# YEMEN ARAB REPUBLIC

URBAN TRANSPORT STUDY IN YEMEN ARAB REPUBLIC FINAL REPORT VOLUME 2, APPENDIX

NOVEMBER 1988.

JAPAN INTERNATIONAL COOPERATION AGENCY



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**NOVEMBER 1988** 

**JAPAN INTERNATIONAL COOPERATION AGENCY** 

国際協力事業団	
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#### LIST OF TABLES & FIGURES

	Page
Appendix to Chapter 2	tage
Appendix Table 2.1.1 Government Expenditures and Receipts	APP.2-1
Appendix Table 2.1.2 Gross Fixed Capital Formation (Total of Private & Public Sectors): 1981-86	APP.2-2
Appendix Table 2.1.3 Per Capita GNP & GDP	APP.2-3
Appendix to Chapter 3	
Appendix Table 3.1.1 Area and Population for Each Zone in Sana'a (1986, 1991 and 2000)	APP.3-1
Appendix Fig. 3.1.1.1 Distribution of Projected Population Density, Sana'a 2000	APP.3-2
Appendix Fig. 3.1.1.2 Population Distribution of Sana'a, 2000	APP.3-3
Appendix Table 3.2.1.1 Number of Housing Units in the Census of 1975 1986 in the Governorates and the Country	APP.3-4
Appendix Table 3.2.1.2 Number of Licences Issued for Houses Construction and Area in the 5 Main Cities	APP.3-5
Appendix to Chapter 4	·
Appendix Note 4.1 General Description of Roads	APP,4-1
Appendix Note 4.2 Road Capacity and Level of Service	APP,4-8
Appendix Table 4.5.1 Link Volume and Capacity in 1987, Sana'a	APP.4-10
Appendix Fig. 4.5.1 Link and Node Number on Road Network, Sana'a	APP.4-17
Appendix Table 4.5.2 Link Volume and Capacity in 1987, Taiz	APP.4-18
Appendix Fig. 4.5.2 Link and Node Number on Road Network, Taiz	APP.4-19
Appendix Table 4.5.3 Link Volume and Capacity in 1987, Hodeidah	APP.4-20

	Page
Appendix Fig. 4.5.3 Link and Node Number on Road Network, Hodeidah	APP.4-22
Appendix Table 4.5.4 Volume and Capacity of Intersections in 1987 and 1992, Sana'a	
Appendix Table 4.5.5 Volume and Capacity of Intersections in 1987 and 1992, Taiz	APP.4-29
Appendix Table 4.5.6	
Volume and Capacity of Intersections in 1987 and 1992, Hodeidah	APP.4-30
Appendix to Chapter 5	
Appendix Table 5.1.1.1 Selected Results of the Traffic Count, Sana'a	APP.5-1
Appendix Table 5.1.1.2 Results of Turning Movement Count, Sana'a	APP.5-4
Appendix Table 5.1.2.1 Selected Results of Traffic Count, Taiz	APP.5-8
Appendix Table 5.1.2.2 Results of Turning Movement Count, Taiz	APP.5-9
Appendix Table 5.1.3.1 Selected Results of Traffic Count, Hodeidah	APP.5-11
Appendix Table 5.1.3.2 Results of Turning Movement Count, Hodeidah	APP.5-10
Appendix Table 5.2.1.1 Travel Speed Survey	APP.5-12
Appendix Fig. 5.4.1 Location Number and Frequency of Accidents	APP.5-22
Appendix Fig. 5.4.2 Composition by Type of Accidents Appendix Table 5.4.1	APP.5-23
Traffic Accidents Situation by Locations (in Sana'a City 1987)	APP.5-30
Appendix to Chapter 6	
Appendix Fig. 6.3.1 Organization of Government of Y.A.R	APP.6-1
Appendix Fig. 6.3.2 Organization of Y.A.R. Transport Sector	APP.6-2
Appendix Fig. 6.3.3 Structure of Ministry of Communication	APP.6-3
-ii-	

	Page
Appendix Fig. 6.3.4 Structure of Ministry of Public Works and Transport	APP.6-4
Appendix Fig. 6.3.5 Administrations Related to Urban Transportation Activities	APP.6-5
Appendix Fig. 6.3.6 General Traffic Office	APP.6-6
Appendix Fig. 6.3.7 Organization of Ministry of Municipalities & Housing	APP.6-7
Appendix Fig. 6.3.8 Organization of Municipality in Sana'a	APP.6-8
Appendix Fig. 6.3.9 Organization of Municipality in Taiz	APP.6-9
Appendix Fig. 6.3.10 Organization of Municipality in Hodeidah	APP.6-10
Appendix to Chapter 7	
Appendix Table 7.3.1 Locations of Interview on Passengers of Public Service	APP.7-1
Appendix Table 7.3.2 Origin-Destination Table of Public Transport Person Trips	APP.7-2
Appendix Fig. 7.3.1 Locations of Interview on Passengers	APP.7-3
Appendix Fig. 7.3.2 Zones for Origin-Destination Table of Public Transport Person Trips	APP.7-4
Appendix to Chapter 8	
Appendix Table 8.4.1 Current Traffic Problems by Section in Sana'a	APP.8-1
Appendix Fig. 8.4.1 Travel Speed Survey Locations, Sana'a	APP.8-7
Appendix to Chapter 10	
Appendix Table 10.2.1 Capacity Analysis of Intersection	APP,10-1
Appendix Fig. 10.2.1 Improvement Plan (1)	APP.10-67

. .

-iii-

	Page
Appendix to Chapter 12	
Appendix Table 12.1 Project Costs, All Projects	APP.12-1
Appendix Table 12.1 Project Cost, Total in Sana'a	
Appendix Table 12.1 Project Costs, No.1-No.16	APP.12-3
Appendix Table 12.2.1 Action Plan of Each Project	
Appendix Note 12.1 Machine Cost Calculation	APP.12-35
Appendix Table 12.(1) Asphalt Pavement A-2	APP.12-36
Appendix Table 12.(1).1) Agg. Subbase Course	APP.12-36
Appendix Table 12.(1).2) Hand BT Base Course	APP.12-37
Appendix Table 12.(1).3) Hand Asphalt Surf	APP,12-37
Appendix Table 12.(1).4) Seal Coating	APP,12-37
Appendix Table 12.(1).5) Prime Coating	APP.12-38
Appendix Table 12.(1).6) Hand Excavation	APP.12-38
Appendix Note 12.2 Work Cost Calculation	APP.12-39
Appendix Table 12.(2) Traffic Signal	APP.12-40
Appendix Table 12.(2).1) Footing and Election	APP.12-40
Appendix Table 12.(2).2) Plumbing	APP.12-41
Appendix Table 12.(2).3) Wiring	APP.12-41
Appendix to Chapter 13	

Appendix Note 13.1 Vehicle Operation Cost	APP.13-1
Appendix Table 13.1.1 Representative Vehicles	APP.13-2

	Page
Appendix Table 13.1.2 Vehicle Life	APP.13-2
Appendix Table 13.1.3 Tire Cost	APP.13-4
Appendix Table 13.1.4 🍃 Fuel and Oil	APP.13-4
Appendix Table 13.1.5 Engine Oil Consumption	APP.13-4
Appendix Table 13.1.6 Fuel Consumption on In-city Streets	APP.13-5
Appendix Table 13.1.7 Spare Parts and Labour	APP.13-6
Appendix Table 13.1.8 Crew Cost and Over-Head Cost	APP.13-6
Appendix Table 13.1.9 Vehicle Efficiency Ratio by Travel Speed	APP.13-7
Appendix Table 13.1.10 VOC Net Economic Cost	
Appendix Table 13.1.11 Trade Account & Government Current Revenues	APP.13-8
Appendix Table 13.1.12 Summary of VOC (Shadow Priced Economic Cost)	APP.13-8
Appendix Note 13.2 Time Value of Travellers	APP.13-11
Appendix Table 13.2.1 Accidents in Japan	APP.13-13
Appendix Table 13.2.2 Regression Analysis; Congestion-Velocity Curves	APP.13-14
Appendix Table 13.4.1 Cost Benefit Streams	APP.13-15
Appendix to Chapter 14	
Appendix Fig. 14.4.1 Zoning for Demand Analysis	APP.14-1
Appendix Table 14.4.1 Bus/Taxi Passenger OD Table by Mode	APP.14-2
Appendix Note 14.4.1 Methodology for Estimation of New Bus Passengers	APP.14-5
Appendix Fig. 14.4.2 An Example of an Operation Diagram	APP.14-6
Appendix Table 14.4.2 Personnel Expenses	APP.14-9

#### ~v-

Appendix Table 14.4.3 Repair and Maintenance Costs	· · · · · · · · · · · · · · · · · · ·		Page APP.14-10
Appendix Fig. 14.5.1 Conceptual Plan for Improvement of Bab Al Yemen Terminal	f		APP.14-11
Appendix Fig. 14.5.2 Conceptual Plan for Improvement of Tahrir Square Terminal	f		APP.14-12
Appendix Fig. 14.5.3 Conceptual Plan for Improvement of Bab Shunb Terminal	E		APP.14-13
		1 1	
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### APPENDIX TO CHAPTER 2

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Appendix Table 2.1.1 Government Expenditures and Receipts

			<u>    (Y</u>	<u>.R. Mill</u>	<u>ion of c</u>	<u>urrent</u> p	<u>rices</u>
Year	1980	1981	1982	1983	1984	1985	1986
Current Expenditure	2,953	3,325	5,181	6,200	5,770	6,046	NA
Capital Expenditure	3,919	3,683	4,017	2,944	3,100	3,422	
Extra Budgetary Expenditure	137	789	1,764	922	1,147	1,528	
Total Expenditure	7,010	7,797	10,962	10,067	10,024	10,996	NA
Revenues	3,050	3,335	3,698	4,405	4,650	5,376	
Grants	666	1,519	2,004	852	761	660	
Budget Deficit	3,294	2,943	5,262	4,807	4,613	6,036	NA
Deficit Financing							
Domestic	1,263	2,024	4,425	3,913	3,807	4,176	
External	2,030	920	847	900	806	972	

Source: Transport Sector Study (COP/RPT Econ. Study Group, October 1986) and CPO January, 1988.

Appendix Table 2.1.2 Gross Fixed Capital Formation (Total of Private & Public Sectors): 1981-86

(In Y.R. Million)

1981198211. Agri. Forest. Fishing436408Mining & Qurry5969Manufacturing376227Electri. Gas, Water1,1111,000Construction8050Whole & Retail Trade526231		1984 1 540 141		1986 (:	1901-00 (% p.a.)	1981	1982	1983	1984	1985	1986	1241-00 ( 2 4 2)
436 59 376 1,111 80 526	547 57 193 497 50 214	540 141	121					-		ļ	(2)	
59 376 1,111 80 526	57 193 497 214 214	141	401	329	-5.82	436	424	592	596	619	529	3.92
376 1,111 80 526	193 497 214 214		26	32	-13.02	59	72	62	157	35	52	-2.6%
1,111 80 526	497 50 214	171	430	282 .	-5.92	376	237	209	191	578	451	3.72
80 526	50 214 22	667	625	500	-17.32	1,111	1,041	538	556	839	801	-6.72
526	214	71	LT L	72	-2.1%	80	52	54	79	104	116	7.72
	7.2.4	201	200	161	-26.7%	526	241	232	224	269	257	-15.42
Transport & Comm. 1) 857 1,069	101	486	240	357	-19.1Z	857	1,013	827	541	322	571	-8.52
Financial Inst. 44 33	58	41	32	49	2.2%	77	*	63	47	44	. 79	12-42
Real Est. & Busin. S. 790 651	713	814	612	577	6.5%	790	778	772	905	820	923	3.22
Community, Social 1,627 1,735	964 I	,180	683	726	-17-52	1,627	1,806	1,044	1,315	.216	1,163	6.92
Total 5,906 5,443 4,	4,057 4,1	38	3,386_3,	,085	-13.92	5,906	5,698	4,393	4,610	4,547	4,938	-3.62
2. (Transport. & Comm.) <sup>1)</sup> (857 1,069	764	486	240	357)	-19.12	(857	1,013	827	541	322	571)	-8.52
(Private Sector) (345 321	347	114	54	43)	-51.6%	(345	234	376	127	60	(69)	-38,02
(Public Sector) (512 748	417	372	194	314)	-10.3%	(512	779	45'L	414	260	502)	47,0-

Statistical Year Book (C.P.O. 1986 & 1987)

Notes: 1) Transport & Communication sector is divided into private and public, which are shown in 2.( ). 2) 1986 figures are provisional.

