

Table I-2-11 (1) Crop Water Requirement of The Ariari Project Area

Crop Water Requirement of The Ariari Project Area (mm/24) CASE-I-1

ZONE (ha)	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec
UPPER ZONE (4750)	6.354	5.885	6.745	7.510	7.225	7.125	7.553	6.404	6.359	7.456	7.523	7.304
1/2	5.950	2.917	2.864	3.509	3.418	3.183	3.377	2.510	2.561	3.629	3.523	3.481
1/5	6.342	3.270	2.919	3.509	3.418	3.185	3.378	2.551	2.606	3.629	3.587	3.901
1/10	6.507	3.523	3.065	3.551	3.418	3.185	3.378	2.551	2.606	3.629	3.587	4.153
1/20	6.672	3.779	3.162	3.551	3.459	3.227	3.378	2.572	2.627	3.670	3.651	4.363
MIDDLE ZONE (9870)	20.580	18.653	18.702	18.928	18.885	18.342	18.389	15.895	15.374	19.873	20.187	18.415
1/2	18.675	7.903	9.000	11.500	10.880	9.974	10.208	7.789	8.084	11.789	11.883	10.778
1/5	18.935	7.979	9.509	11.500	10.880	9.974	10.208	7.789	8.279	11.789	12.013	11.503
1/10	19.116	8.132	9.727	11.530	11.005	9.974	10.208	7.789	8.279	11.789	12.272	11.905
1/20	19.197	8.151	9.956	11.530	11.068	10.103	10.208	7.815	8.279	11.914	12.466	12.147
LOWER ZONE (9115)	20.996	16.587	15.957	16.231	18.026	17.395	17.564	14.371	15.398	19.073	19.395	16.448
1/2	17.520	8.436	9.102	10.933	10.558	9.848	9.987	7.572	7.879	11.512	11.588	10.003
1/5	17.682	8.711	9.525	10.993	10.556	9.835	9.987	7.652	8.004	11.674	11.688	10.510
1/10	18.100	8.981	9.738	11.120	10.816	9.835	9.987	7.752	8.004	11.874	11.750	10.800
1/20	18.241	9.218	9.951	11.241	10.876	9.835	9.987	7.752	8.004	11.735	11.812	11.017
Ground Total (23815)	48.916	40.337	39.398	45.379	41.121	42.639	43.309	37.270	38.352	46.303	47.085	40.158
1/2	42.081	18.255	20.956	25.942	24.854	22.807	23.532	17.871	18.527	27.032	27.084	24.262
1/5	43.180	18.593	21.973	25.004	24.851	22.983	23.573	18.032	18.888	27.032	27.287	25.914
1/10	43.723	20.636	22.528	25.301	25.039	22.990	23.573	18.093	18.888	27.032	27.609	26.898
1/20	44.115	21.179	23.072	25.425	25.203	23.155	23.573	18.239	18.910	27.319	27.929	27.527

Table I-2-11 (2) Crop Water Requirement of The Ariari Project Area

Crop Water Requirement of The Ariari Project Area (m³/s) CASE-1-2

ZONE (m ²)	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec
UPPER ZONE												
(4770)	7,084	5,611	6,333	7,140	7,328	7,126	7,333	6,404	5,248	5,478	5,448	6,722
1-2	4,541	3,621	3,964	3,509	3,416	3,162	3,337	2,510	1,755	1,466	2,114	2,560
1-3	4,535	2,523	2,373	3,631	3,912	3,964	3,996	3,894	3,493	4,012	3,334	4,162
1-10	2,442	2,551	2,369	3,594	3,448	3,485	3,376	3,551	1,755	1,956	1,157	1,372
1-20	5,291	2,776	3,165	3,594	3,439	3,227	3,378	3,372	4,900	1,514	2,304	3,388
MIDDLE ZONE												
(9870)	18,071	14,218	16,785	19,828	18,887	18,342	18,388	15,883	13,740	17,421	18,186	15,278
1-2	15,986	6,342	9,000	11,500	10,680	9,974	10,208	7,768	6,487	9,439	9,535	8,233
1-3	16,318	6,404	9,509	11,500	10,830	9,974	10,208	7,768	6,543	9,439	9,628	10,006
1-10	18,740	6,550	9,727	11,529	11,305	9,974	10,208	7,768	6,543	9,439	9,647	10,484
1-20	18,588	8,530	9,558	11,630	11,868	10,405	10,208	7,945	6,845	9,660	10,005	10,741
LOWER ZONE												
(8145)	18,728	14,264	16,270	18,321	18,428	17,356	17,564	14,971	12,312	16,844	17,588	15,331
1-2	15,048	6,887	9,102	10,372	10,375	9,648	9,987	7,572	6,571	9,228	9,339	8,654
1-3	15,174	7,172	9,533	10,523	10,375	9,675	9,987	7,682	6,571	9,228	9,338	8,488
1-10	18,884	7,444	9,473	11,420	10,816	9,875	9,987	7,732	6,571	9,338	9,334	8,488
1-20	18,910	7,839	9,501	11,243	10,578	9,875	9,987	7,732	6,571	9,338	9,334	8,488
Ground Water (79845)												
1-2	17,889	17,089	18,842	19,378	14,151	14,825	15,305	17,370	12,400	16,355	12,578	17,485
1-3	15,580	15,327	16,366	16,942	14,924	14,907	15,322	17,871	14,714	14,494	14,494	16,135
1-10	16,720	15,365	16,375	16,004	14,854	14,383	15,002	16,022	15,002	14,574	14,568	16,135
1-20	17,233	16,521	17,328	16,504	15,029	14,982	15,372	18,080	15,002	14,574	14,568	16,135
1-20	17,708	16,934	17,072	16,429	15,303	15,465	15,575	18,438	15,045	14,714	14,568	16,135

Table I-2-11 (3) Crop Water Requirement of The Ariari Project Area

Crop Water Requirement of The Ariari Project Area (m3/s) CASE-II-1

Zone (ha)	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec
UPPER ZONE (5040)	7.422	6.345	5.712	6.114	6.316	6.265	6.562	5.520	5.323	6.754	6.711	7.066
1.2	4.797	3.050	1.957	2.404	2.342	2.162	2.366	1.720	1.755	2.488	2.414	2.725
1.5	3.152	2.170	2.023	2.404	2.342	2.182	2.314	1.748	1.783	2.488	2.457	2.702
1.20	4.220	2.622	2.122	2.433	2.342	2.182	2.314	1.748	1.783	2.488	2.457	2.488
1.20	5.510	3.666	2.217	2.433	2.370	2.211	2.314	1.752	1.900	2.514	2.501	2.727
MIDDLE ZONE (3940)	16.122	14.341	14.127	17.033	16.672	16.462	16.387	13.720	13.619	17.480	18.181	19.203
1.2	16.075	6.342	7.244	9.228	6.720	6.003	6.191	6.250	6.457	9.433	9.325	9.721
1.5	16.416	6.403	7.692	9.228	6.730	6.003	6.191	6.250	6.513	9.433	9.679	10.098
1.20	16.587	6.534	7.670	9.332	6.831	6.003	6.191	6.250	6.543	9.433	9.680	10.513
1.20	16.672	6.534	8.063	9.332	6.861	6.107	6.191	6.251	6.643	9.480	10.027	10.781
LOWER ZONE (3660)	10.515	14.179	12.588	15.661	15.905	15.464	15.615	12.953	13.223	16.668	17.403	18.183
1.2	14.957	6.974	7.179	9.979	8.670	7.924	8.202	6.219	6.471	9.433	9.399	9.585
1.5	15.338	7.227	7.611	9.030	8.670	8.076	8.202	6.219	6.574	9.433	9.599	9.404
1.10	15.550	7.443	8.023	9.133	8.719	8.076	8.202	6.387	6.574	9.433	9.651	9.401
1.20	15.668	7.646	8.203	9.235	8.769	8.076	8.202	6.387	6.574	9.433	9.702	9.623
Grand Total (23140)	41.061	34.483	32.426	38.630	38.693	38.311	38.572	32.214	32.441	40.521	42.295	37.953
1.2	35.739	15.363	16.691	20.611	18.741	18.109	18.680	14.188	14.744	21.634	21.348	20.641
1.5	36.696	16.021	17.552	20.662	19.741	18.262	18.708	14.315	15.002	21.634	21.696	22.409
1.20	37.467	16.598	18.024	20.666	19.682	18.262	18.708	14.355	15.002	21.634	21.696	22.414
1.20	37.663	17.050	18.163	21.000	20.020	18.365	18.708	14.460	15.016	21.712	21.219	22.131

Table I-2-11 (4) Crop Water Requirement of The Ariari Project Area

Crop Water Requirement of The Ariari Project Area (mm/24s) CASE-II-2

ZONE (ha)	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec
UPPER ZONE												
(5010)	5.402	2.885	5.710	5.114	6.216	6.255	6.582	5.820	5.211	4.405	5.115	5.187
1.2	1.811	1.725	1.687	2.401	2.511	2.182	2.286	1.720	1.557	.788	.788	1.131
1.4	3.002	1.087	1.026	2.401	2.242	2.182	2.214	1.748	1.566	.788	.788	2.008
1.10	5.001	1.118	2.122	2.122	2.242	2.182	2.314	1.748	1.566	.788	.788	2.018
1.20	5.590	1.133	2.317	2.452	2.370	2.311	2.314	1.782	1.571	.788	.788	2.376
MIDDLE ZONE												
(3540)	14.278	10.220	14.072	16.982	16.627	16.421	16.253	12.862	9.981	12.727	15.261	12.575
1.2	12.031	4.008	7.112	9.228	8.720	8.002	8.181	6.250	4.178	6.092	8.142	7.087
1.4	12.401	1.128	7.812	9.228	8.720	8.002	8.181	6.250	4.278	6.092	8.208	7.521
1.10	12.607	1.228	7.812	9.228	8.651	8.002	8.181	6.250	4.278	6.092	8.243	8.385
1.20	12.698	1.218	8.008	9.228	8.681	8.107	8.181	6.251	4.278	6.138	8.243	8.682
LOWER ZONE												
(8860)	18.128	11.650	17.988	15.881	15.802	15.484	15.615	12.982	11.000	14.487	17.582	14.212
1.2	12.577	5.187	7.172	8.678	8.670	7.921	8.203	6.218	5.035	7.458	7.504	7.218
1.4	12.770	3.208	7.811	9.000	8.670	8.078	8.203	6.218	5.138	7.485	7.504	7.768
1.10	12.008	3.803	8.033	9.122	8.718	8.078	8.203	6.237	5.138	7.487	7.541	8.082
1.20	12.163	3.015	8.005	9.222	8.758	8.078	8.203	6.237	5.138	7.521	7.584	8.318
STANDARD TOTAL												
(22810)	37.081	20.787	32.112	28.778	28.648	28.270	28.528	22.187	24.236	32.610	38.085	32.880
1.2	27.040	10.228	15.868	20.611	19.741	18.108	18.580	14.188	9.234	14.238	14.411	15.797
1.4	28.221	10.802	17.502	20.682	19.741	18.252	18.708	14.318	9.881	14.277	14.482	17.588
1.10	28.013	11.228	17.868	20.888	19.892	18.282	18.708	14.385	9.884	14.277	14.666	18.785
1.20	28.221	11.580	18.120	21.000	20.020	18.282	18.708	14.480	9.888	14.488	14.820	19.538

Table I-2-12 Total Expectation of Water Insufficiency (%)

Zone	Crop	Without System	With System for 1/2	With System for 1/5	With System for 1/10
UPPER ZONE	Paddy Rice	55.62	.27	.09	.02
	Paddy Rice	52.53	1.05	.20	.05
	Maize (1)	0.00	0.00	0.00	0.00
	Soy beans (2)	10.72	2.76	.52	.10
	Sorghum	4.27	1.74	.39	.09
	Cotton	0.00	0.00	0.00	0.00
	Cotton	17.36	2.58	.61	.12
	Plantain	9.66	1.38	.28	.08
	Cacao	5.00	1.15	.30	.06
	Papaya	6.13	1.50	.35	.06
MIDDLE ZONE	Oil Palm	5.00	1.15	.30	.06
	Pastuer	4.17	1.05	.24	.06
	Paddy Rice	56.73	.29	.09	.02
	Paddy Rice	53.36	.61	.14	.02
	Maize (1)	0.00	0.00	0.00	0.00
	Soy beans (2)	22.03	1.73	.32	.04
	Sorghum	14.61	2.06	.39	.05
	Cotton	0.00	0.00	0.00	0.00
	Cotton	24.98	1.27	.24	.02
	Plantain	12.36	.73	.19	.02
LOWER ZONE	Cacao	9.22	.66	.15	.03
	Papaya	11.36	.94	.22	.03
	Oil Palm	9.22	.66	.15	.03
	Pastuer	6.66	.69	.13	.02
	Paddy Rice	57.49	.39	.08	.01
	Paddy Rice	54.03	.57	.12	.02
	Maize (1)	0.00	0.00	0.00	0.00
	Soy beans (2)	16.39	1.46	.30	.05
	Sorghum	7.36	1.77	.36	.05
	Cotton	0.00	0.00	0.00	0.00
Cotton	22.22	1.46	.32	.05	
Plantain	13.13	.95	.20	.04	
Cacao	7.89	.92	.23	.04	
Papaya	12.25	.92	.21	.04	
Oil Palm	7.69	.92	.23	.04	
Pastuer	6.85	.67	.16	.04	

Table I-2-13 EXPECTED PRODUCTION VALUE WITH IRRIGATION SYSTEM

ITEM CROP	WITHOUT		WITH 1/2		WITH 1/3		WITH 1/10	
	AREA (ha)	BNEFIT (10000 \$)	AREA (ha)	BNEFIT (10000 \$)	AREA (ha)	BNEFIT (10000 \$)	AREA (ha)	BNEFIT (10000 \$)
PADDY	13539	5857253	33800	14816003	34023	14970033	34053	14983908
	20521	8730818	160	52478	37	12201	7	2156
	34060	12688072	34060	14988481	34060	14982234	34060	14985664
MAIZE	1297	168670	1323	171969	1325	172196	1325	172243
	26	2664	2	225	0	42	0	5
	1325	171534	1325	172194	1325	172240	1325	172249
SOY BEAN	2271	511039	2697	606870	2740	616493	2748	618393
	479	95743	53	10560	10	2006	2	321
	2750	606782	2750	617430	2750	618499	2750	618710
SORGHUM	1176	222309	1276	241094	1286	244981	1300	245605
	124	20272	24	3992	4	614	1	82
	1300	242581	1300	245086	1300	245605	1300	245687
OTHERS	574	180566	698	220012	707	222844	710	223511
	136	26656	12	2425	3	537	0	93
	710	209322	710	222437	710	223361	710	223604
PLANTAIN(E)	2045	1022276	2285	1142612	2305	1152335	2308	1154548
	265	79634	25	7433	5	1599	1	271
	2310	1101910	2310	1150045	2310	1153934	2310	1154820
CACAO	604	220792	662	236859	666	238455	670	238872
	66	13274	8	1542	2	377	0	73
	670	234066	670	238402	670	238832	670	238945
PAPAYA	377	331467	404	355366	408	359537	410	360584
	33	26666	6	4920	1	1148	0	197
	410	358133	410	360306	410	360565	410	360760
COILPALM	290	252790	316	276570	320	278045	320	278390
	30	12162	2	897	0	198	0	40
	320	264951	320	277467	320	278244	320	278420
PARACUYA	19	12723	20	13459	20	13564	20	13593
	1	103	0	17	0	4	0	1
	20	12627	20	13476	20	13568	20	13594
TOTAL	22392	6679985	43783	16180837	44012	16258198	44054	16289235
	21683	7010193	292	6466	63	18726	11	327
	44075	15890179	44075	16265325	44075	16267224	44075	16292472

Table I-2-14 TOTAL EXPECTED PRODUCTION VALUE

ITEM	WITHOUT		WITH 1/2		WITH 1/3		WITH 1/10	
	AREA (ha)	BENEFIT (1000Ct\$)	AREA (ha)	BENEFIT (1000Ct\$)	AREA (ha)	BENEFIT (1000Ct\$)	AREA (ha)	BENEFIT (1000Ct\$)
SUB-TOTAL	44075	15690173	44075	16255325	44075	16267224	44075	16232472
CATTLE	10200	555308	10200	555308	10200	555308	10200	555308
MAIZE	375	39000	375	39000	375	39000	375	39000
PLANTAIN(E)	50	18000	60	18000	50	18000	50	18000
PAPAYA	430	344000	430	344000	430	344000	430	344000
MARACUYA	10	800	10	800	10	800	10	800
TOTAL	55150	16948287	55150	1923433	55150	19245302	55150	19230580

Table I-2-15 (1) Comparison of Topography and Geology for the Proposed Diversion Site (Sheet 1)

Site	Location	Topography	Rivers	Geology			Remarks
				Petrology	Bearing Capacity	Permeability	
A	<p>Right Downstream from Angostura Bridge</p> <ul style="list-style-type: none"> - V shaped Valley - Gorge with both steep banks - Elevation: 780m A.S.L. - Slope: <ul style="list-style-type: none"> Left Bank 1: 0.87 Right Bank 1: 3.96 	<p>Width: approx. 40m</p> <p>River Bed Slope: approx. 1/50</p> <p>Stability: stable</p> <p>Velocity: large</p> <p>Catchment Area: 773km²</p>	<p>Left Bank: Unconsolidated Sediments (gravel, sand, silt, clay) with 3.8m in thickness and Metamorphic Rocks</p> <p>Right Bank: Heterogeneous colluvial sediment of more than 30m in thickness</p>	<p>Unconsolidated Sediment: firm</p> <p>Metamorphic Rocks: solid</p>	<p>Unconsolidated Sediment: high</p> <p>Metamorphic Rocks: low</p>	<ul style="list-style-type: none"> - Unconsolidated sediment is instable so as to cause land slide. - Large gravel is carried away in time of high water level. - Surrounding area is forest and pasture. - There are collapsible steep slopes and small river terraces in the right bank of downstream. - The site recommended by HIMAT. 	
B	<p>1.5km Downstream from Angostura Bridge</p> <ul style="list-style-type: none"> - Eroded Valley - Both Banks: River terrace with 2 ~ 20m height from river bed. - Elevation: 750m A.S.L. - Slope: <ul style="list-style-type: none"> Left Bank 1: 22.44 Right Bank 1: 3.56 Right Bank 1: 11.31 1: 4.3 	<p>Width: approx. 150m</p> <p>River Bed Slope: approx. 1/55</p> <p>Stability: instable</p> <p>Velocity: large</p> <p>Thalweg: Left Bank</p> <p>Joining Tributary: Right Bank</p> <p>Catchment Area: 780km²</p>	<p>Left Bank: Fluvial Sediment (gravel, sand, and silt)</p> <p>Right Bank: Fluvial Sediment with 4.3m thickness and Sedimentary Rocks (sandstone, mudstone)</p>	<p>Fluvial Sediment: firm</p> <p>Sedimentary Rocks: solid to relatively soft</p>	<p>Fluvial Sediment: high</p> <p>Sedimentary Rocks: low</p>	<ul style="list-style-type: none"> - Approx. 600m downstream from the end of gorge. - At high water time, it occurs that change of sediment distribution and a lateral movement of river course. - At right bank, river terrace is well developed. - Surrounding area is covered with pasture. 	

Table I-2-15 (2) Comparison of Topography and Geology for the Proposed Diversion Site (Sheet 2)

Site	Location	Topography	Rivers	Geology			Remarks
				Petrology	Bearing Capacity	Permeability	
C	<p>4km Down-stream from Lejanias</p> <ul style="list-style-type: none"> - Eroded and Sedimented Valley - Left Bank: Foot Clift and River Terrace - Right Bank: River Terraces (1, 2 and 5m height from river bed) - Elevation: 594m A.S.L. - Slope: Left Bank 1: 0.72 Right Bank 1: 14.72 	<p>Width: approx. 230m</p> <p>River Bed Slope: approx. 1/80</p> <p>Stability: instable</p> <p>Velocity: moderate</p> <p>Thalweg: Left Bank</p> <p>Catchment Area: 815km²</p>	<p>Left Bank: Fluvial Sediment with 1m in thickness and Sedimentary Rocks (mudstone, slate and sandstone)</p> <p>Right Bank: Fluvial Sediment</p>	<p>Fluvial Sediment: firm</p> <p>Sedimentary Rocks: solid to relatively soft</p>	<p>Fluvial Sediment: high</p> <p>Sedimentary Rocks: low</p>	<ul style="list-style-type: none"> - Relatively narrow to downstream and up-stream. - At high water stage, it occurs that change of sediment distribution and a lateral movement of river course. - At right bank, river terrace is well developed. - Left bank is unused land, and Right bank is used for papaya plantation. 	

Table I-2-16 (1) Comparison of Diversion Facilities (Sheet 1)

Item	Site A	Site B	Site C
River Condition			
- Longitudinal Slope	1/50	1/55	1/80
- Design Flood Discharge(m ³ /s)	440	440	460
- High Water Depth(m)	2.3	1.0	0.9
- Flood Water Velocity(m/s)	4.6	2.6	2.1
- Design Droughty Discharge(m ³ /s)	17	17	17
Head Works			
- Fixed Weir (Concrete Gravity)			
Weir Length (L m)	25	155	255
Width of Top (B m)	2.5	2.0	2.0
Weir Hight/Check Water Depth (H/Ha)	2.0/1.5	2.0/1.5	2.0/1.5
Slope of Down Side (1:m)	1 : 1.5	1 : 1.0	1 : 1.0
Apron Length(law m)	10.5	9.5	9.5
Maximum Apron Thickness (ta m)	1.0	1.0	1.0
Riprap Length(lrs m)	35	15	15
- Scouring Sluice			
Width (Bs m)	5.0×2 Gate	5.0×2 Gate	5.0×2 Gate
Apron Length (las m)	25	20	20
Riprap Length(lrs m)	40	20	20
- Intake Works			
Width of Works(Bi m) (for 36.8 m ³ /s)	5.0×5 Gate	5.0×5 Gate	5.0×5 Gate

Table I-2-16 (2) Comparison of Diversion Facilities (Sheet 2)

Item	Site A	Site B	Site C
Head Race			
- Tunnel	r=2.0 Standard Horseshoe Shape	Unnecessary	Unnecessary
Tunnel Length	1.5 km	---	---
Chute (H=30m, L=60m)	1 unit	---	---
- Open Canal (Wet Masonry lining, Bottom Width 5.0m, Canal Depth 3.0m, Longitudinal Slope 1/700)			
Canal Length	9.0 km	9.0 km	2.0 km
Drops (H=2.0m)	65 unit	65 unit	5 unit
Syphon (D=4.0m, L=20m)	1 unit	---	---
Cross Culvert	3.0(H)X3.0(B)X2 L=10.0m 1 unit	3.0(H)X3.0(B)X2 L=10.0m 1 unit	---
Pump Irrigation Facilities			
- Irrigated Area	$A_1 = 260\text{ha}$, $A_2 = 170\text{ha}$, Total 430ha		
- Pump			
Q=0.18m ³ /s, H=30m, P=90kw	---	---	2 unit
Q=0.14m ³ /s, H=10m, P=18kw	---	---	1 unit
- Chloride vinyl pipe			
D=500mm	---	---	1.7 km
D=350mm	---	---	0.9 km
- Farm Pond			
3,300 m ³	---	---	1 unit
2,200 m ³	---	---	1 unit
- Required Energy	---	---	460,000kwh/year

Table I-2-17 (1) Comparison of Cost and Consideration (sheet 1)
 (Unit : Million Col\$)

Item	Site A	Site B	Site C
Construction Cost			
- Head Works	912	1,577	1,735
- Head Race Works	3,533	2,311	285
(Tunnel)	(1,200)	(---)	(---)
(Open Canal)	(750)	(750)	(167)
(Others)	(1,583)	(1,561)	(119)
- Pumping Facilities	---	---	110
Total	4,445	3,889	2,130
Yearly Repayment	535	468	259
Maintenance Cost	111	97	53
Operation cost of Pump	---	---	7
Total Yearly Cost	646	565	319
Consideration			
- Stability of Water Intake	-The water route is stable due to narrow width.	-It is necessary to change and maintain the river route to right side for water intake.	-The same condition as the Site B can be seen.
-Solid Material	-Maintenance of facilities (sluiceway, diversion works) will be significance by reason of flowing of boulders in flood time.	-Almost same condition as the Site A can be seen.	-Flow velocity of solid materials is reduced because of wide river course.

Table I-2-17 (2) Comparison of Cost and Consideration (sheet 2)

Item	Site A	Site B	Site C
<p>Consideration</p> <p>-The condition of Construction</p>	<p>-The scale of diversion weir is the smallest</p> <p>-Head race of tunnel is required.</p> <p>-There is a collapse land near the site and geological unstable place can be seen.</p> <p>-Land slope is steep and problem of access to site is expected.</p>	<p>-The scale of diversion weir is middle.</p> <p>-Most of construction is cutting workes and no geological problem can be expected.</p> <p>-The site is located newer the main road and the problem of the access road is small.</p>	<p>-The scale of diversion weir is the largest.</p> <p>-Most of construction is cutting workes and no geological problem can be expected.</p> <p>-Comparing with other site, the land is flat topogrphically and the problem of the access road is the smallest.</p>
<p>-Maintenance</p>	<p>-The distance of head race is the longest and maintenance of the canal facilities such as tunnel, drop works is increased.</p>	<p>-The same condition as the Site A except tunnel can be expected</p>	<p>-The operation and maintenance of pumping system is required</p>

Table I-2-17 (3) Comparison of Cost and Consideration (sheet 3)

Item	Site A	Site B	Site C
<p>Consideration</p> <p>-Adjustment to the dam plan for hydro-electric power plant at the upper stream of the site</p>	<p>-Dam for hydro-electric power plant is planed at the upper stream of the site and it is necessary to adjust to wasteway of the dam and diversion weir.</p>	<p>-No problem can be expected.</p>	<p>-No problem can be expected.</p>

Note : 1) This table is to compare with each Site and common items are excluded.

2) Construction cost is estimated based on the unit price in Colombia, December, 1988 and following exchange rate is used.

Col\$ 332.56=US\$ 1

3) Maintenance Cost of head race and pumping facilities is excluded in this comparison.

4) Yearly repayment is calculated from equation below:

$$C = I \times \left(i + \frac{i}{(1+i)^n - 1} \right)$$

Where C : Yearly Repayment

i : Interest 12%

n : Durable year 50 years for civil works

20 years for pumping facilities

Table I-2-18 Comparison of Division Structures No.1

Item	System With Diversion Weir (Type A)	System Without Diversion Weir (Type B)
Stability of Water Intake	-Even in the dry season, a stable water intake is possible with diversion weir.	<p>-It is expected that a stable water intake is difficult because of the reasons mentioned below:</p> <ol style="list-style-type: none"> <li data-bbox="911 770 1374 844">1. River width is as large as 200 meters. <li data-bbox="911 898 1374 1061">2. River discharge is so little as nearly equal to the maximum water intake in the dry season. <li data-bbox="911 1115 1374 1279">3. High amount of water will be infiltrated since the river bed consists of conglomerate and sand.
Maintenance	-Bottom of intake works canal can be designed as 1.0 m higher than the existing river bed. Therefore, the sedimentation which flows into the head race will be reduced.	<p>-Large sedimentation flow will be expected since the bottom of intake works will be designed at the same level as the river bed. And the frequency of the sedimentation removal will be increased.</p> <p>-More than two times per year of maintenance will be necessary for the control of water route.</p>

Table I-2-18 Comparison of Division Structures No. 2

(Col\$ 1,000)

Item	System With Diversion Weir (Type A)	System Without Diversion Weir (Type B)
Construction Cost		
1. Earth Works	76,400	52,000
2. Concrete Works	687,442	348,442
3. Riprap	31,382	2,988
4. Gabion	8,126	8,126
5. Gate	851,513	632,931
6. Temporary works	79,700	35,000
Sub-total	1,734,563	1,079,133
Maintenance Cost for a year		
a) Sedimentation Removal	7,000	10,500
b) Control of Water Route	1,620	16,308
Sub-total	8,620	26,808
Maintenance cost for 50 years	431,000	1,340,400
Grand Total of System Cost	2,165,563	2,419,533

Table I-2-19 Comparison of Irrigation Canal System

Item	Plan I		Plan II	
	Quantity	Construction Cost (1,000 Col\$)	Quantity	Construction Cost (1,000 Col\$)
Earth Works				
Excavation	435,000 m ³	235	319,000 m ³	172
Embankment	319,000 m ³	131	203,000 m ³	83
Removal of Surplus Soil	83,000 m ³	104	93,000 m ³	116
Sub-Total		<u>470</u>		<u>371</u>
Concrete Lining	174,000 m ²	<u>418</u>	162,000 m ²	<u>388</u>
Related Structure				
Drop	324 units	1,220	106 units	908
Siphon	19 units	52	118 units	222
Bridge	68 units	111	28 units	96
Sub-Total		<u>1,383</u>		<u>1,226</u>
Grand Total		<u>2,271</u>		<u>1,985</u>

Note : Construction cost is estimated considering the upper part of the irrigation system

Table I-2-20 Comparison of Construction Cost between Canal System

Item	Drop Type (Col\$ 1,000)	Chute Type (Col\$ 1,000)
1. Canal Works		
Earth Works	1,532,919	1,096,107
Lining	1,467,155	6,388,980
Sub-Total	<u>3,000,074</u>	<u>7,485,085</u>
2. Related Structure		
Drop	2,950,212	---
Siphon	103,116	103,116
Bridge	120,747	104,614
Division Works	216,539	216,539
Waste Way	904,184	904,184
Fence	58,272	58,272
Sub-Total	<u>4,353,070</u>	<u>1,386,725</u>
3. Land Acquisition		
	<u>77,206</u>	<u>38,713</u>
Grand Total	<u>7,430,350</u>	<u>8,916,525</u>

Note : Construction cost is estimated considering the upper part of the irrigation system.

