Table VI-30(1/4) POTENTIONAL SEDIMENT DISASTER SITES ON ARTERIAL ROAD

Location	Catchment	Slope/	Torrent	** Vegetation	Geology	Potential	Disaster
No.	Area(ha)	Lentgh(m)	Gradient*	Cover	deorogy	Type***	Rank
1	126	2,750	12.50	1	Pels	S	6
2	40	500	7.14	1	Peis	S	6
3	247	3,125	12.50	1	Peis	S	1
4	10	625	8.33	1	Pels	S.	6
5	55	1,000	4.17	1	Peis	S	. 6
6	41	1,125	5.00	1	Pels	S	6
7	39	500	2.78	1	Peis	D	1
8	408	3,250	12.50	1	Peis	S	1
9	406	2,875	12.50	1	Pels	· S ·.	1
10	31	250	1.79	1	Peis	\$	6
11	. 34	750	3.57	1	Peis	D,	- 5
12	151	1,500	8.33	1	Peis	: S .	. 1
13	318	3,250	12.50	1	Pet	S	. 6
14	. 88	1,250	3.57	1	Pet	a	1
15	. 28	1,750	2.78	1	Pet	D	5
16	46	1,500	5.00	i	Pet	\$	6
17	278	2,250	12.50	1	Pet	S	6
18	128	1,750	5.00	1	Pet	S	1
19	115	1,500	6.25	1	Pet	\$	6
20	145	2,250	8.33	1	Pet	S	1
21	64	1,250	6.25	1	Pet	S	6
22	245	3,250	8.33	1	Pet	5	6
23	41	750	5.00	1	Pet	S	6
24	148	1,750	6.25	1	Pet	. S	6
25	230	2,625	5.00	1	Pet	S	6
26	444	3,875	8.33	1	Pet	. \$	6
27	123	1,250	4.17	1	Pet	S	6
28	341	3,875	8.33	ī	Pet	S	6
20 29	58	1,000	2.78	1	Pet	D	5
30	29	500	2.50	1	Pet	D	5
	31	500	2.50	1	Pet	.D	: 5
31	14	. 500	2.78	1	Pet	D	5
32		250	2.50	1	Pet	0	5
33	13			1	Pet	n	5
34	8	250	3.13 2.50	1	Pet	D	5
35	26	1,375			Pet	D	5
36	24	500	2.08	1	Pet	p	5
37	40	1,250	2.78	1		0	5
38	21	500	1.67	1	Pet Pet	D	5
39	31	625	1.92	1		ם ם	3
40	33	875	2.78	4	Pet		3
41	30	625	2.50	4	Pet	D D	3
42	21	625	2.08	4	Kp "~~		. 3
43	21	875	3.57	4	Кср	. D	
44	36	500	2.50	4	Kag	D	3
45	56	1,250	6.25	4	Gr	S	4
46	66	1,250	5.00	4	Kag	S	4
47	196	2,000	25.00	4	Karn	\$	1
48	231	3,500	25.00	4:	Pcs	S	1

Table VI-30(2/4) POTENTIONAL SEDIMENT DISASTER SITES ON ARTERIAL ROAD

Location	Catchment	\$1ope/	Torrent	**	Conlami	Potentia1	Disaster
No.	Area(ha)	Lengh(m)	Gradient*	Vegetation Cover	deo togy	Type***	Rank
49	26	500	1.67	4	Peis	F	2
50	39	875	2.08	4	Pels	D	3
51	169	2,000	3.13	. 4	Peis	D	3
52	46	1,250	1.47	4	Peis	F	2
53	58	1,250	1.67	4	Pels	F	2
54	274	2,750	1.79	4	Pet	Ð	1
55	470	3,750	4.17	4	Pet	\$	1
56	103	1,500	2.50	4	Pels	. D	. 3
57	85	750	1.67	4	Peis	F	2
58	33	750	3.57	4	Pet	D	3
59	·· · 18	500	3.13	4	Pet	Ð	3
60	75	1.250	5.00	4	Pet	- \$	4
61	21	750	6.25	4	Pet	S	4
62	26	625	8.33	4	Pet	S .	4
63	186	2,125	12.50	4	Pet	- S	4
64	126	2,625	8.33	4	Pet	S	4
65	24	750	12.50	4	Pet	S	4
66	98	1,500	8.33	4	Qpt	S	4
67	303	3,250	8.33	4	Qpt	S	4
68	104	2,000	12.50	4	Qpt	S	4
69	145	2,750	6.25	- 4	Qpt	S	. 4
70	94	750	6.25	. 4	Pet	S	4
71	86	1,250	8.33	4	Pet	S	4
72	47	750	12.50	4	Pet	S	4
73	20	1,000	3.13	1	Qpt	D	. 1
74	74	1,750	4.17	1	Opt	. \$	4
75	139	1,750	8.33	ī	Peis	S	4
76	316	3,500	8.33	- 1	Peis	S	6
77	109	1,250	6.25	1	Peis	Š	6
78	410	2,875	5.00	1	Pels	S	1
79	32	750	2.78	1	Pels	D	1
80	193	2,000	6.25	i	Peis	S	6
81	21	500	2.08	2	Peis	Ď	. 5
82	54	1,000	4.17	2	Peis	S	6
83	22	1,250	3.57	. 2	Peis	D	-
84	27	1,000	3.57	2	Peis	D	. 5
85	34	1,250	4.17	2	Peis	.S	6
86	46	1,250	5.00	2	Peis	S	6
87	183	3,250	12.50	2	Gr	S	. 6
88	96	2,250	6.25	2	Gr	S	. 6
89	190 468	2,250	8.33	2	Gr Gr	S	1
90	18	3,375 375	8.33	2	Gr De is	S	6
91			3.13		Peis	D	5
92	16	500	3.13	2	Peis	D	5
93	18	625	3.57	2	Peis	D	5
94	13	250	3.13	2	Pels	D	1
95	157	2,125	8.33	2	Peis	S	6
96	300	3,000	6.25	2	Peis	S	6

Table VI-30(3/4) POTENTIONAL SEDIMENT DISASTER SITES ON ARTERIAL ROAD

Location	Catchment Area(ha)	Slope/	Torrent	** Vegetation	Geology	Potential	disaste
NO.	M.eg(IIg)	Lengh(m)	Gradient*	Cover	uco logy	Type***	Rank
97	532	4,250	12.50	2	Pels	S	6
98	983	5,875	12.50	2	Pels	\$.	6
99	91	1,250	8.33	2	Qp1	S	6
100	21	500	2.50	2	Pets	D	5
101	36	750	3.13	. 2	Peis	D	5
102	22	625	2.27	2	Pels	D	5
103	483	4,250	3.57	2	Pets	D	. 5
104	109	750	2.50	2	Peis	D	: 5
105	118	1,750	3.13	2	Peis	Ď	5
106	104	875	2.50	2	Peis	D	. 5
107	659	5,000	6.25	2	Peis	S	6
108	348	3,000	6.25	5	Gr	S	6
109	75	875	2.27	5	Peis	D	3
110	68	1,125	2.50	5	Peis	D	3
111	147	2,250	2.27	5	Gr	D	3
112	65	1,250	2.08	5	Pets	D	. 3
	31	750	1.92	5	Pets	D	3
113	535	4,250	5.00	5	Gr	S	6
114		4,250 750		5	Peis	D	3
115	87		2.78			S	6
116	132	1,500	5.00	5	Peis		
117	181	1,625	6.25	5	Peis	S	6
118	50	1,000	5.00	5	Pels	S	6
119	169	2,000	12.50	5	Pels	S	. 6
120	700	4,500	8.33	5	Gr	S	6
121	82	1,250	4.17	5	Peis	\$	6
122	94	1,625	3.13	5	Peis	D	3
123	468	4,250	8.33	5	Pcm	\$	•
124	264	2,875	5.00	5	Peis	S	6
125	273	2,750	6.25	5	Pets	S	
126	58	1,000	3,57	5	Pcm	D	1
127	53	750	3.57	5	Pcm	· D	3
128	. 73	1,250	6.25	5	Peis	S	6
129	300	2,625	6.25	. 5	Peis	S	
130	64	750	3.57	. 5	Peis	D	
131	45	1,625	3.13	5	Pcm	D	3
132	58	1,625	3.57	5	Pcm	D	
133	313	2,750	3.57	- 5	Pcm	Đ	
134	33	750	2.50	5	Pcm	u, D	
135	33	750	2.50	5	Pcm	D	3
136	268	2,250	8.33	5	Pcm	S	(
137	321	3,000	5.00	1	Pet	S	
138	87	750	6.25	ì	Pet	S	
139	21	250	3.13	1	Pet	D	
	29			1	Pet	D	,
140		750	1.92		Pet	D	;
141	.79	1,375	2.08	1		ם	(
142	27	375	2.34	1	Pet	S	
143	238	1,625	6.25	1	Pet		
144	37	500	2.27	1.	Pet	D	

Table VI-30(4/4) POTENTIONAL SEDIMENT DISASTER SITES ON ARTERIAL ROAD

Location No.	Catchment Area(ha) -			** Vegetation	Geo logy	Potential	Disaste
	in outliny	Lengh(m)	Gradient*	Cover	4001093	Type***	Rank
145	81	750	3.13	1	Pet	D	5
146	63	375	6.25	. 1	Tmpa	S	1
147	76	500	2.78	. 1	Tmpa	D	5
148	24	500	1.92	1	Tmpa	D	- 5
149	9 ·	250	1.79	. 1	Tmpa	D	1
150	166	2,000	6.25	2	Tpev	S	- 6
151	36	1,250	8.33	. 2	Tpev	\$. 6
152	41	250	12.50	2	Tpev	S .	. 6
153	31	750	6.25	1	Tmi	S	. 6
154	21	750	6.25	. 1	Tmi	S	6
155	350	2,000	12.50	1	Tmi	S	5
156	34	875	3.57	1	Tmi	D	6
157	755	8,500	12.50	2	Qpt	S	6
158	474	5,375	6.25	2	Qpt	S	- 6
159	39	1,000	8.33	. 2	Tpev	S	6
160	197	2,000	12.50	. 2	Qpt	. S .	6
161	100	1,250	8.33	2	Qpt	S	. 6
162	277	4,000	12.50	2	Tpev	S	- 6
163	855	7.875	12.50	2	Qpt	S	. 6
164	•	_	-	1	Tmoa	8	: 1
165	-	_	_	1	Tmpa	В	1
166	- ,	••	· _	1	Tmpa	В	6
167		_		2	0pt	. В	6
168		-	-	2	Qpt	В	6
169		-	•	2	Qpt	. В	6
170	-	_	_	2	Pcm	В	1

Note: *: Gradient is expressed with a reciprocal.

**: Vegatation cover is classified as below:

- 1: High forest area
- 2: Low forest area
- 3: Cultivation area
- 4: Low shrab area
- 5: Grassland
- ***: Type of disaster is classified as below:
 - S: Sediment Flow
 - D: Debris Flow
 - F: Slope Failure
 - B: Bank Erosion

Table VI-31 COMPARISON OF APPLICABLE SABO DAM TYPE (ACTION PLAN)

Item	Gravity Dam	Fill Dam	Arch Dam	Steel Frame Dam	Concrete Block Dam
Structure	Concrete, rubble concrete or wet masonry type is applicable; overflow and debris flow are treated safely; and, the most conventional type	Embankment type of rock or earth; spillway is indispensable to discharge flood flows.	Thin concrete structure, all loads are supported by river bank and bed; concrete volume for dam body is smaller than that of gravity dam.	Gabion mattresses formed by steel bars are mounted; dam body is permeable and sustainable against deviation of dam foundation; dam height is limited to 15 m at maximum.	Dam body is piled up of concrete blocks; and hence permeable and sustainable against deviation of dam foundation; dam height is limited to 15 m at maximum.
and	Compacted sand and gravel or rock foundation; countermeasures are required for piping in the fine-sand foundation.	Foundation treatment is indispensable; wide river section is most applicable for this type.	Dam base and abutment shall be composed of hard and massive rock.	This type is applicable for the sites of river deposit consisting fine and coarse sand and gravel.	This type is applicable for the sites of river deposit consisting fine and coarse sand and gravel.
later ia Is	Concrete or rubble concrete	Earth or rock, and concrete for spillway	Concrete	Steel bars and boulders or cobble stones	Concrete
Construc- tion lethod	Multi-stage const- ruction is possible since concrete may withstand over- flowing.	Construction is generally difficult due to complicated structure.	River diversion is indispensable by means of diversion channel or tunnel.	Rapid and easy; river diversion and foundation treatment are simple.	Rapid and easy; river diversion and foundation treatment are simple.

Table VI-32 TOPOGRAPHICAL AND GEOLOGICAL CONDITIONS OF SABO DAM SITES (ACTION PLAN)

I tem	Description		C-5 Dam Site	N-1 Dam Site
Riverbed	Width	60m	40m	100m
	Elevation	EL. 161,4 m	EL. 469.6 m	EL. 850.3 m
Dam Crest	Width	105m	80m	165m
:	Elevation	EL. 181.0 m	EL. 480.0 m	EL. 870.0 m
Right Bank	Geology	Fresh outcrop of fine sandstone	Terrace Deposit	Gneiss with schist
	Slope	1/1.1	1/4.0	1/0.8
·	Land Use	Forest	Pan American Highway, field	Sugarcane field
eft Bank	Geology	Debris deposit	Bluffs of black	Debris deposit
		(Muck of PAN-AM Highway)	schist	:
4	Slope	1/1.75	1/0.1	1/3.3
	Land Use	Banana plantation	Existing road	Waste land
Riverbed condition	Estimated Depth to Bedrock	More than 10 m	More than 10 m	More than 10 m
- 11	Gravel Diameter	10 - 30 cm	10 - 50 cm	10 - 30 cm
	Bearing Capacity	More than 50 t/m2	More than 50 t/m2	More than 50 t/m2
Remarks			Dam height	Construction of a
4 4 4		•	should be less than	20 m high dam is
f		-	10 m judging from	possible if the
		debris deposit on		debris deposit on
		the left bank is	condition	the left bank is removed

Table VI-33 STRUCTURAL DIMENSIONS OF PROPOSED SABO DAMS (ACTION PLAN)

Item	C-1 Dam	C-5 Dam	N-1 Dam
Location	Chama River 3.0km upstream of confluence with Mocacay River	Chama River 500m downstream of Chama No. 4 Bridge	Nuestra Senora River 300m upstream of confluence with Chama River
Dam Site			
- River Gradient	1/110	1/100	1/30
- River Width	160 m	70 m	100 m
- Design Flood	2,300 m3/s	1,950 m3/s	610 m3/s
(1/100)		## 	
		CA1 Evene Dece	Rubble Concarete
)am type	Rubble Concrete (Gravity Dam)	Steel Frame Dam	(Gravity Dam)
		£	
Height	22 m	9 m	22 m
.	(20 m)*	(8 m)*	(20 m)*
Length			
- Top	160 m	234 m	180 m
- Bottom	100 m	65 m	125 m
		•	
Overflow Depth	5.4 m	5.9 m	2.3 m

^{* :} Figures in parentheses indicate the height of dam crest above riverbed

Table VI-34 STRUCTURAL DIMENSIONS OF PROPOSED CONTINUOUS LOW DAMS (ACTION PLAN)

4631446-556

Item	Mucusas	Mucusuru	Mucusos
Number of Low Dams	10	5	: . 3
Average River			.a. (a) 40 40 40 40 40 40 40 40 40 40 40 40 40
Gradient	1/20	1/10	1/10 - 1/6.7
Average River			•
Width	30 m	20 m	35 m
Design Flood (1/100)	30 m3/s	60 m3/s	20 m3/s
Dam Type	Wet Masonry	Wet Masonry	Wet Masonry
and the second of the second	(Gravity) Dam	(Gravity) Dam	(Gravity) Dam
Dam Height	4 m	4 m ·	4 m
	(3 m)*	(3 m)*	(3 m)*
Dam Length		• • •	
- Top	27 ~ 68 m	25 - 58 m	22 - 39 m
- Bottom			10 - 20 m
			en transfer
Overflow Section		٠	
Donah	5.6 m	5.6 - 6.0 m	5.6 m
- Depth	••• m		•••

^{* :} Figures in parentheses indicate the height of dam crest above riverbed.

