | 8 | 8 | 29 | 609 | 77 | 26 | 103 | 1,000 | 0 | | | |
| | | Sub-total | 240 | 63 | 63 | 105 | 2,205 | 608 | 208 | 816 | | 454 | 843 | 42 | |
| | Nov. | 5 | 51 | 4 | 75 | 22 | 462 | 39 | 248 | 287 | 1,000 | 175 | | 21 | |
| | | 5 | 43 | 6 | 91 | 17 | 357 | 58 | 301 | 359 | 998 | 0 | | | |
| | | 5 | 21 | 4 | 12 | 4 | 84 | 39 | 40 | 79 | 1,000 | 3 | | | |
| | | 5 | 1 | 10 | 30 | 0 | 0 | 97 | 99 | 196 | 804 | | | | |
| | | 5 | 18 | 12 | 24 | 2 | 42 | 116 | 79 | 195 | 651 | | | | |
| | | 5 | 17 | 12 | 24 | 1 | 21 | 116 | 79 | 195 | 477 | | | | |
| | | Sub-total | 151 | 48 | 256 | 46 | 966 | 465 | 846 | 1,311 | | 178 | | | |
| | Dec. | 5 | 41 | 9 | 18 | 16 | 336 | 87 | 60 | 147 | 666 | | | | |
| | | 5 | 44 | 12 | 24 | 17 | 357 | 116 | 79 | 195 | 828 | | | | |
| | | 5 | 99 | 3 | 6 | 50 | 1,050 | 29 | 20 | 49 | 1,000 | 829 | 45 | | |
| | | 5 | 109 | 6 | 12 | 56 | 1,176 | 58 | 40 | 98 | 1,000 | 1,078 | 59 | | |
| | | 5 | 5 | 12 | 30 | 0 | 0 | 116 | 99 | 215 | 785 | | | | |
| | | 6 | 9 | 15 | 30 | 0 | 0 | 145 | 99 | 244 | 541 | | | | |
| | | Sub-total | 307 | 57 | 120 | 139 | 2,919 | 551 | 397 | 948 | | 1,907 | | | |
| | | Total | 3,189 | 707 | 1,275 | 1,390 | 29,190 | 6,831 | 4,222 | 11,053 | 1,187 | 18,783 | 112 | | |

4. Drainage Plan

4.1 General

Rainfall on terraced experimental fields shall be drained to the surrounding drainage canal network connected to the farm pond. Excessed water from the farm pond shall be drained to the existing drainage canal along the National road : Jalan Raya Darmaga. Rainfall on the soil conservation experiment fields, workstation and workshop and part of link road shall be drained through the drainage canal toward the Cihideung River.

4.2 Design modulus of drainage

The design modulus of the drainage facilities has been decided in consideration of the importance of their functions in referring the short duration rainfall intensity (Table C1-15) as follows :

- (1) drainage canals
to drain fully 10-Yr, 15 minutes rainfall intensity : 183.5 mm/hr
- (2) lysimeter (a precise measurement fields) and side drainage canal of the link road
to drain fully 100-Yr, 5 minutes rainfall intensity : 289.3 mm/hr
- (3) spillway of the farm pond
to drain fully 100-Yr, 30 minutes rainfall intensity : 183.5 mm/hr

Therefore, the design modulus of drainage are calculated as follows :

- (1) drainage canals
 $q = 100 \times 183.5 \times 10^{-3} / 3,600 = 0.0051 \text{ m}^3/\text{sec} / 100 \text{ m}^2$
- (2) lysimeter and side drainage of link road
 $q = 100 \times 289.3 \times 10^{-3} / 3,600 = 0.0080 \text{ m}^3/\text{sec} / 100 \text{ m}^2$
- (3) spillway of farm pond
 $q = 100 \times 98.6 \times 10^{-3} / 3,600 = 0.0027 \text{ m}^3/\text{sec} / 100 \text{ m}^2$

4.3 Measurement devices to be installed in the drainage network for future water balance study

Measurement devices at the paddy experimental fields and lysimeter are proposed to be a kind of rectangular weir.

For the purpose, the dimension and discharge are calculated by the Itaya weir formula as follows :

$$Q = C \times B \times H^{1.5}$$

$$\text{where } C = 1.785 + \frac{0.00295}{H} + \frac{0.237 \cdot H}{D}$$

$$- 0.428 \cdot \sqrt{\frac{(B-B1) \cdot H}{B \cdot D}} + 0.034 \cdot \sqrt{\frac{B}{D}}$$

Q : Overflow discharge in m^3/sec

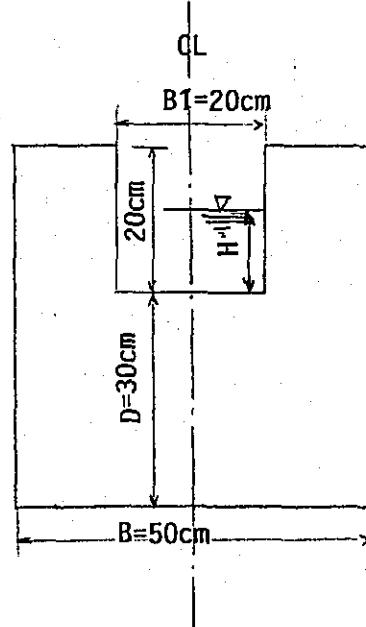
B : Canal width in m

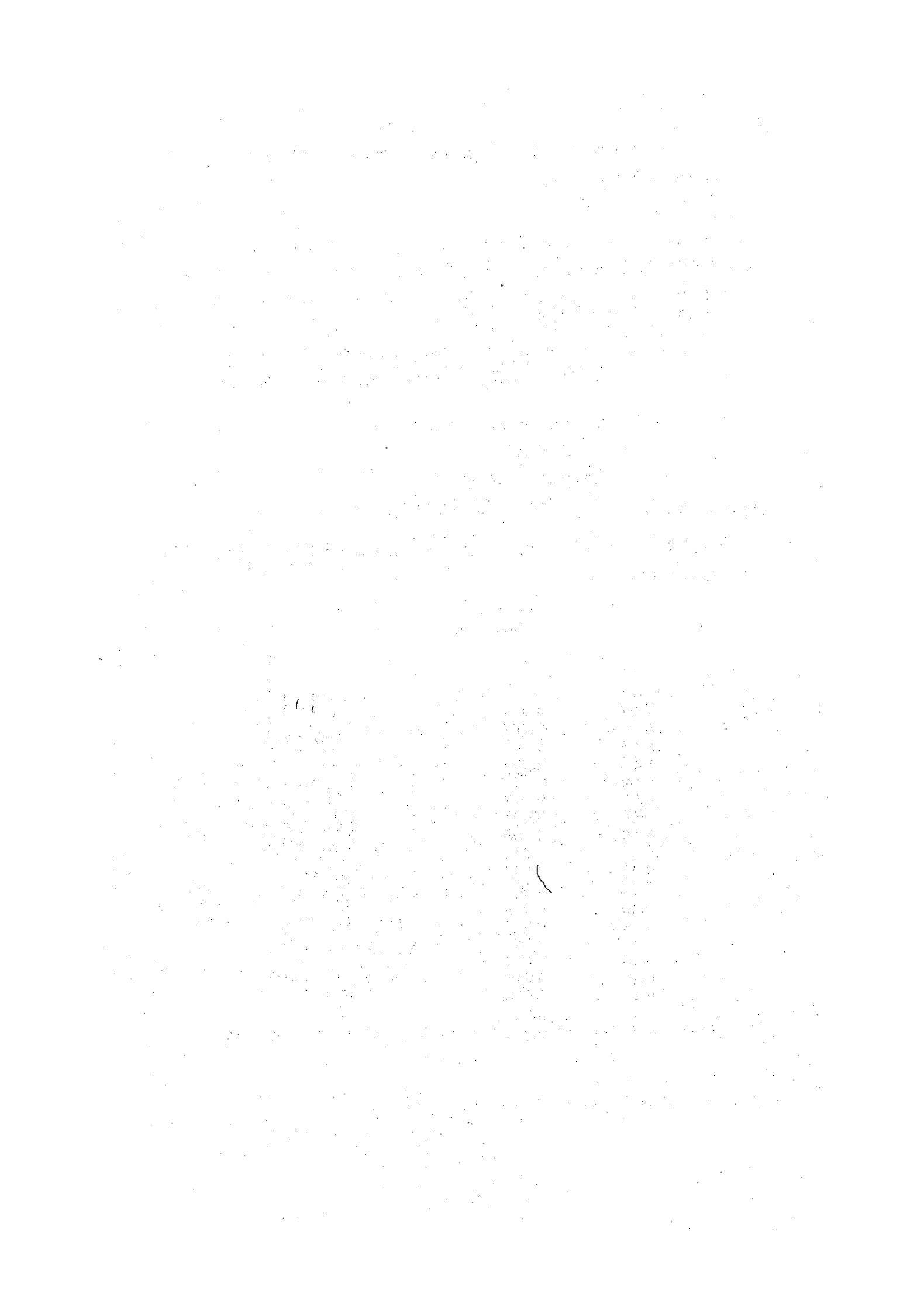
$B1$: Overflow width in m

D : Damming up height in m

When $B1 = 0.2$ m, $B = 0.5$ m, $D = 0.3$ m, the overflow discharge Q is calculated as follows :

| H | Q |
|------|-------|
| 0.01 | 0 |
| 0.02 | 0.001 |
| 0.03 | 0.002 |
| 0.04 | 0.003 |
| 0.05 | 0.004 |
| 0.06 | 0.005 |
| 0.07 | 0.007 |
| 0.08 | 0.008 |
| 0.09 | 0.009 |
| 0.1 | 0.011 |
| 0.11 | 0.013 |
| 0.12 | 0.014 |
| 0.13 | 0.016 |
| 0.14 | 0.018 |
| 0.15 | 0.002 |
| 0.16 | 0.022 |
| 0.17 | 0.024 |
| 0.18 | 0.026 |
| 0.19 | 0.029 |
| 0.2 | 0.031 |





付属資料 C 5 工事明細書

| Division | Work Item | Amount (Rp.) |
|---------------|-------------------------------------|--------------|
| Division-I | Land Levelling | 26,005,000 |
| Division-II | Link Road | 35,894,000 |
| Division-III | Farm Pond | 32,445,000 |
| Division-IV | Irrigation Canal | 6,610,000 |
| Division-V | Drainage Canal | 72,195,000 |
| Division-VI | Soil Conservation Test Field | 25,731,000 |
| Division-VII | Irrigation Test Field - Paddy Field | 2,420,000 |
| Division-VIII | Irrigation Test Field - Upland | 1,538,000 |
| Division-IX | Tractor Test Field | 487,000 |
| Division-X | Tractor Test Road | 13,344,000 |
| Grand Total | | 216,669,000 |

Division-I: Land Levelling

| Bill No. | Item | Unit | Q'ty | Unit Price (Rp.) | Amount (Rp.) | Remarks |
|----------|--|----------------|---------|------------------|--------------|---------------------|
| I-1 | Tractor Test Road Area and Link Road Area (BN: No.2+23.0 - BW: No.1) (A = 6,500 m ²) | | | | | |
| 1-1 | Excavation (Top Soil) | m ³ | 1,950 | 1,381 | 2,692,950 | No. Eq-1-2 |
| 1-2 | Excavation | m ³ | 1,935 | 1,654 | 3,200,490 | No. Eq-1-3 |
| 1-3 | Spreading | m ³ | 1,935 | 691 | 1,337,085 | No. Eq-3-3 |
| | I-1 Sub-Total | | | | 7,230,525 | |
| I-2 | Paddy Field Area, Farm Pond Area and Link Road Area (A: No. 0 - A: No. 2 + 35.0) (A = 8,300 m ²) | | | | | |
| 2-1 | Excavation (Top Soil) | m ³ | 2,310 | 1,381 | 3,190,110 | No. Eq-1-2 |
| 2-2 | Excavation | m ³ | 2,300 | 1,654 | 3,804,200 | No. Eq-1-3 |
| 2-3 | Spreading | m ³ | 2,300 | 691 | 1,589,300 | No. Eq-3-3 |
| | I-2 Sub Total | | | | 8,583,610 | |
| I-3 | Upland Area (A = 5,300 m ²) | | | | | |
| 3-1 | Excavation | m ³ | 20.0 | 1,654 | 33,080 | No. Eq-1-3 |
| 3-2 | Spreading | m ³ | 4,000.0 | 691 | 2,764,000 | No. Eq-3-3 |
| | I-3 Sub-Total | | | | 2,797,080 | |
| I-4 | Tractor Test Field Area and Link Road Area (A: No.2 + 35.0 - B: No.0) (A = 5,700 m ²) | | | | | |
| 4-1 | Excavation | m ³ | 1,290.0 | 1,654 | 2,133,660 | No. Eq-1-3 |
| 4-2 | Spreading | m ³ | 3,200.0 | 691 | 2,211,200 | No. Eq-3-3 |
| | I-4 Sub-Total | | | | 4,344,860 | |
| I-5 | Soil Conservation Test Field Area and Link Road Area (BW: No.1 - BW: No.1 + 20.0 & C: No.0 - C: No.1 + 20.0) (A = 3,200 m ²) | | | | | |
| 5-1 | Excavation | m ³ | 1,300.0 | 1,654 | 2,150,200 | No. Eq-1-3 |
| 5-2 | Spreading | m ³ | 1,300.0 | 691 | 898,300 | No. Eq-3-3 |
| | I-5 Sub-Total | | | | 3,048,500 | |
| | Division-I Total | | | | 26,004,575 | (Say 26,005,000) |

