DETAILED DESIGN STUDY ON WEST WHARF THERMAL POWER PLANT PROJECT

FINAL REPORT-I

VOLUME 2

JANUARY 1990

JAPAN INTERNATIONAL COOPERATION AGENCY

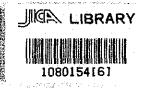
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THE ISLAMIC REPUBLIC OF PAKISTAN

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WEST WHARF THERMAL POWER PLANT PROJECT

DETAILED DESIGN STUDY

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INTRODUCTION

1.1 General

The transmission line between the West Wharf Thermal Power Plant and the Baldia Grid Station has been studied, surveyed and checked, with the decisions planned as follows.

o Between the substation of the West Wharf Thermal Power Station and the site of tower No. 1 of existing 66 kV Baldia line and S.I.T.E. line (1.15 km)

220 kV underground O.F. cable in tunnel

o Between tower No. 1 and tower No. 5 of existing 66 kV line (1 km)

Overhead line of composite towers consists of 2 circuits of 220 kV line and 2 circuits of 132 kV line

o Between tower No. 5 of existing 66 kV line and the Baldia Grid Station (22.9 km)

Overhead line of 2 circuits of 220 kV line

The area where the transmission line will be constructed is situated in a tropical zone exhibiting high temperature, high humidity and extremely low precipitation.

Also, as the area is situated nearby the sea, it has been concluded that the facilities shall be provided with effective measures against corrosion.

1.2 Summary of Design

ITEM	DESCRIPTION			
Nominal voltage	220 kV	132 kV		
Route length	23.8 km	1.0 km		
Number of circuits	2 cct	2 cct		
Supporter	Latice steel tower	Latice steel composite tower		
Conductor	ACSR/AS 330 mm ² x 2	ACSR/AS 680 mm ²		
Ground wire	OPGW 190/90 mm ²	4		
Insulator	Fog type suspension insulator \$254 mm	Fog type suspension insulator \$254 mm		
Suspension string	22 pc./string	14 pc./string		
Tension string	23 pc./string	15 pc./string		
Frequency	50 Hz	50 Hz		

2. TRANSMISSION LINE ROUTE AND TOWER HEIGHT

As a result of the site survey and the discussion with KESC's engineers and concerned authorities relating to the route of 220 kV transmission line, the optimum route was studied and selected taking into account the future extension plan of the transmission system, physical aspects of the tower site conditions, availability of land acquisition, ease of construction and maintenance, and the detour route around the Air Force Base.

The proposed route of the 220 kV transmission line is as shown in DWG. No. WLT-1001.

The limitations of tower heights are divided into three classes, 33 m, 45 m and 66 m so as not to interfere with the taking-off or landing of aircraft. Sections to be applied to each height limitation are as shown in DWG. No. WLT-1001.

3. CONDUCTOR

3.1 Characteristics of Conductor

(1) ACSR/AS 330 mm²

)	ACSK	/AS 330 mm	4 T. C. S. C
	(a)	Composite wire	
	•	Sectional area	379.6 mm ²
		Construction	
		Al	26/4.0 mm
		AS	7/3.1 mm
		Minimum ultimate tensile strength	10,950 kg
		Overall diameter	25.3 mm
		Weight per km	1.239 kg
		DC resistance at 20°C	0.0835 ohm/km
	(b)	Aluminum wire	
		Diameter	4.0 mm
		Minimum tensile strength	16.17 kg/mm ²
		Minimum elongation in 250 mm	1.9%
		Minimum conductivity at 20°C	61%
	(c)	Aluminum-clad steel core wire	
		Diameter	3.1 mm
		Minimum tensile strength	130 kg/mm^2
		Minimum elongation in 250 mm	1.5%
		Minimum conductivity at 20°C	23%
		Minimum stress at 1% extension	110 kg/mm ²
	,	Minimum number of twisting before stranding	20 times

(2) ACSR/AS 680 mm²

(a) Composite wire

(a)	Composite wire	
-	Sectional area	766.8 mm ²
	Construction	
	Al	54/4.0 mm
	AS	7/4.0 mm
	Minimum ultimate tensile strength	20,180 kg
	Overall diameter	36.0 mm
-	Weight per km	2,446 kg
	D.C. resistance at 20°C	0.0408 ohm/km
(b)	Aluminum wire	
	Diameter	4.0 mm
	Minimum tensile strength	16.17 kg/mm ²
	Minimum elongation in 250 mm	1.9%
	Minimum conductivity at 20°C	61%
(c)	Aluminum-clad steel core wire	
	Diameter	4.0 mm
	Minimum tensile strength	130 kg/mm ²
4	Minimum elongation in 250 mm	1.5%
	Minimum conductivity at 20°C	237
	Minimum stress at 17 extension	110 kg/mm ²
	Minimum number of twisting before stranding	20 times

3.2 Current Carrying Capacity

The concept for the conductor is to have enough capacity in continuous operation for full load in one circuit. Consequently,

the capacity is calculated on the basis of a 400 MW load for 220 kV and a 165 MVA load for 132 kV line, and were determined by power flow analysis and KESC instructions.

Required current capacity;

220 kV:
$$I = \frac{P}{\sqrt{3} \text{ V } \cos \phi} = \frac{400 \text{ MW}}{\sqrt{3} \text{ x } 220 \text{ x } 0.85} = 1,235 \text{ (A)}$$

132 kV:
$$I = \frac{P}{\sqrt{3} \text{ V}} = \frac{165 \text{ MVA}}{\sqrt{3} \times 132} = 722 \text{ (A)}$$

According to the calculation results shown in Table 3.1, ACSR/AS 330 mm² has 526A and 655A of capacity at 80°C and 90°C of conductor temperature, respectively, and ACSR/AS 680 mm² has 797A and 1010A of capacity at 80°C and 90°C respectively, with these values deemed to have sufficient current capacity.

Table 3.1 CURRENT CAPACITY

◆ Allowable Current

5.3 mm	Amb. Temp. = 48 deg.	5 m/sec.		
23	.= 4	11	0000	A 68.
	.Temp	٠ ٧	1.0	Ia = 525.89 A
Dia	Amb	¥in	I. K	Ia
mm2		-	.0042	
8.9	deg		ta =1	
320	80	6	52 Be	08700
ond. Name : ACSR/AS 330 mm2Sec.Area = 326.8 mm2 Dia = 2	Temp.=	.Ratio=	=0.9505	0.000
n2Sec.	Max	Rad	×	Hr
330 mm	5 /km	/cm2	35/km	
R/AS	083	≫	0.10	
: ACS	0deg=	tion=	ax.T=	429
Name	3.at 2	Radia	.at ™).0012
nd.	. Res	lar	Res) }

Allowable Current

3 mm	deg.	m/sec.		
25.3	48	ī,	Ö	⋖.
	Amb.Temp.=	11 ·	= 1.00000	= 654.78 A
Dia	Amb.	Wind V.	*	Ia =
3 mm2	deg.		=1.00396	
326.8		6	Beta	107
: ACSR/AS 330 mm2Sec.Area = 326.8	Max Temp.=	Rad. Ratio=	Max.T= 0.1069/km X =0.93555 Beta =1.00396 K	Hr = 0.0009
1/AS 330 mm	.0835 /km	.1 W/cm2	0.1069/km	
Cond. Name : ACSR	DC Res.at 20deg≈	Solar Radiation=	DC Res.at Max.T=	Hw = 0.0012406

• Allowable Current

mm	deg.	m/sec.		
36	48	r.	 1	
	Amb. Temp. =	Wind V. =	= 1.0259	Ia = 797.47
Dia	Amk	¥1.	3 4	E H
678.8 mm2	deg.		=1.01929	
678.	80	σ.	Beta	.00
. ACSR/AS 680 mm2Sec.Area =	Max Temp.=	ation= .1 W/cm2 Rad.Ratio=	X =1.39303 Beta	Hr
1/AS 680 mm	.0408 /km	.1 W/cm2	Max.T= 0.0506/km	
Cond. Name : ACSF	DC Res. at 20deg=	Solar Radiation=	DC Res.at Max.T=	Hw = 0.0010419

Allowable Current

36 mm	deg.	m/sec.		
36	48	r.	2	¥
Dia	Amb. Temp. =	Wind V. =	K = 1.0307	Ia =1010.26 A
678.8 mm2	90 deg.	σ,	ta = 1.018	
: ACSR/AS 680 mm2Sec.Area =	Max Temp.=	Rad.Ratio=	X =1.37109	Hr = 0.0009107
R/AS 680 mm	.0408 /km	.1 W/cm2	ax.T= 0.0522/km	
Cond. Name : ACS	DC Res.at 20deg=	Solar Radiation=	DC Res.at Max.T=	HW = 0.0010400

3.3 Sub-conductor Spacing in Phase

Nominal spacing distance

400 mm

Configuration

Horizontal

The nominal spacing distance of ACSR/AS 330 mm² twin conductor shall be 400 mm based on the following.

- (a) The larger the nominal spacing distance becomes, the smaller the inductance becomes. However, the mode has a tendency of saturation.
- (b) The larger the nominal spacing distance becomes, the larger the capacitance becomes. However, the mode has a tendency of saturation.
- (c) Corona noise level is minimum when the spacing distance is equal to the length of about ten times the conductor diameter. In the range of a spacing distance smaller than the above, it increases sharply, while for larger spacing distance, it increases slowly.
- (d) The smaller the nominal spacing distance is, the greater the effect of wind pressure reduction. However, should the distance be excessively small, both subconductors are prone to be irregularly moved, stuck or distorted due to wind pressure.
- (e) It is not desirable to frequently change the voltage drop of transmission line or corona voltage due to irregular changing of the spacing distance of subconductors and/or wind pressure.

Therefore, the nominal spacing distance shall be selected so that the curve indicating electrical characteristics, such as the relationship between change of inductance and electrostatic capacity, corona voltage and that of nominal spacing distance, is as flat as possible.

(f) In addition to electrical and mechanical characteristics, coordination with the design of insulator strings and stringing work, particularly the design of "vehicle for midair performance" for mounting spacers as well as the weight of workers mounting the vehicle, shall be taken into account in deciding the nominal spacing distance.

Based on the above, the nominal spacing distance shall be 400 mm.

4. GROUND WIRE

4.1 Characteristics of Ground Wire

(1) OPGW 190/90 mm²

Construction 1/5.2 mm OP unit + 7/4.0 mm AS

+ 12/4.47 mm HA1

Overall diameter 22.2 mm

Cross sectional area

Nominal 283.59 mm²

Minimum ultimate tensile

strength 10,500 kg

Weight per km 1,136 kg

DC resistance at 20°C 0.129 ohm/km

Maximum continuous operating temperature 150°C

Maximum one second operating temperature 300°C

System fault current 40,000 A x 1 sec.

(2) Optical cable

Optical fiber type Single mode

Number of optical fiber 5

Optical attenuation at wave length 1.3 µm Max. 0.5 dB/km

(3) Aluminum-clad steel wire

Diameter 4.40 mm

Minimum ultimate tensile strength 116 kg/mm²

Minimum elongation in 250 mm 1.5%

Minimum conductivity at 20°C 20.3%

Minimum stress at 1% extension

Minimum aluminum thickness

125 kg/mm²

0.22 mm

4.2 Temperature of Ground Wire

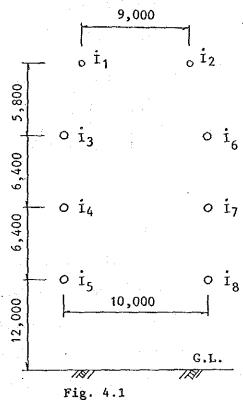
From the viewpoint of the mechanical strength of the ground wire and characteristic of the optical fiber, the temperature of ground wire shall be lower than 150°C under normal operation and lower than 300°C at the time of one line fault of which the duration is not more than one second.

(1) Under normal operation:

Conductor temperature affected
by electro magnetic induced
current shall be lower than

150°C.

Assuming the conductor arrangement is as shown in Fig. 4.1, induced current will be calculated as follows.



Mutual inductance will be as follows.

Mij =
$$\left[2 \log_e \frac{2}{K \text{ dij}} - 0.1544 + \frac{2\sqrt{2}}{3} \text{ K (hi + hj)}\right]$$

- j { $\frac{\pi}{2} - \frac{2\sqrt{2}}{3} \text{ K (hi + hj)} } \times 10^{-4}$ (H/km)

$$K = \sqrt{4\pi\sigma\omega \times 10^{-14}}$$

 $dij = \sqrt{Dij^2 + (hi - hj)^2}$ (cm)

Self inductance will be,

Li = {
$$2 \log_e \frac{2}{Kri} - 0.1544 + \frac{4\sqrt{2}}{3} Khi + \frac{\mu si}{2}$$

- j (
$$\frac{\pi}{2}$$
 - $\frac{4\sqrt{2}}{3}$ Khi) } x 10⁻⁴ (H/km)

Mutual and self impedance will be,

$$Z_{ij} = j\omega M_{ij}$$
 (\Omega/km)

$$Z_{i,j} = r_i + j\omega Li$$
 (Ω/km)

Induced current in the ground wire will be,

Where;

Electric conductivity of earth (m /m)

hi : Conductor height (cm)

Dij: Horizontal distance between conductors (cm)

ri : Equivalent radius of conductor (cm)

μsi: Specific permeability of conductor

Now, assuming that $\sigma = 100 \text{ m V/m}$, $\mu \text{si} = 5 \text{ and the current of}$ each phase is 1200 A, the induced current will be,

$$i_1 = i_2 = -122.4 + j 21.48$$
 (A)

$$\dot{i}_1 = \dot{i}_2 = 124.3$$
 (A)

According to the calculation result given below, the temperature of the OPGW will be lower than 64°C, thereby satisfying the requirements.

Allowable Current

(2) At one line fault

Conductor temperature must be lower than 300°C at the fault of line.

The fault current carrying capacity of overhead ground wires is generally calculated by the following formula.

$$I = n \times \sqrt{\frac{C \cdot \ln (\theta \cdot \alpha + 1)}{\alpha \cdot Ro t}}$$
 (A)

Where,

I : Fault current (A)

 α : Temperature coefficient of resistance $(\Omega/^{\circ}C)$

Ro: Electrical resistance at initial condition (Ω/cm)

t: Duration time (sec.)

C: Heat capacity (J/cm. OC)

O: Temperature rise (OC)

n: Number of ground wires

The temperature rise under the following conditions is obtained as described hereunder.

To = 65°C : Initial conductor temperature

$$\alpha = 0.0038/^{\circ}C$$

$$C = 7.72 \text{ J/cm}^{\circ}C$$

t = 1.0 sec.

Ro = 0.129 x
$$10^{-5}$$
 x { 1 + 0.0038 (65 - 20)} = 0.151 x 10^{-5} (Ω/cm)

$$\left(\frac{1}{n}\right)^{2} \times \alpha \times \text{Roxt}$$

$$X = \frac{1}{n}$$

$$= \frac{20,000^2 \times 0.0038 \times 0.151 \times 10^{-5} \times 1}{7.72} = 0.297$$

$$\Theta = \frac{e^{X} - 1}{\alpha} = \frac{e^{0.297} - 1}{0.0038} = 91^{\circ}C$$

Therefore, the temperature of the ground wire will be,

$$Tc = To + \Theta = 65 + 91 = 156 < 300^{\circ}C$$

5. INSULATOR STRING

5.1 Number of Insulator Discs per String

Insulator disks shall be 254 mm diameter fog type suspension insulators.

Insulator string	220 kV	132 kV
Suspension insulator string	22 discs	14 discs
Tension insulator string	23 discs	15 discs

The reason why the tension string has one more disc than the suspension string is that the increase in the length of string has little effect on the tower height. Also, from the viewpoint of maintenance, it is more difficult to exchange an insulator disc on a tension string than on a suspension string.

