0					•					
Depth S. Dep	CONSOLIDATION TEST RESULTS									
Depth S. Dep	Project Model Infrastructure Project and Chareonraj Pumping station in 1488									
10	Boring No		į.		1		the state of the s			
10					·l	· · · · · · · · · · · · · · · · · · ·				
20. 3	5 10 %									
E 0 . 2	SS U Vertical Strai									
0 0.1 0.2 0.3 0.5 1.0 2 3 5 1.0 2 0 50 50	b://w0.3	Section (Control of Control of Co								
Restrict 90 % Consolidation Permeability Strain Height of Sample Height of			0.2 0.3 0.5	I O Vertx	2 2 2 2 2	5 N 20	· · · · · · · · · · · · · · · · · · ·			
Recompression Ratio RR RR RR RR RR RR RR RR	Pressure	90%	Coef. of		,					
Initial — — — Degree of Saturation, S 96		Consol.								
10.106	Ksc	Time min	CY ,10 cm7	K, IU cm/sec	2 %					
0.06 - 0.02 Solid Height of Script, FB 0.698 0.125 25.0 8.6 1.72 1.32 Diometer of Sample 0 6.35 cr 0.25 25.0 8.4 0.74 2.42 Wet Unit Weight 1 1 1.43 g/ 0.50 73.96 2.6 0.58 7.97 Dry Unit Weight 1/4 0.75 g/ 1 50.41 3.0 0.63 18.54 Uquid Limit LL 86.6 9/ 2 26.52 4.9 0.33 25.19 Plextle Limit PL 3/1.9 9/ 8 Compression Ratio CR 0.36 86 Recompression Ratio RR 0.04	Initial									
0.125 25.0 8.6 1.72 1.32 Discrete of Sample 0 6.35 0.25 25.0 8.4 0.74 2.42 Wet Unit Weight 1 1 1.43 9/ 0.50 73.96 2.6 0.58 7.97 Dry Unit Weight 1 d 0.75 9/ 1 50.41 3.0 0.63 18.54 Uquid Limit LL 86.6 9/ 2 26.52 4.9 0.33 25.19 Plextle Limit PL 3/1.9 9/ 8 Compression Ratio CR 0.36 8 Recompression Ratio RR 0.04	0.06	-				·	0.698			
0.25 25.0 8.4 0.74 2.42 Hell Off Help Off	0.1.25						6.35 a/c			
0.50 73.96 2.6 0.58 7.97 Dry Off Response 0.75 1 50.41 3.0 0.63 18.54 Uquid Limit LL 86.6 9/ 2 26.52 4.9 0.33 25.19 Plaxtle Limit PL 3/1.9 9/ 8 Compression Ratio CR 0.36 Recompression Ratio RR 0.04	0.25						1.43			
1 50.41 3.0 0.63 18.54 Oqea Game	0.50						0.75			
2 26.52 4.9 0.33 25.19 Pickile Climi 12 8 Compression Ratio CR 0.36 Recompression Ratio RR 0.04			i				00.0			
16 Recompression Ratio PR 0.04	2	26.52	4.9	0.33	25.19					
	8	<u> </u>		<u> </u>						
	16			·		Specific Sorrity G	2.67			

CONSOLIDATION TEST RESULTS									
Wedel Infractive Project Chargoniai Pumping Station 1400									
Project PX			Locotion						
Boring No	В-2	! Sampk	No. PST-7	Dept	h 7.0-7.80 m.	Date 9/3/88			
0 5 10 % x 15 2 25 15 0 . 10 0 . 0.5 0 . 15 0 . 0.5 0 . 0.5 0 . 0 . 0 . 0 . 0 . 0									
0	0.1	0.2 0.3 0.3	1.0 Vertic	2 3 col Pressure	5 XO Z	0 30 50 Ko			
Pressure	90%	Coal. of	· Coef. of			initio1 Final			
11033016	Consol.	Consolidation	Permeability	Verlical Stroin	$\tilde{\sigma}_{Vm} = 0.4 \text{ ksc}$ Height of Scripte, H	cm. 2.5			
Ksc	Time min	Cr ,10 ⁻⁴ cm ² / _{soc}	K, IO cm/sec	£%	Water Content, W	% 87.8			
loital	<u></u>				Degree of Saturation, S	% 96			
0.125	3.61	59.9	7.76	1.62	Solid Height of Sample, H				
0.25	23.04	9.0	1.28	3.40	Diameter of Sample 0				
0.50	21.16	9.1	1.49	7.49	Wet Unit Weight 1	1.45 9/cc			
l	42.90	3.8	0.57	14.99	Ory Unil Weight d				
2	43.56	3.1	ი.26	23.36	Uquid Limil U.				
4					Plastic Limit PL	%			
8			<u> </u>		Compression Ratio CR	0.26			
16			 		Recompression Ratio RR	0.06			
					Specific Gravity G	2.66			

		0.0				····			
CONSOLIDATION TEST RESULTS Project Model Infrastructure Project Location Bang Bo, Samut Prakan 1488									
Project 10	der Intr	ascructure	Projection	Chareon Bang Bo Provinc	raj Pumping station ,Samut Prakan	1488			
Boring Na	B-2	Sample	No. PST-9	Death	0 10 0 00	\ 88.			
0									
5	8-1 1 14 					Salational alamente de la sockettament			
10	[] []-H-1-111								
Ħ									
15 ejozjø		7	北土韓副						
20 20 20 20 20 20 20 20 20 20 20 20 20 2									
			7/	7					
5 25 등 25 - 9 . 15									
e 11									
E 11.12									
0.10									
		3 2 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3							
0.05									
0	8.1	0.2 0.3 0.5		2 3 cod Prescure	5 10 30 ,k=	50 KO			
	90%	Coal. of	Coef, of	Verlical	$\bar{\sigma}_{\text{vm}} = 0.62 \text{ ksc}$	initial Final			
Pressure	Consol.	Consolidation	' Permeability	Stroin ,		cm. 2.5			
Ksc	Time min	CY,10 ⁻⁴ cm//sec	K, IO 7 cm/sec	. ≰%	Water Content, W	% 97.2			
Iritial					Degree of Saturation, S	% 99			
0.125		-		0.41	Solid Height of Sample, Hi	0 69 cm.			
0.25	11.56	18.6	2.49	. 2.09	Oignmeter of Sample 0 Wet Unit Weight 1 1	6.35 cm.			
0.50	17.64	11.2	0.99	4.32	Well Unit Weight } 1 Dry Unit Weight } d	1.45 g/cc 0.74 g/cc			
1	67.24	2.7	0.41	23.20	Liquid Limit LL	107.4 %			
2	07.29	1.0			Plastic Limit PL	36.8 %			
8					Compression Ratio CR	n.40 ·			
)6					Procompression Parlia PR	0.055			
					Specific Granity G	2.65			

CONSOLIDATION TEST RESULTS Project Model Infrastructure Project Location Bang Bo, Samut Prakan Job No Proyince 1488 Dorth 11.00-11.80 Data 9/3/88 Sample Na. PST-11 Boring Na. σχ/₂ξ σχ. 15 0.10 0.05 Vertical Pressure, kic $\tilde{\sigma}_{\text{vin}} = 0.78 \text{ ksc}$ Final initial 90% Cocl. of - Coef, of Verlical Pressure Stroin, Consol. Consolidation ' Permeobility Height of Sample, H cm. 2.5 K, 10 7 cm/sec € % % Water Control , W Ksc Time min 102. Degree of Saturation, S Initial Solid Height of Somply, Hi 0.66 cm. 0.125 7:84 27.8 2.07 0.93 cm. Diameter of Sample 0.25 19.36 11.0 0.97 2.03 6.35 81 g/cc Maj Unit Weight 0.50 1.43 27.04 7.5 0.85 4.86 g/cc 104.04 1.7 0.22 11.27 Dry Unit Woight 0.70 % 3.7 0.27 Liquid Limit 40.96 18.44 % 2.7 0.14 44.89 28.75 Ploatic Limit 0.35 Compression Ratio CR 8 0.042 Procompression Ratio PR -16 2.65 Specific Grovity

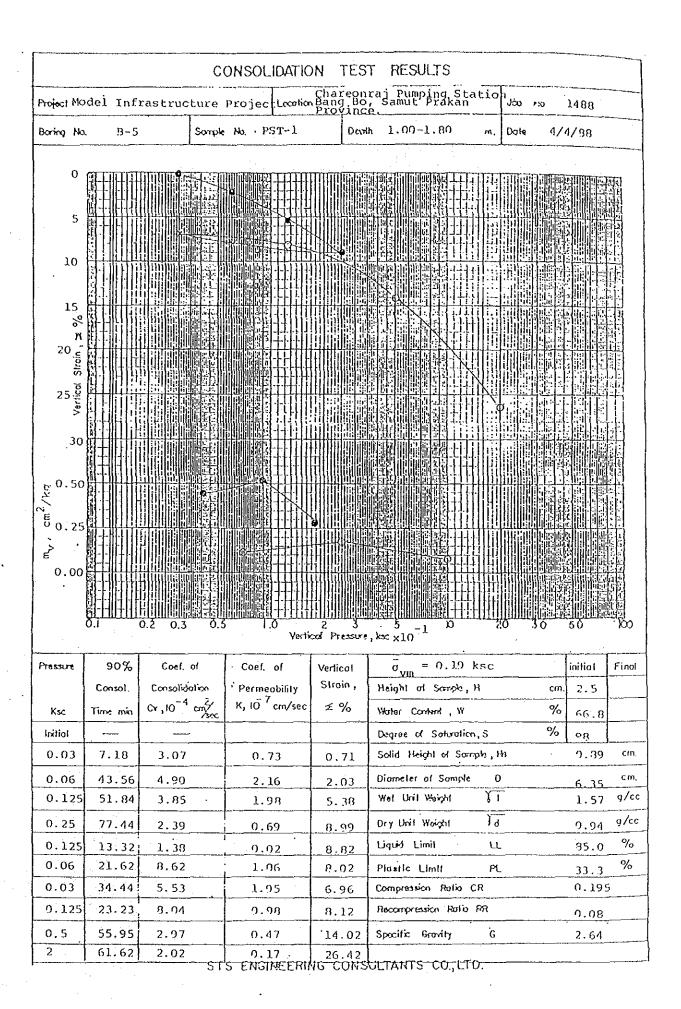
		C	ONSOLIDATIO	ON TES	OT RESULTS	•
Project "	wast It	ifrastructure	Projection to	Chareon Bang Bo	oraj Pumping stationud	1488
Boring N	a B-2	Som	k No. PST-14	- provinc	Alt: 14.00-14.80 m. Doi	
	***************************************	·			27.00 100	³ 9/3/กร
				Illiaireach	Sign in this of the contraction	ing Charles and Aller and
: _						
0						
5						
,						
10						
%			X LLEGIL			
า 15 <u></u>						
15 5						
20 jiệ						
>						
25						
א א '						
ช ระ 30						
> E						
0.10						
0.05						
0.05						
0						
_	O.1	0.2 0.3 0.3	O I.O Verti	od Presors	5 XO 20 , kas	30 50 NO
Pressure	90%	Coel. of	Coef. of	Vertical	$\bar{\sigma}_{\rm Vm}$ - 1.0 ksc	inilial Final
	Consol	Consolidation	Permeobility	Stroin ,	Height of Somple, H	cm. 2.5
Ksc	Time min	CY ,10 -4 cm2/	K, 10 7 cm/sec	<i>≲</i> %	Water Content , W	% 88.9
Initial					Degree of Saturation, S	% 97
0.125	3.61	60.7	2.77	0.57	Solid Height of Somph, Hi	0.73 cm.
0.25	17.64	12.2	0.72	1.31	Diameter of Sample D Wel Unit Weight 1	6.35 cm.
0.50 I	17.64	11.7	1.06	3.57		1.45 g/cc
2	30 60	6.4 2.7	0.51	7.52	Dry Unit Weight 1 d	0.77 9/cc 112.4 %
4	49	2.7	0.21	15.26 25.60	Plastic Limit PL	42.3 %
8				~3.00	Compression Ratio CR	0.37
ъ					Recompression Ratio RR	0.045
					Specific Gravity G	2.64