Table VI-35 STRUCTURAL PLAN OF PROPOSED RETAINING WALLS (Action Plan)

No.	Location	Length (m)	Height (m)	Type *
1.	Mesa de Virgen	200	2.0	Concrete
2.	La Honda	150	2.0	Concrete
3.	La Palmita	150	2.0	Concrete
4.	La Providencia	50	2.0	Concrete
5.	Cacute	70	2.0	Concrete
6.	La Vega **	200	2.0	Concrete
	lotal	820		***

Note *: Leaning-to-slope type with a slope of 1.0:0.5.

Table VI-36 STRUCTURAL PLAN OF PROPOSED REVETMENT (Action Plan)

Location/River	Length (m)	Keight (m)	Type *
El Pedregal/ Chama	20	4.5	Wet masonry
Cacute/ Chama	160	4.5	Wet masonry
Tampaul/ Chama	60	4.5	Wet masonry
El Salado/ Chama	60	4.5	Wet masonry
La Vega*/ Chama	400	4.5	Wet masonry
La Vega/ Qd. El Diablo	20	4.5	Wet masonry
	720	के कहा कहा कहा हुआ अबह कहा गाँउ का का कर गाँउ का का का का का	
	El Pedregal/ Chama Cacute/ Chama Tampaul/ Chama El Salado/ Chama La Vega*/ Chama	El Pedregal/ Chama 20 Cacute/ Chama 160 Tampaul/ Chama 60 El Salado/ Chama 60 La Vega*/ Chama 400 La Vega/ Qd. El Diablo 20	El Pedregal/ Chama 20 4.5 Cacute/ Chama 160 4.5 Tampaul/ Chama 60 4.5 El Salado/ Chama 60 4.5 La Vega*/ Chama 400 4.5 La Vega/ Qd. El Diablo 20 4.5

Note *: Slope of revetment is generally set at 1.0:0.5 to protect the rever bank from scouring by flood

^{**:} Around the confluence between the Chama and the Nuestra Senora Rivers.

^{**:} La Vega is located at around the confluence of the Chama and Nuestra Senora rivers.

Table VI-37 Relationship Between Grain
Size and Justin's Critical Velocity

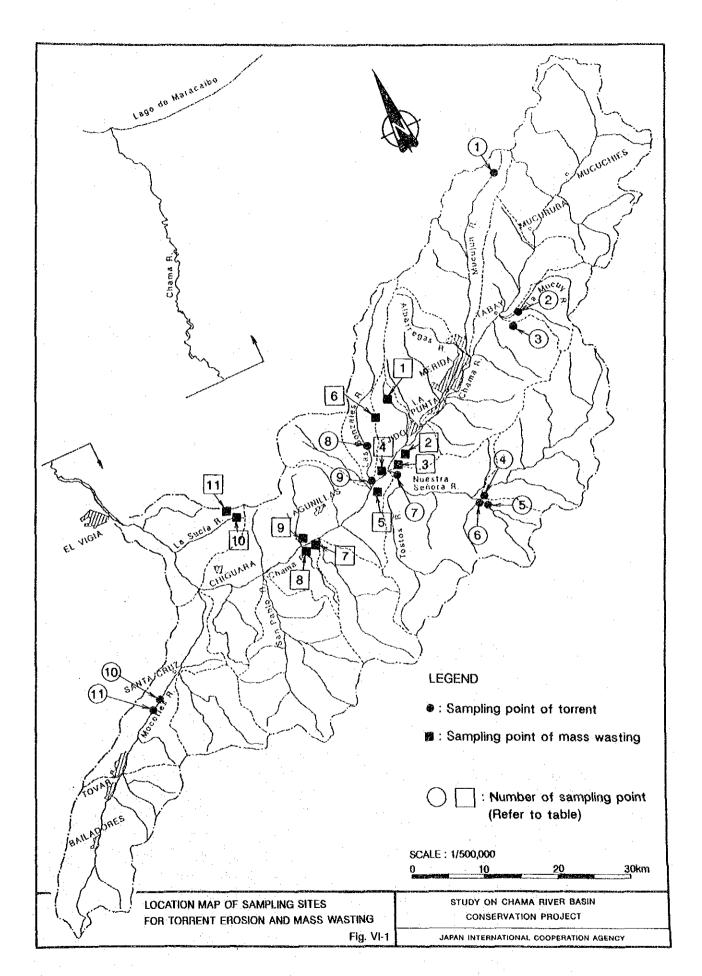
Grain Size	Justin's
drain 2176	Critical Velocity
(mm)	(cm/sec)
5.00	22.86
3.00	17.71
1.00	10.22
0.80	9.14
0.50	7.23
0.30	5.60
0.10	3.23
0.08	2.89
0.05	2.29
0.03	1.77
0.01	1.02

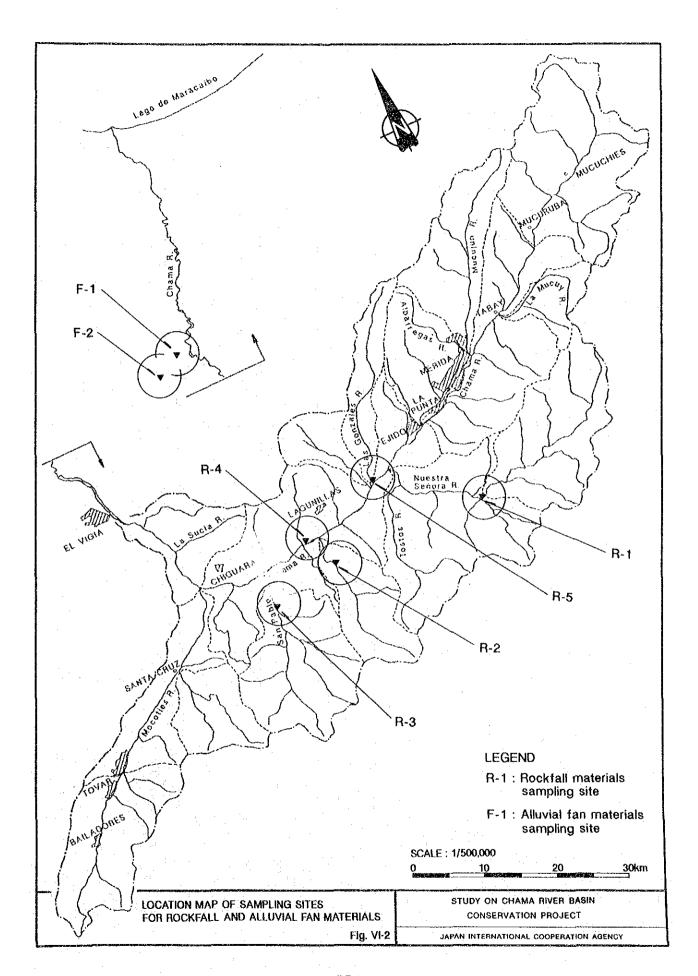
Table VI-38 COEFFICIENT OF PERMEABILITY FOR VARIOUS RIVERBED MATERIALS

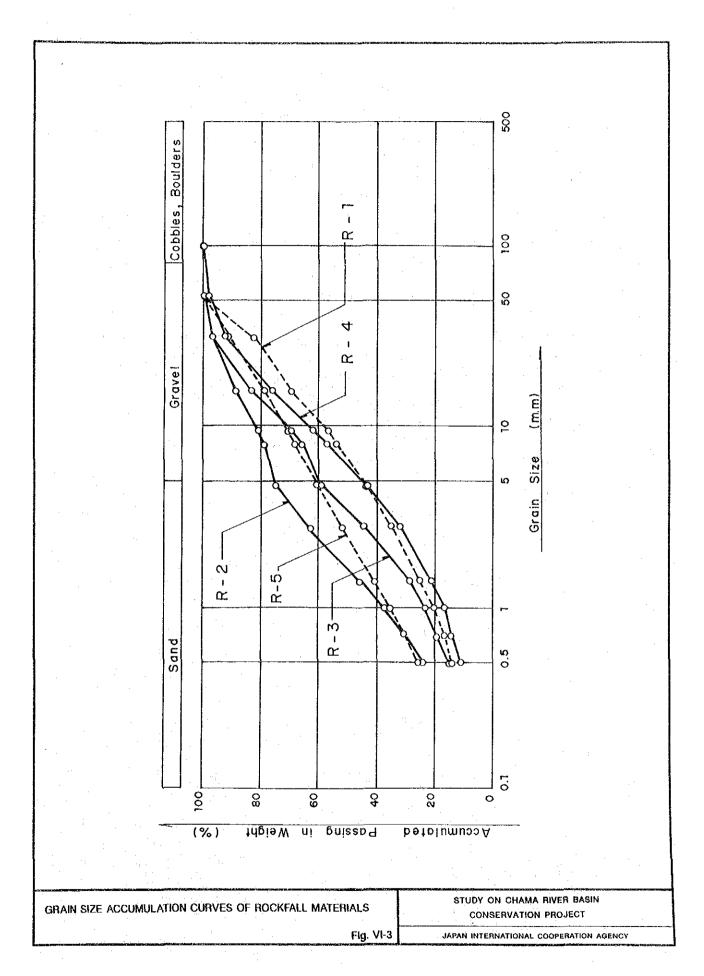
	Coefficient of Permeability (cm/s)											
	10 ³	10 ² 10 ¹	10 ⁰	10 ⁻¹	10-2	10-3	10 ⁻⁴	10-4	10 ⁻⁵	10 ⁻⁶	10 ⁻⁷	10-8
Reverbed Materials		Gravel	 	Sand, Layor o and gr				ne sand lt, etc	-	į	Clay, Honperm soil	eable

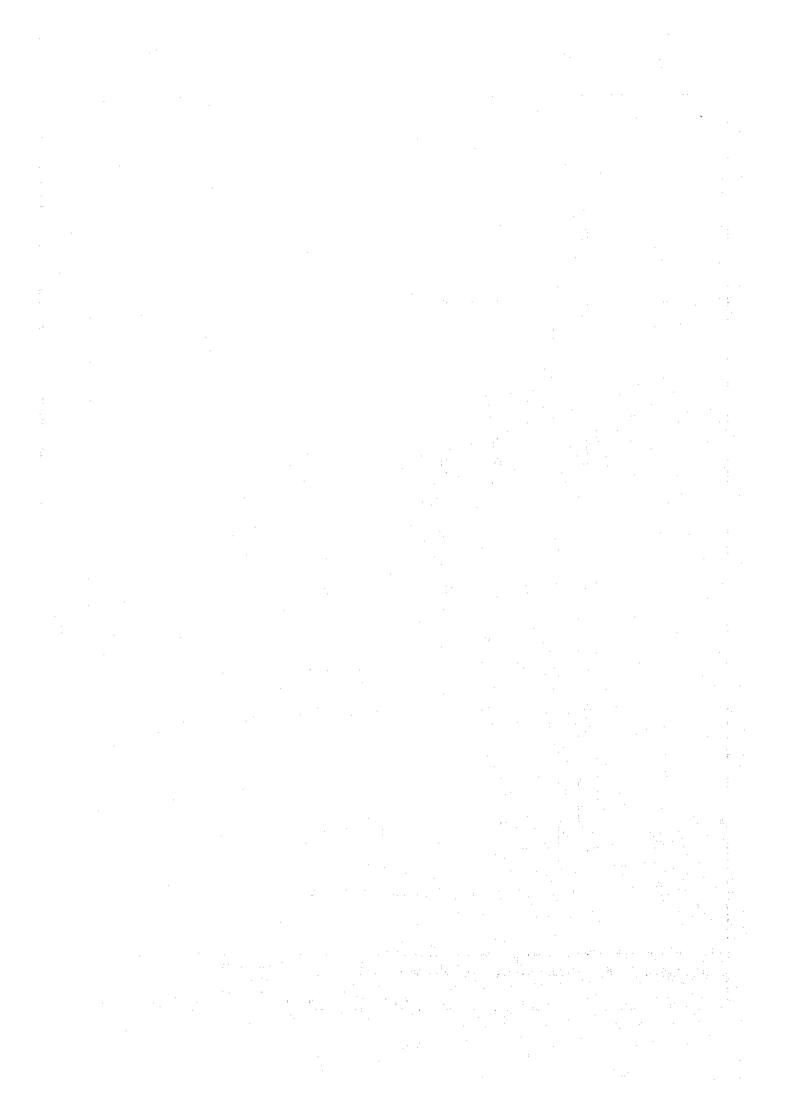
Table VI-39 Porosity Depending on Geologic Stratum

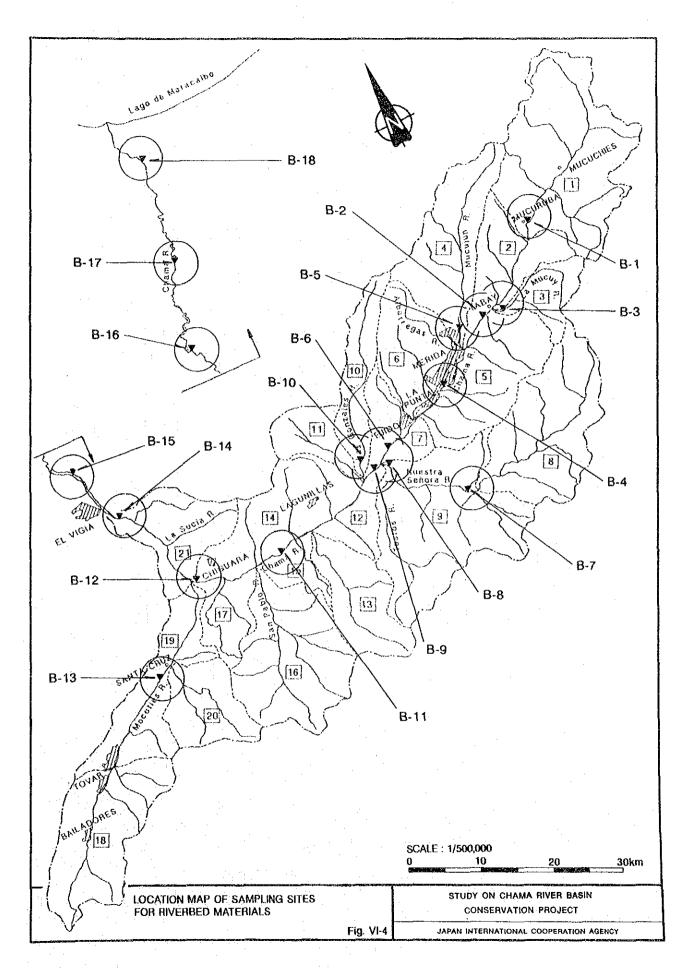
Geologic Stratum	Porosity	Water Content	Effective Porosity	
Stratum	(%)	(%)	(%)	
Alluvium	25	10	15	
Granu le	35	20	15	
Sand-Dune	30-35	10-15	20	
Mad	45-50	30	15-20	
Diluvium	30	10-15	15-20	
Sand	35-40	5-10	30	
Loam	50-70	30-50	20	
Clay	50-70	45-60	5-10	

