

1.2 Minutes (Explanation of Basic Design Draft Report)

MINUTES OF DISCUSSION

OF

THE BASIC DESIGN STUDY

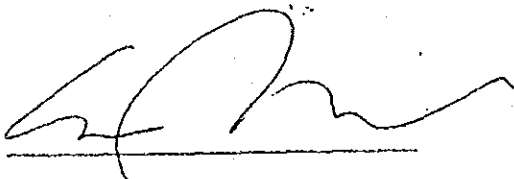
ON

THE PROJECT FOR CONSTRUCTING THE BUS TERMINAL IN KATHMANDU,  
THE KINGDOM OF NEPAL

In response to the request of His Majesty's Government of Nepal for Grant Aid for the Project for Constructing the Bus Terminal in Kathmandu (hereinafter referred to as "the Project"), the Government of Japan decided to conduct a Basic Design Study on the Project and entrusted the study to the Japan International Cooperation Agency (JICA). JICA sent the Basic Design Study Team headed by Mr. Hiroomi MOTOZAKI, Special Assistant to the Director of the Division, Transport Promotion Division, Regional Transport Bureau, Ministry of Transport, to the Kingdom of Nepal from 30 January to 23 February, 1989.

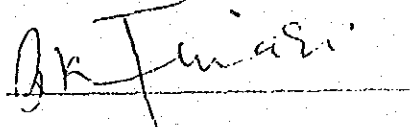
As a result of the study, JICA prepared a draft final report and dispatched a draft final report explanation team headed by Mr. Satoshi MACHIDA, Deputy Director, Second Basic Design Study Division, Grant Aid Planning and Survey Department, JICA to explain and discuss it from July 16 to July 23, 1989.

Both parties had a series of discussions on the report and have agreed to recommend to their respective Governments that the major points of understandings reached between them, attached herewith, should be examined towards the realization of the Project.



Mr. Satoshi MACHIDA  
Leader,  
Basic Design Study Team  
JICA

Kathmandu, July 21, 1989



R. K. TIWARI  
Joint Secretary  
Ministry of Panchayat  
and Local Development

A T T A C H M E N T

1. The Nepal side has principally agreed to the basic design proposed in the Draft Final Report.
2. The Nepal side has understood Japanese grant aid system and confirmed that the necessary measures will be taken by the Nepal side as shown in Annex- I, which is in line with the Annex- III of THE MINUTES OF DISCUSSIONS on the Project signed on 13 February 1989, on condition that the grant aid by the Government of Japan would be extended to the Project.
3. The Nepal side stated that necessary budget will be provided for the Project to ensure the effective operation and maintenance of the Project constructed under the grant aid.
4. Ten copies of the Final Report in English will be submitted to the Nepal side through JICA by the end of August 1989.
5. In connection with the Annex- I, item 1, the Nepal side stated that there would be difficulty for the Nepal side to conduct reclamation of the proposed site and requested the team to include the reclamation in the scope of Japanese grant aid.

The team understood the request and promised to convey it to the Japanese Government for further consultation.

6. The Nepal side explained that it was preparing legal measures directing long and middle distance buses to depart from and arrive to the proposed terminal only, as well as managing organization of the terminal for implementation of the Project.

The Nepal side also stated the content of planned legal measures and managing body would be informed to the Japanese Government when those plans were formulated.

A N N E X - I

The necessary measures to be taken by His Majesty's Government of Nepal are as follows.

1. To clear, level and reclaim the site in accordance with basic specification provided by the Basic Design Study Team prior to commencement of the construction.
2. To provide facilities for distribution of electricity, water supply, drainage, telephone system and other incidental facilities to the site.
3. To provide data and information necessary for the Project.
4. To take any legal measures to direct long and middle distance buses to depart from and arrive to the proposed terminal only.
5. To clarify the type of management of the terminal and/or any part of the terminal.  
( Direct management, consignment, rental, etc. )
6. To secure the connection bus services from the new terminal to the existing terminal and also to the other final destination of the passenger.
7. To bear two kinds of commissions to the Japanese foreign exchange bank for the banking services, based upon the "Banking Arrangement", namely, the advising commission of the "Authorization to Pay" and payment commission.
8. To ensure prompt unloading, tax exemption and customs clearance at the port of disembarkation in the Kingdom of Nepal and prompt internal transportation therein of the products purchased under the Grant.

9. To accord Japanese nationals whose services may be required in connection with the supply of the products and the services under the verified <sup>W/R</sup> contract such facilities as may be necessary for their entry into the Kingdom of Nepal and stay therein for the performance of their work. (S)
10. To exempt Japanese nationals engaged in the Project from custom duties, internal taxes and other fiscal levies which may be imposed in the Kingdom of Nepal with respect to the supply of the products and services under the verified contracts.
11. To provide and/or acquire necessary permissions, licenses and other authorizations necessary for carrying out the Project.
12. To bear all the expenses, other than those to be borne by the Grant, such as gardening, fencing, gates, exterior lighting etc..

RF

(S)

### 1.3 Members of Basic Design Study Team

#### 1) Basic Design Survey

| Assignment                 | Name             | Position  |
|----------------------------|------------------|---|
| Team Leader                | Hiroomi MOTOZAKI | Special Assistant to the Director of the Division, Transport Promotion Division, Regional Transport Bureau, MINISTRY OF TRANSPORT |
| Project Coordinator        | Ryoji YAGINUMA   | Planning Division, Grant Aid Planning and Survey Department, JAPAN INTERNATIONAL COOPERATION AGENCY                               |
| Architectural Planner      | Kenjiro HIROSE   | AZUSA SEKKEI CO., LTD.  |
| Architectural Designer     | Chuichi YAMAKAWA | AZUSA SEKKEI CO., LTD.  |
| Civil Engineering Designer | Shiro MATSUNO    | AZUSA SEKKEI CO., LTD.  |
| Operation Planner          | Akio MORIKAWA    | AZUSA SEKKEI CO., LTD.  |
| Equipment Planner          | Kozo ISHIZAKA    | AZUSA SEKKEI CO., LTD.  |
| Facilities Designer        | Wataru SHIROKAWA | AZUSA SEKKEI CO., LTD.  |

2) Explanation of Basic Design Draft Report

| Assignment                | Name             | Position  |
|---------------------------|------------------|---|
| Team Leader               | Satoshi MACHIDA  | Deputy Director<br>Second Basic Design Study<br>Division, Grant Aid<br>Planning & Survey<br>Department<br>JAPAN INTERNATIONAL<br>COOPERATION AGENCY |
| Architectural<br>Planner  | Kenjiro HIROSE   | AZUSA SEKKEI CO., LTD.  |
| Architectural<br>Designer | Chuichi YAMAKAWA | AZUSA SEKKEI CO., LTD.  |
| Operation<br>Planner      | Akio MORIKAWA    | AZUSA SEKKEI CO., LTD.  |

#### 1.4 Itineraries of Basic Design Study Team

##### 1) Basic Design Survey

| Date                     | Members            | Activities  | Place     |
|--------------------------|--------------------|---|-----------|
| January<br>29, Sunday    | Hirose<br>Morikawa | . Leave Tokyo by TG 641   | Bangkok   |
| 30, Monday               | Hirose<br>Morikawa | . Arrive in Nepal by TG 311<br>. Courtesy visit to JICA Office<br>. Explanation of Survey<br>Schedule and Contents  | Kathmandu |
| 31, Tuesday              | Hirose<br>Morikawa | (1) Visit Saja Yatayat Repair<br>Shop<br>(2) Courtesy visit to Japanese<br>Embassy<br>(3) Courtesy visit to MPLD<br>Submit questionnaire<br>(4) Tender call for Soil<br>Investigation   |           |
| February<br>1, Wednesday | Hirose<br>Morikawa | (1) Conference at MPLD<br>(2) Conference at KNP<br>(3) Contract for Soil<br>Investigation   |           |
| 2, Thursday              | Hirose<br>Morikawa | (1) Visit proposed sites<br>(No.5, No.8, No.9)<br>(2) Conference at KNP<br>(3) Traffic Survey at Existing<br>Bus Terminal   |           |
| 3, Friday                | Hirose<br>Morikawa | (1) Traffic Survey at Existing<br>Bus Terminal<br>(2) Attend the commencement of<br>soil investigation work<br>(3) Schedule arrangement at<br>JICA office<br>(4) Conference at KNP<br>Receive lay-out drawing of<br>Existing Bus Terminal |           |

| Date                                       | Members  | Activities  | Place     |
|--|--|---|-----------|
| February<br>4, Saturday<br>(Local holiday) | Hirose<br>Morikawa   | (1) Check survey results  |           |
| 5, Sunday                                  | Hirose<br>Morikawa<br><br>Motozaki<br>Yaginuma<br>Yamakawa<br>Shirokawa<br>Matsuno | (1) Attend the commencement of<br>topographical survey<br>(2) Conference at KNP<br><br>. Leave Tokyo by TG 641  | Bangkok   |
| 6, Monday                                  | Hirose<br>Morikawa<br><br>Motozaki<br>Yaginuma<br>Yamakawa<br>Shirokawa<br>Matsuno | (1) Meeting at KNP<br>* Stop soil investigation<br>work due to obstruction<br>by land owners<br><br>. Arrive in Nepal by TG 311   | Kathmandu |
| 7, Tuesday                                 | Motozaki<br>Yaginuma<br>Yamakawa<br>Shirokawa<br>Matsuno<br>Hirose<br>Morikawa     | (1) Courtesy visit to Japanese<br>Embassy, JICA office and<br>MPLD<br>(2) Verbal interim report to<br>JICA office<br>(3) Visit proposed sites<br>(No.5, No.8, No.9)<br>(4) Complete the boring work<br>at site No.8   |           |
| 8, Wednesday                               | Motozaki<br>Yaginuma<br>Hirose<br>Morikawa<br>Matsuno<br><br>Yamakawa<br>Shirokawa | (1) Check the draft of Minutes<br>of Discussion at JICA<br>office<br>(2) Site Survey<br>(3) Prepare report on site<br>selection<br><br>(1) Prepare a list of facilities<br><br>(1) Team meeting<br>Study appropriate size of<br>the terminal based on<br>traffic survey results |           |



| Date                                | Members  | Activities  | Place     |
|-------------------------------------|--|---|-----------|
| February<br>9, Thursday             | Motozaki<br>Yaginuma<br>Hirose<br>Morikawa<br>Yamakawa<br>Shirokawa<br><br>Matsuno             | (1) Conference at MPLD on draft<br>of Minutes of Discussion<br>(2) Courtesy visit to Ministry<br>of Finance<br><br>(1) Survey of No.8 Site  |           |
| 10, Friday<br>(National<br>holiday) | Motozaki<br>Yaginuma<br>Hirose<br>Morikawa<br>Yamakawa<br>Matsuno<br><br>Ishizaka              | (1) Reconnaissance survey on<br>ring road<br>(2) Survey on existing bus<br>terminal<br><br>. Leave Tokyo by TG-641  | Bangkok   |
| 11, Saturday<br>(Local<br>holiday)  | Motozaki<br>Yaginuma<br>Hirose<br>Morikawa<br>Yamakawa<br>Shirokawa<br>Matsuno<br><br>Ishizaka | (1) Reconnaissance survey on<br>city road<br>(2) Team meeting<br>(3) Data arrangement<br><br>. Arrive in Nepal by TG 331<br>(1) Join team meeting   | Kathmandu |
| 12, Sunday                          | Motozaki<br>Yaginuma<br>Hirose<br>Morikawa<br>Yamakawa<br>Shirokawa<br>Matsuno<br>Ishizaka     | (1) Explanatory meeting with<br>related organizations<br>and discussion on draft<br>of Minutes of Discussion<br>at MLPD<br>(2) Reconnaissance survey on<br>proposed sites<br>(3) Courtesy visit to Ministry of<br>Housing and Physical Planning |           |

| Date                   | Members   | Activities   | Place   |
|------------------------|---|--|---------|
| February<br>13, Monday | Motozaki<br>Yaginuma<br>Hirose<br>Morikawa<br>Yamakawa<br>Shirokawa<br>Matsuno<br>Ishizaka<br><br>Matsuno   | (1) Discussion on the Minutes draft at JICA office<br>(2) Sign on Minutes of Discussion<br>* Two sites were proposed in the Minutes<br><br>(1) Reconnaissance survey on the new site<br>(2) Data arrangement |         |
| 14, Tuesday            | Hirose<br>Morikawa<br>Ishizaka<br>Yamakawa<br>Shirokawa<br>Matsuno<br><br>Motozaki<br>Yaginuma  | (1) Team meeting<br>(2) Conference on the new site at KNP.<br><br>(1) Courtesy visit to Japanese Embassy<br>. Left Nepal by TG 312   | Bangkok |
| 15, Wednesday          | Hirose<br>Morikawa<br>Ishizaka<br>Yamakawa<br>Shirokawa<br>Matsuno<br><br>Hirose<br>Shirokawa<br>Ishizaka<br>Yamakawa<br><br>Hirose<br>Shirokawa<br>Matsuno<br><br>Motozaki<br>Yaginuma | (1) Conference on Soil Investigation for the new site at KNP<br><br>(1) Survey on private engine workshop<br>(2) Visit to Shaja Yatayat<br><br>(1) Survey on the new site<br><br>. Arrive in Tokyo by TG 740 |         |