Division-II: Link Road

| Bill No. | Item | Unit | Q'ty | Unit Price (Rp.) | Amount (Rp.) | Remarks |
|----------|---|----------------|---------|------------------|--------------|---------------------|
| II-1 | Link Road: A (B = 5.0m, L = 180.0m) | | | | | |
| 1-1 | Spreading | m ³ | 489.6 | 691 | 338,314 | No. Eq-3-3 |
| 1-2 | Compaction | m ³ | 489.6 | 1,456 | 712,858 | No. Eq-4 |
| 1-3 | Sub Base Course (t = 150) | m ² | 900.0 | 2,778 | 2,500,200 | No. 14 |
| 1-4 | Form Work | m ² | 252.0 | 8,108 | 2,043,216 | No. 8 |
| 1-5 | Concrete | m ³ | 23.4 | 98,646 | 2,308,316 | No. 7-2 |
| 1-6 | Asphalt Pavement (t = 50) | m ² | 900.0 | 7,531 | 6,777,900 | No. 11 |
| 1-7 | Wet Masonry | m ² | 10.0 | 52,531 | 525,310 | No. 19 |
| | II-1 Sub-Total | | | | 15,206,114 | |
| II-2 | Link Road: B (B = 4.0m, L = 204.0m) & C (B = 4.0 m, L = 70.0 m) | | | | | |
| 2-1 | Spreading | m ³ | 663.1 | 691 | 458,202 | No. Eq-3-2 |
| 2-2 | Compaction | m ³ | 663.1 | 1,456 | 965,474 | No. Eq-4 |
| 2-3 | Sub Base Course (t = 150) | m ² | 1,096.0 | 2,778 | 3,044,688 | No. 14 |
| 2-4 | Form Work | m ² | 383.6 | 8,108 | 3,110,229 | No. 8 |
| 2-5 | Concrete | m ³ | 35.6 | 98,646 | 3,511,798 | No. 7-2 |
| 2-6 | Asphalt Pavement (t = 50) | m ² | 1,096.0 | 7,531 | 8,253,976 | No. 11 |
| | II-2 Sub-Total | | | | 19,344,367 | |
| II-3 | Gate, Setting & Base | | | | | |
| 3-1 | Gate, Setting & Base | L.S. | 1.0 | | 1,344,000 | |
| | II-3 Sub-Total | | | | 1,344,000 | |
| | Division-II Total | | | | 35,894,481 | (Say 35,894,000) |

Division-III: Farm Pond

| Bill No. | Item | Unit | Q'ty | Unit Price (Rp.) | Amount (Rp.) | Remarks |
|----------|--|--------------|---------|------------------|--------------|---------------------|
| III-1 | Farm Pond ($V = 1,000 \text{ m}^3$) | | | | | |
| 1-1 | Excavation (by Equip.) | m^3 | 1,725.0 | 3,126 | 5,392,350 | No. Eq-2-3 |
| 1-2 | Excavation | m^3 | 81.0 | 3,025 | 245,025 | No. 1-1 |
| 1-3 | Hauling | m^3 | 210.0 | 1,326 | 278,460 | No. 2-1 |
| 1-4 | Compaction | m^3 | 210.0 | 1,606 | 337,260 | No. 5 |
| 1-5 | Smoothing | m^2 | 900.0 | 1,826 | 1,643,400 | No. 4 |
| 1-6 | Stone Masonry | m^2 | 194.0 | 16,664 | 3,232,816 | No. 10 |
| | III-1 Sub-Total | | | | 11,129,311 | |
| III-2 | Spillway | | | | | |
| 2-1 | Excavation | m^3 | 130.6 | 3,126 | 408,256 | No. Eq-2-3 |
| 2-2 | Form Work | m^2 | 175.1 | 8,108 | 1,419,711 | No. 8 |
| 2-3 | Reinforcement-Bar | ton | 2.0 | 1,727,500 | 3,455,000 | No. 9 |
| 2-4 | Concrete | m^3 | 40.5 | 93,710 | 3,795,255 | No. 7-1 |
| 2-5 | Backfill | m^3 | 55.6 | 1,606 | 89,294 | No. 13 |
| | III-2 Sub-Total | | | | 9,167,516 | |
| III-3 | Pump, Catch Basin, Stairs & Suction Box | | | | | |
| 3-1 | Excavation | m^3 | 13.4 | 3,025 | 40,535 | No. 1-1 |
| 3-2 | Form Work | m^2 | 24.5 | 8,108 | 198,646 | No. 8 |
| 3-3 | Reinforcement-Bar | ton | 0.2 | 1,727,500 | 345,500 | No. 9 |
| 3-4 | Concrete | m^3 | 4.1 | 93,710 | 384,211 | No. 7-1 |
| 3-5 | Backfill | m^3 | 6.4 | 1,606 | 10,278 | No. 13 |
| 3-6 | Pump No. 1 (Farm Pond), Setting & Base | L.S. | 1.0 | | 1,709,000 | |
| 3-7 | Pump No. 2 (Cihideung River), Setting & Base | L.S. | 1.0 | | 5,764,000 | |
| | III-3 Sub-Total | | | | 8,452,170 | |
| III-4 | Inlet (3 nos.) | | | | | |
| 4-1 | Excavation | m^3 | 63.0 | 3,126 | 196,938 | No. Eq-2-3 |
| 4-2 | Form Work | m^2 | 123.2 | 8,108 | 998,906 | No. 8 |
| 4-3 | Reinforcement-Bar | ton | 0.7 | 1,727,500 | 1,209,250 | No. 9 |
| 4-4 | Concrete | m^3 | 13.0 | 93,710 | 1,218,230 | No. 7-1 |
| 4-5 | Backfill | m^3 | 45.0 | 1,606 | 72,270 | No. 13 |
| | III-4 Sub-Total | | | | 3,695,594 | |
| | Division-III Total | | | | 32,444,591 | (Say 32,445,000) |

Division-IV: Irrigation Canal

| Bill No. | Item | Unit | Q'ty | Unit Price (Rp.) | Amount (Rp.) | Remarks |
|----------|--|----------------|-------|------------------|--------------|--------------------|
| IV-1 | Irrigation Canal (L = 96.0 m) | | | | | |
| 1-1 | Excavation | m ³ | 35.5 | 3,025 | 107,388 | No. 1-1 |
| 1-2 | Form Work | m ² | 144.0 | 8,108 | 1,167,552 | No. 8 |
| 1-3 | Reinforcement-Bar | ton | 0.9 | 1,727,500 | 1,554,750 | No. 9 |
| 1-4 | Concrete | m ³ | 17.3 | 93,710 | 1,621,183 | No. 7-1 |
| 1-5 | Backfill | m ³ | 18.2 | 1,606 | 29,229 | No. 13 |
| | IV-1 Sub-Total | | | | 4,480,102 | |
| IV-2 | Concrete Box (1 m x 1 x 1 x 1 nos. & 0.5 m x 0.5 x 0.5 x 7 nos.) | | | | | |
| 2-1 | Excavation | m ³ | 23.1 | 3,025 | 69,878 | No. 1-1 |
| 2-2 | Form Work | m ² | 26.6 | 8,108 | 215,673 | No. 8 |
| 2-3 | Reinforcement-Bar | ton | 0.2 | 1,727,500 | 345,500 | No. 9 |
| 2-4 | Concrete | m ³ | 3.3 | 93,710 | 309,243 | No. 7-1 |
| 2-5 | Backfill | m ³ | 17.4 | 1,606 | 27,944 | No. 13 |
| | IV-2 Sub-Total | | | | 968,238 | |
| IV-3 | Crossing of Farm Road (3 nos.) | | | | | |
| 3-1 | Excavation | m ³ | 17.6 | 3,025 | 53,240 | No. 1-1 |
| 3-2 | Concrete | m ³ | 5.0 | 93,710 | 468,550 | No. 7-1 |
| 3-3 | Concrete Pipe (ø300) | m | 18.0 | 34,626 | 623,268 | No. 18 |
| 3-4 | Backfill | m ³ | 10.3 | 1,606 | 16,542 | No. 13 |
| | IV-3 Sub-Total | | | | 1,161,600 | |
| | Division-IV Total | | | | 6,609,940 | (Say 6,610,000) |

Division-V: Drainage Canal

| Bill No. | Item | Unit | Q'ty | Unit Price (Rp.) | Amount (Rp.) | Remarks |
|----------|--|----------------|---------|------------------|--------------|---------------------|
| V-1 | Drainage Canal: U-Gutter (L = 1,051.0) | | | | | |
| 1-1 | Excavation | m ³ | 620.5 | 3,126 | 1,939,683 | No. Eq-2-3 |
| 1-2 | Concrete Pipe ø500 (Half) | m | 1,051.0 | 27,825 | 29,244,075 | No. 12 |
| 1-3 | Form Work | m ² | 1,261.0 | 8,108 | 10,224,188 | No. 9 |
| 1-4 | Concrete | m ³ | 105.1 | 93,710 | 9,848,921 | No. 7-1 |
| 1-5 | Backfill | m ³ | 525.5 | 1,606 | 843,953 | No. 13 |
| 1-6 | Smoothing | m ² | 1,220.7 | 1,826 | 2,228,998 | No. 4 |
| | V-1 Sub-Total | | | | 54,329,818 | |
| V-2 | Drainage Canal: Open Ditch (L = 400.0 m) | | | | | |
| 2-1 | Excavation | m ³ | 200.0 | 3,126 | 625,200 | No. Eq-2-3 |
| 2-2 | Smoothing | m ² | 764.0 | 1,826 | 1,395,064 | No. 4 |
| | V-2 Sub-Total | | | | 2,020,264 | |
| V-3 | Drainage Canal: Conc.-Pipe (L = 120.0 m) | | | | | |
| 3-1 | Excavation | m ³ | 192.0 | 3,126 | 600,192 | No. Eq-2-3 |
| 3-2 | Form Work | m ² | 72.0 | 8,108 | 583,776 | No. 9 |
| 3-3 | Concrete | m ³ | 32.4 | 93,710 | 3,036,204 | No. 7-1 |
| 3-4 | Concrete Pipe (ø500) | m | 120.0 | 56,175 | 6,741,000 | No. 16 |
| 3-5 | Backfill | m ³ | 84.0 | 1,606 | 134,904 | No. 13 |
| | V-3 Sub-Total | | | | 11,096,076 | |
| V-4 | Concrete Box (31 nos.) | | | | | |
| 4-1 | Excavation | m ³ | 85.3 | 3,025 | 258,033 | No. 1-1 |
| 4-2 | Form Work | m ² | 185.3 | 8,108 | 1,502,412 | No. 8 |
| 4-3 | Reinforcement-Bar | ton | 0.8 | 1,727,500 | 1,382,000 | No. 9 |
| 4-4 | Concrete | m ³ | 16.2 | 93,710 | 1,518,102 | No. 7-1 |
| 4-5 | Backfill | m ³ | 55.1 | 1,606 | 88,491 | No. 13 |
| | V-4 Sub-Total | | | | 4,749,038 | |
| | Division-V Total | | | | 72,195,196 | (Say 72,195,000) |

Division-VI: Soil Conservation Test Field

| Bill No. | Item | Unit | Q'ty | Unit Price (Rp.) | Amount (Rp.) | Remarks |
|----------|--|----------------|-------|------------------|--------------|---------------------|
| VI-1 | Soil Conservation Test Field - Plot A, B & C (25.0 m x 20.0 m x 3 plots) | | | | | |
| 1-1 | Excavation | m ³ | 112.0 | 3,126 | 350,112 | No. Eq-2-3 |
| 1-2 | Form Work | m ² | 216.5 | 8,108 | 1,755,382 | No. 8 |
| 1-3 | Reinforcement-Bar | ton | 3.0 | 1,727,500 | 5,182,500 | No. 9 |
| 1-4 | Concrete | m ³ | 59.2 | 93,710 | 5,547,632 | No. 7-1 |
| 1-5 | Backfill | m ³ | 167.1 | 1,606 | 268,363 | No. 13 |
| | IV-1 Sub-Total | | | | 13,103,989 | |
| VI-2 | Sedimentation Tank - Plot A, B & C (L = 61.2 m) | | | | | |
| 2-1 | Excavation | m ³ | 123.0 | 3,126 | 384,498 | No. Eq-2-3 |
| 2-2 | Form Work | m ² | 140.8 | 8,108 | 1,141,606 | No. 8 |
| 2-3 | Reinforcement-Bar | ton | 1.1 | 1,727,500 | 1,900,250 | No. 9 |
| 2-4 | Concrete | m ³ | 21.4 | 93,710 | 2,005,394 | No. 7-1 |
| 2-5 | Backfill | m ³ | 6.1 | 1,606 | 9,797 | No. 13 |
| | VI-2 Sub-Total | | | | 5,441,545 | |
| VI-3 | Soil Conservation Test Field - Plot D & E (25.0 m x 10.0 m x 2 plots) | | | | | |
| 3-1 | Excavation | m ³ | 34.5 | 3,126 | 107,847 | No. Eq-2-3 |
| 3-2 | Form Work | m ² | 76.2 | 8,108 | 617,830 | No. 8 |
| 3-3 | Reinforcement-Bar | ton | 1.2 | 1,727,500 | 2,073,000 | No. 9 |
| 3-4 | Concrete | m ³ | 24.9 | 93,710 | 2,333,379 | No. 7-1 |
| 3-5 | Backfill | m ³ | 95.9 | 1,606 | 154,015 | No. 13 |
| | VI-3 Sub-Total | | | | 5,286,071 | |
| VI-4 | Sedimentation Tank - Plot D & E (L = 20.9 m) | | | | | |
| 4-1 | Excavation | m ³ | 42.0 | 3,126 | 131,292 | No. Eq-2-3 |
| 4-2 | Form Work | m ² | 48.1 | 8,108 | 389,995 | No. 8 |
| 4-3 | Reinforcement-Bar | ton | 0.4 | 1,727,500 | 691,000 | No. 9 |
| 4-4 | Concrete | m ³ | 7.3 | 93,710 | 684,083 | No. 7-1 |
| 4-5 | Backfill | m ³ | 2.1 | 1,606 | 3,373 | No. 13 |
| | VI-4 Sub-Total | | | | 1,899,743 | |
| | Division-VI Total | | | | 25,731,348 | (Say 25,731,000) |

