THE REPUBLIC OF GUATEMALA MINISTRY OF AGRIGULTURE, CATTLE AND FOOD RESOURCES

FEASIBILITY STUDY ON THE MONJAS IRRIGATION PROJECT FINAL REPORT



VOLUME II: APPENDIX 2

JULY 1988

JAPAN INTERNATIONAL COOPERATION AGENCY



JIER LIBRARY 1067716[9]

,8/11

THE REPUBLIC OF GUATEMALA MINISTRY OF AGRICULTURE, CATTLE AND FOOD RESOURCES

FEASIBILITY STUDY ON THE MONJAS IRRIGATION PROJECT FINAL REPORT



VOLUME II: APPENDIX 2

JULY 1988

JAPAN INTERNATIONAL COOPERATION AGENCY

国際協力事業団 18111

VOLUME II: APPENDIX

TABLE OF CONTENTS

1.1.			Page
1.	INTR	ODUCTION	1-1
2.	SOCI	O-ECONOMIC BACKGROUND	2-1
3.	PRES	ENT CONDITIONS OF THE STUDY AREA	3-1
	3.1	Socio-economic Condition	3-1
	3.2	Natural Conditions	3-4
•		3.2.1 Topography	3-4
		3.2.2 Meteorology	3-12
	•	3.2.3 Hydrology	3-54
	: .	3.2.4 Geology, Hydrogeology and Seismology	3-67
		3.2.5 Soils and Land Classification	3-122
	3.3	Agriculture	3-160
		3.3.1 Land Use	3-162
٠.		3.3.2 Agricultural Production	3-162
		3.3.3 Livestock Production	3-169
		3.3.4 Agricultural Management	3-171
		3.3.5 Marketing and Processing of	
		Agriculgural Products	3-173
* .		3.3.6 Related Agricultural Institutions	3-175
	3.4	Existing Irrigation Facilities	3-219
4.	DEVE	LOPMENT PLAN	4-1
	4.1	Basic Conception of the Project	4-1
		4.1.1 Water Resources Development	4-1
٠.		4.1.2 Study of Development Alternatives	4-3
	4.2	Development Plan	4-76
	-	4.2.1 Irrigation Plan	4-78
	•	4.2.2 Agricultural Plan	4-127
٠		4.2.3 Marketing and Processing of	
		Agricultural Products	4-159
	•	4.2.4 Related Agricultural Institutions	4-164

						Page 4-168
	4.3	Facility 4.3.1		gulating Reservo		4-170
		4.3.2	the state of the s	Facility Plan .	The second secon	. 4-197 . 4-211
	4.4	4.4.1 4.4.2	Unit Cost	on for Submerged		4-212 4-213
5.	PROJ	ECT IMPLE	MENTATION, O	PERATION AND MAIN	NTENANCE PLAN .	, 5-1
6.	PROJ	ECT EVALU	ATION		•••••	. 6-1
			·		·	·
	•			e de la companya de La companya de la co		
						•



- 4.1 Basic Conception on the Project
 - 4.1.1 Water Resources Development
 - (1) Study of the Proposed Dam Sites

 Table A.4.1.1-1 Summary of Geological Feature of Dam

 Sites
 - Table A.4.1.1-2 Comparative Table on the Optimum Dam Sites
 - Fig. A.4.1.1-1 Geological Map at Guirila Dam Site
 - Fig. A.4.1.1-2 Geological Map at Ostua Dam Site
 - Fig. A.4.1.1-3 Geological Map at San Fedro Dam Site
 - (2) H-Q Curves of Studies Dams
 Table A.4.1.1-3 Height-Volume and Height-Area
 Fig. A.4.1.1-4 Height-Volume and Height-Area Curves
 - (3) Groundwater Development Plan
 - Table A.4.1.1-4 Groundwater Requirement
 - Table A.4.1.1-5 Construction Cost of New Well
 - Table A.4.1.1-6 Maintenance Cost of Existing Well
 - Table A.4.1.1-7 Rehabilitation Cost of Existing Well in San Pedro Sector
 - Table A.4.1.1-8 Proposed Electric Charge
 - Fig. A.4.1.1-5 Field Irrigation System
 - Table A.4.1.1-9 Groundwater Irrigation Facilities
 - 4.1.2 Study of Development Alternatives
 - (1) Inflow of Guirila Dam

 Table A.4.1.2-1 Inflow of Guirila Dam

 Table A.4.1.2-2 Total Inflow of Guirila Dam
 - (2) Probability of Guirila Dam Inflow
 Fig. A.4.1.2-1 Probability of Inflow
 Table A.4.1.2-3 Probability of Guirila Dam Inflow by
 Iwai's Method
 - (3) Water Balance Calculation
 - Table A.4.1.2-4 Summary of Water Balance Calculation by Developed Area
 - Table A.4.1.2-5 Water Balance Calculation by Developed Area
 - Fig. A.4.1.2-2 Probability of Exceedance on Reservoir Storage of Guirila Dam
 - Table A.4.1.2-6 Probability of Exceedance on
 Reservoir Storage of Guirila Dam by
 Iwai's Method

- (4) Operation of Dam

 Fig. A.4.1.2-3 Result of Reservoir Operation Study

 Table A.4.1.2-7 Operation Study of Guirila Dam
- (5) Operation and Maintenance Cost of Alternative Plans
- (6) Water Charge of Production Cost
 Table A.4.1.2-8 Relationship between Water Charge and
 Production Value

4.1.1 Water Resources Development

(1) Study of the Proposed Dam Sites

The following five proposed dam sites are selected and studied in due consideration of topographic, geological and social conditions (Fig. 4.2.1-1).

- Guirila Dam Site
- Ostua Dam Site
- Blanco Dam Site
- San Pedro Dam Site
- Achiotes Dam Site

a. Guirila Dam Site

1. Topography and geology

Topography:

As a result of wide erosion, gentle topography is formed to a large extent. In both banks, terraces show conspicuous flat plains.

Geology:

This dam site consist of welded tuff with very low grade welding however, massive and relatively impermeable condition is suggested. The bed of river deposits including terraces is estimated several meters.

ii. Study of dam site

The Guirila dam site is located at about 4 km south ward from Casa de Tablas. The characteristics of this dam site are as follow:

- The left bank forms a gentle topography and occupies a half of the crest length. The river course is on the right bank, and the shape of valley is an inverted tropezoid.
- The crest length is long in about 1km, but the dam volume becomes small due to use of a gentle topography of the left bank.
- The saddle dam is required on the depression of right bank over the right abutment.
- Both abutments have enough creep ratio for seepage water.
- The dam site possess a favorable topography for the spillway. And also, the scale of spillway becomes small due to small catchment area in $26~\rm{km}^2$.

- The reservoir capacity at this dam site is bigger than the other dam site, because the pocket of reservoir is wide and the river bed slope is gentle in 1/120.

The features of main dam site and saddle dam site are as follows.

		14 Table 1		
•	Main dam site		Saddle dam site	
A COLOR OF THE PARTY OF THE PAR				
Right abutment	slope 1 t	to 2.5	slope 1 to	11.0
Left abutment	slope 1	to 2.7	slope 1 to	1.5
Width of river bed	30 m		30 m	•
Span height ratio	23	1	29	
•				

The geology of the dam site consist of low welded tuff, and sand gravel covers in several meter thickness on the welded tuff. The core trench for impervious zone should be placed on the welded tuff after removal of sand gravel layer.

The dam of about 50m height will be suitable for this dam site judging from the bearing capacity of low welded tuff.

The live capacity of reservoir is obtained 39.6 MCM from height-volume and height-area curve.

On the other hand, the height of saddle dam becomes about 31m from topography and geology condition.

b. Ostua Dam Site

1. Topography and geology

- Topography
 The valley of this site shows U-shape and 200m width in bottom. In the right side of the river a flat plain like terrace composed of basalt lava is found at about 10m higher than river level.
- Geology
 This site consists of welded tuff and basalt. As to characteristic, welded tuff is a low welding and a weak rock however, massive and less permeable. On the other hand, basalt is a solid, while permeable due to many open joints.

11. Study of dam site

The Ostua dam site is located at approximately 1.5km upstream from the confluence of the Ostua river and the Blanco river. This dam site is selected by the following reasons:

- The place where the foundation of the dam site is covered by thin terrace deposit and both abutments are narrowed.
- The river bed slope is steep 1/50. Therefore, a downstream is favorable position for the dam site in order to obtain more reservoir capacity.
- Both abutments have enough creep ratio for seepage water.
- The dam site has favorable topography for the placement of spillway.

The topographic features of this dam site are as follows:

	the contract of the contract o
Right abutment	slope 1 to 1.5
Left abutment	slope 1 to 2.0
Width of river bed	60 m
Span height ratio	4.7
	The second secon

Considering the topography, the dam site has favorable shape for a fill dam.

The dam height corresponding to the capacity of the Guirila dam is estimated approximately 76m from the height-volume and height-area curve.

As a conclusion, it is too difficult to construct a large dam of 70m dam height from viewpoint of the geological condition. Because, the bed rock of the dam site is low welded tuff and basalt layer overlies on the bed rock. It is presumed that pervious layer exist below the basalt layer. A considerable leakage water from the foundation will be anticipated, and the foundation treatment becomes difficult and entails great construction cost in this geological condition.

The dam scale at this site will be limited to maximum dam height of 50m (gross capacity of reservoir 14 MCM) due to the geological condition and the property of impervious material.

c. Blanco Dam Site

1. Topography and geology

- Topography
 Topographical features of this site is shown by gentle mountain slopes and a wide river deposit layer. Slope is about twenty degree at both slopes, especially a left slope shows a more gentle. In addition terraces, 200 to 30m wide are distributed.
- Geology
 Both mountain slopes are composed welded tuff top of which are overlaid by a thin basalt lava.
 This welded tuff is a weak rock with low welding grade. The river deposit may be shown very thick.

11. Study of dam site

The Blanco dam site is located at approximately 1.5km upstream from the confluence of the Ostua river and the Blanco river. The dam site has the topography of converse trapezoid, and the right abutment uses in common the left abutment of the Ostua dam. There exist wide river bed and developed terrace deposit at the dam site.

The right and left abutments form gentle slope of 1 to 3.0 and 1 to 2.5, respectively and the span height ratio is 10 on the longitudinal section along the dam axis. A fill dam is suitable for this dam site judging from the topography.

The geology of this dam site and the Ostua dam site is the same, the maximum dam height will be limited in 50m like the Ostua dam. And also, it is presumed that pervious layer exists below the welded tuff. Therefore, the foundation treatment becomes difficult and costly.

d. San Pedro Dam

- 1. Topography and geology
 - Topography
 This dam site shows V shape. Steep slope (forty to fifty degree) is formed in both banks. River width is narrow about 15m on an average.

This site is composed of porous basalt, basalt lava and andesite. Porous basalt is a stratified layer of basalt bombs and shows loose in solidification and high in permeability. Basalt lava is a fine, compact and hard rock however, may have high permeable due to dominant open joints. Andesite lava shows fine to medium grain and a hard rock however, fragile matrix is shown. High permeability is foreseen from many open joints.

ii. Study of dam site

The San Pedro dam site is located at about 700m southeast from El Ovejero. The left abutment is fromed by a small mountain having summit elevation of 1,258m which part of the Tahual volcano jutted out. The right abutment is caldera rim of the Retana lake.

This position is the narrowest valley and its topographic feature is as follows:

Right abutment	slope 1 to 2.0
Left abutment	slope 1 to 1.5
Width of river bed	30 m
Span height ratio	4.6

This vallley has a suitable shape for a dam site like the Ostua dam site.

According to the geological reconnaissance around the dam site, the geology of left slope consists of fine scoriaceous material between river bed and elevation 1,200m. It is presumed that the coefficient of permeability of scoria layer is the range of 10^{-2} to 10^{-3} cm/s. Basalt lava covers on the scoria layer.

There exist fracture zone with void at the river bed, and cracky andesite laid on the fracture zone forms the right abutment.

The existance of fault is observed on the direction of N-S at the dam site. It is not easy to construct a dam on this geological condition.

e. Achiotes Dam

i. Topography

- Topography and geology
 This site shows a locally small V shape valley. Hill
 top of both banks is located at some meter higher than
 the river bed. River deposit is thinly distributed.
- Geology
 This site consists of welded tuff showing very loose in welding and volcanic ash. Therefore, permeability of these lithologies is relatively low.

11. Study of dam site

The Achiotes dam site is located at approximately 3.0km north-northeastern from Casa de Tablas. The reservoir scale of this dam site is small, but it is possible to utilize as a regulating reservoir.

The features of the dam site are as follows:

- The layer of terrace deposit is thin and the width of valley is narrow.
- The river bed slope is steep 1/60. Therefore, it is difficult to expect sufficient storage capacity for a small scale dam.
- It is guessed that leakage from the foundation is not so much, because the geology of the dam site and the reservoir foundation is composed of massive welded tuff.
- The property of welded tuff is soft due to low welding degree, but has sufficient bearing capacity for the fondation of fill dam.
- The spillway becomes small scale because of small catchment area (13.6 km²). Therefore, it is possible to construct a spillway on the foundation of welded tuff. The topographic feature along the dam axi as follows:

· · · · · · · · · · · · · · · · · · ·	
Right abutment	slope 1 to 7.0
Left abutment	slope 1 to 3.0
Width of river bed	20 m
Span height ratio	7.3
· ·	•

Considering the topography and geology of the dam site a fill dam is suitable as the dam type. A favorable storage capacity is about 5 MCM for this dam site.

(3) Groundwater Development Plan

In establishing the groundwater development plan, this paragraph describes the basic concept, intake plan, development work cost, and irrigation plan.

- 1) Basic development policy
- Groundwater resources in the Study area are considered subsidiary resources of surface water.
- Groundwater development is restricted to Mojarritas Sector (512 ha) and San Pedro Sector (288 ha), both of which are remote from the dam site, have many existing wells, and are proven that pumping is hydrogeologically feasible.
- The area of a irrigated field by one well is 15 ha, and no well of common use is planned because local inhabitants have no custom of a common control system.
- Existing wells and facilities are further improved in productivity by means of cleaning and re-digging.
- New wells are of such type that farmers involved in development have been familiar with operation and maintenance.
- Emphasis is placed on least expensive construction cost, wherever practicable.

2) Water intake plan

a. Plan pumping volume and pumping time

Assuming that the pumping irrigation area covers about 800 ha out of benefited area of 4,800 ha, pumping volume is estimated at about 6.31 x 10^6 m³ per year (Table A.4.2.1-5), that is, an annual water requirement per unit area is about 7,900 m³/ha. In designing wells to pump this water requirement, reference should be made to peak water demand.

For the purpose of groundwater irrigation in the area of about 800 ha, the maximum volume of total water requirements is obtained for final 10 days in January.

568 ha x 0.74 1/sec/ha x 1/1000 x 10 days x 24 hours x 3600 = $363.2 \times 10^3 \text{ m}^3$

In this case, total pumping volume is found as follows.

 $363.2 \times 10^6/10 \text{ days } \times 24 \text{ hours } \times 3600 = 420 \text{ l/sec}$

This pumping volume is less than the average of the actual pumping volume per well (about 15 1/s), and regarded as being within the limit of safety pumping volume.

Assuming that an irrigation area per well is 15 ha approximate to the present average volume, Mojarritas Sector (512 ha) and San Pedro Sector (288 ha) require 35 wells and 20 wells, respectively, 55 wells in total. Thus, pumping volume per well is approximately 7.6 1/sec.