The number of insulator discs shall be designed so that no flashover against switching surge impulse occurs. The design shall also take into consideration the effects of salt contamination. The required number of discs for switching surge shall be 11 and 7 discs for 220 kV and 132 kV lines, respectively. Minimum flashover voltage under contamination on 254 mm normal suspension insulator disc shall be calculated by using the following formula.

$$Vt = \frac{28 \text{ k}}{(\frac{\omega}{0.1})^{1/5} \{1.5(K^{1/3} + 2) + \frac{5}{8} K\}}$$
 (kV)

Vt: Minimum flashover voltage of 254 mm normal suspension insulator disc (kV)

w: Salt deposit density on outer surface in lower face of

disc (mg/cm²)

K: Soil deposit density = 0.1 (mg/cm^2)

k : Correction factor

k = 1.15 for effective ground system

k = 1.25 for non-effective ground system

As the transmission line route is located in a coastal area, it is predicted that salt contamination will be considerably heavy. Therefore, assuming the salt deposit density as 0.5 mg/cm², minimum flashover voltage shall be calculated as 6.2 kV and 6.7 kV for 220 kV and 132 kV, respectively. For fog type insulator, it shall be multiplied by 1.3 to become 8.0 kV and 8.7 kV.

Required withstand voltage shall be,

$$V = V_n \times \frac{1.15}{1.1} \times \frac{1}{\sqrt{3}} q$$

Vn: Nominal voltage (kV)

q: Voltage build-up rate at fault

q = 1.3 for effective ground system

 $q = \sqrt{3}$ for non-effective ground system

220 kV line:

$$V = 220 \times \frac{1.15}{1.1} \times \frac{1.3}{\sqrt{3}} = 173$$
 (kV)

Required number of discs: $N = \frac{173}{8.0} = 21.6$ 22

132 kV line:

$$V = 132 \times \frac{1.15}{1.1} \times \frac{\sqrt{3}}{\sqrt{3}} = 138$$
 (kV)

The existing 132 kV line has only 12 discs per string. Also, considering that the longer the insulator string becomes, the higher the tower height, 14 discs will be adopted for the proposed 132 kV line, so as to handle the density of 0.3 mg/cm² of salt deposit.

5.2 Arcing Horn

There are three main purposes of the arcing horn. One is to avoid flashover on the surface of insulator discs by containing it between horns when lightning surge impulse occurs. Another is to shift the surface arc to the horn at the time insulators become contaminated so as to minimize damage to insulator discs. The other is to restrain corona discharge from insulator discs and/or hardware.

It is understood that the probability of occurrence of lightning surge is negligible in the proposed area. Also, as the insulator strings will be considerably long in view of salt contamination, it is not a practical technique to make discharge between the horns, as this requires extending their length.

Consequently, it is advantageous to allow the flashover to occur at the tower body in the rare case of a lightning attack. Moreover, the horns shall be designed to lighten the share voltage of discs located at the charged end as well as countermeasures against surface arc.

6. INSULATION CLEARANCE

(1) Standard insulation clearance

The standard insulation clearance will be 10% larger than the arcing horn gap so as to allow flashover between horns. However, in the case of this project, as flashover will be allowed to discharge to the tower body, the clearance shall be determined by taking into account the horn gap in normal cases and BIL, or Basic Insulation Level, of the substation.

Consequently, 1,600 mm for the 220 kV line and 1,050 mm for 132 kV line will be appropriate.

(2) Minimum insulation clearance

This clearance shall withstand the switching surge immpulse.

For 220 kV:

Maximum circuit voltage

$$220 \times \frac{1.2}{1.1} = 240 \text{ (kV)}$$

Switching surge voltage

240 x
$$\frac{\sqrt{2}}{\sqrt{3}}$$
 x 2.8 = 549 (kV)

- $\sqrt{2}$: Ratio of absolute value of sine wave to crest value
- $\sqrt{3}$: Voltage ratio of phase-to-ground to phase-to-
- 2.8 : Multiple factor of switching surge

Minimum clearance (bar gap)

$$549 \times 1.2 = 658 \text{ (kV)} \rightarrow 1,400 \text{ mm}$$

1.2: Deterioration factor of insulation by ground level and others

For 132 kV:

Maximum circuit voltage

132 x
$$\frac{1.2}{1.1}$$
 = 144 (kV)

Switching surge voltage

144 x
$$\frac{\sqrt{2}}{\sqrt{3}}$$
 x 3.3 = 388 (kV)

3.3: Multiple factor of switching surge
Minimum clearance (bar gap)

$$388 \times 1.2 = 466 \text{ (kV)} \rightarrow 900 \text{ mm}$$

(3) Clearance diagram

		* .	•	unit: m
	Description	220 kV	132 kV	Remarks
A	Standard clearance	1,600	1,050	
D	Minimum clearance	1,400	900	
Cs	Normal clearance for suspension tower	2,000	1,680	Cs = A+K+B
Сj	Normal clearance for tension tower	1,650	1,100	Cj = A+K
E	Abnormal clearance	1,550	1,070	E = D+L
J	Depth of jumper	3,000	2,000	
K	Consideration for tension member of cross arm	50	50	
В	Consideration for angle of catenary	350	580	Note 1
L	Consideration for step bolt and post member	150	170	

Note 1:

220 kV: 1,000 x tan 15° + 1,600 (sec 15° - 1) = 324 350 mm

132 kV: 2,000 x tan 15° + 1,050 (sec 15° - 1) = 573 580 mm

Where; 1,000, 2,000: Distance between hanging members of

cross arm

15°: Angle of catenary of conductor

7. TOWER DESIGN

7.1 Design Conception

(1) Standard

Tower design, in principle, shall be in accordance with JEC - 127 (1965), or equivalent.

(2) Conductor

Twin conductor of ACSR/AS 330 mm² for 220 kV line and single conductor of ACSR/AS 680 mm² for 132 kV line shall be applied.

Maximum tension of conductors shall be 4,000 kg for ACSR/AS

330 mm² and 6,000 kg for ACSR/AS 680 mm².

(3) Ground wire

Two OPGW 190/90 mm² with 3,800 kg maximum tension shall be applied. Shield angle shall be less than 30°.

(4) Unbalance tension on tower

(a) Normal condition

- o Suspension and angle towers

 No unbalance tension will be applied.
- o Dead-end towers

 Full tension of all conductors and ground wire in the same span shall be applied.
- o Section towers

One-third of maximum tension of all conductors and ground wire in the same span shall be applied.

(b) Abnormal condition

Unbalance tension and torsional force caused by breakage of any one conductor or two conductors in one phase in case of bundle conductors or ground wire shall be added to the normal condition.

Unbalance tension on suspension tower may be decreased but shall not be lower than 60% of assumed tension of conductor. This deduction shall not be applied on ground wire.

(5) Safety factor

Safety factor shall be more than 1.8 for normal condition and more than 1.2 for abnormal condition based on yield strength or buckling strength.

(6) Standard span

Standard span shall be 400 m. The standard span has been decided based on the following study.

- (a) Type, size and number of conductor
- (b) Type and construction of supporter
- (c) Topographic and climatic conditions in the area along the transmission line route
- (d) Applicable standards for safety based on those applied in Japan

Generally, the standard span of supporter is decided by carrying out a comparative study on the estimated total

construction cost after designing several types of towers corresponding to their span. The spans considered to be justifiable are based on the experience of the consultant in the past. These spans are as follows.

Type of supporters	Standard span (m)
Wooden pole	75 - 120
Steel pole	150 - 200
Steel tower for transmission line of up to 77 kV	200 - 300
Steel tower for 154 kV line	250 - 350
Steel tower for 275 kV line	300 - 400
Steel tower for 500 kV line	350 - 450

(7) Wind pressure

On tower:

Tower	height	less	than	40	m	280	kg/m ²
Tower	height	less	than	50	m	300	kg/m ²
Tower	height	less	than	60	m .	320	kg/m^2
Tower	height	less	than	70	m	340	kg/m^2
Tower	height	less	than	80	m	360	kg/m^2
Tower	height	less	than	90	m	380	kg/m ²
Tower	height	less	than	10	Q m	400	kg/m^2

On conductor:

•	Single conductor Twin conductor	kg/m ²
On ir	asulator string:	kg/m ²

(Wind velocity v = 136 km/h = 37.8 m/sec.)

$$P = \frac{1}{2} \rho CV^2$$

- $= 0.5 \times 0.125 \times C \times 37.8^2 \text{ (kg/m}^2)$
- q: air density (kg.sec²/m⁴)
- C: Coefficient of air resistance
 - C = 1.0 for single conductor
 - C = 0.9 for twin conductor
 - C = 1.4 for insulator string

(8) Sag calculation

Ambient temperature Max. 48°C

Min. 0°C

Conductor temperature Max. 80°C

In no case shall ice on the conductor be considered. EDS condition shall be 25°C temperature with no wind.

Results of calculation are as shown in the attached Tables 7.1, 7.2 and 7.3.

Table 7.1 *** SAG CALCULATION ***

CONDUCTOR WEIGHT	: ACSR/AS 3 = 1.239 (= 7450 (K	30 mm2 kg/m) g/sq.mm)	•	CROSS S.4 DIAMETER EXPANSION	AREA = 379 = 25 N M. = .00	9.64 (sq.mm .3 (mm) 000203 (/deg	(S)	
BASE TENSION	N = 4000	(kg)	**					
SPAN (m)	N TEMP) (deg.C)	WIND P. (kg/sq.m)	ICE (mm)	GRAV.	RES.WT. (Kg/m)	HOR.TENS. (Kg)	SAG (m)	
H. TEMP.	. 0	81.00	O					
H	0	1.0	0	0.0			÷	
0		0	0	•	. 23	401.4	. 42	
ശ	0	0.	0	٠	. 23	539.2	. 28	
0		0	0		. 23	642.2	. 48	
IJ	0	٥.	0	*	. 23	720.3	1.02	
\circ	0	۰.	0	٠	. 23	780.3	3.91	
ഥ		0	0	•	. 23	827.1	7.16	
\circ	8	0	0	•	ŝ	854.0	0.77	
ĽΩ	0	٥.	0	•	. 23	893.4	4.74	
09	08 00	0.00	0	0.0	1.239	1917.31	29.080	
រ	0	0	0	•	. 23	936.8	3.78	
0	0	۰.	0	•	ന	952.9	8.85	
ıΩ	0	٠.	O	٠	.23	966.3	4.30	
\circ	0	0	0	•	. 23	977.6	0.12	
R.	0	ි,	0	•	ŝ	987.2	6.30	
O	0	0	0		က	995.4	2.86	
\circ	0	0	0	•	ŝ	374.7	0.43	
Ç	0	0	0	•	വ	138.1	1.59	
40	0 55	0	0	0.0	ധ	921.7	2.89	

SAG CALCULATION *** * * * Table 7.2

CSR/AS 680 2.446 (kg/ 7250 (kg/s	0 8 / 8	mm2 m) q·mm)		CROSS S.A DIAMETER EXPANSION	REA = 76 = 36 M. = .0	6.79 (sq.mm) (mm) 000207 (/deg.	m> g.C)	
TENSION .) 0009 =	(kg)						
SPAN (m)	TEMP (deg.C)	WIND P. (kg/sq.m)	ICE (mm)	GRAV.	RES.WT. (kg/m)	HOR.TENS. (kg)	SAG (m)	×
	0	0.	0	•				
	0	00.06	0	0.0				
200	80	0.00	0	•	.44	375.5	. 1 <u>4</u>	52
50	80	00.0	0	0.0	2.446	2635.60	7.250	47
00	80	`+	0	٠	.44	829.4	.72	44
50	80	00.0	0	•	.44	975.7	2.58	42
00	80		0	•	. 44	087.5	5.84	40
20	80		0	٠	. 44	174.1	9.50	ಚ
00	80	•	0	•	.44	242.2	3.57	38
50	80		0	•	.44	296.4	.05	38
00	80	•	0	•	. 44	340.0	2.95	37
50	ω	•	; •	•	, 44	375.6	8.26	37
.00	80	•	0	٠	. 44	404.9	4.00	36
20	80		0	•	. 44	429.4	0.15	36
00	80	•	0	•	.44	449.9	6.72	36
50	08	٠	0	•	. 44	467.2	3.71	36
00	80	•	0	•	. 44	482.0	1.12	36
00	0	*	0	•	.44	866.3	2.65	32
00	25	٠	0	•	•	568.5	3.70	ວ ໝ
00	ເກ ນາ	•	0	•	. 44	282.5	4.90	38
			-					

Table 7.3 *** SAG CALCULATION ***

6		SAG (m)		0.405		. 97	3.423	.33	.33	.69	. 47	3.64	7.20	21.160	5.49
.59 (sq.mm) 2 (mm) 00176 (/deg.C)		HOR.TENS. (kg)		510.0	200.5	870.5	592.9	393.9	393.9	260.0	169.8	2107.42	062.8	2030.04	2005.24
REA = 283 = 22: M. = .00		RES.WT. (kg/m)		1.136	1.136	1.136	1.136	1.136	1.136	. 13	. 13	1.136	1.136	1.136	1.136
CROSS S.A DIAMETER EXPANSION		GRAV.	0.0	0.0					•	•		0.0	٠	0.0	•
•	•	ICE (mm)	00	0	0	0	0	0	0	0	0	0	0	0	0
/90 (kg/m) kg/sq.mm) (kg)	(kg)	WIND P. (Kg/sq.m)	90.00	0.00	00.0	0.00	0.00	0.00	00.0	0.00	00.0	0.00	0.00	0.00	00.0
OPGW 190/90 1.136 (kg/m 9400 (kg/sq	3800	TEMP (deg.C)	0.0	0	0	0	0	0	0	0	0	0	0	0	0
CONDUCTOR : 0 WEIGHT = ELASTIC M. =	BASE TENSION =	SPAN (m)	TEMF.	100	150	200	250	300	300	350	400	450	200	550	009
S돌림	BA		Ξij												

×

(9) Distance between conductors

- (a) 220 kV line
 - (i) Experienced distance Horizontal distance:

$$C_h = 1.5 \times \frac{220}{1.1 \times 25} = 9.5$$
 (m)

Vertical distance:

$$C_{v} = 1.0 + \frac{220}{1.1 \times 45} = 5.4$$
 (m)

(ii) Transverse swing by wind

$$C_{h} \ge (D-\epsilon) \frac{Sm - S}{Sm} + 2 (d+L) \sin\Theta + \epsilon + 2r$$

=
$$(4 - 0.84) \frac{600 - 400}{600} + 2 (12.9 + 4.3) \sin 12.17^{\circ}$$

$$+ 0.84 + (0.4 + 0.0253) = 9.6$$
 (m)

$$\Theta = \tan^{-1} \frac{Ww}{Wc} = \tan^{-1} \frac{10.6 \times 25.3 \times 10^{-3}}{1.239} = 12.17^{\circ}$$

where;

D: distance between busbars of outdoor substation (m)

ε: power-frequency flashover distance (m)

Sm: maximum span length (m)

S: applied span length (m)

d: sag at 55°C (m)

L: insulator string length (m)

Θ: swinged angle of conductor (deg.)

r: radius of conductor (m)

Wc: weight of conductor (kg/m)

Ww: wind pressure on conductor at wind velocity of 13 m/sec. (kg/m)

(iii) Statistical method

Generally, the swing of conductors will not be simultaneous at all instances. The probability of conductor being staid within the standard deviation (σ) from the mean swing angle ($\bar{\theta}$) is 68.26% and within 2σ is 95.44%. Taking into account to close conductors with 2σ , the required distance between conductors should be more than 6.2 m horizontally according to the following formula. Refer to Fig. 7.1.