Division-VII: Irrigation Test Field - Paddy Field

| Bill No. | Item | Unit | Q'ty | Unit Price (Rp.) | Amount (Rp.) | Remarks |
|----------|--|----------------|-------|------------------|--------------|--------------------|
| VII-1 | Paddy Field (25.0m x 30.0m x 4 plots) | | | | | |
| 1-1 | Excavation | m ³ | 690.0 | 1,654 | 1,141,260 | No. Eq-1-3 |
| 1-2 | Spreading | m ³ | 690.0 | 691 | 476,790 | No. Eq-3-3 |
| 1-3 | Smoothing | m ² | 186.0 | 1,826 | 339,636 | No. 4 |
| 1-4 | Spreading (Top Soil) | m ³ | 600.0 | 684 | 410,400 | No. Eq-3-2 |
| | VII-1 Sub-Total | | | | 2,368,086 | |
| VII-2 | Weir at Outlet for Irrigation Water (4 nos.) | | | | | |
| 2-1 | Excavation | m ³ | 1.7 | 3,025 | 5,143 | No. 1-1 |
| 2-2 | Form Work | m ² | 2.6 | 8,108 | 21,081 | No. 8 |
| 2-3 | Concrete | m ³ | 0.2 | 93,710 | 18,742 | No. 7-1 |
| 2-4 | Backfill | m ³ | 1.6 | 1,606 | 2,570 | No. 13 |
| | VII-2 Sub-Total | | | | 47,536 | |
| VII-3 | Weir at Inlet for Irrigation Water (4 nos.) | | | | | |
| 3-1 | Concrete | m ³ | 0.02 | 93,710 | 1,874 | No. 7-1 |
| 3-2 | Form Work | m ² | 0.3 | 8,108 | 2,432 | No. 8 |
| | VII-3 Sub-Total | | | | 4,306 | |
| | Division-VII Total | | | | 2,419,928 | (Say 2,420,000) |

Division-VIII: Irrigation Test field - Upland

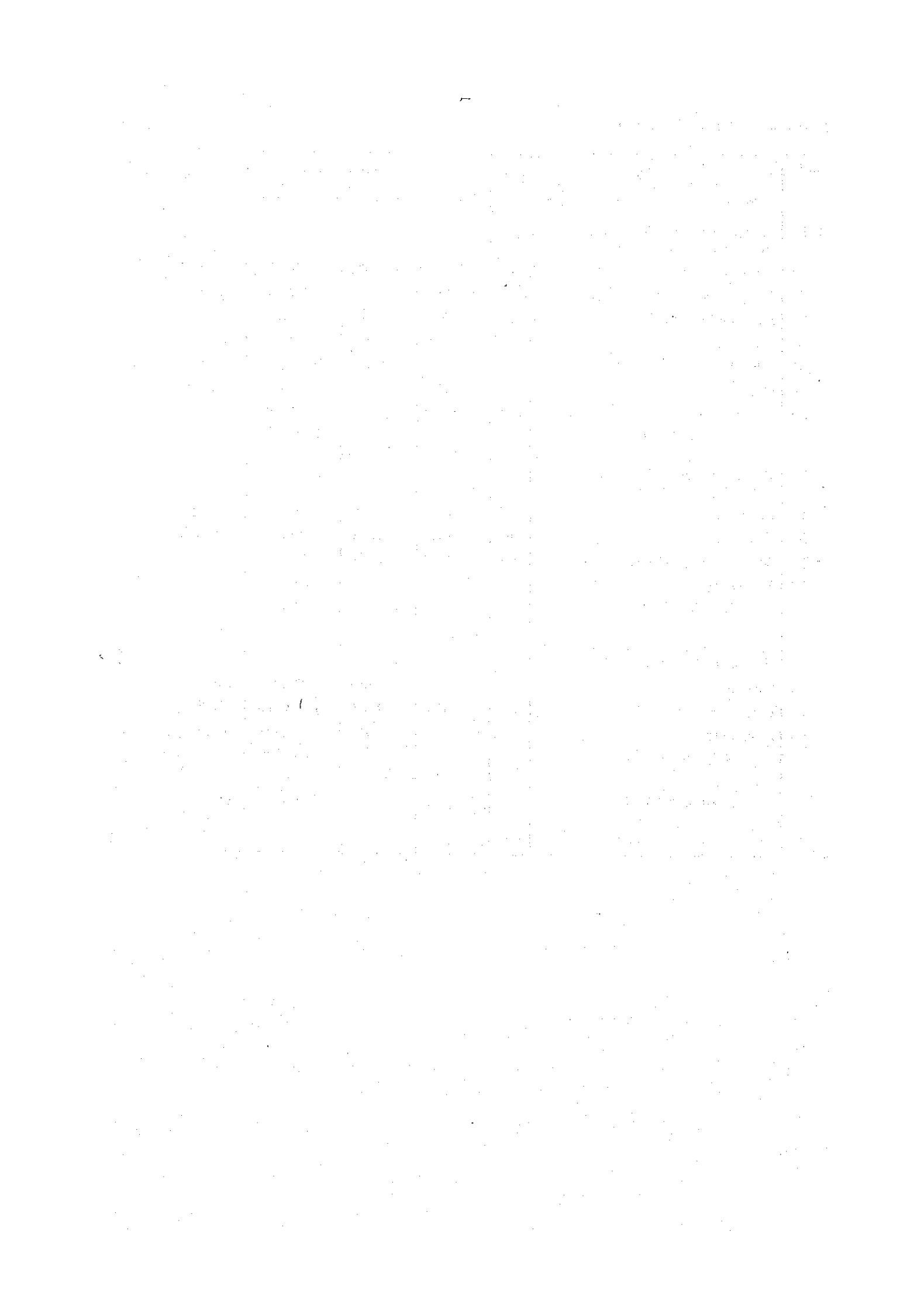
| Bill No. | Item | Unit | Q'ty | Unit Price (Rp.) | Amount (Rp.) | Remarks |
|----------|--|----------------|-------|------------------|--------------|--------------------|
| VIII-1 | Upland (30.0 m x 90.0 m x 1 plot) | | | | | |
| 1-1 | Spreading (Top Soil) | m ³ | 440.0 | 684 | 300,960 | No. Eq-3-2 |
| 1-2 | Hauling (Top Soil) | m ³ | 100.0 | 1,326 | 132,600 | No. 2-1 |
| | VIII-1 Sub-Total | | | | 433,560 | |
| VIII-2 | Farm Road: E (B = 3.0 m, L = 100.0 m) | | | | | |
| 2-1 | Spreading | m ³ | 43.0 | 691 | 29,713 | No. Eq-3-3 |
| 2-2 | Compaction | m ³ | 43.0 | 1,456 | 62,608 | No. Eq-4 |
| 2-3 | Sub Base Course (t = 150) | m ² | 300.0 | 2,778 | 833,400 | No. 14 |
| 2-4 | Smoothing | m ² | 98.0 | 1,826 | 178,948 | No. 4 |
| | VIII-2 Sub-Total | | | | 1,104,669 | |
| | Division-VIII Total | | | | 1,538,229 | (Say 1,538,000) |

Division-IX: Tractor Test Field

| Bill No. | Item | Unit | Q'ty | Unit Price (Rp.) | Amount (Rp.) | Remarks |
|----------|--|----------------|-------|------------------|--------------|------------------|
| IX-1 | Tractor Test Field (86.0 m x 35.0 m x 1 plot) | | | | | |
| 1-1 | Spreading (Top Soil) | m ³ | 480.0 | 684 | 328,320 | No. Eq-3-2 |
| 1-2 | Hauling | m ³ | 120.0 | 1,326 | 159,120 | No. 2-1 |
| | IX-1 Sub-Total | | | | 487,440 | |
| | Division-IX Total | | | | 487,440 | (Say 487,000) |

Division-X: Tractor Test Road

| Bill No. | Item | Unit | Q'ty | Unit Price (Rp.) | Amount (Rp.) | Remarks |
|----------|--|----------------|-------|------------------|--------------|---------------------|
| X-1 | Tractor Test Road: D: Concrete Pave. (B = 3.0 m, L = 150.0 m) | | | | | |
| 1-1 | Spreading | m ³ | 231.0 | 691 | 159,621 | No. Eq-3-3 |
| 1-2 | Compaction | m ³ | 231.0 | 1,456 | 336,336 | No. Eq-4 |
| 1-3 | Sub Base Course (t = 200) | m ² | 450.0 | 3,702 | 1,665,900 | No. 15 |
| 1-4 | Form Work | m ² | 36.0 | 8,108 | 291,888 | No. 8 |
| 1-5 | Wire Mesh | m ² | 450.0 | 5,968 | 2,685,600 | No. 17 |
| 1-6 | Concrete | m ³ | 54.0 | 98,646 | 5,326,884 | No. 7-2 |
| 1-7 | Smoothing | m ² | 366.0 | 1,826 | 668,316 | No. 4 |
| | X-1 Sub-Total | | | | 11,134,545 | |
| X-2 | Tractor Test Road: Gravel Pave. (B = 3.0 m, L = 150.0 m) | | | | | |
| 2-1 | Spreading | m ³ | 65.0 | 691 | 44,915 | No. Eq-3-3 |
| 2-2 | Compaction | m ³ | 65.0 | 1,456 | 94,640 | No. Eq-4 |
| 2-3 | Sub Base Course (t = 150) | m ² | 450.0 | 2,778 | 1,250,100 | No. 14 |
| 2-4 | Smoothing | m ² | 147.0 | 1,826 | 268,422 | No. 4 |
| | X-2 Sub-Total | | | | 1,658,077 | |
| X-3 | Tractor Test Road: Earth Road (B = 3.0 m, L = 150.0 m) | | | | | |
| 3-1 | Spreading | m ³ | 132.0 | 691 | 91,212 | No. Eq-3-3 |
| 3-2 | Compaction | m ³ | 132.0 | 1,456 | 192,192 | No. Eq-4 |
| 3-3 | Smoothing | m ² | 147.0 | 1,826 | 268,422 | No. 4 |
| | X-3 Sub-Total | | | | 551,826 | |
| | Division-X Total | | | | 13,344,448 | (Say 13,344,000) |



付属資料 C 6 労務費及び材料単価

LABOUR COST

| Item | Unit | Unit Price (Rp.) |
|----------------------------|------|---------------------|
| Labour | m.d | 3,500 |
| Foreman | m.d | 5,000 |
| Carpenter | m.d | 4,000 |
| Head of Carpenter | m.d | 5,000 |
| Stone Worker | m.d | 4,000 |
| Head of Stone Worker | m.d | 5,000 |
| Steel Worker | m.d | 4,500 |
| Head of Steel Worker | m.d | 5,000 |
| Asphalt Worker | m.d | 4,000 |
| Driver | m.d | 4,000 |
| Operator (Heavy Equipment) | m.d | 5,000 |
| Assistant Operator | m.d | 4,000 |
| Mechanical | m.d | 4,000 |
| Electrical | m.d | 5,000 |

MATERIAL COST

| Item | Unit | Unit Price (Rp.) | Remarks |
|-----------------------|----------------|---------------------|------------|
| Sand | m ³ | 12,500 | |
| Gravel | m ³ | 12,500 | |
| Gravel for Pavement | m ³ | 13,000 | |
| Stone | m ³ | 15,000 | |
| Lumber | m ³ | 150,000 | |
| Reinforced Iron Bar | kg | 750 | |
| Nail | kg | 1,500 | |
| Wire for Binding | kg | 1,250 | |
| Cement | bag | 4,650 | 40 kg |
| Asphalt Pitch | ton | 49,500 | |
| Tack Coat | m ² | 1,020 | |
| Gasoline | lit | 385 | |
| Diesel | lit | 200 | |
| Concrete Pipe ø500 mm | pc | 50,000 | L = 1 m |
| Concrete Pipe ø300 mm | pc | 145,150 | L = 4.72 m |
| PVC Pipe ø2" | stick | 22,200 | L = 4 m |
| PVC Pipe ø4" | stick | 67,000 | L = 4 m |
| Wire Mesh | m ² | 5,400 | |

付属資料 C 7 工事単価

LIST OF UNIT PRICE

| Item | Unit | Unit Price (Rp.) |
|--|----------------|---------------------|
| 1. Unit Price by Manpower | | |
| No. 1 Excavation by Manpower | | |
| No. 1-1 Normal Soil | m ³ | 3,025 |
| No. 1-2 Hard Soil | m ³ | 4,032 |
| No. 2 Hauling by Manpower | | |
| No. 2-1 Distance (L) less than 30 m | m ³ | 1,326 |
| No. 2-2 Distance (L) more than 30 m | m ³ | 14L + 1,050 |
| No. 4 Smoothing of Face Excavated or Filled up | m ² | 1,826 |
| No. 5 Compacting by Manpower | m ³ | 1,606 |
| No. 6 Compacting by Compactor | m ³ | 1,169 |
| No. 7 Concrete Mixed by Portable Concrete Mixer | | |
| No. 7-1 σ28 = 175 kg/cm ² | m ³ | 93,710 |
| No. 7-2 σ28 = 225 kg/cm ² | m ³ | 98,646 |
| No. 8 Wooden Form of Concrete | m ² | 8,108 |
| No. 9 Processing & Assembling of Reinforced Iron Bar | ton | 1,727,500 |
| No. 10 Stone Masonry | m ² | 16,664 |
| No. 11 Asphalt Pavement (t = 50 mm) | m ² | 7,531 |
| No. 12 Half Concrete Pile (ø500) | m | 27,825 |
| No. 13 Backfill by Manpower | m ³ | 1,606 |
| No. 14 Sub Base Course (t = 150 mm) | m ² | 2,778 |
| No. 15 Sub Base Course (t = 200 mm) | m ² | 3,702 |
| No. 16 Concrete Pipe (ø500) | m | 56,175 |
| No. 17 Wire Mesh | m ² | 5,968 |
| No. 18 Concrete Pipe (ø300) | m | 34,626 |
| No. 19 Wet Masonry | m ² | 52,531 |

| Item | Unit | Unit Price (Rp.) |
|--|----------------|---------------------|
| 2. Unit Price by Using Construction Equipment | | |
| No. Eq-1 Excavation by Bulldozer (11 ton) | | |
| No. Eq-1-1 Sand | m ³ | 1,183 |
| No. Eq-1-2 Normal Soil | m ³ | 1,381 |
| No. Eq-1-3 Clayey Soil | m ³ | 1,654 |
| No. Eq-2 Excavation by Back-hoe Shovel (0.35 m³) | | |
| No. Eq-2-1 Sand | m ³ | 2,458 |
| No. Eq-2-2 Normal Soil | m ³ | 2,430 |
| No. Eq-2-3 Clayey Soil | m ³ | 3,126 |
| No. Eq-3 Spreading by Bulldozer (11 ton) | | |
| No. Eq-3-1 Sand | m ³ | 615 |
| No. Eq-3-2 Normal Soil | m ³ | 684 |
| No. Eq-3-3 Clayey Soil | m ³ | 691 |
| No. Eq-4 Compaction by Vibration Roller (3 ton) | | |
| | m ³ | 1,456 |
| 3. Operation Cost of Construction Equipment | | |
| No. OP-1 Bulldozer (11 ton) | day | 325,234 |
| No. OP-2 Back-hoe Shovel (0.35 m ³) | day | 409,850 |
| No. OP-3 Vibration Roller (3 ton) | day | 181,514 |

