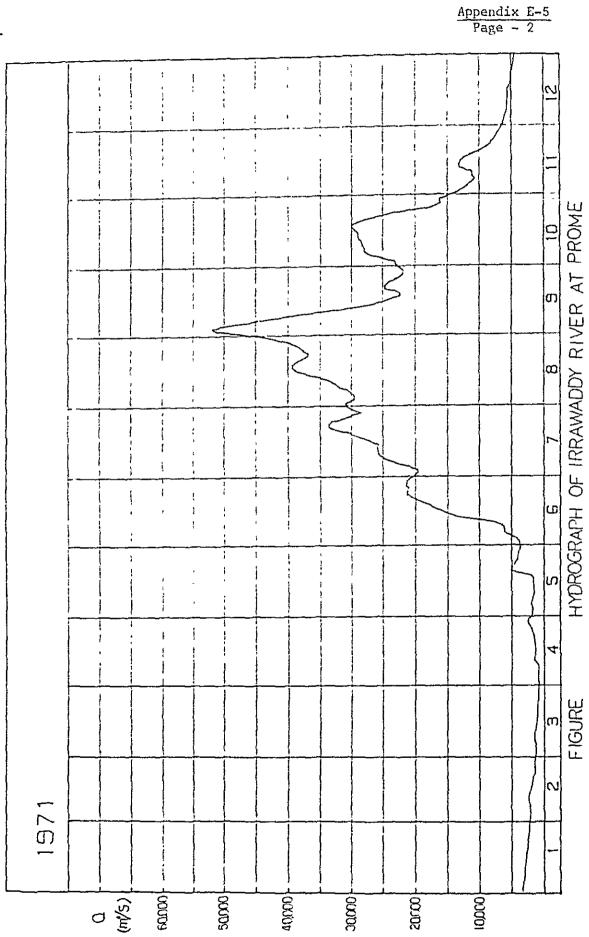
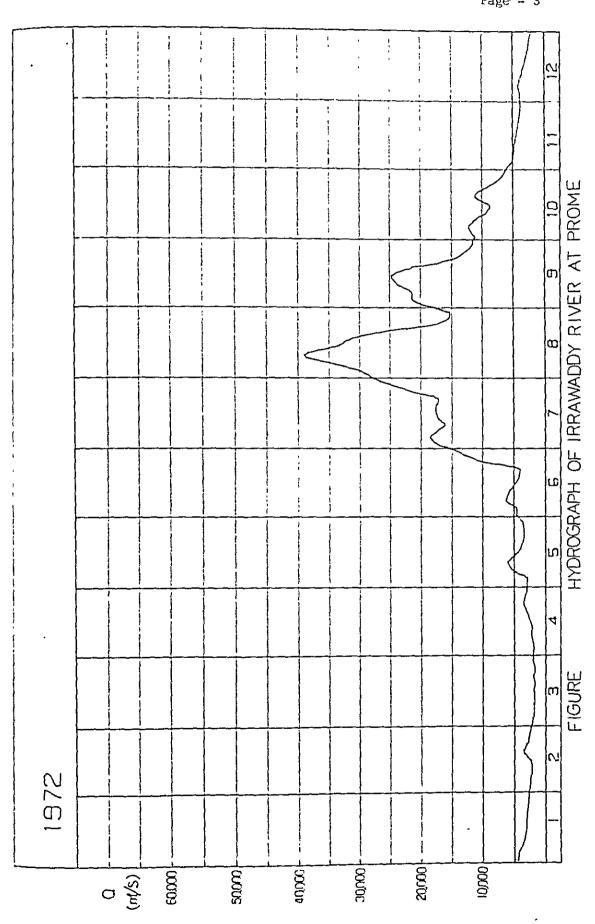
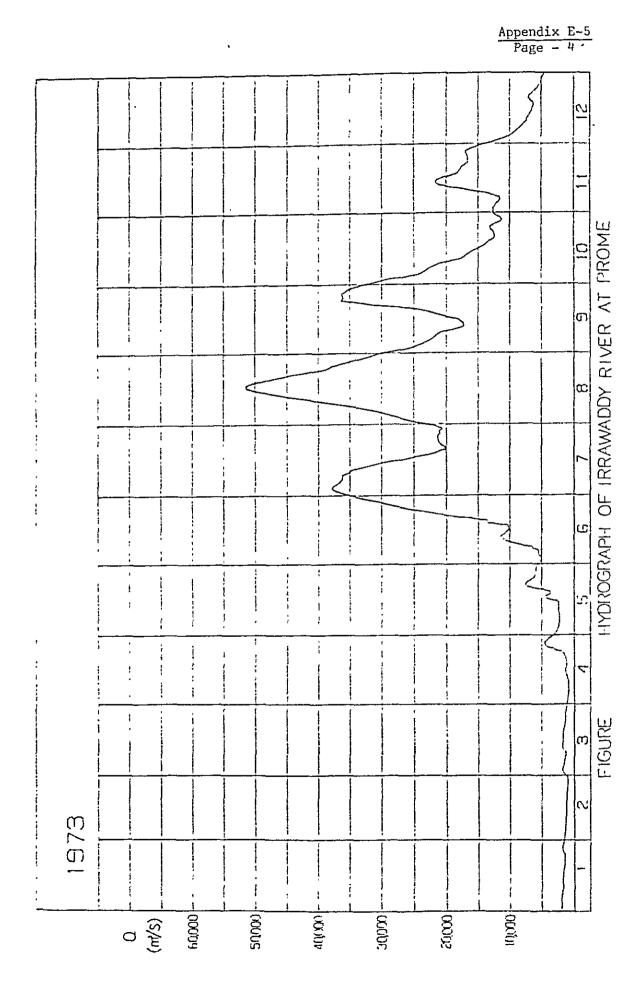


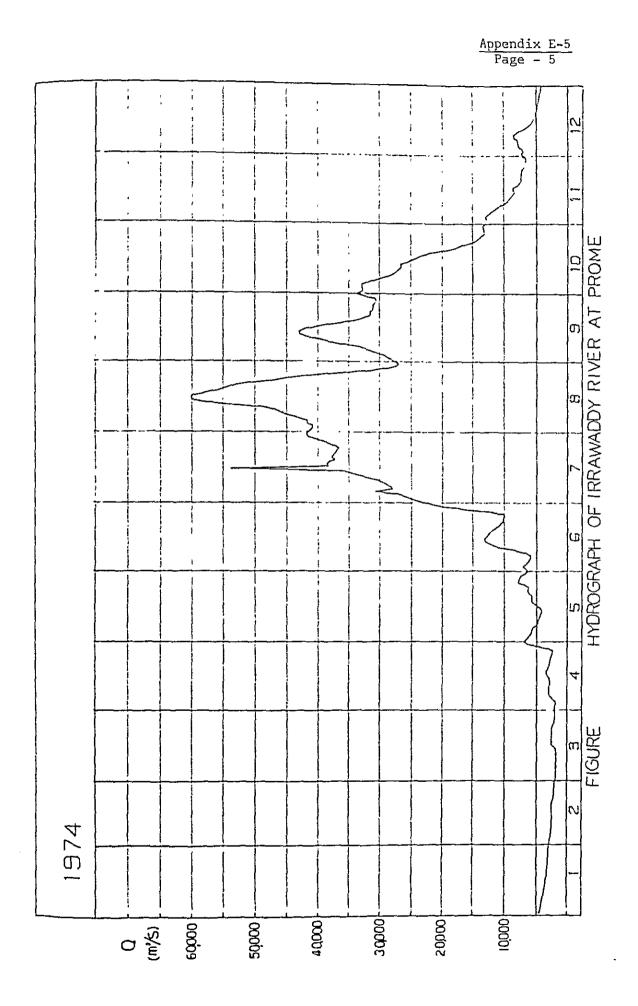
APPENDIX E-5 HYDROGRAPH OF IRRAWADDY RIVER AT PROM (1970-1977)



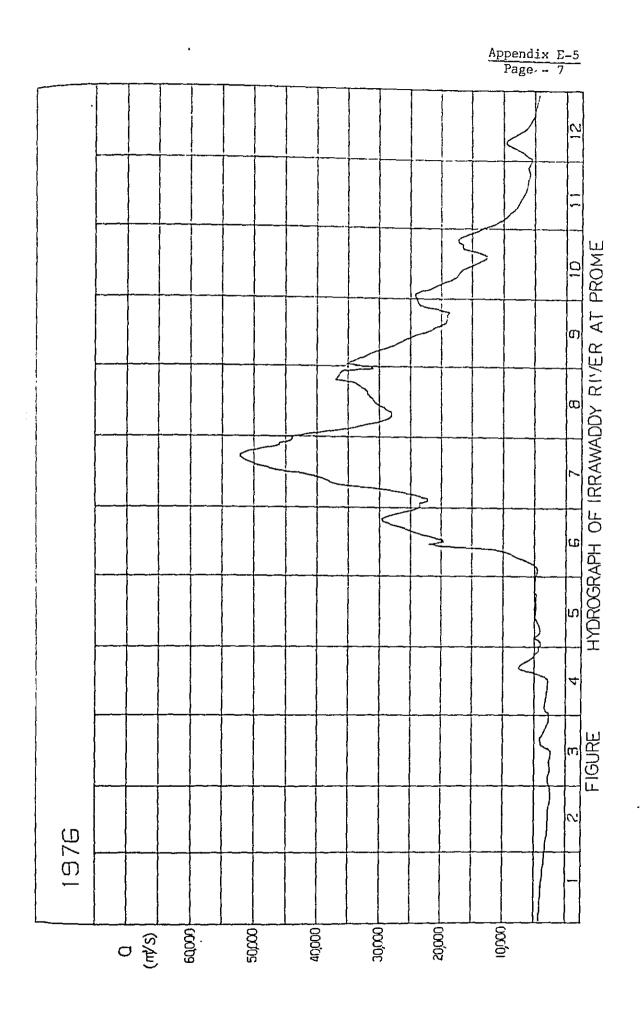


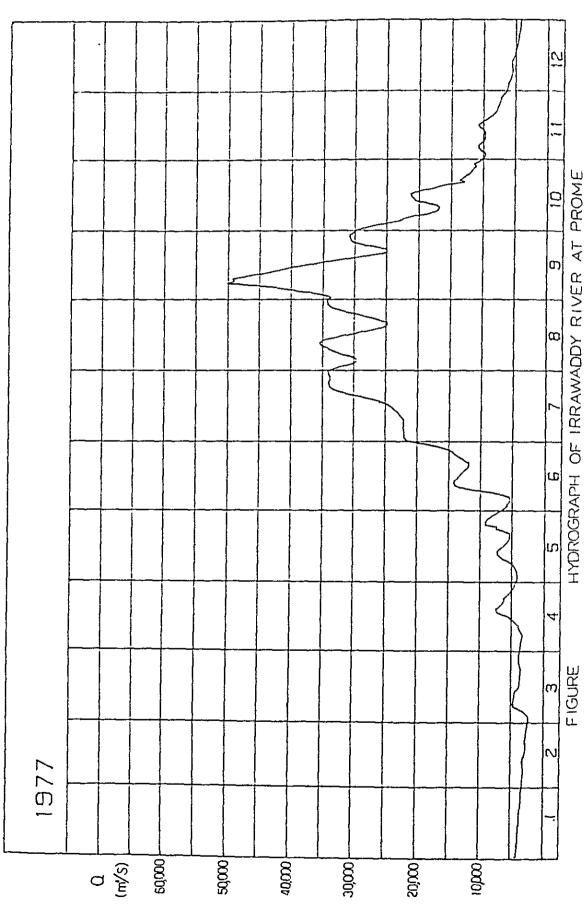
Appendix E-5 Page - 3



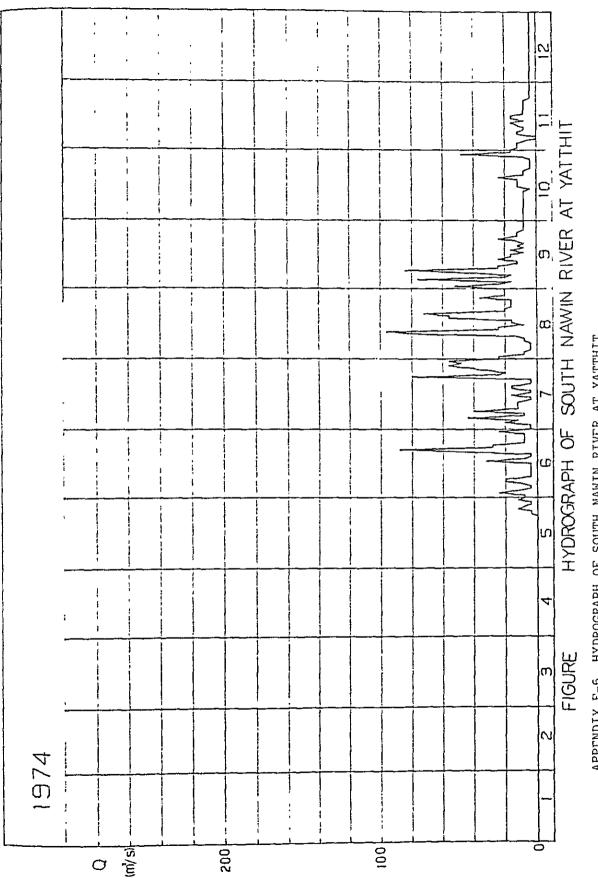


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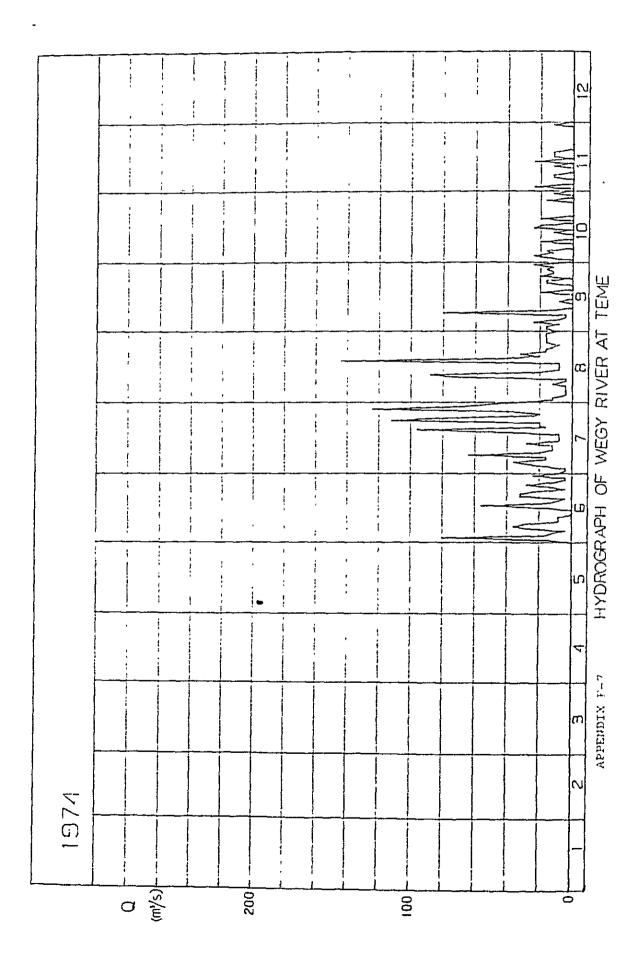