Annual pumping time per well is calculated as shown below.

$$T = \frac{6.31 \times 10^9}{7.6 \text{ 1/s} \times 3600 \text{ sec} \times 55 \text{ wells}} = 4193 \text{ hours}$$

Pumping time is 18 hours max. per day, and a recovery time of 6 hours is provided.

b. Intake well

The intake well should have a diameter of 100 mm (4 inches) considering maximum daily water supply. The well is designed to a depth of 80 m at Mojarritas Sector, and 100 m at San Pedro Sector. Layout of wells depends on the influence radius of the well, which is estimated at 350 m from data of existing wells. Therefore, wells are spaced at an interval of 400 m, with a safety factor taken into account. In summary, 55 wells are planned in total. More exactly, Mojarritas Sector has 17 new wells of 100 mm in diameter and 80 m in depth, and 18 existing wells to be repaired. San Pedro Sector has 16 new wells of 100 mm in diameter and 100 m in depth, and 4 existing wells to be repaired or re-digging.

The casing is used carbon steel pipes, and joints are subjected to socket full-circled welding. The screen is selected that meets the thickness of the aquifer. The SP layer inspection and specific gravity layer inspection are carried out immediately after digging, and screen length is determined. The screen is of slot type and gravel packed at the outside bore wall section. The packed gravel is sealed with clay on the top so as to prevent objectionable water from penetrating from the upper layer.

c. Water pump

In order to select pump type, the submergible pump is employed which is superior to the vertical turbine pump considering the following advantages.

- Given the design discharge, the submergible pump generally requires a smaller digging diameter than the vertical turbine pump. This results in less initial investment.
- The submergible pump requires no special tools and devices during installation. Therefore, this pump causes less trouble for maintenance.

- Excellent operation efficiency entails less expensive pump operation expenses.
- Farmers in this Area are familiar with operation and maintenance of this pump.

The water intake facilities are composed of the submergible pump, water lift pipe, air valve, combination meter, check valve, sluice valve, power cable, control electrodes and cables, and field panel.

d. Prime mover output

The shaft power of the pump is found from the obtained discharge Q and total lift using the following equation.

$$Ps = 0.163 \times rQH/2$$

In the next, the prime power output P is obtained in the following equation, including the allowance.

$$P = Ps (1 + \lambda)$$

Where, Ps = shaft horse power, kW.

r: Unit Weight of Wafer (kg/2)

Q: Discharge Volume (m³/min)

H: Total Head (m)

?: Efficiency of Pump (= 75%)

P: Horse Power of Motor (kW)

 $Ps = 0.163 \times 1 \times 0.46 \times 60/0.75$

÷ 6.0

P = 6.0 (1 + 0.2)

= 7.2 (kW)

Both Sectors are provided with 10 HP pumps manufactured to the pump specification. The 10 HP pump commonly used in the Study has a pumping capacity of about 8.4 1/sec according to the capacity curve of the pump, assuming that the total head is 60 m (as obtained from private well diggers by hearing). This value sufficiently covers water requirements per well.

3) Construction cost and maintenance expense

a. Construction cost

Groundwater development is put into practice for following Sectors as shown below.

Sector	New well	Existing well to be repaired
Mojarritas	17	18
San Pedro	16	4 1/

1/ Three wells require re-digging to a depth of 100 m.

Construction cost, repair expenses, etc. are shown as below.

New well construction cost (*1)

```
17 wells x Q82,700 = Q1,405,900 ...... Mojarritas Sector
16 wells x Q90,500 = \frac{Q1,448,000}{Q2,853,900} ..... San Pedro Sector
Subtotal
```

Maintenance expense (*2) and re-digging cost of existing well (*3)

```
18 wells x Q5,900 = Q106,200 ... Mojarritas Sector

1 well x Q6,500 x 1.7 (*4) = Q11,100 ... San Pedro Sector

3 wells x Q23,200 = Q69,600 ... San Pedro Sector

Subtotal Q186,900

Grand Total Q3,040,800
```

- *1 Refer to Table A.4.1.1-5.
- *2 Refer to Table A.4.1.1-6.
- *3 Refer to Table A.4.1.1-7.
- *4 Well depth: Approximately 170 m

b. Operation and Maintenance expenses

Operation and Maintenance expenses consist of maintenance expense imposed once a 5 years and electric charges. Annual operation and maintenance expenses are shown as below.

Annual Operation and Maintenance Cost by Sector

(Unit: O/ha/yr)

Sector	Repair cost	Electric charges	Total	
Mojarritas	79	353.15	432.15	
San Pedro	87	353.15	440.15	

c. Groundwater cost

The following calculation shows groundwater cost necessary for obtaining a pumping discharge per unit from the well to be newly developed in San Pedro Sector.

Item	Price (Q)	Note
Development Cost	90,500	see Table A.4.1.1-5
for New Well Annual Maintenance	1,300	see Table A.4.1.1-6
Cost Electric Charge	5,297	Q 6,500 - 5 years Q 353.15 x 15 ha
Annual Instalment	0.0805 (1 = 5%)	, 0.1175 (i = 10%),
Rate	durable period	: 20 yrs, i : annual interest = 7.6 liter/s x 4193 hrs)
Annual Pumping Discharge	114,720 m (110 Trock of Wasse was

Case of 5% (= 1)

Unit Cost of Groundwater = $\frac{90,500 \times 0.0805 + 1,300 + 5,297}{114,720}$

 $= 0.12 \text{ Q/m}^3$

Case of 10% (= i)

Unit Cost of Groundwater = $\frac{90,500 \times 0.1175 + 1,300 + 5.297}{114,720}$

 $= 0.15 \, Q/m^3$

4) Groundwater irrigation plan

In the Study area irrigation groundwater is generally supplied directly to farm land with the submergible pump of the well.

The irrigation plan is summarized as below.

Proposed irrigation area: 15 ha Crop: Vegetables

Irrigation system : Sprinkler irrigation system, which

enables furrow irrigation.

Irrigation interval : 7 days

Normal sprinkler pressure: pressure 1.5 kgf/cm²

Soil : Vertisol

a. Design

- Total water requirement 4.5 mm/day

Evaporation loss : 5%

Field loss : 5 mm/day

Irrigation intensity: 2.1 mm/hr (standard value of plant soil)

- Irrigation water depth, d mm

d mm/day = 4.5 mm/day x 7 x (1 + 5%) + 5 mm/day= 38.1 mm/day Irrigation system for 2.1 ha per day (15 ha for 7 days)

1. Total water requirement, q

$$q' = 2.1 \times 100 \times 100 \times 38.1/1000 = 800.1 \text{ m}^3/\text{day}$$

If a transmission loss is 10%, then $q = 800.1 \text{ m}^3/\text{day} \times 1.1 = 880.1 \text{ m}^3/\text{day}$.

- Irrigation time

$$t = \frac{Q}{Irrigation\ Intensity} = \frac{880.1 \times 1000 \times 1000 \times 1000}{2.1 \times 100000 \times 100000 \times 10} = 4.19 \div 4.2 \text{ hr}$$

- Design of irrigation facilities
 - i. Distribution and discharge

$$Q = \frac{880.1 \text{ m}^3}{4.2 \text{ hr x } 60 \text{ x } 60} = 0.0582 \text{ m}^3/\text{sec}$$

Pipe diameter
If maximum Vmax is 1.0 mm, then

pipe area $A = 0.0582/1.0 = 0.0582 \text{ m}^2$

Therefore

pipe diameters D = 0.27 m

The mean pipe diameter is to be 100 mm (4 inches).

The YU pipe is used that sufficiently withstands an inner pressure of 1.5 kg/cm^2 .

11. Sprinkler interval, L

If a sprinkler system uses a nozzle 5.2×3.2 in diameter under a pressure of 1.5 kg/cm, then

spray irrigation diameter Dc = 25.0 mspray irrigation diameter q = 30.0 /min and, spray irrigation intensity r = 8.0 mm/hr

Therefore, the sprinkler is as follows, with influence of wind taken into account.

 $L = Dc \times 0.5 = 12.5 m$

b. Work quantity

Water source - Deep well (depth: 80 m or 100 m)

- Submergible pump and incidental facilities

Water Supply pipe VU 100, 250 m per 2 ha

i. Underground pipeline

- excavation, normal soil
$$V_1 = 1.2 \times 0.5 \times 250 = 150 \text{ m}^3$$

$$V_2 = \frac{0.1^2}{4} \times 250 = 2 \text{ m}^3$$

- refilling
$$v_3 = 150 - 2 = 148 \text{ m}^3$$

ii. Coupling

- excavation

$$V_1 = \frac{1.0^2}{4} \times 0.5 = 0.50 \times \frac{200m}{15m} = 7$$

- Refilling

$$v_2 = 7.0 - 0.7^2 \times 0.5 \times \frac{200}{15} = 4 \text{ m}^3$$

- Form

$$s = 0.7 \times 0.5 \times 8 \times \frac{200}{15} = 38 \text{ m}^2$$

- Plain concrete

$$v_1 = (0.7^2 \times 0.5 - 0.4^2 \times 0.35) \times \frac{200}{15} = 2.52 \text{ m}^2$$

- Valve 50, (13.3)

iii. Sprinkler set

1. Component: Nozzle

5 sets

Riser pipe : 5 se

Relocatable pipe: 45 m

2. Quantity per 2 ha

$$\frac{200}{15}$$
 x 2 = 26.6 = 26.6 sets

Table A.4.1.1-9 summarizes the necessary work quantity.

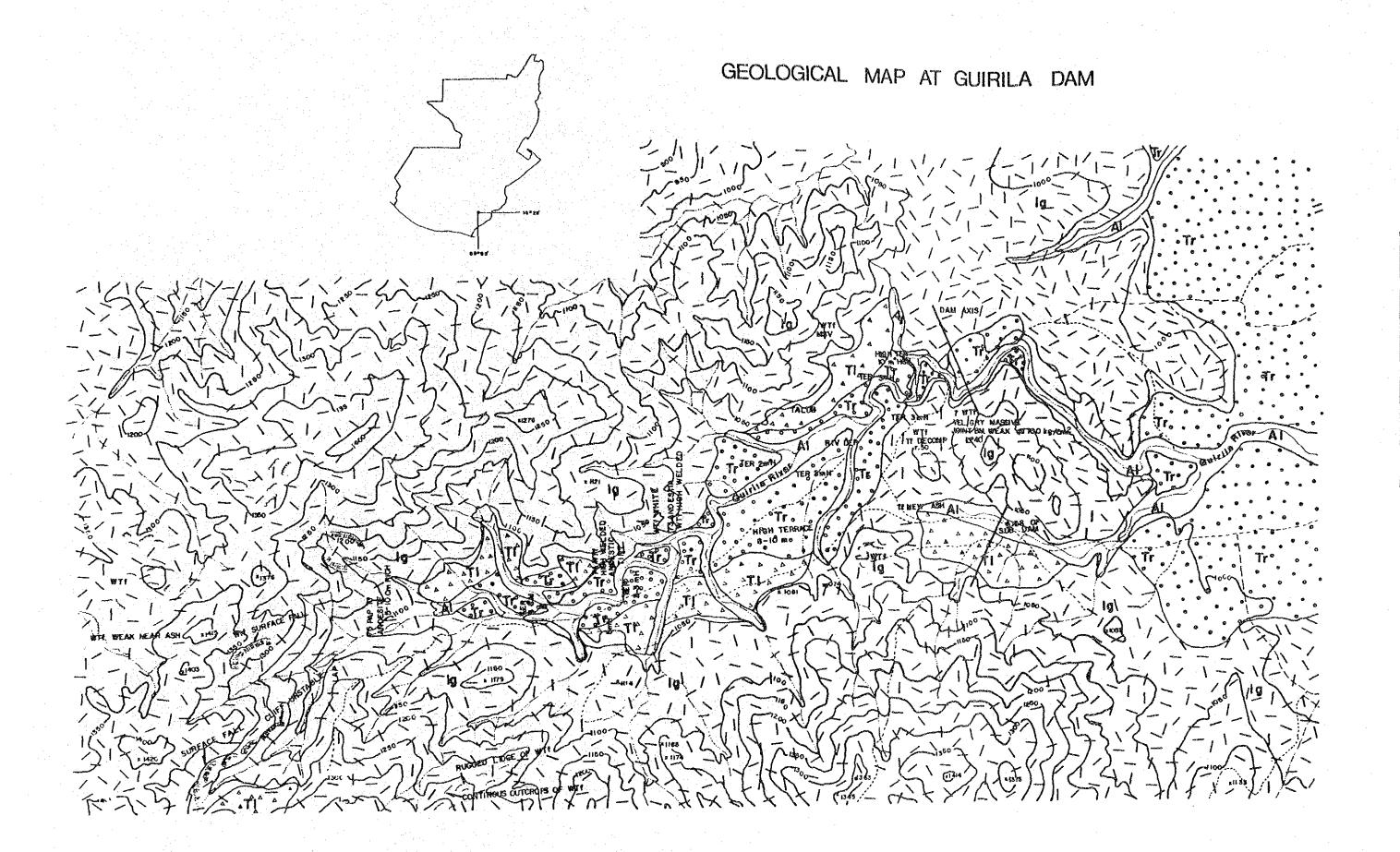
Table A.4.1.1-1 Summary of Geological Feature of Dam Sites

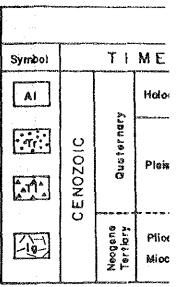
$\perp /$	Dam Site					
Item		Guirila River	Ostua River	Blanco River	San Pedro River	Los Achlotes (Regulating)
	Geomorphological Features	Widely eroded valley gentle slope	U-shape valley Wide plain of basalt lava in the right bank	Very thin ridge Extensively wide alluvial plain	V-shape valley	Small scale of V-shape valley
	Rock Type	Welded Tuff	Welded Tuff and Basalt	Welded Tuff	Porous Basalt, Basalt Lava Andesite	Welded Tuff
	Hardness Toughness	Weak rock	Welded tuff: Weak rock Basalt: Hard rock	Weak rock	Porous Basalt: Loose, weak Basalt Lava: Hard rock Andesite:	Weak
	Permeability	Low	High in the contact zone of basalt layer and welded tuff	Low	Very high	Low
	River deposit and Talus deposit	Thin, 5 m + in thickness	Common about 10 m in thickness	Very wide and thick Assumed more than 20 m	Thinly scatter	Thinly scatter
	Remarks	Low permeability of foundation rock	Welded tuff is weak for large spillway High permeability	Thin ridge for abutment Extensively wide and thick river deposit	Very high permea- bility in the porous basalt and basalt lava	Massive and less permeable layer for foundation
	Evaluation for Dam Site	Better	Relatively Bad	Unsultable	Relatively Bad	Ordinary (Dam scale is small)
١.						