| Date                                | Members   | Activities  | Place |
|-------------------------------------|---|---|-------|
| February<br>16, Thursday            | <p>Hirose<br/>Morikawa<br/>Ishizaka<br/>Yamakawa<br/>Shirokawa<br/>Matsuno</p> <p>Hirose<br/>Shirokawa<br/>Ishizaka</p> | <p>(1) Conference at NTEA<br/>* Confirmation of organization</p> <p>(2) Data arrangement</p> <p>(3) Cost survey</p> <p>(1) Visit to NEA, survey on power supply</p> <p>(2) Survey on private engine workshops and city bus terminals</p>  |       |
| 17, Friday                          | <p>Hirose<br/>Morikawa<br/>Ishizaka<br/>Yamakawa<br/>Shirokawa<br/>Matsuno</p> <p>Hirose<br/>Shirokawa<br/>Ishizaka</p> | <p>(1) Survey on similar facilities<br/>* New Airport Passenger Terminal<br/>* National Tuberculosis Center</p> <p>(2) Team meeting</p> <p>(3) Conference at KNP<br/>* On area and shape of the site</p> <p>(4) Cost survey</p> <p>(1) Visit Water Supply and Sewerage Corporation<br/>Survey on water supply and sewerage</p> <p>(2) Survey on bus maintenance at TATA agent</p> <p>(3) Survey on private bus maintenance shop</p> |       |
| 18, Saturday<br><br>(Local holiday) | <p>Hirose<br/>Morikawa<br/>Ishizaka<br/>Yamakawa<br/>Shirokawa<br/>Matsuno</p>  | <p>(1) Team meeting</p> <p>(2) Data arrangement</p> <p>(3) Study on basic plan and conceptional drawing</p>   |       |

| Date                   | Members  | Activities   | Place   |
|------------------------|--|--|---------|
| February<br>19, Sunday | Hirose<br>Morikawa<br>Yamakawa<br>Matsuno<br><br>Shirokawa<br>Ishizaka | (1) Visit to and study at<br>Department of Road<br>(2) Visit to and study at<br>Bagmati Regional office<br>(3) Data arrangement<br><br>(1) Visit to and study at<br>Nepal Telecommunication<br>Corporation<br>(2) Survey on tyre renewal shops   |         |
| 20, Monday             | Hirose<br>Morikawa<br>Ishizaka<br>Yamakawa<br>Shirokawa<br>Matsuno     | (1) Verbal interim report to<br>JICA office<br>(2) Conference at NTEA<br>(3) Team meeting<br>(4) Data arrangement<br>(5) Traffic survey at the exist-<br>ing bus terminal  |         |
| 21, Tuesday            | Hirose<br>Morikawa<br>Ishizaka<br>Yamakawa<br>Shirokawa<br>Matsuno     | (1) Conference at KNP<br>(2) Study on organization<br>of the new bus terminal<br>(3) Data arrangement<br>(4) Prepare conceptional drawing  |         |
| 22, Wednesday          | Hirose<br>Morikawa<br>Ishizaka<br>Yamakawa<br>Shirokawa<br>Matsuno     | (1) Conference at MPLD<br>(2) Team meeting<br>(3) Data arrangement<br>(4) Prepare conceptional drawing<br>(5) Prepare draft of organization<br>chart for the new bus terminal  |         |
| 23, Thursday           | Hirose<br>Morikawa<br>Ishizaka<br>Yamakawa<br>Shirokawa<br>Matsuno     | (1) Courtesy visit to Japanese<br>Embassy and JICA office<br>(2) Conference at MPLD<br>* Submit a conceptional plan<br>* Submit comments on Topo-<br>graphy and Subsoil of<br>New Plant Site<br>* Submit a draft schedule<br>* Receive a copy of the<br>letter re: final decision<br>on proposed site<br><br>. Leave Nepal by TG 312 | Bangkok |

| Date                   | Members  | Activities                  | Place |
|------------------------|--|-----------------------------|-------|
| February<br>24, Friday | Hirose<br>Morikawa<br>Ishizaka<br>Yamakawa<br>Shirokawa<br>Matsuno | . Arrive in Tokyo by TG 740 |       |

2) Explanation of Basic Design Draft Report

| Date                                 | Activities  | Place     |
|--------------------------------------|---|-----------|
| July<br>16, Sunday                   | . Leave Tokyo by CX-509<br>Arrive in Bangkok by CX-2705   | Bangkok   |
| 17, Monday                           | . Arrive in Nepal by TG-311<br>. Courtesy visit to MPLD<br>Explanation of the report to Mr. Tiwari,<br>Joint Secretary<br>. Courtesy visit to Japanese Embassy<br>. Courtesy visit to JICA Office | Kathmandu |
| 18, Tuesday<br>(National<br>holiday) | . Explanation of the report to Mr. Dongol, KNP<br>. Confirmation on site of the boundary of<br>the land which is to be acquired by KNP  |           |
| 19, Wednesday                        | . Courtesy visit to Mr. Thapa, Secretary, MPLD<br>. Explanation of the Report at MPLD   |           |
| 20, Thursday                         | . Reconnaissance survey on borrow pit sites<br>. Explanation meeting with related organization  |           |
| 21, Friday                           | . Sign Minutes of Discussion<br>. Visit to JICA Office<br>. Visit to Japanese Embassy   |           |
| 22, Saturday<br>(Local holiday)      | . Leave Nepal by TG-312   | Bangkok   |
| 23, Sunday                           | . Arrive in Tokyo by CX-700, CX-508   |           |

### 1.5 List of Persons Met

|  |   |  |
|--|---|--|
| Ministry of Panchayat and Local Development                            | Secretary<br>Joint Secretary<br>Under Secretary<br>Section Secretary          | Mr. D.B. Thapa<br>Mr. R.K. Tiwari<br>Mr. N. Ghimire<br>Mr. A. Ghimire              |
| Kathmandu Nagar Panchayat  | Chairman<br>Chief Officer<br>Engineer   | Mr. S.P. Bhattarai<br>Mr. S. Adhikari<br>Mr. D. Dongol                             |
| Ministry of Works and Transport<br>Dept. of Transport<br>Dept. of Road | Joint Secretary<br>Engineer<br>Chief of Design Section<br>Mechanical Engineer | Mr. G.P. Ranjitkar<br>Mr. R.R. Sthapit<br>Dr. S.B.S. Tuladhar<br>Mr. H.L. Rajbahak |
| Ministry of Finance  | Under Secretary   | Mr. T. Neopane   |
| Kathmandu Town Development Committee                                   | Member Secretary  | Mr. S. Shrestha  |
| Bagmati Zone Office  | Engineer  | Mr. S.P. Upodhya   |
| Sajha Yatayat  | General Manager   | Mr. M.R Satyal   |
| Nepal Transport Entrepreneurs Association                              | Chairman<br>General Secretary   | Mr. S.C. Giri<br>Mr. H.P. Adhikari   |
| Water Supply and Sewerage Corporation                                  | Manager   | Mr. P.L. Jashi   |
| Nepal Electricity Agency   | Manager   | Mr. G.K. Shrescho  |
| Nepal Telecommunication Corporation                                    | Engineer  | Mr. S.M. Singn   |

|                           |  |   |
|---------------------------|--|---|
| Embassy of Japan in Nepal | Ambassador<br>Councilor<br>Secretary   | Mr. K. Arichi<br>Mr. T. Nishina<br>Mr. T. Muromoto              |
| JICA, Nepal Office        | Resident Representative<br>Deputy Representative<br>Assistant Resident Representative<br>Assistant Resident Representative | Mr. S. Kumano<br>Mr. Ayukawa<br>Mr. M. Sugimoto<br>Mr. M. Oyama |

2. Survey Data of Existing Bus Terminal

2.1 Traffic Survey

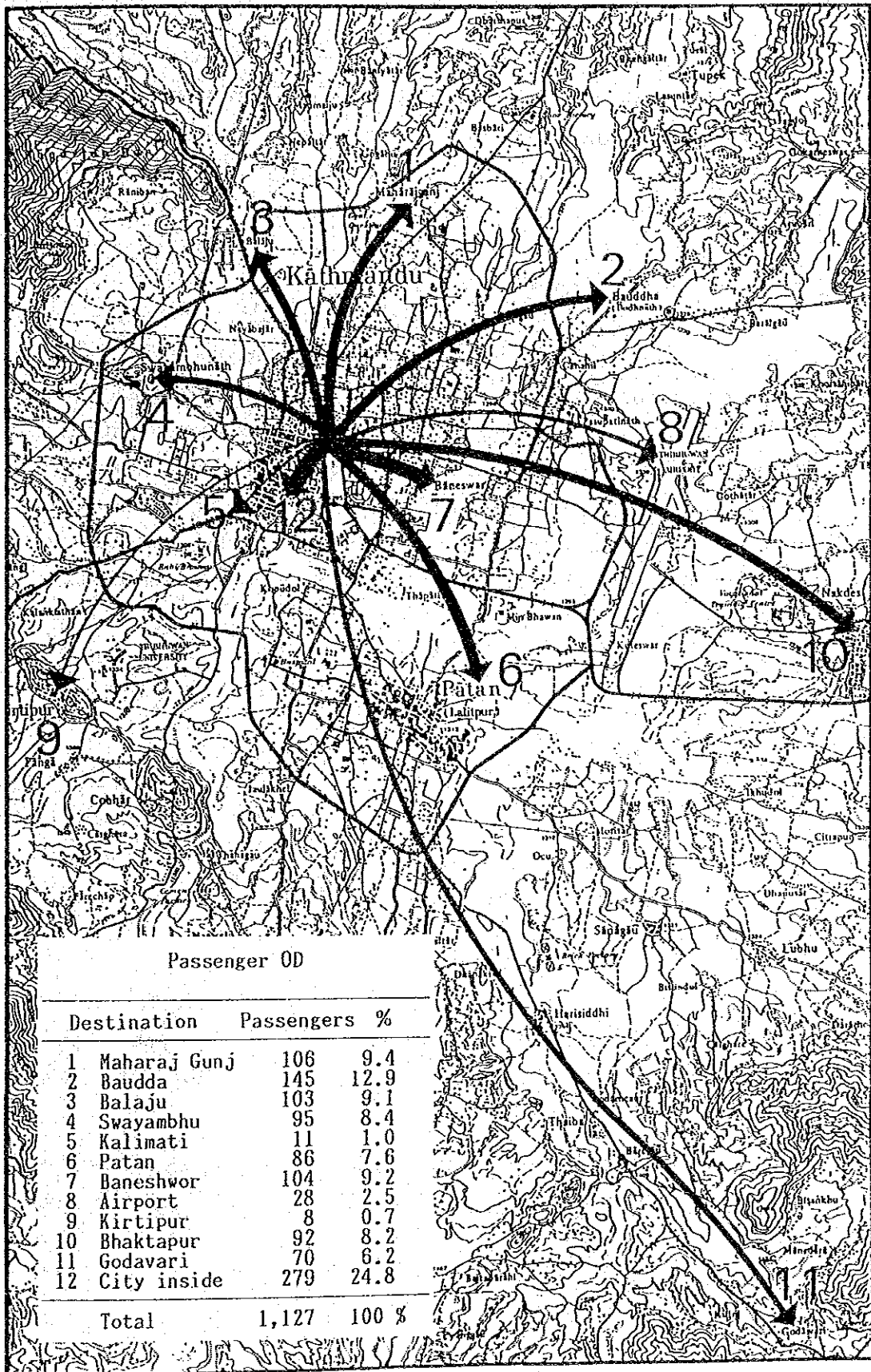
Bus Terminal Traffic Survey

(Unit: Vehicle/Hour)

| Time  | Incoming |      |       | Outgoing |      |       |
|-------|----------|------|-------|----------|------|-------|
|       | Bus      | Taxi | Tempo | Bus      | Taxi | Tempo |
| 0-1   | 0        | 0    | 0     | 0        | 0    | 0     |
| 1-2   | 0        | 0    | 0     | 0        | 0    | 0     |
| 2-3   | 0        | 0    | 0     | 0        | 0    | 0     |
| 3-4   | 0        | 0    | 0     | 0        | 0    | 0     |
| 4-5   | 3        | 4    | 5     | 2        | 1    | 5     |
| 5-6   | 14       | 13   | 16    | 7        | 155  | 23    |
| 6-7   | 20       | 28   | 33    | 7        | 25   | 26    |
| 7-8   | 18       | 46   | 27    | 14       | 25   | 24    |
| 8-9   | 12       | 35   | 23    | 4        | 47   | 45    |
| 9-10  | 11       | 34   | 22    | 11       | 30   | 25    |
| 10-11 | 4        | 27   | 17    | 11       | 18   | 12    |
| 11-12 | 10       | 38   | 36    | 12       | 19   | 19    |
| 12-13 | 9        | 36   | 27    | 9        | 23   | 27    |
| 13-14 | 7        | 32   | 25    | 9        | 34   | 26    |
| 14-15 | 14       | 52   | 29    | 12       | 21   | 16    |
| 15-16 | 10       | 70   | 34    | 18       | 32   | 18    |
| 16-17 | 15       | 111  | 82    | 34       | 39   | 26    |
| 17-18 | 10       | 85   | 82    | 31       | 32   | 33    |
| 18-19 | 8        | 69   | 39    | 18       | 29   | 14    |
| 19-20 | 5        | 45   | 29    | 14       | 23   | 11    |
| 20-21 | 1        | 18   | 8     | 7        | 6    | 5     |
| 21-22 | 0        | 13   | 7     | 0        | 0    | 0     |
| 22-23 | 0        | 0    | 0     | 0        | 0    | 0     |
| 23-24 | 0        | 0    | 0     | 0        | 0    | 0     |
| TOTAL | 171      | 756  | 541   | 220      | 419  | 355   |

Observation Date: Feb. 20, 1989

## 2.2 Passenger OD Survey





### 3. Condition of Present Bus Maintenance Facility in Kathmandu

At present, in the Kathmandu Metropolitan district there is one public bus maintenance facility operated by Sajha Yatayat and about 40 small private repair shops. The capacity of these facilities are described below.

#### 1) Sajha bus maintenance facility

This facility constructed in 1972 under grant aid from Japan is the only bus maintenance facility in the Kingdom of Nepal, and its main purpose is to provide maintenance for the 102 buses operated by Sajha Yatayat. Among the 102 buses, 82 buses are supplied from Japan under grant aid and an expert on bus maintenance is dispatched from JICA.

- Bus accommodation capacity:

5 buses

- Repair equipment:

forklift, brake tester, speedometer tester, headlight tester, tyre changer, fuel supply stand, lute, car washing equipment, etc.