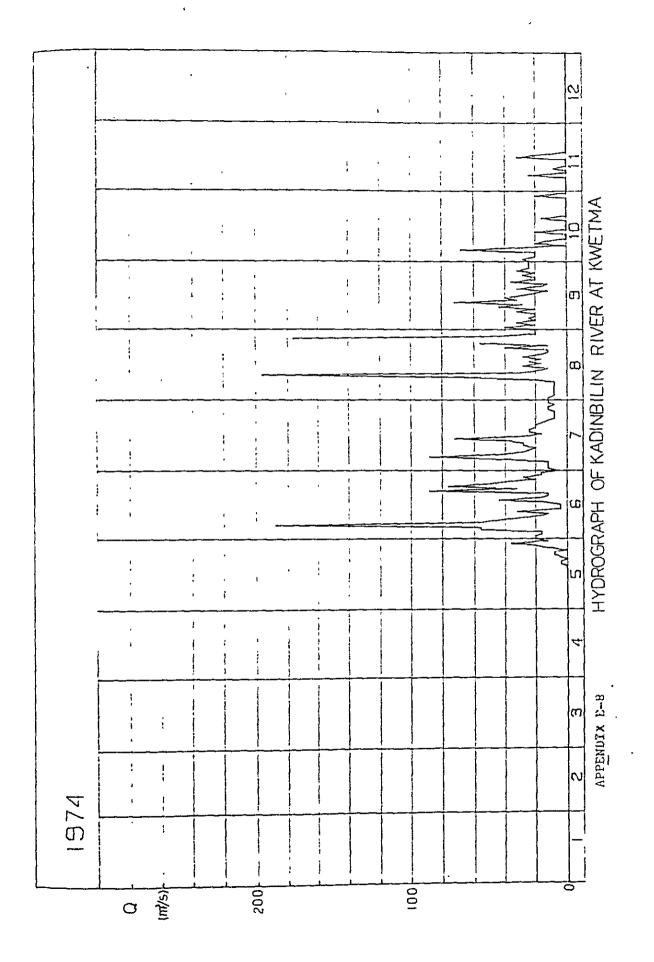


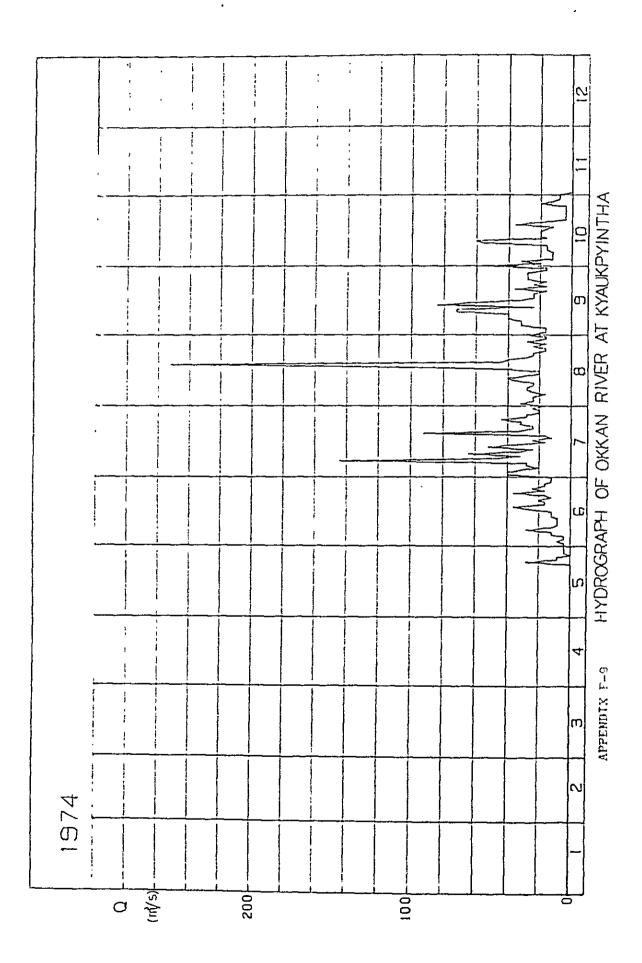
Appendix E-5 Page - 8



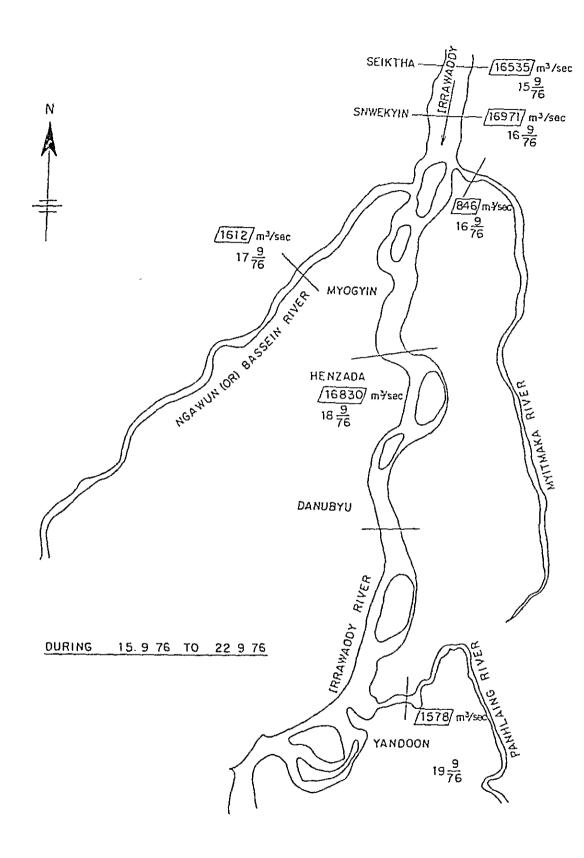


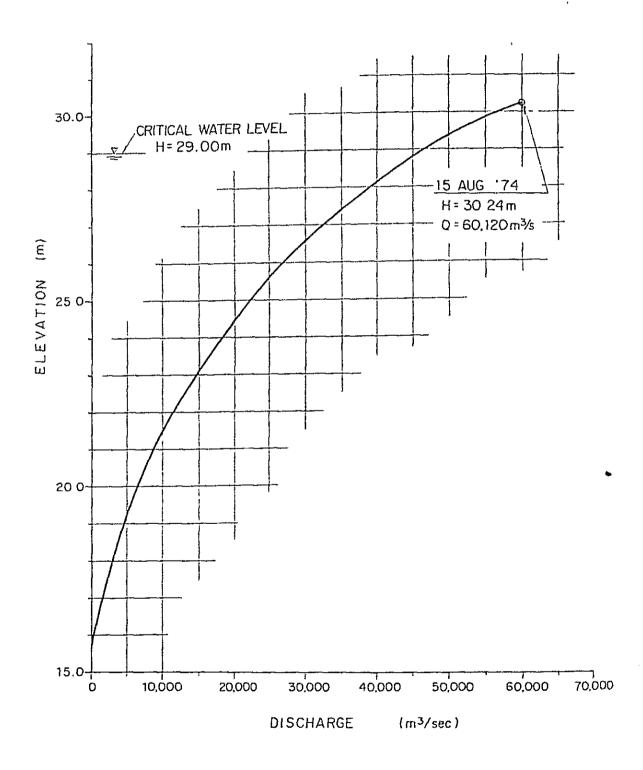




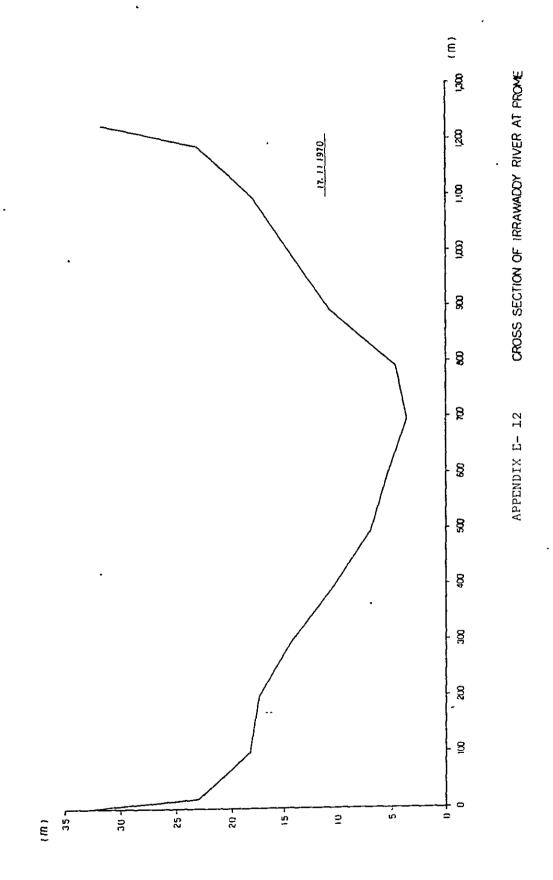


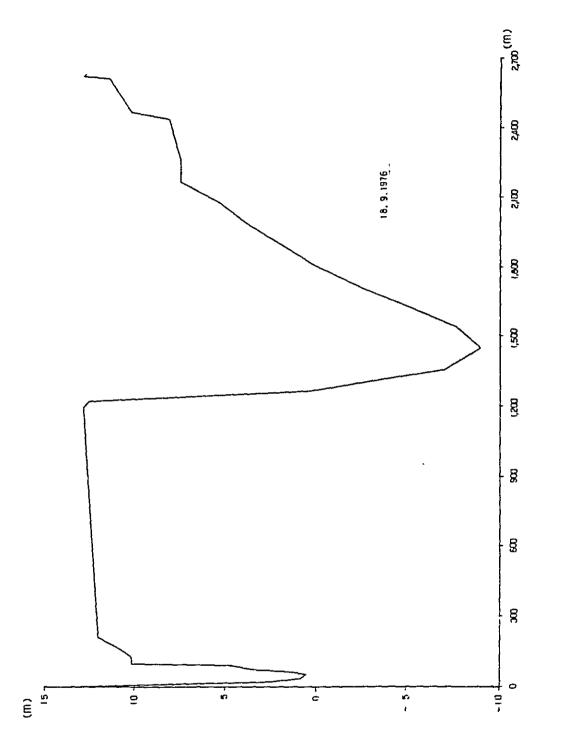
APPENDIX E-10 DISTRIBUTION OF DISCHARGE OF IRRAWADDY RIVER





APPENDIX E-11 RATING CURVE OF IRRAWADDY RIVER AT PROME





APPENDIX E-13 CROSS SECTION OF IRRAWADDY RIVER AT HENZADA

APPENDIX E-14	SUCCESSIVE	RAINFALL	(THARRAWADDY,	PROME.	HENZADA)
			· · · · · · · · · · · · · · · · · · ·		

1			
(Un	1t	: mm	}

					(0	MIC: MODY
		Maximum			Maximum	<u>. </u>
Year	Tharrawaddy	Prome	Henzada	Tharrawaddy	Prome	Henzada
1947	115.32	47.75	-	132.84	66,29	-
40	121.41	65.79	83.82	151.13	151.41	119.13
49	-	-	-	-	-	-
1950	92.96	-	84.07	111.00	-	111.76
51	106.43	116.08	114.55	161.29	124.97	167.64
52	101.60	98.04	134.37	152.91	130.81	144.27
53	94.49	138.68	99.06	152,40	148.59	168.66
54	117.86	117.86	-	142.75	120.14	-
55	92.96	95.25	154.94	113.79	95.50	187.96
56	83.06	84.58	104.14	134.37	113.28	123.95
57	104.65	60.45	-	171.96	111.51	-
58	98.55	61.98	84.84	130.30	76.96	115.06
59	86.87	55.88	91.69	128.52	100.08	174.75
1960	197.10	83.82	88.14	210.82	198.20	129.29
61	150.37	112.52	231.65	174.75	135.89	278.64
62	127.25	107.95	127.76	161.29	178.05	162.56
63	122.68	68.83	118.11	186.18	91.69	199.39
64	109.73	84.58	121.92	127.51	113.28	204.47
65	93.98	99.06		120.40	157.99	-
66	71.88	62.99	82.80	112.27	66.55	116.33
67	-	62.99	_		84.07	_
68	118.62	64.01	98.04	143.00	89.15	130.05
69	69.85	115.06	152.40	107.95	150.11	168.15
1970	205.99	59.94	95.00	249.94	71.88	127.00
1970 71	78.00	93.00	90.00	143.00	178.00	160.00
71 72	84.00	56.00	80.00	117.00	66.00	105.00
72	246.00	126.00	139.00	297.00	165.00	202.00
	120.00	131.00	76.00		176.00	112.00
74	188.00	120.00	96.00		128.00	106.00
75		107.00	155.00		136.00	240.00
76	185.00	61,00	96.00		73.00	148.00
77	112.00	01,00	30.00	100.00		

Note:-No Data

SUCCESSIVE RAINFALL (THARRAWADDY, PROME, HENZADA)

(Unit: mm)	: mm)
------------	-------

	3 dav	Maximum		6 day	Maximum	
Year	Tharrawaddy	Prome	Henzada	Tharrawaddy	Prome	Henzada
	Indifiandudy		·		-	
1947	146.30	86.36	~	223.77	126.24	-
48	159.26	120.40	152.91	277.62	151.89	263.14
49	-	-	~	-	-	-
10						
1950	119.38	-	140.21	200.15	-	196.34
51	198.37	139.70	222.25	335.03	230.89	355.35
52	179.32	130.81	155.19	228.35	169.16	219.46
53	152.91	154.43	196.85	213.36	180.85	236.22
54	165.61	123.70		266.95	208.53	-
55	125.73	108.20	187.96	164.59	148.08	197.61
56	168.15	137.16	160.02	227.33	186.69	234.95
57	220.98	153.16		288.54	195.33	-
58	159.77	92.46	134.62	206.76	126.49	180.34
59	166.37	102.36	226.82	212.85	125.48	309.37
					_	
1960	223.77	181.10	169.67	272.03	206.50	207.77
61	180.59	143.76	300.99	232.66	177.55	354.33
62	180.85	196.60	180.09	235.20	245.36	274.32
63	227.84	126.49	250.19	291.85	151.13	336.55
64	141.99	137.16	249.43	150.62	186.69	328.42
65	155.19	159.77	-	233.68	180.34	-
66	141.73	87.12	134.62	246.63	112.78	220.22
67	-	93.98	-	-	112.17	-
68	178.05	92.20	176.53	254.51	117.35	304.29
69	124.46	221.23	170.94	181.36	316.23	234.95
1970	288.04	105.93	144.02	359.16	124.97	233.93
71	207.00	198.00	226.00	254.00	232.00	334.00
72	153.00	68.00	167.00	182.00	104.00	228.00
73	343.00	185.00	251.00	371.00	209.00	322.00
74	154.00	202.00	137.00	269.00	221.00	241.00
75	241.00	130.00	172.00	246.00	160.00	247.00
76	291.00	142.00	263.00	319.00	151.00	273.00
77	153.00	86.00	171.00	212.00	127.00	297.00

Note:-No Data

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APPENDIX E-15 PROBABILITY ANALYSIS OF THE MAXIMUM WATER LEVEL AT PROME

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		(**X	27653-16	26013-24	25855.54	24.01162	24830-42	24642.24	24540.68	23867.84	23664 59	23664.59	23295.63	22617.16	22473.48	22140.66	22046.20	21904.98	21811.15	21787.75	21207.91	20910.48	20638.44	516712.75 23486.94	
****		X++2	914-46	877-94	814.38	10°7/8	850.89	846-81	846.48	829.44	824.26	824.26	815-67	799.76	796-37	168.49	786.24	182.88	780.64	780.08	766.18	159-00	752.40	18030.41 819.56	
PROJECT **	-	HAZEN PLOTIZI	61-13	93.18	86.64 94.00	70.55	75.00	70.45	65.91	61.36	56.82	52.27	41.73	43.18	38.64	34.09	29.55	25.00	20.45	15.91	11.36	6+82	2.27		
DDY 4/P	Ŧ	THOMAS PLOT(I)	95.65	91.30	80°96 83 £1	78-26	13.91	69-57	65.22	60-87	56.52	52.17	47.83	43-48	39-13	34.78	30.43	26.09	21-74	17.39	13.04	8-70	4 • 35	нүү	
I RK AWADDY	UNIT= 1	74 = 74 =	2-19212	201020102	2-16340	2-15517	2.14604	2.14298	2.14123	2.12982	2.12586	2.12586	2.11923	2.10679	2.10411	2.09785	2.09606	2.09337	2-09157	2.09112	2.07984	2-07395	2.06849	46.67287 2.12149 =	
EEDANCE DN	PROME	Y = LOG(X+B)	1.48058	1.411/3	12072-1	1-46805	1-46494	£.46389	1.46329	1.45939	1.45803	1.45803	1.45576	1.45148	1-45056	1-44840	1-44778	l.44685	1.44623	. 1.44607	1-44217	1.44012	1.43823	32.04272 1.45649	0.75390
PROHABILITY OF EXCEEDANCE	XIMUM WATER LEVEL AT	8+X	30.240	20.5305	29.540	29.380	29.170	29.100	29.060	28.800	28.710	28.710	28.560	28.280	28.220	28.080	28.040	27.980	27。940	27-930	27.680	27.550	27.430		= <[6++X2]/[
	NAXIMUN NAI	(X) 90 T	1.48058	1-4-113	1-47041	1.46805	1-46494	l.46389	1.46329	1.45939	1-45803	1-45803	1-45576	1.45148	1.45056	1-44840	1.44778	1.44685	1-44623	1-44607	1.44217	1.44012	1.43823	629.598 32.04272 28.618 1.45649 YH PODIC(28.619 1.111.42004.001000)	= !!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!</td
***** THE	i	×	30°240	79.570	29.540	29.380	29.170	29.100	29-060	28.800	28.710	28.710	28.560	28.280	28.220	28.080	28.040	21.980	21-940	21.930	21.640		21.430	629.598 28.618 2017/128.014	KUUT < XXH-XH+XH+ZH XXXH-3+XXH+XH+Z
		YEAR	1974	9161	1471	1977	1968	0/61	8561	1956	1461	4 C F T	1963	1961	2961	5961 2962	1969	51.61	7761	1413	1 404	1061	1 400	9 W	
		QRDER		1 11	r 1	ŝ	. 0	~ ·	að (- s	2:		21	2:		<u>.</u>	<u>o</u> <u>f</u>				2 4	• •	22	TOTAL Méan	

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	1 ++++	ТНЕ РАСНАНІСІТУ	ŋΕ	EXCEEDANCE ON	[HRAWADDY	4/H	PROJECT	* * * *
	 ×	МАХІНИН НА	MATER LEVEL AT	T PHOME UNIT	1 • 1	x	-	
		***	63 – V A	L U E ***	:			
дарея 1 2	x1 30_240 29.630	xs 21+430 21+550	x I a x S 8 2 9 4 4 8 3 8 1 6 4 3 0 6	x[*X5-X0*2 57.610 57.6180	-2-107 -2-107	2 * X0-(X1 + X5 -0,454 0,036 T0TAL B1 MEAN B = MEAN B =	- 1	61 -24-375 -58-776 -83-151 -41-575 0-0
	***	THE PROBA	PROBABLE VALUES E	BY TINAL'	HETHOD ++	*		
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2	0	0.01	۱ 0	1.4		0*0	28.60	8
ri -	m	10-0	· · ·	1.4	.	0.0	28.9	4
4 V	2 + "O	769 0.017 951 0.017		1-4647	29.151 20.288		29.151	- 5
· • 0	۰	10.0		1.4	: .:	0.0	29.3	
7	~	10-01	۰. ۱	-	÷.	0.0	29.47	
¢Ç I	•	Ó			÷.	0.0	24° 27	
с с -	∞ c	10.0	••			0.0	5 ° C C	0
22	~ 0						9.4.0	7.4
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13	0	10-01	.0.1	_	÷	0-0	29.70	69
14		10-0				0-0	29 - B(22
15	••	0-01	•••	. .	÷.	0.0	29-8	32
202	1.15		• •				10.05	
30	• ~	0.0				0	0.0	201
35	7	0.01	ò	-		0.0	30.1	58
40	1.38	0.01	ō	-	ō.	0-0	30.2	16
45	1-42	10*0	ċ	-	ċ.	0,0	30+2	58
50	3	0-01	•		ċ.	0.0	. 30.2	95
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200	1.82		0.031		30"740	0.0	30.	
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300	1-91	10.01	1 0-03	1.4894	0.85	0.0	m	58

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APPENDIX E-16 PROBABILITY ANALYSIS OF DAILY MAXIMUM RAINFALL AT THARRAWADDY

PROJECT ***** THE PROBABILITY OF EXCEEDANCE ON IRRAWADDY M/P

	С # 6 X .	14886936.00 8741046.00 6331625.00 6331625.00 5399898.00 3399898.00 1789717.00 178970.00 178970.00 178970.00 178980.00 1789717.00 166020.00 1532402.00 1532402.00 154662.00 154662.00 154662.00 1648771.00 957184.81 843555.00 1648771.00 957184.81 843555.00 957194.00 174555.00 3714155.25 855599.50 3714155.25 87288.00 3714155.25 87288.00 3714155.25 87288.00 3714155.25 87288.00 3714155.25 87288.00 3714155.25 855509.50 957794.00 174552.00 3714155.25 855509.50 957794.00 174552.00 3714155.25 855509.50 957794.00 174552.00 3714155.25 855509.50 957794.00 174552.00 3714155.25 855509.00 174552.00 3714155.25 855509.00 174552.00 3714155.25 855509.00 174552.00 3714155.25 855509.00 174552.00 2557507.00 2557507.00	
-	Z++X	60516.00 353449.97 353449.97 353449.97 353449.97 35255.00 22610.52 15050.00 147400.00 147400.00 14400.00 14400.00 14400.00 14400.00 14400.00 14400.00 14400.00 15565.00 12544.23 86422.33 86422.33 86422.33 86422.33 113265.00 15565.00 15546.000 15546.00000000000000000000000000000000000	
UNIT-1 M M	HALEN PLUT(X)	4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	
	THUMAS PLOT(%)	7 7 7 7 7 7 7 7 7 7 7 7 7 7	
DAILY MAXIMUM RAINFALL AT THARRAWADDY	Z¢¢} ₹¢¢}	$\begin{array}{c} \bullet & \bullet $	
MUM RAINF	18+x1901 = 1	2.30499 2.10499 2.104904 2.104904 2.104904 2.104904 2.104904 2.104904 1.48714 1.48714 1.48714 1.48714 1.48714 1.48715 1.49148 1.1956944 1.195694 1.195694 1.1956944 1.195694 1.195694 1.195694 1	
AILY MAXI	81 + X	<pre>2.37491 201.021 2.27440 1152.044 2.27440 1152.044 2.27440 1152.043 2.10461 1152.043 2.10461 1152.043 2.10461 1152.043 2.10461 1152.043 2.004820 1154.043 2.004820 1154.043 2.00480 1155.043 1.00480 1155.04480 1155.04480 1.00480 1155.04480 1155</pre>	
	(X) 90 T	Z-29449 Z-29449 Z-29449 Z-29449 Z-29449 Z-1716 Z-29449 Z-1716 Z-104194 Z-1716 Z-104194	
×	×	246-000 136-000 136-000 136-000 136-000 126-359 126-359 126-359 126-359 126-359 126-359 126-359 126-359 126-359 126-596 126-59	
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BI -47.260 -35.483 -49.765 -132.508 -44.169 -44.169 PROJECT ***** 110.876 147.420 173.909 216.979 2261.326 231.847 2561.326 341.298 341.298 341.298 X=C-B 2+XU-[X]+XS] -87.322 -49.348 -44.576 10fal bf HEAN b = HEAN b = -44.169 -44.169 -44.169 -44.169 -44.169 -44.169 -44.169 -44.169 -44.169 Ð ***** DAILY MAXIMUM RAINFALL AT THARRAWADDY ***** THE PROBABILITY OF EXCEEDANCE ON IRRAWADDY M/P x1+x5 4126-448 1751.004 2317-059 66.706 103.250 1129.740 172.807 193.67 193.67 193.67 254.056 254.056 254.056 254.156 254.126 C=10++A THF PRUBABLE VALUES BY 'IWAI' HETHUD **** x1•x5-x4•*2 315-850 211-816 215-860 1.8444 2.0139 2.1131 2.2376 2.2376 2.52871 2.4049 2.4729 2.4729 2.5208 A*74+E*R א - אארטנ 0.0 0.1897 0.4847 0.4624 0.4624 0.5244 0.5244 0.5248 0.5448 x[•x5 17183.094 14801.250 19374.105 £ • K 0.3188 0.3188 0.3188 0.3188 0.3188 0.3188 0.3188 0.3188 ¥ ***** x5 49.85U 11.882 u.v u.s951 u.s952 t.s950 t.6450 t.6450 č.035u č.035u č.035u ÷ •••• × , x1 246.UUU 205.494 197.104 REIUKH-PERIOD (YEAR) 2000 2000 2000 2000 2000 2000 2000 Снрен

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Lug(x) Lug(x) 2.10127 2.10127 2.10127 2.10127 2.10127 2.10227 2.00673 2.00673 2.00673 2.00673 2.00673 2.00673 1.12222 1.12222 1.12222 1.12222 1.12222 1.12222 1.12222 1.12222 1.	DAILY MAXIMUM RAINFALL AT PROME	LL AT PROME YY = 2 YY = 2 Y	_	UNIT-L M M I. HALEN PLUITEN 94-128 91-48 91-48 91-48 81-44 8	X**2 X**2 19233.24 17161.00 15876.00 14400.00 13434.09 13239.25 13239.25 11653.19 11653.19 11653.19 11653.19 11653.19 11653.25 11642.65 9012.65	X**3 X**3 2667341-00 2268091.000 2000376-00 1728000-00 1728000-00 1554045-00 1554045-00 1553334-00 1553334-00 1553334-00 155545-00 125563-06
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PRORABILITY ANALISIS OF DAILY MAXIMUM RAINFALL AT PROME ¢ ∆DDENNIY F_17

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PROJECT

***** THE PROBABILITY OF EXCEEDANCE ON IRRAWADDY M/P

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1.4520 0.1808 0.2625 2.2155 164.231 5.296 1.6450 0.1808 0.2974 2.2503 177.970 5.296 1.6450 0.1808 0.2974 2.2503 177.970 5.296 2.0150 0.1808 0.3243 2.22823 191.538 5.296 2.0150 0.1808 0.3649 2.3209 209.40 5.296 2.1450 0.1808 0.3950 2.3460 2.22.828 5.296	0	1.2967	0.1808	0.2344	2.1874	153.950	5.296	148-654
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1.0215 0.1808 0.3243 2.2823 191.538 5.296 2.0350 0.1808 0.3679 2.3209 209.340 5.296 2.1450 0.1808 0.3950 2.3480 222.828 5.296	0	1.6450	0.1908	0.2974	2-2503	177-970	5.296	172 674
2.0150 0.1808 0.3679 2.3209 209.140 5.296 2.1450 0.1808 0.3950 2.3480 222.828 5.296	00	1.0215	0,1808	0:3243	2.2823	191.538	5.296	186-242
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	00	2.1450	0.1808	0<96.0	2.3480	222.828	5-296	217-532

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Appendix E-17 Page - 2

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	2++X	53660-77	24025.00	24006-39	23225.75	19321.00	14054.21	16323.12	14864.48	13949.96	13122.61	10845.13	9812.88	9612.62	9216.00	9216-00	9024-23	8407 . 78	8100.00	7768.30	7197.14	7068-43	7025.79	6856.50	6400-00	5776.00	142879.44 12715.18	
BABILITY OF EXCEEDANCE ON IRRAWADDY MZP PROJECT																											ι.	
PROJECT	HAZEN PLOT(\$)	98.00	44.00	90 . 00	86.00	82-00	18.40	14.00	70-00	66.00	62.00	58.00	54.00	50.00	46.00	42.00	38.00	34.00	30-00	26-00	22-00	18-00	14.00	10.00	6.00	2-00		
a .	THUMAS PLUTITI	96.15	92.31	38.46	44.62	80.17	76.92	13-08	69.23	65.38	61.54	51.69	53.65	50.00	46.15	42.31	38.46	34.02	30.77	26+92	23.08	19.23	15.38	11.54	1.69	3.45	2	-
EXCEEDANCE ON IRRAWADDY M/P	¥Υ = Υ*+Ζ	5.06651	4.02669	4.02565	3.98160	J. /3339	J.64050	3.50076	3.36896	3.27829	£9981°E	2.90663	2.75234	2.71997	2,65316	2.65316	2.01949	2.50434	2.44245	2,3/198	2.24003	2.20819	5+161-2	2.15385	2.02775	1.83077	74.09370	
EDANCE ON MUM RAINFA	Y = LOG{X+8]	2.25089		2,00640	1.44540	1.93220	10806-1	1.87103	1.83547	[.81061	1.18604	1.70488	1.65902	L.64923	1.62885	1.62885	1.61348	1.58251	1.56283	1.54012	1.49667	1.48600	1.48238	1.46/60	1.42399	1.15306	42.68709 1 20324	0.31705
ITY OF EXCEN	¥+¥	1/9.144	101.540	101.485	946.46	85.540	30.912	14.305	6 d •466	64.650	61.100	50.680	45.606	44.590	42.546	42.540	41 = 542	38.240	36.540	34.684	31,382	30.620	30.366	29.350	26.540	22.540	נ ר י	
דאנ האספאסונו דיר סר פאוביצ	(x } 90 J	2.36483	LEU91.5	2.19016	2.18298	2.14301	2.12829	2.10640	2.08607	2.01229	2.05901	2.01762	1.99590	1.99142	1.98227	1.9828	٠.		1.95424	٠,		. .	Ĩ.	v	1.40309	70	5018.04	
. ×	×	231.048	155.000	156.950	152.400	139,000	114-366	127.762	121.920	118.110	114.554	104.140	99.060	98°044	96.000	96.000	94*996	91.694	90.000	٦,	84.836	84.014	83.320	~	5	76.000	2799,304	HOUT < (2*N/(N-T)
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2	000.341	80.000		12400-000	000-662	-			
154	154.940	92-804		15954.651	221.144	1218,472	101	= 19	-160.363
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# @ 1 U M N								:	;
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	0.9062		0.3170	0.2813	1.4448	96.808	-53.454	-	62
	1.2967		0.3170	0-4111	2.1186	104-151 5	-53.454		155
	1.4520		0.3170	0.4604	2.1678	-	-53-454	-	06
	1.6450		0/11-0	0.5215		-	-53-454		8 6 8
	1.8215		0.3170	0.5775		-	-53.454	-	200
	2.0350		0116-0	0.6452		~	-53-454	-	109
	2.1850		0,11,0	0.0427	2.4002		-53.454	4 304-776	176