Appendix	Table	2.1.3	Per	Capita	GNP	á	CDP

	1981	1982	1983	1984	1985	1986	1981-86 p.a.
Population	8,540	8,682	8,826	8,973	9,122	9,274	1.7%
GNP							
Cur. P in Mill. Per capita GNP	18,627	23,169	23,727	25,416	37,210	44,726	19.1%
in Ryals	2,181	2,669	2,688	2,832	4,074	4,773	17.0%
Const. prices In 1981, Mill.	18,627	20,057	19,315	19,453	23,055	24,072	5.3%
Per capita GNP	2,181	2,310	2,188	2,168	2,664	2,701	4.4%
GDP Cur. P in Mill	13,111	16,395	17,729	19,297	30,939	37,472	23.4%
er capita GDP in Ryals	1,535	1,888	2,008	2,150	3,575	4,205	22,3%
Const. prices in 1981, Mill.	13,111	14,193	14,432	14,770	19,139	20,254	9.1%
Per capita GDP in Ryals	1,535	1,635	1,635	1,646	2,098	2,184	7.3%
	SNP Sur. P in Mill. Per capita GNP in Ryals Sonst. prices In 1981, Mill. Per capita GNP SUP Sur. P in Mill Per capita GDP in Ryals Sonst. prices In 1981, Mill. Per capita GDP	Population8,540SNPSur. P in Mill.18,627Per capita GNP in Ryals2,181Const. prices n 1981, Mill.18,627Per capita GNP cur. P in Mill13,111Per capita GDP in Ryals1,535Const. prices n 1981, Mill.13,111Per capita GDP in Ryals1,535Const. prices en 1981, Mill.13,111Per capita GDP in Ryals13,111	Population       8,540       8,682         SNP       Sur. P in Mill.       18,627       23,169         Per capita GNP       2,181       2,669         Const. prices       2,181       2,669         Const. prices       18,627       20,057         Per capita GNP       2,181       2,310         SDP       2,181       2,310         SDP       13,111       16,395         Per capita GDP       1,535       1,888         Const. prices       13,111       14,193         Per capita GDP       13,111       14,193         Per capita GDP       13,111       14,193	Population       8,540       8,682       8,826         SNP       2000       23,727       23,169       23,727         Per capita GNP       18,627       23,169       23,727         Per capita GNP       2,181       2,669       2,688         Const. prices       18,627       20,057       19,315         Per capita GNP       2,181       2,310       2,188         SDP       2,181       2,310       2,188         SDP       2,181       2,310       2,188         SDP       2,181       16,395       17,729         Per capita GDP       1,535       1,888       2,008         Const. prices       13,111       14,193       14,432         Per capita GDP       13,111       14,193       14,432	Population       8,540       8,682       8,826       8,973         SNP       Sur. P in Mill.       18,627       23,169       23,727       25,416         Per capita GNP       in Ryals       2,181       2,669       2,688       2,832         Sonst. prices       n       1981, Mill.       18,627       20,057       19,315       19,453         Per capita GNP       2,181       2,310       2,188       2,168         SDP       Sur. P in Mill       13,111       16,395       17,729       19,297         Per capita GDP       in Ryals       1,535       1,888       2,008       2,150         Const. prices       13,111       14,193       14,432       14,770         Per capita GDP       in 1981, Mill.       13,111       14,193       14,432       14,770	Population       8,540       8,682       8,826       8,973       9,122         SNP       Sur. P in Mill.       18,627       23,169       23,727       25,416       37,210         Per capita GNP       in Ryals       2,181       2,669       2,688       2,832       4,074         Const. prices       n       1981, Mill.       18,627       20,057       19,315       19,453       23,055         Per capita GNP       2,181       2,310       2,188       2,168       2,664         SDP       2,181       2,310       2,188       2,168       2,664         SDP       2,181       13,111       16,395       17,729       19,297       30,939         Per capita GDP       1,535       1,888       2,008       2,150       3,575         Const. prices       13,111       14,193       14,432       14,770       19,139         Per capita GDP       13,111       14,193       14,432       14,770       19,139         Per capita GDP       13,111       14,193       14,432       14,770       19,139	Population       8,540       8,682       8,826       8,973       9,122       9,274         SNP       Sur. P in Mill.       18,627       23,169       23,727       25,416       37,210       44,726         Ser capita GNP       in Ryals       2,181       2,669       2,688       2,832       4,074       4,773         Sonst. prices       18,627       20,057       19,315       19,453       23,055       24,072         Per capita GNP       2,181       2,310       2,188       2,168       2,664       2,701         SDP       2ur. P in Mill       13,111       16,395       17,729       19,297       30,939       37,472         Per capita GDP       in Ryals       1,535       1,888       2,008       2,150       3,575       4,205         Const. prices       13,111       14,193       14,432       14,770       19,139       20,254         Per capita GDP       13,111       14,193       14,432       14,770       19,139       20,254

Statistical Year Books (CPO 1986, 1987)

Notes: 1. Estimated by using the population in 1981 and 1986.

- 2. B 2) Estimated by using the ration of GDP in constant prices and current prices.
- 3. Per capita figures in 1981-86 are calculated in this study.

## APPENDIX TO CHAPTER 3

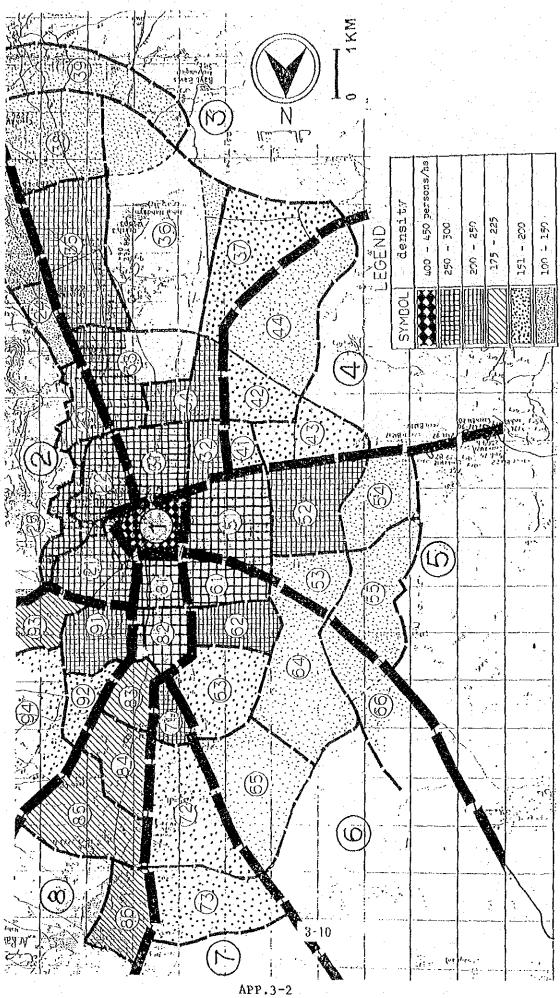
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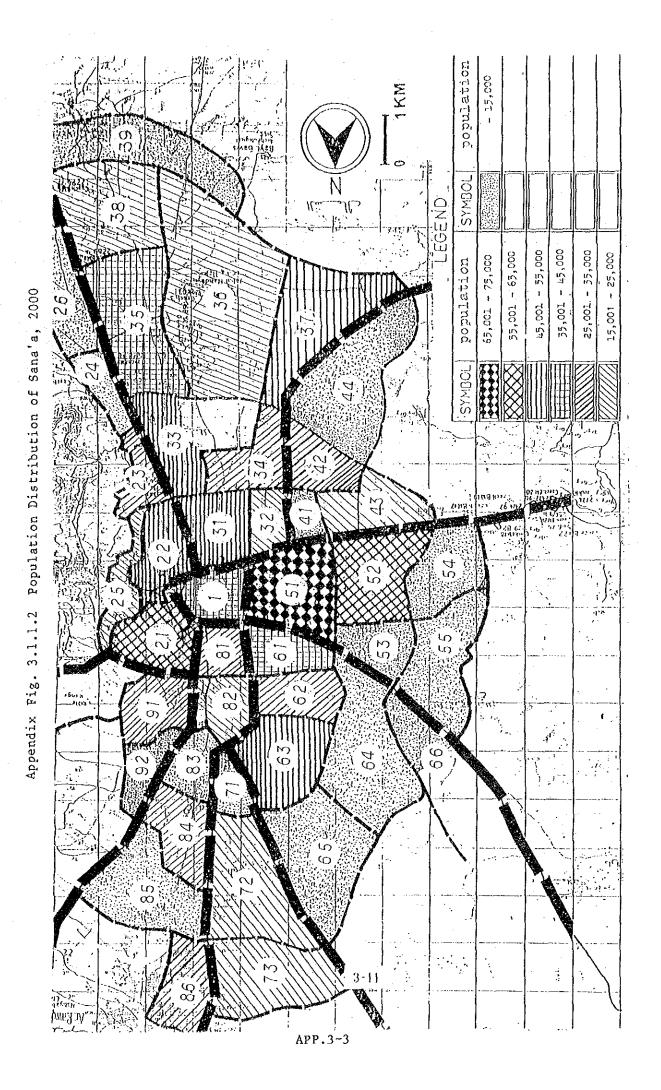
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Appendix Table 3.1.1.1 Area and Population for Each Zone in Sana'a (1986, 1991 and 2000)

							1. State 1.			
Sector	Area In	Area No	Total	Pop	ulation		·····	Prosp	ected	Revised
		Peoples		Actual	Proje	ected	Projecte			Urban
		•			<b>J</b> -		Gross	Area		Area
Zone	(ha)	(ha)	(ha)	(1986)	(1991)	(2000)	Density	(2000)	(1991)	(1986)
1 11	108.0	52.0	160.0	40,000	42,000	42,000	400	100%	100%	95%
2 21	220.0	4.0	224.0	22,000	33,000	55,000	250-300	100%	60%	40%
22	180.6	22.2	202.8	25,000	31,000	45,000	250-300	100%	70%	55%
23	120.0	·	120.0	10,500	16,000	24,000	200-250	100%	70%	40%
24	59.5	60.5	120.0	2,000	3,000	6,000	100-150	100%	50%	30%
25	77.0	13.5	90.5	6,000	10,000	20,000	250-300	100%	50%	30%
26	453.0	50.2	503.2	3,000	5,000	17,000	-100	100%	40%	20%
Total	1110.1	150.4	1260.5	68,500	98,000	167,000				
3 31	166.1	47.6	213.7	26,500	36,000	45,000	250-300	100%	80%	60%
32	102.2	4.6	106.8	16,500	21,000	23,000	200-250	100%	90%	70%
33	171.0	38.6	209.6	24,000	33,000	47,000	250-300	100%	70%	50%
34	144.2	51.3	195.5	16,000	21,000	32,000	200-250	100%	65%	50%
35	347.0	140.0	487.0	7,000	20,000	48,000	200-250	70%	30%	10%
36	242.5	720.0	962.5	1,000	6,000	18,000	100-150	60%	20%	3%
37	299.3	.8	300.1	5,000	22,000	52,000	150-200	100%	50%	10%
38	404.0	21.0	425.0	2,000	4,000	16,000	100-150	40%	40%	5%
39	393.0	44.0	437.0	1,000	4,000	12,000	100-150	30%	10%	3%
	2269.3	1067.9	3337.2	99,000	167,000	293,000			. •	
4 41	64.1	11.3	75.4	8,000	9,000	11,000	150-200	100%	80%	70%
42	174.0		174.0	9,000	17,000	30,000	150-200	100%	55%	30%
43	139.5	81.7	221.2	5,000	9,000	24,000	150-200	100%	40%	20%
44	468.0	52.0	520.0	1,000	2,000	16,000	100-150	35%	5%	3%
Total	845.6	145.0	990.6	23,000	37,000	81,000				
5 51	269.4	60.4	329.8	56,500	60,000	67,000	250-300	100%	90%	85%
52	287.4	43.8	331.2	23,000	34,000	57,000	200-250	100%	60%	40%
53	52.0	112.0	164.0	2,500	3,000	5,000	100-150	100%	70%	50%
54	119.0	118.0	237.0	1,500	3,000	7,000	100-150	60%	25%	10%
55	178.0	177.0	355.0	2,000	7,000	13,000	100-150	75%	40%	10%
Total	905.8	511.2	1417.0	85,500	107,000	149,000				
6 61	159.9	13.8	173.7	24,000	32,000	40,000	250-300	100%	80%	60%
62	130.1	34.4	164.5	8,000	16,000	29,000	200-250	100%	60%	30%
63	269.6	65.1	334.7	9,500	23,000	47,000	150-200	100%	50%	20%
64	95.0	283.0	378.0	500	2,000	12,000	100-150	100%	20%	3%
65	73.0	217.0	290.0	1,500	3,000	9,000	100-150	100%	30%	15%
Total	727.6	613.3	1340.9	43,500	76,000	137,000				
7 71	24.5	65.3	89.8	2,500	4,000	5,000	200-250	100%	80%	50%
72	323.5	17.0	340.5	4,500	12,000	25,000	150-200	50%	25%	10%
73	344.5	18.0	362.5	1,500	5,000	,	150-200	30%	10%	3%
Total	692.5	100.3	792.8	8,500	21,000	41,000				
8 81	102.7	12.1	114.8	18,000	23,000	25,000	250-300	100%	90%	70%
82	86.3	71.6	157.9	11,000	15,000	21,000	250-300	100%	70%	50%
83	84.8	57.9	142.7	4,500	9,000	14,000	175-225	100%	60%	30%
84	152.0	64.3	216.3	5,500	13,000	26,000	175-225	100%	50%	20%
85	250.0	28.4	278.4	2,000	9,000	13,000	175-225	30%	20%	5%
86	217.2	24.0	241.2	7,500	16,000	33,000	175-225	85%	40%	20%
Total	893.0	258.3	1151.3	48,500	85,000	132,000			-	
9 91	165.4	30.0	195.4	9,500	14,000	26,000	200-250	80%	45%	30%
92	50.8	5.0	55.8	1,000	3,000	7,000	150-200	90%	40%	40%
93		-	46.7	.,	-,	.,	100-150			
Total	216.2	35.0	297.9	10,500	17,000	33,000				
Grand							<u> </u>			
	7768.1	2933.4	10748.2	427,000	650.000	1,077,500				
	7700.C.	~ / J J + **	10740.6	1-11000			·····			