Breakdown of Unit Price

No. 1-1 Excavation by Manpower
 (Soil Condition: Normal Soil)

Rp. 3,025/m³

| Item | Q'ty | Unit | Unit Cost | Cost | Remarks |
|-----------------|-------|------|-----------|-------|---------|
| Labour | 0.75 | m.d | 3,500 | 2,625 | |
| Foreman | 0.025 | m.d | 5,000 | 125 | |
| Temporary Works | 10 | % | | 275 | |
| Total | | | | 3,025 | |

No. 1-2 Excavation by Manpower
 (Soil Condition: Hard Soil)

Rp. 4,032/m³

| Item | Q'ty | Unit | Unit Cost | Cost | Remarks |
|-----------------|-------|------|-----------|-------|---------|
| Labour | 1.0 | m.d | 3,500 | 3,500 | |
| Foreman | 0.033 | m.d | 5,000 | 165 | |
| Temporary Works | 10 | % | | 367 | |
| Total | | | | 4,032 | |

No. 2-1 Hauling by Manpower
 (Distance ≤ 30 m)

Rp. 1,326/m³

| Item | Q'ty | Unit | Unit Cost | Cost | Remarks |
|-----------------|------|------|-----------|-------|---------|
| Labour | 0.33 | m.d | 3,500 | 1,155 | |
| Foreman | 0.01 | m.d | 5,000 | 50 | |
| Temporary Works | 10 | % | | 121 | |
| Total | | | | 1,326 | |

No. 2-2 Hauling by Manpower
(Distance > 30 m)

| Item | Q'ty | Unit | Unit Cost | Cost | Remarks |
|---|------|------|-----------|------|---------|
| $K = \frac{a}{275} (L + 75) \times 1.1$ where; a = Unit Price, a = Wages for Labour, L = Hauling Distance (m) | | | | | |

$$K = \frac{3500}{275} (L + 75) \times 1.1 = 14.0L + 1,050 (\text{Rp.})$$

No. 4 Smoothing of Face Excavated or Filled up

Rp. 1,826/m²

| Item | Q'ty | Unit | Unit Cost | Cost | Remarks |
|-----------------|------|------|-----------|-------|---------|
| Labour | 0.46 | m.d | 3,500 | 1,610 | |
| Foreman | 0.01 | m.d | 5,000 | 50 | |
| Temporary Works | 10 | % | | 166 | |
| Total | | | | 1,826 | |

No. 5 Compacting by Manpower

Rp. 1,606/m³

| Item | Q'ty | Unit | Unit Cost | Cost | Remarks |
|-----------------------|------|------|-----------|--------------------------|---------|
| per 10 m ³ | | | | | |
| Labour | 4 | m.d | 3,500 | 14,000 | |
| Foreman | 0.12 | m.d | 5,000 | 600 | |
| Temporary Works | 10 | % | | 1,460 | |
| Total | | | | 16,060/10 m ³ | |
| per m ³ | | | | 1,606 | |

No. 6 Compacting by Compactor

Rp. 1,169/m³

| Item | Q'ty | Unit | Unit Cost | Cost | Remarks |
|--------------------------------|------|------|-----------|--------------------------|-------------------------|
| per 10 m ³ | | | | | |
| 1. Worker | | | | | |
| Labour | 2.30 | m.d | 3,500 | 8,050 | |
| Foreman | 0.07 | m.d | 5,000 | 350 | |
| Sub-total | | | | 8,400 | |
| 2. Fuel & Others | | | | | |
| Fuel | 0.9 | lit | 200 | 180 | 6 lit/day x 0.15 day |
| Others | 15 | % | | 27 | |
| Sub-total | | | | 207 | |
| 3. Depreciation & Others | 0.15 | day | 13,457 | 2,019 | |
| 4. Temporary Works & Others | 10 | % | | 1,063 | |
| Total | | | | 11,689/10 m ³ | |
| per m ³ | | | | 1,169 | |

No. 7-1 Concrete ($\sigma_{28} = 175 \text{ kg/cm}^2$)
 (Mixed by Portable Concrete Mixer)

Rp. 93,710/m³

| Item | Q'ty | Unit | Unit Cost | Cost | Remarks |
|-----------------------------|-------|----------------|-----------|--------|---------|
| 1. Material | | | | | |
| Gravel | 0.82 | m ³ | 12,500 | 10,250 | |
| Cement | 8.75 | bag | 4,650 | 40,688 | |
| Sand | 0.55 | m ³ | 12,500 | 6,875 | |
| Sub-total | | | | 57,813 | |
| 2. Worker | | | | | |
| Labour | 7.0 | m.d | 3,500 | 24,500 | |
| Foreman | 0.23 | m.d | 5,000 | 1,150 | |
| Sub-total | | | | 25,650 | |
| 3. Fuel & Others | | | | | |
| Mixer Fuel | 0.22 | lit | 200 | 44 | |
| Others | 20 | % | | 9 | |
| Vibrator Fuel | 0.22 | lit | 200 | 44 | |
| Others | 20 | % | | 9 | |
| Sub-total | | | | 106 | |
| 4. Depre. & Main. | | | | | |
| Mixer | 0.061 | day | 20,742 | 1,265 | |
| Vibrator | 0.071 | day | 5,027 | 357 | |
| Sub-total | | | | 1,622 | |
| 5. Temporary Works & Others | 10 | % | | 8,519 | |
| Total | | | | 93,710 | |

No. 7-2 Concrete ($\sigma_{28} = 225 \text{ kg/cm}^2$)
 (Mixed by Portable Concrete Mixer)

Rp. 98,646/m³

| Item | Q'ty | Unit | Unit Cost | Cost | Remarks |
|-----------------------------|------|----------------|-----------|--------|---------|
| 1. Material | | | | | |
| Gravel | 0.88 | m ³ | 12,500 | 11,000 | |
| Cement | 9.5 | bag | 4,650 | 44,175 | |
| Sand | 0.57 | m ³ | 12,500 | 7,125 | |
| Sub-total | | | | 62,300 | |
| 2. Worker | 1 | Complete | | 25,650 | No. 7-1 |
| 3. Fuel & Others | 1 | Complete | | 106 | No. 7-1 |
| 4. Depre. & Main. | 1 | Complete | | 1,622 | No. 7-1 |
| 5. Temporary Works & Others | 10 | % | | 8,968 | |
| Total | | | | 98,646 | |

No. 8 Wooden Form of Concrete

Rp. 8,108/m²

| Item | Q'ty | Unit | Unit Cost | Cost | Remarks |
|-------------------------------|-------|----------------|-----------|-------------------------|-----------------------------|
| per 10 m² | | | | | |
| 1. Form | | | | | |
| Wooden Plate | 0.196 | m ³ | 150,000 | 29,400 | (1) |
| Wooden Frame | 0.113 | m ³ | 150,000 | 16,950 | (2) |
| Iron Nail | 3.0 | kg | 1,500 | 4,500 | (3) |
| Sub-Total 1 | | | | 50,850 | (4)=(1)+(2)+(3) |
| Depre. Cost of 1 | 30 | % | | 15,255 | (5) |
| 2. Support | | | | | |
| Square Lumber | 0.339 | m ³ | 150,000 | 50,850 | (6) |
| Log | 0.154 | m ³ | 150,000 | 23,100 | (7) |
| Sub-Total 2 | | | | 73,950 | (8)=(6)+(7) |
| Depre. Cost of 2 | 20 | % | | 14,790 | (9) |
| 3. Other Materials | | | | | |
| Nail & Others | 1.1 | kg | 1,500 | 1,650 | (10) |
| Wire | 0.8 | kg | 1,250 | 1,000 | (11) |
| Oil Paint | 0.15 | lit | 1,000 | 150 | (12) |
| Others | 3 | % | | 985 | (13)=(5)+(9)+(10)+(11)+(12) |
| Sub-Total | | | | 3,785 | (14) |
| 4. Worker | | | | | |
| Carpenter | 3.36 | m.d | 4,000 | 13,440 | (15) |
| Labour | 4.14 | m.d | 3,500 | 14,490 | (16) |
| Foreman | 0.12 | m.d | 5,000 | 600 | (17) |
| Sub-Total | | | | 28,530 | (18) |
| 5. Trans. of Materials | 15 | % | | 18,720 | (19)=(4)+(8) |
| Total | | | | 81,080/10m ² | (20)=(5)+(9)+(14)+(18)+(19) |
| per m² | | | | | |
| | | | | 8,108 | |

No. 9 Processing & Assembling of Reinforced Iron Bar

Rp. 1,727,500/ton

| Item | Q'ty | Unit | Unit Cost | Cost | Remarks |
|------------------------|------|------|-----------|----------------|---------|
| per 100 kg | | | | | |
| 1. Materials | | | | | |
| Reinforced I.B. | 110 | kg | 750 | 82,500 | |
| Wire for Binding | 2 | kg | 1,250 | 2,500 | |
| Sub-Total | | | | 85,000 | |
| 2. Process. & Assembl. | | | | | |
| Steel Worker | 12 | m.d | 4,500 | 54,000 | |
| Labour | 9 | m.d | 3,500 | 31,500 | |
| Head | 0.45 | m.d | 5,000 | 2,250 | |
| Sub-Total | | | | 87,750 | |
| Total | | | | 172,750/100 kg | |
| per ton | | | | 1,727,500 | |

No. 10 Stone Masonry

Rp. 16,664/m²

| Item | Q'ty | Unit | Unit Cost | Cost | Remarks |
|--------------|-------|----------------|-----------|--------|---------|
| 1. Materials | | | | | |
| Stone | 0.385 | m ³ | 15,000 | 5,775 | |
| Gravel | 0.33 | m ³ | 12,500 | 4,125 | |
| Sub-Total | | | | 9,900 | |
| 2. Worker | | | | | |
| Stone Worker | 0.64 | m.d | 4,000 | 2,560 | |
| Labour | 0.58 | m.d | 3,500 | 2,030 | |
| Sub-Total | | | | 4,590 | |
| 3. Others | 15 | % | | 2,174 | |
| Total | | | | 16,664 | |

No. 11 Asphalt Pavement ($t = 50 \text{ mm}$)Rp. 7,531/m²

| Item | Q'ty | Unit | Unit Cost | Cost | Remarks |
|------------------------------|-------|------|-----------|----------------------------|---------|
| per 100 m² | | | | | |
| 1. Worker | | | | | |
| Asphalt Worker | 24.07 | m.d | 4,000 | 96,280 | |
| Labour | 22.52 | m.d | 3,500 | 78,820 | |
| Sub-Total | | | | 175,100 | |
| 2. Materials | | | | | |
| Asphalt Pitch | 9.38 | ton | 49,500 | 464,310 | |
| Gasoline | 2.1 | lit | 385 | 809 | |
| Sub-Total | | | | 465,119 | |
| 3. Fuel & Others | | | | | |
| Gasoline | 5.13 | lit | 385 | 1,975 | |
| Others | 10 | % | | 198 | |
| Sub-Total | | | | 2,173 | |
| 4. Depre. & Main. | | | | | |
| Tamper/Rammer | 1.25 | day | 10,000 | 12,500 | |
| 5. Temporary Works & Others | 15 | % | | 98,234 | |
| Total | | | | 753,126/100 m ² | |
| per m ² | | | | 7,531 | |

No. 12 Half Concrete Pipe (ø500 mm)

Rp. 27,825/m

| Item | Q'ty | Unit | Unit Cost | Cost | Remarks |
|--|------|------|-----------|---------------|---------|
| 1. Materials | | | | | |
| Half Concrete Pipe | 1 | m | 25,000 | 25,000 | |
| 2. Worker | | | | | |
| Labour | 0.4 | m.d | 3,500 | 1,400 | |
| Foreman | 0.02 | m.d | 5,000 | 100 | |
| Sub-total | | | | 1,500 | |
| 3. Temporary Works & Others | | | | | |
| | 5 | % | | 1,325 | |
| Total | | | | 27,825 | |

No. 13 Backfill by ManpowerRp. 1,606/m³

| Item | Q'ty | Unit | Unit Cost | Cost | Remarks |
|-----------------------------|------|------|-----------|--------------------------------|---------|
| per 10 m³ | | | | | |
| Labour | 4 | m.d | 3,500 | 14,000 | |
| Foreman | 0.12 | m.d | 5,000 | 600 | |
| Temporary Works | 10 | % | | 1,460 | |
| Total | | | | 16,060/10 m³ | |
| per m³ | | | | | |
| | | | | 1,606 | |

No. 14 Sub Base Course ($t = 150 \text{ mm}$)

Rp. 2,778/m²

| Item | Q'ty | Unit | Unit Cost | Cost | Remarks |
|------------------------------|------|----------------|-----------|----------------------------|----------|
| <i>per 100 m²</i> | | | | | |
| 1. Material | | | | | |
| Gravel | 16.5 | m ³ | 13,000 | 214,500 | |
| 2. Worker | | | | | |
| Labour | 11.0 | m.d | 3,500 | 38,500 | |
| Foreman | 0.15 | m.d | 5,000 | 750 | |
| Sub-Total | | | | 39,250 | |
| 3. Compaction | 16.5 | m ³ | 1,456 | 24,024 | No. Eq-4 |
| Total | | | | 277,774/100 m ² | |
| <i>per m²</i> | | | | | |
| | | | | 2,778 | |

No. 15 Sub Base Course ($t = 200 \text{ mm}$)

