			LIST OF DIS	CONTINUITIES	S IN ADITS (1 of	3)	
Adit	Crack	T. Ď). (M)	Strike&dip	Width	Contained materials	Hater
No.	No.	Left wall	Right wall	(°)	(BM)		seepage
DA-1	1		0.8	N23E 48NW	1	Serpentine	
	2		2.0	N15W 38NE	1 ¹¹	11	
	3	1.9		N75E 63NH	5.	Open	
	4	4.0		N62W 53NE	1	Oxide	
· · ·	5	4.0		N18E 70NW			
	6			N78E 49SE			1
	7	5.4		N32E 90	10	Sheared	
	8	7.0	1 - T	N80E 50SE			
	9		8.7	E-W 38S	0 ∼1.0°°	Talc	
	10		10.3	N76E 46SE	0~1	Serpent ine	.
	11	11.3		N48W GONE	and a second		
	12		11.4	N40E 80WW	an a	Slickenside	
÷.,	13	12.2	er an tra	E-W 60S			
	14	13.1		N56E 35NH	1~5	Serpentine+Talc	
· · · ·	15		17.0	N22E 90			
	16		17.5	N34E 26NH	0~200	Serpentine	
	17	17.9		NBOW GGNE	10~30	Oxide	
	18		18.8	N42E 34NW			
	19	20.2	10,0	N70E 90	2~10	Serpentine	l.
	20	21.6		NGON 53NE	2~10	<i>w</i>	
	21	21.8		N77W 86NE			+
	1	21.0		N28E 52NW			
··-·	22	22.0	23.2	N32E 78NW	2~3	Serpentine	
	23	00 E	20.2	NG3W GONE	2~3	or point the	
	24	23.5					
	25	25.0	00.0	E-W 80N	0 40	Connentine Ovide	
	26		26.3	N31E 34NW	2~10	Serpentine+Oxide	0
	27	26.0	00.7	N78H 64NE	5	Serpentine	
	28		32.7	N13E 34NW		· · · · ·	
	29	33.2		N18W 37NE		н Пология (1996) - с	
	30	34.2	 	N76W 65NE			
	31	34.7		NG4E GGSE			
	32	36.0		N11E 47SE	1	Oxide	
	33	39.0		N77E 71NW	3~4(30)	Serpentine	
	34	39, 4		N56E 78SE	1~2	<i>n</i> .	
	35	41.1		N77E 38NW	1~5	ана на	
	36	43.0		N4OE 23NW			

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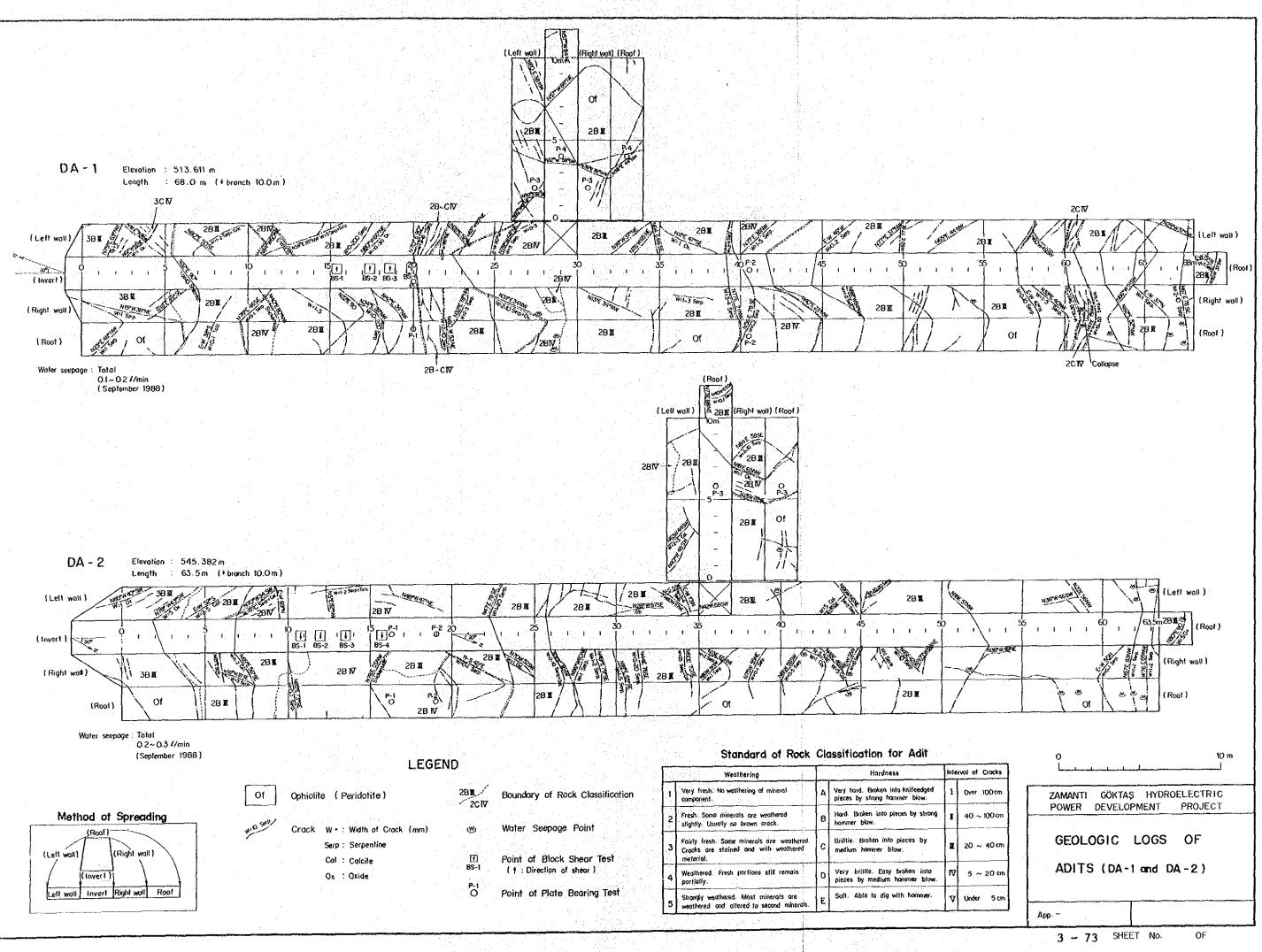
.

LIST OF DISCONTINUITIES IN ADITS (2 of 3)

	97	45 0		E-W 46N	0~2	Serpentine	
4.1 1	37	45.8	46.9	N86W 84NE	1~2		
a - 14	38 39	49,9	40.0	N77E 37NW			
	35 40	49.9 49.9	Se ga até di dia. Nga katé di dia ka	NGOE 77SE			
	40	43. 5 53. 0		NGSE 44NH			0
	41	57.7		E-W 42N	0~10	Serpentine	
	43	58.3	a de la composición d	N60₩ 495₩			
	44		59.3	N53E 40NH	1~5	Serpentine	
	45		61.8	N67E 75NW	10~50	Serpentine+Talc	0
	46		63.3	N62E 52NH			
	47		63.3	N66H 51SH	an di Barto general Barto general		0
	48		65.6	E-W 37N	1	Serpentine	0
	49		67.3	N67E 78SE	2~10	1	0
	50	67.5		N25W 37SW			
	51	68.0		E~W 75N	1	Serpentine	
	52	68.0		N50W 37SW			
Bran	53	1.2	· ···· ····	NGOW 61NE			
-ch	54	1.5		N50E 82SE			
	55	2.7	in the state of the	N58E 44NW			
	56		2.8	N76E 76NW			
	57	4.0		N32W 58SW			
	58	5.9		N57W 84NE			
	59	9.0		N80E 38NW			
	6 0		10.0	N57W 84NE			
DA-2	61	0.		N85W 40SW	1	Oxide	
	62	3.0		N78W 43SW	5		
	63	5.3	÷	E-₩ 528	2~5	Calcite	
	64		5.9	N65E 90			
	65		5.9	N55W 37SW	15 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 -	Serpentine	
	66	7.2	,	NG5E 56SE	1~2	Calcite	
	67	8.3		N70W 34SW	0~1	Serpentine+Calcite	
	68	9.4		E-W 69N			
	69	· ·	10.1	N85E 73SE			
	70	12.4	<u>.</u>	N 5E 82NW	1~2	Serpentine+Talc	
	71		15.4	N78E 55NH		Slickenside	
	72	17.6	- - 	N48W 47NE	n and and the		
	73		21.5	N-S 45E	0~1	Serpentine	
	74		23.5	N47E 78SE	1 ~20	1	

LIST OF DISCONTINUITIES IN ADITS (3 of 3)

مستسيغ							· · · · · · · · · · · · · · · · · · ·
	75		24.4	N70W 52SW	1	Calcite	
	76	25.8		N30E 80SE	2 ~10	Serpentine+Calcite	
	77		27.5	N86H 60NE	1	Serpentine	
	78		28.9	N49E 79SE	1~2	n	-
:	79	a de la companya de	30.1	N18E 65SE	1~5	n	
	80		31.4	N44E 76SE	2 ~20	"	
	81	32.0		N28H 67SH	itin an ann an a	·····	0
	82	33.0		N-S 59E) 		
	83	33.3		NSON 57NE			
	84	34.1		E-4 73N	5~6	Serpentine	
	85		34.1	NGOE 70SF	10+15	Serpentine+Calcite	
	86	35.0		N42W 68SH			
	87		36.2	N80W 51SW	1	Serpentine	
	88		36.7	N13E 65NW	2	n –	
	89	• · ·	38.5	N75W 55NE	0~1	'n	
	90	t	40.8	N81₩ 58SW	0~5	"	0
	91		42.7	N-S 54E	1	Calcite	0 0
	92		43.4	N48E 46SE	5	11	0
	93		44.3	E-N 55N	10	Serpentine+Calcite	0
	94	44.2		N86H 58NE	5	Serpentine	:
	95		48.0	N45E 42SE	10	"	- -
	96		48.7	N77W G3NE			
	97	50.6		N18E 57NW			0
	98		52.4	N36W 49NE	4 1	>	
21 (99	58,5		N36W 46SH		(
	100	58.4		N22E 56NW			0
	101	· · · · · · · · · · · · · · · · · · ·	60.3	E-W 50N	0~1	Serpentine	
	102		61.7	N67E 83NW	1~2	· · · · · · · · · · · · · · · · · · ·	0
	103		62.7	N76E 69NW	1~2	· <i>"</i>	0
	104		63.5	N80E 90	5	Oxide	0
Bran		1.8		N40H 48SH	• · · · · · • • • •		
-ch		3.0		N63H 44SH	2~3	Calcite	0
	107		5.0	N25W 78KE			
	108		6.6	N18E 65NW	1	Oxide	
	109		8.5	N84E 58SE	2~10	Serpentine	
	110	10.0		N73E 88NW	2		
	111		10.0	N40E 63SW	1 · · · · · · · · · · · · · · ·	Serpentine	
			10.0	HTVL OVON	· · ·		[]



LIST OF ROCK ANALYSES

Microscopic Sample Sampling Location Chemical X-ray No. Observation Analysis Diffraction Dam Site Adit "DA-1" G-1 0 Dam Site Right Bank Ô G- 2 G- 3 Reservoir Upstreammost Part Ø Left Bank . Anna S G-4 Reservoir Upstreammost Part 0 0 Right Bank G- 5 0 0 . G- 6 Headrace Tunnel Route 0 Ø TB-2 Depth105.0m G- 7 Headrace Tunnel Route 0 Ø TB-2 Depth146.5m Headrace Tunnel Route G- 8 0 0 TB-2 Depth152.0m G- 9 Left Bank of Zamanti River \odot \bigcirc 2km Downstream from KUP Mah. 6-10 Powerhouse Site \bigcirc etek lehender anderen Reservoir Area Near the G-11 0 Confluence of the Zamanti River and the Topoctas River Dam Site Adit "DA-1" 6-12 \odot TD. 57. 5m Adit "DA-1" 0 Dam Site G-13 TD, 61. On

©: Carried out

		e Kasta (* 1							¹¹ :/
	Microsco	opic O	bserv	vatior	1				
Project:	<u>an an a</u>								
Locality:				i ga e Mirini Ali					
Sample No.	G - 1		Slice	e No.			1111 1111 1111	n na Star Na Star Na Star	
Rock Name:	Peridote		÷			Na †∌ j		i tita T	
Texture:	Granular								
Rock forming	minerals:					•			
Olivine :	Subhedral(0. Serpentine g width) of ol	rows	in mi	ı) .crocr	acks	(0.04	~0 .	2mm	in
Serpentin	e:Replace in	micro	crack	s of	oliv	ine.			
Chromite:	Subhedral(0.n	mm),	lark	in co	lor,	rare.			
						t. tett			-
					ан Жалараан				
	an e na ministrati anti stitu e e statu inita			141.070				· .	
Description:	ne vezete da almando en attane - atanet habade ne ma bar		:		tyle: Grant Bar Angele:				
- -	h,olivine ric	h per:	ldoti	te wi	th r	are c	hrc	omite	
Very fres	h,olivine ric s replaced by				en kon	7 - 6 - 6 - 6 - 6 - 6 - 6 - 6 - 6 - 6 -	ĥrç	omite	
Very fres Olivine is	s replaced by				en kon	7 - 6 - 6 - 6 - 6 - 6 - 6 - 6 - 6 - 6 -	hrç	mite	
Very fres Olivine is Degree of alt	s replaced by	Serpe	entin	e rar	ely.				
Very fres Olivine is Degree of alt	s replaced by teration:	Serpe	entin	e rar	ely.				
Very fres Olivine is Degree of al Very weak	s replaced by teration:	Serpe	entin	e rar	ely.				
Very fres Olivine is Degree of alt Very weak Occurence:	s replaced by teration: .Serpentine g	Serpe	entin	e rar	ely.				
Very fres Olivine is Degree of alt Very weak Occurence:	s replaced by teration: ,Serpentine g	Serpe	entin	e rar	ely.				
Olivine is Degree of al Very weak Occurence: Macroscopic (s replaced by teration: ,Serpentine g	Serpe	entin	e rar	ely.				

Project:

Locality:

Sample No. G - 2 Slice No.

Rock Name: Peridotite

Texture:

Tanàna dia dia kaominina di

Rock forming minerals:

Olivine : Subhedral(0.5 to 1.0mm) Serpentine grows in microcracks of olivine rarely.

Serpentine:Replace in microcracks of olivine.

Chromite:Subhedral(0.n mm), dark in color, rare.

Description:

Very fresh, olivine rich peridotite with rare chromite.

Olivine is replaced by Serpentine rarely.

Degree of alteration:

Very weak, Serpentine grows in microcracks of olivine.

Occurence:

Macroscopic Observation:

Yellowish green color.

Remarks:

Microscopic Observation

Project:	
Locality:	
Sample No. (G-4 Slice No.
Rock Name: I	Linestone
Texture: bio	
Rock forming	g minerals:
calcite	fine grain with pale gray color grains (0.n mm) forming material of calcite micro-
	vein
	grains (0.0n to 0.n mm) replaces microfossils

Biomicrite is cut by calcite microveins. Many microfossils (0.2 - 0.3 mm) and rare shell (?) are observed and replaced by calcite.

Description:

Degree of alteration:

None or very weak

Occurence:

Macroscopic Observation:

Fine with pale gray color

Remarks:

	Microscopic Observation
Project:	
Locality:	
Sample No. G-	
Rock Name: Li	
Texture: gran	ule and the second s
Rock forming	minerals:
calcite	fine grain : 0.00n to 0.01 mm
	coarse grain : 0.1 to 0.2 mm
	$\frac{\partial f}{\partial t} = \frac{\partial f}{\partial t} $
Description:	nde fan de service de la construcción de la construcción de la construcción de la construcción de la construcci La construcción de la construcción d
وحووا وحصص أأتا المكادات	d calcite are observed with dotted. Calci
Coarse graine	
Coarse graine	d calcite are observed with dotted. Calci
Coarse graine	d calcite are observed with dotted. Calci
Coarse graine veins are obs Degree of alt	d calcite are observed with dotted. Calci erved, rarely. eration:
Coarse graine veins are obs Degree of alt recrystallize	d calcite are observed with dotted. Calci erved, rarely.
Coarse graine veins are obs Degree of alt recrystallize	d calcite are observed with dotted. Calci erved, rarely. eration: d to granular calcite crystal grains
Coarse graine veins are obs Degree of alt recrystallize	d calcite are observed with dotted. Calci erved, rarely. eration: d to granular calcite crystal grains
Coarse graine veins are obs Degree of alt recrystallize	d calcite are observed with dotted. Calci erved, rarely. eration: d to granular calcite crystal grains
Coarse graine veins are obs Degree of alt recrystallize Occurence:	eration: d to granular calcite crystal grains
Coarse graine veins are obs Degree of alt recrystallize Occurence: Macroscopic O	eration: d to granular calcite crystal grains

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Project:	a Ata in an an an Ata in an an				
Locality:		an a a a a a a a a a a a a a a a a a a			
Sample No. G-6	na an an tha an	Slic	e No.		
Rock Name: Lim	estone	<u>, , , , , , , , , , , , , , , , , , , </u>			
Texture: biomi	crite				
Rock forming m	inerals:				
calcite	fine grain,	with pale g	ray color		
	grains (0	n mm), fo	rming ma	terial of	calcit
	microveins	with >10 mm	width		
	grains (0.0	on to 0.n mm)	, replace	microfoss	ils
quartz	rarely obse	erved (0.00n	mm)		
"limonite"	rarely obse	erved in grai	n boundar	y of fine	calcite
carbonaceous	Datter	rarely obse calcite	rved in g	rain boun	dary of
Description:	· · · · · · · · · · · · · · · · · · ·				
Biomicrite is	cut by calc	ite micro ve	ins. Mici	cofossils	(0.2 to
0.3 mm) are	replaced by	calcite.	Quartz gi	cains are	rarely
observed and	"limonite"	(iron hydro	oxide)	and carb	onaceous
matter penetrat	ed into gra	in boundary (of fine ca	alcite.	en en la fina en la composition la composition de la composition la composition de la composition la composition de la composition la composition de la composition de la composition la composition de la composition de la composition de la composition la composition de la composition de la composition de la composition de la composit

Degree of alteration:

Recrystallization of calcite is observed partially.

Occurence:

Macroscopic Observation:

fine with pale yellowish gray

Project:				
Locality:		an a		aing and and a
Sample No.	G-7	Slice No.	<u>, </u>	
Rock Name:	Quartz sandstone			
Texture:	fragmental			

Rock forming minerals:

quartz angular grain (0.1 to 0.2 mm)

clay mineral fine lamellar grain of sericite

calcite rare

opaque mineral rare

Description: Angular quartz grains are cemented by clay minerals. Micro veins of lamellar quartz and sericite are cut rarely the stone. Calcite grain and opaque mineral are also observed, rarely. Some grains composed with sericite will be alteration products of feldspar grains.

Degree of alteration: Clay mineral (sericite) will be formed by hydrothermal reaction.