Table I-2-21 Main Canal NO.1

NO	L (Km)	Q (m ³ /s)	B (m)	I	h (m)	V (m/s)	H ₁ (m)	H ₂ (m)	TYPE
1	2.3	36.725	2.5	1/4050	3.30	1.50	3.70	3.40	C-a
2	3.8	36.725	2.5	1/4050	3.30	1.50	3.70	3.40	C-c
3	9.0	17.705	1.5	1/2500	2.36	1.49	2.70	2.45	C-a
4	8.0	16.904	1.5	1/2400	2.29	1.50	2.70	2.40	C-a
5	5.6	15.463	1.5	1/2250	2.16	1.50	2.50	2.25	C-a
6	4.8	14.745	1.5	1/2200	2.11	1.50	2.50	2.20	C-a
7	4.5	8.647	1.0	1/1550	1.65	1.49	2.00	1.75	C-a
8	4.1	6.113	1.0	1/1250	1.36	1.49	1.70	1.45	C-a
9	2.2	5.340	1.0	1/1500	1.25	1.48	1.60	1.35	C-a
10	4.3	4.785	1.0	1/4300	2.00	0.60	2.30	-	So-a
11	4.7	4.066	1.0	1/3850	1.82	0.60	2.10	-	So-a
12	3.8	2.209	1.0	1/2600	1.27	0.60	1.50	-	So-a

Note L : Canal Length h : Water Depth
 Q : Design Discharge V : Velocity
 B : Canal Bottom Width H₁: Canal Hight
 I : Longitudinal Slope H₂: Lining Hight

Table I-2-21 Main Canal NO.2

NO	L (Km)	Q (m ³ /s)	B (m)	I	h (m)	V (m/s)	H ₁ (m)	H ₂ (m)	TYPE
1	4.7	17.008	1.5	1/2450	2.30	1.49	2.70	2.40	C-c
2	4.8	15.077	1.5	1/2250	2.14	1.49	2.50	2.25	C-c
3	5.4	12.597	1.5	1/2000	1.93	1.49	2.30	2.05	C-c
4	4.2	9.639	1.0	1/1650	1.76	1.50	2.10	1.85	C-b
5	2.3	3.676	1.0	1/3750	1.77	0.60	2.00	—	C-b
6	3.6	1.790	1.0	1/2300	1.13	0.59	1.30	—	C-b

Table I-2-21 Main Canal NO.3

NO	L (Km)	Q (m ³ /s)	B (m)	I	h (m)	V (m/s)	H ₁ (m)	H ₂ (m)	TYPE
1	4.1	3.001	1.0	1/3150	1.52	0.60	1.80	—	So-a
2	3.8	2.158	1.0	1/2550	1.25	0.60	1.50	—	So-a
3	3.4	1.233	1.0	1/1750	0.89	0.60	1.10	—	So-a
4	1.5	0.461	0.5	1/ 950	0.62	0.59	0.80	—	So-b

Table I-2-22 Secondary Canal NO.1

NO	L (Km)	Q (m ³ /s)	B (m)	I	h (m)	V (m/s)	H ₁ (m)	H ₂ (m)	TYPE
1	1.2	0.102	0.5	1/ 700	0.28	0.46	0.50	--	So-b
2	1.2	0.132	0.5	1/ 900	0.35	0.45	0.50	--	So-b
3	1.4	0.266	0.5	1/1200	0.47	0.46	0.60	--	So-b
4	3.2	0.450	0.5	1/1000	0.66	0.59	0.80	--	So-b
5	1.5	5.001	1.0	1/1100	1.20	1.48	1.50	1.30	C-b
	4.6	3.388	1.0	1/3400	1.64	0.60	1.90	--	So-a
	4.0	2.697	1.0	1/2950	1.43	0.60	1.70	--	So-a
	3.9	1.789	1.0	1/2250	1.12	0.60	1.30	--	So-a
	5.3	1.328	1.0	1/1800	0.92	0.60	1.10	--	So-a
	2.2	0.136	0.5	1/1000	0.43	0.44	0.60	--	So-b
6	2.2	1.098	1.0	1/1600	0.82	0.60	1.00	--	So-a
	4.1	0.732	1.0	1/1350	0.72	0.60	0.90	--	So-b
7	3.8	1.694	1.0	1/2150	1.08	0.60	1.30	--	So-a
	3.5	1.030	1.0	1/1550	0.79	0.60	1.00	--	So-a
	4.3	0.569	1.0	1/1150	0.60	0.59	0.80	--	So-b
8	1.8	0.813	1.0	1/2000	0.84	0.53	1.00	--	So-b
	3.0	0.421	0.5	1/2000	0.75	0.45	0.90	--	So-b
9	1.5	1.320	1.0	1/1800	0.97	0.60	1.20	--	So-a
	4.3	0.989	1.0	1/1800	0.90	0.58	1.10	--	So-b
	1.8	0.190	0.5	1/1500	0.47	0.41	0.70	--	So-b
10	2.5	0.461	0.5	1/2000	0.78	0.46	1.00	--	So-b

Table I-2-22 Secondary Canal NO.2

NO	L (Km)	Q (m ³ /s)	B (m)	I	h (m)	V (m/s)	H ₁ (m)	H ₂ (m)	TYPE
1	1.8	0.296	0.5	1/1500	0.59	0.46	0.80	—	So-b
2	1.8	0.401	0.5	1/1900	0.72	0.45	0.90	—	So-b
3	3.0	0.296	0.5	1/1600	0.60	0.45	0.80	—	So-b
4	2.0	0.417	0.5	1/2000	0.75	0.45	0.90	—	So-b
5	2.2	0.449	0.5	1/2100	0.78	0.45	1.00	—	So-b
6	2.7	0.417	0.5	1/2000	0.75	0.45	0.90	—	So-b
7	2.0	0.372	0.5	1/1800	0.69	0.45	0.90	—	So-b
8	2.6	0.369	0.5	1/1800	0.69	0.45	0.90	—	So-b
9	1.8	0.266	0.5	1/1500	0.56	0.45	0.70	—	So-b
10	2.1	0.704	1.0	1/2800	0.85	0.45	1.00	—	So-b
	0.8	0.226	0.5	1/1300	0.50	0.45	0.70	—	So-b
11	1.1	0.731	1.0	1/2800	0.86	0.46	1.10	—	So-b
	2.3	0.465	0.5	1/2100	0.79	0.45	1.00	—	So-b
12	0.5	0.585	1.0	1/2400	0.74	0.46	0.90	—	So-b
	0.9	0.452	0.5	1/1600	0.74	0.50	0.90	—	So-b
13	1.8	0.558	1.0	1/2300	0.71	0.46	0.90	—	So-b
	1.6	0.425	0.5	1/1500	0.70	0.50	0.90	—	So-b
14	2.4	0.425	0.5	1/1900	0.74	0.46	0.90	—	So-b
15	2.0	1.010	1.0	1/2000	0.83	0.54	1.00	—	So-a
	1.4	0.452	0.5	1/2000	0.77	0.46	1.00	—	So-b
16	3.1	1.727	1.0	1/2200	1.10	0.60	1.30	—	So-a
	0.8	0.731	1.0	1/2200	0.81	0.50	1.00	—	So-b
	2.9	0.399	0.5	1/1900	0.72	0.45	0.90	—	So-b
17	2.9	0.384	0.5	1/1800	0.70	0.46	0.90	—	So-b
18	2.8	0.390	0.5	1/1800	0.70	0.46	0.90	—	So-b
19	2.5	0.348	0.5	1/1700	0.66	0.46	0.90	—	So-b

Table I-3-1 Peak Runoff Discharge (m³/sec)

	A (km ²)	Return Period											
		1/2		1/5		1/10		1/20		1/50			
		t(hour)	RI(mm/hr)	PQ(m ³ /s)	t(hour)	RI(mm/hr)	PQ(m ³ /s)	t(hour)	RI(mm/hr)	PQ(m ³ /s)	t(hour)	RI(mm/hr)	PQ(m ³ /s)
Avichule-1 *	4.40	1.93	3.38	14.86	1.56	5.14	32.62	1.54	6.41	28.20	1.45	7.68	33.77
Avichule-2 *	8.50	2.32	2.98	25.31	2.01	4.53	38.53	1.86	5.65	48.04	1.75	6.77	57.52
Cano Seco-1	15.60	2.76	2.69	41.96	2.38	4.07	63.56	2.21	5.06	78.98	2.07	6.05	94.42
Cano Seco-2	6.90	2.19	3.10	21.38	1.89	4.72	32.55	1.75	5.88	40.58	1.64	7.04	48.59
Cano Guanayas-1	10.43	2.47	2.86	29.87	2.13	4.36	45.47	1.97	5.43	56.58	1.85	6.51	67.87
Cano Guanayas-2	20.40	2.98	2.56	52.12	2.57	3.87	78.95	2.39	4.81	98.11	2.24	5.75	117.29
Cano Guanayas-3	13.57	2.42	3.57	48.40	2.16	4.97	67.48	2.03	5.92	80.31	1.93	6.83	92.54
Cano Guanayas-4	23.93	2.85	3.20	76.57	2.54	4.46	106.76	2.39	5.31	127.05	2.27	6.12	146.57
Cano Upin-1	22.27	3.05	2.51	55.95	2.54	3.81	84.76	2.45	4.73	105.32	2.30	5.65	125.91
Cano Upin-2	50.00	3.87	2.12	106.09	3.34	3.23	161.49	3.09	4.03	201.33	2.90	4.82	241.06
Cano Urichare-1	23.82	2.98	2.81	55.86	2.61	4.08	97.18	2.44	4.97	118.29	2.31	5.84	138.99
Cano Urichare-2	16.29	2.79	2.67	43.45	2.41	4.04	65.82	2.24	5.02	81.79	2.10	6.00	97.78
Cano Urichare-3	9.82	2.31	3.33	32.66	2.03	4.83	47.46	1.89	5.88	57.78	1.79	6.91	67.89
Cano Urichare-4	34.31	3.16	5.72	102.47	2.81	4.96	142.87	2.65	4.16	170.03	2.52	2.99	196.15
Cano Venado-1	16.50	2.68	3.01	49.77	2.35	4.38	72.34	2.20	5.33	88.05	2.08	6.26	103.46
Cano Venado-2	10.01	2.32	3.32	33.07	2.04	4.82	48.07	1.90	5.87	58.51	1.80	6.89	68.75
Cano Mucuya-1	4.30	1.90	3.44	14.80	1.65	5.21	22.42	1.53	6.48	27.86	1.43	7.74	33.30
Cano Mucuya-2	18.40	2.77	2.95	54.26	2.43	4.29	78.87	2.27	5.22	96.00	2.14	6.13	112.80
Cano Mucuya-3	11.50	2.42	3.23	37.11	2.12	4.69	53.93	1.98	5.71	65.65	1.87	6.71	77.13
Cano Mucuya-4	15.60	2.52	3.47	54.17	2.24	4.84	73.53	2.11	5.76	89.89	2.01	6.65	103.70
Cano Sardinata-1	2.30	1.59	3.88	8.92	1.38	5.88	13.52	1.28	7.30	16.79	1.20	8.73	20.08
Cano Sardinata-2	25.25	3.03	2.78	70.09	2.66	4.03	101.87	2.48	4.91	124.00	2.35	5.77	145.70
Cano Sardinata-3	11.45	2.31	3.68	42.19	2.05	5.14	58.82	1.93	6.11	70.00	1.84	7.05	80.75
Cano Tapato	13.88	2.44	3.55	49.29	2.17	4.95	68.72	2.04	5.89	81.79	1.94	6.80	94.35

note : * Existing Drainage Canal A=Catchment Area (km²)

t=Lag Time of Flood(hour) RI=Rainfall Intensity(mm/hr)

PQ=Peak Flood Discharge(m³/sec)

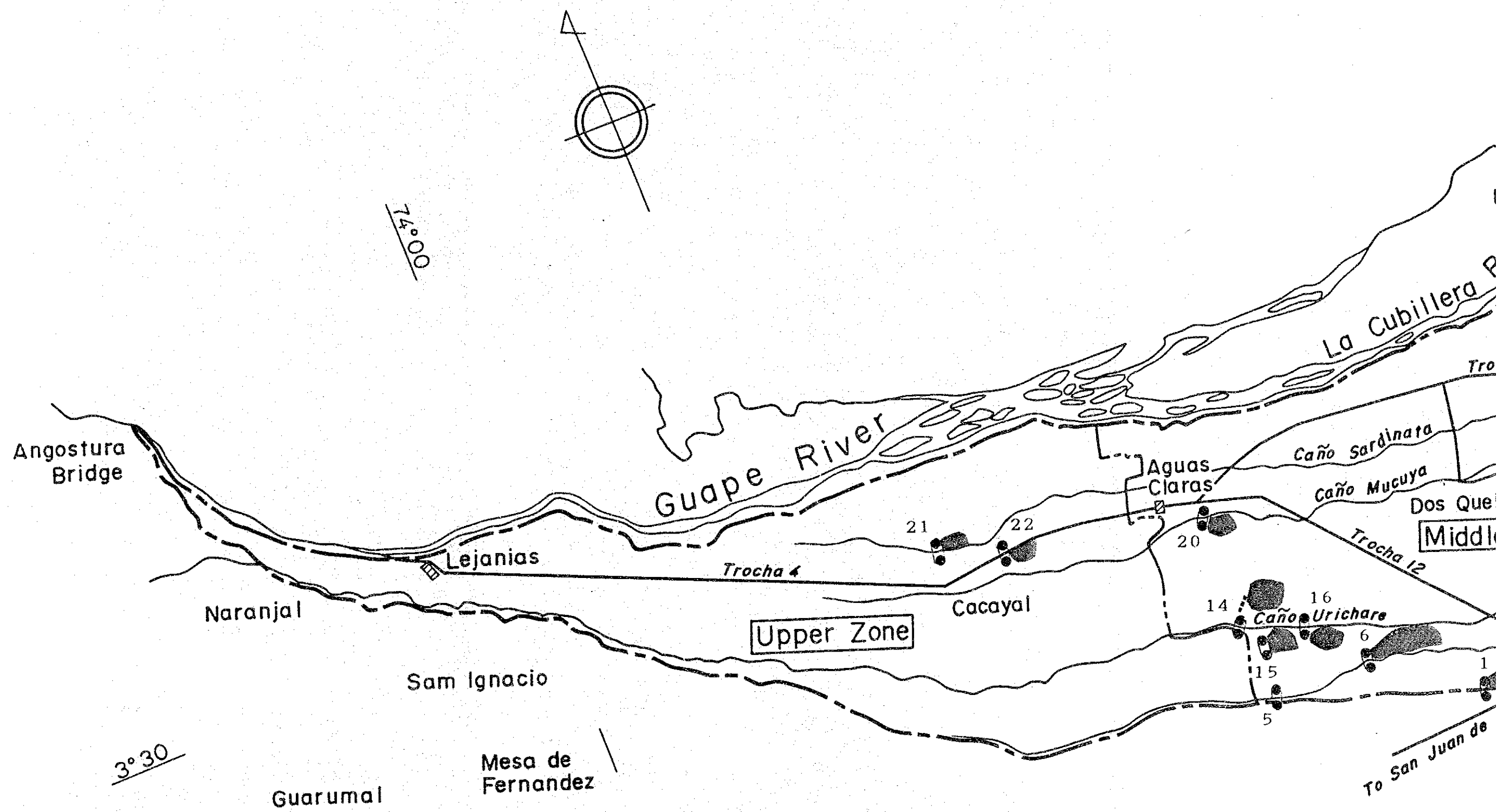
Table I-3-2 Summary of Inundation Time

Name of Caño	Return Period 1/2		Return Period 1/5		Return Period 1/10		Return Period 1/20	
	T (hr)	Q (m ³ /s)	T (hr)	Q (m ³ /s)	T (hr)	Q (m ³ /s)	T (hr)	Q (m ³ /s)
Avichure 2	1.8	19.22	3.0	23.11	3.4	25.49	3.7	27.61
Avichure 1	3.5	14.87	6.0	16.56	6.9	17.61	7.7	18.76
Avichure 2	1.8	19.22	3.0	23.11	3.4	25.49	3.7	27.61
Avichure 1 ★	---	18.49	3.8	20.13	5.1	21.43	5.8	22.92
Caño Seco	2.3	12.18	3.5	13.79	4.1	14.73	4.7	15.64
Caño Hogotes	2.9	36.84	3.6	52.94	3.8	61.68	4.0	69.87
Caño Upin 2	---	54.37	2.5	64.00	3.1	88.30	3.3	110.66
Caño Upin 1	---	104.28	3.3	142.10	4.3	188.49	4.9	192.19
Caño Guanayas 4	1.1	70.23	2.4	94.67	2.9	104.97	3.0	115.72
Caño Guanayas 3	---	68.54	3.5	84.19	4.6	94.40	4.9	103.51
Caño Guanayas 1	---	67.12	3.9	90.78	5.1	99.73	5.2	97.45
Caño Guanayas 2	---	142.94	3.6	206.99	5.1	239.20	5.1	267.95
Caño Urichare 4	1.1	68.06	2.4	124.25	2.8	138.38	3.0	160.92
Caño Urichare 3	---	68.50	3.9	114.65	4.4	127.97	4.7	140.03
Caño Urichare 1	1.9	66.87	3.6	111.85	4.2	123.57	7.4	134.12
Caño Urichare 2	---	66.61	1.7	106.80	2.2	120.12	3.1	128.73
Caño Venado 2	6.0	8.52	10.5	8.99	12.0	9.23	13.3	9.43
Caño Venado 1	---	48.61	1.7	66.29	4.2	78.53	6.3	90.94
Caño Venado 2 ★	1.7	26.27	2.7	32.05	3.0	34.93	3.3	37.32
Caño Venado 1	---	49.62	3.4	70.10	5.5	85.57	7.1	100.16
Caño Mucuya 4	2.6	38.51	3.6	45.67	4.0	48.66	4.2	53.15
Caño Mucuya 3	---	47.25	3.3	50.50	4.0	56.36	5.3	61.19
Caño Mucuya 2	---	50.73	3.1	61.47	3.5	71.66	7.3	77.42
Caño Mucuya 1	---	50.09	3.1	65.40	3.0	68.12	7.3	73.91
Caño Sardinata 3	2.8	31.10	3.0	37.32	3.5	41.31	3.7	44.52
Caño Sardinata 2	---	60.03	2.2	71.23	3.9	78.88	5.6	91.21
Caño Sardinata 1	1.7	49.80	3.1	100.46	5.2	127.29	5.8	125.73
Caño Iaparo	2.0	14.52	2.9	31.63	3.1	57.75	3.2	63.08

Note I : Inundation Time (hr)

Q : Peak Flow for Lower Basin (m³/s)
H : Maximum Water Level (m)

FIGURES



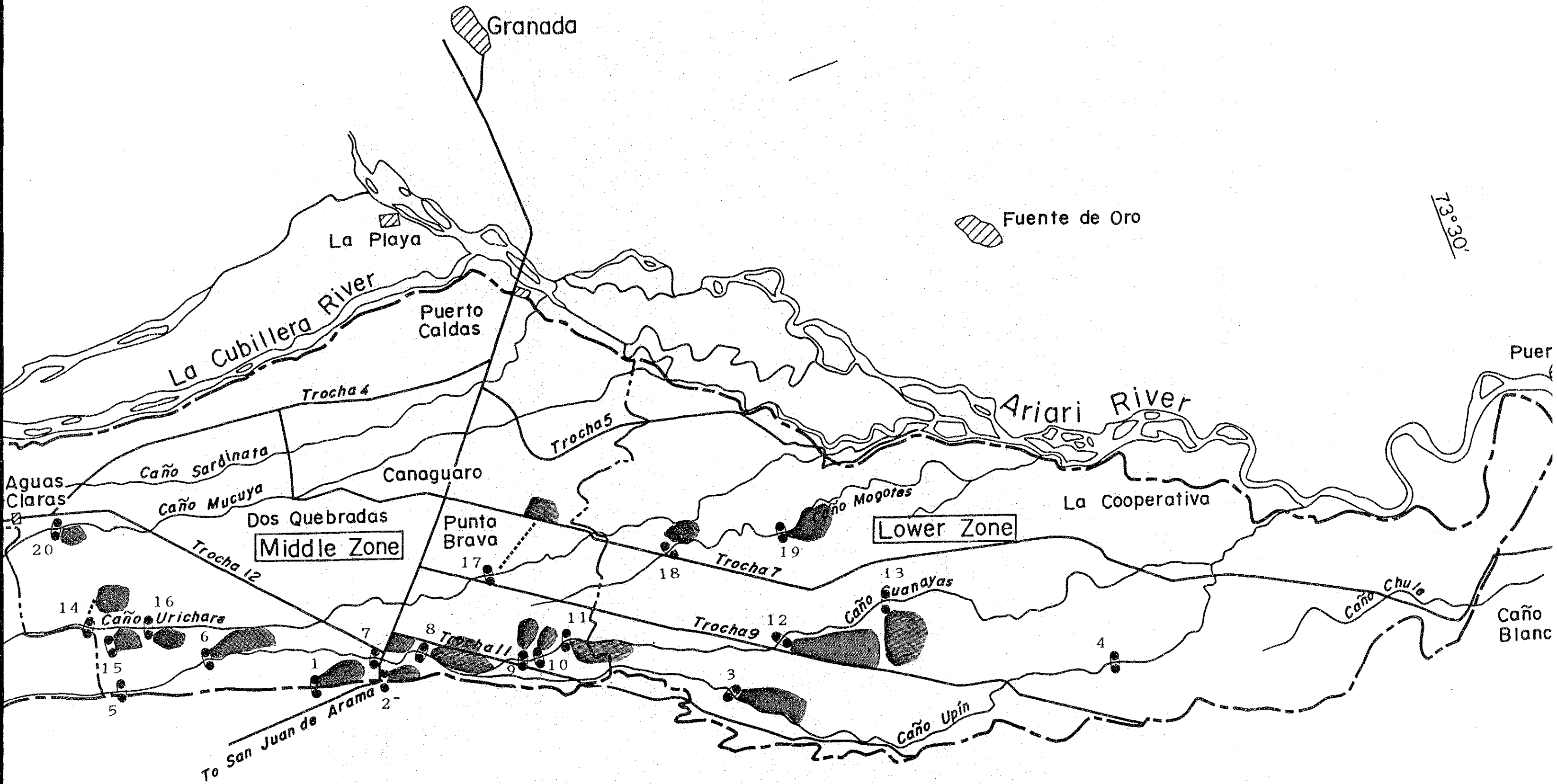
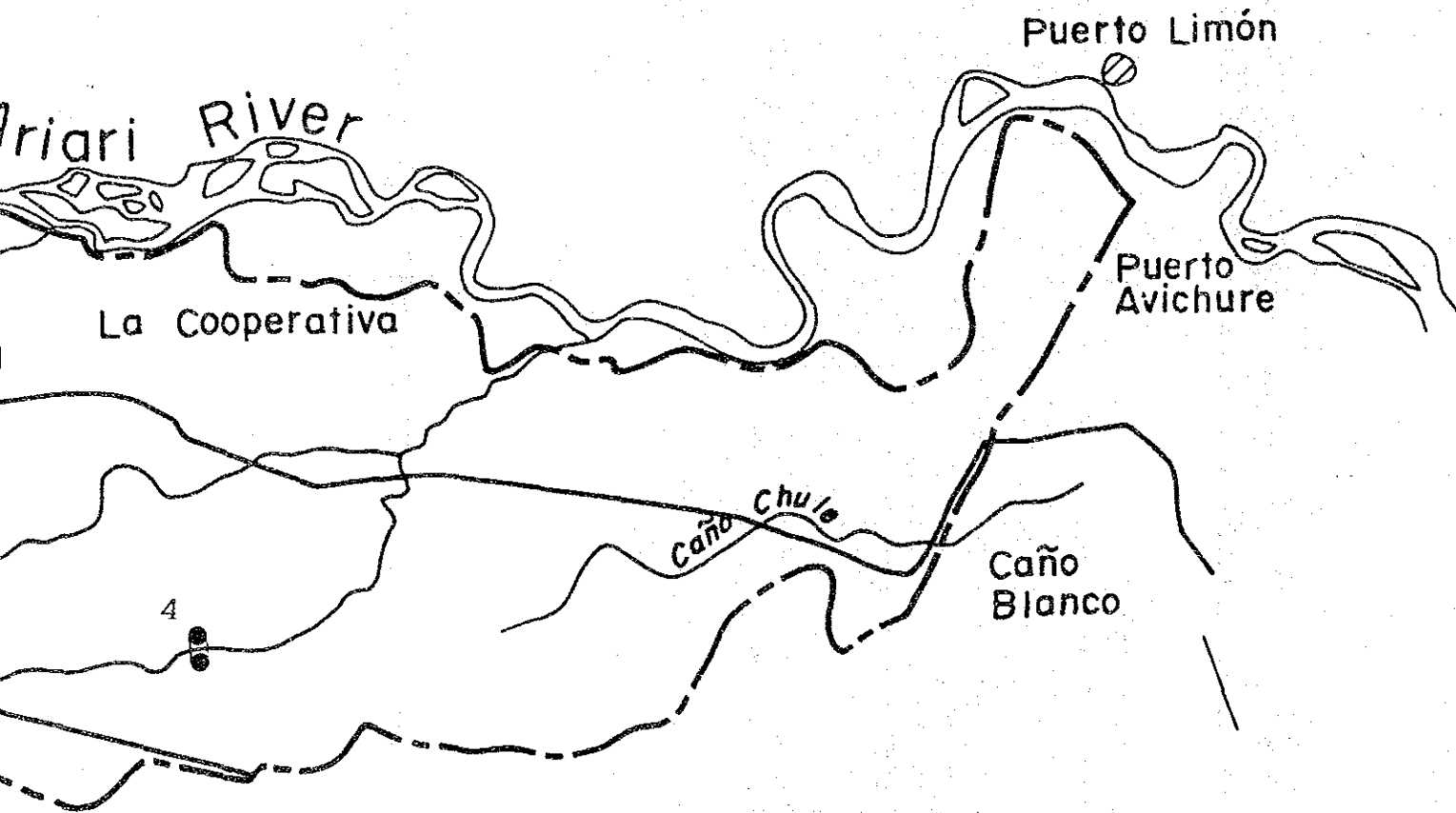


Fig. I-2-1 EXISTING IRRIGATION AREA

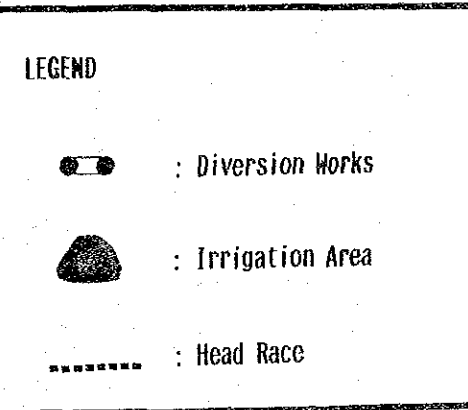
Fuente de Oro

73°30'



Dimensions of Diversion Works

No.	Material	Height(m)	Width(m)
1	Concrete	1.0	5.0
2	Stone Sand Bag	0.5	7.0
3	Stop Log	1.6	11.5
4	Stop Log	1.0	10.0
5	Stop Log	1.0	7.0
6	Concrete	0.6	8.0
7	Stone Sand Bag	0.6	11.0
8	Stop Log	1.5	7.0
9	Stop Log	1.4	7.0
10	Stop Log	1.7	6.5
11	Concrete	2.1	7.5
12	Stop Log	1.5	12.0
13	Stop Log	1.3	9.0
14	Concrete	1.4	11.0
15	Concrete	0.9	5.0
16	Sand Bag	0.5	7.0
17	Stop Log	1.2	8.0
18	Concrete	0.8	5.5
19	Concrete	1.5	6.0
20	Stop Log	0.8	7.5
21	Sand Bag	0.7	5.0
22	Stop Log	0.9	4.5