$$\sigma = \frac{43.5h \cdot p \sqrt{\nu} \cdot d \cdot s}{\sqrt{\beta \gamma} \cdot (\sqrt{\frac{\gamma}{\alpha}}) \frac{5}{6}}$$

$$\alpha = \frac{w}{g} \cdot \frac{8 d^2 s}{15}$$

$$\beta = a\overline{v} (1 + \cos^2 \overline{\Theta}) \frac{8 d^2s}{15}$$

$$\gamma = (a\overline{v}^{-2}\sin\overline{\Theta} + w\cos\overline{\Theta}) \frac{2}{3} d s$$

$$\nu = \frac{1}{15kS} - \frac{2}{3(kS)^3} + \frac{2}{(kS)^4} - \frac{8}{(kS)^6}$$

$$+\frac{2e^{-ks}}{(KS)^4}(1+\frac{2}{KS})^2$$

$$k = ko \frac{\omega}{\sqrt{3}}$$

$$ko = 0.335$$

$$\omega = \sqrt{\frac{\gamma}{\alpha}}$$

where;

 $h : \cos \overline{\Theta}$

d : sag (m)

S : span (m)

 \bar{p} : wind pressure on conductor (kg/m) = a_{ν}^{-2}

w : weight of conductor (kg/m)

g : gravitational acceleration 9.8 m/sec.²

(iv) Conclusion

Horizontal distance: more than 9.6 m

Vertical distance: more than 5.4 m

- (b) 132 kV line
 - (i) Experienced distance

Horizontal distance:

$$C_h = 1.5 + \frac{132}{1.1 \times 25} = 6.3 \text{ (m)}$$

Vertical distance:

$$C_{\rm v} = 1.0 + \frac{132}{1.1 \times 45} = 3.7 \text{ (m)}$$

(ii) Transverse swing by wind

$$C_h \ge (3 - 0.504) \frac{550 - 400}{550} + 2 (14.9 + 3) \sin 8.84^{\circ}$$

$$+ 0.504 + 0.036 = 6.72$$
 (m)

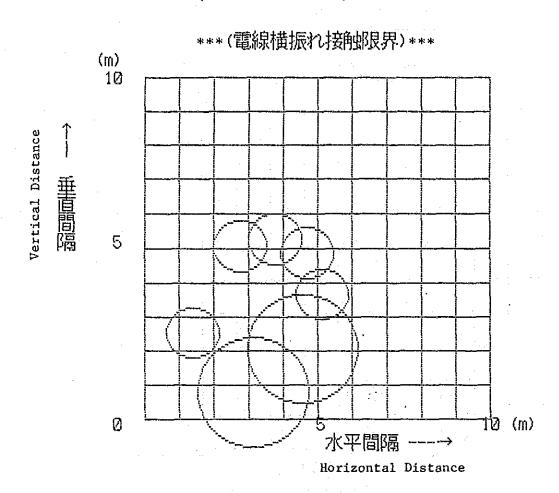
(iii) Statistical method

Refer to Fig. 7.2

(iv) Conclusion

Horizontal distance: more than 6.8 m

Fig. 7.1 CONDUCTOR SWING BY WIND (STATISTICAL METHOD)

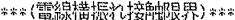


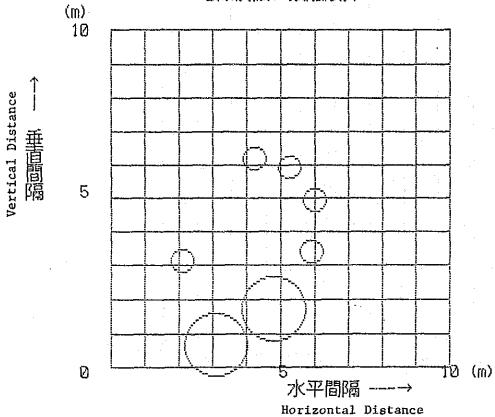
Conductor	電 線 (Tmax)	ACSR/AS 330 * 2 4000 (kg)
Voltage Required Clearance	電 圧 所要離隔	220 (KV) V≤20m/sec 1612.65 mm V>20m/sec 752.65 mm
Applied Span Ruling Span	径 間 等 価 径 間	450 (m) 400 (m)

Wind Conductor Verocity Temperature	Loading Factor	Sag	Tension	Swinged Angle	St andard Deviation
風速 電線温度 (m/s) (°C) 15.0 55.0 20.0 55.0 25.0 55.0 30.0 55.0	負荷係数 1.0000 1.0000 1.0000 1.0000	弛度 (m) 16.32 16.32 16.32 16.32	張力 (kg) 1922 1922 1922 1922	横振れ角 θ(°) 14.5 24.7 35.7 46.0 54.6	標準偏差 σ (°) 2.2 3.5 4.4 4.7 4.5
35.0 55.0 40.0 55.0	1.0000	16.32	1922	61.4	4.0

Fig. 7.2 CONDUCTOR SWING BY WIND

(STATISTICAL METHOD)





Conductor	電線	ACSR/AS 680 * 1
	(Tmax)	6000 (kg)
Voltage	電 圧	132 (KV)
Required Clearance	所要離隔	V ≦ 20m/sec 918 mm
Clearance	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	V > 20m/sec 348 mm
Applied Span	径 間	450 (m)
Ruling Span	等価径間	400 (m)

Wind Verocity	Conductor Temperature	Loading Factor	Sag	Tension	Swinged Angle	Standard Deviation
風 速	電線温度	負荷係数	弛 度	張力	横振れ角	標準偏差
(m/s)	(°C)		(m)	(kg)	θ (°)	σ (°)
15.0	55.0	1.0000	18.86	3283	11.7	2.1
20.0	55.0	1.0000	18.86	3283	20.2	3.4
25.0	55.0	1.0000	18.86	3283	29.9	4.5
30.0	55.0	1.0000	18.86	3283	39.6	5.1
35.0	55.0	1.0000	18.86	3283	48.4	5.2
40.0	55.0	1.0000	18.86	3283	55.8	4.9

Vertical distance: more than 3.7 m

(c) Vertical distance between 220 kV line and 132 kV line

		Uni	it: m
A	В	C	D
2.9	3.0	3.0	3.8
2.0	1.65	1.65	1.65
1.8	1.8	1.8	1.8
0.5	0.5	0.5	0.5
7.2	6.95	6.95	7.75
	2.9 2.0 1.8 0.5	2.9 3.0 2.0 1.65 1.8 1.8 0.5 0.5	2.9 3.0 3.0 2.0 1.65 1.65 1.8 1.8 1.8 0.5 0.5 0.5

(10) Tower type

Туре	Circuit number	Deviation angle	Wind span	Weight span
AS	2	3°	250 m	300 m
A	2	- 3 ^o	400	500
AL	2	30	500	550
В	2	15 ⁰	300	300
С	2	35 ⁰	350	400
D	2	0°,60°	300	300
DR	2	90 ⁰	300	350
A4	4	3 ⁰	350	400
D4	4	00	250	300
DR4	4	75 ⁰	350	350

Configurations of each tower type are as shown in DWG. NOS. WLT-1101 to WLT-1103, and the clearance diagrams are as shown in DWG. NOS. WLT-1151 to WLT-1153.

(11) Clearance from land or obstacles Minimum clearance (m) 132 kV Particulars 220 kV 7.75 7.75 Normal ground, open and agricultural land 9.20 9.20 Main road 4.00 3.20 Trees 12.00 . 12.00 Railway 6.00 4.50 Residential building 3.20 4.00 Telecommunication line Shield wire of power line 4.00 3.20 4.00 3.20 Iron bridges, etc. 15.00 15.00 Highest water level of large river

(12) Accessories

(a) Spacer

The spacer for the bundle conductor shall be fitted in the mid-span and in the jumper connections.

(b) Vibration damper

The vibration damper shall be double torsional damper having the following weight.

ACSR/AS 330 mm² 14 lb ACSR/AS 680 mm² 18 lb OPGW 190/90 mm² 12 lb

(c) Armor rod

The preformed armor rod shall be fitted in suspension strings.

(d) Connection of conductor

Dead-end clamp and mid-span joint sleeves shall be of the

compression type.

7.2 Cable Connection Point

Due to space limitation at the site of tower No. 1, connection of the overhead lines to the underground cables shall be made at every circuit aligned in series, and shall be as shown in DWG. NO. WLT-1104, DWG. NO. WLT-1105 and DWG. NO. WLT-1106. Cables shall be laid in the tunnel to be constructed for extending the cable tunnel from the W.W. P.P. along the centerline of tower No. 1 and the gantries.

7.3 Preliminary Tower Design

(1) General

The tower design presented herein aims at obtaining a general idea of the tower weight, reaction force for its foundation, and estimation of the budget of the project. Design is based on DWG. No. TLT-01 to WDG. No. TLT-09. Design results given in this report are considered to be highly adequate in spite of some design conditions which are slightly different from those of actual towers.

(2) Design Condition

Tower designs presented hereunder are in accordance with JEC-127 (1965), except where otherwise stipulated.

(a) Tower type

	and the second s		A Company of the Comp	
Tower type	Circuit number	Deviation angle	Wind span	Coefficient of vertical load
AS	2	3 ⁰	250	0.03
A	2	30	400	0.05
AL	2	3 ⁰	500	0.03
B	2	15 ⁰	300	0.03
С	2	35 ⁰	350	0.03
D	2	60 ⁰	300	0.03
DR	2	900	300	0.03
A4	4	30	350	0.03
D4	4	60 ⁰	250	0.03
DR4	4	75 ⁰	350	0.03

(b) Conductor

	Name	Max. tension kg	Weight kg/m	Diameter mm
	OPGW 190/90	3,800	1.136	22.2
	ACSR/AS 330	4,000	1.239	25.30
	ACSR/AS 680	6,000	2.446	36.00
(c)	Insulator string			

Insulator strings are as shown in DWG. No. WLT-1201 to DWG. No. WLT-1209. Insulator disks are as shown in DWG. No. WLT-1210.

220 kV suspension string

Weight : $7.3 \times 22 \times 2 + 78 = 399.2 \quad 400 \text{ kg/support}$

Wind pressure: $(0.027 \times 22 \times 2 + 0.33) \times 126 = 191.3$

200 kg/support

220 kV double tension string

: $7.3 \times 23 \times 2 \times 2 + 116 = 787.6$ 790 kg/support Weight

Wind pressure: $\{0.027 \times 23 \times (1+0.3) \times 2 + 0.47\} \times 126 = 262.7$

270 kg/support

132 kV double suspension string

Weight: $7.3 \times 16 \times 2 + 75 = 308.6$ 310 kg/support

Wind pressure: $\{0.027 \times 16 \times (1+0.3) + 0.33\} \times 126 = 112.3$

120 kg/support

132 kV double tension string

Weight : $7.3 \times 17 \times 2 \times 2 + 119 = 615.4 \quad 620 \text{ kg/support}$

Wind pressure: $\{0.027 \times 17 \times (1+0.3) \times 2 + 0.47\} \times 126 = 209.6$

210 kg/support

(d) Safety factor

Normal condition

Abnormal condition

1.2

(e) Slenderness ratio

- (i) Less than 200 for main posts and main members of crossarms
- (ii) Less than 220 for compression members other than (i)
- (iii) Less than 250 for redundant members used for reinforcing compression members

(f) Effective buckling length ratio

Main post 1.0
Bracing 0.9

(g)	Weight ratio of plates and bolts	Suspension tower	Tension tower
	Upper side of waist	0.3	0.3
	Lower side of waist	0.15	0.15
	Crossarm	0.3	0.35

(3) Calculation Results

Calculation results are as shown in the pages listed hereunder.

AS : TLG-1-39 to TLG-1-44

A : TLG-1-45 to TLG-1-50

AL : TLG-1-51 to TLG-1-56

B : TLG-1-57 to TLG-1-62

C : TLG-1-63 to TLG-1-68

D: TLG-1-69 to TLG-1-75.

DR : TLG-1-76 to TLG-1-82

A4 : TLG-1-83 to TLG-1-91

D4 : TLG-1-92 to TLG-1-100

DR4: TLG-1-101 to TLG-1-110

		TOWER TYPE AS	
Item	· :	Calculation	Load (kg
Wind Pressure	G.W.	22.2 x 90 x 250 x 10 ⁻³	500
(HC)	c ₁₋₃	25.30 x 2 x 81 x 250 x 10 ⁻³	
	Ins.	200	1,225
Horizontal Transverse	G.W.	3,800 x sin 1.5° x 2	199
Component of Tension (Ha)	C ₁₋₃	4,000 x sin 1.5° x 2 x 2	419
Conductor	G.W.	1.136 x 250	284
Insulator Weight (Wc)	c ₁₋₃	1.239 x 2 x 250	
	Ins.	400	1,020
Effect of Vertical	G.W.	3,800 x 0.03	114
Angles (Va)	C ₁₋₃	4,000 x 2 x 0.03	240

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(AS)			យ		0	00	. c	0	ø	٥	Q	0	0	ó	0	٥	0	o	0	0	0	0	0	0	٥	٥	o
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	E S S		C1-3	419	0	0 0	1 C	847	က	1925	LΩ	*=4	ß	91	4191	٥	0	268	258	269	200	484	505	346	273	224	180
	r. R	На	b	199	59	175	462	620	771	901	1036	1096	1044	1003	696	-	-	64	↤	Ø	110	0		- 42	-33		-22
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		STRENGTH	(U2)	91	391	517	25175	164	164	181	909	239		22	69456	29	24	11	01	32	76	6664	94	65	66	84	3930
		L/r		119		84	\$ C	67	67	81	ស	99	•	30 20	56	4	Ø	0	0	0	0	103	0	Ø	S	4	145
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		SIZE		*09	* 09	* 000	1120* 8	50%	50*1	50*1	50*1	50*1		7120*17	50*1	45*	* 0:0	40 %	. 70*	7.2*	75*	L 75* 6	*08	*06	. 404	7 3 4 7	L 75* 6
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			C 1225		419	4800	240	1020			3	1	•		(U2) U2	U2/U1
.52		1.26	2		105	3466	144	358	4338	0	4338	L100*10	353	181	5495	1.27
0.00		0.00		00	00	754	154	384	239	505	539 505	L 90* 6	379	187	950	1.88
.80		2.40	٩	622]	13416	575	2443	17269	0	17269	L200*20	671	172	24404	1.41
0.00	٠	2.45			0	0	589	2501	3089	0	3083	1,175*12	587	200	66173	21.42
80	1	0.00		0	Q	3818	o 	•	o i	2558	2558	L 65* 6	170	134	4003	1.56
55		1.38	9	624	214	12238	331	1408	14815	O	14815	1200*15	663	169	19284	1.30
0.00		1.47		0	0	0	354	1503	1857	0	1857	1175*12	708	206	56173	35.63
. 71		00.0		0	0	3394	٥	٥	0	2274	2274	L 65* 6	184	145	3412	1.50
.34		1.36	"	627	214	1.1231	328	1391	13791	٥	13791	L200#15	655	167	19742	1.43
0.00		1.46		0	Q	0	350	1488	1838		1838	L175*12	700	204	66173	36.01
.63		0.00		٥	0	3030	0	0	0	2030	2030	1. 65* 6	193	156	2942	1.45

CROSSARM (IN TOWER BODY)