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PROBABILITY ANALYSIS OF SUCCESSIVE 2 DAYS MAXIMUM RAINFALL AT THARRAWADDY
RAINFALL AT
DAYS MAXIMUM R
2 DA
SUCCESSIVE
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ANALYSIS OF
PROBABILITY
APPENDIX E-19

		r sax	26198064-00	15612991-00	13624000-00	9369902.00	6453757.00	5336617+00	5084716.00	4195868.00	4195868.00	3575117-00	3539602-00	3451847-00	2924327-00	2924207.00	2908771.00	2628072.00	2425870.00	2352637.00	2344259-00	2212344.00	2123011-00	2013059.00	1745162.00	1601613-00	1473447.00	1415035.00	1367555.00	1257961-00	148267344 - 00	5112667-00
	_		U4209-00	62467.97	00-00016	44445.05	34663.71	30538.24	29569.54	24014.45	26014.45	23380.84	23225.75	22840.26		20449-00	20376.98	19044-00	18054.21	1/689.00	17646.98	16978.60	16518.41	16258.27	14495.19	13689.00	12948.61	12604.09	12320-54	53.1	787265-25	27147.07
PROJECT	UNIT- M M	HAZEN PLUT(\$}	94 . 28	94.83 01 10	87.93	84.48	81.03	11.59	74.14	10.69	67.24	61.19	60°34	56.90			46.55	43.10	39.66	36.21	32.76	29.31	25.86	22.41	18.97	15.52	12.07	8-62	5.17	L.72		
M/P	AWADDY	FHUMAS PLUT (T)	40-07	67°66	80.67	1.33	80.00	76.67	55.61	10.00	66.67	56.60	60.00	56.67	54.13	50.00	10.04	66.69	40.00	16.67	66.66	30.00	24.67	23.33	20.00	16.67	19.33	10.00	6.67	J.33		**
PROBABILITY OF EXCEEDANCE ON IRRAWADDY M/P	CESSIVE 2 DAY MAXIMUM RAINFALL AT THARRAWADDY	Z**Y = YY	20162.4	05134-3	4, 81778	4.44712	4.06548	٠	3.4116.6	3.54985	3.59985	3.41724	3.40565	3.37439	3.17867	J.17862	5.17218	3.04679	2.94528	2.40575	2-90112	2.82527	2.11039	2.13432	1 6 1 6 4 • 7	2.J7089	2.24276	2.17861	Ē	1.98340	94.61834	= 41££.L
EDANCE ON	UM RAINFA	Y ≈ LGG(X+B)	2.33114	2-22425	2.19495	2.10882	2°01635	11496-1	16560.1	1.89733	[[19]]	1-84858	1-84544	1.83750	1.74208	1.78287	1.78106	1.14551	1./1618	1.10463	1.10327	1-68085	1.06445	1.65479	1.0001/	1.93477	1-49/58	1.47601		1.40835	19669.54	= 1.01013 = 0.34415 46.44876 = 1.34826
ry of exce	P DAY MAXIN	£1+13	214.655	196.701	156.455	2128.415	168.601	42.407	84.613	14.945	74-945	1001	< <n.01< td=""><td>69./85</td><td>149-09</td><td>60.655</td><td>60.403</td><td>55.055</td><td>52.021</td><td>249-04</td><td>10.4.04</td><td>156:15</td><td>46.179</td><td></td><td></td><td>500-55</td><td>199975</td><td>20.923</td><td>24.443</td><td>25+605</td><td></td><td>2017</td></n.01<>	69./85	149-09	60.655	60.403	55.055	52.021	249-04	10.4.04	156:15	46.179			500-55	199975	20.923	24.443	25+605		2017
	0	(X) 101		2.38021	2.37840	16656.5	2.26994	2-24242	2,23542	2.20761	2.20761	2.18443	2.18298	<571.5	2-17534	4E441.2	2 2 4 2 1 - 2	5-13988	2-12B29	612385	2.12333	26511-2	2.10196	50001°7		A1000.42	11960-2	2.05024	2.04531	2.03322	41-30644	120.001 2 14270 2015(20//1/1)1(2/20//20/2) 2015(2/20//20/2)11(2/20/2) 2015(2/20/20/2)11(2/20/2)2)2(2/20/2) 2016(2/20/2)2)2(2/20/2)2)2(2/20/2)2)2(2/20/2)2)2(2/20/2)2)2(2/2)2(2/2)2)2(2/2)2(2/2)2)2(2/2)2(2/2)2)2(2/2)2(2/2)2)2(2/2)2(2/2)2)2(2/2)2(2/2)2)2(2/2)2(2/2)2(2/2)2)2(2/2)2(2/2)2)2(2/2)2(2/2)2(2/2)2)2(2/2)2(2/2)2)2(2/2)2(2/2)2)2(2/2)2(2/2)2(2/2)2)2(2/2)2(2/2)2(2/2)2)2(2/2)2(2/2)2(2/2)2)2(2/2)2(2/2)2)2(2/2)2(2/2)2)2(2/2)2(2/2)2)2(2/2)2(2/2)2)2(2/2)2(2/2)2)2(2/2)2(2/2)2)2(2/2)2(2/2)2)2(2/2)2(2/2)2(2/2)2)2(2/2)2(2/2)2(2/2)2(2/2)2)2(2/2)2(2
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PROJECT	UNIT - M M - I		2+XU-1X1+X5) -100-154	-20-121			μX						•••		-	
ď	ADDY				2 2	* * * *	n	-82.345	-42.345	-82.34	-82.345	-82.345	-82.345	-82-34	-42.345	-82,345
AWADDY M	at Tharraw	***		3719.098		ME THOD	C=10++A	64.584	101.498	132-433	180.46J	204.096	231.824	213.526	523-948	364.837
***** THE PROBABILITY OF EXCEEDANCE ON IRRAWADDY M/P	SUCCESSIVE 2 DAY MAXIMUM RAINFALL AT THARRAWADDY		X1+X5-XU++2 404-950	352.268		,[v"], X	A≖YM+E•K	1.0101	2.0149	2.1220	2.2564	2.3098	2.3763	2.4370	Ži, 105	2-5621
F EXCEED	MAXIMUI	- VALUE		26944.309		VALUES B	г е К	0.0	0.2048	0.3119	0-446J	1064-0	U.566L	0.6269	0.7UU4	0752°D.
IABILITY 0	SIVE 2 DAY	() +++++		-		INE PRUBABLE VALUES BY	¥	U.3442	0.3442	0.3442	0.3442	0.3442	0.3442	0.3442	U.J44Ž	0.3442
THE PROB		•	45 107-450	112.268			-		1945.0	0.7062	1.2961					
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Appendix E-19 Page -2