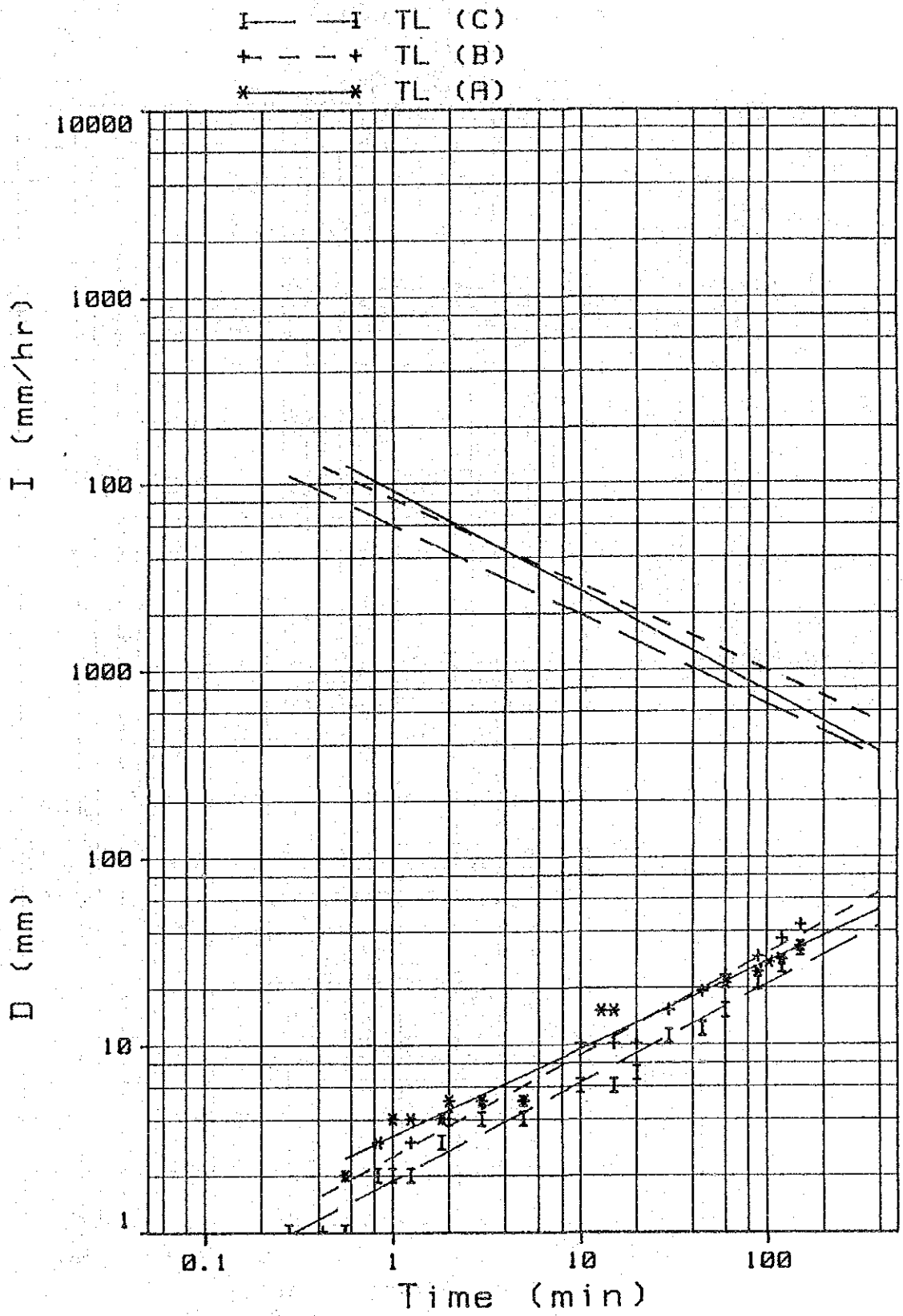


Fig. I-2-3 (1) INTAKE RATE OF TL

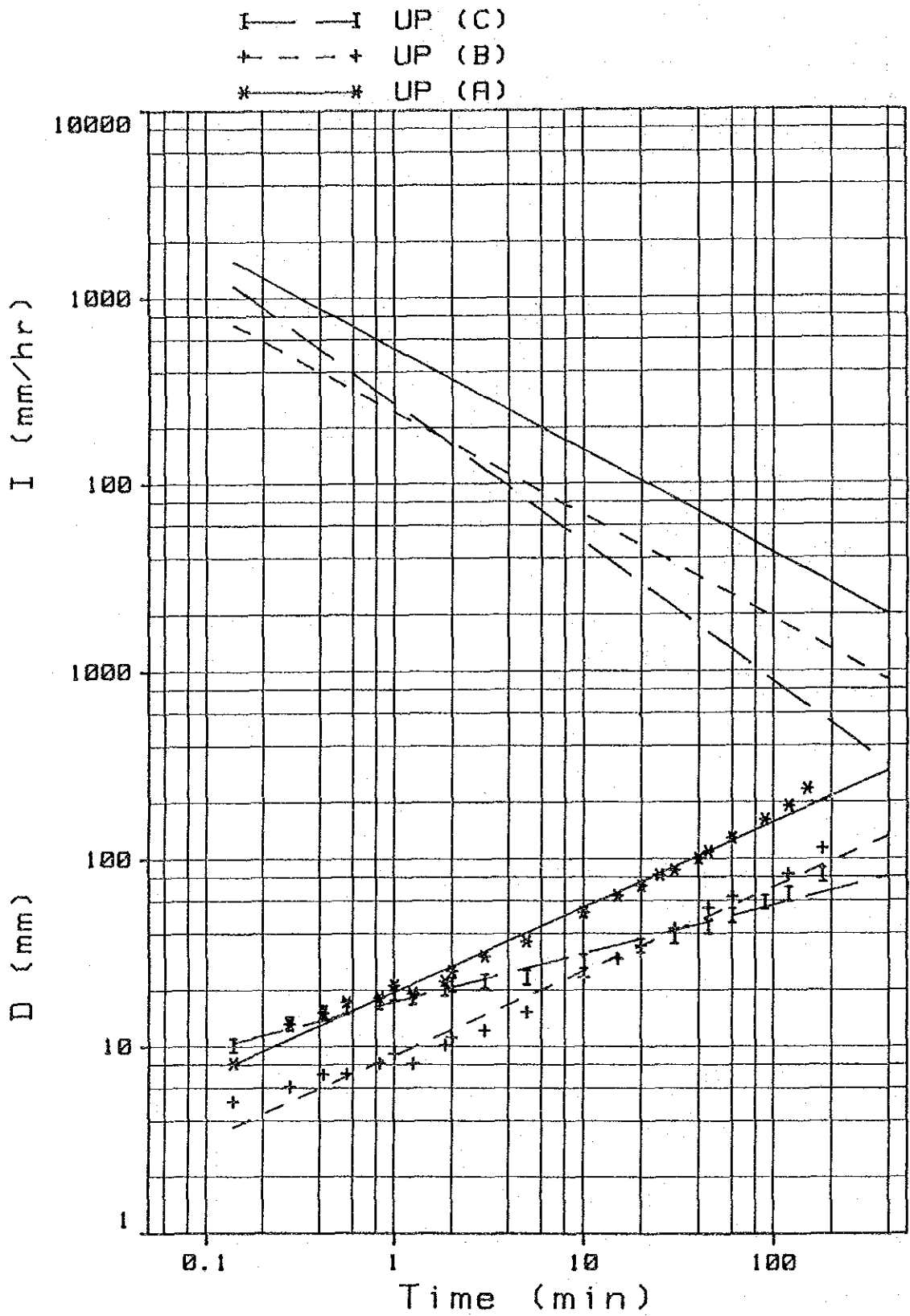


Fig. I-2-3 (2) INTAKE RATE OF UP

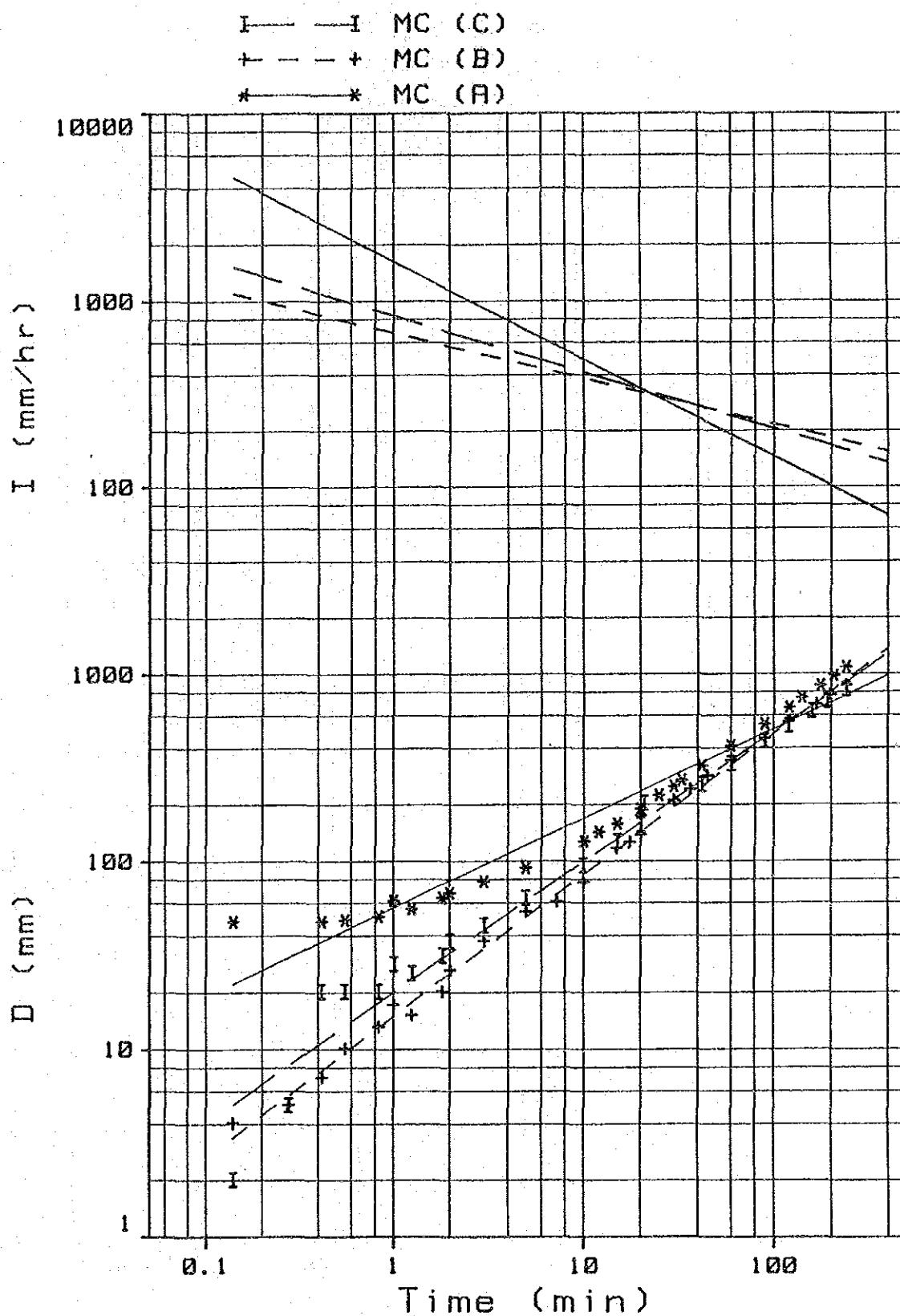


Fig. I-2-3 (3) INTAKE RATE OF MC

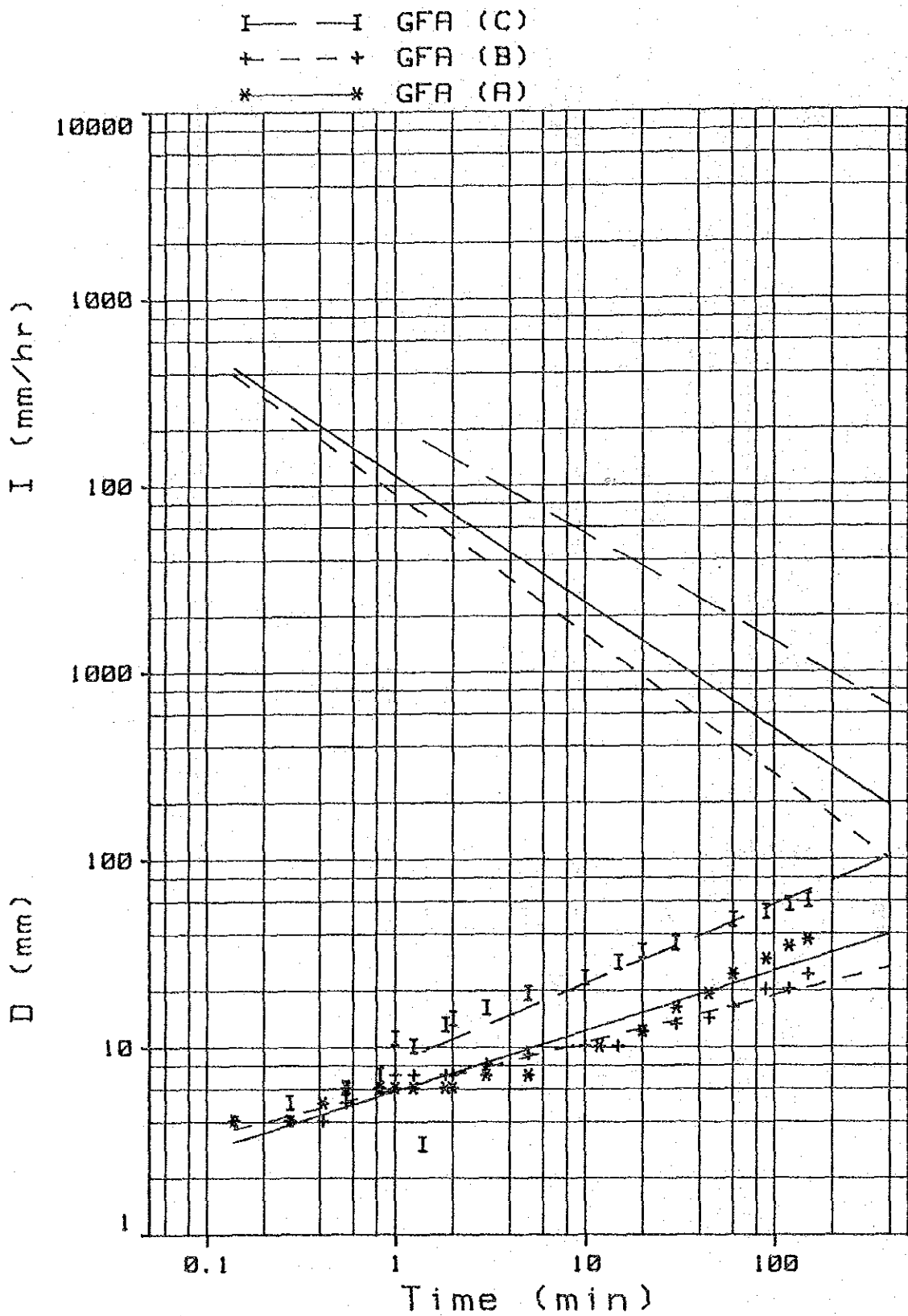


Fig. I-2-3 (4) INTAKE RATE OF GFA

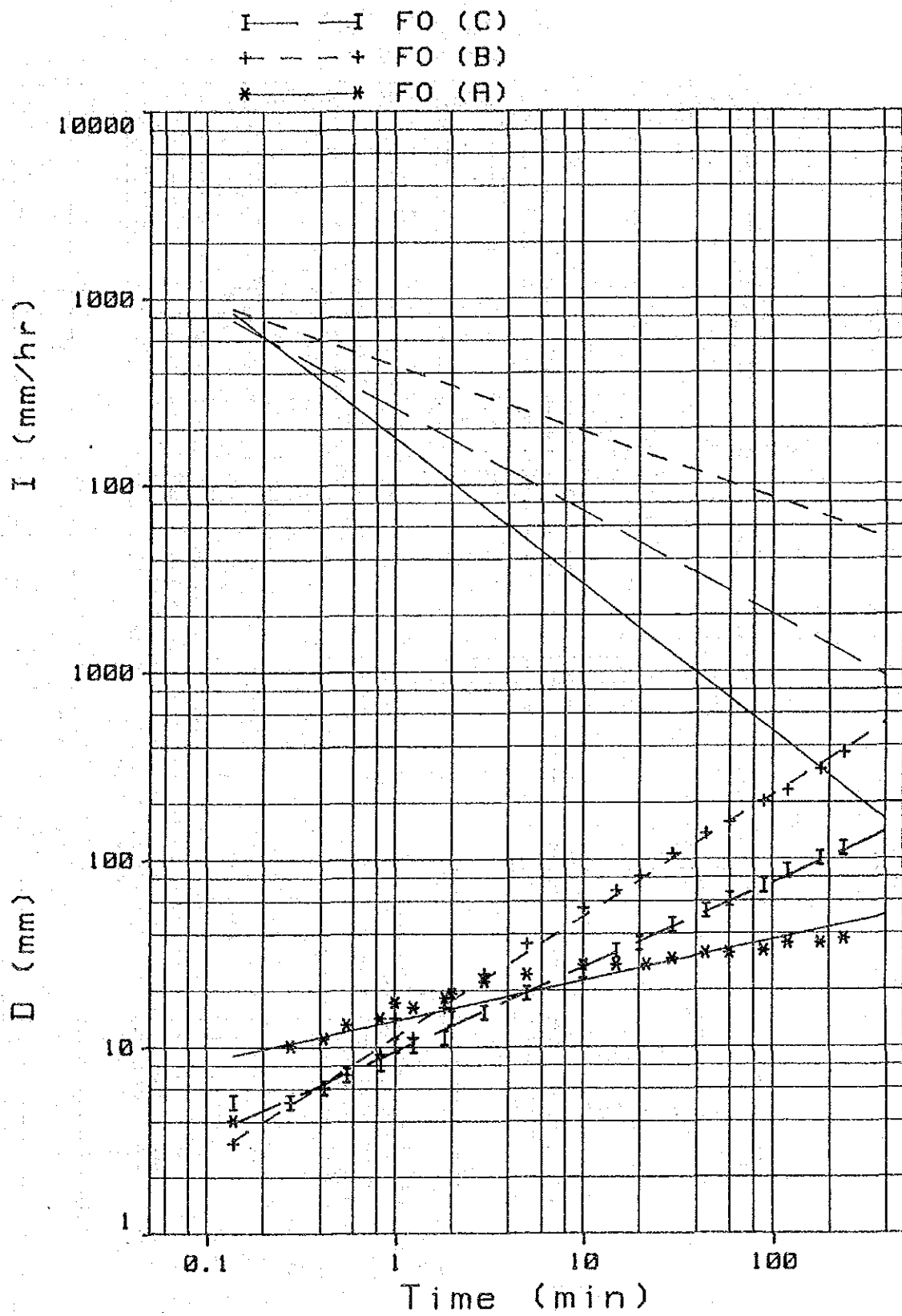


Fig. I-2-3 (5) INTAKE RATE OF FO

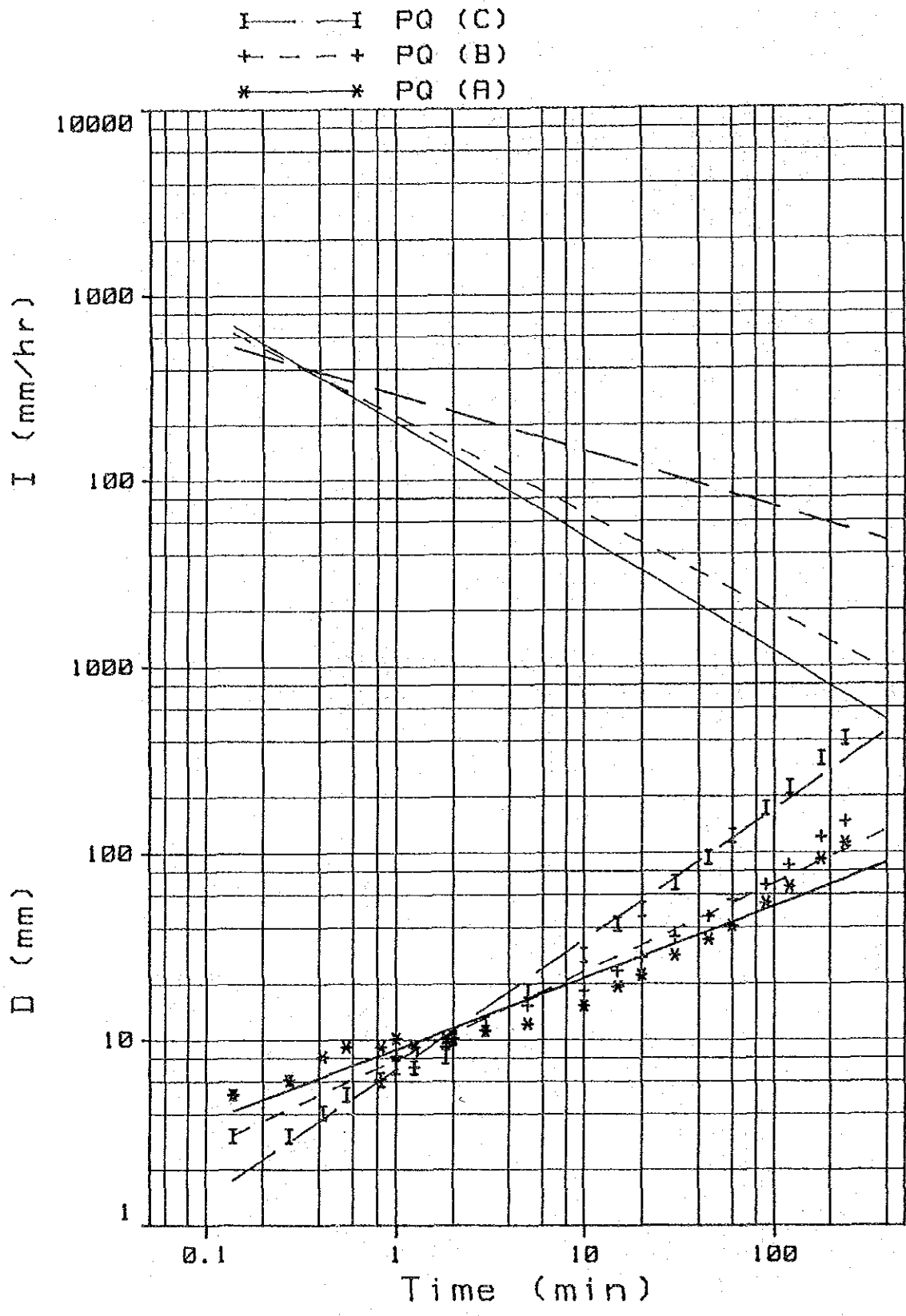


Fig. I-2-3 (6) INTAKE RATE OF PQ

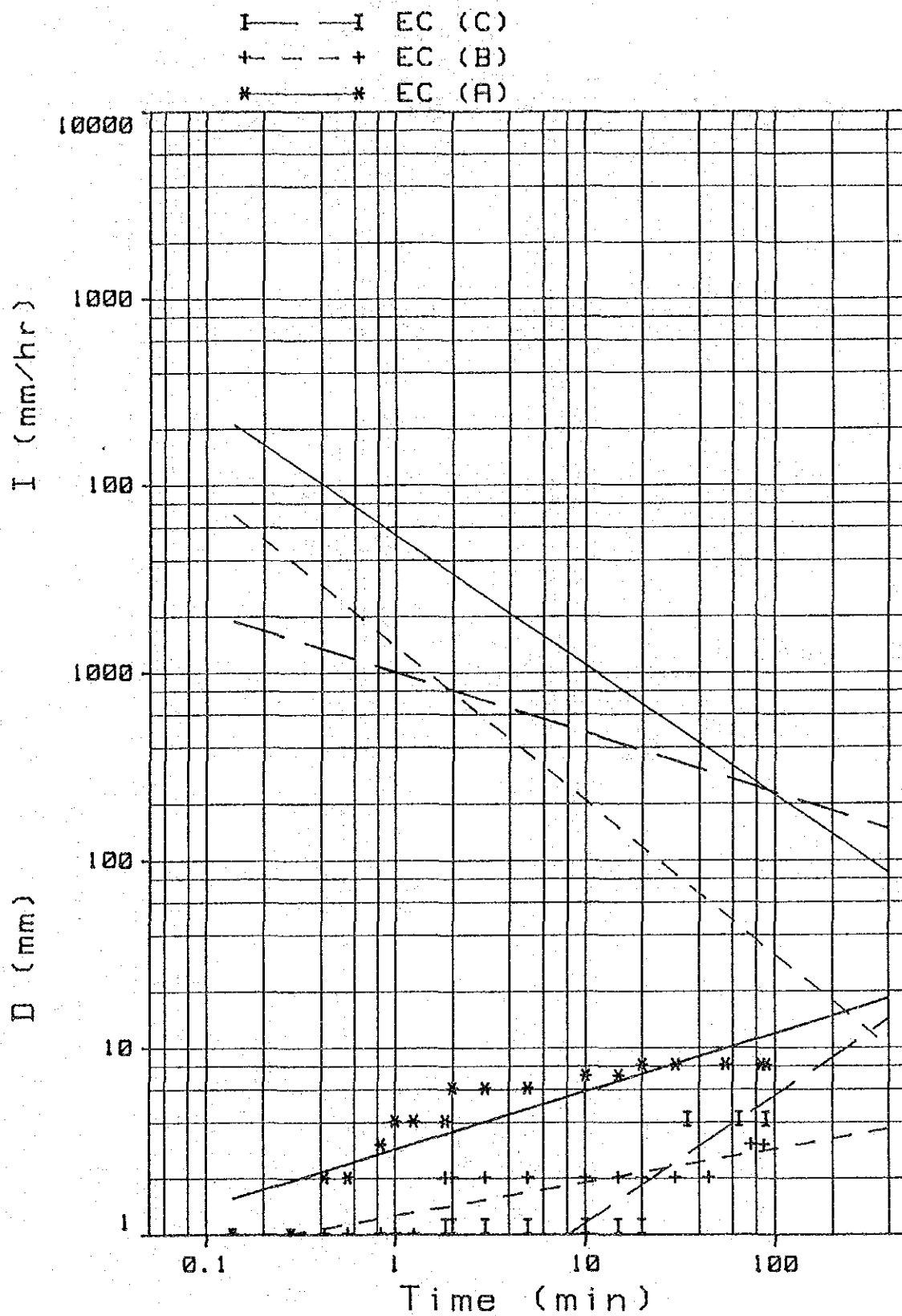


Fig. I-2-3 (7) INTAKE RATE OF EC

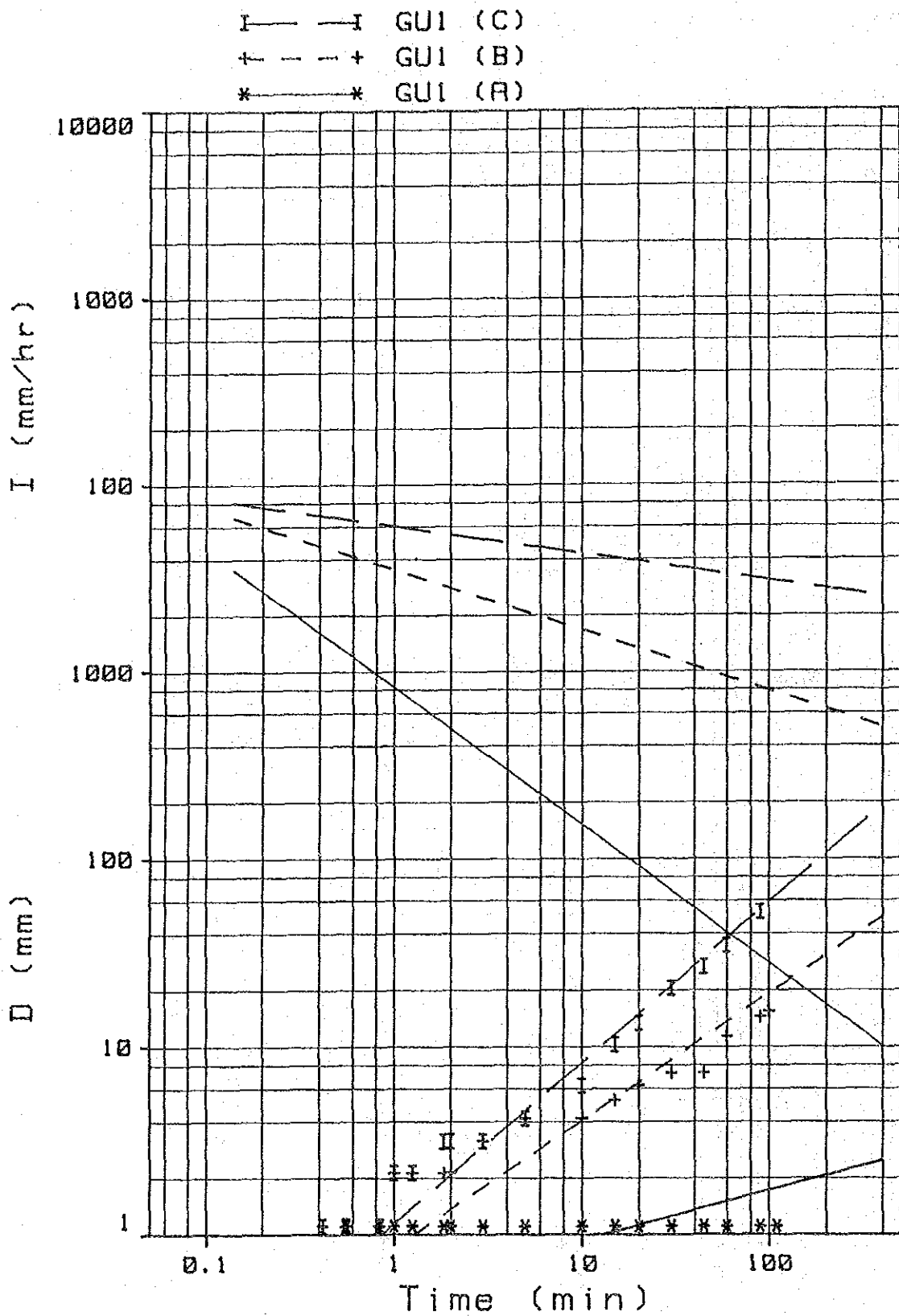


Fig. I-2-3 (8) INTAKE RATE OF GUI

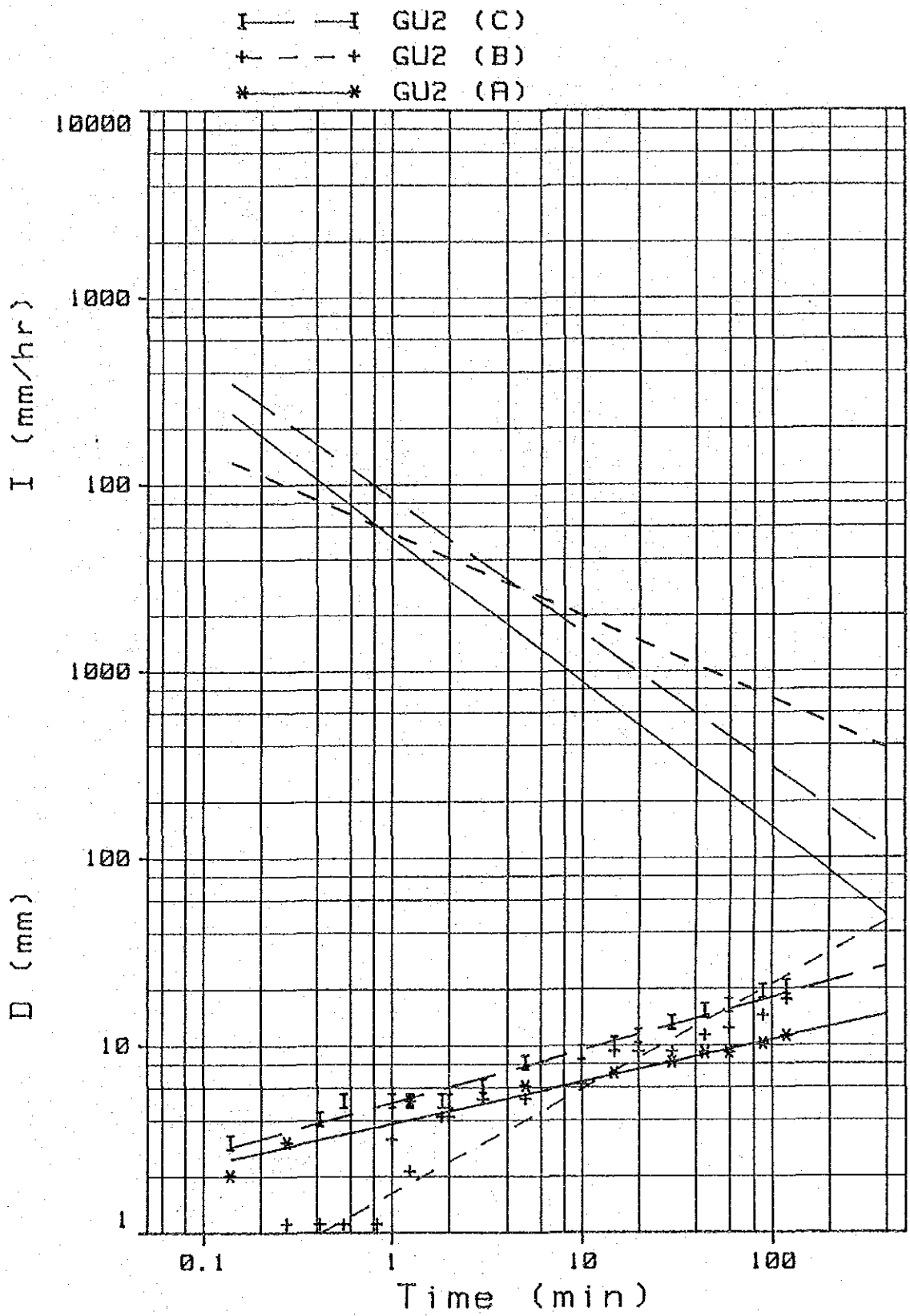
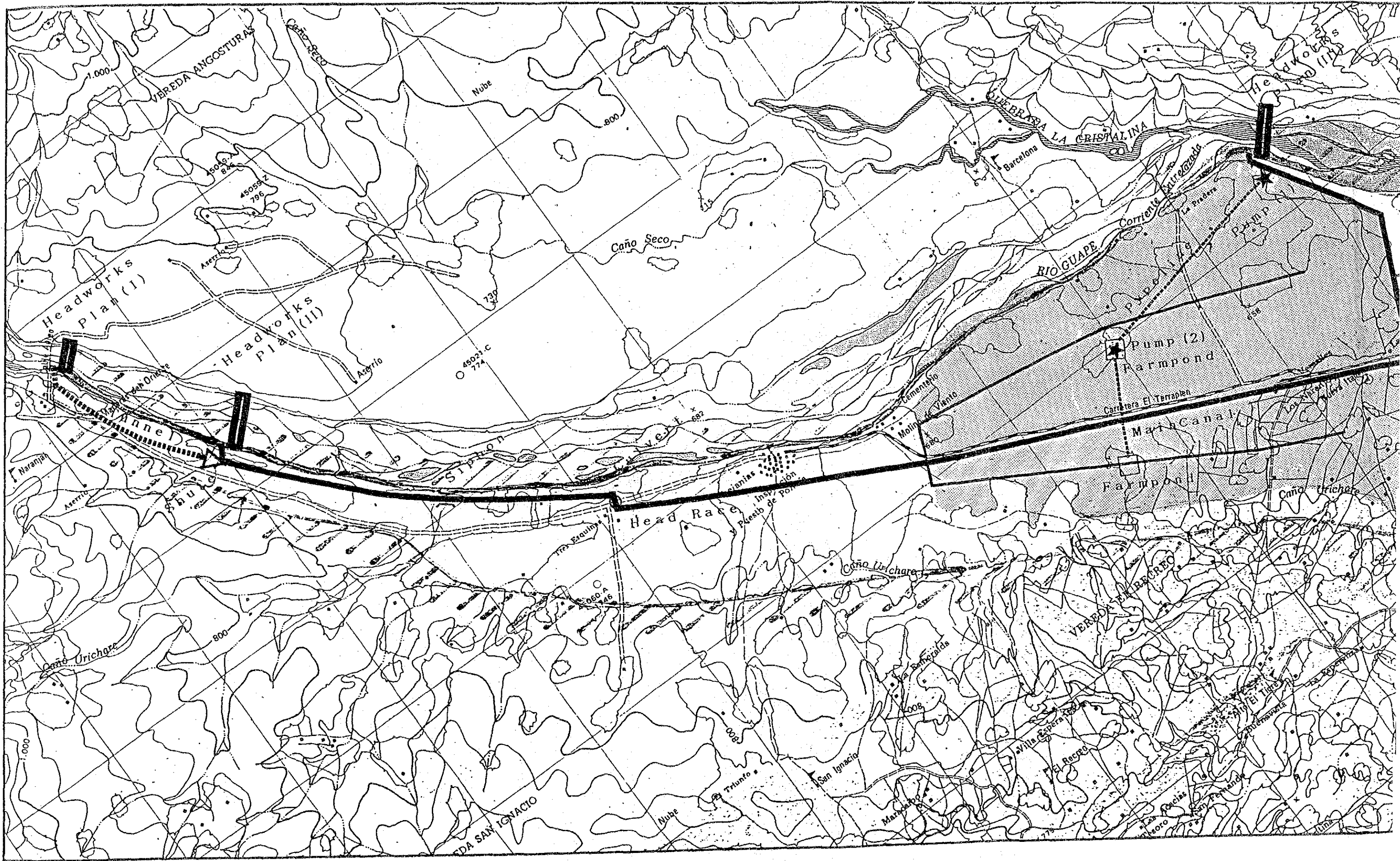


Fig. I-2-3 (9) INTAKE RATE OF GU2



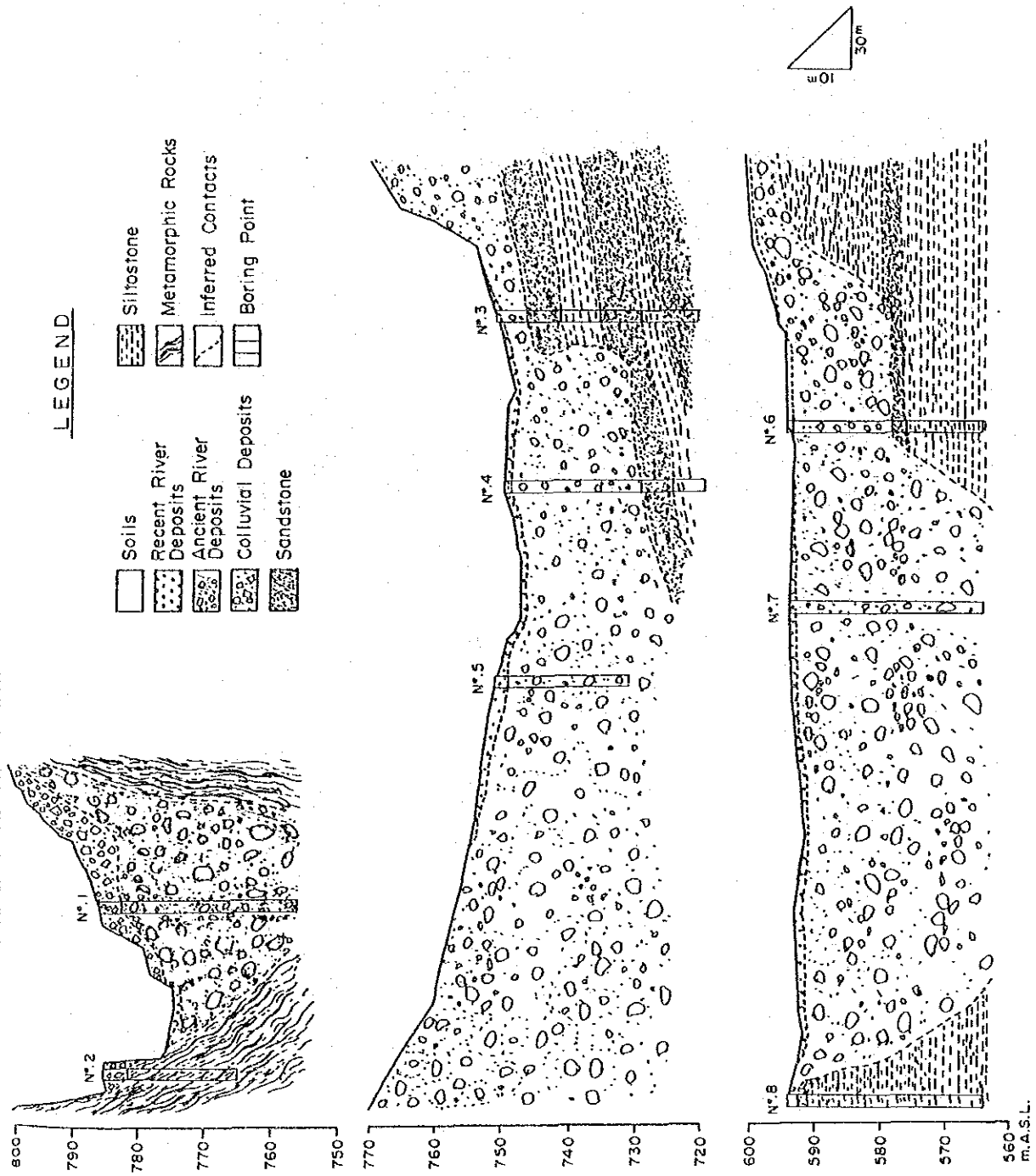


Fig. I-2-5 Geological Profile at Proposed Site of Head Works

BORING LOG

Boring No. 1 (Alt. I-1)

Elevation 785.54 m A.S.L.

Inclination Vertical

Location Right Margin of the Cuape River at Angostura Bridge

Total Depth 30 m

Date Oct. 1988

Scale (m)	Elevation (m)	Depth (m)	Thickness (m)	Columnar Section	Colour	Lithology	Observation	Sampling			N-Value
								Depth (m)	%	RQD	
1					Light beige		Angular - sub-angular pebbles and gravels of metamorphic, plutonic and volcanic origins	0.00-0.50	SS		
								0.50-1.00	100	0	
2					Reddish		medium compacted. layers of coarse sand with fragments of shell	1.00-1.90	48	24	
								1.90-2.40	SS		
3	782.54	3.00	3.00		Light beige	Medium - fine Pebbles		2.40-3.00	38	0	
	782.04	3.50	0.50					3.00-3.50			
4					Reddish	and	Silt layer	3.50-4.20	77	0	
								4.20-5.00	33	0	
5					Reddish			5.00-5.30			
								5.30-5.70	63	0	
6					Grayish beige	Coarse - medim - fine gravels		5.70-6.20	SS		
								6.20-7.45	92	0	
7					Grayish beige	In matrix		7.45-8.00	62	0	
								8.00-8.70	72	0	
8					Grayish beige	of coarse, medium and fine sand and some portion of silt & clay		8.70-9.60	82	26	
								9.60-10.00	68	0	
9					Grayish beige		Round and sub-round pebbles and gravels of metamorphic, plutonic and volcanic origins	10.00-10.30	100	57	
								10.39-11.00	70	0	
10					Grayish beige			11.00-11.90	74	0	
								11.90-13.30	79	70	
11					Grayish beige			13.30-13.70	90	0	
								13.70-14.10	100	38	
12					Grayish beige			14.10-15.50	34	0	
								15.50-16.30	42	0	
13					Grayish beige			16.30-17.80	29	0	
								17.80-19.30	46	0	
14					Grayish beige			19.30-19.70	45	0	
								19.70-21.00	26	0	
15					Grayish beige			21.00-22.50	38	8	
								22.50-23.00	100	44	
16					Grayish beige			23.00-24.00	16	0	
								24.00-25.50	24	0	
17					Grayish beige			25.50-26.00	76	0	
								26.00-27.50	27	0	
18					Grayish beige			27.50-29.00	20	8	
								29.00-30.00	38	0	
19	755.54	30.00									

Fig.I-2-6 (1) BORING LOG

BORING LOG

Boring No 2 (Alt. 1-2)

Elevation 785.10 m A.S.L.

Inclination Vertical

Location Left Margin of the Guape River at Angosture Bridge

Total Depth 20m

Date Oct. 1988

Scale (m)	Elevation (m)	Depth (m)	Thickness (m)	Columnar Section	Colour	Lithology	Observation	Sampling			N-Value
								Depth (m)	%	RQD	
1					Grayish beige	Coarse - fine pebbles and gravels in matrix of sandy silt	Angular-sub-angular pebbles and gravels of metamorphic, plutonic and volcanic origins.	0.00-1.50	hand	du	
2	782.50	2.60	2.60				Medium compacted	1.50-2.00	55		
								2.00-2.50	55		
3	781.30	3.80	1.20		Gray	Sandy silt with coarse fine gravels	Sub-round-sub-angular gravels	2.50-3.00	55		
								3.00-3.80	37	0	
4								3.80-4.30	100	15	
5								4.30-5.00	100	12	
6								5.00-6.00	100	18	
7								6.00-7.50	77	35	
8								7.50-8.25	100	15	
9							Clear schistosity	8.25-8.40	100	0	
							Gentle folding	8.40-9.00	95	10	
10					Dark green and black	Phyllite	Many fractures	9.00-10.00	83	26	
11							Moderately weathered	10.00-10.80	95	20	
12								10.80-12.00	90	25	
13								12.00-13.50	88	32	
14								13.50-14.50	100	23	
15								14.50-16.00	95	26	
16								16.00-17.00	93	15	
17								17.00-18.00	97	22	
18								18.00-19.50	100	12	
19								19.50-20.00	99	10	
20	765.10	20.00									
21											
22											
23											
24											
25											
26											
27											
28											
29											
30											

Fig. I-2-6 (2) BORING LOG

BORING LOG

Boring No 3(Alt.11-1)

Elevation 750.64m A.S.L.

Inclination Vertical

Location Right Margin of the Guape River at Alvaro Ordoñez Farm

Total Depth 30 m

Date Oct. 1988

Scale (m)	Elevation (m)	Depth (m)	Thickness (m)	Columnar Section	Colour	Lithology	Observation	Sampling			N-Value
								Depth (m)	%	RQD	
1	750.34	0.30	0.30		Dark brown	Soil	Contain roots. Moderately compacted Round-sub-round pebbles and gravels of metamorphic, plutonic and volcanic origins. In matrix of sand and some silt.	0.00-0.30	83	0	
								0.30-1.10	88	0	
								1.10-2.00	78	73	
								2.00-3.50	51	0	
4	746.44	4.20	3.90		Light gray	Fine sandstone and partially coarse sandstone	Moderately hard rock Fractured with calcite veins. Some alternation of silt and gravel layers. Partially weathered with beige colour.	3.50-4.30	63	0	
								4.30-5.80	97	36	
								5.80-6.80	51	10	
								6.80-7.30	50	0	
9	741.34	9.30	5.10		Dark gray	Siltstone	Bland-moderately hard Very fractured. Some alternation of clay and sandstone layers.	7.30-8.80	56	0	
								8.80-10.30	74	0	
								10.30-11.85	63	7	
								11.85-14.00	82	13	
15	735.44	15.20	5.90		Grayish beige	Fine sandstone	Moderately hard-hard. A little fractured with veins of calcite. Some alternation of silt layer. Some layers of coarse sandstone.	14.00-15.30	78	11	
								15.30-16.70	88	28	
								16.70-18.00	81	30	
								18.00-19.40	72	21	
22	729.04	21.60	6.40		Dark gray	Siltstone	Bland-moderately hard Fractured.	19.40-21.60	68	18	
								21.60-22.90	75	9	
								22.90-24.45	77	14	
								24.45-26.00	69	17	
26	726.34	24.30	2.70		Grayish beige	Fine sandstone	Hard rock. Some alternation of silt and gravel layers.	26.00-27.30	72	23	
								27.30-28.80	70	18	
								28.80-30.00	86	29	
30	720.64	30.00									

Fig.I-2-6 (3) BORING LOG

BORING LOG

 Boring No 4(Alt. 11-2)

 Elevation 749.59 m A.S.L

 Inclination Vertical

 Location River Bed of the Guape River
at Alvaro Ordoñez's Farm

 Total Depth 30 m

 Date Oct. 1988