		UNIT	UNIT STRESS			Hc	На	ρ,	٧a	о <u>ж</u>		DESIGN STRESS	MAX		STREM	STRENGTH OF MEMBER	MEMBER	
		AH	ΑЬ	AV .	ڻ	500	199	2280	114	284			} :				CTOCKOTO	1
				-	ပ ပ	1225	419	4800	240	1020		A . NWL		SIZE	٦	7	(U2)	S.F U2/U1
	·		0.72	1.19		0	0	1636	136	339	474	1414	1414	L100#10	233	119	12188	8.62
G		0.17	0.00	0.42		87	35	0	47	118	2.87	0	287	L 60* 4	233	195	4588	15.98
S			00.0	5		0	0	0	135	337	472	0	472	L 60*.4	236	199	4585	9.72
S		İ	00	0.42		0	0	0	48	120	168	0	168	L 60* 4	233	195	1168	6.95
	2		1.38	2.36		٥	0	0099	566	2403	2969	6411	6411	L200*20	240	62	76000	11.85
ີ່. ບ			00.0	0.43		111	38	0	103	437	683	0	689	L 60* 4	240	202	4585	6.65
ינט	:	3	00.0	2.36		•	0	0	567	2410	2977	0	2977	1, 50 * 4	236	199	4585	1.54
so (0.00	0.00	0.42		0	٥	0	101	430	531	0	531	L 60* 4	236	199	1131	2.13
	O .		1.25	1.35	, , , ,	0	0	0009	325	1381	1706	5163	5163	L200*15	260	99	57750	11.19
ຸ ດ		0.10	00	0.27		122	42	0	65	276	505	0	505	L 60* 4	260	218	4585	9.07
S)			00.0	1.36		Φ	0	0	327	1389	1715	0	1715	7 60* 4	253	212	4585	2.67
(0.00	0.00	0.26		0	0	٥	63	268	331	o ;	331	L 60* 4	253	212	066	2.99
	°		1.14	1.33		0	0	5486	320	1359	1679	4801	4801	L200*15	280	17	57750	12.03
က လ			0.00	0.29		134	46	0	70	297	547	0	547	1.70* 6	280	204	8226	15.03
S		00.0	0.00	1.34		٥	0	0	322	1367	1689	0	1689	L 65* 6	273	215	7483	4.43
S)			00.0	0.28		0	0	0	68	289	358	0	358	L 65* 6	273	215	1553	4.34
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LOAD FOR FOUNDATION

		:		·		(A	S)
No.		DES	IGN STR	ESS	MAX	WT	No.
		NML	A.NML	DIAG. WIND	(U1)		
	Ç	27184	25426	29630	29630		
	T	17374	18854	19820	19820		
9	Qf	3672	4252	2337	0 -	15,443	9
	Qs	3031	4627	1018	0		
	QBf	1052	2497	695	0		
	QBs	564	2813	228	0		
	С	29318	26749	32131	32131		
	T	19084	19892	21898	21898		
10	Qf	3813	3998	2478	0	16,291	10
	Qs	3172	4372	1102	O		
	QBf	961	2087	673	0		
	QBs	568	2342	252	0		
	С	31573	28169	34880	34880		
	T	20682	20872	23989	23989		
11	Qf	3994	3826	2659	0 -	17,606	11
	Qs	3353	4200	1211	0.		
	QBf	910	1759	681	0		
	QBs	597	1962	287	0		
	C	34053	29758	38015	38015		
	T	22171	21797	26133	26133		
12	Qf	4242	3753	2906	0	19,586	12
	Qs	3601	4128	1360	0	-	*
	QBf	918	1526	736	0		
	QBs	670	1687	345	0		1.

:		TOWER TYPE A	4
Item		Calculation	Load (kg)
Wind Pressure	G.W.	22.2 x 90 x 400 x 10 ⁻³	799
(HC)	c ₁₋₃	25.30 x 2 x 81 x 400 x 10 ⁻³	
	Ins.	200	1,839
Horizontal Transverse	G.W.	3,800 x sin 1.5 ⁰ x 2	199
Component of Tension (Ha)	c ₁₋₃	4,000 x sin 1.5° x 2 x 2	419
Conductor and	G.W.	1.136 x 400	454
Insulator Weight (Wc)	c ₁₋₃	1.239 x 2 x 400	1 1
	Ins.	400	1,391
Effect of Vertical	G.W.	3,800 x 0.05	190
Angles (Va)	c ₁₋₃	4,000 x 2 x 0.05	400

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(A)	LA	78	9,771 9,655 10,650	5,48	19,991			
	S.F U2/U1	0.7	7 - 1 0 0 - 1 2 0 0 0 0 0 2 0 0 0 0 0		1.90	0400	1.222	1.25
	STRENGTH (U2)	588	51.51 17518 51642 51642	2002 2008 1008	85368 74275	67 24 11 01	6 6 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	3817 3738 4014
	L/r	110	101 67 70 70	4 00 00 to	0.00	44000	1028 1032 1066 1221 1233	1240
	Lk	440	7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	१५०० ४	173	40044	160 151 167 215	169 220 281
	SIZE	2000 2000 * * *	L120*** L150*** L150***	* * * * * * * * * * * * * * * * * * *	L175*12 L175*12	4 % % % %	7 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	0 * 0 0 1 1 2 2 8 8 1 1 1 2 2 8 9 8 9 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
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CROSSARM

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STRENGTH OF MEMBER	STEENGTS		148 8082 1.68 213 2210 2.53 187 950 1.88	172 24404 1.29 200 63725 14.51 134 4003 1.56	169 19284 1.22 206 56173 25.05 145 3412 1.50	167 19742 1.33 204 66173 25.32 156 2942 1.45		RENGTH OF MEMBER	STDENCTH	(02) 02	98 15113 9.38 195 4585 10.39 199 4585 6.00 196 1168 4.30	62 76000 10.48 202 4585 4.71 186 6691 1.58 199 1131 1.50	66 57750 10.23 218 4585 6.45 212 4585 1.88 212 990 2.10	71 67750 10 05
STS	 	7 7710	L120* 8 353 L 90* 6 379 L 45* 4 164	L200*20 671 L175*12 687 L 65* 6 170	1200*15 663 1175*12 708 1 65* 6 184	1200*15 655 1175*12 700 L 65* 6 198		115	SIZE		L120* 8 233 L 60* 4 233 L 60* 4 236 L 60* 4 239	L200*20 240 L 60* 4 240 L 65* 6 236 L 60* 4 236	L200*15 260 L 60* 4 260 L 60* 4 253 L 60* 4 253	1200415
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UNIT STRESS	AH AP AV G	U	0.53 1.52 1.26 0.00 0.00 1.35 0.00 0.33 0.00	0.51 2.80 2.40 0.00 0.00 2.45 0.00 0.80 0.00	1 0.51 2.55 1.38 5 0.00 0.00 1.47 6 0.00 0.71 0.00	0.51 2.34 1.36 0.00 0.00 1.46 0.00 0.63 0.00	CROSSARM	UNIT STRESS	AH AP AV G	C	M 0.00 0.72 1.19 S 0.17 0.00 0.42 SF 0.00 0.00 1.19 SS 0.00 0.00 0.42	M 0.00 1.38 2.36 S 0.09 0.00 0.43 SF 0.00 0.00 2.36 SS 0.00 0.00 0.42	M 0.00 1.25 1.35 S 0.10 0.00 0.27 SF 0.00 0.00 1.36 SS 0.00 0.00 0.26	M 0.00 1.14 1.33
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LOAD FOR FOUNDATION

		: .	•				(A)
No.		DE	ESIGN S	TRESS	MAX	WT	No.
		NML	A.NML	DIAG. WIND	(U1)		
	С	34928	30599	36278	36278		
	T	24179	23397	25529	25529		
9	1 Q	4814	5013	3203	0	15,481	9
	Qs	3294	4799	1104	0		
	QBf	1328	2678	908	0		
	QBs	585	2822	237	0	·	
	C	37514	32212	39150	39150		
	T	26340	24725	27976	27976		
10	Qf	4965	4764	3354	0	16,330	10
	Qs	3445	4550		0		
	QBf	1189	2235	852	0		
	QBs	592	2350	264	0	<u> </u>	
	С	40216	33922	42299	42299		
	T	28318	25950	30401	30401		
11	Qf	5170	4607	3559	0	17,778	11
	Qs	3650	4393	1318	0		
	QBf	1109	1887	841	0	4	
	QBs	634	1979	308	0		
	С	43219	35851	45978	45978		
	T	30214	27138	32974	32974		
12	Qf	5461	4558	3850	0	19,991	12
	Qs	3941	4344		0		
	QBf	1101	1637		0 -		
ارسنار رسند السد	QBs	728	1710	379	0		
	C	46690	38111	50415	50415		
	T	32050	28302	35774	35774		
13	Qf	5870	4639	4259	0	23,263	13
	Qs	4350	4425	1738	0		
	QBf	1186	1501	1020	0		
	QBs	893	1558	491	0		

		TOWER TYPE AL	
Item		Calculation	Load (kg)
Wind Pressure	G.W.	22.2 x 90 x 500 x 10 ⁻³	999
(HC)	C ₁₋₃	25.30 x 2 x 81 x 500 x 10 ⁻³	
	Ins.	200	2,249
Horizontal Transverse	G.W.	3,800 x sin 1.50 x 2	199
Component of Tension (Ha)	C ₁₋₃	4,000 x sin 1.5° x 2 x 2	419
Conductor	G.W.	1.136 x 500	568
Insulator Weight (Wc)	c ₁₋₃	1.239 x 2 x 500	
	Ins.	400	1,639
Effect of Vertical	G.W.	3,800 x 0.03	114
Angles (Va)	c ₁₋₃	4,000 x 2 x 0.03	240

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CROSSARM

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0.51	2.80	2.40	1143	213	13416	575	3927	19274	0	19274	L200*20	129	172	24404	1.27
36		2.45		0	0	589	4020	4609	0	4609	L175*12	687	200	61277	13,30
3		0.00	0	0	3818	o 	0	0	2558	2558	L 65* 6	170	134	4003	1.56
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8		1,47	0	0	0	354	2417	2771	0	2771	L175*12	708	206	66173	23.88
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0.51	2.34	1.36	1151	214	11231	328	2237	15161	0	15161	L200*15	655	167	19742	1.30
8		1.46		0	0	350	2392	2742	0	27.42	L175*12	700	204	66173	24.13
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CROSSARM (IN TOWER BODY)

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	C1-3	2400	10703 10703 0 1200 925	10504 10504 1200 721	10348 10348 0 1200 562	10226 10226 0 1200 436	10132 10132 0 1200
S	9	1140	5963 1 5963 1 570 570	5674 1 5674 1 570 570 -125	5449 1 5449 1 570 -97	5272 1 5272 1 570 570 -76	5136 1 5136 1 570
S E	C1-3	419	3390 3390 628 213 0	3774 3774 628 0 166	4074 4074 628 0 129	4309 4309 628 0 101	4490 4490 628 0 78
S T R	U	199	1041 1041 99 0 -28	00 60 60 00 00 00 00 00 00 00 00 00 00 0	951 951 99 0	920 920 920 930 930 930	896 896 99 0
웃	C1-3	2249	8204 8204 3374 0 1145	0267 0267 3374 0 892	1878 1878 3374 0 695	3142 3374 3374 540	24115 24115 3374 3374 421
=	U	566	5225 1 5225 1 500 500 -140	4972 2 4972 2 500 -109	4775 2 4775 2 500 - 85 0	4620 2 4620 2 500 500 - 66	4501 4501 500 -52
· A	L.	0.05	381 381 125 0 16	409 4099 1255 100	431 431 125 0 9	4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	462 462 125 0
H	S	0.1	7624 7624 0 2491 312	8186 8186 0 2491 243	8625 8625 8625 2491 0	8970 8970 2491 147	9235 9235 0 2491 0
	± ,		4700 4700 845 270 270	5527 1034 1034 358	6626 6626 1286 1286 475 475	8110 8110 1627 1627 634	10094 2094 2094 2094 858
S	ПС		. 09 . 09 . 50 . 50 . 51	. 50 . 50 . 50 . 50	.73 .50 .50 .31	22 23 24 24 24	0.72 0.72 1.50 0.19
ਨ ਜ਼ ਨ	 පු		. 94 8 . 94 8 . 50 1 . 50 1	633 633 550 130 000 000	117 117 117 117 117 117 117 117 117 117	2.60 10 2.60 10 0.50 1 0.50 1 0.18 0	2.93 10 2.93 10 0.50 1
ST	ු පු :	2		2.00 2.00 2.00 1.13 00 1.13	23.24 00.50 00.50 00.10 00.10	6.0000 6.0000 6.00000 8.00000	3.57 3.57 0.50 0.50
UNIT	ប		7.46 7.50 0.50 0.05 0.05 0.05	4.38 0.50 0.50 0.04 0.04	0.50 0.50 0.00 0.03 0.03	44.26 0.50 0.50 0.02 0.02	4.22 6.22 0.50 0.50 0.50
7	υ		5.23 5.23 6.50 6.50 6.150 6.14 6.10 6.10 6.10 6.10 6.10 6.10 6.10 6.10	4.98 6.50 6.50 6.50 6.11 7.00 7.11	4.78 4.78 0.50 0.50 0.09 0.09	4.62 4.62 0.50 0.50 0.07 0.07	4.51 4.51 0.50 0.50 0.50
			OF PARTY SEE	P P P P P P P P P P P P P P P P P P P	OF SE	OF 2 See See See See See See See See See S	3 of 2 of 2 of 2 of

						(AL)
No.		DES	IGN STR	RESS	MAX	WT	No.
- 4		NML	A.NML	DIAG.WIND	(U1)		
	С	40264	34148	40657	40657		
	T	28778	26452	29171	29171		•
9	Qf	5571	5459	3781	0	16,653	9
	Qs	3336	4766	1130	0	e de la companya de la companya de la companya de la companya de la companya de la companya de la companya de	
	QBf	1475	2715	· ·	0 -		
·	QBs	582	2736	240	0		· · · · · · · · · · · · · · · · · · ·
	С	43556	36220	44246	44246		
	T	31483	28131	32173	32173		
10	Qf	5760	5205	3970	0	17,829	10
	Qs	3525	4511	1243	0		•
	QBf	1297	2214	948	0		1
	QBs	601	2231	275	0		
	C	46811	38296	48005	48005		
	T	33819	29592	35012	35012		
11	Qf	6012	5076	4222	0	19,665	11
	Qs	3777	4383	1394	0	•	2
	QBf	1206	1856	934	0	:	
	QBs	664	1869	332	0		
	C.	50290	40546	52251	52251		
	T	35968	30950	37930	37930		
12	Qf	6353	5071	4563	0	22,324	12
	Qs	4118	4378	1599	0		
	QBf	1203	1621	991	0		
	QBs	781	1631	417	0		
	C	54354	43206	57412	57412	* *	2
	T	37923	32197	40982	40982		
13	Qf	6820	5204	5031	,0,	26,542	13
	Qs	4586	4511	1879	0		
	QBf	1302	1507	1137	. 0	100	
	QBs	973	1515	544	0	tie et e	

		TOWER TYPE B	and the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second s
Item		Calculation	Load (kg)
Wind Pressure	G.W.	22.2 x 90 x 300 x 10 ⁻³	599
(HC)	c ₁₋₃	25.30 x 2 x 81 x 300 x 10 ⁻³	
	Ins.	270	1,500
Horizontal Transverse	G.W.	3,800 x sin 7.5° x 2	992
Component of Tension (Ha)	c ₁₋₃	4,000 x sin 7.5 ⁰ x 2 x 2	2,088
Conductor and	G.W.	1.136 x 300	341
Insulator Weight (Wc)	c ₁₋₃	1.239 x 2 x 300	
(,	Ins.	790	1,533
Effect of Vertical	G.W.	3,800 x 0.03	114
Angles (Va)	c ₁₋₃	4,000 x 2 x 0.03	240