CONSOLIDATION TEST RESULTS										
Project M	Project Model Infrastructure Project Charconraj Pumping station 155 155 1488									
Boring No		1	No. PST-1	<u>Provinc</u> Dool	1	DoN 8/3/88				
•		1		l						
ر 2 سرباه در	0.1 0.2 0.3									
Pressure	90% Coef.	. of	· Coef. of	Verlical	σ̄ _{vm} ≈0.16 ksc	initio1 Final				
	Consol. Consoli	dation	Permeobility	Stroin ,	Height of Scrobe, H	cm. 2.50				
Ksc	Time min CY 10	4 cm2	K, IÕ ⁷ cm/sec	£%	Water Content, W	% 94.2				
loitial					Degrae of Saturation, S	% 197				
0.03	:			ባ ኅ1	Solid Height of Scripts, H	a 9.70 cm.				
0.06	7.34 27	.3	۴.95	ባ, 76	Diameter of Sample D					
0.125	15.0 13	.9	5.60	3.38	Wel Uril Weizin 8 1					
0.25		.2	1.92	7.24	Dry Unit Weight 13					
0.50		.7	1.23	14.05	Liquid Limil LL					
1	36.0 4	.1	0.46	19.70	Plastic Limit PL	34.4 %				
3		<u> </u>			Compression Ratio CR	0.23				
4		i			Recompression Ratio PR	0.03				
					Specific Gravity G	2.65				

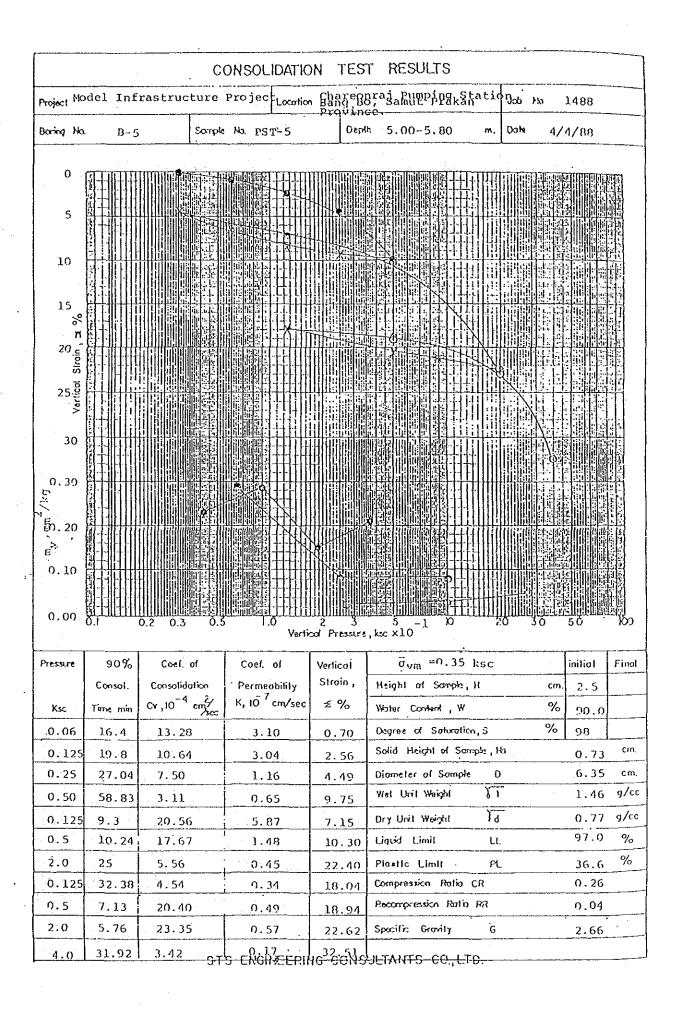
			_	÷		1			
CONSOLIDATION TEST RESULTS									
Project Model Infrastructure Project Charegorgj Pumping station									
Boring N			k No. PST-5	Provi			-		
			7 7% 751-5	Des	sh 5.00-5.80 m.	Date 8/3/88	·		
0. 5 10% n 15. 1		O.2 O.3 O.	Yerti	2 3 cod Pressure	' k≈ ×10				
Pressure	90% Consol.	Coef. of Consolidation	· Coef. of	Verlicol Stroin ,	$\sigma_{\text{vm}} = 0.3 \text{ ksc}$		inol		
Ksc	Time min	CY 10 4 cm/	Permeobility K, 10 ⁷ cm/sec	£ %	Height of Sample, H Water Content, W	% 90.3			
lailial	Tales litas	/50c	<u>.</u>		Degree of Saturation, S	% 98 .			
0.03	-	<u>-</u>		0.01	Solid Height of Sample, He		cm.		
0.06				0,03	Diameter of Sample D		cm.		
0.125	10.24	20.6	7.70	2.46	West Unit Weight \$1		g/cc		
0.25	23.04	8,7	1.54	4.67	Dry Unil Weight 18		/cc		
0.50	33.44	4.7	1.09	10,46	Liquid Limit LL		%		
1	34.81	4.4	0.74	18.83	Plastic Limit PL		%		
2	38.44	3.3	0.19	24.79	Compression Ratio CR	0.28			
4					Recompression Halin RR	0.06			
6					Specific Gravity G	2.65			

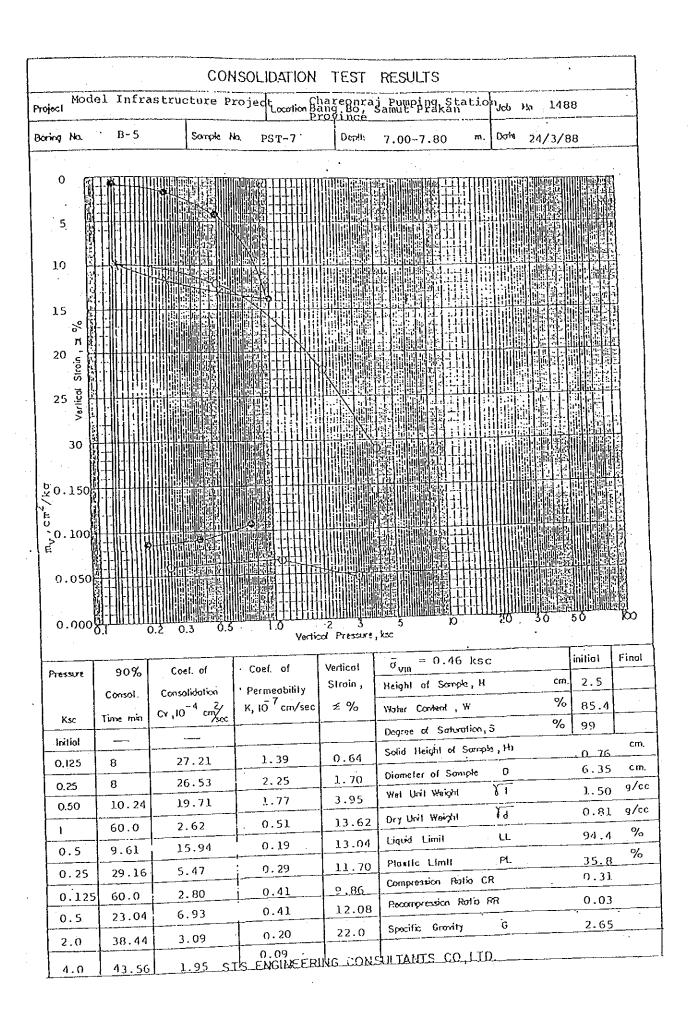
CONSOLIDATION TEST RESULTS										
Project Model Infrastructure Projectomic Bang Bo Samut Prakan										
Boring Na	. в-3	Sample	No. PST-9	Debyl Droxiuc	,)	appl 8/3/88				
0 5 10 15 % 7 10 10 10 10 10 10 10 10 10 10 10 10 10		Sample Sample Control of the Control				3/3/88				
Pressure	90%	Coef. of	· Coef. of	Verlical	n _{vm} = 0.6 ksc	initial	Finol			
ļ	Consat.	Consolidation	Permaobilily K, 10 ⁷ cm/sec	Stroin,	Height of Sorph, H	cm. 2.50				
Ksc	Time min	CY,10 ⁻⁴ cm//sec	K, IU cm/sec	<i>≴</i> %	Water Cantent, W	% 23.4				
loitial					Degree of Saturation, 5	% nn				
0.06				0.12	Solid Height of Sample, Hi	0.67	cm.			
0.125	4.84	44.7	6.95	1.13	Diometer of Somple D	6.35	cm			
0.25	6.76	31.5	2.34	2.06	Well Unit Wright 81	1.44	g/c			
0.50	13.69	15.0	1.14	3.96	Dry Unil Weight 18	0.73	g/c			
1	51.34	3.4	0.55	1217	Uquid Limil LL	109.7	%			
Ź	39.69	-3:7	0.33	21.กร	Plastic Limit PL	38.2	%			
2	34.31	3.3	0.19	31.25	Compression Ratio CR	0 34				
8					Recompression Ratio RR	ი .036				
					Specific Growiny G	2.70				
			. 1	0 - 66	,					

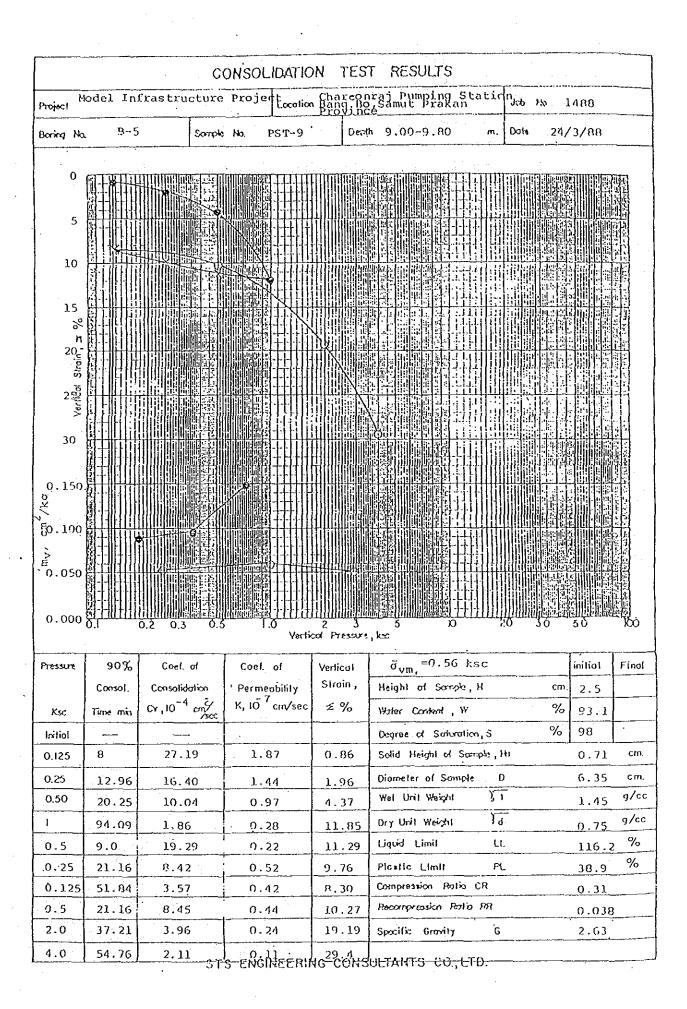
		·	· · · · · · · · · · · · · · · · · · ·			
			4SOLIDATION			
rojoci Mod	el Infrastr	ucture Pr	cojec Location	Chareonr Bang Bo Province	aj Pumping stationa	1488
Joring Ha	B-3	Sample 1		Death	13.0-13.8 m. Da	
			· · · · · · · · · · · · · · · · · · ·			:
0 15% x, mo, m 15 10 15% x, mo, m 15 10 15 10 15 10 15						
0	0.1 0.2	0.3 0.5	1.0 Vertic	2 3 cd Pressure	$\frac{5}{10^{-1}}$ $\frac{1}{100}$ $\frac{1}{100}$,
Pressure Ksc	Consol. Con	oct. of solidation 0 ⁻⁴ cm ² /sec	Coef. of ' Permeabilily K, 10 ⁻⁷ cm/sec	Verlical Strain , ≤ %	$\sigma_{\rm VM}$ =0.85 ksc Height of Somple, H Water Control , W	initial Final cm. 2.5 % 92.3
Irilial					Degree of Surjustion, 5	% 97 cm.
0.06	-			0.016	Solid Height of Scrapts, H	
0.125	7.29 .	29.7	3.95	0.88	Diameter of Sample D	
0.25	17.64	12.0	0.78	1.69		1.49
0.50	26.01	7.8	0.48	3 - 22		
1	33.06	5.6	0.43	7.08		0/-
2	75.69	1.9	0.19	17.43	Plastic Limit PL	0.35
ı	68.89	1.4	0.007	27.13	Compression Ratio CR	
8			:		Focompression Partin PR	0,025
			ļ	1	Specific Generalty G	2.65