Table A.4.1.1-2 Comparative Table on the Optimum Dam Sites

Synthetic Estimation	-	2	m,
Order	нӨ	40	ოტ
Coefficient of Reservoir Capacity	13.50	9.20 (13.40)	4.60 (8.10)
Order	~⊖	H@)	წ
Dam Volume	2.63 мсм	1.53 MCM (3.60) MCM	2.80 MCH (5.10) MCM
Order	⊕	7 (0	%
Dam Height	m 0.64	50.0 m (76.5) m	50.0 m (74.0) m
Reservoir Capacity	Live Capacity 39.6 MCM Gross Capacity 40.9 MCM	Live Capacity 5.1 MCM (39.6) Gross Capacity 14.0 MCM (48.5)	Live Capacity 11.2 MCM (39.0) Gross Capacity 13.0 MCM (41.4)
Order	r-4	ю	2
Catchment Area Flood Discharge for Spillway	Catchment Area 26 km ² Flood Discharge 461 m ³ /s	Catchment Area 177 km ² Flood Discharge 1900 m ³ /s	Catchment Area 36 km ² Flood Discharge 510 m ³ /s
Order	m	н	8
Topography	Left Abutment slope 1:2.7 Right Abutment slope 1:2.5 Span-height Ratio	Left Abutment slope 1:2.0 Right Abutment slope 1:1.5 Span-height Ratio	Left Abutment slope 1:2.5 Right Abutment slope 1:3.0 Span-height Ratio
Dam Site	Guirila	Ostua	Blanco

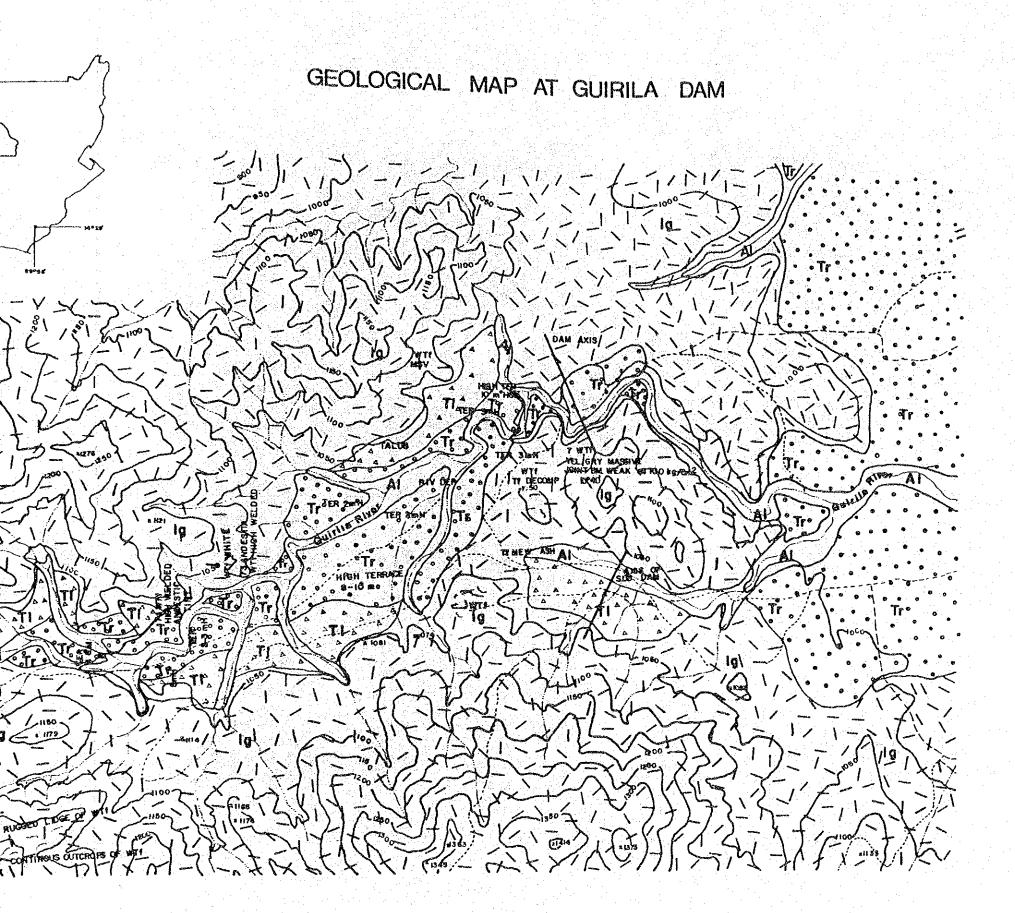
(Notes) Figure of () and order of (), in case of live capacity of reservoir 39.6 MCM at the Ostua and Blanco dam sites.

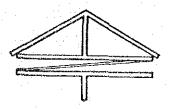




1002

Fig. A.4.1.1-





			And the law was too be made and the special contraction of the special cont	EOL	OGY
Symbol		Ti	ME	NAME	Rock Type and Characteristic
Ai		Å	Holocens	Alluvial Deposit	Recent river deposit, send and gravel and boulder rich.
	010	Suaternar	District	Terroce Deposit	Sand and gravel layer, boulder rich.
[aria]	ENOZ	Š	Pleistocene	Telus Deposit	Tuff origin silty acil associated with large boulders.
	၁	Neogene Terttory	Pliocene Miocene	Welded Tum	Law Welding Weak rock. Massive and low permeability.

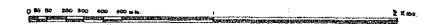
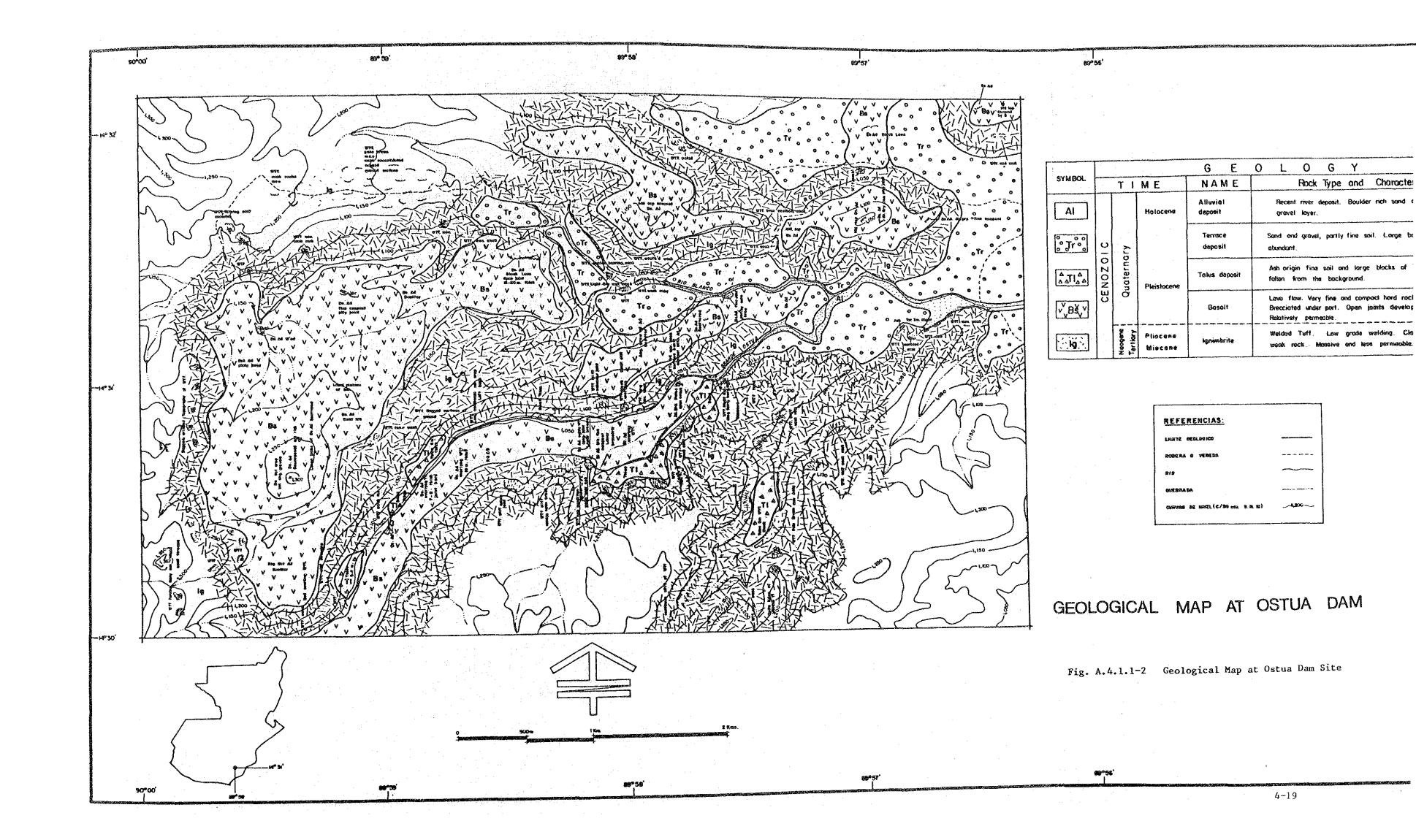
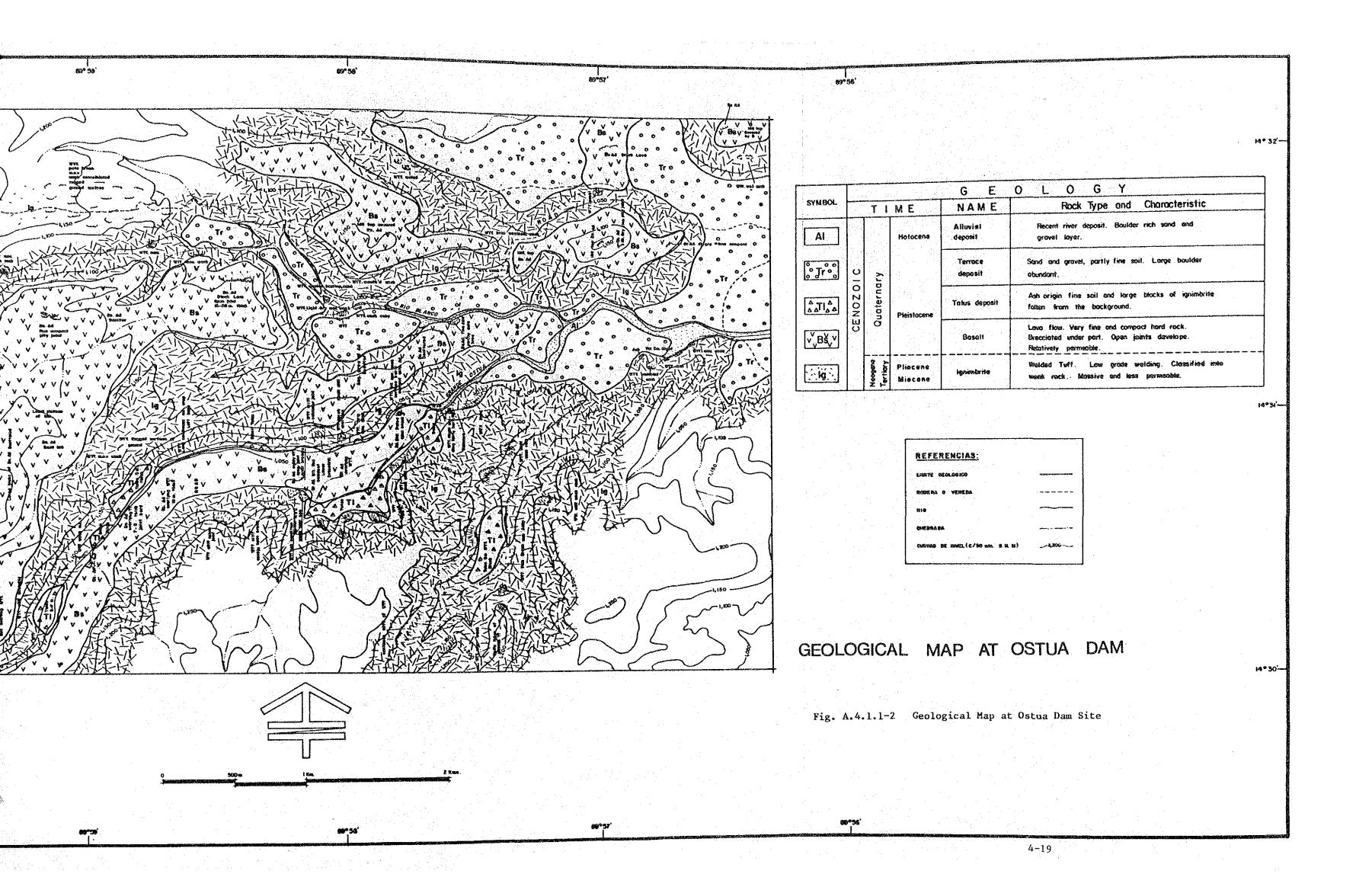


Fig. A.4.1.1-1 Geological Map at Guirila Dam Site





GEOLOGICAL MAP AT SAN PEDRO DAM

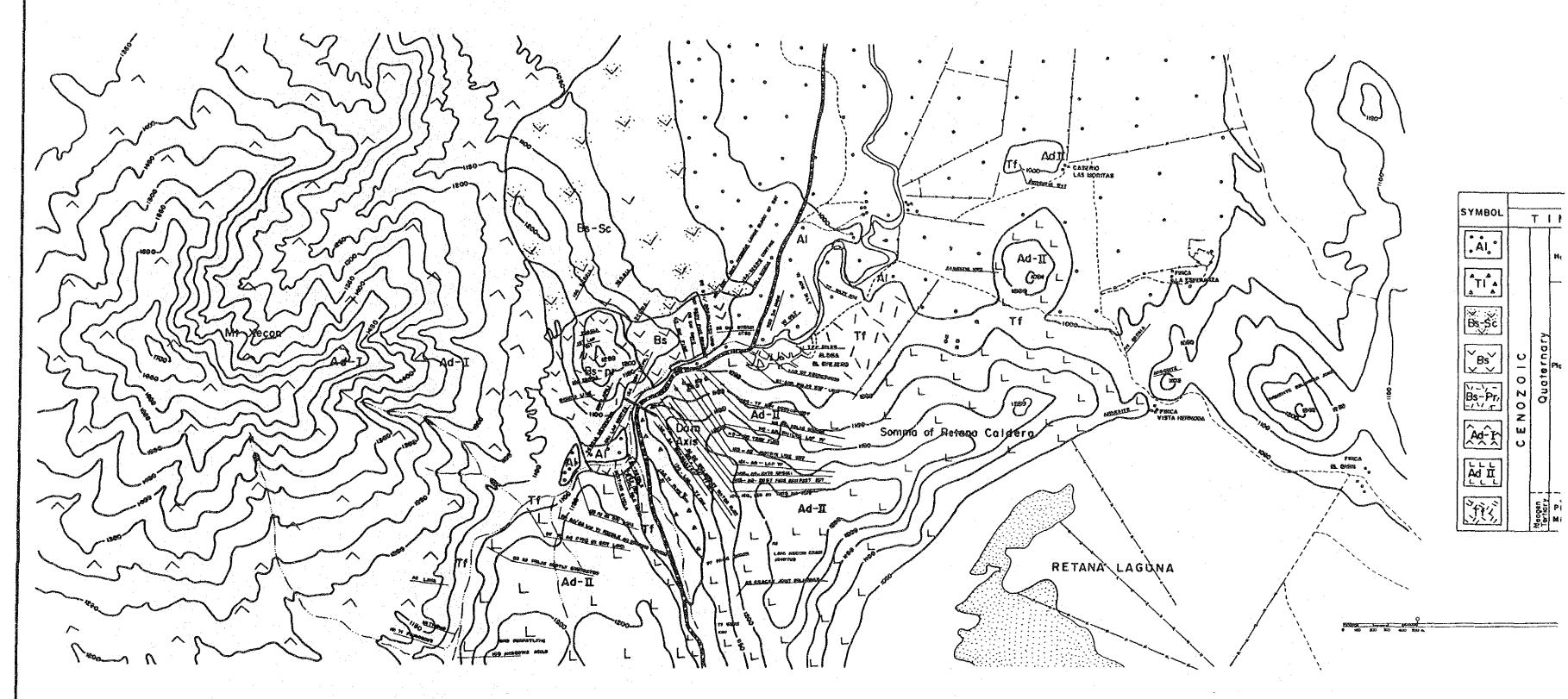
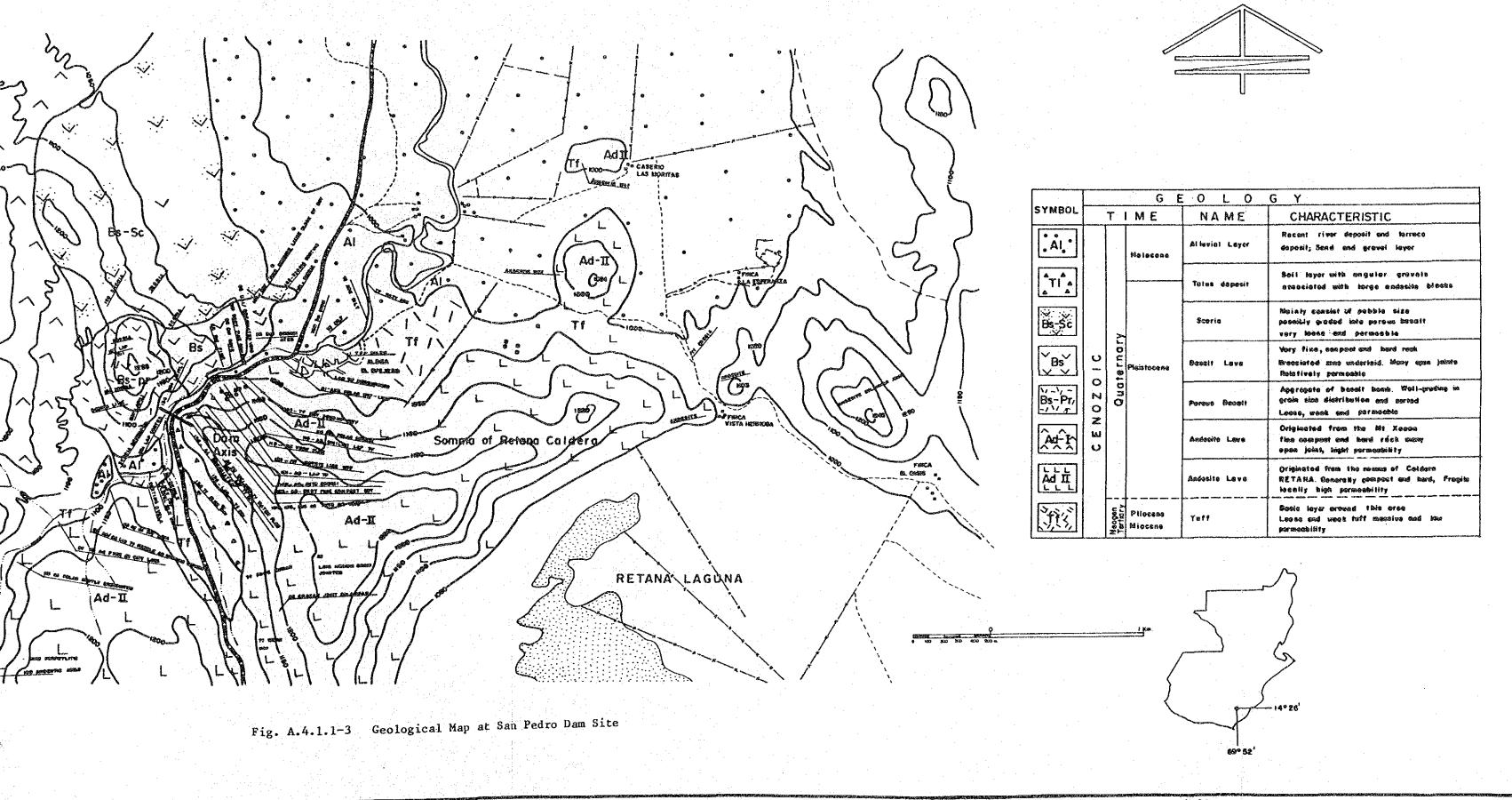