			No.			62	က	4	w	ω	7	œ	6	10		11	H	N	e	4	ĸ	S		∞	6	10	ĮI
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(B)			យ	;	٥	0	0	0	0	0	0	O	0	0		0	0	0	0	0	0	0	٥	0	0	0	0
			Tw		157	210	926	1136	85	Ξ	79	3082	44	4024		4969	0	0	0	0	0	0	0	0	٥	0	0
			۳ ک		57	57	P	177	ch.	O	$\overline{}$	-	-	$\overline{}$		417	0	0	0	0	٥	0	0	0	0	0	0
			O B	İ	170	170	937	937	2	5	47	2471	7	47		2471	٥	ø	0	0	0	0	0	0	0	0	0
			ሆ	.	٥	0	0	0	0	0	0	0	0	0		0	1519	1444	1468	6625	5119	5689	4519	4335	3418	2622	2028
;			C1-3	4000	٥	0	0	2216	5767	8923	-	.,	6.3	.,	,	3539	٥	0	0	2945	2275	2799	2224	2340	1845	1415	1095
		a.	9	1900	663	1940	3246	4872	6369	7697	8929 1	9251 1		8138 1		7756 1	4	80	2	4	95	1065	4	S	***	-	-244
	5 5	_	C1-3	2088	٥	0		1157	6	20	92	160	87	566		17063	0	0	0	IJ	_	2782	C)	6	ശ	_	890
	TRE	На	ე	992	346	5	69	2544	35	10	99	0		ch.		4049	597	558	577	648	200	556	442	-272	1215	-165	-127
	S	HC	C1-3	1500	٥	Ö	Ö	831	2162	4099	6403	8335	9962	11251		12252	0	0	0	1104	853	1997	8	36	0	826	639
		_	9	868	509	612	8	1537	8	45	2	6	5	56		2447	361	343	349	391	305	336	267	-164	-130	66-	-77
		HTA	ĹĿ	0.05	м	4	10	30	56	91	ŝ	159	1-	6		204	8	ო	ဖ	20	13	31	28	74	11	O)	7
			S	1.0	2.8	88	200	602	1123	1827	2593	3184	3557	3849		4078	46	r.	3	ð	t٠٠	630	9	œ	~		132
į			HT		26	~	7	773	33	18	22	ø	5.4	Z,		6724	45	117	218	418	482	732	758	414		774	1080
			o L	, i		•	•	0.55	•	•	•	•	•	•		8.17	•		•	•		1.33			•	•	0.43
ODY	E S S		ဗ				•	0.00	•	•		•		•		2.06						0.00		•	•		0.27
я В	STR		S					0.0	٠							2.72	•					0. 70	•		•	•	0.14
TOWER	NIT		. 2			٠	•	0.55	٠	٠	٠	•		٠		3.38	•	-		•		0.63		•			0.01
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	(B)	ΙM		က	4	7.0	40,	7,413	1,16	,32	3,78	60,09	19,875										
		S.F	U2/U1	7.	တ			2	4	۲.	4		1.35	9.	ß	c,	4	ις (7		4. r	1.26	1.33
		STRENGTH	(U2) (103	03	750	132	57912	691	185	348	586	71443	98	88	241	33	5.7	20 0	5:	7 6	400	15 65 65 65
		LZr	44	0	102	CV I	72	n 0	74	55	. 97	O ် အ	68	2	3	136	\circ	σ,	\circ	\circ	σ	14.0	171
		Lk		ထ	ø	2	~ (170	- (1)	6	9	~	232	4	4	9	0	· •1	~ ∢	∞	⊅ ∙₹	227	303
		SIZE		*06	*06	*06	* 0 8	L120* 8	20*1	75*1	75*1	75*1	L175*12	*09	60 *	*09	300*	*06	*00!	* 000	* * *	9 *08 7	Š
: :		MAX	(U1)	0	~	TC)	6	16074 23138	3 62	86	32	ω	52790	84	81	S	9	67	21	57	9 6	3428	7
	y *	SS	DIAG.WIND	7	4	H	926	16074	2 4 5 5 5 5 5	866	327	784	52790	0	0	0	0	O :	0	0	0 (
		DEST GN STRESS	A.NML D	60	76	58	937	14845	920	416	719	004	42970		8	95	6	67	12		200	4 00	
		DES	NML	ဖ	8	0.9	912	15789	174	770	12	29	50595	8	3	ដ	4	4	43	29	26	2495	7
		No.	1. 1. 1. E. F. F. F. F. F. F. F. F. F. F. F. F. F.	rit	2	ຕ	4	ເກ ແ) (~	ø	6	10	11	1	6 2	ന	4	ល់	9	7	∞ (o ⊆	. .

CROSSARM

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		: : :	5.F U2/U1	1.28	4.29	2.82	1.77	15.54	1.24	1.33	15.80	1.23	1 23	16.08	1.23
(B)	MEMBER		STRENGTH (U2)	6295	1620	833	32628	34999	2942	22348	34999	2400	18941	34999	1995
)	STRENGTH OF MEMBER	· · •	77	136	218	200	130	217	156	146	214	173	143	210	189
	STRI	•	J	240	588	176	510	559	198	200	550	219	490	541	240
			S12E	L 90* 7	L 70* 6	L 45* 4	L200*15	L130* 9	L 65* 6	L175*15	L130* 9	L 65* 6	L175*12	L130* 9	L 55* 6
	MAX	Ξ	5	4910	378	296	18480	2253	2369	16795	2215	1956	15428	2180	1616
	STRESS	A NMI.		٥	0	296	0	0	2369	0	0	1956	0	0	1616
	DESIGN STRESS	NIAI		4910	378	٥	18480	2253	0	16795	2215	0	15428	2180	0
	S/A	341	1533	228	283	٥	1776	1948	0	1741	1915	0	1709	1885	0
	Væ	114	240	92	95	٥	278	308	0	273	300	0	267	295	0
	d.	3800	8000	3677	0	441	14560	0	3536	12894	0	2920	11539	0	2412
	На	992	2088	579	0	٥	1086	0	0	1098	0	٥	1113	0	0
	Нс	G 299	C 1500	350	0	٥	780	0	0	789	0	٥	799	0	0
	ŞŞ	ΑV		0.67	0.83	0.00	1.16	1.27	00.0	1.14	1.25	0.00	1.11	1.23	0.00
	UNIT STRESS	АЬ		0.97	00.0	0.12	1.82	0.00	0.44	1.61	0.00	0.36	1.44	00.0	0.30
	NO	АН		0.58	00.0	0.00	0.52	00.0	0.00	0.53	0.00	0.00	0.53	0.00	0.00
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CROSSARM (IN TOWER BODY)

i	S	UNIT STRESS	SS	HC	Ha	ß.	٧a	.¥c	DESIGN	DESIGN STRESS	MAX		STR	STRENGTH OF MEMBER	MEMBER	
	AH	AP	AV	G 599	992	3800	114	341		NW V			-	'		!
		-		C 1500	2088	8000	240	1533		2	10	S12E	1	1 / T	(U2)	U2/U1
×	0.00	0.41	0.57	0	0	1574	65	195	260	1229	1229	1 90* 7	248	140	5894	4.80
ស	0.30	00.0	0.35	181	299	0	90	118	637	0	637	1, 60* 4	248	209	4585	7.20
Ω (≖'	00.0	00.0	0.56	0	0	0	64	190	254	0	254	L 60* 4	258	217	4585	18.07
SS	0.00	0.00	0.36	0	0	0	41	122	163	0	163	L 60* 4	248	209	1023	6.27
×	0.00	0.88	111	0	0	7000	267	1708	1975	6013	6013	L200#15	280	7.1	57750	09.6
	0.14	00.0	0.32	214	298	0	76	488	1077	0	1.077	L 70* 6	280	204	8226	7.64
ST	0.00	00.0	1.13	0	0	0	271	1729	1999	0	1999	L 65* 6	268	211	7483	3.74
SS	0.00	0.00	0.30	0	0	0	7.3	467	540	0	540	1.65*6	268	211	1606	2.97
*	00.0	0.77	1.08	0	0	6129	259	1655	1914	5389	5389	L175#15	310	91	43145	8.01
2	0.16	0.00	0.35		341	0	ະຕ	540	1210	0	1210	L 75* 6	310	508	8968	7.41
	00.0	0.00	1.09	0		0	262	1676	1939	0	1939	L 70* 6	298	218	8226	4.24
SS	0.00	00.0	0.34	0	0	0	81	519	601	0	601	L 70* 6	298	218	1632	2.72
¥	0.00	0.68	1.05	°	0	5412	251	1603	1854	4868	4868	1175*12	340	66	32289	6.63
S	0.18	0.00	0.39	277	386	0	66	592	1348	0	1348	7 80* 6	340	215	9711	7.20
SF	00.0	00.00	1.06	0	0	0	254	1624	1878	٥	1878	L 80* 6	328	208	9711	5.17
SS	0.00	00.0	0.37	0	0	0	83	572	661	C	199	1 80% B	328	900	305	2 11

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i İ			Va		417	714	417	417
· 		18.7	O E		2471 0 0 0 0	2471	2471 0 0 0 0 0	2471 0 0 0
i	.* -				2876 2876 2876 2876 2876	2203 2203 2203 2203	0 1586 1686 1686	0 1279 1279 1279 1279
İ	·		C1-3	4000	13056 13056 2000 1552	13149 13149 2000 11189	13221 13221 0 2000 0 910	13277 13277 2000 2000 690
		ď	9	1900	8717 8717 950 950	8173 8173 950 950 -265	7755 7755 0 950 -203	7425 7425 0 950 -154
	SSB	ਰ	C1-3	2088	12585 12585 3133 0 1262	14571 14571 3133 967 0	16097 16097 3133 0 740	17299 17299 3133 561 561
İ	S T R	На	U	992	4551 4551 496 -181	4267 4267 496 -138	4049 4049 496 -106	3877 3877 496 -80
		HC	C1~3	1500	9036 9036 2249 0 906	10462 10462 2249 694 694	11558 11558 2249 0 531	12421 12421 2249 403 0
	!		g	599	2750 2750 300 -109	2578 2578 300 -84	2446 2446 300 0 -64	2343 2343 300 1 49
	!	4	tı.	0.05	166 166 71 0	182 182 71 0 8	195 195 71 0 6	206 206 71 0
		HTA	S	1.0	3310 3310 1413 214	3648 3648 0 1413 164	3907 3907 0 1413 0	4111 4111 0 1413 95
!		1	H		4072 4072 880 880 275	4825 4825 1084 1084 366 366	5851 5851 1367 1367 498 498	7309 7309 1768 1768 681 681
Z O	S.		ТС		6.03 6.03 1.50 0.60 0.60	6.98 6.98 1.50 1.50 0.46	7.71 7.71 1.50 1.50 0.35 0.35	8.28 8.28 1.50 1.50 0.27
ATI	RES		ខ		0.75 0.50 0.50 0.39 0.39	1.36 0.50 0.50 0.50 0.30	1.83 0.50 0.50 0.23 0.23	2.20 2.20 0.50 0.50 0.17
OCO	T S T		3		2.01 0.50 0.50 0.20	2.33 2.33 0.50 0.50 0.15	2.57 2.57 0.50 0.50 0.12	2.76 0.50 0.09 0.09
F i	. I N D		Ü		3.26 0.50 0.50 0.01	3.29 0.50 0.50 0.01	3.31 3.31 0.50 0.50 0.01	3.32 3.32 0.50 0.50 0.01
-			9		4.59 0.50 0.50 0.18	44.000 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	4.08 4.08 0.50 0.50	3.91 0.50 0.50 -0.08
			, oN		S OF C OS C OS C OS	0.000000000000000000000000000000000000	C T 10 of ost obs	C T II Qf QS QBf QBf

							(B)
No.		DE:	SIGN STR	RESS	MAX	WT	No.
		NML	A.NML	DIAG. WIND	(U1)	· · · · · · · · · · · · · · · · · · ·	· · · · · · · · · · · · · · · · · · ·
	С	39129	34964	40115	40115		
	T	30078	28900	31064	31064		
8	Qf	7128	6703	2809	. 0	12,326	8
	Qs	2292	4803	881	0		
	QBf	2164	3377	875	. 0		
·	QBs	489	3294	218	0	· :	· · · · · · · · · · · · · · · · · · ·
	С	43219	37767	44495	44495		
	T	33439	31214	34715	34715		
9	Qf	7332	6389	3013	0	13,784	9
	Qs	2496	4489	1003	0		1 1
	QBf	1814	2691	826	.0		
	QBs	531	2628	261	0		
	С	47109	40421	48876	48876		
	T	36173	33094	37941	37941	•	
10	Qf	7616	6232	3297	0 .	16,095	10
	Qs	2780	4332	1174	0		
	QBf	1605	2205	850	0		:
	QBs	623	2157	330	0		1
	С	51310	43274	53855	53855		:
	T	38485	34681	41030	41030	1	
11	Qf	8016	6228	3697	0	19,875	11
	Qs	3180	4328	1414	0	•	
	QBf	1521	1876	948	<u>o</u>		
	QBs	776	1840	432	0		

		TOWER TYPE C	
Item		Calculation	Load (kg)
Wind Pressure	G.W.	22.2 x 90 x 350 x 10 ⁻³	699
(HC)	c ₁₋₃	25.30 x 2 x 81 x 350 x 10 ⁻³	
	Ins.	270	1,705
Horizontal Transverse	G.W.	3,800 x sin 17.5° x 2	2,285
Component of Tension (Ha)	C ₁₋₃	4,000 x sin 17.5° x 2 x 2	4,811
Conductor and	G.W.	1.136 x 350	398
Insulator Weight (Wc)	c ₁₋₃	1.239 x 2 x 350	
	Ins.	790	1,657
Effect of Vertical	G.W.	3,800 x 0.03	114
Angles (Va)	c ₁₋₃	4,000 x 2 x 0.03	240

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			N.			040		ម	9		8\$	ou ≿	3	17	2 5		₹	84	ო	4	ശ	io t	~ 0	x) d	10,			13
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5	UNIT STRESS	SSS		유	Жа	۵۰	× ×	υ ₃ ε	DESIGN	N STRESS	MAX			STRE	STRENGTH OF	MEMBER	
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8288	0.00	1.27 0.32 1.29 0.31		213	601	8000	305 76 309 73	2109 527 2131 506	2415 1418 2439 579	6978	6978 1418 2439 579	1200*20 1 70* 6 1 65* 6 1 65* 6		280 280 269 269	204 204 212 212	76000 8226 7483 1598	10.89 5.80 3.07 2.76
8288	0.00	1.24 0.35 1.25 0.34	:	0 24 0	684 0	2032	297 85 300 81	2053 584 2074 552	2350 1595 2375 644	6286 0 0 0	6286 1595 2375 644	L200*15 L 75* 6 L 70* 6 L 70* 6		310 310 299 299	209 209 218 218	54801 8968 8226 1625	8.72 5.62 3.46 2.52
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		5	1900	8977 8977 0 950 0	8372 8372 0 950 -295	7907 7907 950 950	7541 7541 0 950 0	
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No.		DE	SIGN ST	RESS	MAX	WT	No.
		NML	A.NML	DIAG. WINI	(U ₁)	· ·	
	С	67077	54056	68521	68521		
	T	55512	46308	56955	56955		
10	Qf	12379	10435	3224	0	16,927	10
	Qs	2867	5402	1074	. 0		
	QBf	3452	4454	936	0		
	QBs	555	3553	246	0		
	C	73317	58214	75104	75104		
	T	60829	49847	62616	62616	•	
11	Qf	12599	10081	3443	. 0	18,772	11
	Qs	3087	5048	1206	0		
	QBf	2813	3525	885	0		
	QBs	594	2835	289	0		
	С	78954	61973	81299	81299		
	Т	65053	52659	67398	67398		
12	Qf	12909	9904	3753	0	21,598	12
	Qs	3396	4871	1392	0		
	QBf	2390	2856	914	0		
	QBs	691	2328	364	0		
	С	84679	65794	87896	87896		
	T	68531	54975	71748	71748		
13	Qf	13352	9898	4197	0	26,093	13
	Qs	3840	4865	1658	0		
	QBf	2149	2392	1030	. 0		
	QBs	861	1992	478	0		