Appendix Fig. 3.1.1.1 Distribution of Projected Population Density, Sana'a 2000





#### Appendix Table 3.2.1.1

۰.,

Number of Housing Units in the Census of 1975 1986 in the Governorates and the Country

	Number	of Housing Un	its	Average rate of
Governorates	1975	1986	%	annual growth
Sana'a	131,853	273,002	207.1	6.84 %
Taiz	176,178	265,560	150.7	3.80
Al-flodeidah	145,574	209,603	144.0	3.37
Ibb	154,291	216,002	140.0	3.11
Dhamar	85,500	123,846	144.8	3.42
Најја	64,969	118,056	181.7	5.58
Sa'ada	27,992	47,924	171.2	5.01
Al-Mahwit	31,072	45,542	146.6	3.54
Al-Beida	30,914	46,752	151.2	3.83
Marib	7,706	15,284	**	- <b></b>
Al-Jawf		8,007	**	-
Total	856,059	1,369,578	160.0	10.44

Source: Statistical year Book 1986 (C.P.O 1987)

	ana		Taiz		r		I b b		Dhamar			
	nces	0   1 -   -1   -1   -1   -1   -1	icences	Are Are	icenci	ea (m2)		i ≺C i	Licences	Area Area		Area Area An2
1976	1,598	551,512	 	241,855	661	324,970	941	51,811	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1 L L L L	3.7441.	1.170,148
1977	2.423	784,994	1,118	97,764	001	125,046	216	39,704		·	4,157 1,(	1,047,508
1978	2,862	993,970	1,660	359,294	101	164,597	252	80,619			5,185 1,3	598,480
6161	2,172	829,404	1,541	318,329	387	248,604	350	91,668			4,450 1	488,005
1980	1,674	570,230	1,578	269,594	340	312,570	370	154,391	373	109,943	4,335 1,-	1,416,728
1981	2,352	752.808	1,156	188,858	307	108,341	360	75,050	233	73,071	4,418 1,1	198,128
1982	3,478	911,411	951	114,252	150	42,659	312	30,977	256	68,088	5,147	1,167,397
1983	3.124	862,428	1,032	149,435	2.02	42,148	124	34,949	617	112,298	5'I 106'F.	1,201,238
1984	1 3,993 I	1,217,091	1,300	409,944	270	91.740	183	48.621	351	125,018	6,097 1,6	892,414
1985	3,542 1	1,107,430	2,070	582,134	50 <del>1</del>	131,791	359	76,008	43 <b>0</b>	90,186	6,9111,5	1,987,549
1986	2,709	763,892	1.432	544,537	102	133,845	567	114.159	290	146.250	5.400 1.	.702.683

Source:Office of Municipalities in Main Cities in Statistical Year Book (1987)

APP.3-5

### APPENDIX TO CHAPTER 4

مغيرين وعرب

Sec. 1

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#### Appendix Note 4.1 General Description of Roads

#### 4.1.1 Sana'a

#### 1) Airport road

Connecting the airport at a distance of 13 km north side of the city, it extends further to the north town of Al Hayfah. The road extends to the south and the name becomes Al Qiyada street from the intersection with Ring road and goes to the center of the city with the name of Ali Abudul Mughni road. The road becomes 4 lanes from the intersection with Sadah road to the city center.

#### 2) Sadah road

This is an arterial road to Sadah, a northern city of Yemen. The road is 4 lanes up to the crossing with Airport road and becomes 2 lanes in the further suburban sections.

#### 3) Marib road

The road extending to the eastern city of Yemen, Marib, has 2 lanes except for the inside of the Ring road. The area from Ring road to Old city has become commercial area, and light industries have developed recently at the area outside the junction of the north-eastern boulevard.

#### 4) Taiz road

It connects Sana'a with southern cities of Yemen, Taiz, Ibb, Dhamar, etc. It has paved 4 lanes from Old city to Ring road and paved 2 lanes from Ring road to the south. The district between Old city and 45 m road is commercial area and areas of light industries. They are extending to the south along the road. Housing development is going on extensively in the area outside Sana'a bypass.

The paved 2 lane section from the Ring road to the police check point of 3.5 km is under work of widening to paved 4 lanes. The work is scheduled to be completed by the end of 1988.

#### APP.4-1

#### 5) Haddah road

The road to the southern suburban area, Haddah district, has paved 6 lanes from the intersection of Az Zubayri up to Sana'a bypass and pavement becomes 2 lanes at outside of Sana'a bypass. Commercial area continues from Az Zubayri to Ring road and housing development is going on along the road out of Ring road.

#### 6) Az Zubayri street

Crossing Sana'a from east to west, the road name becomes Hodeidah road which goes to the important port city, Hodeidah. The section of 5.2 km from Old city to Sana'a bypass has 6 lanes and beyond it in the suburban area the road becomes paved 2 lanes. But Az Zubayri street from Bab Al Yemen to the intersection at Haddah road, the capacity is reduced because of so many parking on the shoulders.

#### 7) Wadi Dahr road

This is a radial road extending to north-west and reaching to Shibam and Thula. Sana'a University campus located on 1.5 km length along the Wadi Dahr road from Ring road to Sana'a bypass has a schedule of construction of buildings on the southern side. At the same time the road section along the campus is closed and a new bypass will be constructed. Most sections from Old city to Ring road have 4 lanes (partially 2 lanes) with shoulders. It becomes paved 2 lanes outside the Ring road.

8) Roads surrounding Old Sana'a

It is composed of the following 6 roads;

- \* Ali Abdul Mughni street; West side road of the old city with 4-6 lanes, its roadside area is the commercial and business center of the Sana'a.
- \* Shuub street; North side road of 2 lanes with partial shoulders. There are many stores along both sides of the road.
- \* Al Mashad street; Connection road on the north east between Shuub street and Wadi Al Qasr street. It is a 2 lane paved

APP.4-2

road and a cemetery is located along the road.

- \* Wadi Al Qasr street; East side road of 4 lanes with median. Along the road a cemetery is located. Citadel link of Nugum qat market branches off at mid-point of this road and is connected to Ring road.
- \* As Salam street and Street No. 23; These roads are one way each other, connecting Az Zubayri street and Wadi Al Qasr street. Road width is 7 meters, and many stores are along the street.
- \* As Zubayri street; It is a 6 lanes road along the South Castle Wall of Old city.

#### 9) Ring road

Rounding road at radius lengths of 1.5 km to 2.5 km, the whole sections are completed in 1983. The section from Wadi Dhar road to Airport road have 6 lanes with 2 meter width median and there are many stores and houses along the road. The section between Airport road and Marib road is composed of 4 lanes and comparatively narrow in width.

The section from Marib road to Taiz road was completed a few years ago. It has 6 lanes with 3 meters median. Traffic volume is relatively small and roadside areas are not intensively developed. The section passes the hilly terrain and there is a segment with a 5% gradient. One public park is under construction and another is in planning. The section between Taiz road and Az Zubayri street has 4 lanes and the center opened drainage of 5m width.

The section from Az Zubayri street to Wadi Dahr road has a 2 meter width center opened drainage. Each direction of the road has a width of 7.1 meters while only 1 lane is available to the traffic because of many parkings. There are Sana'a University and shopping stores along the road.

10) North-eastern boulevard and 45 meter road

North-eastern boulevard and the 45 meter road were constructed

to support the development toward north and south respectively due to the steep sloped mountains of the east and west areas. North-eastern boulevard has been completed half at the east side of Airport road. From Airport road to Sadah road the boulevard has 6 lanes ensuring enough width of shoulders and parking lanes. The eastern section from Sadah road has 4 lanes paved and a 30 meter width ROW. The boulevard joins at the Eastern boulevard which has a 6 lane section to the Ring road and then southward to Old city through Street No. 24.

The 45 meter road, running the east-west direction in the southern part of the city is located between Ring road and Sana'a bypass. It has been paved with 2 lanes.

11) Sana'a bypass (60 m road) is constructed outside of 45 meters road from Taiz road in the south to Wadi Dhar road in the northwest and paved with 2 lanes.

#### 4.1.2 Taiz

1) Jamal street

As a main road in the northern part of the old city, it has 4 lanes and runs in parallel to Jaynai street & 26th September street. It connects with Sana'a road in the eastern side and with Hodeidah road in the western side.

2) Jaynai street & 26th September street

It extends from east to west in parallel to Jamal street. Road width is narrow and the eastern one third has 2 lanes under one way control. Many shops and stores are along the road.

3) Center boulevard

Radial road of paved 2 lanes extending toward north from the eastern part of Jamal street. housing construction and a new Qat market are on the roadside. 4) First Ring road

A half circle road with paved 4 lanes connecting to Jaynai street. The half circle is located from east to the center of the city. There is no bridge at the western Sailah which enforces traffic to detour.

#### 5) 2nd Ring road

As a half circle road located outside the First Ring road, it connects to Sana'a road at the eastern side and planned to intersect the Hodeidah road at the western side of the city. It is designed to have 4 lanes and the eastern half of the road is paved while at the western side ROW has been just ensured.

6) Park way

As a planned road outside the 2nd Ring road, its ROW has been ensured.

7) As Samil street

It is a 2 lane road connecting Jamal street and 26th September street. The alignment is poor because of developed houses and stores. GLTC bus terminal is located.

8) 13th June street and Qasr Al Shaab street

It is located in the eastern part of the city and has a function as a bypass of Jamal street. There are houses, government offices along the road.

#### 9) Sabir street

It is a 2 lane gravel surfaced road to southern Sabin Al Mawadin village constructed on the steep terrains of Mt. Sabir.

#### 10) Salah street

It is located in the southeast side of the city with 2 lanes. This road continues to the old palace.

#### APP.4-5

#### 11) South Ring road

A half circle road constructed on the southern steep terrains of Mt. Sabir. The bridge has not been completed yet at Al Jahmaliyah in the eastern part of the road.

#### 4.1.3 Hodeidah

1) Sana'a street

This is the main street in Hodeidah with 4 lanes. Many stores along the route extend toward east from the central triangle park of the city. The street name becomes Sana'a road from the crossing with Zaid street and goes to Sana'a and Taiz.

2) Port road

It is a 4 lane paved road with houses and public facilities such as school, police station and park along the route. It goes to the Hodeidah port from Al Corniche street passing by the central triangle park.

3) Zaid street and Gamal street

It is a half circle road of 4 lanes surrounding the city. It has the function as a bypass from Hodeidah port to Sana'a road.

4) Corniche street

It is a 4 lane road from south to north along the Red Sea. There is a fish port-market along the route.

5) Jizan road

It is a 2 lane road from Zaid street extending to Jizan in Saudi Arabia by crossing over the boundary. The roadside in the city area is not urbanized yet.

#### 6) Shamsan street

It is a 4 lane road toward northeast from Sana'a street. The road name becomes Jizan road after crossing Zaid street.

7) 50 meters road

This is a planned bypass to the port, but now only 2 lanes have been paved at the section from Port road to Jizan road. There are houses and market along the route and the northern side is still wasteland.

#### Appendix Note 4.2 Road Capacity and Level of Service

The followings are quoted from "Highway Capacity manual, special Report 209, (Transportation Research Board, USA, 1985).

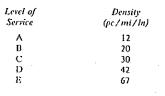
#### LEVELS OF SERVICE

#### Measures of Effectiveness

Freeway operating characteristics include a wide range of rates of flow over which speed is relatively constant. This means that speed alone is not adequate as a performance measure by which to define levels of service.

Although speed is a major concern of drivers with respect to service quality, freedom to maneuver and proximity to other vehicles are equally important parameters. These other qualities are directly related to the *density* of the freeway traffic stream. Further, rate of flow increases with increasing density throughout the full range of stable flows (see Figure 3-3).

For these reasons, density is the parameter used to define levels of service for basic freeway segments. The densities used to define the various levels of service (LOS) are as follows:



These values are boundary conditions representing the maximum allowable densities for the associated level of service. The LOS-E boundary of 67 pc/mi/ln has been generally found to be the *critical density* at which capacity most often occurs. This corresponds to an average travel speed of 30 mph and a capacity of 2,000 pcphpl for 60-mph and 70-mph design speeds. The exact speed and density, however, at which capacity occurs may vary somewhat from location to location.

#### Level-of-Service Criteria

Level-of-service criteria for basic freeway segments are given in Table 3-1 for 70-mph, 60-mph, and 50-mph design speed elements. To be within a given level of service, the *density* criterion must be met. The average travel speeds and maximum service flow rates indicated in the table are expected to exist under *ideal* conditions for the given densities. Actual average travel speeds for traffic streams under non-ideal conditions may be somewhat lower than the values shown.

Design speed depends on the combination of horizontal and vertical alignment. Other influences on driver behavior, such as the development environment, local driving habits, and other factors, may cause the relationship among density, speed, and flow to differ from the typical values of Table 3-1. Where local speed-flow-density data are available, they may be used as a guide in determining which design speed best represents local conditions.