Fig. A.4.1.1-3 Geological Map at San Pedro Dam Site

GEOLOGICAL MAP AT SAN PEDRO DAM



(2) H-Q Curves of Studies Dams

Table A.4.1.1-3 Height-Volume and Height-Area (1)

Guirila Dam:

EL	<u>Δ Η</u>	Area	Ave. Area	Unit Volume	Accumulated Volume
EL 1,000	_	- -		 -	
1,010	10	359,300	179,650	1,796,500	1,796,500
1,020	10	963,875	661,587	6,615,870	8,412,370
1,030	10	1,773,400	1,368,637	13,686,370	22,098,740
1,040	10	2,342,137	2,057,768	20,577,680	42,676,420
1,050	10	2,829,662	2,585,899	25,858,990	68,535,410
		and the second s			

Ostua Dam:

EL	ΔН	Area	Ave. Area	Unit Volume	Accumulated Volume
EL 1,030		· .			
1,040	10	59,375	29,687	296,870	296,870
1,050	10	304,687	182,031	1,820,310	2,117,180
1,060	10	667,187	485,937	4,859,370	6,976,550
1,070	10	928,125	797,656	7,976,560	14,953,110
1.080	10	1,262,500	1,095,312	10,953,120	25,906,240
1,090	10	1,593,750	1,428,125	14,281,250	40,187,490
1,100	10	1,884,375	1,739,062	17,390,625	57,578,115

Blanco Dam:

EL	<u> </u>	Area	Ave. Area	Unit Volume	Accumulated Volume
EL 1,030	·	-			-
1,040	10	101,562	50,781	507,810	507,810
1,050	. 10	412,500	257,031	2,570,310	3,078,120
1,060	10	728,125	570,312	5,703,120	8,781,240
1,070	10	965,625	846,875	8,468,750	17,249,990
1,080	10	1,256,250	1,110,937	11,109,370	28,359,360
1,090	10	1,584,375	1,420,312	14,203,120	42,562,480
1,100	10	1,962,500	1,773,437	17,734,370	60,296,850

Table A.4.1.1-3 Height-Volume and Height-Area (2)

San Pedro Dam:

EL	ΔΗ	Area	Ave. Area	Unit Volume	Accumulated Volume
127 1 OFF					
EL 1,055					
1,060	-5	143,750	67,188	355,940	335,940
1,070	10	343,750	239,062	2,390,620	2,726,560
1,080	10	596,875	470,312	4,703,120	7,429,680
1,090	10	848,438	722,656	7,226,560	14,656,240
1,100	10	1,182,812	1,015,625	10,156,250	24,812,490

Achiotes Dam:

EL	<u> </u>	Area	Ave. Area	Unit Volume	Accumulated Volume
EL 1,000	- ;	-	<u>-</u>	***	
1,010	10	40,625	20,312	203,120	203,120
1,020	10	190,625	115,625	1,156,250	1,359,370
1,030	. 10	392,187	291,406	2,914,060	4,273,430
1,040	10	623,437	507,812	5,078,120	9,351,550
1,050	10	881,250	752,343	7,523,430	16,874,980
1,060	10	1,165,625	1,023,437	10,234,370	27,109,350

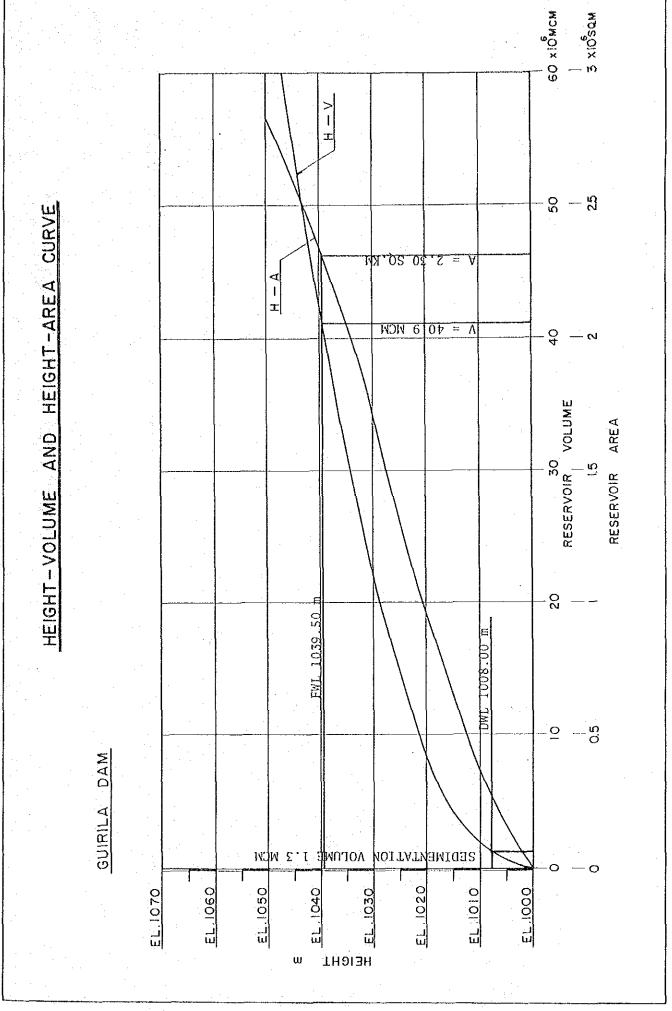


Fig. A.4.1.1-4 Height-Volume and Heihgt-Area Curves (Guirila Dam Site)

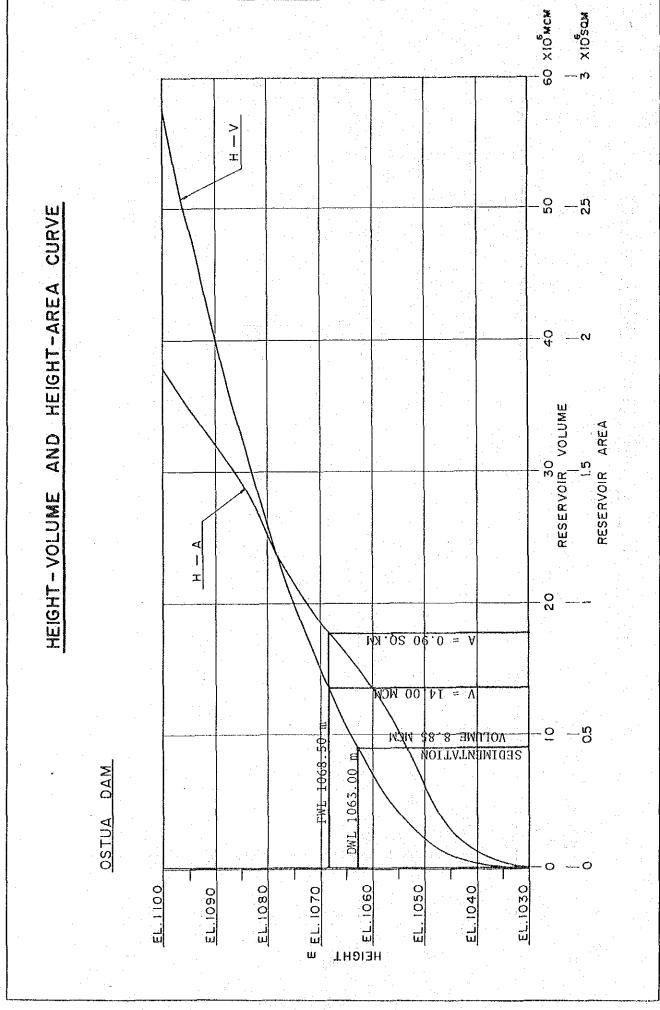


Fig. A.4.1.1-4 Height-Volume and Heingt-Area Curves (Ostua Dam Site)

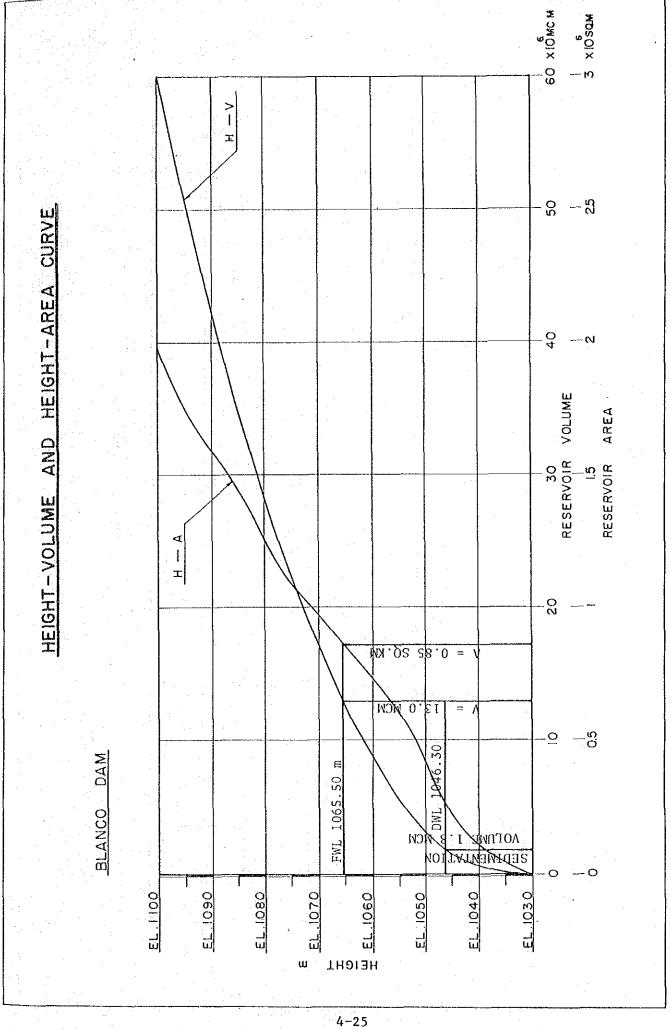
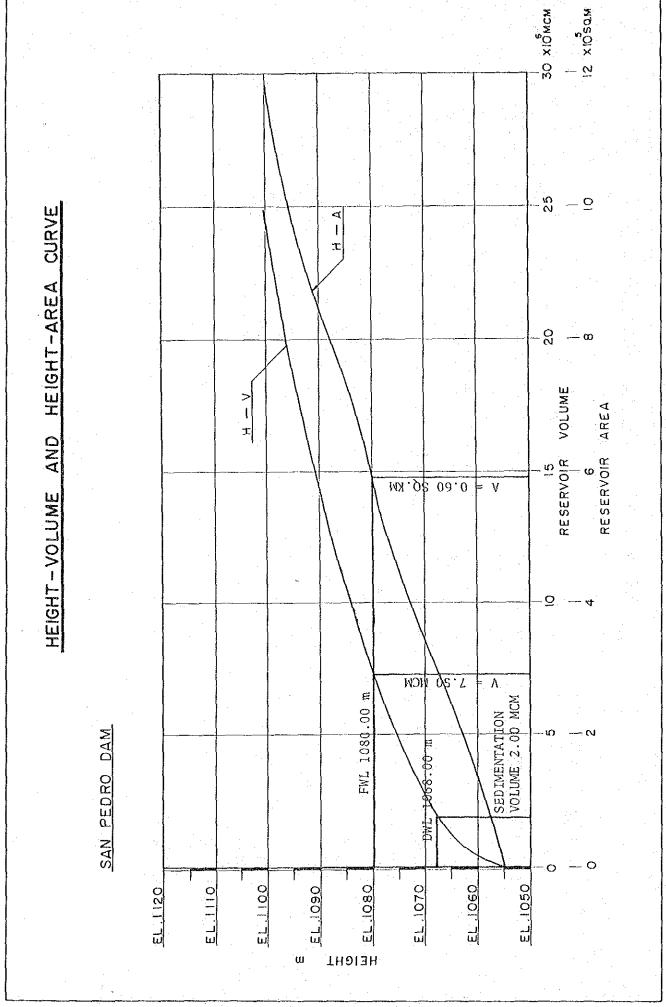


Fig. A.4.1.1-4 Height-Volume and Heingt-Area Curves (Blanco Dam)