:		TOWER TYPE D	
Item		Calculation	Load (kg
Wind Pressure	G.W.	22.2 x 90 x 300 x 10 ⁻³	599
(HC)	c ₁₋₃	25.30 x 2 x 81 x 300 x 10 ⁻³	
· : ' · · ·	Ins.	270	1,500
Horizontal Transverse	G.W.	3,800 x sin 30 ⁰ x 2	3,800
Component of Tension (Ha)	C ₁₋₃	4,000 x sin 30° x 2 x 2	8,000
Conductor and	G.W.	1.136 x 300	341
Insulator Weight (Wc)	C ₁₋₃	1.239 x 2 x 300	
	Ins.	790	1,533
Effect of Vertical	G.W.	3,800 x 0.03	114
Angles (Va)	c ₁₋₃	4,000 x 2 x 0.03	240

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			e >		57	52	144	177	297	297	297	417	417	-	417	·	0	0	0	0	o,	0	0	٥	0	0	0
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		i	CI-3	4000	0	0 9	145	4320	7065	6256	193	420	513	387	2942	0	0	0	2443	2372	2265	2368	2307	2216	2282	~	1182
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	ESS		C1~3	8000	0	0 (1000	8641	413	21787	171	127	49986]	428	57483	0	0	0	4887	4743	4531	9013	8780	8433	3647	99	1889
	STR	Ha	ဟ	3800	1308	3845	0.47	410	46	6106	8130	62	22	7274	15144	2282	2188	2242	2099	2038	1946	1838	1790	1719	-2431	7	-1260
		lic.	C1-3	1500	0	0 (2 7	620	49	084	945	737	370	0176	10775	٥	0	G	916	889	849	1689	1646	1581	684	00	354
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	585	DIAG. WIND	I. თ	m	001	717	27621	944	234	789	468	099	9958	103442	0		0	O	0	0	0	0	0	0	C		>
	DESIGN STRESS	A NML D	4	68	84	446	22226	086	102	286	539	381	74841	648	80	73	2879	4	24	93	1231	08	172	22	147		0
	SEG	NML	9.5	90	96	703	27379	899	165	969	339	504	97827	121	69	99	2835	859	46	23	357	S	300	69	. ທີ) U	ņ

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		tı V	C2/C1	1.35	, o	l is	15.55	1.71	15.82	1.23		16.07	• II		2.94		16.03	•		16.44	1.23	۲.	13.65	1
(a)	MEMBER	STRENGTH	(17.2)	8748	801	32628	34999 2942	33941	34999	2400	23198	34999	2001	8748	1625 801	1 8	34999	2942	20189	34999	2400	22	28331	
	STRENGTH OF 1	: \		122	203	130	217	127	214	173	143	210		122	218 203	142	211	156	138	205	173	134	216 189	
i : !	STRE		4	240	179	510	198	500	549	219	490	540		240	299 179	490	542	198	475	528	219	460	514 240	
		3718		L100* 7 L 70* 6	45 *	L200*15	L130* 9 L 65* 6	00*1	L130* 9	*		L130* 9 L 65* 6		*00	1, 70 * 6 1, 45 * 4	 	L130* 9	*	L175*12	L130* 9	L 65* 6	75*1	L120* 8 L 65* 6	
	MAX	111	5	6489	273	LO I	2250 2369	19904	2213	1956	18579	2178		6489	377 273	1 0	2184	ശ	7.9	2128	95	12016	2074	
	STRESS	มสพ. ช	י יאויין ר	00	273	0	2369	0		1356	o	1616	:	0	273	0	0	2369	0	0	1956	0	1616	; }
	DESIGN S	1 11/2		6489	0	21554	2250 0	19904	2213	0	18579	2178		6489	377	12	2184	0	12793	2128	0	12016	2074	,
İ	N/G	341	1533	227	30	1776	1946 0	I 15-	1913	0	1709	1883		227	83 283 283	2	1888	0	5	1840	0	1603	1793	,
;	Va	114	240	76	0	278	305	i t~	568	0	267	295 0		76	හ හ	j o	296	0	259	288	0	251	281	,
	Ω.,	3800	8000	3596	408	14560	3536	12894	0	2920	11539	2412		3536	408	7000	0	3536	6129	.· •	2920	5412	0 0 0 0	3
	Ha	3800	8000	2238	• •	4160	00	4208	0	0	4264		,	2238	00	4000	0	٥.	4000	0	o l	4000	00	,
	Ж	599	1500	353	0	780	00	789	0	0	799	0 0		353	00	750	0	0	750	0	0	750	00	,
A RM	SS	AV	ပ	0.67	0.00	1.16	1.27	1:14	1.25	0.00	1.11	1.23	20.0	29.0	0.83	1.11	1.23	00.0	1.08	1.20	0.00	1.05	1.17	>
CROSSARM	UNIT STRESS	a. V	ļ	0.95		1.82	0.00	1.61	00.0	0.36	1.44	000	20.0	0.95	0.00	0.88	00.0	0.44	0.77	00 0	0.36	0.58	0.00	>
ับ	Š	АН		0.59	00.00	0.52	00.00	0.53	0.00	0.00	0.53	000	20.0	0.59	。。 。。	0.50	0.0	00.00	0.50	00.0	0.00	0.50	0000	?
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CROSSARM (IN TOWER BODY)

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	IND	UNIT STRESS	SS	유	На	ռ.	ka Va	S X	DESIGN STRESS	TRESS	MAX			STRENGTH	STRENGTH OF MEMBER	
	ЧY	AP.	λγ. (6 2 3 9	3800	3800	114	341	NESS.	A NR41	<u>:</u>	3112	₽-		ļ .	Į.
				C 1500	8000	8000	240	1533			٠.	3	4		(1:2)	V27U1
Z.	00-0	0.40	0.57	°	0	1526	64	193	257	1195	1195	L100* 7	25			6.50
y)	0.31	00.0	0.35	187	1183	٥	40	120	1529	0	1529	L 60* 4	253		3 4585	3.00
T	00.0	0.00	0.55		0	0	63	189	252	0	252	L 60* 4	26			18.22
SS	0.00	0.00	0.36	0	0	0	41	124	165	0	165	L 60* 4	25		213 985	5.96
¥	0.00	0.88	1.11	0	0	7000	267	1708	1975	6013	6013	L200*15		*.	11 57750	
en:	0.14	00.0	0.32	214	1143	0	16	488	1921	0	1921	L 70* 6	:			
S	00.0	00:0	1.13	0	0	0	270	1725	1995	0	1995	L 65* 6			212 7483	3.75
SS	0.00	00.0	0.31	0	0	0	7.4	410	544	٥	544	L 65* 6	270			
Z	00.00	0.77	1.08	ľ	0	6129	259	1655	1914	5389	5389	L200*15				ĺ
t/i	0.16	00.0	0.35	245	1305	0	83	540	ì	0	2175	L 75* 6				
tr.	00.0	00.0	1.09	٥		o ·	262	1673		0	1935	L 70* 6				4.25
SS	0.00	0.00	0.34	3		o [82	522		0	604	L 70* 6	300		219 1612	
×	0.00	0.68	1.05	ľ	0	5412	251	1603	1854	4868	4868	1175*15				8.17
v	0.18	00.0	0.39	277	1478	0	დ 6	592	2441	0	2441	I 80* 6				3.98
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			F.3		4101	-4101	0	0	0	0		-4676	0	0	0	0	5890	-5890	0	0	0	0
			87		417	0	0	0	0	0	417	٥	0	0	0	6	417	0	0	0	0	0
			b C		2471	0	0	0	0	0	2471	0		0	0	0	2471		0	0	٥	0
			σ		0	0	2657	2657	2657	2657	0	0	1859	1859	8	1859	0		1285	1285	1285	1285
		£	C1-3	4000	13915	13915	9	2000	0	1434	12858	12868	0	2000	0	1003	12112	12112	0	2000	0	693
	S		ဟ	1900	8933	8933	0	950	0	-764	7738	7738	0	950	0	1535	6877	6877	٥	950	0	-369
	R E S	Hà	CI-3	8000	50601	50601	12000	0	2292	0	54185	54185	12000	0	1604	0	56769	56769	12000	0	1108	0
	5 7		U	3800		17866			-1528		477		900		-1069		13754	13754	1900	Φ.	-739	0
		22	C1-3	1500	9485	9485	2249	0	430	0	10157	10157	2249	0	301	0	10641	10641	2249	0	208	0
			G	599	2818	2818	300	0	-241		~	2441		٠	1		2169	2169	300	0	-117	٥
		HTA	ì	0.05	173	173	7.1	Ö	~3	0	176	176.	7.1	0	_	0	179	179	7.1	0	~	0
		==	s	1.0	3463	3463	0	1414	Q.	43	3530	3530	0	1414	0	30	ഥ	3578	0	1414	0	73 73
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OUNDATION	Т \$.		Ç			2.11	_					2.26					2.37	2.37	0.50	0:20	0.02	0.05
ĮТ О	UNI	!	Ü		3.48	ري 48	0.50	0.50	-0.17	-0.17	3.22	3.22	0.50	0.80	-0.12	-0.12		3.03				
			IJ		30		20	20	40	40	4.07	4.07	0.50	0.50	-0.28	-0.28		3.62	•	•	•	•
			No.	į	O		10 Of	S)	CB.	QBs	Ü		11 01	So	OBF	OBs	ບ	۲	12 Qf	S.	QBf	QBs

				e e e e e e		(D)
No.		DE	SIGN ST	RESS	MAX	WT	No.
		NML	A.NML	DIAG. WIND	(U1)		
	С	93073	71682	94640	94640		
	T	81984	64253	83552	83552		
10	Qf	17618	13584	3028	0	16,402	10
	Qs	2513	4803	1013	0	1.0	
	QBf	1067	2494	254	0	•	
	QBs	155	2844	78	0		
	Ç	95712	72748	97578	97578		
	T	83473	64548	85339	85339		
11	Qf	17871	13219	3281	0	18,703	11
	Qs	2766	4439	1164	0		•
	QBf	923	1864	355	0		
÷	QBs	285	2109	161	0	· .	
	С	99066	74490	101539	101539		
	T	84399	64663	86872	86872	4	
12	Qf	18276	13106	3686	0	23,560	12
	Qs	3171	4325	1407	0		
	QBf	918	1476	525	0		
	QBs	477	1645	279	O	• .	

		TOWER TYPE DR	
Item		Calculation	Load (kg)
Wind Pressure	G.W.	22.2 x 90 x 300 x 10 ⁻³	599
(HC)	c ₁₋₃	25.30 x 2 x 81 x 300 x 10 ⁻³	
	Ins.	270	1,500
Horizontal Transverse	G.W.	3,800 x sin 45 ⁰ x 2	5,374
Component of Tension (Ha)	c ₁₋₃	4,000 x sin 45 ⁰ x 2 x 2	11,314
Conductor and	G.W.	1.136 x 300	341
Insulator Weight (Wc)	c ₁₋₃	1.239 x 2 x 300	·
	Ins.	790	1,533
Effect of Vertical	G.W.	3,800 x 0.03	114
Angles (Va)	c ₁₋₃	4,000 x 2 x 0.03	240

No. G C1 C2 C3 TC HT S F G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-3 G C1-	No																				
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3 1.70 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.		.01 0.0	•	-	٠	ന	96	rv.	909	0	3	Ö	92	0	0	170	21	304	0	0	7
4 2.40 0.36 0.00 0.00 0.36 778 501 25 1439 1620 16387 1220 5794 4220 0 937 177 1303 0 6 3.67 1.77 0.00 0.00 1.77 1942 1312 66 2200 2649 19723 19984 6973 7065 0 1704 297 2436 0 774 422 1312 0.00 0.00 1.77 1942 1312 66 2200 2649 19723 19984 6973 7065 0 1704 297 2436 0 774 424 2.39 0.38 0.00 2.72 2441 1840 92 2540 44645 9065 11935 0 1704 297 2436 0 1704 297 2436 0 1704 297 2436 0 1704 297 2436 0 1704 297 2436 0 1704 297 2436 0 1704 297 2436 0 1704 297 2436 0 1704 297 2436 0 1704 297 2436 0 1704 297 2436 0 1704 297 2436 0 1704 297 2436 0 1704 297 2436 0 1704 297 2436 0 1704 297 2436 0 1704 297 2436 0 1704 297 2436 0 1704 297 2436 0 1704 297 2436 0 1704 297 2436 0 1704 297 2436 0 1704 297 2436 0 1704 297 2436 0 1704 297 2436 0 1704 297 2436 0 1704 297 2436 0 1704 297 2436 0 1704 2436 0 1704 137 2436 0 1704 137 2436 0 1704 137 2436 0 1704 137 2436 0 1704 137 2436 0 1704 137 2436 0 1704 137 2436 0 1704 137 2436 0 1704 137 2436 0 1704 137 2436 0 1704 137 2436 0 1704 137 2436 0 1704 137 2436 0 1704 137 2436 0 1704 137 2436 0 1704 137 2436 0 1704 137 2436 0 1704 137 2436 0 1704 137 2436 0 1704 137 2436 0 1704 137 2436 0 1704 137 2436 0 1704 137 2436 0 1704 137 2436 0 1704 137 2436 0 1704 137 2436 0 1704 137 2436 0 1704 137 2436 0 1704 137 2436 0 1704 137 2436 0 1704 137 2436 0 1704 137 2436 0 1704 137 2436 0 1704 137 2436 0 1704 137 2436 0 1704 137 2436 0 1704 137 2436 0 1704 137 2436 0 1704 137 2436 0 1704 137 2436 0 1704 137 2436 0 1704 137 2436 0 1704 137 2436 0 1704 137 2436 0 1704 137 2436 0 1704 137 2436 0 1704 137 2436 0 1704 137 2436 0 1704 137 2436 0 1704 137 2436 0 1704 137 2436 0 1704 137 2436 0 1704 137 2436 0 1704 137 2436 0 1704 137 2436 0 1704 137 2436 0 1704 137 2436 0 1704 137 2436 0 1704 137 2436 0 1704 137 2436 0 1704 137 2436 0 1704 137 2436 0 1704 137 2436 0 1704 137 2436 0 1704 137 2436 0 1704 137 2436 0 1704 137 2436 0 1704 137 2436 0 1704 137 2436 0 1704 137 2436 0 1704 137 2436 0 1704 137 2436 0 1704 137 2436 0 1704 137 2436 0 1704 137 2436 0 1704 137 2436 0 1704 137 2436 0 1704 137 2436 0 1704 1		0.0 02.	•	•	•	*	215	17	1021		915		23		٥	937	177	05	0	0	,
5 3.65 1.08 0.00 0.00 1.08 1276 8.94 452 0.5794 4320 0.937 177 1536 0 7 4.24 2.39 0.00 1.77 2.742 1312 66 2200 2540 4084 9055 9059 0 1704 297 2836 9579 0 1704 297 2836 9579 0 1704 297 2826 9579 0 1704 297 2836 9579 0 1704 297 2826 9579 0 1704 297 2826 9579 0 1704 297 2826 9579 0 1704 297 2826 9579 0 1704 297 2826 9579 0 1704 297 2826 9579 0 1704 297 2726 1707 2826 5620 1707 1817 9570 18485 70591 10071 1817 407 1707	٠	.40 0.3	•		•	75	501	25	1439	54	290	0	20	55	0	937	177	ဗ္ဗ	0	0	
6 3.54 1.77 1.00 0.00 1.77 1.94 2.97 2.436 0 7 4.24 2.98 0.30 0.00 1.77 1.98 0.98 0.00 2.74 1.80 0.945 2.640 4.854 965 1.984 6.97 3.76 2.822 0 170 2.25 0.00 3.96 3.678 2.645 2.640 4.4854 9065 11935 0 1704 2.97 2.815 0 1704 2.97 2.815 0 170 2.616 2.645 2.646 3.485 965 11935 0 1704 2.97 2.815 0 171 417 417 417 417 417 417 417 417 417 417 417 417 417 417 417 417 417 417 417 417 417 417 417 417 417 417 417 417 417 418 418 4		.05 1.0			•	2	808	4. D	1828	8	638	225	6	33	0	937	177	က က	0	0	
7 4.24 2.89 0.33 0.00 2.72 2741 1840 92 2540 4084 2851 9578 0 1704 297 287 287 2860 5845 2864 4854 987 100 317 3070 154 2860 587 100 2471 417 4198 0 2471 417 4198 0 2471 417 4198 0 2471 417 4198 0 2471 417 4198 0 2471 417 4198 0 2471 417 4198 0 2471 417 4198 0 2471 417 4198 0 0 2471 417 4198 0 0 0 2471 417 4198 0 0 0 0 2471 417 4198 0 0 0 0 0 2471 417 4198 0 2471 417 417 417 417	ż	.67 1.7			٠	o :	1312	99	2200	9	972	966	97	9	φ.	1704	297	53	0	0	
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	T	112166	83772	114336	114336		
11	Qf	23733	17147	3384	0	21,316	11
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	QBs	487	1651	284	0		