#### DESCRIPTION OF LEVELS OF SERVICE

The levels of service have been defined to represent reasonable ranges in the three critical variables: average travel speed, density, and flow rate. The basic shape of the typical speed densityflow curves requires that as level of service moves from A to F, the range of densities and speeds covered by each level becomes larger, while the corresponding range of service flow rates becomes smaller.

The values in Table 3-1 reflect the influence of the 55-mph speed limit. Even with this speed limit clearly signed and reasonably enforced, average travel speeds for the better levels of service are still expected to be slightly higher than the 55-mph limit. Where enforcement is particularly stringent, or where lower speed limits are posted, speeds may be somewhat lower than those given in Table 3-1.

	TABLE 3-1. LEVELS OF SERVICE FOR BASIC FREEWAY SECTIONS	
-		_

		70 MPH DESIGN SPEED			60 MPH DESIGN SPEED			50 mph Design speed		
LOS	DENSITY (PC/MI/LN)	SPEED <sup>b</sup> (MPH)	v/c	MSF <sup>*</sup> (FCPHPL)	SPEED <sup>b</sup> (MPII)	\$/c	MSF <sup>A</sup> (PCPHPL.)	SPEED <sup>b</sup> (MPH)	v/c	MSF <sup>4</sup> (PCP1IFL)
A B C D E F		$\ge 60$ $\ge 57$ $\ge 54$ $\ge 46$ $\ge 30$ < 30	0.35 0.54 0.77 0.93 1.00	700 1,100 1,550 1,850 2,000	$ \begin{array}{c} - \\ \geq 50 \\ \geq 47 \\ \geq 42 \\ \geq 30 \\ < 30 \end{array} $	0.49 0.69 0.84 1.00	1,000 1,400 1,700 2,000	$\begin{array}{c}\\ \geq 43\\ \geq 40\\ \geq 28\\ < 28\end{array}$	0.67 0.83 1.00	1.300 1.600 1,900

<sup>a</sup> Maximum service flow rate per lane under ideal conditions.

<sup>6</sup> Average travel speed.

<sup>c</sup> Highly variable, unstable.

NOTE: All values of MSF Rounded to the nearest 50 pcph.

General descriptions of operating conditions for each of the levels of service are as follows:

1. Level-of-service A—Level A describes primarily free flow operations. Average travel speeds near 60 mph generally prevail on 70-mph freeway elements. Vehicles are almost completely unimpeded in their ability to maneuver within the traffic stream. The average spacing between vehicles is about 440 ft, or 22 carlengths, with a maximum density of 12 pc/mi/ln. This affords the motorist a high level of physical and psychological comfort. The effects of minor incidents or breakdowns are easily absorbed at this level. Although they may cause a deterioration in LOS in the vicinity of the incident, standing queues will not form, and traffic quickly returns to LOS A on passing the disruption. 2. Level-of-service B—Level B also represents reasonably

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3. Level-of-service C--Level C provides for stable operations, but flows approach the range in which small increases in flow will cause substantial deterioration in service. Average travel speeds are still over 54 mph. Freedom to maneuver within the traffic stream is noticeably restricted at LOS C, and lane changes require additional care and vigilance by the driver. Average spacings are in the range of 175 ft, or 9 car-lengths, with a maximum density of 30 pc/mi/ln. Minor incidents may still be absorbed, but the local deterioration in service will be substantial. Queues may be expected to form behind any significant blockage. The driver now experiences a noticeable increase in tension due to the additional vigilance required for safe operation.

4. Level-of-service D—Level D borders on unstable flow. In this range, small increases in flow cause substantial deterioration in service. Average travel speeds of 46 mph or more can still be maintained on 70-mph freeway elements. Freedom to maneuver within the traffic stream is severely limited, and the driver experiences drastically reduced physical and psychological comfort levels. Even minor incidents can be expected to create substantial queuing, because the traffic stream has little space to absorb disruptions. Average spacings are about 125 fl, or 6 car-lengths, with a maximum density of 42 pc/mi/ln.

5. Level-of-service E—The boundary between LOS D and LOS E describes operation at capacity. Operations in this level are extremely unstable, because there are virtually no usable gaps in the traffic stream. Vehicles are spaced at approximately 80 ft, or 4 car-lengths, at relatively uniform headways. This, however, represents the minimum spacing at which stable flow can be accommodated. Any disruption to the traffic stream, such as a vehicle entering from a ramp, or a vehicle changing lanes, causes following vehicles to give way to admit the vehicle. This condition establishes a disruption wave which propagates through the upstream traffic flow. At capacity, the traffic stream has no ability to dissipate even the most minor disruptions. Any incident can be expected to produce a serious breakdown with extensive queuing. The range of flows encompassed by LOS E is relatively small compared to other levels, but reflects a substantial deterioration in service. Maneuverability within the traffic stream is extremely limited, and the level of physical and psychological comfort afforded to the driver is extremely poor. Average travel speeds at capacity are approximately 30 mph.

6. Level-of-service  $\dot{F}$ ---Level F describes forced or breakdown flow. Such conditions generally exist within queues forming behind breakdown points. Such breakdowns occur for a number of reasons:

a. Traffic incidents cause a temporary reduction in the capacity of a short segment, such that the number of vehicles arriving at the point is greater than the number of vehicles that can traverse it.

b. Recurring points of congestion exist, such as merge or weaving areas and lane drops, where the number of vehicles arriving is greater than the number of vehicles traversing the point.

c. In forecasting situations, any location presents a problem when the projected peak hour (or other) flow rate exceeds the estimated capacity of the location.

It is noted that in all cases, breakdown occurs when the ratio of actual arrival flow rate to actual capacity or the forecasted flow rate to estimated capacity exceeds 1.00. Operations at such a point will generally be at or near capacity, and downstream operations may be better as vehicles pass the bottleneck (assuming that there are no additional downstream problems). The LOS F operations observed within a queue are the result of a breakdown or bottleneck at a downstream point. The designation "LOS F" is used, therefore, to identify the point of the breakdown or bottleneck, as well as the operations within the queue which forms behind it.

The extent of queuing, and the delays caused by queuing, are of great interest in the analysis of congested freeway segments. Chapter 6 contains a methodology for estimating the queue length and delays behind a bottleneck with known arrival and discharge rates. The procedure allows a rough quantification of the extent of congestion created by a LOS I<sup>2</sup> situation.

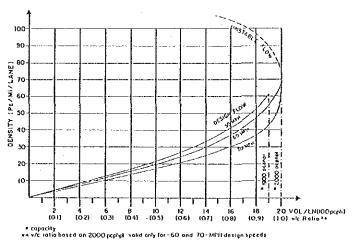


Figure 3-3. Density flow relationships under ideal conditions.

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Link	Node From		Dir.	Leng. (10m)	Sect. Lane	lnt, Lane	Wid.	Adj Factor	Cap /hr	Link Volume Peak-H Day	Volume/Cap. LV/C TOT	Velo Peak	city Off-P
									1000	207 4177	0.283 0.230		
11	23	24	1	11	1	1	10.0	0.97	$\begin{array}{r}1399\\1399\end{array}$	249 3235	0.177 -	· ·	
11	24	23	2	11	1	1	10.0	$0.97 \\ 0.96$	1381	397 4177	0.287 0.233		
12	12	23		103	1	1	16.1	0.96	1381		0,180 -		
12	23	12	2	103	1	1	16.1		1381		0.509 0.622	1.1	
13	9	12	1	118	1	1	16.0	0,96	1381	1016 10984			1
13	12	9	2	118	1	1	16.0	0,96	1381	640 7360	0.463 0.524		
14	4	9	1	200	1	1	16.0		1381	810 9315	0.586 -		
14	9	4	2	200	1	1	17.6	0.95	1376	916 10531	0.665 0.576	16	24
21	21	24	1	41	2	1	17.6	0.95	1376		0.486 -	17	37
21 22	24 13	21	2 1	41 71	2	2	16.5	0.96	2759		0.390 0.345	37	56
22	21	21	1	71	ž	2	16.5	0.96	2759		0.299 -	38	53
23	21	13 13	1	103	2	2	19.0		2744		0,407 0.361	37	49
23	13	· 8	2	103	. 2	. 2	19.0	0.95	2744	865 10236		37	52
23	5	8	1	55	3	2	24.8	0.94	2709		0.412 0.366	44	37
24		5	2	55	3	2	24.8	0.94	2709	865 10236	0.319 -	23	27
25	2	- 5	1	46	1	1	6.0	0,94	1357	910 10465	0.670 0.636		
25	5	2	2	46	ĩ	1	6.0	0.94	1357		0.602 -		
26	1	2	1	200	î	ĩ	6.0	0.94	1357	850 9775	0.626 0.637		
26	2	1	2	200	ĩ	ī	6.0	0.94	1357	880 10120	0,648 -		
31	7	14	1	78	3	2	21.0	0.95	2732	1384 17028	0.506 0.569	26	28
31	14	7	2	78	3	2	21.0	0.95	2732	1726 17925	0.631 -	40	51
32	6	7	ĩ	28	3	2	25.7	0.94	2704	1366 15709	0.505 0.509	41	43
32	7	6	2	28	3	2	25.7	0.94	2704	1392 16008		32	55
33	5	6	1	75	3	1.5	21.4	0.95	2047		0.659 0.715	24	19
33	5	5	2	75	3	1.5	21.4	0.95	2047	1579 18159		2.2	19
34	3	. 5	1	200	1	1	18.1	0.99	1430	1365 15698	0,954 0.905	1	
34	5	3	2	200	1	1	18.1	0.99	1430	1226 14099			
41	26	27	1	40	1	1	9.0	0.97	1402		0.151 0.151		
41	27	26	2	40	1	1	9.0	0.97	1402	0 0			
42	2.7	28	1	21	2	1	14.7	0.96	1385		0.153 0.359	34	
42	28	27	· 2	21	2	- 1	14.7	0.96	1385		0.565 -	25	27
43	28	29	1	44	- 2	· 1	14.7	0.96	1385		0.153 0.359	24	39
43	29	28	2	44	2	· 1	14.7	0.96	1385		0.565 -	11	22
44	. 29	-30	1	45	. 2	1	14.7	0.96	1385		0.153 0.359	24	39
44	30 .	29	2	45	2	1	14.7	0.96	1385	and the second	0.565 -	11	22
45	30	31	1	27	2	1	14.7	0.96	1385		0.503 0.405	33	48
45	31	30	2	27	2	1	14.7	0.96	1385		0.306 -	19	27
46	31	32	1	34	2	1	24.1	0.94	1356		0.731 0.623	19	26
46	32	31	2	34	2	1	24.1	0.94	1356		0.516	24	45
47	32	33	1	147	1	1	7.0	0.98	1408		0.691 0.658	39	44
47	33	32	2	147	1	1	7.0	0.98	1408		0.625 - 0.571 0.502	36	52
48	33	34	1	200	1	1	7.0	0.98	1408				
48	34	33	2	200	1	1	7.0	0.98	1408		0.433 -		10
51	61	62	1	82	. 3	<u>-2</u> 2	25.6	$0.94 \\ 0.94$	2704 2704	2172 25796	0.760 0.781	28 43	40
51	62	61	2	82	3		25.6	0.94	2704		0.760 0.781		36 12
52	62	63	1	14	3 3	2 2	25.5	0.94	2705	2057 20602		13 29	25
52	63 63	62 64	2	14 13	3	2	25.5	0.94	2705		0.607 0.619	13	12
53	63 64	63	2	13	3	2	25.5	0.94	2705	1707 19631		29	25
53 54	64	65	1	25	3	2	25.0	0.94	2705		0.555 0.679	29	26
54 54	65	64	2	25	3	2	25.0	0.94	2708	2177 26034		24	13
	65	99	1	20 49	3	2	23.5	0.94	2708		0.665 0.664	28	32
55	00	33	1	49	3	2	60.0	0.24	2111	1001 20100	0.000 0.004	20	32