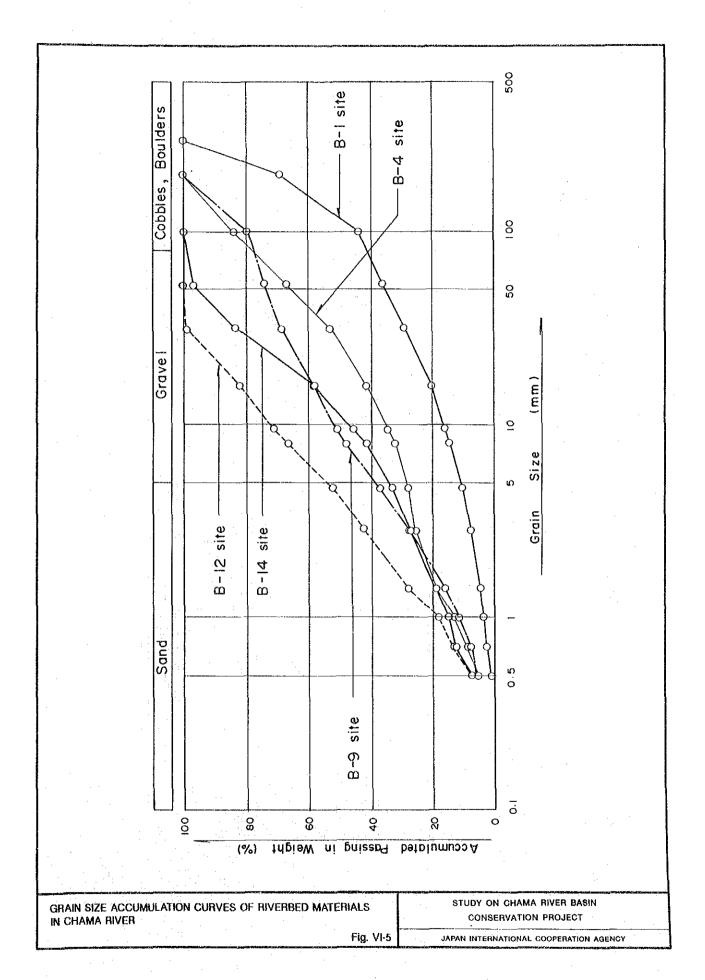


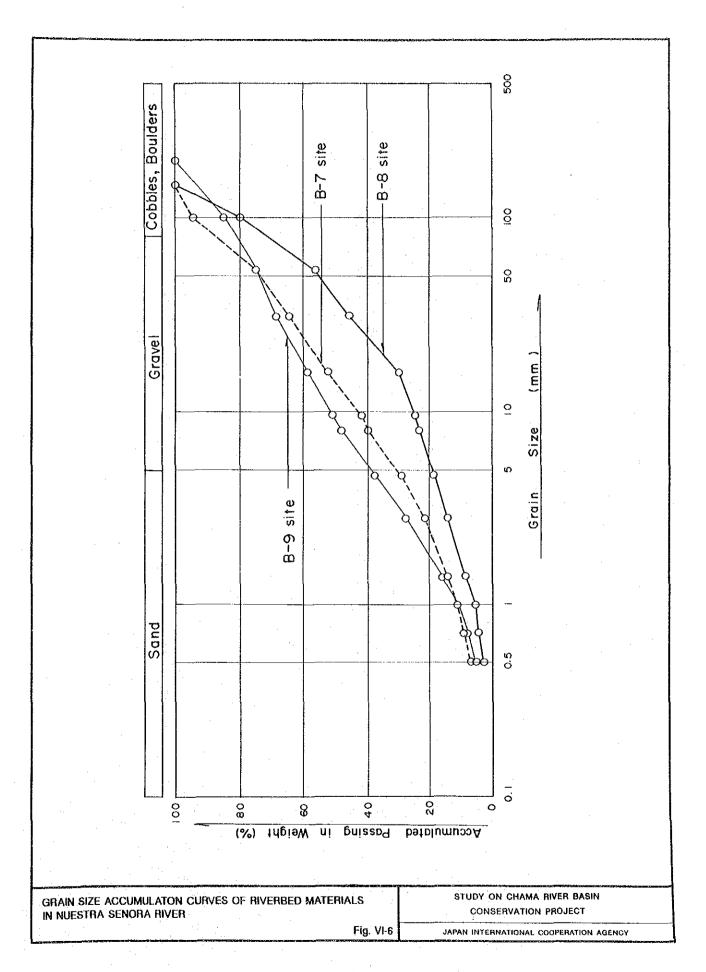


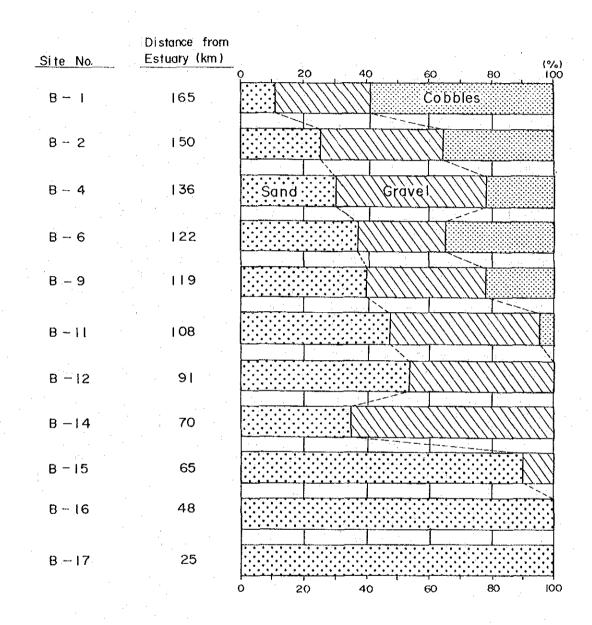










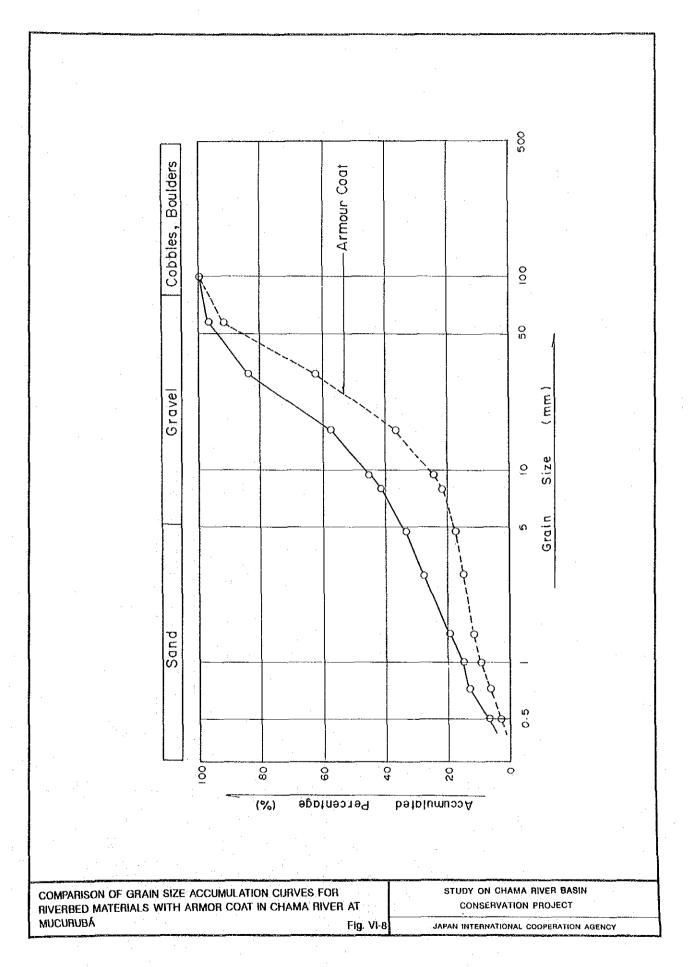


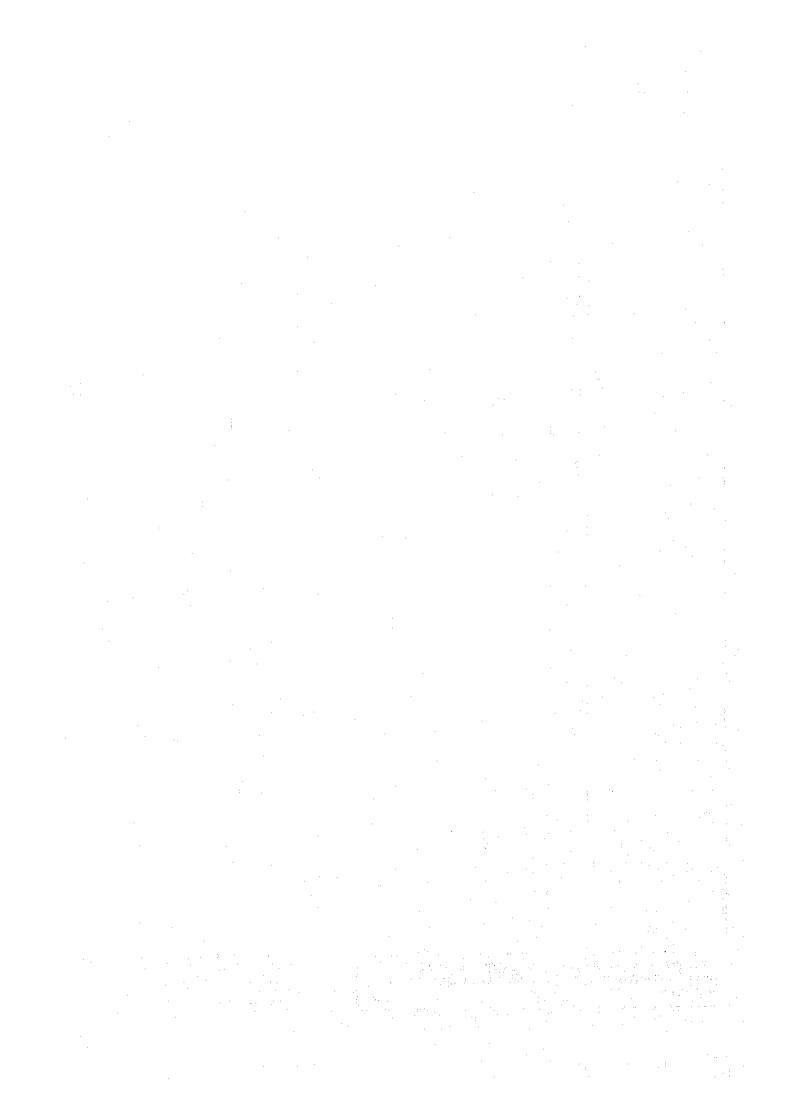
COMPARISON OF GRAIN SIZE DISTRIBUTION FOR RIVERBED
MATERIALS IN CHAMA RIVER
Fig. VI-7