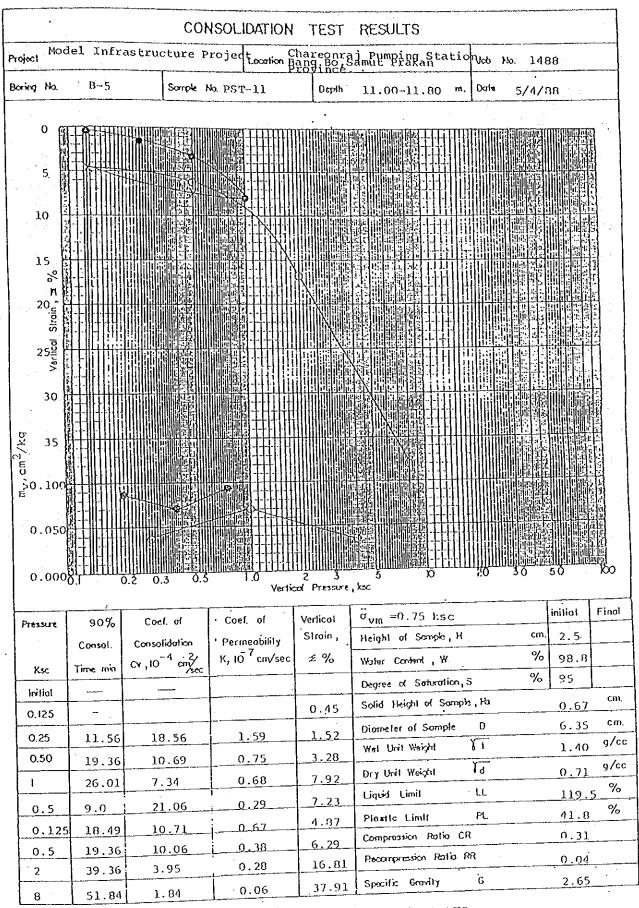


		CON	SOLIDATION	TEST	RESULTS			
rojeciMode.	l Infras	tructure Pro	oject Locolion Ba	areonraj	Pumping Statio mut Prakan	Job Ho	1488	
Boring Na.	R-5		b. PST-3	Derdh	3,00~3,80 m.	and the second second	3/98	
		<u>l:</u>	· · · · · · · · · · · · · · · · · · ·			 		
0 5 10 15 % Trivial Strain Str								<u> </u>
0.00		.2 0.3 0.5		2 3 d Pressue,	5 -1 ×0	20 30 30	50	- Roo
			Yertyo	~ (1630);			initiol	Final
Pressure	90%	Coel. of	Coef. of	Verlical	σ _{vm} = 0.21 ks		cm. 2.5	
	Consol.	Consolidation	Permeobility	Stroin,	Height of Sample, H		% 93.0	
Ksc	Time min	Cr,10 ⁻⁴ cm/xcc	K, IÓ ⁷ cm√sec	£%	Water Content, W		% 97	
0.06	8	27.22	6.99	9.79	Degree of Saturation,		0.67	Cm.
0.125	25	8.30	3.22	3.31		0	6.35	C m
0.25	46.74	4.19	1.18	6.83	Diameter of Sample Well Unit Weight	81	1.44	g/c
0.50	55.95	3.03	0.79	_13.31_		Yd	0.75	g/c
0.125		7.68	3.74	10.72	Dry Unil Weight		95.5	
0.123	23.81	6.39	9.66	14.32	Liquid Limit	LL		0/.
L.,	32.04	3.92	0.30	25, 81	Plastic Limit	PL	36.2 0.97	
3.0				22.35	Compression Ratio Cl	R 		
2.0	·	127,42	1.19				~	
0.125	4.84	,27,42		22.92	Recompression Ratio F	तर 	0.23	
	·	23.89	0.33		Recompression Ratio F Specific Gravity	[.] G	2.65	

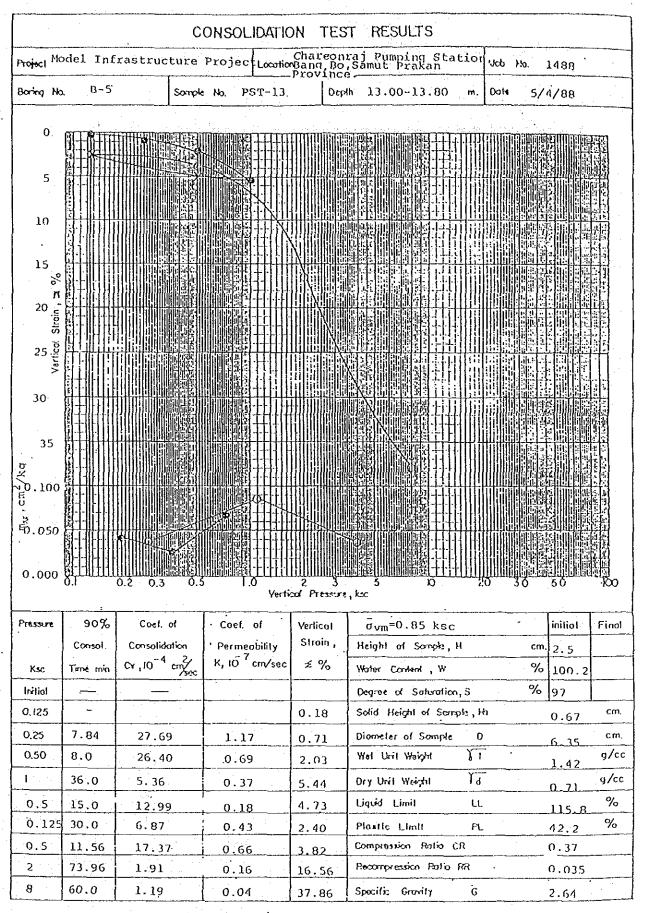




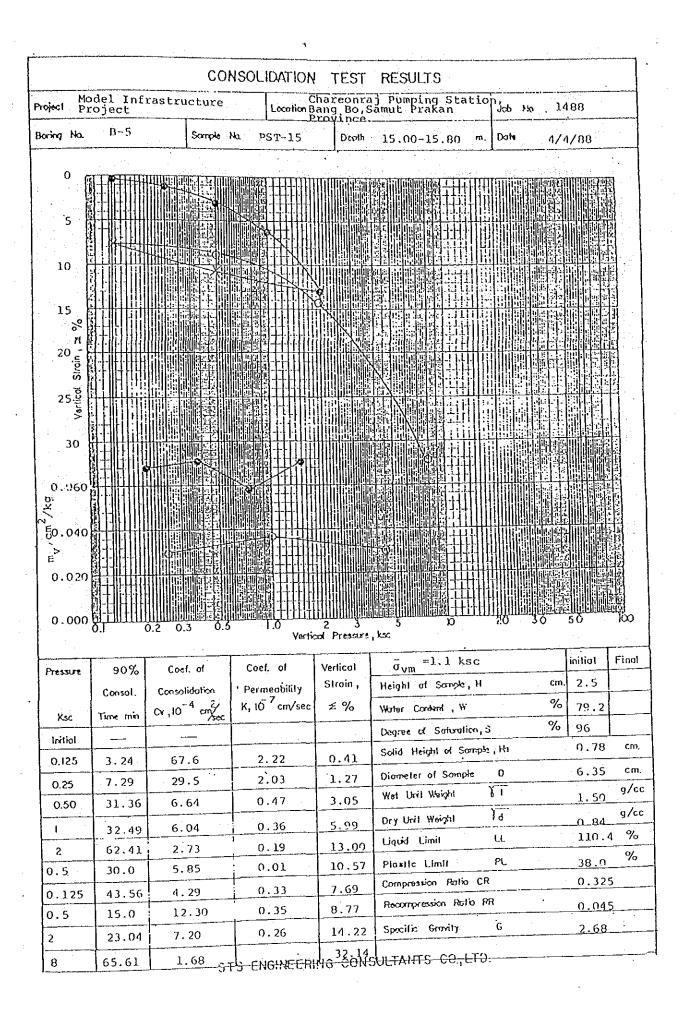


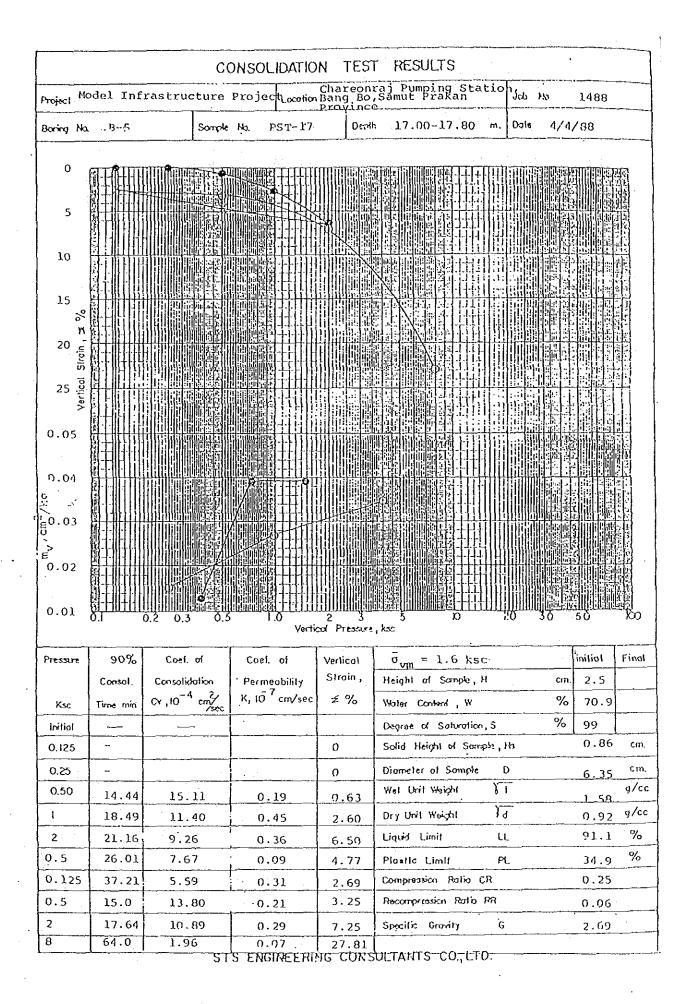


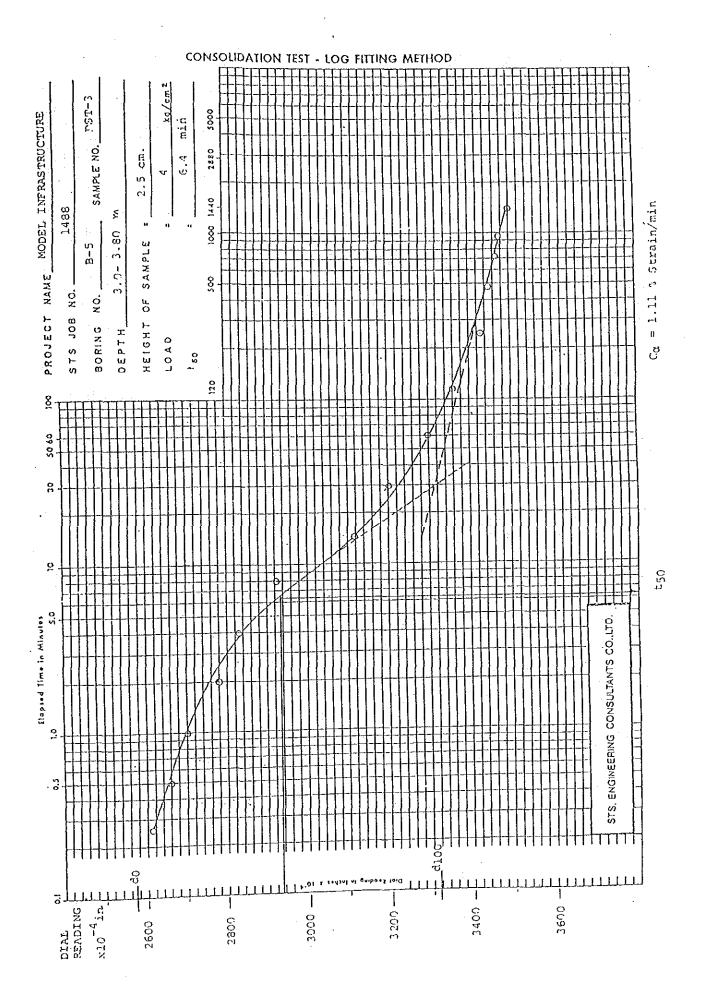
STS ENGINEERING CONSULTANTS CO., LTD.