	Node			Leng.	Sect.	Int.		Adj.	Cap.	Link Volume	Volume/Cap.	Veloc	ity
Link	From	To	Dir.	(10m)	Lane	Lane	Wid.				LV/C TOT	Peak O	ff-P
55	99	65	2	49	3	2	23.5	0.94	2717	1805 20758		14	43
56	99	66	1	25	3	2	23.5	0.94	2717		0.665 0.664	28	32
56	66	99	2	25	3	2	23.5	0.94	2717	1805-20758		14	43
57	66	67	1	14	3	2	23.9	0.94	2714		0.601 0.600	17	32
57	67	66	2	14	3	2	23.9	0.94	2714	1626 18699		6	13
58	67	68	1	21	-3	2	23.8	0.94	2715		0.549 0.551	32	40
58	68	67	2	21	. 3	2	23.8	0.94	2715	1501 17262		28	50
59	68	69	1	45	3	2	23.2	0.94	2718		0.497 0.501	13	17
59	69	68	2	45	3	2	23.2	0.94	2718	1376 15824		33	40
60	69	70	1	53	3	2	24.0	0.94	2714		0.431 0.477	37	43
.60	70	69	2	53	3	2	24.0	0.94	2714	1423 16365		14	40
61	70	71	1	13	3	3	24.0	0.99	4332		0.243 0.269	26	36
61	71	70	2	13	3	3	24.0	0.99	4332	1281 14732		30	50
62	71	72	1	165	3	3	24.0	0.99	4332		0.162 0.179	64	61
62	72	71	2	165	3	3	24.0	0.99	4332		0.197 -	52	61
63	72	73	1	0	3	3	24.0	0.99	4332		0.129 0.143		
63	73	72	2	0	3	3	24.0	0.99	4332		0.157 -		4.5
-71	66	76	1	40	3	2	20.6	0.95	2734		0.233 0.334	31	46
71	76	66	2	40	3	2	20.6	0.95	2734	1190 13685		17	33 60
72	76 77	77 76	1 2	30 30	3 3	1.5	23.2	0.94	2039 2039	801 9211 1097 12615	0.392 0.465	43 34	31
73	77	79	1	30 7	3	1.5	23.2 23.9	$0.94 \\ 0.94$	2039		$0.354 \ 0.362$	34 10	10
73	79	- 77	2	7	3	2	23.9	0.94	2714	1004 11464		19	23
74	79	80	1	37	3	2	20.0	0.94	2858		$0.336 \ 0.344$	24	20
74	80	79	2	37	3	3	20.0	0.99	2858	1004 11464		20	44
75	80	92	1	78	3 3	ž	20.0	0.95	2738		0.405 0.414	24	59
75	92	80	2	78	3	2	20.0	0.95	2738	1157 13212		34	58
76	92	94	ĩ	85	3	2	20.0	0.95	2738		0.324 0.366	36	30
76	94	92	2	85	3	2	20.0	0.95	2738	1116 12834		35	59
77	94	95	ĩ	200	ĭ	1	13.5	0.99	1230		0.541 0.707		
77	95	94	2	200	ī	i	13.5	0.99	1230	1075 12363			
80	101	88	1	24	2	î	15.7	0.96	1382		0.873 0.948	23	23
80	88	101	2	24	2	ì	15.7	0.96	1382	1415 16273		25	28
81	61	101	1	144	2	1	15.7	0,96	1382		0.873 0.948	23	23
81	101	61	2	144	2	1	15.7	0.96	1382	1415 16273		25	28
82	88	90	1	. 84	1	1	6.2	0.98	1411	1100 12775	0.779 0.756	21	32
82	90.	88	2	84	1	1	6.2	0.98	1411	1036 13526	0.734 -	24	35
83	90	97	1	148	1	1	7.0	0.98	1408	1363 15675	0.968 0.911	24	37
83	97	90	2	148	1	1	7.0	0.98	1408	1203 13835	0.854 -	27	33
84	97	98	1	200	1	1	7.0	0.99	1429	2138 24587	1.496 1.191	35	30
84	98	97	2	200	1	1	7.0	0.99	1429	1268 14582	0.887 -	33	48
111	12	13	1	32	3	2	20.0	0.95	2738	612 8942	0.223 0.260	15	21
111	13	12	2	32	3	2	20.0	0.95	2738	812 9326	0.296 -	23	37
112	13	14	1	89	3	2	16.0	0.96	2762	761 9406	0.275 0.275	23	42
112	14	13	. 2	89	3	2	16.0	0.96	2762		0.274 -	27	37
113	14	15	1	51	3	2	26.0	0.94	2702		0.380 0.405	34	45
113	15	14	2	51	3	2	26.0	0.94	2702	1162 13363		16	57
114	15	16	1	56	3	2	25.9	0.99	2858		0.346 0.359	58	59
114	16	15	2	56	3	2	25.9	0.99	2858	1067 12271		63	53
115	16	17	1	105	3	2	25.9	0.94	2702		0.352 0.356	47	56
115	17	16	2	105	. 3	. 2	25.9	0.94	2702	973 11190		55	57
116	17	32	1	11	3	2	23.1	0.94	2719		0.336 0.329	13	21
116	32	17	2	11	3	2	23.1	0.94	2719	879 10109	0.323 -	26	66

	Node From	 To		Leng. (10m)	Sect. Lane	lnt. Lane	Wid.	Adj. Factor	Cap. /hr.	Link Volume Peak-H Day	Volume/Cap. LV/C TOT	Veloc Peak C	
								0.06	1200	1318 15157	0.955 1.006	36	42
121	32	36	-1		2	1	16.2	0,96	1380	1461 16802	1.058 -	17	46
121	36	32	. 2	- 51	2	1	16.2	0.96	1380	1461 16779	1.020 1.042	16	29
122	36	39	ĺ	25		1	16.2	0.99	1429	1521 17492	1 064	41	36
122	39	36	2	25	2	· 1	16.2	0.99	1429	1021 17454	0.766 0.789	25	31
123	39	48	1	70	2	1	16.4	0.96	1380		0.811 -	2.5	34
123	48	39	2	70	- 2	1	16.4	0.96	1380	1120 12000	0.837 0.867	24	27
124	48	50	1	25	2	1	16.3	0.96	1380		0.857 0.001	13	23
124	50	48	2	25		1	16.3	0.96	1380	1237 14220	0.938 0.867	25	26
125	50	. 51	1	25	2	1	16.3	0.99	1429	1341 15424	0.795 ~	- 30	- 57
125	51	50	2	25	2	1	26.3	0.99	1429	1137 13076	1 160 1 039	25	26
126	.51	52	1	10	2	. 1	16.9	0.95	1378	1612 18538	1.169 1.038	30	-57
126	52	51	2	10	2	1	16.9	0.95	1378	1249 14364	0.900 -	5.7	20
127	52	69	1	2.5	2	1	16.5	0.96	1379		1,168 1.037	26	21
127	69	52	2	25	2	1	16.5	0.96	1379	1249 14364	010.00		
131	69	75	. 1	71	2	1	16.0	0.96	1381		0.577 0.597	41	41
131	75	69	2	.71	2	1	16.0	0,96	1381		0.616	13.	44
132	75	78	1	58	2	1	16.0	0.96	1381		0.577 0.597	52	54
132	78	75	2	58		1	16.0	0.96	1381		0.616 -	42	54
133	78	80	ĩ	34	2	1	19.0	0.96	1372		0.580 0.600	44	26
133	80	78	2	34	2	1	19.0	0.96	1372		0.620 ~	14	19
133	84	- 80	1	80		2	23.4		2717	713 8753	0.262 0.280	36	33
	80	-84	2	80	3	2	23.4	0,94	2717	812 9614	0.298 ~	28	44
141			1	95	3	2	25.6	0,94	2704	1235 14180	0.456 0.400	30	31
142	100	84	2	95	л З	2	25.6	0.94	2704	932 10718		35	48
142	84	100	1	95 71	3	2	25.6	0.94	2704		0.456 0.400	30	31
143	100	88			3	2	25.6	0.94	2704			35	48
143	88	100	2	71	3	2	24.0	0.94	2714	883 10028	0.325 0.297	29	12
151	87	88	1	40	3	2	24.0	0.94	2714		0.269 -	15	30
151	-88	87	2	40		- 2	23.0	0.94	2720		0.139 0.178	52	53
152	11	87	ĩ	435	3		23.0	0.94	2720		0.216 -	49	49
152	87	11	2	455	. 3	2			2720		0.220 0.220	40	40
153	11	12	1	101	. 3	2	23.0	0.94	2720		0.219 -	61	69
153	12	11	2	101	3	2	23.0	0.94			0.713 0.595	35	36
161	25	26	1	10	3	2	22.8	0.94	2721			14	38
161	26	25	2	10	3	. 2	22.8	0.94	2721	1297 14916		35	36
162	20	25	1	38	3	2	19.9	0.95	.2738		0.469 0.530	14	38
162	25	20	2	38	3		19.9	0.95	2738	1618 18607		9	34
163	14	20	1	70	3	2	21.0	0.95	2732		0.423 0.454	-	
163	20	14	2	70		2	21.0	0.95	2732	1326 13635		12	20
171	64	81	1.	65	2	2	15.4	0.96	2765		0.452 0.401	32	33
171	81	64	2	65	2	2	15.4	0.96	2765	967 13260		22	27
172	81	82	1	25	2	2	15.4	0.96	2765		0.271 0.240	29	30
172	82	81	2	25	2	2	15.4	0.96	2765		0.209 -	43	36
173	82	83	1	32	2	2	13.4	0.96	2765		0.271 0.240	30	46
173	83	82	2	32	2	. 2	13.4	0.96	2765	580 6670	0.209 -	37	50
174	83	84	1	.27	2	2	24.8	0.94	2709	725 8338	0.267 0.238	15	21
174	84	83	2	27	2	2	24:8	0.94	2709	565 6498	0.208 -	40	41
175	84	91	1	80	2	2	13.4	0.94	2778	640 7360	0.230 0.205	50	48
175	91	84	2	80	2	2	13.4	0.94	2778		0.179 -	29	19
176	91	96	ĩ	90	2	2	15.4	0.96	2765		0.115 0.103		
176	96	91	2	90		2	15.4	0.96	2765		0.090 -		
181	-90	91	ī.	211	1	1	6.9	0.98	1408		0.303 0.269		
181	91	90	2	211	1	1	6.9	0.98	1408		0.236 -		
181	91	92	ว้	71	1	1	7.0	0.98	1408		0.213 0.188		
104	. 91	26	. *	11	· •	T		v	1 - 100	.000 0400	VI210 VI100		

		Node			Leng.	Sect.	Int.		Adj.	Cap.	Link V	olume	Volume/Cap	. Vel	ocity
	Link	From	То	Dir.	(10m)	Lane	Lane	Wid.	Factor	/hr.	Peak-H	l Day	LV/C TO	DT Peak	Off-P
			• • • • <u>•</u> •				*****								
	182	92	91	2	71	1	1			1408	230		0.163		
	191	97	96		294	1	1	8,9	0.97		407		0.290 0.37	/3	
	191	96	97	2	294	1	1			1402	639		0.455	~	
	192	96	94	1.	58	1	1	8.9	0.97	1402	280		0.199 0.26	60 	
	192	94	96	2	58	1	1	8.9	0.97	1402	450		0.320	-	
	193	93.	94	1	200	1	1	9.0	0.97	1402	170		0.121 0.15	<b>b</b> b	
	193	94	93	2	200	1	1	9.0	0.97	1402	270		0.192	~ 	
÷	194	72	93 72	1	211	1	1	8.9	0.97	1402	270		0.192 0.18		
	194	35	72	2	211	1	1	8.9	0.97	1402	170				
	195	. 72		12	218	1	1	8.9	0.99	1429	270		0.188 0.15		
	195 196	33	35	1	218 218	1 1	1	8.9 8.9		1429	$170 \\ 270$		0.118		
	196	- 35	33	2	218	1	1	8.9	0.99	1429	170		0.188 0.15	-	
	201	. 8	7	1	102	3	3	38.5	0.99	3940	157		0.118 0.039 0.03	21	
	201	7	8	2	102	3	3	38.5	0.91	3940	89		0.022	-	
	202	. 9	8	. 1	45	1	1	16.9	0.95	1378	157		0.113 0.08	۱Q	
	202	8	ğ.	2	45	1	i	16.9	0.95	1378	89		0.064	-	
	203	10	9	1	143	î	1	16.9	0.95	1378	160		0.116 0.09	10	
	203	9	10	2	143	î	ì	16.9	0.95	1378	90		0.065	-	
	204	10	11	1	170	3	2	24.1	0.94	2713	90		0.033 0.04	16	
	204	11	10	2	170	3	2	24.1	0.94	2713	160		0.058	-	
	211	87	89	1	40	1	1	7.3	0.97	1407	508		0.361 0.38	50	
	211	89	87	2	40	1	1	7.3	0.97	1407	478	5497	0.339	-	
	212	89	90	1	41	1	1	7.2	0.97	1407	508	5842	0.361 0.35	0	
	212	90	89	2	41	1	1	7.2	0.97	1407	478	5497	0.339	-	
	311	26	43	1	35	3	2	22.8	0.94	2721	2155	24783	0.791 0.63	34 26	34
	311	43	26	2	- 35	3	2	22.8	0.94	2721	1297	14916	0.476	- 41	
	312	43	44	1	- 21	3	2	20.5	0.95	2735			0.787 0.77	4 12	
	312	44	43	2	21	3			0.95	2735			0.760		
	313	44	45	1	. 18	3		27.5	0.93	2693			0.920 0.81		
	313	45	44	2	.18	3	2	27.5		2693			0.710	- 25	
	314	45	58	1	17	3		25.7	0.94	2703			0.916 0.81		
	314	58	45	2	17	3	2	25.7	0.94	2703		23565			
	315	58	64	1		3	2	23.1	0.94	2719			0.911 0.80		
	315	64	58	2	38	3	2	-23.1	0.94	2719		23565		- 14	40
	321	78	92	- 1	122	1	1	0.0		1357	135		0.099 0.09	19	
	321 331	92 79	78 78	2 1	122 50	1	1 1	0.0	0.94	$1357 \\ 1357$	$135 \\ 135$		0.099 0.09	-	
	331	79	79	2	50	1	1	0.0	0.94	1357	135		0.099 0.09	-	
	332	83	79	. 1	79	1	1	0.0	0.94	1357	135		0.099 0.09	-	
	332	79	83	2	79	1	1	0.0	0.94	1357	135		0.099 0.08	-	
	341	74	93	1	55	î	1	0.0	0.94	1357	135		0.099 0.09	a di	
	341	93	74	2	55	1	1	0.0	0.94	1357	135				
	342	71	74	1	88	í	1	0.0	0.94	1357	270		0.198 0.19		
	342	74	71	2	88	1		. 0.0	0.94	1357	270		0.198	-	
	351	24	25	1	73	2	î	13.2	0.96	1389	527		0.379 0.39	4	
	351	25	24	2	73	2	ĩ	13.2	0.96	1389	570		0.410	-	
	361	22	23	ĩ	40	ĩ	0.5	5.1	0.98	707			0.869 0.75	i3	
	361	23	22	2	40	0.5	0.5	5.1	0.98	707	450		0.636	·	
	362	22	60	1	155	2	2	16.0	0.96	2762	691		0.250 0.28	10	
	362	60	22	2	155	2	2	16.0	0.96	2762	860		0.311	-	
	371	22	24	1	60	1	1	9.1	0.97	1402	615		0.438 0.37	'9	
	371	24	22	2	60	1	1	9.1	0.97	1402	450	5175	0.320	-	