Height-Volume and Heihgt-Area Curves (San Pedro Dam Site) Fig. A.4.1.1-4

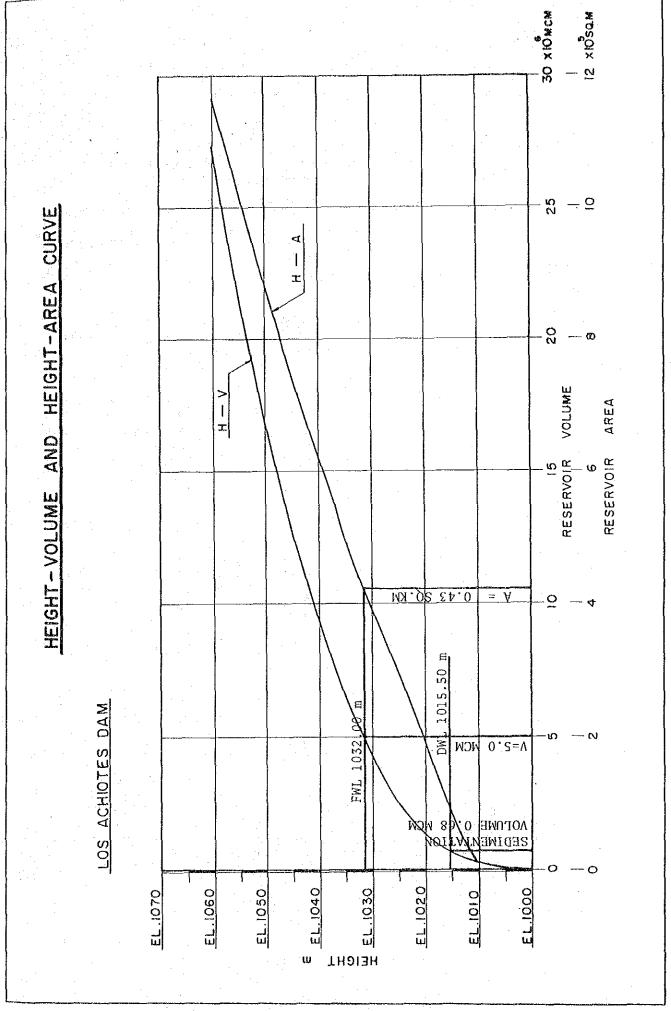


Fig. A.4.1.1-4 Height-Volume and Heihgt-Area Curves (Achiotes Dam)

Groundwater Requirement

Month	Day 10day	Irrigation (ha)	Unit Water Requirement (liter/sec/ha)	Water Requiremen x10 ³ m ³
	В	331	0.32	91.5
May	М	345	0.23	68.6
 -	L	359	0.20	62.0
2	В	418	0.06	21.7
Jan.	М	476	0.05	20.6
	L	535	0.03	13.9
•	В	602	0.04	20.8
Jul.	M.	668	0.05	28.9
	L	735	0.06	38.1
	В	735	0.08	50.8
Aug.	M	735	0.14	88.9
. 0	\mathbf{r}	735	0.12	76.2
	В	713	0.15	90.4
Sep.	M	691	0.15	89.6
• .	\mathbf{L}	668	0.12	69.3
	В	624	0.25	134.8
Oct.	M	579	0.24	120.1
	L	535	0.31	143.3
	В	579	0.59	295.2
Nov.	M	579	0.51	255.1
_	L	602	0.49	254.9
	В	602	0.49	254.9
Dec.	М	602	0.51	265.3
	L	602	0.58	301.7
. •	В	610	0.61	321.5
Jan.	M	618	0.63	336.4
	L	627	0.67	363.0
	В	568	0.74	363.2
Feb.	M	510	0.77	339.3
•	L	451	0.81	315.6
	В	415	0.81	290.4
Mar.	_ M	379	0.81	265.2
a	L	343	0.86	254.9
	B	312	0.84	226.4
Ápr.	M	281	0.84	203.9
.E	L	251	0.81	175.7

¹⁾

Area obtained from proposed cropping pattern
Unit water requirement of surface water x 0.476 (Irrigation Efficiency) - 0.62 (Field Application Efficiency)
Unit water requirement x ha x 10days x 24hrs x 3,600 2)

³⁾

Table A.4.1.1-5 Construction Cost of New Well

(unit: Q)

	II . D. I	77. 1	Price		Wata
Item	U. Price	volume	Mojarritas Sec. S	. Pedro Sec.	Note
Transportation		1 unit	1,500	1,500	machine, equipment
Installation & Remove		1 unit	1,000	1,000	equipment
Boring	205	80m, 100m	16,400	20,500	ø 10 ,"
Casing		1 unit	10,400	13,000	including installation
Screen	420	50 m	21,000	21,000	including installation
Gravel Packing	5	80m, 100m	400	500	
Cementing Well Cleaning		1 unit 1 unit	100 800	100 1,000	
Pumping Test Electric		1 unit 1 unit	1,500 400	1,500 500	
Prospecting Submergible Pump		1 unit	11,500	11,500	10 HP including
Installation of Electric	24	300m	7,200	7,200	installation
Cable Transformer Contingency		1 unit 10%	3,000 7,500	3,000 8,200	
Total			82,700	90,500	
			(source : INS	LVUMEH)

Table A.4.1.1-6 Maintenance Cost of Existing Well

Item	Unit	Price	(Q) Volume	Price (Q)	Note
Transportation			1 unit	1.000	machine, equipment, etc
Installment &			1 unit	500	Totalio, oquipmono, oo
Cleaning		60	65 hrs	3,900	Mojarritas Sec.
		18 3.5	75 hrs	4,500	San Pedro Sec.
Pump Maintenance			1 unit	500	
			······································		
Total				5,900	Mojarritas Sec.
		•			San Pedro Sec.

(source : Private Company)

Table A.4.1.1-7 Rehabilitation Cost of Existing Well

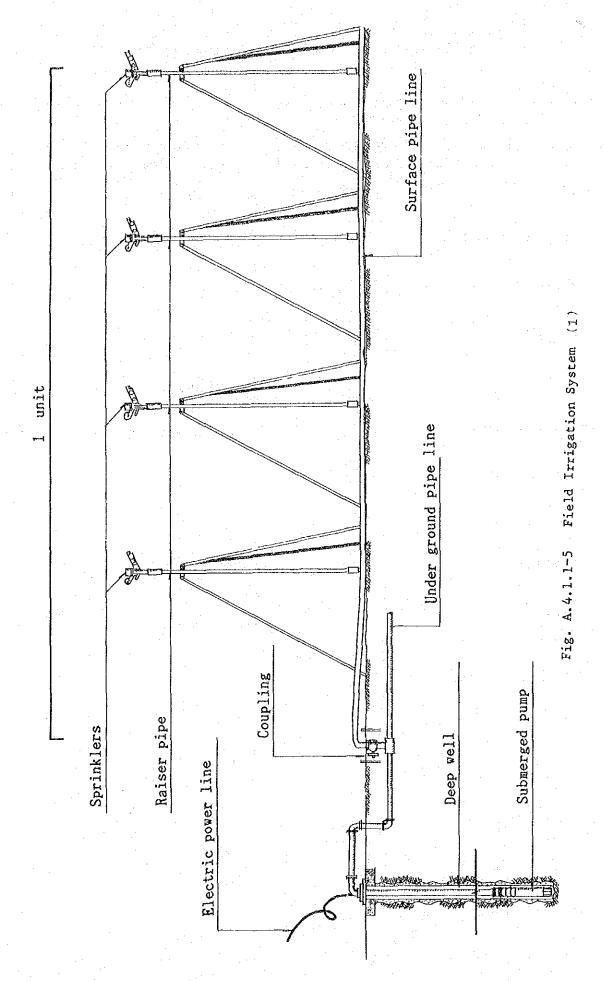
Item	Unit Price	(Q) Volume	Price (Q)	Note
Transportation Installment &	პაითი ა, თ. იგ. / მილი გაბან და თაფხაც ჩნა მიამ _{მგ} ა _{ს გ} <u>ა და გა</u> გამამთი თუგეგ გეგ	l unit l unit	1,500 1,000	machine, equipment
Remove Boring	205	21 m	4,300	ø 10 " including pipe
Screen	420	21 m	8,800	including installment
Gravel Packing Cementing	50	21 m 1 unit	1,000 100	
Well Cleaning		l unit	4,500	
Pumping Test Pump Maintenance		l unit 1 unit	1,500 500	
Total			23,200	

Table A.4.1.1-8 Proposed Electric Charge

Item	
Pumping Hour	4,193 hrs
Pump Power	7.5 kW
Consumed Electricity	31,448 kWh
Electric Charge	
Basic Charge	$Q 2,96 \times 7.5 \text{ kW}$
	= Q 22.2
Consumption Charge	$Q 0.134 \times 100 \text{ kWh} \times 7.5 \text{ kW} + Q 0.128 \times$
	$100 \text{ kWh } \times 7.5 \text{ kW} + Q 0.108 \times 31.248 \text{ kWh}$
	= Q 3571.28
Utilization Charge	$Q 1.35 \times 7.5 \text{ kW}$
of Electric	= Q 10.13
Installation	
Sub-total	Q 3,603.61
Combustible Adjustment	Q 1,693.70
(40%) + IVA (70%)	
Grand-total	Q 5, 297.31
Electric Charge per ha	Q 353.15

Table A.4.1.1-9 Groundwater irrigation Facilities

Item	2.0 ha Unit quantity	15 ha Calculation	Total quantity
VU 100	250 m	15 ha x $\frac{250}{2 \text{ ha}} = 1875 \text{ m}$	1875 m
Coupling, valve	13.3	$15 \times \frac{13.3}{2} = 99.75 = 100$	100
Excavation	$150 + 7 = 157 \text{ m}^3$	$15 \times \frac{157}{2} = 1177.5$	1178 m
Refilling	$148 + 4 = 152 \text{ m}^3$	$15 \times \frac{152}{2} = 1140$	1140 m
Form	37 m ²	$15 \times \frac{37}{2} = 277.5$	277.5
Plain concrete	2.75 m ³	$15 \times \frac{2.75}{2} = 20.625$	20.625 m
Sprinkler set Nozzle		15 ha 5	5.4
	5	$\frac{15 \text{ ha}}{7 \text{ days}} \times \frac{5}{2 \text{ ha}} = 5.36$	
Riser pipe	5	$\frac{15 \text{ ha}}{7 \text{ days}} \times \frac{5}{2 \text{ ha}} = 5.36$	5.4
Pipe	5	$\frac{15 \text{ ha}}{7 \text{ days}} \times \frac{5}{2 \text{ ha}} = 5.36$	48.2 m



4-32

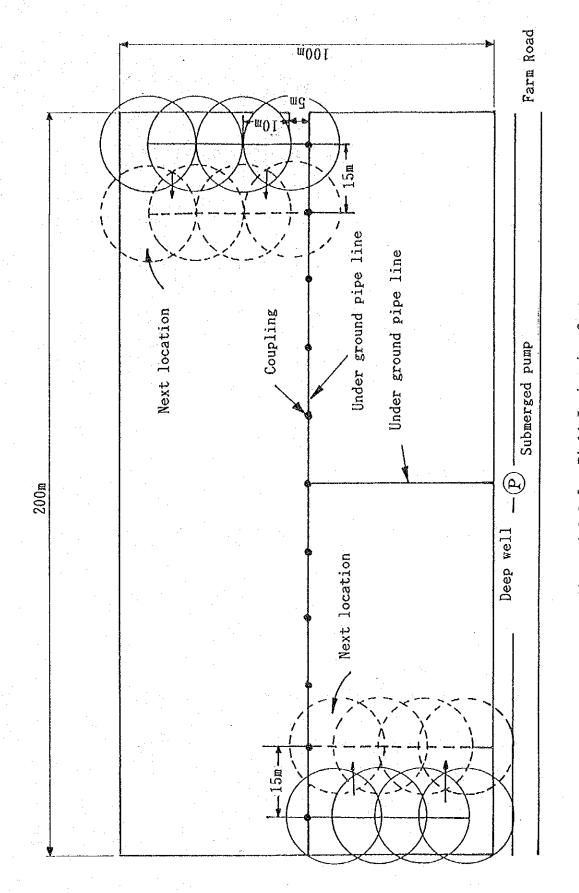


Fig. A.4.1.1-5 Field Irrigation System (2)

(1) Inflow of Guirila Dam

Table A.4.1.2-1 Inflow of Guirila Dam

(Units; MCM)

		Driving C	anal Capac	city (m³/s)	, 1 Fil
Year	3.0	4.0	5.0	6.0	7.0
1967	49.3	56.6	61.2	65.2	68.4
68	64.0	74.1	83.0	90.6	99.0
69	74.3	86.9	98.6	109.1	118.4
70	55.6	64.4	72.3	79.6	86.4
. 71	55.0	62.4	68.5	73.9	78.9
72	19.4	20.5	21.4	22.2	22.8
73	65.3	77.1	88.1	98.2	106.5
74	45.6	52.4	58.3	63.4	67.8
75	39.2	45.5	50.8	55.3	59.4
76	40.8	45.8	50.0	53.8	57.4
77	21.9	23.7	25.1	26.2	27.2
78	55.1	60.8	65.9	70.0	73.4
79	50.4	57.7	63.8	69.4	74.6
80	54.5	62.1	68.7	74.7	79.8
81	57.8	64.2	68.2	71.1	73.3
Mean	49.9	56.3	62.9	68.2	72.9
Max	74.3	86.9	98.6	109.1	118.4
Min	19.4_	20.5	21.4	22.2	22.8

V = Qqui + Qost

V; Inflow of Guirila Dam

Qqui; Discharge of Guirila river (direct)

Qost; Diverted water from Ostua river (Indirect)

Table A.4.1.2-2 Total Inflow of Guirila Dam (1)

Year: 1967 [x1000 m3]

		Intake	Canal	Capac	ity (m	3/sec)	Runoff	Inflo	w by (Canal (apaci	У
Per	1 OQ	3	4	5	6	7	GUIRILA	3	4	5	6	.7
	1	721	721	721	721	721	90	811	811	811	811	811
MAY	. 2	1152	1152	1152	1152	1152	144	1296	1296	1296	1296	1296
hu en pe	3	554	S S 4	554	554	554 	69	623	623	623	623	623
	4	905	905	905	905	905	113	1018	1018	1018	1018	1018
JUN	S	893	893	893	893	893	111	1004	1004	1004	1004	1004
	6	1830	2036	2122	2179	2179	272	2102	2308	2394	2451	2451
	7	1852	1986	2073	2076	2076	259	2111	2245	2332	2335	2335
JUL	. 8	1521	1718	1891	2064	2182	273	1794	1991	2164	2337	2455
	9	1820	1874	1874	1874	1874	234	2054	2108	2108	2108	2108
	10	1779	1895	1892	2035	2035	254	2033	2149	2146	2289	2289
AUG	11	2592	3456	4320	5184	8008	1783	4375	5239	6103	6967	7791
	12	2851	3802	4752	5643	6392	1294	4145	5096	6046	6937	7686
	13	2395	2832	2955	3041	3128	472	2867	3304	3427	3513	3600
SEP	14	1593	3368	3678	3788	3849	480	2073	3848	4158	4268	4329
	15	2542	3100	3392	3565	3737	514	3056	3614	3906	4079	4251
	16	2592	3456	4320	5161	5938	941	3533	4397	5261	6102	6879
OCT	17	2592	3410	4096	4631	5075	945	3537	4355	5041	5576	6020
	18	2034	2042	2042	2042	2042	255	2289	2297	2297	2297	2297
	19	2294	2596	2818	2901	2901	362	2656	2958	3180	3263	3263
NOV	20	1279	1279	1279	1279	1279	160	1439	1439	1439	1439	1439
· 	21	786	786	786	786	786	98	884	884	884	884	884
	22	542	542	542	542	542	68	610	610	610	610	610
DEC	23	360	360	360	360	360	45	405	405	405	405	405
	24	355	355	355	355	355	48	403	403	403	403	403
-	25	236	235	236	236	236	30	266	266	266	266	266
JAN	26	170	170	170				191		191	191	191
	27	103	109	109	109	109	13	122	122	122	122	122
	28	129		129	129		16	145	145	145	145	145
FEB	29	99	99	99	99	99	12		111		111	
	30	73	73	73	73	73	9	82	82	82	82	82
1.	31	72	72	72	72	72	9	81	81		81	81
MAR	32		79	79	.79	79		89	89		89	
	33	86	86	86	38	86	11	97	97		97	97
	34	429	429		429	429	53 44	482	482	482	482	482
APR	35	353	353	353	353	353	44	397	397	397		397
	36	100	100			100		112		112	112	112
TOTAL		39769	47053	51707	55666	58898	9524	49293	56577	61231	65190	68422