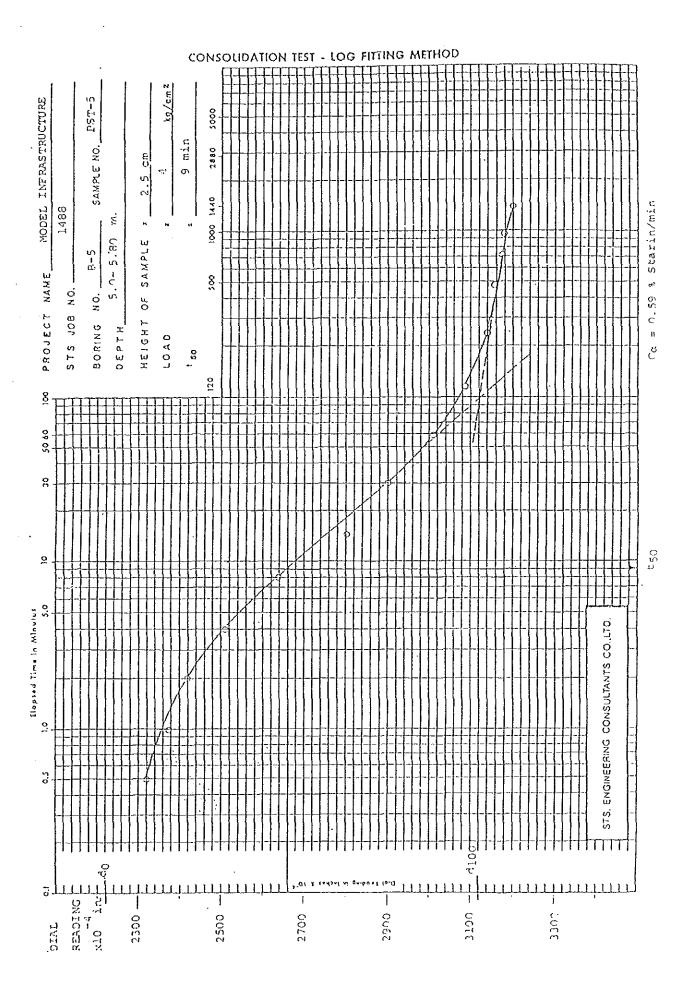


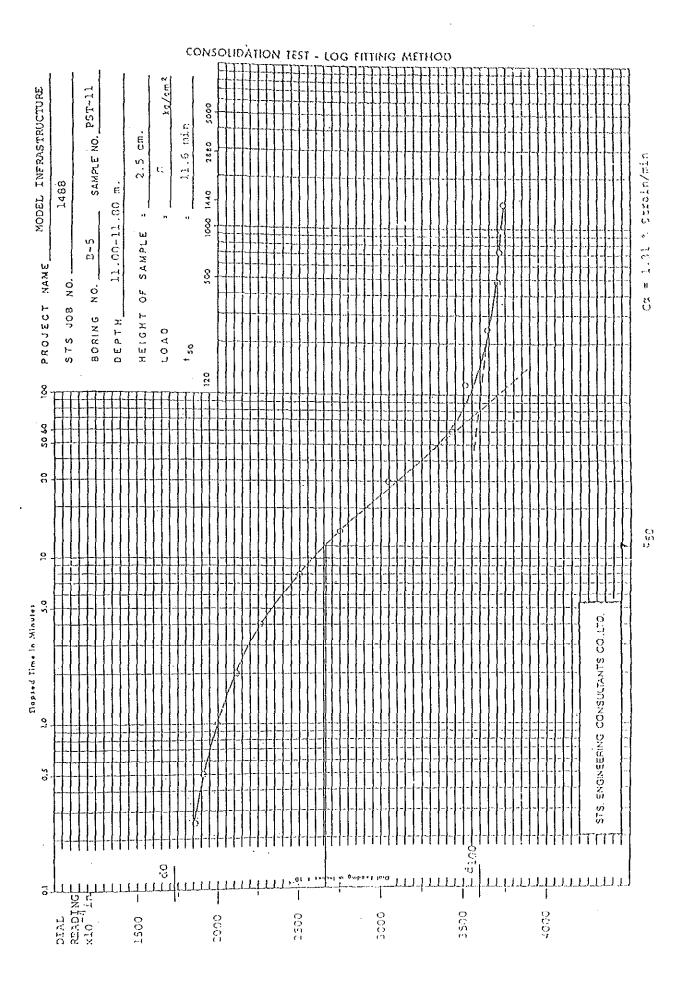
STS ENGINEERING CONSULTANTS CO., LTD.

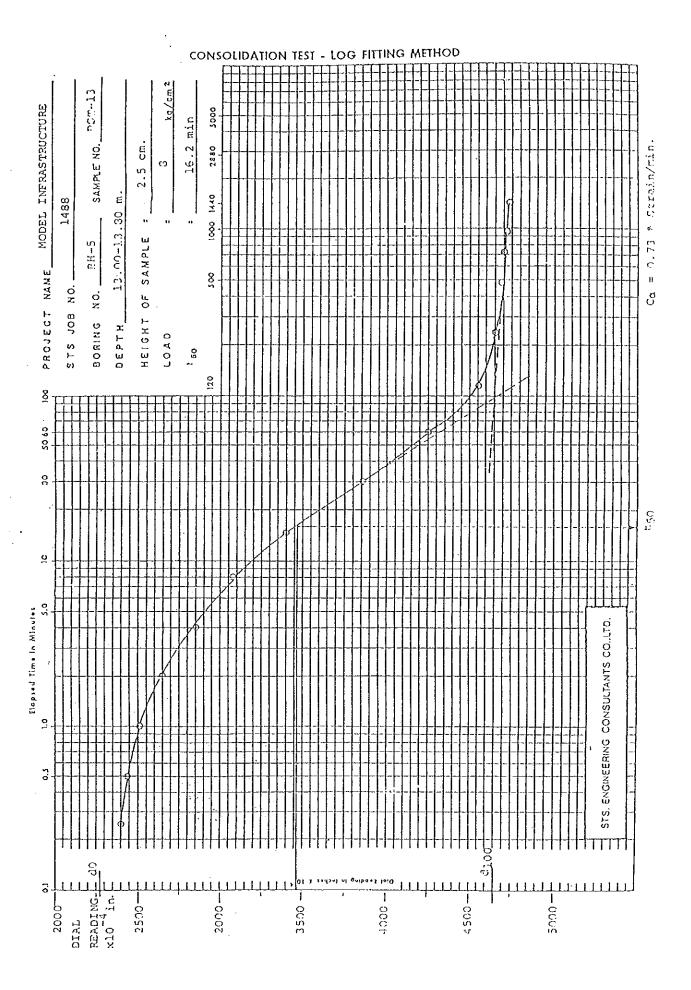


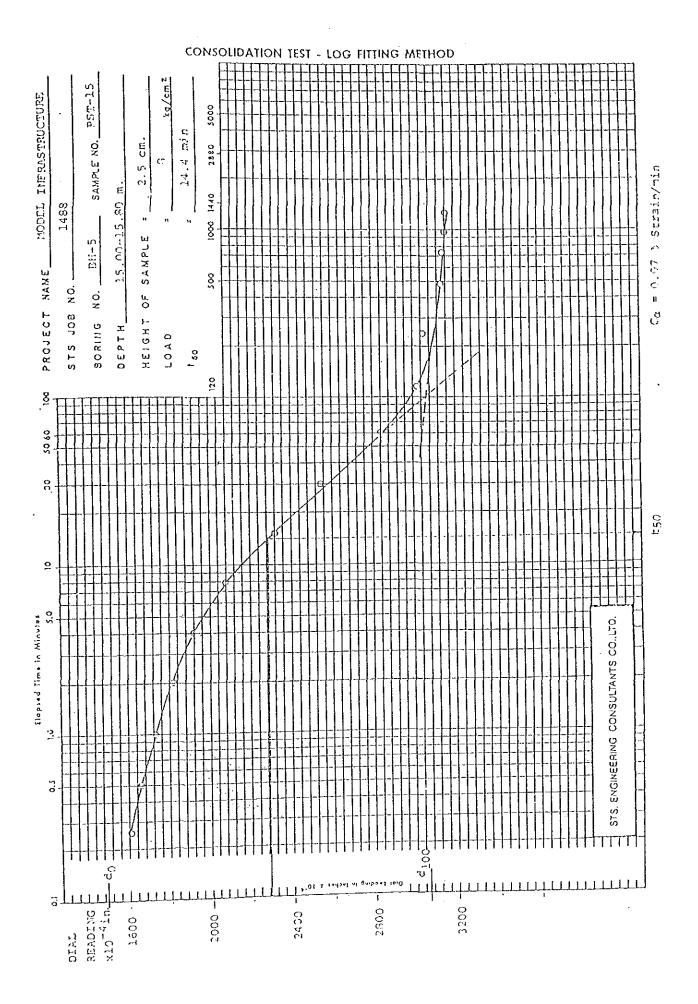


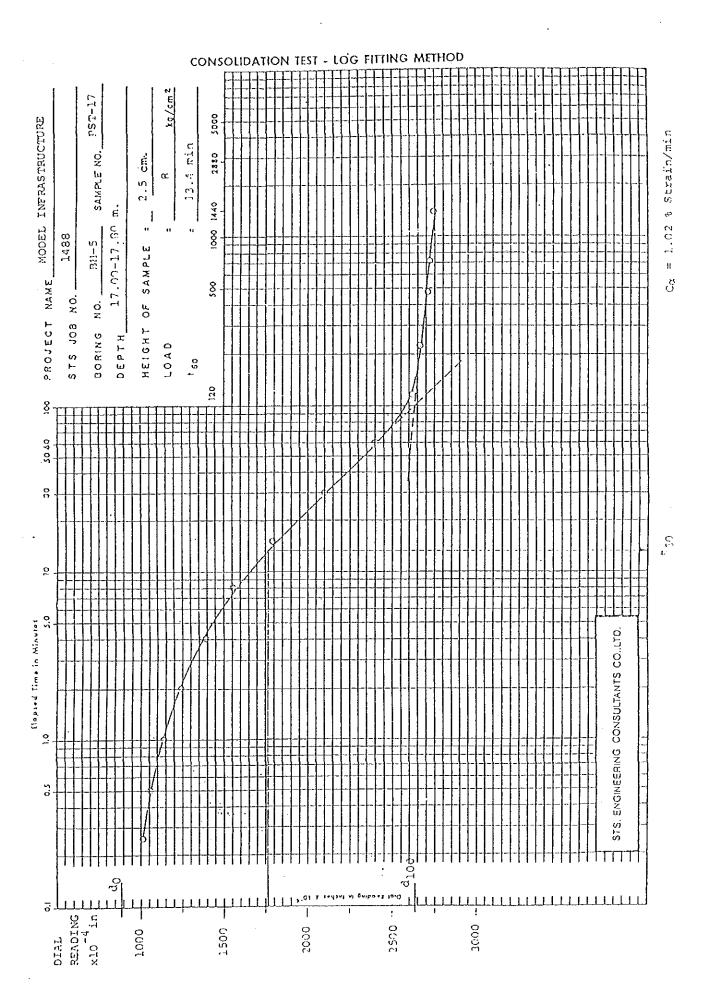












D

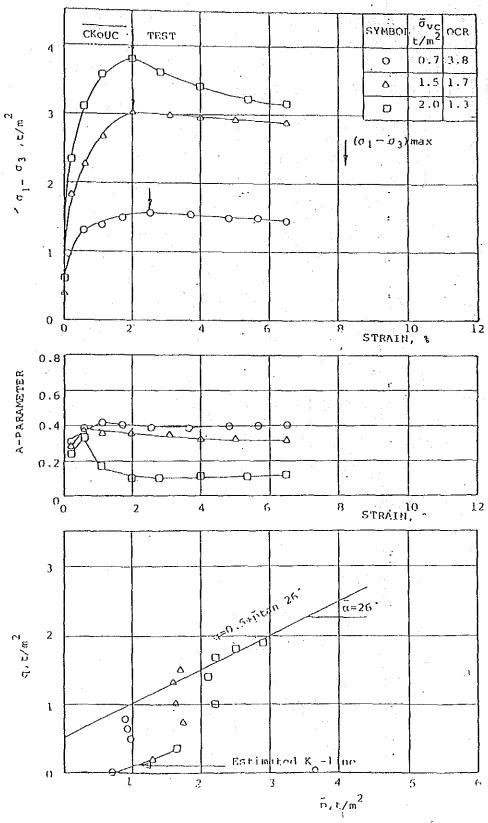
ANISOTROPICALLY CONSOLIDATED UNCRAINED TRIAXIAL

COMPRESSION TEST RESULTS

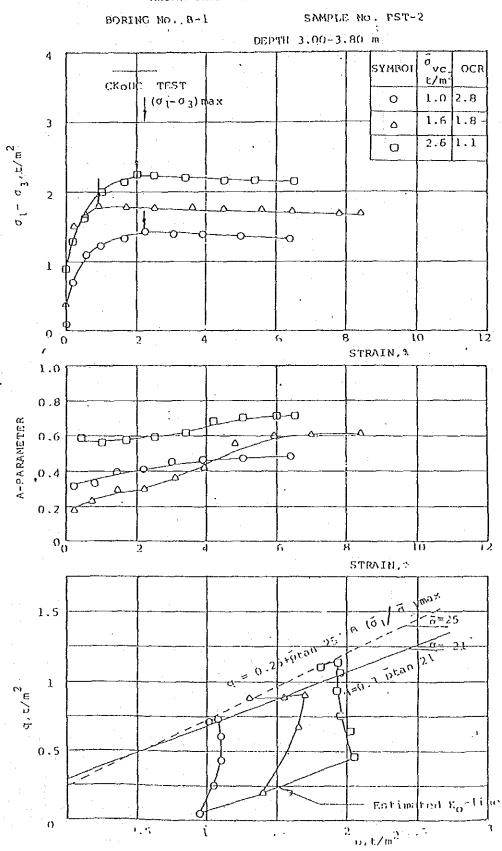
BORING No. 8-1

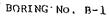
SAMPLE No. PST-1

DEPTH 1.00-1.80 m.