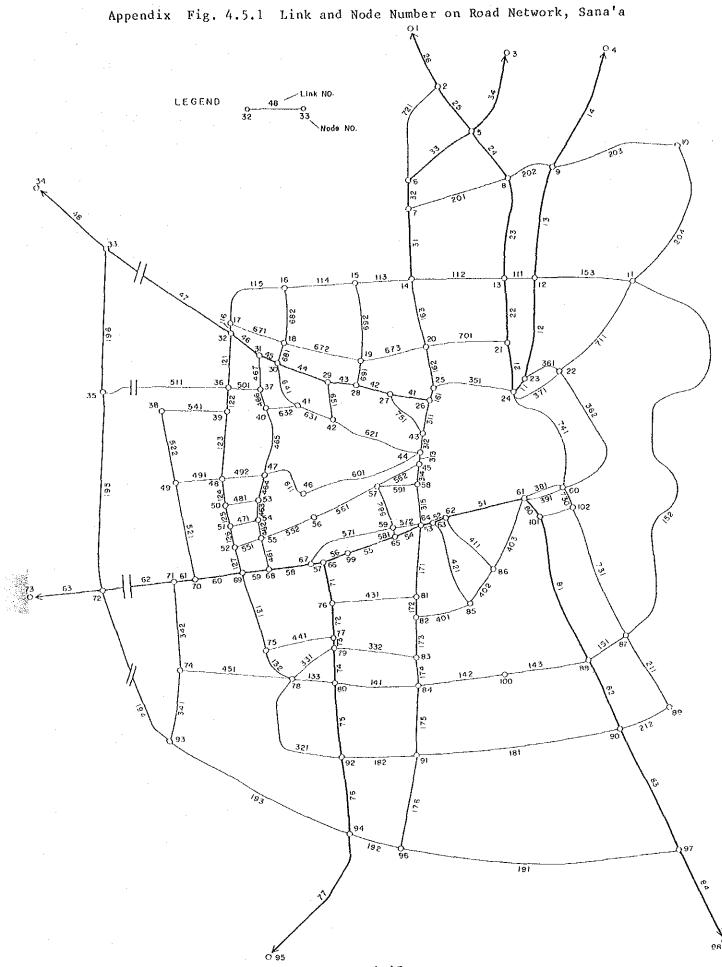
Appendix Table 4.5.1	Link Volume	and	Capacity	in	1987,	Sana'a
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Link	Node From	 To		Leng. (10m)	Sect. Lane	lnt. Lane	Wid.	Adj. Factor	Cap. /hr.	Link Vo Peak-H	Day	LV/C	e/Cap. TOT	Peak	clty Off-P
~~ <b>~</b> ~~~									1408						
381	60	61	1	36	. 2	1	6.8		1408	0171	1549	0.651		1.1	
391	61	60	2	35	2	1	7.1	0,97	1357	135	1500	0.099	0,099		
401	85	82	1	67	1	1	0.0		1357	135	1500	0.099			
401	82	85	2	67	1	1	0.0		1357	135	1500	0.099	0.099		
402	86	85	- 1	36	1	1	0.0		1357	135	1500	0.099	-		1.1
402	85	86	2	36	1		0.0		1357	135	1500	0.099	0.099		
403	61	86	1	70	1	1	0.0		1357	135	1500	0.099			
403	86	61	2	70 64	1	1	0.0		1357	135	1500	0.099	0.099		
411	62 86	86 62	1	64	1	1	0.0		1357	135	1500	0.099	.**		
411 421	63	85	1	85	i	î	0.0		1357	135	1500	0.099	0.099		
421	85	63	2	85	ì	î	0.0		1357	135	1500	0.099	· -		
421	81	76	1	- 80	1	î	0.0		1357		1500	0.099	0.099		
431	76	81	2	80	1	1	0.0		1357	135	1500	0.099			
441	77	75	1	66	1	ī	0.0		1357	135	1500	0.099	0.099		
441	75	77	2	66		î	0.0		1357			0.099			
451	78	74	ĩ	100	1	Ī	0.0		1357			0.099	0.099		
451	74	78	2	100	ĩ	í	0.0		1357	135	1500	0.099			
461	55	68	ĩ	31	1	1	7.6	0.97	1406	648	7452	0.460	0.391		
461	68	55	2	31	1	1	7.6	0.97	1406			0.322	.**		
462	54	55	1	2	1	i	11.9	0.96	1393	648		0.465	0.395	31	35
462	55	54	2	2	1	i	11.9	0,96	1393	454	4981	0.325	-	9	43
463	53	54	1	23	1	1	11.9	0.96	1393	648	7452	0.465	0.395	31	35
463	54	53	. 2	23	1	}	11.9	0,96	1393			0.325	-	9	43
464	47	53		37	1	1	11.9	0.96	1393			0.465		7	27
464	53	47	2	37	1	1	11.9	0.96	1393			0.325	· · · ·	22	33
465	40	47	1	66	1	1	.12.9	0.96	1390			0.510		24	33
465	47	40	2	66	1	1	12.9	0.96	1390			0.539		16	24
466	37	40	1	15	1	1	11.2	0.97	1395			0.508		36	42
466	40	37	2	15	2	1	11.2	0.97	1395			0.537		20	36
457	31	37	1	30	2	2	16.1	0.96	2761			0.280	0.330	23	49
467	37	31	2	30	2	2	16.1	0.96	2761	1051 1				33	37
471	54	51	1	28	1	1	0.0	0.94	1357			0.099			
471	51	54	2	28	1	1	0.0		1357			0.099	· -		
481	53	50	1	36	1	1	0.0	0.94	1357			0.099			
481	50	53	2	36	1	1	0.0	0.94	1357			0.099	· -		
491	48	49	1	55	2	1	16.0	0.96	.1381			0.329	0.288		
491	49	48	2	55	2	1	16.0	0.96	1381			0.248			
492	47	48	1	40	- 1	.1	0.0		1357			0.099	0.099		
492	48	47	2	40	1.	1	0.0	0.94	1357			0.099	~ ~ ~		
501	37	36	1	29	1	1	10.7	0.97	1397			0.197	0.212		
501	36	37	2	29	1	1	10.7	0.97	1397			0.226	A 150		
511	36	35	1	164	1	1	8.4	0.97	1404			0.198	0.155		
511	35	36	2	164	1	1	8.4	0.97	1404			0.107	A AAA		
521	49	70	1	75	1	1	0.0	0.94	1357			0.099	0.033		
521	70	. 49	2	75	1	1	0.0		1357			0.099	~ ~ ~ ~		
522	38	49	1	66	1	1	0.0	0.94	1357			0.099	0.033		
522	49	38	2	66	1	1	0.0		1357			0.099	- 10 <sup>-</sup>		
541	39	38	1	70	1	1	0.0		1357			0.198	0.138		
541	38	39	2	70	1	1	0.0	0:94	1357			0.198	0.000		
551	55	52	1 2	25	1	1	0.0	0.94	1357			0.099	0.033		
551	52	55		25	1	1	0.0		1357			0.099	0 000		
552	56	55	1	53	1	1	0.0	0.94	1357	135	1200	0.099	0.038		

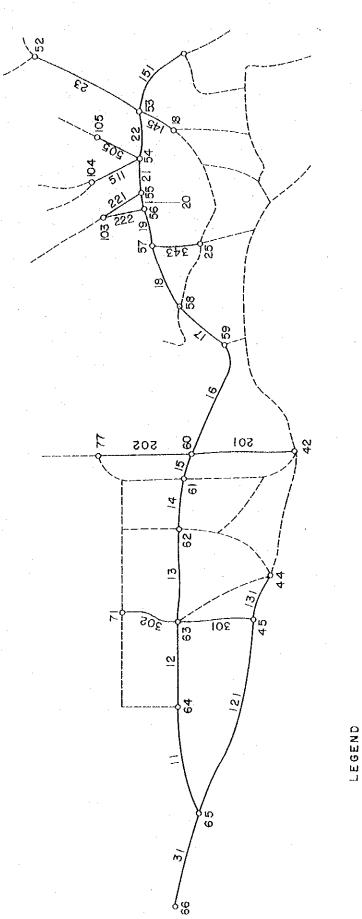
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	Node			Leng.	Sect.	Int.		Adj.	Cap.	Link Volume	Volume/Cap.	Veloci	ity
Link	From	То		(10m)						Peak-H Day		Peak Of	f-P
552	55	56	2	53	1	1	0.0	0.94	1357		0.099 -		
561	57	56 57	1	118	1	1	0.0	0.94	1357		0.099 0.099		
561 562	56 45	57	2	118 50	1	1	0.0	0.94	1357		0.099 -		
562	57	45	1	50	1	1	0.0	$0.94 \\ 0.94$	$1357 \\ 1357$		0.099 -		
503	59	67	Ì	53	1	1	0.0	0.94	1357		0.099 0.099		
571	67	59	2	53	1	1	0.0	0.94	1357		0.099 -		
572	64	59	ĩ	24	Î	i	0.0	0.94	1357		0.099 0.099		
572	59	64	2	24	ī	1	0.0	0.94	1357		0.099 -		
581	59	65	ĩ	5	î	î	0.0	0.94	1357		0.198 0.198		
581	65	59	2	5	1	ī	0.0	0.94	1357		0.198 -		
582	57	59	1	58	1	1	0.0	0.94	1357		0.099 0.099		
582	59	57	2	58	1	1	0.0	0.94	1357		0.099 -		
591	58	57	1	50	1	1	0.0	0.94	1357	135 1500	0.099 0.099		
591	57	58	2	50	1	1	0.0	0.94	1357	135 1500	0.099 -		
601	44	46	1	112	1	1	5.1	0.98	1414	507 4567	0.358 0.358	25	25
601	46	44	2	112	1	1	5.1	0.98	1414	0 0			
611	46	47	1	50	1	1	8.1	0.97	1405		0.360 0.360	18	24
611	47	46	2	50	1	1	8.1	0.97	1405	0 0			
621	44	42	1	87	1	1	9.2	0.97	1401		0.441 0.441	14	25
621	42	44	2	87	1	1	9.2	0.97	1401		0 -	• • •	~~
631	42	41	1	40	1	1	9.0	0.97	1402		0.228 0.228	38	32
631	41	42	2	40	1	1	9.0		1402	0 0		23	25
632	41 40	40 -11	. 1	0	2	2 2	12.0	0.96	2786		0.048 0.048	23	35
632 641	40	30	1	44	2	2	$12.0 \\ 15.2$	0.96	$2786 \\ 2766$		0.048 - 0.048		
641	30	41	2	44	2	2	15.2	0.96	2766		0.048 -		
651	42	29	ĩ	40	ĩ	ĩ	9.0	0.97	1402		0.213 0.155		
651	29	42	2	40	1	î	. 9.0		1402		0.096 -		
671	18	17	ī	60	2	2	0.0	0.94	2715		0.381 0.297		
671	17	18	2	60	2	2	0.0		2715		0.214 -		
672	19	18	1	78	2	2	0.0	0.94	2715		0.381 0.297		
672	18	19	2	78	2	2	0.0	0.94	2715	582 6693	0.214 -		
673	20	19	1	56	1	1	13.5	0.96	1388		0.746 0.582		
673	19	20	2	56	2	• 1	13.5	0.96	1388		0.419 ~		
681	18	30	1	27	1	1	0.0	0.94	1357		0.027 0.048		
.681	30	18	2	27	1	1	0.0	0.94	1357		0.069 -		
682	16	18	1	51	1 -	1	0.0	0.94	1357		0.027 0.048		
682	18	16	2	51	1	1	0.0		1357		0.069 -		
691	19	29	1	28	1	1	0.0	0.94	1357		0.028 0.049		
691	29	19	2	28	1	1	0.0		1357		0.070 -		
692	15 19	$\frac{19}{15}$	1 2	80 80	1	1	0.0	0.94 0.94	$\frac{1357}{1357}$		0.028 0.049		
692 701	21	20	2	78	1	1	$0.0 \\ 13.5$	0.94	1388		0.070 - 0.475 0.414		
	20	21	2	78	1	1	13.5	0.96	1388		0.354 -		
701 711	11	22	1	107	1	1	7.1	0.90	1408		0.095 0.095		
711	22	11	2	107	1	1	7.1	0.97	1408		0.095 -		
721	2	6	ī	98	2	1	16.0	0.96	1381		0.406 0.462		
721	6	ž	2	98	2	1	16.0	0.96	1381	716 8234			
730	102	87	ī	24	1	1	8.2	0.97	1404		0,688 0.696		
730	87	102	2	24	1	1	8.2	0.97	1404	990 11385			
731	60	87	1	166	1	1	8.2	0.97	1404		0.688 0.696		
731	87	60	2	166	1	1	8.2	0.97	1404	990 11385	0.705 -		