PROBABILITY ANALYSIS OF SUCCESSIVE 2 DAYS MAXIMUM RAINFALL AT PROME APPENDIX E-20

***** THE PROBABILITY OF EXCEEDANCE ON IRRAWADDY M/P PROJECT *****

X: SUCCESSIVE 2 DAY MAXIMUM RAINFALL AT PROME UNIT - M M I

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1/10 1/10 1/10 2.2905 200-419 2.290142 5.29044 90-00 91-45 1/11 1/11 1/11 1/11 1/11 1/11 1/11 91-10 91-45 1/11 1			¢				7			7	
1971 118.000 2.200.465 2.201.465 5.29846 91.48 1975 116.000 2.21561 197.55 197.41 91.48 1965 151.988 2.11762 187.55 197.41 91.48 1975 151.988 2.11762 187.55 2.25612 5.00298 91.03 1975 148.590 2.11792 172.479 2.25612 5.09788 91.03 1975 154.900 2.113345 158.255 2.19966 91.43 91.44 1975 114.600 2.113345 158.255 2.19946 4.98575 77.59 1975 115.000 2.11164 51.175 2.11844 7.7564 65.279 1975 114.000 2.110410 2.11141 2.10940 60.57 67.24 1975 114.000 2.11244 155.647 2.11244 155.647 60.507 1976 111.284 2.095411 2.11244 155.647 60.567 60.567 1975 111.284 2.01744 155.647 2.01747 125.647 60.567	1	142	114.054	2.25055	200.419	2.30194	ŝ	96.67	98-28	31703-20	5644880.00
1514 116.000 2.24755i 194.365 2.247145 5.272495 5.10511 80.000 91.46 155 157.910 2.217145 187.3155 2.2572405 5.10511 80.000 91.43 155 157.910 2.217145 187.315 2.2572405 5.10511 80.000 91.43 1955 157.814 2.17545 17.455 2.712495 5.00278 80.000 91.43 1951 196.07 2.11349 158.255 2.19936 4.93717 70.00 77.59 1952 195.800 2.11146 2.11564 4.91717 70.00 71.59 1954 1954 124.000 2.11144 2.01417 135.647 2.1124 4.5119 1954 124.100 2.111.284 2.01417 135.647 2.1124 4.5119 55.450 1954 111.284 2.01417 135.647 2.11244 4.5119 51.47 55.47 1956 111.284 2.01410 135.647 2.11244 2.01410 2.01410 2.11244 1957 111.284	2 1	1761	1/8.000	2,042.5	200-365	2.30142	ű.	66.69	94.83	91684.00	5639752.00
1/17 165.000 2.41946 181.305 2.225612 5.01938 80.00 81.03 1965 150.114 2.11946 181.305 2.225612 500108 80.00 81.03 1965 150.114 2.11319 170.55 2.225815 500104 81.03 81.04 196 135.000 2.11319 150.355 2.19946 4.83717 70.00 81.05 1976 135.000 2.11319 158.255 2.19946 4.83717 70.00 81.05 1976 135.000 2.11316 158.255 2.19946 4.83717 70.00 81.05 1975 124.010 2.11354 159.155 2.19514 4.91017 70.00 81.05 1976 124.142 2.01710 131.411 2.15044 2.1124 50.00<		1514	116.000	2.24551	148.345	2.24146	5.2783	90.00	91.38	30976.00	5451776.00
1965 151.784 2.11962 180.751 2.255012 2.00298 80.00 81.03 1953 164.590 2.117642 182.65 2.19954 715.95 71.59 1951 1951 14.650 2.11954 156.67 71.59 71.59 1951 1951 195.175 2.19354 158.365 2.19946 4.9317 70.00 1951 1954 19549 0.1010 2.11549 159.175 64.010 61.249 1975 128.000 2.10142 2.09401 191.241 4.63049 65.67 61.249 1975 128.010 2.10141 150.365 2.11715 4.73946 63.33 63.45 1975 128.010 2.09401 147.313 2.11614 4.6717 4.6313 55.01 1976 111.504 2.05417 135.649 2.11241 4.54719 54.313 53.455 1996 104.010 2.01417 135.649 2.01241 4.6717 4.6717 4.6717 1996 104.410 2.0141 135.647 2.01441	-	F1 (-)	165.000	2.21748	187.345	2.27269	ŝ	96.67	61.93	27225.00	4492125-00
1950 150.114 2.117642 112.479 2.236/13 5.00298 80.00 81.03 1951 195.870 2.11799 180.100 2.11799 17.259 75.149 1952 115.870 2.11319 158.255 2.19946 4.83717 70.00 71.259 1952 115.870 2.11319 158.255 2.19946 4.83717 70.00 71.259 1952 115.8010 2.11154 150.105 2.19159 61.03 65.90 1951 124.000 2.10164 195.115 2.19159 61.010 61.343 1951 124.000 2.10164 2.1515 2.19159 61.010 61.343 1954 124.000 2.01447 195.449 2.11241 4.54719 50.00 55.95 1954 111.2844 2.05411 135.649 2.11241 4.63700 56.90 56.90 1954 111.2844 2.05411 135.649 2.11241 4.63700 56.90 56.90 1955 111.1506 2.0411 135.649 2.11241 4.63704		1965	151.988	2.19862	180.355	2.25012		83.33	84-48	24960.19	3943408.00
1953 140.590 2.11199 170.955 2.22200 4.94575 75.67 77.59 1951 1952 110.000 2.11354 158.365 2.19946 4.83177 70.00 74.14 1952 110.010 2.11354 158.365 2.19946 4.83177 70.00 67.24 1952 110.010 2.11064 153.175 2.119346 4.83177 70.00 67.24 1951 124.968 2.095417 155.649 2.115343 4.63900 56.67 55.96 1954 120.142 2.095417 115.0449 2.11241 4.63900 56.67 55.49 1954 111.284 2.095417 115.0449 2.11241 4.63710 55.45 1954 111.284 2.09717 135.649 2.11241 4.55719 55.45 1954 111.284 2.09717 135.649 2.11241 4.55719 55.45 1954 111.506 2.09718 131.5447 2.11241 4.55717 4.2070 1956 191.647 2.01441 2.01244 2.05419 <t< td=""><td>-</td><td>1469</td><td>150.114</td><td>2.17642</td><td>112.414</td><td>2.23613</td><td>°.</td><td>80.00</td><td>81.03</td><td>22534.20</td><td>3382697.00</td></t<>	-	1469	150.114	2.17642	112.414	2.23613	°.	80.00	81.03	22534.20	3382697.00
1916 13.6.000 2.13354 158.365 2.19966 4.83317 70.000 70.69 1951 135.100 2.113319 159.155 2.19916 4.13117 70.000 70.69 1951 135.100 2.11064 159.255 2.19916 4.131717 70.000 70.69 1951 125.142 2.07969 147.5343 2.16519 4.73996 65.33 65.99 1954 120.142 2.07969 147.5343 2.16519 4.73990 65.010 60.34 1954 111.284 2.05417 135.649 2.11514 4.56719 55.090 56.990 1954 111.284 2.05417 135.649 2.11541 4.57719 50.00 56.990 1954 111.284 2.05417 135.649 2.11541 4.67719 50.00 56.990 1954 1956 111.284 2.05417 2.15419 4.67617 4.32649 50.00 56.990 1954 1956 111.284 2.05719 4.1721 310.617 50.010 50.010 50.617 50.617 <t< td=""><td>-</td><td>1953</td><td>148.590</td><td>2.17199</td><td>110.955</td><td>2.23288</td><td>4.</td><td>16.67</td><td>77.59</td><td>22078.97</td><td>3280713-00</td></t<>	-	1953	148.590	2.17199	110.955	2.23288	4.	16.67	77.59	22078.97	3280713-00
1951 155.090 2.19319 158.255 2.19936 4.83717 70.00 70.69 1952 1972 10.4010 2.10124 150.365 2.10159 65.33 65.33 65.33 1951 124.708 2.10740 147.33 2.10154 4.63900 55.45 55.49 1954 120.142 2.07969 147.234 2.01430 50.00 55.49 1954 120.142 2.07969 147.244 2.15441 4.63900 55.00 55.49 1955 111.284 2.05447 135.649 2.11541 4.54719 53.13 55.45 1956 111.284 2.05417 135.649 2.11541 4.554719 50.00 55.45 1956 101.204 2.01424 130.569 2.11544 4.47677 44.10 50.00 55.45 1956 1957 111.5906 2.01420 12.7775 2.115044 4.47677 44.10 50.60 24.110 27.17 20.00 27.17 24.10 27.17 20.20 21.16 21.16 24.17 24.17 <td< td=""><td>-</td><td>9161</td><td>134.000</td><td>2.13354</td><td>158.365</td><td>2.19966</td><td>5</td><td>13.33</td><td>74.14</td><td>18496.00</td><td>2515456.00</td></td<>	-	9161	134.000	2.13354	158.365	2.19966	5	13.33	74.14	18496.00	2515456.00
1952 190.010 2.11664 15.175 2.19796 66.67 67.24 1975 124.000 2.00780 150.175 2.17115 4.73996 63.33 63.379 1954 124.000 2.00780 145.513 2.15343 4.63900 56.67 55.24 1954 120.142 2.07407 135.649 2.15441 4.57719 54.33 53.45 1954 111.284 2.05417 135.649 2.11344 4.54719 54.00 56.67 55.45 1954 111.284 2.09740 135.649 2.11344 4.54719 54.00 56.67 55.45 1954 111.284 2.09740 2.01424 135.649 2.11344 4.54719 54.00 55.45 1956 1994 1995 100.003 127.775 2.01740 4.0.00 39.45 55.45 1956 95.504 195.444 2.01740 2.01470 4.0.00 39.45 4.100 1956 1956 19609 112.0047 4.43710 4.0.00 30.45 4.101 2.027	-	1961	135.840	2.13319	158.255	2.19936	. 5	70.00	70-69	18466.08	2509354.00
1575 128.000 2.10721 150.305 2.11715 4.73996 63.33 63.79 1954 124.968 2.00760 147.333 2.16340 4.70152 60.00 60.34 1954 113.284 2.05417 135.649 2.115341 4.54719 59.00 60.00 60.34 1956 111.284 2.05417 135.649 2.11544 4.54719 50.00 50.00 50.67 1956 111.284 2.05417 135.649 2.11544 4.54719 50.00 50.00 50.00 50.00 50.00 50.00 50.00 50.00 50.01 50.	-	1952	110.010	2.11664	153.175	2.18519	3	66.67	67.24	17111.25	2238321-00
1951 124.964 2.09600 147.333 2.16330 60.00 60.34 1954 120.142 2.05417 135.649 2.13241 4.63900 56.67 55.67 1954 120.142 2.05417 135.649 2.13241 4.54719 55.01 55.67 1954 111.284 2.05417 135.649 2.13241 4.54719 51.00 56.67 1956 1964 105.410 2.10444 135.649 2.11506 4.0201 $4.17.77$ 5.0547 51.200 4.10107 51.20003 417.77 52.01049 4.47677 $4.12.017$ 4.10007 51.070 411007 41007 <td< td=""><td>-</td><td>1975</td><td>128.000</td><td>2-10721</td><td>150.345</td><td>2-11/15</td><td></td><td>63.33</td><td>63.19</td><td>16384.00</td><td>2097152-00</td></td<>	-	1975	128.000	2-10721	150.345	2-11/15		63.33	63.19	16384.00	2097152-00
1954 120.142 2.07969 142.507 2.15383 4.63900 56.67 56.90 1956 111.284 2.05417 135.649 2.11241 4.54719 53.33 53.45 1956 111.284 2.05417 135.649 2.11241 4.54719 50.00 50.00 1956 111.506 2.01424 135.649 2.11544 4.47717 44.33 51.10 1956 100.204 2.01424 135.649 2.11594 4.47677 44.33 51.00 50.00 1957 195.410 2.01424 130.569 2.11594 4.47677 44.310 40.6527 50.00		1951	124.468	2.09680	147.343	2.16030		60.00	60.34	15616.99	1951623-00
1956 111.206 2.05417 135.649 2.13241 4.54719 53.45 1964 111.206 2.095417 135.649 2.11341 4.52719 46.67 50.00 1964 101.206 2.095417 135.649 2.11344 4.52719 46.67 40.00 1964 101.206 2.09412 135.649 2.11504 4.52719 45.103 50.00 1956 195.410 2.09541 135.649 2.11504 4.52719 45.103 50.20 1956 195.410 2.02240 122.641 2.09713 4.52717 40.07 39.66 1953 1955 1955 1.22.641 2.05713 4.23177 30.00 29.21 1963 89.1074 1.94694 19.47013 2.00713 4.23177 30.00 29.31 1964 89.1074 1.945945 114.059 2.00710 4.03177 30.00 29.31 1964 89.1074 1.945945 1.97164 1.97777 30.00 20.41 1964 89.106 1.94727 1.99127 1.97177 </td <td></td> <td>1954</td> <td>120.142</td> <td>2.07969</td> <td>192.591</td> <td>2-15383</td> <td></td> <td>50.67</td> <td>56-90</td> <td>14434.09</td> <td>1734139-00</td>		1954	120.142	2.07969	192.591	2-15383		50.67	56-90	14434.09	1734139-00
1964 111.284 2.05417 135.649 2.11241 4.54719 50.00 50.00 1951 111.506 2.01424 135.649 2.11504 4.52279 40.67 40.555 1960 109.204 2.01424 130.605 2.01424 30.60 30.60 30.60 1960 1994 105.410 2.01441 2.01644 4.52179 40.60 39.66 1953 1954 105.410 2.02208 122.641 2.02059 31.33 32.76 1953 95.504 1.99637 112.059 2.01740 4.35943 30.60 32.76 1954 95.504 1.92466 105.413 2.02713 4.20117 30.00 23.33 22.41 1964 84.074 1.92466 105.413 2.02713 4.2011 25.677 25.241 1971 73.000 1.92466 105.413 2.00733 1.9177 30.00 25.41 1976 60.594 1.92465 194243 1.91913 23.33 22.41 1966 60.548 1.92413 1.940	-	1956	111.284	2.05417	135.649	2.13241		51.13	53.45	12833.25	1453801.00
1957 111.506 2.077J0 133.071 2.1200 4.52279 40.67 4.4.55 1960 108.204 2.01444 130.569 2.11504 4.47677 4.3.33 45.10 1950 1964 108.204 2.01444 130.569 2.11504 4.47677 4.3.33 45.10 1950 1954 108.076 2.012204 1127.775 2.10044 4.47677 4.3.31 45.110 1955 1959 106.076 2.012204 112.177 20.00 29.31 25.241 20.201 25.264 25.241 20.201 25.264 25.264 25.264 25.264 25.264 25.264 25.264 25.264 25.264 25.264 25.264 25.264 25.264 25.264 26.274 26.077 26.2077 26.274 27.271 <t< td=""><td>-</td><td>1904</td><td>111.284</td><td>2.05417</td><td>135.644</td><td>1,2,1,3,4,1</td><td></td><td>50.00</td><td>50.00</td><td>12833.25</td><td>1453801.00</td></t<>	-	1904	111.284	2.05417	135.644	1,2,1,3,4,1		50.00	50.00	12833.25	1453801.00
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$		1551	111.506	2.04102	133.871	2-12009	4.52219	40.67	46.55	12433.51	1386411-00
1948 105.410 2.022UB 127.77> 2.10644 4.43710 40.00 39.66 1959 105.410 2.002033 122.441 2.081792 4.35543 30.67 36.21 1959 105.04 1.98002 117.669 2.007143 4.23177 30.67 36.21 1953 1954 1.98002 114.519 2.097113 4.19173 30.67 25.86 1961 64.074 1.98012 111.519 2.097113 4.19163 23.33 22.41 1961 64.074 1.92666 106.449 2.09710 4.19163 23.33 22.41 1967 10.00 1.92662 94.241 1.99772 13.33 12.07 1977 13.000 1.96562 94.241 1.94772 3.7945 19.07 5.52 1977 1.9662 1.9772 1.97972 1.9.00 3.9177 15.07 1966 66.294 1.96428 1.97472 3.7945 10.00 5.17 1972 60.000 1.94772 3.79361 1.700 5.417 <t< td=""><td>_</td><td>1960</td><td>104.204</td><td>2-01424</td><td>130.569</td><td>2.11504</td><td>4.47671</td><td>65.64</td><td>43.10</td><td>11708-10</td><td>, 1266862.00</td></t<>	_	1960	104.204	2-01424	130.569	2.11504	4.47671	65.64	43.10	11708-10	, 1266862.00
1959 105.076 2.00033 122.441 2.08192 4.35943 36.67 36.21 1955 95.554 1.98002 117.865 2.07140 4.23177 30.00 29.31 1955 95.554 1.98002 114.659 2.07140 4.23177 30.00 29.31 1963 89.1594 1.995014 114.659 2.05710 4.19163 26.67 25.86 1961 89.154 1.995014 114.659 2.02710 4.19113 23.33 22.41 1961 84.074 1.99514 114.659 2.02710 4.19913 23.33 22.41 1961 84.074 1.99514 194.949 3.94827 20.00 8.97 15.52 1971 71.000 1.96562 94.247 1.97472 3.99772 13.33 12.07 1966 66.544 1.86249 94.265 1.97472 3.99772 13.33 12.07 1972 66.244 1.8213 84.945 1.9000 3.93784 6.070 9.6524 1971 66.244 1.8247 84.4	-	848	105,410	2.02208	127.175	2.10044	3	40.00	39.66	11111.26	1171237-00
1955 95.504 1.98002 117.869 2.057140 4.29069 31.33 32.76 1963 91.694 1.96234 114.059 2.05713 4.19163 25.67 25.86 1963 91.694 1.992466 106.439 2.005713 4.19163 25.67 25.86 1964 89.154 1.992466 106.439 2.00713 4.19163 23.33 22.41 1964 84.074 1.992466 106.439 2.00719 4.19913 23.33 23.43 1977 73.000 1.92466 95.365 1.4773 3.91777 13.33 12.07 1970 1.1.842 1.86324 95.355 1.9772 3.99772 13.33 12.07 1972 66.548 1.82447 86.5913 1.94628 3.79860 5.17 5.17 1972 66.544 1.82447 86.541 1.94628 3.79860 5.17 5.17 1972 66.544 1.82447 86.913 1.94628 3.79860 5.17 5.17 1972 66.544 1.82447 1.9462	_	6561	100-076	2.00033	122.441	2.08792		30.01	36.21	10015.20	1002280-25
1 1963 91.694 1-96234 114.059 2.05713 4.23177 30.000 29.31 2 1964 84.074 1.956164 11.519 2.067135 4.17163 26.67 25.86 3 1967 84.074 1.956164 11.519 2.067135 4.17163 26.67 25.86 5 1977 73.000 1.997065 95.3271 1.99700 3.99827 20.00 18.97 5 1977 73.000 1.997665 95.3271 1.99707 3.99827 20.00 18.97 5 1977 73.000 1.96627 95.3271 1.99707 3.99827 20.00 18.97 5 1972 13.000 1.9652 95.3271 1.9772 3.99772 13.33 12.07 6 1972 60.0548 1.81247 86.913 1.94939 5.477 5.477 5.477 5.477 5.477 5.477 5.477 5.477 5.477 5.477 5.477 5.477 5.47945 5.477 5.476 5.477 5.477 5.47945 5.477	_	1955	95.504	1.98042	[[1.4.869	2-07140		13.13	32.76	9121-00	871092-00
2 156d 89.154 1.95014 111.519 2.04735 4.19163 25.67 25.46 3 1961 84.074 1.92466 106.439 2.02710 4.10913 23.33 22.41 5 1972 1.92466 106.439 2.02710 4.10913 23.33 22.41 5 1972 1.92602 94.247 1.99706 3.94827 20.00 18.97 5 1972 7.000 1.06332 95.365 1.97427 3.94977 15.52 1 1966 66.544 1.05332 94.247 1.94496 3.94977 15.52 1 1966 66.544 1.94542 3.49772 3.79445 1.00 8.62 1 1966 66.544 1.94542 1.94480 3.79445 1.00 8.62 1.77 1 1966 66.544 1.815413 1.94482 1.79445 1.000 8.62 1.772 1 1972 66.544 1.81541 84.455 1.94628 1.794628 1.725 1 1972 6		1963	91.694	1.96234	114.059	2.05113		30.00	29.31	8407.78	770942.81
3 1967 84.074 1.92466 105.419 72.02710 4.10913 23.33 22.41 5 1972 71.926 1.92666 95.327 1.99706 3.94827 20.000 18.97 5 1972 71.000 1.96532 95.327 1.99706 3.94827 20.000 18.97 5 1972 71.000 1.96532 95.355 1.97792 13.33 12.07 6 1970 71.8454 1.949495 3.99772 13.33 12.07 7 1966 64.544 1.82313 84.913 1.94472 3.99772 13.33 12.07 8 1966 64.544 1.82313 84.913 1.94472 3.99772 13.33 12.07 8 1972 64.544 1.82313 84.945 1.9000 1.962 1.94772 3.79800 3.33 1.72 7.17 8 1972 64.544 1.8164126 1.72 5.17 5.17 5.17 10 1972 60.000 1.81954 80.4628 1.19480 3.33	-	156J	89.154	1.95014	11.514	2.04735		20.67	25.86	1948.43	708633-63
<pre>4 [Y58 7c.Y62 [.88c28 95.327 [.9Y706 J.94827 20.00]8.97 5 1977 73.000 [.8552 95.355 1.97739 J.91797 16.67 15.52 1970 73.000 [.86332 95.355 1.974427 3.89772 13.33 12.07 6 1970 66.548 1.82313 86.913 1.94489 J.79301 0.00 8.62 9 1972 66.244 1.82313 84.955 1.94489 J.78800 3.33 1.72 10.00 1972 66.249 59.27850 61.04130 131.54826 1972 60.000 [.81954 88.365 1.94628 J.78800 3.33 1.72 10. 10. 10. 11. 12. 10. 13. 14. 15.540 2.94409 13.551 14. 15.540 2.94409 13.5515 14. 15.542 54. 10.1542 54. 10.1542 54. 10.1542 54. 10.1542 54. 10.1542 54. 10.1542 54. 10.1542 54. 10.154 55 54. 10.154 55 54. 10.154 55 54. 10.154 55 54. 10.15 54. 10.154 54. 10.154 55 54. 10.154 55 54. 10.154 55 55 55 55 55 55 55 55 55 55 55 55 5</pre>		1961	84.074	1.92466	106.439	. 2.02710		23.33	22.41	1068.43	594270.81
5 1977 73.000 1.86332 95.365 1.97939 J.91797 16.67 15.52 5 1970 71.842 1.86362 94.247 1.97427 3.89772 13.33 12.07 1 1966 66.544 1.82313 86.913 1.94896 3.79945 10.00 8.62 8 1972 66.544 1.82147 88.365 1.94628 J.79961 5.37 5.17 9 1972 66.000 1.81954 88.365 1.94628 J.78800 3.33 1.72 1AL 3362.449 59.27850 61.68130 131.54826 AA XH 115.540 2.04409 YH 2.115942 4.53615 YHH A HOUIS(2*N/(N-1)+47YM-YM*Y) - J.15942 4.53615 YHH A HOUIS(2*N/(N-1)+47YM-YM*Y) - J.15942 4.53615 YHH		1458	10.162	1-88028	156.321	1-99706		20.00	18.97	5923.14	455856.88
5 1470 71.042 1.45662 94.247 1.47427 3.89772 13.33 12.07 7 1966 66.548 1.8213 86.913 1.94896 3.79845 10.00 8.62 8 1977 66.548 1.81547 86.913 1.94696 3.79845 10.00 8.62 9 1977 66.544 1.81547 84.455 1.94628 5.17 9 1972 66.000 1.81954 88.365 1.99658 5.178 10.1 33.33 1.172 3.78800 3.333 1.772 10.1 33.449 54.4628 54.2169 4.53615 4. 10.1 41.54826 4.53615 774 4.53615 4. 10.1 41.54826 4.53615 4.53615 4. 10.1 41.54826 4.53615 4.53615 4. 10.1 41.54847 4.53615 4.53615 4.		1917	000-61	1.86332	95.365	1.97934	1.91797	16.67	15-52	5329.00	389017-00
<pre>1 1966 60.548 1.82313 84.913 1.94896 3.79845 10.00 8.62 8 1947 66.294 1.82413 84.659 1.94472 3.79301 5.07 5.17 9 1972 60.000 1.81954 80.365 1.99628 J.78800 3.33 1.72 1AL 3362.449 59.27850 61.04130 131.54826 4. 1AL 3362.449 59.27850 7M 2.12694 4.53615 YYM N = 115.546 2.04409 = 0.15942 54 + 53615 YYM </pre>		1470	11-842	1-45662	94 247	1.41421	3.89772	66.61	12.07	5167.02	371415-25
В 1947 66.244 1.82147 88.659 1.94772 3.79301 5.47 5.47 9 1972 60.000 1.81954 88.365 1.94628 J.78800 3.33 1.72 ГАL 3362.449 59.27850 61.08130 131.54826 An XM = 115.540 2.04409 YM = 2.12694 4.53615 • YYM H = HUUI<(2.01/1N-1)+01YM-YMPYM)> 0.15942 4.53615 • YYM 5.4 • HOUI<(2.01/1N-1)+01YM-YMPYM)> 0.15942 4.53615 • YYM		1966	66.548	1.82313		1.94896	3.79845	10.00	8-62	4428.63	294716.25
9 1972 60.000 1.81954 80.365 1.94628 J.78800 J.33 1.72 Tal JJ62.429 59.27850 61.681J0 131.54826 An XM = 115.540 2.04409 YM = 2.12694 4.53615 * YYM N = 1001<22*N/IN-11+01YM-YMYD = 0.15942 5.4 * 1001<2.XM-XM+XM>		5	66.294	1-82147	84.659	1.94172	J. 79301	6.47	5.17	4394.89	291354.75
<pre>IAL 3362.429 59.27850 61.08130 131.54826 42 Ab xm = 115.544 2.04409</pre>		~	66.000	1.61954	84.165	1.94628	J. 78800	3.33	1 - 72	4356.00	287496.00
AA XM = l15.54c 2.U4409 YM = 2.12694 4.53615 = YYM K = KUU1<{2•N/{N-1}}•{YYM-YM•YM}> = 0.15942 54 = ROU7 <xxm-xm+xh> = 34.68524</xxm-xm+xh>	CIAL			05875.64		61-64130				424148-44	57650400.00
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PROJECT .	(1+XS) 686 926 184 184 8 * 8	X=C-B	111-585 144-289 164-450 193-244 205-893 205-893 205-893 239-051 239-051 264 276-368
_	2*X0-{X1+XS1 -22.686 -22.926 -22.926 -21.180 101AL 81 * HEAN 8 *		22,365 22
THE PROBABILITY OF EXCEEDANCE ON IRRAWADDY M/P SUCCESSIVE 2 DAY MAXIMUM RAINFALL AT PROME		H£⊺HOD + C≈10++A	133-949 166-654 186-814 215-609 218-257 228-257 245-016 245-016 245-129 241-416 241-416 242-129 298-733
e probability of exceedance on Irrawaddy P Successive 2 day maximum rainfall <u>at</u> prome	V A L U E ••••• X1*X5-XU*2 244.054 244.294 242.548 1 242.548	1Y •1441° ∆≖YH+E*R	2.1269 2.2216 2.2216 2.3337 2.3337 2.3584 2.4513 2.4513 2.4513 2.4753 2.4753
JF EXCEEC	8 - √ A XI**S X X1751.559 X1762.441 11762.441	PROBABLE VALUES BY K E+K #	0.00 0.10449 0.215 0.215 0.22051 0.22023 0.22023 0.22023 0.22023 0.22044 0.22223 0.22445 0.22223 0.22445 0.22223 0.22445 0.22223 0.22445 0.22223 0.22445 0.22223 0.22445 0.22223 0.2245
BABILITY (SSIVE 2 DA	:	PROBABLE K	0.1594 0.1594 0.1594 0.1594 0.1594 0.1594 0.1594 0.1594 0.1594
	× 000	• • • • • 1HE E	0.0 0.5451 0.9062 1.4520 1.6450 1.6450 1.6450 1.8215 2.1450 2.1450
• ×	x x 178.400 176.000 176.000		
	1 1 2 3 3	461UKN- Plkiud 17644)	200 200 200 200 200 200 200 200 200 200

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1 = = = = = = = = = = = = = = = = = = =		2161	1975	1950	1974	1958	9961	1948	9567	0/61	0951	8951	7561	1977	1971	2961	1351	1769	1953	1959	1955	1963	5/61	1924	1976	1961	үедн		
154.082 2.1 RODI < 12*N/(N-1) RODI < 12*N/(N-1) XXXH-3*XXM*XM+2	640 *??	105-000	106.000	111.760	112.000	115-062	116.332	119+126	123.552	127.000	982-621	8,00061	144.272	148.000	160.000	162-560	167.640	168.148	108.150	174.752	181.960	066"567	202.000	204.470	240 000	278.638	×		×
YM = HGDT<[2*N/(N-1]]*{YH-YH*YH} = RGGT <xxh-xm*xm*z+y**j) (sx*ej)="<br">[XXXH-3*XXH*XH+2*XH**J)/(SX*eJ)=</xxh-xm*xm*z+y**j)>	54.44827	2.02119	2-02531	2.04829	2-04922	2.0003	2.06570	2.07601	2.09325	2.1034O	2.11155	2.11410	91651"2	2.17026	2.20412	2.21101	2-22438	2.22569	2.22700	2.24242	2.27407	01662.7	2.30535	2.31063	12085.7	2.44504	L00(X)		SUCCESSIVE 2 DAY MAXIMUM RAINFALL AT HENZADA
(FoaXS)/(F a c[HJaHJaH HZ		54 + 3 7 4	55.314	01.134	61-374	64.436	o5.706	68.500	73.320	76.374	78.600	79.422	93.046	91.314	109.374	111.934	117-014	117.522	010.010	124.126	137.334	140.764	151.3/4	153-844	193.14	228-012	X+8		2 DAY MAXII
= 1.98895 = 0.24545 _43.53371 _ 0.99718	49.72386	1.73539	1-74331	1.78528	1.78794	1.80913	1.81760	1.43509	1.86526	1.88295	1.84215	1.84444	1.97149	1.98944	2.03891	2.04896	2.06824	2.07072	2-07199	2.09386	2.13778	2.17250	2.18005	2.18708	2.21132	2-35796	LUG(X+8)	۲ ۲	MUM RAINFA
	99.62135	3.01158	11650 5	1.1000	1.19689	3.27295	3,30366	3.96916	3-41619	3.54548	88f65°F	3.60977	3.88677	3.95390	4.13/1/	4 19824	4.27761	4.28539	4.29315	4-38426	4.57009	4.71974	4.75262	4.78332	61981 5	5.55996	X**5	44 -	LL AT HENZ
* YYH		3.85	1.09	11-54	86.43	19.23	23.08	26.92	30.11	70 - 55	38.40	42.31	61 G4	00.00		21.09	4C°19	03.30		80.51	10.92	BO . / /	29.48	99.40	5.75	96-15	PLU1(1)	THUMAS	
		2.00		10.00	10 00		~~ 00	20.00		34.00	30.00	42,00	40.00							10 10	10.00	82+00	00+00	00.06	00.45	00.86	6 E 11 D 14	HAZEN	UNIT_4 MM
29239+13	656418-88	1105500		00 75511 57 505671	13694 20	13614 00			50.001/1	12122-77		10 116 71	27 C1071	00 71000 00°L0617	51004 OD				2027777777	<pre>CK 42440</pre>	76 85307 21-87666	70 04125	70 43400 00 40004			17639.06			-
4 - 6 0 0 0 0 0 0 0	119302096.00		1157625-00		1305014-00	1404928-00	00 - 21 22 23 1	00-7120101	1490515.00	100700100	00.0858700		00 - 61 70 0 16		1747700	00-0009609	4205766-00	4711211-00	4754169-00	4797388-00	00 7177ES	00 9670777 2264101961	00 7104604 00 704 74 70			21633184.00	×**5		

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APPENDIX E-21 PROBABILITY ANALYSIS OF SUCCESSIVE 2 DAY MAXIMUM RAINFALL AT HENZADA

PROJECT, •••••

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.... THE PROBABILITY OF EXCEEDANCE ON IRRAWADDY M/P

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	*	••••• EHL	11040040	איטאמורב עמנטבא אי ז	,] ¥ H I , _ Å H	нетной 🚥	• • • •	
PERICO (YEAR)	- E AR J	بر	r	H# 3	A≠YH+E¢K	C=10+*A	Я	X=C-8
2		0.0	2425	0 . 0	0696.1	91.448	-50.620	148.114
		1465.0	0.2455	0.1461	0461.5	136.465	-50.626	197-091
10		0.9062	0.2455	0.2224		102.697	-50.626	213.323
01		1.2961	0.2455	6916.0		202.875	-50.620	253.501
205		1 4520	0.2455	U. 1504		221-437	-50.626	272.113
100		1.6450	0.2455	0.4038		247.013	-50.626	291.639
200		1.0215	U-2455	0.4471		212.924	-50.026	323.550
200		2.0350	45450	0.4995		201.925	-50.626	358.551
1000	-,	2.1850	U.2455	10.7361		335.168	-50.626	385.794

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APPENDIX E-22 PROBABILITY ANALYSIS OF SUCCESIVE 3 DAY MAXIMUM RAINFALL AT THARRAWADDY