Occurence:

Macroscopic Observation:

fine with white color

Remarks:

•			
	Microsco	opic Observation	
Project:	en de la companya de		
Locality:			
Sample No.	G8	Slice No.	
	Limestone (muddy)	anda a second a secon A second a s	an start and a
Texture:		ne <u>n en en</u>	n an
Rock forming	g minerals:		
calcite	fine and irregul	ar form	
· ·	idiomorphic grai	n ser estas en en el	teres e de la se
	grain (0.n mm),	forming material of calc	ite micro-
	veins		
quartz	subangular grain	(0.00n to 0.0n mm)	بالدار منطق وجوار مارد میرون معاد با افراد افراد
quartz feldspar	subangular grain rare	(0.00n to 0.0n mm)	
		a service de la construcción de la La construcción de la construcción d La construcción de la construcción d	
feldspar	rare rare and iron su	a service de la construcción de la La construcción de la construcción d La construcción de la construcción d	own muddy
feldspar opaque	rare rare and iron su Calcite grains	lfide mineral	
feldspar opaque Description material.	rare rare and iron su Calcite grains Quartz, feldspar	lfide mineral are cemented by pale br	observed
feldspar opaque Description material. rarely.	rare rare and iron su Calcite grains Quartz, feldspar	lfide mineral are cemented by pale br and opaque mineral are calcite and muddy mat	observed
feldspar opaque Description material. rarely. M carbonaceous	rare rare and iron su Calcite grains Quartz, feldspar Microveins of fine s matter (?) cut the	lfide mineral are cemented by pale br and opaque mineral are calcite and muddy mat	observed
feldspar opaque Description material. rarely. M carbonaceous Degree of al	rare rare and iron su Calcite grains Quartz, feldspar Microveins of fine s matter (?) cut the	lfide mineral are cemented by pale br and opaque mineral are calcite and muddy mat	observed
feldspar opaque Description material. rarely. M carbonaceous	rare rare and iron su Calcite grains Quartz, feldspar Microveins of fine s matter (?) cut the	lfide mineral are cemented by pale br and opaque mineral are calcite and muddy mat	observed
feldspar opaque Description material. rarely. M carbonaceous Degree of al	rare rare and iron su Calcite grains Quartz, feldspar Microveins of fine s matter (?) cut the	lfide mineral are cemented by pale br and opaque mineral are calcite and muddy mat	observed
feldspar opaque Description material. rarely. M carbonaceous Degree of al none ?	rare rare and iron su Calcite grains Quartz, feldspar Microveins of fine s matter (?) cut the	lfide mineral are cemented by pale br and opaque mineral are calcite and muddy mat	observed
feldspar opaque Description material. rarely. A carbonaceous Degree of al none ?	rare rare and iron su Calcite grains Quartz, feldspar Microveins of fine matter (?) cut the teration:	lfide mineral are cemented by pale br and opaque mineral are calcite and muddy mat	observed
feldspar opaque Description material. rarely. A carbonaceous Degree of al none ? Occurence: Macroscopic	rare rare and iron su Calcite grains Quartz, feldspar Microveins of fine matter (?) cut the teration:	lfide mineral are cemented by pale br and opaque mineral are calcite and muddy mat	observed

Project:

Locality:

Sample No. G-9

Rock Name: Quartz sandstone (pale bluish red)

Slice No.

Texture: fragmental

Rock forming minerals:

quartz angular grain (0.00n to 0.0n mm)

clay mineral fine lamellar grain of sericite

calcite a small amount

feldspar a small amount

mafic mineral rare, hornblende ?

"limonite" a small amount

hematite

Description: Angular quartz grains withsmall or rare ammounts of calcite, feldspar, mafic minearl and hematiteare cemented by clay minerals. It is penetrated with limonite then colored pale brownish red.

Degree of alteration: Clay mineral (sericite) will be formed by hydrothermal reaction.

Occurence:

Macroscopic Observation:

fine with pale brownish red color

Remarks:

Project:		·		
Locality:			na sana ang sana sa	
Sample No. G-	-10	Slice	e No.	
Rock Name: Qu	lartz sandston	e (arkose ?)	an in the second states	
Texture: fra	agmental			
Rock forming	minerals:			
quartz	angular gra	in (0.0n to 0	n mm)	
feldspar	K-feldspar a	and plagiocla	ise and the state	e for her start with the
biotite	flaky grain	with weakly	altered in pa	rtially
hornblende	rare	1. 1. 1.		
calcite	cementation	material of	mineral grain	S antan da sa alianti
Description:	Quartz, fe	eldspar, bio	tite and horn	blende grains
are cemented	by fine altere	ed biotite fl	akes and calc	ite.
			······	
Degree of alt	eration: no	one or very w	eak	and shall a sea
	· .			
Occurence:				
· ·				an an an an an an an Arraighte
Macroscopic Ol	bservation:			
		1		
Remarks:	<u> </u>			
:				
		······································	<u></u>	
		<i>9</i> .		
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Microscopic Observation Project: Locality: Sample No. G-11 Slice No. Rock Name: Peridotite Texture: granular Rock forming minerals: olivine subhedral (0.5 to 10 mm), serpentine growing as network shape subhedral (0.n mm) pyroxene Ca-plagioclase a small amount serpentine replace olivine grain and in microcracks in olivine chromite subhedral (0.n mm), dark brown in color, rare Description: Olivine rich peridotite with Ca-plagioclase, pyroxene and rare chromite. Olivine is replaced by serpentine partially. Degree of alteration: Serpentine grows in cracks of olivine. Occurence: Macroscopic Observation: Remarks:

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Microscopic Observation Project: Locality: Slice No. Sample No. G-12 Rock Name: Peridotite Texture: granular Rock forming minerals: subhedral (0.5 to 10 mm), serpentine replaced with olivine cracks, partially subhedral (0.n mm) and the second of the second sec pyroxene a small amount of the best are a control of Ca-plagioclase replace olivine grain and in microcracks of serpentine olivine chromite subhedral (0.0n to 0.n mm), dark brown color, rare Description: Olivine rich peridotite with Ca-plagioclase, pyroxene and rare chromite. Olivine is replaced by serpentine partially. Degree of alteration: serpentine grows in cracks of olivine.

Occurence:

Macroscopic Observation:

Remarks:

Chemical analysis of rocks

Sample NO.	G-3	G-4	G-5	G-6	G-7	G-8	G-9
Rock Name	Limestone	Limestone	e Limestone	Limestone	e Sandstone	: Limestone	Sandstor
	wt.X	wt.X	wt.%	wt.X	wt.%	wt.X	wt.X
SiO ₂	0,05	0.99	0.08	0. 18	90.10	22, 48	78. 82
Al ₂ O ₃	0.02	2.26	0.42	4.36	7.20	4,96	6, 26
MgO	0, 16	0.79	1.67	1.82	0.39	0.33	0. 16
CaO	55.03	51.89	53.20	50. 52	0.58	25.80	4.17
SO3	0. 01	0. 19			0. 81	1.34	0. 48

diffraction X-ray

1 . Sample Name

G-13 "

2. Measurement Condition

Voltage	30kV
Current	20mA (30mA for Oriented aggregate)
Target	Cu
Filter	and a second
Slit	1°DS - 0.1mm - 1°SS
Scale Range	2000cps
Time constant	2sec
Measurement Range(2 θ)	2°~ 71°
Scanning Speed	2°/min
Chart Speed	2cm/min
Hardware	XD-610 (Shimadzu Corporation)
Software	DP-61 System (Shimadzu Corporation)

3. Treatment

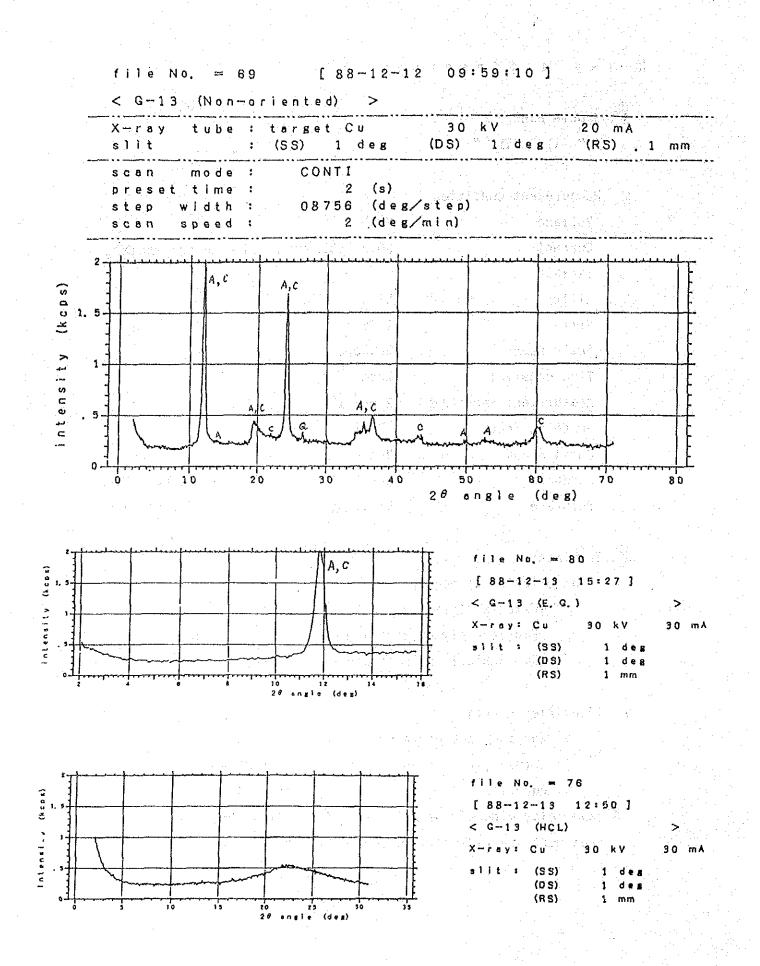
At Oriented aggregate

Water elutriation treatment	20=	2° ~	- 31°
Ethylene glycol treatment	2 <i>0</i> = 3	2° ~	- 16°
Hydrochloric acid treatment	2 <i>θ</i> = :	2° ~	- 31°

4. Identified mineral

- A: Antigorite (Serpentine group) ···· Abundant
 - C: Chrysotile (Serpentine group) Abundant
- Q: Quartz ···· Rare

* Other clay minerals is not detected at ethylene glycol treatment and hydlochloric acid treatment.



4. ĝ

3-10 Plate Bearing Test

· · · ·																					$p_{i}^{(1)} = \frac{1}{2} \left(\frac{1}{2} \left(\frac{1}{2} - \frac{1}{2} \right) \right) \left(\frac{1}{2} \left(\frac{1}{2} - \frac{1}{2} \right) \right)$	Unit: 10-3 mm
		No.	<1)	<2>	<u><3></u>	<u> </u>	<5>	<6>	<7>	<8>	<9>	<10>	<11>	<12>	<13>	<14>	<15>	<16>	<17>	<18>	<19>	
Location	<u>Loa</u>	d Condition Rock Classifi-	0 kgf/cm ² 15 kgf/cm ²	<u>15</u> 15	<u>30</u> 30	<u>45</u> 45	<u>60</u> 60	0 60	<u>60</u> 60	<u>60</u> 60	<u>0</u> 65	<u>20</u> 65	<u>40</u> 65	<u>60</u> 65	<u>65</u> 65	0 65	<u>20</u> 65	<u>40</u> 65	<u>60</u> 65	<u>65</u> 65	0 kgf/cm ² 65 kgf/cm ²	Test Results
DA - 1 P - 1 TD 20.0 m	Invert	cation	4	9	18	30	46	10	52	71	12	17	35	48	55	17	20	39	61	64	21	$D = 271,400 \text{ kgf/cm}^2$ Et = 251,500 kgf/cm ² Es = 327,400 kgf/cm ² Cf = 45 %
	Crown	2B III: b	22	28	58	91	122	73	127	137	83	92	117	140	147	92	98	123	146	151	94	D = 107,700 Et = 189,200 Es = 239,500 Cf = 19
DA - 1 P - 2 TD 40.5 m	Invert	2B IV : c	29	38	74	115	163	96	174	180	93	106	147	175	185	111	127	165	190	199	120	D = 81,200 Et = 137,400 Es = 163,500 Cf = 8
	Crown	2B IV : c	4	5	12	22	32	27	32	36	29	34	37	42	44	29	37	45	49	52	36	D. = $370,400$ Et = $856,000$ Es = $809,700$ Cf = 80
DA - 1 p - 3 TD(B)2.1 m	Left Wall	2B III: b	83	89	116	145	171	121	182	193	130	148	175	197	204	154	170	198	215	222	164	$\begin{array}{rcl} D &=& 123,300\\ Et &=& 192,000\\ Es &=& 207,500\\ Cf &=& 18\\ \hline & & & & & \\ \hline & & & & & & \\ \hline & & & &$
	Right Wall	2B III: b	28	42	70	91	121	64	122	137	75	96	118	136	141	92	114	138	157	162	94	D = 131,000 Et = 220,600 Es = 216,400 Cf = 26
DA - 1 P - 4 TD(B)4.0 m	Invert	2B 111: b	25	31	57	79	109	67	107	117	81	87	107	125	131	90	94	114	131	136	94	D = 132,100 Et = 239,600 Es = 306,900 Cf = 25
	Crown	2B III: b	77	88	107	124	139	94	137	143	9 8	120	133	145	148	114	121	133	144	147	116	D = 199,000 Et = 379,000 Es = 369,800 Cf = 14
DA - 2 P - 1 TD 16.2 m	Invert	2B IV : c	19	50	82	120	225	168	311	324	245	314	369	390	398	354	389	413	427	432	383	D = 55,000 Et = 179,700 Es = 142,300 Cf = 9
	Crown	2B IV : c	49	71	129	183	253	181	280	297	183	202	238	262	268	175	218	272	314	320	220	D = 56,400 Et = 126,400 Es = 137,200 Cf = 17
DA - 2 P - 2 TD 19.0 m	Invert	2B IV : c	7	16	41	77	113	49	119	148	76	93	121	145	152	77	93	123	150	156	81	D = 103,100 Et = 167,700 Es = 189,800 Cf = 41
	Crown	2B IV : c	198	291	371	458	545	423	594	665	503	578	624	652	667	510	581	628	657	663	525	D = 39,900 Et = 120,700 Es = 92,900 Cf = 42
DA - 2 p - 3 TD(B)5.8 m	Invert	2B IV : c	95	145	314	504	671	424	751	778	493	633	734	797	815	571	709	810	866	883	593	D = 19,200 Et = 57,500 Es = 46,400 Cf = 8
	Crown	2B IV : c	Cancele	d dat	s								1							a ta t		

3-10-1 Deformation for Calculation of Modulus of Elasticity and Test Result on Plate bearing Tests

Note: Stress level of Et to be $20 - 65 \text{ kgf/cm}^2$

3-10-2 Calculation Sheets of Plate Bearing Tests

DA-1,P-1,TD20.0 m	DA-1,P-2,TD40.5 m	DA-1,P-3,TD(B)2.1 m	DA-1,P-4,TD(B)4.0 m	DA-2,P-1,TD16.3 m	DA-2,P-2,TD19.0 m
(Invert)	(Invert)	(Left wall)	(Invert)	(Invert)	(Invert)
BEARING DATA IN.(P7)	BEARING DATA IH. (P7)	BEARING DATA IN. (P7)	BEARING OATA IN.(P7)	SEARING DATA IN. (P7)	BEARING DATA IN.(P7)
DATA INPUT END	Data Ihput Eno	DATA INPUT END	DATA INPUT END	DATA INPUT END	Data input end
CONFIRM DATA (P8)	CONFIRM DATA (PS)	CONFIRM OATA (P8)	CONFIRM DATA (PS)	CONFIRM DATA (P8)	CONFIRM DATA (P8)
4 9 18 30 46	29 38 74 115 163	83 89 116 145 171	25 31 57 79 109	19 58 82 120 225	7 16 41 77 113
C(60)= 18 52 71	C(60)= 96 174 188	C(60)= 121 182 193	C(60)= 67 107 117	C(60)= 168 311 324	C(60)= 49 119 148
12 17 35 48 55	93 186 147 175 185	130 148 175 197 204	81 87 107 125 131	245 314 369 398 398	76 93 121 145 152
17 20 39 61 64	111 127 165 198 199	154 170 198 215 222	90 94 114 131 136	354 389 413 427 432	77 93 123 158 156
FINAL DATA= 21	FINAL DATA= 120	FINAL DATA= 164	FINAL DATA= 94	FINAL DATA= 383	FINAL DATA= 81
DATA CONFIRMED END	DATA CONFIRMED END	DATA CONFIRMED END	DATA CONFIRMED END	DATA CONFIRMED END	DATA CONFIRMED END
8EARING.T RESULT(P9)	BEARING.T RESULT(P9)	BEARING.T RESULT(P9)	SESRING.T RESULT(P9)	BEARING.T RESULT(PS)	BEARING.T &ESULT(P9)
S= 1.2 R= 0.984	S= 0.359 R=-0.996	S= 0.545 R= 1	S= 0.584 R= 0.997	S= 0.243 R= 0.913	S= 0.456
DEFORMATION MODULAS	DEFORMATION MODULAS	OEFORHATIOH MODULAS	DEFORMATION MODULAS	DEFORMATION MODULAS	DEFORMATION MODULAS
D (KG/CM2)= 271480	D (KG/CH2)= 81208	D (KG/CH2)= 123380	D (KG/CH2)= 132190	D (KG/CA2)= 55000	D (KG/CH2)= 103100
CREEP RATIO CF(0/0)	CREEP RATIO CF(0/0)	CREEP RATIO CF(0/0)	CREEP RATIO CF(0/0)	CREEP RATIO CF(0/0)	CREEP RATIO CF(0/0)
18 52 71 CF= 45	96 174 180 CF= 8	121 182 193 CF= 18	67 107 117 CF= 25	168 311 324 CF= 9	49 119 148 CF= 41
ELASTICITY HODULUS	ELASTICITY HODULUS	ELASTICITY HODULUS	ELASTICITY MODULUS	ELASTICITY MODULUS	ELASTICITY MODULUS
ES(65)= 341900 31280	ES(65)= 159800 16710	ES(65)= 198788 21620	ES(65)= 294100 31960	ES(65)= 96100 188500	ES(65)= 193500 18610
0	0	8	0	MEAN ES(65)= 142300	0
MERH ES(65)= 327400	NEAN ES(65)= 163500	NEAN ES(65)= 207508	NERN ES(65)= 306900	S= 0.529 R= 0.95	NEAN ES(65)= 189800
S= 1.226 R= 0.992	S= 0.579 R= 0.992	S= 0.814 R= 0.998	S= 1.837 R= 0.999	S= 1.059 R= 0.984	S= 0.77
S= 0.997 R= 0.998	S= 0.635 R= 0.991	S= 0.883 R= 0.987	S= 1.082 R= 0.999	ET20-65= 119780 2396	
ET20-65= 277400 2255	ET20-65= 131000 1437	ET20-65= 184200 1997	ET20-65= 234500 2447	00	
00	00	80	00	NEGN ET28-65= 179700	
NEAN ET20-65= 251500 Result Cal. END	NEAN ET20-65= 137400 RESULT CAL. END	NERN ET20-65= 192000 Result Cal. END	NEAN ET20-65= 239600 Result Cal. END	RESULT CAL. END	RESULT CAL. END
(Crown)	(Crown)	(Right wall)	(Crown)	(Crown)	(Crown)
BEARING DATA IN.(P7)	BEARING DATA IN.(P7)	BEARING DATA IN.(P7)	BEARING DATA IH.(P7)	BEARING DATA IN.(P7)	BEARING DATA IN.(P7)
DATA INPUT END	DATA INPUT END	DATA INFUT END	DATA INPUT END	DATA INPUT END	DATA INPUT END
CONFIRM DATA (P8)	CONFIRM DATA (P8.	CONFIRM DATA (P8)	CONFIRM DATA (P8)	CONFIRM DATA (P8)	CONFIRM DATR (P8)
22 28 58 91 122	4 5 12 22 32	28 42 70 91 121	77 88 107 124 139	49 71 129 183 253	198 291 371 458 545
C(60)= 73 127 137	C(60)= 27 32 36	C(60)= 64 122 137	C(60)= 94 137 143	C(60)= 181 280 297	C(68)= 423 594 665
83 92 117 140 147	29 34 37 42 44	75 96 118 136 141	98 128 133 145 148	183 282 238 262 268	503 578 624 652 667
92 98 123 146 151	29 37 45 49 52	92 114 138 157 162	114 121 133 144 147	175 218 272 314 320	518 581 628 657 663
FINAL DATA= 94	FINAL DATA= 36	FINAL DATA= 94	FINAL DATA= 116	FINAL OATA= 220	FINAL DATA= 525
DATA CONFIRMED END	DATA CONFIRMED END	DATA CONFIRMED END	DATA CONFIRMED END	DATA CONFIRMED END	DATA CONFIRMED END
8ERRING.T RESULI(P9)	BEARING.T RESULT(P9)	BEARING.T RESULT(P9)	BEARING.T RESULT(P9)	8EARING.T RESULT(P9)	BERRING.T RESULT(P9)
S= 0.476	S= 1.638	S= 0.579	S= 0.88 R= 0.997	S= 0.249 R= 0.997	S= 0.177 R= 1
DEFORMATION MODULAS	DEFORMATION MODULAS	DEFORMATION MODULAS	DEFORKATION MODULAS	DEFORMATION HODULAS	DEFORMATION NODULAS
D (KG/CH2)= 187709	D (KG/CH2)= 370400	D (KG/CH2)= 131000	D (KG/CM2)= 199800	D (KG/CH2)= 56409	D (KG/CH2)= 39900
CREEP RATIO CF(0/0)	CREEP RATIO CF(0/0)	CREEP RATIO CF(0/0)	CREEP RATIO CF(0/0)	CREEP RATIO CF(0/0)	CREEP RATIO CF(0/0)
73 127 137 CF= 19	27 32 36 CF= 88	64 122 137 CF= 26	94 137 143 CF= 14	181 280 297 CF= 17	423 594 665 CF= 42
ELASTICITY MODULUS ES(65)= 229700 24920	ELASTICITY MODULUS ES(65)= 980200 63920	ELASTICITY MODULUS Es(65)= 222800 21000	ELASTICITY MODULUS Es(65)= 294100 44550	ELASTICITY HODULUS ES(65)= 173000 10140	ELASTICITY MODULUS ES(65)= 89700 96100 MEAN ES(65)= 92900
0 NEAN ES(65)= 239500	0 MERN ES(65)= 809700	0 MEAN ES(65)= 216400	U NEAN ES(65)= 369800	MERH ES(65)= 137200	S= 0.522 R= 0.987
S= 0.826	S= 4.442 R= 8.976 S= 3.126 R= 8.976 ET28-65= 1984808 707	S= 1.608 R= 0.998 S= 0.943 R= 0.997 ET20-65= 227900 2132	S= 1.61 R= 1 S= 1.74 R= 1 ET20-65= 364300 3936	S= 0.683 R= 0.989 S= 0.435 R= 0.992 ET20-65= 154500 9830 A	S= 0.545 R= 0.982 ET20-65= 118100 1232 80 NEAN ET20-65= 128790
80 NEAN ET29-65= 189290 RESULT CAL. END	100 NEAN ET20-65= 856800 Result Cal. END	00 HEAN ET20-65= 220600 Result Cal. END	00 MEAN ET20-65= 379000 RESULT CAL. END	NEAN ET20-65= 126400 Result Cal. END	RESULT CAL. END