Rp. 3,702/m²

| Item | Q'ty | Unit | Unit Cost | Cost | Remarks |
|------------------------------|------|----------------|-----------|----------------------------|----------|
| <i>per 100 m²</i> | | | | | |
| 1. Material | | | | | |
| Gravel | 22.0 | m ³ | 13,000 | 286,000 | |
| 2. Worker | | | | | |
| Labour | 14.7 | m.d | 3,500 | 51,450 | |
| Foreman | 0.15 | m.d | 5,000 | 750 | |
| Sub-Total | | | | 52,200 | |
| 3. Compaction | 22.0 | m ³ | 1,456 | 32,032 | No. Eq-4 |
| Total | | | | 370,232/100 m ² | |
| <i>per m²</i> | | | | | |
| | | | | 3,702 | |

No. 16 Concrete Pipe ($\varnothing 500$ mm)

Rp. 56,175/m

| Item | Q'ty | Unit | Unit Cost | Cost | Remarks |
|-----------------------------|------|------|-----------|--------------|---------|
| per 10 pieces (10 m) | | | | | |
| 1. Material | | | | | |
| Concrete Pipe | 10 | nos. | 50,000 | 500,000 | |
| 2. Worker | | | | | |
| Labour | 10 | m.d. | 3,500 | 35,000 | |
| 3. Temporary Works & Others | 5 | % | | 26,750 | |
| Total | | | | 561,750/10 m | |
| per m | | | | 56,175 | |

No. 17 Wire MeshRp. 5,968/m²

| Item | Q'ty | Unit | Unit Cost | Cost | Remarks |
|------------------------|------|----------------|-----------|----------------------------|---------|
| per 100 m ² | | | | | |
| 1. Material | | | | | |
| Wire Mesh | 110 | m ² | 5,400 | 594,000 | |
| 2. Worker | | | | | |
| Labour | 0.8 | m/d | 3,500 | 2,800 | |
| Total | | | | 596,800/100 m ² | |
| per m ² | | | | 5,968 | |

No. 18 Concrete Pipe (ϕ 300 mm)

Rp. 34,626/m

| Item | Q'ty | Unit | Unit Cost | Cost | Remarks |
|----------------------|------|------|-----------|----------------|---------|
| per 1 piece (4.72 m) | | | | | |
| 1. Material | | | | | |
| Concrete Pipe | 1 | nos. | 145,150 | 145,150 | |
| 2. Worker | | | | | |
| Labour | 3 | m.d | 3,500 | 10,500 | |
| 3. Temporary Works & | | | | | |
| Others | 5 | % | | 7,783 | |
| Total | | | | 163,433/4.72 m | |
| per m | | | | 34,626 | |

No. 19 Wet Masonry

Rp. 52,531/m²

| Item | Q'ty | Unit | Unit Cost | Cost | Remarks |
|-----------------------|------|----------------|-----------|---------------------------|---------|
| per 10 m ² | | | | | |
| 1. Materials | | | | | |
| Stone | 3.5 | m ³ | 15,000 | 52,500 | |
| Gravel | 3.0 | m ³ | 12,500 | 37,500 | |
| Concrete | 3.6 | m ³ | 93,710 | 337,356 | No. 7-1 |
| VP (ϕ 50 mm) | 1.5 | m | 5,550 | 8,325 | |
| Sub-Total | | | | 435,681 | |
| 2. Worker | | | | | |
| Stone Worker | 3.30 | m.d | 4,000 | 13,200 | |
| Labour | 7.05 | m.d | 3,500 | 24,675 | |
| Foreman | 0.80 | m.d | 5,000 | 4,000 | |
| Sub-Total | | | | 41,875 | |
| 3. Others | 10 | % | | 47,756 | |
| Total | | | | 525,312/10 m ² | |
| per m ² | | | | 52,531 | |

No. Eq-1 Excavation by Bulldozer (11 ton)

| Item | Q'ty | Unit | Cost (Rp.) | Remarks |
|--------------------|------|----------------|------------|------------------------------------|
| Operation Cost | | | 325,234 | OP-1 |
| Temporary Works | 10 | % | 32,523 | |
| Total | | | 357,757 | |
| Eq-1-1 Sand | 1 | m ³ | 1,183 | Production 302.4 m ³ /d |
| Eq-1-2 Normal Soil | 1 | m ³ | 1,381 | Production 259.0 m ³ /d |
| Eq-1-3 Clayey Soil | 1 | m ³ | 1,654 | Production 216.3 m ³ /d |

No. Eq-2 Excavation by Back-hoe Shovel (0.35 m³)

| Item | Q'ty | Unit | Cost (Rp.) | Remarks |
|--------------------|------|----------------|------------|------------------------------------|
| Operation Cost | | | 409,850 | OP-2 |
| Temporary Works | 10 | % | 40,985 | |
| Total | | | 450,835 | |
| Eq-2-1 Sand | 1 | m ³ | 2,458 | Production 183.4 m ³ /d |
| Eq-2-2 Normal Soil | 1 | m ³ | 2,430 | Production 185.5 m ³ /d |
| Eq-2-3 Clayey Soil | 1 | m ³ | 3,126 | Production 144.2 m ³ /d |

No. Eq-3 Spreading by Bulldozer (11 ton)

| Item | Q'ty | Unit | Cost (Rp.) | Remarks |
|--------------------|------|----------------|------------|------------------------------------|
| Operation Cost | | | 325,234 | OP-1 |
| Temporary Works | 10 | % | 32,523 | |
| Total | | | 357,757 | |
| Eq-3-1 Sand | 1 | m ³ | 615 | Production 582.1 m ³ /d |
| Eq-3-2 Normal Soil | 1 | m ³ | 684 | Production 523.3 m ³ /d |
| Eq-3-3 Clayey Soil | 1 | m ³ | 691 | Production 517.4 m ³ /d |

No. Eq-4 Compaction by Vibration Roller (3 ton)

| Item | Q'ty | Unit | Cost (Rp.) | Remarks |
|-----------------|------|----------------|------------|------------------------------------|
| Operation Cost | | | 181,514 | OP-3 |
| Temporary Works | 10 | % | 18,151 | |
| Total | | | 199,665 | |
| Eq-4 | 1 | m ³ | 1,456 | Production 137.1 m ³ /d |

No. OP-1 Operation Cost of 11 ton Bulldozer

Rp. 325,234/day

| Item | Q'ty | Unit | Unit Cost | Cost | Remarks |
|------------------|------|------|-----------|---------|---------|
| 1. Worker | | | | | |
| Operator | 1.0 | m.d | 5,000 | 5,000 | |
| Assistance | 0.5 | m.d | 4,000 | 2,000 | |
| Sub-Total | | | | 7,000 | |
| 2. Fuel & Others | | | | | |
| Diesel Oil | 59.5 | lit | 200 | 11,900 | |
| Others | 30 | % | | 3,570 | |
| Sub-Total | | | | 15,470 | |
| 3. Depreciation | 7 | hr | 43,252 | 302,764 | |
| Total | | | | 325,234 | |

No. OP-2 Operation Cost of 0.35 m³ Back-hoe Shovel

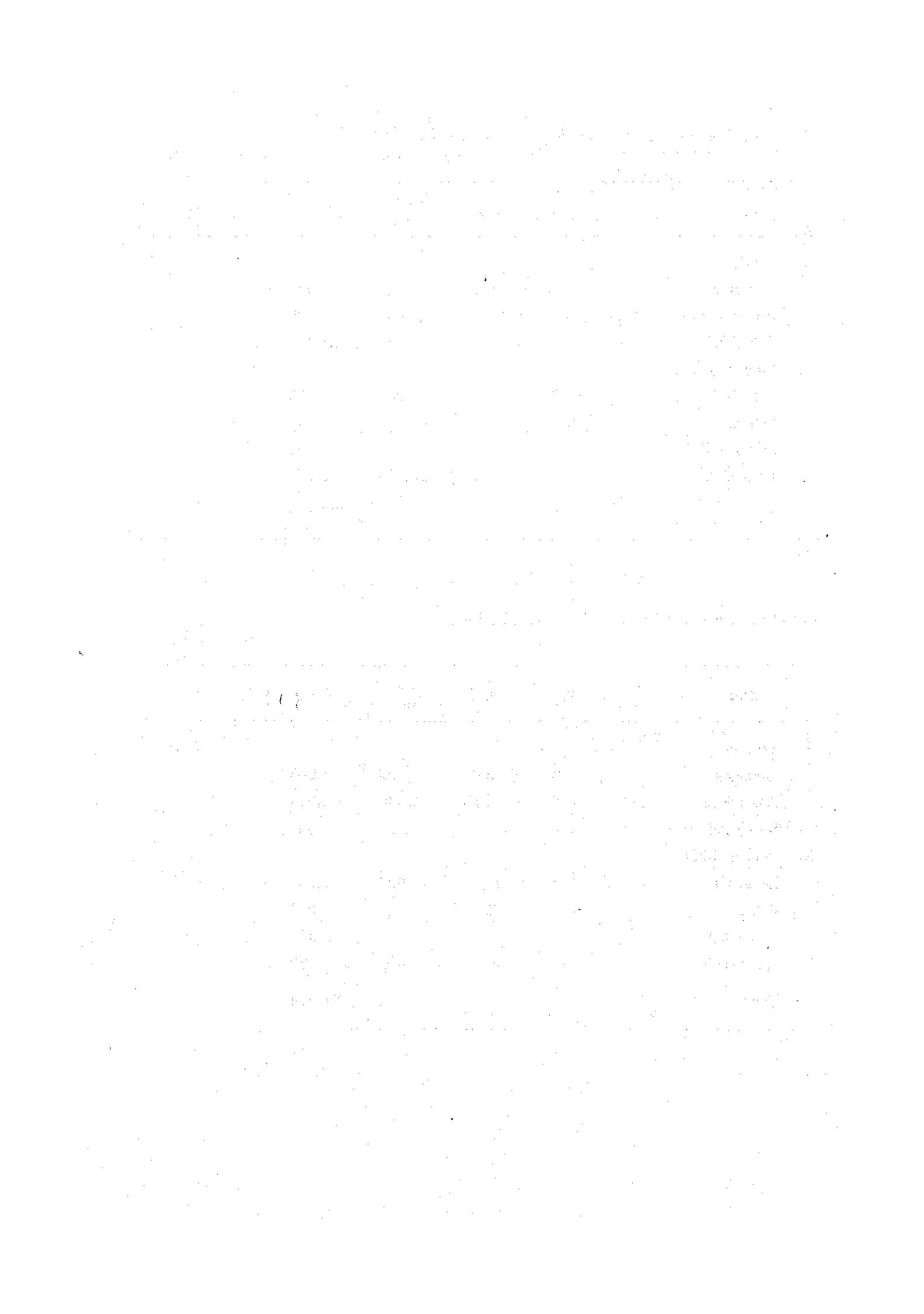
Rp. 409,850/day

| Item | Q'ty | Unit | Unit Cost | Cost | Remarks |
|------------------|------|------|-----------|---------|---------|
| 1. Worker | | | | | |
| Operator | 1.0 | m.d | 5,000 | 5,000 | |
| Assistance | 0.5 | m.d | 4,000 | 2,000 | |
| Sub-Total | | | | 7,000 | |
| 2. Fuel & Others | | | | | |
| Diesel Oil | 35.0 | lit | 200 | 7,000 | |
| Others | 30 | % | | 2,100 | |
| Sub-Total | | | | 9,100 | |
| 3. Depreciation | 7 | hr | 56,250 | 393,750 | |
| Total | | | | 409,850 | |

No. OP-3 Operation Cost of Vibration Roller 3 ton

Rp. 181,514/day

| Item | Q'ty | Unit | Unit Cost | Cost | Remarks |
|------------------|------|------|-----------|---------|---------|
| 1. Worker | | | | | |
| Operator | 1.0 | m.d | 5,000 | 5,000 | |
| Assistance | 0.5 | m.d | 4,000 | 2,000 | |
| Sub-Total | | | | 7,000 | |
| 2. Fuel & Others | | | | | |
| Diesel Oil | 8.9 | lit | 2,000 | 1,780 | |
| Others | 30 | % | | 534 | |
| Sub-Total | | | | 2,314 | |
| 3. Depreciation | 7 | hr | 24,600 | 172,200 | |
| Total | | | | 181,514 | |



付属資料 C 8 全体計画

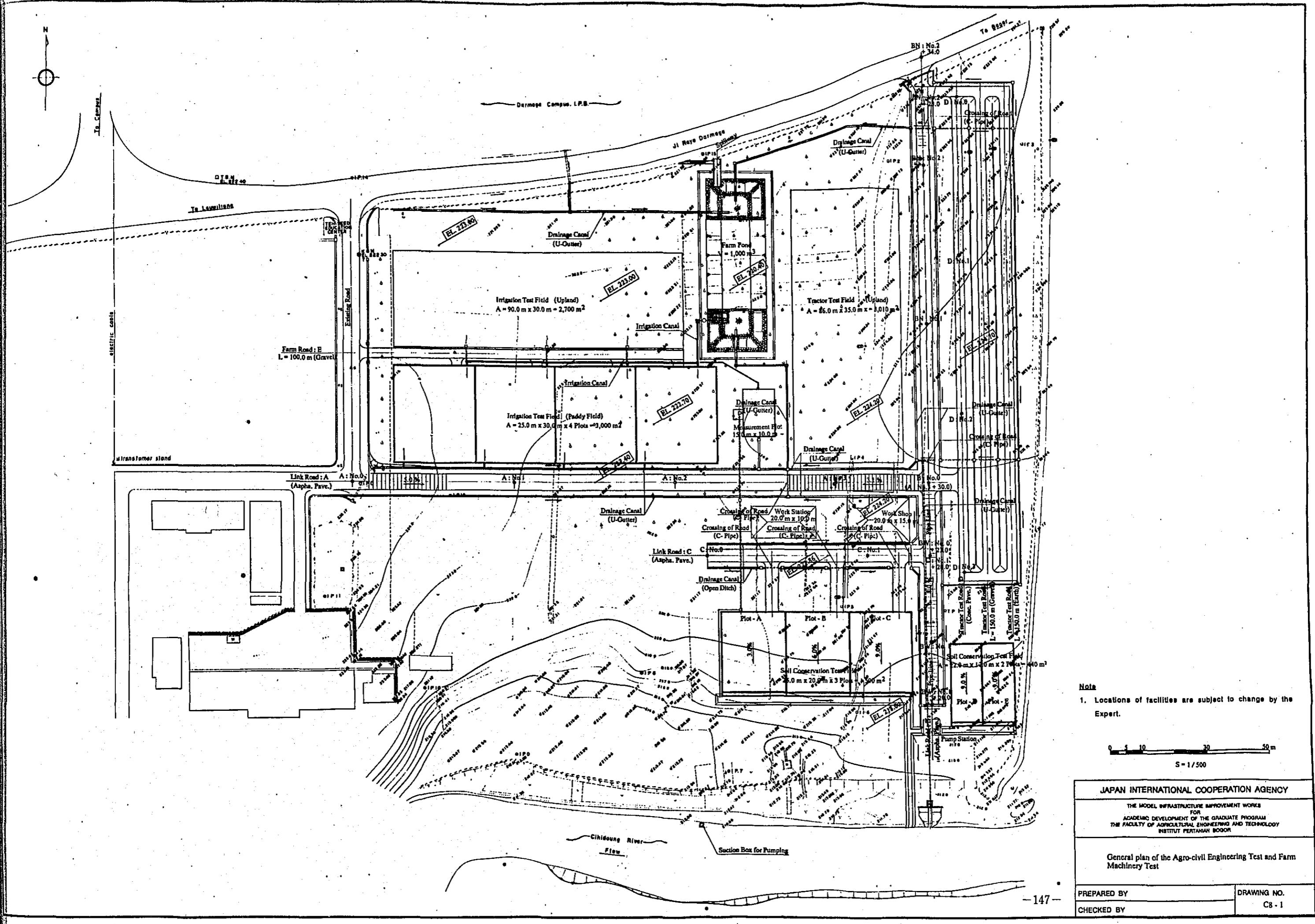
Based on the Basic Plan which was described in the Letter of Team Leader of the Detailed Design Survey Team of JICA dated January 16, 1990, general plan of the agro-civil engineering tests and farm machinery tests fields has been prepared at the depth of the detailed design study, as shown in Drawing C8-1.