Scale (m)	Elevation (m)	Depth (m)	Thickness (m)	Columnar Section	Colour	Lithology	Observation	Sampling			N-Value
								Depth (m)	%	RQD	
1					Light-dark gray	C.-f. pebbles and gravels in matrix of sand, and some portion of silt	Round-sub-round pebbles and gravels of metamorphic, plutonic and volcanic origins	0.00-1.30	Hand dug		
2			1.30-2.00					86	0		
								2.00-2.60	95	0	
3								2.60-3.00	100	0	
4								3.00-4.30	31	0	
5								4.30-4.80	30	0	
6								4.80-5.80	30	0	
7								5.80-6.50	72	0	
8								6.50-7.50	50	0	
9								7.50-8.00	80	0	
10								8.00-9.00	67	0	
11								9.00-10.10	51	0	
12								10.10-11.50	41	0	
13								11.50-12.00	43	0	
14								12.00-12.90	32	0	
15								12.90-14.00	16	0	
16								14.00-15.30	20	0	
17								15.30-16.00	14	0	
18								16.00-16.70	23	0	
19								16.70-18.00	65	0	
20				18.00-18.80	52	0					
21				18.80-19.50	72	0					
22				19.50-20.50	43	0					
23				20.50-21.80	60	15					
24				21.80-23.20	51	12					
25				23.20-24.00	78	30					
26				24.00-25.00	86	38					
27				25.00-25.60	86	16					
28				25.60-27.10	77	15					
29				27.10-27.90	71	11					
30				27.90-29.00	85	9					
				29.00-30.00	82	10					

Fig.I-2-6 (4) BORING LOG

BORING LOG

Boring No 5(Ali-11-3)

Elevation 750.73 m A.S.L.

Inclination Vertical

Location Left Margin of the Guape River
at Alvaro Ordoñez's Farm

Total Depth 20 m

Date Oct., 1988

Scale (m)	Elevation (m)	Depth (m)	Thickness (m)	Columnar Section	Colour	Lithology	Observation	Sampling			N-Value				
								Depth (m)	%	RQD					
1	750.73	0.50	0.50		Dark brown	Soil	Contains root	0.00-0.50	SS		~10				
								0.50-1.00	SS						
2	748.73	2.00	1.50		Dark beige	C.-f. silty sand and gravels		1.00-2.00	50	0					
3					Light gray	C.-f. pebbles and gravels in matrix of sand and some silt	Moderately compacted Round-sub-round pebbles and gravels of plutonic metamorphic and volcanic origins Some alternation of silt and coarse sand layers	2.00-4.00	40	6					
4								4.00-6.00	34	0					
5								6.00-6.80	43	0					
6								6.80-8.00	62	0					
7								8.00-9.50	36	0					
8								9.50-10.40	52	0					
9								10.40-11.50	65	0					
10								11.50-12.80	43	0					
11								12.80-13.50	49	0					
12								13.50-14.80	56	0					
13								14.80-16.00	68	0					
14								16.00-17.40	40	0					
15								17.40-18.80	51	0					
16								18.80-21.00	56	0					
17															
18															
19															
20	730.73	20.00													
21															
22															
23															
24															
25															
26															
27															
28															
29															
30															

Fig.I-2-6 (5) BORING LOG

BORING LOG

Boring No 6(Alt.111-1)

Elevation 594.88 m A.S.L.

Inclination Vertical

Location Right Margin of the Guape River at Finca La Pradera

Total Depth 30 m

Date Nov. 1988

Scale (m)	Elevation (m)	Depth (m)	Thickness (m)	Columnar Section	Colour	Lithology	Observation	Sampling			N-Value				
								Depth (m)	%	RQD					
1	593.88	1.00	1.00		Dark brown	Soil	Contain roots	0.00-1.30	Hand dug						
2					Light gray	C.-f. pebbles and gravels in matrix of sand and a little portion of silt	Moderately compacted Round-sub-round pebbles and gravels of plutonic, volcanic and metamorphic origins	1.30-2.50	75	0					
								2.50-2.60	100	0					
								2.60-3.00	68	0					
								3.00-3.30	87	0					
								3.30-3.60	70	0					
								3.60-4.60	40	0					
								4.60-5.70	41	0					
								5.70-6.10	55	0					
								6.10-6.40	67	0					
								6.40-7.10	57	0					
								7.10-8.20	80	0					
								8.20-10.05	19	0					
								10.05-11.90	68	0					
								11.90-13.30	55	0					
								13.30-14.70	79	0					
				14.70-15.80	72	0									
16	579.08	15.80	14.80												
17					Light beige	H. sandstone	Compacted clear stratification	15.80-17.10	96	28					
								17.10-18.20	88	32					
18	596.88	18.00	2.20												
19									Light-dark gray	Siltstone and partially sandy siltstone	Moderately compacted Carbon layers f. sandstone layer Clear stratification	18.20-19.20	67	0	
												19.20-21.00	64	5	
												21.00-22.30	82	12	
												22.30-23.20	77	7	
												23.20-24.00	68	10	
												24.00-25.40	82	16	
												25.40-26.30	60	7	
				26.30-27.00	51	0									
				27.00-28.15	56	0									
				28.15-28.80	64	5									
29															
30	564.88	30.00						28.80-30.00	71	11					

Fig.I-2-6 (6) BORING LOG

BORING LOG

Boring No. 7(A.L.111-2)

Elevation 594.42 m A.S.L.

Inclination Vertical

Location River Bed of the Guape River
at Finca la Pradera

Total Depth 30 m

Date Nov. 1988

Scale (m)	Elevation (m)	Depth (m)	Thickness (m)	Columnar Section	Colour	Lithology	Observation	Sampling			N-Value								
								Depth (m)	%	RQD	0	10	20	30	40	50			
1								0.00-1.30	Hand dug										
2								1.30-2.00	68	0									
3								2.00-2.90	72	0									
4								2.90-3.60	47	0									
5								3.60-5.10	63	0									
6								5.10-5.80	55	0									
7								5.80-6.70	40	0									
8								6.70-8.00	57	0									
9								8.00-9.20	83	0									
10								9.20-10.10	61	0									
11								10.10-11.40	43	0									
12						Light gray	C.-f. Pebbles and gravels in matrix of sand and some portion of silt	metamorphic origin	11.40-12.00	70	0								
13								Some silt layer	12.00-13.20	55	0								
14								Some coarse sand layer and pockets	13.20-14.10	67	0								
15									14.10-15.20	43	0								
16									15.20-16.40	41	0								
17									16.40-17.50	57	0								
18									17.50-18.70	66	0								
19									18.70-19.50	55	0								
20									19.50-20.10	45	0								
21									20.10-20.80	41	0								
22									20.80-21.90	36	0								
23									21.90-23.00	80	0								
24									23.00-23.70	55	0								
25									23.70-25.10	47	0								
26									25.10-25.80	40	0								
27									25.80-26.70	32	0								
28									26.70-27.40	58	0								
29									27.40-28.50	64	0								
30	564.42	30.00							28.50-29.20	78	0								
								29.20-30.00	58	0									

All values show more than 50

Fig.I-2-6 (7) BORING LOG

BORING LOG

Boring No. B(Alt. 111-3)

Elevation 594.01 m A.S.L.

Inclination Vertical

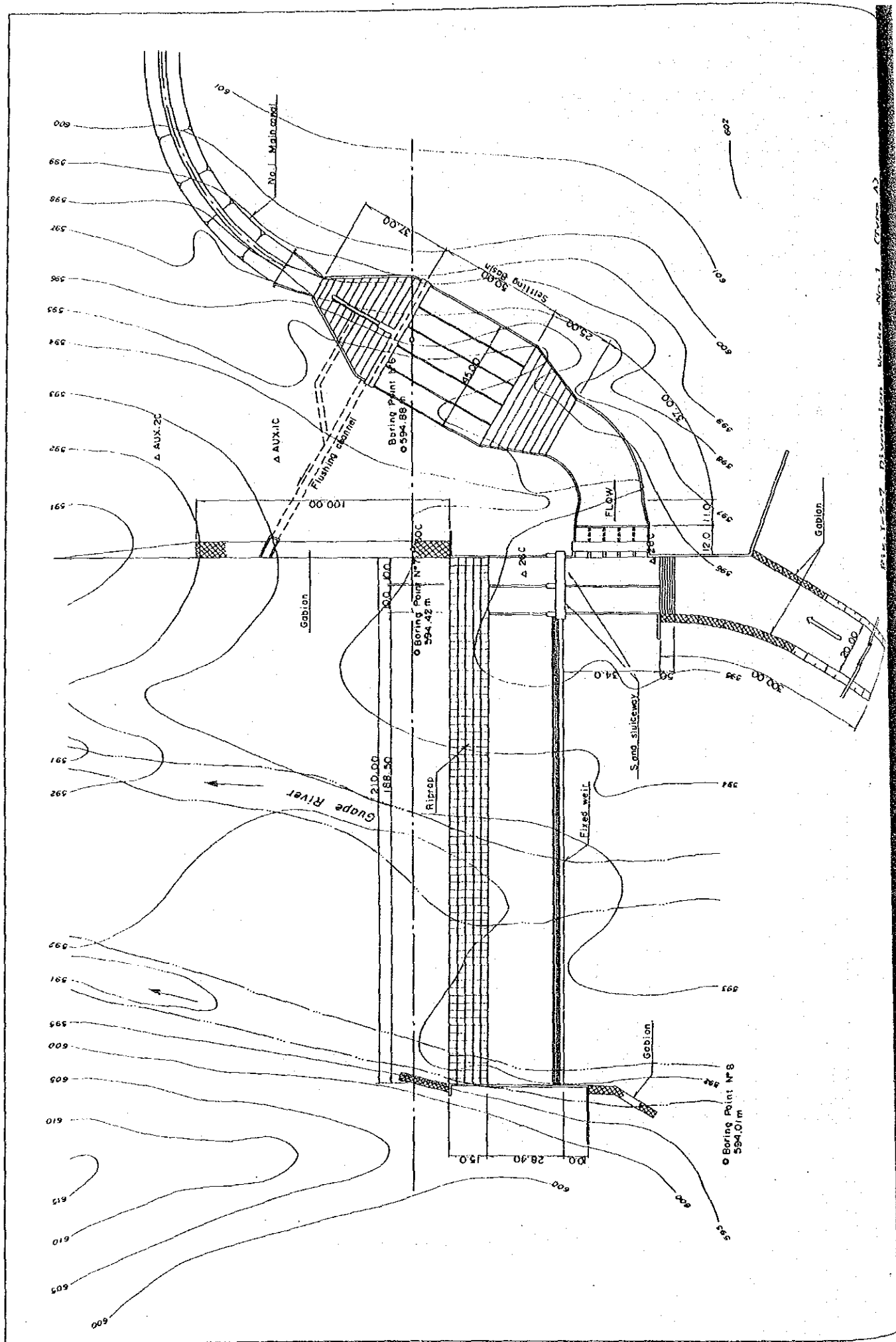
Location Left Margin of the Guape River at Finca la Prodera