Table A.4.1.2-2 Total Inflow of Guirila Dam (2)

n			Canal	Capaci	ty (m3	3/sec)	Runoff of	Inflo	w by (Canal (Capaci	ty
Per	100	3	4	5	6	7	GUIRILA	3	4	5	6	7
	1	289	289	289	289	289	36	325	325	325		325
MAY	2 3	725 1222	725 1222	725 1222	725 1222	725 1222	91 153	816 1375	816 1375	816 1375	816 1375	816 1375
	4	2352	2826	3162	3237	3237	404	2756	3230	3566	3641	3641
JUN	5	2592	3456	4245	5023	5735	1257	3849	4713	5502	6280	6992
	6	2592	3456	4320	5184	6048	1808	4400	5264	6128	6992	785E
	7	2592	3456	4320	5184	5979	1047	3639	4503	5367	6231	7028
JUL	8	2547	3131	3571	3833	4072	558	3105	3689	4129	4391	4630
	9 	1832	1832 	1832	1832	1832	229	2061 	2061	2061	2061	2061
	10	1794	1989	2142	2200	2200	275	2069	2264	2417	2475	2479
AUG	11	1748	1771	1771	1771	1771	221	1969.		1992	1992	1992
	12	2025	2051	2051	2051	2051	256 	2281	2307	2307	2307	2307
	13	2451	3085	3655	4172	4573	851	3302	3936	4506	5023	5424
SEP :	14	2592	3456	4320	5184	€048	1690	4282	5146	6010	6874	7738
٠.	15	2592	3456	4320	5184	6048	1757	4349	5213	6077	6941	7805
	16	2592	3456	4143	4388	4423	552	3144	4008	4695	4940	4979
OCT	17	2592	3341	3948	4553	5081	1144	3736	4485	5092	5697	6225
	18	2851	3802	4752	5693	6520	2471	5322	6273	7223	8164	8991
	19	2592	3456	4320	4930	5185	656	3248	4112	4976	5586	5841
NOV	20	2456	2842	2960	2960	2960	370	2826	3212	3330	3330	
	21	1311	1311	1311	1311	1311	164	1475	1475	1475	1475	1479
	22	829	829	829	829	829	103	932	932	932	932	932
DEC	23	540	540	540	540	540	٤7	607	4 5 4	607	607	
	24	465	465	465	465	465	58 	523	523	523	523	52 3
	25	318	318	318	318	318	40	358	358	358	358	358
JAN	26	237	237	237	237	237	30	267		267	and the second second	267
	27 	182	182	182	182	182	. 23 . 	205	205		205	205
	28	115	115	115	115	115	14	129		129	129	129
FEB	23	99		99	99	99			111	111	111	111
	30 	45 	45	45 	45	45 	6	51 	51 	. 51 	51	51
	31	60	60	60	60	60	7.				67	67
MAR	32 33	50 65	50 65	50 65	65	50 65	8 8	56 73	56 73	56 73	56 73	56 73
	<u>-</u>		90		90	90	11	101	101	101	101	101
APR	34 35	90 66	66		66		8		74			
1 12 11	36	96	96	96	96		and the second second	The second of the second of	108	108		
							16395		24061			~~~~~

Table A. 4.1.2-2 Total Inflow of Guirila Dam (3) Year : 1969 [x1000 m3]

Peri	od	Intake	Canal	Capac	11 1 1 100	3/	m of top	In Flo	ar bor C	Canal C	erecit	
1013	~~					3/sec/ 	Runoff of	111110	w by		apacio	, у .
	e i e	3	4	5	Б	7		3	4	5	6	
A	1	90	90	90	30	90	11	101	101	101	101	10
MAY	2	338	338	338	338	338	42	380	380	380	380	38
	_3 	1959	2219	2461	2548	2634	401	2360	2620	2862	2949	308
	4	2592	3456	4225	4772	5003	702	3294	4158	4927	5474	570
JUN	5	2592	3416	4091	4509	4781	645	3237	4061	4736	5154	542
	-5 	2592	3456	4320	5184	6048 	1964	4556 	5420	6284 	7148	80
	7	2592	3456	4320	5184	5048	3264	5856	6720	7584	8448	93.
JUL	8	2592	3456	4320	5067	5674	1617	4209	5073	5937	6684	72
	3	2791	3408	3803	4040	4169	522	3313	3930 	4325	4562	469
	10	2592	3456	4287	4978	5670	1592	4184	5048	5879	6570	72
	11	2592	3456	4320	5184	6048	1599	4191	5055	5919	6783	76
	12	2852	3802	4752	5660	6490	1165	4017	4967	- 5917 	6825	76
	13	2592	3456	4320	5184	6048	3201	5793	6657	7521	8385	92
BEP	14	2592	3456	4320	5184	6048	1656	4248	5112	5976	6840	77
	15	2592	3456	4320	5184	6048	2142	4734	5598	6462	7326	81
	16	2592	3456	4320	5184	6048	1348	3940	4804	5668	6532	73
DCT	17	2592	3456	4170	4714	5041	656	3248	4112	4826	5370	56
<u> </u>	18	2727	3161	3410	3583	3676	469	3196	3630	3879	4052	41
	19	1543	1543	1543	1543	1543	193	1736	1736	1736	1736	17
IOA :	20	1069	1069	1069	1069	1069	133	1202	1202	1202	1202	12
	21 	705	705	705	705	705	88	793	793	793	793	
	22	596	596	596	596	596	74	670	670	6,70	670	6
	23	518	518		518		65	583	583	583	583	5
	24	493	493	493	493	493	62	555	555	555 	555	5
!	 25	385	385	385	385	385			433	433	433	4
	26		309		309	309	39 38	348	348		348	3
	27	303		303	303	303	38	341	341	341	341	3
	28		293	293	293	293	36 35 27	329	329	329	329	. 3
		277		277		277	35	312		312	312	3
;	30	218	218	218	218	218	27	245	245	245	245	2
	31		242	242	242	242	30 23	272	272			2
1AR	32				189	189	23	212		212	212	2
	33	197	197	197	197	197	25	222	222	222	222	2
	34		187	187	187	187	23				210	2
		652				652	81		733			
·	36 	239	239	239	230	239	30	269	269	269	260	2
TOTAL		50276	62865	74602	84993	94317	24046	74322	86911	986481	.090391	.183

Table A.4.1.2-2 Total Inflow of Guirila Dam (4)

(x10.00 m3) Year: 1970

Per	iod	Intake	Canal	Capac	ity (m	3/sec)	Runoff of	Inflo	ow by (Canal (Capaci	ty
		3	4	5	5	7	and the first of t	3	4	5	6	7
	1	116	116		116	116	14	130	130	130	130	130
MAY	· 2	634 499		634 499	634 499	634 499	79 62	713 561	713 561	713 561	713 561	713 561
		- حادث مراسات			الماليات		محمو فالمراج والمحمد					
TT (A.)	4	359	359	359	359	359	45	404	404	404	404	404
JUN	5 6	736 1292	736 1292	736 1292	735 1292	736 1292	92 161	828 1453	828 1453	828 1453	828 1453	828 1458
		1500		 anka		0007	opo	1000	0150		9459	 24 do
JUL	. 7	1592	1852 3091	2049 3783	2161 4474	2247 5119	298 1186	1890 3587	2150 4277	2347 4969	2459 5660	2549 6309
JUL	8 9	2401 2852	3802	4752	5703	6653	1932	4784	5734	6684	7635	8585
	10	2592	3456	4320	5184	6048	1410	4002	4866	5730	6594	7458
AUG	11	2592	3456		and the second second	5004	1615	4207	5071	5935	6799	7619
	12	2851	3605	4213	4732	5206	1721	4572	5326	5934	6453	6927
	13	2592	3456	4320	5184	6048	1974	4566	5430	6294	7158	8022
SEP	14	2592	3456	4320	5129	5719	873	3465	4329	5193	6002	6592
	15	2592	3456	4320	5184	6048	1135	3'727	4591	5455	6319	7183
	16	2592	3456	4320	5095	5708	1065	3657	4521	5385	6160	6773
OCT	17	2510	2984	3186	3186	3186	398	2908	3382	3584	3584	3584
	18.	2437	2691	2753	2753	2753	344	2781	3035	3097	3097	3097
	- 19	1493	1493	1493	1493	1493	186	1679	1679	1679	1679	1679
AOA.	20	968	968	968	969	968	121	1089	1089	1089	1089	1085
	21 	741	741	741	741 	741	92	833	833	833	833	833
	22	469	469			469	58	527	527	527	527	
DEC	23	357	357			357	45	402	402	402	402	402
· 	24 	357	357 	357	357 	357 	45 	402	402	402	402	402
	25	254	264	254		264	33	297	297	297	297	297
JAN			237		1.1	237				267	and the second second	
	27 	252	252		252 	252 	31	283	283	the second second	283	
	28	157					20					100
FEB							17		4 7 4		152	
	30 	70	. 70 	70	70		9	79	79 	79	79	79
	31	423	-	596			77		673	100		
MAR		134			134	134	17	151	151	151	151	
	 33	88	88				11	99	99	99	99	99 -
	34			236	236			265			265	
APR		.120					15	135	135		135	
: 	.36 	62	52 	62	62 	62	8	70 	70	70	70	70
TOTAL		40394	49133	57028	64360	71130	15248	55642	64381	72276	79608	86378

40394 49133 57028 64360 71130 15248 55642 64381 72276 79608 86378

Table A.4.1.2-2 Total Inflow of Guirila Dam (5)

Year	: 19	71										
P=	riod	Intake	Canal	Capac	ity (m	3/sec>	Runoff	Inflo	ow by (Canal (Capacit	ъу
1 0	1 100	3	4	5	6	7	GUIRILA	3	4	5	6	
	1	68	68		68	68	9	77		77	77	7
MAY	2	378	378	378	378	378	47	425	425	425	425	429
	3	392	392	392	392	392	49	441	441	441	441 	441
	4	807	807	807	807		101	908	908	908	908	908
JUN	5	2097	2335	2412	2412	2412	301	2398	2636	2713	2713	2713
		1060	1060	1060	1060	1060	132	1192	1192	1192	1192	1192
	7	499	499	499	499	499	62	561	561	561	561	561
JUL	8	2234	2556	2816	3000	3172	443	2677	2999	3259	3443	3619
	9 	2041	2288	2308	2308	2308	288 	2329	2576	2596	2596 	2598
	10	2530	3221	3912	4560	5158	774	3304	3995	4686	5334	5932
AUG	11	2451	2805	2987	3100	3187	546	2997	3351	3533	3646	3733
	12	2851	3801	4640	5391 	 	2836	5687	6637	7476	8227	8919
	13	2592	3456	4320	5184	6048	1589	4181	5045	5909	6773	7637
SEP	14	2453	2936	3271	3504	3669	477	2930	3413	3748	3981	4140
	15	2535	3283	3939	4474	4906	1149	3684	4432	5088	5623	6055
· 4 .	16	2592	3456	4320	5184	6048	4048	6640	7504	8368	9232	10098
DCT	17	2592	3456	4320	5184	Б048	1554	4146	5010	5874	6738	7602
	18 	2852	3566 	4021	4378	4645 	694 	3546 	4260	4715 	5072 	5339
	19	1753	1753	1753	1753	1753	219	1972	1972	1972	1972	1972
NOV	20	1088	1088	1088	1088	1088	136	1224	1224	1224	1224	1224
~ <i>~-</i>	21	882	882	882	882 	882	110	992	992	992 	992	992
	22	600	600	600	600	600	75	675	675	675	675	679
DEC	23	468	468	468	468	468	58	526	526	526	526	526
	24 	336	336	336	336	336 	42 :	378	378 	378	378 	378
	25	and the second second		243	243		30					273
JAN	26	144			144	144		162				
	27 	129	129	129	129	129	. 16	145	145	145 	. 145	149
	28	100		100	100	100		113				113
FEB	29	76	76	76	76		9		85			
	30 		55 	55 <i>-</i>	55	55	7	62	62	62 	62 	6:
	31	52	52	52	- 52		7	: 53	59			59
MAR	32 33	68 28	68 28		68 28			77 31	77 31	77 31	77 31	71 31
												
	34	27										31
APR		28 89	28	28 89			3 11		100	- 31 100		3. 100
		03 	53 			03 		100	100	100	100	100
TOTAL	L	39190	46529	52636	58049	63054	15868	55058	62397	68504	73917	78922

Table A.4.1.2-2 Total Inflow of Guirila Dam (6) [×1000 m3] Year: 1972

Year	: 19	72									~~~~~	
Per	iod	Intake	Canal	Carac	ity (m	3/sec)	Runoff of	Inflo	w by	، بينو هناه هناه پيتو مناو بيد د د د د د د د د د د د د د د د د د د د	Capaci	
		3	4	5	6	7	GUIRILA	3	4	5	6	
· -> +- +-	1	56	56	56	 56	 56	7	63	63	63	63	69
MAY	2	488	488	488	488	488	61	549	549	549	549	545
•	3	265	265	265	265	265	33	298	298	298	298	298
	4	1763	2041	2301	2560	2819	738	2501	2779	3039	3298	3557
JUN	S	970	970		970	970	121	1091	1091	1091	1091	1031
	6		715	715	715	715	89	804	804	804	804	804
	7	341	341	341	341	341	43	384	384	384	384	384
JUL	8	317	317	317	317	31,7	4,0	357	357	357	357	
	9	2484	3030	3586	3987	4246	746	3230	3836	4332	4733	4992
	10	1176	1176	1176	1176	1176	147	1323	1323	1323	1323	1323
AUG	11	508	508		508	508	63	571	571	571	571	571
	12	1080	1253	1421	1507	1594	201	1281	1454	1622	1708	1795
	13	1252	1252	1252	1252	1252	156	1408	1408	1408	1408	1408
SEP	14	882		882	882	882	110	992	992	992	992	992
-	,15	620	620			620	77	697	697	697	697	697
	16	508	508	508	508	508	63	571	571	571	571	571
OCT	17	405	405	405	405	405	51	456	456	456	456	456
	18	278	278	278	278	278	35	313	313	313	313	313
	19	164	164	154	154	164	21	185	185	185	185	185
VON	20	433	433	433	433	433	54	487	487	487	487	487
•	21	193	193	193	193	193	24	217	217	217	217	217
	22	152	152	152	152	152	19	171	171	171	171	171
DEC	23	152	152	152	152	152	19	171	171	171	171	
	24	155	155	155	155	155	19	174	174	174	174	174
	25	128	128	128	128	128	16	144	144	144	144	144
JAN	26	106	107	. 107	107		and the second second	and the second			120	120
	27	113	113	113	113	113	14	127	127	127	127	127
	28	113	113	113	113	113	14				127	127
FEB	29	82	82	82	82			32			92	
	30	65	65	65	65	65	8	73	73	73		
	31	68	68	67	67		8	76		75	75	75
MAR	32				A CONTRACTOR OF THE PARTY OF TH	58			€5		65	bb
	33	57	57	57	57	57	7 .	64	64	64	64 	
	34	68	68	68	68	68		77	77		1.15	77
APR	35		83		83				93			93
	36	82	82	82	82	82	10	92	92	92	92	92
TOTAL		16380	17438	18361	19107	19712	3063	19443	20501	21424	22170	22779

Table A.4.1.2-2 Total Inflow of Guirila Dam (7)