61

DA-2,P-3,TD(B)5.8 m (Invert) BEARING DATA IN. (P7) DATA INPUT END

CONFIRM DATA (P8) 95 145 314 504 671 C(60)= 424 751 778 493 633 734 797 815 571 789 818 866 883 FINAL DATA= 583 DATA CONFIRMED END

BEARING.T RESULT(P9) S= 8.885 R= 0.999

DEFORMATION MODULAS D (KG/CH2)= 19208

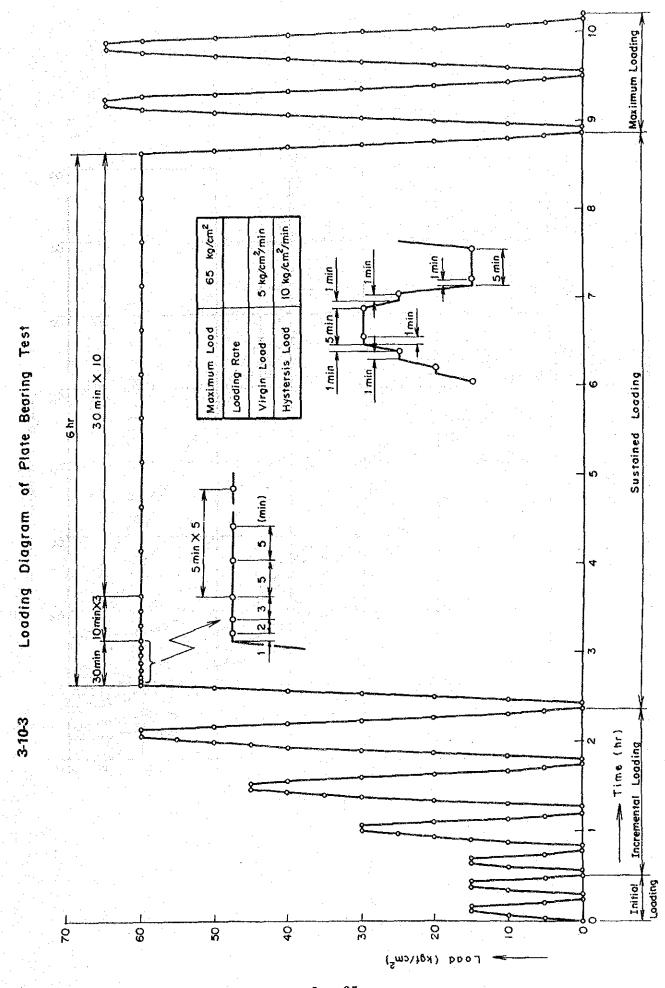
CREEP RATIO CF(0/0) 424 751 778 CF= 8

ELASTICITY MODULUS ES(65)= 45700 47100 NEAN ES(65)= 46400

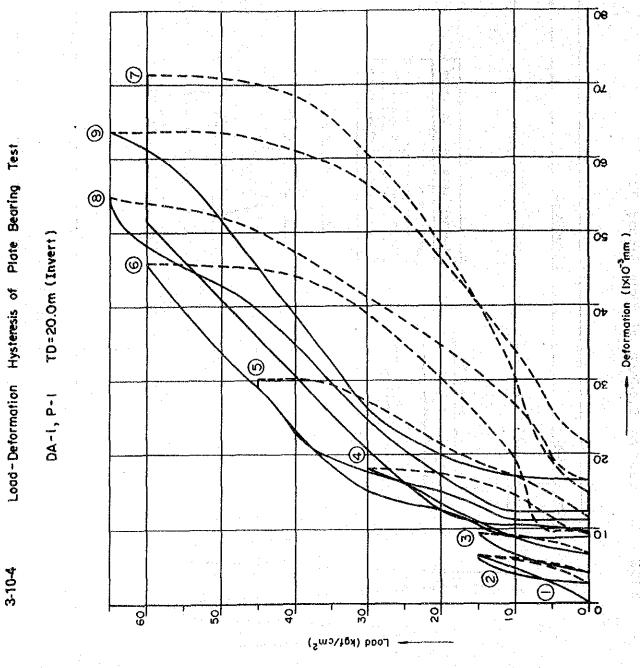
S= 0.248 R= 0.986 S= 0.259 R= 0.979 ET20-65= 56200 58700 MEAN ET20-65= 57500 RESULT CAL. END

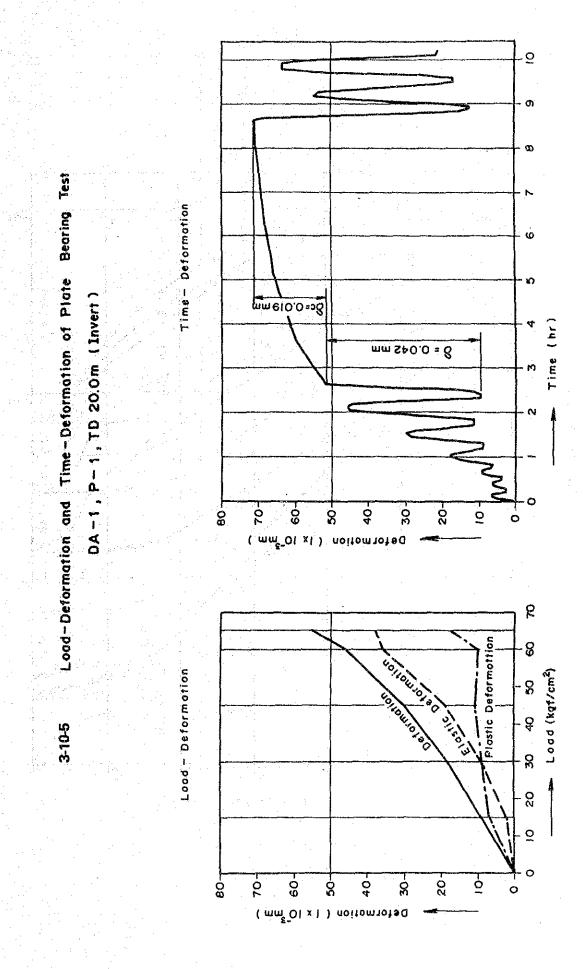
(Crown)

(Canceled data)



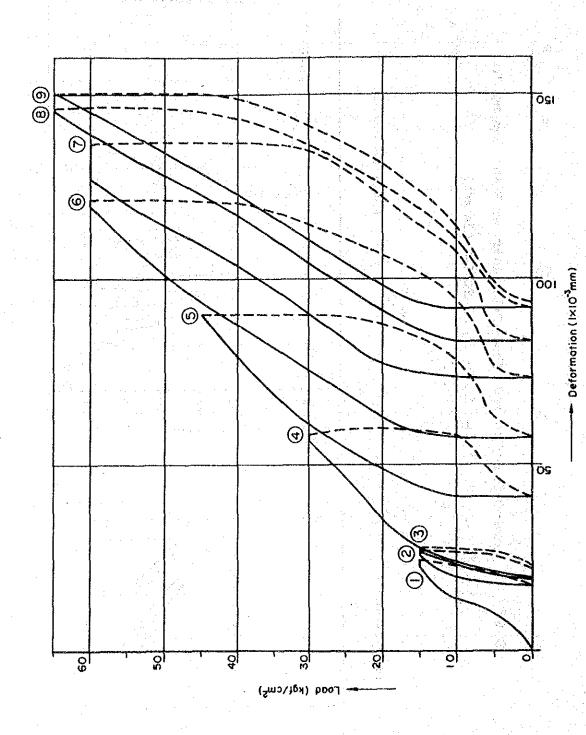
.

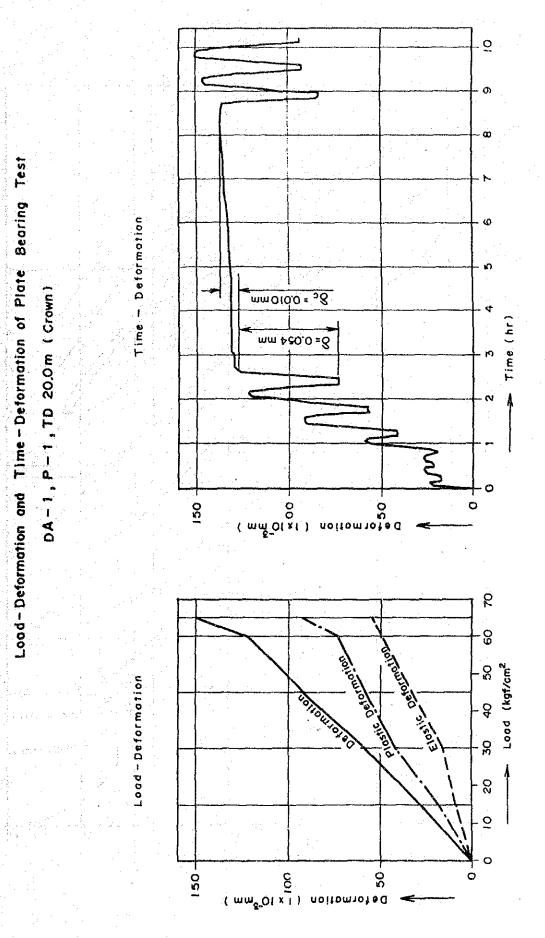




Load-Deformation Hysteresis of Plate Bearing Test

DA-1, P-1 TD=20.0m (Crown)

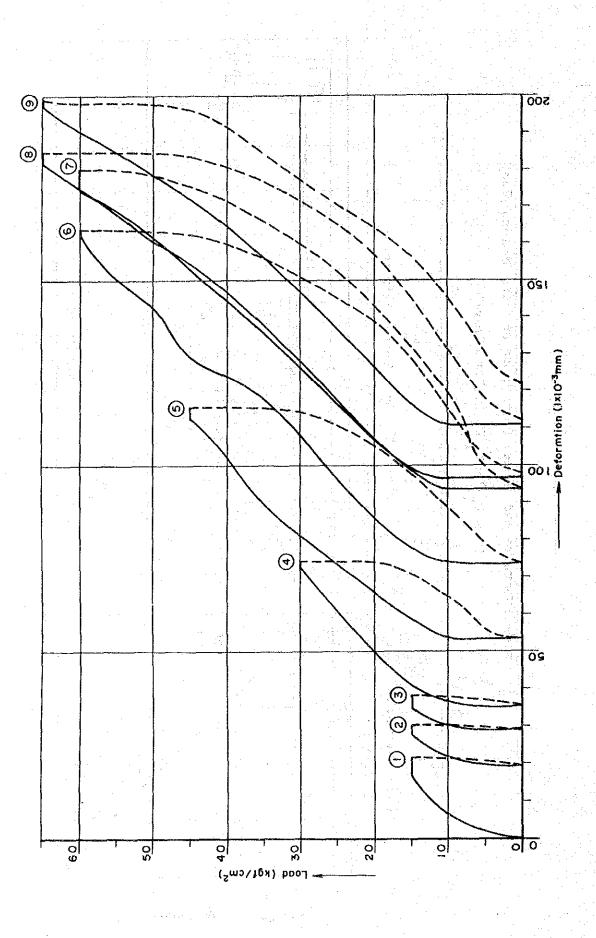


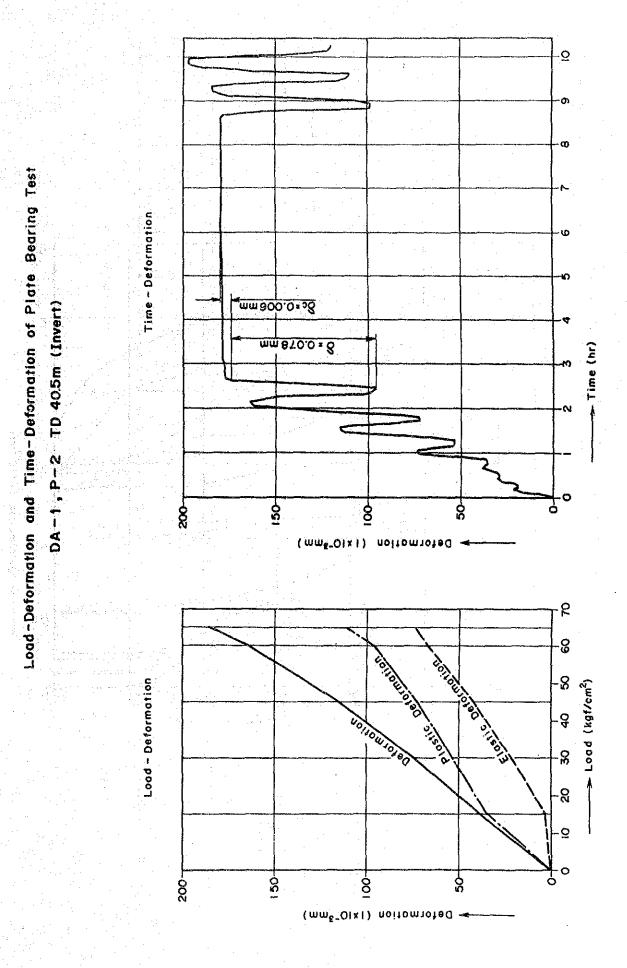


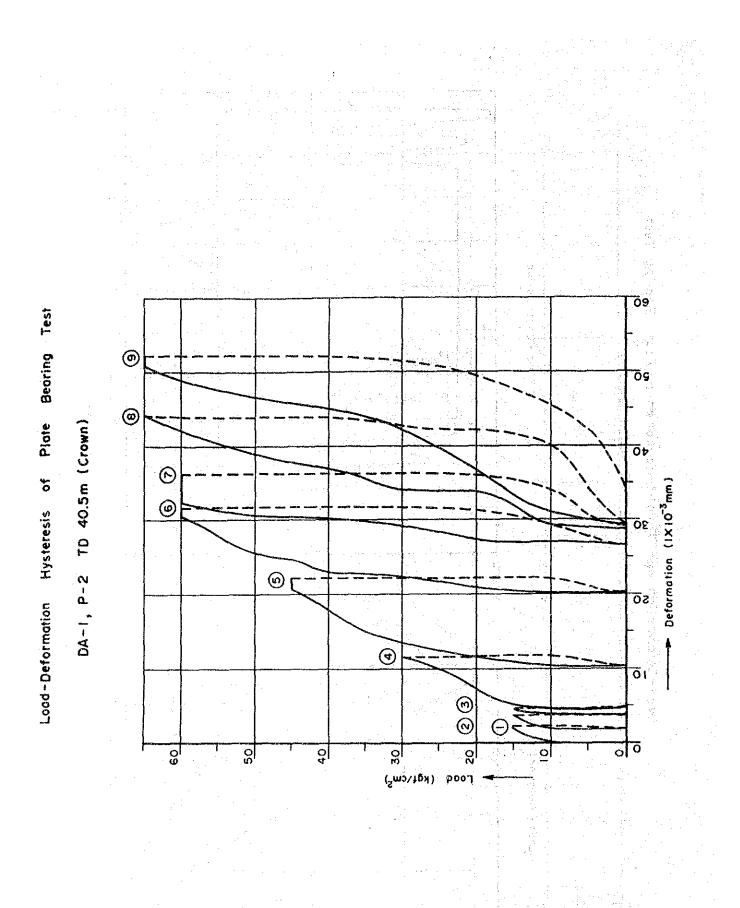
: 3 - 99

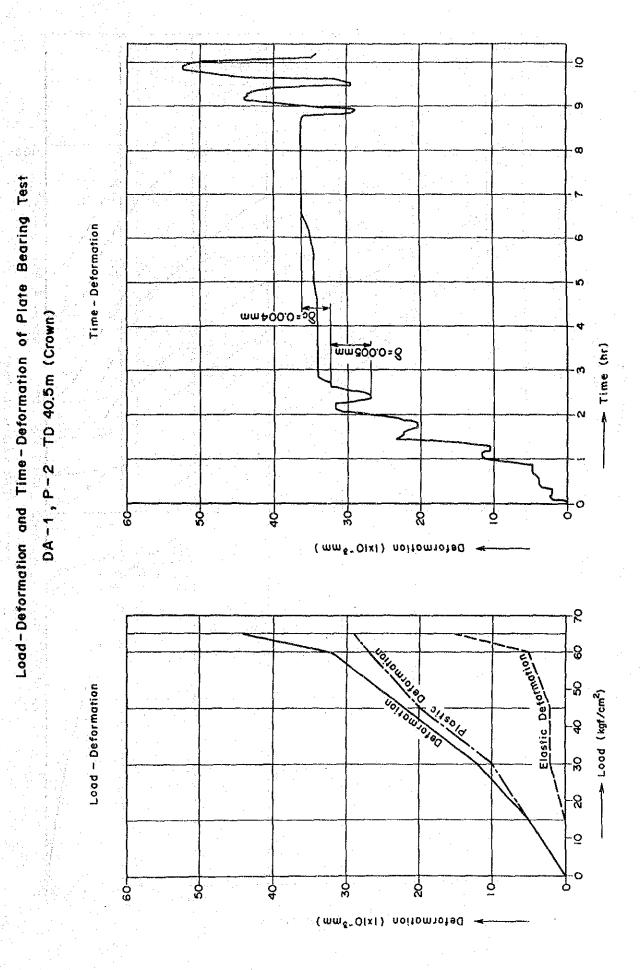
Load-Deformation Hysteresis of Plate Bearing Test