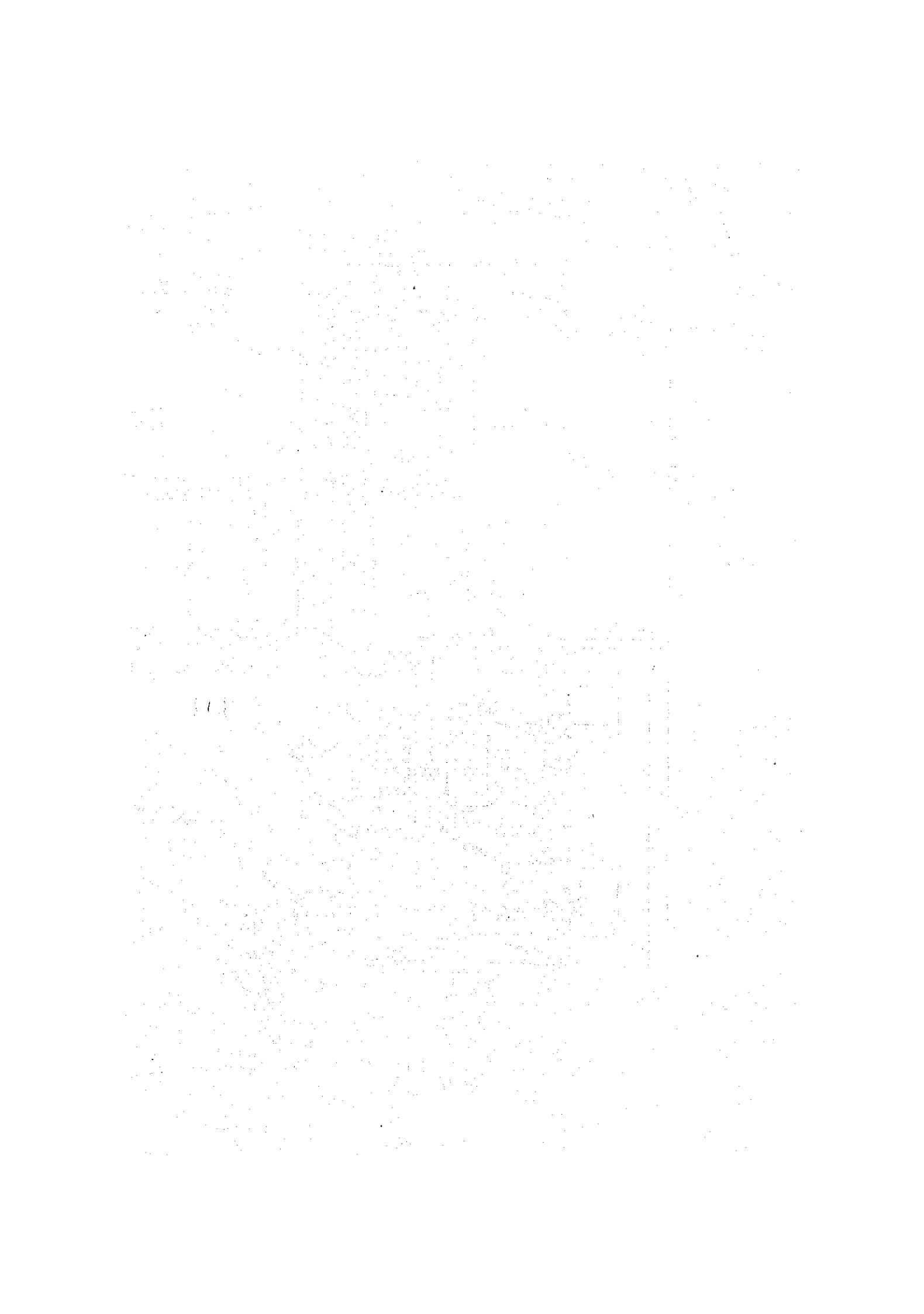
After deliberation on basic needs, urgency and priority for the components of the general plan as well as their required construction cost in comparison with available fund, the components of the Model Infrastructure Improvements Works have been decided as follows :

1. land leveling and land preparation,
2. link road,
3. drainage facilities,
4. irrigation facilities (excluding the Cihideung pump station and its related pipe line except pump machine)
5. soil conservation test fields,
6. paddy irrigation tests fields,
7. upland irrigation tests fields,
8. tractor test field, and
9. tractor test roads.

Accordingly, the following components of the said general plan shall be left behind in further consideration on the self-construction of the Indonesian side :

1. measurement plot (lysimeter)
2. the Cihideung pump station and its related pipe line except pump machine,
3. workshop and workstation, and
4. others, if any.





付属資料 C 9 溼溉用水水収支測定プロット（ライシメーター）

1. Site allocation

The site for the measurement plot has been allocated to the surrounding area by the farm pond in the north, the tractor test field in the east, the link road in the south and the paddy experimental field in the west. The available land is about 17 m in width and 26 m in length.

2. Structure

This is used for study on the water balance at a paddy field. It is made of watertight reinforced concrete with outflow measurement devices for amounts of surface water and percolated water.

The dimensions of the structure are 10 m in width, 15 m in length and 2 m in height. The structural framework consists of reinforced concrete walls and a bottom slab. Two rectangular weirs are provided at the inlet and the outlet canals respectively in order to measure amounts of water coming into and going out from the measurement plot. The percolated water into the soil is collected with perforated PVC pipes installed on the bottom slab and measured it at the outlet box by bulk. While, the inside of the measurement plot is filled with arable soil on filter with adequate thickness of gravel and sand.

3. Design

The rates of irrigation water necessary for the experiments in the measurement plot are the same as the paddy experiment fields. The irrigation water is supplied from the farm pond.

For surface drainage during heavy rainfall concentration, the maximum capacity of the measurement weir was decided with the following criteria:

$$Q = R_5^{100} \cdot A$$

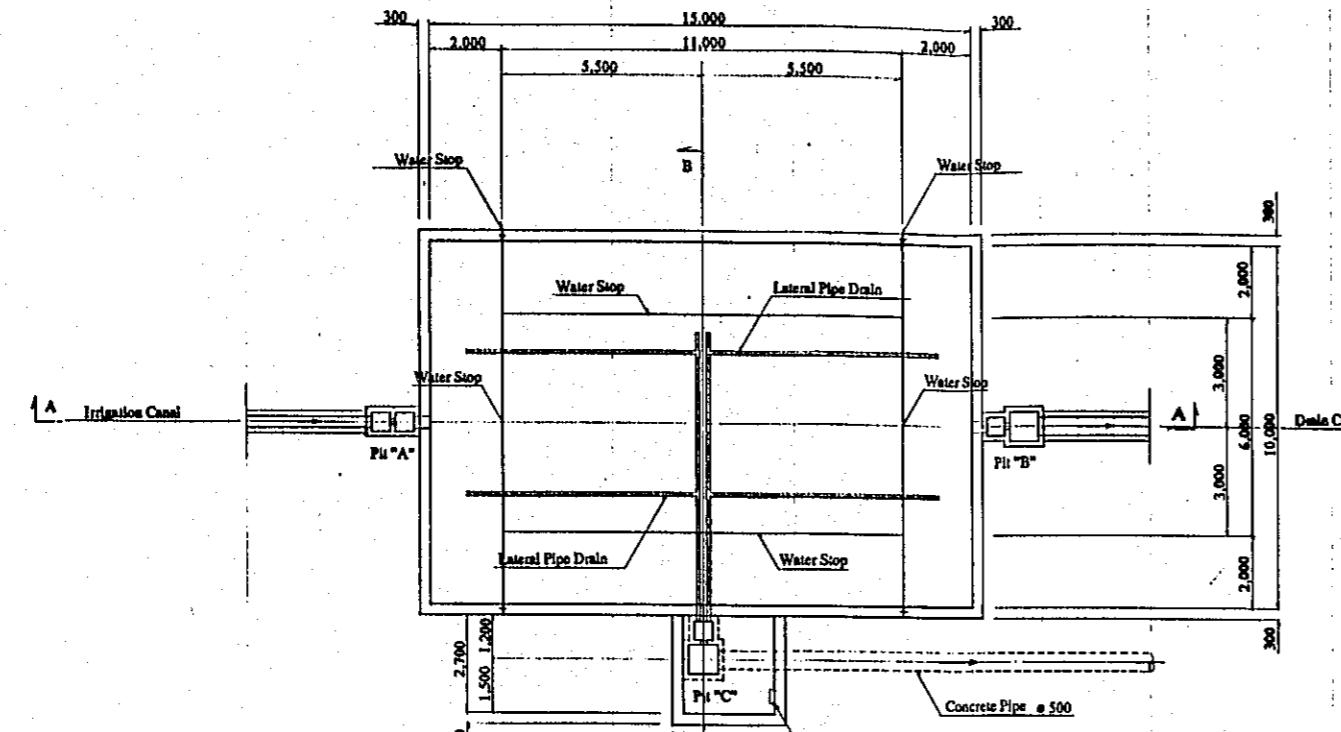
Where ; Q : Design discharge
 R_5^{100} : 5 minutes rainfall intensity of 100 years
return period = 289.3 mm/hr
 A : Catchment area = 150 m²
Therefore ; Q = 289.3 mm/hr x 150 m²
= 0.012 m³/sec

The dimension of the drainage canal of concrete flume is :

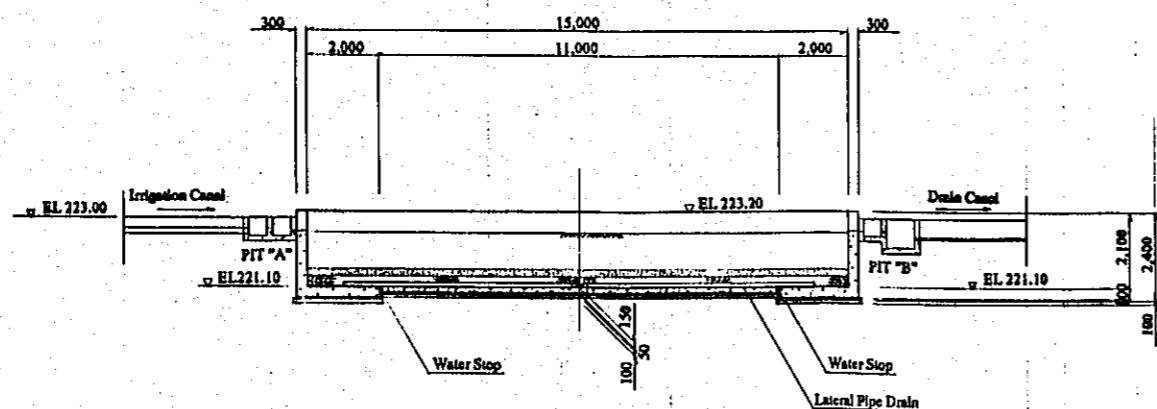
$$Q = 0.012 \text{ m}^3/\text{sec}, \quad \text{Canal width} = 0.5 \text{ m}, \quad \text{Canal slope} = 0.001$$
$$n = 0.015, \quad \text{Water depth} = 0.08 \text{ m}, \quad \text{Canal depth} = 0.3 \text{ m}$$

The structure is designed as shown in Drawing C9-1.

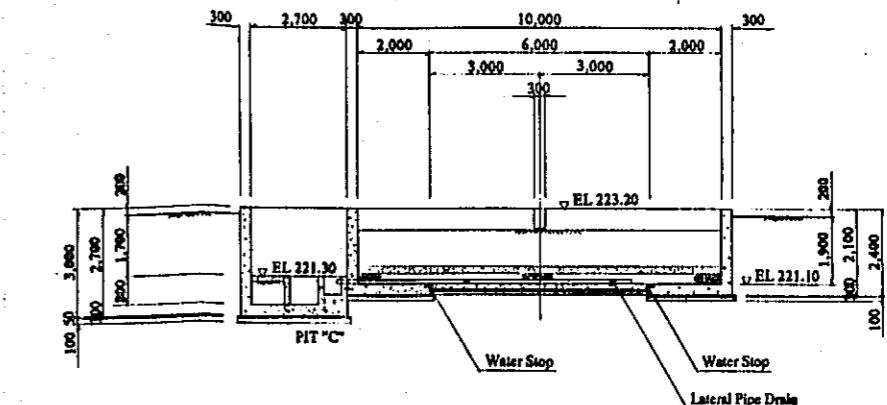
The Cost is estimated at Rp. 28,050,000.