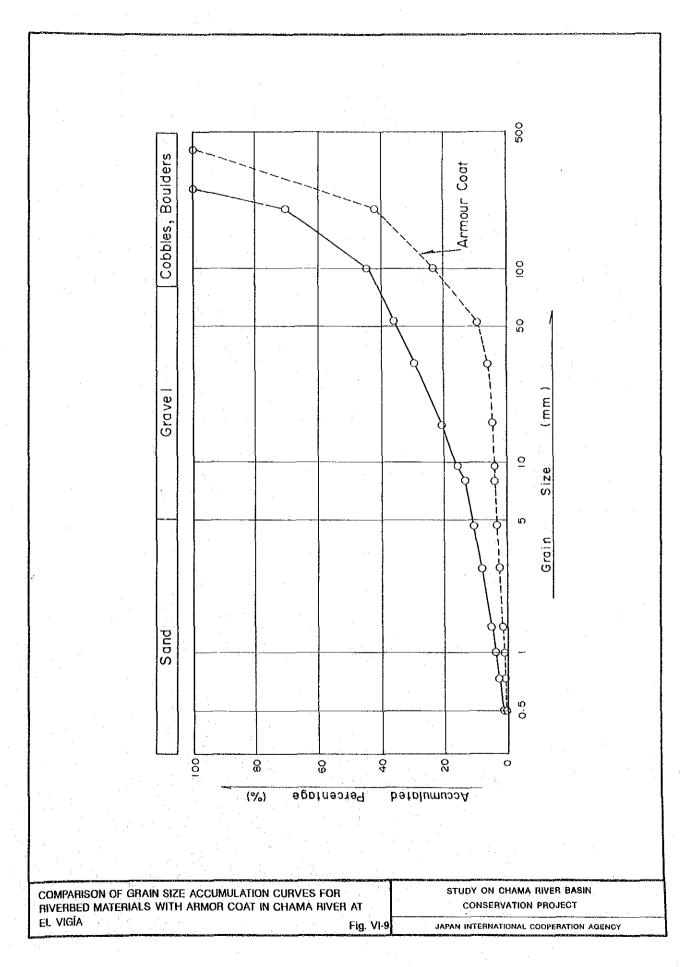
STUDY ON CHAMA RIVER BASIN
CONSERVATION PROJECT

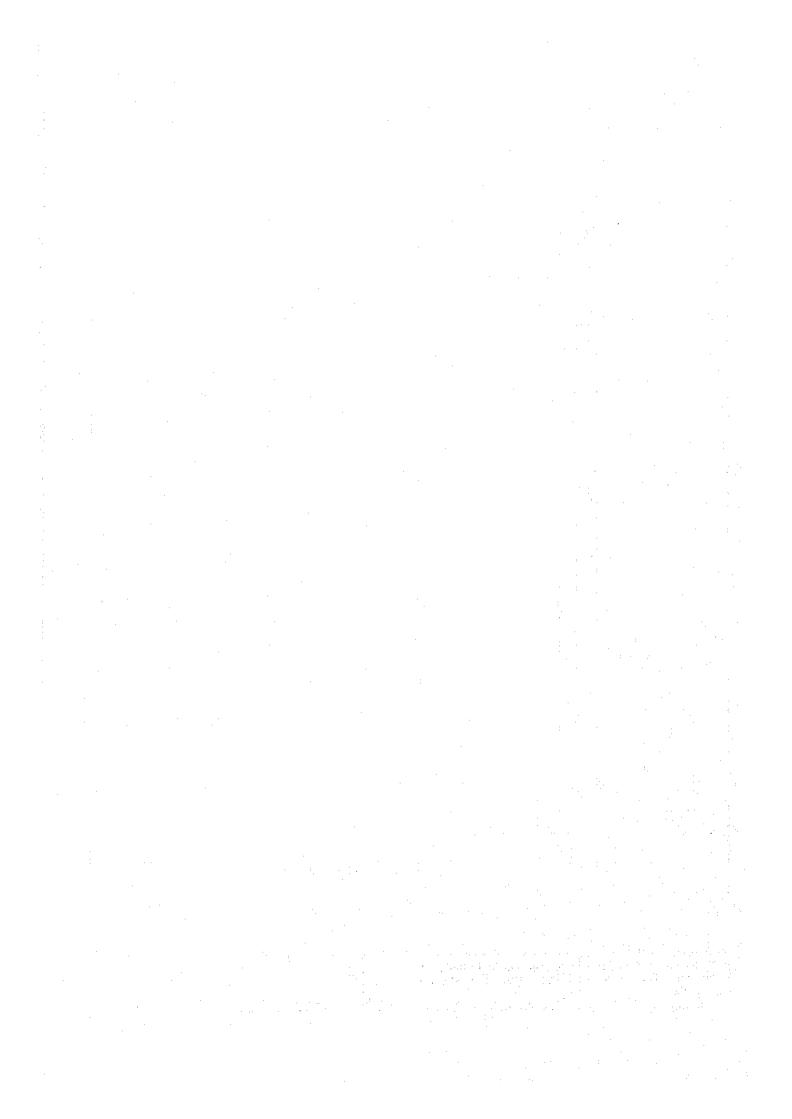
Fig. VI-7

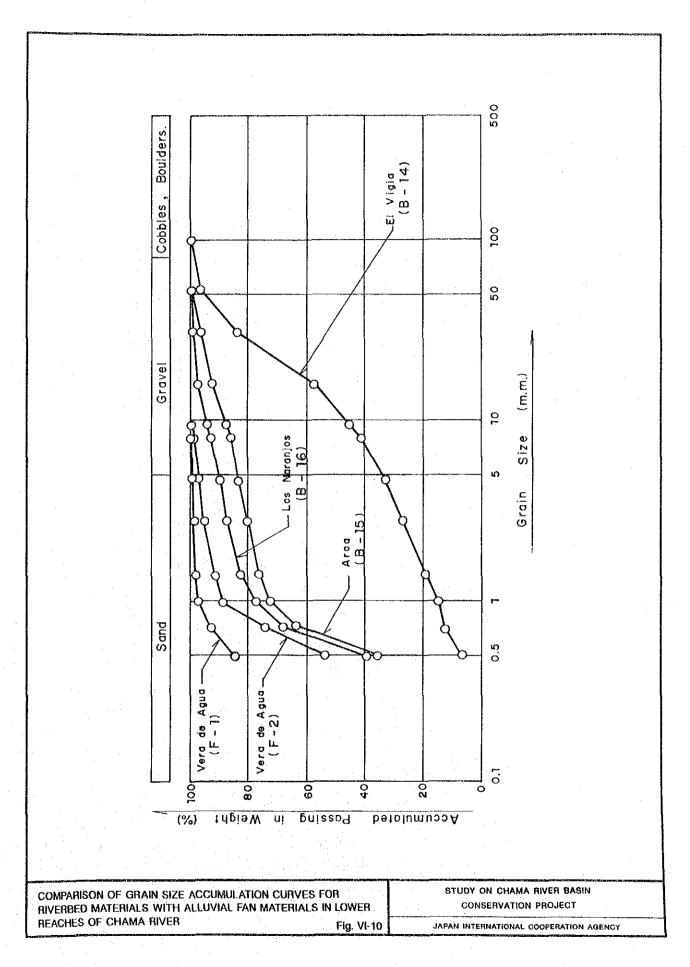
JAPAN INTERNATIONAL COOPERATION AGENCY

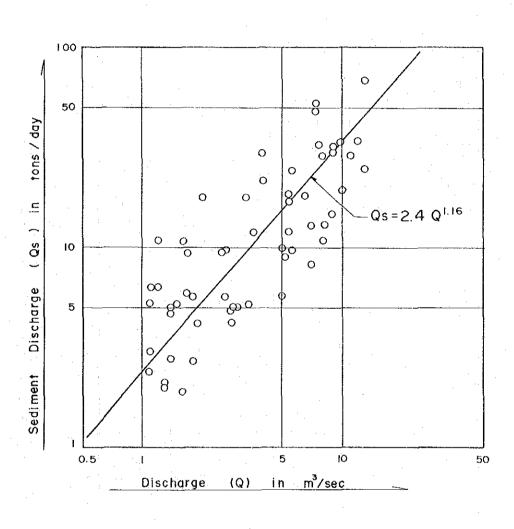










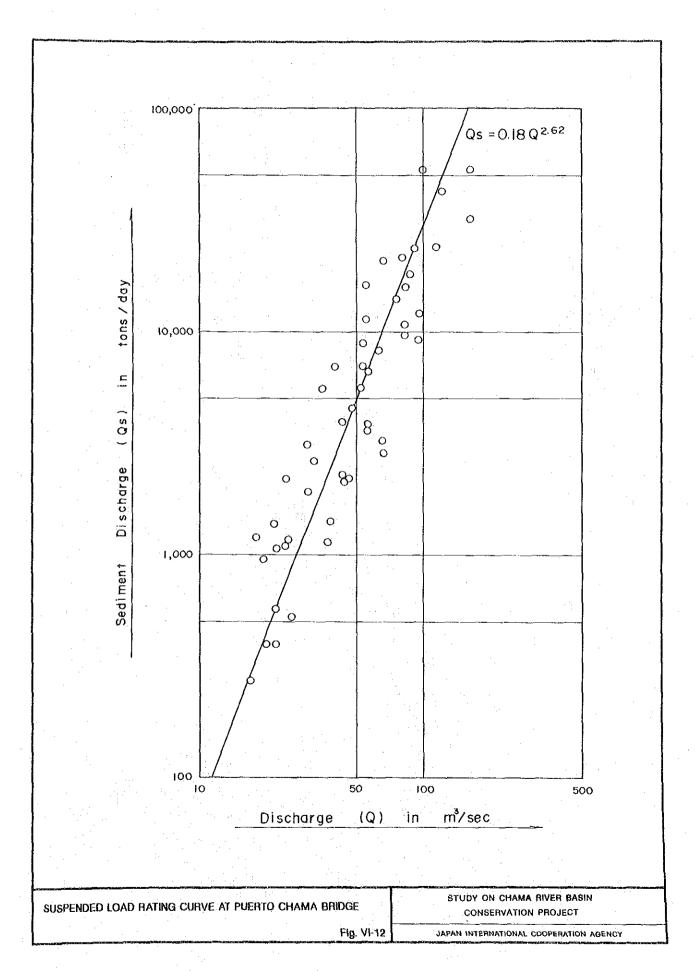


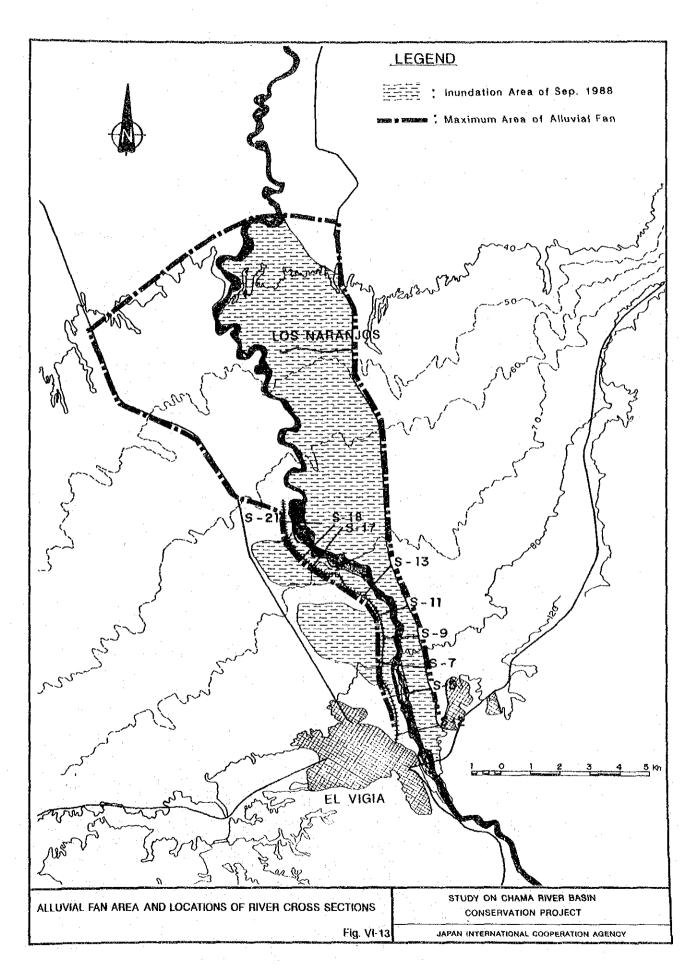
SUSPENDED LOAD RATING CURVE AT MUCURUBÁ STATION

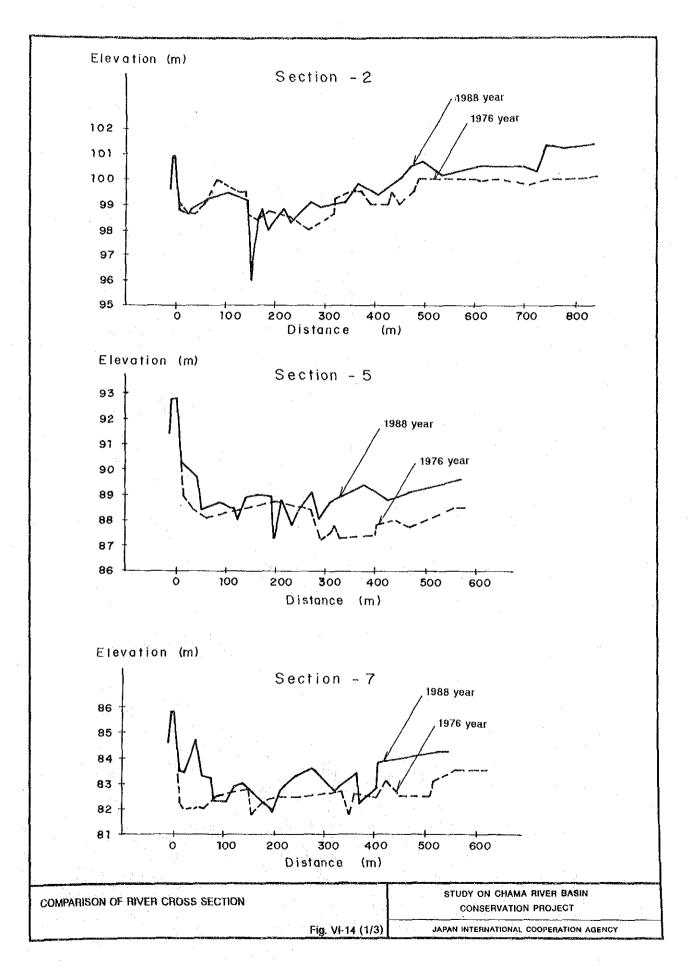
STUDY ON CHAMA RIVER BASIN
CONSERVATION PROJECT

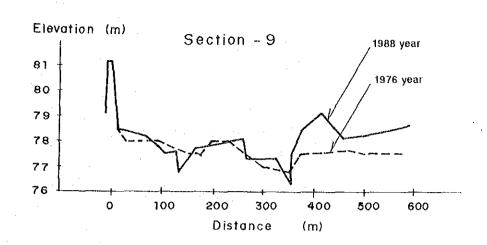
Fig. VI-11

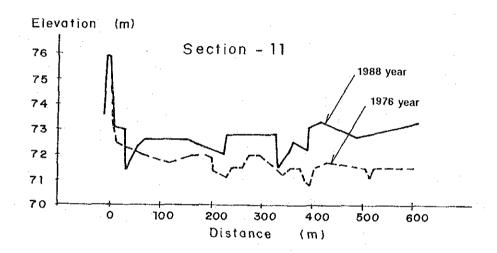
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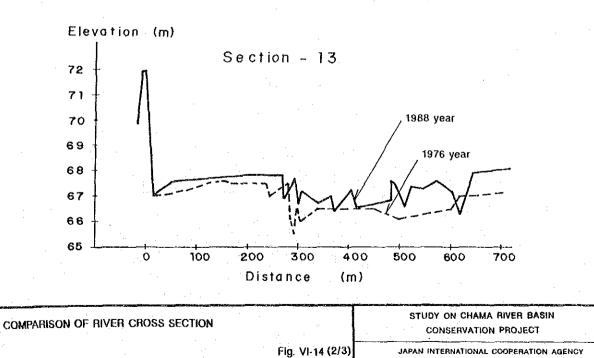