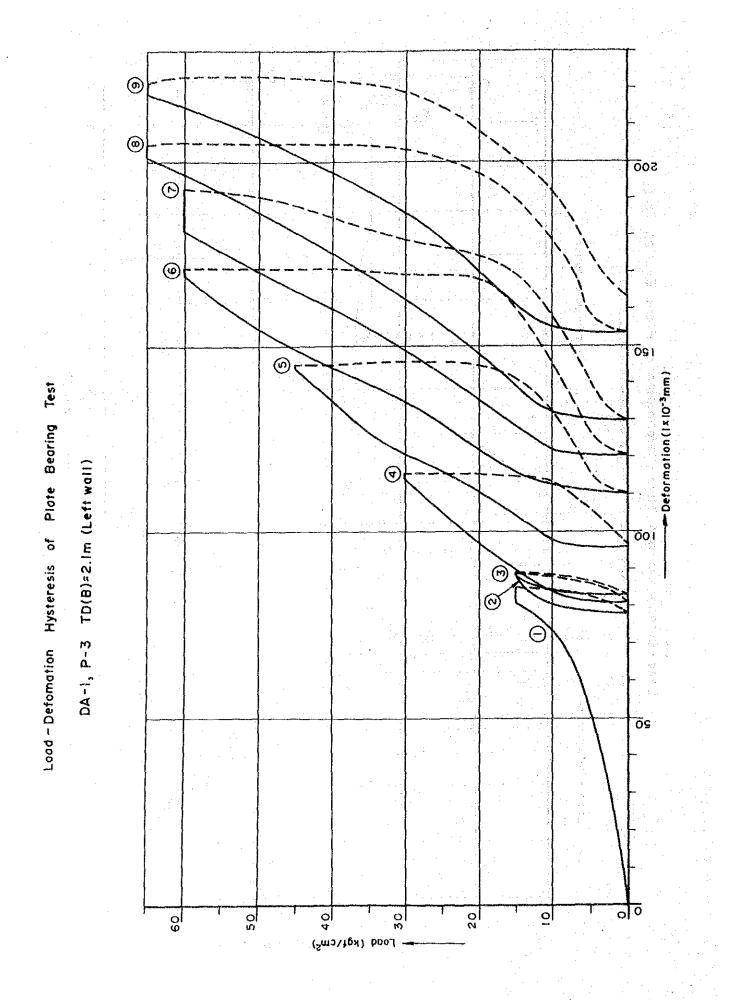
DA-1, P-2 TD=40.5m (Invert)

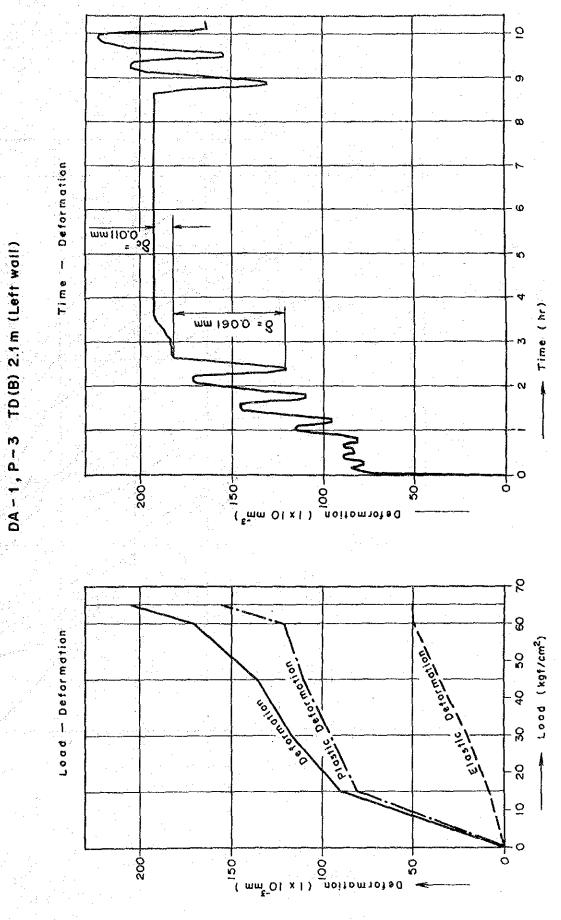






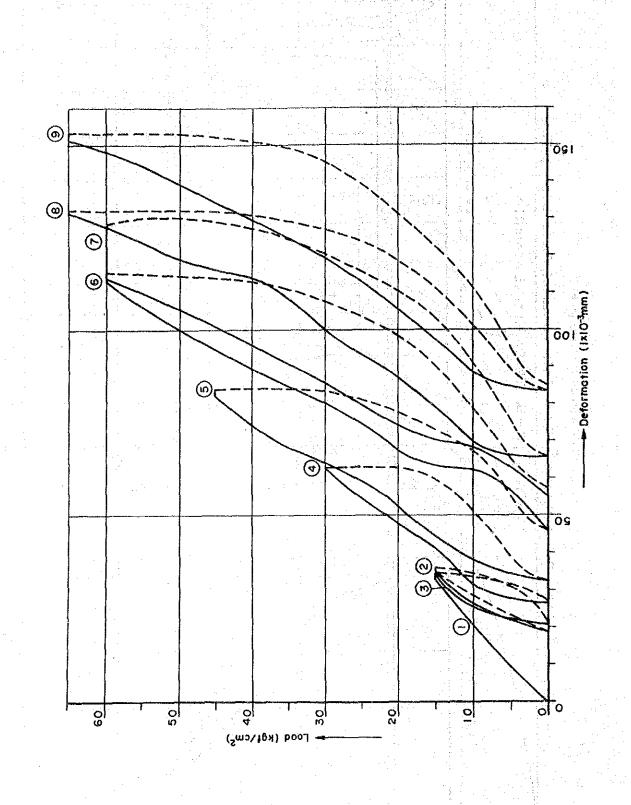


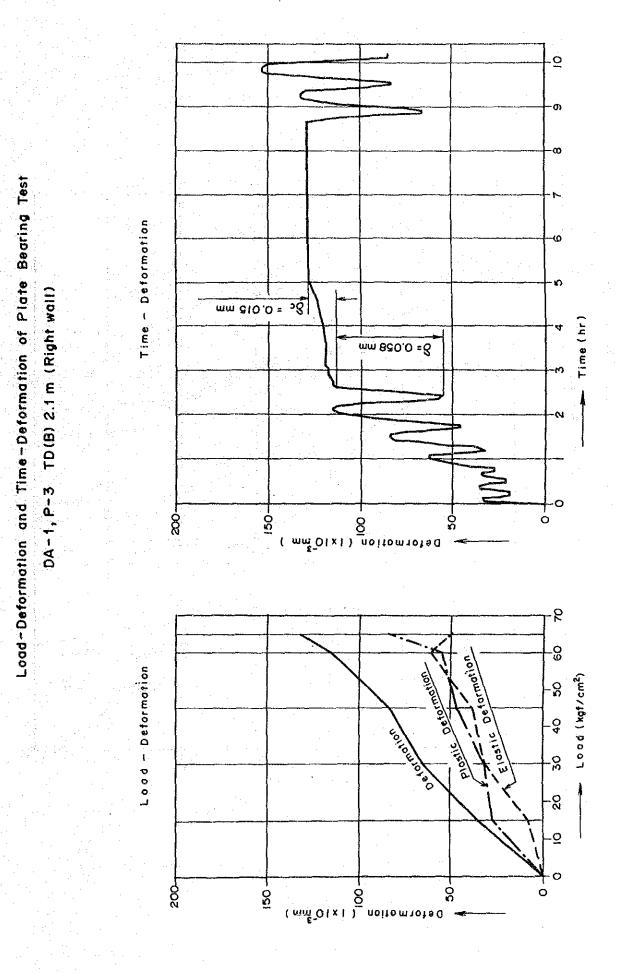




Load-Deformation and Time-Deformation of Plate Bearing Test DA-1, P-3 TD(B) 2.1 m (Left wall) Load-Deformation Hysteresis of Plate Bearing Test

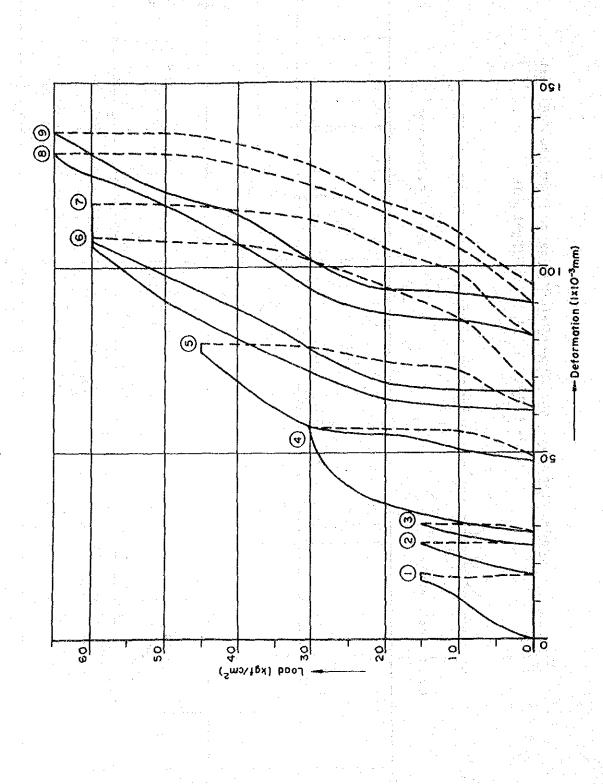


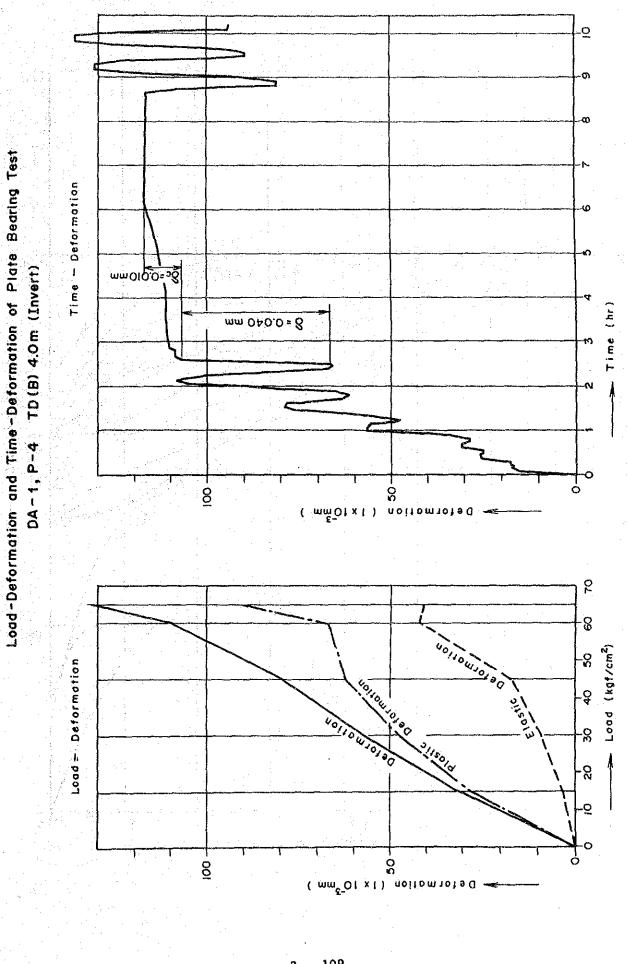


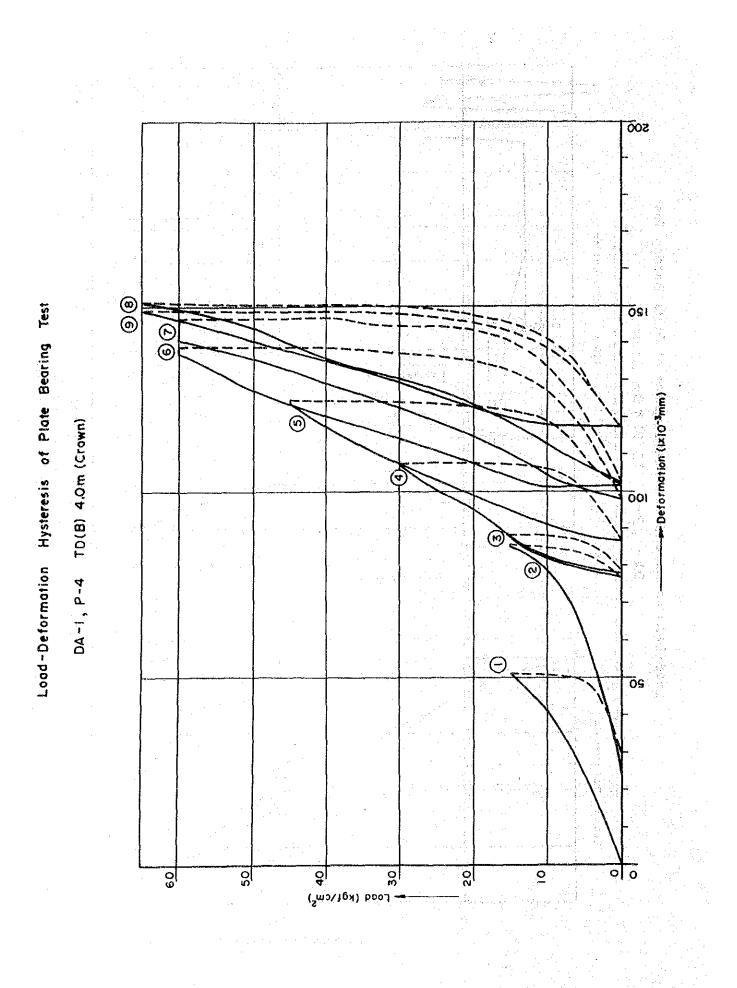


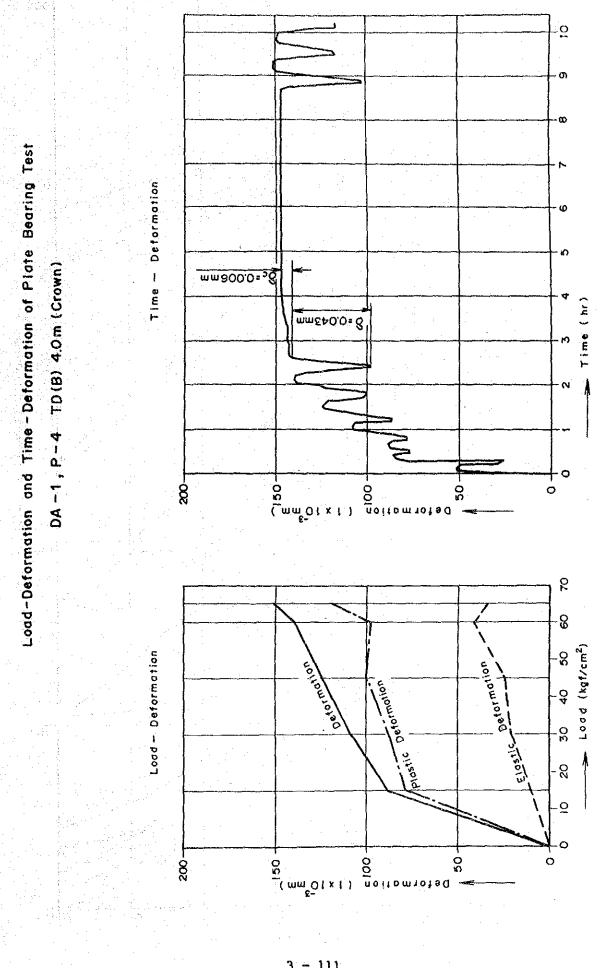
Load-Deformation Hysteresis of Plate Bearing Test

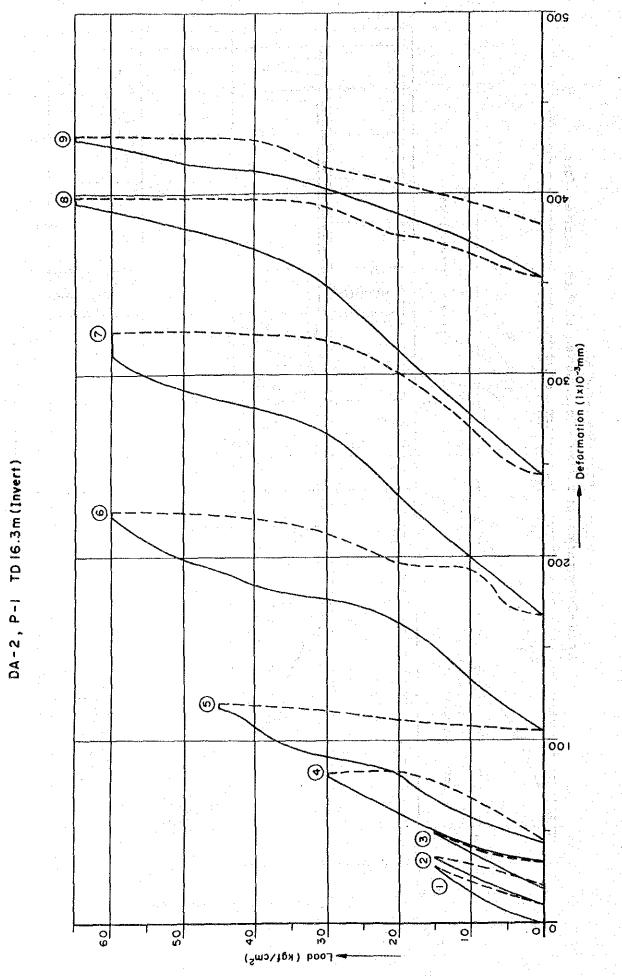
DA-1, P-4 TD(B)=4.0m (Invert)