Item		Calculation	Load (kg
	G.W.	22.2 x 90 x 350 x 10 ⁻³	699
Wind	c ₁₋₃	25.30 x 2 x 81 x 350 x 10 ⁻³	<u></u>
Pressure (HC)	Ins.	200	1,635
	c ₄₋₆	36.00 x 90 x 350 x 10 ⁻³	
	Ins.	120	1,254
Horizontal Transverse	G.W.	3,800 x sin 1.5° x 2	199
Component of Tension (Ha)	c ₁₋₃	4,000 x sin 1.5° x 2 x 2	419
	C ₄₋₆	6,000 x sin 1.5° x 2	314
	G.W.	1.136 x 350	398
Conductorn and	c ₁₋₃	1.239 x 2 x 350	· · · · · · · · · · · · · · · · · · ·
Insulator Weight (Wc)	Ins.	400	1,267
	C ₄₋₆	2.446 x 350	
	Ins.	310	1,166
Effect of Vertical	G.W.	3,800 x 0.03	114
Angles (Va)	C ₁₋₃	4,000 x 2 x 0.03	240
	C ₄₋₆	6,000 x 0.03	180
		TLG-1-83	

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CROSSARM (IN TOWER BODY)

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0.00 0.54 1.33 0 0.2311 240 1555 1795 2751 L150*10 353 119 18812 6.18 0.19 0.00 0.52 244 61 0 0 244 1582 1826 L 80* 6 338 214 9711 5.3 0.00 0.00 1.36 0 0 244 1582 1826 L 80* 6 338 214 9711 5.3 0.00 0.00 0.50 0 0 0 244 1582 1826 L 80* 6 338 214 1941 15.3 0.00 0.00 0.50 0 0 1924 227 1472 1699 2428 L150*10 402 214 1541 2.7 0.00 0.53 0 0 0 231 1499 1730 0 0 0 0 0 0 0 0 0 0	, –	0000	1.000	1.3	~	0 9 0 0	8	320 70 322 68	3430	01 02 42	02	002	200*1 70* 65* 65*	280 280 273 273	71 204 215 215	775 822 748 155	1 ~ 0 6 6
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M 0.00 0.45 1.19 0 0 1620 214 1389 1603 2160 2160 L150*10 450 152 12088 5.6 S 0.02 0.06 0.48 87 0 119 772 1326 0 1326 L120* 8 450 189 28331 21.3 F 0.00 0.00 1.21 0 0 219 1416 1634 0 1634 L120* 8 434 183 28331 17.3 S 0.00 0.064 0 0 115 745 860 0 860 L120* 8 434 183 5348 6.2	SO	2000 0000	0000	0.10) G	73	6.	227 106 231 102	1472 689 1499 662	69 16 73 76	42	42 16 76 76	* * * 0 0 0 0 * 1	402 402 386 386	135 204 217 217	518 471 122 213	2046
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FOUNDATION

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			C4-C6		65	S	.20	. 50	0.973	;	.41	.41	1.500	.50	.80	.80	.86	.86	1.500	.50	.67	. 67	0.07	10.078	. 50	08.	. 56	.56
			C1-C3		6.56	.56	.50	.50	-0.045	۳ ک	6.48	48	1.500	50	.03	0.03	6.41	4.1	1.500	.50	0.03	. 03	6.36	16.361	1.50	တ	.02	0.05
	S		9၁		.90	90	. 50	. 50	0.416	, ,	65	65	0.500	.50	.34	დ. 4	.27	. 27	0.500	. 50	.28	. 28	. 79	2.796	.50	. 50	. 23	.23
	RES		CS		88	88	. 50	.50	0.324	3	.47	47	0.500	.50	.26	.26	.95	95	0.500	.50	. 22	. 22	.35	3,359	.50	. 50	.18	.18
	T S T	· · · · · · · · · · · · · · · · · · ·	C4		.86	.86	0	. 50	0.233	3	. 28	.28	0.500	. 50	. 19	. 19	.63	.63	0.500	.50	.16	.16	. 92	3.923	. 50	.50	.13	.13
	UNI		C3		34	.34	.50	. 50	0.095		(C)	.51	0.500	.50	.07	.07	.65		0.500	.50	90.	90.	77.	4.773	.50	.50	.05	.05
			C2		52	52	.50	. 50	-0.015	T 0 ° 0	.49	49	0.500	. 50	.01	0.	.47	. 47	0.500	.50	.01	.01	. 45	5.454	.50	. 50	.00	00.
			CI		70	.70	.50	. 50	-0.125	77.0	.47	.47	0.500	.50	.10	, i	2	6.29	0.500	. 50	0.08	.08	13	6.134	8	.50	.07	.07
			O		22	. 22	. 50	.50	-0.174		90	90	0.500	. 50	. 14	. 14	64	64	0.500	.50	0.12	23	. 43	6.432	.50	.50	.10	0.10
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ပ	16199	18730	936	5050	27080	7807	<u>د</u> ئ	(1)	1775	8233	16091	5153	Ç	587	3849	7153	0	0
	16199	18730	986	5050	27080	7087	1437	6939	1775	8233	16091	5	0	0	0	-	0	0
	2315	0	203	350	2452	1881	66	628	471	0	0	0	1729	0	0	0	0	0
	2315	4054	٥	0	0	0	0	0	0	570	1200	006	1729	Ö	0	0	٥	0
QBf	804	0	7.1	-121	-74	1220	-35	-19	306	0	0	0	1729	0	0	0	0	0
OBs	804	280	0	0	0	0	0	0	0	0	0	748	1047	0	0	0	0	0
U	18296	19236	962	4830	26945	lσn	1374	၂ င္တ	32	7874	1 0	5	0	687	3849	7808	0	٥
H	18296	19236	962	4830	26945	9297	1374	6905	2329	7874	15546	5913	0	0		-7808	0	0
17 Qf	2669	0	203	350	2452	88	66	62	47	0		0	43	0	0	0	0	0
	2669	4054	0	0	0	0	0	0	0	570	1200	006	1437	0	0	0	0	0
	396	0	15	-101	-62	1014	-29	-16	254	0	o	0	23	0	0	0	0	0
QBs	962	233	0	0	0	0	٥	0	0	0	٥	622	870	٥	0	0	0	٥
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	3128	0	203	350	2452	1881		628	471	0	0		1,197	0	0	0	0	0
	3128	4054		0	0	0			0	570	1200	006	1197	0	0	0	0	0
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19 Qf	3713	0	203	350	2452	1881	66	628	471	0	0	٥	988	0	0	0	٥	0
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LOAD FOR FOUNDATION

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No.		DI	ESIGN S	TRESS	MAX	b/T	No.
		NML	A.NML	DIAG. WIND	(01)		
	C	78193	63170	86536	86536	-	
	T	59351	50546	67694	67694	•	
16	Qf	8399	6785	4466	0	28,613	16
	Qs	6369	6229		0		
	QBf	2094	2561	660	0		
	QBs	1083	1929	552	0		· ·
	C	83282	66214	92648	92648		
	T	63130	52713	72497	72497		
17	Qf	8753	6827	4821	0	31,231	17
	Qs	6723	6271	2615	0		
	QBf	2034	2326	843	0	•	
:	QBs	1195	1800	636	0		
	С	88589	69470	99288	99288		
	Ť	66751	54839	77451	77451		
18	Qf	9212	6974	5280	0	34,603	18
	Qs	7182	6418	2891	0		
	QBf	2077	21.94	1085	0		
	QBs	1378	1756	759	0		
	С	94702	73314	107157	107157		
	T	70259	56937	82714	82714		•
19	Qf	9797	7231	5865	0	39,814	19
	Qs	7767	. 6675	3241	. 0		
	QBf	2213	2149	1388	0	· ·	
	QBs	1632	1786	923	0		

		TOWER TYPE D4	
Item		Calculation	Load (kg)
	G.W.	22.2 x 90 x 250 x 10 ⁻³	500
Wind Pressure	c ₁₋₃	25.30 x 2 x 81 x 250 x 10 ⁻³	
(Hc)	Ins.	270	1,295
	C ₄₋₆	36.00 x 90 x 250 x 10 ⁻³	
·	Ins.	210	1,020
Horizontal Transverse	G.W.	3,800 x sin 30 ⁰ x 2	3,800
Component of Tension (Ha)	C ₁₋₃	4,000 x sin 30 ⁰ x 2 x 2	8,000
	C ₄₋₆	6,000 x sin 30 ⁰ x 2	6,000
	G.W.	1.136 x 250	284
Conductor and	c ₁₋₃	1.239 x 2 x 250	an e
Insulator Weight (Wc)	Ins.	790	1,410
, ,	C ₄₋₆	2.446 x 250	
	Ins.	620	1,232
Effect of Vertical	G.W.	3,800 x 0.03	114
Angles (Va)	C ₁₋₃	4,000 x 2 x 0.03	240
	C ₄₋₆	6,000 x 0.03	180

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			C1-C3		§ §	38	. 36	88.	2.5	96.	5.159 6.964	2	0.70	1.85	3.87	14.771	7.0.4	1.41	8	00.	8:	10	5.0	. 12	1.097	7.5	'n		.20	2.0	92	1,55	-1.141 -0.825
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	SIZE		L100*10	*00	200	*09	20*1	20*1	*00	1*00	*00	00*2		1	100000	4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	7 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	2000	****	250*3	250*3	250*3	*09	*09	L 65* 6	*06	*06	*06	100*1	1*001	*001	150*1	0*1	20*	50*1	30*	50*7	50*	1.65* 6	*08	*00
	MAX	(01)	1884	š	982	598	740	903	197	758	7	65 55	0700	100	170,00	200	9000	3 6 6 6 6	7767	3667	2539	2041	6.4	62	2821	47	36	816	341	22	292	893	708	314	844	584	8	84.6	-	20	98
	RESS	IAG. WEND	1876	9	982	698	740	903	197	758	č	658	0 7 6 6	96	201701	0 6	2000	000	787	3667	2539	204	0	0	0	0	0	0	0	0	0	٥,	0	0	0	0	0	0	0	٥	0
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(04)		S.F U2/U1	1.67 4.92 4.89	1.39 16.72 1.38	1.26 17.01 1.36	1.38 17.28 1.37	1.44 15.53 5.01	1.53 15.77 7.66	1.59 15.95 18.52
	MEMBER	STRENGTH (U2)	5532 1625 801	21483 34999 1958	18247 34999 1597	18941 34999 1328	13493 28331 1663	13943 28331 1726	14281 28331 2540
{ } }	STRENGTH OF MEMBER	1/1	135 218 203	149 217 168	145 214 186	143 210 204	143 195 215	141	139 190 199
	STF		240 299 179	510 558 198	500 549 219	840 240	426 465 295	419 458 324	414 453 354
		SIZE	L 90* 6 L 70* 6 L 45* 4	L175*15 L130* 9 L 60* 5	L175#12 L130# 9 L 60# 5	L175*12 L130* 9 L 60* 5	L150*10 L120* 8 L 70* 6	L150*10 L120* 8 L 75* 6	L150*10 L120* 8 L 90* 6
	MAX	(a	3317 330 164	15480 2093 1421	14498 2058 1174	13716 2025 970	9370 1824 332	9125 1797 225	9008 1776 136
	STRESS	A. Neal	0 0 164	0 0 1421	0 0 1174	0 970	332	0 0 225	136
	DESIGN STRESS	NEJL	3317 330 0	15480 2093 0	14498 2058 0	13716 2025 0	9370 1824 0	9125 1,797 0	9008 1776 0
	ن بد	284 1410 1232	189 236 0	1632 1788 0	1601 1759 0	1571 1731 0	1457 1592 0	1433 1567 0	1416 1549 0
	٧a	114 240 180	76 95 0	278 305 0	273 299 0	267 295 0	213 233 0	209 229 0	207 226 0
	ŝ.	2280 4800 3500	2157 0 245	8736 0 2121	7737 0 1752	6923 0 1447	3673 0 496	3288 0 337	2981 0 204
	Ha	1020 8000 6000	601 0 0	4160	4208	4264	3441	3585	3764 0 0
	Hic	G 500 UC 1295 LC 1020	294 0	673 0	681 0	089	585 0	609 0	640 0
.	55	AV U	0.67	1.16	1.14	1.11	1.18	1.16	1.15
	T STRESS	ΑV	0.95	1.82	1.61 0.00 0.36	1.44	0.00	0.00	0.83 0.00 0.06
	TIND	AH	0.59	0.52 0.00 0.00	0.00	0.00	0.00	0.00	0.00
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CROSSARM (IN TOWER BODY)