Total Depth 30 m

Date Nov. 1988

Scale (m)	Elevation (m)	Depth (m)	Thickness (m)	Columnar Section	Colour	Lithology	Observation	Sampling			N-Value
								Depth (m)	%	RQD	
1	593.71	0.30	0.30		brown	Soil	Contain roots	0.00-1.00	Hand dug		
	592.51	1.50	1.20		Light beige	Pebbles and gravels	Moderately compacted.	1.00-1.60	83	0	
2	590.81	3.20	1.70		Light beige	H. sandstone	Compacted	1.60-2.50	95	7	
3							Clear stratification	2.50-3.20	88	16	
4							Moderately compacted	3.20-5.00	72	5	
5							Carbon layers	5.00-6.80	80	32	
6							Sandy siltstone	6.80-8.15	64	12	
7							Clear stratification with slight dip toward the east	8.15-9.60	85	8	
8							f. sandstone layer	9.60-10.80	60	3	
9							Partially weathered	10.80-12.30	78	13	
10					Light-dark gray Partially sandy siltstone	Partially sandy siltstone	Gravel contained zone	12.30-13.30	73	4	
11										13.30-14.90	
12								14.90-16.30	77	15	
13							f. sandstone layer	16.30-17.70	84	14	
14								17.70-19.40	63	10	
15								19.40-20.70	60	8	
16								20.70-22.00	83	11	
17								22.00-23.30	88	21	
18								23.30-24.70	80	27	
19								24.70-26.20	69	19	
20								26.20-26.90	74	17	
21							Gravel layer	26.90-27.70	70	2	
22								27.70-29.00	82	14	
23								29.00-30.00	86	22	
24	564.01	30.00									

Fig.I-2-6 (8) BORING LOG



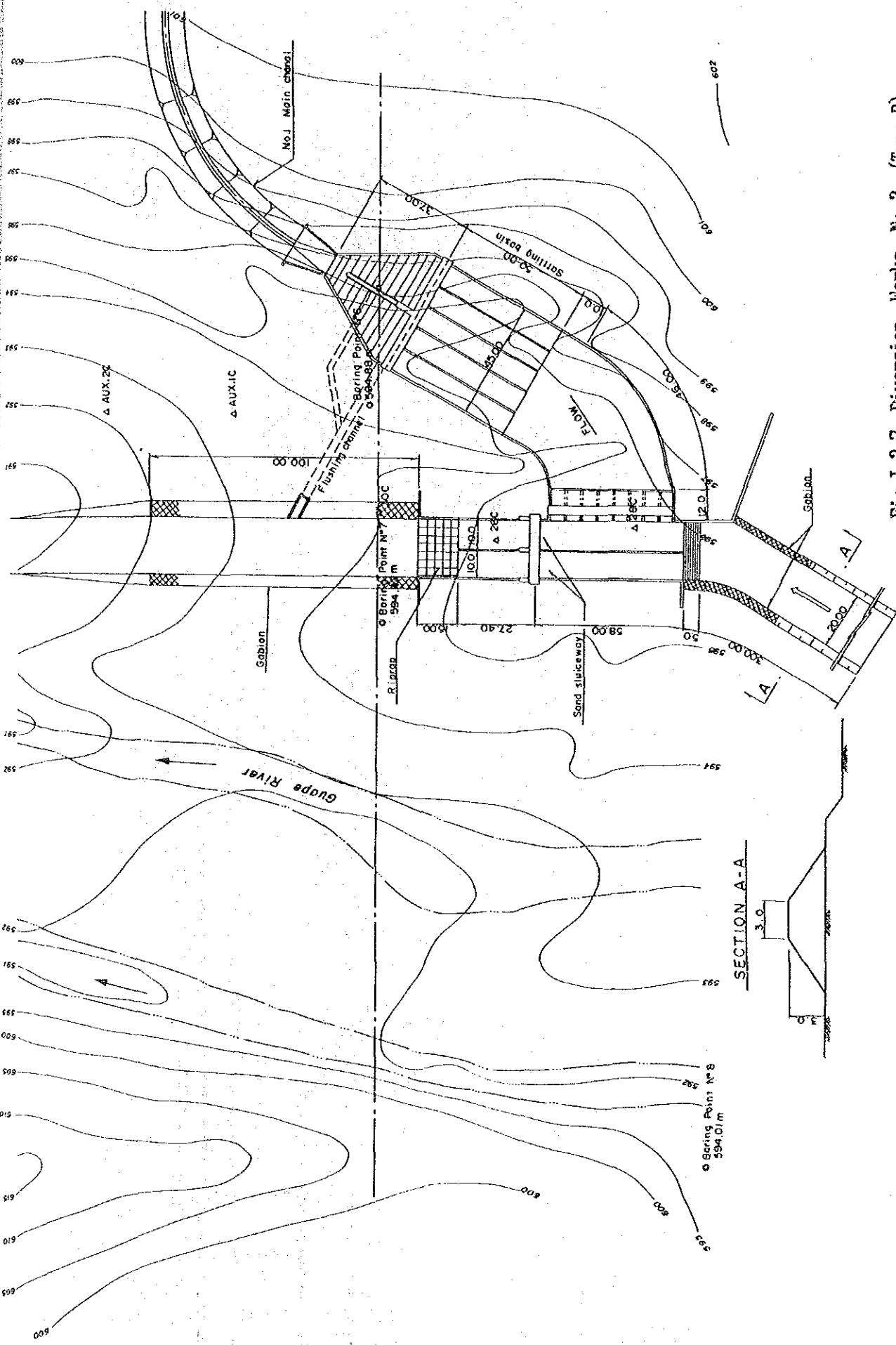


Fig. I-2-7 Diversion Works No. 2 (Type B)

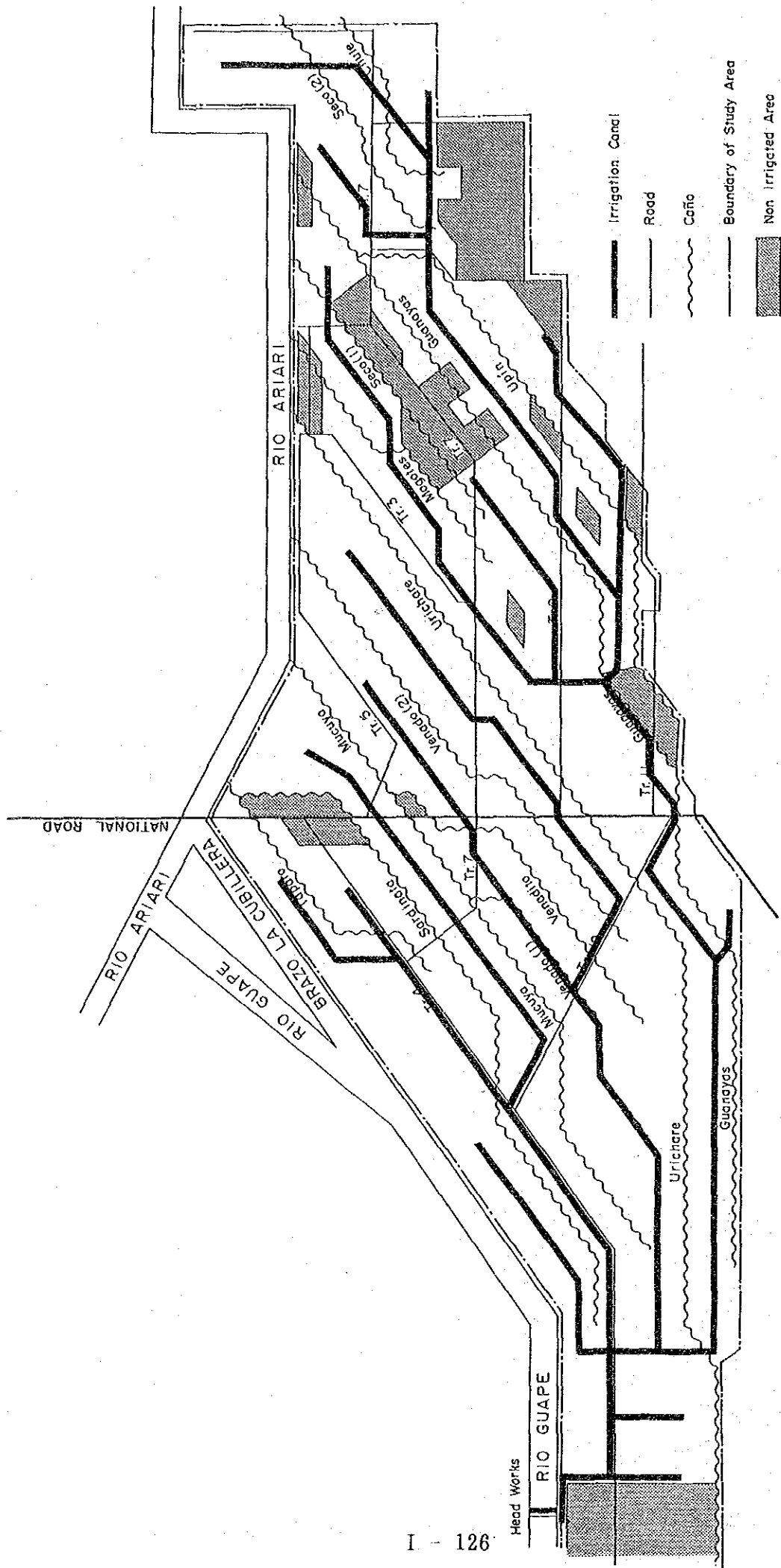
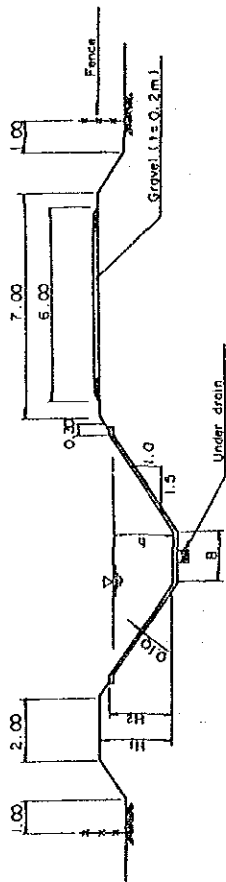
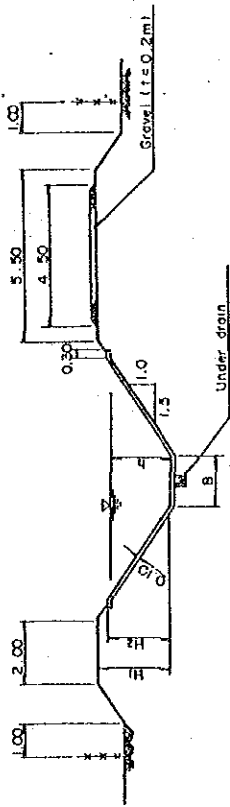


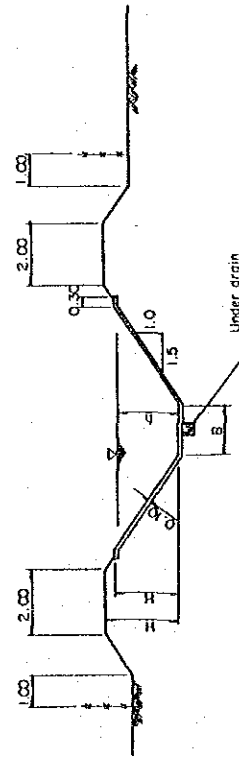
FIG. I-2-8 IRRIGATION CANAL SYSTEM PLAN I



C-a TYPE STANDARD SECTION



C-b TYPE STANDARD SECTION



C-c TYPE STANDARD SECTION

Canal Dimensions

Type	B	H ₁	H ₂	n	Q
C-1	2.5	3.7	3.4	1.5	36.725 ~ 35.509
C-2	1.5	2.7	2.5	1.5	17.672 ~ 17.034
C-3	1.5	2.7	2.4	1.5	16.872 ~ 16.018
C-4	1.5	2.5	2.3	1.5	15.424 ~ 14.997
C-5	1.5	2.5	2.1	1.5	14.717 ~ 14.209
C-6	1.0	2.0	1.8	1.5	8.631 ~ 8.225
C-7	1.0	1.7	1.5	1.5	6.102 ~ 5.428
C-8	1.0	1.6	1.4	1.5	5.330 ~ 5.032

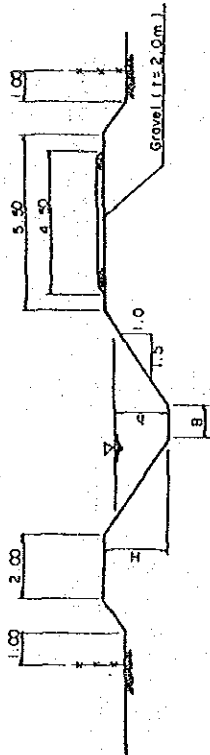
note B :Width Of Bottom(m)
H₁ :Height Of Canal(m)
H₂ :Height Of Lining(m)
n :Side Slope
Q :Design Discharge(m³ /sec)

Fig. I-2-10 Standard Section of Irrigation Canal (Concrete Lined)

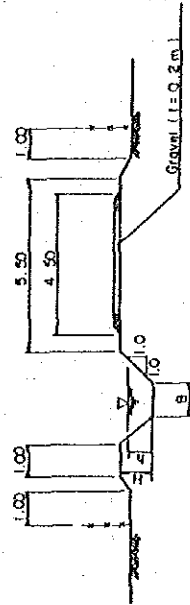
Canal Dimensions

Type	B	H	h	n	Q
So-1	1.0	2.3	2.0	1.5	4.776~4.328
So-2	1.0	2.1	1.8	1.5	4.058~3.558
So-3	1.0	1.9	1.7	1.5	3.382~2.962
So-4	1.0	1.8	1.5	1.5	3.004~2.531
So-5	1.0	1.7	1.4	1.5	2.692~2.124
So-6	1.0	1.5	1.3	1.5	2.205~1.934
So-7	1.0	1.5	1.3	1.5	2.205~1.717
So-8	1.0	1.3	1.1	1.5	1.786~1.154
So-9	1.0	1.1	0.9	1.5	1.326~0.541
So-10	1.0	1.0	0.8	1.5	1.096~0.730
So-11	1.0	0.9	0.7	1.5	0.731~0.257
So-12	1.0 0.5	1.1 0.9	0.9 0.6	1.0	Under 0.723

note B:Width Of Bottom(m)
 H:Height Of Canal(m)
 h:Height Of Lining(m)
 n:Side Slope
 Q:Design Discharge(m³ /sec)



So-a TYPE STANDARD SECTION



So-b TYPE STANDARD SECTION

Fig. 1-2-11 Standard Section of Irrigation Canal (Unlined)

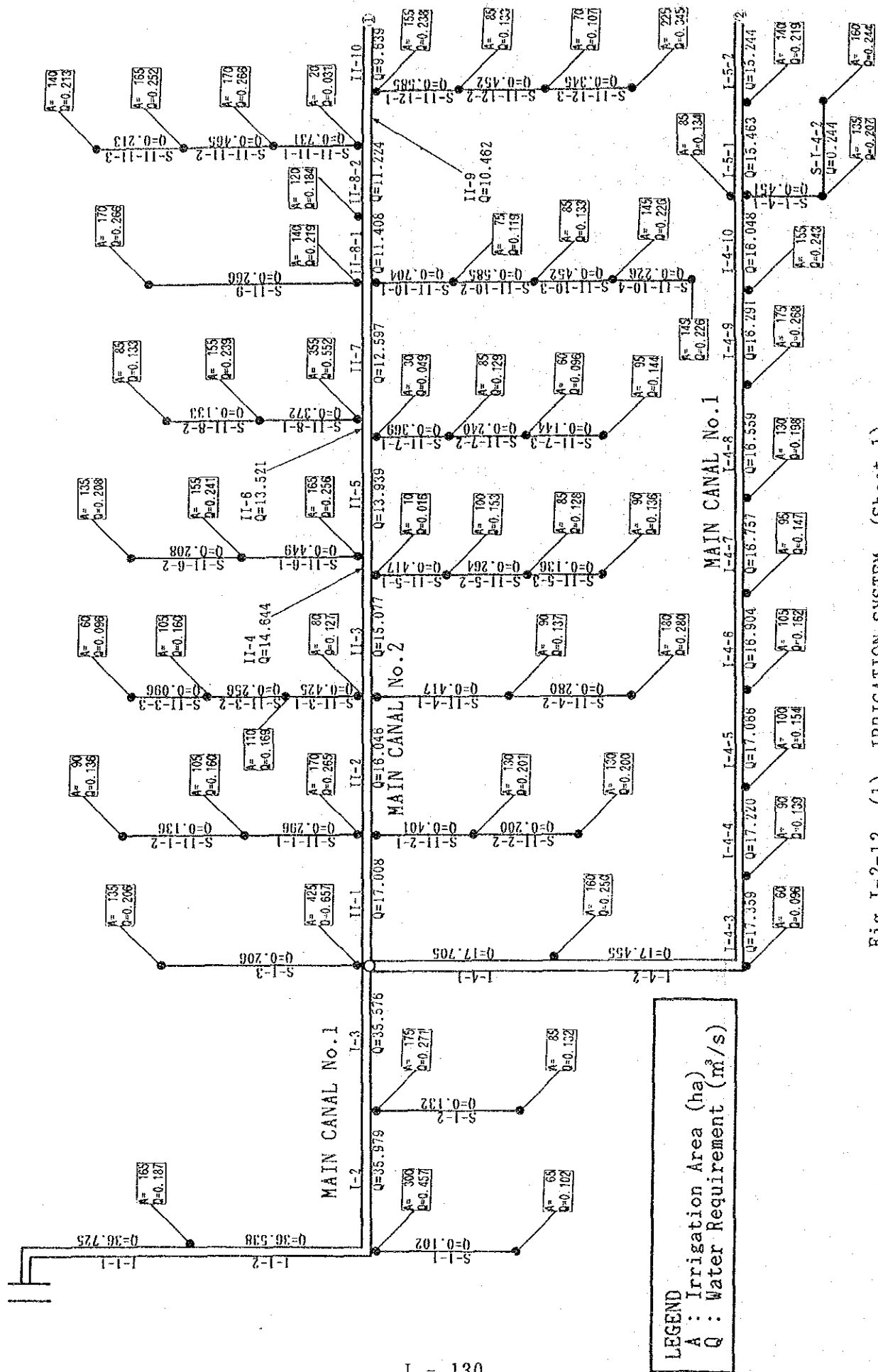


Fig. I-2-12 (1) IRRIGATION SYSTEM (Sheet 1)

LEGEND
 A : Irrigation Area (ha)
 Q : Water Requirement (m³/s)

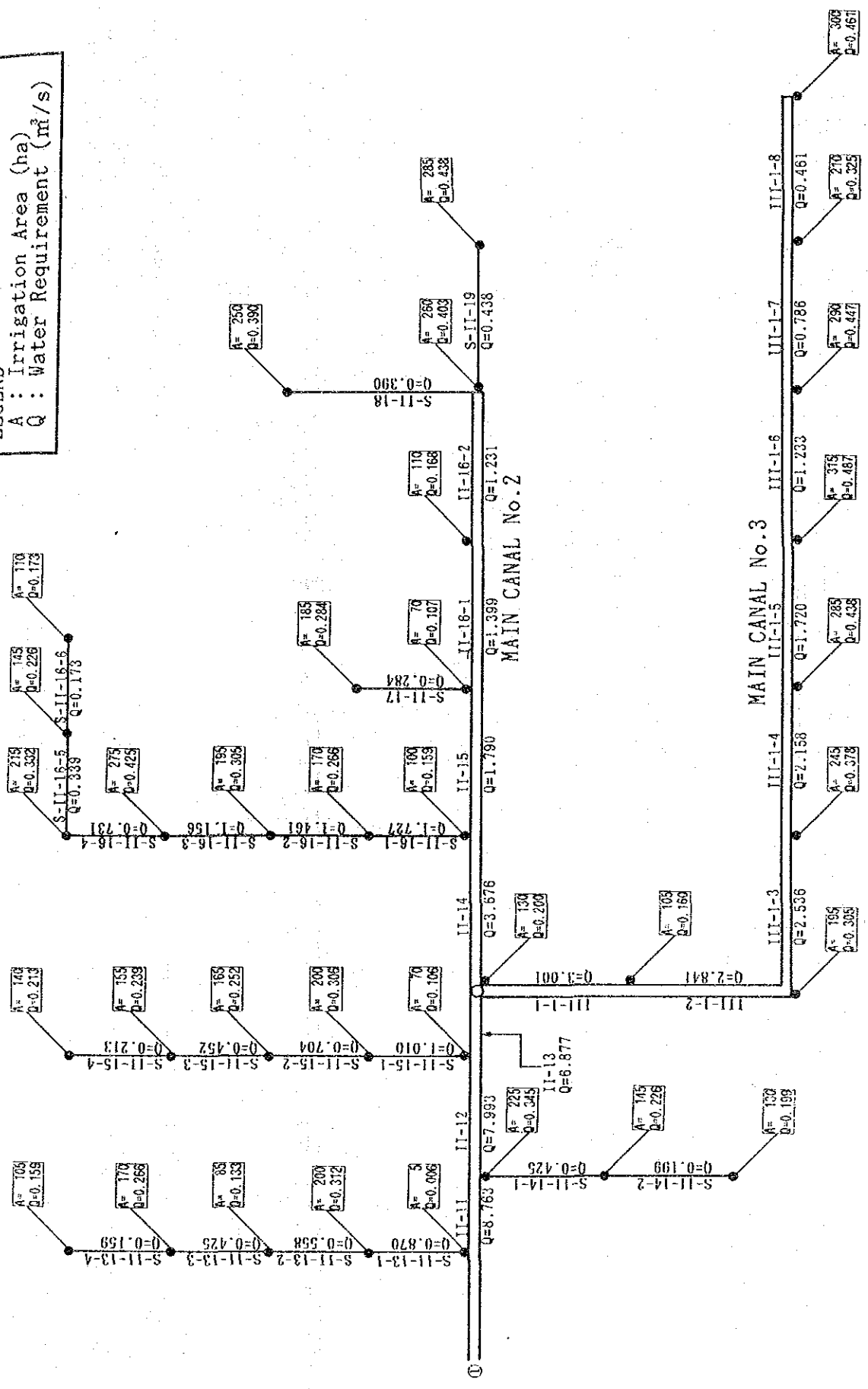


Fig.I-2-12 (2) IRRIGATION SYSTEM (Sheet 2)

LEGEND
 A : Irrigation Area (ha)
 Q : Water Requirement (m³/s)

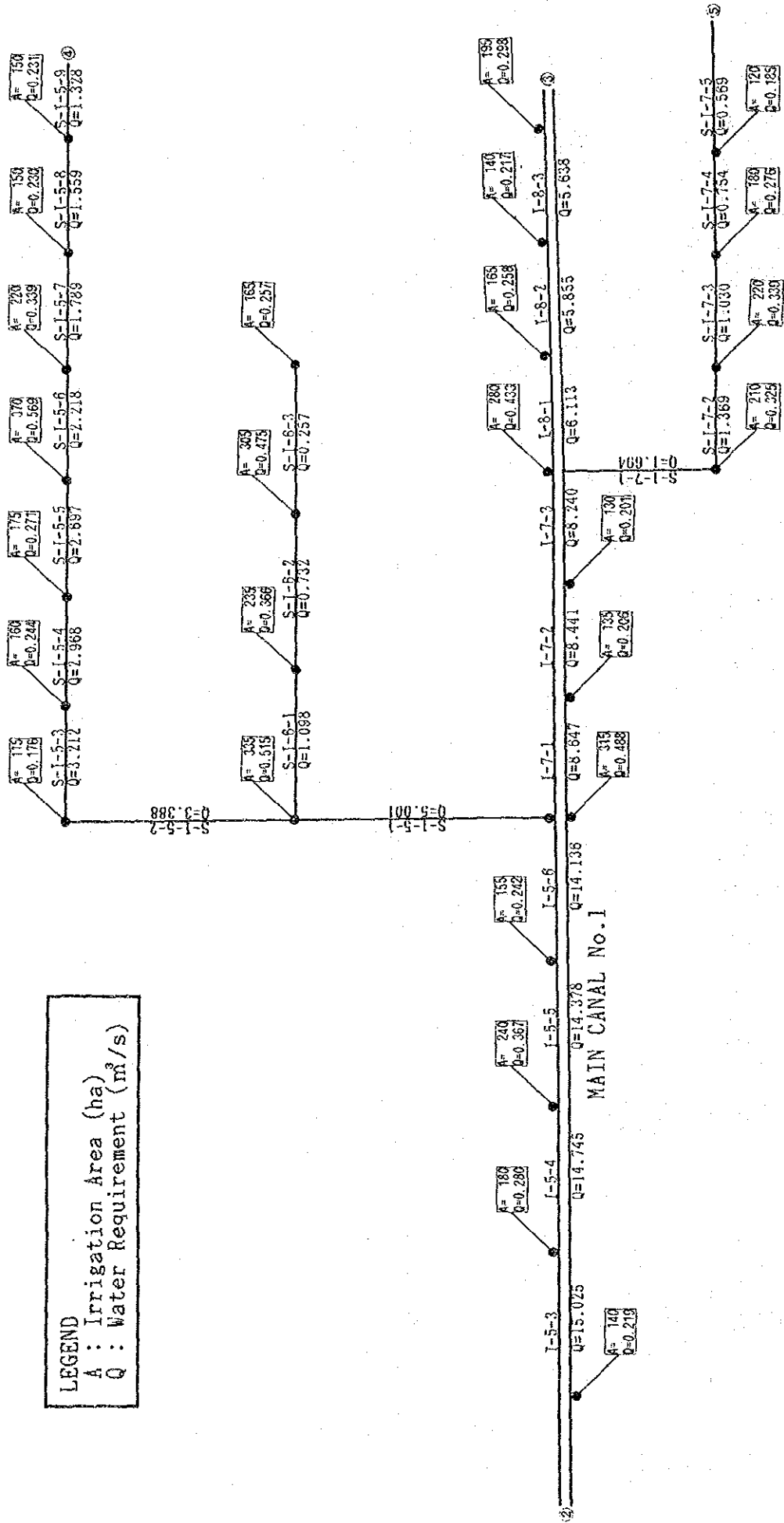


Fig. I-2-12 (3) IRRIGATION SYSTEM (Sheet 3)

LEGEND
 A : Irrigation Area (ha)
 Q : Water Requirement (m³/s)

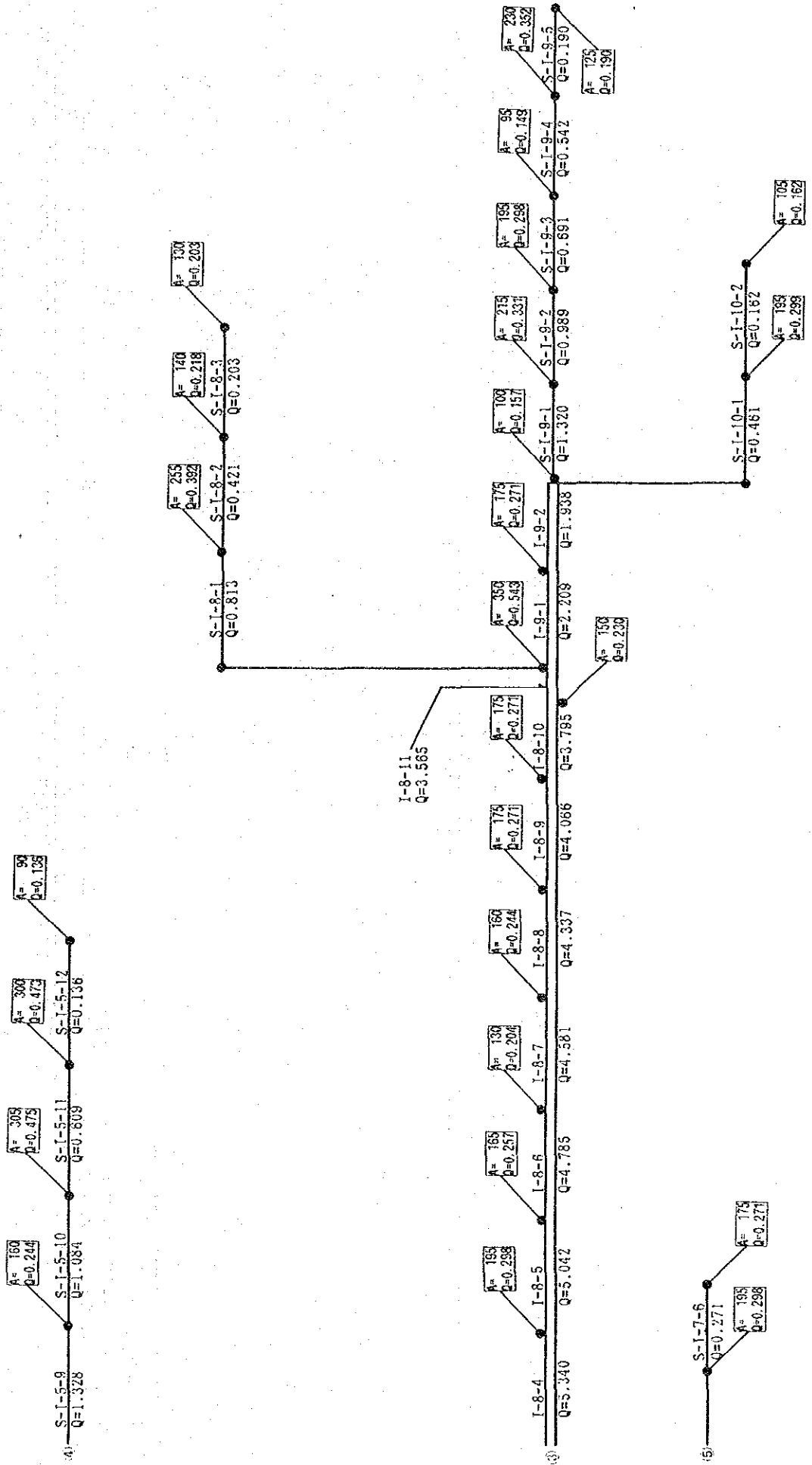


Fig. I-2-12 (4) IRRIGATION SYSTEM (Sheet 4)