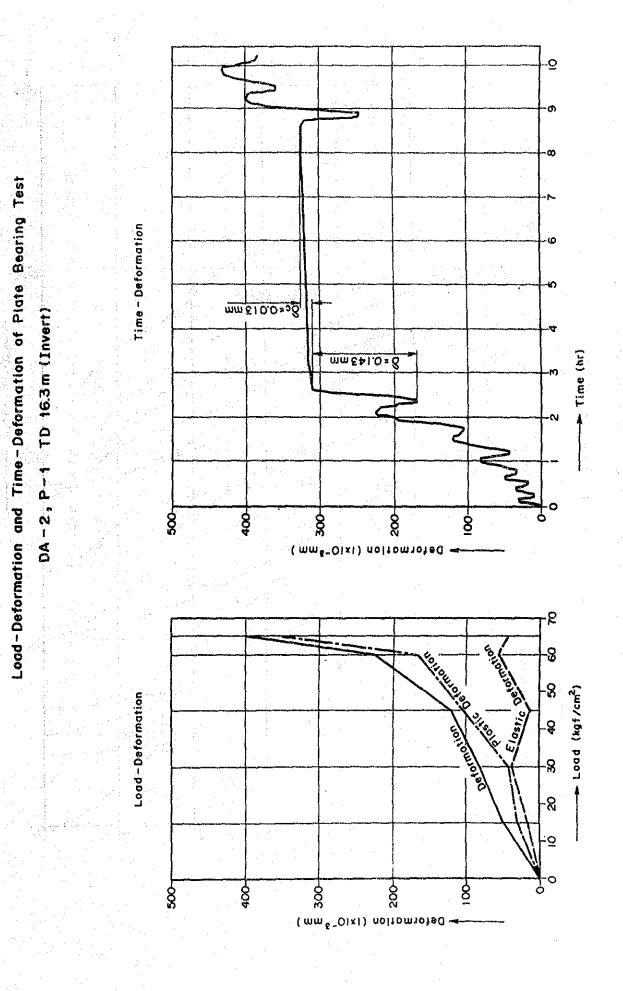






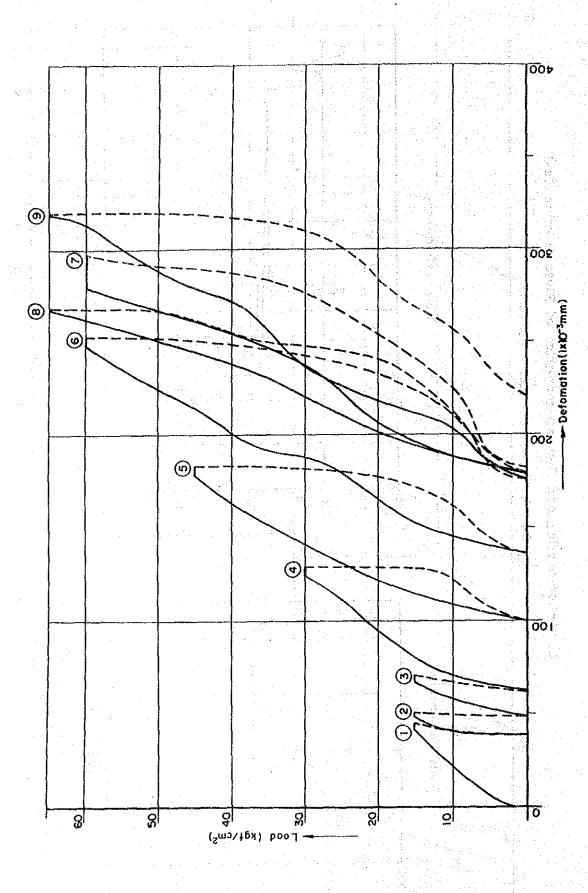


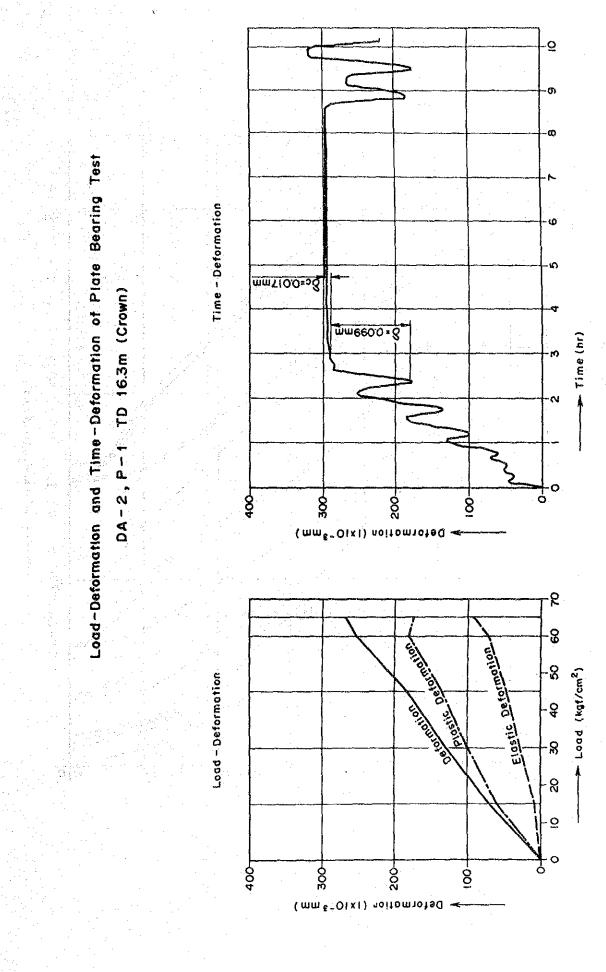
Load-Deformation Hysteresis of Plate Bearing Test



Load-Deformation Hysteresis of Plate Bearing Test

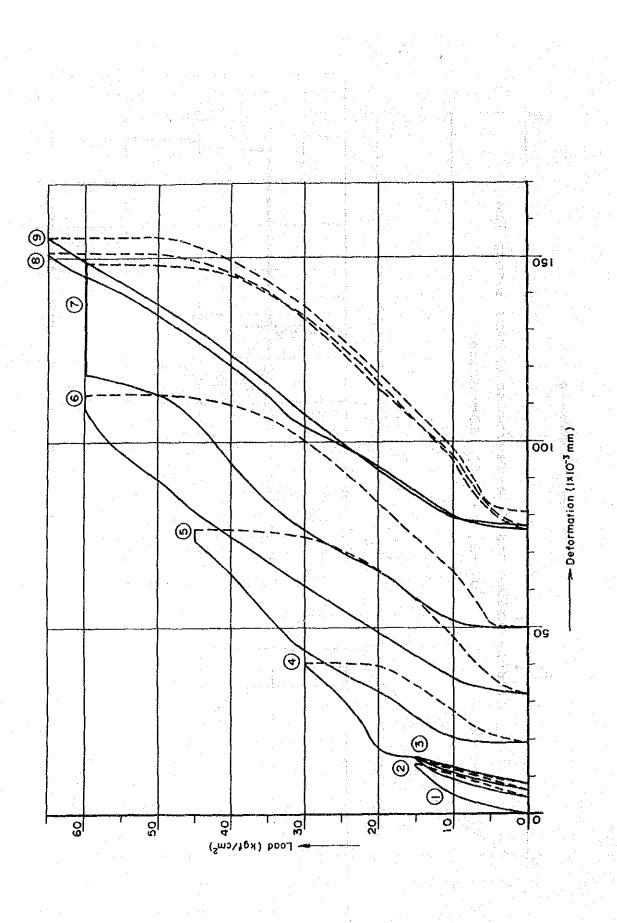


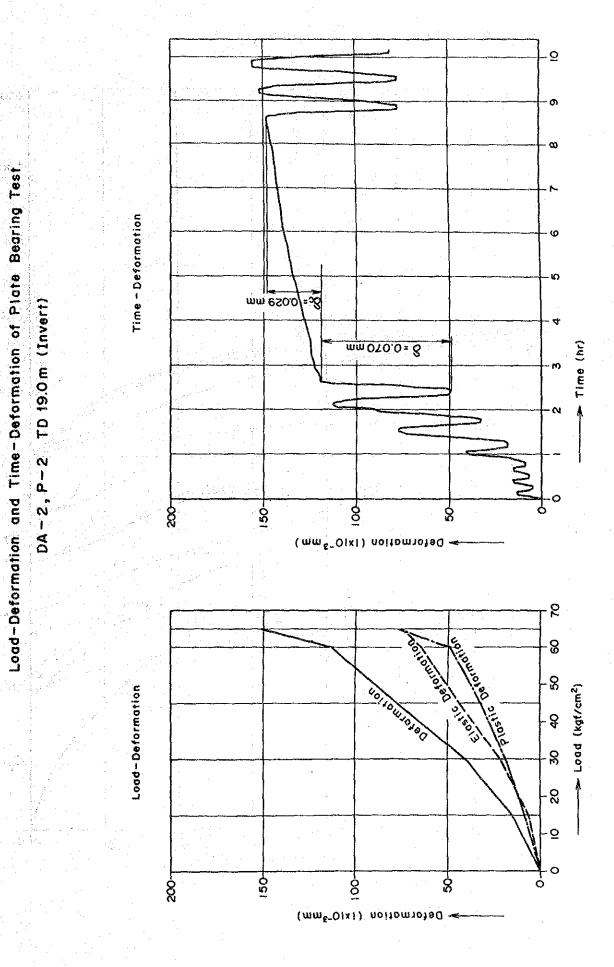




Load - Deformation Hysteresis of Plate Bearing Test

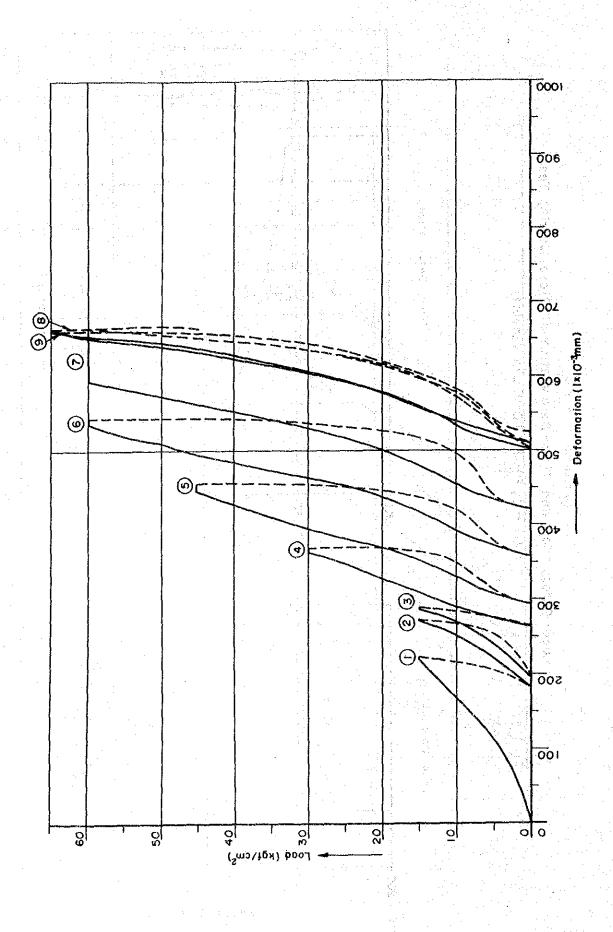
DA - 2 , P- 2 TD 19.0m(Invert)

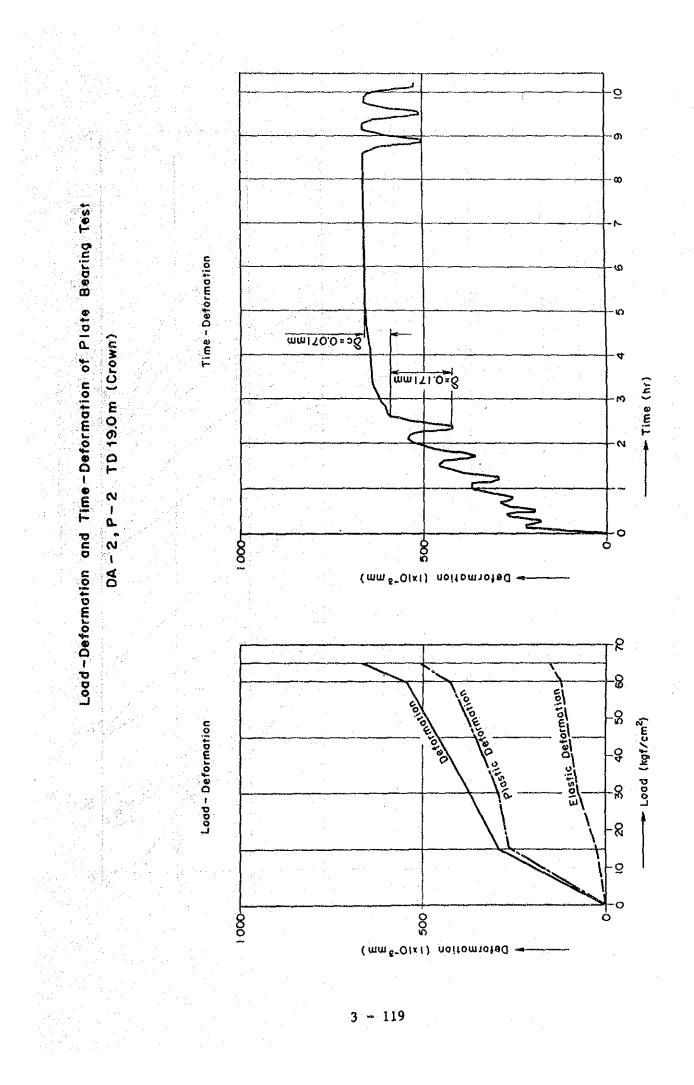




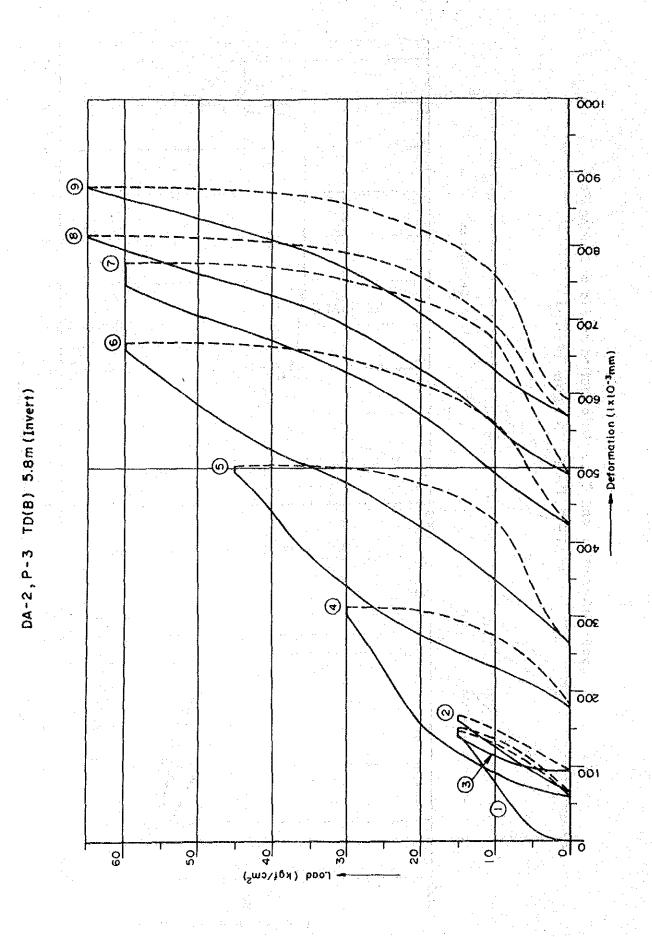
Load-Deformation Hysteresis of Plate Bearing Test

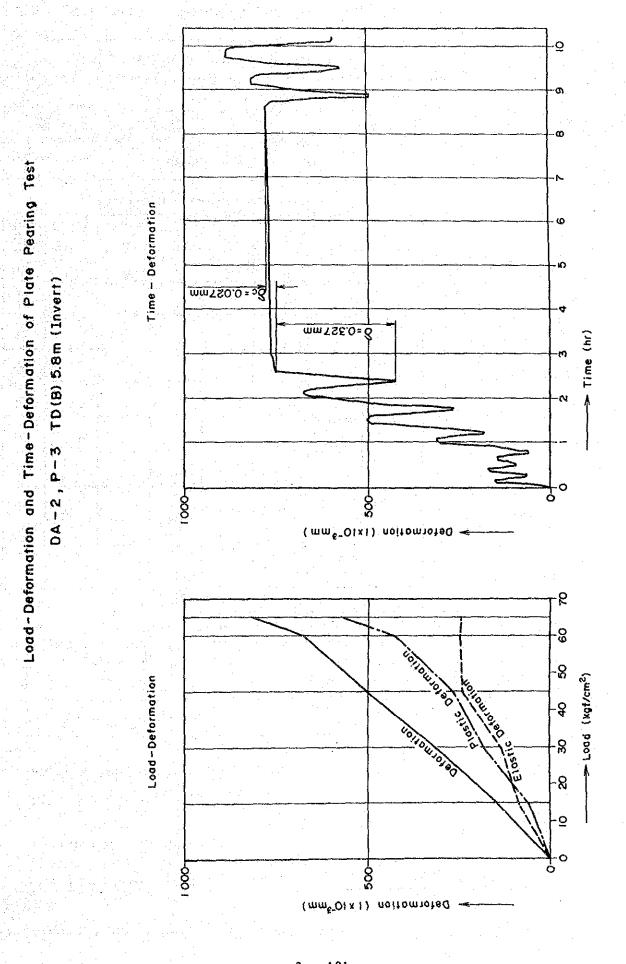






Load-Deformation Hysteresis of Plate Bearing Test





Lood Plat Geo	Location Ing Radius logicat Ci k Grade	<u>a = /</u> lassificat	<u>5 cm</u>			20.0m olite Ø	Date Mer	g Point <u>Invert</u> asured <u>24 Nov 1988</u> 1 by
Stress		e formatio		asuremen 10 ⁻³ mm	1 () () () () () () () () () (1		
(kg/cm²)	5	δŧ	50	Σδ	Σδρ	Rem	orks	B
15	6	3	3	6	3			Stress
15	3	2	1	6	4			dp 50 Deformation
15	5	2	and a state	9	7			<u> </u>
30	11	9	2	18	9		in Arrita	5
45	21	19	2	30		Creep	Creep	Deformation
60						Deforma-	Foctor Ct (%)	
60	<u>35</u> 42	<u>36</u> 30	-1 12	46 5-2	10			Time
65	(61)	(59)	(2)	(71)	12	$\frac{19}{C1 \cdot \frac{5c}{5}}$	45 × 100	ð : Total deformation
	43	<u> 85 </u>	5	<u> </u>	17	1	× 100	Sp : Plastic deformation
65	47	43	4	64	21	= 45		25" : Cumulative total deformation 25p : Cumulative plastic deformat
				a daga da ang				δc : Creep deformation
			Coe	fficients	Relat	ed to D	eformatio	n
1	Modulus	formatio		Tongenti	al Mo	dulus of	Elosticit	y Secant Modulus of Elasticity
		(kg ¹ /cm²		Et (kg	′an²)	Stress	Levei (ke	
	271,	.400		251.5	00	2	0~65	327,400
D c V AF	ж Е = <u>{</u>	$\frac{1-\gamma^2}{2\alpha}$	<u>Δ</u> F <u>Δ</u> W ο (0.2~(ο (μς)	$\frac{(1-\sqrt{2})}{2}$	a : Plat Geformat	Colculatio e radius on Increme rmation inc	(cm) nt due to	ΔF Deformation