- Maintenance capacity:

Maintenance capacity is quite difficult to estimate since the supply of spare parts is erratic, but on an average it may be estimated to be as follows:

|                                     |           |
|-------------------------------------|-----------|
| monthly inspection and maintenance: | 2-3 buses |
| repair:                             | 2-3 buses |

The capacity of this facility is even insufficient for maintaining buses operated by Sajha Yatayat and it is planned to be enlarged by the 1988 grant aid from Japan.

2) Private car repair shops

There is no large maintenance facility nor maintenance cooperations for maintaining private buses and each bus company must provide its own maintenance. However, since private bus companies are small companies operating 5 buses or less, they do not have their own maintenance facilities, with the exception of 2 or 3 companies. Therefore, scheduled maintenance and inspection are not performed. Broken down buses are sent to the private repair shops in Kathmandu Metropolitan where parts for engines and transmission are renewed, tyres repaired, metal work performed and other repair works are conducted. An outline of these shops are as described below.

a) Special repair shops

There are 3 repair shops in Kathmandu Municipality which specializes in repairing and renewing parts for engine, fuel pump, transmission, differential gears and other units. Although the equipment and machinery are old, they have various types of machine tools and the quality of their work is quite high. The employees number only 10 to 20 workers, and when compared with the workers at public maintenance facility, their level of skill is high and the turnover of workers is low.

● Equipment:

crankshaft grinder, cylinder boring machine,  
plane grinder, lathe, milling machine, drill,  
fuel pump tester

● Maintenance capacity:

|                    |                  |
|--------------------|------------------|
| engine overhaul    | 2-3 units/week   |
| fuel pump overhaul | 15-20 units/week |

b) Ordinary car repair shop

The ordinary car repair shops mostly do not have garages for large vehicles and repairs are performed outdoors. The number of employees are less than 10 and their skill level is quite low.

● Equipment:

air compressor, welding machine, etc.

● Repair capacity:

Replacing tyres, spare parts and consumable parts are the work performed mainly and so it is difficult to judge the repair capacity.

Judging from the above condition of maintenance facilities, the bus maintenance facility is insufficient to service and maintain the 1,920 buses registered in 1986. Especially, there is no facility to provide scheduled inspection and maintenance for private buses.

INDEX NO. : 1030

STATION : KATHMANDU AIRPORT

YEAR : 1986

4. Data

4.1 Meteorological Data at Kathmandu Airport

1) Data in 1986

| Month | AIR TEMPERATURE °C |                   |                  |             |                              | RELATIVE HUMIDITY % Observed at |                 | VAPOUR PRESSURE mb. Observed at |                   | Total             | PRECIPITATION mm.         |                      |      |      |         |    |
|-------|--------------------|-------------------|------------------|-------------|------------------------------|---------------------------------|-----------------|---------------------------------|-------------------|-------------------|---------------------------|----------------------|------|------|---------|----|
|       | Mean               |                   | Absolute extreme |             | Number of days<br>(≥30) (≤0) | 0840                            |                 | 1740                            |                   |                   | Maximum in 24 hrs. & date | Number of rainy days |      |      |         |    |
|       | Max.               | Min.              | Max. date        | Min. date   |                              | Max.                            | Min.            | Max.                            | Min.              |                   |                           | >= 1.0               | 10.0 | 25.0 | > 150.0 |    |
| JAN   | 18.3               | 2.7               | 21.2<br>7        | 0.1<br>23   | 0                            | 0                               | 97              | 65                              | 8.3               | 9.5               | 0                         | 0                    | 0    | 0    | 0       | 0  |
| FEB   | 20.1               | 3.5               | 23.4<br>24       | 0.0<br>1    | 0                            | 1                               | 96              | 58                              | 9.2               | 9.9               | 23                        | 20 / 11              | 2    | 1    | 1       | 0  |
| MAR   | 24.6 <sub>a</sub>  | 7.2               | 30.6<br>30 a     | 3.0<br>2    | 2 <sub>a</sub>               | 0                               | 79 <sub>b</sub> | 43 <sub>a</sub>                 | 11.2 <sub>b</sub> | 9.3 <sub>a</sub>  | 16                        | 7 / 13               | 5    | 5    | 0       | 0  |
| APR   | 26.4               | 11.1              | 29.6<br>19       | 6.9<br>6    | 0                            | 0                               | 74              | 54                              | 14.3              | 13.4              | 93                        | 24 / 5               | 11   | 7    | 4       | 0  |
| MAY   | 27.1               | 13.9              | 29.4<br>31       | 9.6<br>24   | 0                            | 0                               | 73              | 58                              | 16.8              | 16.4              | 97                        | 21 / 15              | 10   | 5    | 5       | 0  |
| JUN   | 28.9               | 18.9              | 32.0<br>5        | 12.8<br>2   | 8                            | 0                               | 79              | 71                              | 22.6              | 22.6              | 316                       | 65 / 29              | 18   | 9    | 5       | 3  |
| JUL   | 28.2 <sub>b</sub>  | 20.1 <sub>a</sub> | 30.2<br>4 b      | 19.1<br>1 a | 1 <sub>b</sub>               | 0 <sub>a</sub>                  | 84 <sub>a</sub> | 81 <sub>c</sub>                 | 23.8 <sub>a</sub> | 24.2 <sub>c</sub> | 381                       | 78 / 16              | 22   | 11   | 6       | 3  |
| AUG   | 28.7 <sub>a</sub>  | 19.5 <sub>a</sub> | 30.8<br>10 a     | 18.0<br>5 a | 5 <sub>a</sub>               | 0 <sub>a</sub>                  | 84              | 78 <sub>a</sub>                 | 23.3              | 24.2 <sub>a</sub> | 219                       | 62 / 3               | 20   | 12   | 7       | 0  |
| SEP   | 26.9               | 18.0              | 30.4<br>8        | 15.8<br>21  | 1                            | 0                               | 87              | 81 <sub>a</sub>                 | 21.2              | 21.6 <sub>a</sub> | 221                       | 48 / 1               | 15   | 10   | 2       | 3  |
| OCT   | 24.8               | 12.3 <sub>a</sub> | 27.4<br>3        | 8.2<br>25 a | 0                            | 0 <sub>a</sub>                  | 93              | 71                              | 15.9              | 16.5              | 80                        | 26 / 12              | 6    | 2    | 3       | 1  |
| NOV   | 22.3               | 8.1               | 25.2<br>6        | 5.6<br>29   | 0                            | 0                               | 97              | 72                              | 12.0              | 13.4              | 0                         | 0                    | 0    | 0    | 0       | 0  |
| DEC   | 18.7               | 2.8               | 24.0<br>3        | -0.2<br>31  | 0                            | 1                               | 98              | 68                              | 8.3               | 10.0              | 49                        | 32 / 19              | 4    | 2    | 1       | 1  |
| YEAR  | 24.6               | 11.5              | 32.0<br>JUN      | -0.2<br>DEC | 17                           | 2                               | 87              | 67                              | 15.6              | 15.9              | 1495                      | 78 / JUL             | 113  | 64   | 34      | 11 |

Missing number of days :  
a = 1; b = 2; c = 3;

2) Absolute Extreme Temperature, 1976-1984

(Unit: °C)

|     | January | February | March   | April   | May     | June    |
|-----|---------|----------|---------|---------|---------|---------|
| Max | 22.0    | 24.5     | 28.2    | 32.3    | 33.0    | 34.0    |
| D/y | (17,81) | (26,81)  | (29,77) | (25,80) | (18,79) | (3,79)  |
| Min | -2.0    | -2.2     | 0.5     | 3.7     | 8.9     | 11.1    |
| D/y | (4,83)  | (2,83)   | (13,78) | (1,78)  | (8,77)  | (29,82) |

|     | July   | August  | September | October | November | December |
|-----|--------|---------|-----------|---------|----------|----------|
| Max | 31.3   | 31.0    | 31.2      | 29.8    | 26.4     | 23.7     |
| D/y | (8,79) | (29,78) | (9,82)    | (2,84)  | (1,83)   | (14,78)  |
| Min | 17.8   | 13.0    | 11.8      | 4.2     | 2.4      | -2.0     |
| D/y | (4,76) | (6,84)  | (29,82)   | (31,83) | (30,76)  | (31,76)  |

Note: D/y indicates date followed by year.

Source: Climatological records of Nepal volume I, II & III.

3) Annual Rainfall, 1976-1984

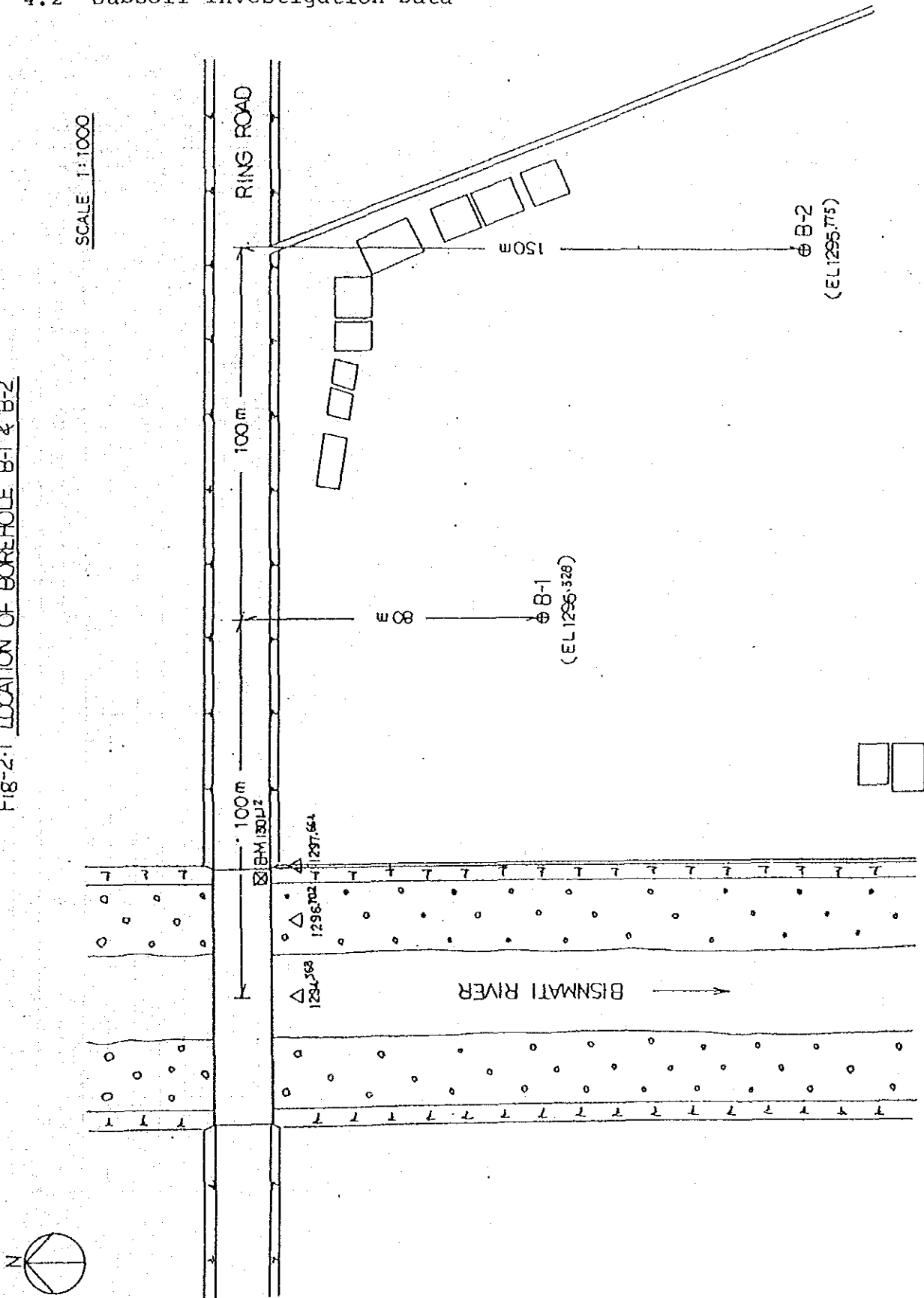
(Unit: mm)

| Year          | 1976 | 1977 | 1978 | 1979 | 1980 | 1981 | 1982 | 1983 | 1984 |
|---------------|------|------|------|------|------|------|------|------|------|
| Precipitation | 1489 | 1298 | 1556 | 1356 | 1341 | 1370 | 1168 | 1449 | 1313 |

Source: Climatological records of Nepal Volume I, II and III.