Table A.4.1.2-2 Total Introv of Cartagorian (1973)
Year : 1973

Per	iod	Intake	Canal	Capac	ity (m	3/sec)	Runoff of	Inflo	ow by C	Canal (Capacit	У
1 61		3	4	5	6	7	GUIRILA	3	4	5	6	
	1	99	99	99		99	12	111	111	111	111	11
MAY	2 3	116 116	116 830	116 830	116 830	116 830	15 104	131 934	131 934	131 934	131 934	13 93
عد سرمد پس سخ	 4	627	627	627	627	627	78	705	705	705	705	70
JUN	5 6	2351 2592	3042 3456	3733 4320	4424 5131	5115 5743	866 1170	3217 3762	3908 4626	4599 5490	5290 6301	598 691
	 .7	2519		3632	4021	4243	538	3057	3705	4170	4559	478
JUL	8	1767	1853	1940	2026	2113	275	2042	2128	2215	2301	238
	9	2852	3802	4733	5485 	6082	865	3717	4667 	5598	6350	694
	10	2532	3456	4320	5012	5498	745 1583	3337 4175	4201 5039	5065 5903	5757 6767	624 748
AUG	11 12	2592 2851	3456 3802	4320 4718	5184 5522	6300 2900	2319	5170	6121	7037	7841	861
	13	2592	3456	4011	4929	5465	1133	3725	4589	5144	6062	659
SEP	14 15	2592 2592	3456 3456	4315 4272	4980 5049	5270 5827	687 1313	3279 3905	4143 4769	5003 5585	5667 6362	599 714
	 16	2592	3456	4320	5184	6048	1751	4343	5207	6071	- 69 3 5	779
OCT	17	2592	3456	4320	5184	6048	2701	5293	6157	7021	7885	874
	18	2851	3802	4752 	5643 	6474	1358 	4209	5160	6110 	7001 -	783
	19	2592	3290	3589	3600	3600	450	3042	3740	4039	4050	405
VOV	20 21	1469 1241	1469 1241	1469 1241	1469 1241	1469 1241	184 155	1653 1396	1653 1336	1653 1396	1653 1396	169 139
	22	700	700	700	700	700	 88	788	 788	788	 788	78
DEC	23	492	492	492	492	492	62	554	554	554	554	55
	24	383	383	383	383	383	48	431	431	431	431	43
	25	348		348	348	348	43	391	391	391	391	39
JAN	26 27	283 269	283 269	283 269	283 269	283 269		318 303	318 303	318 303	318 303	30
,	 28	168	168	168	168	 168	21	189	- 189	189	189	18
FEB	- 7				149	149	19		168			16
	30	85	85	85	85	85	11	96	96	96	96 	
war.	31	258	258	258	258	258	the second second second	290		290		29
MAR	32 33	257 95		257 95	257 95	257 95	32 12	289 107	289 107	289 107	289 107	28 10
	34	52	52	52	52	.52	6	58	58	58	 58	
APR	35		and the second second	58		58	7	65 51	65		65	9
	36	45	~ 				6		51	5 1	51 	·
TOTAL		46543	58430	.69320	79398	87750	18758	65301	.77188	88078	981561	.065

Table A.4.1.2-2 Total Inflow of Guirila Dam (8)

Year: 1974 (x1000 m3)

Per.	i del	Intake	Cana I	Capaci	ity (m	3/sec}	Runoff of	Inflo	ow by (Canal C	apacı	
rei	100	3	4		6	7	GUIRILA	3	4	5	6	منو ومه سنة متر ي
	1	106	106	106	106	106	13	119	119	119	119	11
MAY	2	293 2373	293 2938	292 3456	292 3975	292 4493	36 920	329 3293	329 3858	328 4376	328 4895	32 54):
- وند وخد همه جنو پي	4	2588	3279	3758	4045	4218	576	3164	3855	4334	4621	479
JUN	5	2592	3438	4215	4994	5771	1434	4026	4872	5650	6428	720
	6	2592	3456	4320	5184	6048	1581	4173	5037	5901	6765	762
	7	2592	3452	4190	4736	5192	775	3367	4227	4965	5511	596
JUL	8	2592	3279	3883	4310	4576	661	3253	3940 2612	4544 2612	4971 2612	523 261
	9	2260	2322	2322 	2322	2322 	290	2550 		2012	2012	201
1.	10	952	952	952	952	952	119	1071	1071	1071	1071	107
AUG	11	797	797	797	797	797	99	896	896	896	The second second	89
	12	1189	1189	1189	1189	1189	149	1338	1338	1338	1338	133
	13	1500	1759	2018	2208	2294	314	1814	2073	2332	2522	260
SEP	14	2519	3101	3585	3942	4129	899	3418	4000	4484	4841	
·.	15	2592	3456	4320	5184	6048	1602	4194	5058	5922	6786	769
	16	2494	3031	3406	3655	3802	486	2980	3517		4141	428
CT	17	1477	1477	1477	1477	1477	184	1661	1661	1661	1661	16
	18	967	967	967	967 	967 	121	1088	1088	1088	1088	108
	19	601	601	601	601	601	75	676	676	676	676	e.
40A	20	369	369	369	369	369		415	415	415	415	4
	21	300	300	300	300	300	·38	338	338	338	338 	3;
	22	283	283	283	283	283	35	318	318	318	318	3.
DEC	23	215	215	215	215	215	27	242	242	242	242	2
	24	197	197	197	197	197	24	221	221	221 	221	2:
	25	119	119	119	119	119	15	134	134	134	134	1
JAN	26	76	76	76	76	76	10	88	86	86	86	1
	27 	59	59	59 	59	59 	7	66 	66	56 	66	
	28	54	54	54	54	54	7	61	61	61	61	. 1
FEB	29	32	32	32	32		4	36	36	36		;
	30	27	27	27 	27	27 	3	30	30	30 	30	
	31	36	36	36	36		5	41	41	41	41	
MAR	32 33	36 31		36 31	31 36		4 4	40 35	40 35	40 35	40 35	;
	34	28	 28	 28	 28	 28	з	31	31	31	 31	
APR	35	24	24	24	24	24	3	27	27		27	
	36	31	31	31	31	31	4	35	35	35		
TOTAL		3/1993	41810	 47779	52853	 57191	10573	45566	52383	58345	63426	 677(

4330 41010 47772 32030 37131 10370 10333 32000 33013 30133 3713

Table A.4.1.2-2 Total Inflow of Guirila Dam (9)

rear	. 13	:/a 								_ ,		
Pen	riod	Intake	Canal	Capac	ity (m	3/sec)	Runoff of	Inflo	ow by (Canal (Capaci	
		3	. 4	5	6	7	GUIRILA	3	4	5	6	7
، مه مجند پي ب	1	54	54	-54	54	54	7	61	61		61	61
MAY	2	97	• 97	97	97	97	12	109	109	109	109	109
	3	413	413	413	413	413	52	465	465	465	465	465
	4	278	278	278	278	278	35	313	313	313	313	313
JUN	5	260	260	the state of the state of	260	260		293	293	293	293	293
	6	212	212	212	212	212	26	238	238	238	238	238
	7	45	45	45	45	45	362	407	407	407	407	407
JUL	8	180	180	180	180		22	202	202	202	202	202
	9	454	454	454	454	454	57	511	511	511	511	511
	10	628	628	628	628	528	79	707	707	707	707	707
AUG	11	764	764	764	764	764	95	859	859	859	859	, 859
	12	2085	2276	2405	2491	2577	331	2416	2607	2736	2822	2908
	13	2592	3456	4266	4908	5426	1101	3693	4557	5367	6009	6527
SEP	14	2592	3456	4239	5017	5791	1805	4397	5261	6044	6822	7596
	15	2592	3373	4045	4606	5125	958	3550	4331	5003	5564	6083
	16	2592	3371	4148	4927	5673	1393	3985	4764	5541	6320	7066
OCT	17	2592	3456	4320	5184	6013	1231	3823	4687	5551	6415	7244
	18	2785	3576	4079	4451	4781	878	3663	4454	4957	5329	5659
1.	19	2593	3404	3932	4332	4634	700	3293	4104	4632	5032	5334
NOV	20	1964	2254	2455	2455	2455	307	2271	2561	2762	2762	2762
> 	21	796	796	796	796	796	99	895	895	895	895	895
	22	622	629	629	629	629	79	701	708	708	708	708
DEC	23	233	233	233	233	233	29	262	262	262	262	
	24	269	259	269	269	269	34	303	303	303	303	303
	25	145	145	145	145	145	18	163	163	163	163	163
JAN		108			108		13	121			121	121
	27	68		68		 	8	76	76	76	76	76
•	28	78		78	78	78	10		88	. 88	88	88
		97					12	109				
	30	89	89	89 		89	11	100	100	100	100	100
		68		68	68	68	9	77	77	77	77	77
MAR		62				62	8	70	70	70	70	70
	33	54		54			7	61	. 61	-51	61	18
	34	364	424	424	424	424	53	417	477			
APR					184	184	23	207		207		
	36	284	284	284	284	284	35	319	319	319	319	319
TOTAL	4 .	29293	35595	40862	45344	49448	9932	39225	45527	50794	55276	59380

Table A.4.1.2-2 Total Inflow of Guirila Dam (10)

		The second second				and the second s	
	1000	the second second			the second secon		(×1000 m3)
Yes	ar · 1976		and the second second				
100				and the second second	and the second s		

		1976		والمتكون للفاصلة					و حد بناو بناو حو می و			
Desa	امما	Intake	Canal	Сарас	ity (m	3/sec)	Runoff	Inflo	ow by (Canal (Capaci	5 y
Per	100	3	4	5	6	7		3	4	5	6	
	1	312	312	312	312	312	39	351	351	351	351	35
MAY	2	541	541	541	541	541	67	€08	608	608		60
	3	655	655	655	655	655	82	737	737	737	737	73
	4	1512	1858	2185	2445	2704	562	2074	2420	2747	3007	326
JUN	5	2592	3456	4221	4908	5443	1116	1.00	4572	5337		659
	6	2592	3456	4320	5184	6048	1772	4364	5228	6092	6956	782
	7	2592	3456	4320	5184	6048	1679	4271	5135	5999	6863	772
JUL	8	2413	2850	3091	3210	3296	417	2830		3508	3627	371
	9	1149	1149	1149	1149	1149	143	1292	1292	1292	1292	129
	10	542	542	542	542	542	68	610	610	610	610	6.
AUG	11	823	823	823	823	823	103	926	926	926	926	
	12	977	1002	1002	1002	1002	125	1102	1127	1127	1127	115
	13	1906	2213	2386	2559	2731	386	2292	2599	2772	2945	31
3EP	14	1252	1252	1252	1252	1252	156	1408	1408	1408		14
	15	1394	1480	1480	1480	1480	185	1579	1665	1665	1665	: 160
	16	2592	3422	4199	4942	5602	996	3588	4418	5195	5938	65
CT	17	2144	2403	2579	2676	2721	340	2484	2743	2919	3016	30
	18	1041	1041	1041	1041	1041	130	1171	1171	1171	1171	11
	19	-593	593	593	593	593	74	667	667	667	667	66
VOV	20	543	543	543	543	543	68	611	611	611	611	6.
· 	21	464	464	464	464	464	58	522	522	522	522 	5:
	22	334	334	334	334	334	42	376	376	376	376	3
DEC	23	281	281	281	281	281	35	316	316	316	316	
	24	284	284	284	284	284	35	319	319	319	319	3.
	25	190	190	190	130	190	24	214	214	214	214	2
TAN	26	183	183	183	- 2	183		206		206	_	2
	27	220	220	4.7	220	220		247				
	28	179	179	179	179	179	* * *	201	201	201	201	2
EB	29	166				166	21			-	187	
	30			122	122	122	15	137	137			1:
	31	150	150		150	150	19	169	169	169	169	
1AR	32		144				18		162	152		
	33	194		194		194	24	218	100	218	218	2.
	34	111	111	111	111	111	14	125	125	125		1
\PR		455	542	614	614	614	77	532	619	691	691	6
		183		183	183	183	23	206	206	206	206	21
								~ ~ ~ ~ ~				

Table A.4.1.2-2 Total Inflow of Guirila Dam (11)

[x1000 m31 Year: 1977 the state and st Intake Canal Capacity (m3/sec) Runoff Inflow by Canal Capacity ---- of Period -----. .7 7 GUIRILA 162 162 MAY 2. 1318. JUN 2940 3112 -----_____ 538. JUL AUG 1072 1167 SEP 2425 3105 OCT NOV 21. DEC JAN .177 FEB MAR. APR . 7 18348 20175 21550 22664 23614 21887 23714 25089 26203 27153 TOTAL

Table A.4.1.2-2 Total Inflow of Guirila Dam (12)

(×1000 m3)

Year	: 19	378						g 450 464 504 644 \$64 468 8	نية بدر بيد يكر يسر بـــ		1 X 1 U	oo mal
Par	iod	Intake	Canal	Capac	ity (m	3/sec}	Runoff of	Inflo	w by	Canal	Capaci	ty
101		3	4	5	6	7	GUIRILA	3	4	5	6	
	1	38	38	38	38	38	5	43	43	43	43	43
MAY	. 2	39	39	39	39	39	5	44	44	4 44	44	44
	3	499	499	499	499	499	62	561	561	561	561	561
	4	570	570	570	570	570	71	641	641	641	641	641
JUN	5	557	557	557	557	557	70	627	627	627	627	627
	6	862	937	937	937	937	117	979	1054	1054	1054	1054
	7	1530	1576	1576	1576	1576	197	1727	1773	1773	1773	1773
JUL	. 8	2188		2885	3175	3426	544	2732	3083	3429	3719	3970
	9	2648	3064	3336	3509	3653	472	3120	3536	3808	3981	4125
. :	10		1051	1051		1051	131	1182	1182	1182	1182	1182
AUG	11	843	843	843	843	843	105	948	948	948	948	948
	12	1041	1217	1390	1507	1594	612	1653	1829	2002	2119	2208
	13	2592	3456	4320	5184	5961	1272	3864	4728	5592	6456	7233
SEP	1,4	2592	3415	4095	4471	4699	688	3280	4103	4783	5159	538
	15	2592	3456	4320	5038	5680	1350	3952	4816	5680	6398	7040
	16	2592	3456	4320	5073	5756	1135	3727	4591	5455	6208	6891
OCT	17	2592	3456	4320	5110	5791	1048	3640	4504	5368	6158	6833
	18	2669	3007	3162	3175	3175	396	3065	3403	3558	3571	3571
	19	2094	2094		2094	2094	the state of the s	2356	2356	2356	2356	2350
NOV	20	1963	1963	1953	1963	1963	245	2208	2208	2208	2208	2208
	21 	1718	1718	1718	1718	1718	214	1932	1932	1932	1932	1932
	22	1747	1747	1747		The second second	218	1965	1965	1965	1965	1969
DEC	23	1522	1522	1522	1522	1522	190	1712	1712	1712	1712	1712
	24 	1298	1298	1298	1298	1298	162	1460	1460	1460 	1460	1450
	25	389	989	989	389	989	123	1112	1112	1112	1112	1112
JAN	26	731	731	731		731	91	822	822	822	822	822
	27 	676	676	675	676	676	85	761	751	761	761	761
	28	557	557	557	557	557	70	627	627		627	627
FEB	29	557	557		557		70		€27		627	627
	30	427	427	427	427	427	53	480	480	480	480	480
	31	509	509	509	509	509	64	573	573		573	573
MAR	32	509	509		509	509		573			and the second second	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
	33	551	551	551 	551	551 	69	620 	620	620	620	620
	34	461	461	461	461	461	58	519	519	519	519	519
APR	35	461		461	461	461		519	519	and the second second		
	36	428	428	428	428	428	53	481	481	481	481	481
rotal		44693	50374	55456	59550	53043	10439	55132	60813	65895	69989	73482

Table A.4.1.2-2 Total Inflow of Guirila Dam (13)

Year: 1979 [x1000 m3]