Link	Node From				Sect. Lane			Adj Factor							
741	24	60	1	145			0 0	0,94	1357	847	97.11	0.624	0.532	25	28
741	60	24	2	145	î	1		0.94	1357			0.439		24	žĭ
751	27	43	1	45	· 1	1	0.0	0.94	1357	783	9005	0.577	0.577		
751	43	27	2	45	1	1	0.0	0.94	1357	0	0	0	-		



								· ·			
	Node			Leng.	Sect	Int.		۸dj.	Cap.	L-V Volume/C	ap.
Link	From	To	hir	(10m)	Lane	Lane	Wid.	Factor	/hr.	Peak-H LV/C	TOT
Link	riom				Lunc						
11	64	65	1	26	2	2	16.1	0.96	2762	884 0.320 0.	327
- 11	65	64	2	26	$\overline{2}$	2	16.1	0.96	2762	926 0.335	••
12	63	64	1	47	2	2	20.0	0.95	2738	1157 0.422 0.	473
12	64	63	2	47	2	2	20.0	0.95	2738	1435 0.524	*
13	62	63	. 1	34	2	2	20.0	0.95	2738	1780 0.650 0.	587
13	63	62	2	34	2	2	20.0	0.95	2738	1439 0.525	-
13		62	1	19	2	2	20.0	0.95	2738	2425 0.885 0.	723
	61	0∠ 61	2	19	$\tilde{\tilde{2}}$	2	20.0	0.95	2738	1537 0.561	-
14	62 60	61	1	10	2	2	23.4	0.94	2712	2425 0.894 0.	730
15	61	60	2	10	2	2	23.4	0.94	2712	1537 0.566	-
15		- 60	1	46	2	2	17.4	0.95	2753	1892 0.687 0.	589
16	59		2	46	2	2	17.4	0.95	2753	1356 0.492	_
16	60	59 59		24	2	2	17.4	0.95	2753	1520 0.552 0.	539
17	58		1	24	. 2	2	17.4	0.95	2753	1448 0.525	-
17	59	58	2	24 25	2	2	18.0	0.95	2750		573
18	57	58	1		2	2	18.0	0.95	2750	995 0.361	-1
18	58	57	2	25	2	2	18.0	0.95	2750	1585 0.576 0.	561
19	56	57	1	10	2	2	18.0	0.95	2750		<b></b> ·
19	57	56	2	10	2	2	18.0	0.95	2750		561
20	55	56	1	10	2	2	18.0	0,95	2750	1502 0.546	
20	56	55	2	10				0.95	2750	1075 0.390 0.	348
21	54	55	1	13	2	2	18.0	0.95	2750	840 0.305	
21	55	54	2	13	2	2	18.0	0.95	2750	1075 0.390 0.	348
22	53	54	1	20	2	2	18.2		2750	840 0.305	-
22	54	53	2	20	2	2	18.2	0.95		1114 0.404 0.	283
23	52	53	1	48	2	2	17.5	0.95	2753	998 0.362	
23	53	52	2	48	2	2	17.5	0,95	2753	1387 0.492 0.	662
31	65	66	1	26	2	2	16.1	0.98	2816		000
31	66	65	2	26	2	2	16.1	0.98	2816	1729 0.613	808
121	45	65	1	76	1	2	11.4	0.97	1395	681 0.488 0.	000
121	65	45	2	76	1	1	11.4	0.97	1395	1011 0.724	151
131	44	45	1	17	1	1	13.0	0.96	1390	704 0.506 0.	191
131	45	44	. 2	17	1	1	13.0	0.96	1390	1086 0.781	000
145	53	18	1	17	1	1	9.7	0.97	1400		322
145	18	53	2	17	1	1	9.7	0,97	1400	427.0.305	101
151	10	53	1	30	1	1	12.9	0,96	1390	790 0.568 0.	481
151	53	10	2	30	1	1	12.9		1390	576 0.414	100
201	60	42	1	39	2	2	16.9	0.95	2756	580 0.210 0.	189
201	42	60	2	39	2	2	16.9	0.95	2756	467 0.169	1 ~ 0
202	77	60	1	28	2	2	14.9	0.95	2768	800 0.289 0.	178
202	60	77	2	28	2	2	14.9	0.95	2768	188 0.067	
221	103	55	· 1	24	0	0	0.0	0	0		.11
221	55	103	2	24	2	2	0.0	0.94	2714	300 0.110	-
222	103	56	1	24	2	2	0.0	0.94	2714		.11
222	56	103	2	24	0	0	0.0	0	0	0 0	
301	63	45	1		1	2	0.0	0.94	1357	300 0.221 0.	221
301	45	63	2	27	1	2	0.0		1357	300 0.221	-
302	71	63	1	20	1	2	0.0	0.94	1357	300 0.221 0.	221
302	63	71	2	20	1	1	0.0	0.94	1357	300 0.221	
343	57	25	1	16	1	1	10.3	0.97	1398	398 0.284 0.	421
343	25	57	2	16	1	2	10.3	0.97	1398	780 0.557	
505	105	54	1	22	1	1	0.0	0.94	1357	150.0.110 0.	110
505	54	105	2	22	1	1	0.0	0,94	1357	150 0.110	-
511	104	54	1	22	1	1	0.0	0.94	1357	150 0.110 0.	110
511	54	104	2	22	1	1	0.0	0.94	1357	150 0.110	



Appendix Fig. 4.5.2 Link and Node Number on Road Network, Taiz

31-----Link No. 65----Node No.

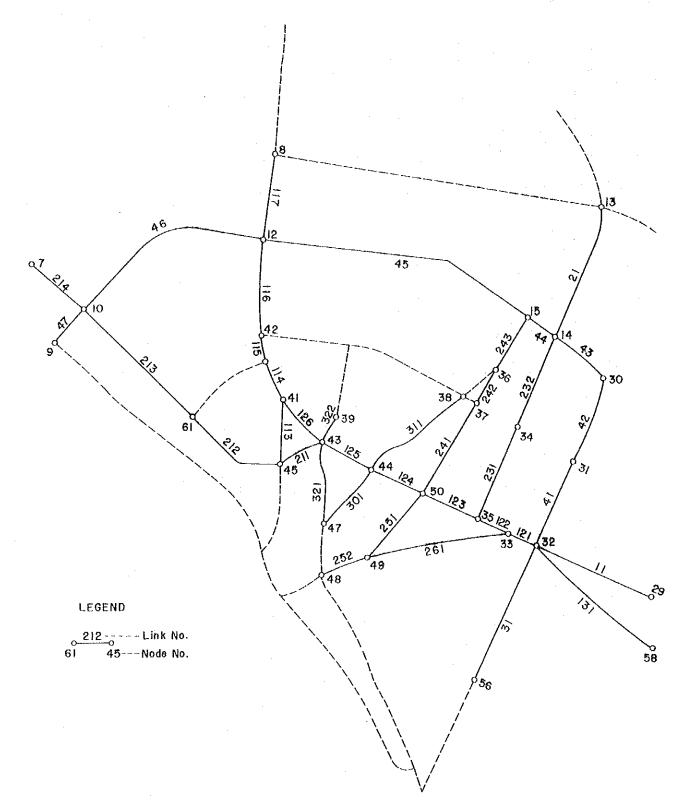
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# Appendix Table 4.5.3 Link Volume and Capacity in 1987, Hodeidah

	Node			Leng.	Sect.	lnt.		Adj.	Cap.	L-V Volume/Cap.
Link	From	Τo	Dir.	(10m)	Lane	Lane	Wid.	Factor	/hr.	Peak-H LV/C TOT
							~ ~ ~ ~ ~			
11	59	32	٤	50	2	2	22.0	0.94	2726	864 0.316 0.296
11	32	29	2	50	2	2	22.0	0.94	2726	750 0.275 ~
21	13	14	1	80	}	2	11.4	0.97	1395	371 0.265 0.259
21	14	13	$\hat{2}$	80	1	2	11.4	0.97	1395	
31	32	56	ī	90	2	2	17.2	0.95	2754	
31	56	32	2	90	2	2	17.2	0.95	2754	
-11	31	32	ĩ	60	3	3	25.3	0.94	4059	569 0.140 0.149
41	32	31	2	60	3	3	25.3	0.94	4059	644 0.158 -
42	30	31	1	60	3	3	25.3	0.94	4059	569 0.140 0.149
42	31	30	2	60	3	3	25.3	0.94	4059	644 0.158 -
			- 1	50	3	3	25.3	0.94	4059	569 0.140 0.149
43	30	14		-	3	3	25.3	0.94	4059	644.0.158 -
43	14	30	2	50	2	2	17.7	0.95	2751	386 0.140 0.132
44	14	15	1	22		2	17.7	Q.95	2751	341 0.123 -
44	15	14	2	22	2	2		0.95	2751	386 0.140 0.132
45	15	12	1	270	2		17.7		2751	341 0.123
45	12	15	2	270	2	2	17.7	0.95		309 0.112 0.105
-16	12	10	1	140	2	2	17.7	0.95	2751	273 0.099
46	10	12	2	140	2	<b>2</b>	17.7	0.95	2751	
47	10	9	1	17	2	2	0.0	0.94	2714	70 0.025 0.025
47	9	10	2	17	2	2	0.0	0.94	2714	70 0.025
113	41	45	1	42	2	2	14.2	0.96	2772	823 0.296 0.296
113	45	41	2	0	0	0	0.0	0	. 0	0 0 -
114	40	41	- 1	20	2	2	18.5	0.95	2747	1196 0.435 0.436
114	41	40	2	20	2	2	18.5	0.95	2747	1201 0.437 -
115	42	40	1	15	2	2	18.5	0.95	2747	1196 0.435 0.436
115	40	42	2	15	2	2	18.5	0.95	2747	1201 0.437 -
116	12	42	Ł	70	2	2	18.5	0.95	.2747	718 0.261 0.261
116	42	12	2	70	2	2	18.5	0.95	2747	721 0.262 -
117	8	12	1	50	2	2	18.5	0.95	2747	502 0.182 0.183
117	12	8	2	50	2	2	18.5	0,95	2747	505 0.183 -
121	32	33	1	21	2	2	22.0	0.94	2726	1698 0.622 0.151
121	33	32	$\hat{2}$	$\overline{21}$	$\frac{-}{2}$	2	22.0		2726	1559 0.371 ~
122	33	35	1	27	2	2	22.0	0.94	2726	1698 0.62 0.597
122	35	33	2	27	2	-2	22.0	0.94	2726	1559 0.571 -
123	35	50	ĩ	38	$\tilde{2}$	$\overline{2}$	22.0	0.94	2726	1738 0.637 0.655
123	50	35	$\hat{2}$	38	2	2	22.0		2726	1837 0.673 -
123	50	44	-1	40	2	2	22.0		2726	1891 0.693 0.630
	44	50	2	40	2	2	22.0		2726	1547 0.567 -
$\begin{array}{c}124\\125\end{array}$	44	43	ĩ	-40	2	2	22.0	0.94	2726	1528 0.560 0.547
	44	44	2	40	2	2	22.0		2726	1458 0.534
125		44	1	39	3	3	12.4	0.96	4175	1580 0.378 0.378
126	43	41	2	39	0	0	0.0	0.50	0	0 0 -
126	41			39 50	2	2	11.0	0.97	2792	376 0.134 0.108
131	58	32	1			2	11.0		2792	228 0.081 -
131	32	58		50	2				2192	0 0 0.430
211	43	45	1	0	0	0	0.0			
211	45	43	2	30	2	2	8.8		2804	1206 0.430 -
212	45	61	1	75	2	2	0.0	0.94	2714	220 0.081 0.081
212	61	45	2	75	2	2	0.0		2714	220 0.081 -
213	61	10	1	100	2	2	0.0		2714	220 0.081 0.081
213	10	61	2	100	2	2	0.0		2714	220 0.081 -
214	10	7	l	50	2	2	0.0		2714	150 0.055 0.055
214	7	10	2	50	2	2	0.0		2714	
231	34	35	1	60	2	2	18.0		2750	742 0.269 0.216
231	35	34	2	60	2	2	18.0		2750	
232	14	34	1	70	2	2	18.0	0.95	2750	742 0.269 0.263