## 4.2 Subsoil Investigation Data

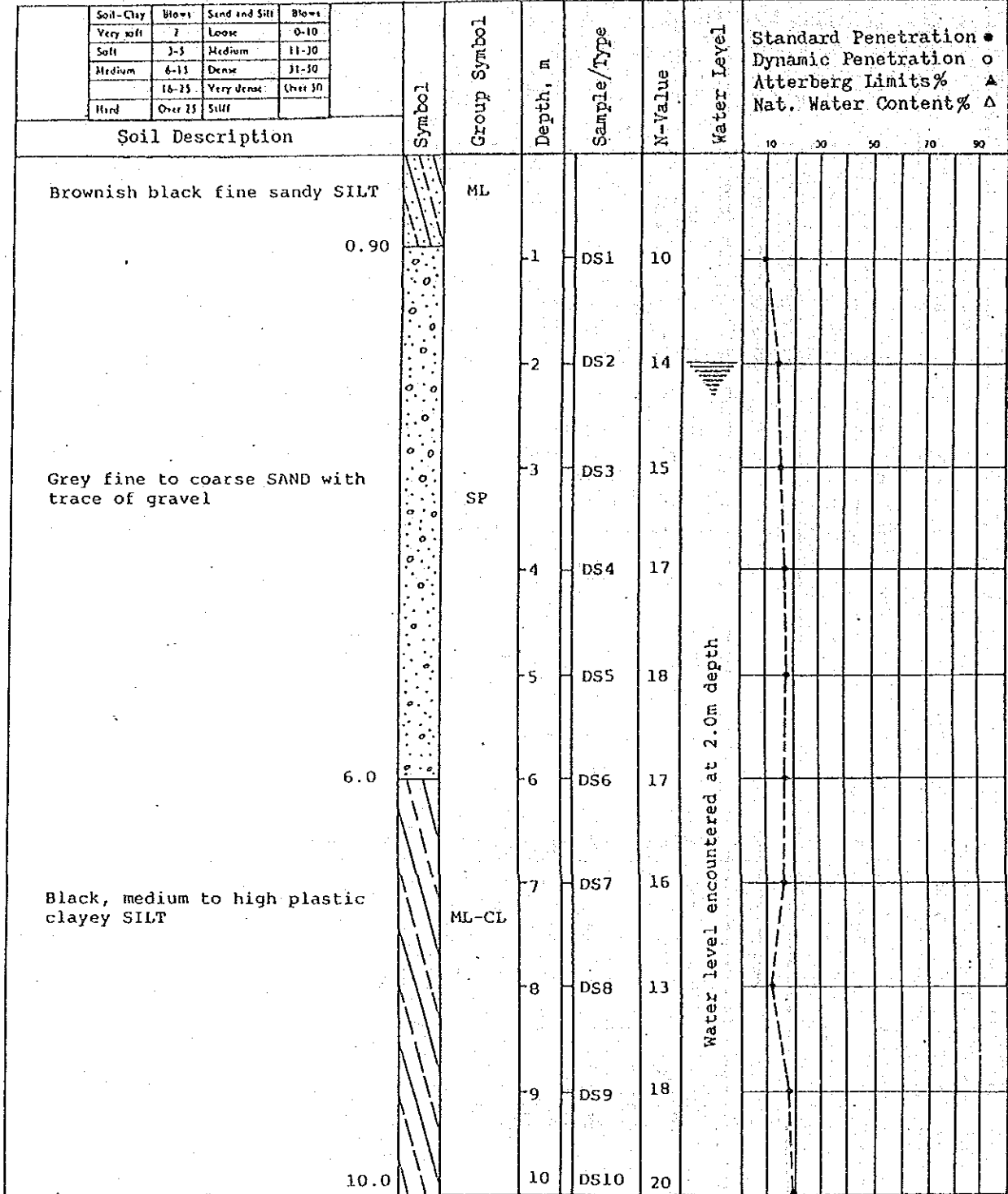
Fig-2-1 LOCATION OF BOREHOLE B-1 & B-2



LOG OF BORING B-1

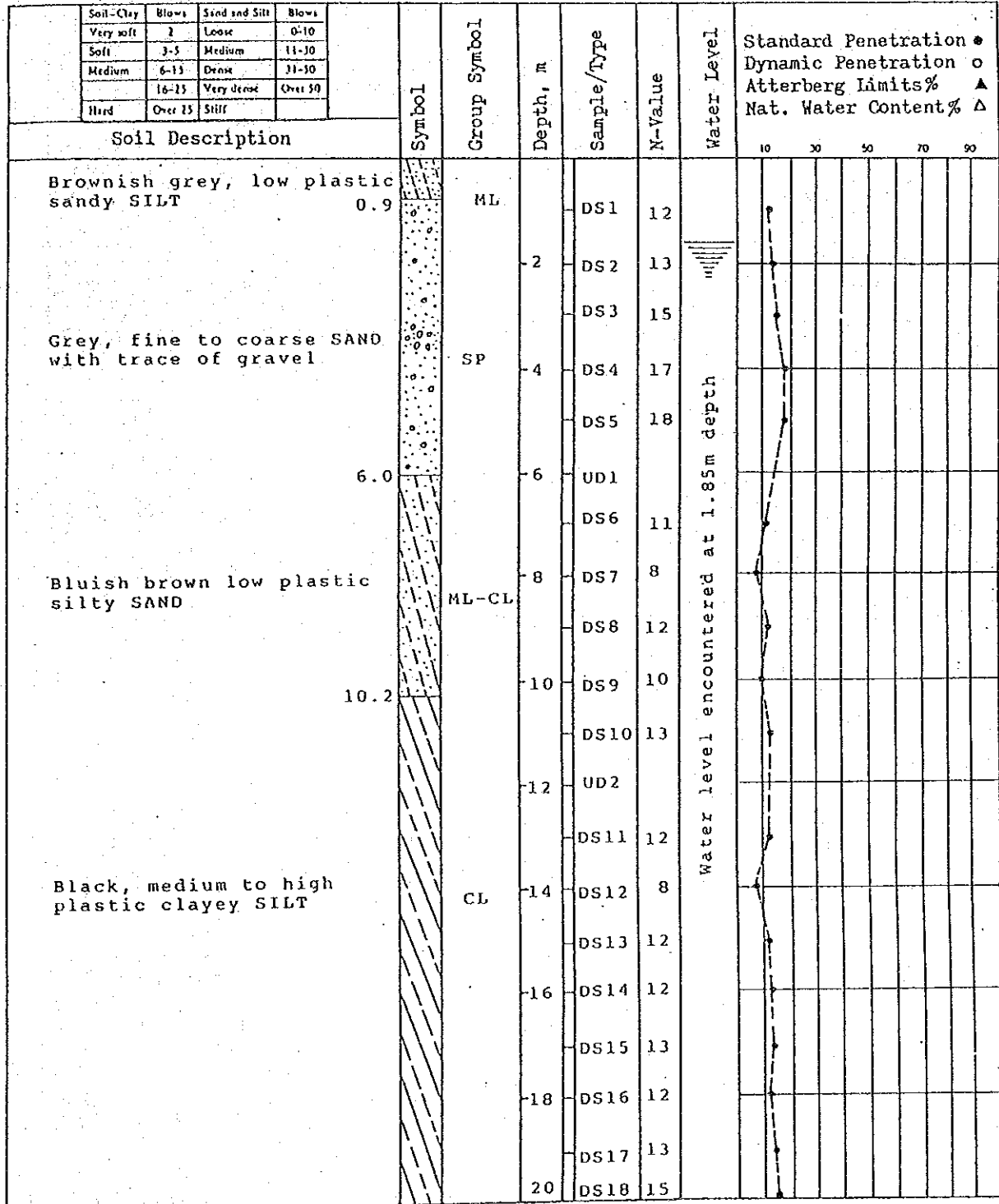
(Balaju)

Date: 15.2.1989



LOG OF BORING B-2  
(Balaju)

Date: 17.2.1989





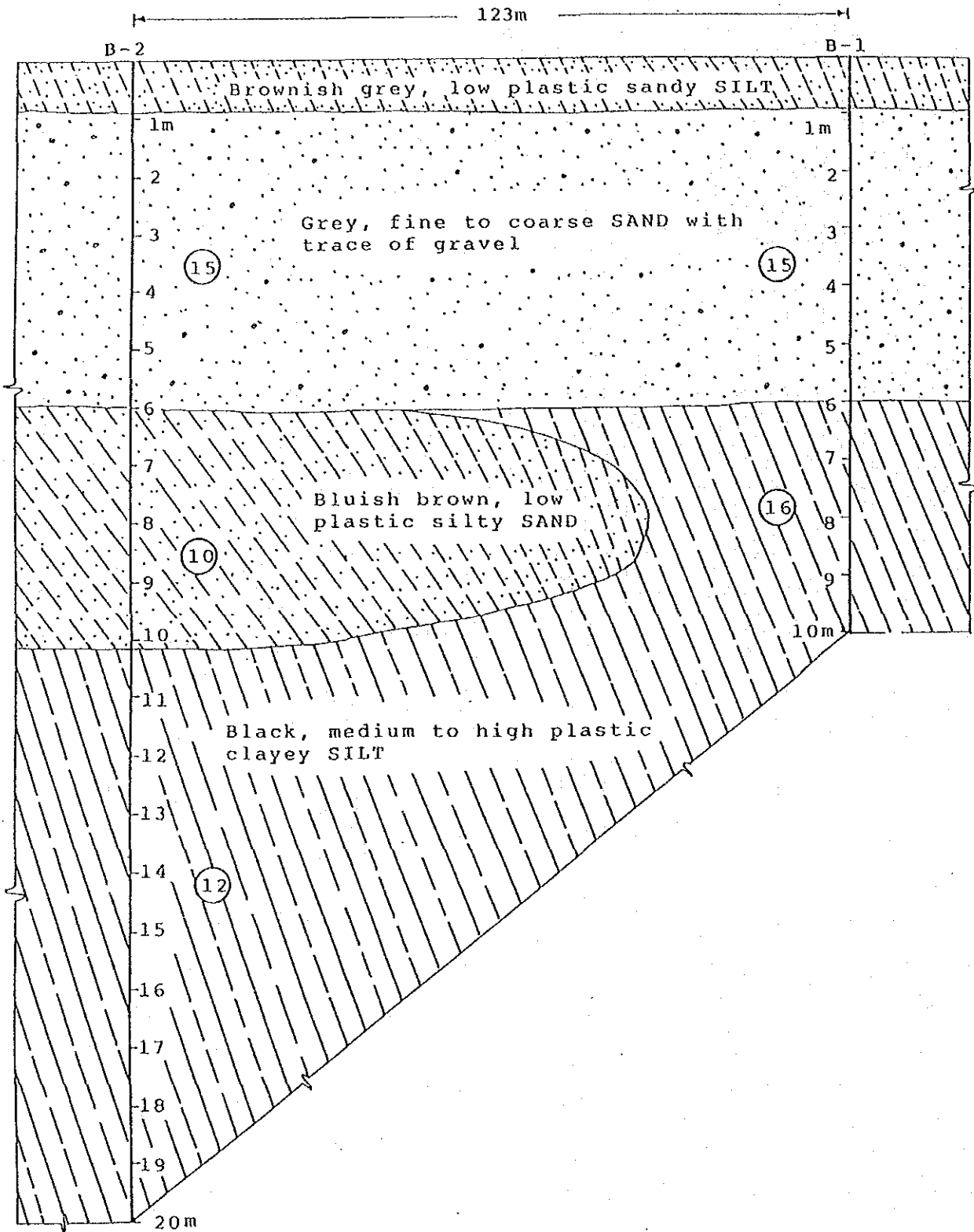


Fig-4 Geological soil profile along borehole B-1 and borehole B-2

Note: (15) Average SPT value for the strata

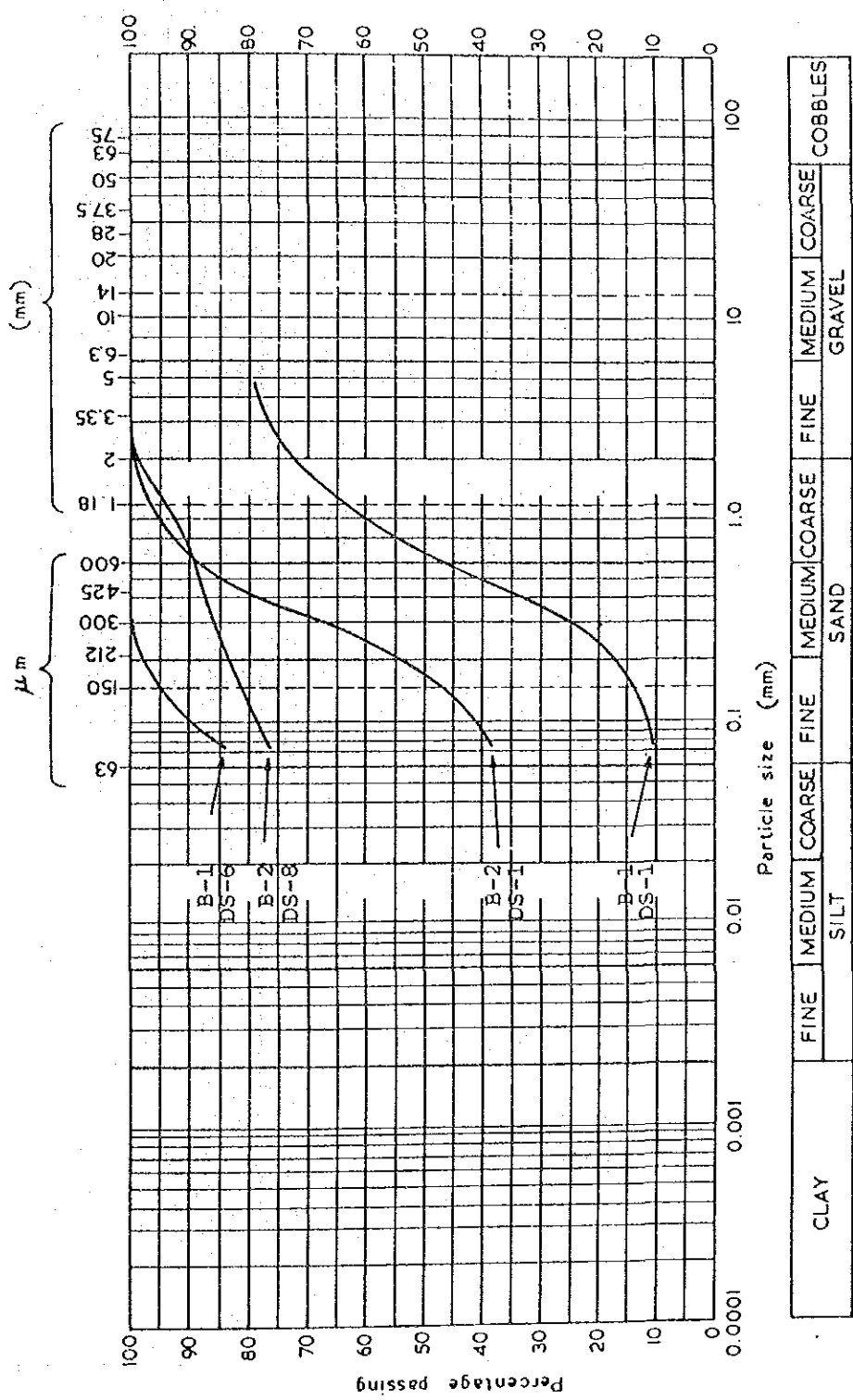


Fig - 6 Typical grain size curves from borehole B-1 & borehole B-2 (Balaju)