3-10-6 Plate Bearing Test Results and Data Sheet

				ING TI						SHEET (1) cological lassification <u>(</u>	o. 1: Aito	
oodi ladiu	Location ng Plate s	<u>d =</u>	15 cm	n Dat	e Mea	sured _	24N	it Invel bv: 1988 gcm² Measu		assification (ock Grade 2)	M: D	and an and a second
	Capacity Diamete	the second s	. 2 4 cm	<u>ou</u>		errore V						
	60	•	100000		• • • • •						11년 1월 28일 - 11일 11일 - 11일 - 11일 11일 - 11일 - 11	
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	Stress (kg/cm ²) 8 8	:###	in an			† • • • • • • • • • • • • • • • • • •	· · · · ·		 State of the second seco	1	γ	
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	ť			<u></u>								
· .	0	2 TI	4 Ime Elo	6 spsed (hi	(8 '}	10	•	(I)		Side		
				attern		nple)	· · · ·	Invert	ᠵᠯ᠇ᠵ	Loading	Plate	
	Time	Stress	Jack		Detorm			(x 10 ⁻³ mm)				1.
ime	Elopsed	(kg ^f /cm ²)	Pressure (ko ¹ /m ²)	O R		iauge Re		<u>0+@</u> +0 23	Σδ	Rema		
	0			0	0	0	e	0	0			
	2	5	·					2.7	<u>2.7</u> 4.7		یة در دو مربع مع د م	-
	4	10	:	<u> </u>	2	/ 2	<u></u>	2	<u> </u>			-
	10	15		0	0	0		0	6.4			
·	12	5		- z	- 2	-1		-77	4.7		en 21 - Souria Romandouri	
	14	0		- Z 0	- /	- 2		- Z 0	2.7			
	20	10		4		3		1,3	4			-
	22 26	15		3	/	<u>2</u> 0	n agin An an an	2 0.3	6.3			-
	28			- 1	/	- /		-1	ۍ ع	8		
	30	0		- Z	~ /	- 1		-1.3	the second s	(11)		
1>	<u>34</u> 36	0		0		2		0	4.0	(4)		
	38	15		ઝ	Ż	3		2.7	9,4	(0)		-
<u>2</u> 2	42 44	<u>15</u>		- 1	-1	- 2		-1.3	9.4	(9)	<u> </u>	-
	46	0		- 1	-1	-2		-1.3	6.8			
	<u> </u>	0 10		- /-	Q	0		-0.3	6.5 8.8			
	52	15		3	<u>2</u> Z	2		2.3	8.0			
	56	20		2	4	1		2.3	13.4			
	58 1:00	<u>25</u> 30		<u> </u>				2.7	16.1			-
3>	1:04	30		0	0	0		0	.18.1	(18)		
	1:06	20		- 2	0	2		- 0.7	. 7.4	<u> </u>		-
	1:08 1:10	10		- 4	-3 -4	- 2		-3	14.4	<u> </u>		
	1:12	0		- 4	-/	- <u>-</u> Z		- z.3	9.1			-
	1:16 1:18	0		- /	0	0		-0.3 0	8.8			
	1:20	20		2	2	2		3.7	12.5	l		
					· · · ·		танана 1	na an a		an a		· · ·

بحصني والمستحدين									DATA S	
Tim●	Time	Stress	Jack		Defor			x 10 ⁻³ mm)		D
	Elopsed	()o/cm ²)	(kg ^f /cm²)	ÐR			Army	K3	IS	Remdrks
	1:22	30		2	2	4		2.7	15.2	
	1:24	35		4	2	4		3.3	18.5	
	1:26	40		7	3	5		5.00	23,5	
	1:28	45		8	3	6		5.7	29.2	
<4>	1:32	45		0	3	0		1	30.2	(30)
	1:34	40		0	0	0		0	30.2	
	1:36	30		- 2	- 4	-3		:3	27,2	
	1:38	20		-6	- 4	- 7		-57	21.5	
	1:40	10		- 6	-5	- 2		-4.3	17.Z	
	1:42	5		- 3	- Z	- 3		-2.7	14.5	
	1:44			-6	- 7	- Z		-3	11.5	
	1:48	_		0	0	-1		-0,3	11.2	
	1:50			0	0	0		0	11.2	
	1:52			1	3	0		1,3	12.5	
	1:54	30		8	3	5		5,3	178	
in an an	1:56	40		5	4	7		5.3	23.1	**************************************
	1:58		<u>}</u>	6	4	8		6	29.1	
	2:00	50		3	5	6		4.7	3.8	
	2:02	55		5	4	8		5.7	39.5	
	2:04	60		2		9		6	45.5	
<u> <5 ></u>	2:08			0	0			0.3	4.08	(46)
<u>~~</u>	2:10	50		0	0			-0.3	45.5	
	2:12	40	$\frac{1}{1}$	4 1	0	-4		- 1,3	442	
	2:14	30		- 6	- 2	- 8		-5.3	38.9	
	≹÷	frankriger and			- 4	-9			30.Z	
	2:16	20		-13	-5			-8.7		
	2:18	10		_ 16	-3	-10		-10.3	19.9	
	2:20	1		- 13	han the			-17.3	9.6	
77	2:22	the second distance of		-0		0		- 0	9.6	(10)
<6>	2:26			0	0	0	a	0		
	2:28	_		3	0	0	· · · · · · · · · · · · · · · · · · ·		10.6	
	2:30	20	<u> </u>		4			2	20.9	
	2:32	30	<u> </u>	15	6	6		10	30.9	
	2:34	**************************************		11	9	1.3		10.3	41.2	
<u></u>	2:36	50	<u></u>	10		12		10,5	5/5	(52)
<7>		60	<u> </u>	12	7	12		0,3	51.8	
	2:40			0	0	Ó		0.7	52.5	
	2:43					+		0,3	52.8	
	2:48			0	0			0.7	53.5	
	2:53	60	┟┈┈┙		<u> </u>	0			54.5	
1947 - 1957 - 1977 	2:58	60	<u></u>		$-\frac{1}{1}$	+		1	55.2	
	3:03			<u> </u>	0			0.7		
	3:08	60		1-1-		0		0.7	55.9	 A second s
	3:18	60		2	1	1-4		1.3	57,2	
	3:28	60	1.4.2	2		$1 \leq l$		1.3	58,59,8	

ma	Time	Stress		Olsplac		matlan Gauge R		x 10 ⁻³ mm)	1944 C 1977	Remarks
	Elcosed		(kd/cm ²)	the second s		Qe		23	58	
	4:08	The second s		3	Z	2		2.3	\$2.1	
	4:38	60		2	Z	Z		2	641	
	5:08	60		2	1	2		1.7	15.8	
	5:38	60		1	0	2		1	66.8	
a second and a second	6:08	60		/	1	2		13	68.	
	6:38	60		1	0			0.7	688	
	7:08	60		2	1	1		0.7	19.5	
	7:38	60		1	0			0.7	702	
	8:08	60		2	/			0.7	70.9	
87	8:38	60		2	0	1		0.3	712	(71)
	8:40	50		0	0	-1		- 0.3	70.9	
	8:42	40	ļ	- 3	0	- 4		- 2.3	68.6	
	8:44	30		- 7	- 3	-15		- 8.3	603	
	8:46	20		- 15	- 6	-15		-12	48.3	
	8:48	10		-22	-9	-22		-17.2	30,6	
	8:50	5		- 18	-9	- 7		-11.3	19.3	
	8:52	0		- 7	-4	- 2		- 4.3	15.0	
(9)	8:56	0		- Z	- 2	- 4		- 2.7	12.3	(12)
	8:58	10		0	0	0		0	12.0	
10>	9:00	20		8	3	4		5_	17,3	(17)
<u> </u>	9:02	·	·	12	4	7		7.7	25	
117	1			11	7	12		10	35	(35)
	9:06	50	·	8	7	9		8	43	
12 >	9:08	60		5	S	6		5.3	48.3	(48)
<u> </u>	9:10	65		7	5	S		5.7	54	
115	9:14	65			1	1	}	1	55	(55)
	9:16			0	- 1	- 2		-/	54	
	9:18	50		- 2	- Z	- 2		- 2	52	
	9:20	40		- 6	3	5		- 4.7	47.3	
	9:22	30		- 7	-4	- 7		-6	41.3	
	9:24	20		-8	- 5	- 7	1	- 6.7	24.6	
:	9:26	10		-9	-0	-9		8	Zh.6	
	9:28	5		-9	<u>-5</u>	- 7	t	-7	19.6	
	9:30	Ō		- 3	-3	-3	1	- 3	16.6	
14>	9:34	0		0	<u> </u>	0		0	16.5	(17)
<u>~~</u>	9:36	10		0	0	1	1	0.3	16.9	
153	9:38	20		5	2	2		3	19.9	(20)
	9:40	30		10	3	6		6,3	26.2	
16 >	9:42	40		12	. 9	17	1	12.7	28.9	(39)
	9:44	50		19	9	10	1	12.7	51.6	ing an an an ann ann ann ann an ann an ann an a
17>	9:46	60		10	-7-9-	10	 	9.7	61.3	(61)
	9:48	65		4	///	2	<u> </u>	2.3	63.6	
182	9:52	65		0	0	0	<u> </u>	0	63.6	(64)
<u>رمب</u>	9:54	60		0	0	0		0	63,6	
	9:56	50	:	0	$-\underline{v}$	0	<u>}</u>	0	63.6	
					<u> </u>		- 12	_ L		

	PL	ATE	BEARII	NG TE	รา	ali (janu yang a di kang a di kang a		n an fair ann ann an Anna ann ann ann ann ann ann	DATA S	HEET (4)
	Time	Stress	Jock		Detor	mation)	x 10" ³ mm)		
Time	1 At	1 1 1 1 1 A		Dispice	ement	Gauge Re	ading	0 + 0 m	C	Remarks
go o Consta		(kg/cm2)	Pressure (kg/cm²)	<u>e</u> e		Ø®)	23	Σδ	
	9:58	40		~ 2	-1	- 5		- 27	60.9	
and and a second se	10:00			- 5	- 2	-6		- 43	56.6	
	10:02	the second s		-12	- 4	-14		-10	46.6	
	10:04	the second s		- 15		-16		- 12.7	33.9	
	10:06			- 10		<u> - 6 </u>		- 7.7	26.2	
	10:08	the second s			- 3			- 47	21.5	
<u> </u>	10:12	0		0	-1	0		0,3	21.2	(2/)
					/	┼───┤		<u></u>		<u> </u>
		<u> </u>	+	<u> </u>		╁╍╍╍╌┤				
	<u> </u>	}	 			╆╼╾-┼	······			1
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	<u></u>	<u> </u>		<u> </u>	<u> </u>					
		<u> </u>		<u> </u>	 	<u> </u>			ļ	
	19. <u>11 - 2</u> 11 ^{. 11} . 12	}			}	┼╌╌╌┤		<u> </u>	<u> </u>	
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<u></u>				<u> </u>	<u> </u>	+			<u> </u>	
		<u> </u>		┟╍╍╍╍					1	
<u></u>	 	<u> </u>	<u> </u>	<u> </u>		╬╌╍╌─┤		<u> </u>		
		 	$\frac{1}{2}$	+	<u> </u>			<u>}</u>		
		<u> </u>		+			 		1	
				+						
				1		1				
		1								

PLATE BEARING TEST RESULTS DA-1, P-1, TD 20.0M Measuring Point Crown Test Location Date Measured 24 Nov. 1988 Looding Plote Rodius 0 = 15 cm Ophio lite Geological Classification Measured by Deformation Measurement Results (x10⁻³ mm) Deformation Stress Remarks kg2m2) Σδ 5.00 50 50 δ ress 1 15 ີ່ຈ 24 18 24 18 Deformation 15 JD Se 9 5 4 27 22 15 6 3 28 9 19 δc 30 58 39 16 Z342 Jeformation 45 Creep 49 91 58 Creep 33 16 Deforma-Factor tion 60 SE(x10mm) Cf (%) 15 73 49 64 122 Time 54 (64) 44 10 127 60 83 10 54) (10) (137)Ct = - 5 x 100 δ | Total deformation 65 92 9 64 55 147 de Elastic deformation $=\frac{10}{54} \times 100$ δp Plastic deformation 65 94 $\Sigma\delta^{-}$: Cumulative total deformation 59 57 Z 151 25p : Cumulative plastic deformation = 19 Sc : Creep deformation Coefficients Related to Deformation Secont Modulus Tangential Modulus of Elasticity Modulus of Elasticity of Deformation Es (kg/cm²) Et (kgf/cm²) Stress Level (kg/cm2) (kg/an2) D 20~65 239.500 189,200 107,700 Modulus of Deformation, Modulus of Elasticity Calculation Formula D or E = $\frac{(1-\nu^2)}{2\alpha} \cdot \frac{\Delta F}{\Delta W} = \frac{\pi \alpha (1-\nu^2)}{2} \cdot \frac{\Delta \sigma^2}{\Delta \delta}$ a : Plate radius (cm) V : Poisson's ratio (0.2~0.3) Deformation AF ; Load Increment (k) ΔW : Deformation increment due to ΔF $\Delta \sigma$: Deformation increment due to $\Delta \sigma'$ Δσ: Stress increment (kg/cm²) Remarks

dius <u>a z</u> dius <u>ck</u> Copacity	<u>7-1, P-1, TD 2</u> <u>15 cm</u> Da <u>200 ton</u> Ma <u>200 ton</u> Ma <u>200 ton</u> Ma	te Measured	24.11	t Crown	2 0	CIUCICUI AL INTO	
60			· <u>///// · · ·</u>	<u>ightm²</u> Measur	R	pological assilication <u>Ophiolita</u> ock Grade <u>2812 :(b)</u>	and an an and
	, have a c c c c c c c c c c c c c c c c c c	18			uun		
40- 00 X	2 6		na af sin sin Tari	\mathbb{C}			
		iff it		n n thai a sh		Side	-
20- A						\bigcirc	
				Side		<u>d</u> e	
0 2 0 1	4 6	8 10			<u>କ୍</u> ମିତ୍ର	Side	
and the second	Time Elopsed (h Iding Pattern	and the second)	Invert		Loading Plate	
Time Stress	1 4440	Deformation	The second s	(x 10 ⁻³ mm)			Ì
e Elopsed	Pressure Disploc	ement Gauge	Reading	<u>0+0</u> +0 83	IS	Remarks	
0 0		0	0	0	0		
2 5	- 2	4	28	10	10		
6 15	5	13	9	9	23		
10 15	0	<u> </u>	2 5.	<u> </u>	24.3		
14 0	0	- 3 -	6	- 3.0	17.6		
<u> </u>	0		0 5	0	17.6]
22 15	2	<u>8</u> 2	8	6	25.9 26.9		-
28 5	0	- 21 -		- 1,31	25,6		
30 0 34 0	- /	- 5 -	5	-3.7 -0.3	<u>21.9</u> 21,6	(22)	
361 10		3	2	1.7	230	and the second	1
38 15 > 42 15			5	3.3	26.6	(28)	4
44 5		- 2 -	/	-/	26.6		
46 0 50 0			6 0	- 4	19.0		
52 10 54 15	0		/	47	23, W 28		
56 20	5	- 2	7 7	7	28		1
58 25 1:00 30	5 4		0	11.3	46.0 56.3		-
> 1:04 30	2	2	3	1.7	58	(58)]
1:06 20	5	- 2 -	0	1.7	<u>۶۶.7</u> کک		
1:10 5	- 4	-17 -	12	- 11	47		
1:12 0 1:16 0	- 1	- 8 -	0	- 5.3 0	41.7		-
1:18 10 1:20 20	- / 0	0	9	-0.3	49.1		
11.201 20		14	/: 	<u>_</u>			

	PL	Ale	BEARII	NG TE	51			DATA	SHEET (2)
	Time	Stress	Jack		Detor		(x 10"3 mm)	and the second data was not as a se	
Time	Elopsed		Pressure (ko ^f /cm ²)			auge Reading	1 <u>0+@</u> 13 *3	IS	Remarks.
A CALLER Constant	1:22	30		8	14	15	12.3	61.4	
	1:24	35		3	15	5	7.6	69	
	1:26	40		6	16	10	10.6	29.6	
	1:28	45		7	15	10	10.6	90.2	ور من معرف العربي العربي المحمد العربي المحمد العربي العربي العربي العربي العربي العربي العربي العربي العربي ا
247	1:32	45		0		0	0.3	905	(91)
	1:34	40		6	0	Ő	0	90.5	<u> </u>
	1:36	30		0	0	0	0	90,5	
	1:38	20		0	-5	- 3	- 2.7	028	
	1:40	10		-4	-13	-12	-9.7	78.1	
	1:42	5		- 8	- 25	-13	-15.3	62.8	
	1:44	0			- 8	- 7	- 5.3	57.5	, <u></u>
	1:48	ō	1	a	0	4	0	57.5	
	1:50	10	1	Ó	Ö	0	0	.575	
میں کی میں در دیکھ جارت در روانہ	1:52	20		ð	11	S	5.3	62.8	
9 1 K.	1:54	30	State State	5	20	13	12.7	255	
	1:56	40		2	16	14	12.8	87.8	
	1:58	45		3	9	6	6	938	
<u> </u>	2:00	50		5		7	7.3	101.1	
	2:02	55		1 .	10	9	9.	110.1	
	2:04	60		6	12.	9	9,7	119,8	
(5)	2:08	60	{		<u>× ×</u> 	1 7 1 1 1 1	17	121.5	(122)
	2:10	50		ð	0	0	0	121.5	
<u> </u>	2:12	40	<u> </u>		0		- 0.7	120.8	
	2:14	30		- 2	- 9	- 2	- 6,3	114.5	
in a start and a	2:16	20		1		-11	- 8	106.5	
	2:18	10		- 3	-10		-/2.3	942	
	2:20	and the subscript of the local division of t		- 8	- 20 - 29		-18	76.2	
	2:20			-1	- 4	1 1	- 3	13,2	
(6)	2:26		<u> </u>	-i		- 4	0		- (73)
767	2:28	10		0	0	0	0	10.Z	
	2:30	20		0	10		37	76.9	
	2:32	30	+	5	21	1.5	13.7	90.6	
	2:34	40		8	18	12	1 2	103,0	
	2:34	50		11	(13	113	114.6	
<u> </u>	2:38	60		7 8	14	13	12.3	126.9	(127)
<u> </u>	2:40	60	-	0	 			122.9	
	2:43	the second s		$\left \begin{array}{c} 0 \\ 1 \end{array} \right $	2	2	17	1 129.0	· 1
<u> </u>	2:48		+	0		0	0.0	1 121.1	
	2:53	60	+			e	0.3	1,30.3	-
<u></u>	the state of the s		+	2	0	0	0.3	130.5	
	2:58	60	+	0		1	0.7	131.2	
	3:03	60				0	0.3	131.5	,
	3:08	60		1-0		0	0.0	12/5	
<u></u>	3:18	60			<u>a</u>		0	131.5	-
	3:28	60 60		1-0-	- <u>0</u>	0		13/3	