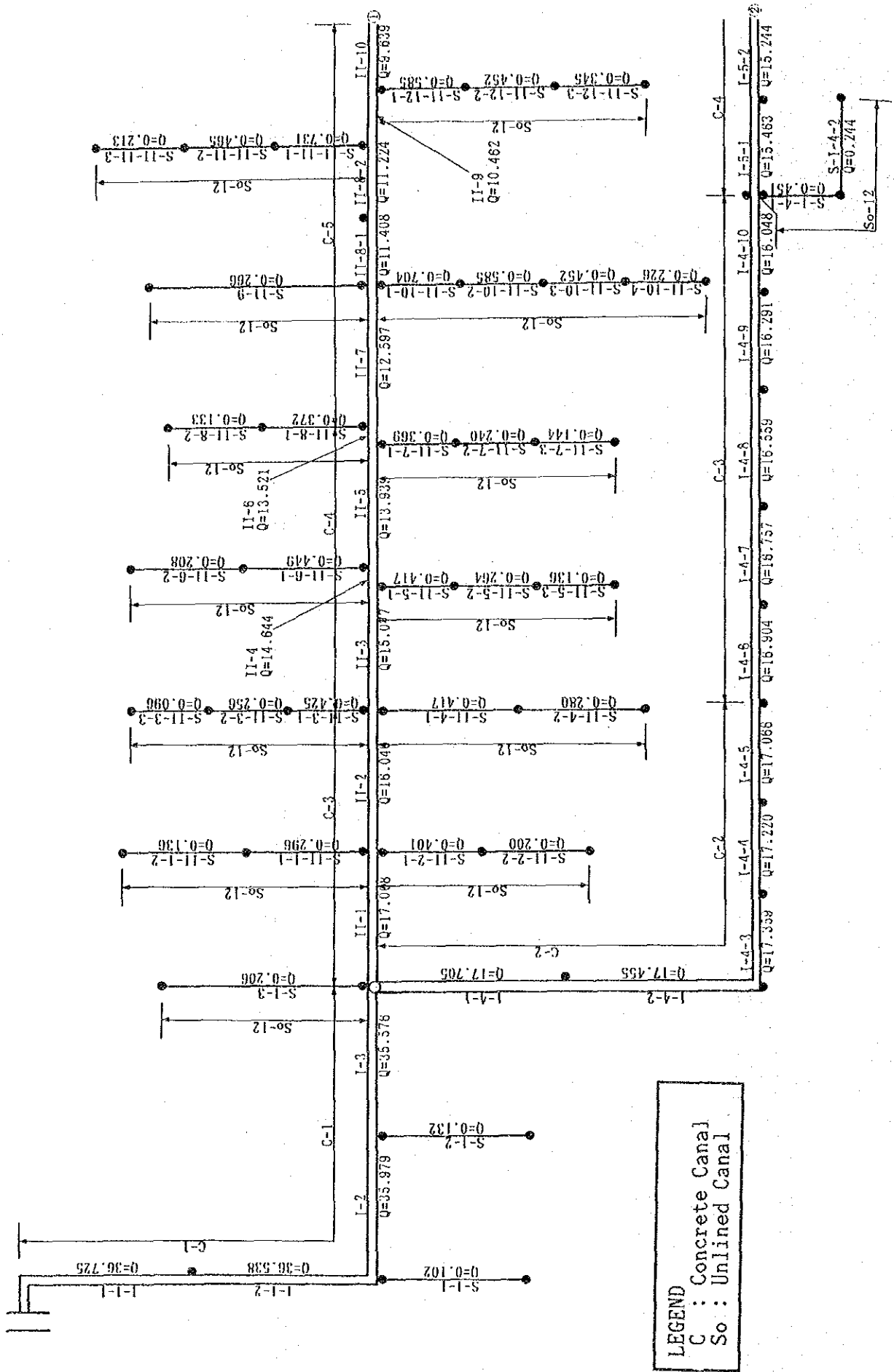


FIG. I-2-12 (5) IRRIGATION SYSTEM (Sheet 5)

LEGEND
 C : Concrete Canal
 S : Unlined Canal

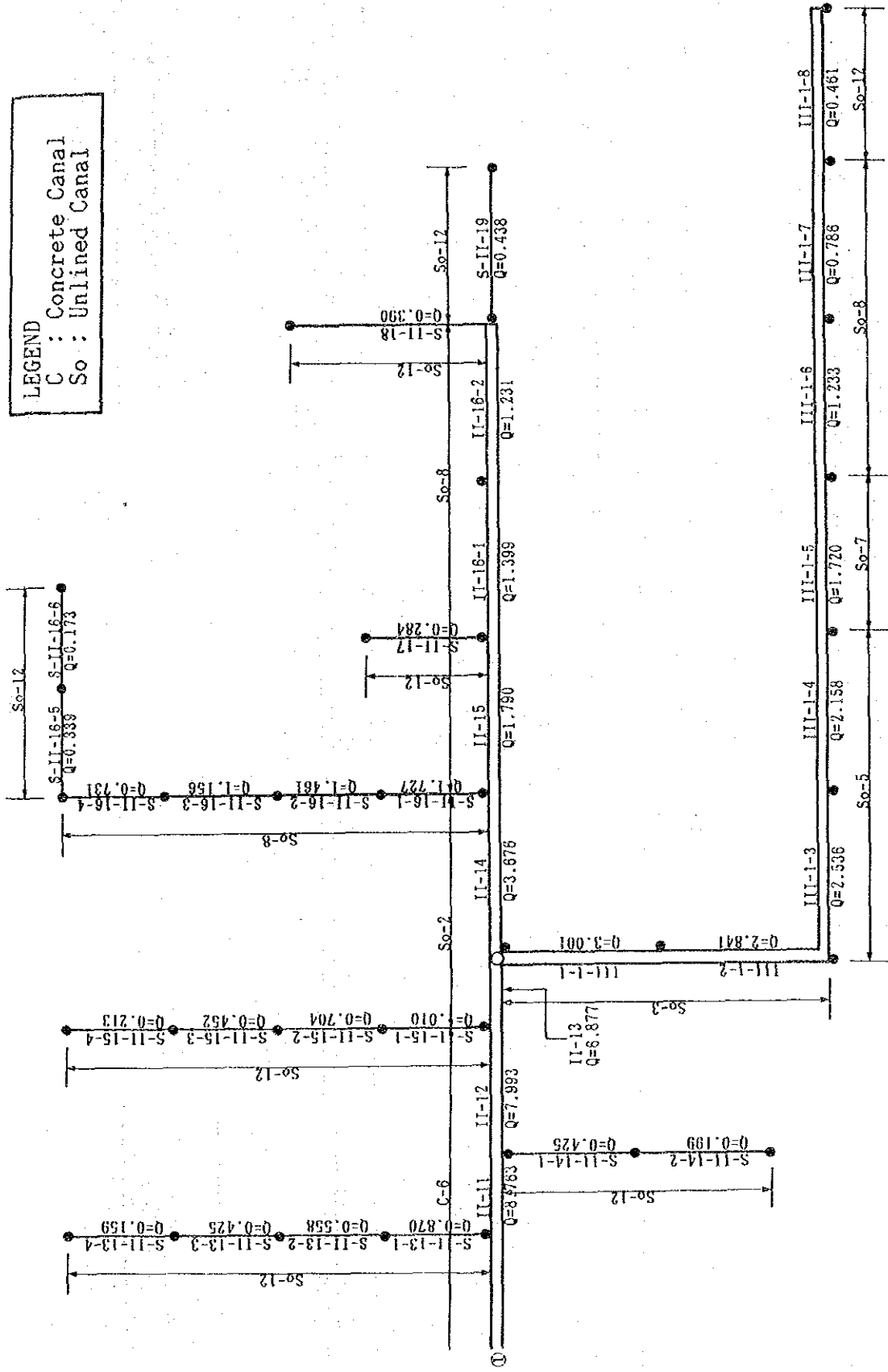


Fig. I-2-12 (6) IRRIGATION SYSTEM (Sheet 6)

LEGEND
 C : Concrete Canal
 So : Unlined Canal

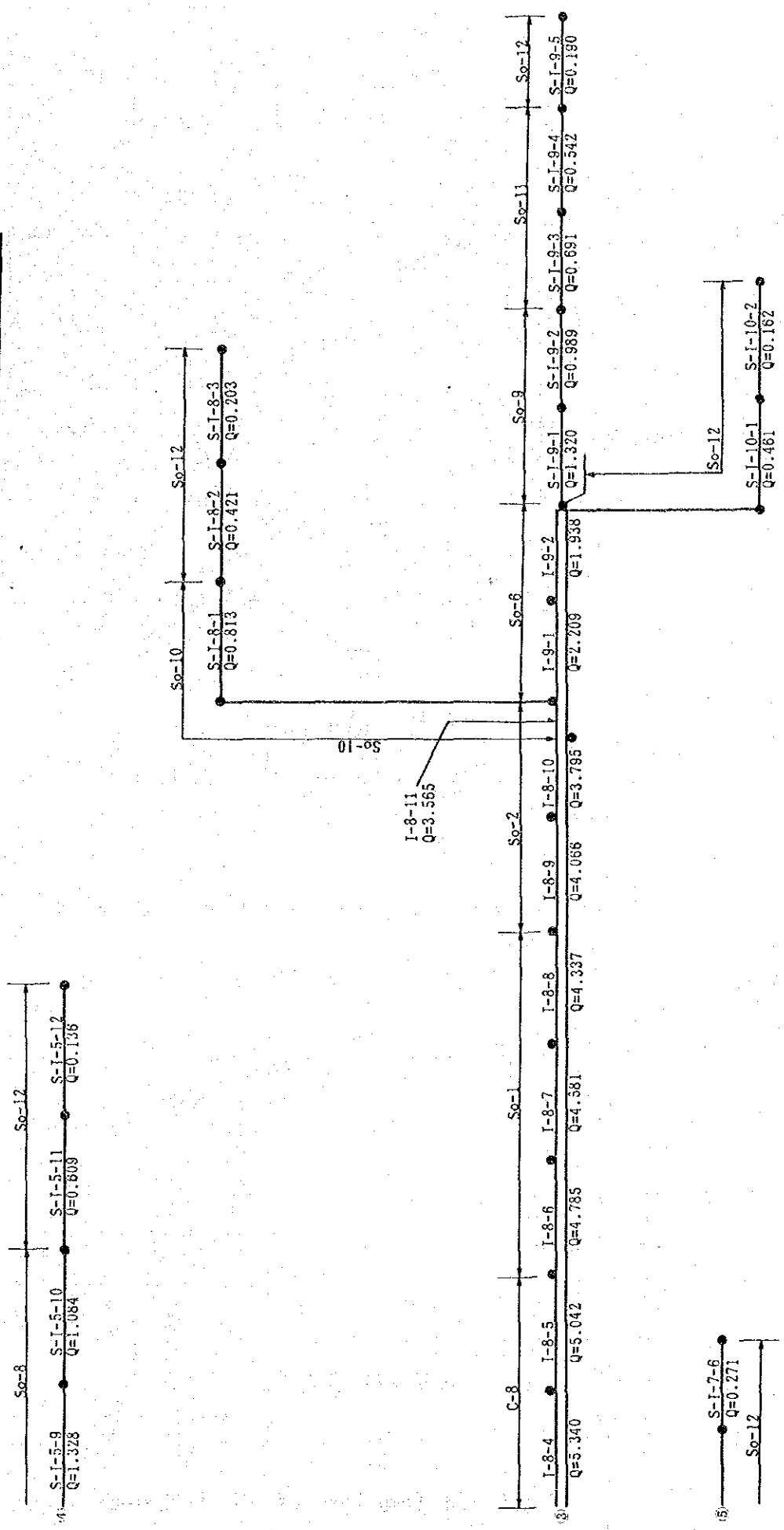
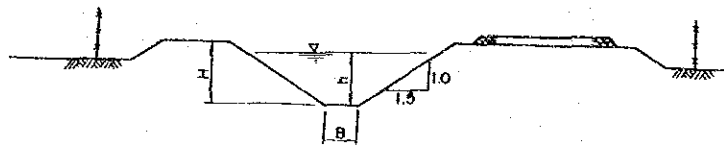
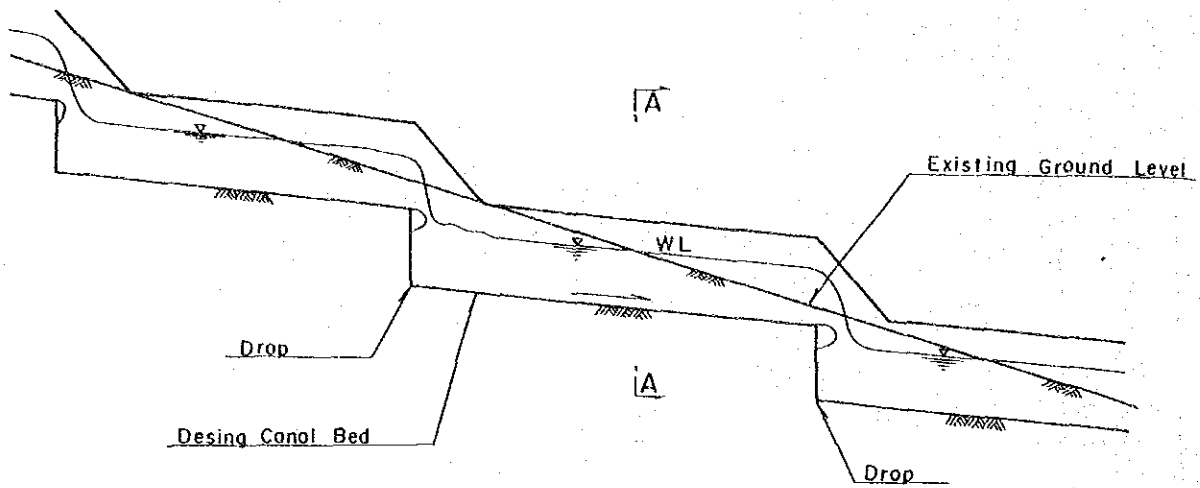
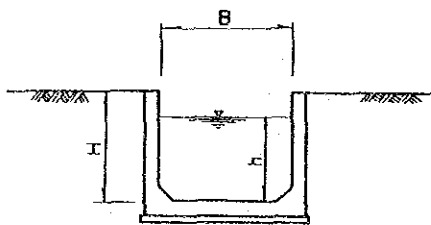
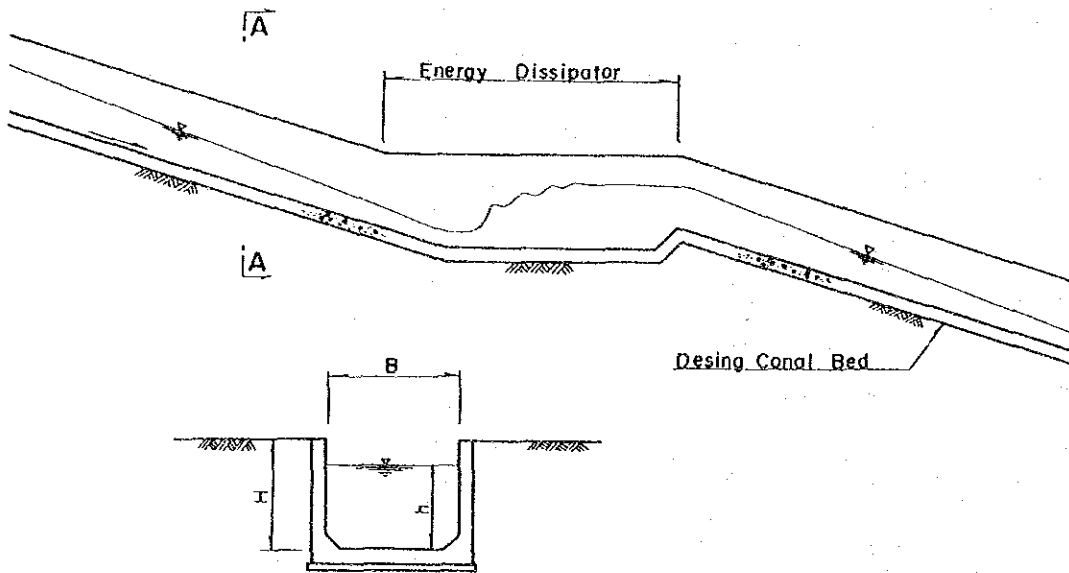


Fig. I-2-12 (8) IRRIGATION SYSTEM (Sheet 8)



SECTION A-A

DROP TYPE

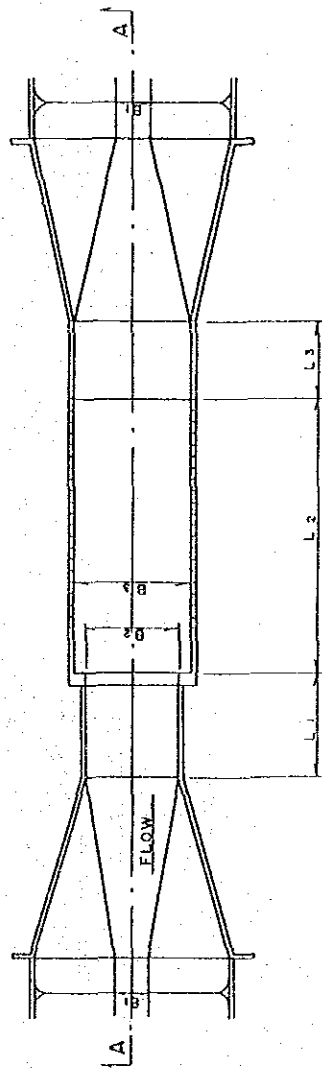


SECTION A-A

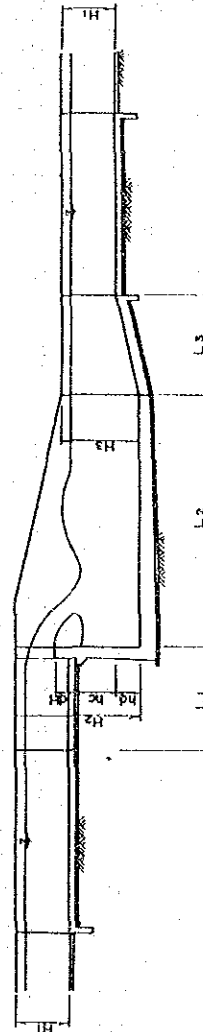
CHUTE TYPE

Fig.I-2-13 Camprison of Canal System

DROP



PLAN



SECTION A-A

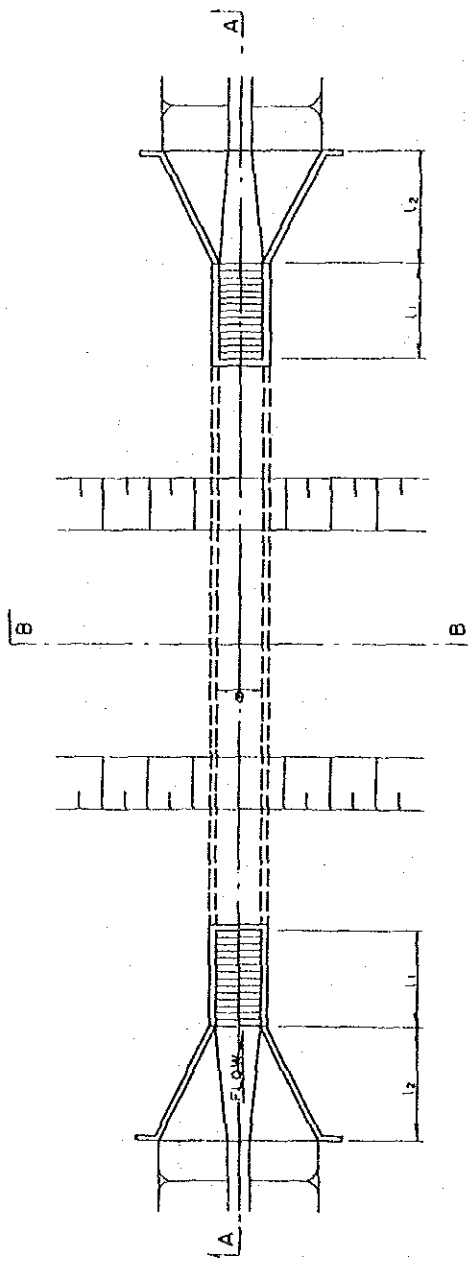
DIMENSIONS

(m)

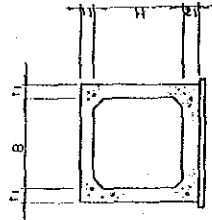
TYPE	Q (m ³ /sec)		H1	H2	dH	hc	hd	B1	B2	B3	L1	L2	L3
	max	min											
1	37	36	3.8	7.0	0.6	2.0	1.2	2.5	4.6	5.6	5.5	17	4.8
2	18	17	2.7	5.9	0.6	2.0	1.2	1.5	4.1	5.1	4.9	14	4.8
3	17	14	2.5	5.6	0.6	2.0	1.1	1.5	4.1	5.1	4.6	12	4.4
4	14	11	2.3	5.4	0.6	2.0	1.1	1.5	4.0	5.0	4.5	11	4.4
5	11	9	2.1	5.1	0.6	2.0	1.0	1.0	3.7	4.7	4.4	9.5	4.0
6	9	6	2.0	4.9	0.6	2.0	0.9	1.0	3.6	4.6	4.3	9	3.6
7	6	3.8	2.0	4.8	0.6	2.0	0.8	1.0	2.7	3.7	4.3	8.5	3.2
8	3.8	3.3	1.9	4.7	0.6	2.0	0.8	1.0	2.3	3.3	4.3	8	3.2
9	3.3	2.5	1.8	4.5	0.5	2.0	0.7	1.0	2.2	3.2	4.2	7.5	2.8
10	2.5	2.2	1.6	4.3	0.4	2.0	0.7	1.0	2.0	3.0	4.2	7	2.8
11	2.2	1.7	1.5	4.2	0.35	2.0	0.7	1.0	1.9	2.9	4.2	6.5	2.8
12	1.7	1.3	1.3	3.9	0.25	2.0	0.6	1.0	1.7	2.7	4.1	6	2.4
13	1.3	1.0	1.0	3.6	0.2	2.0	0.6	1.0	1.5	2.5	4.1	5.5	2.4
14	1.0	0.1	0.9	3.5	0.2	2.0	0.6	1.0	1.2	2.2	4.0	5	2.0
15	2.0	1.7	1.3	2.8	0.35	1.0	0.5	1.0	1.8	2.8	3.4	5	2.0
16	1.7	1.3	1.1	2.6	0.25	1.0	0.5	1.0	1.6	2.6	3.4	4.5	1.6
17	1.2	0.1	1.0	2.4	0.2	1.0	0.4	1.0	1.5	2.5	3.2	4	1.6

Fig. I-2-14 Related Structure No.1 (Drop)

SIPHON-I



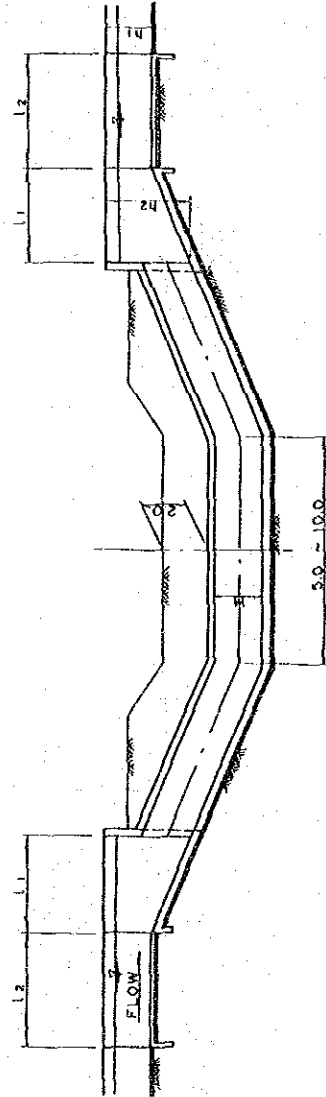
PLAN



SECTION B-B

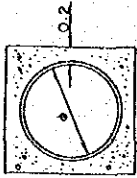
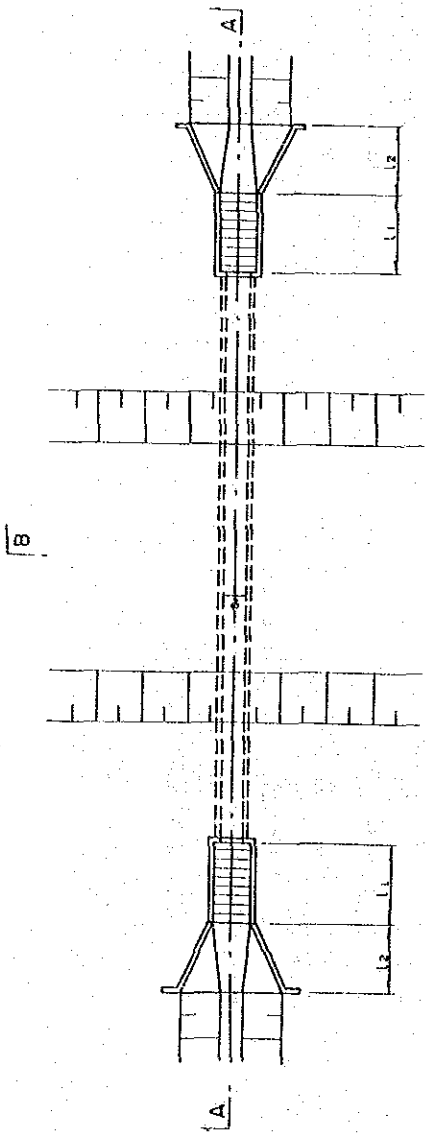
DIMENSIONS

TYPE	Q (m ³ /sec)		B	H	h ₁	h ₂	l ₁	l ₂	l ₁	l ₂
	max	min								
1	37	36	3.5	3.5	3.7	6.0	6.0	5.0	0.4	0.45
2	18	15	2.5	2.5	2.7	4.5	4.5	5.0	0.3	0.35
3	13	8	2.0	2.0	2.1	3.5	3.5	5.0	0.5	0.35
4	6	2.5	1.5	1.5	2.1	3.0	2.5	5.0	0.3	0.35

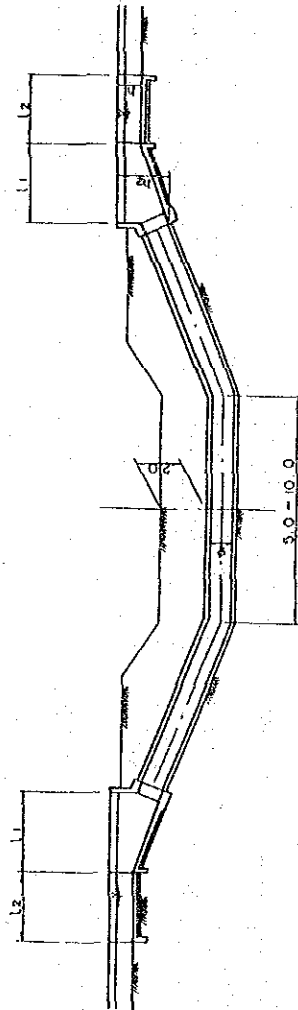


SECTION A-A

SIPHON-2



SECTION B-B

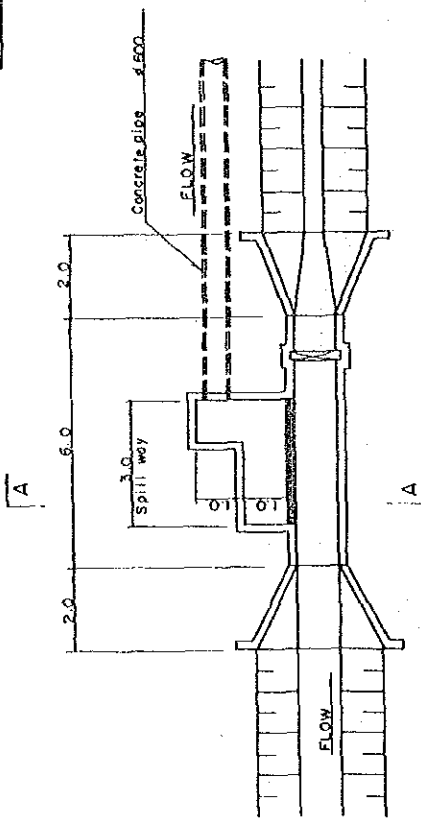


DIMENSIONS (m)

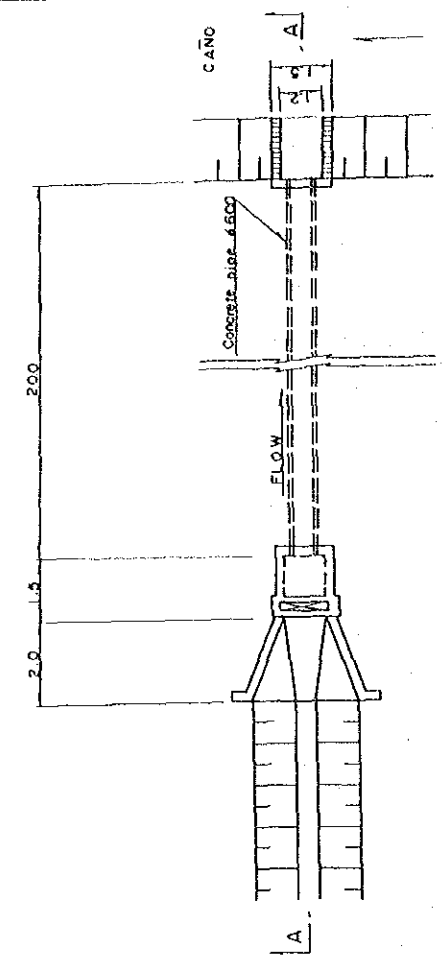
TYPE	Q (m ³ /sec)		φ mm	n ₁	n ₂	L ₁	L ₂
	max	min					
1	2.5	1.5	1200	1.5	2.8	3.5	3.0
2	1.5	1.0	1000	1.2	2.4	3.0	3.0
3	1.0	0.5	800	0.9	2.1	3.0	2.0
4	0.5	0.1	600	0.9	1.8	2.5	2.0