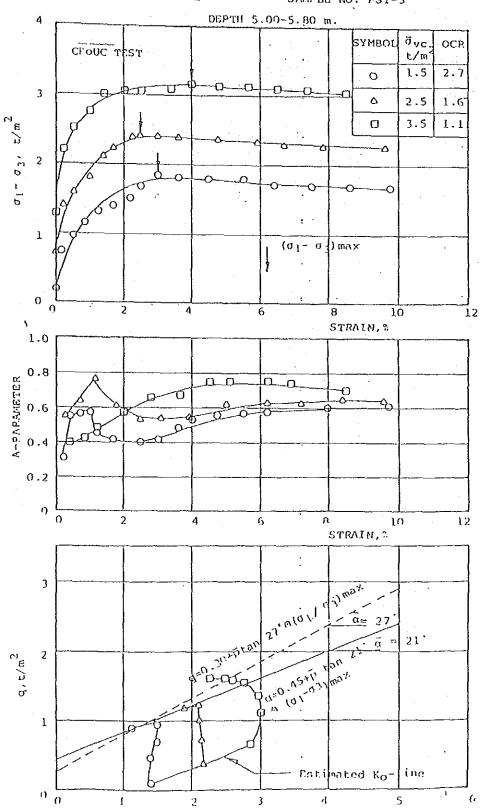


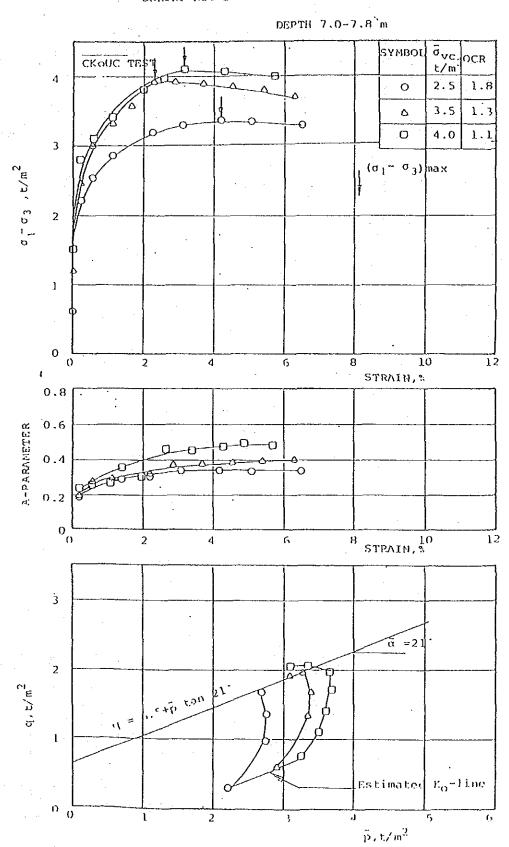
MODEL INFRASTRUCTURG PROJECT



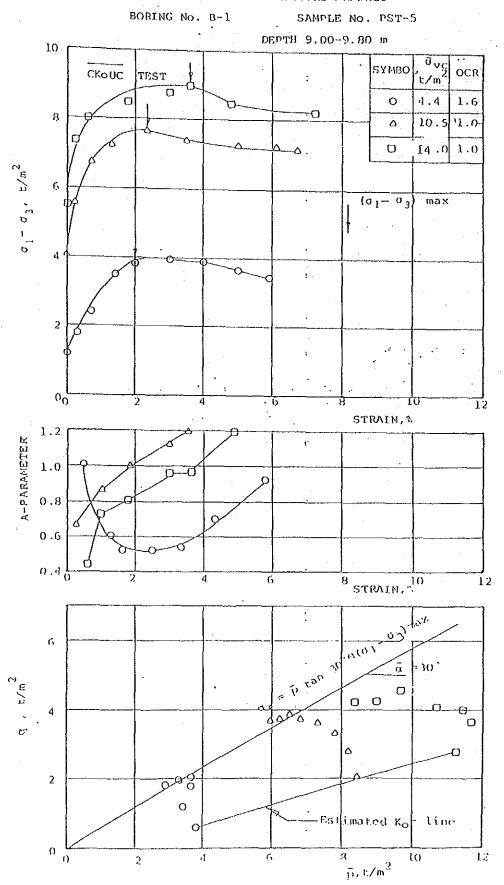


SAMPLE No. PST-3

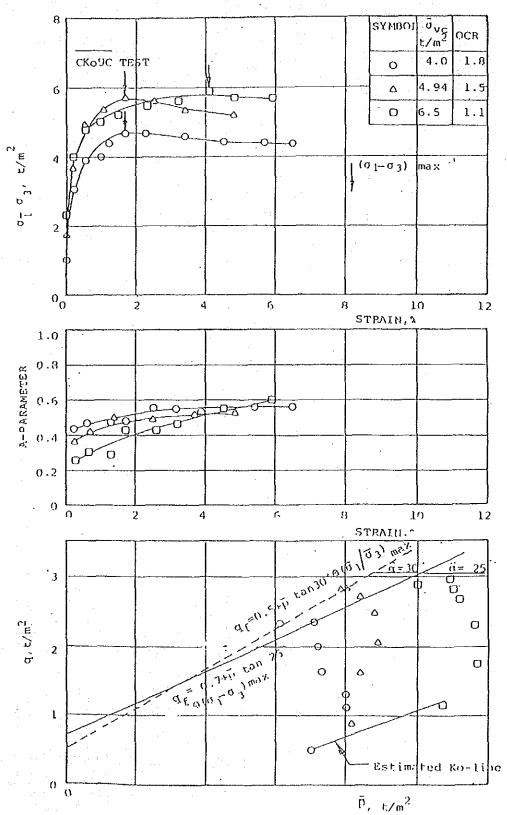




MODEL INFRASTRUCTURE PROJECT



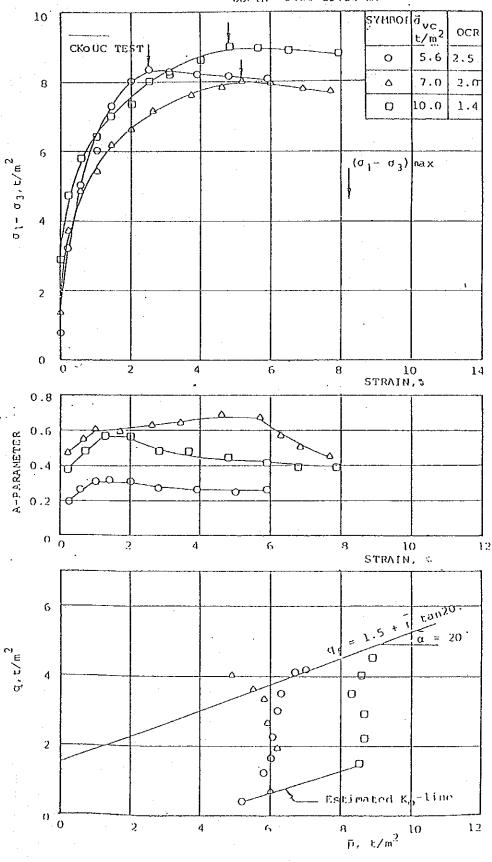
DEPTH 11.00-11.80 m.



MODEL INFRASTRUCTURE PROJECT BORING No. B-1 SAMPLE No. PST-7
DEPTH 13.20-14.00 m. Jol SYMBOI. $\tilde{\sigma}_{VC}$ OCR CKOUC TEST 4.68 1.9 0 6.3 1.5-۵ O 9.95 1.0 (01-03) o_{c}^{0} 10 12 STRAIN, % 1.0 A PARAMETER 9.0 8:0 0.2 10 STRAIN, 2 for ACE ß 30. 4 \Box 0 ٠ ۵ 0 2 0.9 Estimated K - Line $0 \frac{1}{0}$ 12 6 Я 10 2

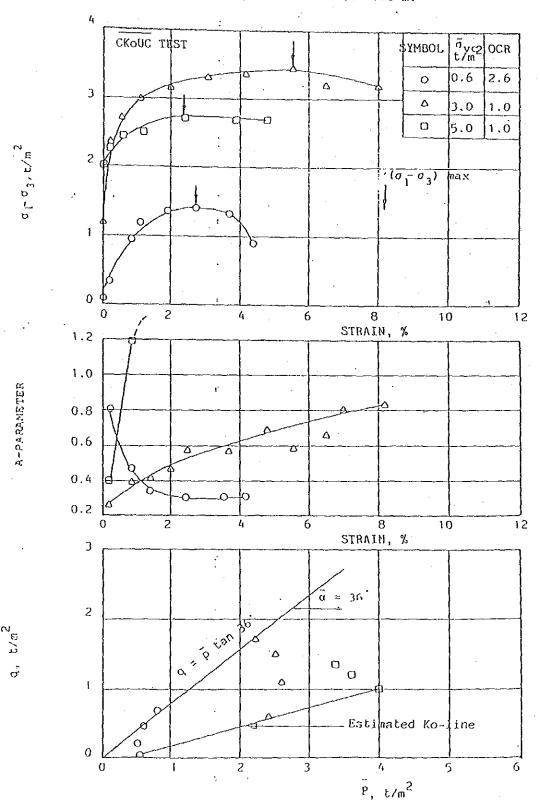
 $\bar{\tilde{\mathbf{p}}},~\mathrm{t/m}^2$

BORING No. B-1 SAM: LE No. PST-8
DEPTH 15.00-15.80 m.



MODEL INFRASTRUCTURE PROJECT BORING NO.B-3 SAMPLE NO.PST-1

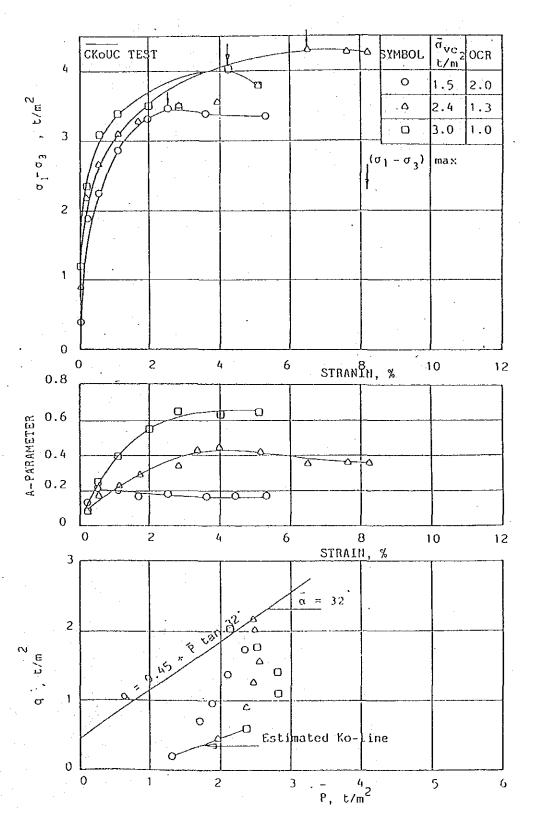
DEPTH 1.00-1.80 m.