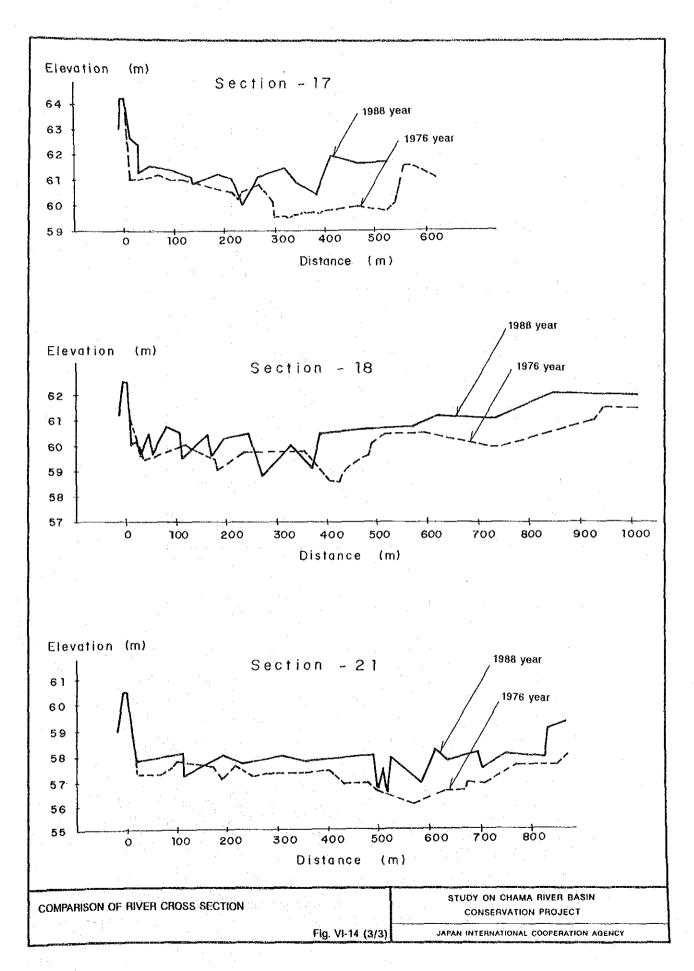


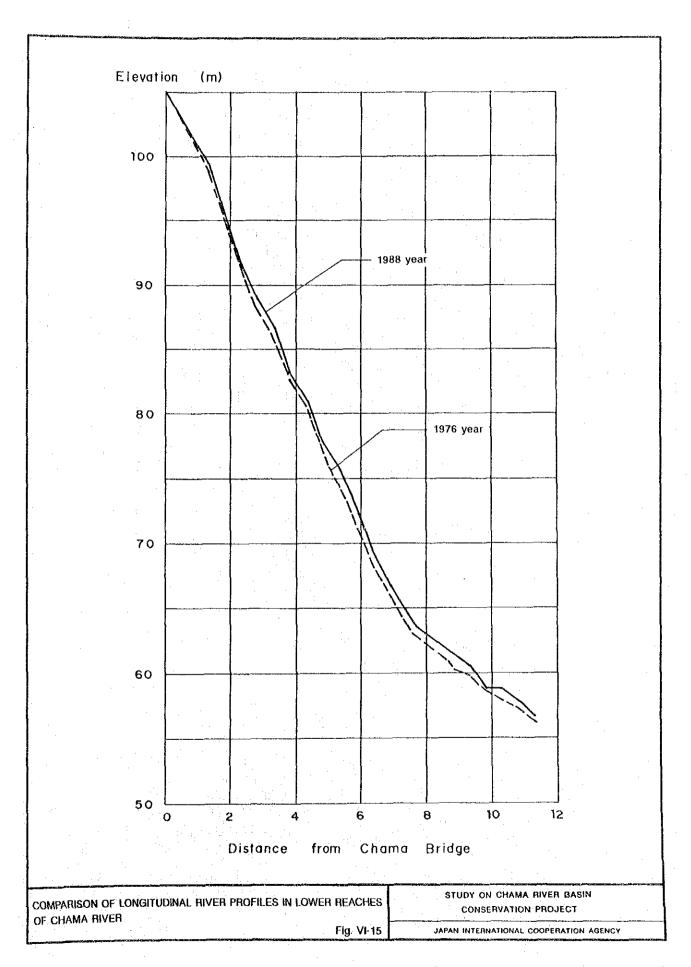


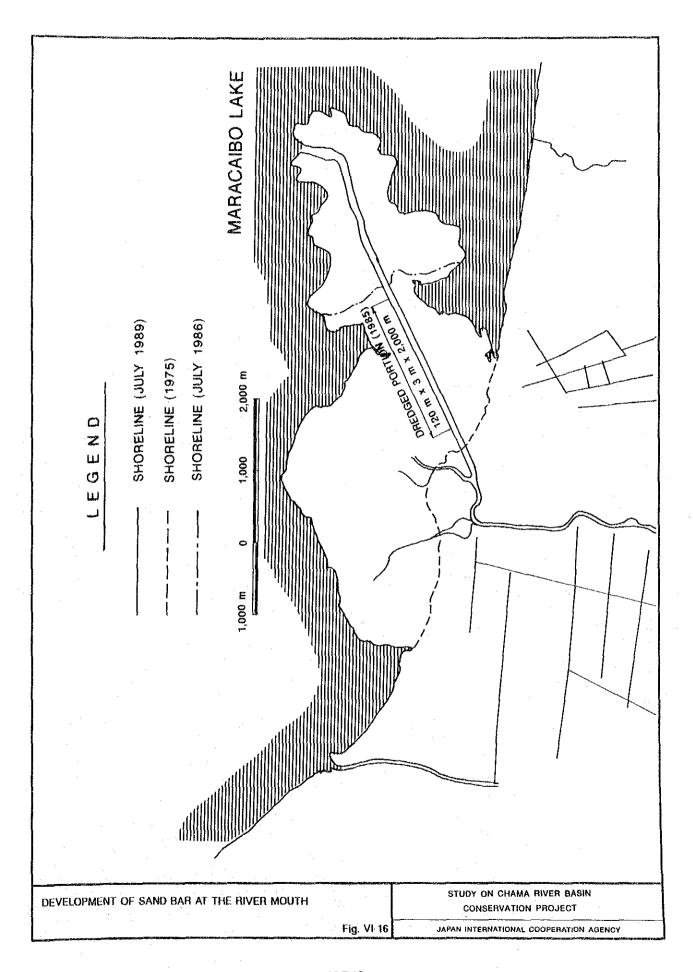


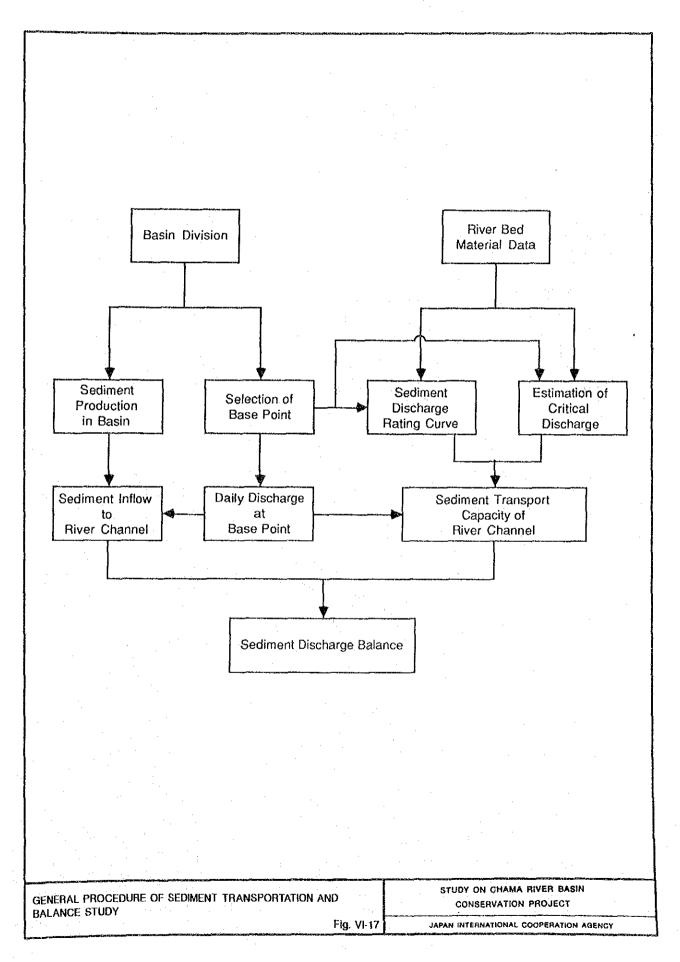


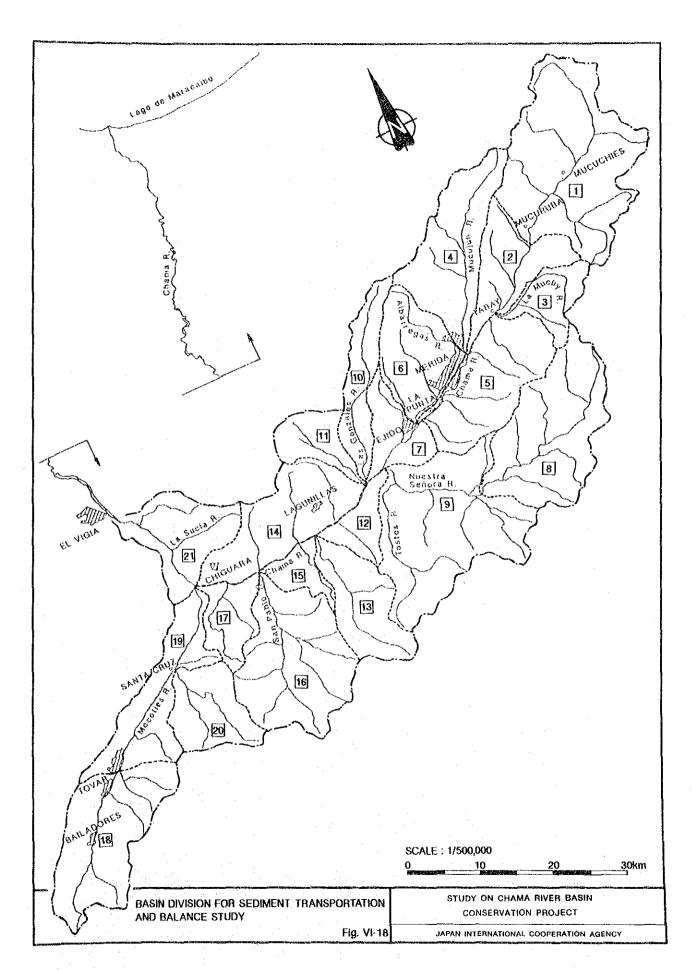


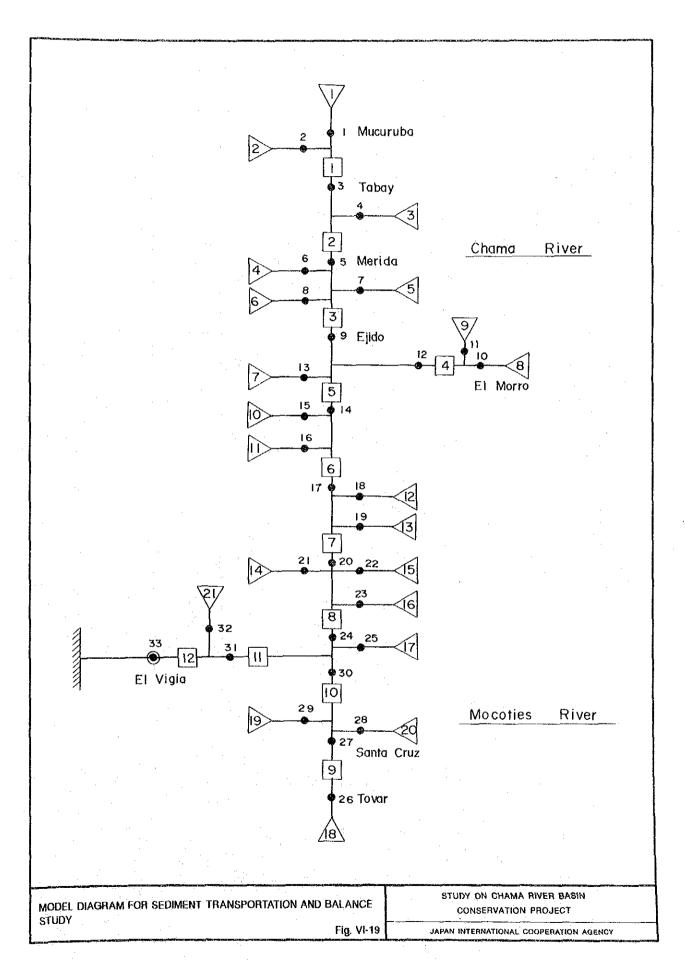


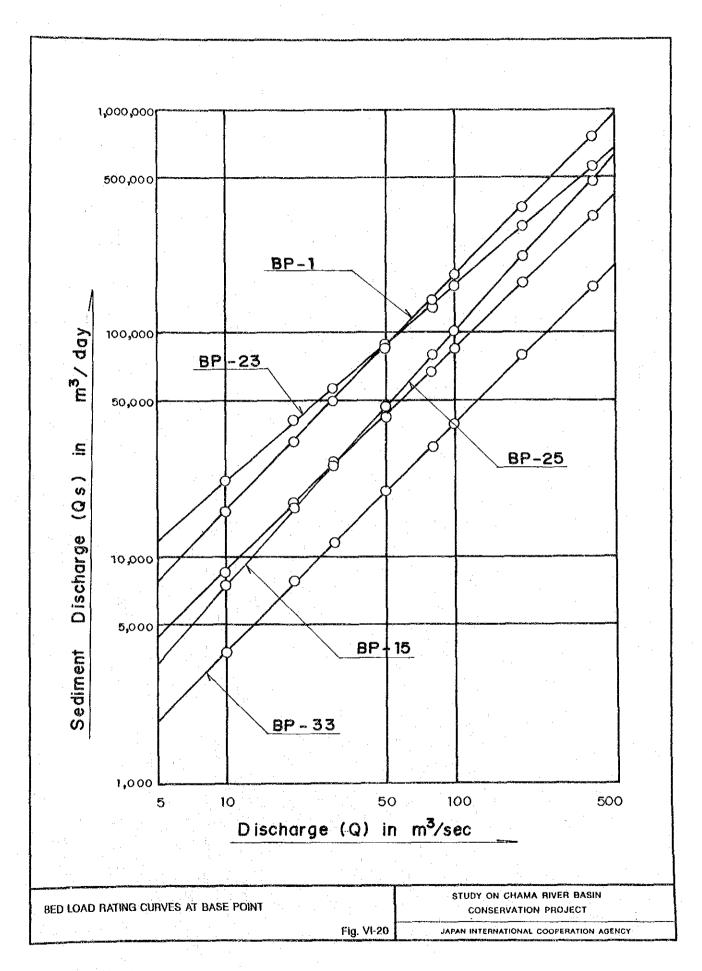


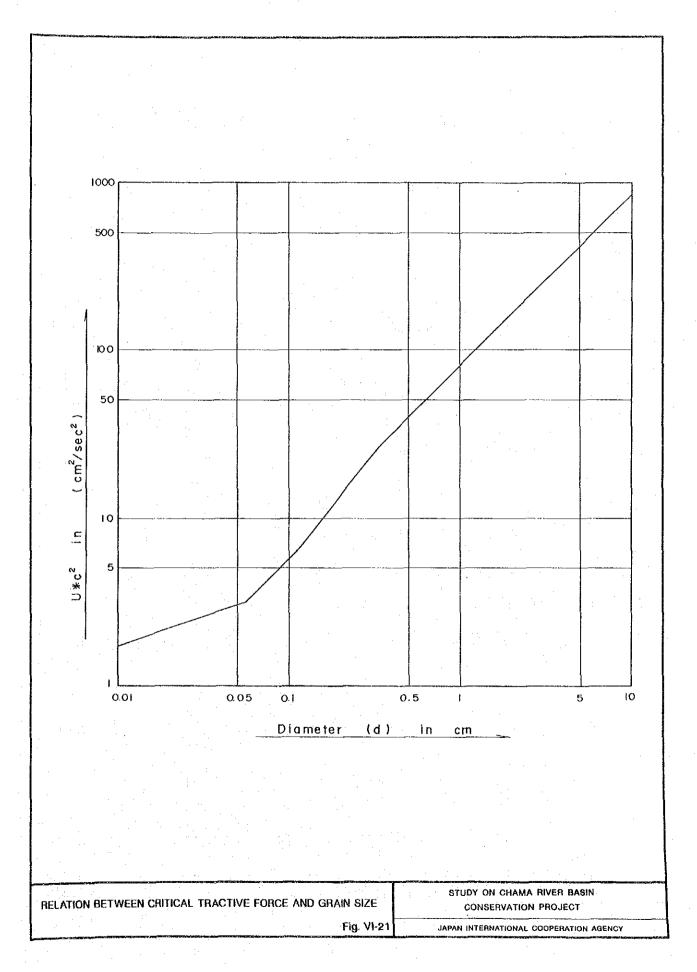


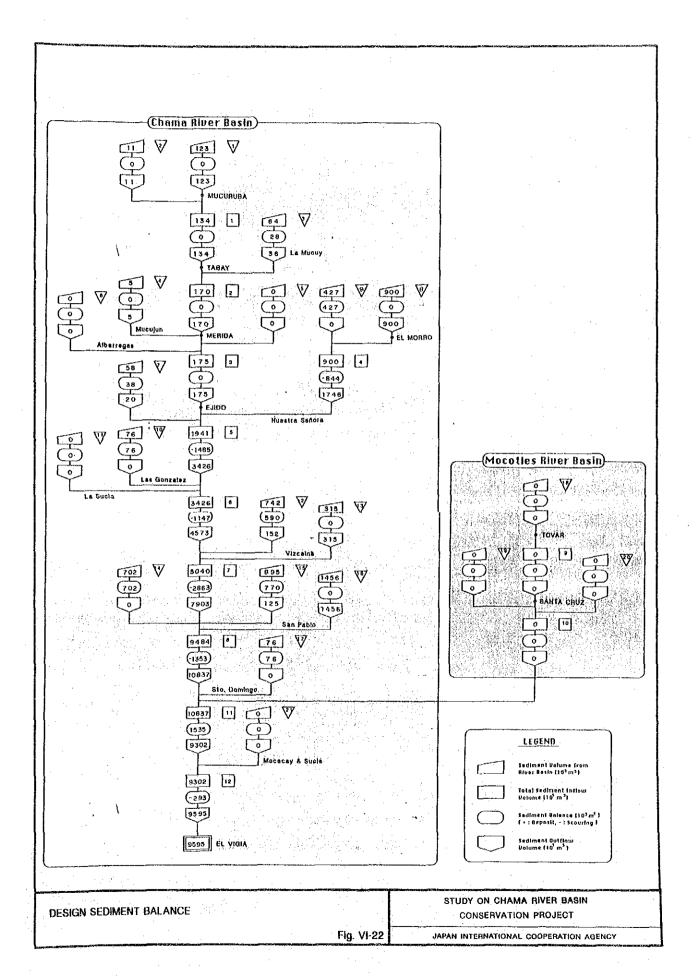


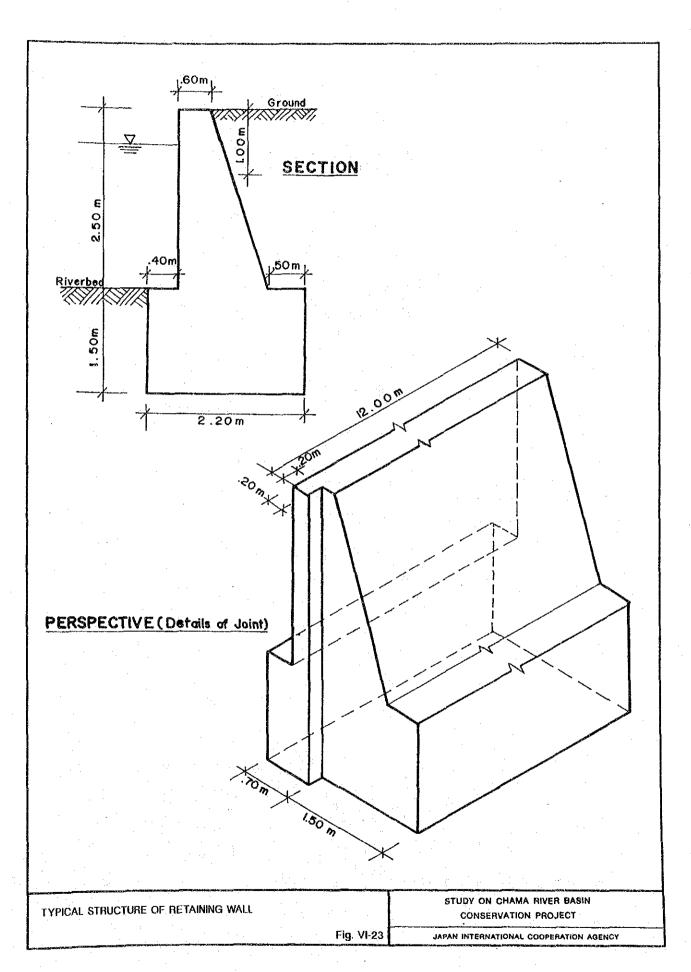


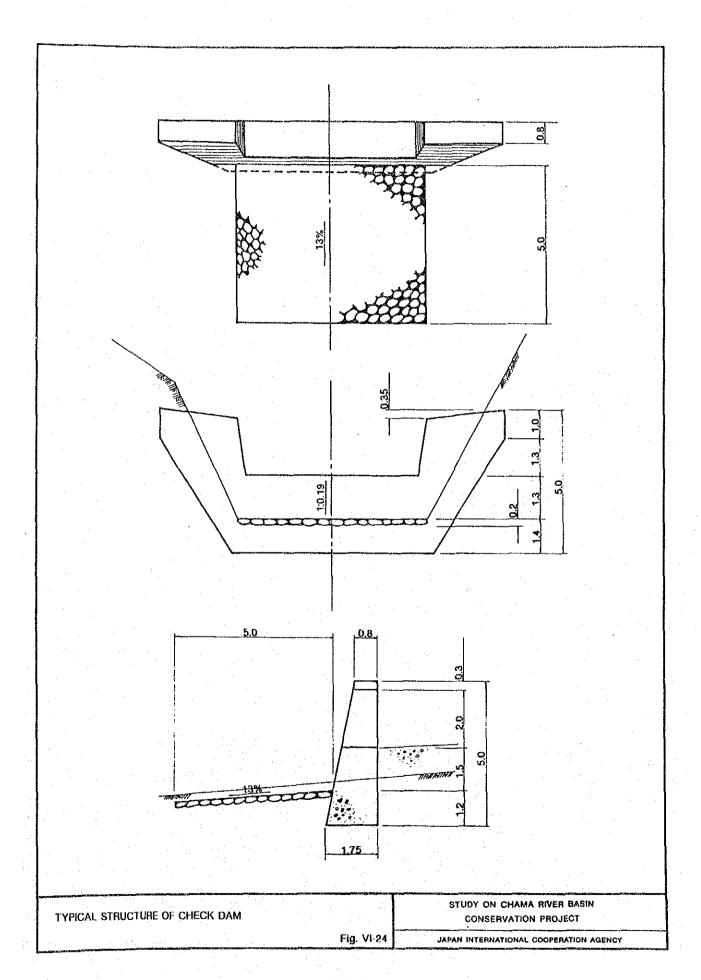


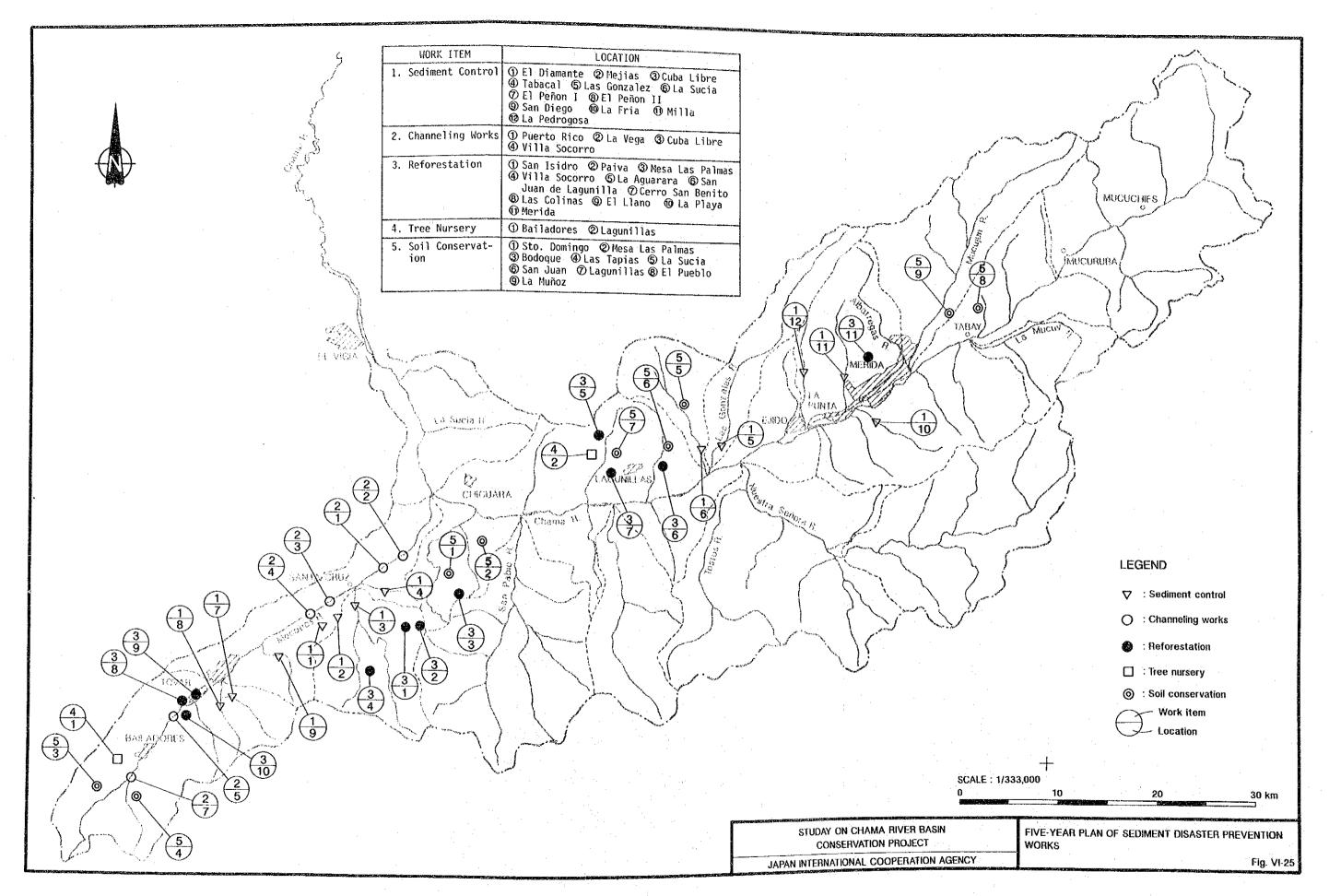