Table-5 Summary of geotechnical properties of foundation soils from laboratory test (Balaju)

| Borehole    | Depth, m    | Samples |      | Natural moisture % | Atterberg limits |    |     | Modulus of elasticity from SPT-value kg/cm <sup>2</sup> | Direct shear test |                       | Specific gravity |
|-------------|-------------|---------|------|--------------------|------------------|----|-----|---|-------------------|-----------------------|------------------|
|             |             | DS      | UD   |                    | LL               | PL | PI  |   | $\phi^\circ$      | C, kg/cm <sup>2</sup> |                  |
| B-1         | 1.0 - 1.45  | 1       |      | 16.8               |                  |    |     | 375   | 34                | 0                     | 2.639            |
|             | 2.0 - 2.45  | 2       |      |                    |                  |    |     |   |                   |                       |                  |
|             | 3.0 - 3.45  | 3       |      | 11.2               |                  |    |     |   |                   |                       |                  |
|             | 4.0 - 4.45  | 4       |      |                    |                  |    | 450 | 32  | 0                 |                       |                  |
|             | 5.0 - 5.45  | 5       |      | 12.8               |                  |    |     | 450   |                   | 2.642                 |                  |
|             | 6.0 - 6.45  | 6       |      | 26.7               |                  |    |     |   |                   |                       |                  |
|             | 7.0 - 7.45  | 7       |      |                    |                  |    |     | 465   |                   | 2.620                 |                  |
|             | 8.0 - 8.45  | 8       |      | 43.8               | 38               | 29 | 9   |   |                   |                       |                  |
|             | 9.0 - 9.45  | 9       |      |                    |                  |    |     |   |                   |                       |                  |
|             | 9.55-10.0   | 10      |      | 53.2               | 42               | 30 | 12  |   |                   |                       |                  |
| B-2         | 1.0 - 1.45  | 1       |      |                    |                  |    |     | 350   |                   |                       | 2.661            |
|             | 2.0 - 2.45  | 2       |      | 13.2               |                  |    |     |   |                   |                       |                  |
|             | 3.0 - 3.45  | 3       |      | 11.8               |                  |    |     |   |                   |                       |                  |
|             | 4.0 - 4.45  | 4       |      |                    |                  |    |     | 450   |                   |                       | 2.652            |
|             | 5.0 - 5.45  | 5       |      | 17.2               |                  |    |     |   |                   |                       |                  |
|             | 6.0 - 6.30  |         | 1    |                    |                  |    |     | 300   | 23                | 0.125                 |                  |
|             | 7.0 - 7.45  | 6       |      |                    |                  | 24 | 19  | 5   | 25                | 0                     | 2.621            |
|             | 8.0 - 8.45  | 7       |      | 27.1               |                  |    |     |   |                   |                       |                  |
|             | 9.0 - 9.45  | 8       |      |                    |                  | 28 | 21  | 7   | 320               |                       | 2.610            |
|             | 10.0 -10.45 | 9       |      |                    |                  |    |     |   |                   |                       |                  |
|             | 11.0 -11.45 | 10      |      | 39.3               | 35               | 25 | 10  |   |                   |                       |                  |
|             | 12.0 -12.30 |         | 2    |                    |                  | 36 | 27  | 9   |                   |                       |                  |
|             | 13.0 -13.45 | 11      |      |                    |                  | 42 | 31  | 11  | 240               |                       |                  |
|             | 14.0 -14.45 | 12      |      | 47.2               |                  |    |     |   |                   |                       |                  |
|             | 15.0 -15.45 | 13      |      |                    |                  | 54 | 36  | 18  | 350               |                       |                  |
|             | 16.0 -16.45 | 14      |      | 43.8               | 49               | 33 | 16  |   |                   |                       |                  |
|             | 17.0 -17.45 | 15      |      |                    |                  |    |     |   | 350               |                       |                  |
|             | 18.0 -18.45 | 16      |      | 52.7               | 56               | 37 | 19  |   |                   |                       |                  |
| 19.0 -19.45 | 17          |         |      |                    | 59               | 37 | 22  | 350   |                   | 2.605                 |                  |
| 19.55-20.0  | 18          |         | 48.7 |                    |                  |    |     |   |                   |                       |                  |

NOTE:

- DS = disturbed sample
- UD = undisturbed sample
- LL = liquid limit
- PL = plastic limit
- PI = plasticity index
- $\phi^\circ$  = angle of internal friction
- C = cohesion of soil

Table-9 Allowable bearing capacity from standard penetration test (Balaju)

| Depth, m   | Borehole B-1                   |  | Borehole B-2                   |  |
|------------|--------------------------------|--|--------------------------------|--|
|            | Corrected SPT value blows/30cm | Allowable bearing pressure tons/m <sup>2</sup> | Corrected SPT value blows/30cm | Allowable bearing pressure tons/m <sup>2</sup> |
| 1.0- 1.45  | 10                             | 9  | 12                             | 10.5   |
| 2.0- 2.45  | 14                             | 12.5   | 13                             | 11.5   |
| 3.0- 3.45  | 15                             | 13   | 15                             | 13.0   |
| 4.0- 4.45  | 16                             | 13.5   | 16                             | 13.5   |
| 5.0- 5.45  | 16                             | 13.5   | 16                             | 13.5   |
| 6.0- 6.45  | 16                             | 13.5   |                                |  |
| 7.0- 7.45  | 15                             | 13   | 11                             | 10.0   |
| 8.0- 8.45  | 13                             | 11.5   | 8                              | 7.0  |
| 9.0- 9.45  | 16                             | 13.5   | 12                             | 10.5   |
| 10.0-10.45 | 17                             | 15   | 10                             | 9.0  |
| 11.0-11.45 |                                |  | 13                             | 11.5   |
| 12.0-12.45 |                                |  |                                |  |
| 13.0-13.45 |                                |  | 12                             | 10.5   |
| 14.0-14.45 |                                |  | 8                              | 7  |
| 15.0-15.45 |                                |  | 12                             | 10.5   |
| 16.0-16.45 |                                |  | 12                             | 10.5   |
| 17.0-17.45 |                                |  | 13                             | 11.5   |
| 18.0-18.45 |                                |  | 12                             | 10.5   |
| 19.0-19.45 |                                |  | 13                             | 11.5   |
| 20.0-20.45 |                                |  | 15                             | 13.0   |

### CALIFORNIA BEARING RATIO TEST

Project: Kathmandu bus terminal

Sample No: 1

Depth, m: 0-2m

Location: Near borehole B-1

Technician: K. Thapa

Date: 21.2.1989

Soil Classification: Homogeneous mixture  
of sand and silt

| Condition of Sample              | Before Soaking | After Soaking |
|----------------------------------|----------------|---------------|
| Weight of Wet Sample + Mould gm  | 12.130         | 12260         |
| Weight of Mould gm               | 7.673          | 7673          |
| Weight of Wet Sample gm          |                | 4587          |
| Volume of Sample cc              |                | 2248          |
| Wet Unit Weight (Unsoaked) gm/cc |                | 2.04          |
| Avg. Moisture Content %          |                | 20.41         |
| Dry Unit Weight, gm/cc           |                | 1.69          |

No. of Layers: 3

Period of Soaking: 4 Days

No. of Blows Per Layer: 55

Swell: 1.77mm & 1.390%

| Penetration<br>mm | Standard Load<br>kg/cm <sup>2</sup> | Test Load |                    | Corrected C.B.R.   |      |
|-------------------|-------------------------------------|-----------|--------------------|--------------------|------|
|                   |                                     | kg        | kg/cm <sup>2</sup> | kg/cm <sup>2</sup> | %    |
| 0.5               |                                     | 18.2      | 0.93               |                    |      |
| 1.0               |                                     | 34.8      | 1.77               |                    |      |
| 1.5               |                                     | 57.3      | 2.92               |                    |      |
| 2.0               |                                     | 76.1      | 3.88               |                    |      |
| 2.5               | 70.0                                | 91.2      | 4.65               | 6.64               | 6.64 |
| 5.0               | 105.0                               | 149.8     | 7.63               | 7.27               | 7.27 |
| 7.5               |                                     | 211.7     | 10.79              |                    |      |
| 10.0              |                                     | 259.5     | 13.23              |                    |      |
| 12.5              |                                     | 302.6     | 15.42              |                    |      |

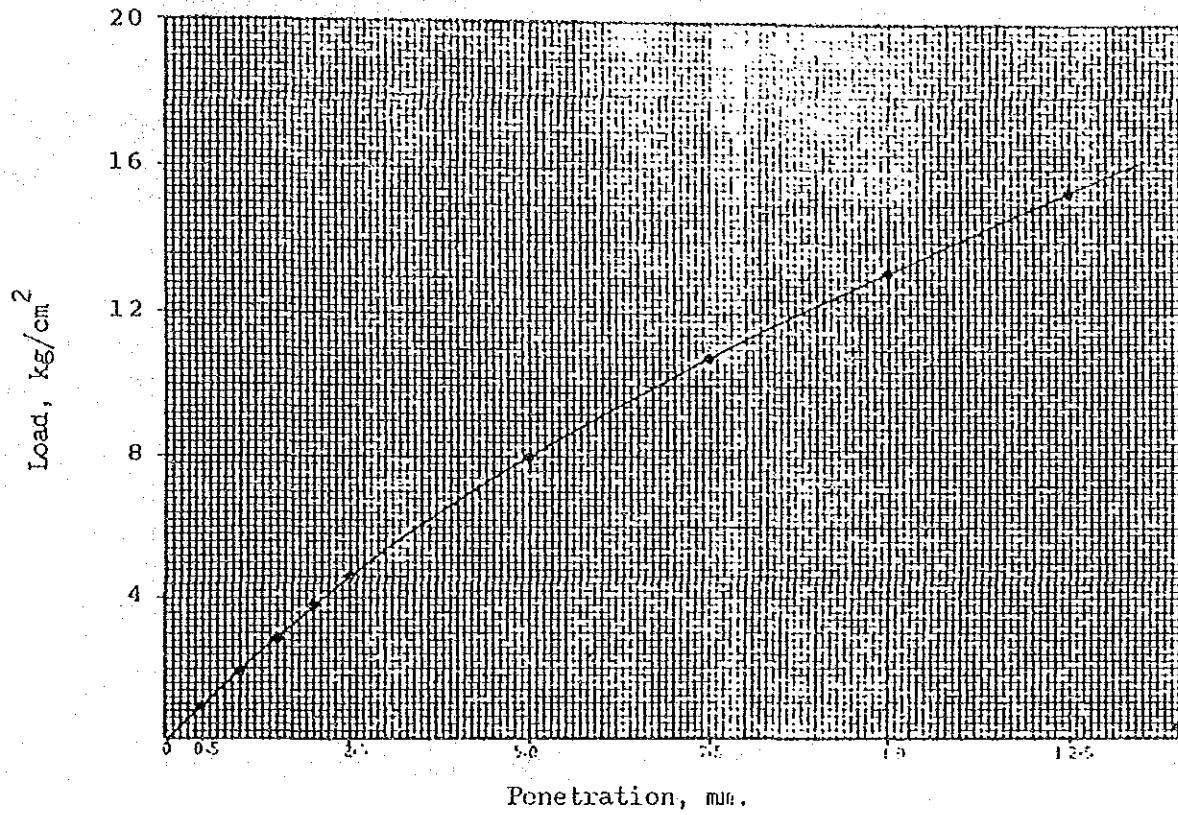


Fig - Load-Penetration Curve

Remarks:

### CALIFORNIA BEARING RATIO TEST

Project: Kathmandu bus terminal      Sample No: 2      Depth, m: 0-2m  
 Location: Near borehole B-2      Technician: K. Thapa      Date: 21.2.1989  
 Soil Classification: Homogeneous mixture  
 of sand and silt

| Condition of Sample              | Before Soaking | After Soaking |
|----------------------------------|----------------|---------------|
| Weight of Wet Sample + Mould gm  | 12.030         | 12160         |
| Weight of Mould gm               | 7.515          | 7515          |
| Weight of Wet Sample gm          |                | 4645          |
| Volume of Sample cc              |                | 2248          |
| Wet Unit Weight (Unsoaked) gm/cc |                | 2.07          |
| Avg. Moisture Content %          |                | 19.44         |
| Dry Unit Weight, gm/cc           |                | 1.73          |

No. of Layers: 3      Period of Soaking: 4 Days  
 No. of Blows Per Layer: 55      Swell: 3.04 mm & 2.39 %

| Penetration<br>mm | Standard Load<br>kg/cm <sup>2</sup> | Test Load |                    | Corrected C.B.R.   |      |
|-------------------|-------------------------------------|-----------|--------------------|--------------------|------|
|                   |                                     | kg        | kg/cm <sup>2</sup> | kg/cm <sup>2</sup> | %    |
| 0.5               |                                     | 16.6      | 0.85               |                    |      |
| 1.0               |                                     | 34.9      | 1.78               |                    |      |
| 1.5               |                                     | 56.4      | 2.88               |                    |      |
| 2.0               |                                     | 74.7      | 3.81               |                    |      |
| 2.5               | 70.0                                | 89.6      | 4.57               | 6.52               | 6.52 |
| 5.0               | 105.0                               | 156.0     | 7.95               | 7.57               | 7.57 |
| 7.5               |                                     | 214.1     | 10.91              |                    |      |
| 10.0              |                                     | 265.6     | 13.54              |                    |      |
| 12.5              |                                     | 307.1     | 15.65              |                    |      |