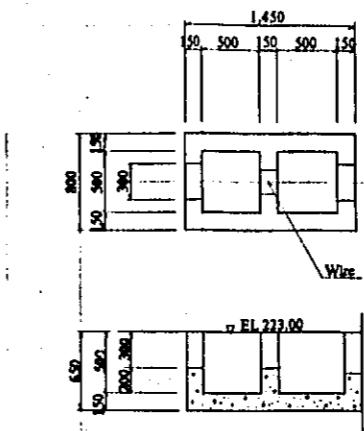
PLA



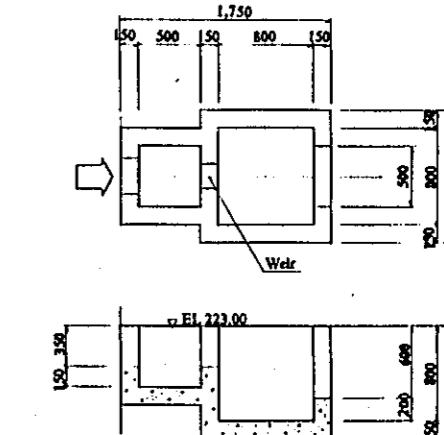
SECTION A -



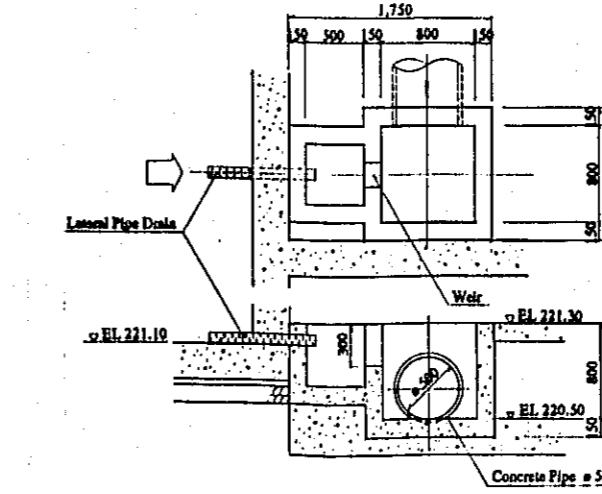
SECTION B.



PT



PIT "B"



TYPICAL SECTION

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INSTITUT PERTANIAN BOGOR

MEASUREMENT PLOT

PREPARED BY

CHECKED BY

DRAWING NO.
C9 - 1

the \mathcal{V} of \mathcal{W} is the set of all $\mathbf{v} \in V$ such that $\mathbf{v} \cdot \mathbf{w} = 0$ for all $\mathbf{w} \in W$. This is equivalent to saying that \mathbf{v} is orthogonal to every vector in W .

Given a subspace W of V , we can find its orthogonal complement \mathcal{V} by taking the set of all vectors in V that are orthogonal to every vector in W . This set is also a subspace of V , and it is called the orthogonal complement of W .

For example, if $V = \mathbb{R}^3$ and $W = \text{span}\{\mathbf{w}_1, \mathbf{w}_2\}$ where $\mathbf{w}_1 = (1, 0, 0)$ and $\mathbf{w}_2 = (0, 1, 0)$, then the orthogonal complement of W is the set of all vectors $\mathbf{v} = (x, y, z)$ such that $\mathbf{v} \cdot \mathbf{w}_1 = 0$ and $\mathbf{v} \cdot \mathbf{w}_2 = 0$. This is the set of all vectors $\mathbf{v} = (x, y, z)$ such that $x = 0$ and $y = 0$, which is the z -axis.

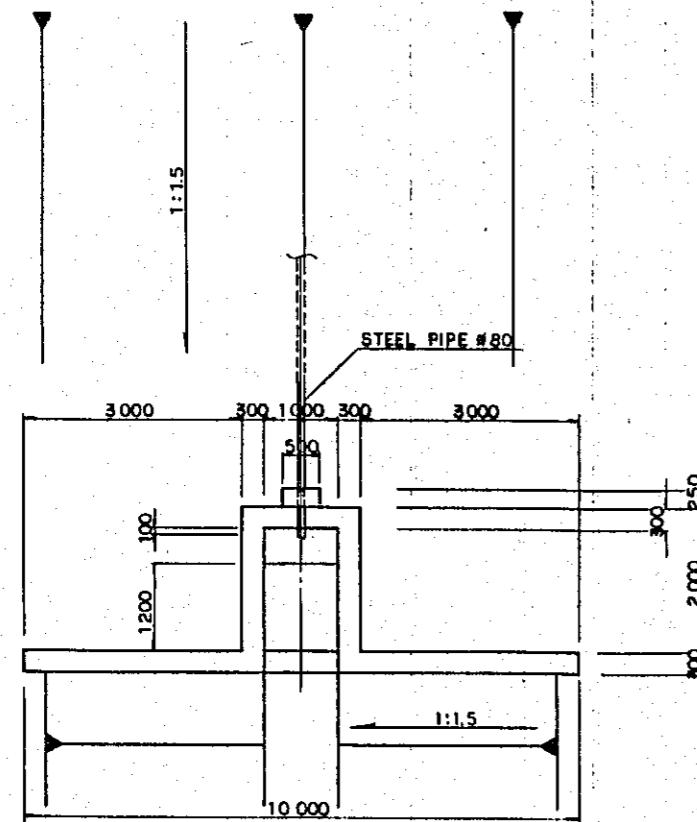
In general, the orthogonal complement of a subspace W of V is a subspace of V that contains all vectors in V that are orthogonal to every vector in W . It is denoted by W^\perp .

付属資料 C 1 0 チイヒ ドゥンポンプ場

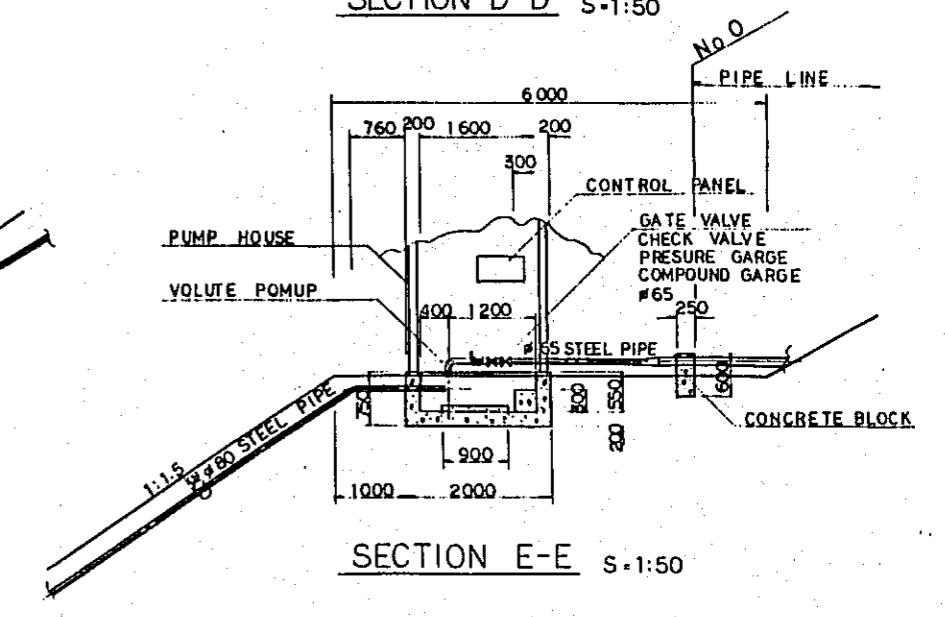
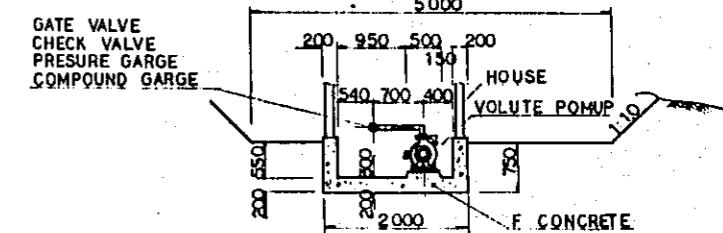
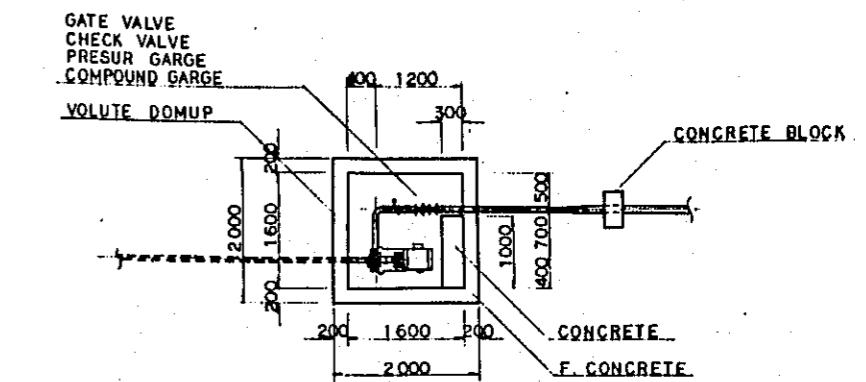
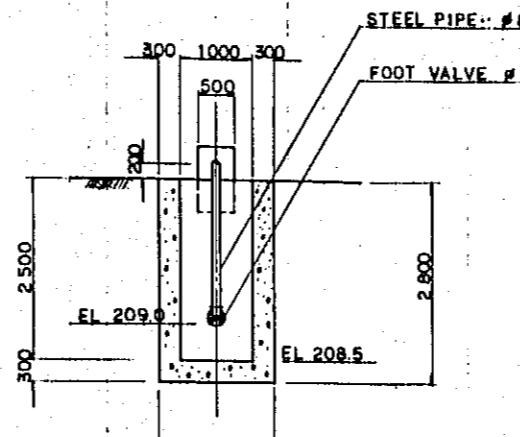
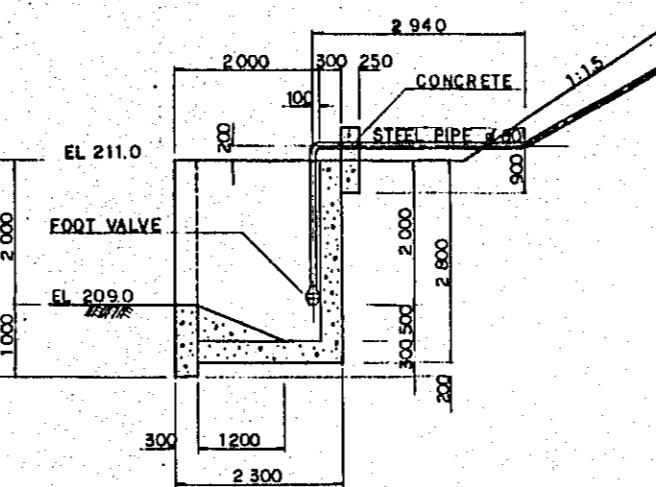
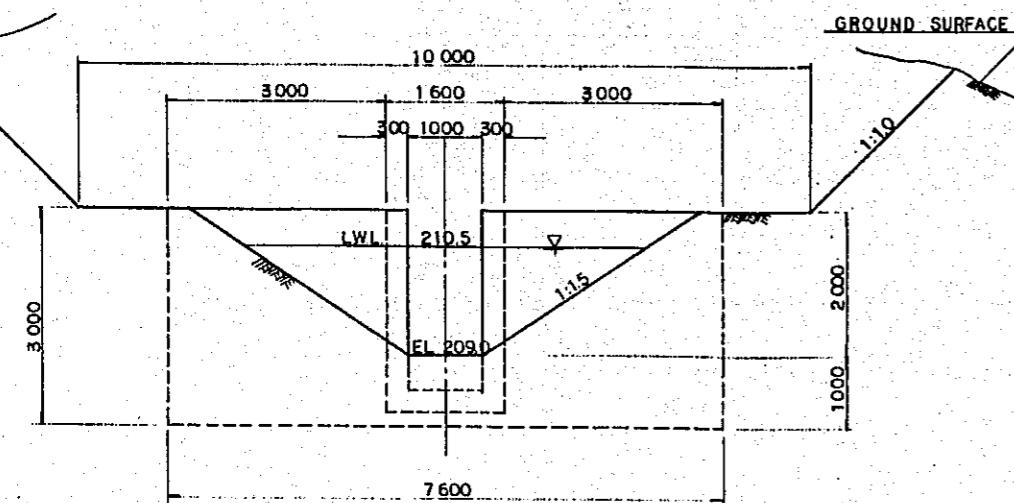
As the result of the water balance calculation the required pump capacity is found at 180 lit/min with 40 mm of pump bore.

The location and the design drawing of the Cihideung pump station and pipe line are shown in Drawing C10-1 and C10-2.

The construction cost is estimated at Rp. 32,831,000 for pump station and Rp. 2,767,000 for pipe line.