••••• THE PROBABILITY OF EXCEEDANCE ON IRRAWADDY M/P PROJECT

X: SUCCESSIVE 3 DAY MAXIMUM RAINFALL AT THARRAWADDY UNIT - M M 1

	E + + X	40353600.00	24642160.00	23896784.00	13997521-00	11827095-00	11205429.00	10790920-00	8869743+00	7806453-00	5914807.00	5889922.00	5/66533.00	5644880.00	4754168.00	4604946.00	4541961.00	4078050.00	4039214.00	3737871.00	3652264.00	3581577.00	3581577.00	3575117.00	3131612.00	2862431.00	2847103.00	1987541.00	1927919.00	1701352-00	231210416-00 7972772-00	
-	7**X	111649.00	84681.00	82964.63	58081.00	51910.13	50014.17	48832.13	42849-00	39352.21	32105.97	32614.11	12151.07	J1703.20	28273-75	21618-95	21425-99	25525.16	25363.09	24085.16	23/16.00	23409.00	23409+00	23380.84	21404。84	20160.01	20087.95	15808.02	15490.28	14251.57	1065042.00 36725.59	
	HAZEN PLUT(%)	98.28	44.83	91.38	61.93	84.48	81-03	11.59	74.14	10.69	67.24	63.19	60.34	56.40	53.45	50.00	40.55	43.10	39.66	36.21	32.16	16.05	25.86	22.41	16-97	15.52	12.07	8.62	5.17	L - 72		
	THUMAS PLOTIX)	96.67	66.60	90.00	86.61	83.33	00.00	16.67	13.33	10-00	66.67	61.33	60-00	10.05	53.53	50.00	40.61	43.33	40.00	30-67	11.13	30.00	20.67	66.62	20.00	16-67	13.33	10-00		3.33	н ү н	
SUCCESSIVE SUAT MAXIMUM RAINFALL AT THARRAWAUUT	7**7 2**7	26458.d	5.33888	5.3/032	4.86584	4. <i>1</i> 0343	4.65094	4.01415	4.42086	4.24246	4.00453	4.00412	3.98200	3.95964	J.117UL	3.14255	3.72761	3.60452	1-59894	3.51233	3.48620	3.46406	3.44406	1.46201	9,20949	3.20115	1.19693	2.14500	2-10430	2.53233	113,60046 3.41933 =	
MUM RAINIA	LUG1X+81	16012.5	44636.5	2:31139	2.20586	2-16874	2.15660	2.14806	2.10258	2-071-95	2.00213	2.00103	1.94549	1.98989	24544.1	129451	01066-1	1.89961	1.89709	1.82422	1-46714	1.8612U	1.86120	1.80065	1.81920	1-1091-1	1.78400	1.65001	1,6444B	1.59133	57.12209 1 = 1.96973 = 0.28606	52.29128 87542.1 =
	X+B	202.044	210.644	207-680	164.644	141.442	143.611	140.624	124.644	110.018	100.492	144.238	90.968	91.648	81.192	86.014	45.252	14-410	18.902	14.038	13.644	12-044	12.694	244-21	65-948	060.10	01.376	45.374	401-44	14.024	5-26790 2-25062 -111*{YYM-YN+YM]>	
	1 nr (x)	42554.5	2-46345	2,45945	2.38202	(1) (1.2	2.34901	2.344.35	10416.5	2-24148	16162.5	2.25610	2.25364	44045.5	2.22509	2.22108	80512-2	2.20348	2.20210	2.19088	24281+2	2.18969	2.18469	2.18443	2.16526	2-15224	19161.2	5-660-2	2.09503	2.01693		
Ϋ́	×	000.6-6	291-000	284.036	100-122	860.155	223-174	220-940	207-000	198.374	100.049	180.574	119.324	178.054	148.144	-	-	159.760	842.041	155.194	154-000	153.000	000.641	152.908	146.304	141-986	561.191	125.130	124-460	115.300	5346.445 6 184.367 RCUT<12*N/IN	*ビスージメメン 1011 エメキビメン *ビンズ *ゴーゼメンズ
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PROJECT .	1 + X S } 2 1 9 2 2 9 2 8 0 5 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	X = C - B	111.623 218.481 218.481 249.462 299.462 299.461 355.961 355.961 389.633 473.683 473.683
5	2 * XU- (X - 102+ - 59+ - 57+ 101 AL B MEAN		
THE PROBABILITY OF EXCEEDANCE ON IRRAWADDY M/P SUCCESSIVE 3 DAY MAXIMUM RAINFALL AT THARRAWADDY	x 1 + x 5 9 2 3 4 - 660 4 5 0 5 - 1 80 4 5 0 2 - 0 1 0	ME FHQU + C=10++A	43.261 134.425 169.414 219.414 219.414 242.706 242.706 242.706 394.582 394.329
DANCE ON IRRA JM RAINFALL AT	x1+x5-x0++2 462-380 412-460 414-466	Υ - ΙμαΙ' Α≖γμ•ε•κ	1.4991 2.1400 2.1400 2.1400 2.4403 1451 2.4403 1451 2.4403 2.4400
r OF EXCEED. DAY MAXIMUN	x1*x5 40947-324 36217-844 36214-734	РАШИАВLE VALUES ИҮ '[₩Δ]' R E*k А×ҮН+E*K	0,100 0,1102 0,1592 0,4154 0,5154 0,51550 0,51500 0,515500 0,515500 0,5150000000000
ROBABILITY CESSIVE 31	22 24 24 24 24 24 24 24 24 24 24 24 24 2	THE PRUBABLE R	0.2861 0.2861 0.2861 0.2861 0.2861 0.2861 0.2861 0.2861 0.2861 0.2861 0.2861 0.2861
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•	x1 343.000 291.000 288.036	кМ- (YEAR)	~ <u>~</u> ~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~
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PROBABOLITY ANALYSIS OF SUCCESIVE 3 DAY MAXIMUM RAINFALL AT PROME APPENDIX E-23

10828172.00 8242408.00 7762392.00 7598424.00 6331625.00 5939765.00 593961.00 25971323.00 2863289.00 2863289.00 2863289.00 2863289.00 2863289.00 2863289.00 2863289.00 2863289.00 2863289.00 2726394.00 2726394.00 2726394.00 2725636962.00 833052.56 1745161.00 1745161.00 1745161.00 1745161.00 1745161.00 1745161.00 1745161.00 1745161.00 177545.00 83052.56 197222.56 197222.56 197222.56 197222.56 197222.56 1745161.00 177552.00 177552.00 177552.00 1072545.00 1072545.00 1072545.00 900-6189016 9106819-00 636056.00 314432.00 644076-31 EeeX 511809.94 19717.58 4624.00 2**X PROJECT **** -HAZEN PLUT(T) THOMAS PLUT(%) 956-67 957-67 95 THE PROBABILITY OF EXCEEDANCE ON IRRAWADDY M/P **Η**λλ ≠ SUCCESSIVE 3 DAY MAXIMUM RAINFALL AT PROME 130.62100 J. 90/8/ J. 90326 J. 80907 J. 19458 J. 19451 J. 41237 2**Y ≍ *Y 2.34944 2.31037 2.30173 LOG(X+B) 2-04357 2-04355 66610°2 ..98370 .976d3 .95168 - 94620 10516. 16196. L.84726 194.945 187.349 187.349 183.449 183.449 185.511 155.511 155.511 155.511 155.511 155.511 155.511 155.511 155.041 113.159 114.25.455 122.047 122.047 122.047 122.159 122.155 104.11 10.5555 10.5555 10.5555 10.5555 10.5555 10.5555 10.5555 10.555 223.583 204.349 200.349 96.329 44.805 94.551 89.471 88.344 70.J44 801.68 8+X 2.3445 2.29545 2.29567 2.29567 2.295795 2.25792 2.25792 2.25792 2.15529 2.15529 2.15529 2.15529 2.15723 2.15723 2.15723 2.15723 2.15723 2.15723 2.15729 2.15729 2.15729 2.19206 2.19206 2.19236 2.19206 2.2,0206 2 154699 194474 194474 194474 119469 1193450 1193450 1193450 2,01014 20119. (X) 20 7 221.234 202.000 198.000 181-102 155-706 154-432 151-15 87.122 86.360 86.000 86.000 96.596 85.000 02+362 086.66 92.456 92.242 × × YEAN т х S ž CHCER ICIAL Méan

n h i Frank i Angelan h i A

THE PROBABILITY OF EXCEEDANCE ON IRRAWADDY M/P PROJECT	SUCCESSIVE 3 DAY MAXIMUM RAINFALL AT PROME	с п	*X5-XU**2 X1+X5 Z*X0-[X1+X5) B1 289.234 -15 <i>1</i> 4.482 -50.135 -50.135	753.445 -30.174 480.719 -26.534	IGTAL BI = NEAN B =	B * 2.349	• [HA] * HETHUD ****	∆≈⋎⋈+E¢R C≖10¢≠A b X≖C−B	131,367 2,349	168.828 2.349	192.489 2.349		242.292 2.349	262.831 2.349	2.4520 283.135 2.349 280.785	309-801 2.349	2.5185 330.026 2.349 327.677
DANCE ON IRRAW	JM RAINFALL AT							A=YH+E+R C	2.1185	2.2274	2.2844	2.3559	2.3843	2.4197	2,4520	2.4911	2-5185
EEDANCE OF	IMUM RAINF	- עארטנ		•	_		יןאטטאטרפ values איע יואאוי			•							
TY OF EX	3 DAY MA		x1*xS 15043.906	11372.000		t.	ABLE VALU	т *ш		11 0.1040			31 0.2459		2526.0 15		
PROBABILI	CCESSIVE	****	x5 60.000	86,000 86,460			тне рицва	Ŧ	0.1831	0.1811	U.183	0.1831	0-1831	-			
••••• THE	x: SU		x [221.234 6				* * *	ш	0.0	0.5951	0.9062	1.2567	1.4520	1-6450	1.0215	2.0350	2.1850
			СНБЕР X 1 221	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	n			461UHN- PLH100 17641	7	2	10	0F	50	100	200	500	1 000

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PROBABILITY ANALYSIS OF SUCCESIVE 3 DAY MAXIMUM RAINFALL AT HENZADA APPENDIX E-24

27268096-00 18191440-00 15660537-00 15660537-00 15660537-00 15669574-00 15669574-00 15669574-00 115699 100-0011200 11679176-00 546763-00 5467463-00 5467463-00 5467463-00 5467463-00 5467463-00 5475463-00 5 201482256•00 8059290•00 5 + + X 90594.81 69169.00 62595.00 62595.00 62295.00 62295.00 51448.18 5148.18 51948.48 338749.00 49395.04 33162.82 33162.82 292816.19 292816.19 292816.19 292816.19 292816.19 292816.19 292816.10 292816.10 292816.10 292816.10 292816.10 292816.10 292816.10 292816.10 292816.10 292816.10 292816.10 292816.10 292816.10 292816.10 29381.00 293822.00 20381.00 203822.00 20382.00 20382.00 20382.00 20382.00 20382.00 20382.00 20382 950375-06 38015-00 X # # 2 **** ~ HAZEN PLUT(2) PROJECT THUMAS PLUTIXI 992.31 849.42 849.42 849.42 849.42 847.42 847.42 845.42 853.45 85 THE PROBABILITY OF EXCEEDANCE ON IRRAWADDY M/P HΥΥ SUCCESSIVE 3 DAY MAXIMUM RAINFALL AT HENZADA h 4.47210 111.80243 ΥΥ = Σ**2

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скоен 30	×1 300-440 1	¥\$ 14.620	×1+X5 40519.223	•1×	x1+x5-x0++2 435-610	X1+X5 6455+523	2+X	_
26	-	34.620	55405-043		397.620	1341.344	-28-493	93
2	1 000.162	000-76	000-196.46	5	000.885	106.626	101AL #1 = = = = = = = = = = = = = = = = = =	•
	* * * *	THE PRUB4	THE PRUBABLE VALUES BY 'IMAI'	Es UY	. [4 4] .	METHOD +	****	
PLRICD IYEAR)	п	x	E+K		A=YM+E+K	C+10++A	Ą	X=Ú−IJ
2	0.0	0.2015	15 0.0		1011.2	124.861	-51.149	182-630
5	1364.0			194	2.2300	169.831	-53.769	223.600
10	0.9062	0.2015		0.1826	2.2927	196.198	-53.769	244.967
30	1.2467			612	2.3114	235.163	-51.769	268.932
20	1.4520			0.2925	2.4027	252.730	-53.769	306.499
100	1.6450			114	2.4415	276.402	-53.169	330.171
200	1.8215			670	2.4171	299 986		353.155
500	2.0350	0,2015		100	2.5201	341.219	-53.769	384.988
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APPENDIX E-25 PROBABILITY ANALYSIS OF SUCCESIVE 6 DAY MAXIMUM RAINFALL AT THARRAWADDY

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ITY OF EXCI Ğ DAY MAXI	H+X	Z-56937 5548 354-244 Z-569379 522-2548 Z-5528 322/2575 Z-5528 322/2575 Z-552615 229-294 Z-46515 254-199 Z-44345 254-199 Z-44345 254-199 Z-44445 254-199 Z-44445 254-199 Z-44445 254-199 Z-4464 254-199 Z-40541 221.9915 Z-35066 219-241 Z-35066 219-241 Z-35061 101-211-015 Z-35061 101-211-015 Z-25001 101-015 Z-25001 101-015 Z-2500	+××××××××××××××××××××××××××××××××××××
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	YEAR	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	SX SX ES
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X: SUCCESSIVE G DAY MAXIMUM RAINFAL. AT THARRAWADDY b v A L U E ***** 2** b v A L U E ***** 2** b v A L U E ****** 2** b v A L U E ****** 2** b b v A L U E ****** 2** b b v a L U E ****** 2** b <th></th> <th>• • • • •</th> <th>THE PRC</th> <th>א גיוונא פ</th> <th>DF EXCE</th> <th>EDANCE ON I</th> <th>THE PROBABILITY OF EXCEEDANCE ON IRRAWADDY M/P</th> <th></th> <th>PROJECT *****</th> <th>: -</th>		• • • • •	THE PRC	א גיוונא פ	DF EXCE	EDANCE ON I	THE PROBABILITY OF EXCEEDANCE ON IRRAWADDY M/P		PROJECT *****	: -
<pre>x1 x5 x1+x5 x1+x5 x1+x5-x0*** x1+x5 1.000 150.622 558040.734 521.622 -2320.871 9.176 164-572 59114.133 523.748 912.527 10.000 181.356 60158.926 516.382 2557.320 181.356 60158.926 516.382 2557.320 ************************************</pre>		×		ESSIVE G D	аү махн	40M RAINFAL	. AT THARRAWI		UNIT -[M	
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1.000 150.662 59840.134 521.622 -2320.871 9.176 164-592 59114.133 523.748 912.527 9.176 164-592 59114.133 523.748 912.527 9.176 164-592 59114.133 523.748 912.527 9.176 164-592 59114.133 523.748 912.527 9.176 181.356 60758-926 516.342 2557.320 9.176 181.356 60758-926 516.442 2557.320 9.176 1441 0.0 2 256.73 256.41 10.1991 0.1401 0.00437 2.4420 276.41 266.41 0.1902 0.1401 0.1215 2.4420 216.41 266.21 216.52 10.1902 0.1401 0.20437 2.4420 216.208 216.52 <th>14. T. 11</th> <th>-</th> <th>7 X</th> <th>×</th> <th>۲• X S</th> <th>7 + + () x - 5 X + 1 X</th> <th>X1+X5</th> <th>1 < X + 1 X 1 - N X + Z</th> <th></th> <th></th>	14. T. 11	-	7 X	×	۲• X S	7 + + () x - 5 X + 1 X	X1+X5	1 < X + 1 X 1 - N X + Z		
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L R E-R A=YM+E+R C=10**A U-U U-U U-U U-U Z-3581 Z20**A U-U U-U U-U U-U Z-3581 Z20**A U-U U-U U-U U-U Z-3581 Z20*181 U-U U-U U-U U-U Z-3581 Z20*181 U-UU U-U U-U U-U Z-4458 Z0*026 U-U U-U U-U U-U Z0*125 Z0*026 U-Z061 U-U U-1215 Z-5425 Z0*026 Z0*128 U-Z010 U-1401 U-Z041 Z-5562 Z05*204 Z0*1261 U-A500 U-1401 U-Z041 Z-54265 Z11-6510 Z0*141 U-A500 U-1401 U-Z041 Z-6445 X11-6510 Z0*141 Z-U450 U-1401 U-Z041 Z-6445 X1-1610 Z0*141 Z-U450 U-1401 U-Z041 Z-6445 X1-1610 Z0*141 Z	HE LUHN-									
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2.1450 0.1401 0.3074 2.4656 463-070				11407	0.284	-	441.110	-12.159	453.869	
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	SUCCESSIVE	G DAY MAXI	MUM RAINE	O DAY MAXIMUM RAINFALL AT PROME	យរ	M M)- LINU	-	
			* >	= 77	THUMAS	HAZEN		
×	{ x } 907	£1 + X	FUG[X+8]	5 e e 2	PLUT(1)	PL01(\$)	X++2	n + + X
りをちょうも		400.1UE	2.47869	-	90-01	93.28	100001-19	31623344.00
245.364		230.219	2.36214	-	66.69	44.83	60203.45	14771752-00
232.000	2.30549	216.855	2.3361/	5.45768	0.0	m	53824.00	•
230.886		215.741	£9165.5		86.67	1.9	Ň	12308132-00
221.000		205.855	2.31,356	ທີ	n,	84.48	4841-00	10793861-00
209.300		143.855	2.28748		0.0	61.03	43681.00	9129329.00
208.534		141.389	2.28643	ທ້	10-01	11.59	43486.39	9068388.00
206-502		146.141	2.24184	'n	13-33	74.14	42643.04	8805870.00
195.326		180.181	2.25311	ъ.	10.00	10.69	38152-21	7452115-00
186.690		1/1.545	2.23438	4	66.67	67.24	34853.12	6506726°00
186.690		111.545	2.21438	3	63.33	63.79	34853.12	6506726-00
1 80 - 848		165.703	2-21933	4	60.00	60.34	32/05+98	5914808.00
180.340		165.195	2.21800		56-67	56.90	32522+49	5865104.00
117-546		162.401	2.21059	3	51.13	53.45	31522.55	5596700-00
169.L04		154.019	2-18/57	4	20-00	\$0°-00	28616-44	4640869-00
160-001		144.455	2,16093	3	46-67	46.55	25600-00	4096000.00
151.872		1,1,1,1,1	2-13592	4	66.64	43.10	23071.15	3504321.00
151.130		115.985	2.13349	4	40.00	39.66	22840.25	3451846.00
151.000		246.211	2.13307	4	36.67	36.21	22801-00	3442951.00
148.082		112.517	2.12364	ч. Ч	33.33	32.76	21928.26	3247178-00
121.000		458.111	2,04865	3	00.06	29.31	16129.00	2048383.00
126.442		111.347	2.04668	4	26.67	25.46	16000.21	2023897.00
126.235		60-111	2.04568	4.18483	23.43	22.41	15936.01	2011729.00
125-476		166.011	2.04270	4.11200	20.00	18.97	15744.20	1975518.00
124.918			2.0+069	4.10442	16.67	15-52	15616.98	1951622-00
122.174		107.029	2.02950	+.11887	13.33	12.07	14926-47	362
117.348		102.201	2-00446	4.03/93	10.00	8-62	13770 54	1615943-00
112.776		97.631	1.98459	J.95845	6-67	5.17	12718.41	543
104.000		228°88	1.94068	J.19735	3-33	L-72	10816-00	1124864-00
		-	63.12814	131.90195			927112-13	185422928+00
172.23	2.22013 YM		= 2-17685	4. <i>1</i> 5524 =	үүн		31969.38	6393894-00
	ί.Σ		- 0.1051.0 -					

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APPENDIX E-26 PROBABILITY ANALYSIS OF SUCCESIVE 6 DAY MAXIMUM RAINFALL AT PROME

	- X V		11	-60.412	-4.301	19-276	-45.436	~15.145	- 15. 145			9-	908	310	280	143	224	101	845	186	615
PROJECT	M M)- TINU		+ X 5 J	:13	5	131	W	"	=			X=C-B	165.408	208-810	236.280	276.	294.224	318-101	341-845	186-211	376-615
	NÙ		(< X + X) - OX + 7	-88.213	-26-123	-17.331	IGIAL BI	MÊAN Ê	ىد	• • • • •		Ð	-15.145	221061-	-15.145	-15.145	-15.145	-15.145	-15.145	-15.145	-15.145
THE PROBABILITY OF EXCEEDANCE ON IRRAWADDY M/P	AT PROME	÷	5 X + 1 X	010-9263	112.348	-334.082				мЕТНОЙ ••		C = 10++A	150.263	143.641	221.135	261.197	219.013	103.016	326.700	351.810	141.470
DANCE ON IR	SUCCESSIVE & DAY MAXIMUM RAURFALL AT PROME	***** 7 A 7 V A	X1+X5-XU++2	420.230	041-bcC	347.34H				THE PRUHABLE VALUES NY "[WA]"		А≖Үм+Е≠К	2.1169	2.2311	2.3447	2.4170	2.4451	2.4815	2.5141	1646.5	2.5815
OF EXCEE	AY MAXIMI	- م ا	X (X)X		27611.148	21224.114				VALUES N		н+3	0.0	0.1102	0.1678	0.2401	6692-0.	0.3046	1,56.0	0.1763	0.4046
BABILITY	ESSIVE & D	8	×							PRCHAULE		a	0.1852	0.1052	0.1452	0.1852	0.1452	561.0	U.IU52	4.1452	0.1452
	X: SHCCE	•	X 5	104-400	112.1	111.348						4	0.	0.5951	0.9062	1.2967	1.4520	.4450	1.8215	2.0150	0,1850
* * *	â			316.230	245.364	212-000				4 9 3 9 5		EARJ	n	•	8			-	-	2	
			CHDEN		2	~					PEIUKN-	FEHIOU TYEAR)	~	ŝ	10		50	001	200	500	0001

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PROBABILITY ANALYSIS OF SUCCESIVE 6 DAY MAXIMUM RAINFALL AT HENZADA APPENDIX E-27

38119552,00 37259696,00 3195240,00 3196240,00 29510240,00 28175408,00 28175408,00 28175408,00 20542912,00 20542912,00 13997521,00 13997521,00 12969577,00 12969577,00 12969577,00 12969577,00 12969577,00 12969577,00 12969577,00 44869696.00 44485968.00 10679668.00 10569191.00 8969339.00 7716834.00 7569007.00 520947712.00 20837904.00 5845101.00 E**X 126270.56 125549.63 11365-75 111556-00 111556-00 101860-88 101568-00 95710-88 92593-44 92593-44 75251.31 74529.00 69244.63 61009.00 55799.00 55701.46 55201.46 55201.46 55201.46 51964-00 48495-92 48160-89 43169.16 39050.46 38550.14 32522.48 1825670-00 73026-75 X + + 2 **** NNIT - LINU PROJECT HALEN PLOT(I) 94.00 94.00 94.00 94.00 94.00 94.00 94.00 94.00 94.00 954.00 954.00 954.00 954.00 954.00 954.00 954.00 85.000 85.000 85.000 85.000 THUMAS PLUT (T) 90.15 92.31 94.55 84.65 84.65 84.65 70.92 70.92 250.02 250 THE PROBABILITY OF EXCEEDANCE ON IRRAWADDY M/P 6.45U14 = YYM SUCCESSIVE & DAY MAXIMUM RAINFALL AT HENZADA 6.70661 6.66409 6.51919 6.51319 6.45734 6.45734 6.25734 6.28064 6.27201 6.27201 6.27201 6.27201 6.27201 6.24508 6.24508 6.98701 6.98171 6.887171 6.887171 6.84717 6.847327 6.47327 6.73584 6.08008 0.0454 ×γ γ¢α2 5.99494 5.87082 161.25343 2.62169 2.61586 2.60906 2.59535 Y = LOGIX+8} 2.64229 2.62433 2-55327 2-54113 2-52048 2-51255 2.49484 2.48389 2.46578 2.45042 2.4446 2.44390 2.58149 2.50440 2.50612 2.50440 2.58971 2-55487 2.50301 19285-2 2.42248 = RU01<xxAH-XH+XH> = RU01<xxAH-Z+XH+Z+XH+==]/(5X==3)= 0.26789 =[XXXH-3=XXH+Z++Z+XH==]/(5X==3)= 438-826 421-046 421-046 418-496 412-496 495-496 393-868 3888 292-263 282-108 280-838 434.842 141.446 158.816 351.496 320.716 304-714 147.640 331.446 125.496 118.430 319.446 119.446 312.496 244.830 8+X 2,54941 2,52105 2,52375 2,52375 2,50786 2,50786 2,49048 2,49048 2,47276 2,43826 2,43826 2,43826 2.43616 2.42019 2.19270 2.19202 2.17342 2.17048 2.17098 2.17098 2.170909 2.195193 2.357285 2.357285 2.357285 2.357285 2.29301 2.55065 .31759 .29581 LUG(X) <#X+#X+#X+>100H = 273.300 263.144 241.000 241.000 241.000 241.000 234.950 234.950 234.914 2234.000 114.000 128.422 122.010 122.010 304-292 220.218 219.456 201.112 354.330 191.612 214.320 1 80.140 955.340 × × YEAR X X X V IUTAL GHOER MEAN