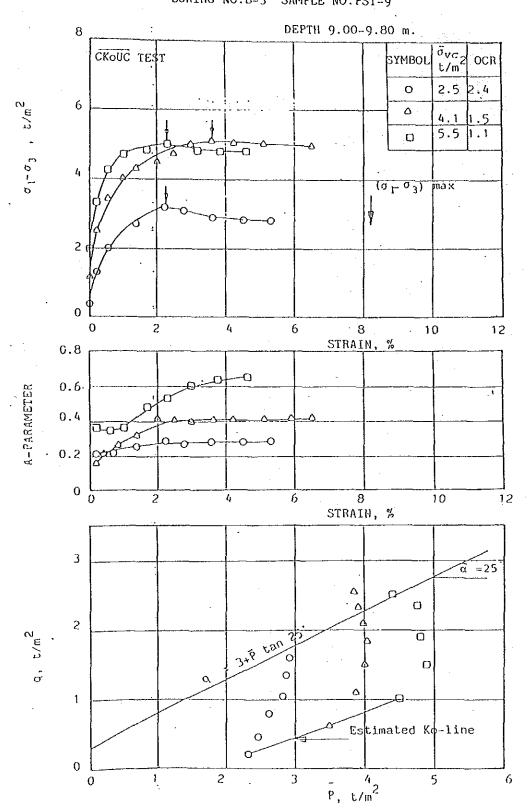
MODEL INFRASTRUCTURE PROJECT

BORING NO.B-3 SAMPLE NO.PST-5

DEPTH 5.00-5.80 m.



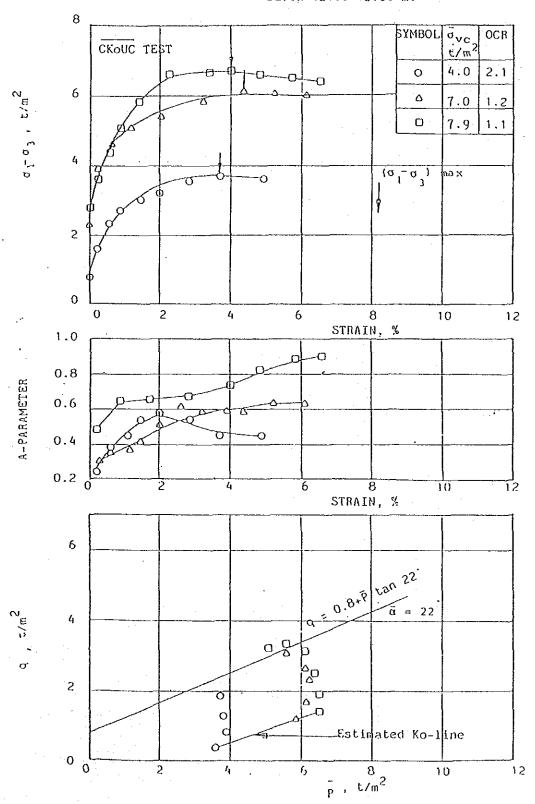
MODEL INFRASTRUCTURE PROJECT BORING NO.B-3 SAMPLE NO.PST-9



MODEL INFRASTRUCTURE PROJECT

BORING NO.B-3 SAMPLE NO.PST-13

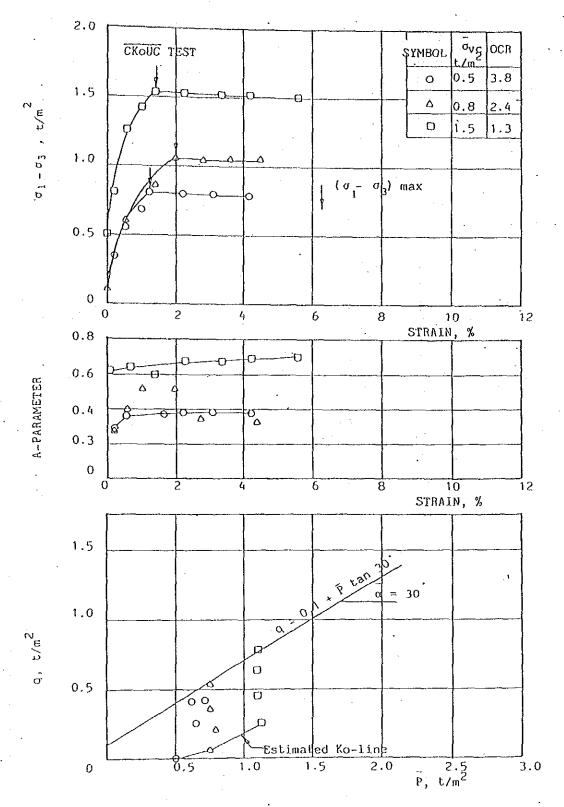
DEPTH 13.00-13.80 m.



MODEL INFRASTRUCTURE PROJECT .

BORING NO. B-5 SAMPLE NO.PST-1

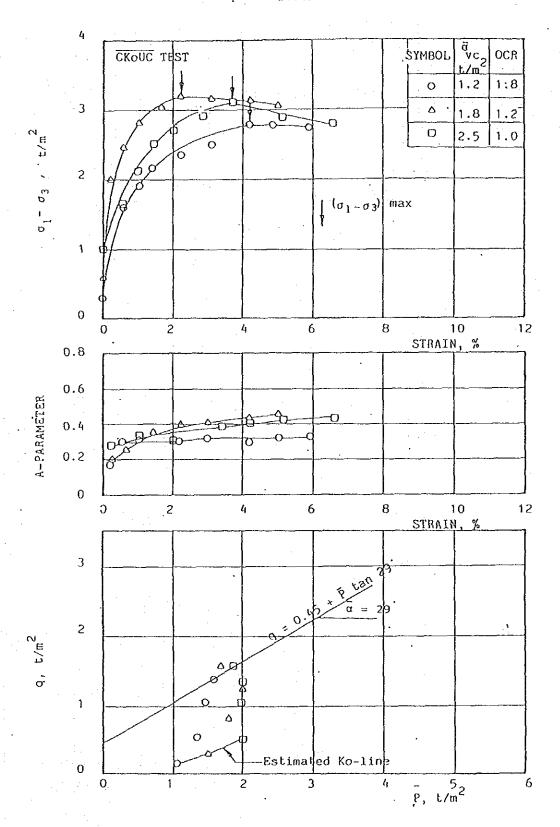
DEPTH 1.00-1.40 m.



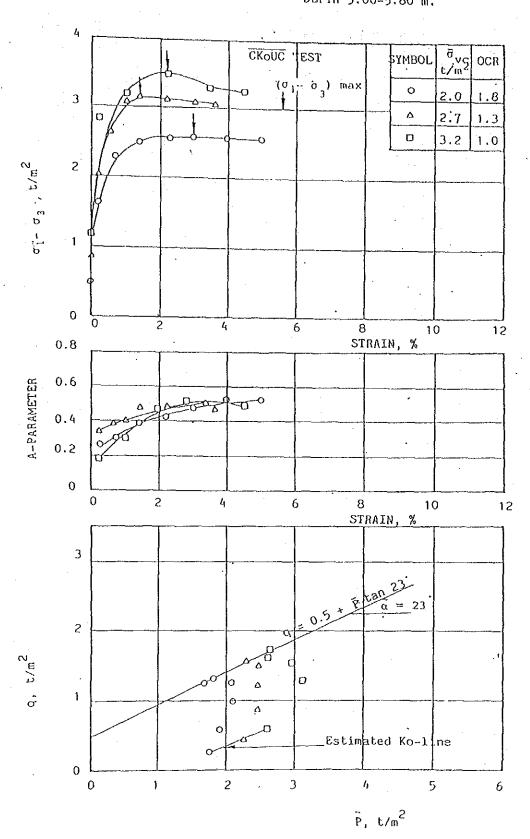
MODEL INFRASTRUCTURE PROJECT

BORING NO. B-5 SAMPLE NO. PST-3

DEPTH 3.00-3.80 m.

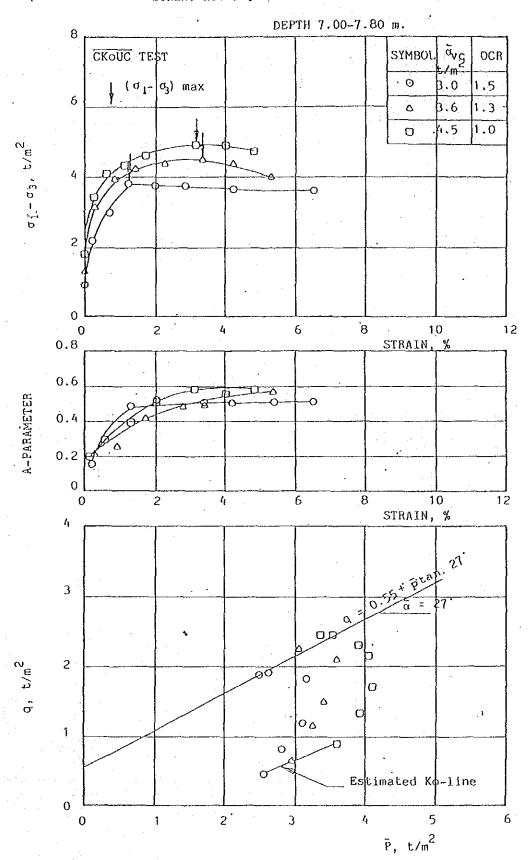


MODEL INFRASTRUCTURE PROJECT BORING NO. B-5 SAMPLE NO. PST-5 DEPTH 5.00-5.80 m.