### Appendix Table 4.5.3 Link Volume and Capacity in 1987, Hodeidah

					-							
. •	Node			Leng	Sect.	Int,		Adj.	Cap.	L-V	Volume	e/Cap.
	From	To	Dir.	(10m)	Lane	Lane	Wid.	Factor	Zhr.	Peak-H	1 LY/C	то1
		~ -	2		2	2	18.0	0,95	2750	706	0.256	
-232	34	14	-	70			18.0	0.95	2750		0.250	
241	37	50	1	68	2	2						
241	50	37	2	68	2	2		0.95	2750		0.162	
242	36	37	1	30	2 2 2	2	18.0	0.95	2750		0.2	
242	37	36	2	30	. 2	2			2750		0.162	
243	15	36	1	38	2	2	18.0	0,95	2750		0.2	0.228
243	36	15	2	38	2	2	18.0	0.95	2750	706	0.256	-
251	50	49	- 1	68	2	2	18.5	0.95	2747	374	0.136	0.132
251	49	50	2	68	2 2 2 2	2	18.5	0.95	2747	355	0.129	-
252	49	48	1	25	2	2	18.5	0.95	2747	374	0.136	0.192
352	48	49	2	25	2	2	18.5	0.93	2747	681	0.247	-
261	33	49	1	115	ō	ō	0.0		0	0	0	0.232
261	49	33	2	115	i	1	8.0	0.97	1405	326	0.232	-
301	44	47	ī	50	ô	0	0.0		0		0	
301	47	44	2	50	ĩ	2	8.0	0.97	1404	•	0.185	
.311	38	44		82	2	2	18.9	0.95	2744		0.127	
			2	82	2	. 2	18.9	0.95	2744		0.145	
311	44	38	2		2	. 2						A 22.
321	43	47	Ţ	56	l	1	0.0		1357		0.221	
321	47	43	2	56	1	1	0.0	0.94	1357		0.226	
322	39	-13	1	20	1	1	0.0	0.94	1357		0.182	0.172
322	43	39	2	20	1	1	0.0	0.94	1357	220	0.162	-



Appendix Fig. 4.5.3 Link and Node Number on Road Network, Hodeidah

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8	Vel Peek		-						40				45		07	ি ব বি ব	•		37							61		49		с Ч С						9 0 5 0							110 5-10		1\ **		26			
4 •	2	195-0		5	0.0	÷.	• •	н н	i c u	050.1	ı	6	0   0   1	• •	1 125		,	Ŧ,	0.993	1	1		1.130		-i -	•	•	0.511	ï	•	0.977		•		1.327	•	1		I.326	•	1 220	4	1	0.800	ı	÷.,	1.233	•		
	LV92 P/C	0.961	83	က် ( လ် (	2	5 C 2 C	3 -	> 1) T 16	<u>.</u>	-4 ¢ 7 ¢	0 0 0	90 ( 17 (	0 0	n ⊮ †⊂	3 C	1 C	ŝ	080	46	34	00		4.0	וו ת ס כ	20	22	0	51	ເລ. ຕຸເ	20	הית קיו⊂	. 4	22	40	6.4	ຕ	<u>.</u>		ຕີເ	0 1 0 1	0 C	10	. မာ ဂ	2	'n	ີ ເລັ່	с, с	ò	ຕ. ແ ເ	
	/Cap. TOT	0.648		1.485	8.00	0		i i		051-1	1	ļ	0.8.0	, ,	101 C	:	I	•	0.669	1	1	1	0.780	¢ F	4 I 2 - 2 7 - 2	1	t	0.344	•	I	ן מ ת ת כ	5	1		0.895	1	t		÷68.0	1	1 0 0 1 0 0	1 0 ,	1	0.540			0.831	•	11	
,  	LV87 P/C	0.648 0.625	60	00	00 i	0 C D C	4 6	30	2		200	2	5.0	ີ່ເ	20	11-	18	0.00	3	50	0.0		9 9 5 9	ວິເ	20	2	58	77	50	τ. 	7 4 7 0	2 (~	~	2	5.	י תו י תו	~; ·	2	сі (	8 10 10 10 10 10 10 10 10 10 10 10 10 10	įċ	2 6	1 61	i Ö	61	ŝ		õ		
	~ <sup>–</sup> –		5	99	87	2 C 9 5	30	4 - 5 e	7 9 77 0	2	300	20		4 0 2 c	្រុស ភូន		) H												5		⊃ 42 ≻1 č		06	잂	ମ ମ			() 1-	9 6	01 0 10 1	0 -	- U - T				10	ဗ်	ш	863 863	•
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Appendix Table 4.5.4 Volume and Capacity of Intersections in 1987 and 1992, Sana'a

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Appendix Table 4.5.4 Volume and Capacity of Intersections in 1987 and 1997. Sana'a

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Appendix Table 4.5.4 Volume and Capacity of Intersections in 1987 and 1992, Sana'a

1       1       0       0.44       1357       1335       200       0.099       0.294       0.147       0.442         1       1       0       0.044       1357       1335       200       0.099       0.294       0.147       0.442         1       1       1       0       0.044       1357       1335       200       0.099       0.295       0.147       0.442       135         1       1       1       1       0       0.044       1357       1335       200       0.099       0.295       0.147       0.442       135       0.134       0.147       0.442       135       0.134       0.147       0.442       135       0.134       0.134       0.147       0.442       135       0.147       0.442       135       0.147       0.442       135       0.147       0.147       145       0.147       145       0.147       145       0.147       145       0.146       0.146       135       0.146       135       0.146       135       0.146       0.147       145       145       145       145       145       145       145       145       145       145       145       145       145       145	9	ίΓ.	Leng. (10m)	Sect. Lane	(TU)	Int. Lane	wid.	Adj. Factor	Capa Sect	city (F)	х х 87 с	olume 1992	P/C	/Cap. TOT	567J	r/cap. ToT	Veloc Peak Of	1 ty
1       0       0.201       1207       120       0.000       0.000       0.0117       0.1117       0.1117       0.1117<	1		1 00 4					100	1 17 11 1 17 10 1 17 10 1	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1 ere 1 ere 1	100				.   	, ; ; ; ; ; ; ; ; ; ; ; ; ; ; ; ;	5 6 8 8
1       1       0       0.94       1357	1 V		36.0		-1 =			50	133	1	14	0	0.00	0.29	5 25	0.44		
35       2       0.54       1257       1357	r, -,		0.		г <b>ч</b> ,	~ * 7	•	00	() () () () () ()	000		0.0	0,0		4			
2       2       0.95       2700       540       651       650       0.95       1710       551       553       0.95       1711       511       52       0.95       1714       511       52       0.95       1714       511       52       0.95       1714       511       52       0.95       1714       511       52       0.95       1714       511       52       0.95       1411       111       111       123	-1.0		4 40 0 00		-1	-4 +		20	ວ 10 ວ ຕ3 ∹ ლ	0 0 1 1 1		5 O		0.29		4		
4.4       1       2       8.2       0.97       140.       555       0.97       147.       558       773       0.97       147.       15       0.197       147.       15       0.197       147.       155       0.197       147.       558       1735       0.066       0.254       0.155       0.156       0.157       0.157       0.156       0.155       0.156       0.156       0.155       0.156       0.156       0.256       0.156       0.155       0.156			40.0		1 (1)	। त्ता	~	6.0	10	4	3	3	0.0					53
4.0       3       23.95       0.94       2714       407       565       733       1056       0.231       0.431       0.133       0.631       0.431       0.133       0.631       0.431       0.133       0.631       0.431       0.133       0.631       0.431       0.133       0.631       0.431       0.133       0.631       0.431       0.133       0.631       0.441       0.441       0.441       0.441       0.441       0.441       0.441       0.441       0.441       0.441       0.441       0.441       0.441       0.441       0.441       0.441       0.441       0.441       0.441	Ч		144.		~	**	œ	0	14C	10 10	<del>6</del>	01 00 72 1	.н. о		80			
4.0       1       3       15.65       0.097       1407       147       1407       147       1407       147       1407       147       1407       147       1407<	<u>ମ</u>		0 1		C)	4	ন হ হ হ	0	52	ר די ה די ומ י	(	085			<u> </u>			.02 202
3       25.6       0.94       27.4       407       147       153       0.256       0.321       1031	сı -		40		~	মা (	· · ·	0,0	140	in in	1 0	601 1-1	0 0	0.40	- 1 - 1	.68		
3       2.55       0.94       774       407       147       140       15       0.53       10.54       0.53       10.54       0.53       10.54       0.53       10.54       0.53       10.54       0.53       10.54       0.53       10.53       10.55       10.53       10.55       10			4 I 7 I 7 I		(	(n (	ດ ດີ - ດີ	0,0	20 C	4 4		50 C						
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4       1       7       0.97       147       170       0.75       0.53       0.700       0.53       0.700       1.035       27       27       27       27       27       27       27       23       0.54       0.53       0.54       0.53       0.54       0.54       0.54       0.54       0.54       0.54       0.54       0.54       0.54       0.54       0.54       0.54 <td< td=""><td>· · ·</td><td></td><td>סק</td><td></td><td><b></b> ،</td><td> ،</td><td>,</td><td>00</td><td></td><td>140</td><td></td><td>200</td><td>10</td><td></td><td>10 0</td><td></td><td></td><td></td></td<>	· · ·		סק		<b></b> ،	،	,	00		140		200	10		10 0			
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200       1       1       8.95       0.97       1.00       1.00       0.192       0.484       0.192       0.114         200       1       1       1       2.55       0.171       1.00       0.192       0.144       0.117         200       1       1       1       2.55       0.171       1.00       0.197       0.197       0.197       0.197       0.197       0.197       0.196       0.144       0.179       1.444         200       1       1       1       1.55       0.99       1230       1402			2		-4 -	r-1 T	œ	0		v t m r	<u>e</u> i -	ç ç			0 0			
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200       1       1       7       0.99       1429       1265       1880       0.887       2.311       1.416       1.416       3.426       3.426       3.426       3.426       3.45       0.94       2717       4076       1807       2.679       0.446       1.418       2.218       235         25       3       23.45       0.94       2717       4076       1805       2679       0.446       1.451       2.218       235         71       3       2       3       23.45       0.94       2717       4076       1805       2679       0.443       -       0.6557       -       23         71       3       2       3       23.45       0.94       2717       4076       1805       2679       0.443       -       0.6557       1.313       215       225       23	ел		ମ ୧୮		-1		ð	0	4	4	9	5	0	. (	0	•	ï	
200       1       1       7       0.99       1429       1429       1429       1429       2170       1.496       1.496       2.218       23         49       3       2       3       23.45       0.94       2717       4076       1807       2676       0.443       -       0.655       13.3       33         25       3       23.45       0.94       2717       4076       1807       2676       0.443       -       0.656       13.3       33         25       3       23.45       0.94       2717       4076       1805       2676       0.443       -       0.656       13.3       33         21       3       2       3       25.6       0.94       2704       4056       1237       0.234       0.340       0.792       33         23       2       3       25.6       0.94       2764       1207       1789       0.464       -       23       30         24       2       1       2       15.65       0.96       1382       2764       1415       2098       0.705       -       23         144       2       1       1       1       2054	C1		20		-	-		0	4	14	1	$\frac{2}{2}$	æ ⊒	19		67 · 67	(r) (	20 4 9 19
14       2       3       25.6       0.94       27.1       4076       1805       2676       0.442       0.886       0.556       1.313       14         71       3       2       3       25.6       0.94       27.1       4076       1805       2676       0.442       0.561       1313       14         71       3       2       3       25.6       0.94       27.04       4056       1231       0.204       70.79       310 <td>*** 1</td> <td></td> <td>02 · 02</td> <td></td> <td> (</td> <td></td> <td>, ,</td> <td>0</td> <td>भ । म द</td> <td>4 5</td> <td>2</td> <td>06</td> <td>4</td> <td>н Т Т</td> <td>-4 C</td> <td>12.2</td> <td>י) רי</td> <td>&gt; &lt; &gt; ⊂</td>	*** 1		02 · 02		(		, ,	0	भ । म द	4 5	2	06	4	н Т Т	-4 C	12.2	י) רי	> < > ⊂
71       3       25.6       0.94       2704       4056       1235       1831       0.204       -       -       -       30         95       3       25.6       0.94       2704       4056       1235       1831       0.204       -       0.451       -       -       30         95       3       2       5.6       0.94       2704       4056       932       1382       0.229       0.340       0.792       35         24       2       1       2       15.65       0.96       1382       2764       1415       2098       0.511       0.948       0.773       15       23         144       2       1       1       1       2       15.65       0.966       1382       2764       1415       2098       0.756       1406       1404       1404       990       1468       0.7705       -       1.020       2.065       1.1406         142       1       1       1       1       1404       1404       966       1432       0.698       1.020       2.0655       2.0655       2.0655       2.0655       2.0655       2.0655       2.0655       2.0655       2.0655       2.0655	-		4 0		40	<b>יי ר</b> י	20	> c		204	0 a 1	n (C	 	0.88		1.35	4	1 61
95       3       2       3       25.6       0.94       2704       4056       932       1382       0.229       0.340       0.792       35         24       2       1       2       15.65       0.96       1382       2764       1207       1789       0.436       -       23       1       23         144       2       1       2       15.65       0.96       1382       2764       1415       2098       0.511       0.948       0.758       1.406         144       2       1       1       2       2382       2764       1415       2098       0.511       0.948       0.758       1.406         142       1       1       1       8.2       0.977       1404       1404       966       1432       0.689       1.020       2.065       2.065         24       1       1       1       8.2       0.977       1404       1404       966       1432       0.689       1.020       2.065       2.065			11~		1 6)	ы (п	- 10 2. (\) 3	0	10	10		¦⊷ m	0	) 	0	l 7 2	1 (7)	10
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