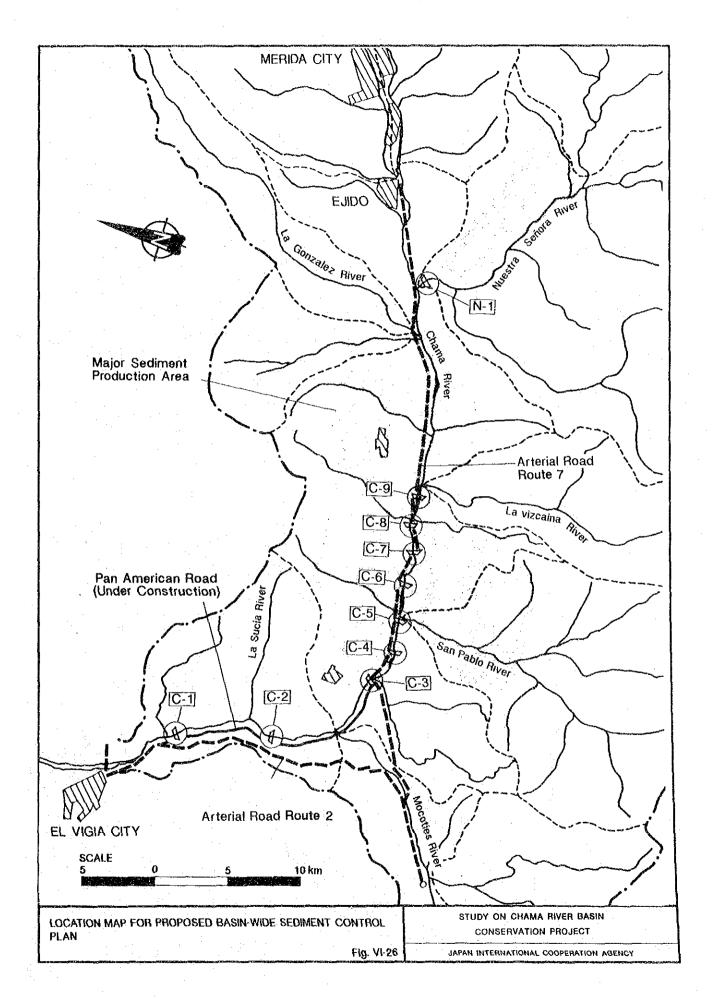


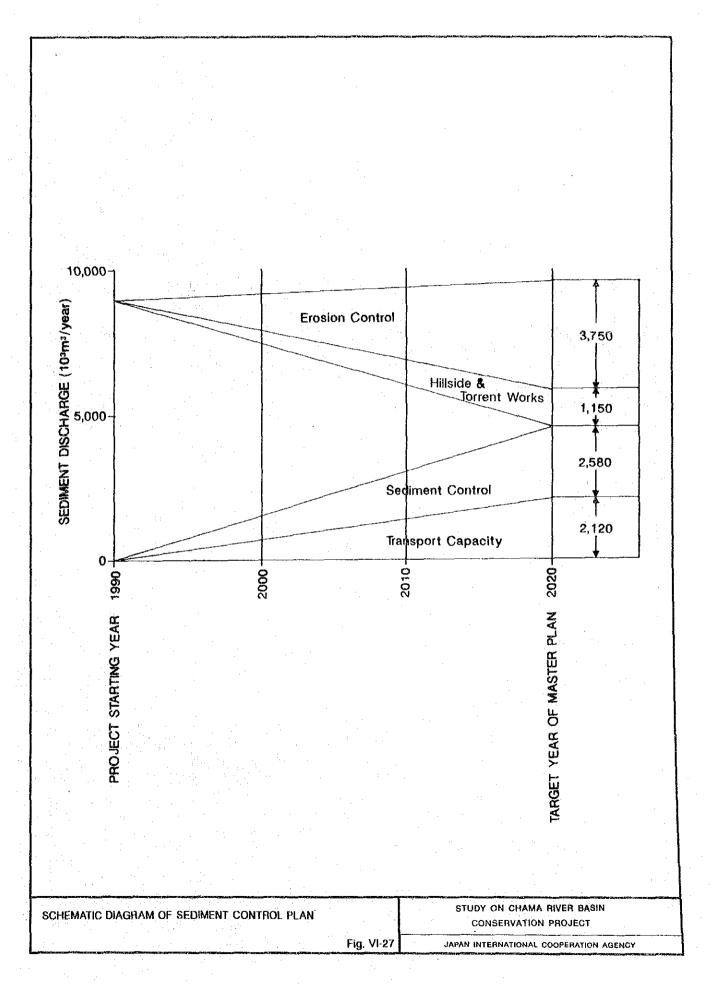


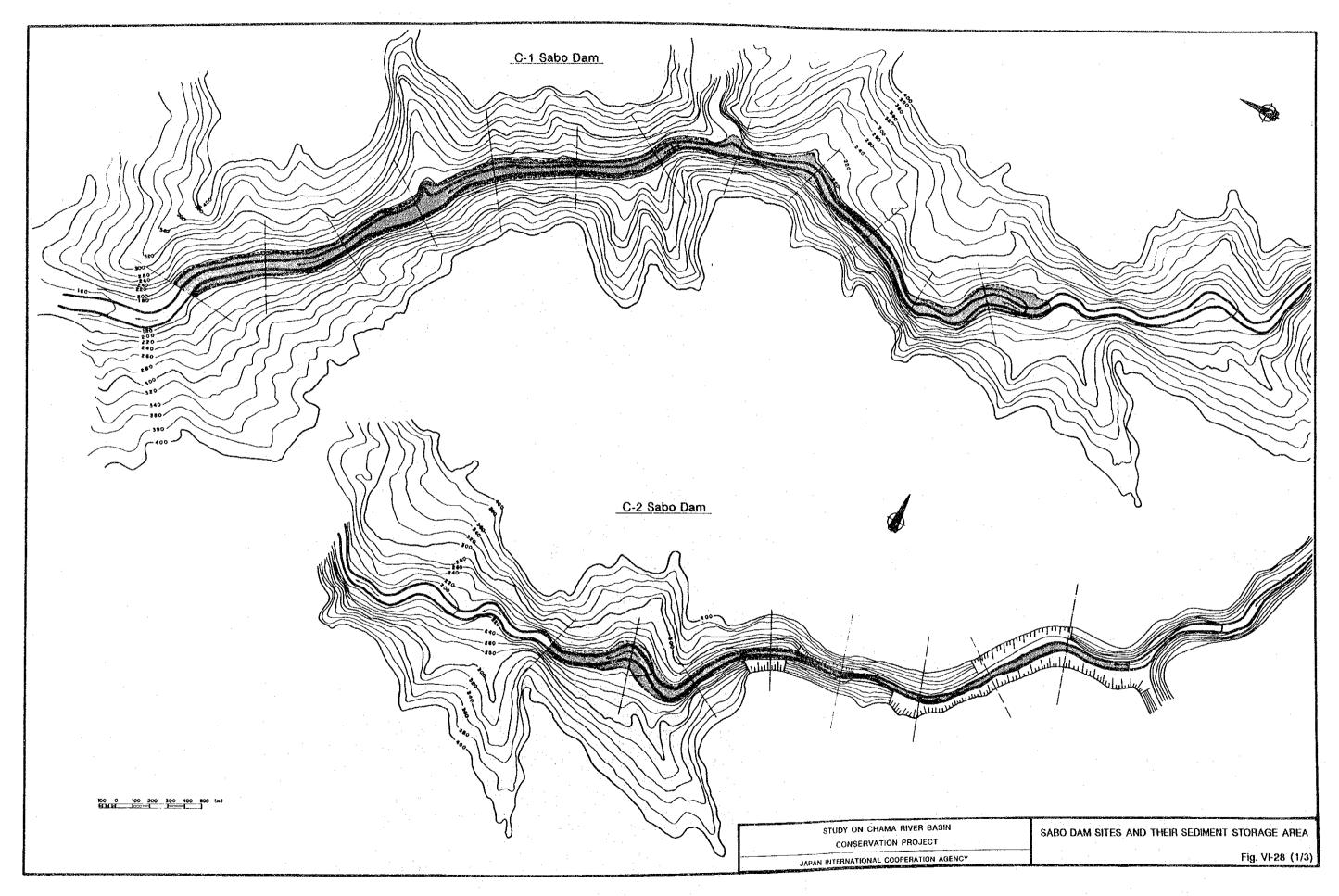


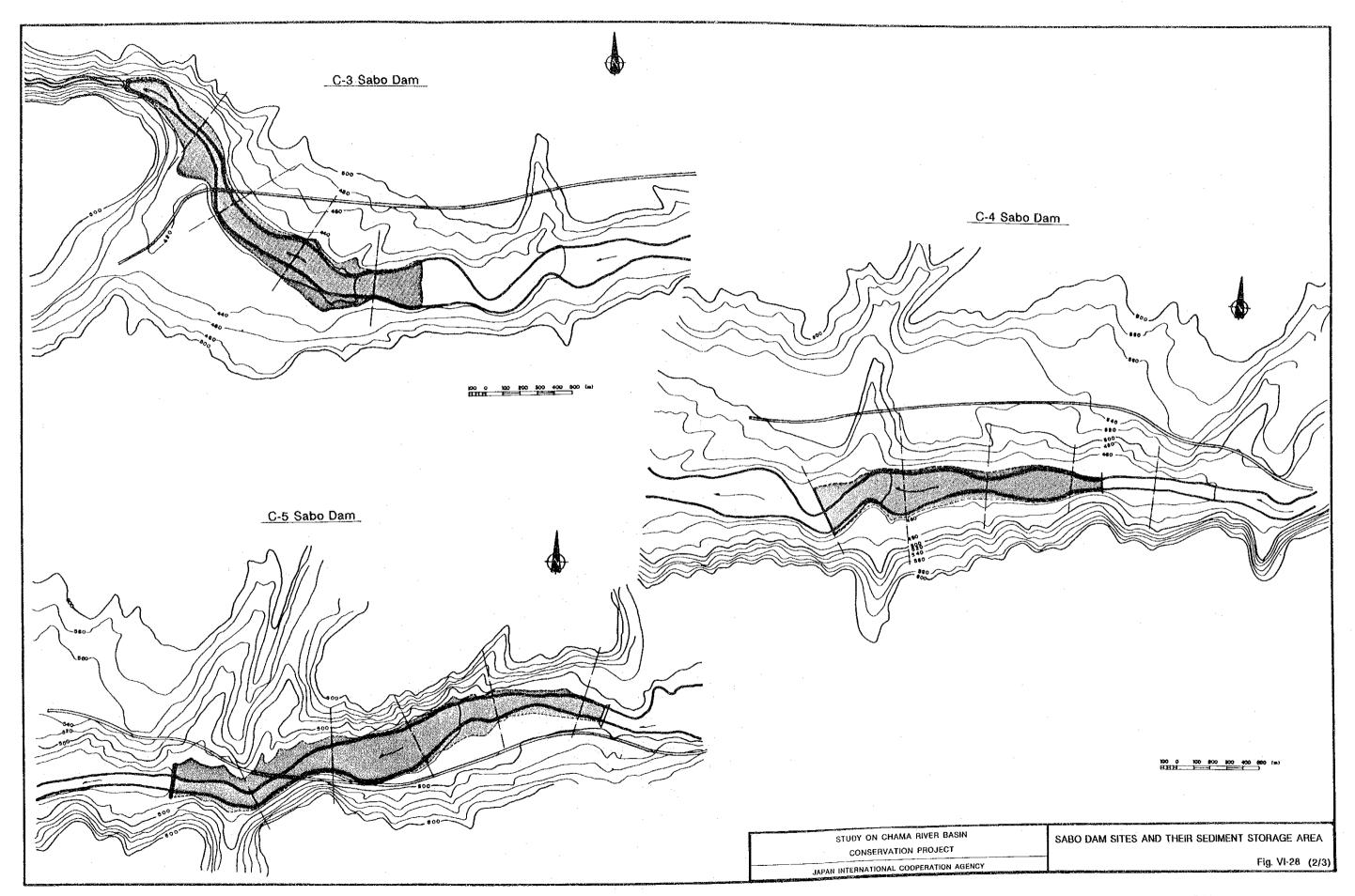


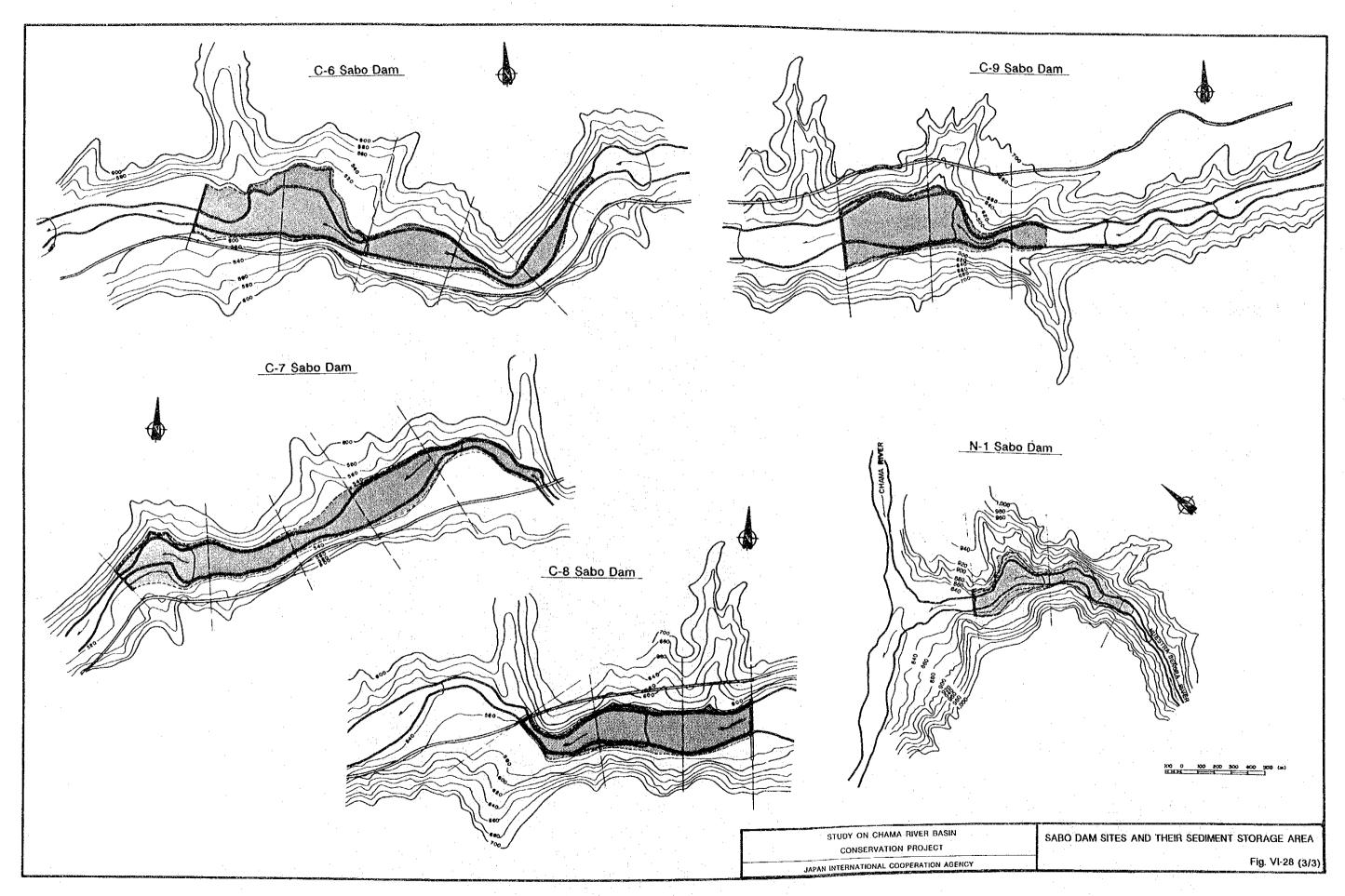


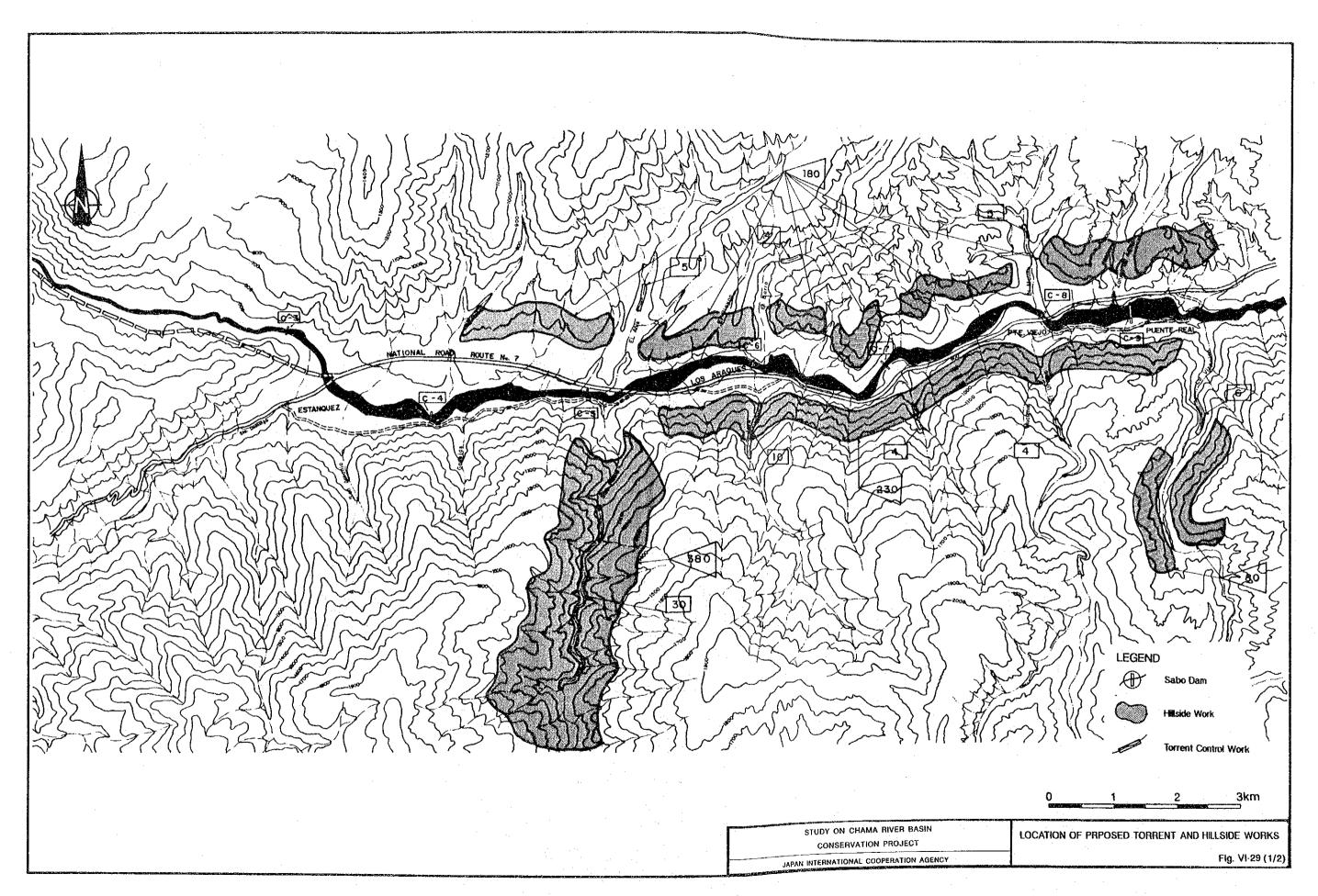


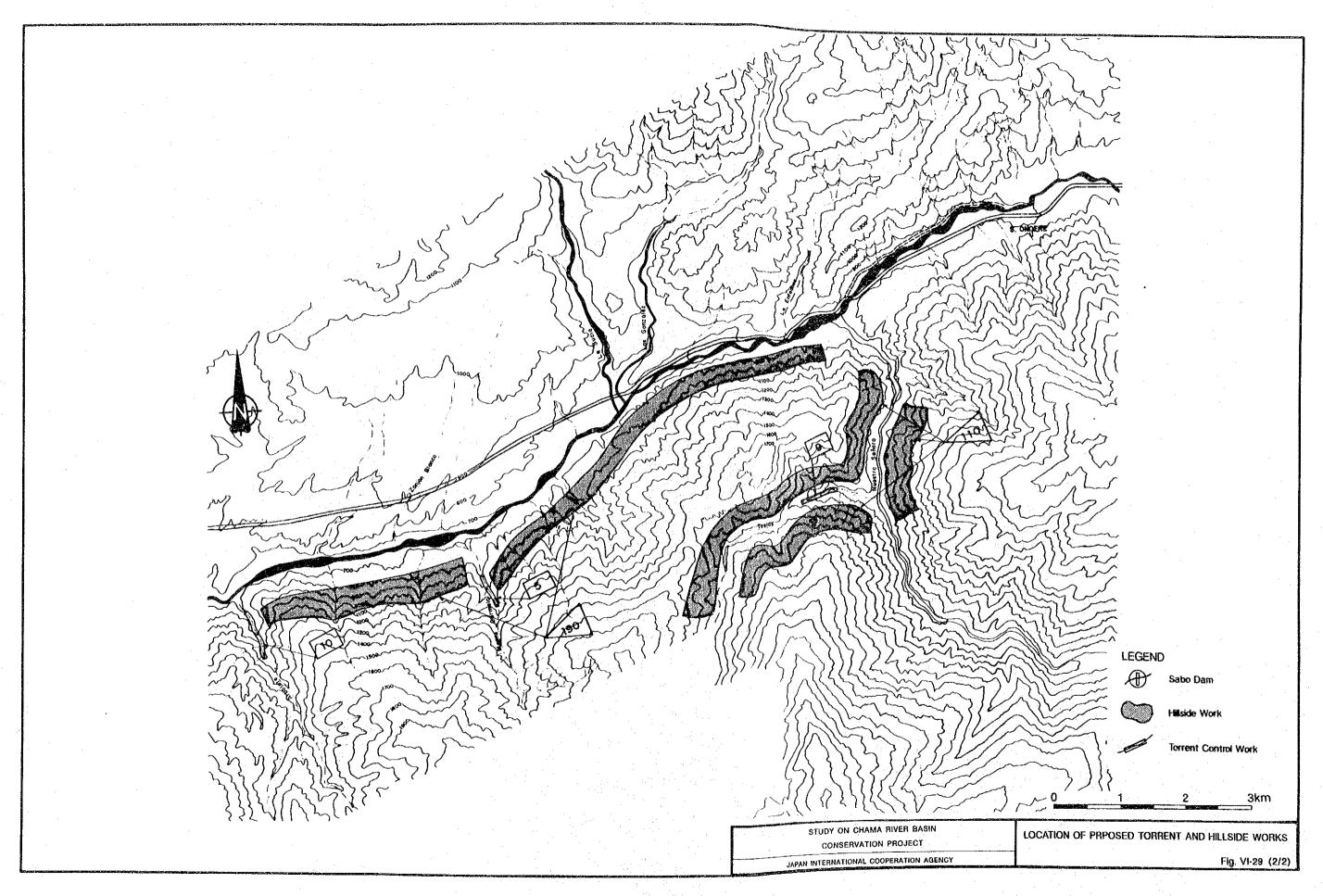


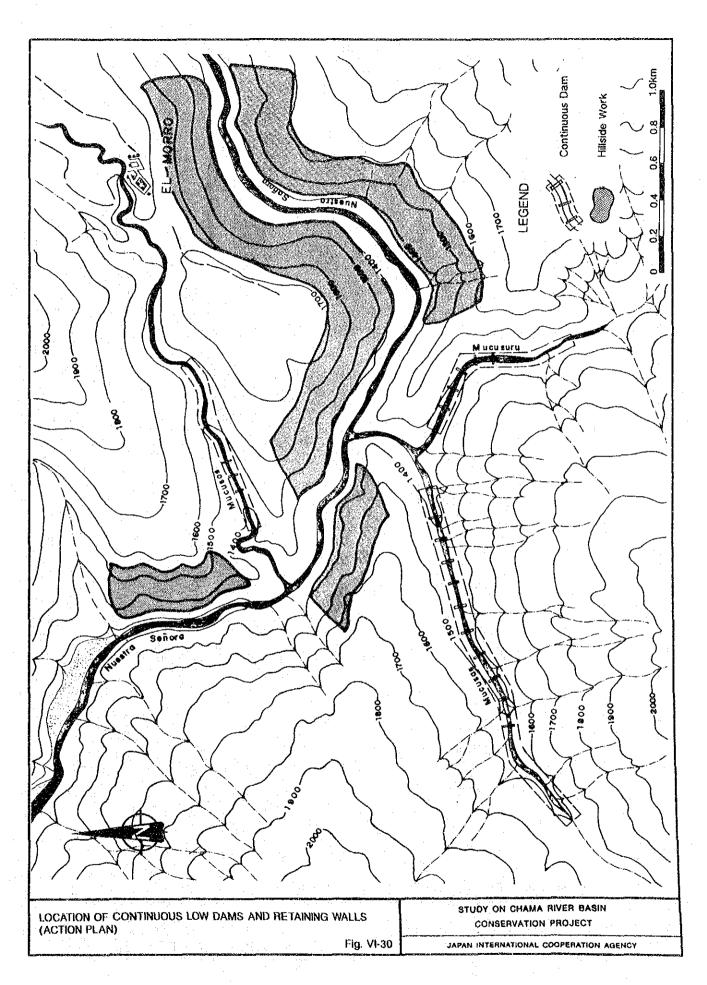


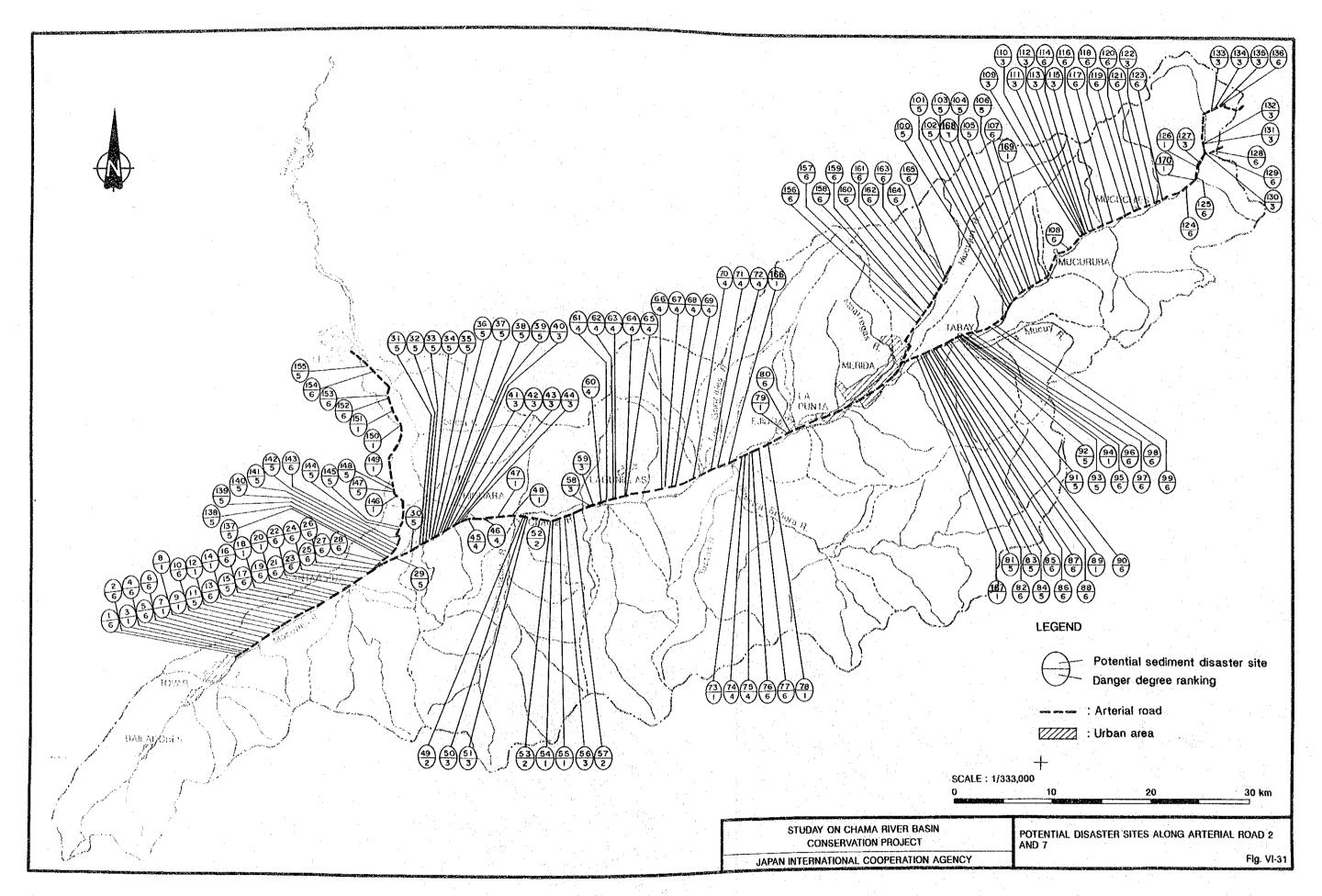


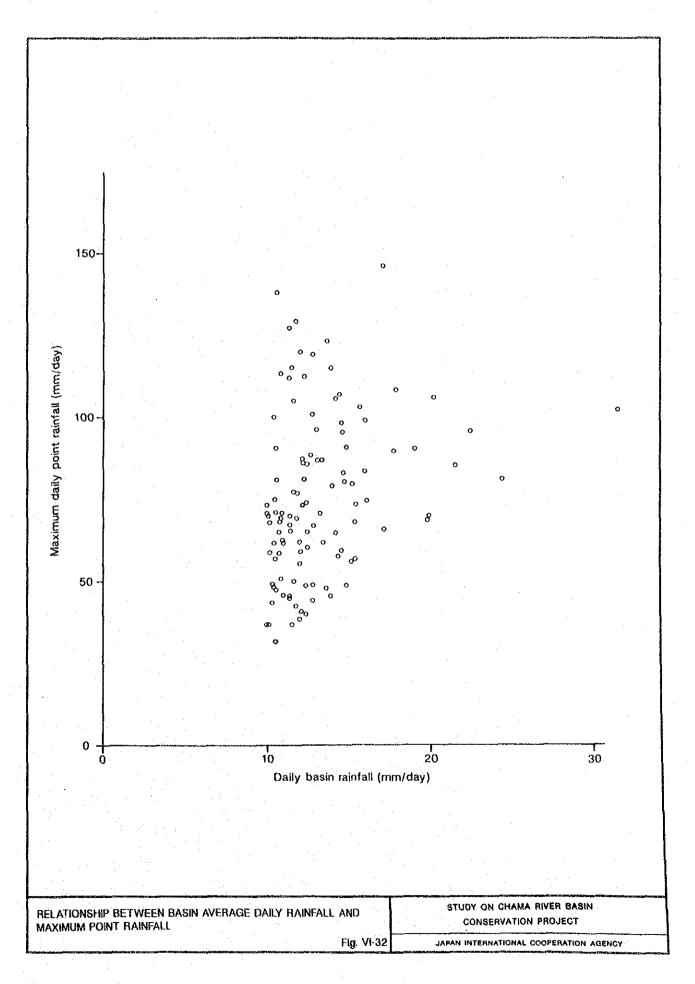


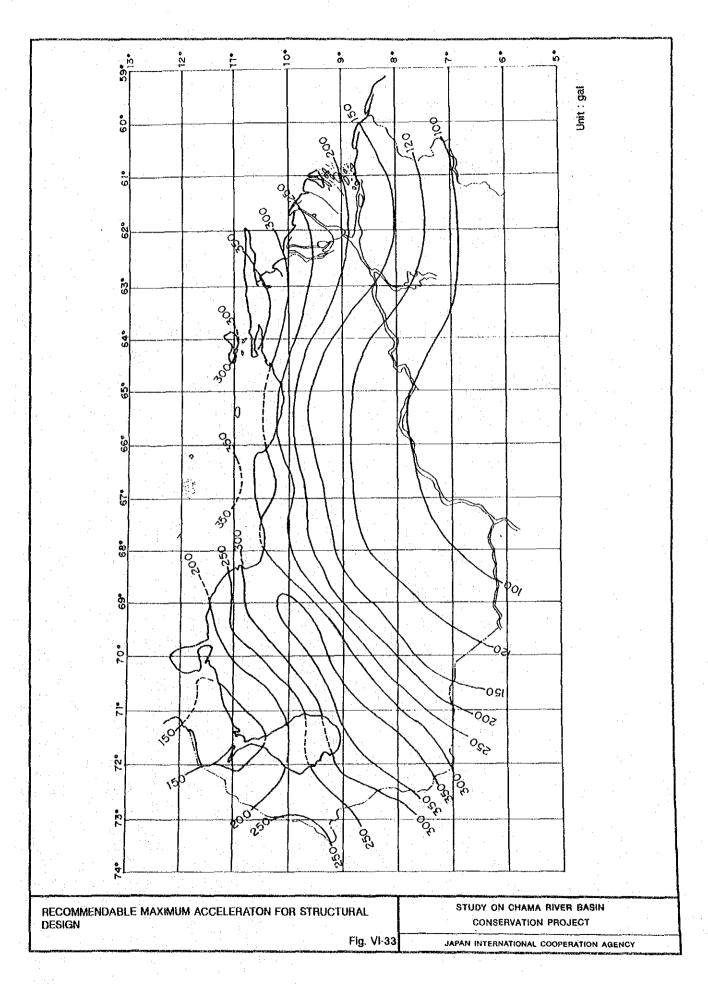




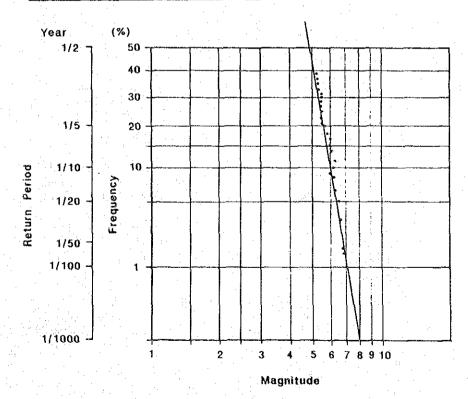








No.	Day	Month	Year	Magnitude	Frequency	Return Period