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	(U-(x1+x5) -15.424 -30.410 -13.900 -13.900 TAL B1 EAN B =	, X	
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PROJECT *****

••••• THE PROBABILITY OF EXCEEDANCE ON IRRAWADDY M/P

SUCCESSIVE & DAY MAXIMUM RAINFALL AT HENZADA

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Appendix E-27 Page - 2

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APPENDIX E-28 5-DAYS TOTAL RAINFALL AT THARRAWADDY

			1976 (Unit:	mm)
Day	July Daily	August Daily	September Daily	October Daily
1	6.0	17.0	22.0	5.0
2	2.0	26.0	1.0	J.U
- 3	45.0	_	1.0	3.0
<i>L</i> į	23.0	7.0	10.0	39.0
5	27.0	-		3.0
Sub-total	103.0	50.0	34.0	50.0
6	4.0	2.0	_	-
7	40.0	4.0	4.0	2.0
8	6.0	-	54.0	-
9	27.0	6.0	4.0	_
10	18.0	1.0	1.0	-
Sub-total	95.0	13.0	63.0	2.0
11	6.0	37.0	1.0	21.0
12	6.0	2.0	12.0	-
13	3.0	52.0	14.0	2.0
14	~	3.0	5.0	3.0
15	4.0	58.0	28.0	5.0
Sub-total	19.0	152.0	60.0	31.0
16	3.0	15.0	7.0	-
17	21.0	1.0	-	-
18	53.0	2.0	-	9.0
19	55,0	-	_	-
20	14.0	-	-	6.0
Sub-total	146.0	18.0	7.0	15.0
21	25.0	•	-	49.0
22	3.0	-	3.0	59.0
23	-	-	13.0	-
24	2.0	4.0	41.0	-
25	14.0	2.0	25.0	-
Sub-total	44.0	6.0	82.0	108.0
26	22.0	13.0	3.0	-
27	9.0	1.0	5.0	3.0
28 -	7.0	3.0	7.0	_
29	-	52.0	-	-
30	3.0	32.0	-	-
31	8.0	-	-	-
Sub-total	49.0	101.0	15.0	3.0

APPENDIX E-29 5-DAYS TOTAL RAINFALL AT HENZADA

1971 (Unit: mm)

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Day	July Daily	August Daily	September Daily	October Daily
1	8.0	10.0	4.0	15.0
2	51.0	85.0	-	-
3	26.0	10.0	-	-
4	32.0	4.0	46.0	1.0
5	4.0	21.0	9.0	1.0
Sub-total	121.0	130.0	59.0	17.0
6	3.0	11.0	_	-
7	46.0	47.0	-	~
8	5.0	10.0	-	~
9	8.0	14.0	26.0	~
10	32.0	4.0	-	-
Sub-total	94.0	85.0	26.0	-
11	84.0	9.0	-	-
12	1.0	5.0	1.0	5.0
13	6.0	36.0	4.0	1.0
14	8.0	2.0	-	, 🗕
15	-	47.0	~	-
Sub-total	99.0	99.0	5.0	7.0
16	11.0	2.0	20.0	-
17	35.0	2.0	~	
18	36.0	8.0	5.0	-
19	70.0	29.0	-	-
20	90.0	4.0	-	-
Sub-total	242.0	45.0	25.0	-
21	66.0	6.0	2.0	-
22	37.0	41.0	5,0	-
23	2.0	28.0	-	-
24	20.0	12.0	-	-
25	51.0	6.0	1.0	-
Sub-total	176.0	93.0	8.0	-
26	36.0	35.0	2.0	8.0
27		23.0	30.0	22.0
28	22.0	14.0	5.0	33.0
29	32.0	16.0	10.0	15.0
30	21.0	1.0	33.0	7.0
31	~	12.0	-	-
Sub-total	111.0	101.0	80.0	85.0

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(A=5,844 ha)

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Period	5 Day <u>Total</u> (mm)	Discharge (m ³)	Accumulated Discharge (m³)	Inner Water Level (m)	Outer Water Level (m)	Remark
7.1-5	103	3,009,660	3,009,660	12.20	13.57	-
10	95	2,775,900	5,785,560	12.40	14.27	
15	19	555,180	6,340,740	12.45	14.95	
20	146	4,266,120	10,606,860	12.75	15.27	
25	44	1,285,680	11,892,540	12.85	15.26	
31	49	1,431,780	13,324,320	12.95	15.52	
8.1-5	50	1,461,000	14,785,320	13.00	15.65	
10	13	379,860	15,165,180	13.05	15.84	
15	152	4,441,440	19,606,620	13.12	16.42	
20	18	525,960	20,132,580	13.15	16.55	
25	6	175,320	20,307,900	13.15	15.90	
31	101	2,951,220	23,259,120	13,20	15.01	
9.1-5	34	993,480	24,252,600	13.25	14.74	
10	63	1,840,860	26,093,460	13.30	14.95	
15	60	1,753,200	27,846,660	13.35	15.32	
20	7	204,540	28,051,200	13,35	15.11	
25	82	2,396,040	30,447,240	13.40	15.08	
30	15	438,300	30,885,540	13.42	15.00	
10.1-5	50	1,461,000	32,346,540	13.45	14.69	
10	2	58,440	32,404,980	13.45	14,41	
15	31	905,820	33,310,800	13.50	14.04	
20	15	438,300	33,749,100	-	13.03	
25	108	3,155,760	36,904,860	-	11.63	
31	3	87,660	36,992,520	-	11.02	

Note: Outer Water Level --- Gamon ST. + 2.0 m

APPENDIX E-31 WATER BALANCE AT INGABU AREA

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					$\{A = 15, 0\}$	00 ha)
Period	5 Day <u>Total</u> (mm)	Discharge (m ³)	Accumulated Discharge (m ³)	Inner Water Level (m)	Outer Water Level (m)	Remark
7,1-5	121	9,075,000	9,075,000	10.25	11.68	
10	94	7,050,000	16,125,000	10.40	11.97	
15	99	7,425,000	23,550,000	10.60	12.78	
20	242	18,150,000	41,700,000	11.00	13.08	
25	176	13,200,000	54,900,000	11.20	13.00	
31	111	8,325,000	63,225,000	11.30	13.41	
8.1-5	130	9,750,000	72,975,000	11.40	13.40	
10	86	6,450,000	79,425,000	11.45	13.79	
15	99	7,425,000	86,850,000	11.50	14.45	
20	45	3,375,000	90,225,000	11.60	14.06	
25	93	6,975,000	97,200,000	11.65	13.44	
31	101	7,575,000	104,775,000	11.75	11.91	
9.1-5	59	4,425,000	109,200,000	11.80	12.28	
10	26	1,950,000	111,150,000	11.80	13.10	
15	5	375,000	111,525,000	11.80	13.34	
20	25	1,875,000	113,400,000	11.80	12.62	
25	8	600,000	114,000,000	11.80	12.37	
30	80	6,000,000	120,000,000	11.90	12.59	
10.1-5	17	1,275,000	121,275,000	11.90	12.60	
10	-	-	121,275,000	11.90	11.92	
15	7	525,000	121,800,000	11.90	11.51	
20	-	-	121,800,000	-	10.52	
25	~	-	121,800,000	-	8.67	
31	85	6,375,000	128,175,000	-	8.14	

Note: Outer Water Level --- Henzada ST. (1974)

(A = 15,000 ha)

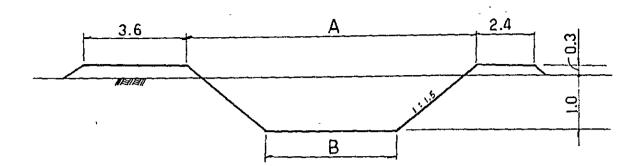
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APPENDIX E-32 WATER BALANCE BY PUMP DRAINAGE AT INGABU AREA

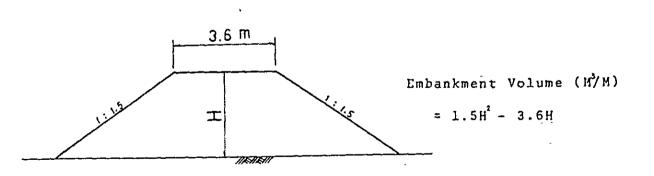
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42	' .,				(A=15,0)00 ha)
Period	5 day <u>Total</u> (mm)	Discharge (m ³)	Accumulated Discharge (m³)	Inner Water Level (m)	Outer Water Level (m)	Remark
7.1-5	121	9,075,000	3,891,000	10.10 -	11.68	
10	94	7,050,000	5,757,000	10.15	11.97	
15	99	7,425,000	7,998,000	10.20	12.78	
20	242	18,150,000	20,964,000	10.50	13.08	
25	176	13,200,000	28,980,000	10.70	13.00	
31	111	8,325,000	31,084,200	10.75	13.41	
8.1-5	130	9,750,000	35,650,200	10.80	13.40	
10	86	6,450,000	36,916,200	10.80	13.79	
15	9 9	7,425,000	39,157,200	10.95	14.45	
20	45	3,375,000	37,348,200	10.90	14.06	
25	93	6,975,000	39,139,200	10,95	13.44	
31	101	7,575,000	40,493,400	11.00	11.91	
9.1-5	59	4,425,000	39,734,400	10.95	12.28	
10	26	1,950,000	36,500,400	10.90	13.10	
15	5	375,000	31,691,400	10.75	13,34	
20	25	1,875,000	28,382,400	10.70	12,62	
25	8	600,000	23,798,400	10.60	12,37	
30	80	6,000,000	24,614,400	10.60	12,59	
10.1-5	17	1,275,500	20,705,400	10.50	12.60	
10	-	-	15,521,400	10.35	11.92	
15	7	525,000	10,862,400	10.25	11.51	
20	-	~	5,678,400	10.15	10.52	
25	-	-	494,400	10.00	8.67	
31	85	6,375,000	648,600	10.00	8.14	
) ma 	1					

Note: Outer Water Level --- Henzada ST. (1974) Pump Discharge --- 12 m³/sec



Type	Area (HA)	Discharge (M/SEC)	A (M)	<u>B</u> (M)	<u>Cut</u> (M7M)	Embankment (M7M)
I	500	1.6	4.4	0.5	2.0	2.1
II	1,000	3.2	6.4	2.5	4.0	2.1
III	1,500	4.8	8.4	4.5	6.0	2.1
IV	2,000	6.4	10.4	6.5	8.0	2.1
v	3,000	9.0	14.4	10.5	12.0	2.1



APPENDIX E-33

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TYPICAL CROSS SECTION OF DRAINAGE CANAL AND EMBANKMENT

APPENDIX E-34 DIFFERENCE EXPRESSION OF THE FUNDAMENTAL EQUATIONS

In the flow status of a river, there are two physical phenomena. One is a steady flow that is constant with time, other is an unsteady flow that is changeable with time.

In analysis of an unsteady flow, it is necessary to solve the differential equation. But this equation is a non-linear type, so it is very difficult to solve it directly. Then, it will be solved by means of numerical analysis, which is a kind of mathematical simulation. Here, the Dr. Shiraishi's method is adopted that is famous and popular in Japan.

Hydraulic characteristics of an unsteady flow as a mathematical model are given by simultaneous solution of both the equation of motion and that of continuity. With the down stream boundary as origin the fundamental equation of a one-dimensional flow are expressed as follows;

$$\frac{1}{g}\left(\frac{\partial v}{\partial t}\right) + \frac{1}{g}\frac{\partial}{\partial x}\left(\frac{v^2}{2}\right) + S + \frac{\partial h}{\partial x} + \frac{n^2 |v|}{R^4 x^3} v = 0$$
(1)

$$\frac{\partial A}{\partial t} + \frac{\partial Q}{\partial x} - q = 0 \tag{2}$$

Where;

- g: acceleration of gravity (9.80 m/sec²)
- v: velocity (positive for the upper stream direction)(m/sec)
- t: elapsed time (sec)
- x: distance in longitudinal directions on a horizontal datum plane (m)
- s: river bed slope
- h: water depth (m)
- n: Manning's roughness conefficient
- R: hydraulic radius (m)
- A: cross-sectional area including swampy zone
- 0: discharge through a section (m^3/sec)

q: lateral inflow per unit length (positive for inflow, negative for outflow) (m³/sec/m)

In case of hydraulic analysis of mathematical model, these equation, (1) and (2), are converted into difference expressions. Then, for the given initial condition, boundary condition and geometric conditions, the numerical integration is performed. It is desirable to constitute the efficient and economic grid system from the point of the electronic computer performance. The calculation proceeds from the down stream to the upper stream with the distance interval Δx and the time interval Δt . The selection of the time interval to be used is not arbitrary. It is well-known that solving by finite differences method will not produce a stable solution unless the distance interval and the time interval are related to the velocity of the long wave, such as

$$\Delta t < \left| \frac{\Delta x}{v_{max} \pm \sqrt{g h_{max}}} \right|$$
(3)

If the value of Δt exceeds that given above, the transmission of the hydraulic phenomena goes beyond the tracing speed in the mathematical model and the solution is led to uncoveragence. The value of Δt and Δx must be determined to satisfy the expression (3), by speculating in advance the maximum possible velocity and water depth.

The accuracy of the mathematical model is determined by the difference expressions of the fundamental equations. By Dr. Shiraishi, the method of the central difference expression with respect to distance x and time t is studied.

In the difference expression suffix i is used for distance and n for time.

The difference center is taken at the point (i, n-1), and from the initial conditions and the boundary conditions, the unknown values at the point (i, n) are obtained. From the downstream to the upper stream, the calculation proceeds with distance interval x and the time interval t. (See Figure 1)

1) Difference Expressions of the Equation of Motion

In the equation of motion (1), the central differences for respective terms are expressed as follows.

$$\frac{\partial v}{\partial t} = \frac{n^{v}i - n - 2^{v}i}{\Delta t}$$

$$\frac{\partial h}{\partial t} = \frac{n - 1^{h}i + 1 - n - 1^{h}i - 1}{\Delta x}$$

$$\frac{\partial v^{2}}{\partial x} = \frac{n - 1^{v^{2}}i + 1 - n - 2^{v^{2}}i - 2}{2\Delta x}$$

$$S = \frac{Z_{i+1} - Z_{i-1}}{\Delta x}$$

$$h = \frac{n - 1^{h}i + 1 + n - 1^{h}i - 1}{2}$$

$$V = \frac{n^{v}i + n - 2^{v}i}{2}$$

$$[V] = [n - 2^{v}i]$$

Here, z is the bottom elevation, that is the river bed elevation.

The value of $n^{v}i$ is calculated by substituting the difference expressions above into the equation of motion (1). (See Figure 2)

The value of $n^{v}i$ is thus drived from two values of water depth at time n-1 and three values of velocity n-2.

2) Difference Expressions of the Equation of Continuity

In the equation of continuity (2), the central differences for respective terms are expressed as follows.

$$\frac{\partial A}{\partial t} = \frac{n^{A}i - n - 2^{A}i}{\Delta t}$$
$$\frac{\partial Q}{\partial x} = \frac{1}{\Delta x} \left(\frac{A_{2} + A_{3}}{2} V_{m} - \frac{A_{1} + A_{2}}{2} V_{g} \right)$$

The cross-sectional area at point m is given by $(A_2 + A_3)/2$, and that at point l is $(A_1 + A_2)/2$. The velocity at points m and l, Vm and VL, respectively, are already obtained from the equation of motion. Hence the discharge through point m is given by $(A_2 + A_3)Vm/2$ and that through point is $(A_1 + A_2)VL/2$. (See Figure 3)

To obtain the cross-sectional area in the above difference expressions above, the backward water depth is used. The reason for it is that if a forward unknown value is used, the calculation becomes fairly complicated. Moreover, the central difference expression with respect to distance gives sufficient accuracy, because the change in cross-sectional area with respect to distance is far larger than that with respect to time.

The inflow to and outflow from the open channel concerned are treated by the term q.

The values of n^Ai is calculated by substituting the difference expressions above into the equation of continuity (2). (See Figure 4)

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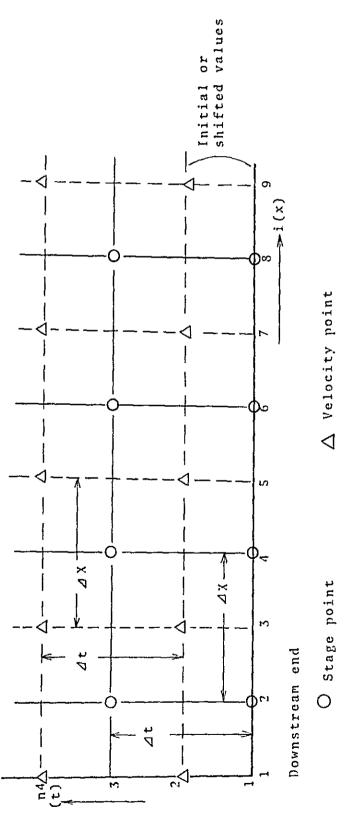
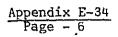
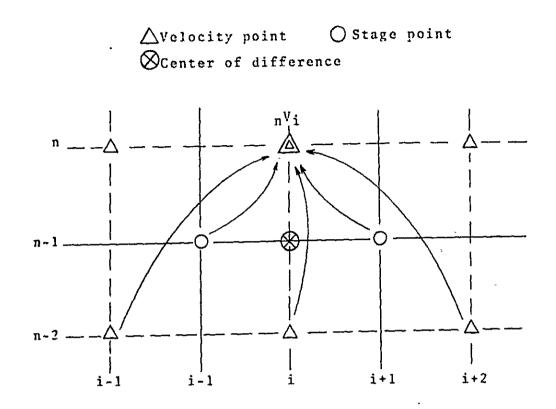


FIGURE 1 OPERATIONAL GRID SYSTEM

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FIGURE 2. OPERATIONAL GRID SYSTEM OF THE EQUATION OF MOTION

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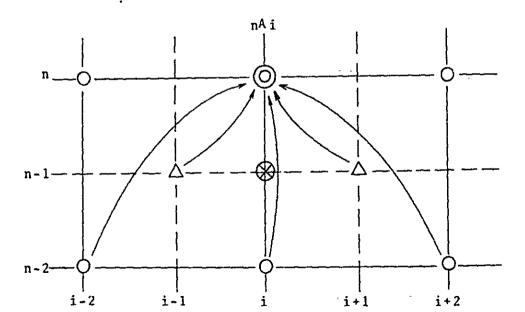
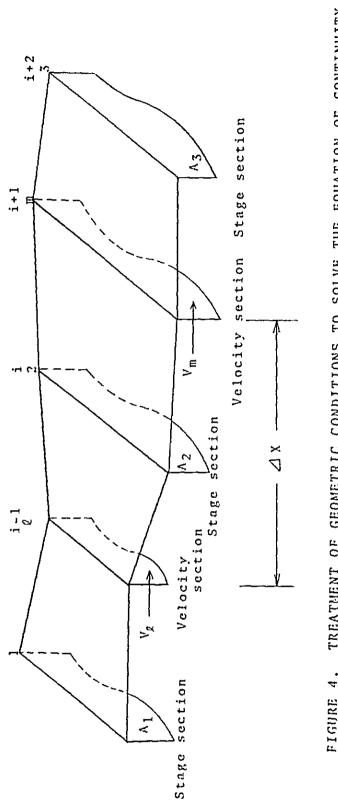


FIGURE 3. OPERATIONAL GRID SYSTEM OF THE EQUATION OF CONTINUITY





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APPENDIX E-35 THE RESULT OF HYDRAULIC ANALYSIS

1 14 1 8-349 0-124 7-124 351-7 351-7 351-7 351-1 2-400 1-0000 - 14 - 84 - 84 - 84 - 134 - 134 - 134 - 12 (13)(8.785 0.236 33.5 142.2 142.2 0.03000 l ---~)[9)(10)[11)[12][1 4 5.704 6.464 7.J11 8.039 6 10 0.427 0.422 0.413 0.378 C 115.3 109.1 115.7 81.3 2 2464 2.354 2.30.3 214.9 1 2.464 1.556 1.766 1.745 1 9 1.0.0300 0.000 0.0 \$ NU. NG. L PALNE NO. PRINT PKINT ------ננינייט
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 4.470
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 0.354
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 0.431

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 143.1
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 5
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 6
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 2.422
 2.415