MODEL INFRASTRUCTURE PROJECT

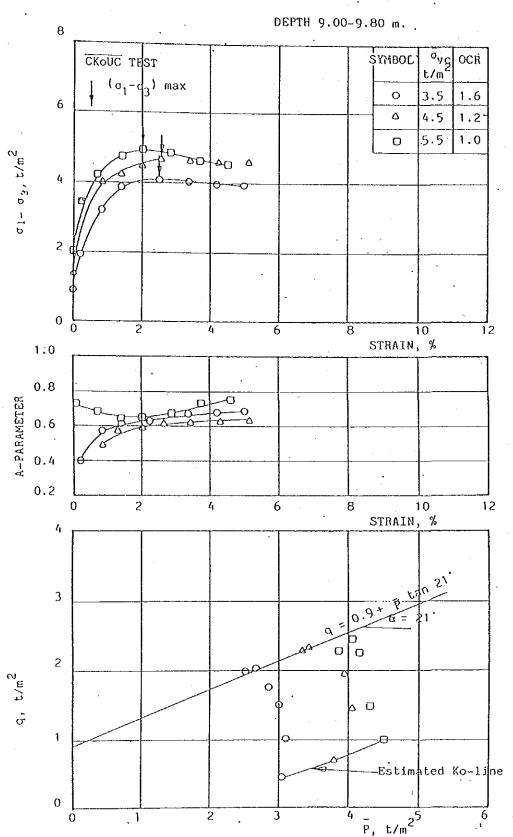
BORING NO. B-5 SAMPLE NO. PST-7



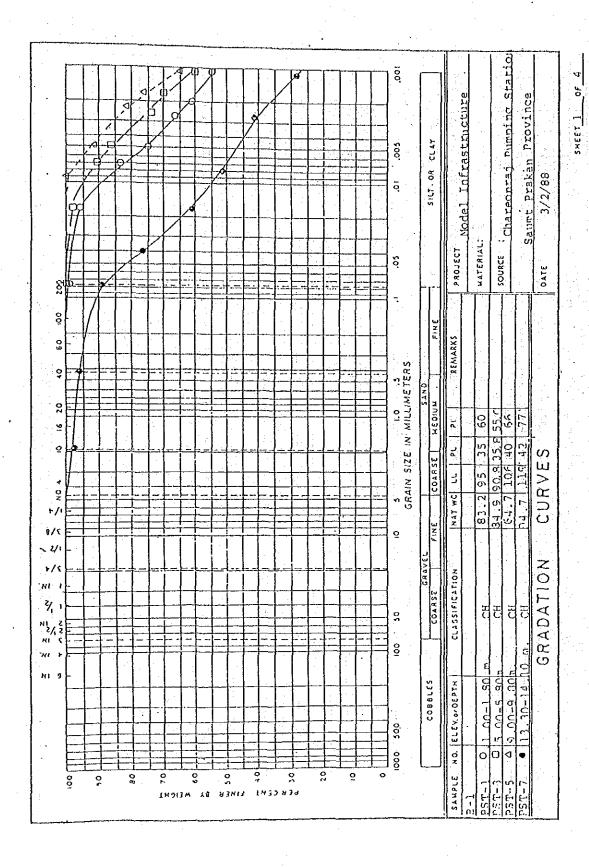
MODEL INFRASTRUCTURE PROJECT

BORING NO. B-5

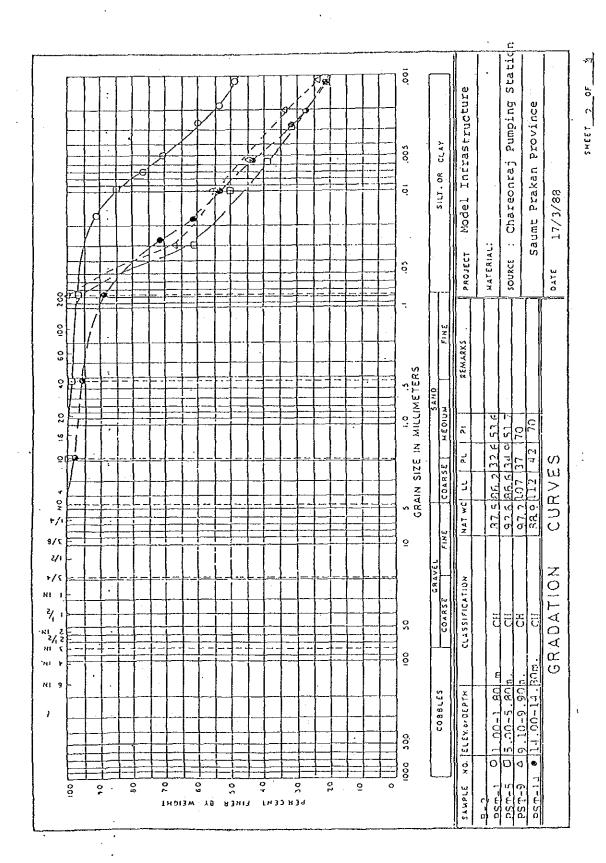
SAMPLE NO. PST-9



GRADATION CURVES RESULTS

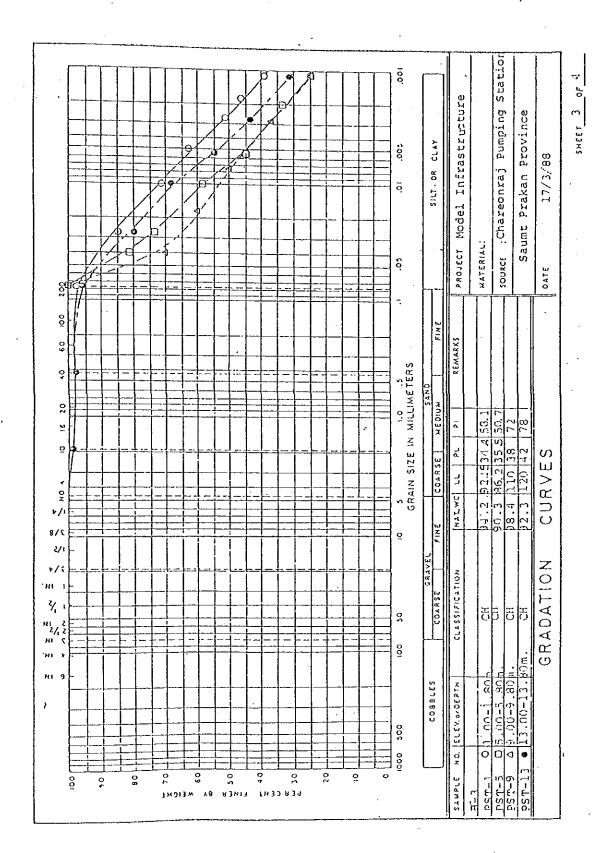


STS ENGINEERING CONSULTANTS CO., LTD.

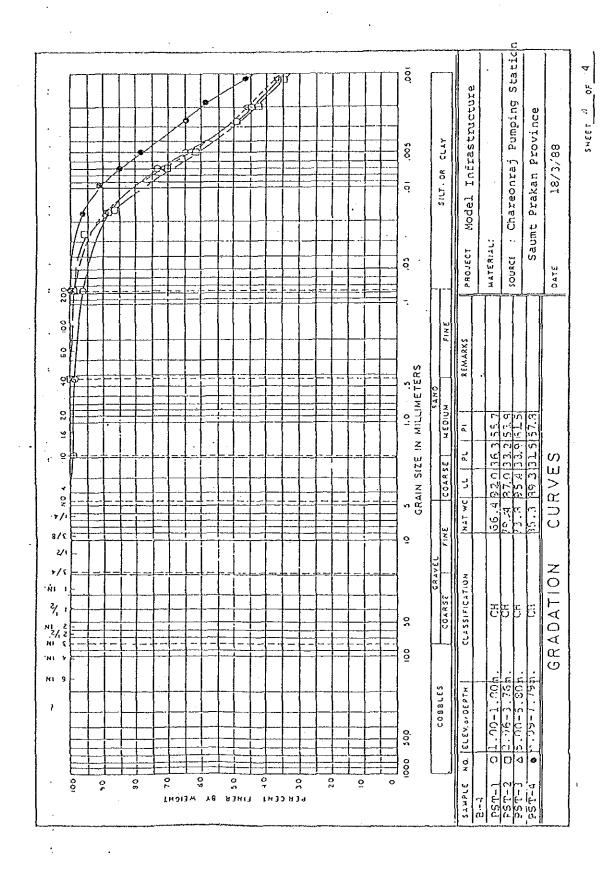


-

STS ENGINEERING CONSULTANTS CO., LTD.

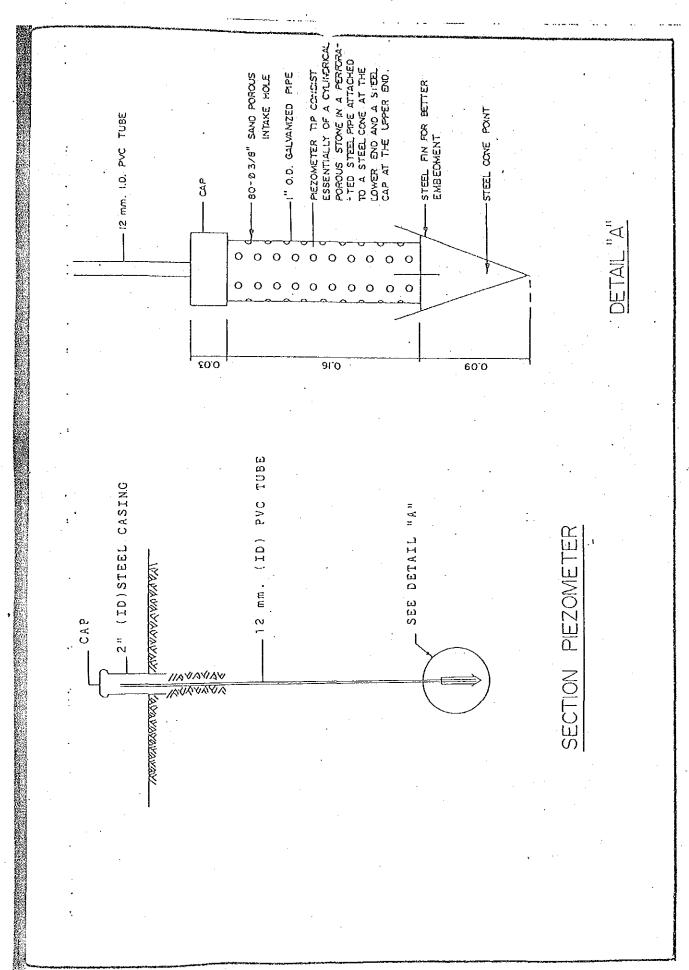


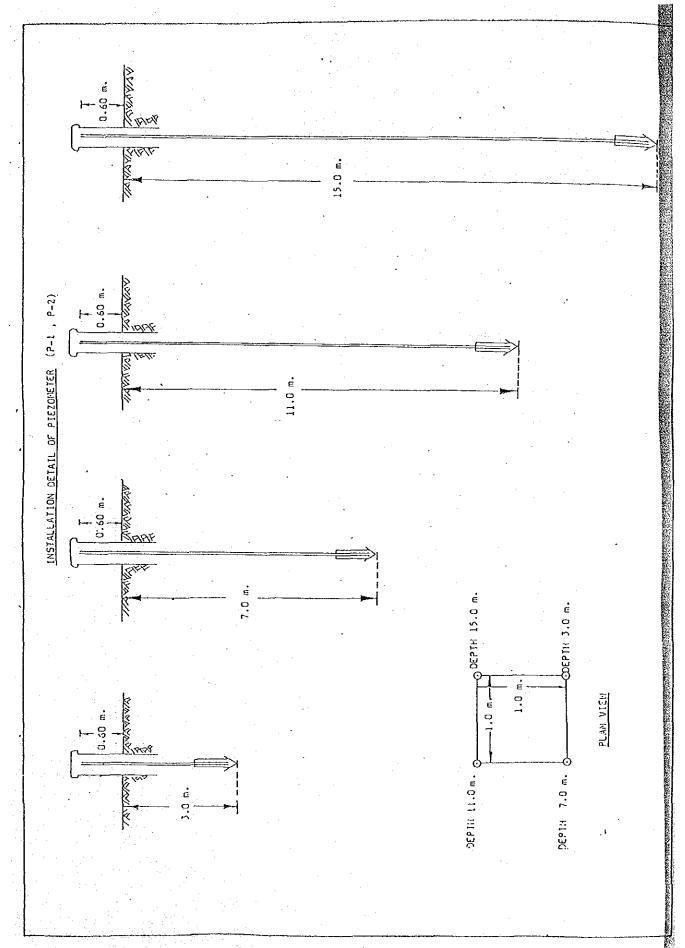
STS ENGINEERING CONSULTANTS CO., LTD.



STS ENGINEERING CONSULTANTS CO., LTD.

TYPICAL OF PIEZOMETER INSTALLATION & RECORDS





		PIEZOM	OMETRIC LEVEL RECORD	ECORD	PROJECT: MODEL INF	MODEL INFRASTRUCTURE
		STATION CHAREONRAJ	PUMPING DATE OF INSTALLATION	572/88 5/2/88		
Dole	P1/1 (TIP -3.0 M)	M) P1/2 TIP -7.0 M.)	Plystre -11.0 M.)	P1/4(TIP -15.0 M.)		Ramark
/2/88	0.35	0.095	0.18	0.80		Piezometer
5/2/88	0.52	0.39	0.472	2.58		level is
7/2/88	0.57	0.43	0:50	2.62		below the
/3/88	0.51	0.40	0.49	2.64		top of PVC
/3/85	0.52	0.35	0.51	2.70		tube
3/3/88	0.51	0.34	0.51	2.71		
1/3/88	0.525	0.32	0.51	2.72		
2/3/88	0,525	0.315	0.515	2.73		
!						
:						
!						
						-

		,					 T	· •	····	· 	 	' 	 		<u> </u>	1
ASTRUCTURE		Remark	Piezometer	level is	below the	top of PVC .	tube		•			•				
PROJECT: MODEL INFRASTRUCTURE																
RECORD	ALLATION 5/2/88	P2/4(TIP -15.0 M.)	0.66	2.15	2.20	2.25	2.29	2.30	2.30	2.32	:				-	
ZOMETRIC LEVEL RE (m)	PUMPING DATE OF INSTALLATION	P2/3 [TIP -11.0 M.)	0.21	0.626	0.636	0.635	0.66	0.64	0.66	0.67						
PIEZO	STATION CHAREONRAJ PI	P2/2TIP -7.0 M.)	0.15	0.382	0.384	0.38	07.0	0.395	0.385	0.39						
		-3.0 M)	0.66	0.78	0.79	0.785	•	0.775	0.615	0.465						
		Dats	5/2/88	26/2/88	27/2/88	1/3/88	3/3/88	88/6/0	0 1/3/88	2/3/88						

CHEMICAL TEST & X-RAY DIFFRACTION TEST RESULTS

CHEMICAL TEST RESULTS

Project

Model Infrastructure

Location

Chareonraj Pumping Station, Bang Bo, Samut

Prakan Province.