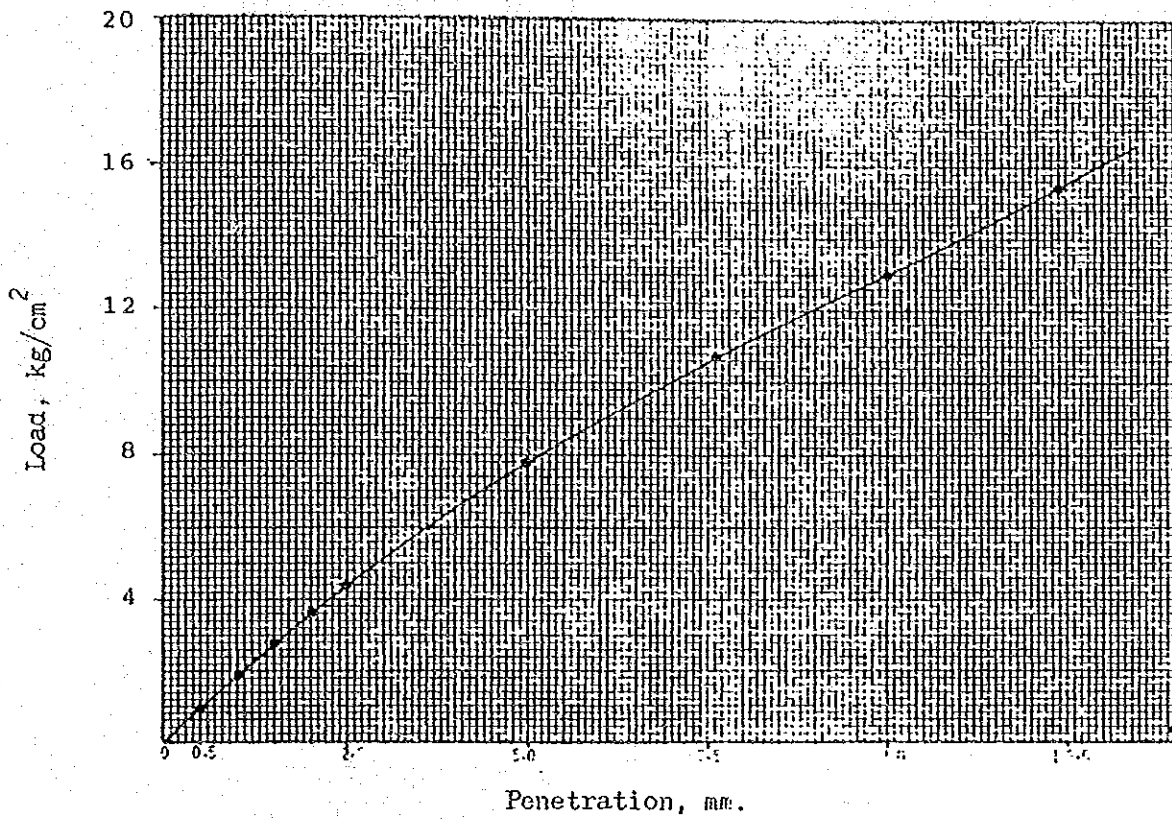


Fig - Load-Penetration Curve

Remarks:



4.3 Excerpts from Manual for Asphalt/Cement Pavement  
Asphalt Pavement

Road Classification by Traffic

Table 2-3 Road Classification by Traffic

| Classification | One Way Daily Traffic of Heavy Vehicles |
|----------------|---|
| L              | Less than 100                           |
| A              | 100 to 250                              |
| B              | 250 to 1,000                            |
| C              | 1,000 to 3,000                          |
| D              | More than 3,000                         |

Relations among Design CBR,  $T_A$  and  $H$

Table 2-6 Target Values for  $T_A$  and for the Total Pavement Thickness,  $H$ , cm.

| Design CBR | Road Classification |     |       |     |       |     |       |     |       |     |
|------------|---------------------|-----|-------|-----|-------|-----|-------|-----|-------|-----|
|            | L                   |     | A     |     | B     |     | C     |     | D     |     |
|            | $T_A$               | $H$ | $T_A$ | $H$ | $T_A$ | $H$ | $T_A$ | $H$ | $T_A$ | $H$ |
| 2          | 17                  | 52  | 21    | 61  | 29    | 74  | 39    | 90  | 51    | 105 |
| 3          | 15                  | 41  | 19    | 48  | 26    | 58  | 35    | 70  | 45    | 83  |
| 4          | 14                  | 35  | 18    | 41  | 24    | 49  | 32    | 59  | 41    | 70  |
| 6          | 12                  | 27  | 16    | 32  | 21    | 38  | 28    | 47  | 37    | 55  |
| 8          | 11                  | 23  | 14    | 27  | 19    | 32  | 26    | 39  | 34    | 46  |
| 12         | —                   | —   | 13    | 21  | 17    | 26  | 23    | 31  | 30    | 36  |
| 20 or more | —                   | —   | —     | —   | —     | —   | 20    | 23  | 26    | 27  |

Pavement Structure

Table 2-7 Minimum Combined Thickness of Binder and Surface Courses (Unit:cm)

| Road Classification | Minimum Combined Thickness of Binder and Surface Courses |
|---------------------|--|
| L, A                | 5  |
| B                   | 10 ( 5)  |
| C                   | 15 (10)  |
| D                   | 20 (15)  |

Note: Figures in ( ) indicate the minimum thickness applicable to pavements with bitumen stabilized bases.

$$T_A = a_1 T_1 + a_2 T_2 + \dots + a_n T_n \quad (2.4)$$

where  $a_1, a_2, \dots, a_n$ : Coefficients of relative strength given in Table 2-8.

$T_1, T_2, \dots, T_n$ : Thickness of individual layers of pavement, cm.

Table 2-8 Coefficients of Relative Strength for Calculating  $T_A$

| Pavement Course            | Method and Material of Construction Used       | Conditions  | Coefficient |
|----------------------------|--|---|-------------|
| Binder and Surface Courses | Hot asphalt mix for binder and surface courses |   | 1.00        |
| Base                       | Bituminous stabilization                       | — Hot-mixed, Marshall stability: 350kg or more                    | 0.80        |
|                            |  | — Cold-mixed, Marshall stability: 250kg or more                   | 0.55        |
|                            | Cement Stabilization                           | — Unconfined compressive strength (7 days): 30kg/cm <sup>2</sup>  | 0.55        |
|                            |  | — Unconfined compressive strength (10 days): 10kg/cm <sup>2</sup> | 0.45        |
|                            | Lime Stabilization                             | — Modified CBR: 80 or more  | 0.35        |
|                            | Mechanically Stabilized Gravel and Slag        | — Modified CBR: 80 or more  | 0.55        |
|                            | Hydraulic Mechanically Stabilized Slag         | — Unconfined compressive strength (14 days): 12kg/cm <sup>2</sup> | 0.55        |
| Penetration Macadam        |  |   |             |
| Subbase                    | Crusher-run, Slag, Sand, etc.                  | — Modified CBR: 30 or more,                                       | 0.25        |
|                            |  | — Modified CBR: 20 or more, less than 30                          | 0.20        |
|                            | Cement Stabilization                           | — Unconfined compressive Strength, (7 days): 10kg/cm <sup>2</sup> | 0.25        |
|                            | Lime Stabilization                             | — Unconfined compressive Strength (10 days): 7kg/cm <sup>2</sup>  | 0.25        |

Note: Layer coefficient for any construction method or material other than those listed in Table 2-8 should only be adopted when based on established engineering experience.

## Design Section of Concrete Pavement

(Unit: cm)

| Traffic Classification | Design CBR for Sub-grade                      |  | 4  | 6   |
|------------------------|---|--|--|---|
|                        | Sub-base                                      |  |  |   |
| L.A                    | Granular Material                             |  | <div style="border: 1px solid black; padding: 2px; width: 100%;">Concrete Slab</div> <div style="border: 1px solid black; padding: 2px; width: 100%;">CBR &gt; 80</div>  | <div style="border: 1px solid black; padding: 2px; width: 100%;">Concrete Slab</div> <div style="border: 1px solid black; padding: 2px; width: 100%;">CBR &gt; 80</div>               |
|                        | Stabilization with Cement (Granular Material) |  | <div style="border: 1px solid black; padding: 2px; width: 100%;">Concrete Slab</div> <div style="border: 1px solid black; padding: 2px; width: 100%;">Stabilization with Cement</div>  | <div style="border: 1px solid black; padding: 2px; width: 100%;">Concrete Slab</div> <div style="border: 1px solid black; padding: 2px; width: 100%;">Stabilization with Cement</div> |
| B                      | Granular Material                             |  | <div style="border: 1px solid black; padding: 2px; width: 100%;">Concrete Slab</div> <div style="border: 1px solid black; padding: 2px; width: 100%;">CBR &gt; 80</div> <div style="border: 1px solid black; padding: 2px; width: 100%;">CBR &gt; 20</div> | <div style="border: 1px solid black; padding: 2px; width: 100%;">Concrete Slab</div> <div style="border: 1px solid black; padding: 2px; width: 100%;">CBR &gt; 80</div>               |
|                        | Stabilization with Cement (Granular Material) |  | <div style="border: 1px solid black; padding: 2px; width: 100%;">Concrete Slab</div> <div style="border: 1px solid black; padding: 2px; width: 100%;">Stabilization with Cement</div>  | <div style="border: 1px solid black; padding: 2px; width: 100%;">Concrete Slab</div> <div style="border: 1px solid black; padding: 2px; width: 100%;">Stabilization with Cement</div> |

#### 4.4 Excerpts from Indian Standard (Seismic Loads)

pressure on the roof may be assumed as:

- 0.6  $p$  on both slopes of the roof over a length from the gable end equal to the mean height of the roof from the surrounding ground-level, and
- 0.4  $p$  over the remaining length of the roof on both slopes.

##### 4.6.2 LOCAL EFFECTS

4.6.2.1 The pressures and suctions specified in 4.6.1 are average values and may be exceeded locally. In designing individual components of roofs, such as sheeting, the values given in 4.6.1 shall be increased numerically by 0.3  $p$ .

4.6.2.2 All fastenings for roof sheetings shall be capable of resisting the pressures on the sheeting as specified in 4.6.2.1. Fastenings within a distance of 15 percent of the length of the roof from the gables shall be capable of resisting a suction of 2.0  $p$  on the area of roof sheeting they support.

#### 5. SEISMIC LOAD

##### 5.1 General Principles

5.1.1 Earthquake shocks cause a movement of ground on which the structure is situated. This movement causes the structure to vibrate. The vibrations may be resolved in any three perpendicular directions and the design of structures, made safe for the components of vibrations in the three directions acting simultaneously, shall be considered safe unless otherwise specifically stated. The predominant direction of vibration is horizontal.

5.1.2 The vibration intensity of ground expected at any location depends upon the magnitude of earthquake, the depth of focus, the distance from the epicentre and the strata on which the structure stands. The important structures shall be designed for the maximum vibration intensity expected at the place.

5.1.3 The response of the structure to the ground vibration is a function of the nature of foundation soil; materials, form, size and mode of construction of the structure; and the duration and the intensity of ground motion. This section specifies design acceleration for structures standing on soils which will not considerably settle or slide appreciably due to vibration lasting for a few seconds.

5.1.4 In the case of structures designed for horizontal seismic force only it shall be considered to act in any one direction at a time. Where both horizontal and vertical seismic forces are taken into account, horizontal

force in any one direction at a time may be considered simultaneously with the vertical force as specified in 5.3.4.

5.1.5 The vertical seismic coefficient shall be considered only in the case of structures in which stability is a criterion of design or for overall stability except as otherwise stated in the relevant clauses.

##### 5.2 Permissible Increase in Stresses

5.2.1 PERMISSIBLE INCREASE IN MATERIAL STRESSES — Whenever earthquake forces are considered along with other normal design forces, the permissible stresses in materials, in the elastic method of design, may be increased by one-third provided that for steels having a definite yield stress, the stress will be limited to the yield stress; for steels without a definite yield point, the stress will be limited to 80 percent of the ultimate strength.

5.2.2 PERMISSIBLE INCREASE IN ALLOWABLE BEARING PRESSURE OF SOILS — For permissible increase in allowable bearing pressure of soils, reference may be made to Part VI Structural design, Section 2 Foundations.

##### 5.3 Seismic Coefficient for Different Zones

5.3.1 For the purpose of determining the seismic forces, the country is classified into five zones, as shown in Fig. 13 (see P 22). Unless otherwise stated, horizontal seismic coefficients for static design in different zones shall be taken as follows (see also 5.3.2 and 5.5):

| Zone No. | Horizontal Seismic Coefficient $\alpha_h$ |
|----------|---|
| V        | 0.08                                      |
| IV       | 0.05                                      |
| III      | 0.04                                      |
| II       | 0.02                                      |
| I        | 0.01                                      |

5.3.1.1 For dynamic design, the acceleration spectra shown in Fig. 15 and multiplying factor  $F$  as given in Appendix A shall be used.

5.3.2 Depending upon the soil-foundation systems (see Part VI Structural design, Section 2 Foundations) on which the structure is founded, the horizontal seismic coefficient given in 5.3.1 and Factor  $F$  given in Appendix A, shall be multiplied by a factor  $\beta$ . The value of  $\beta$  for various cases shall be as given in Table 5.

5.3.3 The seismic coefficients for some important towns and cities are given in Appendix B.

TABLE 5. VALUE OF  $\beta$  FOR DIFFERENT SOIL-FOUNDATION SYSTEMS  
( Clause 5.3.2 )

| Sl. No. | TYPE OF FOUNDATIONS  | VALUE OF $\beta$ FOR SOIL TYPE |                    |                   |
|---------|--|--------------------------------|--------------------|-------------------|
|         |  | I<br>Rock or Hard Soils        | II<br>Medium Soils | III<br>Soft Soils |
| (1)     | (2)  | (3)                            | (4)                | (5)               |
| 1)      | Bearing piles resting on soil Type I or raft foundation              | 1.0                            | 1.0                | 1.0               |
| 2)      | Friction piles, combined or isolated RCC footing with tie beams      | 1.0                            | 1.0                | 1.2               |
| 3)      | Isolated footings without tie beam or unreinforced strip foundations | 1.0                            | 1.2                | 1.5               |
| 4)      | Well foundation  | 1.0                            | 1.2                | 1.5               |

5.3.4 The vertical seismic coefficient, where applicable ( see 5.1.5 ) may be taken as half of the horizontal seismic coefficient given in 5.3.1.