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 2.412
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Page - 6 ۰. ۰. 14 11 10-785 0-355 0-355 228-1 642-3 642-3 0-0300 14 1 11.023 0.202 137-5 679-2 679-2 679-2 0.03000 14 1 16-842 0-303 197-2 651-1 651-1 - -1 13 1 10-663 0-384 160-8 160-8 418-3 2-224 0-03000 0 13 11 10,535 0,426 168,3 168,3 168,3 195,4 10,03000 0 1 13 11 10.947 0.329 156.0 474.0 2.355 0.03000 ł . -٠ --5 2 11 , (1 11)(12)(9.540 10.343 1 9.541 0.545 2.459.1 377.7 7.15.9 693.5 1 0.03000 0.03000 0. 12 15 9.651 9.515 2.815 2.420 2.420 0.03000 12 1(9.951 0.507 307.4 606.6 2.700 2.700 ì ġ 52 į -----(PRINT | PRINT PRINT 11 11 1 9-263 0-555 363-4 654-5 2-885 2-33400 0 LL 1 3-481 3-538 3-6-4 3-6-4 5-533 2-533 3-3900 ţ. ĺ -ł 10 112 8.112 0.550 0.550 330.9 2.110 2.005 1011 8-567 4-2567 4-23-67 7-275 7-27 [10)[8-685 0-645 470-2 728-5 3-204 0-03000 (ì K I VEK K I VEK 1 9 1 1.928 0.05.7 659.7 5.240 0.03000 0 1 9 1 7-940 6-052-5 6-25-5 1-2-206 1-2-206 1-2-206 1-2-206 9.25.5 1.255.5 r • THE HYDRAULLC AVALYSIS UP THE MUDLE KEACHES CP MYITMAKA doundary : Ci> nummarkaik Stafiun : C2> confluence mith irramaduy sectidim : 11) * Ci> : (5) udami 51. ; (11) udamun 51. ; (14) * C2> inffruen : dam 9au um 1JJJJ * : 01 * JJ sec. Periud : duming Jume TO Jeptember 1974 8 11 7-22 1 0-660 5 414-7 6 24-7 6 3-516 0 4-03000 1 4 197 7 197 7 197 0 674 6 214 0 242 3 498 0 3 498 e 4 7 1 6 414 0 6 40 0 6 40 0 6 40 4 4 1 0 6 4 1 4 2 4 2 4 0 0 0 0 0 1 1 0-680 0-680 0-680 0-680 0-680 0-680 0-680 0-680 0-000 1 1 6 1 5-736 0-517 451-2 451-2 0-050-2 0-050-2 1 6 1(5-046 0-686 440-6 440-6 440-6 3-620-6 3-621 3-3300 0 1 ~ -~ 0010 0110 0010 5 16 5 ** : MULH •0 HUKK HUUH ĭ] -----Ī 10 401-4 644-0 549-2 5-255 725-2 7002-5 ļ 3 16 3-978 3-978 5-19 1-919 1-919 9-0-0 9-0-0 9-0-0 9-0-0 1 ---DAY yeu DAY v v v 1 2 1 3.671 4.53.0 4.53.0 4.67.0 1.62.0 1.22.2 1.22.2 1.22.0 0.000 0.2 < 2 > 11.023 10.442 10.735 17 14 6 RIVER (NG.) (I) SECTIUN (ND.) (I) MATEX ST. (M) 3.450 WELULITY (M/SEC) 0.515 ULSUANCE (M+2/S) 0.0215 DISCAANUE (M+2/S) 0.0210 SECTUN (M+2/S) 11086.0144 HY. AADIUS(M) 6.444 AUUNNESSIMANNING) 0.03000 0. BUUNUAHY [NU.] < 1 > < WATER STAGE [M] 3.755], WIVER [NO.] []] SECTION [NO.] []] WATER ST. [M] 3.755] VELUCITY [M/SEC] 3.463] VELUCITY [M/SEC] 3.463] DISCHARGE [M003/S] 573.1 5 SECTION [M002] 12446] SECTION [M002] 1246] SECTION [M002] 1466] 1466] SECTION [M002] 1466] 1466] 1466] 1466] 1466] 1466] 1466] 1466] 1466] 146 v я 1 śi 1 > 1 > 3-846 UAY 1 0 av DAY] ------v v BOUNDATY (NU-) C WATER STAUE (N) C BIV-H (NC-) F Stufter St. (N--) F WELULITY (N-2) DELEULATY (N-2) SELEULATY (N-2) SUUSH 455(41001 0) U (• 0N) BOUNDARY WATER STAGE ł

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Appendix E-35

ł Appendix E-35 Page - 9 ł i 14 1 10.633 1.354 1 2.1345 6.1849 9.88 9.88 1.03000 1 10-145 0-293 159-4 3-562 10-241 0-333 186-3 559-1 559-1 3-647 0-03000 (9)(10)(11)(12)(13)(14) 6.641 7.363 8.156 8.976 9.939 10.145 0.493 0.478 0.474 0.461 0.370 0.293 2.141 2094 198.4 11810 0.293 2.2141 2094 198.4 18.7 3928 3.562 2.307 1.999 2.165 1.781 1.882 3.562 0.03000 0.03000 0.03000 0.03000 0.03000)(11)(12)(13)(0 8.062 8.897 9.982 18 0.467 0.470 0.402 187.3 176.7 121.3 4 401.2 375.8 302.0 2 2.133 1.712 1.903 0 0.03000 0.03000 0.0 1 11 11 12 11 13 11 13 11 4 8-472 9-371 10-375 1 4 0-532 0-519 0-428 4 256-9 1572 2-054 4 426-5 476-9 366-6 4 2-240 2-159 2-092 0 0.13000 0-03000 0-03000 26 1 ---27.) 28 1 PRINT NO-PRINT NO. ---- PRINT NO. -Ï :1 ÷ AIVER River ij 9 11 5-560 0.475 0.476 187.4 187.4 187.4 2.293 0.03000 1 9 6+753 2+5+3 2-25+3 7-27+7 2+327 2+327 2+327 HYDRAULIC ANALYSIS UF THE MODEL OF THE MIDDLE REACHES OF MYITMAKA VOARY : <1> KUNHAYKAIK STATION : <2> COMFLUENCE WITH IRRAWADDY TION : (1) = <1> ; (5) UAWL ST. ; (11) GAMHUN ST. ; (14) = <2> ERVAL : DX= 9500 OR 10000 M ; DT = 600 SEC. ŧ 11 5 11 6 11 7 11 8 11 15 4.705 4.981 5.416 5.984 27 0.380 0.436 0.460 0.499 1 250.2 233.7 209.0 1 255.8 468.4 418.9 1 5.580 3.115 2.781 2.556 1 0.0.03000 0.03000 0.03000 0. i 6 10 5 954 0 479 1 4479 1 4484 4 1441 2 5 5 3 3 0 0 0 ÷ 7)(0.442 0.468 219-7 219-7 469-7 2.785 2.785 01.00 1 ł 539.1 539.7 539.7 539.7 539.7 539.7 539.7 5300 (1 1 0,,,,,,,, ÷ 0100) 0:00 1 • BOUNDARY : (12 KUNHAYKAIK STATION : (Section : (1) = (12 ; (5) Uammi ST. ; (imterval : UX= 4500 Om 10000 m ; 0 period : DUMING JUME [0 september 1974 ; ----- HOUK : 26 DAY] HUUR : " MOR)-----11 3 11 4 11 3 4.445 4.249 4.245 1.332 4.245 0.2312 4.245 2.11 4.245 8.17 5 5.201 0.000 0.000 0.0 *********** ۱ 4-535 0-327 204-4 814-9 414-9 414-9 4-410 0-03000 1- 13 144 ł i RIVER (ND.) [] [2] 3] SECTIUN (ND.) [1 2] 4.435 WATER ST. (N 1 4.334 4.437 WELDCITY (M/SEC) 0.235 0.283 0.284 DISCHARGE (M00-3/S) 313.5 288.2 278.1 SECTUN (100-3/S) 313.5 288.2 278.1 SECTUN (100-3/S) 313.5 5.200 HY. HADIUS(M) 6.965 6.022 5.200 ROLGHNESS(MANNING) 0.03G00 0.03000 0 T DAY - " 27 DAY" 1 DAY J RIVER ING. 1 [1] 2 1 SECTUM (NO.) [1] 2 1 MATER ST. (M 1 4.334 4.379 VELUCITY (MSEC) 0.247 0.260 OLENAMGE (M**2/5) 328.4 300-1 SECTION (M**2) 1332.7 1155.9 HY. RADIUS(M 1 6.965 6.025 ROUGHNESS(MANNING) 0.03000 0.02000 0. 10.145 252.44 ~ ~ ~ BDUNDARY (ND.) < 1 > < 2 > Water Stage (M) 4.517 10.633 HY. FAULUS (4) 7.002 6.144 HQUUT.FOS (14NNL 4) 3.05000 6.0000 1-2-01 +FE-+ 24 T T T T T T R 1 1 1 4+517 0+200 214+1 1347+2 1347+2 BOUNDARY (NO.) < 1 > WATER STAGE (N] ~ 4.334 BOUNDARY (NO.) < 1 > #AIER STAGE { H } 4.344 (DAY Ŧ . ļ RIVER (NG. 1 SECTION (NG.) WATER ST. (M.) VELULIY (4/56C) DISUMARUN (444C) SELTIC: (444C) 1 ĺ | ! 1 ſ ſ 1 , ***** 1 1 , e -, 1 **...**,

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Appendix E-35

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Appendix E-35 Page - 14

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Appendix E-35

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i (9)(10)(11)(12)(13)(14) 12.081 12.006 13.170 13.854 14.991 15.796 0.781 0.485 0.467 0.960 1.000 0.999 1491.7 1435.3 1862.7 1600.9 1698.8 1584.5 2422.9 2278.7 2148.0 1468.1 1698.8 1584.5 5.307 0.03000 0.03000 0.03000 0.03000 0.03000 14 1 15-960 1-042 1754-6 1754-5 1647-3 7-574 1-574 ł T 11 11 11 12 11 13 11 14 13.140 13.896 15.113 1 10 0.906 1.006 1.042 1 105.0 1405.0 14676 1 1 2125.0 1698.8 1993.0 1 1 2.252.0 16.98.8 19310 0 0.03000 0.03000 0-03000 0-Т L ł " ---**1** 52 **2**8 ŗ ſ 넕 PRINT NO. I PAINT NO-; ; PAINT í . Ļ , (2) (6) (7) (8) (9) (10) (9.550) 10.239) 10.534) 11.453] [2.012]2.534] 0.411 0.740 J.725 0.730 0.767 0.820] 110.3 | 1969.2 | 1349.6 | 1349.6 | 1743.4] 2.1221 2.000.0 2.526.1 2.524.1 2.187.4 2 2.1221 2.1200 0.23000 0.03000 0.03000 0.03000 0.0 ł , 1 ki ver River 1 THE HYDRAULIC AMALYSIS UF THE MODEL OF THE MIUDLE REACHES UF MYITMAKA Buumdart : <1> kummatkaik statium ; <2> Lonfluènce mith ikkamadut Section : (1] = <1> ; (5) uammi ST. ; (11) Gammun ST. ; (14) = <2> inteaval : DX* 9500 ur luuuu m ; DT = buu Séc. inteaval : DX* 9500 ur luuuu m ; DT = buu Séc. Peaidu : During June TQ séptember 1974 ì 11 a 11 7 11 8 11 12 144194 10.825 11.481 1. 13 0.750 0.7749 0.762 11 1.5 1972.7 1843.4 1943.7 11 14 262849 2516.4 2552.2 21 18 4.525 4.511 4.513 21 10 0.03000 0.03000 0.03000 0-1 1 ł ŧ ţ ---0::0 0100 0110 ١ : WOOH)-----" XNDH HUUH :) (4. 4 4. 126 1.2451 1.2451 2.251 2.251 2.2000 5 5 5 Ī) | | | İ 5 ---DAY UAY UAY ŧ ¥ × 1 1 2 1 1 1 2 1 1 247 1 2 1 1 1973.8 1905.3 1 1 84.4 8 1905.3 1 1 84.4 8 1905.2 1 1 8.712 8.090 0.9 0P6*51 < 2 > 15.796 < 2 >
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Appendix E-35 Page - 21 4 14 1 16-263 1-067 2038-9 1910-9 1910-9 7-580 7-580 14 1 16.215 0.995 0.995 1863.7 1873.3 1873.3 1.579 0.03000 1 14 1 16-217 1-042 1970-4 1890-2 1890-2 0-03000 -0 (13)(15.379 1 1.031 1.031 2160.3 1 2095.8 1 4.813 13 1(15,364 1,051 1,051 2,181,2 2075,1 4,812 4,812 0,03000 (13 11 15-434 0-987 0-987 2147.4 2147.8 4-816 4-816 0-03000 1 , l ł l _ (69 -29 \$ If 10)(11)(12)(0 12.405 13.598 14.371 1. 2 0.475 0.951 0.944 1. 9 2325.7 2349.3 2264.4 2 3 2657.1 2470.1 231.5 2. 8 0.172 6.172 6.224 2. (3)(4)(5)(6)(7)(8)(9)(10)(11)(12)(8.524 9.185 9.413 10.347 11.002 11.651 12.270 12.827 13.477 14.232 1.007 0.910 0.799 0.741 0.743 0.748 0.802 0.853 0.929 0.997 1933.2 1950.7 1982.7 20591 1981.9 20858 2084.1 2182.2 2209.7 2109.7 1919.7 2130.9 2440.2 2180.4 2655.3 2117.2 2594.5 2379.1 2115.7 2 1919.7 2130.9 2440.2 2180.4 2.514 2.514 2.341 5.172 6.070 5.220 7.350 5.333 4.532 4.514 2.514 2.341 5.172 6.070 5.220 7.3500 3.03000 0.0300 (3)(4)(5)(6)(7)(6)(9)(10)(11)(12)(8.488 9.140 9.759 40.347 40.940 11.408 12.224 12.784 13.426 14.184 1.002 0.907 0.404 0.744 0.743 0.746 0.2801 0.9850 1.925 1905.2 1924.4 1954.8 2015.5 1954.7 2044.1 2046.0 2125.8 2168.4 2052.6 1902.3 2122.9 2447.9 2745.5 2375.3 2675.4 2500.9 2340.2 2041.4 7.347 5.337 5.332 4.511 4.513 2675.4 2555.4 2500.9 2047 6.219 7.347 5.337 5.332 4.511 4.513 2675.4 0.03000 1 ġ ġ. Q 1 PRINT PRINT ł PRINT i 1 ١ -... 1 l ļ REV**e**r Rever ٠ 1 7 1 6 1 9 1 4 11.049 11.703 12.330 1 2 0.775 0.772 0.812 2 2126.3 2136.3 2157.9 2 4 2 2126.3 2136.3 2157.9 2 4 4.515 4.517 2058.3 2 4 4.515 4.515 0.03000 0.03000 0. ÷ AAULIC ANALYSIS OF THE WODEL OF THE MIDDLE REACHES UF MYIFMAKA Y : <l> KUMMAYKAIK STATION : <2> LONFLUENCE WITH IMRAMADOY : [1] = <l> : [5] DAWL ST. : [11] GAMAUN ST. : [16] = <2> L : DX= Y500 GR LUU00 M : UT = 600 SEC. : DUAING JUNE TO SEPTEMBER 1974 1 6 1 6 1 4 9-855 10.434 1 5 9-835 10.4242 1 5 0013-5 2091-2 2 2513-4 201310 2 5 5-334 2-533 2 0 0.33000 0-33000 20 ł ł 1 0010 0:00 } 0110 1 HOUR : •• ** HUUK NUUK , 1 4 1 9-228 9-906 9-916 --8118 2-181-2 2-182 --21200 1 ŧ Ĭ) -----; į -^ 472 DAY 1 ł DAY RIVER (MD.) (1) 2) (SECTION (MD.) (1) 2) (WATEN ST. (M) 7.291 7.855 6 VELOGITY (M/SEC) 1.047 1.004 1 DISCHAUGE (M003/S) 20294 1949.2 19 SECTIUN (M002) 1938.1 186.2 9 19 MY. KADIUS(M) 4.865 8.259 7 RDUGHNESS(MANNING) 0.03000 0.030 DAY
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Appendix E-35 Page - 25 3 1(4 1(5 1(4 1(7)(4)(9)(10)(11)(12)(13)(14) 9.553 10.124 10.702 11.2%4 11.431 12.440 13.035 13.567 14.206 14.946 16.083 17.159 0.944 0.461 0.777 0.777 0.729 0.734 0.764 0.786 0.4845 0.9299 15.32 3409.0 3074.8 2.311.2 2.301.7 2.422.0 2.537.9 2504.4 2637.2 2711.9 2952-7 2954.4 3163.2 3409.0 3074.8 2.470.4 2.742.2 3119.0 3479.9 3472.9 3495.6 3455.3 3496.1 3103.9 2481.5 20 7.364 0.1311 0.03100 0.031000 0.03000 0.03000 0.03000 0.03000 0.03000 14 14 1 17.418 1.120 3162.2 2622.9 7.602 0.03000 (1)(2)(3)(4)(5)(4)(7)(8)(9)(10)(11)(12)(12)(13)(14) 8.662 9.142 9.674 10.233 10.805 11.362 11.940 12.563 13.183 13.744 14.425 15.199 16.301 17.325 0.988 0.973 0.927 0.895 0.779 0.779 0.737 0.742 0.768 0.806 0.870 0.954 14.001 4.077 1.147 2.311.3 2312.3 2.944.9 2401.3 2406.4 2401.2 2402.4 219.4 3.371.1 3320.1 3545.4 3456.3 256.3 2.340. 2371.0 2535.3 2408.6 3199.0 3565.3 3521.2 3618.5 3623.8 3720.5 3481.0 3540.9 3416.3 2750.8 2.345 0.33700 0.03000 0.03000 0.03000 0.03000 0.03000 0.03000 0.03000 0.03000 0.03000 0.03000 ~ t 52 46 PRINT NO. - (PRINT NO. (PRINT NU-í 1 1 ł K [VER ~ H] VER ł AULIC AMALYSIS UF THE MODEL OF THE MIDDLE REACHES OF MYITMAKA : <1> <1> KUNHAYKAIK STATIUN : <1) = <1> [5] UAHWI SF.] (]] UAHMUN SF.] (]4) = <1> : UX= 9500 OM 10000 M : UX= 9500 OM 10000 M : UX= 9500 OM 2000 M : UX= 9500 OM 2000 M : UX= 9500 OM 2000 M : UX= 9500 OM 2000 M : UX= 974 4 ÷ ŧ 1 Ì İ ۱ , -01010 ł 1 0:00 01:10 ł ł ŧ i : NUCH)-----: YNDH J-----: YNOH)-----; **UUDED.U UUDED.U** 1 ---I 74 DAY **DAY** ÛΑΥ v v v 244240 244240 244140 244240 244240 244240 244240 2443400 2443400 1 11.326 2 11 THE HYDRAULIC A BOUNDARY : <1> SECTIUN : (1) INTERVAL : DX= PERIDO : OURI 1 > < 2 > 8-479 17.159 L > < 2 > 8.815 I7.41d 76 22 ţ ; RIVEA (NO. 1 [1] SECTION (NO. 1 [1] WATEN ST. (M 1 8.479 . VELUCITY (M/SEC 1 1.022 2 DISCHANGE (M**3/5) 2324-6 2 BISCTIUN (M**2) 2274-5 2 HY. MADIUS(M) 9.3944 ROUGHNESSIMANNIGJ 0.03000 0. . R <u>,</u> ж 1 > 8.662 YAU • DAY (UAY L v v v
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-, , Page - 27 17-170 2770-2 2627-6 7-597 7-597 7-597 0-03000 14 1 17-083 1-033 2642-1 2558-4 7-595 0-03000 17.021 0.968 2429.8 2429.8 2509.9 7.594 0.03000 1 ŕ HI 12 1(13)(3 15.411 16.253 1 4 0.853 0.957 1 1 3867.9 3203.6 20 3 3854.0 3347.0 22 4 6.222 4.866 2 0 0.03000 0.03000 0.01 ' (12)(13)(15-505 16-291 0.849 0.909 33891.7 3402-3 3991.7 3402-3 6-254 4-868 -1 0.03000 ł 81) ţ _ -8 **5** 6.254 0.03000 1 ġ ş NG. 1 1 1 1 1 1 4-883 1 0.794 3 3262-1 3 46.234 3 0.90300 0-PRINT 11 11 14-945 1 0-846 3 3423-0 3 4194-8 3 6-235 0 0-03000 0 PRINT (PRINT i --1 1 7 1 8 1 9 1 10 11 1 6 12.932 13.441 13.949 14.407 14 7 0.734 0.727 0.725 0.744 1. 3240.7 3299.0 3281.0 392.7 32 2. 4415.9 4535.7 4536.9 4560.2 41 2. 4415.9 4535.7 4536.9 4560.2 40 2. 0.03000 0.03000 0.03000 0.0300 0.0 [10][14-441 7 0-760 1-760 5494-8 1 4503-3 0 6-209 0 0-03000 0 f 1 Ł HYDRAULIC ANALYSIS OF THE MODEL OF THE MIUDLE REACHES UF MYITMAKA RIVER NUARY : <1> KUMMAYKAIK STATIUM : <2> CUNFLUENCE WITH IMMAWADDY RIVER TION : <11 = <1> ; <51 DAWH ST< ; <14 GAMMUN ST< ; <14) = <2> EAVAL : DX# 9500 UN 10000 M ; DT = 600 SEC. IOD : DUWING JUNE TO SEPTEMBER 1974 t 11 7 11 8 11 9 11 2 12.920 13.500 14.012 1 7 3.736 0.731 0.732 1. 2 2.5262.0 3327.6 3339.1 5. 1 4.3221 4.561 7. 5.214 4.615 5.650 0. 1 6 11 12.492 1 3.797 1 3300.2 4 4449.0 t +50.0 0.03300 ~ -; 00:00 0::0 0010 • ļ ** +4 ** HOUK MOH)-----Ī 1 ł ii <u>_</u> -ł £ DAY DAY ΡAΥ 1 1 1 2 1 8.876 9.778 1 1.349 1.264 1 1.258.7 3361.1 3 2416.5 2659.5 3 9.346 8.385 3 0.03000 0. v v v 2 11 9-751 1-261 1-261 3337-5 2647-3 8-384 8-384 2 11 9-142 1-206 3340-9 2643-4 ł 17.043 447.8 5.03000 17.170 1 > < 2 > 8.845 17.021 81 80 28 1 BUUNDARY : 4 SECTIUN : 6 INTEAVAL : 6 PERIOU : 6 RIVER (NU.) [1] SECTION (ND.) [1] MATEN ST. (N) 8-860 VELOCITY (N/SEC) 1.360 VELOCITY (N/SEC) 1.360 DISCHAHUE (Nee 3/S] 3229-8 3 SECTION (Nee 2) 24160 NY. HADIUSIN) 9-346 RUUGHNESS(MANNING! 0-U3DD0 0. R 4 8-845 1-345 3234-3 2445-5 2445-5 9-346 0-03640 98 1 8-860 1 > 8. b76 ł (DAY DAY ΤE _ v v RIVEN [NU-] [SECTIUN [ND-] [WATER ST. [ND-]] VELUCITY [N/SEC] DISCHARLE [M+*2] 2 FUUGHNESS[MANNING] 0. v SECTION (NO.)(WATEM ST. (MO.) VELOCITY (MYSEC) DISCHARGE (M**3/5) SELTION (M**2) HY. KADIUS(M) 0 RQUGHWESS(MANWING) 0 Î Î Î Î ġż BOUNDAMY Water Stage BOUNDARY Waten Stage BOUNDARY Water Stage RIVEN İ 1