Pα	riod	Intake	Canal	Сарас	ity (m	3/sec)	Runoff of	Inflo	w by (anal (Capacit	,у
. G	ir rou	3	4	S	. 6	7 .	GUIRILA	3	4	5	6	
	1	530	530	530	530	530	66	596	596	596	596	59
MAY	2	1370	1,434	1434	1434	1434	180	1550	1614	1614	1614	1614
	3	421	421	421	421	421	52	473	473	473	473	47:
	4	528	528	528	528	528	66	594	594	594	594	59
JUN	5	1519	1634	1634	1634	1634	204	1723	1838	1838	1838	183
	6	360	360	360	360	360	449	809	809	809	809	80
	7	2592	3456	4320	5184	1.5	1209	3801	4665	5529	6393	725
JUL	8	2483	2884	3106	3279	3423	434	2917	3318	3540	3713	385
	9	2624	3071	3341	3476	3562 	449	3073	3520	3790	3925	401
	10	1902	2207	2413	2548	2634		2296	2601	2807	2942	302
AUG	1.1	1098	1271	1443	1616	1789	629	1727	1900	2072	2245	241
- 24 - 20	12	2851	3802	4752	5702	6653	2134	4985	5936	6886	7836 	878
	13	2592	3456	4320	5184	6048	1466	4058	4922	5786	6650	751
SEP	14	2592	3456	4320	5184	6048	1833	4425	5289	6153	7017	788
	15	2592	3389	4027	4557	4981	700	3292	4089	4727	5257	568
e i p	16	2199	2324	2410	2496	2554	319	2518	2643	2729	2815	287
OCT	17	2592	3375	3962	4461	4893	757	3349	4132	4719	5218	565
	18	2600	3071	3380	3638	3811	671	3271	3742	4,051	4309	448
	19	1296	1382	1468	1555	1573	196	1492	1578	1664	1751	176
NOV	20	634	634	634	534	634	79	713	713	713	713	71
	21	473	473	473	473	473 	59 	532 	-532	532 	532 	53
	22	373	373	373	373	373	47	420	420	420	420	42
DEC	23	233	293	293	293	293	36	329	329	329	329	32
	24	245	245	245	245	245	31	276	276 	276	276 	27
	25		173		179		22				201	20
JAN	26	149			149				168		168	18
	27	154	154	154	154	154	19	173	173	173	173 	17
	28	105			105	105	13					
	29	95		95			12		107		107	
	30		66 	66 	66 	66 	8	74	· 74	74 	74 	7
	31	. 58			58	58	7.	65				6
	32	. 64		64		64		72		72		
	33	83	83	83	83	83 -	10	93	93	93	93	9
	34						18			159		15
	35						21	185	and the second second			
	36	140	140	140	140	140	18	158	158	158	158	15
TOTA	L.	38157	45467	51585	57203	62340	12635	50792	58102	64220	69838	7497

Table A.4.1.2-2 Total Inflow of Guirila Dam (14)

Year : 1980

[x1000 m3]

Per	iod	Intake	Canal	Capac	ity (m	3/sec)	Runoff of	Infl	ow by	Canal (Capaci	ty
		3	4	5	6	7	GUIRILA	3	4	5	6	
	1	115	115	115		2	14	129	129			and the second
MAY	2	130	130	130	130		16	146	146	146	146	
 . .	3	690	690	690	690	690	86	776	776	776	776	778
	4	578	578	578	578	578	72	650	650	650	650	650
JUN	-5	3539	4316	5094	5872		114	3653	4430	5208	5986	6734
	- 6 	2585	3337	4007	4611	5188	1223	3808	4560	5230	5834	6411
	7	1287	1287	1287	1287		161	1448	1448		1448	1448
JUL	8	1117	1117	1117	1117		139	1256	1256	1256	1256	1256
	9.	2790	3568	4345	5122	5813	1356	4146	4924	5701	6478	7169
	10	2532	3456	4320	5128	5906	1299	3891	4755	5619	6427	7205
AUG	11	2592	3092	3332	3466	3466	433	3025	3525	3765	3899	3899
	12	2803	3447	3878	4186	4376	598	3401	4045	4476	4784	4974
	13	2592	3429	4085	4634	5104	841	3433	4270	4926	5475	5945
SEP	14	2592	3456	4283	5061	5839	1378	3970	4834	5661	6439	7217
	15	2592	3456	4320	5184	5951	885	3477	4341	5205	6069	6836
	16	2592	3295	3810	4186	4328	547	3139	3842	4357	4733	4875
OCT	17	2002	2002	2002	2002	2002	250	2252	2252	2252	2252	2252
	18 	1492	1492	1492	1492	1492	186	1678	1678	1678	1678	1678
	19	1032	1032	1032	1032	1032	129	1161	1161	1161	1161	1161
VOV	20	992	992	992	992	992	124	1116	1116	1116	1116	1116
	21 	1004	1004	1004	1004	1004	125	1129	1129	1129	1129	1129
	22	713	713	713	713	713	89	802	802	802	802	802
DEC	23	615	615	615	615	615	77	692	692	692	692	692
	24	660	560	660	660	660	82	742	742	742	742	742
	25	500	500	500	500	500	62	562	562	562	562	562
JAN		423		423			53	476		476	4.4	
	27 	404	404	404	404	404 	50	454	100	454		454
	28	357	357	357		357	45	402		402	402	402
FEB	29	331	331	331	331	331	41		372			
	30	246	246	246	246		31	277		277 	277	277
	31	292		232	232		36	328	328		328	
MAR	32		371	371	371	371	46	417		417		
	-33	321	321	321	321	321	40	361	361	361	361	361
	34	236	236	and the same	236		30		266	266		* .
APR	35	264	264	264		264	and the second s	297		297		
	36 	339		339		339 	42	381		381	381	381
TOTAL		43780				69102	10733	44.7			74694	79835

Table A.4.1.2-2 Total Inflow of Guirila Dam (15)

Per	i od		Canal	Capac	ity (m	3/sec)	Runoff	Inflo	w by C	Canal C	apacit	,У
		3	4	5	6	7	GUIRILA	3	4	5	6	7
	1	311	311	311	311	311	39	350	350	350	350	350
YAM	2	275 537	275 537	275 537	275 537	275 537	34 67	309 604	309 604	309 604	309 604	309 604
				 444	444	444	 56	500	500	500	500	500
TITLE	4 5	444 865	444 865	865		865	108	973	973	973	973	973
JUN	6	2503	2727	2855		2895	361	2864	3088	3216	3256	3256
	 7	2378	2995	3540	3994	4367	700	3078	3695	4240	4694	5067
JUL	8	2592	3659		4589	4897	756	3348	4415	4808	5345	5653
	9	2852	3755	4383	4672	4768	600	3452	4355	4983	5272	5368
	10	2151	2454	2492	2492	2432	311	2462	2765	2803	2803	2803
AUG	11	2486	3154	3752	4270	4681	689	3175	3843	4441	4959	5370
	12	2593	3038	3288	3339	3455	431	3024	3463	3719	3830	3886
	13	2515	3000	3228	3401	3563	488	3003	3488	3716	3889	4051
SEP	14	2586	3258	3769	4072	4331	713	3299	3971	4482	4785	5044
	15	2592	3456	4118	4636	5154	1256	3848	4712	5374 	5892 	6410
	15	1263	1263	1263	1263	1263	158	1421	1421	1421	1421	1421
CT	17	711	711	711	711	711	89	800	800	800	800	800
	18 	1534	1653	1653	1653	1653	206	1740 	1859	1859	1859	1859
	19	2430	2531	2531	2531	2531	316	2746	2847	2847	2847	2847
VOV	20	1920	1920	1920	1920	1920	240	2160	2160	2160	2160	2160
	21	1525	1525	1525	1525	1525	191	1716	1716	1716	1716	1716
	22	1316	1316	1316	1316	1316	164	1480	1480	1480	1480	1480
DEC	23	1123	1123	1123	1123	1123	140	1263	1263	1263	1263	1263
	24 	1335	1335	1335 	1335	1335 	167	1502 	1502 	1502	1502	1502
	25	1033	1033	1033	1033	1033	129	1162	1162		1152	1162
JAN	28	809	809	809	809		101	910	910	910	910 889	910
	27 	790	790	790	790	790	99	889 	889	889 	885	889
	28	641	641	641	641		80	721	721	721	721	721
FEB	29	629	629	629		629	78	707		707	707	707
	30	503	503	503	503	503	. 63	566 	566 	566 	566	566
	31	629	629	629	629	629	78	707	707	707	707	707
MAR	32	560	560	560	560	560	70	630	630	630	630	630
		565 	565	565	56S	565 	71	636 	636 	636 	636 	636
A DIS	34	493	493	433	433	493	62	555	555	555	555	555
APR	35 36	514 514	514 514	514 514	514 514	514 514	64 64	578 578	578 578	578 578	578 578	578 578
						~						
TOTAL		48517	54985	58966	61909	64092	9239	57756	64224	68205	71148	73331

(2) Probability of Guirila Dam Inflow

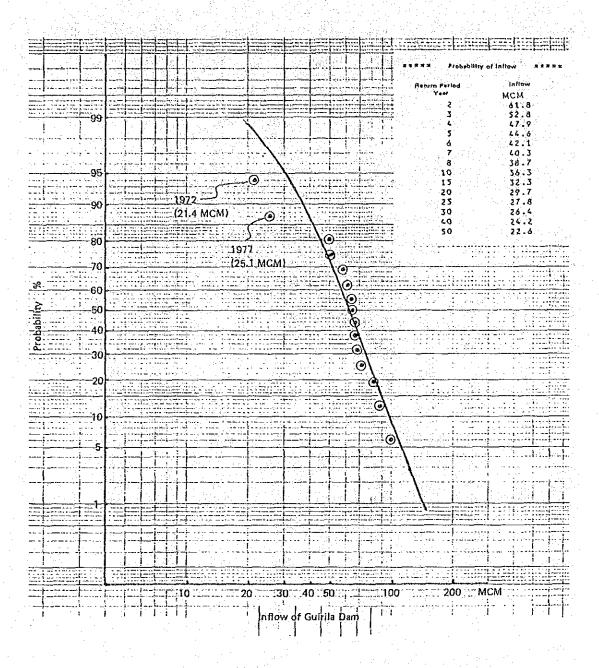


Fig. A.4.1.2-1 Probability of Inflow

Table A.4.1.2-3 Probability of Guirila Dam Inflow by Iwai's Method

						e Set											
Return	59.9	35.6	3.5	3.4	2.3	2.0	1.9	1.7	1.6	ب	9.	2.5	1,2		н н		. 1 .
X**2	457.96	630.01	2500.00	2580.64	3398.89	3745.44	4070.44	4342.81	4651.24	4692.25	4719.69	5227.29	6889.00	7761.61	9721.96	65389.23	4359.28
Hazen Plot (%)	29.96	00.06	83,33	76.67	70.00	63,33	56.67	50.00	43.33	36.67	30.00	23.33	16.67	10.00	3,33		
Thomas Plot (%)	93.75	87.50	81.25	75.00	68.75	62.50	56.25	50.00	43.75	37.50	31.25	25.00	18.75	12.50	6.25		
(LOG-(X+B))**2	4,65846	4.70615	5.00430	4.01329	5.09598	5.12721	5.15487	5.17699	5.20099	5.20410	5.20617	5.24319	5.35003	5.39937	5.49797	77.03905	5.13594
TOG-(X+B)	2,15835	2,16937	2,23703	2,23904	2.25743	2,26433	2.27043	2.27530	2,28057	2.28125	2.28170	2.28980	2,31301	2,32365	2.34478	33.98604	2.26574
X+B	144.0	147.7	172.6	173.4	180.9	183.8	186.4	188.5	190.8	191.1	191.3	194.9	205.6	210.7	221.2		
X-901	1,33041	1,39967	1.69897	1.70586	1.76567	1.78675	1.80482	1.81889	1.83378	1.83569	1.83696	1.85914	1.91908	1.94498	1.99388	26,53455	1,76897
×	21.4	25.1	50.0	50.8	58.3	61.2	63.8	6.59	68.2	68.5	68.7	72.3	83.0	88 1	98.6	943.9	62.9
Year	1972	1977	1976	1975	1974	1967	1979	1978	1981	1971	1980	1970	1968	1973	1969		
Order	p-4	2	ന	4	Ŋ	9	7	∞	6	10	ᆏ	12	13	14	15	Total	1/N

(3) Water Balance Calculation

Table A.4.1.2-4 Summary Water Balance Calculation by Developed Area [x1000 m31

-	n gyfrag ag plate tri trama skynny ar staffin far sy'r i				the state of the s	egypenya kanantari ara da kanantari ara kanantari ara kanantari ara kanantari ara kanantari ara kanantari ara k	
	·	Drivic	ig Can	al Car	расі бу І		
	Year	3 m3/sec	4 m3/sec	S m3/sec	6 m3/sec	7 m3/sec	
~	1967	31468	31468	31468	31468	31468	
2	1968	30623	30623	30623	30623	30623	
1	1969	30995	30995	30995	31004	30995	
~	1970	32865	32692	32692	32673	32673	
4800	1971	33551	33551	33551	33551	33551	
3	1972	39836	39835	39836	39836	39836	
1	1973	31255	31255	31255	31255	31255	
3	1974	37690	37690	37691	37691	37691	
9	1975	32515	32448	32448	32448	32448	
7	1976	34636	34549	34477	34477	34477	
ĝ	1977	38478	38478	38478	38478	38478	
E	1978	21754	21754	21754	21754	21754	to the second
9	1979	34486	34400	34314	34227	34209	
IPRIGATION AREA:	1980	30431	30432	30431	30431	30431	
	1981	21479	21479	21479	21479	21479	
		21-110	31,775				
	Year	3 m3/sec	4 m3/sec	S m3/sec	6 m3/sec	7 m3/sec	
~	1967	27363	27963	27963	27963	27963	
		27240	27240	27240	27240	27240	
2	1968	27157	27157	27157	27166	27157	
-	1969	29077	28904	28304	28885	28885	
4350	1970	23667	29667	29667	29667	29667	
ရှိ မ	1971	35649	35648	35649	35643	35649	
1.	1972	27632	27632	27632	27632	27632	
1 3 1	1973	33823	33823	33824	33824	33824	
E)	1974	23052	28985	28985	28985	28985	
₹	1975	30848	30761	30689	30689	30689	
Z	1976	34295	34295	34295	34295	34295	
ĕ	1977	18606	18606	18606	18606	18606	
) <u>{</u>	1978	30683	30597	30511	30424	30406	
1 2	1979		26594	26593	26593	26593	2
IRRIGATION AREA:	1980	26593	17360	17960	17960	17960	
	1981	17360	1/300	11300	1,200		
	Year	3 m3/sec	4 m3/sec	5 m3/sec	6 m3/sec	7 m3/sec	
	1001						
~	1967	25237	25237	25237	25237	25237	
Ę	1968	24609	24609	24609	24509	24609	
<u> </u>	1969	24172	24172	24172	24181	24172	
	1970	26131	25958	25358	25933	25939	•
4000	1971	26738	26738	26738	26738	26738	
4	1372	32396	32395	32396	32396	32396	;
	1973	24814	24814	24814	24814	24814	
AREA:	1374	30838	30838	30839	30839	30839	
翼	1975	26381	26314	26314	26314	26314	
-	1976	27902	27815	27743	27743	27743	
IRRIGATION	1977	31077	31077	31077	31077	31077	
Ę	1978	16226	16226	16226	16226	16226	
છ	1979	27737	27651	27565	27478	27460	
띮	1980	23608	23609	23608	23608	23608	
当	1881	15325	15325	15325	15325	15325	
1	• • • • • • • • • • • • • • • • • • • •					•	L

Note:

 $V = \sum_{i=1}^{\Sigma} (Qin - Qout)$

where; V; Reservoir Storage

Qin; Inflow of Dam

Qout; Release from Dam and Loss.