#### 5.4 Design Live Loads

5.4.1 For various loading classes as specified in Table 1, the horizontal earthquake force shall be calculated for the full dead load and the percentage of live loads as given below:

| Load Class                                       | Percentage of Design Live Load |
|--|--------------------------------|
| 200, 250, 300, stairs and balconies              | 25                             |
| 400, 500, 750 and 1 000, garage, light and heavy | 50                             |

NOTE 1 — The percentage of live load given above shall also be used for calculating stresses due to vertical loads for combining with those due to earthquake forces. Under the earthquake condition, the whole frame may be assumed as loaded with live load except the roof.

NOTE 2 — The proportions of the live load indicated above for calculating the horizontal seismic forces are applicable to average conditions. Where the probable loads at the time of an earthquake are more accurately assessed, the designer may alter the proportions indicated or even replace the entire live load proportions by the actual assessed load.

NOTE 3 — If the live load is assessed instead of taking the above proportions for calculating horizontal earthquake force, only that part of the live load shall be considered which possesses mass. Earthquake force shall not be applied on impact effects.

5.4.2 For calculating the earthquake force on roofs, the live load may not be considered.

#### 5.5 Miscellaneous Buildings

5.5.1 Buildings provided for accommodating essential services which will be of post-earthquake importance, such as power stations, hospitals, emergency relief stores, foodgrain storage structures, water works and water towers shall be designed for one and a half times the seismic coefficient specified in 5.3.1 or one and a half times the  $F$  value specified in Appendix A.

5.5.2 Towers, tanks, parapets, smoke stacks, chimneys and other vertical cantilever projections attached to buildings and projecting above the roofs shall be designed for five times the horizontal seismic coefficient specified in 5.3.1. However, compound walls need not be designed for increased seismic coefficient except where the environmental circumstances indicate that their collapse may lead to serious consequences.

5.5.3 All horizontal projections like cornices and balconies shall be designed to resist a vertical force equal to five times the vertical seismic coefficient specified in 5.3.4 multiplied by the weight of the projection.

NOTE — The increased seismic coefficient specified in 5.5.2 and 5.5.3 are for designing the projecting part and its connection with the main structure. For the design of the main structure such increase need not be considered.

5.6 Design of Buildings — For the application of seismic forces for the design of buildings, reference may be made to good practice [ VI-1(3) ].

## 6. SOIL AND HYDROSTATIC PRESSURES

6.1 In the design of structures or parts of structures below ground-level, such as basement floors and walls, the pressures exerted by the soil or water or both shall be duly accounted for on the basis of established theories. Due allowance shall be made for possible surcharge from stationary or moving loads.

6.2 While determining the lateral soil pressure on slender structural members, such as pillars which rest in sloping soils, the width of the member shall preferably be taken as twice its actual width. The relieving pressure of soil in front of the structural member concerned may generally not be taken into account ( see Fig. 14 ).

6.3 Safeguarding of structures and structural

members against overturning and horizontal forward movement shall be verified. Live loads having favourable effect shall be disregarded for the purpose. Due consideration shall be given to the possibility of soil being permanently or temporarily removed.

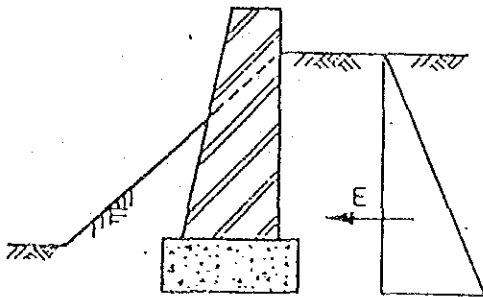
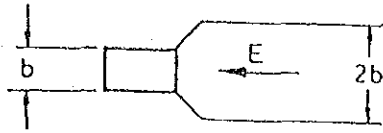


Fig. 14

## 7. ERECTION LOADS

7.1 All loads required to be carried by the structure or any part of it due to placing or storage of construction materials and erection equipment including all loads due to operation of such equipment, shall be considered as 'erection loads'. Proper provisions shall be made to take care of all stresses due to such loads.

## 8. OTHER FORCES

8.1 Impact, vibrations, temperature effects, shrinkage, creep and such other phenomena produce effects on structures some of which may be similar to those caused by external loads specified in 2 to 7. Adequate provision should be made for the effects of one or more

of these phenomena separately or in appropriate combination with the specified external loads in accordance with the recommendations of the appropriate design sections.

## 9. LOAD COMBINATIONS

9.1 A judicious combination of the working loads specified in 2 to 7 keeping in view the probability of their acting together and their disposition in relation to other loads and the severity of stresses or deformations caused by the combination of the various loads, is necessary to ensure the required safety and economy in the design of a structure.

9.2 The various loads specified in 2 to 7 should, therefore, be combined in accordance with the stipulations in the appropriate design sections. In the absence of such recommendations, however, the following load combinations, given for general guidance, may be adopted:

- a) Dead load alone.
- b) Dead load plus partial or full live load whichever causes the most critical condition in the structure.
- c) Dead load plus wind or seismic loads.
- d) Dead load plus such part of or whole of the specified live load whichever is most likely to occur in combination with the specified wind or seismic loads plus wind or seismic loads.
- e) Dead loads plus such parts of the live load as would be imposed on the structure during the period of erection plus wind or seismic loads plus erection loads.

NOTE — For design purposes, wind load and seismic forces shall be assumed not to act simultaneously. Both forces shall, however, be investigated separately and adequately provided for.

9.2.1 While considering the load combinations recommended in 9.2, the effects of other forces mentioned in 8 should also be taken into account.

## APPENDIX A

( Clauses 5.3.1.1 and 5.5.1 )

### SPECTRA OF EARTHQUAKE

#### A-1. GENERAL

A-1.1 Spectrum of an earthquake is the representation of the maximum dynamic response of idealized structures during an

earthquake. The idealized structure is a single degree of freedom system having a certain period of vibration and damping. The maximum response is plotted against the natural period of vibration and can be

expressed in terms of maximum absolute acceleration, maximum relative velocity or maximum relative displacement. For the purpose of design, acceleration spectra are very useful, as they give the seismic force on a structure directly by multiplying it with the generalized or modal mass of the structure.

## A-2. AVERAGE SPECTRA

A-2.1 Prof G. W. Housner has proposed average spectra on the basis of studies on response spectra of four strongest earthquakes that have occurred in USA (see Fig. 15 which shows the average acceleration spectra).

A-2.2 To take into account the seismicity of the various zones, the ordinates of the average spectra are to be multiplied by a factor  $F$ . This factor  $F$  depends on the magnitude, duration and form of the expected earthquake, distance of the site from expected epicentre, soil conditions, resistance deformation characteristics of the structure, etc. For elastic design with permissible increase in stresses as given in 5.2, the approximate values of this factor for the seismic zones of India are given below:

| Zone | F Value |
|------|---------|
| V    | 0.7     |
| IV   | 0.4     |
| III  | 0.3     |
| II   | 0.2     |
| I    | 0.1     |

NOTE 1—It may be pointed out that during the expected maximum intensity of earthquakes in the

various seismic zones, structures will be subjected to a bigger force. But the capacity of the structure in plastic range will be available for resisting such forces. If the energy absorption method of design is used, these values will have to be multiplied by 3 to 6 in order to obtain the appropriate design factors for the expected earthquake.

NOTE 2—The values of  $F$  shall be multiplied by 1.5 for structures mentioned in 5.3.1 for elastic design. For inelastic design, the multiplier (3 to 6) takes the importance of the structure into account. For very important structures, however, it would be preferable to determine this factor more precisely.

## A-3. DAMPING IN STRUCTURES

A-3.1 The variety of damping displayed in different types of structures has made the choice of a suitable damping coefficient for a given structure largely a matter of judgement. However, some values are given below to indicate the order of damping coefficient in various types of structures:

| Type of Structure                    | Damping Coefficient in Percent of Critical |
|--------------------------------------|--|
| a) Steel structures                  | 2 to 5                                     |
| b) Concrete structures               | 5 to 10                                    |
| c) Brick structures in cement mortar | 5 to 10                                    |
| d) Timber structures                 | 2 to 5                                     |
| e) Earthen structures                | 10 to 30                                   |

NOTE—It may be mentioned here that in the elastic range, damping displayed by structures is much lower than that given above. It may lie between 1 and 4 percent for the above type of structures at low stresses. The values given thus presume some inelastic deformations or fine cracking to take place when this order of damping will occur.

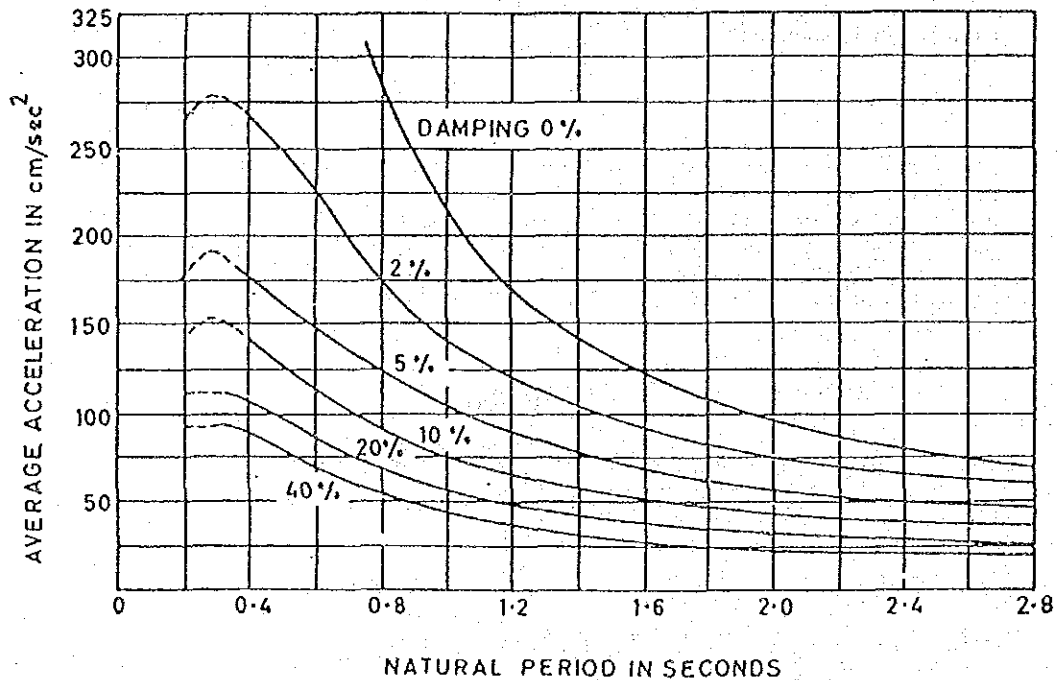


Fig. 15 Average Acceleration Spectra

#### A-4. METHOD OF USING THE SPECTRA

A-4.1 Let the period of a structure be 0.8 second and the damping 5 percent critical. Referring to Fig. 15, the spectral acceleration,

$S_a$  is 125 cm/sec<sup>2</sup>. If the structure has mass  $M = 12.0$  kg/sec<sup>2</sup>/cm and is to be located in zone V, the acceleration to be used for design would be  $0.7 \times 125 = 87.5$  cm/sec<sup>2</sup>, and the seismic force  $P$  would be given by  $P = 87.5 \times 12 = 1050$  kg.

### APPENDIX B

(Clause 5.3.3)

#### SEISMIC COEFFICIENTS FOR SOME IMPORTANT TOWNS

| TOWN        | ZONE | HORIZONTAL SEISMIC COEFFICIENT<br>$a_h$ | TOWN              | ZONE | HORIZONTAL SEISMIC COEFFICIENT<br>$a_h$ |
|-------------|------|---|-------------------|------|---|
| Agra        | III  | 0.04                                    | Jabalpur          | III  | 0.04                                    |
| Ahmadabad   | III  | 0.04                                    | Kanpur            | III  | 0.04                                    |
| Ajmer       | I    | 0.01                                    | Katmandu          | V    | 0.08                                    |
| Allahabad   | II   | 0.02                                    | Kohima            | V    | 0.08                                    |
| Almora      | IV   | 0.05                                    | Kurnool           | I    | 0.01                                    |
| Ambala      | IV   | 0.05                                    | Lucknow           | III  | 0.04                                    |
| Amritsar    | IV   | 0.05                                    | Ludhiana          | IV   | 0.05                                    |
| Asansol     | III  | 0.04                                    | Madras            | II   | 0.02                                    |
| Aurangabad  | I    | 0.01                                    | Madurai           | II   | 0.02                                    |
| Bahraich    | IV   | 0.05                                    | Mandi             | V    | 0.08                                    |
| Bangalore   | I    | 0.01                                    | Mangalore         | III  | 0.04                                    |
| Barauni     | IV   | 0.05                                    | Monghyr           | IV   | 0.05                                    |
| Barilly     | III  | 0.04                                    | Moradabad         | IV   | 0.05                                    |
| Baroda      | III  | 0.04                                    | Myost             | I    | 0.01                                    |
| Bhatinda    | III  | 0.04                                    | Nagpur            | II   | 0.02                                    |
| Bhilai      | I    | 0.01                                    | Nainital          | IV   | 0.05                                    |
| Bhopal      | II   | 0.02                                    | Nasik             | III  | 0.04                                    |
| Bhubaneswar | III  | 0.04                                    | Nellore           | II   | 0.02                                    |
| Bhuj        | V    | 0.08                                    | Panjim            | III  | 0.04                                    |
| Bikaner     | III  | 0.04                                    | Patiala           | III  | 0.04                                    |
| Bokaro      | III  | 0.04                                    | Patna             | IV   | 0.05                                    |
| Bombay      | III  | 0.04                                    | Pilibhit          | IV   | 0.05                                    |
| Burdwan     | III  | 0.04                                    | Pondicherry       | II   | 0.02                                    |
| Calcutta    | III  | 0.04                                    | Poona             | III  | 0.04                                    |
| Calicut     | III  | 0.04                                    | Raipur            | I    | 0.01                                    |
| Chandigarh  | IV   | 0.05                                    | Rajkot            | III  | 0.04                                    |
| Chitradurga | I    | 0.01                                    | Ranchi            | II   | 0.02                                    |
| Coimbatore  | III  | 0.04                                    | Roorkee           | IV   | 0.05                                    |
| Cuttack     | III  | 0.04                                    | Raurkela          | I    | 0.01                                    |
| Darbhanga   | V    | 0.08                                    | Sadiya            | V    | 0.08                                    |
| Darjeeling  | IV   | 0.05                                    | Simla             | IV   | 0.05                                    |
| Dehra Dun   | IV   | 0.05                                    | Sironj            | I    | 0.01                                    |
| Delhi       | IV   | 0.05                                    | Srinagar          | V    | 0.08                                    |
| Durgapur    | III  | 0.04                                    | Surat             | III  | 0.04                                    |
| Gangtok     | IV   | 0.05                                    | Tezpur            | V    | 0.08                                    |
| Gauhati     | V    | 0.08                                    | Thanjavur         | II   | 0.02                                    |
| Gaya        | III  | 0.04                                    | Tiruchchirappalli | II   | 0.02                                    |
| Gorakhpur   | IV   | 0.05                                    | Trivandrum        | III  | 0.04                                    |
| Hyderabad   | I    | 0.01                                    | Udaipur           | II   | 0.02                                    |
| Imphal      | V    | 0.08                                    | Varanasi          | III  | 0.04                                    |
| Jaipur      | II   | 0.02                                    | Vijayawada        | III  | 0.04                                    |
| Jamshedpur  | II   | 0.02                                    | Vishakhapatnam    | II   | 0.02                                    |
| Jhansi      | I    | 0.01                                    |                   |      |   |
| Jodhpur     | I    | 0.01                                    |                   |      |   |
| Jorhat      | V    | 0.08                                    |                   |      |   |

NOTE—The coefficients given are according to 5.2.1 and should be suitably modified for important structures according to 5.2.2 and 5.4.