1	19	. Apr	1952	6.88	0.0167	1/ 60.0
2	3	Aug	1950	6.75	0.0333	1/ 30.0
3	21	Apr	1957	6.63	0.0500	1/ 20.0
4	14	Mar	1932	6.25	0.0667	1/ 15.0
	13	Nov	1921	6.25	0.0833	1/ 12.0
5 6 7	10	Jul	1919	6.25	0.1000	1/ 10.0
7	10	Jul	1919	6.25	0.1167	1/ 8.6
8	22	Mar	1910	6.10	0.1333	1/ 7.5
8 9	4	Nov	1933	6.00	0.1500	1/ 6.7
10	4	Nov	1933	6.00	0.1667	1/ 6.0
11	4	Aug	1910	5.80	0.1833	1/ 5.5
12	27	Jan	1970	5.70	0.2000	1/ 5.0
13	27	Dec	1911	5.50	0.2167	1/ 4.6
14	22	Jan	1947	5.50	0.2333	1/ 4.3
15	21	Jun	1912	5.50	0.2500	1/ 4.0
16	16	Mar	1929	5.50	0.2667	1/: 3.8
17	13	Nov	1921	5.50	0.2833	1/ 3.5
18	12	Aug	1944	5.50	0.3000	1/ 3.3
19	11	Oct	1926	5.50	0.3167	1/ 3.2
20	21	Dec	1967	5.40	0.3333	1/ 3.0
21	18	Jul	1965	5.30	0.3500	1/ 2.9
22	7	Jan	1965	5.30	0.3667	1/ 2.7
23	19	May	1970	5.10	0.3833	1/ 2.6
24	19	Sep	1965	5.00	0.4000	1/ 2.5
25	10	Nov	1956	5.00	0.4167	1/ 2.4
26	9	Sep	1966	5.00	0.4333	1/ 2.3



Data: 1910 - 1970

RESULTS OF FREQUENCY ANALYSIS FOR SEISMISITY

Fig. VI-34

STUDY ON CHAMA RIVER BASIN CONSERVATION PROJECT

JAPAN INTERNATIONAL COOPERATION AGENCY