Fig. I-2-14 Related Structure No.3 (Siphon-2)

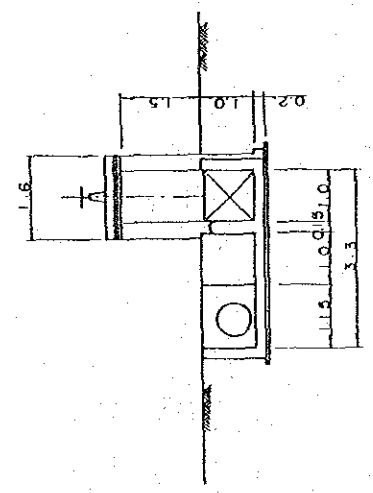
WASTE WAY - 2



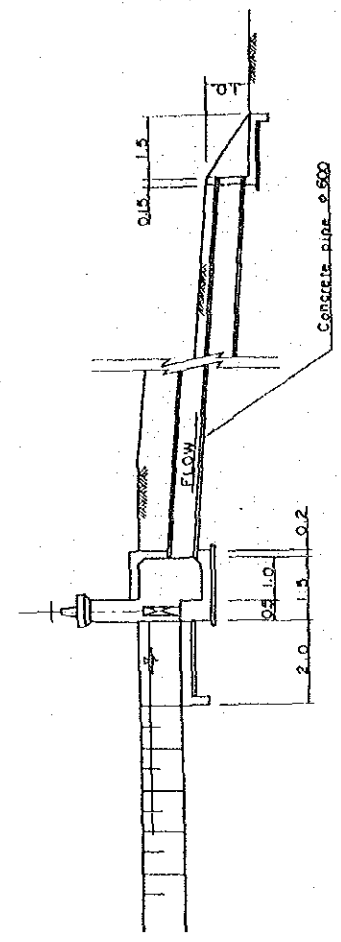
PLAN



PLAN



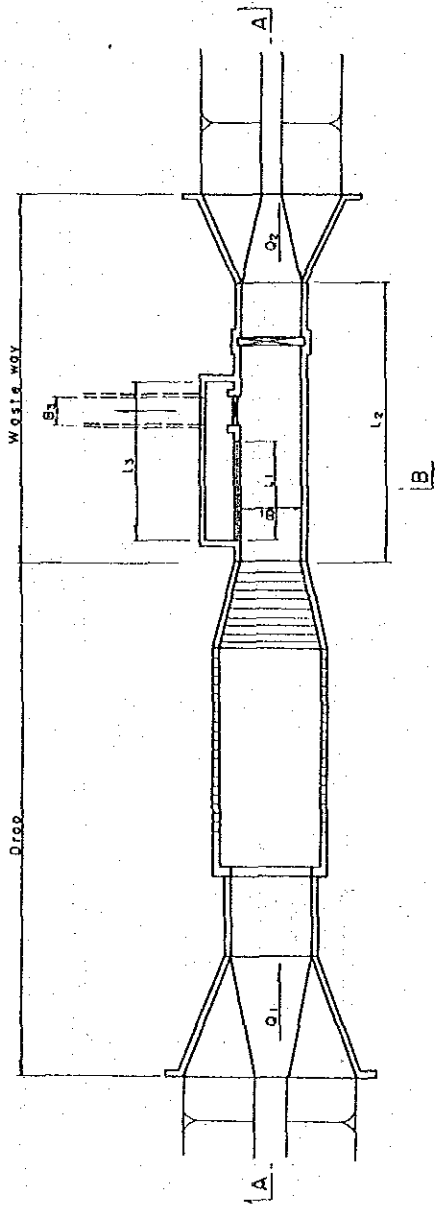
SECTION A-A



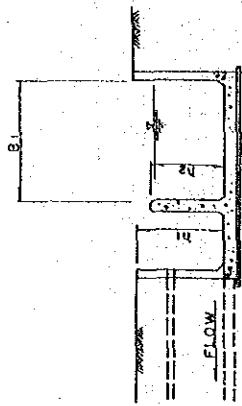
SECTION A-A

Fig. I-2-14 Related Structure No. 5 (Wasteway-2)

WASTE WAY - I



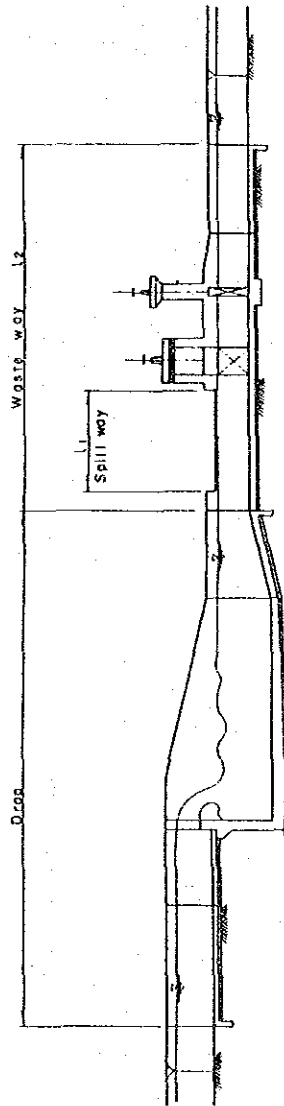
PLAN



SECTION B-B

DIMENSIONS

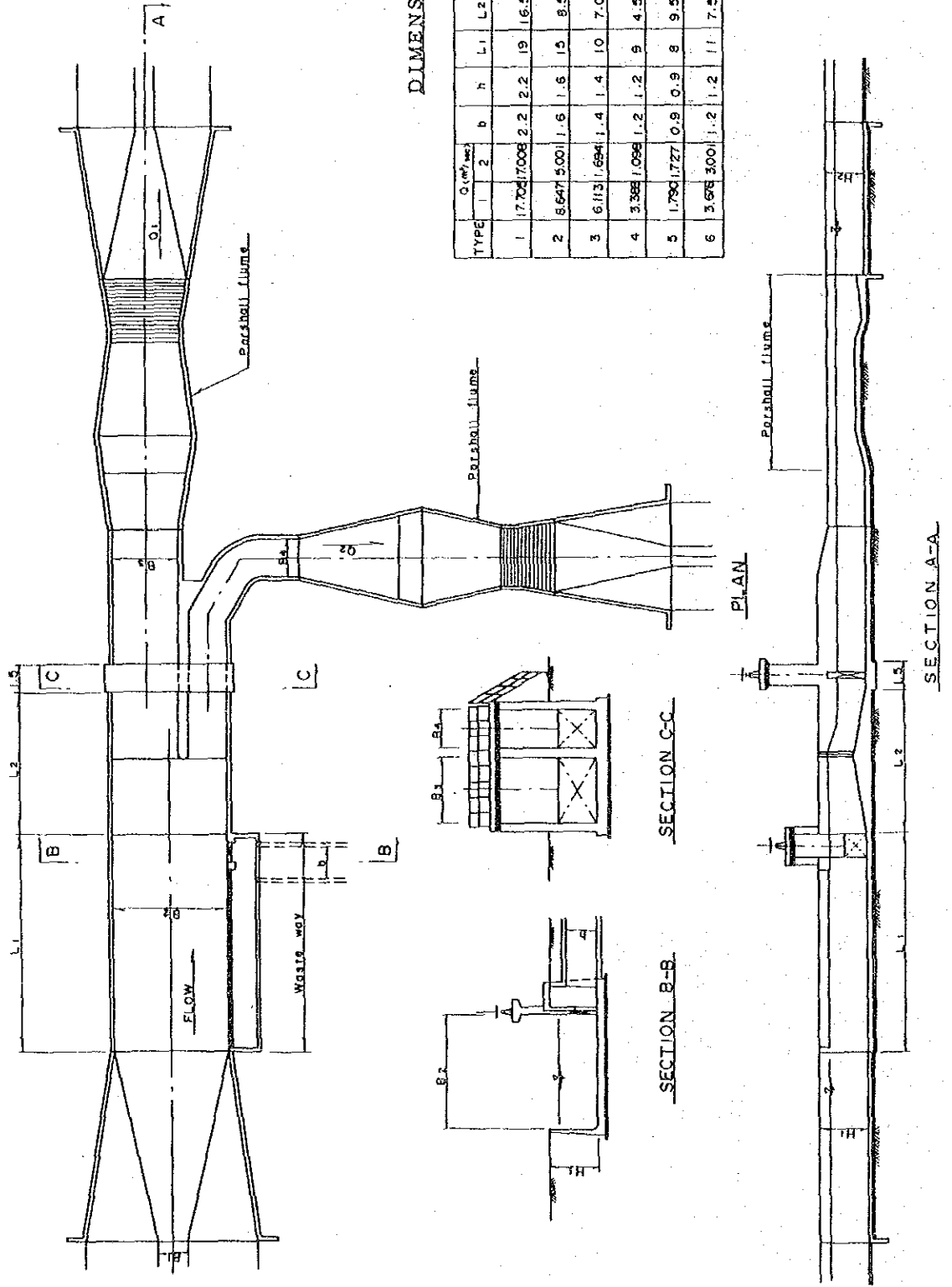
TYPE	Q ₂ (m ³ /sec)	B ₁	B ₂	h ₁	h ₂	l ₁	l ₂
1	15~18	4.5	2.0	2.7	2.25	5.0	15.0
2	12~13	3~10	3.5	2.0	2.3	1.85	7.0
3	5~7	3~6	2.5	1.5	1.7	1.35	4.0
4	3~5	2~5	2.5	1.2	1.40	3.0	8.0
5	1~3	0.5~2	1.5	1.000	1.2	0.95	3.0



SECTION A-A

Fig. I-2-14 Related Structure No.4 (Wasteway-1)

DIVISION WORKS-I (LONGITUDINAL TYPE)



DIMENSIONS.

TYPE	Q (cfs) (m ³ /sec)		b	h	L ₁	L ₂	H ₁	H ₂	B ₁	B ₂	B ₃	B ₄
	1	2										
1	17.70	17.008	2.2	2.2	19	16.5	3.7	2.7	2.5	10.4	5.0	4.9
2	8.647	5.001	1.6	1.6	15	8.5	2.5	1.5	1.5	6.0	3.5	2.0
3	6.113	1.694	1.4	1.4	10	7.0	2.0	1.7	1.0	5.3	3.0	1.8
4	3.388	1.098	1.2	1.2	9	4.5	1.5	1.9	1.0	4.4	2.4	1.5
5	1.790	1.727	0.9	0.9	8	9.5	2.0	1.3	1.0	4.1	1.8	1.8
6	3.678	3.001	1.2	1.2	11	7.5	2.1	2.0	1.0	5.2	2.4	2.5

DIVISION WORKS-2 (GATE-CONTROLLED TYPED)

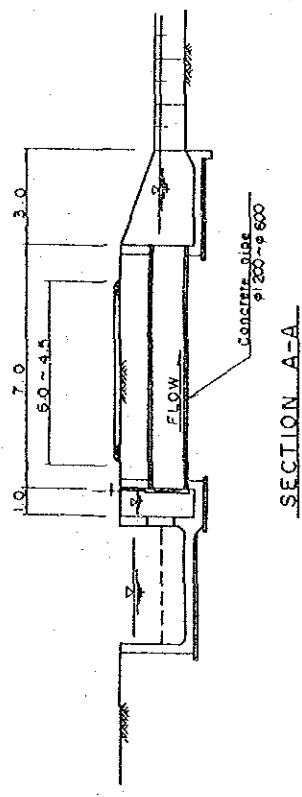
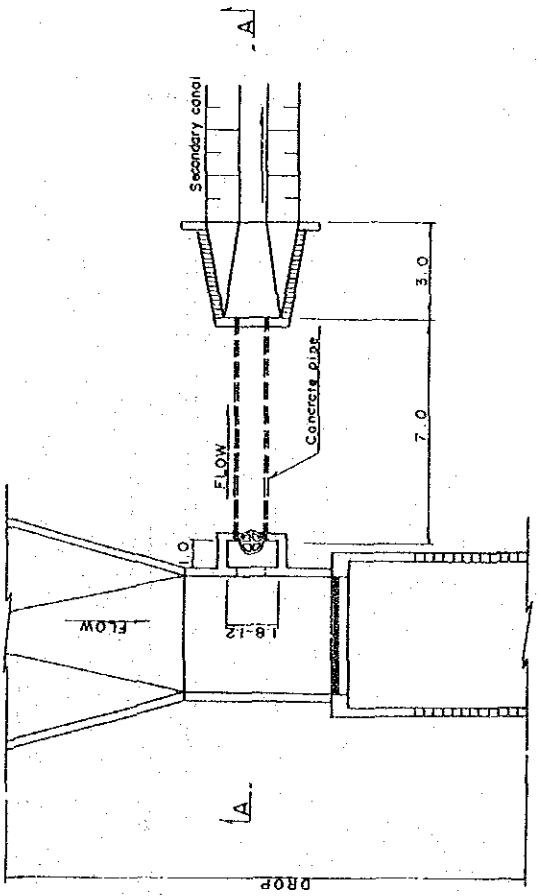
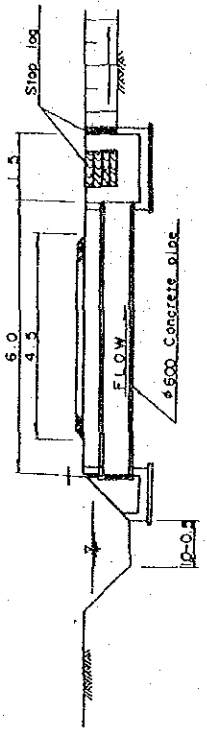
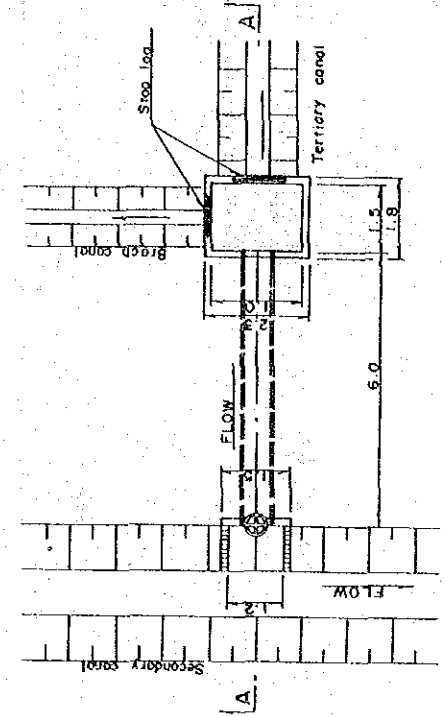
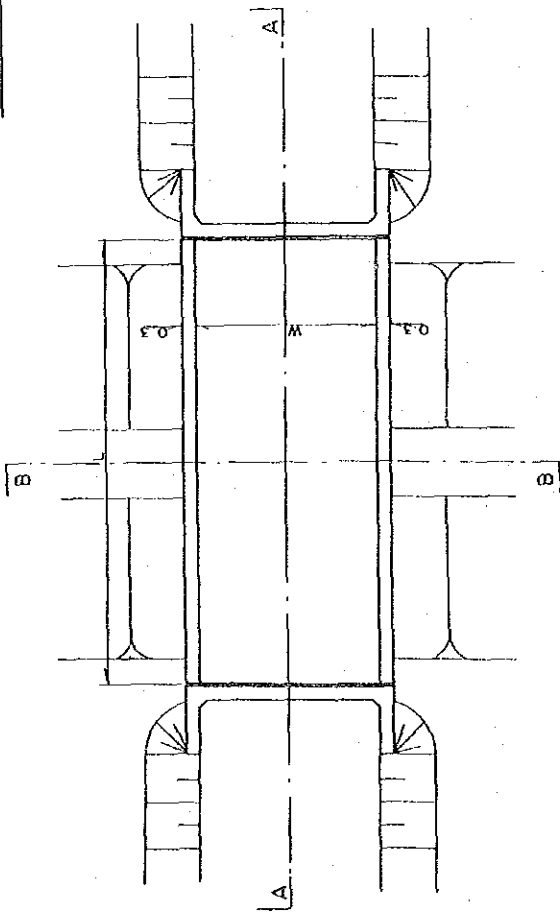
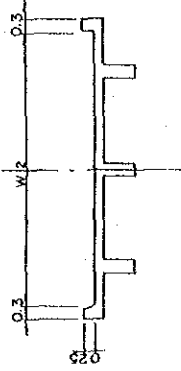
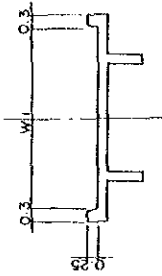


Fig. I-2-14 Related Structure No.7 (Division Works-2)

BRIDGE



PLAN



SECTION 8-B

DIMENSIONS

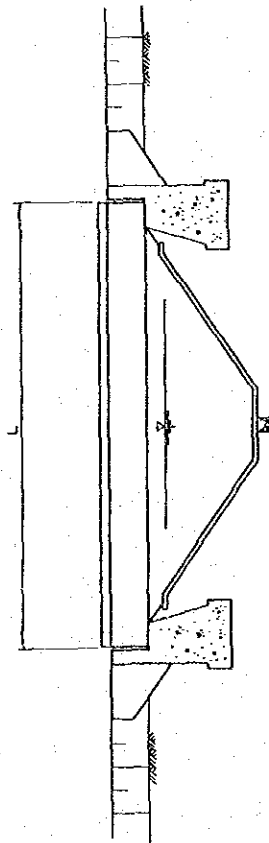
UNIT: (m)

TYPE	Q (ml/sec)		L	W	
	max	min		W1	W2
1	37	36	14.8	4.0	6.0
2	17	16	10.8	4.0	6.0
3	16	12	10.2	4.0	6.0
4	11	9	8.7	4.0	6.0
5	9	8	8.2	4.0	6.0
6	6	5	7.2	4.0	6.0
7	2	0.1	6.2	4.0	6.0

REMARK

W = 4.0 : ON-FARM ROAD

W = 6.0, 8.0 : TRUCHA



SECTION A-A

FIG. I-2-14 Related Structure No.8 (Bridges)

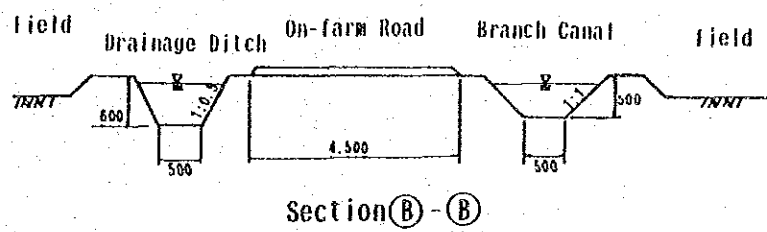
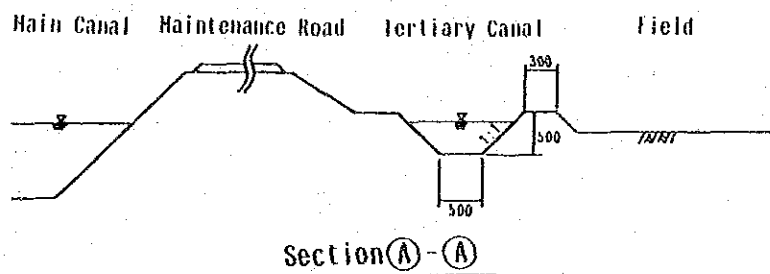
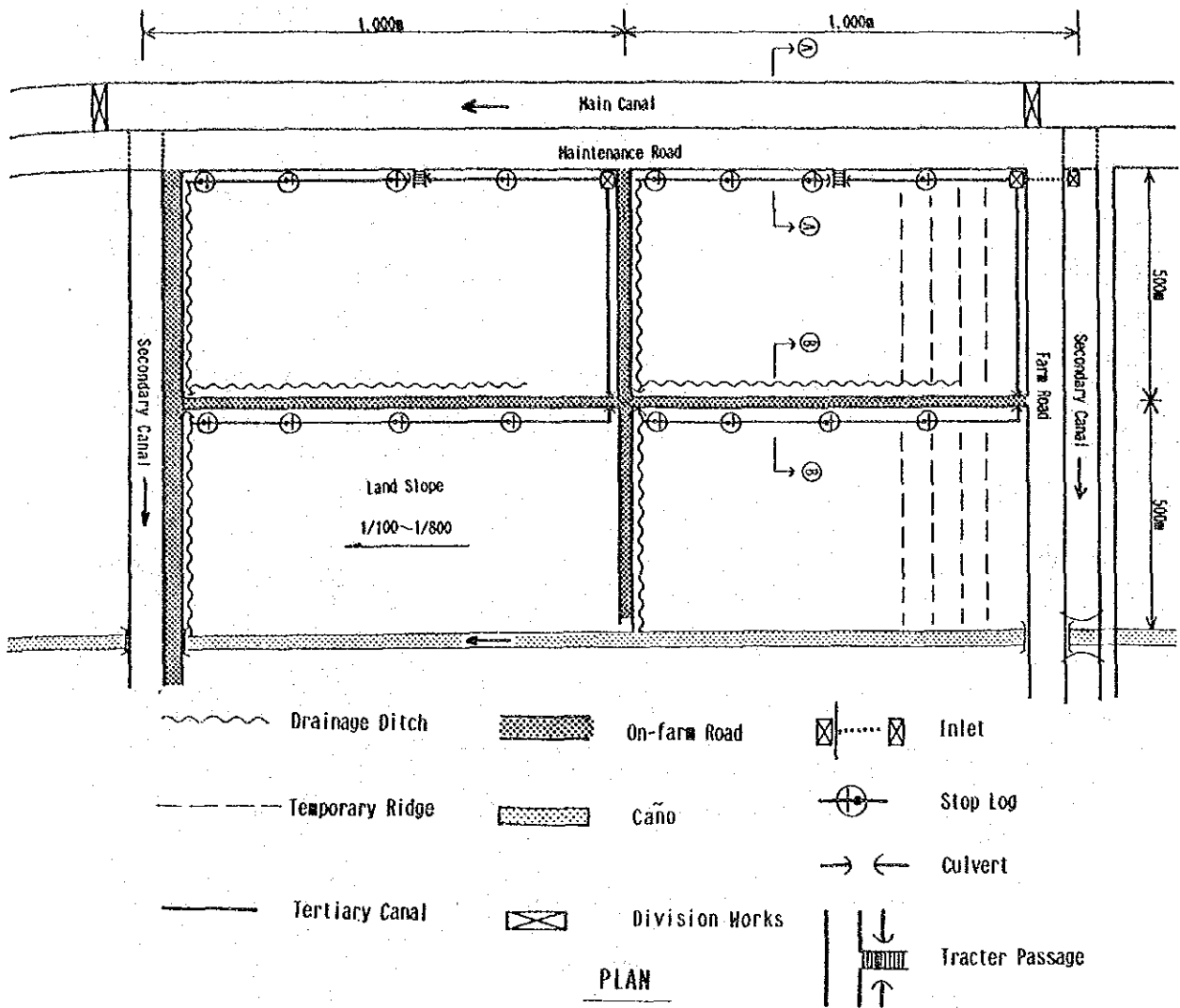