#### 4.5 Estimated Power Demand

##### Designed Power Capacity

|  |   |          |
|--|---|----------|
| Terminal building  | $2,025 \text{ m}^2 \times 0.035 \text{ kW/m}^2 =$ | 710 kW   |
| Other buildings  | $1,034 \text{ m}^2 \times 0.02 \text{ kW/m}^2 =$  | 20.7 kW  |
| Water Supply & drainage equipment<br>(incl. bus washing equipment) |   | 32.5 kW  |
| Outside lighting   |   | 48.5 kW  |
| Total  |   | 172.7 kW |

##### Estimated monthly average power usage

|                                   |   |            |
|-----------------------------------|---|------------|
| Terminal building                 | $71.0 \text{ kW} \times 0.45 \times 18 \text{ H/D} \times 30 \text{ D} =$ | 17,250 kWh |
| Other buildings                   | $20.7 \text{ kW} \times 0.14 \times 18 \text{ H/D} \times 30 \text{ D} =$ | 1,560 kWh  |
| Water Supply & drainage equipment | $32.5 \text{ kW} \times 0.2 \times 18 \text{ H/D} \times 30 \text{ D} =$  | 3,510 kWh  |
| Outside lighting                  | $48.5 \text{ kW} \times 1.0 \times 6 \text{ H/D} \times 30 \text{ D} =$   | 8,730 kWh  |
| Total                             |   | 31,050 kWh |

#### 4.6 List of Other Data

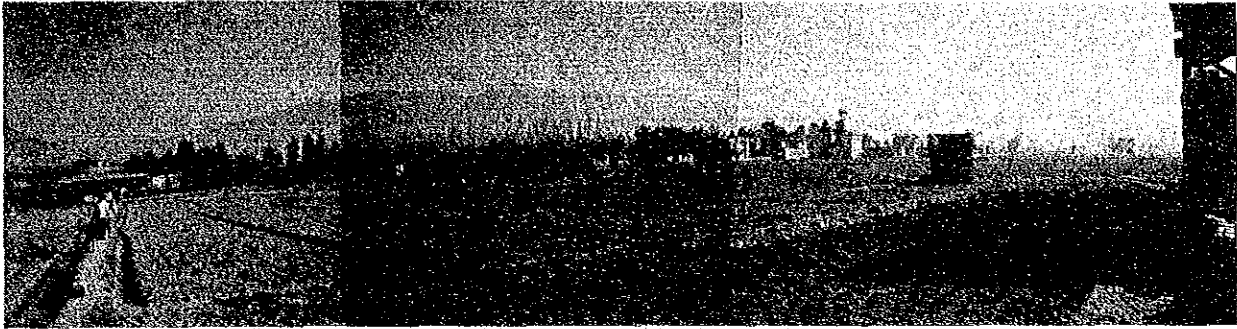
- The Seventh Plan 1985-1990  
(A Summary) Part I  
National Planning Commission
- Climatological Records of Nepal  
1985-1986  
Min. of Water Resources,  
Dep. of Hydrology and  
Meteorology
- Surface Water Records of Nepal  
Supplement No.11, 1976  
Dep. of Irrigation,  
Hydrology and Meteorology
- Statistical Year Book of Nepal 1987  
National Planning Commi-  
ssion,  
Central Bureau of Statistic
  
- Soil Investigation Report for  
Proposed Site (Samakhusi District)  
KNP - Nissaku Co.
- Topographical Survey Map for  
Proposed Site (Samakhusi District)  
KNP - Creative Designer,  
Co.
- Soil Investigation Report for  
No.8 Site  
Nissaku Co.
- Topographical Survey Map for No.8  
Site  
Creative Designer, Co.
  
- Standard Drawings  
Urban Roads and Drains  
Min. of Housing & Physical  
Planning  
Min. of Panchayat & Local  
Development
- Nepal Road Standards - 2045  
Min. of Works and Transport  
Dep. of Roads
- Urban Roads Standards  
Management Support for Town  
Panchayat Project

● Preliminary Drawings  
(Existing 1987)

Min. of Public Works &  
Transport  
Min. of Panchayat & Local  
Development

- |  |               |
|--|---------------|
| - Kathmandu-Lalitpur Road, and Drain                                     | DWG No. F-119 |
| - Kathmandu-Lalitpur Water Supply Reticulation Network                   | DWG No. F-120 |
| - Kathmandu-Lalitpur Service Public Transports Street Lighting & Markets | DWG No. F-121 |
| - Kathmandu-Lalitpur Sewerage & Solid Waste Existing Network             | DWG No. F-122 |

#### 4.7 Photographs



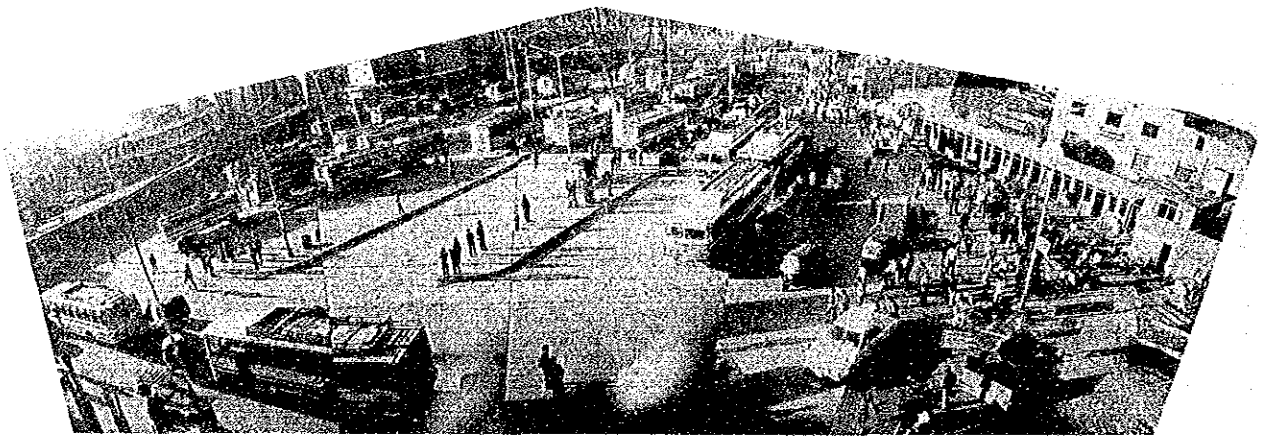
Proposed Bus Terminal Site (Distant View of Ring Road)



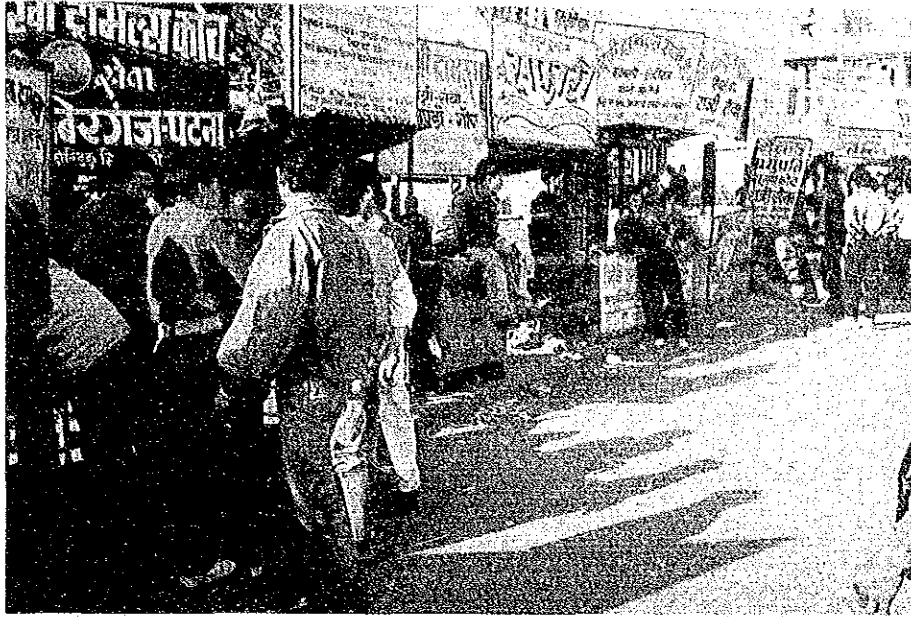
Proposed Bus Terminal Site  
(View from the Vishumati River/Ring Road Bridge)



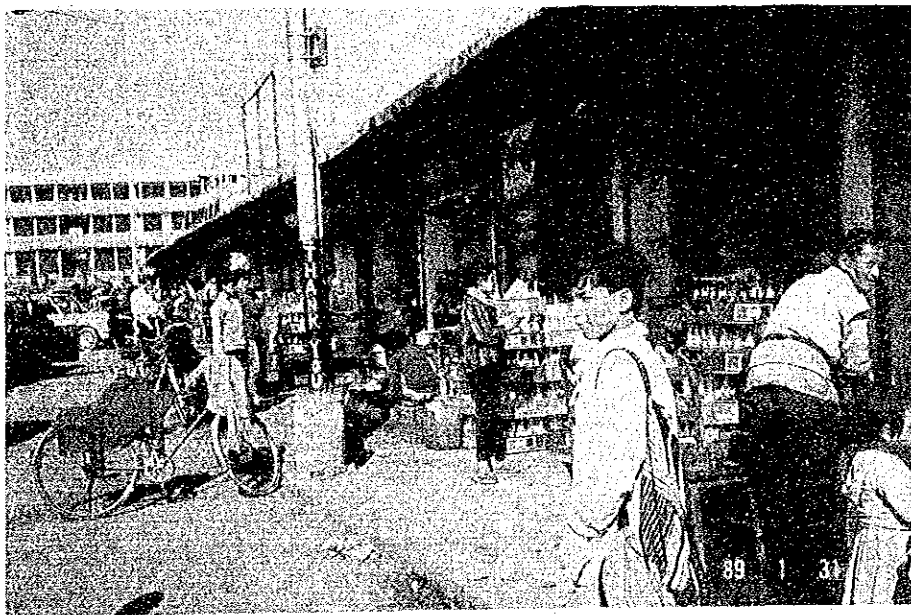
Existing Bus Terminal PM 4:50



Existing Bus Terminal AM 8:00  
(Holiday)



Existing Bus Terminal (Temporary Ticket Stand)



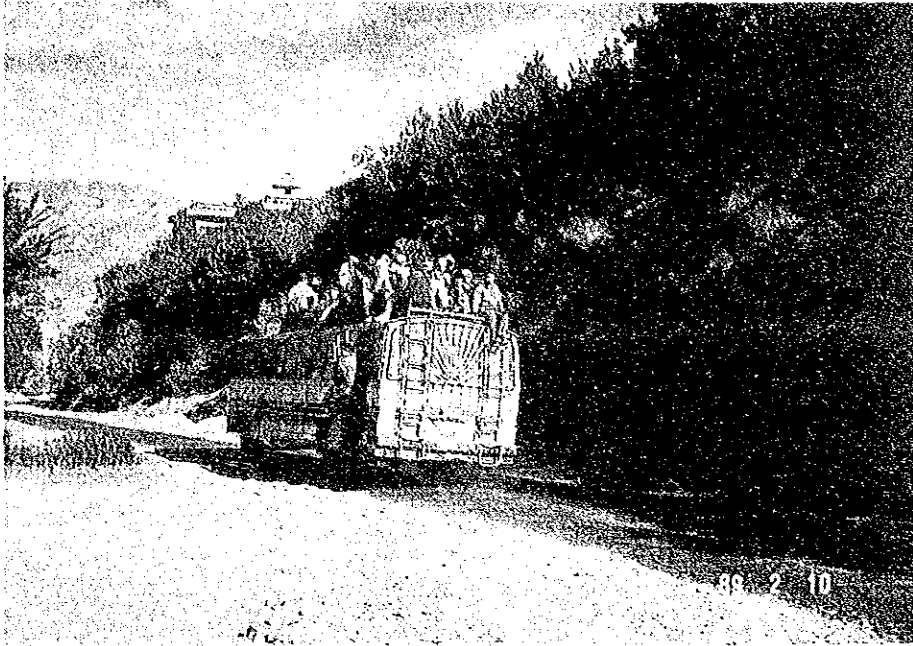
Existing Bus Terminal (Shop and Eating House)



Existing Bus Terminal (Baggage Loading/Unloading)



Existing Bus Terminal (Baggage Loading/Unloading)



Running Bus



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