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	}							x 10 ¹³ mm)		
Time	Tì∕n●	Stress		Olsploc	Deloti	Contraction of the local division of the loc		<u>x 10 - mm</u>		Remarks
	Elopsed		(ko/cm²)			0 e		ن 2	IS	11 Ψ 111 Ψ 1 Τ Ψ 1 Ψ 11 Ψ 1 Ψ 1 Ψ 1
	4:08	60		0	1	0		0.3	1.71.8	
	4:38	60		0	0	0		0	101.8	
	5:08	60		0	1	1		0.7	132.5	
	5:38	60		/		0		0.7	143.2	
	6:08	60		0	/	1		0.7	1.34.9	
	6:38	60		1	2	. 1		1.3	1352	
	7:08	60		0	1	1		0.7	135.9	
	7:38	60		0		0		0.3	136.2	
	8:08	60		1	0	1		0.7	136.9	
< 8 >	8:38	60		0	0	0	<u></u>	0	1.76.9	(137)
	8:40	50		0	0	0		0	106.8	
	8:42	40		0	1	- 1		0	136.9	
	8:44	30		- 1	2	-9		- 2.7	1342	
	8:46	20		- 4	-23	-10		-12.3	121.9	
	8:48	01		- 8	-23	- 13	ang mananan ang	-147	107.2	
	8:50	5		-10	-30	- 20		- 20	87.2	
	8:52	0		-1	- 8	- 3	i de la composición d	-4	83.2	
(9)>	8:56	0		0	0	0		0	83.2	(83)
	8:58	10		0	0	0		0	83.2	
(10>	9:00	20		0	17	8		8.3	91.5	(92)
<u></u>	9:02	30		5	20	14		13	104.5	
(1)>	9:04	40		7	18	13		12.7	117.2	(117)
	9:06	50		7	15	11		11	1282	
(12)	9:08	60		7	16	11		11.3	139.5	(140)
	9:10	65		4	2	8	-	6,3	145.8	
(13)	f	65			2,	0		0.7	146.5	(147)
	9:16	60		0	0	0		0	146.5	
	9:18	50		0	0	0		0	146.5	
	9:20	40		0	-4	_گ-		>	143.5	
	9:22	30		- 4	-9	~ 9		- 7.3	136.2	en e
	9:24	20		-5	-17	-11		- 11	1252	
	9:26	.10	····	- 8	-22	-14		-147	110.5	
	9:28	5		- 7	- 20	-11		-12.7	97.8	
	9:30	0		- 2	-10	- 5		- 5.2	92.1	
(14)	9:34	0		0	0	0		0	92.1	(92)
	9:36	10		0	0	0		0	92/	
15>	9:38	20		0	13	4		5.7	97.8	(98)
<u></u>	9:40	30		4	20	14		12.7	110.5	
16 >	9:42	40		8	17	12		12.0	122.8	(123)
	9:44	50		7	45	13		11.7	134.5	
175	9:46	60		7	- 25	11		11	1455	(146)
	9:48	65			6	6		5	150,5	
(18)	9:52	65		0	0	0			150.5	
107	9:54	60		0	0	0		1	150.5	
	9:56	50	······································	0	1	0		D	150.5	

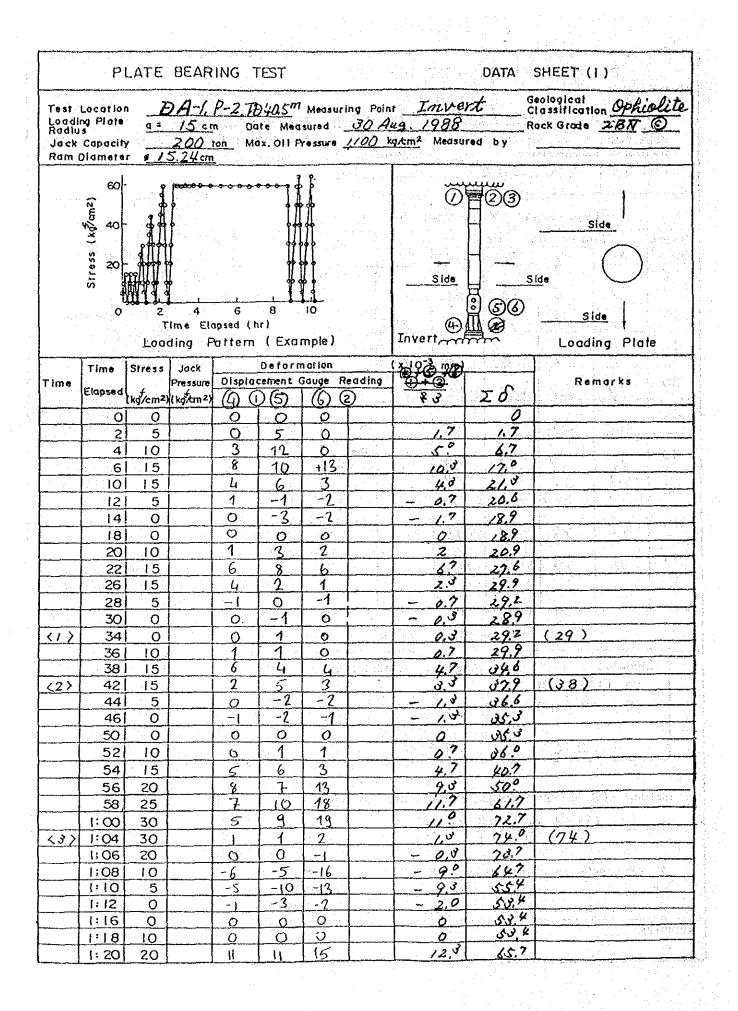
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	٩L	ATE I	BEARII	NG TE	ST				DATA S	HEET (4)
Time	Time	Stress		Displac	The second s	Gauge: Re	ading	x 10 ⁻³ mm)	zδ	Remarks
		(kg/cm2)	Pressure (kg/cm²)	Øæ)0	9 6	}	23	20	
	9:28	40	<u> </u>	2		-5		- 2	1485	المركز
	10:00			- 2	-10	-9		-7	141.5	· · · · · · · · · · · · · · · · · · ·
	10:02			- 8	-15			-10.7	130.8	
	10:04			- 9	- z7	-15		17	113.8	
	10:06	Statement Statements	<u></u>	- 8	- 23	-14		-15	98.8 93.8	
100	10:08	the second s		-2	- 9	- 4		- 5		(94)
(///)	10.12					0	·····	0	93.8	
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	t	<u> </u>	1	1	1	1	1	1		1.

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PLATE BEARING TEST RESULTS DA-1, P-2, TD40.5m Measuring Point Invert a= 15 cm Date Measured 30 Aug. 1988 Test Location Looding Plots Rodius <u>a = 15 cm</u> Ophiolite Measured by Geological Classification Rock Grade 287 Deformation Measurement Results (x10⁻³ mm) Deformation Stress **Remarks** (katem2) 25 250 50 \mathfrak{T}_{p} 8 Stress 15 21 Z 19 21 19 Deformation 15 δo δe 29 30 11 10 ደሪወ 15 9 3 35 6 38 δο 30 39 18 74 53 21 Daformation 45 Creep Creep 62 73 42 115 20 Deforma-Factor tion w 60 õē (xiOmm) 67 96 cf (%) 90 63 Tima 174 78 81 60 8 6 84) 87) 3) (180) 93 5 : Total deformation ct = - 5 x 100 65 92 185 74 18 de : Elostic deformation 111 = - x100 δp : Plastic deformation 65 88 25 : Cumulative total deformation 79 9 199 120 Bob. : Cumulative plastic deformation de : Creep deformation Coefficients Related to Deformation Tangential Modulus of Elosticity Secant Modulus Modulus of Elasticity of Deformation Es (ka^f/cm²) Et (kg/cm^2) Stress Level (kg2m2) D (ka/am2) 163.500 20~65 81,200 137.400 Modulus of Deformation, Modulus of Elasticity Calculation Formula D or E = $\frac{(1-v^2)}{2a}$, $\frac{\Delta F}{\Delta W} = \frac{\pi a (1-v^2)}{2}$, $\frac{\Delta \sigma}{\Delta \delta}$ V : Poisson's ratio (0.2~0.3) 0 : Plate radius (cm) Deformation ΔF : Load increment (M) ΔW : Deformation increment due to ΔF $\Delta \sigma$: Deformation increment due to $\Delta \sigma'$ A o : Stress increment (kg/cm²) Remarks



	Pι	ATE	8EARII	NG TE	EST			DATA S	SHEET (2)
	Time	Stress	Jack		Detor	mation	(x 10-3 mm)		
l'ime	Elopsed	(ht/cm²)	Pressure (Kg/cm²)	the second second		auge Recolling		I.S	Remarks
	1:22	30		8	16	24	15.03	81.0	an a
	1:24	35		6	7	13	8.6	89.6	
	1:26	40		9	11	19	100	102.6	
	1:28	45		्र	7	16	10?	112.6	
(4)	1:32	45		2	2	4	2.7	115.3	(115)
	1:34	40		0	0	0	0	115,0	
	1:36	30		1	-1	-3	- 10	114.3	
	1 38	20		-5	-6	-17	-93	105 .	
	1:40	10		- 12	-13	-25	-16.7	88.3	
	1:42	5		- 7.		-12	-10?	78.V	
	1:44	0		-5	-6	-4	- 50	73.3	
<u></u>	1:48	0		1	0	-1	0	733	
	1:50	10		0	0	1	0,3	70.6	
	1:52	20		10	12	15	12.5	856	
<u></u>	1:54	30		20	21	26	22.3	108.2	
<u> </u>	1:56	40		10	13	23	15.0	123.5	
<u>.</u>	1:58	45		3	4	11	6.	129.5	
	2:00	50		5	14	20	10?	142.5	
	2:02	55		12	1	11	80	150,5	
	2:02	60		10	8	17	11.7	162.2	-
122	2:04	60		0	0	3	10	163.2	(163)
<u><\$></u>			<u> </u>				- 0,3	162.9	
<u></u>	2:10	50		0	0		- 3, 3	F	
	2:12	40				-5	- 90	159.6	<u></u>
	2:14	30		-3	-8	-16	- 4-	150.6	
<u> </u>	2:16	20		-9	-5	-22	-120	1286	
	2:18			-19	-19	-35	- 24.0	143	
	2:20		ļ	-13	-14	-18	-117	102.6	
	2:22	0		-5	-7	-2	- 4.7	97.9	
<u> <6></u>	2:26	0		1	-2	-2	-1.7	96.2	(96)
	2:28	10		0	0	0	0	96.2	
	2:30	20		8	+1]	12	10,3	106.5	· · · · · · · · · · · · · · · · · · ·
<u>, È sua</u>	2:32	30		12	18	2.9	19.7	126.2	
- <u></u>	2:34	40	L	10	15	28	17.7	143.9	
	2:36	50		15	15	23	17.7	161.6	2. ~11)
72	2:38	60		10	8	20	12.7	1743	(174)
	2:40			5_	3	2	3.3	177.6	
	2:43	and the second s	<u> </u>	0	0	1	0,3	177.9	
, 	2:48	60	1	0	0	0	0	177.9	
	2:53	60	<u> </u>	0	0	1 1	0.3	178.5	
	2:58	60		0	0	0	0	1782	<u> </u>
	3:03	60		0	0	0 0	0	178.2	
	3:08	60		1	0	1_1	0.7	178.9	
	3:18	60		0	1	0	0,3	179,2	
	3:28	60	1.1.5	0	0	0	0	179.2	مەرىپەر « مىلىدىنە» مادەسە» يىلىدىنە بىلەر يەرىپى بىرى بىرى بىرى بىرى بىرى بىرى بىرى
	3:38			0	0	0	0	179.2	

		Stress	1004		Detori	mation	(10-2 mp)		
Time	Tim●	Stress	Pressure	Olspiac			ading	0+0	5	Remarks
	Elopsed		(kc/cm ²)	**************************************			F	23	Σδ	
	4:08	60		0	0	0		0	179.2	
	4:38	60		0	0	0		0	179.2	
	5:08	60		ŏ	0	0		0	179.2	
	5:38	60		Ŏ	1	1		0.7	179.9	
	6:08	60		-1	0	0		- 0.3	179.6	
	6:38	60		ò	0	0		0	179.6	
	7.08	60		0	1	0		0.3	179.9	
	7:38	60		0	0	0		0	179.9	
	8:08	60		0	0	0		0	279.9	
<8>	8:38	60		0	0	Ŏ		0	179.9	(180)
(87	8:40	50		-3	0	-2		-1.7	178.2	
		+		-8	-4	<u> </u>		- 7.0	171.2	
	8:42	40		-1	-15	-18		-11.0	1599	
	8:46			-14	-12	-26		- 17.3	142.6	
	f	20		-17	-19	-34		-23,3	119.0	
	8:48	10		[-23	-17		-20°	99.0	
<u></u>	8:50	5	· · · · · ·	- 20				-60	93.3	an a
	8:52	0		-5	-7	-6		O	93.3	(93)
(9)	8:56	0		0	0	0			93.0	
	8:58	10		0	0	0		0	106.0	(106)
(10)	9:00	20		10	15	14			128.3	(7007
	9:02	30_	· ·		20	30		220		(147)
$\langle 11 \rangle$	9:04	40		12	15	28		183	146.6	(/4/)
	9:06	50		10	11	21		140	160.6	(175)
<u><!--2--></u>	9:08	60		15	_1/	17		14.3	174.9	11/13/
······	9:10	65		· 5	6	9		6.7	181.6	(100)
<u><13></u>	9:14	65		6		1		30	184.6	(185)
	9:16	60	<u>.</u>	0	-1	-1		0	184.6	
	9:18	50	<u> </u>	0	.1	-1	<u> </u>	0	184.6	
	9:20	40		-5	-1	-6	· · · · ·	- 40	180.6	
	9:22	30		-6	-6	-16		-93	171.0	
	9:24	20		57	-14	-24		-140	157.0	
	9:26	10		-20	-21	-38		- 26,3	130.7	
	9:28	5		-10	-13	-17		-1,3,3	117.4	
	9:30	0		-5	-6	-5		- 50	112.	
<14>>	9:34	0		0	-2	-2		- 1.3	110,8	(///)
	9:36	10		0	0	0		0	110.8	
<15>	9:38	20		13	16	18		15.7	126.5	(127)
	9:40	30		12	17	31		20.0	146,5	
(16)	9:42	40		10	17	27	ļ	18.0	1645	(165)
	9:44	50		10	11	19		133	177.8	
(17)	9:46	60		12	K	17		12.3	190!	(190)
	9:48	65		7	6	9		2.0	197.4	
(18)	9:52	65		1	l.	2		1,3	198.7	(199)
101	9:54	60		0.	-2		1	_ 10	1977	
	9:56	50		-1	1	-1	1	-0,3	197.4	

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	PL	ATE I	BEARII	NG TE	ST	· ·		· · · · ·	DATA S	HEET (4)
Tìme		Stress	Jack Pressure (ka/cm?)		thems	nation Gauge Re			Σδ	Remarks
	9:58	40		-7	-2	-9		- 6.0	191.4	
<u></u>	10:00			-11	-10	-21		-140		
	10:02			-6	-12	-23		- 13.7	177.4	
	10:04		┟╴╴╴	-14	-20	-33		- 19.0	144.7	
	10:06				-14	-20		-15.0	129.7	
	10:08	and the second days of the secon		-7	-10	-6		- 77	1220	
(19)	10:12			-1	-2	-2		-17	120,3	(120)
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PLATE BEARING TEST RESULTS DA-1, P-2, TD 40.5m Measuring Point Crown Test Location Loading Plate Radius Date Measured 30 Aug. 1988 0=15 cm Ophialite Measured by Geological Classification Rock Grade Deformation Measurement Results (x10"3 mm) Deformation Stress Remarks (kg/cm²) 5. δp 25 Σδρ δ Stress 15 2 0 2 2 2 Deformation 15 δe δp 2 0 2 4 4 280 15 1 0 1 5 5 δc 30 ځ 7 2 12 10 **Deformation** 45 Creep Creep 12 2 10 22 20 Deforma-Factor tion M 60 SE (xiOmm) -ی 22 27 Ct (%) 12 Time 02 3 Z 5 60 9) 7) (2)(36) 29 80 4 Ct = - 5 x 100 5 : Total deformation 65 15 15 29 0 44 Je : Elastic deformation δp · Plastic deformation ×100 ۍ 65 23 \$2 5 25 : Cumulative total deformation 18 36 = 80 ESp : Cumulative plastic deformation $\delta \mathbf{c}$: Creep deformation Coefficients Related to Deformation

Modulus of Deformation	Tangential Modu	ulus of Elasticity	Secant Modulus of Elasticity
D (kg/cm²)	Et (kg/cm²)	Stress Level (kg ² cm ²)	Es (kg ^f cm ²)
370,400	856,000	20 - 65	809.700

Modulus of Deformation, Modulus of Elasticity Calculation Formula

D or E = $\frac{(1-V^2)}{2a} \cdot \frac{\Delta F}{\Delta W} = \frac{\pi \alpha (1-V^2)}{2} \cdot \frac{\Delta \sigma}{\Delta \delta}$

Deformation

0 : Plate radius (cm) V : Polsson's ratio (0.2~0.3) AW: Deformation increment due to ΔF AF : Load increment (kg) $\Delta \sigma$: Deformation increment due to $\Delta \sigma$ Δ σ : Stress Increment (ko/cm²)

Remarks

adi Idiu Ick	Location			ING TI					DATA	SHEET (1)
ck		n Đ	A-1P	-2.70	40.5m	Measuri	ng Poin	t Crown	G G	eological Lassification Ophialite
	ng Platé s	q =	15 ci	n Dat	e Mea	sured _		30 Aug. 1	<u>988 </u> R	lock Grade 2BN C
	Capacity Diamete	/ <u> </u>	<u>200</u> 5.24 cm	ton Max	e Oli Pi	185511F8	<u>,100 x</u>	g/cm² Measu	red by	
			¥		9				and the second	
	60	`	proses a		0010				冒(2)3)	
	Stress (kų/am²) N Å		Î	•		1	1997			Ans There of the second second
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je s		2	· 4	6 ∋pséd (hr	8 .\	10	1	Ô	<u>h 96</u>	Side
				attern		mole)		Invert		Loading Plate
			<u></u>		Deform		مراجع المراجع ا	(x 10 ⁻³ mm)	<u></u>	Lougany (1910
n 8	Time		Jack Pressure			Sauge R	and the second division of the second divisio	()+(2+3)		Remarks
	Elopsed		(kg/cm ²)	designed the second sec		3		23	Σδ	
	0	0		0	0	0		0	0	
	2	5		0		0		0		
	4	10 15		0		0		0.3	<u> </u>	
	10	15		0	4	0		0.3	2.3	
	12	5		0	0	0		0	Z.3	
	14	0		/	0	0		-0.3	2.0	
	18	0	1.11 (1.11) 1.11	0		0	·	0	2.0	a ya angina na shira in barbara. Mari
	20 22	10		0	0	04		0	<u>2.0</u> 3.7	
÷	26	15				<u> </u>		0	3.7	
	28	5		0	0	0		0	3.7	
	30	0		0	0	0		0	3.7	
	34	0		2		0		0	3.7	(4)
	<u> </u>	10		0	0	0		<u>D.3</u> 0.3	<u>4,0</u> 4,3	
2.2	42	15		0	1	0		0.4	4.7	(5)
	44	5		0	0	_0		0	47	
	46	0			0	0	h	0	4.7	
	<u>50</u> 52	0		0	0	0		0	<u>4.7</u> <u>4.7</u>	
	54	15	{	0	<u> </u>	0		0.7	<u> </u>	
	56	20		0		2		2.0	7.4	Andre and a state of the state of the
	58	25	ļ	/	3	3		2.3	9.7	
	1:00	30	ļ		0			67_	114	(1.2)
32	1:04 1:06	30 20	 			0		0.3	117	(12)
	1:08	10		$\frac{\partial}{\partial t}$	0	0		0	11.7	
	1:10	5		0	- 2	0		- 0.7	110	
	1:12	0		-/	- /	0		-0.7	10,3	n per per se a se
	1:16	0	<u> </u>	0	0	0	<u> </u>	0	103	17 S. 3. (34) (37)
	1:18 1:20	<u>10</u> 20		0	<u></u>	0	<u> </u>	0	11.7	