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		S.F V2/V1	6.48 7.48 20.82 6.81	11.50 4.44 4.03 3.13	9.57 4.28 4.57 2.87	9.69 4.12 5.57 3.29	6.86 5.27 9.90 3.94	6,31 20,16 5,91	5.89 7.78 21.39 4.53	
(+4)	MEMBER	STRENGTH (U2)	4953 4585 4585 985	46502 8226 7483 1584	34982 8968 8226 1612	32289 9711 9711 2033	14048 14718 14718 3108	11633 28331 28331 5139	9791 28331 28331 4300	
	STRENGTH OF	1.7 г	142 213 220 213	202 212 212 212	90 209 219 219	99 215 209 209	212 202 204 204	154 193 186 186	168 210 204 204	
į	STR	L.	253 253 262 253	280 280 270 270	310 310 300 300	340 340 330	417 417 402 402	4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	500 500 485 485	
		SIZE	000 1 1 1 600 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	L175*15 L 70* 6 L 65* 6 L 65* 6	L175*12 L 75* 6 L 70* 6 L 70* 6	L175*12 L 80* 6 L 80* 6 L 80* 6	L150*10 L100* 7 L100* 7 L100* 7	L150*10 L120* 8 L120* 8 L120* 8	L150*10 L120* 8 L120* 8 L120* 8	
.	MAX	I-I	764 613 220 145	4045 1853 1856 506	3657 2098 1800 562	3331 2355 1744 618	2048 2791 1486 788	1843 3195 1405 869	1663 3639 1324 950	
	STRESS	A. NHL	764 0 0	4045 0 0	3657 0 0 0	3331 0 0 0	2048 0 0	1843	1663	
	DESIGN	NML	225 613 220 145	1837 1853 1856 506	1781 2098 1800 562	1724 2355 1744 618	1456 2791 1485 788	1375 3195 1405 869	1294 3639 1324 950	
	Wc	284 1410 1232	160 100 157 103	1570 448 1586 432	1522 497 1538 480	1474 545 1490 528	1270 714 1297 687	1200 785 1226 758	1129 855 1155 829	
	ķ	114 240 180	6 640 0 40 0 63 0 41	00 267 0 76 0 270 0 74	7 259 0 85 0 262 0 82	7 251 0 93 0 254 0 90	01 186 0 104 0 190 0 100	6 175 0 115 0 179 0 111	18 165 0 125 0 169 0 121	
2	fla P	0 2280 0 4800 0 3600	0 91 0 0	43 420	0 3677 05 0 0 0	0 324 0 0	9 86 0 0	62 62 0	0 118 0 0	
	Hc	500 1020 295 8000 020 6000	\$ 000 \$ 000 \$ 000	185 0 0	211 13 0	239 14 0	287 16 0	334 19 0	386 22°	
		AV G I LC 1	0.87 0.38 0.38	1.11 0.32 1.13 0.31	1.08 0.35 1.09 0.34	1.05 0.39 1.06 0.37	1.03 0.58 1.05 0.56	0.97 0.64 1.00 0.62	0.92 0.69 0.94 0.67	
	T STRESS	AI:	0000	0.00	0.77 0.00 0.00 0.00	0.00	0.00	0.38	00.00	
	LINI	## ##	0.00	00.00	0.00 0.16 0.00	00.00	0.00	0.00	0.00	
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			C4-C6		25	4.257	. 50	. 50	.68	. 68	.29	23	1.500	.50	.49	49	90	.06	.50	.50	0.344	.34
			C1-C3		3.07	13.074	. 50	50	.99	0.99	1.57	57	1.500	50	.70	.70	0.47	. 47	1.50	50	-0.497	49
			92		.72	0.724	. 50	50	.36	.36	26	. 26	0.500	20	25	. 25	67	.67	. 50	50	0.181	∞.
	RESS		CS		41	1.419	. 50	. 50	. 22	. 22	76	.76	0.500	.50	. 16	. 16	0.0	.02	.50	50	0.115	. 1.
·	TST		C4		11.	2.114	. 50	. 50	.09	.09	.26	.26	0.500	.50	90.	90.	.36	.36	. 50	.50	0.048	.04
:	N D		င္သ	:	41	3.417	. 50	.50	.13	. 15	. 18	. 18	0.500	. 50	.10	.10	. 02	.02	.50	. 50	-0.076	.07
• .			C2		ις 13	4.358	0	\circ	0.33	CO I	.85	IJ	0.500	0	ŝ	0.23	49	\circ	.50	O	-0.166	ψ '
			Cl	:	.29	5.299	.55	. 50		.51	53	, 33	0.500	50	.36	.36	96	96.	. 50	. 50	-0.255	.25
			ত		رب است	6.139	.50	20	.67	.67		12		. 50	. 47	.47	38	80	30	. 50	-0.335	.33
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	0 %		Ì	00	00	4104	00	00		0000
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	C4-6	1800	3805 3805	006	652	4068	000	464	4262	900 0 326
	P C1-3	2400	12718 12718	1200	00	10872	1200	00	9507	1200
· ·	b	1140	8669 6998	570	00	5847		00	4994	570
· .	C4-6	6000	25540 25540	0006	4130	31763	0006	2944	36367	200 200 200 200 200
· .	Ha C1-3	8000	104593	12000	-7944	92625	12000	-5662	83770	-3973
	U	3800	23328	0061	-2548	19489		-1816	16648	-1274
	C4-6	1020	4342	1530	702	5400	1530	500	6182	. B
	HC C1-3	1295	16926 16926	1942	-1286	14990	1942	-916	13557	-643
	O	200	3066	220 0	23.5 0	2562	12 (-239	2188	-168
	HTA F	0.05	459 839	13 13 13 13 13 13 13 13 13 13 13 13 13 1	-20	429	9 C	-14	406	1000
	π s	1.0	9182	0 2698	-401	8577	·	-286	8130	2699
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LOAD FOR FOUNDATION

					<u> </u>		(D4)
No.		DE	SIGN ST	RESS	MAX	WT	No.
		NML	A.NML	DIAG. WIND	(11)		
	C	212338	150787	221616	221616		
	T	186396	133406	195674	195674		
17	$\mathbf{Q}\mathbf{f}$	30131	20921	5052	0	42,303	17
	Qs	6073	5606	2699	0	•	
	\mathbf{QBf}	0	0	0	0		
	QBs	0	812	0	0	_	
	С	203618	143708	213261	213261		
	T	174091	123925	183735	183735		
18	Qf	30648	21057	5569	. 0	49,472	18
	Qs	6590	5742	3010	. 0		
	QBf	0	0	0	0		
	QBs	230	826	66	Ŏ		
	С	200208	140509	210904	210904		· · · · · · · · · · · · · · · · · · ·
	Ť	164550	116618	175246	175246		
19	Q f	31481	21459	6402	0	61,734	19
	Qs	7423	6144	3509	Ō	,,	
	QBf	0	0	136	ŏ		
	QBs	746	971	397	0 :	1	

		TOWER TYPE DR4	
Item		Calculation	Load (kg)
	G.W.	22.2 x 90 x 350 x 10 ⁻³	699
Wind	c ₁₋₃	25.30 x 2 x 81 x 350 x 10 ⁻³	
Pressure (HC)	Ins.	270	1,705
	C ₄₋₆	36.00 x 90 x 350 x 10 ⁻³	
	Ins.	210	1,344
Horizontal Transverse	G.W.	3,800 x sin 37.5 ⁰ x 2	4,627
Component of Tension (Ha)	c ₁₋₃	4,000 x sin 37.5° x 2 x 2	9,740
	c ₄₋₆	6,000 x sin 37.5° x 2	7,305
	G.W.	1.136 x 350	398
Conductor and	c ₁₋₃	1.239 x 2 x 350	
Insulator Weight (Wc)	Ins.	790	1,657
	C ₄₋₆	2.446 x 350	
	Ins.	620	1,476
Effect of Vertical	G.W.	3,800 x 0.03	114
Angles (Va)	c ₁₋₃	4,000 x 2 x 0.03	240
•	C ₄₋₆	6,000 x 0.03	180

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(DR4)		C4-C6	100	90	0	0,1	30	. 0	0.000	. 00	8	8	8	1.041	.69	.94	5.5	5						•	•	000	۰.	9	ŝ	٧.	∹ a	. 0	٠.	0.499
		CI-C3	183	38	36	86		96	5.159	.21	0.70	1.85	2.92	13.877	4.57	2.76	1.67	0	8	00	ું:	9 15	.56	.12	ρ. Ο .	1.710	.51	13	. 20	5	56	55	1.14	-0.720
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	17 S	ឌ	100	90	9	0,4	20	0	0.000	8	97	43	86.	3.500	69	. 42		•	8	ô.	88	200	8	ွင့်	35	0.682	.60	45	8	÷.	4 C	0.23	0.17	-0.110
KODX	D N	8	83	38	8	86	3 6	.98	1.609	.07	.58	.95	င္ပ	4.924	83	.25	. 89	?		. •				•		0.570	n O	3	40	e .	200	9	0.38	-0.240
OWER B		បី	1 ? 9	? ?	C.	o, r	. "	6	3.551	.75	 	46	. 25	6.247	5	.09		3	8	00.	85	200	.56	رن د	70.	0.458	40	33	32	27	2 6	.80	0.58	-0.308
TOW		Ö	34.	32.	.40	9.0	23	77	5.284 5.795	. 26	ž,	.81	ॅं	7.427	S	83	60.	7	69.	.57	e n		.51		4.	0.358	31	. 23	. 25	2	7 0	1.05	.77	00
		No.	6	v 60	4	ט לט	۰,	ω	10	11	12	ლ :	4.	6 T	17	8 -	о C	2	 #4	C 3	ლ <	r in	9	٠.	20 C	î 0		12		4.1	0 4	17	198	70 70 70

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		SIZE	*06	L 70* 6 L 45* 4	L175*15	L130* 9 L 60* 5	L175*15	L130* 9 L 60* 5		L175*12 L130* 9	L 60* 5	L150*10	L120* 8 L 70* 6	1.150*10	L120* 8	L 75* 6	L150*10	L120* 8	L 90* 6
MAX		o	3701	424 164	16885	2407	15910	2367		15139 2330	970	10594	2140	10383	2108	225	10311	2084	136
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412 792 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	114 398 240 1657 180 1476	8 7 NHL A.NML 6	ın	SIZE	ہ ا	L/r	STRENGTH (U2)	S.F. U2/U1
852 4870 0 0 0 0 0 0 0 0 0 0 0 0 0	76 265 95 330 0 0	5 3701 0 0 424 0 0 0 164	3701 424 164	1 90 c 6 1 45 c 6	240 299 179	135 218 203	5532 1625 801	3.83 4.89
852 4870 0 0 0 0 0 0 852 4870 0 0	267 1846 296 2041 0 0	6 12035 0 1 2336 0 0 1421	12035 2336 1421	L175*12 L130* 9 L 60* 5	490 542 198	142 211 168	18972 34999 1958	14.98 1.38
852 4870 0 0 0 0	259 1789 288 1989 0 0	9 11448 0 9 2277 0 0 1174	11448 2277 1174	L175*12 L130* 9 L 60* 5	475 528 219	138 205 186	20189 34999 1597	1.76 15.37 1.36
0.000	7 251 1733 0 281 1938 7 0 0	3 10953 0 8 2218 0 0 970	10953 2218 970	L150*12 L120* 8 L 60* 5	460 514 240	155 216 204	13677 28331 1328	12.77
1.03 6/2 3533 1501 1.17 0 0 0 0.00 0 496	1 186 1522 5 210 1720 5 0	2 7634 0 0 1930 0 0 332	7634 1930 332	L130* 9 L100* 7 L 70* 6	371 420 295	144 213 215	10350 14718 1663	1.36 7.62 5.01
0.97 672 3653 1376 1.11 0 0 0 0.00 0 337	5 175 1438 0 201 1644 7 0 0	8 7314 0 4 1845 0 0 225	7314 1845 225	L130* 9 L100* 7 L 75* 6	351 401 324	136 204 219	11605 14718 1726	1.59 7.98 7.66
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(DR4)	STRENGTH OF MEMBER	L/r STRENGTH (U2)	3 142 4953 3 213 4585 2 220 4585 3 213 985	0 82 46502 0 204 8226 0 212 7483 0 212 1584	10 91 43145 10 209 8968 00 219 8226 00 219 1612	40 99 32289 40 215 9711 30 209 9711 30 209 2033	17 141 14048 17 212 14718 02 204 14718 02 204 3108	9 154 11633 193 28331 3 186 28331 3 186 5139	00 168 9791 00 210 26699 85 204 28331 85 204 4300
		SIZE	1. 90* 6 25 1. 60* 4 25 1. 60* 4 26 1. 60* 4 25	L175*15 28 L 70* 6 28 L 65* 6 27 L 65* 6 27	L175*15 31 L 75* 6 31 L 70* 6 30 L 70* 6 30	L175*12 34 L 80* 6 33 L 80* 6 33 L 80* 5 33	L150*10 41 L100* 7 41 L100* 7 40 L100* 7 40	L150*10 45 L120* 8 45 L120* 8 44	L150*10 50 L120* 8 50 L120* 8 48 L120* 8 48
	RESS MAX	NIME (11	07 807 0 816 0 283 0 186	0 4230 0 2239 0 2135 0 582	36 3836 0 2536 0 2070 0 646	5 3505 0 2848 0 2005 0 711	7 2217 0 3391 0 1744 0 925	3 2003 0 3884 0 1649 0 1019	3 1813 0 4426 0 1554 0 1114
	DESIGN ST	NML A.	5 289 80 0 816 0 283 4 186	6 2113 423 7 2239 5 2135 8 582	9 2048 383 4 2536 8 2070 5 646	1984 350 2848 2005 711	2 1708 221 6 3391 4 1744 4 925	38 1613 200 40 3884 69 1649 09 1019	3 1518 181 6 4426 1554 3 1114
RODY)	P Va WC	0 114 398 0 240 1657 0 180 1476	16 64 22 0 40 14 0 63 22 0 41 14	00 267 184 0 76 52 0 270 186 0 74 50	77 259 178 0 85 58 0 262 180 0 82 56	47 251 1733 0 93 640 0 254 1752 0 90 621	01 186 152 0 104 85 0 190 155 0 100 82	76 175 14 0 115 9 0 179 14	88 165 1355 0 125 102 0 169 138 0 121 99
IN TOWER	Hc He F	99 1344 2280 05 9740 4800 44 7305 3600	0 0 9 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 42 44 1391 0 0	0 0 36 178 1589 0 0	315 1800 32 0 0 0 0	0 0 16 378 2053 0 0 0 0	0 0 13 440 2389 0 0	509 2767 11
SARM	STRESS	AV 6 6 UC 17 LC 13	40 0.57 0.00 0.35 0.00 0.35 0.00 0.35	.88 .1.11 .00 0.32 2 .00 1.13	77 1.08 00 0.35 00 1.09 00 0.34	68 1.05 00 0.39 00 1.06 00 0.37	44 1.03 00 0.58 00 1.05 00 0.56	38 0.97 00 0.64 00 1.00 00 0.62	33 0.92 00 0.69 00 0.94 00 0.67
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		C1-C3		3.07	13.074	1.50	1.50	99	0.99	1.57	57	1.500	.50	.70	0.70	0.96	.96	1.50	1.50	Ġ	0	0.47	. 47	1.500	.50	49	0.49
		CG.		.72	0.724	. 50	. 50	.36	.36	.26	. 26	0.500	. 50	25	.25	.49	. 49	.50	. 50	0.216	.21	.67	67	0.500	. 50	.18	. 18
RESS		CS		41	1.419	.50	. 50	. 22	. 22	.76	.76	0.500	50	. 16	.16	90	.90	. 50	. 50	0.137	.13	.02	.02	0.500	. 50	7	. 11
TST		C4		11.	2.114	0	. 50	.09	000	.26	. 26	0.500	. 50	90.	90.	.31		.50	. 50	0.058	.05	.36	.36	0.500	50	.04	.04
I Z D	- 1	 C3	-	41	3.417	.50	. 50	5		1.8	.1.8	0.500	500	. 10	.10	60	60:	.50	.50	060.0-	.09	.02	.02	0.500	. 50	.07	.07
		C2		35	4.358	.50	50	0.33	က	85	85	0.500	.50	0.23	23	.65	.65	.50	0.50		0.19	49	49	0.500	0.50	.16	0.16
		C1		.29	5.299	. 50	.50	.51	0.51		.53		. 50	0.36	36	21	21	.50	.50	30	(1)	3.9	3.96	0.50	0.50	-0.25	-0.25
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No.		Ω	ESIGN S	TRESS	MAX	WT	No.
		NML	A.NML	DIAG. WIND	(U1)		
	С	257252	180880	265341	265341		
	T	227954	161250	236043	236043		
17	Qf	36527	25207	5807	0	47,425	17
	Qs	6176	5675	2802	0		
	QBf	0	0	. 0	0		
	QBs	0	768	0	0		
	С	245879	172024	254391	254391		
	T	213000	149995		221512		
18	Qf	37054	25349		0	54,587	18
	Qs	6703	5818	3118	0		
	QBf	0	0		0	·	
	QBs	189	799	39	0		
	С	242780	169442	251791	251791		
	Ť	206451	145102		215462		
19	Qf	37687	25687	6966	0	61,486	19
	Qs	7336	6156	3498	0	•	
	QBf	0	0	0	0		
	QBs	687	1022	350	0		
	С	241795	168372	251579	251579		
	T	200804	140908	210589	210589		
20	Qf	38413	26103	7692	0	70,809	20
- *	Qs	8062	6572	3933	0		
	QBf	0	0	373	.0		
	QBs	1187	1267		0		