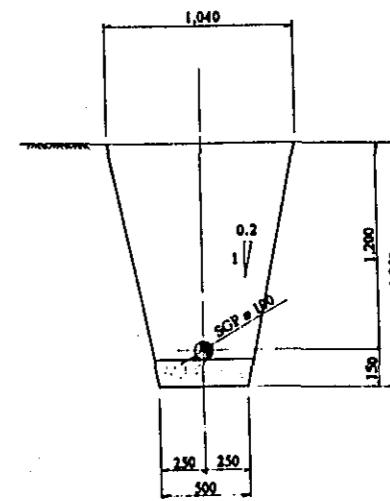
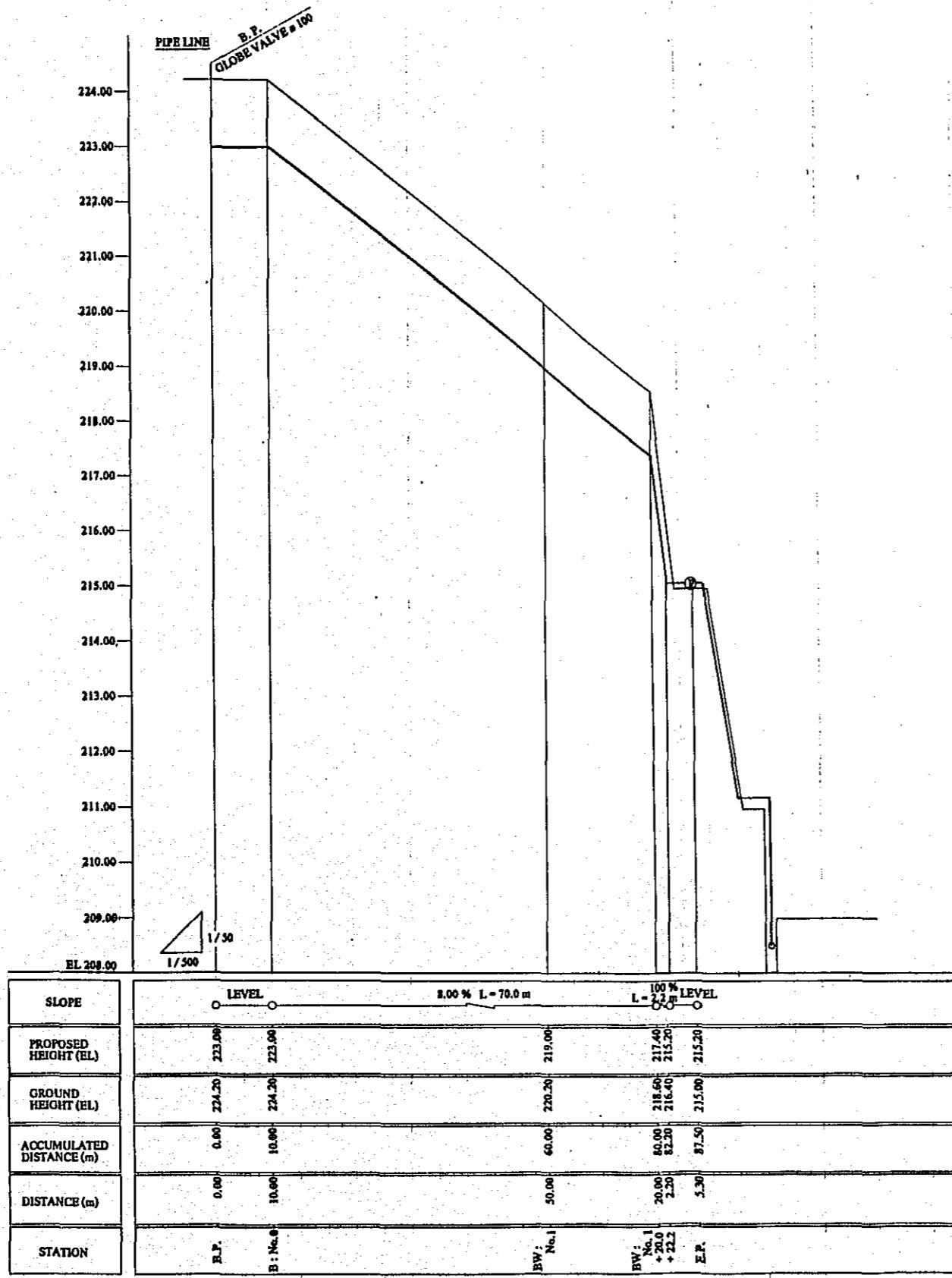
PLAN S-1:50



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The Cibideung Pump Station



TYPICAL SECTION

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INSTITUT PERTHANIAN BOGOR

PIPE LINE

PREPARED BY
CHECKED BY

DRAWING NO.
C10-2

the first time, and the first time I have seen it. It is a very large tree, and has a very large trunk. The bark is rough and textured, and the leaves are large and green. The tree is located in a park, and there are other trees and bushes around it. The sky is clear and blue, and the sun is shining brightly. The overall scene is peaceful and serene.

付属資料 C 1 1 ワークショップ・ワークステーション

The design conditions of the Workshop / Workstation are based on the discussion results during the field survey.

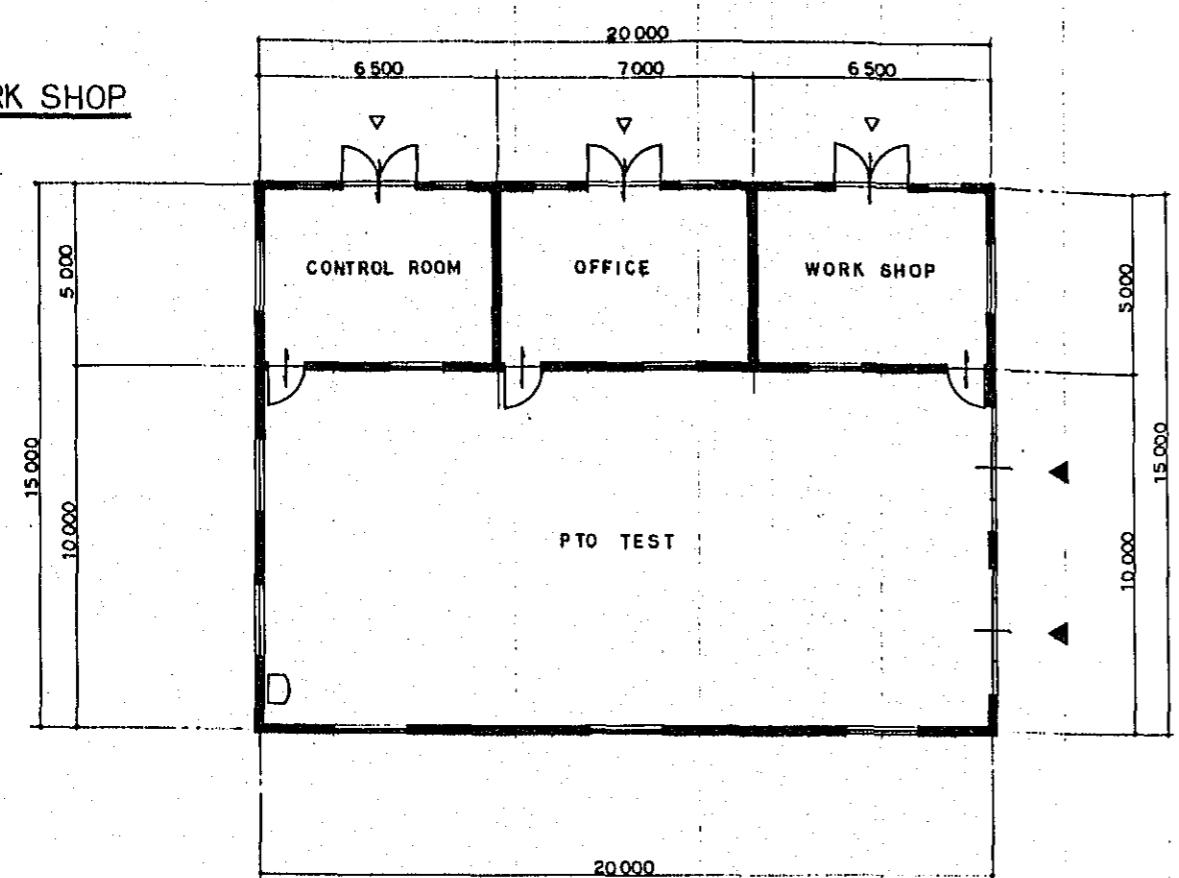
Major elements of the building structures are as follows ;

Floor : concrete
Wall : concrete blocks with cement mortar finishing
Column : reinforced concrete
Roof : cement slate roofing

The design of the Workshop/Workstation is shown in Drawing C11-1.

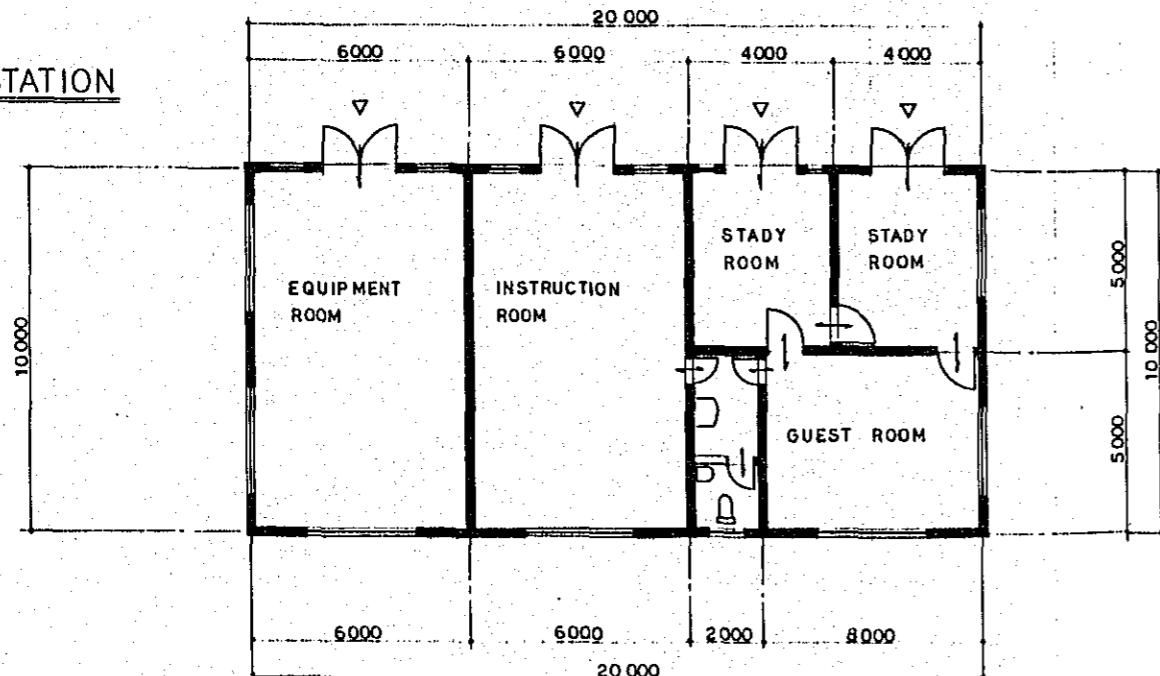
The Construction Cost is estimated at Rp. 138,000,000 in total.

WORK SHOP

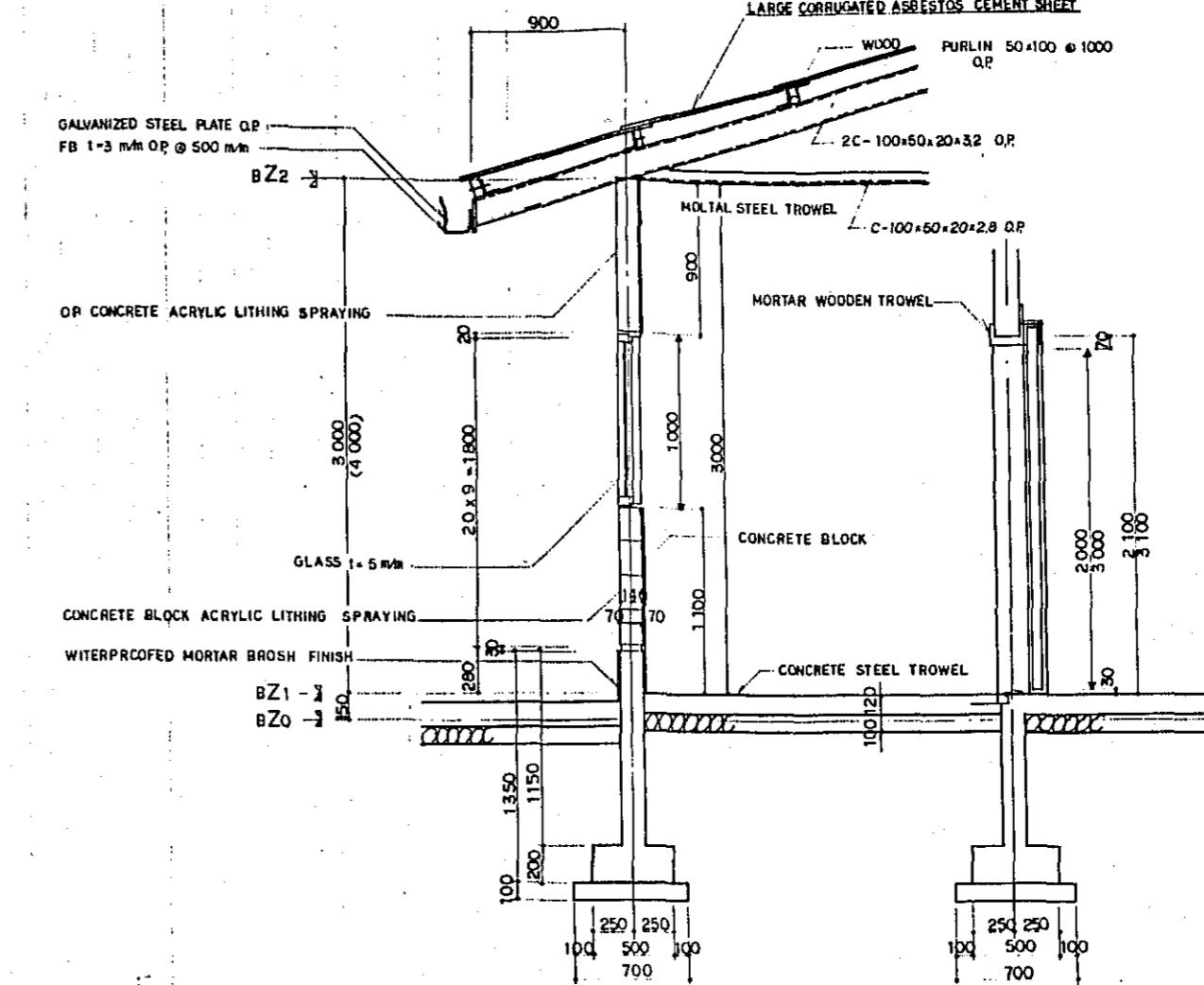


PLAN S=1:100

WORK STATION



PLAN S-1:100



SECTION DETAIL S-1:20

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WORKSHOP AND WORKSTATION

PREPARED BY

DRAWING NO.
C11 - 1

JICA

1

2