Fig. I-2-15 STANDARD FARM LOT

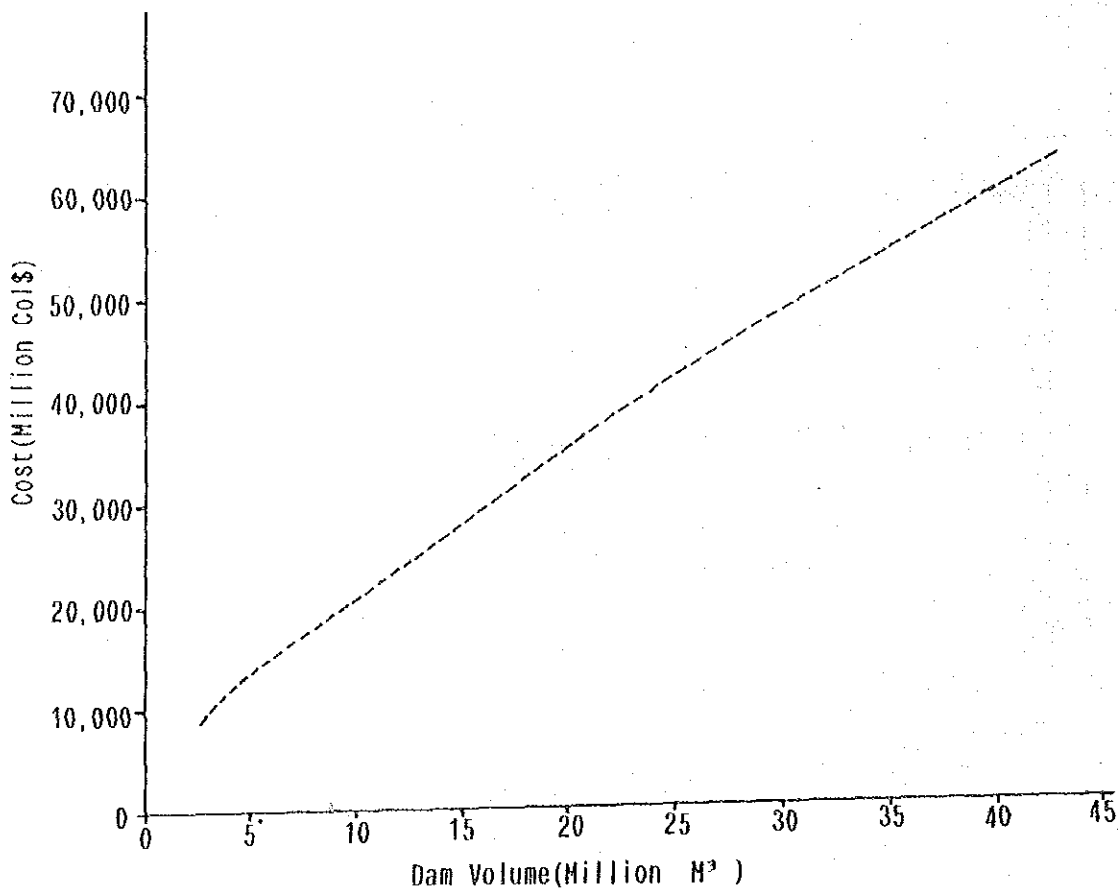


Fig. I-2-16 RELATION BETWEEN WATER STORAGE VOLUME AND COST OF DAM

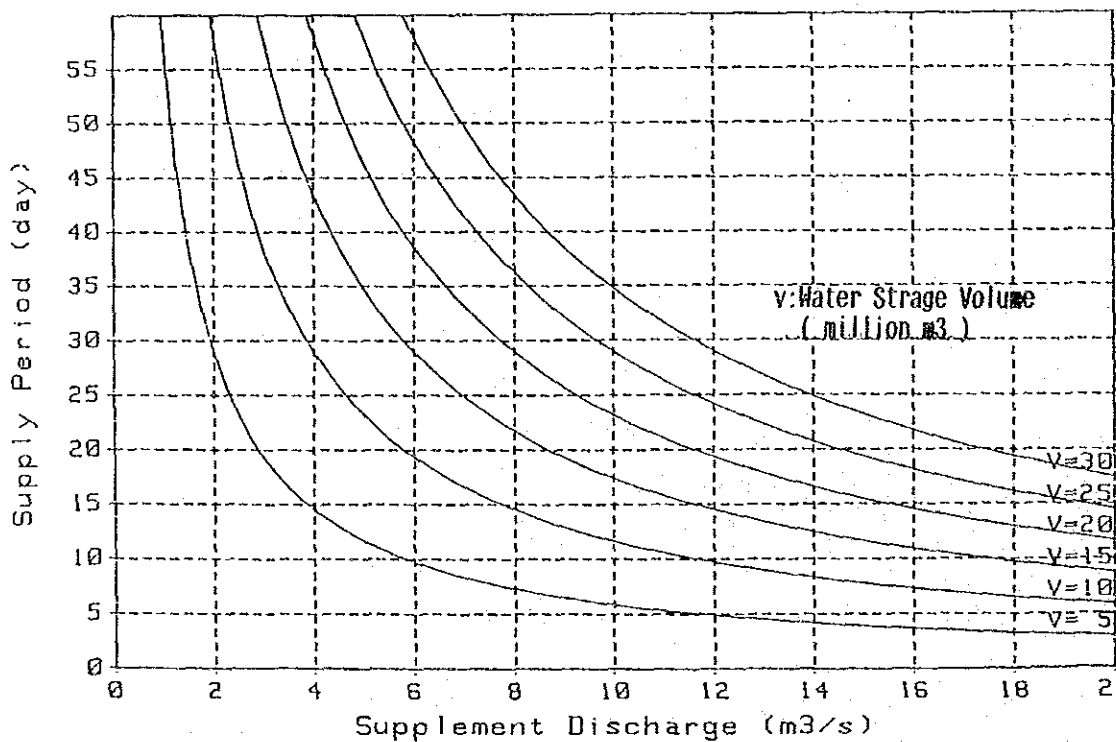


Fig. I-2-17 RELATION BETWEEN WATER STORAGE VOLUME AND WATER SUPPLY

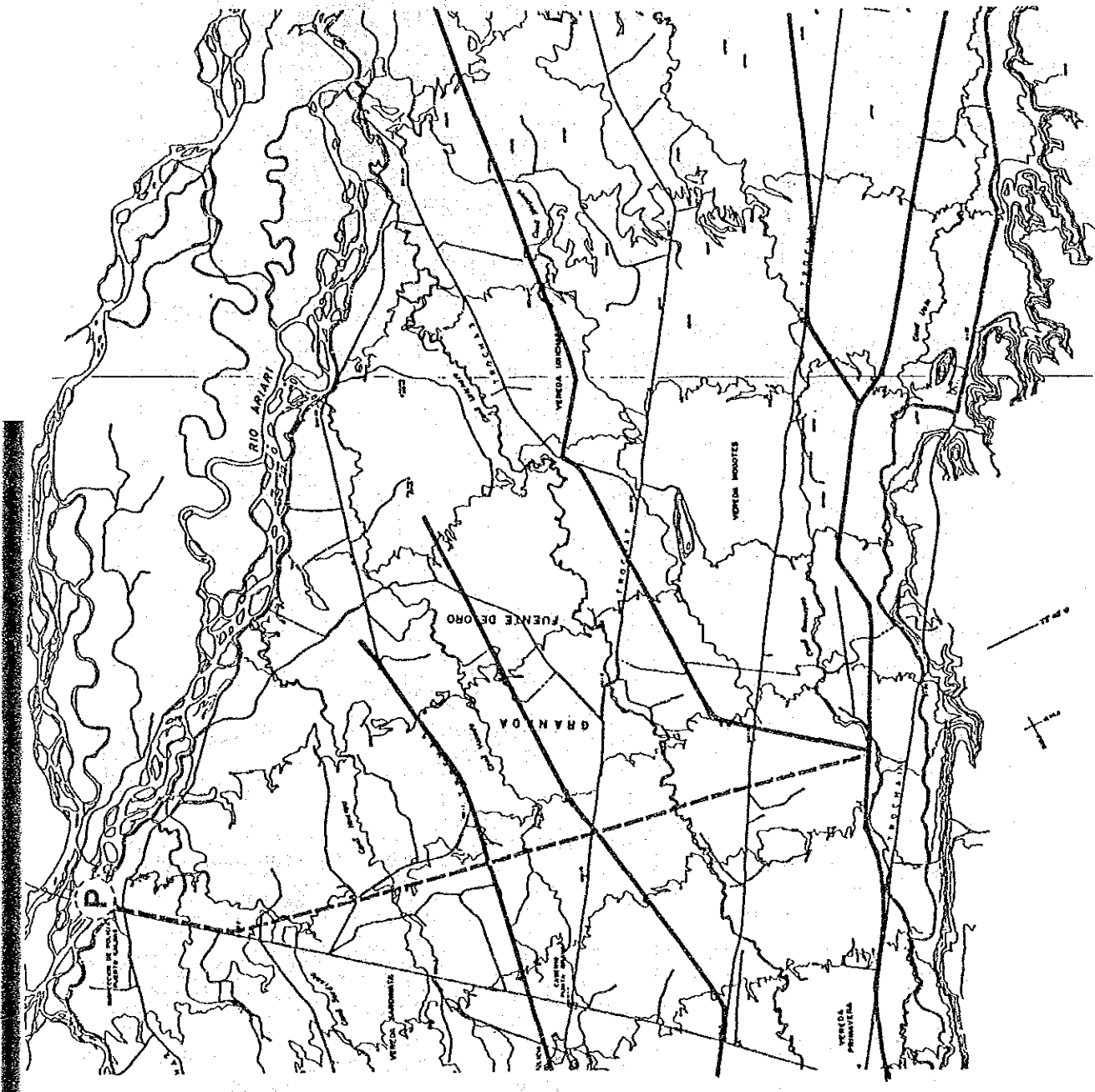
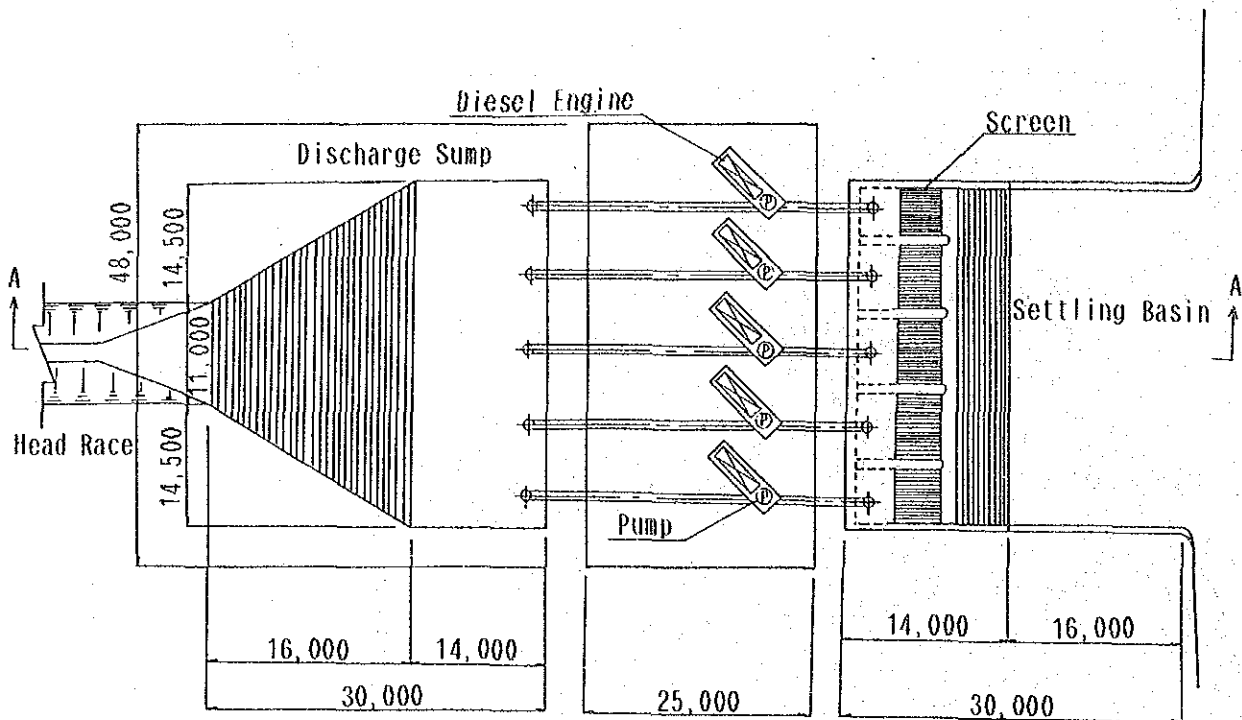
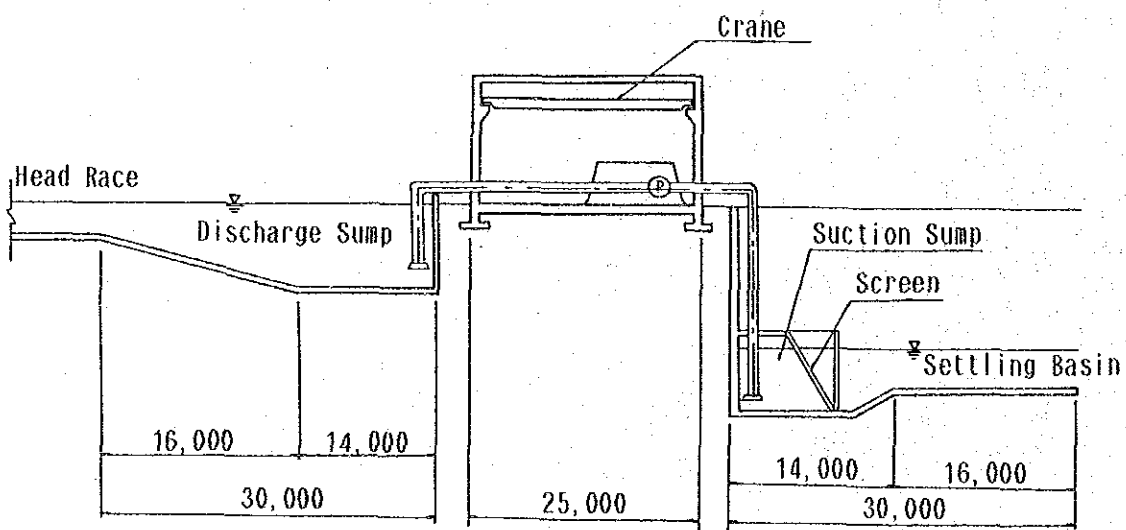


Fig. I-2-18 Preliminary Layout of Pumping System



Plan



Section A-A

Fig. I-2-19 PLAN OF PUMP STATION

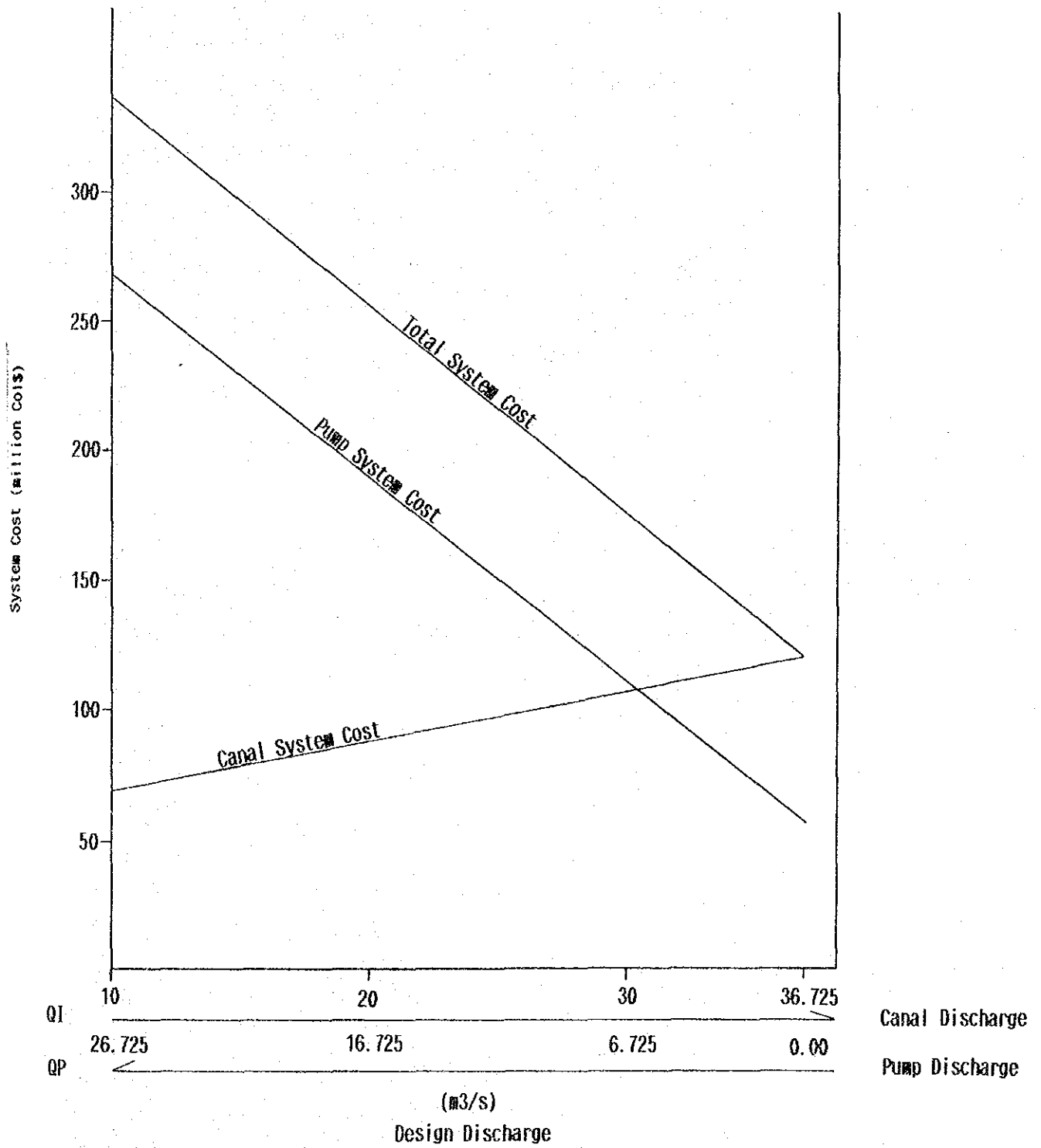
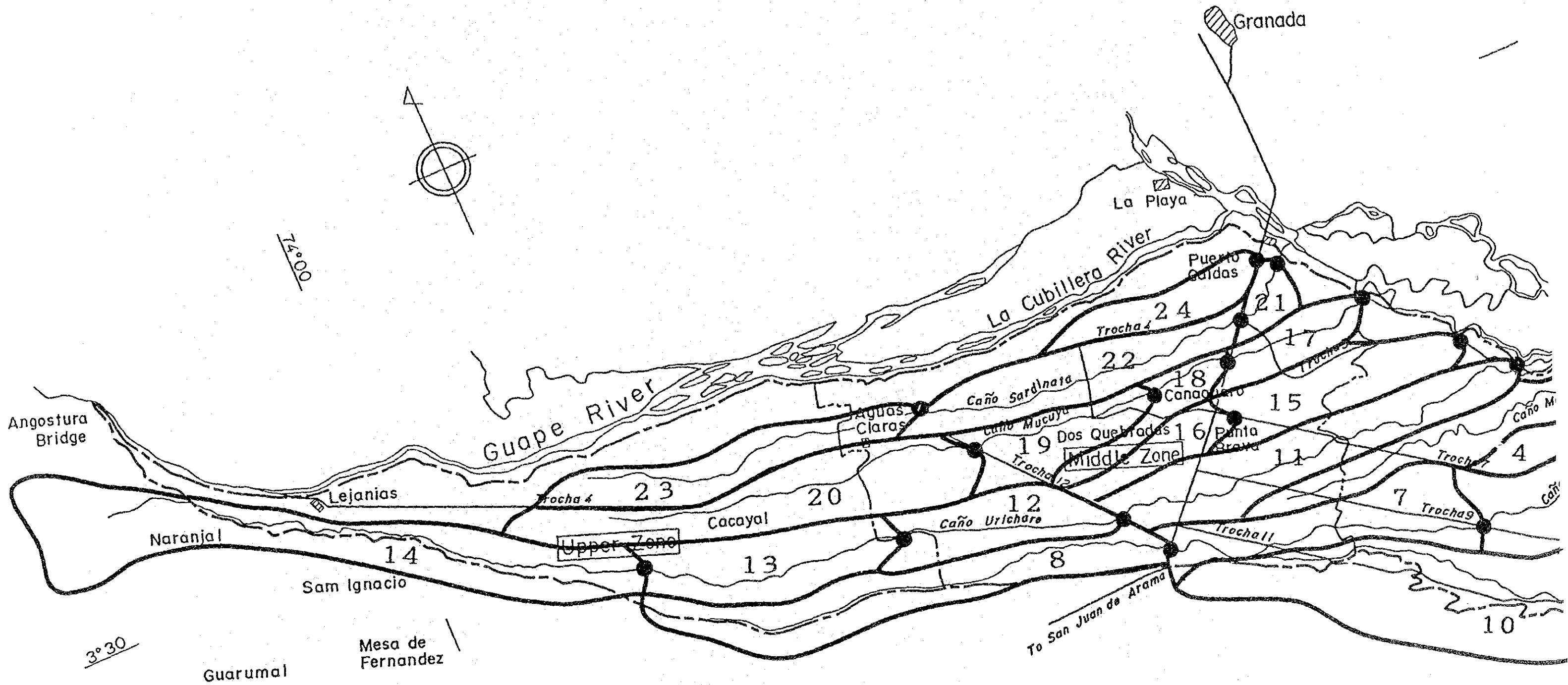
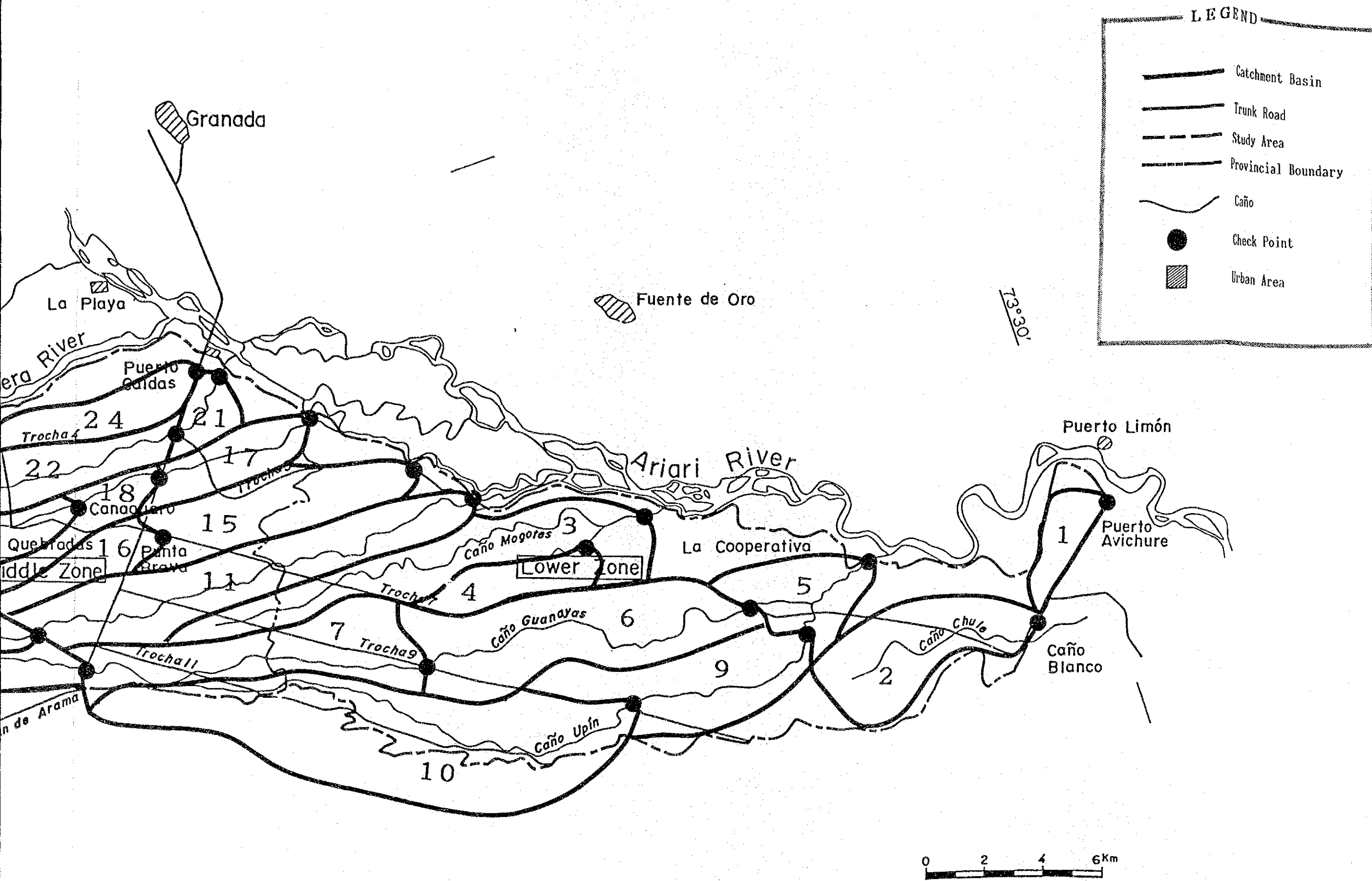


Fig. I-2-20 Relationship between System Cost and Water Distribution



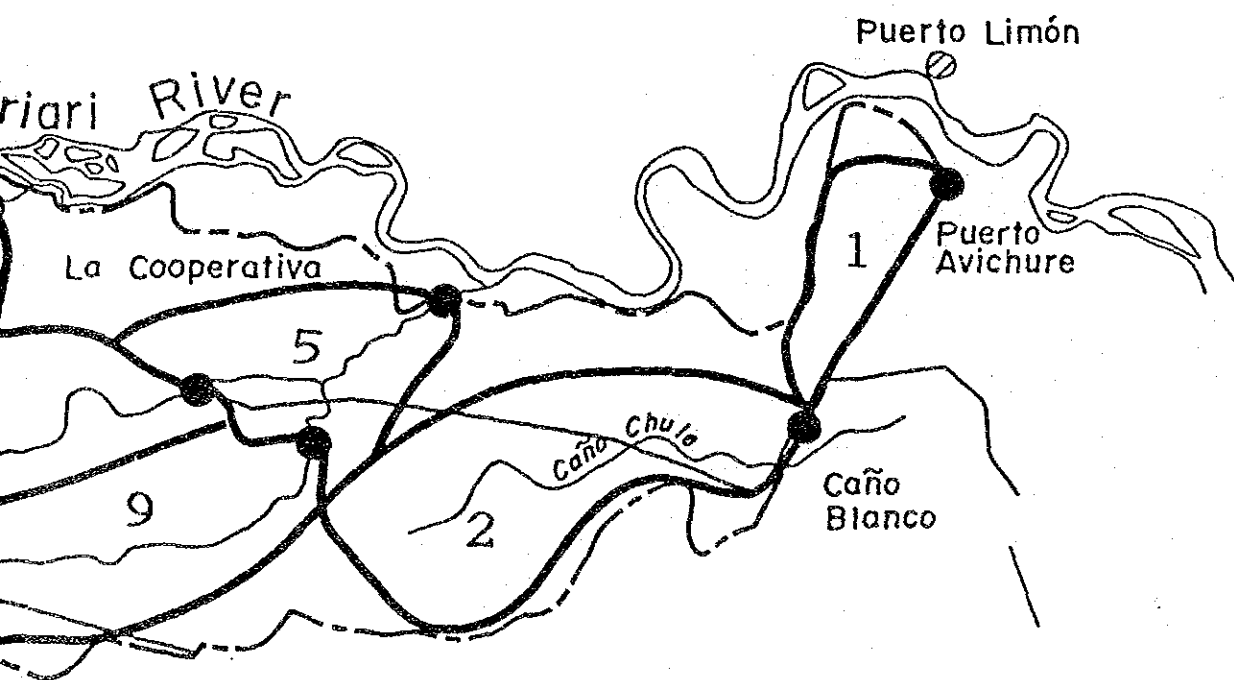
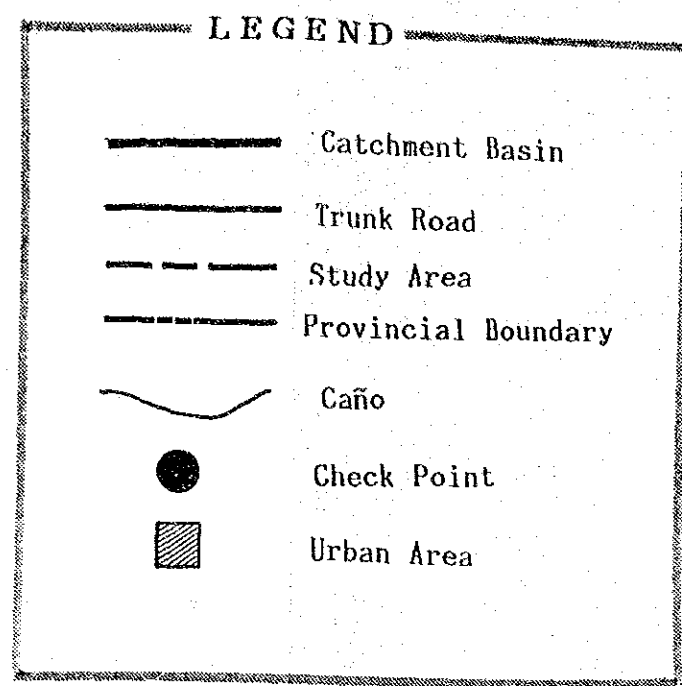


Number	Caño	Area(l)
1	Avichure	4
2	Avichure	8
3	Caño Mogotes	15
4	Caño Seco	6
5	Caño Guanayas	10
6	Caño Guanayas	20
7	Caño Guanayas	13
8	Caño Guanayas	23
9	Caño Upín	22
10	Caño Upín	50
11	Caño Urichare	23
12	Caño Urichare	16
13	Caño Urichare	9
14	Caño Urichare	34
15	Caño Venado(2)	16
16	Caño Venado(2)	10
17	Caño Mucuya	4
18	Caño Mucuya	18
19	Caño Mucuya	11
20	Caño Mucuya	15
21	Caño Sardinata	2
22	Caño Sardinata	25
23	Caño Sardinata	11
24	Caño Taparo	13

Fig. I-3-1 Drainage System in the Study Area

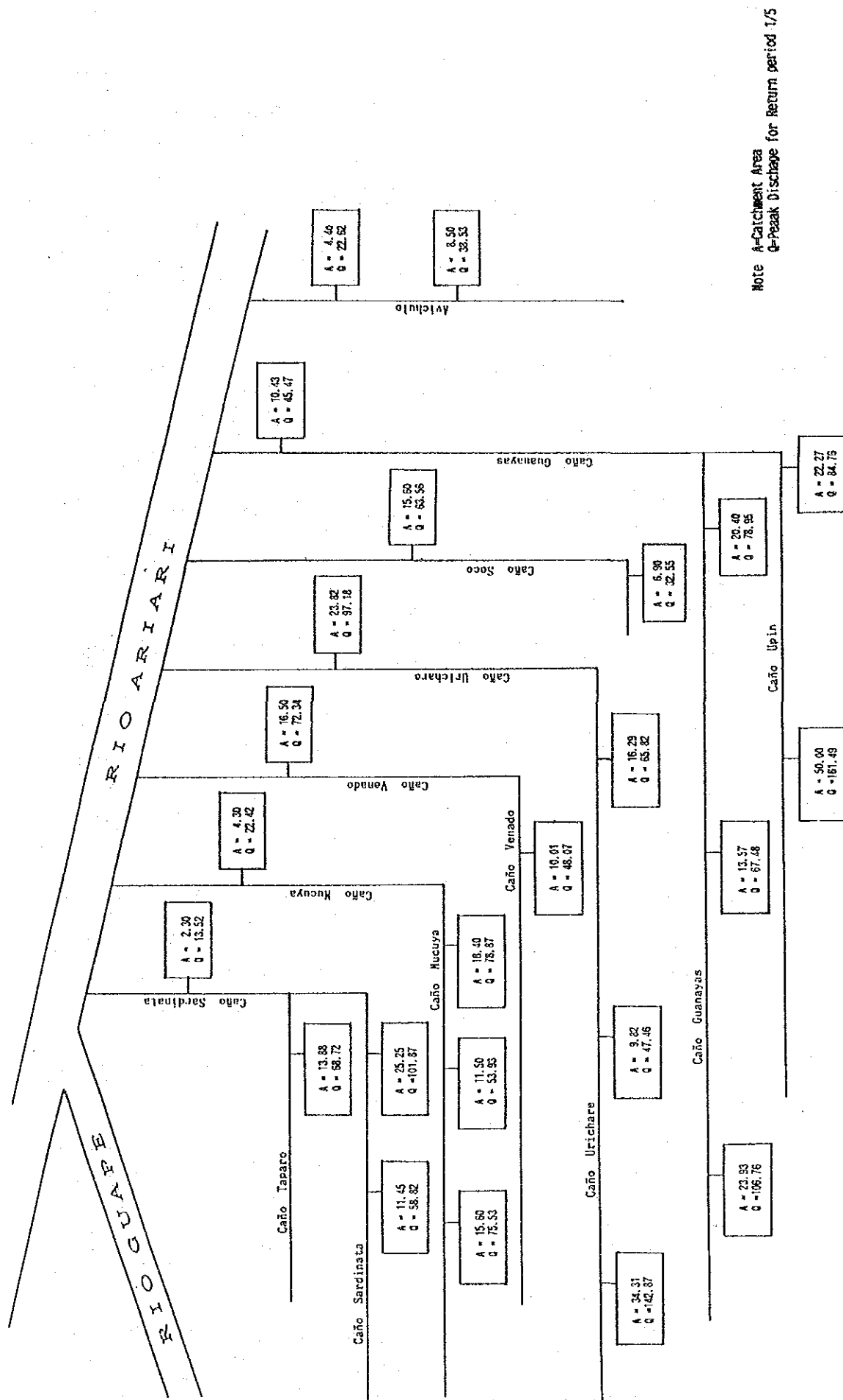
ente de Oro

13°30'



Number	Caño	Area(km2)
1	Avichure	4.40
2	Avichure	8.50
3	Caño Hogotes	15.60
4	Caño Seco	6.90
5	Caño Guanayas	10.43
6	Caño Guanayas	20.40
7	Caño Guanayas	13.57
8	Caño Guanayas	23.93
9	Caño Upín	22.27
10	Caño Upín	50.00
11	Caño Urichare	23.82
12	Caño Urichare	16.29
13	Caño Urichare	9.82
14	Caño Urichare	34.31
15	Caño Venado(2)	16.50
16	Caño Venado(2)	10.01
17	Caño Mucuya	4.30
18	Caño Mucuya	18.40
19	Caño Mucuya	11.50
20	Caño Mucuya	15.60
21	Caño Sardinata	2.30
22	Caño Sardinata	25.25
23	Caño Sardinata	11.45
24	Caño Taparo	13.88

Fig. I-3-1 Drainage System in the Study Area



Note A=Catchment Area
Q=Peak Discharge for Return period 1/5

Fig. I-3-2 Drainage System and Runoff Peak Discharge