Time	Time Elopsed		Pressure					$\frac{10^{-3} \text{ mm}}{2}$	ς Σδ	Remarks
			(kg/an-)		And in case of the local division of the loc	0.0			ويرجرها بترزنانا بجارا والمتكا	
	1:22	30		2	3_			20	13.7	
<u></u>	1:24	35		0	<u> </u>	2		1.3	15.0	
	1:26	40		2	4	3		3.0	180	
	1:28	45		2	4	2		2.7	20.7	
<u> </u>	1:32	45				2		1.6	223	(22)
	1:34	40		0	0	0		0	22,3	
	1:36	30	ļ	0	0	0		0	22.3	
	1:38	20	 	0	0	2	<u> </u>	0	2.2.3	
	1:40	f	 	0	-1	0		- 0.3	22.0	
	1:42	5			-3	0	14 C.	- 1.0	21.0	
	1:44	0		0	-2	0	· ·	- 0.7	20.3	
	1.48	and the second second	<u> </u>	0	0	0		0	20.3	<u></u>
	1:50	10		0	0	0		0	20.3	
in a start and a start a start Start a start a	1:52	20		0	2	0	*	0.7	210	
а — 777 Добра	1:54	30		0	4	0		1.3	22,3	
	1:56	40		0	2	0		0.7	23.0	
	1:58	45		/ ·	2	0		1.7	24.7	
	2:00	50		2	0	1		1.0	25.7	
	2:02	55	1	2	2	3		2.3	28.0	
	2:04	60	 	2	4	2		2.7	20.7	
(5)	2:08	60		2		0		1.0	31.7	(32)
	2:10	50		/	1	0		0	31.7	
	2:12	40	<u> </u>	0	0	0		0	31.7	
	2:14	30		0		0		0	31.7	
	2:16	20		l		/		- 0.3	· · · · · · · · · · · · · · · · · · ·	+
	2:18	Contraction of the local division of the loc		0	-6	╞━┉━┛┉┓┠┉╸	<u></u>		29.4	+
	a de la companya de l	10		┟╌────┤	and the second se	0		-2.0		·
	2:20	The second s		0	<u> </u>	0		- 1.7	377	
	2:22			- e	- 2	-1		- 1.0	26.7	(14)
(6)	2:26	Station Station Station		0	0	0		0	26.7	(27)
	2:28	10			0	0	• •	0.3	27.0	
	2:30	فالمسيبين أكجارهم والمراجع	 	0		0		03	27.3	
*****	2:32			0	<u> </u>	0		17	29.0	
	2:34		<u> </u>	0	4	0		1.3	30,3	· {
	2:36		<u></u>	-0		<u>e</u>		0.3	<u>vo.6</u>	(22)
(7)	2:38	فمصبح جردت صعا		0	3	2		1.7	<u>323</u>	(32)
	2:40		 	0	_0	0		<u> </u>	32.3	
	2:43			0		0		0	32.3	+
	2:48		<u> </u>		<u></u>			10	3.3.3	
	2:53			0		2		0.7	340	+
	2:58	Street, or St	ļ	0	0	0		0	340	+
	3:03			0	0	10	<u></u>	0	34.0	
	3:08			0	0	0			34.0	
	3:18	60	 	0	0	0	منتجنب	<u> </u>	340	
	3:28			0	0	<u>e</u>		0	340	-
	3:38	60	L	0	0	0		0	34.0	

	PL	ATE	BEARII	NG TI				x 10" ³ mm)	DATA S	HEET (3)
-	Time	Stress	Jack		and the second	mation		چن <u>ہ محمد ش</u> تی میں م	l de la serie de la serie Este serie de la	
Time	Elupsed	Ĵ.		Displacement Gauge Reading			$\frac{0+2}{2}$	$\Sigma \delta$	Remarxs	
• • • • • • • • • • • • • • • • • • •	ļ		(ka/cm²)	OR	20	<u> </u>		23		
	4:08	60		0	0	- 0		0	340	
	4:38	60		0	0	0		0	34.0	
	5:08	60			0	0		0.3	(243	
	5:38	60		1	0	0	1.1.1	03	346	
	6:08	60			0	0		0.4	350	
	6:38	60		2		/		1,3	36.3	
	7:08	60		0	0	0		0	363	
<u></u>	7:38	60		0	0	0	le de la compañía de	0	363	
	8:08	60		0	0	0		0	36.3	
	8:38	60		0	0	0		0	363	(36)
<u>< 8 ></u>	8:40							0	36.3	
		50			0	0		0	30.3	
	8:42	40			0	0				
	8:44	30		_0_		-1		<u> </u>	36.3	
	8:46	20		0	0	-/		~ 0.3	36.0	
	8:48	10	· · ·	0	-5	-/		- 2.0	04.0	
	8:50	5		0	-7	3	· · · · · · · · · · · · · · · · · · ·	- 3.3	00.7	
	8:52	0		-1	0	-3		- 1.3	29.4	
(9)	8:56	0		0	-2	0		- 0.7	28.7	(29)
	8:58	10		0	2	0		0.7	294	
(10)	9:00	20		0	14	~/		4.3	33.7	(34)
	9:02	30		0	-3	4		0.3	34.0	
(11)	9:04	40		0	S	4		3.0	27.0	(37)
	9:06	50		0	3	3		2.0	39.0	
12>	9:08	60			2	6		3.0	42.0	(42)
121	9:10	65			· · · · · · · · · · · · · · · · · · ·	Z		z.0	44.0	
· · · · · · · · ·	<u></u>			<i>Q</i>	4					(44)
(13)	+	65			0	0		0		1.7.7.1
	9:16	60		0		0		- 0.3	43.7	
	9:18	50		0	0	0		0	43.7	and the second
	9:20	40		Q		0	·····	0	43.7	· · · · · · · · · · · · · · · · · · ·
	9:22	30		0	/	-2		- 1.0	42.7	
	9:24	20		0	-1	-1		- 0.7	42.0	
	9:26	10		_0_	-5	0		- 1.7	40.3	
	9:28	5		0	-14	-4		- 6.0	34.3	
	9:30	0		0	-8	-5		- 43	30.0	
14>	9:34	0		0	-1	-1		- 0.6	29.3	(29)
	9:36	10	[N	4			17	31.0	
15>		20	1	0	15	Z		5.7_	36.7	(37)
	9:40	30		0	10	6		5.3	42.0	
:16>	9:42	40		0	5	4		3.0	45.0	(45)
101	9:44	50		0	<u> </u>	3		1.7	46,7	
	9:46	60				5	·	4	49.0	(49)
17>				0	2			2.3		NT / /
	9:48	65			2	2		1.6	50.6	(63)
(18)	9:52	65		1	2	2		17	52.3	(52)
	9:54	60		0	0	0		0	52,3	

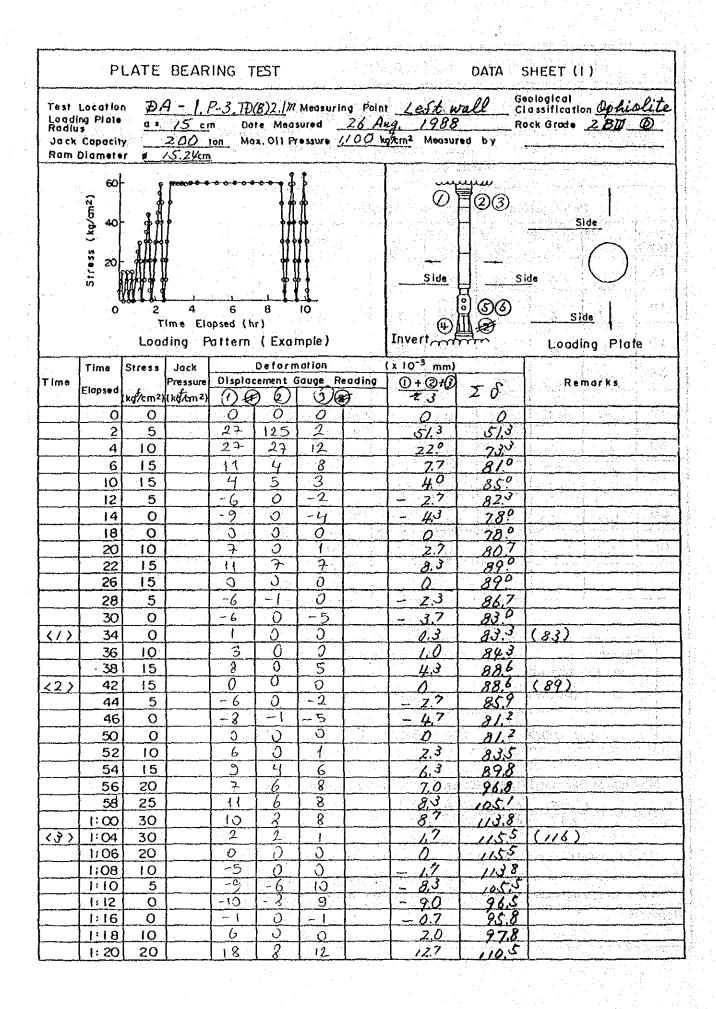
PLATE BEARING TEST

DATA SHEET (4)

	Time	Stress	Jack		Defors	nation	}	x 10 ⁻³ mm)			
Time	Elapsed	e en la companya de la			Displacement Gauge Reading				0+2/0		Remarks
		(kotm²)	(Kg ⁷ cm²)	D &	ŤØ	$\bigcirc $		<u>()+@</u> # 3	Σd		
	9:58	40		0	0	-1		- 0,3	520		
2.5 ₆ 0 1.1	10:00	30		0	0	-2		- 0,7	51.3	······································	
	10:02	······	and the second	0	-/	-1		- 0.6	50.7		
	10.04			0	-8	-3		- 3.7	1170		
	10:06	And the owner of the owner owne		Õ	-0	-4		- 3.3	<u>47.0</u> <u>43.7</u>		
	10:08			- 1	-10	-10		- 70	36.7		
1193	10:12			-1	-1	0	·····	-0.7	36.0	(36)	
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na an a							} 			· ····································	
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					<u> </u>	<u> </u>		}			
			<u></u>	 		1	<u> </u>				
			 		<u>+</u>	}	<u></u>				
<u></u>				<u> </u>	}	}	<u> </u>				
			}			<u> </u>	<u> </u>			-	
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la de la composición de la composición En composición de la c							 	<u> </u>		· · · · · · · · · · · · · · · · · · ·	
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						at an age				· · · · · · · · · · · · · · · · · · ·	
	16 35	<u></u>				<u> </u>	<u> </u>	· · · · ·			
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17		in a start									
		1.11			<u> </u>]	Ì			
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		<u> </u>	<u>}</u>				 			**************************************	
	<u> </u>	<u> </u>	<u> </u>				 				
				 							
	<u> </u>		<u></u>	 				<u></u>			

PLATE BEARING TEST RESULTS <u>DA-1, P-3, TD(B)2.1m</u> Measuring Point <u>Left Wall</u> <u>1= 15 cm</u> <u>1: 15 cm</u> <u>0 phiolite</u> Measured by Test Location Loading Plate Radius o = 15 cm Geological Classification Rock Grade Deformation Measurement Results (x10⁻³ mm) Deformation Stress **Remarks** (ký/cm²) Sp 25 250 5. 8 ess 15 85 78 85 78 7 Deformation 15 SP Se 5 89 83 Z ጄδα 15 - 2 89 81 6 8 δ_{c} 30 96 35 15 116 20 Deformation 45 Creep Creep 145 110 49 35 14 Deforma-| Factor tion 60 56(x10mm) Cf (%) 121 61 50 11 171 Time 52 9 61 182 60 18 9 11 63) (193) 130 72) $Cf = -\frac{\delta c}{\delta} \times 100$ 5 : Totol deformation 65 204 154 Se : Elastic deformation 50 24 74 = 11 ×100 **Sp** Plastic deformation 65 $\Sigma\delta^{-}$: Cumulative total deformation 68 58 10 222 164 = 18 25p : Cumulative plastic deformation de : Creep deformation Coefficients Related to Deformation Secant Modulus Tangential Modulus of Elasticity Modulus of Elasticity of Deformation Es (kg/cm²) Et (kg/cm2) Stress Level (kg/km²) (ka/an2) D 20~65 123,000 192,000 207.000 Modulus of Deformation, Modulus of Elasticity Calculation Formula Dor E = $\frac{(1-\nu^2)}{2\sigma}$, $\frac{\Delta F}{\Delta W} = \frac{\pi\sigma(1-\nu^2)}{2}$, $\frac{\Delta\sigma}{\Delta S}$ V : Poisson's ratio (0.2~0.3) 0 : Plate radius (cm) Deformation ΔW : Deformation increment due to ΔF AF Load Increment (kg) $\Delta \sigma$: Deformation increment due to $\Delta \sigma^*$ tΔa: Stress increment (kg/cm²) Remarks

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1.1.1. <u>- 1.1.</u> y	PL	ATE	BEARIN	VG TE	ST	DATA SHEET (2)					
Time i	Time	Stress			Defor	and the second	the state of the second se	x 10 ⁻³ mm)			
	Elopsed		Pressure (kg/cm²)			auge Re		$\frac{0+2}{2}$	IS	Remorks	
	1:22	30		13	3	10		10,3	120.3	۲۰۰۰ ۲۰۰۰ ۲۰۰۰ ۲۰۰۰ ۲۰۰۰ ۲۰۰۰ ۲۰۰۰ ۲۰	
	1:24	35		8	4	6		6,0	126.8		
	1:26	40		111	7	3		8.7	1355		
	1:28	45		10	Ĵ,	8		8,3	1438		
(4)	1:32	45		2	Э	2	*****	1,3	145!	(145)	
	1:34	40		0	0	0		0	145.1	_ <u>}</u>	
	1:36	30		0.	J	2		0.7	1458		
	1:38	20		-4	0			- 1.3	1445		
	1:40	10		- 19	- 9	-10	- <u></u>	-12.7	131,8		
	1:42	5		-22	-11-0	-16		- 163	115,5		
	1:44	0		-12	-3	0		- 5.0	110,5		
	1:48	0		1	<u>э</u>	0		-03	110.2		
	1:50	10		8	Э	9		Z.7	1129		
	1:52	20		16	1	11		93	122.2		
	1:54	30		16	3	14		12.7	1349		
	1:56	40		12	· 7-	9	а. 14	9.3	1442		
	1:58	45		8	5	3		5.3	149.5	a service and the service of the ser	
	2:00	50		8	5	3		5.3	154.8		
	2:02	55	1	9	7	5		7.0	161.8		
	2:04	60		10	3	4		7.7	169.5		
15>	2:08	60		3	0	2		1.7	171.2	(171)	
<u>~~/</u>	2:10	50		0	0	0		0	171.2		
	2:12	40		0	0	0		0	171,2		
	2:14	30		-5	3	0		- 17	169.5		
	2:16	+		-2	-6	4		- 1,3	168,2		
	2:18	10		-33	-18	-13		- 23.3	1449		
<u></u>	2:20	<u> </u>	<u> </u>	-20	-15	-19		- 18.0	1269		
	2:22			-15	10	-3	<u> </u>	- 60	120.9		
(6)	2:26	And in case of the local division of the loc		0	1 D	Ō		0	120.9	(121)	
~~~	2:28			5	2	3		1.7	122,6		
	2:30	-		20	8	10		12.7	17.63		
<del></del>	2:32	and the second se	1	15	10_	16		1.3.7	149.0		
	2:34		1	15	9	10		11.3	160,3		
2	2:36	and the second s	+	15	12	7		11.3	171.6		
(7)	2:38	_		14	1.11	5		100	181.6	(182)	
- 1 - 6	2:40		1	0	0	1		0.3	181.9		
<del></del>	2:43		1	2	1	4.		1,3	183 -		
	2:48		· [	0	0	0		0	1832		
	2:53		1	0	5.0	1.2		0	183. ²		
	2:58		-	1	5	.0.	1	0,3	183.5		
	3:03	a de la companya de l		17	1.0	10	1	0.3	1838		
	3:08			2	3	0	<u> </u>	1,7	1855		
	3:18	60		3	4	$\frac{1}{2}$		73	1878		
	3:28		-{	2	2	6	<u> </u>	3.3	191.'		
	3:38			$+\frac{z}{1}$	3		<del> </del>	17	192,8		

Time	Time	Stress	Jock	1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.	Deter	mation	(	x 10 ⁻³ mm)		
			Pressure	Displa	cement	Gauge R	ading	0+0+0	120	Remarks
	Elopsed		(ko/cm²)	Ø£	2	Q &	3	23	58	
	4:08	60		2	3			0	192.8	
	4:38	60		• •	0	9		0	192.8	
	5:08	60		)	्र	2		0	192,8	
	5:38	60		2	)	0		0	192.8	
A	6:08	60		J	0	0		0	192,8	
	6:38	60		2	0	0		0	192.8	
	7:08	60		Э.	<u> </u>	୍ଚ		0	192.8	
	7:38	60		Э	)	3		0	192,8	
	8:08	60		0	3	С.		0	1928	
(8)	8:38	60		0	0	3		0	192.8	(193)
	8:40	50		- 1	- 5	0		- 20	190.8	
	8:42	40		-9	- 8	-1		- 10	184.8	
· · · ·	8:44	30		- 8	-10	0		- 6.	,788	
	8:46	20		- 0	- 3	0		- 43	1745	
	8:48	10		-20	-17-	-13		- 16.7	1578	
	8:50	5	e alerticit	-23	- 11	-19		-177	140!	
	8:52	0		-22	- 1	-8		-10,3	129.8	
(9)	8:56	0		)	J	0		0	129.8	(130)
	8:58	10		6	·	1		z. ³	132.1	
(10>	9:00	20		21	. 11.	15		15.7	147.8	(148)
<u>.</u>	9:02	30		2.5	1.11	15		15,3	1/3	
$\langle 1 \rangle$	9:04	40		41	12	12		11.7	1748	(175)
	9:06	50		15	14	6	1941 - Start Bright 19	11.7	1865	
2	9:08	60		- 14	13	Ц		10.3	196.8	(197)
	9:10	65		6	5	2		4.3	201.1	
(13)	9:  4	65	1. 	3	4	3	1	3.3	2044	(204)
	9:16	60		1	J	1		0,7	za5.1	
	9:18	50		-2	0	2		0	zas.1	
	9:20	40		-2	1 J	2		0	7051	
	9:22	30		-1	0	1	ļ	- 2,0	205.' 203.'	
	9:24	20		-12	-7	-1		- 6.7	196.4	
	9:26	10		-19	-16	-13		-180	178,4	
	9:28	5		-26	-13	-20		-18.0 -19.7	158.7	a the Alexandre Alexandre Alexandre
	9:30	0		- 3		-5		-50	153.7	
(14)	9:34	0		0	0		<u> </u>	0.3	1540	(154)
142	9:36	10	<u> </u>	3	2	0		10	155.0	
(15)	9:38	20	<b> </b>	21	5	14		15.0	170.0	(170)
<u></u>	9:40	30		13	3	17		16.3	1863	
<16>	9:42	40		14	ý Ý			11.3	197.6	(198)
<u>, 07</u>	9:44	50		14	5	5	1	90	206,6	
117	9:46	60		12	1.5	3		9.0 8,3	2149	(215)
472	9:48	65		5	5		+	3.7	218.6	1 2.2
(18)	9:52	65		4	2		1	3,0	221,6	(222)
107	9:54	60	<b> </b>			$\frac{1}{1}$	<u> </u>	0,3	221.9	
	9:56	50	}	0	5	3		1.0	222.9	