Boring	Sample	Depth,m	pil	Salinity:	ci_	So ₄	о.м.	Remark
No.	No.			ppt	pom	mag	9,	
B-1	PST-1	1.00-1.80	6.7	26	14576	400	4.0	
	PST-3	5.00-5.80		21	11162	268	4.8 2.9	
	PST-5	9.00-9.80	7.8	16	9291	345	3.5	in the
	PST-7 []	3.30-14.1	7.9	14	7616	365	3.6	ponded
•				• '				area
		-					 	
B-2	PST-l	1.00-1.80	7.6	23 '	11080	91	3.8	
•	PST-5	5.00-5.80	7.4	22	13181	31	2.9	
	PST-9	9.10-9.90	7.1	12 .	9438	38	3.2	on land
	PST-14	14.00-14.8	8.3	14	7731.	90 .	3.7	
						·		

4. Basic Plan

BASIC PLAN

 $0 F \cdot$

DETAILED DESIGN

 \mathtt{OF} .

MODEL INFRASTRUCTURE PROJECT

FEBRUARY 24th, 1988

I. OBJECTIVES OF THE MODEL INFRASTRUCTURE PROJECT

The objectives of the Model Infrastructure Project throughout the execution of the detailed design, construction and monitoring are as follows;

- Setting up the monitoring system for mechanical behaviour of the excavated soft soil foundation.
- 2) Obtaining the mechanical behaviour of the excavated soft soil foundation.
- Examining the applicability of the method of slope stability analysis using circular slip surface for the excavated soft soil foundation.
- 4) Studying the applicability of prediction for the stress and deformation occurring in the excavated soft soil foundation by the Finite Element Method (F.E.M.) using an Elasto-viscoplastic model.
- 5) Suggestions and recommendations on the design and investigation for the soft soil foundation.

II. SCOPE OF WORKS FOR DETAILED DESIGN

In order to achieve the objectives mentioned above, the detailed design of the testing canal facility and its monitoring system are conducted on the basis of the following basic viewpoints.

1. Project site

The Model Infrastructure Project for soft soil foundation will be carried out in the area neighbouring the Charoenraj Pumping Station. The site of the Model Infrastructure project has been provided by RID.

- 2. Basic Plan for the Testing Canal Facility
 The testing canal facility consists of four slopes which take
 into consideration the project site condition. Since the main
 purpose of this project is to obtain the behaviour of the soft
 soil foundation caused by excavation work, surcharge load will
 not be carried out in principle.
- 3. Untreated Slope Structures

Two slope sections are planned to be constructed to leave them in the form of an untreated natural state. One of the non-treatment slope structures is to be applied for the study of long-term stability. The other non-treatment slope structure is to be used for the study of short-term stability.

4. Improved Slope Structures

The improved slope structures will be undertaken for the following purposes:

- Countermeasures against damage and failure of the existing structures, and preparation work.
- 2) Study of the effects of improved methods in the improved slope structures.

As examples of countermeasures among the various available improvement methods for the soft soil foundation, the final improvement methods will be selected from three already proposed methods (sand compaction pile treatment, soil cement column treatment, and gravel compaction pile treatment)

5. Monitoring System

The monitoring system will be utilized in the following way;

- 1) Auto-measurement monitoring system
- 2) Measurement and observation by topo-survey work.

The auto-measurement monitoring system will be installed at the project site. Also, the observation data obtained from the auto-measurement monitoring system will be recorded at the project site. The data obtained from the monitoring system will be analyzed in

the I.E.C.. Efforts should be made to ensure that the monitoring instruments will be installed before the start of the excavation work.

6. Others

The construction work of the testing canal facility will be conducted using Model Infrastructure Improvement Work funds. The hardware and software for the auto-measurement monitoring system are to be purchased using IEC project funds. The budget for the monitoring system will be decided by the JICA taking into account the limitations of IEC project funds.

III. IMPLEMENTATION PROCESS OF DETAILED DESIGN

The implementation process of the detailed design shown in Fig-1 is as follows:

1. Investigation

I.l Geotechnical Investigation

In order to obtain as much accurate data as possible, the following geotechnical investigation will be performed.

- 1) In-situ Tests
 - a. Field Vane Tests
 - b. Boring and Sampling
- 2) Laboratory Tests
 - a. Standard triaxial compression tests for clay samples obtained from the project area.
 - b. Unconfined compression tests for clay samples obtained from the project area.
 - c. Physical property tests for materials of the sand compaction piles and the gravel compaction piles.

1.2 Topo-survey Work

Additional topo-survey work for the area surrounding the Project site will be made.

2. Preliminary Analysis

The preliminary analysis for the detailed design work will be performed by the circular slip method using the computer system in the IEC.

The preliminary analysis conditions are as follows;

- 1) The depths of the testing canal facility are 4m and 3m.
- 2) The preliminary analysis are conducted on the basis of the trial and error method using the several different slope gradients of the testing canal facility.

3. Preliminary Design

The depth and slope gradients of the testing canal facility will be decided from the results of the preliminary analysis. A value of a little less than 1.0 for the safety factor will be adopted as the safety factor for the slope applied for the short-term slope stability study. The safety factor for the slope used for the examination of long-term slope stability study will be selected as about 1.5 the value of the safety factor.

The strength of the piles used for the improved slope structures will be determined by taking into account the design examples learned from experienced knowledge of similar phenomena. It is necessary to consider whether to carry out protection of the slope surfaces of the testing canal facility.

4. Decisions Regarding the Form the Testing Canal Facility and Monitoring System

The size and shape of the testing canal facility will be decided by taking into account the space allocated to the project site, the construction plan, and the construction cost.

The detailed design work will be continued in Japan on the basis of the agreement and decisions mentioned above.

The basic installation plan for the monitoring system is presented in Table-1.

The instrument installation plan will be formulated after having recived the results of the analyses and used as reference taking into account other relevant data.

5. Field Report

The field report will be prepared at the end of the field work in Thailand. The field report may cover the following items:

- a. Layout and preliminary design for the preparatory work for the construction of the testing canal facility.
- b. Layout and preliminary design for the foundation improvement work.
- c. Preliminary slope stability analysis for excavated slopes using the circular slip method.
- d. Preliminary design on the monitoring system
- e. Draft construction plan
- f. Rough estimated construction cost
- g. Preparation of basic drawings

6. Office Work in Japan

The detailed design work in Japan will be carried out on the basis of the agreement between the detailed design team and R.I.D in the field report.

At the stage when the office work is completed, the draft and final report of the detailed design of the Model Infrastructure Project for the soft soil foundation will be submitted to RID through the JICA Thailand office.

The geotechnical data obtained from the in-situ tests and laboratory tests will be altered and, if necessary, analysis using the circular slip surface method will be conducted in Japan. Analysis using the compound slip surface method will also be carried out.

In order to predict the behaviour of the non-treatment slope structures, the elasto-visco plastic analysis using FEM will be carried out and conducted in Japan. The main contents of the final report are as follows:

- 1) Results of investigation work
- 2) Results of analysis work
- 3) Design of testing canal facility
- 4) Plan of monitoring system for the canal testing facility
- 5) Construction plan of the testing canal facility and installation plan of monitoring system
- 6) Amounts and construction cost of the testing canal facility
- 7) Specifications of monitoring system
- 8) Design drawing
- 9) Draft of tender documents
- 10) Reference of design and construction plan

7. Others

In the case of no heavy deformation occurring clearly in the non-treatment slope structure to examine short-term stability after construction of the excavation work, studies should be made into whether the embankment work shall be embarked upon or not.

IV. CONDITIONS FOR CARRYING OUT THE MODEL INFRASTRUCTURE PROJECT

In order to carry out the investigation, design and construction of the testing canal facility, RID has very generously assumed responsibility for the following collaboration with the Detailed Design Team.

- 1. Necessary Collaboration for the Investigation and Design Work
 - STS Co. conducts in-situ tests and laboratory tests, if it meets with the approval of the RID. Some in-situ and laboratory tests will be kindly performed by the RID.
 - 2) RID has agreed to support the geotechnical investigation of sand and gravel used in construction.
 - Consultation with the construction company concerning the construction cost and construction planning.

- 4) RID has granted permission for the use of the computer system at the IEC for performing the slope stability analysis and will provide the necessary computer people.
- 2. Preparation Work Necessary for Construction
 - RID will kindly provide the spoil area.
 - 2) The existing pumping operation facility will be used for setting up the monitoring system, if necessary arises.
 - 3) If re-location of the existing staff accommodation is necessary as a result of the construction work, if possibleit will have to be moved.
 - 4) The Detailed Design Team would appriciate efforts by the RID to provide engineers for the monitoring work of the testing canal facility.
 - 5) Unfortunately the RID will have to pay for the electricity charges for the drainage pumps after construction of the testing canal facility because the IEC has no budget to cover these charge.

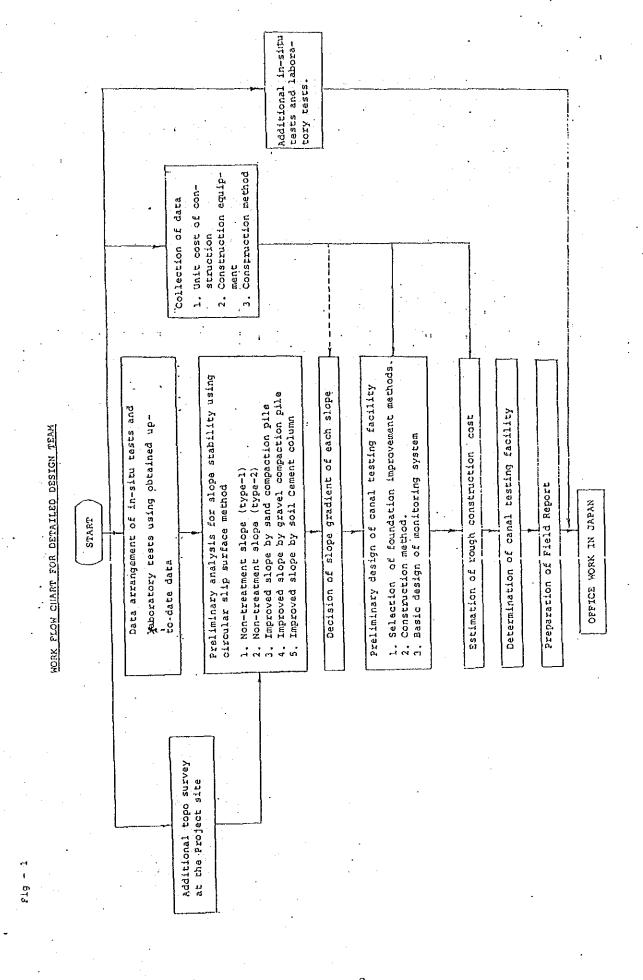


Table - 1 Purpose of Installation

.

Name of Instrument	Measured litem	? Purpose of Installation	Non-Treament slope l	Non-Treament slope 2	Improvement slope 3 4
1. Surface displacement Slope surface gauge and relative dispression for topo-survey	Slope surface deformation and relative displacement	10'measurs slope surface deformations in the excavated slopes.			(Pile for topo-survey)
2. Indinometer	Horizontal deformation in slope foundation	Horizontal deformation To measure horizontal deformation in the slope in slope foundation foundations causing failure, lateral flow and heaving.	\circ		0
3. Piezometer	Pore pressure in slope foundation	To measure the groundwater level and pore pressure behaviour occuring in the slope foundation.	0	Ö	0
5 4. Open pjezometer .	14		0	\circ	C
5. Differential settle- ment gauge (Non-treatment slope 1)	In the case that the embankment is filled, settlement of foundation.	To measure the vertical differential settle- ment of the slope foundation.	0	· [·	

OUTLINE OF THE TENTATIVE SCHEDULE FOR THE PROJECT

*		· '
1988	Japanese Side	<u>Thai Side</u>
	_	\mathcal{F}_{i}
February '	Detailed Design Survey (mission) Basic Plan of Detailed Design	Preparation of land etc.
March	26th Feb	
		·
	Field report 23rd Mar	
April	Detailed Design (in Japan)	
	late in April	
i	*	•
May	· *	
	*	
•	Final Report	-
	middle of May	Form A4 for equipment
		Request of Construction worklate in May
	. :	
June		through JICA Office
	JICA HQ	
	· · · · · ·	Form Al, for expert
		early in Jun
	Consultation with Ministry of	· .
	Forein Affairs	
	late in June	
July	244.0	
J W. J		Exchange of Verbal Note
August	Dispatch of Supervising Expertearly in Aug	
•	Remittance of Budget	
	early in Aug	
	and the same of th	•
		·
	Contract assigning Procedure	
	early in Aug	
**		
Ch	Start of Construction work	
September	Start of Construction work	
•	early in Sep	
	1	
	·	