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ANALYSIS JF THE MUDEL UF > KUNHAYKAIK STATION 6 = <l> ; (5) UANWE 56 5 = 4500 UK 10000 M</l>	<pre>Mic JUNE TO SEPTEMBER 1274 DAY 1</pre>	0.1 1
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- -Appendix E-35 - .-". Page - 30 . (10)(11)(12)(13)(14) 13.473 13.698 13.955 14.375 14.760 0.522 0.548 0.584 0.501 0.651 1761.8 1413.8 1017.0 870.9 860.7 1761.8 1413.8 1017.0 810.2 1291.0 0.161.0 0.03000 0.03000 0.03000 0.03000 1411 15.120 0.626 848.0 1354.3 7.437 0.03000 (14) 15.545 0.775 0.775 1134.6 1464.9 164.9 10.03000 į 1 13 11 14-796 1 0.6538 988-9 1548-9 1548-9 1.548-9 1.548-9 2.03000 0.0 ţ, Ŧ ŝ 13 1(15.065 0.741 1300.5 1756.3 1756.3 4.708 0.03000 0 ł 1 16 ~ к 3 i 9 1 10 11 11 12 11 1 12 11.440 13.694 13.972 14.311 14 94 0.563 0.569 0.654 0 7 2203.1 2082.4 1992.2 1460.9 9 5 3915.1 2087.0 2890.8 2233.3 15 4 3915.1 3657.0 2890.8 2230.0 0.0 8 i 5 14-511 0-686 1732-9 2526-9 6-228 0-03000 0 ž ģ PRINT NO. 3 9 ł (10)(11)() 13-872 14-164 14 0.585 0.6532 0.632 10 0.585 0.632 10 0.585 1974-9 10 0.0100 0.03000 0.0 PRINT ; PRINT ł -_ K I VEK R I VEK 1 2 11 2 11 5 11 5 11 5 11 5 11 6 11 7 11 8 11 9 11 9-247 10-178 10.464 11.625 12-134 12-945 13-247 1 1.552 1.157 0.464 0.614 0.712 0.631 1.655 1.0531 1.552 1.157 0.464 0.614 0.612 0.631 1.6454 1276-7 2942 1.160.0 2.7714 0.9401 1.6940 5 2 2 2 2 2 2 2 2 2 4 4 4 1 4 1 4 10 10 1 3040-9 2 4 180 7.310 0.01200 0.01310 0.01310 0.0353 0.03000 0.03000 0.01310 0.01300 0.0310 RIVER (NO. 1 (1) SECTUM (NO. 1 (1) SECTUM (NO. 1 1) SECTUM (NO. 1 1) VATER ST. (M) WATER ST. (M) SECTUM (NOSEC ţ THE HYDRAULIC ANALYSIS UF THE MODEL UF THE MIDDLE REACHES UF MYITMANA BUUNDARY : <I> KUNHAYKAIN STATICN : <2> COMFLUENCE MITH IRRAWADDY SECTION : (1) = <I> ; (5) JAWWI ST. ; (11) GAMMUN ST. ; (14) = <2> INTERVAL : DX= 9500 UR LUJUU M ; DI = 600 SEC. PERIOU : DURING JUNE TU SEPTEMBER 1974 1 ł 1 ł ļ 1 00:0 --00:00 0:00 ł ļ •• •• ** HULR HUUH ----- (HUUR RIVER (ND-)[1]] SECTIUN (ND-)[1]] 2][4][4] MATEN ST-(M) 8.281 9.363 10.317 11.119 VELUCITY (M/SEC) 1.455 1.373 1.468 0.976 VELUCITY (M/SEC) 1.455 1.373 1.468 0.976 VELUCITY (M/SEC) 1.455 1.373 1.468 0.976 VELUCITY (M/SEC) 1.455 1.373 1.468 0.976 VELUCITY (M/SEC) 1.455 1.373 1.475 HY, RADIUSIM) 9.344 0.381 7.375 6.377 HY, RADIUSIM) 9.344 0.381 7.375 6.377 ATUGHNESS(MANNING) 0.03000 0.03000 0.034000 0 ; Ĭ -, . 1 . 1 1 -DAY 1 -^ ÷ 91 DAY DAY v v v < 2 > . 15.120 BDUNUAHY (NO+) < 1 > C 2 > Water Stage (M) 8+357 15+545 ŝ 89 1 × < 8+205 < < 1 > < 8.281 . . μ 0000010 DAY 1 DAY DAY -----v RIVER [ND.] [SECTIGN [ND.] [WATEN ST. [ND.]] VELUCITY [M/SEC] DISCHANGE [MM#1/5] SELTION [44#2] HY. PAUTUS[MANWING] U. - ON J BGUNDAFY Mater Stage BOUNDAFY Mater Stage :

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Appendix E-35

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 MIUDLE REALHES UF MYITMAKA • Cunfluence aith ikramaduy i) Lammon St= ; [14] = <2> IC ANALYSIS UF THE MODEL OF THE MIDDLE REAL CLS KUMMAYKAIK STATIUN : (2) CUNFUCENCE (1) = (1) = (2) CUNFUCENCE (1) = (1) = (1) LAMMON ST (1) = (1) LAMMON ST (2) = 9500 GR 10002 m \cdot 10 DF = 900 SEC. DURING JUNE TU SEPTEMBEN 1974 Ì 0100 1 6 0010 0110 1 HOUR 1 UAY 1 ----- 1 HUVA : ----- HOUK : SECTIUN (NO.)(1)(2)(3)(4)(WATEA ST. (M) 7.595 8.563 9.453 10.208 VELOCITY (N/SEC) 1.301 1.305 1.113 0.940 VELOCITY (Ne3/5) 2711.2 2784.3 2731.4 2.624.3 DISCHARGE (Nee3/5) 2711.2 2784.3 2731.4 2.624.3 SECTIUN (Mea2) 2006.6 2121.5 2416.9 2792.5 HY. RADUGHNESS(MANNING) 0.03000 0.03000 0.03000 2515-9 2515-9 2515-9 2229-1 2229-1 2229-1 2-150 2-100 2-222 -95 DAY J 96 DAY × ~ ~ ~ HY__ XAulUS(M] _______ 4.340 ROUGH 4-55[MARNE4G] 0-03000 BOUNDARY [ND.] < 1 ') < 2 > WATER STAGE ('M | 7.306 14.972 7.443 14-816 25 THF HYDRAULI BUUNDARY 1 < Section 2 (Inferval 7 0 Period 1 0 ' n H 4 1.335 2552.0 1941.4 BOUNDARY (NO.) < 1 > 4 WATER STAGE (M) 7.595 ^ 0.03000 1.306 DAY (DAY YEO), -----1 BDUNDAHY (NG.) < 1 Watek stage (H) 7. -RIVEN (NG- 1 (SECTION (NO- 1 (WATER ST- (NO- 1 (VELOCITY (N/SEC) DISCHARGE (N++3/S) SECTION (N++2/S) HY- ADIUSIM 3 ROUGHNESSIMANNING1 0 1 RIVER (ND.) SECTIUN (ND.) (MATEA ST. (M.) (VELOCITY (M/SEC) DISCHARGE (M**3/5) S15+++ 700K) (H/SEC SECTION IN HY - AAUTUSIM RIVEN SECTION MATEN ST. () VELUCITY () DISCHANGE () , **¦**

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Appendix E-35 Page - 34 (i3)(i4.976 i5.844 14.976 i5.844 1.050 1.050 1.171.6 i697.5 1.187.7 1616.9 1.687.7 7564 1.4.657 7.564 (3)(4)(5)(6)(7)(8)(9)(10)¹ (1,056) 13.54) (4.782)5.659 8.659 9.499 10.023 10.534 11.018 11.483 11.405 12.414 0.643 0.966 1.032 1.036 1.101 0.443 0.774 0.677 0.643 0.639 0.681 0.79 0.642 1.391.3 1585.9 1573.8 2192.1 2.132.1 2036.7 1960.4 1729.3 1633.1 1531.7 1449.4 1612.3 1391.3 1585.9 1513.8 2199.1 2.244.8 2630.5 2097.7 2690.0 2553.9 2259.4 1911.9 1912.1 1440.2 1537.4 1519.2 1991.3 2244.2 5.338 4.538 4.519 2.553.9 2259.4 0.4040 0.03000 0.03000 0.03000 0.03000 0.03000 0.03000 0.03000 0.03000 0.03000 0.03000 0.03000 0.03000 1 1 13 10 RIVER [NG.] [1] SECTICN (NG.] [1] SECTICN (NG.] [1] [2] [3] [4] [5] [6] [7] [8] [9] [10] [12 947] 3.712 [4.976 WATEK ST. [N] 7.016 7.796 8.587 9.314 9.931 JU-442 10.935] 1.425]L.840 1.299 0.699 1.006 1.050 VELICITY [N/SEC] 1.218 1.147 1.034 0.926 0.712 0.680 0.455 0.661 0.711 0.79 0.499 1.006 1.050 VELICITY [N/SEC] 1.218 1.147 1.034 0.926 0.712 0.680 0.455 0.661 0.711 0.79 0.790 0.790 0.770.6 1.050 VELICITY [N/SEC] 1.218 1.201 9.2118 2.0066 9.978.9 1918.8 1712.6 1.650.0 1.591.3 1556.1 1780.0 1574.2 1771.6 DISCHARGE [N**3/S] 2247.9 2201.9 2201.9 2218.4 2066 9.978.9 1918.8 1712.6 1.650.0 1.591.3 1556.1 1780.0 1.564.8 1687.7 DISCHARGE [N**2] 1246.0 1854.6 1953.4 2244.6 2564.5 2842.5 2823.0 2615.0 2246.6 1956.7 1940.4 1564.8 1687.7 HY. HADIUS[N] 8.693 8.215 7.350 6.441 5.336 4.534 4.511 4.512 5.270 6.164 0.000 0.03000 (PAINT NO. 103 1 , , 1 (PHINT NO. 102"] ~ 51 NG. TOL ÷ PRINT -: 1 ! H I VEN H I VEN , 1 ł THE HYDRAULIC ANALYSIS UF THE HOUEL UF THE HIDULE KEACHES OF MYITMAKA BDUNDAXY : (1) KUNHAYKAIK STATION : (2> CUNFLUENCE WITH IRMANDUY SECTIUN : (1) = (1) : (5) UAWWI ST. ; (11) UAWNUN ST. ; (14) = (2) INTERVAL : DX= 950U UR IDUUJU M PERIUD : DURING JUNE TU SEPTEMBER 1974 ī i , { ; į _ -0::0 0:00 01:0 : ноик : : NUDH 1-----., YUUH J LOL DAY) UAY- I DAY J 2)(7-835 1-210 2254-1 2 1803-6 1803-6 1 0-03000 0 < 2 > < BDUNDANY (NOC) C 1 > C 2 > C Water.Stage (M) C 138 15-493 ~ ~ ~ 103 **a** 102 RIVER (NG.) [1] SECTIUN (NO.) [1] MATER ST. (M) [1] VELOCITE (M.SEC) 1.239 1 DISCHARGE (M.SEC) 1.239 1 DISCHARGE (M.S.C) 1.231.5 2 SECTION (M.S.C) 1.881.3 18 HY. KADIUS(M) 8.702 8 ROUGHNESS(MANNING) 0.33000 0.0 = YAO 1 2.032 ņ BOUNDAMY (N0.) < 1 > WATER STAGE (M) 7.016 DAY ΟAY -v RIVEA (NG.) (SECTIUN (NG.) (WATEN ST. (NG.) (VELJCITY (N/SEC) DISCRAGE (M003/S) SELTIUN (M002)) HY. AJDIUS(M) 10 , (*, 5 -BOUNDANY Waten Stage 5 ۴ ۲ ł

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, Appendix E-35 Page - 37 7 • ł ---. . ļ ----r ţ RIVEN [ND.] [] [2] [3] [4] [5] [6] [7] [6] [9] [10] [11] [12] [13] [14] SECTION [ND.] [1] [2] [3] [4] [5] [6] [7] [6] [9] [19] [10] [1] [1] [1] [2] [13] [16] MATLET ST.] [7] 7] 9 2000 9.068 9.049 10.221 [ULTS | 11.320 11.900 12.432 12.899 13.393 14.029 15.649 15.809 VELOCITY [MASEC] 1.018 1.002 0.948 0.468 0.468 0.714 0.709 0.719 0.734 0.768 0.658 0.955 0.966 0.975 DESCHARGE [M00.55] 141.9 2099.2 2096.2 2101.9 2131.1 2199.8 2101.5 2129.1 2035.4 2005.8 1935.4 1680.6 1546.1 DESCHARGE [M00.57] 2104.4 2095.2 2101.8 2442.4 2773.2 3076.6 2962.5 2559.5 2773.5 2537.5 2315.9 1817.6 1743.6 1590.3 HY. AAOIUSIM] 9.315 8.310 7.357 0.347 9.4542 4.552 4.523 5.3349 6.172 6.032 6.215 4.659 7.556 HY. AAOIUSIM] 9.315 8.310 7.357 0.3470 0.04400 0.03000 0.03000 0.03000 0.03000 0.03000 0.03000 0.03000 MIVER [NU.] [1] SECTION [NO.] [1] SECTION [NO.] [1] MATEK 5T. [N] 7.91 3.400 9.013 9.004 10.239 10.764 11.311 11.863 12.797 13.277 13.894 14.921 15.614 MATEK 5T. [N] 7.931 3.400 9.013 9.005 10.239 10.765 0.705 0.714 0.714 0.740 0.816 0.913 0.935 0.924 MATEK 5T. [N] 7.931 3.403 0.965 0.466 10.239 10.705 0.702 0.714 0.740 0.816 0.913 0.933 0.924 MATEK 5T. [N] 7.931 3.4031 2.1955 0.466 0.705 0.705 0.714 0.714 0.740 0.816 0.913 0.923 DISCHARGE [MMATES] 11.053 1.031 2.1955 2.131.4 2.175.5 2.051.1 2.964.2 1924.3 1864.9 1836.1 1549.4 1383.5 SECTION [MMMAZ] 2.089.4 2.089.4 2.213.8 2453.7 2.146.2 3086.0 2.953.1 2046.2 1924.3 1864.9 1836.1 1645.0 1497.8 MATEK ADJUSEM 1 9.276 8.369 7.357 0.344 4.543 4.550 4.523 5.348 6.112 5.979 6.156 4.625 7.529 MATEKADUSEM 1 9.270 0.03000 0.03000 0.03000 0.03000 0.03000 0.03000 0.03000 0.03000 0.03000 0.03000 0.03000 1 ł •
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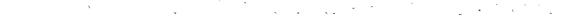
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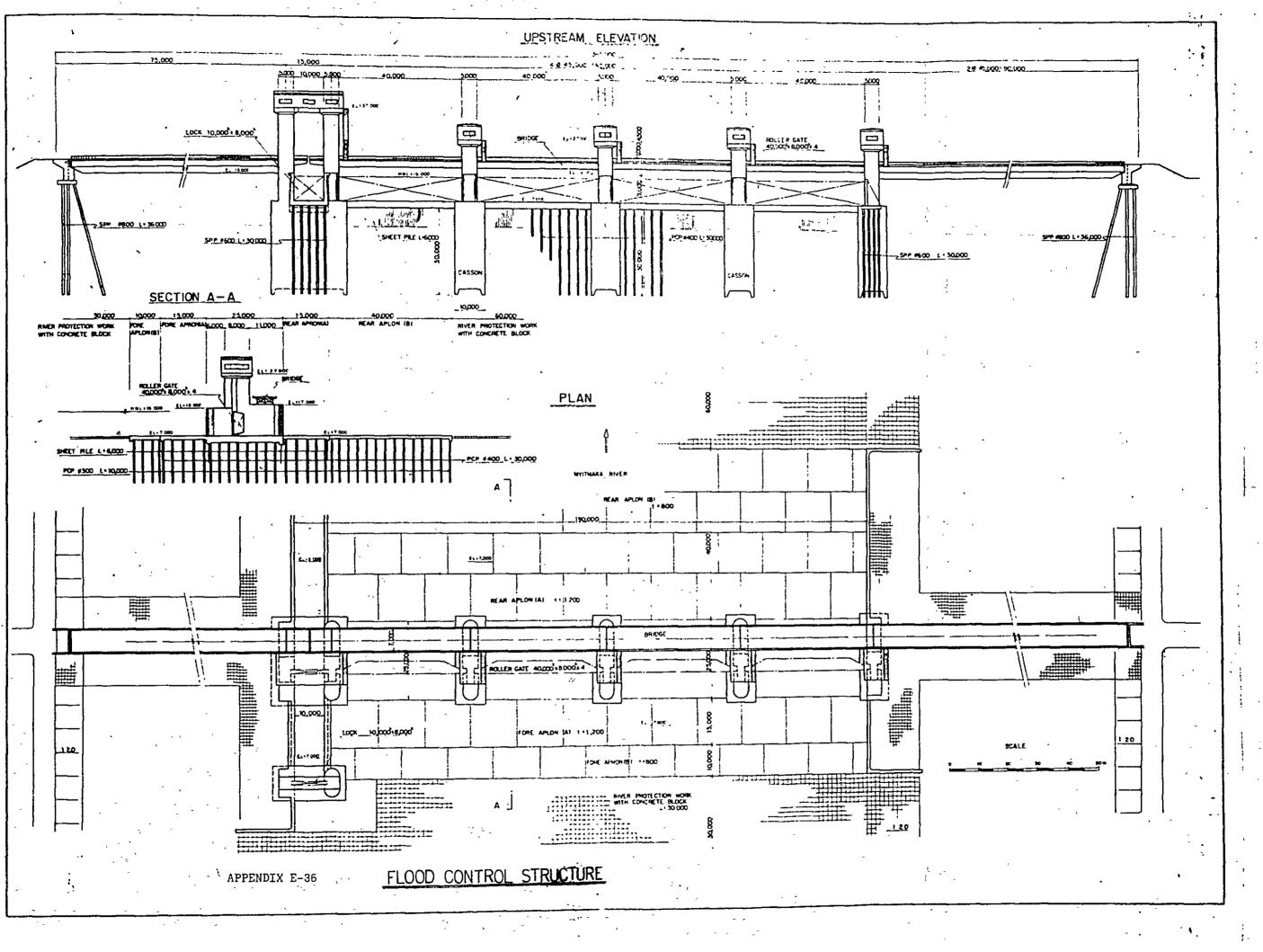
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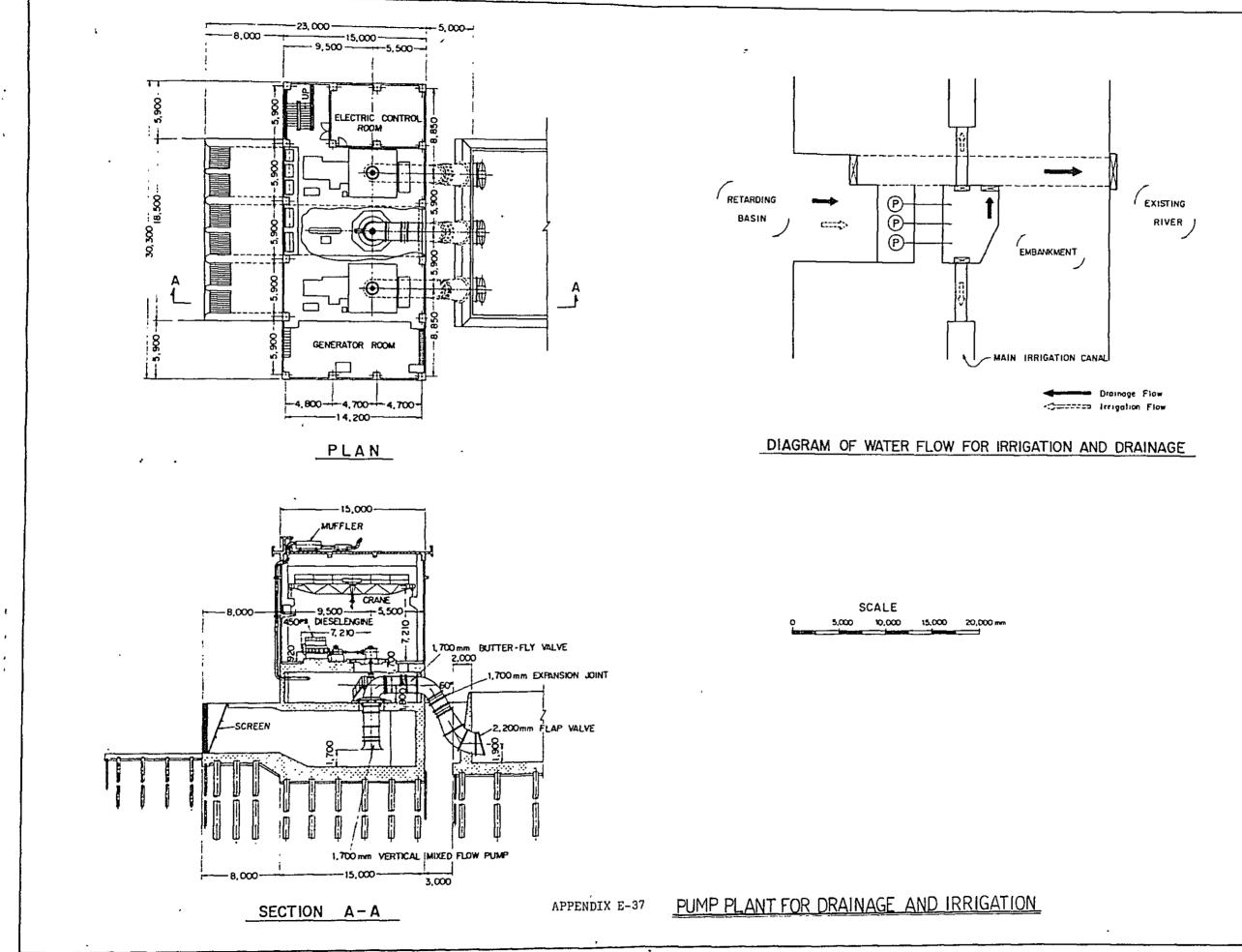
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